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2 inputs per channel with independent mixing (ability to mix 4 inputs into one channel on stereo machine).
Signal level meter for each channel operative on playback as well as record.
Tape/original switching through to output stages.
Re-record facility on stereo models for multiplay, echo effects etc, without external connections.
Meters switchable to read 100 kHz bias and erase supply with accessible preset adjustment. Three outputs per channel i.e. (1) line outlevel responise. (2) line out-after tone controls. (3) power output-8-15 ohms.

Power output 10W per channel.
Independent tone controls giving full lift and cut to both bass and treble each channel.
Retractable carrying handle permitting carrying by one or two persons.

U.K. Retail prices from $£ 175$ incl. P.T.


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## Some notes on Bridge Measurement by WAYNE KERR

## Number 4

## The Electric Field

The first three issues of these notes have described the basic principles of the Transformer Ratio Arm Bridge and have shown how high impedance components, such as small capacitors, can be accurately measured at the end of very long lengths of screened cable. The use of the bridge neutral connection enables the capacitance of the connecting cables to be isolated from the component being measured, the balance point of the bridge being unaffected by the presence of the screened cables. In this issue the use of the neutral connection to control the electric field surrounding an electrode forming part of a parallel plate or coaxial capacitor is described.


Figure 1

If a parallel plate capacitor is drawn, together with the associated electrostatic field, it will be apparent that the measured capacitance of this arrangement can be considered as the sum of two components; $\left({ }_{C}\right)$, the value for the centre part of the field in which the lines of force are linear, and $\left(C_{F}\right)$, the value for the non-linear fringe field. Figure 1 illustrates these fields.

The electrical value for such a capacitor is exceedingly difficult to calculate, owing to the complicated nature of the fringe field, and so it has become common practice to use plates which are large in diameter and also placed closely together, in order to reduce to a minimum the effect of the fringe field. Furthermore, a difficulty arises in the determination of the permittivity of a substance comprising the dielectric. This is a simple ratio of the capacitance of the plates with the material placed between them to the capacitance of the plates in free space. In theory, an infinitely large disc of material would be necessary in order to carry out such a measurement and avoid errors due to lines of force in the fringe field traversing the edge of the disc.

The transformer ratio arm bridge offers a practical solution to these difficulties and Figure 2 shows how these errors can be eliminated by the use of the bridge neutral connection.

The right hand circular electrode is surrounded by an annular guard ring and is separated from it by a thin ring of insulating material.

When the system is balanced, both the central electrode and the guard ring are at the same potential and the bridge will only measure the capacitance formed by the central part of the field ( $\mathrm{C}_{\mathrm{B}}$ ).

Further consideration of this arrangement shows that the thickness of the insulation in the annular gap becomes a limiting factor in the accuracy of the measurement-a wide gap would start to produce locally curved lines of force proportional to the width of the insulation. Fortunately, a technique developed recently enables an insulating layer to be produced only a few microns thick substantially removing this difficulty.

So far, the discussion of the transformer ratio arm bridge and its application to capacitance measurement has neglected a fundamental necessity, the creation of a precise standard of capacitance. The techniques already described can be used to design a basic standard, dependent only on the determination of the exact mechanical dimensions and the velocity of light for its achievement.


Figure 2
The ability to measure the capacitance between two electrodes precisely without correction being necessary for the effect of the fringe field creates new possibilities in metrology as well as electronics. Bridges can be constructed to measure reciprocal capacitance, and as the distance between linearfield electrodes varies as $1 / C$, a voltage output can be given from the bridge directly proportional to this distance.

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Electronics, Television, Radio, Audio

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Electronies in civil aviation


This month's cover symbolizes the report on electronics in civil aviation which will be found on p. 511.

## OUR NEXT ISSUE

Pickup Survey-a critical review of the various types of transducer available. A Thermistor Hygrometer using a single i.c. operational amplifier is described.
Review of the London Audio Fair.

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Volume 75 Number 1409
Number 1409


## How we set the trend in plastic film capacitors

Ten years ago, Mullard introduced the C296 series of plastic film capacitors to replace the paper components then used exclusively in consumer applications in the UK. The film used is polyethylene-terephalate generically known as polyester. This revolutionary film transformed the British capacitor market. It enabled Mullard to reduce component size by as much as $15 \%$ compared with paper types. Working voltages were up to 400 V d.c. Insulation resistances greater than $50,000 \mathrm{M} \Omega$ at $20^{\circ} \mathrm{C}$ were achieved for the first time in commercial quantities. The polyester film itself was nonhygroscopic and chemically inert. It was wound with aluminium using an extended foil technique to give minimal self-inductance. And the finished capacitors were encapsulated in hard, water repellent lacquer, which was unaffected by temperatures up to $150^{\circ} \mathrm{C}$.

New techniques New manufacturing techniques were then introduced in plastic film capacitors, which allowed a metallised layer to be deposited on the film. This reduced our capacitor
sizes by up to a further $50 \%$. About this time, the general acceptance of printed circuits created a strong demand for various components in different shapes, with particular dimensions to close tolerances. And because we at Mullard anticipated this trend we now produce the C280 miniature metallised film capacitors. These small devices have radial terminations in the standard 1.E.C. $0 \cdot 1$ inch grid spacing, making them the economic answer to the problems of improving packing densities and reducing assembly production times. Due to their distinctive colour coding, small size and wide capacitance range the demand for these capacitors is far in advance of all others. The 400 V units have a more recent polyester film (polycarbonate) which reduces losses at frequencies of 20 kHz and above. This also applies to the C281 series with their axial leads and moulded encapsulation.

Development Work of course continues, and encouraging results are being achieved with capacitors for a.c. power handling, for example for interference suppression and power factor correction, using polypropylene films.

Higher demand The demand for discrete passive components has increased enormously during the last ten years. And today there is a
continual demand for polyester capacitors in the range $0.00{ }_{\mu} \mathrm{F}$ to $10_{\mu} \mathrm{F}$ for most applications in the domestic field.

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## Wireless World

## Domestic Broadcasting

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It is now 20 years since the Copenhagen Plan for medium- and long-wave broadcasting in Europe was implemented and the present chaotic state in the medium-wave band beggars description.

There are those who consider that the situation in the medium-wave band is beyond redemption and that only a v.h.f. national network can provide a worthwhile service (see 'Letters' p.518). While we would whole-heartedly agree with this view on the grounds of the quality of service v.h.f. provides we would like to see a bolder plan introduced by the broadcasting authorities in this country for the efficient use of the medium-wave band. We are not necessarily pleading for a new European plan-the U.K. would probably be worse off as the result of such a reallocation-but, are the potentialities of this band being fully exploited? Have we moved very far since the introduction of the B.B.C.'s Regional Scheme in, was it 1936? We believe the aerials at Brookmans Park, London, are very little different from those originally used!

Talking of aerials. Readers may have seen in the lay press references to the scheme put up by Hughie Green for 100 local radio stations in the medium-wave band. At first sight this seemed ludicrous in the present congested state of the band but the scheme, which was rejected by the Post Office, depended, to some extent at least, on the use of directional aerials serving a very limited area of up to five miles radius with a low-power ( 2 kW ) transmitter. While the use of such aerials would certainly avoid the stations causing interference with other transmitters sharing the frequencies it would not eliminate interference from Continental stations. Incidentally, Mr. Green's scheme was based on a survey conducted by a German company. A British company declined to carry out the work because the kind of publicity arising from the proposed scheme would impair its relationships with "two of its most important customers, the Post Office and the B.B.C ".

In our August leader we considered, somewhat philosophically, the utilization of the radio spectrum, suggesting that the channels should be "tailored" to the information they are to carry. Some readers took us to task for this; commenting that our attention should have been directed to the B.B.C.'s use of its existing resources. One reader, who listed the 16 frequencies used by the B.B.C. in the medium- and long-wave bands, asked why the technique of synchronizing transmissions (as was done during the 1939-45 war to prevent them being used for homing by enemy aircraft) is not more widely used. Synchronization does, of course, necessitate national network operation and therefore precludes any "regional" variations. Such a network, or networks, provided by the B.B.C. could, and should, be supplemented by low-power local stations of the type envisaged by Mr. Green-whether they be commercially operated or as a non-commercial enterprise by a local authority.

It may not generally be known that the B.B.C. has been experimenting with compatible single-sideband transmissions in an endeavour to improve the signal-to-noise ratio in the medium-wave band. When the results of the experiments have been assessed maybe we shall hear of a scheme as bold as the television changeover from 405 to 625 lines.

# A Design in Retrospect 

by J. Dinsdale, м.A.


#### Abstract

The designs for high-quality audio amplifiers published in 1961 and 1965 gave rise to several hundred letters from readers. In this article those letters referred to the designer have been analysed to establish the most popular topics of interest, and some of the more interesting suggestions and comments are examined in detail.


When Dick Tobey and I published our first articles in $19611^{1,2}$ describing the design of a transformerless high-quality audio amplifier using transistors, we did not expect to awaken more than a passing interest among a few enthusiasts. It was therefore with a mixture of surprise and delight that we received (and duly answered) over 100 letters from readers of Wireless World. Of these letters, the majority were either from engineers who were not conversant with transistor techniques (especially the use of complementary transistors and the application of a.c. and d.c. feedback) or from constructors wishing to know where certain components might be obtained. There were also a few letters from more perceptive readers who offered some useful advice and criticism, and these proved to be of great value later on in developing the mk.II system.

The circuit had originally been developed from a servo-amplifier, which was found to have an exceptionally good frequency response and low distortion. The idea of using the so-called quasi-complementary class $B$ stage, in which complementary driver transistors are followed by an output pair of transistors of a single type had first been proposed by H. C. Lin in $1956^{3}$. The circuit which Tobey and I devised took advantage of Lin's concepts, but incorporated a modified form of feedback which gave lower distortion while maintaining satisfactory gain and phase margins for the whole amplifier. Tobey and I were both very keen on sound reproduction at that time (mid-1959) and we were anxious to exploit the then very new devices called semiconductors, which were

[^2]only just becoming available to home constructors in the U.K. at reasonable prices. I was then listening (single channel) via a Williamson amplifier with Partridge output transformer feeding a 12 -in Magnavox loudspeaker in a bass reflex enclosure. My pickup at that time was a Collaro Studio ' $P$ ', later to be replaced by the Decca ffss mk.I which, when used with the S.M.E. 3009 series 1 arm and Garrard 301 turntable, gave results which at that time I considered to be little short of miraculous. However, the size and weight of the Williamson amplifier, and the heat produced by the valve heaters, made the prospect of constructing another identical amplifier for stereo distinctly unattractive. So when we found that a transistor servo amplifier, which we had developed for the inertial navigation system of a guided missile, sounded very nearly as good as the Williamson, could be assembled on a printed circuit board 5 inches square, and required only 40 V d.c. at less than 1 A peak current to give 10W into a loudspeaker load, we decided to modify the design to make it as good as possible for high-quality sound reproduction.

The performance of the transformerless quasi-complementary circuit developed by Tobey and myself appeared to be far superior (on paper) to the circuits then available (which employed transformers) and listening tests seemed to confirm this.

The two articles published at the end of 1961 described a class B quasi-complementary transformerless power amplifier and a pre-amplifier with comprehensive input, filter and tone-control facilities. The techniques used are commonplace nowadays, but they attracted considerable interest when published. Features in the power amplifier which were novel at that time included the quasi-complementary output stage and the use of a thermal feedback loop (utilizing the variation with temperature of the voltage across a diode junction) to stabilize the operating point of the output stage (and hence crossover distortion) against changes in ambient temperature. The method of earthing the equipment for single-channel operation was discussed, with particular reference to the
high asymmetrical currents whith flow in the output stage of a class B amplifier. The article also suggested how to select suitable transistors in the light of cut-off frequency, gain and noise.

The pre-amplifier employed two transistors, and gave an adequate performance without being particularly elegant. The method of equalizing the playback characteristic on disc replay utilized the selfinductance of the magnetic pickup in order to avoid designing a high-impedance input circuit. This method was subsequently found to be both difficult to apply with a single channel, and distinctly undesirable for two-channel operation because it caused excessive cross-channel interference. The tone controls used a Baxandall-type circuit, and the output fed directly into the power amplifier. The point was made that by applying the feedback networks for both the tone controls and the filters around the same stage, the characteristics of the two controls interacted in a beneficial way to increase the slope of the h.f. filter when the treble control was set to maximum boost. The stereo balance control operated by varying the feedback ratio around the second stage. This provided only 6 dB variation between channels, a figure subsequently found to be inadequate, and also tended to interfere with the operation of the tone controls. The complete system had been in operation since October 1959, some two years before publication, and we hoped that most of the obvious defects had been eliminated.
The mk.II design was constructed during 1963, and details were published early in 19654,5. The reason for publishing the new version was to improve the areas of weakness in the previous design, and to provide full details of the construction, which our correspondence had shown were badly needed. It also gave an opportunity of discussing some of the more interesting points in the design. The principal area of difference was in the pre-amplifier, which had been largely re-designed. The range of input circuits was closer to that then available from valve amplifiers, and the method of equalization for disc replay had been made completely independent of the inductance of the pickup. The tone controls and filters were much the same as before, but the balance control now utilized a log/antilog twin-gang potentiometer to give an infinite

Table 1. Performance of Mk. II system

Output power 10W r.m.s. per channel
Frequency response Total harmonic distortion
Signal-to-noise ratio
Power requirements
Controls $\pm 3 \mathrm{~dB}$ from 35 Hz to 20 kHz $\pm 3 \mathrm{~dB}$ from 35 Hz to 20 kHz
$0.3 \%$ at 1 kHz and 10 watts $0.3 \%$ at 1 kHz
70 dB at 10 W
40 V at 800 mA (max.) or 150 mA (average)
Input selector (microgroove. standard, radio. microphone. tape replay). treble, bass, filter. tape replay). balance, function volume,
(stereo. reverse stereo. mono) Radio: -60 dB at 10 kHz Mic: -50 dB at 10 kHz
Less than $0.25 \Omega$

Channel separation
Output impedance
availability; the majority requested information on the $n-p-n$ transistor, originally the 2 N 388 A . The articles had not specified where this component could be obtained. This was an unfortunate omission as germanium n-p-n transistors with a $V_{C B}$ of 45 V are not easily obtained, even now. There were a few alternatives, such as the 2 N 2613 (RCA) and the AC127Z (Mullard), none of which was quite as good as the 2 N 388 A for its sustained gain over the specified working range of collector current. A number of writers proposed using alternatives especially the OC139 or OC140, as these were the only British germanium $n-p-n$ transistors then commonly available. Unfortunately, the value of $V_{C B}$ for the OC139 and OC140 is only 25 V , and it is possible for the full h.t. of 40 V to appear across the transistor. A number of disappointed constructors did in fact write saying that they had blown up OC139s in the circuit.

Several constructors attempted to use a silicon $n-p-n$ transistor, allied with a germanium p-n-p transistor, for the complementary pair, but the characteristics of the dissimilar materials only serve to upset the symmetry of the amplifier. In addition, the thermal loop via the diode, which compensates for changes in ambient temperature, relies on all the transistors possessing similar values of $V_{B E}$, and the effect of using a silicon transistor is to prevent this temperature compensation from operating correctly. If a silicon $n-p-n$ transistor is to be used, then the complementary $p-n-p$ transistor should also be silicon, to preserve the symmetry of the circuit. When the mk.II circuit was published it was equally difficult to obtain silicon $\mathrm{p}-\mathrm{n}-\mathrm{p}$ transistors.

## Component tolerancing

The components used in most circuits, and the audio amplifier is no exception, may be divided into three categories when it comes to tolerancing.

## These are:-

(i) Components whose values are by no means critical, where $\pm 50 \%$ is more than adequate. This applies to most electrolytic capacitors, resistors used to suppress switch clicks, etc.
(ii) Components whose value determines d.c. operating points: $\pm 10 \%$ is normally adequate.
(iii) Components whose value sets a precise parameter, for example equalization of recording characteristics, roll-off frequencies, etc. Here, the tolerance should strictly be determined from the maximum acceptable departure from the desired characteristic.

In this design I decided to recommend $\pm 2 \%$ for the components in category (iii)

Many of the letters received, especially after the 1961 articles, referred to component

Table 3. Principal topics of correspondence
$\left.\begin{array}{lccc} & \begin{array}{c}\text { Number of Times } \\ \text { Mentioned } \\ \text { Topic } \\ \text { In Letters }\end{array} \\ \text { 1. Suppliers of n-p-n transistors } \\ \text { 2. Matching and equalization of } \\ \text { magnetic pickups }\end{array}\right)$
as a compromise between faithfulness to the R.I.A.A. equalization curve, and reasonable price and availability. It is also worth noting that any inherent accuracy of equalization is nullified by the action of tone controls. Nevertheless I received a number of letters complaining that the performance of an amplifier departed by 5 dB from the R.I.A.A. curve (one of these from a man who had used $\pm 20 \%$ capacitors) and other letters saying that a design which had to rely on $\pm 2 \%$ components could not possibly be a viable proposition. I think that here one literally pays one's money and takes one's choice, and I would recommend $\pm 2 \%$ tolerance where stated for those readers interested in achieving the published sensitivity (optional) or the standard equalization curves (desirable). Incidentally although the Mullard polyester capacitors specified in the equalization circuits are rated at $\pm 10 \%$ from $0^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$, intensive tests on these established that over the normal domestic ambient temperature range of $15^{\circ}$ to $25^{\circ} \mathrm{C}$, the values remained within $\pm 2 \%$ of nominal.

All other resistors were specified as $\pm 5 \%$ even though in many cases $\pm 10 \%$ would have been adequate, on account of the high degree of negative feedback. The use of $5 \%$ resistors was principally to facilitate postal fault diagnosis, by ensuring that the d.c. operating conditions in all models of the amplifier would be closely controlled.

## Tape recorder modifications

Many correspondents requested information concerning the use of the amplifier with domestic tape recorders. First of all, how should the amplifier be connected to the "record" input socket? This connection is normally best taken from the collector of the second transistor via a suitable coupling capacitor, the value depending on the input impedance of the tape recorder. The signal will be equalized at this point, and at a level of $30-50 \mathrm{mV}$ r.m.s.; all controls are bypassed since one normally relies on those of the tape recorder itself. If the input impedance of the recorder is $1 \mathrm{M} \Omega$ (a typical figure) then the coupling capacitor should be of value $0.5 \mu \mathrm{~F}$.

The earthing can also lead to trouble, and it may be found worthwhile to avoid possible earth-loops by disconnecting the tape recorder mains earth and using that of the pre-amplifier. This approach is satisfactory provided that the tape recorder is individually earthed again when it is disconnected from the preamplifier.

The other tape recorder queries mainly concerned input to the pre-amplifier. Although equalization for $7 \frac{1}{2}$ i.p.s. from a low output tape head was provided in my design, I really expected users to take the output from the replay pre-amplifier on the recorder itself into the radio or auxiliary sockets on the pre-amplifier. I was therefore surprised to learn that many users required information on equalization for tape speeds of $1 \frac{7}{8}, 3 \frac{3}{4}, 7 \frac{1}{2}$ and 15 i.p.s. at various sensitivities. The C.C.I.R. standard of $70 \mu \mathrm{~s}$ for $7 \frac{1}{2}$ i.p.s. was used in the published design. For the two lower speeds the time constants become $140 \mu$ s and $280 \mu \mathrm{~s}$, and the value of the feedback capacitor must be proportionately increased in each case. If the resistor in series with the feedback capacitor is changed, to alter the sensitivity, the capacitor value will need adjusting to preserve the correct time constant.

## Disc replay equalization

There has been much discussion in recent years in Wireless World and elsewhere, on the importance of accurate equalization of the disc replay characteristic, and the best means of achieving this. As far as magnetic pickups are concerned, the most appropriate way of dealing with these is to present the device with the manufacturer's recommended load impedance (normally $47 \mathrm{k} \Omega$ ) and then to apply the R.I.A.A. replay characteristic by means of negative feedback. Provided that the high input impedance is achieved by feedback techniques, so that the base of the input transistor can be connected to ground via the pickup itself (and a suitable blocking capacitor), and the gain demanded from the stage is not excessive, this will result in low distortion and a good signal-tonoise ratio. It must be remembered here first, that if a transistor has a gain of (say) 100, then the amplifier stage containing this transistor should not be expected to give a gain greater than 10 ; and secondly that the R.I.A.A. characteristic requires nearly 10 times more power gain ( 18 dB extra voltage gain) at 20 Hz than at 1 kHz where sensitivity is normally specified.

In the mk. II design the input impedance is $47 \mathrm{k} \Omega$ closely, and the stage voltage gain in the 'LP' position is 12 at 1 kHz rising to about 110 at 20 Hz . This bears
favourably with the minimum specified gain of 100 for both $\operatorname{Tr}_{1}$ and $\operatorname{Tr}_{2}$. Many correspondents have written to me complaining of a lack of bass in the 'LP' position. I have examined two such cases, and both were caused by low-gain transistors in $T r_{1}$ and $T r_{2}$ positions; the stage was just not capable of providing the extra 18 dB at 20 Hz . A final word of caution on this subject: it is always advisable to check the output waveform on an oscilloscope when measuring frequency response curves. There is otherwise the danger of starting the test at 1 kHz , and failing to notice that the additional gain at lower frequencies is causing the waveform to square off and hence give an incorrect reading. The correct method of conducting this test is to present the input of the preamplifier with the inverse of the R.I.A.A. playback characteristic, and then to check the output for a flat response at the appropriate level.

Turning to amplitude-sensitive pickups (the piezo-electric types such as crystal and ceramic) many letters have implied a basic misunderstanding of how these devices operate. Curve A in Fig. 1 shows the amplitude of movement of the recording (cutting) stylus when recording a flat signal at all frequencies. Curve $B$ shows the output of a velocity-sensitive (magnetic) pickup tracking the signal of curve A; the output is proportional to the rate of change of magnetic flux linkage, and will thus increase with frequency. Application of the R.I.A.A. playback equalization (shown in curve C) to curve $B$ will give a flat response. The output of a perfect amplitude-sensitive pickup would be expected to mirror curve $A$, but the output of crystal and ceramic pickups is purposely modified by the mechanical characteristics of the mounting in such a way as to compensate for the recording characteristic and provide a reasonably flat output under no-load conditions. However, the performance of these pickups has, in my experience proved somewhat disappointing and 1 have obtained far better response curves from correctly equalized magnetic pickups. The equivalent electrical circuit of a crystal or ceramic pickup may be approximated by a constant voltage generator in series with a capacitor, as


Fig. 1. Recording/ playback curves.

(a)

(b)

Fig. 2. (a) Equivalent circuit and (b) response of crystal pickup.
shown in Fig. 2(a). When this is loaded by a resistor, as must occur when it is con nected to the input of the pre-amplifier the resultant response is as shown in Fig. 2(b) the turnover frequency $f_{1}$ being given by the expression

$$
f_{1}=\frac{1}{2 \pi C R}
$$

The value of $C$ is fixed by the design of the pickup itself, and may lie in therrange $200-2000 \mathrm{pF}$, and the value of $R$ is the apparent input impedance of the preamplifier as seen by the pickup.
There are three methods of loading a crystal pickup, as shown in Fig. 3:
(i) Employ a very high load-resistance (1 to $4 \mathrm{M} \Omega$ ) with no further electricald equalization since this is performed approximately by the mechanical circuit of the pickup. This will place $f_{1}$ below the audible frequency spectrum.
(ii) Load the pickup with a relatively low resistance and equalize by using a feedback circuit composed of a series capacitor and resistor with the same time constant as the pickup capacitance and loading resistor.
(iii) Load the pickup by the more complex circuit described in my letter to Wireless World which provides, in combination with the mechanical circuit of the pickup, an output closely resembling that from a magnetic pickup. This may now be equalized exactly as for velocitysensitive devices.

Since the inbuilt mechanical equalization is not affected by electrical loading, the output of a crystal pickup when loaded by a low resistance as in method (ii) will only approximate to the output of a velocitysensitive device and equalization of this output by the conventional R.I.A.A. network will only approximate to an ideal response.
My choice of velocity-loading for crystal pickups was made because it permitted a single position 'LP' on the inpur switch, instead of two positions 'LP Magnetic' and 'LP Crystal'. In addition a number of high quality ceramic pickups require a loading impedance greater than $1 \mathrm{M} \Omega$ to achieve a bass response to 40 Hz using method (i) and my circuit is not ideally suited to this. Subsequent work has confirmed that resistive loading followed by equalization via method (ii) above is marginally best. Method (iii) is the easiest to implement with my published design, as in this case the feedback network is the same as that used for magnetic pickups. I would however emphasize that the optimum velocity-loading network varies for each pickup, \and is ideally associated with the pickup itself (mounted in the arm at the
cartridge terminals) rather than in the amplifier. It is possible to adopt more complex equalization networks, as advocated for example by Mr. J. L. Linsley Hood ${ }^{\text {B }}$, but my personal experience suggests that it is better to purchase a good magnetic pickup.

In spite of using the exact values of components for equalizing replay characteristics, the true response curves will not be obtained unless the treble and bass controls are set to a true 'flat' position, which may not coincide with the geometrical centre of rotation, or indeed may not be the same for both sections of a twinganged control. For this reason, several correspondents asked for the values of resistors for a switched control, and these are given in Fig. 4. The preferred switch is the Radiospares 2-pole 6-way midget wavechange switch, which is about the same diameter as the potentiometers it replaces.

## Stereo switching

It was found convenient to carry out mode switching, i.e. stereo / reverse stereo / mono, at the output of the pre-amplifiers. The 'reverse stereo' position permits channels to be reversed so as to use the loudspeakers with the best bass response in the most appropriate channel (where non-identical speakers are employed); it can also be used to transpose the 'positions' of instruments from left to right, and reverse the 'direction' of trains and other stereo demonstration gimmicks. However, a number of readers have pointed out that by combining the two channels at this point for mono operation, the balance control must be set truly mid-way for correct cancelling of the out-of-phase component of the signal, and also the signal-to-noise ratio is degraded by 6 dB . These are certainly valid points, but the switching problems involved if the channels are paralleled earlier in the pre-amplifier make any alternatives undesirable.

## Input switching

It is clearly a disadvantage to run the leads from the input sockets right up to the front panel for switching. A better arrangement would be to place the input switching wafer at the extreme rear of the unit, with wiring directly from the input sockets. The 'feedback switching' wafer should be placed at the front of the unit as at present, and the switch should of course have a long shaft.

## Power, sensitivity and distortion

On occasion, correspondents have asked whether the output power can be increased. The power available from a transformerless class B output stage depends on the applied voltage and the loudspeaker impedance. More specifically it is given by

$$
P=\frac{(V-v)^{2}}{8 R}
$$

where $P=$ output power (r.m.s. watts), $V=$ supply volts, $v=$ volts lost in output transistors, etc., and $R=$ load impedance.

Thus for a given load impedance, the only way to increase the power is to increase the supply voltage. This is possible only if the transistors and other components will stand


Fig. 3. Methods of loading crystal pickups. In 2 and 3 the time constants of the loading and feedback networks must be matched.
the increased voltage without breakdown. Alternatively, the load impedance may be reduced (e.g. from 15 to $8 \Omega$ ). In this event the additional power is supplied by increased currents in the output and driver stages, and this is liable to result in increased crossover distortion.

The sensitivity of the power amplifier is given closely by the expression

$$
\frac{R_{f}+R_{e}}{R_{e}}
$$

where $K_{f}$ is the feedback resistor from the amplifier output to the emitter of the first transistor and $R_{e}$ is the value of the unbypassed emitter resistor of the first stage. (In the mk. Il circuit, the sensilivity is

$$
3900+39
$$

39
i.e. 100.) The sensitivity of the pre-amplifier is given by

$$
A \frac{\left(R_{f}+R_{e}\right)}{R_{e}}
$$

where $R_{f}$ is the impedance of the appropriate feedback network, $R_{e}$ is the unbypassed emitter resistor of the first stage, and $A$ is the attenuation of the input network (if any). If (as some readers have enquired) it is necessary to increase the sensitivity, this may be carried out in either the power amplifier or pre-amplifier or both. However attempts to do this may result in increased distortion, worsening of the signal-to-noise ratio, and impairment of the frequency response.

Several readers wrote to say they were experiencing severe distortion, and subsequent investigation showed that they were using a $3-\Omega$ loudspeaker with the $15-\Omega$ design. As a result, the output and driver


Fig. 4. Switched tone control networks.


Fig. 5. Loading network for high-sensitivity earphones.
stages were supplying a higher current than the design permits, and crossover distortion was excessive. I do not recommend reducing the load to below $8 \Omega$ (when using the $40-\mathrm{V}$ design) if distortion is to be kept reasonably low. It is worth noting that the component of crossover distortion remains fairly constant regardless of output power level, and as a result the distortion increases from $0.2 \%$ at 10 W to $0.5 \%$ at 0.5 W (both figures measured at 1 kHz ). At higher frequencies the distortion is still larger. If the amplifier is to be used to drive earphones, which normally require a very low power, it is worth loading
the output with a resistor network in order to ensure that the amplifier itself operates at a power level of a few watts. Fig. 5 shows a suitable network for this purpose. If load impedances of less than $15 \Omega$ are to be used, the values of the coupling capacitors $C_{7}$ and $C_{8}$ should be increased in order to maintain a satisfactory bass response. As a rule of thumb, $1000 \mu \mathrm{~F}$ should be used with $15-\Omega$ loadspeakers, increasing to $2000 \mu \mathrm{~F}$ for $8-\Omega$ speakers.

The use of two electrolytics $\left(C_{7}\right.$ and $\left.C_{8}\right)$ is recommended for reducing the 'plop' sound when switching on both mono and stereo systems; a single pair of electrolytics shared by the earthy ends of both speakers is not recommended because it introduces audible cross-talk and distortion in stereo systems owing to the finite impedance (frequency-variable) of these components. It is worth noting that there will be audible hum when two electrolytics are used per amplifier unless a choke (e.g. 50 mH ) is used in the power supply to provide additional smoothing.

If the power amplifier is to be run either as a separate unit or with a different preamplifier, it is important to ensure that the input is loaded to ground by an impedance of under $10 \mathrm{k} \Omega$. Failure to do this will not only reduce the signal-to-noise ratio but will prevent the series feedback from operating correctly.

One potential source of catastrophic failure in the power amplifier is the biasing diode, setting the quiescent current of the output stage. If this diode fails, or the bases of the driver transistors are open-circuited for any other reason, then the output transistors will both be turned hard on and will fail in less than one second. It is for this reason that the resistor in series with the diode should not be replaced by a potentiometer, as these are notorious for intermittent loss of contact. A good alternative would be to use a fixed resistor with a trimming potentiometer in parallel. Failure of the potentiometer would not then be catastrophic. It is possible to use in place of the diode a suitable transistor as a 'super diode', i.e. with its collector and base strapped together.

More than one reader has commented on
the increase of supply current with signal frequency; this is however quite normal with this amplifier. It arises because the output transistors (OC35s, etc.) have a very low cut-off frequency $f_{T}$ of about 5 kHz . The supply current rises with frequency for two allied reasons: firstly as the gain of the output transistors decreases, the very high feedback around the amplifier automatically increases their base currents to maintain the correct amplifier gain; secondly, the non-conducting transistor does not cut off until just after the conducting transistor has started to turn on, and so there is a short period during which current flows through both transistors. In spite of the above situation, the performance of the complete amplifier remains within the quoted limits. Obviously, distortion increases with frequency, but total harmonic distortion is still below $1 \%$ at 15 kHz . Furthermore, the percentage of the audio power spectrum which lies above 5 kHz in music is very low, so the performance of music remains at a satisfactory distortion level.

Interested readers are referred to the note "Dinsdale Amplifier Mod" .

## Transistor alternatives

It was perhaps inevitable that, from the beginning, queries would be raised regarding alternative transistors. In many instances there were a number of well-known alternatives; but it was with care that the 1961 articles specified the polarity, gain and voltage rating of each device. In spite of this, many correspondents enquired whether quite unsuitable transistors could be used; some complained that they had used these, and not unnaturally the devices had failed, often carrying more of the circuit with them because of the overall d.c. feedback. For the benefit of those about to embark on this design a list of currently available transistor alternatives is given in table 4, but this is by no means exhaustive. An important point concerns the complementary drive pair $\left(T r_{3} / T r_{4}\right)$. It is vital that both of these devices and the diode are of the same material (germanium or silicon). If a silicon pair is used, then two silicon diodes in series with the resistor should be employed.

## Instability

A number of writers complained of insta-

Table 4. Transistor alternatives

|  | Transistor Number | Type | $\begin{aligned} & \text { Gain } \\ & \text { (Typical) } \end{aligned}$ | Max. Working Voltege | Typical Types |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 会 | $\left.\begin{array}{l} 1 \\ 2 \\ 3 \end{array}\right\}$ | p-n-p. small-signal, low-noise | 60 at $/ \mathrm{c}=1 \mathrm{~mA}$ | 10 | $\left\{\begin{array}{l} \text { OC44 } \\ \text { OC75 } \\ \text { AC107 } \\ \text { SN2613 } \\ \text { (Selected for } \\ \text { (ow noise) } \end{array}\right.$ |
|  | 1 | D-n-D. small-signal, low-noise, high frequency | 60 at $I_{c}=1 \mathrm{~mA}$ | 6 | $\begin{aligned} & \mathrm{OC44} \\ & 2 \mathrm{~N} 2613 \end{aligned}$ |
|  | $\left.\stackrel{2}{3^{*}}\right\}$ | p-n-p. sustained gain, over wide, current range | $30 \mathrm{at} t_{c}=100 \mathrm{~mA}$ | 40 | $\begin{aligned} & \text { OC77 } \\ & \text { ACY } 17 \end{aligned}$ |
|  | 4* |  | 30 at $/{ }_{c}=100 \mathrm{~mA}$ | 40 | $\left\{\begin{array}{l}\text { NKT227 } \\ \text { 2N385A } \\ \text { 2N388A }\end{array}\right.$ |
|  |  | wide, current range |  |  | $\left\lvert\, \begin{aligned} & \text { 2N1605A } \\ & \text { OC28 } \\ & \text { OC29 } \\ & \text { NKT401 }\end{aligned}\right.$ |
|  | $5 \& 6$ | p-n-p. good turn-off characteristic | $30 \mathrm{at}{ }_{c}=3 \mathrm{~A}$ | 40 | $\left\{\begin{array}{l}\text { AD140 } \\ \text { OC35 } \\ \text { OC36 } \\ \text { 2N2147 } \dagger\end{array}\right.$ |

bility. Without exception, the effect, which occurred only when pre-amplifier and power amplifier were connected together, took one of two forms:
(i) supersonic oscillation from 30 to 50 kHz .
(ii) subsonic oscillation at below 2 Hz .

The first of these is generally caused by feedback from the output of the power amplifier (loudspeaker terminal) to the input to the pre-amplifier between which two points the phase difference is such as to give positive feedback. If this oscillation (which tends to start as the volume control is advanced and is exacerbated by treble boost) is allowed to continue, it will rapidly lead to thermal breakdown of the output transistors and the destruction of high-frequency loudspeakers (especially ribbons). The remedy is to use screened input leads (a sound precaution anyway) and to ensure that the pre-amplifier and power amplifier are well screened within the unit itself. It is worth noting thn all complaints of this nature stemmed from equipment in which one of these points had not been complied with. The subsonic oscillation occurs in the pre-amplifier, and is due to the high-pass filter via the resistor coupling the emitters of the first and last transistors. Faulty decoupling capacitors will lead to this low-frequency motor-boating.

## Noise testing

The input transistor of the pre-amplifier, $T r_{1}$, requires its base to be loaded to ground via not more than $10 \mathrm{k} \Omega$ in order to maintain the correct function of the emitter feedback. If this condition is not fulfilled, a serious degradation of signal-to-noise ratio occurs. Normally the base is loaded via the impedance of the microphone, pickup or tape head in use (or by padding resistors if these are in circuit). In fact resistive and inductive loading give an audible difference to the character of the background noise; some observers have suggested that the "pink" noise resulting from inductive loading is more pleasing than the "white" noise due to resistive loading. However, this illustrates the obvious need to provide the appropriate loading resistor (or transducer) at the input terminal before noise tests are carried out. Failure to do this gives a misleading picture, which a number of constructors were quick to discover, especially as open-circuit highgain input terminals have on occasion been known to pick up local radio interference. Thus the magnetic pickup terminal (for example) should be loaded to ground by about $2 \mathrm{k} \Omega$ (a typical pickup impedance) for testing signal-to-noise ratio.

In general the interposing of resistor networks between a signal source and the input transistor will degrade the signal-tonoise ratio. This is because the signal and noise are attenuated in equal manner, and in addition the resistors themselves will generate noise. However, where the signal has to be attenuated (as for example with high-output crystal pickups) it is worth while ensuring that the apparent source impedance presented to the input transistor is optimized to about $1 \mathrm{k} \Omega$ Table 5 shows the results of an experiment which illustrates this latter point, about which, incidentally, there has been much correspondence, including letters published in Wireless World. The signal-to-noise ratio is

Table 5. The effect of input loading on noise level

| $R_{1}$ | $R_{2}$ | Signal/noise <br> ratio |
| :---: | ---: | :---: |
| $\Omega$ | $\Omega$ | $(\mathrm{dB})$ |
| 100 k | 1 k | 60 |
| 1.2 M | 12 k | 55 |
| 4.7 M | 47 k | 40 |
| 10 M | 100 k | 21 |

largely dependent on the voltage amplifying transistors, especially $T r_{1}$ and $T r_{2}$ in the preamplifier and $T r_{1}$ in the power amplifier. The use of low-noise devices in these positions cannot be emphasized enough, with the added proviso that $T r_{1}$ in the power amplifier must also be a high frequency $(15 \mathrm{MHz})$ device to enable the feedback to operate correctly.

## Earthing

The 1961 articles did not emphasize sufficiently the need for avoiding earth-loops, to judge from the correspondence on this subject he currents flowing in the output valves of the then conventional valve amplifiers were small, and the effects of incorrect earthing were negligible. The precautions necessary to avoid distortion due to the high asymmetrical currents flowing in the output of a transistor amplifier were mentioned in both articles, but correspondence still arrives complaining of troubles due to this cause. Rather than repeat the necessary precautions here, I would refer readers who are in doubt to the original articles and to the correspondence in Wireless World'. Two readers wrote describing the pick-up of radio/TV interference giving an audible signal. These phenomena were never entirely solved, as they ceased in both cases on re-wiring the systems, and could not be reinduced. They may have been due to a semi-dry joint acting as a detector diode.

Immediately after publication of the mk. II design in 1965, there was a considerable correspondence discussing methods of avoiding an earth loop. It was clear that the method proposed by Mr. C. Artus ${ }^{6}$ was far more elegant than that originally published, and I have now adopted this method. Most of the alternative earthing schemes proposed by readers failed to appreciate the need to prevent the asymmetrically-distorted output waveform from appearing in series with the input signals, and were therefore not valid solutions to the problem. However one method which several readers proposed was to design the complete power amplifier and pre-amplifier circuits symmetrically on either side of an earth 'tree-trunk'. This method avoids earth-loops, but it introduces other problems in the areas of overall screening between channels, screening between power amplifier and pre-amplifier in each channel, and wiring to the front panel controls. In addition, the complete board tends to be some 12 inches square, and this is not easy to accommodate in a cabinet. I still believe the Artus solution to be the most elegant.

## Stabilized power supply

The power supply specified in both sets of articles consisted simply of an unstabilized capacitor-loaded bridge-rectified supply. The mk.II version included additional chokecapacitor smoothing. The disadvantages of this type of supply are first that the output voltage falls with prolonged loud sounds, and
secondly that with this fall in voltage there is a corresponding rise in hum level. The drop in output voltage can lead to premature "squaring off" of the waveform, and hence gross distortion and may also affect the "character" of the sound in an unmusical way. The increase of hum, which admitredly occurs only with loud sounds and is thus not immediately audible itself, produces a most unpleasant effect by modulating the output at 100 Hz . This effect is particularly noticeable with organ music. The remedy is to use a stabilized or semi-stabilized supply.

## Pilot lamps and mains switching

The use of a d.c. pilot lamp has been criticized on the grounds of false economy. Nevertheless I have measured an improvement of 10 dB in hum level resulting from using a d.c. lamp. The use of a neon mains indicator introduces a "buzz", and steps must be taken to eliminate this with suitable r.f. chokes.

A further source of hum is the a.c. mains switch ganged to the volume control; if this switch can be positioned as far as possible from the pre-amplifier circuitry, so much the better. Placing the mains switch external to the amplifier is satisfactory, provided there is little chance of switching the amplifier on or off with the volume control at maximum rotation. Alternatively it might be possible to place the switch at the rear of the unit, with a long shaft connecting it to the front panel.

## Fault diagnosis

Nearly half the letters I received described a set of symptoms and requested a diagnosis. I had carried out many tests during development of the circuit and had also helped personally in the construction and commissioning of over twenty amplifiers, so many of the symptoms were familiar, and could be identified. I always invited correspondents to let me know if my recommendations were successful, and many of them kindly replied giving me this information. This in turn helped others.

The greatest difficulty however occurred with letters describing modifications which were either proposed or which had been carried out and did not work, or which used different components to those specified. This situation frequently applied when commercial kits based loosely on the original design had been used. The kits or equipment often used cheaper components, and alternative transistors which were not suitable. In all of these cases, once the situation was established, it was possible to replace the faulty components with those originally specified, and in most cases the equipment then met the original specification.

I am always loath to recommend modifications especially where this involves personal expenditure by constructors, unless I have


Fig. 6. Test circuit to investigare effect of input loading on noise level.
personally checked and tested the proposed alterations. As may be imagined I do not have the time or money to check all of these queries personally, especially as many involved proprietary equipment which it was desired to connect to my amplifier. In general, I feel that an author cannot normally be expected to comment with authority on modifications to his design; at the same time, I welcome letters describing modifications which have been carried out successfully.

## Use with commercial equipment

The 1965 article referred to the difficulty of designing equipment which will work equally well with every pickup, tape deck, microphone, tuner, and loudspeaker marketed. Sensitivities and impedances (which are often complex and non-linear) are by no means standardized, and one can choose only a reasonable compromise; this is, after all, what the manufacturers of commercial amplifiers do. Perhaps one should increase the number of input sockets and switched alternatives, but this would put the price out of the home constructor bracket.

Nevertheless, a number of letters either enquired whether a particular tape head (for example) would work with the amplifier, or else complained that a certain device did not work satisfactorily. In these latter cases, inspection of the manufacturer's literature (where available) was generally enough to explain why either the gain or input impedance of the amplifier were not suitable for the device in question. To offer alternative input circuits was a temptation that had to be resisted, because I could not guarantee that all the other performance characteristics of the amplifier would be maintained, without building and testing the proposed new circuit myself.

## Conclusions

It is now ten years since the "Tobey-Dinsdale Amplifier" was developed. It is still advertised in both kit and made-up form, and a number of commercial equipments have been based on the original circuit. A conservative estimate based on the supply of kits and transistors by two well-known companies suggests that over ten thousand of these amplifiers have been manufactured. It is not now the best available. Recent tests have shown that the quasicomplementary class B output stage produces audible crossover distortion, especially at low signal levels, and this in turn leads to aural fatigue. Nevertheless, I would like to believe that the amplifier, appearing when it did, fulfilled a need by providing an incentive for more able designers than myself to identify and tackle the principal obstacles in the design of a high-quality amplifier. This they have now done, and many amplifiers now on the market give an excellent performance.

Can anything be learned from a retrospective study such as this? I hope that if I have the opportunity again to write an article describing a circuit I will try to remember the following points:
(i) All components should be precisely defined, and a number of commercial sources should be given.
(ii) Alternative components should be given whenever possible (especially semiconductors).
(iii) Suppliers of printed circuit boards and metal work should be named.
(iv) It is obviously impossible to satisfy everyone; however if the design can give a number of options which between them cover all anticipated uses, then constructors can make the appropriate choice.

Of course one tries to design a system which will give perfect reproduction of music, and I personally regard distortion figures, frequency response curves, and all the other scientific and pseudo-scientific terms as a tiresome but necessary means to the ideal end. But when I heard a visitor to the 1965 London Audio Fair say to his companion, "The trouble is all this music-it's a pity I can't sit down and listen to the hi-fi", I decided to forget about pleasing everybody.

I will also try to remember that when writing to an author with queries, all relevant information should be given and the enclosure of a st amped addressed envelope is appreciated. And finally, if the author's suggestions prove to be successful, then writing to tell him so will make him feel far happier and it may make it easier for him to diagnose similar faults on other people's equipment.

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- A reprint of these two articles is available from Dorset House, Stamford Street, London SE1, price Ss.


## Appendix

Derivation of component values for R.I.A.A. disc equalization

$$
\begin{aligned}
& \text { Network impedance }= \frac{R_{1}\left[\frac{1}{p C_{1}}+\left(\frac{R_{2} / p C_{2}}{R_{2}+1 / p C_{2}}\right)\right]}{R_{1}+\left[\frac{1}{p C_{1}}+\left(\frac{R_{2} / p C_{2}}{R_{2}+1 / p C_{2}}\right)\right]} \\
&=\frac{R_{1}\left[1+p R_{2}\left(C_{1}+C_{2}\right)\right]}{1+p\left(C_{1} R_{1}+C_{1} R_{2}+C_{2} R_{2}\right)+p^{2}\left(C_{1} R_{1} C_{2} R_{2}\right)} \\
&=\frac{R_{1}\left(1+p T_{2}\right)}{\left(\mathrm{I}+p T_{1}\right)\left(\mathrm{I}+p T_{3}\right)} \quad \text { where } T_{1}=\frac{1}{2}\left(b+\sqrt{b^{2}-a}\right) \\
& T_{2}=R_{2}\left(C_{1}+C_{2}\right) \\
& T_{3}=\frac{1}{2}\left(b-\sqrt{\left.b^{2}-a\right)}\right. \\
& \text { nd } b=C_{1} R_{1}+C_{1} R_{2}+C_{2} R_{2} \\
& a=4_{4} C_{1} C_{2} R_{2} .
\end{aligned}
$$

For the case where $T_{1}=3180 \mu \mathrm{~s}$

$$
\begin{aligned}
& T_{2}=318 \mu \mathrm{~s} \\
& T_{3}=75 \mu \mathrm{~s}
\end{aligned}
$$

It may be shown that:

$$
\begin{aligned}
& C_{1} R_{1}=.2940 \\
& C_{2} R_{2}=8 \mathbf{I} \cdot 2 \\
& C_{1} R_{2}=237
\end{aligned}
$$

( $C$ in microfarads, $R$ in ohms)
From these expressions the values of components for the equalization networks may be derived starting with a suitable value of $R_{2}$ to set the sensitivity.


Standard R.I.A.A. curve for microgroove disc relay $f_{1}=50.049 \mathrm{~Hz}(3180 \mu \mathrm{~s}), f_{2}=500.49 \mathrm{~Hz}$ (318. $\mu \mathrm{s}$ ) and $f_{3}=2121.5 \mathrm{~Hz}(75 \mu \mathrm{~s})$.

Equalization network


# Cassette System for $\frac{1}{4}$-in Tape 

Tape Systems Lid, of Egham, Surrey, have developed a mechanically simple yet robus tape transport system for use with cassettes employing $\frac{t}{t}$-in tape. Together these comprise the Packette System-Packette being the trade name of the new cassette.

Besides employing inherent advantage over $\frac{1}{8}$-in tape with respect to mechanical strength, recording quality, alignment with the tape heads, and ease of manufacture, the Packette is edge driven. This action is achieved by building the pinch wheel into each Packette. There are both reel-to-reel and continuous-loop types.

The tape deck has a chassis of nylonreinforced plastic and few moving parts. It can be operated in any position and be fitted with a variety of a.c. /d.c. motors and


The plastic chassis loaded with a tape Packette and fitted with a drive motor.
tape heads to meet many intrumentation and audio requirements. The same deck can be driven at speeds down to $15 / 16$ i.p.s. and wow and flutter can be as low as $0.1 \%$ at $1 \frac{7}{8}$ i.p.s. Modified Marriott heads are employed for audio use-a composite erase record/play head-block has been developed for double track use such as in language laboratories where recordings are made on one track whilst a second track is in play-back.

The single drive motor employed runs at constant speed in the same direction for all operations-lape speed and direction changes are achieved by simple mechanical modules.

Of course there is no fundamental reason why traditional tape speeds should be employed in a new system-there simply has to be correct equalization for any speed chosen.

A Packette system has been developed for use in a language laboratory, and models are available from E. J. Arnold \& Sons Lid, Butterley Street, Leeds LS10 1AX.

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# Electronics in Civil Aviation 

## An impression of the current state of civil avionics obtained at a recent London conference

The devil we know is better than the devil we don't-and so say * nearly all of us. This message was repeated over and over again in various ways by speakers discussing diverse aspects of electronics in civil aviation at the Royal Festival Hall, London, September 15 th to 19 th.

On the face of it one would think that it would not be beyond the capability of the electronics industry to provide civil aviation with all they need in the way of control, measurement and computing equipment. In fact if the electronics engineers were given their head and if the aviation boys took things at their face value a whole host of new electronic aviation aids would soon appear but, if this happened, chaos, collision and catastrophe would be the order of the day.

Revolutionary equipment could well, on paper at least, do away with all the known limitations of existing systems but such equipment would certainly introduce a number of unknown features which would lead to hazardous situations simply because these features are unknown. This has been proved in the past, as was pointed out in a paper by J. Benjamin of the Royal Aircraft Establishment, in military aviation where strategic necessity has led to radical change, sometimes with disastrous consequences.

Another important factor to be taken into account when


A possible solution to the problem of clearly presenting navigation information to the crew was suggested by f. G. Carr and F. S. Stringer and is shown above. The c.r.t. display shows the outputs of four navigation systems-two inertial navigators, Loran and Decca. The display graphically shows the positional information from the four equipments and shows how the outputs of three of the equipments differ from the one selected, which happens to be inertial navigator No. 2.
considering change in civil aviation is that airborne equipment of the type we are considering requires large, very expensive, ground installations for support. Any change would mean that all the ground installations throughout the world would have to be replaced.

There is no question that a vast improvement must take place in the facilities available to civil aviation. However, this will be achieved by evolution and not revolution. Figures given by E. Davies, of Marconi, in a paper on surveillance radar showed that in the twelve months ended July 1968 the total aircraft movements (take offs or landings) at Heathrow, Gatwick, Luton and Stanstead was 400,000 . During the same period another 700,000 movements were contributed by 26 other airports in the London area. The average movements for the period worked out at 125 per hour with peaks in the region of 250 movements per hour. According to P. G. Masefield, chairman of the British Airport Authority, the number of movements by 1980 will triple. This means 20 runways will have to run at a constant rate of 40 movements per hour.

To handle the necessary amount of traffic "all weather" operation will become essential and automatic landing will become routine even in extremely adverse weather conditions.

Civil aviation therefore has to find ways of handling all these aircraft in all sorts of weather. This will mean across-the-board improvements in airborne and ground installations with the lion's share of the problem on the heads of electronics engineers.

## Automatic landing

The problem here is not one of accuracy, existing systems are perfectly adequate in this respect; it is not one of reliability, because reliability can be had at a price; it is the overall integrity of the system. Integrity is a word that was much bandied about at the conference. In this context it means that a system will operate correctly when required and that it will be known to be operating within its specified limits at any particular time and may therefore be trusted.

Consider a typical automatic landing installation. The well known, and established, instrument landing system (i.l.s.), operating in conjunction with heading information is responsible for bringing the aircraft in line with, and just over the threshold of, the runway. Being a radio system relying on radiated beams it is sensitive to interference and, on a number of airfields, it just cannot be installed because of the terrain.

In the later stages of the landing radio altimeters on board the aircraft play an important part. These can be sensitive to multi-path reflections and aircraft attitude.

The automatic pilot and automatic throttle used to carry out the landing contains tens of thousands of electronic components, scores of motors, servo systems, amplifiers, integrator and feedback loops. How can one be sure that this complex system is $100 \%$ serviceable? Is it sufficient to fit three
of them and take the majority decision as being the right one? In this context the words fail-safe, fail-soft, fail-operative, fail-obvious, probability, comparator, monitor, duplex, triplex and duplicate monitored were repeated over and over again.

In most of the areas mentioned no real solutions to these problems exist as yet. In a paper by W. Hilton, of Sperry Gyroscope, a fail-obvious comparator for airborne systems was described which gave a warning if the monitored equipment or the comparator itself failed. With this system, if the comparator failed, the monitored equipment must also be considered to be unserviceable because the pilot, even if he knows that it is the comparator at fault, has no way of ensuring that the monitored equipment itself has not failed also. Even if the idea is extended indefinitely-a monitor to monitor the monitor, to monitor the monitor . . . there can still be no absolute certainty. The accepted thing is that the probability shall be that a system shall not fail more than once in $10^{7}$ landings.

Will the designers have to take into account freak conditions? For instance an aircraft returning to an airfield at which a visual landing is impossible due to bad weather and when, for some reason, a diversion airfield is not available. In a case such as this a pilot would want to know the degree of unserviceability of his equipment in order to determine whether an automatic landing is a justifiable risk. Probably the only way of doing this would be to employ a large number of equipment measuring sensors controlled by a digital computer.

With the i.l.s. the picture is a brighter one. Some time ago the R.A.E. designed c.p.i.l.s. (correlation protected instrument landing system) which is now being developed and will be produced by the Plessey Company.

The system employs hyperbolic phase fields and correlation detection to generate guidance misalignment signals with inherent integrity and, with suitable choice of transmitter modulation, the system is compatible with existing v.h.f. instrument landing systems. The only additional airborne equipment consists of a microwave aerial and mixer unit which may be fed directly into the existing i.l.s. The idea therefore conforms to the rule of evolution rather than change, it provides the pilot with a choice of v.h.f. or microwave i.l.s., and overcomes many of the v.h.f. i.1.s. interference and site problems.

## Air traffic control

The other area of great difficulty is in air traffic control. It is thought that large digital computers will be able to perform the necessary predictions and calculations for the safety of all aircraft in the controlled area. This will include handling emergency situations and taking into account the presence of military aircraft which, according to E. Davies, may suddenly change flight level at rates of up to $60,000 \mathrm{ft}$ per minute.

The problem is in getting adequate information on all movements in the area so that the computers can be kept up to date on a rapidly changing situation.

In this field many improvements are required to radar systems. Airfield radar can be divided into two types; primary radar which is responsible for general surveillance and tracking, and secondary radar which consists of an airborne transponder that gives information on the aircraft carrying it when interrogated by a ground installation.

Primary radar needs to be of higher resolution to separate targets which are close together; higher scan rates must be achieved so that any new target may be quickly spotted; and dwell time on any particular target must be increased so that stationary clutter can be minimized and additional doppler information (velocity etc.) can be derived.

All these requirements are in obvious conflict and M. A. Radford, of Marconi, suggested that the solution may lie in the use of multiple receiver and electronic scanning techniques.

Secondary radar suffers from a variety of defects. One of these is difficulty in siting the aerial on the aircraft and even when two aerials are carried, contact is not certain due to the
screening effect of the airframe. With present equipments the only information transmitted is aircraft identity and height.

Secondary radar however is rapidly increasing in importance and will eventually oust the primary radar from its premier position. C. Ullyatt, of R.R.E., says that primary radar will probably be used mainly to handle those aircraft which for some reason cannot take part in the secondary radar system, and for keeping track of airfield ground movements. Mr. Ullyatt gave a paper describing a new transponder which followed the law of evolution. Basically it consists of an auxiliary unit which can be fitted to, and addressed through, the existing transponder. The new equipment would be capable of transmitting a great deal of information and during an emergency could transmit the state of the aircraft systems to the ground.

## Navigation

Extremely accurate navigation is essential to enable aircraft to operate in the fairly close proximity required if the number of movements predicted for the future is to be met. J. G. Carr and F. S. Stringer, of the R.A.E. (Mr. Stringer described hyperbolic navigation systems in our August issue), suggested at the conference that two or more current navigation aids could be operated under the direction of a management digital computer and explained how a Comet-4 was being modified to do research along these lines. In this system a highly accurate point position fixing aid is used with a long-term reference system so that the limitations of both are overcome.

Mr. Stringer suggested that the Kalman filtering technique could be used to great advantage now that digital computers of adequate capacity are available. Although such a technique is not liable to become economically attractive until storage becomes cheaper.

With the Kalman technique, a mathematical error model of each of the sensors is stored in the computer, the parameters of these models are adjusted throughout the flight every time a position comparison is made so that as time progresses the model becomes a closer approximation to the truth. The computer uses these stored values of error parameters to correct the navigation information to produce position data that is more accurate than any of the sensors could have achieved separately. In effect the navigation system is being continuously calibrated during the flight, and the longer the flight the more accurate the system becomes.

Civil aviation is rapidly approaching a point when far reaching decisions on electronic equipment for the next decade will have to be taken. We can only hope that the evolution of suitable equipment will not be overtaken by the demands on the airlines for more airborne seats.

## Correction

"Low-cost 15W Amplifier" Oct. 1969.
The common emitter resistor $\mathrm{R}_{6}$ in Fig. 1 should be $4.7 \mathrm{k} \Omega$ not $47 \mathrm{k} \Omega$.

Fig. 4, showing curves of t.h.d. against frequency for different powers and loads, was incorrectly annotated. The correct specifications are shown below.



## Some highlights from the last German national exhibition

Good German citizens, and a good many non-Germans, flocked in their thousands to -e the 26 th German radio exhibition, the Deutsche Funkausstellung, which was held at Killesberg, iust outside Stutgart, from August 29th to September 7th. On the first three days, the Friday, Saturday and Sunday, 245,000 people attended the exhibition. Total attendance over the ten days that the exhibition was open was 703,000 which created an all-time record and exceeded all expectations.

Colour TV and hi-fi equipment were the principal attractions at the exhibition, coupled with a huge television studio, run by the first and second programme authorities A.R.D. and Z.D.F., which seated 1,400 people per performance. A clever idea here for people who could not get inside the studio was a travellator to convey them past the long observation window so that they all had a good view but were unable to loiter. High-quality speakers conveyed the sound to them.
One of several large halls, in fact the major area of Hall No. 1, was occupied by various exhibits and demonstrations of the Bundespost, the German equivalent of our Post Office, who included among them an historical exhibit of television apparatus. There was the 30 -line Nipkow mirror helix, an old 441 -line receiver, and a 180 -line or 441 -line camera that was used during the Olympic Games in 1936, where Walter Bruch (now Prof. Dr. Bruch) inventor of the PAL colour system, was employed as a camera operator.

Probably the most significant exhibit, however, was the $12-\mathrm{GHz}$ television broadcasting equipment, which was actually a working model, comprising transmitter, aerial, receiver dish and translator to Band IV and V channels. At present there are three television services available in Germany, and all the channels in Bands I, III, IV and V are apparently fully occupied by them.

To make room for additional services, which will include an educational one, the Bundespost has been experimenting with still higher frequencies, around 12 GHz , actually between 2.5 and 2.7 cm as was reported in Wireless World in July this year.

The exhibit showed the kind of equipment that would be used. The transmitter employs a conical aerial, with a reflector, which can be seen in the accompanying photograph, and has a circular radiation pattern in a horizontal plane. The reflector
receives energy from a vertical horn projecting from the apex of the cone. Weather protection is provided by a transparent cover which encloses the whole aerial.

For reception a parabolic aerial is employed, as in the photograph, which is mounted on a mast together with a translat-


Transmitting aerial for the experiniental television service on 12 GHz .


Receiving paraboloid, with translator on the mast, for the 12 GHz service.
or to convert the microwave frequency range to, say, u.h.f., so that it can be applied to a normal domestic receiver.

In the experimental model shown the receiving aerial would cost about DM. 200 (approximately $£ 20$ ), but the translator was estimated 10 cost about DM. 8,000 , which would render the system too expensive for any but the largest blocks of flats. It was expected, however, that by quantity production, using a quartz crystal controlled oscillator and a cavity resonator type of tuning system, the price could be reduced considerably. The system is envisaged for use only in the centre of a town which it could 'flood' with direct radiation. Its maximum radius of service is about 20 km (about 12.5 miles).

## Novel Car Aerial

One of the surprises among the commercial exhibits was a new type of car radio aerial called the Alpha 3 and shown by Hans Kolbe \& Co. under their 'fuba' brand name (which they always spell with a small ' $f$ '). It was designed by Hans Kolbe in conjunction with Professor Meinke, of the Institute for High Frequency Technique at Munich.

Incorporating a wing mirror, it is intended to be used as such. This alone is an asset today when vandals enjoy an orgy of snapping off telescopic aerials.

Inside the housing is a printed-circuit panel containing three aerial loops and two


Wing mirror car aerial introduced by Hans Kolbe.
transistor amplifiers, one for a.m. and the other for f.m. Even in car radios in Germany where there are some .000 v.h.f. stations it is necessary to make provision for f.m. reception, and this aerial system covers all a.m. broadcasting frequencies from 150 kHz to 25 MHz as well as the v.h.f./f.m. range in Band II.

The rim of the mirror forms part of the aerial pick-up system. It is made of rustless steel and is shaped to fit in its spring-loaded mounting as a ball joint, so that it can be adjusted in its application as a wing mirror.
 showing the printed circuit. board.

Its internal construction can be seen from the accompanying illustration. The aerial loops, mirror rim and the electronic assembly form an integrated whole whose impedance matches the transistor input elements. The low impedance of the device helps to avoid interference pick-up. On v.h.f. the aerial loops form a bandpass circuit which rejects interference from transmissions outside the v.h.f. radio band, even though their field strength may be high. In the wideband a.m. coverage special design features are incorporated to prevent static interference and cross-modulation. The outputs of the two amplifiers are combined and matched to the coaxial cable. Also a protective diode is provided to by-pass static surges, which can wreck the input transistor in a car radio receiver.

Power supply to the amplifiers is taken via a separate lead from the car's electrical system, and the amplifiers will operate on 6 V to 15 V at $5-11 \mathrm{~mA}$.

The price of the Alpha 3 aerial in Germany is expected to be about DM. 90 (say £9).

## Cheaper V.T.Rs

Another surprise was the sudden appearance of video tape recorders by several manufacturers at the domestic-user level of about DM.2,000 (£200). Blaupunkt (a member of the Bosch Group and known in the U.K. as Blue Spot), Grundig, and Telefunken all showed prototypes, and Philips had two models, one (type LDL 1000) priced as low as DM.1,880.

Telefunken uses $\frac{1}{2}$ inch tape on 18 cm (about 7 inch) reels at $19 \mathrm{~cm} / \mathrm{sec}$ (about $7.5 \mathrm{in} / \mathrm{sec}$ ) giving a playing time of 60 minutes. It is said to be equally suitable for colour and monochrome recording, and the company hope with improved tape oxides to
better the present 3 MHz bandwidth.
Philips use $\frac{1}{3}$ inch tape, of which a length of 480 metres (a little under $1,600 \mathrm{ft}$ ) will run for about $\frac{3}{4}$ hour. The instrument uses transistors throughout and operates from the mains. Of transportable proportions, it weighs 12 kg (about $26 \frac{1}{2} \mathrm{lb}$ ). Sound and synchronizing signals are carried on narrow edge bands.

## Home Cine TV

Something more than a coincidence must have led NordMende to produce at the same exhibition as the series of domestic, or entertainment, video tape recorders their Colorvision equipment. This unit comprises a colour television receiver and an 8 mm film scanner and reproduces the cine film on the screen of the TV receiver. The optics and film transport mechanism were developed in association with another company, Paillard S.A. (Bolex).

It is quite a domestic piece of equipment housed in a large console cabinet. The colour receiver occupies the left half of the cabinet and the film scanner, together with a separate tape cassette unit for the sound commentary, the right-hand half.

Advantages claimed for this method of reproducing cine film pictures are that it is silent in operation, does not require complete blacking-out of the room, provides the user with complete control through his TV receiver of such parameters as brightness, contrast and colour saturation, a still picture (it can hold one frame as long as required without any risk of overheating), it can be left ready for use in a living room without any need for elaborate setting-up procedure, and of course it provides the purchaser with a built-in 25 -inch colour receiver.

The model on show was a prototype (but it was being demonstrated) and the price was not fixed, but it was believed it would be somewhere around DM.4,000 (about $£ 400$ ).

Full technical details are not available, but visible inspection showed that the film scanner employed a raster on the screen of a small oscilloscope and that the film passed through an optical lens system continuously, without a frame-by-frame gate. It is not clear, for instance, how the 18 picture-per-second sequence that they quote for the Super-8 film is synchronized with the picture frequency of the receiver; nor how


Philips domestic sound and vision recorder type LDL 1000.
the continuous film transport can be stopped to produce a still.

From the film scanner the picture is broken up optically by dichroic mirrors into its red, green and blue components, which are then converted electrically into colourdifference signals prior to their application to the receiver. The sound commentary is quite independent, but it is incorporated in the same compartment as the film scanner.

## All-embracing home entertainment

Another quite original idea shown by NordeMende was the Vario-Center, a fully comprehensive high-fidelity domestic sound and vision entertainment device in a severely contemporary but original styling. In appearance it resembled a large sphere with three slices cut off the sides to provide flat vertical surfaces, and a fourth slice off the top to present a flat horizontal surface.

On one of the vertical surfaces is mounted a NordeMende integrated stereo amplifier with a four-band a.m./f.m. tuner and control unit, with $30+30 W$ continuous sine-wave output (model 8002/ST); on another surface is their model 8002/T4 tape recorder; and on the third the latest (hybrid) transistor 25 -inch colour TV receiver. On the horizontal surface at the top is a Perpetuum Ebner PE2020 record player with a Shure M75MG cartridge.

Loudspeaker systems comprise two semispherical enclosures each with three bass, three middle and two tweeter units. They can each handle up to 50W.

## Electronic record players

Because the show was national, several importing companies held private shows in various parts of the town. One of these was held by Paillard-Bolex G.m.b.H., of Munich, who are distributors in Germany for the Swiss-made Thorens equipment.

They were showing an entirely new Thorens disc record playing deck (type TD125) with several interesting features. One feature is the shock-absorbent mounting for the turntable and pickup. Only the turntable and pickup, together with some electronic components are mounted on the chassis, and the whole chassis assembly weighs about 15 lb . Its inertia, together with the springy suspension, enables quite violent vibrations to be absorbed.

The only link between the two, apart from the springy suspension, is the ( $10: 1$ ratio) drive belt, a soft slim rubber band which absorbs any vibration. No gears are employed, and there is no mechanical speedchange device. Driving power for the 16 -pole


Thorens record player which fearures a shock-absorbent mounting for the turntable and pick-up.


Simplified diagram of the Blaupunkt v.h.f. television tuner using varicap diodes.
synchronous motor is derived from a 20 W transistor amplifier driven from a Wien bridge oscillator, whose frequency determines the speed of the turntable in three steps for 16, 33 and 45 r.p.m. Rumble is claimed to be better than -68 dB (DIN 45539 weighted standard).

For speed monitoring, stroboscopic markings for 50 and 60 Hz mains on the underside of the turntable base are optically conducted to a window at which they can be compared with a neon lamp. A variable potentiometer provides $\pm 2 \%$ correction. The deck can be operated from battery or mains.

Finally, a feature that can be seen in the Thorens photograph is a new st"le for switch knobs that was evident on quite a number of stands in the exhibition. This is the large flat type of knob seen in the foreground, which measures about $50 \times 30 \times 6 \mathrm{~mm}$ and looks like a bar of chocolate. The three, seen here are slide-type controls for speed change, on /off and pickup raising and lowering.

In contrast to the entirely free suspension of the Thorens was that of Braun in their new PS 600 record player, which they cautiously state to be their first automatic player. This one lifts and lowers the pickup automatically, but it can also be adapted to change records. Its vibration-absorption is similarly effective, but to avoid the possibility of an oscillation being set up in the freely-floating system they have equipped it with critical hydraulic damping. Like the Thorens, too, this player has electronic control and electrical speed change.

Braun also introduced at the show a new type of loudspeaker cone which they call a 'Kalottenmembran'. Used as the middle-frequency unit in their 4-unit L. 710 enclosure (two bass, one middle and one high-note) the new material permits a 'flatter' cone angle and thus provides a better 'spread' of sound in the upper frequencies.

## Electronic TV tuning

Monochrome television was to be seen on every set-maker's stand, but colour was claiming the attention of both exhibitor and visitor. From the British observer's point of view the most interesting feature, both in colour and monochrome, was capacitancediode tuning used by all but one manufacturer (Körting).

One of the great simplifications of the


Grundig all-band television tuner, with electronic tuning and band-swicching, compared with a standard matchbox. It has no moving parts.
diode tuning technique is that once the circuits are set up and aligned, tuning of any number of stages can be effected by the adjustment of a single potentiometer. Press-button tuning is reduced practically to the need to switch a single low-voltage lowcurrent d.c. line, each button being associated with its own potentiometer. As a result, remote control by a multi-way cable is simply an extension of the press-button unit on the set, and no motors are required.

Several manufacturers offered remote control, some by cable-less ultrasonic devices. Saba was actually demonstrating an ultrasonic remote control that changed programme and controlled colour saturation and volume. It was interesting to observe that all manufacturers included saturation adjustment on ther remote-control units, and some included contrast was well. These facilities of course require motors.

A simplified diagram of the Blaupunkt v.h.f. electronic tuner, shown in the accompanying drawing, which is representative of general practice in Germany. In addition to diode tuning it also incorporates diode band switching, and both tuning and band switching include the u.h.f. tuner, which is omitted from our simplified diagram.

Three circuits are tuned by BA142 diodes, as shown by the diode/capacitor symbols used in Germany to present a varicap diode. Band switching is effected by three BA136 diodes and an AA142 diode. On the right is shown the assembly of programme selector switches and potentiometers, of which there are usually six or seven, with a single lead between it and the tuner. Another lead would be necessary for band switching, of course, and that is controlled by an
angular adjustment of the slider potentiometer shaft. Power supply for tuning is always derived from an integrated-circuit voltage-stabilizing circuit. Slide-type controls seem to have taken over from rotary knobs in most kinds of domestic equipment.
Prices in Germany for colour receivers range generally around DM. 2,300 for a 25 inch table model, DM. 2,000 for 22 inch and DM. 1,700 for 19 inch. For monochrome 23 inch is the norm, and a table model would sell at about DM. 550 upwards.

A number of exhibitors had two loudspeakers in their 25 -inch table colour TV receivers and some had tone controls, but a rather unexpected innovation from the country that originated the PAL system was the provision on two or three makes of colour tone controls. These take the form of slider potentiometers calibrated with red or yellow at one end and blue the other, and they attenuate the blue gun emission (for a 'warmer' colour) or vice versa.

Prices of colour sets were all fixed by registration with the Kartelamt, but monochrome prices were all 'recommended', as they are here. Either way there is an added 'value tax', equivalent there to our purchase tax except in severity. It is always included in the quoted price and it amounts to $11 \%$ of the retail value of the goods. It is added at all stages along the distribution line and is still $11 \%$ even if the price is cut, because the final seller charges the full tax but deducts from it what has already been paid at other stages down the line. It sounds as though administration might be expensive.


The special Funkausstellung stamp.

## News of the Month

## Register of engineers

The creation and administration of a composite register of "the engineering community" is foreshadowed by an announcement from the Council of Engineering Institutions. At a meeting of the Board on September 4th it was unanimously resolved that "the Council of Engineering Institutions will, in collaboration with other interested parties and subject to the agreement of the Privy Council, initiate the formation of an organization to create and administer a composite register covering the principal sections of the engineering community, currently chartered engineers, technician engineers, and engineering technicians".

A working party, consisting of one representative from each of the fourteen Institutions within C.E.I., which include the I.E.E. and I.E.R.E., under the chairmanship of Sir Arnold Lindley, has been set up to implement the resolution. The first duty of this working party will be to prepare a submission to the Privy Council to get agreement to such modifications to the C.E.I. Charter and By-Laws as may be necessary and then to determine which other interested parties should be invited to collaborate.

## Aesthetics and electronics

The Marconi-Elliott Microelectronics factory at Witham, Essex, has won for the London architects Anthony B. Davies and Associates the gold medal award for industrial architecture made triennially by the Incorporated Association of Architects and Surveyors.


The sampling technique used in pulse code modulation, which was invented by Alec Reeves, of Standard Telecommunications Laboratories, Harlow, is symbolized on one of the four stamps issued to mark the establishment of the new Post Office Corporation.

## Colour TV show

The colour television show organized by the B.B.C., I.T.A. and B.R.E.M.A. started its tour in Leicester on October 14th. The venues and dates for the exhibitions until the end of the year are: Stockport, Town Hall, Oct. 27-Nov. 1; London, Euston Station forecourt, Nov. 8-29; Birmingham, Mecca Ballroom, Dec. 5-10; Glasgow, McLellan Galleries, Dec. 16-20.

Incidentally, according to B.R.E.M.A., deliveries of colour receivers for August were 1,000 higher than for the same month of 1968 but the total of 60,000 for the first eight months of the year was 18,000 lower.

## Technical design competition

Designers and technicians under the age of 35 , who are still undergoing professional training or who have not worked professionally for more than two years, can take part in the competition for the Braun prize for technical design.

This competition which is to be held in 1970, is the second of its type. The first was held in 1968 when Germany and Japan won the major awards. The winning individuals or teams can receive up to DM 25,000 ( $=£ 2,500$ ). To give some idea of the range of designs eligible, in 1968122 projects were filed-from a cooking plate to a transportation system.
The competition is sponsored by Braun Aktiengesellschaft, 6242 Kronberg / Ts., Postfach 115 116, Germany, in co-operation with "Gestaltkreis" of the Federal Association of German Industries.

## Airfield control radar

An X-band airfield control radar, called the ACR430, intended to meet the needs of small airfields has been introduced by Plessey Radar. The new equipment, which replaces the earlier ACR424 has a dual role in that it continuously radiates one beam for general purposes.

A single aerial reflector system fed by twin horns and dual transmitter/receivers provides the two-beam coverage. One horn illuminates the reflector to give a cosecant squared pattern for surveillance. The other horn partially illuminates the reflector producing a pencil beam with the accuracy
required for surveillance radar approaches. Circular polarization is used to reduce the effects of precipitation clutter.

The output from a particular horn-transmitter/receiver combination can be switched to either or both displays which, together with the master control unit, can be up to 1,000 metres away from the aerial without the need for line amplification equipment. Two 300 mm ( 12 inch ) diameter displays provide selection of four range scales from 4 to 32 nautical miles.

## European multi-role combat aircraft

A European company was set up, on the signing of an agreement in Munich recently, called Avionica Systems Engineering GmbH which will be responsible for planning the electronic systems for the European multirole combat aircraft. The company will have its headquarters in Munich and will consist of members drawn from the following three companies: Elliott Automation and Advanced Military Systems Ltd [U.K.], Elektronik-Systems-Gesellschaft [West Germanyl, and FIAR-CGE and Selenia Industries Elettroniche Associate S.p.A. (Italy).

The new company will receive a contract for the electronic systems for the new aircraft from Panavia, which is also a consortium consisting of: the British Aircraft Corporation, Messerschmitt-Bolkow-Blohm and Fiat from the same three countries.

## The Ferranti award

The British Computer Society has set up an annual award for the best candidate in its professional examinations.

The award, which is $£ 150$ donated by Ferranti, will be made by the council of the society on the recommendations of the chairman of the education board.

The first recipient of the award was Geoffrey Hollis who is a computer systems analyst with the Gulf Oil Company.

## Solar flare early warning installation

A system of 24 -hour forecasts of the best frequencies to use in the shortwave band has been worked out by Swedish Telecommunications Administration. This will make use of a telescope installed for this purpose on the roof of a building at Farsta outside Stockholm. The telescope will be used to register solar flares and provide an early warning of disturbance to radio communications.

## Tape player for colour

Lasers and holographic techniques have been employed by R.C.A. to play back, through a colour television set, full-colour programmes recorded on very cheap transparent plastic tape. A laboratory model of the SelectaVision tape player system was recently unveiled in America and is expected to be on sale to the public in the early 1970s. The cost should be about $\$ 400$ for the player and less than $\$ 10$ for a half-hour recorded tape. The system is claimed to be as easy to operate as a record player.

## "The engineer is a woman'"

In an effort to encourage women to enter the engineering professions the Ministry of Technology has produced a film called "The Engineer is a Woman". In the film five women from mechanical, civil, electronic and electrical engineering, explain how and why they became engineers. The film is intended for 13- to 18 -year-olds and can be obtained free of charge for non-theatrical use from: The Central Film Library, Bromyard Avenue, Acton, London W. 3 .

## Semiconductor expanded

## plant

The Ferranti semiconductor assembly plant at Ormsgill, Barrow-in-Furness, is to be doubled in size to over 50,000 sq.ft. By about mid 1970 the plant will be capable of fissembling more than 20 million semiconductor components per year from material processed at the "parent" plant at Gem Mill, Chadderton, Oldham.

## Data book demise

After being well known to engineers for over 30 years the Mullard Data Handbook, which consisted of a large number of black loose leaf folders, is to be discontinued. In its place three multi-part books are being prepared which will list data in the same format as before, on Mullard's design range of components.

Book one (blue cover) of the new series will cover semiconductor devices and integrated circuits and will be divided into six parts. Book two (orange cover) will deal with valves and tubes and will have five parts. Book three (green cover) will be in three parts and will provide data on components and materials.

Users who took out new subscriptions to the original handbook service during or after

## Operational Ampli-fiers-Pt. 10

We regret the omission from this issue of the concluding instalment of the series of articles on operational amplifiers by G. B. Clayıon.

May 1968 will receive equivalent replacements from the first set of the new publication free of charge.

The fourteen parts will cost 12s each and should be available between now and January 1970, depending on the part required. Every year each part will be up-dated and reprinted and will be available at the same price; 12s. Orders for the new handbook should be sent, with remittance, to Central Technical Services, Mullard House, Torrington Place, London W.C.1.

## Mini-computer

A physically small computer, known as the 18 C , is being developed by Arcturus Electronics Ltd, with the backing of the National Research Development Corporation. It uses medium scale i.cs and has a 16 -bit word length. Parity checks are built in. Data can be manipulated between several registers without returning to the main memory. It has a multi-register configuration-two registers may be used as index registers. The memory may vary in size from 256 to 32,000 words. Production is to begin soon and the 18 C will be available in a desk-top console on a seven-inch tall standard rack-mounted package. Both versions will hold up to 8,000 words of memory or interfaces for peripheral devices. It is expected that the selling price with 4,000 18-bit words of memory and a Teletype ASR 33 will be under $£ 4,000$. A system with 256 words of memory could, in quantity, sell for under $£ 2,000$.

## Portable radio receives weather broadcasts

Zenith Radio Corporation have produced an a.m./f.m. portable radio with all the usual facilities plus a pre-tuned channel of 162.55 MHz . On this frequency there are almost continuous broadcasts in America giving information on local weather and water conditions, so the radio should be popular with all those who enjoy "messing about in boats". The price in the U.S.A. will be just under $\$ 50$.

## Satellite link for Indonesia

Indonesia's new communications satellite ground station will link the country with the U.S.A., Europe, Japan, Australia, Hong Kong, Singapore and Malaysia. The station is located in Djatiluhur, Java, approximately 100 km from the capital and was built by the defence communications division of International Telephone and Telegraph Corporation. It is equipped to provide a variety of international communication Services-ielephone, telegraph, facsimile, leased channel service, alternate voice-data and both colour and monochrome television.

## I.E.E.-I.E.R.R.E. liaison

For some time there has been gradual drawing together of the I.E.E. and the I.E.R.E. and many joint meeungs and conferences have been arranged. Now a joint liaison committee has been set up "To examine, and to report on, the advantages, disadvantages and problems of possible methods of combining the activities of the two institutions in a manner which would be in the best interests of the members of both institutions, and to make recommendations for the closer working together of the two institutions."


A panoramic view of the "largest semiconductor factory in Europe"; Mullards at Southampton. With almost 400,000sq.ft. of floor space and a staff of 3,000 Mullards are endeavouring to obtain a larger share of the world's semiconductor market. Dr. F. E. Jones, managing director of Mullard, has predicted that by 1980 the market for transistors will be $16,000 \mathrm{M}$ units and for integrated circuits $8,000 \mathrm{M}$ units, requiring over 1,000 tons of silicon a week. Mullard have other semiconductor plants at Stockport and Blackburn and are building another at Thornaby in Yorkshire which should start production at the end of the year and will eventually have a floor area of 200,000 sq. $f$ t.

## Letters to the Editor

The Editor does not necessarily endorse opinions expressed by his correspondents

## The B.B.C. should think again

Now I have heard everything! Twenty years after implementing the Copenhagen Wavelength Plan, nearly fifteen since v.h.f, broadcasting was begun, and just at the time when this service has reached the remotest parts of the Kingdom, the British Broadcasting Corporation is "prepared to consider" reallocating the medium-frequencies! Why? Where is the technical and economic sense in this?

Do the B.B.C's engineers really think that they can hoodwink the public at large into believing that by transmitting Radio 1 on two medium-frequencies to cover the country, all the interference problems will disappear overnight? This reallocation would end the daytime distortion caused by interaction between the ground-waves of adjacent transmitters using 1214 kHz , but it will certainly do nothing to overcome the night-time fading and the ear-splitting beat interference from the Albanian station at Scutari. Neither is $908 \mathrm{kHz}_{z}$ going to be satisfactory with the East German Burg transmitter occupying this channel.

Radio 1 is supposed to be a national programme, so surely it should take its place alongside Radios 2, 3 and 4 on v.h.f. where the service coverage extends-potentiallyto $99.7 \%$ of the population. If money is not available to establish a complete nationwide Radio 1 v.h.f. network, then I think that the B.B.C. should be required to give an undertaking that all the proposed local stations should carry it at least during the evening periods when the medium-frequency transmissions are subject to fading and foreign interference.

Again, why bother at this time to improve Radio 4 m.f. coverage when that achieved on v.h.f. will still be better by between one and two per cent of the population?

In proposing to reallocate and improve m.f. reception and thereby continue the side-byside duplication of three programmes on two entirely different transmission systems, the B.B.C. is going to leave itself and we listeners in as big a muddle as ever. V.H.F. receiver sales will be retarded and a useful opportunity to work out with fellow E.B.U. Members a phased close-down of non-essential transmitters lost.

If the B.B.C. is still staffed by competent professional broadcasters and engineers, why
do they not put forward a bold, imaginative Plan for the seventies rather than palliatives more suited to the fifties? This, sir, is a sincere plea to ask the B.B.C. to think again.

## AUSTIN UDEN,

Aylesbury,
Bucks.

## Logic Display Aid

During the building and testing of the Wireless World Logic Display Aid, which is an extremely useful and clever device for the laboratory, we have found a number of errors.

The first anomaly is on page 258 of the June issue and concerns component values in the dian circuit. Resistors $R V_{S}(12)$ and $R V_{7(14)}$ in the circuit are of $500 \Omega$ but were found to be too low in value to reduce the current sufficiently to control the output voltage to the required level. Actual measured values in the boards built were $R V_{5(12)} 3.6 \mathrm{k} \Omega$ and $R V_{7(14)} 1.56 \Omega$, but $10 \mathrm{k} \Omega$ components were used as these were available at the time.

The multivibrator, IC6/B2 on page 311 July issue was found to run at about 12 kHz with the capacitors of the shown value. Using $0.022 \mu \mathrm{~F}$ raised the frequency to about 24 kHz which was considered to be satisfactory.

An error is to be found on page 377 of the August issue, Fig. 62. Pin 5 of IC2 should go to pin 16 socket 7 and not 17 as shown.

When construction had reached board 8 it was found that in the assembly a ZN330E was fitted for IC4 as in the component list, but a ZN362E was needed. The component list states one too many ZN330Es and one too few


Fig. 1

ZN362E. The ZN330E was used in position 4 on board 8. The extra gate needed was found on board 8 , IC5, the wiring of which is shown in Fig. 1.

Fig. 64 also has an error; pin 1 and pin 12 of IC3 should go to pin 8 of IC4.

On page 419 , Fig. 66 , pin $8 / \mathrm{B} 2$ should be relabelled pin 23/B2. The K signal comes from P9/B8 not P5/B6 and the T signal from P5/B8, not $\mathrm{P} 9 / \mathrm{B} 6$.

A different arrangement for the video was employed as shown in Fig. 2. This provides bright-up pulses only when clock pulses and video are present, completely eliminating any


Fig. 2
fly back signals. The second gate was used as an inverter so providing positive or negative bright-up as this may be required for future use in the instrument built. Also a more sophisticated video amplifier was used, as a circuit board was salvaged from a project abandoned some time ago.
H. J. BACON,

Barking Regional College of Technology.
The author replies:
I am much indebted to Mr. Bacon for taking the trouble to note the errors in the article. This will make life easier for other constructors. His idea of providing a switch to select either positive or negative going brightup pulses is a good one. Yet another way of obtaining satisfactory video blanking will be described in part 8 of the series of articles as the original blanking circuit did not perform very well with some oscilloscopes.

I would be very pleased to hear from others who have used the display aid for teaching as it would be useful to have an assessment of the instrument's value as a teaching aid and to hear of the students' reaction to it.
Brian Crank.

## F.M. receiver bandwidth

It is disappointing to find Mr. L. Ibbotson stating, in his otherwise informative contribution, that something like 180 kHz i.f. bandwidth will provide 15 kHz audio bandwidth when a maximum frequency deviation of 75 kHz is employed (W.W. June 1969, "Test Your Knowledge", Q.9).

The i.f. bandwidth (for a single sinewave tone) is determined by the Bessel expansion of the equation for the modulated wave:

$$
\begin{aligned}
& e=E \sin \left(\omega_{d} d-m \cos \omega_{m} t\right) \text { i.e. } \\
& e=E \\
&-\mathcal{J}_{0}(m) \sin \omega_{1}(m) \cos \left(\omega_{c} \pm \omega_{m}\right) t \\
&-\mathcal{J}_{2}(m) \cos \left(\omega_{c} \pm 2 \omega_{m}\right) t \\
&+ \\
& \ldots \text { etc. to infinity. }
\end{aligned}
$$

$\mathcal{I}_{n}(m)$ is the Bessel coefficient of the first kind, order $n$ and argument $m$ modulation index $=\frac{\text { deviation frequency }}{\text { modulating frequency }}$
the standard convention is that the significant sidebands are all whose amplitude is greater than $1 \%$.
In the case quoted, the mod. index $=75 / 15$ $=5$, and reference to a table of Bessel Functions will show that $\mathcal{J}_{8}(5)$ is the last order of argument 5 which is greater than $1 \%$ (it is $1.841 \%$, whereas $f_{9}(5)$ is $0.552 \%$ ). Hence there are 8 pairs of significant sidebands.
The bandwidth $=2 \times n \times \bmod$. freq., where $n$ is the number of pairs of sidebands. With 8 pairs,
bandwidth $=2 \times 8 \times 15 \mathrm{kHz}=240 \mathrm{kHz}$.
From above it will be seen that if the i.f. bandwidth is only 180 kHz , then mod. freq. $=$

$$
\frac{180}{2 \times 8} \mathrm{kHz}=11.25 \mathrm{kHz}
$$

A listening comparison will quickly demonstrate the validity of the foregoing, the 'rule of thumb' sets really are disappointing. One -iuch may be the 'F.M. Tuner Using Integrated Circuits' described in the same issue. If its bandwidth ( 3 dB down) is in fact 160 kHz , then it will have an audio bandwidth of only 10 kHz .
L. E. WaUGH,

New Malden,
Surrey.

## The author replies:

I agree with the result quoted by Mr. Waugh that if we wish to include all side frequencies with an amplitude greater than $1 \%$ of the unmodulated-carrier amplitude, then for a modulating frequency of 15 kHz and a maximum deviation of 75 kHz an i.f. bandwidth of 240 kHz is required. I do not agree, however, that this is the standard convention. Some authorities, it is true, claim that all side frequencies with amplitudes greater than $2 \%$ of the unmodulated-carrier amplitude should be included-this would require the inclusion of 7 pairs of side frequencies and hence a bandwidth of 210 kHz .

I do not agree that restricting the i.f. bandwidth to 180 kHz will restrict the received audio bandwidth to 11.25 kHz ; f.m. does not work that way. If an audio signal with components up to 15 kHz is radiated, then the same range of audio signal components will be received-together with an amount of nonlinear distortion products determined by the degree by which we restrict the i.f. bandwidth. L. Ibbotson.

## Listener fatigue and ultrasonics

In an article in the April, 1969, issue Mr. Linsley Hood suggested that "listener fatigue" may be due to the ability of many transistor amplifiers to give large power outputs at supersonic (ultrasonic) frequencies which cause a , response in modern high-quality speaker systems.

I have been carrying out experiments deliberately feeding "white noise" through a high-pass filter to Mr. Linsley Hood's class A amplifier which was coupled to a commercial three-speaker high-quality reproducing system. This arrangement was found to be capable of producing a vague feeling of discomfort over a period of some hours whether
or not normal programme material was being handled.

Further experiments with specific ultrasonic frequencies indicated that, with my apparatus, the discomfort was noticeable only at fairly high power levels ( 3 W or more), and at frequencies just out of audible range ( $20-$ 25 kHz ).

Other evidence on this subject has been obtained from users of high-powered ultrasonic cleaning equipment, who report vague feelings of discomfort and a desire to move away when working in the vicinity of such apparatus.

Bearing in mind that, although normal programme material may not contain appreciable signals at ultrasonic frequencies, such unwanted signals can arise in equipment; there seems to be a strong argument for always using a steep-cut low-pass filter circuit with high-quality amplifiers.

The extra realism or "presence" sometimes claimed for apparatus having a response far beyond the sonic spectrum may in fact be a very mixed blessing.
Norman W. Vale,
Mickleover,
Derby:

## Second-order active filter

I would like to correct various errors which crept into my note 'A Simple SecondOrder Active Filter' (Wireless World, April 1969, p. 185).

The formula quoted was derived using a high gain infinite input impedance amplifier; it should have been

$$
\frac{e_{0}}{e_{i}}=\frac{-\mathbf{I}}{\mathbf{1}+\alpha s T+(s T)^{2}}
$$

where $\tau=R C$ and the 3 dB frequency is given by

$$
w_{c}=\frac{I}{T}
$$

The degree of peaking is governed by choice of $\alpha$, with critical damping (no peaking) for $\alpha=2$. However, critical readers will have noticed that my values for

$$
c_{s}\left(=\frac{\alpha c}{3}\right)
$$

for the practical responses given, do not agree with the theoretical transfer function. This is due to the finite input impedance of the transistor pair. This does not detract from the utility of the circuit however. Better agreement would be obtained by reducing both $R$ and $R_{c}$ ( 33 k ) and increasing $C$.
John Firth,
Ottawa,
Canada.

## Operational amplifiers

Your August, 1969, issue includes Part 7 of the series of articles on operational amplifiers by G. B. Clayton which contains two points on which I would like to comment. The first concerns the circuit diagram under the heading 'Monostable Multivibrator (1)'. If this diagram is correct the circuit cannot work
in the manner described by the author, for a negative pulse cannot be applied to terminal $A$ from the input point labelled 'trigger'. If, on the other hand, diode $D_{2}$ is shown the wrong way round, the waveform labelled $e A$ will have a positive level, in the stable state, whose value depends partially on the value of the unlabelled resistor adjacent to $D_{2}$ on the figure.

The other point worth a comment concerns the section 'Regenerative Comparator'. The author's illustration of a rectangular hysteresis loop illustrates a common situation in which the loop gain is high for all values of output p.d. $e_{o}$ except those very close to the saturation values. But this is a particular case. Regenerative circuits such as these reach their threshold levels when the loop amplification reaches unity, and for small values of the feedback ratio A the switching points can occur at values of $e_{0}$ that are considerably less than the saturation values. There is a further comment worth making in relation to this situation. If integrated circuit operational amplifiers are used as regenerative comparators with small hysteresis, as required in many applications, it will be found that the elimination of high frequency parasitic oscillations becomes a very difficult problem indeed. It may become necessary then to use two stages. The first stage is a non-regenerative comparator with the required degree of amplification obtained by negative feedback and the second stage is a regenerative comparator with ample hysteresis and well-defined threshold levels.

## H. Sutcliffe,

Professor of Electronic Engineering, University of Salford.

The author replies:
I would like to thank Professor Sutcliffe for his comments. The circuit diagram under 'Monostable Multivibrator (1)' is in error, the diode $D_{2}$ has been shown the wrong way round. The positive level of the waveform $e_{A}$ shown in the text as $\beta V_{o}^{+}$max will, as Professor Sutcliffe points out, be partially dependent on the value of the unlabelled resistor, the effect is small however if as I had assumed (but neglected to state) the value of $R_{1}$ is considerably less than the value of the unmarked resistor.

Regarding his second comment, the use of low $\beta$ and hence small hysteresis is, I would think, likely to give rise to parasitics at switching in any form of regenerative comparator, whether using i.c. op. amps or not. I would therefore consider the case discussed in the text as being the usable form of a regenerative comparator circuit although it is strictly a particular case. Professor Sutcliffe's comment will make readers aware of the difficulties of using small hysteresis with regenerative comparators.
G.B. Clayton.

## More "Letters" are on p. 535

## Personalities

This year's I.E.E. Faraday Lecturer is J. H. H. Merriman, C.B., O.B.E., M.Sc., A.Inst.P., F.I.E.E., a director of the new Post Office board. Mr. Merriman, who is 54 , and a physics graduate of the University of I.ondon, joined the Post Office Research Station, Dollis Hill, in 1936. Six years ago he became assistant engineer-in-chief of the l'ost Office, and in 1965 deputy engineer-in-chief. Two years later he was appointed to the new post of director of engineering and in August 1967 he became senior director: development. He was recently appointed member for technology of the board of the new Post Office Corporation. Last Deceniber Mr. Merriman accepted the invitation to become visiting professor in the department of electronic science and telecommunications at the University of Strathclyde, Glasgow.

John A. Saxton, D.Sc., Ph.D., the new chairman of the Electronics Division of the I.E.E., is director of the Radio \& Space Research Station at Dition Park, Slough, Bucks. Dr. Saxion, who is 55 , was, until his appointment to the Research Station in 1965, director of the U.K. Scientific Mission in Washington, D.C., and scientific attaché at the British Embassy there. He was for a time on the staff of the college before joining the Radio Division of the National Physical Laboratory, and in March last year he accepted a visiting professorship in physics at University College, London.

Donald G. Fink, general manager of the Institute of Electrical and Electronics Engineers, New York, has received the Outstanding Civilian Service Award of the United States Army Electronics Command "For his outstanding and dedicated service since 1963 as a member, vice-chairman, and chairman of the United States Army Electronics Command Electronics Advisory Group, Fort Monmouth, New Jersey, which has materially assisted in the advancement of the systems concept in tactical communications and resulted in great benefits to the Electronics Command and the Army".

Sir Raymond Brown, O.B.E., Comp.I.E.R.E., has relinquished his appointment as Head of Defence Sales of Her Majesty's Government, which he had held for over three years, and has rejoined Racal Electronics Lid as president. Sir Raymond, who, until his Government appointment, was chairman and managing director of the company of which he was co-founder, was knighted in this year's Birthday Honours. E. T. Harrison continues as chairman of the board and chief executive.

Bryan 1. H. Wilson, M.A. A.M.Inst.P., has become chief scientist at the Allen Clark Research Centre of The Ilessey Company, at Caswell, Northants, which he joined in 1953 and where he has been leader responsible for solid-state research since 1963. He is a graduate of Jesus College, Cambridge, where he took the natural sciences tripos. Much of Mr. Wilson's early work was concerned with the development of silicon integrated circuits. Subsequently, his activities have included the development of photocells and thermoelectric materials.
C. R. Knowles, M.A., is appointed chief engineer, and S. Woodcock, B.Sc., products manager responsible for selling and marketing in the components group of Ferranti's Electronic Display Department. The components group manufactures cathode-ray tubes (and associated coils), valves and photon devices. Mr. Knowles, who is 32, graduated in natural sciences from Jesus College, Cambridge. He joined Ferranti L.d in 1961 as a development engineer in the cathode-ray tube laboratory. He became chief development engineer for valves in 1967 and was made assistant works manager in October of that year. Mr. W'oodcock, after military service in the Far East, graduated from Leeds University in 1950 and joined Ferranti in 1951 as a member of the physical laboratory. He worked initially on the development of the aluminizing process for TV picture tubes and on phosphor screens, but later switched to work on industrial and radar tubes. Since 1966 he has been chief engineer, c.r.t. development.

Arthur I. Llewelyn, O.B.E., B.Sc., has been appointed director of the Ministry of Technology's Computer Aided Design Centre, Cambridge, which began operating earlier this year, and aims to develop the application of c.a.d. techniques in indusiry in co-operation with Cambridge University. Mr. Llewelyn, after studying at the University of Wales Engineering Department, Cardiff, joined Bawdsey Research Station at the outbreak of war where he was concerned with the early developments of radar, and later was responsible for early airborne pre-control andnavigationalcomputing systems. In 1960 he took up an appointment with NATO as scientific adviser to the Allied Air Forces Central Europe. Mr. Llewelyn returned to the U.K. in 1965 and joined the Ministry of Technology and has latterly been head of the Computer Advisory Service.

This year's recipient of the David Sarnoff Gold Medal of the American Society of Motion Picture and Television Engineers is Peter C. Goldmark, B.S., Ph.D., president and director of research of C.B.S. L.aboratories, Stamford. He started his professional career with Pye Radio in Cambridge, where in 1935 he was in charge of television engineering. Dr. Goldmark, who was born in Budapest, Hungary, received his doctorate in physics from the University of Vienna, and after service with P'ye went to the United States and joined the Columbia Broadcasting System as chief engineer in 1936. In addition to his position in C.B.S. which he has held since 1954 Dr . Goldmark is a visiting professor in medical electronics in the Department of Radiology at the University of Pennsylvania Medical School.
W. Roy Thomas, F.I.E.E., aged 51, is appointed group technical executive of Plessey Electronics Group where he will be responsible for co-ordination of all research and development work for the research centres, at West Leigh and Roke Manor. Mr. Thomas had been with Ellioti-Automation since 1952 where latterly he was group chief scientist, a director of Elliott Space \& Weapon Automation L.td and E A Radar Systems Lid and chairman of Elliott Electronic Tubes Lid. From 1939 to 1952 he was with the Royal Aircraft Establishment, Farnborough, where he was concerned with work which culminated in the design of the TRIDAC three dimensional missile-aircraft simulator. At Elliots he was responsible for the development of FACE, the field artillery control system using the 920B computer. Latterly Mr. Thomas co-ordinated the activities of the six research laboratories of Elliott Automation concerned with advanced techniques in computers, avionics, radar, optoelectronics microcircuits and space. Mr. Thomas is chairman of the joint E.E.A./S.B.A.C. avionics research committee for guided weapons, space and electronics. He is also the
U.K. representative on the organizing executive committee of EUROSAT.

Frank H. Taylor, F.I.E.E., has been appointed a senior principal research engineer at Standard Telecommunication Laboratories, Harlow, Essex, which he joins from S.T.C's Radio Producis Group, New Southgate. Mr. Taylor had been technical manager and systems manager for the group's aviation and communications business.
P. J. Allin, B.Sc., A.M.I.E.E., aged 28, has joined Intercontinental Systems Inc. (UK) Lid, of Woking, as terminal systems engineer. Mr. Allin oblained his degree in electronic engineering at the City University (formerly Northampton College) after which he spent six years at the Central Electricity Research Laboratories in I.eatherhead. Since 1966 he has been with Cable and Wireless as an electronics designer.
R. O. K. Turvey, B.Sc.(Eng.), M.I.E.E. has been appointed general manager of Cole Electronics' manufacturing division (formerly known as C. A. Cook I.id.) at Wickford, Essex. Mr. Turvey held previous appointments as chief engineer of the Transmission Division of A.E.I. Woolwich and as manager of the Terminal Equipment Department of Submarine Cables Ltd.
C. P. Crompton, M.I.E.R.E., who joined Orbit Controls I.td, of Cheltenham, as a senior project engineer on its formation 18 months ago, has been appointed chief engineer. Mr. Crompton, who is 41 , previously held senior engineering posts with Advance Controls Lid., Racal Communications I.td., and the Sperry Gyroscope Co.

The appointment of EIvin F. Collins as electronics production manager is announced by Solartron Electronic Group, Farnborough. He succeeds Dennis Burton, recently appointed director of production. Mr. Collins, aged 38, has been with Solartron for eleven years, latterly as product manager for digital instruments. Prior to joining Solartron he worked as a test gear engineer with the Ministry of Supply.
G. W. Mackenzie, M.I.E.R.E. has been appointed by the B.B,C. Head of Enginering, Northern Ireland. He joined the Corporation in 1941 at the Edinburgh studio centre. In 1954 he became a lecturer in the Engineering Training Department where, since 1963, he has been head of the technical operations section.
T. Aspin has been appointed technical manager of the Industrial Electronics Division of Mullard L.td and becomes a director of Associ:
Semiconductor Manufacturers Lid and of the Mullard Radio Valve Company Lid. Mr. Aspin joined Mullard in 1946 and since 1966 has been general product manager of the company's Consumer Electronics Division.

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## Active Filters

## 4. Basic theory: Active circuits

by F. E. J. Girling* and E. F. Good*

The essence of active-filter design is ealisation of 2 nd-order response with 2 factor $>\frac{1}{2}$ without using both capacitance and inductance. Three simple -eedback loops are analysed: (1) two ags and negative gain, (2) a lag-lead -network with positive gain, (3) a -alanced parallel-T network and -regative gain; and the basic relationthips between available gain and maxinum $Q$ are derived. An abstract discussion of sensitivity to variations -n amplifier gain and in passive com--onent values is also attempted.

## st-Order network

We have seen in Part 2 that the two Istrder transfer functions $I /(1+p T)$ and $T /(\mathrm{I}+p T)$, can be realised with $C R$ setworks; and it follows that any transfer nction that can be reduced to a product of st-order factors can in principle be realised y a $C R$ network (though buffer amplifiers nay be very helpful in a practical situation). -There is no active-filter problem.

## -ind-Order networks

For a 2 nd-order transfer function, for xample

$$
1 /\left(1+\frac{1}{q} p T+p^{2} T^{2}\right)
$$

he condition of $q=\frac{1}{2}$ marks a dividing line: when $q<\frac{1}{2}$ passive $C R$ realisation is yossible, but when $q>\frac{1}{2}$, not. (The :ondition $q<\frac{1}{2}$ is, of course, covered by the garagraph above, since then the transfer iunction may be resolved into two real -Ist-order factors.) The limitation can be emoved, however, by the use of gain and eedback.
For the basic system with $100 \%$ feedback shown in Fig. I(a)

$$
\begin{equation*}
\frac{V_{o u t}}{V_{i n}}=\frac{\mu}{1-\mu} \tag{1}
\end{equation*}
$$

If, therefore, as in Fig. i(b),

$$
\mu= \pm A F(p)= \pm A F_{1}(p) / F_{2}(p)
$$

where $F_{1}(p)$ and $F_{2}(p)$ are the numerator 3nd denominator respectively of $F(p)$,

$$
\begin{equation*}
\frac{V_{\text {out }}}{V_{i n}}=\frac{( \pm A) F_{1}(p)}{F_{2}(p)-( \pm A) F_{1}(p)} \tag{2}
\end{equation*}
$$

The aperiodic gain constant is written ( $\pm A$ ) so that $A$ may be a positive quantity whether the amplifier gain is positive or negative. In general this simplifies the labelling of diagrams and discussion of changes in the magnitude of $A$. In addition in the following analysis, to emphasise the difference and to avoid confusion when making comparisons, $A$ is used when the gain factor is negative and $K$ when it is positive. Three circuit configurations will be analysed:

1. A two-lag network and negative gain,
2. A lag-lead (Ist-order band-pass) network and positive gain,

## ${ }^{\text {or Royal Radar Establishment }}$



Fig. I(a). Schematic of active feedback system; (b) the same in which $\mu$ is arbitrarily divided into a
frequency-dependent factor and an aperiodic factor.


Fig. 2. A basic method of increasing $Q$ factor.
3. A balanced parallel-T network and negative gain.

## Two lags and negative gain

The transfer function of a two-lag network may conveniently be written as shown in Fig. 2, so that $q_{0}$ and $T_{0}$ are the initial values of $q$ and $T$ for the system; i.e., the values before feedback is applied. By setting $\beta=1$ the system becomes of the same form as Fig. I, and by substituting in equn. (2)

$$
F_{1}(p)=1, F_{2}(p)=1+\frac{1}{q} p T_{0}+p^{2} T_{0}^{2}
$$

the loop-closed transfer function is obtained as

$$
\begin{align*}
\frac{V_{\text {out }}}{V_{\text {in }}}= & -\frac{A}{1+\frac{1}{q} p T_{0}+p^{2} T_{0}^{2}+A} \\
= & -\frac{A}{A+1} \times \\
& \frac{1}{1+\frac{p T_{0}}{q_{0}(A+1)}+\frac{p^{2} T_{0}^{2}}{A+1}} \tag{3}
\end{align*}
$$

Comparison with the standard form for a 2nd-order denominator, $1+p T / q+p^{2} T^{2}$, then gives

$$
\begin{equation*}
T=T_{0} /(A+1) \tag{4}
\end{equation*}
$$

and

$$
\begin{equation*}
q=q_{0}(A+1)^{1} \tag{5}
\end{equation*}
$$

Thus, remembering that the nominal cut-off or undamped resonant frequency $\omega_{c}=1 / T$, we find that the application of feedback multiplies both $\omega_{c}$ and $q$ by $(A+1)^{1}$. The effect is shown in Fig. 3, although these curves are drawn for the situation where $A$ is constant and the varying parameter is the feedback fraction $\beta$. By substituting $I / p T$ for $p T$, or otherwise, the corresponding results for a loop containing two leads are found to be that $q$ is multiplied and $\omega_{c}$ is divided by $(A+1)^{1}$.

Generally the dependence of cut-off frequency on amplifier gain is undesirable in a practical circuit. But there are ways of reducing it to a second-order effect, for example by combining the amplifier and one of the lags into a feedback integrator; and the relation between $q$ and loop gain, equn. (5), still applies.
When

$$
\begin{equation*}
A \gg 1, q=q_{0} A^{\frac{1}{2}} \text { approx. } \tag{6}
\end{equation*}
$$

from which the sensitivity of $q$ to small changes in zero-frequency gain, $A$, is obtained as

$$
\begin{equation*}
\frac{\Delta q}{q}=\frac{1}{2} \cdot \frac{\Delta A}{A} . \tag{7}
\end{equation*}
$$

This is a satisfactory result to the extent that there is no magnification of errors, and one would expect that in a practical circuit $A$ would be stabilized by using an amplifier of much higher gain, say $A_{0}$, reduced to the required gain $A$ by negative feedback-

$$
\begin{equation*}
A=\frac{A_{0}}{1+A_{0} \beta^{\prime}} \tag{8}
\end{equation*}
$$



Fig. 3. Showing the effect of negative ģain and feedback on a two-lag network. A is constant, $\beta$ varies.

Black's formula, which may be rearranged to

$$
\begin{equation*}
\frac{1}{A}=\frac{1}{A_{0}}+\beta \tag{9}
\end{equation*}
$$

Thence, by differentiation, if $\beta$ is constant

$$
\begin{equation*}
\frac{\Delta A}{A}=\frac{\Delta A_{0}}{A_{0}} \cdot \frac{A}{A_{0}} \tag{10}
\end{equation*}
$$

which is the well-known result for a negative-feedback system, viz. relative changes in closed-loop gain are proportional to relative changes in open-loop gain multiplied by the ratio closed-loop gain to open-loop gain (i.e., the ratio of required gain to available gain). Thus, in principle, by making $A_{\mathrm{v}} / A$ large enough the dependence of $A$ on $A_{0}$ can be reduced as much as may be desired. It is to be expected, however, that in practice when $A_{0} / A \rightarrow \infty$


Fig. 4. Nyquist plot for feedback loop with two lags and negative gain.
it will be found that $A$ is affected by changes in $\beta$, and that equn. (7) becomes effectively

$$
\begin{equation*}
\frac{\Delta q}{q}=-\frac{1}{2} \cdot \frac{\Delta \beta}{\beta} \tag{11}
\end{equation*}
$$

This result also is satisfactory, as it again shows that the circuit does not exaggerate changes in component values.
Because for a passive $C R$ network $q_{0} \ngtr \frac{1}{2}$, and often because of practical constraints is considerably $<\frac{1}{2}$, equn. (5) shows that even for a moderate value of $q$ (say $q=5$ ) a quite high minimum value of $A$ is needed. Consequently in a "designable" circuit, where a higher intrinsic gain will be used than the minimum needed, the gain used may be of the order 1,000 or more. This may seem a high price to pay. Nevertheless the two-lag loop (if the high-pass equivalent is included) is the basis of all the preferred methods of realising active filters -because of the low sensitivity to errors in component values. This low sensitivity derives from the fact that if $A$ is a real number; i.e., shows no appreciable phase shift over the band of frequencies for which the magnitude of the loop gain is $\geqslant 1$, the system is essentially stable no mapter what variations there may be in gain or in component values. This is made clear by the Nyquist plot for the ideal loop. Each lag contributes a maximum phase shift of $90^{\circ}$, and together they give a cardioid-


Fig. 5. Block diagrams for synthesis of feedback loops containing two lags, or their analogue (two leads, or two "tuned circuits").
shaped curve as shown in Fig. 4. The curve does not cross the horizontal axis, the limiting phase shift being $180^{\circ}$, and so can never encircle the point I , jo.

The results of this analysis of the two-lag loop are summarized in the block diagrams of Fig. 5, which can be useful as the starting point for some practical designs, particularly of bandpass filters using the low-pass to bandpass transformation rules.

Equns. (4) and (5) give the initial value $T_{0}$ that must be chosen to give a closed-loop value $T$ as

$$
\begin{equation*}
T_{0}=q T / q_{0} \tag{12}
\end{equation*}
$$

and the value of gain, $A$, required to raise $q_{0}$ to $q$ as

$$
\begin{equation*}
A=\left(q / q_{0}\right)^{2}-1 \tag{13}
\end{equation*}
$$

These results are incorporated in Fig. s(a). When the passive network can be represented as two equal isolated lags, Fig. $s(\mathrm{~b}), q_{0}=\frac{1}{2}$, and $q / q_{0}=2 q$. Consequently $T_{0}=2 q T$, and $A=4 q^{2}-1$. Where there are two unequal lags, they may be multiplied together and treated as case (a). Since $q_{0}$ will be $<\frac{1}{2}, A$ will be greater than for case (b).

The discussion of two simple lags and gain may appear to be an out-of-date approach when it is already known that many practical circuits are going to be built around high-gain operational amplifiers used as integrators. But loop gain is of such fundamental importance to the design of an active filter, that it is always necessary at least to know that enough has been provided to satisfy a given specification. A high-gain integrator is easily shown to be equivalent to a lag and gain, and the results of this section will be found to provide a unified basis for the analysis of a wide range of problems.

## A lag-lead network, or network with "tuned-circuit" response

The transfer function for tuned-circuit response, with centre frequency $\omega_{0}=1 / T$, $Q$ factor $q_{0}$, and normalized to unity gain at the centre frequency is

$$
\frac{\frac{1}{q_{0}} p T}{1+\frac{1}{q_{0}} p T+p^{2} T^{2}}
$$

Except that the gain at the centre frequency is always less than unity, the transfer function of a passive $C R$ lag-lead network is of the same form and may be represented as in Fig. $6, k<$ I. (See Part 3,equn. (23) and Table I.)

Substitution in equn. (2) gives for the transfer function with the feedback loop closed:

$$
\begin{align*}
\frac{V_{\text {out }}}{V_{\text {in }}} & =\frac{\frac{k K}{q_{0}} p T}{1+\frac{1}{q_{0}} p T+p^{2} T^{2}-\frac{k K}{q_{0}} p T} \\
& =\frac{\frac{k K}{q_{0}} p T}{1+\frac{1-k K}{q_{0}} p T+p^{2} T^{2}} \tag{14}
\end{align*}
$$

This shows that the feedback leaves the centre or resonant frequency unaltered (which was to be expected from consideration of symmetry), and increases the $Q$ factor [if $0<k K<I$ ], since now

$$
\begin{equation*}
q=q_{0} /(1-k K) \tag{15}
\end{equation*}
$$

Clearly as $k K \rightarrow 1$ the increase in $q$ becomes very great, and when $k K>1$ the $Q$ factor becomes negative and the circuit will oscillate. The system is, in fact, equivalent to the familiar application of "reaction" to a tuned circuit in a simple radio receiver. As a method of increasing $Q$ factor, and gain at the centre frequency, the system is very effective, but likely to be tricky unless means can be found to stabilize the performance.

The sensitivity to small relative changes in loop gain is easily derived from equn. (15) by differentiation and substitution as

$$
\begin{equation*}
\frac{\Delta q}{q}=\frac{\Delta(k K)}{k K}\left(\frac{q}{q_{0}}-1\right) \tag{16}
\end{equation*}
$$

When $q \gg q_{0}$ relative changes in loop gain are exaggerated by the factor $q / g_{0}$ approximately, and this is a useful warning if $q_{10}$ and $k$ may be taken as constant and $K$ is the factor most susceptible to uncontrolled changes.

The same conclusion can be deduced from the Nyquist plot, which, as shown in Fig. 7, is a circle passing through the origin, the diameter $O D$ representing $k K$ the loop gain at the centre frequency. When $q / q_{0} \gg I_{2}$ $\mathrm{OD} \rightarrow \mathrm{I}$, since as equn. (IS) tells us, $q / q_{0}=1 /(1-O D)$. Small changes in OD then give much greater relative changes in the gain margin ( $1-O D$ ) and consequently large changes in performance over a band of frequencies corresponding to a section of the plot centred on the point $D$; i.e., at and around $\omega_{0}$

However, when a gain factor critically affects performance, the factor and consequently the performance may (and should) be stabilized by feedback, as is well known (see equans. (8), (9), et sequ.). Then $K \rightarrow I / \beta$ very nearly, and $\beta$ is typically determined by two resistors as shown in Fig. 8, so that

$$
\begin{equation*}
K=1 / \beta=\left(r_{1}+r_{2}\right) / r_{1} \tag{17}
\end{equation*}
$$

and the sensitivity of $K$ to changes in $r_{1}$ and $r_{2}$ is given by

$$
\begin{equation*}
\frac{\Delta K}{K}=-\frac{\Delta r_{1}}{r_{1}}\left(1-\frac{1}{K}\right) \tag{18}
\end{equation*}
$$

and a similar expression (without the prefixed minus sign) for $\Delta r_{2} / r_{2}$.

When $K \gg 1$ changes in $r_{1}$ and $r_{2}$ cause proportional changes in $K$, and so, because of the magnification of errors in $K$ shown by equn. (16) for $q \gg q_{0,}$ working in this region necessitates holding $\left(r_{1}+r_{2}\right) / r_{1}$ to a much tighter tolerance than the required tolerance on $q$. Even when $K=2,\left(r_{2}=r_{1}\right)$, changes in either resistance cause changes in $K$ which are relatively only half as great. Admittedly accurate and stable resistors are not difficult to come by, but as a general principle it is preferable to avoid this region. When $K \rightarrow 1, \quad\left(r_{2} \ll r_{1}\right)$, the sensitivity of $K$ to changes in $r_{1}$ and $r_{2}$ becomes very small; and of great interest is the limiting condition when $100 \%$ negative feedback is applied, then $\beta=1, r_{2}$ dis-
appears, and $K=A_{\mathrm{v}} /\left(A_{0}+1\right)$, thus $K \rightarrow \mathbf{1}$ as $A_{11} \rightarrow \infty$ and does not depend on the accuracy of any component. Performance is still affected by $k$ and $q_{0}$, and as these are in general mutually dependent, the system will now be analysed explicitly as a loop containing a lead-lag network.

If the frequency-dependent network can be represented by the lead-lag transfer function

$$
\begin{align*}
& \frac{p T_{2}}{1+p T_{2}} \cdot \frac{1}{1+p T_{1}} \\
& =\frac{p T_{2}}{1+p\left(T_{1}+T_{2}\right)+p^{2} T_{1} T_{2}} \\
& k=\frac{T_{2}}{T_{1}+T_{2}}, \text { and } q_{0}=\frac{\sqrt{T_{1} T_{2}}}{T_{1}+T_{2}} \tag{21}
\end{align*}
$$

Hence, substituting in equn. (15), we find

$$
\begin{align*}
q & =\frac{\sqrt{T_{1} T_{2}}}{T_{2}(1-K)+T_{1}}  \tag{23}\\
& =\frac{1}{x(1-K)+\frac{1}{x}}\left[\text { where } x=\sqrt{\frac{T_{2}}{T_{1}}}\right] \tag{24}
\end{align*}
$$

When $K<\mathrm{I}$, this expression is of a familiar form and gives

$$
\begin{equation*}
q_{m a x}=\frac{1}{2 \sqrt{1-K}} \tag{25}
\end{equation*}
$$

when the ratio of time constants

$$
\begin{equation*}
x^{2}=\frac{1}{1-K} \tag{26}
\end{equation*}
$$

Thus when $K=\frac{3}{4}, q_{\text {max }}=1 ; \quad K=\frac{1}{1} \frac{5}{6}$, $q_{\text {max }}=2 ; K=\frac{63}{64}, q_{\text {max }}=4$; etc. This behaviour is shown in the lower and righthand half of Fig. 9.

When $K=\mathrm{I}$, there is no maximum and

$$
\begin{equation*}
q=x=\sqrt{\frac{T_{2}}{T_{1}}} \tag{27}
\end{equation*}
$$



Fig. 6. Positive gain and a network with "tuned-circuit" response, given by equn. (14).


Fig. 7. Nyquist plot for positive-feedback loop containing lead-lag network.


Fig. 8. Positive-gain amplifier with gain stabilized by feedback.

Fig. 9. Illustrating equn. (25). Shows the effect of the gain $K$ and the ratio $T_{2} / T_{1}$ on a lead-lag loop with positive gain.


As already mentioned we can make $A \rightarrow I$ very closely by applying $100 \%$ negative feedback to a high-gain amplifier, as for example by the emitter-follower connection. Provided that the $Q$ factor aimed at is not too close to $q_{m a x}$, as given by equn. (25), performance depends almost only on the ratio of the two time constants. The information about $q_{\text {max }}$ contained in equn. (25) is perhaps easier to interpret if we substitute $A_{0} /\left(A_{0}+1\right)$ for $K$ [where $A_{0}=$ internal gain]. The equation then becomes

$$
\begin{equation*}
q_{\max }=\frac{1}{2} \sqrt{ }\left(A_{0}+1\right) \tag{28}
\end{equation*}
$$

This result is the same as that deduced for two lags and negative gain, equn. (5), when $q_{0}=\frac{1}{2}$ (the maximum possible value), and $A=A_{\mathrm{o}}$ (the full internal gain of the amplifier); and the identity demonstrates that in circuits which do not exaggerate the effect of component tolerances as $q$ is raised there is no substitute for amplifier gain. When

$$
\begin{equation*}
K>1, q=\infty \text { when } x^{2}=1 /(K-1) \tag{29}
\end{equation*}
$$

This is shown by the curves in the upper and left-hand part of Fig. 9. By choosing $K$ correctly high $Q$ factors can be obtained with any value of $T_{2} / T_{1}$. But in general in this region, except close to the diagonal representing $K=1$, it can be seen from the shape and spacing of the curves that high values of $Q$ factor are obtained at the expense of high sensitivity to both $K$ and the ratio $T_{2} / T_{1}$; i.e., the faftiliar disadvantages of positive feedback appear.

## Active filters using a balanced parallel-tee network

It has been shown in Part 3 that the paralleltee network consist of a low-pass network and a high-pass network connected in parallel; and also that if the input voltage is introduced at the foot of the tees bandpass response is obtained and the network may be analysed as a lag-lead network and a lead-lag network in parallel. The existence of these parallel paths gives the parallel-tee network some special properties which can be useful. But, in general, filter circuits using the parallel-tee network contain, from one point of view, redundant components; i.e., they contain more components than the minimum necessary to obtain the specified order of response. Synthesis and analysis depend on the assumption that the six components of the network are accurately matched. Such circuits therefore fall outside the main theme of this series. They do, however, show a very modest gain requirement for a given $Q$ factor compared with the two-lag loop. It is of interest, therefore, to derive the relation between $q$ and available loop gain for the feedback system shown in Fig. 10(a). The notion behind the setting up of such a system is, of course, that as feedback is increased the response at high and low frequency is depressed and the $-3 / \mathrm{dB}$ points move closer together.

The effect is shown in Fig. 10(b), which is drawn for the situation where $A$ is constant and the feedback fraction $\beta$ is the parameter which is varied. The figure has been drawn for $q_{0}=\frac{1}{2}$, the greatest value that can be
obtained from a passive $C R$ network: in practice $q_{0}$ is likely to have a lower value, say $\ddagger$ (see Part 3).

By setting $\beta=1$, so that the zerofrequency loop gain is simply $=-A$, and substituting in equn. (2), we find

$$
\begin{align*}
\frac{V_{\text {out }}}{V_{\text {in }}} & =\frac{-A\left(1+p^{2} T^{2}\right)}{1+\frac{1}{q_{0}} p T+p^{2} T^{2}+A\left(1+p^{2} T\right)^{2}} \\
& =-\frac{A}{A+1} \times \\
& \frac{1+p^{2} T^{2}}{1+\frac{1}{q_{0}(A+1)} p T+p^{2} T^{2}} \tag{30}
\end{align*}
$$

which shows that

$$
\begin{equation*}
q=q_{0}(A+1) \tag{31}
\end{equation*}
$$

or

$$
\begin{equation*}
q \simeq q_{0} A, \text { when } A \gg 1 . \tag{32}
\end{equation*}
$$

Thus $q / q_{0} \propto A$, and consequently for $q / q_{0} \gg \mathrm{I}$ a much smaller value of $A$ is required than in a two-lag loop (where $\left.q / q_{o} \propto A^{1}\right)$.

The linear relationship between $q$ and $A$ gives

$$
\begin{equation*}
\frac{\Delta q}{q}=\frac{\Delta A}{A} \tag{33}
\end{equation*}
$$

or

$$
\begin{equation*}
\frac{\Delta q}{q}=\frac{\Delta q_{0}}{A_{0}} \cdot \frac{A}{A_{0}} \tag{34}
\end{equation*}
$$


(a)

(b)

Fig. ro. (a) Feedback loop containing parallel-T network. (b) Shows increases in $Q$ factor by application of feedback.
when $A$ is obtained from an amplifier of high gain, $A_{0}$, to which additional negative feedback is applied.

It can hardly be emphasized too strongly, however, that performance is sensitive to unbalance in the parallel- $T$ network, and that consequently errors in component values can easily invalidate the results derived above.

## Loop gain and through gain

It is the nature of the closed feedback loop that determines the inherent characteristics of the resulting resonant circuit, viz. the undamped resonant frequency and the $Q$ factor, which manifest themselves in the denominator of transfer functions of the type $F(p)=V_{\text {out }} / V_{\text {t }}$. It is, of course, often possible to enter or leave the circuit in several ways, and this gives a choice of numerator functions. But provided all voltage sources are of effectively zero internal impedance so that they do not alter the impedances of the branches into which they are introduced, and that all output voltages are observed without adding any appreciable shunt admittance,* the denominator of $F(p)$ is invariant, being a reflection of the natural motion of the circuit (i.e., of the way in which transients decay).

In simple cases the nature of the transfer functions obtained from the various possible connections can often be predicted from inspection of the circuit. Thus, for example, in Fig. II(a) for an input $V_{1}$ there is a two-lag network between input and output, and the response is low-pass. For an input
${ }^{\text {a }}$ There are parallel arguments for current sources and current outputs.


Fig. It. Showing how a change in the position of the input can convert a low-pass filter to band-pass and vice versa.


Fig. 12. Active parallel-T system with alternative input connections.
$V_{2}$ there is a lead-lag network between input and output, and the response is simple band-pass (or "tuned-circuit"), with (of necessity) $T(=1 / 1, \mathrm{c})$ and $q$ the same as for the response to $V_{1}$. Similarly in Fig. 11(b) for an input $V_{1}$ there is a lead-lag network between input and output, and the response is simple band-pass: for an input $V_{2}$ there is a two-lag network between input and output, and the response is low-pass. These properties are not peculiar to active networks, and examples of the multiple responses that can be obtained from a passive network have been given in Part 3.

For each circuit, if one transfer function is known, simple reasoning will lead to the others. Thus we already know that for Fig. $\mathrm{ro}(\mathrm{a})$ the transfer function for an input $V_{1}$ is, using equn. (3), and in Part 3 equn. (3) and Table I
$\frac{V_{\text {out }}}{V_{1}}=-\frac{A}{A+1} \cdot \frac{1}{1+p T / q+p^{2} T^{2}}$
where

$$
\begin{aligned}
& T=\sqrt{\frac{C_{1} C_{2} R_{1} R_{2}}{A+1}} . \\
& q=\frac{\sqrt{(A+1)\left(C_{1} C_{2} R_{1} R_{2}\right)}}{C_{1} R_{1}+C_{1} R_{2}+C_{2} R_{2}}
\end{aligned}
$$

and we can derive the transfer function for $V_{2}$ from this equation by finding a relation between $V_{1}$ and $V_{2}$ and substituting.
$V_{1}$ can be replaced by a current source $V_{1} / R_{2}$ in parallel with $R_{2}$, and $V_{2}$ by a current source $V_{2} p C_{2}$ in parallel with $C_{2}$. The two current sources are effectively connected between the same two nodes (the output impedance of the amplifier being by definition zero) and so will give the same output if they are equal to one another, $V_{1} / R_{2}=V_{2} p C_{2}$. Hence the wanted relationship is $V_{1}=V_{2} p C_{2} R_{2}$, and the required transfer function

$$
\begin{equation*}
\frac{V_{\text {out }}}{V_{2}}=-\frac{A}{A+1} \cdot \frac{p C_{2} R_{2}}{1+p T / q+p^{2} T^{2}} . \tag{36}
\end{equation*}
$$

For Fig. Io(b) we have, from equns. (14), (15), and Table I of Part 3

$$
\begin{equation*}
\frac{V_{\text {out }}}{V_{1}}=\frac{k K p T / q_{0}}{1+\frac{1}{q_{0}}(1-k K) p T+p^{2} T^{2}}, \tag{37}
\end{equation*}
$$

where
$k=\frac{C_{2} R_{2}}{C_{1} R_{1}+C_{1} R_{2}+C_{2} R_{2}}$,
$\frac{1}{q_{0}}=\frac{C_{1} R_{1}+C_{1} R_{2}+C_{2} R_{2}}{\sqrt{ }\left(C_{1} C_{2} R_{1} R_{2}\right)}$,
$T=\sqrt{ }\left(C_{1} C_{2} R_{1} R_{2}\right)$
i.e.
$\frac{V_{\text {out }}}{V_{1}}=\frac{K p C_{2} R_{2}}{1+\frac{1}{q_{0}}(1-k K) p T+p^{2} T^{2}}$.
By the method of the previous paragraph we then find $V_{2}=V_{1} p C_{2} R_{2}$, and consequently

$$
\begin{equation*}
\frac{V_{\text {out }}}{V_{2}}=\frac{K}{1+\frac{1}{q_{0}}(1-k K) p T+p^{2} T^{2}} . \tag{39}
\end{equation*}
$$

Superficially this 1.p. transfer function suggests that gain is not stabilized by feedback. In a practical situation, however, we should have $K=A_{0} /\left(\beta A_{0}+1\right)$, where $\beta A_{0} \gg 1$.

To keep the analysis as simple as possible Fig. Io(a) was drawn with the parallel-tee network in the forward path. To obtain "tuned-circuit" response the input, now called $V_{2}$, could be reconnected as in Fig. 19 (Part 3), leading to the arrangement shown in Fig. 12. Other examples of the multiple-response potentialities of one basic loop will be found in later parts

## R. F. amplifier for f.m. tuner

In reply to the letter in last month's issue regarding the problem of radiation from the local oscillator of the integrated circuit f.m. tuner described in the June issue, the author (G. J. Newnham), stated that a suitable r.f. amplifier was being prepared. Below we give the circuit diagram and layout he has supplied.


The 90 MHz amplifier employs a $316-04$ i.c. made by Marconi-Elliott Microelectronics. Both coils consist of five turns of $18 \mathrm{~s} . \mathrm{w} . g$. (0.3in diameter, 0.25 in long), and $L_{1}$ is centre-tapped.

## BAILEY AMPLIFIER REPRINT

In our September issue we announced that the reprint of the articles by Dr. A. R. Bailey on his $20-\mathrm{W}$ and $30-\mathrm{W}$ amplifiers and pre-amplifier "will be on sale within the next month". We regret that plate-making and printing difficulties have seriously delayed publication. It now seems likely that the reprint will not be available until the end of November. We apologise to the many readers whose orders have not been executed.

## New Books

Transistor Audio and Radio Circuits, from Mullard, is a manual of established and practical circuits for use by radio and audio service engineers, equipment manufacturers, students and home constructors. A wide range of circuits, from portable radio receivers to high-quality amplifiers is presented in detail and a chapter is devoted to test equipment. The chapter headings are: silicon and germanium transistors; basic h.f. circuits; basic a.f. circuits; radiograms, record players and portable radios; tape recorders; car radios; high-quality audio equipment; high-quality f.m. tuners; test equipment. Appendices cover biasing arrangements for h.f. circuits, B.B.C. test-tone transmissions, and six data charts and nomograms. Pp. 205. Price 30s, (p. and p. 2s.) Mullard Lid, Mullard House, Torrington Place, London W.C. 1 .

Servicing with the Oscilloscope, by Gordon King, presents the oscilloscope, from a practical standpoint, as a valuable aid to servicing and fault-finding in radio, television and audio equipment, including the latest stereo-radio and colour television circuits. The illustrations include many photographs of oscilloscope traces encountered when testing both faulty and correctly operating equipment. Pp. 176 including a three-page index. Price 28s. Butterworth \& Co. (Publishers) Ltd, 88 Kingsway, London W.C. 2 .
Hi-Fi and Tape Recorder Handbook, by Gordon J. King, is based on the author's previous book The Practical Hi-Fi Handbook published by Odhams Books in 1959 and now out of print. There are fifteen chapters written in a technically uncomplicated manner. The first chapter discusses special terms in the audio vocabularyincluding decibel, phon, and harmonicsand explains the principles of recording and of stereophony. The rest of the book expands all these terms in relation to voltage amplifiers, valve and transistor power amplifiers, loudspeakers and disc and tape systems. The final chapter is on video tape-recording. Detailed circuits and photographs of commercial equipment are used in the discussions. There are two appendices-on amplifier specifications, and on test tapes and recordsand a good index. Pp.304. Price $\{2$. Butterworth \& Co. (Publishers) Ltd, 88 Kingsway, London W.C. 2.

Glide Path, by Arthur C. Clarke, recalls the struggles of a group of scientists, flyers and specially trained servicemen to perfect a radar talk-down system for planes during World War II. This novel is not prophetic, but documents a rapid and important technical development in communications. Pp. 229. Price 30s. Sidgwick \& Jackson Ltd, 1 Tavistock Chambers, Bloomsbury Way, London W.C.1.

# Living with Hi-Fi 

## A wife's definition of 'tolerance'

by Heather Dinsdale

Although I have a great deal of sympathy for wives whose husbands seem to be married to a car, or a fishing rod, or a set of golf clubs, I claim a special consideration for those poor wives like myself whose husbands are dedicated to sound reproduction (I use the phrase advisedly) in any shape, form or size. To start with, all the work has to be done indoors; there is none of this banishing him to the garage, the river or the golf links. The


Husbands . . . dedicated to sound reproduction
hi-fi units invade the whole house, interconnected with long snake-like cables which are always placed just inside doorways for the unwary wife and children to trip over. The mess is not even confined to the visual senses; the most execrable sounds literally shake the house from time to time, especially when the baby has just been put to bed. This is all performed in the name of the great god hi-fi. ("I'm sorry, but the baby will just have to get used to it.")

The sheer size of the loudspeakers is another thing. Before we got married I was given my annual brainwashing at the Audio Fair, and I gradually learned that large loudspeakers sound better than small. My great mistake was to admit this. Now, my protests that we are being crowded out of house and home by bigger and bigger speakers are countered by impossible rationalizations. ("But you did say at the Audio Fair that those huge horns sounded very good.")

It is bad enough giving house room to completed hi-fi units; up to a point they
have their uses for standing vases of flowers on, but the flowers mysteriously disappear shortly before the whole house shakes to the closing scene of "Götterdämmerung". (Presumably the vases would shatter if they were left in the room.) But those of you who think that I am being unreasonable have not had to live with an amplifier through all its stages from design and development to demonstration. There are, in fact, five distinct phases: design, development, testing, manufacture and demonstration.

The design phase begins quietly. It is characterized by my hustand developing an increasing absent-mindedness and loss of memory where household chores (e.g. wash-ing-up) are concerned. For some reason this loss of memory does not apply to meal-times. Scraps of paper covered in hieroglyphics are left all over the house, and the slide-rule features prominently. The postman staggers up the drive laden with manufacturers' catalogues, and I find myself taking down meaningless telephone messages. Isn't it funny how the 'phone always rings while I'm feeding the baby; perhaps I ought to tell Mrs. Parkinson!

## Testing

Once the design is completed, development can begin. This is normally done on the floor. I have carried out a careful research pro-
gramme on the action of vacuum cleaners, and I can now report that resistors and transistors are always sucked up in preference to dirt and dust. ("Have you seen a thing looking like a little striped shrimp? It's gone where? But that was part of a matched set-took me hours. You'll have to empty the bag.") During the development phase, various instruments with small television screens appear and stand around the room. These offer infinite attraction to the children. ("Don't touch that-it's Daddy's. Yes, that's a green snake. No, you mustn't feed it.") I have discovered that there is a technique for getting solder out of carpets, but not for removing the actual burn mark. We have solved this latter problem by using a dark brown rug, and the smell of burning hair disappears quite quickly if you leave the windows open. At one time I got very upset when I thought he wanted to use the breadboard, but I know now that a breadboard is not a board, and has nothing to do with bread, either. Once the breadboard has been made, we start the testing phase. Previously, testing has consisted of making measurements on meters but now the ears are assaulted. Certain records have been earmarked (sic) 'demonstration quality' and these are played at varying volumes, with small modifications made to the amplifier between each test. I must admit that some of these records do sound extremely good-in moderation. Unfortunately, after it has been struck about 12 times in the hour, Donner's hammer (in "das Rheingold") seems to take up residence in my head. When we lived in a flat, the neighbours downstairs remarked one day on the apparent proximity of the railway station. I hadn't the heart to explain that we had recently invested in a Transacord recording of Pacifics (whatever they may be), and we were "just trying it out". It is, incidentally, an interesting and valuable fact that both our children enjoy very loud sounds, but it doesn't help in the subjective assessment of noise levels. ("But Darling, how can I hear if there is any hum or hiss if the baby's bawling in the background.")

When the tests have been finished we may go back to the drawing board, in which case the whole rigmarole I have described is liable


to be repeated. Otherwise, we proceed to manufacture. I must admit that the units finally produced look quite presentable. Thank goodness that the breadboards don't last for ever!

## Manufacture

Manufacture requires extensive use of the kitchen table for "metal bashing". ("Can't possibly use the garage-too damp and draughty.") The metal arrives as large sheets, and is first carefully marked out. Next the holes are drilled on the table or the floor as convenient, using a thick board as a back. ("I'm afraid the drill missed the board, Dear. I don't think the hole is too noticeable.") I once thought that drilling was the final operation, but no! Most of these little holes are pilots. Some of them have to end up square, and these produce the worst sound of all. A small vice is clamped to the kitchen table, and the small holes are opened out using hacksaws and files. The screeching sound is really dreadful. It fills the head, and seems to continue long after the work has been completed. A thin film of metal dust covers everything for days afterwards. After the holes have been cut, the metal is bent (blessed relief, this operation is silent), and we come to painting. Normally I quite like the smell of paint, but the crackle-finish paint with which all the metal work is treated has the most horrible odour. I was intrigued at the beginning to see whether the attractive crackle finish came straight out of the tin, and was disappointed to see that it looked just like conventional paint. Then the awful truth slowly dawned on me. The paint had to be treated in the gas cooker-my cooker-and despite my protests, the horr-
ible smelly paint was bundled into the oven. I carefully examined the oven after the operation, and mercifully the smell had disappeared. The Sunday joint tasted just as good as ever the following day, so now we cure crackle paint quite regularly. ("Don't know what you were rabbiting about! It must be done in the oven, whether it smells or not.")

The little components are fixed on to printed circuit boards, which first have to be designed. After a roughly pencilled layout, adhesive black tape is carefully stuck in position, along with small circles and other rather rude-looking shapes. This process can be carried out anywhere, including railway carriages and even in bed. Unfortunately it leaves a trail of short black suicky pieces wherever it goes. Removing short pieces of sticky tape from the carpets is even more difficult than removing solder, and it is hard to keep the children away from it. Luckily, this phase does not last long, but when the boards come back, all cut and drilled, I must say goodbye to the kitchen table again. Soldering irons are very useful for determining the melting point of plastics. We soon discovered that plastic tablecloths melt easily and give off an obnoxious smell when burnt, and we now have a selection of household articles, including an alarm clock, a salad fork and a toy duck all with neat round holes depicting the path of the soldering iron.

If anyone asks me what is the most effective domestic missile, I reply without hesitation: wire ends from cutting resistor leads to size. The short wires boomerang back and forth across the room, and it is only by sheer good fortune that the whole family have not sustained serious injuries. The wires lodge in the most unusual places and continue to


This process can be carried out anywhere . . . even in bed!
turn up months after the exercise in ballistic missiles has finished. I found many years ago as a child that the most effective way of locating dropped drawing pins is to crawl around on hands and knees. I can report with feeling that the best way of finding dropped wire ends is to sit on the upholstered fumiture without too many clothes on.

## Demonstration

When manufacture has been completed, we come to the final phase: demonstration. This resembles the earlier testing phase, but is more intensive. In addition, visitors turn up at the most unexpected times to "hear the new amplifier". We also have long listening sessions while minute adjustments are made. At about this time, I begin to think that perhaps it has all been worthwhile, because of the fine musical results. We have also met a number of interesting people and been in correspondence with many more.
I read once of some advice to young girls thinking of marriage: "Don't, but if you must, don't marry an engineer." If you marry an audio engineer, be prepared for a completely different way of life, governed by the everlasting search for better sound quality, in which all normal domestic planning is


Advice to young girls . . . don't!
subordinate to loudspeaker positioning and the need to allow the designs to appear. In every engineer there is a designer trying to get out, and if you try to inhibit him, then sullenness sets in, leading to moroseness and maybe a lot worse.

I must conclude: he's been muttering for some weeks about designing a colour television set, and I am getting more and more worried about what this might entail. I might as well not bother; if he has decided to do it, then it must be done, and a mere wife is powerless to stop it. At least our test-cards will be in colour (I doubt if he will have time for actually watching programmes) and as the work proceeds the sound of metal-bashing, the smell of burning plastic, and the barrage of small wires will ensure that I know exactly what he is doing.

I wonder what the children will be when they grow up?

# Transistor Distortion Characteristics 

# The performance of transistors in voltage amplifying circuits 

by J. L. Linsley Hood

Developments in transistor manufacture have led to the ready availability of inexpensive devices. In particular, the planar silicon types (which are characterized by high gain, low leakage current, low noise and good high frequency characteristics) allow the construction of a.c. amplifying circuits having a performance which is better than all but the best of existing valve circuits.

Unfortunately, when transistors are used as voltage amplifiers the shape of the base voltage/collector current characteristics gives rise to waveform distortion, and the conditions which are most favourable for high stage gain and high input impedance (high collector load impedance, low $I_{c}$ ) are also those which lead to high levels of (predomimantly second-harmonic) distortion.

The performance of five different silicon transistor types is shown in Figs.1-3, and that of two germanium types in Fig.4, as measured at 1 kHz using circuit A . In each case the actual value of the emitter bias resistor was adjusted so that the collector voltage was equal to half the supply voltage.

In general, the higher the current gain of the transistor, and the larger the collector load resistor, and the output voltage as a proportion of the supply voltage, the greater the total harmonic distortion. Also, as would be expected from the $I / V$ curves, the silicon transistors gave higher distortion levels than the germanium types, and also, in the cases examined, had higher current gains.

No significant difference in performance was observed between different transistors of the same type having similar current gains, although those of planar construction gave a somewhat higher gain/distortion ratio than those with diffused junction.

This type of non-linearity is important, for example, in audio pre-amplifier tone control circuitry, where compensation networks in the negative feedback path are employed as in circuit B, to modify the gainfrequency characteristics. At the mid-point frequency of such an amplifier, the gain may be unity and the distortion factor consequently very low, but where the feedback is reduced in order to obtain, say, treble or bass lift, the output distortion will increase by the same amount.

Also, conventional audio power amplifiers may require an input signal of the order of $0.6-1.0 \mathrm{~V}$ r.m.s. (equivalent to $1.7-2.8 \mathrm{~V}$ peak to peak) and as can be seen from Figs.1-3, a simple transistor amplifier of the type shown


Fig. 1. Curves of total harmonic distortion against output voltage for a Mullard $n-p-n$ silicon BC109 with $\mathrm{h}_{\mathrm{fe}} \simeq 300$.
$\mathrm{h}_{\mathrm{fe}} \simeq 300$.
Circuit A.

$$
\int^{2} \underset{V_{\text {out }} \text { (Peak to peak) }}{4}
$$

Fig. 2. Broken-line curve for Motorola n-p-n silicon 2N3904 with $\mathrm{h}_{\mathrm{fe}} \simeq$ 200. Other curves for Motorola $p-n-p$ silicon
2N 3906 with



Fig. 3. Curves for Ferranti $n-p-n$ silicon $2 N 697$ with $\mathrm{h}_{\mathrm{fe}} \simeq 80$, and Texas Instruments $n-p-n$ silicon 2 N3707 with $\mathrm{h}_{\mathrm{fe}} \simeq 180$. Circuil $A$.

in circuit A would introduce $1-2 \%$ harmonic distortion. If $0.1 \%$ total harmonic distortion is the target figure, the largest output which could be obtained from such a circuit would be some 180 mV peak to peak, equivalent to some 60 mV r.m.s.

The use of negative feedback improves matters, but the reduction in distortion is accompanied by a reduction in gain. Using a higher supply voltage will increase proportionately the output signal voltage available at a given distortion level, and a single stage amplifier of this type, such as shown in circuit C , operating from a 15 V supply rail and designed to have an output of 1 V r.m.s. at $0.1 \%$ t.h.d., has a stage gain of only 4 or 5 .

Since the reduction in the distortion is more nearly equal to the reduction in gain when the open loop gain is high, a better answer is to use a two-stage amplifier, such as that shown in circuit D. Here the output transistor is operated under favourable conditions, with a fairly low value of collector load resistance, and with an input circuit of fairly high impedance, while the input transistor is only required to deliver a small output voltage swing. The open loop gain of the circuit is approximately 8000, and the total harmonic distortion over the frequency range 20 Hz to 20 kHz is less than $0.04 \%$ at 8 V peak to peak. Since the stage gain is determined by $\left(R_{1}+R_{2}+R_{3}\right) / R_{1}$, if $R_{1}$ is reduced the gain (and distorion content) will be proportionately increased. For example, if $R,=20 \Omega$, the stage gain will be 100 , and the distortion factor at 8 V peak to peak will be $0.1 \%$.

The use of such a circuit as the final stage of an audio pre-amplifier ${ }^{\text {- }}$ allows the preceding stages to operate at lower output voltage levels, with advantage in terms of harmonic distortion. Further, several such stages could be used in cascade, with passive $R C$ or $L C$ networks, for tone control purposes.

[^3]Announcements
'Sound 70 International' is the title being given to next year's exhibition of the Association of Public Address Engineers. It will not be held at Harrow as in the past but at the Camden Town Hall, Euston Road, London N.W.1, from 10th to 12th March.

The 1st International Exhibition of Recreation and Leisure will be held in Geneva, Switzerland from May 28th to June 7th 1970. The organizers are making a special feature of amateur radio activities.

The British Computer Society is moving its headquarters from Dorset Square to 29 Portland Place, London W.1.
"Talking About Colour Television" is the title of the latest filmstrip produced by the Mullard Educational Service. The film is intended for students with a working knowledge of monochrome television and is available, with a 54 -page teacher's book, from The Slide Centre Ltd, Portman House, 17 Brodrick Road, London S.W. 17.

RCA has announced plans to invest more than $\mathbb{C} 375,000$ in a new plant in Jersey, Channel Islands, as an improved base for expanding its commercial electronic products activities in Europe.

ITT Components Group Europe has opened a new branch office at 28d Glenacre Road, Cumbernauld, Scotland.

GNT Automatic A/S (has moved from St Helens Place, London, to 10 College Road, Harrow, Middx. (Tel: 01-863 4378).

Guest Electronics Lid., Nicholas House, Brigstock Road, Thornton Heath, Surrey, will in future be known as Guest International Lid.

Davall Electronics Led, which was recently acquired by Erie Electronics Lid, South Denes, Greal Yarmouth, Norfolk, has been re-named Eric Controls Lid.

Crouzet (England) Lid, of Brentford, Middx, announce that they are changing their name to Crouzet Litd and will shortly be adding aerospace electronics and process control equipment to their products.

Alfred Imhof Ltd have announced that conditional contracts have been exchanged whereby their parent company Parnell Investments Lid will acquire the entire issued share capital of Bedco Lid. There will be a single trading company called Imhof-Bedco Lid.

Danish agents. SEMCO, of Copenhagen, have been appointed agents for components manufactured by Electrosil Lid, Pallion, Sunderland, Co. Durham.
A Canadian company is being formed jointly by International Computers Lid and International Management Associates. The company, International Computers (Canada) Lid, will have exclusive rights to market the I.C.L. 1900 Series computers in Canada.

Technical Measurement Corporation (U.K.) Lid, 14 Yeading Lane, Hayes, Middx, have been appointed European distributors for Nuclear Equipment Corporation, of California, manufacturers of solid-state deeectors and preamplifiers, non-dispersive x-ray photon spectrometers and NIMAMP operational amplifiers for nuclear applications.

V-F Instruments Lid, Gloucester Trading Estate, Hucclecote, Gloucester GL3 4AA, have been appointed exclusive U.K. agents for Data Device Corporation, of New York. The range of products manufactured by the American company includes: operational amplifiers, A/D converters, D/A converters, multiplexers, logarithmic modules and instrumentation amplifiers.

Racal Elektronik GmbH, 5300 Bonn, Adeuauerallee 89 a, is a new company formed by the Racal Electronic Group in Western Germany.

The Beyer microphone company of Western Germany has formed a company in the U.K. for the distribution of its products. The new company, Beyer Dynamic (G.B.), is operating from 1 Clair Road, Haywards Heath, Sussex.

The audio products of the Pioneer Electronic Corporation of Tokyo are to be markered in Britain by the Hi-Fi Division of Shriro (UK) Lid, 8 Bush I.ane, Cannon Street, London E.C.4.

Celdis Ltd, Reading, Berks, have been appointed by General Instrument (UK) Lid to market their range of semiconductors and tantalum capacitors.
An agreement has been signed between GEC-AEI (Elecironics) Lid of Stanmore, Middlesex, and Kollsman Instrument Lid of The Airport, Southampion, for the manufacture and sale by Kollsman of various types of induction digitizer. These units, developed and patented by GEC-AEI Electronics, give a digital representation of the angular position of a shaft.

The Digital Systems Department of Ferranti Lid has been awarded a contract by the Ministry of Defence valued at over $\{300,000$, for the manufacture of digital data link equipment for the Royal Navy.

Plessey Radar has received orders valued at approximately $£ 50,000$ for the WF3 windfinding radar 10 be supplied to meteorological organizations in Australia, Ceylon, Pakistan and the U.K.

Pye TVT Lid has installed an $[8,000$ closedcircuit television system for surveillance on the east and west towers of the Severn Bridge.

Redifon Lid, Wandsworth, London S.W. 18, has been awarded a contract for the manufacture and installation of eleven ship radio stations. Five stations are to be built for Canadian Pacific Steamships Lid, the remainder for the Bibby Line and ACL, the Atlantic Container Line consortium. The company is also supplying $\ell 85,000$ worth of radio equipment for twenty-six BP and Shell tankers.

Police walkie-talkies. Rank Telecommunications has received an order from the Metropolitan Police, valued at $\{122,000$, for the supply of Mitre two-way personal radio transceivers.

Plessey Telecommunications Group has received contracts worth over $\{350,000$ from the G.P.O. for eight electronic telephone exchanges.

The G.P.O. has awarded a contract worth almost \& 300,000 to Standard Telephones and Cables Lid, for the provision of a microwave radio system to transmit bulk telephone traffic and television signals between Birmingham and Bristol.

Eastern Electricity have awarded a $\int 0.5 \mathrm{M}$ contract to Ferranti for the supply of telemetry/telecontrol equipment to be used for the remote supervision and control of over 400 Eastern Electricity substations.

## Circuit Ideas

## I.C. driver for power amplifier

By virtue of its very large input and output voltage ranges and excellent common mode rejection, i.c. type 709 may be made the basis of a power amplifier. Obtaining sufficient voltage swing to drive a complementary class B output stage, is achieved by complete exploitation of the bootstrap principle. Suppose that the op. amp. gives a maximum output swing $\pm V_{o}$ and will operate with a common mode input voltage in the range $\pm V_{i}$, both $V_{o}$ and $V_{i}$ being measured relative to the op. amp. power supply in the normal way. Both sides of the op. amp. power supply are bootstrapped in phase with the output in such a way that, when the output is at $+V_{0}$ the supply has been bootstrapped up by an amount equal to $V_{i}$ so that the input is now at $-V_{i}$. Thus the total swing obtained relative to earth is $\pm\left(V_{0}+V_{i}\right)$. Typical values for a 709 running off $\pm 15 \mathrm{~V}$ supplies are $V_{0}=$ 14 V and $V_{i}=10 \mathrm{~V}$, giving a total peak-topeak swing of 48 V which should increase to about 55 V if the 709 is run at its rated limits.

This principle has been employed in the circuit shown. $C_{2}, R_{1}, R_{2}$ and the corresponding primed components cause the op. amp. power supply to be bootstrapped by about $40^{\circ}{ }_{0}$ of the output voltage, and the capacitors also provide a bootstrap for the drivers in the normal way. The d.c. voltage across the load is held by feedback to a few millivolts (the 709 input offset voltage) and the gain is such that row output is obtained from just under 200 mV input. $\quad C_{1}$ was a $500 \mu \mathrm{~F}$, reversible electrolytic, but $50 / \mathrm{F}$ would be adequate for normal audio purposes and it could probably be an ordinary, polarized component. Alternatively it could be omitted completely if one were prepared to tolerate a few tenths of a volt d.c. across the load or to trim the 709 offset voltage to zero. The diodes between the 709 inputs eliminate any possibility of latch-up occurring, and the frequency compensation components shown were found to give an adequate margin of stability in the circuit built. It was necessary to use a fairly low-impedance signal source (below about $5 \mathrm{k} \Omega$ ), otherwise strong high-frequency oscillation occurred, but


Power amplifier employing op. amp. type 709.
this is thought to be a result of the particular circuit layout employed.

The 3 dB points for the circuit given were at about 1.5 Hz and 150 kHz . Distortion was not measured, but it should be very low since the circuit has roughly 55 dB of negative feedback at low frequencies.
J. M. A. Wade

Cavendish Laboratory,
Cambridge

## Constant amplitude oscillator

A stable sinusoidal output, independent of any change in supply voltage, can be obtained using the circuit shown below. The output from the wien bridge oscillator is fed back to the gate of the f.e.t. after rectification and smoothing. Since the drain-source voltage is much less than the gate-source voltage (negative), the dynamic resistance


Uscillator giving constant amplitude sinewave output with unstable supply.
of the f.e.t. varies linearly with the latter. Any variation in supply voltage, which apparently changes the output, will change the dynamic resistance of the f.e.t. keeping the output constant. The frequency of oscillation of the circuit shown is 5 kHz . Variation in frequency is only $0.02 \%$ with a $30 \%$ change in supply voltage.
A. Basak

Chelsea College of Science \& Technology, London S.W. 3

## An invitation

If you have developed or happened upon an original circuit configuration to perform a simple or a complex operation, or have used standard components in an unconventional manner, we would like to hear from you. Send a concise description, in the form of a circuit diagram and notes, and we will consider its publication as a circuit idea. $£ 5$ is paid for each contribution published.

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# Wireless World Logic Display Aid 

# 7: Some more modifications and a description of the prototype 

designed by B. S. Crank*

This month sees the end of the description of the instrument. Next month's article, the last in this series, will be devoted to a few logic circuits that may be used with the instrument for instructional purposes. The last two possible modifications will now be described.

7: Enabling any display area to be switched to any mode of operation
This is an extension of modification 6 and the only requirement is that modification 4 should have been carried out. Four complete sets of control switches laid out as in the left hand side of Fig. 85 are incorporated. The switches are mounted in four rows, one row for each display area, and each row contains Venn, Truth, and Karnaugh control switches plus switches to control the content of the Truth table third column. The switches marked $S_{0}$ are pressed when it is desired to have no third column (two-variable Truth table) in any particular display area. The $S_{0}$ switches have no connections to them and therefore do not appear in any of the circuit diagrams, their sole purpose is to mechanically cancel the associated $\mathrm{C}=0$ and $\mathrm{C}=1$ switches.

Each row of switches fitted in this modification (do not confuse with modification 8 switches of Fig. 85) consists of two sets of three-button miniature radio switches, supplied by G.W. Smith, and as specified in the parts list for the basic instrument.

By gating the outputs of the bistables $Q$ and $W$ each row of switches is made operative for one display area only. The outputs of all the switches are then combined in gating to produce the control signals for the basic logic circuit. Fig. 86 gives the extra circuitry necessary.

The outputs of the bistables $Q$ and $W$ are combined in NAND gates $1,3,4$, and 5 to produce signals corresponding to each display area. These outputs are the negative form of the required address signal ( $\bar{Q} \bar{W}, \bar{Q} \bar{W}, \bar{Q} W$, and QW). Each of these four signals is fed to a set of three mode control switches (Venn, Truth and Karnaugh). The output of all switches for the same mode (four each for Venn, Truth and Karnaugh) are combined in NAND gates 18,20 and 21. For instance, all the Venn switches are connected to gate 18 to provide the V control signal for the main logic unit.

Imagine that the following switches are pressed, $S_{1}, S_{7}$, $S_{13}$, and $S_{18}$, and also imagine that both the X and the Y counter hold all zeros. The bistables $Q$ and $W$ will be reset so the $\bar{Q}$ and $\bar{W}$ lines will have a voltage upon them. Both inputs to gate 1 will therefore be UP and the output of gate 1 will be DOWN. Notice that the outputs of

[^4]

Fig. 85. Layout of the switches on the front panel.
gates, 3,4 and 5 will be UP because at least one of their inputs will be DOWN.

The DOWN at the output of gate 1 will appear at the input of gate 18 via $S_{1}$ so that the output of gate 18 will be UP, switching the main logic unit into the Venn diagram mode of operation. The inputs to gates 20 and 21 will either be UP, or open, so that the outputs of these gates will be DOWN as will the T and K control signals. Notice that because the output of gate 18 is DOWN the output of gate 19 will be UP, switching both dians to the Venn operating mode.

Sixteen pulses from the clock generator will trace the first column of dots in display area 1. The sixteenth pulse will set bistable Q and bring the beam in the c.r.t. to the top-left-hand dot of display area two. Now the Q and $\bar{W}$ lines will be UP.

The output of gate 3 will go down and the outputs of gates 1,4 and 5 will go UP. The output of gate 18 will go DOWN and the output of gate 19 will go UP. The V control signal will therefore also be DOWN and the dians will be switched to the Venn/Karnaugh mode.

The DOWN at gate 3 will be relayed via $S_{7}$ to gate 20 and the K control signal will go UP switching the main logic unit to the Karnaugh map mode of operation. All other outputs of this circuit to the main logic unit will be DOWN.

Fifteen more pulses from the clock generator will trace the first column of dots in display area 1 . The sixteenth next pulse will set the first bistable in the X counter ( E ) and reset the $Y$ counter to all zeros. $\bar{Q} \bar{W}$ will now exist and the main logic unit will be switched to Venn operation (gate 1,5 , and gate $18 / 19$ ) in the same way as before. The second column of dots will then be traced out, first in display area number 1 and then in display area number 2
with a change-over to Karnaugh operation in between.
This process will repeat itself sixteen times with the main logic unit being switched from Venn to Karnaugh operation as the dot passes out of display area 1 into display area 2. After the sixteen repetitions the beam will be at the bottom right-hand corner of display area two (having scanned both display areas one and two), 512 clock pulses will have been generated, the $X$ and $Y$ counter will be in the following state $\mathrm{ABCDQE} F \mathrm{FH} \overline{\mathrm{W}}$ and the main logic unit will be in the Karnaugh mode of operation.

One more clock pulse will drive the counter to $\bar{A} \bar{B} \bar{C} \bar{D} \bar{Q} \bar{E} \bar{F} \bar{G} \bar{H} W$ and place the spot at the top left-hand corner of display area number three. $\bar{Q} W$ now exists. Gate $4, S_{13}$ and gate 21 will cause the main logic unit to be switched to the Truth table mode. When display area number four is reached QW will exist and gate $5, S_{18}$ and gate 21 will keep the instrument in the Truth table mode. After 512 more clock pulses both display areas three and four will have scanned and the process will repeat itself starting with display area number one again.

At the same time as all this was going on the output variables of the instrument, as decoded by the various variable forming logic circuits and controlled by the V , K , and T control signals derived from Fig. 86, were being fed to some sort of external logic circuit. The output of this logic circuit was being used to intensity modulate the
c.r.t. beam either directly or via the 1 and 0 character generators as dictated by the $\mathrm{V}, \mathrm{K}$, and T control signals.

From the above description it can be seen how any of the display areas could have been switched to any of the operating modes if desired. If, for instance, $S_{2}, S_{7}, S_{12}$, and $S_{17}$ had been pressed, all four displays areas would operate in the Karnaugh map mode. If the buffer stages only of Fig. 84 were incorporated then a six variable Karnaugh map would result. It is advised that these stages be added with this modification because of the greater flexibility afforded.

Having described the circuitry required to produce the $\mathrm{V}, \mathrm{K}$ and T control signals it is now necessary to have a look at the third column of the Truth table and the Truth table variable $\mathrm{T}_{\mathrm{c}}$.

Output $\overline{\mathrm{GH}}$ from the main logic unit, which, if you remember, addresses the third column of the Truth table, is inverted in gate 2 to form GH, and is fed to gates $7,10,13$ and 16. Also fed to these gates are the four combinations of $Q$ and $W$ which have been inverted in the gates $6,9,12$ and 15 . The switches $S_{4}(b), S_{9}(b), S_{14}(b), S_{19}(b)$ select $C=0$ in the Truth table by feeding the outputs of gates 7 , 10,13 , and 16 to gate 22. The output of gate 22 is inverted in gate 23 because the main logic unit requires the inverse of the $\mathrm{T}_{\mathrm{c}}=0$ signal. For $\mathrm{T}_{\mathrm{c}}=1 S_{5}(b), S_{10}(b), S_{15}(b)$, $S_{20}(b)$ and gates 24 and 25 are employed.


Fig. 86. The circuit of modification 7 .


These switches can therefore be used to cause all 1 s to be displayed in the third column of a Truth table ( $\mathrm{T}_{\mathrm{c}}$ ). Another pole (a) on the same switches causes the $C_{T}$ or $\overline{\mathrm{C}}_{\mathrm{T}}$ output variable of the main logic unit to be gated with $Q$ and $W$ area addressing signals which are combined in gate 26 to provide $C_{T}$ for the main logic unit. This ensures that when $\mathrm{C}=0$ in column three of a Truth table $\overline{\mathrm{C}}_{\mathrm{T}}$ is presented to the external logic circuit, when $C=1$ then $C_{T}$ is output.

As mentioned earlier the switches $S_{0}$ (Fig. 85) do not have any electrical connections and serve only to cancel out the $C=0$ and $C=1$ switches so that the $C$ column of the Truth table is blank.

8: Adding individual comparison facilities for each display area
This modification is carried only when modifications 4 and 7 have been incorporated. It enables up to two external logic circuits to be connected to the Display Aid and enables any display area to be switched to show the output of circuit one or the output of circuit two or the difference between circuit one and circuit two. The circuit diagram is shown in Fig. 87.

Z and $\overline{\mathrm{Z}}$ inputs to the instrument are provided by the two transistor double inverter stages. The gating system is identical to that shown in Fig. 79 and described under modification 3, only now there are four of them, one for each display area. An additional gate for each display area ( $35,36,37$ and 38 ) combines the output of the comparators with the area address signals available at gates $6,9,12$, and 15 of Fig. 86.

The output of gates $35,36,37$, and 38 are combined in gate 39 to provide the Z input for the main logic unit. The layout of the switches is shown at the right hand side of

Fig. 85. Taking area one as an example: closing $S_{21}$ will show the output of external circuit one in area one; pressing $S_{22}$ will show the output of external circuit number two in area one; pressing both $S_{21}$ and $S_{22}$ will show the difference between external circuits one and two in area one.

## Switch combinations

It will be interesting at this point to see how the various photographs shown in part one of this series (p. 198, May issue) were produced.

In photograph A a binary full adder was connected to the display aid, the SUM output was connected to the Z input. The switches which were pressed were as follows:
area one: Truth table ( $S_{3}$ ); C $=0\left(S_{4}\right)$, and circuit one ( $\mathrm{S}_{21}$ ).
area two: Truth table ( $S_{8}$ ); C $=1\left(S_{10}\right)$ and circuit one ( $S_{23}$ ),
area three: Karnaugh map ( $S_{12}$ ); and circuit one ( $S_{25}$ ), area four: Venn diagram ( $S_{16}$ ); and circuit one ( $S_{27}$ ).

For photograph B the external logic circuit was an AND gate with its output connected to the $Z_{1}$ input of the display aid. The input of the AND gate was connected to the output variables $\overline{\mathrm{A}}, \overline{\mathrm{B}}$ and $\overline{\mathrm{C}}$. Switch positions were as follows:
area one: Truth table $\left(S_{3}\right) ; \mathbb{C}=0\left(S_{4}\right)$, and circuit one $\left(S_{21}\right)$
area two: Truth table ( $S_{8}$ ); C =1 ( $S_{10}$ ), and circuit one $\left(S_{23}\right)$


Fig. 88. A block diagram showing the interconnection of units in the type $U$ instrument.
area three: Venn diagram ( $S_{11}$ ); and circuit one ( $S_{25}$ ) area four: Karnaugh map ( $S_{17}$ ); and circuit one ( $S_{27}$ )

In photograph $C$ the output variable $A$ was connected directly to the $Z_{1}$ input and the output variable $\bar{A}$ was connected to the $Z_{2}$ input of the display aid. Switch positions were as follows:
area one: Venn diagram ( $S_{1}$ ); and circuit one ( $S_{21}$ )
area two: Karnaugh map $\left(S_{7}\right)$; and circuit one $\left(S_{23}\right)$
area three: Venn diagram ( $S_{11}$ ); and circuit two ( $S_{26}$ )
area four: Karnaugh map ( $S_{17}$ ); and circuit two ( $S_{28}$ )
Two binary adders were used to produce photograph D. One of the adders was deliberately made unserviceable and its SUM output was connected to $\mathrm{Z}_{1}$. The sum output


To the three stages of switching for the other display areas
(Above) Fig.89. Part practical layout for type $U$ instrument. The two i.cs are $Z N 346 E s$.


ZN330E
ZN330E

the type $U$ instrument.
of the serviceable adder was connected to $Z_{2}$. Switch positions were as follows:
area one: Venn diagram ( $S_{1}$ ); and circuit one ( $S_{21}$ ) area two: Venn diagram ( $S_{6}$ ); and circuit two ( $S_{24}$ )
area three: Venn diagram ( $S_{11}$ ); and difference ( $S_{25}$ and $S_{26}$ )
area four: Karnaugh map ( $S_{17}$ ); and difference ( $S_{27}$ and $S_{28}$ )

The above examples were given in order that the reader may see how to operate the instrument so that the various logic and switching circuits can be more readily understood.

## Building the type $U$ logic display aid

The prototype instrument was type U as mentioned in the list of compatible modifications given last month and as such incorporates modifications 4,7 and 8 . It is proposed to give some practical details of this instrument, but of course it would be impossible to give the same detail for all 21 types.

The system block diagram is shown in Fig. 88. This does not require any comment, however, it should be of value when the time comes to interconnect all the various units.

Fig. 89 gives a wiring diagram for the switching circuits for display area number one. The three switching circuits for the other three display areas are wiredup in almost the same way. The only difference is that the $\overline{\mathrm{GH}}$ output of the main logic circuit only requires to be inverted once (gate 2, Fig. 86) which is done in Fig. 89. This means that when all four stages are wired-up there will be three spare two-input gates. These can be used to partly fill the need for some of the buffer-amplifiers needed for the E and F variables for six-variable Karnaugh map operation.

Fig. 90 shows how the output side of the switching circuit is wired-up. The numbers near the integrated circuits of Figs. 89 and 90 correspond to the gate numbering in Figs. 86 and 87.

If one examines Fig. 73 (p.421, September issue) the necessary components for modifications 7 and 8 can be seen mounted on a board on the extreme right behind the mains transformer. The board in the foreground, bolted to the main logic unit, contains the parts necessary for modification 4.

Faults on this part of the circuit (modifications 7 and 8) can be very, very trying. The reader is advised to take extreme care with the construction. It is a good plan to adopt some form of colour-coding system, particularly with the switch wiring, and stick to it.

The switches themselves do not have any mounting holes, so the procedure adopted in the prototype was to solder them to mild steel angle which was bolted to the front panel; however, this is a matter of personal preference.

The description of the Wireless World Logic Display Aid is now complete and we wish you well with the construction.

Next month, in the last article in this series, a simple modification will be described showing how the aid may be used with a 19-inch oscilloscope and some external logic circuits will also be suggested.

## Amplifier efficiency

Mr. Vanderkooy's letter (August issue, p.381), set me thinking. Why waste audio power in an emitter load, why not replace it by a constant current source adjusted to give the correct standing current, and, of course, having a relatively high dynamic impedance? (Fig. a.). The only a.c. load is now provided by $R$, and so the emitter of the output transistor should be at half the supply potential.


With the transistor full on, current through the load will be, instantaneously, $(V / 2) / R$ and with it cut off, the current will be $I$. These two currents should be equal, i.e. $I=V /(2 R)$, e.g. with a supply of 30 volts and load of 15 ohms, the standing current should be 1 amp . Efficiency should be $25 \%$ if the constant current source is ideal and the output transistor has zero saturation voltage.
To test the theory, I used Mr. Vanderkooy's circuit, replacing the 22 -ohm emitter resistor by the hurriedly devised and far from ideal arrangement of Fig. b. Using a supply of 32 volts and a standing current of 1 amp , output power at the onset of symmetrical clipping was just over 5 watts. Increasing the supply to 40 volts and the current to 1.2 amps , the maximum output rose to nearly 10 watts, an efficiency of about $20 \%$. This is not a new idea-a similar circuit was used by P. F. Ridler for the output stage of his "Low Distortion RC Oscillator"(W.W., August 1967, p.383), and it needs a fairly large heat-sink area, but ten watts or so may be obtained without resorting to water cooling! Of course, all one has to do now is to drive the lower transistor and one arrives at Mr. Linsley Hood's class A circuit!
IAN G. JOHNSON,
Farnborough, Hants.

## Radio in airship R100

The Electrical Engineering Squadron at this Station has undertaken to renovate, on behalf of the Royal Air Force Museum, the experimental receiver, Type RX18A, from the R100 airship.

We would be grateful if you could publish this appeal for information on the receiver, especially with regard to valve types and coil winding details.
R. M. Harrison (F/O),
R.A.F., Syerston,

Newark, Notts.

## Test Your Knowledge

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## 18.: Waveguide components and techniques

In all the questions it is assumed that the basic waveguide is standard rectangular and that it is propagating the dominant mode.

1. The behaviour of a waveguide component or circuit can often be inferred by analysis of the equivalent twin-transmissionline circuit. In constructing the analogue the transmission-line wires are taken to lie:
(a) along the centre lines of the broad walls of the guide
(b) along the centre lines of the narrow walls of the guide
(c) along a pair of opposite corners of the guide
(d) along a pair of adjacent corners of the guide separated by a broad guide wall.
2. If a waveguide component, in which changes of guide dimensions occur, is to be designed with the aid of the equivalent transmission-line circuit, appropriate values of line impedances to use for the various guide sections are in each case:
(a) the wave impedance of the section of guide
(b) the wave impedance multiplied by the narrow guide dimension
(c) the wave impedance multiplied by the wide guide dimension
(d) the wave impedance multiplied by the narrow guide dimension and divided by the wide guide dimension.
3. A waveguide component may be found to contain an "iris" (a thin metal plate or plates perpendicular to the guide axis extending part of the way across). The purpose of the iris is generally to:
(a) protect the component by providing a point at which sparking will occur first if the component is overloaded
(b) "match out" a mismatch in the component
(c) suppress higher order modes
(d) prevent dust from reaching certain parts of the component.
4. A waveguide component is required to have a slot in the guide wall parallel to the axis of the guide, and the slot must not radiate a significant amount of microwave energy. The slot:
(a) may be anywhere in the guide walls
(b) may be anywhere in a wide wall, but must not be in a narrow wall
(c) must be either along the centre line of a wide wall or a narrow wall
(d) must be along the centre line of a wide wall.

[^5]5. In order to determine, with the aid of a Smith Chart, a point at which a susceptance can be placed to match a mismatched waveguide termination, three of the following need to be known (and nothing more). Select the redundant information:
(a) the v.s.w.r.
(b) the position of the voltage minimum nearest to the source of mismatch
(c) the frequency
(d) the guide-wavelength.
6. The principle of reciprocity is obeyed:
(a) by all waveguide components
(b) by no waveguide components
(c) by all waveguide components except certain ferrite devices
(d) only by certain waveguide components containing ferrites.
7. If the construction of a waveguide component requires two similar small discontinuities to be introduced into the guide, the distance between them:
(a) should be as small as possible
(b) should be as large as possible
(c) should be a whole number of half guide-wavelengths.
(d) should be an odd whole number of quarter guide-wavelengths.
8. In a microwave resonant cavity the electric and magnetic fields:
(a) have maximum amplitudes which coincide in space, and are in phase
(b) have maximum amplitudes which coincide in space, and are in phase quadrature
(c) are in phase, and the maximum amplitude of one coincides in space with the minimum amplitude of the other
(d) are in phase quadrature, and the maximum amplitude of one coincides in space with the minimum amplitude of the other.
9. It is desired to build a resonant cavity, to resonate at a given frequency, having as high $\mathrm{a} Q$ as possible (the general form of the cavity being specified). The cavity should be designed to have:
(a) as large a volume as possible
(b) as large a surface area as possible
(c) a maximum ratio of volume to surface area
(d) a minimum ratio of volume to surface area.
10. A resonant cavity terminates a waveguide. The v.s.w.r. in the guide at the
resonant frequency of the cavity is found to be $2: 1$ and the position of the standing-wave pattern at resonance is the same as its position when the frequency is well away from resonance. The coupling parameter of the cavity is:
(a) zero, (b) $\frac{1}{2}$, (c) unity, (d) 2.
11. Most microwave generators require to feed a waveguide in which the V.S.W.R. at the input does not exceed a specified value (often 1.5:1). If a generator feeds a waveguide with a large mismatch the main effect is:
(a) electrical breakdown in the waveguide
(b) a reduction of power output from the generator in all cases
(c) a change in generator frequency only
(d) both power output and frequency instability.
12. In a waveguide choke coupling an effective good contact is achieved at the waveguide wall by moving the actual point of physical contact one quarter wavelength back along a half-wave short-circuited guide section (the choke). The choke ring cut into the flange always has a much wider slot than the gap between the flanges (which forms the first half of the choke). The reason for this is:
(a) convenience of manufacture
(b) to give the joint broad-band properties.
(c) to prevent arcing at the corner
(d) so that dirt will not be trapped in the choke ring.
13. In a simple coaxial line to waveguide transformer (probe launching section) the distance between the probe and the shortcircuit in the guide should be approximately:
(a) one half free-space wavelength
(b) one half guide wavelength
(c) one quarter free-space wavelength
(d) one quarter guide wavelength.
14. In a directional coupler the coupling holes:
(a) must be in broad faces of both guides
(b) must be in narrow faces of both guides
(c) must be in the broad face of one guide and the narrow face of the other
(d) may be either in the broad faces of both guides or the narrow faces of both guides.
15. In a compensated magic $T$ (hybrid junction):
(a) each arm is isolated from the other three
(b) each arm is isolated from two of the other three
(c) each arm is isolated from the arm opposite
(d) only one pair of arms are isolated from each other.
16. Of the forms of attenuator listed below one reflects energy rather than absorbing it.
It is:
(a) the resistive film attenuator
(b) the piston attenuator
(c) the flap attenuator
(d) the rotary vane attenuator.

Answers and comments, page 549


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# World of Amateur Radio 

the field. His death was equally tragic. He was executed by the Germans in November 1944 on suspicion of espionage when caught searching for fragments of an exploded V2 rocket in a prohibited area.

There can be little doubr that the Dutch concerts helped create the demand by wireless enthusiasts in the U.K. for the start of regular broadcasting. In 1921, following an appeal in Wireless World, about $£ 750$ was subscribed by British enthusiasts to allow the concerts to continue.

## Television interference

The recently released Post Office statistics for cases of interference to television and radio reception in 1968 show a marked increase in the number ascribed to amateur and other transmitters. Of 70,254 interference cases closed by the P.O. investigators, 1151 or just over $1.5 \%$ were ascribed to amateur transmitters. The number has risen apprecíably in the past five years or so. It is widely believed by amateurs that modern TV receiver installations, particularly those fitted with transistor wideband mast-head (or back-ofset) pre-amplifiers, are much more susceptible to strong local signals on frequencies far removed from the TV channels than older receivers. Another increasing problem is the number of viewers using set-top aerials which can be much more susceptible to interference.

Amateurs are however hoping that the spread of u.h.f. television will result in a marked easing of the position, since instances of amateurs causing interference on Bands IV and $V$ are far rarer than on v.h.f.

The Post Office statistics also show the rising incidence of interference generated by thermostat controls in domestic gas and oil-fired central heating systems, particularly after some months of operation. Electrical interference from such contact devices now exceeds that from electric motors, previously the most frequent cause of interference.

In Brief: Membership of the R.S.G.B., in the year to June 30 th , rose by 1347 to a total of 15,392-this compares with an increase of 644 in the previous year. The membership now includes rather over one-half (some 8000) of all British licensed amateurs. Its overseas membership is $1378 \ldots$. The Australian Post Office has approved the installation by amateurs of unattended v.h.f. repeater stations operating on the $144-\mathrm{MHz}$ band .... The French P.T.T. is to support, at the next congress of the Universal Postal Union, a proposal that would admit QSL cards in the "small packet" post . . . The Scottish v.h.f. convention is being held at The Carlton Hotel, North Bridge, Edinburgh, on October 26th; the convention includes a dinner, lectures and an exhibition (GM3OWU, "Westerlea", 9 Juniper Avenue, Juniper Green, Midlothian, EH14 5EG) . . . For the first time amateurs have spanned the English Channel using the $10-\mathrm{GHz}$ band. Dain Evans, G3RPE, operating portable near Dover contacted the French amateur station F2FO/P near Cap Gris Nez. The British station had an output of only 15 mW with a 10 -inch dish aerial.

Pat Hawker, G3VA

## New Products

## Sub-miniature Television Camera

A sub-miniature television camera (type BC1103), believed to be the smallest commercially available in the world, has been designed by E.M.I. for inspection of the inside of pipes and for operation in inaccessible locations under arduous conditions. The BC1 103 consists of two units, the cylindrical camera head and a camera control unit. The camera head measures only 24 mm in diameter and 122 mm in length, is complete with integral lens and lighting unit, and is sealed to prevent the ingress of moisture and dirt. A 13 mm (t-inch) vidicon camera tube is used and the high performance head amplifier employs f.e.ts and integrated circuits. The lens lighting unit incorporates a lens with an angle of view of approximately $40^{\circ}$. The $\mathrm{f} / 6$ camera lens gives adequate depth of field for pipes of bore from 25 mm to 65 mm . The camera head can be connected to its associated control unit by up to 65 m of steel reinforced camera cable. The camera control unit

(shown in the photograph with the camera) weighs only 19 kg . The control unit provides all the power, scanning and processing circuits for the camera channel. Broadcast type 625/525 line synchronizing pulses ensure compatibility with all makes of video monitors and video tape recorders. Three camera controls (target, beam and electrical focusing), in addition to the lighting intensity controls and the power on /off switch are mounted on a recessed front panel. An air pump is fitted to the camera control unit to provide cooling and to enable the camera head to be operated continuously in ambient temperatures up to $45^{\circ} \mathrm{C}$. E.M.I. Electronics L.td, Hayes, Middx.
WW307 for further details

## Digital A.C./D.C.Multimeter

Apart from the benefits gained from a digital display, the TE 360 multimeter from Guest International exhibits best-case accuracy figures of $\pm 0.1 \%$ of reading, $\pm 0.1 \%$ of f.s.d., and is capable of a wide variety of measurements. These include 20 ranges covering a.c. and d.c. voltage and d.c. current, and five ranges of resistance. Voltage may be measured up to 1 kV , current up to 2 A , and resistance up to $2 \mathrm{M} \Omega$


Input impedance varies from $10 \mathrm{M} \Omega$ to $1 \mathrm{kM} \Omega$ on d.c. volts and is $10 \mathrm{M} \Omega$ on all a.c. voltage ranges. The display includes 3 digits and over-range indication, polarity and decimal points. Readings are given at 0.2 s intervals and there are optional facilities for b.c.d. and print command outputs. Power requirements are 115 or $230 \mathrm{~V}, 50$ to 60 Hz . A battery version is available. Price $£ 198$. Guest International Lid, Nicholas House, Brigstock Road, Thornton Heath, Surrey, CR4 7JA. WW 327 for further details

## Video Test-signal Generator

A complete set of signals for checking and measuring the video characteristics of television studio equipment, transmission links and transmitters is provided by a new test-signal generator available from Pve Unicam. All signals generated conform to C.C.I.R., I.E.C., and C.M.T.T. requirements. The generator, lhilips I'M $5572 / 74$, features integrated-circuit design virtually throughout and consists of three modules which are housed in a case 132 mm high. The three units-blanking mixer and power supply unit, sine-wave generator and pulse generator-are interconnected by either cable or plug-in connectors, and the complete generator can be expanded through the addition of further modules. The sine-wave unit can be used as a fixed-frequency, multiburst or video-sweep generator. In the first mode of operation it provides $1-10 \mathrm{MHz}$ signals variable in 1 MHz steps. In the second, it produces $1-5 \mathrm{MHz}$ multiburst signals with or without black-white reference lines, and in the third it gives sweep signals from 100 kHz 10 MHz with or without 1 MHz markers. Various types of test signal for checking the performance of video-transmission circuits, videoamplifiers, etc., are provided by the pulse generator unit. These include square-wave, sawtooth, staircase and sine signals. Square-wave signals are available with repetition rates of 0.5 and 50 Hz , and 15 and 250 kHz , and all have risetimes of less than 60 ns . However, filters can be switched in to ensure standard risetimes. Sawtooth signals

provided consist of line-frequency sawtooths with or without intermediate lines at the black-white level. The staircase signal has either five or ten steps. Both types of signal can have superimposed $1-10 \mathrm{MHz}$ or colour sub-carrier signals added in the blanking mixer. Where a superimposed colour sub-carrier is used with the above signal, it is also possible to switch in a colour-burst signal. The amplitude of all components in the composite signal can be adjusted via controls on the blanking mixer, and other controls permit, for example, black-white signals to be clipped or limited as required. It is also possible to invert the set-up level and include or exclude frame information from the composite signal. Pye Unicam Ltd, York Street, Cambridge.
WW310 for further details

## Four-quadrant Multiplier

Philbrick/Nexus Research, is now offering a small four-quadrant multiplier. The model 4450 is compatible for use as a computing element in the laboratory and, in applications where an accurate multiplication process is required with no limitations as to the polarity of the input signals. Several applications such as modulation, frequency doubling, and power measurements, can be accomplished using the model 4450 . The multiplier operates at rated accuracy to 10 kHz with full output voltage capabilities to 100 kHz , Its output is representative of the instantaneous product of two input signals. Only one external

trim is required for setting up. An optional scale factor trim mav be used to improve accuracy to $\pm 0.6 \%$ typical ( $\pm 1$, maximum) referred to 10 V full-scale output. When scale-factor trim is not used, accuracy is $\pm 1 \%$ typical and $\pm 2 \%$ maximum. The price of the model 4450 in quantities of $1-9$ is $£ 4110$ s each. Philbrick/Nexus Research, 81 a North Street, Chichester, Sussex. WW309 for further details

## Frequency-synthesized Drive Unit

An h.f. drive unit, designated type GK 203, is announced by the Communications Division of Redifon. All solid-state and self-contained, with integral power unit, the GK 203 uses frequency synthesis to develop 285,000 channels in 100 Hz steps from 1.5 to 30 MHz and to generate modulated signals in seventeen selectable modes of transmission. The new unit can be used with
most h.f. transmitters and linear amplifiers. While the GK 203 will accept an input from an external frequency standard, it incorporates an internal reference source which can be used as a standard for other equipment. Where several of these drive units are used, an economy may be effected by omitting the reference source from all except one master unit. Transmission modes cover c.w., m.c.w., d.s.b., compatible a.m., s.s.b. with fully suppressed carrier or with pilot carrier at -16 dB or -26 dB levels, and, as an optional extra facility, i.s.b. at either of two pilot carrier levels. On all services employing a single sideband the u.s.b. or 1.s.b. mode is selectable by a front-panel switch. Automatic volume compression can be switched in to maintain a high modulation index even at

low speech levels, and automatic voice or tone activation of transmit/stand-by switching can also be selected. Sidetone and two forms of muting are available for associated receiver, to provide aerial muting or a.g.c. desensitizing. Redifon Lrd, Broomhill Road, Wandsworth, London S.W.18.
WW329 for further details

## 6,000-watt Amplifier

A 6,000 -watt amplifier has been developed by Derritron. Whilst primarily designed for operating with a 19501 l thrust vibrator, this amplifier can be used as a variable frequency power source. The amplifier incorporates an oscillator and a closed-circuit water cooling system, and uses silicon transistors throughout. Check-our facilities are included and the amplifier is protected against overload. Derritron Electronics Lid, Sedlescombe Road North, Hastings, Sussex.
WW314 for further details

## Multi-waveform Generators

The series 500 waveform generators from Environmental Equipments is designed to provide the functions of many different instruments, such as square-wave generator, sine-wave oscillator, sweep generator, f.m. modulator, variable repetition-rate pulse-generator, ramp and raster generator, stimulation and simulation signal in medical research, control signals for aerospace and environmental testing. These generators feature bipolar-sine, square, triangle, ramp, reverse ramp and pulse outputs. In addition models 504 B and 505 B add haversine and havertriangle waveforms. The wide frequency range extends from 0.0001 Hz (greater than 2 hours) to 1 MHz ( $1 \mu$ ) covering requirements from biological to radio frequencies. Models 503B and 505B offer precise control of frequency by an external voltage. By applying a 0 to $+5 \mathrm{~V}, 0$ to -5 V , or 0 to $\pm 2 \frac{1}{2} \mathrm{~V}$ the frequency can be swept
over a $50: 1$ range-usable range is 100:1. All models have triple output amplifiers giving pushpull output if required, high output voltage, and adjustable d.c. offset. Gating, triggering (single shot) and variable start/stop phase are also available. Typical waveform specifications are: sine distortion, less than $1 \%$, triangle linearity better than $99 \%$, square wave rise/fall times 50 ns . Environmental Equipments Lid, Denton Road, Wokingham, Berks.
WW338 for further details

## Solid-state High-voltage Equipment

Miles Hivolt have produced an instrument enabling a 25 kV 1 mA supply to be contained within a panel height of only 133 mm . The output of this instrument, the Hivolt TH25, can be shortcircuited indefinitely, or load flash-over can occur without damage either to the driver transistors or the associated circuits. Plug-in printed circuit boards are used in a modular design. The e.h.t. generator comprises an oscillator module and a moulded voltage multiplier stack. The TH25 is fully metered for current measurement. The voltage is set by means of a ten-turn potentiometer. Although the Hivolt TH25 is produced in such a small size, heat dissipation has been kept extremely low and there is no undue temperature rise. The equipment is designed for bench or rack mounting. Alternatively, the company are supplying the model TH20 which may be accommodated in manufacturers' equipment and as such does not require metering. In this case the voltage adjustment is by means of a ten-turn preset potentiometer normally set by the user within the range $10-20 \mathrm{kV}$. Miles Hivolt Ltd, Shoreham, Sussex.
WW306 for further details

## Transistor-switched Indicator Lamps

Available from Oxley Developments is a new range of transistor-switched indicator lamps, for use with negative logic. They use a $p-n-p$ transistor, and are switched ON by a negative signal. The new units have complementary characteristics to the current range of transistor-switched indicator lamps. The "Barb" feature permits simple fixing on the front of the panel and allows close grouping of the units. The removable lens cap, available in seven colours, facilitates bulb replacement from the front of the panel. Also, lens caps can be supplied which are virtually unbreakable. Oxley Developments Company Ltd, Priory Park, Ulverston, North Lancs.
WW319 for further details

## Digital Integrated Circuit Tester

A compact, low cost, integrated circuit tester, manufactured by John Reeve Instruments, (designated the 51B) provides push-button selection of any test pin on most standard types of d.t.l. and t.t.l. circuits. Measurements are displayed on a 5 in scale-length meter. Fully protected against overload and fitted with self-contained variable

power supplies and a pulse generator, the instrument is completely portable. Flexibility in operation is assured by utilizing manual control and dispensing with the need for programming cards. Up to 16 circuit pins are provided for on the basic instrument and packages of any configuration may be tested by using test sockets with adaptors which plug into the front panel of the instrument. The tester can be used in conjunction with various items of ancillary equipment for checking other types of logic or displaying circuit characteristics on a transistor curve tracer. Fully automatic functional tests and semi-automatic test sequencing can be carried out using special plug-in units. Price £235. John Reeve Instruments, 8 Ownstead Gardens, South Croydon, Surrey. CR2 OHH.
WW303 for further details

## Digital Clock and Time Code Generator

A series of integrated circuit digital clocks and time code generators is available from Sintrom Electronics. The digital clock, the 30,000 , designed for use with computers, data logging, data processing and digital readout systems requiring real or elapsed time inputs, is available in over 7,000 standard versions. Outputs, in b.d.c. or Nixie decimal front panel displays, can be in units of less than a second or as long as a month. The b.c.d. output is available in serial and/or parallel format. A wide variety

of timebases is available. An interlock circuit allows the external system to 'hold' the clock during readout without introducing any timing error. The time code generator, which provides I.R.I.G. and N.A.S.A. time code formats in both modulated carrier and level shift forms in addition to b.c.d. outputs, provides timing information to analogue recorders as well as to digital systems. Many versions are available with choices of timebase, power supply, output format and displays. Sintrom Electronics Ltd, 2 Castle Hill Terrace, Maidenhead, Berks.
WW331 for further details

## L.F. Signal Generator

A v.l.f. and l.f. signal generator (type 422) is announced by the Airmec division of Racal. It is a solid-state crystal-monitored digital-display instrument, and has a continuously variable output from 0.005 Hz to 50 kHz . The 10 V square

and sinewave outputs are available via a built-in matched $600 \Omega 80 \mathrm{~dB}$ attenuator and an unattenuated triangular output is provided at 5 V p-p about earth. The 422 is suitable for many applications, including the audio, servo and medical fields. A coarse tuning control gives continuity of tuning by making the direction of rotation for frequency increase reversible for successive half-ranges of the frequency decade switch. This "zig-zag" arrangement obviates the necessity of reversing the coarse control back over its full travel when switching between decades. Accuracy is up to $\pm 2$ parts in $10^{5}$ with stability of 1 in $10^{4}$ over 30 min . The precision with which selected frequencies are displayed is demonstrated by the least significant digit in the readout indicating micro-hertz for the lowest frequency range. The use of high-frequency basic oscillatory circuit ensures that the output frequency can be altered with no appreciable time delay. This, together with the fast presentation readout time of 110 milliseconds for any frequency, enables changes of output frequency of the instrument to be effected and displayed instantaneously. Racal Instruments Lid, Bennet Road, Reading, Berks.
WW302 for further details

## Miniaturized Reed Switch

The FR/Hamlin reed switch MTRR-2 has been reduced in size. The glass length is now $0.54 \mathrm{in}(13.7 \mathrm{~mm})$ instead of 0.625 in , but the diameter remains at 0.090 in . Contact rating is 10 W maximum at 250 mA . The off-centre gap makes the MTRR-2 ideal for permanent magnet applications. FR Electronics, Wimborne, Dorset.
WW334 for further details

## Megohmmeters

General Radio have announced two new megohmmeters; types 1863 and 1864. These meters are useful for measuring insulating materials as well as capacitor or semiconductor leakage. Although similar in appearance and accuracy, their operating ranges differ in order to meet differing needs. The 1863 can measure resistances from $50 \mathrm{k} \Omega$ to $20 \mathrm{~T} \Omega\left(2 \times 10^{13} \Omega\right)$ at five test voltages from 50 to 500 V . The 1804 (illustrated) can measure resistances from $50 \mathrm{k} \Omega$ to $200 \mathrm{~T} \Omega$ at 200 test voltages from 10 to 1000 V . Each

has an output voltage that is proportional to meter reading for limit testing. General Radio Company (U.K.) Led, Bourne End, Bucks. WW301 for further details

## Op. Amp. Power Supply

Weir's compact new model 915/912 power supply is suitable for use with most makes of operational amplifier requiring a balanced 12 or 15 V regulated d.c. supply at currents up to 100 mA . The units have long-term overload and short-circuit protection effected by constant current limiting at approximately $120 \%$ of rating. The two outputs can also be used in series to provide single outputs of 30 V or 24 V at 100 mA . Both outputs have dual remote sensing for use where the power unit has to be located at some distance

from its load. Connections can be made via a printed circuit edge connector which is supplied with the unit. Regulation drift is less than $0.05 \%$. Ripple and noise are less than $1 \mathrm{mV} p-\mathrm{p}$. Weir Electronics Ltd, Durban Road, Bognor Regis, Sussex.
WW318 for further details

## Wire-wound Resistors

Impectron now distribute a resistor, called the Cerwistor, in which instead of the usual method of winding the resistance wire on the outside of a tube or bar of porcelain it lies inside the porcelain. This construction ensures that even the thinnest resistance wire is given mechanical protection. The Cerwistor is small in relation to the rated dissipation, and its flat body takes up very little space. It is available in 3-, 5-, 8 - and 10 -watt ratings at standard preferred values as recommended by I.E.C. series E24 which means 24 values between 1 and 10 , between 10 and 100 , etc. The insulation resistance is greater than $1000 \mathrm{M} \Omega$ (with silicon protection even greater than $100,000 \mathrm{M} \Omega$ ). Standard tolerance is $\pm 5 \%$ of the nominal resistance value, better tolerances can be supplied as specials. Impectron Lid, King Street, London W. 3.
WW315 for further details

## Miniature Stabilized Power Unit

The PU40 miniature power unit from Fenlow provides stabilized d.c. voltages between $\pm 10 \mathrm{~V}$ and $\pm 15 \mathrm{~V}$ set by two external resistors. The input is the mains supply of 210 to 225 V 40 to 60 Hz . It is an encapsulated unit measuring approx. $82 \times 63 \times 25 \mathrm{~mm}$ and has the following performance. Output current 40 mA on each line with short-circuit protection. Line regulation is $0.01 \%$ for input voltage variation between 210 and 255 V . The no-load to full-load regulation is $0.01 \%$, and the total noise and ripple less than 2 mV on each line. The unit is intended to drive a number of operational amplifiers, but its price of $£ 20$ should mean that it will find much wider applications as a building block for use in small

mains-powered instruments and also for experimental work in the laboratory. Fenlow Electronics Lid, Whittet's Eyot, Jessamy Road, Weybridge, Surrey
WW308 for further details

## Contact Cleaner

A glass fibre eraser available from Garfory' Lilley and Brother is suitable for contact and commutator cleaning, as well as for the preparation of joints prior to soldering. This brush will remove not only oxidization, but many forms of contamination from copper, aluminium, steel, etc., without damage to the components. The eraser consists of a stiff glass fibre brush mounted in a pencil shaped metal body. The exposed brush length can be adjusted for wear by a screw device fitted at the top of the body. Refills are available in boxes of 25 brushes. Garford-Lilley and Brother Ltd, 3 Hampton Court Parade, East Molesey, Surrey
WW336 for further details

## Trimmer Potentiometer

Reliance Controls have introduced four new trimmers. The CW' 52 miniature wire-wound trimmer is unsealed and available in a resistance range of $20 \Omega$ to $20 \mathrm{k} \Omega$ with a resistance tolerance of $\pm 10 \%$. Mechanical adjustment is 20 turns. Pin configuration is $0.2 \mathrm{in}, 0.3 \mathrm{in}$ and 0.4 in with 0.5 in between the outer pins. The CW5 2 can also be used for panel mounting and allows for adjustment through a panel up to $\frac{1}{5}$ in thick. The CW52 is thus an unsealed version of the already established fully sealed CW'51. The CW53 and CW54 are two new sealed trimmers with the same electrical specification as the CIW52. The CW53 is

based on a dual in-line configuration with a 0.5 in spacing along, a 0.3 in spacing across, the body. The wiper connections on this trimmer are duplicated for mechanical stability. The CW54 has a $0.3 \mathrm{in}, 0.4 \mathrm{in}$ and 0.1 in pin configuration with 0.7 in between outer pins. The CWS5 is an unsealed version of the CW54 with identical electrical specifications. All these trimmers are manufactured with terminals of gold-plated brass and wipers of gold-plated beryllium copper. Reliance Controls Ltd, Drakes Way, Swindon, Wilts.
WW311 for further details

## D.C. Amplifier

Advance Industrial Electronics announce the introduction of the new Zeltex Model 240 f.e.t.-
input differential amplifier designed for use in low-level d.c. transducer, gain-switching and un-loading-circuit applications. The unit features a built-in feedback network, adjustable closed-loop gain. Gain is set to any value between 1 and 1000 with an external resistor. High input impedance ( $10^{11}$ ohms) and an 80 dB common mode rejection ratio (at any gain setting) make the Model 240 suitable for industrial, medical and biological applications. The gain-bandwidth product is 1 MHz min . The unit can be soldered to a p.c. board or plugged into an optional mating connector. Price (1-9) £37. Advance Industrial Electronics, Raynham Koad, Bishops Stortford, Herts. WW321 for further details

## Universal Digital Comparator

A digital comparator, the 6003 B , designed to provide computer decision-making facilities when used in conjunction with any digital output detice, is now available from Sintrom. It will accept síngle or multiple input data-groups from the parent digital equipment, compare the input to present limits, and within 20 ms indicate one of five possible output decisions. The decision signals are in the form of contact closures and front panel lights. The model 6003B will accept

information from any digital equipment with outputs in 1-2-4-8 or 1-2-4-2 parallel b.c.d. form, whether the signal indicates frequency, voltage, capacitance, data card or computer information. One comparator can provide up to five output decisions, totalling 17 digits maximum and limit settings can be quickly made by means of front panel thumbwheel switches or remote programming from other equipment. Comparator units can be stacked to increase output decisions. Sintrom Electronics Lid, 2 Castle Hill Terrace, Maidenhead, Berks.
WW316 for further details

## Transient Amplitude Detector

A battery-operated transient amplitude detector capable of reproducing a 30 ns width pulse 10 $90 \%$ amplitude accuracy has been developed by, and is now available from, Electro-Metrics Corporation, a subsidiary of Fairchild Camera and Instrument Corporation. The unit, designated model TAD-66, makes use of a high impedance differential probe for handling input signals from 0.001 V to 25 V . Four peak detectors, operating in parallel, sample and hold the input signal after amplification-iwo operating on the normal input and two on the input inverted-to assure fully redundant peak detection. The outputs of each pair of peak detectors are fed to amplitude comparators. Each comparator sees only the highest signal level that was fed to the detectors. A timing and sampling system alternately samples the outputs of the comparators to provide a pulse train, each pulse representing the highest transient seen during the sample time of the peak detectors. Sampling rates are variable from 10 Hz to 1200 Hz from built-in triggering, or up to 10 kHz from external triggering. Slow sampling rates provide data that can be displayed on oscilloscopes and X-Y plotters. At the highest rates, the outputs are handled by a computer or other fast reacting device. The 30ns pulse-width handling capability means that the TAD-66 will handle signals accurately at frequencies from 10 Hz to up to nearly


50 MHz . If amplitude accuracy is not important and only indication of a transient is required, the unit will sample, hold and provide an output indication of a transient with a width of only a very few nanoseconds. The unit is battery-operated and has both a $600 \Omega$ balanced output and a $50 \Omega$ single-ended output for connecting to external display devices. Fairchild Electro-Metrics Corporation, 88 Church Street, Amsterdam, New York 12011, U.S.A.
WW313 for further details

## Digital Multimeter

Fluke International announces a digital multimeter which uses an analogue-to-digital converter with only one-fifth of the parts normally required. The unit, Model 8300 A , has five digits plus $20 \%$ over-ranging. The basic unit measures 0 to 1100 V d.c. in three ranges. Sampling speed is 25 ms . Low-cost options include a.c. voltage, millivolt-ohms, external reference (ratio) and fully isolated remote programming and data output. Because the new a.-d. technique substantially cuis down on the number of components used, a number of operating characteristics are improved. The new technique used in the Fluke 8300A is

based on storage capacitors, a single b.c.d. counter and a resistive ladder network to serially determine and display all digits. It is called the recirculating remainder A to D system. Fluke International Corporation, Garnett Close, Watford WD2 +TT.
WW 322 for further details

## Transistor Arrays

Two general-purpose transistor arrays have been added to the range of linear i.cs available from R.C.A. The CA3026 and CA3054, which contain dual independent differential amplifiers with associated constant current transistors on a common monolithic substrate, have wide applications in low-power systems at frequencies from d.c. 10 120 MHz . Bias and load resistors have been purposely omitted to allow maximum application flexibility. The monolithic construction of the arrays gives close electrical and thermal matching between each pair of amplifiers, making these devices particularly useful in dual channel applications. The six n-p-n transistors which form each pair of amplifiers are general purpose types exhibiting low l.f. noise and a gain bandwidth product in excess of 300 MHz . The CA 3026 is contained in a hermetic 12 -lead TO-5 package and is rated for operation from $-55^{\circ}$ to $+125^{\circ} \mathrm{C}$. The CA3054, which is electrically identical to the CA3026, is contained in a 14 -lead dual in-line plastic package for applications requiring a limited operating temperature range, between $0^{\circ} \mathrm{C}$ and $+85^{\circ} \mathrm{C}$. The
many applications of these devices include dual sense amplifiers, dual Schmitt triggers, multifunction combinations, i.f. amplifiers, product detectors, doubly balanced modulators and demodulators, balanced quadrature detectors, cascade limiters, synchronous detectors, pairs of balanced mixers, synthesizer mixers and balanced cascode amplifiers. The CA3026 and CA3054 are available at 15 s 6 d each for quantities of 100 plus from R.C.A's three distributors: Semicomps Northern Lid, Robert Electronics Lid, and Electronic Component Supplies (Windsor) Lid. Large orders of 1,000 plus should be made direct to R.C.A. Ltd., Sunbury-on-Thames, Middlesex.
WW324 for further details

## Oscilloscope Probe Adaptor

Sealeciro have developed a new right-angled sub-miniature adaptor for use with oscilloscope probes. Designated Conhex 55-005-0119, the device will convert standard shielded probes to right angled devices and is particularly useful for

multiple test point monitoring in complex circuitry. The unit can be screwed into the end of the oscilloscope probe assembly in place of the standard tip. All metal parts are gold plated and the insulator is of Tefion. Sealectro Lid, Farlington, Portsmouth, Hants.
WW317 for further details

## Remote Programming Digital Multimeter

Dana Electronics announce a new range of programmable digital meters-the 4433/235 (nonisolated output) and the $4434 / 235$ (isolated output). Both have isolated programming facilities for a.c., d.c., ohms and active filter as standard. The 4434 has the added feature of a built-in delayed command generator. These delays are appropriate to the function or filter speed called up and release the systems engineer from settingtime problems. The delayed command can be

over-ridden at any time by direct command. Prices: $4433 / 235-£ 1,050 ; 4434 / 235-\Omega 1,150$. Dana Electronics L.d., Dallow Road, Bilton Way, Luton, Beds.
WW326 for further details

## Monolithic Linear Multiplier

A monolithic linear four-quadrant multiplier, the MC1595, is available from Motorola. The output voltage is a linear product of two input voltages and a constant scale factor. The circuit is so designed that the scale factor and the input/output voltage ranges can be adjusted by the user to accommodate a wide variety of applications. Good linearity is obtained-typically $0.5 \%$ error for the X -input and $1 \%$ for the Y -input. Other features of the MC1595 are good temperature stability and an input voltage range of $\pm 10 \mathrm{~V}$. Applications of the MC1595 include arithmetic opera-
tions (multiplication, division, squaring, finding square roots, and determining mean square), detection (a.m., f.m., phase and synchronous), modulation /demodulation (a.m. and balanced), frequency doubling, direct reading electric power measurements, trigonometric operations, and electronic gain control. Also available is a relaxed specification version with a temperature range of $0^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$, known as MC1495L. The multiplier is housed in a TO-116, 14-pin, dual in-line ceramic package. Motorola Semiconductors Lid, York Hose, Empire Way, Wembley, Middx.
WW330 for further details

## P.C. Board Holder

The Keyston Mark 11 printed circuit work-holder is suitable for bench mounting or free standing. The work frame accepts boards up to $15 \times 10$ in ( $380 \times 250 \mathrm{~mm}$ ) and up to $\frac{\mathrm{in}}{\mathrm{in}}$ ( 3 mm ) thick and the working angle may be adjusted to suit the individual operator. The trunion mountings have

positive notch locations allowing the board to be reversed in a single operation. Extra guide rails can be fitted for simultaneous multi-assembly of smaller boards. A foam component-clamping pad is available. Keyston Engineers Ltd, 8 Tettenhall Road, Wolverhampton, Staffs.
WW312 for further details

## Instrument C.R.T.

The M-O Valve Co. announces an extension to its range of high performance instrument c.r.ts, with the introduction of the 1400 B -a single gun, mesh-p.d.a. type having a display of $10 \mathrm{~cm} \times 8 \mathrm{~cm}$

and an overall length of only 35 cm . The X -sensitivity is $11 \mathrm{~V} / \mathrm{cm}$ and the Y -sensitivity $5 \mathrm{~V} / \mathrm{cm}$. Deflection linearity is better than $5 \%$. A typical final anode voltage for the 1400 B is 12 kV and under these conditions it can be used in oscilloscopes having bandwidths of 100 MHz . The M-O Valve Co. Ltd, Brook Green Works, London W.6. WW323 for further details

## "'Communications" Transistors

Twenty new "communications" transistors manufactured by T.R.W. Semiconductors Inc, California, are now available from M.C.P. Electronics. All are designed to be capable of withstanding severe mismatch under adverse load or phase conditions. These 12.5 V devices are divided into four families. The five designated 2N5687-91 are for use in the $20-88 \mathrm{MHz}$ band and they range in power from 1.5 to 40 W . Series $2 \mathrm{~N} 5702-6$ is for use in the $144-175 \mathrm{MHz}$ band with a similar
output power range. Five transistors designated 2N5697-5701 cover the $450-470 \mathrm{MHz}$ band and have power outputs from 0.25 to 20 W . The fourth series, $2 \mathrm{~N} 5710-14$, is specifically designed for high level a.m. modulation applications. Power output in this group ranges from 0.3 to 20W. M.C.P. Electronics Ltd, Alperton, Wembley, Middlesex. WW305 for further details

## Electronic Switches

Now available from Interplanetric is a range of electronic switches, which employ Schottky diodes, for applications where high reliability, small size and fast switching is required. With low distortion and good transient response, the performance is claimed to be superior to that of balanced mixers used as switches. Low-loss, wide band, ferrite networks further contribute to the efficiency of the switches. Switching port voltages have been selected such that a positive voltage turns the switch on, and a negative voltage turns the switch off, thus avoiding the threshold uncertainty which results when zero switching voltage is used. Models are available with a built-in driver operating from a standard unipolar switching input compatible with common integrated circuitry. Interplanetric, 39-49 Cowleaze Road, Kingston upon Thames, Surrey.
WW332 for further details

## Pulsed J-band Gunn Diode

A pulsed J-band ( $12-18 \mathrm{GHz}$ ) hybrid mode Gunn effect oscillator has been announced by Plessey. Designed principally for use in high resolution, short range radar, these devices are made from epitaxial gallium arsenide layers grown by a process originating from the Allen Clark Research Centre at Caswell. The devices can be operated in both coaxial and waveguide cavities. Power outputs are up to 5 W under $1 \mu \mathrm{~s}$ pulsed conditions, and p.r.fs up to 50 kHz . Conversion efficiencies are between 7 and $12 \%$. Rise times are typically less than 2 ns , and typical input requirements are $30 \mathrm{~V}, 2 \mathrm{~A}$. Plessey Components Group, Microelectronics Division, Cheney Manor, Swindon, Wiltshire. WW333 for further details

## Heatsink Extrusion

The latest heatsink material to be added to the Jermyn range is the A25/2007. This extrusion offers a very large surface area with a substantial mounting web for the semiconductor. A feature of the extrusion is its light weight: for example a thermal resistance of $0.5^{\circ} \mathrm{C}$ per watt is typical for the heatsink type A25/2022 which is black anodized and has an overall size of approx. $115 \times$ $120 \times 140 \mathrm{~mm}$ long. The extrusion is also available in lengths up to 1 metre. Jermyn Industries, Vestry Estate, Sevenoaks, Kent. WW325 for further details


## Radiotelephone Fixed Station

A new radiotelephone fixed station has been announced by Pye Telecommunications Ltd. Known as the F30FM, the fixed station, which is fully solid-state, is suitable for simplex or duplex operation in one of four frequency bands in the range $32.5-174 \mathrm{MHz}$. There is

a choice of $12.5 \mathrm{kHz}, 20 / 25 / 30 \mathrm{kHz}$ or $40 / 50 / 60$ kHz channel spacing and the transmitter has a power output of 30 W . Modular construction in conjunction with printed circuit sub units provides easy access to all components and simplifies servicing. Pye Telecommunications Ltd, St Andrew's Road, Cambridge.
WW337 for further details

## Low Reverse-leakage Rectifiers

Solitron of America announce a series (F927) of high-voltage axial lead, low reverse-leakage rectifiers. The series has a pi.v. range of 5,000 to $25,000 \mathrm{~V}$ and a reverse leakage of $1 \mu \mathrm{~A}$ at $25^{\circ} \mathrm{C}$, and will handle 0.5 A at $55^{\circ} \mathrm{C}$ in free air. The

devices can be applied in all standard, single and polyphase rectifier circuits. The units are corona free and said to meet stringent electrical, mechanical and environmental specifications. Solitron Devices, Inc, 256 Oak Tree Road, Tappan, N.Y.10983, U.S.A.

WW320 for further details

## Phase Sensitive Detector

AIM Electronics announces a new phase sensitive detector type PSD 122A which has an output drift less than $0.005 \%$ per ${ }^{\circ} \mathrm{C}$ and with a full scale deflection of $\pm 5 \mathrm{~V}$. This means that zero drift is less than $250 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$. Linearity is better than $0.05 \%$ and there is an overload indicator which shows when the incoming signal is outside the permitted limits. The dynamic range is over 70 dB . The instrument has its own meter built in. The unit accepts a reference signal of over 100 mV r.m.s., which is used either as a quadrature or in-phase reference to the measured signal. The measured signal is 1 volt r.m.s. for full scale deflection of the meter (corresponding to $\pm 5$ volts at the monitor socket). The sensitivity may be increased to $1 \mu \mathrm{~V}$ r.m.s. input for full scale deffection by the use of AIM's standard range of filters and amplifiers. The PSD 122A has an input bandwidth of 150 kHz and a noise equivalent bandwidth of 0.025 Hz . Price $£ 147$. AlM Electronics Ltd, The River Mill, St. Ives, Huntingdon. WW 304 for further details

## November Meetings

Tickets are required for some meetings: readers are advised, therefore, to communicate with the society concerned

## LONDON

Sth I.E.E.-"Some feasibility studies of synchronized oscillator systems for p.c.m. telephone networks" by M. R. Miller and "Wisdom: a method of synchronizing distributed systems to a p.c.m. system" by P. A. Wing at 17.30 at Savoy Pl., W.C. 2.

5th I.E.R.E.-"C.A.D. of communication systems and circuits" by I'. S. Brandon at 18.00 at the London School of Hygiene \& Tropical Medicine, Keppel St., W.C. 1.

6th K.T.S.-"The application of silicon diode arrav targets in television camera tubes" by A. J. Wooigar and C. J. Bennett at 19.00 at the I.T.A., 70 Brompton Rd., S.W.3.

7ih I.E.E.-Colloquium on "Bio-electrical engineering and power sources" at 14.30 at Savoy PI., W.C.2.

7th Brit. Acoustical Soc.-"Microwave acoustics" at 17.00 at Imperial College, S.w. 7.

11th I.E.R.E.-Discussion on "Studies of the lower atmosphere by modelling techniques" at 18.00 at 9 Bedford Sq., W.C.1.
12th I.E.E.- "Mintech and the electronics industry" by I. Maddock at 17.30 at Savoy PI., W.C.2.

12th I.E.E.- "Noise problems in measurement" by Dr. E. A. Faulkner at 17.30 at Savoy Il., W.C.2.

12th I.E.R.E.-"I.ocomotive-borne computer for continuous train control" by M. S. Birkin at 18.00 at 9 Bedford Sq., W.C. 1 .
12th Soc. Environmental Eng.-"The British calibration service" at 18.00 at Imperial College, Mech. Eng. Dept., Exhibition Rd., S.W. 7

12th S.E.R.T.-"Industrial electronics" by A. F. Giles at 19.00 at the London School of Hygiene \& Tropical Medicine, Keppel St., W.C. 1.

13th I.E.R.E./I.E.E.-Second lecture on "Physiology for engineers" at 18.00 at St. Bartholomew's Hospital Medical College, E.C. 1.
13th R.T.S.--"Colour recording-a look at the 'video printing' and 'Vidtronics' systems" by R. J. Venis and J. Muliner at 19.00 at the I.T.A., 70 Brompton Rd., S.W. 3.

14th I.E.R.E./I.E.E.-Discussion on "Computer standardization: bane or blessing?
(an examination of the issues especially with respect to $1 / 0$ interfaces)" at 14.15 at Savoy I'I., W.C.2.

17th I.E.E.-Discussion on "Alternatives to degree examinations as a means of assessment" at 17.00 at Savoy PI., W.C.2.
18th I.Mech.E.-Discussion on "Computer aided design" at 09.30 at 1 Birdcage Walk, S.W. 1
18th I.E.R.E.-"Solid state television receivers-a pattern of second generation designs for monochrome and colour" by P. L. Mothersole at 18.00 at the London School of Hygiene \& Tropical Medicine, Keppel Si., W.C.1.

19ih I.E.E.-Discussion on "Instruments for the recovery of signals from noise" at 17.30 at Savoy PI., W.C.2.

20th Inst. Electronics.-"A technique for the evaluation of data communication networks" by M. B. Ashdown at 18.30 at the London School of Hygiene \& Tropical Medicine, Keppel St., WV.C.1.

21st I.E.E.-Colloquium on "R.F. and microwave industrial heating" at 10.00 at Savoy II., W.C.2.

21 st I.E.E.- "Recollections of the early days of the thermionic valve industry" by
S. R. Mullard and L. S. Harley at 17.30 at Savoy PI., W.C.2.

26th I.E.R.E.-"Management by objectives" by D. Simpson at 18.00 at 9 Bedford Sq., W.C.I.

27th R.T.S.-Symposium on "Professionalism and training in educational television" at 17.00 at the I.T.A., 70 Brompion Rd., S.W. 3.

## BELFAST

25th I.E.R.E.-"Audio frequency hi-fi amplifiers" by I. Hardcastle at 18.30 at the Ashby Inst., Queens University, Stranmillis Rd.

## BIRMINGHAM

12th R.T.S.-"Electronic video recording" by Sir Francis McLean at 19.00 at Broadcasting House, Carpenter Rd.

## BRIGHTON

11th I.E.R.E.- "The place of the library in electronic engineering" by Miss E. Garratt at 18.30 at the College of Technology.

## BRISTOL

19th I.E.E./I.E.R.E.-"E.M.I. 2001 colour television camera" by I. J. P. James at 19.00 at the University.

27th I.E.E.-Faraday Lecture "People, communications and engineering" by J. H. H. Merriman at 18.30 at Colston Hall.

28th I.E.E.-Faraday Lecture at 10.00 (students) at Colston Hall.

## CAMBRIDGE

13th I.E.R.E./I.E.E.- 'Digital control of radar displays" by H. Giles at 20.00 at the University's Engineering Labs, Trumpington St.

## CARDIFF

121h I.E.R.E.-"Moire fringe measurement and numerical control of machine tools" by A. T. Shepherd at 18.30 at the University of Wales, Inst. of Science \& Technology.

13th-"The electron microscope" by B. Rees at 19.00 at the University of Wales Institute of Science \& Technology, Cathays Park.

14th S.E.R.T-"Traffic control" by A. Gregory at 19.30 at Llandaff Technical College, Western Avenue.

## CHATHAM

20th I.E.R.E.-"The Concorde flight control and landing systems" by 1). M. Fryer at 19.00 at the Medway College of Technology.

## COVENTRY

13th I.E.R.E.-"The use of light frequencies in communications" by R. B. Dyott at 19.15 at the Lanchester College of Technology.

## DORKING

5th I.E.E.-"Medical electronics" by Dr. D. W. Hill at 19.30 at Martineau Hall, Dorking Halls.
25th I.E.E.-"Computer aided design" by J. A. Weaver at 19.30 at the Star \& Garter Hotel.

## DURHAM

26th I.E.E.T.E.-"Modern techniques of air-traffic control" by J. Henderson at 19.30 at the Universitv's Science Labs, South Road

## GloUCESTER

18th I.E.E.T.E.-"Electrics and electronics in aircraft" by H. Hill at 19.30 at the Technical College, Brunswick Rd

## HIGH WYCOMBE

18th I.E.E.-"Elementary principles of digital computers" by L. F. Cowan at 19.15 at the College of Technology.

## HUDDERSFIELD

27th IE.R.E.-"Lasers" by Prof. O. S. Heavens at 19.00 at the College of Technology, Dept. of Electrical \& Electronic Engineering.

## LEICESTER

13th I.E.R.E.- "Ground station aerials for satellite communications" by D. H. Shinn at 18.30 at the University Physics Lecture Theatre.

## LIVERPOOL

12th I.E.R.E.-"Aircraft and instrumentation" by C. A. Williams at 19.00 at the University's Dept. of Electrical Engineering.

## LOUGHBOROUGH

18th I.E.R.E./.E.E.-"Impact of microclectronics for circuit engineers" by C. S. Den Brinker at 18.30 at the University of Technology, Edward Herbert Bldg.

## MAI.VERN

13th I.E.R.E.-"Airborne collision avoidance systems" by S. S. D. Jones at 19.30 at the Abbey Hotel.

## MANCHESTER

18th I.E.R.E.-"Automobile electronics" by W. F. Hill at 19.15 at the Renold Bldg., U.M.I.S.T., Altrincham St.

27ih S.E.R.T.-"Siereo broadcasting" at 19.30 at Renold Bldg, U.M.I.S.T.

## NEWCASTLE-UPON-TYNE

5th S.E.R.T.- "The Post Office Tower of London" by A. W. Mead at 19.30 at the Charles Trevelyan Technical College, Maple Terrace.
12th I.E.R.E.-"Application of positive temperature coefficient thermistors" by C. G. Smith at 18.00 at the Polytechnic (Rutherford College), Dept. of Physics \& Physical Electronics.

## NEWPORT, I.O.W.

14th I.E.R.E. "Radar in a marine environment" by H. Giles at 19.00 at the Technical College.

## PLYMOUTH

13th I.E.E./I.E.K.E.-"Satellite communication" by J. Lawson at 19.00 at the University.

## READING

24th I.E.E--"Hi-fi" by J. Moir at 19.30 at the J. J. Thomson Laboratory, the University, Whiteknights Park.
25th I.E.R.E.-"Automatic test equipment" by O. H. Davie at 19.30 at the J. J. Thomson Laboratory, the University, Whiteknights Park.

## RUGBY

18th I.E.E.-Faraday Lecture "People, communications and engineering" by J. H. H. Merriman at 14.30 (students) and 19.30 (public) at the Granada Cinema.

## RUGELEY

61h l.E.R.L.-"Electronic musical instruments" by Leslie E. A. Bourne and B. Arnold at 19.00 at Shrewsbury Arms Hotel, Market St.

## SOUTHAMPTON

25th I.E.E.-Faraday Lecture "People, communications and engineering" by J. H. H. Merriman at 10.30 and 14.30 (students) and 18.30 (public) at the Guildhal!.

## Literature Received

For further information on any item include the appropriate $W W$ number on the reader reply card

## ACTIVE DEVICES

We have received the following literature from Nobel Electronics, Nobel House, 5-7 High St, Welling, Kent.

Semiconductor summary 1969, listing STC digital and linear i.cs, transistors and diodes WW401
Semiconductor price list for above catalogue ....................WW402
RCA Great Britain Ltd, Lincoln Way, Windmill Road, Sunbury-on-Thames, Middx, have produced the following publications:

RCA solid-state products guide .....................................WW403
SK series replacement guide
Mounting hardware supplied with semiconductor devices......WW404
Mullard minibook No. 3 "Semiconductor devices" has been prepared by the Mullard educational department as an introduction to semiconductor devices for those with only a very basic knowledge of electronics. It is available from Mullard Educational Service, Torrington Place, London W.C.1, price 5s.
Amendments for the AEI Semiconductors and Technical Data Book have been prepared by AEI Semiconductors, Carholme Road, Lincoln.

12A, amendments for Vol. 1
WW406
12B, amendments for Vol. 2
WW407

## PASSIVE COMPONENTS

West Hyde Developments, 30 High St, Northwood, Middx, have published a catalogue which describes the Contil Mod-2 range of p.v.c. coated instrument cases

WW408
Ferranti Ltd, Dunsinane Ave, Dundee DD2 3PN, Scotland, has the following microwave literature available:

The full range of products manufactured by Oxley Developments Co. Ltd, Priory Park, Ulverston, Lancs., such as Barb insulators, plugs and sockets and trimmer capacitors, is described in a catalogue ................WW411 Received from Erie Electronics Ltd, South Denes, Great Yarmouth, Norfolk, the following literature:

Moulded track potentiometers
WW412
Additional data sheets and price list for Erie catalogue
WW413
"Battery replacement guide" gives the RCA equivalent for batteries in the domestic products of over 300 manufacturers. RCA Great Britain Ltd, Lincoln Way, Windmill Road, Sunbury-on-Thames, Middx.

WW414

## HARDWARE

The "Zip Twist" fastener, which can be pushed on to studs of fragile material and given a quarter-of-a-turn to lock and which has a self-threading action for removal, is the subject of a leaflet from the Carr Fastener Co. Ltd, Stapleford, Nottingham NG9 8AJ
The "Pana Vise", which is a bench mounted vice allowing work to be held a any compound angle within a half sphere, is described, with accessories, in literature from Special Product Distributors, 81 Piccadilly, London WIV OHL

WW416
P.T.F.E. shapes, including rod, tube, sheet, strip and sleeving, are described in publication from Polypenco Lid, Gate House, Welwyn Garden City, Herts.

WW417

## EQUIPMENTS

A Ins rise-time sampling unit, the type S-5, which has a $1 \mathrm{M} \Omega-15 \mathrm{pF}$ input impedance, is described in a leaflet from Tektronix UK Ltd, Beaverton House, Harpenden, Herts

WW418
The following two booklets are available from Aveley Electric, South Ockendon, Essex:

Systron Donner analogue computers ( $10 / 20-40 / 80$ )
WW419
Aveley news (monthly) giving information on equipment imported from Germany

WW 420

A digital integrated circuit tester (type 51B) is the subject of a leaflet from John Reeve Instruments, 8 Ownstead Gardens, Sanderstead, South Croydon, Surrey CR2 OHH

WW421
A series of low-noise broadcast quality microphone amplifiers are described in a leaflet from Elcom (Northampton) Lid, Weedon Road, Industrial Estate, Northampton

WW422
A wide range of instrumentation is described in a booklet "New electronics for measurement, analysis and computation" from Hewlett-Packard, 224 Bath Rd, Slough, Bucks

WW423

## GENERAL INFORMATION

Available from the City and Guilds of London Institute, 76 Portland Place, London WIN 4AA, a publication called "SI Symbols, abbreviations \& conventions", price 2 s .
We have received two more books in the "Measurements concepts" series from Tektronix U:K. Ltd, Beaverton House, Harpenden, Herts. They cost 10s each including postage.
"Spectrum analyzer measurements" and "Automated test systems".
The latest edition of the British Amateur Electronics Club Newsletter contains a report of the Club's exhibition of electronic games and articles of constructional interest. Mr. C. Bogod, 26 Forrest Road, Penarth, Glam.
The following literature has been produced by the British Standard Institution, 2 Park Street, London W1Y 4AA:

PD6435: "Instructions to technical committees for the preparation of generic specifications for electronic parts of assessed quality", price 21s.
BS9500: "Sockets of assessed quality for electronic tubes and valves and plug-in devices: generic data and method of test," price 16 s .

## HF Predictions - November



It will be seen that the MUF for Johannesburg is just below 35 MHz for an eight-hour period with very small variations. This should provide excellent conditions in the $26-\mathrm{MHz}$ broadcasting band and the $25-\mathrm{MHz}$ amateur band. The South America curve tends to a similar shape and favourable daylight conditions can also be expected. The Far East route will require full use of frequency complements to combat the continually changing MUF.

LUFs depend partly on geographic variation of atmospheric noise level and therefore, unlike MUFs, do not apply to both directions of a route. Those shown were calculated by Cable \& Wireless Ltd for reception of specific point-to-point services in the U.K. but serve as a guide for all modes and services.

## Answers to ${ }^{6}$ Test Your Knowledge"-18

Questions on page 536

1. (a) The analogy is often justified by regarding the -guide as consisting of two centre-line strips joined by a conuminous row of quarter-wave stubs (making up the rest of the guide walls) on each side. This analysis is not, however, strictly correct since currents in the broad faces of the guide walls are not entirely transverse.
2. (d) This result is arrived at by considering the average value of the mean-square voltage across the wide faces of the guide, and the power flowing in the guide.
3. (b) Depending on its form the iris is equivalent to an inductance, capacitance, or combination of the two, shunting the guide. Its normalized admittance can be calculated from its dimensions.
4. (d) The slot must not interest lines of current flow in he guide walls.
5. (c) The position for the susceptance (post or iris) is found in terms of guide-wavelengths distance from the reference voltage minimum.
6. (c) Waveguide isolators, circulators and gyrators are non-reciprocal. These all use ferrite materials.
7. (d) In this way the reflections from the two cancel. The smaller the number of quarter-wavelengths (at the design frequency) the greater the range of frequencies over which the reflections will almost cancel.
8. (d)
9. (c) The energy stored depends on the volume of the cavity, the power dissipated on the cavity surface area.
10. (b) Since the standing wave pattern is in the same position at resonance as it is well away from resonance the cavity is undercoupled. Hence the coupling parameter is $1 / \mathbf{w}$.s.w.r.
11. (d) Since the source of reflection is genèrally many wavelengths from the input any slight change in frequency will cause a large change in the impedance which the guide presents to the generator. This, in turn, affects both the frequency and power output of the generator.
12. (b) This is an application of the high-low impedance principle in which alternate quarter-wave sections of high and low impedance guide are used.
13. (d) The wave travelling towards the short circuit suffers a reversal of phase on reflection, and this, added to the phase lag of $a$ radians introduced by the journey to the short circuit and back, causes the wave reflected from the short circuit to be in phase with the wave propagated directly in the required direction in the wave guide.
14. (d) To couple out energy from a guide a hole has to interrupt only lines of current flow, but the fields stimulated in the other guide must be correctly oriented to propagate in that guide.
15. (c) Matching elements are incorporated in the junction to achieve this condition.
16. (b) In the piston attenuator the atenuation is provided by a section of cut-off waveguide.

## the chuice <br>  <br> $\square$ <br> PREESTON BOWPONENTS <br> <br> are known all over the world <br> <br> are known all over the world FOR FOR originality originality <br> <br> and Quality

 <br> <br> and Quality}
## TAKE SWITCHES

Bulgin Moulded Insulation Switches are manufactured by the latest automatic methods with constant testing assuring that the highest standards of performance and finish are always maintained. All front of panel parts are plated in brilliant chrome, except where moulded operators are used, these are black. Internal contacts and solder tags are heavily silver plated for the best possible connection, all other metal parts are suitably protected against corrosion. and the polished black moulded bodies give excellent insulation.
A wide range of different models are available. Operation can be Toggle, Biased Toggle, Biased Push-Push (successional) Action, Push-Pull, Slider, key and Semi-Rowary shaft. Connection in all cases is to Solder Tags, with screw Terminals available to order as an alternative on some of the models. A wide range of modifications can be supplied, to agreed quantity orders. Proof test $=2 \mathrm{KV}$. at $50 \mathrm{c} / \mathrm{s}$ I.R. $\$ 100 \mathrm{M} 52$ drawing or recovered at 500 V .
The comprehensive range of Bulgin proprietary Switches of "laminated" construction, have, during recent years been supplemented by improved models of "moulded body" construction. Careful attention to design, and new production techniques have largely offset increased costs to the advantage of our customers. Every effort has been made to cover the largest field of application, without wasteful duplication or perpetuating types for which no reasonable demand now exists.



In the Profes-
sional and Commercial field the moulded range is increasingly being used and preferred and with this in mind we have produced a Wall Chart illustrating and describing the complete range of Moulded Switches now available, cross referenced to the old laminated types which they are replacing. in order to assist our customers select the current versions. In addition to this we also have a single sheet leaflet available showing the detailed test and inspection reports on SM.259/PD Single Pole type. the SM270/2 Double pole change over type and the SM.277/2. SM301/2. High Rating. D.P.M.8. and Double pole change over types. Ask for ref.

## SEND FOR COMPREHENSIVE MOULDED SWITCH/LAMINATED SWITCH EQUIVALENT LIST REF 1536/C.

[^6]
# Real \& Imaginary 

by Vector

## "Plus ça change, plus c'est la même chose"

This month I'm going to do something that I'm rather good at, namely sitting back and letting someone else do the work. The excuse for doing so is contained in a paper read at a meeting of the Institution of Electrical Engineers under the title "Co-ordination of Research in Works and Laboratories".
In his introduction H. R. Constantine, the author, reminds us that to be a great and prosperous nation today implies being at the forefront in scientific genius and in engineering capacity. He then takes his first sideswipe at us by saying that there was a time when this country was able to hold its own against any other nation, but that we are now in the process of falling asleep while others surpass us.
He goes on to say that the reasons why we have lost our commercial supremacy are not to be found in any lack of ability or want of inventive genius. Our backsliding has been mainly due to the lack of responsiveness by government authorities, manufacturers and financial leaders to the needs of scientific genius. Many examples (he says) could be given of new ideas or inventions devised by British brains which have been ignored here and have subsequently been taken up abroad. The situation is aggravated by the national characteristics of selfishness and stubbornness which prevents a Britisher from communicating his methods to his fellow workers. (Strong meat for any Learned Society to digest!)

Arguing for more co-ordination in research the author notes that powerful banking organizations exist to offer a stronger financial front against foreign competition while various employers' associations are in being to further business. There are also selling organizations to promote exports, so why not a research combine also?
He then sets out one approach to the problem. This envisages the establishment of a vast national research laboratory (or complex of laboratories) under the control of a government-appointed body consisting of en-gineer-representatives of universities and industry. The administrative side would be undertaken by another body, chosen for its business ability.

This maxi-laboratory would take over the whole of the pure research now done by universities, colleges, technical institutions and private or works laboratories. Any manufacturer who wanted a given matter researched would apply to the central au-
thority who would be in a position to tell him what had already been done in that particular line and to advise him regarding the best way to continue. Any research project brought to a successful conclusion would be passed to the central 'bank' where it would be freely available to any British manufacturer who wanted it. (Note that these suggestions apply only to pure research; each manufacturer would be free to conduct his own applied research.)

Having painstakingly built a nationalized edifice brick by brick (only a few of the main features have been decribed above) the author puts a substantial charge of high explosive in its basement and proceeds to light the blue touchpaper. The proposal (he maintains) is impracticable on grounds of cost. He then expounds an alternative scheme. This, much abbreviated, is a method of co-ordinating existing laboratories. It proposes a central board of control composed of private individuals representing the various interested parties-universities, manufacturers and so on. This board would keep full records of what individual laboratories were doing and would maintain records of published research work on the largest possible scale. The board would be given full powers to order any laboratory to undertake a specific piece of research or to leave another alone.
One essential feature of the scheme is to provide a posse of travelling engineers whose duties would be to visit the various laboratories at frequent intervals and to report back to H.Q. giving general and detailed accounts of what was afoot, or of research that was needed. New ideas would also be culled. As with his first suggestion the author recognizes that one of the prime requirements would be the establishment of an efficient central records office.
At this juncture the author pauses to consider the evils of continuing with a muluplicity of independent laboratories, each working in comparative ignorance of what others were doing. He makes the following points:-
(1) In general, manufacturers' laboratories tend to attempt too many researches at once and are not properly equipped to do any one of them.
(2) They are usually under the ultimate control of a top executive whose orientation is towards sales, not research.
(3) It is physically impossible for each individual firm to acquire and maintain a
technical library on a scale that ensures it contains information on everything.
(4) Each laboratory is intensely jealous of all rivals and will on no account let others know what it is doing. As a result, twenty firms could be carrying out exactly the same research work.
Item (4) is clearly a major stumbling block and the author is at pains to deal with it. In his scheme a manufacturer's research information would be sent to the central board under a strict seal of security; it would be used primarily for records purposes, to ensure that overlapping of projects did not take place.
University laboratories would still continue with their routine laboratory training programmes; the central board would be interested only in the absolutely new experimental work in hand. The board would work in close liaison with the univepsity authorites, merely ordering that specified research should be carried out over a certain period and giving general instructions as to how it should be approached.
Patents are one of the headaches in any such scheme and the author deals faithfully with this problem also. He suggests that an equitable solution would be to invest the central board with the responsibility of deciding whether it was worth while to take out a patent application in any given circumstance; if it were, the board would do so, paying all the attendant expenses. It would then proceed to dispose of the rights to those manufacturers declaring themselves interested, in consideration of agreed payments. After these payments had been pooled, the inventor and his assistants would be appropriately rewarded.

The author concludes by saying that in spite of the detailed proposals set out, the chief purpose of the paper is to draw attention to the need for fresh thinking on how research could best be handled, both in the national interest and for the benefit of manufacturers and universities. His final words are an appeal to the Institution to take the initiative and convene a conference of all potentially interested parties, "in order to settle in the first place the absolute necessity for some such concerted action and to come to some decision as to the general outlines that such a scheme would have".
In the discussion that followed the reading of the papers, the proposals were damned with faint praise. Some words of the final speaker are, I think, worth recording:
"I am perfectly certain it is a waste of energy to try to centralize the whole business of research . . overlapping lof research projectsl is a very good thing. There is a certain sporting element in overlapping and I think if an Englishman is to make any progress in research or anything else he must be able to feel that there is a certain amount of sport at the back of it all-money is not sufficient. There must be that sporting element of rivalry ...."
And that's about all I've room for; the paper itself is very much longer. But one final word if I may: The paper was read before the Institution just over fifty years ago and was published in the gournal of the I.E.E. in October, 1920. Meanwhile, relax. You're not being nationalized yet.



## Project 60 an exciting alternative

The buyer of an amplifier today has a remarkably wide variety to choose from. It is unlikely that a purchaser would have real difficulty in finding a unit that met all his requirements, although the price might not be as low as could be wished. The only snags are that one's needs can change and that the technically correct amplifier may be physically inconvenient. If you are confident that there is an amplifier available, of the right size and price, which will meet all your needs for the forseeable future, then that is your best buy. If not, however, we can offer you another possibility which we believe to be an exciting alternative approach. That alternative is Project 60.
Project 60 is a range of modules which connect together simply to form a complete stereo amplifier with really excellent performance. So good, in fact, that only 2 or 3 amplifiers in the world can compare with it in overall performance.
The modules are: 1 . The $\mathrm{Z}-30$ high gain power amplifier, which is an immensely flexible unit in its own right. 2. The Stereo 60 preamplifier and control unit. 3. The PZ. 5 and PZ. 6 power supplies. A complete system comprises two Z-30's, one Stereo-60 and a PZ-5 or PZ -6. The power supplies differ in that the PZ-6 is stabilised whilst the PZ-5 is not. This means that the former should be used where the highest possible
continuous sine wave rating is required. In a normal domestic application there will not be a significant difference between using either power unit unless loudspeakers of very low efficiency are being used.
All you need to assemble your system is a screwdriver and a soldering iron. No technical skill or knowledge whatsoever is required and, in the unlikely event of you hitting a problem, our customer service and advice department will put the matter right promptly and willingly.
Perhaps the greatest beauty of the system is that it is not only flexible now but will remain so in the future. We shall shortly be introducing additional modules which will include a comprehensive fllter unit, a stereo F.M. tuner and an even more powerful amplifier for very large systems. These and all other modules we introduce will be compatible with those shown here and may be added to your system at any time.
Project 60 modules have been carefully designed to fit into virtually every known type of plinth or cabinet and templates provided enable you to position them. Only holes have to be drilled into the wood of the plinth and any slight slips here will be covered completely by the aluminium front panel of the Stereo 60. The Project 60 manual gives all the instructions you can possibly want clearly and concisely.

# z-30 TWENTY-FOUR WATT CONTINUOUS SINE WAVE POWER AMPLIFIER 

The Z-30 is a complete power amplifier of very advanced design employing 9 silicon epitaxial planar transistors. Total harmonic distortion is incredibly low being only $0.02 \%$ at full output and all lower outputs. As far as we know, no other high fidelity amplifier made can match this specification, no matter what the price. Thus you can be utterly certain that your Project 60 system will do full justice to your other equipment however good it may be. The $\mathbf{Z - 3 0}$ is unique in that it will operate perfectly, without adjustment, from any power supply from 8 to 35 volts. It also has sufficient gain to operate directly from a crystal pickup. So in addition to its use in a high fidelity system you can use a Z-30 to advantage in your car or a battery operated gramophone for your children, for example. These, and many other applications of the Z-30, are covered in the Project 60 manual.

## SPECIFICATIONS

Power output-15 watts continuous sine wave into 8 ohms using a 35 volt supply: 24 watts continuous sine wave into 3 ohms using a 30 volt supply.

## APPLICATIONS

High fidelity amplifier: car radio amplifier: record player fed direct from pick-up. Intercom: electronic music and instruments: P.A.. laboratory work, etc. Full details of these and many other applications are given in the manual supplied with your $Z .30$.


Ready buif, tested and guaranteed, with 2.30 manual.

89/6

Frequency response: 30 to $300,000 \mathrm{~Hz} \pm 1 \mathrm{~dB}$.
Signal to noise ratio: better than 70 dB unweighted.
Distortion: $\quad 0.02 \%$ total harmonic distortion at full output into 8 ohms and at all lower output levels.
Size :
$3 t \times 2 \ddagger x$ inches.
Input sensitivity: $\quad 250 \mathrm{mV}$ Into 100 Kohms.
Damping Factor:
$>500$.
OutpurClass AB
Loudspeaker impedances 3 to 15 ohms.
Power requirements: 8 to 35 V.d.c.

## STEREO SIXTY PREAMPLIFIER AND CONTROL UNIT

The Stereo 60 is a stereo preamplifier and control unit designed for the Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout and great attention has been paid to achieving a really high signal-to-noise ratio and excellent tracking between the two channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs. The tone controls are also very carefully designed and tested.

## SPECIFICATIONS

- Inpur sensitivities-Radio-up to 3 mV : Magnetic Pickup- 3 mV Correct within $\pm$ $1 d B$ on R.I.A.A. curve. Ceramic Pickup -up to 3 mV : Auxillary-up to 3 mV . - Output-1 volt.
- Signal-to-noise ratio-better than 70 dB
- Channel marching - within 1 dB .
- Tone Controls-TREBLE + 15 to -15 dB at 10 KHz ; BASS +15 to -15 dB at 100 Hz .
- Power consumption 5 mA
- Power requirement-PZ.5 or PZ. 6 - Power requirement-P2.5 or P2.6. with black brush
- Mounting on cabinet front by spindle bushes and adjustable brackets.


Ready built, rested and guaranteed
£9. 19s. 9d.

## SINCLAIR POWER SUPPLY UNITS



PZ-5
30 volts unstabilised-sufficient to drive two Z-30's and a Stereo 60 for the majority of domestic applications.

Price: £4. 19s. 6d.
PZ-6 35 volts stabilised-ideal for driving two Z-30's and a Stereo 60 when very low efficiency speakers are employed.

Price: $£ 7.10 \mathrm{~s}$. 6 d .

## AT THE AUDIO FAIR STAND 95

## GUARANTEE

If at any time within 3 months of purchasing Project 60 modules from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service purchase
 22 NEWMARKET ROAD, CAMBRIDGE Pleose send

## SINCLAIR IC-10

## 10 WATT MONOLITHIC INTEGRATED CIRCUIT AMPLIFIER AND PRE-AMP



A 13 transistor circuit measuring only one twentieth of an inch square by one hundredth of an inch thickl

## the world's most advanced high fidelity amplifier

The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by one hundredth of an inch thick, has an output power of 10 watts. It contains 13 transistors (including two power types), 2 diodes, 1 zenor diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.
The IC-10 is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of the usual tone and volume controls and a battery or mains power supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs, servo amplifiers (it is d.c. coupled throughout), etc. Once proven, the circuits can be produced with complete uniformity which enables us to give a 5 -year guarantee on each IC-10, knowing that every unit will work as perfectly as the original and do so for a lifetime.

## USE THIS ORDER FORM FOR YOUR IC-10

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| \| for which l enclose cash/cheque money order |  |

## SPECIFICATIONS

Output: Frequency response Total harmonic distortion: Load impedance:
Power gain: Supply voltage: Size:
Sensitivity:
nput impedance: Adjustable extemally up to 2.5 M ohms.

## CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages. making battery operation eminently satisfactory.

## APPLICATIONS

Each IC-10 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transistors.
SINCLAIR
IC-10


AUDIO PHOTO-CINE FAIRS, OLYMPIA, STAND 95 SINCLAIR RADIONICS LIMITED 22 NEWMARKET RD, CAMBRIDGE Tel: 022352731

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Think of a stereo amplifier delivering 12 watts R.M.S into 15 ohms per channel and having a total harmonic distortion of $0.1 \%$ at full output at 1 kHz . Think what an overload factor of 29dB means on all inputs. Think what it means, too, to have a top-flight amplifier housed in a cabinet of elegantly original design that is both beautiful and completely practical back and front. Think what such an amplifier with its many desirable features might cost - then remember that by assembling the Peak Sound "Englefield" yourself from the pre-built lab. tested modules we design and make, you can own One of the best designed amplifiers you have ever heard for about £38. The ease with which you can do this will delight you. So will the performance and appearance of the complete equipment. The Englefield system enables you to use the exclusive design cabinet for either a $12+12$ watt assembly or $25+25$ watt assembly, the pre-amp and tone control unit module being common to either. Each has its own built-in necessary power supply unit.

## SPECIFICATION

Using two Peak Sound PA 12.15 s . SCU 400 and PS 45 K Power output per channel 13 watta into $15 \Omega$ : 18 w into $8 \Omega$ : 24 w into $3 \Omega$. all R M S
Frequency bandwidth -10 Hz to 45 k Hz for $1 \mathrm{d8}$ at 1 wall
Total Harmonic Distortion at 1 kHz at 115 w into 15 s
Input senartivities- Mag P.U $\quad 35 \mathrm{mV}$ imp.
Mag P.U 35 mV Imp
R|A.A.
equalized Tape-
100 mv linear: Radio 100 mV
linear
29aB on all input channels -65 d 8 on all inputs
Volume: Trebia $1+12$ to $\begin{array}{ll}-12 d 8 \text { af } 10 \mathrm{kHz}: \text { Bass } \\ -12 d 8 & \text { to }+12 d 8 ~ \\ -100 \mathrm{Hgl}\end{array}$ ilter $9 \mathrm{kHz}^{10}+12 \mathrm{~dB} 100 \mathrm{~Hz}$ ) ctave: 9 kHz of 12 dB /per octave: Mo
Balance
Jang iwo PA 2515 amplifiers and PS/68S power supply

35 w into 8 watts

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A highly efficient and dependable
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5-10 MULLARD 10-10
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## COMPONENTS, ACCESSORIES, etc.



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Betrery Record Player. Mude by Collaro. This is mide up on anit plate with speed aelector and plck up. The turntable Atited with the funcous "Atudio cartridge. Price 68/6. Poat and lan. $6 / 6$
 85 Wate Tubular Element. Very well made, unit. The ietment is wound on - poreelain former then oncaeed in a

pued sa single pole, 10 A. contacte 250 volt working. Bingle hoie Axing. $2 / 6$ each. 24 - dozen.
Door 8 witeh, Contacts open when pluager In depreased Maite by Arrow. $3 / 6$ each. $38 /-$ per dozen. 230 volt working Rotary Appliance switec. $16 \mathrm{~A}, 230$ rolt on moulded ceranilo
 This in an excellent Lotally encloned motor, powerful enough otc. Its npeed is 1.450 pm . Maide, wanaing machine


## FLEX BARGAINS

 Bcreenedlasulated and cobourex, the
3 corese lald together and metal braided overall. Price
15 A 3
3 cores, protected by tough rubber sheath then black coltod braided with white tracer. A normal domeetic fiex as fitted
 10A a Core Noo-kink Thax. As above but cores are 28/0076 or cut 10 your length $1 / \theta y \mathrm{~d}$. yd . 1005 d . coll $\mathbf{£ 7 . 1 0 . 0}$ A 2 Core Flex. An above, but 2 cores each 23,0076 as used

## 3-CORE WATERPROOF FLEX

8A. 23/0076 clrcular PVC covered as nited to electric drill and most portable appliances, dieal ertension lead. Regrla Elliot Sealed Contset Reed Relay. Three clrcuits cloned by vol or looma. $8 / 6$ each.
Slim Tubular Mierophone. For hand holding or frontal plugs for cassette tape recorder but sultable for most amps. 18/6
S00MA Moviag Coll Meter. 21 n. funh mounting round meter
TANGENTIAL HEATER UNIT


UNIT
Winter ls coming
but act today and but act today and
you won't dis.
may. This heater unf. This the very
untest type, most Intest type, most
eflctent mad
quiet running. Io blower heatere costing $\mathcal{C 1 5}$ and more. Wh hav or and Unlts complete, wired ready to fit into canees, i.e. motor impeller, 3 kW , heater switchlog 1 , 2 and 3 kW . nnd with thermal anfety cut-out. Can be fitted lnto any metal line
case or cabinet. Only need on/ofis awitch,' 70/6. Postage and case of cabinet. Ony need on/s.
insurance $6 / 6$. Don't mise this.

STEREO CABINET
Size 25 in . $\times 14 \mathrm{ln}$. $\times 9 \mathrm{tin}$. deep-apeaker compartment each end. Oeptre portion with hinged lid and removable bottom has platiorm for autochanger and room for ampliter. Two tone (red and grey) rexine covered but lou apenker ends need metal
Carriage and packing 15/.


## SOLDER GUN A muat for every busy man, ives alnont Instant heat; alao illuminate BIO JOB 250 watt model $98 / 6$ (saver you over E 3.10 ), poat and the. $6 / 6$.

## BUY TIME SLOT METERS

If you Mre out equipment such na TV apta by the hour then thene shot
metern are what you require. We have 3 typen Rd meteriare what you require. We have 3 typen, ge. un hour, $1 /-$ and hour
and $1 / 6$ ni hnur. Brand new. Made oy the famous Weton Company. and $1 / 6$ and hnur. Brand new. Mat


## HORSTMANN 'TIME \& SET' SWITCH

(rama hmp 8 witch). Juat the thing it you want to come home to a witch on tme of your electric fires, etc., up to can delay the eething thme or you can use the Ares, ettch to, up to 14 hours from
of up to 3 hour. Equall on perfod price probably around 25 . Bpecial snip price 29/8. Pout and
ins. 4/6. ANELS
DISTRIBUTION PANELS
Jart what you need for work bench or lab. $4 \times 13 \mathrm{mmp}$
sockets in metal box to take standand 13 mmp funed




## ELECTRIC TIME SWITCH

Made by Brnithathene are AOmalnsoperated, NOTCLOCK WORK Idesil for mounting on rack or shelf or can be bulk into box with
13 A encket. 2 completely and justeble time periods per 24 hour sA ehangenver contacte will nwitch circuit on or off during thene perioda.


## 3 STAGE PERMEABILITY TUNER



This Tuner in a precinion inntrument made by the famoun "Cyldon" Company for the equally famous Radiomoblie Car Railo. it is a medumn ware tuner
(but set of longwave colla avallable as an extra if requifed) with a frequency




## THE TWENTYLITE <br> 

A Flunrescent Ilghting uolt tanade by the famolas Athan company, with auper allent
polyester Allied ehoke and radlo suppressed t tarler. The tube springs in astud
out and the whole uit to beant out and the whole ubit is beautifully
made and tinished while enamel. Amaz. made and finduhed White enamel. Amaz-
ingly evonotnical. If laft on all the thme unit). Mensures 2 tt , long. Is ldeal Kitchen, Bedroom, Hallwmy, Porch, Loft, etc. (uses t unit). Measures 2tt, Iong. Is ldeal Kitchen, Bedrom, Hallway, Porch, Lott. etc. Don't
misa this amazing offer, $38 / 6$ with tube. Assembled ready to inatill. Pont nad Ins
$6 / 6$ extra.


## DREAMLAND CLOCK SWITCH

The wonderful DREAMLAND mains operated clock switch will antomatically awitch your blanket on and off each evening and you will always have a warm bed. It's luminoua; you can always ace the tlme and it's a really beautiful unit. Anldesigift. Can almo cont rol taperecorder, radio, lamp, ete.. up to $500 \mathrm{w}, 38 / 6$ plus $3 / 6$ post and ins.

1 WATT AMPLIFIER PRE-AMP head Gistorn -hutghy equally uftablent made for microphone or pich tapeLimited quantity $28 / 6$. Full circult diage ar plek up.
tape controls $5 /-$. be controls $\$ /$


## VARYLITE

Will dim incandeacent lighting ap to 600 whtt from full brilliance to out.
 may be fited la place of this. of mount
plastic boz with control knob $£ 3.18 .6$.

## HI FI BARGAIN

FULL F1 18 INCE LOUDSPEAEER. This is undoubtedy one the finest loudepeakern that we have- Thin is undoubtediy one of ond li atrongly recomanended for Hi -Fi load and Bhythro atal frame public addreas.
Plux Density 11,000 ganss-Total Flux 44,000 Maxwellm-Power
Hand



 18th. 100 watt $£ 24 \cdot 10.0$.

MINIATURE WAFER SWITCHES


2 pole, 2 way - 4 pole, 2 way- 3 pole, 3 way4 pole, 3 way- 2 pole, 4 way- 3 pole, 4 way2 pole, 6 way- 1 pole, 12 why. All at $3 / 6$ WATERPROOF HEATINA ELEMEENTATING
26 yarda length $70 W$. Sel-ragulating
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## AC FAN

Binall bat very powerful
maina motor with 64 in . blades. Ideal for cooling equipment or as extracefficlent. 17/6, post $4 / 6$. efficlent. 17/6, post $4 / 6$. Mount from back or
front whit ABA berews.


QUICK CUPPA
Minl Immeralon Heater, 350 w . 200/240v-
Boila full cup in about two Use any socket or lamp holder. Haviene ni bednide for tea, baby's lood, otc. $18 / 6$,
poost and innurance $1 / 6$. 18 v , car mode post and insur
alao available.

## RADIO STETHOSCOPE

Easiest way to fand find--tracen algnal
from nerial to speaker-when algnal stope you've found the fauk. Une It on pleto kit comprisess two special transis. tors and Anp parts
 instead of earpiece $7 / 6$

## MAINS TRANSISTOR POWER PACK

 sble output operate traniator ats and amplifiers. Adjust Working. Taked the place of any of the following batcertes: PP1, PP3, PP4, PP8, PP7, PP9, and others, KIt comprises: condensers and tatructions. Real anip loed resistor plus $3 / 6$ postage.PROTECT VALUABLE
FROM THERMAL RUNAWAY OR OVERHEATtrumstars, otc., which use beat-atnks can easily be
protected. simply make the contaot the rmostat part of equipment renerally, can
 by having thermontats in atrategle apots on the calng, Our 90 deg. to 190 deg. F. or with the dinl removed range netting PHILIPS TRIMMER 0-30pf an old deslgn but one which has
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MOTOR
Very powerful 7 r.p.ma., operates fróm
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## SPRING COIL LEADS

na fitted to teiephones.
\&/6 ench, 3 core $2 /=$ each,

## PP3 BATTERY ELIMINATOR

 Rua your armall iranalstor radio ifomthe maina-full wave circult. Made up ready to wire tato your set nid
sdJustable high or low current.
$8 / 6$ each.

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CONDENSER
Proved design, ideal for strait
circuits $2 / 6$ each. $84 /-$ doz.


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＂SPECIAL OFFER＂
Solartron Highly Stabilised P．S．U． Model SRS I5IA
Putput $20-500 \mathrm{y}$ ．in two ranges．Positive line at 300 mA ．Variable output 170 v ．fixed；0－170 v． variable．Two A．C．outputs at 6.3 v．A．C．are provided．
These units are offered in first－class condition． For A．C．mains． $200-250$ v．A．C．Overall case dimensions $20 \times 16 \times 10$ ins．approx． Price $€ 35$ ．$\quad$ Packing and carriage 30／－ Hand book available with P．S．U．
＊TRANSISTORISED STABILISED＊ Low Voltage P．S．U．Type 4D
$3-30 \mathrm{v}$ ．D．C．at 3 amps．Fully variable．
Current limiting control．
Sensing facilities for remote operation．
Protected and fused for $110 / 250$ v．A．C．mains． Small size only： $5 \frac{1}{2} \times 5 \times 11$ ins．deep．
Stability：1000－1．
Ripple：$I \mathrm{mV}$ ．max．Weight： 16 lbs ．
These units are buile to high present－day standards and are offered BRAND NEW BOXED at $\$ 20$ inclusive of post and packing．

## ALSO AS ABOVE

1 amp model．Type 48
Size $4 \times 3 \frac{1}{2} \times 7$ ins．Weight： 6 lbs．
Price $\mathbf{E 1 3 . 1 0 . 0}$ inclusive of post and packing．

## UHF RECEIVER R．D．O．

With 3 R．F．cuning units to cover $38-1000 \mathrm{MHz}$ ． These receivers are built to U．S．Navy specifica－ tions and are ideally suitable for laboratory and communications use．For 240 v．A．C．operation． Price El 05.

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## PORTABLE 12 v．BA゙がきRIES

 Non－spillable lead acid type．Rating： 12 v ．4 amp．hours，will withstand heavy overloads 4 amp．hours，
without damage．
Size $4 \times 4 \times 4$ ins．Weight： 4 lbs ．
Supplied fully sealed／charging instructions． BRAND NEW BOXED $45 / \mathrm{F}$ ．Post and packing $4 / 6$ Ideal for Model Boats and Photo Floods，etc．

A．E．I．MINIATURE UNISELECTORS Coil resistance 250 ohms．Type 2200A．Supplied with base．Quantities available．


Price $\mathbb{E 4}$ ．19．6
VIBRATING REED FREQUENCY METERS Range $55-75 \mathrm{c} / \mathrm{s}$ in 2 scales，having total length of 10 ins．for 110 v ．（or 240 v ，with transformer）． Manufacturer：Trub Tauber，Zurich．Price \＆12．10．

NIFE BATTERIES－NICKEL IRON We have for disposal complete sets comprising 2 batteries to a total of 12 V ．at $180 \mathrm{amp} /$ hours． Supplied filled as NEW CONDITION
Price $\mathbb{4} 45$ per set．Carriage extra．

DIRECTIONAL COUPLERS FOR
REFLECTOR POWER MEASUREMENT One of the major uses of a directional coupler is to obtain a sample of the R．F．Power in a trans－ mission line and apply it to an indicator．We can supply couplers with a power handling capacity of up to 300 Watts，the response is flat over the $66-88 \mathrm{Mc} / \mathrm{s}, 156-184 \mathrm{Mc} / \mathrm{s}$ and $200-450 \mathrm{Mc} / \mathrm{s}$ bands． Two pick－up probes are mounted on the coupler， one giving incidence the other reflective power the voltage developed is rectified and may be fed to a calibrated meter，C／W 50 ohm plugs． Price 60／－．

## R．F．ATTENUATORS TYPE A38

These attenuators are contained in a screened cast case and are suitable for the audio to VHF range up to $300 \mathrm{Mc} / \mathrm{s}$ ．Input level 0.5 watts max． Impedance 75 ohms．Attenuation 80 dB in steps of 20 dB ．Weight： 9 oz．Panel mounting．List price fl 10 ．Special offer price $85 /$ post paid．

BURNDEPT R．F．PLUGS
These difficult－to－obtain plugs，suitable for Londex aerial，C／O relays and other types of equipment， are supplied NEW EX CABLES at $4 / 6$ each or 3 for $12 /-$ ．Post and packing 6 d ．

## EDDYSTONE DIALS

Complete tuning unit，Catalogue No．898．Com－ plete with logging scale／flywheel tuning and fixing instructions．Supplied BRAND NEW BOXED． 70／－．Post and packing 4／6．

EDDYSTONE DIE－CAST BOXES
Contains sensitive amplifier originally intended for amplification of P．E．cells．C／W input socket，fuse， signal lamp，P．S．U．（mains）amplifier，fully transis－ torised．BRAND NEW 32／6．Post and packing 2／6．

## LEDEX ROTARY SWITCHES

Standard wafer size： 13 ins．Single－pole 12 －way， 3 －bank flange mounting． 48 v ．D．C．coils．Minimum voltage 30 v．D．C．Supplied BRAND NEW $45 /-$ Similar to above but one wafer with long spindle to enable user to make up to own requirements． Coil voltage： $30-48$ v．D．C．BRAND NEW $35 /-$

## NON－INDUCTIVE RESISTORS

These are high quality heat sink type．Rated at 15 ohms， 250 watt．Size only $4 \frac{1}{2} \times 2 \times 2 t$ ins． A Dale product at a surplus price．Only $19 / 6$ each， post and packing $2 / 6$ ．

## IMHOFS INSTRUMENT CASES

Finished in mottled grey stove enamel with satin Finished in mottled grey stove enamel with satin
finish trim．Size width for standard 19 in．equip－ finish trim．Size width for standard 19 in．equip－
ment．Height 10 ins．Depth 15 ins．With front ment．Height 10 ins．Depth 15 ins．With front
panel and ventilated rear panel．Supplied BRAND panel and ventilated rear panel．Supp
NEW $£ 4.10 .0$ each．Carriage $10 /-$.

## COMMUNICATIONS RECEIVERS

Redifon R50M． $16.5 \mathrm{Kc} / \mathrm{s}-32 \mathrm{MHz}$ in 8 bands． These well－known receivers are in world－wide These well－known receivers are in worially built to marine specifications． use．Especially built to marine specifications． Price as new $\neq 105$ ．Used model reconditioned to
specification $\notin 85$ ．Supplied with mains 240 v．A．C． specific
P．S．U．

## CINCH PRINTED CIRCUIT <br> CONNECTORS

Edge type，gold plated．Length 5 ins．30－way， 5／16 spacing． 4 for 10／－．Post and packing 1／－． Quantities available

HIGH VALUE RESISTANCE
BOX TYPE R． 7003
Specification．Range： $0.01-11 \cdot 10$ Megohm in 0.01 Megohm divisions．Accuracy： 0.05 per cent． Maximum power rating： 0.1 watt per step．Case： Hammer finished stove enamel． List price $£ 60$ ．Our price $£ 22$ ． 10.0 ．

## PORTABLE WHEATSTONE

BRIDGE
Specification．Type：Moving Coil Galvanometer． Ranges：（1） 0.05 to 5 ohms；（2） 0.5 to 50 ohms； （3） 5 to 500 ohms；（4） 50 to 5,000 ohms；（5） 500 co 50,000 ohms．Scales：Switched．Slidewire： 0.5 to 50．Galvanometer Scale： $10-10$ ．Case： Moulded plastic．Internal Source： 4 v ．Dry battery． Operating Temperature：+10 to +35 deg．C． Operating Humidity： 0 to 80 per eent $0 . \mathrm{m}^{\mathrm{kg} \text { ．}}$ List price E 25 ．Our price $\mathrm{E9.19.6}$ ．

PORTABLE MULTIRANGE METER


Specification．Ranges： $0-60$ and $0-300 \mu \mathrm{~A}, \mathrm{D} . C$. $0-3,0-30$ and $0-120 \mathrm{~mA}$, D．C． 1.2 and 12 amps D．C． $0.6^{-3}$ and $6-30 \mathrm{~mA}$ ．A．C．24－120 mA A．C． $0.24-12$ A．A．C． $3-12-30-300-600-1,200$ and 6,000 v．D．C． $0.6-3,2 \cdot 4-12,6-30,60-300,120-600$ $240-1,200$ and $1,200-6,000$ v．A．C． $3-333 \mathrm{ohms}$ ， $0.3-30 \mathrm{Kohms}, 0.03-3$ mezohms D．C．Resistance -12 Kohms， 0 Decibels．Frequency： 50 cps．Input Resistance D．C．20，000 ohms／volt．Input Resist Resistance D．C．： 20,000 ohms volt．Input Resist ance A．C．： 2.000 ohms voit．Temperature Range mm ．Weight： 8 kg ．Supplied with 2 voltage mm．Weight： 8 kg．Supplied with 2 voltage
dividers，$H . V$ ．leads，spare rectifiers， 1.5 and 22.5 v ．battery

List price $£ 25$ ．Our price $£ 10.19 .6$ ．
RHODE AND SCHWARZ EQUIPMENT Polyskop II． $0.5-1,200 \mathrm{MHz}$ ．
Diagraph Type ZDD． $300-2,400 \mathrm{MHz}$ ．
Signal Generator and Klystron Power Supply
Type SMCB． $1 \cdot 7-5,000 \mathrm{MHz}$ ．
UHF Signal Generator Type SCR．1，000－ $1,900 \mathrm{MHz}$ ．

## UHF Millivoltmeter Type URV．

BOONTON SIGNAL GENERATOR
TS 497／B／URR
Attenuation 0.1 micro v － 100 mV ．
Supplied in very good condition．
Supplied in very good condition．
Frequency coverage： $2-400 \mathrm{MHz}$ ．
SCHOMANDLE FREQUENCY METER FDI with Type FDMI Adaptor
Range： $30-900 \mathrm{MHz}$ ．
Approved by G．P．O．as standard for mobile communications equipment，etc．

MARCONI DIGITAL FREQUENCY METER TF 1325／2
Range，with plug－in，up to 220 MHz ．
Supplied AS NEW E325 with plug－ins．
ADVANCE FREQUENCY COUNTER TIMER－TYPE TC IA
6 digit in line read out．
List price $£ 390$ ．Our price $£ 95$.
FLUKE DIFFERENTIAL V．T．V．M．
MODEL 821A
Range： $0-500 \mathrm{v}$ ．and $001-10 \mathrm{v}$ ．as null detector．
ENGLISH ELECTRIC INSULATION TESTERS
Fully variable to 10 kV ．Metered output on voltage and current for 240 v ．A．C．operation． voltage and current for 24 each．
Supplied AS NEW at 63 ．

Marconi TF913 AM／FM signal generator． Marconi TF894 audio tester $10 \mathrm{c} / \mathrm{s}-12 \mathrm{KHz}$ Marconi TF899 A．C．millivoltmeter
Marconi TFI95 BFO range $0-40 \mathrm{KHz}$
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Marconi TF723A crystal calibrator
Marconi TF762C UHF signal generator 200－ 400 MHz
Marconi TF3 40 output power meter
Marconi TF102 amplitude modulator
Marconi TFllo4 television sweep generator
Marconi TF6758 pulse generator
Marconi TF6758 pulse generato
Marconi TF886A circuit magnification meter
Marconi TF329G／I circuit magnification
Marconi TF329G／．．．．．．．．．
meter
Marconi TFl345／2 digital frequency meter with 2 plug－ins．Range continuous to 220 MHz ．As new
Marconi TF890A／4RF＂$X$ band signal gen－ erator
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Marconi TFl44G signal generator $\ddot{8} 5 \mathrm{KHz}$ 25 MHX

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## INFRA-RED TRANSMITTERS \& RECEIVERS

## INFRA-RED PHOTO RECEIVER - MSP3

Ulira sensitive detector/amplifier for infra-red (Gallium Arsenide) or visible light optical links reception. Spectral response 9500 A. Robust, cylindrical package is coaxial with incident light to facilitate optical alfignment and heat sinking.

85/

max ratings
Total dissipation (in Ifee aith, $T_{\text {omb }}=25^{\circ} \mathrm{C}$ ) $\quad 100 \mathrm{~mW}$. Derating Factor......... $2 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ Outpur Current Intensity $\quad 100 \mathrm{~mA}$. Voltage $\quad . \quad 25 \mathrm{~V}$. Operating Temperature . From Supplied complete with suitable lenses, full Technical Data and Application Sheets, including Line of Sight Speech Link.

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CADMIUM SULPHIDE CELLS (Cds)
Inexpensive light sensitive resistors which require only simple circuitry to work as lights, exposure meters, brightness controls, automallc porch lights, etc, Not polarity conscious - use with A.C. or D.C. Spectral response covers whole vislble light range.
 MKY101-C
Epoxy sealed. In, diam. $x$ in. thick. Resistance at 100 Lux -500 to 50 mW . Maximum voltage $150 \mathrm{~A} . \mathrm{C}$. or D.C. Maximum curreni

MKY71


Glass sealed with M.E.S. base. Glass envelope in in. diam.. overall length 1 in. Resistance at 100 Lux - 50 Kohms 10150 Kohms. Maximum

## PHOTOGENERATIVE CELLS



REED SWITCH COILS \& CAPSULES

i mal of multiple switch circuits in an extremely small space. They eliminate the bulk and open contact disadvantage of electro-mechanical relays: hermetically sealed contact isolation ensures longlife aliability. Small enough to combine with solid-state components on printed circuit boards. Ideal for witching matrices, binary kis, control systems. etc. These were removed intacr from highly expensive computer mechanisms and are guaranteed to be in perfect working order. Each capsule end for the removal and replanement or nd to
Types available
R/C2 Two reed switches. contacts normally open. Size overall: $1 / \mathrm{k} \times \mathrm{i} \times \mathrm{in} .5$ - post free R/C4 Four reed swithes. contacts normally open. Size overall: $1 i x i x \mid$ in 10 -post free R/C6 Six reed switches. 4 contacts normally open, 2 normally closed. Size overall: 1 i $\times 1$ if $\times$ in.
$15 /$ post free

Unique devices in a brand new electronic field that can be exploited in a wide rang of applications. Miniaturized construction and solid state clrcuit design is combined with ourstanding modulation and switching capabilities to provide infinite possibiti ties as short distance speech and data links. remote relay controls, safety devices burglar alarms, batch counters, level detectors, etc., etc.

GALLIUM ARSENIDE LIGHT SOURCE-MGA 100 Filamentess. infra-red emitter in a robust, sealed cylinder coaxial with beam to facilltare oplical
alignment and heat sinking.

post free
max ratings
Forward current IF max." D.C..... 400 mA . Forward peak current If mox." (pk)......6A Power dissipation $\quad . \quad 600 \mathrm{~mW}$. Derating factor for $T_{\text {amb }}$ greater than $25^{\circ} \mathrm{C}$. Reverse voltage $V_{R}$ max aluminium hear sink $1 \mathrm{in} . x \frac{1}{1} \mathrm{in} . x \frac{1}{2}$ in.
Supplied complete with suitable lenses, full Technical Data and Application Sheets. including Line of Sight Speech Link.

## FIBRE OPTICS

Highly flexible light guides that transmit light to inaccessible places as easlly as electricity is conducted by copper wires. Fibre optics make it possible to control. and to operate photoct devices, lagic circuits, or one source to many places at once sible. Proops offer both glass flbre optics or Inexpensive Crofon plastic fibres for hundreds of experinents or serious applications in a fascinating new science.

RANK TAYLOR-HOBSON ENGINEERS KITS


Basic fibre optic components that demonstrate new ways of employing light in serious appliallons. Two kits are available : each contains hign-grade glass-fibre light guides consisting lexible sheaths with ferruled, optically polished ends. together with connecting and light source components. Each is supplied complete with card wallets containing technical and application data

Contains: $3 \mathrm{~mm} . \times 18 \mathrm{in}, 6 \mathrm{~mm}$. $\times 12 \mathrm{in}$. light
guides: 1.5 mm . $Y$ 'guide with two 12 in . long tails: 24 in. long 12 exit component for cading or punched card applications. 24 in . lengiths of Grofon 64 filament and monofilament plastic light guide. Also, coherent solids consisting of 25 mm . diam. Field flattening lens. 6 mm . $\mathrm{mm} \times 25 \mathrm{~mm}$ image inverior Complete with 2-way adaptor, fibre optic torch and batteries $3 \mathrm{~mm} . / 3 \mathrm{~mm}$. and $3 \mathrm{~mm} / 1.5 \mathrm{~mm}$ connectors.
£16
£28
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Newly developed plastic light transmitting media made by Du Pont and consisting of 64 special plastic flbres, each . 10 in. diam. and bundled together in a tough. flexible sheath. Can be used for many serious projects and inexpensive prototype work. Ends can be ground flat, dyed or No loss of light through bending. 12-page data and applications booklet supplied.


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Sutable for light dimming and motor control circuits
Gate-controlled, full-wave. A.C. silicon swith whith integral frigger that block or conducts instantly by applying reverse polarity voltage. Suitable for A.C operation up to 250 volts; controls currents up to 1440 watts. Size only $\frac{8}{}$ In. diam. $x \frac{1}{1 /}$ in. high. Complete with heat slnk. data and applicatlons
information. 45/-post free


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## ELECTRONIC ANTENNA CHANGEOVER SWITCH

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An extremely flexible closed-circuit system made by Britain's largest manufacturer of electronic equipment. The basic system comprises two units-camera and control monitor. The units are fully transistorised with a wide use of printed circuitry making for compact size, simple installation and high reliability (both in and out of doors). High sensitivity and 625 line resolution ensure excellent picture quality under normal lighting conditions. Closed circuit television provides the penetrating, all-seeing eye that scans, inspects, controls and directs-that is today accepted as invaluable in almost every aspect of industry, commerce, transport and education. A wide range of accessories are available which further increase the system's almost limitless applications.

## A LIMITED QUANTITY OF COMPLETE SYSTEMS AVAILABLE



SYSTEM SPECIFICATION Scanning standards: 625 line, 50 fields, $2: 1$ interlace. Horizontal resolution: 600 lines, Bandwidth: $8 \mathrm{Mc} / \mathrm{s}$ over complete system. Linearity: $\pm 2 \%$ positional error. Geometry: $\pm 2 \%$ of rectangle averaged over picture. Auto Sensitivity: over the range $60: 1$ in light value-normal picture obtained with illumination of only 2 ft . candles ( $50 \%$ subject reflectance) at lens aperture of $\mathrm{f} / 2$. Spectral Response: Panchromatic. Ambient Temperature: Max. temperature for all units $-30^{\circ} \mathrm{C}$. to $+55^{\circ} \mathrm{C}$. Power requirements $90 / 130 \mathrm{v}$. and 200/240 V. A.C., $50-60 \mathrm{c} / \mathrm{s}$. Consumption: 45 watts including camera. Camera Lenses: Standard 16 mm . cine lenses with " $C$ " mounts are normally used. Accessories : See under Camera and Control Monitor.


## CAMERA

Totally enclosed dustproof unit only $3 \frac{1}{4} \times 4 \times 10 \frac{1}{2}$ in., weighing 4 lb . Finished in two-tone blue/grey. Vidicon tube. Automatic sensitivity control enables the camera to maintain full picture quality over a brightness range of $60: 1$. 625 line width of $8 \mathrm{Mc} / \mathrm{s}$. All supplies are , frame synchronised to mains supply. 600 lines horizontal picture definition with a band width of $8 \mathrm{Mc} / \mathrm{s}$. All supplies are obtained from the control monitor (consumption 5 watts),

## CAMERA ACCESSORIES

Lonses: Superb quality 25 mm . $(1 \mathrm{in}) \mathrm{f} /$.1.8 . "C" mount lenses made especially for this system are available. also a limited quantity of motorised zoom lenses.
Remotely Controlled Weatherproof Pan and Titt Heads: Pan $340^{\circ}$ at $6^{\circ}$ per sec. Tilt $+50^{\circ}$ at $4^{\circ}$ per sec $230 / 250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$ operated.
Remotely Controlled Pan and Tit for Indoor Use Only : Details as above.
Weatherproof Camera Housing: Windscreen Wiper. 75 w . heater. internal circulation fan, mounting bracket for

## CONTROL MONITOR

14 In. screen, overall size $16 \times 14 \times 18 \mathrm{in}$. (excluding Remote Control Unit on which Monitor is shown), weight 30 lb . Panel controls provided: Mains on/off. Contrast. Brightness, Remote Focus. Preset controls (under side panels) include Frequency lock. Monitor height. Frame linearity. Camera height, Camera width, Auto sensitivity, Camera linearity, Cable colrection, Video Gain. Beam Current, Y shif, Electrostatic focusing for camera and monitor. Additional input: Video -100 mV peak white positive into 50 ohms: Synch. 2 v . peak/peak negative. Output: 100 mV peak white positive 2 v . peak/peak negative. Ambient temperature range $-30^{\circ} \mathrm{C}$. to $+55^{\circ} \mathrm{C}$.

## ACCESSORIES

Remote Control Switching Unit (shown under Control Monitor): Controls auxiliary functions at the camera, i.e pan/tit, zoom, windscreen wiper. etc. Size $18 \times 14 \times 3 \mathrm{in}$., welght 8 lb
Distribution Unit: Used for selecting the required picture from those available on the control monitors and distributing it to the appropriate viewing monitor. Size $19 \frac{1}{2} \times 13 \frac{1}{2} \times 8 \frac{1}{\mathrm{in}}$., weight 30 lb
Viewing Monitors: These are conventional domestic type receivers-19 in. and 23 in . models available
Owing to the complexity and limited quantity of unita available this equipment is available to CALLERS ONLY.

## LASKY'S BASIC SYSTEM PRICE



1-camera (complete with Vidicon) less lens, 1-Control Monitor, 25 yds, of cable. PRICES FOR LENSESANDACCESSORIES ON APPLICATION.


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$A C V=08 \cdot 30 \cdot 120-800-1.200 \mathrm{~V}$ al 10 NO
OC Current: $0-0.06-8.60-600 \mathrm{~mA}$
Rosittence: $0 \quad 10 \mathrm{~K} \cdot 100 \mathrm{~K} \cdot 1 \mathrm{M} \cdot 10 \mathrm{M} / \mathrm{hms} 158$



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ACV: 0-3-10-50-250-1,000V at $2.5 \mathrm{KOPN} 0.1 .5 \cdot 5 \cdot 25-125-500 \mathrm{~V}$ at 5 KOPW OC $\mu \mathrm{A}: 0.25 \mu \mathrm{~A}$ a $125 \mathrm{~mA}: 0.50 \mu \mathrm{~A}$ ot 250 mA

OCAmpa: :-5A al $125 \mathrm{mV}: 0-10 \mathrm{~A}$ at 250 mV .
Output Copactor $(0.1$ iff, 400 VW$)$ In series win ACV renges
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## NO EXCUSES! NO DELAYS! FROM STOCK! UABIIBBLE YOLTAGE TRANSFORWIERS <br>  <br>  <br> INSULATION TESTERS (NEW) <br> 500 VOLTS, 500 megohms Price £28 carriage paid. <br> 1,000 VOLTS, 1,000 megohms, <br> § 34 carriage paid. <br> 5Amp.AC/DC VARIABLE VOLTAGE OUTPUT UNIT $\begin{array}{ll}\text { Output } 0-260 \mathrm{v} . ~ A . C . ~ \\ \text { Output } & 0-240 \mathrm{v} \text {. D.C. }\end{array}$ Fitted large scale am- meter and voltmeter. Neon indicator, fully fused. Serong ateraccive metal case $15 \mathrm{in} . \times$ 8 tin. $\times 6$ in. Weighe 24 8łin. X6in. Weighs 24 lb. Infinitely variable, smoothstepless voltage, smoothstepless voltage variation over range. variasion over range. Similar in appearance so illustrasion below. manm <br>  <br>  <br> \{ 36 volt 30 amp . A.C. or D.C. Variable L.T. Supply Unit INPUT OUTPUT CONTINUOUSLY VARIABLE 0.36 . <br> Fully isolated. Fitted <br> metal case with voltmeter. Am- $\$$ <br> meter, Panel Indicator and chrome $\left\{\begin{array}{l}\text { handles. Input and Output fully } \\ \text { fused. Ideally suited for Lab, or }\end{array}\right.$ <br>  <br> CONSTANT VOLTAGE TRANSFORMER <br> SERVICE TRADING COMPANY <br> 

## SERVICE TRADING CO

LIGHT SENSITIVE SWITCHES Kit and parts Including ORP. 12 Cadmium Sulphide Phozocell. Relay Transistor and Clicuit. Now supplied with new Slemens High Spaed Relay for 6 or 12 voli operations. Price $25 /-$, plus $2 / 6 \mathrm{P}$. \& P.
ORP 12 and Circult $10 /=$ post pald.

220/240 A.C. MAINS MODEL Incorporates maini transformer rectifor and special circuit 47/6, plus 3/6 P. \& P. circuit 47/6, plus $\frac{3 / 6 \text { P. \& P. }}{\text { LIGHT }}$ SOURCE AND PHOTO CELL MOUNTING
Precialon englneered light source
with edjustable lens assembly and

E
里 0 ventilated lamp houslng to take ORP.I2 or slmilar cell with optic window. Both unirs are ainglo hole fixing. Price por pair e2/i5/0 plus $3 / 6$
P. A.P.


IN8ULATED TERMINAL8 Available In bieck, red, whit Y Y/low, per dor, P. \& P. $2 /=$,

SANGAMO WESTON
Dual range volemeter. $0-5$ and $0-100 \mathrm{~V}$. D.C. FSD I mA. In carrylng case with
sests prods and leads. $32 / 6$. P. \& P. $3 / 6$.

## RADIO ALTIMETER

This precision Instrument is
basod on a 24 v. D.C. LOW basod on a 24 v. D.C. LOW
INERTIA (integrating) Motor.
The Motor orives two

olerance gear-trains, including slipping clutch. Offered at fraction of manufacturer's price: $32 / 6$, plus $6 /-\mathrm{P}$. \& $P$. LATEST TYPE SELENIUM BRIDGE RECTIFIERS 30 vole $3 \mathrm{amp} ., 11 /-$, plus $2 / 6$ P. \& P
30 volt 5 amp., $16 /$, plus $2 / 6$ P. \& P.

AUTO TRANSFORMERS. Sep up, step down. $110-200-220-240 \mathrm{v}$. Fully shrouded. New. 300 watt P. \& P. 6/6. 1.000 watt type $65 / 15 / \mathrm{Feach}$, P. \& P. $7 / 6$. COPPER LAMINATE PRINTED CIRCUIT BOARD. Large sheet $15 \frac{1}{2} \times 5 \frac{1}{i n}$. 3 for $10 /=$ post paid.
( 3 minimum order).

| SEMI-AUTOMATIC "BUG" SUPER SPEED MORSE KEY <br> 7 adjustments, precision tooled. speed adjustable $10 \mathrm{w} . \mathrm{p} . \mathrm{m}$. to as high as desired. Waight $2 \ddagger 16$. $44 / 12 / 6$ post paid. |
| :---: |
|  |  |
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|  |  |

## NEW MODEL

## HIGM FREQUENCY

TRANSISTORISED MORSE OSCILLATOR
Adjustable tone control. Fitted with moving coll speaker also earpitece for personsl monitoring. Complate with
morse key. $45 /$ plus $3 / 6 \mathrm{~d}$. p. \& p .

## NICKEL CADMIUM BATTERY

## 1.2 v. 35 AH. size 81 high $\times 3 \times 1$. $30 \%$ each, plus $4 /$

 Pintered Cedmium Type 1.2 v . 7 AH . Size: hoight 3 i in., widet 2 in. $x$ Itin
## DRY REED SWITCHES

$2 \times$ lamp Dry Reads (makes concects) mounted in 870 ohm 9 -10v coil. Size $3 \mathrm{in} . x$ 3 fin. $x$ tin. New. Price $8 / 6$ par palr. Post Pald.
of the above mentloned unles ( 12 Reeds. 6 colls) firted in motal box. Size $4 \mathrm{in}, \times 3 \mathrm{in}$. $\times$ Itin. Mig. by Elliote Bros. New 45/- atch. Post Paid.
Telephone Dlals (New) 14'6d, Post Pald. 250 v. A.C. SOLENOID
havy duty type. Approx. 3lb. puil
12 v. D.C. SOLENOID
pprox. lib. pull. IO/G, P. \& P
50 v. D.C. SOLENOID


50 v. D.C. SOLENOID

## PRECISION INTERVAL TIMER

 From 0-30 seconds (repetitive). Jewelled witch. Ex. equipment; tested. $17 / /$, plus 216. CONDENSERS
New at a fractio
2.500 mid .100
10,000 mid. 35


## FROPOWER RHEOSTATS <br> (NEW) Coramic constructlon windEnamel, haavy duty brush assembly designed STOCK IN THE FOLLOWING II VALUES 100 WATT I ohm IOa., 5 ohm 4.7e., 10 ohm 3e $25 \mathrm{ohm} 20 ., 50 \mathrm{ohm}$ l.4e., 100 ohm le., 250 ohm $7 \mathrm{e}, 500 \mathrm{ohm} 45 \mathrm{e} ., 1,000 \mathrm{ohm} 28 \mathrm{cmA}$. $1,500 \mathrm{ohm}$ 230 mA ., $2,500 \mathrm{ohm}$.2e. Diameter 3 ith . Shaft length i/n. dis. $19 / \mathrm{In}_{1}$. 27/6, P. \& P. 1/6: 50 WATT $1 / 5 / 10 / 25 / 50 / 100 / 250 / 500 / 1,000 / 1,500 /$ 2,500 ohm. All at 21/-, P. \& P. P. 1/6. 25 WATT $10 / 25 / 50 / 100 / 250 / 500 / 1,000 / 1,500 / 2,500$ 25 WATT $10 / 25 / 50 / 100 / 250 / 5$ ohm, All at $14 / 6$, P. \& P. $1 / 6$. Bleck Silver Skirted knob callbrated In Nos, I-9. If in. dia. brass bush. Ideal for above Rheostats, J/6 aach.

## 

* THREE EASY TO BUILD KITS USING XENON WHITE
\% LIGHT FLASH TUBES. SOLID STATE TIMING * TRIGGERING CIRCUITS. PROVISION FOR EX. inseruments in the laboratory or workshop. It is
invaluable for the study of movemens and checking
of speeds. Many uses can be found in the psychiatric and photographic fields, also in the sintertainment EXPERIMENTERS "ECONOMY" KIT I to 36 Flash per sec. All electronic components NEW INDUSTRIAL KIT
 - HY-LYGHT STROBE
* This strobe has been designed for use in large - the light output at 30 f.p.s. and utilizes a silica
tube for longer life expectaney, printed circuiz for easy
assembly, also aspectal trigger coil and output capacitor.
Light 7-INCH POLLISHED REFLECTOR Ideally suited
7
for above Strobe Kits. Price $10 / 6$ \& $2 / 6 \mathrm{p}$. g . or * pose paid withkits. PARVALUXTYPE SD19230/250VOLT AC REVERSIBLE GEARED MOTORS 30 r.p.m. 40 Ib . Ins. Posit
drive spindle adiustable different angles. Mountie to 3 tantial cast aluminium ban sub equlpmene. Tessed and in irs class running order. A really fraction of maker's price. 6 gns



## BODINE TYPE N.C. 1

 GEARED MOTOR(Type I) 71 r.p.m. torque 10 lb . In. (Type 2) 28 r.p.m. torque 20 lb . in
 reverslble $1 / 80 \mathrm{th}$ h.p. 50 cycle. 28 mp The above ewo prectsion made U.S.A. motors are offered In 'as new' condition. Input voltage of motor $230 / 240 \mathrm{v}$ A.C. Inpue complate with eransformar for $230 / 240 v$ A.C. Input
former $\mathbf{E 2 . 2 . 6}$ plus $4 / 6 \mathrm{~d}$ P \& P $6 / 6 \mathrm{P}$. \& P. or less eransThese motors are id azl \&or P. urtains, display stands, vending ting aerials, drawing LARGE DIGIT 12 v.D.C. MAGNETIC COUNTER
4 in . drum, callbrated 1-9. Figures 1 i in . high $\frac{10}{} \mathrm{in}$. wide. Set of 1 m , Ib . Ic/o
contacts operated by drum cam. The units can be used in pairs and are ideally sulted for batch or lap recording or for the many purposes where
large easily read numerals are required,
VEEDER ROOT COUNTER 230 V. A.C. 50 cycle 5 figure counter 230 v. GEARED MOTOR (as illustrated)
6 R.P.M. or 10 R.P.M
230 v. A.C. non-reversible, approx


MINIATURE UNISELECTOR 3 banks of 11
homing bask. 40 ohm
plus $24-36$ v. D.C. operation. Carefully removed from equlpment and
UNISELECTOR SWITCHES NEW 4 BANK 25 WAY FULL WIPER 25 ohm eoil, $24 \times$. D.C. oporation. 6s.17.8, plus $2 / 6 \mathrm{P}$. \& $P$.
6 BANK 25 WAY FULL WIPER 25 . ohm coill, 24
66 . 10.0 , plut $2 / 6$ P. D.C.
a. 8-BANK 25-WAY FULL WIPER
24 r.D.C. oparation, $67 / 12 / 6$, plus 4/- P. \& P

## RELAYS

BULK PURCHASE ENABLES US TO OFFER THE FOLLOWING NEW SIEMENS PLESSEY, otc. MINIATURE PLUG IN RELAYS AT A HIGHLY COMPETITIVE PRICE

## WORKING

| $\mathrm{COIL}$ | WORKING D.C. VOLT | CONTACTS | PRICE |
| :---: | :---: | :---: | :---: |
| 170 | 9-12 | $4 \mathrm{clo} \mathrm{H.D}$. | 14/6 |
| 170 | $9-12$ | $3 \mathrm{c} / \mathrm{O}+1 \mathrm{H} . \mathrm{D}$. | 12/6 |
| 280 | 6-12 | $2 \mathrm{c} / \mathrm{o}$ incl. base | 14/6 |
| 280 | $9-18$ | $4 \mathrm{c} / \mathrm{o}$ incl. base | 15/6 |
| 700 | 12-24 | $2 \mathrm{c} / 0$ Incl. base | 12/6 |
| 700 | $16-24$ | $4 \mathrm{c} / \mathrm{o}$ incl. base | 15/6 |
| 700 | 16-24 | 4M 28 incl. base | 12/6 |
| 250 | 20-40 | 2 e/o H.D. incl. base | 12/6 |
| 2500 | 30-50 | $2 \mathrm{c} / 0 \mathrm{H.D}$. incl. base | $12 / 6$ |
| 9000 | 40-70 | $2 \mathrm{c} / 0 \mathrm{incl}$, base | 101. |
|  | H.D. $=$ Hea | vy Duty | T PAID |



## MINIATURE RELAYS

- 12 vole D.C. operation. 2 c/o 500 M.A. coneaces. size lin. $x t x \frac{1}{1}$ in. Price $11 / 6$ Post paid
$30-36 \mathrm{v}$. D.C. operation. $2 \mathrm{c} / 0500$ M.A. contacts.
3.200 ohm coil. Size only $i \times \frac{1}{1} \times 4$ in. 86 past paid.


## 230 VOLT AC RELAYS

## contacts, $17 / 6$ Post Paid.

LONDEX four c/o 3 amp
A.C. AMMETERS 0-1, 0.5, 0-10.0.15, 0-20 amp. F.R $2 \neq i n$. dia. Allat $21 /$ each. $2 \frac{1}{i n}$. Flush round all at $21 /-$ each. $P$, \& $P$, extra. M. $0-300$ v. A.C. Rect. M-Coil 2 tin.
$0-300$ v. A.C. Rect. M-Coil 3 $\frac{1 n}{}$. Type W23

## SANWA MULTI RANGE TESTERS <br> NEW MODEL UD-50 MULTI

 TESTER, 20,000 O.P.V. MIRRORSCALED WITH OVERLOAD PRO. SCALED WITH OVERLOAD PRO 0.5 v., 5 v. 250 v., 1,000 v. A.C. voles
 $0.5 \mathrm{~mA}, 5 \mathrm{~mA} ., 50 \mathrm{~mA} ., 250 \mathrm{~mA}$. Size: $5 \mathrm{t} \times 3 \mathrm{~m} \times 18 \mathrm{in}$ Complate with beterias $\mathbf{~} 7.5 .0$
end test prods.

## RING TRANSFORMER

## functional Versatlle Educationa

This multi-purpose Auso Tranaformer, with
lirge centre aperture, can be uste as Doubl wound currene Tranuformer. Auto Tranuformer
H.T. or L.T. Tranuformer. by Almply hand wind ins she required number of curnithrough the conte E. 8 . Uiing she RT, 100 V . A. Model she ouspur could be wound Price: RT.joova jil's eurni par volr, $6250+3 / 6 \mathrm{p}$. and p .
demonstration transformer (STENZYL TYPE) Two removable colls
tapped ate
0,110,
220 tapped
and $6,12,36$ volts respecs.
and tively. A composite apparatus designed for class demonstration. Electro Magnetic Induction, lumping ring,
induction lamp, relationship between fiold intensity and
 ampere rurns, Inducsion L.T. TRANSFORMERS All primaries $220-240$ voles
Type No. Taps

$$
\begin{aligned}
& \text { pe No. } 34 \text { Sec. Taps } \\
& 30,32,34.36 \mathrm{v} . \text { at } 5 \text { amps. } \\
& 30,40,50 \mathrm{v} \text {. at } 5 \text { amps. }
\end{aligned}
$$

$$
\begin{aligned}
& 30,40,50 \mathrm{v} \text { at } 5 \mathrm{amps} \\
& 10,17.18 \mathrm{v} \text { at } 10 \mathrm{amp} \\
& 6.12 \mathrm{v} \text {. at } 20 \mathrm{amps} \text {. }
\end{aligned}
$$

$$
\begin{aligned}
& 17,18,20 \mathrm{v} \text { at } 20 \mathrm{amps} . \\
& 6,12,20 \mathrm{at} 20 \mathrm{mps} .
\end{aligned}
$$

SHOWROOMS NOW OPEN
AMPLE PARKING


## TYPE I3A DOUBLE BEAM OSCILLOSCOPES BARGAIN



An excellent general purpooe D/B oselllloscope. T. B. 2 cp $750 \mathrm{Kc} / \mathrm{e}$. Bandwidth $5.5 \mathrm{Mc} /$ ating vollage 0/110;200/250 A.C. Supplied in excellen working condition. e22/10/Or complete with all screm e2fien. Curriake 30

## MARCONI CT44

 TF956 AF ABSORPTION WATTMETER £20. Carr. 20\%.SOLARTRON CD. 1016 OSCILLOSCOPE Double beam. D.C.To B Mc/s. Excellent condl

CLASS D. WAVEMETERS

CLASS D WAVEMETERS No. 2 operation. Complete with calibrotion charth Excellent condition $\mathbf{2 1 2 / 1 0 / 0 . \text { Carr. } 3 0 / \text { -. }}$
EDDYSTONE V.H.F. RECEIVERS 770R. $19.165 \mathrm{Mc} / \mathrm{s}$. E150
Both types in excellient condition

LELAND MODEL 27 BEAT $20 \mathrm{Kc} / \mathrm{s}$. Output 5 K or 500 ohms. $200 / 250$
 A.C. Ontere
Carriage $10 /$


ARF- 100 COMBINED AF-R SIGNAL GENERATOR
 20.200 .000 cpm . Bquare arye $20-30.000$ eps. O/
HIGH [MP

 On. Incorporates duad purpose meter to monitor
P output and $\%$ nood. on R.F. $220 / 240 \mathrm{~V} . \mathrm{A} . \mathrm{C}$. VOLTAGE STABILISER TRANS FORMERS. ${ }^{780-260 \mathrm{v} \text {. input. Output } 230 \mathrm{~s}}$ Avallable 150 w or 226 w . E12.10.0. Cerr. $5 /$ TE-20RF SIGNAL GENERATOR
 Accurate wide range
algnal generator cover
ing $120 \quad \mathrm{ke} / \mathrm{s}-260$
$\mathrm{Mc} / \mathrm{s}$. on 8 bandi. Directly Calbrated. eration 200/2
Brand new, tions. £15

## PEAK SOUND PRODUCTS

Full range of Amplutier, kits, speakers in ntock E22 SINE SQUARE WAVE AUDIO GENERATORS
 20 cpe to Square Output ime 5.000 ohms. 200 250 r. A.C. operation,
new and gularan-
teed with inatruc ${ }_{\text {tion manual }}^{\text {tead }, ~} \mathrm{El6.10.0}$. MARCONI
TF885 VIDEO OSCILLATORS $0.5 \mathrm{mc} / \mathrm{B}$ Bine Square Wave 845 , Carr. 201LAFAYETTE TE-46 RESISTANCE

 ohms. Also checks
impedance turns
ratho insulation ratio insulation
$200 / 250$ Brand New. $£ 17.10$

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## TY75 AUDIO GENERATOR

Bine Wave $20 \mathrm{CPg}-200 \mathrm{Kc} / \mathrm{s}$ Square Whave 20 CPB - 30 output. Output suriable up to
6
volts.
$220 / 240$
volta A.C. E16. Carr. 7/6. Bize $210 \times$ $150 \times 120 \mathrm{~mm}$.

MARCONI TF195M BEAT FREQUENCY OSCILLATORS TE-20D RF SIGNAL GENERATOR
 Accurate Elde range elg.
Hish generator covering
$120 \mathrm{Kc} / \mathrm{s}-\mathrm{B} 00 \mathrm{Mc} / \mathrm{B}$ on 6 bands. Directy can brated. Varisble RF.
sttepuator, XLeal socket for calltrian
tion. $220 / 240 \mathrm{~V}$. A.


ADVANCE TEST EQUIPMENT
 ments in ezcens of $100 \mathrm{Mc} / \mathrm{e}$ and D.C. measure-
mente np to 1000 v . with nccuracy of $\pm 2 \%$. D.C. VM.79, UHP MILIIVOLTMETER. Translutorived. 0.3 Ma. Reasistance 1 ohm -10 megohiuns. $£ 125$. HIB. AUDIO SIGNAL OENERATOR. $50 \mathrm{Kc} / \mathrm{s}$, dine or squnre ware. Price $£ 30$.
18 B . AUDIO SIGNAL GENERATOR.




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modela at 84.15 .0 . Camt, $5 /$.,


LAFAYETTE LA-224T TRANSISTOR STEREO AMPLIFIER


19 transistors, 8 diodes, IHP musle power 30 watt.
at 8 ohms. Res. $30-20,000 \pm 2 \mathrm{~dB}$ at 1 w . Distortlon $1 \%$ or less. Inputa 3 mV and 250 mV . Output
$3-16$ ohms. Beparate $\mathbf{L}$ and $\mathbf{R}$ volume controle. Treble and bans controls. stereo phone Jack.


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Brand new, guaranteed and carriage paid
High quality construction. Input 230 v 50 cycles.
Output full variable from $0-260$ volts. Bulk quantities available
1 amp . $-85 / 10 / \mathrm{F} ; 2.5 \mathrm{amp}$ - $-58 / 15 /-; 5 \mathrm{amp}$. $\mathrm{f} 9 / 15 /$
8 amp.- $14 / 10 /-10 \mathrm{amp}$.- $218 / 10 /$-; 12 amp .- $221 ; 20 \mathrm{amp}$ - 23


MULTIMETERS for EUERY purpose:


MODEL TE-90 50.000 Mirror geale overiosd grotec-
dion. $0 / 3 / 12 / 60 / 300 / 600 / 1,200$
. D.C. $0 / 8 / 30 / 120 / 300 / 1200.0$ V.D.C. $0 / 6 / 30120 / 300 / 1.200 . \overline{ }$ $6 \mathrm{~K} / 160 \mathrm{~K} / 1.6 / 16 \mathrm{MEO} 0$


MODEL TE-80. 20,000 O.P.V $0 / 10 / 80 / 100 / 500 / 1,000$ V. A.O
$0 / 5 / 25 / 50 / 230 / 500 / 1,0000$.
D.C. $0-50 \mu \mathrm{~A}$.
$5 / 50 / 500 \mathrm{~mA}$ D.C. $0-50 \mu \mathrm{~A} .5 / 50 / 500$
$06 \mathrm{KK} / 60 \mathrm{~K} / 600 \mathrm{~K} / 6 \mathrm{meg}$.
m

84/17/6.
TE-51, NEW $20,000 \Omega$
VOLT MULTMMETER, with overlowd protectlon, and
nolirro
scale, $0 / 6 / 60 / 120$, 1,200 v. A.C. $013 / 30 / 60 / 300 / 2$
$600 / 3.000 \mathrm{~F} . \mathrm{D} . \mathrm{C} .0 / 60 \mu \mathrm{~A} / 12$ /soom A.D.C. $0 / 80 \mathrm{~K} / 6$ mes
ohm. $8 \mathrm{~m} / \mathrm{B}$. P. \& P. $2 / 6$.
 MODEL 20 k Q/Volt $5 / 25 / 50 /$ $250 / 300 / 2,500$ v. D.C. ${ }^{5 / 25 / 50 / 10 / 50 /}$
$100 / 500 / 1,000$ v. A.C. $0 / 50 \mu \mathrm{~A} /$



MODEL TE-70, 30,000 O.P.V $0 / 3 / 15 / 80 / 360 / 600 / 1,200$
D. $. \mathrm{C}, 0 / 6 / 30 / 120 / 60 / 1,200$
A. $0 / 30 \mu \mathrm{~A} / 3 / 30 / 300 \mathrm{~mA}$
 MODEL TE-12, 20,000 O.P.V $3 / 0.6 / 0 / 30 / 120 / 600 / 1,200$
 $60 \mathrm{Meg.a} .50 \mathrm{KP} / \mathrm{PF}^{2} \mathrm{MPD}$

## 

 LAPAYETTE 87 Range SuperSOK
volvi. Mulkimeter.
D. volts $125 m \mathrm{~m}-1000 \mathrm{v}$. A.C.
volte $1.5 \mathrm{~F}-1000 \mathrm{D}$. D.C. Cur-
tent $25 \mathrm{AA}-10$ Amp. Ohms rent $25 \mu A-10$ Amp. Ohms
$0-10$ Meza. D.B. -20 to $+81 / 10 / \%, \mathbb{P}, \& \quad \mathbb{P}, 3 / 6$.

MODEL PT-34. 1,00 O.P.V.O/ $60 / 30 / 1,550 /$
$600 / 1.000 \mathrm{~V}$ a.c. end d.c. $01 / 1100 / 500 \mathrm{~mA}$.
d.c. $0 / 100 \mathbb{K} \mathrm{~B} 38 / 6$.
 d.c. $0 / 100 \mathrm{~K}$ \& $38 / 6$.
P. A P. $1 / 6$.


TRANSISTOR FM TUNER
 6
Higy
TRANBABTOR TUNER BIZE ${ }_{21}^{2 N L Y} 3$ In. $x \operatorname{in}$. $x$ 2Jin. 3 I.F. stangea
Double tuned dion Crimbleator. ande output to feed moat amplifier. Operaten
$88-108 \mathrm{Mc/n}$. Ready on 9 volt battery. Coverage $88-108$ Mc/n. Ready
bullir ready for ube. Fantastio value for money E6/7/6. P. \& P. $2 / 6$.
BTEREO MULTIPLEX ADAPTORS, $99 / 6$.

## SINCLAIR EQUIPMENT

 212. 12 watt amplidier 88/6. STEREO 25. Pre-amplifer £9/19/8. Q. $1+$ Bpeakere $£ 7 / 19 / 6$. NOW AVAILABLE ICIO. $59 / 6$ ALL POBT PAID. SPECLAL OFFER$2 \mathrm{Z12}$ amps. P24 Power Gupply Oleno 25 Preamplifer Q. 14 Bpesket 35 watt Integrated Ampliner SYSTEM ${ }_{\text {£ }}^{128}$ 35 wath integratod Amplifiter, $£ 28$.
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ECHO HS-606 STEREO
HEADPHONES

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Ebch headphone contalas Buitit in individual leval controls. $25-18.000$ e.p.e tereo plug. E5/18/6. $P$. $P$ 2/6.

| TRANSISTORISED |  |
| :---: | :---: |
| TWO-WAY |  |
| TELEPHONE |  |
| INTERCOM |  |
| Operative over mmazingly long |  |
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| cations. Beautifully finished |  |
| In ebony. supplied completewith batiertes and will brackets, |  |
|  |  |
| £6/19/6 pair. P. \& P. 3/6. |  |

TEIII DECADE RESISTANCE ATTENUATOR db. Co range 0-111 Uahulanectlons.
 $10)+(1 \mathrm{db} \times 10)$
$+10+20+30+$
40 db . Frequency: DC to $200 \mathrm{KHZ}(-\mathrm{sb})$.

 CAR LIGHT
Heary duty tight flauber employn a condenser dincharge principle operating on eloctro
 cal relay. (An tiset.)
Housed in strong plastio Housed in strong plastio
case. lashing
rate
 $\begin{array}{ll}\text { minute. } 12 & \text { volt D.C. } \\ \text { operation. } & \text { Maximum }\end{array}$ Iowd 6 ampa. Blze 2 Hith
dia. by tia. Supplited brand new at atraction
of oriminat cout. $6 / 6$ each RECORDING HEADS
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9 \& 10 CHAPEL ST., LONDON, N.W.I
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AMERICAN HIGHLY STABILISED
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Reguiation between 7.15 voles D.C. at 20 amps. Fitted 0-30 D.C. ammetor, 0-15 D.C. voltmater and overload pro-
tection switch. Built to very high specification. Bench or tection switch. Built to 2 very high specification. Bench or
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$240 / 110$ vole 400 watts, Mains. Transformer available if $240 / 110$ volk, 400
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## SPECIAL OFFER OF L.T. TRANSFORMERS

Pri $110-120 \mathrm{v} .200-240 \mathrm{v}$. See. rapped 12,$18 ; 24,30 \mathrm{v} .8 \mathrm{a}$.
Table top connectlons. Fully eropicalised. 75/.. Carr. $7 / 6$. Table top connections. Fully cropicalised. 75/.. Carr. 7/6 Pri tapped Illov. 220-250v. Sec. 55v. 24a., T4v. 10a., 60v. 2a Terminal connections. Size $9 \times 7 \frac{1}{2} \times 7$ ins. Weighe 651 bs 610.19.6. Carr. 15/-.

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The first edition of this textbook written by members of the BBC Engineering Division was very well received. Now sections, such as information on circuits based on transistors, have now been added to the original material which deals with the application to television of sinusoidal, rectangular, sawtooth and parabolic waves. Also, sections dealing with the generation of waves have been extensively re-written. Television engineers and engineering students should find this volume most helpful.
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MAINS INPUT: $220 / 250$ volts
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X101 10w. SOLID-STATE HI-FI AMP


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 $\begin{array}{llll}5 & \text { metts } & 0.35 k: & A t \\ \text { Ressponse: Minsus } \\ 3\end{array}$
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## 50 WATT AMPLIFIER

 with six electronically mixed inputs. Suitable for use with: weble gutars. gram, tuner, organ. etc. Separate bass and
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Complete stereo systems comprising BALFOUR 4 speed auto player with stereo head 2 DUO speaker systems size $12 \times 6 \frac{x}{}$. ${ }^{2}$. Plinth (less cover) and the DUETO stereo amplifier. All above items

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3 speed 2 track Tape Deck complete with nesads. Takes 7 in. spool. Incorporating 3 ${ }_{\text {E21 }}$ mutors. A.C. mains. 240 volis, listed at

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CA8005 RF Amplifler with $100 \mathrm{mc} / \mathrm{s}$ bandwidth. Max. dissipation 26 mW . For use us RF ampilfler, balanced mixer, product detector or self-osciliating míxer.
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WESTINGHOUSE EPOXY ENCAPSULATED WIRE ENDED MINIATURE RECTIPIERS
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K8iseA 5.6 V D814B ${ }_{\text {B. }}^{\text {B.8 }}$ 5 watta 8 stud mounted $25 \%$ toleranco ${ }_{22}^{27}$ D 816 A
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$\begin{array}{ll}27 \\ 33 V & \text { D8168 } \\ 3816 \mathrm{~V}\end{array}$
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All at $7 / 6$

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 iree air or $1 \cdot 1$ W on heat nink. Price, per palr, $8 /$ /Max. collector-base voltage - 2 VV . Max collector current 30 mmA .
Price, each

SILICON MATCHED DIODE PAIRS IN4981 Two dhodes in common TO92 epoxy case. Beparate anode lemis and joint cathode. Dhoder are statlenlly and slinat ion 200 mW . Salable for TV horizontal phave discrimisatora
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DIGITAL VOLT-OHMMETER BK 2-6


Flectro-mechanical instrument with sequential energization of electro-magnetic relays. Projection systern display. Automatic range and polarity
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> 0.01 to $1,000 \mathrm{~V}$. D.C. only. Accuracy: Input resistance: $\quad 1$ megohm minimum Resistance measurement rance: Resistance measurement range: 100 ohms to $1999 \mathrm{k} / \mathrm{hhms}$ Accuracy: Sampling: Hand-operated, local or $\begin{array}{ll}\text { Power supplles: } & \text { remote } \\ & 115 \mathrm{~V} . / 23\end{array}$

PRICE - £I28.0.0

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Gated bi-directonal Silicon Thyristors with integral erigger. The triac will control up to 1440 watts a sheet mand frequency. Supplication complete with dats dimmer circuits. $8^{\text {m/ }} / 8{ }^{2}$
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release of electronic valves, tubes, klystrons, etc.

## APPOINTMENTS VACANT

## We're young, successful, and expanding

The Dolby Audio Noise Reduction System has in only three years changed international studio practice, providing a new master recording standard. The system is briefly described in our advertisement on page 40 of this issue.
As well as designing and manufacturing professional equipment (of which $80 \%$ is exported), we research into consumer applications, and recently the first domestic tape machines using a simplified version of the system were released under license in the U.S.A. But this is only the beginning of a long line of new applications.
We are situated in south London in a modern four-storey building which includes laboratories, offices and production facilities. We are still small - just 60 people - but are expanding rapidly in all departments; the search is for people who have the capability of growing with us. Prospects are excellent and the rewards attractive. We have these immediate technical vacancies:

## ELECTRONICS ENGINEERS

## ELECTRONICS

ENGINEER
(PRODUCTION)

We are looking for several top-flight engineers under 30, with a university degree in physics or electrical engineering and at least two years' experience in electronic circuit design. The jobs involve not only research and development, but in addition the design of both professional and consumer products, based on Dolby noise reduction techniques. Where products are concerned, the designer will liaise with the production department during all stages of manufacture.
Candidates should be familiar with modern techniques - ICs and FETs, for example - and should be experienced in both linear and non-linear circuitry as applied in the frequency range dc to 20 MHz .
Salaries from $£ 1,800$ to $£ 2,500$. Write or phone with brief details to David Robinson, Chief Engineer.
The candidate will be a graduate engineer under 30 , with a university degree in physics or electrical engineering. He will be responsible to the Production Manager for electronic aspects of production. These will include the design and introduction of specialized test equipment and procedures, together with the provision of general technical advice to the electronic test department. He will liaise with the engineering department on technical matters and will have the opportunity of investigating and introducing new production techniques. He will have a minimum of two years' design experience and preferably experience also in giving technical support in a production department.
Salary from $£ 1,800$ to $£ 2,500$. Write or phone with brief details to Bob Tallon, Production Manager.
DESIGN DRAUGHTSMAN Flexibility is the keynote in our requirement for a design draughtsman under 30 for a position in the Design Department, which is responsible for all design aspects of the company.
His primary duties will be to interpret details from design schemes and prepare complete mechanical manufacturing drawings for the production of light electro-mechanical units. In due course, he will be expected to produce his own design schemes from initial sketches or proposals. He must have some understanding of electronic circuits and be capable of developing, from initial circuit information, the necessary tape masters and associated details for printed circuit production.
The candidate must also have an artistic inclination, for as a secondary activity he will assist in the layout and preparation of artworks for advertising, technical literature and exhibitions.
It is essential that his draughting and presentation should be of the highest standard.
Salary from $£ 1,500-£ 2,200$. Write or phone with brief details to Ron Free, Senior Designer.

## DOLBY LABORATORIES

346 Clapham Road, London, S.W. 9<br>Telephone: 01-720 1111


if they know something about radio transmitters, receivers, ancillaries or systems.
If you have been in the business anywhere from two to twenty years we've a place for you at our Communications Division, London, S.W. 18

For details of our red carpet treatment ring Ted Jackson, our top man in handbooks, at 01-874 7281 (he thinks he is ex-directory so try 01-399 1917 if it's more convenient out of office hours).

## REDIFON *

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## SERVICE ENGINEERS

Our Instruments Company is currently expanding its activities and range of products.

Senior and Intermediate vacancies exist at the Service Department situated in Reading Berks.

The Department is furnished with modern test and fault finding equipment and the work is varied and interesting. Equipments are modern analogue and digital devices incorporating the latest techniques in instrumentation.

Previous servicing experience is desirable but our main requirement calls for an enthusiastic sound approach to the servicing of our wide range of products.

Applications in writing please to.
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Racal Instruments Ltd.,
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Reading,
Berks.

## COHIDNATE engmincering

NCR requires additional ELECTRONIC, ELECTRO MECHANICAL ENGINEERS and TECHNICIANS to maintain medium to large scale digital computing systems in London and provincial towns.

Training courses will be arranged for successful applicants, 21 years of age and over, who have a good technical background to ONC/HNC level, City and Guilds or radio/radar experience in the Forces.

Starting salary will be in the range of $£ 900 / £ 1,250$ per annum, plus bonus. Shift allowances are payable. after training, where applicable. Opportunities also exist for Trainees, not less than 19 years of age, with a good standard of education, an aptitude towards and an interest in, mechanics, electronics and computers.

Excellent holiday. pension and sick pay arrangements. Please write for Application Form to Assistant Personnel Officer
NCR, 1,000 North Circular Road.
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quoting publication and month of issue.
Plan your future with


# Rank Precision Industries Limited 

## BROADCAST DIVISION

## RANK CINTEL

The Cintel section is rapidly expanding its Development and Research Departments of professional television studio equipment．To strengthen their teams the following engineers are required．

## senior electronic design engineer

To work on development work on T．V．studio equipment． Successful applicant should have experience in this field together with B．Sc．or Dip．Tech qualification．Salary up to £2．500．

## senior mechanical

## designer

To work on colour telecine machines and other allied broad－ casting equipment．The work which is varied involves the development of small mechanisms and electromechanical devices．Salary up to $£ 2,500$ ．

## intermediate engineers test engineers

Are also required to assist in the Cintel programmes．

## works staff

Bench Testers：To work on the professional T．V．studio equip－ ment．No special qualifications are required for these positions but some experience in the T．V．field is preferable．

## TELECOMMUNICATIONS

The Telecommunications section has been in the field of communication for many years and holds major contracts． Increased activity demands new teams for work on Military Communication Equipment．

## Its The Rank Organisation

Holders of The Queen＇s Award to Industry for 3 successive years．

## section leader－

## military communications

Will be required to build up a team for the following pro－ jects．New lightweight man portable equipment，H．F．and V．H．F．channel generator by frequency synthesis．Initially the work involves responsibility for design aspects of an H．F．equipment undergoing a quality assurance programme． Age immaterial．Salary up to $£ 2.500$ ．

## senior development engineers

To assist the section leader on the above projects．Success－ ful applicants should have experience in this field together with the ability to lead in an objective fashion．

## intermediate engineers test engineers

Are also required to assist in the Telecommunications programmes．

## works staff

Testers：To work in the Test and Inspection department on the Telecommunications programmes．Experience in this field is necessary for most positions．

These positions carry good salaries together with the ex－ cellent fringe benefits available to all Rank Organisation employees．Sick Pay entitlements and holiday entitlements have recently been increased．
Location initially at Welwyn Garden City，moving to the new factory at Ware，Herts，before June 1970.
Applications to：

## Personnel Manager， <br> Rank Precision Industries Ltd．， <br> Bessemer Road， <br> Welwyn Garden City，Herts． <br> Tel：Welwyn Garden City 23434



That's Burroughs. And choosy about the company we keep. Are YOU a top dog? With the right sort of pedigree? Degree in engineering, (Honours Graduate or Ph.D.) with inbred ability and the stamina to hold your top place in a highly competitive field? Then BURROUGHS is the place for you.

## DEVELOPMENT ENGINEERS

(Mechanical or Electronic)

to join one of the foremost companies in Britain's fastest growing industry. In addition to your degree you will have a minimum three to five years' experience in one or more branches of a light engineering industry and require to have the ambition and talent to go to the top in one of the world's greatest companies.
The positions on offer give an opportunity for top dogs to get in at the beginning of an engineering expansion programme in Burroughs, Cumbernauld and further develop personal engineering skills and promotion prospects.
Salary is no stumbling block-we know we have to pay top salaries for top dogs.
Our plant is located in the green belt between Stirling, Edinburgh and Glasgow. You can readily commute from a rural village or market town with facilities for golf, angling, yachting or ski-ing and still be within easy reach of excellent schools and universities.
Please write or telephone (reverse charges) to:-
Tom Bennett,
Engineering Division,
Burroughs Machines Ltd.,
Cumbernauld,
Scotland.
Tel. 22111 (ext. 29)


## DEMEN EMBNIEANTG <br> New opportunities in electronics

E.M.I. Limited offer worthwhile careers to experienced Design Engineers in the following categories :-

## MICROELECTRONIC DESIGN

Working in close liaison with Production Engineers with the responsibility for the design of new tooling methods. A good knowledge of Jig and Tool work is required.

## TELEVISION DESIGN

The work involves the design of custom-built T.V. Studio and Outside Broadcast Vehicle Equipment and would be of interest to persons familiar with Commercial Quantity Production Methods. JIG \& TOOL DESIGN
A vacancy has occured for an experienced Jig and Tool Designer to undertake Jig and Tool Design in all its aspects

## SPECIAL PURPOSE MACHINERY

## DESIGN

For interesting and varied work on the design of new special purpose Machinery and Tools.

There are also vacancies for Draughtsmen to carry out the design of printed circuit boards from diagrams and experience of packaging techniques would be an advantage

For all the above positions a minimum of O.N.C. or equivalent qualification is required. Starting salaries are attractive, being commensurate with qualifications and experience.

Working conditions are excellent and full social and welfare facilities including a contributory pension scheme with free life assurance are available.

Apply in writing stating area of Interest to.

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## RADIO ENGINEER

FOR

## UGANDA

We have a vacancy for a well trained radio engineer with a good knowledge of electrical and electronic problems.

The person we are looking for should be a good organiser, must have real interest in his work and must be willing to train local staff. There are unlimited opportunities as the successful applicant will receive on the spot training in our medical and $X$-ray dept. This will necessitate regular journeys to all parts of Uganda. Our terms of service are good, the climate is wonderful and the work unusual. We offer good local and overseas leave facilities.

Those interested should write to:
Twentsche Overseas Trading Co. (Uganda) Ltd.,
P.O. Box 7160,

KAMPALA,
Uganda,
giving details of previous experience, age and marital status.

# THE DEPARTMENT OF CIVIL AVIATION, ZAMBIA Require 

# Radio Engineers 

## Salary in scale up to $\mathbf{E 2 7 8 2 .}$ Tour of 36 months offered. Generous leave on full salary. $\mathbf{2 5 \%}$ End-of-Tour gratuity.

Commencing salary according to experience in scale Kwacha 2736 (£Stg.1596) rising to Kwacha 3216 ( $£$ Stg. 1876 ) a year, plus an Inducement Allowance of $£$ Stg. 568 - £Stg.615. A Direct Payment of $£ \operatorname{Stg} .268-£ \operatorname{Stg} 291$ is also payable direct to an officer's U.K. Bank account: Both gratuity and direct payment are normally TAX FREE. Free passages. Quarters at low rental. Children's education allowances. Generous leave on full salary or terminal payment in lieu. Pension scheme available under certain circumstances.
Candidates must be under 55 years of age and should possess
8 years relevant experience following :-
(i) an apprenticeship of 5 years, or
(ii) possession of a Service Trade Certificate, or
(iii) possession of an I.C.A.O. certificate or
(iv) equivalent.

In addition, candidates should have a sound experience of the theoretical principles of and experience in the maintenance of the first two and at least one other of the following groups of communications and navigational aid systems:

1. Medium powered H.F. Transmitters and associated Receivers:
Frequency Shift Keying; S.S.B. and D.S.B. Equipment; Medium Frequency Non-Directional Radio Beacons.
2. Low and High powered V.H.F., A.M. Equipment.
3. V.H.F. Omni range; Automatic VHF Direction Finders. Distance Measuring Equipment.
4. Instrument Landing System.
5. Radar X Bank Terminal and P.P.I Talk Down Equipment.
6. Audio and Remote Control Equipment; Public Address Equipment; Afrport Magnetic Tape Recorders; Inter Office Communication; Underground Control Cables; Impulse and D.C. Switching System.
7. Teleprinter Telegraphy (torn tape) and associated Page Printers; Tape Recorders (autoheads); Semi-Automatic Message Switching System.
Duties include the maintenance, overhaul and installation of ground terminal radio communication equipment and navigational aids at Airports and Flight Information Centre.
Possession of a valid driving licence will be an advantage.
Apply to CROWN AGENTS, 'M' Division, 4 Millbank, London, S.W.I, for application form and further particulars stating name, age, brief details of qualifications and experience and quoting reference number M2Z/690315/WF.
join the men who lead

# Device Technology Engineer 

A qualified man is urgently required to work as a senior member of a team at present engaged on the aspects of choice and design of solid state devices. These include microcircuits and hybrid circuits for use in high reliability equipment.
Applications are invited from Electronics Engineers or Physicists with a sound knowledge of microcircuit technology and design. At least three years' experience in the application of the above mentioned devices is essential.


Please write or phone for on application form, quoting Rof. 1462. to: Mr. E. Buckmaster,
1462 Personnel Department.
British Aircraft Corporation, Guided Weapons Division.
Stevenage, Herts. Tel: Stevenage 2422.

# RESEARCH and DEV ELOPMENT <br> <br> ELECTRONIC <br> <br> ELECTRONIC ENGINEERS 

 ENGINEERS}

...OUR WORK

Expanding exports and the increasing complexity of our products have intensified our development programmes for digital and analogue computers, linkage and special purpose computer peripherals. We wish to establish new teams of electronic engineers and if you are interested in joining us
... YOUR QUALIFICATIONS should include a degree, H.N.C. or equivalent. You should have relevant experience, coupled with enthusiasm and ability and

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with Redifon will be a good salary, stability of employment, a wide range of interesting work and an opportunity to expand your experience into new fields in ...

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We design and manufacture flight simulators and electronic teaching machines for world-wide markets. The laboratories are situated in a pleasant part of Sussex at Crawley, mid-way between London and the South Coast.

Application forms may be obtained from:
H. C. Hall, Personnel Manager, REDIFON LIMITED.
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Computicket are moving rapidly towards the full implementation of their entertainment seat booking system. This service. which operates in real-time. will ultimately involve hundreds of on-line C.R.T. terminals sited in a wide variety of public places.
vanety of public places. London area to perform a vital role in this exciting new service.
Applicants should have had experience in the maintenance of electromechanical and electronic equipment situated in the field and should be happy to find themselves part of a technically advanced but none-the-less consumer orientated team.
Condtions of employment are attractive and salary will be in the region of £ 1.500 p.a.

## Electrical Engineers

Rolls-Royce and Associates Limited is engaged in an extensive programme of design, development and procurement of nuclear propulsion plant. We have immediate vacancies for:-

## Electronic Engineers

to be responsible for the design, development and engineering of nuclear reactor control and instrumentation systems. Applicants should be of graduate status.

## Electrical Designers

to be responsible for the preparation of design schemes. Applicants should have H.N.C. in Electrical Engineering and have completed an engineering apprenticeship. A minimum of 2 years' drawing office experience is essential.
Salaries are commensurate with age, qualifications and experience. A generous proportion of relocation costs will be met by the Company with special assistance for house purchase where necessary.

Please apply in writing, or by telephone for an application form to The Personnel Manager,
Rolls-Royce and Associates Limited,
P.O. Box 31, Derby DE2 8BJ or telephone Derby 61461 extension 213.

# University of Reading department of psychology Electronic Engineer (A.E.O.) 

Applications are invited for the post of ASSISTANT EXPERIMENTAL OFFICER in the Departmert of Psychology. Applicants must have an H.N.C. in Electronics or equivalent qualifica. tion. The successful applicant will be expected to be familiar with the design and assembly of simple analogue and digital electronic equipment, such as Timers. Logic for automation of experiments, High Sensitivity Audio and D.C. Amplifiers for electroshysiological work. Experience in the use of semi-conductor devices and integrated circuits would be an asset. The applicant will be expected to supervise the servicing of existing equipment; there will be a good opportunity to gain experience in servicing a small computer. The initial appointment will be made at A.E.O. level. Salary $£ 872-£ 1,454$ per annum. The point of entry will depend on qualifications and age. Applications, quoting M.62, to Assistant Bursar (Personnel), University of Reading, Reading. Berks.

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HAVE THE FOLLOWING VACANCIES IN THEER ORGANISATION
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Young man incerested in Electronic Musical Young man incerested in Electronic Musical Instruments with a good general knowledge of Write, or Telephone 723-1008/9 Extn. 1 or 2.

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Young mian with a good general knowledge of HIGH FIDELITY EOUIPMENT required for our retail HiFFI SALES DEPT. Please contace MR. STEVEN:, Telephone 723-6963. 2585

# CHIEF TELEPHONE ENGINEER OVERSEAS 

International Aeradio Lid are a thriving world-wide organisation of some 3500 employees engaged in the fields of communications and with 18 overseas subsidiary and associate companies. Major expansion has created the requirement for a Chief Telephone Engineer for one of the group's associated Telephone companies in the Arabian Gulf area. He will supervise a team of expatriate engineers and be responsible for the engineering administration and short-term carrying functions. A good theoretical background is essential together with specialist practical knowledge in at least two of the following fields:
a) Electronic Common Control Exchanges.
b) Local junction and subscriber's distribution network.
c) Subscriber's apparatus including PABX's.
d) Telex systems.
e) Coaxial cable transmission systems.
f) VHF radio relay transmission systems.

The position offers unusually good career prospects to the right man. A substantial tax-free starting salary will be offered including in addition. free furnished accommodation, marriage, child and educational allowances, free leave passages and medical attention, and concessions on holiday air fares after a year's service.

Please apply stating briefly details of age and qualifications to:

## PYE TVT the leaders in closed circuit television

## Supervisory Test Engineers Studio Equipment-Audio

Two competent men are required for sections engaged on fault-finding and testing to specification of a wide range of professional audio equipment including mixing desks, power amplifiers and ancillary units for O.B. vehicles.
Good experience with solid state amplifiers and ability to carry out measurement are essential.
We offer attractive salaries and conditions of employment. Local housing may be made available.
Please apply with brief details of experience to:

Personnel Officer, PYE TVT LIMITED Coldhams Lane, Cambridge, Telephone Cambridge (0223) 45115

## QUFD

If you think:
a. You'd like to work for Quad,
b. You have the right qualifications,
c. It would be better to work in Huntingdon* than in the big city rat-race,
drop us a line. We urgently need technicians and engineers for both Audio and VHF, and would be pleased to discuss the prospects with you.
Write initially, giving full details of your training and experience to:

## Mr. J. H. Walker, The Acoustical Mfg. Co. Ltd., St. Peter's Road, Huntingdon.

* Look it up on the map: Quad helped to put it there!


## THE GENERAL POST OFFICE has VACANCIES for RADIO OPERATORS II at its COAST RADIO STATIONS

Applications are invited from men between 21 and 35 years of age who must hold either the Postmaster General's First or Second Class Certificate of Competence in Radiotelegraphy or an equivalent Certificate issued by a Commonwealth Administration or the leish Republic.
SALARIES HAVE BEEN INCREASED and the scale now begins at £807, for those entering at the age of 21 , pising to a maximum of $£ 1,188$. There will be a further increase on 1 st January, 1970.
The posts will be temporary in the first place but successful applicants will be eligible to enter the open competitive selection for permanent appointment.
Applicants should write to: The Inspector of Wireless Telegraphy, Union House, St. Martin's-le-Grand, London, E.C. 1 ortelephone 01-432 5628 for further information.

## Ex-Service TECHNICIANS

A number of ex members of H.M. Services have joined us recently as prototype engineers working successfully on complex electronic equipment. We have three more vacancies and would like to hear from those who have left H.M. Service or are about to leave.

Apply: Personnel Officer, Pye TVT Limited, Coldhams Lane, Cambridge.

Telephone Cambridge (0223) 45115
2557

## THE UNIVERSITY OF HULL <br> AUDIO-VISUAL CENTRE SOUND SUPERVISOR

The Audio-Visual Centre in the University is engaged in the production; to fully professional standards, of television programmes, films and sound recordings for educational purposes. Applications are invited for the post of Sound Supervisor. Preference will be given to candidatés with an H.N.C. or equivalent qualification together with experience in the operational and mainfenance aspects of professional sound broadcasting and recording equipmient. The duties will be to assist in both operations and maintenance of the equipment used in the Centre. Salary range: $£ 1,578-£ 2,006$.
Further particulars may be obtained from the Registrar to whom applications ( 3 copies) should be sent by 27th October, 1969.

2592

## CONTINUOUS

## Expansion

## Installation Engineers Technicians \& Testers

Ref. 25720
To test and commission Multiplex, Co-axial Line and Microwave Radio Systems.

Ideal candidates will be less than 45 years of age with practical experience on some of the above equipment. These challenging posts call for drive, initiative and common sense. It is necessary for applicants to be prepared to work anywhere in the U.K.

Applications should be addressed to The Personnel Officer. STC Chester Hall Lane. Basildon, Essex. wave and Line Division based at Basildon are growing fast. In order to keep pace with this consistent growth rate we require


## Test Technicians <br> Ref. 27221

The diversity of products manufactured at the Basildon Plant demands experienced resting staff for work on complex transmission systems
Candidates should hold an ONC in elec. trical engineering and be able to offer considerable practical experience in the field of testing and fault clearing all types of land-unit, pcm and microwave equipment.

University of Birmingham Department of Medicine ELECTRONICS TECHNICIAN
required for work concerning the development and maintenance of electronic and physical apparatus used in medical research. Qualifications: O.N.C. or equivalent. Experience in digital forms of data acquisition desirable but not essential.
Salary: £773-£1,077.
Apply: Assistant Secretary (Personnel), Personnel Office, University of Birmingham, P.O. Box 363, Edgbaston, Birmingham, 15, quoting reference: 417/T143.

2555

## TEST ENGINEERS AND INSPECTORS

Owing to rapid expansion due to large export orders on Marine Radar we have urgent vacancies for

## TEST ENGINEERS

with a good electronic background, and preferably with radar experience. EIECTRO MECHANICAL INSPECTORS MECHANICAL INSPECTOR
Please apply in writing to the Personnel Officer The Plessey Company Limited Martin Road, West Leigh, Havant Hampshire quoting ref. HAV/169/B

## CAREERS IN RECORDING

PHILIPS PHONOGRAPHIC INDUSTRIES in Baarn, Holland, offer excellent career possibilities to young men between 22 and 30 years of age to join the Classical Recording Department as trainees.
Candidates will be required to reside in Holland and should have a thorough knowledge of at least one European language, ideally German or French.

A good musical knowledge is essential and experience in the audio field would be an advantage.

Duties will include editing recorded tapes according to instructions in the score and responsibility for the installation and maintenance of recording equipment.

Please apply in writing, sending brief details of age, education and work experfence to:-
The Personnel Officer,
Philips Records Limited,
Stanhope House,
Stanhope Place,
LONDON, W.2.
Initial interviews will be held in London.

## PYE TVT the leaters in closed circuit television <br> Electronic Design Engineer Pulse and Logic Circuitry <br> A vacancy of exceptional interest for a young design engineer has arisen. He will join a team working on television studio equipment using digital techniques of an advanced nature. <br> Applicants will be of at least H.N.C. standard and have three years or more of design experience using transistor and integrated circuits <br> Age preferably 24/30. <br> Attractive conditions of employment and commencing salary will be offered. <br> Please apply with brief employment details to: <br> Personnel Officer, <br> PYE TVT LIMITED <br> Coldhams Lane, Cambridge. <br> Telephone: Cambridge (0223) 45115

## 

Due to expansion there are excellent opportunities for Test Engineers in our laboratories and production departments, testing Radio, Navigator and Survey equipment.
Applicants with first-class background of T.V. and Radio Servicing or Telecommunications, Electronic and Control Circuiting should apply giving details of experience. Conditions are excellent and salaries will be commensurate with ability and experience.

[^9]
## THE UNIVERSITY OF LEEDS

British National Cosmic Ray Experiment, Haverah Park, Near Leeds.

Required immediately an EXPERIMENTAL OFFICER to assist with the design and development of electronic apparatus. Minimum qualifications: degree or equivalent in physics or electronic engineering.

Salary in range $£ 995-£ 1,460$. Applications should be made in writing, giving details of qualifications and experience, to the Administrative Assistant, Physics Department, University of Leeds, Leeds, LS2 9JT.

## DUBLIN <br> BROADCAST ENGINEER

With experience of maintenance and development of TV and sound studio equipment.
Required for radio and TV production and training studios.
Applications with a resume of relevant experience should be sent to the Director, The Communications Centre, Booterstown Avenue, Co Dublin. Terms of contract negotiable.

## ELECTRONICS TECHNICIAN

to be responsible to Group Engineer for maintenance, calibration and installation of a wide range of electronic equipment used in medical and engineering fields of Hospital work. Qualifications to level of H.N.C. desirable with wide experience in maintenance and calibration of electronic equipment
Salary range £1030 to £1365 p.a. Starting salary may be above minimum. Post offers ideal opportunity for man to join vital and growing service with prospects for advancement.

Application forms from Group Engineer, Reading and District Hospital Management Committee 3 CRAVEN ROAD - READING • BERKS.

2584

## TECHNICAL ASSISTANT

Men under 30 with science or engineering degree or equivalent required to work in London office of large firm of patent agents, to deal with inventions covering a wide range of subjects and to be trained to join the surprisingly highly-pald ranks of Chartered Patent Agents.

Write Mr. R. L. Andrews, 28 Southampton Buildings, Chancery Lane, London, W.C.2, or telephone 4055611.

## URGENTLY REQUIRED

ALL TYPES OF RADIO TELEPHONE EQUPPMENT
ESPECIALLY PYE CAMBRIDGE AND VANGUARD MOBILES. ALSO BASE STATIONS ANY CONDITION, WORKING OR NOT. Top prices paid. WE ALSO REPAIR ALL TYPES OF RADIO TELEPHONE EOUIPMENT

## SOUTHERN RADIO \& T.V. SERVICE

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## GOVERNMENT OF UGANDA

## REQUIRES

# BROADCASTING ENGINEERS 

to serve on contract for one term of 21-27 months in the first instance. Salary according to experience in scale Uganda Shg.21120-27780 (CStg.1232-1620) a year, plus an Inducement Allowance, normally tax free, of £Stg.778-886 a year, paid direct into the officer's bank in U.K. Gratuity $25 \%$ of total emoluments drawn. Liberal paid leave. Accommodation provided at reasonable rental. Outfit and education allowances. Free passages. Contributory pension scheme available in certain circumstances.
Candidates must possess the City and Guilds Final Certificate in Telecommunications (with Radio) or an equivalent qualification and have wide practical ex-
perience of technical broadcasting equipment including transmitting and studio control equipment.
The officer will be required to undertake senior operational duties including the maintenance of broadcasting equipment in transmitting stations and studios; outside broadcasts and recordings in remote districts, and to give assistance with the training of junior engineering staff.

Apply to CROWN AGENTS, 'M' Division, 4 Millbank, London, S.W.I, for application form and further particulars stating name, age, brief details of qualifications and experience and quoting reference number M2K/690995/WF.

CLARKE \& SMITH MANUFACTURING CO. LTD. have vacancies for
Audio Electronics and Small Mechanism Design Engineers
to work on Language Laboratory Systems and Electronic Equipment for Education Projects. Good salaries and progressive positions. Applicants, who should have qualifications equivalent to H.N.C. standards, should apply to:

Mr. T. A. Julian,
Wallington
Wallington
Surrey,
Tel:01-
Tel: 01-669 4411

West Sussex County Education Committee BOGNOR REGIS COLLEGE of EDUCATION Upper Bognor Road • Bognor Regis - Sussex Applications are invited for the post of

## TECHNICIAN

for Closed Circuit Television
Person appointed will be expected to have sound practical knowledge of cameras, control and recording equipment used in Closed Circuit Television and be capable of carrying out day to day maintenance. Applications will be considered from those with relevant experience in the electronics field who desire to extend this to Television. Salary scale: $£ 930-£ 1,095$ per annum, according to experience. Additional remuneratlon payable in respect of certain specialist qualifications.
Application form and further details from the Administrative Officer at the College. 2590

## Radio Technicians INSTALLATION AND MAINTENANCE £1,100-£1,500 <br> YOUR WORK

Will be concerned with the maintenance and installation of equipment at sirfields. inland and marine mobite networks and on North Sea drilling rigs. You will be basec at Southall and London Airport and you may also be required to make brief trips

## OUR REQUIREMENT

You should have experience in one or more
HF Receivers and Transmitters up to 1 KW using SSB. ISB and FSK technicues:
Remote control systems operating over G.P.O. landlines:
Teleprimters and Telegraph machines and error correction equipment.

## OUR OFFER

Includes membership of an excellent contributory pension and life assurance scheme and concessions on holiday air fares can be obtained at nominal cost to most parts of the world. after a year's service. Salary will be negotiated and range from E1.100-£1.500.

## YOUR FUTURE

Excellent long-term career prospects are offered for both U.K. and Overseas employment.
IAL are a tast-expanding world-wide Company. engaged in the field of communications. aviation services and engineering
with over 3.000 emplovees bround the world.
Please write stating briefly age and experience to the

## Personnel Officer (R),

IAL
INTERNATIONAL AERADIO LIMITED
aeradio house - hayes road - southall - middlesex

## PYE TVT the leaders in closed circuit television

## Electronic Test Engineers

 TV Broadcast EquipmentDue to rapid expansion we have several additional vacancies for test engineers to work on a variety of units making up an advanced system of TV broadcast equipment.
Applicants will preferably have several years' experience of testing TV transmission broadcast equipment and be thoroughly familiar with the use of complex oscilloscopes for critical measurements of test parameters.
Attractive conditions of employment and commencing salary will be offered.
Please apply with brief employment details to:

Personnel Officer PYE TVT LIMITED
Coldhams Lane, Cambridge. Telephone Cambridge (O223) 45115

## reterererererererer Electrical Engineer

The Industrial Applications Department of the Electrical Research Association has a vacancy for an Electrical Engineer.
The successful applicant will be working with a group required to make investigations into the generation, propagation and measurement of high frequency transient disturbances in control and computer systems.
QUALIFICATIONS required are a degree, H.N.C. or equivalent in Electrical Engineering, with preferably industrial or research experience, in high frequency pulse techniques or electronic circuitry.
SALARY: this appointment will be in a grade with
 salary depending on qualifications and age which is likely to be between 22 and 28 years.
Please apply to
The Personnel Officer, Ref: 1A2,
Electrical Research Association,
Cleeve Road, Leatherhead, Surrey.

## THE UNIVERSITY OF HULL AUDIO-VISUAL CENTRE STUDIO ENGINEER

(Videotape and Telecine)
Applications are invited for the post of Studio Engineer (Videotape and Telecine) in the Television Studios of the University's Audio Visual Centre. Preference will be given to candidates with an H.N.C. or equivalent qualification, logether with experience in the maintenance and operational aspects of magnetic recording equipment (either one inch helical scan or two inch broadcast) and/or Telecine equipment. The duties will be to operate and maintain videotape recording and Telecine equipment used in the Centre and if necessary further training will be given.
Salary range: $£ 1,056 \cdot £ 1,311$.
Further particulars may be obtained from the Registrar to whom applications (3 copies) should be sent by 27th October, 1969.

2593

## UNIVERSITY OF BIRMINGYAM Department of Electron Physics Electronics Engineer

required to join the space research group in the Department of Electron Physics. The work is concerned with the design of electronic instrumentation for scientific rockets and satellites. The successful candidate will be expected to follow a project from initial design through environmental testing and space vehicle installation to pre-launch count down. This programme involves travel within the U.K. and to overseas launch sites. The post requires specialist experience in complex analogue solid state circuits and applicants should possess Grad. I.E.E.E., H.N.D., H.N.C. or equivalent qualificatlons. Those wishing to see something of the work before making a formal application are invited to telephone Professor J. Sayers, $021-472$ 1301. Ext. 1801.
Salary £1380- £2045.
Applications should be sent to the Assistant Applications should be sent to the Assistant
Secretary (Personnel), Personnel Office, University of Birmingham, P.O. Box 363, Birmingham 15, reference 105/TO/155. 2561

## RADIO AND INSTRUMENTATION ENGINEERS

Required for WEST AFRICAN PROJECTS
C.O.D.E.C.O.

62 STEPHYNS CHAMBERS - BANK COURT
MARLOWES • HEMEL HEMPSTEAD - HERTS
2403

## DEPUTY SUPERINTENDENT OF POLICE <br> (Signals Branch) <br> Government of Brunei

Candidates, must have City and Guilds Telecommunications Intermediate Certificate, with not less than five years' experience. Experience in a Police Force or Armed Forces is desirable.
The Officer is to assist the Force Signals Officer in installasion, mainsenance and servieing of V.H.F. and H.F. equipment, supervision of Signals Stores and Workshops and Scaff.
Salary range $22,125-22,518$ P.A. plus inducemens allowance (2441-2474) P.A. The Appointment is on contratt with gratuity for one tour of three years.
Candidates, who should be Nationals of the United Kingdom or Republic of Ireland, should apoly quoting RC216/28/02 giving full name; age, qualifications and experience to:

The Appointments Officer,
MINISTRY OF OVERSEAS DEVELOPMENT, Room E301, Eland House, Stag Place, London, S.W.I.

## THE COLLEGE OF AERONAUTICS

The following appointments are to be made in the High Frequency Section of the DEPARTMENT OF ELECTRICAL AND CONTROL ENGINEERING and are open to candidates who have experience in waveguide techniques.

## TECHNICAL OFFICER LABORATORY STEWARD

The vacancies are in the high frequency and radar laboratories which are concerned with postgraduate teaching and research in radar, radio and microwaves. Experience in the aviation field is not an essential requirement.

The TECHNICAL OFFICER will supervise the day-to-day activities in the laboratorles and be responsible for the construction of specialised experimental equipment. Candidates should have passed the graduateship examination of the I.E.E., I.E.R.E., or possess a H.N.C. or equivalent qualification. Salary in scale rising to $\mathbb{E 1 , 6 2 3}$ p.a.

The LABORATORY STEWARD, who should have relevant training and experience, will be appointed in a scale rising to $\{1,077$ with a supplementary allowance of $E S O$ p.a. for possession of a H.N.C. or equivalent qualification.
37 hour week of five days, generous holidays, staff superannuation and sick pay schemes.
Application form from Staff Records Officer. The College of Aeronautics, Cranfield, Bedford.

## SITUATIONS VACANT

A FULL-TIME technical experienced salesman reA quired for retall sales: write giving detalls of age, previous experience, salary required to-The Manager,

A SSISTANT MAINTENANCE ENGINEER required by A the CENTRAL OFFICE OF INFORMATION for their Radio Division. Candidates should have had wide experience in maintenance of professional tape recording and studio equipment Theoretical knowledge to City and Guild Intermediate level would be an advantaike,
as would experience in sound recording. Salary according as would experience in sound recording. Salary according
to expertence and quallinations on a range $\mathbb{E} 1.215$ to \& $1,560 \mathrm{pa}$. Five-day week of 41 hours (inclusive of meal breaks). 18 days pald annual leave. Please send postcard for application form to Manager (PEA/274/ EW). Wireless World, Department of Employment and Productivity, Professional and Executive Register,
Atlantic House, Farringdon Street, London, E.C.1. Atlantic House, Farringdon Sticet, Clorms, 30 , October, 1969.
[2602
A UDIO DEVELOPMENT ENGINEER. Electro-Musical A Industry. Watkins Electric Music Lid., 66 Oftey Road, London, 8.w.9. Tel. 01-735 6568. Please write in
[2574

CHESTER. Experienced TELEVISION ENGINEER With a liking for the occasional quality Hi Fi job TV Deld mechanic. 5-day 40 -hour week. Independent frm. Please write giving past experience to Mr. P. K. Caveen, PETERS (ELECTRICAL) LTD., 2 Charles
[2570

## NORTH STAFFORDSHIRE COLLEGE OF

Constituent College of the Proposed North Staflord hire Polytechnic. ENGINEERINO DEPARTMENT (Electrical and Electronic Division). Appllcations are nvited from candidates with a University Derree or an (a) SENIOR LECTURER IN ELECTRICAL ENGINEERINO: (b) LECTURER GRADE II IN ELECTRICAL ENGINEERING. The successiful candidate for post (a) will be responsible for subjects in the feld of coma muntcstions engineering, including Telecommunications Televiston and Radio. He will be required to undertake the organisation of short courses in Telecommunica-

## 

## ELECTRONIC TECHNICIANS

are required to work on calibration, fault-finding and testing of telecommunications measuring instruments. The work is varied and will enable technicians with experience of r.f. circuits to broaden their knowledge of the latest techniques employed in the electronics and telecommunications industries by bringing them into contact with a wide range of the most advanced measuring instruments embracing all frequencies up to u.h.f.
Entrants may be graded as Testers, Test Technicians or Senior Test Technicians according to experience and qualifications. Our expanding production programme geared to our recognised export achievement provides security of employment combined with good prospects of advancement, not only within these grades, but into other technical and supervisory posts within the Company.
Salaries are attractive and conditions excellent. A Pension Scheme includes substantial life assurance cover provided by the Company. Assistance with removal may also be given in appropriate cases. Please apply in writing, giving brief details including age, experience and salary to

The Recruitment Manager,
Marconi Instruments Ltd.
 Longacres, St. Albans, Herts.


Member of GEC-Marconi Electronics Limited
2530

For some of our distributors in AFRICA we require

## SERVICE MANAGERS

They will be responsible for the organisation, administration and promotion of our distributors' Service Departments, including spare parts management.

A good practical and theoretical technical background in radio and television is necessary and experience of service and spare parts administration is important. Further requirements are a background in Service Workshop management and training of repairmen.
Products to be serviced include television, radio and household appliances. Salary commensurate with qualifications and experience.

Applicants should submit full background details.
Apply to Box No. W.W. 2558.

## MICROWAVE ENGINEERS

## OVERSEAS

## THE POSTS

Excellent career opportunities exist for Microwave Engineers to join the International Aeradio worldwide organisation for overseas employment.

## OUR REQUIREMENTS

The men selected will be responsible for the maintenance of a solid set wideband multihop microwave system. Applicants should have experience in the following: $\star$ Overall system appreciation.

* Alignment and testing procedures of solid state microwave systems and the associated supervisory and terminal carrier channelling equipment.
* Preventive maintenance procedures and rapid and accurate fault diagnosis on the above types of system.


## YOUR FUTURE

IAL offers first-class career prospects. The company is fast expanding with over 3,000 employees engaged in the fields of telecommunications at more than 50 bases around the world. The present turnover is in the region of $£ 8$ million per annum and is expected to exceed the $£ 19$ million mark within 10 years.

## OUR OFFER

Includes a substantial tax-free salary: marriage, children's and educational allowances, free furnished accommodation, medical attention and leave passage

To apply for one of these positions please write giving brief details of age, qualifications and career to date to:

General Manager Personnel,
IAL
INTERNATIONAL AERADIO LIMITED

aemadio mouse hayes road southall midolesex

will be expected to encourage research in these fields tive duties. The successful candidate for post (b) will be required to teach Radio and Television Servicing subjects, and should have some experience in Colour TV work. In additton. he will be expected to assist with the normal range of Telecommunicattons and Electronic Subjects covered by the Department. Salary Scale: £2.417. Further detalls and appllcation forms obtalned from the Registrar. North Staffordshire College of Technology, College Road, Stoke-on-Trent. College
[2577 ELECTRONIC PROTOTYPE WIREMAN, wide techEnlcal knowledge, seeks position overseas; permanent or contract.-Reply Rex. W. Harris. 36 Cilfton Road,
London, N.8. R ADIO ENGINEER for installation/service Yacht RR.T., Automatic Plots, some Radar. Clean driving licence essential. Must Hue in or near London. Knowledge and liking of boating an advantage. Telesonic REDIFON LTD, require fully experienced TELER COMMUNICATIONS TEST ENGINEERS and ELECTRONICS INSPECTORS. Good commencing salaries. We would particularly welcome enquirtes the Services. Please write giving full detalls to The Personnel Manager, Redifon Ltd., Broomhtil Road,
Wandsworth, S.W.18.
[26
SERVICE ENGINEER. We spectalise in the repair Recorders and sime of 16 mm Sound Prolectors. Tape another engineer with some knowledge of Audio Ampliffers. Must be able to drive, Write: Burgess Lane $\&$ Co. Ltd. Thornton Works, Thornton Avenue, Chis-
wick. London, W.4.
TAPE RECORDER ENGINEER required for workshop London. Write to paxicting machines in Central London. Write to PAXDICTATOR (SOUTHERN) LTD.
THE UNIVERSITY OF LEEDS: Department of Physics. Electronlcs Techalelan required for post in electromics workshop involving maintenance and bullding
of a wide range of prototype apparatus. O.N.C. or equivalent. Salary on scale $£ 773$ - $£ 1,077$ Piease apply in writing, glving detalls of quallfications and experience, to the Administrative Assistant, Physics Department, The Unlversity, Leeds, LS2 9JT. [2564
WE HAVE VACANCIES for Four Experienced Test Applicants Finding and Testing of Mo have Experience of Fault Equipment. Excellent Opportunities tor promotion due Manager Works, Pye Teiecommunications Ltd., Cambrids Extn. 327. 15 MeV LINEAR ACCELERATOR. Assistant to help mechanical knowledge; accelerator experience not essential. Salary up to $£ 1,200$. Applications to SecreCambridge. Tennis Coart Road, Cambridge.
[2575

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BRAND NEW ELECTROLYTICS, $15 / 16$ volt $0.5,1,2$, B 5, 6, 8, 10, 15, 20, 30, 40, 50, 100, 200 mfds ., 8d. Mullard 25 voit $6.4,12 \cdot 5,25,50,80$ mids., 10 d ., $1 \cdot 6$. 160 mids., $1 /=$ Minimum order $7 / 6$., postaze $1 /=$ per order.-The C.R. Supply Co., 127 Chesterfeld Road,
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[2587
$B^{\text {UILD }}$ IT in a DEWBOX quality plastics cabinet $12 \mathrm{in} . \times 21 \mathrm{in}$. $\times$ any length. D.E.W. Lrd. (W), Ringwood Rd. FERNDOWN, Dorset. S.A.E. for leaflet.
Write now-Right now.
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INTEGRATED CIRCUITS at lowest price. GE Type PA 234, Watt Audlo Amplifier $17 / 6$ each tnc. data. 25 Volt, 200 mW , hie 100 min . Epoxy for economy Passivated for reliabllity, $1 / 9$ each. C.W.O. P. \& P. 1/per order, JEF ELECTRONICS, 12 York Drive, Grappen[2565 5 Ring 01-723 4143, weekday evenings. $T$ ELESCOPIC AERIAL MAST, ex Covernment, al Buyer collects. ROPER, 84 Goldthorn Hill, Wolver hampton
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D 396
UHF KITS and T.V. SERVICE SPARES. Suitable for Colour: Leading British Makers dual $405 / 625$ six position push button transistorised tuners
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\&s. 405/525 transistorised sound \& vislon IF panels ${\underset{\text { curpose }}{ } 2 \text { 15s. } 0 \mathrm{~d} \text {. Incl. Circults and data, P/P 4/6. Basic dual }}_{405 / 625}$
 UHF tuners, PLESSEY incl. valves $55 / \%$. P/P $4 / 6$. EKCO/FERRANTI 4 position push button type. incl. valves, leads, knods £ 510 s . Od.. $P / P$ 4/6. SOBELL/ GEC UHF tuner kit incl. Valves, right angle slow motion drive assy, leads. fittings, knobs, instructions
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$P / P$ 4/6. LOPTs, Scan colls, Frame output trans:formers, Mains droppers etc., avallable for most popu-

# Commercial Product Engineer for Gas Discharge Tubes 

This vacancy should prove attractive to a professionally qualified engineer with industrial experience, preferably in development and production or the design of electronic equipment. who now wishes to embark on a commercial career.
He would be responsible to the Commercial Product Manager for the Technical/Commercial product policy for a wide range of hot and cold cathode gas discharge tubes and similar devices, such as Numerical Indicators, Counters, Thyratrons and Reed Inserts. He should be prepared to travel frequently, both within the U.K. and overseas. Expected to negotiate on technical and commercial matters, he must be able to work together with Market, Production, Development and Research Personnel at all levels. This job is located at Mitcham, Surrey Please write to the Personnel Manager, Mullard Linited, Mullard House, Torrington Place, London, W.C.1., quoting reference RBT/ 1019
$\xrightarrow{\text { Mullard }}$

## UNIVERSITY OF CAMBRIDGE

 CAVENDISH LABORATORY
## ELECTRONICS ENGINEER

To collaborate with physicists in design construction and implementation of electronic circuitry incorporated in experimental apparatus in the Surface Physics research group of the laboratory.

Experience in solid state circuitry essential

Degree or equivalent in electronic engineering or physics desirable.

Salary in range up to $£ 1,400$ p.a. depending on experience, qualifications and age.

Applications to:
The Secretary,
Cavendish Laboratory, Free School Lane, Cambridge.

## OXLEY ${ }^{\circ} \Phi$ <br> Applications are invited for the position of <br> Assistant to the Works Director <br> of Oxley Developments Company Ltd., Ulverston.

Applicants must be about 30 years of age and have Higher National Certificate or a degree in Science. Preference will be given to someone with all or part of the following experience or qualifications:-
(1) Knowledge of modern manufacturing methods in electronics, small mechanical components and mechanisms
(2) Assistant or deputy to a Works Manager in a thriving concern.
(3) Experience in dealing with people, production control, and shop floor conditions; experience in cost accounting.
Oxley Developments is a vigorous and expanding Company offering scope and opportunity for the right man. The Works are located in open countryside at the southern end of the Lake District.
Applications giving details of education, qualifications, experience and salary and including copies of two references or names and addresses of referees to be addressed to:

The Personnel Manager,
Oxley Developments Company Ltd. PRIORY PARK • ULVERSTON • NORTH LANCASHIRE

## NCR SYSTEMS TESTERS

To bring-up, fault find and prove functions of electronic systems used in complex business machines by logical diagnosis. Candidates should possess an O.N.C. (Electrical) or R.T.E.B. Certificate, or City and Guilds Certificate (Subjects 47, 48 or 49) and have experience in one of the following areas:-

Computers, Radar, Tele-communications, Radio and T.V., etc.
These are Staff appointments carrying attractive salaries which are fully commensurate with qualifications and experience. Other employment conditions include 3 weeks' Annual Holiday, Pension Plan, etc. Effective assistance with housing will be provided.

```
NAME............................................. AGE...............
ADDRESS
QUALIFICATIONS
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For Application Form return coupon to :-
The Personnel Department,
THE NATIONAL CASH REGISTER CO.
(Manufacturing) LTD.,
Kingsway West,
DUNDEE DD1 9 QY

# ? <br> CIVILSERVICE 

RADIO AND ELECTRONIC ENGINEERS<br>Board of Trade (Civil Aviation)

Qualified engineers required as Assistant Signals Officers in the field of Civil Aviation for the provision and installation of advanced electronic equipment-including the latest type of radar, telecommunications, navigational aids, etc.
Qualifications: Degree with 1 st or 2nd class honours in Electrical Engineering or Physics, or have passed all examinations for M.I.E.E., A.M.I.E.R.E. or A.F.R.Ae.S.
Age: 23 and normally under 35 on 31st December, 1969 (extension for H.M. Forces or Overseas Civil Service).
 Pensionable appointments. Good prospects of promotion.
Application Forms are obtainable by writing to the Civil Service Commission, Savile Row, London, W1X 2AA, or by telephoning 01-734 6010, ext. 229 (after 5.30 p.m. 01-734 6464 "Ansafone" service). Please quote S/85/ASO.

## CLOSED CIRCUIT TELEVISION ENGINEER MARCONI MARINE

MARCONI MARINE is a major supplier of shipborne television installations and equipment and an engineer is required in the Company's Television Section at Chelmsford for the system planning of closed circuit and entertainment television systems.
Applications are invited from Engineers with practical experience of closed circuit television systems and in particular it would be desirable that this experience has been obtained with a major equipment manufacturer.
Additionally, experience in the development of television broadcast equipment would be advantageous coupled with experience in system costing.
Qualifications of H.N.C. level are necessary but the prime requirement is to produce practical results at the right price.

Applications, in strictest confidence, to:
Personnel and Operating Manager,
The Marconi International Marine Co. Ltd.,
Elettra House, Westway,
Chelmsiord, Essex

## AIR FORCE DEPARTMENT RADIO TECHNICLANS

Starting pay according to age, up to $£ 1,189$ p.ą. (at age 25 ) rising to $£(, 500$ p.a. with prospects of promotion.

> Vacancies at RAF Sealand, Near Chester
> RAF Henlow, Bedfordshire
> and RAF Carlisle, Cumberland

Interesting and vital work on RAF radar and radio equipment.
Minimum qualification, 3 years' training and practical experience in radio engineering.
5-day week-good holidays-help with further studies-opportunities for pensionable employment.
Write for further details to:
Ministry of Defence, CE3h (Air),
Sentinel House,
Southampton Row,
London, W.C.I.
Applicants must be UK residents.

Lar makes. TV signal boosters transistorised PYE/ Labgear B1/B3, or UHP battery operated 75/-. UHF
mains operated 97/6. UHF masthead $85 /-$ pasi free. mains operated 97/6, UHF masthead 85/-, past free. SUPPLIES, 64 GOLDERS MANOR DRIVE, LONDON, N.W.11. CALLERS 589B, HIGH ROAD. N, FINCHLEY, N. 12 (near GRANVILLE RD.). Tel. 01-448 9118 . [60


#### Abstract

QUALIFIED experienced Design Engineer aeek Q Financial Support to develop small company manufacturing high reliablity control equipment. Possible for assembly/servicing ease; continuous research and expansion. Box No. W.W. 2569 Wireless world.


## TEST EQUIPMENT ESURPLUS ANO SECONDMAND

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[^3]:    'Linsley Hood, J. L., "Modular Pre-amplifier Design", Wireless World, July 1969.

[^4]:    * assistant editor, Wireless World.

[^5]:    * West Ham College of Technology, London, E. 15.

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