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VOLUME 54 NUMBER 8 ISSUE 862

BRITAINS LEADING JOURNAL FOR THE RADIO & ELECTRONIC CONSTRUCTOR

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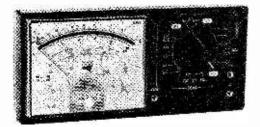
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SPECIFICATIONS:

OUTPUT POWER 15W R.M.S. Into 8Ω: DISTORTION 0·1% at 1·5W. INPUT SENSITIVITY 500mV. FREQUENCY RESPONSE 10Hz-16kHz-3dB. SUPPLY VOLTAGE ± 18V.

Price £6·27 + 78p VAT P&P free.



25 Watts into 8Ω

The HY50 leads I.L.P.'s total integration approach to power amplifier design. The amplifier features an integral heatsink together with the simplicity of no external components. During the past three years the amplifier has been refined to the extent that it must be one of the most reliable and robust High Fidelity modules in the World.

FEATURES: Low Distortion—Integral Heatsink—Only five connections—7 amp output transistors—No external components

APPLICATIONS: Medium Power Hi-Fi systems—Low power disco—Guitar amplifier

SPECIFICATIONS: INPUT SENSITIVITY 500mV OUTPUT POWER 25W RMS into 8 Ω LOAD IMPEDANCE 4-16 Ω DISTORTION 0-04% at 25W

at 1kHz SIGNAL/NOISE RATIO 75dB FREQUENCY RESPONSE 10Hz-45kHz—3dB. SUPPLY VOLTAGE ± 25V SIZE 105 50 25mm Price £8 18 + £1 ·02 VAT P&P free

HY120

60 Watts into 8Ω

The HY120 is the baby of I.L.P.'s new high power range. Designed to meet the most exacting requirements including load line and thermal protection this amplifier sets a new standard in

modular design.

FEATURES: Very low distortion—Integral heatsink—Load line protection—Thermal protection—Five connections—No external components

APPLICATIONS: Hi-Fi—High quality disco—Public address—Monitor amplifler—Guitar and

organ SPECIFICATIONS INPUT SENSITIVITY 500mV. OUTPUT POWER 60W RMS into 8Ω LOAD IMPEDANCE 4-16Ω DISTORTION 0·04% at 60W at 1kHz SIGNAL/NOISE RATIO 90dB FREQUENCY RESPONSE 10Hz-45kHz – 3dB SUPPLY VOLTAGE

HY200

120 Watts into 8Ω

The HY200 now improved to give an output of 120 Watts has been designed to stand the most rugged conditions such as disco or group while still retaining true Hi-Fi performance.

FEATURES: Thermal shutdown—Very low distortion—Load line protection—Integral heatsink—No external components

APPLICATIONS: Hi-Fi—Disco—Monitor—Power slave—Industrial—Public Address

SPECIFICATIONS
INPUT SENSITIVITY 500mV
OUTPUT POWER 120W RMS Into 8 Ω LOAD IMPEDANCE 4-16 Ω DISTORTION 0-05 % at 100W at 1kHz. SIGNAL/NOISE RATIO 96dB FREQUENCY RESPONSE 10Hz-45kHz – 3dB SUPPLY VOLTAGE

±45V SIZE 114 50 85mm Price £27·99 + £2·24 VAT P&P free.

HY400

240 Watts into 4Ω

The HY400 is I.L.P.'s "Big Daddy" of the range producing 240W into 40! It has been designed for high power disco address applications. If the amplifier is to be used at continuous high power levels a cooling fan is recommended. The amplifier includes all the qualities of the rest of the family to lead the market as a true high power hi-fidelity power module. FEATURES: Thermal shutdown-Very low distortion-Load line protection-No external

APPLICATIONS: Public address—Disco—Power slave—Industrial

SPECIFICATIONS OUTPUT POWER 240W RMS into 4 Ω LOAD IMPEDANCE 4-16 Ω DISTORTION 0·1% at 240W at 1 kHz SIGNAL NOISE RATIO 94dB FREQUENCY RESPONSE 10Hz-45kHz – 3dB SUPPLY VOLTAGE

±45V INPUT SENSITIVITY 500mV SIZE 114 100 85mm Price £38-61 + £3-09 VAT P&P free.

POWER SUPPLIES PSU36 suitable for two HY30's £6.44 plus \$1 p VAT. P/P free. PSU56 suitable for two HY50's £8.18 plus £1.02 VAT. P/P free. PSU50 suitable for two HY50's £8.18 plus £1.17 VAT. P/P free. PSU50 suitable for one HY20's £14.58 plus £1.21 VAT. P/P free. PSU50 suitable for one HY20's £15.19 plus £1.21 VAT. P/P free. PSU180 £25.42 + £2.03 VAT. B1 £0.48 + £0.06 VAT.

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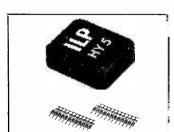
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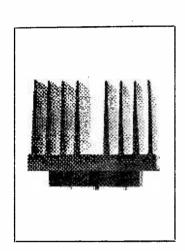
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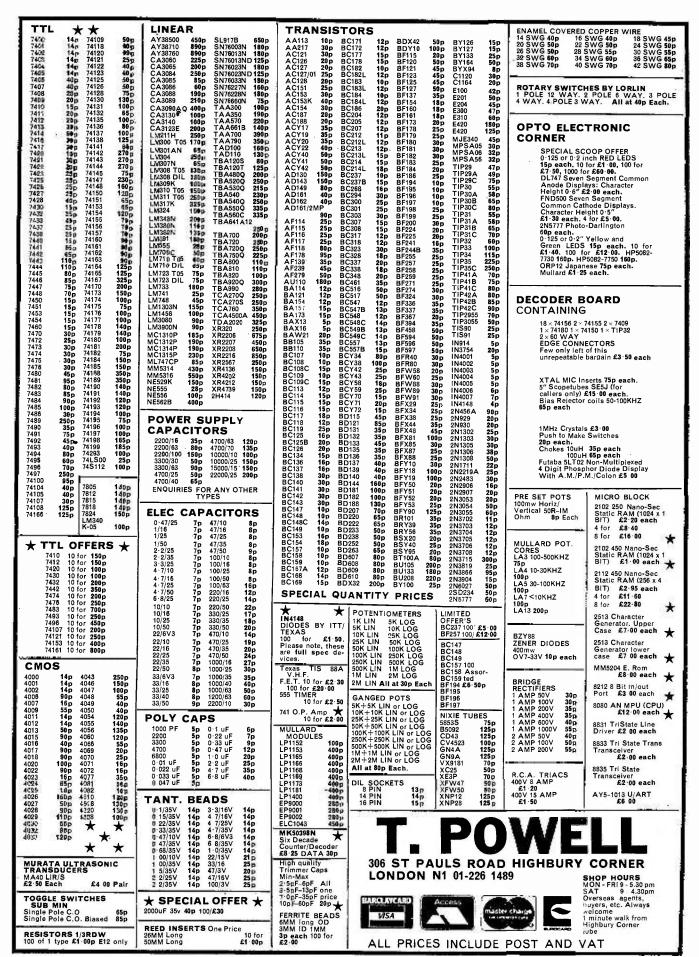
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7400		7491 7491 A		74186		4051	1100	12p BC109B 12p	BC559C	ME0491	,	TIS93 ZTX108	120*	2N4239	135p*	MC1458 50p*	7805 5v+ 95p	Š SAVERS Š
	N 15p	7492	58p	74190	120p	4054	120p	BC109C 12p	∣ 18p¹	18	3p	ZTX502	18p*	2N4292	19p*	MC1103 95n*	7812 12+ 95p	741 Op/Amps 5 for £1 ♣
7402	16p	7493		74191	120p	4055	140p	BC147 9p	BCY58 22p	MJE340		2N696	35p	2N5172	18p*	MC7242 120p*	781515+ 95p	
7403 7404	16p	7494 7495		74192 74193	99p 99p	4056 4060	130 p	BC148 9p* BC149 10p*		65p MPS2369) *	2N918	39p 20p	2N5245 2N5296	35p* 52p*	MFC4000B 128p*	7818 18+ 95p	★ 555 Timer 4 for £1 ⊀
7404		7495		74194	160p	4060			BCY70 18p BCY71 22p	200	,	2N930 2N1131	20p 25p	2N5457	35p*	MHQ3476	7824 24+ 95 p	文 TIL209 LED 10 for £1 文
7406	40p	7497	290p	74195	110p	4067	430p	BC158 10p	BCY72 22p	MPSA06		2N1132	29 p	2N5458	38p*	90p*	7905 5v — 95p	X BAX13 Diode 20 for £1 📉
7407		74100	140p	74196	100p	4068	25p	BC159 11p*	BCY78 20p	30p)*	2N1613	21 p	2N5459	19p*	MPQ372585p*	7912 12— 95p	6v2 Zener 400 mW 20 for £1
7408		74104		74197 74198	130p 250p	4069	27p	BC169C	BD121 95p	MPSA12 45p	.*	2N1711	27p	2N5460 2N62027		NE555 30p NE556 65p	7915 15- 95p	
7409 7410	18p	74105 74107	75p	74199	250p	4070 4071	65p	14p* BC172 12p*	BD131 50p	MPSA56	,	2N1893	36p 34p	2N6545		NE560 320p	7918 18— 95p	XXXXXXXXXXXXXX
7411	26p	74109	60p	74221	175p	4072	30 p	BC177 17p*	BD135 38p BD136 37p	32n)*	2N2218 2N2218A	28 p	3N128	113p*	NE561 395p	7924 24 — 95p	Dil Electrolytic
7412	25p	74110	60p	74H00	45p	4073	30p	BC178 17p*	BD137 36p	R2008B	_	2N2219	31 p	3N201	69p*	NE561B 430p		Sockets Capacitors
7412A		74111	75p	74H05 74H10	45p	4076		BC179 18p*	BD139 36p	200 p R2010B)*	2N2219A	32p	3N204 40361	75p* 48p	NE562B 420p NE565 125p	Bridge	8nin 44n 40v
7413	40p	74116 74118				4081		BC182 10p*	BD140 36p	200p	.*	2N2221	23p	40360	45p	NE566 155p	Rectifiers	144 40_ 0.8ur, 15ur, 33ur.
7414 7416	60p 40p		225p			4082	25p	BC183 10p* BC184 11p*	BD234 70p	TIP29 3	8p	2N2221 A 2N2222	24p	40362	48p	NE567 170p SFC2741 25p	50v 1A 20p	14pin 12p 47uF 10p* 16pin 14p 100uF, 150uF 18p*
7417	40p	74120	130p	74510		4093 4098	120n	BC187 30p*	BF194 10p*		11p	2N2222 2N2222A	21 p	40407	59p	SFC2741 25p	100v 1A 22p	18pin 25p 63v
7420	18p	74121	32p 54p	/4LS1	53 60 P	4099	145p	BC212 11p*	BF195 12p* BF224 20p*		16p 3p	2N2368	20p	40408	93p 292p	SN72702 60p* SN72709 AN	200v 1A 28p 400v 1A 38p	20nin 28p 1uF, 1.5uF, 2.2uF,
7421 7422	43p 28p	74122 74123	75p			4160		BC212L	BF240 18p*		lop dol	2N2369	19p	40411 40412	69p	90p*	50v 2A 46p	1 20nin 30n 3 3uF, 4 7uF, 6 8uF,
7422	26p	74125	75p			4161	105p	11p* BC213 11p*	BF241 18p*	TIP30A 4	14p	2N2646 2N2904	30p 25p	40673	99p	SN72733N	100v 2A 50p	24pin 34p 10uF, 15uF, 22uF, 47uF 12p*
7425	33p		65p	СМО	s	4162 4163	105p 105p	BC213L	BF244B		0p	2N2904 2N2904A	29p	40841 40871	78p	125p*	200v 2A 52p	28pin 42p 1000uF 25v 27p*
7426	43p	74128	82p	4000	18p	4174	110p	11p*	35p* BF257 35p*		7p 11p	2N2905	24p	40872	95p 106p	SN76003 255p*	400v 2A 60p 40v 15A 170p	40pin 52p 220uF40v 25p*
7427 7428		74130 74132	110p 82p	4001	18p	4475	100p	BC214 13p* BC214L	BF258 32p*		15 p	2N2905A	25p	100.2	.,,,,	SN76013N	40V 13A 110p	22uF 16v 8p*
7430	18p		60p	4006 4007	33D	4104	105p	13p*	BF259 36p*	TIP31B 5	1p	2N2906	20p			171p*		Management of the Control of the Con
7432	38p	74136	80p	4008	120p	4408	710p 710p	BC237 16n*	BF324 36p*		8p	2N2906A 2N2907	21p	LINEAL		SN76023N	Triacs	LED
7433		74137	60p 85p	4009	50p	4410	715p	BC237A	BF337 36p*		14p	2N2907A		CA3011	140p*	172p* SN76033N	100v 2A 32p 200v 2A 50p	TIL209 13p TIL228/1 24p
7437 7438	38p	74141 74142	3000	4010	60p	4419	280p	16p* BC237B	BFR39 30p* BFR40 30p*		19p	2N2926	13p	CA3014 CA3018	145p*	259p*	400 2A 75p	TIL212/1 25p TIL232/1 21p
7440	18p	74145	95p	4011 4012	18p	4499	550p	16n*	BFR41 30p*		i3p	2N2926G	13p	CA3019	*q08	SN76110	100v 6A 50p	TIL216/1 21p TIL 234/1 23p TIL220 16p CLIPS 2p
7441		74147	210p	4040	50p	4433 4435	1250p 800p	BC238 16p*	BFR52 20p*	TIP33 5	i8p	2N3053	24p	CA3020	170p*	73p* SN76115 97p*	200v 6A 65p	TIL220 16p CLIPS 2p
7441N 7442	120p	74148 74150	160p 130p		110p	4435	290p	BC238A 16p*	BFR79 30p* BFR80 30p*	TIP33A 6	4p 2p	2N3055	55p	CA30231	265p*	SN76227 93n*	400v 6A 75p	
7443		74151	81p	4015	95p	1451	290p	BC238B	BFR81 30n*		3p	2N3702 2N3703	11p*	CA3028	88p*	SN76660 50p*	100v 10A 75p	Ceramic Plate
7444	120p		85p		30D	4501	95p	16p*	BFX29 30p	TIP34 6	4p	2N3703 2N3704	110*	CA3046	86p*	TBA120S 150p*	200v 10A 99p	Miniature Caps
7445 7446	97p	74154 74155	140p 97p		110p	4302	120p	BC238C	BFX29 30p BFX30 34p BFX84 30p	TIP34A 7	11p	2N3705	44 - *	CA3048	290p*	TBA540Q	400v 10A 120p	1·8—4700pF 6p*
7447		74156	96p	4019	50p	4503 4506	65p	BC337 18p*	BFX84 30p		19p	2N3706	13p*	CA3075 CA3080	280p*	380n*		
7448	85p	74157	98p	4020	120p	4507	55 p (BC338 16n*	BFX86 30p		14p	2N3707 2N3708	13p* 13p*	CA3089	E COD	TBA550Q 380p*	Thyristors	Diodes
7450	18p	74159	250p	4021	115p	4508	295p	BC516 505*	BFX87 30p		24p	2N3709	13p*	l <u>.</u>	340p*	TBA641B11	50v 1 A 32p	1N914 4p 1N4148/9 4p
7451 7453		74160 74161	110p 110p	4023	22p	4510	apb	BC517 50p*	BFX88 30p	TIP35B 25	1p 18p	2N3819	22p*	CA3130 CA3140	120p	240p*	200v 1A 50p	1N916 4p OA 200 9p
7454	18p	74162	100p	4024	80p			BC547 16p*	BFY50 22p BFY51 22p		4p	2N3820	30 h	CA3160	120p	TBA651 180p*	50v 3A 49p 400v 3A 70p	1N4001/2 6p OA202 9p 1N4003/4 7p BAX 13 8p
7460	18p	74163			20p	L	.:	BC547A 16p*	BFY52 22p BFY90 90p	TIP36A 24	lep	2N3823 2N3903	69p* 15p*	LM301 A	N I	TBA800 348p* TBA810S	100v 5A 52p	1N4005/4 7P BAX 13 8P
7470		74164	120p	4026 4027	140p	BC107	sistors	BC547B		TIP36B 27	6p	2N3904	16p*		30p	352p*	600v 5A 90p	l
7472 7473		74165 74166	150p 160p		95n	BC107	7A	16p*	BRY39 45p BSX19 20p	TIP36C 31	45 q8	2N3905	18p*	LM318 LM324	200p 70p	TBA820 239p*	400v 7A 75p 200v 10A 70p	 ************
7474		74167	320p	4029	120p		12p	BC548 16p*	BSX20 20p	TIP41A 6	i4p	2N3906	18p*	LM339	85p	TBA920 295p*	400v 16A 99p	
7475		74170	260p		50p	BC107	/B 12p	BC549 16p* BC550 14p*	BU105		/2p	2N4036 2N4037			280p	30n	200v 30A 180p	12 Volt RTL Logic X (Sim to 300 series- High X
7476 7480	38p	74172 74173	650p	4033 4034	250p	BC108	12p	BC556 15p*	180p* BU108		3p i4p	2N4058	12p*	LM380 LM381 A	95p*	UA7471CP		↑ Noise Immunity. ★
7481		74174	110p		130p	BC108	BA	BC557 14p*	250p*	TIP42A 7	71p	2N4059	11p*	l	145p*	25p	Resistors	🗴 D2 +D3 i/p Nand Gates 🟃
7482	90p	74175	95p	4040	120p		12p	BC557A	BU204		/9p	2N4060	11p*		100p		·25W 1·5p*	∑ 25p ⊀
7483 7484	100p	74176 74177				BC108	BB	14p* BC557B	230p* BU205		91 p 74 p	2N4061 2N4062	12p*	LM747	70p	Zeners	100 Same value	💆 D2 i/p/ Nand + Quad Inv 🛪
7485		74177	120p 110p	4043	100p	BC108	12p RC	16n*	2265	TIP3055 6	14P 58p	2N4062 2N4123	14p*	LM748 FPQ346	7 85p*	D7V99c	£1.00	【 ② o/c 25p ★
7486	36p	74181	320p	4046	140p		12n	BC558 12p*	BU208	TIS43 3	11p*	2N4124	31 p*	FSA251	OM I	400mW	value £1⋅00 ⋅5W 2p* 1W 5p*	******
7489	340p	74182	150p	4047	100p	BC109	10p	BC559 16p*	1 240p*	TIS90 1	9p*	2N4125	15p*	<u> </u>	90p*	2v7-18v 8p*	1W 5p*	
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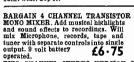
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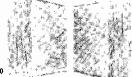
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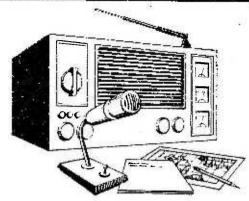
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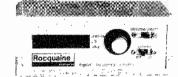
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DEPT. PWI2, P.O. Box 6, Ware, Herts **COMPONENTS SHOP: 18 BALDOCK** STREET, WARE, HERTS.

High quality audio modules for Stereo and mono

S450

STEREO FM TUNER Fitted with phase lock-loop





FREQUENCY RANGE	88-108 Mhz
SENSITIVITY	3 0 μV
BANDWIDTH	250 kHz
SPURIOUS REJECTION	50 dB
SELECTIVITY ± 400 kH2	55 dB
AUDIO OUTPUT (22 3 KHz devi	ation) 100 mV
STEREO SEPARATION	30 dB
SUPPLY REQUIREMENTS	20 to 30V (90m A max)
AERIAL IMPEDANCE	75 ohms
DIMENSIONS	240mm × 110mm × 32mm

The 450 Tuner provides Instant programme selection at the touch of a button ensuring accurate tuning of 4 pre-selected stations, any of which may be altered as often as you choose, simply by changing the settings of the pre-set controls. Features include FET input stage, Vari-Cap diode tuning. Switched AFC LED Stereo Indicator.

Stereo 30

AUDIO



OUTPUT POWER	7 Watts RMS
LOAD IMPEDANCE	8 ohms
TOTAL HARMONIC DISTORTION	Less than 5% (Typically 3%)
FREQUENCY RESPONSE	50 Hz to 20 kHz ± 3dBs
TONE CONTROL RANGE	± 12 dBs at 100Hz and 10kHz
SENSITIVITY	190 mV for full output
INPUT IMPEDANCE	1 M ohms
TRANSFORMER REQUIREMENTS	22 V.A.C. rated at 1A
DIMENSIONS (Less controls and panel)	200mm × 130mm × 33mm

The Stereo 30 comprises a complete stereo pre-amplifier, power amplifiers and power supply. This, with only the addition of a transformer or overwind will produce a high quality audio unit suitable for use with a wide range of inputs i.e. high quality ceramic pick-up, stereo tuner, stereo tape deck etc. Simple to install, capable of producing really first class results, this unit is supplied with full instructions, black front panel, knobs, main switch, fuse and fuse holder and universal mounting brackets.

AL60

MODULE 25 Watts RMS

£4 .55 + 35p p&p + 121% VAT

25 Watts RMS
30-50 V
8-16 ohms
Less than 1% (Typically 06%
20 Hz to 30 kHz × 2 dBs
280 mV for full output
90°C
103mm × 64mm × 15mm

This high quality audio amplifier module is for use in audio equipment and stereo amplifiers and provides output powers up to 25 RMS with distortion levels below 0.1%.

AL80

AUDIO AMPLIFIER MODULE £7·15*



	OUTPUT POWER	35 Watts RMS
	SUPPLY	40-60 V
	LOAD IMPEDANCE	8-16 ohms
١	TOTAL HARMONIC DISTORTION	Less than 1% (Typically 06%
l	FREQUENCY RESPONSE	20 Hz to 30 kHz × 2 dBs
ı	SENSITIVITY	280 mV for full output
l	MAX. HEAT SINK TEMPERATURE	90°C
ŀ	DIMENSIONS	103mm × 64mm × 15mm
l		

The AL80 is similar in design to the AL60 above and is of the same high quality but provides output powers up to 35W with distortion levels below 0.1%.

AL250

125W R.M.S. POW

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1938	
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A. C. L. S.	
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-	

£17 .25* + 40p pap + 8% VAT

125 Watts RMS continuous OUTPUT POWER OPERATING VOLTAGE 50-80 V FREQUENCY RESPONSE 25 Hz 20 kHz measured at 100 Watts SENSITIVITY FOR 100 WATTS INPUT IMPEDANCE
TOTAL HARMONIC DISTORTION
50 WATTS into 4 ohms
50 WATTS into 8 ohms 33 K ohms

This unit, designated AL250, is a power amplifier providing an output of up to 125W RMS, into a 4 ohm load.

AL30A

AUDIO AMPLIFIER MODULES

+ 121% VAT

£3 .75 + 35p p&p

30 V	
10 Watts RMS	
ON Less than 25%	
8-16 ohms	
100 K ohms	
50 Hz-25 kHz ± 3 dBs	
75 mV for full output	
74mm × 63mm × 28mm	

These low cost 5 and 10 watt modules offer the utmost in reliability and performance, whilst being compact in size

SPM80

STABILISED POWER SUPPLY £4 .25 + 35p p&p



INPUT A.C. VOLTAGE	33-40V	
OUTPUT D.C. VOLTAGE	33 V nominal	
OUTPUT CURRENT	10 mA-1·5 amps	
OVERLOAD CURRENT	1.7 amps approx.	
DIMENSIONS	105mm × 63mm × 30mm	

Within ± 1 dB from 20 Hz to 20 kHz

+ 10-20 dBs at 15 kHz

Better than 65 dBs (All Inputs)

Better than 26 dBs (All inputs)

± 15 dBs at 75 Hz

Designed to power two AL60s at 15 Watts per channel simultaneously. Circuit Techniques include full short circuit protection. 20 Hz to 20 kHz × 1 dB Less than 1% (Typically 07%) 100 mV/100 K ohms 100 mV/100 K ohms 3.5 mV/50 K ohms 3.5 mV/50 K ohms

SENSITIVITY INPUTS

EQUALISATION

BASS CONTROL RANGE

SIGNAL/NOISE RATIO

INPUT OVERLOAD

TREBIE CONTROL RANGE

FREQUENCY RESPONSE

1. TAPE 2. RADIO TUNER 3. MAGNETIC P.U.

PA100



£15.80

20 to 40 V 300 × 90 × 33mm (less controls) DIMENSIONS A top quality stereo pre-amplifier and tone control unit, the PA100 provides a comprehensive solution to the front end requirements of stereo amplifiers or audio units. The six push button selector switch gives a choice of inputs together with two filters for high and low frequencies.

MPA30

MAGNETIC CARTRIDGE PRE-AMPLIFIER



£2.95 +35p p&p + 121% VAT

Enjoy the quality of a magnetic cartridge with your existing ceramic equipment using the MPA 30 which is a high quality preamplifier enabling magnetic cartridges to be used where facilities exist for the use of ceramic cartridges only.

SENSITIVITY	3.5 mV for 100 mV output
EQUALISATION	Within ± 1 d8 from 20 Hz to 20 kHz
INPUT IMPEDANCE	50 K ohms
SUPPLY	18 to 30 V-re earth
DIMENSIONS	110 × 50 × 25mm (inc DIN socket)

PA12



£7·10 + 30p p&p + 121% VAT

The PA12 Stereo Pre-Amplifier chassis is designed and recommended for use with the AL 20/30 Audio Amplifier Modules, the PS12 power supply and the T538 Transformer. Features include on/off volume. Balance. Bass and Treble controls. Complete with 1961 tape output.

FREQUENCY RESPONSE	20 Hz-20 kHz (-3dB)
BASS CONTROL	± 12 dB at 60 Hz
TREBLE CONTROL	± 14 dB at 10 kHz
INPUT IMPEDANCE	1 Meg. ohm
INPUT SENSITIVITY	300 mV
CROSSTALK	—60 dB
SIGNAL/NOISE RATIO	65 dB
OVERLOAD FACTOR	± 20 dB
TAPE OUTPUT IMPEDANCE	25 K ohms
DIMENSIONS	152mm × 84mm × 25mm

PS12 POWER SUPPLY

Designed for use with the AL30A S.450 and MPA30 in conjunction with transformer T538. INPUT VOLTAGE OUTPUT VOLTAGE OUTPUT CURRENT SIZE

17-20v AC 27-30v DC 300mA 60mm × 43mm × 26mm + 1550 p&p 400mX 43mm × 26mm

+ 35p p&p + 12;% VAT

GE 100 NINE CHANNEL MONO-GRAPHIC EQUALIZER

The GE100 has nine 1 octave adjustments using integrated circuit active filters. Boost and Cut limits are ± 12d8. Max. Voltage handling 2 V RMS. T. H.O., 0.65%, input impedence 100K. Output impedence less than 10 K. Frequency response 20 Hz - 20 KHz (3dB). The nine gain controls are centred at 50, 100, 200. 400, 800, 1,500, 3,200, 6,400 and 12,800 Hz. The suggested gain controls are 10 K LIN sliders (not ± 35p pAp supplied with the module) See Paks S31 and 16192. + 12;% VAT

\$630 POWER SUPPLY BOARD for GE100 15-0-15 VOLT £5-50 +

SIREN ALARM MODULE

American Police screamer powered from any 12 voit supply into 4 or 8 ohm speaker. Ideal for car burglar alarm, freezer breakdown and other security purposes. Order No. S15. No. BP124.
Only £3-50 + 8% VAT + 35p p&p

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TC60 KIT

A beautifully designed genuine TEAK WOOD veneered cabinet to put the professional touches to your home built amplifler. Full set of parts incl. Front & Back Panels, Knobs. Chassis, Fuses, Sockets, Noen, etc. Ideal for the MA60. Size: 425mm > 290mm > 95mm.

Price £19 95 + 12½% VAT + 86p p&p

TRANSFORMERS

T538 For use with S.450 AL30A MPA30 Order No. 2036 Price: £3·20 + 55p pap + 125% VAT T2050 For use with Stereo 30 Order No. 2050 Price: £3·25 + 55p pap + 125% VAT BMT80 For use with AL60 SPM80 Order No. 2034 Price: £5·40 + 86p pap + 125% VAT BMT250 For use with AL250 Order No. 2034 Price: £6·35 + £1·10 pap + 121% VAT Order No. 2035 Price: £6:35 + £1:10 p&p + 121% VAT Order No. 2035



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<u>Happenings</u>

One, and that with the most widespread effect on the population both here and abroad, is the major reshuffle of frequencies in the medium and long wave broadcast bands effective on 23rd November. Since the first provisional plans were published earlier in the year, there have been a number of revisions, and the additional long-wave channel on 227kHz will not now be used by BBC Radio 4. Full details of the changes as they affect UK programmes are given elsewhere in this issue. The BBC has spent £3 million on new m.f. and l.f. transmitters in an effort to improve reception of its services after the changeover date. Let's hope it proves to have been worthwhile!

Undoubtedly the shift of Radio 4 to the long waveband will inconvenience many listeners whose receiver does not cover that band. Already, several designs have appeared for converters, which transpose the signals received on 200kHz to a channel in the medium waveband. In this issue we feature a unit suitable for use with a car radio, and we hope to publish one for portable radios in the very near future. The loss of 647kHz to the Overseas Services is a great pity.

If you're thinking of buying a new receiver, make sure it includes medium, long and v.h.f. bands for the best choice of programmes. If you want a new tuner for your hi-fi system, why not build the *PW* Dorchester?

The other event is the first staging of a new exhibition intended specifically for the amateur electronics constructor and experimenter. It's called "Breadboard 78" and it's on at the Seymour Hall, Seymour Place, London W1 from 21—25th November, daily from 10 am to 7 pm. Some sixty manufacturers and retailers, many of them regular advertisers in *PW*, will be exhibiting and there should be lots of interesting things to see.

Practical Wireless will be there showing a selection of projects, past, present and future, and we hope we'll see you there too.





Sylvia M. Barrett-Secretary

On leaving secretarial college, Sylvia, an Essex girl, got her first job with the British India shipping company in their London dock office. When her parents and brother Ray moved to Dorset, she and her husband Richard soon followed, a change they never regretted.

Before joining Practical Wireless last year, Sylvia worked for two large local electronic/engineering companies and for several years had her own small business which included long-distance chauffeuring. She also assists in running a local taxi firm with her husband, a qualified Company Secretary.

An avid sun worshipper, Sylvia loves to travel abroad to countries where the sun is hottest. Besides her secretarial work, she enjoys dressmaking, driving and motor-cycling, but her favourite pastime is Latin & Ballroom dancing, in which she and Richard have won many competition and examination awards.

NEWS..

NEWS..

NEWS...

Goonhilly 4

On 5th September 1978, Marconi Communication Systems Limited, formally handed over the new Goonhilly 4 earth terminal to the Post Office.

Designed for use with the next generation of communication satellites operating in the 11/14GHz frequency bands the new terminal was built as a joint-venture project with the Department of Industry, the Post Office and Marconi.

The equipment includes a 19-metre diameter antenna with a four reflector beam feed for frequency re-use, 2kW power amplifiers, up and down converters and high speed (120Mbit/s) digital modems.

Goonhilly 4 will be initially used with Europe's Orbital Test Satellite, OTS2, (forerunner to the European Communications Satellite, ECS) which was launched on 11th May, 1978 to prove the technology for digital satellite communications in the 11/14GHz frequency bands. The results of the OTS test programme will be particu-

larly relevant to the 1980's when 11/14GHz operation will be used for the European and other regional satellite communication systems and for international services via Intelsat V.

Club news

The following clubs inform me that they would like to increase their membership and would like to extend a welcome to anyone caring to attend their meetings.

First, the North Bristol Amateur Radio Club—G4GCT, who meet at the Lockeaze Community Association, Romney Avenue, Bristol, every Friday at 1900hrs.

The club has a Trio FT.200 transceiver, feeding into a trap dipole and recently installed an 8-element 2m beam, they also hold an RAE class during the winter.

Further details from W. G. R. Wilby G2BSU, 10 Wolseley Road, Bristol BS7 8EN.

Next, the Wisbech Radio Club—G8NED, who meet fortnightly in the private bar, of The Five Bells public house, Parson Drove (which is 5 miles west of Wisbech).

Further details from J. Arnold G8NPH, 5 Princes Road, Wisbech, Cambs PE13 2PG.

Finally, the Scottish v.h.f. and s.w. DXers Club, who specialise in v.h.f., (bands 1, 2 and 3) and u.h.f. DXing. They meet every second Saturday of the month at 1430hrs in members' homes.

The club operates a 'net' to alert members to 'openings', be they tropospheric or sporadic-E and would be interested in hearing from other enthusiasts in Scotland, Cumbria, Northumbria and Northern Ireland. In fact, anyone actively interested in anything above 30MHz is more than welcome.

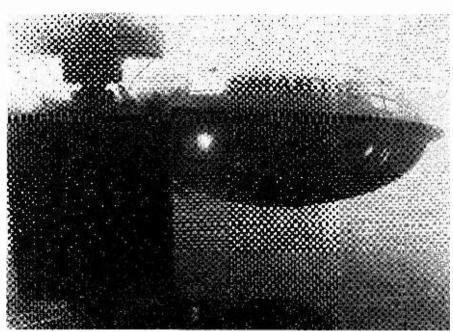
Further details from Frank Luman, 2 Ormonde Drive, Glasgow G44 3SJ. Tel: 041-637 5958.

SMARTIE

A completely new type of microcomputer-controlled unmanned inspection system, built to operate in the poor visibility and hostile operating conditions of the North Sea, has been launched by Richmond-based Marine Unit Technology Limited.

The new system is code-named SMARTIE (Submarine Automatic Remote Television Inspection Equipment). It is elliptical in cross-section and is basically a highly mobile underwater vehicle equipped with a battery of underwater t.v. cameras. These will consist of at least one low-light silicon intensified target (SIT) camera and a high resolution vidicon camera. The vehicle is driven by an elctrically-powered submersible pump and is therefore propellerless.

Apart from the relatively straightforward procedures of interpreting manually, input control signals from the operator's console, and controlling vehicle speed and direction. For low visibility work, the microcomputer can accept input from the submersible's magnetic compass and gyro, and project an artificial navigation target' which the operator can follow on his video screen even though the craft may be passing through an area of zero visibility.

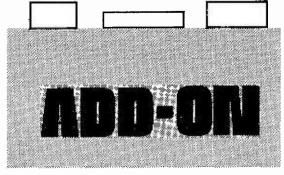


The vehicle will be supplied with power and control signals by a single umbilical cable under 0.5cm in diameter. The video signal will be continuously transmitted back to the surface via the same cable, unlike most unmanned submersibles that are supplied by very bulky multicore cables which can present very

real problems of signal interaction and physical drag by the cable on the vehicle.

SMARTIE will not be sold to the offshore industry for the time being. Instead, a complete underwater inspection will be offered.

Marine Technology Ltd., 3 Friars Lane, Richmond, Surrey TN9 1NL.



ERIC DOWDESWELL G4AR

The short-wave listener with his first communications receiver cannot be expected to get the best from it until a fair amount of time has been spent listening and getting the feel of the set, and of s.w. propagation conditions. There will be a tendency to cast an eye on the ads in various radio magazines for add-on accessories which claim to give improved reception.

Whether they will or not much depends upon the receiver. If it is from the highest price bracket it is very unlikely that much can be done externally to improve it. Indeed, any additions would be an insult to the designer! If, however, the set is really basic, without an r.f. stage and only simple ceramic filters in the i.f. stage/s and a conventional audio output stage, then it is going to need all the help it can get.

This article sums up the pros and cons of add-on units because they make excellent DIY projects and most can be bought in kit form or ready-built. But, remember, all of them, except a passive audio filter, will add some noise to the normal noise of the set. What we want is less noise and more signal and the simplest way of achieving that is probably cheapest. A better aerial system! Add-on units fit the bill because they restrict the bandwidth being amplified, at the r.f. input, at the i.f. stage or in the audio circuits.

Preselectors

A common tendency, where a listener considers that signals ought to be stronger, is to add a preselector (sometimes referred to as a pre-amplifier, wrongly in my opinion, as this term is usually reserved for audio work). If the receiver already has one or more r.f. stages then the preselector may prove to be worse than useless, causing increased cross-modulation, especially where strong signals are concerned. If the set has no r.f. stage at all then a preselector will be very worthwhile.

When obtaining a preselector make sure that it is a tuneable one and not aperiodic (wideband) and that it covers the s.w. bands on the receiver with which it is to be used. It must be connected to the receiver with proper coaxial cable, such as that used on TV installations, using proper coaxial fittings as it is essential that the signals reach the receiver via the preselector and not through any unscreened wire connected to the aerial terminal of the set.

The band switch should include a position where the aerial is switched directly to the receiver, eliminating the preselector and, generally, turning off the power supply to the preselector. Not an essential feature but highly desirable. An r.f. gain control is essential but if one is not fitted it is an easy matter to modify the preselector.

When using the preselector, first switch it to the straight-through position and tune the set to a steady but not too strong signal in, say, the 19m band, with the set's r.f. gain about half way. Switch in the preselector on the appropriate range and tune it for an increase in signal strength, which should be very marked. Note if there are any spurious signals that were not on the original signal. If there are this is a sign of internally generated cross-modulation and the r.f. gain on the preselector should be reduced until the spurious signals disappear.

Always ensure that the preselector is tuned "on the nose" to any signal being received and never detune it to act as a volume control. If a calibrated dial is fitted check that the frequency at which it peaks corresponds, more or less, to the signal frequency. At the higher frequencies it is very easy to tune the preselector to the second channel frequency which produces a marked increase in noise but no increase in wanted signal strength.

If, for example, the wanted signal is on 15050kHz then the second channel frequency is 15050kHz plus twice the set's i.f., usually around 470kHz, making 15990kHz which is not so far removed, as far as the tuned circuit is concerned, from 15050kHz. Many a preselector has been condemned because it has been tuned wrongly.

A preselector is sometimes chosen because it is thought that it will improve the "selectivity" of a receiver. This refers to the problem of adjacent channel selectivity where the preselector cannot help to any marked degree, but it does greatly reduce the second channel interference, previously referred to, by introducing more tuned circuits at the signal frequency.

Preselectors tend to be of more use at the higher frequencies especially if the main receiver is an older one lacking in sensitivity at the h.f. end. Do not be afraid to switch the preselector in and out of circuit to see if it is really effective. Sometimes it will be found to be an improvement and sometimes not, much

depending upon the frequency involved.

Q-Multipliers

Adjacent channel selectivity is the main failing of most communication receivers, especially the cheaper variety, and, come to think of it, the not-so-cheap ones now available. Selectivity is governed entirely by the quality of the i.f. filters, generally the one immediately following the mixer stage. Ceramic filters are frequently extolled today as being the best, but only because they are cheaper for the set manufacturer and eliminate expensive alignment time. The three usual modes of reception in which we are interested, a.m., a.m.(s.s.b.) and c.w. all require different i.f. bandwidths for optimum reception and a single bandwidth i.f. filter can only be a compromise. Unfortunately, separate filters can make a receiver rather expensive.

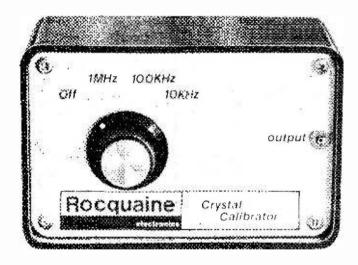


The only external aid to improved i.f. selectivity is some form of "Q-multiplier" which can be wired into the set with a couple of screened leads and virtually no modification to the set itself. In effect it extracts some of the i.f. signal and passes it through the external i.f. stage and back into the set. The external stage, or Q-multiplier, has a feedback control which allows the bandwidth to be sharpened up thus improving the selectivity, often to the point where the multiplier goes into oscillation. It only peaks signals over a comparatively narrow band of frequencies, rather than producing the ideal square-topped bandwidth characteristic, but it can be very effective for c.w. reception.

When buying or making a Q-multiplier ensure that its operating frequency is the same as that of the set to which it is going to be fitted. There is usually some form of adjustment to peak it to the i.f. after installation. Like the preselector there should be an "off" position that effectively by-passes the Q-multiplier.

Calibrators

No receiver should be used without some means of checking its calibration instantly. The better sets will have an internal crystal oscillator operating on 100kHz producing markers at that interval throughout the s.w. bands. Sets intended for the US market may have this broken down to 25kHz for checking the limits of the mandatory sub-bands in that country.



Rocquaine Electronics produce this crystal calibrator, an important accessory for a communications receiver

My own preference is for an external 1MHz crystal oscillator divided down to provide outputs at 100kHz and 10kHz, in addition to the fundamental 1MHz. After that it is not difficult to interpolate down to 1kHz especially if there is a decent bandspread dial on the receiver, which is quite sufficient to pinpoint an amateur or broadcast station for reference purposes.

The output of the calibrator is inserted into the set at the aerial terminal, again using coaxial cable. If possible fit a three-way wafer switch to provide "aerial only", "aerial plus calibrator" and "calibrator only". If the aerial is permanently connected then marker signals can often be lost or difficult to locate among other signals.



DFM from Roquaine Electronics operates up to 40MHz. It can be coupled to the receiver to provide direct readout of frequency. Unusually, wavelength can also be displayed

It is desirable for the receiver to have some means of either moving the dial cursor line or the frequency of the local oscillator in order to bring the set's calibration into line on any range. A small value tuning capacitor is often used in parallel with the oscillator section of the ganged tuning capacitor or an additional potentiometer if the oscillator is varicap tuned. Then the nearest calibration point on the dial can be made to agree with a marker signal from the calibrator, around the frequency of the station being checked.

My own method of measuring a station's frequency is to first note the approximate frequency and then check the 100kHz points on the set's dial against the calibrator, either side of the station, adjusting the vernier control if necessary to make the dial and calibrator agree. Then the 10kHz markers are switched on and counted down or up from one of the 100kHz markers. The station finishes up between two 10kHz points after which the frequency can be estimated to about a kilohertz. Sounds longwinded but, in fact, can be done in seconds, with some practice.

Note that all the usual causes of frequency drift in a set such as mains variations, temperature changes, vibration, etc., are eliminated by checking against a crystal standard over a very short period of some seconds only. Some experts recommend the preparation of calibration charts for every range of a receiver, checking every 100kHz point against the standard and noting the difference. This is an extremely tedious and entirely unnecessary procedure and certainly unreliable. A heavy knock or an enforced repair to the set and all the work done in preparing the graphs has gone down the drain, apart from the uncertainty of all the other factors previously noted.

One more point to watch. Ensure that the signal is tuned in for maximum strength, preferably using the S-meter if one is fitted, rather than relying upon the ear. The beat frequency oscillator should be used when making these frequency measurements and must be correctly adjusted and checked again from time to time.

To set the b.f.o., turn it off, tune in a reasonably strong signal, on the m.w. band if possible, where it is more likely to be steady in strength, again using the S-meter, then switch on the b.f.o. and adjust the beat frequency to zero. This point should coincide with the datum point on the b.f.o. knob or dial. Now, if it doesn't, either mark the zero-beat point on the panel or set the knob to the datum point and adjust the frequency of the b.f.o. internally until the zero-

beat agrees with the datum. Either way, it is essential to know when the b.f.o. is zero-beat and it must be set at that point whenever a frequency measurement is to be made. A marker from the crystal calibrator can be used, in lieu of a station, in making this adjustment.

Audio Filters

Audio filters are a common way of increasing the adjacent selectivity of a receiver but the importance of obtaining adequate selectivity as early as possible in the receiver cannot be overemphasised, thus giving subsequent filters a better chance of doing their job and avoiding the overloading of stages by strong signals.

The average audio stage is pretty flat in response compared to what is really required, especially on the amateur bands. The vast majority of amateurs use s.s.b. with commercial equipment where the audio bandwidth is deliberately restricted to about 300 to 3000Hz, considered the minimum necessary for adequate intelligibility on speech. So it is pointless for the audio stages to be any better than this, unless the SWL is particularly interested in the broadcast bands where better quality audio may be desirable.

On c.w. the bandwidth should be very sharp indeed and bandwidths down to a few tens of hertz are common although a couple of less selective positions are advisable. A simple way to restrict audio bandwidth is to fit an external filter between the set and the headphones. Commercial filters available may offer switchable bandwidths of, say, 80, 110 and 180Hz which are a joy to use on c.w. However, given the choice, such a filter should be fitted immediately after the detector stage and before the first audio stage, where signal levels are low, if it is to give of its best.

Some audio filters are passive, that is they do not contain any amplifying device, but consist of inductors and capacitors to resonate at, say, 750Hz or so. These will not provide such narrow bandwidths as previously quoted without "ringing", an effect that causes notes from c.w. signals to be sustained so that at high speeds the dots and dashes merge making the signal unreadable.

Although I have mentioned headphones before in other articles I am not going to miss the opportunity to do so again! They are an extremely important part of the receiving set-up. Not a luxury, but an absolute necessity for the serious DXer, to be preferred to a speaker at all times, unless listening to Capital Radio while doing some other work in the shack!

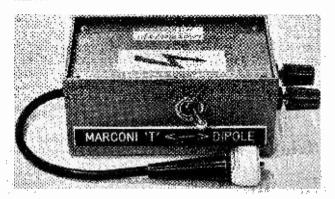
To go back a bit in time, the old magnetic diaphragm type of headset had a high resistance of 2 to $4k\Omega$, was extremely sensitive and frequently formed the anode load of the detector or first audio stage. No further amplification was necessary, hence the popularity and great sensitivity of the old t.r.f. receivers. These headsets had a very peaky response, frequently with a peak around 1000Hz, thus forming an excellent mechanical filter in themselves. When the c.w. beat note was adjusted to the same frequency the result was quite startling!

These old headphones had little response at low frequencies so any hum on the power supply was completely attenuated. In all, every desirable feature for the DXer. But along came hi-fi and stereo and low impedance headsets with every undesirable characteristic as far as DXing is concerned! If you can find a pair of high impedance headphones try con-

necting them to the receiver's low impedance output with a transistor type step-up audio transformer. An old valve-type output transformer is ideal.

Aerial Tuners

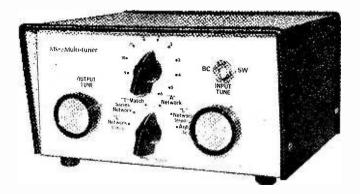
The best receiver going will do even better if it is allowed to, by providing it with a good aerial system suitable for the frequency band in use, as distinct from an odd length of wire. Any aerial can be likened to a tuned circuit where the voltage developed across the circuit is at a maximum when it has the same resonant frequency as the incoming signal. An odd length of wire will be resonant at some frequency or other but an aerial tuning unit (a.t.u.) will ensure that it is resonant at the desired frequency at all times.



A ferrite-cored transformer is used in this wideband aerial matching unit by G2DYM Aerials and Projects

An a.t.u. can be bought or it makes an ideal home project, because a simple a.t.u. need only consist of a tapped coil and a tuning capacitor initially. A more comprehensive one would have another capacitor and calibrated knobs plus a wafer switch to select the appropriate tap on the coil. An a.t.u. is simply an r.f. transformer changing the impedance at the end of the aerial wire to that of the input impedance of the receiver.

When using an a.t.u. the aerial is connected to the input terminal or socket and the output goes, via a short length of coaxial cable, to the aerial and earth terminals of the receiver. Most receivers today have a low impedance input, 50 to 75Ω , so the a.t.u. will take care of the mismatch between aerial and set.



This a.t.u. from Stephen-James allows any length of aerial to be resonated on the h.f. amateur bands. It also covers the m.w. broadcast band

Continued on page 59

(A) Dorchester

PART 1



ALL-BAND TUNER

W.S. POEL

The past few months have seen the introduction of several new i.c.s which greatly simplify the design of quality radio receivers. However, the term "simplification" refers specifically to the basic circuit complexity and not functional capability. In the process of integration, various techniques have been evolved, substantially advancing the art of mass production to a level where it closely approaches the performance achieved by some of the more revered communication-grade devices.

The i.c. employed in this project is a characteristic example of low cost/high technology components that are no longer merely an integrated version of an age-old discrete configuration but combinations of some very useful communications-type building blocks which provide an entire radio tuner on one speck of silicon. This is not to be confused with the ZN414 approach, which is strictly t.r.f.—a technique little better than a high input-impedance h.f. audio amplifier and peak detector.

The TDA1090 from Sprague is typical of state-of-the-art i.c. technology in low-cost a.m./f.m. receiver systems. It includes not only a very sensitive a.m. circuit (with an exceptionally-linear two-terminal local oscillator and balanced peak detector) but also all the features of the widely used CA3089E in its f.m. configuration.

Sprague may be a relatively new name to many readers but they have been market leaders in the USA for many years and were amongst the first to successfully integrate such consumer functions cost-effectively. The TDA 1090 is spearheading an attack on the world market for radio manufacturing—and from the performance of the tuner described in this article, it will be readily apparent that they have a potential industry standard to offer in the TDA1090.

Though not intended as a portable radio device, some may consider the current consumption figure of 16-23mA (a.m./f.m.) to be within the bounds of acceptability for this application.

The TDA1083 would probably be a better choice for portable receivers, offering basically similar features, though without the f.m. tuner options—such as a.g.c., tuning meter drive, mute etc; it includes an 800mW audio stage.

The TDA1090 therefore is best suited to mains or automobile applications. It is very much aimed at the hi-fi market, with a basic specification that offers the same degree of performance as the CA3089E for f.m. and a 20dB S/N figure for an a.m. signal of just $6\mu V$. The application considered here takes full advantage of the fact that the a.m. section is provided with a fully balanced input mixer stage and an excellent local oscillator system that produces a waveform of exceptional purity, minimising the chance of h.f. imaging whistles.

Circuit Description

The basic block diagram of the TDA1090 and its functions is shown in Fig. 1. Here the device can be seen to use the same i.f. for processing both a.m. and f.m. signals. In the a.m. mode however, the local oscillator and mixer are employed with substantial a.g.c. to keep the operation linear. The a.g.c. also controls these stages, helping to maintain the excellent signal capabilities of this type of system. The a.m. overload point is at 50mV—a dynamic range of some 80dB.

Use of a.g.c. on the local oscillator leads to a drawback if the device is to be used for s.s.b. reception however, since it will inevitably cause a degree of

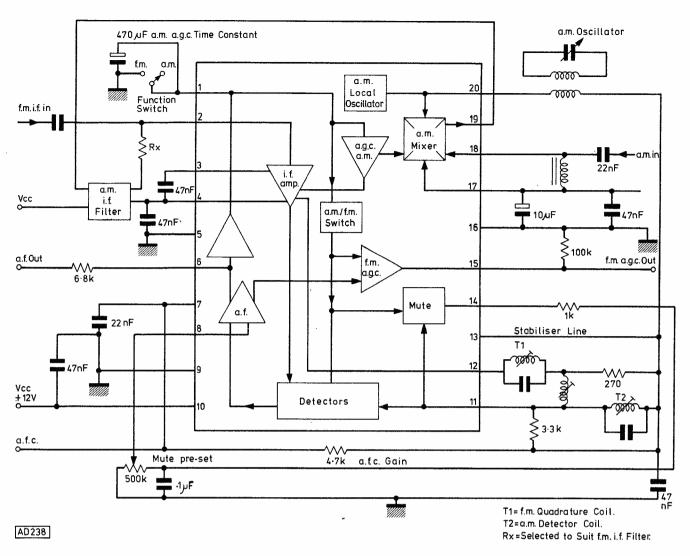


Fig. 1: Basic block diagram of the TDA1090 a.m./f.m. receiver chip with external circuitry required

oscillator-pulling at high frequencies. Although a very minor problem, this effect is sufficient to become annoying on s.s.b., even though completely unnoticeable on a.m.

The i.f. system is a four stage differential amplifier used at a gain of 82dB in the f.m. mode, and 26dB for a.m., the mixer stage making up for lost gain in the latter case. These figures represent the practical limits before instability and noise become problematical—although doubtless they will be improved at some time in the future.

The a.m. detector (Fig. 2) deserves special attention, since it is one of the fundamental features contributing to the success of this design.

The a.m. envelope is taken from the detector i.f. at pin 12 and then processed in a balanced arrangement at relatively low levels of i.f. voltage. Instability from feedback attributed to higher voltages—a problem inherent in such devices as the CA3123E/ μ A720 series—is virtually overcome.

The f.m. detector (Fig. 3) is the familiar fourquadrant mixer, found in the CA3089E series. It is driven differentially from the i.f., the quadrature signal being provided by the usual tuned circuit between pins 11 and 13. Basically, its operation relies on the fact that perfectly symmetrical transitions of the f.m. carrier will create an output voltage which is proportional to the phase/frequency response of the tuned circuit. The distortion will depend almost exclusively on the linear characteristics of the detector coil across the bandwidth of the incoming signal.

As with the CA3089E, the total harmonic distortion may be reduced by the use of secondary (and even tertiary) tuned circuits critically coupled to the primary quadrature coil. This enables greater bandwidths to be achieved whilst maintaining good linearity. For a perfectly-tuned signal there will be no basic offset (Fig. 4), but should the signal be to one side of its centre point, the d.c. offset generated in the detector can be used to provide the a.f.c. voltage for tuning correction. The f.m. and a.m. audio is arranged to appear at the same pin, obviating the need for switching.

In the case of f.m., the functions of muting, a.g.c. and meter drive are all basically related to signal amplitude and are simply peak detected and routed to the appropriate pin for external adjustment. The mute level will thus be dependent on i.f. noise levels, as well as basic signal headroom and is going to be

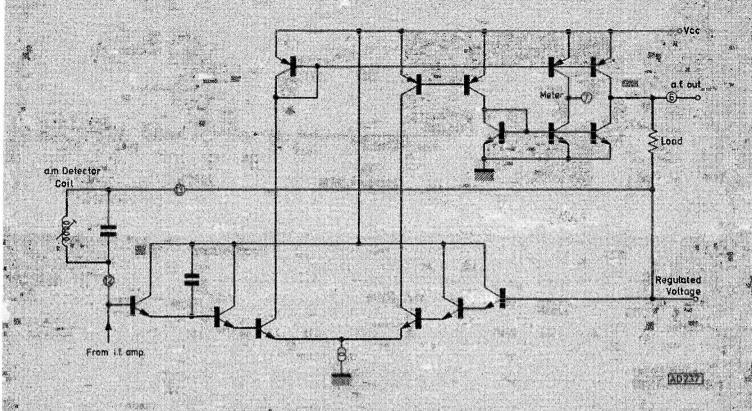


Fig. 2: Equivalent circuit of the a.m. detector section of the TOA1090 plus necessary external components

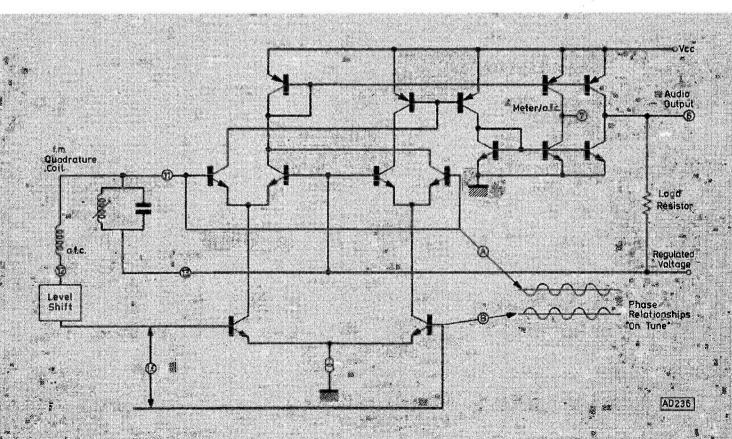


Fig. 3: Equivalent circuit of the f.m. detector section a of the TDA1090 plus necessary external components ,

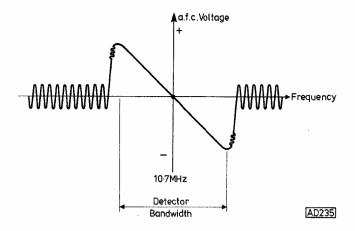


Fig. 4: Voltage/frequency characteristic of the f.m. detector

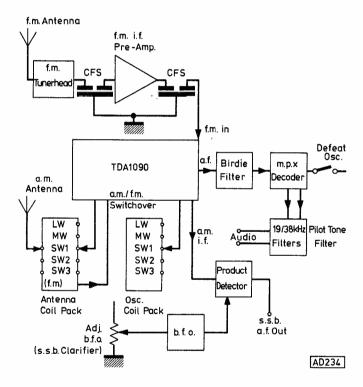


Fig. 5: Complete block diagram of the PW "Dorchester" all-band a.m./f.m. tuner

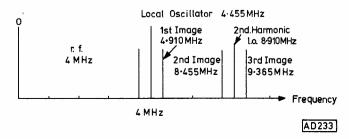


Fig. 6: Local oscillator output spectrum and image responses due to oscillator impurity

critical when used in conjunction with external gain at $10.7 \mathrm{MHz}$.

The CA3089E illustrated this shortcoming very clearly until developments of the KB4420A from Toko and HA1137W from Hitachi built in a degree of offset to accommodate high gain front end and i.f. preamp systems. In this configuration, an f.m. antenna sensitivity of $1\mu V$ is achieved with functional mute—and this represents the optimum attainable without an external muting circuit. It is nevertheless quite acceptable, and in many instances superior to some expensive hi-fi tuners.

The Complete Tuner

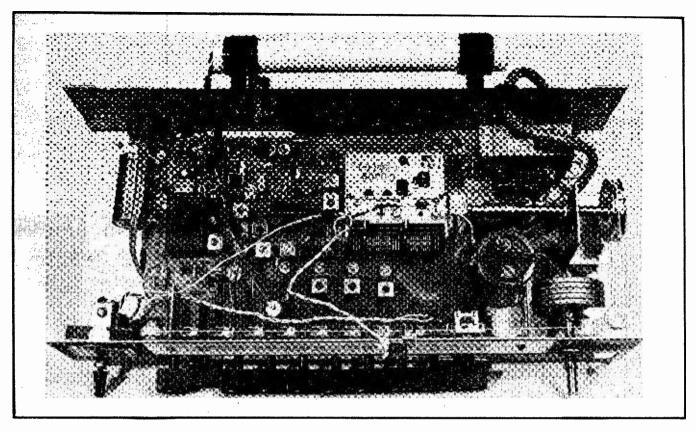
A block diagram of the complete tuner is shown in Fig. 5. The application of the TDA1090 uses a Toko type AT3302UG tunerhead, which combines a high quality a.m. tuning capacitor, with an f.m. tuner whose performance complements the overall design concept.

This is a really comprehensive radio tuner—covering all known radio broadcast bands (with the exception of the more unusual f.m. bands used in some parts of the world.) As well as short-wave broadcasts, it is also possible to receive amateur and commercial transmissions, though not to the stability necessary for communications-standard s.s.b. beyond SW2. This is due to a.g.c. action on the local oscillator (mentioned earlier), and the simple mechanics of stable tuning where such a large number of channels are covered within a single range. For instance, SW3 covers from 12 to 30MHz: 180,000 segments of 100Hz. generally considered to be the necessary resolution for s.s.b. By comparison, an amateur-bands-only tuner would typically cover 500 kHz, representing 5000 channels.

An electronic bandspread may be added by means of a single varicap across the local oscillator section of the variable capacitor. This will assist tuning at h.f. but will not entirely ameliorate basic mechanical shock and thermal problems. On a.m. broadcasts, a surprising degree of stability is achieved once the signal is tuned: generally rather better than can be expected from a discrete tuner of this type. In fact, there is no real reason—apart from the stability aspects—why varicap tuning could not be employed for the whole unit—but the additional care and techniques required are outside the scope of this article.

Two-stage tuning of s.w. is generally frowned upon as being inadequate and it is certainly true that many discrete s.w. designs do suffer from a variety of heterodynes brought about by image reactions. If the r.f. stage is tuned to, say 10MHz, and the local oscillator (high) at 10·455MHz, the basic image problem will be due to signal at 10·455 MHz+0·455MHz (i.e. where the local oscillator is 455kHz l.f. of the image) frequency. This problem can only be rectified by good r.f. selectivity, and is frequently blamed for heterodyne interference of another sort, namely that

TABLE ONE	- BAND COVERAGE	AD239
	LF	HF
LW	175 kHz	250 kHz
MW	525kHz	1605kHz
SW1	1·5 MHz	4·2 M H z
SW2	4 MHz	13 MHz
SW3	12 MHz	30 MHz
FM	88	108 MHz



Internal view of the prototype tuner

brought on by harmonics of the local oscillator, rather than the fundamental. In this case, a further diagram Fig. 6 serves to illustrate the nature of the effect.

The local oscillator second harmonic may be as little as 3-6dB down in some discrete circuits, where linearity is compromised to keep costs low by omitting the necessary impedance matching in order to avoid coil loading. So the mixer stage is then also presented with the out-of-band results of two-times the local oscillator frequency, plus and minus the i.f. All of which leads to an unruly cacophony of whistles in the short-wave bands!

The TDA1090 employs a type of oscillator that is far more linear than most discrete types—and furthermore, requires only a single switched connection for the necessary feedback winding, as opposed to the more usual configuration of less-elegant oscillator designs. The second harmonic of the oscillator is kept to below -50dB at most frequencies, substantially reducing the requirements of r.f. stage selectivity.

The net result is a tuner that can just about equal the performance of many lesser three-stage designs. There is no reason why a further r.f. stage should not be used in the form of a preselector—but with the high sensitivity of the basic circuit, it is important to use some form of gain control.

Pin 17 of the i.c. is an a.g.c. function on a.m., falling from 1.8V at maximum gain, to around 0.5 volt with an input to the i.c. of 1mV or so. This may either be used directly, or amplified to provide greater effect. Apart from additional gain, a large antenna may make an input attenuator a more useful extra and the unique pin diode network—the TDA1061—makes a good choice.

The f.m. side of the design includes all the usual functions, including a low pass filter, and stereo decoder. From the tunerhead the i.f. is fed through a 10·7MHz filter placed as close to the output as possible since even an inch or two of track would permit sufficient h.f. pickup to cause a swamping effect in the limiting amplifier of the i.c. A single transistor i.f. pre-amp provides an extra 10dB or so gain (over and above filter losses), and is a useful means of matching both ceramic filters. The decoder is nothing too esoteric. Whilst the Author is only too aware of the vast array of very high spec. devices, the HA1197, HA11223, TCA4500 and so forth, the long-established 1310 type of decoder has been used here.

The basic tuner is intended to be hi-fi, low-cost. More recent versions of the 1310 from Toko and Hitachi have provided superior separation and distortion to fill this particular requirement. A more pedantic approach to the whole project would be to use double detector coil arrangements, and the like, but then the unit could not have been readily copied by the enthusiast, unless sophisticated test equipment was to hand.

A pre-aligned pilot tone filter block is used to take out obtrusive 19/38kHz whistles when recording but this may simply be linked out if not required.

Finally, the block diagram shows a MOSFET product detector, fed from a high-stability f.e.t. b.f.o. As mentioned, s.s.b. reception is not up to the best communications standards, but this arrangement will make the most of the unit's capability up to about 14MHz.

Next month we move on to consider the practical circuitry and construction methods.

troduction to S.A.MONEY

A group of devices related to the flip-flops is that of the monostable circuits. Unlike the flip-flop, with its two stable states, a monostable device, as its name implies, has only one stable condition, which is usually its reset state where the Q output is at 0.

If a clock pulse is applied at its input a monostable will be triggered into the Set state, with Q at 1, in much the same way as a normal flip-flop. After some time delay, governed by a resistor-capacitor network. the circuit will return automatically to its normal reset state with Q at 0. Thus the Q output consists of a pulse at the 1 level whose length is determined by the time constant of the R-C network.

Practical Monostable Circuits

A monostable circuit can readily be produced by using a CMOS D-type flip-flop connected as shown in Fig. 58. In the stable state of the circuit the flip-flop will sit with its Q output at 0. Capacitor C will be discharged so that the Reset input will also be at 0 and therefore is inactive. Now, assuming that the D input is held at 1, if a clock pulse is applied the flipflop will switch to the Set state and the Q output will rise to the ·1 level.

When Q is at 1 the capacitor will charge towards the 1 level through the resistor R. After a period of time the voltage across the capacitor will have risen to the level where the Reset input is activated. For a CMOS flip-flop this threshold level will be about half the supply voltage. When the capacitor voltage rises above the threshold level it will activate the Reset input and force the flip-flop to return to its reset

state with \mathbf{Q} at $\mathbf{0}$.

As the Q output falls to 0 the capacitor will start to discharge through the resistor R. When its voltage falls below the threshold level again the Reset input will be disabled which in turn will allow the flip-flop to respond to input clock pulses once more. After some period of time the capacitor will have discharged back to the 0 level again and the circuit will be ready to start a new cycle of operations. The various waveforms that will appear in the circuit as it operates are shown in Fig. 59.

The time period for which Q is at the 1 level will be governed mainly by the values of the resistor and capacitor although the voltage level of the Q output, when it is at 1, and the threshold level of the Reset input will also have some influence. For this circuit the time delay can be calculated from the formula:

$$t = -CR \, \log_e \frac{V_t}{V_q} \, seconds$$

where C is capacitance in farads, R is resistance in ohms, Vt is the threshold voltage for the Reset input and V_q is the 1 level voltage at the Q output.

For a CMOS flip-flop where V_t is roughly equal to half V_q the equation simplifies to:

t=0.69 CR

and this equation will be found to be common to most of the monostable circuits in both CMOS and TTL type devices.

Because monostables are often used in logic systems they are available as logic elements in most of the types of digital logic. As an example, in the 74 series

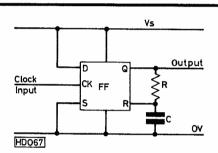


Fig. 58: Monostable circuit using a CMOS D-type flip-flop

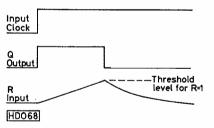


Fig. 59: Waveforms for the monostable circuit of Fig. 58

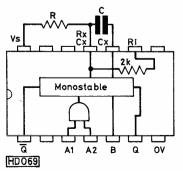


Fig. 60: The 74121 monostable and its external timing components

TTL types, the 74121 is a single monostable circuit and its internal arrangement and pin connections are shown in Fig. 60.

To make the 74121 reasonably versatile it has three clock inputs, A1, A2 and B. The B input is designed to be triggered by a pulse or logic level transition which goes from 0 to 1, whilst the A inputs are clocked by pulses going from 1 to 0. When either of the A inputs is fed by a clock pulse the monostable will be triggered, which is convenient if the circuit is required to respond to clock pulses from two separate sources.

The A and B inputs can be used to inhibit one another thus giving a simple means of gating the incoming clock pulses. The B input is only effective if at least one of the A inputs is at 0. Similarly the A inputs will respond to clock pulses only when the

B input is held at 1.

To allow flexibility in the choice of values the R and C timing components are connected external to the package with the capacitor between pins 10 and 11 and the resistor from pin 11 to the +5V supply as shown in Fig. 60. There is a timing resistor with a nominal value of $2k\Omega$ built into the chip and this can be used by simply joining pin 9 to the +5V supply. This is useful for some circuits, where timing is not critical, since the only external component needed is a single capacitor. For accurate time periods however the external resistor should be used and it is possible by suitable choice of values for R and C, to produce time delays from 100ns up to about $0\cdot 1$ second.

Two separate monostable circuits in a single package are provided in the 74123 whilst in the CMOS logic there is also a dual monostable device with the type number 4528.

Retriggerable Monostables

One problem with a simple monostable, such as that shown in Fig. 58, is that once it has been triggered it will not respond to any further clock pulses until it has completed its timing cycle. These later clock pulses would simply try to switch the monostable into the set condition when it is already there. The clock pulses will usually have no effect upon the state of the R-C timing network.

At the end of the timing cycle, when the Reset input is active, any applied clock pulses will be ineffective since they will be overridden by the reset action itself. In fact there will be a short period after the end of the timing cycle when the monostable cannot be triggered by an input clock pulse because

the Reset input is still active.

For some applications of monostables it would be an advantage if each new clock pulse would make the circuit start a new timing cycle even if the monostable is already in the middle of a timing cycle. Such a monostable circuit is called a Retriggerable monostable and a typical example is the 74122 in the TTL range. In CMOS the two monostables in a 4528 are of the retriggerable type.

In a retriggerable monostable the clock pulse not only sets the monostable but also discharges the timing capacitor to its original state so that a new timing cycle starts. If the circuit is already set the result is that the timing cycle is extended so that a complete timing period occurs after the last clock pulse before the circuit resets. This type of monostable often has a direct reset input as well which

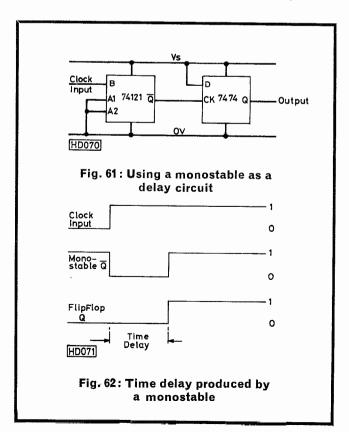
will override any timing cycle that is in progress and force the monostable to return immediately to its reset condition.

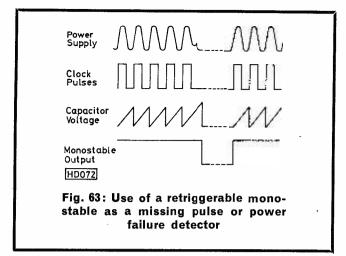
In the simple monostable circuit of Fig. 58 if the flip-flop is triggered again immediately after a cycle has completed the capacitor may not have had enough time to discharge completely. Now the new timing cycle starts with the capacitor already partly charged. As a result the reset input voltage will reach the threshold level earlier and the length of the new timing period will have been reduced from normal. This problem has been overcome in most of the monostable elements available in TTL and CMOS by incorporating a rapid discharge circuit for the timing capacitor so that it recovers rapidly after the end of a timing cycle. In the circuit of Fig. 58 this could be achieved by connecting a diode across the resistor R so that the diode conducts and discharges the capacitor when Q goes to θ .

Using Monostables

How can a monostable be used in a practical logic system? One obvious application is to use it as a simple pulse generator. Here the monostable is triggered each time a pulse is required and the output from Q or \bar{Q} will provide the desired pulse output. The width of the pulse will be controlled by the timing components of the monostable and its polarity by whether it is taken from Q or \bar{Q} . The input required to produce a pulse is simply a logic transition either from Q to Q or Q or

A second application of the monostable is that of producing a time delay. Here the trailing edge of the pulse produced at the output of the monostable is used to trigger a flip-flop or another monostable as shown in Fig. 61. If the monostable is triggered it





will go through its timing cycle and then trigger the following stage thus producing a delayed action as shown in Fig. 62. The length of the time delay produced will be determined by the timing components used with the monostable circuit.

The retriggerable type of monostable can be used as a missing pulse detector. Here the monostable is clocked by a regular stream of pulses and its timing cycle is set to be about 50 per cent longer than the period between successive pulses. All the while the input pulses are present the monostable will remain set because a new pulse will retrigger it before it can complete a timing cycle. If however one of the input pulses is missing from the stream the monostable will have enough time to complete its cycle and will reset for a time, thus producing an output pulse. This action is shown in Fig. 63.

A retriggerable monostable might be used as the basis for a rapid-acting power failure detector. In this case the clock would be derived from the a.c. power supply, at say 50Hz, and the monostable would have its timing period set at 30ms. Now the monostable will remain set whilst the supply is on. If the supply fails for just one cycle the monostable will time out and may be used to trigger a circuit which switches in a standby power supply.

Similar missing pulse detectors are often used in data systems to detect the gaps between individual data records or between blocks of data which have been recorded onto a magnetic tape or disc.

Astable Circuits

If two monostable circuits are connected back to back as shown in Fig. 64 the system will oscillate continuously. As one monostable times out at the end of its cycle it will trigger the other monostable and vice versa. Such a circuit has no stable condition and is referred to as an Astable. In a logic system astable circuits are generally used for the clock and timing oscillators. In most cases they will be built up from either logic gates, monostables or from simple discrete component circuits. In CMOS however the 4047 is a special device designed to operate as an astable.

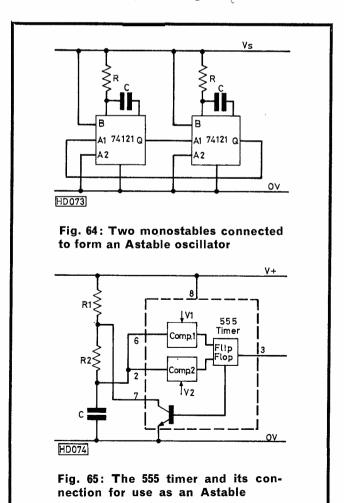
The 555 timer is a linear integrated circuit which is frequently used as an astable oscillator in logic systems. Fig. 65 shows the internal arrangement of the 555 and the way it would be connected to operate as an astable. Here an input voltage is compared with

a pair of internal reference voltages V_1 and V_2 by two voltage comparator circuits which in turn set or reset a flip-flop to control the output.

In the astable arrangement of the 555 when the voltage across the capacitor is zero the flip-flop will be set and the output level will go to 1. Now the capacitor will charge through R1 and R2. As the capacitor voltage rises above level V₁, usually about ²₃ of the supply voltage, the comparator Comp.1 operates and resets the flip-flop. Now the output falls to 0. When the flip-flop is reset it turns on a discharge transistor which effectively shorts the junction of R1 and R2 to 0V so that the capacitor now discharges through R2. When the capacitor voltage falls below level V2, nominally 13 of the supply voltage, the second comparator Comp.2 is activated and this sets the flip-flop again. Now the discharge transistor turns off and the capacitor starts to charge again. This cycle of operations will continue indefinitely so that the capacitor voltage rises and falls between the limits V₁ and V₂ whilst the output alternately switches between the 0 and 1 states. Frequency of operation is determined by the values of R1, R2 and C.

Logic Inputs

So far in this series we have looked at the logical operation of the various types of logic element but now it is time to examine in more detail the input and output characteristics of the logic devices. We shall start by looking at the input characteristics.



It will be remembered that in a TTL device the input signal is fed to one of the emitters of a multiemitter npn transistor. The base of this transistor is usually held at a bias voltage of some $+1\cdot 2$ volts.

Suppose the input were connected directly to 0V to produce a logic 0 input. The input emitter will now become forward biased and the transistor will conduct passing a current of some $1\cdot 6mA$ from its emitter through the external circuit to the 0V line. In practice the input will not be shorted to the 0V line but will be driven by an external circuit which may have some resistance. The emitter current will now produce a voltage drop across the external circuit so that the actual input voltage is no longer zero but some small positive voltage.

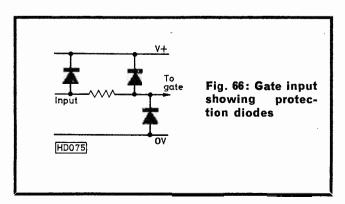
For a typical TTL device any input voltage between 0V and about +0.8V will be treated as a 0 level logic input. This means that the circuit driving the input must be able to "sink" the 1.6mA flowing from the input emitter without producing a voltage drop of more than 0.8V when it is at a 0 logic level. If a simple resistor were connected to 0V to produce a 0 level input the resistor would need to be less than 500 ohms in value.

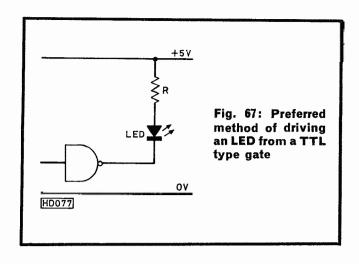
When the logic input is taken to say +5V to produce a logic l input the emitter of the input transistor will be reverse biased and therefore cut off. In fact a small level of leakage current of perhaps $50\mu A$ will flow into the logic input. Normally TTL circuits are designed to accept any input voltage from +2V to +5V as a l level logic input. In this case the driving circuit need not have a particularly low resistance and a typical value resistor for tying an input to +5V for a l level might be about $4\cdot 7k\Omega$.

Input voltages between +0.8V and +2V may be treated as either a 0 or a 1 state by the logic device. Usually if a TTL input is left open circuit it will assume a voltage level of about +1.2V and generally acts as a 1 level input. For reliability however it is advisable to connect up any unused inputs either by tying them directly to 0V or +5V or by joining them in parallel with another input if the device is a gate.

With its MOSFET input stages the CMOS type logic unit presents a rather different input characteristic. Here the input impedance is extremely high, perhaps tens of megohms, and virtually no current flows in either the θ or 1 state.

Because of the very high input impedance of a CMOS device it is very easy for a charge of static electricity to build up at the inputs of a circuit. Static potentials of hundreds of volts may easily occur and if these were allowed to discharge through the device itself it is likely that the internal circuits would be at least partially destroyed. In the early days of MOS and CMOS devices great care was needed when





handling the i.c.s to avoid damage due to static charges. A careless operator could easily destroy hundreds of i.c.s just by touching them. Fortunately today nearly all of the CMOS devices incorporate protection diodes at each input. These diodes which may be arranged as shown in Fig. 66 are designed to allow static charges to leak away before they reach dangerous levels which might damage the chip. Although protection diodes are fitted however it is wise to take some precautions when handling CMOS devices.

Normally CMOS circuits should be stored and handled with all of the pins of the device shorted together. This may be achieved quite easily by pushing the pins through a sheet of aluminium foil or conductive plastic foam. If the device is to be soldered into a circuit board make sure that the soldering iron is properly earthed. It is preferable to mount CMOS i.c.s in sockets so that they can be inserted after all of the construction and wiring is complete.

Any unused inputs of a CMOS device should be tied, either directly or through a resistor, to one of the supply rails. An open circuit input will tend to float as static charges build up on it and the input voltage level may vary continuously with time. Because of its high impedance the input will also tend to pick up stray signals, such as 50Hz power frequency components, and as a result logic operation is likely to be erratic to say the least.

Where a CMOS input is driven from outside the unit or from another circuit card it is as well to treat it in the same way as an unused input by tying it to one of the power rails through a resistor of perhaps $22k\Omega$ to $100k\Omega.$

Logic Outputs

The totem pole type output stage of a TTL device is specifically designed to drive the inputs of other TTL type circuits. When the output is at logic 0 the output stage is capable of sinking a current of some 16mA to ground whilst still maintaining the output voltage below +0.5V to ensure a proper 0 level signal. Thus a standard TTL output will drive ten TTL input circuits reliably. In fact it will be able to drive more than ten circuits most of the time but the load on a device should be limited to ten TTL inputs for reliable logic operation. Some devices, such as the 7440, have a higher output capability and can drive up to 40 TTL inputs.

In the 1 state the TTL output can drive a current of about 0.5mA whilst maintaining a minimum voltage level of +2.5V. This must be borne in mind if the logic device is to be used to drive discrete circuits. If an LED indicator is to be driven by a TTL output it should be arranged as shown in Fig. 67 so that the TTL circuit sinks the current from the lamp rather than trying to drive current into it.

Outputs in CMOS are normally capable of driving or sinking currents of the order 0.5mA and the output voltage levels are likely to switch from about +0.5V up to about 0.5V less than the positive supply

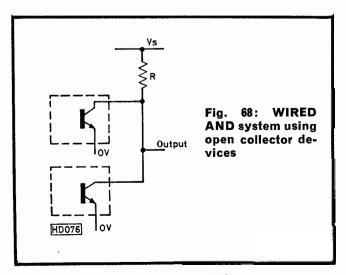
Open Collector Outputs

There are occasions in logic system design where a number of outputs are required to feed into a single line. This can, of course, be achieved by combining the signals in an OR gate to produce a single output. Another approach which comes to mind is the possibility of connecting all of the outputs directly in parallel to a common output line. If this were done using conventional totem pole output stages the results would be disastrous. If one output is at 1 and another at 0 the two output stages will conflict in an attempt to drive the output to both 1 and 0 at the same time resulting in excessive currents in the output transistors. As a result one or both of the output circuits would be destroyed or at least damaged.

By using a modified form of output stage, known as an Open Collector output, it is possible to connect a number of outputs directly in parallel with no damage. In an open collector output the upper transistor of the totem pole is omitted so that the output will only draw current in the 0 state and is effectively open circuit for a 1 output. Open collector outputs are fed to a common load resistor as in Fig. 68. This arrangement works effectively as an AND gate and the configuration is usually known as WIRED AND.

Tri-State Logic

A further development in output stages is the Tri-State output circuit. Here an extra control line allows the output stage to be switched off so that it presents an open circuit to the output terminal. Thus the output can have three states (tri-state) namely 0, 1



and open circuit. In a multi-gate package a single enable line may be used to switch on all of the output stages simultaneously or separate enable lines may be provided for each section of the device.

It is important in a system using paralleled tri-state devices that only one circuit is enabled at any time, otherwise the results would be the same as if normal

output stages were connected in parallel.

Both CMOS and TTL type devices are available with tri-state output stages. In some cases tri-state input circuits may also be provided. Here when the circuit is disabled the input will present an open circuit impedance. Sometimes a circuit, especially in the case of memory devices, may use the same pin for both input and output the function being selected by a control line which enables the appropriate part of the device.

Power Supplies

One aspect of logic systems which is often overlooked is the power supply. In a TTL system the supply voltage must be held within $\pm 0.25V$ of a nominal +5V level for proper logic operation. Gates will often work at lower supply levels than +4.75Vbut flip-flops, counters and shift registers are likely to behave erratically under these conditions.

The TTL circuits tend to draw quite a bit of current and it is quite easy to reach a supply current of an ampere or so with relatively few i.c.s, especially if they are of the more complex type. To maintain proper supply conditions some form of regulated or

stabilised supply will be needed.

In a TTL system where the devices switch at up to 30MHz quite large pulses of current may flow as devices switch. It is important that adequate decoupling of the supply leads is provided to avoid interaction between logic devices. A good rule is to fit a $0 \cdot 1 \mu F$ ceramic capacitor across the supply rail for every three TTL chips in the system. These decoupling capacitors should be distributed around the circuit board to confine circulating currents to local areas of the board.

The CMOS devices are much more tolerant of supply variations and will work with any supply voltage between +3V and about +15V. Current requirements are generally very small since the CMOS stages often take most current as a pulse whilst they are switching from one state to another. These current pulses charge and discharge stray circuit capacitances and usually the supply current will increase as the frequency of logic operation increases. Supply decoupling is required in a CMOS system but need not be as heavy as in a TTL circuit.

Because of their low current demand, CMOS circuits are ideally suited to battery operated systems. A CMOS digital watch chip will run for a year or two

from a tiny cell.

Frequency of switching of a CMOS circuit is affected by the supply voltage and will be higher with the higher supply voltages. Typically a CMOS counter may operate at 10MHz on a 15V supply but this rate would fall to perhaps 3MHz at 10V and only 1MHz at +5V.

Next month we shall look at the way in which a logic system might be designed.

NEXT MONTH IN.

ON SALE 7ST. DEC.



Build the

Sandbanks

Metal Detector
A Pulse Induction (PI) design, specially developed for the enthusiast to build without need for any test gear more elaborate than a multimeter. The circuit combines good sensitivity with low power consumption, and is insensitive to ground effects, salt water, damp

and read our special feature on

Metal Detection

Explaining the various types of detector available, how they work, and their advantages and disadvantages. The regulations covering the design and use of metal detectors. How to go about planning and conducting a search for buried objects, and what to do when you find them!

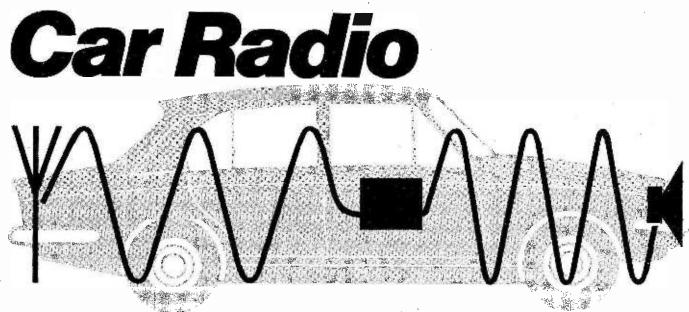


A versatile circuit, based on the SAD1024A "bucket-brigade" device, which allows you to delay audio frequency signals by a fixed or variable amount, producing reverberation or echo effects, pseudo-stereo etc.

An elegant matched pair of l.c.d. digital watches, for him and her, our special offer would make an excellent present. In chrome cases they have time displayed continuously with the date and seconds available at the touch of a button.







LONG WAVE CONVERTER

M.J.HUTCHINSON

The shift in BBC frequencies at the end of 1978 creates a problem for many car radio owners. From November 23rd, Radio 4 programmes will be transmitted on 200kHz, at present used by Radio 2. This will mean that thousands of listeners without long wave facilities will lose the only national alternative to the essentially music stations Radio 1, Radio 2, and Radio 3. These radios fall into two categories:-

- (1) Standard units fitted to Japanese cars
- (2) Units which incorporate an f.m. band and/or cassette playing facilities. Examples are to be found in the Pye, Amstrad, Sony, Pioneer, Sharp and Philips ranges, amongst others.

The provision of an f.m. band does not entirely solve the problem. Reception can be erratic in some areas, and in any case almost four hours is daily used for educational broadcasts.

The need was therefore to find a less expensive alternative to the problem than the purchase of a new receiver. The unit described offers a considerable saving on the £60+ needed to replace a set in the secondary category. Fig. 1 illustrates the operation

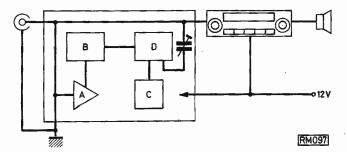


Fig. 1: Block diagram of the Car Radio Long-Wave Converter

of the unit in block diagram form. The aerial cable is tapped within the screened box to provide the signal for the fixed frequency long wave tuner (B). A simple r.f. amplifier stage (A) is used to interface the tuner with the aerial for two reasons. It improves the sensitivity of the tuner and ensures that the additional load does not degrade the signal to the car radio. This solution proved to be better than using an electronic splitting circuit. The aerial cable remains unbroken, so no wide bandwidth amplifier is required for a.m./f.m. sets.

The Circuit Technique

A 1600kHz oscillator (C) provides a signal which is modulated (D) by the audio output of the tuner. The resulting r.f. signal is fed into the aerial system via a trimmer capacitor. The radio will now receive the original 200kHz signal at around 1600kHz on the medium wave band.

Fig. 2 shows in detail the r.f. buffer amplifier. Like all stages of the unit it is powered by the car's 12 Volt supply. Using the f.e.t. means that no undue load is placed on the aerial line.

The l.w. tuner is varicap tuned and designed around the HA1197 i.c. Although it is unaffected by the fluctuations in the car's supply it is essential that the tuning voltage be derived from a stable source, and in this case the 10V required is obtained from the oscillator circuit. Capacitor C32 is required to smooth out any peaks from the electrical system which would cause interference, although in practice the value need not be as high as $1500\mu F$; the $4.7k\Omega$ pot on the tuner board sets the audio output level.

The oscillator in Fig 3 is a conventional Colpitts circuit, and the coil is wound on an Ambit 13K series former with a single tuning slug. This, together

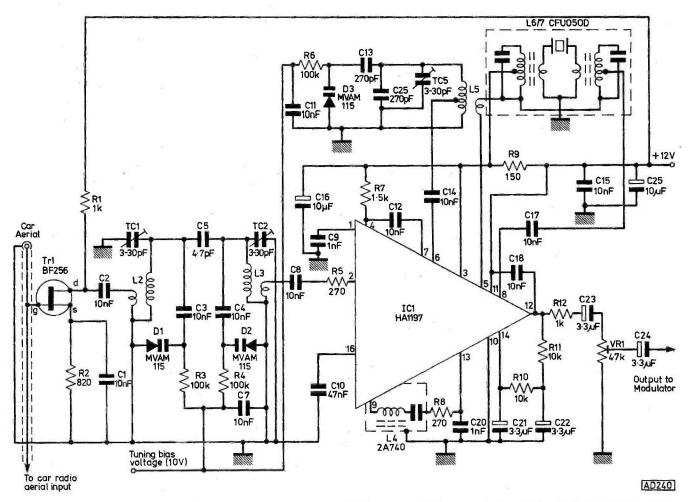
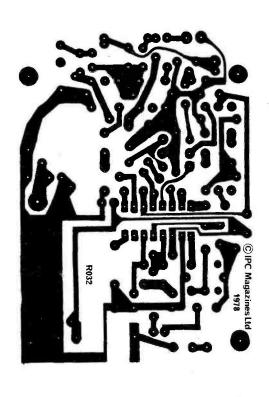
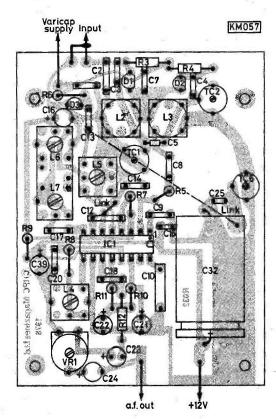


Fig. 2: Circuit diagram of the r.f. amplifier and l.w. tuner (C25 near \pm 12V terminal should be C39). Below we show the full-size p.c.b. pattern of the above circuit and the component layout—capacitor near C2 is C11





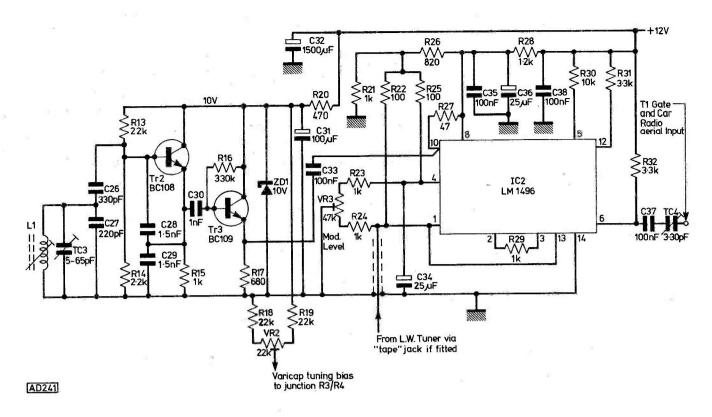
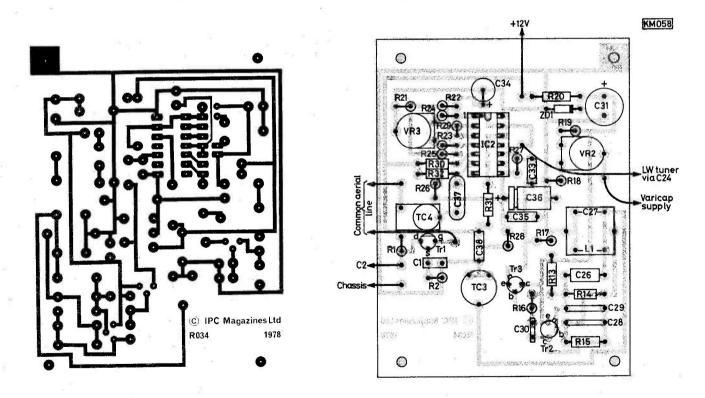


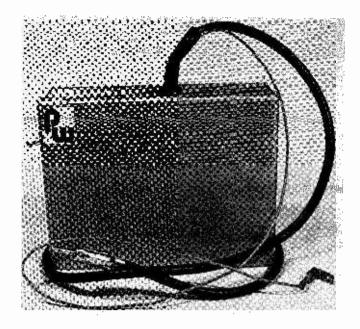
Fig. 3: Circuit diagram of the Oscillator and Modulator. Below we show the full-size p.c.b. pattern of the above circuit and the corresponding component layout



with the trimmer, sets the frequency of the oscillator and in practice a fairly wide frequency range can be obtained.

Fig. 3 also shows the modulator circuit which is designed around the LM1496 i.c. VR1 is used to balance

the level of modulation of the carrier and the outgoing signal is then fed to the aerial via the trimmer capacitor. N.B. The unit described is for a car with a NEGATIVE earth. Older models may have a POSITIVE earth and the unit must be wired accordingly.



Constructional Notes

The circuit should be built in an aluminium box to screen out interference from the car. The screened lead from the unit to the radio should be the low loss type designed for car radio aerials and this can be obtained as an 'aerial extension lead' from car accessory shops. Ideally the unit should be connected to the car radio on/off switch but if this is a problem then it can be connected to a spare 12V terminal. An independent on/off switch may be included if required.

The car aerial plug is connected to the unit, and the outgoing lead is plugged into the car radio aerial socket.

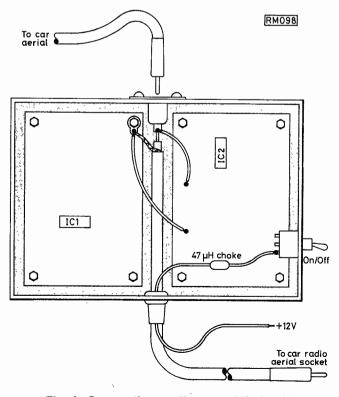


Fig. 4: Connecting up the completed unit

* components

Resistors († c	# # YV (
47Ω	1	- R27
100Ω 150Ω	2	R22, 25
270Ω	2	R9 R5, R8
470Ω	•	R20
680Ω	4.	R17
820Ω	2	R2, 26
1kΩ	7	R1, 12, 15, 21, 23, 24, 29
1·2kΩ	-475	R28
1-5kΩ	1	R7
2·2kΩ	1	R14
3-3kΩ	2	R31, 32
10kΩ	3	R10, 11, 30
22kΩ	3	R13, 18, 19
100kΩ	3 1	R3, 4, 6
330kΩ		
Potentiomete)rc	
alan dan Disembalan dan ger		
all mintature 4.7kΩ	pre-set 1	VRI
22kΩ	4	VR2
47kΩ	1	vrš
Capacitors)	min din Ali Pagalitan Mari 1965 ri Pradi dan di Barangan Ali
Para Matti Calabi	et i set.	
s/mica 4-7pF		C5
220pF	1	
270pF	1	Č25
330pF	4	C26
35 mg 3 1 mg 2 mg 3		
Ceramic Disc 1nF	3	C9, 20, 30
1·5nF	2	C28, 29
10nf	12	C1, 2, 3, 4, 7, 8, 11, 12, 14, 15,
		17,18
47nF	1	HANCIO EL SECUENCIA DE LA COMPANIO
10nF ===	4	C1, C33, 37, 38
Electrolytic (p	rh m	ounting 16V
3.3µF	4	C21, 22, 23, 24
10μF	2	C16, 39
25μF	2	: C36
100μF	1	
Tubular 25V	i da la	
1500µF		C32
Note: C6 and	19 not	
Trimmers (fo	il or coi	mpression types)
3-30pF	:4	TC1, 2, 4, 5
5-65pF	1	TC3
Integrated Cir	cuits	그 하는데 그리는데 얼마 얼마를 먹다고요?
HA1197	4	- ice
LM1496	1.	refice in the first water than the
Transistors		
BF256	1	
BC109	2	Tr2, 3
	k grad	
Zener Diode	mijas Kil Kilon	网络伊尔安亚洲苏斯 计工模型
10V 100mW	a filtra	ZD1
Inductors		
L1-50 turns (of 34 s	w.g. enamelled on Ambit 13k former
L2/L3-1A350	(Toko)), L4-2A740 (Toko), L5-16726 (Toko),
L6/7 CFU050	(Toko)	
Miscellaneous		
Charles Light Light	Albania Car	d socket, tape jack (optional), case
approx. 105 ×	135 × 4	10mm, on/off toggle switch (optional)

Although the unit is connected to the car earth supply by the outer screen of the aerial cable, it is advisable to make an additional link to the car's metalwork direct from the aluminium box in order to ensure good bonding to chassis.

In some cases prominent "spikes" from the generator or ignition system may cause interference. This can be reduced by including a $47\mu H$ choke, (or higher) in the 12V supply line.

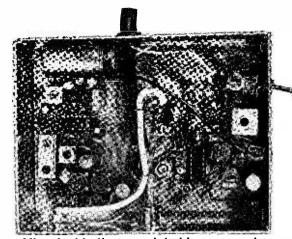
Alignment and Testing

The long wave module can be aligned by ear using the 200kHz transmission if no signal generator is available, or a complete aligned module may be obtained from Ambit International.

The tuning pot should be set to receive 200kHz. The technique is to use a generator or the BBC 200kHz transmission, and a meter connected to the test point on the board. The unit should now be wired into the car system.

Tune the car radio around the 1600kHz area until the long wave signal is heard. Now set the pot on the modulator circuit to achieve the best signal. It may be necessary to adjust the audio output level on the tuner board in order to obtain a distortion free signal. Once this has been obtained then the oscillator should be adjusted so that the signal generated by the unit is obtained on a quiet part of the band.

Bear in mind that the band becomes more crowded after dark, and check the full length of the medium wave band to see that any harmonic signals from the unit do not clash with stations you may require. Some harmonics are inevitable but by trimming the

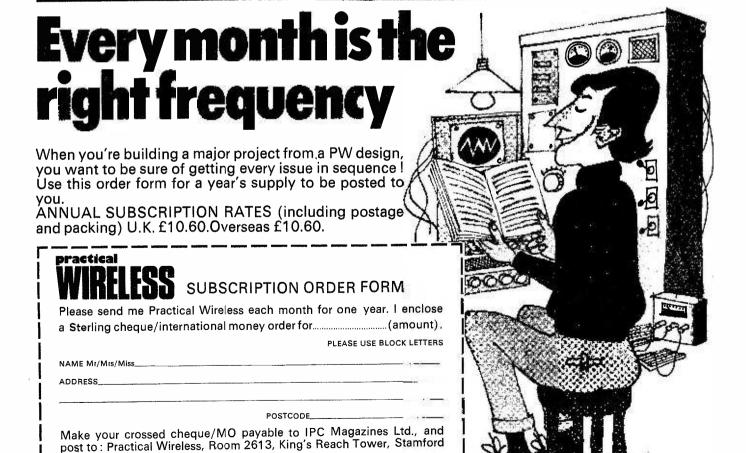


View inside the completed l.w. converter

capacitor in the unit's output line they may be reduced. The aerial trimmer in the car radio may need some adjustment in order to obtain the best results. Finally, if the radio has push button tuning, lock on to the position of the long wave signal.

Additional use of the Unit

The unit may be used in conjunction with a hi-fi system tuner, provided that the tuner has a medium wave facility. In this case a stabilised 12 Volt supply will be required. The plug will almost certainly need to be a different type in order to connect to the a.m. socket of the hi-fi tuner unit. A short length of wire will serve as an aerial.



Street, London SE1 9LS.



Citizen's band

Sir: In the last few years we have heard a lot of talk about a citizen's band for the UK. There are people in this country who can't wait to get their hands on a transmitter and push out a few watts. But have they ever stopped to think what a citizen's band would mean. A citizen's band is what it says; it is a CITIZEN'S BAND i.e. every Tom, Dick and Harry can pick up a transmitter and get on the air. From the trucker to the school boy—and they will come in their millions.

You can be sure that the true citizen's band campaigner will try to use the band as an extra amateur band to make regular local contacts and pass on information and news to other people—impossible because the band will be overcrowded by the Toms, Dicks and Harrys of this world.

Has it never occurred to the citizen's band campaigner to stop campaigning for such a band and start campaigning for a novice amateur band. Here are my ideas for such a band:—

- A simpler version of the R.A.E. to be taken at home with the help of text books. Most of the questions would be on licensing conditions and transmitter interference.
- 2. A successful applicant will be given a call sign. Possibly GN then a number.

3. A log to be kept of all contacts.

- 4. Power output to be limited to about 10 watts with no repeaters. All emissions to be f.m. only, no s.s.b.
- 5. The band allocated to be from 144.5 to 145.0MHz (a dead part of 2m in my opinion), and to be split up into 20 simplex channels, 25kHz apart.
- An emergency channel for climbers and hikers, i.e. channel 1. A licence would be available for a few pounds.

7. Licence to be paid yearly of about £7.

The above ideas are the rough foundations of a novices' amateur band and should be treated as such. If such a band is ever introduced it should never be called a citizen's band or advertised as such.

J. S. Goodier Stockport

Pen-Pal

Sir: I am seeking a pen-pal, my work is in automationresearch and development. My hobby is digital electronics and I would like to correspond and perhaps exchange technical literature and periodicals with anyone who has similar interests.

> Mr. Z. Kalab 79804, Urice 369, Okr, Prostejov Czechoslovakia

Ideas

Sir: I think the recently introduced "Blob Board" series of circuit boards are even better than sliced bread and much more easily solderable! I use mainly the ZB1C range, which accommodate various different combinations of (up to) 16-pin DIL devices, for various logic applications.

In this usage, I've found that lots of the pins have to be connected to positive or negative supply rails, and, frequently, to each other. It greatly simplifies wiring, and leaves much more room for other components, if such connections are made using conductive paint rather than wire jumpers. Crossovers are not possible, of course, but a bit of forethought can minimise the need for these.

I doubt if the same technique is possible using Veroboard—but, then, the Blob Boards are much more convenient anyway!

R. T. Third Fraserburgh

Sir: I was interested in your Audio Filter described in the May 1978 issue. However there is a simpler way of getting a similar effect if you have on hand an old fashioned a.f. transformer as used in valve sets of the 1920s and '30s. These had a primary inductance that tuned to around lkHz with a capacitor of about $0.001\mu F$. By connecting this capacitor across the primary and also parallel feeding with a similar series value, and tuning the secondary with a pre-set of suitable value a very efficient narrow-band filter is produced. I used this with valves very satisfactorily and an added feature is that if a volume control of some 1 megohm is also connected across the secondary, this gives a variable bandwidth according to the signal being handled. A similar effect could probably be obtained using an f.e.t.

The only problem likely to be encountered, is that if connected too early in the amplifier there may be hum pick-up.

K. A. Smith Ross-on-Wye

Data

Sir: I have recently obtained an "Audio Frequency Response Curve Tracer, Model 1900" manufactured by Industrial Electronics of London WC1. The serial number is 544.

If any other of your readers have any information concerning the maintenance and use of this equipment, that I could photocopy and return. I would be grateful if they could send it to me.

G. H. Honigman 34 Silverdale Road Gatley, Cheadle Cheshire SK8 4QS

Sir: I would like to get in touch with any reader who has built the 'Seekit' metal locator, published in the May and June 1977 issues of *Practical Wireless*.

J. Hinde 12A Station Road East Horsley Leatherhead Surrey

PRODUCTION LINES alan martin

Nice pair

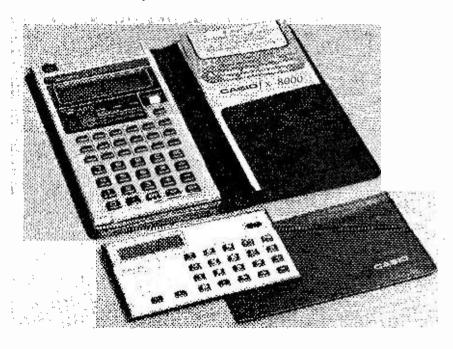
Just received from Casio, two scientific calculators which live up to the Casio reputation for quality.

First, the fx-8000 a pocket calculator measuring 145 \times 70 \times 8mm. The fx-8000 boasts 28 separate functions which include all the normal scientific requirements, plus two stopwatch and two timer facilities.

Second, the Mini card fx-48 which possesses most of the advantages of the fx-8000 less the stopwatch and timer features. This truly biscuit-sized

calculator measures only 90 imes 55 imes 4mm with a well spaced easy-to-operate keyboard.

Both the calculators are presented in smart wallets with full operating instructions, and are available from Tempus at discount prices, which include VAT and p&p, (the RRP is shown in parentheses) the fx-8000 £29.95 (£35.95) and the Mini card fx-48 £19.95 (£24.95). Tempus, Dept. P.W., 19|21 Fitzroy Street, Cambridge CB1 1 EH. Tel: 0223 312866.



Stick with it

Two new products from Loctite (UK) Ltd will be of interest to the home constructor and handyman. Loctite Handy Strip is a plastic, putty-like substance based on epoxy resin, and can be used to fill, bond or seal almost all materials. Handy Strip comes in a 10 inch strip, part blue, part white. Just tear off the amount required, knead it until it becomes a uniform white in colour. Once mixed it remains workable for 2 hours and

sets hard within 24 hours. Ideal for use on items such as aerial arrays.

Loctite Glass Bond is a clear onepart adhesive for bonding glass to glass or glass to metal. It is cured by by the ultraviolet radiation which is present in natural daylight—within 10 seconds in strong sunlight, about 1—2 minutes on a cloudy day.

Both products have been used with success by PW staff members, and are available from hardware and DIY stores.

Airlite 62 Headset

This headset has been adopted as standard equipment by over 50 international airlines and many of the world's leading aircraft manufacturers. It is also used extensively by British and overseas armed forces for airborne and ground communications, in addition to satisfying requirements in the hovercraft, air traffic control, flight simulator, broadcast, oil and gas industries.

A variety of noise-cancelling microphone capsules and earpieces to cater for all applications can be supplied and the headset may be terminated with many different types of connector. Rugged in construction, it is fully type-approved by the F.A.A. and A.R.B. to WR603.

Price varies according to type and quantity, but for a single unit would be typically £50-60. The headset is designed and distributed by Clement-Clarke International Ltd., Airmed House, Edinburgh Way, Harlow, Essex. Tel: 0279 24331, Telex 81338.



Frequency Shift

Those worried by the problem of losing their favourite programmes on Radio 4 when it moves to the long waves in November can draw comfort from a small unit called the Ambitune. This takes the BBC's 200kHz (1500m) long wave channel and converts it to around 900kHz on the medium wave band, reradiating it so that it can be picked up on your medium wave receiver's ferrite rod aerial. It is **not** suitable for use with car radios. Tests we have made around the Bournemouth area have proved very satisfactory.

Measuring just 85mm square by 25mm thick, the Ambitune is powered by a single PP3 or similar type of 9 volt battery. Using the MN1604 manganese alkaline equivalent, a battery life of some 700 to 900 hours is claimed.

The Ambitune costs £6 including post, packing and VAT, and is available from Ambit International 2 Gresham Road, Brentwood, Essex CM14 4HN.



not been proved by us, and we cannot therefore guarantee their effectiveness. They should at least provide a basis for experimentation. Why not send us your idea? If it is published, you will receive payment

according to its merits. Articles submitted should follow the usual style of PW in circuit diagrams and the use of abbreviations. Diagrams should be clearly drawn on separate sheets, not included in the text.

Each idea should be accompanied by a declaration that it is the original work of the person submitting it, and that it has not been accepted for publication elsewhere.

SHORT-PULSE GATE

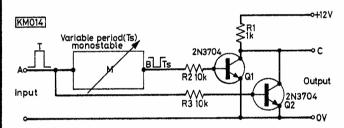


Fig. 1: The circuit diagram

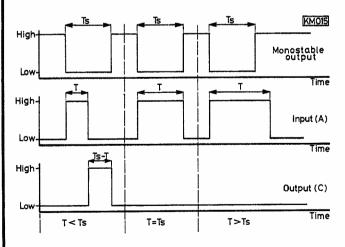


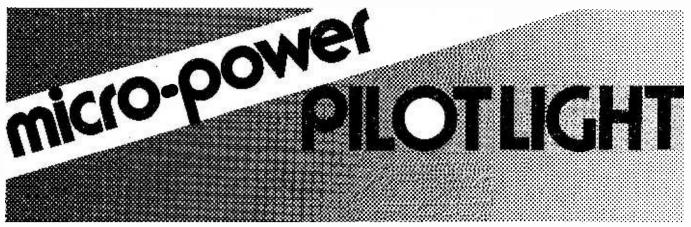
Fig. 2: Input and output waveforms

Considering the circuit of Fig. 1, with the input (A) at ground potential (low), and the output of monostable (M) at +12V (high), Q1 is turned on, and output (C) will be low. Since Q2 is turned off by the low applied to its base, it will not have any effect on the output as the "on" state of Q1 over-rides it. If a positive-going pulse of period T is applied to the input, Q2 will turn on, and the variable period (Ts) monostable will trigger from high to low—this state being applied to the base of Q1, turning it off. As Q1 is off and Q2 is on, the output remains low.

In the case when T is equal to Ts, after a period of T has elapsed, A will return to ground potential turning Q2 off and C will then go high as both O1 and O2 are off. After a further period of Ts=T has elapsed, the monostable will revert to its original condition; Q1 will turn on and C will go low. In this way, an output pulse of Ts-T is realised.

This circuit was developed to enable a system to react to pulses of 0.5s and ignore pulses of a greater length. The monostable type is not specified as it will be related to the minimum length of pulse to be registered.

> T. Austin, Southampton, Hants.



R.A.PENFOLD

Small battery-operated items of equipment rarely incorporate a pilot light, due to the increased demand for power this involves. Modern I.e.d. indicators have changed the situation, as these will give a bright display from a current of only about 20mA, and will give a visible glow under normal lighting conditions. An even lower current consumption can be achieved by storing a small electrical charge and using it to briefly illuminate an I.e.d. In this way the I.e.d. can be fully illuminated for brief periods, at about one second intervals and at currents in the μ A range.

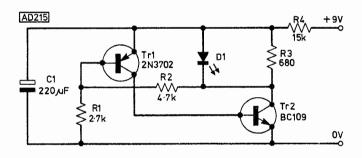


Fig. 1: Circuit diagram of the Micro-Power Pilot Light

A device of this type can be built very cheaply, and is easily miniaturised. Fig. 1. shows the circuit diagram. Here, when the supply is connected, C1 will charge exponentially via R4. When the charge across C1 reaches about 2V, a sufficiently large potential will be produced across the base-emitter junction of Tr1 by the divider action of R1, R2 and R3, for Tr1 to begin to turn on. This will cause a current to flow via its collector into the base circuit of Tr2, causing Tr2 to begin to turn on.

A regenerative action will then take place as Tr1 receives further base current via R2 from Tr2 collector. Tr2 will then receive an increased base current via the collector of Tr1. This will result in Tr2 rapidly turning hard on, causing C1 to be largely discharged through the l.e.d. resulting in it producing a brief flash. When C1 has partially discharged, insufficient circuit potentials will be available to hold Tr2 on, and a regenerative action will again occur. This time it will be the exact opposite of the original action, and will end with both Tr1 and Tr2 turned off. C1 will then begin to charge again, and this process will continue for as long as the supply is connected. With the circuit values shown a flash from the I.e.d. occurs every second or so, the period between flashes depending on the exact value of C1. The average current consumption of the prototype unit is about 450 uA.

\star components

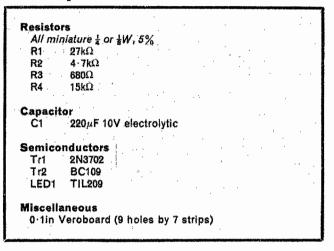
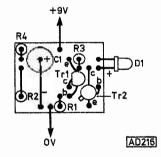


Fig. 2: Component layout on a small piece of Veroboard



The unit is constructed on a 0·1in Veroboard panel having 9 holes by 7 copper strips, and this gives the finished article dimensions of only about $23 \times 18 \times 23$ mm. The component layout of the device is shown in Fig. 2. There are no breaks in any of the copper strips.

The leadout wires of LED1 are not taken through the holes in the Veroboard, but are conveniently soldered direct to the copper strips on the underside of the panel, as shown in Fig. 2. This is advisable as many l.e.d.s have thick leadouts which will not go through the holes in the Veroboard. In fact, it is an advantage to use an l.e.d. having heavy gauge leadouts, as when the finished unit is mounted in the main equipment, LED1 is fitted into its panel clip, and the component panel is then rigidly mounted on its leadout wires.

As the unit is so small, it should be possible to find enough space to fix it into almost any existing equipment.

N.B. MATTEY

www.orne Music Centre

PART4 Cassette & A.M. Units + Full System Wiring

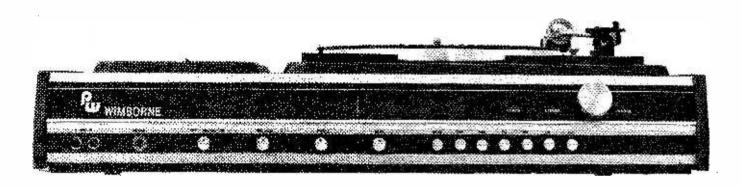


Table 1

Performance Details, A.M. Receiver

Typical Ratings:

S/N Ratio 55dB

Sensitivity 200µV (worst case)

THD 0.8%

Output 200mV approx

AGC FOM 75dB

A.M. Receiver Unit

While the limited dynamic range of the a.m. broadcast bands relegates the system to second place behind f.m. stereo, the extension of local radio and the move to medium wave of several national stations in November makes an a.m. receiver somewhat more attractive.

A central problem involved in designing an effective medium and long wave receiver is to achieve the sensitivity to resolve distant signals, and the selectivity needed to make evening listening (when a good deal of station overlap and fading occurs) a practical possibility. This paradoxical situation, that of wider range, but a more crowded band, can to some extent be overcome by increasing the sensitivity of the "front end" to the level where only a very short aerial is needed to maintain a good s/noise ratio. By coupling this to an oscillator and i.f. amplifier circuit of "tight" selectivity and superior a.g.c. performance, it is possible to achieve a well defined result, as shown by the table of performance figures.

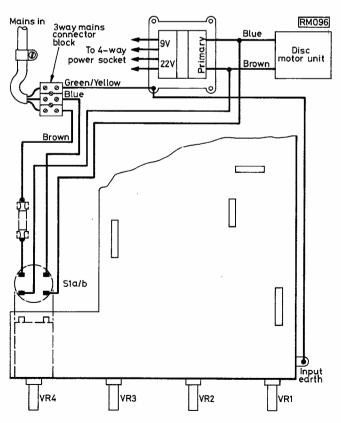


Fig. 1: Mains input cable and transformer details, plus general system wiring

The Basic Circuit

With the above aims in view, the excellent qualities of the HA1197 a.m. "chip" were utilised. The circuit is fairly conventional except that aerial (r.f.) transformers were chosen for the input stage, rather than the usual m.w./l.w. ferrite rod which necessitates some method of "swinging" the rod for maximum signal due to its directional properties. Further, direct coupling to an aerial means that a signal can be "brought in" easily when the unit is being used in say, a building of ferro-concrete where reception is likely to be impaired.

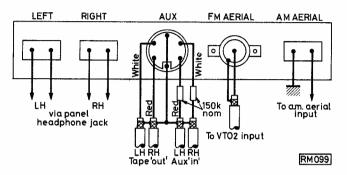
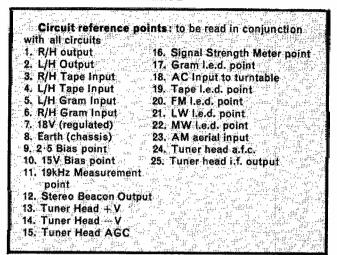


Fig. 2: Connections to the rear panel accessory sockets

Both the r.f. stage, in which the active element is the BF256, and the oscillator circuitry (L12 and associated components) are varicap tuned, in line with the f.m. receiver. Sensitivity is controlled by VR6, and the HA1197 amplifies and delivers the demodulated audio signal through the correction network R51, C81, L13 and R52.

Table 2



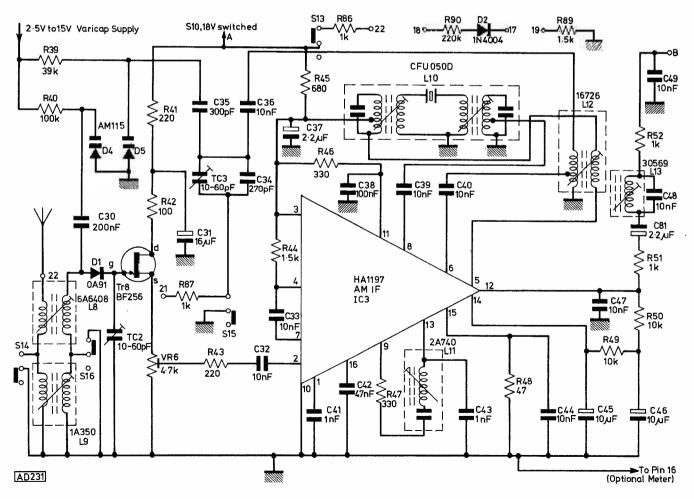


Fig. 3: Circuit diagram of the complete a.m. receiver; Tr8 is shown as Tr12 on the layout diagram shown in part 3 (Nov.)

★ con	npon	ents
Resistors	F0/	
±W carbon fil 47'Ω	m 5% - 3	R7, 37, 48
100 Ω	ž	R42, 67
150 Ω	1	R8
220 Ω	2	R41, 43
. 330 Ω	8	R4, 11, 14, 15, 16, 29
470 Ω 680 Ω	4	R19, 72, 77, 83 R38, 45
1kΩ	11	R1, 2, 9, 10, 25, 51, 52, 68, 73, 86, 87
1 · 5k Ω	2	R35, 44
2+2kΩ	2	R6, 34
2 7kΩ 3 3kΩ	1 3	R22 R36, 75, 81
4.7kΩ	. 4	R23, 33, 69, 70
🦠 8 2kΩ	* 1	R24
10kΩ	9	R12, 13, 17, 49, 50, 76, 79, 82, 85
15k Ω ≯ 18k Ω	8 1	R3, 5, 18, 21, 28, 30, 31, 32
22k Ω		R20
39k Ω	1	R39
47k Ω	1 2	R78, 84
100k Ω *470k Ω	3 2	R40, 74, 80
3.00		R26, 27
Potentiome 4·7Ω	iers 3	VR1, 5, 6 (miniature pre-set)
100kΩ''	Ĭ	VR3 (miniature pre-set)
100k Ω	¥.1≅	VR4 (linear pot)
470k-Ω	1	VR2 (miniature pre-set)
Capacitors		
Silvered mid	a .	
56pF 100pF	4	C25 C22, 23, 24, 80
270pF	1	C22, 26, 24, 80
300pF	1,	C35
470pF	a) 1 1	C65
Ceramic Dis	e 2	C41, 43
10nF	21	C1, 2, 4, 5, 6, 7, 8, 11, 12, 13, 18, 21,
		32, 33, 36, 39, 40, 44, 47, 48, 49
Polycarbona	ite 160V	CQ 10 81
22nF 47nF	o illesii	C9, 10, 61 C42
100nF	4	C3, 14, 29, 38
200nF	4	C30
220nF	2	C64, 67 C19, 66
470nF ₹Polystyrene	2	C19, 66
1nF	1	
2·2nF	3	C70, 71, 72
3 3nF	2	C63, 73
Polyester 2.2nF	4	C62
Electrolytic		
16V	病 : 若	12年4月8月1日建設
10µF	4	C17, 20, 45, 46
16µF	1	C31
25V 100μF	9	C31, 76
1000 µF	1	C27
63V		The second secon
2.50		
- 2·2μF	5	C26, 37, 60, 79, 81
- 2·2μF 100μF	5	
2·2μF 100μF Tantalum Be	5 1 ead 35V	C26, 37, 60, 79, 81 C28
2·2μF 160μF Tantalum Be • 0·47μF 2·2μF	5 1 ead 35V 1 3	C26, 37, 60, 79, 81 C28 C15 — C16, 74, 75
2·2μF 100μF Täntalum Be • 0·47μF 2·2μF 10μF	5 1 ea <i>d 35V</i>	C26, 37, 60, 79, 81 C28
2·2µF 100µF Tantalum Be 10·47µF 2·2µF 10µF Trimmers	5 1 ead 35V 1 3 2	C26, 37, 60, 79, 81 C28 C15 C16, 74, 75 C77, 78
2 · 2µF 100µF Tantalum Bo • 0 · 47µF 2 · 2µF 10µF Trimmers 10 · 60pF	5 1 ead 35V 1 3 2	C26, 37, 60, 79, 81 C28 C15 — C16, 74, 75
2·2µF 100µF Tantalum Bi 10·47µF 2·2µF 10µF Trimmers 10-60pF Integrated C	5 1 ead 35V 1 3 2 3 ircuits	C26, 37, 60, 79, 81 C28 C15 — C16, 74, 75 C77, 78 TC1, 2, 3
2 · 2µF 100µF Tantalum Bo • 0 · 47µF 2 · 2µF 10µF Trimmers 10 · 60pF	5 1 ead 35V 1 3 2	C26, 37, 60, 79, 81 C28 C15 = C16, 74, 75 C77, 78 TC1, 2, 3

Transistors				# 12	
BC148	1	Tr5	1000		
BC238c	3	Tr3, 6	7	1 1	
BC327	1.	Tr4		HE HE E	
BF254	2	Tr1, 2		aromali 📖	
BF256	100	Tr8		a Jefferi	
Diodes					
OA91		1 D1			
13V 100mW	Zener	1 ZD2		1.0	
AM115	10.7	2 D4, 5		1873	
L3 TKA L4, L6 CLN L5, L7 CLN	S30569Z	ት(Toko)	L11 L12	CFU050D 2A740 16726 30569	>(Toko
Miscellaneou	.				
F.M. Tuner	Module	VTO2 (F	Reed	Hampton)	S1-S1
7-button int	erlocked	switch-be	ank (15mm pitcl	h) (Ree
Hampton of	Armon	Products	, We	mbley, Mi	ddx). F
F2 Ceramic I					
d.i.l. socket.					
tors (2 off)	4-way	connector	5 (2	off). Cass	ette un

Construction and Setting Up

The component layout, shown complete with the f.m. section in our November issue, should be adhered to if problems of instability are to be avoided. Simi-

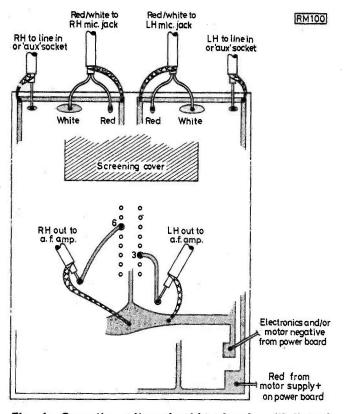
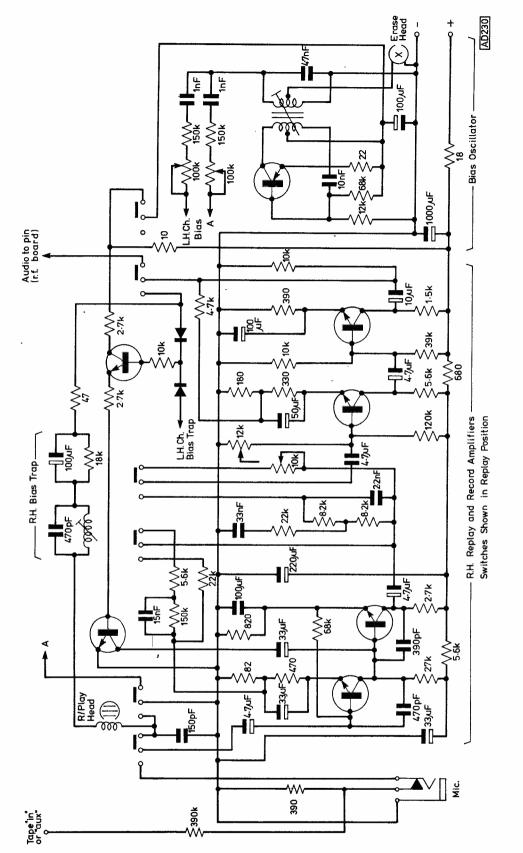


Fig. 4: Cassette unit underside showing "in" and "out" points on each p.c.b.



larly, the sensitivity control (VR6) should not be advanced too far for similar reasons. When setting up, TC2 is used to peak the high frequency end of the m.w. band (194 metres or about 1600kHz), and the cores of L8 and L9 set for maximum output at the low frequency end of each band (530m on m.w. and 150m on l.w.). If no signal generator is available

for this operation, it can be carried out by ear, or in conjunction with an output meter.

Trimmer TC3 is set to produce accurate oscillator tracking across the m.w. band. An additional feature (optional) is the inclusion of l.e.d. points for the display of medium or long wave function in the "on" state.

Fig. 5: The circuit diagram of one complete cassette record/play amplifier. Some oddities have crept in: two electrolytic capacitors are shown unpolarised, a 100 μF (which should have - to chassis) and a 4 $7\mu F$ (+ connection to base of appropriate transistor), a 12 $k\Omega$ fixed

resistor is shown with an unnecessary arrow, and the audio signal "out" (top right) should go to pin 3, r.f. board. This circuit is intended

only as a rough guide for connection and servicing purposes

Aerial Length

In view of the high sensitivity of the r.f. stage, only a short aerial should be used (except in areas of low signal strength), and the prototype performed very well on a 4 metre length of mains cable. Very long aerials may, in some areas, induce i.f. breakthrough, with consequent c.w. (Morse code) interference. However, there is unfortunately no way of eliminating the timebase "whine" from 405 line tv receivers, so the shorter the aerial the better.

Cassette Unit Electronics

It will be noted that no component references are given for the amplifier, and this is due to the fact that the unit is supplied complete, and with input/ output leads wired in. It is not really recommended that the constructor wires up an individual unit since the connecting points on the cassette p.c.b. are minute, but a plan view is shown for those who wish to attempt this. Similarly, a line mains fuse may be fitted in series with the "live" input lead to S1.

General Notes

Cassette Unit: check that the supply rail does not exceed 12V for the motor unit, and 10-12V for the electronics. Where both are fed from the 12V supply, start-up motor "plop" can be eliminated by isolating via a 47Ω (nominal) resistor fitted in series with + connection junction with C301 (1500 μ F). The tag on the component side of the board is then removed and directly linked to +12V on power panel.

> The slide switch for CrO2 can be removed if not required (Reed-Hampton supplied unit only).

Safety Hints:

all chassis and metal parts must be bonded to "earth" line at some point. Before switching on, check with a multimeter that resistance (" $\Omega \times 100$ " range) is virtually infinite, so as to avoid possibly lethal wiring errors. The $150k\Omega$ resistors shown in series with the "Aux in" connections are nominal only, and should be increased where high signal inputs are considered.

Loudspeakers

Although this is technically the final instalment of the "Wimborne", details will appear in the new year of a suitable design for loudspeakers.



KINDLY NOTE!

"Gillingham" SW Receiver Frequency Readout.

IC1 should be type SN7404. (Hex Inverter.)

ZL SPECIAL 2m Beam (November (1978)

We very much regret that on the drawing Fig. 2. (p 23) the dimensions of the rear and front driven elements were omitted. These should be 965mm (reer) and 927mm (Front). We apologise to our readers and the Author for this unfortunate oversight.

STD Charge Timer November 1978:

B15, 1-2Mt) was omitted from the p.c.b. Jayout Fig. 3. It should be connected to the next \$1. contact to that carrying R14 and its other end connected to the common point of the other tuning resistors.

NEW BOOKS

A PRACTICAL INTRODUCTION TO ELECTRONIC CIRCUITS by Martin Hartley Jones. Cambridge University Press, September 1977, Hard-back £9.50, Paper-back £3.95.

The straightforward presentation of technical information at any level is a technique which the initiated finds a simple task, but to make this information at once dynamic and attractive is the preserve of the sensitive writer or engineer. Martin Hartley Jones proves that he is both of these with the publication of this book.

As an example of the originality of approach, the author begins with the vital process of amplification, and unlike many who forget or ignore the value of analogy, provides the excellent example of the original Morse relay, demonstrating how a large output can be controlled by a small input. This leads into considerations of gain, and while some may consider this to be "cart before horse", it seems rational to me to look at Darlington pairs and other circuits designed to achieve gain, before a consideration of the physical processes begins. After all, gain is a vital factor in amplification, to state the obvious.

This is not to say that the general succession of basic approaches is ignored. From voltage amplifiers, the course of the instruction pursues a productive line based upon essentials of theory and practice, from comparisons of f.e.t. and valve techniques, through feedback and impedance matching, to the inevitable final chapters on truth tables and binary counting. The difference lies in some of the intervening material. At long last the differential amplifier is included, along with sections on pulse clipping, thyristors and triacs, inverting amplifiers, and active filters. The work is sound, and the layout of text and diagrams tends to lead the eye and brain rather than push it un-

One point of criticism-how practical is "Practical"? Although many pin-out details, and valve base connection details are shown, there is little consideration of actual physical layout-what should we do about "earth" loops? Nevertheless, the information is there, and very attractively presented. This book must be good value.

Ted Parratt

- OTLINIES

A REVIEW OF RECENT DEVELOPMENTS

In general, the author does not have any more information on products than appears in the article.

Soft Errors

One of the areas in electronics where smaller and smaller has been the key word is memories. News from researchers has brought the startling realisation that packing things into tiny areas can breed problems not previously considered. In the case of dynamic random access memories, a problem occurred called "soft errors". These are errors which can be corrected by simply repeating the operation, but they are a problem.

The 4096 RAM had these worries and now the newer 16K RAMS are causing researchers to examine the problems of soft errors quite carefully. And they've come up with some startling conclusions. One is that these soft errors are caused by alpha particle radiation generated from within the i.c. or, more specifically, from the materials which are used in the packaging. Apparently it's the teeny-weeniest amount of radioactivity which is the source of the troubles-they think. According to the eggheads amongst them, researchers argue that when the alpha particle whizzes through the chip atoms it finally comes to rest, Its energy is absorbed (which is why it stops) and the result is the production of 1-4 million electron hole pairs in a tiny 25µm length. (I wonder whose calculator they used to work that out with?) It's this which is apparently causing all the problems. The answers are not simple and work is currently proceeding in many different directions but all with the same end objective. I'll report more on this fascinating battle as and when news comes in. Meanwhile, if you do happen to wake up one morning with 1.4 million electron hole pairs on your pillow and that old "soft error feeling" at least you'll know what caused them!

CMOS 555

Those who really like to be with it in terms of the latest i.c.s will be pleased to hear that a c.m.o.s. version of the 555 timer looks like being a reality. Magic numbers to look for are ICM 7555. Some technical buffs are mumbling about

currents of only 85µA (160µA for the 7556) plus advantages in timing applications because higher resistance elements will be possible. Batteries should last for a very long time with these chips. Writers of books with such titles as "Five Hundred Million Circuits Using the 555" are doubtless busy rewording and rewriting current circuitry to take commercial advantage of these devices.

Plastic Keys

Burglars in hotels are going to be in for a very hard time if a new electronic lock manages to get off the ground. While there are already many locks of a kind on the market, they usually have signals going to and/or from them via wiring of some sort. In the case of hotels this is often the telephone wiring or mains etc. It's now thought that todays' sophisticated thief might be able to 'tap' into this wiring and open doors, hence the need for a different kind of lock. The new one, not yet on the market commercially, has a really unique feature-no wires. The whole thing is built into the door and runs off. its own batteries.

The key looks like taking the form of a kind of credit card which has a coding put on it at the reception desk. It's a 28-bit code, too, and that means an awful lot of possibilities before you might guess the right one. The door mechanism has a microprocessor and memory so it's virtually a miniature computer built into the door. The guest inserts the card or "key" and the computer will check the number on the card against the number held in its memory; if they tally the door will open.

Then someone thought of a weakness. Perhaps the cards and their codes might be duplicated. So, a "guest" might use a room, copy the key, then return some days later when it was occupied by someone else, and commit a burglary.

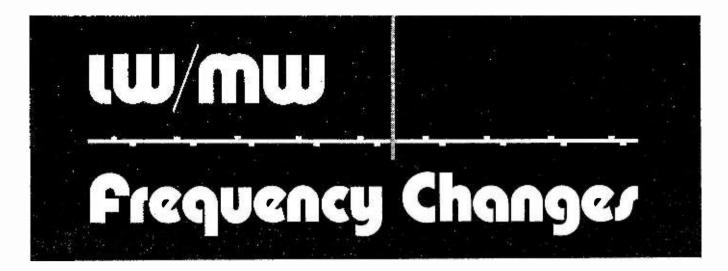
To avoid this, the key carries two 28-bit code capabilities. When a guest checks in, his key carries the old or previous code. But the main desk has put another "new" code into the other 28-bit capability. This new code is generated completely randomly.

When the new guest puts his key into the lock the new code does not tally (because the old code is still in the door lock's memory). Immediately, the door will generate a recheck of the other 28-bit code. This, of course, it recognises. Upon receipt of this, the door will erase the old code from its memory, and reprogram itself with the new code—and open the door. Thus each new guest effectively reprograms his/her door to a new secure code. Wonder what they'll think up for bicycles?

Longer Video

Video recorders seem to be catching on; even the TV rental showrooms have them. Because of the enormous potential market seen in video recording, many companies are competing and nowhere more keenly than in the video cassette field. The early cassettes for this purpose did not last very long and this was a marketing difficulty. However, the latest broadside in the cassette war is from a German manufacturer who is launching a 4hour video cassette. Not so long ago a Dutch company launched a 3-hour cassette. Better to come (for the consumer), a 5-hour version is on the way later this year, while an 8-hour video cassette is in development. If this goes on you'll soon be able to have the whole of Wimbledon in a single package. Then heaven help any visitor who shouts, "Anyone for tennis".





On 23 November, 1978, a new international frequency agreement comes into force. This provides for a considerable increase in the number and power of transmitters in Europe. The BBC is reorganising its arrangements for broadcasting Radios 1, 2, 3 and 4 on medium wave (m.f.) and long wave (l.f.) from that date.

The main object of making the changes has been to make the most effective use of the frequencies which are available, and to alleviate so far as possible the increased interference which is expected to affect many of them. A number of additional transmitters are being installed and listeners should not assume that their present reception of a particular frequency is necessarily any indication of the reception it will provide under the new plan. Full details of the new channels are given in the tables, but the changes and their expected effect are summarised below.

Radio 1 will be transmitted on 1053 and 1089kHz (285 and 275 metres) instead of 1214kHz (247m). By using two medium frequencies instead of one, Radio 1 will have much better coverage, both by day and night. The low-power transmission on 1485kHz (202m) at Bournemouth will be retained.

Radio 2 will be transmitted on 693 and 909kHz (433 and 330m) m.f. instead of 200kHz (1500m) l.f. and 1484kHz (202m) m.f. (Scotland). With two medium frequencies instead of the present l.f. service, Radio 2 will be easier to receive in many areas where the present long-wave service is poor. On the other hand, some areas will suffer increased interference after dark, and here listeners should use v.h.f. whenever possible.

Radio 3 will be transmitted on 1215kHz (247m) instead of 647kHz (464m). There will also be a low-power transmission on 1197kHz (251m) at Cambridge. Radio 3 should be available on medium wave in all the most populous parts of the country, with about the same coverage as for Radio 1 at present. Listeners who cannot receive Radio 3 on m.f. are advised to use v.h.f.

Radio 4 will be transmitted on 200kHz (1500m) l.f. instead of 692, 908 and 1052kHz (434, 330 and 285m) m.f. There will, in addition, be medium-wave transmissions on 603kHz (498m) for Tyneside; 720kHz (417m) for Northern Ireland; 1449kHz (207m) for Aberdeen; and 1485kHz (202m) for Carlisle.

Using l.f. and a number of m.f. channels for local coverage, Radio 4 should be receivable almost anywhere in the UK. In Scotland, Wales and Northern Ireland it will provide an alternative to Radio Scotland, Radio Wales and Radio Ulster. In England, existing Radio 4 services on v.h.f. will continue, providing local news and weather forecasts as at present.

Radio 4 in Northern Ireland will continue to be transmitted on 720kHz/417m. This service will be transferred to a new site with higher power, and should be available throughout most of the province. In some areas an alternative service will be available on l.f.

Radio 4 South West. From 23 November the frequencies of three Radio 4 South West m.f. transmitters will change. Barnstaple will change from 683kHz/439m to 801kHz/375m; Plymouth from 1457kHz/206m to 855kHz/351m; and Torquay from 854kHz/351m to 1458kHz/206m.

With the exception of brief local news and weather reports and the early morning magazine programme Morning Sou'West, the five Radio 4 South West m.f. transmitters—Barnstaple, Exeter (990kHz/303m), Plymouth, Redruth (756kHz/397m), and Torquay—will carry the same programmes as the Radio 4 l.f. service.

Shipping forecasts. From 23 November both the main shipping forecasts and the forecast for inshore waters will be broadcast on Radio 4's long- and medium-wave



Practical Wireless, December 1978

,	Frequency	Wavelength	Power		Frequency	Wavelength	Powe
	kHz	Metres	kW		kHz	Metres	kW
Radio 1				Radio 4			
Barnstaple	1053	285	1	UK Service			
Barrow	1053	285	1	Burghead	200	1500	50
lexhill	1053	285	2	Carlisle	1485	202	1
Sournemouth	1485	202	2	Droitwich	200	1500	400
righton	1053	285	2	Lisnagarvey	720	417	10
Prookmans Park	1089	275	150	Londonderry	720	417	0.25
Jurghead	1053	285	20	Newcastle	603	498	2
roitwich	1053	285	150	Redmoss	1449	207	2
undee	1053	285	1	Westerglen	200	1500	50
areham	1033	275	i		200		
olkestone	1053	285	i	South West			
	1053	285	i	Barnstaple	801	375	2
luli	1089	275	10	Exeter	990	303	1
isnagarvey			10	Plymouth	855	351	i
ondonderry	1053	285				397	2
loorside Edge	1089	275	150	Redruth	756		
ostwick	1053	285	10	Torquay	1458	206	1
edmoss	1089	275	2				
edruth	1089	275	2	Radio Ulster	4044	004	,
tagshaw	1053	285	50	Lisnagarvey	1341	224	100
tart Point	1053	285	100	Londonderry	1341	224	0.25
'ywyn	1089	275	1				
Vashford	1089	275	50	Radio Scotland			
Vesterglen	1089	275	50	Burghead	810	370	100
Vhitehaven	1089	275	1	Dumfries	810	370	2
				Redmoss	810	370	5
tadio 2				Westerglen	810	370	100
			4				
arrow	693	433	1	Radio Wales			
exhill	693	433	1	Penmon	882	340	10
ournemouth	909	330	1	Tywyn	882	340	5
righton	693	433	1	Washford	882	340	70
rookmans Park	909	330	140	Wrexham	882	340	2
urghead	693	433	50	wrexitatii	002	340	2
levedon	909	330	20				
Proitwich	693	433	150				
xeter	693	433	1				
areham	909	330	1				
olkestone	693	433	i	1			
	909	330	0·5	ł			
iuernsey	909	330	1	1			
ersey	909	330	10				
isnagarvey	909	330	1	BBC LOCAL RADIO			
ondonderry			100		MEDIUM WAVE	VHF	
loorside Edge	909	330					Max. erp
lymouth	693	433	1	1	Metres kHz	kW MHz	kW Pol
ostwick	693	433	10	l			
ledmoss	693	433	1	Birmingham	206 1458	10 95.6	5·5 H
edruth	909	330	2	Blackburn			1.6
tagshaw	693	433	50	Brighton			1·6 S 0·5 F
orquay	909	330	1	Bristol	194 1548		5 F
Vesterglen	909	330	50	Carlisle (Main)			5 F
Vhitehaven	909	330	1			0.5	, r
				(relay)			5 F
tadio 3				Cleveland		1 96.6	5 F
				Derby (Main)	269 1116		5·5 S 0·01 V
righton	1215	247	1_	(relay)			
rookmans Park	1215	247	50	Humberside	202 1485		4·5 F
urghead	1215	247	20	Leeds	388 774	I I I I I	5.2
ambridge	1197	251	0.2	Leicester			0·3 S
roitwich	1215	247	30	London	206 1458		16·5 H
areham	1215	247	1	Manchester	206 1458		4·2 S
luli	1215	247	0.15	Medway			5·6 F
isnagarvey	1215	247	10	Merseyside		2 95.8	7·5 S 3·5 H 0·3 S 4·5 H 5·2 S
ondonderry	1215	247	0.25	Newcastle			3-5 F
loorside Edge	1215	247	50	Nottingham			0.3 S
	1215	247	2	Oxford			4·5 F
lewcastle		247	1	Sheffield (Main)			5·2 S
lymouth	1215				200 1000		0·03 F
ostwick	1215	247	1	(relay)	200 000		5 F
ledmoss	1215	247	2	Solent (Main)			υ F
ledruth	1215	247	2	(relay)		0.25	
ywyn	1215	247	0.5	Stoke-on-Trent	200 1503	0.5 96.1	2·5 H
	4045	247	60				
Vashford	1215 1215	247	40	H—Horize	ontal SSlant	VVertical	

transmitters. The late-night forecasts will be broadcast on v.h.f. also.

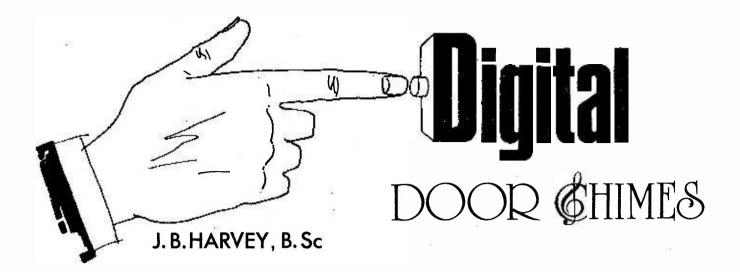
Local Radio. The majority of Local Radio stations will be unaffected by the changes. The exceptions are Radio Leeds, which will change from 1106kHz/271m to 774kHz/388m; Radio Leicester from 1594kHz/188m to 1584kHz/189m; and Radio Solent's service in Bournemouth which will change from 1594kHz/188m to 1359kHz/221m.

Receivers with pre-set station selection. In addition to the changes which have been described, all of the BBC's medium frequencies, both for the National services and for Local Radio, will be increased by a very small amount. These increases will be too small to be noticed on radios having continuous tuning (the great majority) but

receivers with preset (pushbutton) station selection in the m.f. band may require adjustment of the preset controls. This will apply to many car receivers.

VHF services. There are no changes to the BBC's v.h.f. transmissions except in Northern Ireland, where the present Radio 4 v.h.f. network will be transferred to Radio Ulster. Radio Ulster v.h.f. will, however, continue to carry all Schools, Open University and Further Education programmes and some Radio 4 programmes.

We are grateful to the BBC Engineering Information Department for their assistance in providing the information given here. If you require further advice or information, please write to: Radio Changes, BBC, Broadcasting House, London W1A 4WW.



Introduction

Being unimpressed with a simple door bell or chime the author decided to design a circuit that would generate the "Big Ben" sequence when a visitor called. Realising that one might grow tired of "Big Ben" a programmable version was developed, variations in diode linkages producing different tunes; the one in the author's home, which is described here, is currently programmed to generate the opening bars of "Colonel Bogey"!

The component cost is around £5, and the circuit is suitable for battery operation, drawing negligible current in the "standby" mode.

Circuit Description

The circuit can be considered in three sections: the sequence generator and the audio oscillators, designed around c.m.o.s. devices and linked by diodes to produce the tune required, and a simple power amplifier to drive one or more loudspeakers.

Oscillator Operation

Basic to the circuit is a two stage c.m.o.s. oscillator (see Fig. 2). This simple circuit requires only two gates, two resistors and a capacitor and operates as follows. When the waveform (1) at the output of inverter B is in a high or "1" state, capacitor C becomes positively charged. As a result the input to inverter A is high and its output is low or "0". Resistor R2 is returned to the output of inverter A to provide a path to ground for the capacitor to discharge. As long as the output of A is low, the output of B is high. As capacitor C discharges, however, the voltage at the junction of C and R2 approaches and passes through the switching point of inverter A. The output of A goes high, that of B goes low, and capacitor C charges negatively. R2 then provides a discharge path to the supply voltage, and C begins to charge to this voltage. Again the voltage at the junction of C and R2 passes through the transfer point of inverter A; at that instant the circuit again changes state, the output of A going low and of B high, and the cycle repeats.

The time to repeat one cycle is approximately 1.4CR2; the frequency can be made nearly independent of supply voltage and switching point variations by including a large resistor in series with the input

to inverter A: hence R1. The oscillator may be gated on and off by using one of the inputs to gate A as a control line, taking the line high to run, low to inhibit, and this is done in the chime circuit. Since the c.m.o.s. gates used cost around 5p each, the circuit is very economical; indeed it was cheaper to use five separate oscillators in the chime circuit than one oscillator with switchable frequency.

Chime Circuit Operation

When switch S1 is closed, the RS flip-flop comprising gates A3 and A4 is set, the Q output going high and \overline{Q} low (see Figs. 1 and 3). The reset line to the decade counters B & C is cleared, and the clock generator (E1 & E2) is enabled. Now the enable lines to each counter are taken to a second RS flip-flop (RS2); since one output is always high when the other is low, both counters cannot sequence at once, even though they are both clocked simultaneously. Initially, B is enabled and commences counting. On the 9th clock pulse RS2 is set, counter B is frozen and counter C takes up the count.

On the 17th clock pulse both RS flip-flops and counters are reset, and the clock is disabled.

For the sequence to repeat correctly the next time S1 is pressed it is necessary for RS2 to reset before RS1, since the reset drive pulse is taken from counter C, and this disappears when RS1, and hence the counters, are reset. Since both flip-flops are reset by the same drive pulse a race hazard situation exists; this is resolved by including a resistor R3 in the reset line to RS1. R3 in conjunction with the input capacitance of gate A3 gives rise to a small time constant, sufficient to delay the reset of RS1 by the required number of nanoseconds. Should the delay prove insufficient a small capacitor (10-100pF.) can be fitted (C2).

This reset pulse, and consequently the 17th clock pulse, are of short duration, comparable with the propagation delay of a c.m.o.s. gate (typically 25 nS), since in resetting everything in sight the reset pulse is itself eliminated.

Inspection of Fig. 3 shows that a sequence of sixteen discrete pulse outputs is available, each output being one clock pulse in duration; the other outputs of the decade counters are of longer or shorter duration, and so are unsuitable for the present purpose. These sixteen pulses are connected by programming diodes to

the enable lines of five audio oscillators, and it is the positioning of these diodes that determines the note sequence that will be generated. These oscillators are set to operate at suitable audio frequencies, adjustment being provided by VR1-5. The five outputs are isolated from each other by D1-5, and are taken to the input of a simple power amplifier.

Power Amplifier

This amplifier operates in the class D mode, the output being switched between supply and ground at a rate determined by the incoming signal. This has several advantages: there is no quiescent current, the load may be driven directly without the need for a large coupling capacitor, and large amounts of power may be switched into the load with little dissipation in the output transistors Tr2 and Tr3, limited only by the maximum collector current of these transistors (for BC140/BC160 $\rm I_{c}max$ is 1A); consequently no heatsinking is required and therefore the amplifier is very economical.

Other transistors may be used if BC140/BC160 are not readily available, provided that they have reasonable gain and current handling capability. The astute reader will realise that with the load coupled to the amplifier as shown, Tr3 does most of the work; Tr2 would be unnecessary for a purely resistive load, but for an inductive load such as a loudspeaker Tr2 provides an active pull-up and serves to square off the output waveform. D7 and D8 are included to restrict the possibility of breakdown in the output transistors when driving an inductive load.

Construction

The digital door chime may be assembled on veroboard, no special care in layout being necessary; however, a purpose-made printed circuit board is undoubtedly neater, and a suitable layout is shown in Fig. 4; Fig. 5 gives the component locations. If S1 were connected to the circuit via a very long length of wire, spurious pick-up could set off the chimes (although this has not happened on any of the units

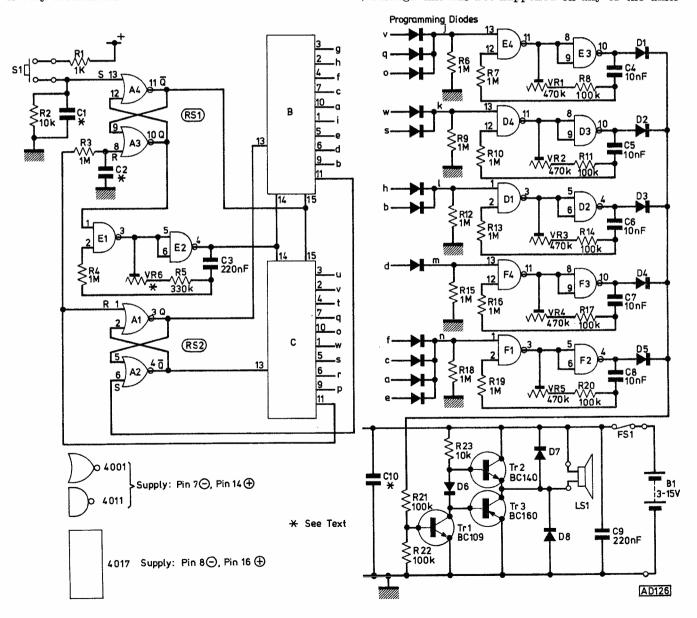


Fig. 1: The circuit diagram is easily divided into three separate sections, the sequence generator on the left, the audio oscillators and the audio amplifier

so far built); a 10nF capacitor (C1) across R2 will eliminate this hazard. C10 may be added for extra supply decoupling, although no problems have been experienced with the prototypes. VR6 may be added to vary the clock rate, and hence the speed at which the tune is played; if this facility is not required then the VR6 position should be linked across on the p.c.b. Finally a fuse has been included in the supply line to protect the power source in the event of a component failure.

Handling C.M.O.S.

Whatever method of construction is used it is necessary to handle the c.m.o.s. devices with care, to avoid damage by static discharge. Unless the constructor is experienced in the handling and soldering of these devices it is advisable to assemble the circuits using i.c. sockets, leaving the fitting of the devices until last. The chips are supplied either in a metal tube or mounted on conductive foam to prevent damage during transit, and they should be left there until they are transferred to the circuit. When handling the i.c.s, avoid working in a very dry atmosphere, wearing a nylon shirt or doing anything else likely to produce a build-up of static. It is a good idea to cover the working surface with a sheet of earthed aluminium foil and keep everything on that. Once in circuit, of course, the i.c.s are safe from further damage by static.

Operation

Unlike t.t.l., c.m.o.s. will operate from any supply in the range 3-15V; in addition the current drawn by c.m.o.s. when powered up but not switching is negligible. Since the power amplifier draws no quiescent current either, the digital door chime may be run off a small dry battery (e.g. PP9), the life of the battery approaching its shelf life, since current is only drawn when the chime is operating. (If you find this difficult to believe, connect a 50μ A meter in the supply lead—there is no deflection on "stand-by").

The current drawn when the unit is running depends almost entirely on the load, the circuit itself drawing around 1mA. The only limitation on load impedance is that the I_omax of the output transistors is not exceeded; e.g. if a 15V supply and a 15 ohm load is used, the peak load current will be 1A, and the r.m.s. power delivered to the load will be 3.75W,

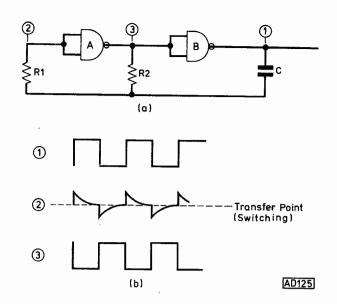


Fig. 2: The basic two stage c.m.o.s. oscillator

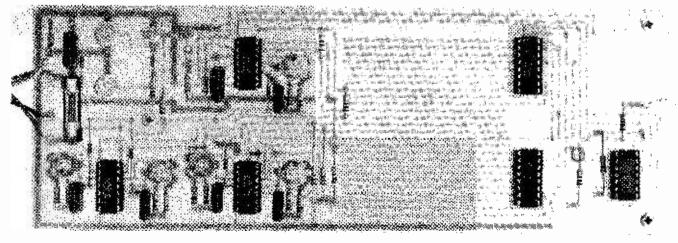
assuming a 1:1 mark-space ratio. Being driven by a square wave the loudspeaker signal is rich in harmonics, the note produced having a penetrating quality that is well suited to its application.

Setting Up

Plug in all the i.c.s and connect the unit to a power supply, with a current meter in the positive lead. There should be negligible current drawn when the circuit is not operating: any permanent quiescent current should be investigated. The five notes may be set up easily by pulling up each enable line (j-n) in turn to give a continuous tone and adjusting the associated preset.

To adjust	Link positive rail to
VR1	I.C.E Pin 13
VR2	I.C.D Pin 13
VR3	I.C.D Pin 1
VR4	I.C.F Pin 13
VR5	I.C.F Pin 1

Finally, close S1 to verify the operation of the entire circuit. The speed at which the tune is played may be adjusted by altering the value of R5 (or tweaking VR6 if fitted).



The prototype p.c.b. seen from the component side

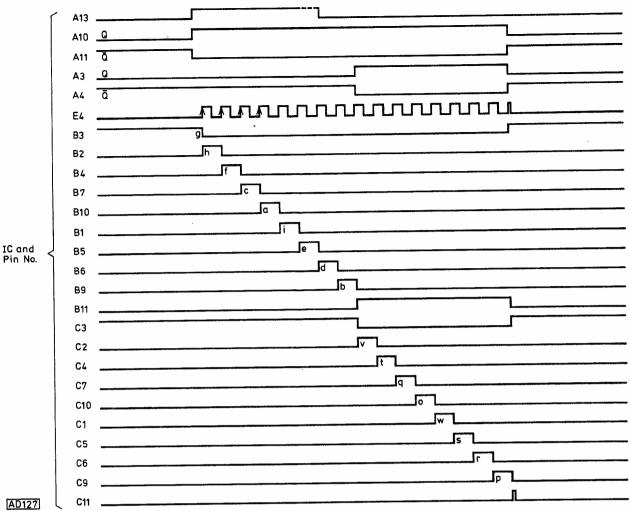
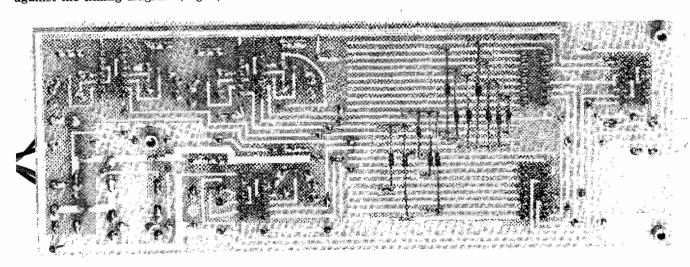


Fig. 3: Timing diagram showing the relationships of the various pulses

Faultfinding (e.g. decoding errors, wrong or missing notes) may be simplified by bridging C3 with a $2 \cdot 2\mu F$ capacitor; this will slow down the clock to 1Hz and allow the circuit operation to be checked at leisure against the timing diagram (Fig. 3) with a meter.

Touch Control

Advantage may be taken of the very high input impedance of c.m.o.s. devices to operate the chimes by touch control instead of a switch. Simply increase R1 to 100k and R2 to 10M, and replace S1 with a pair of touch contacts.



Copper track side of the p.c.b. showing positioning of the diodes

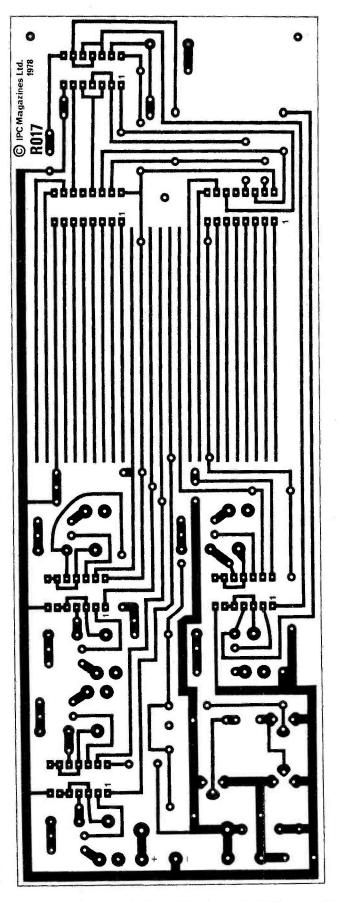
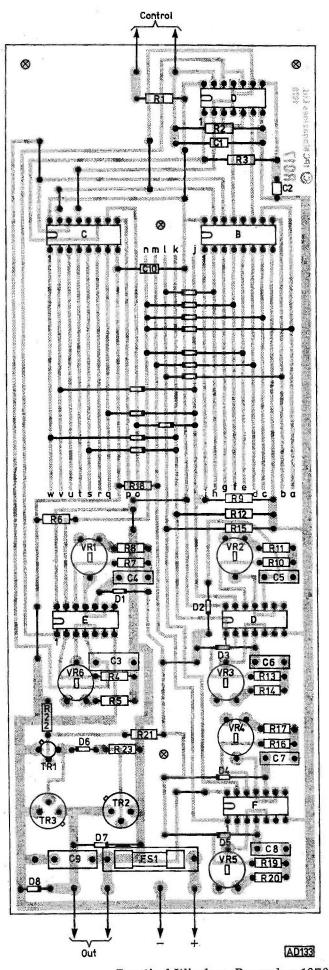
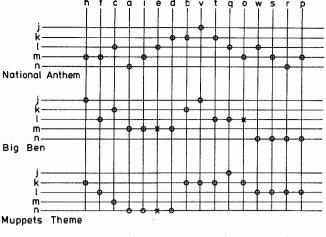


Fig. 4: Above, copper track layout of the p.c.b. (shown full size)
Fig. 5: Right, component layout



Practical Wireless, December 1978



o = Diode Present (Anode to h-p:Cathode to j-n.)
x = No Diode Fitted.

AD1261

Fig. 6: Programming for three sample tunes. This shows the positioning of the diodes on the matrix part of the p.c.b.

* components

Kesist	ors					
All ‡	watt 5%					
R1	1k	R10	1 M	R19	1 M	
, R2	10k	R11	100k	R20	100k	•
R3	1M	R12	1M	R21	100k	
R4	1M	R13	1M	R22	100k	
R5	330k	R14	100k			
R6	1M	R15	1M	:		
- R7	1M	R16	1M	٠.		,
R8	100k	R17	100k			, ,
R9	1M .	- R18	.1M	,	` `	
VR1-	5 all 470k	lin. pre	set		*	
	• • • • • • • • • • • • • • • • • • • •	·				. `
Capac		٠,			- >	
C1	see text	, ,		C6 10	1F 100V	polyeste
C2	see text		3.			polyeste
C3	220nf 100					polyeste
C4	10nF 100	v polye	ester			polyest
C5	. 10nF 100	V polye	ster	C10 se	e text	
	onductor	rs	`.'"			
semic	BC109		A 400	ı. IC	D 4011	
emic Tri			B 401		E 4011	.,`
Tri	DL.1411					
Trt Tr2	BC140 BC160	IC	C: 401	7 IC		100
Tr1 Tr2 Tr3	BC160	1C.	C 401	7 IC	, ,,,,,,	
Tr1 Tr2 Tr3			C 401	7 IC	, ,,,,,	s de s
Tr1 Tr2 Tr3 All d	BC160 lodes 1N4	148	C 401	7 IC		
Tr1 Tr2 Tr3 All d	BC160	148				connecto

Alternative tunes

The circuit as it stands provides sixteen time intervals and five notes, conveniently enabling the first four bars of any number of tunes to be programmed; several examples are shown in Fig. 6. Extra notes may be provided by adding further audio oscillators to the circuit (most economically added in pairs, since there are four Nand gates in each i.c.) and programming them as required; the outputs would be taken via isolating diodes to R21. Finally, really keen constructors can work out for themselves how to add further decade counters to extend the length of the chimes.

RECEIVER ADD-ON ACCESSORIES

Continued from page 25

In use, the object is to find the right amount of inductance, by changing the tapping point on the coil, and the correct amount of capacitance, the point of resonance being indicated by a sharp increase in signal strength. There will be many points at which the signal will peak but there will be a particular ratio of inductance and capacitance giving the maximum signal. Make a note of the tapping point on the coil and the tuning capacitor/s settings for future reference. Do this at the centre of each band of interest. It is worth while taking a little time to find the correct settings, so do not settle for the first peak found.

Stephen-James Ltd, 47 Warrington Road, Leigh, Lancs.

Multi Tuners, Mk1 1·8 to 30MHz, five aerial configurations. Mk2, similar plus m.w. band. Crystal Calibrator, 1MHz, 500kHz, 100kHz, 50kHz, 10kHz, 5kHz and 1kHz. Audio Bandpass Filter, eight switched bandwidths 80Hz to 2·5kHz. Peak and Notch Filter, between receiver and speaker/phones. Preselectors.

Amtest, 55 Vauxhall Street, Rainbow Hill, Worcester WR3 8PA.

Aerial Tuner AT2, 1.5 to 30MHz for end-fed aerials. RF Preselector PRS1, same range, up to 30dB gain. PRM for m.w. coverage to 1.6MHz. PRM Adaptor Unit, for coupling external aerials to internal ferrite rod aerial of receiver.

Cambridge Kits, 45(P) Old School Lane, Milton, Cambridge CB4 4BS.

LF Converter, 100/600kHz converted to 80m band. Tunable Audio Notch Filter, between speaker and receiver, 350 to 6000Hz. Crystal Calibrator 1MHz, 100kHz, 25kHz. All are kits.

G2DYM Aerials and Projects, Whiteball, Wellington, Somerset.

Aerial Matching Unit, designed to combat TV time-base QRM, untuned, wideband for 50Ω to balanced feeder from multi- or single-band dipole. Switch for Marconi T operation on 160m and broadcast band.

Partridge Electronics Ltd, Broadstairs, Kent.

ATU's 111B and LO-Z500 for use with Joystick aerial. **Joymatch Triple purpose ATU**, s.w. and m.w. coverage, in kit form.

Lowe Electronics Ltd, 119 Cavendish Road, Matlock, Derbyshire.

ATU, Daiwa CL22 $1\cdot 8$ to 30MHz for SWL. Converters by Microwave Modules, various for 4m, 2m, 70cm and 23cm to h.f. receiver.

Rocquaine Electronics, Aldebaran, Le Coudre, St. Pierre-du-Bois, Guernsey, Channel Isles.

Crystal Calibrator RQ1, 1MHz, 100kHz and 10kHz, c.w. or modulated output, kit form. Frequency Counter RQ3, up to 40MHz, 4-digit l.e.d. display of frequency or period or wavelength, kit form.

Datong Electronics Ltd, Spence Mills, Mill Lane, Bramley, Leeds LS13 3HE.

Active Antenna AD170, indoor aerial system 60kHz to 70MHz, 3m long dipole plus amplifier, output 50Ω. Up-Converter UC/1, synthesised receiving adapter plus 2m converter for receivers tuning 28-29MHz or 144-145MHz, range 90kHz to 30MHz. Audio Filter FL1, automatic suppression of heterodynes in range 280-3000Hz, variable width notch 25-1000Hz.

Before you rush off to spend your hard earned money, why not stop, think a little, and decide exactly what you need. Don't let the salesman talk you into buying something you will never use; try to get value-formoney

Buy the best that circumstances allow, for you can then expand your use of it as time progresses. A machine only meeting an immediate requirement could be a serious limitation later, so take a few moments to ponder the following points, and put them in order of importance, then find the cheapest machine offering the majority of your choices.

The overall dimensions will depend on whether a truly "pocket-sized" machine is required or not, and the size of the buttons is also often a determining factor. There are those who are not very keen on the closely-spaced buttons usually associated with small calculators, so it may be wise to try one or two in the shop. Some have a kind of "feel": that is, they click when pressed. Others just travel down to a stop with no feel when contact has been made. Again, it will be necessary to look at various types and determine your preferences.

Batteries

A tip on calculators that give key trouble from time to time: if they have not been used for a little while, a thin oxide film builds up on the contacts. This can easily be removed by one or two firm presses on the offending button.

There are three types of battery commonly employed: the ordinary carbon-zinc (torch type) dry battery, the alkaline cell and the rechargeable cell. The alkaline battery will cost about three times as much as the carbon-zinc but lasts approximately three times as long; its characteristics are such that it runs down much more quickly however, giving less warning that replacement is due. If the machine you choose has a suitable socket, a mains unit can be used to conserve battery life. However, it is a good idea in this case to take the batteries out, as under certain circumstances they can be damaged if you do not. The rechargeable type of battery is more expensive still, but can be used again and again. (That is not to say that they do not wear out; they do, and can only be recycled for a limited number of times). When they are low, plugging in the charger will top them up, and on most machines this is achieved whilst the calculator is in use.

If you cannot afford rechargeable cells, or if there

are none available to fit the calculator you are using, there are various ways of prolonging battery life. The easiest is to cultivate the habit of switching off between each sum. It will often be necessary to write down an answer and gather other figures before the next sum is performed, so it is an idea to switch off and on each time.

Another point to watch when buying your calculator is how the machine responds when the battery is low. Some machines flash the display or give similar indications: other give no sign at all other than the display getting dimmer. A frequent check should be kept on battery condition, as the calculator may give wrong answers when the battery voltage falls.

Before we go further, a few words about some possible uses: points which should influence the type of machine that you finally choose. Most people only use calculators for adding up bank statements, checking the family budget and metric conversions—indeed, some are pre-programmed to do these calculations specifically, and for these purposes a standard four-function machine is quite adequate.

Four-function refers to a multiplication, division, addition and subtraction capability: limited facilities, but ideal for many applications such as homework! A scientific calculator, with logarithmic and trigonometric functions, will be much more versatile for the student however, and probably have exponential notation, but it is advisable to check whether it is aceptable at the school or college, as some will allow only certain kinds of machine. A good compromise would have at least two extra and very useful functions: the reciprocal (1/the number) and the square root. Various other buttons are provided on different types of machine and it may be of interest to consider a few examples in the ensuing paragraphs.

Constant function

The constant function allows one to operate repetitively on a whole string of numbers. For example, should you wish to divide several numbers by 2.54, initially enter the first on the list, press "Divide" and then "2.54" followed by "=". It is now only necessary to enter those remaining one-by-one, pressing the "=" sign after each, thus saving several additional operations.

If, instead of 2.54, the constant had been 3.1415926 (pi) then ten button pressings are saved. Machines will differ in this respect, so care is needed; some will have the constant facility initiated by a switch, which

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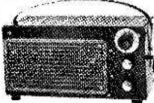


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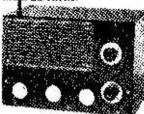
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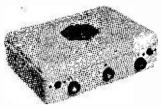


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RADIO CONSTRUCTION KIT O7

A compact small radio kit covering Medium Wave and Long Wave bands. Rugged Micanite con-struction and simple square design allows

square design allows of the same positioning. Ideal for the Garage, Workroom, Kitchen, etc., has seven Transistors and four Diodes, quality Loudspeaker, ready wound Ferrite Rod Aerial and Carrying Strap. Size $4\frac{\pi}{2} \times 4\frac{3}{4} \times 4\frac{3}{4}$. All parts and plans excluding 9v PP7 Battery.

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Build this exciting new design. Now with 7 Transistors and 4 diodes. MW/LW. Powered by 9V battery. Ferrite rod aerial, tuning condenser, volume control, and now with 3in. loudspeaker. Attractive case with red speaker grille. Size 9in. × 5½in. × 2½in. approx. All parts including Case and Plans.

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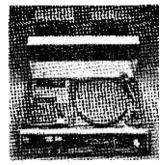
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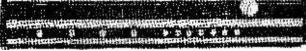


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AMPLIFIER Power Output: Distortion:	Nominal 2×25 watts RMS. THD @ 2×20 watts 0.7%	Intermediate Frequency AM FM Aerial input:	y: 475KHz 10·7KHz
Frequency Range:	@1·5dB 30Hz- 15KHz	AM (internal) AM (external)	Ferrite Rod 2 pin DIN
Tone Control Range: VC-20dB	18dB	FM (external)	Co-axial 75 ohm unbalancedi
Basic Electrical centre Treble Electrical centre	@ 100Hz-14dB	AGC:	
Loudness Control:	—14dB	For 6dB audio change IF Bandwidth	46dB
VC30dB	@ 100Hz+14dB @ 10KHz+11dB	@ max sensitivity RF Sensitivity:	± 1.5KHz @ 6dB
Filters: V C30dB	@ 10KHz-6dB	@ 20dB S/N Ratio 200KHz 600KHz	1500μV/m 500μV/m
Controls:	5 rotary: volume, balance, bass, treble	1400KHz	200μV/m
Switches:	tuning. 9 push button: phono. tape. radio, aux. input. mono/ stereo, ioudness, fil-	FM: RF Sensitivity @ 26dB S/N (mono) 88MHz 100MHz	2·5µV
	ter, speaker switch- ing, separate mains switch.	@ 46dB S/N (mono) @ 46dB S/N (stereo)	16μV 125μV
Meters:	2 signal strength: FM tuning	Distortion: @ Decoder O/P	0.9%
Sockets:	Headphones: 5 pin DIN Aux: AM aerial (ext) FM aerial (co-axial): 4 × 2 pin DIN L/S	Frequency Response: @ ± 1-5dB Stereo Separation: Audio Filter	30Hz-15KHz 40dB Flat to 55KHz 50dB @ 130KHz





TU020

A Hi Fi tuner amplifier

This unit can be built from our modules or as a complete kit. Input for mag cartridge, tape record/playback, MW/LW/VHF stereo, tuner. Uses the same R F Board as does the Wimborne with birdie filters, multiplex filter, varicap tuning on MW and LW.

Items from the Wimborne numbers 2 and 3 can be used for different performance specifications.

SPECIFICATIONS

Power output 25 Watts RMS per	channel
(both channels driven) Total harmonic distortion 0.05%	
Bass 100 Hz ± 12 dB	

SUITABLE SURPLUS MODULES. Fully Wired

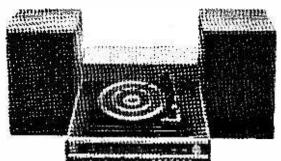
Frequency response ± 1.5 dB 30 Hz-20 KHz

Fully wired modules, Preamplifier, £9·50 £33·95

Power amplifler RF Board Power supply unit Transfomer

FM sensitivity 1-0 μV for 26 dB S/N ratio IF rejection 60 dB image rejection 60 dB Stereo separation 40 dB AM sensitivity 200 μV at 1600 KHz 20 dB S/N ratio. Magnetic PU amp

£7.99 PLEASE ADD £1 for postage and packaging for each item except the mag PU amp which



AU10

A Radio Record Player Kit which has everything you need to make a first class three band STEREO unit. Can be assembled in modular form or from scratch. A professional finish is guaranteed.

SPECIFICATIONS

Amplifier Output Distortion: Controls:

2 × 10W RMS, both channels driven 2×1000 (and, 21) $1\% \pm 2 \times 5$ watts Four rotary 1. OFF/ON/VOLUME Four rotary

2. Balance 3. Treble 4. Bass

Bass @ 100 Hz ±9dB Tone Control Range:

Treble @ 10 kHz ±9dB 2 × 2-pin DIN for 8 ohm loudspeakers 1 switched stereo headphone socket Outputs: 5-pin DIN Aux. Tape in/out socket

Frequency response @ ± 1.5dB 30 Hz—15kHz Separation 40dB Stereo Performance: Audio Filter—flat to 55 kHz—50dB @ 130 kHz 7 Push Button: Phono, Tape, Mono, FM, MW, Controls:

LW. AFC 1 Rotary: Tuning

Radio Tuner Medium Wave 525—1620 kHz Long Wave 155—280 kHz Waveband Coverage: Long Wave FM VHF

88-108 kHz 8-90 RF Board Price Hardware Kit 8.75 Record Deck 13.95 Amplifier & Pots PSU & Transformer

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2 Amplifier Module (11-14) watts RMS per channel, wired and tested, £19.95, kit price £13.95.

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7 Wooden Plinth plus base board £9.95.

8 Perspex dust cover plus hinges £6.50.

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can be useful when working on complex problems, as it can be brought in and out during the course of the sum and used as a pseudo-memory. Other machines have the constant operating all the time, and this can be something of a nuisance if it is overlooked. The number of constant functions will vary from one calculator to another, and on some machines it will operate on multiply and divide only, whereas, in the case of others, it will operate on add and subtract as well.

Most calculators have displays of eight digits, so, if your solution should happen to exceed this, various responses will be elicited from the machine. The most common is for a symbol of some sort to appear on the right-hand side of the answer, and the electronics then prevent any further operations until the "clear" button is pressed; the calculation then has to be attempted in some other way. There are also machines which show a symbol to the left of the display. Pressing the "CE" button will allow you to continue, remembering that the decimal point will be moved eight places to the left; that is to say, the number appears a hundred-million times smaller than it actually is.

Significant

Another type operates in such a way that it is calculating with numbers over a very wide range but only displays the eight most significant digits. In order to find out where the decimal point is, should it not appear, one has to multiply or divide by ten repeatedly, depending on whether noughts or figures are shown. Count the number of times the operation is performed and when the decimal point appears on the display the true answer is the number shown multiplied by ten to the power of plus-or-minus the number of operations carried out. i.e. If 12345678 is displayed, divide by 10 until the decimal point appears. Let us suppose that after three attempts 12345678 is shown. Then the *true* answer is 1,234,567,800 or: $12345678 \times 10 \times 10 \times 10$ i.e. 12345678×10^3 .

The exponential display shows an expression in two distinct parts; the number (or "mantissa") and the power of ten (or "exponent") by which it should be multiplied to give the correct magnitude.

For example $1536=1\cdot536\times10^3$ and could be displayed as $1\cdot536$ 3. Similarly $0\cdot003724=3\cdot724\times10^{-3}$ and would be displayed as $3\cdot724-3$.

Maximum range

Unless there is some other reason for limiting the numbers that can be displayed by this method, the maximum range is 10^{100} to 10^{-104} . To make the electronics simpler, some machines restrict the style of entry so that the decimal point is assumed and fixed after the first digit. Other calculators will allow the number to be entered in any form and adjust the display accordingly.

The floating point is a similar function to the exponential and is available on all but the cheapest machines. It is the ability to give an answer with all the digits available in the display, cutting off only those after the decimal point for which there is no room. If this facility is not available, the machine is said to have a fixed decimal point. The remainder of the number is bunched to the right and hence the machine shows less than it is capable of. When search-

ing for the point, try to establish what happens when the calculator cuts off: some machines just truncate; that is, they ignore the remainder, whilst others will round up.

If the calculator has a floating point facility it could work against you if zero-suppression is not included. For example, the answer to a calculation is given as "1" and the display appears as 1.0000000. With zero-suppression this would be shifted to the right and appear as "1"—an obvious saving in battery power as the display takes the higher proportion of the total current.

Changing sign

Some machines have two buttons fitted both having the minus sign, or alternatively a single button is provided which acts in either or two ways, depending on the state of the calculation. Others are not fitted with this facility and here difficulties may be encountered. The problem is that the minus sign carries out two functions: sometimes it is an "operator": that is, it says something about a number ("this number is negative"). On other occasions it instructs the calculator to make a subtraction. Without a two-button capability—or a double-acting one—you may only be able to make a subtraction, whilst in fact you may wish to change a sign. The solution is to multiply the number by -1, because when the "1" is entered, the minus sign acts as an operator.

The Algebraic and the Reverse Polish are two calculators having these characteristics available. In the case of the Algebraic machine, data is entered as it is spoken—i.e. "one times two equals . . ." etc. Care must be taken however if the expression becomes complex, such as when brackets occur in an equation. These may have to be expanded unless the machine has a "bracket" facility, (usually limited to only two layers).

Reverse Polish

With the Reverse Polish machine a slightly different way of solving the problem is adopted. Each time the number is entered you should ask yourself "can I perform an operation?" if the answer is "yes" then this is exactly what you do; if it is "no" then press the "enter" key which will record the number at the bottom of a small column of registers.

This may at first seem unnecessarily complicated, but is very quick indeed when you become familiar with the technique. As with any piece of technical apparatus, best results will only be achieved when the operations are fully understood. Even the cheapest machine will have modes, perhaps with a constant facility, which can be used to save several key operations and perhaps even a certain amount of rearrangement to the equation.

Example:

 $7 + (3 \times 9)$, would normally be resolved by rewriting as $3 \times 9 + 7$. If the constant is used however the entry becomes 7 + 9 = =

This is only a simple example but shows the difference between the two methods.

The conclusion is, when buying your calculator, reflect at first on its application. Study the manufacturer's specifications and, most important of all, ask about its capabilities, endeavouring where possible to try them out.

Happy calcuating!

The device we are considering this month has been developed by National Semiconductor mainly for use in simple "flasher" circuits using light-emitting diodes. It is economical in use, and is ideal for applications involving the beginner.

The LM3909N

The device itself is encapsulated in a small 8 pin dual-in-line package which can be used in the simple circuit of Fig. 1. Supplies are connected between pins 4 and 5, with pin 5 positive. Initially, the voltage across the l.e.d. (D1) is too small for it to pass an appreciable current; however, C1 charges through internal resistors R2, R3, and R4 and when the potential at pin 8 falls below a certain level, the electronic switch closes and effectively connects pin 2 to pin 4. The voltage across D1 is now equal to the power supply voltage plus the potential across the charged capacitor. D1 then emits a pulse of light of about 5ms duration, and the electronic switch re-opens.

The value of C1 may be $300\mu F$, 3V, in which case the flashing rate will be about one per second, and the current consumption about 0.7 to 0.8 mA.

Supply Levels

An l.e.d. requires at least 1.7V applied before it will conduct and emit light. However, the voltage boost obtained in the Fig. 1 circuit by the switching of the charged capacitor enables flashes to be obtained with supply voltages down to 1.2V. The flash frequency decreases as the applied voltage is reduced; if a rate of one per second is required, pins 1 and 8 should be linked and 1.5V supplied. The maximum permissible voltage before damage occurs in the LM3909N is 6V.

To reduce the current consumption from a 1.5V supply to the absolute minimum, C1 in Fig. 2 is reduced to $100\mu F$ 3V, with pin 1 unconnected. The rate is then little more than one per second and the mean current taken from the battery is about 0.3mA, with a consequent reduction in flashing intensity.

The exact flashing rates stated may not be obtained since electrolytic capacitors have very wide tolerances—up to 100 per cent over their marked value. An increase in capacitance will reduce the flashing rate, but will increase the brilliance of the flash, although it will not have much effect on the current consumption.

Fig. 2 shows a circuit which provides a greater flashing rate (about $2\cdot 6Hz$) for a current drain of about $1\cdot 2mA$.

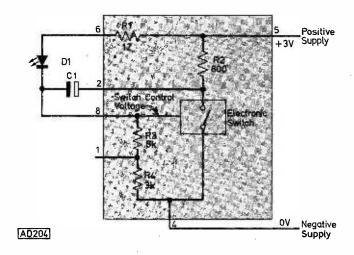


Fig. 1: A flasher circuit, showing the operation of the internal circuitry of the LM3909N

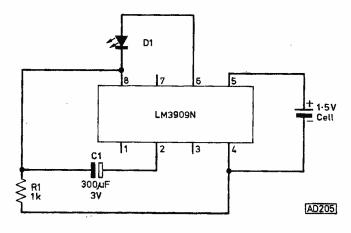


Fig. 2: A 2.6Hz flasher using a 1.5V supply

Torch Finder

One of the most useful LM3909N applications involves its use in the base of a torch with an l.e.d. The latter emits weak flashes of light continuously when the torch is switched off; this enables the torch to be found very easily even in complete darkness. The quiescent current consumption is so small that the normal battery life is almost unaffected. A torch finder of this type is shown in Fig. 3. The LM3909N circuit and the l.e.d. may be fitted into a transparent cap on the base of the torch.

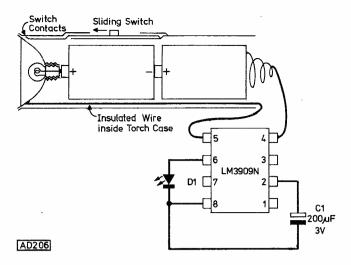


Fig. 3: A simple torch finder

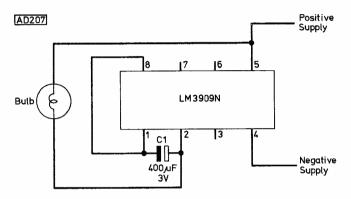


Fig. 4: A flasher using an incandescent bulb

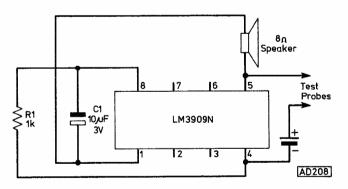


Fig. 5: A simple continuity tester based on the LM3909N

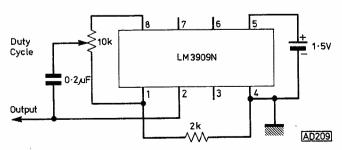


Fig. 6: A square wave generator circuit

Incandescent Bulb Flasher

The circuit of Fig. 4 shows how the LM3909N can cause a small tungsten filament lamp to flash at about 3 flashes in each 2 seconds. In this circuit a small current flows from the positive supply through the bulb and charges the capacitor via the internal resistor connected between pins 1 and 4. This current is much too small to illuminate the bulb and when the potential at pin 8 has fallen by an adequate amount, the electronic switch closes. A larger current can now flow from the supply line through the bulb to pin 2, and ceases when the potential of pin 8 rises and the electronic switch opens. Thus the bulb emits a flash of light.

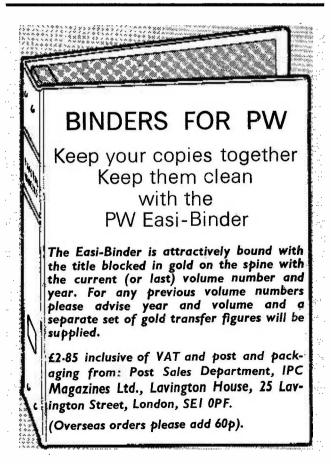
The mean current required by the circuit of Fig. 4 is much greater than that required by the circuits using l.e.d. indicators.

Continuity Tester

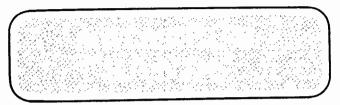
A simple continuity tester is shown in Fig. 5. When the test probes are shorted together, the circuit oscillates and a note is emitted from the loudspeaker. This note is distinguishable from that emitted when the test probes are joined by a resistance of only a few ohms.

Another simple circuit using the LM3909N is shown in Fig. 6 where it is used as an oscillator. This circuit will produce a square wave output with a frequency of about lkHz.

The LM3909N is available from Arrow Electronics Ltd., Coptfold Road, Brentwood CM14 4EN. At the time of writing the price is 95p inclusive of V.A.T., but 25p must be included for packing and postage on orders under £5.







by Eric Dowdeswell G4AR

Another fledgling takes to the air as Michael Walker passes his RAE and becomes G8PRX, but he intends to get the code test over pretty soon. Michael is looking for a cheap, simple transceiver for 2m so any offers to 100 Langdale Road, Woodlesford, Leeds LS20 8XF. As a PS "15-soon 16" year-old Michael blames me for pushing him into getting a licence "but I don't regret it a bit".

Conditions generally on the h.f. bands have not been too good as confirmed by Brian Smith BRS40307 of 15 Courtenay Road, Barry, Glam, so Brian has been busy organising a contest for the FRG-7 Owners Club, formed recently. Write to Brian for details if you sport an FRG-7. A candidate for the club is Joe Porter, a newcomer to the column, living in Belfast. Joe started on the broadcast bands but says that the amateur bands have added a new interest to his life since getting the FRG-7.

John Bell BRS40279 of Melksham, Wiltshire, started SWL'ing only last April with his 1943 AR88 and 120ft of wire which is "more of a ham-string than an aerial". John would like to beg, borrow or steal a handbook for the set so if you can help drop a preliminary line to 12 Windsor Avenue, Melksham, Wilts.

Regular PW reader Bruce Norval G3VHT of 203 Surrenden Road, Brighton BN1 6NN has an old Cossor 3339 'scope but feels he could get more out of it if he had a manual. Anyone oblige? Any expenses gladly refunded, naturally. A quick note from our Simon Robinson reveals that his new call is G8POO with which he is not at all pleased, so he is after his G4 call as soon as possible! Len Adlard of Leigh-on-Sea, Essex, wrote a few words of appreciation for the replies he had concerning info on his R1392 receiver and hopes PW "may long foster the friendship between those interested in radio", which sums up our hobby very well!

Newcomers to the Column

I. D. Calvert residing at 16 Nabwood Drive, Shipley, West Yorks, has progressed from the s.w. broadcast bands to the amateur bands now that he has a Yaesu FR50B but would be happier if he had a manual.

College studies permitting "I.D." intends to swot for the RAE in due course. He reckons the column is far too short so a copy of the letter will be passed to the Editor very soon! W. Sides hailing from Swinton, near Mexborough, has also found the amateur bands, on a Lafayette HA800, which has given him "a new interest in a life that seemed destined to be boring", having retired early due to ill-health. I hope both the above will let me have their Christian names next time round!

In Darlington, Co. Durham, Rod Hunt had fun on the s.w. BC bands with his two-transistor regen' set but couldn't find the amateur bands, until he fitted a super-slow-motion dial. Rod says "If I could starve the kids and divorce the missus I could afford a better set". A bit drastic OM and hope it won't come to that! So, carry on building! An ex-master mariner, Rod was hot on visual code and is now building up his c.w. copying ability and comments on lack of c.w. logs. I'd certainly like to see more, so what about it?

Around the Bands

Martin Leizers (Newport) took his radio on holiday but found little other than a couple of openings on 10m. An FRG-7 plus converter and quarter-wave vertical helped J. S. Goodier (Marple, Cheshire) get on 2m but has not heard much of note. I think a good beam aerial, preferably rotatable, would make a world of difference here, OM. "J.S." commends the Pacific DX Net on 14265kHz s.s.b. on Tuesdays around 0600, for info on activity in that part of the world.

All bands from 10 to 80m have been visited by Ian Marquis of Leigh-on-Sea, Essex, finding OE5CA/YK on the Golan Heights on 80m, VP8NX on 40m, new country CE0AE on Easter Island on 20m plus two really rare ones in ZL2BJU/K on Kermadec Island and VK2AGT/LH on Lord Howe Island, all s.s.b. 15m revealed KC4AAD plus KG6JJY on Guam and KM6FC on Midway, while 10m came up with KZ5RO. A late note from Brian Smith BRS40307 reports J3AH from

Reports on the various bands are welcome and should be sent direct, by the 15th of the month, to:-

AMATEUR BANDS Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey KT21 2TW. Logs by bands, each in alphabetical order.

MEDIUM and SW BANDS Charles Molloy G8BUS, 132 Segars Lane, Southport, PR8 3JG. Reports for both bands must be kept separate.

VHF BANDS Ron Ham BRS15744, Faraday, Greyfriars, Storrington, Sussex RH20 4HE.

Grenada on 80m. Is this the start of the winter activity on the l.f. bands? P29NKV on Papua was also a first for Brian. Steve Turner BRS37620 (Wilmslow, Cheshire) recorded D4CBS of the Cape Verde Islands for a rare one, as did several other listeners. Summer time brought OHO to life with several OH's there on holiday. Remember that OHO is a separate country.

CE9AT in Antarctica is also a different country from the mainland CEs, reported by John Whiting BRS40086 of Fareham, Hants. QSL manager is CE2BIO. This was on 15m. A listen at the c.w. end of 20m brought FB8XS, with ZD9GI on 10m for Dave Greenhalgh (Poynton, Ches).

Bill Rendell (Truro, Cornwall) injured his knobtwiddling finger but that didn't stop him finding some VK7s on 20m s.s.b. plus VP2LDB on St. Lucia and ZL4KI, while 15m yielded CT3AF, YB0ABO and ZB2BÚ.

Club News

The Wessex AR Group had 20 up for the May RAE and 15 made it! Which speaks well for the club's organisation. Needless to say RAE courses are under way again with, incidentally, a reduction in course fees of 50% for OAPs. A nice thought. Sec. is Geoff Cole G4EMN, 6 St. Anthony's Road, Bournemouth. Forthcoming talks are on Fast Scan amateur TV on Nov 3 by G3PYB, G8ADM and G8GYS and the Intruder Watch by Watch organiser G5XB on Nov 17.

The White Rose RS meets at 83 Town Street, Arnley, near Leeds, every Wednesday evening at the White Horse Hotel. Further info, ring Sec. Dick Hughes on 680937. Excellent monthly magazine White Rose Clippings has something for everyone, including constructional articles. The Wigston RC flourishes in Leicester with the previously sole licensee G3Y00 being augmented by six passes at the May RAE. All welcome at the United Reformed Church, Long Street, Wigston Magna at 1930 first Friday of the month. This is a brand new club and much deserving of support.

J. M. Coates G4GYU tells me of the radio club of the 1st Rainworth Scout Group which now boasts of two G8s following the May RAE. Scouts interested in the club contact G4GYU, 30 Abbott Road, Mansfield,

Notts.

The Hon. Sec. of the Radio Amateur Invalid and Bedfast Club Harry, G2CLP, has been able to unload his heavy burden of running the club on to the capable shoulders of Francis Woolley G3LWY, a previous holder of the job. Thought you'd finished eh, Francis? If interested, as a supporter or an invalid, contact her at 9 Rannoch Court, Adelaide Road, Surbiton, Surrey

It was with deep regret that we heard of the death of Tom Darn, G3FGY at the age of 56. A member of the Derby club since 1950, Tom was active in many aspects of Amateur radio, and did much for the handicapped. He will be sadly missed.

Log Extracts

W. Rendell:—20m A7WL VK7AE VP2LDB ZL4KI 8P9JH 15m CT3AF FG7AX P29JS VP9HS YB0ABO ZB2BU

D. Greenhalgh:—20m FB8XS 10m ZD9GI 5B4CY

J. Whiting:—20m OY5J 15m CE9AT P29NYL 6W8FZ 10m 5H3KS

S. Turner:—20m C31MK DA1GR/OH0 D4CBS CP6HI

B. Smith:—80m J3AH 20m CP5ADE 15m P29NKV 10m HK3AXT S79MC 3D6BP

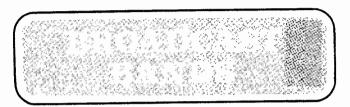
I. Marquis:—80m C31DM OE5CA/YK 40m C31IP OY5J TU2HG VP8NX YN2DX ZB2BL 7X5AB (QSL W2KF) ZD7WT 20m CE0AE ZL2BJU/K VK2AGT/LH VK9ZM VR1AF VR3AK VS5CW YI1BGD 601FG 15m H44LW (?) (Solomon Is.) KC4AAD KG6JJY KM6FC VR3AR VS5XU YB0GF 5W1BN (QSL KH6JEB) 10m C310C KZ5RO 9V1SW.

M. Leizers:-80m VO1FG 40m CE3RR C31IP 20m VP2VPK YB0ONQ HZ1BS/8Z4 15m KZ5AS YB3AE 10m CE3BZB CX7UM C31NX FM7BB

B. Hughes:—20m VP2EEN 15m VE7IG TA1MB FB8XS

J. Bell:—20m C31NM EA8QU PJ4CR TA1ZB VP2VRK

All s.s.b. except those in bold which are c.w.



MEDIUM WAVE DX by Charles Molloy G8BUS

On November 23rd, 1978, the Geneva Plan for the medium waves comes into being. It covers Europe, Asia, Africa and Australasia (ITU Regions 1 and 3) and in Europe it replaces the Copenhagen Plan which has been in operation since 1948.

The total number of channels will be 120 starting at 531kHz and ending on 1602kHz. The spacing between channels will be 9kHz and each frequency will also be an exact multiple of 9kHz which it is claimed will help to reduce heterodynes. In practice this means that in Europe, where the spacing is already 9kHz, the majority of channels will simply move up by 1kHz, a change that will hardly be noticed. except perhaps on receivers with push-button tuning. The long-wave frequencies are unchanged with 15 channels being allocated for broadcasting in Region 1 only as at present. There are some alterations, with the UK being awarded 227kHz as well as 200kHz though both frequencies will have to be shared with other countries.

Many European stations will only move by lkHz and it is probable that the average listener would not even notice the introduction of the new plan but for the decision of the BBC to reorganise its radio programmes on the same date. The changes in Radios 1, 2, 3 and 4 listed elsewhere in this issue have really very little to do with the Geneva plan.

Station Listings

So far as I know, the only published list is the one attached to the Geneva Plan itself which is very expensive and beyond the reach of the majority of us. Parts of this list have been reproduced in some radio club bulletins. In any case this list is of limited value as it refers to authorised frequencies and occupants. How many of these will actually be on the air on November 23rd is another matter altogether. Several countries have published a list of their intentions and no doubt the 1979 edition of the World Radio and TV

Handbook, when it appears early in the new year, will only mention those stations actually in service. In the meantime there may be a lot of uncertainty.

The New Plan and DXing

What effect will the new plan have on medium wave DXing in the UK? Asiatic DX will certainly become more difficult as stations in that continent will, or should now be on European channels. A loop will not be of great help as a lot of the European QRM will be roughly in the same direction as the DX. African DX should not be affected so badly as a loop will be of value in this case. The interesting area will be Region 2 which covers North, Central and South America and the Caribbean. Stations in Region 2 are not affected by the Geneva Plan but QRM from other parts of the world will change.

Region 2

The majority of broadcasters in Region 2 are on frequencies which are multiples of 10kHz. This means that there are some frequencies which are in use in all three regions. These are 540, 630, 720, 810, 900, 990, 1080, 1170, 1260, 1350, 1440 and 1530. This is not very different from the current position but the change may be sufficient in marginal cases to make difficult DX either impossible or alternatively a little easier. Stations such as CBT Grand Falls in Newfoundland on 540, WTIC Hartford on 1080 and WCKY Cincinatti on 1520 may become rarities. Some stations that are easy to log at the moment will become difficult and even WINS on 1010 may be harder to hear as it will be only 2kHz away from European QRM.

As a result of the different channel spacing in Region 2 there are a number of places in the band where maximum separation from Geneva Plan channels occurs. The frequencies come in pairs and start with 580 and 590kHz where the "nearest" European is 4kHz away, then to 670kHz and 680kHz, 760 and 770, 850 and 860 and so on up the band. In Europe these are the DX slots in the band. Finally, there is a major change at the h.f. end of the band above 1540kHz where the spacing in Europe at the moment is 8kHz. 1570kHz will be 4kHz away from QRM instead of sharing a European channel and 1580kHz should become reasonably clear of QRM.

The Geneva Plan will add a new dimension to m.w. DXing not only in the UK but throughout the world though it may be some time before its effects are fully apparent. One can be certain of one thing; the medium waves, the oldest DX band, will remain as attractive and as challenging as ever.

Loops and Portable Receivers

From Liskeard in Cornwall comes a long letter from K. Lewis who uses a 36in loop with a Grundig 305 Transistor receiver, following the method outlined in this column in May 1978. "The receiver is placed on a shelf inside the loop and orientated so that the null of the ferrite rod aerial coincides with the null of the loop. The whole system is mounted so as to enable simultaneous rotation of receiver and loop in one simple operation." Mr Lewis goes on to say that the loop does not have a coupling winding or feeder cable as there is no direct metallic connection of any sort between the loop and receiver. The portable's own ferrite rod aerial picks up signals from the loop as

well as from the station and a considerable improvement in signal strength is the result. Stations logged with this rig between 0230 and 0330 during July and August included CKVO Clarenville on 710kHz and CJYQ St John's on 930 both in Newfoundland, WINS 1010 in New York and CFRB in Toronto also on 1010, Radio Margarita Venezuela 1020 and WQXR in New York on 1560. An unidentified US broadcast on 1020 would almost certainly be the famous KDKA in Pittsburgh.

A number of readers have written to me about problems they encounter when trying to use a loop with a portable and nearly all of these problems arise from a misunderstanding of the principles involved, probably the result of the terminology used. The "null" of a loop is really a shorthand way of saying that there are two directions from which a loop does not pick up any signal. If the loop is positioned so that a "null" points towards an unwanted station it will no longer be heard. Very useful provided that the receiver is not picking up this unwanted station from a second aerial such as the internal ferrite rod aerial that is standard with portable receivers. A loop should only be connected to a receiver that does not have its own aerial. You can easily check this. Disconnect the loop and if the receiver still picks up stations then it must have its own internal aerial. In answer to Martin Liezers—remove the ferrite rod aerial from the back of your DX160, it is not part of the receiver.

A large number of portable type receivers are in use today. Some are quite complicated and expensive and they perform very well indeed on the short waves but to quote F. R. C. Fowle of Somerset West in Cape Province. "I have a Barlow Wadley which seems to be remarkably immune to any add-on aid to reception" and this certainly applies to the loop aerial. A ferrite rod aerial is of course equivalent to a miniloop, but unfortunately the pick-up is not great enough for DXing. If the receiver is mounted at the centre of a loop in such a way that the ferrite rod and loop nulls coincide then the two can be rotated together and an unwanted station will then be capable of being nulled out. No need for a direct connection between the two. The wanted signal picked up the loop is re-radiated and picked up by the receiver's aerial, the whole system operating like an amplifier without power supplies. One of the few examples of getting something for nothing! Although having a touch of the Heath Robinson about it this procedure does enable useful DX to be heard on a portable receiver. The alternative is to purchase a communications receiver or to become discouraged before even sampling the thrills of m.w. DXing.

DX Clubs

David Pristupa writes from Saskatoon in Canada to say that he can receive only North American m.w. stations from his QTH and he invites any DXer who might be in his area to look him up at 3437 Ortona Street, Saskatoon, Canada 57M 3R9. I suggest David that you join one of the two North American DX Clubs that specialise in m.w. DXing. These are the International Radio Club of America (IRCA), PO Box 26254, San Francisco, CA 94126 and the National Radio Club (NRC), Box 99, Cambridge, Massachusetts 02138 USA.

The domestic log published by the NRC is referred to by S. Donnelly of Adlington. This booklet lists all medium wave stations in Canada and the United

States in frequency order and gives the callsign, power, address and other information about them. This listing is for the North American specialist and it can be obtained by non-members of the NRC from the address given above.

DX

Reception conditions during the summer were very good this year and several readers had a go at Middle East DXing during Ramadan, which incidentally is an annual event occurring approximately 10 days earlier each year, by our calendar. David Sidebottom of Fleetwood has a Realistic DX160 and a 33ft long wire and he logged 10 North Americans between 0100 and 0400 with this rig, including WLAM Lewiston Maine on 1470 and WITS Boston on 1510. David would like to know how the new Yaesu Musen FRG-7 compares with the Realistic DX160 on the medium waves. Can anyone help? Replies should go direct to David at 7 Bristol Avenue, Larkholme Estate, Fleetwood FY7 8JQ. Bob Bell of Blyth (FRG-7 and loop) reports hearing two stations on 737 which would be Israel and Iran, Qatar on 952 and two Arab stations on 820. Iran is on 820 and Egypt and Morocco are on 818kHz.

Some really excellent North American DX comes from **Derek Taylor** of Preston who used his FRG-7 and loop during the month of August to pull in WBBM Chicago on 780, CJVA Caraquet NB on 810, WOAI San Antonio Texas on 1200, CKIM Baie Vert Newfoundland on 1240, WEVD New York on 1330, WDEA Ellsworth Maine on 1370 and WEGP Presque Isle Maine on 1390. Derek gives a word of warning about WEVD which is multilingual and can be heard in Hebrew at times though the identification on the hour is in English.

A log of long-wave DX comes from Andrew Rogers of Bristol who used a Vega Spidola with internal aerial to log Minsk on 281kHz at 1958, Algeria in French and Arabic on 251 at 2300 and Brasov Romania on 155 at 2150. Are there any more long-wave DXers around?



SHORT WAVE BROADCASTS by Charles Molloy G8BUS

Loops on the Short Waves

DXers who have a medium wave loop often wonder if it is possible to use one on the short waves. The answer unfortunately is no. Ionospheric scattering becomes significant as frequency increases and as a result the directional properties of the loop gradually disappear as one tunes above 2MHz. The question is raised again by **K. Lewis** of Cambourne who asks if it is possible to use any kind of loop on the 120m tropical band. A difficult question to answer as there is so little DX to be heard on this band but at a guess I would think that a loop would still give some results even if it is only to reduce local static.

Several years ago I built a 3-turn 28in box loop to investigate this problem and I was able to tune the loop between 2MHz and 6MHz using a variable capacitor of about 300pF. During the daytime I could null out MSF (Standard Frequency station at Teddington) on 2.5MHz and 5MHz and the directional effect was still apparent on some stations on the 49m band. After dark MSF could still be nulled out on both frequencies but DX on the 90m band could not. I interpreted the above to mean that the loop would work on the ground wave and short-range sky wave but was no use on long-range signals above 2MHz. There is no sharp dividing line as the null just broadens out as frequency increases.

There is incidentally, a ferrite material called F16 which is effective up to 12MHz. Rods made of this material are available such as item FRD in the Ambit catalogue, which is a rod 8in long and 38 in in diameter, and it could be a useful item for the experimenter. Some receivers use a ferrite rod aerial instead of a whip for short wave reception and it would be interesting to hear from any DXer who has one. Try rotating the receiver to see if the aerial has directional properties.

120 Metre Band

120 metres (2300 to 2499kHz) is one of three bands reserved for local broadcasting in the tropics where the noise level due to thunderstorms makes reception difficult on the medium waves. The other two tropical bands are 90 metres (3200 to 3400) and 60 metres (4750 to 5060kHz). Of the three, 120m is by far the most difficult for DXing and there are probably only a few DXers around who have heard anything on it. At first sight this may seem surprising as propagation should be similar to that on the medium waves i.e. a path of darkness between transmitter and receiver before reception is possible. Unfortunately, 120m is used by commercial stations outside the tropics and the consequent high level of telegraph QRM makes reception rather difficult. Harmonics from m.w. stations are another problem and it is not unknown for BBC Radio 1 to be heard on 2428kHz which is twice 1214 (247m).

What are the chances of hearing the 500 watt Falkland Island broadcasting station on 2385kHz asks Martin Liezers. This station is on the air until 0200 on weekdays, but the chances of hearing it are not very good as a combination of low power and high QRM is not encouraging; but it is possible. If Argentina is coming in well on the medium waves then it might be worthwhile trying 2385. As far as I know it has never been heard in the UK. Stations that have been logged on 120m are Gwelo Rhodesia on 2336 and 2425, Galei Zahal (Israeli Army) on 2442 and in the winter Fuzhou in China on 2430kHz.

Commercial Stations

A number of readers including Andrew Belsey and M. A. Carter have enquired about transmissions that mention circuit or receiver adjustment. These are not broadcasting stations. They are commercial radio links which often transmit recordings with this sort of announcement while their engineers set up the circuit. It is illegal in the UK to listen to these transmissions without a licence and details of them cannot be included in this column.

Readers' Letters

Ian McLean (Port Glasgow) wants to know how many International Reply Coupons he should send to each different country to cover the cost of a reply to a reception report. A single IRC is exchangeable in any country that is a member of the UPU for stamps sufficient for a reply by sea mail. DXers usually send two IRCs for a reply by air mail. IRCs do not seem to be acceptable in some countries, mainly in Latin America.

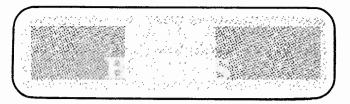
Joseph Pritchard (Nottingham) has made a crystal set using Denco coils, a diode and an old tuning capacitor from a scrap receiver. When connected to a 50ft outdoor aerial it produced earphone signals from the 49m, 41m, 31m and 25m bands. Reception was improved by the addition of a length of wire from the earth terminal of the crystal set to the bed frame! When the output for the earphones was put through a 3-transistor audio amplifier it gave loud-speaker reception of a number of stations including Radio Canada International on the 25m band.

A home-made receiver made out of two integrated circuits, a ZN414 and LM780N pulled in Radio Canada International for Derwyn Williams who lives in Maesteg in Glamorgan. The frequency announced over the air was 6195kHz and he is puzzled by this as RCI is not listed on that channel. The station Derwyn heard is the CBC relay at Daventry in the UK. The trend these days among international broadcasters is to use relay stations near to their target area rather than rely on the uncertainties of propagation over long distances. Radio Japan, for example, has recently been doing tests from the Mediterranean area and if they do open a relay station there it will enable them to be heard well in Europe during the peak listening period in the evening. Direct reception from Japan is best in the morning.

DX

An old Pye receiver, a PR40 preselector and a 100ft wire in the loft brought some interesting DX to Ian McLean (Port Glasgow) who reports hearing Radio Nigeria on 4950kHz at 2300; Voice of Greece on 9565 at 1928, Radio Havana on 17865 at 2112. S. I. Fass (Edgware) has a Yaesu transreceiver type FT901D with an up-converter for short-wave listening. With this rig he managed to pull in Radio New Zealand on 15130kHz at 0645 through heavy QRM. Martin Liezers (Newport) has picked up the English transmission from Radio Uganda on 15325 at 0330 which is intended for North America. Also logged were TWR Guam on 17855 at midnight in English and Radio Reloj Continente (Venezuela) on 5030 at 0400.

Harmonics are in the news again with a report from Harold Brodribb of St. Leonards-on-Sea of the BBC Arabic Service on 29475kHz in the 10m amateur band which is three times 9825, the latter also coming in with a good signal. The receiver is an AR88 with a loft dipole. Goff Curtis reports again from South Harrow with reception of the BBC Eastern Relay (Masirah Island) on 15130 which is on this frequency from 0700 to 0800 and again from 0900 to 1500. Gear in use is an Eddystone 740 and a 20ft Windom aerial. Other DX heard was the BBC Caribbean relay on 17745 at 2000, Tanzania 15435 at 1845, BBC Ascension Island 15260 at 2000, KTWR Guam on 17855 in Chinese at 2300 and Cameroons on 4850kHz at 2200.



by Ron Ham BRS15744

I've said it before and I will say it again, the v.h.f.s are full of surprises. This one occurred on August 28th when a severe ionospheric disturbance, lasting most of the day, closed parts of the h.f. bands. The afternoon aurora, which upset the 2m band, caught us all on the hop because there was no previous solar radio noise to warn us. In fact, we observers of the radio sun had nothing at all to report during August.

Henry Hatch, G2CBB, reported on BBC World Radio Club, that the disturbance began around 0400 and Cliff Ranft, Guildford, Surrey, told me that he recorded two SCNAs (Sudden Cosmic Noise Absorbtion) at 30MHz during the morning of the 25th, and one at 1623 on the 27th. Despite overcast skies, Cmdr Henry Hatfield, Sevenoaks, observed the sun with his spectrohelioscope on the 27th. He saw three sunspots with an "active" plage coming around the east limb and thinks that this caused the event.

Aurora

Although Barry Ainsworth, G4GPW, Lancing, Sussex heard a French station calling GM via aurora at 0815, Charlie Newton, G2FKZ, London reports that the main auroral activity began around 1300 and lasted for about three hours. The Oxford University Radio Club, GM3OUR/P worked 14 countries on 2m during the event. Much of the following day's repeater conversations were about the aurora and the strong signals heard and worked from Germany, Scandinavia and all of the UK.

At 1345, Roy Bannister, G4GPX, Lancing, Sussex worked GI. He phoned Alan Baker, G4GNX, Newhaven, Sussex who rapidly devoured his dinner, raced to his shack, and made c.w. contacts with GM3OUR/P, whose auroral signal was very strong in the south, PA0SGL, and, after three years of trying, worked GD, his 17th country on 2m. Alan found that c.w. was the best mode and although signals were on a general beam heading between 350 and 70 degrees, the best direction was 30 degrees. He also heard a GW working EA and another calling a station in the USSR.

Dave Cox, G8OPR, Andover, Hants worked GM5MJI/P at 58A and John Branegan, GM8OXQ, Saline, Fife, who missed the August event, took part in another aurora during the afternoon of September 9th when he heard tone-A signals from the 2m beacons, GB3GI, GB3LER, GB3GM, and GB3VHF among a host of amateur stations from LA, a few from G and an EI.

Solar Activity

This later aurora was not unexpected because **John Smith**, Rudgwick, Sussex, Henry Hatfield and myself recorded solar radio noise between September 3rd and 10th, the strongest on 5th and 6th, and, on the 5th, Henry saw plenty of plages and filaments on the sun's disc and counted 22 sunspots, mainly in two large groups.

10m Band

Harold Goble, G4FDQ, Lancing, Sussex worked VK0A5 in Mawson, Antartica at 1310 on September 5th and noticed the very high noise level, which often happens on 10m when the sun is "active". On the 3rd, Harold worked two stations in the Channel Islands and commented about the short skip conditions. At 1747 on the 4th he had a 59 contact with ST2SA in Khartoum. Harold Brodribb, St. Leonardson-Sea, Sussex, using a loft-mounted inverted V aerial into his AR88 is delighted with the aerial's performance on 10m. Between the 7th and 10th he heard strong signals from stations in Europe, Russia, South America and South Africa. At 0948 on the 16th very strong signals from Japan pounded in and G4GNX worked one for the first time on 10m.

Sporadic-E

The 1978 sporadic-E season, which really began on May 1st, ended with a big opening around noon on August 26th when, between 0715 and 1140, Ian Rennison, Horsham, Sussex received Band I television pictures from Austria, Hungary, Italy, Portugal, Scandinavia and the USSR. Like myself, Ian received pictures from Norway and Spain during sporadic-E disturbances on August 22nd and 23rd.

Clive Atlowe, Blofield, Norwich heard several Polish f.m. stations on the 23rd and on the 26th he received signals for about 112 hours on Ch. E2 from Rhodesia. Up in Glasgow, Frank Luman watched pictures from Dublin, Hungary and Spain on the 25th and 26th. From Pretoria, South Africa, our reader Ian Roberts writes "I have been DXing on the v.h.f. bands for about one year now, using a 4-element horizontally polarised Yagi (40-70MHz) and a wide band TV pre-amplifier." During August, Ian, whose main interest is DXTV, received various weak video signals around 45MHz and both BBC and French TV sound on 41.5 and 41.25MHz respectively. On September 1st (spring day in the Southern hemisphere), the MUF on the North/South transequatorial path went up to 55MHz and Ian heard signals from the Cyprus beacon, 5B4CY, on 50.5MHz, which may be a "first" for South Africa. His main receiver is a National Panasonic RF8000, and he is delighted with its f.m./a.m./s.s.b./c.w. capability on the v.h.f. bands between 20-230MHz, plus the normal short-wave coverage up to 30MHz.

Tropospheric

The atmospheric pressure between August 20th and September 4th was above 30 0in in southern England and conditions were right for some v.h.f. DX. While holidaying in north Wales, Roy Patrick, whose home is in Mackworth, Derby, took his National receiver 678 feet up on the Great Arms and heard f.m. signals from Manx Radio, RTE, Down Town Radio, Belfast, and Radios Blackburn, Merseyside, Manchester, Sheffeld and Stoke-on-Trent, between 88 and 97MHz. During the evenings of August 21st Alan Baker heard signals on all 2m repeaters from R1 to R7 and 9 and worked F2PI, F6DWG and F9LT on c.w. and Graham Kent, G8HVD, St. Leonards-on-Sea, worked a German station on 2m s.s.b.

John Branegan was listening on 2m in Lancashire and heard West Country stations on August 24th and GMs on the 25th. Back in Saline on the 28th he observed a sudden lift on 70cm. Around this time, Dave Cox, using a Trio TR-7010 into a QQV06-40, 80 watts to a 6-element quad worked all G prefixes in 6 hours and 20 minutes, G, GB, GD, GJ, GM, GW and GU by tropo, and GI at 1404 via aurora.

During the RSGB 2m portable contest on September 3rd, Alan Baker worked DB6KH, 8 French stations, 4 GWs, 3 HB9s, 4 ONs and a PA0, and up north, John Branegan heard several GW stations. The pressure went high again on the 8th, and, as it fluctuated between 30.0in and 30.4in over several days, v.h.f. conditions were good. On the 9th, G4GNX assisted Eric Arnold, G8OUK, Hove, Sussex, to erect his new 2m X10 aerial and rotor on a 30ft pole atop a roof 20ft a.g.l. Imagine their delight when they switched on at 1930 and heard signals through both French and UK repeaters R3 to 7 and worked G8PNA in Buckinghamshire via the Hampshire repeater GB3SN. During the evening of the 13th, I heard GW stations working through GB3LO, Belgian stations through GB3PO and GB3SN, and I am told that EA1TA worked G.

At 1400 on the 17th, Alan Baker heard a G station on holiday in Torquay and using 1 watt from a handheld transceiver, working through the French repeater, FZ3VHB on R7, which was very strong in Brighton, as was the Paris repeater on R6. Alan was alerted to this particular opening by **John Cooper**, G8NGO, Cowfold, Sussex, when he heard HB9 stations calling G.

Microwaves

The two Erns, **Downer**, G8GKV and **Hoare**, G8BDJ, were on Chanctonbury Ring, Sussex as usual for the fourth leg of the RSGB's 10GHz Cumulative contest on August 27th. Although conditions were poor in the morning they both worked F6DLA/P and in the afternoon, when conditions improved, they both worked F1BQ/P, F3LP/P, G3JVL and G8DIC.

Readers' Specials

Congratulations to **David Wakefield**, Worthing, who has been promoted to Corporal in 45F Squadron of the ATC, passed his RAE and is now polishing his Morse ready for that G4 call. Congratulations also to **Roy Hills**, of the Brighton Club, who now sports the call G4HLH.

The Scottish VHF and Short Wave DXers club is going well, members, **Don Bassnett**, **John Cowan** and **Frank Luman** have received v.h.f. signals from almost every country in Europe and TV pictures, in good colour, from Finland, Iceland, Italy, Ireland, Norway and Sweden. The Club hopes to expand its membership into Cumbria, Northumbria and N. Ireland. Readers in those areas who are interested, drop me a line, and I will pass it on.

OSCAR

Although John Branegan spent half of August on a working holiday in Lancashire he took his portable OSCAR rig with him and writes "I had a great time as a G8 particularly on 8J, despite very small simple aerials fixed on my camera tripod". Back in Saline he worked W4AXR, Florida on September 2nd and VE3BNA, Ottawa on the 3rd via OSCAR mode 7B and 8J respectively.



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	PCC189 0 - 65 U26 0 - 85 PCF80 0 - 80 U27 1 - 00	5B/254M 6M6 4-20 12Y4 8-48 6-50 6J4WA 1-75 13D6 0-60
771000 1 25 25	PCF80 0-80 U27 1-60 PCF82 0-40 U191 0-75	
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CY31 0 50 EF92 0 75	PCF201 0 90 UABC80	5R4GY 1-10 6J7G 0-50 19H5 17-00
DAF96 0-60 EF95 0-45	PCF801 0·55 0·60	5U4G 0-95 6K7 0-70 20D1 0-60
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7412 7413	20p 30p	74121 74122	28p 48p	74365 74366	150p 150p	74LS298 74LS373	249p 200p	74C221 4000 SE	175p	CA3130S	375p		130p 155p	BC179 18p	MJ491	200p 225p	2N696 2N697	35p	*2N5087 *2N5089	27p 27p	1N4001/2 1N4003/4
7414	60p	74123	55p	74367	150p	74LS374	195p	4000 31	RIES 15p	CA3140E	70p		175p	*BC182/3 10p *BC184 11p	44 100 00	100p	2N697	25p 45p	*2N5172	27p	1N4005
7416 7417	27p 27p	74125 74126	55p 60p	74368 74390	150p 200p	81LS95 81LS96	120p	4001 4002	17p	CA3160E FX209	75p 7 50 p	RC4151 4	400p	BC187 30p	MJ3001 *MJE340	225p 65p	2N706A 2N708A	20p	2N5179 2N5191	27p 83p	1N4006/7 1N5401/3 1
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7475 7476	36p 35p	74178 74180	160p 93p	74LS139 74LS151	60p	74C08 74C10	27p 27p	4042 4043	80p 90p	15V 7815 18V 7818	90p 90p		00p	VAT	RATES.	A II :	tame at	90/ 1	EVAED	T	
7480	50p	74181	200p	74LS153	60p	74C14	90 p	4044	90p	24V 7824	90p	24V 7924 1	00p	VA. /	MIES.					ı ma	arkea *
7481 7482	100p	74182 74184 A	90p 150p	74LS157 74LS158	60p	74C20 74C30	27p 27p	4046 4047	110p 100p	100mA 5V 78L05	TO-92	100mA TO 5V 79L05 I	80p			wn	ich are	at 12	±%		
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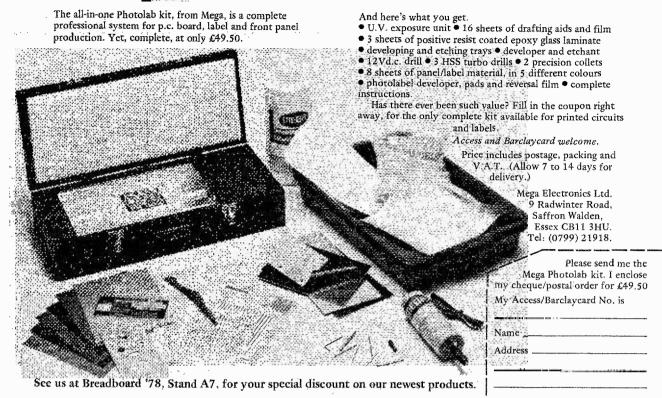
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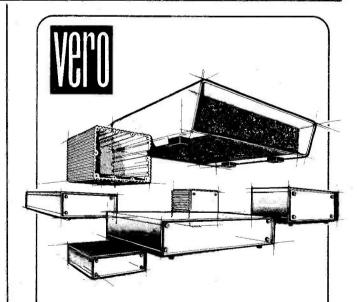
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4023	17p	4086	82p	4558	117
4024	76p	4089	150p	4559	388
4025	17p	4093	50p	4560	218
4026	180p	4094	190p	4561	65
4027	55p	4096	105p	4562	530
4028	72p	4097	372p	4566	159
4029	100p	4098	110p	4568	281
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7413	30	52	7483A			74148	109	1	74251		90	the remaind	er of th
7414	51	130	7484	97		74150	99		74253		105	column is no	ot OST
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7428	35	32	7497	185		74162	92	130	74367			matching to	
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7443	115	1	74113		38	74172	625	t	MISC	FILI	ENY	diode	21p
7444	112	ì	74114		38	74173	170					10 for	15 0 p
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7451	17	24	74123	48	1	74182	160	1	to 150M			November)	
7453	17		74124			74183		210				send 45p to	
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2N1303	0·80 2N3442	1 · 45 2N4123	0·19 2N5294	0-44 AF115	0.70 AC184 0.12	CA3001 4 25	CA3068 3 80	LM360N 3-00	LM1305N 1-52	0.30	SN76023ND
2N1305	0·80 2N3565	0·25 2N4124	9·19 2N5401	0-44 AF118	0.70 BC184L 0.15	CA3002 3:30	CA3070 1.90	LM370N 3:30	LM1307N 1 22	LM78L15CZ	1 30
2N1501	9 35 2N3566	0-25 2N4125	n.49 2N5416	1 65 AF124	0 70 BC205 0 17	CA3005 2:50	CA3071 1-90	LM371H 2:35	LM1310N 2-10	0 · 30	SN76033N2-35
2N1613	0 30 2N3567	0.25 2N4126	a 19 2N5447	6-16 AF139	0 75 BC212A 0 15	CA3006 4-60	CA3072 1-90			LM78224CZ	SN76110N1 - 30
2N1637	9·72 2N3638	9 17 2N4235	1-35 2N5448	0-16 AF200	1-30 BC212LA 9-18	CA3007 4-15	CA3075 1 70				
2N1890	0 30 2N3639	2144200	33	0 20 AF201	1-30 BC213B 0-15			LM373N 3:35	LM1458N 0 45	0.30	SN76115N1 65
							CA3076 2-12	LM374N 3 35		MC1035P 1 90	SN76116N1 - 80
2N1893	0 30 2N3644	0 40 2N4237	1-65 2N5457	0 35 AF239	0-70 BC213LA 0-17	CA3012 1-65	CA3080 1 85	LM377N 1-80	1 M1900N 1 . 94	MC1327P 1 · 70	SN76131N1 30
2N1991	1 · 10 2N3662	0·25 2N4240	1 70 2N5458	9 35 AF240	1 · 25 BC214 0 · 17	CA3013 1-85	CA3080A 2:10		LM1812N 6-20	MC1330P 1 18	SN76226N1 · 68
2N2193	0 50 2N3663	9 · 29 2N4250	● 26 2N5555	0 65 AF279	9-88 BC214L 6-18	CA3014 2 20	CA3086 0:50	LM378N 2-40		MC1352P 1 20	SN76227N1 · 30
2N2194	6-42 2N3702			6 55 AF280	0.95 BC237B 0 15	CA3018 0-75	CA3088F 1-87	LM379S 4-25			SN76228N1 - 55
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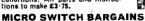
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ohms.
Complete with insulated probes, leads, battery, circuit diagram and instructions.

Unbelievable value only £6.50 + 50p post and insurance FREE Amps ranges kit enable you to read DC current from 0-10 amps. directly on the 0-10 scale. It's free if you purchase quickly but if you already own a mini tester and would like one

TERMS: Cash with order---but orders under £6 must add 50p to offset packing, etc.

BULK ENQUIRIES INVITED. PHONE: 01-688 1833.

J. BULL (ELECTRICAL) LTD

(Dept. P.W.), 103 TAMWORTH RD., **CROYDON CR9 1SG**

Our monthly Advance Advertising Bargains List gives details of bargains arriving or just arrived—often bargains which sell out before our advertisement can appear—it's an interesting list and it's free—just send S.A.E. Below are a few of the Bargains still available from previous lines.

Pot Cores. These are ex-unused equipment. They contain the bobbins. Three sizes available.

		Diameter	Thickness	Price
	2243	4 · 5 cm	3.0 cm	81 p)
FX	2242	3.5 cm	2 · 3 cm	70p per pa
	2240	2 · 5 cm	1 · 6 cm	60p

Quantity Discounts apply.

Component Panel Ref. 3055. Taken from unused P.S.U.'s, these contain 4 × 2N 3055 power transistors with mica insulators all on heat sink and 4 × 3W type variable pots. preset type with spindle locks. Real bargain at £1 ·08.

Component Board 421. Again from unused equipment, major items on these are two-power silicon transistors, Motor Rola ref. SJ. 5433 mounted on a heat sink with mica insulators, also behind the panel are two power rectiflers ST NS 1008. Price 950.

Heavy Duty 3 Core Appliances Lead. 15 Amp wire 6ft long, conventional yellow green, brown and blue cores, grey puc outer, prepared ends, this flex normally sells at 30p per metre. 10 Jeads for £2.50 + 20p. Post £1:00. Good quantity available.

E.H.T. Mains Transformer. With inductance control.

30p per metre. 10 leads for £2:50 + 20p. Post £1:00. Good quantity available.

E.H.T. Mains Transformer. With inductance control normal primary and output voltage 3:5kv. The core, however, is made of a very good quality grain oriented transformer steel, and its flux can be varied by applying a DC voltage to the lower bobbin. We are not sure how much the output voltage may be increased or decreased but using a yout battery we seem to get a rise or fall of about 50 volts. These transformers are unused ex-P.S.U.'s which we are breaking down. Price £4:35.

Music Centre Dust Cover. Size 12" × 10½" × 1½" with attachments for hinging. Price £3:95. Callers only.

Hi Fi Console. This. Is a pleasingly designed shelving arrangement which could tidy up your equipment, sorry but it's another callers only item but a real bargain at £6:50.

Battery Charger Kit. Soon ihe dark nights will be with us and chances are your battery will become gradually discharged. Keep it topped up at low cost from the mains. Our kit consists of transformer, full wave rectifier, charging meter and battery clips. Bargain price £4:50.

Electrical Wiring Cables. 2:5mm twin and earth, flat p.v.c. covered grey outer, 100 metre coils, price £15:60. This is the cable you need for ring main circuits but for lighting a smaller fum cable will do. We can supply this at £9:00.

Power Packs for the Telephone Answering Machines have just arrived, these isolate the machine from the mains and provide the correct voltages for driving the record and layback motors, etc. On metal chassis with voltage selector and fuse, these have a plastic cover to make them sale. Not new of course but fully guaranteed. Price £5:86.

and fuse, these have a plastic cover to make them sale. Not new of course but fully guaranteed. Price £5-£6.

Telephone Answering Machines. We have sold all last month's delivery and the new loft we find rather varied. There are some without cases, some with stightly broken cases and some which look perfect. The description we gave in last month's newsletter cannot apoly to this new lot. So we now restate this as follows:— "Telephone Answering Machine, used, but so far as we can see complete and quite possibly in working order. However, we are allowed to supply these only for breaking up, they should be very suitable for conversion to open reel tape recorder, background music machine, echo chamber, etc. The list of paper on request). They are all untested but we standed to replace any major item in the machine set in our rugues in essistence to fault we will be suitable to the case stightly broken but substantially whole suitable to so the case stightly broken but substantially whole suitable to so the case stightly broken but substantially whole suitable so the suitable suitable so the suitable suitable so the same stightly broken but substantially whole suitable so the suitable s

whole £10:90. Machines with unbroken outer cases £12:50.

wall Mally machines with very good, new looking outer cases £14:50. Post £2:00 per machine less case, others £2:50.

Wall Mounting Thermostat. The Satchwell room stat. This will handle mains heaters up to a total of 20 amp and is settable for normal air temperatures between 30-80°F. Suitable also for greenhouse control. Nicely finished in white enamel. Also has a cover to prevent interference with control setting. Price £3:00.

10 r.p.m. Motor with 230v mains coil, not like the usual of these geared motors, this has a good length of £" shaft price. £3:00.

10 r.p.m. Motor with 230v mains coil, not like the usual of these geared motors, this has a good length of £" shaft price. £3:00.

10 r.p.m. Motor with 230v mains coil, not like the usual of these geared motors, this has a good length of £" shaft price. £3:00.

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10 r.p.m. Motor with 230v mains coil, not like the usual of these geared motors, this has a good length of £" shaft price. £3:00.

11 r.p.m. Motor with 230v mains coil, not like the usual of these geared motors, the shaft price for the gear and price of the little shaft price. £3:00.

12 r.p.m. Motor with 230v mains coil, not like the usual of these geared motors, the shaft price for the shaft price. £3:00.

12 r.p.m. Motor with 230v mains coil, not like the usual of these geared motors, the shaft price for gear has been completed and the shaft price. £3:00.

13 r.p.m. Motor with 230v mains coil, not like the usual of the gear and restrict price. £3:00.

14 r.p.m. Motor with 25:00.

15 r.p.m. Motor with 25:00.

16 r.p.m. Motor with 25:00.

17 r.p.m. Motor with 25:00.

18 r.p.m. Motor with 25:00.

18 r.p.m. Motor with 25:00.

18 r.p.m. Motor with 25:00.

19 r.p.m. Motor with 25:00.

19 r.p.m. Motor with 25:00.

10 r.p.m. Motor with

Price £3 35.

4 Hour Motor, beautifully made by Sangamo. This is 00-240v mains driven motor with gearbox together in one ousing, size approx. 1½" dia, by 1½" deep. If you are commplating making a 24 hour switch with a lot of on/offs, hen this is obviously the motor. Price £1 89.

BENTLEY ACOUSTIC CORPORATION LTD.

7ª GLOUCESTER ROAD, LITTLEHAMPTON, SUSSEX All prices inclusive of V.A.T. at 121% Telephone 6743

OA2 1.20	6AM8A .70 /	6F25 1.00 i	7R7 2:00 r		50CD6G .
OB2 -40	6AN8 .78	6F26 -45	7V7 2.00	18 1.25	4.00
OC3 ·50	6AQ5 -75	6F28 ·85	7Y4 ·80	19AQ5 -65	50EH5 85
OZ4 ·55	6AQ8 .50	6F32 1.00	7Z4 ·80	19BG6G	50L6GT1 · 00
1A3 ·60	6AR5 1.05	6G6G 1.00	8D2 .50	1.00	66KU 1.00
1A5GT -55	6AS7G 1.50	6GH8A 80	8D8 ·52	19G6 6-50	72 .70
1A7GT -60	6AT6 -60	6GK5 .75	9BW6 -90	19H1 4·00	77 •45
1B3GT -55	6AU6 -62	6GK6 2.00	9D7 ·70	19Y3 -40	85A2 1·40
1C2 1.00	6AV6 .65	6GU7 ·90	9U8 ·45	20D1 ·70	85A3 1 40
1D5 1.00	6AWSA1-15	6H6GT -50	10C2 ·70	20D4 2.50	90C1 1.50
1G6GT 1 00	6AX4 75	6J5GT ·65	10C14 ·60	20F2 ·85	108C1 40
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1L4 25	6BA6 -65	6J7G -50	10DE7 .80	20P1 1.00	215SG 1 00
ILD5 .70	6BC8 -90	6J7M · 65	10F1 1.00	20P3 1.00	807 1.10
1LN5 -70	6BE6 -70	6JU8A -90	10F9 -65	20P4 ·84	956 -50
1N5GT 75	6BG6G 1.00	6K7G 50	10F18 -65	20P5 1 50	1625 2-50
1R5 -50	6BH6 1.10	6K8G 50	10L14 ·50	25A6G 1 00	1821 1 00
184 -40	6BJ6 ·75	6K8GT 55	10LD11 75	25L6G 1.00	5687 2.00
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1T4 ·30	6BN8 1.50	6L7 1.50	10PL12 .75	25Y5G ·60 25Z4G ·50	
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3D6 ·40			12AT7 52	30C17 -90	7025 2.00
3Q4 80	6BY7 -45	6P15 · 48 6Q7G · 75	12AU6 50	30C18 2-25	7193 -60
3Q5GT -70	6BZ6 1·50 6C4 ·50	607GT 75	12AU7 -62	30F5 ·70	7475 1.20
384 ·65	6C6 -45	6Q7(M) 75	12AV6 -60	30FL2 2 25	9002 -55
3V4 1.00	6C9 2-00	6R7G -70	12AX7 -62	30L1 ·39	9006 -45
4CB6 -75	6C10 1.00	68A7 .70	12BA6 50	30L15 -75	A3042 6.00
4GK5 ·75	6CB6A 65	68C7GT1 · 00	12BE6 ·85	30L17 -70	ACPEN3.00
5CG8 -75	6C12 ·55	68G7 -70	12BH7 -68	30P4MR -98	AC2PEN
5R4GY 1 · 00	6CD6G 4.00	6SH7 ·70	12E1 8.50	30P12 ·74	1.20
5T4 2.00 5U4G 1.00	6CG8A -90	68J7 -70	12J5GT ·40	30P19/	AC2PEN/
5U4G 1.00	6CL6 .75	68K7 1.00	12J7GT -70	30P4 ·90	DD 1 00
5V4G 1.00	6CL8A 95	68K7GT 70	12K5 1.50	30P16 ·50	AC6PEN
5¥3GT -65	6CM7 ·70	68L7G 2-00	12K7GT - 50	30P18 ·50	1.00
5Z3 1·40	6CS6 .75	68N7G 2.00	12K8 ·75	30PL1 2.20	AC/P4 1.50
5Z4G ·75	6CU5 .90	68Q7 ·70	12Q7GT 50	30PL12 ·62	ACTH11.00
5Z4GT 1.00	6D3 -75	6U4GT 1-00	128A7 ·75	30PL131-30	AL60 1 50
6/30L2 ·90	6DE7 -90	6U7G -55	128C7 -50	30PL141-50	ARP3 .60
6A8G 1 40	6DT6A 85	6U8 .50	128G7 -55	30PL151.30	ATP4 50
6AC7 -70	6EW6 .85	6V6G -50	128H7 ·50	35A3 1.00	AZ1 ·50
6AG5 ·35	6E5 1.00	6X4 95	128J7 ·60	35C5 80	AZ31 1.00
6AG7 70	6F1 -80	6X5GT .50	128K7 -60	35D5 -90	AZ41 50
6AH6 ·70	6F6G .70	6Y6G .95	128N7GT	35L6GT -80	B36 2 00
6AJ5 -70	6F12 ·70	6Y7G 1.25	2.00	35W4 - 55	B719 ·50
6AJ8 -55	6F14 · 90	7A7 1.00	12SQ7 -80	35 Z 3 -80	B729 90
6AK5 .45	6F15 -85	7B6 1.00	128Q7GT	35Z4GT ·70	BL63 2.00
6AK6 1.50	6F16 1.00	7B7 1.00	-80	35Z5GT -80	CL33 2.00
6AK8 -48	6F18 -60	7D6 2.00	128R7 ·75	43 1.25	CV6 -60
6AL5 -25	6F23 1 00	7F8 2.00	13D8 2.00	50B5 ·95	CV988 -25
6AM6 -70	6F24 ·80	7H7 1.00	14H7 ·75	50C5 -70	CV988 -25
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	CY31 1 00 D1 50	EBF80 1 00	EF183 -50	HY90 .55	1.00	UF41 1.00	AA119 -		BF163 - 23
	D63 ·50	EBF83 -45	EF184 .50	KT2 .90	PEN46 1 . 00	UF80 -40	AA120 ·	18 1	BF173 44
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			EH90 75		2.00	UF89 ·52		21 1	BF181 ·47
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' l	DD4 ·80	EC54 1.00	EL34 2.50	KT63 .70	PFL2001 .35	UM84 2.50	AC127	20	BFY51 ·23 BFY52 ·23
	DF83 ·75	EC86 84	EL37 3:00	KT66 3.50	PL33 1 00				BY100 .21
	DF91 ·30	EC88 ·84	EL41 1.00	KT71 1.00	PL36 -80				Daring 01
4.00	DF92 ·25	EC90 ·50	EL81 1 00	KT81 2.00	PL81 ·49	UU12 ·45			BY126 18
-85	DL96 1.00	EC92 1.00	EL83 1.00	KT88 6-75	PL81A .75	UY41 ·70			BY127 ·21
1.00	DH63 .75	EC97 -75	EL84 ·48	L63 ·65	PL82 -50	UY42 ·70			
1.00	DH76 .50	ECC32 1.00	EL86 .60	LN119 .75	PL83 ·50	UY85 ·70			BYZ10 ·30
-70	DH77 ·60	ECC33 2.00		LN152 -55	PL84 ·50	U10 1.00			BYZ11 -30
-45	DH81 1.00	ECC35 2.00		LN309 1 20	PL95 1.00	U12/14 1·15			BYZ12 · 30
1.40	DK32 -60	ECC40 1.00			PL504/500	U18 2.50			BYZ13 30
1.40	DK40 1.00	ECC81 -52	EL360 2.50		1.05	U19 4.00			FSY11A · 26
1.50	DK91 .50	ECC82 -62	EL506 2.00	M8136 2.00	PL505 3-10	T25 1.00			FSY41A ·26
- 40		ECC83 -62	EL509 2.50	M8137 2.00	PL508 1.85	U26 ·90	ACY18	-35	OA9 ·14
1.20	DK92 1.00 DL33 .70	ECC84 -50	EM80 1.00	M8162 2:00	PL509 3-10	U33 1.75	ACY19	35	OA47 12
1.00		ECC85 -50	EM81 1.00	M8195 3.00	PL519 3.75	U35 1.75	ACY20	- 35	OA70 ·18
1.10	DK96 1.00		EM83 1.00	MHL4 1.00	PT4D 1.00	U37 2.00		-35	OA73 18
	DL63 .70		EM84 1.00	MRLD6 -99	PY31 -50	U81 -80			OA79 11
-50	DL82 1.00	ECC88 72	EM85 1.20	MX40 1.00	PY33/2 .50	U191 -50	ACY28		OA79 :11 OA81 :11
2.50	DL92 65	ECC91 .35	EM87 1.45	N150 1.00	PY80 .50	U251 1.00			OA85 ·11
1.00	DL94 1.00	ECC1891 · 00	EMM803	N308 -98	PY81 -60	T 301 1.00	AD161		OA90 ·14
2.00	DL96 1.00	ECC804 · 90	2.50	N709 ·48	PY82 -40	U403 ·90	AF114		OA91 ·11
1 20	DM70 1.25	ECC8072.80	EY51 80	P61 -60		U404 ·75	AF115		0A95 ·11
3.65	DM71 1.75	ECF80 · 65	EY81 1.50			U801 1.00	AF117	-23	OC36 1.00
2-00	DW4 1.15	ECF82 50	EY83 1.50	PABC80 ·45	PY88 1.12		AF121	-35	OC44 ·35
2.00	DY51 2.00	ECF86 80	EY86/7 ·45	PC86 ·80	PY500A 2-05		AF124		CC70 -14
2.00	DY87/6 ·52	ECH 35 2 · 00	EY88 1.00	PC88 -80			AF180	-56	OC71 20
4.70	DY802 50	ECH42 1-00	EY91 50	PC92 ·65	PY800 .60			64	OC72 -13
2.00	E80CC 4.75	ECH81 .55	EY500 1.45	PC95 1.00	PY801 .60	VU111 1.00	AF186	16	OC74 -26
2.00	E80CF 6.00	ECH83 1-00		PC97 ·75	PZ30 -50	VUI20 1.00	BA115		OC75 ·13
6.75	E80F 5.50	ECH84 -75	EZ85 .50	PC900 ·65	QQV08/10	VU133 1.00	BA116	.21	
2.00	E81CC 2-00	ECL80 .55	EZ40 1 00	PCC84 · 39	2.00	W107 1.00	BA129	.14	
- 60	E82CC 2.00	ECL82 -60	EZ41 1.00	PCC85 ·47	QS95/10	W729 1.20	BA130	-12	
1.20	E83F 3.50	ECL83 1.50	EZ80 -42		1.00	X41 1.00	BA148	-20	
- 55	E88CC 1.20	ECL84 .90	EZ81 -45	PCC88 -61	QV04/73·00	X66 2.00	BA153	-18	OC78D 18
- 45	E92CC 4-50	ECL85 -80	EZ90 -95	PCC89 -49	QVO6/20	1	BC: 07	14	OC81 ·30
6 · 00	E180CC5 00	ECL86 -64	FC4 1.00	PCC189 -60	4 70	Transistors	BC108	.14	OC81D -30
3.00	E180F 5.50	ECLL800	GY501 1.40	PCF80 -80	R10 5.00	& Diodes	BC109	-14	OC82 ·13
N .	E182CC5 50	10.00	GZ30 ·75	PCF82 ·45	R19 75	1N4744 ·16	BC113	-30	OC82D ·13
1.20	E188CC5 · 00	EF22 1.00	GZ32 1.00	PCF84 ·70	UABC80 - 45	2N404 ·21	BC115	·18	OC83 ·23
in/~u	E280F12 · 50	EF40 2.00	GZ33 4.00	PCF86 -57	UAF42 .70	2N966 ·61	BCI16	-30	OC84 -28
1 00	E1148 .60	EF41 1.00	GZ34 2.25	PCF2001 · 55	UBC41 · 70	2N1756 -58	BCI18	.26	OC123 ·26
in	EA50 40	EF73 1.75	GZ37 4:00	PCF2011 45	UBC81 .55	2N2147 ·99	BCY10	-58	OC169 -50
n`i-00		EF80 -40	HABC80 -80	PCF801 ·49	UBF80 -50	2N2297 -26	BCY12	-58	OC171 ·40
1.50			HL13C 60	PCF802 -80	UBF89 ·39	2N2369 ·16	BCY33	-23	OC172 41
	EABC80 .48		HL23 1 50	PCF8052 - 25	UBL21 2.00	2N3053 ·38	BCY34	-26	OC204 -50
11.00	EAC91 .55	EF85 -45	HT 65 T. 90	PCF806 -70	UC92 50	2N3121 2 · 90	BCY38	- 26	OC206 1.05
1.50	EAF42 1 · 00	EF86 -52	HL23DD . 68	PCL82 62	UCC84 -90		100		
- 60	EAF801	EF89 ·55	HL41 1.00		UCC85 -50		RANSISTO	R SE	TS:
-50	1.50	EF91 .70	HL41DD	PCL83 2-00 PCL84 -65	UCF80 -80	TPIS (ACID)	R AC154.	AC157	. AA120) 75p
· 50	EB34 .50	EF92 .70	1.00		UCH21 2:00		OC81D 8	2/0	CSI. £1 .00.
1.00	EB91 25	EF93 -65	HL42DD	PCL86 .85	UCH42 1 · 00	140CRon &	2/OC82 - 5	An. S	et of 3/OC83
-50	EBC41 1 · 00	EF94 ·62	1.00	PCL805 .85	UCH81 60		-,000	·	,
2-00	EBC81 1.00	EF95 ·45	JHN 309 1.70	PEN25 1 · 00	UCH81 60	1 tob.			
.50									

|CYIC 1.00 | EBC90 .60 | EF97 .90 | HVR2 1.00 | PEN45 1.00 | UCL82 .75 | 2N3703 .23 | BF158 .21

Special offer of EF50 valves, soiled, but new and tested, £1 each.

All goods are unused, tested, and guaranteed. Despatch charges:—50p on all orders below £25 in value. Orders over £25 post free. Orders despatched same day as received. Any parcel meured against damage in transit for 5p per parcel extra. Terms of business available or request. Many others in stock too numerous to list. Please enclose S.A.E. for reply to any queries. All prices subject to change without notice.

FANE NEW "POP" RANGE SPEAKERS

Improved appearance — higher sensitivity



12" 'POP' 40T Pual 45w £14-95 12" 'POP' 50H 50w £16.99 12" 'POP' £23.95 75 75w 15" 'POP' 65 70w £25.95 15" 'POP' 80 80w £31.95 18" 'POP' 100 100w £52.75 18" 'POP' 150 150w £57.95 SPECIALIST RANGE

Each designed to prothe individual duce sound for its purpose. Robust Cast Alu. Chassis. * As reviewed in Int. Musician.

Linen Cone surround

Rec. Price **£29 · 95** 12" DISCO/80 80w* Fitted large Tweeter 12" DISCO/100 100w Cone €31.95 12" GUITAR/80B , Prs rec for Sass Guitar

12" GUITAR/80B , Prs rec for Sass Guitar
Dual Cone. For L28.95
Dual Cone. For L28.95
441.95 12" GUITAR/80L 80w* For Lead £28·95 12" PA/80 80w Dual Cone. seneral purpor 15" BASS/85* 85w For E £41 · 95 £44.50 15" BASS/100 100w

HIGH FREQUENCY

HORNS J44 Range: 2.5KHz-15KHz Power: 50w with
HPX2R
30w with HPX1R
Imp: 8 ohms
Size approx Size approx 3½" x 3½" x 3" J73 Range: 2 5kHz-20kHz Power: 50w with HPX IR Imp: 8 ohms

104 Range

2KHz-15KHz
Power: 50watt
with HPX1R
70 watt with
HPX2R
Imp: 8 ohms
Size approx 10½" x 3½ x 7½" £16.95
920/2 Range: 1 KHz-18KHz Power:
Power: 100w with HPX1. Imp: 8 ohms
Size approx 100w with HPX1. Imp: 8 ohms Size approx 14" x 9" x 15" Rec. £62.95

HIGH POWER "CROSS-OVERS" HPXIR (3.5KHz) £3.65

Power: 50w with HPX IR Impedance or total impedance of Bass Drivers not to exceed 8 \(\Omega\$. Otherwise use series Horns or attenuation provided with HPX IR and HPX IR. AN ANUFACTURERS OF GROUP & DISCO EQUIPMENT 2 years guarantee on speakers & Horns. Rec Prices INCLUDE V LINEAR PRODUCTS LTD, ELECTRON WORKS, ARMLEY, LEEDS

Manufacturers & Export enquiries to:—
FANE ACOUSTICS LTD, HICK LANE, BATLEY, YORKSHIRE



AND NOW WE ARE PLEASED TO ANNOUNCE OUR

Christmas Bonanza

Prices reduced yet again to aid your Xmas shopping "PRICES HELD TO DEC. 31st. ONLY"

PLEASE NOTE OUR NEW MAILING ADDRESS:-

FLEET HOUSE—WELBECK STREET WHITWELL - Nr. WORKSOP - NOTTS Tel: (0909) 720695652 TELEX: 547616 FLEET G

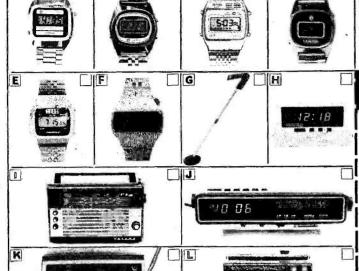
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level input sensitivity provides good quality reception with integral aerial in even poor signal areas. Supplied with Cigar lighter adaptor for car 12V supply Take off, Mains lead, External ae attenuator and integral detachable aerial, Colour brochures available S.A.E. CHRISTMAS OFFER PRICE: £59 40 + £1-75 P & P

BY TICK/S IN BOX/FS.

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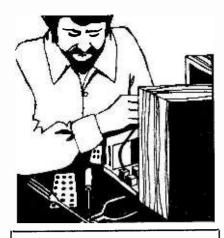
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105	3.0	8 · 56	1 - 32		
106	4-0	11 - 41	1.50		
107	6.0	15 - 66	1 64		
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PR	IM 120/240V S	EC 120/2	40V CT
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*07	20	4 · 40	0.79
149	60	6.70	0.96
150	100	7 - 61	1.14
151	200	11 - 16	1.50
152	250	13 28	1.84
153	350	16.43	1.84
154	500	20 - 47	2-15
155	750	29 - 06	ÕÄ
156	1000	37.20	ÕÄ
157	1500	51 - 38	ŎÂ
158	2000	81 - 81	ŏÃ
159	3000	86 - 66	ŏÃ
	Volts require		

State	Voits requ	ired 115V or	240V.
HIGH	VOLTAG	EISOLATO	R
F	rlm 200/22	OV or 400/440	V
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60	243	6 · 70	1.32
350	247	16-43	1 84
1000	250	37 - 10	ÖÄ
2000	252	6.81	ŎÂ

		30 VO	LT RANGE	
	Pri 22	0/240 Sec	0-12-15-20-24-	30V Volt-
	ages a	ıvailable 3.	4. 5. 6. 8. 9. 1	0. 12. 15.
	18, 20,	24, 30V or	12V-0-12V & 1	5V-0-15V.
			£	P&P
	112	0.5	2 · 64	0.78
	79	1.0	3 57	0.96
	3	2.0	5.77	0.96
	20	3.0	6 · 20	1 · 14
	21	4.0	7 - 99	1 - 14
	51	5.0	9.87	1 · 32
	117	6.0	11 17	1 45
-	88	8.0	14.95	1 64
	89	10.0	17.25	1 · 84
		60 1/0	TRANCE	

	W V U	LI KANGE	
Pri	220/240V 5	Sec 0-24-30-	-40-48-60V
Volt	ages available	e 6, 8, 10, 12,	16, 18, 20,
24,	30, 36, 40,	48, 60 or 2	4V-0-24V
or 30	V-0-30V		,
Ref	Amps	£	P&P
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126	1.0	5 · 91	0.96
127	2.0	7.60	1.14
125	3⋅0	11:00	1 · 32
123	4.0	12 - 52	1.84
40	5.0	15 · 84	1.64
120	6.0	18 - 06	1.84
121	8-0	25 · 56	OA
122	10.0	29 · 55	OA
189	12.0	34 · 06	OA

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	115-210-24		4.01 0.96
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84 1000 0-	115-200-22	0-240 1	8.76 2.08
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U-DEC 'A' 450p*
1000, 2200pF 28p each. SILVER MICA (pF)

JACKSONS VARIABLE CAPS.

CERAMIC TRIMMER CAPACITORS 2-7pF; 4-15pF; 6-25pF; 100KHz 8-30pF 20p 455KHz 100KHz 455KHz 1MHz 385p 323p MINIATURE TYPE: 2·5-6pF; 3-10pF; 3-30pF; 10-40pF 22p 5-25pF; 65pF; 88pF 30p 1 - 80MHz 385 1 · 6MHz 3 · 2768MHz 395p 323p COMPRESSION 3-40pF; 10-80pF 22p 25-200pF 33p 100-500pF 45p 4 · OMHz 323p 4·032MHz 4·032MHz 4·433619M 5·0MHz 323p 135p 355p 275p 395p 8-083333M

TRANSFORMERS* (Mains Prim. 220-240V) 6-0-6V 100mA; 9-0-9V 75mA; 12-0-12V 100mA

95p.
8VA type: 6V-5A 6V-5A; 9V-4A 9V-4A;
12V-3A 12V-3A; 15V-25A 15V-25A 195p.
12VA; 4-5V-1-3A 4-5V-1-3A; 6V-12A 6V-12A 12V-5A 12V-5A; 15V-4A 15V-4A 15V-4A 20V-3A 20V-3A (20p pap) 220p 24VA: 6V-1 5A 6V-1 5A; 9V-1 2A 9V-1 2A; 12V-1A 12V-1A; 15V-4A 15V-4A; 20V-3A 20V-3A (45p pap) 290p

50VA: 60-4A 69-4A; 9V-2-5A 9V-2-5A; 12V-2A :2V-2A; 15V-1-5A :5V-1-5A; 20V-1-2A : 25V-1A :25V-1A; 30V-8A 30V-8A (50p p4p) 350p. 100VA: 12V-4A (2V-4A; 15V-3A 15V-3A; 20V-2-5A 20V-2-5A; 30V-1-5A 30V-1-5A; 40V-1-25A; 50V-1A 50V-1A (60p p&p) \$50p

(N.B. P&P charge to be added above our normal postal charge.)

DENCO COILS
Dual Purpose 'DP'
VALVE TYPE
Ranges: 1-5 BI, YI,
Rd. Wht. 85p
6-7 B, Y, R 75p
1-5 Green 92p
'T type (Transistor Tuning),
Ranges: 1-5 BI, YI,
Rd. Wht. 92p B9A Valve Base 25p RDT2 92p RFC 5 chokes 91p RFC 7(19mH) 96p 1FT 13/14/15/16 17 85p 1FT 18/1-6 or 465 99p TOC1 86p MW 5FR 82p MW/LW 5FR 183p

POTENTIOMETERS (AB or EGEN) Carbon Track, 0.25W Log & 0.5W Carbon Track, 0.25W Log of Linear values 500Ω , 1K & 2K (LIN ONLY) Single 5KΩ-2MΩ single gang
5KΩ-2MΩ single gang D/P switch
5KΩ-2MΩ dual gang stereo
SLIDER POTENTIOMETERS

TRANSISTORS

AC107* AC117*

AC125* AC126*

SLIDER PUTENTIONETERS
0:25W log and linear values 60mm track
5KΩ-500KΩ single gang
10KΩ-500KΩ Dual gang
80p
Self-Stick graduated Alum. Bezels
22p PRESET POTENTIOMETERS
0-1W 50Ω-2-2M Mini. Vert. & Horiz.
0-25W 100Ω-3-3MΩ Horiz.
0-25W 250Ω-4-7MΩ Vert.
} larger 8p 10p 10p

Carbon Noise 99 100+ 5p 1p 1 5p 4p 4p 8p

HEAT SINKS* TO5 85°C TO92 TO5 Silicon Grease 12p 48p 5ml. Tub TO18 12p 20ml. Syringe 125p TO220 22p Insulation Kit for TO3, TO66 TO66 or TO220 3p Kit

EARPHONES FIGARO GAS and | Magnetic | SMOKE | DETECTORS | Types: 109, 308, 812 or | 3-5mm | 18p | 813 | 415p each | Crystal | 33p | Sockets for above | 25p | 2.5mm

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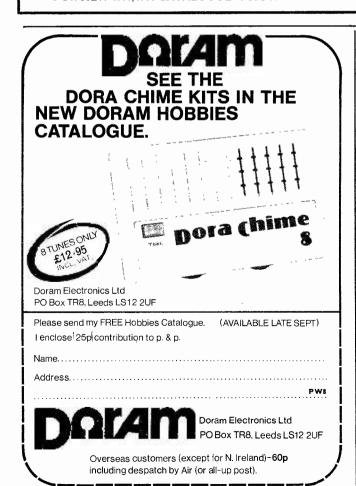
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A SELECTION FROM OUR STOCKS OF FULLY GUARANTEED FIRST QUALITY VALVES

RR	IB3GT		6AH6	0.95	6BU8	0 - 85]	6J5GT	0.80	I2AX7	0.55	ECC84	0 60	EL33	2.50	OD3	0 · 75	PL508	1 · 30
154	IR4			0.65	6BW7	1.00	616	0 - 55	12AY7	0 - 85	ECC85	0.48	EL34	0.95	PABC80	0 45	PL802	2.80
ISS																		
174																		
104																		
125													EL83	0.60				
1.20 1.20													EL84	0.45		0 · 50		
2CW4 4-50 6AN6 0.85 6CG7 0.70 6SG7 0.80 12X4 0.50 ECF20 0.90 ELF504 0.60 6AQ5 0.65 U25 1.00 e6 6AQ5 0.75 6SK7 0.80 12X4 0.50 ECF20 0.95 EM80 0.65 EM80 0.65 PCC85 0.60 U26 1.00 6AR5 1.00 6CM8 1.50 6SN7GT 0.70 1223 0.70 ECF80 0.95 EM80 0.65 EM80 0.65 PCC85 0.60 U26 1.00 6AR5 1.00 6CM8 1.50 6SN7GT 0.70 1223 0.70 ECF80 0.95 EM80 0.65 EM80 0.65 PCC88 0.65 VAF41 0.80 6AS7G 1.20 6CO7 1.20 6SQ7 0.80 19AQ5 0.75 ECH42 1.10 EF80 0.65 ECH42 1.10 EM87 1.00 PCC189 0.75 VAF41 0.80 6AS7G 1.20 6CO7 0.80 19AG5G 0.50 ECH81 0.55 ECH42 1.10 EM87 1.00 PCC189 0.75 VAF41 0.80 6AS7G 1.00 6CO 6AS7G 0.85 6U4GT 0.80 3SA3 0.70 ECH83 0.60 ECH83 0.55 ECH42 0.50 ECH83 0.55 ECH42 0.50 ECH83 0.55 ECH42 0.50 ECH83 0.55 ECH42 0.50 ECH83 0.50													EL86	0.75		0 · 95		
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\$\frac{354}{5AQ5}\$ 0.75 & 6AU6 & 0.50 & 6CS7 & 0.85 & 6U4GT & 0.80 & 35A3 & 0.70 & ECH80 & 0.60 & EYS1 & 0.60 & 0.65 & UBF80 & 0.60 & 0.65 & 0													EM87	1.00	PCC189	1.00	VBC41	0.70
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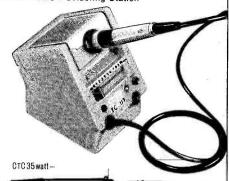
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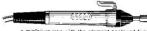
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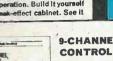
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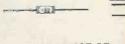


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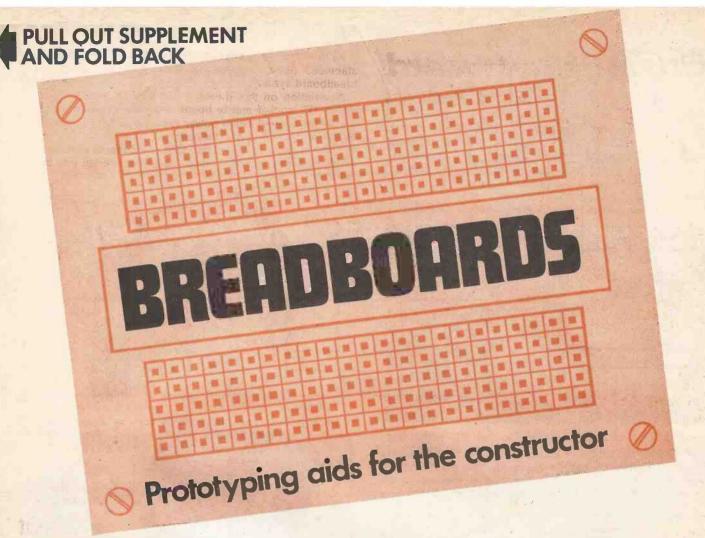


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EXPERIMENTER

The usefulness of any universal plug-in breadboard system can be greatly improved if the boards are mounted onto a box containing a set of stabilised power supplies of the most commonly used voltage levels. Several commercial models are available which provide the constructor with these facilities but they all tend to be rather expensive.

The philosophy behind the PW Experimenter is to provide a reasonably priced, easy to use universal system which is complete with power supplies suitable for both TTL logic and standard op. amps. A small loudspeaker is also contained within the case as it was felt that any self respecting 'Wireless' breadboard system should have a speaker readily available.

Power Supplies

Three stabilised power supplies are contained in the Experimenter and these have been selected to provide the most useful voltages. A stabilised 5 volt supply capable of providing 1A is useful for any work using TTL logic chips, while a positive and negative pair of 15V supplies, with a common 0V terminal, provide the necessary balanced voltage rails for use with i.c. op. amps. To make these two supplies more versatile they are switched to give either ±12V or ±15V at 100mA each.

The power supplies are all similar and use i.c. regulators, fed from a simple full wave bridge rectifier circuit Fig. 1.

These i.c. stabilisers give adequate regulation with full overload protection, are very simple to use and cost very little to buy.

Construction

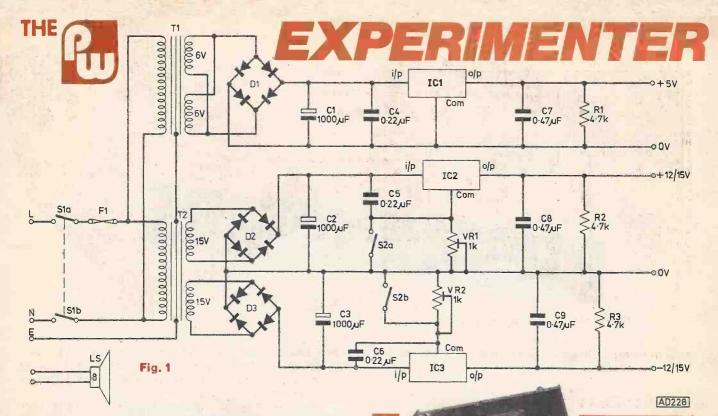
The stabilised supplies are built on a piece of Veroboard as shown in Fig. 2. The actual layout of the components is not critical in any way and could be altered to suit available components.

The 1A 5V positive regulator is mounted on a suitable small heatsink which is screwed to the bottom of the case. The two transformers are also screwed to the case bottom and the regulator board and smoothing capacitors C2 and C3 held in position by double-sided adhesive foam rubber pads.

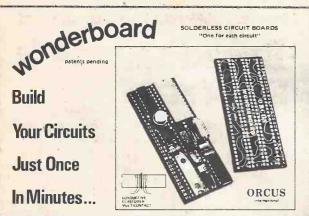
Suitable size holes in the back of the case take a mains fuse holder and the mains cable which is held securely by a suitable cable entry clamp. All soldered joints on the mains side should be sleeved with small rubber tubing and the fuse holder should be fitted with a suitable rubber boot.

The position of the speaker is marked on the case bottom, towards the front, and extra holes drilled to allow the sound to be heard. The speaker is fastened in place with epoxy adhesive.

The case chosen is the largest in the Bimconsole range



and has the advantage of a sloping front on which the universal breadboards can be mounted. The area available will allow almost any of the commercial systems to be fitted and although the prototype Experimenter used the new



It's crazy to build, unbuild, construct and destruct your circuits on expensive "Breadboards". Now very economically on WONDERBOARD, you plug your components into one side of the board, the wires into the other, and you install the finished circuit in your equipment. They're like PC boards, but no soldering (which is enemy No. 1 of prototypes). Change any wire or component any time without disturbing others. Up to six interconnecting wires and one component lead into one multicontact. WONDERBOARDS accept all IC's from 4 to 60 pins and discrete components too.

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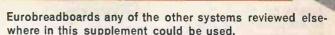
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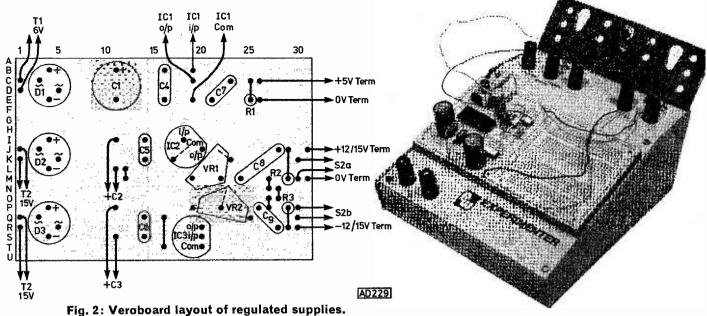


Suitable holes are drilled to take the terminals and the two switches, together with the mains indicator.

The final stage is to complete the wiring to the terminals

Company Addresses

Bandridge Ltd., 80a Battersea Rise, London SW11 1EH.
Boss Industrial Mouldings Ltd., 2 Herne Hill Road,
London SE24 0AU. Charcroft Electronics, Charcroft
House, Sturmer, Haverhill, Suffolk. Continental Specialities Corporation UK Ltd., Spur Road, North Feltham
Trading Estate, Feltham, Middx. TW1 40JW. David
George Sales, r/o 74 Crayford High Street, Crayford,
Kent DA1 4EF. E & L Instrument UK, 62 Queen Anne
Street, London W1M 9LA. Lascar Electronics Ltd., PO
Box 12, Module House, Billericay, Essex CM12 9QA.
Lektrokit Ltd., Sutton Industrial Park, Earley, Reading,
Berks RG6 1AZ. Michael Williams Electronics, 47
Vicarage Ave., Cheadle Hulme, Cheshire SK8 7JP. OK
Machine & Tool UK Ltd., 48a The Avenue, Southampton SO1 2SY. Rhopoint Ltd., Eastman House, 98102 Station Road East, Oxted, Surrey RH8 0AY.



and switches, fit the front panel onto the case and test the power supplies.

Applications

You will find your PW Experimenter an invaluable aid when trying out new ideas. Almost any component can be easily plugged into the various rows of contacts to make up circuits quickly and easily. However you should only use components which have clean leads free from solder blobs otherwise difficulty will be experienced in inserting the leads into the contacts and damage may be caused to the breadboard.

When inserting or removing integrated circuits from the board care must be taken to ensure that the leads are not bent or broken off, Follow the makers instructions supplied with the breadboard and you should find it simple to plug-up any circuit configuration.

* components

Resistors			
±₩ 5%			
4·7kΩ	3	₹1, 2, 3	
Potentiomete	#\$		
Vert. Skeletor			
1kΩ	2	/R1, 2	
	Par Heiseld Par		
Capacitors			
Polyester			
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0·47μF	·*	2// 0/ 3	
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Semiconduct	ors		(ja ka
Silicon Bridge			
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Regulators		S. P. Palitura de la Calaba. El composito de la Calaba	
78L12		C2	
79L12	1	C3	
7805	1	Cf	
Miscellaneou	•		
			470 V 90mm
811 /bmm dia	i. loudspeake	r (1); Case 214	t. min. toggle
(Dimouo1);	curobreaubu Imm nanol m	ounting fuse hol	der and 1 Δ firse
(1) Insulati	nn boot for	fuseholder (1); Cable entry
clamn to fit	mains cabl	e (1): Insulated	l terminals red
(2), blue (3)	black (2)	Fransformer 15	V + 15V 8VA
(Watford Ele	ctronics) (1)	: Transformer	5V + 6V 12VA
(Watford Ele	ectronics) (1); Heat sink (1)	; Indicator 28V
Dan 141 2 C	ore mains ca	ble.	
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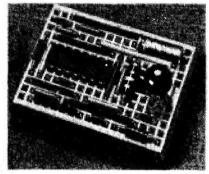
Hole for hole, top value! Lektrokit Breadboards are modular, so they can be linked together to form any size. With a pitch of 0.1", even the smallest breadboard—217L—can accept 8, 14, 16 or 18 pin Dil devices. You just take a component, choose a hole, and push it in.

		,
Model No.	Contacts	Price, each
217L	170	£3.25
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Eleven models, from TC-8 to TC-40 to
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TC-14, £3.25 for the TC-16, etc.
Test clip grips IC's without slipping or
shorting between pins—makes testing
IC's on boards easier, aids removing and
inserting DIP's without damage. Each IC pin can be brought up to a convenient contact post for test leads or probe connections.

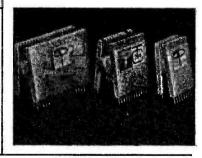


ektrokit Super Strip SS2. ONLY £11.05 inc p & p and VAT Super Strip accepts ALL DIP's—

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Super Strip has 840 contact points, combining a power/signal distribution system with a matrix of 640 contacts in groups of 5. Distribution system has eight bus-bars, each with 25 contact points.





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Survey of AVAILABLE BREADBOARD SYSTEMS

The use of some form of breadboarding system is as old as the art of wireless itself. However the modern system of specially designed pluggable socket systems is far removed from the panel pins in a wooden board of bygone days.

Although the modern systems will accept components having widely varying lead diameters it is essential that the leads are straight at the ends and free from solder. If possible it pays to use new components with full length leads rather than try to force short leads, covered with solder, into the contacts.

Integrated circuits often prove a stumbling block as it takes quite a force to insert or extract 16 pins simultaneously. Most socket manufacturers suggest a method of insertion and withdrawal and it is advisable to follow their recommendations to avoid damaging the i.c. leads.

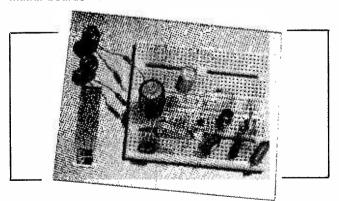
In the following review of available breadboard systems, we have, wherever possible, tried actual samples to see just how easy it is to insert component leads into the contacts. The technical information given, such as contact resistance, etc has been taken from the manufacturer's own published literature. Prices quoted include VAT.

ACE

OK Machine & Tool

There are three models in the ACE series of breadboards, the differences being mainly in size and flexibility. ACE stands for All Circuit Evaluators, and all three models use combinations of plug-in terminal strips and distribution buses all on a 0.1 inch matrix. The various matrix boards are attached to a back plate which also carries two screw terminals for easy supply connection.

The smallest model the ACE 200-K has 728 sockets arranged in a conventional double row of five sockets tied together each side of a central strip. There are two such boards together with a two rail bus. The two larger models have 1,224 and 1,760 socket positions, utilising the same matrix boards as the smaller version.



The matrix boards are also available separately in a wide range of configurations. Moulded in acetal copolymer with nickel-silver contact strips the boards have a removable backing or can be mounted onto a board with screws which are supplied. With suitable combinations of the

bus strips and matrix boards almost any component can be used as long as its leads conform to a 0.1 inch matrix. Leads of up to 0.8mm diameter can be used.

The ACE 200-K is supplied in kit form which is simple to assemble, our sample took about 10 minutes. The retail price of the 200-K is around £13·20 while the largest model, the 218 costs around £32·65.

The ACE 200-K provides the amateur with a reasonably priced easy to use breadboard system which will cope with fairly complex circuits, and components were easily inserted into the sockets. The separate matrix boards and bus strips could be used to make up one's own design of universal breadboarding unit.

Lektrokit are also marketing these boards.

Bimboards

Boss Industrial Mouldings

This is a useful sized board which accepts most d.i.l. i.c. packages as well as any other component with leads spaced on a 0·1 inch grid.

The body is moulded in a blue plastics material with 47 rows of 5 interconnected contacts each side of a central strip across which i.c. packages can be fitted. Two rows of contacts are fitted along the edges of the board for power supply rails.

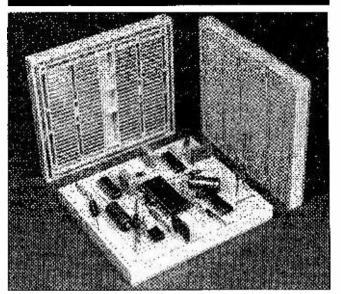
A simple plastics bracket is provided ready punched with various sized holes and slots to take switches, pots and other items which require a mechanical support.

Any number of these boards can be slotted together to make a larger working area for more complex projects.

Contact material is nickel-silver with a contact resistance of better than $10m\Omega$ and a current rating of 1A per strip.

The maximum working voltage between rows of contacts is 240 a.c. and inter-row capacitance is 0.5pF max. Each

THE NEW EUROBREADBOARD



Logically laid out to accept both 0.3" and 0.6" pitch DIL packages as well as Capacitors, Resistors, LED's, Transistors and components with leads up to .85mm dia.

500 individual connections in the central breadboarding area, spaced to accept all sizes of DIL package without running out of connection points.

4 Integral Power Bus Strips around all edges for minimum interconnection lengths.

Double-sided, nickel silver contacts for long life (10K insertions) and low contact resistance (<10m.ohms)

Easily removable, non-slip rubber backing allows damaged contacts to be rapidly replaced.

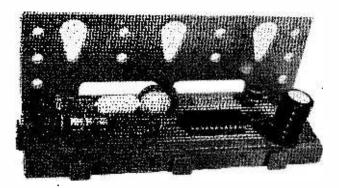
What other breadboarding system has as many individual contacts, offers all these features and only costs £5.80 inclusive of VAT and P.P. — NONE.

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(All prices inclu overseas orders		and P.P.	, but add 15	% for
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contact takes wires of between 0.25 and 0.85mm diameter and wirewrap sockets may be used to carry i.c.s if desired.

The Bimboard is a reasonably priced unit which is versatile and easy to use. Component leads can be inserted fairly easily without too much risk of bending and the vertical mounting bracket for switches and pots is a useful adjunct.

Bimboards also go under two other names; MW Breadboard from Michael Williams Electronics and Professional Prototype Board from RS Components.

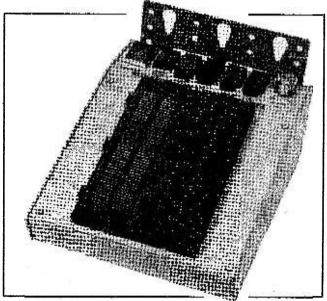
Typical retail price is around £9.70 including VAT. Bimboards are also available mounted on back panels with terminals fitted. Prices range from £22.68 to £42.12 for the 4 board version.

Breadbloc

Lascar Electronics

This unit uses one or two Bimboards mounted onto a sloping front panel of a Bimconsole into which is built two independent stabilised power supplies.

These supplies give 5V at 1A and ± 5 to 15V dual trackin g at 100mA per rail.



A mains switch, indicator and fuse are incorporated and connections to the power supplies are by means of 4mm sockets or push-button terminals.

The remarks made under the Bimboard review obviously apply to the Breadbloc unit while the power supplies make it virtually self-contained and increase its versatility.

The two Bimboard version retails for around £51.80 and the single Bimboard model for £43.16.

Bug System

E&L Instruments

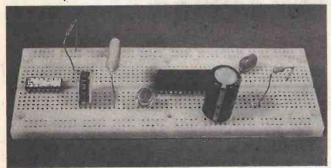
The three sizes of basic breadboard in this range both take any component with leads on a 0·1 inch matrix.

The largest, the SK10 takes up to eight 14 pin d.i.l. integrated circuits of the standard 0-3 inch width across pins. The contact strips are arranged in 63 rows of five linked contacts each side of the central strip. Two continuous rows of linked contacts are placed along each long edge of the base which is moulded in acetal copolymer. Contact resistance is $5m\Omega$ average.

The smaller SK50 unit has 33 rows of five linked contacts and correspondingly shorter continuous linked contacts for power rails. SK20 is a miniature socket.

Versions are available for permanent connection to p.c.b.s and these have tabs protruding from the contact strips downwards to allow soldered connections to be made through the p.c.b.

The basic boards are used in a very wide range of universal breadboarding aids including versions with the basic breadboard unit mounted onto a metal back panel with terminal posts fitted. Other types have built-in power supplies to suit many varied applications. Even more complex systems are available fitted with all sorts of extra equipment such as multimeters, potentiometers, switches and speakers. A version is also made especially for use with microprocessors.



All of these units are based around the three basic breadboard units, and, as a further aid to constructors, a p.c.b. version of the SK-10 unit is available as well as a double SK-10 pattern board with edge connector contacts.

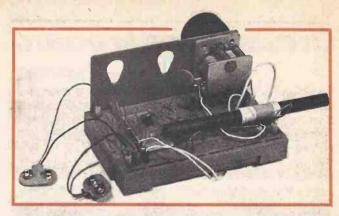
Prices range from £6.95 for the SK50 to £12.07 for the SK10. The universal design aids range from £15.55 for the smallest to £24.72 for the largest and the complete units with power supplies cost from £79.00 upwards with the top-of-the-range Elite 2 which has almost everything built-in costing a mere £1081.00.

DeCs

At the time of writing it has been announced that the manufacturers have gone into liquidation and the future of the DeC series is therefore in doubt. However stocks are held by a number of retailers and we feel that the following review is still valid, although no prices have been given for obvious reasons. Bandridge supply DeCs under their own name.

The S-DeC is intended for use with discrete components and has two sets of seven parallel rows of five interconnected contact strips mounted in a plastics box.

The μ -DeC and T-Dec are both intended for use with i.c.s as well as discretes. The T-DeC has provision for accepting one i.c. held in a special carrier while the μ -DeC takes two i.c.s.



The DeC range of pluggable boards should be familiar to readers of Practical Wireless as the simplest version, the S-DeC was used in a series of articles published during 1977 and the μ -DeC in the more recent μ -DeCnology series.

Eurobreadboards

David George Sales

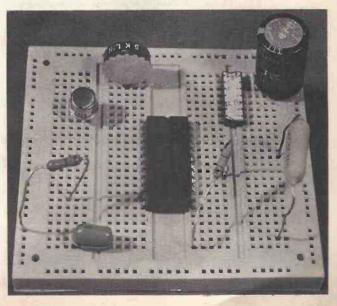
One of the newcomers to the breadboarding scene, the Eurobreadboard has 500 individual contacts in the main area with four power rail strips arranged around the outside. The contacts are arranged in four lines of 25 rows of five interconnected sockets. The basic module pitch is 0.1 inch with the spacing of the lines of contacts at either 0.3 inch or 0.6 inch pitch to accommodate all sizes of d.i.l. i.c.s

The body is moulded in a yellow plastics material with a non-slip rubber backing which is removable to allow access to the contact strips if necessary. Four fixing holes are provided if the unit is to be fastened onto a back panel but no slots are moulded into the edges to allow several boards to be linked together.

The contacts material is nickel silver with a contact resistance better than 10m Ω .

The Eurobreadboard offers versatility at a reasonable price. A wide variety of components including l.s.i. packages can be accommodated and the sockets will take leads of up to 0.85mm diameter without excessive force being needed.

Typical retail prices are £5.80 for one board.

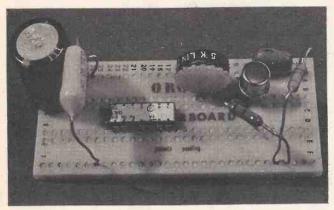


Orcus Wonderboard

Charcroft Electronics

Unlike the usual type of breadboarding system the Wonderboard uses elastomeric multicontacts instead of metal contact strips. The elastomeric contacts, made from a conducting foam rubber material, are moulded into a pattern of holes in a hard plastics material. Two different sizes of Wonderboard are available, the 12 i.c. "Small Wonder" and the 48 i.c. "Big Wonder".

Each hole containing an elastomeric contact is electrically



isolated from its neighbours and to use the board the component leads are inserted into the contact holes and the circuit wired up using a length of thin tinned copper wire threaded through the contact material.

Contact resistance is better than $10\text{m}\Omega$ with a current capacity of 7A. Breakdown voltage is 9kV with an insulation resistance of $10,000\text{M}\Omega$. The contacts will accept wires of 0.2 to 0.8mm diameter with up to six wires in each hole.

The Orcus Wonderboards offer an easy to use breadboarding system which, the makers suggest, could be used to make up a circuit which could then be potted in a clear potting compound to make a permanent unit. All sizes of d.i.l. i.c.s can be used together with any component with leads on a 0·1 inch matrix.

Typical retail prices are £2.80 for the "Little Wonder".

Proto-Boards

Continental Specialities Corp.

This is a large and versatile system. The basic units are the socket matrix boards and bus strips which are available in two different ranges.

The 'Quick Test Sockets' are available in ten different sizes, three double bus strips and seven socket matrix boards. The bases are moulded in a plastics material with a snap together joining system which allows boards to be connected together to produce any size of system as required. The contact strips are made from a prestressed, non-corrosive alloy with sockets on a 0·1 inch matrix. The socket matrix boards have rows of five linked sockets each side of a central strip which allows standard d.i.l. i.c.s to be used.

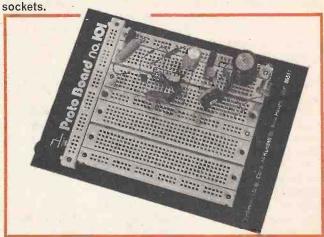
The Experimentor system is similar to the QT sockets but the method of joining boards together is more robust and there are two sizes of board which will accept 0.6 inch centre d.i.l. chips.

The QT boards are used on the Proto-board range of breadboards. There are six different sizes in the range to cater for most needs. Screw terminals are provided on the metal back panel.

At the top of the range are two units which incorporate stabilised power supplies to provide a self contained breadboard system.

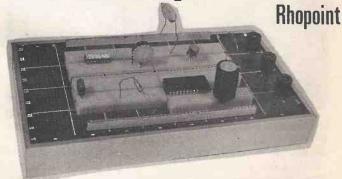
A variation on this theme is the Design Mate 1 which has a QT socket matrix board and bus strips mounted on the front panel with a power supply of 5 to 15V variable at 600mA and a 0-15V meter built in.

The various systems accept most components with leads on a 0·1 inch matrix and leads are easily inserted into the sockets



Retail prices range from £9.94 for the small Protoboard 6 to £80.68 for the top-of-the-range Proto-board 203A. The QT range retails from £1.89 to £7.20 and the Experimentor range from £2.48 to £5.75.

Vector Klip-Block



The Klip-Blok system uses an epoxy glass board which has a matrix of holes punched in it, mounted in an aluminium frame as the base on which a wide variety of insulating blocks containing metal contacts can be assembled.

A wide range of contact blocks are available which give this system enormous flexibility and the capability of taking any shape and size of component.

Individual baseboards can be linked together to expand the working area and boards are available either with or without terminals.

Wire diameters of 0.38 to 0.9mm diameter can be accepted by the beryllium copper, tin-lead coated, contacts which give a contact resistance of about $1 \text{m}\Omega$ and have a current rating of 5A.

The Vector Klip-Blok system is probably one of the most versatile breadboarding systems available but the cost of the various system components must, to a large extent, reduce its appeal to the amateur user.

Typical prices are difficult to give since the ultimate price is governed by the number of blocks and strips purchased. The system shown would cost around £24.00. Starter kits for three d.i.l. i.c.s cost around £5.00.