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# - NEWS \& COMMENT 

120 NEWS . . . NEWS . . . NEWS . . .
128 KINDLY NOTE-notes on published articles
142 P.W. READERS' PCB SERVICE
143 NEXT MONTH IN PRACTICAL WIRELESS-see what's in store!
158 TELEVISION-contents of our 'sister' magazine
160 PRODUCTION LINES-news on products of interestColin Riches
165 HOTLINES on recent developments-Ginsberg 169 ON THE AIR-Amateur Bands-Eric Dowdeswell, G4AR Broadcast Bands SW-Derek Bell Broadcast Bands MW—Charles Molloy
174 NEW BOOKS-read all about it!

## - CONSTRUCTIONAL

122 RHYTHM GENERATOR, Part2-A. S. Webb, B.Sc.
138 RECEIVER CALIBRATION AID-F. G. Rayer
144 DIGITAL FREQUENCY METER, Part 1-T. J. Johnson

## OTHER FEATURES

129 TALKING TRANSISTORS-P. Matthews
137 TECHNICROSS-solution to Puzzle 13
151 P.W. FAULT-FINDING GUIDE, continued-Les Lawry-Johns
157 SPECIAL PRODUCT REPORT-Sinclair 'Black Watch' Kit
166 GOING BACK-invention of the telephone-Colin Riches

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Specitication (each speaker): Impedance 8 ohms. Power handling 15 watts RMS ( 30 watts peak). Response $20-20.000 \mathrm{~Hz}$. Size $20^{\prime \prime} \times 11^{\prime \prime} \times 9 \frac{1}{2}$ "approx. Comparable built units (EMI LE3) sold elsewhere for over $£ 45$ pair.
£22.00 pair complete
Complete with crossover +f 5.20 p\&

Complete with crossover diagram.
 accoustic efficiency for the low powered amplifier. accoustic efficiency for the low powered ampinier The professionai finish can be votained with the minimum of tools, the infinite baffle type enclosures come ready mitred and professionally finished, and fix together with masking tape till glue dries.
The cabinet measures $12^{\prime \prime} \times 9^{\prime \prime} \times 5^{\prime \prime}$ deep approx finished in simulated teak, incorporating a quality $7^{\prime \prime} \times 4^{\prime \prime}$ elliptical speaker, power handling 4 watts. flux density 30.000 maxwells. impedance 8-15 ohms nominal, voice coil dia $\frac{3}{4}^{\prime \prime}$ magnet size $\mathbf{I} \mathbf{6 0} \mathbf{0}$
 $2 \frac{7}{8}$ approx.

## VISCOUNT IV STEREO AMP

## NOWAVALLAKLE $30 \times 310$ IV KIT FORM' WATH <br> COMPLETE $20 \times 20$ SYSTEMS SYSTEM 1 A $\mathbf{f} 6.00$

The new $20+20$ watt Steree Amplifier incorporating the latest silicon transistor solid state circuitry, the RT-VC VISCOUNT IV gives you a powerful 20 watts RMS per channel into 8 ohms. Superb teak-finished cabinat, with anodised !ascia to harmonise with any decor. Polished trim and knobs.
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Front panel socket for stereo headphones. And a host of sockets at the rear - for left and right speakers, tape recorder, auxiliary, tuner, disc and microphone
recorder, auxiliary, tuner, disc and microphone.
SPEEIFICATION. 20 watts RMS per channel 40 watts peak. Suitable $8-15$ ohnis speakers. Total distortion at 10 waits better than $0.2 \%$. Six switched inputs: 1. Magnetic PU. -3 millivedts at 47 K olums (R.I.A.A.): 2. Crystal/ ceramic P.U. -50 millivolts at 50 K ohms (R.IA.A.); 3.4. 6 . Tape Tuner/Aux. -140 millivolts at 50 K ohms (flat frequency response); 5 . Microphone - 3 millivolts at 50 K ohms (flat frequency response).
CONTROLS: Push button ON/OFF, stereo/mono. scratch filter. 6 position rotary selector. Individual rotary controls for treble, bass, balance and volume. Headphone socket, tape out socket. Aux.
mains output. Frequency response: 25 Hz to 25 kHz at fuil rated output. Sigmal to noise
ratio: better than -50 dB on all inputs. Tone control range: Bass $\pm 15 \mathrm{~dB}$ at 50 Hz ; Complete System Treble $\pm 12 \mathrm{~dB}$ at 10 KHz . Power requirements:: 250 V A.C. mains at 60 watts. with these speakers
 cover. Two Dua Type ta mers - Entosure size approx. $192 \times 10{ }_{4} \times 7{ }_{4}^{4}$ in simulated teak. Drive unit 13 " $\times 8^{\prime \prime}$ with 3 "tweeter. 15 watts handling. 30 watts peak.

+ £6.50.p\&p.
SYSTEM 2 \&85.00


## Viscount IV amplifier (As System 1a)

MP60 type deck (As System 1a)
Two Duo Type III matched speakers - Enclosure size approx. $27^{\prime \prime} \times 13^{\prime}$ $\times 11 \frac{1}{2}$. Finished in teak simulate. $\times 1 \frac{1}{2}^{\prime \prime}$. Finishad in teak simulate.
Drive units $13^{\prime \prime} \times 8^{\prime}$ bass driver, and Drive units $13^{\prime \prime} \times 8^{8}$ bass driver, and
two $3^{\prime \prime}$ (approx.) tweeters. 20 watts two $3^{3 \prime \prime}$ (approx.) tweeters. 20 watts
RMS, 8 ohms trequency range RMS. 80 obms freq
20 Hz to $18,000 \mathrm{~Hz}$.
Complete System with thase
speakers $£ 85000+£ 7.00$ p \& p.

PRICES: SYSTEM 1a
Viscount IV R103
ampliliei $£ 2750+£ 1.90 \mathrm{p} \& \mathrm{p}$. 2 Duo Type lla
 MP60 typer deck with Mag. cartisidge de tuxe plinth and cover $£ 22.00+£ 3.30 \rho \& p$. Total if purchased
separately: 679.5 B Availabla complite for only: $\mathbf{f 6 9 0}$
$+66.50 \rho \&$.

## PRICES: SYSTEM 2

Viscount IV R103
amplifier $£ 27.50+£ 1.90 \rho \& \rho$ 2 Dú Type III
${ }_{\text {speakers }} \quad £ 46.00+\mathbf{f 7 . 5 0 p}$ \& p. MP60 type deck with Mag. cartridge de luxe plinth
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+f 7.60 p \& p .

System consists of a $13^{\prime \prime} \times 8^{\prime \prime}$ approx. woofer with a $3^{\prime \prime}$ tweeter. crossover components and circuit diagram. Frequency response: 20 Hz to 20 KHz . Power handling 15 watts RMS into 8 ohms. (Peak 30 watts.)

PUSH BUTTON CAR RADIO KIT THE TOURIST


* IF YOUCAN SOLDER CORRECTLY ON A PHIS KIT CORRECTLY.

NOW YOU CAN BUILD YOUR OWN P USH-BUTTON CAR RADIO: This conseruction kit comprises a fuily built and aligned R.F. I.F. module; Printed circuit board, with ready, mounted integrated circuit output stage and all other components. The push button tuning methanism is fully built and tested ready to mate with the printed circuit board. (once it is assembled) NOTE: No test equipment is required for alignment, but remember you must have the ability to solder on a printed circuit board.
TECHNICAL SPECIFICATION:
(I) Outpur 4 watts RMS output. For 12 volt operation on negative or positive earth. (2) Integrated circuit output stage, pre-builz three stage IF Module. Controls volume
manual tuning and five push buttons for station selection, ifluminated tuning scale covering full, medium and long wave bands. Size chassis $7^{\prime \prime \prime}$ wide $2^{\prime \prime}$ high and $4 \frac{3}{4}$ " deep approx. Speaker including baffle and fixing strip $£ 2 \cdot 00+45$ p. p. \& p. Car Aerial Recommended-fully retractable $\mathbf{£ 1} \cdot 60+$ 40 p. p. \& p. $\mathbf{P r} \mathbf{~ P r e} \mathbf{2 0}$

## SPECHAL OFFER

The Tourist I Kit
Complete with speakers, fixing kit and fully $\underset{\text { aerial. }}{\substack{\text { retrable } \\ \text { ata }}} \mathbf{\$ 1 0 . 5 0}$ aerial.

## STEREO CASSETTE TAPE DECK KIT*

Kit comprises of ready built cassette tape transport mechanism. Featuring pause control solenoid assisted auto-stop. 3 digit tape counter, belt-driven balanced fly wheel. DC molar with electronic speed control. ready built and mounted record/ replay PC board. and two VU meters. power supply PC board. mains transtormer. Input and output sockets and two level controls. Specification power source 240 AC 50 Hz . Output more than 0.5 v imput mike-65dB. $10 \mathrm{~K} \Omega$. OIN $-47 \mathrm{~dB} .100 \mathrm{~K} \Omega$. Track system 2 channel stereo record play-back. Tape speed. 4.8CM/SEC. Frequency response $50-12.00 \mathrm{~Hz}$ signal to noise ratio $\mathbf{- 4 2 d B}$. Recording system AC Bias. Erasing system AC erase. Bias frequency 57 KHz . Size of mechanism $8^{\prime \prime} \times 5^{\prime \prime} \times 3^{1 / 2 "}$ approx unit easy to mount into your cabinet $3^{\prime \prime}$ required to clear
base of mechanism
approx.

## This is an advanced kit not suitable for those without electrical knowledge and those

 unable to solder.f32.50
$+p a p E 7.50$ or send SAE for complete details.
*DISCO AMPLIFIER


Reliant Mk IV Mono Amplifier, ideal for tike small disco ot house parties. Output 20 watts RMS into 8 ohms (suitable for 15 ohms ).
Inputs * 4 electrically mixed inputs. *3 individual mixing controls. *Separate bass and treble controls common to all 4 inputs. *Mixer employing F.E.T. (Field Effect Transistors). *Solid State eircuitry. *Attractive styling.
INPUT SENSITIVITIES - Input - 1). Crystal mic. guitar or moving coil mic. 2 and 10 mV . (Selector switch for desired sensitivity.) - Inputs - 2). 3). 4). Medium output equipment - ceramic cartridge. tuner, tape recorder, organs, etc. - all 250 mV sensitivity. AC Mains, 240 V operation. Size approx: $12 \frac{1}{2}^{\prime \prime} \times 6^{\prime \prime} \times 3 \frac{1}{2}^{\prime \prime}$
$\mathbf{f 2 0 . 0 0}+f 1.35 p \& p$.

Elegant self selector push button player for use with your stereo system. Compatible with Viscount IV system, Unisound module and the Stereo 21 Technical specification Mains input, 240V. Output sensitivity 125 mV .

## SPECIAL OFFER

As above but complete with build yourself Unisound Amplifier Kit (see opposite sanel) +2 'Compact' easy to build
speaker kjts (see $\mathbf{£ 2 5 . 0 0}$ speaker kits (see opposite page)
$+p \& p \in 2.00$

## BUILD YOUR OWN STEREO AMPLIFIER*



For the man who wants to design his own stereo - here's your chance to start, with Unisound -- pre-amp, power amplifier and control panel. No soldering - just simply screw together. 4 watts per channel into 8 ohms. Inputs 120 mV (for ceramic cartridge). The heart of Unisound is high efficiency I.C. monolithic power chips which ensure very low distortion over the audio spectrum. 240V. AC only
Also available with 2 speakers $\left(7^{\prime \prime} \times 4^{*}\right) \mathrm{f} 10+\mathrm{f} 1.75 \mathrm{p} \& \mathrm{p} . \mathbf{f 8} \mathbf{8} \mathbf{8} \mathrm{f} 1.05 \mathrm{p} \mathrm{g} \mathrm{p}$. Also available with the 'Compact' (see opposite page) easy build speaker kit $[13.50+C 2 p \& p$

INCORPORATES: Pre-Amp with full mixing facilities. including switched input for mic with volumé control. switched input for auxiliary with volume control, bass and treble controls, volume control and blend control tor turntabies. Two B.S.R. MP60 type single play professional series decks, fitted with crystal cartridges.

## TECHNICAL SPECIFICATION:

Pro-amp - Output - 200mV. Auxiliary inputs - 200 mV and 750 mV into 1 meg. Mic input - 6 mV into 100 K .240 volt pperation. Turntables capacity $-7^{\prime \prime} .10^{\prime \prime}$ or $12^{\prime \prime}$ recorids. Rumble, wow and flutter Rumble Better than -35 dB . Wow Retter than $0.2 \%$. Flutter Better than Better than $0.2 \%$. Flutter Better than
$0.06 \%$ (Gaumont kalee meter). $0.06 \%$ (Gaumont kalee meter).
Finish - Satin black mainplate with htack wirntable mat inlaid with brushed aluminium trim. Toriearm and controls in black and brushed aluminium.


Console size
(nit Closed $-17 \frac{3}{4} \times 133^{\prime \prime} \times 8 \frac{3}{4}$ "(app.)
 This disco console is idealiy matched for the Peliant IV and Disco 50 or any other quality amplifier.
The unit is finished in błack PVC with contrasting simulated teak edging. diamond spun control knobs with matching control panel.

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 A．C．mains
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tully isole ted maine er with full Wave recti－ ilcatlon giving ade－
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$y_{0}$
suouthing with negligible hum bs rectifer．Wo dual potentiometers are provided fo basd and treble contron，giving bass and treble volume control is used．Batance of the left and right hand channels can be adjusted by means of a sepa rate＇Balance＇control fitted at the rear of the chasela Input sensitivity is approximately $300 \mathrm{~m} / \mathrm{v}$ tor tull peak output of 4 watts per channel（ 8 watts mono），into 3 ohm apeakers．Full negative feedback in a carefully calculated oircuit，allowa high volume levela to be used with negligible $11^{\prime \prime} \mathrm{w} \times 4^{\prime \prime} \mathrm{d}$ ．Overail height including valyes $5^{\prime \prime}$ ．Ready built \＆teated to a high standard．s18－40．P．\＆P． 95 D

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5 in .3 ohin $\$ 1 \cdot 45$, P．\＆P， $35 \mathrm{p} .7 \times 4 \mathrm{in}$ ． 3 ohm $\$ 1 \cdot 69, \mathrm{P} . \& \mathrm{~F}$ ．

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25 Watts (RMS)

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APPLICATIONS; Hi-Fi-Disco-Monitor-Power slave-Industrial-Public Address
SPECIFICATIONS
SPECIFICATIONS 500 mV
OUTPUT POWER 120 W RMS into $8 \Omega$ LOAD IMPEDANCE $4-76 \Omega$ DISTORTION $0.05 \%$ at
100W at 1 kHz . $\pm 45 \mathrm{~V}$
SIZE 11410085 mm
Price $£ 21.20+£ 1,70$ VAT P\&P free.
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2 Pole 2 Way
$\begin{array}{ll}2 & \text { Pole } \\ 2 \text { Pole Way } \\ 3 & \text { way }\end{array}$
$\begin{array}{ll}2 \text { Pole } & 3 \text { Way } \\ 2 \text { Pole } & 4 \text { Way } \\ 2 \text { Pole } & \text { B Way }\end{array}$
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| 12 V | 24V | £ | p | 3-0-3 | 200 | $1 \cdot 37$ | 25 |
| 5 | 25 | $1 \cdot 30$ | 26 | $0-6 \times 2$ | 1 A | i-80 | 45 |
| 1 | -5 | 1.58 | 45 | $0-9 \times 2$ | 330 | $1 \cdot 34$ | 26 |
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| 4 | 2 | 2.52 | 62 | $0-9 \times 2$ | 500 | 1.83 2.60 | 45 59 |
| 6 | 3 | $3 \cdot 76$ | 62 | $0-9 \times 2$ | 1A | $2 \cdot 60$ | 52 |
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| 12 | 8 | 4.93 6.35 | 98 1.20 | 0-20 $\times 2$ | 1 A |  |  |
| 16 20 | 8 10 | 6.35 9.27 | 1.20 1.20 | $0-20 \times 2$ $0-15-27 \times 2$ | 1 1A | 3.08 3.86 | 72 |
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| EC86 | 0.82 | EF184 | 0.98 | PCF201 | 1.50 | PY500A | 1.60 | 30 FL 2 | 1.02 |
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| DL96 | 0.65 | EL30 | 0.60 | PCF802 | 0.55 |
| DY86 | 0.46 | EL37 | 840 | PCF806 | 0.90 |
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| AC128 | 0.15 | BF180, | 0.38 |
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| AC176 | 0.25 | BF181 | 0.96 |


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| AC187 | 0.21 | BF194 |



| AF118 | 0.86 | BFX8B | 0.24 |
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| AF116 | 0.28 | BFY50 | 0.20 |
| AF117 | 0.94 | BFY81 | 0.90 |
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| AF239 | 0.44 | BR100 | 0.40 |
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| BA102 | 0.25 | BY127 | 0.1 |
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| BCY | 0.45 | MPF 105 |


| BCY70 | 0.18 | NKT404 |
| :--- | :--- | :--- |
| BCY71 | 0.92 | $0 A S$ |
| BCY72 | 0.15 | $0 A 10$ |


| BC211 | 0.85 | $0 A 79$ | 0.10 |
| :--- | :--- | :--- | :--- |
| BD121 | 1.00 | $0 A 81$ | 0.18 |
| BD124 | 0.65 | OA91 | 0.07 |


| SN7400 | $0 \cdot 18$ | SN7428 | 0.40 | SN7486 | 0.47 | 8N7414S | 1.26 | SN74192 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SN7401 | $0 \cdot 18$ | SN7430 | $0 \cdot 18$ | GN7480 | 0.55 | SN74150 | 1.75 | 8N74193 | 8.00 |
| EN7402 | $0 \cdot 16$ | SN7433 | 0.87 | BN7491AN |  | SN74151 | 1.00 | gN74194 | 130 |
| EN7403 | $0 \cdot 10$ | SN7437 | 0.37 |  | 1.00 | SN74154 | 8.00 | 8N74195 | 1.10 |
| EN7404 | 0.26 | SN 7438 | 0.87 | GN7492 | 0.70 | SN74155 | 1.00 | BN74196 | 1.20 |
| ENT405 | 0.82 | SN7440 | 0.28 | SN7493 | $0 \cdot 70$ | SN゙74156 | 1.00 | SN74197 | 1.20 |
| BN7406 | 0.48 | SN7441AN |  | SN7494 | 0.80 | BN74157 | 0.95 | SN74198 | $2 \cdot 77$ |
| SN7407 | 0.48 |  | 0.82 | SN7496 | 0.80 | 6N74170 | 2.52 | SN74199 | 2.68 |
| SN7403 | 0.88 | EN7442 | 0.79 | 8N7486 | 0.95 | 8N74174 | 1.57 |  |  |
| SN7409 | 0.88 | 8N7450 | 0.18 | SN 7497 | 8.87 | BN74175 | 1.10 |  |  |
| GN7410 | 0.16 | GN7451 | 0.18 | SN74100 | 1.89 | SN74176 | 1.88 |  |  |
| 8N7411 | 0.25 | GN7453 | 0.16 | SN74107 | 0.45 | SN74190 | 8.00 |  |  |
| GN7412 | 0.80 | GN7454 | $0 \cdot 18$ | SN74110 | 0.58 | SN74191 | 8.00 |  |  |
| SN7418 | 0.36 | EN7460 | $0 \cdot 18$ | SN74118 | 0.90 |  |  |  |  |
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| SN7417 | $0 \cdot 86$ | 6N7473 | 0.41 | 8N74121 | 0.50 | DII. |  | 14 pin |  |
| BN7420 | $0 \cdot 18$ | EN7474 | 0.42 | SN74122 | $0 \cdot 70$ |  |  |  |  |
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10 pes. $10 \cdot 1 \times 7 \cdot 9 \mathrm{in}$. Plus free $\frac{4}{\mathrm{y}}$ lb etching X tals, $53 \cdot 10$.
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Dim. $6 \times 6$ in 50 p each.
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RESIST COATED P.C.B. FIBRE GLASS
$6 \times 6 \mathrm{in}, 65 \mathrm{pa}$ ea.
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$12 \times 12$ in, $2 \cdot 00$ ea.
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$250 \mathrm{mfd} / 63$ volt, 20p. P.P. Bp.
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$\mathbf{4 6 0 , 0 0 0 \mathrm { mfd } / 1 0 \mathrm { volt } , \mathbf { 5 } \mathbf { 2 } \cdot 0 0 \text { . P.P. } 5 0 \text { p. }}$

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AC128 | 12p | M |  | AF117 | 18 p | BCi57 | 7p | BC183L | $11 p$ | BC548 | 12p | BD131 | 35p |
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## SUBSCRIPTIONS - PRACTICAL WIRELESS AND TELEVISION MAGAZENES

WE are still receiving numerous letters requesting subscriptions to Practical Wireless and Television magazines. For those readers who are not aware, we regret that our magazines can no longer be supplied on direct subscription by IPC Limited due to escalating costs.

This action is very much regretted, but it should not mean that any reader is deprived of his/her regular copies of Practical Wireless or Television. Readers should order direct from their local newsagents. Any readers outside the UK who have difficulty in locating a supplier should write to the Editor and he will advise them of their local agent.

## Soldering Catalogue

ANEW catalogue covering a wide range of soldering instruments and accessories is now available from Adcola Products Ltd. The contents include the well-established range of Invader lightweight soldering instruments for operation from either mains or low voltage

## Eoundations

WELL-KNOWN author M. G. Scroggie whose work Foundations of Wireless and Electronics has just reached its 250,000 sale, is shown here being presented with a specially bound copy of his book.

The publishers, Newnes Butterworth also announced the new 9th Edition of Mr. Scroggie's book.
M. G. Scroggie, B.Sc., C.Eng. FIEE was the second radio Amateur, under the callsign 5XJ, to make two-way radio contact across the Atlantic.


Mr. Scroggie, centre, shows his speciallybound book to Fred Judd, G2BCX (right) while a Newnes-Butterworth employee looks on.
supply, the medium ' $A$ ' series range and the heavy duty ' $R$ ' series of tools. Safety stands and stations, desoldering instruments including the Remov-Ic for DIP extraction and desolder braid are also featured together with solder pots, and wire cutting tools. Details of Superspeed cored solder are also featured.

Despatched with the catalogue is a separate four page technical specification covering the Unit 222 electronically switched variable temperature, thermostatically controlled soldering instrument, and a four-page price list. Details of the Bahco range of pliers for electronics use are also included in the form of a separate leaflet.

Copies of the catalogue and supplementary specifications are available free on request from Adcola Products Ltd., Adcola House, Gauden Road, London SW4 6LH (01-622 0291).

## Tyneside Amateur Radio Society

THE Borough of North Tyneside is holding a Festival of Sport and Recreation during July and the Society which operates within the Borough has agreed to take part by establishing an amateur radio station. Members of the public will be invited to see the station in operation and persons interested in the hobby will be assisted wherever possible.

It is intended to go on the air from approximately 10.00 hours on Saturday, 10th July to 18.00 hours on Sunday, 11th July. They hope to be operating on all bands from Top Band to 10 metres and also on 2 metres.

Special QSL cards are now being printed using the Club callsign G3ZQN. All contacts will be sent a card and Special Certificates to be signed by the Mayor of the Borough will be sent to the furthest contact on each band. The venue of the Festival Station is the Pavilion at the Churchill Playing Fields, Monkseaton, Whitley Bay. The venue for normal Society meetings is the Wallsend Community Centre, Vine Street, Wallsend every Monday evening at 20.00 hours. New members will be welcome.

## RADIO SHOW

GOUND and Vision 76, National Exhibition Centre, Birmingham, 28/31 May, 1976

## BBC Stereo Radio from Tacolneston, Norfolk

THE BBC announced that the Radio 2 and Radio 3 VHF transmitters at Tacolneston, Norfolk broadcast in stereo from Friday, 19 March. The start of a full stereophonic service on all three VHF channels is dependent upon the completion of a new pulse code modulation ( pcm ) link to the station at Tacolneston. It is hoped that this will be possible within the next two years, but to provide stereo in the meantime, a rebroadcast link has been installed, and this will make it possible to provide Radio 2 and Radio 3 in stereo to about $1,100,000$ people in Norfolk, Suffolk and the eastern part of Cambridgeshire. Radio 4 stereo programmes will be added to the service when the permanent pcm link has been completed.

With the present extension, BBC stereo radio will be available to approximately 88 per cent of the United Kingdom population. The start of stereo transmissions does not affect listeners using ordinary monophonic receivers, and to take advantage of the stereophonic information, a receiver having a stereo decoder is required. Advice about reception of the BBC's stereophonic service may be obtained from the BBC's Engineering Information Department, Broadcasting House, London WIA 1AA.


## Eagle 1976 calalogue

T0 mark their 25th year in electronics Eagle International have created a comletely different format for the new 1976 catalogue. A comprehensive range of over 500 models including some 45 new products are featured in this absorbing 64 page full-colour publication.

For easy reference the catalogue is divided into nine broad product categories - each page carrying a colour code indicating a particular section. It contains more factual information, comprehensive specifications, frequency response graphs and many additional detail photographs. The sections cover hi-fi, tape, headphones, audio, microphones, public address equipment, intercoms, test equipment and ancillary products, plus a comprehensive index with recommended retail prices.

The section on intercoms includes a useful selection guide and the clamp meter and multimeter guides in the test equipment section are of particular interest. A welcome addition is the connecting lead guide which shows the correct hook-up for a complete hi-fi system. As always every Eagle product line carries a two-year guarantee plus a reputable after-sales service, even after the warranty period.

The new Eagle catalogue for 1976 is available on request from Eagle International, Precision Centre, Heather Park Drive, Wembley, HA0 1SU.

## The Budget and prices in P.W.

IN the April 6th Budget, VAT at the $25 \%$ rate was cut to $12{ }_{2} \%$. At the time of our going to press we were unable to make alterations to all of our advertisements but we would advise readers that some of the prices quoted on our pages will be different and if ordering goods, it might help to check with the advertisers concerned before purchasing.

## Mullard Data Book 1976

THE 1976 edition of the Mullard Data Book is now available. It contains abridged data on the company's range of components for use in consumer applications, including valves, integrated circuits, semiconductor devices, TV picture tubes, capacitors and resistors. Equivalents and comparables are also listed.

Designed for the radio and TV dealer and his service engineers, the pocket-size book runs to 176 pages and, for easy reference, different coloured papers are used. for each of the main sections: blue for semiconductors, yellow for picture tubes and receiving valves and green for capacitors and resistors.

The Mullard Data Book is obtainable for 50p direct from Technical Press Ltd., Freeland, Oxford OX7 $2 A P$.

The 15th century building, part of which has been offered free of charge for anyone in the Wallingford (Oxon) area wanting to join a Radiol Electronics club.


## The Eagle strikes



ANEW symbol has been perfected for Eagle International, which will be systematically applied to all Eagle audio and electronic products, packaging, advertising and promotional material in the coming months.

Marketing Director David Harris says, "The symbol will project an agressive identity for Eagle and will provide an internationally recognisable image for overseas markets". The design adopted is a totemic device depicting . a stylised eagle head which expresses the power and majesty of the keen sighted king of the sky.

## Free offers galore!

ORCHARD Electronics Director Mr. D. M. Trueman recently sent us this picture of the firm's premises at Wallingford, Oxon. He's offering, completely free, one floor of the building to anyone interested in joining/forming an amateur radio and electronics club in the area. If any readers would like to help form something along these lines, Orchard Electronics would be pleased to hear from them.

Another offer from the firm comes in the form of a free transistor (CIL 108) it's the equivalent of the BCl08 and the first 3000 readers who send a stamped, addressed envelope for the Orchard list of components will get one.

If you want a free transistor and components list or are interested in joining up with other enthusiasts to form a club, write to Mr. D. M. Trueman, Orchard Electronics, Flint House, High Street, Wallingford, Oxon, OX10 ODE. (Telephone: Wallingford (0491) 35529 or 36588 ).


## Power supply

The power supply circuit shown in Fig. 8 is of conventional design providing the three regulated voltages required by the rhythm generator. The regulation is necessary to reduce false triggering of the twin-T oscillators which are very sensitive to supply fluctuations and to ensure that the voltage delivered to the M252 chip across pins 9 and 10 remains at $17 \mathrm{~V} \pm 1 \mathrm{~V}$. The total current consumption of the complete generator is very low, about 30 mA when the LED is off rising to 44 mA when on.

## Construction

The construction of the rhythm generator is simplified by the use of three printed circuit boards, one for the snare drum, long cymbals, short cymbals, maracas, M252 chip, clock generator and down-beat indicator; the second for the bass drum, high bongos, low bongos, claves, conga drum and preamplifier and the third for the power supply unit. No detailed procedure for the mounting of the
components is given as this is fairly straight forward although careful soldering is required.

There is, however, one point over which extreme care should be taken. The 'M252 chip and the 4011A NAND gate IC's are manufactured using MOS technology and although various input protection components are built in they are vulnerable to high voltage static electricity. They are normally supplied packed in conductive foam or surrounded in metal foil and should not be removed until ready to be inserted into their respective sockets.

A static charge can build up on anything that is insulated from earth. Friction with modern plastics such as nylon or PVC quickly cause static to accumulate e.g. by combing one's hair or wearing synthetic fibre clothes. A plastic laminate surface on a table with rubber feet could become highly charged after polishing. The basic rule when handling these devices is that the pins should not be allowed to come into contact with anything that is not an earthed conductor. The author uses a pair of metal tweezers connected to earth which automatically earths the body thus making handling completely safe. If the ICs have to be removed from their sockets they should be placed in conductive


Fig. 8: Circuit diagram of power supply giving -12 V and +5 V for IC1, +12 V and -12 V for IC5, and $+5 \mathrm{~V} /+12 \mathrm{~V}$ and VV for the remaining $/ \mathrm{C}^{\prime}$ 's and transistors.


foam or on an earthed metal plate. No alterations should be made to the circuit with these devices in position and they should not be inserted with the power switched on. No apologies are made for stressing these points as a replacement for the M252 chip will cost over $£ 9$ !
Having obtained all the necessary components the enthusiastic constructor often finds it difficult to resist the urge to put everything together as quickly
as possible. Although a lot of the complexity of the circuitry has been taken out of the hands of the constructor and built into the printed circuit boards there is nevertheless a certain amount of interwiring involved. This means that if the generator is not functioning correctly when it has been completed it may be difficult to locate and rectify any fault.

For this reason it is highly recommended that all the components with the exception of the integrated

circuits are individually checked before assembly. With an ordinary multimeter set to measure resistance, check the values of the resistors against their colour codes, check for leakage of the capacitors, the forward drop and reverse leakage of the diodes and transistors (these may be considered as two diodes connected back to back) and the continuity of the transformer windings, chokes and switches. Also carefully examine the copper track on the printed circuit boards for any hair-line cracks or for bridging caused by roller tinning smear or under-etching.

The first step is to assemble the power supply unit on PCB1 referring to the component layout given in Fig 9. Begin by inserting the Vero pins at the appropriate points, followed by the resistors, capacitors, semiconductors and finally the transformer. Having completed the board, check that the capacitors and diodes have been soldered in the right way
round. Temporarily connect the mains to the trans former and ensure that the power supply unit is functioning correctly by measuring the three voltage outputs.
If all is well, proceed to assemble the components in the same order as indicated above on PCB2 and PCB3 according to the layouts in Fig. 10 and Fig. 11. When completed check the circuit boards over for mistakes and for any solder bridging the copper tracks. It is well worth taking some time over this as mistakes are easily made and careful checking now may eliminate time-consuming and possibly expensive trouble-shooting later. Don't forget the links!
The interwiring leads are then soldered to the pins on PCB2 in accordance with Fig. 10 allowing sufficient length of wire. The three stand-offs are next inserted and PCB3 pressed home on top. The wiring to this board may now be completed routing all the




Fig. 11: PCB3, which again is shown full size and contains components for the bass and conga drum, high and low bongos, claves and the preamplifier. The NAND gate used for the bass drum is 'borrowed' from IC3 which is situated on PCB2.
wires from the board below on the right hand side. This allows the top board to be "hinged" from the lower one when fitting and making adjustments. Note that the bass drum oscillator utilises a spare NAND gate in IC3 on the lower board.

## Case assembly

The Vero plastic box type 65-2523E used in the prototype makes a small and very attractive housing. The light grey moulding is removable allowing easy access to the base. Before mounting the boards inside the case four holes must be


Fig. 12: Rear view of the Vero plastic box base, giving details of the drilling dimensions.
drilled in the back of the base as shown in Fig. 12 to accommodate the fuse-holder, foot switch socket, mains input and signal output leads.
The drilling layout for the front panel is shown in Fig. 13. A really professional finish may be achieved by using Letraset for the legend on the panel as in the photograph. The code table (Fig. 2) should be cut out or copied and stuck in the position indicated for easy reference. The panel will then require protection from abrasion and may be sprayed with a protective lacquer such as Letracote Gloss or alternatively covered in a sticky-backed clear film similar to "Libraseal". Both these items are obtainable from most stationers or artists supplies shops. If the film is used it will be necessary to trim it close to the sides of the panel and in the holes with a razor blade to prevent it peeling off.
The boards may now be fitted in the base with power supply unit on the right and the double board assembly alongside on the left. The base incorporates brass inserts for this purpose. These require 3 mm metric screws although at a pinch 6BA could be used if the metric size proves difficult to obtain. The $+12 \mathrm{~V},-12 \mathrm{~V},+5 \mathrm{~V}$ and 0 V supply lines are now connected up from the power supply to the instrument boards and the mains input lead wired in.

The controls are then assembled on the front panel, see Fig. 14. To preserve the neat appearance of the panel the locating lugs on the potentiometers should be filed off and any locating washers supplied with the miniature switches discarded. To prevent rotation in the absence of these, crinkle washers are fitted between the components, and the back of the panel and the nuts screwed up tightly. Note the tag under the stop switch, S1, to allow earthing of the panel.

The light grey case moulding is placed on the base and the panel controls wired in. There is a supporting strut running vertically across the opening of the box and the wiring must be routed so that wires are not trapped between this and the panel. For this reason there are two earth wires running from the code switches, one on either side.

The switches S3 and S4 are fairly close to PCB3 when the panel is screwed in position so the link wire between them should be insulated and pressed flat on the panel to prevent it touching VR4.

## Final adjustments

For making the final adjustments the output of the generator is connected via a screened lead to an external amplifier and loudspeaker. The three 4011A and the 741 ICs may now be inserted. The insertion of an IC into a socket can be a bit of a problem the more so when the IC has to be handled with caution. New sockets are often very tight and a useful tip is to 'ease' the socket by repeatedly inserting and removing an old IC of the same outline until it is free. With VR9 set midway and with the volume of the amplifier at a fairly low level the preset potentiometers VR4 to VR8, should be adjusted in turn until oscillation occurs and then backed off until it just disappears. In some instances it may not be possible to achieve continuous oscillation of the bass drum circuit but this does not matter. The bass drum may be made to sound momentarily by connecting its input, i.e. the non-earthy side of R28, to the +5 V supply. The potentiometer VR4 is then further adjusted to achieve the best sound. The procedure is repeated for the remaining four instruments on PCB3.
The adjustment of the instruments on PCB2 is made by varying VR2 which controls the filtered white noise level in conjunction with VR3 which balances the output from the snare drum with the rest of the instruments on this board. The instruments may again be made to sound by connecting


Practical Wireless, June 1976

their respective inputs momentarily to +5 V . The preset potentiometer VR9 controls the maximum voltage output from the Rhythm Generator and should be adjusted to suit the sensitivity of the external amplifier.

Having completed the preceding adjustments it is worthwhile checking that the voltage between pins 9 and 10 on the M252 socket is $17 \mathrm{~V} \pm 1 \mathrm{~V}$ with pin 9 positive. Switch off the power and carefully insert the M252 chip in its socket, the correct way round! bearing in mind the handling procedure outlined previously. Check through the fifteen rhythms (with S1 open) by entering the various codes given in Fig. 2 on switches S 3 to S . It is important that the tempo is adjusted so that the particular rhythm sounds right and that the snare drum or claves is correctly selected. Final adjustment to the instru-
ments should be made while the generator is running to correct any excessive "ringing", and to achieve the best overall balance of sound. If a foot operated switch is added it should be of the "press to break" type in order to inhibit the generator in its "off" position.
Finally, a word about loudspeakers. The Rhythm Generator by its very nature produces large transient signals especially from the bass drum circuit where, because of its low frequency, large excursions of the loudspeaker cone are required. It is therefore essential that a speaker of adequate power rating is used to avoid permanent damage.
Acknowledgements are due to SGS-ATES for some circuit details.

Note. R4 in the components list, Part 1, was incorrect, and should have read $220 \mathrm{k} \Omega$ and not $22 \mathrm{k} \Omega$.

## STEREO DISCO SYSTEM

## Dec 75.Jan/Feb 76

Some readers report encountering earthing problems with the stereo unit. To obviate the risk of earth loops the following earthing table should be followed. The terminal block, Fig. 14 page 849 , negative side of the bridge rectifier, will be referred to as the "common earth".

Pin 23 RH amplifier
Pin 23 LH amplifier
Pin 2 LH amplifier
Pin 2 LII amplifier
Pin 2 RH amplifier
Pin 23 RH amplifier
Pin 23 LH amplifier Mains earth in

## to Common earth

 to Pin 23 RH amplifier to Pin 2 RH amplifier to E tagstrip B Fig. 11to E tagstrip B Fig. 11
to Neg. RH speaker socket to Neg. LH speaker socket to Copper plane, mains

Copper plane, mains panel to Common earth
Transformer metalwork to E on mains input socket Pin 32 Light Modulator to $E$ on mains input socket Turntable metalwork to Common earth

All connecting leads to the speaker output sockets should be routed well clear of pre-amplifier and mixer panel. Good quality screened lead must be used for the turntable and mixer connections and the screens of these connected as shown in Fig. 11. It will be noted that all these connections are made to the mixer ONLY.

A transformer of low flux leakage must be used if hum is to be eliminated. The hum level of the prototype at maximum gain setting was virtually nil on both channels.

It is an advantage to exchange capacitors C 3 and C5 i.e. C3 to be $100 \mu \mathrm{~F}$ and C5 $25 \mu \mathrm{~F}$. Resistor R19 should be changed to $390 \Omega$. On mono versions of the Disco omit the balance control and make VR9 $10 \mathrm{k} \Omega \log$.

The polarity of C6 in Fig. 6 and on the PCB supplied by the Readers PCB Service is reversed to what it should be. Reverse the capacitor if already fitted.

Before initial switch-on ensure that VR52 is set fully clockwise.

BEFORE the design formulae of transistors are derived, it is necessary to examine how a transistor is capable of amplification. Conduction is simply the movement of electrons in a general direction within a substance. A substance which allows electrons to flow freely through it is called a "conductor", one which does not is called a "nonconductor" or "insulator". The electrons responsible for conduction are those most loosely held by the nuclei of the atoms of the substance and lie in the outer parts of the atoms. These electrons are known as the "bonding" or "valence" electrons and there are usually two or three of these for each atom. Note that the definition of conduction does not imply that the electrons which start from one end of a conductor need be those which reach the other end, although this is usually the case with good conductors. It could happen that after an electron had been re moved from an atom A, leaving a "hole" in A, it could fill up a previously existing hole in an atom $B$, leaving the electron from atom $\mathbf{B}$ to continue. This process is shown in Fig. 1. Note that this is a purely diagrammatical representation of conduction in general, and that in a good conductor all the bonding electrons are quite free from the rest of their atoms.


Fig. 1: Diagram to illustrate the idea of movement of electrons in a conductor.
A point worth mentioning is that electrons are considered to have unit negative charge, which is 1 electron-volt (ev) in value, and that a flow of negative electrons in one direction is denoted by a flow of positive current in the other direction. This fact is brought out in Fig. 2, which depicts a simple battery and resistance circuit. At the negative battery terminal there is available a supply of electrons
which flow through the resistor to the positive terminal where there is a shortage of electrons. In fact, the battery serves just to pump electrons from its positive to its negative terminal, through the internal circuit of the battery. An electric current flows from the positive, through R , to the negative terminal.


W183
Fig. 2: The electron state in the simplest of circuits.
In summing up, it should be remembered that in conductors, including "resistances", the bonding electrons are effectively separate from the rest of the atoms, whereas they are tightly held in insulators. As a matter of interest, this can be illustrated by observing the effect of heat on conduction, through the two classes of materials. An increase in the temperature of a conductor causes a drop in conductance (and increase in resistance) because the increasing vibration of the "stationary" ions impedes the otherwise almost free fiow of electrons. When an insulator is heated it remains as such until a certain high temperature when the insulator "breaks down" into a conductor because the electrons part from the atoms.

## SEMICONDUCTORS

A semiconductor is a substance which falls between the general categories of conductors and nonconductors. In other words, it is a very high resistance conductor at room temperature. As an example, the resistivity of silver, a conductor, is about $10^{-6} \Omega / \mathrm{cm}^{3}$, that of pure germanium, a semiconductor, about 60, and glass, an insulator, $10^{10}$.

(a)

(b)

(c) Wi84

Fig. 3: Three types of germanium, the $n$ and $p$ types being the result of added impurities.

Semiconductors are really insulators which have a low "breakdown" temperature and they behave as insulators when cooled appreciably. Between somewhat below room temperature and about $75^{\circ} \mathrm{C}$ in the case of germanium (approx. $150^{\circ} \mathrm{C}$ for silicon) the resistivity falls very sharply until it is so low that the material acts as a conductor.

It happens that the introduction of traces of impurities into the semiconductor over this temperature range has unusual effects on the resistivity and to see why this occurs it is necessary to take a closer look at the structure of semiconductors. Germanium, an elemental semiconductor, has four bonding electrons, and forms a crystalline type of structure, with each electron teaming up with one other electron from and adjacent germanium atom. Although the bonding pairs of electrons are symmetrically arranged in three dimensions, Fig. 3 has been drawn in two dimensions for simplicity.

Suppose an impurity is introduced into the structure. In diagram Fig. 3(b) so-called "donor" impurities, such as arsenic or phosphorus, which have five bonding electrons, are fitted into the structure. It can be seen that one electron is left over because only four are required for bonding, hence the name "donor". The space electron is weakly held by the donor nucleus. Germanium modified in this way is known as n-type germanium alloy and contains large numbers of virtually free electrons.


Fig. 4 : Illustration of electron flow in a p-n junction.
An opposite effect occurs when "acceptor" impurities, such as aluminium, boron or indium, with three bonding electrons, are added to form p-type germanium, Fig. 3(c). One electron is needed to complete the structure so that there is a positive hole. It can be seen that this p-type germanium is conductive since electrons can be attracted away from nearby atoms to fill the hole. In this way, the passage of a negative electron from $A$ to $B$ corresponds to that of a positive hole from B to A.

There are, therefore, two important types of impure germanium, the n-type which has been treated with a trace of a donor impurity, and the p-type with an acceptor impurity. Electrons can move freely through both $p$ and $n$ alloys so they can be classed as conductors. This is contrasted with pure
or "intrinsic" i -type germanium, in which there is only limited intrinsic conduction at a given energy level.

## THE P-N JUNCTION

When a strip of pure germanium is treated so that one half is of p -type and the other of $n$-type germanium, there is said to be a " $\mathrm{p}-\mathrm{n}$ junction" in the middle. Almost as soon as the junction is formed, some loose electrons break away from the n-layer and a few of these diffuse into the p-layer to fill in the holes nearest the junction. This means that there is a


Fig. 5: The two forms of biasing applicable to a junction.
layer of intrinsic germanium on the p -side of the junction. However, i-type germanium constitutes a comparatively very high resistance and so the electron flow from $n$ to $p$ ceases almost immediately, an equilibrium being set up at a given temperature. This is illustrated in Fig. 4 (a) and (b). Since electrons have moved from the $n$ layer to the $p$ layer, there is a shortage of electrons in the $n$-region and a surplus in the p-region. Another way of saying this is that the $n$-half of the $p$ - $n$ junction has obtained a positive charge with respect to the p-half. This is represented diagrammatically by means of a cell in Fig. 4(c). The value of this "contact potential" is about half a volt, and it is important to remember this.
Consider what happens when an external source of EMF is applied across the junction terminals, and its polarity opposes that of the imaginary cell, as in Fig. 5 (a). This is known as biasing in the reverse direction. Only a small current flows as the insulation or "depletion" region of germanium atoms in the junction is "reinforced" or widened. When the external battery is connected the other way, as in (b), the depletion region is broken down and electrons flow freely from the n-region to the p-region. This is known as biasing in the forward direction. In other words, the p -n junction acts as a rectifier provided that the applied voltage is greater than its contact potential. This simple p-n junction rectifier has found a large number of applications in industry and is currently available in a wide variety of types ranging from modern versions of the "cat's whisker"



##  (DEPT. PW5), SIMMONDS ROAD, WINCHEAP



NEW CATALOGUE 25P
detector to power units capable of handling hundreds of ampères.

It should be mentioned that germanium is not the only semiconductor, there being many covalently bonded crystalline compounds and a few elements which exhibit this effect. Silicon is commonly used today and, in all that has been "written so far, "silicon" can be substituted for "germanium" as both elements have four bonding electrons and function in the same way.

## THE JUNCTION TRANSISTOR

An ordinary junction transistor is basically a strip of semiconductor material, such as germanium or silicon, which has been processed so that it is either all n-type except for a narrow p-region in the middle ( $\mathrm{n}-\mathrm{p}-\mathrm{n}$ transistor) or p-type except for a narrow n-region ( $p-n-p$ transistor). These connections are made to the strip, one to each end (emitter, collector) and one to the centre region (base). The p-n-p transistor has been very popular in Britain for many years, but n-p-n transistors are now becoming more common. The following discussion will be confined to the n-p-n transistor, although what is stated applies also to the p-n-p transistor, but with voltages reversed and "holes" in place of "electrons".


Fig. 6: Polarities of voltages applied to a junction transistor, in this case an $n-p-n$ type.
[W187]
Transistors are normally biased by two external voltage sources, as shown in Fig. 6. When the base lead is disconnected, only a small leakage current flows through the transistor. If the base is given a small positive bias $\mathrm{E}_{\mathrm{B}}$, the emitter-base pn junction is biased in the forward direction and electrons are emitted from the emitter towards the base. Now the base region is very thin, so that a large fraction of the electrons travel on into the collector region where they are attracted by the electron shortage caused by the collector-emitter battery, $\mathbf{E}_{\mathrm{c}}$. This fraction, which is obviously less than unity, is given the symbol " $x$ " and with most transistors has a value of about $0 \cdot 98$. The remainder of the electrons flow out through the base connection.

It has therefore been shown that a small current, Ib, flowing into the base causes a much larger current, Ic, to flow into the collector, and this is what is meant by "current amplification". The ratio, small change in Ic/corresponding change in Ib, is known as the "current gain" of the transistor of a particular working point, and it is denoted by the symbol " $\beta$ ". Many transistors have a $\beta$ of about 50 . It will be shown later that $\beta=\alpha / 1-\alpha$.

## AMPLIFICATION

The emitter of a transistor corresponds to the cathode of a triode valve, the base to the grid and the collector to the anode. The polarities of the bias


Fig. 7: Characteristics of a transistor compared to two types of thermionic valve.
voltages for an n-p-n transistor are similar to those of a triode, but those for a p-n-p type are different. It is convenient at this point to note two important differences between valve and transistor characteristics.
(i) Transistors have a finite base current flow and consequently a low input impedance. Valves do not.
(ii) The collector voltage/current graph of a transistor can be divided into two sections characterised by a low collector (output) impedance at low voltages, and a linear high impedance region of higher voltages. Valves show somewhat different characteristics as illustrated in Fig. 7.
Transistors can be operated in the three modes, common base, common emitter and common collector, similar to their valve counterparts, and these circuits will now be considered in greater detail.

## COMMON BASE

The common base or "collector follower" amplifier circuit is used, like the common grid circuit, for VHF and UHF amplification, as well as to match low impedance to high impedance. Its theoretical and representative practical circuits are shown in Fig. 8.

The current amplification, $A_{I}$, is defined as small change in ic/corresponding change in ib which is equal to $\alpha$. Voltage amplification $A_{7}$, is given by small change in output voltage/corresponding change in input voltage, and since, from Ohm's Law, $V=I \times R$, this can be written as $\frac{\text { ic }}{\text { ie }} \times \frac{\mathrm{R}_{\mathrm{L}}}{\mathrm{r}_{\mathrm{IN}}}$, which is the same as $\alpha \frac{\mathrm{R}_{\mathrm{L}}}{\mathrm{r}_{\mathrm{IN}}}$.

The power gain, $A_{p}$, is the product of voltage and current gain which is $\alpha^{2} \frac{R_{L}}{r_{I N}}$ or just $\alpha \cdot A_{V}$.

The input impedance is defined as $\mathrm{r}_{\mathrm{IN}}=$ small change in ebe/corresponding change in $i_{\text {e }}$. However, from Ohm's Liaw, $V=I \times R$, so that

$$
\begin{aligned}
& e_{b e}=i_{e}\left(r_{l N}+R_{S}\right)=i_{e} \cdot r_{I N}+i_{e} R_{S} . \\
& \therefore i_{e} r_{i n}=e b e-i_{e} R_{S} \\
& \therefore r_{I N}=\frac{e b e}{i_{e}}-R_{S}
\end{aligned}
$$

It is thus shown that the total effective Rin is the sum of the transistor input impedance and the source impedance, Rs, of the input. The transistor input impedance is found to vary greatly with $R_{L}$.

The output impedance, $r_{\text {out }}$, is small change in $\mathrm{e}_{\mathrm{cb}}$ / corresponding change in $i_{c}$.

This quantity tends to increase as the source impedance, Rs, increases.

## Examples

Fig. 9 depicts an impedance converter for matching a $200 \Omega$ (low impedance) moving coil microphone to a 24 V transistorised amplifier with a $10 \mathrm{k} \Omega$ input impedance. A low-noise n-p-n medium power transistor with an $\alpha$ of 0.990 is used. Find, approximately, (a) current (b) voltage (c) power gains of the circuit, assuming $\mathrm{r}_{\mathrm{IN}}=200 \Omega$.
(a) Current gain $=\alpha=0.99$
(b) Voltage gain $=$

$$
\alpha \frac{\mathrm{R}_{\mathrm{L}}}{\mathrm{r}_{\mathrm{IN}}}=\left(0.99 \times \frac{10,000}{200}\right)=50 \text { approx }
$$

(c) Power gain $=A_{I} A_{V}=50$ approx

Note that $R_{L}$ has been made as small as possible to ensure low input impedance and that a resistor R1 has been included in series with the input to increase the transistor output impedance, typically,

(b)

Practical AF


Fig. 8: Transistor in a collector-follower configuration (a) with a practical circuit for audio apptications (b) and high-frequency use (c).


Fig. 9: Circuit using a collector-follower as an impedance matching device, the characteristics of which are discussed in the text.
to over $100 \mathrm{k} \Omega$. This is, of course, shunted by $\mathrm{R}_{\mathrm{L}}$, so that the overall output impedance is nearly $10 \mathrm{k} \Omega$, as required.

## COMMON EMITTER

The theoretical and practical representative circuits of common emitter amplifiers are shown in Fig. 10. The common emitter circuit is widely used for AF and many lower frequency RF applications where a


Fig. 10: Theoretical circuit (a) and two practical circuits (b) and (c) for a common-emitter high gain application.

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high gain is necessary. It is seldom found in VHF applications because common base circuits are more stable and give greater gain.

The common emitter current gain, often denoted by $\beta$, is given by $\beta=\frac{\alpha}{1-\alpha}$, which is derived as follows: $-\alpha=i_{0} / i_{g}$ But $i_{s}=i_{0}+i_{b}$ (Using Kirchoff's 1st Law) (as )

$$
\begin{aligned}
& \therefore a=\frac{i_{c}}{i_{c}+i_{b}} \therefore \alpha\left(i_{c}+i_{b}\right)=i_{c} \text { and eventually } \\
& \frac{i_{c}}{i_{b}}=\frac{a}{1-\alpha}=\beta
\end{aligned}
$$



Fig. 11: Typical audio stage using the common-emitter circuit.

Thus, if for a given transistor $\alpha=0.98$, then $\beta=\frac{0.98}{1-0.98}=49$.
As for common base operation, the voltage gain is calculated from Ohm's Law:-

$$
A_{V}=\frac{\text { small change in } e_{c}}{\text { corresp. change in } e_{c b}}=\frac{i_{c} \times R_{L}}{i_{b} \times r_{I N}}=\beta\left(\frac{R_{L}}{r_{I N}}\right)
$$

The power amplification, being the product of voltage and current amplifications, is given by

$$
\beta^{2}\left(\frac{R_{L}}{r_{I N}}\right) \text { or } \beta\left(A_{V}\right)
$$

As with valves in the common cathode (normal)


Fig. 12: Theoretical and practical circuit for the emitter-follower which can be used to convert a high impedance circult to a low one.
configuration there is a phase change of approximately $180^{\circ}$ between output and input.
Similarly the input impedance $r_{I N}=\left(\frac{e_{b} e}{i_{b}}-R_{s}\right)$.
This quantity is greater (about $1 \mathrm{k} \Omega$ for a small AF transistor) than in the common base mode, and decreases slightly with increasing $\mathrm{R}_{\mathrm{L}}$. The output impedance rout is considerably lower than in the common base mode, and decreases somewhat with increasing $\mathrm{R}_{\mathrm{s}}$.
Fig. 11 depicts the first AF stage in a transistor radio set. Find (a) the current gain (b) the voltage gain (c) the power gain, if the transistor has an $z$ of 0.983 and the input impedance is $1 \mathrm{k} \Omega$. Neglect the loading of the following stage.
(a) $\alpha=0.983 \therefore \dot{\beta}=\frac{a}{1-\alpha}=\frac{0.983}{0.017}=58$ approx
(b) Voltage gain $=\beta \times \frac{\mathrm{R}_{\mathrm{L}}}{\mathrm{r}_{\mathrm{IN}}}=\frac{58 \times 4.7 \times 10^{3}}{1 \times 10^{3}}$

$$
=273 \text { approx }
$$

(c) Power gain $=\beta \times \mathrm{A}_{\mathrm{V}}=58 \times 273=15834$

## COMMON COLLECTOR

This third configuration, sometimes known as the "emitter follower", is used only for matching a high impedance to a low impedance. It is not commonly found elsewhere because little power gain is possible, the voltage gain being less than unity. The current gain is about the same as for common emitter operation. Input impedance is found approximately from $\frac{\beta}{R_{L}}$, output impedance from $\frac{R_{S}}{\beta}$.
Although these are only approximate it is found that accurate values are seldom needed. Fig. 12 shows theoretical and practical common collector circuits.

## PW TECHNICROSS PUZZLE Solution to No. 13 presented last month




IF a home-built receiver or a signal generator is to be calibrated, or a receiver with errors in calibration is to be adjusted, some accurate means of obtaining frequencies for this purpose is required. Assuming that an accurately calibrated signal generator is not available, one method is to employ a harmonic marker giving a range of known frequencies. Such a marker is generally crystal controlled and thus relatively expensive. However, it is possible to dispense with crystals and still obtain a degree of accuracy which is greater than that with which the usual tuning scale can be read visually and which is thus high enough for most purposes.

The unit described here is not crystal controlled, but provides frequencies of $100 \mathrm{kHz}, 1 \mathrm{MHz}$ and 5 MHz , and their harmonics, and can be of enormous aid in calibrating the tuning scales of receivers covering frequencies to 30 MHz or higher.

## HARMONIC CALIBRATION

Fig. 1 shows some of the calibration signals obtained from the unit, and which might be marked on a receiver tuning scale. These will explain how the calibrator aid is used. One fundamental frequency provided is 100 kHz , and its harmonics are multiples such as $200 \mathrm{kHz}, 300 \mathrm{kHz}, 400 \mathrm{kHz}$, and so on. Scale " $A$ " is a typical medium wave range for a receiver and the 100 kHz harmonics furnish calibration points from 600 kHz to 1500 kHz (or 1.5 MHz ). If necessary, the 1000 kHz mark is at once identified by the 1 MHz fundamental frequency provided by the. unit.

(B)

(C)


Fig. 1: Typical dial calibrations on a receiver, all of which can be checked with the callbrator.
Scale " $B$ " is a short wave band, in this instance covering from $1 \cdot 8 \mathrm{MHz}$ to $5 \cdot 1 \mathrm{MHz}$. The $2,3,4$ and 5 MHz tuning points are given by harmonics of the 1 MHz frequency and the 100 kHz (or 0.1 MHz ) har. monics fill in between these. This permits calibration for an Amateur band such as $1 \cdot 8-2 \cdot 0 \mathrm{MHz}$ or 3.5 3.8 MHz to be made easily.

Scale " C " is that of a higher frequency range with 5 MHz points from 15 MHz to 30 MHz given by


The author's protolype built on a metal panel and fitted in a plastic box. General radiation may provide sufficient signal for most purposes but for maximum output the signal can be taken from the coaxial socket.
harmonics of the 5 MHz frequency, and 1 MHz intervals completed by the 1 MHz signal harmonics. There is of course no need to provide only those calibration marks shown in Fig. 1. The 100 kHz signal and its harmonics, the 1 MHz signal and its harmonics, and the 5 MHz signal and its harmonics may be used without breaks over the whole frequency range, up to the frequency limit at which they can no longer be detected.

Each range of harmonics is obtained without any indication of the order of multiplication. For example, if a MW band is dealt with (such as "A") marker signals will be heard at 100 kHz intervals. To number these, it is necessary to discover what the frequency of one such mark is. Here, the 1 MHz signal does this, and the scale can be counted off and numbered up and down from this point.

With a range similar to that at " B " 5 MHz could be identified from the calibrator and 1 MHz harmonics counted off from this. With range " C " it would be necessary to identify readings to one 5 MHz point, either by reference to the expected tuning coverage of the receiver, or by finding a known band, such as the 14 MHz or 21 MHz Amateur band, by listening. Once any single frequency is identified, calibration points can be counted from it, and numbered.


## CIRCUIT

In Fig. 2, Tr 1 is an audio oscillator and modulates the RF oscillator because of the common resistance R7, to allow easy identification of the marker signals. Should TI be other than listed, it may be necessary to reverse connections to one winding to obtain oscillation, or to change Cl or R1 to secure a suitable tone.

Transistor $\operatorname{Tr} 2$ is the RF oscillator and the 4 way switch S1 transfers collector and base circuits to L1, L2 or L3. These inductors are tuned by capacitors $\mathrm{C} 2, \mathrm{C} 3$ and C 4 : and are set to 5 MHz for $\mathrm{L} 1,1 \mathrm{MHz}$ for L 2 , and 100 kHz for $\mathrm{L3}$, by adjustment of the cores. Signal output is taken from the capacitor C8, but in many cases no electrical connection to the output socket is necessary. One pole of the switch breaks the battery circuit.

## CONSTRUCTION

Most of the components are assembled on plain perforated Veroboard $95 \times 41 \mathrm{~mm}$ ( $3^{3}{ }_{4} \mathrm{in} \times 1{ }^{5}$ in ) as in Fig. 3. A bracket cut from scrap metal is bolted to the board which allows the switch to be used to mount the board on the panel. The collector lead of Tr 2 and C6 are connected directly to tags S1a and SIb of the switch. S1c has a flexible connection with a positive clip while the battery negative runs from R7. Put sleeving on all leads where necessary.

The case used has a panel $152 \times 90 \mathrm{~mm}$ ( $6 \times \mathbf{x 1}_{2} \mathrm{in}$ ) but any box of somewhat similar size would be satisfactory. The switch and assembled circuit board fit as in Fig. 4. Holes are also drilled for the three coils and for the output socket. The latter holds a bracket, fitted to retain the battery at the end of the case.
For easy soldering, the coil pins should be scraped first and lengthy heating must be avoided here or the pins may become loose in the formers. Wiring can be finished off from Fig. 4 and a check made that all is in order.

## COIL ADJUSTMENT

The capacitor values are chosen so that adjustment of a coil core allows a fairly small band of frequencies around that wanted to be tuned. Before the unit can be used the cores have to be set with the aid of a radio receiver. To set L 3 to 100 kHz tune the receiver to the long wave programme of BBC on 200 kHz . Switch the calibrator to 100 kHz and turn the core of L3 until a whistle is heard on the programme. This is the second harmonic of 100 kHz . A zero beat or central position will be found, which is

## components list








 thythosinor


 F 100608)




the correct position. Turning the core either way from this will result in a whistle which rises in pitch.

The core of L 2 is most easily set to 1 MHz by using a short wave receiver to tune in' a standard frequency transmission on 5 MHz and adjusting L 2 for zero beat. Check that this is correct by noting that the signal comes up at 1 MHz or 1000 kHz on the MW band of the receiver. L1 can also be adjusted to 5 MHz by this means.

One range may help provide tuning points for another. For example, when the 100 kHz frequency is set using the BBC's long wave transmitter, 1000 kHz can be identified on the receiver MW band and L2 can be tuned to this. Harmonics of 1 MHz will then allow a fairly accurate location of 5 MHz on the receiver, to find the standard frequency signal, so that L2 can be correctly set, and also L1.

Once the cores are correctly positioned, they will need only a small re-adjustment occasionally, and this can be done in a few moments with the aid of the 200 kHz and 5 MHz signals mentioned. The long term stability is of course not that of a crystal controlled oscillator, but if the calibration is checked before using the calibration aid, accuracy easily equals the ability to read an ordinary tuning scale.

For long and medium waves, it may be sufficient to place the unit near the receiver, especially if the latter has a ferrite rod aerial for these bands. For higher frequencies, and higher orders of harmonics,
more coupling is required. A lead from the output socket can then be placed near the receiver aerial socket or can be directly connected, as necessary. With the usual communications type receiver or reasonably efficient short wave receiver, the 1 MHz and 5 MHz harmonics can be heard up to 30 MHz . The upper limit at which the 100 kHz harmonics can be heard depends on the receiver, and these become rather difficult to detect above about 5 MHz , but can be heard well beyond this with a sensitive receiver.

When preparing the scales for an actual receiver, note that the high-frequency end of a band is generally to the left, and that marking become progressively closer together. Despite this, they will have a regular appearance when counted off systematically.

To calibrate or check the calibration of a signal generator tune a receiver to various harmonics of the calibration aid and then tune the generator to zero beat and mark its scale. Where the receiver does not cover the generator frequencies completely, a barmonic of the generator signal may be used. For example, 900 kHz on the receiver can be used for 450 kHz on the generator, or second harmonic.

As the unit is not crystal controlled, remember to check the frequency when it is used to calibrate other equipment. The cores may be locked with 6BA nuts.


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## Specification



WHEN first designing the counter, cost was the first consideration, since it needed to be a versatile instrument, and within the pocket of the home constructor. At the same time it needed to compete favourably with commercial designs, and for this reason the counter design has been kept as simple as possible.
One of the major considerations was in deciding the type of display to be used. Having surveyed the various types available, it was decided to use Doram filament types, as they come complete with ready made PCB's. Alternatively, LED's may be used.

## CIRCUIT DESCRIPTION

The input stage centres around IC1 which has 3 functions; (a) To amplify the incoming signal (or attenuate as appropriate) suitable for operating the counter. (b) To shape the signal into a waveform for operating the counter, and (c) To provide a suitable impedance so as not to unduly load the circuit under test.
The crystal clock, provided by Tr1 and 2 operates at 100 kHz , to provide a square wave to operate the counter. IC3-7 divide the clock down to the required times. The display consists of a four stage counter, IC11-IC14. Four BCD stores, IC15-IC18, and the decoder/driver, IC19-IC22, driving the display. The control logic of the counter is centred on the pulse generator, IC9 and IC10. When in the frequency mode, the signal, having been "cleaned up" is passed into the counter IC14, via the switching system and the gate of IC10, the state of which is determined by the flip flops (FF1 and 2) in IC9.

In operation a clock pulse will change the state of the second flip flop, which in turn will open the gate in IC10 and allow the signal to pass. When the clock pulse ends, the state of the flip flop is reversed, thus ending the count. At the same time a condition is passed to the pulse generator causing it to operate. This has three functions; (1) To enable the stores, thus registering the count in the displays, (2) To reset the counters to zero, (3) To set the first flip flop in IC9, thus enabling the second flip flop to operate on the next clock pulse.

In the period mode, the clock pulse is continually passed to the counter, and the incoming signal now operates the flip flop in IC9. In the time mode the same happens, except that the control signal to IC9 comes from the monostable IC2. This provides a short pulse when triggered by a logic " 0 " at either SK1 or SK2. In the test position the switching system selects a clock time of one second and a frequency of 1 kHz , the counter thus has a display of 1000 .

## OPERATING PRINCIPLES

Referring to Fig 1, the input signal is applied to the input of a counting stage with its associated display, via a switch. Assume for the moment that the signal is a square wave of 1000 Hz , and the switch is closed for exactly 1 second. In that time therefore 1000 cycles will have passed through to the counter. If the counter has 4 decades driving 4 separate dis-


W212
Fig. 1: Block diagram showing the path of a signal applied to the counting stage.
plays, then the number displayed will be 1000 . It follows then, that the maximum frequency of the counter will be 9999 Hz , ie, a maximum of 4 digits in the display.
To increase the maximum frequency of the counter, all we need to do is to shorten the time the switch is closed. Take for example a signal of

## No

## PART 1



1 MHz . If we close the switch for $1 / 1000$ of the time, then the display will again show 1000 but this time it will represent kHz . In a practical counter the switch is replaced by an electronic gate, and the time the switch is closed, is referred to as the gate time. The accuracy is therefore dependent on the accuracy of the gate time, and in the present design this is accomplished by using a highly stable crystal oscillator.

## MODES OF OPERATION

In this design, 3 basic modes of operation have been provided for, these are detailed as follows; Frequency

With reference to Fig. 2, the signal whose frequency is to be measured is applied to the input stage. The function of which, is to either amplify or attenuate the signal and to convert it into a square wave. The gate time is selected by 54 and applies it to the control logic, assuming the counter has


Fig. 2: The incoming signal is converted into a square wave, amplified or attenuated, and applied for one clock pulse.
been reset to zero, the operation is as follows; The gate is enabled for one period of the gate time (clock-period) which allows the square wave to pass through to the counter. At the end of this period, the control logic inhibits the gate, and provides two
pulses. One for enabling the store thus registering the count, and the second to reset the counter. At the same time it enables the gate to open on the


Fig. 3: In order to measure low frequencies, the roles of the clock generator and input stage are reversed.
next clock pulse, the result of which causes the display to update alternate clock pulses.

## Period

The main difference between period and frequency measurement is that the roles of clock generator and input stage are reversed, as shown in Fig. 3. Instead of counting the number of input cycles during one clock period, the number of clock pulses


Fig. 4 : Block diagram showing the method used for time measurement. In this mode, maximum time indicated is 9999 s .


General interior photo graph of the unit showing tayout of olsplays and their associated PCB'sy function sw/tches and math board contathing all fogic and fransistior components.
during one input cycle is counted. The selected clock period is applied to the counter via the gate. The input waveform, after being cleaned up, is applied to the control logic. The store and reset pulses are generated in the same way but this time using the input waveform as the initiating signal. The period measurement is useful for low frequencies, such as those below 10 Hz . At the same time it is more accurate.

## Time

Referring to Fig. 4 it may be seen that time measurement closely resembles that of period. The major difference is that the control signal to the control logic comes from the timer control.

In operation, the time interval selected again passes to the counter and the timer control is connected to the control logic. When the start terminal is connected to 0 V , the timer control produces a short pulse which operates the control circuitry to open the gate. The counter will now count in units as selected. For example, if a time interval of 10 m is selected, the counter will count in units of 10 ms , the display therefore will be in units of 10. A display of 875 therefore represents 8750 ms or $8 \cdot 75$ seconds.

When it is desired to end the count the stop terminal is connected to 0 V , which again produces a short pulse to close the gate and initiate the store and reset sequence. The display will now hold that count until the counter is reset.

## STAGES

A block diagram of the frequency counter is shown in Fig. 5. All of the above modes have been catered for, plus an extra position for testing.
PSU: This section provides the following voltages for the various sections, +5 V for the main circuit board, +5 V for the display, +12 V and -6 V for the input stage.
Input stage. This section converts the incoming waveform to operate the TTL circuits correctly.
Timer control. This stage produces a short pulse to operate the control logic when used in the TIME mode.
Crystal clock. This stage operates at 100 kHz and provides a square wave to operate the dividers.
Dividers. Five stages divide the standard frequency down to the times shown.
Control logic. This performs the following functions; (1) To reset the counter to zero, (2) To store the count reached, (3) To open the gate for the time selected.
Counter/store/decoder/display. These units together perform as a 4 stage counter, to count and display the frequency being measured.
Switching network. The switches incorporated in this section perform the three modes of operation as detailed above.

Referring to the power supply circuit diagram, Fig. 6. T1 provides two windings of $6 \cdot 3 \mathrm{~V}$ at $1 \cdot 8 \mathrm{~A}$. The first winding being half wave rectified with CI


Fig. 5: Diagram showing the complete unit in block form. The crystal clock has a frequency of 100 kHz , which is subdivided down to 1 Hz by means of five 7490 IC's.
providing a small amount of smoothing. This is then used to power the displays. The second winding is bridge rectified by D2-D5, and smoothed by C2. A 5 V regulator is used to provide the required voltage for the remaining circuit. A small amount of smoothing is provided by C3, and RF noise being decoupled by $C 4$. The second transformer T2, supplies 18 V to the bridge rectifier Brl, while the two zener diodes provide +12 V and -6 V for the input stage.

It will be noticed that when all the segments of the displays are on, slight dimming occurs. This is due to the rather simple nature of the supply, although in practice this is quite acceptable, since
when operating with their correct voltage, the displays can be quite dazzling.

## INPUT STAGE

ICl Fig. 7 together with its associate components form the input stage of the circuit. The 710 is a comparator and has two inputs, inverting and noninverting, pins 4 and 3 respectively. In use if the non-inverting input goes more than 5 mV positive than the inverting input, the output goes high. Conversely, if the inverting input goes more positive than the non-inverting input, then the output goes low. R5, 6 and 7 provide positive feedback to the non-inverting input, which causes the device to


Rear: Wew photograph giving detalls of the power supply hoard, regulator and fuse bracket, and smoothing capacitor C2.

## components list


operate as a schmitt trigger, and is used to shape the signal into a square wave. Input protection to the device is provided by the two diodes D8/D9, which conduct at about $0 \cdot 7 \mathrm{~V}$ thus limiting voltage excursions to the IC.

The maximum voltage which may be applied to the instrument, is mainly dependent on the dissipation of R3. In the present design this works out to approximately 14 V . If the power rating of the resistor is increased, to say, 2 W then the input voltage may then


Fig. 6 : Although the above power supply is of a simple form, It has to supply four separate voltages. These are +5 V regulated, +5 V unregulated +12 V and -6 V .


Flg. 7 : Part of the complete circuit diagram showing details of the following stages:-Input stage, timer control, crystal clock, divider stages and switching network.
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# PRACTICAL WIRELESS FAULFFWNDNE CUIDE continued from April 1976 

> In the first part of this Guide Les Lawry-Johns concentrated on test equipment and methods of checking transistors and components. This concluding article deals with the technique of logical fault-finding in a typical piece of equipment, a Music Centre, and on getting the maximum amount of information from observed fault symptoms.


The Chinaglia Belluno P73 single trace oscilloscope has an input impedance of $1 M \Omega$ and the input capacity is 45 pF . The $Y$ amplifier response is $3 d B$ down at 8 MHz .

What's all this got to do with fault finding? Precious little but there are other matters to consider and it is as well to ponder on these as it is very difficult to earn a living at servicing alone. The one that can make a fortune at it will have to be a hard man indeed, and I don't know of him!

General servicing, such as we have in mind, will mainly concern radios and TV receivers, but the latter are adequately covered by our sister magazine Television and so we must concern ourselves here with the radio side, with reference to tape recorders, amplifiers and the like. Recent issues of PW have given a general idea of the methods employed in servicing car radios, unit audios and valved equipment etc. So here we are concerned with fault tracing, diagnosis and handling.

## DISMANTLING

Whilst one glance is all that is required in some cases, to see how a particular set is to be dismantled, in others no amount of inspection seems to reveal how the thing comes apart. If the maker's service information is to hand this may explain all, or it may not. The best thing to do in such cases is to remove what can be removed and hope that this leads on to the next step. For example, if it is a battery operated transistor radio, the cover of the battery compartment, as well as concealing the battery, will often conceal the: main fixing screw, the remaining fixings being tongue-and-groove pressings. Others may require the dial glass to be removed before the main frame screws are revealed. Quite a few require the carrying strap to be removed by a
downward pressure against a spring which then reveals the side fixing screws.

Having overcome this first hazard it is often necessary to remove the panel from the main frame. Care is required here as some of the screws may be employed in securing the dial drive to the panel and these must not be loosened. Reassembling a dial drive can be one of the most frustrating and time-wasting exercises it is possible to imagine so it is well worthwhile assessing the exact purpose of each visible screw. In many cases the relevant screws are marked with a spot of coloured paint to identify them and these are the ones which should be removed first.

## FAULT TRACING

Having gained access one can then get down to the main object of the exercise which is to find out what is wrong and ascertain what is likely to be needed to put it right. We say likely because it is often well-nigh impossible to do this without actually doing the job. This is why it is not feasible to supply an accurate estimate of cost and why, if one is pushed to supply one, the job should be turned down as gracefully as possible. What is more reasonable is a rough estimate combined with a goodly amount of mutual goodwill and trust.


The Paramo loose drill chuck can be quickly fitted to almost any ratchet screwdriver and will take drills up to 6 mm for smaller ratchets and 8 mm for larger ratchets.

A fair amount of battery operated equipment fails to function purely as a result of poor contact in the battery compartment. This is often the result of batteries being left in too long, the resultant weeping of electrolyte corroding any metal which may be in the vicinity. If the battery box is a separate item, it is best to replace it, clear up any spillage from the receiver, with bicarbonate of soda, fit new cells or batteries and make sure the thing works. If there is no battery box, only a compartment, the job may be more complicated even after the spillage has been neutralised and cleaned up. Some improvisation may be necessary to replace corroded springs and this is why an old torch is never thrown away without removing the springs. Even the springs from ball-point pens have their uses when the pen is finished.

Even though there is no sign of trouble, it pays to check that all is well in the battery compartment before moving on. We have bitter memories of a Philips receiver which
used two 9V batteries. One battery read 8 V and the other nothing. There was a good reason for this, since there was a dead short across it! Tracing the leads back, we found they went to the on-off switch and were shorted by the switch. It took a little time to realise that this was quite correct and that the black leads were on the wrong batteries. They had been originally taped to prevent this confusion but the tape had been removed at some time and the owner had finally made the fatal wrong connection and concluded that the set was at fault. The possibility of this happening should have been anticipated by the designer and the batteries should not have been side by side, but there it is, the set was quite old and had functioned for years before this happened.

If a short or partial short is found across the batteries the normal cause is defective output transistors or a shorted electrolytic capacitor. A fair indication can be obtained by switching the meter to the 100 mA range, lifting off one of the battery connections and connecting this to one meter lead, and the other to the battery. The actual connection of course depends upon which lead is lifted. If negative, the positive probe of the meter goes to the lead, the negative to the battery. With the volume control turned down a reading of not more than 20 mA can be regarded as reasonable, depending upon the receiver, the average being quite a bit less than 20 mA but usually over 10 mA . If the meter reads over this either the sound will be deafening where the volume was left turned up or there is indeed a short of some kind.

## THE ‘SHORT'!

Now let's pause here and consider the term "short". It implies that the circuit is of much lower resistance than intended and that it cannot operate correctly. This is the opposite to "open' circuit, which is the other basic fault usually of extremely high resistance. Putting it in the simplest possible terms we can say that there are only two basic faults which can happen to an electrical circuit, either an "open" circuit where nothing happens or a"short" where too much happens! The complication arises due to the degree of the condition i.e. a partial short which is a leak, or a partial open circuit which is a higher resistance than intended. Most appliances consist of not just one circuit but of a great many, so "circuitry" is the better term. The art is to locate the faulty circuit in the shortest time, recognising the nature of the fault and knowing what is needed to put it right.

The first step is to find out what does work as opposed to what doesn't. Let us consider the case of a mains operated Music Centre, consisting of a cassette recorderplayer, a record player with auto changer and radio facilities with stereo VHF plus long and medium wave AM. We will assume this has been received for servicing, without loudspeakers, and with the minimum of information regarding the nature of the fault(s). Probably just a label marked, unhelpfully, "does not work'l This shouldn't be allowed to happen in the first place and more information should have been supplied, but this is an exercise, not an actual case.

A preliminary check shows that the appliance is marked at the rear with the mains input, if you are lucky, complete with lead and not just an awkward input socket with no lead! The loudspeaker terminals or sockets will be marked

 rapidly locating a component on the circuit diagram.
with the matching impedance, probably $8 \Omega$. Possibly $4 \Omega$ but use $8 \Omega$ if in doubt: better to underrun than risk losing the output transistors. Connect suitable speakers and if the mains input lead has a fused plug, check on this first before taking any other action. Remove the fuse and check its rating and whether it is intact. It will probably be intact but it could be too high a rating. Reduce to 3A or less. If, in fact, it has blown, check the receiver end and if there is a filter capacitor across the on-off switch suspect this and use a suitable replacement rated at least 240 V AC or 1 kV DC.
The method of gaining access will depend upon the unit and it must be admitted that there are a few which appear to have been designed with absolutely no regard for service at all! If there is a dust cover, carefully stow this in a safe place, ensure the record deck is locked in the transit position and the PU arm clipped. Turn the unit up on one end and make sure it cannot topple over. If there is a bottom cover, note how many screws secure it. If there are a large number in various places it probably holds some of the units and is probably not meant to be removed for normal service. If it is of light construction and is only secured around the edges it can probably be removed for inspection. If the bottom cover is not meant to be removed, it will probably have either a couple of holes to provide access to the retaining clips of the auto-changer or some screws which reach through and secure the top cover. If in doubt, the maker's service information should be consulted.
Having ensured that the speakers are connected and the mains input is intact, plug in and switch on. The mains indicator light may come on but if it does not, switch on the auto-changer to see if the turntable rotates. If nothing happens it can be assumed the set fuse in the mains
supply, somewhere around the mains transformer, has failed. The rating of this will be around 300 m A surge limiting, the ones with a little spring inside. There are times when these can fail simply because they are fed up with life and a replacement will restore normal operation but a little caution is required here. First look at the fuse to see how it has failed. If it has shattered or is blackened there is no point in putting another one in, and on no account put a fuse in which has a much higher rating. The cause must be traced and rectified.

## FUSES

We all get caught out with fuses sooner or later as it is difficult to carry all ratings and types at all times. A little common sense can be used however and if the original rating was say 315 mA fit one of between 250 mA and 500 mA without too much fuss, but these limits should not be exceeded. If the blown fuse is blackened, there is probably a direct short across the supply or there is a short across the secondary of the transformer, most likely a defective bridge rectifier. The former should direct attention to any mains filter capacitor included after the fuse, rather than across the on/off switch and also to the gram motor, the winding of which may appear blackened. Not very often but it does happen. The latter fault, a bridge rectifier breakdown is quite common. The bridge may be formed by four separate diodes or one block with four lead outs. If it is (they are) defective there is usually some visual sign, a block may be bulged or individual diodes blackened. If the fault is further in, the supply fuse would not normally be the one to fail as there is a fuse included in the lower voltage supply line to the amplifiers and the cassette

# FAULT~FINDING GUIDE 

player etc. This fuse will usually be rated at some 2A and will fail when a short or other overload occurs in the associated circuitry. There is little doubt which fuse is which as they are marked on the panel or at least on the fuse and their situations leave little doubt, the smaller mains fuse being near the mains transformer or on/off switch, the larger rating fuse being on or near the rectifier or main electrolytic smoothing capacitor.

Now there is always the possibility that some bright spark has been there before you and has fitted a heavy fuse in the low voltage (LV) side, say 5A, and that the mains fuse has failed because of this and that the fault will, after all, be found on the amplifier panel. If this is indeed what has happened, leave out both fuses and check, both visually and with a meter, to see if the fault can be spotted or isolated. We say spotted as it is quite common to see some evidence of overheating usually in the small resistors associated with the output transistors, which immediately calls attention to the transistors, or slight discolouration around the audio chips if ICs are used. Also bear in mind the fact that dial lamps are often fed from the LV line or from the transformer secondary and that the lamps themselves can short or the holders into which they are fitted can be defective. If in doubt disconnect the supply lead(s) and check each separately. If no shorts are found, fit the correct fuses and switch on. It is possible that both fuses will hold and the set will operate for some time, say on radio. If this is so, switch over to the cassette player and see what happens. It is possible, again, that the LV fuse will now fail. If it does you then know where the enemy is hiding!
If the fuses hold, it means a long soak test and possibly


The Heathkit Type 670 in-circuit tester is capable of measuring the current in a conductor on a PCB while the circuit is in operation.
a request to inspect the loudspeakers, one of which may have defective wiring. This latter check is not likely to be fruitful as a shorted speaker outlet would normally cause damage to the output transistors or chip arid recovery is most unlikely, but it can happen. If the LV fuse blows on switch-on, you probably haven't conducted your investigation in the true traditions of the service so start again, isolating and testing each take off point, possibly cutting through a track or two to isolate a particular line, joining up with a lead soldered across the gap, not, repeat not, just a blob of solder which may hold for a moment and then crack. When faulty section has been located you may well kick yourself because the visible evidence was there all the time and missed it. If this is not so you can congratulate yourself for tracing it logically, even if it was only a whisker of wire across two tracks at some hidden point.
Now it is quite likely that the fuses may hold but some overheating may be taking place and a resistor or perhaps a heat sink may feel quite hot to touch. Whilst this may be due to a faulty transistor or a leaky capacitor, it is possibly due to a preset control being maladjusted, causing the output circuit to draw too much current. If the circuit is available the voltages can be checked to see if they conform or can be made to conform, otherwise the voltages on the normally working channel can be compared with the defective channel and the right conclusions drawn

## OUTPUT TRANSISTORS

Output transistors often have a smaller transistor wired across their bases with a preset control provided from collector to base, to set the conduction of this smaller transistor. The more it conducts the closer are the potentials of the bases of the output transistors and the less they conduct, and vice versa, with increased conduction producing more heat. If this causes some head shaking in some quarters because it seems hideously wrong we would point out that the reader should do his own homework, we are only concerned here with the practical results not the theory! We could say that if the small transistor were replaced by a simple resistor, the value of which determine the conduction of the output pair, the lower the resistance the less current is drawn, but such a device allows no compensation such as is provided by a transistor, properly set up.

In stubborn cases, the freezer solution aerosol and the hair dryer mentioned in the first part of this saga can be brought to bear and the results obtained by these assessed, to pin-point a certain component or small area which enables one to draw a conclusion, hopefully the right one, and the correct replacements made.

## HUM

One of the most common complaints is not that the equipment does not work at all but that "it hums". The first question must be, assuming this is a stereo outfit, "which side hums, or is it both channels"? If both, the problem is a little easier and is likely to be due to a defective rectifier, probably of the bridge type, which is leaking but not enough to blow a fuse, or a faulty electrolytic capacitor where one of the end contacts is not properly made to the lead-out tab. The electrolytic could be dried up and this is what we would have gone for, once upon a
time. Times change though and so do the habits of certain components. If the rectifier is not running warm and the electrolytic is not at fault it is likely that it was not the right assessment in the first place and that one channel is in fact inoperative, drawing too much current and thus impairing the smoothing. If this is so there is probably output trouble, so back to the previous paragraph!

However, hum is not all in the power supply and output transistors overheating. It can be due to poor earthing, dry joints, defective controls but less often to resistors which have gone "high". Once more, ask the questions. Is it one side only or both, does it occur on radio or gram or both, what effect does the volume control have? When these questions are answered leap into action and head straight to the source of the trouble!


Precision Petite Ltd. produce this very useful 12 V DC electric drill. A stand is a/so available and a kit of tools.

The radio doesn't hum but the gram does, the volume control reducing the hum. Start from the pick-up head, checking the tags first and the way the wires are secured in the tags. Often they are not soldered, merely pressed with the tag making better contact with the plastic insulation than with the actual wire. Correct this and follow through to the underside of the deck where a similar system may be employed, checking the lead-outs and terminals (or phono plugs if used) and the earthing of inner tags or outer screening, as appropriate. Follow on to the input to the amplifier and note that many units use a preamplifier stage for gram input which is not used on radio. The hum could well be occurring in such a preamplifier stage especially if this is a separate unit raised from the main board. These are the simple but essential lines one follows to locate hum, there is nothing complicated about it but some patience is often necessary in order to pin it down.

## DISTORTION

We have mentioned this problem in several articles and do not wish to go on unnecessarily. There are all types of distortion and one's ears become trained to detect the differences between a low supply voltage (the battery's flat!), cross-over distortion where the output stage is
not being allowed to work properly, unbalance where one transistor is working and the other cannot or will not, loudspeaker rubbing where the speech coil is fouling the magnet, the strangled sound of an output valve running into grid current or the clipped noise of a high value resistor stressing the sibilants.

Sounds are very difficult to describe in words and if the ear is not educated enough to enable a short cut to be made, routine tests will have to be made, starting from the supply and working through, checking voltages and, if necessary, the current drawn, plus cold resistance tests etc. to ascertain where the readings depart from those expected. If it takes a long time, don't worry, you'll recognise that sound again and it won't take nearly so long next time.


West Hyde now offer a new range of quality tools including these long-nosed pliers, curved needle-nosed pliers, side and face cutters. The long-nosed pliers have an internal spring to bias them in a normally-open position.

## TAKING VOLTAGE READINGS

It is one thing to take a number of readings, it is another to review them in order to reach the right conclusion. In order to do this one needs to know, within limits, what to expect before any readings are taken. This can be gathered from service information or from previous knowledge of this or a similar circuit. As far as individual stages are concerned, divorced from the preceding and succeeding stages by capacitors or transformers, one or two readings immediately establish the conditions and enable a diagnosis to be made. For example, if a transistor is inoperative, with no emitter reading, although the base and collector
voltages are about right, it does not require much thought to reach the conclusion that the transistor is likely to have an open-circuit base-emitter junction. Note that we said "likely". Now, should the reading show the emitter with a higher voltage than the base, still assuming a straightforward amplifier layout where the collector is relatively high, the emitter and base low, with the base sufficiently above the emitter to allow it to conduct, one can conclude that the transistor cannot operate and one has to find where the emitter voltage is coming from. If there is only a straightforward resistor from emitter to supply or return, it can be concluded that there is a collector to emitter leak in the transistor, which will normally show up on an ohms test.

For example, if the emitter resistor is say 470』, this is the minimum reading to be expected and, if there is doubt, the resistor can be lifted from the circuit at one end to ascertain the exact reading, which should be high, except in the case of one or two specialist types. Where transistors are DC coupled, as in most audio designs, voltage readings.must be looked upon as a very rough guide and not as an instant fault locator. The same can be said for AGC systems where the controlled stages are dependent upon a controlling voltage derived from a source which is itself controlled. If that sounds decidedly awkward, it is.

The audio stages are less awkward since the majority of troubles are usually in the output stage and can be identified by disconnecting the suspect transistor and cold testing it (or them) and associated resistors and then working back from this point.

## GENERAL

These are the general lines to follow. Note what is working and what isn't, disconnect what can be disconnected in order to narrow the field. Accept the fact that you are going to be misled by "red herrings" and write this down to experience. The man that hasn't made a mistake hasn't made anything but you don't have to make the same mistake twice. If a thing looks horribly complicated this is because one is not used to looking at it, but divided into sections there is little to fear although it is still necessary to understand the basic operating principles.

Once the fault has been localised, the rest can be ignored. Concentrate on that section, understand what it is supposed to do before trying to put it right. Get it working properly and then connect up the rest ensuring that this doesn't upset the operation. Start from the supply, get that right or see that it is right, check the output stage as this is where most of the trouble abides and then isolate sections to see which parts are functioning and which are not.

Use the tools you have to the best advantage, including the ears, eyes, nose and sense of touch. Your multi-meter, signal injector, coolants and "heatants", this unlikely last term to include your soldering iron and the hair dryer we spoke of earlier, and above all your ability to think electrically. This. is half the job.

Photographs were kindly supplled by the following companies to whom all queries on the instruments illustrated should be addressed. Heath (Gloucester) Ltd., Gloucester GL2 6EE.
Precision Petite Ltd., 119A High Street, Teddington, TW11 8HG Chinaglia Ltd., 19 Mulberry Walk, London SW3 6DZ Parramore Ltd., Caledonlan Works, Chapeltown, Sheffield S30 4WZ West Hyde Developments Ltd., Ryefield Crescent, Northwood Hills, Northwood, Middx HA6 1NN.

DIGITAL FREQUENCY METER-continued from page 149
be increased to 28 V . However this was not thought too important, since we are generally concerned with low level signals. R8 is added to increase ICl's output current sinking ability. The supply lines are decoupled at RF by the two capacitors C8 and C9.

The input is applied to a standard coaxial socket SK1 by screened lead, and then passes to S2. The purpose of which is to short out the capacitor to allow either AC or DC signals to be measured. It is also used in the DC position when measuring low frequencies, such as those below 25 Hz , and also when in the Period mode.

## TIMER, CRYSTAL, CLOCK AND DIVIDERS

The monostable IC2 uses the external capacitor C10 to achieve a pulse length of about 10 ms to clock FF2 of IC9. The monostable produces this pulse when pins 3 and 4 are connected temportary to 0 V . In the prototype, two sockets are used together with an earth socket to achieve this. In fact only one socket is needed, although two make the connection of external control easier.

Trl is connected as a Colpitts oscillator, Fig. 7 in the emitter follower mode while the crystal X1 works in the parallel mode of resonance. C11 provides series blocking, and R9 base bias. Positive feedback is achieved across the potential divider Cl2 and C13, the centre point being taken to the emitter. Output is developed across R10, and is then fed to the squaring amplifier $\operatorname{Tr} 2$, via C14. Diode D10, together with $\operatorname{Tr} 2$ provides symmetrical clipping of the signal, the output being developed across R11, and finally coupled to the divider stages.

IC3 to IC7 make up the divider stages and are connected in the square wave output mode. They divide the 100 kHz of the oscillator down to the following gate times; $1 \mathrm{~Hz}-1$ second; $10 \mathrm{~Hz}-100 \mathrm{~ms}$; $100 \mathrm{~Hz}-10 \mathrm{~ms} ; 1 \mathrm{kHz}-1 \mathrm{~ms} ; 10 \mathrm{kHz}-100 \mu \mathrm{~s}$.

These outputs are then selected by S4 and passed to $S 3$ where they are passed to either the counter or FF2 as appropriate.

## SWITCHING NETWORK

This hardly needs explanation, since the various paths for the signals etc, may easily be followed in Fig. 7. However, a few points to notice are as follows;

Referring to the range switch $\mathrm{S} 4 \mathrm{a}-\mathrm{j}$. When the test position is selected by $S 3$ (mode) the 1 kHz and 1 Hz times are connected through sections $h$ and a, it is therefore important that no range switches are depressed when in this mode. When masuring frequency, only two gate times may be selected, these are 1s (S4c) and $100 \mu \mathrm{~s}$ ( S 4 i ), therefore pressing any other times will not operate the counter.

Referring to both switches, sections $b$ and $j$. These position the decimal point in the display, eg. when in the TEST and FREQUENCY mode the decimal point will be positioned between the fourth and third digit on the left, thus indicating $1 \cdot 000 \mathrm{kHz}$.

Part 2 continues in the July issue, and will be covering details of the circuit, Veroboard layout, and case construction.


THE Sinclair "Black Watch" is a digital wrist watch of unconventional appearance, as may be seen from the illustration. The watch is available ready-built, or in kit-form, the latter version being priced at under £15, including VAT.
The components supplied include a double-sided glass flbre printed circuit board, a flexible self-adhesive printed circuit, an LED digital display, an 18-pin IC, a quartz crystal, a trimmer, all parts for the case, two cells, a flexible insulated copper screen, a plastic strap, varnish, grease and solder. Assembly and operating instructions are also provided.
The case of the watch is moulded in black plastic material, the back fitting on the front section by "click" retaining lugs. A transparent purple window is fixed in an aperture in the front of the case so that the LED display is visible. Three flexible diaphragms are moulded into the case, two in the front and one in the back. The diaphragms have small pleces of metal foil attached and, when the watch is in use, pressure on the diaphragms causes the foil to short together pairs of contacts. The rear diaphragm is used when setting the watch to the correct time and pressure on the two front diaphragms causes the display to work.

## HOW DOES IT WORK?

The heart of the watch is a quartz crystal which oscillates at $32,768 \mathrm{kHz}$ divided by the IC to obtain one pulse per second, the pulses being counted into minutes and hours by circultry in the same IC. A 4-digit LED display is connected to the IC and brought into action by shorting two pairs of contacts, as mentioned earlier. One pair is used to obtain a display of the hours and minutes held by the watch and the other displays the minutes and seconds. Thus, for a time of


1206 42, the two displays are 1206 and 06 42. If the contacts are shorted together briefly, the display is illuminated for about half a second, or continuously by keeping the contacts closed.
A further pair of contacts is used when setting the watch to the correct time. The hours can be made to advance at one per second until the correct hour is reached and the minutes can also be advanced similarly, while the seconds are held at " 00 ". The only discrete components in the watch are the quartz crystal, a trimmer to allow a small variation in the frequency of the oscillator and a tantalum bead capacitor, though this is omitted from. later kits. The battery consumption is only a few microamps when the dispiay is not in use, but rises considerably when the display is operating. This is the reason why the display cannot be illuminated continuously; battery life would then be very short indeed.

## ASSEMBLY

Assembly of the watch is carried out in a number of stages: preparation and assembly of the PCB; fitting of the flexible PCB; fitting of the insulated copper screen; testing and adjustment; final assembly into case.

The first step is to varnish most of the component side of the glass fibre PCB. The varnish is left to dry, about two to four hours. The ceramic trimmer is then soldered into position on the PCB. The tantalum capacitor is next, followed by the quartz crystal, the display and the IC. This stage is completed by fitting the flexible printed circuit, wrapped round the IC. The flap of the flexible printed circuit carries the two battery contacts.
The watch assembly then looks like the illustration. The total time spent so far will probably be about an hour, excluding the drying time of the varnish. The next step is to fit the insulated flexible copper screen, which is wrapped round the assembly and soldered to one pin of the IC.

## TESTING AND ADJUSTMENT

Testing of the watch is carried out by setting the trimmer capacitor to mid-range and connecting the batteries by a temporary arrangement. If the two pairs of contacts on top of the IC are shorted together, the display should function. Using a radio time-signal, or the telephone clock, the display time is noted at the same time on consecutive days, to determine if the watch is gaining or losing and appropriate adjustment made to the trimmer.
Sinclair say that the watch is ultimately capable of an accuracy of about one second per week. When the accuracy is satisfactory, the watch is fitted into the case, the strap is attached, and the watch is ready to wear.
 mounted on PCB and the flexible printed circuit in position round the IC at left.

For the temporary connection of batteries, Sinclair advise the use of a "Bulldog" clip, but it was very easy to short the batteries accidentally and almost impossible to hold two batteries, a flexible printed circuit and a Bulldog clip in the correct positions, all at the same time! This difficulty was aggravated by a tendency for one digit of the display to light up as soon as the batteries made contact. The instructions said that this might happen and that the remedy was to interrupt the battery supply. Then, of course, the clip, the batteries and the flexible printed circuit tended to part company once more! The problem of accidental short circuits was cured by using insulating tape on one jaw of the clip, but the operation remained very difficult to carry out. The idea of using two wooden clothes pegs (of the spring type), two drawing pins and a piece of insulated wire solved the problem. This enabled the batteries to be fitted one at a time and made the procedure comparatively easy. The adjustment of the watch took some four days to accomplish, but was not difficult, rather a little tedious through having to wait four days before being able to complete the watch.

## FITTING INTO CASE

Trying to fit the watch into the case was where the problems really started. The PCB assembly was too thick for the space available and there were two reasons for this. The impression was that the flexible copper screen had not been part of the original design; the instructions for the fitting of this screen were separate from the main assembly instructions. The two thicknesses of screen obviously reduced the front-to-back clearance between PCB assembly and case. However, the main reason for the difficulty was that the soldered joints were protruding too far from the PCB. The importance of making very small solder joints had not been emphasised sufficiently in the instructions, which merely called for the use of a fine-tipped soldering iron, and "small wire cutters capable of cropping within $\frac{1}{2} \mathrm{~mm}$ of the PCB".

Sinclair have since stated that an improved IC is now being supplied which is free from any effects due to external static. The insulated copper screen is no longer necessary. Sinclair Radionics Ltd., St. Ives, Huntingdon, Cambs.

## PE17 4BR.

## TEEUSTIII



The Decca Bradford chassis was first released in 1970 and is still in production it is one of the best known hybride colour chassis and large numbérs have been sold and rented. This month we start a detailed survey of the chassis, the faults to be, expected, and fautt-finding procedures, dealing with both the 10 and 30 versions.

## SIMPLE CnEV-SCALE GENARGGOR

Three 74 -seres 3 TL i.c. $s_{+}$and two transistors are used to generafe an eight-step wedge suitable for injection frito the video or luminänce stages. The circuit can be modiffed to match either the BBC or the IBA coloy bar standards:

## THYRISTORUTNE OUTPUT STAGES

All line output stages work on the same basio principle but the thyistor circuit at frist glanee appears to bes something entirely different. Be. cause of the characteristics of thyristors, therels added complexity, though the elrcuit still performs the same basic operations. We shall examine the principles, the differences between thyristor and transistor circuits, and practical arrangements.

## SERVICING TELEVIBION RECEIVERS

Les Lawry-Johns describes his experiences with the Pye group's 173 chassis which superseded the 169 in 1973.

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## PRODUCTION LINES

## JONELLE CASSETTES

Stores in the John Lewis partnership have introduced their own brand-Jonelle-blank cassette tapes. They come supplied in the usual snap-pack cases, complete with an index card.
The eassettes are made in England using tape supplied by "a large West German manufacturer". The Jonelle C60 (30 minutes per side) costs 39 p and the C90 ( 45 minutes per side) costs 49p. The John Lewis Partnership (Dept. P.W.) Merchandise Information, Oxford Street, London W1A 1EX. (Telephone 01-637-3434).


AIWA BREAK ALL THE RULES
If you ask an expert in the HiFi field, what he thinks of music centres i.e. a complete system, less speakers, housed in a single cabinet, he would probably quickly eject you from his presence and swear never to speak to you again. His loathing for this particular form of ' HiFi ' was, in the past, justifiable, and could be backed up with test data from both manufacturer and independent reviewer. The fact that true HiFi could not be obtained at a reasonable cost from a system housed in a single cabinet has always been a stumbling block, but Aiwa, have shattered this longheld belief.

With their model, the AF-5080, they have brought together in a single cabinet an AM/FM stereo tuner, a Dolby cassette recorder, a 24W per channel amplifier and record turntable. The tuner section covers LW,


Aiwa's AF-5080 Music Centre

MW and SW on the AM band, while on the FM band, coverage is from 87.5 MHz to 108 MHz . Sensitivity ranges from $550 \mu \mathrm{~V} / \mathrm{m}$ (LW), through to $2.5 \mu \mathrm{~V} / \mathrm{m}$ on the FM band. The amplifier section has a rated output of 24W RMS per channel, with a THD factor at 1 kHz of $0.08 \%$. Power bandwidth is from 20 Hz to 20 kHz .

To satisfy the ever increasing demand for cassette recorders, Aiwa have had the good sense to incorporate a Dolby recorder into the system, which boasts a frequency response of 30 Hz to 17000 Hz (fe-Cr). The cassettes are front loaded, with all controls oil damped, to give precise and noiseless operation.

Moving on to the record playing section, the aluminium turntable is belt driven from a synchronous motor, giving $W \& F$ and $S / N$ figures of $0.1 \%$ and 45 dB 's respectively. The lightweight tubular S-shaped arm, is fitted with an anti-skate device and magnetic cartridge, Recommended tracking force is 2 gms .
Obviously there are many more parameters available than the ones discussed here, but taking into account the stylish cabinet, facilities available and price, a potential buyer would be hard pressed to better this combination, either in music centre form or as separates.

Price of the AF-5080 is $£ 288 \cdot 63$ inc. VAT, and it is distributed by Johnsons of Hendon, (Dept. P.W.) 14 Priestly Way, Eldonwall Trading Estate, London NW2 7TN.

## GOLDRING G. 900

In the item on the G.900 Cartridge in the April issue the total mass should have read 5 gm and the moving mass 0.32 gm . We thank Mr. Sharp of Goldring Limited for bringing these points to our notice.

## CAR INTRUSION ALARM KIT

The new Heathkit GD-1157 not only protects your vehicle from tampering and theft, but it protects your entire car-engine, boot and passenger compartment-from would-be thieves by sounding your car's horn.
The alarm unit itself can be mounted almost anywhere and is connected to pushbutton switches on the doors, bonnet and boot. The entire system can be armed or disabled by a convenient underdash switch. Two controls in the alarm unit set entry and exit delay times so you can enter or leave the car without accidentally triggering the alarm. However, with the system armed the alarm sounds instantly whenever the doors, bonnet or boot are opened. The alarm sounds for approximately two minutes, then resets and repeats the two-minute alarm cycle until the reset switch on the GD-1157 is flipped or the cause of the alarm has been removed.


Once the alarm sounds, the underdash arm/disable switch no longer functions and the only way to disable the system is to flip the set/reset switch on the concealed alarm unit.

There is just one simple printed circuit board to wire and the manual gives complete installation instructions. The kit includes 4 pushbutton switches, mounting hardware and cables. And, to simplify installation, your car's existing courtesy light switches can double as switches for the alarm.

Prices: Kit GD-1157 £18.80 (including $8 \%$ VAT and delivery within the UK). Full details available upon request from: Heath (Gloucester) Ltd', (Dept. R.W.) Bristol Road, Gloucester GL2 6EE or The London Heathkit Centre, 233 Tottenham Court Road, London W1P 9AE.


A major addition to their range of Audio Modules is announced by Bi-Pak Semiconductors, (Dept P.W.) 63 High Street, Ware, Herts.
The unit, designated AL250, is a power amplifier providing an output of up to 125 W RMS into a $4 \Omega$ load.
The module has a sensitivity of 450 mV and a frequency response extending from 25 Hz to 20 kHz whilst distortion levels are typically below $0.1 \%$. The use of $4,115 \mathrm{~W}$ transistors in the output stage makes the unit extremely rugged while damage resulting from incorrect or shortcircuit loads is prevented by a four transistor protection circuit.

The unit is intended for use in many applications such as disco units, sound re-inforcement systems, background music players etc.

Priced at only $£ 15 \cdot 95$ plus V.A.T, the module is supplied with complete instructions and is fully guarenteed.

## BARRIE ELECTRONICS

Barrie Electronics inform us that they market the Bi -Kit range of kits with BSR decks in addition to stocking a very large range of components, especially resistors. The firm also supplies Avo meters.
Where possible, Barrie pride themselves on their 'same day dispatch' service and say that they will be pleased to supply readers with their price lists upon receipt of a stamped, addressed envelope. Barrie E/ectronics (Dept. P.W.) Ltd., 3 The Minories, London EC3N $1 B S$.

## DRILL CHUCK

Paramo Tools have introduced a loose drill chuck, mounted on a spiral ratchet bit. This slides into any spiral ratchet screwdriver, either Paramo or their competitors, to replace the standard screwdriver bit.


Quickly fitted; the chuck will take twist bits up to 6 mm for the smaller two sizes of spiral ratchet, and up to 8 mm for the 131 AH . The speed of replacement of the drill chuck enables drilling and screwing operations to be speedily carried out. The high speed attainable with the spiral ratchet action, of course, makes drilling thin materials easy.

The drill chucks are priced at £ $3 \cdot 15$ plus V.A.T. for all sizes, and are available from your usual Paramo Tool stockist. F. Parramore \& Sons (Dept. P.W.) Ltd., Caledonian Works, Chapeltown, Sheffeld S30 4WZ.

LUX PD-131


Howland-West have pleasure in announcing the Lux PD-131 turntable. It comes without arm, but is fitted with bayonet type mount to take the SME arm. Features include: brushless DC servo-controlled motor (ensures excellent stability of rotational speed and offers high torque): Turntable platter-so designed as to give not only necessary inertia but possible heaviest weight in consideration of motor bearing and resonance/tension of each part of the turntable: Chassis, wooden frame and panel - aluminium die-cast chassis with sufficient strength and weight, 3 mm -thick anodised aluminium panel are firmly assembled together with rubber and the wooden frame has a bumper effect which keeps this turntable immune from vibration: Acrylite case-4mm-thick ( $0 \cdot 16 \mathrm{in}$ ) dust cover: Insulator Compliance and control required for prevention of vibration is obtained by combination of spring, rubber and silicon grease: Unique mirror system stroboscope which permits visual identification of $A C$ line frequency by colour in addition to indication of rotation speed by number of pulses blinking black light.

The price of the turntable, without arm, is $£ 195 \cdot 00$, plus VAT, and it will be available through Lux appointed dealers only. Howland West Ltd. (Dept. P.W.), 3-5 Eden Grove, London N7 8EQ.


Two amplifier kits and BSR deck supplied by Barrie Ltd.

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## ON RECENT DEVELOPMENTS

## IT FOOLS 'EM!

If you are one of those people who enjoys dropping the odd mouthful of technical novelty-try monolythic gyrator. Ageing engineers have known about them for years but the gyrators were costly to fabricate and so did not appear on the market in any great numbers.

A Dutch company has now manufactured what many believe to be the very first'monolythic gyrator. So what are they? Well, they are very small, and when you terminate them with a capacitor, they pretend to be an inductance-but without bulky coils. At present, one adds a single capacitor plus two resistors to form a frequency conscious circuit which can be extremely compact. Another rather startling fact about these gyrators is the size of coil they can fool other electronic circuits into thinking they are. For example a $1,000,000 \mathrm{H}$ (one million Henries) coil can be simulated-and to within $0.2 \%$ too. Just imagine a $1,000,000 \mathrm{H}$ coiland the gyrator chip measures only $3.4 \mathrm{~mm} \times 3.4 \mathrm{~mm}$. Used in resonant circuit applications, a Q of between 500 and 5,000 is achievable.

## A CALCULATING MOVE MATE!

The second idea (l predict) will take off very fast indeed once it becomes available. It's a pocket sized calculator in appearance-but it isn't, if you follow me. Closer examination reveals a miniature chess board engraved or screened on the face together with the necessary buttons to enter moves. The hand held unit employs a microprocessor and the unit was on show at a recent International toy fair. Not available yet but the price looks very reasonable. Just the thing you've always wanted; chess without getting board!

## ELECTRONIC NOSH

With Easter now firmly behind us for another year, it allows a full twelve months to prepare ourselves to receive an electronically cooked hot cross bun. Not really so farfetched and will be in our homes by
next Easter. Gone are theold switches and timers: In their place has come a cooker with digital readout, electronic cooking keyboard and a store of some 120 cooking programs in its own memory banks.

The housewife of the future needs only to mix ingredients as per the cooking book (supplied with the cooker), and then punch in the relevant code for perfect cooking. The grilling and baking programs* can be used with hundreds of different recipes and dishes. The cooker uses two Read-Only Memories (ROMs) and a Central Processing Unit (CPU).

Fancy that; if you want to dial-adoughnut then there's just one place to press!

## CREDITABLE

It is a peculiarity of the hologram that if one tiny part of its area is examined, the whole complete holographic image can be seen. To check authenticity of any one of these cards; it is only necessary to examine a tiny part of the card and the holographic image at that point will show the whole card-as it was originally. This image, together with a direct image of the card being viewed are shown side by side in a special viewer. Any alteration can thus be immediately detected. Clearly a method that will not forge ahead!

## 1k CQ's

Good news for Hams and anyone else interested in producing a number of different frequencles with crystal controlled accuracy. A CMOS LSI digital chip is now on the market which , will provide 1,021 output frequencies from one crystal-a truly digital v.f.o. It will operate from a 5 V line and will accept input frequencies of up to 5 MHz . Another bonus too, it isn't greedy on power; dissipation is only 5 mW . I note that in the United States, a sample by post costs $\$ 1976 \mathrm{c}$. It seems doubtful if the company would send one over to the UK against a remittance but the number to watch for when they become available here is HCTRO320.

Lids on the Amateur bands should note that this is not a heaven-sent device for calling $C Q$ on 1,021 frequencies at the same time!

Bad news for the forgery profession. Alteration of credit cards and the like will soon be quite impossible if a German company gets its system accepted. The original card is photographed using a laser to form a holographic image which is then bound with the original card and sealed in.

## SKINNY C's

How thin is thin? It really depends upon what one is talking about. I was impressed by the thinness of a series of capacitors called Thintrim. These are variable types with an adjustable range from 7 to 45 pF . They measure $0.2 \times 0.2 \times 0.05 \mathrm{in}$. The manufacturers inform that they make another type with a 25 pF maximum value-but of course, that's much smaller! Wonder how many puffs to the pound?

## READ-OUT

Playing games with electronic calculators has been in vogue for some time. The idea is that by turning the unit upside down, it is possible to "read" a message formed by the number displayed. it seems that certain companies are taking the whole thing a few steps further-and it isn't necessary to turn the calculator upside down.

One idea shortly to be introduced allows a calculator to be used as an active terminal for a computer. In this application, it forms a substitute for a teletype terminal. With this unit, it will be possible to talk to the computer and to receive information which will then be displayed on the calculator's readout.


ALEXANDER Graham Bell was born in Edinburgh on 3 March, 1847. His father and grandfather were teachers of elocution and he used a new system of phonetic symbols, invented by his father, to teach the deaf to speak. In 1870 the family emigrated to Canada and Bell established himself in Boston as a teacher of the deaf.

Bell's telephone arose from a chance observation made in 1875 when he was working on his "harmonic telegraph". This was an instrument designed to carry several telegraph messages over a single circuit by using currents of a different frequency for each message, and detecting each signal by a tuned reed and an electromagnet. With two such instruments connected together he noticed that when one reed was twanged the corresponding reed on the other instrument vibrated in sympathy. Bell had assumed that the current generated by a vibrating reed would be too feeble to be of use. The discovery that it could set another reed in motion estab-


Bell's "gallows" telephone.
Science Museum picture.
lished a train of thought that led to his "gallows frame" telephone (see picture). A pair of these, used as transmitter and receiver, produced sounds that were unmistakably vocal, though not intelligible.
On 7 March, 1876 Bell was granted a patent that covered the harmonic telegraph, telephones acting on the principle of the gallows-frame instrument, and also the production of a signal by varying a resistance and thereby controlling the current from a battery. He returned to his telephone experiments, now using a crude variable-resistance transmitter. On 10 March, 1876 his assistant heard the first intelligible sentence conveyed by a telephone, "Mr. Watson-Come here-I want to see you". Since then most telephones have used the variable-resistance principle in their transmitters, though Bell returned to the electromagnetic transmitter and used it to establish the telephone commercially in North America. In August 1877 he came back to Britain to promote the telephone. In January 1878 he demonstrated it to Queen Victoria and in June established The Telephone Company Limited.

Meanwhile Thomas Edison had produced a practical variableresistance transmitter employing compressed lamp-black, which gave a much greater output than Bell's electromagnetic instrument. Edison could not use Bell's receiver because of the patent, so had to invent his own. This was an electrochemical device, the "motograph", which gave loud but poor-quality reproduction and required the user to turn a handle continuously. However, it served its purpose of strengthening Edison's commercial position, and he founded a British company in August 1879 which merged with Bell's in 1880 to
form The United Telephone Company Limited.

By 1880 commercial rivalry was less important to the telephone than its legal status. For ten years public telegraphy in Britain had been a state monopoly run by the GPO. So long as Bell confined the telephone to private wires, relations with the GPO were reasonably cordial. But from the outset he realised that the future of the telephone lay in the operation of exchanges, enabling any subscriber to be connected with any other, and in 1879 both the Bell and Edison Companies opened exchanges in London. The GPO realised that this new development could undermine the revenue of the telegraph service, though it was not sufficiently convinced of the


Alexander Graham Bel/ (1847-1922).
telephone's usefulness to wish to be committed to exploiting it. It was nonetheless able to control the development of the telephone systern after obtaining a High Court judgment that the telephone was a telegraph and a telephone message was a telegram within the meaning of the Telegraph Acts. Commercial companies were licensed and though there were numerous companies in operation during the 1880's, the three largest merged in 1889 to form The National Telephone Company, which thereafter held a dominant position until its licence expired on 31 December, 1911; the GPO then took over full responsibility for the nation's telephone service.
We thank the Science Museum for information used in this article.

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## S.A.E FOR <br> DETAILS




## by Eric Dowdeswell G4AR

THE author of a feature such as this is usually left with mixed feelings after completing his stint for the month. Letters from newcomers to the amateur and broadcast bands or those seeking information on our hobby raise the spirits no end, while established correspondents who write in happily to tell me that they've just passed the Radio Amateurs Examination bring despair, as I realise I've lost a reader but elation to know that a new callsign has come into being.

I believe it is important to find out just how the newcomer has got around to the SW bands. Often it is the result of casually tuning over the SW bands on a domestic receiver and wanting to do it better on a decent receiver. Sometimes it's an offshoot of listening to aircraft, police and other Public Services on the VHF bands, something to be strongly deprecated. There is much more fun on the SW broadcast and amateur bands especially when it leads to getting one's own transmitting licence and talking back to other amateurs.

At one time, when amateur band telephony was strictly double sideband and unsuppressed carrier stuff, it could be picked up and resolved on almost any domestic receiver, even if it did not cover the amateur bands! Enquiries locally usually revealed the amateur concerned but the complainant often became interested to the extent of taking up the hobby himself! Or herself, since there were ladies enjoying the hobby from the early days. However with the development and use of single sideband telephony by amateurs this method of "contact" has virtually disappeared since SSB on a domestic set is just a horrible noise. Come to think of it, it's often a horrible noise on the bands themselves! The QRM remains but the source is harder to locate, often requiring the services of the Post Office, and sometimes leading to unpleasantness all round. I often think that the coming of SSB has led to the amateur becoming more isolated from the general public.

Excellent news of Tim Charles A8927 of Colchester who has passed his RAE and is taking his code exam in a couple of weeks. He was one of the few readers of this column who bothered to send in logs of stations heard on CW. Let's hope the experience will pay off first time for Tim. With a
bit of luck we may get his new callsign before we go to press. So another reader bites the dust! Inevitable, I suppose! The last bit of news from Tim concerned the positive reception of JAZONB on 160 m ! he was 449 on 1908 kHz so Tim can go out in a blaze of glory!

Ray Woodward in Colne now has an RQ80 ATU in front of his CR70A which, with 132ft of wire, albeit at only 10 ft up, has greatly improved reception. He's getting some gear together for the 2 m band and hopes to do well on the VHF's as he is some 700 ft above sea level up there in Lancashire. Paul Barker BRS34898 in Sunderland had a bad month what with the flu and bands in a poor state. SSTV on 20 m brought only G4BFB and I8JTU while on SSB CT4AJ proved to be a non-event being just another CTl in reality!

Steve Cottis of Harrogate worked his way through all the bands from 80 to 10 m . His best on 80 was JDIAKE while KC6AQ relieved the monotony on 20 m . Dennis Anderson writes from Brookwood in Surrey to say that he is now BRS36591 and has joined the Farnborough and District Radio Club and "they are very helpful" which is nice to know. Paul Flatman (Ipswich) could only get on for a few days last month but when he did he found 20 m pretty active but next to nothing on 15 m . A nice one on 80 m reported by Paul was K3HVG/P/HR6 on Swan Island. Paul is about to replace his old faithful HRO receiver but I hope he gets something that turns out to be at least as good. With a few mods the HRO can be turned into a pretty good receiver which will out-perform a lot of the modern sets especially in the areas of cross-modulation and inherent noise.

Stephen Budd A8713 in Worthing found 80 m "unbelievably fantastic" in the early mornings but was not enthusiastic about the rest of the HF bands. He has shelved plans for a 6 -element beam and rotator for 2 m after seeing the "ridiculous prices". Espec" ially, as he says, it would only be for one band. Paul Flatman, Ipswich, is pretty busy with other commitments, his only free time coinciding with the gap between 20 m going dead and 80 m coming alive!

Paul Cowburn writes from Leyland, Lancs for the first time and is full of praise for the help he is getting from local G3RFN on the many problems that beset a newcomer to the SW bands. Certainly everyone new to our hobby ought to try and contact his local amateur or radio society rather than try to steer a lonely path, often in the wrong direction. Paul has a Marconi CR300/2 but finds that its performance tends to drop off at the higher frequencies. When this happens it is not a bad idea to build a crystal controlled converter for say 20,15 and 10 m and use the main receiver as a tuneable IF around 3 to 4 MHz .


## Log extracts

T. Charles:- 160m JA30NB 40 m FM\%AV H13HOT 20m VP2MJ ZP5AO 2 m DM2BEN/P SM7CHX SP1II UR2RDR (auroral opening) via Oscar 7 VE3SAT W2BLV W90II WOEAZ 70 cm PA0GDM PA0MHK
R. Woodward:- 80 m CO2JA HK4DF YV4ATI 8P6FV 20m DU9FB HK6CMA VP2MEV 6W8NW
P. Barker:- 20 m CT2BB VQ9R VU2HI SSTV G4BFB I8JTU
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P. Flatman:- 80m K3HVG/P/HR6 KG4FU 20m DU9FB HR3JJR VK9XI VP8HZ 6W8MW 8P6FU
All SSB except those in bold which are CW.
S. Budd:- 80m A4XFX EP2SN FP8DX HR2FP KG4GG KZ5JM PJ0USA VP1DW VP2ABC VP2DM VP2KJ YN7R 5T5ZR 8P6GN 40m VK7GK ZL2AQ 20m A6XP C5AF KG6JBX TA1MB 5N2ESH 9X5SP 15m ZD7FT 2 m via Oscor 7 DC2ST F6APU PA0JHM
P. Cowburn:- 80m CO2JA JA6BSM ZB2DK 40 m VK2AVA VK5PB VK7DK YA2WJ YV6CD AD3EST (Washington, special event station, 200 years American Independence).


## SHORT WAVE BROADCASTS

 by Derek BellMANY a time and oft the controversy has been bandied about as to the stability of various SW sets. Those who run what are known as communications receivers maintain that their type of set is far and away the best and indeed the only type of set to use for DX. This point is made, often with some force and the right hand firmly round the opponents throat, in order to ensure that he sees the error of his ways! R. Burgess has it seems the best of both worlds in that he has recently purchased a Grundig Satellit 2000 and, though very very expensive, this set has a fair degree of portability and is fine for putting in the car. From his Haywards Heath QTH R.B. has, with the internal aerial pulled in the following:

Radio Aparecida on 9635 at 0000
Radio Nacional Colombia on 4955 at 2300
Radio Abidjan on 11920 at 1940
FEBA Seychelles on 11715 at 1700
Radio Togo on 5047 at 2300
Radio Grenada on 15105 at 2030
This set seems to have the advantage of pulling
in the Latin Americans an hour earlier than they are heard with a cheaper set, and as R.B. says "L.A.'s are at their best in the wee small hours". The latter item on the log, Radio Grenada, was however heard in Huntingdon, Cambs. by Richard King on a Russian Vega Selena, logged at 2000 and who rates the signal at nothing less than fours on the SINPO scale. Alongside this item Richard passes on the info that HCJB Quito is to build a 500 kW transmitter in Indiana USA and quite pricey it sounds. One of the valves for example will cost 17000 dollars!

Another item of station news is that Indonesia is to phase out its short wave broadcasts by 1979. At present these can be heard on a wide range of freqs. from 2300 up to 17792. The transmitters are all of modest power since they are intended to serve only the home listeners but then so are the Latin Americans and these are heard here in the UK every night. I presume that the Indonesian Radio Jakarta with its overseas service will still be active and this can be heard in English on 11790 and 6045 at 2300, 0900 and 1100 with an introduction played on a Hammond organ.

To continue the theme of cheap transistor sets versus the more expensive rig, John Baker of Birkenhead joins in to ask this question and then on his Philips 90L goes on to log:

## Radio Nacional de Brasilia on 11780 at 2100 Radio Australia on 9570 at 0817 <br> RSA on 5980 at 2133

"Do the more expensive communications sets offer better value for money than the portables?" asks John, well let's explore this question a little more. To do so we must call in our overseas reader this month Martin Kennedy from Christchurch, New Zealand. Martin runs a Codar CR70A hanging on the end of a 100 ft long-wire. Pride of the $\log$ is the AFN "National Public Radio" from Greenville USA, this signal arrives either over the Pacific or across the pole according to which way Greenville's aerials are switched. Also featured is Radio Free China from Taiwan on 11825 at 0210 , so it would seem that communications sets earn their keep wherever they are.
"What", you say "about the home built sets then" David Wyatt of Oswestry has built one, a seven transistor superhet with a 20 ft wire. David logs on it

Radio Pakistan on 17910 at 1100
Voice of Turkey on 11808 at 0017
David gives the address of Voice of Turkey for QSL fans as TRT Voice of Turkey, Ankara, Turkey. He requests the address of Radio Canada, which I can supply, and that is P.O. Box 6000, Montreal, Canada, H3C 3A8.

So, what have we learned up to now?, well that both types of set fill a need but that need must depend not only on the pocket but the situation of the user.
Recently an enquiry was featured in this column for information on a certain type of Royal Navy set. An ex-member of the "Andrew" E. J. Scudder adds more to the gen already received. This gentleman had the job of maintaining these sets during the war and informs us that they were made by Eddystone. The main problem was the coil pins it seems as operators would pull the coils forward instead of up thus bending the pins and eventually breaking them off, causing much grief and no small amount

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of Navy language to Mr. Scudder. Thus it seems the more complicated the set, the more it will cost to repair. This repair could result in having to send overseas for spares, increasing the cost and time spent without the use of the set. On the other hand cheap sets are often improved by the addition of aerial tuners and pre-selectors. John Higginhotham of Holyhead has written to say that the Radio Nedérland ATU specification sheet is once more being sent out. Readers will remember that news reached this column recently of RNI being lax in their reply to an enquiry for the plans for this handy bolt-on extra. John viewed in amazement his postbag from stations which totalled five cards and 17 calendars after the Christmas rush was over. I have recently had a card from Radio Sofia wishing me a happy Spring!

The main conclusion is that the cheap transistor radio is fine for a second or bedside set and for the person of limited budget, and that means most of us these days. While the communications set is for those who have the money to spare and the space to fit the set into. The AR88, for instance, needs a stout table just to take the weight! It is of course pointless to expect the cheaper transistor set to pull in the signals that the Grundig Satellit will or some of the American products, or even the Codar, but the use of a cheaper set may fire you to go on to bigger and better things and even aspire to the RAE.

So until next month I will simply say 73 s to you and yours.


READER "Steve" who lives in Truro, Cornwall reports hearing CFGO in Ottawa on about 1440 kHz at 0305 GMT after Radio Luxemburg had closed down for the night. CFGO does operate on 1440 kHz and is heard quite often in the UK. Steve uses a Philips IC326 receiver coupled to the co-ax downlead of his VHF TV aerial. The receiver is placed on top of the co-ax, the screen of which is earthed and this gives a very good boost to reception. Steve mentions hearing Radio Sweden on approx. 1151 kHz as well as on 1178 kHz which is the listed frequency. This effect is almost certainly due to a spurious signal generated within the receiver as a result of overloading by the pick-up from the co-ax downlead aerial. Portable receivers are normally designed to work with the comparatively low signal input from a ferrite rod aerial. Care should be taken when an external aerial is used that the coupling is not too close otherwise the increased
signal strength obtained will be accompanied by whistles and spurious signals.
Quite often the medium wave tuning scale on a receiver is not accurate enough to show the frequency to the nearest 5 kHz or so. The DXer is then uncertain which one of two of even three channels he is listening to and problems with station identification can arise. A logging scale, if the receiver has one, can be used to improve matters. This scale is marked from 0 to 100 or perhaps, 0 to 1000 and is used with a sheet of graph paper to plot a curve that will enable logging scale divisions to be converted to frequency. Known local broadcasting stations can be used to mark a number of points on the graph, these points being joined with a continuous line to form a curve which is used to convert frequency to logging scale reading and vice versa.

An alternative is to use a crystal calibrator. The writer's has switched outputs of $10 \mathrm{kHz}, 50 \mathrm{kHz}$ and 100 kHz which are found to be adequate for MW DXing. The calibrator is connected to the receiver in parallel with the aerial and it acts as a miniature transmitter to give marker points at intervals across the band. The method used by the writer is to draw up a table giving a logging scale reading for each 10 kHz point on the medium waves which is very useful when DXing North Americans where the stations are on channels which are multiples of 10 kHz . A more usual method is to switch-in the calibrator in place of the aerial and use the 100 kHz markers to identify sections of the band and the 10 kHz markers to tune to an exact channel. "Odd" frequencies between the 10 kHz points can be estimated. Domestic type receivers in the UK are usually marked in metres on the tuning scale. To convert, divide 300,000 by the wavelength in metres, to get the frequency in kHz .

Roy Patrick reports from Mackworth, Derby with news of his recent broadcasts from Radio Derby on "Late Night Derby". He has been telling listeners about DXing and says it was nice to be on the other end for a change. Roy's medium wave catches made on a Trio 9R59D receiver include CJCH in Halifax, Nova Scotia on 920 kHz ; CJON St. John's on 930 kHz ; WINS in New York City on 1010 kHz ; WHN also in NYC on 1050 kHz ; CBA Moncton, New Brunswick on 1070 kHz and Urumchi in China on 1525 kHz at 2300GMT with a programme in Russian. Good luck with your broadcasting Roy!
When two adjacent broadcasting stations are identified by wavelength rather than by frequency it will be difficult to decide from this information whether they will interfere with each other. Only the frequency separation in kHz is of value since the bandwidth of a receiver and hence its selectivity, the ability to separate adjacent signals, is measured in kHz . On the medium and long waves in Europe the majority of channels have a separation of 9 kHz . At the HF end of the MWs, channel 107 ( 1484 kHz ) corresponds to $202 \cdot 2$ metres while channel 106 ( 1475 kHz ) corresponds to $203 \cdot 4 \mathrm{~m}$, the difference in wavelength being $1 \cdot 2 \mathrm{~m}$. At the LF end of the band channel $5(566 \mathrm{kHz})$ is 530 , while channel $4(557 \mathrm{kHz})$ is 539 m the difference in this case being 9 m . On the long waves 209 kHz corresponds to 1435 m and 200 kHz to 1500 m the difference being 65 m . From an interference point of view the "distance" between the two stations in each case is the same, namely 9 kHz but the wavelength separation varies between $1 \cdot 2 \mathrm{~m}$ and 35 m .


The advantages of using kHz instead of metres are so obvious that the practice is now in use by DXers and broadcasting authorities in most parts of the world. In the UK, FM stations on VHF are quoted by their frequency in megahertz though the use of metres on the medium and long waves lingers on. In North America, where the separation is 10 kHz the medium waves, or "Broadcast Band" extends from 540 kHz to 1600 kHz . Receiver manufacturers often drop the last zero, and mark the scales 54 to 160 , a practice that can be seen on many imported domestic receivers on sale in the UK.

An interesting letter from Ian Rennison in Horsham, Sussex tells of a holiday spent in Richmond, Virginia, USA where he heard US radio first hand. He mentions picking-up WKBW Buffalo NY on 1520 kHz on a car radio and commenting that he had clearer reception of the same station back home! WKBW is often a strong signal here in the UK just before sunrise at this time of year. Ian has been trying to pick up WRVA Richmond on 1140 kHz and asks if it has been logged in this country. WRVA has been heard but not often because of the
directional aerial system in use at the transmitter. WRVA and CBI in Nova Scotia both transmit on 1140 kHz and to reduce mutual interference each station has a directional aerial which has a null towards the other. The null from WRVA is towards the North East which is also the bearing of the DXer in the UK and as a result, CBI comes in well in the UK while WRVA is something of a rarity. Ian's excellent $\log$ of DX heard at Horsham on a Trio 9R59D receiver, medium wave loop and PW differential loop amplifier includes 19 Canadians (CKVO is the unidentified one on 710 kHz ); 20 from the US the more outstanding being WSB Atlanta, Georgia on 750 kHz ; WHO Des Moines on 1040 kHz and KMOX St. Louis on 1120 kHz , along with a number from the Caribbean area such as CMKV Radio Rebelde in Cuba on 600 kHz , Radio Demerara, Guyana on 760 kHz and Radio Belize on 834 kHz .

[^2]

THE ELECTRONIC MUSICAL INSTRUMENT MANUAL

## By Alan Douglas

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11
12
22
28
12
13
14
13
14
16
30
40
30
28
28
18
18
18
18
18
52
15
95
75
40
40
85
55
50
45
45 BD1
BD1
BD14
BDY
BDY
BF11
BF17
BF17
BF17
BF180
BF181
BF184
BF185
BF194
BF195
BF19
BF19
BF22
BF24
BF25
BF25
BF25
BF59
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LM300H
LM301

| 170p | SN72702 | 809 |
| :---: | :---: | :---: |
| 38p | SN76033 | 150p |
| 90p | SN76115 | 200p |
| 160 p | TAA550B | 36p |
| 65 | TAA621A | 203p |
| 148p | TAA661A | 180p |
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| 99p | REGULA | RS ${ }^{4}$ |
| 325p | 723 C DIL／TO | 5 45p |
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(Continued from other side)

| CHOKE | FOOT |
| :--- | :--- |
| Miniature | SWITCH* |
| +Podal |  |
| 100 mH 80 p | E2 80 |

KNOBS* fits ${ }^{\frac{1}{4}}{ }^{\prime \prime}$ shaft with grub screw, excep sliders).
 K2 Slim sllvered aluminium K4 Black serrated. Metal top with line indicator 33 mm diam. K4A As above but 25 mm diam K5 Black fluted metal top and skirt calibrated 0 $0-10.37 \mathrm{~mm}$ diam. K6 PK2 as K5, pointer on skirt K7 Black, knurled, tapered. Metal K8 Elack or silvered for slider pot

## PANEL METERS* Full scal

$59 \times 46 \times 35 \mathrm{~mm}$ req. $1 \frac{11^{\prime \prime}}{}$ hole

| $0-50 \mu \mathrm{~A}$ | $0-100 \mathrm{~mA}$ |
| :--- | :--- |
| $0-100 \mu \mathrm{~A}$ | $0-500 \mathrm{~mA}$ |
| $0-500 \mu \mathrm{~A}$ | $0-1 \mathrm{AmP}$ |
| $0-1 \mathrm{~mA}$ | $0-50 \mathrm{VDC}$ |
| $0-5 \mathrm{~mA}$ | $0-300 \mathrm{~V} D \mathrm{DC}$ |
| $0-10 \mathrm{~mA}$ | ${ }^{11} \mathrm{~S}^{11}$ |
| $0-50 \mathrm{~mA}$ | ${ }^{14} \mathrm{VU}^{\prime}$ |

"Vu"
-8. 82.85 each $08 \times 82.5 \times 38 \mathrm{~mm}$ rea. 60 mm panel hole

TRANSFORMERS (Mains Prim. 220-240V) $6-0-6 \mathrm{~V} \quad 100 \mathrm{~mA} \quad 90 \mathrm{p} \quad 9-0-9 \mathrm{~V} 2 A^{*} 220 \mathrm{p}+$ -0-9V $100 \mathrm{~mA} \quad$ g0p $30-24-20-15-12-0$ $12-0-12 \mathrm{~V} \quad 100 \mathrm{~mA} \quad 90 \mathrm{p} \quad 2 \mathrm{~A}^{*}$ multi tappings* $15-0-15 \mathrm{~V} 100 \mathrm{~mA} 195 \mathrm{p}$ Prim. 120/240V.45+ $0-120-12 \mathrm{~V} 150 \mathrm{~mA} 160 \mathrm{p}$ Prim. 12024 \& 12 V $0-60-6 \mathrm{~V} \quad 280 \mathrm{~mA}$
$0-120-12 \mathrm{~V} 500 \mathrm{~mA}$

237p+ A $237 \mathrm{p}+$ ITT' Pulse Transfor-$24-0-24 \mathrm{~V} 500 \mathrm{~mA} 160 \mathrm{p}+\quad$ mer Miniature $1: 1$ $9-0-9 \mathrm{~V}$ 1A* 198p+ 12-0-12V 1A* $185 \mathrm{p}+\quad$ LT44 Mini. Driver. $\begin{array}{lll}15-0-15 V & 1 A^{*} & 198 p+ \\ 18-0-18 V & \text { A. } & 230 \mathrm{p}+\mathrm{t} .20 \mathrm{~K}, \text { Sec. } 1 \mathrm{~K} \\ 54 \mathrm{p}\end{array}$ $18-0-18 V 1 A^{*} \quad 230 p+$ LT700 Min. O/P Pri, $\begin{array}{ll}\text { Multi tappings } & \text { 285p } \\ 6 \rightarrow-6 \mathrm{~V} 1 \cdot 5 A^{*} & 180 \mathrm{p}+\end{array}$
 Please add 48p p\&p charge to all prices marked + , above our normal postal charge.)

| Connectors* Snap on PP3 6p Snap on PPy 9p |  |  | JACK PLUES |  | SOCKETS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Screened | Plastic body $1 p$$1 p$$10 p$$10 p$ | Open | Moulded |
| $\begin{aligned} & 2 \cdot 5 \% m \\ & 3 \cdot 5 \mathrm{~mm} \\ & \text { Std. MONO } \\ & \text { Std. STEREO } \end{aligned}$ |  |  |  |  | metal |  |
|  |  |  | 14 p |  | Tp | contacts |
|  |  |  | 14p |  | 13 p | 17p |
|  |  |  | 327 |  | 13 p | 22p |
|  | $\begin{array}{r} 9 p \\ 10 p \end{array}$ | DIN <br> 2 pin Loudspeaker <br> $3,4,5\left(180^{\circ} \& 240^{\circ}\right)$ |  |  | Plugs | Sockets |
|  |  |  |  |  | 12p | 8 p |
| am | $20 p$ | CO-AXIAL (TV) |  |  | $10 p$ | 8p |
| d skirt |  | PHONO |  |  |  | (Sing |
| skirt | 22p | assorted colours |  |  | 7p | (Double) |
|  | 22p | Meta | l screened |  | 12p | (Triple) |
| 0mm | 22p |  |  |  | 6 p | 7p |
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## INDEX TO ADVERTISERS



| Electro-Tech Components | ... |  | 177 |
| :---: | :---: | :---: | :---: |
| Electro-Time ... | ... |  | 183 |
| Electrovalue Ltd. ... | $\ldots$ |  | 4 |
| Elliott Blunt Audio |  |  | 102 |
| Elvins Electronic Musical Instruments ... 109 |  |  |  |
| Flairline Supplies | ... |  | 192 |
| Fraser-Manning Ltd. |  |  | 188 |
| G.T. Technical Information Service ... 187 |  |  |  |
| Garfields | ... |  | 188 |
| Greenbank Electronics | $\ldots$ |  | 184 |
| Greenweld Electronics |  |  | 108 |
| Greenway Electronics | $\ldots$ |  | 182 |
| H.A.C. Short-Wave Supplies ... ... 180 |  |  |  |
| H.M. Electronics ... ... | $\ldots$ |  | 189 |
| Harversons Surplus | ... |  | 103 |
| Heathkit | ... | 112, | 135 |
| Helme Audio | .. |  | 188 |
| Henry's (Radio) Ltd. | $\ldots$ |  | 110 |
| Holme Electronics | ... |  | 186 |
| I.L.P. Electronics Led. ... ... ${ }^{\text {a }}$ (13 |  |  |  |
| Intertext I.C.S. ... |  |  |  |
| Kensington Supplies ... ... ... 186 |  |  |  |
| Kinnie Components | ... | $\ldots$ | 116 |
| K.K.S. Trading | ... | $\ldots$ | 164 |
| Kramer | ... |  | 180 |
| Lasky's Radio ... ... ... 98, 102 |  |  |  |
| Lewis Radio | $\ldots$ | $\ldots$ | 118 |
| Linear Products |  |  | 162 |
| London Electronic College | $\cdots$ |  | 187 |
| Lynx Electronics ... | ... |  | 162 |
| Mack's Electronics ... ... ... 179 |  |  |  |
| Magnum Publications |  |  | 187 |
| Manor Supplies |  |  | 176 |
| Maplin Electronic Supplies |  |  |  |
| Marco Trading |  |  | 186 |
| Marshall, A. \& Sons |  |  | 181 |
| Milward, G. F. |  |  | 159 |
| Minikits Electronics |  |  | 189 |
| Multicore Solders (Bib Hi-Fi) |  | ... | 164 |


| Newmart Electronics | ... | $\cdots$ | 109 |
| :---: | :---: | :---: | :---: |
| Orchard Electronics | $\cdots$ | $\cdots$ | 164 |
| Partridge Electronics Ltd. | ... | $\cdots$ | 182 |
| P.B. Electronics | ... | ... | 177 |
| Polytechnic of North London | ... | ... | 188 |
| Pulse Electronics | ... | ... | 104 |
| Precision Petite | $\ldots$ | $\ldots$ | 168 |
| Radio Component Specialists | ... |  | 175 |
| Radio Book Service ... | ... |  | 187 |
| Radio Exchange Ltd. | ... |  | i 13 |
| Ramar Construction Services | ... |  | 188 |
| Radio Society of G.B. ... | $\ldots$ |  | 136 |
| R.S.C. (Hi-fi) $\quad$ O. |  |  | , 99 |
| R.S.T. Valve Mail Order Co. |  |  | 115 |
| Radio \& T.V. Components Ltd. |  |  | 101 |
| Riversdale... | ... | ... | 102 |
| Salop Electronics | ... | $\cdots$ | 188 |
| Saxon Entertainments Ltd. | ... | ... | 167 |
| Scientific Wire Company, The | ... | ... | 189 |
| Simtech Engineering Ltd. | ... | ... | 186 |
|  | $\cdots$ | $\ldots$ | 108 |
| Southern Valve Co. | $\ldots$ | $\ldots$ | 178 |
| Surplectronics ... | $\cdots$ | ... | 168 |
| Swanley Electronics | ... | ... | 172 |
| Tape Talk | $\ldots$ |  | 187 |
| Technomatic Ltd. | $\ldots$ |  | 189 |
| Teleradio Electronics | ... | 188, | 189 |
| Time-Micro Electronics | ... |  | 119 |
| Trampus Electronics | ... |  | er 1 |
| Vero Electronics | - | $\ldots$ | 172 |
| Viking Brews ... | ... | ... | 109 |
| Watiord Electronics | ... |  | 191 |
| West London Direct Supplies | ... | ... | 192 |
| Wilmslow Audio ... | $\ldots$ | ... | 105 |
| Wrights, S. G. ... | $\ldots$ | $\ldots$ | 114 |
| Xeroza Radio ..i ... | $\cdots$ | $\cdots$ | 119 |
| Z. \& I. Aero Services ... | $\cdots$ | ... | 192 |

Newmart Electronics
109

Partridge Electronics Ltd.
B. Electronics ...

Pulse Electronics London ... ... 104
Precision Petite ... ... ... ... 168
Radio Component Specialists ... ... 175
Radio Book Service ... ... ... 187
Ramar Construction Services ... ... 188
Radio Society of G.B. ... ... ... 136

R.S.T. \&alve Mail Order Co. ... $\quad$ IOO, 101
salop
Saxon Entertainments Ltd. ... ... 167
Scientific Wire Company, The ... ... 189
$\begin{array}{lllll}\text { Simtech Engineering Ltd. ... } & 186 \\ \text { Sintel }\end{array}$

| Sintel |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Southern Valve Co | $\ldots$ | $\ldots$ | $\ldots$ | 178 |


| Surplectronics | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 168 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Swanley Electronics | $\ldots$ |  |  |  |  |

Tape Talk ... ... ... ... ... 187
$\begin{array}{llll}\text { Technomatic Ltd. ... } & . . & . . & 189 \\ \text { Teleradio Electronics } & \ldots & \ldots & 188,189\end{array}$
Time-Micro Electronics ... ... ... 119

Vero Electronics ... ... ... ... 172
Viking Brews
Watford Electronies ... ... 190, 191
West London Direct Supplies ... ... 192

| Wilmslow Audio ... .... ... 105 |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Wrights, S. $G$. | .. |  |

Xeroza Radio ..: ... ... ... l19
Z. \& 1. Aero Services

192

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