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NEWS \& COMMENT
24, 25 NEWS ... NEWS ..... NEWS34 BOOKS RECEIVED38 LETTERS-readers voice their views
46,57 HOTLINES on recent developments-Ginsberg47 NEXT MONTH IN PRACTICAL WIRELESS
58, 59 PRODUCTION LINES-news on products of interest-Colin Riches
60 CQ ! CQ! CQ! CQ! CQ!65 P.W. READERS' PCB SERVICE
70 TELEVISION-contents of our 'sister' magazine73 ON THE AIR-A mateur Bands-Eric Dowdeswell, G4ARBroadcast Bands SW-Derek BellBroadcast Bands MW-Charles Molloy
78 KINDLY NOTE-notes on published articles

- CONSTRUCTIONAL
26 3-BAND R.F. MINI AMPLIFIER-F. G. Rayer29 TAKE 20, No. 74 (Snap Machine)-David Andrews32 A.F. SIGNAL SOURCE-W. Mooney48 RHYTHM GENERATOR-A. S. Webb B.Sc.66 SIMPLE LOGIC INDICATOR-Peter Hemingway
OTHER FEATURES
30 TECHNICROSS-Puzzle No. 1331 SPECIAL PRODUCT REPORT-Bi-Pre-Pak 'Super Spark'Capacity Discharge Ignition Kit
37 GOING BACK-Colin Riches41 GENERAL SERVICING, Part 3, Valve Radios-Les Lawry-Johns62 ECONOMY CONVERSIONS-B. B. Rafter
69 IC OF THE MONTH—Motorola MC1312P QuadraphonicDecoder
EXTRA THIS MONTH!
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# HY 5 

Preamplifier

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## SUBSCRIPTIONS - PRACTICAL WIRELESS AND TELEVISION MAGRZINES

WE are still receiving numerous letters requesting subscriptions to Practical Wireless and Television magazines. For those readers who are not aware, we regret that our magazines can no longer be supplied on direct subscription by IPC Limited due to escalating costs.

This action is very much regretted, but it should not mean that any reader is deprived of his/her regular copies of Practical Wireless or Television. Readers should order direct from their local newsagents. Any readers outside the UK who have difficulty in locating a supplier should write to the Editor and he will advise them of their local agent.

## Grimsby R.R.S.

THE Grimsby Amateur Radio Society has moved to a new QTH. The address is now the New Alexandra Social Club, Alexandra Road, Cleethorpes.

The meetings are held fortnightly on Thursday evenings at 8 p.m. Old and new members are always made welcome as is anybody with an interest in short wave listening, amateur radio, electronics etc.

If anyone would like further details, please contact George Smith, G4EBK, Hon. Sec., b' Fenby Close, Grimsby, South Humberside, DN37 9QJ.

## RNARS events

THE following is the 1976 calendar of events of the Royal Naval Amateur Radio Society, the headquarters of which, G3BZU, are located at HMS Mercury, Leydene, Hampshire. If you would like any further information, contact Mike Matthews, G3JFF at the above address.
16-24th April
HMS Belfast activity period. GB3RN all bands. 24 hour day operation. Further details G3HZL QTHR.
20th June
HMS Mercury Mobile Rally.

## 28-30th August

Portsmouth Dockyard-Navy Days. GB3RN and displays in conjunction with HMS Mercury Communications Exhibit.

## 16-17th October

JOTA scout camp and Amateur radio teach-in at HMS Mercury/ G3BZU.

## Fuse Standards

T$\rightarrow$ HE British Standards Institution has published a revision of BS 88 now entitled Cartridge fuses for voltages up to and including $1,000 \mathrm{~V}$ a.c. and $1,500 \mathrm{~V}$ d.c. There are two parts: Part 1 General requirements, and Part 2 Supplementary requirements for fuses of standardised dimensions and performance for industrial purposes.

Part 1 specifies general requirements, including characteristics, construction, performance, and proving tests for all types of cartridge fuses. Subsequent parts will give supplementary requirements in different applications. Part 2 is for industrial purposes, and specifies fuses most commonly used in the United Kingdom. These two parts of BS 88 substantially agree with IEC publication 269. The earlier edition of the standard has been withdrawn.

BS 88 Part 1 price $£ 5 \cdot 50$ and Part $2 £ 3.50$ may be obtained from BSI Sales Department, 101 Pentonville Road, London N1 9ND.

## BBC Radio Leicester

BBC Radio Leicester's medium-wave service is transmitting from a new, improved aerial at Freemen's Common.

The medium-wave service, on 188 metres ( 1594 kHz ), can be received at distances of twenty miles or so from the transmitter in daytime, but after dark the coverage is restricted by interference from other transmitters. The vhf programme is transmitted on $95-1 \mathrm{MHz}$.

## N. Radio Societies Association

THE Annual Convention and Exhibition of the N.R.S.A., which is sponsored by radio societies in the North of England, will take place at Belle Vue, Manchester on Sunday 25th April 1976.

The doors will open at llam and there will be a large number of trade exhibitors, as well as club display stands. A trophy will be awarded for the best club stand and there will also be a variety of demonstrations connected with different aspects of amateur radio.

Other attractions will include a Grand Raffle, an Inter-Club Quiz and a Construction Contest.

Comprehensive talk-in facilities will be provided on 2 metres $145 \cdot 5 \mathrm{MHz}$ (FM), 145 MHz (AM), and on $144 \cdot 290 \mathrm{MHz}$ (SSB); also on 4 metres $70 \cdot 26 \mathrm{MHz}$ (AM \& FM). There will be a GB3NRS HF bands station operating from the exhibition.

For long distance travellers it is hoped to offer talk-in through the local repeaters GB3MP (ChR6) and GB3RF (ChR7). Both these repeaters are scheduled to be on the air before the event, and there is considerable interest in mobile operation throughout the North West.

The N.R.S.A. is a non-profit making body which relies on the income from this convention and the small subscription from member societies in order to organize the following year's event. Further information can be obtained from the Publicity Officer:-Mr. Gordon Adams, 2 Ash Grove, Knutsford, Cheshire, WA16 8BB. Telephone:-Knutsford 4040.

## BBC Radio MedwayHoo

BBC Radio Medway's mediumwave service on 290 metres $(1034 \mathrm{kHz})$ is now transmitted from a new aerial at Hoo and the old station at Gillingham has closed down.

The vhf service from Wrotham, on 86.7 MHz , is unaffected by this change.

## RTTY news

THE British Amateur Radio Teleprinter Group announced the start on 7th March, 1976, of its RTTY News Bulletin service for radio amateurs.
Initially, the transmissions are made every Sunday according to the schedule below; later it is expected that more transmitting stations will be added to those listed.
The material transmitted will include test tapes for machines and systems plus news of specific RTTY interest.
The licence for GB2ATG is a broadcast, not a communications licence so transmitting stations will not be able to reply to any calls using this callsign.

| Time | Frequency | Signal Characteristics | Transmitting Stations |
| :---: | :---: | :---: | :---: |
| 1. 1200 hrs | 3590 kHz | $45 \cdot 45$ bauds FSK 170 Hz shift | $\begin{aligned} & \text { G3IIR, } \\ & \text { G3OZ'F, GW3IGG } \end{aligned}$ |
| 2. 1230 hrs | $144 \cdot 60 \mathrm{MHz}$ | (i) 45.45 bauds FSK, 850 Hz shift <br> (ii) $45 \cdot 45$ bauds AFSK, 170 Hz shift, $2125 / 2295 \mathrm{~Hz}$ tones | $\begin{aligned} & \text { G3IIR, G30UF, } \\ & \text { G3OZF } \end{aligned}$ |

## Summer School

THE Department of Electrical Engineering Science at Essex University will be holding its annual Electronics Summer School for teachers during the week July 12-16 this year. Three courses will be run simultaneously. The "Linear Circuit Design" course is concerned with the use of transistors and operational amplifiers in analogue applications and the basic circuits of a hi-fi amplifier are investigated in detail. The "Digital Circuit Design" course concentrates on the use of the transistor as a switch and develops design using integrated logic circuits; a digital patchboard is used to introduce the concepts of combinational and sequential logic design.
"Small Computer Systems" is a new course which should be of interest to mathematics teachers as well as those interested in electronics; the aims of the course are to introduce a typical small computer, the PDP-8, to investigate how it is used and to discuss its function in schools.

Further information on the Summer School can be obtained from R. J. Mack, Department of Electrical Engineering Science, University of Essex, Wivenhoe Park, Colchester CO4 3SQ, telephone Colchester (0206) 44144, extension 2408 or 2299.

## Amateur Computer Club

IF you would like to find out more about the Amateur Computer Club, send a stamped, addressed envelope to J. T. C. Aslen, Club Secretary, 7 Doordells, Basildon, Essex. Telephone: Basildon 411125 or 0484-56712.

They have recently published a design for a low-cost computer and they think they will have working models by the middle of this year.

## Longleaf Rally

THE 19th Longleat Mobile Rally will take place at Longleat House, Longleat Park, near Warminster, Wiltshire, on Sunday June 27, 1976.

As in previous years, the trade stands will be housed in large marquees. The rally is to start at 10 a.m. and talk-in stations will be operational on $160 \mathrm{~m}(1920 \mathrm{kHz})$, $80 \mathrm{~m}(3775 \mathrm{kHz})$ and 2 m ( $145 \cdot 50-$ $\mathrm{kHz}+\mathrm{VFO}$ ). Callsigns will be announced nearer the date. There will be a walking DF hunt at 3 p.m. on Top Band and there will be a Grand Raffle. Overnight camping will be allowed from 6 p.m. on Saturday 26th. Further gen from Brian Crocker, G3ULJ, Organiser, 36 Portland Street, Staple Hill, Bristol, BS16 4PT.

## Hol news from Heathkit



HEATHKIT announce their "Modulus" system of audio units. The range comprises a digital AM/FM tuner/2-4 channel preamp/control centre; a stereo receiver of "medium" or "high" power; and a 4-channel receiver "medium" or "high" power. You build in to your system what you want. Optionals include FM Dolby CD-4 Demodulator and SQ Decoder. All these items and more feature in the Aprịl/May 1976 Heathkit Catalogue supplement. - Heath (Gloucester) Limited, Dept. PW46, Gloucester, GL2 6EE.

## Barking Society

THE Barking Radio and Electronics Society G3XBF/ G8GPK, have recently started a new activity dealing with all aspects of closed circuit television. This section is attempting to build its own studio, but is hampered by a lack of members and may be forced to close. They feel there must be a need for a Video club in their area and have asked us to mention its formation in the News section of P.W. The society also runs a Morse Class on Tuesday evenings. Further details of any of their activities can be obtained from J. R. Wiles at Society HQ, Westbury Recreation Centre, Westbury School, Ripple Road, Barking, Essex, IG11 7PT. (Telephone: 01594 4009.)

# saticl lix  

THIS tuned RF amplifier will be found to provide quite substantial gain, and is of great help in bringing weak signals up to a level where they can be received properly. Even with a sensitive receiver having two RF amplifiers and a number of IF stages, it can result in the satisfactory reception of signals which are otherwise virtually impossible to copy.

With stronger signals, which would in any case be received satisfactorily, the unit helps to reduce second channel intereference, which can be troublesome with some receivers. However, its main use is in improving reception where a poor aerial, or the low signal strength of the wanted transmissions, makes adequate reception otherwise impossible.

## CIRCUIT DETAILS

Three coils are used, L1, L2 and L3, Fig. 1. Switch S1 selects the required coil. One section of VC2 (208pF) is used for L2 and L3. For the lowest frequency range L1, VC1 is also in circuit, giving 384 pF in all. As a result, three ranges as follows are obtained:-


Range $1-15-32 \mathrm{MHz}$
Range $2-5 \cdot 5-15 \mathrm{MHz}$
Range $3-1 \cdot 6-5 \cdot 5 \mathrm{MHz}$
It is of course not essential to provide tuning in this way. But if a value of about 365 pF is used for all bands, Ranges 1 and 2 will overlap considerably, while the use of 200 pF or so for each band will curtail the coverage of L3 at the low frequency end.


## component list

| Renistors: |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |
| - VR1 $25 \mathrm{k} \Omega$ Lin. potentiometer |  |  |  |  |  |  |  |  |
| Capacitors |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| Capacitors <br> C1 47pF* C4 100 nF |  |  |  |  |  |  |  |  |
| © C2 10 nF C5 100pF |  |  |  |  |  |  |  |  |
| *C3 10nF <br> VC1/VC2* Jackson type 00, 176/208pF gang. |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| $\underset{T r 1}{\text { Semiconductors }}$ |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| 8 L1, 'Blue' valve type Range 3. L2, 'BRange 4. L3, 'Blue valve type Rang |  |  |  |  |  |  |  |  |
| Denco miniature dual purpose). RFC1, RF choke ${ }_{\text {\% }}$ |  |  |  |  |  |  |  |  |
| type Denco RFC5. Jackson type 4832 two speed |  |  |  |  |  |  |  |  |
| drive with knobs. S1a ${ }^{\text {c }}$ b, c, 3-pole 4 -way |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| *. extra $127 \times 101 \mathrm{~mm}$ plate. (Home Radio). Four 12 mm |  |  |  |  |  |  |  |  |
| 4 high rubber feet. Two insulated aerial sockets. |  |  |  |  |  |  |  |  |
| - Coax socket. Tag strip comprising 8 tags. Battery |  |  |  |  |  |  |  |  |
| clip. Two matching control knobs. |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |

Results would be the same, but it is felt that having three ranges which include all bands from 1.6 MHz to 32 MHz in this way is probably better.

Switch section Sla/b Fig. 2 is for coil coupling windings while the third section of the switch, Sle, is for on-off purposes. An alternative aerial socket A2 is fitted for use instead of A1, when the unit is required to tune fairly sharply. Any end-connected aerial can be used.
Potentiometer VR1 allows amplification to be reduced when strong signals are present, as these might overload the receiver. This control however does not reduce gain to the level where no signals can be received.
Coupling to the receiver is from the RF choke


Fig 2 : The three-pole four-way switch S1Is of the rotary type, and front panel mounted.

RFCl and capacitor C5. This will work satisfactorily with receivers having a high nominal aerial input impedance. With receivers having a low impedance, overall gain can be increased by using an impedance matching coil, but this would either have to be tuned in addition to the aerial coils, or be a broad-band device.

When using the unit with communications type and similar receivers, it was found necessary to employ a screened co-axial lead to the receiver. The power supply is a small internal battery, the drain being only a few milliamps, depending on the setting of VR1.

## CABINET

A low-cost and effective screening box and case can be made easily from a $127 \times 102 \times 51 \mathrm{~mm}$ "universal chassis" with an extra $127 \times 101 \mathrm{~mm}$ flat plate, which is later attached with self-tapping screws for the top.

As the coil fixing bushes and core-adjusting screws


Plan view of the amplifier with the top plate removed. The ganged capacitor VC1/2 is driven via reduction gearing to provide precision tuning.
of the coils project through the bottom of the case, four plastic feet are required to raise it about 13 mm . First drill one $127 \times 51 \mathrm{~mm}$ member for the front, and fit the switch, VR1, and drive. The bottom $127 \times$ 51 mm flat plate is screwed on, and can be drilled to take VC1/2, which is held with one or two 4BA bolts. Washers or other distance pieces are necessary to raise the gang slightly, to get it level with the drive coupling. The capacitor fixing screws must not be too long, or they will short circuit or damage the capacitor. A final lining-up of drive and capacitor is easy if the drive fixing holes are on the large side.

Nearly all wiring is completed before the sides and back of the case are fitted. The back is prepared by drilling it for the aerial sockets and co-axial outlet and a clip is made to hold a PP4 battery. When the back is fitted, one 4BA bolt is used for an earth connection.


Fig. 3: The schemat/c shown here gives the location of all com. ponents, and the wiring between components and controls.

## WIRING DETAILS

Leads are run approximately as in Fig. 3. The tagstrip is raised on 12 mm long bolts. As unnecessary coupling between gate 1 and drain circuits is likely to cause instability, G1 is connected directly to VC2. For the same reason, the drain lead is lengthened


The case is constructed from a single Universal Chassis with an extra plate. Size is approximately $101 \times 127 \times 51 \mathrm{~mm}$.
and taken to the tag holding C5 and the RFC, both adjacent tags being earthed as in Fig. 2. Trl is gateprotected, and no special precautions need be taken when fitting it, provided the soldering iron is earthed and overheating is avoided.

The coil pins may need scraping, before soldering. Lengthy heating should also be avoided here, or the pins may move. Connections to the switch can be seen from Figs. 2 and 3. All these leads must be reasonably short and direct.

When the sides and back are fitted, connections can be made to A1, A2 and the co-axial socket. The battery is placed with its positive end toward Ll.

Earthing is provided by a terminal, or by the co-axial lead to the receiver. Having the latter unnecessarily long may reduce signal strength in some cases.

A frequency scale for the tuning need not be provided, as the amplifier is simply tuned to bring about an improvement in signal strength. With the unit switched to the Range needed for the receiver frequency, tuning should be found to peak up signals considerably. This will be most apparent with weak signals, or with the receiver AGC off. If the receiver has a tuning meter, this will show correct tuning. The coil cores are set to give coverage approximately as described. Exact coverage is not important, provided the ranges overlap slightly.

Should whistles accompany reception, especially with VR1 at maximum gain, Trl is oscillating. This is most likely when using an unscreened receiver aerial lead, especially if this is near the aerial connection to the unit. Tuning the booster should be found to peak up signals or aerial noise but not cause heterodynes or oscillation.

# TAKE <br> DAVID ANDREWS 

## No. 74 SNAP MACHINE

## A series of simple transistor projects, using not more than twenty components.



THERE have been lots of designs for simple Snap indicators published. Most, however, suffer from the problem that indication of the winner only lasts as long as the competitor presses his button. For that reason the following design has a built-in memory which ensures that the winner is indicated for an indefinite period until a reset button is pressed.

For the benefit of those who have not come across a Snap indicator before let's briefly explain the object and principle of operation. For games of skill involving two people it is sometimes desirable to find out who answers the question first. Before attempting to answer, the person has to commit himself to answering by pressing a button which lights a lamp and inhibits the opponent's button and lamp from operating.
The psychological impact of the Snap indicator
$\star$ components list

enhances a game's excitement considerably. The indicator could equally well be used in conjunction with the classical "Snap" card game.

## Flip-flop circuit

Inspection of the circuit will show that $\operatorname{Tr} 1$ and $\operatorname{Tr} 4$ form a simple flip-flop which becomes cross-coupled when either of the push-buttons S1 or S2 is closed. This action illuminates the LED on the side of the push-button in question and prevents the opponent's LED operating. This circuit differs from many others by the inclusion of $\operatorname{Tr} 2$ and $\operatorname{Tr} 3$ which respectively aot as "latches" to $\operatorname{Trl}$ and $\operatorname{Tr} 4$. If SI is depressed Trl switches on and LEDl lights up. The collector potential of Trl falls to zero thus preventing any base current drive to Tr4 inhibiting the other player's


Complete circuit diagram of the Snap Machine, showling fllp-flop Trf and Tr4, and latches $\mathrm{Tr}_{2}$ and Tr 3 .
 and LED'S. The size of the board is for guidance only.
circuit. The potential at the positive end of LED1 also falls towards zero and this provides a source of base current for $\operatorname{Tr} 2$ which is a PNP device. The collector voltage of Tr 2 rises towards the positive supply rail providing an alternative source of base current to Trl through R2.

If the player's finger is removed from the pushbutton this alternative supply of base current keeps Trl switched on and LED1 illuminated. At the same time the circuitry around $\operatorname{Tr} 4$ and LED2 is still inhibited, the only way to switch LED1 out and reset the circuit for another attempt is to break the circuit between the emitters of $\operatorname{Tr} 2$ and $\operatorname{Tr} 3$ and the positive rail, with the normally closed pushbutton S 3 .

## Board layout

Provided the layout is carefully followed there should be no problems in the assembly of this circuit. Use normally open push-buttons for S1 and S2 and a NORMALLY CLOSED one for S3. It is important to connect the LEDs with the right polarity. The CATHODE of the device should be connected to the collector of its driving transistor. Using the specified devices the cathode end can be identified by a very small indent on the base of the red plastic or by the fact that there is a wider shoulder on the top of the cathode lead-out wire. When using other LEDs check the polarity carefully.


## ACROSS

3 Grateful for this lack of fidelity? (9)
8 Spoken part chorally introduced? (4)
Steamiest form of radio? (8)
Untrue of Dylan's radio play? (6)
2 Drily cut off but I shall shortly be heard! (4)
4 Gets the message and sticks to the script! (5)
5 Cine movement in southern France? (4)
17 Demand precision in complex acting? (5)
19 Coverage of the first garden programme? (4)
I love her broadcasting manner (5)
River said to be in slow motion (4)
Set off because of the French component? (6)
A tuner in civil aviation? (8)
One piece heard from the deepest bass? (4)
He sings of a drink and a lake $(5,4)$

## DOWN

1 How to get on without feedback? (9)
Programme that takes the broader view? (8)
4 Toy with this in Children's Hour? (4)
5 A giant in Welsh programmes? (5)
$6 \& 20$ Down She's on the air fitfully $(6,6)$
7 Actors gloomy over this? (4)
1 The language you hear on Irish radio! (4)
12 Its creation may be quite a project? (5)
13 Welcome the end of transmission? (9)
16 An impressionable comic? (8)
18 Pitch of an oscillating note? (4)
20 See 6 Down
23 Kind of breakthrough the talkies made? (5)
24 He mustn't miss a word! (4)
25

N case you do not feel like wading through this review to the very end we will have the conclusions first! This kit is easy to assemble and to fit to a car. It worked first time and starting the car is much easier now, especially in cold weather. Is it a good buy? At $£ 7 \cdot 96+8 \%$ VAT it certainly is!
The circuit employed is similar to that which appeared in PW in June 1971, repeated in June and July 1972. However there are a few refinements which are very much worthwhile, all concerned with extra reliability. A two-transistor oscillator working at an audio frequency uses the primary winding of a transformer, the secondary feeds a bridge rectifier producing around 350 V DC output. This is applied to a thyristor, the gate of which is triggered by the car's contact breaker on the distributor. The 350 V pulse is fed via a $1 \mu \mathrm{~F}$ capacitor to the primary of the coil. In case you are worried about 350 V being applied to the 12 V coil it should be pointed out that 350 V is roughly the back voltage developed by the primary winding when the 12 V supply is broken by the contact breaker, the basis of the ordinary ignition system.

## INFO

The general information sheet supplied with the kit tells me that a Mr. Kettering was responsible for the original system some 60 years ago, so l've learned something! This sheet is full or useful information but unfortunately it is poorly reproduced in a very small type face, the explanatory diagrams being almost unreadable. Bi-Pre-Pak are not alone in this sad habit of neglecting the all-important "gen" accompanying electronic equipment generally and kits in particular. It may seem to the seller to be an economy, saving a few pence in this manner, but I can assure all those guilty that they are making a big mistake. The second information sheet supplied deals with the assembly of the kit and installation instructions. This is better produced but even so the circuit diagram was broken up in parts due to poor reproduction. Mr. Davis of B-P-P has assured me that this matter and a few spelling errors are being attended to.
However, it must be said that the printed circuit board is one of the best ever seen. The amount of information printed on the board makes the aforesaid circuit diagram almost superfluous! The PCB was assembled in a couple of hours, without going mad. The ends of all component leads were scraped clean whether they needed it or not. An old habit, but it pays off, ensuring a good soldered joint every time. Little sketches of the transistors, diodes and the thyristor on the circuit diagram and the PCB eliminate any possible error here when it comes to wiring them in.

During assembly the PCB was laid across the open top of the die-cast aluminium box, a great help. This box may seem to be rather extravagant, representing a fair part of the cost of the kit, but it does have an excellent seal all round, rather important considering the muck that can be found in the engine compartment of the average car! To aid the sealing a piece of thin plastic sheet was interposed when the lid of the box was finally screwed down.

## ANTI-THEFT

To my mind the biggest feature of the kit, not sufficiently underlined by B-P-P, is the ability to switch back to normal ignition at any time thus eliminating that fear in the back of the mind that the electronic ignition might let you down one day! It is important to note that if the switches are placed in opposite positions the car is totally immobilised, which is much easier than removing the rotor from the distributor! These two switches are mounted on the PCB and used to mount the board on the lid of the box. The neon lamp protruding through the lid is one of those little" extras" that instil confidence, indicating that the unit is producing the 350 V required, further confirmed by the high pitched whistle from the oscillator indicating that all is well.

## INSTALLATION

On applying 12 V from a car battery in the workshop, nothing happened! No current was being drawn by the unit. A check revealed that the fuse had been omitted! This is a piece of fuse wire soldered across two points on the PCB, thus saving a fuseholder. The fuse duly fitted, the unit worked at once producing the 350 V output at the rectifier. The PCB can be wired for positive or negative chassis but it should be noted that the black wire goes to the chassis regardless of the chassis polarity. The PCB is not electrically connected to the box so this lead must not be omitted.
The unit was fitted to a Triumph Herald 12/50 of 1965 vintage and tested during the very cold spell in February when temperatures were below freezing for several days on end. The box was bolted to the left-hand vertical panel continued on page 60 The photograph in the heading shows the printed circuil board which is fitted to the lid of the die-cast box by the locknuls on the switches. As can be seen the PCB is well annotated. The zig-zag lines are the alternative links for posilive or negative chassis connections. The two transistors are mounted vertically at the extreme righthand end of the board.

W. MOONEY

THE rapid decrease in the price of CMOS (4000 series) digital integrated circuits, and the amazing reduction in quiescent power consumption compared to the popular 74 series, makes experiment with these devices a tempting proposition. Quiescent power consumption is of the order of 10 nW per gate for the 4000 series and is therefore negligible, whereas consumption by the 74 series is about 10 mW per gate. Despite conflicting requirements of fast switching speed and low power consumption, these devices will still work well up to 10 MHz .

The signal source described here, uses only one IC which contains two 3 -input NOR gates and an inverter. The source provides a square-wave of about 1 kHz at a voltage of $99 \%$ of the battery voltage. Two outputs are provided, one via a $1 \mu \mathrm{~F}$ capacitor which should give a good square wave into high impedance loads, and a second output via a 100 pF capacitor, picking off the RF harmonics for signal injection.

The current drawn from the battery is less than $30 \mu \mathrm{~A}$ and increases with the application of a load to the output. The device will continue to work until the supply voltage drops to below 3 V , when the off load current will be about $10 \mu \mathrm{~A}$.

## Power consumplion

In a normal N or P channel MOS gate as in Fig. la the quiescent power consumption is high because a load resistor is used. Therefore in this instance when the output is in the low state a current must flow through the resistor in order to decrease the output voltage. This resistor must be fairly low so as to drive the following stage when a low output is required. But if too low, the current required to produce a low state will be too high. A compromise is therefore arrived at. If the load resistor is replaced by a MOSFET of opposite polarity (Complementary)

to the lower MOSFET as in Fig. lb the need for such a compromise is obviated as this load fulfils both requirements.

In the high output state the lower MOSFET switches off becoming, in effect, a high resistance of about $10^{13} \Omega$ and the top MOSFET becomes a low resistance of about $300 \Omega$. When a low output is required the resistors effectively change place, the upper MOSFET switching off and the lower MOSFET switching on. In the complementary MOSFET circuit (CMOS) the power consumed in the high or low state is therefore negligible and the great majority of the power is consumed during switching.

For a brief period curing the switching action both MOSFETS will be equally on and will have a relatively low resistance. At this instant the current peaks to typically 1.5 mA with a 10 V supply rail. When the CMOS gate is in a normal digital environment carrying step pulses, the power consumed due to this effect is practically zero. The consumption is then purely due to the capacitance of the load, typically 5 pF per gate.



Fig. 2: Internal configuration of the CD4000. Gates 'a' and 'b' are NOR gates and 'c' /s an Inverter.

## Toial power

The total power consumed (Pt) by a particular gate carrying regular step pulses is therefore the sum of the quiescent power $(\mathrm{Pq})$ in the high or low state, and the switching power. The switching power is dependent on the frequency (f), the voltage difference between the high and low states (approx. the supply voltage Vdd) and the capacitance of the load (C). Bringing these together we get:

$$
\mathrm{Pt}=\mathrm{Pq}+\mathrm{CVdd}{ }^{\circ} \mathrm{f}
$$

This is arrived at from the familiar expression for the energy stored in a capacitor ${ }^{1}{ }_{2} \mathrm{CV}^{2}$.

In the source described here the conditions are somewhat different as the inputs to both gates are part of a timing circuit. This circuit slows down the transition through the high current portion of the transfer characteristic, giving a higher current drain than would be expected from the above expression. However at a maximum of $30 \mu \mathrm{~A}$ it still compares very favourably with an equivalent circuit using discrete bipolar devices.

## Circuit operation

The internal layout of the CD4000 IC used in this circuit is shown in Fig. 2, the parts marked (a) and (b) are the NOR gates and (c) the inverter. The circuit of the oscillator is shown in Fig. 3, all inputs to each gate are strapped together, the operation now being the same as that of the inverter where a low input produces a high output and vice versa. The circuit will be recognised as a multivibrator type of oscillator, the frequency determining components being $\mathrm{Cl} / \mathrm{R1}$ and $\mathrm{C} 2 / \mathrm{R} 2$. In this circuit $\mathrm{Cl}=$ C 2 and $\mathrm{R} 1=\mathrm{R} 2$, thus giving a squarewave of equal mark/space ratio.
Circuit operation is best understood by freezing the cycle at a point in time when the output of gate (a) has just jumped from zero up to nearly the supply voltage. The voltage on the input to (b) will follow this rise since Cl is discharged and the output of (b) will now be zero. The voltage on the input to (b) will slowly drop towards zero as C2 charges up, and at some point (about $40 \%$ of the supply voltage) will cause the output of (b) to jump quite rapidly to

## components list

| Resistors |  |  |
| :---: | :---: | :---: |
| R1 10 Ma |  | 1M3 |
| R2 10MS |  | see text |
| All resistors $10 \% \div W$ |  |  |
| Capacitors |  |  |
| C1 100pF SM |  | 100 pF SM |
| C2 100pF SM |  | tuF 50 V elect: |
| Semiconductors |  |  |
| IC1 CD4000 |  |  |

## Miscellaneous

S1, miniature slide switch. Aluminium box $76 \pi$ $50 \times 25 \mathrm{~mm}$ type AB12, available from Home Radio. Printed circuit board $45 \times 25 \mathrm{~mm}$. Three 3 mm plugs and sockets. Three 1.5 V cells, type D23.
the high state. As Cl is discharged, the input to (a) will follow this increase causing the output of (a) to drop. It will now remain low until Cl charges through R1 to the point where the output of (a) goes high once more and the cycle repeats. At the times of the cycle when the output of (a) or (b) drops to a low state the associated capacitor will be charged up and this charge results in a negative voltage appearing on the following input. A lucky spin-off of the input protection circuitry now occurs as this negative potential forward biases certain diodes thus


Fig. 3: The above drawing shows the complete circuit of the osclllator. With the component values shown, the output frequency is about 700 Hz .
quickly discharging the relevant capacitor.
The output from gate (b) is passed through the inverter which isolates the oscillator from the load and squares up the waveform. The supply line is not decoupled as it is quite unnecessary and tends to make starting difficult by removing the switch-on kick. No specific arrangements have been made for starting but should the oscillator stop for any reason, simply switching off for a few moments, and then on again, will usually start the oscillator running.

## Construction

The device is constructed in a ready made aluminium box measuring $76 \times 50 \times 25 \mathrm{~mm}$. The PCB, Fig 4 switch and terminals were attached to the lid of the box as is the power source which consists of three 1.5 V cells, type D23, connected to give over


Fig. 4: PCB showing foll side to the left, and component overlay to the right. The board is shown full size.
4.5V when new. These small cells are not very popular but a little searching is worth while as they offer a considerable saving in space, being only about 10 mm in dia. and 30 mm long. A long life is expected of these batteries and they are therefore glued together and then to the case, making the connecttions by direct soldering. If it is decided to use mercury cells, direct soldering should be avoided for safety reasons.

The IC was found to be remarkably robust as the inputs are protected by an array of zener diodes to prevent static build up. However in the interests of good practice the soldering iron should be earthed and precautions taken to prevent personal static build up. The timing capacitors are silvered mica but any low leakage type will do. The output capacitors should have a suitably high working voltage if work with valve or high voltage transistor equipment is envisaged.

## The source in use

The output frequency of the device with the component values given here is about 700 Hz . The squarewave is quite good with harmonics extending well into the short wave region. The output voltage is dependent on the supply voltage and the device will work well down to below 3 V . Under 3V, however, starting becomes increasingly difficult. The quiescent current consumption at 3 V is less than $10 \mu \mathrm{~A}$.

The device has been used for fault finding in AM receivers and audio amplifiers, although the use of a square-wave generator does not end here, especially if an oscilloscope is to hand. For example, the action


Fig. 5: The output amplitude of the Signal Source may be a little high for some purposes, and this simple attenuator should be used when necessary.
of tone controls and various filters can then be observed directly. One fundamental property of a symmetrical square-wave is that the RMS and aver-
age voltage are equal. This property was demonstrated with a prototype when the battery voltage was found to be 4.8 V ( 20 k ohm/Volt meter), the output indicatéd on the AC range was exactly 2.4 V RMS.

Some form of potential divider should therefore be used before injecting the signal into the more sensitive stages of audio amplifiers, otherwise serious overload will occur giving misleading results. A simple attenuator as shown in Fig. 5 will be adequate, the value of R 4 being altered as required. For example with 2.4 V input and $\mathrm{R} 4=1 \mathrm{k} \Omega$ the output will be $2 \cdot 4 \mathrm{mV}$. Some levels to expect when dealing with AF stages are as follows:
Output from magnetic cartridge ................... 3 mV
Output from ceramic cartridge ................... 80 mV
Output from crystal cartridge ................... 300 mV
Output from cassette replay head ................ 0.5 mV
Input from, tape, tuner, or aux $\ldots \ldots . . . . . . .$.
Although it should be remembered that the battery life will be reduced by applying heavy loads to the source, it is possible to drive an $8 \Omega$ loudspeaker directly although this hasn't been tried for more than a few seconds.

# HODKS RECEIVED 

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|  | 12 V 100 MA |  |  | 14 V 40 MA |
|  | $14 \vee 75 \mathrm{MA}$ | F | 4MM | 2.7 V 60 MA |
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## GOING BACK... 1970 B0 $55^{5040^{30800 ~}}$

'ftlystery' 环ereiber

IHAVE received a letter from one of our younger Going Back enthusiasts-John Narborough, aged 16, from Uckfield in Sussex.

He tells me that he has quite a collection of vintage radio equipment and during his three or four years of being a PW reader, prompted by reminiscences from his dear old dad who used to dabble in radio in the ' 20 s he has become extremely interested in the earlier days of wireless.

He says he is finding-much to his mother's delight-that it is becoming increasingly hard to find items of equipment (that do not have misguidedly high price tags) with which to "clutter" up the home. Nevertheless, John considers that he has one or two prizes in his collection.

John'would like to know if any other Going Back readers could help him concerning the item in the two smaller photographs. The set is built into an oak cabinet which has a drop-down front. Three valveholders are mounted at the top with filament rheostats below. Also included are the usual tuning and reaction con-

and a reaction control for some external piece of equipment-possibly a frame aerial-even though there are $\mathbf{A E}$ and E terminals on the panel. The wiring (it's a pity but a few of the components are missing) indicates that the set is probably an early '20s' design and there is a transformer wound "like a coil in cylinder form", the core of which comprises individual iron wires. Under the detector valve socket (centre) there is a screw-in variable grid leak and coil changing system of plugs and sockets. An engraved "wiper" type switch gives ranges from 200


## Fintage $\mathbb{C O}$ :

## INFORMATION WANTED

. . . Circuit diagram or the Works Publication WP 137 (mentioned on label giving valve details) of a Burndept Screened Portable. Valves are PM1HF, PM1A, PM12 and PM252. The set requires a 2 V accumulator, 108 V HT with 66 V tapping and 18 V (tapped every 1.5 V ) grid battery.-John Hein, 13 Blane Avenue', Blanefield, via Glasgow, G63 9HU.


## Early morning maths

While thumbing through my husband's $P W$ (February), I noticed the Editors comments on digital watches. We have had a digital clock for over a year now, and although I can cope with the 24 hour system on it, I am still sometimes frustrated by having to mentally subtract numbers from 60 to find out how long it is to the next 'o'clock'.

My suggestion (I know nothing about the electronic practicability of it) is that we return to the 12 hour system, and that the display reads the minutes first, with 'to' or 'past' in the middle, i.e. 27 past 7 or 29 to 8 . This would abolish the need for mental arithmetic early in the morning as the time to get up approaches! Mrs F R Tasker (Hardwicke)
PS. What happened to the crossword?
This is fitted in when space permits-Ed.

## Crystal controlled pendulum

Your editorial in the February issue of Practical Wireless caused me a little quiet amusement.
As a retired airline captain, I am used to learning to accept new instrument faces, hence the digital presentation causes me no pain. However, this does not deafen me to the complaints of the female side of my family ever since I constructed a digital clock. I am. sure that quite a lot of people have to make a distinct effort to convert mere numbers
to a more conventional mental picture of time.

A few months ago, I wrote to another journal making such a point and asking if they would publish a circuit which would marry the accuracy of a crystal timer to a balance wheel or pendulum clock. This could be achieved by comparison perhaps, plus suitable correcting impulses. I said I was sure that this would please hobbyists and horologists not to mention their womenfolk! The editor did not agree, hence my amusement.

You, of course, refer only to wrist watches. In this case could not a miniature stepping motor drive conventional hands, as employed, I believe, in certain makes of watch?-E Rodley (Guildford).

## IC DFM

Is it not time to revisit the subject of the Digital frequency meter?
Surely, amongst the readership of $P W$ there is someone capable of contributing a device of sound economic sense, from the vast array of ICs now available?B A Martin (Solihull)
We hope to be satisfying people, such as Mr Martin, very shortly -Ed.

## Heavy duly charge

As a reader of PW for many years and also a keen motorist (DIY), I submit a humble request for an article on a battery charger, something a little more sophisticated than the straight forward trickle charger. I would suggest a charging rate from about 2A to 8A (for rapid charge), and using full wave rectification. Suitable also for 6 V or 12 V batteries. I'm sure one could be built much cheaper than a commercially bought one.-C. Law (Blackburn)
(Potential contributors-please note)

## The price of stock

Reading Mr B. A. Pearson's letter of complaint re transistor prices in the March issue, stirs me from my customary lethargy (and it takes a lot to do that) and
prompts me to put another view which may not be popular with all your readers.
In the first place, the correct price for an OC71 of reputable make should have been 74 p plus VAT. In the second place the dealer should be thanked for keeping this type of transistor in stock, bearing in mind the fact that these are not exactly the most sought-after transistors and in any case can be obtained in bulk at give away prices as seconds or surplus which the average dealer would not care to keep or sell.
The third item is this. The average man in the street knows nothing of the pitfalls involved in running a business (be it small or large). He knows he needs an OC71 and for convenience pops into his local dealer trusting that he will have some in stock. It could have been any one of hundreds of different types held in stock against the time they are needed (if they are) together with hundreds of valves, resistors, capacitors etc. Who pays for the stock which just lies there as a convenience? There is no way of knowing what will be asked for. If Mr Pearson thinks it is so lucrative I suggest he draws up an imaginary stock list, pays for it all (mentally that is, I doubt if he would be so bold as to do it) and then tries to sell it at 25p per go, that is if he has thought to stock the item required.-Les Lawry-Johns (Gravesend, Kent)

## Very puzzling

I have taken PW for some years now, and whenever possible attempt to complete the 'Technicross' puzzle. However, after many frustrating months, I feel that it would be beneficial to those taking part if the answers were published in the same issue as the puzzle. Waiting a month for the correct answers tends to lessen the enjoyment of the game.
Perhaps I may also suggest, that on the whole, the questions are a little. obscure for the general readership of PW, including myself! Am I just a little thick or is this a generally held thought amongst the readership? -A W Bunting (Kent)
We would be pleased to hear from other readers about their views on this feature.

## NEW MULLARD \& MAZDA VALVES

All individually boxed and guaranteed. Full trade discounts to bona fide companies. Price and availability lists on application.

| DM70 | 0.69 | EF80 | 0.68 | PCC84 | 0-63 | PL504 | 1.02 | 30C15/ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DY86/7 | 0.58 | EF83 | 1-10 | PCC8s | 0.90 | PL508 | 1.80 | PCF800 1.22 |
| DY80. | 0.63 | EF85 | 0.68 | PCC88 | 0.98 | PL509 | 1.77 | $30 \mathrm{Cl17} \quad 1.29$ |
| EABC80 | 1-16 | EF86 | 1.60 | YCOC89 | 0.78 | PL802 | 2.03 | 30018/ |
| EB91 | 0.78 | EF89 | 1.47 | PCC189 | 0.91 | PY33 | 0.78 | PCF805 1-29 |
| EBC81 | 0.89 | EF91 | 1-35 | PCP80 | 0.68 | PY81/800 | 0.56 | 30F5/PF818 |
| EBF80 | 063 | EF92 | 1.51 | PGP82 | 1.87 | PY82 | $0 \% 0$ | 1.85 |
| EBF83 | 068 | EF95 | 1.68 | PCF88 | 0.78 | PY88 | 0.63 | - |
| EBF89 | 0.60 | EF183 | 0.69 | PCF200 | $1-30$ | PY500A | 1.15 | FCEA00 0.98 |
| EC85 | 0.88 | EF184 | 0.89 | PCF201 | 1.30 | PY800 | 0.58 | $30 \mathrm{FL2} 1.02$ |
| EC88 | $0-88$ | EH90 | 0.91 | PCF801 | 0.78 | PY801 | 0.56 | $30 \mathrm{FL12} 124$ |
| EC90 | 0.84 | EL34 | 1.81 | PCF60' | 0-78 | U26 | 1.22 | 30 FL14 1.20 |
| EC97 | 0.69 | EL36 | 1.15 | PCF806 | 0.78 | U191 | 1.17 | $30 \mathrm{LI} / \mathrm{PCC8} 4$ |
| ECC81 | 0-54 | EL84 | $0-58$ | PCH׳00 | 1.80 | U193 | 0.58 | 0.68 |
| ECC82 | 0.58 | EL86 | 1.21 | PCL88 | 0.68 | UABC80 | 1.01 | $30 \mathrm{L15} /{ }^{\text {3 }}$ |
| ECC83 | 0.58 | EL95 | 0.89 | PCL83 | 0.73 | UBC81 | 0.80 | FCC805 1.85 |
| ${ }_{\text {ECC8 }}$ | 0.68 | EM81 | 1.84 0.89 | PCL84 | 0.69 | UBF89 | 0.65 | $\begin{array}{ll}30 \mathrm{Ll7} & 1.12 \\ 30 \mathrm{P} 4 \mathrm{MP} & 1.88\end{array}$ |
| ECC88 | 0.78 1.08 | EY86 | 0.89 0.50 | PCLS 5 | $0 \cdot 78$ | UCC85 | 0.68 | $30 \mathrm{P} 4 \mathrm{MR} \quad 1.68$ |
| ECC189 | 0.77 | EY86/87 | 0.58 | PCL86 | 0.78 | UCH81 | 1.80 | PC801 1-82 |
| ECF80 | 0.63 | EY88 | 0.81 | PCL805/85 | 0 | UCL82 | 0.78 0.78 | $30 \mathrm{P19} 1$ |
| ECF82 | 0.90 | Ez80 | 0.68 | PD500 | 2.11 | UL84 | 0.78 1.06 | PC802 1.08 |
| ECP86 | 0.78 | EZ81 | 0.83 | PFL200 | 0.91 | UY85 | 0.73 | $30 \mathrm{PLI} /$ |
| ECH81 | 1.50 | GY501 | 1.30 | PL36 | 1.08 | 6/30L2/ |  | PCL801 1.85 |
| ECE83 | 1.06 | GZ34 | 1.06 | ${ }_{\text {PL81 }}$ | 0.91 1.08 |  |  | 30PL13/ |
| ECH84 | 1.30 | $0 \mathrm{C83}$ | 0.60 | PL81A | 1.08 | ECO804 |  | PCL800 1-47 |
| ECL80 | 0.78 | PC86 | $1-05$ | PL82 | $0-48$ | 6F23/EF812 |  | 30PL14/ |
| ECL82 | 0.69 | PC88 | 1.05 | PL43 | 1.80 |  | $1-16$ | PCL88 1.78 |
| EGIS3 | 078 | PC97 | 0.58 | PL84 | 0.78 | 30C1/PCF80 |  | 30 PL 15144 |
| ECL86 | 0.78 | PC900 | $0 \cdot 65$ | PL500 | 1-02 |  | 0.68 |  |

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Individually boxed and guaranteed but of European or other origin at greatly reduced prices. Quotations for any valve not listed. Send SAE for lists.

|  |  |  |  |  |  | PYS00 <br> PY81/800 | $\begin{aligned} & 1.10 \\ & 0.50 \end{aligned}$ | 6J5M 8.550 | $\begin{aligned} & 0.88 \\ & 0.45 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | PY801 | 0.85 | 656 | 0.85 |
| Individually boxed and |  |  |  |  |  | EP41 | - 00 | ${ }^{6 J 70}$ | 0.10 |
| guaranieed but of Euro- |  |  |  |  |  | T861 | 0.85 1.50 | 6J7M 6K6GT | 0.65 0.80 |
|  |  |  |  |  |  | U14 | 0.76 | 8K7 | 0.88 |
| pean or other origin at |  |  |  |  |  | U25 | 1.00 0.85 | ${ }^{6 K 7} \mathbf{6 K}$ | 0.45 |
|  |  |  |  |  |  | $\mathrm{U}^{2} 26$ | 0.85 | 6K8G | 0.45 |
| greatly reduced prices. |  |  |  |  |  | U19 ${ }^{\text {U }}$ | 0.76 | 6K8M | 0.70 |
| Quotations for any |  |  |  |  |  | UAF42 | 0-75 | 6 LBG | 1.25 |
|  |  |  |  |  |  | UBC41 | 0.60 | 6L6GC | 0.60 |
| valve not listed. Send |  |  |  |  |  | UBC81 | 0.80 | 6Q7G | 0.40 |
| for lists. |  |  |  |  |  | UBF80 | 0.50 | 607M | 0.60 |
|  |  |  |  |  |  | UBF89 | 0.60 | 68L7GT | 0.55 |
|  |  |  |  |  |  |  | 0 | 68N7GT | 0.5 |
| AZ1 | 1.00 | EF37A | 1.50 | N78 | $5 \cdot 00$ |  |  |  |  |
| A231 | 1.00 | EP39 | 1.25 | $\mathrm{OA}_{2}$ | 0.46 | UCL8? | 0-80 | 6U5G | 1.50 |
| CBL31 | 1.40 | EF80 | 0.85 | OB 2 | 0.45 | UCL83 | 0.40 0.70 | 6V8G | 0.80 |
| CL33 | 1.50 | EF85 | 048 | PC88 | 0-85 |  | $0 \cdot 70$ | 6V8GT | 0.60 |
| CY31 | 1.00 | EF88 | 050 | PC88 | 0.65 | UF89 | 0-76 | ${ }^{6 \times 6}$ | 0.45 |
| DAF91 | 040 | EF89 | 0.85 | PC97 | 0.55 | UL41 | -0.60 | 6X6GT | 0.46 |
| DaF96 | 0.00 | 91 | 0.40 | PC900 | 0.55 | UL84 | 0.50 | $7 \mathrm{B6}$ | 0.80 |
| DCC90 | 1.35 | EF92 | 0.80 | PCC84 | 0.45 | UYid | 0.85 | $7 \mathrm{B7}$ | 0.80 |
| DF91 | 0.40 | EF95 | 0.45 | PCO88 | 0.88 | UY85 | 0.45 | $7 \mathrm{C5}$ |  |
| DF98 | 0.80 | ${ }_{\text {EFF183 }}$ | 0.80 0.40 | PCCs9 | 0-58 | VR105/30 | 0.40 | ${ }_{7} \mathbf{C}$ | 2.00 |
| DK91 | 0.50 | ${ }_{\text {EFF183 }}$ | 0.40 | PGCI 89 | 0-85 | VR150/30 | 0.45 | 7H7 | 0 |
| DKK96 | 1.00 0.76 | EL32 | 0.80 | PCF80 | 0.40 | 1 RS | 0.60 | 787 | 0.80 |
| DL92 | 050 | EL33 | 8.00 | PCP86 | 0.65 | 185 | 0.40 | 787 | d. ${ }^{\text {c }}$ |
| DL94 | 0.48 | EL34 | 0.70 | PCF801 | 0.60 | 174 | 0-50 | 7 Y 4 | 0.30 |
| DL98 | 0.56 | EL36 | 0.80 | PCF802 | 0.56 | 384 | 0.80 | 12AT6 | 0.45 |
| DY88 | 0.45 | EL37 | 8.40 | PCP805 | $0-90$ | ${ }_{\text {BR4GY }}$ | -20 | 12AT7 | 0.48 |
| DY87 | 0.46 | EL41 | 080 | PCF80¢ | 0.80 | bU4G | 1.25 | 12AUU7 | 0 |
| DY802 | 0.47 | EL42 | 1.65 | PCF808 | 1.00 | EU4GB | 0.70 | 12AX 7 | 0.818 |
| EABC80 | 0.88 | EL84 | 0.85 | PCL82 | 0.45 | ${ }^{6} \mathrm{Y} 3 \mathrm{GT}$ | - 0.65 | 12BA6 | 0.50 |
| EAF42 | 0.70 | EL95 | 0.80 | PCL83 | 0.70 | SZ4G | 0.95 | 12 BE - | 0.60 |
| E891 | 0.80 | EM80 | 0.65 | PCL84 | $0-50$ | 6/30L2 | 0.90 | 30 Cl | 0.40 |
| EBC33 | 1.00 | EM81 | 0.80 | PCL85 | 0.60 | 6AK | 0.46 | 30 Cl 5 | 1.00 |
| EBC41 | 0.75 | EM84 | 0.40 | PCL86 | 0.60 | 6AM5 | 2.00 | 30 Cl 7 | 1.00 |
| \& BC81 | 0.40 | EMB8 | 1.00 | PCL805/85 |  | 6AQS | 0.50 | 30C18 | 0.90 |
| EBF80 | 0.40 | EM87 | 1.00 |  | 0-60 | 6AB7G | 1.00 | 30Fs | 1.00 |
| EBF83 | 0.40 | EY81 | 0.45 | PD500 | 150 | 6at6 | 0.60 | 30FL1 | 1.00 |
| EBF'89 | $0 \cdot 82$ | EY88 | 0.50 | PEN4S | $0 \cdot 85$ | 6AUE | 0.40 | 80FL2 | 1.00 |
| EBL91 | 2.00 | EZ40 | 0.60 | PL36 | 0.68 | ${ }^{\text {6 B A }}$ | 0.88 | 30 FLl 4 | 1.00 |
| ECC81 | 0.45 | E241 | 0.76 | PL81 | 0.55 | 6BE6 | 0.46 | 30 L 15 | 0.95 |
| ECCA2 | 0.88 | E280 | 0.80 | PLA2 | 0.50 | 68H6 | $0-75$ | 30 L 17 | 0.95 |
| EOCA3 | $0-88$ | E281 | 0.81 | PL83 | $0-50$ | 6BJ6 | 0.76 | 30P4MR | 1.30 |
| ECCs 4 | 0.85 | GY501 | 0.90 | PL84 | 0.50 | 6B97A | 0.65 | 30 Pl 12 | 1.00 |
| ECC8s | 0.45 | GZ30 | 0.65 | PL500 | 0.86 | 68R7 | 1-20 | 30 P 19 | 0.95 |
| ECC88 | 0.60 | G232 | 0.65 | PL504 | 0.85 | 6887 | 140 | 30PLI | 0.95 |
| RCHs5 | 1.50 | GZ34 | 0.75 | PL508 | 0.90 | 68w6 | 100 | 30PLIs | I. 10 |
| ECH42 | 0.85 | HN309 | 1.50 | PL509 | 1.55 | 6BW7 | 1.00 | 30PLI | 1.10 |
| ECH81 | 0.85 | KT61 | $3 \cdot 00$ | PLa02 | 8.00 | 8C4 | 0.40 | 35W4 | 0.80 |
| RCH83 | 0-50 | KT88 | 3.40 | PX25 | 3.60 | ${ }^{6 C D 6 G}$ | 1.60 | 3524GT | 0.70 |
| ECL80 | 0.60 | KT81 7 | )2-00 | PY33 | 0.68 | ${ }^{8 C H} 6$ | 2.20 | socd 6 | 1.20 |
| ECL82 | 0.48 | KT81 | 1.75 | PY81 | 0.50 | 6CW4 | 3.00 | 807 | 1.00 |
| ECL83 | 0.75 | K T88 | $3 \cdot 65$ | PY82 | 0.45 | $6 \mathrm{~F}^{23}$ | 0.90 | 8131 TT | 17.50 |
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| AC107 | 0.81 | BF115 | 0.8 |
| :--- | :--- | :--- | :--- |
| AC126 | 0.25 | BF167 | 0.25 |

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| $\mathrm{ACl28}$ | 0.15 | BF179 | 0.88 |
| :--- | :--- | :--- | :--- |
| $\mathrm{AC178}$ | 0.25 | BF180 | 0.88 |
| $\mathrm{AC187}$ | 0.21 | BF181 | 0.85 |


| AC178 | 0.26 | BF180 | 0.86 |
| :--- | :--- | :--- | :--- |
| AC187 | 0.21 | BF181 | 0.86 |
| AC188 | 0.80 | BF194 | 0.10 |
| A 0821 | 0.85 | BF195 | 0.18 |


| AC188 | 0.80 | BF194 | 0.10 |
| :--- | :--- | :--- | :--- |
| AOY21 | 0.85 | BF195 | 0.18 |
| AOY39 | 0.75 | BF197 | 0.16 |
| AD140 | 0.80 | BF200 | 0.82 |


| AD140 | 0.60 | BF200 | 0.88 |
| :--- | :--- | :--- | :--- |
| AD149 | 0.75 | BFS61 | 0.85 |
| AD161 | 0.44 | BP898 | 0.25 |
| AD162 | 0.44 | BPW | 0.81 |


| AD182 | 0.44 | BFW10 | 0.61 |
| :--- | :--- | :--- | :--- |
| AF115 | 0.86 | BFX29 | 0.88 |
| AF116 | 0.85 | BFI88 | 0.8 |
| AF117 | 0.8 | BFY50 | 0.80 |


| AF114 | 0.80 | BFY88 | 0.84 |
| :--- | :--- | :--- | :--- |
| AF117 | 0.94 | BFY80 | 0.20 |
| AF186 | 0.48 | BFY51 | 0.90 |
| AF230 | 0.44 | BFY52 | 0.20 |


| AF239 | 0.44 | BFY82 | 0.20 |
| :--- | :--- | :--- | :--- |
| ABY27 | $0-88$ | BR100 | 0.40 |
| A8Y28 | 0.8 | BY100 | 0.27 |
| BA102 | 0.25 | BY126 | 0.14 |
|  | BY127 | 0.10 |  |


| BA102 | 0.25 | BY126 | 0.14 |
| :--- | :--- | :--- | ---: |
| BA115 | 0.10 | BY127 | 0.12 |
| BC107 | 0.14 | BZXB1 Rerie |  |


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|  | BC14 | 0.30 | CREB3-40 |
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| BO147 | 0.10 | 0.40 |  |
| CRE3-40 | 0.65 |  |  |




| BO182L | $0-11$ | MJE995s | 1.2 |
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| B0184L | $0-18$ | MJESOS | 0.7 |


| BO1B4L | 0.15 | MJESOBS | 0 |
| :--- | :--- | :--- | :--- |
| BC338 | 0.16 | MPF102 | 0 |
| BOYt2 | 0.85 | MPF108 | 0 |



| BOY70 | 0.18 | NKT104 | 1.0 |
| :--- | :--- | :--- | :--- |
| BOY71 | 0.82 | OA8 | 0.7 |
| BCY72 | 0.18 | OA10 | 0.40 |


| BCZ11 | $0-65$ | 0479 | 0.10 |
| :--- | :--- | :--- | :--- |
| BD121 | 1.00 | 0461 | 0.18 |


| ENT400 | 0-18 | SN7428 | 0.40 | 8N748日 | 0.47 | BN74145 | $1 \cdot 26$ | SN74192 | 00 |
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| SN7405 | 0.29 | SN7440 | 0.28 | SN7493 | 0.70 | 8N74156 | 1.00 | BN74197 | 1.20 |
| SN7408 | 0.48 | SN7441AN |  | SN7494 | 0.80 | SN74157 | 0.95 | BN74198 | 8.77 |
| SN7407 | 0.48 |  | 0.92 | GN7495 | 0.80 | SN74170 | 8.58 | SN74199 | 8.58 |
| SN7408 | 0.28 | 8N7442 | 0.79 | SN7488 | $0 \cdot 65$ | BNT4174 | $1 \cdot 57$ |  |  |
| BN7409 | 0.28 | SN7450 | 0.16 | 8N7497 | 8.87 | 8N74175 | $1 \cdot 10$ |  |  |
| SN7410 | 0.16 | BN7451 | 0.18 | SN74100 | 1.89 | GN74170 | 1-26 |  |  |
| SN7411 | 0.25 | gN7453 | 0.16 | SN74107 | 0.45 | 6N74190 | $8 \cdot 00$ |  |  |
| 8N7412 | 0.80 | BN7454 | 0.16 | 8N74110 | 0.58 | 8N74191 | 2.00 |  |  |
| SN7413 | 0.88 | BN7460 | 0.16 | SN74118 | 0.90 |  |  |  |  |
| SN7418 | 0.88 | SN7470 | 0.88 | SN74119 | 1-68 |  |  |  |  |
| SN7417 | 0.88 | SN7473 | 0.41 | SN74121 | 0.50 | DIL |  | 4 pi |  |
| 9N7420 | 0.16 | SN7474 | 0.48 | SN74122 | 0.70 |  |  |  |  |
| 8N7422 | 0.25 | BN7480 | $0-80$ | 8N74123 | 1.00 | SOCKE |  | 16 pln |  |
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3-VALVE RADIOS

Valved radios are still great favourites with many people. The main reason is economy, as a mains operated transistorised set large enough to provide the same bass response tends to be expensive whilst battery operated sets are either too small to sound good or are too expensive to run, bearing in mind the fact that a PP9 battery, for example, is now over 50 p . In addition to this, some people have a sentimental attachment to their valve radios. We are quite fond of an old couple in their nineties, who have a 1933 Ultra! We will not go into the servicing of this type of set, however! Suffice to say that we have kept it going for them for more years than we care to mention.

## Transformerless

Valved radios generally fall into two types, the heavier type having a mains transformer and parallel-fed valve heaters and the lighter ones with no transformer and series heaters. The latter is more commonly encountered and we will consider this type first.

With no transformer to provide low voltage supplies, the normal 240 V mains has to be adapted to provide the HT and heater requirements. If we accept that one of the mains supply leads, preferably the neutral, can be connected directly to the chassis or metalwork, the design can be simplified so that all that is necessary is a means of reducing the mains voltage to that required by the total number of valve heaters in series. This is usually done by inserting a wirewound resistor in the top end of the series chain to drop the voltage to that required. A tapping on this resistor can be used to supply the HT rectifier, which is usually a valve, and the current drawn by the HT must be added to that drawn by the valve heaters when calculating the value of the dropping resistor. The arrangement is shown in Fig. 1 except that a dial lamp and shunt resistor have been inserted into the chassis return to neutral (or one side of the mains at any rate).

The advantage of using a valve rectifier is twofold. First, the valve warms up slowly with the rest and therefore the HT builds up slowly as the rest begin to draw current. Therefore the HT is rarely more than, say, 200 V . This takes the strain off all the capacitors on the HT line and leads to greater reliability. Secondly, the voltage drop across the rectifier heater in addition to that of the other valves reduces the rating of the dropper so that the heat concentration is reduced in this area. Obviously the
higher the total voltage of the valve heaters the lower the value of the dropper. This is why nearly all European radios of this type used 100 mA valves of the "U" series (UY85, UL84, UCL82 etc.). Countries with a low mains voltage (say the US) of about 110 V used a different range of valves taking more current and dropping less voltage. Some years ago it was quite common to find a series chain of 0.3 A valves ( $25 Z 4,25 \mathrm{~L} 6 \mathrm{etc}$.), or a $0 \cdot 2 \mathrm{~A}$ chain (CY31, CL33 etc.), a $0 \cdot 15 \mathrm{~A}$ chain or even a $0 \cdot 16 \mathrm{~A}$ would you believe! Also a $0 \cdot 1 \mathrm{~A}$ chain which is the most likely line-up to be found in sets of more recent


Fig. 1 In $A C / D C$ receivers the heater chain and HT supply were generally of this type.
The number of valves used could vary but the minimum was usually four including the rectifier, this line-up being, for example, UCH81 frequency changer, UBF89 IF amp, detector and AGC, UCL82 audio amplifier and output, and a UY85 rectifier. A variation on this theme was a UCH81 as above with another UCH81 as an IF amplifier and audio amplifier with a UL84 output, using two crystal diodes for detection and AGC. The one advantage with this system was the possibility of changing over the two UCH81s if the one in the FC stage was reluctant to oscillate (which is something they often did, or didn't!).

The main disadvantage of series-heated valves is
the fact that rectifier and output valves are well up the live mains end with only the dropper and perhaps the dial lamps (some designs) at a higher potential. This means that there is increased stress between the heater and the cathode of the valve with the consequent risk of breakdown, and induced hum in the case of the output valve. It comes as no surprise therefore to find the fault of "no valves glowing" is often due to the heater of the rectifier being open circuit. It is not that the heater just feels like failing, it is most often blown due to the failure of insulation, the high potential AC on the heater suddenly finding itself provided with a short cut via the main electrolytic capacitor and chassis. The rectifier heater is thus treated to an extremely gay life of somewhat short duration. If there are dial lamps in the way, these will probably fail also. A similar short in the output valve may or may not blow the heaters, only cause them (rectifier and output only) to glow brightly.

## Common faults

Now let us consider a few of the more common complaints and their cures. One of the most common is hum. Tackling this in a set with series heated valves is a little different from a set with parallel heaters. In the latter case one tends to reach for an electrolytic capacitor of adequate voltage rating, usually 350 V or more, and connect this across the HT line in one of two places, reservoir section to chassis or smoothing section to chassis, to see which section is at fault. The series heated chain does add the probability of heater-cathode leakage so that although the test electrolytic capacitor can still be tried, one is not surprised if there is no difference. The next step is to see if the hum continues with the volume turned down. If it does, it is reasonable to suspect that the output valve (probably a UL84 or UCL82) has heater-cathode leakage or is drawing grid current, the net result being the same. So change the valve.
If the receiver uses a printed panel, there is the added possibility of leakage across the surface of the panel or through it. The affected area will usually


-set manufacturers often seem more concerned with appearances-
be blackened and a little cutting away of the plastic, perhaps combined with replacing the affected tracks with wire, may have to be resorted to. Set manufacturers seem often more concerned with appearance than efficiency and mount resistors close up to the panel with the leads cut short. Replacements should be made with longer leads so that the resistors stand well up off the panel, however ugly this may appear. Resistors, like politicians, should be open and above board!
Do not omit to check the grid resistor of the output valve which sometimes goes high particularly if the valve has been drawing grid current. A grid leak resistor of say $1 \mathrm{M} \Omega$ or $470 \mathrm{k} \Omega$ can often rise to many megohms leaving the grid floating and humming away to itself. Quite often the hum varies with the volume control setting and this means we have to look back to the preceding stages. Usually either the IF amplifier, say UF89, or the frequency changer (UCH81) is at fault and the latter, being more expensive of course, is usually the culprit!

## No results

One of the most common complaints is that the valves light up but there is precious little other activity. The usual reason is that the smoothing resistor has failed but one must not assume this. The output transformer could have an open circuit primary or there may be no supply to the rectifier due to an open circuit surge resistor ( RI in Fig. 1), perhiaps little Johnny has moved or unscrewed the internal loudspeaker muting devices on the external speaker panel.(you did it, but blame Johnny anyway).

So we must proceed logically. If there is a fine upstanding dropper it is no trouble to check all sections with a neon when the set is on or an ohmmeter when the set is off (if you're too lazy to switch the meter to the AC range and check the voltages on the dropper tags with the set on). Many sets did not use a single dropper however and the surge limiter may be a separate wirewound resistor
mounted in a more inaccessible position. If the value cannot be read it can be assumed to be in the region of $100 \Omega$. If a printed panel is used, the resistor may be intact but it could have parted company with its print beneath.

Assuming the rectifier is receiving its supply however, there should be HT on at least one of the main electrolytic capacitor tags. If there is a good voltage on one but not the other the smoothing resistor (or choke if it's an older set) could well be open circuit. The value of this will depend upon whether it has to pass the total HT current. Quite often, the output transformer primary is directly connected to the rectifier and therefore the anode current of the output valve does not pass through the smoothing resistor. In this case the value may be quite high, say about $3 \mathrm{k} \Omega$. If the voltages are ok at both the smoothing tags, check the voltage at the anode of the output valve. If output transformers have a bad habit it is that they go open circuit on the winding which feeds the anode! This means a new transformer. If an exact replacement is not to hand an alternative can be used, the important thing being that the correct impedance matching is maintained. Very generally speaking, a small battery output valve requires a high impedance, the normal type of valve encountered in mains operated sets a medium impedance, whilst a low impedance is only required for more high powered amplifier type valves (and output triodes if you can remember that far back).

-a hefty charge which can tickle you pink-
Don't forget that if there is no discharge path through the HT line, the reservoir capacitor can be left with a hefty charge which can tickle you pink if you let it! The capacity is not that used in TV receivers (about 100 to $300 \mu \mathrm{~F}$ ) which can really cause a spark but even a $32 \mu \mathrm{~F}$ on a 300 V line can pack a punch which is not to be sneezed at!

The Thorn group made a large number of models with the " $U$ " series of valves on a printed panel where not only the smoothing resistor had a habit
of becoming $\mathrm{O} / \mathrm{C}$ but also parted company with its print, as did the surge resistor to the UY85 anode. These were fairly small wirewound resistors and serve as an illustration of what we have been going on about in the above text.

## The audio amplifier

Having checked the HT supply and output stage, and ensured the latter is operating under the correct conditions, with the cathode bias components in order (resistor the right value and the capacitor doing its job) check the output grid to ensure there is no positive reading. If there is such a reading, the valve could be drawing grid current, highly likely, or the coupling capacitor from the audio amplifier anode could be leaking, less likely but still a strong possi* bility. We then turn to the preceding stage which is normally either a separate triode section in the output valve or the triode section in a valve like a UABC 80 (three diodes and a triode in one envelope). The only component likely to require attention is the anode load resistor which is normally about $220 \mathrm{k} \Omega$. This does tend to "go high" producing loss of volume and a peculiar form of distortion (stressing the sibilants, you could say). This is no trouble as the voltage at the anode will be very low and this itself suggests the resistor is the primary subject.

A low voltage need not be due to the resistor and if this proves to be of correct value, attention should be directed to the control grid. This is normally biased by a high value resistor of up to $10 \mathrm{M} \Omega$. If the coupling capacitor (the charge on this determines the bias with the resistor) is leaky, the bias is cancelled and the valve draws too much current. The voltage drop across the anode load is therefore excessive and is responsible for the condition. Some receivers do use cathode bias, and where this is so the cathode capacitor could be shorted, or the grid coupler could still be leaky, but most receivers have the cathode directly coupled to chassis as this simplifies the design.

Most sets have the volume control feeding the control grid and if the coupling capacitor is leaky the position of the control will vary the distortion to an extent. Which of course brings us to the vexed subject of noisy controls. Usually a squirt of cleaning fluid into a convenient gap in the housing will bring the control to heel but it is sometimes difficult to find or make a gap. The construction of the control either makes this operation very easy or very difficult and it is sometimes necessary to partially strip it or replace it completely. The control itself is not always responsible however and associated capacitors should be checked for leakage as control tracks do not take kindly to the passage of DC current. This is particularly so in the case of some makes of unit audios and radiograms of more recent origin but since these are transistorised this thorny subject will not be pursued further.

## The IF stage

The detector and AGC circuitry in valved receivers very rarely gives trouble so we may be forgiven for nipping smartly past these and delving into the IF stage. Once again this can be quite simple, with the cathode chassis connected and the control grid biased from the AGC line. Note that valves are always reversed biased, i.e. the control voltage pushing the
valve toward cut-off and is therefore negative-going. The HT supply to the anode and screen is via a decoupling resistor of some $1 \mathrm{k} \Omega$ with a capacitor to chassis of from 0.047 to $0 \cdot 1 \mu \mathrm{~F}$. This decoupling point can be the screen pin of the valve base with a short lead to the IF transformer primary, or to the latter point with a short connection to the screen pin.

Separate supplies are often used so that the screen grid of the IF amplifier can be connected to the same electrode on the frequency changer base and two resistors are often used as a potentiometer to hold the screens steady, typical values being say $22 \mathrm{k} \Omega$ from HT to the valve base with a $47 \mathrm{k} \Omega$ to chassis. As the majority of the current passes through the upper resistor, $22 \mathrm{k} \Omega$, this is often the one to change value and thus drop the applied voltage. This is sometimes the cause of the complaint, "My radio has been getting weaker and weaker and now you can hardly hear it".
Instability is another common disorder and this can vary from whistles and screeches to non-operation due to the paralysing effect of the AGC being overloaded by the instability. This can be a trifle tedious to overcome and the normal remedies are not always effective. The usual first step is to try bridging the decoupling capacitors with a test $0.05 \mu \mathrm{~F}$ or similar. Bridging from screen to chassis may stop all complaints right away and you then go on your way rejoicing. But more extensive checking around may have to be resorted to, bridging other capacitors associated with the IF and frequency changer stages, the AGC line and the HT line. If none of these efforts produce results, check the alignment of the IF transformers, the valves, earth contacts (especially if these are riveted) and the main electrolytics.

## Frequency changer stage

For AM reception this is usually a conventional triode heptode such as a UCH81. The complaint of no normal reception with, perhaps, some background mush is often the result of the valve becoming defective and refusing to oscillate (triode section). When it is oscillating there should be a negative voltage on the triode grid. If this is absent a new valve will usually put things right. If it doesn't, a general check up on the capacitors and resistors, comparatively few in number, associated with the section will usually restore signals. A defective coil is sometimes difficult to locate if it is suffering from shorted turns but with a bit of luck the trouble may be the result of a badly soldered lead-out or even an open circuited lead-out which can be repaired.

The mixer section is similarly wired to the IF amplifier and the same remarks apply regarding resistors changing value, leaky decoupling capacitors and the like. It varies in the arrangement of the control grid which is blocked from the aerial coils as a rule with a fairly low value capacitor, say 100 pF , and with a fairly high value resistor connecting to the AGC line.

The aerial circuit may consist of a ferrite rod on which is mounted the tuning coils with leads to the tuning gang, the wavechange switch and chassis, but there are infinite variations on this theme. If there is no ferrite rod (the design is older) there is usually a cluster of coils around the wavechange switch and an open circuit on one may result in the others being put out of action. They are probably slug tuned for padding with separate trimmers for lining up the high frequency end of the scale. Where ferrite rods
are fitted the actual rod is the slug and the position of the coils on the rod is varied for padding on the low frequency end of the scale.

## VR퐆N

Receivers with these facilities have a separate section due to the higher frequencies involved. The aerial input can conveniently be a half-wave dipole made simply by opening up a piece of twin flex to the required length and stapling this in the cabinet. This is all very well in some areas but if serious listening is demanded a more elaborate system is needed with the correctly matched down lead, $75 \Omega$ coaxial on most UK stuff, $300 \Omega$ balanced twin on imported, as a rule. We will not go into the pros and cons of these different inputs here as they are pretty well known and have been discussed at length in previous issues.

The aerial input is taken to the tuning coils and thence to the first section of a double triode, as a rule, say a UCC85. The second half functions as an oscillator. Nine times out of ten replacement of this valve will restore normal signals if these fail suddenly, the tenth time being the result of defective resistors or capacitors. The actual tuning may be carried out by separate sections on the gang capacitor or by varying the position of the slugs in the aerial and oscillator coils. The output of this usually small section is fed to the IF stages, there may be more than one, through separate transformers to a ratio detector. The two diodes involved in this latter operation may be in a valve envelope (as in the UABC80 for example) or separate germanium or silicon diodes if the valve line-up does not include such a valve.


Fig. 2. AC-only sets have the conventlonal mains transformer with the valve heaters in parallel.

## C-only sets

The advantage of using a mains transformer is that the valve heaters can be wired in parallel (all at the same low potential) so that the stress between the cathode and heater is largely removed, and that the chassis can be isolated from the mains. Note we said, "can be." Some receivers sacrifice this advantage
on the grounds of economy. Some transformer supplied sets use a series chain of heaters but this is all a matter of design considerations.

Some pretty weird and wonderful sets were imported some years ago using difficult valves which did tax one's resources but this is a story of its own which we may relate on another occasion. The average type of AC mains set which is likely to be encountered and which is probably worth renovating will have a transformer supplying a full wave rectifier and valves having 6.3 V heaters (possibly 5 V for the rectifier heater). The rectifier may have between 250 and 350 V applied to its anodes from a centre tapped winding, the centre tap being chassis connected. The output of the rectifier is taken to the reservoir capacitor which may have a value of between 8 and $32 \mu \mathrm{~F}$. The circuit is then much the same as that previously described, using a smoothing resistor, a choke or part of the output transformer before the smoothing capacitor. The rectifier valve may be directly heated (cathode is the heater) which has a very fast warm up or indirectly heated (separate cathode) which warms up and becomes operative with the other valves. The latter imposes less stress on the capacitors, Fig.2.

-old timers which really need tracking down-
If a rectifier valve is difficult to obtain and it is decided to wire a couple of silicon diodes across the base, this stress must be recognised as the switch-on surge may be greater than the rating of the capacitors, To avoid this the inclusion of a thermistor between the rectifier output and the reservoir capacitor will add to the long term reliability of the receiver.

Valves such as the EZ80 and EZ81 are still generally available and should be used whenever possible. Older types such as the EZ40 and the like need a bit more finding but it is the old timers like the 5Z4 and 5Y3 which really need tracking down and it is here that the diodes may have to be used.

Little need be said about the other stages. They follow the lines already discussed but one is more likely to find different output stages in higher priced radiograms etc. For example, a cheaper type may use a single EL84 (or ECL86, for example) for each
channel if the instrument is stereo whilst higher quality grams which are more likely to be worth saving may have four such valves, two in push-pull for each channel. The complication arises not only in the output transformers but in the drive from the audio stage to the output pair. An output transformer primary may have five lead outs, HT to the centre tap, a tap for each screen (this provides a degree of feedback) and the outer taps for the anodes.

Valves in push-pull need differing grid drives so that some form of phase splitter is necessary. A common method is to use a triode suspended midway between the HT line and chassis with one output valve driven from the anode and the other from the cathode (when the anode is positive going, the cathode is negative thus providing the "I push, you pull' requirement). This in turn means that the grid of the triode is returned to cathode at a fairly high potential. There are so many variations on this theme that detailed description is impractical, at least in this article, so that one should not be surprised if the voltages in the driver stages appear abnormal. Stereo does at least supply us with a ready made comparison circuit so that if one side is working well we know what to expect in the side which isn't. Get the voltages right and most else falls in line. Where they are wrong, check the resistors for correct value and the capacitors for leakage. Then suspect the valves.

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'Direct response advertisements, display or postal bargains where cash had to be sent in advance of goods being delivered", Classified and catalogue mail order advertising are excluded.

## ON RECENT DEVELOPMENTS

## NOSEY!

Electronic noses have been around on the Amateur construction scene ever since suitable sensors became available. These, however, have found most use in such applications as fire/smoke detection etc.

A Watford company has managed some success with an explosives detector. It's called the unassuming name PD2, weighs a mere 22lbs and lives in an innocent-looking suitcase. The unit gives a positive response when explosives are detected. An audible alert sounds immediately after taking an air sample containing explosive vapour. The unit is so sensitive that it is able to detect the tiniest traces of explosives such as those which might be found on a persons hands after handling ex-plosives-or on their clothing. The photograph shows a security officer checking a bag. If you want one of these units the UK price is around £2,150. Probably not a high price for something that nose what it's about.

## THE 'CHIT'

The NRDC (National Research Development Corporation) has encouraged many good ideas and another has just found its way into my hands. It's called CHIT, standing for CHeap Input Terminal and was developed at the National Physical

Laboratory. The approach used is quite ingenious. Two oblong lengths of resistive material are laid one on top of the other.

When a point (a pencil) is used to draw or write on the top oblong, the pressure causes the air gap between the two resistive surfaces to decrease and the two oblongs make contact at the point of impact. Electrodes are connected to each of the oblongs at their ends and when a current is passed through one of the oblongs, a uniform voltage gradient is developed along its entire length. The voltage at the exact point of contact i.e.: wherever the pencil tip happens to be pressing at any given instant in time, will be proportional to the pencil point's position on the $x$ axis. The other oblong is used as a sort of wiper of a potentiometer and will attain this voltage. The two oblongs are switched, electronically, so that first one oblong is acting as a position indicator and the other the wiper of a pot, then the roles are reversed due to the electronic switching. Thus the point can be monitored in both $x$ and y axis.

Using this method as an input terminal, handwritten characters can be transmitted, signatures verified, line drawings, circuits etc can be transmitted. Perhaps it won't be too long before you will write a letter on such a device and it will be transmitted at the same instant and received immediately. We seem to


[^1]have come a long way since the Penny Black back in 1840. If it comes, it could mean that many postmen will be looking for a new post-do you see?

## FLAT TV SCREENS

From time to time 1 have made comments about flat screen television "tubes". 'Research and development has been going on in this area for some time and the latest effort to come to my attention looks very promising. First, the US Airforce is going to try out the ideaand believe you me the American military do not waste time on impractical ideas no matter how clever they might be. The device is the brainchild of Hughes Aircraft who have vast expertise in many areas not the least of which is electronics. Some 18 months ago Hughes brought out a lin ${ }^{2}$ liquid crystal display which was capable of showing a television picture. The company successfully deposited a number of liquid crystal picture elements on a piece of silicon which also contained the excitation circuitry. Manufacturing defects caused problems but once these were overcome Hughes steamed ahead. Now, four on the lin. miniature "tv screens" have been butted up together to form a $2 \times 2 \mathrm{in}$. display comprising a $100 \times 100$ cell array.

It has been rumoured that the US Airforce has shown great interest in using the new approach for things like scan-converted radar, forwardlooking infrared and possibly in head-up displays for gun aiming. In sunlight, it's difficult to see the cathode ray tube type of display whereas the LCD component is reflective and thus thrives in such conditions. Another distinct advantage is that crts commonly required high voltages-often thousands of volts. The LCD array requires only 25 V . Plans are already afoot to produce a larger array and it is easily technically feasible.

## Avessatile  comnonent! DIGITAL FREQUENCY <br>  METER <br> You'll probably find that you have a lot of the components already! An interestimg constructional project which will give much satisfaction when it's completed. Readout to, typically, 27 MHz or more depending upon the IC's used. Gate times of $100 \mu s$ to Is. Input 50 mV to 10 V and time intervals Ims to 9999s.

## PTalking Transistors

-getting to know how they work



MORE and more people these days are taking an interest in making their own music and to that end electronics is playing an everincreasing part. Witness the number of constructional articles that have appeared for synthesisers, organs, electronic pianos, musical boxes, guitars etc. An essential part of most music is rhythm and what

| CODE |  |  |  | Snare/ Claves | RHYTHM |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input 8 | Input 4 | Input 2 | Input 1 |  |  |  |
| 1 | 1 | 1 | 0 | S | Waltz | 3/4 |
| - 1 | 1 | 0 | 1 | S | Jazz Waltz | 3/4 |
| 1 | 1 | 0 | 0 | S | Tango | 2/4 |
| 1 | 0 | 1 | 1 | S | March | 2/4 |
| 1 | 0 | 1 | 0 | S | Swing | 4/4 |
| 1 | 0 | 0 | 1 | S | Foxtrot | 4/4 |
| 1 | 0 | 0 | 0 | S | Slow Rock | 6/8 |
| 0 | 1 | 1 | 1 | S | Pop Rock | 4/4 |
| 0 | 1 | 1 | 0 | S | Shuffle | 2/4 |
| 0 | 1 | 0 | 1 | C | Mambo | 4/4 |
| 0 | 1 | 0 | 0 | C | Beguine | 4/4 |
| 0 | 0 | 1 | 1 | C | Cha Cha | 4/4 |
| 0 | 0 | 1 | 0 | C | Bajon | 4/4 |
| 0 | 0 | 0 | 1 | C | Samba | 4/4 |
| 0 | 0 | 0 | 0 | C | Bossa Nova | 4/4 |
| 1 | 1 | 1 | 1 | - | No selected |  |

Fig. 2: Table of Rhythm selectlon input codes. Thls table may be cut out and stuck on the facia of the unit.


Fig. 1 : Basic block diagram of the Rhythm Ger


[^2]better method of turning a solo performance into a duo than with the addition of a drummer and full drum kit all contained in a box measuring little more than $205 \times 152 \times 102 \mathrm{~mm}(8 \times 6 \times 4 \mathrm{in})$ ! In addition such a portable unit could well provide the rhythm section for a small group or a novel gimmick on the disco scene.

This article describes the construction of a Rhythm Generator containing nine percussion instruments which can be programmed to play any one of fifteen different rhythms. Emphasis has been placed on simplicity of construction and low cost without sacrificing the faithful reproduction of the sound of each instrument. Anyone who has had some experience of soldering and knows one end of a diode or electrolytic capacitor from the other, should, with a little care and patience, be able to make this unit. Several MOS (Metal Oxide Semiconductor) integrated circuits are used but for those who are not familiar with the handling of this type of device full instructions will be given. In the meantime do not be tempted to remove them from the protective conducting foam packing.

## Generator block diagram

Fig. 1 shows the block diagram for the Rhythm Generator. The heart of the generator is the M252AA MOS integrated circuit manufactured by SGS-ATES. This device incorporates a memory programmed with fifteen different rhythm patterns which are selected by a 4 -bit binary code. The four code inputs are designated IN8, IN4, IN2 and IN1 each one capable of being switched to ' 0 ' (i.e. ' 0 ' $V$, switch closed) or ' 1 ' (i.e. +5 V , switch open) by S3, S4, S5, S6 respectively. Thus $16\left(2^{\frac{1}{2}}\right)$ combinations are possible, fifteen of which are used to programme the following rhythms:- Waltz, Jazz Waltz, Tango, March, Swing, Foxtrot, Slow Rock, Pop Rock, Shuffle, Mambo, Beguine, Cha Cha, Bajon, Samba and Bossa Nova. Details of the particular codes are given in Fig. 2 with code 1-1-1-1 having no selected rhythm.

The chip is driven by a square wave from the


Fig. 3: Block diagram of the M252AA Rhythm Generator. Rhythms are selected by applying either a logic ' 1 ' or ' 0 ' to the input gates of the IC.
clock generator, the frequency of which determines the tempo of the rhythm. Once a code has been selected the various instruments are triggered in the correct sequence to provide the particular rhythm pattern. Only eight of the nine instruments are used at any one time, the snare drum being manually selected by S2 for the Waltz, Jazz Waltz, Tango, March, Swing, Foxtrot, Slow Rock, Pop Rock and Shuffle whilst the claves are used for the remaining South American rhythms. The outputs from the instrument simulators are combined and fed to a preamplifier incorporating volume and tone controls.

A down-beat indicator in the form of an LED is included to mark the beginning of each rhythm pattern. A combined stop and reset facility (S1) allows the generator to be stopped and restarted at the beginning of a bar. This feature permits the rhythm to be brought in on the down-beat after the introduction to a piece of music has been played. To make this easier while playing, a socket has been provided wired in parallel with the stop switch Sl on the panel, so that a foot operated switch may be connected.

## The M252 Rhythm Generator

The internal operation of the M252 IC is shown in Fig. 3. The clock input is first divvided by two and this output drives a 5 -stage counter which resets every 32 pulses for rhythms of $4 / 4$ time and after every 24 pulses for $3 / 4$ time. The counter states are then decoded to drive the ROM (Read Only Memory) matrix which has been pre-programmed with the fifteen different rhythms. The binary code that has been entered to select a rhythm is decoded and used to determine the reset point of the counter and to programme the multiplexer to select that
particular rhythm from the output of the memory matrix This output is then fed to the driver circuit which modifies the pulses to make them suitable for triggering the percussion instruments. The output section also includes logic circuitry to reset the memory outputs to zero after each reading so that the output will always be able to provide the correct trigger edge during the following beat.

The internal reset pulse of the counter is routed to an output connection (pin 7) which, with the addition of a blocking diode to separate the signals, can furnish the down-beat indication 'as well as allowing the external resetting of the rhythm.

## Clock Generator

The clock generator circuit, see Fig. 4, is a simple astable multivibrator utilising two 2 -input NAND gates (IC2b and IC2c) together with the timing components R3, VR1 and C1 to provide a square wave output to drive the M252 chip. By closing the STOP switch (S1) the clock is inhibited with its output remaining at " 1 " and at the same time the M252 is reset via IC2a and D1. Upon opening the switch the output immediately goes to ' 0 ' thus generating the first command pulse and the rhythm commences with the first beat of the bar i.e. the down-beat.

The frequency of the clock may be continuously varied from approximately 5 Hz to 50 Hz by the tempo control VR1. The relationship between the clock frequency and the rhythm tempo is given by the following formula:-

No. of bars/min $=$
Clock frequency $x$ No. of bars per rhythm pattern $\times 60$
No. of counts per rhythm $\times 2$


Fig. 4: Part of the circuit containing the clock generator, downbeat indicator, snare drum, long cymbals, short cymbals and maracas. These

# The Black Watch kit 

 £14.95! * Practical-easily built by anyone in an evening's straightforward assembly. * Complete-right down to strap and batteries.* Guaranteed. A correctlyassembled watch is guaranteed for a year. It works as soon as you put the batteries in. On a built watch we guarantee an accuracy within a second a day-but building it yourself you may be able to adjust the trimmer to achieve an accuracy within a second a week.


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Runs on two hearing-aid batteries (supplied). Easily re-set using special button-no expensive jeweller's service.

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The heart of the Black Watch is a unique IC designed by Sinclair and custom-built for them using state-of-the-art technologyintegrated injection logic.
This chip of silicon measures only $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ and contains over 2000 transistors. The circuit includes
a) reference oscillator
b) divider chain
c) decoder circuits
d) display inhibit circuits
e) display driving circuits

The chip is totally designed and manufactured in the UK, and is the first design to incorporate all circuitry for a digital watch on a single chip.

... and how it works
A crystal-controlled reference is used to drive a chain of 15 binary dividers which reduce the frequency from $32,768 \mathrm{~Hz}$ to 1 Hz . This accurate signal is then counted into units of seconds, minutes, and hours, and on request the stored information is processed by the decoders and display drivers to feed the four 7 -segment LED displays. When the display is not in operation, specia! power-saving circuits on the chip reduce current consumption to only a few microamps.

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$\qquad$
$\qquad$


$\star$ components list


$\xrightarrow{\text { Output }}$


Fig. 5: Basic circuit of a damped sinusoidal oscillator, comprising a 'Twin-T' ringing oscillator utilising a NAND gate.

For rhythms of $4 / 4$ time and for the March and Tango the number of counts per rhythm pattern is 32 , each rhythm pattern covering two bars. The tempo is thus variable from approximately 9 to 94 bars $/ \mathrm{min}$. In the case of rhythms of $3 / 4$ and $6 / 8$ time the counter resets after 24 pulses and there are two bars per rhythm pattern giving a tempo from 13 to 125 bars $/ \mathrm{min}$.

The Shuffle, $2 / 4$ time, has four bars per rhythm pattern and resets after 24 pulses giving a variation of $25 \mathrm{bars} / \mathrm{min}$ to $250 \mathrm{bars} / \mathrm{min}$ which is twice the tempo of the Waltz and over $2^{1}{ }_{2}$ times that of the $4 / 4$ rhythms, for the same setting of VRl. It is for this reason that the tempo control covers such a wide range and will need adjustment especially when

Fig. 6 : Circuit diagram left shows the five ringing oscillators for bass drum, high and low bongos, claves and conga drum. All five circuits feed into a common pre-amplifier.
The circuit below shows the various power requirements for the IC's

changing to the Shuffle. To facilitate the exact setting of the tempo, control knobs of the type with a graduated skirt are recommended.

The internal reset pulse of the generator chip is only 2 to $3 \mu \mathrm{~S}$ long so it is too short to light a lamp. It is also necessary that the lamp should light on the negative edge of the reset pulse which occurs at the beginning of the bar. The down-beat monostable circuit, see Fig. 4, comprises C2, C3, R4, R5, R6, R7, IC3a and IC3b. It lengthens the short downbeat trigger pulse to around 350 mS by latching the output of IC3b to ' 0 ' until C3 has charged up to above the " 1 " input trigger level of IC3a. It operates on negative-going pulses only and the resulting ' 0 ' output from IC3b is inverted by the NAND gate IC3c to switch on Trl thus lighting the LED.

## Percussion Instruments

The percussion instruments may be divided into two categories, those that consist of damped sinusoidal oscillations and those consisting of damped filtered white noise. In the first category are included the bass drum, high bongo, low bongo, conga drum and claves. The general circuit shown in Fig. 5 consists of a simple twin-T ringing oscillator utilising a NAND gate which is adjusted to a point slightly below oscillation by VRla. The different sound of each instrument is achieved by choosing the correct values of C2a and C3a to determine the required frequency of operation and by regulating its decay time (damping) by VRla to obtain longer or shorter sounds.
The trigger pulse from the M252 is a square wave which must be differentiated by Cla and R2a and allowed one-way entry by diode Dla to produce a short pulse which is sufficient to set the oscillator ringing but not to interefere with the damping of the oscillation. Resistor Rla is necessary to keep the input at earth in the absence of a command pulse since the outputs of the M252 are open drain types.
Fig. 6 shows the circuit of the five ringing oscillators used and gives values for the three frequency determining capacitors for each instrument. The tolerance of these capacitors is not too critical but it should be kept within $20 \%$, which is reflected in the types specified in the component list.

However, a problem does exist in the case of the high and low bongos. The frequency of operation and therefore the capacitor values of these two instruments is very close and $10 \%$ tolerance has been specified in this instance. This still means it is possible in an extreme case that the frequencies of operation could be identical and if this does occur $5 \%$ types may be substituted to overcome the problem.

In the second category falls the long cymbals, short cymbals and maracas, for which the basic type of circuit is shown in Fig. 7. Transistor Trlb is switched on during the short trigger pulse from the M252 chip and charges C2b. This capacitor then discharges through R4b to the base of Tr3b. The white noise produced by Tr2b by the zener effect of the reverse biased base-mitter junction is also applied to the base of Tr3b via C3b. During the discharge of $\mathrm{C} 2 \mathrm{~b}, \mathrm{Tr} 3 \mathrm{~b}$ can amplify this noise. The degree of amplification, however, follows the discharge curve of C 2 b and therefore a damping of a variable length is obtained depending on the values of C 2 b and R 4 b . The inductor Llb and the capacitor C4b allow selective amplification of certain frequencies to obtain a more realistic sound of the instrument being simulated.

The distinctive metallic sound of the snare drum caused in the real intrument by catgut snares stretched across the drum-head is realistically simulated by combining filtered white noise from this circuit with high bongo. The long cymbal and short cymbal circuits dispense with Trlb and differ only in decay time. The maracas simulator is unusual in that it is the only instrument in which the sound increases gradually and then decays. This effect is achieved by means of an integrator-differentiator circuit D4, D5, R19, R20 and C8, see Fig. 4.

## Pre-amplifier

The outputs of the nine instruments are mixed and fed to the input of the pre-amplifier through the preset potentiometer VR9, Fig. 6. The active element of the amplifier is the ubiquitous 741 op.amp used in the non-inverting mode. A simple variable low-pass filter, C35 VR10, acts as a tone control and the output level is adjustable by means of the potentiometer VR11.

PART 2, to be published next month, will cover details of the power supply, PCB's, construction and setting-up.


MORE


## THE FLASHER

If it's escaped your attention, the LM3909 chip is well worth looking at if you need some form of flashing light. In its simplest form the IC needs only a 1.5 V battery and a suitable capacitor to make a flashing light which will keep going for a very long time-like two years with an akaline cell. One useful circuit suggested by the manufacturers is to mount the chip, I.e.d. and capacitor into the base of a torch. The tiny flashing light can be seen in the dark making it easy to always find your torch. Ideas for toys, models etc. come readily to mind and I reckon that this IC will fast become a favourite with amateur constructors.

## LIQUID CRYSTAL PICS.

Electronics and photography have always been close allies for the hobbyist. Of interest to both will be the work being carried out at the Hughes Aircraft Company. Researchers there are working on what they call a light cell. The idea is to enhance the image being reproduced. To do this photographically is not so easy, and present electronic solutions are not ideal.
The Hughes approach is quite ingenious. The light from the desired image (i.e. the varying tones formed by the brightness of the light in the various parts of the image) is allowed to strike a cadmium-sulphide layer which modulates the resistivity of the photoconductive layer. This in turn varies the voltage which is applied to a liquid crystal layer. The characteristics of the liquid crystal can be altered thus giving control over the image which is finally transmitted. Resolution is presently 60 lines/millimetre and the device requires only 6 V .

## COMPUTER-FACILITY FOR $£ 7.50$

A new general-purpose microprocessor shortly to be introduced by National Semiconductor, and priced around $£ 7 \cdot 50$ in quantity lots, is expected to generate keen interest in present users of Random Logic.

SC/MP is an 8-bit PMOS microprocessor operating at 2 microsec cycle time and requiring only a single 12 V supply with a useful margin of $\pm 2 \mathrm{~V}$. It generates its own timing on the chip, and will be ideally suited to simple control and timing functions.

Designers working with appliance controls, building monitors, fuelinjection units, traffic signal control, word-processing systems, electronic toys, etc. will find the SC/MP right in both design and cost, claims N.S.

Multiple SC/MP can communicate with each other when they share a common bus. Logic on each chip senses when the bus is in use, so when one SC/MP ceases transmission (or reception) the next can take over. If it declines, the next but one is invited.
A simple control system can be developed using one SC/MP and a programme memory-which can be selected from a wide range of standard memory parts. Such a system could access up to 4 kilobits of memory and could provide the control logic for simple industrial systems, TV games, small traffic-control systems, etc.

## I.R. HEADSETS

A recent development in the West German colour television market has * caused quite a stir among other europeans. Apparently infrared audio headsets are now becoming in-
creasingly common as a standard fitment to the receivers. Another application of the infrared audio. system is to teach children whose hearing is impaired. The infrared is transmitted to a minute IR receiver which is an integral part of the headphones thus leaving one free to move about anywhere within the range of the IR beam. One German company is readying a two-channel stereo transmission system. The signals for each of the two channels is modulated onto two separato carriers. These are set at 200 kHz and 280 kHz . These frequencies are then transmitted via the infrared beams.

## VIDEO DISCS

The video home-player scene has taken on a new look. A large French company recently confessed that it is going into production with an inexpensive optical video discplayer. What is interesting is that the company, looking some years ahead, sees the distinct possibility of cheap throw-away video discs which will be sold at newsagents just like magazines.

## GAMING CHIPS

In a previous issue (Hotlines, Practical Wireless, March 1976) I mentioned tv games. US semiconductor giant Fairchild has announced that it is going into this area in a big way. Plans haven't been completely revealed as yet but it would seem promising for the home constructor if this company were to start manufacturing chips specifically designed for things like tele-tennis, tele-football etc. Please note; they haven't started making them so don't look for ICs yet a while.


## OUR CQ "COLUMN"

If you wish to have a "CQ" request in Practical Wireless, we would be grateful if you could write it out in the same style we print it. This helps us to help you by saving time trying to take extracts from long letters and deciphering names and addresses.

Thank you.

Please mention

# PRODUCTION LINES colini rictes 

## ITT SOUNDERS

ITT are marketing a range of piezo ceramic sounders. The smaller ones shown in the picture comprise a thin piezo-electric vibrator and solid-state oscillator. One very special feature of the units is their exceedingly low power consumption with high sound pressure level.

The circular device at the top left of the photograph is Model U250RDID2H which gives a continuous short pulsed or long pulsed tone facility from 24 V . Operating voltage is $5-35 \mathrm{~V}$ at 10 mA with an oscillating frequency of 2.7 kHz . Sound level is over 90 dB . The small black sounder (centre)-the U5-35R runs at 4 mA with a continuous tone only. Output is over 70dB. The bottom left unit (U1-50RD2) has continuous or long pulsed tones and runs on 12 V at 10 mA . The bottom right unit (U3$5 D R$ ) is a 24 V continuous tone sounder which draws 8 mA .

The sounders make very good alarms for use inside the home i.e. they could be wired to fire alarms, smoke detectors, mains failure alarms for freezers etc. etc. and their very low current consumption makes them ideal for this purpose.
The horn-type sounder RHA 102 (top right) is a real "ear-splitter" which incorporates a sensitive drive unit and solid-state oscillator amplifier. Two separate tones are pro-vided-warble at $1200 \mathrm{~Hz}-1700 \mathrm{~Hz}$ at 180 c.p. minute, and continuous 1000 Hz , and these can be used individually by connecting the appropriate pair of wires to the 12 V d.c. supply. Current consumption of this model is 400 mA and it pushes out 98 dB of noise making it eminently suitable for applications where warning signals are required e.g. fire and intruder systems, factories, hotels, vehicle alarms and so on. Prices, not yet fixed are believed to be quite reasonable. Further gen by sending a stamped addressed envelope to Mr. K. W. Stanton, ITT Components Group Europe, Standard Telephones and Cables Ltd., Materials Division, (Dept. P.W.) Edinburgh Way, Harlow, Essex SM20 2DE. Phone Harlow 26811.

## BENCH GRINDERS

Industrial power tool manufacturers, Wolf Electric Tools Ltd., have introduced two new 5 in ( 125 mm ) Bench Grinders to complement their 6in. and 8 in . industrial model range. The new machines are designed for light industrial and home workshop use and those of you who are still of the "Chassis bashing fraternity".

Model 8252 is fitted with an 80 grit fine grinding wheel and a 60 grit coarse wheel while the more versatile model 8159 is fitted with a 80 grit grinding wheel and an 8 mm chuck, enabling its use with small accessories for polishing, sanding etc.


Both models are supplied with adjustable tool rests and eye protection for grinding work. Recommended price of either model is, $£ 41 \cdot 95$, excluding V.A.T. Wolf Electric Tools Ltd., (Dept. P.W.) Station House, Harrow Road, Wembley HA9 6TJ.

EQUIPMENT CASES

H.M. Electronics have announced two rather attractive equipment cases. Model DC. 1 (with the sloping front) which, say the makers, was designed with digital clocks in mind, can also be used for mixer units, electronic dice or some of the many projects published in our pages. The second case is the Mini-bec case which measures 7 in $\times 3$ in. (or the decimal $178 \mathrm{~mm} \times 76 \mathrm{~mm}$ ). Both units would give home-built equipment a really professional finish for they are wellmade in aluminium with black crackle tops with teak end sections. In addition, the DC. 1 has a green front panel. Prices: the DC. 1 costs $£ 3 \cdot 75$ $+75 p$ post and packing incl. VAT and the Mini-bec is priced at $£ 2 \cdot 99+$ 75p post and packing incl. VAT. Further information from H.M. Electronics, (Dept. P.W.) 275a Fulwood Road, Sheffield S10 3BD.


## ADC ACCUTRAC

A unique electronic turntable-the "Accutrac"-operated by remote control-has been introduced by Audio Dynamics Corporation, a subsidiary of BSR' Ltd.

The Accutrac 4000, the first of three units on the market comprises three separate but interrelated component pieces; the automatic direct drive electronic turntable, a remote receiver and a hand-held cordless transmitter. From the comfort of an easy chair, listeners can programme exactly what they want to hear on a given album by selecting tracks indicated numerically on the transmitter. The message is then transmitted to the receiver, which is located in convenient proximity to the turntable and the receiver in turn activates the turntable's arm, which places the stylus precisely at the beginning of the track selected by the listener. The receiver's L.E.D. (Light Emitting Diode) winking "eye" lets the listener know that the information has been received and held in total memory.

Up to twenty-four commands can be programmed in any order required. The transmitter can also be pro-

grammed to reject, cue, repeat and clear, as well as play, in fact virtually all you have to do is to place a record on the turntable. Track selection can be determined by a quick look at the album jacket and favourite selections can be repeated over and over again without the listener even having to move an inch.
How does the Accutrac actually work? The Accutrac process begins with the logic circuitry built into the turntable, a direct drive unit. In the Accutrac system, there are electronic speed-sensing circuits within the motor itself, constantly monitoring the turntable's speed accuracy and instantaneously correcting the speed.
In a sense, Accutrac has' eyes. A tiny solid-state infra-red generator and detector is built into the special ADC LMA-1 cartridge (an advanced version of the XLM). The generator focuses a tiny beam of infra-red light onto the record and senses the surface of the disc. Although the arm is raised, lowered and moved automatically by its own servo-motor, it always tracks the groove with perfect freedom because from the instant the stylus touches the record, the arm is totally decoupled from the servo-motor and controls.
Separate control circuits for each speed allow individual adjustment and switching from 33 to 45 rpm now involves just a simple reliable switch-no mechanisms. In order to prevent floor shake, footsteps or acoustic feedback from reaching the stylus in the groove, the arm and motorboard are suspended on springs that have been computercalibrated to provide maximum isolation and security. Price is about £300. BSR Limited (Dept. P.W.), Powke Lane, Cradley Heath, Warley, West Midlands, B64 5QH, England.
Diagram showing the infra-red $T x / R x$ (left). The Accutrac deck with remote control $T x / R x$ (below).


## 8-FUNCTION CALCULATOR WITH CONSTANT AND MEMORY ANNOUNCED BY T.I.



A new 8-function electronic calculator recently launched by the European Calculator Division of Texas Instruments Limited is designated the TI-2550-II. The new calculator features the basic five functions-add, subtract, multiply, divide, and per-cent-with an automatic constant on all five functions plus a full four-key memory (memory plus, memory minus, memory recall, and. clear memory). In addition it features the widely used slide rule calculator functions of square root, square and reciprocal. Recommended retail price of this new calculator is $£ 29.95$ inc. V.A.T. and accessories.

The "reverse key" is especially useful to divide the quantity in the memory by the quantity in the display. The square root, square, and reciprocal keys operate only on the displayed quantity; they do not complete any pending operation. Thus, the calculator can easily solve problems such as the square root of the sum of squares without using the memory.

For maximum readability, the negative sign is always displayed immediately to the left of the first displayed digit. A ninth character on the extreme left of the display is used to indicate a quantity stored in the memory as an error and overflow indication.

Packaged in a 5.8 by 3.2 by 1.25 in . ( $14.7 \times 8.1 \times 3.2 \mathrm{~cm}$ ) case and weighing less than 8 ounces ( 230 grammes), the TI-2550-II comes with battery pack containing two fast-charge nickel-cadmium batteries, the AC9900 adapter/charger and owner's manual. Texas Instruments Ltd., (Dept. P.W.) 165 Bath Road, Slough SL1 4AD Berkshire. Telephone Slough 35544.
adjacent to the coil, keeping the connecting leads as short as possible, thinking that these new "electrics" might cause interference to the car's radio. In the event it was possible to switch from normal to electronic ignition without any difference being noted to the general noise level on the radio. The holes in the box were drlled out to take $\frac{1}{\mathrm{i}}$. bolts, one fitted with a soldering tag to take the black chassis lead from the unit. All existing push-on tags were retained, spade tags being fitted to the leads from the unit. At any time the unit can be removed and the wiring replaced in a couple of minutes.

## ON THE ROAD

The installation instructions are very good. If more than one wire is found on the "SW" terminal of the coil all should be removed and connected to the blue wire from the unit. A short piece of insulating sleeving was fitted over each exposed connection and the wires taped together neatly. Some slack was left in the wires to allow for movement of the engine on its mountings.


Basic circuit of a capacity discharge Ignition system. There are many variations of this theme to be found.

The Herald, normally driven by the daughter of the family, was left out in the open during the cold spell and the engine started every morning after the second go on the starter plus half the usual amount of choke. This was a distinct improvement on the normal performance in average temperatures. To the reviewer this aspect of electronic ignition is most important with the consequent saving in wear and tear on the battery and the starter. Performance at speed was noticeably better, the car seeming to have more power and to run more smoothly in the 60 to 70 mph range, no doubt due to the virtual elimination of the contact breaker bounce problem at high engine speeds. There was a certain amount


The completed unit, ready for installation in the car. The switches are shown in their 'antl-thlef' positions. Electronic ignition is operative with both switches to the right and normal Ignition when they are to the left. A small neon lamp protrudes through the grommet, bottom centre, Ilghting when the unit is functioning properly.
of rough running at low speeds especially when the foot. was lifted from the accelerator. At this point no attention had been paid to the sparking plugs or contact breaker which had been in use for several thousand miles without attention other than checking the gaps from time to time.

## CONCLUSIONS

New plugs and contact breaker set were fitted and the rough running disappeared, gaps being set at the usual 25 and 15 thou respectively. Increased gap on the plugs is usually recommended with electronic ignition but this has not been tried yet. Daughter normally keeps a record of petrol bought and miles run so this was very useful in trying to assess whether there was an improvement in petrol consumption. It is unfortunate that a lot of rubbish is written about sensational improvements in this field with electronic ignition but it is seldom borne out in practice. An improvement of about two miles a gallon was found but a lot more mileage will have to be run before a definite figure could be given.

No doubt if the Herald were kept in tip-top order with frequent checks on engine performance with test equipment the electronic ignition would not make so much difference to its performance, except at high speeds, but the Herald was an ordinary car, receiving less care than it really deserves, yet it benefited considerably from the electronic ignition. Considering the price of the Bi-Pre-Pak kit it is a very good investment indeed.
The Super Spark Ignition Kit is available from Bi -Pre-Pak for $£ 9.09$ including VAT and post and packing from 222 West Road, Westcliff-on-Sea, Essex SS0 9DE.
A.E.D.


## ISSUES WANTED

..issues of P.W. (either 1969 or 1970) containing details of a short wave converter (used RCA CA3028).-W. D. Smith, 46 Santon Way, Seascale, Cumb.
. issues of P.W. containing details of mods to the 19 set (? 1960).-D. Collings, c/o Glossop School, Talbot Road, Glossop SK13, Derbyshire.
..P.W. March and April 1971. Also P.W. May 1972. S. Brown, 12 Waverley Road, Middleton, Manchester, M24 3JG.
..P.W. July 1961 and August 1961-G. Farrer, 16 Duncan Road, Gillingham, Kent.

## INFORMATION WANTED

.. manual and circuit diagram for Pye Ranger 2207V.C. Sedgwick, 38 Eaton Road, Kempton, Beds., MK42 7RP. . .on Pamphonic type 601 A, 601B (or Cossor 601 A and 601B) amplifiers.-D. Evans, 29 Malton Road, Liverpool, L25 8QU.

## EQUIPMENT FOR DISPOSAL

. 60 Practical Wireless's from 1971 to 1975, resistors, capacitors, (fixed and variable), transistors, (PNP and NPN with long leads), speakers ( 3 ohms to 35 ohms), valves (DL96, DAF types). Please send a stamped addressed envelope for a list.-J. Owens, 26 Ardd Fawr, Dolgellau, N. Wales.

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Some of those hardest hit by the general heavy increases in dry battery prices over the last few years are the "senior citizens" who live on a tightish budget and rely to such a great extent for news, entertainment and especially "company" on their transistor portables, sometimes themselves quite senior! It is, of course, possible in many cases, though not in all, to replace batteries by a small mains unit and this will soon repay its cost by savings in replacements at anything between 52 p and 85p a time. Perhaps the easiest sets to convert in this way are the portables of any vintage using the PP9 or equivalent battery, as this can usually be replaced by a mains unit of identical size, either bought complete, made up from data published, or from kits advertised or from the spares box.

Many portables, however, dating from the days before complementary symmetry in output stages, have a split secondary "single-ended" push-pull power
stage requiring a double 4.5 V battery, and since the PP11 or similar now costs 85 p, replacement is a big item in a modest budget. Here again, it is possible to buy a ready-made mains unit giving two 4.5 V outputs, but they are more expensive than the single 9 V units, not so easy to make up from the spares box, and I have never seen a kit for one.

The solution is, really, to convert the output stage of such a set from double $4 \cdot 5 \mathrm{~V}$ to single 9 V working. Even if the user then continues to use batteries, this will bring down his replacement costs by over $30 \%$ from 85 p to 52 p and of course there are cheaper 9 V mains units available and they are much simpler to make up. I recently came across an OAP faced with the problem of the expense of the P11 and I managed to convert his set from double 4.5 V to single 9 V working in what proved to be an extremely simple manner, once the PCB had been extracted from the case and examined. The set proved to have a fairly common split battery, pushpull output stage, as in Fig. 1. This had to be converted to single battery working with as little disturbance as possible of the existing PCB and the controls. In fact, it proved possible by re-soldering only two connections:-

Lead A from the speaker in Fig. 1 was cut where it entered the 4 -pin battery plug and re-soldered to point $X$ on the double pole switch at the back of the volume control.
Lead B from the speaker was transferred, on the PCB, from the negative side of the capacitor (100uF) to the positive side, at point C.
These changes thus produced the standard single 9V output stage, as in Fig. 2. All that remained was to change the battery plug from the original 4 -pin (for two 4.5 V outlets) to an ordinary 9 V type, using the cut-away top from a defunct PP9 battery. The conversion was then complete, much to the pleasure of our old friend, for whom it will now be possible, if he so wishes, for me to make up a small 9V mains unit to enable him to use his beloved portable at minimum cost.


Fig. 1, left, shows a typical output stage using two 4.5 V batteries. Fig. 2, right, is the same circult converted to operate from a single 9 V battery.


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| 200 | $7 \cdot 26$ | 80 |  |  |  |  |  |
| 250 | 8.80 | 1 - 10 |  |  |  |  |  |
| 350 | 10.59 | 1.18 |  |  |  |  |  |
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| :---: | :---: | :---: | :---: |
| 12 V | 24 V | ¢ |  |
| -5 |  | $1 \cdot 30$ | 26 |
| 1 | . 5 | $1 \cdot 58$ | 45 |
| 2 | 1 | 2.05 | 45 |
| 4 | 2 | $2 \cdot 52$ | 62 |
| 8 | 3 | 3-76 | 62 |
| 8 | 4 | 4.30 | 85 |
| 10 | 5 | $4 \cdot 67$ | 85 |
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$$
\begin{aligned}
& \text { SWITCHES } \\
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## Peter HEMINGWAY

THIS device was designed as a result of reading àn article in PW some 3 years ago (Logiprobe, by L. Cook, October 1972). The device described there was somewhat cumbersome, and prompted me to design a unit which was simpler, cheaper and more compact. The fact that this device is so simple means that it can be built into a small and very handy body, such as a felt-tip pen or as the prototype was, built into a discarded test probe.

## Circuit Details

The circuit is basically a potential divider with two LED's to indicate the current flow through their respective resistors. The value of the resistors is not too critical and can be of any value from $330 \Omega$ to $\mathrm{lk} \Omega$. However, if resistors of less than $330 \Omega$ are used, damage to the LED's may result, and if too high a value, the LED's will be too dim. As R1 and R2 must be of the same value, they should also be of $10 \%$ tolerance, and ${ }^{1} \mathrm{~W}$ so that they are able to fit into the case.
The LED's used in the prototype are 5 mm types, one green to indicate logic O (or OV ) and the other, red, to indicate logic 1 (or +1 V ). To cut the cost even more, 3 mm diameter LED's could be used.

As previously stated the prototype was built into a test probe of slightly smaller dimensions than a felt-tip pen. The drawing opposite illustrates a cross section of the unit showing the internal wiring and components. The supply leads to the probe should be terminated in a pair of crocodile clips in order that the probe can be connected to the same power supply as that used by the TTL circuitry under test.
After the probe has been tested and found to be working satisfactorily, the wires and LED's are fixed in place with a glue such as polystyrene cement or Araldite.

## Testing

A quick method of testing the probe, is to connect the supply leads to their respective terminals of a 6 V battery. If all is well, both LED's should light at half brightness (half brightness will also be displayed when the probe is connected to a point that is either floating or at an inadmissible voltage (e.g. $2 \cdot 1 \mathrm{~V}$ ). When the probe is touched to a positive terminal, D1 (red) should light, and similarly when the probe is touched to the OV terminal, D2 (green) should light.
If these results are not obtained it is probably due to the fact that one or both diodes are connected the wrong way round.


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Number 58

## Motorola MC1312P Quadraphonic decoder

TTHE Motorola MC1312P and MC1313P are 14-pin dual-in-line devices which have been especially designed for decoding the two composite signals from quadraphonic records into the four separate audio channels. The matrix system used in these devices is suitable for use with inputs encoded on the "SQ" system which was developed by the Columbia Broadcasting System and which is now used by most of the large recording companies. It is also suitable for the decoding of SQ quadraphonic broadcast programmes, but it remains to be seen whether such material will be transmitted in the UK.

## THE TWO DEVICES

The MC1312P is designed for home entertainment applications and introduces less harmonic distortion, typically $0.1 \%$, than the MC1313P, typically $0.25 \%$. The MC1313P is intended for use in quadraphonic vehicle systems where it provides an excellent per. formance at supply voltages as low as 8 V .

The MC1312P has a higher typical input impedance, $3 \mathrm{M} \Omega$, than the MC1313P, $1 \cdot 8 \mathrm{M} \Omega$. In addition, the MC1312P can provide outputs of up to at least 2 V RMS whilst the MC1313P provides at least 0.8 V RMS before the total harmonic distortion rises to $1 \%$. The MCl313P has the advantage that it can operate in a cold vehicle at temperatures down to $-40^{\circ} \mathrm{C}$ whilst the MC1312P characteristics are specified down to $0^{\circ} \mathrm{C}$. The MC1312P has a lower signal to noise ratio, 80 dB , with the input shorted, as opposed to 74 dB for the MC1313P under certain conditions.

## TYPICAL CIRCUIT

A typical circuit for the use of either of these devices is shown in Fig.1. It is recommended that the component values shown should have a tolerance of $\pm 5 \%$ for optimum performance in this circuit. The absolute maximum permissible power supply voltage is 25 V , but the MC1312P is usually operated from a 20 V supply and the MC1313P from a 12 V vehicle supply. The current consumption of the MC1312P is in the range 11 to 21 mA and that of the MC1313P 6.5 to 12.5 mA at their respective normal operating voltages.

The SQ encoded right hand channel signal is
labelled $\mathbf{R}_{T}$ (for total right signal) in Fig.1, whilst $\mathrm{L}_{\mathrm{T}}$ is the total left hand signal. The device essentially separates the total right hand signal into two separate audio signals, namely the right hand front signal ( $\mathrm{R}_{\mathrm{F}}$ ) at pin 11 and the right hand back signal $\left(R_{B}\right)$ at pin 14. These two output signals are fed to separate power amplifiers which feed the appropriate


Fig. 1: Typical circuit utilizing the MC1312P or MC1313P. The devices are similar in application except for the supply voltage which is about 20 V for the former and 12 V for the latter.
loudspeakers. Similarly, the total left hand signal is separated to produce two audio output signals at pin $2\left(\mathrm{~L}_{\mathrm{F}}\right)$ and at pin $3\left(\mathrm{~L}_{\mathrm{B}}\right)$. The impedance at each of the four outputs is typically $5 \mathrm{k} \Omega$.

The two output voltages are about the same as the input voltage for that side, the tolerance in the signal amplitude ratios $L_{F} / L_{T}$ and $R_{F} / R_{T}$ being $\pm 1 \mathrm{~dB}$. The balance between the two forward channels also has a tolerance of $\pm 1 \mathrm{~dB}$. The amplitudes of the output signals to the two rear amplifiers are at a level of typically -3 dB relative to those to the two front amplifiers.

Internally these devices contain two preamplifiers which are respectively fed with the input $R_{T}$ and $L_{T}$ signals via the blocking capacitors C9 and C10. These preamplifiers each feed two "all pass" networks, shown in Fig.1, which produce phase shifts of $90^{\circ}$ without amplitude variations. Each phase shifted signal is fed into an internal resistor matrix together with the original output from the preamplifier, the two outputs from each matrix forming the required front and back signals.

It is generally desirable to enhance the centre front and the centre back separation. This is effected by connecting a resistor between pins 2 and 11 (front outputs) and between pins 3 and 14 (back outputs). For $10 \%$ front channel blending, a $47 \mathrm{k} \Omega$ resistor may be connected between pins 2 and 11 and for $40 \%$ back channel blending a $7 \cdot 5 \mathrm{k} \Omega$ resistor between pins 3 and 14

The devices are readily available from advertisers in this magazine.


## IETEVADII

## IN THE MAY ISSUE

## DIRECT-READING CAPACITANCE METER

This simple battery-powered design, based on the use of an NE555 timer l.c., gives direct indication of capacitance values from a few picofarads up to $10 \mu \mathrm{~F}$. A d.c. test voltage is used, allowing the measurement of polarised capacitors and the capacitance of reversebiased semiconductor junctions.

SERVICING THE TANDBERG CTV2-2 CHASSIS
The Tandberg CTV2-2 chassis is in many ways typical of the latest generation of large-screen, $110^{\circ}$ deflection continental colour recelvers, with a switch-mode power supply and making extensive use of i.c.s. W. S. J. Brice decribes the various faults he has encountered.

## AERIAL PERFORMANCE

Roger Bunney and Ian Beckett have been investigating the relative performance of various well-known u.h.f. aerials. Their resufts form an interesting follow-up to Pat Hawker's recent articles.

SMALL PICTURE AND RELATED FAULTS
Lack of height, bottom cramplng and other forms of nonlinearity, and fleld sync problems are common faults with older TV sets. John Law provides a comprehensive guide to the causes of such taults.

## FIELD TE CIRCUIT FOR THE PIL TUBE

Recent solid-state chassis use a wide variety of field timebase circuits. As an example of some of the latest techniques $S$. George investigates the circuit used in the Korting 55636 chassis, which is fitted with a PIL colour tube.

## WHICH PATTERN?

E. Trundle's test equipment survey next takes a look at the various patterns available to the service engineer.

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## by Eric Dowdeswell G4AR

IT has always amazed me to realise that the act of sitting down and taking a written examination, successfully, should enable anyone to go on the air with 150 watts DC input, or the equivalent in SSB, without ever having touched a piece of radio equipment in their life! The results of the misuse of such a transmitter on the neighbouring TV's are not hard to imagine! Even if the transmission is 'clean' and up to the standards required by the Home Office the newcomer will not have the faintest idea on how to tackle TVI problems. Unfortunately, it is only after the 'black box' has been bought, at some expense, that these troubles come to light, which accounts for the number of commercial transceivers one sees for sale in our magazines, by newly licensed amateurs. And some other hobby gets another newcomer!

But it is no good carping about the problem if one is not prepared to suggest an alternative. The answer must be to return to the days when one could start with an 'artificial aerial' licence enabling experiments with transmitters to be made on a dummy load, followed by a minimum period on CW only with low power, say 25 watts and then on to the full licence. In this way a tremendous amount of experience can be gained and, above all, interest is continuously stimulated. Now, pushing buttons on the 'black box' soon palls, because one is learning precisely nothing other than the procedure of talking to another amateur and that's just as simple as talking on the telephone!

Nothing new in all this of course, so what's the snag? Just that the licensing authority would not be prepared to undertake the additional work involved. But in the interests of amateur radio could not the RSGB undertake to administer such a scheme? With official approval, of course, with the Home Office just issuing the bits of paper. Oh, well, just a thought!

Stephen Budd A8713 of Worthing reckons that since the sunspot numbers seem pretty constant now we could be at the bottom of the cycle so he's looking forward to better times. Well, I think we have been at the bottom for some time and in spite of the fact that new spots have already been seen for the new cycle it will be a year or so before any significant
improvement is noticeable. Paul Turner in Bishops Stortford turned his spell in bed with flu to good use by extending his aerial and putting his new QR666 close to hand. He likes this Trio model except that he feels he'd like a higher ratio drive on the bandspread to assist with resolving SSB on the higher frequency bands.

Now for the good news! Jeremy Hinton of Newcastle, Staffs., is now ex-A8962, thank goodness, and proud owner of G8LIZ for the moment but could have his G $4+3$ by this time, as he was about to take his Morse test any day. He couldn't wait to get on the air and so popped round to G8KTW's shack for a quick QSO with his new call.

Plenty of useful info in the latest Bulletin from Stew Perry W1BB for the 160 m addicts. Like W8LRL who made WAC in two hours in the CQ 160 m competition in January! As Stew says, 'WOW'! Seems OK1ATP write about his 160 m beam in the Oct 75 QST. Anyone have any info on this? Depends whether it goes up or outwards before I could try it out! Stew worked EA8CR/9 for his No. 127 country on the band. Paul Barker in Sunderland zoomed in on the SSTV contest but bad conditions limited his results in Europe. The ARRL contest the same weekend didn't help either as no-one seemed to respect the accepted SSTV frequencies.

Peter Readings, not too far away from me, in Woking, was taken by my remarks on newcomers to amateur radio, in the March issue. He started in 1935 with a one-valve PW design for the short waves and getting back again now is brushing up for the RAE, in due course. Martin Chapple A9090 in Leamington Spa writes in for the first time. Aged 14, he was 'converted', as he puts it, to amateur radio when he visited a local special events amateur station. He progressed rapidly to a Trio 9R59DS and a looft wire and now contemplates a Microwave Module for 2 m and 8 -element yagi plus the same again for 70 cm . He queries the many odd prefixes to be heard these days. The best way to find out where they are is to look at the ITU block allocations rather than the usual prefix list, which is obviously going to be out of date the moment it is printed. R. Berry of Colne thought he was interested in the VHF bands until he got his 9R59DS going on 20 m and now has the DX bug. He heard TG9TI helping in the earthquake disaster which hit Guatemala.

Alan Doherty in Portrush, Co. Antrim found plenty on 80 m in the early hours with 3D2KG pushing his total of countries heard on that band to 172 . He has an FR400SDX and FR50B for keeping an ear on two bands at once! I wouldn't mind the FR400SDX by itself! His inverted-V on 80 m is likely to be changed to a delta loop before long. More info, please! Peter


Allen A8677 was pleased with the improved results from using a 132 ft wire and found ZL3NR/C on 80 m , which can't be bad!

A most interesting letter from Jim Durrant G4CEX of Solihull, in which he supports my views on the lack of encouragement being offered to the newcomer by the RSGB. He plodded on alone "the only English book I found of help was the one by Frank Rayer" (well-known PW contributor). "When I got my ticket I joined the RSGB automatically but gave them up after a couple of years as a bad job . . . don't think I have seen one article in Radcom that would be of any use to a beginner". Need I say more? He continues "I wish the powers-that-be in the RSGB would take notice of your remarks and really do something for the novice!" Congrats Jim on sticking to it and I know you will not regret getting your ticket, in spite of the obstacles.

A letter in a similar vein from A. J. Lees of Bournemouth, copy to the RSGB, says he always recommends beginners to take PW "as this magazine has done more for beginners than any other magazine". He says "the newcomer eagerly scans Radcom to no avail and becomes disillusioned and thinks he lras wasted his money". If you are listening regularly how about some reports OM?? Alan Dixon A9037 of Kingston sympathises with Steve Cottis who had trouble getting on an RAE course. Alan was only 14 when he started his course last September and has just heard that he has passed his RAE in
the December exam! Fantastic! So cheer up, Steve, it can be done.

Finally, a note from Les Light G3KDL, Hon. Sec. of the Radio Society of Harrow, club calls G3EFX and G8JMR. Meetings every Friday at 8 pm at the Harrow Sea Cadets HQ, Woodlands Road, Harrow. Features during April are a debate on HF and VHF propagation and a talk on mobile operation by Fred Barnes G3AGP. Two evenings a month are kept for practical work and construction. So flock along folks, nothing to lose but your bus fare!

I have been asked to dispose of a Hallicrafters S108 receiver. Valves, thank goodness, MW to to 32 MHz continuous, with amateur bands 10 to 80 m on main dial, BFO, noise limiter and excellent manual. Condition is very good and has been checked out by yours truly. Sorry, but must be inspect and collect, which a buyer would probably prefer anyway!

## Log extracts

S. Budd:- 80m A4XGC CO2JA C3ILC EA9FC FG7AR/FS7 HZ1SH PJ0USA OE6DK/YK ZL3GG ZL3NR/C 9Y4NP 40m VK3ZL 6W8FP 15 m A4XGC ZD8AR 9VlSH 20m FG7AR/FS7 ST2SA (14250 0700 Fridays) VS6BL YB1HF 9N1MM
P. Barker:- 20 m SSTV CT1JI F9XY IlSU IOPCB OZ5FG SM5EEP 20m A6XP EA8CR/9 OE6DK/YK OE7XBI (Olympic Games, Innsbruck)
A. Doherty:- 80m EA8CR/9 FL8DJ HK1CHL HP3XWB HR3JJR KL7HFQ PJ8CO VP2DQ 574LW 3D2KG 20m YN7NHW
P. Allen:- 80 m WB9AJF/6Y5 ZL3NR/C 15 m TU2EI 5N2ESH OE6DK/YK (Golan Heights) C9MJO (Mozambique) 3B8CV

All stations are SSB except those of P. Barker, all SSTV.


## SHORT WAVE BROADCASTS by Derek Bell

A"defector", if I may call him that, from the ranks of the licensed amateurs is Allan King G4BKM of London who forwards a sample of the duplicated report forms he sends out in search of QSL cards. These forms give all the relevant information in neatly spaced sections with the largest space devoted to the ten minutes of programme content that stations usually require. Despite this, Allan complains that Radio Pakistan turned down a request and on checking the tape recording of the broadcast all details were found to be correct. It seems to me to be a case of the station log being at fault!

Two more newcomers to the hobby ask questions that I must deal with in two sections, A. B. Towler of Newcastle on Tyne would like to know what to put into reception reports to gain QSL cards. This should comprise the following: time in GMT, frequency, your set and aerial type, the SINPO rating
of the signal, ten minutes verbatim of the programene content and your name and address. It also helps to say a few kind words and say "please"! Information on types of set, aerial systems etc can be obtained from the many very good leaflets issued by Radio Nederland, PO Box 222, Hilversum, Holland. I do not know of any duplicated report forms for sale but the Post Office air letter form should suffice provided that one does not have to send IRCs to the station.

Sylvia Wood of Godalming is our second newcomer although she is seeking. help to get her RAE "ticket" so we may seen loose her. Ah well! win some, lose some! The path to this side of our hobby starts by getting the Guide to Amateur Radio from the RSGB. Meantime, Sylvia, you will have to be content with joining we mere DX fanatics. The log you were asking about is usually a tattered notebook that the DXer keeps of the time, date, frequency and station name in order to jog his memory or give him a guide as to what was heard and at what time of year, since not only does reception vary with the season but we are now in the sunspot minimum of the solar cycle and it will be 1978 before we can expect the beginning of any improvement.

Midst all the gloom however, David Sewell sends us a selection of his best and these are Latin American stations. This aspect of our hobby attracts many listeners who like to specialise in these stations. since there are many differing styles and programme content is equally varied. Look forward

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to Lara Venezuela on 4800 at 0220 , Juventud Venezuela on 4900 at 0050 , Barquisimeto Venezuela on 4990 at 0135 . These were all pulled in on Dave's Trio 9R59DS with a trap dipole 25 feet high, but all the same, undoubtedly and verily, only for nightowls!

Ian Walker of Crouch End, London is baffled by a station he heard on 2300 and 2750 simultaneously. This came in on Ian's Sony ICF5500M via the set's telescopic aerial. The clue to the ident of this station is its claim to be "The voice of Soviet public opinion'! The station is Radio Peace and Progress and very little is known of its staff or its aims for that matter. Ian describes the programme content as documentary on political topics.

Just a short while ago the latest edition of the Radio RSA bulletin plopped on to the mat at chez Bell. This leaflet, a mere shadow of its former self, covers the period of the summer schedules starting in March and indicates that RSA will use 5980, 7270, $11900,11970,17780,15155,15220$ and 21535 kHz . Their signals are radiated, with short breaks, twenty four hours a day to various target areas and in different tongues, but, strangely, while they have English transmissions they only specify North America as an English target area while the other area is just designated "Europe".
Robin Bayley of Kingswood School, Wolverhampton reports the 15155 RSA service in German at 1800 , on a Marconi R1475 with a long wire, plus NHK Tokyo on 15430 at 0805, TWR Bonaire on 11920 at 0030, Radio Nacional de Brazil on 11780 at 2100. Another youngster is Stewart Fenwick of Clack-
mannan in Scotland, who reports that Radio Pyongyang recently sent him a QSL after 106 days and 1 use this to mention that reports have ,been noticed of late that the station in Fukien, China has reemerged after a long period, on 2430 . This station is very rarely reported and I can remember at a European DX Council conference a German DXer showing me one of their QSLs, written on rice paper in Chinese, which he had waited a donkeys age to get. At this time he claimed the station was a small transmitter working mobile so if any one chances on them please let us know all the details.

Ken Smith of Ross-on-Wye has some enquiries to make about the Voice of America transmitter at Rhodes. He thinks that the frequency has changed for the 2100 session and asks for any information of new frequencies. As I have said above, it is about this time of year that the schedules change and so it is possible that this station has disappeared from its usual part of the spectrum. A reader who just wants to be known as "SS" suggests that the Radio Australia signal on 9745 mentioned recently, in fact comes from Melbourne as he monitored it over Christmas. This may well be since stations, through many causes, have to depart from the published schedules and the poor old scribe slaving over a hot tripe-writer can only rely on his friends who write in to keep him up to date. SS also craves info on "what to do with aerials", well, one thing not to do is to fasten them rigidly to trees, since, as happened to a friend of mine in the recent gales, the tree swayed and down came the lot! The answer to this is to secure the long wire with one of those rubber "ropes" that are used on motor cycle panniers and car roof racks. If it is an inverted " $L$ " longwire have the foot of the " $L$ " running down from the support post and not down the house wall, and feed into the house via a wire run from the far end of the aerial. That brings this session to a close so I will wish you and yours best 73 s .


## MEDIUM WAVE DX

 by CHARLES MOLLOYTHIS MONTH Alan Crookes reports from his new QTH in Sheffield. He had to rebuild his loop after moving house but his 'shack' is now fully operational and he is using a Murphy B40A communications receiver to pull-in his medium wave DX. Stations logged include WINS, the all-news station in New York City, which transmits on 1010 kHz with a power of 50 kW and three locals in Newfoundland, CBN in St John's on 640 kHz , CKVO in Clarenville on 710 kHz and CJON St John's on 930 kHz . Alan points out that the announcement "VOCM Radio Service" from CKVO is misleading since CKVO is not mentioned in many station listings, including the 1975 World Radio and TV Handbook, as it came on the air as recently as December 1974. The VOCM Radio Service is a local network in Newfoundland with VOCM on 590 kHz in St John's as the key station. Other members of
the network, in addition to CKVO, are CHCM in Marystown on 560 kHz , CKCM in Grand Falls on 620 kHz , CKGA in Gander on 730 kHz and CKIM Baie Vert on 1240 kHz , all of which have been heard recently in the UK. VOCM is one of the few medium wave stations in Canada to use the prefix $V$ in its callsign; the majority start with the letter $C$. Newfoundland became the 10th province of Canada in 1949 but VOCM and four other well established broadcasters managed to hold on to their original call letters that were issued when the territory was still a Crown colony.

The World Radio and TV Handbook, generally regarded as the DXers 'bible' is published annually in Denmark and distributed in the UK by Billboard Publications. It is printed in English and can be ordered through bookshops. It costs $£ 5$. The WRTVH lists all known broadcasting stations (and TV stations) with the exception of low power locals in the USA and low power relays elsewhere. AM broadcasting stations are listed by frequency and there is a section for each country which gives the hours of transmission, adiresses and QSL information. The less pretentious "Guide to Broadcasting Stations" at 80 p is produced in the UK by Butterworth and is on sale in many bookshops. AM broadcasters in Europe and North Africa are listed along with a selection of the more powerful medium wave transmissions from other parts of the world.


This is a very useful book for the beginner. A similar publication "World Radio TV Listings" is available for 60p.

The Foreign Broadcasting Information Service of the United States Government produces "Broadcasting Stations of the World Part 2" at intervals of about two years. All broadeasting stalions localest outside the United States and in the Frequency range 150 kHz to 26 MHz are listed. This bulky paperback can be obtained for $\$ 2 \cdot 50$ postpaid from the Superintendant of Documents, Goverument Printing Office, Washington, DC 20402, USA. Quote Pr.Ex-7.9:972 Part 2 and be prepared for a wait of several weeks!

Steve Whitt (London) refers to a wavetrap which he inserted between his loop acrial and the input to his communications receiver, in order to reduce local interference on 1546 kHz . It is a parrailel tuned circuit which can be tuned across the medium wave band. It offers a high impedance at its resonant frequency and a low impedance at all others and when it is placed in series with the aerial lead, it will reduce the strength of an unwanted station, leaving others unaffected. A medium wave tuning coil and appropriate variable capacitor, or pre-set, to tune across the medium wave band, are the only components required. The coupling winding is not used. Tune the receiver to the unwanted signal, adjust the wavetrap for minimum signal strength and the receiver can be used normally.
S. Lydon (Kingston-on-Thames) has been trying, without șuccess, to tune-in to the Irish Speaking Radio (Radio ua Gaeltachta), a network of VHF and MW transmitters in the Republic of Ireland. There are three outlets on the medium waves; Connemara on 539 kHz with a power of 2 kW , Kerry on 962 kHz with 1 kW and Donegal on 1250 kHz with 10 kW . In spite of their proximity to England these stations are rather difficult to pick-up, mainly on account of co-channel interference. The writer, from his QTH
in North West England, can hear Connemara during the evening after dark, using a Marconi Mercury receiver and a medium wave loop. The station is on the air from 1800 to 2100 approximately and with a bit of luck might just be audible in the London area. Radio na Gaeltachta is an example where DX means Difficult rather than Distant. Torshavn in the Faroe Islands on 584 kHz is another 'Difficult' station. Some DXers, including the writer, have had to wait for years before receiving a rather attractive QSL card as a reward for persistance.
D. R. Mayhew reports hearing Kinshasa in Zaire on 692 kHz and Dakar in Senegal on 764 kHz , using a Philips receiver and medium wave loop aerial. Medium wave stations in Africa are often heard well in the UK at this time of year. A loop is very useful for listening to this continent since the DX lies to the south and the interference from Europe, in general, comes from the east so it is not difficult to null-out the QRM. Stations to look for during the evening are Tenerife in the Canary Islands which broadcasts in Spanish on 620 kHz ; ELBC in Monrovia, Liberia which has English programming on 629 kHz ; Enugu, Nigeria which is a weak signal clear of interference on 1320 kHz at 2300 ; Nouakchott, Mauretania on 1349 kHz and, from the Republic of Guinea, Conakry which is a strong signal on 1403 kHz after 2300 hrs . There are two long wave stations in Africa, both coming in at good strength in the UK. From the top of a mountain near Azilal in Morocco the home service in Arabic is transmitted with 800 kW on 209 kHz , while from nearby Algeria the French programme comes from Tipaza with a power of 1500 kW on 245 kHz .

## BROADCAST BANDS

Short Wave reports by the 15 th of the month to Derek Bell c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD. Medium Wave Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3 JG .

## AMATEUR BANDS

Logs covering any Amateur band/s in band/ alphabetical order by the 25th of the month to Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey, KT21 2TW.


## TELZ TENNTS SCORING TNYT <br> September ${ }^{5}$

Some readers have queried the origin of the timing signals used for this unit. 'The signal Q3 originates at pin 13 of IC53, signal SP2 at pin 3 of IC56 and signal SP6 at pin 8 of IC57. Note also that IC32 is shown as a 7410 which should read 7400, as in circuit diagram.

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The illustration shows the iwo P．C．B．module kits already assembled，one has 8 mm high digits， the other has 16 mm high digits．Also shown is an example of a completed clock．
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B.H. Component Factors Led

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83
6

Bi-Pak Ltd
i. 72

Bi-Pre-Pak Ltd.
.. 19
Birkett, I. ...
Boffin Projects
... 81
British Institute of Engineering Tech-
nology ... ... ... 18, 64,
British National Radio \& Electronics
School
6, 67
J. Bull (Electrical) Litd. $\quad .$.

Bywood Electronics
4
C.D.I. Ltd.

36
Cambridge K̈irs
91
Cambridge Technical Devëlopments Ltd.
Caranna C.
90
Chromasonic Electronics .... .... Cover iii
C.J.L. Ltd.

76

Cleveland Süplies | 76 |
| :--- |
| 89 |

Codar Radio Co
Colomor (Electronics) Ltd.
76

Copper Supplies
96
Crescent Radio Ltd

| .. |
| :--- |
| 1 |
| ... 75 |

Crofton Electronics 91
D.E.W. Ltd. 92
35
Doram
Eaton Audio
Electronics Design Ässociates
Electronic Mail Order Ltd.
Electronic Supplies (Print-a-Kit)
Electro-Tech Components
Electrospares
Electrovalue Ltd

| Flairline Supplies |  |  | ... |  | 84 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| G.T. Technical Information Service |  |  |  | ... | 90 |
| Garfields ... | , | .. | ... |  | 91 |
| Goldring Ltd, |  | ... | ... |  | 61 |
| Greenbank Elect | ronics | ... |  |  | 77 |
| Greenweld Elect | ronics |  |  |  | 64 |
| Grimsby Electron | ics |  |  |  | 89 |
| H.A.C. Short-Wave Supplies |  |  | ... |  | 93 |
| H.M: Electronics |  | ... | ... |  | 91 |
| Harverson Surplu |  | ... | ... | $\cdots$ | 17 |
|  |  |  | $\ldots$ | $\cdots$ | 91 |
| Home Radio Com | pone | Led. |  |  | 21 |
| I.L.P. Electronics | Ltd. |  |  |  | 9 |
| Integrex Ltd. |  | ... |  |  | 68 |
| Intertext I.C.S. |  | ... | $\ldots$ |  |  |
| Kensington Supplies Kinnie Components |  |  | $\cdots$ |  | 90 |
|  |  | -. | ... |  | 40 |
| Lasky's Radio Lewis Radio. Linear Products Lynx Electronics |  |  |  |  | 12 |
|  | ... |  |  |  | 64 |
|  | $\cdots$ |  | ... | ... | 63 |
|  | ... | ... | ... | ... | 16 |
| M.C.L. ${ }^{\text {Manor Supplies }}$ |  |  |  |  | 89 |
|  | $\ldots$ |  | $\cdots$ | $\cdots$ | 81 |
| Magnetic Component Magnum Publications |  |  | .. | ... | 70 |
|  |  | ... | $\ldots$ |  | 92 |
| Maplin Electroni Marco Trading | Supp |  | -. | Cover |  |
|  |  | ... | ... |  | 89 |
| Marshall, A. \& SonsMawson Associates |  | ... | ... |  | 12 |
| Milward, G. F. . |  |  | ... | $\cdots$ | 89 |
|  |  | ... | ... | $\ldots$ | 63 |
| Minikits Electronics |  | $\ldots$ | $\cdots$ |  | 91 |
| Newmart Electronics |  | ... | ... |  | 20 |
| Orchard Electronics |  | ... | ... | ... | 6 |
| Partridge Electronics Led. |  |  | $\ldots$ |  | 93 |
| P.B. Electronics |  | ... | $\ldots$ | .. | 77 |
| Pulse Electronics |  | ... |  |  | 8 |
| Precision Petite | ... | $\ldots$ | ... | ... | 86 |

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EF91 \& 0 <br>
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EBC33 \begin{tabular}{lll}
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\end{tabular} EBF

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EC5 EC5 \begin{tabular}{ll|l}
ECC81 \& 0.45 \& EL504 <br>
ECC82 \& 0.35 \& EL821 <br>
\hline

 

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\end{tabular}



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