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| ECT | 709C Op Amp |
| W02 1A 200V 38p |  |
| BY164 1-4A 200V | 741C Op Amp 8/14 D.1.L./TO99 25p |
| MDA952/2 6A 57p | ${ }_{\text {747 }}{ }^{\text {Amp }}$ Dual Op ${ }^{\text {c1. } 20}$ |
| $\begin{aligned} & \text { MDA952/26A } \\ & 100 \mathrm{~V} \end{aligned}$ |  |
|  | 748C Op Amp |
| ZENER DIODES | 414 Radio 1.C |
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## TRANSFORMERS

| MAINS ISOLATING PRI．120／240V．SEC．120／240． CENTRE TAP WITH SCREEN 115 V or 240 V Sec ．only |  |  |  |
| :---: | :---: | :---: | :---: |
| Ref． |  |  |  |
| No． | （Watts） |  |  |
| 07 | 20 | $3 \cdot 77$ | ． 5 |
| 149 | 60 | 4.69 | 0.72 |
| 150 | 100 | $5 \cdot 33$ | 0.85 |
| 151 | 200 | 8． 54 | $1 \cdot 12$ |
| 152 | 250 | 10.32 | 1．41 |
| 153 | 350 | 12.47 | 1.41 |
| 154 | 500 | 14.33 | 1.61 |
| 155 | 750 | 21.94 | BRS |
| 156 | 1000 | $30 \cdot 57$ | BRS |
| 157 | 1500 | 34.89 | BRS |
| 158 | 2000 | 38.92 | BRS |
| 159 | 3000 | 61－48 | BR |

30．VOLTRANGE Prim． $200-240 \mathrm{~V}$
Sec． $0-12-15-20-2$
Sec．0－12－15－20－24－30V

| Ref． | Amps | 1. |
| ---: | ---: | ---: |
| No． | 11 |  |
| 12 | 0.5 | 1.90 |
| 79 | 1.0 | 2.52 |
| 3 | 2.0 | 3.77 |
| 20 | 3.0 | 4.70 |
| 21 | 4.0 | 5.56 |
| 51 | 5.0 | 6.73 |
| 117 | 6.0 | 7.52 |
| 88 | 8.0 | 10.20 |
| 89 | 10.0 | 10.36 |

60 VOLT RANGE Prim．200－240V
5 ec．0．24－30－40－48－60V Ref． No．Amps $f$ \＆

## 12

## ここ

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## 

 $\begin{array}{rrrrr} & 5.0 & 12.07 & 1.41 \\ 120 & 8.0 & 15.75 & \text { BRS } \\ 122 & 10.0 & 19.40 & \text { BRS } \\ 189 & 120 & 20.4 & \text { BS }\end{array}$\section*{12 and or 24 Volt PRIMARY 240－250 VOLTS} | Ref． | Amps |  |  | $0 \& D$ |
| :---: | :---: | :---: | :---: | :---: |
| No． | $12 v$ | $24 v$ | $£$ | 6 |
| 111 | 0.5 | 0.25 | 1.54 | 0.28 |
| 213 | 1.0 | 0.5 | 1.86 | 0.58 |
| 71 | 2 | 1 | 2.41 | 0.58 |
| 18 | 4 | 2 | 2.97 | 0.72 |
| 70 | 6 | 3 | 4.43 | 0.72 |
| 108 | 8 | 4 | 5.09 | 0.85 |
| 72 | 10 | 5 | 5.50 | 0.85 |
| 116 | 12 | 6 | 5.80 | 0.97 |
| 17 | 16 | 8 | 7.48 | 0.97 |
| 115 | 20 | 10 | 10.91 | 1.61 |
| 187 | 30 | 15 | 14.20 | 1.41 |
| 226 | 60 | 30 | 17.67 | BRS |
| 20 |  |  |  |  |

50 VOLT RANGE
Prim．200－240V
Sec．0－19－25－33－40－50V

| Ref． |  |  | $0 \&$ |
| :--- | ---: | ---: | ---: |
| No． | Amps | \＆ | $E$ |
| 102 | 0.5 | $\mathbf{2 . 7 1}$ | 0.58 |
| 103 | 1.0 | 3.55 | 0.72 |
| 104 | 2.0 | 4.95 | 0.85 |
| 105 | 3.0 | 6.10 | 0.97 |
| 106 | 4.0 | 7.98 | 1.12 |
| 107 | 6.0 | 12.71 | 1.25 |
| 118 | 8.0 | 13.63 | 1.61 |
| 119 | 10.0 | 17.75 | BRS |

## AUTO TRANSFORMERS Ref VA Auto ToDs No（Wotts）

## $f$ D\＆

$4 p$ 113 20 0－115－210－240 $\begin{array}{ll}1.75 & 0.51 \\ 3.05 & 0.72\end{array}$ $\begin{array}{ll}3.05 & 0.72 \\ 4.33 & 0.72\end{array}$ $-\infty$
0 $\begin{array}{ll}.33 & 0.7 \\ 6.11 & 0.85 \\ .36 & 1.25\end{array}$ 150
300
500
$\square$ 500
1000 2000
3000 3000
CASED AUTO TRANSFORMERS Mains lead inpur \＆USA 2 pin outlets $\begin{array}{llll}20 \mathrm{VA} & 63.29 & \text { P\＆P } 60.72 \text { Ref } 113 \mathrm{~W} \\ 50 \mathrm{VA} & 6.37 & \mathrm{P} \& \mathrm{P} 60.85 & \text { Ref } 4 \mathrm{~W}\end{array}$ 500VA 110.97 P\＆P $£ 1.25$ Ref 67 W 1000VA E18．39 P\＆P BRS Ref 84W

SCREENED MINIATURES $\begin{array}{ll}\text { Ref } \mathrm{mA} & \text { Voles } \\ 238 \\ 200 & 3-0-3\end{array}$
$\begin{array}{lll}238 & 200 \\ 212 & 1 A, ~ I A & 0-0,3 \\ 23 & 0-6\end{array}$ $\begin{array}{llll}13 & 10, & 9-6,-6 \\ 235 & 330,330 & 0-9,0-9\end{array}$ $\begin{array}{ll}207 & 500,500 \\ 200 & 0-8,9,9 \\ 20 & 0.8-9\end{array}$ $\begin{array}{lllll}208 & \text { IA．IA } & 0-8-9, & 0-8-9 \\ 236 & 200, & 200 & 0.15, ~ & 0.15\end{array}$ $214300,3000-20,0.20$ $\begin{array}{ll}221 & 1 A \text { ，} 1 A \\ 206 & 0-15-20,0-15-20\end{array}$ 203 500， $5000.15-27,0.15-27$ $\begin{array}{lll}204 \text { IA，IA } & 0-15-27,0-15-27 \\ 5112 & 500 & 12,15,20,24,30\end{array}$ BRIDGERECTIFIERS

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| ECF8： | 0.90 | H：Y\％ | 0.81 | PD500 211 | URA4 1.03 | PC802 1.00 |
| ECF86 | 0.78 | EZ80 | 0.63 | PFLi200 0.81 | UYB＇ 0.63 | 301 PLI |
| ECH8I | 1.29 | E．7．41 | 0.53 | PL36 106 |  | PCL801 1.35 |
| ECH83 | 1.08 | （1）2501 | $1 \cdot 30$ |  | $\operatorname{ECO} 0+1.20$ | ${ }^{30 \mathrm{PLL} 3 / 3} \mathrm{PCL} 001.47$ |
| ECH84 | 1.17 | （：734 | 0.91 | PLYI． 100 |  | P0PL800 1－47 |
| ECL8t | 0.78 | P＇xo | 1.05 | PLA：－ 0.48 | 6F23／EFSI2 1.16 |  |
| HCL82 | 0.89 | PCos | 1.05 | Pl83 129 | 116 | $\begin{array}{ll}\text { P（LLX8 } & 1.72 \\ 30 & 1644\end{array}$ |
| ECL83 | 0.78 | PCW\％ | 0.53 | PLX4 078 | $30 \mathrm{Cl} / \mathrm{PCFF} 0$ | 30 PL 5 ¢ 144 |
| ECLkti | 0.73 | PCOM | 0.65 | Plint 102 | 0.63 |  |

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Individually boxed and guaranteed but of Euro－ pean or other origin at greatly reduced prices． Quotations for any valve not listed．Send SAE for lists．

| ists． |  |  |  |  |  | URC8I <br> 1：BF80 | $\begin{aligned} & 0.80 \\ & 0.80 \end{aligned}$ | 6SNTOT | $\begin{aligned} & 0.85 \\ & 0.85 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | UBF89 | 0.50 | 68Q7GT | 0.40 |
| A 21 | 0.75 | EF39 | 1.25 | Kगいす！ | 1.80 | UCC85 | 0.50 | 6051 | 1.80 |
| AZ31 | 0.60 | EFHO | 0.85 | MCt4 | 1.00 | UCH42 | $0 \cdot 80$ | $8 \vee 66$ | 080 |
| Cblal | 1.40 | F，res | 0.46 | N78 | $5 \cdot 00$ | UCH8I | 0.50 | 6V6GT | 0.80 |
| Clu3 | 1.60 | HPrs | 0.50 | OA2 | 0.85 | UCL8＇2 | 0.40 | $6 \times 1$ | 0.45 |
| $\mathrm{CH}^{1}$ | 0.60 | EF89 | 0.85 | OB2 | 0.45 | UCL83 | 0.70 | $6 \times 60$ | 0.45 |
| Daf91 | 0.40 | FFyl | 0.40 | PCR6 | 0.08 | TF4l | 0－76 | 6x50T | 0.65 |
| DAFER | 0.60 | EFY： | 0.80 | PC8N | 0.85 | UF89 | 0.80 | $7 \mathrm{B6}$ | 0.80 |
| DCC90 | 1.86 | EFus | 0.45 | PC97 | 0.58 | ULAl | 0－4 | $7 \mathrm{B7}$ | 0.80 |
| DF91 | 0.40 | EF98 | 0.80 | PC900 | 0．88 | UL84 | 0.50 | 7 CD | 1．10 |
| DF96 | 0.60 | EF183 | 0.40 | PCC8 | 0.45 | UY 41 | 0.55 | 706 | 1.00 |
| DKPI | 0.80 | EFIH4 | 0.40 | PCC88 | 0．68 | UY85 | 0.46 | 7H7 | 0.80 |
| DK9！ | 1.00 | EL32 | 060 | PCC89 | 0.65 | VR105／30 | 0.40 | $7 \mathrm{R7}$ | 0.30 |
| DKPH | 0.75 | FL33 | 8.00 | PCCIR9 | 0.65 | VR150j30 | 0.45 | 787 | ． 88 |
| 1 LP\％ | 0.80 | EL34 | 0.70 | PCF80 | 0.40 | 1 R 6 | 0.50 | 7 Y 4 | 0.80 |
| 12L94 | 0.48. | EL．39 | 0.60 | ${ }^{\text {PCP8 }}$ | 0.69 | 185 | 0.40 | 12AT8 | 0.45 |
| DL96 | 0.68 | EL37 | 2.60 | PCF86 | 0.65 | 1T4 | 0.40 | 12 AT 7 | 0.6 |
| DY86 DY87 | 0.45 0.46 | EL4 | 0.90 1.88 | PCP801 | 0.60 | 384 | 0.50 | 12AU6 | 0.80 |
|  | 0.47 | ELA | 1.88 0.85 | ${ }^{\text {PCFP80d }}$ | 0.55 | $3{ }^{3}$ | 0.46 | 12AU7 | $0 \cdot 5$ |
| EABCHO | 0.88 | EL95 | 0.80 | PCFF806 | 0.80 | $8 \mathrm{ER4GY}$ | 1.00 | 12AX7 | 0.8 |
| EAF4： | 0.70 | ELL80 | 8.00 | PCF808 | 1.00 | ${ }_{8}^{8184}$ | 0.85 0.65 | A6 | 0 |
| EB91 | $0 \cdot 30$ | EM80 | 0.85 | PCL82 | 0.45 | ${ }_{624 G}$ | 0.66 0.65 | ${ }^{12 \mathrm{BE}}$ 306 | 0.80 0.40 |
| EBC33 | 1.00 | EM81 | 0.80 | PCL83 | 0.70 | 6／30L2 | 0.90 | 30 Cl 15 | 1.00 |
| EBC41 | 076 | EM84 | 0.40 | PCLS | 0.60 | 8AKE | 0.45 | 30 C 17 | 1.00 |
| EBF80 | 0 | EM85 | 1.00 | PCL8S | $0 \cdot 60$ | 6AM5 | 1.00 | 30 C 18 | 0.90 |
| EBr83 | 0.40 | EM87 | 1.00 | PCLAA | 0.60 | 6apo | 0.80 | 30 F 6 | 1.00 |
| EBF89 | 0.38 | EY86 | 0.45 | PCL805／85 |  | 6A87G | 1.00 | 30 FLL | 1.00 |
| E日L31 | 2.00 | EY86 | 0.6 |  | 0.80 | 6AT6 | 080 | 30FLL | 1.00 |
| ECC81 | $0 \cdot 45$ | EZ40 | 0.80 | Pbs00 | 180 | 6aU6 | 0.40 | 30 FLI 4 | 1.00 |
| ECCS | $0-38$ | E241 | 0.78 | PEN45 | $0 \cdot 86$ | ${ }^{6 B A 6}$ | 0.28 | 30 L 18 | 0.98 |
| ECC83 | 0.38 | Ez80 | 0.80 | P136 | 0.88 | 6BE6 | 0.18 | 30 LL 7 | 0．08 |
| ECCR4 | 0.35 | E281 | 0.81 | PL81 | 0.55 | 68H6 | 078 | 30P4MR | 1.40 |
| ECC85 | 045 | GY501 | 0.90 | PL83 | 0.50 | 6BJ6 | 0.76 | $30 \mathrm{Pl}{ }^{\text {3 }}$ | 1.00 |
| ECC8s | 0.80 | G230 | 0.85 | PL83 | 0.60 | ${ }^{68 B Q 7 A}$ | 0.85 | 30 P 19 | 0.98 |
| ECH35 | 1.50 | QZ32 | 0.85 | PL86 | 0．80 | ${ }_{6}^{6 B R 7} 7$ | 1.20 | 30 PL 1 | 0.95 |
| ECH42 | 085 | （1234 | 0.75 | PLLE0 | 0.85 | ${ }_{6}^{6887}$ | 140 | $30 \mathrm{PL1} 3$ | 1.10 |
| ECH81 | 035 | ©237 | 1．80 | PLS04 | 0.86 | 6BW6 | 1.00 | 30 PL 14 | 1.10 |
| ECH83 | 0.80 | HN309 | 1.80 | PLS08 | $0 \cdot 00$ | 6BW7 | 100 | 35 W 4 | 0.60 |
| ECL80 | 0.60 | K T61 | 2.50 | PLo09 | 1.65 | 6C4 | 0.6 | 352401 | 0.70 |
| ECL82 | 0.42 | K T66 | 2.85 | ${ }^{\text {PL80\％}}$ | 1.26 | 6CD6G | 180 | 50CD6G | $1 \cdot 20$ |
| ECL83 | 0.75 | KT81（7C5） |  | PX25 | 8.60 | 6CH6 | 1.50 | 807 | 1.00 |
| ECL86 | 0.55 |  | 1.80 | PY33 | 0.63 | 6CW4 | 3.00 | 813ITT | 14.00 |
| ECLL800 | 8． 50 | KT81 | $1-78$ | PY81 | 0.50 | 6 F 23 | $0 \cdot 00$ | 813 U8BR | 6.00 |
| FF37．4 | 180 | K TR | 3.25 | PY\％ | 0.65 | 6 F －25 | 1.00 | 86 ffa | 1.20 |

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| AAZ13 | 0.12 | BD131 | $\begin{aligned} & 0.83 \\ & 0.42 \end{aligned}$ | Quantity |  | discounts |  |  | ก |
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| ACl27 | 0.25 | HF173 | 0.28 |  |  |  |  |  |  |  |  |  |
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| AC17 | 0.25 | BF180 | 0.88 | OADI | 0.07 | 2TX500 | 0.13 | 2N2904 | 0.20 |
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| ACy 34 | 0.75 | BF197 | 0.15 | OC2\％ | 2.00 | 7TX550 | 0.18 | 2N2906 | － 20 |
| A 1 l 40 | 0.60 | B $\mathrm{F}^{2} \mathbf{0} 0$ | 0.82 | Oと\％ | 1.25 | 1 N 914 | 0.06 | 2N2926 | 0.12 |
| AD149 | 0.50 | BFS61 | 0.25 | OC25 | 0.40 | IN400！ | 0.08 | 2N3053 | －18 |
| AD161 | 0.44 | BFB98 | 0.25 | OC28 | 0.68 | IN4002 | 0.07 | 2N3053 | 0.45 |
| A D162 | 0.44 | BFW10 | 0.61 | OC36 | 0.55 | IN4003 | 0.08 | 2N3525 | 0.91 |
| AFIJ | 0.25 | BFI29 | 0.28 | OC36 | 0.60 | IN4004 | 0.08 | 2N3614 | －65 |
| AFlis | 0.25 | BFX88 | 0.24 | OC4t | 0.40 | IN 4006 | 0.10 | 2N3615 | 0.05 |
| AF117 | 0.4 | BFY50 | 0.20 | 0 CH | 0.20 | IN4006 | 0.18 | 2N3702 | 0.11 |
| AFise | 0.48 | BFY61 | 0.20 | OCt5 | 0.20 | IN4007 | 0.12 | 2N8703 | 0.14 |
| AF＇239 | 0.44 | BFY5d | 0.80 | ${ }^{0} \mathrm{C} 71$ | 0.25 | IN 0006 | 0.08 | 2N8704 | 0.14 |
| ABY＇7 | 0.88 | BY 100 | 0.27 | OC7\％ | 0.80 | 189：1 | 0.07 | 2N9706 | － 0.11 |
| ABY28 | 0.88 | BY126 | 0.14 | OC75 | 0.85 | 182033 | 0.20 | 2N 3707 | 0.18 |
| BA102 | 0.25 | BY127 | 0.15 | Ocs 1 | 0.28 | 182051， | 0 CO | 2N3708 | 0.07 |
| BA115 | 0.10 | BZX61 | neriea | 0c811） | 0.28 | 182100． | 0.10 | 2N3700 | － 10 |
| $\mathrm{BCL}^{\text {c }} 07$ | 0.14 |  | 0.20 | OC812． | 0.45 | 183010 | － 1 | 2N3710 | 0－11 |
| BC108 | 0.18 | AZY88 ser | erion | OC83 | 0.35 | 2N696 | －15 | 2N3711 | $0 \cdot 11$ |
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| BCII3 | 0.15 | clest．05 | 0.85 | 0 Cl 70 | 0.80 | 2N706 | 0.10 | 2N8820 | － 60 |
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| BC143 | 0.80 | CRE3－05 | 0.40 | OC200 | 0.76 | 2N1131 | － $2 \cdot$ | 2N3903 | － 15 |
| RC14 | 0.10 | CRB3－40 | 0.65 | OC20］ | 1.50 | 2N1132 | － 54 | 2Na904 | － 20 |
| BC148 | 0.08 | MJE340 | 0.47 | OC209 | 1.50 | 2N1302 | $0 \cdot 11$ | 2N8908 | － 26 |
| BCIbgC： | 0.16 | MJE370 | 0.68 | OC20s | 0.75 | 2N1303 | 0.13 | 2N8906 | － 0.25 |
| BC182 | 0.12 | MJEE20 | 0.85 | 0CP71 | 1.20 | 2N1304 | － 0 | 2N405＊ | 0.15 |
| BCid2L | 0.18 | MJE2985 | 1．27 | ORP12 | 0.80 | 2N 1304 | － 11 | 2N405\％ | 0.10 |
| BC184L | 0.18 | MJEs05s | 0．75 | ORP60 | 0.55 | 2N1306 | 028 | 2N4080 | 0.18 |
| He338 | 0.15 | MPF102 | 0.40 | TIC4 | 0.89 | 2N1307 | $0 \cdot \underline{8}$ | 2N4001 | 0.18 |
| BCY82 | 0.85 | MPFI03 | 0.85 | TIC220D | 1.60 | 2N1808 | － 5 | 2N4062 | 0.14 |
| BCY 8 | 0.88 | MPF104 | 0.85 | TILSOS | 0.20 | 2N1800 | 0.80 | 2N4209 | － 30 |
| BCY 34 | 0.45 | MPFI0S | 0.36 | 2TX107 | 0.12 | 2N1613 | － 11 | 3N125 | 1.76 |
| B0y 70 | 0.18 | NET404 | 1.00 | ZTE108 | 0.10 | 2N1414 | 0.85 | 2N141 | － 11 |
| BCY71 | 0.92 | OAs | 0.78 | 2TE300 | 0.18 | 2N2147 | － 78 | 40860 | － 40 |
| BCY7A | 0.15 | OAl0 | 0.40 | ZTI 301 | 0.14 | 2N2150 | 0.78 | 40861 | － 6.4 |
| HCZII | 0.85 | 0470 | 0.10 | ZTX 302 | 0.18 | 2N2369A | 0.18 | 40382 | 0.40 |
| Indi21 | 1.00 | OAB1 | 0.18 | ZTY 304 | 0.24 | 2N2646 | $0 \cdot 0$ | 40430 | 0.85 |
| 9NT400 | 0.16 | 8N7428 | 0.40 | HN7486 | 0.47 | 8N74145 | 1.26 | 8N74192 | 8.00 |
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| 8N7404 | 0.26 | 8N7438 | 0.87 | 8．7492 | 0.70 | 9N74155 | 1.00 | SN－4198 | 1.20 |
| 8N7405 | 0.22 | MN7440 | 0.28 | SN7493 | 0.70 | sN74156 | 100 | 8N74197 | 1.20 |
| EN740f | 0.42 | HNT44AN |  | 8 B 7494 | 0.80 | SN74157 | 0.95 | 8N74198 | 2.77 |
| 8 N 7407 | 0.42 |  | 0.92 | SN7498 | 0.80 | 8N74170 | 2.68 | ¢N74！日 | 2． 82 |
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| EN7409 | 0.28 | BN7450 | 0.16 | SN7497 | 3.87 | ¢N74175 | 110 |  |  |
| 8N7410 | $0 \cdot 18$ | 8N7451 | 0.16 | EN74100 | 1.89 | SN74176 | 1.28 |  |  |
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# 日 <br> Tr <br> C <br> <br> ELIZABETHAN <br> <br> ELIZABETHAN STEREO TUNER AMPLIFIER 

 STEREO TUNER AMPLIFIER} FOR SPEAKERS AT FANTASTIC
REDUCTIONS

This compact Tuner Amplifier gives you full medium wave and V.H.F. coverage and FM stereo. With inputs for your turntable and tape recorder It has rotary tuning, Volume, Balance, Bass and Treble controls and push button selection switches fo Phono/tape FM Stereo. FM mono, Medium wave and A.F.C. has built-in stereo beacon and switched headphone sacket. Technical Specifications 15 transistors, 11 diades, integrated circuit. Power output 8 watts. Size of tuner amplifier: $4^{\prime \prime} \times 10^{\prime \prime} \times 15^{\prime \prime}$ approx. Finished in selected rosewood veneer with brushed aluminium front panel and matching controls.


## BSB DEEKS WITH PLINTHS ATEATASTICREDUCIONS



MP 60 Type (illustraied) $\quad £ 16 \cdot 00$ Less Cartridge D\& $\quad$ \& $£ 1-50$ C141 (not illusirated) Autlod Whereo C £12.00 Clita Stereo Cartridge Auto. whth Stereo
Crystal Cartridge
All pllnths hnished in matching Teak veneer

BTV C

## THE 'COMPACT'

EASY BUILD SPEAKER KIT
A compact bookshelf speaker system giving a high electro accoustic efficiency for the low powered amplifier
The professional finish can be obtained with the minimum of tools, the infinite baffle type enclosures come ready mitred and professionally tinished, simply apply glue, fold up around baffle board, and fix together with masking tape till glue dries.
The cabinet measures $12^{\prime \prime} \times 9^{\prime \prime} \times 5^{\circ}$ deep approx finished in simulated teak, incorporating a quality $7^{\prime \prime} \times 4^{\prime \prime}$ elliptical speaker, power handling 4 watts, flux density 30.000 maxwells, impedance 8 - 15 ohms nominal, voice coil dia
$\frac{3}{4}$ " magnet size $2 \frac{7}{6}{ }^{\prime \prime}$ approx.
£6.00
pair inclusive. $P$ \& $P\{\$ .70$

## EASY TO BUILD SPEAKER KITS

These superb simulated teak-finished speaker kits have been specially designed by RT-VC for the cost-conscibus hi-fi enthusiast who wants top quality speakers but doesn't want to spend the earth. Built to EMI's exacting specitication, these new RT-VC speaker kits ( 350 type kit) incorporate $13^{\prime \prime} \times 8^{\prime \prime}$ woofer. $3 \frac{1}{4}^{\prime \prime}$ tweeter and matching crossover.
Easily put together with just a few basic tools. Specification (each speaker): Impedance 8 ohms Power handling 15 watts RMS ( 30 watts peak) Response $20-20,000 \mathrm{~Hz}$. Size $20^{\prime \prime} \times 11^{\prime \prime} \times 9 \frac{1}{2}^{\prime \prime}$ approx. Comparable built units (EMI LE3) sold elsewhere for over $£ 45$ pair.

## £22.00 pair complete +55.20 p\&p

Complete with crossover Components and circuit diagram


EMI 350 KIT
$\mathbf{£} 7.25+£ 1.20 \rho 8 p$
Complete with crossover Components and circuit diagram

System consists of a $13^{\prime \prime} \times 8^{\prime \prime}$ approx. woofer with a $3^{\prime \prime}$ tweeter. crossover components and circuit diagram. Frequency response: 20 Hz to 20 KHz . Power handling 15 watts RMS into 8 ohms. (Peak 30 watts.)

## viscoukt iv stereo system

System 1a. $£ 69.00$
The now $20+20$ watt Stereo Amplifier incorporating the latest silicon transistor solid state circuirry. the RT-VC VISCDUNT IV gives you a powertul 20 watts RMS per channet into B ohms. Supert teakfinished cabinet, with anodised fascia to harmonise with any decor. Polished trim and knobs.
The VISCOUNT IV thas a comprehensive range of controls - volume, bass, treble, balance. mono/stereo, mode selector, and scratch filter
Front panel sacket tor stereo headphones And a host of sockets at the rear - for left and right speakers, tape recorder, auxiliary, tuner, disc and microphone.
SPECIFICATION: 20 watts RMS per channet 40 watts peak. Suitable $8-15$ ohms speakers. Total distortion 10 watts better than $0.2 \%$. Six switched inputs: 1 . Magnetic $P \cdot U .-3$ millivolts 47 K ohms (R.IAA.); 2. Crystal/ceramic P.U. - 50 millivolts a 50 K ohms (R.IA.A): 3. 4. 6 Tape Tuner/Aux - 140 millivalts $\& 50 \mathrm{~K}$ othms (flat frequency response): 5 . Microphone -3 millivolts a 50 K ohms (fflat frequency rasponse).
CONTRDLS: Push button ON/OFF, stereo/mono. scratch fitter. 6 position rotary selector. Individual rotary controls for treble, bass, balance and volume. Headphone socket, tape out socket. Aux. mains oupput. Frequency response: 25 Hz to 25 KHz \& full rated output. Sipnel to noise ratio: better than -50 dB on ald inputs. Tone control range: Bass $\pm 15 \mathrm{~dB} 50 \mathrm{~Hz}$ : Treble $\pm 12 \mathrm{~dB} \in 10 \mathrm{KHz}$ Power requirements: 200-250V A.C. mains © 60 watts. Approx. size: $15 \overline{7}^{\prime \prime} \times 3^{\prime \prime} \times 10^{\prime}$ MP60 type deck with maguetic cartridge, de luxe plinth and cover
Two Ouo Type lla matched spaakers - Enclosure size approx $19 \frac{1^{-"}}{} \times 107^{\prime \prime} \times 7 \frac{7^{\prime \prime}}{4}$ in simulated -teak. Drive unit $13^{\prime \prime} \times 8^{\prime \prime}$ with $3^{\prime \prime \prime}$ tweeter. 15 watts handling. 30 watis peak.
Complate Syrtem with these speakers $\mathbf{1 6 9 . 0 0}+\varepsilon 650 p \& p$.

## System 2. £85.00

Viscount IV ampiifieier (As System 1a) MP60 type deck (As System 1a) Two Duo Type III matched speakars - Enclosure size approx. 27" $\times 13^{\prime \prime}$ $\times 11^{\frac{1}{2}}$. Finisthed in teak simulate. Drive units $13^{\prime \prime} \times 8^{\prime}$ bass driver, and two ${ }^{3 \prime \prime}$ (approx.) tweeters. 20 watts RMS. 8 ohms frequency range 20 Hz to $18,000 \mathrm{~Hz}$.
Complete System with these speakers $£ 85.00+£ 7.60$ p \& p

PRICES: SYSTEM IE
Viscount IV R103
mpaltifier $£ 27.50+£ 1.90 \rho 8 \mathrm{p}$ ${ }_{\text {speakers }}^{2 \text { Ovo Type lise }} \mathrm{E} 30.00+\mathrm{Ec} .50 \mathrm{p} \& \mathrm{p}$
 de luxe plinth
and cover $\quad \mathbf{f} 22.00+\mathbf{f} 3.30 \mathrm{p} \& \mathrm{p}$ Total in purchased
superataly: $£ 79.50$
Available complete for anty: $\mathbf{f} 6900$
f6. 50 p \& p.

PHICES: SYSTEM 2
Viscount IV R103
amplifier $\quad \mathbf{f} 27.50+\mathrm{f} 1.90 \mathrm{p} \& \mathrm{p}$.
2 Duo Type III
speakers $\mathrm{E} 46.00+\mathrm{E} 7.50 \mathrm{p} 8$
MP60 type deck with Mag. cartridge
te luxe plinth

Total if purchased
separately: $\quad$ 95S
Available complete for only $£ 85.00$ Scotland and the Orkneys P \& P Surcharge

- $\mathbf{f 7} .60$ p \& p. System 1 a $£ 1.75$ System $2 £ 3.50$


## PUSH BUTTON CAR RADIO KIT=- THE TOURIST TT*



NO SOLDERING REQURED

## NOW BUILD YOUR OWN

 PUSH BUTTON CAR RADIOEasy to assemble construction kit comprising fully completed and tested printed circuit board on which no soldering is required. All connections are simple push fit type making for easy assembly. Fine tuning push button mechanism is fully built and tested to mate with printed circuit board. TECHNICAL SPECIFICATION: (1) Dutput 4 watts RMS output. For 12 volt operation on negative or positive earth. (2) Integrated circuit output stage pre-built three stage IF Module.

Controls volume manual tuning and five push buttons for station selection, illuminated tuning scale covering full, medium and long wave bands Size chassis 7" wide 2" high and 4$\}^{*}$ deep approx.
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## 

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T certainly seems that the era of the quartz controlled digital wrist watch is with us and the price war is going to make them a much more attractive proposition than their mechanical counterpart. Added to their apparent advantages are their novelty value, the "one upmanship" value to their current owners (their status symbol will not last for much longer) and the fact that the constructor with reasonably average ability can make his own from the several attractively priced kits that are now available.

We wonder, however, if the excitment over these devices is a little premature. In their present form are they really a good substitute for their mechanical cousins? We think that the present generation of digital watches leaves a lot to be desired and while we admire the technological achievements in bringing this revolution about we hope that in the next year or so matters might be improved.

For example, do they really tell us the time we require? When we look at our present day wrist watches we are usually making a mental calculation as to "how long we have to wait to catch a train" or "if the bus went five minutes ago what time should we return if they run every 45 minutes". We seldom need to be told the precise time and would rather have an indication of the time difference between now and a future or past event. The conveniently divided face of a conventional watch shows us, at a glance, in multiples of five minutes exactly what we are after without any form of arithmetic calculation- 15 minute periods are even easier to assess. On the other hand a digital watch requires us to carry out a definite arithmetic calculation which, although simple, is open to error. If you haven't got a digital watch make a mental note to check elapsed time on one of the public digital displays at a railway station and then see how much easier it is with your antique analogue display wrist watch

We see two possible solutions to this problem. The first most obvious one is a totally different type of display which simulates a conventional watch face. Admittedly the technical problem is enormous and, at the present time the cost would be prohibitive. One would require at least sixty positions of display elements running radially round the face and then one should be able to select the length and positions of any two elements to depict the hour and minute hands. The numerical value of the positions round the clock face could be engraved in the case material or, conceivably, these could be made to light up as miniature LED displays. A second type of display which might be more practicable in the light of current manufacturing costs is a couple of "Line of Light" displays each one made up of 60 dots.

Our second solution would be to make more use of the logic capabilities of LSI integrated circuits. Rather than build calculators into a wrist watch would it not be better to have a chip which will accept a specified time from a miniature keyboard? The display would immediately show the difference in time (either positive or negative) between now and then. While we like the arithmetic nicety of our second solution we cannot, honestly, see it catching on because of the inconvenience factor.

It would be interesting to hear if readers have any views on this subject and at the same time it would be nice if someone could explain to us the value of a digital wrist watch that automatically compensates for leap years on a four year cycle when the batteries run down every year!

LIONEL E. HOWES-Editor

## PRACTICAL WIRELESS MAGAZINE REQUIRES A TECHNICAL EDITOR

If you feel that you are the person to fill this challenging and rewarding position write to the Editor, Practical Wireless, IPC Magazines Ltd., Fleetway House, Farringdon Street, London EC4 4AD.

## Radio Licence Fees

TTHE Wireless Telegraphy (General Licence Charges) (Amendment) Regulations 1975 were laid before Parliament to apply from 1 December, 1975, an 'across-the-board' increase of $60 \%$ to all fees for the standard radio licences, except broadcast receiving licences. Fees for standard radio licences have remained unchanged since 1968.

Standard-form licences are specified in the Schedule to the Wireless Telegraphy (General Licence Charges) Regulations 1968. They include licences which authorise the transmission and reception of radio by ships, aircraft, mobile radio-telephones, radio-microphones, radio-paging devices, radars, radio beacons, radio amateurs and model control.

The Home Office states that the increases are now necessary because the income from fees is no longer sufficient to cover the cost of licensing and administering the particular uses of radio.

The new rates are as follows: Private Mobile Radio $£ 6 \cdot 50$ for the first two stations and $£ 3 \cdot 60$ for each subsequent station. Ships $£ 5 \cdot 50$; Aircraft $£ 4$; Model Control £2.40 (5 years); Amateur £4•80; Induction Communication $£ 4 \cdot 80$ ( 5 years); Induction Communication (with return speech) $£ 6 \cdot 50$; Radio Paging $£ 7 \cdot 20$; Radio Paging ( 27 MHz ) (with return speech) £16; Radio Paging (UHF systems) (with return speech) $£ 26 \cdot 40$; and Radio Microphone $£ 4 \cdot 80$.

BARRIE Electronics telephone number was printed incorrectly in both the December and January issues. It should have read $01-488-3316 / 7 / 8$. We apologise for any inconvenience caused.

## Oui Oui

THE next Paris Components Show, or to give it the correct title, Le Salon des Composants Electroniques, will be held at the Parc des Expositions, Porte de Versailles from April 5th to 10th, 1976.

## Eagle Laboratories

TTHE TEST and development laboratories at Eagle International of Wembley have recently been acoustically treated and re-equipped with new Bruel \& KJaer instruments at a cost of $£ 12,000$. These instruments are the standard for acoustic and electro-acoustic measurements anywhere in the world.

Eagle International are manufacturers and distributors of highfidelity, in-car, public address, intercom and test equipment and a wide range of electrical and electronic components. The new laboratory instruments will enable the most accurate measurements of frequency nesponse, signal-to-noise ratio, distortion, etc., to be made on amplifiers and tape recorders. Comparison measurements can be made on loudspeakers and microphones. The effect of acoustic treatment in the laboratories has been to reduce the reverberation time at 1 kHz from $2 \cdot 0$ seconds to less than 0.2 seconds.

Picture shows Percy Gander, Technical Director of Eagle International, testing an Eagle A2006 Amplifier on the Bruel \& KJaer instruments in the re-equipped laboratories at Precision Centre, the company's Wembley headquarters.


## Heard buit not seen

3Mhas recently put into full-scale operation its new tape manufacturing facility at Gorseinon, near Swansea. The $£ 3^{1}{ }_{2} \mathrm{~m}$ scheme includes an automatic cassette assembler known as the 'Snowflake', and a number of cassette winders known as 'Raindrops'. These, coupled with the firm's tape coating machine, are now producing a range of cassettes which exhibit marked improvements over the previous handassembled models.

Scotch Dynarange, New High Energy, Chrome and dual-layer Classic cassettes are now all manufactured on 3M's automatic assembly lines. The mechanics are common to each range within the Scotch family .... 3M's Recording Materials Division is so confident about the trouble-free operation of its cassettes that it is currently calling them "The Jambusters" in a national retail campaign which highlights their jam-free properties.

Detailed improvements in Scotch cassette design include the following: (1) Larger, permanently fixed one-piece pressure pad for better head-to-tape contact and signal uniformity; (2) Posi-Trak backing-a tape backcoating process for a smooth wind and reduction of static-induced dust attraction which can lead to annoying drop-outs (3) Fixed polished metal guideposts which eliminate the mechanical movement associated with nylon wheels and so reduce wow and flutter.

In addition, 3M claims that its ultrasonic welding technique produces a warp-free housing for the tape. The company points out that the 'Snowflake' machine will accept only components that are made to very fine tolerances, and will in fact physically reject any part which is below specification. No fewer than 25 quality control checks are made during cassette manufacture, including the tests made during manufacture of the tape itself.

Any Scotch cassette found to be faulty will be replaced immediately by the retailer under 3M's no quibble guarantee. Recording Materials Division, 3M United Kingdom Limited, 380-384 Harrow Road, London W9 2HU Tel: 01-286 6044.

## E.B. Catalogue



If you would Ilke a copy of this instrument catalogue send 50 (UK) £1 (overseas) to Electronic Brokers Ltd., 49-53 Pancras Road, London NW1 2QB. It will prove invaluable to schools, colleges, universities and covers items from Transfer Osci/lators to Pen Recorders and Distortion Measuring Equipment to Muitimeters.

## High and Mighty

MEMBERS of the South West Face British Everest Expedition took with them a Hacker Super Sovereign RP75MB five-band receiver. It was supplied by Hackers in a special weather protective casing.

## Semicomps move

SEMICOMPS Limited have moved to new premises at Wellington Road, London Colney, St. Albans, Herts, AL2 1EZ. Telephone: Bowmans Green 24522. S.C.S. Components, the division responsible for sales to the amateur and TV service industry, will move at the same time to the above address.
Coincidental with the move is the installation of an $L 8500$ Burroughs computer programmed to handle all functions of the Company other than stock control. This machine is being installed in anticipation of an upturn in business activity during 1976 and will enable at least a 50 per cent increase in orders without the need for additional staff.

## 2 CHANNE: <br> STEREO MIXER <br> A. Joyce C.Eng MIERE



THE majority of stereo music centres have the facility for recording via a microphone, or from either a radio, disc player or auxiliary sources. The facility of microphone recording is usually underemployed, as results at recording especially with music accompaniment are usually poor. If an extra record player or other source is used for this purpose, the difficulties of correct balance and room acoustics become very evident and impair the results obtained.

Attempts at making tapes for home movie accompaniment etc. prove to be difficult due to the editing and mixing limitation. However, if a tape deck is chosen as the additional alternative source, and a mixer unit is constructed, all the drawbacks are overcome. The ability to feed the input of the tape deck into the music centre, and vice-versa,
enables one to edit tapes in both directions, although it must be said that unit matching may be necessary. The ability to use the source to act as an accompaniment to the microphone, requires the use of a mixer, and in either editing or mixing, all re-recordings are achieved electronically and are relatively unaffected by room acoustics. The unit described here, was designed with all of these requirements in mind.

## CIRCUIT CONSTRUCTION

It would be fairly easy to evolve a printed circuit board for the amplifiers, but the plain veroboard and terminal pin method was chosen, since this permits easy alteration to component values for


Fig. 1: Circuit diagram of one of the microphone amplifiers. The other is identical, but its components have been given the suffx ' $a$ ', in the component list.
experimentation, and places no restrictions on the physical size of components. Two $0 \cdot 1$ in matrix plain veroboard panels $140 \times 45 \mathrm{~mm}$ are used, with one being employed for the microphone amplifier, Fig. 1,


为

Fig 2; The mixer amolifier shown left has two inputs. The music input feeding direct from the DIN sacket, and the microphase Input feeding via the mic. ampll fier. Again the secand channel is itentical with components suffixed ' 2 '.
and the other for the mixer amplifier, Fig. 2. Both having right and left channels, the left channels being virtually mirror images of the right channels. The earth rails are kept to the bottom of the boards so that they are near to the chassis connections. The positive rails are mounted near to the top of the boards so that a cross wire from the power supply suitably connects the positive supply to the boards.

When starting the construction, it is advisable to place the components on the board and then push in the terminal pins as dictated by the spacing. The component wires may then be given a loop around the pin and the surplus cut away. When all the particular wires to a pin have been madc. soldering can take place. After the veroboard wiring has been completed a thorough check should be made, and if all is OK, they should be put to one side for future chassis mounting. All inter-amplifier connections and switching leads Fig. 3, are made with screened cable. the outer of which is earthed. Colour coding of the leads is employed to assist in checking and/or fault finding.

The power supply unit Fig. 4, is constructed on the chassis which is to be described later. The transformer has two sets of LT windings which should be paralleled to obtain the $15-0-15 \mathrm{~V}$ output. The bridge rectifier is bolted to the smoothing capacitor bracket, while the regulaton transistor is clamped to the aluminium screen with its connecting pins facing inwards. The screen incidentally, acts as a very useful heat sink. An LED was added in the prototype, and connected in series with an appropriate resistor. The value of which determines the intensity of light output and current drain on the supply.

## AMPLIFIER GAINS AND UNIT MATCHING

The gains of the amplifiers are determined by the ratio of the feedback resistors, (R5 and R10 in Figs. 1 and 2,) to that of the input impedance (approx. $50 \mathrm{k} \Omega$ ). The mixer amplifier values given will have a voltage gain of two, and the microphone amplifiers a


Almost all of the components are mounted on the two plain Veroboards. The top board contains the microphone amplifier while the lower one contains the mixer amplifier. These boards are shown full size.

voltage gain of 66. Some alteration of these values may be necessary depending upon the input levels, although a higher voltage gain for the microphone amplifiers is not advisable, as the frequency response of the output may suffer:

Values are not given for the inter-unit attenuating resistors, as these should be selected to satisfy the input/output levels and impedances of the basic units.

## CHASSIS CONSTRUCTION

The top and rear of the unit acts as the chassis, with all the components mounted underneath. It is made from 20 SWG aluminium sheet $256 \times 200 \mathrm{~mm}$,
bent at right angles to form a top $204 \mathrm{~mm} \times 200 \mathrm{~mm}$, with a back about 52 mm in depth. This then slides into the base retaining case from the rear, along the side top-edge grooves. It holds itself by the front and side grooves and may be secured with screws in the side back edge cuit aways, or into an additional back strut fixed on the hardboard base. This forms a solid box construction with easy chassis access.

The component parts which require basic chassis mounting are placed on the underside of the top panel section to achieve a reasonably spaced layout, Fig. 5. Their positions are marked, and the slots for the slider potentiometers are cut. The holes for the end brackets of these pots are additionally used for

## components list




Fig. 4: Regulated power supply circuil diagram. The transformer T1, is a 6VA $0-15 \mathrm{~V}, 0-15 \mathrm{~V}$ 240V type with the two secondaries wired in parallel. C12 and C13 inay be substituted for a single 10,000 нF electrolytic.
securing the veroboard panels in a vertical position. This minimises top panel drill holes, while the screwheads are ultimately concealed by adhesive bezels.

The holes for the power supply screen fixing, and holes for sockets, pilot lamp, switches, fuse and mains lead are now marked and drilled, and the
wood effect formica or adhesive contact vinyl.
The top and sides of the aluminium chassis may also be covered in the wood effect vinyl and the self-adhesive slider bezels put on top of this before the knobs are finally fitted and general labelling carried out.


Fig. 5: Internal pholograph showing component layout, board positioning and power supply. The vollage regulator is mounted on the aluminium screen adjacent to the transformer and smoothing capacitors.
fixed components mounted. The power supply smoothing capacitors are now secured by a clamp fixed to the internal screen which also holds the regulator transistor. The veroboard panels are now mounted and a check made that sufficient clearance still exists. All inter-board and switch connections can now be made, with a final check being made before power is applied.

## CASE CONSTRUCTION

The case size of the prototype was pre-determined by making it identical in size to the tape deck, and in this instance was $215 \mathrm{~mm} \times 220 \mathrm{~mm}$ by 10 mm deep. The retaining case of the unit has a hardboard base, with 12 mm thick wooden sides and front. These are rebate grooved 6 mm from the inside top edges. The sides only are additionally cut away at the back to a depth equal to the rebate groove. The front and sides are then glued and pinned at the corners and base. A finish can be applied to the case, by either using

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Subscribers should place an order with their local newsagents so that they may continue to receive their magazine on a regular basis.

## pu"Easubuild" <br> 

IN THIS the final part of the P.W. Disco system articles, we will look at construction of the cabinet, interwiring and construction of the mains and mixer panels, fault finding and use of the Disco.

## MIXER CONSTRUCTION

The photographs and drawings clearly show details of mixer construction (Fig. 11). As noted before, tandem pots are required for stereo, together with a balance control and mono/stereo switch. A mono mixer would use single gang pots and would not have either the balance control or the mono/stereo switch.

The drawings are for a stereo mixer but for clarity only one section of each of the tandem controls has been shown. The wiring for the second channel is simply duplicated.

The chassis for the mixer is a piece of $1^{1}{ }_{2} \mathrm{~mm}$ ( $1 / 16 \mathrm{in}$ ) double-sided copper laminate which is earthed, and screens the input circuitry. All earth connections are simply made by soldering directly to the copper.

The completed mixer is so simple that a visual check should reveal any faults.

## MAINS PANEL

To reduce the possibility of hum pickup, the mains switching, fuses and light modulator controls are mounted on a separate mains panel which is situated at one end of the sloping console panel well away from the mixer (Fig. 12).

On/off switches for the amplifier and sound-tolight unit are mounted on the mains panel together with their two respective fuses, the light modulator intensity control, and three over-riding switches, one for each light channel. These switches short out the thyristor in each channel giving full output of each colour for special effects.

[^1]
## PANEL PREPARATION

Both the mixer and mains panel can be conveniently made from 1.5 mm ( $1 / 16 \mathrm{in}$ ) fibreglass laminate. After drilling all necessary holes the panel can be covered with non-glossy white 'Fablon' and lettering applied with Letraset. A thin spraying of clear polyurethane or Letracote gives the surface some protection. The Fablon is cut away with a modelling knife to expose the component mounting holes. When fixing the controls to the panel a washer should be used underneath the pot nut to prevent the Fablon pulling when the nut is tightened.

## PLINTH ASSEMBLY

Arrangements have been made for a complete cabinet kit to be available in knock-down form as shown in the diagram (Fig. 13). Constructors who enjoy woodwork can prepare the pieces as shown in the cutting list. Attention must be paid to the long mitre joints of the panels $E, F$ and $G$. These


The two turntables mounted in the deck board with the front panel attached ready for foining to the plinth assembly.


Fig. 11: Construction of the mixer, made from double-sided copper board, one of the sides being used as a common earth plane.
must be cut very accurately and the mitre angle maintained to ensure that the edges mate.

Assembly is quite straightforward and is summarised in the steps below. lin $x$ lin timbers are used for all right-angled joints.

1. Screw side panels G to baseboard C.
2. Screw lampholder panel D to baseboard C and side panels G.
3. Screw panel A to baseboard C and side panels G, first cutting out for the spot bulbs.
4. Screw panel $F$ to baseboard $C$ and side panels G.

At this stage all the electronics should be installed.
A professional finish can be ensured by using countersunk mirror screws which have brightly chromed flat heads. The three lampholders for the light display are fixed to panel D spaced as shown in the diagram so that the reflectors will coincide with the apertures in the front panel.

The light modulator p.c.b. is mounted on 25 mm (lin) stand-off insulators as shown in the photograph. The mains wiring between the p.c.b. and the lampholders and switches is twisted lightly together to reduce radiated interference.

The plinth base is drilled for large ventilation holes and the power transistor heatsinks (two for stereo) are mounted directly above. By spacing the heatsinks 38 mm ( $1_{2}$ in) from the bottom of the plinth, plenty of space is left for free circulation of cooling air. Although by no means essential a small instrument cooling fan could be set into the base to provide additional draught.
Stand-off insulators are used to mount the amplifier boards adjacent to the heatsinks.

## INTERWIRING

Both the mixer and mains panels are now fitted on to the control panel using small chrome-plated wood screws. The control panel is then dropped in place. Screened cable is used for the connections between the mixer and amplifier boards. The braidings should all be connected together and earthed at one end-this is most easily done at the mixer.


Fig. 12: Interwiring of the mains panel. This again is made from double-sided copper laminate board.


Next the mains panel is carefully connected, taking great care to check the connections against the circuit diagrams. When dealing with mains voltages there must not be the slightest possibility of an error occurring.

The mains earth goes from the input plug to the light modulator board and the main earth point. The following earth returns should all be taken direct to this earth point: power supply negative; right-hand amplifier power earth; left channel

speaker return; right channel speaker return; turntable metalwork.

A short link of heavy gauge flexible wire connects the left-hand amplifier power earth to the corresponding point on the right-hand p.c.b. The earth connection from the mixer is also connected to the right-hand amplifier earth.

It is at this stage that the unit can be tested if the separate sections have not already had bench tests. Adjustments are made as detailed earlier.

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## LIGHT SWITCH



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## Below are some of the items in our December Wewtiettor.

Cannon plug, 37 pin with flex. grip. Difto socket erip. 82 per psir +16 p Post 20 p

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All that now remains is to cut out the plinth top panel to suit the two turntables and screw it to the back panel, A. The two decks are mounted in the plinth and wired to both mains and the mixer. The plinth top panel simply screws to the rest of the console. The control panel can be secured after the final tests.

The pickup cartridges are mounted as in the deck manufacturer's instructions and the turntables set to the required tracking weight for the cartridge ( 4 g for the 9TAHC).

## EXTERNAL INPUTS

External inputs are provided for Tape ( 150 mV ), MICROPHONE ( 4 mV ). AUXILIARY $(300 \mathrm{mV})$ and two external pickups, Pu1 and Pu2 ( 20 mV ).

The tape and aux inputs will accept the outputs from most radio tuners, cassette or tape recorders and any other equipment offering a "line" output. Equipment such as TV receivers and certain radios and record players have live chassis power supplies and no attempt should be made to connect these to the inputs of the Disco Console, or indeed to any other equipment.

The microphone input is intended for use with medium quality dynamic types. Should any tendency towards bass boom be noticed, then the bass boost switch can be set at the "off" position.

The pickup inputs are effectively in parallel with the pickup cartridges installed in the console and serve as external pickup sockets or as outputs for feeding to a headphone monitor amplifier for cueing or, Pre Fade Listen (PFL).

## MIXING

Operation of the Mixer is self-explanatory and the layout of the control panel assist easy operation. Each input has an associated level control which is used to adjust the overall balance between inputs and for smooth selection of one or other input.

The cross fade control is used to swing from one turntable to the other for a smooth change of record. At intermediate positions of the control the two turntables are mixed.

The balance and volume controls are used together with the bass and treble controls to adjust the sound level and tone for the room. Adjustment of the balance control may be necessary to compensate for differing loudspeaker efficiencies on each channel.


The completed Disco system.

## OPERATION OF THE DISCO CONSOLE

The amplifier used in this design will deliver its maximum power of 100 W into a load of $4 \Omega$. Naturally speakers of adequate power rating should be used if the unit is to be played loud and a number of speakers can be combined on each channel to achieve the required impedance. For example, two $8 \Omega 50 \mathrm{~W}$ loudspeakers or four $15 \Omega 25 \mathrm{~W}$ speakers in parallel would be suitable.
To minimise power loss the connecting cable should be heavy duty. When several speakers in different cabinets are to be paralleled, least power loss will occur if the parallel connections are made near to the Console. In this way the length of cable carrying the combined speaker currents will be reasonably short.

## LOUDSPEAKER

Heavy duty loudspeaker drive units suitable for Disco applications are widely advertised in the electronics magazines. Generally a single unit is designed to cover a fairly wide frequency response and additional tweeters are rarely used: high power tweeters are very expensive. Sealed infinite baffle enclosures are usually employed, the constant volume air damping serving to restrain cone movement. To reduce internal resonance or "boxiness" the internal walls are lined with wadding to absorb any reflections.

When two or more drive units are fitted in a cabinet it is important to connect them in phase so that the cones move together. Otherwise the air damping will not be effective. Phasing can be simply
continued on page 857


Fig. 15: Layout of the controls on the front of the mixer and mains pane/s which are mounted on the sloping front panel of the Disco console.


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# Dadio Break-through A lookat interference in Hi-Fi equipment_-............art 1 



AGLANCE at the problem pages in the various audio magazines soon indicates two complaints which have become uncomfortably common with audio equipment in the last few years. The first problem is the unwanted break-through of radio stations, the second being "noises off" originating from refrigerators and other thermostatically controlled devices. Several articles have appeared in which these problems and possible cures have been discussed, but what has not been pointed out is that these problems originate from the same deficiencies in the audio system in that it is too sensitive to radio frequencies.

## NATURE OF INTERFERENCE

It may come as a surprise to realise that refrigerators generate radio waves, but when pioneers such as Marconi were spanning the Atlantic the power they fed into the aerial system was generated by a spark, and the code they sent consisted of what we would now consider to be little more than bursts of interference. Whilst 'fridges and switches and other units which generate sparks radiate over a wide frequency range, Marconi's "interference" was concentrated as much as possible around one frequency by means of a tuned circuit, but the principle is the same.

Obviously it should be possible to suppress refrigerators and light switches to stop them interfering with audio equipment, but this is rather a pointless operation as it still leaves the audio equipment wide open to any other radio waves which are strong locally.
High fidelity amplifiers (if they are to be worthy of the name) must amplify small signals over a wide range of frequencies until they are powerful enough to operate the loudspeakers, and a good case can be made out (in the interest of minimum distortion and best transient response etc.) for having the frequency range over which they operate somewhat wider than the normal audio range.

The frequency response of an amplifier is, perhaps, something with which the advertiser can impress the uninitiated, and hence even before the "transistor invasion," we started to see specifications such as "flat from $1 \mathrm{c} / \mathrm{s}$ to $1 \mathrm{Mc} / \mathrm{s}$. ." The fact that some of these units also produced cannon-like crashes from every switch or thermostat in the house, and brought through a local radio amateur or taxi radio operator seemed to be ignored in the interests of progress! Valiant attempts were made to pass the problem on to the refrigerator manufacturers, station operators, Post Office engineers or anyone else who would hold it in their lap with the hope, perhaps, that if the problem was ignored long enough it would go away!

Radio frequency interference ( RFI ) has, however, refused to go away, and with the advent of the printed circuit board and the transistor, the situation has certainly not improved, much domestic audio equipment being far too sensitive to any form of electromagnetic radiation. With the numbers of refrigerators, freezers, central heating systems and radio transmitters of all kinds mushrooming at the same time as sales of inadequately protected audio equipment, it looks like things are going to get considerably worse before they get better!

Fortunately some of the more enlightened audio manufacturers have sat up and taken notice, and it is to be hoped that their efforts, perhaps urged on with the threats which recent legislation seems to hold over the retail trade, will eventually result in more adequately protected equipment. In the meantime it is hoped that the following will put the matter in perspective and hopefully help readers to cure troubles with existing installations and perhaps even influence designers of audio equipment.

## SOME THEORY

Before the audio content can be extracted from an amplitude modulated (AM) radio wave it has to be detected. In the detector stage of a receiver the active device, usually a diode, is connected so as to be non-linear. However all valves and transistors will detect radio waves to some extent if they are subjected to a strong enough signal, pushing them on to the non-linear part of their characteristics.
Compare the circuit of a simple crystal receiver with that of the first stage of a transistorised amplifier, Fig.1. Here the similarity is very apparent, particularly if it is remembered that the transistor is only a development of old-fashioned crystal diode. The complete crystal set naturally incorporates an


Fig. 1: A simple untuned crystal receiver, left, can be compared with a typical trans/stor audio amplifler stage.
aerial and a tuned circuit to enable one to select

- the required station. The audio system does not deliberately incorporate either, but any wire will act as an aerial and in the absence of tuning any strong local signals are picked up on the, often, too generous speaker, pick-up, tape, mains or other interconnecting leads.

It is possible to fit filter chokes to the various leads and, in most cases, to cure RFI troubles even where an inadequately protected amplifier is involved. On the basis that protection is better than a cure we shall look at basic amplifier design and see what can be done by the manufacturer. Service engineers and the more knowledgeable enthusiast will see the possible modifications that may be incorporated in existing equipment.

The writer would warn that alterations to the circuit panels of amplifiers should only be undertaken by those who have the experience and test equipment needed to sort out any difficulties that may arise. Radio amateurs in particular are warned that it is bad policy to undertake internal modifications to other people's equipment as one tends then to be automatically blamed for any subsequent faults that may arise.

## SIGNAL HANDLING CAPABILITIES

Before a stage can detect radio frequencies it has to be pushed to the non-linear part of its characteristic. Stages which are designed to handle a few millivolts of audio are therefore much more likely to act as unwanted detectors than are driver and output stages which will handle much larger signals without overloading. Improvements in transistor technology have tended to extend the frequency response of all small audio transistors well into the VHF range so that their improved characteristics have made the problem worse. This is a point worth remembering should an old amplifier suddenly develop RFI problems after it has been serviced, as it is just possible that by replacing an old transistor with a modern type, unwanted VHF or UHF reception may occur where it was not previously evident.


Flg. 2 : A resistor and capacitor connected as shown here can frequently eliminate interference from an audio stage.

Most unwanted noises in amplifiers tend to originate in the input stages not because these stages make the most noise, but because the input stages are followed by a great deal of amplification and hence the smallest inputs are greatly magnified. The same argument applies to RFI problems as the smallest amount of signal detected in, say, the pickup input stage will still produce a very considerable sound from the loudspeaker. Fig. 2 shows how RFI
protection can be added to such a stage. Note that the sensitive part of the transistor is the base/ emitter junction so the capacitor must be connected as shown and not between base and chassis.

## CAPACITORS

Capacitors in practice possess inductance, and even resistance, as well as the required capacity. Maximum possible effectiveness in reduction of RFI susceptibility would necessitate a perfect capacitor soldered in with zero length leads. In practice the best type of capacitor to use is the disc ceramic and if this is soldered in with the shortest possible leads the inductance and resistance will be small enough to make it effective up to the VHF range. The best value of capacitor is a compromise as it is desirable not to affect the response of the amplifier at the higher audio frequencies.


Fig. 3: RFI is often introduced into amplifiers via input cables when their screening is not properly earthed. Capactior shown dotted should be fitted to all such cables.

When modifying a stereo amplifier it is as well to add the capacitors in one channel only so that any adverse effect on the frequency or square-wave performance can be judged by comparison with the unmodified channel. Usually it is best to fit the largest values of capacitors possible without affecting the audio response unless the RFI is above 5 MHz or so when there is no need to fit a capacitor more than a few hundred pF. Remember, that to be effective at the higher frequencies the leads must be very short, as an inch of connecting wire will add enough inductance to make the capacitor completely ineffective in the VHF region.

Above 100 MHz or so it becomes increasingly impossible to make Cx (Fig.2) effective and here Rx comes into its own. If Rx is several hundred times the input impedance of the transistor unwanted VHF and UHF signals will be reduced in proportion. In cases of trouble with break-through of radar, or other extremely high frequency signals, the length of lead from Rx to the transistor and Rx itself may even act as an aerial. In these extreme cases a cure can usually be effected by slipping a few ferrite beads on to the base lead of the transistor. This modification converts the lead into an RF choke and can be quite effective in the VHF range as well.

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$0-5 \mathrm{~mA} \quad 170 \quad 0-5 \mathrm{~mA}$
$0-10 \mathrm{~mA}$
$0-50 \mathrm{~mA}$
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50 Volts
Prim 200-240V gec. $19,25,38,40,807$

|  |  |  |  |
| :---: | :---: | :---: | :---: |
| Amp | Ref. | Price | Post |
|  | No. | $f$ | 2 |
| 0.5 | 102 | 2.71 | 0.61 |
| 1 | 103 | 3.58 | 0.76 |
| 2 | 104 | 5.30 | 0.85 |
| 3 | 105 | 8.10 | 0.85 |
| 4 | 106 | 7.97 | 1.08 |
| 6 | 107 | 12.93 | 1.18 |
| 8 | 118 | 18.75 | 1.44 |
| 10 | 119 | 17.79 | 1.86 |

60 Volts
Prim. 280 2407.
Sec. $24,30,40,48,60 \mathrm{~V}$.

| Ampt | Ref. | Price | Post |
| :---: | :---: | :---: | :---: |
|  | No. | ع | * |
| 0.5 | 124 | 2.51 | 0.72 |
| 1 | 126 | 3.75 | 0.72 |
| 2 | 127 | $5 \cdot 36$ | 0.85 |
| 3 | 125 | 7.91 | 0.97 |
| 4 | 123 | 8.80 | $1 \cdot 18$ |
| 6 | 40 | 10.22 | 1.18 |
| 6 | 120 | 18.10 | $1-36$ |
| 8 | 121 | 15.74 | O.A. |
| 10 | 122 | 20.10 | O.A. |
| 12 | 189 | 18-87 | O.A. |

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Prim. 240V with mroen.


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| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Price | Price | Price |  |
| VA | Ref. |  | Plugs | Open | Post |
| Tapped st 115, 220, 240 Volts |  |  |  |  |  |
|  |  |  |  |  |  |
| Tapped at 115, 200, 220, 240 Volts |  |  |  |  |  |
| 150 | 4 | 8.89 | 0.25 | 4.28 | 72 |
| 200 | 65 | $7 \cdot 67$ | 0.25 | 5.21 | 0.78 |
| 300 | 66 | 8.67 | 0.25 | 6.11 | 0.85 |
| 500 | 67 | 11.82 | 0.25 | 9.48 | 1.18 |
| 750 | 83 | 14.81 | 0.95 | 11.30 | 1.28 |
| 1000 | 84 | 18.38 | 0.95 | 14.35 | 1.44 |
| 1500 | 93 | 23.28 | 0.95 | 19.28 | O.A. |
| 2000 | 95 | 35.07 | 1.80 | 25.48 | O.A. |
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Besides protecting the individual sensitive stages of an amplifier, it is also advisable to restrict the ways that radio frequencies can gain entrance to the circuit boards of amplifiers, especially in the low level stages. Naturally on any properly installed equipment one would expect all pick-up, tape, radio and any other low level connections to be well screened, but as will be seen this screening is not at all effective at the radio frequencies with which we are concerned.

As an examination of most amplifiers will show, the "earthy" side of the input socket is not connected to chassis but is returned to the main printed circuit panel. This is done to achieve a one-point earth arrangement in the interest of minimum hum. Fine as this arrangement may be from a hum point of view, it is very unsatisfactory as far as RFI is concerned, as radio frequency signals which are present on the outside of the screen of the connecting cables go down to earth via the amplifier's printed circuit panel. Printed circuits can have quite an appreciable impedance at radio frequencies which results in radio frequency voltages being developed across the board and, likely as not, being injected into the sensitive stages of the amplifier, Fig.3.


FIg. 4: After treatment of transistors all input sockets should have by-pass capacitors fitted with the shortest possible leads.

Fortunately there is a simple remedy for this problem, this being to connect a capacitor from the earthy side of each input socket directly to chassis, as shown. Once again the value of the capacitor will be somewhat of a compromise, a few hundred pF being the best at the higher frequencies, and perhaps say $0 \cdot 1 \mu \mathrm{~F}$ or so if troubles are due to a station on the long waves. In practice a disc ceramic capacitor of about $0.01 \mu \mathrm{~F}$ connected with the shortest possible leads between the earthy side of the input sockets and chassis will be found quite effective at most frequencies.

## THE SUGDEN A21 AMPLIFIER

Several years ago the Sugden A21 stereo amplifier did not contain very much RFI protection. It gave excellent sound quality and sold well but retailers, such as my company, found that customers were complaining of hearing calls from local radio amateurs, taxi stations or clicks and plops from thermostats and electric lights. Fortunately James Sugden, the designer, was (unlike some who could be named!) only too anxious to improve his product in any way possible. A high power amateur radio transmitter was used to carry out some tests. The results of these tests were that capacitors were added between base and emitter of each of the four transistors in the preamplifiers, and one added directly behind each of the input sockets, Fig.4.

## TO BE CONCLUDED

DISCO STEREO SYSTEM-continued from page 850.


The completely interwired mixer panel viewed from the rear.
checked by connecting a 4.5 V battery across the speaker terminals and seeing that both cones move in the same direction.

Phasing is also important when connecting a number of cabinets to the console and it is useful to colour code loudspeaker leads to eliminate guesswork -the usual code is that when the red lead is positive the cone moves outwards.

With an output power of 100 W per channel, this Disco Console is capable of producing very high sound levels and apart from the general nuisance aspect it should be remembered that research has shown that regular exposure to high sound levels can be damaging to the hearing mechanism.

With the best will in the world it is possible to construct a piece of equipment which turns out to be faulty on 'switch-on'. Any faults in the pre-amp section can be easily traced but the power amplifier poses some problems as it is a DC coupled design.

To reduce the possibility of damage three 24 V 12 W bulbs can be connected in series in place of the 2A DC fuse during testing. The lamps will limit the short circuit current to a relatively safe 500 mA , while still giving virtually the full supply voltage if the ampli. fier is not drawing excess current. Under no signal conditions the amplifier should operate with Tr15 emitter (Tr16 collector) at half supply voltage. Trll emitter should be at almost full supply voltage.

When a new amplifier has been put together using 'off-the-shelf' components which may have been stored a while it may be that the electrolytics are not properly formed, giving rise to an initial surge at 'switch-on' which may damage $\operatorname{Tr} 9$ or $\operatorname{Tr} 10$. To reduce the possibility of damage in this way only fresh electrolytics should be used, otherwise stored components should be formed before use.
Note: In the components list in Part 1, under Power Amplifier, Miscellaneous, the heatsinks specified should be as follows: R.S. Type 154 heatsinks for Tr11, $\operatorname{Tr} 111, \operatorname{Tr} 13, \operatorname{Tr} 113, \operatorname{Tr} 14, \operatorname{Tr} 114 ;$ and $\operatorname{TO} 03$ insulating kits for $\operatorname{Tr} 15, \operatorname{Tr} 115, \mathrm{Tr} 16, \operatorname{Tr} 116$.

Also it has been found that an improvement in performance is obtained by increasing R19 to $560 \Omega$.

In Fig. 2 C 13 should be $10 \mu \mathrm{~F}$ as stated in the components list.

In the Light Modulator components list, $p 782$ January 1976, C30 should be $8 \mu \mathrm{~F}$ and C32 should be $0 \cdot 5 \mu \mathrm{~F}$ as in Fig. 5, p 783.
NOTE: In Part 2 Fig. 5, bottom of secondaries of T2, T3 and T4 should go to cathodes of SCR's and not to anodes (neutral) line. In Fig. $6 \mathbf{C 1 1}$ should read C12 and vice versa.

## THE U115B

ONE of the dreams of amateur radio set builders was a radio which was contained on a single chip. One popular path to this dream was the ZN414 IC which contains a very useful t.r.f. approach. I hear that a new chip will shortly be introduced to professional set manufacturers which could be of great interest to home constructors. The magic number to remember is U115B.
The U115B is reported to contain, on its $2 \mathrm{~mm}^{2}$ surface, all the major functional bits and pieces for an a.m. receiver plus an f.m. demodulator. It appears that the only components external to this IC are the various tuned circuits-tuning capacitor and coil, i.f.t's, etc. and a potentiometer to control volume although it is also reported that certain discrete devices are also needed for the f.m. circuitry. If one was only interested in a.m. then presumably very few external components would be required to build a superhet receiver.

One problem often associated with this type of chip is that there is only sufficient drive available at the output to give very small power, and further stages of audio amplification are commonly needed. Not so with the U115B. The chip contains tuner, local oscillator, mixer for a.m. reception, demodulator ditto, i.f. stage, a.f. amplifier, and an f.m. demodulator. The range for acceptable working voltage is very wide; from 3 V to 11 V , and the twist in the tail is that it will provide 800 mW into $8 \Omega$ which, of course just conveniently happens to be one of the standard impedances for loudspeakers.

## L.E.D. DISPLAYS

Digital displays are now commonplace and are employed in a wide variety of applications. Those which use the l.e.d. approach usually require some form of driver stage to literally drive the l.e.d. arrays and some form of memory is also often employed too. I was pleased to note that one manufacturer is marketing an l.e.d. array in which the numbers are formed by a series of l.e.d's
arranged in a dot pattern. That in itself is not, of course, so special. However, something else is built in on the same chip-all the necessary decode and drive circuitry. If that isn't enough, a memory is also included and the whole thing has just eight pins in a dual in-line configuration.
The display itself is almost $0 \cdot 3 \mathrm{in}$. high and it is also TTL compatible. All you (the user) have to do is simply to address the device directly with a four-line BCD input. I fear that before very long, even more circuitry will end up on the chipperhaps even the user will find himself there one day.

## CQ!

Early Amateur radio stations comprised a transmitter, receiver and frequency meter. The latest commercial stations offered to the Amateur are compact, table-top units which house all these separate items in a single package. I see that an instrument manufacturer has followed this approach and now offers an oscilloscope, digital multimeter and a digital counter all in a single, compact case. It really is a very desirable property, but I will not mention further details (a) because of lack of space, (b) so's not to make you discontented with what you have and (c) the price would ruin your New Year. Keep smiling!

## ENERGY

I note with interest that in the US much work is bubbling on the photocell front. Energy from the sun, and with no moving parts is a great attraction-and the energy so gained is free-my life. Of course, one hears lots of rumours about cell efficiencies etc. but practical details are harder to come by. However, I hear that one array of cells on order (to be delivered shortly) will provide some 40 kW of energy. Elsewhere I hear that a number of companies in the US are ready to supply panels of cells around $6 \times 4 \mathrm{ft}$ providing some $5 \frac{1}{2} \mathrm{~W}$
per square foot. There is even mention of 50 -cent cells by 1980 .
While on the subject of power, hands up if you've heard about the latest in long-life batteries. Not those that your dealer is always trying to "cell" you (sorry, pun intended) but those using nickel and hydrogen. These new beasties are claimed to offer up to four times the watt/hours per pound as is currently available from state-of-the-art nickel-cadmium cells. No further information at present but sufficient to say that the US military are already designing these batteries into their satellite programme. Definitely batteries that will be out of this world!

## AHH SO!

Damn clever those Chinese-but are the Japanese even more clever? Certainly one electronics company is trying hard to prove that this is the case. Early in 1976, one Japanese company is to launch what is thought by many (including mistress Ginsberg) to be the most elaborate channel selection device ever. It has been developed specially for use with colour televisions and it allows the owner/viewer to programme in his selection of chosen TV programmes for the day. The readout on the TV screen itself displays the time selected and the channel selected at that particular time. Once programmed, the device will automatically select or tune the appropriate channel at the correct time Up to 16 programmes can be selected and "dialled" in.
The circuit is rumoured to contain a chip which is only just over $5 \mathrm{~mm}^{2}$ and contains nearly 8,250 transistors. No mention of price but what with extra sophistication driving the prices up, plus more than a little help from inflation, 1 really do wonder if The Six Million Dollar Man will be watched on the Six Million Dollar TV Set!

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## Jaraday 3yecture

THE 1975-76 Faraday Lecture, organised by the Institution of Electrical Engineers, is being given by F. Howard Steele, Director of Engineering at the Independent Broadcasting Authority. His lecture, "The Entertaining Electron", unravels the technical mysteries of television.

The first presentation of the Lecture took place in The City Hall, Cardiff on Monday, November 24th at 6.30 p.m.

Mr . Steele is assisted by two deputy lecturers: Alan James, the IBA's Network Manager and Dr. Boris Townsend, Head of the IBA's Engineering Information Service.

Each year the Institution of Electrical Engineers invites an eminent electrical or electronic engineer to present the Faraday Lecture. The Lecture was instituted in 1924 to commemorate Michael Faraday, the British physicist who in 1831 discovered electro-magnetic induction and so set in motion a whole new industry.

The lecture tour programme is as follows: Birmingham, The Town Hall, 26-27 January, 1976; London, The New London Theatre, 3, 4, 5, 6 February, 1976; Exeter, The Great Hall, Exeter University, 26 February, 1976; Bradford, St George's Hall, 9 March, 1976; Nottingham, The Albert Hall, 11 March, 1976; Liverpool, Philharmonic Hall, 19 March, 1976; Manchester, Free Trade Hall, 22-23 March 1976; Glasgow, The Kelvin Hall, 21 April, 1976; Edinburgh, The Usher Hall, 23 April, 1976; Newcastle, The Newcastle City Hall, 27 April, 1976; Portsmouth, The Guildhall, 4 May 1976.

The presentation follows the Faraday tradition in its many
practical demonstrations and working models-but it also borrows from television production techniques in exploiting audiovisual aids including film, videotape and large screen television displays.
The Lecture makes full use of a special, complex mobile stage in explaining both the technology and the role of engineering in the production and presentation of television programmes.
The latest technological developments that may help to mould the shape of television during the coming decade are explained in a manner that seeks to make them understandable and meaningful to the interested lay-man, irs an informative yet entertaining manner.

The Lecture ranges over the developments of the technology, from the earliest Baird 30-line television, to optical waveguides, quadraphonic sound and Oracle teletext.


Baird's 'Televisor'
-Science Museum Photograph.

Modern colour television operations will be explained with the aid of film and video-tape recordings, with some of the first displays to be given in the United Kingdom by means of a new "large-screen" television display system.
The advances made possible in the unfolding pattern of television technology with the aid of computers will be emphasised by teletext, by the latest DICE standards conversion and by such applications on adaptive aerials that adjust under the control of a small computer to minimise interference from several different sources.

The mobile stage will permit a series of demonstrations in which the aim will be to show how science and engineering have become so much a part of everyday living that the viewer takes the technology virtually for granted-but technologists continue to seek new ways of using "the entertaining electron" to create ever more convincing illusions and to expand home entertainment systems into new and exciting fields.

Tickets for the Lecture are free and are available from Mrs. B. Newman, IEE, Savoy Place, London, WC2R OBL. The Lecture lasts approximately $1^{1} 4$ hours.

## 建aird Television 1930

THE "Televisor" (see left) was manufactured by the Plessey Company for Baird Television and was priced at 25 guineas. It was intended for reproduction of Baird's 30 -line transmissions which the BBC radiated on an experimental basis from 1929 onwards.

The picture signal from the owner's radio receiver varied the brightness of a special neon lamp having a rectangular luminous electrode. The lamp was viewed through the 30 small holes arranged in a spiral round the outside of the large disc which rotated at 125 revolutions per second. This form of scanning had been patented by Nipkow in 1884.

A magnifying lens in front of the disc increased the effective picture size to about $50 \times 75 \mathrm{~mm}$.

The motor driving the disc was synchronised by means of a cogged wheel on its shaft which was in between the pole-pieces of an electromagnet energised by the picture signal.

## Hectronic plumber

Working on the principle of "fools rushing in, etc." and realising all that was needed was a good plumber with a small blowlamp I had a go at the TeleTennis project. I went a bit mad with the ferric chloride bottle but after a couple of attempts the boards were made and the thing worked. All praise for the clear instructions which I realise must frustrate the pundits as even I was able to cope.
There is one problem arising. Now, being an electronics expert, as acknowledged by my daughters, they consider that a small organ of a couple of octaves would be a piece of cake by Christmas! So what about it, PW?
-P. J. Gale (Aylesbury) P.S.-Yes! The kids are better at the damned game than me! (Thank you for the fow kind words Mr. Gale, your wish was granted in the January issue. We hope it will make a suitable Christmas project for very many of our readers. Incidentally, we think you are being just a bit too modest about your constructional abilities!)

## Short thanks

I would like to thank the gentleman who sent me 'PW' July 72 for which I asked in your CQ column.
He did not enclose name and address but it was postmarked Leeds.

Incidentally, I have on three occasions replied to a "CQ" offering assistance to a query but in no case have I received an answer.W. G. Philpott (Rye, Sussex).

## Boost your signal

Reading your October issue of $P W$, I noticed the article on a signal booster for portable radios. I lost no time in constructing a mock-up of the design and can confirm its efficiency. However, I think you will find that it is unnecessary to amplify the output of the coil if a reasonably good aerial is used. If the coil is made to a similar design as the ferrite rod aerial in the I.C. tuner (also in the supplement) all that is necessary is for the unit to be positioned, with the core aligned with that in the set. I find it desirable to wind this coil in such a way that it tunes from 200 to 550 m when the aerial and earth are connected to the extra ends. There will be some signal loss if taps, separate coupling coil or series capacitor are employed. This means finding the number of turns by experiment.
I have not yet tried the long waves, but I think the results should be similar, though I suppose the coupling would not be quite so efficient.
I feel sure your readers would be glad to know that signal boosting can be obtained this way without the complication of transistors and associated extra com-ponents.-K. H. Smith (Ross-onWye).

## What price progress?

Derek Bell's notes in the December issue of Practical Wireless (Shortwave broadcasts, p701), about the oldest set in regular use, prompts me to write about an Amplion "Delegate" which my wife bought at a jumble sale a year ago, for twenty pence.

Having replaced a broken dropper resistor, and receiving nothing but a cultured hiss, I was led, by intuition and experience to the oscillator/mixer valve, where however, voltages seemed normal. Replacing the valve gave no joy. After hours of cogitating, I was reduced to quite purposeless poking at the valve-holder tags with a plastic knitting needle. Suddenly, the set burst into life, but died again when the prod was removed.

When the valve-holder was
broken open, I found that the interior connection had corroded away. If I had done what the books say, and measured the voltages at the valve pins, instead of the valve-holder tags, I should have been all right!

The only clue to the age of the set, is the marking of the various Radio 4's as "London Regional", "North Regional", and Radio 2 as "Light". It uses a barretter (imagine!), and is contained in a lovely inlaid walnut rectangular cabinet $330 \times 205 \times$ 165 mm . The speaker is hidden behind a beautiful set of tiny louvres. It is a little cracker; the aerial socket is connected to the outer braiding of a disused TV aerial, and on SW, the Voice of America may easily be received. I think it has a wider frequency response than most modern portable AM receivers, and is in regular daily use.

One wonders just where miniaturisation has taken us; this set uses five large valves, whopping IF transformers, large air coils, and a barretter to boot. Yet in size, it is no larger than the average modern portable set.
H. Padmore (Blackpool)

## Sockel-to-me

At the time of writing, one of your advertisers, CT Electronics, has for sale small signal TO18 (BC107/8/9) transistor sockets. After having purchased a fair number of these sockets, I've found a simple way of modifying them for 4 and 6 lead IC's like the $\mu$ A703 used in the SW Pre-amplifier September '75.

The correct socket for this device costs around 35 p, but the 'CT' sockets cost $4{ }^{1}{ }_{2} \mathrm{p}$ each. Two are required for each four or six lead device.

To construct these, file the 'open' edge of the socket until the two small pips on the underside are half removed. The filed edges of the two sockets should now be Araldited together making a single unit. This arrangement will hold the IC tightly with a little careful bending of the leads, and is of course very much cheaper.M. J. Shepherd (Canvey Island).

Have you ever wished that you could gel some radio programmes 11 your cassette player? Build this simple funer unil and load it into your player wherever you gel fed up with your lapes.


Crystal Calibrutar


Using seven cheap CMOS devices this calibrator provides outputs to well above 30 MHz from a 1 MHz crystal. Decade dividers provide outputs down to $\mathbf{1 H z}$ if required, for checking counters and other digital circuitry at speeds slower than normal.


ALL THE
REGULAR FEATURES
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THIS receiver covers approximately 500 kHz to 30 MHz and is constructed so that it can be developed by the addition of extra stages, which in turn give better reception and extra facilities such as the reception of CW and SSB. Because a large, comprehensive receiver has circuitry which can represent quite a long period spent on construction, before it is finished and can be operated, there is considerable advantage in beginning with a simpler circuit, to which further stages can be added. A working receiver is then obtained quickly. Difficulty in locating a fault in a relatively complicated receiver is also avoided, as the working of extra stages will be checked as they are added.

## CIRCUIT DETAILS

Shown in Fig. 1 is a block diagram of the whole circuit, but only stages $2,3,5$ and 7 need be wired initially to obtain a receiver of good general performance. A brief description of the function of each section in Fig. 1 should be of help in understanding how the receiver is improved as optional stages are added.
(1) The RF amplifier is a protected dual-gate FET giving a worth-while increase in sensitivity. Being tuned the RF stage also helps to eliminate second channel interference. An RF gain control is
fitted as strong signals can overload the mixer.
(2) FET mixer, to which the aerial may be taken directly when making the basic receiver. Output from this stage is at the intermediate frequency of 1.6 MHz .
(3) FET separate oscillator. It must be noted that the devices in stages (1), (2) and (3) use valve type coils, not transistor types.
(4) An optional intermediate frequency stage to increase sensitivity and selectivity. It can be used as a crystal filter with a single crystal and phasing capacitor. The maximum selectivity obtainable with such a circuit is high, but selectivity is easily degraded or the crystal cut out to provide optional levels of selectivity, and for the reception of AM.
(5) This section has two IF amplifiers, with five $1 \cdot 6 \mathrm{MHz}$ tuned circuits. So there are seven tuned circuits in all when (4) is used giving the IF section good skirt selectivity to reject unwanted signals.
(6) This is an optional pre-amplifier to boost audio signals, and may not be felt necessary in some cases.
(7) An audio IC which requires few components and gives sufficient loudspeaker volume from a 9 V battery supply. As with any receiver having considerable gain it is of course, possible to overload
Fig. 1 : below, is a block dlagram to show the functions of the various stages. Those stages in heavy outline are the essential ones for the basic recelver. Fig. 2, right, is the circuit for the first three stages but the RF stage, Tri, can be omitted initially, as explained in the text.


output (or even other) stages, so the gain and volume controls have to be operated in a sensible manner.
(8) The beat frequency oscillator/carrier oscillator allows reception of CW and SSB signals. A.s an envelope detector can give satisfactory CW and SSB reception, in addition to $A M$, when the relative strengths of CW/SSB on the one hand, and BFO on the other, are suitable, this type of detector is provided in section (5).
(9) A regulated supply for the oscillators is not essential but avoids frequency modulation effects, particularly when the extra stages or BFO are in use.

This simple-to-build design makes life very easy for those building their first receiver. The set is soon operational on any required range with just one set of coils. Further optional stages can be added, one at a time, finishing off with the switching of the four ranges to provide coverage of the medium wave band and all the short wave bands.
Facilities provided by the complete receiver include:

> RF Amplifier Bandspread Tuning Beat Frequency Oscillator Crystal IF Filter Noise Limiter Mains Power Supply Unit.

## TUNING ARRANGEMENTS

A 3-gang capacitor tunes stages (1) (2) and (3). Layout is arranged to allow addition of a ganged bandspreading capacitor later, which is useful for Amateur or other narrow short wave bands. To obtain best performance without banks of pre-set trimmers, stages (1) and (2) have panel trimmers. These allow the peaking up of weak signals at any frequency and with almost any aerial.

The bands covered are approximately as follows

("Range l" being the maker's long wave band, which is omitted):

$$
\begin{array}{ll}
\text { Band } 1 \text { (Range 2) } & 1500 \text { to } 500 \mathrm{kHz} \\
\text { Band } 2 \text { (Range 3) } & 1.7 \text { to } 5 \cdot 0 \mathrm{MHz} \\
\text { Band } 3 \text { (Range 4) } & 5 \cdot 0 \text { to } 12 \mathrm{MHz} \\
\text { Band } 4 \text { (Range 5) } & 13 \text { to } 30 \mathrm{MHz}
\end{array}
$$

Coverage may be adjusted to include the 1500 1700 kHz sector, but it should be understood that instability must be expected around the 1.6 MHz region in this case, the receiver IF.

Bandchanging is by plug-in coils. Advantages of this are the simplicity plus avoidance of a multi-way switch. There is also no need to purchase coils for bands not wanted. A set of coils can be changed in a few moments, and even this is not necessary if most interest is in one particular range of frequencies. However, the layout is arranged so that bandswitching can be added later, the switch and coils occupying the space below the RF/mixer/ oscillator assembly.

It is not necessary that the optional stages are added in the order in which they are described, as some other combination might be preferred. For example, the BFO could be added to sections $2,3,5$ and 7, instead of later.

## METALWORK

Assuming that the bandspreading and other extra controls will be fitted eventually, it is best to punch or drill for these at the beginning. Unused holes in the panel can be covered, or have the controls only installed. The layout of units will be seen from Fig. 3. The panel is $12 \times 7$ in and the chassis is $10^{1}{ }_{2} \times 6^{1}{ }_{2} \times 2 \mathrm{in}$. Place panel and chassis together and mark the holes on the chassis. To fit the cabinet the panel edge is about ${ }^{3}$ in below the chassis. Panel and chassis are held together by the controls, or initially, by bolts with large washers.

The bandsetting and bandspreading capacitors have their spindle centres $3{ }_{4}$ in apart. Bolt the main tuning capacitor directly to the chassis. Slotted or enlarged holes, with washers. will allow the exact


View of the RF-Mixer-Oscillator unit of Fig. 2. The aluminium containers in which the coils are supplied are used as screening cans.
position to be adjusted a little, if necessary, to line up with the drive correctly. As the bandspreading capacitor is smaller it is raised with 4BA nuts so that its shaft is at the same height. Small holes can be drilled in the chassis later, provided metal fragments are not allowed to fall into the capacitors or other components, but large holes should be made before mounting any parts.

The cabinct could be prepared later. Punch or cut holes (at least lin in diameter) opposite aerial, earth and speaker sockets. If the top is to be made to open, to reach plug-in coils or the battery, either of two methods can be used. Both have been found satisfactory, but the second takes longer.
(1) (The easy way!) Drill out the six rivets which hold the top to back and sides. Pivot the top by two 6BA bolts through the side rivet holes near the


Fig. 3: Details for marking out the front panef. Most of the holes will be itin. diameter but check with actual componenls used, It is advisable to drill all the holes from the start even if the optional slages are not added untiil fater. After fitting the chassis to the panel check that they fit into the catinnt properly.

back. Fit a small knob or terminal head to lift the lid, which closes on the side flanges of the case.
(2) Mark off about lin from the sides, front and back. Drill small holes to start a metal saw and cut out this piece. Clean the edges with a file, and fit a cabinet hinge (or two small hinges) at the back. The opening part rests on two $6 \times$ lin strips bolted inside and projecting into the aperture. Fit a lifting knob.

## RF, MIXER AND OSCILLATOR

The circuit of these stages is shown in Fig. 2. The RF stage can be omitted, as described, but is included here so that the method of connecting it
is clear. If the RF stage is not used, connect the aerial to 9 of coil L2, taking pin 8 to chassis. Tr 1 and all components up to C4 and R5 are then not required.
VC1/2/3 is the ganged capacitor for main tuning, while VC4/5/6 is for bandspreading. Capacitors VC7 and VC8 are panel trimmers to peak the aerial circuit L1 and mixer circuit L2. With the oscillator trimmer TCl set at about half capacitance, no other trimmers need be fitted.

A "Blue" coil is used for L1, a "Yellow" coil for L2, and a "White" ( $1 \cdot 6 \mathrm{MHz}$ osc.) coil for L 3 . Pl to P4 are individual padders, automatically in circuit for each range. Pin $X$ of the "White" coils is different for each range, so that only the required padder is

actually in circuit. Potentiometer VR1 controls Trl gain by changing the gate 2 voltage. Tr3 is the separate oscillator and it can be supplied either from the 9 V line, or from a zener stabilised circuit, when the BFO is fitted.

It will be realised that three coils (Blue, Yellow and White) are used for any one band, but that coils need not be obtained for bands not required. Range 4 is best for general short wave reception, while Range 2 can be omitted if no MW reception is wanted. Range 3 coils would cover both LF Amateur bands, 80 and 160 m . Coverage on each band depends on the core setting of L3 and all cores are adjusted so that some threaded rod projects. With TC1 suitably adjusted. VC7 and VC8 should
peak signals' near the high frequency end of a band ( $\mathrm{VCl} / 2 / 3$ nearly open). The cores of L 1 and L 2 are then set so that little re-adjustment of VC7 or VC8 will be needed near the low frequency end of the band ( $\mathrm{VCl} / 2 / 3$ nearly closed).
Some misadjustment of L1 or L2 will cause no loss of efficiency, provided VC7 or VC8 is not fully open, or fully closed for best results. As initial wrong positioning of L1 or L2 cores, or VC7 or VC8 can result in complete loss of signals, check these if needed when first using a new range of coils. Subsequently, if L3 or TC1 is adjusted to obtain correct coverage, readjust the aerial and mixer to suit.
It should be noted that the IF transformers are

Fig. 5. Circult of the IF ampiliter stages and detector diode D1. Ensure that the diode is connected the right way round. Fig. E: on the next page, shows the commanent and wiring sides of the if ampliper board, Cheek that the BF194 goes into the Tct mositlon and the BFY95. into the 1 tis locitian.



Board $3^{\prime \prime} \times 1^{3} / 4^{\prime \prime}$

pre-aligned to 1.6 MHz by the maker, so their cores should be left alone, except for a final small adjustment. The aerial, mixer and oscillator coils, however, are supplied in metal cans and for this reason are not set, and the cores must be screwed so that several turns of rod project, as described.

To leave the chassis clear below, the coil holders are fixed to the top of a metal frame $5 \times 2 \times 1^{1}$ in high, see photograph. This is readily made by taking an $8 \times 2 \mathrm{in}$ flanged "universal chassis" side and cutting a 90 -degree portion out of each flange $1^{1}{ }_{2}$ in from the ends, so that a right-angled bend can be made. Secure a piece of $0 \cdot 15$ in matrix plain perforated board with 6BA bolts. Wiring can then be carried out as in Fig. 4. The board is shown flat so that the wiring can be seen. Bolt a $2 \times 1^{1}$ in metal screen between aerial and mixer coil holders (it can be cut from a spare universal chassis side) and fit a coil can lid at each holder position. This is done by punching valveholder holes in the lids and holding them with the bolts which secure the coil-holders.

Fig. 4 shows the lead-outs for the RF mixer, and oscillator devices. "MC" points are tags bolted to the box. Connections should be short and direct and wiring and components for the aerial and RF circuits should be clear of Trl drain and later tuned circuit components. It is helpful to put short pieces of coloured sleeving on the FET leads, say red for drain, white for gate 1, brown for gate 2, and leave source leads bare.

Leads for external circuits are required, and may also be colour coded for easy identification later. A wire (blue) from pin 8 Ll is long enough to pass through the chassis to the aerial socket. Leads run from pin 6 of L1 (brown), pin 6 of L2 (brown) and pin 1 of L3 (black) to VC1, VC2 and VC3. A lead (pink) from Trl G2 circuit runs to VR1. A connection (grey) goes directly from drain of $\operatorname{Tr} 2$ to the IF amplifier. Positive circuit connections can be made to pins or by flying leads. Two leads run from MC tags at L1 and L2, Fig. 4, to the rotor contact plates of the ganged capacitor, to provide short RF circuits.

When this unit is finished it is placed near the ganged capacitor when it can be tilted sufficiently to allow soldering the leads to $\mathrm{VCl} / 2 / 3$. These should be as short as possible. The unit is set in position on the chassis and secured with self-tapping screws from below. Cut down Tr1 G2 lead and solder to VR1. R2 is soldered directly to VR1. A lead from VR1 runs to positive on the board.

A vertical screen was found necessary between RF and mixer leads to the bandspreading capacitor, when this was fitted, see photographs. It can be cut from a universal chassis runner. Wires running down from the tuning capacitor to the, panel trimmers should also be clear of each other. Trimmer TC1 is soldered to stiff leads from VC3.

When coils are fitted, small holes in the top of the screening cans allow the cores to be adjusted. Screening of all the coils is essential when the RF stage is fitted. The possibility of the RF stage becoming unstable as the RF gain control is advanced depends somewhat on frequency, as well as on loading by the aerial and the shielding mentioned is to prevent this.

## BASIC IF AMPLIFIER

This is unit (5) in Fig. 1 and employs the circuit in Fig. 5. The mixer drain will be connected to pin 1 of IFT1. When the additional IF amplifier is made,


Front ;iev of the receiver with only the basic stages fitted. The unused holes can be blanked ofi. They also act as a strong incentive to complete the optional stages.


Fig. 7 : centre, is the circuit of the TBA800 aurilo oulput stage. Capacitor C17 is connected directly across VR2 and C16 is wired directly between D1 and VR2 so they do not appear in Fig. 8. Initially, test and align the recelver with a battery for power. Later a mains power unit can be built and used for routine listening. Such a unit is shown in the fhotograph above and details of its construction will tie given next month.


Fig. 3: The circult of the audio stage Fig. 7 is laid out on veroboard as shown here. The holes in the board may need enlarging slightly to take the pins of the IC. Note that the socket for the loudspeaker, fed from this board, must be completely isolated from the panel.
this connection is removed. The mixer drain is then connected to the IFT of the extra stage and the collector circuit of this stage is taken to pin 2 of IFT1 in Fig. 5.

In Fig. 6 is shown the assembly and wiring of the IF amplifier. First drill threc holes for the 6BA bolts MC and the lower core access holes of IFT] and IFT2. The IF section is located behind the bandspread capacitor. Place the bare board on the chassis and mark or drill the holes mentioned. Components are then fitted as shown in Fig. 6. The three MC tags are secured with ${ }^{1}$ in bolts. Extra nuts on these allow the board to be mounted so that leads clear the chassis. External connections can be made on the board or leads.

When this section is fitted and working a slight adjustment to the cores may be necessary, for best results. Use a correctly shaped tool (such as the Denco TT5) as a wedge-shaped blade may crack the cores so that they jam. Clip a $10 \mathrm{k} \Omega / \mathrm{V}$ or similar high-resistance meter, set to the $2 \cdot 5$ or 10 V range, from diode negative to chassis. Tune in a stable signal correctly (a BBC local MW transmission is suitable) and adjust VC7 and VC8 for maximum meter reading. Then rotate the five cores of the IFTs a little either way, as required, to give the best meter reading.


Plan view of the cormpfefind receiver with all stages fitted. The small board to the right of the IF amolifier board is the extla IF stage with a crystal filter to be described next month. The smaller gang capacitor to these left is for Dandspreading.


Fig. 9: Details of the battery supply circuit. The stabilised supply at 6.2 V is part of the BFO circuit and can be used to feed the first oscillator stage if required. The photograph below is the back of the basic receiver with the audio board in the foreground, the If amplifier at left centre and the mixer and oscillator assembly at the far end.


## AUDIO AMPLIFIER

Fig. 7 shows the circuit of this section which is wired on a separate board, as in Fig. 8. This is prepared and fitted to the chassis near VR2, in a similar way to the IF board. Though a $1 \Omega$ resistor is not difficult to obtain two $2 \cdot 2 \Omega$ resistors in parallel can be used instead. Note that the speaker output jack socket contacts must both be isolated from the metal chassis. This requires a socket of all-insulated type, or with a "dead" bush, or the use of insulating washers. An alternative is a pair of separate sockets for wander plugs.

This stage should take about 8 to 10 mA , rising to 20 to 30 mA with average volume. The TBA800 tabs are bent up to clear the board, but are not soldered to a heat sink. An $8 \Omega 2$ speaker may be used, but current drain is a little higher than when a $15 \Omega$ unit is connected.

## BATTERY CIRCUIT

Fig. 9 will be of assistance in wiring the battery circuit. Battery positive goes to the switch on the volume control VR2. A lead from here runs to positive on the audio amplifier. The board has a spare positive pin, to which a $220 \Omega$ resistor is soldered, and the lead from here runs to the positive pin provided on the IF amplifier board. A $1000 \mu \mathrm{~F}$ 10 V capacitor is connected from this pin to a chassis tag. When the lst or additional IF stage is fitted, this positive point supplies it also, as in Fig. 9.

When the BFO is not fitted, supply the oscillator stage $\operatorname{Tr} 3$ via a $3 \cdot 3 \mathrm{k} \Omega$ resistor from the positive tag of the IF board ( $1000_{\mu} \mathrm{F}$ capacitor positive). This point also supplies the RF and IF gain controls. When the BFO is fitted, it provides a 6.2 V stabilised point, which is connected to the BFO switch, as in Fig. 9. This point also supplies ine oscillator $\operatorname{Tr} 3$ via a $1 \mathrm{k} \Omega$ resistor. This resistor, and the $3 \cdot 3 \mathrm{k} \Omega$ resistor mentioned, is additional to the resistor in the RF/mixer/oscillator assembly, so that it can be easily changed when the stabilised circuit is available.
NEXT MONTH:-ADDING THE BFO, EXTRA IF STAGE WITH CRYSTAL FILTER, INTRODUCING BAND-SWITCHING.

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## 'CURRENT DUMPING' QUAD AMPLIFIER



Quad announced their 'current dumping' amplifier a short time ago and we can now show a picture of the unit. 'Current dumping' describes a new technique used in the output stages.

Essentially, a current dumping amplifier comprises a heavy-duty high power amplifier (the current dumper) which provides nearly all of the current drawn by the load-and a high quality low power amplifier which provides the control. These are so arranged that any error in the high power section is exactly compensated by an error signal from the low power section. Thus performance is solely dependent upon the low power amplifier, which can be made very good indeed.

Since the output device linearity is not important, biasing is unnecessary and crossover and thermal tracking problems disappear. The output devices themselves need not be matched thus allowing inherently more reliable types to be employed.

The Quad 405 is the first practical realisation of this new circuit technique. Designed to drive modern low efficiency loudspeakers, the 405 has an output of 100 W per channel into $8 \Omega$ with a claimed total distortion of less than $0.01 \%$ at mid frequencies.

The Quad 405 costs $£ 115$ plus VAT. Quad, The Acoustical Manufacturing Co. Ltd., (Dept. P.W.), Huntingdon, PE18 7DB.

## GOLDRING DECK KIT

A belt-driven turntable constructional kit has recently been announced by Goldring Limited.

Called Model CK2, it comes complete with detailed instructions so putting it all together is fairly simple. The deck has two speeds ( $33 \frac{1}{3}$ and 45 RPM) selected by a rocker switch. Simplified belt coupling to a small low-speed synchronous motor reduces rumble. Wow and flutter is said to be kept within a $0.15 \%$. The pickup arm is counterbalanced with adjustable stylus pressure from 0.5 g . There is a removable plug-in shell and an anti-skate device.


The kit, which is an easy-toassemble version of the G. 102 Turntable assembly, costs £27. Further information may be obtained from Goldring Limited, (Dept. P.W.), 10 Bayford Street, Hackney, London, E8 3SE. Telephone 01-985-1152.

## 12V MINI DRILL



Precision Petite Ltd. of Teddington market a miniaturised drill $(125 \mathrm{~mm}$ in length) for 12 V operation which has been designed for comfortable holding in the hand thus enabling extremely precise work to be carried out-even drilling holes of some tenths of a millimetre. A very comprehensive range of tools and accessories ranging from grindstones to milling and routing burrs is available and the firm will be pleased to supply full details on receipt of a stamped addressed envelope.

The drill on its own costs $£ 7$ with postage and packing of 35p and a drill stand for vertical drilling is $£ 3.75$ ( +58 p post and packing). A complete kit of accessories-comprising 30 tools costs $£ 15.01$ (p.p. 75p) and a transformer for mains operation if required is priced at $£ 5 \cdot 50$ (p.p. 75 p). -Precision Petite Limited, (Dept. P.W.) 119a High Street, Teddington, Middlesex, TW11 8HG. Tel. 01-977-0878.


## AMPLIFIER KITS

Our advertisers Radio Component Specialists of Croydon tell us that they have released a new amplifier in kit form. Called the RCS 'Minor' 10W amplifier, it comes in two ver-sions-mono or stereo. The mono kit uses 13 semiconductors and the stereo version 22 semiconductors. Volume, bass, treble and mains on/ off controls are mounted through the front panel which has white lettering on a black background.

The specification reads: 10 W into 8 ohms; 7W into 15 ohms. Response $=20 \mathrm{~Hz}$ to 30 kHz with distortion at less than $0.5 \%$. Noise $=-60 \mathrm{~dB}$. Input, up to 200 mV . Size of completed unit, $240 \mathrm{~mm} \times 75 \mathrm{~mm} \times 50 \mathrm{~mm}$ ( $9 \frac{1}{2} \times 3 \times 2$ in.).

The kit comes complete with full instructions, printed circuit board, fascia panel and all components. The mono version is $£ 12 \cdot 50$ and the stereo version £20 (VAT included). Postage on either kit is 45p.-Radio Component Specialists, (Dept. P.W.) 337 Whitehorse Road, Croydon. Tel. 01-684 1665.


The Heathkit ID-1590E Digital Electronic Wind Speed and Direction Indicator kit features a bright 2-digit planar gas discharge readout to display wind speed. During construction, one picks out the two readout modes one requires from three available-miles, knots or km per hour. A switch on the rear panel chooses either of two selected modes and front panel lights show which is in use. A rear-panel switch and controls on two circuit boards calibrate the ID-1590E.

The wind direction indicator uses incandescent bulbs to mark 8 principal compass points. Two adjacent bulbs light at the same time to indicate an intermediate direction.

Installation is said to be very simple -the remote transmitter boom clamps onto any 1 to $1 \cdot 5 \mathrm{in}$, rooftop TV aerial mast and is connected to the receiver unit with optional cable. The kit for the ID-1590E costs £49 including 8\% VAT and delivery within the UK. Cables come in three lengths-50ft ( $£ 5 \cdot 30$ ), 100ft. ( $£ 9 \cdot 20$ ) and 150ft. (£14-30). Heath (Gloucester) Limited (Dept. P.W.), Bristol Road Gloucester, GL2 6EE.


## STEREO CAR RADIO

Radiomobile Limited, announce an AM-FM stereo car radio, model 1190 FMS. It employs a six button tuner, combined with manual tuning, facilitating simple pre-setting of any 3 FM, 2 Medium wave and 1 Long wave station. Amplifier produces 5 watts per channel and a bass/treble tone control is provided. A balance control allows adjustment from left to right channels. The FM stereo tuner employs Active Interference Rejec-tion-a complete circuit module.
Automatic Frequency Control circuitry provides spot-on tuning and a DIN socket provides the facility of accepting the input from a stereo tape deck.
Technical Specifications:
Power supply: 12V negative earth; current consumption: 0.5A (up to $2 \cdot 5 \mathrm{~A}$ at maximum output).

Tuning ranges (Minimum): FM: $87 \cdot 5-104 \cdot 5 \mathrm{MHz}, \mathrm{MW}: 525-1620 \mathrm{kHz}$, LW: $150-275 \mathrm{kHz}$. Semiconductors: 70 (41 transistors, 3 integrated circuits, 26 diodes). Speaker impedance: $1 \cdot 75-3 \cdot 5$ ohms per channel. Tape socket sensitivity: 30 mV for 5 watts output per channel. Further details and latest prices from Gill Turner, Radiomobile, Good Relations Ltd., (Dept. P.W.) Kimbolton House, 117 Fulham Road, London, S.W.3.


The Radiomobile 1190 AM/FM radio.

## CASIO CALCULATORS

Casio, the multi-million pound Japanese calculator and electronics group, has established a subsidiary company in the U.K. known as Casio Electronics Co. Ltd. The firm's primary aim is to market a range of low-cost pocket calculators and a recently developed electronic watch.
In Japan, Casio claim to have $54 \%$
struction. There is also a 4-way constant facility. The readout is on a green digitron tube panel, unnecessary zeros being suppressed. An LSI chip is employed and power consumption is 0.2 W . Provision is made for a mains PSU but the Personal Mini has its own internal batteries which give about 10 hours' continuous use. (HP11's).

The Caslo Personal Mini calculator. Recommended price £6.95, but some of our advertisers are offering them for under $£ 5 /$

of the domestic market and claim that they are the world's largest manufacturer in this field. This new UK subsidiary joins similar organisations in Germany and the USA.
One of the firm's most successful calculators is the Casio Personal Mini which has already sold over 5 million units in three years. This model divides up to 6 digits, adds, subtracts and multiplies up to 12 . Should the wrong button be pressed, pressing the 'correct' (C) button automatically cancels the previous in-

At the other end of the range is the FX-101 10-digit scientific calculator with independent memory and scientific notation. It handles a broad range of calculations up to $10^{ \pm 9 \theta}$, and has a veryimpressivespecification. Recommended price of the Personal Mini is $\mathbf{2 6 . 9 5 - b u t ~ s e e ~ P . W . ~ a d v e r t s ~}$ for discount prices. Full details may be obtained on the whole range of Casio equipment from Mr. R. G. Rayner, General Sales Manager, Casio Electronics Co. Ltd., (Dept. P.W.) 28 Scrutton Street, London, EC2A 4TL.

## Now...the most exciting Sinclair kit ever

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# SIMPLE ULTRASONIC 

IF one wishes to control a relay from a remote unit without the use of any connecting wires, one must utilise some form of wave signal which travels between a transmitter and a receiver. Radio waves and microwaves are very suitable for this purpose, but the equipment required is usually fairly complex and expensive and a licence must be obtained before the equipment can be used. Another possibility involves the use of light waves which fall on a photosensitive cell. In this case the main problem is that the system is also sensitive to daylight. Sound waves can be used, but the region is then rather unpleasant to work in and the equipment responds to spurious noises.

## ULTRASONICS

Ultrasonic communication utilises waves in the air which are just like sound waves except that their frequency is so high that one cannot hear them. This article describes a very simple transmitter unit and receiver unit which can be used for the remote control of a relay in the receiver. The relay closes when 40 kHz waves from the transmitter fall on a transducer in the receiver.
Although ultrasonic transmitter and receiver units have been published from time to time, the units to be described here have the advantage that very simple circuits are employed; the only active devices required are a single IC in each of the two units.

The maximum range at which satisfactory operation can be attained is generally of the order of 10 m . It is not possible to quote an accurate value for the range, since it varies considerably with the presence of reflecting objects. The range is considerably greater in an indoor corridor than in the open air, since the walls of the corridor reflect the waves towards the receiver unit. The waves are attenuated as they pass through the air and this limits their maximum range for reliable control.

## TYPICAL APPLICATIONS

Ultrasonic beams can be used to operate a relay and the closing of the relay contacts can then be used to perform any desired switching operation. For example, an ultrasonic transducer can be mounted on the front bumper of a car. When the driver reaches his home, a pulse from the transmitter is used to actuate a relay which automatically opens the garage doors without the driver leaving his seat. When the car is taken out of the garage, a similar pulse can be used to close the doors. Another use for a very small ultrasonic unit could be for the remote switching of radio or television channels from
an arm-chair, where the coil turret of a receiver is made to rotate one step each time a pulse is received from the transmitter.
If one wishes to communicate with one's neighbour, it is illegal to connect the two houses with wires, since this would infringe the Post Office monopoly (Post Office Act, 1969, Section 24.1). However, the writer has obtained confirmation from the Post Office that the use of ultrasonic waves for communication does not infringe their monopoly and no licence is required. Therefore transmitted waves could be modulated and sent in the form of morse signals.

Finally, the equipment described here could also be employed as an intruder alarm. If the beam passes across a corridor, any interruption of the beam by an intruder will cause the relay to open and this can be used to sound an alarm. The intruder will not detect the ultrasonic beam, so if the alarm sounds at a remote point, the intruder will have no means of knowing that his presence has been detected.

## TRANSDUCERS

The ultrasonic transmitting transducer used in this project generates ultrasonic waves in the air when a suitable alternating voltage is applied across its terminals. This voltage may be a square or a sine wave, but the frequency must be close to the resonant frequency of the transducer. A similar transducer is used in the receiver, and when ultrasonic air waves strike this receiver a voltage at the uultrasonic frequency appears across the transducer terminals. This voltage is generally very small (typically ranging from about 50 V to 100 mV ) and must therefore be amplified considerably in the receiver unit before it can be used to control a relay.

The transducers themselves act like a small loudspeaker and a small microphone which will operate only near to their resomant frequency. They have the same circuit symbol as a loudspeaker. A miniature transducer type SE05B has been chosen for use in this equipment and it is available in two types which are designated "40T" and "40R". The SE05B-40T type should be used in the transmitter and the SEO5B-40R in the receiver. Although the equipment will function with the 40T and 4OR units interchanged or with two units of the same type, optimum results can be expected only if the 40 T


BRIAN DANCE M.Sc
unit is used in the transmitter and the 40R unit in the receiver.

The 40T and 40R units have an identical appearance, being mounted in small aluminium cases about 1 cm in diameter by 1 cm in length. One of the two connecting pins at the back of the device is connected to the metal case, which should be earthed.
Internally the transducers contain piezoelectric ceramic bimorph plates which resonate mechanically at the 40 kHz ultrasonic frequency. Another type of transducer which operates at 25 kHz is available from the same supplier and is suitable for use in the same type of circuit, but the frequency of oscillation of the transmitter circuit must be reduced by increasing C2 or R3 of Fig. 1. Air trans-


Fig. 1: Schematic of the HBF4001AE integrated circuit, showing the four two-input NOR gates.This IC is used as the heart of the transmitter.
ducers are not normally used at frequencies above about 100 kHz , since the attenuation of the waves in air increases with frequency and efficiency of energy transfer to and from the air becomes smaller at higher frequencies.

## TRANSMITTER LOGIC

An oscillator circuit is required which will feed a 40 kHz signal at a level of a few volts to the transducer. A simple transistor astable circuit can be used, but the use of an IC simplifies the design.

The transmitter circuit used in the prototype is shown in Fig. 1. It employs the SGS-ATES HBF 4001 AE COS/MOS quad 2-input NOR gate. The two NOR gates on the left hand side form a square wave oscillator, the frequency of which can be varied by means of VRI. The two NOR gates on the right hand side are buffer amplifiers which drive the transducer in push-pull. All of the NOR gates in the device are interchangeable, so the pin connections shown in Fig. 1 can be varied considerably if one wishes. The transmitter can be switched on and off by a switch in the supply line where a current of about 6 mA flows in the case of an llV supply. However, it may be more convenient to use the switching
system shown, where the current through Sl is very minute. The switching can also be performed by a logic signal applied to pin 13 in the circuit shown.
COS/MOS devices have input impedances of the order of a million megohms and are therefore susceptible to damage by electrostatic charges. The manufacturers recommend that:

1. The device leads should be kept in contact with conductive material except when they are connected in a circuit.
2. Soldering iron tips should be earthed.
3. Devices should not be removed or inserted into circuits whilst the power is applied.
4. Signals should not be applied to unused inputs when the power is not applied.
In practice, however, the devices are well protected, although its wise to obey the rules to avoid disappointment. Its also wise to employ a mica or polystyrene capacitor for C2 of Fig. 1 or a ceramic type with a tolerance of not more than $\pm 20 \%$.

## RECEIVER

The IC used in the receiver is the ULN-2212 manufactured by Sprague Electric Ltd. This is a 16 pin DIL device which has been developed for use in television sound systems; it contains an IF amplifier, an electronic volume control and a 1 W audio power amplifier. In the application being described, the 40 kHz signal from the transducer is amplified by the IF section of the device and then converted into a steady voltage. This voltage is fed to the input of the power amplifier section which can provide enough output current to control a large relay. Thus the use of this device greatly simplifies the external circuitry.

The receiver circuit is shown in Fig. 2. The transducer signal is fed to the internal differential amplifier connected to pins 10 and 11. The resistor R2 keeps the bias at pin 10 at about the same value as that at pin 11, and C2 decouples pin 11 so


Fig. 2: The Ultrasonic receiver chip, ULN2212 shown here, contains an IF amplifler, electronic volume control, and a $1 W$ audio amplifler.
that there is very little 40 kHz voltage at this point. The 40 kHz amplifier incorporates its own limiter
circuit，so the output is almost constant for input signals exoeeding about $200 \mu \mathrm{~V}$ at pin 10 ．
The 40 kHz output can be taken from pin 16，but an output signal of larger amplitude is obtainable from pin 2．The electronic volume control circuit is connected inside the device between pins 16 and 2. The output from pin 2 is connected via C3 to the diode pump circuit of D1 and D2．When C3 discharges， the current passes through D2 into C5．It then charges again via D1 during the other part of the 40 kHz waveform．Thus the upper end of C5 becomes positive when an ultrasonic signal is falling on the receiver transducer．

## POWER AMPLIFIER

The input of the power amplifier is connected to pin 3 and the output to pin 7．In the application for which the ULN－2212 is intended，an audio signal is capacitively coupled to pin 3 and this pin is at a slightly positive potential（about +2 V ）．In this case， the output at pin 7 is half the supply line voltage．
The presence of R 4 in the input circuit to the power amplifier reduces the potential at this non－ inverting input，and the output at pin 7 falls to a fraction of a volt when no ultrasonic signal is present．The relay therefore remains open．If an ultrasonic signal now falls on the transducer，the output from the diode pump biases pin 3 to a potential more positive than its quiescent value．The ouput voltage rises to about +11 to +13 V and the relay closes．It will open again whenever the ultrasonic signal is interrupted．

When the current ceases to flow through the relay coil，a relatively high transient voltage is developed across this coil owing to its inductance．This transient voltage is short circuited to earth by the diode D3．If this diode is omitted，the transient voltage may possibly damage the IC．The absolute maximum supply voltage which may be fed to the device is 18 V ，but it is wise to keep the supply voltage below this value to avoid the possibility of damage．The ULN－2212 incorporates a circuit which provides automatic shutdown of the power stage if the silicon chip becomes excessively hot．The supply current with the relay open is about 35 mA ，but this increases considerably when the relay closes，the value depending on the type of relay．The output current from pin 6 is automatically limited to 800 mA by the internal circuit of the IC and this protects the device from damage if the output is earthed．

## RELAY TYPE

The relay chosen for the prototype is the eco－ nomical Keyswitch type MS1B with a 12 V 26 mA coil．Its contacts can switch 5 A at up to 250 V AC and this is adequate for most applications，since it represents $1 \cdot 25 \mathrm{~kW}$ ．The direct current which can be controlled by this relay is smaller than the alternating current，since alternating voltages fall to zero twice per cycle and this breaks any arc which is formed．

The ULN－2212 can however，provide enough output current to control a large relay which may require about 120 mA at 12 V ．However，it is wise to mount such a relay away from the receiver transducer， since the vibrations may cause a malfunction．

## SETTING UP

The frequency of the transmitter may be set to approximately the optimum value by adjusting VR1 with a plastic tool，so that the transmitter unit takes a maximum current from the power supply．It is then delivering maximum power to the transducer． This current varies with the power supply voltage to the transmitter，being typically about 3.5 mA （ $7_{2}{ }_{2} \mathrm{~V}$ supply）， 5 mA （ 9 V supply）， $7 \mathrm{~mA} \quad\left(10{ }^{1}{ }_{2} \mathrm{~V}\right.$ supply）， 9 mA （ 12 V supply）and $11 \mathrm{~mA}\left(13{ }^{1} 2 \mathrm{~V}\right.$ supply）．The transmitter output power and，therefore， the maximum range of satisfactory operation falls considerably if the transmitter power supply voltage is reduced below $71_{2} \mathrm{~V}$ ．

A final adjustment of VR1 may be made by con－ necting a $20 \mathrm{k} \Omega / \mathrm{V}$ meter across R1．If the receiver is switched on，the voltmeter should read about $1^{1}{ }_{2} \mathrm{~V}$ ．If the two transducers are facing each other and the transmitter is switched on，the reading should increase to about 3 V ．The transducers are then separated and turned so that they no longer face each other and the meter reading will start to fall．VR1 is then adjusted for maximum reading．

The transducers can be obtained from Hall Elec－ tronics， 48 Avondale Road，London E17 8JG for $£ 3 \cdot 75$ per pair inc．VAT and $p / p$ ．The ULN2212 is avail－ able from Phoenix Electronics， 139 Havant Road， Drayton，Portsmouth P06 2AA for $£ 3.50$ inc．VAT and $p / p$ ．The HBF4001AE is available as the CD4001AE from advertisers．

## CORRECTION

## SIMPLE HOME PROJECTS－3 December 1975

## Random Number Selector

In the circuit ${ }^{\text {diagram，pins } 3} 3$ and 7 on IC2 should also be connected to pin 11. This may be done by a solder bridge as shown here at＇$y$＇．
A link is also required between the points marked＇$x$＇and this is made on top of the PCB．It can be clearly seen in the photograph of the finished unit，im－ mediately to the right of capacitor C 2 ， centre bottom．


## agazines Ltd． 1975

Enlarged section of the PCB showing solder bridge at
＇$y$＇and wire link on top of the board at＇$x x^{\prime}$ ．


TTHE use of integrated circuits has enormously simplified the design of VHF receivers, but at present discrete components are still employed in the frontend unit, since no suitable ICs for use at about 100 MHz are available. The development of the new SD6000 IC by Signetics for use as a VHF amplifier and mixer therefore marks an important step in FM receiver design.

The SD6000 is encapsulated in a normal 8 pin dual-in-line plastic package and can be used to design tuners which have a better performance than the best of those which employ bipolar devices.


Fig. 1: Internal view of the SD6000 showing the protective zener dlodes, the two dual-gate MOSFET devices, and the pin connections.

## INTERNAL CIRCUIT

As shown in Fig. 1, the SD6000 contains two dualgate MOSFET devioes. These are ' $N$ ' channel enhancement components made by ion implantation and the special D-MOS (Diffused Metal Oxide Silicon) technique used to fabricate the earlier Signetics D-MOS discrete devioes. Each of the gates is protected by a zener diode which will bypass to the substrate (pin 5) any static or other voltages more
positive than +25 V or more negative than -0.3 V . No special precautions are required when handling the SD6000 or when soldering it into a circuit.

The two devices are positioned in the package in such a way that coupling between them is minimised. This assists stability and minimises radiation of the local oscillator signal from the aerial. The D-MOS fabrication technique enables precisely controlled channels, less than 1 micron long, to be produced with extremely low parasitic capacitances, the resulting D-MOS devices being ideal for VHF use. Although the internal construction of D-MOS devices differs from that of other enhancement MOSFETs, the principles of operation are the same.

## ADVANTAGES

Dual-gate D-MOS devices have inherently linear characteristics, wide dynamic range and excellent cross-modulation characteristics. They provide high gain and have a very low noise figure. The feedback capacitance from drain to gate is only about 0.03 pF . Gate leakage currents and drain to source leakage currents are typically $\ln A$, whilst the maximum permissible drain current is 50 mA .

## A PRACTICAL CIRCUIT

The SD6000 has been specifically designed for use in the RF amplifier and mixer stages of high performance FM receivers, but it will doubtless find other VHF applications. A typical FM front-end circuit with ganged tuning capacitor for a signal frequency range of 88 MHz to 108 MHz is shown in Fig. 2, but varicap diode tuning has also been employed with the device.

The circuit provides a typical power gain of 30 dB at 100 MHz , the typical noise figure being only 2.5 dB (maximum noise figure 3 dB ). Commercially available tuner units seldom have a noise figure of less than 6 to 7 dB , whilst some have a much higher noise figure. Both the noise figure and the available gain of the RF stage are fairly independent of the drain


Flg. 2: A typical clrcuit for an FM tuner using the SD6000 in the RF and mixer stages. The above circuit covers a frequency range from 88 MHz to 108 MHz .
current provided that the latter exceeds about 7 mA , see Fig. 3.

The bandwidth of the RF amplifier is about $2 \cdot 5 \mathrm{MHz}$ at the -3 dB point and that of the mixer 300 kHz , the latter value being mainly controlled by the properties of the tuned circuit in the output transformer. AGC is applied to the second gate of the RF stage (pin 3); the 50dB typical operating


Fig. 3: Graph of the noise figure and available gain of the RF stage plotted against the drain current.
range of the AGC is extremely wide. The change of gain with the gate 2 voltage at 100 MHz is shown in Fig. 4 for the case where gate 1 is at +10 V and the drain to source potential is 15 V .

A PNP 2N4126 provides the oscillator voltage to gate 2 of the mixer through C14, the signal voltage from the RF stage being applied to gate 1. This type
of circuit enables very high isolation to be obtained between the local oscillator circuit and the input and hence reduces radiation from the oscillator frequency. The oscillator stability is about $40 \mathrm{kHz} / \mathrm{V}$ change in the supply line and $+10 \mathrm{kHz} /{ }^{\circ} \mathrm{C}$ temperature change.

The typical conversion gain of the mixer stage plotted against the drain current is shown in Fig. 5, the high and constant conversion gain of 19 dB being obtained at drain currents of 4 to 11 mA . As in the case of the RF stage, the D-MOS construction of the mixer provides excellent cross modulation performance and very low noise. The conversion transconductance is typically 10 mmhos .


Fig. 4 : Curve of the AGC characteristic of the RF gain. The 50dB galn change is equivalent to a change of voltage gain of 316 times.

## PRECAUTIONS

When using the SD6000, it should be remembered that the absolute maximum value of the drain to source current is the unusually low one of 50 mA .
continued on page 890


by Eric Dowdeswell G4AR

MY comments in the December issue, on honesty in log-keeping, seem to have met with quite a lot of supporit. P. B. Flatman of Ipswich, back on the bands after a three year break, always makes a point of hearing the callsign of a station twice, preferably phonetically, before putting it in his log. He admits that some of the entries in his earlier logs just could not have been heard, although they had been entered in all good faith at the time. 'P.B.' also got going on one of my own pet 'hates', namely the amateur who asks the DX station for his callsign several times and then gives the DX 'S9 + 20dB'! Mistakenly, of course, he thinks the flattery will somehow persuade the DX to send the QSL card by return of post!

In the same way, a station in a CW contest will give a report of 599 to every station worked. Why? Because 599 sent in the shortened form is .. and it saves a lot of time which can be important when working 50 or 60 stations an hour. The fact that the information is quite false seems to be overlooked in the race for points and more points. But, getting back to the ' $\mathrm{S} 9=20 \mathrm{~dB}$ ' phobia, more rubbish is spoken on and about ' $S$ ' meters than anything else. Why do people place such implicit faith in a meter that does nothing more than show a rise or a fall in signal strength? There must be at least six factors affecting its readings and no two locations are going to have the same factors so why do operators think that S9 on a FT101 in John O'Groats is the same as S9 on a different FT101 in Cornwall? A lot of rubbish!

Martin Kessel (Stoke-on-Trent) has been inactive due to revision work for the RAE, which I trust he has now duly passed. He's been trying to get a one valve regen set going on the 2 m band but in defence of our hobby and his local viewers I trust he never succeeds! Philip Williams BRS35031 of Bridgnorth enjoyed the lift on 2 m in late October, as did many other readers, copying many stations deep into Europe with his TC7 Mk II with the G8AEV converter and an 8-element yagi at 20ft at a QTH which is 200ft a.s.l.

Alan Rae, recently GM8GRO, went on to take the Morse test and is now GM4ENN and sporting a Swan transceiver on the HF bands. It's always good to lose readers from this column in this way! Alan

Doherty BRS34968 (Portrush Co. Antrim) comments on the fantastic aerial systems being used by PAOGMW on 80 m in the search for DX. Alan uses a G5RV for the HF bands and a 132 centre-fed wire for the LF's. Any more detailed info on the GMW aerial farm would be welcome. Alan reports cards received from KM6EA, HI8XKP, YB0ABV, among many others.

Mike Bennett (Slough) picked up a couple of rare ones in VK9XX on Christmas Island and FR7ZL/G on the Glorieuses Is. on 15 and 20 m respectively. Paul Barker (Sunderland) has been busy swopping his SSB hat for his SSTV one as conditions allowed, finding EA3ADW and 9K2DO excellent copy in the latter mode on 20 m and LU2JC and W1BGW on 15 m . Tim Charles (Colchester) has been looking for ZL3RB on 160 m following reports of successful QSOs with Europe but getting up on sked is a problem with Tim! He has now heard 21 countries on Top Band, the latest being 9H1CG. He has been hearing all continents on 80 m plus his first JA's on the band, peaking between $15-1600$, so presumably they are coming over the pole. Tim also mentions PAOGMW working the west coast Americans on the long path in the middle of the afternoon, plus KH6 and many JA's. This is on 80 m , by the way! GMW's secret is now revealed, it's Quads on 80 m . Yes, in the plural! Tim is another who, hopefully, will have passed his RAE, taken on December 1st.

Barry Middleton G4DBS asks me to reveal all, about the Lincoln Short Wave Club G3IXH, of which he is Hon. Sec. More members are wanted, particularly younger ones, so trot off to the Lecture Room, Lincoln Astronomical Society, Westcliffe Street, off Burton Road, Lincoln at 1930 any Wednesday. The club operates a net on 2 m at 2000 hours every Thursday with G4DBS and G4DFH as control stations and again on Sundays at 1100 hours on 80 m or 3700 kHz to be precise, with G3TOA in charge.

Neil Whiteside A8859 (Hitchin) also enjoyed the exceptional conditions on 2 m and commented upon the number of Continentals working through the repeater GB3PI. Stephen Budd A8713 (Worthing) caught VX9A on Sable Island for a new country, now approved as such by the ARRL although any normal person would call it VE1! QSLs to VE3GMT. Andrew Swiffin A8603 (Cheadle) now has a Pye Ranger for 4 m and is busy building the PW 2 m converter so it looks as though he has got fed up with HF bands! Actually he has been round all the bands from 15 to 80 m with good effect.
Steve Cottis A8961 (Harrogate), aged 14, was told he was too young to join the local RAE course. Rubbish, said I, and told him to get in there and insist upon his rights. Good heavens, 14 year olds


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## M. DZIUBAS

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are passing the RAE and Morse test every day, or so it seems! However, this does not mean that I go along with the present system which I have always believed to be an utterly futile examination. It ought to be linked to a practical examination but more of this anon.

## Log extracts

A. Swiffin:-80m OE2SCL/YK 15m TJIEZ (QSL PA0EZ) YB1AB ZS3BK 5T5BJ 5X5NK
S. Budd:- 20 m YJ8AN VX9A FK8CJ VR4DX 15 m CR9AJ PZ9AJ VX9A ZD8AA 4W1AF 9N1MM 10m FH8CY 9Q5SW
N. Whiteside:- 2m HB9AMH/P IB6BTI OZ60L SM7WT
T. Charles:- 160m K1PBW VE1BCZ W2PV W9LI 9H1CG 80m FP8CT HP3AU JAIERK UA9CM VS6DO ZL3LV 20m VP2GM 2m DM2CZI HB9ZF SM6BZC SP5JC
M. Bennett:- 20 m BV2B FG0MM FR7ZL/G 8R1X 15m VK9XX 9N1MM 10m C9MLF
P. Williams:-2m DJ6GO DC1QD PA0JHW
P. Flatman:- 15m EA9FC FM7AQ KZ5AS FR7BE TG9MP ZS4AW 20m FY0BHI 9X5PT

## M. Kessel:- 80m 9X5SP 5L7F 9H1C

A. Doherty:- 160 m EA8CR 80 m JAlJRK 5L7F 9Y4NP 40m JA1DJL JX2HK 20m KG4GG PZ1DR VP8HZ VK1SD VX9A VE8RE 6W8FP SSTV 20m EA3ADW I2PHO 9K2DO OE8TWK 15m LU2JC W1BGW

All stations are SSB except those in bold which are CW.


## SHORT WAVE BROADCASTS by Derek Bell

OUR COLUMN this month opens with a letter from someone who derives more enjoyment than most of us from roaming the world via the short wave spectrum. This is John Buxton of Shepton Mallet who is disabled and therefore has many hours of the day and night to pass away. As a change from sending logs, since his present set is so poorly calibrated, John sends a chatty letter urging a listen to "Beat of the Drum" on Voice of Turkey, Sundays around 2215 on 9515. It is, says John, a very funny show. I can perhaps help John, because there is an organisation that is set up to help just such DXers as John. This is Handicapped Aid Programme run by Ted Hindle, 13 Thirlmere Road, Preston, Lancs. Not only does this worthy cause help the handicapped DXer with equipment but would like surplus equipment from anyone who cares to help. This gear is checked over and then sent to someone in need.

By the time this is read the new schedules will have settled down. Paul Cowburn from Leyland writes that the following have been announced:-

Radio Israel 2000 on 981574127395
Radio Finland 140018302030 on 11755.61209550
Radio R.S.A. 2050 to 2150 on 151551190095257270
No doubt there are a few more which I will pass on as they come to hand.
Andrew Walker of Leeds asks for advice on when to .send International Reply Coupons. As a rule-ofthumb I always recommend that IRCs be sent to stations that rely on donations, such as religious or charity stations, but a great many state or commercial stations ask for IRC's and one has to hope to hear the stations themselves insist on IRCs in their chat.

Recently this column featured "National Public Radio" and your scribe confessed to being puzzled by this station. Both A. Harris of London and Stewart Fenwick of Clackmannan write to enlighten us. It seems that this phrase is used in the news broadcasts of the American Forces Radio and Television Service. Stewart, in fact, sends the address as NPR 20/25 M Street, North West Washington, DC, 20036 USA.
Niels Montanana raises the old question of how one identifies a foreign language when one does not speak it? The solution is to have one or two key phrases in the old memory box and I suppose that the one most stations use is the equivalent of "This is so-and-so calling". The following quick course of language lessons may help:-

French "Ici Radio so-and-so"
German "Hier ist Radio so-and-so" (Pron. "hear isst")
Portuguese "Aqui Radio etc (Pron. "ah key")
Russian "Govorit Moskva" (Pron. gov-or-it)
Holland, by the way, uses a similar phrase to the German one.

David Lovatt, the proud new owner of a Codar CR70A, has latched on to a station that perplexes him, namely Radio Television Ivorienne. This is a French language station that serves the Ivory Coast Republic and comprises five transmitters the largest one being a hundred kilowatter transmitting on 1241 and 11920 in English from 1830 to 1955.

David has had a QSL from the Turin standard frequency station on 5000 with 5 kW . Such stations are very good for calibrating the set since there is an electronic tick every second exactly on the frequency.
Roy Patrick from Mackworth, Derby, writes to let us know that IBRA. Radio is now sending a special QSL for the Malta relay programme Radio Mediterranean. Roy uses a Trio 9R59DS with the ever faithful Joystock aerial and he is a tropical bands fan and, although a little late, the following may well be worth noting:-

Radio Rumbos, Venezuela, 4970 late evenings or 0500.

Ecos del Torbes 4980 evening or early morning
Radio Continenta 5030 evenings or early morning so if you are an early bird or night owl why not try for one of the hundreds of South Americans.

From Rugely, Staffs, in fact from the QTH of John Godwin, comes news that HCJB Quito are to build a 500 kW transmitter in order to beam the gospel into the USSR. Also, John says, Radio Sri Lanka are now putting out a show for the UK every evening on 15120 from 1900 to 2000 . The clue to

identification is a jazz version of "Tea for Two", used as a link. For QSLs write to Sri Lanka Broadcasting, Colombo, Sri Lanka.

With a prewar HRO plus his Joystick aerial John set out bright and early searching for VLT9 Papua on 9520 , but, to his delight, he happened on Radio New Zealand on 9540 with its service for the Pacific Islands. The best times, John says, are between 0800 and 0900 from this $7 \cdot 5 \mathrm{~kW}$ station.

As a change from the winter of the UK let us turn to a DXer who has his 130 foot long wire secured "half way up a coconut tree". This is E. M. Sivaguru of Port Dickson, Malaysia, who has a Philips B5X06T. He logs such DXotics as:-

11500 Radio Nederland, Tananarive relay, at 1520
11860 Voice of Free China, Taiwan, at 1405
153925 Voice of Phophecy, India, at 1615
17810 FEBC, Radio Int. Manila, at 1630
and has a quiet chortle at the UK radio twiddler who has to listen hard for Australia, NZ or suchlike southern hemisohere transmitters which E.M. can pull in, as they say, "on a piece of wet string".

Turning now to QSLs John Higginbotham has harsh words to say about Radio Baghdad who it seems are sending out QSLs and "skeds" together but the skeds are for 1974! J. W. Farrer sends a list of the reply times from various broadcasters and tops is Radio Australia with an airmail reply taking 105 days, while Radio Finland takes 10 days and our own BBC World Service takes 25 days.

Some time ago news reached your column that Radio Israel was to start a DX show. P. K. Gulati has sent in the first report on this show. It is aired on 15100 every Saturday night at 2030 and another DX show mentioned is that of Radio Austria on 9690 every Sunday at 0915 and repeated at 1805 on the same frequency.

It is time to wind up so wishing you 73 s for 76 I will close apologising for those letters that space has ruled out due to the very heavy postbag this month.


## MEDIUM WAVE DX

## by CHARLES MOLLOY

PAUL BOOKBINDER writes from Maidenhead with news of his first transatlantic DX on the medium waves. Using a Grundig Satellit 1000 with built-in ferrite rod aerial he logged WINS on 1010 kHz at 0300 . "Reception was good but only lasted about ten minutes; very interesting to hear local domestic news and traffic reports direct from New York". Paul, who is building a medium wave loop aerial has been active on the long waves too and has
received a QSL card from Kiev, Ukraine on 209 kHz . Congratulations Paul on a fine achievement, you should really pull in the DX once your loop is in use.

Glyn Morgan of Tredegar, Gwent, has been having trouble with his HA230 communications receiver. He is temporarily using an Astrad VEF 17 transistor portable with internal aerial for his DXing and his catches include WCBS in New York City on 770 kHz , Tenerife in the Canary Islands on 620 kHz and an unidentified Arabic station on 863 kHz (probably Ksar-es-Souk, Morocco). Glyn prefers to use his Astrad in its portable form to take advantage of the directional effect of the internal aerial. A ferrite rod aerial behaves in the same way as a loop. Interference is reduced and there is often an improvement in signal-to-noise ratio too but the loop has much greater pick-up which makes it more suitable for the serious DXer. Hope your HA230 is soon back in service Glyn though you seem to be doing very well without it.

More news of transatlantic medium wave DX comes from Samuel White who lives in Larne in Northern Ireland. Using a Strad 553 W receiver with a 60 ft . long outdoor aerial he heard CJON in St John's in Newfoundland on 930 kHz "quite clear at good volume". Reception on the lower frequencies is now better than it has been for many years owing to the approach of the minimum of the current sunspot cycle. DXers may agree with Lawrence Bennett of Bristol who writes "Because of the recent poor conditions on shortwave I decided to try my hand at Medium Wave DXing". Lawrence has received a number of good QSL cards and souvenirs from German stations and he mentions a book on DXing issued by Sender Freies Berlin, 566 kHz . You have to null-out Athlone on the same channel to receive this one.

Twelve-year-old Michael Walker of Leeds has got hold of an old 6 valve Emud receiver which is of German origin. He used it with a 30 ft . outdoor aerial to hear Sweden Calling DXers from Radio Sweden on 1178 kHz . Michael received a QSL card and a copy of the DXers Newsletter issued by this programme. The English version of Sweden Calling DXers is broadcast weekly on a Tuesday at 2300 and often includes items of interest to the medium wave DXer.

An interesting letter comes from F. A. Ainsley of Hartlepool in Cleveland who confesses to being a keen medium wave DXer both in Australia and England. He has been experimenting with loop and vertical aerials and has managed to combine the two at the input of his homemade receiver in such a way as to produce a single null similar to that obtained when direction finding equipment is in the Sensing mode. With this null pointing towards Europe he managed to $\log$ WCBS in New York City on 770 kHz , WINZ in Miami and WBT in Charlotte, North Carolina.

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Medium Wave Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG.
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SPECIAL
PRODUCT
REPORT


- HE "Oxford" series of calculators is Sinclair's bid to increase their penetration of the calculator market. The Oxford 300 is aimed at the growing "electronic slide rule" market and it looks like being a success.

The pocket-size scientific calculator field was pioneered by Hewlett Packard, closely followed by Texas Instruments who have become market leaders in the US. Hewlett Packard's HP35 was the first machine on the market which, competitively priced, virtually overpowered the existing calculator market overnight and made H-P a great deal of money. Since the launch of the HP35 in 1972, the market has expanded to allow prices to fall until to day simple calculators start at under $£ 10$. Most of the scientific calculators are in the $£ 50$ to $£ 150$ range, so at $£ 30$ plus $8 \%$ VAT, the Sinclair Oxford 300 is worth a close examination.

Sinclair have produced three models in the Oxford range, the 100,200 and 300 , in an attempt to capture the market of calculator users from schoolboys and housewives, through commercial and business users, to scientists and engineers. They hope to claim a $35 \%$ share of the market by the end of 1975.

CONSTRUCTION
The Oxford 300 consists of a keyboard, a printed circuit board containing the main circuits and a display unit. The keyboard has 19 keys and a switch, all mounted on a paxolin assembly fitted into the case. The keys have a nice positive feel, making a click when operated. Replacement of a faulty keyboard would take enough time to be significant in cost.

The calculating power is contained in a single integrated circuit soldered, together with an interface IC and a few other components on to a neat printed circuit board which is mounted on plastic pillars and retained by three push fit pop studs. With only 17 connections, this board is easily changed but, since it contains the computing IC replacement would be expensive. The display unit is welded to the case and is the most difficult part to remove. The general standard of construction inside this calculator may be described as top domestic quality.

PACKAGING
Whilst one can be reasonably enthusiastic about the Oxford 300's internal construction, the same cannot be said about the outside packaging. According to Sinclair, "final styling of the Oxfords was determined by an exhaustive market research exercise in which a number of alternative case styles were researched for their modern and professional appearance, convenience and customer acceptability", The others must have been bad for this black case can only be described as dull.

A second criticism is the on/off switch, disguised as a function button on the main keyboard. It is a slider switch, rather difficult to operate and a potential failure point. A degree/radian switch is fitted on the back of the case in a position much more suitable for an on/off switch. Swapping these two switches would seem to be both logical and more functional.

The keyboard is of the dual function type in which a "function" key is used to obtain the alternative functions. This type of keyboard has the advantage that price is kept to a minimum as opposed to the discrete function keyboard which may have 40 or more keys for the same capability. The necessity of using a function key in an algebraic machine

not only increases the number of operations necessary when performing calculations but it also means that considerable care has to be exercised as well.

The Oxford range is not designed with pocket use in mind although they should fit the average size pocket. The display is angled in such a way that it can be read with the machine on a desk. The keys are larger than most pocket calculators making desk top operation easier.

All three calculators in the range are mains or battery operated and should not be confused with the rechargeable battery facilities offered on more expensive machines.

FACILITIES
Algebraic logic is used as opposed to reverse Polish scientific notation as employed in the Sinclair Scientific calculator. This simplifies operation for the average user since calculations are carried out in the same way as they are written down. The Oxford provides a constant facility on all four arithmetic functions. There is also a very flexible memory with $M+$ (add to memory), $M$ - (subtract from memory), MEx (exchange display and memory), MC (memory clear) and MR (memory recall) functions available. Trig functions sin, cos, tan and arcsin, arccos and arctan are provided with a switch to select either degree or radian operation. Other functions provided are $\log _{e^{x},} e^{x}, \sqrt{x,} 1_{e} x$ and a $\pi$ key. There is no $x^{2}$ function which can be rather frustrating at times although squaring can be carried out using the constant facility.

Sinclair provide an adequate booklet showing examples of how to use the calculator. The display gives results in eight digit floating decimal point format or in scientific notation with a five digit mantissa and a two digit signed exponent. Numbers can be entered in either notation, the machine automatically adjusting the notation when the operation key is pressed. There is a machine clear and a last entry clear facility provided by pressing the clear key either once or twice. Each of the four arithmetic functions has the ability to store a constant so that if, for example $k \times a=i s$ entered then subsequent numbers may be multiplied by $k$ simply by pressing say $b=$ to give $k \times b$.

CONCLUSION
The Oxford 300 is a powerful little package that will appeal to many users at the price offered. The functions provided are more than adequate for the run of the mill scientific problem and the algebraic notation certainly makes it easier to use than the Sinclair Scientific.

Fig. 5: Graph of the mixer unit conversion gain, plotled against drain cur. rent.


Readers may wish to use a power supply during their experiments which will not give more than 50 mA , to prevent possible damage to the SD6000. The absolute maximum permissible drain to source voltage is 20 V .

As with all VHF circuits, precautions must be taken when using the SD6000 to keep all wires carrying radio frequencies very short. The writer found the SD6000 circuits he has tried reasonably immune from spurious oscillation, but nevertheless begin-
ners are strongly advised to experiment at lower frequencies before moving to the 100 MHz region.

The use of the SD6000 will enable FM tuners, including car radio VHF receivers, to be made which have a better performance and somewhat simpler circuitry than those which have been available up to now.

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| :---: | :---: | :---: | :---: | :---: |
| $0 \cdot 3$ | 748c TO | $0 \cdot 4$ | POTENTIOMETERS <br> Lin or Log 4" Bash-Spindle 2* FMF |  |
| /6/7 | 748 c DIL | 0.2 |  |  |
| AF118 <br> 0.18 <br> 0.35 | TBA800 | 695 |  |  |
| AF118 0.35 | TBA810 | 1.3 | $5 \mathrm{~K} \Omega-2 \mathrm{M} \Omega$ 8ingle/D/PB |  |
| $\mathrm{BC107/8/9}$ $\mathrm{BC147/8/9}$ | 2N414 |  | $5 \mathrm{~K} \Omega-2 \mathrm{M} \Omega$ Dual Stereo $\quad 0.46$ |  |
| ${ }^{\text {BC147/8/9 }} 00.07$ | S.C.E |  | $\qquad$ |  |
| BC157/8/9 | 1s 100V 0-4 |  |  |  |
|  | $1 \pm 200 \mathrm{~V}$ | 47 | T.T.L'A Price ea. T.T.L's Full Range <br> $7400 \cdot 1 / 2 / 3$ 018 Btocked <br> $7404 / 5$ 016 Standard low power <br> $7406 / 7$ 096 Bchotky |  |
| BC182/3/4 $0 \cdot 10$ | 14.400 V | 0.50 |  |  |
| BCY70/1/2 | 3.400 V | 0.82 |  |  |
| 0.18 | ZERERS |  |  |  |
| $132$ | $\begin{array}{ll} 2.7 v-33 v & 0.00 \end{array}$ |  |  |  |
| BF194/5/6 0-10 |  |  | $\begin{aligned} & 7410 \\ & 741677 \end{aligned}$ | I.C. ${ }_{\text {DIL }}$ 80CX Erss ${ }^{\text {Price ea, }}$ |
| MJE376 0.68 | BZX61 beries$3 \cdot 3 v \cdot 33 v$ |  | $\begin{aligned} & 7422 / 3 / 5 / 6 \\ & 7428 \end{aligned}$ | 8 PIN $\quad 0.12$ |
| JE371 |  |  |  | 14 PIN 018 |
| 1301/2/3/4 | ALI-BOXRS |  | $3432$ | 16 PIN 0.14 |
|  | $24 \times 84 \times 17^{\prime \prime}$ |  | $\begin{array}{r} 7437 / 8 \\ 7441 / 2 \end{array}$ |  |
| 2N2908 015 | $4 \times 4 \times 11^{\prime \prime}$ |  | T450/1/3/4 | 14 PIN |
| 2N2926 all 0.08 | $4 \times 22 \times 1{ }^{\prime \prime}$$4 \times 2 \times 2^{\prime \prime}$ |  | $\begin{aligned} & 7470 / 72 \\ & \hline 178176 \end{aligned}$ | 16 PIN 0.18 |
| 2N3053 0.15 | $\begin{aligned} & 3 \times 2 \times 1^{-1} \\ & 6 \times 4 \times 2^{\prime \prime} \end{aligned}$ |  | 7480  <br> 7482 0.42 <br> 183  |  |
| 2 N 30540 |  |  |  |  |
|  | 7 $\times 2 \times 2{ }^{\text {- }}$ |  | 7482 7483 | IN914/4148 0.05 <br> IN $4001 / 7$ 008 |
| [3702/3/4 |  |  | 7454 |  |
| 2N3705/6 0.11 | VEROBOARD |  | 74.0 |  |
| 2N3707/8/8 | . 1 Matrix Prioe ea |  |  | $\begin{aligned} & \text { 8PEAKEB8 } \\ & 7^{\prime \prime} \times 4^{\prime} \text { FANE } 1-80 \\ & 8.8 \cdot 150 H M \\ & 36 \mathrm{p} \text { P P extra } \end{aligned}$ |
| 2N3819 $\begin{array}{r}0.08 \\ 0.28\end{array}$ | $31 \times 5$ |  | 74318 |  |
| TIP29A 0.45 |  |  | 74141 |  |
| TIP30A 0.52 |  |  |  |  |
| TIPs1 0.8 |  |  | Send for FREE CATALOGUE. Listing over 2,000 Items. 8.A.E. please. Quantity Discounts |  |
| TIP32 0.68 |  |  |  |  |  |
| TIP41A 0.65 |  |  |  |  |  |
| TIP42A 0.73 |  |  |  |  |  |
| BRIDGE RECTLFIERS |  | DEPT. W.5, 299/301 BALLARDS LANE, |  |  |
| P.I.V. 14.24 | $\begin{array}{lll} \mathbf{A} & 4 \mathrm{~A} & 6 \mathrm{~A} \\ 10 & 0.45 & 0 \end{array}$ |  | LONDON N12 8NP |  |
| $50 \quad 0.200 .30$ |  |  |  |  |  |
| $\begin{array}{lll}100 & 0.82 & 0.37 \\ & \end{array}$ | $\begin{array}{ll} 0.68 & 0.69 \\ 0.57 & 0.68 \end{array}$ | sanl onder only. daah with ordor, POSTAGE \& PACEING U.K. g0p. ADD V.A.T. TO |  |  |
| $\begin{array}{lll}200 & 0.25 & 0.48 \\ 400 & -88\end{array}$ |  |  |  |  |  |  |  |
| 400 800 0.87 <br>  0.88  | $\begin{array}{ll} 0.60 & 078 \\ 0.68 & 0.87 \end{array}$ |  |  |  |  |  |  |

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3 dB (upper limit set by transmitter) 3 d8 (upper limit se by transmitt
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10mA-1 5 amps
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Frequency Reapone + 1d? 20
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50 K oh mes
P.U. Input equalizes to RTAA curve within ida from 20 Mz to 20KHz, Supply 20.35 V at 20 m A. 5 mm maiont $-299 \mathrm{~mm} \times 89 \mathrm{~mm} \times$ OUR PRICE ? + ?
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The Stereo 30 comprises a complete stereo pre-ampllfier, power ampiffers will produce a hlgh quallty audio unit sudition of a transtopmer or overwind inputs lie. high quality celty audio unit suitable for use with a wide overwind Simple to Instali, capable of producing, stereo tuner, stereo tape reck ee of Is supplled with fult instructions, black frolly flist class results, this unit luse and fuse holder and universal mounting pranel, knobs, mains switeh, stalled in a record plinth, cabinets of your own construction o it to be in. avallable. Ideal for the beglnner or the gour own construction or the cabinet In performance with minimum of installation difficulty (cino requires HIn 30 mint .)
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 30
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Frequency response $\pm 3 d B P o=2$ watls $50 \mathrm{~Hz}-25 \mathrm{KHz}$ Sensilivily for Rated OlP-Vs $=25 \mathrm{v}$. RL $=800 \mathrm{hm}$



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Frequency Response $20 \mathrm{~Hz}-20 \mathrm{KHz}$
( -3 d 8 )
Bass and Treble rarige $\pm 12 \mathrm{~dB}$
Input Impedance $\{$ meg ohm
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Sire $452 \mathrm{~mm} \times 4 \mathrm{~mm} \times 33 \mathrm{~mm}$


Power supply for AL10/20/30, PA12, S450 etc. Input voltagr $15-20 v$ A.C. Output voltage $22-30 v$ D.C. Output Current 800 mA Max. Size $60 \mathrm{~mm} \times 43 \mathrm{~mm} \times 26 \mathrm{~mm}$.
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1FT．11．Midget IF transformers sultable for use with valves＇NEOSID＇Iron dust core tuning，complete with screening can 78 p 8ize－ $2-5 \mathrm{~m} . \mathrm{m}$ gquare $\times 49 \mathrm{~m} . \mathrm{m}$. M／c．
IFT．18．Minlature IF transtormer wound on ferrite pot core with adjustable core tuning complete with screening can 70 p Bise－ $11 \mathrm{~m} . \mathrm{m}$ equare $\times 18 \mathrm{~m} . \mathrm{m}$ ． $470 \mathrm{~K} / \mathrm{c}$ ． 12．14．Minhature leat IF transformer as above． 705 If．18．Miniature IF transormer SPDC a above but 11F．17．Miniature last IF tranalormer as above．OAD IFT．18． $465 \mathrm{~K} / \mathrm{c}$ of $1 \cdot 6 \mathrm{M} / \mathrm{c}$ ．Donble tumed tranetormer complete with ecreentig can．8is Bize－11mam equare $x$ $58 \mathrm{~m} . \mathrm{m}$ ．
ITF．15．A $10-7 \mathrm{M} / \mathrm{c} 1 \mathrm{~F}$ tranaformer，Double tuned complete with screening can． $759+25 \%$ VAT slize $-21 \mathrm{~m} . \mathrm{m}$ high $\times 11 \mathrm{~m} . \mathrm{m}$ square．

|  | DRHCO TRAM8ISTOR TUMIHG COHS <br> Colla for Transigtor Superhets and Converters suituble for chmssin or B9A base mounting． <br> T．COILS <br> BLUE：Aerial cotl with base input winding YELLOW：Interstage R．F．coll with cplgs RED：Osciliator coll for $465 \mathrm{Kc} / \mathrm{s}$ I．P． WHITE：Oacillator coll for $1-6 \mathrm{Mc} / \mathrm{s}$ I．F． |  |  |
| :---: | :---: | :---: | :---: |
| RAMGE |  | 1，T | $2 . T$ |
| $\begin{aligned} & \text { Mc/s } \\ & \text { METRES } \end{aligned}$ |  | $\begin{aligned} & 0.16-0.4 \\ & 2000-760 \end{aligned}$ | $\begin{aligned} & 0.515-1.545 \\ & 580-194 \end{aligned}$ |
| RANGE | 9．T | 4.7 | $5 . \mathrm{T}$ |
| Mc／a | 1．67－5．3 $180-67$ | S－15 $60-20$ | $10.5-81.5$ $28-9.5$ |

PRICE：BLUR：Range 1－88p；Rangen 2－5－74p YELLOW：Range 1 －Bap；Rangea 2－5－74p RED：Ranges $1-5-74$ P
WHITE；Ranges $1-5-74$

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X25 8pare Bits No． $50,51,52=44 \mathrm{y} \mathrm{earh}$
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2440／2 pare Blent $21-10$
BT3．Soldering Iron Stand Suitable for all modela $-\mathbf{~ - ~} \mathbf{1 1} \cdot 10$
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$\mathrm{ACl} 42 \mathrm{~K}=85 \mathrm{D}$
AA129 $=6 p$
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PP1 awitched 3，4t，6，71， 9 and 12．volls at $500 \mathrm{~m} / \mathrm{a}$ ，with on／of $\times 55 \mathrm{~mm} \times 75 \mathrm{~mm}$ ．
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Pin insertion tool

Plit 36 pins（etate 1 or $\cdot 15$ ）
LOUDAPEAKEP量 4 $\qquad$ $22^{\prime \prime} 8 \mathrm{ohm}$
$22^{\prime \prime} 40 \mathrm{ohm}$
$2 t^{\prime \prime} 80 \mathrm{ohm}$

1100 $21^{\prime \prime} 80 \mathrm{ohm}$
${ }^{5}{ }^{\prime \prime} 8$ ohm

$10^{\prime \prime} 8 \mathrm{ohm}$ dual cone ceramic 5 s． 76 $8^{\prime \prime} \times \mathbf{8}^{\prime \prime} \mathbf{8}$ ohm Perman＇t Maynet $\mathbf{8 1 - c 0}$ fier with Vol＇e． and Tone Conirols．Approx． 9 watts into 8 ohm per channel needs $9 / 12$ volt DC supply and is complete an a $21^{\prime \prime} \times 71^{\prime \prime}$ P／C board
ideal for domeatic record players，etc．A Bargaln at
$6+25 \%$ VAT

## 10－IHCE 8 OHE DUAL COMR

 Manufactured Dy＂ELAC＂to a vory high atandard these loud Apeakers are a real bargainAPRC：－8Ize $=10^{\prime \prime}$ Dual Cone Power $=10$ Wast Cone Power＝10 Watt $+25 \%$ Our Price－ 8875 p ench

## MAIT K KTHECTOR

Kaynector connects any Electrleal Equipisent to the malni supply in meondi Ideal for bench，garage can be made（max．load 13 A fued）．



ALणInIU童 BOX路 $+8 \%$

|  | $\underline{L}$ | W | H |  |
| :---: | :---: | :---: | :---: | :---: |
| AB7 | 21 | 61 | 11 | 84 |
| AB8 | 4 | 4 | 11 | E8 |
| AB9 | 4 | 21 | 11 | 84 |
| AB10 | 4 | 81 | 11 | 68 |
| AB11 | 4 | 21 | 2 | 54 |
| AB13 | \％ | 2 | 1 | 45） |
| AB13 | 6 | 4 | 2 | 89 |
| AB14 | 7 | 5 | 21 | 818 |
| AB15 | 8 | d | 5 | 0 |
| AB16 | 10 | 7 | 3 | 01.86 |
| AB17 | 10 | 41 | 8 | 11.00 |
| AB18 | 12 | 5 | 3 | 11.0 |
| AB19 | 12 | 8 | \＄ | 12．60 |

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Handy boxes for construction projecta．Moulded extrusion relle for P．C．or chaanin panele．Fitted with 1 mm front
panela．
1005
$=105 \mathrm{~mm} \times 73 \mathrm{~mm} \times 45 \mathrm{~mm}=55 \mathrm{p}$,
$1006=180 \mathrm{~mm} \times 75 \mathrm{~mm} \times 47 \mathrm{~mm}=78 \mathrm{~F}$
$1021=100 \mathrm{~mm} \times 74 \mathrm{~mm} \times 45 \mathrm{~mm}$－ $31 \cdot 28$
$1021=106 \mathrm{~mm} \times 74 \mathrm{~mm} \times 45 \mathrm{~mm}$（Bloping front）-85
TLLERCOPIC AERLAL
Nine wection fully awlvelling telescople acrial with 4 BA ningle bolt axing or two hole Axing bracket．
Fuily extended $=48^{\prime \prime} \quad$ Fuliy closed
Our Price $50 p+\mathbf{P} / \mathrm{P}+\mathrm{VAT}$（a） $25 \%$
LOW MOISE LOW PRICE CASIETHIA $+8 \%$
Good quallty tape is well made ecrev type caneottes
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38 mm hole for mounting．
ME6 $=0$ to 50 micro smp Full 8 cal

ME9 $=0$ to $1 \mathrm{~m} / \mathrm{a}$ Full Bcale

ME1］$=0$ to $10 \mathrm{~m} / \mathrm{s}$ Full Scalr MR1v -0 to $50 \mathrm{~m} / \mathrm{s}$ Full Scat $\mathrm{ME13}=0$ to $100 \mathrm{~m} / \mathrm{a}$ Full Bcale MR14－ 0 to $500 \mathrm{~m} / \mathrm{m}$ Full Beale ME15 $=0$ to $1 \operatorname{amp}$ Full Reale MR16 $\sim 0$ to 60 volte
ME17 $\sim 0$ to 300 volte

WAFER EWITCEDS

| Pole | 12 Way |  |  |
| :---: | :---: | :---: | :---: |
| 2 Pole | 2 Way | $\square$ |  |
| 2 Pola | 8 War |  |  |
| 2 Pole | 4 Way |  |  |
| 2 Pola | 6 Way |  |  |
| ${ }^{5}$ Pold | 4Way |  |  |
| 4 Pole | S Way | 87 gem | $\cdots$ ． |

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Resistance:
500 $\Omega$ - $500 \mathrm{k} \Omega$
Level: - 10 to $+12 \mathrm{db}$
Sensitivity:
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Instrument is powered by re-chargeable nickel cadmium batteries.
PRICE £10. 65


AC/DC MULTIMETER TYPE U4323 Apart from usual multimeter facilities the instrument incorporates fixed frequency Audio ( 1 kHz ) and I.F. ( 465 kHz ) Oscillators. 22 ranges covering AC Voltage 2.5-1000V: D.C. Voltage 0.51000 V ; D.C. current $50 \mu \mathrm{~A}$ to 500 mA and resistance 0 to $1 \mathrm{M} \Omega$. Sensitivity 20,000 o.p.v. Oscillator output voltage-1V minimum.
PRICE: $89 \cdot 20$

D.C. current $50 \mu \mathrm{~A}-2 \cdot 5 \mathrm{~A}$; A.C. current: $500 \mu \mathrm{~A}-2 \cdot 5 \mathrm{~A}$; $\mathrm{AC} / \mathrm{DC}$ voltage: $1-1000 \mathrm{~V}$; Resistance $300 \Omega-500 k \Omega$; Capacity up to $0.5 \mu \mathrm{~F}$; Transmission level: -15 to +2 db ; Sensitivity: $20 \mathrm{k} \Omega / \mathrm{V}$ D, $2 \mathrm{k} \Omega / \mathrm{V}$ AC.
PRICE $\mathrm{E14}$ - 25

PLEASE NOTE THAT NO OVERLOAD PROTECTION IS INCORPORATED IN ANY OF THESE INSTRUMENTS.
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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 3.70 | 62 |  |  |  |  |  |
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| .5 | -25 | 1.14 | 26 |  |
| 1 | 1 | 1.40 | 45 |  |
| 2 | 1 | 1.95 | 45 |  |
| 4 | 2 | 2.45 | 52 |  |
| 6 | 3 | 3.50 | 52 |  |
| 8 | 4 | 3.90 | 65 |  |
| 10 | 5 | 4.35 | 65 |  |
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