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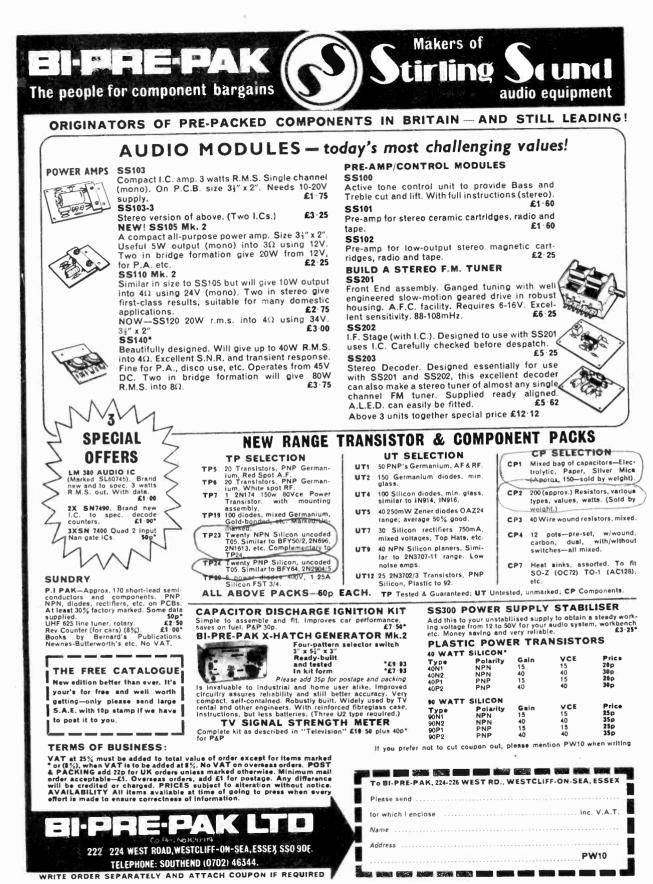
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panel reqd, ME6 0-50 µA, ME7	CASSETTES & TAPES C60 C90 C120
0-100 µA, ME8 0-	EMI Sound Hog 38p 48p 58p
500 µA, ME9 0-1	Compact Low Noise 320 410 500
mA, ME10 0-5mA, ME11, 0-10 mA, ME12 0-50 mA, ME13 0-100 mA,	BASFLH 55p 75p 97p
ME14 0-500 mA, ME15 0-1 amp.	LH Super 72p 90p £1.00 P&P 25p per order 10 or more P&P
ME16 0-50 volts AC, ME17 0-300 volts AC, ME18 "S", ME19 "VU".	FREE
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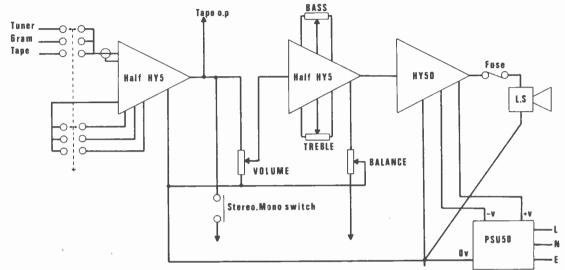
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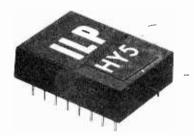
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MONO ELECTRICAL CIRCUIT DIAGRAM WITH INTERCONNECTIONS FOR STEREO SHOWN



The HY5 is a complete mono hybrid preamplifier, ideally suited for both mono and stereo applications. Internally the device consists of two high quality amplifiers—the first contains frequency equalisation and gain correction, while the second caters for tone control and balance.

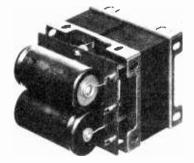
TECHNICAL SPECIFICATION Imputs: Magnetic Pick-up 3mV RIAA: Ceramic Pick-up 30mV: Microphone 10mV; Tuner 100mV; Auxillary 3-100mV; Main output dob (0:775V RMS). Active Tene Controls: Treble 1 120b at 10KHz; Bass ± 12db at 100Hz. Distortion: 0:5% at 1KHz. Signal/Noise Ratio: 68db, Overload Capability: 40db on most sensitive Input. Supply Voltage: ± 16-25V.



The HY50 is a complete solid state hybrid Hi-Fi amplifier incorporating its own high conductivity heatsink hermetically sealed in black epoxy resin. Only five connections are provided, input, output, power lines and earth.

power lines and earn. TECHNICAL SPECIFICATION Output Power: 25W RMS into 8Ω. Load Impedance: 4-16Q. Input Sensitivity 0db (0·775V RMS). Input Impedance: 47kD, Distortion: Less than 0·1% at 25W typically 0·05%. Signal/Noise Ratio: Better than 75db Frequency Response: 10Hz-50KHz ± 3db. Supply Voltage: ± 25V. Size: 105 x 50 x 25mm.

PRICE £5.98 + 48p VAT P. & P. & P. free



The PSU50 incorporates a specially designed trans-former and can be used for either mono or stereo systems.

TECHNICAL SPECIFICATIONS Output voltage: 50V (25-0-25V). Input Voltage: 210-240V. Size: L.70. D.90. H.60mm.

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Glass fibre P. C.B.s to suit AY-5-1224 clock chip and display etc. (Easily modified to give additional 4 range 'stopwatch' facility, our brief application note AN-D1 free on request, explains how). Board size 112 x 98mm. Type 1224-704E/PCB for 8mm high display 95p Type 1224-74E/PCB for 8mm high display 95p

SOONI

50 Hz clock timebase suggested circuit (single chip design using 3·2768 HMz crystal)—detailsfree. 1 Hz clock timebase suggested circuit (single chip design using 2·097152 MHz crystal)—details free.

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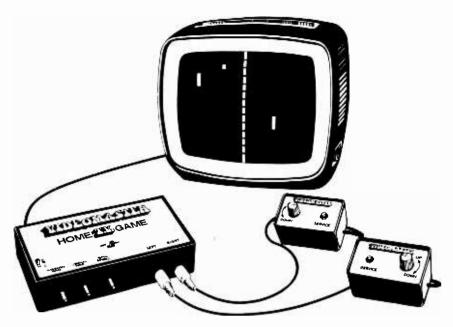
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Practical Wireless, November 1975

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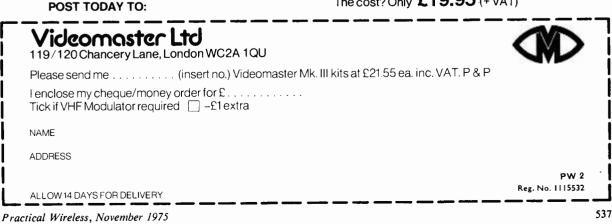
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Pak 1	fo. Description \$p	Pric
U 1		. 0.6
U 2		. 0.6
US	75 Germanium gold bonded sub-min. like OA5, OA47	. 0-6
U 4	30 Germanium transistors like OC81, AC128	0-6
U 5	60 200mA sub-min. silicon diodes	. 0.6
U 6	30 Sil. Planar trans. NPN like BSY95A, 2N706	. 0.6
U 7	16 Sil. rect. TOP-HAT 750mA VLTG. RANGE up to 100	0.6
U 8	50 Sil. planar diodes DO-7 glass 250mA like OA200/202	. 0-6
UΡ	20 Mixed voltages, 1 Watt Zener Diodes	. 0.6
U10	20 BAY50 charge storage diodes DO-7 glass	. 0.6
U 11	20 PNP Sil. pianar trans. TO-5 like 2N1132, 2N2904	. 0.6
U13	30 PNP-NPN Sil. transistors OC200 & 28104	. 0.6
U14		. 0-6
U15		. 0.6
U16		. 0.6
U17	30 Germanium PNP AF transistors TO-5 like ACY 17-22-	0.6
U18		. 0.6
U19		. 0.6
U20		0-6
U21		. 0.6
U23	and the second of the second sec	. 0.6
U24		. 0.6
U25		. 0.6
U26		0.6
U29		. #1-20
U82		0.6
U33		0.6
U34		0.8
USS		0.6
U86		. 0.6
U37		0.6
U38		0.6
U39		0.8
U40		0-6
U43		0.6
U44		0.6
U45		. \$1-20
U46		0.60
U40 U47	10 TO220AB plastic tracs 50V 6A	\$1.20
U48	9 NPN Sil. power transistors like 2N3055	£1·2
U40	12 NPN Sil. plastic power trans. 60W like 2n5294/5296	41.2
	No's mentioned above are given as a guide, to the type of	
the p	ak. The devices themselves are normally unmarked.	40.1001

				Q41	S Plastic NI
XCLUDE VAT AT 25% TO ALL *ADD 8% * NO VAT dd 20p overseas		uA.7812/L130 12 (Equiv. to uA.7815/L131 15	ATORS	Q43 Q44 Q45 Q46 Q47 Q48 Q49 Q50 Q51 Q52	3 Finkete 41 5 BC 107 N 5 BC 113 N 3 BC 113 N 3 BC 115 N 4 NPN high 2 × BC 16 3 BCY 70 P 3 NPN tran 52 7 BSY 28 N 7 BSY 28 N 7 BSY 95A 8 BY 100 ty 25 811. & Ge pew
inimum order 7		uA.7818 18V	MVR18V) \$1.2	Q54	6 TIL 209 1
*	THYRIS	TORS		*	UNTES
TO18 TO92 T 10 0.18 0.15	1A 3A 5A 105 T066 T06 - - - 0 20 0 25 0 3 0 25 0 25 0 4 0 25 0 80 0 5 0 80 0 85 0 45 0 80 0 85 0 65	6 TO64 TO48 T 6 0.36 0.48 (8 0.48 0.51 (0 0.50 0.57 (5 0.57 0.68 (9 0.69 0.78 (1 0.78	.0.A 16A 30 .0.48 TO48 TO .0.51 0.54 £1 .0.57 0.58 £1 .0.62 0.62 £1 .0.71 0.77 £1 .0.99 0.90 1.28 \$1.39 \$4	48 man spec ideal 18 Pak 43 UIC 68 UIC 79 UIC 79 UIC 07 UIC	ufacturers "Fr part Functions from the mak l for iearning. Wo. Contents 00 = 12 × 7400 01 = 12 × 7400 02 = 12 × 7402 03 = 12 × 7403 04 = 12 × 7404 05 = 12 × 7404 05 = 7406
AA119 0.068 B AA120 0.068 B AA120 0.068 B AA120 0.068 B AA230 0.069 B BAA230 0.068 B BA100 0.010 B BA116 0.11 B BA143 0.15 B BA144 0.15 B BA155 0.15 B BA164 0.15 B BA165 0.16 B BA173 0.15 B BB104 0.15 B	Price Y101 012 Y105 018 Y114 012 Y124 013 Y127 016 Y128 016 Y130 0.17 Y127 016 Y128 0.16 Y130 0.17 Y144 0.51 Y127 0.16 Y128 0.16 Y1210 0.30 YZ211 0.31 YZ212 0.41 YZ213 0.36	Type Price BYZ16 0.41 BYZ17 0.86 BYZ18 0.86 BYZ19 0.86 BYZ19 0.86 GG62 (0.49) Eq) CG62 0.40 CG62 0.40 CG63 0.40 CA10 0.47 CA10 0.47 CA79 0.47 CO479 0.47	OA85 O OA90 O OA91 O OA95 O OA90 O OA90 O OA90 O OA90 O OA202 O BD10 O BD19 O 1N344 O 1N914 O 1N916 O 1N916 O 18021 O	UIC UIC UIC UIC UIC 09 07 07 07 07 07 07 07 07 07 07 06 07 06 07 06 07 06 07 06 07 06 07 06 07 06 07 07 07 06 07 06 07 06 06 06 07 06 07 06 07 07 07 07 07 07 07	$\begin{array}{c} 0.7 = 8 \times 7407\\ 10 = 12 \times 7410\\ 13 = 8 \times 7413\\ 20 = 12 \times 7420\\ 30 = 12 \times 7420\\ 40 = 12 \times 7440\\ 41 = 5 \times 7441\\ 42 = 5 \times 7441\\ 42 = 5 \times 7441\\ 43 = 5 \times 7443\\ 44 \times 5 \times 7444\\ 45 = 5 \times 7445\\ 46 = 5 \times 7445\\ 46 = 5 \times 7445\\ 46 = 12 \times 7457\\ 53 = 12 \times 7457\\ 54 = 12 \times 7454\\ 54 = 12 \times 7454$

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	Q	U,		LIT	Y TE	STE	D P/	AKS
	Pak I					Tested Pak	CB	Price
	Q 1 Q 2					ors PNP transistors	PNP	0.60 0.60
	Q 3	4	00	277 typ	pe trans i	stors		0.60
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	Q 6				insistors		•••	0.60
	Q 7					s PNP hig		0-60
	Q 8 Q 9				ansistor pe transi		•••	0.60
	Q10		00	71 ty	pe trans	istors		0.60
	Q11	2	AC	2 127/ (P/NP1		omplement	ary pa	irs 0.60
	Q12		AI	F 116 ty	ype tran	sistors		0.60
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	Q26	8	0/	195 G		un diodes		in-
	Q27	2		[69 A 600]	 PIV Sill	 con rectifie	 TS IS425	0.60 B 0.60*
	Q28	2	Sil	licon pe	ower rec	tifiers BY2	2 13	0.60
	Q29	4	8i 1>	. trans (2N698	sistors 2 B .	2×2N696,	1×2N6	97, 0.60
	Q30	7	Bi	licon 89	witch tra	nsistors 21	N706 NP	N 0.60
	Q31 Q32					x 2N1131,		
	Q33		88	licon N	PN tran	sistors 2N	1711	0.60
	Q34	7	SI (c)	l. NPI ode P39	N tranı 97) .	a. 2N2369), 500M	Hz 0.60
ŀ	Q35	3	61	llcon P		-5 2×2N2		lχ
	Q.36	7			 FO-18 pl	 astic 300 1	 MHZ NP	. 0-60 N 0-60
1	Q37	3	21	13053 1	NPN Sill	icon transi	stors	0·60
	Q38 Q39	5	PI M	NP trai	nsistors :	$3 \times 2N3703$	$2 \times 2NS$	702 0.60 705 0.60
l	Q39 Q40	5	N.	PN trai PN trai	nsistors :	3 × 2N3704 3 × 2N3707	$2 \times 2NS$	708 0.60
Ŀ	Q41	8	P	astic N	PN TO:	18 2N3904	••	0.60
L	Q43 Q44	0 5	B	C 107 P PN trai	NPN tra naistors	панцога 3 × BC 108,	 2 × BC 1	0.60 09 0.60
L	Q45	8	B	C 113 b	NPN TO	-18 transis	tors	0.60
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	Q47		2	\times BC 10	68.			0.60
	Q48	3	B	CY 70	PNP tra	ansistors T 2×BFY	0-18 51 1 - B	0.60
	Q49	3	52	2				0.60
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L	Q51 Q52	7	B	BY 95A Y 100 t	A NPN t tvoe silk	ransistors con rectifie	300MHz 18	0.60 £1.20
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L	spec idea	' fre l foi	om rie	the ma arning	about I	.C.'s and e	ecificatio	ns, but are ntal work.
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	UIC	03 = 04 =	12	×7403 ×7404	0.60	UIC70 UIC70 UIC80	5= 8×7 3= 8×7)= 5×7	475 0-60 476 0-60
	TILC	06 =	- A	×7405 ×7406	0-60	UIC80 UIC81) == 5×7 L == 5×7	480 0-60 481 0-60
	UIC	07 =	8	× 7407 × 7410	0-60	UIC82	2 <u>=</u> 5 × 7	482 0.60
	UIC	13=	- 8	×7413	0.60	UIC83	$3 = 5 \times 7$ $3 = 5 \times 7$	482 0.60 483 0.60 486 0.60
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	UIC	47 -	- 5	$\times 7447$	0.60	UIC19	$21 = 5 \times 7$ $41 = 5 \times 7$	4121 0.60
		ŏ0 =	-12	× 7448 × 7450	0-60	UICI	$51 = 5 \times 7$ $54 = 5 \times 7$	4151 0.60
	UTC	ŏ3 =	12	×7451 ×7453	0.60	UICI	93=5×7	4193 0.60
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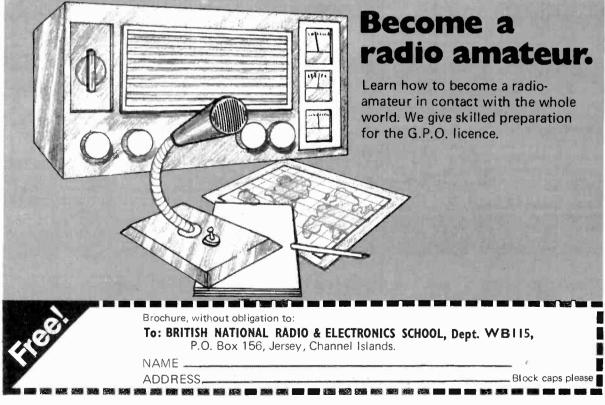
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EBF89 0.50 EF183 0.69 PCF86 0.73 EC86 0.82 EF184 0.69 PCF200 1.13	PY500A 1-18 PCE800 0-98 PY800 0-56 30FL2 1-02	ACY39 0.75 BF197 0.16 OC20 2.00 ZTX550 0.18 2N2906 0.20 ACY39 0.75 BF200 0.82 OC23 1.25 1N914 0.06 2N2926 0.12
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ECC81 0.54 EL84 0.58 PCF806 0.73 ECC82 0.53 EL86 1.06 PCH200 1.30	U193 0.56 0.68 UABC80 1.01 30L15/ UABC81 0.69 PCC805 1.85	AD162 0.44 BFX29 0.28 OC36 0.60 IN4004 0.08 2N3614 0.65 AF115 0.25 BFX88 0.24 OC42 0.40 IN4005 0.10 2N3615 0.65
ECC83 0.53 EL95 0.78 PCL82 0.63 ECC84 0.63 ELL80 2.81 PCL83 0.73	UBF89 0.65 30P4MR 1.68	AP116 0-54 D2 00 020 0C44 0-20 IN4008 0-18 2N3702 0-11 AP117 0-54 BF750 0-20 0C45 0-20 IN4007 0-12 2N3703 0-12 AP185 0-45 BF752 0-20 0C71 0-18 IN4009 0-06 2N3704 0-14
ECC88 0.91 EM84 1.34 PCL85 0.72 ECC189 0.77 EM87 1.25 PCL86 0.78	UCC85 0.66 30P1Z/ UCH81 1.30 PC801 1.22 UCL82 0.78 30P19/	AF239 0.48 BR100 0.40 OC72 0.88 1N4148 0.06 2N8705 0.15 ASY27 0.88 BY100 0.27 OC76 0.80 18921 0.07 2N8706 0.11
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ECH81 1.29 EZ80 0.68 PL36 1.06 ECH83 1.06 EZ81 0.53 PL81 0.91	UY85 0-63 PCL801 1-35 6/30L2/ ECC804 1-20 PCL800 1-47	BC107 0.14 0.20 OC81Z 0.45 183010 0.35 2N3710 0.11 BC108 0.18 BZY88 series OC83 0.27 2N696 0.15 2N3711 0.11
ECH84 1.17 GY501 1.80 PL81A 1.06 ECL80 0.78 GZ34 0.91 PL82 0.48 ECL82 0.69 PC86 1.05 PL83 1.29	6F23/EF812 30PL14/ 1.16 PCL88 1.72	BC109 0-12 0-10 0-10 0-140 1-14 2N697 0-18 2N8919 0-38 BC113 0-15 CR81-05 0-35 0-C170 0-30 2N706 0-10 2N8820 0-56 BC117 0-21 CR81-40 0-50 0-C171 0-80 2N706A 0-13 2N8829 0-50
ECL82 0.69 PC86 1.05 FL83 1.29 ECL83 0.72 PC88 1.05 PL84 0.78 ECL86 0.73 PC97 0.53 PL500 1.02	30C1/PCF80 30PL15 144	BO143 0-80 CRB3-05 0-40 OC200 0-55 2N1181 0-35 2N3903 0-15 BO147 0-10 CRB3-40 0-85 OC201 1-00 2N1182 0-34 2N8904 0-20
NEW VALVEO	PY83 0.60 6F28 0.75	BC148 0-08 MJE340 0-47 OC202 0-90 2N1802 0-18 2N3906 0-25 BC169C 0-15 MJE370 0-88 OC203 0-55 2N1803 0-18 2N3906 3-25 BC182 0-18 MJE520 0-55 OCP71 1:20 2N1804 0-38 2N4056 6-15
NEW VALVES	PY88 0.58 6J5M 0.65 PY500 1.10 6J5G 0.45 PY81/800 0.50 6J6 0.85	BO162L 013 MJE2955 1.27 ORP12 0.60 2N1305 0.33 2N4059 0.10 BO184L 013 MJE3055 0.75 ORP60 0.55 2N1306 0.38 2N4060 0.13
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AZ1 0.75 EF39 1.25 KTW61 1.50	UBF89 0.50 68Q7GT 0.40 UCC85 0.60 6U5G 1.50	BN7403 0.16 BN7417 0.87 1.00 SN74184 2.00 BN74195 1.10 BN7404 0.28 BN7438 0.37 BN7492 0.70 BN74155 1.00 SN74196 1.20 BN7405 0.28 BN7438 0.37 BN7492 0.70 BN74155 1.00 SN74196 1.20
AZ31 0.60 EF80 0.35 MU14 1.00 CBL31 1.40 EF85 0.45 N78 8.50 CL33 1.50 EF86 0.50 OA2 0.45	UCH42 0.80 6V6G 0.80 UCH81 0.50 6V6GT 0.60 UCL82 0.40 6X4 0.45	BN7406 0.42 BN741AN BN7494 0.80 BN74157 0.95 BN74198 2.77 BN7407 0.42 0.92 BN7495 0.80 BN74170 2.52 BN74199 2.52
CY31 0.60 EF89 0.85 OB2 0.45 DAF91 0.40 EF91 0.40 PC86 0.65	UCL83 0.70 6X5G 0.45 UF41 0.75 6X5GT 0.55	BN7408 0-28 BN7442 0-79 BN7496 0-96 BN74174 1-57 BN7409 0-28 BN7450 0-16 BN7497 8-87 BN74175 1-10 BN7410 0-18 BN7451 0-18 BN7410 1-89 BN7417 1-28
DCC90 1.86 EF95 0.45 PC97 0.55 DF91 0.40 EF98 0.80 PC900 0.55	UF89 0.50 7B6 0.80 UL41 0.85 7B7 0.80 UL84 0.50 7C5 1.80	8N7411 0.25 8N7453 0.16 8N74107 0.46 8N74190 2.00 8N7412 0.80 8N7454 0.16 8N74110 0.58 8N74191 2.00
DF96 0.60 EF183 0.40 PCC84 0.45 DK91 0.50 EF184 0.40 PCC88 0.62 DK92 1.00 EL32 0.60 PCC89 0.55	UY41 0.55 7C6 1.00 UY85 0.45 7H7 0.80	BN7416 0.88 BN7470 0.88 BN74119 1.68 BN7417 0.88 BN7473 0.41 BN74121 0.50 DIL 14 pin 15p
DK96 0.75 EL33 2.50 PCC189 0.85 DL92 0.50 EL34 0.70 PCF80 0.40	VR150/30 0.45 787 8.25 1R5 0.50 7Y4 0.80	BN7420 0-16 BN7474 0-42 BN7412 0-70 BN7422 0-25 BN7480 0-80 SN74123 1-00 BN7423 0-87 BN7483 1-10 BN74114 0-90 SOCKETS 16 pin 17p
DL96 0.55 EL37 2.60 PCF86 0.65 DY86 0.45 EL41 0.90 PCF801 0.60	185 0.40 12AT5 0.45 1T4 0.40 12AT7 0.45 384 0.50 12AU6 0.50	VAT THIS MONTH'S
DY87 0.45 EL42 1.65 PCF802 0.55 DY802 0.47 EL84 0.85 PCF805 0.90 EABC80 0.88 EL95 0.60 PCF806 0.80	3V4 0.85 12AU7 0.88 5R4GY 1.00 12AX7 0.88	VAT
EAF42 0.70 ELL80 2.00 PCF808 1.00 EB91 0.80 EM80 0.55 PCL82 0.45	5Y3GT 0.65 12BE6 0.60 5Z4G 0.65 30C1 0.40	To be added • OSCILLOSCOPE TUBES
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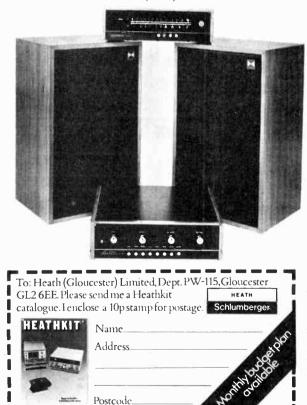
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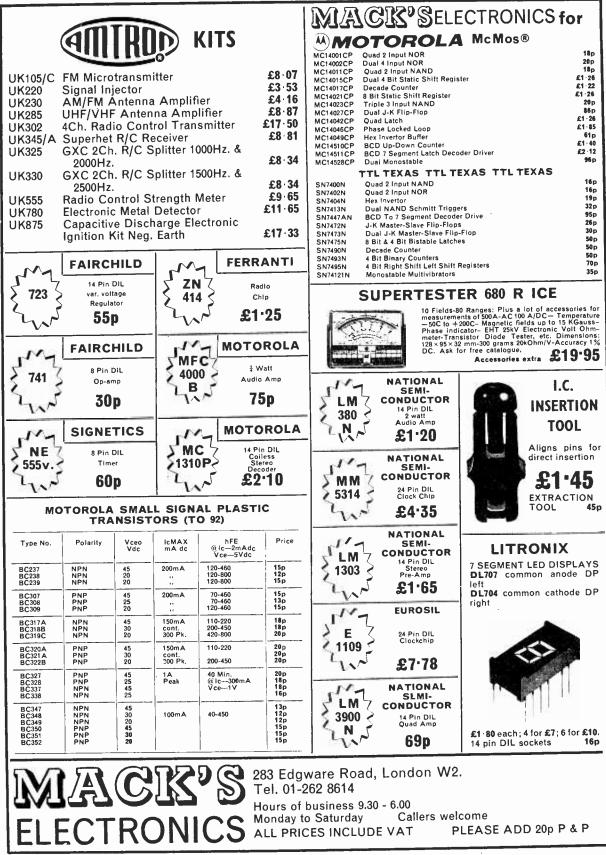
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Our Price £34.00 each

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EMI 350 KIT

System consists of a 13" × 8" approx. woofer with a 3" tweeter, crossover components and circuit diagram. Frequency response: 20 Hz to 20 KHz. Power handling 15 watts RMS into 8 ohms. (Peak 30 watts.)

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A compact bookshelf speaker system giving a high electro accoustic efficiency for the low powered amplifier. The professional finish can be obtained with the minimum of tools, the infinite baffle type enclosures come ready mitred and professionally finished, simply upply glue, fold up around baffle board, and fix to jether with masking tape till glue dries.

The cabinet measures 12"x9"x5" deep approx finished in simulated teak, incorporating a quality 7'x4" elliptical speaker, power handling 4 watts, flux density 30.000 maxwells, impedance 8-15 ohms nominal, voice coil dia 3" magnet size 27" approx.

EASY TO BUILD SPEAKER KITS

These superb simulated teak-finished speaker kits have been specially designed by RT-VC for the cost-conscious hi-fi enthusiast who wants top quality speakers but doesn't want to spend the earth. Built to EMI's

exacting specification, these new RT-VC speaker kits (350 type kit) incorporate $13'' \times 8''$ woofer $3\frac{1}{2}''$ tweeter and matching crossover.

Easily put together with just a few basic tools. Specification (each speaker): Impedance 8 ohms. Power handling 15 watts RMS (30 watts peak). Response 20–20,000 Hz. Size 20" × 11" × 94" approx. Comparable built units (EMI LE3) sold elsewhere for over £45 pair.



Complete with crossover Components and circuit diagram



System 1a. £69.00

The new 20+20 watt Storeo Amplifier incorporating the latest silicon transistor solid state circuitry, the RT-VC VISCOUNT IV gives you a powerful 20 watts RMS per channel into 8 ohms. Superb teak-finished cabinet, with anodised fascia to harmonise with any decor. Polished trim and knobs. The VISCOUNT IV has a comprehensive range of controls - volume, bass, treble, balance, mono/stereo,

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CONTNOLS: Push button UN/UPF, stereo/mono, scratch filter. 6 position rotary selector. Individual motory control for treble, bass, balance and volume. Headphone socket, tage out socket. Aux. mains output. Frequency response: 25 Hz to 25 KHz a full rated output. Signal to noise ratio: better than -50 dB on all inputs. Tone control range: Bass ± 15 dB \pm 50 Hz; Treble ± 12 dB \pm 10 KHz. Power requirements: 200-250V AC. mains \pm 60 wetts. Approx. size: $15\frac{1}{4} \times 3^{-1} \times 10^{-1}$. MP60 type deck with magnetic cartridge, de luxe plinth and cover. Two Duo Type IIa matched speakers — Lenclosure size approx. $19\frac{1}{4} \times 10\frac{1}{4} \times 7\frac{1}{4}$ in simulated teak. Drive unit 13" \times 8" with 3" roweter. 15 watts handling. 30 watts peak. Complete System with these speakers <u>£69.000</u> + £6.50 p & p.

System 2. £85.00

Viscount IV amplifier (As System 1a) MP60 type deck (As System 1a)

MPbU type deck (As System 1a) Two Duo Type III matched speakers – Enclosure size approx. 27" × 13" × 11 4". Finished in teak simulate. Drive units 13" × 8" bass driver, and two 3" (approx.) tweeters. 20 watts RMS, 8 ohms frequency range – 20 Hz to 18,000 Hz. Complete System with these speakers COLOR - CE SOL & S.

peakers £8500 +£7.60 p&p.

PRICES: SYSTEM 1a Viscount IV R103 amplifier 2 Duo Type IIa £27.50+£1.90 p & p. speakers £30.00 + £8.50 p & p. MP60 type deck with Mag. cartridge de luxe plinth £22.00+£3.30 p& p and cover Total if purchased separately: £79.50 Available complete for only: £69.00 +£6.50 p & p.

PRICES: SYSTEM 2 Viscount IV Rt03 £27.50+£1.90 e & i amplifier

2 Duo Type III £46.00+£7.50 p & p. speakers MP60 type deck with Mag. cartridge de luxa plinth and cover £22.00 + £3.30 p & p. Total if purchased separately: £95.50 Available complete for only £85,00

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Controls volume manual tuning and five push buttons for station selection, illuminated tuning scale covering full, medium and long wave bands.

scale covering run, user Size-chassis 7" wide 2" high £9.50 + £1.05 p & p. £9.50 + £1.05 p & p. Speaker including baffle and fixing strip £2.00 +45p p & p. Car Aerial Recommended - fully retractable £1.60+40p p & p.

The Tourist I Kit For the experienced constructor. If you can solder on a printed circuit board you can build this model. Same technical specification Price £8.20+£1.05 p & p. as Tourist TT.

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Stereo 21, easy to assemble audio system kit. No soldering required

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unusually interesting variation on the modern deck plinth. Includes – BSR 3 speed deck, automatic, manual facilities together with stereo cartridge. fwo speakers with cabinets.

Amplifier module Ready built with control panel speaker leads and full, easy to follow assembly instructions

tul, easy to ionow assembly institutions. Specifications – For the technically minded: Input sensitivity 600mV Aux, input sensitivity 120mV. Power output 2.7 watts per channel. Dutput impedance 8–15 ohms. Stereo headphone socket with automatic speaker cutout. Provision for auxiliary inputs – ratio, tape, etc., and outputs for taping discs. Overall Dimensions. Speakers approx 15 $\frac{1}{2}^{+} \times 8^{+} \times 4^{+}$. Complete deck and cover in closed position approx. 15 $\frac{1}{2}^{+} \times 12^{+} \times 6^{+}$.

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Extras if required. Optional Diamond Styli £1.60. Specially selected pair of stereo headphones with individual level controls and pædded earpieces to give optimum performance £5.80.



Reliant Mk IV Mono Amplifier, ideal for the small disco or house parties. Output 20 watts RMS into 8 ohms (suitable for 15 ohms).

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for use with your stereo system. Compatible with Viscount IV system, Unisound module and the Stereo 21. Technical specification Mains input, 240V, Output sensitivity 125mV.

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The future of Amateur Radio

THE life blood of amateur radio is the spectrum space allocated to the amateur service between 1.8MHz and 25GHz. Without these precious frequencies, the radio amateur of today would become just another broadcast station listener. The regulation of the frequencies available to the various services, i.e. aeronautical, amateur, broadcasting, marine and so on, is governed by the conferences of the International Telecommunication Union which is the specialist agency of the United Nations for telecommunications. During the ITU conference the 144 member nations of the ITU vote on the proposals before them and in this way the future of frequency allocations is determined.

The last major ITU conference was in 1959 and there has been relatively little change in the spectrum allocation for amateurs since that time. The next major meeting is scheduled for October 1979 and the agenda will include a review of all frequencies comprising the usable spectrum. This means that each and every amateur service allocation will come under the scrutiny of the conference. On their decision alone will depend whether your present equipment will continue to be usable, or will be just another piece of surplus gear.

The possibilities and dangers arising from the 1979 World Administrative Radio Conference have been known and recognised by national societies and the International Amateur Radio Union for some considerable time. A great deal of preparatory work has already been undertaken and it is now clear that the amateur service will at this conference present a unified plan for its future modified only by minor regional differences. At the conferences of the ITU only the member nations are elegible to vote. However, the IARU is one of the few organisations recognised by the ITU and therefore entitled to attend its conferences as an observer where it may also speak and present papers.

Thus, while the IARU may participate actively in the conference its most essential work must take place in the co-ordination and advice offered to national societies throughout the world. It is the national societies only who can approach their own telecommunication administrations to seek their support for the future of the amateur service. It will be appreciated that in many countries this is a difficult task, never more difficult than in Africa. This is a challenge which has been accepted by the IARU and the national societies and the work of securing support for radio amateurs will continue without slackening until October 1979.

It would be unwise to give publicity to much of the work that has been, and will be done, and it is only the result that can prove its effectiveness or otherwise.

Now, as never before, the amateur service must be seen by all who come into contact with it to be something that is worth retaining and whose work and activity justify the present spectrum space allocated to it. Every radio club in every country has a part to play in this effort. It is the local radio clubs who bring together the individual radio amateurs and who form the backbone of the national societies. Those responsible for the conduct of a radio club should familiarise themselves with the position as it is today and with the steps that must be taken if the future is to be assured. Having done this they can then offer guidance to the individual members and initiate activity which will be of benefit not only to the amateur service but hopefully to the community at large.

continued on page 551

Practical Wireless P. C. Board Readers Service

I N the October issue of Practical Wireless we announced that this magazine will be introducing a 'new' readers service whereby our 'copyright' printed circuit boards for selected PW constructional projects will be offered to readers.

We are anxious this service shall represent good value and our boards to be of the highest standards, therefore we are taking a further month to finalise the details which we hope to publish in full in the near future.

Reprints

E still have some copies of the Tele-Tennis reprints. If you would like one, send 82p to: Chief Cashier, (P.W. Tele-Tennis, IPC Magazines, Tower House, Southampton St., London, WC2E 4QX.

Special offer

H^{I-FI} enthusiasts buying cassette decks which accept chromium dioxide cassettes will find there is a dearth of prerecorded CrO₂ cassettes. To ensure that purchasers of BASF machines are able to use their machines to the full, BASF is giving them the opportunity to buy BASF prerecorded CrO₂ cassettes at special low prices.

The repertoire contains 22 titles, four of which are double albums. The price of the cassettes is $\pounds 3.90$ for a single album and $\pounds 5.80$ for a double album, but BASF are offering them at $\pounds 1.99$ and $\pounds 2.99$ (inclusive of VAT) respectively. Six of the titles have been recorded in quadraphonic and these are available at no extra cost.

All the purchaser has to do is ask for a BASF Cassette Offer order form when he buys a BASF machine, tick the titles he wants and send the form with a cheque or postal order for the correct amount to BASF at its Knightsbridge, London, a d d r e s s. Customers may only send in one order form so they should ensure that they have all the titles they require.

NEWS ...



ANY interesting new models are introduced in the latest Heathkit Catalogue: They are TM-1626 Stereo Microphone Mixer; TA-1620 Public Address Control Amplifier with optional Booster Amplifier, Speaker Column, or Distribution Trans-former; ID-1590E Digital Electronic Wind Speed and Direction Indicator: IM-1212 Digital Multimeter; IO-4560 DC-5MHz, 100mV Oscilloscope; IO-4540 DC-5MHz, 20mV Oscilloscope; IG-4505 Oscil-loscope Calibrator; IP-2700 Series of Digital and Analogue Power IMA-18-1 Solid-state Supplies: Conversion Kit for valve-type Heathkit VVm's; SR-205 Single Pen Chart Recorder; SR-206 Dual Pen Chart Recorder.

Heath also tell us that their electronic organ (shown in October "Production Lines") is on show at the Tottenham Court Road showroom.

The latest Heathkit Catalogue is now available: To postal enquiries, enclosing a 10p stamp for return postage, from: Heath (Gloucester) Ltd., Bristol Road, Gloucester GL2 6EE.

"Radio Exchange"

DUE to a printing error the above advertiser's full page advertisement in the September, 1975 issue was incorrectly priced. The magazine apologises for any inconvenience caused to readers.

Practical Wireless, November 1975

British 'Scope

NEWS

HE only independent British oscilloscope manufacturers,

Scopex Instruments, have just launched an addition to their range of low cost oscilloscope. The new 'scope, called the 4S-6, is intended for use in educational, service and amateur areas.

The new instrument follows the design philosophy of other machines in the range with emphasis on ease of use, with controls kept to a minimum and well labelled. Price is only £88 yet the specification is equivalent to similar units costing as much as twice that price. Main features are a maximum sentitivity of 10mV/cm and a bandwidth of 6MHz. The screen is a big $6 \times$ 8cm for ease of viewing. The weight of the unit is only 4.5kg making it eminently suitable for field work. One feature of the 4S-6 only found on oscilloscopes



NEWS.

costing about £100 more is the beam locate facility which allows even the most inept operator to locate and return the trace to screen.

For further information contact Scopex Instruments, Pixmore Industrial Estate, Pixmore Avenue, Letchworth, Herts.

THE FUTURE OF AMATEUR RADIO

---continued from page 550

There are several forms of scientific activity in which the individual radio amateur can participate and play a valuable part. There is no other organisation in the world that can command the services of so many able technicians capable of carrying out specialist work at no cost to the community. As an example, we cite propagation research, possibly using the beacons already established in several parts of the world. Amateur progress in microwaves has astonished professional workers and this is a fertile field for experiment and development. The amateur satellite programme is another area where the skills of construction or mere observations can vitally assist research activity. In addition to participation in scientific activity the radio amateur must ensure that his transmissions are beyond reproach both in technical characteristics and in the messages conveyed. There are many listeners to amateur radio transmissions and the listener can only judge the quality by what he hears. Regrettably in many cases the quality leaves much to be desired.

The Radio Society of Great Britain* has always played a leading part in the representation of amateur radio at international levels. It is already heavily involved in the preparations for 1979 and will continue to make a maximum effort on behalf of *all* UK radio amateurs.

The future of amateur radio now depends upon the IARU, the national societies, the local clubs and, not least of all, the individual operator. Will you play an active and responsible part in the world wide activity intended to ensure the future of amateur radio?

LIONEL E. HOWES-Editor

* Radio Society of Great Britain, 35 Doughty Street, London, WCIN 2AE

WITH the increasing number of local radio stations occupying the VHF band, an accurate frequency indication is very desirable. The tuning scale provided on most FM tuners is rarely accurate enough to differentiate between two adjacent stations because it depends on the linearity of a variable capacitor, or a varicap diode for its accuracy. This problem is overcome in very expensive synthesiser tuners by generating the local oscillator digitally using a programmable frequency divider and a reference oscillator.

Martin Oliver*

It is possible to provide the same digital display of frequency with a conventional tuner by counting the local oscillator frequency, and this method does not require much modification of the tuner.

The frequency counter described in this article gives an accurate tuning indication over the 88-108 MHz band, and can be easily modified to cover other ranges. It was designed to be used with a Heathkit model AJ1214, but it should work with most transistor tuners.

ISOLATION

PART 1

It is important that the tuner chassis is fully isolated from the mains. Most modern tuners use a mains transformer to provide a low voltage supply for transistor circuits, and the chassis is connected to earth through the mains plug or is left floating. Check carefully that the chassis is not connected



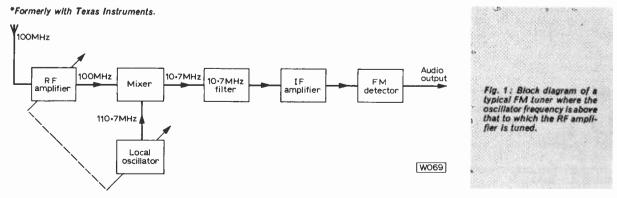
directly to the line or neutral pin of the mains plug as it is then dangerous to connect external components to it and this circuit **must not be used**.

One problem which usually occurs, when building high frequency circuits is the need for special equipment, such as HF signal generators and oscilloscopes to set the circuit up. To get around this problem, broadband circuits are used in the HF sections of this design so there are no coils to be aligned, and the only equipment needed is a multimeter.

The unit is built on Veroboards contained in a separate metal case, and is connected to the tuner by coax cable. A metal box is needed as a screen between the tuner's sensitive front end and the logic ICs.

FM TUNER OPERATION

Before explaining how the circuit works, a brief description of the operation of an FM tuner may be useful. Fig. 1 shows a simplified block diagram of a



Practical Wireless, November 1975

"conventional" tuner. It is assumed to be tuned to a station on $100 \cdot 0$ MHz. A signal picked up by the aerial is amplified by the RF amplifier to a level suitable for the mixer. The local oscillator runs at a frequency $10 \cdot 7$ MHz above or below the frequency to which the RF amplifier is tuned. The output from the mixer is the IF frequency which is the difference between these two signals, i.e. $10 \cdot 7$ MHz. The mixer feeds the IF amplifier via a bandpass filter which gives the tuner its selectivity.

It is not possible to measure directly the frequency of the signal from the aerial because this consists of many other stations apart from the one being received. Because of this the local oscillator is used, but as this is not the same frequency as the station being received, a correction must be made in the counting circuit. In the example of Fig.1, 10.7MHz must be subtracted from the measured frequency before it can be displayed.

Fig. 1 shows the local oscillator at a higher frequency than the RF amplifier. This is the more usual case, but if the oscillator was lower, i.e. $89 \cdot 3MHz$ then $10 \cdot 7$ would have to be added to the count.

SYSTEM OPERATION

A block diagram of the complete system is shown in Fig. 2. The system operates by enabling a 'gate' for an accurately defined sampling period and counting the number of input cycles which occur during that time. TTL decade counters are used, but be-

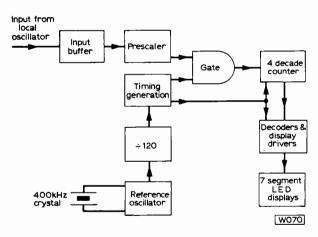


Fig. 2: Block diagram of the complete Digital Readout System.

cause the local oscillator frequency can be above 100MHz it must be divided to a frequency which TTL can handle. This is done in the prescaler, which divides the input frequency by three. So if the local oscillator varied over the range 99 to 119MHz the output of the prescaler would be between 33 and 40MHz which is low enough for the TTL counters.

It is important that the local oscillator is not loaded by the circuit connected to it as this would reduce the output or shift the frequency. To avoid this a high input impedance buffer is used. This is the only part of the circuit which is mounted inside the tuner.

To give the correct display for the number of digits used, a counting period of $300\mu s$ is needed. To get the required accuracy a crystal must be used, but to oscillate with a period of $300\mu s$ it would be

very large and expensive. In this design a 400kHz crystal is used followed by series of counters to divide the frequency by 120.

IF OFFSET COMPENSATION

The adding or subtracting of the IF frequency is accomplished by using presettable decade counters, (one for each displayed digit).

To add 10.7 to the displayed frequency the counters are loaded with this number before counting starts. The output from the counters is in binary coded decimal (BCD) and the decoders convert this to drive the seven segment LED displays. Because the most significant digit (hundreds) can only be 0 or 1, a separate decoder is not needed. The counting and display sequence takes 4.8ms as follows:

- 1) Load counters with IF offset frequency 300 µs 2) Enable input gate to counters 300 µs
- 2) Enable input gate to counters
 3) Display result
 300μs
 4.2ms

During 1) and 2) the display is blanked, and this modulates the light output at about 200Hz, but the eye cannot follow this, and the display appears steady.

ELIMINATING JITTER

With counters of this type there is always an uncertainty of ± 1 digit depending on the phase difference between the input and the sampling pulse. This normally causes the last digit to jitter, but when the last digit jitters between 9 and 0 the next digit is also affected. This is especially troublesome in this case as nearly all UK stations are on multiples of 100kHz, so the fifth digit (10kHz) would normally be zero and the jitter would pass on to the next digit.

The problem is overcome by adding 50kHz to the number which is loaded into the counter. Now, when a station is tuned in, the last digit reads five instead of zero, and the jitter is confined to this digit. Although it cannot be displayed as tens of kilohertz the last digit is used to indicate how accurately the station is tuned in. If the last digit is 3, 4, 5, 6 or 7 it is blanked. When it is 0, 1 or 2 a minus sign is displayed and for 8 or 9 a plus sign appears. This tuned in, and still gives sufficient accuracy.

INPUT BUFFER

Fig. 3 shows the circuit of the input buffer. which is simply an emitter follower. This has the advantage of a low output impedance, which is needed to drive

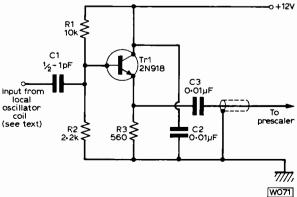


Fig. 3: Circuit diagram of the input buffer.

INPUT BUFFER	LOGIC BOARD AND DISPLAY	
$ \begin{array}{c} \text{Resistors} \\ \text{R1} 10k\Omega \\ \text{R2} 2\cdot 2k\Omega \\ \text{R3} 560\Omega \end{array} $	Resistors R20, R21 820Ω (2 off) R22-R30 330Ω (9 off) R31 680Ω R32-R45 330Ω (14 off) R46 180Ω	
Capacitors C1 ½1pF (see text) C2, C3 0·01µF ceramic	All ±W ±5%	
$\begin{array}{c} \textbf{Transistor} \\ \textbf{Tr1 2N918} \\ \hline \\ \textbf{PRESCALER} \\ \textbf{Resistors (All \pm 5\% \ 4 \text{W}) \\ \text{R4 100\Omega} \\ \text{R5 47\Omega} \\ \text{R5 47\Omega} \\ \text{R6 470\Omega} \\ \text{R12 68\Omega} \\ \text{R5 47\Omega} \\ \text{R6 470\Omega} \\ \text{R14 220\Omega} \\ \text{R7 2-7} \text{K}\Omega \\ \text{R7 2-7} \text{K}\Omega \\ \text{R15 1-5} \text{K}\Omega \\ \text{R8 82\Omega} \\ \text{R16 12} \text{K}\Omega \\ \text{R9 180\Omega} \\ \text{R17 10} \text{K}\Omega \\ \text{R10 180\Omega} \\ \text{R18 2.2} \text{K}\Omega \\ \text{R11 68\Omega} \\ \text{R19 220\Omega} \\ \text{VR1 220\Omega miniature preset} \\ \hline \\ \textbf{Capacitors} \\ \textbf{C4-C8 0.01} \text{//F ceramic (5 off)} \\ \text{C9 20pF trimmer (DAU or similar)} \\ \end{array}$	Capacitors C11 0·1μF ceramic C12 680pF polystyrene C13 470pF polystyrene C14-C20 0·1μF ceramic (7 off) Semiconductors IC2 SN7404N IC3 SN7408N IC4 SN7408N IC5 SN7408N IC6 SN7493AN IC7 SN7493AN IC8 SN74196N IC8 SN74196N IC9 SN7447AN LED1 TIL304 LED5 TIL304	
C10 0·01µF ceramic Semiconductors Tr2-Tr4 2N918 (3 off) ICI SN72733N Texas	Crystal X1 400kHz (Channel 16, FT241—Interface Quartz Devices Ltd. 29 Market St., Crewkerne, Somerset. Tel. Crewkerne 2578).	

the 75 Ω coax lead connecting the tuner to the display circuit.

The input is taken from the local oscillator tuned circuit where the signal is about 1V peak-to-peak. A very low value coupling capacitor C1 is used to reduce the loading at this point.

The 12V supply can be taken from the tuner itself as the current drain is only 4mA. If there is no convenient 12V line in the tuner, then a separate wire can be taken from the 13V line in the main unit.

The coax cable couples the buffered local oscillator signal to the prescaler.

PRESCALER CIRCUIT

The basis of the prescaler is an SN72733 video amplifier (IC1 in Fig. 4). This is biased as a Schmitt trigger by connecting the output to the non-inverting input via R13. This is then made to oscillate by the feedback provided by R15, R14 and C9, where C9 sets the frequency.

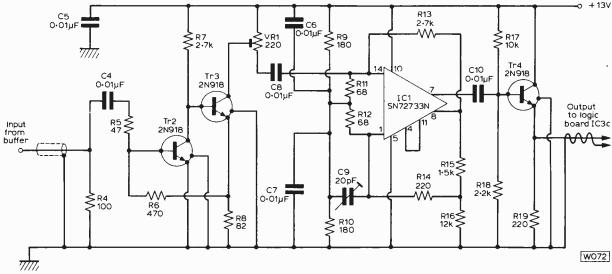
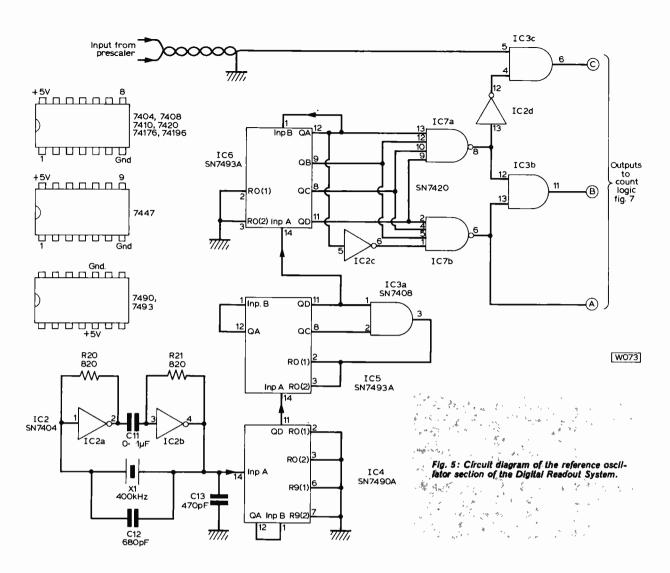




Fig. 4: Circuit diagram of the prescaler unit which uses the Texas SN72733N video amplifier IC.



The signal from the buffer is amplified and coupled to the 733 oscillator which locks to one-third of the local oscillator frequency. The trimmer, C9, is used to adjust the free running frequency to the centre of the band so that the 733 can be pulled higher or lower in frequency.

Tr2 and Tr3 are connected as a DC feedback pair which gives reasonable gain over a wide frequency range. The gain is adjustable with VR1 to allow for variations in the amplitude of the local oscillator signal.

The other output of the 733 is fed to an emitter follower Tr4 which provides a low impedance drive at the correct level for the TTL circuit.

REFERENCE OSCILLATOR

Fig. 5 shows the circuit diagram of this section. The reference oscillator is made from SN7404 inverters which are biased into the linear region by resistors connected from output to input.

Two inverters are needed to give positive feedback. The frequency of 400kHz is determined by the crystal X1. Capacitors C12 and C13 are needed to prevent the circuit oscillating at one of the crystal's harmonic frequencies. TTL counters are used to reduce the reference frequency. IC4 is an SN7490A which contains divide by two and divide by five circuits. By connecting output QA to input B it will divide the input frequency by 10. IC5 contains a divide by two and a divide by eight circuit. To give the necessary output frequency this must divide by twelve which is

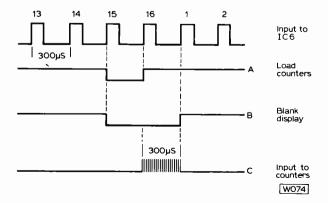


Fig. 6: Waveforms at various positions in Fig. 6.

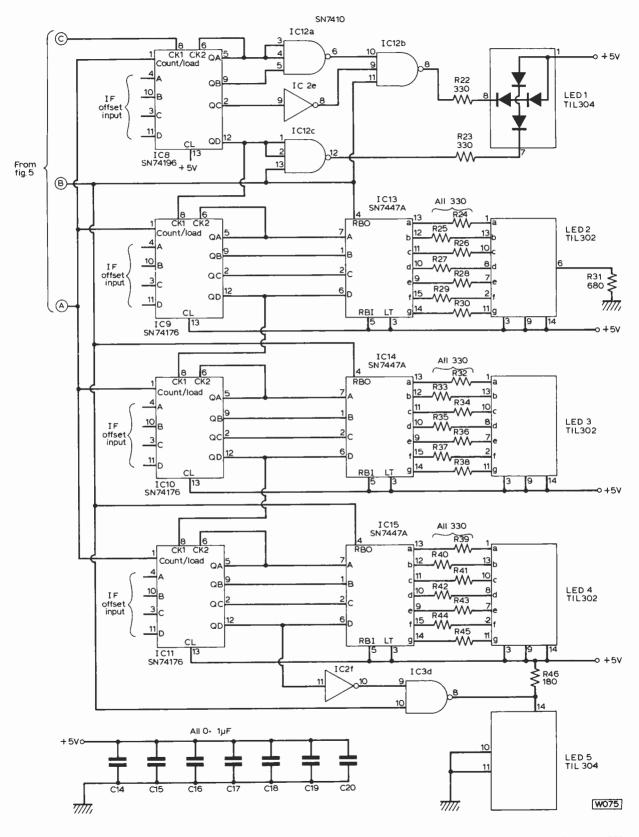


Fig. 7: Circuit diagram of the Counting and Display Logic.

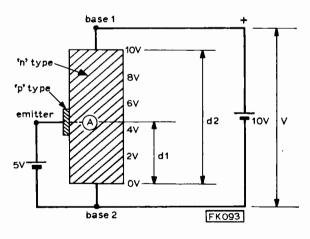
continued on page 558 Practical Wireless, November 1975

UNIJUNCTION TRANSISTOR TESTER

THE unijunction transistor tester described here is basically a simple go/no-go tester, giving some indication of the intrinsic stand-off ratio. The total cost of components is about 80p, provided a multimeter with a suitable range is available.

Unijunction Theory

To understand the operation of this instrument, a certain basic knowledge of unijunction theory is necessary. A unijunction consists of a bar of N type silicon with contacts at each end. On this bar there is a P-N junction. When a voltage V is applied across the Bar, a voltage which is less than V appears at A. The voltage at A is found by multiplying V by $\frac{d1}{d2}$ When the emitter voltage rises above that at A by about 0.7V, current begins to flow through the now forward-biased P-N junction. This reduces the voltage at A, so that the current continues until the voltage at the emitter falls below 0.7V. The ratio $\frac{d1}{d2}$ is the Intrinsic Stand-Off Ratio.



Theoretical circuit of a unijunction transistor with external biasing supplies. In this example, electrons will flow from the emitter, as the potential across base 1 and 2 is greater than that across the emitter and base 2.

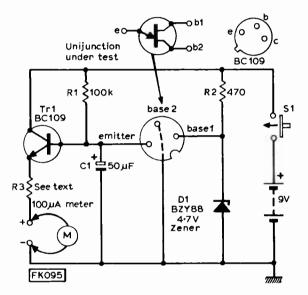
Practical Circuit

The device described in this article works as follows: C1 charges through R1 until the voltage at the emitter rises 0.7V above the ISR x 4.7. This figure being the voltage between the bases, kept constant by the zener D1. At this moment the device starts to conduct and the capacitor C1 is rapidly

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discharged. The cycle now repeats.

Tr1 performs two functions. First, it increases the resistance of the meter by a factor equal to its h_{fe} , and secondly, it removes by reason of its base/ emitter drop of 0.7V, the drop of the unijunction when it fires, giving true representation of the ISR.

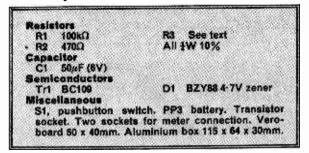


Circuit of the Unijunction tester, making use of an external meter. If the circuit is to be constructed with an integral meter, then one of about 100 µA FSD should be chosen.

Construction

Although details are given for the PCB, layout is not at all critical and comprises only six components. A high gain transistor should be used for Tr1 such as the BC109, as the input impedance should be as high as possible. For the same reason, the meter should have a movement of around 100μ A, or if

★ components list

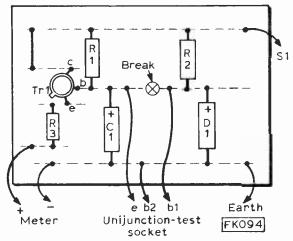


a suitable multimeter is available, then this could be used in place of a permanent meter. The value of R3 can be calculated as follows:

$$R3 = \frac{477}{\text{Sensitivity for fsd on meter}} - \text{Meter resistance}$$

A 5% resistor should be used here, as no advantage will be gained by the use of a more accurate one, especially as the diode itself is of 5% tolerance. The PCB was fixed inside a small aluminium box with sockets for the meter.





Component layout can be constructed on veroboard as shown above, or on a PCB. As components only number six, layout is not at all critical.

Use

Switch on and plug a unijunction transistor into the socket. The needle on the meter wlil move slowly across the scale, until at one point, the needle should flip back to near zero. If the meter is scaled 0 to 1 linearly, the ISR will be given by the maximum reading on the meter scale. If however, the voltage continues to rise, or does not rise at all, the unijunction is faulty.

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May-August 72

Send 30p + 7p (post and packing) to: Chief Cashier (PW Texan), IPC Magazines, Tower House, Southampton Street, London, WC2E 9QX **FM ,TUNER DIGITAL READOUT**—contd from page 556 achieved by resetting to zero on the twelfth input pulse. IC3a does this by feeding a positive pulse to the reset inputs when outputs QC and QD go high. The output from QD has a period of 300μ s which is the correct width for the sampling pulse.

IC6 is also an SN7493N and is used to generate timing pulses for the counting and display logic. It counts up to 16 and then resets to zero and outputs 15 and 16 are selected by the two NAND gates IC7a and b. The output at 15 (A in Fig. 5) loads the presettable counters with the IF offset, and the pulse at 16 gates the prescaler output into these counters. The output of IC3b is used to blank the displays. These pulses are shown in Fig. 6.

COUNTING AND DISPLAY LOGIC

The circuit is shown in Fig. 7. ICs 8 to 11 are the decade counters which are cascaded by feeding the QD output to next clock input. Also QA is connected to CK2 of each counter to cascade the two halves of each IC. The most significant digit (100MHz) can only be 0 or 1 so a decade counter is not needed.

The data inputs A-D are either connected to ground or +5V depending on the value of the IF offset. This is loaded into the counters when the count/load inputs are low. The counter outputs are in BCD form so decoder/driver ICs are used to drive the seven-segment LED displays (IC13, 14 and 15). These provide high current output to drive LEDs, and blanking can be achieved by putting a logic low on the RBO pins. The 330Ω resistors between the decoders and the displays determine the LED current, and R31 sets the current for the decimal point. For LED1 (+ or - indicator) a different circuit is used. The arrangement of IC12a, 12b and 2e illuminates the horizontal bar of LED1 when the output of IC8 is 0, 1, 2, 8 or 9. The vertical bar is also illuminated when the count is 8 or 9 due to IC12c. If the count is 3, 4, 5, 6 or 7 neither bar is on and the display is blanked. LED5 only displays 1 if QD of IC11 is low. If the count is 80 or 90MHz then QD is high and LED5 is blanked. The display blanking pulse B is also applied to IC12c and IC3d to blank LED1 and 5 during counting.

The capacitors C14-20 are to decouple the power supply. This is important because of the high edge speeds of the counting logic.

In Part 2 the power supply circuit is described and construction details and setting up procedure are given.

OUR "CQ" COLUMN

On page 603 of this issue, we have some CQ requests for back-numbers. **Please help us to help you**, if you want a "CQ" published, and you can do that by following the style on page 603 when you write to us. Please keep CQ's as short as possible.

CQ's should be sent to THE "CQ" COLUMN, Practical Wireless Editorial, Fleetway House, Farringdon Street, London, EC4A 4AD.



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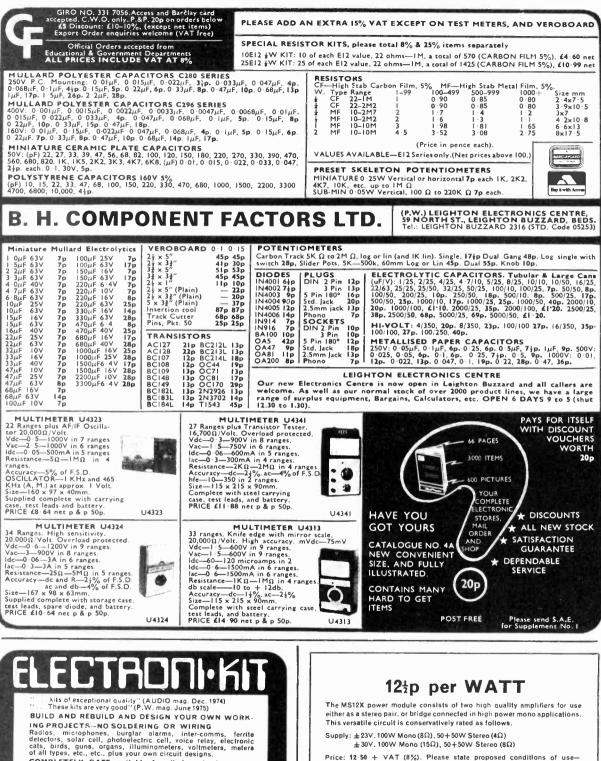
Now with free earniece and switched socket, 10 Transistors, Latest 4" 2 watt Ferrite Magnet Loudspeaker. 9 Tuneable Wavebands, MW1, NW2, LW, SW1, SW2, SW3, Trawier Band, VHF and Local Stations also Aircraft Band. Built in Ferrite Rod Aerial for MW/LW. Chrome plated 6 section Telescopic Aerial, can be angled and rotated for peak short wave and VHF listening. Push Pull using

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-IOTLINES

POWER

ON reading past Ginsberg articles it seems that the small, minute marvels have hogged the limelight, probably because they really are remarkable achievements. However, to redress the balance let us take a look at something a shade bigger. It concerns power, and the laser. The generation of power is a problem. Solar cells, wind-driven generators, mirrors which focus the sun's rays have all featured in the news.

Now it just so happens that if you take a very small amount of a material and compress it sufficiently it may just be possible to arrange pressures and densities high enough to support fusion—when lighter atoms get together to form heavy ones and when they do, they give off energy which might be harnessed.

Experts claim that a tiny pellet of deuterium and tritium can, with the aid of a quick pulse from a 1MJ (one mega-joule) laser, be compressed by a factor of up to 10,000.

Another approach finds workers constructing a kind of ring arrangement in which electron beams are individually concentrated on a single pellet of material in the centre. Certainly on the drawing board stage (at least) is such a beasty which treats said pellet to a burst of electron beams whose total combined power amounts to some $2\frac{1}{2}$ trillion Watts (that's $2 \cdot 5 \times 10^{12}$ Watts).

Just to complete the story, capacitors are used as a means of storing energy for the system. Two banks are employed and each consists of 38, 60kV, 1.85μ F capacitors. Oil dielectric transmission lines are employed and these are housed in a tank of transformer oil—40,000 gallons of it!

A final piece of news on the subject is that one particular machine under development produces a 10ns pulse of 40 trillion Watts.

27MHz

If you've ever tuned a radio receiver to around 27MHz you may well have picked up a weird cacophony of callsigns and titles not to mention some very strange conversations. Almost certainly you will have been listening in to conversations on the American "Citizens Band". Although power is (in theory) limited, no formal exams are required in order that one might transmit. Note; this is in America and does NOT apply in the UK.

While the Citizens Band has been a source of debate for some time, a new idea has surfaced and looks like being a 'winner'. The thought is that a particular frequency or channel within the Citizens Band should be an emergency channel. This allows anybody and everybody to have a Citizens Band hand-held transceiver (walkie talkie) in, say, their car. Any accident could be immediately reported and a request for assistance would be almost instantaneous. One voluntary network has already sprouted up in Ohio and others could follow.

It occurs to me that old people living alone could easily have immediate access to help from the outside world. Mountain climbers etc. could also find the system of use. It is almost certain that the scheme would not be permitted in the UK due mainly to the stringent Post Office/Home Office regulations concerning the radiation of energy, a point on which they are quite fussy to say the least. Quick, check the radiation from the local oscillator of your broadcast receiver. And what about those TV timebases?

Speaking of TV reminds me that the central research laboratory of Japanese giant Hitachi has been working on a video disc player using the optical approach. Some half hour recording of colour pictures and sound has been recorded on a 12in. disc. Luminance, chrominance and sound are contained in the 54,000 holograms on the disc each hologram being only one millimetre in diameter. So densely is the information stored that the disc needs to rotate at only 6 r.p.m. It is interesting to note that in systems employed by two other major manufacturers, the discs rotate at 1,800 r.p.m.

BLIMPS ARE COMING

Look out—the Blimps are coming. They may sound like a second class limp but in reality they are huge balloons which are floated up to a certain altitude (around 10,000ft.) and then tethered. The Blimps have with them a large antenna and transceiving equipment. The idea is that it's cheaper to have a balloon that it is to have a satellite in order to transmit and receive information over greater

ON RECENT DEVELOPMENTS

distances, particularly at the very high frequencies. No, it's not hot air, even the American military is increasing its interest in balloon borne radar. Makes you wonder about Amateur radio Hams' reaction. Perhaps Lisle Street will soon be selling Ex. Govt. barrage balloons. What better for portable stations—with a high wind it could get them off to a good start and raise them in the eyes of others!

RAZOR-SHARP TIME-KEEPING

News from abroad informs that there's a newcomer on the digital watch scene—Gillette, the company of razor fame. A research and development agreement has been signed between Gillette and some American electronics companies for carrying out investigations in the field of quartz modules for digital watches.

"MESFETS"

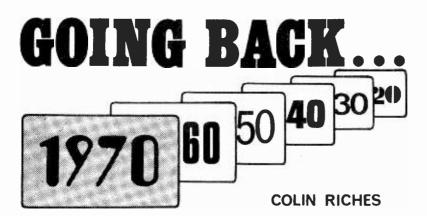
Another newcomer, this time to the semiconductor scene, is a device called the MESFET. Adding another S after the first would be a fair word for some early Ginsberg experiments with FETS! For the technically oriented, these devices are described as Schottky-barrier field-effect transistors. Efficiencies of 68% at 4GHz and over 40% at 8GHz have been claimed so clearly they're not just a pretty face. I hope to have more information shortly on these devices.

"SAWS"

When one talks about crystal oscillators it's usually about a bulk crystal—a chunk of crystal between two supports. Generally, the higher the frequency, the smaller (and often thinner) the piece of crystal is. There is a limit to how small and fragile one can make a crystal of this kind which is why fundamental frequencies are commonly no higher than 25MHz.

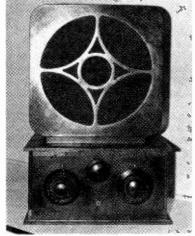
Marconi Research Laboratory has developed the SAW (surface acoustic wave) technology to a point where it can manufacture a compact and rugged crystal oscillator with a fundamental frequency of 1.2GHz.





Anyone help?

R. H. F. Mayman of 59 Delamere Street, Crewe, Cheshire has recently come across this interesting receiver, complete with speaker, and wonders if any other readers can help him with more information.



Apparently, the set was purchased in Crewe many years ago. It carries only a dealer's name and no details of a manufacturer. Valves are $2 \times PM2$ and $1 \times PM1LF$. The loudspeaker is simply marked "Blue Spot."

New books

ADAM Hilger Limited, publishers, 29 King Street, London, WC2E 8JH, have recently announced the first three volumes of a set of books entitled "The Story of Radio" by W. M. Dalton, Ch.Eng., M.I.E.R.E.

Volume 1 "How Radio Began" covers the basics from early experiments with electricity and magnetism. An interesting chapter on Wireless Telegraphy describes experiments and discoveries by such pioneers as Clark Maxwell, Hertz and Marconi. A chapter headed The Thermionic Valve contains items on the Edison Effect, Audion Tube, and early valve circuits.

Vol. 2, "Everyone an Amateur" begins the story after World War 1; and contains sections on the British Broadcasting Company and the Rediscovery of Short Waves.

It tells how during the early years of peace after the First World War, the seepage of official information and the knowledge of wartime developments brought home by ex-service men led to an enthusiasm for radio fostered almost entirely by amateurs. They built their own transmitting stations and receivers, compelled Governments to provide public broadcasting services, and eventually astounded the world by their unaided achievements in long distance low-power short-wave communication. This second volume of Mr. Dalton's comprehensive history pays tribute to these devoted pioneers and, in recounting the birth-pangs of the British Broadcasting Company, tells how Everyman carried on building his own receiver in a craze from which, Mr. Dalton has said, 'a few of us never quite recovered.'

Vol. 3, "The World Starts to Listen" takes the story a little further: by the mid-twenties, the early amateurs were ready to turn professional, the world was ready to buy their sets. The B.B.C. had become a Corporation —and respectable—and people had started to listen to its programmes in preference to twiddling dials in a search for distant stations; and so the quality of broadcast sound improved. Valves were already being applied in many other fields, but they were still battery operated. Mr. Dalton thus continues his step-by-step story of the development of radio.

These books are very interesting but also very expensive, for they are priced at $\pounds 4.50$ each volume. It's a pity because I feel that this is a text which has been needed for a long time now. Still, with inflation roaring ahead $\pounds 4.50$ will be the price of half a dozen resistors soon so . . .

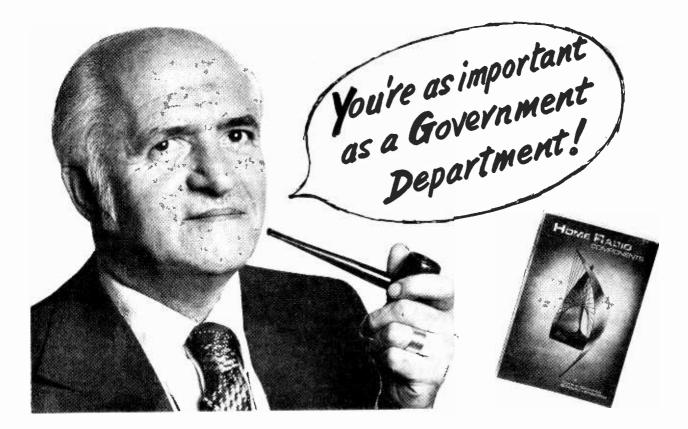
Cassette History

S OME while ago I gave mention to the double LP set that the BBC issued to mark 50 years of broadcasting. Well, now they've issued the complete recording on cassette. It's entitled "BBC 1922-1972, 50 Years' of Broadcasting", and comes as a double-play cassette No. HRMC 050.

The tracks are produced by Alan Burgess and narrated by



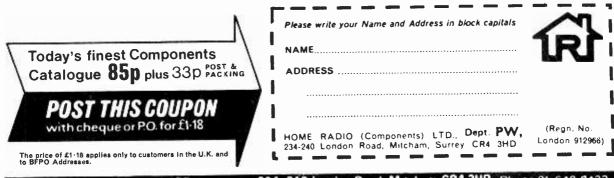
Rene Cutforth and endeavour to recapture in a hundred minutes many great occasions at home and abroad and people whose voices became known through the medium of 50 years of BBC Radio. Broadcasting pioneers such as Lord Reith and Peter Eckersley can be heard as well as the first Christmas broadcast by King George V and historic broadcasts by famous wartime announcers. The tape also reflects musical events over the years from Twenties syncopation to The Beatles. Please don't try to obtain it from the BBC because they don't have a sales department for records and cassettes, but contact your local record shop. They're sure to be able to get one for you.



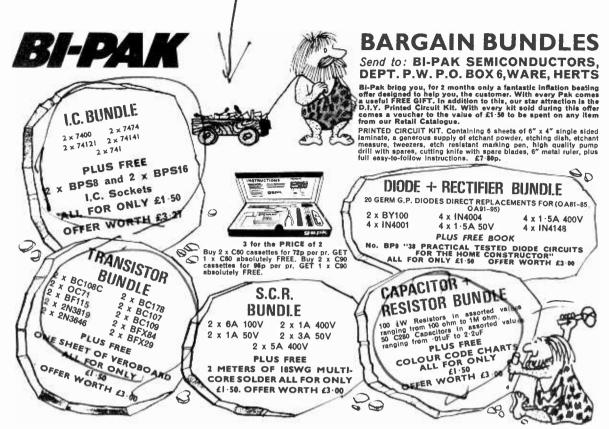
.... at least, to Home Radio Components you are. I'm thinking of their Credit Account Service. They have of course always run accounts for supplying firms, colleges and Government Departments, but for years it was impractical to provide the same facilities for individuals. However, Home Radio Components have always looked upon their smallest customers just as important as their biggest, and after much thought and planning they devised a Deposit Credit Account matched to the needs of the small individual buver.

The service is very convenient in many ways. For instance, thanks to their answerphone service exclusively for the use of Credit Account customers, you can take advantage of the cheap phone rates after 6pm week-nights and any time Saturday and Sunday. You not only save money, but you can often get your components much quicker. Briefly, the Credit Account Service works like this—you pay a deposit (you choose the amount) and you immediately get credit for *double* that amount. Home Radio then send you special order forms and pre-paid envelopes, and advise you each month how much you have spent. You save quite a bit on postage costs, and having to draw only one cheque or P.O. a month makes quite a worthwhile additional saving. No wonder nearly 1000 customers are already using this service. Why not join them and save yourself money and frustration? First you will need the Home Radio Components catalogue. No constructor should be without one! For a book having 240 pages, listing about 6000 components, illustrating nearly 2000, the price of 85p is modest indeed. True, postage and packing adds another 33p, but every catalogue contains vouchers to the value of 70p when used against orders.

Full details of the Deposit Credit Account and an application form are included in the Catalogue. To take your first step to simpler, quicker component buying send the coupon with your cheque or P.O. for £1.18 today.



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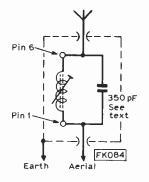
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ANTI-BREAKTHROUGH TRAP

A parallel tuned wavetrap can greatly reduce an interfering signal due to second channel or where intermediate frequency breakthrough is troublesome. The circuit uses a Denco Blue Range 3 coil and the trap is constructed in the maker's aluminium can provided. The 350pF capacitor is for 1.6MHz IF's, but the coil will tune 1500kHz to 6MHz with a trimmer capacitor of 500pF max. A Blue Range 2 is required for the MW band.



Adjustment of the core in the coil will also extend the range over which the trap will tune. For best rejection of an unwanted signal aim for minimum capacity and maximum inductance (core within the coil), provided the trap still shows a sharp point of rejection.

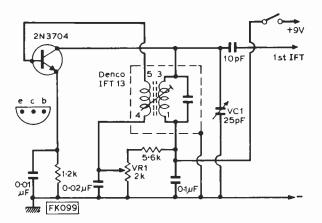
The trap must be connected as close as possible to the receivers aerial and earth terminals if it is to be effective.

'Q'---MULTIPLIER

A CIRCUIT having a high "Q" tunes more sharply, and is thus more selective, than one with a lower "Q". The "Q"-multiplier uses a regenerative stage to enhance the "Q" of a coil tuned to the receiver's intermediate frequency.

Potentiometer VR1 controls regeneration but the circuit should not be allowed to oscillate. Variable capacitor VC1 allows the multiplier frequency to be moved across the receiver's IF passband. In use a "Q"-multiplier is sometimes considered difficult to adjust which probably explains why it is not used more often, but, properly set up, it affords a very economic way of providing a substantial increase in IF selectivity.

The output coupling capacitor is connected to the primary of the first IFT of the receiver, to the "hot" end of the coil and not a tapping. The multiplier should be placed as near as possible to this IFT. The coil core is set so that it tunes to the receiver's IF, around 465kHz, with VC1 half way in. Realignment of the particular IFT may be needed on some sets. Potentiometer VR1 is set so that the multiplier is almost oscillating, equivalent to the point of maximum selectivity.



If a particular transistor does not oscillate smoothly reduce the battery voltage or include a resistor of between 100Ω and $1k\Omega$ in series with the switch. The unit can be built in a metal box external to the receiver but the output lead must then be coaxial cable, as short as possible, with the outer screen earthed. The output capacitor should now be placed at the IFT in the receiver.

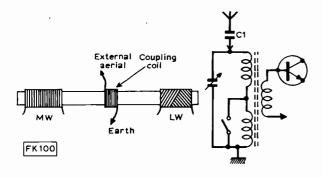
EXTERNAL AERIAL COUPLING

An external aerial will considerably increase the range of a portable type radio or allow it to be used in circumstances where the internal ferrite rod aerial is unsuitable, such as in a vehicle where the bodywork acts as a screen.

The external aerial is connected to a coupling coil added to the ferrite rod. The winding should be about 35 turns of 36SWG insulated copper wire but neither the number of turns nor the wire gauge are at all important. "Earth" in the circuit is the chassis of the receiver.

A short coaxial cable should be used to connect the external aerial to the receiver in a vehicle, to reduce electrical interference. But do not use screened cable as part of the aerial when the aerial is being added to increase range.

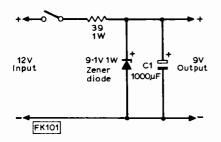
A capacitor C1 can be used as an alternative to



the coupling coil but its value must be kept low or it will detune the receiver's aerial circuit. A trimmer capacitor of a maximum value of about 15pF can be tried. If the receiver has an aerial circuit trimmer control this can be used to maintain correct tuning when an external aerial is connected via C1.

9V FROM 12V

T r a 9V battery-operated receiver is frequently used in a vehicle it is more economical to use the vehicle's 12V battery than to replace the dry batteries. With the zener diode the output voltage is substantially constant despite the changes in current drawn by the radio.

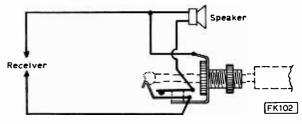


Capacitor C1 should be as large a value as possible with 1000μ F as a minimum. The 12V supply can be found at several places in a vehicle but choose one that gives a minimum of electrical noise in the receiver. If the parts are fitted in a box with dry battery terminals on the outside no changes need be made to the receiver which can be plugged in at any time. The terminals can be taken from the top of a defunct battery but be careful to observe the correct polarity.

HEADPHONE SOCKET

This simple modification involves fitting a suitable socket to a receiver to take a headset or earpiece. The circuit is arranged so that the speaker is cut out when the headset is plugged in to the socket. If the receiver's speaker is around 15 to 80Ω the usual low impedance headset will function without any trouble. If the output impedance is low, 3Ω or so, the load can be maintained by wiring a resistance or say $3 \cdot 3\Omega$ across the headset, It can be fitted inside the headset plug in some cases.

The socket should be suitable for the headphone plug, normally 2.5mm or 3.5mm or 1_4 in. in diameter,



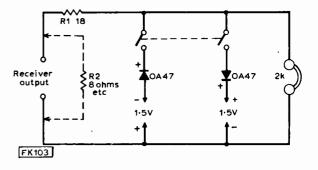
but there is no reason why different sizes should not be connected in parallel to accommodate different headsets or earpieces.

This modification must **NOT** be made to TV equipment, where the chassis is generally alive.

NOISE LIMITER

This small unit prevents sudden and uncomfortable bursts of noise or signal reaching the speaker or headset. It is particularly effective when the receiver is being operated at maximum gain on a weak signal. The diodes, which must be germanium types, shunt strong signals but leave weak signals unaffected.

Values shown are for output circuits of around 15 to 80Ω , but for higher values increase R1 to suit. If a lower impedance load must be maintained, wire a suitable value resistor, such as 3 or 8Ω , across the unit's input, shown dotted.



Headphones of $2k\Omega$ impedance or higher are best for this particular circuit when the limiting voltage is comparatively low. The single cells can be replaced with resistors of about 5.6 Ω with only a slight loss of limiting action. In this case no switches are needed. The components can be fitted into a small box with a lead and plug at one end and socket at the other. Alternatively the limiter can be wired round the receiver's output socket or terminals.

TOP CUT TONE CONTROL

THIS simple circuit may seem hardly worth a mention but in fact it is very effective at reducing the level of whistles caused by adjacent or second channel interference. It will also help to compensate for the deficiencies of small speakers notorious for their effectiveness at the top of the audio range!

The capacitor should be $0.1\mu F$ or $0.25\mu F$ with a

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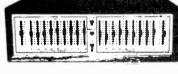
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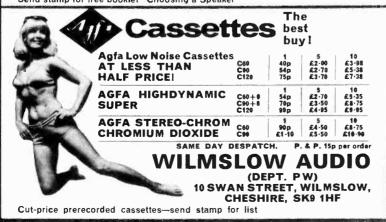
SPEAKERS Baker Group 253, 8 or 15 ohm Baker Group 353, 8 or 15 ohm Baker Group 537, 8 or 15 ohm Baker Baker Advers 12' dCone Baker Advers 12' dCone Celestion G12K 8 or 15 ohm Celestion G12K 8 or 15 ohm EMI 13 x 8'' type 350 8 or 15 ohm EMI 13 x 8'' type 350 8 or 15 ohm EMI 13 x 8'' type 350 8 or 15 ohm EMI 13 x 8'' type 350 8 or 15 ohm EMI 13 x 8'' type 350 8 or 15 ohm EMI 13 x 8'' type 350 8 or 15 ohm EMI 13 x 8'' type 350 8 or 15 ohm EMI 13 x 8'' type 350 8 or 15 ohm EMI 13 x 6'' cone tweeter Eagle CT10 tweeter 8 or 16 ohm Eagle HT15 hon tweeter Eagle CT10 tweeter 8 or 16 ohm Eagle HT16 hon tweeter Eagle FR6 Eagle FR6 Eagle FR6 Elac 0'' dCone 10RM239 8 ohm Elac 6'' GRM171 d/c roll surr. Elac 6'' GRM171 d/c roll surr. Elac 6'' GRM171 d/c roll surr. Fane Pop 55 dWatt 12'' Fane Pop 50 watt 15'' Fane 80T 8'' d/c roll surr. Fane 90 born Fane 90 born Fane 90 born Fane 90 born Fane 90 born Fane 90 born 12P db or 15 ohm Goodmans 12P db or 15 ohm		Goodmana 12P-G8 or 15 ohm Goodmana Audiomax 12AX 100 watt Goodmana Audiomax 12AX 100 watt Goodmana 15P 8 or 15 ohm Goodmana 15P 8 or 15 ohm Goodmana Hidax 750 Goodmana Axilom 100 12" Goodmana Audiom 100 12" Goodmana Twinaxiom 10 Kef 121 Kef 115 Kef 810 Kef 8200 Kef DN8 Kef DN12 Kef DN12 Kef DN12 Kef DN12 Kef DN12 Kef DN12 Kef DN13 Kef	£15-95
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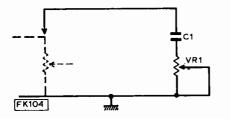
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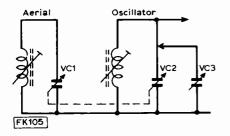
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 $5k\Omega$ potentiometer for VR1 in the case of transistorised receivers, and 0.02μ F to 0.05μ F with $25k\Omega$ to $50k\Omega$ for VR1 for high impedance circuits, such as are found in valved receivers. The connection is made to the top of the audio gain control but a tone control of this type must not be used in that part of a receiver in which negative feedback is already incorporated.

BANDSPREADING

B ANDSPREADING is very effective at alleviating the critical tuning that is often experienced on the short wave bands. In a simple superhet receiver the aerial and oscillator circuits are tuned by a twogang variable capacitor VC1/VC2. Simple band-spreading consists of adding a small value variable capacitor VC3 in parallel with the oscillator section VC2. VC3 is typically 5pF, mounted at a convenient point on the front panel and fitted with a slow-motion drive.



A capacitor similar to VC3, and ganged with it, can be connected in parallel with VC1 to maintain alignment of the aerial circuit but problems of tracking arise, especially if the receiver is bandswitched, so VC3 alone is advised.

The degree of bandspreading achieved by VC3 will depend on the frequency involved and the ratio of VC3 to the value of VC2 at any point on the dial. At low frequencies VC3 can be increased to 15 or 25pF.

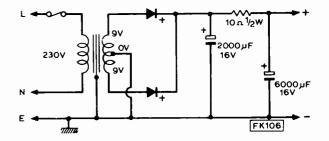
9V DC MAINS UNIT

This circuit will provide 9V DC to replace the batteries in transistor radios and similar equipment. A transformer with a secondary of 9-0-9V at 100mA should be sufficient for most purposes. The silicon diodes should have a minimum PIV rating of 50V. Those in the 1N4000 range are suitable.

Output voltage will depend to some extent on the current drawn by the external load but small

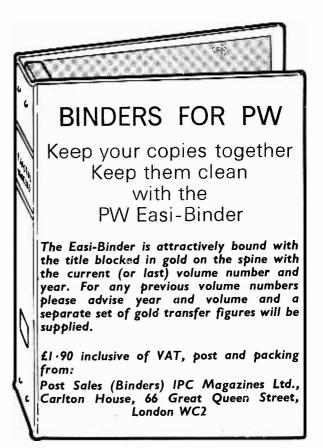
Practical Wireless, November 1975

variations are not usually of much importance with the average receiver. A zener diode could be added to stabilise the output voltage at a particular value.



The core of the transformer should be earthed, as well as the secondary centre tap, and a fuse in the mains supply is highly desirable. If the mains hum level is objectionable, in spite of the large value of smoothing capacitors used in this circuit, try fitting two capacitors, in parallel across the mains input, between fuse and transformer primary. The junction of these diodes should then be taken down to earth. The capacitors should be about 0.1μ F each rated at NOT LESS than 750V working. Ensure the unit is disconnected from the mains before trying out this modification.

If an output of opposite polarity is required then reverse the diodes and the electrolytic capacitors.



BUDGET STEREO SYSTEM BARNARD

READERS who have followed me so far will remember that we have replaced the ceramic pickup with a magnetic one (at the same time, of course, taking out any tone compensating components such as resistors in series or parallel with the pickup), constructed and fitted a preamplifier with its own power pack and have dealt with the problem of mains hum induced into the windings of the magnetic cartridge.

The result is very greatly improved reproduction of gramophone records over the treble range but distressingly "boomy" bass. This poor quality in the bass region is almost sure to be due to shortcomings in the design and construction of the loudspeakers but, before starting on this problem, it is probable that some tidying up is necessary on the work already done.

The first point is in the form of a warning; some makes of integrated circuit used in the preamp are very noisy in operation and for this reason I do not advise buying unknown makes over the counter on the assurance that they are "just as good"—they may be, but it is expensive to find out that they are not. Buy any of the well-known makes and be safe!

'TIZZY' SOUND

After playing several records on my own budget stereo after modification, I became aware of a "tizzy" sound whenever I touched the pickup arm, and, at the same time, I noticed an alarming increase in the pops and bangs whenever our refrigerator or central heating cut in or out. Since this followed the work I had done, it seemed very sensible to examine very closely the earthing arrangements on the input side of the new preamplifiers. In the original arrangement with the ceramic cartridge, the braided earth sleeve of the cartridge leads terminated on a tagboard on the underside of the Garrard deck and from this point another screened lead took over and fed the signal to the first stage of the main amplifier. This is the usual arrangement and is normally perfectly satisfactory. However when the additional amplifier is added with its high gain it may not be, and it certainly was not in the case of my own set-up!

I found it necessary to connect the braid at the tagboard direct to the record deck, which is itself connected direct to chassis by a separate lead from the motor terminal board. This, of course, gives a perfect "hum loop" situation but in this case it did not produce any hum. So that is how I have left it but I feel fairly sure that this will not be the solution in all cases and it may be found necessary to carry out a good deal of patient work on the earthing arrangements before a satisfactory solution is found. However, in my case the live condition of the pickup arm was completely overcome and the pops and bangs reduced to minor proportions

I had to do a lot more work to remove this annoying impulse interference altogether. This applies to a great deal of audio equipment and has been covered in many articles and books. I will not repeat it in this article but content myself by saying that you will probably use quite a few 0.01μ F capacitors before you eliminate it completely!

IMPROVING THE LOUDSPEAKERS

The obvious and major criticism of the sound quality from the system so far is loud resonant onenote bass. Any hi-fi expert will tell you that anything on the price of a loudspeaker over £30 has been spent on improving the sound below 50Hz. As our purpose is to spend as little money as possible, it is quite obvious some compromise is essential.

When you remove the back from the budget loudspeaker, do not expect to find much sophistication, it is likely to be basic though fundamentally good value. In my own case, the speaker cabinets were approximately $18 \times 13^{1}_{2} \times 7^{1}_{4}$ in. deep. This is rather larger than the average and gives a cubic capacity of about 1760in.³, very suitable for an 8in. speaker when the cabinet is totally enclosed. Inside were two units, an 8in. general-purpose speaker and a cone tweeter. Neither unit was very robustly constructed. The tweeter was fed by a 4μ F electrolytic capacitor, there being no crossover unit apart from this.

The inside of the cabinet was bare wood but the cabinet back was lined with a thick covering of foam plastic. The only surprise was a 2in. diameter hole in the front (in addition of course to those for the speakers) through which I assume the bass from inside the cabinet joined that from outside, hopefully in phase, thereby increasing the acoustic efficiency considerably in the lower region. With this arrangement it is not surprising that the modest rated 6W of audio was enough for the noisiest of teenage parties!

AIR TIGHT

The enclosures were constructed from chipboard and close examination of the edges at the back showed a lot of gaps which suggested to me that the quality of board left a good deal to be desired from a hi-fi point of view. Nevertheless, the general construction was solid enough and the backs fitted



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2N6 2N6 2N7 2N7 2N7 2N9 2N9 2N1 2N1 2N1 2N1 2N1 2N1 2N1 2N1	97 98 99 06 08 16 18 302 304 306 308 711 2102	16p 82p 59p 14p 17p 28p 32p 18 ¹ p 26p 31p 47p 45p 60p	2N4037 2N4036 2N4058 2N4052 2N4289 2N4920 £ 2N4923 £ 2N5245 2N5294 2N5296 2N5457 2N5458	42p 67p 18p 15p 34p 1 10 83p 1 00 47p 48p 48p 48p 48p	AF280	90p 70p 79p	BF115 BF154 BF159 BF180 BF181 BF184 BF194 BF195 BF196 BF197 BF198	87p 36p 20p 27p 35p 36p 12p 12p 13p 15p	OC28 OC35 OC42 OC45 TIP29A TIP29C TIP31A TIP32A TIP33A 4 TIP34A 1	76 ± p 60 p 32 p 32 p 58 p 62 p 74 p 1 01 1 51 2 90 13 70 10 90 98 p
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Other subjects

tightly and securely. The result of all this examination immediately explained the loud and poor quality bass since the cones of the two 8in. speakers had no mechanical damping at all and, once set in motion by a low frequency signal, were free to carry on moving at their resonant frequency for an appreciable time after the signal had stopped.

The only and rather obvious answer to the problem was to set about making the cabinets *enclosures* in the proper meaning of the word, that is to say, make them as air-tight as possible so that the cone movements would be restricted by air pressure. This is, of course, the principle of the "infinite baffle" and most of the smaller good quality speakers are designed on this principle. The first job therefore was to block the unused hole in the cabinet front with a piece of good quality chipboard or 5-ply which was glued and screwed into position.

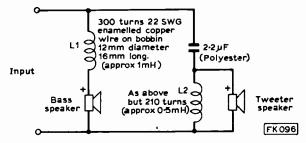


Fig. 1 : Circuit details of the cross-over unit. Care should be taken in the winding of the coils, to ensure that the units for both channels are exactly the same.

CROSSOVER UNITS

The first major item of expenditure is a pair of crossover units which I believe are essential. The actual crossover frequency in this application is not critical and anything in the region of 3kHz will be suitable. Shopping around will most likely find a pair for less than £5 but for those who prefer to make their own, and do not mind tedious coil winding, Fig. 1 gives constructional and wiring details. Care must be exercised in connecting these to ensure that both follow the same wiring pattern so that problems do not arise later in getting both loudspeaker systems to operate in phase. Most speaker units have one tag marked with a red dot and if this is connected through the crossover unit to the live speaker lead in both cases, all will be well.

The next job was to line the interior of both cabinets with some soft sound-absorbing material. A good look around the household will usually reveal something suitable which will avoid dipping into the pocketbook. I found some surplus carpet underfelt of the rubberised variety and this is very suitable. Avoid very thick and heavy materials for, although they absorb sound, they also tend to reduce the effective cabinet volume which is undesirable. The material is fixed in place with small tacks and a little glue in strategic places. The photograph shows the interior of one cabinet after this treatment with the crossover unit in position. This photo also shows two other items not yet dealt with. Fixed to the back is a 50Ω wirewound potentiometer and the cone tweeter has been replaced by a superior dome type.

After completing the work and testing for several weeks, although the results were very pleasing, I

decided to extend the frequency response in an upward direction and to improve sound dispersion and thus the stereo effect. To do this I bought a pair of good quality dome tweeters (about £6 each). This certainly had the desired effect but I found that the new tweeters were very efficient and, since all the work I had done had tended to reduce the efficiency of the 8in. speakers, the overall effect was out of balance and the tweeters tended to predominate. For this reason, the 50Ω 3W potentiometers are fitted and they are, in effect, volume controls for the tweeters enabling the required balance to be obtained while playing programme material, Fig. 2.

VACANT SPACES

The last job in improving the speakers is to fill in the vacant spaces around the speaker units with more sound-absorbing material. For this, underfelt and similar material is not suitable as it is much too dense. The recommended material is BAF wadding which can be bought from most hi-fi shops for about 80p per sq. yd. I experimented with ordinary domestic cotton wool and found it very effective in this application, readily available in rolls about 12in. wide. It should be very carefully unrolled without teasing it out and then cut to suitable lengths. For my cabinets I inserted two pieces, 18in. long very loosely rolled, each side of the 8in. units. A shorter piece similarly rolled fills the spaces above the big speakers and behind the tweeters. The object is to replace some of the air in the enclosure with the wool but not to introduce a solid substance which would effectively reduce the enclosure capacity. For larger or smaller cabinets the actual quantity of BAF wadding or wool must be found by trial and error, too much will have the effect of killing the bass response but the correct amount removes all traces of any unpleasant "boxy" tone.

We are now at the stage where we can replace the backs on to the enclosures and our aim is to make them airtight so as to put a brake on those bouncing cones, so the backs must fit well and be screwed down tight. Pay particular attention to the holes through which the leads are taken as it may be necessary to fill these with putty or some similar substance in order to avoid large air leaks.

By the way, when I say "airtight" I do not mean this too literally! There has to be some escape of pressure or the cones would never be able to move at all. So some leakage is essential and this is almost certain to take place through the gap between the speech coil and polepiece and it is also doubtful if the cone suspension is completely airtight in units of this quality. So in making the enclosure and its

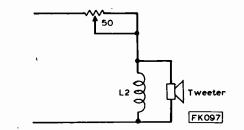
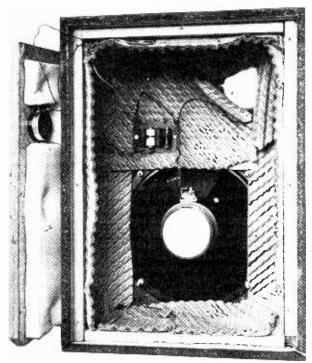


Fig. 2: 50Ω3W potentiometer shown in-circuit, to provide some control over the tweeters.



Interior view of the speaker enclosure, showing the rubberised carpet underlay fixed in position. The vacant space should now be filled with BAF wadding.

back as airtight as possible you are very unlikely to overdo it.

The two enclosures (we are fully entitled to call them that) can now be tested out on a signal. It will be obvious that the efficiency has been reduced in the middle and bass areas so the volume control will be further advanced than before this work was done. But the quality of sound should be immensely improved. The bass in particular will be "tight" and musical and it should be possible to advance the bass boost much further than before whilst still maintaining good tonal balance and really pleasant quality.

I believe the foregoing lines of attack will apply with great benefit to almost all budget loudspeakers. It is necessary before starting any work to assess very carefully the shortcomings of the speakers as supplied and to decide what improvements are required and then to examine the interior of the cabinets and the unit or units to decide what work is likely to be most beneficial. This will always reveal problems in the bass area no matter what else and the first answer to this is always cone damping. This inspection must also cover close examination of the cabinets themselves; if the construction seems weak and they sound hollow when tapped with a metal object, it may be necessary to fit wood struts in strategic places to make sure they will not rattle or resonate of their own accord.

SFITTING A TUNING METER

Few budget stereos run to a tuning meter, but they nearly all have an AFC circuit which is intended automatically to adjust for any minor tuning errors and to correct any tendency to drift in the RF oscillator. A reliable tuning indicator which shows when the tuning point of minimum distortion and minimum background noise is found is almost essential to anyone who takes his music seriously.

The circuit arrangements for a meter which peaks at the exact tuning point are very simple. A moving coil meter with FSD of about 100μ A connected with about 30 to $40k\Omega$ in series is connected across the large electrolytic in the discriminator circuit. These meters are expensive to buy especially if you want to pick one that fits nicely with the styling of your system. I had a very elegant meter which exactly suited the styling of my unit audio but it required ImA for FSD. We cannot use such a meter across the discriminator as it has an internal resistance of only 50 Ω or so. The answer is to arrange the meter to be in circuit only when tuning and to remove it while we are listening.

One way is to fit a small press-button switch which brings the meter into circuit when made but disconnects it when open. This button is pressed when changing stations, the tuning adjusted until the meter peaks and the button then released, restoring the circuit to normal.

SPACE CONTACTS

Examination of the AFC switch revealed a pair of unused contacts. The usual arrangement is a simple make-and-break single pole switch which joins the AFC line to chassis when it is disabled but since manufacturers of budget stereo seldom design special switches for such a simple function it is very likely that you will find at least one pair of unused contacts which can be used to switch the meter in and out. The position then is that we disable the AFC when we want to tune and then tune for peak reading on the meter. After this we return to the AFC position, leaving the AFC diode to take care of any oscillator drift, the meter remaining out of circuit until we want to change stations.



The photograph above shows the meter fitted on my budget stereo alongside the AFC switch which controls it. It works extremely well and I get dead accurate tuning every time. I had to experiment with various values of resistance in series with the meter and finally fixed on $6.8k\Omega$ which gives between half and three-quarter scale reading on an 800μ V signal at my aerial. By a slight circuit modificontinued on page 604

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THE transmitted sound quality of television is inherently very high, but due to severe limitations in the audio side of domestic TV receivers, it is rarely heard at its best. This article describes a high performance TV Sound Tuner for feeding into a hi-fi system or tape recorder, enabling full benefit to be gained from the broadcast.

Up-to-date techniques have been used to provide push button varicap tuning and high sensitivity. Three integrated circuits are used and a ceramic filter with quadrature detector ensures easy setting up without instruments.

TV SYSTEM

Television in Britain is transmitted on 625 lines with a line rate of 15.625kHz and 50Hz field rate. The video is transmitted as amplitude modulation of an RF carrier, while the sound channel is broadcast as frequency modulation of a sound carrier spaced 6MHz from the vision carrier. Fig. 1 shows a block diagram of the sound section of a TV receiver.

In all frequency changing operations in the receiver the sound carrier remains spaced 6MHz from the video. After final video detection the result at the output of the video detector is video and a 6MHz FM sound carrier, the vision carrier having been transferred to zero frequency. The audio is simply recovered from the FM carrier by frequency discrimination, using a conventional discriminator or the more recent "quadrature" detector.

CIRCUIT DESCRIPTION

The pre-assembled and aligned IF sub-assembly used in this project performs the function of IF amplifier, vision detector, 6MHz limiter amplifier and 6MHz quadrature discriminator.

The IF amplification and associated bandwidth shaping is performed in two Philips G8 colour receiver modules employing four transistors. The vision detector is included in the second module, giving video and 6MHz sound carrier at its output.



A 6MHz ceramic filter is used as a simple bandpass filter to remove the video and shape the characteristics of the following 6MHz amplifier.

Amplification at 6MHz is carried out in the TAA570 (or similar) IC, which also performs quadrature FM demodulation using only a single tuned circuit.

Fig. 2 shows the circuit diagram of the PW Sound Tuner.

The volume control is connected directly to the subassembly audio output and feeds Tr2, which is a simple emitter follower, to ensure that the TV Sound Tuner has a low output impedance. This enables long lengths of screened cable to be used on the output without any significant loss of treble.

The varicap tuner used in the prototype is the Mullard ELC1043, commonly used in contemporary

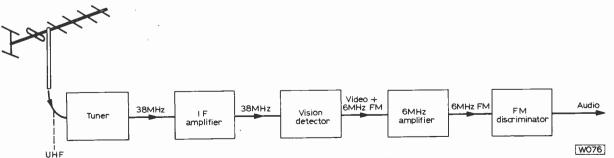
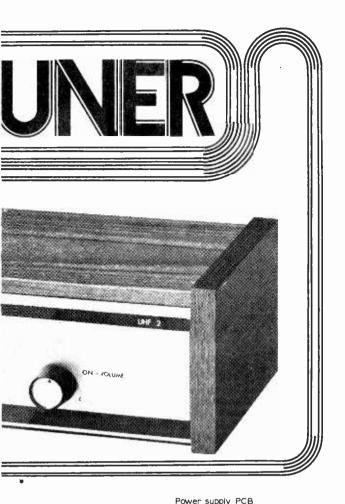


Fig. 1 : Block diagram of the sound section of a TV receiver.



receivers and available at reasonable prices through surplus channels.

The ELC1043 has facilities for AGC but as it is not required in this unit, a potential divider, consisting of R10 and R9 connected across the supply, is used to bias the AGC terminal for optimum gain. Power for the RF stages and oscillator is taken directly from the 12V supply to the sub-assembly.

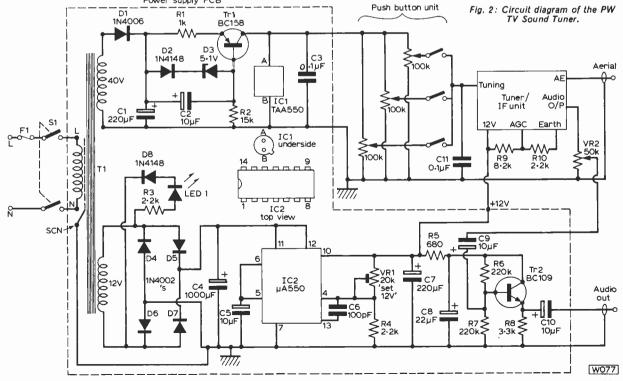
To tune the ELC1043, a DC voltage variable between 0.3V and 30V is applied to the "tuning" terminal. This covers channels 21 to 68 for UHF reception. To achieve the necessary tuning resolution, multi-turn pots have to be used, in this case being neatly combined with the channel selection buttons in a commercial varicap push button control unit. These are available to give three, four, five or six preset channels and consist of the requisite number of preset pots connected across a stable 30V supply, with each wiper being selected by a push button and connected to the "tuning" terminal on the ELC1043. A small capacitor (C11) is used to remove any noise introduced by the tuning pots.

The IF output of the tuner feeds directly through a 1000pF capacitor into the first G8 module on the sub-assembly.

POWER SUPPLY

The mains transformer used in this project has two secondaries, one of 40V to feed the varicap diodes, and one of 12V for the IF sub-assembly, tuner and output emitter follower. The complete circuit of the power supply is shown in Fig. 2.

The 12V supply (actually adjusted to 11.5V) is obtained by full wave rectifying 12V AC from the transformer in a bridge made from D4 to D7, and smoothing with C4. Voltage regulation is necessary to prevent oscillator drift in the front end and is performed by IC2, a μ A550 regulator package.



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This device works by comparing a reference of 1.63V produced at pin 6 with a fraction of the output voltage on pin 10, determined by R4 and VR1. Pin 4, connected to the junction of R4/VR1, is the inverting input to the comparison amplifier and pin 5 is the non-inverting input (connected directly to the reference).

The regulator acts to maintain the voltage on pins 4 and 5 equal, ensuring that the output is constant. VR1 is variable so that the required 11.5V output may be precisely set.

Capacitor C5 is included to smooth the reference while C6 is high frequency compensation, necessary for stability.

30V SUPPLY

A very high degree of stabilisation is required for the 30V supply as a few tens of millivolts change would cause appreciable detuning. Conventionally, a TAA550 IC regulator is used to stabilise the varicap diode supply in receivers. This is a two terminal device which is connected as a Zener diode, but which has very good temperature stability.

Continuing the analogy with a Zener diode, the dynamic resistance is quite low at around 10Ω but to make this resistance totally negligible compared to the source resistance a constant current source has been adopted in this design to ensure excellent tuning stability even with large mains voltage changes.

Transistor Tr1 in conjunction with Zener D3 and R1 forms a 5mA constant current source, with temperature compensation of Tr1 V_{be} provided by D2 (D3 with a Zener voltage of $5 \cdot 1V$ would have a virtually zero temperature coefficient).

The varicap control unit is connected directly across the TAA550 and drains little current as each tuning pot is 100 Ω . However, should a five or six button unit be used, R1 should be reduced to 820 Ω to maintain an optimum 5mA in IC1.

On-Off indication of the tuner is provided by LED1 mounted on the front panel. R3 serves as a current limiting resistor while D8 is included as reverse voltage protection.

CONSTRUCTION

The IF sub-assembly is purchased fully assembled and aligned so there is no work to do in this area. Both the ELC1043 and a three button unit will mount directly on one end of the PCB which has all the necessary printed wiring on the foil side. The push button unit is supported by two 38mm 6BA bolts passing through the board and held captive between two units on each bolt. By adjusting these units, the buttons can be made to coincide with the cut-outs in the front panel.

A four station control unit can be accommodated on the PCB but an additional hole would have to be drilled. Larger units would have to be mounted directly on the chassis and the dimensions adjusted accordingly.

The connections for the push button units are shown in Fig. 3.

Before soldering the ELC1043 to the board, R10, R9 and C11, which mount under the tuner, must be soldered in place. R10 is on the copper side of the board and, to ensure that it does not short to the chassis, should be completely covered by a 25mm length of 5mm plastic sleeving.

POWER SUPPLY BOARD

Both the 12V and 30V supplies and the output emitter follower are constructed on a single PCB, the layout of which is shown in Fig. 4.

Constructors who prefer to make their own boards should have no difficulty, the only point to watch being the spacing of the pads for IC2 (0·lin apart, rows spaced 0.3in). As an alternative, fully prepared boards will be made available—details in the component list.

Five mounting holes are drilled in the board, one at each corner and one adjacent to the transformer to prevent the board sagging.

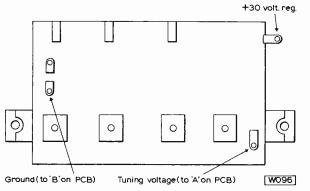
The transformer has two 6BA mounting lugs and when soldered in position, two corresponding holes should be drilled in the PCB and the transformer secured with a couple of short bolts.

Assembly of the board is quite straightforward, with particular care being taken with the orientation of electrolytics, diodes, ICs and transistors.

METALWORK

The complete TV Sound Tuner is mounted in a "U' shaped aluminium chassis with holes for the mains lead, panel mounting mains fuse, output lead and aerial socket on the back panel. The front of the chassis is masked by a front panel, secured with the pot nut on the volume control.

Fig. 5 shows the metalwork for the chassis and front panel. To absorb any tolerances the PCB should be marked from the actual boards held in situ.



Push button mounting holes

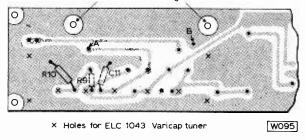
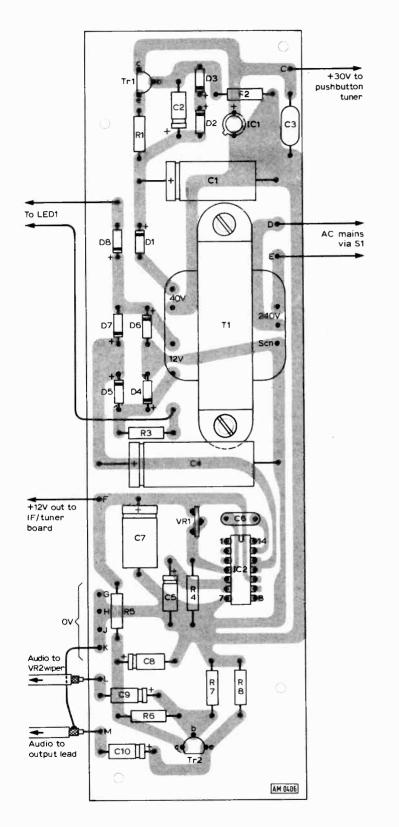


Fig. 3: Connections for the pushbutton tuner unit (left) and details of the mounting of the Mullard ELC1043 tuner on the PCB (above).



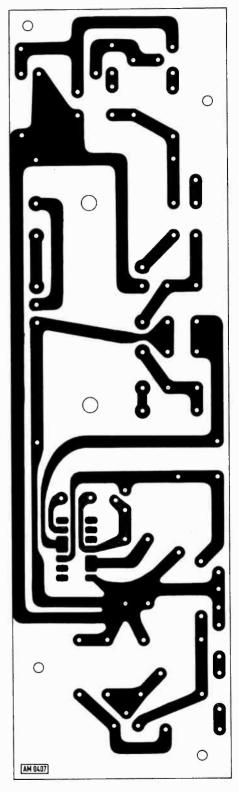


Fig. 4: Layout of the components on the power supply printed circuit board (left) and full size printed circuit master (right). Practical Wireless, November 1975

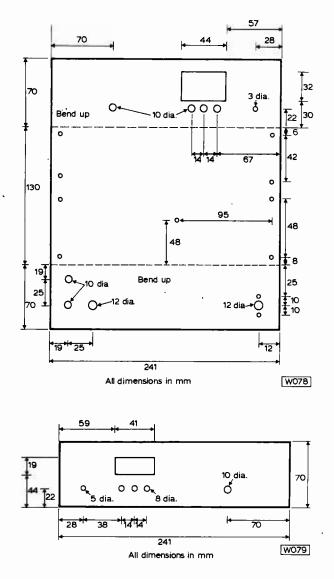


Fig. 5: Drilling details for the chassis (top) and point panel (bottom). Materials can be 18 s.w.g. aluminium.

The two PCB's are supported by 6mm stand-off collars on 6BA bolts. These collars make contact between the earth plane of the IF panel and the chassis, so the screws must be tight, with shakeproof washers used between the collars and the PCB.

VOLUME CONTROL MOUNTING

The ganged volume on-off control is mounted in the hole provided on the front panel which coincides with a clear area of the IF board. Providing that the control is physically small it will fit in without any trouble.

Mains wiring to the control will pass directly over the 6MHz ceramic filter which is very susceptible to RF pickup. To reduce the possibility of interference, a small tinplate shield is soldered to the mounting clip of the second G8 module, to cover the filter and associated components. The photograph shows the details.

	* * #
Resistors (All ±W)	
R1 1kΩ (820Ω if 5 or 6 b R2 15kΩ	utton unit is used)
R3 2·2kΩ	
R4 2.2ki)	
R5 680()	
R6 220k0	
R7 220kl3 R8 3-3kl2	
R9 8·2kΩ	
R10 2.2kΩ	일이는 것으로 한 그는 것 같아요. 것 같아.
VR1 20kD skeleton prese	t ** «*
VR250k1 log pot with d.	p.d.t. switch (S1)
Capacitors	
C1 220µF 63V elect	C7 220µF 16V elect
C2 10µF 25V elect	C8 22µF 25V elect
C3 0 1 F polyester	C9 10µF 10V elect
C4 1000µF 16V elect C5 10µF 25V elect	C10 10µF 10V elect C11 0 1µF polyester
C6 100pF ceramic	Cir o me polyester
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Semiconductors Tr1 BC158	
Tr2 BC109	
D1 1N4006	
D2 1N4148 D3 5 1V 400mW Zener	
D3 5-1V 400mW Zener	
D4-D7 1N4002 (4 off) D8 1N 4148	
IC1 TAA550	
1C2 #A550 (NE550A)	
LED1 TIL209	
Miscellaneous	
T1 Type M1103	
IF Sub-Assembly	
Pushbutton control unit	uner (or ELC1042 for VHF) *
S1 Double pole mains s	
F1 500mA fuse and pan	el mounting holder
Sk1 Coaxial aerial sockel	
PSU, chassis, cabinet, fr	ead, mains lead, PCB for ont panel, knob.
	lable from Monty Enter-
prises, 2 Silver St., Donc	aster, price £3.95 - VAT.
A wooden box is availa	ble from Birch & Ridley.
Watson Road, Worksop	, price £2.25 + VAT + g. The metal chassis and
front panel can be obta	ined from Richard Friday
Ltd., Old Coach House,	ined from Richard Friday Greystone Yd., Moorgate,
Hotherham, Yorks, price	£5.65 + VAT - 35p
postage and packing.	LC1043 tuner, and push-
button unit are all availa	ble from Manor Supplies,
172 West End Lane, Lon	don NW6, price £6.80
45p, £4.20 - 30p and £1	20 + 25p respectively. If
all three are purchased p	& p is 50p.
N	~

WIRING

To avoid earth loops and the attendent difficulties it is important that the only ground connection between the PCB's is that made as part of the power supply wiring. Screened leads should be used for the signal wiring from the IF board to the volume control and from the volume control to the PSU board (input to emitter follower) but the screen of the lead should be cut short and not connected to the PSU panel.

ľ

Quadrature Coil

AM 0405

Fig. 6: Position of the quadrature coil which may need adjusting. A photograph of the completed unit is shown right. Note the small metal shield between the volume control and the board.

The screened output lead (with a plug to suit the hi-fi system on the other end) has its braiding connected to the ground terminal of the PSU board to maintain earth continuity with the rest of the equipment.

To keep the mains wiring away from the emitter follower, the switch leads pass between the two panels and under the PSU board near the mains transformer.

By using a transformer isolated supply, no 'live chassis' hazards exist and the aerial connection can be made directly to the aerial terminal on the end of the ELC1043. On most units an earth braiding connection has to be made by soldering directly to the tuner case adjacent to the 'aerial' connector.

FRONT PANEL

The front panel for the prototype was sprayed with car 'touch up' paint and lettering and lines applied using Letraset. A final spray of clear polyurethane protects the lettering from fingermarks and abrasions.

The window for the tuning indicators on the control unit was made from a piece of 6mm clear Perspex carefully filed to size and affixed with a couple of dabs of epoxy cement. A waterproof felt tip pen was then used to mark the window area for each button.

Assembly of a wooden case depends on the facilities available and the skill of the constructor. As a guide, the case for prototype is a simple 'hood' made from veneered plywood. The front panel, of course, covers any screws that may be used to hold the chassis in the cabinet.

SETTING UP

After a thorough check of all wiring, component values, etc., VR1 is set to minimum resistance and power applied. By increasing VR1 it should be possible to set the supply rail to exactly $11 \cdot 5V$.

No adjustment is possible on the tuning diode supply but it is as well to check that the voltage is of the right order. Plugging the output lead into an amplifier and turning up the volume should give a high level of hiss, with possibly a couple of foreign radio stations as well. Plugging in an aerial and adjusting the tuning controls should give the local region TV stations loud and clear.

Channel numbers are not marked on the push button units but the pointer at the bottom indicates channels at the low end of the UHF band. The three regional stations are always grouped together with BBC1 being the lowest channel number, ITV next, then BBC2.

Tuning will be a little difficult at first without the picture to help. For each station, several tuning points will be apparent, close to each other. The correct one will be towards the higher channel number end of the group, just before a region of 'vision buzz'.

When tuning has been mastered any remaining buzz can be carefully taken out by tuning the quadrature coil (see Fig. 6) with the CORRECT TRIMMING TOOL. No more than one turn adjustment should be needed as it is merely to compensate for the capacitance of the metal chassis, etc. No other tuned circuits (i.e. those in the front end or G8 units) should be touched as specialist gear is needed to set them up again.

The Sound Tuner is very sensitive and, while it would be silly to expect good results from the proverbial "piece of wire", a weak signal (such as would produce a quite noisy black and white picture and very poor colour) would be sufficient. This means that a splitter in the main receiver TV co-ax will furnish plenty of signal or alternatively a second small aerial could be installed.

The Sinclair DM2 Multimeter. Comprehensive. Accurate. Portable. And really rugged. Yet only £59.(PLUS VAT)



State-of-the-art circuit design, incorporating high-quality components, has resulted in a professional, $3\frac{1}{2}$ digit instrument of outstanding performance and reliability at a realistic price.

A custom-designed MOS LSI digital processing IC controls the auto-polarity dual-slope-integration A to D converter. The circuit built around this IC uses a MOSFET op-amp input buffer with 0.1% metal-film resistors. The result is excellent accuracy and stability with a very high basic input impedance.

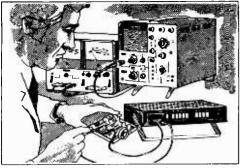
The instrument reads to \pm 1999 and has a basic accuracy on the 1 V DC range of 0.3% \pm 1 digit. Four 8 mm LED displays provide excellent legibility and angle of view. Battery operation allows complete independence of mains supply.

The Sinclair DM2 has all the capability you need. Just take a look at its features and compare them with higher-priced multimeters. You'll find the DM2 is their equal in virtually everything – except price !

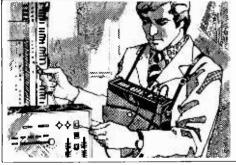
Features of the Sinclair DM2

5 functions giving 22 ranges DC volts – 1 mV to 1000 V AC volts – 1 mV to 500 V DC current – 0.1 μ A to 1 A AC current - 1 µA to 1 A Resistance – 1 Ω to 20 M Ω Easy to use Automatic polarity, push-button selection for all ranges and modes from a single input terminal pair. Easy to read Big, bright 8 mm LED display gives a quick, clear reading. 31 digit display Display reads from 000 to 1999. Overload indicator. Protected Separate fuses for current and resistance circuits. Accurate Dual slope integration. High stability.

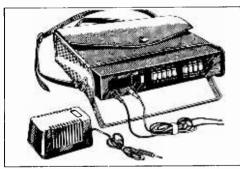
Rugged construction Tough metal casing takes the roughest treatment - try standing on it! Two power sources Supplied with a 9 V battery, giving 60-hour typical life. Mains adaptor also available. Portable Weighs only 3 lb approx, including battery. Measures only 2 in x 9 in x 6 in approx. Optional extras Mains adaptor - £3.19 inc VAT. Carrying case - £5.40 inc VAT. 12-month no-quibble quarantee



Use it in your laboratory . The DM2 sits rigidly on its combined carrying handle/stand.



Use it on the move. Keep the DM2 in its carrying case - it's always ready for use.



All you need to use the DM2...anywhere. Mains adaptor...carrying case...multimeter...you're ready for quick, efficient metering – whatever the situation.

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Interested in a quantity discount?

Use the coupon to arrange a demonstration and get details of prices on 5 or more instruments.

Sinclair Radionics Ltd, London Road, St Ives, Huntingdon, Cambs., PE17 4HJ. Tel: St Ives (0480) 64646. VAT Registration No: 213 8170 88.



The Sinclair DM2 Multimeter: full technical story

DC Volts Range	Accuracy	Input	Resolution
nange	Accuracy	Impedance	
1 V	$0-3\% \pm 1$ Digit	> 100 M Ω	1 mV
10 V	$0.5\% \pm 1$,	10 Μ Ω	10 mV
100 V	$0.5\% \pm 1$ "	10 M Ω	100 mV
1000 V	0 50/ / 4	10 M Ω	1 V
	0•5% ± 1 ,, verload – 350 V on 1 V ru		••
Waximum of	1000 V on all o		
ACVolts			
Range	Accuracy	Input	Frequency
		Impedance	Range
1 V	1.0% ± 2 Digits	10 M Ω/40 pF	20 Hz-3 KHz
10 V	1·0% ± 2 "	10 M Ω/40 pF	20 Hz3 KHz
100 V	2·0% ± 2 ,,	10 M Ω/40 pF	20 Hz–3 KHz
1000 V	2·0% ± 2 "	10 M Ω/40 pF	20 Hz–1 KHz
Maximum o	verload – 300 V on 1 V ri	ange	
	500 V on all ot	her ranges.	
DC Curren		Input	-
Range	Accuracy	Impedance	Resolution
100 µA	2-0% ± 1 Digit	10 KΩ	100 nA
1 m A	0·8% ±1 "	1ΚΩ	1 μA
10 mA	0·8% <u>+</u> 1 ,,	100 Ω	10μΑ
100 mA	0·8% ±1 "	10Ω	100 µ A
1000 mA	2·0% ± 1 ,,	1Ω	1 mA
Maximum o	verload – 1 A (fused).		
AC Current		Frequency	
Range	Accuracy		
1	1.5% 2 Digits	Range 20 Hz-1 KHz	
1 mA	1.5% ± 2 Digits	20 Hz-1 KHz	
10 mA	1·5% ± 2 ,,	20 Hz-1 KHz	
100 mA	1.5% ± 2 "	20 Hz-1 KHz	
1000 mA	2.0% ± 2 "	20 12-1 112	
Maximumo	verload – 1A (fused).		
Resistance Range	Accuracy	Measuring	
		Current	
1 KΩ	1 0% ± 1 Digit	1 mA	
10 KΩ	1·0% ± 1 "	100 µA	
100 KΩ	$1.0\% \pm 1$	10 µ A	
1000 KΩ	1·0% ± 1 "	1μΑ	
10 M Ω	$2.0\% \pm 1$ "	100 nA	
0			

Overload protection - 50 mA (fused).

Readers outside the UK, please write for details of your local distributor to : Sinclair Equipment International Ltd, 33 Beauchamp Place, London SW1 1NU.

Huntingdon, Cambs., PE17 4E Please send me:	*I enclose a cheque for £
Multimeters @ £63.72	
Mains adaptors @ £3.19 inc VAT. Carrying cases @ £5.40 inc VAT.	*My Access/Barclaycard number :
I am interested in 5 or more multimeters. Please arrange a demonstration.	*I enclose an official company order – signed and dated.
Please send details of quantity discounts.	Please complete or delete as applicable.
Name	
Address	
	Please print



M ORE than 74 exhibiting firms with over 120 trade names filled the hotels Majestic and Cairn at Harrogate this year, when Audio 75 was held from August 29th to 31st.

To report on every item seen and to mention every firm would fill half-a-dozen issues of Practical Wireless, so we have chosen a few which we think will particularly interest our readers.

Alba

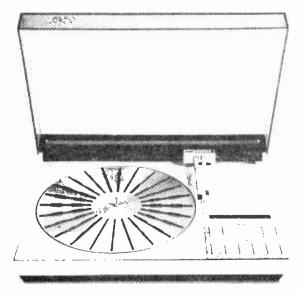
Alba exhibited a portable radiogram, Model 3200. It employs a 2-speed player and an a.m. radio and operates from $6 \times HP2$ batteries or from the mains Also on show was their UA 8080D teak-finished 3-piece suite with a 3-band tuner, stereo 3W per channel amplifier and a BSR autochanger.

Model UA 9070D is a music centre comprising a.m./f.m. tuner, $2 \times 8W$ amplifier, BSR changer and a cassette recorder—all in a teak cabinet with matching speakers.

Bang & Oluísen UK Ltd

Beocentres 1400 and 1800 were shown along with an impressive range of assorted equipment styled in the unique B & O way.

The 1400 has a stereo. a.m./f.m. radio, 20W per channel amplifier and a built-in cassette recorder. Price in teak. £249.50. The 1800 model has a similar



Bang and Olufsen's 6000 model.

specification but features an automatic record player instead of a recorder.

Amongst the range of Beogram record decks on show was the very sophisticated Beogram 6000 electronically controlled 4-channel deck with built-in CD4 decoder and MMC 6000 cartridge. Price is £387.90 but you do get a free copy of Mahler's 5th Symphony recorded in CD4 thrown in!

BASF UK Ltd

This firm was showing at Harrogate for the first time and exhibited their comprehensive range of reel-to-reel tapes and cassettes with a special display on the recently released 'LH Super Range'. With LH tape, the principle is as follows:

The magnetic particles of normal ferric oxide tape are comparatively large and irregularly shaped. Apart from increasing the noise level, this also reduces the sensitivity of cassettes at high frequencies, where the shorter wavelengths approach the length of the particles, because of the slow running speed.

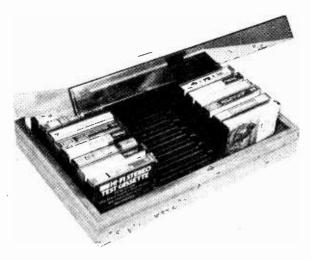
A Low Noise tape overcomes this by using smaller particles. LH Tape (Low noise/High output, invented by BASF in 1967) also uses smaller particles, but at a much greater density, giving a higher output on playback. LH Super is a very recent breakthrough in ferric oxide tapes from BASF. It extends the LH principle by using a new high density coating process and the smaller and more evenly sized particles of Maghemite (the mineralogical name for specially processed gamma Fe_2O_3 oxide).

The result is a full 50 per cent increase in sound quality. This can be seen by recording at OVU level, where the harmonic distortion is just $2 \cdot 5$ per cent—half the figure set by the DIN standard.

Even compared to BASF LH tape, LH Super is said to give a 3dB increase in recording level and over 2dB less tape hiss. Also seen were the automatic switching CrO_2 cassette machines—the Compact CC9110 at £35, the CC902 (£65) and the CC9302 with mixing facilities and a four-band receiver, priced at £90. Cassette decks on show were the 8200 (£180) and the 8100 at £120. See details of the BASF special offer in our News... pages.

Bib Hi-Fi accessories

Bib, as is usual at this type of exhibition had their full range of Hi-Fi accessories on show. Of particular interest was the new cassette storage unit Ref 86 which holds 30 cassettes in their containers. Fitted with a tinted acrylic hinged lid, the base of the unit comes in a simulated teak effect and the whole cabinet measures $15in \times 4^{1}_{4} \times 10^{1}_{2}in$ wide. Price is £6.60 excluding VAT.



Bib's new cassette storage unit.

BSR Ltd

BSR unveiled a new slimline plinth and cover, made to compliment the company's range of McDonald turntables. The plinth, in teak, is cantilevered out from a matt black base which gives the whole thing an illusion of 'floating' an inch or so above the surface of whatever it is stood upon.

The firm's belt-driven turntables were also featured, and, I feel, represent very good value for money. Top of the range is the BDS 90, upon which we hope to include a review in a later issue of P.W. It has a constant-speed high-torque motor with a heavy non-magnetic turntable. The tubular magnetic pickup arm has a concentric gimbal style mount and is fitted with counterbalance, bias compensation and a silicon-damped cueing device. Wow and flutter figure is quoted as ± 0.13 per cent.



The BDS 90 deck from BSR.

Eagle International Ltd

On show for the first time to the general public was the 2000 range, including the A2004 and A2006 amplifiers, turntables D2005 and D2006, headphones type H2008 and H2009, tuner T2008 and the S2002, 2003, 2004, 2005 and 2006 range of speakers.



Some of the Eagle equipment on display.

The 2004 amplifier is rated at 20W per channel. It has a facility for two extra speakers to give simulated quad. The 2006 has a similar spec. with the addition of 'sound effects controllers'. The A2004 costs £65 and the A2006, £85.

Eagle were also exhibiting equipment under the Beltek name and had their M1150 Dolbyised stereo cassette deck priced at £158 on show. Also there was the M1130 deck which was very similar but did not have the Dolby feature.

Fidelity Radio Ltd

The Fidelity range included the UA4 budget stereo system priced at £48.60. Features are a two-speed record deck, 5W per channel amplifier and two whitefinish speakers. The UA7 priced at £65.40 uses a BSR three speed record deck. The UA3 system is very similar in styling and priced at £87.96 with BSR changer, $2 \times 4W$ sine wave amplifier and a.m./ f.m. tuner.

One of the latest additions to the range is the UA6 system at £144.68. This comprises Garrard SP25 single play record deck with magnetic cartridge; 10W per channel amplifier, a.m./f.m. stereo radio tuner. A tape socket and a socket for stereo head-phones are provided. Top of the range is the MC2 Music Centre with BSR record changer, a.m./f.m. stereo radio, stereo cassette recorder/player, $2 \times 4W$ amplifier. Storage is provided for cassettes.

GEC (Radio & Television) Ltd

Music Centre Model 2917 has a.m./f.m. stereo radio, stereo cassette recorder/player and Garrard 6300 auto/manual 3-speed record player. The amplifier is rated at 10W per channel and provision is made for "ambio" sound. Price: £242.75. At £234.09 comes model 2919. It uses Garrard SP25 single play record deck; 4-band tuner with decoder fitted; and has a 15W per channel amplifier with provision for ambio sound. In teak, with matching speakers.

Top of the range is the model 2820, £271.21. Features include: 20W per channel amplifier with ambio facility; f.m. stereo radio tuner with electronic touch tuning, calibrated tuning meter, and interstation quieting; Garrard 86SB single play record deck with Shure magnetic cartridge.

Model 2821 is a combined 4-band stereo radio with BSR C141R record deck and $2 \times 7W$ amplifier, two speakers, it is priced at £121.66. Model 2816. (£147.72) has 4-band radio with BSR P128R record deck and a 15W per channel amplifier.



The Goldring L65 deck.

Goldring

Model L65—the latest addition to the Goldring Lenco range was shown. Particular items of interest are the automatic functions of the tonearm, the viscously damped suspension and the anti-skating device which with separate scales is adjustable for elliptical and spherical styli.

Other items in the specification are:

Speed: 33^{1}_{3} and 45 r.p.m. Wow and flutter weighted according to DIN 45507: <+/-0,12% Rumble unweighted according to DIN 45539: >38 dB Rumble weighted according to DIN 45539: >57 dB.

Turntable: Dia. 300 mm Weight 1.4 kg.

Tonearm: With a super light weight aluminium headshell suitable for use with all international standard cartridges. Stylus pressure adjustable 0-5 gm.

Mains voltage: 110V/60Hz, 220V/50Hz Power Consumption: Approximately 2.5 VA.

Measurements: Chassis $405 \times 300 \times 2$ mm. Depth required below chassis 54 mm. With plinth and dust cover $426 \times 321 \times 148$ mm.

Weight: With plinth and dust cover 6.75 kg, and packing 8.6 kg.

The Goldring Lenco ST800 compact stereo system was also on show. Incorporating the GL78 transcription unit, fitted with a G800E cartridge, it has an f.m. tuner fitted with three pre-set station buttons. Output is 40W per channel and slider controls are provided for volume, bass, treble and balance.

Also shown was the Goldring range of stereo magnetic cardtridges—including the easily replaceable stylus system types 820 and 800 series.

JVC (UK) Ltd

JVC model 1845 shown on the stand features a 3-band a.m./f.m. tuner with $2 \times 15W$ rms amplifier, front loading cassette deck with CrO_2 facility and noise suppressor. This comes with a belt-drive transcription turntable with magnetic cartridge. The tuner is fitted with tuning meter and loudness control. Price, including speakers, is £280 plus VAT.

Model MC-1820L features a stereo cassette deck of the same design as the company's more expensive ANRS decks, plus an a.m./f.m. stereo tuner 16W per channel amplifier all housed in low profile cabinet. Price, exclusive of speakers, is £145 plus VAT.

JVC have developed a new I.C. for their ANRS (Automatic Noise Reduction System). It is said to improve both performance and reliability and lower the cost of incorporating ANRS in existing equipment.

Compactness is the keynote of the new ANRS circuit now and the relatively few external components used in the unit allows the whole p.c. assembly to occupy half the area previously taken up.

Philips Electrical Ltd

The Philips range on show was so vast that we can only mention a few items of their equipment.

Model RH734 tuner-amplifier covers a.m./f.m. bands and has a 30W per channel output. Price is £207·18. The RH732 tuner-amp has a similar radio specification but a 12W per channel output. It sells at £172·45. A matching record deck for either unit is the new GA427 belt-drive model fitted with a GP400 magnetic cartridge. Price is £62·50.

Another recent addition to the Philips range is the RH741 4-band tuner with a 15W per channel amplifier. An interesting feature of this model is the visual indication on scales for bass and treble response. Price is £167.83.

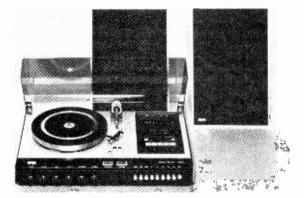
The GF907 record playing system is in a crackle black and silver finish (something different anyway!) The deck employs the GC007 belt-drive turntable fitted with a GP400 cartridge. The amplifier is rated at 15W per channel output and the price is quoted as £184.61.

Top of the range of music centres is the new RH832 priced at £781.25. The spec. includes: 4-channel pre-amplifier with built-in SQ decoder and connection for CD4 demodulator; 2-speed electronically controlled record playing deck with GP422 magneto-dynamic cartridge; a.m./f.m. tuner equipped for stereo f.m. and 4-channel (SQ) transmissions.

Pye Ltd

Pye's Sound Project ZU440 record player/f.m. radio/ cassette recorder was on show. It features 'disc jockey' mixing. The cassette unit has DNL (Dynamic Noise Limiter) and the amplifier delivers 15W per channel. The tuner has decoder fitted. Price, including two 2-unit speakers and mono microphone, £364.88.

ZU540 combines f.m. tuner with stereo beacon and four station push buttons; transcription type 2-speed record deck; cassette recorder with Dolby system and CrO_2/Fe_2O_3 automatic sensing. The amplifier is rated at 2×20W. The speaker assemblies use a bass/mid range unit with a line tweeter. Price is £475.48.



Sound Project ZU540 from Pye/Ekco. Practical Wireless, November 1975

HARVERSONIC SUPER SOUND HARVERSONIC MAINS OPERATED SOLID SUPERSOUND 13 HI-FI MONO 10 + 10 STEREO AMPLIFIER KIT STATE STEREO FM TUNER AMPLIFIER A superb solid state audio ampli-





Yung atte smoothing with negligible hum. Valve line up:-2 ~ SCL286 Triode Periodes. 1 × EZ80 as rectifier. Two dual potentioneters are provided for bass and treble control, giving bass and treble boost and cut. A dual volume control is used. Baiance of the left and cut. A dual volume control is used. Balance of the left and right hand channels can be adjunted by means of a sepa-rate 'Balance' control fitted at the rear of the chassis. Input sensitivity is approximately 300mly' for full peak output of 4 watts per channel (8 watts mono), into 3 ohm speakers. Full negative feedback in a carefully calculated distortion. Supplied complete with knobs, chassis size 11" w × 4". Overall height including valves 5". Ready built & tested to a high standard. £12:50. P. & P. Sp. ALL-PURPOSE POWER SUPPLY UNIT 200/240v. A.C. ALL-PURPOSE FOWER SUPPLY UNIT 200/240V. A.C. input, Four switched fully smoothed D.C. outputs giving 6v. and 74v. and 9v. and 12v. at 1 anno on load. Fitted insulated output terminals and pitot lampin indicator. Hammer finish metal case overall size $6'' \times 3\frac{1}{2}'' \times 2\frac{1}{2}''$. Ready built and PRICE £6.35 P. & P. 55p.

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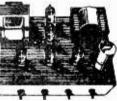


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Model 1570 is a unit audio console in a teak cabinet having record storage facilities. The amplifier is rated at 15W per channel. The tuner is a.m./stereo f.m. and the record deck is a single play unit. Twin 2-unit speaker assemblies are included in the quoted price of £237.58.

Model SXO940 is priced at £199 with a tuner including s.w. band, cassette deck and GC014 single play record deck. The amplifier rating is $2 \times 5W$.

Priced at $\pounds 230.91$, which includes speakers and metal stand, is the model 5024 comprising 3-band radio/cassette recorder and 3-speed stereo record player.

Pyser Ltd

On show was the new Marantz 1040 integrated stereo amplifier. Rated at 20W per channel, it features professional type graphic tone controls and main/remote speaker switching with ambience and loudness compensation. Price: £132 plus VAT. Also shown was the new 1070 amplifier and the model 2325, $2 \times 125W$ stereo receiver with Dolby.



Marantz 1040 stereo amplifier.

Rank Radio International

On view for the first time was the SP range of Wharfedale loudspeakers. Two models make up the range, the Dovedale SP and Airedale SP. Both are floor standing reflex enclosures.

The Dovedale SP is a 60 litre enclosure handling 60 watts DIN whilst the larger Airedale contains 100 litres and accepts 100 watts DIN. The Dovedale has two in-phase bass drivers, one mid-range and one high frequency unit. The Airedale has a bass driver, two mid-range units covering between them the range of frequencies between 300Hz and 5kHz and a high frequency unit.

The Airedale SP has a bass cut-off frequency of 27Hz (-3dB) which represents the lower limit of human audibility. The Dovedale SP is little higher with a bass cut-off of 35Hz (-3dB). Both respond to beyond the limits of audibility at high frequencies.

The Dovedale SP and Airedale SP are available in Teak with removeable speaker grilles at the respective recommended retail prices per pair of $\pounds 182.71$ and $\pounds 274.10$ including VAT.

Skantic (UK) Ltd

Skantic introduced their new model 17532 17W per channel stereo hi-fi music centre. This unit includes an f.m. stereo radio and there are push buttons for selection of five pre-set stations.

The Skantic turntable has a 16 pole synchronous motor, an anti-skating device and easily adjustable stylus pressure. The arm includes a Pickering V15



Rank Radio International's latest models.

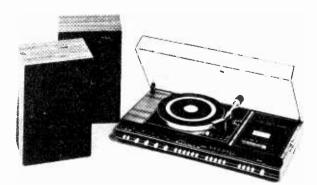
AT2 magnetic cartridge. The cassette recorder is completely designed and manufactured by Skantic's own engineers. The tape deck also has a built-in DNI. noise reduction system, an autostop and chrome dioxide switching system. A VU meter for recording and playback levels and a digital counter are also included.

The 17532 exceeds European standard DIN 45 500 and is ready for ambiophonic stereo. The unit is available in Rosewood, teak or walnut high grade veneer as well as white or black lacquer.

Skantic's newly designed speakers, which are included with the 17532, each have a power handling capacity of 30 watts. Each speaker has two units a 20cms unit for bass and middle range and a 2.5cms dome-tweeter.

Features of the unit include loudness compensation filter selector; switchable sockets for headphones and inputs for two microphones.

Price including speakers: Rosewood—£308·78+ VAT; Teak—£288·75+VAT; Walnut W/B—£302·33 +VAT.



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 83 amp 43, 407, 84, 80, 86, 40, 48, 06 48, 70

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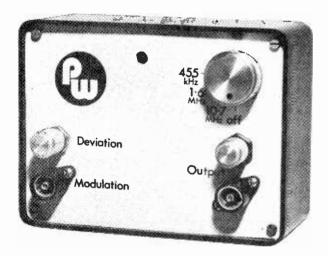
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List of Circs and Manuals available on request.

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F REE running oscillators designed around TTL ICs are notorious for poor frequency stability. The most significant factor contributing to frequency drift is variation of the supply voltage, and it is this apparent 'disadvantage' that is exploited in this circuit.

The FM Signal Generator (Wobbulator) is an essential piece of apparatus for setting up the HF circuits of FM receivers, and is extremely useful for the fast, accurate alignment of AM IF strips. In the conventional RF signal generator a continuous carrier is generated at constant frequency. A second signal at (usually) audio frequency is then applied to this RF signal varying the RF output voltage amplitude in direct relationship to the second, modulating frequency. In the FM signal generator the RF waveform is generated at constant amplitude and the modulating tone is used to vary the frequency of the RF signal.

The simple Wobbulator described here provides signals at three selected centre frequencies with provision for wide frequency deviation using external modulating sources. Although the RF signal is based on a square waveform rather than the more conventional sine wave, the effect of this difference is negligible in practice.

Basic circuit

The basic circuit of the free running TTL multivibrator is shown in block form in Fig. 1, and is probably the simplest circuit available to the amateur constructor! If Ct is omitted the oscillator comprises three positive logic NAND gates in series. In this configuration the mode of operation is quite straightforward. If the input at gate 1 is 'low' the output will be 'high'. Gate 3 thus has a 'low' input and a 'high' output and since the output of gate 3 drives the input of gate 1 a self-oscillating loop is created.

The operating frequency of this oscillator is deter-

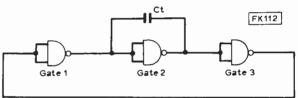


Fig. 1 : Block diagram of a basic TTL oscillator.

mined by the signal propagation delays through the gates. For the SN7400 gate the propagation delay for the 'low' state is approximately 8.0ns and for the high state 18ns. As the oscillator alternates between two 'low' plus one 'high' state, and two 'high' and one 'low' state the total delay alternates between (8+18+8)ns and (18+8+18)ns. The typical average delay is thus: $\frac{34+44}{2}$ or 39ns, giving typical free-running frequency of $\frac{1}{39 \times 10^{-9}}$ Hz or 25MHz.

As the two delays are not equal the output is not a 1:1 mark/space ratio squarewave and in practice stray capacitance and internal inbalances tend to emphasise the delay difference to give a ratio nearer 2:1.

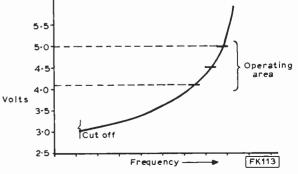


Fig. 2: Frequency plotted against voltage for a TTL oscillator. As can be seen, the relationship is non-linear.

Frequency variation

The oscillator frequency can be varied by altering the propagation delay time, by modifying the rise time of the transfer pulse. This is the function of Ct. It is possible to use a series of capacitors across one, two or all three of the gates to give a more stable arrangement but in practical circuits this complication is rarely justified. The effect of Ct is surprisingly linear and for the purpose of initial trials the oscillator frequency can be expressed as: If Ct=22pF then F=11MHz and if Ct=500pF, F=500kHz.

These values as calculated should be treated with some caution as tolerances can lead to quite significant modifications to Ct to obtain a given frequency of operation. The equation thus indicates an approximation for Ct, the actual value has to be found by experiment.

The oscillator frequency increases with increasing supply voltage, Fig. 2, and as can be seen the frequency/voltage relationship is non-linear. However, if we consider a relatively small voltage change $(\pm 0.5V)$ the linearity is sufficiently good to make the control of frequency by means of varying the supply voltage a worthwhile proposition.

The simplest arrangement for varying the supply voltage is the series emitter follower shown in Fig. 3 in which the base of the transistor is biassed by means of a potential divider and the collector taken to a suitable positive supply. In this arrangement the voltage appearing at the emitter is equal to the base voltage less the base/emitter voltage drop of the transistor (0.6V in the case of silicon). If a variable voltage is now applied to the base of the transistor the emitter voltage will rise and fall in phase with the base voltage so that the emitter 'follows' the base voltage.

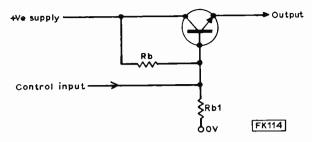


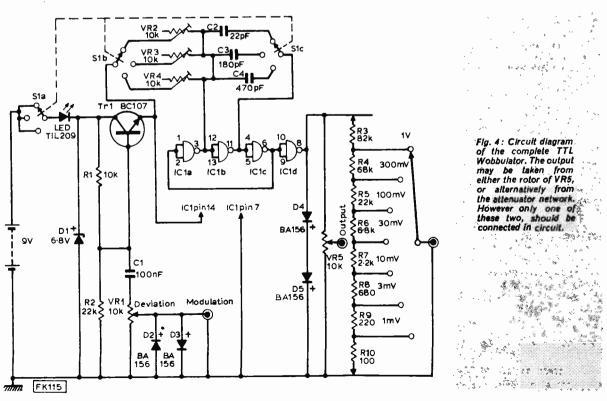
Fig. 3: The theoretical series emitter follower shown here, varies the voltage, and thereby the frequency of the oscillator to which it is connected.

Practical circuit

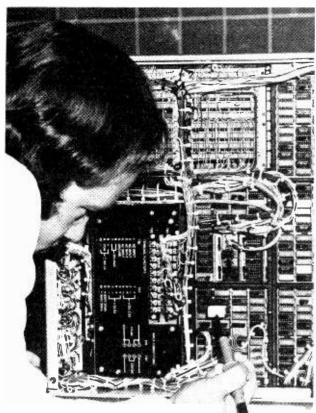
In the practical circuit Fig. 4, the timing capacitor (Ct of Fig. 1) is switched by means of S1c to provide three spot frequencies, the values shown giving spot frequencies of 455kHz, 1.6MHz and 10.7MHz. Variable resistors VR2-3-4 are incorporated to

Variable resistors VR2-3-4 are incorporated to set the precise operating frequency. These resistors modify the current flows to the gate inputs and provide a small degree of frequency adjustment on each range. It is important that these resistors should be set to the highest possible value to minimise the gate bias, as overbiassing can lead to erratic running and poor stability. If it is found that the tuning resistor has to be set to a value of less than $2k\Omega$, then an alternative timing capaictor should be sought.

The SN7400 is a quadruple NAND gate, and since



Practical Wireless, November 1975



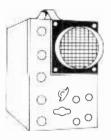
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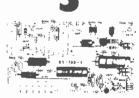
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only three gates are used for the oscillator, the fourth gate can be used as a buffer to prevent the output load from affecting the operation of the oscillator. The output from the buffer gate depends very much on the device used. The cheap, low-noise immunity gates give a swing of about 2V, while the more expensive can manage 3V or so. These output levels are too high for most purposes and the circuit of an optional attenuator circuit is shown in Fig. 4. As the output from the gate is a squarewave the simplest way of maintaining constant amplitude to the attenuator is to clip the signal at a predetermined level. This is the function of the diode network D4/D5 which limits the output to 1.8V. The clipped signal is then fed to VR5 or the resistive ladder network (R3-R10) which makes up the attenuator.

Modulation

The modulating signal is AC coupled to the base of Tr1 to prevent any residual DC component of the waveform from de-tuning the oscillator. The diodes D2 and D3 wired back-to-back limit the modulating signal. Silicon diodes are again used here with a forward voltage drop of 0.6V so that they need at least 0.6V across them before they conduct. If the input signal exceeds this value one or other of the diodes conduct shorting the excess signal to earth.

The potentiometer VR1 determines the level of modulating signal reaching Tr1 base and therefore controls the frequency variation of the oscillator with respect to input voltage. This potentiometer is thus the deviation control. The zener diode D1 limits the rail voltage to 6.8V. An alternative mains power unit is shown in Fig. 5.

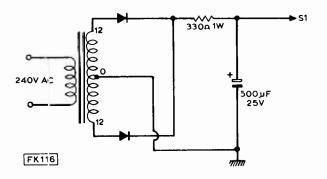


Fig. 5: Alternative mains power supply. This is recommended if prolonged use is to be made of the Wobbulator.

Construction

The oscillator and modulator are built on a piece of 0.1 in. matrix veroboard, Fig. 6. The layout is not critical and may be built on any scrap piece of veroboard. The trimming capacitors and resistors are wired directly on the range switch while the resistors comprising the alternative attenuator chain are similarly mounted round the output range switch (not shown in photograph).

Using an aluminium box $130 \times 100 \times 50$ mm deep, the battery powered version can be neatly accommodated on the metal panel as shown in the photographs. The mains powered version can be built

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into the same size box if the Doram transformer specified is used. However, as this involves some rather careful 'packing' of components, the less experienced would be well advised to opt for a larger box.

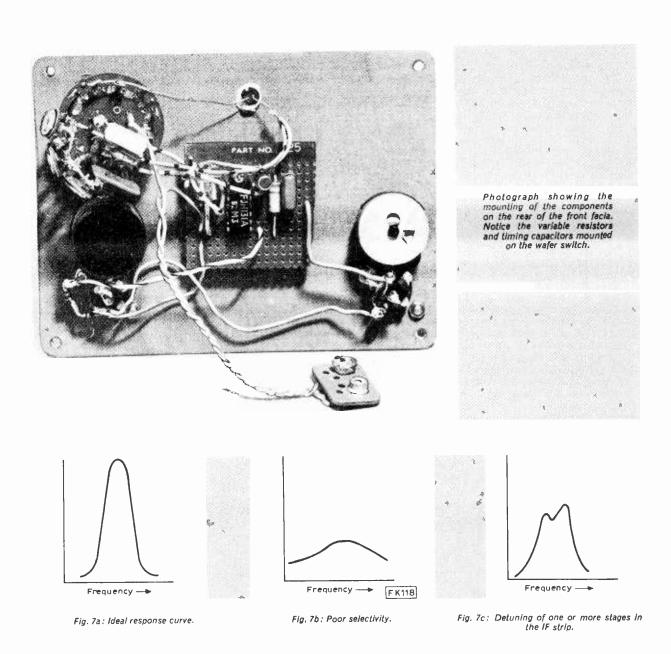
Calibration

Carefully check the wiring, switch on and check that Tr1 emitter voltage is $4.5V (\pm 0.2V)$. R1 should be adjusted if necessary to obtain this voltage. The spot frequencies must next be established. During this setting-up procedure the modulation input must be shorted to earth. Using an 'all-band' communications type receiver, feed the attenuated output from the wobbulator into the aerial socket. With the BFO switched on, the wobbulator output can be detected and VR2-3-4 adjusted until the required three spot frequencies are obtained. The attenuator function can also be checked against the 'S' meter.

In the absence of a suitable communications receiver the spot frequencies will have to be set up against known frequency IF strips. The output from the wobbulator should be injected into the first IF transformer, the most convenient point being at the mixer stage. A voltmeter should then be connected across the AGC line and the appropriate VR adjusted until maximum AGC voltage is detected. The spot frequency is then set to the centre frequency of the IF.

Resistors 10kΩ R8 - 680Ω R1, 22kΩ 220Ω **R**2 R9 100Ω **R**3 82kΩ R10 R4 **68k**Ω VR1 10kΩ **R5** $22k\Omega$ VR2 10kΩ 6.8kΩ 10kΩ **R6** VR3 **R7** 2·2kΩ VR4 10kΩ 10kΩ All 5% 1 or 1W VR5 Capacitors 100nF .180pF C1 **C**3 **C2** 22pF 470pF \$ ' Semiconductors DA **BA156** Trl BC107 BZY96 6-8V zener D5 **BA156** D1 D2 **BA156** IC1 SN7400 BA156 D3 Miscellaneous LED type TIL209. Two coaxial sockets. Four knobs. Four-way three-pole wafer switch." 0-1in. matrix-veroboard 40 x 30mm. Metal box 130 x 100 x 50mm. Single pole, seven way wafer switch. Optional power supply Mains transformer, sub. miniature 12-0-12V, type 196-274 Doram Electronics. Two rectifier diodes type 1N4001, 330Ω 1W resistor, 500µF 25V electrolytic capacitor. this . * ×: # 4 · • .° ð. 2

★ components list



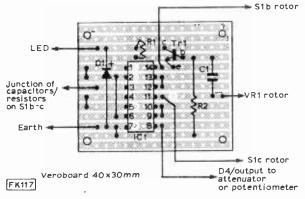


Fig. 6: The circuit should be laid out on 0.1in. matrix Veroboard as shown above.

Operation

To use the wobbulator effectively an oscilloscope with an X deflection output is required which is fed into the modulation socket of the wobbulator and the Y input (vertical deflection) is coupled to the detector of the intermediate frequency strip under test. The wobbulator output is then applied to the IF transformers in turn starting with the last IF and progressing to the first. The response shown on the cathode ray tube should be as Fig. 7a. Figs. 7b and 7c show poor selectivity and detuning of one or more stages respectively. With care it will be found that this technique will give up to 6dB more gain and greater selectivity than the usual method of amplitude modulated signal generator plus ear!

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RELAT DANGAIN Type 600 relay, 2 changeover one open and one closed contact. Twin 500 ohm colls make this suitable or closing off DG 6v, DC 12v, DC 24v or AC mains using resistor and rectifier. 40p each. Resistor and rectifier 20p extra.. and Post VAT 20p.

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	. 5 amp	·85
	. 2 amp	1.85
	. 3 amp	1.75
	. lamp	-95
9	. 35 amp	2.50
	liamp	1.20
12v	. 1 amp	1.00
6.5v-0.6 5v	. 1 amp	1.50
18v	. lamp	1.50
24v	. 2 amp	2.25
24v	. 3 amp	8.50
12-0-12v	. 50mA	1.20
6-0-6v	. 50mA	1.80
8-0-8v	. ł amp	1.50
18-0-18v	. 2 amps	8.50
0.5	. 11 amp	1.95
50v 2 amp & 6.3v .	. lamp	4.50
	. 1 amp	7.50
	. 8 amp	4.50
	. 37 авър	28.00
80v tapped 75v & 70v	4 amp	5.50
	. 1.5 amps	1.75
275-0.275v at 90mA &	64v 3 amps .	2.25
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00. 1	. (intermittent)	5-50
Charger Transformers	(
P	. 2 amps	1.50
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Add 30p per piece to co	ver postage and VAT	

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AUDIO AMPLIFIER

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ISA ELECTRICAL PROGRAMMER Learn in your sleep: Have radio playing and kettle boiling as you awake—switch on lights to ward off intruders—have a warm house to come home to. Ul these and many other things you can do if you invest in an electrical programmer. Clock by famous maker with 15 anp. on/off switch. Switch-on time can be set anywhere to stay on up to 6 hours. Inde-te on the set anywhere to stay on up to 6 hours. Inde-60p, or wita glass front, chrome bezel, £1:50 extra.

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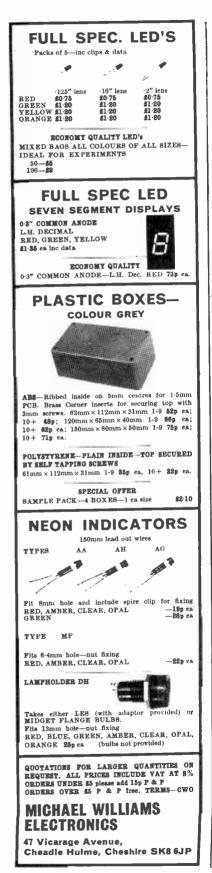


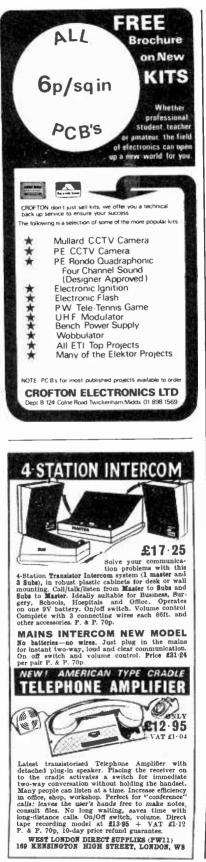


















SHORT WAVE BROADCASTS by Derek Bell

B EARING out my long-held view that the HAC one-valver is the ideal simple set for the beginner, Andrew McIntee from Craichie, by Forfar, in Scotland, opens this month's offering with the logging of New Zealand on 11780 at 0900. This is only a 7.5 kW station and to pull it on the HAC is worthy of a round of applause at least. Andrew does admit though that he has a 180ft long wire aerial and has fitted an ATU. Speaking of which, I hear that one of the advertisers in PW is testing a new aerial tuning unit and if it is a success it will be launched in the near future. I have no news on the price as yet but will keep you informed.

This month certainly seems to be rich in unusual loggings, it must be the revivification caused by the summer holidays! This is evidenced by John Spinks of Great Moulton, Norfolk who, using his Trio and the old faithful Joystick on the garage roof, he has pulled in the following:—

Radio Bolivar on 4770 at 0120 Radio Bucaramanga on 4845 at 0115 Kinshasa, Zaire on 4880 at 2150 Radio Yaounde, Cameroon on 4972 at 2140 Sibu, Sarawak on 5005 at 2215

In fact John's complete log contains a fistfull of very rarely reported stations and even had me trying for a few of them, nice work, John! **Robert Hill** of Crewe is off to Portugal for his holidays, a little late perhaps but he found time to drop us a line logging ELWA Liberia on 11895 at 0920. Aside from cramming for the dreaded 'A' levels Robert has fitted a reel-to-reel tape recorder to his Invicta 8027 and seems to be set fair to record some station ID's in order to refresh his memory, if need be.

Another old friend of ours is John Higginbotham of Holyhead and this worthy gentleman sent a long amusing letter regarding his domestic set-up. It seems that he has the same problem that many DXers face, namely, where to put all the bits and pieces! John says that his mother was "fed up with the bedroom looking like a workshop". Thus it is that he has moved into a garden shed. Fine on the shed John, but remember that radios in the main are precision instruments and do not take kindly to damp. The best thing to do is to keep the sharpest of eyes on the humidity and try to beg, borrow or steal some form of heating. Thanks to this column John has pulled Radio Afghanistan on 15195 at 1130. He also QSL'd Pekin and the score to date on replies is as follows:— One calendar, two books, seventeen(!) magazines, two QSL cards, three skeds, three report forms and one notebook! Personally I can't see what they hope to achieve but they still keep sending out all this literature.

Two writers this month focus the spotlight on Radio Mexico. Harold Emblem from Mirfield, Yorks reports them testing on 15285 at 2205 while Jonathan Marks of Norwich writes that on 15125 they were asking in English and French for reports at 2258 while 2309 the language changed to Spanish. This indicates to me that they are trying to establish themselves in Europe in competition with Radio Nacional de Brazil. They asked for reports, without IRCs, to be sent to Radio Mexico, PO Box 20/620, Mexico City, Mexico and promise that accurate reports will get a Radio Mexico pennant.

Another address for QSLs comes from Chris Clarke of Shipdam who passes on the info that the American religious station WYFR asks for reception reports to be sent to Family Radio, Oakland, California, N 4621 U.S.A. Far across the Indian Ocean both India and Sri Lanka broadcast to their citizens in other lands. One person who reports them is **P. K. Gulati** of Guildford who sends the loggings of Air Delhi on 1110 and 7150 at 1900 plus Radio Sri Lanka on 1200 at 1730.

The popular question of QSL cards is raised by Jeremy Hinton who hails from Newcastle, Staffs. He asks what is the average time for a reply? Well Jeremy, this all depends on the station and its eagerness to maintain good relations with its audience. I will not deny that some stations lose reports or are plain lazy, and recently some American DXers got their replies back after ten years! You mentioned, Jeremy, that Radio Nederland refused you a QSL because you omitted to report the frequency. These details are important to the engineers in order that they can judge if their signal is reaching the target area.

A very welcome letter comes from Malta and asks if the writer is justified in sending reports to PW. I regret that I could not decipher the name but I believe it to be **Vincent Canabatt**. Well, Vincent your part of the world is very rich in transmitters and if you can hear them then there is a very good chance that we in the UK will. PW is read in a good many countries overseas and your tips will help them a lot. All that is needed is to write the station name, frequency, and time in GMT. It is also of interest



if you include any unusual details such as addresses or any news of future events that the station may broadcast.

There has been a very heavy post so inevitably many letters have to be left out, so to the writers I can only apologise and say 'keep trying' and to everyone wish best 73s and so close the column for this month.



by Eric Dowdeswell G4AR

I am very glad to notice, in the various amateur radio magazines, an upsurge in operating using quite low power. As one would expect, those who try this very interesting work usually get quite a kick out of working stations thousands of miles away when using milliwatts of power and ordinary receiving type transistors. The work is virtually all on CW and the point in mentioning it is to ask those of you who are interested in copying code to have a look at the LF ends of the various bands for those chaps calling 'CQ QRP'.

Needless to say, one can spend a lot of time calling without getting a reply so, for a change, these stations would probably welcome reports from listeners. CQ Magazine runs a regular feature on QRP work which makes very intriguing reading! With the widespread abuse of licence power limitations in various countries it is good to hear of those who have gone in the opposite direction! Let us hope it will be a continuing trend.

The summer hang-up is really showing now with relatively few reports coming in. Readers are no doubt taking every advantage of the sub-tropical weather we have been enjoying for so long. Let's hope they are building up a great reserve of strength for the forthcoming DX season which will be quite tough with the bottom of the sunspot cycle not yet reached.

Fortunately, **Paul Barker** (Sunderland) has kept his nose to the grindstone possibly due to the added incentive of being able to watch slow-scan TV. 'Catch of the Month' for Paul was 9X5AV on 20m SSTV but for sheer excellent picture quality Paul gives full marks to DL7DE in Berlin. (Marks—oh dear!) Paul points out that prefix C9 is now being used in place of the old CR7 reporting C9MIC as active in this strife-torn country. He also notes YR as a special prefix for Rumania but if I went to my very ancient collection of QSL cards I could find one showing YR as the old prefix used by that country! I think someone once said something about "all is change but nothing changes'.

Mike Bennett (Slough) didn't mention too many catches but all are very much worth while, such as C21NI on Nauru and FP0YY on St. Pierre and Michelon and the Mount Athos DXpedition SV1GA/A. Jeremy Hinton A8962 (Newcastle, Staffs) had trouble with his Trio 9R59DS, which I hope I have been able to straighten out, so his log is very short this month. Back to Mike Bennett who sends some info on changes to licensing areas in PY land, too long to publish, but first suffix Z indicates a foreign operator such as PY1ZAA while similar suffixes W, X or Y indicate a novice licence. Just in case you ever hear one operating car mobile, his call will add /MT!

Although Neil Whiteside has been on holiday with a 160m receiver in Dorset, away from his usual QTH in Hitchin, I am sorry to say he allowed local attractions to divert him from amateur radio! Let's hope he has got back on to the straight and narrow by now!

Ian Jay (Mansfield) has really got the knack now of only listing those stations of real interest including VP2 and ZL2 on 40m SSB. Tim Charles (Colchester) apologises for lack of a log last month but his excuse is 'great changes going on in the shack', which, I suppose, is fair enough! Main receiver is now a Heathkit GR64 plus a home-built Q mulitplier. He tried to flog his CR70A at the Anglian Mobile Rally, without success, but I suspect he will be glad, in the long run, to keep it as a second receiver. Can't have too many of them around the place! Tim quotes latest UK calls issued as G8KMM and G4EHT in the middle of August but there will be many more with their hard-earned bits of paper 'ere you read this.

Stephen Budd A8713 (Worthing) has very wisely erected a Lazy-H beam which he thoroughly recommends. He doesn't mention its size but if it has 66ft centre-fed elements then it is a very good performer indeed, with open line feeder and an ATU, for 40m to 10m. The usual problem is getting enough height above earth for the lower elements to be really effective. The bi-directional beam obviously passes through the Pacific because he logs such interesting ones as KB6CU on Canton Is., four KG6's on Guam and KJ6CF on Johnston Is. all of which come into the 'rare' category. That was on 20m SSB but I hope Stephen will try that beam on the other bands in due course.

Log extracts

S. Budd:— 20m HS5AKW KB6CU K1MTJ/KG6 WB4LEE/KG6 KG6JBE KJ6CF KL7BJW KM6EA KS6FF KS6FK ST2SA VR1AT VS5DB ZD8LS

T. Charles:— 40m VK3XB 20m HC5PC JW5NM VR1PE ZL1EGM 2m DB0VR PI3VAD (repeater) SP3BUE

I. Jay:— 40m CO2GS OJ0MA VP2MCT ZL2AGY 80m HZ1AB TR8DG VU2GDG 20m H18MOG SV0WKK (Crete) TG5YN VP2LBR VP2SN VS5DB 5L2FW 7X2BK

N. Whiteside:— 80m 9X5SP 5Z4LW 20m XE1APA KZ5RS

J. Hinton:- 15m A4XFW JY5UNM HI6EA

M. Bennett:— 20m C21NI FB8ZG FP0YY FR7ZW PJ8MS SV1GA/A 15m CX2BE LU6EAU ZP5IL 10m LU5DBA OJ0MA

P. Barker:— 20m C9MIC JA0AXV YR2KBQ 7X2BK 7X5AB PV0SH (Singapore) 9V0SN 9Y4HM 20m SSTV DJ9NG DL7DE F3RT 18WAM OH5RM OK2OI 9X5AV

All stations are SSB except those in bold which are CW.





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MEDIUM WAVE DX by CHARLES MOLLOY

ORTH AMERICAN medium wave stations are often heard here in the UK. A path of darkness between transmitter and receiver is required for medium wave propagation and this occurs to North America some five to six hours after sunset in the UK. During the winter months Canadians can be heard as early as 2300, to be followed an hour later by outlets situated on the eastern seaboard of the United States. North Americans operate on channels spaced 10kHz apart and they are allocated callsigns which are used frequently as a means of identification, followed by the city or town where the studios are located. Listen on 930kHz for CJON St. John's in Newfoundland. It is the most consistent North American, its time zone is 312 hours behind GMT and it can be found on the low frequency side of AFN Berlin on 935kHz.

Other Canadians which are heard regularly when conditions are favourable are CBN St. John's on 640kHz; CHER Sydney, Nova Scotia on 950kHz; CBA Moncton, New Brunswick on 1070kHz. Broadcasts from the United States to look for are WABC on 770kHz, WINS on 1010kHz and WNEW on 1130kHz, all in New York City; WIIDH on 850kHz in Boston on 850kHz and WCAU in Philadelphia on 1210kHz.

Steve Whitt (London) reports "I can't wait for winter DX conditions to test my loop aerial and I'm looking forward to a batch of North American goodies". Steven is now using the PW medium wave loop aerial and balanced FET pre-amplifier (April 1973) with his Chapman S6BS communications receiver and he reckons this aerial is far better, more sensitive and more directional, than his 30ft longwire on the roof. Stations logged on this new set-up include Radio Andorra on 701kHz, Radio Dakar in Senegal on 764kHz and CJON St. John's Newfoundland on 930kHz, three continents!

CQ! CQ! CQ! CQ!

ISSUES WANTED

.. Television for March, April, May, June 1974. R. Mehrotra, F-114 D.D.A. Colony, Naraina, New Delhi-28, 110028, India.

.. August 1973 issue of P.W.—T. J. Flanagan, 17 Addison Crescent, Old Trafford, Manchester, M16 0WN.

..January to April 1973 P.W. inclusive also June 1973 and March and April 1974 P.W.—K. Hunter, 31 Cwmbath Road, Morriston, Swansea, SA6 7BA.

..1950 March, November, December. 1952 January March, April, August, September. 1953 May—all Practical Wireless. —J. Luxton, Bergheim, Battery Hill, Fairlight, Hastings, TN35 4AP.

...P.W. for February 1974, February 1966, April 1969 and June 1969 plus any subsequent issues dealing with aerials, April 1970, June 1970 plus any subsequent issues dealing with the LF Bands Transceiver, April 1972. Also P.E. for

Practical Wireless, November 1975

Harold Emblem sends a really outstanding log of summer DX heard at his QTH in Mirfield, Yorkshire, on an Eddystone 730/4 communications receiver using a long wire and a medium wave loop. DX heard includes CBT Grand Falls, Newfoundland on 540kHz; CKVO Clarenville, Nfid on 710kHz; CBNM Marystown, Nfid on 740kHz; WABC New York City on 770kHz; CBH Halifax, Nova Scotia on 860kHz; CJCH in Halifax on 920kHz; CBM Montreal on 940kHz; CHNS Halifax on 960kHz; WINS New York City on 1010kHz; WNEW also in NYC on 1130kHz; WCAU Philadelphia 1210kHz; CKEC New Glasgow, N.S. 1320kHz; WLAC Nashville, Tennessee on 1510kHz and WKBW in Buffalo, N.Y. on 1520kHz.

Peter Bowyer (Kettering) uses a Murphy A168 for DXing on the medium waves and reports hearing AFN Augsburg and Radio Tirana, Albania both on 1394kHz and Trans World Radio, Montecarlo on 1466kHz. Fifteen-year-old Stephen Boyle of Auchterarder, Perthshire used a Philips 90RL210 with an externally mounted MW loop. Stations logged include Radio Norway on 1578kHz (in English at midnight GMT) and Radio Tirana, Albania on 1394kHz again.

Joseph Bite (Dublin) and Derek Vivian (Jersey C.I.) ask which type of receiver is the most suitable for MW DXing. Communications receivers such as the Trio 9R59DS, AR88, CR100 or the Heathkit GR78 (which operates from batteries or mains) have the sensitivity and selectivity that will bring optimum results. Simpler receivers when connected to a good aerial will, however, pull in a considerable amount of DX on the medium waves.

BROADCAST BANDS Short Wave reports by the 15th of the month to Derek Bell c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD. Medium Wave Logs to Charles Molloy, 132 Segars 4 Lane, Southport, PR8 3JG.
AMATEUR BANDS Logs covering any amateur band/s in band/ alphabetical order by the end of the month to Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey, KT21 2TW.

April 1965 and February 1966.—S. A. Rizvi, P.O. Box 2671 ' Tripoli, Libya.

...December 1970 and January 1971 issues of P.W.--J. M. Beil, 60 Wendover Road, Harlesden, London, NW10.

...all issues of P.W. including December 1971.—B. Disselmann, Skovlyporten 3-1, DK-2840, Holte, Denmark.

..issues of P.W. or the circuits of the P.W. Sound Effects Synthesiser first published in March 1971 (circuits 3-11 wanted).—D. Weeks, S.A.C., K8093975, GESF, R.A.F. Wildenrath, B.F.P.O. 42.

...any back issues of Practical Wireless, Television.--Craig Sellen, Box 853, Wayne, N.J. 07470, U.S.A.

..issues of P.W. containing instructions of the VHF Transistor Receiver with blueprint (around July 1965).— J. W. Cooling, 33 Flat Sorrel Court, 1 The Green, Mt. Sorrel, Leicestershire.

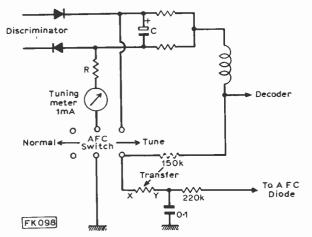
..P.W. May 1971—J. Rendall, 59 Hood Avenue, Southgate, London, N14 4QJ.

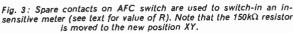
...P.W. January 1972 to October 1972 Inclusive, P.W. March 1973—June 1973 inclusive and P.W. October 1973.— G. F. McCarthy, Ballymodan Place, Bandon, Co. Cork, Ireland.

IMPROVE YOUR BUDGET STEREO SYSTEM —continued from page 574

cation I arranged that the audio is completely muted when tuning. Fig. 3 shows the final arrangement.

Any circuit changes should only be done after reference to the manufacturers circuit diagram to make quite sure that no unpleasant or even disastrous effects will result. The AFC circuit shown is common to almost all budget stereos. The AFC and audio are fed from the discriminator output via a high value resistance (typically $150k\Omega$) to the AFC switch. The AFC line is decoupled after the switch





(typically 220k Ω and 0 1μ F). The 150k Ω prevents the audio from being shorted to chassis when the AFC is disabled. In the new circuit arrangement, however, we want to lose it so that muting takes place when tuning, done by moving the 150k Ω to the diode side of the switch. With printed circuit boards the easiest way of doing this is to short out the existing 150k Ω with a wire link and to carefully cut the foil on the other side of the switch, bridging the gap with a new 150k Ω resistor.

The end product is superior to that provided on more expensive systems. We tune for a peak on the meter in complete silence, selecting the wanted station by the position of the tuning scale and then switching in the AFC to take care of drift. The muting works quite smoothly and there are no loud noises when it is switched in and out.

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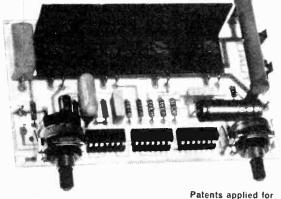


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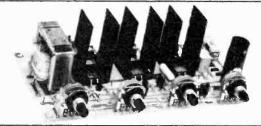
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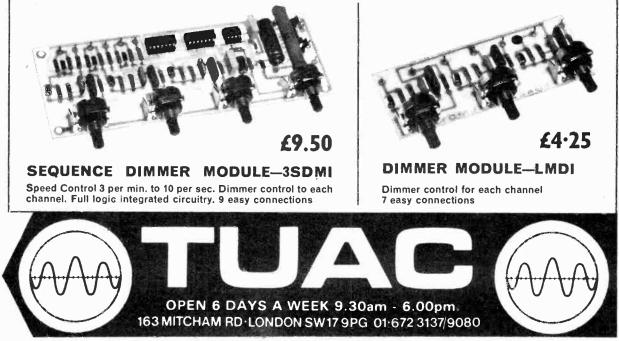
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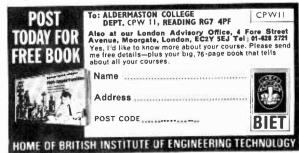
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33 68	16 16	7	
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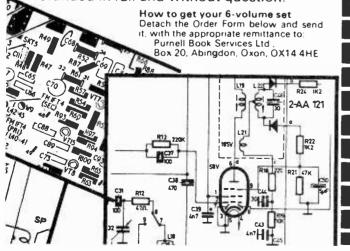
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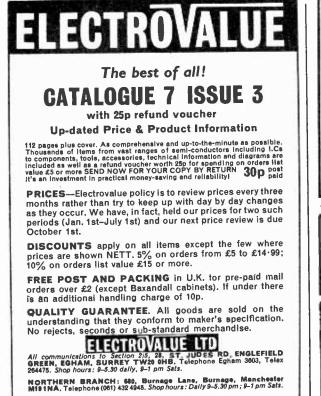
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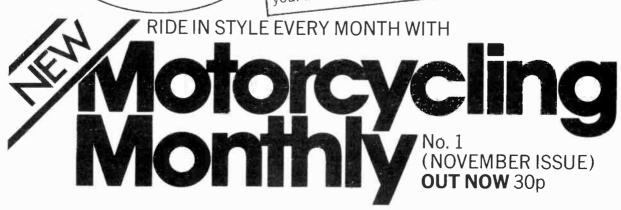
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FERRITE RODS i" diam. 2" - 8p; 5i" - 18p; 6i" - 20p	11 500mA-15A 3p 5A,7A,10A,13A.5p Anti-surge 20mm HOLDERS Panel Single 5p 100,250,500,800mA, Panel Single 5p 1A, 16, 2, 25, 315, 20mm Chassis 16p 5A 5A 7p each 11 Chassis 22p	SPEAKERS 8Ω 0·5W 2¼″ & 3″ 62p	23x17" 105p 78p 60p calibrated G-10.3/min dia. 34x17" 145p 115p 75p 4x17" 185p — 110p Pkt of 36 pins 22p K6 PK2 as K5 with pointer on skirt 20p Spot face cutter 52p Final 10p & skirt. Calib. 0-10, 30mm 20p Pin insertion tool 72p K8 Black or slivered for slider pot 7p

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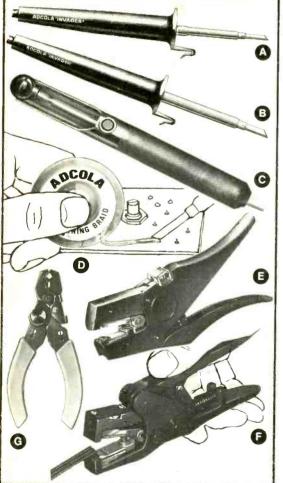
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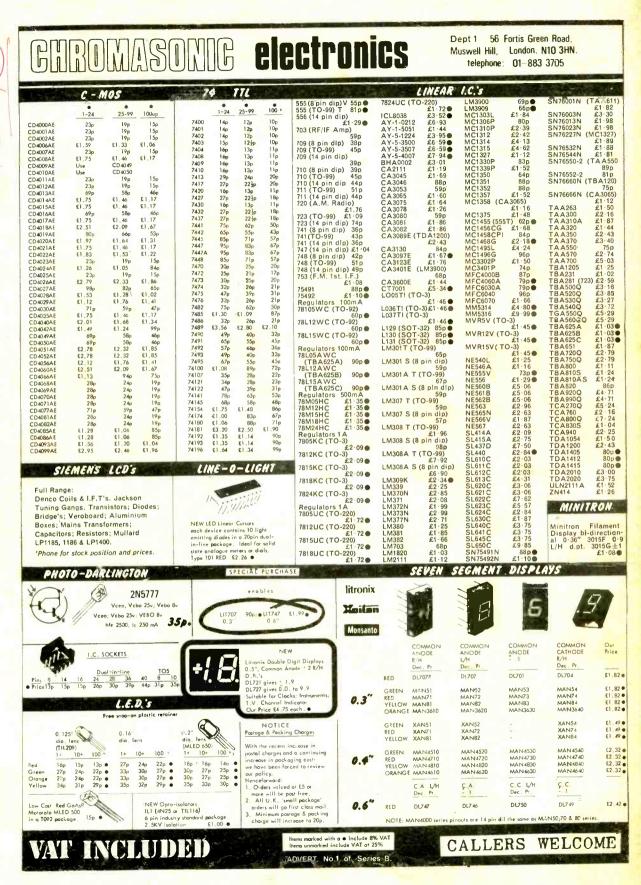


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