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#### Abstract

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| $=12 \times 7407$ | $\mathrm{UIC10}=12 \times 7410$

$\mathrm{UIO13}=8 \times 7415$ UIC20 $=12 \times 7420$ $\begin{aligned} & U I C 30=12 \times 7420 \\ & \text { U }\end{aligned}$ UIC40 $=12 \times 7440$ UIC41 UIC4
$\begin{array}{ll}\text { UIC41 }=5 \times 7441 & 0.60 \\ \text { UIC4 }=6 \times 7442 & 0.60 \\ \text { UIC43 }=5 \times 7448 & 0.60\end{array}$

| $\mathrm{UIC43}=$ | $5 \times 7448$ | 0.60 |
| :--- | :--- | :--- |
| 0.40 |  |  |
| $1044 \times 744$ | 0.60 |  |

UIC45 $=5 \times 7445$
UIC4 $5=5 \times 7446$
UIC47 $=5 \times 7447$

| U1C48 $=5 \times 7448$ |
| :--- |

UIC50 $=12 \times 7450 \quad 0.6$
$\begin{array}{ll}\text { UIC } 51=12 \times 7451 & 0.60 \\ \text { UIC } 8=12 \times 7453 & 0.60\end{array}$
$\begin{array}{ll}\text { UICJ8 }=12 \times 7453 & 0.60 \\ \text { UIC54 }=12 \times 7454 & 0.60\end{array}$
UIC80 $=12 \times 7460$
Price
0.60
0.60
0.60
0.60
0.60
0.60
0.60
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0.60
Pat Io. Contomte
UIC72 $=8 \times 7472 \quad 0.60$ $\mathrm{UIC73}=8 \times 7473 \quad 0.60$ UIC74 $=8 \times 7474 \quad 0.60$ UIC75 $=8 \times 7478 \quad 0.60$ $\mathrm{UIC78}=8 \times 7478 \quad 0.60$ $\begin{array}{lll}\text { UIC80 }=5 \times 7480 & 0.80 \\ \text { UIC81 } & =5 \times 7481 & 0.80\end{array}$ UIC81 $=5 \times 7481 \quad 0.60$
UICB2 $=6 \times 7482$
UIC8S $=5 \times 7483$
UCB $=5 \times 7486$
UIC8 $=5 \times 7486$
UIC90 $=5 \times 7490$
U1C90 $=5 \times 7490 \quad 0.80$
$\begin{array}{ll}\mathrm{UIC91}=\delta \times 7491 & 0.60 \\ \mathrm{UIC92}=8 \times 7492 & 0.60\end{array}$
$\begin{array}{ll}\mathrm{UIC92}=8 \times 7492 & 0.60 \\ \mathrm{UIC93}=8 \times 7493 & 0.60\end{array}$
$\begin{array}{ll}\text { UIC93 }=8 \times 7493 & 0.60 \\ \text { UIC94 } & 8 \times 7494 \\ 0.60\end{array}$
UIC94= $8 \times 7494$
UIC95 $=8 \times 7496$
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| DAF91 | 0.40 | EF91 0.40 | PC86 | 0.65 | UF41 | 0.75 | $6 \times 5 \mathrm{GT}$ | 0.56 |
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## System 1a. $\mathbf{f 6 9 . 0 0}$

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THE life blood of amateur radio is the spectrum space allocated to the amateur service between 1.8 MHz and 25 GHz . Without these precious frequencies, the radio amateur of today would become just another broadcast station listener. The regulation of the frequencies available to the various services, i.e. aeronautical, amateur, broadcasting, marine and so on, is governed by the conferences of the International Telecommunication Union which is the specialist agency of the United Nations for telecommunications. During the ITU conference the 144 member nations of the ITU vote on the proposals before them and in this way the future of frequency allocations is determined.

The last major ITU conference was in 1959 and there has been relatively little change in the spectrum allocation for amateurs since that time. The next major meeting is scheduled for October 1979 and the agenda will include a review of all frequencies comprising the usable spectrum. This means that each and every amateur service allocation will come under the scrutiny of the conference. On their decision alone will depend whether your present equipment will continue to be usable, or will be just another piece of surplus gear.

The possibilities and dangers arising from the 1979 World Administrative Radio Conference have been known and recognised by national societies and the International Amateur Radio Union for some considerable time. A great deal of preparatory work has already been undertaken and it is now clear that the amateur service will at this conference present a unified plan for its future modified only by minor regional differences. At the conferences of the ITU only the member nations are elegible to vote. However, the IARU is one of the few organisations recognised by the ITU and therefore entitled to attend its conferences as an observer where it may also speak and present papers.

Thus, while the IARU may participate actively in the conference its most essential work must take place in the co-ordination and advice offered to national societies throughout the world. It is the national societies only who can approach their own telecommunication administrations to seek their support for the future of the amateur service. It will be appreciated that in many countries this is a difficult task, never more difficult than in Africa. This is a challenge which has been accepted by the IARU and the national societies and the work of securing support for radio amateurs will continue without slackening until October 1979.

It would be unwise to give publicity to much of the work that has been, and will be done, and it is only the result that can prove its effectiveness or otherwise.

Now, as never before, the amateur service must be seen by all who come into contact with it to be something that is worth retaining and whose work and activity justify the present spectrum space allocated to it. Every radio club in every country has a part to play in this effort. It is the local radio clubs who bring together the individual radio amateurs and who form the backbone of the national societies. Those responsible for the conduct of a radio club should familiarise themselves with the position as it is today and with the steps that must be taken if the future is to be assured. Having done this they can then offer guidance to the individual members and initiate activity which will be of benefit not only to the amateur service but hopefully to the community at large.
continued on page 551

## Praclical Wireless P. C. Board Readers Service

I$N$ the October issue of Practical Wireless we announced that this magazine will be introducing a 'new' readers service whereby our 'copyright' printed circuit boards for selected PW constructional projects will be offered to readers.

We are anxious this service shall represent good value and our boards to be of the highest standards, therefore we are taking a further month to finalise the details which we hope to publish in full in the near future.

## Reprints

WE still have some copies of the Tele-Tennis reprints. If you would like one, send 82p to: Chief Cashier, (P.W. Tele-Tennis, IPC Magazines, Tower House, Southampton St., London, WC2E 4QX.

## Special offer

HI-FI enthusiasts buying cassette decks which accept chromium dioxide cassettes will find there is a dearth of prerecorded $\mathrm{CrO}_{2}$ cassettes. To ensure that purchasers of BASF machines are able to use their machines to the full, BASF is giving them the opportunity to buy BASF prerecorded $\mathrm{CrO}_{2}$ cassettes at special low prices.
The repertoire contains 22 titles, four of which are double albums. The price of the cassettes is $£ 3 \cdot 90$ for a single album and $£ 5 \cdot 80$ for a double album, but BASF are offering them at $£ 1.99$ and $£ 2 \cdot 99$ (inclusive of VAT) respectively. Six of the titles have been recorded in quadraphonic and these are available at no extra cost.
All the purchaser has to do is ask for a BASF Cassette Offer order form when he buys a BASF machine, tick the titles he wants and send the form with a cheque or postal order for the correct amount to BASF at its Knightsbridge, London, address. Customers may only send in one order form so they should ensure that they have all the titles they require.

## Heathkit Catalogue

 HEATHKIT

MANY interesting new models are introduced in the latest Heathkit Catalogue: They are TM-1626 Stereo Microphone Mixer; TA-1620 Public Address Control Amplifier with optional Booster Amplifier, Speaker Column, or Distribution Transformer; ID-1590E Digital Electronic Wind Speed and Direction Indicator; IM-1212 Digital Multimeter; IO-4560 DC-5MHz, 100 mV Oscilloscope; IO-4540 DC-5MHz, 20 mV Oscilloscope; IG-4505 Oscilloscope Calibrator; IP-2700 Series of Digital and Analogue Power Supplies; IMA-18-1 Solid-state Conversion Kit for valve-type Heathkit VVm's; SR-205 Single Pen Chart Recorder; SR-206 Dual Pen Chart Recorder.

Heath also tell us that their electronic organ (shown in October "Production Lines") is on show at the Tottenham Court Road showroom.

The latest Heathkit Catalogue is now available: To postal enquiries, enclosing a 10 p stamp for return postage, from: Heath (Gloucester) Ltd., Bristol Road, Gloucester GL2 6EE.

## "Radio Exchange"

D
UE to a printing error the above advertiser's full page advertisement in the September, 1975 issue was incorrectly priced. The magazine apologises for any inconvenience caused to readers.

## British 'Scope

THE only independent British oscilloscope manufacturers, Scopex Instruments, have just launched an addition to their range of low cost oscilloscope. The new 'scope, called the $4 \mathrm{~S}-6$, is intended for use in educational, service and amateur areas.

The new instrument follows the design philosophy of other machines in the range with emphasis on ease of use, with controls kept to a minimum and well labelled. Price is only $£ 88$ yet the specification is equivalent to similar units costing as much as twice that price. Main features are a maximum sentitivity of $10 \mathrm{mV} / \mathrm{cm}$ and a bandwidth of 6 MHz . The screen is a big $6 \times$ 8 cm for ease of viewing. The weight of the unit is only 4.5 kg making it eminently suitable for field work. One feature of the 4S-6 only found on oscilloscopes

costing about $£ 100$ more is the beam locate facility which allows even the most inept operator to locate and return the trace to screen.

For further information contact Scopex Instruments, Pixmore Industrial Estate, Pixmore Avenue, Letchworth, Herts.

## THE FUTURE OF AMATEUR RADIO

There are several forms of scientific activity in which the individual radio amateur can participate and play a valuable part. There is no other organisation in the world that can command the services of so many able technicians capable of carrying out specialist work at no cost to the community. As an example, we cite propagation research, possibly using the beacons already established in several parts of the world. Amateur progress in microwaves has astonished professional workers and this is a fertile field for experiment and development. The amateur satellite programme is another area where the skills of construction or mere observations can vitally assist research activity. In addition to participation in scientific activity the radio amateur must ensure that his transmissions are beyond repreach both in technical characteristics and in the messages conveyed. There are many listeners to amateur radio transmissions and the listener can only judge the quality by what he hears. Regrettably in many cases the quality leaves much to be desired.

The Radio Society of Great Britain* has always played a leading part in the representation of amateur radio at international levels. It is already heavily involved in the preparations for 1979 and will continue to make a maximum effort on behalf of all UK radio amateurs.
The future of amateur radio now depends upon the IARU, the national societies, the local clubs and, not least of all, the individual operator. Will you play an active and responsible part in the world wide activity intended to ensure the future of amateur radio?

LIONEL E. HOWES-Editor

* Radio Sociely of Great Britain, 35 Doughty Street, London, WCIN 2AE


# OISITRAL RERDCUT 

SYSTEM for Flll tuners PART 1 Martin Oliver*

directly to the line or neutral pin of the mains plug as it is then dangerous to connect external components to it and this circuit must not be used.

One problem which usually occurs, when building high frequency circuits is the need for special equipment, such as HF signal generators and oscilloscopes to set the circuit up. To get around this problem, broadband circuits are used in the HF sections of this design so there are no coils to be aligned, and the only equipment needed is a multimeter.
The unit is built on Veroboards contained in a separate metal case, and is connected to the tuner by coax cable. A metal box is needed as a screen between the tuner's sensitive front end and the logic ICs.

## FM TUNER OPERATION

Before explaining how the circuit works, a brief description of the operation of an FM tuner may be useful. Fig. 1 shows a simplified block diagram of a
*Formerly whth Texas Instruments.


Flg. 1: Block diagram of a typical FM tuner where the oscillator frequency is above that to which the RF amplifier is tuned.
"conventional" tuner. It is assumed to be tuned to a station on $100 \cdot 0 \mathrm{MHz}$. A signal picked up by the aerial is amplified by the RF amplifier to a level suitable for the mixer. The local oscillator runs at a frequency 10.7 MHz above or below the frequency to which the RF amplifier is tuned. The output from the mixer is the IF frequency which is the difference between these two signals, i.e. $10 \cdot 7 \mathrm{MHz}$. The mixer feeds the IF amplifier via a bandpass filter which gives the tuner its selectivity.

It is not possible to measure directly the frequency of the signal from the aerial because this consists of many other stations apart from the one being received. Because of this the local oscillator is used, but as this is not the same frequency as the station being received, a correction must be made in the counting circuit. In the example of Fig. $1,10 \cdot 7 \mathrm{MHz}$ must be subtracted from the measured frequency before it can be displayed.

Fig. 1 shows the local oscillator at a higher frequency than the RF amplifier. This is the more usual case, but if the oscillator was lower, i.e. $89 \cdot 3 \mathrm{MHz}$ then 10.7 would have to be added to the count.

## SYSTEM OPERATION

A block diagram of the complete system is shown in Fig. 2. The system operates by enabling a 'gate' for an accurately defined sampling period and counting the number of input cycles which occui during that time. TTL decade counters are used, but be-


Fig. 2 : Block diagram of the complete Digital Readout System.
cause the local oscillator frequency can be above 100 MHz it must be divided to a frequency which TTL can handle. This is done in the prescaler, which divides the input frequency by three. So if the local oscillator varied over the range 99 to 119 MHz the output of the prescaler would be between 33 and 40 MHz which is low enough for the TTL counters.

It is important that the local oscillator is not loaded by the circuit connected to it as this would reduce the output or shift the frequency. To avoid this a high input impedance buffer is used. This is the only part of the circuit which is mounted inside the tuner.

To give the correct display for the number of digits used, a counting period of $300 \mu \mathrm{~s}$ is needed. To get the required accuracy a crystal must be used, but to oscillate with a period of $300 \mu \mathrm{~s}$ it would be
very large and expensive. In this design a 400 kHz crystal is used followed by series of counters to divide the frequency by 120.

## IF OFFSET COMPENSATION

The adding or subtracting of the IF frequency is accomplished by using presettable decade counters, (one for each displayed digit).

To add $10 \cdot 7$ to the displayed frequency the counters are loaded with this number before counting starts. The output from the counters is in binary coded decimal ( BCD ) and the decoders convert this to drive the seven segment LED displays. Because the most significant digit (hundreds) can only be 0 or 1, a separate decoder is not needed. The counting and display sequence takes 4.8 ms as follows:
$\begin{array}{ll}\text { 1) Load counters with IF offset frequency } & 300 \mu \mathrm{~s} \\ \text { 2) } \\ \text { 3) Enable input gate to counters } & 300 \mu \mathrm{~s} \\ \text { 3) Display result } & 4.2 \mathrm{~ms}\end{array}$
3) Display result $\quad 4 \cdot 2 \mathrm{~ms}$ modulates the light output at about 200 Hz , but the eye cannot follow this, and the display appears steady.

## ELIMINATING JITTER

With counters of this type there is always an uncertainty of $\pm 1$ digit depending on the phase difference between the input and the sampling pulse. This normally causes the last digit to jitter, but when the last digit jitters between 9 and 0 the next digit is also affected. This is especially troublesome in this case as nearly all UK stations are on multiples of 100 kHz , so the fifth digit ( 10 kHz ) would normally be zero and the jitter would pass on to the next digit.
The problem is overcome by adding 50 kHz to the number which is loaded into the counter. Now, when a station is tuned in, the last digit reads five instead of zero, and the jitter is confined to this digit. Although it cannot be displayed as tens of kilohertz the last digit is used to indicate how accurately the station is tuned in. If the last digit is $3,4,5,6$ or 7 it is blanked. When it is 0,1 or 2 a minus sign is displayed and for 8 or 9 a plus sign appears. This arrangement eliminates flicker when a station is tuned in, and still gives sufficient accuracy.

## INPUT BUFFER

Fig. 3 shows the circuit of the input buffer. which is simply an emitter follower. This has the advantage of a low output impedance, which is needed to drive


## INPUT BUFFER

Resistors
$\left.\begin{array}{ll}\text { R1 } & 10 \mathrm{k} \Omega \\ \text { R2 } & 2 \cdot 2 \mathrm{k} \Omega \\ \text { R3 } & 560 \Omega\end{array}\right\}$ All $\pm 5 \% \pm W$

## Capacitors

$\begin{array}{ll}\text { C1 } & \frac{1}{2}-1 \mathrm{pF} \text { (see text) } \\ \text { C2, C3 } & \begin{array}{l}0.01\end{array} \mathrm{~F} \text { ceramic }\end{array}$
Transistor
Tr1 2 N918

## PRESCALER

Resistors (All $\pm 5 \% \frac{1}{2}$ W)

| R4 | $100 \Omega$ | R12 | $68 \Omega$ |
| :--- | :--- | :--- | :--- |
| R5 | $47 \Omega$ | R13 | $2.7 \mathrm{k} \Omega$ |
| R6 | $470 \Omega$ | R14 | $220 \Omega$ |
| R7 | $2 \cdot 7 \mathrm{k} \Omega$ | R15 | $1 \cdot 5 \mathrm{k} \Omega$ |
| R8 | $82 \Omega$ | R16 | $12 \mathrm{k} \Omega$ |
| R9 | $180 \Omega$ | R17 | $10 \mathrm{k} \Omega$ |
| R10 | $180 \Omega$ | R18 | $2 \cdot 2 \mathrm{k} \Omega$ |
| R11 | $68 \Omega$ | R19 | $220 \Omega$ |

VR1 $220 \Omega$ miniature preset
Capacitors
C4-C8 $\quad 0.01 \mu \mathrm{~F}$ ceramic ( 5 off )
C9 $\quad 20 \mathrm{pF}$ trimmer (DAU or similar)
C10 $\quad 0.01 \mu \mathrm{~F}$ ceramic
Semiconductors
Tr2-Tr4 2N918 (3 off)
ICl SN72733N Texas

## LOGIC BOARD AND DISPLAY

| Resistors |  |
| :--- | :--- |
| R20, R21 | $820 \Omega$ (2 off) |
| R22-R30 | $330 \Omega$ (9 off) |
| R31 | $680 \Omega$ |
| R32-R45 | $330 \Omega(14$ off) |
| R46 | $10 \Omega$ |
| All $\ddagger W \pm 5 \%$ |  |

## Capacitors

| C11 | $0.1 \mu \mathrm{~F}$ ceramic |
| :--- | :--- |
| C12 | 680 pF polystyrene |
| C13 | 470 pF polystyrene |
| C14-C20 | $0.1 \mu \mathrm{~F}$ ceramic ( 7 off) |

Semiconductors


## Crystal

X1 400 kHz (Channel 16, FT241-Interface Quartz Devices Ltd. 29 Market St., Crewkerne, Somerset. Tel. Crewkerne 2578).
the $75 \Omega$ coax lead connecting the tuner to the display circuit.

The input is taken from the local oscillator tuned circuit where the signal is about 1 V peak-to-peak. A very low value coupling capacitor Cl is used to reduce the loading at this point.

The 12 V supply can be taken from the tuner itself as the current drain is only 4 mA . If there is no convenient 12 V line in the tuner, then a separate wire can be taken from the 13 V line in the main unit.

The coax cable couples the buffered local oscillator signal to the prescaler.

## PRESCALER CIRCUIT

The basis of the prescaler is an SN72733 video amplifier (ICl in Fig. 4). This is biased as a Schmitt trigger by connecting the output to the non-inverting input via R13. This is then made to oscillate by the feedback provided by R15, R14 and C9, where C9 sets the frequency.


Fig. 4: Circuit diagram of the prescaler unit which uses the Texas SN72733N video amplifier IC.


The signal from the buffer is amplified and coupled to the 733 oscillator which locks to one-third of the local oscillator frequency. The trimmer, C9, is used to adjust the free running frequency to the centre of the band so that the 733 can be pulled higher or lower in frequency.
$\operatorname{Tr} 2$ and $\operatorname{Tr} 3$ are connected as a DC feedback pair which gives reasonable gain over a wide frequency range. The gain is adjustable with VRl to allow for variations in the amplitude of the local oscillator signal.

The other output of the 733 is fed to an emitter follower Tr 4 which provides a low impedance drive at the correct level for the TTL circuit.

## REFERENCE OSCILLATOR

Fig. 5 shows the circuit diagram of this section. The reference oscillator is made from SN7404 inverters which are biased into the linear region by resistors connected from output to input.

Two inverters are needed to give positive feedback. The frequency of 400 kHz is determined by the crystal X1. Capacitors C12 and C13 are needed to prevent the circuit oscillating at one of the crystal's harmonic frequencies.

TTL counters are used to reduce the reference frequency. IC4 is an SN7490A which contains divide by two and divide by five circuits. By connecting output QA to input $B$ it will divide the input frequency by 10 . IC5 contains a divide by two and a divide by eight circuit. To give the necessary output frequency this must divide by twelve which is


Fig. 6: Waveforms at various positions in Fig. 6.


Fig. 7: Circuit diagram of the Counting and Display Logic.

# UNIUNCTION + TRANSISTOR TESTER 

 R.MEREDITHTHE unijunction transistor tester described here is basically a simple go/no-go tester, giving some indication of the intrinsic stand-off ratio. The total cost of components is about 80 p, provided a multimeter with a suitable range is available.

## Unijunction Theory

To understand the operation of this instrument, a certain basic knowledge of unijunction theory is necessary. A unijunction consists of a bar of N type silicon with contacts at each end. On this bar there is a $P-N$ junction. When a voltage $V$ is applied across the Bar, a voltage which is less than $V$ appears at $A$. The voltage at $A$ is found by multiplying V by $\frac{\mathrm{d} 1}{\mathrm{~d} 2}$ When the emitter voltage rises above that at A by about $0 \cdot 7 \mathrm{~V}$, current begins to flow through the now forward-biased P-N junction. This reduces the voltage at $A$, so that the current continues until the voltage at the emitter falls below $0 \cdot 7 \mathrm{~V}$. The ratio $\frac{\mathrm{d} 1}{\mathrm{~d} 2}$ is the Intrinsic Stand-Off Ratio.


Theoretical circuit of a unijunction transistor with external biasing supplles. In this example, electrons will flow from the emitter, as the potential across base 1 and 2 is greater than that across the emitter and base 2.

## Practical Circuit

The device described in this article works as follows: Cl charges through Rl until the voltage at the emitter rises 0.7 V above the ISR $\times 4 \cdot 7$. This figure being the voltage between the bases, kept constant by the zener Dl. At this moment the device starts to conduct and the capacitor Cl is rapidly
discharged. The cycle now repeats.
Trl performs two functions. First, it increases the resistance of the meter by a factor equal to its $\mathrm{h}_{\mathrm{fe}}$, and secondly, it removes by reason of its base/ emitter drop of 0.7 V , the drop of the unijunction when it fires, giving true representation of the ISR.


Circuit of the Unijunction tester, making use of an external meter. If the circuit is to be constructed whth an integral meter, then one of about $100 \mu$ A FSD should be chosen.

## Construction

Although details are given for the PCB, layout is not at all critical and comprises only six components. A high gain transistor should be used for Tr such as the BC109, as the input impedance should be as high as possible. For the same reason, the meter should have a movement of around $100 \mu \mathrm{~A}$, or if

## $\star$ components list


a suitable multimeter is available, then this could be used in place of a permanent meter. The value of R3 can be calculated as follows:
$R 3=\frac{4 \cdot 7}{\text { Sensitivity for } \mathrm{fs} \text { on meter }}-$ Meter resistance
A $5 \%$ resistor should be used here, as no advantage will be gained by the use of a more accurate one, especially as the diode itself is of $5 \%$ tolerance. The PCB was fixed inside a small aluminium box with sockets for the meter.
$50 \times 40 \mathrm{~mm}(0.1$ inch veroboard)


Component layout can be constructed on veroboard as shown above, or on a PCB. As components only number six, layout is not at all critical.

## Use

Switch on and plug a unijunction transistor into the socket. The needle on the meter wlil move slowly across the scale, until at one point, the needle should flip back to near zero. If the meter is scaled 0 to 1 linearly, the ISR will be given by the maximum reading on the meter scale. If however, the voltage continues to rise, or does not rise at all. the unijunction is faulty.

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FM ,TUNER DIGITAL READOUT—contd from page 556 achieved by resetting to zero on the twelfth input pulse. IC3a does this by feeding a positive pulse to the reset inputs when outputs QC and QD go high. The output from QD has a period of 300 as which is the correct width for the sampling pulse.

IC6 is also an SN7493N and is used to generate timing pulses for the counting and display logic. It counts up to 16 and then resets to zero and outputs 15 and 16 are selected by the two nand gates IC7a and b. The output at 15 (A in Fig. 5) loads the presettable counters with the IF offset, and the pulse at 16 gates the prescaler output into these counters. The output of IC3b is used to blank the displays. These pulses are shown in Fig. 6.

## COUNTING AND DISPLAY LOGIC

The circuit is shown in Fig. 7. ICs 8 to 11 are the decade counters which are cascaded by feeding the QD output to next clock input. Also QA is connected to CK2 of each counter to cascade the two halves of each IC. The most significant digit ( 100 MHz ) can only be 0 or 1 so a decade counter is not needed.

The data inputs A-D are either connected to ground or +5 V depending on the value of the IF offset. This is loaded into the counters when the count/load inputs are low. The counter outputs are in BCD form so decoder/driver ICs are used to drive the seven-segment LED displays (IC13, 14 and 15). These provide high current output to drive LEDs, and blanking can be achieved by putting a logic low on the $R B O$ pins. The $330 \Omega$ resistors between the decoders and the displays determine the LED current, and R31 sets the current for the decimal point. For LED1 ( + or - indicator) a different circuit is used. The arrangement of IC12a, 12b and 2 e illuminates the horizontal bar of LED1 when the output of IC8 is $0,1,2,8$ or 9 . The vertical bar is also illuminated when the count is 8 or 9 due to IC12c. If the count is $3,4,5,6$ or 7 neither bar is on and the display is blanked. LED5 only displays 1 if QD of ICll is low. If the count is 80 or 90 MHz then QD is high and LED5 is blanked. The display blanking pulse B is also applied to IC12c and IC3d to blank LED1 and 5 during counting.

The capacitors C14-20 are to decouple the power supply. This is important because of the high edge speeds of the counting logic.

In Part 2 the power supply circuit is described and construction details and setting up procedure are given.

## OUR "CQ" COLUMN

On page 603 of this issue, we have some $C Q$ requests for back-numbers. Please help us to help you, if you want a "CQ" published, and you can do that by following the style on page 603 when you write to us. Please keep CQ's as short as possible.

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## POWER

0N reading past Ginsberg articles it seems that the small, minute marvels have hogged the limelight, probably because they really are remarkable achievements. However, to redress the balance let us take a look at something a shade bigger. It concerns power, and the laser. The generation of power is a problem. Solar cells, wind-driven generators, mirrors which focus the sun's rays have all featured in the news.
Now it just so happens that if you take a very small amount of a material and compress it sufficiently it may just be possible to arrange pressures and densities high enough to support fusion-when lighter atoms get together to form heavy ones and when they do, they give off energy which might be harnessed.
Experts claim that a tiny pellet of deuterium and tritium can, with the aid of a quick pulse from a 1 MJ (one mega-joule) laser, be compressed by a factor of up to 10,000 .

Another approach finds workers constructing a kind of ring arrangement in which electron beams are individually concentrated on a single pellet of material in the centre. Certainly on the drawing board stage (at least) is such a beasty which treats said pellet to a burst of electron beams whose total combined power amounts to some $2 \frac{1}{2}$ trillion Watts (that's $2.5 \times 10^{12}$ Watts).

Just to complete the story, capacitors are used as a means of storing energy for the system. Two banks are employed and each consists of 38 , $60 \mathrm{kV}, 1 \cdot 85 \mu \mathrm{~F}$ capacitors. Oil dielectric transmission lines are employed and these are housed in a tank of transformer oil-40,000 gallons of it!

A final piece of news on the subject is that one particular machine under development produces a 10 ns pulse of 40 trillion Watts.

## 27 MHz

If you've ever tuned a radio receiver to around 27 MHz you may well have picked up a weird cacophony of callsigns and titles not to mention some very strange conversations. Almost certainly you will have been listening in to conversations on the American "Citizens Band". Although power is (in theory) limited, no formal exams are required in order that one might
transmit. Note; this is in America and does NOT apply in the UK.

While the Citizens Band has been a source of debate for some time, a new idea has surfaced and looks like being a 'winner'. The thought is that a particular frequency or channel within the Citizens Band should be an emergency channel. This allows anybody and everybody to have a Citizens Band hand-held transceiver (walkie talkie) in, say, their car. Any accident could be immediately reported and a request for assistance would be almost instantaneous. One voluntary network has already sprouted up in Ohio and others could follow.

It occurs to me that old people living alone could easily have immediate access to help from the outside world. Mountain climbers etc. could also find the system of use. It is almost certain that the scheme would not be permitted in the UK due mainly to the stringent Post Office/Home Office regulations concerning the radiation of energy, a point on which they are quite fussy to say the least. Quick, check the radiation from the local oscillator of your broadcast receiver. And what about those TV timebases?
Speaking of TV reminds me that the central research laboratory of Japanese giant Hitachi has been working on a video disc player using the optical approach. Some half hour recording of colour pictures and sound has been recorded on a 12 in . disc. Luminance, chrominance and sound are contained in the 54,000 holograms on the disc each hologram being only one millimetre in diameter. So densely is the information stored that the disc needs to rotate at only $6 \mathrm{r} . \mathrm{p} . \mathrm{m}$. It is interesting to note that in systems employed by two other major manufacturers, the discs rotate at 1,800 r.p.m.

## BLIMPS ARE COMING

Look out-the Blimps are coming. They may sound like a second class $\operatorname{limp}$ but in reality they are huge balloons which are floated up to a certain altitude (around $10,000 \mathrm{ft}$.) and then tethered. The Blimps have with them a large antenna and transceiving equipment. The idea is that it's cheaper to have a balloon that it is to have a satellite in order to transmit and receive information over greater
distances, particularly at the very high frequencies. No, it's not hot air, even the American military is increasing its interest in balloon borne radar. Makes you wonder about Amateur radio Hams' reaction. Perhaps Lisle Street will soon be selling Ex. Govt. barrage balloons. What better for portable stations-with a high wind it could get them off to a good start and raise them in the eyes of others!

## RAZOR-SHARP TIME-KEEPING

News from abroad informs that there's a newcomer on the digital watch scene-Gillette, the company of razor fame. A research and development agreement has been signed between Gillette and some American electronics companies for carrying out investigations in the field of quartz modules for digital watches.

## "MESFETS"

Another newcomer, this time to the semiconductor scene, is a device called the MESFET. Adding another $S$ after the first would be a fair word for some early Ginsberg experiments with FETS! For the technically oriented, these devices are described as Schottky-barrier field-effect transistors. Efficiencies of $68 \%$ at 4 GHz and over $40 \%$ at 8 GHz have been claimed so clearly they're not just a pretty face. I hope to have more information shortly on these devices.

## "SAWS"

When one talks about crystal oscillators it's usually about a bulk crystal-a chunk of crystal between two supports. Generally, the higher the frequency, the smaller (and often thinner) the piece of crystal is. There is a limit to how small and fragile one can make a crystal of this kind which is why fundamental frequencies are commonly no higher than 25 MHz .
Marconi Research Laboratory has developed the SAW (surface acoustic wave) technology to a point where it can manufacture a compact and rugged crystal oscillator with a fundamental frequency of $1 \cdot 2 \mathrm{GHz}$.

## Cimblers

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## Anpone help ?

M
R. H. F. Mayman of 59 Delamere Street, Crewe, Cheshire has recently come across this interesting receiver, complete with speaker, and wonders if any other readers can help him with more information.


Apparently, the set was purchased in Crewe many years ago. It carries only a dealer's name and no details of a manufacturer. Valves are $2 \times$ PM2 and $1 \times$ PM1LF. The loudspeaker is simply marked "Blue Spot."

## 路解 hooks

ADAM Hilger Limited, publishers, 29 King Street, London, WC2E 8JH, have recently announced the first three volumes of a set of books entitled "The Story of Radio" by W. M. Dalton, Ch.Eng., M.I.E.R.E.

Volume 1 "How Radio Began" covers the basics from early experiments with electricity and magnetism. An interesting chapter on Wireless Telegraphy describes experiments and discoveries by such pioneers as Clark

Maxwell, Hertz and Marconi. A chapter headed The Thermionic Valve contains items on the Edison Effect, Audion Tube, and early valve circuits.

Vol. 2, "Everyone an Amateur" begins the story after World War 1 ; and contains sections on the British Broadcasting Company and the Rediscovery of Short Waves.
It tells how during the early years of peace after the First World War, the seepage of official information and the knowledge of wartime developments brought home by ex-service men led to an enthusiasm for radio fostered almost entirely by amateurs. They built their own transmitting stations and receivers, compelled Governments to provide public broadcasting services, and eventually astounded the world by their unaided achievements in long distance low-power short-wave communication. This second volume of Mr . Dalton's comprehensive history pays tribute to these devoted pioneers and, in recounting the birth-pangs of the British Broadcasting Company, tells how Everyman carried on building his own receiver in a oraze from which, Mr. Dalton has said, 'a few of us never quite recovered.'

Vol. 3, "The World Starts to Listen" takes the story a little further: by the mid-twenties, the early amateurs were ready to turn professional, the world was ready to buy their sets. The B.B.C. had become a Corporation -and respectable-and people had started to listen to its programmes in preference to twiddling dials in a search for distant stations; and so the quality of broadcast sound improved. Valves were already being applied in many other fields, but they were still battery operated. Mr. Dalton
thus continues his step-by-step story of the development of radio.

These books are very interesting but also very expensive, for they are priced at $£ 4 \cdot 50$ each volume. It's a pity because I feel that this is a text which has been needed for a long time now. Still, with inflation roaring ahead $£ 4 \cdot 50$ will be the price of half a dozen resistors soon so . . .

## Cassette Thistory

SOME while ago I gave mention to the double LP set that the BBC issued to mark 50 years of broadcasting. Well, now they've issued the complete recording on cassette. It's entitled "BBC 1922-1972, 50 Years' of Broadcasting", and comes as a double-play cassette No. HRMC 050.

The tracks are produced by Alan Burgess and narrated by


Rene Cutforth and endeavour to recapture in a hundred minutes many great occasions at home and abroad and people whose voices became known through the medium of 50 years of BBC Radio. Broadcasting pioneers such as Lord Reith and Peter Eckersley can be heard as well as the first Christmas broadcast by King George $V$ and historic broadcasts by famous wartime announcers. The tape also reflects musical events over the years from Twenties syncopation to The Beatles. Please don't try to obtain it from the BBC because they don't have a sales department for records and cassettes, but contact your local record shop. They're sure to be able to get one for you.

. . . . at least, to Home Radio Components you are. I'm thinking of their Credit Account Service. They have of course always run accounts for supplying firms, colleges and Government Departments, but for years it was impractical to provide the same facilities for individuals. However, Home Radio Components have always looked upon their smallest customers just as important as their biggest, and after much thought and planning they devised a Deposit Credit Account matched to the needs of the small individual buyer.
The service is very convenient in many ways. For instance, thanks to their answerphone service exclusively for the use of Credit Account customers, you can take advantage of the cheap phone rates after 6 pm week-nights and any time Saturday and Sunday. You not only save money, but you can often get your components much quicker. Briefly, the Credit Account Service works like this-you pay a deposit (you choose the amount) and you immediately get credit
for double that amount. Home Radio then send you special order forms and pre-paid envelopes, and advise you each month how much you have spent. You save quite a bit on postage costs, and having to draw only one cheque or P.O. a month makes quite a worthwhile additional saving. No wonder nearly 1000 customers are already using this service. Why not join them and save yourself money and frustration? First you will need the Home Radio Components catalogue. No constructor should be without one! For a book having 240 pages, listing about 6000 components, illustrating nearly 2000, the price of 85 p is modest indeed. True, postage and packing adds another 33 p , but every catalogue contains vouchers to the value of 70 p when used against orders.
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## ANTI-BREAKTHROUGH TRAP

Aparallel tuned wavetrap can greatly reduce an interfering signal due to second channel or where intermediate frequency breakthrough is troublesome. The circuit uses a Denco Blue Range 3 coil and the trap is constructed in the maker's aluminium can provided. The 350 pF capacitor is for 1.6 MHz IF's, but the coil will tune 1500 kHz to 6 MHz with a trimmer capacitor of 500 pF max. A Blue Range 2 is required for the MW band.


Adjustment of the core in the coil will also extend the range over which the trap will tune. For best rejection of an unwanted signal aim for minimum capacity and maximum inductance (core within the coil), provided the trap still shows a sharp point of rejection.
The trap must be connected as close as possible to the receivers aerial and earth terminals if it is to be effective.

## 'Q'-MULTIPLIER

Acircurr having a high " $Q$ " tunes more sharply, and is thus more selective, than one with a lower " $Q$ ". The " $Q$ "-multiplier uses a regenerative stage to enhance the " $Q$ " of a coil tuned to the receiver's intermediate frequency.
Potentiometer VR1 controls regeneration but the circuit should not be allowed to oscillate. Variable capacitor VCl allows the multiplier frequency to be moved across the receiver's $1 F$ passband. In use a " Q "-multiplier is sometimes considered difficult to adjust which probably explains why it is not used more often, but, properly set up, it affords a very economic way of providing a substantial increase in IF selectivity.

The output coupling capacitor is connected to the primary of the first IFT of the receiver, to the "hot"
end of the coil and not a tapping. The multiplier should be placed as near as possible to this IFT. The coil core is set so that it tunes to the receiver's IF, around 465 kHz , with VCl half way in. Realignment of the particular IFT may be needed on some sets. Potentiometer VR1 is set so that the multiplier is almost oscillating, equivalent to the point of maximum selectivity.


If a particular transistor does not oscillate smoothly reduce the battery voltage or include a resistor of between $100 \Omega$ and $1 \mathrm{k} \Omega$ in series with the switch. The unit can be built in a metal box external to the receiver but the output lead must then be coaxial cable, as short as possible, with the outer screen earthed. The output capacitor should now be placed at the IFT in the receiver.

## EXTERNAL AERIAL COUPLING

AN external aerial will considerably increase the range of a portable type radio or allow it to be used in circumstances where the internal ferrite rod aerial is unsuitable, such as in a vehicle where the bodywork acts as a screen.

The external aerial is connected to a coupling coil added to the ferrite rod. The winding should be about 35 turns of 36SWG insulated copper wire but neither the number of turns nor the wire gauge are at all important. "Earth" in the circuit is the chassis of the receiver.

A short coaxial cable should be used to connect the external aerial to the receiver in a vehicle, to reduce electrical interference. But do not use screened cable as part of the aerial when the aerial is being added to increase range.

A capacitor Cl can be used as an alternative to

the coupling coil but its value must be kept low or it will detune the receiver's aerial circuit. A trimmer capacitor of a maximum value of about 15 pF can be tried. If the receiver has an aerial circuit trimmer control this can be used to maintain correct tuning when an external aerial is connected via Cl.

## 9V FROM 12V

IF a 9 V battery-operated receiver is frequently used in a vehicle it is more economical to use the vehicle's 12 V battery than to replace the dry batteries. With the zener diode the output voltage is substantially constant despite the changes in current drawn by the radio.


Capacitor C 1 should be as large a value as possible with $1000 \mu \mathrm{~F}$ as a minimum. The 12 V supply can be found at several places in a vehicle but choose one that gives a minimum of electrical noise in the receiver. If the parts are fitted in a box with dry battery terminals on the outside no changes need be made to the receiver which can be plugged in at any time. The terminals can be taken from the top of a defunct battery but be careful to observe the correct polarity.

## HEADPHONE SOCKET

THIS simple modification involves fitting a suitable socket to a receiver to take a headset or earpiece. The circuit is arranged so that the speaker is cut out when the headset is plugged in to the socket. If the receiver's speaker is around 15 to $80 \Omega$ the usual low impedance headset will function without any trouble. If the output impedance is low, $3 \Omega$ or so, the load can be maintained by wiring a resistance or say $3 \cdot 3 \Omega$ across the headset, It can be fitted inside the headset plug in some cases.

The socket should be suitable for the headphone plug, normally 2.5 mm or 3.5 mm or $1_{4}$ in. in diameter,

but there is no reason why different sizes should not be connected in parallel to accommodate different headsets or earpieces.

This modification must NOT be made to TV equipment, where the chassis is generally alive.

## NOISE LIMITER

This small unit prevents sudden and uncomfortable bursts of noise or signal reaching the speaker or headset. It is particularly effective when the receiver is being operated at maximum gain on a weak signal. The diodes, which must be germanium types, shunt strong signals but leave weak signals unaffected.

Values shown are for output circuits of around 15 to $80 \Omega$, but for higher values increase R1 to suit. If a lower impedance load must be maintained, wire a suitable value resistor, such as 3 or $8 \Omega$, across the unit's input, shown dotted.


Headphones of $2 \mathrm{k} \Omega$ impedance or higher are best for this particular circuit when the limiting voltage is comparatively low. The single cells can be replaced with resistors of about $5 \cdot 6 \Omega$ with only a slight loss of limiting action. In this case no switches are needed. The components can be fitted into a small box with a lead and plug at one end and socket at the other. Alternatively the limiter can be wired round the receiver's output socket or terminals.

## TOP CUT TONE CONTROL

This simple circuit may seem hardly worth a mention but in fact it is very effective at reducing the level of whistles caused by adjacent or second channel interference. It will also help to compensate for the deficiencies of small speakers notorious for their effectiveness at the top of the audio range!

The capacitor should be $0 \cdot 1 \mu \mathrm{~F}$ or $0 \cdot 25 \mu \mathrm{~F}$ with a

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$5 \mathrm{k} \Omega$ potentiometer for VR1 in the case of transistorised receivers, and $0.02 \mu \mathrm{~F}$ to $0.05 \mu \mathrm{~F}$ with $25 \mathrm{k} \Omega$ to $50 \mathrm{k} \Omega$ for VRl for high impedance circuits, such as are found in valved receivers. The connection is made to the top of the audio gain control but a tone control of this type must not be used in that part of a receiver in which negative feedback is already incorporated.

## BANDSPREADING

Bandspreading is very effective at alleviating the critical tuning that is often experienced on the short wave bands. In a simple superhet receiver the aerial and oscillator circuits are tuned by a twogang variable capacitor VC1/VC2. Simple bandspreading consists of adding a small value variable capacitor VC3 in parallel with the oscillator section VC2. VC3 is typically 5 pF , mounted at a convenient point on the front panel and fitted with a slowmotion drive.


A capacitor similar to VC3, and ganged with it, can be connected in parallel with VCl to maintain alignment of the aerial circuit but problems of tracking arise, especially if the receiver is bandswitched, so VC3 alone is advised.

The degree of bandspreading achieved by VC3 will depend on the frequency involved and the ratio of VC3 to the value of VC2 at any point on the dial. At low frequencies VC3 can be increased to 15 or 25pF.

## 9V DC MAINS UNIT

THIS circuit will provide 9 V DC to replace the batteries in transistor radios and similar equipment. A transformer with a secondary of 9-0-9V at 100 mA should be sufficient for most purposes. The silicon diodes should have a minimum PIV rating of 50 V . Those in the 1 N 4000 range are suitable.

Output voltage will depend to some extent on the current drawn by the external load but small
variations are not usually of much importance with the average receiver. A zener diode could be added to stabilise the output voltage at a particular value.


The core of the transformer should be earthed, as well as the secondary centre tap, and a fuse in the mains supply is highly desirable. If the mains hum level is objectionable, in spite of the large value of smoothing capacitors used in this circuit, try fitting two capacitors, in parallel across the mains input, between fuse and transformer primary. The junction of these diodes should then be taken down to earth. The capacitors should be about $0 \cdot 1 \mu \mathrm{~F}$ each rated at NOT LESS than 750 V working. Ensure the unit is disconnected from the mains before trying out this modification.

If an output of opposite polarity is required then reverse the diodes and the electrolytic capacitors.


READERS who have followed me so far will remember that we have replaced the ceramic pickup with a magnetic one (at the same time, of course, taking out any tone compensating components such as resistors in series or parallel with the pickup), constructed and fitted a preamplifier with its own power pack and have dealt with the problem of mains hum induced into the windings of the magnetic cartridge.

The result is very greatly improved reproduction of gramophone records over the treble range but distressingly "boomy" bass. This poor quality in the bass region is almost sure to be due to shortcomings in the design and construction of the loudspeakers but, before starting on this problem, it is probable that some tidying up is necessary on the work already done.

The first point is in the form of a warning; some makes of integrated circuit used in the preamp are very noisy in operation and for this reason I do not advise buying unknown makes over the counter on the assurance that they are "just as good"-they may be, but it is expensive to find out that they are not. Buy any of the well-known makes and be safe!

## 'TIZZY' SOUND

After playing several records on my own budget stereo after modification, I became aware of a "tizzy" sound whenever I touched the pickup arm, and, at the same time, I noticed an alarming increase in the pops and bangs whenever our refrigerator or central heating cut in or out. Since this followed the work I had done, it seemed very sensible to examine very closely the earthing arrangements on the input side of the new preamplifiers. In the original arrangement with the ceramic cartridge, the braided earth sleeve of the cartridge leads terminated on a tagboard on the underside of the Garrard deck and from this point another screened lead took over and fed the signal to the first stage of the main amplifier. This is the usual arrangement and is normally perfectly satisfactory. However when the additional amplifier is added with its high gain it may not be, and it certainly was not in the case of my own set-up!
I found it necessary to connect the braid at the tagboard direct to the record deck, which is itself connected direct to chassis by a separate lead from the motor terminal board. This, of course, gives a perfect "hum loop" situation but in this case it did not produce any hum. So that is how I have left it but I feel fairly sure that this will not be the solution in all cases and it may be found necessary to carry out a good deal of patient work on the earth-
ing arrangements before a satisfactory solution is found. However, in my case the live condition of the pickup arm was completely overcome and the pops and bangs reduced to minor proportions

I had to do a lot more work to remove this annoying impulse interference altogether. This applies to a great deal of audio equipment and has been covered in many articles and books. I will not repeat it in this article but content myself by saying that you will probably use quite a few $0.01 \mu \mathrm{~F}$ capacitors before you eliminate it completely!

## IMPROVING THE LOUDSPEAKERS

The obvious and major criticism of the sound quality from the system so far is loud resonant onenote bass. Any hi-fi expert will tell you that anything on the price of a loudspeaker over £30 has been spent on improving the sound below 50 Hz . As our purpose is to spend as little money as possible, it is quite obvious some compromise is essential.

When you remove the back from the budget loudspeaker, do not expect to find much sophistication, it is likely to be basic though fundamentally good value. In my own case, the speaker cabinets were approximately $18 \times 13^{1}{ }_{2} \times 7^{1}{ }_{4} \mathrm{in}$. deep. This is rather larger than the average and gives a cubic capacity of about $1760 \mathrm{in} .^{3}$, very suitable for an 8 in . speaker when the cabinet is totally enclosed. Inside were two units, an 8 in . general-purpose speaker and a cone tweeter. Neither unit was very robustly constructed. The tweeter was fed by a $4 \mu \mathrm{~F}$ electrolytic capacitor, there being no crossover unit apart from this.

The inside of the cabinet was bare wood but the cabinet back was lined with a thick covering of foam plastic. The only surprise was a 2 in. diameter hole in the front (in addition of course to those for the speakers) through which I assume the bass from inside the cabinet joined that from outside, hopefully in phase, thereby increasing the acoustic efficiency considerably in the lower region. With this arrangement it is not surprising that the modest rated 6 W of audio was enough for the noisiest of teenage parties!

## AIR TIGHT

The enclosures were constructed from chipboard and close examination of the edges at the back showed a lot of gaps which suggested to me that the quality of board left a good deal to be desired from a hi-fi point of view. Nevertheless, the general construction was solid enough and the backs fitted

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tightly and securely. The result of all this examination immediately explained the loud and poor quality bass since the cones of the two 8in. speakers had no mechanical damping at all and, once set in motion by a low frequency signal, were free to carry on moving at their resonant frequency for an appreciable time after the signal had stopped.

The only and rather obvious answer to the problem was to set about making the cabinets enclosures in the proper meaning of the word, that is to say, make them as air-tight as possible so that the cone movements would be restricted by air pressure. This is, of course, the principle of the "infinite baffle" and most of the smaller good quality speakers are designed on this principle. The first job therefore was to block the unused hole in the cabinet front with a piece of good quality chipboard or 5 -ply which was glued and screwed into position.


Fig. 1: Circuit details of the cross-over unit. Care should be taken in the winding of the coils, to ensure that the units for both channels are exactly the same.

## CROSSOVER UNITS

The first major item of expenditure is a pair of crossover units which I believe are essential. The actual crossover frequency in this application is not critical and anything in the region of 3 kHz will be suitable. Shopping around will most likely find a pair for less than $£ 5$ but for those who prefer to make their own, and do not mind tedious coil winding, Fig. 1 gives constructional and wiring details. Care must be exercised in connecting these to ensure that both follow the same wiring pattern so that problems do not arise later in getting both loudspeaker systems to operate in phase. Most speaker units have one tag marked with a red dot and if this is connected through the crossover unit to the live speaker lead in both cases, all will be well.

The next job was to line the interior of both cabinets with some soft sound-absorbing material. A good look around the household will usually reveal something suitable which will avoid dipping into the pocketbook. I found some surplus carpet underfelt of the rubberised variety and this is very suitable. Avoid very thick and heavy materials for, although they absorb sound, they also tend to reduce the effective cabinet volume which is undesirable. The material is fixed in place with small tacks and a little glue in strategic places. The photograph shows the interior of one cabinet after this treatment with the crossover unit in position. This photo also shows two other items not yet dealt with. Fixed to the back is a $50 \Omega$ wirewound potentiometer and the cone tweeter has been replaced by a superior dome type.

After completing the work and testing for several weeks, although the results were very pleasing, I
decided to extend the frequency response in an upward direction and to improve sound dispersion and thus the stereo effect. To do this I bought a pair of good quality dome tweeters (about $£ 6$ each). This certainly had the desired effect but I found that the new tweeters were very efficient and, since all the work I had done had tended to reduce the efficiency of the 8in. speakers, the overall effect was out of balance and the tweeters tended to predominate. For this reason, the $50 \Omega 3 \mathrm{~W}$ potentiometers are fitted and they are, in effect, volume controls for the tweeters enabling the required balance to be obtained while playing programme material, Fig. 2.

## VACANT SPACES

The last job in improving the speakers is to fill in the vacant spaces around the speaker units with more sound-absorbing material. For this, underfelt and similar material is not suitable as it is much too dense. The recommended material is BAF wadding which can be bought from most hi-fi shops for about 80p per sq. yd. I experimented with ordinary domestic cotton wool and found it very effective in this application, readily available in rolls about 12 in . wide. It should be very carefully unrolled without teasing it out and then cut to suitable lengths. For my cabinets I inserted two pieces, 18in. long very loosely rolled, each side of the 8in. units. A shorter piece similarly rolled fills the spaces above the big speakers and behind the tweeters. The object is to replace some of the air in the enclosure with the wool but not to introduce a solid substance which would effectively reduce the enclosure capacity. For larger or smaller cabinets the actual quantity of BAF wadding or wool must be found by trial and error, too much will have the effect of killing the bass response but the correct amount removes all traces of any unpleasant "boxy" tone.

We are now at the stage where we can replace the backs on to the enclosures and our aim is to make them airtight so as to put a brake on those bouncing cones, so the backs must fit well and be screwed down tight. Pay particular attentior to the holes through which the leads are taken as it may be necessary to fill these with putty or some similar substance in order to avoid large air leaks.

By the way, when I say "airtight" I do not mean this too literally! There has to be some escape of pressure or the cones would never be able to move at all. So some leakage is essential and this is almost certain to take place through the gap between the speech coil and polepiece and it is also doubtful if the cone suspension is completely airtight in units of this quality. So in making the enclosure and its


Fig. 2: $50 \Omega 3 W$ potentlometer shown In-circult, to prov/de some control over the tweeters.


Interior view of the speaker enclosure, showing the rubberised carpet underlay fixed in position. The vacant space should now be fllled with BAF wadding.
back as airtight as possible you are very unlikely to overdo it.

The two enclosures (we are fully entitled to call them that) can now be tested out on a signal. It will be obvious that the efficiency has been reduced in the middle and bass areas so the volume control will be further advanced than before this work was done. But the quality of sound should be immensely improved. The bass in particular will be "tight" and musical and it should be possible to advance the bass boost much further than before whilst still maintaining good tonal balance and really pleasant quality.

I believe the foregoing lines of attack will apply with great benefit to almost all budget loudspeakers. It is necessary before starting any work to assess very carefully the shortcomings of the speakers as supplied and to decide what improvements are required and then to examine the interior of the cabinets and the unit or units to decide what work is likely to be most beneficial. This will always reveal problems in the bass area no matter what else and the first answer to this is always cone damping. This inspection must also cover close examination of the cabinets themselves; if the construction seems weak and they sound hollow when tapped with a metal object, it may be necessary to fit wood struts in strategic places to make sure they will not rattle or resonate of their own acoord.

## FITTING A TUNING METER

Few budget stereos run to a tuning meter, but they nearly all have an AFC circuit which is intended automatically to adjust for any minor tuning errors and to correct any tendency to drift in the RF oscillator. A reliable tuning indicator which shows
when the tuning point of minimum distortion and minimum background noise is found is almost essential to anyone who takes his music seriously.

The circuit arrangements for a meter which peaks at the exact tuning point are very simple. A moving coil meter with FSD of about $100 \mu \mathrm{~A}$ connected with about 30 to $40 \mathrm{k} \Omega$ in series is connected across the large electrolytic in the discriminator circuit. These meters are expensive to buy especially if you want to pick one that fits nicely with the styling of your system. I had a very elegant meter which exactly suited the styling of my unit audio but it required $\operatorname{lmA}$ for FSD. We cannot use such a meter across the discriminator as it has an internal resistance of only $50 \Omega$ or so. The answer is to arrange the meter to be in circuit only when tuning and to remove it while we are listening.

One way is to fit a small press-button switch which brings the meter into circuit when made but disconnects it when open. This button is pressed when changing stations, the tuning adjusted until the meter peaks and the button then released, restoring the circuit to normal.

## SPACE CONTACTS

Examination of the AFC switch revealed a pair of unused contacts. The usual arrangement is a simple make-and-break single pole switch which joins the AFC line to chassis when it is disabled but since manufacturers of budget stereo seldom design special switches for such a simple function it is very likely that you will find at least one pair of unused contacts which can be used to switch the meter in and out. The position then is that we disable the AFC when we want to tune and then tune for peak reading on the meter. After this we return to the AFC position, leaving the AFC diode to take care of any oscillator drift, the meter remaining out of circuit until we want to change stations.


The photograph above shows the meter fitted on my budget stereo alongside the AFC switch which controls it. It works extremely well and I get dead accurate tuning every time. I had to experiment with various values of resistance in series with the meter and finally fixed on $6.8 \mathrm{k} \Omega$ which gives between half and three-quarter scale reading on an $800_{\mu} \mathrm{V}$ signal at my aerial. By a slight circuit modifi-
continued on page 604

## oet the

 partru going!

## with our PW 'Ecsubauld'

$$
\begin{aligned}
& \text { STEREO BISCO SUSTEM } \\
& \text { (100+100W) }
\end{aligned}
$$

This high-power stereo disco plus light show, has been designed for the home constructor who requires the home constructor who reguires in both sound and looks Specitications include a THD of $0.1 \%$ at 60 W and the latest BSR belt drive turntable units. Mixing facilities provide crossfade and mic. plus aux. inputs.
The light show, which comprises three colours, operates on the sound to light principle.


## PRAGTIGAL自ililiss

THE transmitted sound quality of television is inherently very high, but due to severe limitations in the audio side of domestic TV receivers, it is rarely heard at its best. This article describes a high performance TV Sound Tuner for feeding into a hi-fi system or tape recorder, enabling full benefit to be gained from the broadcast.

Up-to-date techniques have been used to provide push button varicap tuning and high sensitivity. Three integrated circuits are used and a ceramic filter with quadrature detector ensures easy setting up without instruments.

## TV SYSTEM

Television in Britain is transmitted on 625 lines with a line rate of 15.625 kHz and 50 Hz field rate. The video is transmitted as amplitude modulation of an RF carrier, while the sound channel is broadcast as frequency modulation of a sound carrier spaced 6 MHz from the vision carrier. Fig. 1 shows a block diagram of the sound section of a TV receiver.

In all frequency changing operations in the receiver the sound carrier remains spaced 6 MHz from the video. After final video detection the result at the output of the video detector is video and a 6 MHz FM sound carrier, the vision carrier having been transferred to zero frequency. The audio is simply recovered from the FM carrier by frequency discrimination, using a conventional discriminator or the more recent "quadrature" detector.

## CIRCUIT DESCRIPTION

The pre-assembled and aligned IF sub-assembly used in this project performs the function of IF amplifier, vision detector, 6 MHz limiter amplifier and 6 MHz quadrature discriminator.

The IF amplification and associated bandwidth shaping is performed in two Philips G8 colour receiver modules employing four transistors. The vision detector is included in the second module, giving video and 6 MHz sound carrier at its output.


## Alan C.AINSLIE

A 6 MHz ceramic filter is used as a simple bandpass filter to remove the video and shape the characteristics of the following 6 MHz amplifier.

Amplification at 6 MHz is carried out in the TAA570 (or similar) IC, which also performs quadrature FM demodulation using only a single tuned circuit.

Fig. 2 shows the circuit diagram of the PW Sound Tuner.

The volume control is connected directly to the subassembly audio output and feeds $\operatorname{Tr} 2$, which is a simple emitter follower, to ensure that the TV Sound Tuner has a low output impedance. This enables long lengths of screened cable to be used on the output without any significant loss of treble.

The varicap tuner used in the prototype is the Mullard ELC1043, commonly used in contemporary


Fig. 1 : Block dlagram of the sound section of a TV recelver.

receivers and available at reasonable prices through surplus channels.

The ELC1043 has facilities for AGC but as it is not required in this unit, a potential divider, consisting of R10 and R9 connected across the supply, is used to bias the AGC terminal for optimum gain.

Power for the RF stages and oscillator is taken directly from the I2V supply to the sub-assembly.
To tune the ELC1043, a DC voltage variable between 0.3 V and 30 V is applied to the "tuning" terminal. This covers channels 21 to 68 for UHF reception. To achieve the necessary tuning resolution, multi-turn pots have to be used, in this case being neatly combined with the channel selection buttons in a commercial varicap push button control unit. These are available to give three, four, five or six preset channels and consist of the requisite number of preset pots connected across a stable 30 V supply, with each wiper being selected by a push button and connected to the "tuning" terminal on the ELC1043. A small capacitor (C11) is used to remove any noise introduced by the tuning pots.

The IF output of the tuner feeds directly through a 1000 pF capacitor into the first G8 module on the sub-assembly.

## POWER SUPPLY

The mains transformer used in this project has two secondaries, one of 40 V to feed the varicap diodes, and one of 12 V for the IF sub-assembly, tuner and output emitter follower. The complete circuit of the power supply is shown in Fig. 2.

The 12 V supply (actually adjusted to 11.5 V ) is obtained by full wave rectifying 12 V AC from the transformer in a bridge made from D4 to D7, and smoothing with C4. Voltage regulation is necessary to prevent oscillator drift in the front end and is performed by IC2, a $\mu \mathrm{A} 550$ regulator package.


This device works by comparing a reference of $1 \cdot 63 \mathrm{~V}$ produced at pin 6 with a fraction of the output voltage on pin 10, determined by R4 and VR1. Pin 4, connected to the junction of R4/VR1, is the inverting input to the comparison amplifier and pin 5 is the non-inverting input (connected directly to the reference).
The regulator acts to maintain the voltage on pins 4 and 5 equal, ensuring that the output is constant. VR1 is variable so that the required 11.5 V output may be precisely set.
Capacitor C5 is included to smooth the reference while C6 is high frequency compensation, necessary for stability.

## 30V SUPPLY

A very high degree of stabilisation is required for the 30 V supply as a few tens of millivolts change would cause appreciable detuning. Conventionally, a TAA550 IC regulator is used to stabilise the varicap diode supply in receivers. This is a two terminal device which is connected as a Zener diode, but which has very good temperature stability.
Continuing the analogy with a Zener diode, the dynamic resistance is quite low at around $10 \Omega$ but to make this resistance totally negligible compared to the source resistance a constant current source has been adopted in this design to ensure excellent tuning stability even with large mains voltage changes.

Transistor Trl in conjunction with Zener D3 and Rl forms a 5mA constant current source, with temperature compensation of Tr1 $V_{\text {be }}$ provided by D2 (D3 with a Zener voltage of $5 \cdot 1 \mathrm{~V}$ would have a virtually zero temperature coefficient).

The varicap control unit is connected directly across the TAA550 and drains little current as each tuning pot is $100 \Omega$. However, should a five or six button unit be used, R1 should be reduced to $820 \Omega$ to maintain an optimum 5 mA in IC1.

On-Off indication of the tuner is provided by LED1 mounted on the front panel. R3 serves as a current limiting resistor while D8 is included as reverse voltage protection.

## CONSTRUCTION

The IF sub-assembly is purchased fully assembled and aligned so there is no work to do in this area. Both the ELC1043 and a three button unit will mount directly on one end of the PCB which has all the necessary printed wiring on the foil side.


The push button unit is supported by two 38 mm 6 Ba bolts passing through the board and held captive between two units on each bolt. By adjusting these units, the buttons can be made to coincide with the cut-outs in the front panel.

A four station control unit can be accommodated on the PCB but an additional hole would have to be drilled. Larger units would have to be mounted directly on the chassis and the dimensions adjusted accordingly.

The connections for the push button units are shown in Fig. 3.

Before soldering the ELC1043 to the board, R10, R9 and C11, which mount under the tuner, must be soldered in place. R10 is on the copper side of the board and, to ensure that it does not short to the chassis, should be completely covered by a 25 mm length of 5 mm plastic sleeving.

## POWER SUPPLY BOARD

Both the 12 V and 30 V supplies and the output emitter follower are constructed on a single PCB, the layout of which is shown in Fig. 4.

Constructors who prefer to make their own boards should have no difficulty, the only point to watch being the spacing of the pads for IC2 ( $0 \cdot$ lin apart, rows spaced 0.3 in ). As an alternative, fully prepared boards will be made available-details in the component list.
Five mounting holes are drilled in the board, one at each corner and one adjacent to the transformer to prevent the board sagging.
The transformer has two 6BA mounting lugs and when soldered in position, two corresponding holes should be drilled in the PCB and the transformer secured with a couple of short bolts.
Assembly of the board is quite straightforward, with particular care being taken with the orientation of electrolytics, diodes, ICs and transistors.

## METALWORK

The complete TV Sound Tuner is mounted in a " $U$ ' shaped aluminium chassis with holes for the mains lead, panel mounting mains fuse, output lead and aerial socket on the back panel. The front of the chassis is masked by a front panel, secured with the pot nut on the volume control.
Fig. 5 shows the metalwork for the chassis and front panel. To absorb any tolerances the PCB should be marked from the actual boards held in situ.


Fig. 3: Connections for the pushbutton tuner unit (left) and details of the mountling of the Mullard ELC1043 tuner on the PCB (above).


Fig. 4 : Layout of the components on the power supply printed circuit board (left) and full size printed circuit master (right).


Fig. 5: Drilling detalls for the chassis (top) and iont panel (bottom). Materials can be 18 s.w.g. aluminium.

The two PCB's are supported by 6 mm stand-off collars on 6BA bolts. These collars make contact between the earth plane of the IF panel and the chassis, so the screws must be tight, with shakeproof washers used between the collars and the PCB.

## VOLUME CONTROL MOUNTING

The ganged volume on-off control is mounted in the hole provided on the front panel which coincides with a clear area of the IF board. Providing that the control is physically small it will fit in without any trouble.

Mains wiring to the control will pass directly over the 6 MHz ceramic filter which is very susceptible to RF pickup. To reduce the possibility of interference, a small tinplate shield is soldered to the mounting clip of the second G8 module, to cover the filter and associated components. The photograph shows the details.

```
Resistors (All iW)
    R1 1k\Omega2 (8200 if 5 or 6 button unit is used)
    R2 15k\Omega
    R3 2.2k\Omega
    R4 2.2k'2
    R5 68052
    R6 220k\Omega
    RT 220ks
    R8 3.3k\
    R9 8.2k\Omega
    R10 2.2k\Omega
    VRI 20kS1 skeleton preset
    VR250k$1 log pot with d.p.d.t. switch (S1)
Capacitors
\begin{tabular}{lll} 
C1 & \(220 \mu \mathrm{~F} 63 \mathrm{~V}\) elect & \(\mathrm{CT} 220 \mu \mathrm{~F} 16 \mathrm{~V}\) elect \\
C 2 & \(10 \mu \mathrm{~F} 25 \mathrm{~V}\) elect & C \\
C & \(22 \mu \mathrm{~F} 25 \mathrm{~V}\) elect \\
C & \(0.1 \mu \mathrm{~F}\) polyester & C 9 \\
\(10 \mu \mathrm{~F}\) & 10 V elect \\
C 4 & \(1000 \mu \mathrm{~F} 16 \mathrm{~V}\) elect & \(\mathrm{C} 1010 \mu \mathrm{~F} 10 \mathrm{~V}\) elect \\
C 5 & \(10 \mu \mathrm{~F} 25 \mathrm{~V}\) elect & \(\mathrm{C} 110.1 \mu \mathrm{~F}\) polyester \\
C 6 & 100 pF ceramic &
\end{tabular}
```


## Semiconductors

Tri BC15a
Tr2 BCiog
D1 1N4006
D2 1 N4148
D3 $5: 1 \mathrm{~V} 400 \mathrm{~mW}$ Zener
D4-D7 1N4002 (4 off)
D8 IN 4148
iC1 TAA550
1C2 14 A550 (NE550A)
LEDI TIL209

## Miscellaneous

T1 Type M1103
IF Sub-Assembly
Mullard ELC1043 varicap tuner (or ELC1042 for VHF)
Pushbutton controi unit ( 100 K per section)
S1 Double pole mains switch (ganged with VR2)
F1 500 mA fuse and panel mounting holder
Ski Coaxial aerial socket
Screaned audio output lead, mains lead, PCB for PSU, chassis, eabinet, front panel, knob.
The transtormer is available from Monty Enterprises, 2 Silver St., Doncaster, price £3. 95 _V VAT. A wooden box is available from Birch \& Ridley, Watson Road, Worksop, price $£ 2 \cdot 25+$ VAT 50 p postage and packing. The metal chassis and front panel can be obtained from Richard Friday Ltd., Old Coach House, Greystone Yd., Moorgate, Rotherham, Yorks, price $£ 5 \cdot 65$ + VAT - 35p postage and packing.
The If Sub-assembly, ElC1043 tuner, and pushbutton unit are all avaiiable from Manor Supplies, 172 West End Lane, London NW6, price £6.80 $45 p, ~ £ 4 \cdot 20-30$ p and $\$ 1 \cdot 20+25 p$ respectively, If all three are purchased $p$ \& $p$ is 50 p .

## WIRING

To avoid earth loops and the attendent difficulties it is important that the only ground connection between the PCB's is that made as part of the power supply wiring. Screened leads should be used for the signal wiring from the IF board to the volume control and from the volume control to the PSU board (input to emitter follower) but the screen of the lead should be cut short and not connected to the PSU panel.


To keep the mains wiring away from the emitter follower, the switch leads pass between the two panels and under the PSU board near the mains transformer.

By using a transformer isolated supply, no 'live chassis' hazards exist and the aerial connection can be made directly to the aerial terminal on the end of the ELCl043. On most units an earth braiding connection has to be made by soldering directly to the tuner case adjacent to the 'aerial' connector.

## FRONT PANEL

The front panel for the prototype was sprayed with car 'touch up' paint and lettering and lines applied using Letraset. A final spray of clear polyurethane protects the lettering from fingermarks and abrasions.

The window for the tuning indicators on the control unit was made from a piece of 6 mm clear Perspex carefully filed to size and affixed with a couple of dabs of epoxy cement. A waterproof felt tip pen was then used to mark the window area for each button.

Assembly of a wooden case depends on the facilities available and the skill of the constructor. As a guide, the case for prototype is a simple 'hood' made from veneered plywood. The front panel, of course, covers any screws that may be used to hold the chassis in the cabinet.

## SETTING UP

After a thorough check of all wiring component values, etc., VR1 is set to minimum resistance and power applied. By increasing VR1 it should be possible to set the supply rail to exactly 11.5 V .

No adjustment is possible on the tuning diode supply but it is as well to check that the voltage is of the right order.

Plugging the output lead into an amplifier and turning up the volume should give a high level of hiss, with possibly a couple of foreign radio stations as well. Plugging in an aerial and adjusting the tuning controls should give the local region TV stations loud and clear.

Channel numbers are not marked on the push button units but the pointer at the bottom indicates channels at the low end of the UHF band. The three regional stations are always grouped together with BBCl being the lowest channel number, ITV next, then BBC2.

Tuning will be a little difficult at first without the picture to help. For each station, several tuning points will be apparent, close to each other. The correct one will be towards the higher channel number end of the group, just before a region of 'vision buzz'.

When tuning has been mastered any remaining buzz can be carefully taken out by tuning the quadrature coil (see Fig. 6) with the CORRECT TRIMMING TOOL. No more than one turn adjustment should be needed as it is merely to compensate for the capacitance of the metal chassis, etc. No other tuned circuits (i.e. those in the front end or G8 units) should be toucher as specialist gear is needed to set them up again.

The Sound Tuner is very sensitive and, while it would be silly to expect good results from the proverbial "piece of wire", a weak signal (such as would produce a quite noisy black and white picture and very poor colour) would be sufficient. This means that a splitter in the main receiver TV co-ax will furnish plenty of signal or alternatively a second small aerial could be installed.

## The Sinclair DM2 Multimeter.

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# The Sinclair DM2 Multimeter: fuil technical story 

| DCVolts Range | Accuracy | Input Impedance | Resolution |
| :---: | :---: | :---: | :---: |
| 1 V | 0.3\% $\pm 1$ Digit | $>100 \mathrm{M} \Omega$ | 1 mV |
| 10 V | $0.5 \% \pm 1$, | $10 \mathrm{M} \Omega$ | 10 mV |
| 100 V | $0 \cdot 5 \% \pm 1$ " | $10 \mathrm{M} \Omega$ | 100 mV |
| 1000 V | $0.5 \% \pm 1$., | $10 \mathrm{M} \Omega$ | 1 V |
| Maximum overload-350 V on 1 V range |  |  |  |


| ACVolts Range | Accuracy | Input Impedance | Frequency Range |
| :---: | :---: | :---: | :---: |
| 1 V | 1.0\% $\pm 2$ Digits | $10 \mathrm{M} \Omega / 40 \mathrm{pF}$ | $20 \mathrm{~Hz}-3 \mathrm{KHz}$ |
| 10 V | $1.0 \% \pm 2$, |  | $20 \mathrm{~Hz}-3 \mathrm{KHz}$ |
| 100 V | 2.0\% $\pm 2$, | 10 M / $/ 40 \mathrm{pF}$ | $20 \mathrm{~Hz}-3 \mathrm{KHz}$ |
| 1000 V | 2.0\% $\pm 2$ | $10 \mathrm{M} \Omega / 40 \mathrm{pF}$ | $20 \mathrm{~Hz}-1 \mathrm{KHz}$ |
| Maximum overload-300 V on 1 V range |  |  |  |
| DC Curren |  | Input |  |
| Range | Accuracy | Impedance | Resolution |
| $100 \mu \mathrm{~A}$ | 2-0\% $\pm 1$ Digit | $10 \mathrm{~K} \Omega$ | 100 nA |
| 1 mA | $0.8 \% \pm 1$, | 1 K S | $1 \mu \mathrm{~A}$ |
| 10 mA | 0.8\% $\pm 1$, | 100s2 | $10 \mu \mathrm{~A}$ |
| 100 mA | $0.8 \% \pm 1$ " | $10 \Omega$ | $100 \mu \mathrm{~A}$ |
| 1000 mA | 2.0\% $\pm 1$ | $1 \Omega$ | 1 mA |
| Maximum | load-14 (fused). |  |  |
| AC Current |  |  |  |
| Range | Accuracy | Frequency Range |  |
| 1 mA | 1-5\% $\pm 2$ Digits | $20 \mathrm{~Hz}-1 \mathrm{KHz}$ |  |
| 10 mA | $1.5 \% \pm 2$, | $20 \mathrm{~Hz}-1 \mathrm{KHz}$ |  |
| 100 mA | 1.5\% $\pm 2$, | $20 \mathrm{~Hz}-1 \mathrm{KHz}$ |  |
| 1000 mA | 2.0\% $\pm 2$ | $20 \mathrm{~Hz}-1 \mathrm{KHz}$ |  |
| Maximum overload-1A (fused). |  |  |  |
| Resistance |  |  |  |
| Range | Accuracy | Measuring Current |  |
| $1 \mathrm{~K} \Omega$ | 1.0\% $\pm 1$ Digit | 1 mA |  |
| $10 \mathrm{~K} \Omega$ | $1.0 \% \pm 1 \quad$ " | $100 \mu \mathrm{~A}$ |  |
| $100 \mathrm{~K} \Omega$ | $1.0 \% \pm 1 \quad$, | $10 \mu \mathrm{~A}$ |  |
| $1000 \mathrm{~K} \Omega$ | 1.0\% 1 1 | $1 \mu \mathrm{~A}$ |  |
| $10 \mathrm{M} \Omega$ | 2.0\% $\pm 1$. | 100 nA |  |
| Overload protection-50mA (fused). |  |  |  |

Readers outside the UK, please write for details of your local distributor to :

## Sinclair Equipment International Ltd,

 33 Beauchamp Place, London SW1 1NU.



MORE than 74 exhibiting firms with over 120 trade names filled the hotels Majestic and Cairn at Harrogate this year, when Audio 75 was held from August 29th to 31st.

To report on every item seen and to mention every firm would fill half-a-dozen issues of Practical Wireless, so we have chosen a few which we think will particularly interest our readers.

## Rlba

Alba exhibited a portable radiogram, Model 3200. It employs a 2 -speed player and an a.m. radio and operates from $6 \times \mathrm{HP} 2$ batteries or from the mains Also on show was their UA 8080D teak-finished 3 -piece suite with a 3-band tuner, stereo 3 W per channel amplifier and a BSR autorhanger.

Model UA 9070D is a music centre comprising a.m./f.m. tuner, $2 \times 8 \mathrm{~W}$ amplificr, 13 SR changer and a cassette recorder-all in a teak cabinet with matching speakers.

## Bang \& Olufsen UK Lid

Beocentres 1400 and 1800 were shown along with an impressive range of assorted equipment styled in the unique $\mathrm{B} \& 0$ way.

The 1400 has a stereo. a.m./f.m. radio, 20 W per channel amplifier and a built-in cassette recorder. Price in teak. $£ 249 \cdot 50$. The 1800 model has a simila


Bang and Olufsen's 6000 model.
specification but features an automatic record player instead of a recorder.

Amongst the range of Beogram record decks on show was the very sophisticated Beogram 6000 electronically controlled 4 -channel deck with built-in CD4 decoder and MMC 6000 cartridge. Price is $£ 387.90$ but you do get a free copy of Mahler's 5th Symphony recorded in CD4 thrown in!

## BASF UK Ltd

This firm was showing at Harrogate for the first time and exhibited their comprehensive range of reel-to-reel tapes and cassettes with a special display on the recently released 'LH Super Range'. With LH tape, the principle is as follows:

The magnetic paricles of normal ferric oxide tape are comparatively large and irregularly shaped. Apart from increasing the noise level, this also reduces the sensitivity of cassettes at high frequencies, where the shorter wavelengths approach the length of the particles, because of the slow running speed.

A Low Noise tape overcomes this by using smaller particles. L.H Tape (Low noise/High output, invented by BASF in 1967) also uses smaller particles, but at a much greater density, giving a higher output on playback. LlI Super is a very recent breakthrough in ferric oxide tapes from BASF. It extends the LH principle by using a new high density coating process and the smaller and more evenly sized particles of Maghemite (the mineralogical name for specially processed gamma l'e $\mathrm{O}_{\text {; }}$ oxide).

The result is a full 50 per cent increase in sound quality. This can be scen by recording at OVU level, where the harmonic distortion is just $2 \cdot 5$ per centhalf the figure set by the DIN standard.
Even compared to BASF LH tape, LII Super is said to give a 3 dB increase in recording level and over 2 dB less tape hiss. Also seen were the automatic switching $\mathrm{CrO}_{2}$ cassette machines-the Compact CC9110 at £35, the CC902 ( $£ 65$ ) and the CC9302 with mixing facilities and a four-band receiver, priced at £90. Cassette decks on show were the 8200 ( $£ 180$ ) and the 8100 at $£ 120$. Sec details of the BASF special offer in our News . . . pages.

## Bib Ei-Fi accessories

Bib, as is usual at this type of exhibition had their full range of $\mathrm{Hi}-\mathrm{Fi}$ accessories on show. Of particular interest was the new cassette storage unit Ref 86 which holds 30 cassettes in their containers. Fitted with a tiated acrylic hinged lid, the base of the unit comes in a simulated teak effect and the whole cabinet measures $15 \mathrm{in} \times 4^{1}{ }_{4} \times 10^{1}{ }_{2} \mathrm{in}$ wide. Price is $£ 6 \cdot 60$ excluding VAT.


Bib's new cassette storage unit.

## BSP Lid

BSR unveiled a new slimline plinth and cover, made to compliment the company's range of McDonald turntables. The plinth, in teak, is cantilevered out from a matt black base which gives the whole thing an illusion of 'floating' an inch or so above the surface of whatever it is stood upon.

The firm's belt-driven turntables were also featured, and, I feel, represent very good value for money. Top of the range is the BDS 90 , upon which we hope to include a review in a later issue of P.W. It has a constant-speed high-torque motor with a heavy non-magnetic turntable. The tubular magnetic pickup arm has a concentric gimbal style mount and is fitted with counterbalance, bias compensation and a silicondamped cueing device. Wow and flutter figure is quoted as $\pm 0.13$ per cent.


The BDS 90 deck from BSR.

## Eagle International Lid

On show for the first time to the general public was the 2000 range, including the A2004 and A2006 amplifiers, turntables D2005 and D2006, headphones type H2008 and H2009, tuner T2008 and the S2002, 2003, 2004, 2005 and 2006 range of speakers.


The 2004 amplifier is rated at 20 W per channel. It has a facility for two extra speakers to give simulated quad. The 2006 has a similar spec. with the addition of 'sound effects controllers'. The A2004 costs $£ 65$ and the $\mathrm{A} 2006, £ 85$.

Eagle were also exhibiting equipment under the Beltek name and had their M1150 Dolbyised stereo cassette deck priced at $£ 158$ on show. Also there was the M1130 deck which was very similar but did not have the Dolby feature.

## Fidelity Radio Lid

The Fidelity range included the UA4 budget stereo system priced at $£ 48 \cdot 60$. Features are a two-speed record deck, 5 W per channel amplifier and two whitefinish speakers. The UA7 priced at $£ 65 \cdot 40$ uses a BSR three speed record deck. The UA3 system is very similar in styling and priced at $£ 87.96$ with BSR changer, $2 \times 4 \mathrm{~W}$ sine wave amplifier and a.m./ f.m. tuner.

One of the latest additions to the range is the UA6 system at $£ 144 \cdot 68$. This comprises Garrard SP25 single play record deck with magnetic cartridge; 10W per channel amplifier, a.m./f.m. stereo radio tuner. A tape socket and a socket for stereo head-phones are provided. Top of the range is the MC2 Music Centre with BSR record changer, a.m./ f.m. stereo radio, stereo cassette recorder/player, $2 \times$ 4W amplifier. Storage is provided for cassettes.

## GEC (Radio \& Television) Lid

Music Centre Model 2917 has a.m./f.m. stereo radio, stereo cassette recorder/player and Garrard 6300 auto/manual 3 -speed record player. The amplifier is rated at 10 W per channel and provision is made for "ambio" sound. Price: $£ 242 \cdot 75$. At $£ 234$-09 comes model 2919. It uses Garrard SP25 single play record deck; 4-band tuner with decoder fitted; and has a 15 W per channel amplifier with provision for ambio sound. In teak, with matching speakers.

Top of the range is the model 2820, £271.21. Features include: 20 W per channel amplifier with ambio facility; f.m. stereo radio tuner with electronic touch tuning, calibrated tuning meter, and interstation quieting; Garrard 86 SB single play record deck with Shure magnetic cartridge.

Model 2821 is a combined 4-band stereo radio with BSR C141R record deck and $2 \times 7 \mathrm{~W}$ amplifier, two speakers, it is priced at $£ 121 \cdot 66$. Model 2816. (£147.72) has 4-band radio with BSR P128R record deck and a 15 W per channel amplifier.


The Goldring $L 65$ deck.

## Goldring

Model L65-the latest addition to the Goldring Lenco range was shown. Particular items of interest are the automatic functions of the tonearm, the viscously damped suspension and the anti-skating device which with separate scales is adjustable for elliptical and spherical styli.

Other items in the specification are:
Speed: $331_{3}$ and 45 r.p.m. Wow and flutter weighted according to DIN 45507: $<+/-0,12 \%$ Rumble unweighted according to DIN 45539: $>38 \mathrm{~dB}$ Rumble weighted according to DIN 45539: $>57 \mathrm{~dB}$.
Turntable: Dia. 300 mm Weight 1.4 kg .
Tonearm: With a super light weight aluminium headshell suitable for use with all international standard cartridges. Stylus pressure adjustable $0-5 \mathrm{gm}$.
Mains voltage: $110 \mathrm{~V} / 60 \mathrm{~Hz}, 220 \mathrm{~V} / 50 \mathrm{~Hz}$ Power Consumption: Approximately $2 \cdot 5 \mathrm{VA}$.
Measurements: Chassis $405 \times 300 \times 2 \mathrm{~mm}$. Depth re. quired below chassis 54 mm . With plinth and dust cover $426 \times 321 \times 148 \mathrm{~mm}$.
Weight: With plinth and dust cover 6.75 kg , and packing 8.6 kg .

The Goldring Lenco ST800 compact stereo system was also on show. Incorporating the GL78 transcription unit, fitted with a G800E cartridge, it has an f.m. tuner fitted with three pre-set station buttons. Output is 40 W per channel and slider controls are provided for volume, bass, treble and balance.

Also shown was the Goldring range of stereo mag. netic cardtridges-including the easily replaceable stylus system types 820 and 800 series.

## JVC (UK) Lid

JVC model 1845 shown on the stand features a 3-band a.m./f.m. tuner with $2 \times 15 \mathrm{~W}$ rms amplifier, front loading cassette deck with $\mathrm{CrO}_{2}$ facility and noise suppressor. This comes with a belt-drive transcription turntable with magnetic cartridge. The tuner is fitted with tuning meter and loudness control. Price, including speakers, is $£ 280$ plus VAT.

Model MC-1820L features a stereo cassette deck of the same design as the company's more expensive ANRS decks, plus an a.m./f.m. stereo tuner 16 W per channel amplifier all housed in low profile cabinet. Price, exclusive of speakers, is $£ 145$ plus VAT.

JVC have developed a new I.C. for their ANRS (Automatic Noise Reduction System). It is said to improve both performance and reliability and lower
the cost of incorporating ANRS in existing equipment.

Compactness is the keynote of the new ANRS circuit now and the relatively few external components used in the unit allows the whole p.c. assembly to occupy half the area previously taken up.

## Philips Electrical Lid

The Philips range on show was so vast that we can only mention a few items of their equipment.

Model RH734 tuner-amplifier covers a.m./f.m. bands and bas a 30 W per channel output. Price is $\mathfrak{£ 2 0 7} \cdot 18$. The RH732 tuner-amp has a similar radio specification but a 12 W per channel output. It sells at $£ 172 \cdot 45$. A matching record deck for either unit is the new GA427 belt-drive model fitted with a GP400 magnetic cartridge. Price is $£ 62 \cdot 50$.

Another recent addition to the Philips range is the RH741 4-band tuner with a 15 W per channel amplifier. An interesting feature of this model is the visual indication on scales for bass and treble response. Price is $£ 167 \cdot 83$.

The GF907 record playing system is in a crackle black and silver finish (something different anyway!) The deck employs the GC007 belt-drive turntable fitted with a GP400 cartridge. The amplifier is rated at 15 W per channel output and the price is quoted as £184.61.

Top of the range of music centres is the new RH832 priced at $£ 781 \cdot 25$. The spec. includes: 4-channel pre-amplifier with built-in SQ decoder and connection for CD4 demodulator; 2-speed electronically controlled record playing deck with GP422 magnetodynamic cartridge; a.m./f.m. tuner equipped for stereo f.m. and 4-channel (SQ) transmissions.

## Pye Lid

Pye's Sound Project ZU440 record player/f.m. radio/ cassette recorder was on show. It features 'disc jockey' mixing. The cassette unit has DNL (Dynamic Noise Limiter) and the amplifier delivers 15 W per channel. The tuner has decoder fitted. Price, including two 2 -unit speakers and mono microphone, £364-88.

ZU540 combines f.m. tuner with stereo beacon and four station push buttons; transcription type 2-speed record deck; cassette recorder with Dolby system and $\mathrm{CrO}_{2} / \mathrm{Fe}_{2} \mathrm{O}_{3}$ automatic sensing. The amplifier is rated at $2 \times 20 \mathrm{~W}$. The speaker assemblies use a bass $/ \mathrm{mid}$ - range unit with a line tweeter. Price is $£ 475 \cdot 48$.


Sound Project ZU540 from Pye/Ekco.

SUPERSOUND 13 HI－FI MONO AMPLIFIER

A nuperb solid state auilio ampli－ er．Brand new component roughout． 5 silicon trat ransistors in push－pul Fuil ware rectification Output approx．
whats．Frequeucy sponse $12 \mathrm{~Hz} 30 \mathrm{KHz} \pm$ 3ab．Fully integrated uparate Volume．Hass buost and Treble cut controls．Suitable fur 8－15 ohm speakers．Input for pprox， 40 my for full output．Supplled ready built and teated，with knobs，escutcheon panel，input and output plugs．Overall size $3^{\mu}$ high $\times 6^{\prime \prime}$ wide $\times 7 t^{\prime \prime}$ deep．A 200／250V．PRICE E15－00．P．\＆P．65p．
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a $u$ a alse lint $11:-2=$ BCLA8 Triode Pentodes． $1 \times$ EZ 80 as rectifer．Two dual potentlometers are provided for buas．A dual volume control is used．Balance of the left and right hand channels can be ailjusted by means of a sepa－ rate＇Balance＇control fitted at the rear of the chassis． Input sensitivity is approximatels $300 \mathrm{~m} / \mathrm{y}$ for tull peak output of 4 watts per channel（ 8 watts mono），into 3 ohm apeakera．Full negative feedback in a caretully calculated nircuit，allows high volume levels to be used with negligible distortion．supplea complete with knobs，chassis size $11 "$＂$\times 4$＂d．Overall height including valved $5^{\prime \prime}$ ．Ready
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\＆12．50．F．$\&$ P． 85 p. ALL－PURPOBE POWER SUPPLY UNIT 200／240v．A．C． Input．Four awitched fully amuothed D．c．outpate giving 68．and 7 fv ．and 9 y ．and 12 v ．at 1 arup on loail． Fitted Insulated output terminals and pllot larip indicator Heady builtand PRICE 6.35 P．\＆P．55p VYNAIR \＆REXINE SPEAKERS \＆CAEINET FABRICA app． 54 in．Wide．Our price 21.80 Jd．length．P．\＆P． 30 p per yn．（min． 1 yd．）．s．a．E．or ramplea．

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 better than 80 mV into 1 MQ ．Full power bandwiuth $\pm 31 \mathrm{~B} 1-15,000 \mathrm{~Hz}$ ．Bass bouat approx．to $\pm 12 \mathrm{~dB}$ ． Treble cut approx．to -16 d B．Negative feedback 18 dB over main ntup．Power requirementa 3 s．at 1.0 mimp． Overall size $122^{\prime \prime} w . \times 8 " d . \times 2 \mathbf{g}^{\prime \prime} h$ ．
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Almo a vaitable ready built and tented $\mathbf{8 3 2} \mathbf{6 0}$ ．Port Free Note：The atore amplifier is suilable for feeding fun mone surees into，inplets（e．g．mike，radio，twin recora decks，ele． and twill then provide mixing and fading faellitien for mad


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AMPLIFER EAB4 ME Designed for Hi－Fi seproduc tion of records．A．C．Main uperation．Ready bullt on wated heavy gauge metal chansis，size $7 t^{\prime \prime}$ w．$\times 4^{\prime \prime} \mathrm{d} . \times$
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ECC8s， 4！＂h．Incorporates ECC8s， fil．84，EZ80 ralves．Heavy
duty，double wound maina tranoformer and output trans－ utrol and now with improved control giving besa and treble lift and cut．Negative feedhack line．Output 4t watta．Front panel can te detached and leadn extended for remote mounting of controls．Complete with knota，v

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gible thum．Separat inputa for mike and gram allow record and annomacements
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Model 1570 is a unit audio console in a teak cabinet having record storage facilities. The amplifier is rated at 15 W per channel. The tuner is a.m./stereo f.m. and the record deck is a single play unit. Twin 2 -unit speaker assemblies are included in the quoted price of $£ 237 \cdot 58$.

Model SX0940 is priced at $£ 199$ with a tuner including s.w. band, cassette deck and GC014 single play record deck. The amplifier rating is $2 \times 5 \mathrm{~W}$.

Priced at $£ 230 \cdot 91$, which includes speakers and metal stand, is the model 5024 comprising 3 -band radio/cassette recorder and 3 -speed stereo record player.

## Pyser Lidd

On show was the new Marantz 1040 integrated stereo amplifier. Rated at 20 W per channel, it features professional type graphic tone controls and main/remote speaker switching with ambience and loudness compensation. Price: $£ 132$ plus VAT. Also shown was the new 1070 amplifier and the model $2325,2 \times 125 \mathrm{~W}$ stereo receiver with Dolby.


Marantz 1040 stereo amplifier.

## Rank Radio International

On view for the first time was the SP range of Wharfedale loudspeakers. Two models make up the range, the Dovedale SP and Airedale SP. Both are floor standing reflex enclosures.

The Dovedale SP is a 60 litre enclosure handling 60 watts DIN whilst the larger Airedale contains 100 litres and accepts 100 watts DIN. The Dovedale has two in-phase bass drivers, one mid-range and one high frequency unit. The Airedale has a bass driver, two mid-range units covering between them the range of frequencies between 300 Hz and 5 kHz and a high frequency unit.

The Airedale SP has a bass cut-off frequency of $27 \mathrm{~Hz}(-3 \mathrm{~dB})$ which represents the lower limit of human audibility. The Dovedale SP is little higher with a bass cut-off of $35 \mathrm{~Hz}(-3 \mathrm{~dB})$. Both respond to beyond the limits of audibility at high frequencies.

The Dovedale SP and Airedale SP are available in Teak with removeable speaker grilles at the respeclive recommended retail prices per pair of $£ 182.71$ and $£ 274 \cdot 10$ including VAT.

## Skantic (UK) Lld

Skantic introduced their new model 1753217 W per channel stereo hi-fi music centre. This unit includes an f.m. stereo radio and there are push buttons for selection of five pre-set stations.

The Skantic turntable has a 16 pole synchronous motor, an anti-skating device and easily adjustable stylus pressure. The arm includes a Pickering V15


Rank Rajio International's latest models.
AT2 magnetic cartridge. The cassette recorder is completely designed and manufactured by Skantic's own engineers. The tape deck also has a built-in DNI. noise reduction system, an autostop and chrome dioxide switching system. A VU meter for recording and playback levels and a digital counter are also included.

The 17532 exceeds European standard DIN $45 \cdot 500$ and is ready for ambiophonic stereo. The unit is available in Rosewood, teak or walnut high grade veneer as well as white or black lacquer.

Skantic's newly designed speakers, which are included with the 17532, each have a power handling capacity of 30 watts. Each speaker has two units a 20 cms unit for bass and middle range and a 2.5 cms dome-tweeter.

Features of the unit include loudness compensation filter selector; switchable sockets for headphones and inputs for two microphones.

Price including speakers: Rosewood-£308.78+ VAT; Teak-£288.75 + VAT; Walnut W/B-£302.33 +VAT.


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ALUMINTUM PANELS $18 \mathrm{~A} . \mathrm{w} .8 .8 \times 4 \mathrm{in}, 15 \mathrm{p} ; 8 \times 8 \mathrm{im} .25 \mathrm{p}$; $14 \times 8 \mathrm{in} .25 \mathrm{p} ; 10 \times 7 \mathrm{in}, 80 \mathrm{p} ; 12 \times 8 \mathrm{in} .80 \mathrm{p} ; 12 \times 8 \mathrm{in} .40 \mathrm{p} ;$
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FREE running oscillators designed around TTL ICs are notorious for poor frequency stability. The most significant factor contributing to frequency drift is variation of the supply voltage, and it is this apparent 'disadvantage' that is exploited in this circuit.

The FM Signal Generator (Wobbulator) is an essential piece of apparatus for setting up the HF circuits of FM receivers, and is extremely useful for the fast, accurate alignment of AM IF strips. In the conventional RF signal generator a continuous carrier is generated at constant frequency. A second signal at (usually) audio frequency is then applied to this RF signal varying the RF output voltage amplitude in direct relationship to the second, modulating frequency. In the FM signal generator the RF waveform is generated at constant amplitude and the modulating tone is used to vary the frequency of the RF signal.

The simple Wobbulator described here provides signals at three selected centre frequencies with provision for wide frequency deviation using external modulating sources. Although the RF signal is based on a square waveform rather than the more conventional sine wave, the effect of this difference is negligible in practice.

## Basic circuit

The basic circuit of the free running TTL multivibrator is shown in block form in Fig. 1, and is probably the simplest circuit available to the
amateur constructor! If Ct is omitted the oscillator comprises three positive logic NAND gates in series. In this configuration the mode of operation is quite straightforward. If the input at gate 1 is 'low' the output will be 'high'. Gate 3 thus has a 'low' input and a 'high' output and since the output of gate 3 drives the input of gate 1 a self-oscillating loop is created.

The operating frequency of this oscillator is deter-


Flg. 1: Block dlagram of a bas/c TTL oscillator.
mined by the signal propagation delays through the gates. For the SN7400 gate the propagation delay for the 'low' state is approximately $8 \cdot 0 \mathrm{~ns}$ and for the high state 18 ns . As the oscillator alternates between two 'low' plus one 'high' state, and two 'high' and one 'low' state the total delay alternates between $(8+18+8) \mathrm{ns}$ and $(18+8+18) \mathrm{ns}$. The typical average delay is thus: $\frac{34+44}{2}$ or 39 ns , giving typical free-running frequency of $\frac{1}{39 \times 10^{-9}} \mathrm{~Hz}$ or 25 MHz .

As the two delays are not equal the output is not a 1:1 mark/space ratio squarewave and in practice stray capacitance and internal inbalances tend to emphasise the delay difference to give a ratio nearer 2:1.


Fig. 2: Frequency plotted against voltage for a TTL oscillator. As can be seen, the relationship /s non-linear.

## Frequency variation

The oscillator frequency can be varied by altering the propagation delay time, by modifying the rise time of the transfer pulse. This is the function of Ct. It is possible to use a series of capacitors across one, two or all three of the gates to give a more stable arrangement but in practical circuits this complication is rarely justified. The effect of Ct is surprisingly linear and for the purpose of initial trials the oscillator frequency can be expressed as: If $\mathrm{Ct}=22 \mathrm{pF}$ then $\mathrm{F}=11 \mathrm{MHz}$ and if $\mathrm{Ct}=500 \mathrm{pF}, \mathrm{F}=500 \mathrm{kHz}$.

These values as calculated should be treated with some caution as tolerances can lead to quite significant modifications to Ct to obtain a given frequency of operation. The equation thus indicates an approximation for Ct , the actual value has to be found by experiment.

The oscillator frequency increases with increasing supply voltage, Fig. 2, and as can be seen the frequency/voltage relationship is non-linear. However, if we consider a relatively small voltage change ( $\pm 0.5 \mathrm{~V}$ ) the linearity is sufficiently good to make the control of frequency by means of varying the supply voltage a worthwhile proposition.

The simplest arrangement for varying the supply voltage is the series emitter follower shown in Fig. 3 in which the base of the transistor is biassed by means of a potential divider and the collector taken to a suitable positive supply. In this arrangement the voltage appearing at the emitter is equal to the base voltage less the base/emitter voltage drop of the transistor $(0.6 \mathrm{~V}$ in the case of silicon). If a variable voltage is now applied to the base of the transistor the emitter voltage will rise and fall in
phase with the base voltage so that the emitter 'follows' the base voltage.


Fig. 3: The theoretical series emitter follower shown here, varies the voltage, and thereby the frequency of the oscillator to which it is connected.

## Practical circuit

In the practical circuit Fig. 4, the timing capacitor (Ct of Fig. 1) is switched by means of Slc to provide three spot frequencies, the values shown giving spot frequencies of $455 \mathrm{kHz}, 1 \cdot 6 \mathrm{MHz}$ and $10 \cdot 7 \mathrm{MHz}$.
Variable resistors VR2-3-4 are incorporated to set the precise operating frequency. These resistors modify the current flows to the gate inputs and provide a small degree of frequency adjustment on each range. It is important that these resistors should be set to the highest possible value to minimise the gate bias, as overbiassing can lead to erratic running and poor stability. If it is found that the tuning resistor has to be set to a value of less than $2 k \Omega$, then an alternative timing capaictor should be sought.
The SN7400 is a quadruple NAND gate, and since


Flg. 4 : Circult diagram of the complete TTL Wobbulator. The output may be taken from etther the rotor of VR5, or alternatively from the attenuator network. However only one of these two, should be connected in circuit


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only three gates are used for the oscillator, the fourth gate can be used as a buffer to prevent the output load from affecting the operation of the oscillator. The output from the buffer gate depends very much on the device used. The cheap, low-noise immunity gates give a swing of about 2 V , while the more expensive can manage 3 V or so. These output levels are too high for most purposes and the circuit of an optional attenuator circuit is shown in Fig. 4. As the output from the gate is a squarewave the simplest way of maintaining constant amplitude to the attenuator is to clip the signal at a predetermined level. This is the function of the diode network $\mathrm{D} 4 / \mathrm{D} 5$ which limits the output to $1 \cdot 8 \mathrm{~V}$. The clippea signal is then fed to VR5 or the resistive ladder network (R3-R10) which makes up the attenuator.

## Modulation

The modulating signal is AC coupled to the base of Trl to prevent any residual DC component of the waveform from de-tuning the oscillator. The diodes D2 and D3 wired back-to-back limit the modulating signal. Silicon diodes are again used here with a forward voltage drop of 0.6 V .so that they need at least 0.6 V across them before they conduct. If the input signal exceeds this value one or other of the diodes conduct shorting the excess signal to earth.

The potentiometer VR1 determines the level of modulating signal reaching $\operatorname{Tr} 1$ base and therefore controls the frequency variation of the oscillator with respect to input voltage. This potentiometer is thus the deviation control. The zener diode D1 limits the rail voltage to $6 \cdot 8 \mathrm{~V}$. An alternative mains power unit is shown in Fig. 5.


Fig. 5: Alternative mains power supply. This is recommended if prolonged use is to be made of the Wobbulator.

## Construction

The oscillator and modulator are built on a piece of 0.7 in. matrix veroboard, Fig. 6. The layout is not critical and may be built on any scrap piece of veroboard. The trimming capacitors and resistors are wired directly on the range switch while the resistcrs comprising the alternative attenuator chain are similarly mounted round the output range switch (not shown in photograph).

Using an aluminium box $130 \times 100 \times 50 \mathrm{~mm}$ deep, the battery powered version can be neatly accommodaled on the metal panel as shown in the photographs. The mains powered version can be built
into the same size box if the Doram transformer specified is used. However, as this involves some rather careful 'packing' of components, the less experienced would be well advised to opt for a larger box.

## Calibration

Carefully check the wiring, switch on and check that Tr 1 emitter voltage is $4 \cdot 5 \mathrm{~V}( \pm 0 \cdot 2 \mathrm{~V})$. Rl should be adjusted if necessary to obtain this voltage. The spot frequencies must next be established. During this setting-up procedure the modulation input must be shorted to earth. Using an 'all-band' communications type receiver, feed the attenuated output from the wobbulator into the aerial socket. With the BFO switched on, the wobbulator output can be detected and VR2-3-4 adjusted until the required three spot frequencies are obtained. The attenuator function can also be checked against the ' $S$ ' meter.

In the absence of a suitable communications receiver the spot frequencies will have to be set up against known frequency IF strips. The output from the wobbulator should be injected into the first IF transformer, the most convenient point being at the mixer stage. A voltmeter should then be connected across the AGC line and the appropriate VR adjusted until maximum AGC voltage is detected. The spot frequency is then set to the centre frequency of the IF.

## components list




Photograph showing the mounting of the components on the ress of the front facla. Notice the varlable resistors and timing capacilors mounted on the wafer swifth.


Fig. 7a: Ideal response curve.


Fig. 7c: Detuning of one or more stages in the If strip.


Fig. 6: The circuit should be laid out on 0.1in. matrix Veroboard as shown above.

## Operation

To use the wobbulator effectively an oscilloscope with an $X$ deflection output is required which is fed into the modulation socket of the wobbulator and the $Y$ input (vertical deflection) is coupled to the detector of the intermediate frequency strip under test. The wobbulator output is then applied to the IF transformers in turn starting with the last IF and progressing to the first. The response shown on the cathode ray tube should be as Fig. 7a. Figs. 7b and 7c show poor selectivity and detuning of one or more stages respectively. With care it will be found that this technique will give up to 6dB more gain and greater selectivity than the usual method of amplitude modulated signal generator plus ear!

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& 3 \text { pole, } 3 \text { way- } \text { pole, } 3 \text { way- } \\
& \text { pole, } 4 \text { way- } 3 \text { pole, } 4 \text { way } 2 \text { yote } \\
& 6 \text { way-1 pole, } 12 \text { way. A1 :it } 38 \text { p } \\
& +15 \text { p post } \$ \text { YAT eaill. }
\end{aligned}
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SHORT WAVE BROADCASTS by Derek Bell

BEARING out my long-held view that the HAC one-valver is the ideal simple set for the beginner, Andrew McIntee from Craichie, by Forfar, in Scotland, opens this month's offering with the logging of New Zealand on 11780 at 0900 . This is only a 7.5 kW station and to pull it on the HAC is worthy of a round of applause at least. Andrew does admit though that he has a 180 ft long wire aerial and has fitted an ATU. Speaking of which, I hear that one of the advertisers in PW is testing a new aerial tuning unit and if it is a success it will be launched in the near future. I have no news on the price as yet but will keep you informed.

This month certainly seems to be rich in unusual loggings, it must be the revivification caused by the summer holidays! This is evidenced by John Spinks of Great Moulton, Norfolk who, using his Trio and the old faithful Joystick on the garage roof, he has pulled in the following:-

Radio Bolivar on 4770 at 0120
Radio Bucaramanga on 4845 at 0115
Kinshasa, Zaire on 4880 at 2150
Radio Yaounde, Cameroon on 4972 at 2140
Sibu, Sarawak on 5005 at 2215
In fact John's complete log contains a fistfull of very rarely reported stations and even had me trying for a few of them, nice work, John! Robert Hill of Crewe is off to Portugal for his holidays, a little late perhaps but he found time to drop us a line logging ELWA Liberia on 11895 at 0920. Aside from cramming for the dreaded ' $A$ ' levels Robert has fitted a reel-to-reel tape recorder to his Invicta 8027 and seems to be set fair to record some station ID's in order to refresh his memory, if need be.

Another old friend of ours is John Higginbotham of Holyhead and this worthy gentleman sent a long amusing letter regarding his domestic set-up. It seems that he has the same problem that many DXers face, namely, where to put all the bits and pieces! John says that his mother was "fed up with the bedroom looking like a workshop". Thus it is that he has moved into a garden shed. Fine on the shed John, but remember that radios in the main are precision instruments and do not take kindly to damp.

The best thing to do is to keep the sharpest of eyes on the humidity and try to beg, borrow or steal some form of heating. Thanks to this column John has pulled Radio Afghanistan on 15195 at 1130. He also QSL'd Pekin and the score to date on replies is as follows:- One calendar, two books, seventeen(!) magazines, two QSL cards, three skeds, three report forms and one notebook! Personally I can't see what they hope to achieve but they still keep sending out all this literature.

Two writers this month focus the spotlight on Radio Mexico. Harold Emblem from Mirfield, Yorks reports them testing on 15285 at 2205 while Jonathan Marks of Norwich writes that on 15125 they were asking in English and French for reports at 2258 while 2309 the language changed to Spanish. This indicates to me that they are trying to establish themselves in Europe in competition with Radio Nacional de Brazil. They asked for reports, without IRCs, to be sent to Radio Mexico, PO Box 20/620, Mexico City, Mexico and promise that accurate reports will get a Radio Mexico pennant.

Another address for QSLs comes from Chris Clarke of Shipdam who passes on the info that the American religious station WYFR asks for reception reports to be sent to Family Radio, Oakland, California, N 4621 U.S.A. Far across the Indian Ocean both India and Sri Lanka broadcast to their citizens in other lands. One person who reports them is $\mathbf{P}$. K. Gulati of Guildford who sends the loggings of Air Delhi on 1110 and 7150 at 1900 plus Radio Sri Lanka on 1200 at 1730 .

The popular question of QSL cards is raised by Jeremy Hinton who hails from Newcastle, Staffs. He asks what is the average time for a reply? Well Jeremy, this all depends on the station and its eagerness to maintain good relations with its audience. I will not deny that some stations lose reports or are plain lazy, and recently some American DXers got their replies back after ten years! You mentioned, Jeremy, that Radio Nederland refused you a QSL because you omitted to report the frequency. These details are important to the engineers in order that they can judge if their signal is reaching the target area.

A very welcome letter comes from Malta and asks if the writer is justified in sending reports to PW. I regret that I could not decipher the name but I believe it to be Vincent Canabatt. Well, Vincent your part of the world is very rich in transmitters and if you can hear them then there is a very good chance that we in the UK will. PW is read in a good many countries overseas and your tips will help them a lot. All that is needed is to write the station name, frequency, and time in GMT. It is also of interest

if you include any unusual details such as addresses or any news of future events that the station may broadcast.

There has been a very heavy post so inevitably many letters have to be left out, so to the writers I can only apologise and say 'keep trying' and to everyone wish best 73 s and so close the column for this month.


## by Eric Dowdeswel/ G4AR

Iam very glad to notice, in the various amateur radio magazines, an upsurge in operating using quite low power. As one would expect, those who try this very interesting work usually get quite a kick out of working stations thousands of miles away when using milliwatts of power and ordinary receiving type transistors. The work is virtually all on CW and the point in mentioning it is to ask those of you who are interested in copying code to have a look at the LF ends of the various bands for those chaps calling 'CQ QRP'.
Needless to say, one can spend a lot of time calling without getting a reply so, for a change, these stations would probably welcome reports from listeners. CQ Magazine runs a regular feature on QRP work which makes very intriguing reading! With the widespread abuse of licence power limitations in various countries it is good to hear of those who have gone in the opposite direction! Let us hope it will be a continuing trend.

The summer hang-up is really showing now with relatively few reports coming in. Readers are no doubt taking every advantage of the sub-tropical weather we have been enjoying for so long. Let's hope they are building up a great reserve of strength for the forthcoming DX season which will be quite tough with the bottom of the sunspot cycle not yet reached.

Fortunately, Paul Barker (Sunderland) has kept his nose to the grindstone possibly due to the added incentive of being able to watch slow-scan TV. 'Catch of the Month' for Paul was 9X5AV on 20 m SSTV but for sheer excellent picture quality Paul gives full marks to DL7DE in Berlin. (Marks-oh dear!) Paul points out that prefix C9 is now being used in place of the old CR7 reporting C9MIC as active in this strife-torn country. He also notes YR as a special prefix for Rumania but if I went to my very ancient collection of QSL cards I could find one showing YR as the old prefix used by that country! I think someone once said something about "all is change but nothing changes'.

Mike Bennett (Slough) didn't mention too many catches but all are very much worth while, such as C21NI on Nauru and FP0YY on St. Pierre and

Michelon and the Mount Athos DXpedition SV1GA/A. Jeremy Hinton A8962 (Newcastle, Staffs) had trouble with his Trio 9R59DS, which I hope I have been able to straighten out, so his $\log$ is very short this month. Back to Mike Bennett who sends some info on changes to licensing areas in PY land, too long to publish, but first suffix Z indicates a foreign operator such as PY1ZAA while similar suffixes W , X or Y indicate a novice licence. Just in case you ever hear one operating car mobile, his call will add /MT!

Although Neil Whiteside has been on holiday with a 160 m receiver in Dorset, away from his usual QTH in Hitchin, I am sorry to say he allowed local attractions to divert him from amateur radio! Let's hope he has got back on to the straight and narrow by now!

Ian Jay (Mansfield) has really got the knack now of only listing those stations of real interest including VP2 and ZL2 on 40 m SSB. Tim Charles (Colchester) apologises for lack of a $\log$ last month but his excuse is 'great changes going on in the shack', which, I suppose, is fair enough! Main receiver is now a Heathkit GR64 plus a home-built Q mulitplier. He tried to flog his CR70A at the Anglian Mobile Rally, without success, but I suspect he will be glad, in the long run, to keep it as a second receiver. Can't have too many of them around the place! Tim quotes latest UK calls issued as G8KMM and G4EHT in the middle of August but there will be many more with their hard-earned bits of paper 'ere you read this.

Stephen Budd A8713 (Worthing) has very wisely erected a Lazy-H beam which he thoroughly recommends. He doesn't mention its size but if it has 66 ft centre-fed elements then it is a very good performer indeed, with open line feeder and an ATU, for 40 m to 10 m . The usual problem is getting enough height above earth for the lower elements to be really effective. The bi-directional beam obviously passes through the Pacific because he logs such interesting ones as KB6CU on Canton Is., four KG6's on Guam and KJ6CF on Johnston Is. all of which come into the 'rare' category. That was on 20 m SSB but I hope Stephen will try that beam on the other bands in due course.

## Log extracts

S. Budd:- 20 m HS5AKW KB6CU KlMTJ/KG6 WB4LEE/KG6 KG6JBE KJ6CF KL7BJW KM6EA KS6FF KS6FK ST2SA VR1AT VS5DB ZD8LS
T. Charles:- 40 m VK3XB 20 m HC5PC JW5NM VRIPE ZLIEGM 2m DB0VR PI3VAD (repeater) SP3BUE
I. Jay:- 40 m CO2GS OJ0MA VP2MCT ZL2AGY 80m HZ1AB TR8DG VU2GDG 20m H18MOG SV0WKK (Crete) TG5YN VP2LBR VP2SN VS5DB 5L2FW 7X2BK
N. Whiteside:- 80m 9X5SP 5Z4LW 20m XE1APA KZ5RS
J. Hinton:- 15 m A4XFW JY5UNM HI6EA
M. Bennett: - 20 m C21NI FB8ZG FP0YY FR7ZW PJ8MS SV1GA/A 15m CX2BE LU6EAU ZP5IL 10m LU5DBA OJ0MA
P. Barker:- 20 m C9MIC JA0AXV YR2KBQ 7X2BK 7X5AB PV0SH (Singapore) 9V0SN 9Y4HM 20 m SSTV DJ9NG DL7DE F3RT 18WAM OH5RM OK2OI 9X5AV

All stations are SSB except those in bold which are CW.


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|  |  | SN72741 74126 p | $\begin{array}{ll} \text { BSX19/20/21 } & 16 \mathrm{p} \\ \text { MJE2955 } & 90 \mathrm{p} \end{array}$ |  | APACITORS |
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## MEDIUM WAVE DX by CHARLES MOLLOY

NORTH AMERICAN medium wave stations are often heard here in the UK. A path of darkness between transmitter and receiver is required for medium wave propagation and this occurs to North America some five to six hours after sunset in the UK. During the winter months Canadians can be heard as early as 2300, to be followed an hour later by outlets situated on the eastern seaboard of the United States. North Americans operate on channels spaced 10 kHz apart and they are allocated callsigns which are used frequently as a means of identification, followed by the city or town where the studios are located. Listen on 930 kHz for CJON St. John's in Newfoundland. It is the most consistent North American, its time zone is $3^{1}{ }_{2}$ hours behind GMT and it can be found on the low frequency side of AFN Berlin on 935 kHz .

Other Canadians which are heard regularly when conditions are favourable are CBN St. John's on 640 kII ; CIILR Sydney, Nova Scotia on 950 kHz ; CBA Moncton, New Brunswick on 1070 kHz . Broadcasts from the United States to look for are WABC on 770 kIIz , WINS on 1010 kHz and WNEW on 1130 kHz , all in New York City; WIIDII on 850 kHz in Boston on 850 kIIz and WCAU in Philadelphia on 1210 kHz .

Steve Whitt (london) reports "I can't wait for winter DX conditions to test my loop aerial and I'm looking forward to a batch of North American goodies". Steven is now using the PW medium wave loop acrial and balanced FET pre-amplifier (ApriI 1973) with his Chapman S6BS communications receiver and he reckons this aerial is far better, more sensitive and more directional, than his 30 ft longwire on the roof. Stations logged on this new set-up include Radio Andorra on 701 kHz , Radio Dakar in Senegal on 764 kIIz and CJON St. John's Newfoundland on 930 kIIz , three continents!

Harold Emblem sends a really outstanding $\log$ of summer DX heard at his QTH in Mirfield, Yorkshire, on an Eddystone 730/4 communications receiver using a long wire and a medium wave loop. DX heard includes CBT Grand Falls, Newfoundland on 540 kHz ; CKVO Clarenville, Nfld on 710 kHz ; CBNM Marystown, Nfld on 740 kHz ; WABC New York City on 770 kHz ; CBH Halifax, Nova Scotia on 860 kHz ; CJCH in Halifax on 920 kHz ; CBM Montreal on 940 kHz ; CHNS Halifax on 960 kHz ; WINS New York City on 1010 kHz ; WNEW also in NYC on 1130 kHz ; WCAU Philadelphia 1210 kHz ; CKEC New Glasgow, N.S. 1320 kHz ; WLAC Nashville, Tennessee on 1510 kHz and WKBW in Buffalo, N.Y. on 1520 kHz .

Peter Bowyer (Kettering) uses a Murphy A168 for DXing on the medium waves and reports hearing AFN Augsburg and Radio Tirana, Albania both on 1394 kHz and Trans World Radio, Montecarlo on 1466 kHz . Fifteen-year-old Stephen Boyle of Auchterarder, Perthshire used a Philips 90RL210 with an externally mounted MW loop. Stations logged include Radio Norway on 1578 kHz (in English at midnight GMT) and Radio Tirana, Albania on 1394 kHz again.

Joseph Bite (Dublin) and Derek Vivian (Jersey C.I.) ask which type of receiver is the most suitable for MW DXing. Communications receivers such as the Trio 9R59DS, AR88, CR100 or the Heathkit GR78 (which operates from batteries or mains) have the sensitivity and selectivity that will bring optimum results. Simpler receivers when connected to a good aerial will, however, pull in a considerable amount of DX on the medium waves.

## BROADCAST BANDS

Short Wave reports by the 15 th of the month to Derek Bell c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD. Medium Wave Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG.

## AMATEUR BANDS

Logs covering any amateur band/s in band/* alphabetical order by the end of the month to " Eric Dowdeswell G4AR, Silver Firs, Leatherhead s: Road, Ashtead, Surrey, KT21 2TW.

April 1965 and February 1966.-S. A. Rizvi, P.O. Box 2671 • Tripoli, Libya.
.December 1970 and January 1971 issues of P.W.-
J. M. Bell, 60 Wendover Road, Harlesden, London, NW10. all issues of P.W. including December 1971.-B. Dlsselmann, Skovlyporten 3-1, DK-2840, Holte, Denmark.
. issues of P.W. or the circuits of the P.W. Sound Effects Synthesiser first published in March 1971 (circults 3-11 wanted).-D. Weeks, S.A.C., K8093975, GESF, R.A.F. Wildenrath, B.F.P.O. 42.
.any back issues of Practical Wireless, Television.Cralg Sellen, Box 853, Wayne, N.J. 07470, U.S.A.
..Issues of P.W. containing instructions of the VHF Transistor Receiver with blueprint (around July 1965).J. W. Cooling, 33 Flat Sorrel Court, 1 The Green, Mt. Sorrel, Leicestershire.
. P.W. May 1971-J. Rendall, 59 Hood Avenue, Southgate, London, N14 4QJ. ..P.W. January 1972 to October 1972 Inclusive, P.W.
March 1973-June 1973 inclusive and P.W. October 1973...P.W. January 1972 to October 1972 Inclusive, P.W.
March 1973-June 1973 inclusive and P.W. October 1973.G. F. McCarthy, Ballymodan Place, Bandon, Co. Cork, Ireland.

## CQ! CQ! CQ! CQ!

## ISSUES WANTED

. Television for March, Aprll, May, June 1974.R. Mehrotra, F-114 D.D.A. Colony, Naraina, New Delhi-28, 110028, India.
. August 1973 Issue of P.W.-T. J. Flanagan, 17 Addison Crescent, Old Trafford, Manchester, M16 OWN.
. January to April 1973 P.W. Inclusive also June 1973 and March and April 1974 P.W.-K. Hunter, 31 Cwmbath Road, Morriston, Swansea, SA6 7BA.
. 1950 March, November, December. 1952 January March, April, August, September. 1953 May-all Practical Wireless. -J. Luxton, Bergheim, Battery Hill, Fairlight, Hastings, TN35 4AP.
.P.W. for February 1974, February 1966, Aprll 1969 and June 1969 plus any subsequent issues dealing with aerials, April 1970, June 1970 plus any subsequent issues dealing with the LF Bands Transcelver, April 1972. Also P.E. for

## IMPROVE YOUR BUDGET STEREO SYSTEM

-continued from page 574
cation I arranged that the audio is completely muted when tuning. Fig. 3 shows the final arrangement.

Any circuit changes should only be done after reference to the manufacturers circuit diagram to make quite sure that no unpleasant or even disastrous effects will result. The AFC circuit shown is common to almost all budget stereos. The AFC and audio are fed from the discriminator output via a high value resistance (typically $150 \mathrm{k} \Omega$ ) to the AFC switch. The AFC line is decoupled after the switch


Fig. 3: Spare contacts on AFC switch are used to switch-in an insensitive meter (see text for value of R). Note that the $150 \mathrm{k} \Omega$ resistor is moved to the new position $X Y$.
(typically $220 \mathrm{k} \Omega$ and $0.1 \mu \mathrm{~F}$ ). The $150 \mathrm{k} \Omega$ prevents the audio from being shorted to chassis when the AFC is disabled. In the new circuit arrangement, however, we want to lose it so that muting takes place when tuning, done by moving the $150 \mathrm{k} \Omega$ to the diode side of the switch. With printed circuit boards the easiest way of doing this is to short out the existing $150 \mathrm{k} \Omega$ with a wire link and to carefully cut the foil on the other side of the switch, bridging the gap with a new $150 \mathrm{k} \Omega$ resistor.
The end product is superior to that provided on more expensive systems. We tune for a peak on the meter in complete silence, selecting the wanted station by the position of the tuning scale and then switching in the AFC to take care of drift. The muting works quite smoothly and there are no loud noises when it is switched in and out.

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