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## also:

CAR WIPER DELAY UNIT MODEL TRAIN CONTROLLER


# bRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELEGTRONICS cONSTRUGTOR 

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negative overload is also provided The instrument is fitted with a combined carrying handle and combined carrying handle and provided for the connection of a external power supply. RANGES
DC VOLTS: $1 \mathrm{v}, 10,100 \mathrm{v} .1000 \mathrm{v}$ AC VOLTS: $1 \mathrm{v}, 10 \mathrm{v} .100 \mathrm{v}, 1000 \mathrm{v}$ DC CURRENT: $1 \mathrm{~mA}, 10 \mathrm{~mA}$ $100 \mathrm{~mA}, 1000 \mathrm{~mA}$. AC CURRENT:
$100 \mathrm{~mA}, 1000 \mathrm{~mA}$
RESISTANCE: $1 \mathrm{k}, 10 \mathrm{k}, 100 \mathrm{k}, 1000 \mathrm{k}$ OUR PRICE E59.95 P \& P 50p RUSSIAN CI16 Double Beam OSCILLOSCOPE 5 MHz pass band.
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$440 \mathrm{kHz}-280 \mathrm{MHz}$ in six coils. 500 Aa
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ted from 9 -volt battery. 100 microted from 9 -volt battery. 100 micro-
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| ${ }_{2004}^{1004}$.: .. | ${ }_{\substack{\text { f3.85 } \\ \text { E3.80 }}}$ |  |  |
| 50004. | ${ }^{\text {E33.75 }}$ |  |  |
|  | ${ }_{\text {¢ }}{ }_{\text {¢3.85 }}$ |  |  |
| 1 mA .. .. .. | E3.76 |  |  |
| 5 mA . | ${ }^{\text {c3, }}$ 565 |  |  |
| 10 mA .. | ¢ $\begin{gathered}\text { ¢3.76 } \\ \text { ¢3.75 }\end{gathered}$ |  |  |
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| ${ }_{5 A}^{14 D C}$ DC.. | c3,76 | 300 VDC 15 VAC | cele |
| 10ADC .. | ${ }_{\text {E }} \mathbf{8 3 . 7 5}$ | 300 AC VOM Mer |  |
| 5 V DC | E3.75 | VU Moter | ع4.09 |


| CLEAR PLASTIC MODEL SW100 <br> Size: $100 \times 80 \mathrm{~mm}$ |  |  |  |
| :---: | :---: | :---: | :---: |
| 50 i A . | E4.70 |  |  |
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| 500uA $50.0 .504 A$ | E4.40 ¢ 4.60 |  |  |
| $100-50100 \mathrm{HA} .$. | C4.60 |  |  |
| 1mA ... .. | ¢4.40 |  |  |
| 1ADC* | ¢4.40 | , |  |
| 5ADC - .. | ¢4.40 |  |  |
| $20 V$ DC .-. | ¢4.40 | 150 V AC .. .. | C4.55 |
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CLEAR PLASTIC

| 100at ${ }^{\text {gre }}$ | ${ }_{5}^{56.60}$ | \%ecentrex |  |
| :---: | :---: | :---: | :---: |
| 200uA .. - | ¢5.60 |  |  |
| 500 uA | C5.40 |  |  |
| 50-0-504A .. | c\$.56 |  |  |
| 100-0.1004A.. | ¢5.50 $\mathbf{5 5 . 3 5}$ | = |  |
| 1 mA | E6.36 |  |  |
| 1-0.1mA .. | ¢5.35 |  |  |
| 5 mA .. .. | f5.35 |  |  |
| 10 mA | ¢5.35 |  |  |
| 50 mA .. .. | ¢5.35 |  |  |
| 100 mA .. .. | ¢5.35 | 300 V DC .. | E5.40 |
| 500 mA .. .. | c5.35 | 15 V AC .. | f6. 45 |
| 1ADC .. .. | f5. 35 | 300 V AC .. | c5.45 |
| 5A DC | E5.35 | S Metar 1mA.. | f5. 35 |
| 15A DC | E5.35 | VU Mater .. | c5.70 |
| 30A DC .. .. | ${ }_{6} 5.55$ | TA AC .. | c5. 35 |
| 10 V 0 | c5.35 | $5 A$ AC | f5.36 |
| 20V DC | f5.35 | 10A AC .. .. | f5.35 |
| 50 V DC | c5. 35 | 20A AC ., | C5.35 |
| 150V DC ., | c5. 35 | 30A AC .. .. | f.5.35 |



## CLEAR PLAST Size: $42 \times 42 \mathrm{~mm}$

## 504 A 100 uA

200 hA
$500 \mathrm{u} A$
$50-0.50 \mathrm{uA}$
$500-50 \mathrm{uA}$
$100.0-100 \mathrm{u}$
$500.0-500 \mathrm{uA}$..
$\underset{\substack{10-1 \mathrm{~mA} \\ 2 \mathrm{~mA}}}{\operatorname{lom}^{2}}$
2 mA
5 mA
10 mA
5 mA
10 mA
20 mA
20 m
50 m
100
150
50 mA
100 mA
150 mA
200 mA
300 mA
500 mA
750 mA
1 ADC
$2 A \mathrm{DC}$
$5 A D C$
10 DDC
$3 V D C$
$10 V \mathrm{OC}$
$15 \cup$ OC

## CLEAR PLAS Size: $59 \times 46 \mathrm{~mm}$

$50 \mathrm{uA} \times 46 \mathrm{~m}$

50uA
A-100
$A$.
A..
$m A$
DA
$D C$
DCC





##  <br> 20 V DC 50 V 100 V 150 V 300 V 500 V 750 V 15 V 50 V 150 V 300 V 500 V SMe <br> $D C$ $D C$ $D C$ $D C$ $D C$ $D C$ $A C$ $A C$ $V A C$ $A C$ $A C$ <br> 令: : : : : : : : : : : <br> 

BA
250
50
100

50
BAKELITE MODEL MR 65 Size: $80 \times 80 \mathrm{~mm}$
$25 u A$
501
1000
5004
CLEAR PLASTIC MOOEL MR GEP
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|  |  |  |  |  |  | UBC81 | $0 \cdot 50$ | 6 SLLFGr | 0.65 |
| SAE for lists. |  |  |  |  |  | UBF80 | 0.50 | 6SN7GT | 0.55 |
|  |  |  |  |  |  | UBF89 | 0.60 | 68Q7GT | 0.40 |
| AZ1 | 0.75 | EF39 | 1.25 | MU14 | 1.00 | UCG85 | 0.80 | 6U6G | 1.50 |
| AZ31 | 0.60 | EF80 | 0.85 | N78 | 3.60 | UCH | $0 \cdot$ | 6V6G | 0.80 |
| CBL31 | 1.40 | EF85 | 0.45 | 0.42 | 0.45 | UCH8 | 0 | 6V6GT | 0.60 |
| CL33 | 1.60 | EF86 | 0.80 | OB2 | 0.45 | UC | O | ${ }_{6 \times 4}$ | 0.45 |
| CY31 | 0.60 | EF89 | 0.85 | ${ }^{\text {PC86 }}$ | 0.65 | UF41 | 0 | 6X5G | 0.45 |
| DAF91 | 0.40 | HF91 | 0.40 | PC88 | 0.65 | UF41 | 0.75 | 6X5ET | 0.55 |
| DAF96 | 0.60 | EF92 | 0.60 | PC97 | 0.55 | UF8 | 0.50 | 7B6 | 0.80 |
| DCC90 | 1.85 | EFP95 | 0.46 | ${ }^{\text {PC900 }}$ | 0.55 | UL41 | $0 \cdot 85$ | 7B7 | 0.80 |
| DF91 | 0.40 | EF98 | 0.80 | PCC84 | 0.45 | UL84 | 0.60 | $7 \mathrm{C5}$ | $1 \cdot 80$ |
| DF96 | $0 \cdot 60$ | EF183 | 0.40 | PCC88 | 0.62 | UY485 | 0.55 0.45 | ${ }_{7}^{706}$ | 1.00 |
| DK91 | 0.60 | EFIP4 | 0.40 | PC089 | 0.55 | $\mathrm{UY85}^{\text {VR105/30 }}$ | 0.45 | ${ }^{7} \mathbf{7 8 7}$ | 0.80 |
| DK92 | 1.00 | EL32 | 0.60 | PCCi89 | 0.65 | VRL150/30 | 0.40 | 787 | 0-80 |
| DK96 | 0.75 | EL33 | $2 \cdot 50$ | PCF80 | 0.40 | IRS | 0.50 | ${ }_{7}^{787}$ | 2.85 0.80 |
| DL92 | 0.50 0.48 | EL34 | 0.70 0.60 | PCF82 | 0.42 | 185 | 0.40 | $7 Y 4$ $12 A T 6$ | 0.80 0.45 |
| DL96 | 0.55 | EL37 | 250 | PCF | 0.60 | 1T4 | 0.40 | 12AT7 | 0.45 |
| DY86 | 0.45 | EL41 | 0.90 | PCF880 2 | 0.60 | 384 | 0.50 | 12AUG | 0.60 |
| DY87 | 0.45 | EL49 | 1-65 | PCF805 | 0.90 0.90 | 3V4 | 0.85 | 12AU7 | 0.88 |
| DY802 | 0.47 | EL84 | $0 \cdot 85$ | ${ }^{\text {PCF }} 808$ | ${ }_{0}^{0.80}$ | 5R4GY | 1.00 | 12AX7 | 0.88 |
| EABC80 | 0.88 | EL95 | 0.80 | PCF808 | 1.00 | 5U4G | 0.55 | 12BA6 | 0.50 |
| EAF42 | 0.70 | ELL80 | 2.00 | PCL88 | 0.45 | ${ }_{5 \mathrm{~S} 4 \mathrm{C}}^{\text {5 }}$ | 0.65 | 12BE6 | $0 \cdot 60$ |
| EB91 | 0.85 | EM80 | 0.56 | PCL83 | $0 \cdot 70$ | 6/30L2 | 0.85 0.90 | 30 Cl | 0.40 |
| EBC33 | 1.00 0.75 | EM81 | 0.80 | PCL84 | 0.50 | 6AK5 | 0.45 | 30015 | 1.00 |
| EBC41 | 0.76 0.40 | EM84 | 0.40 | PCL85 | 0.60 | 6AK5 | 0.45 1.00 | $30 \mathrm{Cl7}$ | 1.00 |
| EBF80 | 0.40 | EM85 | 1.00 | PCL86 | 0.50 | 6AQ5 | 0.50 |  | . 60 |
| EBF89 | 0.40 | EY51 | 0.45 | PCL806/85 |  | 6AS7G | 1.00 | 30F6 | .00 |
| ERF89 | 0.82 | EY86 | 0.45 |  | $0 \cdot 60$ | 6AT6 | 0.60 | 30 FLL 2 | 1.00 |
| EBL31 | 8.00 | EZ40 | 0.80 | PD500 | $1 \cdot 60$ | 6aU6 | 0.40 | 30 FL 14 | 1.00 |
| ECC81 | 0.45 | EZ41 | 0.75 | PENA5 | $0 \cdot 85$ | 6BA6 | 0.38 | 30 L 15 | 0.95 |
| ECCO82 | 0.88 | EZ80 | 0.80 | PL36 | 0.68 | 6BE6 | 0-45 | 30 L 17 | 0.95 |
| ECC83 | 0.38 | E281 | 0.31 | PL81 | 0.65 | 6BH6 | 0.75 | $30 \mathrm{P4M}$ | 1.80 |
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| ECOS | 045 | Gz30 | 0.66 | PL83 | 0.60 | 6BQ7A | 0.55 | 30P19 | 0.95 |
| ECC88 | 0.60 | GZ32 | 0.65 | PL84 | 0.50 | 6BR7 | 1.80 | 30PL1 | 0.95 |
| ECH35 | 1.50 | GZ34 | 0.75 | PL500 | 0.85 | 6BS7 | $1 \cdot 40$ | $30 \mathrm{PL13}$ | 1.10 |
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E12: 10, 12, $15,18,22,27,33,39,47,56$,
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E24: 11, 13, 16, 20, 24, 30, 36, 43, 51, 62.
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Values available: $5 \mathrm{k}, \quad 10 \mathrm{k}$. $25 \mathrm{k}, 50 \mathrm{k}, 100 \mathrm{k}, 250 \mathrm{k}, 500 \mathrm{k}$. 1M, 2M.
Log. Siagle-gang
Lin, Single-gang (+1K) 17p
Log. or Lin. Single-gang with
switch
$\mathbf{3 6 p}$ $\underset{\text { without switch. }}{\text { Log. }}$ or Lin. ${ }_{54 \mathrm{p}}^{\text {Ling }}$ Slider 60 mm track. Myetal (knob extra 7p)
Values available: 1k; $5 \mathrm{k} ; 10 \mathrm{k}$. 25k; $20 \mathrm{k} ; 100 \mathrm{k} ; 250 \mathrm{k} ; 500 \mathrm{k}$; 1M; 2M.
Lin. Single Gang Log Single Gang 86 p
88 p
$\mathbf{4 5 p}$ Presets: 0.1W Vertical or Horizontal. ${ }_{4 \mathrm{k}}^{102} \Omega, 220 \mathrm{k}, 470 \Omega, 1 \mathrm{~K}, 2 \mathrm{k} 2$. ${ }_{220 \mathrm{k},}^{4 \mathrm{k} 7} 10 \mathrm{k}, \mathrm{k}, 1 \mathrm{M}, ~ 47 \mathrm{k}, 100 \mathrm{k}$.

## © CAPA

Sub-miniature
Axial 1 ead electrolytic

|  |  | Mid |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6p |  |  |  |  |
|  | 6p | $68{ }^{16}$ |  |  |  |
|  | ${ }^{6 p}$ | 68.63 |  |  |  |
|  | ${ }^{\text {bp }}$ | 1.00 | I | fit | $\checkmark$ Price |
| 40 | ${ }^{\text {6p }}$ | 10010 | p |  |  |
| 63 | 6p | 100 | ${ }^{60}$ | 470 | 2516 p |
| 25 | 6p | 10063 | 16 D | 470 | 40 25p |
| 63 | 6 p | 1506 | d | 680 | 6-31 |
| 16 | 6p | 15016 | 8D | 680 | 16 16p |
| 40 | ${ }^{6 p}$ |  | ${ }^{\text {6p }}$ |  | 25 25p |
| 63 | 6p | 15040 | 14p | 680 | 40 |
| 10 | 6p | 15063 | 16p | 1000 | 414 p |
| 25 | ${ }^{60}$ | 2204 | ${ }^{60}$ | 1000 | $10 \mathrm{16p}$ |
| 63 | ${ }^{\text {bp }}$ | 22010 | 67 | 1000 | 16 25p |
| 6.3 | 6p | 22016 | ${ }^{60}$ | 1000 | 25 28p |
| 16 | ${ }^{\text {6p }}$ | 22025 | 14p |  | 6.316p |
| 40 | 6p | 3340 | d | 1500 | 10 25p |
|  | Bp | 22063 | 258 | 1500 | 16 28p |
| 10 | 6p | 330 | ${ }^{60}$ | 2200 | 6.325p |
| 25 | 6 p | 33310 | ${ }^{60}$ | 2200 | 10 25p |
|  | 6p | 33016 | 14p | 3300 | 6.328p |
| 63 | 6p | 33063 | 28p |  | 4 28p |
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| P360 3-pin 1.5A Chassis Plug with |  |  |  |  |  |
| SA2190 3-pin 5 A Chassis Plug |  |  |  |  |  |
| SA1862Linesocket tor |  |  |  |  |  |
|  |  |  |  |  |  |
| P437 3-pin 5A Chassis Socket with Line Plug 66p |  |  |  |  |  |

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 \& DIODES

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MFC4000B
MFC6040
NE555V (8-pin DIL

TG3402
$\mu \mathrm{A} 741 \mathrm{C}$ (8-pin DIL)
$\mu \mathrm{A} 741 \mathrm{C}(14-\mathrm{pin} \mathrm{D}$ ${ }_{\mu}{ }^{\mu 7774 C}$ (14-pin DIL) $)$ $\mu$ AF48C (8-pin DIL) ZN414 (TO18)
VOLTAGE REGOLATOR
 $\mu \mathrm{A} 8815 \mathrm{~F} 5 \mathrm{~V} 1.5 \mathrm{~A}$ (TO3) El .75
$\mathrm{MNR} 5 \mathrm{~V}, 12 \mathrm{~V}, 15 \mathrm{~V}, 500 \mathrm{~mA}$ (T03)
$\mu 178 \mathrm{MO} 55 \mathrm{~V} 50 \mathrm{~mA}$
$\mu \mathrm{A} 8 \mathrm{ML5} 15 \mathrm{~V} 500 \mathrm{~mA}$ ) 51.05 $\mu A 78 \mathrm{ML5}$
(Plastic Dower)
500 mA
(Plastic power) $61 \cdot 05$ $\mu \mathrm{A} 78 \mathrm{LO} 5 \mathrm{SV}$
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9 p
10 p
10 p
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Open-type metal
It
Std. Mono Open-type metal

9p
9p
10p
" Std. Mono Moulded with ${ }^{2}$
break contacts 149
$4^{\prime \prime}$ Std. Stereo Open-typt
metal

break contacts
PHONO
Pastic-topped Plug
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Chassis Socket Single

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 $5 \Omega 200 \mathrm{~mW}$50p

- 100 mi 85p
(Size both approx, $30, \geq 7,25 \mathrm{~mm}$ ) Min. mains
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 $\begin{array}{lllllllll}100 & 0.28 & 0.32 & 0.52 & 0.59 & 0.52 & 0.55 & 0.59 & 1.27 \\ 200 & 0.39 & 0.41 & 0.54 & 0.54 & 0.55 & 0.64 & 0.70 & 1.54 \\ 400 & 0.48 & 0.54 & 0.68 & 0.82 & 0.64 & 0.67 & 0.83 & 1.76\end{array}$ $\begin{array}{lllllllll}400 & 0.48 & 0.51 & 0.34 & 0.54 & 0.63 & c .67 & 0.83 & 1.76 \\ 600 & 0.59 & 0.68 & 0.75 & 0.82 & 0.74 & 0.88 & 1.03 & 1.98 \\ & 0.75 & 0.85 & 1.07 & 1.38 & \end{array}$ $\begin{array}{ccccccccccc}600 & 0.59 & 0.68 & 0.75 & 0.75 & 0.85 & 1.07 & 1.38 & - \\ 800 & 0.70 & 0.77 & 0.88 & 0.88 & 0.99 & 1-32 & 1.65 & 4.40\end{array}$

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PIV $300 \mathrm{~mA} 750 \mathrm{~mA} \quad 1 \mathrm{~A} \quad 1.5 \mathrm{~A} 3 \mathrm{~A} \quad 10 \mathrm{~A} \quad 30 \mathrm{~A}$ $\begin{array}{lllllllllll}50 & 0.05 & 0.06 & \text { 1N4001 } & 0.05 & 0.08 & 0.15 & 0.21 & 0.60\end{array}$ $\begin{array}{llllllllll}100 & 0.06 & 0.70 & 1 N 4002 & 0.06 & 0.10 & 0.17 & 0.23 & 0.75\end{array}$ $\begin{array}{lllllllll}200 & 0.08 & 0.10 & 1 N 4003 & 0.07 & 0.12 & 0.22 & 0.25 & 1.00 \\ 400 & 0.08 & 0.15 & 1 N 4004 & 0.08 & 0.15 & 0.30 & 0.38 & 1.35\end{array}$ $\begin{array}{llllllllll}600 & 0.09 & 0.17 & 1 N 4005 & 0.10 & 0.18 & 0.36 & 0.45 & 1.95\end{array}$ $\begin{array}{llllllllll}800 & 0.12 & 0.19 & \text { 1N } 4006 & 0.11 & 0.20 & 0.38 & 0.55 & 2.10\end{array}$ $\begin{array}{cccccccccccc}1000 & 0.14 & 0.30 & 1 N 4007 & 0.12 & 0.25 & 0.48 & 0.65 & 2.50 \\ 1200 & 10.35 & & & 0.30 & 0.58 & 0.75 & 8.00\end{array}$

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$$
\begin{array}{ccc}
\text { Programme } & \text { Hot Water } & \text { Central Heating } \\
0 & \text { Oft } & \text { Of } \\
1 & \text { Twice Daily } & \text { Off } \\
2 & \text { All Day } & \text { Oft } \\
3 & \text { Twice Daily } & \text { Twice Daily } \\
4 & \text { All Day } & \text { All Day } \\
4 & \text { Continuously } & \text { Continuously } \\
5 & \text { cencrame other than central heati }
\end{array}
$$



Sultable, of course, to programme other than central heating and hot water, for instance, programme upstairs and downstairs electric heating or heating and this Programner. Maing operateri. Size 3in $\times 3$ in $\times$ 2in deep. Price 84.85 as thisetrated but lyss case.


## TAPE DECK

In metal casee with carrylng handle, heavy Hy Fheel and capptan drive. Tape speed 3. Mains operated on metal plationm win tape head and
guide. Not new but in good order. Price $\varepsilon 1 \cdot 95$ gadde. Not new but in goo
plus 81 post and insurance.

## TANGENTIAL HEATER UNIT

This heater unit is the very latest type, most efficient and quiet runuing. Is as fitted in Hoover and blower hesters costing $£ 15$ and more. We have a few only Comprises motor, impelier, with thermal safety out ut. Can be fitted into any metal line case or cabinet
 Only peeds control switch. 2 kW Model $42 \cdot 75$. Don't
miss this. Control Switeh 44 p plus YAT. P. ${ }^{2} \mathrm{P}$. 40p.

## SHORTWAVE CRYSTAL SET

Although this uses no battery it gives really amazing results. You will receive an amazing assortment of stations over the 19.25 .31 .39 metre bands-Kit contains chassis front panel and all the parts. $81 \cdot 25-c r y s t a l$ earphone 50p.
SPIT MOTOR
$200-250 \mathrm{~V}$ Induction motor, तriving a Carter gearbox with 3 1t" output drive shaft running at 5 revs p.m. Intended or rossting chickens, aljo for ariving modelo- windmiling,
coloured disc ighting effects, etc. $\mathbf{2} 2.50$ plus 200 post and ins.

## INFRA-RED BINOCULARS

 Made for military purposes during
and immediately after last war to enable snipers, vehicle drivers, etc to see in the dark. The binoculars have to be fed from a high voltage source ( 5 KV approx.) and pro viding the objects are in the rays of an intra-red beam, then the binoculars will enable these objects tube contains a complete optical lens system as well as the infra-red cell, tech tube contsins a complete optical lens system as well as the infrawred cell, tech good working order. In tact they were never issued and are still in original coses, but since they were made a long time ago, they can hard
without guarantee. Price $\mathbf{1 1 6 \cdot 5 0}$ per aet + fi carriage.
BATTERY CHARGERS
Famous Atlas in metal case with meter, output leads terminated by crocodile clipg. For 6 or 12 y charging simply in maker's original packing. Two models: 1it amp al- 89 and $3-4 \mathrm{amp} 82.98$. Please add 40 p postage for one and 75 p


12 VOLT I $\frac{1}{2}$ AMP POWER PACK
This comprises double-wound $230 / 240 \mathrm{~V}$ mains trans Price 28.50 plus 20 pert Power Pack. Output voltage adjustable from $15-40 \mathrm{~V}$ in ateps-maximum load 250 W -that is from 6 amp at 40 V to 15 arnp at 15 V . This really is a high power heavy duty unit with dozens of workshop uses. Output voltage adjust ment is very quick-simply interchange push on
moothing by $3,000 \mathrm{mF}$. Price $26 \cdot 95$ plus 81.00 post.

TERMS:-ADD 8\% V.A.T.
Send postage where quored-other items, post free if order for these items is 16.00 , otherwise add 30 p

NEW ITEMS THIS MONTH
The bargains in this column are just some of the tems which appeared in the Decomber supplement to our catalogue. Fou can recelve thit catalogue and the
Ireboratory volt meter, ES1. This is the conventional square care, size $7^{\prime \prime} \times 7^{\prime \prime} \times 3 \frac{1^{\prime \prime}}{}$ with a leather carrying handle and robber feet for horizontal and vertical standing. The meter is intended for horizontal use on the bench and has a mirrored scale. Hefty terminals along the top delect the 3 ranges $0-150 \mathrm{v}, 0-300 \mathrm{v}$ and $0-600 \mathrm{v}$ D.c. Price 26 plus ai post and insurance.

Laboratory amp meter, companion instrument to the above, but to read $0-20$ amps 50 cycles, 55 plus 5
Soil heating transformer, $4 v, 5 v$ or $6 v$ outpat, very heavy duty secondary rated at 250 amps , price 820 plus carriage $f 2$ first 100 miles then $\$ 1$ per 100 miles extra.
7 watt atereo/mono amplifier with usual awitching and controls, in attractive teak style case, 29. 3 core lead, $7^{\prime \prime} 6^{\prime \prime}$ long, ribbed, virtually noңkinkable $23 / 36$ conductors, so OK for 8 amps .
Price 10 p each.
0-1 mA meter $2 \frac{1}{2}^{\prime \prime}$ square, Hush mounting, English make ex equipment but perfect. \&1-76. 0-100 microamp meter, as the above, but 22-25. Solenoid 4-6v, size approx. $1^{\prime \prime} \times 1^{\prime \prime} \times 4^{\prime \prime}$ thick, twin coils give excellent pull. Mounted in frame but easily removeable from this frame, ftted with
lever giving approx. $4^{\prime \prime}$ push or pull. Price 80 p lever

Cold cathode tube Swiss made "Elasta" type no. ER 12A. We have no technical information on this tube and if any reader has this we will be obliged for any information. Price of the tubes
80 p each.
AC maina operated relay with single changeover 10 amp contacts, open type single screw fixing through the base. 50 p each.


Push switch, metal
body and metal
push, normally on.
These are replace-
ments in many
"break glass, fire
alarms. Made by
Arrow, contact rat-
fng 250v 5 amps. 80p each.

## MAINS TRANSISTOR POWER <br> <br> PACK

 <br> <br> PACK}Designed to operate translstor sets and amplifiers. Adjustable output $6 \mathrm{~V} ., 9 \mathrm{~V} ., 12$ Takes the place of any of the following
batteries: PP1, PP3, PP4, PP6, PP7, PP9 and others. Kit comprises: main transiormer
rectifler, smoothing and load resistor, conrectifer, smoothing and load resistor, condensers and instructions. Real snip at only
$\$ 1 \cdot 50$.

Puih witoh, double pole changeover contacts rated at 10 amps 250 volts made by the American Honeywell Co. A very reliabie and robust switch with plenty of applications, Oblong plastic body, only a fraction of its proper price, namely $80 p$

Ditto but single pole changeover, fits into a hole Size $1 \times$. Price 15 p each. the two switches above do not require a knob as they have a pollshed and tapered plunger). Ditto, but dished knob. 100 extra with knob.
Two now speakers, $5^{\prime \prime}$ round 8 ohm impedance 5 watt output, $21 \cdot 65$ plus 200 post and 5 midG GOODMANS speaker don't misg it . ${ }^{\text {GOODMANS speaker don't ralss it) }}$
AN/FHM tuning condenser as fitted to many Japanese and Homp Kong portables, this has two main tuning sections and four trimmers, approx
Battery charger kit comprising 2 amp transformer, 2 amp full wave rectifter and 2 amp meter suitable for charging 6 y or 12 v . Special bargain price 1.50 the kit plue 30p port

MacDonald record auto-changer with cueing arm
and ceramic stereo cartridge. This is a very and ceramic stereo cartridge. This is a very superior auto changer and one we can thoroughly plus \&l post and finurance. Plinth and cover (the plins th has to be modiffed very slightly) available price 84.95 plus 61 post, or if yout buy both together you can get a discount of $\& 1$.


Instrument case measures $18^{\prime \prime} \times$
$12^{\prime \prime} \times 12^{\prime \prime}$. This is a very well-made case bnit up on an angled frame work specially designed for instruments which has rounded corners and edges. Into thts framework fits the 8 panels. All
panels are louvred for ventilation, side panels are also fitted with handles which drop down and in the down poistion are almoat fiush; the bottom panel has four rubber feet, the ment panel and fuses, the front panel you provide yourself. These instrument cases would probably cost around $\boldsymbol{z 1 5}$ each. We have approx. 100, not new but in very good condition and offer them at \% each plus carriage.
Battery condition testers. This is another item we are pleased to say in stock again. Price now $\$ 3.50$.

目田回＊COMPLETE STEREO SYSTEM
System 1a．£62．00
40 Watt Amplifier．Viscount III－R102 now 20 watts per channel（ 40 watts peak）．
All systems include：
Viscount III amplifier－volume，bass，treble and balance controls，plus switches for mono／ stereo，on／off function and bass and treble filters．Plus headphone socket． Specification：
20 watts per channel into 8 ohms 40 W peak．Total distortion＠ $10 \mathrm{~W} @ 1 \mathrm{kHz} 0.1 \%$ ．P．U．I （for ceramic cartridges） 150 mV into $3 \mathrm{Meg} . P . U .2$（for magnetic cartridges） 4 mV at 1 kHz into 47 K ．equalised within +1 dB R．IA．A．Radio 150 mV into 220 K ．（Sensitivities given at full power）．Tape out facilities：headphone socket，power out 250 mW per channel．Tone controls and filter characteristics．Bass：+12 dB to $-17 \mathrm{~dB} @ 60 \mathrm{~Hz}$ ．Bass filter： 6 dB per octave cut．Treble control：treble +12 dB to $-12 \mathrm{~dB} @ 15 \mathrm{kHz}$ ．Treble filter： 12 dB per octave． Signaf to noise ratio．（all controls at max．）－58dB．Crosstalk better than 35 dB on all inputs．Overload characteristics better than 26dB on all inputs．Size approx． $13 \frac{3}{3} \times 9^{\prime \prime} \times 3 \frac{3^{\prime}}{}$.
Garrard SP 25 deck with magnetic cartridge，de luxe plinth and cover．
Two Duo Type Ha matched speakers－Enclosure size approx． $19 \frac{1^{\prime \prime}}{4} \times 9 \frac{1}{2}^{\prime \prime} \times 7 \frac{34^{\prime \prime}}{}$ in simulated teak．Drive unit $13^{\prime \prime} \times 8^{\prime \prime}$ with $3^{\prime \prime}$ tweeter． 15 watts handling． Complete System with these speakers $\mathbf{f} 62.00+£ 5.50 p$ \＆$p$ ．
System 2． $\mathbf{f 8 2 . 0 0} \quad$ Viscount III amplifier（As System 1a）
Garrard SP 25 deck（As System 1a）
Two Duo Type III matched speakers－Enclosure size approx． $27^{\prime \prime} \times 13^{\prime \prime} \times 11 \frac{1}{2}$＂Finished in teak simulate．Drive units $13^{\prime \prime} \times \mathbf{8}^{\prime \prime}$ bass driver，and two $3^{\prime \prime}$（approx．）tweeters． 20 watts RMS， 8 ohms frequency range -20 Hz to 18.000 Hz ． Complete System with these speakers $£ 82.00+\mathrm{f} 6.50 \mathrm{p} \& \mathrm{p}$ ．

PRICES：SYSTEM 1a

| Viscount III R102 <br> amplifier | $£ 27.00+£ 1.60 \mathrm{p} \& \mathrm{p}$ |
| :--- | :--- |
| 2 Duo Type fla speakers | $£ 26.00+£ 5.50 \mathrm{p} \& \mathrm{p}$ |
| Garrard SP 25 with Mag．cartidge <br> de luxe ptinth <br> and cover | $£ 21.00+£ 2.80 \mathrm{p} \& \mathrm{p}$ |

$+£ 5.50 \mathrm{p} \& \mathrm{p}$

## PRICES：SYSTEM 2

| Viscount III R102 <br> amplifier | $£ 27.00+£ 1.60 p \& p$ |
| :--- | :--- |
| 2 Duo Type IH speakers | $£ 39.00+£ 6.40 p \& p$ |

Garrard SP 25 with Mag．cartridge
de fuxe plinth
and cover
£21．00＋£2．80p\＆
total： $\mathbf{8 8 7 . 0 0}$
Available complate for only： $\mathbf{f 8 2 . 0 0}$
$+£ 6.50 p \& p$

## EMI SPEAKERS AT FANTASTIC REDUCTIONS

## LE－4 SPEAKERS

Superb performance and beautifully finished in selected teak veneers．A professional standard four－way speaker system giving 25 watts RMS power handling．Bass unit is $14^{\prime \prime} \times 9^{\prime \prime}$ with $8^{\prime \prime} \times 5^{\prime \prime}$ unit for mid－range and twin $3^{\prime \prime}$ high frequency units to give monitor type quality and performance．
Specification－Size $33^{\prime \prime} \times 14^{\prime \prime} \times 16^{\prime \prime}$ approx．Impedance 8 ohms．Power handling 25W RMS．（Peak 50 watts．） Frequency range $35 \mathrm{~Hz}-20 \mathrm{KHz}$ ．
Our Price $\mathbf{£}^{29.00}$
（normally $f 56.97$ ）$+f 5 p \& p$ ．

## EASY TO BUILD SPEAKER KITS

These superb simulated teak－finished speaker kits have been specially designed by RT－VC for the cost－conscious hi－ 4 i enthusiast who wants top quality speakers but doesn＇t want to spend the earth．Built to EMI＇s exacting specification， these new RT－VC speaker kits（ 350 type kit） incorporate $13^{\prime \prime} \times 8^{\circ}$ woofer， $3 \frac{1}{4}^{\prime \prime}$ tweeter and matching crossover．
Easily put together with just a few basic tools． Spocification（each speaker）：Impedance 8 ohms． Power handling 15 watts RMS（ 30 watts peak） Response $20-20,000 \mathrm{~Hz}$ ．Size $20^{\prime \prime} \times 11^{\prime \prime} \times 9 \frac{1}{2}$＂ approx．Comparable built units（EMI LE3）sold elsewhere for over £45 pair．
£18．95 pair complete
Complate with crossover Components and cricut tragram

EMI 350 KIT System consists of a $13^{\prime} \times 8^{\prime \prime}$ approx．woofer with a $3^{\prime \prime}$ tweeter， crossover components and circuit diagram．Frequency response： 20 Hz to 20 KHz ．Power handling 15 watts RMS into 8 ohms． （Peak 30 watts．）
Completa with crossover Components and circuit diagram $\mathbf{f 5 . 5 0}+£ 1 p \& p$ ．

## 20 WATT SPEAKER SYSTEM＊



System consists of a $13^{\prime \prime} \times 8^{\prime \prime}$（approx．）eliptical wooter unit with a $8^{\prime \prime} \times 5^{\prime \prime}$（approx．）mid－range unit incorporating parasitic tweeter and crossover compenents and circuit diagram
Technical Specification：Bass Unit：Flux density－ 100 K ，speech coil $-1 \frac{1}{2}$＂．Cone．Triple laminated paper with P．V．C．surround．Mid－Range Unit：Flux density－ 33 K ，speech coil－ $1^{\prime \prime}$ with parasitic tweeter．Power handling： 20 watts RMS，impedance－ 8 ohms， frequency response－Dur Price $\mathbf{f 7 . 5 0}$ 20 Hz to $18,000 \mathrm{~Hz}$ ．

Complete $+\mathrm{f} 1.35 p \& p$ ．

## DECCA STEREO AMPLIFIER CHASSIS <br> Specification：4＋4 watts into 8 ohms．Input Sensitivity 4 mV into 47K（for magnetic cartridges）．AC Mains only 240 V ．Controls－volume hass，treble，on／oft，mono／stereo switch．Chassis size 11 ＂$\times 5 \frac{1}{2} \frac{1}{2}^{\prime \prime} \times 3 \frac{1}{4}{ }^{\prime \prime}$ approx． <br> £5．95＋ $\mathrm{f1} \mathrm{p}$ \＆ p ． <br> 

## PUSH BUTTON CAR RADIO KIT- THE TOURIST TT*

 NO SOLDERING REQUIRED

NOW BUILD YOUR OWN PUSH BUTTON CAR RADIO
Easy to assemble construction kit comprising fully completed and tested printed circuit board on which no soldering is required. All connections are simple push fit type making for easy assembly. Fine tuning push button mechanism is fully built and tested to mate with printed circuit board. TECHNICAL SPECIFICATION: (1) Dutput 4 watts RMS output. For 12 volt operation on negative or positive earth. (2) Integrated circuit output stage, pre-built three stage IF Module.

Controls volume manual tuning and five push buttons for station selection, illuminated tuning scale covering full, medium and long wave bands. Size chassis 7" wide 2" high
and $4 \frac{3}{4}$ " deep approx. $\quad \mathbf{~} 8.00+90 p$. p \& $p$ Speaker including baffle and fixing strip $£ 1.65$ $+37 p$ p \& p. Car Aerial Recominended - fully retractahle $£ 1.37+32 \mathrm{p}$ p \& p .
The Tourist I Kit For the experienced constructor. If you can solder on a printed circuit board you can build this model. Same technical specification as Tourist TT. Price $\mathbf{£ 7 . 0 0}+90 p \mathrm{p}$ \& $p$.


## Fact not Fiction

THE varicap silicon junction diode, with its variable capacity effect, has been with us for many years. There is widespread use of these devices in tuner heads for domestic VHF/FM and TV and UHF TV for automatic frequency control (AFC) and/or electronic tuning. The use of low-cost varicap diodes has been restricted to these applications because of the limited capacity swing they offer.
Numerous manufacturers with an eye on the market potential of this device, have been actively engaged in the development of varicaps that fulfil the special requirements of long and medium waveband receivers.
In recent months these long-awaited devices have been released by Motorola in several combinations. The MVAM1 triple varicap package forms the "heart" of the "PW Apollo"' Triple Varicap Medium Wave Tuner/Receiver appearing in this issue.
Thus overnight, electronic tuning for long and medium waveband receivers is fact and not fiction for the home constructor. To this end, a new-style slider potentiometer was commissioned for the PW "All Electric Wireless" to simplify the tuning arrangements.

Remote control tuning is no problem. During tests on the prototype PW receiver, remote control tuning was achieved with the slider potentiometer connected to the receiver chassis via 30 metres ( 100 feet approx.) of cable!

The "PW Apollo" series will reveal, month by month, a number of fascinating applications utilising this new unique varicap package. Just to whet your appetite, this triple (or double) varicap device could be used in conjunction with a general coverage receiver and oscilloscope to give a spectural display of radio signals. Also, how about an electronic remote tuning car radio with the AM/FM radio unit tucked away safely in the car boot?

The applications of this new varicap package are numerous and we prophesy that it will bring about many radical changes and new ideas in electronic technology. The PW "All Electric Wireless" could set the trend and be the forerunner of a multitude of receiver designs that will now permeate our exploding technology.

Begin reading the facts in the "PW Apollo" series, Part 1 on page 44.

LIONEL E. HOWES, Editor.

## Bentley Acoustic Corporation Ltd.

Following complaints from readers we have now received an undertaking from Bentley Acoustic Corporation Ltd., that their practice of deducting expenses from refunds made to readers has now ceased and we are assured that all future refunds will be made in full.

## Write to them

 HIS year seems to have got off to a relatively slow start when it comes to news of the latest happenings in the electronics world. The PW office usually receives a mountain of press releases that take a fair time to sort out. However, after thumbing our way through the correspondence that has arrived, and we must add, throwing out that more applicable to Nuclear Research Stations and the like, we've come up with the following pot-pourri of news, forthcoming events and a few noteworthy new components. It should be pointed out however, that the following are in a shortened form designed to 'whet the appetite'. If, therefore, more information is required, an address and sometimes the phone number of the firm concerned is given with the story. Write to them, not to PW!
## Mail order success

DURING the last few months of last year, Chromasonic Electronics of North Londom (see advert. in this issue) announced their intention to start a return-of-mail service. In the months following, the firm states, not one letter received by 3 pm has been left over for processing on the following day. They add that, in addition, telephone enquiries for technical or product price information are not discouraged, as is the case with many firms. Data sheets for semiconductors are also available and cost $6 p$, A4 size, plus postage.

## Knowledge

I$F$ any reader, thirsting for knowledge, wishes to attend an 'all in' three day symposium covering a wide range of test gear and techniques, then why not attend 'Test 75' at the University of Kent between July 7 th and 10 th. Cost is around $£ 45$ and correspondence should be sent to the Symposium Secretary, SERT, Faraday House, 8-10 Charing Cross Rd, London WC2H 0HP. Tel: 01-240 1152.

## JVC moves

WE start with the news that JVC (UK), distributors of $\mathrm{Hi}-\mathrm{Fi}$ and television products, have transferred to new premises. The move due to 'enormous growth since 1969' took place earlier this year with a new showroom, sales department, warehouse and service department. Location is now in the Eldonwall Trading Estate, Staples Corner, 6-8 Priestly Way, London NW2 7AF. Tel: 01-450 2621.

## Hey Wack!

ANYONE out there live in Liverpool or surrounding district-Yes? Well, as from the 24th January BBC Radio Merseyside ( $95 \cdot 8 \mathrm{MHz}$ ) has been utilizing slant polarization. This, according to the BBC Engineering Department, is to improve reception for portable receivers and VHF car radios.

## Another calculator

RECENTLY many companies have been jumping on the calculator bandwagon and although there is now a bewildering number to choose from, here's just one more!!! It's a desk-top model, designated the CBM1500 and hailing from the States. Functions include sin, cos, tan, arc, pi, and roots as well as straightforward numbers. A memory is also included. Price is around the $£ 70$ mark and it can be obtained from Guildford Tapes \& Calculators, Ia Onslow St., Guildford, Surrey.


New desk-top calculator, the CBM1500 from Guildford Tapes \& Calculators.

## Radio notes

AQUICK note here for the amateur radio enthusiast. The Midland Amateur Radio Society will be staging the North Midlands Mobile Rally at Drayton Park, Tamworth, on Sunday 20th April. Further information from A. Walton (G3ZKQ), Birmingham and Midland Institute, Birmingham 3.

## More Beeb cuf-backs

A
LTHOUGH possibly of more interest to the readers of our sister magazine, Television, it has come to our notice that the BBC, 'due to its financial position,' and the need to 'Save it', has found it necessary to curtail the BBC-2 trade test transmissions. Each weekday for about $5^{1}{ }_{2}$ hours, installers, dealers and servicemen will be at a considerable inconvenience, particularly those installing new aerials and receivers. With the tremendous influx of cash due from the recent TV licence fee increase, one wonders what the $B B C$ will do with all that extra money !

## Radio Society get-together

THE RSGB 21st National VHF convention is to be held at the Winning Post Hotel, Whitton, Twickenham, Middlesex, on the 10th and 11th of May.

The programme comprises lectures and demonstrations on amateur space communications, microwaves and VHF propagation. Starting at 11 am on the 10 th , the lecture sessions are on Saturday afternoon and Sunday morning, with the Saturday evening taken up with a dinner dance.
The whole event costs $£ 3$ per person, or 80 p for lectures and trade show only. Further details from RSGB, 35 Doughty Street, London WC1N 2AE, marking the envelope 'VHF Convention'.

## Summer school

ESSEX University will be holding its annual Electronics Summer School for the week of July 7-11th and comprises two courses running simultaneously. The first course, ESS 8 -Linear Circuit Design, is concerned with the use of transistors and operational amplifiers in linear applications. The second, ESS 9-Digital Circuit Design, concentrates on the use of the transistor as a switch and develops designs using integrated logic circuits.

A full laboratory programme backs up the topics covered in lectures, and tutorials are held to discuss the design for the practical sessions. Further information from Bob Mack, Dep. of Electrical Engineering Science, University of Essex, Colchester, CO4 3SQ.

#  <br> m Model Train Bontroller JOHN LEWIS <br> SPEED controllers available to the general public are either mains or battery powered, both suffering inherent design faults. One of the overiding faults centres on the fact that it is based on a variable resistor placed between the supply and the tracks. It therefore follows that any control action which varies the speed of the train, also varies the current available to the motor and consequently the torque or pulling power. This is satisfactory at high speeds but at lower ones problems arise since it is here that one requires more pulling power in order 

 to get the train started. What usually happens is that the control has to be well advanced before any movement occurs and then quickly turned back once the train is moving. This of course results in erratic and unrealistic motion of the train.The author realised that this problem could be overcome by the use of a square wave of constant frequency and amplitude, but with a variable mark/ space ratio. Fig. 1 shows what is meant. When the mark/space ratio is $50 \%$, the time that the voltage is ON is the same as the time that the voltage is OFF, giving an average value of the voltage as shown. If the mark/space ratio is altered so that the ON time is increased, the average value of the voltage will rise and hence the train will speed-up. Conversely if the mark/space ratio is decreased the train will slow down. The motor integrates the pulses and interprets them as changes in voltage rather than current thus giving maximum torque at the required speed. In fact, with this arrangement it is possible to control the train from flat-out down to literally inching round the track, greatly increasing the realism.

## THE INTEGRATED CIRCUIT

The controller is based on the inexpensive 555 integrated circuit. Basically it can be used either as a monostable or an astable circuit as shown in Fig. 2.


For those who are not familiar with its operation Fig. 3 may help. Internally. there is the equivalent of two voltage comparators, a flip flop and an output stage. The comparator connected to pin 2 responds to a voltage of ${ }_{3} V_{c o}$, whilst the comparator on pin 6 responds to ${ }_{3} V_{c c}$. These comparators change the state of the flip-flop and hence the output.

If we look at the astable application which is the one used in this controller we see that both pin 2 and pin 6 are connected to the capacitor and so sense the voltage across it. The capacitor charges up via resistors R1 and R2 and when the voltage across it reaches ${ }^{2}{ }_{3} V_{\text {ee }}$ the comparator on pin 6 will trigger and the flip-flop changes state, driving the output low. At the same time as this occurs, pin 7 is effectively shorted to earth and the capacitor now starts to discharge through R2. When the voltage across C2 reaches ${ }^{1}{ }_{3} V_{\infty}$ the comparator on pin 2 will be triggered, the flip-flop reset with the output going high and the earth to pin 7 removed. This means that C2 can start recharging again. The cycle repeats itself with the frequency being dependent on the values of C2, R1 and R2.

To calculate the frequency the formula

$$
\mathrm{f}=\frac{1 \cdot 44 \times \mathrm{C} 2(\mu \mathrm{~F})}{\mathrm{R}} \frac{1(k \Omega)+2 \mathrm{R} 2(k \Omega)}{}
$$

is used. It can be seen that the values of R1 and R2



Fig. 1: Square waves of constant amplitude and frequency but with variable mark/space ratios.


Fig. 2: The 555 integrated circuit connected in monostable and astable modes respectively.
will determine the time for which the output is either high or low. If R1 equals R2 then the charge up time will be twice that of the discharge time, since the capacitor charges up through both R1 and R2 but only discharges via R2. By choosing appropriate values one can get a mark/space ratio of $50 \%$ or more with the circuit shown. If a diode is added across pins 6 and 7 a duty cycle of less than $50 \%$ can be obtained, and if R1 and R 2 are replaced with a variable resistor one can get a wide range of mark/ space ratios.

The other feature of the IC is the reset available on pin 4 , provided that the potential on this pin is maintained at more than $1 V$ the circuit will operate normally. However if the potential falls to zero then the IC is inhibited and no output is obtained. It was decided to use this facility as an automatic short circuit protection.


Fig. 3 : Diagram of the 555 showing internal arrangement and external biasing components.

## FINAL CIRCUTT

The final circuit can be seen in Fig. 4. The 555 is connected in the astable mode, with the diode added between pins 6 and 7. Using the values of C1 and VR1 shown a nominal frequency of 144 Hz is obtained though the values could be altered should one wish to experiment with other frequencies of operation. The resulting square wave at pin 3 is used to drive


Fig. 4: Complete circuit of controller, showing automatic cut-out system, speed control potentiometer VR1 and reversing switch.
the base of the output transistor Tr l while the output from its emitter is taken to the track via a reversing switch S2.

The return path of the current is through R1, a low value resistor which forms the sensing element of the short circuit protection. When the current flows through R3 a voltage drop is produced across this resistor depending on the current flowing, and is tapped off by VR2. This voltage is then applied to the gate of the thyristor SCR1. Without going into too much detail it will be remembered that a thyristor behaves like an open circuit switch passing negligible current until a suitable positive potential is applied to its gate. When this happens it turns on and conducts in a manner similar to a diode. The gate loses all control at this point and the thyristor stays on even though the gate bias is removed. The amount of potential required to trigger the thyristor varies from type to type and this is catered for by VR2.

If a short does occur on the track the current passing through R1 will increase, resulting in a higher voltage drop, and consequently the turning on of the thyristor. This lights the bulb, LP1, which indicates that something is wrong. With LP1 coming on the potential at the top of the thyristor drops from $V_{c c}$ to almost zero, and since pin 4 is connected to this point the IC will be inhibited, and its output will drop, thus cutting off the power to the track. A push button S 1 , is provided to reset the circait once the short has been removed. The diode D4 ensures


Fig. 5: Optional power supply, utilizing full-wave bridge rectification. Output must be less than 18 V DC.
that the voltage presented at pin 4 is low enough to inhibit the IC, by raising the negative point of the IC, 0.6 V above the negative rail voltage. The sensitivity of the protection circuit can be adjusted by VR2 enabling it to trigger should the train be excessively loaded. Once a fault has been cleared the reset button is pressed and the train will restart. On the prototype, VR2 was a normal pot, although obviously a skeleton preset would do the same job.

## POWER SUPPLY

The circuit will work from any commercially produced $12 \mathrm{~V}-18 \mathrm{~V}$ DC supply which is adequately smoothed. If there are any doubts about the smoothness of the supply, include a $2000 \mu \mathrm{~F}$ capacitor of at least 25 V working across the output.

If required a simple DC power supply can be easily built and a suitable one is shown in Fig. 5.

## SAFETY

Since the circuit is certainly going to be used by children, great care must be taken to ensure that it is electrically safe. Check that all main leads and transformer terminals are adequately insulated and the whole should be enclosed in a metal box which is earthed. On the prototype no mains switch was incorporated, only a neon indicator. The reasoning behind this is that it ensures that the controller is

## components list

| Resistors |  |
| :---: | :--- |
| R1 | $\mathbf{2 . 2 n} 3 \mathrm{~W}$ |
| VR1 | $100 \mathrm{k} \Omega$ linear potenfiometer |
| VR2 | $100 \Omega$ Trim potentiometer or skeleton type |

Capacitors
C1 $0 \cdot 1 \mu \mathrm{~F} \quad \mathrm{C} 2 \quad 0.01 \mu \mathrm{~F} \quad \mathrm{CB} 2000 \mu \mathrm{~F} 25 \mathrm{~V}$
Semiconductors
Tr1 2N3055
IC1 555-Signetics or Motorola
SCR1 3RCio or any general purpose thytistor rated at 0.5 A and 25 PIV .
D1, D2, D3, D4 BAY72 or 4 N914 or any general purpose silicon diode
D5 1N4001
D6 Bridge rectifier-any general purpose type rated at least 2A

Miscellaneous

| LP1 | 12V indicator lamp |
| :--- | :--- |
| S1 | switch-push to break |
| S2 | switch-toggle DPDT centre off. |
| T1 | Transformer-nominal $12 \mathrm{~V}, 1+5 \mathrm{~F}$, Possible |
|  | to use flament transformer and connect the |
|  | two 6.3 V windings in series. |

Mains neon. Mains cable clamp and solder tag. Metal box approx. $185 \times 115 \times 75 \mathrm{~mm}$ ( $74 \times 4 \frac{1}{2} \times 3 \mathrm{in}$.) Veroboard $0 \cdot 1 \mathrm{in}$. pitch $76 \times 31 \mathrm{~mm}\left(3 \times 1 \frac{1}{4} \mathrm{n}\right.$ ).
switched off and unplugged from the mains when not in use, and not merely switched off internally. However, opinions will differ and a suitable switch can be easily incorporated if desired. It is worth mentioning here the diodes D2 and D3 shown on the circuit diagram. In the prototype the power supply gave 19 V under no-load conditions and the maximum working voltage of the 555 is 18 V . Rather than mess around with a zener diode etc., it was decided to drop $1 \cdot 2 \mathrm{~V}$ just by using these diodes. Thus these and D4 ensure that the IC is actually running at $17 \cdot 2 \mathrm{~V}$. If the supply is less than 18 V under no-load conditions, D2 and D3 can of course be omitted. D5, which is across the reversing switch $S 2$ is there to suppress the negative-going spike produced by the motor at the end of each pulse, which could damage Tr1.


Fig. 6: Component layout on Veroboard, showing track breaks and externa/ connections. Tr1 (2N3055) and SCR1 (3RC10) shown to the right must be fitted using insulating washers. Connections to the collector of Tr1 and anode of SCR1 are via solder tags.


## Oily waves

I feel I must write and protest at the tone of your editorial of March 1975 Practical Wireless.

I fail to see why you appear so "anti" about exchanges between North Sea oil rigs and their bases. Apart from 1625 kHz which is used by Ekofisk to work into Stavanger, all other off-shore installations work directly into British or Continental coast radio stations in the Maritime Service. The stations heard in the 80 metre band are exchanging traffic on ISB with Humber Radio or Wick Radio, or on SSB with Cullercoats or Stonehaven radio and thence by land line to shore based subscribers.

All these communications are taking place at the rate of 36 p per minute and represent revenue to the Ministry of Post and Telegraphs. I fail to understand why any off-shore station should be expected to continually identify itself when the call is being monitored and charged by a coast station Radio Operator?

Life off-shore can be arduous and dangerous and the many oil rig and barge workers who may phone their wives during the evening should be entitled to a little privacy during the QSO. they're paying enough for it!-Stan Crabtree G30XC (Radio Operator, FORTIES ALPHA).

## PW PSU mod

Having constructed a bench power supply unit to the same basic design as that described in PW, September 1973 by J. Lewis, B.Sc., I feel the following observation may be of use to your readers.

The author comments in the final paragraph: "a residual ripple . . . could be eliminated by
adding a $100 \mu \mathrm{~F}$ capacitor. . ." I found that even a $1000 \mu \mathrm{~F}$ made little difference when used with a particular piece of equipment which was sensitive to hum on the supply rails; I therefore added, to the circuit of Fig. 9 in the article, a $10 \mu \mathrm{~F} 64 \mathrm{~V}$ electrolytic, between pins 3 and 4 of the NE550A (negative to pin 4) thereby providing AC negative feedback and substantially reducing the hum ( 100 Hz ripple).

I consider that a larger value would produce a greater improvement, but my unit is now sufficiently ripple free for my re-quirements.-P. J. Brent (Scotland).

## Natural scale

I'm surprised at Mike Hughes! In his article on the PW Easybuild Electronic Organ, he states that "organ purists will wince" at the use of the equal temperament scale. This scale has been in use on keyboard instruments since the time of Bach. In fact it is in use in all musical instruments which are "pre-tuned" such as the clarinet, trumpet, oboe etc.

The idea behind the equal temperament scale is quite simple. The relationship between a note and the one an octave above, is that the higher note has twice the frequency of the lower. A violinist, in order to achieve this will in fact halve the length of his string. The frequency ratio for notes a fifth apart is $2: 3$. For notes a third apart it is $4: 5$ and so on.

In the equal tempered scale, as Mike Hughes says, there is an exact mathematical ratio between each half tone in the scale. This ratio is $1: 0594$, and since there are twelve half tones to the scale, $1: 0594^{12}=2$. This makes the frequency ratio of the third $1: 1 \cdot 259$ and not $1: 1 \cdot 25$ as on the natural scale. Similarly the fourth ratio is $1: 1 \cdot 34$ and not $1: 1 \cdot 33$. The fifth becomes $1: 1.498$ instead of 1:1.5.

These differences are not enough to be noticed in ordinary circumstances, but violinists, and singers etc, when playing on their own, will play in the natural scale; and when with the piano or organ etc. will play equal tempered.

Incidentally, Bach was the first to write specifically for the equal tempered system in his "Well Tempered Clavier." - P. G. Quartermain (Sussex).

## Cramped bands

Your editorial 'Thou shalt not listen' draws timely attention to a problem which is becoming increasingly frustrating to the DX listener. For about one year now, I have been very interested in long range reception on UHF TV and VHF radio.

I find that the ordinary VHF set offers good scope for DX work, except that the $88-108 \mathrm{MHz}$ band is cluttered with taxi and police signals. So much of the band is given over to these, that the broadcast band is "bunched" to such an extent that many stations use the same frequency, and others are so close to each other that the nearer ones eclipse the more distant.

Even with a six-element array, I cannot now receive Radio Humberside because it is obliterated by Radio Piccadilly; RTE Kippure is wedged between Radio Merseyside and Radio Manchester and can only be heard by using screening. Radio Sheffield, on its lower frequency, is jammed by taxi calls, and on its higher frequency is jammed by the police.

Recently I picked up an interesting signal in Dutch. After waiting a long time for station identification, I was frustrated by a taxi firm which drowned out the station identification when it did come. (I still don't know which station I was listening to!)

All these problems could easily be solved by allocating the whole $88-108 \mathrm{MHz}$ band to broadcasting. Surely the police do not enjoy being overheard and would prefer to be on a virtually inaccessible band?

Which raises another question; What is to happen to Bands I and III when the 405 line TV service is phased out in a few years time? My own suggestion is that these channels should be allocated to educational television; schools broadcasts during the day and Open University in the evening.John T. Haines (Lancs).

## Ouch!

I thought you might be interested in the specification of a tnansistor radio seen in a mail order catalogue;
"clear reception on 3 wavebands VHF/MW/LW. Clear $2^{1}{ }_{2} \mathrm{in}$. dynamic speaker giving 300 kW output. Complete with earphone." -R. Rix (Norfolk).

# M. J. HUGHES M.A., C. Eng. MIERE 

This, the third part of the PW Easybuild Organ, carries on from the April issue, and covers in detail the keyboard wiring and the testing of the main PCB.

## 8FT PITCH

Readjust VR6 for maximum and adjust the pre-set VR5 until the signal level of the square wave output approximately matches that of the spike signal. To complete this rough setting up of the 8 ft tones set the triangular wave slider VR8 to maximum. The sound should be more mellow but of similar amplitude to the square wave signal. Now adjust the preset control across the 8ft integrator VR7. Adjustment to its full extreme in one direction will have no effect but if its value is reduced to zero ohms the amplitude of the signal will fall abruptly to a very low level. Set it to the point just before the signal level starts to fall off which will prevent nasty keying noises when this tone is used. Now try mixing the different waveforms together to hear the general effect of the three signals in various proportions. Do not expect too much at this stage because we have yet to line up the 16 ft . pitch.

## 16FT PITCH

Exactly the same procedure should be adopted by placing the lead from the 16ft. input pin on to a mid-frequency tone pad. Start with the spike waveform by advancing VR10 and adjust the preset VR9 until the level is approximately similar to the equivalent tone at 8ft pitch. Advance VR12 and use VR11 to set the level for the square wave. Finally, advance VR14 and adjust VR13 in exactly the same way as for the integrator pre-set at 8 ft . pitch. Now experiment by connecting the 8 ft . and 16 ft . inputs to identical notes an octave apart at the same time, and listen to the full effect of the different tone colours produced by the main controls. When they are all advanced to maximum the loudspeaker might overload, in which case use the pre-set VR15 as a master control. Ideally the loudspeaker should be just on the edge of overloading when the volume control is at maximum. More will be said about this when dealing with the phono output.


## CALIBRATION

Check that the vibrato control functions correctly and roughly tune the master oscillator so that the organ is set to international pitch. Do this by adjusting $C 7$ while listening to the tone from leadout number 23 (this should be International A at 440 Hz ), and can be checked against a piano (the A immediately above middle C) or against the BBC's morning radio test transmission.

When tuning, the tune control should be set midway. It may be that C7 has to be almost fully compressed to get the organ in tune. When correctly set up the tune control should shift the frequency by about one full tone, but this will vary slightly from one unit to another, depending on the internal capacitance of D1 and D2.

A wider degree of tune can be produced by reducing the value of $R 6$ to about $4 \cdot 7 \mathrm{k} \Omega$ but this is not recommended because the vibrato effect will be too fierce when VR2 is set to its lowest frequency position.

The bulk of the electronics is now finished, the next stage is the assembly of the keyboard contacts and the wiring associated with them. This is a very repetitive operation and calls for a reasonable amount of patience and care.

## KEYBOARD

Make sure that the correct components have been obtained. A 49 note $C$ to $C$ keyboard as specified will be required, together with 49 contact blocks. These blocks are very delicate and should be handled carefully to ensure that the fine gold-plated contact wires are not bent. Each block comprises four wires held
in position by the phenolic laminates and rivets. Fig. 10 shows such a block and the dotted lines show the disposition of the wires as they run through the centre.

For the purposes of description each wire should be designated with a letter ' $a$ ', ' $b$ ', ' $c$ ', and ' $d$ '. Wires ' $a$ ' with ' $b$ ' form one contact pair and ' $c$ ' with ' $d$ ' the other; in every instance the pair $a / b$ will be used to route signals into the 8ft busbar and c/d into the 16 ft busbar.

The contacts are actuated when a key is pressed and the action can be checked by careful inspection of the underside of the keyboard. When a note is depressed the key pushes a small plastic actuating link out from under the keyboard. This is designed to push the wires ' $a$ ' and ' $d$ ' of each contact block into electrical contact with their corresponding ' $b$ ' and ' $c$ ' wires. One of the jobs that has to be done is to fix each contact block into position so that this simple mechanical action can be effected.

## PALLADIUM BUSBARS

The blocks are so designed so that when a key is not pressed the signal coming from the tone generator is shorted to earth. To avoid the problems of connecting a separate earth lead to each switch assembly, use is made of an earth busbar. Each block has a small hole positioned near its "nose" and if inspected carefully it will be seen that the wires ' $a$ ' and ' $d$ ' exactly centre on the hole.

The keyboard suppliers will provide a special rod made from palladium which is designed to run through this hole, and through the equivalent holes of all the other contact blocks. This rod forms the earth busbar and it should be clear that under normal circumstances wires ' $a$ ' and ' $d$ ' are kept in contact with the rod by their own springiness. When it comes to inserting the rod, make sure that ' $a$ ' and ' $d$ ' wires are displaced towards their ' $b$ ' and ' $c$ ' counterparts so that the rod passes through the hole without hindrance and is on the correct side of the wires. Four palladium rods should have been obtained, each of which is about the length of one of the keyboard octaves.


Fig. 10: Details of the keyboard switch assemblies (Kimber Allen) NOTE. It is important, when a key is operated, that the outer contacts of the assembly break from the earth busbar before they make contact with the $8 f t$ or 16 ft busbars. These are adjusted by bending the "cranked" contacts away from the outer ones, with a pair of forceps, while operating each note in turn.

To make assembly easier, four SRBP plates (also obtainable from the keyboard suppliers) should be obtained. The contact blocks are glued on to these before the sub-assembly is screwed to the keyboard sub-frame.

## KEYBOARD WIRING

The equivalent of 98 tag posts are required (strips with tags rivetted on 6 mm ( ${ }^{1}{ }_{4}$ in) centres will do nicely) and these are used to terminate the 60 signal wires coming from the numbered positions on the main printed circuit board. Ideally there should be


Photograph of complete underside of organ keyboard, showing details of switch positioning, wiring and keyboard resistors.
one strip carrying 26 tags and three strips carrying 24 tags each. The tags are also used for routing the signals under the keyboard for the two pitches.

In principle a signal from the tone generator is terminated at one of the tag posts and a $100 \mathrm{k} \Omega$ resistor feeds from that tag to the ' $a$ ' wire of the adjacent contact block. A connection is also made from that same tag post to the tag post for the same note an octave higher, but for this higher note key, the tag post corresponding to the ' d ' contact wire should be used. A $100 \mathrm{k} \Omega$ resistor bridges across from this latter tag to the ' d ' contact. This looping from one octave to the next is how the signals are routed from the tone generator to give notes one octave apart (on the two pitches) when a single key is pressed.

A glance at the underside wiring diagram Fig. 11 and wiring schedule will show the general principle. The wires coming straight from the tone generator board go (in every case except the bottom octave) to the 8 ft pitch contacts and the loop connections to the 16 ft contacts of the identical note an octave higher. The bottom octave is slightly different because there is, of course, no lower octave from which to do the looping for the 16 ft pitch connections. Instead there are eleven extra wires coming from the main board to look after the 16 ft pitches for all this bottom octave except for bottom ' $c$ '.

There are not quite enough notes to provide a 16 ft pitch for the lowest C on the keyboard so the 8 ft and 16 ft contacts are simply looped together for this note. This is a slight nuisance but is a sacrifice one has to make for simplicity and low cost.

The wiring in Fig. 11 might look a little frighten-
ing but in actual fact it is very simple and only needs care and patience in the routing of the wires.

## CONTACT ASSEMBLY

Before any thoughts of wiring however, the contacts must be assembled. To do this, turn the keyboard upside down and place the four SRBP plates exactly butting againt each other on the wide flat portion of the keyboard sub frame; between the trough where the key pivots and the apertures for the actuator links. Slide the plates from side to side until the butt joint between the centre two plates exactly corresponds to the centre of the actuator link for the central ' $C$ ' of the keyboard. This should position the boards symmetrically about the midpoint of the keyboard.

Having obtained this poition use a pencil to make marks on the boards which correspond to the centre lines of every actuating link of the keyboard. Use a set-square to project these marks across the board at every position and pencil in a centre line, this will mark where the contact block has to be glued into place. Draw another line 9.5 mm ( ${ }_{8}$ in) from the edge of the boards furthest away from the actuators which will act as a guide for positioning the blocks so that they line up with each other. This prevents problems when feeding the earth bus bar through the holes!

Using an epoxy resin glue (preferably the fastsetting variety) put a small smear of glue on the side of each contact block opposite the side having the rectangular notch and position each block


Fig. 11 : Detalls of keyboard switch wiring, showing looping arrangements from one octave to another. This diagram shows only the bottom octave and the first two notes of the second octave, and therefore should be used in conjunction with the wiring schedule opposite.

| Keyboard Resistors | $\begin{gathered} \text { PCB } \\ \text { connections } \end{gathered}$ | Other keyboard connections | Note | Octave | Keyboard Resistors | $\begin{array}{\|c\|} \text { PCB } \\ \text { connections } \end{array}$ | Other keyboard connections | Note | Octave |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RK1 | 314 | RK25 | C 16 ft$\}^{\prime}$ | ＊ 4 | RK51 | －4 | － | $C \geqslant 16 \mathrm{ft}$ | 4 |
| RK2 | 31 T | RK25 | C 8 ft \} |  | RK52 | 59 | RK75 | C $=8 \mathrm{ft}$ |  |
| RK3 | 56 \％ | － | $C ; 16 \mathrm{ft}$ |  | RK53 | － | － | D 16ft |  |
| RK4 | 57 ¢ | RK27 | C $\ddagger 8 \mathrm{ft}$ |  | RK54 | 4 | RK77 | D 8 ft |  |
| RK5 | $1 E$ | － | D 16ft |  | RK55 | － | － | D\＃16ft |  |
| RK6 | 2 E | RK29 | D ．8ft |  | RK56 | 9 | RK79 | $\mathrm{D}=8 \mathrm{ft}$ |  |
| RK7 | 6 \％ | － | $D=16 \mathrm{ft}$ |  | RK57 | － | － | E 16ft |  |
| RK8 | 79 | RK31 | $D=8 \mathrm{ft}$ |  | RK58 | 54 | RK81 | E 8ft |  |
| RK9 | 51. | － | E 16 ft |  | RK59 | $-1$ | － | F 16ft |  |
| RK10 | 52 年 | RK33 | E $\quad 8 \mathrm{ft}$ |  | RK60 | 14 窇 | RK83 | F 8 ft |  |
| RK11 | 11 艺 | － | F 16 ft |  | RK61 | $-\frac{m}{5}$ | － | $F=16 \mathrm{ft}$ |  |
| RK12 | 12 J | RK35 | $F \quad 8 \mathrm{ft}$ | Bottom | RK62 | 19 E | RK85 | $F=8 \mathrm{ft}$ |  |
| RK13 | 16 | － | $F=16 \mathrm{ft}$ | octave | RK63 | － | RK8 | G 16 ft | ㄷ．Third |
| RK14 | 17 4 | RK37 | $F=8 \mathrm{ft}$ |  | RK64 | 49 | RK87 | G 8 8 ft | 叁 octave |
| RK15 | 46 | RK39 | $\begin{array}{ll}\text { G } & 16 \mathrm{ft}\end{array}$ |  | RK65 | － | － | G\＃ 16 ft | 気 |
| RK16 | 47 匈 | RK39 | G 8 8ft |  | RK66 | 44 | RK89 | G\＃8ft |  |
| RK17 | 41 E | － | $\mathrm{G}=16 \mathrm{ft}$ |  | RK67 | － | － | A 16 ft |  |
| RK18 | 42 E | RK41 | $\mathrm{G}=8 \mathrm{ft}$ |  | RK68 | 24 | RK91 | A 8ft |  |
| RK19 | 21 \％ | － | A 16ft |  | RK69 | 24 | RK91 | $A \neq 16 \mathrm{ft}$ |  |
| RK20 | 22 8 | RK43 | A 8 ft |  | RK69 | $\overline{29}$ | RK93 |  |  |
| RK21 | 26 \％ | － | $A=16 \mathrm{ft}$ |  | RK70 | 29 | RK93 | A \＃8ft |  |
| RK22 | 27 彦 | RK45 | $A \pm 8 \mathrm{ft}$ |  | RK71 | － | － | B 16ft |  |
| RK23 | $36 \stackrel{\text { 免 }}{ }$ | － | B 16ft | ¢ | RK72 | 39 | RK95 | B $\quad 8 \mathrm{ft}$ |  |
| RK24 | 37 | RK47 | B 8ft | 年 | RK73 | － | － | C 16ft | 1 |
| RK25 | － | － | C 16ft | 岕 | RK74 | $34 \downarrow$ | RK97 | C 8 ft | V |
| RK26 | 32 | RK49 | C 8ft | $\xrightarrow{\mathrm{c}}$ | RK75 | － 4 | － | C． 16 ft |  |
| RK27 | －4 | － | $C=16 \mathrm{ft}$ | ¢ | RK76 | 60 | － | C $=8 \mathrm{ft}$ |  |
| RK28 | 58 | RK51 | $C=8 \mathrm{ft}$ | 皆 | RK77 | － | － | D 16ft |  |
| RK29 | － | － | D 16ft | 立 | RK78 | 5 | － | D 8 ft |  |
| RK30 | 3 | RK53 | D 8 ft |  | RK79 | － | － | D \＃ 16 ft |  |
| RK31 | － | R | $\mathrm{D}=16 \mathrm{ft}$ |  | RK80 | 10 | － | D \＃8ft |  |
| RK32 | 8 | RK55 | $D=8 \mathrm{ft}$ |  | RK81 | － | － | E 16ft |  |
| RK33 | $-\frac{1}{\underline{E}}$ | － | E 16ft |  | RK82 | 55 | － | E $\quad 8 \mathrm{ft}$ |  |
| RK34 | 53 \％ | RK57 | E 8 8t |  | RK83 | －空 | － | $F \quad 16 \mathrm{ft}$ |  |
| RK35 | － | － | F 16 ft |  | RK84 | 15 E | － | F 8ft |  |
| RK36 | 13 E | RK59 | F 8ft |  | RK85 | － | － | $F \ddagger 16 \mathrm{ft}$ |  |
| RK37 | － | － | $F=16 \mathrm{ft}$ |  | RK86 | $20 \stackrel{\circ}{\circ}$ | － | $F \pm 8 \mathrm{ft}$ | Top |
| RK38 | 18 \％ | RK61 | $F=8 \mathrm{ft}$ | Second | RK87 | － | － | G $\quad 16 \mathrm{ft}$ | octave |
| RK39 | － | － | G 16ft | octave | RK88 | 50. | － | G $\quad 8 \mathrm{ft}$ | 1 |
| RK40 | $48 \stackrel{\text { a }}{\text { a }}$ | RK63 | G 8ft | ＜ | RK89 | － | － | $G \# 16 \mathrm{ft}$ |  |
| RK41 | $-\stackrel{3}{4}$ | － | $\mathrm{G}=16 \mathrm{ft}$ | 단 | RK89 | － 45 | － | G\＃8ft |  |
| RK42 | 43 | RK65 | G＊8 ft | 등 | RK90 | 45 | － | A $\begin{aligned} & \text { A } \\ & \text { ctit }\end{aligned}$ |  |
| RK43 | － | － | A 16 ft | 管岕 | RK91 | － | － | A 8 8ft |  |
| RK44 | 23 | RK67 | A 8ft |  | RK92 | 25 | － | A ${ }_{\text {A }} 16 \mathrm{ft}$ | ， |
| RK45 | － | － | $A=16 \mathrm{ft}$ | 릉 | RK93 | － | － | A－ 16 ft |  |
| RK46 | 28 | RK69 | $A \pm 8 \mathrm{ft}$ | $\pm$ | RK94 | 30 | － | $A=8 \mathrm{ft}$ |  |
| RK47 | － | － | B 16¢ft | ＂ | RK95 | － | － | B 16ft |  |
| RK48 | 38 | RK71 | B 8 ft | 式気 | RK96 | 40 | － | B 8ft |  |
| RK49 | － | － | C 16ft | － | RK97 | － | － | C 16ft | 1 |
| RK50 | $33 \%$ | RK73 | C 8 ft | 을 ${ }^{\text {V }}$ | RK98 | $35 \downarrow$ | － | C 8 ft | $\downarrow$ |

Main PCB to keyboard wiring schedule．Refer to Fig． 11 to begin with，in order to start the process going．Once begun，the wires going to the PCB，and the loop wires between tags，will follow in a logical sequence；as the wiring schedule above shows，
＊Due to divider limitations，this note is the same on both $8 f t$ and 16 ft pitches．
exactly on the centre lines already drawn. Do not try glueing the block corresponding to the central " C " of the keyboard at this stage because it wll be straddling a joint between two of the boards. NOTE; if fast-setting epoxy is being used do not mix up too much at a time because it will be found that it takes about ten minutes to position the twelve contacts on each board and the glue will be starting to go off as the first board is finished.

Set the contact assemblies to one side for the glue to harden. When they are really firm, drill a hole between the outer pair of contacts on each board to take self-tapping fixing screws. Next, offer the boards up to the keyboard so that the 'a' and ' $d$ ' wires of each contact block exactly rest over their corresponding actuating links. Press the boards down against the restraining action of the springiness in the contact wires and mark through the screw holes on to the metalwork of the keyboard frame. Again remove the boards and very carefully drill selftapping holes in the metal where marked; do not allow the drill to break through the metal in an uncontrolled manner as damage may be caused to the underside of the plastic-covered keysi
Before screwing the contacts into place butt the two centre boards together on a flat surface and glue the final contact block across the butt joint. For added rigidity it is worth running a thin fillet of resin down each side of this block. Let this set really hard and then carefully screw the two central boards into place under the keyboard.

## CONTACT EARTHING

Take two of the palladium rods and by carefully lifting each pair of ' $a$ ' and ' $d$ ' contacts, pass the rods through the earth busbar holes of the blocks that are in position-work from either end for each rod. Where the rods meet near the centre let them overlap by about 6 mm ( ${ }_{4} \mathrm{in}$ ) and solder them together. If necessary trim off the end of each rod so that they protrude by about 133 mm ( ${ }_{2}{ }_{2}$ in) from the two extreme end contact blocks. Now screw the remaining two contact assemblies into position and insert the final two palladium rods from either end. Again, let them overlap the ends of the rods already in place and solder them together.

Now put bends in the shorter ends of the ' $b$ ' and ' $c$ ' wires for each contact block. The ' $c$ ' wire should be bent upwards until it is almost vertical and the ' $b$ ' wire up through about $45^{\circ}$. It will now be possible to get the test probes of a continuity test meter (ohms range on a multimeter) across the contact connections to test each one. This test is very important because clearing up problems at this stage will greatly simplify tests later on.

Although the keyboard must be kept upside down, make absolutely sure that none of the keys are depressed (use books to stand the keyboard off the working surface). Check that there is continuity between every 'a' and 'd' wire and the earth busbar. If any of them show open circuit, gently bend up the end of the contact wire that rests on the actuating link, so that the wire will settle itself further down inside the block assembly to touch the earthing bar.

Next, check that when a key is pressed there is continuity between the corresponding pairs of $a / b$ and $c / d$ contacts. Of course, continuity should be
broken when the key is released. Ideally, contact should be made when the key is depressed just over half of its total travel and the wires ' $b$ ' and ' $c$ ' carefully bent to allow this to happen. To make the organ easier to play each key should make contact at exactly the same degree of depression as its neighbour.

This completes the assembly and initial tests of the contacts. There is one more test to come but this must be reserved until some signals are available.

## TAGSTRIP ASSEMBLY

Proceed to solder in the 8 ft and 16 fft busbars. These are simply lengths of straight tinned copper wire soldered to every contact block's ' $b$ ' or ' $c$ ' connection. One wire runs from the ' $b$ ' wire of the central " $C$ " block and is soldered to every ' $b$ ' wire for the higher notes (this is the 8ft busbar for the top two octaves). Similarly another wire is run from the ' $c$ ' connection of the same block to all the higher note ' $c$ ' connections (16ft busbar for the top two octaves). Likewise two busbars run from the " $B$ " below central "C" for 16 ft and 8 ft pitches for the bottom two octaves, a study of Fig. 12 should make these connections clear. Make sure that every connection is well made and that there are no dubious or dry joints.

It now remains to assemble the tag strips into position. The lengths of the strips should be such that there is a tag available for every ' $a$ ' and ' $d$ '


Fig. 12 : Diagram showing orientation of contact blocks, busbars and wiring for the split keyboard switches.

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wire of all the contact blocks and ideally they should be in an exactly corresponding position on the opposite side of the pivot trough of the keyboard. In practice it is unlikely that tag strips having the correct pitch will be available but for the prototype it was found that standard "miniature" tag strips having 6 mm ( ${ }^{1} 4 \mathrm{in}$ ) pitch would do, provided they were broken up into approximately octave lengths, the accumulative error in the pitch being taken up with a gap at the octave breaks.

One strip, to correspond to the bottom octave, should carry 26 tags and be centrally located between the " $C$ " and the " $C$ " an octave higher. A length of insulating strip (an old piece of blank Veroboard will do) should be cut and stuck with epoxy resin to the underside of the tag strip and, when set, the whole assembly should be glued into position opposite the contact blocks for the bottom octave. The ledge between the edge of the hinge and the pivot trough is an ideal place to stick the strips. The next three octaves should be dealt with by using strips each carrying 24 tags.

When all the tags are firmly glued into position all 98 keyboard resistors between the tags and their corresponding contact wires can be soldered in. All the resistors are $100 \mathrm{k} \Omega$ and if an ohmeter is available it's just as well to check each one before it is used. When using a large quantity of the same component there is always a chance that there may be an odd one out.

## LOOP WIRING

Now comes the tedious bit. All the loop wires between the tags an octave apart must be connected up. Be very careful to start-off correctly by triple checking the following procedure.

Start by linking the two tags associated with bottom " C " and then run a lead of fine flexible insulated wire from the right hand pin of that pair to the left hand pin of the pair going to " C " an octave higher (i.e. from RK2 to RK25). Next, go from the right hand tag of bottom $C=$ to the left tag of $\mathrm{C}=$ an octave higher (i.e. from RK4 to RK27). As long as the procedure is started off correctly there is little chance of error because the procedure is repetitive. There are no links to be made from top $C$ to higher frequency notes or any other notes in the topmost octave apart from C itself.

When making these loops cut the wires to exactly the right length and strip off exactly the right amount of insulation each time, then it will be found that the wires tuck down together very neatly. At the same time try to connect to the tags as far down them as possible (near to the insulating board) because there is still another wire to connect to most of the tags and space will be required to solder. Once the loops are in place the wires can be tied together to make the loom more robust, using waxed twine or alternatively black crochet thread.

## PCB WIRING

The main wiring loom that runs from the printed circuit board to the keyboard has now to be constructed. Put the keyboard to one side and clear a nice amount of room to carry out the following


Fig. 13: Annotated photograph of prototype organ, showing close-up view of actual keyboard wiring and switch block assemblies.
wiring very methodically. First cut twelve $1 \cdot 22 m$ ( 4 ft ) lengths of fine connecting wire. Strip off 6 mm ( ${ }^{1} 4 \mathrm{in}$ ) of insulation from one end of each piece. Pick up the lengths one at a time and with the first piece insert it through the hole numbered 35 on the PCB (insert it from the top side of the board) and solder it into place very carefully, taking care not to bridge any of the fine tracks with solder blobs. Cut off any excess wire at the joint.

This wire will, eventually, be connected to the tag going to the topmost "C" of the keyboard (at RK98); refer to the wiring schedule where it can be seen that the wire going into this point is numbered " 35 " to correspond with the printed board designations. Using sellotape and a small piece of paper make a flag carrying the number 35 and fix it to the free end of this wire. Take the next piece of wire and solder it to output 40 of the PCB and do likewise. Continue in this way, refering to the wiring schedule for details of which outlet the wire should go to and make sure that every wire has a correctly numbered flag on it.

Next, cut off twelve 910 mm (3ft) lengths of wire and continue with the same procedure for the next octave down. When these are complete, cut a dozen wires each of $760 \mathrm{~mm}\left(2^{1}{ }_{2} \mathrm{ft}\right)$ in length, then 610 mm (2ft) and finally 460 mm ( $1^{1}{ }_{2} \mathrm{ft}$ ) for the bottom twelve notes. By the time the last dozen connections to the board are reached it will be found that the wires might tend to twist together. Try to avoid this happening. A good way is to let the wires
dangle over the edge of the table and make sure that they all run parallel from the board.

When this has been done, double check the wiring and ensure that there are no short circuits across the lead-outs on the board (use the ohmeter as described in Part 2). As a check on the wiring, take each of the free ends of the wires in turn, bare them, one at a time, and check continuity between that wire and the numbered contact on the board that corresponds to the flag on the wire. Any dubious connections must be rectified.

Do not, at this stage, attempt to connect the free ends of the wires to the keyboard. Tie the groups of wires together into bundles of 12 , corresponding to their different lengths, and then carefully put the board to one side and start building the cabinet. Final wiring is done when all the component parts are properly positioned within the final enclosure.

## NOTES

On some main PCB layouts supplied by PW, it may appear that pins 1 and 2, reading clockwise, of IC5 are shorted together. This is incorrect, so on the PCB itself, very carefully run a sharp knife between the track of pin 1 and pad of pin 2 to clear.

The author has pointed out that the decoupling effect of R12 is excessive and can cause a supply line drop to the divider circuitry. This gives rise to apparent instability of the dividers at some settings of the Vibrato and Tune controls. It is therefore suggested that R12 be reduced to $10 \Omega$ or short circuited completely to overcome this problem.

In the components list published March 1975 values
of VR7 and C5 were incorrectly stated. They should have read:-

VR7 220k $\Omega$ miniature vert. preset.
C5 2200pF
The keyboard resistors designated R31-R128 in the components list, have been redesignated RK1. RK98 to simplify the description of the keyboard wiring.

Watford Electronics, 35 Cardiff Rd, Watford, Herts., have brought it to our attention that they are able to supply the complete semiconductor complement including the divider IC's AY-1-5051.

SCS Components of Northfield Industrial Estate, Beresford Avenue, Wembley, Middlesex, HA0 1YY, have informed us that as they are distributors for many semiconductor manufacturers, they too are in a position to supply the IC's for the Easybuild Organ. Telephone number for SCS components is 01-903 3168.

Just a quick reminder now for those readers interested in constructing their own PCB. PW is offering a full-size paper drawing of the PCB, showing track layout. For those who require one of these, please write, marking envelope "Easybuild Organ" to Practical Wireless, Fleetway House, Farringdon Street, London EC4A 4AD, and enclosing a PO or cheque for $25 p$ and a $10 x 8$ in size S.A.E.

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MODEL TRAIN CONTROLLER-continued from page 24.


## LAYOUT

Component layout of the prototype is shown in Fig. 6, while Fig. 7 shows the diecast box, although any form of metal enclosure could be used. For children's use it was decided that the knob on VR1 should be as large as possible so that little fingers
could grasp it easily. After some use the reversing switch was replaced by a similar switch only this one had a centre off position making train driving much easier. With a little practice one can accelerate smoothly away from rest with quite large loads or even inch forwards and backwards with no difficulty.


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Celestion G12H 8 or 15 ohm Celestion G15C 8 or 15 ohm Celestion G18C 8 or 15 ohm Coral $6 \frac{1}{1 /} \mathrm{d} / \mathrm{cone}$ roll surr. 8 ohm Coral 8 d/cone roll surr. 8 ohm EMI $13 \times 8150 \mathrm{~d} / \mathrm{c} 38 \mathrm{or}$ EMI $13 \times 8450 \mathrm{t} / \mathrm{cw}, 8$ or 15 ohm EMI $13 \times 8$ type 3508 or 1 EMI $13 \times 820$ watt base 15 hm EMI 61" 938504 or 8 ohm EMI $5^{\prime \prime}$ 98132CP 8 ohm
EM1 $8 \times 5 \mathrm{~d} /$ cone, roll surr 10 wat EMI $2{ }^{\frac{1}{4} "}$ tweeter 97492AT Eagle DT33 30 watt tweeter Eagle HT15 horn fweeter Eagle CT5 cone tweeter
Eagle CT10 tweeter 8 or 16 hm Esgle MHT10 horn twer Eagle crossover CN23, CN28, CN216 Eagle FR4 Eagle FR65
Elac 9×5, 59RM109 15 ohm $59 R M 1148$ ohm
Elac 6is 6RM171 d/c roll surr
Elac 61" 6RM220 d/con
Elac 4 tweeter TW4 $10^{\prime \prime} \mathrm{d} /$ cone 10 RM 2398 ohm Elac $8^{\prime \prime} 8 \mathrm{CS} 1753 \mathrm{ohm}$ Fane Pop 15 watt $12^{\prime \prime \prime}$ Fane Pop 25/2 25 watt 12
Fane Pop 40 watt $10^{\prime \prime}$
Fane Pop 50 watt $12^{\prime \prime}$
Fane Pop 55 12" 60 watt
Fane Pop 60 watt $15^{\prime \prime}$
Fane Pop 100 watt $18^{\prime \prime}$
Fane Crescendo 12A 100 watt $12^{\prime \prime}$
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Fane Crescendo $15^{\prime \prime} 100$ watt
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Fane $801 \mathrm{~T} 8^{\prime \prime} d / c$ roll surr. Fane 807T $8^{\prime \prime} \mathrm{d} / \mathrm{c}$ roll surr.
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HAve you ever driven a car in heawy mite of spotty rain (typical Byitsh weatherl), yní found that instead of providing a clear, view the wipers meroly smear the windscrecn thating Gisibility even worse sthañ ever? The reason for ${ }^{\text {thif }}$ is, that the avefage cars, windscreen wipers nuy function well in heavy rain, but, when it is only caining lighty notenough rain lands on the wind screen between one sweep of the wipers and- lue following one to lubricate the wipet blades as they travel across the screen
The Car Wiper Delay Unif đescribed kere sitves this problém and provides clear visiblity in all types of ran. The wipers are, allowed to sweep actoss the 5* Screeh at their normal speed, but a delay is intro ducea, in tientreen wipet sweeps, whore the delay Can be adjusted to suit the prevalling weather.

The circuit is suitad 0 , all wehicles whetiver

elentrically driven self parking wipurt f fe. wirnually all vevilles, but apologies to owners of 100 E 's with tachum uriven wipers D.

## CIRCUIT DESCRIPTION

The drext is, cannected across the existing wiper ifiteli as showin in Ag. 1, which shows tho arrangement for a retacle having a riegative earth.

The wiper motor'ls normally connected trat the sgnition swreh to the Ive terminal of the car buterg so bhat when the wiper switch is closed the other? motor lead is earthed and the wipers are frought into operation.
A revint switch 45 rounpected of the wiper mechanism which ensures that when tho wipers are switched off the motor contrines, to run Entll the Wper blades are arked this sell-parkipg Tgechanism, operates in Conjuncion with औle wiper Delay Unit and enables á cheap Liyristot to be deet in plice oftac elay which is nsunlly cound in simple thellof circitw.

When St is closed, 12 selts wiefers across ife circuit since there 35 a low renkinnoo fath through the notor armatiry to the lattery kye terminal and Uíe cirrent drawn by the dicust puting the delay thtrot is negligible


Fig. 1: The clrcuit diagram of the Car Wiper Delay Unit. The circuit to the right of the dotted line is typical for a car with negative earth and the wiper switch in the earth lead

The voltage across C2 is initially zero but rises exponentially due to the charging current through VRI and R2. This voltage is monitored by the level detecting circuit consisting of $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$.

## SCHMITT TRIGGER

This part of the circuit is known as a "Schmitt trigger" and operates as follows. Initially Trl is cut off, since the voltage on C2 is low. Trl collector is high and is coupled via R 6 to $\operatorname{Tr} 2$ base, so that Tr 2 is turned hard on.

Since R4 and R5 are equal, the voltage at the junction of the two emitters is half the supply voltage i.e. 6 volts. Now when the voltage on the base of $\operatorname{Tr} 1$ approaches ( $6+\mathrm{V}_{\mathrm{be}}$ ) volts, i.e. $6 \cdot 6$ volts, Trl begins to conduct. Its collector voltage falls and Tr 2 is turned off, causing Tr 1 to conduct even harder until it is saturated.

The negative going voltage at the collector of Tr 1 is applied via R7 to the base of $\operatorname{Tr} 3$, which amplifies the current available to drive the gate of the thyristor CSR1; thus the thyristor conducts and the wiper motor operates. R9 is included to protect the thyristor against current surge when the motor first conducts.

## THYRISTOR OPERATION

When a thyristor is made to conduct it will continue to do so even if the gate current is removed until the anode current falls below a threshold known as the "holding current". Consequently if the Delay Unit were being used to drive, say, a lamp then the lamp would remain on until the current were interrupted by opening S1, and similarly if the wipers were not of the self-parking variety then they would continue to function. However, at this point the self-parking mechanism comes to the rescue.

A fraction of a second after the thyristor conducts the self-parking switch makes contact, shorting out points $A$ and $B$. The switch thus diverts the motor current from the thyristor and removes the gate current, turning off the thyristor but allowing the wipers to complete one sweep of the windscreen. In addition C2 discharges through D1 and R1 in readiness for the next delay period. (R1 limits the discharge current to a safe value for DI.)

At the end of the sweep the self-parking mechanism switches off the wiper motor, 12 volts
is restored across the circuit and the cycle of events is repeated.

Capacitor CI is included to protect the circuit against possible voltage spikes from the car's ignition circuits, although no trouble has been experienced in the prototypes.

## DELAY PERIOD

The delay period is determined by the time taken for the voltage on C2 to reach $6 \cdot 6$ volts, and is approximately equal to $0.7 \times \mathrm{CR}$ ( C in farads, R in ohms). Thus with the components specified the maximum delay is 28 seconds.

A delay of several minutes may be obtained by increasing C2; e.g. $500 \mu \mathrm{~F}$ gives three minutes. However, such a long delay is rarely required and adjustment in the most useful range of approximately one to ten seconds becomes very critical. VRI should not be increased in value to obtain a greater delay since there may then be insufficient base current to turn on Trl.

## components list

## Resistors

| Resistors |  |  |  |
| :--- | :--- | :--- | :--- |
| R1 | $100 \Omega$ | R7 | $10 \mathrm{k} \Omega$ |
| R2 | $1.5 \mathrm{k} \Omega$ | R8 | $390 \Omega$ |
| R3 | $1 \mathrm{k} \Omega$ | R9 $0.5 \Omega 3 \mathrm{~W}$ |  |
| R4 | $1 \mathrm{k} \Omega$ | R10 $0.5 \Omega 3 W$ |  |
| R5 | $1 \mathrm{k} \Omega$ | R11 $22 \mathrm{k} \Omega$ |  |
| R6 | $47 \mathrm{k} \Omega$ |  |  |

All resistors $5 \%$ 皆W except where stated
VR1 500ks linear

## Capacitors

| C 1 | $47 \mu \mathrm{~F}$ | 25 V elect. |
| :--- | :--- | :--- |
| C 2. | $80 \mu \mathrm{~F}$ | 25 V elect. |

Semiconductors
Tr1 BC109 (or BC149)
Tr2 BC109 (or BC149)
Tr3 BC187 (or BC159)
D1 1N4148
D2 TLL209 light emitting diode
CSR1 BTY84 100V 12A (Henry's Radlo)
Miscellaneous
Veroboard $63 \times 95 \mathrm{~mm}\left(2 \frac{1}{2} \times 3 \frac{3}{4} \mathrm{in}\right), 0.15 \ln$ mattix,
S1 Single pole onfoff switch
Knob. Materials for case and heatsink.


## kom-pre-hense-iv

> As no doubt you've noticed, Home Radio Components Ltd. are always going on about how comprehensive their catalogue is! So out of interest I looked up the word in a dictionary. It said . . . "KOM-PRE-HENSE-IV, having the quality of comprising much; extensive; full."
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Fig. 2: Lajout of the components on the Veroboard panel and interwiring details. The copper strips run horizontally. The connection to the thyristor anode is made via a solder tag on the heatsink

An indicator is optional, but useful to show when the Wiper Delay Unit is in operation: a small red light-emitting diode D2 was used in the prototype. LEDs have now become comparable in price to a bulb plus bulb-holder and are widely advertised; the one used in the prototype came complete with a little plastic clip for panel mounting.

A bulb could, of course, be used instead, but note that since the indicator will turn off during the course of each wiper sweep, the bulb or LED should be run at a reduced current to avoid distraction at night: hence the high value for R11.

## CONSTRUCTION

The circuit may conveniently be constructed on a $3^{3}{ }_{4} \times 2^{1}{ }_{2}$ in piece of 0.15 in pitch Veroboard. If the layout in Fig. 2 is used then no track breaks will be necessary to accommodate the circuit, although care must be taken to ensure that any nuts and bolts used do not make contact with the tracks.


Fig.3: Connections for the four types of wiper arrangements Negative encountered. (a) Negative earth, wiper switch in earth lead (b) normally earth, wiper switch in live lead (c) Positive earth, wiper switch in earth lead (d) Positive earth, wiper switch in live lead.

The thyristor is mounted on the board using a small bracket. Note that although the wiper motor typically draws 5A the thyristor and R9, R10 run quite cold, because they only conduct for a fraction of a second during each wiper sweep, the self-parking switch taking over for the rest of the sweep.

The thyristor specified is rated at 12 A which is over twice the current drawn in this circuit. However it is readily available for less than 50 p which is considerably cheaper than any thyristor in the 5 A range, with the added bonus of substantial overload protection.

## INSTALLATION

The method used to install the completed circuit will depend on the vehicle for which it is intended. The prototype was mounted in a simple box formed from two pieces of aluminium sheet and sprayed with aerosol paint to match the car: if this is done then it is a good idea to rough up the aluminium surface with fine glasspaper to improve paint adhesion. Alternatively the controls may be mounted directly onto the dashboard and connected to the circuit board by flying leads.

The circuit should be constructed so as to be entirely isolated from the car chassis, the earth connection being provided by a single lead from point A or B, depending on the polarity of the car's electrical system.
In view of the current drawn fairly thick wire should be used to connect up the Wiper Delay Unit to the vehicle. The circuit is identical for systems of either polarity, only the connections being different (see Fig. 3). Thus it is not necessary to construct another circuit if you exchange your elderly positively earthed car for a newer model with a negative earth. Neither is it necessary to have one side of the circuit at chassis potential: so long as the circuit is fully isolated from the chassis it may be used with a vehicle whose wiper switch is connected to the live side of the wiper motor, provided of course that the wipers are self-parking.
The circuit will work without modification in vehicles using 6 volt or 24 volt electrical systems, the delay time being almost independent of supply voltage.

## ON RECENT DEVELOPMENTS

## WATCH OUT

A few Ginsbergs' back I mentioned that it might be prudent to wait for a while if you were intending to purchase a digital watch. I advised this on inside information that a big digital watch price war was imminent in the US. Seems I was right. At a recent trade show, some watches were offered at $\$ 75$ (that's about $£ 30$ if you reckon $\$ 2 \cdot 5$ to the $£ 1$ ). Bowmar has already introduced a two button watch with an led readout which gave the date in addition to the more usual hours and minutes. Note:Bowmar is currently filing for bancruptcy in the US and rumours of a $\$ 20$ million loss are circulating and and have already been reported in print in the States.

Keep an eye out for Timex who are already well-known for lowpriced time pieces. They already have a liquid crystal watch with a less than $\$ 90$ price tag. I still say hang on-they should go a lot lower yet (more inside information; besides, remember calculators!).

## ERE EAR!

How many times have you come across the sentence "Have you heard . ..", or "Did you hear about... etc etc. Sad to say many human beings haven't heard-they're deaf. Way down in the inner ear are minute hair cells each of which "tunes' to different frequencies. Its a simple case of no hairs no hearing, or maybe the hairs are damaged or useless. Then, someone remembered that all the ear does, hair cells and all, is to feed minute electrical signals to the auditory nerve and hearing is established. Somewhere along the line it was reasoned that if only those minute signals could be correctly fed to the auditory nerve, the brain would never know what was sending them. Provided they were right, the brain would believe that it was receiving them from its old friend the ear.

Enter electronics. A system was devised for sending the necessary impulses to the auditory nerve. The results were successful yet disappointing. The upper frequency limit appeared to be around 300 Hz and that certainly wouldn't fool the
brain. It wouldn't even permit the interpretation of speech.

Then, some scientists at Stanford University took an interest, and they've come up with-yes, you've guessed it, an electronic earhole; and it looks like being a winner. What was needed, they claimed, was not a single electrode, but four electrodes. The new circuit, a mixture of thick film and CMOS, promises to offer to the brain, frequencies up to 4 kHz . Now this isn't good enough for listening to hifi, but it does cover all the speech frequencies and if you've previously lived in a completeley silent world that 4 kHz upper limit is really something.

The tiny circuit is implanted but no electrodes are inserted through the skin. Instead, the inputs to the implant are sent over a minute radio link. The link also supplies the few milliwatts of power needed by the circuitry on the implant itself. The information as to which electrode receives which impulses, their amplitude, duration etc. is sent in using an ultrasonic link.
Externally, the "patient" carries a package which houses the microphone, ultrasonic link, the coding circuitry etc. By the end of this year the scientists hope to have the first "patient" hearing. It would, of course, be so easy to finish this story with a funny line, but I think a sincere round of applause would be much better.

## ELECTRONIC <br> FRANKENSTEIN

Still talking matters medical, I'm very interested to hear about Bell Labs and its involvement with lead polsoning. The Labs have come up with a very quick and easy way to check for lead poisoning and the instrument only takes one minute to perform the necessary tests. It requires only a tiny drop of blood, too. Once inside the machine, the blood sample is illuminated by a beam of blue light and the light emission is carefully measured. If excessive amounts of lead are present the blood will give off a red light which is of a specific frequency. The redness, or rather its intensity, is shown on a digital meter. Strangely,
the red light comes from a substance which the blood's haemoglobin makes, when lead is present, called zinc protoporphyrin. The instrument is so sensitive that it can detect down to five trillionths of a gram of zinc protoporphyrin in the single drop of blood required for the sample.

A very interesting aspect of this story is just why Bell Labs is bothering with human blood? Just what has blood got to do with electronics?

According to Bell, the scientists are extremely interested in understanding the electronic properties of large molecules. This interest extends to those molecules which control complicated metabolic and neurological processes in biological systems. Pity Baron Frankenstein isn't still alive unless . . .!

## TIMER I.C.

It looks like another IC has arrived just to confuse the electronicsorientated amateur photographer, especially if he intends making up an electronic timer. Perhaps one of the most popular is the Signetics 555 chip. Now, Ferranti has launched its ZN1034E. The IC is a mixture of digital and linear technology all on the same chip. The company claims that only three external components are required and that accurate time periods provide ranges from milliseconds to weeks.

The chip contains an oscillator whose frequency is determined by an external capacitor and resistor. Output from the oscillator is fed to a divide-by-12 digital divider which can provide timing intervals up to 7,500 times the original time constant of the external capacitor and resistor. At 5 V the chip consumes a modest 5 mA and has a regulator built in. Temperature stability is claimed to be less than $0.01 \% /{ }^{\circ} \mathrm{C}$. The price of a one-off is £2.99p from one of the company's many distributors-NOT from Ferranti direct.

# ЛИ? 

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## Also

DIREGT GOMMERSMOREGEMMER


Although direct convertion receivers have been around for a long time published designs have been few, Ours covers the 160 and 80 m amateur bands but the range cab beextented quite easily.

## and Repairing Hi-FiAmplifiers

As the author points out, there is a right way and a wrong way to service solid state audio amplifiers, and the wrong way can prove expensive ! We indicate the right way.

## DON'T MISSTHIS ISSUE!~ON SALE IN MAY

# Pu apollo genier TRIPLE VARICAP MEDIUM WAVE TUNER/RECEIVER <br> of a capacitor with the depletion layer forming the 

dielectric (see Fig. 1.1).

If a reverse bias is placed across the diode, charges will be drawn away from junction increasing the width of the depletion layer. In other words the plates of the capacitor will be moved apart, thus decreasing the capacitance. The diode may therefore be viewed as a voltage variable capacitor.


Fig. 1.1: As the reverse bias across a diode increases the width of the depletion layer increases and hence the junction capacitance decreases.

All diodes exhibit this effect, the actual capacitance depending on the doping of the semiconductor material during manufacture and the area of the junction. A "varicap" diode is simply one where the degree of doping and geometry of the diode have been controlled to give predictable and repeatable capacitance variations as the bias is varied.


## VARICAP DIODES FOR MW

The main limitation in the application of varicap diodes to lower frequencies ( 3 to 30 MHz ) has been the high cost of devices that are capable of giving a wide capacitance range. The well-known VHF diode, the BBl 04 has a maximum capacitance ratio of only $2 \cdot 8$ as the reverse bias is varied from 3 to 30 V , the total capacity swing being about 55 pF . This is completely inadequate for MW operation where swings of about 260 pF are required.

Another crucial factor in producing varicap diodes for MW operation is the matching of the diodes to provide accurate tracking of the various stages (aerial, RF, and oscillator). The wide capacity swing means that very close tolerance has to be observed throughout the manufacturing process, causing prices to be high.

Because of the very large potential market for low cost, high capacitance varicap diodes several manufacturers have been trying to develop a suitable production process. Recently Motorola have produced two integrated circuits: the MVAM1 consisting of three matched diodes; and the MVAM2 which contains two.

The MVAM1 consists of three diodes with swings of greater than 400 pF per diode and a capacitance ratio of 26 as the bias voltage is changed from 1 to 25 V . They are matched to within $\pm 1.5 \%$ over the entire range. Price is under $£ 3$.

The availability of these diodes means that the designer is no longer constrained by the mechanics of cord drives, scale gearing, etc.

To complete the innovation of electronic tuning, a new style of long throw slider potentiometer has been produced to simplify tuning and scale arrangements. A cursor can be attached to the wiper of the potentiometer to give a direct reading of stations without the need for complicated mechanisms.

Fig. 1.2 shows how the MVAM1 would be applied to a typical superhet tuner. Each diode will exhibit approximately the same capacitance swing, and since the oscillator will be running at the signal frequency plus the intermediate frequency according to conventional superhet practise, it will be necessary to reduce the effective capacity swing in the oscillator section so that it will track at $\mathrm{f}_{\mathrm{six}}+\mathrm{f}_{\mathrm{if}}$.

This is simply achieved by inserting a padder capacitor in series with the tuning diode, the exact value being determined by the value of the inductors employed in the various tuned circuits.

Some tracking error will be inevitable, but this can casily be kept to a tolerable level by careful design of coils.

To set the ends of the ranges for the diodes, a preset resistor is included at each end of the tuning slider.

The slider potentiometer is simply used to tap off a voltage which is applied to the diodes. It is not advisable to employ too low a bias voltage since the $Q$ and cross modulation factors may be adversely affected.

## VARICAP TUNER OPTIONS

Items such as preset station selectors, be they pushbutton or touch sensitive switches, can be employed in exactly the same way as they might be used at VHF.

Remote tuning is no problem: the tuning voltage can be fed down a long cable to a remote receiver with no adverse effect since it is strictly DC. Thus the receiver may be placed in a convenient spot where it is shielded from interference whilst the controls are close at hand.

Some of the other applications for the triple varicap diodes are in sweep generators and spectrum analysers, in self-tuning AM/FM receivers with band scanning and station hold facilities, and in transmitter low power stages, specifically in the oscillator where synthesis techniques are used.

## MW TUNER

In order for the enthusiast to experiment with the new device a simple IC receiver will be described in detail. This requires a power supply of 9 to 12 V plus a separate tuning bias for the varicap of up to 25 V . Various power supplies will be described, the particular one that is chosen being up to the user.

The circuit of the tuner board is shown in Fig. 1.3. The IC used is available under various type numbers depending on manufacturer, NE546, LM1820, $\mu \mathrm{A} 720$, or CA3123E, and provides all the active components for a superhet receiver.


Fig. 1.2: The MVAM1 may be used with a conventional superhet circuit to control the tuned frequencies of the aerial, RF and oscillator stages.


Fig. 1.4: A simple audio amplifier which can be used with the tuner.
A tuned RF stage is used which enhances selectivity and helps reception in the evening when local stations suffer from interference on adjacent frequencies from continental stations.

After the RF stage there is a conventional mixer stage followed by a ceramic filter which enhances IF selectivity. The IF amplifier then feeds into a detector transformer with a conventional silicon diode to detect the AM envelope. The audio output can then be fed into an external power amplifier or a simple amplifier can be incorporated into the design, a suggested circuit being shown in Fig. 1.4.

It is not recommended that substitutes for the specified coils be used.

## CONSTRUCTION

When using ICs that operate in a linear mode at RF frequencies, it is virtually essential to use a printed circuit board if instability and associated problems are to be avoided. A suitable layout is shown in Figs. 1.5 and 1.6. On no account should Veroboard be used. Use a soldering iron of not more than 25 W and avoid prolonged heating of IC pins.

The prototype which can be seen in the photographs was built as a battery-operated radio with the option of either pushbutton or remote slider tuning control. The pushbutton unit consists of six independently variable preset potentiometers one of

which is selected when a pushbutton is pressed. The common wiper output is taken to the tuning voltage input on the board via a changeover switch S 2 used to select the remote slider potentiometer.

An internal 2 W amplifier is incorporated within the case using the LM380 IC and its associated components (See Figs. 1.7 and 1.8). The speaker is mounted in the lid of the case.

An output socket is fitted at the back of the case to allow the connection of the remote slider tuner. The two outer connections to the slider can be commoned with the outer connections to the pushbutton unit but the wiper of the slider must be selected by the changeover switch. Twin-core screened cable was used to connect the slider potentiometers and the main unit.

A metal case was used since the radio was to be used with an external aerial via the coaxial socket on the back of the case. Should the constructor wish to use a ferrite rod aerial, the box must, of course, be plastic. Details of a suitable ferrite rod aerial, which is simply connected in place of the aerial coil T1, are given in Fig. 1.9.

The volume control and the on/off switch are the only controls mounted on the front panel.
A complete interwiring diagram for the receiver is shown in Fig. 1.10.

Should the constructor wish to use an external amplifier the output can be taken directly from the tuner board take-off point.

Ordinary rotary potentiometers can, of course, be used in place of the slider pots, but tuning is more difficult.

## TUNING VOLTAGE

In the circuit shown, a negative voltage is required for the diodes, so with the standard procedure of negative earth, this poses a few problems. Since the varicap diodes are reversed biased, the only current that flows is that through the tuning potentiometer.


Figs. 1.5 and 1.6: Full size printed circuit board layout for the tuner with component locations. The external aerial lead is connected on the reverse

# tecknowledgey 

AMBIT has something more to offer the experimentally minded constructor. More than a unique range of inductive components, the best in radio linear integrated circuits, and our 'by return' service for all items in stock - and you cannot get much faster than that. We have tecknowledgey. And plenty of it. Tecknowledgey is the sort of data and information service that puts other component suppliers to shame.
So next time you want to buy a VHF tunerhead, a complete FM tunerset, or just one ICwouldn't you like some tecknowledgey to help you make certain that you are as well up in modern electronic technology as a component/information service that is as well informed as AMBIT ?

## The ELECTRICWIRELESS

The new Motorola varicap developments, the MVAM 1 \& 2, represent the biggest advance in AM radio design since the introduction of the semiconductor. AMBIT has both types available, plus the sort of coil and filter backup that can only be available through the world's largest manufacturer of consumer radio inductors and filters. TOKO of course.
APOLLO PROJECT: the semiconductors: MVAM1, CA3123E, IN4148 package price $£ 4.00$ the coils and filter: YHCS11100AC2, 6A6371,Y18576AQ,CFU050D package price $£ 1.40$ the PCB: 75p the complete kit for the radio module: $£ 8.00$ the unique long slider: $£ 3.00$ the push button unit o/a
When you buy from AMBIT, we will keep you informed of all the latest developments in this new varicap technology.

# and the rest: 

Larsholt 7252 FM tunerset, a unique 'antenna to audio' system with a spec that includes $1 u V$ for $26 d B S / N$ muting, AFC, AGC, scan tune and lots more. Built and tested for $£ 20$.
TOKO EF5603 tunerhead. The very best from the range, with four signal frequency tuned circuits and MOS input stage.Built and tested for $£ 8.40$ TOKO EC3302. A low cost, but high performance varicap tunerhead with AFC compatible with any quad. det. IC IF system. Built and tested for $£ 5$ Larsholt 8319, the 'head' section of the 7252 tunerset; with AFC, AGC varicap control, dual MOSFET. Top quality Danish make for $£ 7.74$. TOKO MT3302; the EC3302 with three stage FM and two stage AM mechanical geared tuning capacitor. FET input stage. Only $£ 5.30$.

91200 Our double linear phase filter FM IF system with the CA3089E. Which means the lowest distortion FM IF with mute, Meter drive, AFC twin BBR3125N Built and T for $£ 9$ FM1185 A low cost FM IF with the CA3089E, ceramic filter, mute etc. Mini size and high spec for $£ 4.35$. 993090 The 'no compremise' top quality MPX stereo decoder with twin pilot tone filter, LED beacon audio preamps, $\& 100 \mathrm{mV}$ sensitivity. The best you can buy for $£ 7.60$. 91310 Lower cost MPX decoder, but still no corners cut with the module. Twin pilot tone filter, LED beacon, PLL IC. All for just $£ 5.10$.
Accessories for varicap FM radios: Illuminated edgewise panel meters scaled 88-104 (frequency) and with $0-10$ (sig.Strength). $£ 2.35 \mathrm{ea} £ 4.50 \mathrm{pr}$.

A brief selection from the main information folder:

We haven't got space here to go into detail, so use our new short form list service, for a fult list-for the price of a stamp. Coils for everything from audio to VHF, and plenty of stock from our 'by return' service.
Also linears, and other top technology electronic parts. Magnifier time: CA3089E including det.coil £1.94. CA3090AQ inc coil ( 2 mH ) $£ 3.75$. 8038 CC Siggeh chip and VCO $£ 3.10$. MC1310P PLL decoder only $£ 2.20$. 7800 voltage regs - see lists for gen. TOKO 455 kHz mech filters $£ 1.45$. Ceramic filters for 455 kHz 50 p , and for 10.7 MHz 40 p each. Linear phase filters BBR3125N for true 'no distortion' 10.7 MHz IF amps $E 1.35$ each, or $£ 2.50$ per pair. Also 560 series PLL, LM380/381 Also 560 series PLL, CM380/381
TBA810, TBA651, CA3123E, 1496, TBA810, TBA651, CA3123E, 1496, accessories and hardware to make the service complete.

Terms: CWO please. All prices EXCLUDE VAT. P\&P 15p per order. Min.Invoice $£ 5.00$. Min CWO $£ 1.00$ Catalogue (complete with stacks of data) 40p. OR send us an SAE for short form list and summary (FOC) All enquiries to be accompanied by an SAE please. Please avoid burdening our phone service with requests that can be /easily dealt with via post. All our goods are brand new and manufacturers first quality types. We sell no 'seconds' at all.

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Fig. 1.3: Complete circuit diagram of the tuner section of the Apollo. Note that a $20 \mathrm{k} \Omega$ preset or fixed resistor is required at the end of the remote


If a $50 \mathrm{k} \Omega$ potentiometer were used then with a 27 V supply the current would be $500 \mu \mathrm{~A}$. This makes it quite feasible to use three PP3 batteries for the tuning bias, the use of batteries also alleviating the problems of smoothing and decoupling.

If the whole unit were to be run from the same set of batteries then the fluctuations in volume would cause variations in the supply voltage which would, in turn, affect the tuning voltage.

The most elegant method of supplying the necessary voltages is by using the 78 series of three-terminal voltage regulators. These are ICs which take the unregulated supply and turn it out at a predetermined voltage. In the circuit given, (Fig. 1.11) the main module supply is regulated by the 78 L 12 , which is a 100 mA low cost three pin 12 V regulator, and tuning voltage by the 7924.

The overall stability is excellent, the set staying in tune over a wide temperature range.

## SETTING UP

With all the components in place, check for solder bridges, dry joints, etc. Connect the audio amplifier, and then, having tested the voltages beforehand, connect the tuning supply and the main supply.

Set the tuning potentiometer to midway and adjust T1 (or slide the ferrite rod into the aerial coil) until some noise is heard from the AF section. (Holding on to the coil on the ferrite rod will assist in this procedure, as the effect of hand capacity will enhance the sensitivity.)
Although the IF coils are very nearly aligned, it may be necessary to adjust the tuning poteniometer until a strong local station is heard, then peak the detector coil by a slight turn of the core. Then trim the ceramic filter input and output transformersthis will need only a fraction of a turn.

If a signal generator covering IF frequency $(470 \mathrm{kHz})$ is available then loosely couple the output to the circuit and peak for maximum.

To align the RF and aerial stages tune to the low frequency end of the medium wave and either find a station or, using the generator, slide the coil along the ferrite rod (or trim T1) for maximum output. A means of metering this is to monitor the voltage between the detector diode and earth, using a high impedance voltmeter. Note that the voltage goes increasingly negative with increasing signal.



Fig. 1.7: Full size printed circuit board layout for the amplifier and fig. 1.8 component location.


Fig. 1.9 : Ferrite rod aerial winding details. The four leads are connected to the corresponding points on the tuner board and the external aerial connection (E) is not used.


Fig. 1.11: A mains operated supply which will power the tuner and amplifier boards and give the required negative tuning voltage.
Trim the core in the RF stage transformer and then reset to the high frequency end of the MW band. Having established a signal, trim the capacitor in the aerial circuit for maximum. For this tuner the scale should be arranged so that the low end of the frequency range just covers 550 kHz , and the high end covers 1500 kHz .
Reference to your local papers should reveal the frequencies of local radio stations and these may then be used to provide markers. Alternatively, the signal generator or frequency counter may be used for calibration.
The actual frequency being received will be 470 kHz less than the oscillator, in conventional superhet fashion.

NEXT MONTH THE USE OF THE TRIPLE VARICAP IN SWEEP OSCILLATORS WILL BE DISCUSSED

## 

## Sir Oliver modre

EXPERIIMENTIS made by Hentz in the 1880's into the field of electromagnetic radiation through the ether inspired Lodge, who had already obtained repute as an eminent physicist. He amplified and developed the results obtained by Hertz and really pioneered work on coherers.

The detection of wireless signals using the coherer principle was largely due to Oliver Lodge, who in 1889 experimented with two metal spheres which were sited so close to each other that they were separated by a minute film of air.

When current was applied the passage of the spark made the spheres 'cohere'. All it needed to restore the spheres to their original highly resistive condition, was a slight mechanical shock or jolt.

Various pastes, liquids and


This Science Museum photo shows the display devoled to Sir Oliver in their radio gallery.


Sir Oliver in his laboratory c. 1920.

Oliver had, in fact, missed the correct answer by a fraction.

1895 saw Lodge working with Dr. Alexander Muirhead and together they developed the LodgeMuirhead system of wireless telegraphy.

The Lodge-Muirhead coherer which must have been amongst the most sensitive made, consisted of a sharp-edged steel wheel which just touched the surface of a pool of mercury covered with a thin film of oil. The wheel was driven by clockwork. High frequency oscillations were enough to break down the oil film while the continuously rotating wheel ensured that decoherence took place as soon as the signal stopped.

In 1897, Lodge and Muirhead patented several of their ideas and in 1911, the Marconi Company acquired them. In that year, Sir Oliver was made a scientific adviser to the Marconi Co.

## Points

## arising . . .

## REACTION TIMER

April 1975. In the circuit diagram Fig. 1 page 1098, R3 should be shown as $27 \mathrm{k} \Omega$ and R 4 as $47 k \Omega$. The component list is correct.

## PW 'ASCOT' CASSETTE DECK

Part 3 April 1975. Note:-Fig. 5 Part 2 'collector' should read 'emitter'.



## W.K.F. ELECTRONICS

In the March 1975 issue of Practical Wireless, we stated that printed circuit boards could be supplied at the price of 70 p irrespective of size, etc.

This needs clarification. The 70p charge only applies to single page size (6in. x $8 \frac{1}{2} i n$. ) p.c.b.'s on SRBP and not fibre glass.
W.K.F. Electronics are prepared to quote separately for sizes larger than our single page size, i.e. Practical Wireless Electronic Organ main board $£ 5 \cdot 50$ in fibre glass, with power
supply board. All boards are fully drilled and roller tinned.
Prices do not include postage and packing charges. As postal charges have once again been increased (and this applies to all mail order products) please add extra for postage-allowing approximately 10 p per p.c.b. W.K.F. Electronics, Welbeck Street, Whitwell, Worksop, Notts.

## TELE-TENNIS REPRINTS

These are still avallable from:
Chief Cashier (P.W. Tele-Tennis) IPC Magazines, Tower House, Southampton St., WC2E 9QX. Price is $75 p+5 p$ postage.

## "EUROPA B"

The Solid State Modules "Europa B" is a 10 metre to 2 metre s.s.b. transverter. It is an updated version of the very successful"Europa". It is a linear transmit and receive converter for use with either a separate transmitter and receiver or transceivers. Any transmission mode fed into the unit is re-transmitted on 2 m . When used with Musen, Sommerkamp or Yaesu gear the "Europa B" takes its power supply direct from the accessory socket on the .h.f. equipment. When used in conjunction with other gear, the required voltages may be taken from the h.f. equipment or S.S.M.'s matching p.s.u.

The "Europa B" has a slightly different front panel, round knobs and an internal aerial change-over relay.

An SO 239 aerial socket is fitted.
The specification of the "Europa $B^{\prime \prime}$ includes some of the following features: dual-gate MOSFETS in the receive converter, bipolar transistor oscillator chain; valves in transmit converter; low receive noise figure; ten times more accuracy on frequency because of the much closer tolerance crystal used in the oscillator section; 200W p.e.p. input; transmit drive requirement 100 mW and receive converter gain -30 dB .

Price, with valves is $£ 88$. Without valves $£ 74$. Valves required are: 2 off QQV03/10 and 1 off QQV06/40A.

Further details may be obtained from Solid State Modules, 63 Woodhead Road, Solid, Lockwood, Huddersfield HD4 6ER.

TELEFUNKEN CASSETTE DECK
The Telefunken MC3300 HiFi is a stereo cassette deck to DIN 45500 standard. It embodies the Dolby system for noise suppression, has an Electro $\mathrm{CRO}_{2}$ tape selector, HNS audio head, i.e. maximum band modulability and automatic stereo recording level control with manual override. Speech/music changeover switch is coupled with Radio/microphone input selector. Features

include: 2 extra large illuminated peak voltage meters, also operational during playback. 3 slide controls for record left, record right and headphone volume. Headphone socket, speaker switch. Hluminated signals for record, playback, forward and rewind, stop, Dolby and $\mathrm{CRO}_{2}$. 5 rocker switches for electrical function selection. Electronically governed d.c. motor. 3 digit memory counter (memory can be cut out). Electronic end-of-tape and interference detector with stop feature.

Frequency range with chromium dioxide tape is said to be $30-15000$ kHz . Signal to noise ratio with chromium dioxide tape $>57 \mathrm{~dB}$; Noise Suppression Dolby JC; wow and flutter; before tape $< \pm 0.18 \%$ and playback $< \pm 0 \cdot 12 \%$. Recommended Retail Price is $£ 215 \cdot 00$ AEG-Telefunken (UK) Ltd., Bath Road, Slough, SL1 4AW.


## JVC SPEAKERS

Model SK8, recently added to JVC's speaker range is designed for systems handling up to 25 W r.m.s.

The cabinet houses an 8 in . freeedge woofer and a 1 in concave dome tweeter. An acoustic suspension principle is used to achieve a frequency response of 35 Hz to 20 kHz . Crossover frequency is 2.5 kHz and fundamental resonance frequency 67 Hz . Sound pressure level is quoted as $88 \mathrm{~dB} / \mathrm{W}(8 \Omega)$ at 1 M . The SK8's are $17 \frac{1}{2} \mathrm{in}$. high, $9 \frac{3}{16} \mathrm{in}$. wide and $8 \frac{1}{16} \mathrm{in}$. deep. Recommended retail price is $£ 38.50$ each plus VAT. Further information may be obtained from JVC (UK) Limited, Eldonwall Trading Estate, 6/8 Priestley Way, London, N.W.2.

## "DINO" MULTIMETER

The "Dino" multimeter, like the Dolomiti and Cito multimeters hails from the Chinaglia stable.

This 38 -range meter has a basic sensitivity of $200 \mathrm{k} \Omega / \mathrm{V}$ d.c. and $20 \mathrm{k} \Omega / \mathrm{V}$ a.c.

The d.c. current ranges extend from $5 \mu \mathrm{~A}$ right up to 5 A , the voltage ranges from 100 mV to 1.5 kV , and the resistance ranges allow identification from $0 \cdot 2 \Omega$ up to $1 \mathrm{kM} \Omega$. Indeed, in the one package this instrument provides most of the measuring requirements needed for modern semiconductor technology. A.C. ranges extend from 5 mA to 5 A and 5 V to 1.5 kV , whilst there are six dB ranges.

The Dino is built to the usual high Chinaglia standards with shockproof ABS case, Class I, $40 \mu \mathrm{~A}$, $2 \cdot 5 \mathrm{k} \Omega$ movement mounted in sprung jewels and using a core-magnet system. Protection diodes guard the movement against overload. A fullview instrument face combined with anti - parallax mirror help avoid ambiguity of reading. Range switching is achieved using a simple five-position rotary switch in conjunction with separate range sockets for each selection.

A second version of the instrument is available with all the normal ranges, test leads and case, and with an additional internal universal signal injector. The USI version provides a modulated r.f. output rich in harmonics right up into the u.h.f. zones, making the instrument a simple dynamic analysis equipment capable of injecting a signal and observing the result.

A further optional extra is a 30 kV probe to complete the TV servicing facility.
For further information contact Alberto Coniglio, Chinaglia (U.K.) Ltd., 19 Mulberry Walk SW3 6DZ. Tel. 01-352 1897.


## SELF-ADHESIVE CABLE CLIPS

Special Products Distributors Ltd. who market a wide range of tools and equipment inform us that they can supply self-adhesive wiring clips. They grip instantly on any smooth surface to give a strong and permanent fixing-ideal for workshop and radio shack wiring! Insulation of the adhesive pad is said to break down at between 2.5 and 3 kV . Price of the clips is $£ 1 \cdot 40+$ VAT per hundred (size A)-up to $\frac{1}{4}$ in dia. Size B $£ 180$ + VAT per 100 for $\frac{3}{8}$ in dia. wires. Further gen on these and other products from Special Products Distributors Ltd., 81 Piccadilly, London W1V OHL.

## TELE-TENNIS KITS

Marshalls, who have branches in London and Glasgow tell us that they can now supply complete TeleTennis kits for £37, plus VAT and postage.-A. Marshall and Son (London) Limited, Dept. P.W., 42 Cricklewood Broadway, London NW2 3HD (Tel. 01-452 0161).


## NEW CATALOGUES

Arrow Electronics have announced the 6 th edition of their mail order catalogue. It contains details and prices of components, etc. ranging from neons to nuts and bolts and resistors to Mullard modules. For your free copy, send to Arrow Electronics Ltd., 7 Coptfold Road, Brentwood, Essex CM14 4BN.

The Studio Electronics catalogue has special emphasis placed on quadraphony and contains details of various electronic musical instruments. For a free catalogue, write to Studio Electronics Ltd., P.O. Box 18, Harlow, Essex CM18 6SH.

The 1975 Home Radio catalogue is now available. It contains a wealth of information on components and prices and is well-worth having on the bookshelf.-Home Radio (Components) Ltd., 234-240 London Road, Mitcham, Surrey CR4 3HD.

A new catalogue from Elvins gives details of prices of electronic organ components and kits. Send a stamped addressed envelope for a copy of the catalogue to Elvins Electronic Musical Instruments, 12 Brett Road, Hackney, London E8 1 JP .

## BBC CASSETTES

Latest cassette releases from the BBC include "Show of the Week" (includes Baby We Can't go WrongCilla Black, Angel of the MorningOlivia Newton-John). It's a stereo cassette RMC 4014. Bang on a Drum is a kiddies tape (stereo MRMC 004) which includes songs from Play School and Play Away.

Stereo MRMC 018 "Hits on a Harp" is David Snell playing popular numbers on a harp. It's a very pleasing sound and makes terrific background music.

RMC 4017 is a "Top of the Pops" stereo cassette which contains BBC TV's best of the pops available over recent months.

Finally, one for Dickens fans (MRMC 021)—one track features Ebenezer Scrooge (Patrick Magee) and supporting cast in a special dramatisation. The other side is Abel Magwitch (John Hollis)-the convict in Great Expectations. Both tracks, which feature full supporting cast, are ideal for introducing younger children to Dickens and should also hold the interest of older children (and Mums and Dads) who already know the stories.-BBC, London W1A 1AA.


## CRYSTAL CONTROLLED CONVERTER

This employs a crystal oscillator and multiplier chain, RF stage and mixer. The crystal control results in frequency stability otherwise not obtainable combined with reliable read-out of frequencies on a calibrated receiver. As the oscillator frequency is fixed the receiver operates as a tunable IF. A screened communications type receiver with screened aerial input socket is thus almost essential, otherwise short wave transmissions over the tunable IF range will break through at considerable volume. A converter of this type is generally used for specialised reception over a narrow band, such as 144 to 146 MHz , but it can be employed for some other freqencies.

In each case, reception can be in any mode catered for by the main receiver. The usual communications receiver will permit CW, AM and SSB reception which will be of advantage for 2 m amateur signals. Few receivers will permit proper FM reception, though some will give "slope detection" of FM signals, which may be suitable for speech.

## CIRCUIT

The aerial input goes to L1, with a tapping for impedance matching. A second tap supplies the source of the grounded gate FET RF stage Trl, Fig. 4. This stage has less gain than a grounded source stage, does not need neutralising and is capable of broader band coverage. Coils L2 and L3 couple signals to the gate-protected mixer $\operatorname{Tr} 2$. The use of three signal-frequency circuits (L1, L2 and L3) helps remove spurious responses.

The oscillator $\operatorname{Tr} 5$ uses a 35 MHz crystal doubling in each of the grounded base stages $\operatorname{Tr} 4$ and $\operatorname{Tr} 3$, so that L 6 is tuned to 140 MHz . This arrangement is intended for reception of $144-146 \mathrm{MHz}$ amateur band signals, tuning over the range $4-6 \mathrm{MHz}$ on the receiver. L4 in the mixer drain circuit is resonant
near 5 MHz and L 5 couples the output to the receiver, with a screened co-axial lead.

In converters of this type various output frequency ranges may be chosen. An output of $4-6 \mathrm{MHz}$ is likely to give quite open tuning with any receiver while a higher frequency, such as $14-16,24-26$ or $28-30 \mathrm{MHz}$ may be preferred where the receiver is efficient on these ranges and the scale is sufficiently open. A frequency sector which requires bandswitching the receiver is probably best avoided. Where an output other than 4 to 6 MHz is planned, the crystal, L10, L8, L6 and L4 must be modified to suit. The output frequency (L4) will be the difference between the signal frequency ( L 1 to L 3 ) and final oscillator frequency (L6).

As the oscillator chain consumes about 20 mA the converter is run from an external battery. Its main advantage lies in the frequency stability of this type of oscillator, avoidance of hand capacity and similar effects and the ability to re-tune on the receiver to a specific frequency.

## RF MIXER BOARD

This board is shown in Fig. 5. Two tags MC fixed with ${ }^{1}$ in. 6BA bolts provide connecting points to the metal case. All connections between components should be as short as possible, noting that the "Tetfer" trimmers have tags which fit the 0.15 matrix board. Veropins are placed for L1, L2 and L3, the coils being wound with 20 swg tinned copper wire, Fig. 6.

Coil L4 has 60 turns of 32 swg enamelled wire wound in two layers, 40 turns being close wound, followed by 20 turns on a layer of tape. A further layer of tape is put on and L5 wound on top, Fig. 6.

## components list

## CRYSTAL CONTROLLED CONVERTER

Resistors

| R1 | $270 \Omega$ | R6 $100 \mathrm{k} \Omega$ | R11 | $450 \Omega$ |
| :--- | :--- | :--- | :--- | :--- |
| R2 | $390 \Omega$ | R7 $39 \Omega$ | R12 | $56 k \Omega$ |
| R3 | $120 \mathrm{k} \Omega$ | R8 | $150 \Omega$ | R13 |
| R4 | $560 \Omega$ |  |  |  |
| R5 | $220 \Omega$ | R9 $68 \Omega$ |  |  |

All 5 or $10 \% \frac{1}{3}$ or $\frac{1}{4}$ W
Capacitors

| CL | 1000 pF | CB | 1000 pF |
| :--- | :--- | :--- | :--- |
| C 2 | 100 pF | C | 1000 pF |
| C 3 | 100 pF | C 10 | 1000 pF |
| C 4 | $0.047 \mu \mathrm{~F}$ | C 11 | 1000 pF |
| C5 | 10 pF | C 12 | 22 pF |
| C6 | 3.3 pF | C 3 | 1000 pF |
| C7 | $0.01 \mu \mathrm{~F}$ | C 14 | 10 pF |

Tubular or disc ceramic preferred.
TC1/2/3/4 10pF trimmers (Jackson 'Tetfer')
Semiconductors

| Tr1 | MPF102 | Tr4 | BC109 |
| :--- | :--- | :--- | :--- |
| Tr2 | 40673 | Tr5 | 2N706 |
| Tr3 | ZTX108 |  |  |

Miscellaneous
Formers $\frac{5}{16} \mathrm{In}$. dia. (2) with cores (for VHF use). Former $\frac{7}{16} \mathrm{in}$. dia with core ( $\mathrm{L} 4 / \mathrm{L} 5$ ). Veroboard $3 \frac{3}{6} \times \frac{7}{8} i n$, and $3 \frac{7}{4} \times 1 \frac{1}{8} \mathrm{in}$. 0 - 45 in . matrix. Universal chassis $5 \times 4 \times 2 \mathrm{in}$, with extra $5 \times 2 \mathrm{in}$, flanged plate and $5 \times 4 \mathrm{in}$, flat plate (Home Radio) Co-axial sockets (2) On/off switch. X 4 , crystal 35 MHz (wire leadouts) (Senator Crystals, 36 Valleyfield Rd., London, SW162HR).

all 20 s.w.g. tinned copper



This coil is then connected to the co-axial output socket and metal box utilizing a screened lead to keep down the strength of unwanted signals in the 4 to 6 MHz range.

## OSCILLATOR BOARD

The oscillator and multipliers are wired as in Fig. 7. All connections should be very short, including chassis returns such as to the base of $\operatorname{Tr} 4$ and $\operatorname{Tr} 3$ and from C11 and C8 to base. Coil winding information is given in Fig. 6.

## CASEWORK

Cut ${ }^{3} \mathrm{in}$. from each flange of a $5 \times 2 \mathrm{in}$. flanged plate so that this will fit inside the box ends. The $5 \times 2 \mathrm{in}$. screen is bolted centrally to the $5 \times 4 \mathrm{in}$. flat plate and the two $4 \times 2 \mathrm{in}$. flanged ends are fixed using bolts or self-tapping screws. Co-axial input and output sockets and on/off switch are fitted to these ends.
The flat plate is drilled for the bolts "MC" of the RF Mixer and oscillator boards. Each bolt has
two extra nuts so that they can be locked tightly, with adequate clearance under the boards. A lead passes from C6 through a hole in the screen to L6. The box sides and top are added only after the converter is tested and adjusted.

## OSCILLATOR ADJUSTMENT

The easiest method of adjustment is to place an indicating wavemeter set to 35 MHz near L 10 , and aligning the core of L10 until a deflection shows that oscillations are present. Set the core of L10 a little off the peak giving maximum RF or the oscillator may not start every time it is switched on.

Move the wavemeter set to 70 MHz , near 18 and adjust the core for maximum indication. Repeat the same procedure at 140 MHz with the trimmer TC4 and the wavemeter near L6. Later, L10, L8 and TC4 can be readjusted slightly for best results. The doubler chain output, with optimum tuning, is excessive for best results, causing unnecessary background noise. This is cured by slightly de-tuning for best reception.
-continued on page 58

## A series of simple transistor projects, using not more than twenty components.

THIS month's project came about after a request from a young lady for "something to liven up her appearance" at a New Year's Eve fancydress party. She wanted a gadget to cause small lights to flash on and off about her person but, for obvious reasons, whatever it was had to be small enough to be secreted away somewhere in her costume!
We offer the circuit for the benefit of other forward-thinking young ladies and anyone else who is interested in a very economic and novel twist to a well proven idea.

## Circuit

To cut down on current consumption, and to prevent any possible overheating of the fine wires, which had to run around the lady's anatomy, it was decided to use general purpose LEDs which would give a good light output for currents of the order of 5 to 20 mA . Quite clearly the project called for a multivibrator and after some thought transistors were ruled out, the main reason being that the final encapsulation would be too thick whereas a dual-inline package integrated circuit, while taking up more or less the same area, would give a much thinner package for the end product.


Fig. 1 : Basic circuit using two gates of the IC.
${ }^{j}$ By using a standard quad two input NAND gate (SN7400) it was found possible to make two such flashers from the single chip and by benefitting from the use of solid tantalum capacitors the whole circuit was housed on a piece of Veroboard approximately $1^{1} 2 \times$ lin. The batteries ( $4 \cdot 5 \mathrm{~V}$ required) were three SP11 types soldered together in series, with ample interconnecting leads so that they could be discretely tucked away in various parts of the clothing without contributing too much to the bulk of the equipment.

The layout we are giving in this article is slightly larger than the prototype because we have included the LEDS on the same board and have laid out all the resistors horizontally, for clarity. Any other would-be party-goers could run pairs of 32 SWG enamelled copper wire from the board to the individual LEDs which can be sewn into the clothing.


Fig. 2: Layout for complete unit with four LEDs.
The basic circuit for one of the flashers is shown in Fig. 1. Two of the gates from the package are cross coupled with capacitors Cl and C 2 to form the multivibrator. Timing is contnolled by these oapacitors and the resistors R1 and R2 returned to the earth rail. To get reasonably low flashing speeds it is necessary to use large values of capacitance because it is undesirable to increase the values of R1 and R2 above that specified. With the values given the cycle lasts for approximately half a second. To alter the speed increase or decrease the values for C 1 and C2 and leave the resistors as they are.

Initially it had been expected that it would be necessary to feed the output of each side of the multivibrator into each of the two remaining gates on the chip to act as buffers but after experimentation this was not found to be necessary. There was sufficient current available to drive the LEDs direct

## components list

| R1 | $4 \cdot 7 \mathrm{k} \Omega$ | R8 $100 \Omega$ (see text) |
| :---: | :---: | :---: |
| R2 | 4:7kS | CIJC4 $47 \mu \mathrm{~F} 6 \mathrm{~V}$ tantalum |
| R3 | $100 \Omega$ (see text) | (see text) |
| R4 | $100 \Omega$ (see text) | D1/4 MV 5025 (or G.P. |
| R5 | $4.7 \mathrm{k} \Omega$ | Light emitting diode) |
| $R 6$ | 4.7ka | IC1 SN7400 |
| R7 | $100 \Omega$ (see text) | Piece of veroboard |



## RF SECTION

If any equipment is available providing a signal in the 2 m band, adjust TC1, TC2 and TC3 for best reception of the signal. Peak the core of L 4 at about 5 MHz or at the wanted part of the frequency band. If no tuning-up signal is available, set these trimmers about half open and try to locate a 2 m transmission. In many areas it will probably be necessary to do this at week-ends or other times when the band is known to be active. Once a signal is heard, trim for best volume. It could be necessary to stretch or compress L1, L2 or L3 a little, if any trimmer comes at the limit of its travel. If necessary L4 may be peaked by temporarily placing an aerial near the drain lead of Tr 2 and setting the core of L 4 for best volume with a 4 to 6 MHz signal.

With a 35 MHz crystal and L 6 operating at 140 MHz the 4 MHz point on the receiver dial will be 144 MHz ,


Finished converter with boards mounted either side of screen.
while $4 \cdot 5 \mathrm{MHz}$ is $144 \cdot 5 \mathrm{MHz}, 5 \mathrm{MHz}$ is 145 MHz and so on. The band 4 MHz to 6 MHz thus tunes 144 MHz to 146 MHz .
The oscillator section requires about 20 mA and the RF/Mixer about 10 mA , so a PP9 or similar battery is suitable.
Though the need to avoid breakthrough of $4-6 \mathrm{MHz}$ signals has been mentioned, it should be repeated
that complete screening in the way described is necessary.

For maximum possible efficiency the positions of the coil tappings can be the subject of experiment. A small coupling capacitance made from a length of twin insulated wire can also be added between the top ends of L2 and L3. However, good results should be obtained without this, and with the tappings as shown.

## TAKE 20-continued from page 56

without there being any significant influence on the running of the multivibrator.
The current through the diodes has, of course, to be limited through R3 and R4. The values given, 100 ohms, provide maximum light output but the current consumption of the circuit as shown is about 20 mA . This can be reduced significantly by increasing the values of the two limiting resistors but at the expense of light output.

## Construction

The layout, shown in Fig. 2, shows two such flashers on the single layout. The designations in Fig. 1 refer to the left-hand pair of gates of the integrated circuit. The right-hand pair are comnected to an identical circuit, even the timing capacitors are the same, but alternative values for C3 and C4 can be substituted.

When using the tantalum capacitors make sure they are connected with the correct polarity. Alternately, use conventional electrolytics but they will take up considerably more space on the board and modify the layout accordingly. Likewise take very great care to wire the LEDs with the correct polarity, particularly if they are on the ends of flying leads! With the type specified the cathode (end connecting to the limiting resistor) is identified by a very small indent at the base of the encapsulation, which can be felt with the finger nail.

For the more adventurous extend the circuit to give three pairs of flashing lights using a standard hex inverter. Notice that each of the gates used in this circuit is operating as a straightforward inverter with the pairs of inputs shorted together.

All the components are readily available from $P W$ advertisers but we regret we are unable to supply the name and address of the young lady who inspired the project!

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| 7404 | 0.18 | 0.16 | 0.15 | 7450 | $0 \cdot 15$ | $0 \cdot 14$ | 0.13 | 7492 | 0.51 | $0 \cdot 46$ | 0.42 |
| 7405 | 0.18 | 0.16 | $0 \cdot 15$ | 7451 | 0.15 | 0.14 | 0.13 | 7493 | 0.48 | 0.44 | 0.41 |
| 7408 | 0.18 | 0.16 | 0.14 | 7453 | 0.15 | 0.14 | $0 \cdot 13$ | 7495 | $0 \cdot 68$ | 0.61 | 0.57 |
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| 7413 | 0.32 | 0.31 | 0.30 | 7472 | 0.28 | 0.25 | $0 \cdot 23$ | 74121 | $0 \cdot 34$ | 0.31 | 29 |
| 7417 | 0.30 | 0.29 | 0.28 | 7473 | 0.33 | 0.34 | 0.28 | 74123 | $0 \cdot 68$ | 0.61 | 0.57 |
| 7420 | $0 \cdot 15$ | 0.14 | 0.13 | 7474 | $0 \cdot 33$ | $0 \cdot 31$ | $0 \cdot 29$ | 74141 | 0.79 | 0.72 | 0.67 |
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## REPORT



NOT very many years have passed since the appearance in this country of the first digital multimeter selling at under $£ 100$. Now a number are available at around $£ 60$-quite a drop even if you don't take into account the intervening fall in the value of the pound. As in the case of pocket calculators, the main factor behind this fall in price lies in the adoption of LSI techniques for the heart of the circuitry.
One of this new generation of digital multimeters is the DM2 by Sinclair Radionics-their second venture into the field. In common with most of the lower priced digital meters it uses an integrating converter, in this case one based on the dual-slope technique which offers a number of advantages over the simple system. A description of the basic principles of the dual-slope integration d.v.m. would probably be of interest to those not already familiar with them.


Fig. 1: The dual-slope integration technique.

## Dual slope integration

The unknown voltage $V x$ is applied to a voltage-to-current converter whose output charges a capacitor over a fixed time $t 1 / t 2$, see Fig. 1, controlled by a standard frequency oscillator. The voltage V1 attained by the capacitor at the end of this fixed time is proportional to the unknown voltage $V \mathrm{x}$.

At time t2, the capacitor is disconnected from $V x$ and connected instead to a reference voltage of the opposite polarity, -Vref. It will then discharge at a rate set by $-V$ ref until its voltage reaches zero again at time t3. The period $t 2 / t 3$ is thus proportional to $V 1$, which was in turn proportional to $V x$, so by measuring that period we will have an indication of the unkown voltage. The measurement is simply performed by feeding the output of the standard frequency oscillator to a digital counter via a gate which is arranged to open at time $t 2$ and close again at $t 3$. By suitable scaling the counter will indicate directly the applied voltage.

Because the same oscillator both controls the charge period and measures the discharge time, its actual frequency is not important-the only requirement is that it should not change during the measurement. For similar reasons, the value of the capacitor is not critical; it just needs to have good short-term stability. Thus temperature changes and long-term drifts have little effect on the instrument's accuracy.

## Operating speed

Since integration by its very nature and definition takes time, integrating meters are not fast in operation. They are therefore unsuitable for applications where a rapidly fluctuating input is to be monitored, for instance where a control is to be set quickly to produce a certain voltage reading, or in data-logging systems where successive sampling of a number of input levels is required. To this cloud there is a silver lining, however, for this slow response will integrate out noise spikes which can upset faster reading instruments.

The Sinclair DM2 is a $3 \frac{1}{2}$ digit instrument. For the benefit of those readers unversed in d.v.m. terminology, this means

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5 im .3 oltu 51,95 ，P．\＆P．15p． $7 \times 4 \mathrm{in}$ ． 3 ohtn $\$ 1 \cdot 40$ ，P．\＆P． $20 \mathrm{p}, 10$ ． 6 in ． 3 or 15 ohra $\varepsilon 2 \cdot 10$ ，P．\＆P． 30 p ．E．M．I． E．M．I． 133 \＆ 8 in．with high fiur ceramic magnet with larasitig tweeter 3， 8 or 15 ohm $88 \cdot 60, P$ ．$\&$ P．30p．
E．M．f． 13 8in．3． 8 or 15 ohm with inbuilt tweeter and crusiorer netrork $\$ 4 \cdot 65$, P．\＆P． 30 p ．
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BRAND KEW．Bakers Loudgipeakers at shbstantial dis－ counts．LSin．15w．H／7）Speakers，3， 8 or 15 ohms，State which．Current produetion hy well－known Britigh maker．
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AMPLIFIER HAB4 MK II Designed for Hi－Fi reproduc－ tion of records．A．C．Mains operation．Ready built on phassis，size $7 \frac{1}{2}^{\prime \prime}$ w．$\times 4^{\prime \prime} d . x$
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Super reproduction of both music and speech，with negll－ gible hum．Separate inpula for mike and gram allow records and announcements
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## BRITISH NATIONAL RADIO

 AND ELECTRONICS SCHOOLit has a four-digit display of which the first (most significant) digit can only be 0 or 1. A variation of this can occur where, as in the DM2, the leading (left hand) zero is suppressed to avoid displaying unnecessary information which might confuse the operator, In this case the first digit is either a blank or a 1. The result in either case is to extend the indication range of the instrument from 0-999 to 0-1999, a very useful extension requiring the minimum of additional circuitry.
The readout in the DM2 uses four $8 \mathrm{~mm}(0 \cdot 3 \mathrm{in}$.) 7 -segment l.e.d. displays; the necessary decoder and driver circuits are included in the custom LSI chip. Two sets of push-buttons select the five functions-a.c. voltage and current, d.c. voltage and current, and resistance-and the four range multipliers from 1 to 1000 . Automatic dual-polarity operation is incorporated, as is automatic over-range and overload indication. In each case the relative information appears in the l.e.d. display on otherwise unused segments of the most significant digit.

## Power supply

For convenience and portability, the instrument is battery powered, up to 60 hours of use being obtained with a single standard PP9 or equivalent. Sockets are provided at the rear of the instrument for an external power supply. This must provide a stable 9 V with a current capability of 70 mA average, 150 mA surge. One minor criticism is that these sockets are unlabelled as to function or input requirements*. An instrument which is so easily operated is likely to be quickly separated from its operating instruction leaflet, which clearly

* Sinclair tell us that these sockets will be clearly identified in future production.


This photograph shows the uncluttered interior layout. Interconnections on the push-bution switch banks are made via a small subsidiary p.c.b.

## Maker's specification

```
D.C. VOLTAGE
    Rapge Resolution
\begin{tabular}{cc}
1 V & 1 V \\
10 V & 10 mV \\
100 V & 100 mV \\
1000 V & 1 V.
\end{tabular} TACE
A.C. Y
Range
10v
10 V
100 y
71000Y
```

Steviracy $03 \% \geq 1$ digit

Accuracy
$10 \% \pm 2$ digits
D.C. CURRENT

A.C.CURRENT

Hange 1 mA 10 mA
100 niA
1000 mA

## Accuracy.

$20 \% \pm 1$ digit
$0.8 \% \div 1$ digir
$20 \%+10$ oigit

RESISTANCE


* Maximum input on a.c. yoltage is 500 V .
- Additional ranges obtaiñed by speciad switching combinations:

TYPICAL TEMPERATURE COLEFFICIENTS

| D. ranges | $0.03 \%$ per ${ }^{\circ} \mathrm{C}$ |
| :--- | :--- |
| A.c. ranges | $0.05 \%$ per ${ }^{\circ} \mathrm{C}$ |
| Resistance ranges | $0.05 \%$ per ${ }^{\circ} \mathrm{C}$ |

OPERATING TEMPERATURERANGE $0^{\circ} \mathrm{C}$ to $+50^{\circ} \mathrm{C}$

Suze
Meig t $56 \mathrm{~mm}(2 \cdot 2 \mathrm{in})$
Width $225 \mathrm{~mm}(8.8 \mathrm{in})$
Dépth 155 mm ( 6 1iñ )
excluding knobs, feet and handle

## WEIGHT

$1 \mathrm{~kg}(2.216 \mathrm{~s})$ excludipg battery
warns that no more than 10 V must be applied. This omission would seem to be a potential source of damage. A separate a.c. mains power unit giving a suitable 9 V supply is available from Sinclair.

The basic measurement range of the instrument is 1 V d.c., giving a resolution of 1 mV with over-range to $\pm 1999 \mathrm{~V}$. A m.o.s.f.e.t. operational amplifier input stage achieves an input impedance of $100 \mathrm{M} \Omega$ on this range; the voltage divider chain reduces this to $10 \mathrm{M} \Omega$ on the other d.c. voltage ranges. A mean averaging a.c. to d.c. converter is used for the a.c voltage and current ranges. Its frequency range is 20 Hz 3 kHz on voltage ranges up to $100 \mathrm{~V}, 20 \mathrm{~Hz}-1 \mathrm{kHz}$ on the 1000 V and current ranges.

The DM2 can safely withstand a considerable overload on the lower voltage and current ranges, while fuse protection is incorporated for the current and resistance ranges.


## by Eric Dowdeswell G4AR

JUST a few words this month on the log extracts that appear at the end of this feature. Probably the majority of listeners to the amateur bands get drawn into the exciting race of hearing, and getting confirmation, of as many different countries as possible, thereby qualifying for various certifcates and awards. The log extracts given here are designed to highlight the more unusual stations and prefixes that appear on the bands and thus enable vacancies to be filled in our 'wanted' list, be they countries or prefixes. Modern DXpeditions frequently take unto themselves a special call sign to make their appearance doubly attractive.
To those of you who are kind enough to send in logs for this column may I ask that you restrict your entries to stations that come within the above category? Six a month would be exceptional!
John Porter (Baslow, Derbys) concentrated on 20 m CW and I wonder if John has noticed that his best DX tends to be in a north/south line as befits his east/west dipole. Could be missing something good off the ends! Tim Charles (Colchester) tells us about TT2CF due on from the Cocos Isles, for a rare one, with SSB on the usual bands plus CW on Top Band! Don't laugh, it's not impossible! Not long ago KV4FZ managed to work all continents (WAC) in eight hours on this band! Tim also mentions that the Gambia has dropped ZD3 in favour of C5.
Paul Heath (Wolverhampton) bemoans the "pretty hopeless reception other than 80 m " but with an R1155 I'd tend to suspect the receiver rather than conditions! Paul is in the process of doing some rewiring to it so let's hope for better things. Mike Green (Northwich) suggests that Max France might do better with Oscar if he used crossed dipoles instead of verticals. Agreed, but even better is some simple way of tracking the satellite, perhaps a handheld aerial, in order to increase the period of reception. Andrew Swiffin A8603 (Cheadle) has now got a crystal-controlled converter for the HF bands, feeding into a PW design as a tuneable IF. This is a very efficient way of ensuring success on these frequencies if the main receiver is not too hot.
Paul Broadhurst (Near Clevedon) stuck to 80 m and found A51TY in Bhutan and YB0AAG in Djarkarta for a couple of interesting prefixes. His 150ft wire feeds a Trio 9R59DS and PR40 preselector. Steve Blake (Aylesbury) has moved to "join the men up on VHF"! Hey, that's not nice at all! A 6-element Yagi feeds a converter into his Codar CR7OA at 28 to 30 MHz .

Graham Bleakley QSL/Publicity bod for the West of Scotland ARS GM4AGG reports demolition of the club's premises so write to him at 82 Ash Road,

Cumbernauld, Dumbartonshire for current details of venues and club meetings. Alan Rae (Glasgow) has now got his Morse up to a decent speed and found some goodies that he had previously missed. Those who take the trouble to learn the code are rewarded with a completely new world of interest, virtually another language. Roger London A8673 (London SE2) was one of several who copied the jungle outfit of HP1XJS/P/HP7 for an unusual catch, this time on 15 m SSB.
Peter Walton (Llanfair P. G., Gwynedd) at 12 years of age is our latest recruit, with an Eddystone 358 and 85 ft of wire. Stephen Budd A8713 (Worthing) was worried at not being able to give me the frequencies of stations to better than 10 kHz on his AR88. Not to worry Steve, since very few stations are crystal controlled nowadays. Listen for the sudden rise in the QRM, the DX will be underneath, in what was a quiet slot a few minutes previously! Again from Tim Charles, "phew, 45 minutes to copy out the log." This time I can't say that there are any ordinary ones in his list, ranging from 160 to 2 m , with the exception of 10 and 15 m . He likes to listen through the GB3PI repeater on 2 m but finds it jammed up whenever there is a lift in conditions.
Graham Nicholls G4DLB (Banbury) has stuck to working stuff on 2 m and 70 cm on CW, SSB and FM and enjoyed the recent good conditions enabling him to get into SM on 2 m and PA0 on 70 cm . M. C. P. Bennett (Slough) mentions the CG3 stations, normally VE3, in Listowel, Canada, celebrating some town event! Any more candidates for the "How stupid can you get" competition??

## Log extracts

M. Green:- 80 m HK3LT ZL1BCC 5U7AH 20 m TU2DP VP8HZ JY9CR (POB 2788 Amman) 15m A4XFE HZ1AT VQ9BP
J. Porter:- 80m A2CCY 8P6ES 20 m CT2BP PJ3SF ZD8TM 5T5FP 15m ZD8TM
A. Doherty:- 80 m HC2YL VQ9M PZ1AE 20 m VK9ZQ 8P6ES 15m EP2SN KV4AD 80m TA3HB VP9GD XW8FA YB0ABV 5U7AH
A. Swiffin:- 80 m PJ3DO VU2DGD 20m CT3AR EA9FB VE8RCS
P. Broadhurst:- 80 m A51TY CT2AE YB0AAG 5B4BC 9G1DY
S. Blake:- 2 m F1DJR GI8EWM GM8FFX SM6DKU
P. Barker:- 80 m A4XVB 20m PZ5FB TA2SC TJ1AD VS5MC 20m (SSTV) DJ4SS EA4DT HA2KRB I8MGQ OH5RM YU2CDS
A. Rae:- 160 m PY1RO 80 m AP2KS ZB2CF ZL4KF
S. Budd:- 80m 7X0EEG 20m CR4BS FL8DA JY9CR VQ9BP 4W1GM 15m WB2POJ/VQ9
G. Nicholls:--2m worked ON5NY OZ1OF SM7AED 70 cm worked G3KMS GW3UCB/P
M. Bennett:- 80 m A4XVC ET3ZU HK4WWB VS5MC 9M2BU 20m EL5G HR6SWA HV1CN HV3SJ TU2EP 15m A4XFU HZ1AT TJ1AD
M. Sole:-HZ1TA MII PY6AHM TR8DG XU1DX ZL3PE 3V8BU 40 m ZL1AQ
T. Charles:- 160 m KV4FZ KZ5WA VE1WE STRAY W2KH WA4GTB W6UD WB8APH 80 m FL8DN HC2TR KZ5WA KL"DRT KS4IZ TG8KT XE3LK YS2HM ZL1BEA 5N2ESH 5T5DY 8R1AG 40m CO2NV XE6WHK ZD3P ZL1FM 20m C5AR (Gambia) KC4AZ VP8NP XT2AE 2m DC2BE GC4ASO SM6FBQ
Stations SSB except those in bold which are CW.

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| J45 | Suits 2 SA35 or 1 SA50 (4 ohm) | ¢6.50 | $\begin{gathered} \text { Carriage } \\ 50 \mathrm{P}, \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| PU70 | Suits $25 A 50$ ( 8 ohm ) or 2 SA100 | 49.50 | $\begin{aligned} & \text { Carriage } \\ & 60 \mathrm{p} \end{aligned}$ | STABILISED

PS45 Suits 2 SA35 or $\mathbf{5 5 \cdot 5 0 ~ C a r r i a g e ~}$
MT45 $\underset{\substack{\text { Transformer for } \\ \text { above } \\ \text { M } \\ \text { P3.90 }}}{\substack{\text { Carriage } \\ 50 \mathrm{p}}}$

PS70 Suits 2 SAl00 $\mathbf{E 6 . 5 0}$
MT70 $\underset{\substack{\text { Transformer or } \\ \text { above }}}{\boldsymbol{6 5} 50}$
Carriage
N.B. PS70 is not suitable for the SA50

## Mk II STEREO DISCO MIXER $\mathbf{E 2 9 \cdot 5 0}$

This well tried unit mixes two deeks, Carr. 60p ceramic eartridge, and features mic over-rides any ceramic cartridge, and features mic over-ride pius separate full range bass and treble controls on both mic and deck inputs. Ample headphone power is mains operared. Fitted with sturdy screening case. Controls: Mic vol, base, treble. Left/Right fade, deck
 volume, bass, treble, h/phone select. vol, Mains. Size $17 \frac{1}{2}$ in $\times \operatorname{3in} \times 4$ in deep.

## 

Thousands sold of this extremely popular mono version. A mic input may be fitted using the VA30 (see below). Low consumption from a 9 V batzery. Features the same high standards of reproduction as the Stereo vorsion Controls: H/phone solect, yol, Left deck vol, Right deck vol, bass, treble, master vol. Size $12 \frac{s}{4} i n \times$ in $\times$ in deep.


## 3-CHANNEL SOUND-LITE $\mathbf{E 2 4 . 7 5}$ Carr.

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## MEDIUM WAVE DX <br> by CHARLES MOLLOY

THE Newfoundland station CJON on 930 kHz was my first Transatlantic DX contact ever, on November 9th. In January reception was fairly consistent and only on three of the nights that I stayed up to 0200 was the station unreadable" writes Steve Whitt from NW London. Steve uses an HRO communications receiver with a 40 ft outdoor aerial to pull in his medium wave DX which includes CBM in Montreal on 940 kHz with a news bulletin and WNEW in New York City on 1130 kHz with a basketball commentary. Transatlantic reception in the UK starts about six hours after sunset and even during the summer months reception is possible for an hour before sunrise.

Roy Patrick reports again from his new QTH at Mackworth in Derby with a fine log of reception from both North and South America, West Africa and the Middle East. His receiver is a Trio 9R59D and he logged Morocco on 818 kHz CJCH in Halifax, Nova Scotia on 920 kHz at 0215 , CJON St. John's on 930 kHz at 0145 , Radio el Mundo in Buenos Aires, Argentina on 1070 kHz at 0240 , Voice of America in Rhodes on 1259 kHz with sign-on at 0300 , Kuwait with Arabic music at 0250 on 1345 kHz and Conakry in Guinea on 1403 kHz at 0020 . Roy mentions hearing a broadcast in. Arabic on 1205 kHz which is almost certain to be Radio Sanaa in the Yemen Arab Republic, a fine catch.

## SHORT WAVE BROADCASTS

## by Derek Bell

WE have been set a challenge this month by Johin Godwin from Rugeley, He wants us to try for, as he puts it, "the elusive ZL3" this is a $7^{1}{ }_{2} \mathrm{~kW}$ station in New Zealand. Mr. Godwin's method is to try Radio Australia on the 25 m band to see if the path is open. Then he tunes 15 kHz higher to 11780 and listens for a very weak signal. John reports that it usually has rapid flutter and that he has to have everything screwed up tight on his pre-war HRO receiver and dare not" even breathe too deeply for fear of losing it! The best time is 0845 to 0930 and the address for a QSL is: New Zealand Broadcasting Corp., P.O. Box 2396, Wellington 1 N.Z., but please send two International Reply Coupons to pay for the return postage.
"Nothing special here but the best I can get." So says Eric Chowanietz of Braunstone, Leicester. He then goes on to list the following:
T.R.T. Voice of Turkey on 11880 at 2300

Radio Cairo on 9700 at 2245
Radio Finland on 9555 at 1620.
All this on a Fidelity Comet transistor set. Reader Bob Stone from Plymouth writes to enquire if any one knows of a "Radio Dominicana" on 5967. The only one I can trace is Radio TV Dominicana of Santo Domingo in the Dominican Republic. The trouble is that as far as I can see their only outlet is on the medium wave. Christopher Hasman is the

Harold Emblem of Mirfield in Yorkshire is still active on the medium waves with his Eddystone 730 receiver and medium wave loop aerial. He has logged four Canadian stations, CBN St. John's in Newfoundland on $640 \mathrm{kHz}, \mathrm{CBH}$ in Halifax, Nove Scotia on 860 kHz , CJON St. John's on 930 kHz and CHNS in Halifax on 960 kHz together with Radio Sahara in Spanish Sahara on 656 kHz . Others include Radio Andorra on 701 kHz , Bagdad on 760 kHz , Yerevan, Armenia on 863 kHz , Rajkot, India on 1070 kHz and Conakry, Guinea on 1403 kHz . Harold reports hearing Tashkent, Uzbekistan well at 0300 hrs on 908 kHz over Thourah, Iraq on the same frequency.

Fred Dinning of Dunlop, Ayrshire has sent an outstanding log of North American DX. Using his SP600 receiver, $6000 \mathrm{ft}(!)$ Beverage aerial and medium wave loop he logged 72 stations in Canada and the United States between 0300 and 0800 during the first week of January. The most notable logged are WMAQ in Chicago on 670 kHz , WOR in New York City on 710 kHz , WSB Atlanta, Georgia on 750 kHz , WJR in Detroit on 760 kHz , WBBM Chicago on 780 kHz ; WGY Schenectady, NY on 810 kHz , WBAP Fort Worth in Texas on 820 kHz , WCCO Minneapolis on $830 \mathrm{k} \cdot \mathrm{Hz}$, WHAS Louisville, Kentucky on 840 kHz , KOA Denver, Colorado on 850 kHz , WWL New Orleans on 870 kHz , WLS Chicago 890 kHz , WCFL Chicago 1000 kHz , KDKA Pittsburg on 1020 kHz , WHO Des Moines on 1040 kHz , CHUM Toronto on 1050 kHz , KING Seattle on 1090 kHz , KMOX St. Louis 1120 kHz , KSL in Salt Lake City on 1160 kHz and WOAI San Antonio, Texas on 1200 kHz . Fred's $\log$ is an indication of the improved conditions on the medium waveband now that we are approaching the minimum of the sunspot cycle, expected in 1976. Medium wave DXers can confidently look forward to a return of the outstanding DX of ten years ago when a few of the more common North Americans were, on occasion, heard in this country on transistor portables.
proud new owner of a Bush VTR178 and he' takes us into the realms of inner space by logging the last Russian space flight between 121 and 146 MHz . This was achieved using a BBG1 TV aerial. Christopher also informs us that the US-Soviet joint flight in July will be using the same frequencies. However, sadly, the TV aerial has gone back to its rightful owner and Christopher is appealing for help.

An example of the "giveaway" comes from Frank Allen of Ilfracombe. On his QR666 he logged and QSLed Radio Pyongyang on 6576 at 2000 and they replied by sending two ten-inch double sided LP records of an opera based on a hosiptal at war, along with a multitude of books and stamps. The QR666, by the way, is the replacement for the phased out Trio 9R59DS and costs a lot more than the old workhorse! A self-confessed crystal-set addict is Andrew McIntee of The Schoolhouse, Craichie, Forfar. This gallant Scot owns three of them and has pulled in, among others:

Radio Messiah on 6050 at 1915.
This is a new one on me, can anyone give some more gen. Arthur Bell is no relation, honestly, but by chance he picked up PW and got hooked on the SW page. Being, as he says, a greenhorn he admits to being all at sea with the frequency figures. These are always in megahertz, Arthur, and the times are always twenty-four hour clock and given in Greenwich time only. The hertz equals one cycle per second, thus a megahertz equals the old megacycle.

The metre band system used by some stations, covers a small segment of the spectrum. For example, the twenty metre amateur band runs from 14 to 14.350 MHz or over 350 kHz . Regarding a list of stations of the world, the "Radio and TV Handbook", published by BillBoard Publications should fill the void. Finally, I can say, Arthur, that to log Radio Australia on an Astrad 17 is pretty good going!
A letter that came some time ago but unfortunately had to be held back was from G. E. W. Hewlett. This gentleman has been DXing since (would you believe) 1928! He built. a one-valve receiver and later added it to another rig in order to improve them both. This was done by plugging the first set, as an RF amplifier, into the detector valve socket of the second. As a result of this a QSL came from VK3LR, or, as it later became, Radio Australia. Since then Mr. Hewlett has become a confirmed radio fan "down under" and can quote, at the drop of a hat, all the times and frequencies of this far-away station. In fact, Mr. Hewlett sometimes spends up to eight hours a day monitoring the VK's.

My enquiries recently about FEBA in the Seychelles seem to have borne fruit. I have beside me a logging by Roy Wooden of Staines who reports FEBA on 11715 and says that it puts out English on Tuesdays and Wednesdays from 1745 to 1800. However, Roy advises us to get in soon as the service to the Middle East will be phased out and more emphasis will be placed on the Far Eastern, South African and Indian Ocean islands, with, perhaps, the loss to us here in Europe of this signal.

Having written the above about "us here in Europe", I was surprised to have in the mail an air
letter from David Samuel in Johore Baru, Malasia. David comes to the aid of our recent enquirer who had a daughter in Thailand and sends the tip that perhaps she listens to the BBC World Service from the Malasia relay. Many thanks David for the welcome gen. Another reply to an enquiry comes from John Dipré of Stoke Newington, London. He would like to help our reader who was suffering from "anaemia" of the 60 m band so, if Glenn Tobin is interested, John will make all as clear as crystal for him. John reports thirteen different countries on the band using a VEF204. Among them Honduras, Costa Rica, Togo and the Sudan. Pass your secret on, John, and we will all share it!
From the steel town of Sheffield comes David Williams to give us the low-down on the $2 \cdot 5,5,10$ and 15 MHz fixed frequency time signals. He writes that the United States Bureau of Standards puts out signals on these frequencies from stations in Hawaii and Washington with IDs. on the hour. The voice ID from Hawaii is a woman (or xyl, as they say) and a man from Washington. Turning now to station news Radio Portugal recently announced that they are to stop QSLs until further notice, but that they hope to start a DX show soon, while Radio Baghdad has started to send out copper emblems with some of their QSLs. The one and only "Happy Station" on Sunday from Radio Nederland, has announced an alternate frequency of 5965 , the old ORTF slot. RN has also been testing on 5955 from 0930 to 1050 and would like reports. A new DX show starts soon on Liverpool's local "Radio City." This station moves into VHF in February and the DX show is on the late night show, alternate Sundays, in the "wee small hours."


Your reviewer has been using a DM2 for about three months for servicing and experimentation and has found it rellable and easy to use. The display is quite bright and is fitted with a violet filter to improve its contrast. Even so, if your workbench is near a window or has a good bench-lamp you will find that you need to tuck the meter away in a shady corner for easy reading.

Complete screening of the instrument is provided by the case, based on robust aluminium extrusions. The dual purpose handle/bench stand is useful, as is the optional carrying case which allows the DM2 to be used slung around the neck.

In the absence of any suitable instruments for comparison, I cannot really comment upon the accuracy of readings
obtained except to say that a selection of $1 \%$ resistors checked out well and other results were always "as expected".

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| 0.5 | $0 \cdot 26$ | 111 | 1.28 | 0.22 |
| 1 | $0 \cdot 5$ | 213 | $1 \cdot 58$ | 0.22 |
| 2 | 1 | 71 | 2.08 | 0.22 |
| 4 | 2 | 18 | 2-68 | 0.38 |
| 6 | 3 | 70 | 3.80 | $0 \cdot 42$ |
| $\varepsilon$ | 4 | 108 | 4.20 | 0.52 |
| 10 | J | 74 | 4.80 | 0.52 |
| 12 | 6 | 116 | $5 \cdot 01$ | 0.52 |
| 16 | \% | 17 | 6.22 | 0.52 |
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| 3 |  |  | 4.10 | $0 \cdot 42$ |
| 4 |  |  | 4 4 | 052 |
| 5 |  |  | 5.80 | 0.42 |
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| 60 | 149 | $7-95$ | $0-80$ | $4-00$ | 0.38 |
| ---: | ---: | ---: | :--- | :--- | :--- |
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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Amps | Ref. No. | $\underset{\substack{\text { Price } \\ £}}{\substack{\text { en }}}$ | $\begin{gathered} \text { Pust } \\ \mathbf{E} \end{gathered}$ | Amps | Ref. No. | Pribr E | Post <br> cos |
| 0\% | 102 | $2 \cdot 38$ | U.30 | $0 \cdot 3$ | 124 | 2.08 | 0.38 |
| 1 | 103 | 3.00 | 0.38 | 2 | 126 | 2.98 4.68 | 0.38 |
| 2 | 104 | 4.57 | 0.42 | 3 | 125 | 6.84 | 0.62 |
| 2 | 105 | 5.20 | 0.52 | 4 | 123 | 7.94 | 0.67 |
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| Volt: |  | Milliamus |  | Lef. <br> No. | Price : | Pust E |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sec. 1 | See. \% | Sec. 1 | Sec. 2 |  |  |  |
| 3-0-3 | - | 200 | -- | 238 | 1.23 | $0 \cdot 10$ |
| 0-6 | 9-6 | 504 | 500 | 234 | 1.80 | 0.10 |
| 0-6 | (0-6 | 1.000 | 1000 | 212 | 1.88 | 0-22 |
| 9-0-9 |  | 100 | - | 13 | 1.28 | 0.10 |
| 0-9 | 0-4 | 336 | 330 | 235 | 1.48 | $0 \cdot 10$ |
| 0-8-4 | 0-8-9 | 500 | 500 | 207 | 1.75 | 0.22 |
| 0-8-9 | 9-8-9 | 1000 | 1000 | 208 | 280 | 0-30 |
| 15-0-1\% | $\cdots$ | 40 | - | 240 | 1-2t | $0 \cdot 10$ |
| 0-15 | 0-15 | 200 | 200 | 230 | 1.80 | 0-10 |
| 20-0-20 |  | 30 | -- | 241 | 1-28 | 0.10 |
| 0-20 | 0-20 | 150 | 150 | 237 | $1-30$ | 0.10 |
| 0-15-20 | 5-15-2们 | 500 | 500 | 205 | $2 \cdot 47$ | 0.38 |
| 0-20 | (-20 | 300 | 300 | 214 | 1.72 | $0 \cdot 22$ |
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| 20-12-6-12 20 | $\cdots$ | 700 ( | /C) | 221 | 2-31 | $0 \cdot 30$ |
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$$
\begin{aligned}
& \text { MIDGET 220V } 55 \mathrm{~mA}, 68 \mathrm{BA} \\
& \text { EEATER TRAMS. } 6 \cdot 3 \mathrm{~V} \frac{1}{2} \mathrm{gmp}
\end{aligned}
$$

. $.42 \cdot 50$
. .28 .00
. .84 .85

$$
\begin{aligned}
& 8 \text { zmp. } 6,8,10,12,16,18,20,24,80,86,40,48,60 \varepsilon 7 \cdot 50 \\
& 5 \text { amp. } 6,10,12,16,18,20,24,80,86,40,48,60 \\
& 8,5,8,10,13 V 5 \mathrm{amp} .\{1-59 ; 6-0 \cdot 6 V 500 \mathrm{~mA} 90 \mathrm{p}
\end{aligned}
$$ $8,5,8,10,13 V 5 \mathrm{amp}$ ． $21.59 ; 6-0-6 \mathrm{~V} 500 \mathrm{~mA} 90 \mathrm{p}$ 8V 1 amp 95 p 12 V 300 mA 75 p 12 V 500 mA 85 p 12 V 750 mA $95 \mathrm{p} .10,30,40 \mathrm{~V} 2 \mathrm{amp} £ 2.20 \mathrm{~V} 3 \mathrm{amp} 92.40 \mathrm{~V}, 3 \mathrm{~A}, ~ £ 2-50$ ．


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$20 \mathrm{~Hz}-200 \mathrm{kHz}$
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sistor tester －C3025 Deluxe meter i－300mHz
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sistor tester
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one tester
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Marriot XRPS $/ 36 \frac{1}{4}$ Track Med．
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A high stability signal generator using the low distortion Wien bridge principle．Covering 10 Hz to 100 KHz in 4 ranges．Adjustable output from 1 mV to 1 V ．Sine and Square wave output
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Covering 150 KHz to 220 MHz in 8 ranges．Built in AF mod．Output up to 50 mV ．Crystal callbration faci！ities． Large linear scale with slow motion drive．
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 $0-70 \%$
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Measures $1 \mu \mathrm{H}$ to 100 H in 4 ranges $\pm 5:: \geq \approx=-\Xi \Sigma_{s}, Q$ measurement from $0 \cdot 1-1.000 \pm 10 \%$
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[^0]:    Wire Wqund Rasigtors. Our selectlan of thixed values. sh for fif: 50 . 100 for $\pm 4-00$.
    Addio Ampllfier Modula. Multatd. LP11T3, output power. nombilal to vatt sixpply voltage +24 voil, with data and cirestit, $\$ 2.50$
    Ferguson Sterecgram chassis Bhodel 3357 , ail translator, medium long, VHFiFM. a watts per channel $5 / \mathrm{K}$. with connuction data, less tonirg scale, Ezo. Post paid.
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     50p each.
    
    
     $3^{*}<1 " 300_{\mathrm{p}} ; 4 / 0, \mathrm{~F}$ thive an: $1 i^{*} 25 \mathrm{p}$ : 200022000 of $25 \% 2^{\prime \prime} \times 3 * * 35 p: 700,4 F$
    
    
    
    
     4,00\%; ;F 25y $3^{N} \times 1 \frac{1}{3}^{-1} 4 \mathrm{An}$.
    Matehetd pair of bookxholf speakers. Tisnk finlsh, size $12^{*} \cdot \mathrm{a}^{*} \times 5^{*} .8 \times 58^{N}$ ehrmis cerranile, 5 vialls RMS. Complote with dir leacs. \&11.00 pair.
    Thorn TV IF chassis, 950 series (letes valves), ©1-74.
    UHF S25 transistor pusir iufton tuner (NSF Telefunken) is uged on Drake AS24br. Brand neve aind broxed, E3-25. Ligit Dependent Resigtors (RCA
    
    P.F Eparis (not conijuter osnela) 1 all 6 transistor Einade whive band. 1 otl 4 transistor audio. 1 off $\frac{1}{}$ transistor E1-60, thres boards.
    Repanco Trangformers AF 1 , AF 2 , TT45, 46, 47, 49, 53, 55. 20p each.
    LiAh, M,W, VHF Tungr $\$$ transistor In kit form, complete with fulf assembly instructions. svt supply, positive earth. Oiput tonam, Buit-in A.A. aerial. $\mathrm{BE} 5-169 \mathrm{M}$ Mcs. $85 \cdot 75$.
    Sterea Decoder using MCi310. Fully assambied, can ba used with cur twner sit, With date, c4-25,
    Mains Broppers, 10 filxed values, $\mathbf{8} 1-0 \mathrm{o}$.
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[^1]:    The Sinclair Multimeter DM2 is available from retailers or direct from Sinclair Radionics Ltd., London Road, St: Ives, Huntingdonshire PE17 4HJ. Recommended retail prices are as follows :-

    DM2 complete with battery and test leads $\mathbf{8} 59+$ VAT Carrying case $£ 5+$ VAT
    Mains converter £2.95 + VAT.

