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# BRITAN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELEGTRONICS COISTRUCTOR 

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We regret that we are unable to supply back numbers of Practical Wireless. Readers are recommended to enquire at a public library to see copies. Requests for specific back numbers of Practlcal Wireless and Television only can be publlshed in our CQ Column.

\author{

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[^0]

Units listed belo
(a) DISCOMASTER TWIN TURNTABLE CONSOLE wit integral 100 W amplifier (b) PAIR OF HI-FI HEAD. PHONES
(c) MATCHING DYNAMIC
'MIKE' (attached to h'phone)
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## DIODES

OA90, OA91, OA95, 80 each: OA202, 11p. Other semiconductors; AC128, 17p: AF117 34p; BFY51 23p. Full lists and technical data will be found in

## RESISTORS

| Code | Watts | Ohms | 1 to 9 | 10 to 99 | 100 up |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | note be | (0) |
| C | 1/3 | 4.7-470K | 1.3 | $1 \cdot 1$ | 0.9 nett |
| C | 1/2 | 4.7-10M | $1 \cdot 3$ | $1 \cdot 1$ | 0.9 nett |
| C | 3/4 | 4.7-10M | 1.5 | $1 \cdot 2$ | 0.97 nett |
| C | 1 | 4.7-10M | $3 \cdot 2$ | $2 \cdot 5$ | 1-92 nett |
| MO | 1/2 | 10-1M | 4 | $3 \cdot 3$ | $2 \cdot 3$ nett |
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| OAZ 200 | OC 206 |
| OC 22 | SX 754 |
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| 0 O 26 | 2R 21 |
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A.C.S. Dundee.

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## NEW MULLARD \＆MAZDA VALVES

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| DM70 | 0.68 | EF80 |
| :---: | :---: | :---: |
| DYE1 | 085 | EF83 |
| DY88／7 | 042 | EF88 |
| DY802 | 0.45 | EF86 |
| EABC80 | 1.00 | EF89 |
| EB91 | 0.88 | EF91 |
| EBC81 | 0.76 | EFP9 |
| EBF80 | $0-50$ | EF95 |
| EBF83 | 0.89 | EFP183 |
| EBF89 | 0.68 | EF184 |
| EC86 | 0.76 | EH90 |
| EC88 | $0 \cdot 77$ | EL34 |
| HCC81 | 0.45 | EL36 |
| ECC82 | 0.48 | EL81 |
| ECCs | 0.45 | EL84 |
| ECC84 | 0.55 | EL85 |
| ECC8s | 0.59 | ELP8 |
| ECC88 | 0.75 | EL95 |
| ECCl 89 | 0.71 | EL91 |
| ECF80 | 0.50 | ELL80 |
| ECF82 | 0.78 | HM84 |
| ECF86 | 0.71 | EM87 |
| ECH81 | 1.00 | EY51 |
| ECFP3 | 1.00 | EY80／87 |
| ECH84 | 0.78 | EY88 |
| ECL80 | 0.58 | EZ80 |
| ECL82 | 0.81 | E281 |
| ECL83 | 0.68 | GY501 |
| ECL8 6 | 0.88 | GZ34 |


|  | PC86 | 0.75 |
| :---: | :---: | :---: |
|  | PC88 | 0.75 |
| 0.46 | PC97 | 0.45 |
| 1.03 | PC900 | 0.58 |
| 0.43 | PCCA 4 | 0.52 |
| 0.90 | PCC88 | 0.80 |
| 0.81 | PCC89 | 0.65 |
| 130 | PCC189 | 0.65 |
| 1.40 | PCF80 | 0.51 |
| 1.36 | PCF82 | 1.80 |
| 0.60 | PCF86 | 0.65 |
| 0.60 | PCF200 | 0.85 |
| 0.56 | PCF201 | 0.87 |
| 0.95 | PCF601 | 0.65 |
| 1.05 | PCF802 | 0.71 |
| 0.90 | PCF806 | 0.66 |
| 0.47 | PCH200 | 0.88 |
| $0 \cdot 55$ | PCL82 | 0.54 |
| 0.95 | PCL83 | 0.86 |
| 0.70 | PCL84 | 0.59 |
| 1.81 | PCLAS | 0.82 |
| 1.30 | PCL86 | 0.83 |
| 1.18 | PCL805／8 | 5 |
| 1－18 |  | 0.68 |
| $0-88$ | PD500 | 1.55 |
| 0.42 | PFL200 | 0.80 |
| 0.64 | PL36 | 0.88 |
| 0.61 | PL81 | 0.75 |
| 0.40 | PL81A | 0.88 |
| 0.90 | PL82 | 0.50 |
| 0.78 | PL83 | 0.08 |


| PL84 | 0.68 |
| :---: | :---: |
| PLS04 | 0.88 |
| PL508 | 1.05 |
| PL509 | 1.55 |
| PL802 | 0.98 |
| PY33 | 0.66 |
| PY81／800 | 0.50 |
| PY82 | 0.55 |
| PY88． | 0.60 |
| PY500A | 1.05 |
| PY800 | 0.60 |
| PY801 | 0.50 |
| U26 | 1.00 |
| U191 | 1.00 |
| U193 | 0.50 |
| UABC80 | 0.90 |
| UBC81 | 0.70 |
| UBF89 | 0.60 |
| UCC85 | 0.60 |
| UCH81 | 1.00 |
| UCL82 | 0.70 |
| UCL83 | 0.70 |
| UF89 | $0-80$ |
| UT．84 | 0.85 |
| UY85 | 0.50 |
| 6／30L2 |  |
| ECC804 | 1.00 |
| 6F23／EF812 <br> $30 \mathrm{CL} / \mathrm{PCF} 80$ <br> 1.05 <br> 0.61 |  |
|  |  |
|  |  |
|  |  |



## NEW VALVES

Individually boxed and guaranteed but of Euro－ pean or other origin at greatly reduced prices． Quotations for any valve not listed．Send SAE for lists．

|  |  |  |  |  |  | AP41 | 8.00 | ${ }^{6 J 6}$ | 0.30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | SP61 | 0.76 | 6．57M | $0 \cdot 45$ |
| Individually boxed and |  |  |  |  |  | T41 | 1.60 0.75 | 6.76 6K6GT | 0.40 0.75 |
|  |  |  |  |  |  | U25 | 0.75 0.85 | $\begin{aligned} & 6 \mathrm{~K} 6 \mathrm{GT} \\ & 6 \mathrm{~K} 7 \mathrm{M} \end{aligned}$ | 0.75 0.45 |
| guaranteed but of Euro－ |  |  |  |  |  | U26 U191 | 0.85 0.75 | 6K7G | 0.85 0.70 |
| pean or other origin at |  |  |  |  |  | UABCB0 | 0.40 | 6K8G | 0.70 0.45 |
|  |  |  |  |  |  | UAF49 | 0.78 | 6K25 | 1.00 |
| greatly reduced prices． |  |  |  |  |  | UBCA1 | 0.75 0.45 | ${ }^{6 L 69}$ | 0.56 0.50 |
| Quotations tor any |  |  |  |  |  | UBF80 | 0.40 | 6Q7a | 0.60 |
|  |  |  |  |  |  | UBF89 | 0.40 | 6SL7GT | 0.48 |
| valve not Iisted．Send |  |  |  |  |  | UCC65 | 0.46 | 68N7GT | 0.48 0.60 |
| SAE for lists． |  |  |  |  |  | CCH81 | 0.40 | 6UEG | 0.76 |
|  |  |  |  |  |  | UCL82 | 0.85 | 0V8G | $0 \cdot 40$ |
|  |  |  |  |  |  | UCL83 | 0.70 | 6V6GT | 0.50 |
| AZ1 | 0.60 | EF80 | 0.96 | PC86 | 0.60 | UF41 | 0.75 | 6X4 | 0.40 |
| AZ3I | 0.56 | EF85 | 0.85 | PC88 | 0.80 | UF89 | 0.40 | 6X5G | 0.45 |
| CBL31 | 180 | EF86 | 0.80 | PC97 | 0.50 | UL4l | 0.85 | 6X5GT | 0.46 |
| CL33 | 1.50 | EF89 | 0.88 | PC900 | 0.48 | UL84 | 0.48 | 7B6 | 0.75 |
| CY91 | 0.50 | EF91 | 0.87 | PCC84 | 0.30 | UY41 | 0.48 | 787 | $0 \cdot 70$ |
| DAF91 | 0.80 | EF92 | 0.50 | PCC88 | 0.55 | TY85 | 0.40 | 7 C 5 | 1.80 |
| DAF96 | 0.60 | EF95 | 0.40 | PCC89 | 0.50 | V R 105－30 | 0.40 | 7 CB | 0.76 |
| DCC90 | 1.85 | EF98 | 0.75 | PCCl89 | 0.60 | VR150－30 | 0.40 | ${ }^{7} \mathrm{H7}$ | $0 \cdot 70$ |
| DF91． | 0.80 | EF183 | 0.80 | PCF80 | 0.40 | OA2 | 0.40 | 7R7 | 0.75 |
| DF96 | 0.50 | HF184 | 0.85 | PCF82 | 0.85 | OB2 | 0.40 | 787 | 8． 25 |
| DK91 | 0.45 | EL32 | 0.60 | PCF86 | 0.60 | 1R5 | 0.45 | 7Y4＇ | 0.76 |
| DK92 | 0.70 | ELas | 1.75 | PCF801 | 0.60 | 186 | 0.80 | 12AT6 | 0.40 |
| ${ }_{\text {DLP }}{ }_{\text {DK }}$ | 0.60 | $\underset{\text { EL3 }}{\text { EL }}$ | 0.60 0.50 | ${ }_{\text {PCFP802 }}$ | 0.50 | 174 | 0.80 | 12AT7 | 0.40 |
| DLP4 | 0.88 | EL37 | 2.50 | PCF806 | 0.75 | 3 V 4 | 0.40 0.70 | 12AU6 | 0.45 |
| DL98 | 0.55 | EL41 | 0.80 | PCF808 | 0.90 | 6R4GY | 0.80 | 12AX7 | 0.88 |
| DY86／7 | 0.36 | EL42 | 0.90 | PCL82 | 0.85 | 5 C 40 | 0.40 | 12BA6 | 0.45 |
| DY802 | 0.87 | EL84 | 0.28 | PCL83 | $0 \cdot 68$ | 5V49 | 0.60 | 12BE6 | 0.50 |
| EABC80 | 0.88 | EL． 95 | 0.40 | PCL84 | 0.45 | SY3GT | 0.45 | 30 CI | 0.40 |
| EAF42 | 0.76 | ELL80 | 1.95 | PCL8s | 0.60 | SZ4G | 0.45 | 30 Cl 5 | 1.05 |
| EB91 | 0.88 | EM80 | 0.45 | PCL86 | 0.45 | 6／30L2 | 0.90 | 30 Cl 7 | 1.10 |
| Ebrcas | 1.00 | EM81 | 0.60 | PCL805／85 |  | 6AKJ | 0.50 | 30 Cl 8 | 0.80 |
| EBC41 | 0.75 | EM84 | 0.85 |  | 0.60 | 6AM5 | 1.00 | 30F5 | $1 \cdot 10$ |
| EBC81 | 0.35 | EM85 | 1.00 | PD500 | 1.80 | －AQb | 0.45 | 30FL1 | 0.80 |
| EbF80 | 0.40 | EYSI | 0.40 | PEN45 | 0.75 | 6AB7G | 0.85 | 80FL2 | 0.75 |
| EBF83 | 0.40 | EY86 | 0.40 | PL36 | 0.63 | 6AT6 | 0.45 | 30FL14 | 0.80 |
| EBF89 | 0.88 | EZ40 | 0.75 | PL81 | 0.50 | 6AU6 | 0.80 | 30L15 | 1.05 |
| EBLa 31 | 1.50 | ER41 | 0.75 | PL82 | 0.45 | 6BA6 | 0.28 | 30 LIT |  |
| FCC81 | 0.40 | EZ80 | 0.88 | PL83 | 0.45 | 6BE6 | 0.85 | 30P4MR | 1.85 1.80 |
| ECC82 | 0.88 | EZ81 | 0.89 | PL84 | 0.40 | 6BH6 | 0.75 | 30P4MR | 1.60 1.05 |
| ECC83 | 0.88 | GY501 | 0.90 | PL500 | 0.80 | 8BJ6 | 0.55 | $30 \mathrm{P12}$ | 1.05 |
| ECC84 | 0.80 | GZ80 | 0.45 | PL504 | 0.80 | 6BQ7A | 0.55 | $30 \mathrm{P19}$ | 1.00 |
| ECC85 | 0.40 | GZ32 | 0.60 | PL508 | 0.90 | 6BR7 | 1.00 | 30PL1 | 0.85 |
| ECC88 | 0.40 1.85 | GZ34 GZ37 | 0.65 1.95 | PL509 | 1.55 0.95 | 6887 | 1.85 | 30PL13 | 1.20 |
| ECH42 | 1.00 | HN309 | 1.60 | PX4 | 8.50 | ${ }_{6}^{6 B W 6}$ | 0.80 0.90 | 30PL14 | 1.25 |
| ECE81 | $0 \cdot 80$ | KT61 | $1 \cdot 75$ | PX25 | 3.50 | 6C4 | 0.65 | 35w4 | 0.50 |
| ECH83 | 0.45 | KT66 | 2.50 | PY33 | 0.68 | 60D5 ${ }^{\text {d }}$ | 1.80 | 35Z4GT | 0.70 |
| ECL80 | 0.55 | KT81 ${ }^{(71}$ |  | PY8I | 0.50 | $6 \mathrm{CH6}$ | 1.40 | 50CD6G | 1.80 |
| ECL82 | 0.35 |  | 1.30 | PY82 | 0.85 | ${ }^{60} 4$ | 1.00 | 807 | 0.50 |
| ECL83 | 0.70 0.40 | $\mathrm{KT}^{\mathbf{K} \mathrm{K}^{1} 8}$ | 1.75 8.90 | PY83 PY88 PY809 | 0.88 0.40 | ${ }_{6}^{6 F 23}$ | 1.05 1.00 | 813 ITT | 1.50 813 |
| ECLL800 | 8.20 | KTW6I | 1.00 | PY500 | 1.05 | 6 F 28 | 0.70 | 813 UBST |  |
| EF37A | 1.20 | MU14 | 1.00 | PY81／800 | 0.50 | 6．J5M | 0.85 |  | 5．75 |
| EF39 | 1.20 | N78 | $2 \cdot 75$ | PY801 | 050 | 6J59 | 0.45 | 866A | 1.00 |

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\section*{AA119 0．7 BD132 |  | 0.7 |  |  |
| :--- | :--- | :--- | :--- |
| AAZ13 | 0.10 | BD132 | 0.50 |
|  | BF115 | 0.22 |  | | AAZ15 | 0.10 | BF115 | 0.22 |
| :--- | :--- | :--- | :--- |
| AC107 | 0.35 | BF167 | 0.25 |
| BF173 | 0.28 |  |  | | AA2107 | 0.35 | BF173 | 0.28 |
| :--- | :--- | :--- | :--- |
| AC128 | 0.25 | BF179 | 0.38 |
| AC126 | 0.25 | BF180 | 0.35 |
| AC127 | 0.20 | BF181 | 0.35 |
| AC128 | 0.25 | BF194 | 0.18 |
| AC176 | 0.25 | BF194 | 0.13 | AC18 ACl 88

ACY 2
ACY 3 <br> 际合 <br> $\mathrm{AD14}$
$\mathrm{AD16}$

$\mathrm{AD16}$ <br> \[
$$
\begin{aligned}
& \text { AFl1 } \\
& \text { AFl1 } \\
& \text { AFII }
\end{aligned}
$$

\] <br> \[

$$
\begin{aligned}
& 4 \text { All } \\
& \text { AFII } \\
& \text { AFI86 }
\end{aligned}
$$

\] <br> \[

$$
\begin{aligned}
& \text { AF18 } \\
& \text { AF23! } \\
& \text { ASY2 }
\end{aligned}
$$
\] <br> ABY2

ABY2 $B_{A}$
$B_{A} 11$

$B_{C l}$ <br> $\qquad$ <br> BC10 <br> |  | 0.21 | CRSA |  |
| :--- | :--- | :--- | :--- |
| BC14 | 0.40 |  |  |
| BC14 | 0.30 | MJE340 | 0.50 |
|  | 0.12 | MJE370 | 0.68 | <br>  <br> |  | BC184L | 0.12 | MPF102 |
| :--- | :--- | :--- | :--- |
| BCY | 0.76 |  |  |
| BCY32 | 1.80 | MPF103 | 0.88 | <br> | BCY32 | 1.80 | MPF104 |
| :--- | :--- | :--- |
| BCY33 | 0.88 | MPF105 |
| BCY34 | 0.45 | NKT404 | <br> 品 | BCY71 | 0.16 | 0.20 | OA10 |
| :--- | :--- | :--- | :--- |
| BCY72 | 0.16 | 0. |  |
| BCZ11 | 0.85 | 0.40 | 0.10 | <br> | BD121 | 0.85 | OABI | 0.10 |
| :--- | :--- | :--- | :--- |
| BD124 | 0.50 | OA91 | 07 |
| BD131 | 0.45 | OA202 | 0.08 |
|  | 0.10 |  |  |}

All transistors，I．C＇s offered are new and branded． Manufactured by Mul． lard，Texas，RCA，Fer－ ranti，Motorola，ITT， Fairchild，Lucas，etc． Quantity discounts on application．Send SAE for full lists．

| SN7400 | 0.28 | 8N7425 | 0.87 | BN7473 | 0.45 | SN74107 0.51 | 6N74167 | 1.09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SN7401 | 0.20 | GN7427 | 0.37 | SN7474 | 0.48 | ON74110 0.57 | EN74170 | 8.88 |
| BN7402 | 0.20 | BN7428 | 0.48 | BN7476 | 0.59 | SN74111 0.86 | EN74174 | 1.80 |
| BN7403 | 0.80 | －8N7430 | $0 \cdot 20$ | BN7476 | 0.45 | EN7418 1.00 | GN74175 | 1.2 |
| BN7404 | 0.80 | －EN7432 | 087 | EN7480 | 0.80 | 6N74119 1－92 | SN74176 | 1.44 |
| EN7405 | 0.80 | BN7433 | 0.43 | EN7482 | 0.87 | $\begin{array}{ll}\text { EN74121 } & 0.67\end{array}$ | EN74190 | 2.30 |
| BN7408 | 0.40 | BN7437 | 0.48 | BN7483 | 1.20 | SN74122 0.80 | EN74191 | 2.80 |
| gN7407 | 0.40 | GN7138 | 0.48 | 6N7484 | 1.00 | SN74128 1.44 | EN74192 | 2.8 |
| 8N7408 | 0.25 | EN7440 | 0.80 | 6N7486 | 0.60 | SN74141 1.00 | BN74193 | $2 \cdot 80$ |
| EN7409 | 0.38 | 8N7441A |  | 8N7490 | 0.75 | BN74145 1.44 | BN74194 | 1.72 |
| CN7410 | 080 |  | 0.85 | BN7491AN |  | BN74180 2.80 | BN74108 | 1.44 |
| EN7411 | 0.83 | 8N7442 | 0.85 |  | $1 \cdot 10$ | SN74151 1.15 | SN74190＇ | 1.58 |
| BN7412 | 0.88 | 6N7450 | 0.80 | 6N7492 | 075 | BN74154 2.80 | BN74197 | 1．58 |
| EN7413 | 0.30 | 6N7451 | 0.20 | GN7493 | 0.76 | $\begin{array}{ll}\text { SN74155 } & 1.15\end{array}$ | BN74198 | 3.16 |
| BN7416 | 0.30 | 6N7453 | 0.20 | 6N7494 | 0.85 | $\begin{array}{ll}\text { SN74156 } & 1.15\end{array}$ | 8N74198 | 8.88 |
| 6N7417 | 0.80 0.80 | BN7454 BN7460 | 0.20 0.20 | BN7498 | 0．88 |  |  |  |
| －8N7420 | 0.20 0.28 | BN7460 SN7470 | 0.20 0.33 | BN7496 BN7497 | ＋1．09 |  |  |  |
| SN7423 | 0.40 | 8N7472 | 0．38 | 8N74100 | 2－16 | SOCKET | 16 pin | $7 p$ |

$$
\begin{aligned}
& \text { VAT } \\
& \text { 10\% to be } \\
& \text { added to } \\
& \text { all orders } \\
& \text { including }
\end{aligned}
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For the man who wants to design his own stereo - here's your chance to start, with Unisound - pre-amp, power amplifier and control panel. No soldering just simply screw together, 4 watts per channel into 8 ohms. Inputs: 120 mV (for ceramic cartridge). The heart of Unisound is high efficiency I.C. monolithic power chips which ensure very low distortion over the audio spectrum.


Elegant self selector push button player for use with your stereo system. Compatible with Viscount III system, Unisound module and the Stereo 21 Technical specification Mains innput. 240V. Output sensitivity 125 mV Comparable unit sold eleswhere at £24.00 approx. Yours for only
$\mathrm{f} 10.95+90 \mathrm{p}$ \& p

## COMPLETE* STEREO SYSTEM

## System1. $£ 51 \cdot 00$ <br> 40 Watt Amplifier. Viscount III - R102 now 20 watts per channel.

System I includes:
Viscount Ill amplifier-volume, bass, treble and balance controls, plus switches for mono/ steres on/off function and bass and treble filters. Plus headphone socket.
Specification
20 watts per channel into 8 ohms. Total distortion @ 10W @ $1 \mathrm{kHz} 0 \cdot 1 \%$. P.U. 1 (for ceramic cartridges) 150 mV into 3 Meg. P.U. 2 (for magnetic cartridges) 4 mV a 1 kHz into 47 K . equalised within $\perp 1$ IB R.I.A.A. Radio 150 mV into 220 K . (Sensitivities given at full power). Tape out
facilities: headphone socket, power out $250 \mathrm{~m} \mid \mathrm{W}$ per channel. Tone controls and filter
characteristics. Bass: +12 dB to -17 dB a 60 Hz . Bass filter: 6 dB per octave cut. Treble control treble +12 dB to -12 dB a 15 kHz . Treble filter: 12 dB per octave. Signa/ to noise ratio: (all controls at max.) - 58 dB . Crosstalk better than 35 dB on all inputs. Overload characteristics better than 26 dB on all inputs. Size approx. $13 \frac{33^{\prime \prime}}{} \times 9^{\prime \prime} \times 3 \frac{3^{\prime \prime}}{4}$.
Garrard SP 25 Mk III deck with magnetic cartridge. de luxe plinth and hinged cover
Two Duo Type II matched speakers - Enclosure size approx. $17 \frac{11^{\prime \prime}}{} \times 10^{\frac{3}{4}}{ }^{\prime \prime} \times 6^{\prime \prime}$
in simulated teak. Drive unit $13^{\prime \prime} \times 8^{\prime \prime}$ with parasitic tweeter. 10 watts handling.
Complete System $\mathbf{f 5 1} 00$

## System 2. $£ 60 \cdot 00$

Viscount III amplifier (As System)
Garrard SP 25 Mk III deck (As System I)
Two Duo Type IIIA matched speakers - Enclosure size approx. $31^{\prime \prime} \times 13^{\prime \prime} \times 11 \frac{11^{\prime \prime}}{}$
 20 watts, 8 ohms. Freq. range 20 Hz to 20 kHz .

## Complete System $£ 69 \cdot 00$

PRICES: SYSTEM 1
Viscount III R102

| amplifier | $£ 24.20+£ 1 p \& p$ |
| :--- | :--- |

2 Duo Type ll speakers $£ 14.00+£ 2.20$ p\&p
Garrard SP 25 with
Mag. cartridge
de luxe plinth
and hinged cover $\quad \mathbf{f} 21.00+\mathrm{f} 1.75 \mathrm{p}$ \& p
total: $\mathbf{£ 5 9 . 2 0}$
Available complete for only:
£51.00
$+\mathbf{E 3 . 5 0 p \& p}$

## PRICES: SYSTEM 2

Viscount III R102
amplifier
$\mathbf{f} 24.20+\mathfrak{f 1} \mathrm{p} \& \mathrm{p}$
2 Duo Type III A speakers $£ 39.00+£ 4.00$ p \& p
Gerrard SP 25 with
Mag. cartridge
de luxe plinth
and hinged cover
$\mathrm{f} 21.00+\mathrm{f} 1.75 \mathrm{p} \& \mathrm{p}$
total: $£ 84,20$
Available complete for only:
£69.00
$+\mathbf{£ 4 . 0 0} \mathbf{p} \mathbf{f} \mathbf{p}$

## EMI SPEAKERS AT FANTASTIC REDUCTIONS



## 20 WATT SPEAKER SYSTEM

System consists of a $13^{\prime \prime} \times 8^{\prime \prime}$ (approx) eliptical woofer unit with a $8^{\prime \prime} \times 5^{\prime \prime}$ (approx.) mid range unit incorporating parasitic tweeter and crossover components.
Technical Specification:
Bass Unit
Flux density-100 K, speech coil-1嘸", Cone, Triple laminated paper with P.V.C. surround.

Mid Range Unit
Flux density-33K, speech coil-1" with parasitic tweeter.
Power Handling
20 watts R.M.S., impedance -8 ohms, frequency response -20 Hz to $18,000 \mathrm{~Hz}$.
OUR PRICE
£6.60. Complete
$+90 \mathrm{p} \boldsymbol{\mathrm { G }} \mathrm{p}$.


15" 14A/780 BASS UNIT
Bass unit on a rigid diecast chassis. Superior cone material handles up to 50 watts RMS, and is treated to give a smonth frequency response. Resonance 30 Hz . flux density 360,000 Maxwells. Impedance at 1 kHz is 8 ohms . $3^{\prime \prime}$ voice coil.
Recommended retail price $\mathbf{£ 4 0} 80$.
OUR PRICE $£ 18.70+£ 1.50$ p\&p


Five matched speakers and crossover unit for handling up to 45 watts, frequency response from 20 to $20,000 \mathrm{~Hz}$. Huge 19" $\times 14^{\prime \prime}$ (approx.) high efficiency Bass-Speaker with 16.500 -gauss magnet buitt on a heavy diecast frame.
The four 10.000 gauss tweeters, each $3 \frac{1}{4}$ " dia. ap prox. are fed by the crossover which critically adjusts signal for maximum fidelity. Impedance at 1 kHz is 8 ohms Bass coil 2", others 0.5"
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## PORTABLE DISCO CONSOLE

INCORPORA TES $*$ Pre-Amp with full mixìing facilities, including switched input for mic with volume control, switched input for auxiliary with volume control, bass and treble controls, volume control and blend control for turntables.
Two $\mathrm{B}_{\mathrm{S}} \mathrm{S}_{8}$ single play professional series decks, fitted with ceramic cartrídges and diamond styll.
The turntables are designed and precision engineered They combine clean modern styling with superb reproduction. Their many special features include square section aluminium tonearms, (high precision low mass design fully counterbalanced, with calibrated stylus pressure control for perfect tracking), and conveniently grouped easy to read linear controls. The turntables have viscous cueing devices which allows the tonearms to be placed or lifted at any point on the record.
The two lightweight cartridge shells have slide-ïn-holders to facilitate easy inspection of needles and cartridges.

technical specification:
Pre-amp - Output -200 mV . Auxiliary inputs -200 mV and 750 mV into 1 meg. Mic input-6mV into 100 K. 240 volt operation Turntables capacity $-7^{\prime \prime}, 10^{\prime \prime}$ or $12^{\prime \prime}$ records.
Rumble, wow and flutter - Rumble - Better than - 35dB. Wow - Better than $0.2 \%$. Flutter - Better than 0.06\% (Gaumont kalee meter).
Finish - Satin black mainplate with black turntable mat inlaid with brushed aluminium trim. Tonearm and controls in black and brushed aluminium.

Console size - Unit Closed - $17 \frac{3}{4}^{\prime \prime} \times 13 \frac{3}{4}^{\prime \prime} \times 8 \frac{3^{\prime \prime}}{}$ (approx)
Unit Open $-35 \frac{33^{\prime \prime}}{4} \times 13 \frac{33^{\prime \prime}}{4} \times 4 \frac{1}{\frac{1}{2}^{\prime \prime}}($ approx $)$
This disco console is ideally matched for the Reliant IV and Disco 50 or any other quality amplifier.
The unit is finished in black PVC with contrasting simulated teak edging diamond spun control knobs with matching control panel.
Yours for only $£ \mathbf{~} 39.00+£ \mathbf{~} \mathbf{5 0} \mathbf{~ P}$. \& $\mathbf{P}$.

DISC050


45 WATT R.M.S. MONO DISCOTHEQUE AMPLIFIER Ideal for Disco Work. Output Power: 45 watts R.M.S. Frequency Response 3 dB points 30 Hz and 18 KHz . Total Distortion: less than $2 \%$ at rated output. Signal to noise ratio: better than 60 dB . Bass Control Range: 13 dB at 60 Hz . Treble Control Range: 12 dB at 10 KHz . Inputs: 4 inputs at 5 mV into 470 K . Each pair of inputs controlled by separate volume control. 2 inputs at 200 mV into 470 K , Size: $19 \frac{1}{4} \times 10^{\prime \prime} \times 8^{\prime \prime}$ (approx.) Amplifier $\mathbf{£ 2 7 . 5 0}+\mathbf{£ 1 . 5 0} \mathbf{p}$. \& p

Special Offer: Disco 50 plus two 15" E.M.I. speakers type 14A/780 (as illustrated on previous page) Complete $£ 55.00+\mathbf{E 4 . 0 0} \mathbf{p} \& \mathrm{p}$.


Reliant Mk IV Mono Amplifier, ideal for the small disco or house parties. Outputs 20 watts R.M. S. into 8 ohms (suitable for 15 ohms). Inputs *4 electrically mixed inputs. *3 individual mixing controls.
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A parce of integrated circuits made by the famous Piessey Company. A in-a-lifetime offer of Micro-electronic devices well below cost of manufactare The parcel contains 5 ICs all new and periect, first-grade device, defmitely not sub standard or seconds. 4 of the ICs are single silicon chip GP amplimers Full circuit details of the ICs are included and in addition you will receive a lis of many different ICs available at bargain prices 250 upwards with eircuits an technical data of each. Complete parcel only 81 post paid
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## MULLARD UNILEX STEREO SYSTEM

 There is no doubt that it is a good system, we believe that for the money strate gladly at our Tamworth Road depot. Prices of the individual items for this:-$\begin{array}{lll}1 \text { Unilex Amplifier } & \text { Ref. EP. } 9000 & \text { E1. } 60 \\ 1 \text { Unilex Pre-Anp } & \text { Ref. EP. } 9001 & 81.80\end{array}$ 1. Unilex Power Unit Ref. EP. 9002 \&2.80

1 Control panel kit with spun aluminium
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## 

DISTRIBUTION PANELS
Just what you need for work bench or lab.
$4 \times 13 \mathrm{amp}$ sockets in metal box to take



## SHORTWAVE CRYSTAL SET

Although this uses no battery it gives really amazing results. You will 1 wrt.
Kit contains chassis front panel and all the parts. $£ 1 \cdot 25$-crystal earphone $\mathbf{3 3 p}$.

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HORSTMANN "TIME AND SET"' SWITCH
A 30 amp Switch). Just the thing if you want to come home to a warm house without it costing you a fortune. You cart helay the switch on time of your electric fires, etc., up to 14 hours from setting time or you can use the switch to give a boost on period of up to 3 hours. Equally suitable to control processing. Regular price probe
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Light switch kit with this, $51 \cdot 78$
Light Switch
The above kit made up ready to work and tested, £2-95.

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Six speeds are available 500, 850 and 1,100 r.p.m. and $8,000,12,000$ \& 15,500 r.p.m. Shaft is $t$ in. diameter and approximately 1 im long. $230 / 240 \mathrm{v}$. Its speed may be further controlled with the use of our Thryrister controller. Very powerful and useful motor size Price 979 plus 23p postage and


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 All in module form, each ready built complete With heat sinks andconnection tags, data connection tags, data
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SPIT MOTOR
200-250v induction motor,

driving a Carter gearbox with a $1 \frac{1}{2}$ " output drive shaft running at 5 revs p.m. Intended for roasting chickens, also for driving
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For digital instruments, counters, timer clocks, etc. Hi-vac XN.3. Price 90p each 10 for $x 9$.

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STC seaLed relays. Makers type rei. 6945. Th se ate metai oncased plug in with two pairs changeover consauts. Approx. size $11^{\prime \prime}$ high $\times 1^{\prime \prime} \times \frac{1}{\prime \prime}^{\prime \prime}$.
We understand these are vacrumt sealed. Two We understand these are vachume sealed. Two
types availani. $6 y$ (45 ohms coll price $£ 1 \cdot 50$; 24 y types availahl 6 y (45 ohm
(700 ohms coil) price $£ 1.75$.
STC sealed relay. Again, type 6945, sealed metal STC sealed relay. Again, type
cas plug in but for 12 v operation ( 170 ohms coil) and with 2 pairs normal open contacts. $21 \cdot 25$.

## WALL THERMOSTATS

Wall mounting and in a handsome plastic casp.
(Cream and beige). Adjustable by slider (lockable) (Cream and beige). Adjustable by slider (lockable) and may be set to control temperatu panel is engraved and indicates (frost twarm) (very warm), etc. The thermostat will control heaters, etc., up to 15 amp it normal mains voltage and is ideal f
living room bedroom and greenhous etc. Price $\mathbf{8 1} \cdot 65$. Don't miss this.

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Also makes good car emergency light. Thu $14-$ - .
standard 2 foot 20 watt tube and operates froiri a 12v. car battery drawing approx. 1A. This gives illumination per amp/hour of battery life far is rycess to filament lamps and in fact to the minialure 8-13 watt camping lights often offered. Complete unit ready to operate, in strong white cnamelled metal frame. These would normally selfer these at $\mathbf{f 4} 50$ plus 40 p post and packing.

## WINDSCREEN

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## CONTROL

Wary speed of your Wiper to sult con-
ditions. All parts and instructions to


## 6 DIGIT COUNTER

 Resettable. 440 ohm coil up to 25 impulses per second. Ex-equipment, but guperfect, $£ 2 \cdot 20$ each.
4 digit counter as
4 digit counter as specified for


## PRESSURE SWITCH

## Containing a 15 amp. change ove

switch operated by a diaphragn,
which in turn is operated by air pressure through a small metal tube. The operating pressure is adjustable
but is set to operate in approx. 10 in .
of water. These are quite low pressure devices and can in fact be operated simply by blowing finto the inlet tube. Original use was for washing :rachines to turn off water when tub has reached rorrect level but no doubt has many other

$$
\text { Atplimfinns } 8138 \text {, each. }
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12 VOLT It AMP POWER PACK
This comprises doublewound $230 / 240 \mathrm{~V}$ mains
transformer with full wave rectifier and $2000 \mathrm{~m} / \mathrm{f} / \mathrm{d} /$ smoothing. Price $\mathbf{2 2} 20+$
Heavy Duty Mains Power Pack Output voltage adjustable froni $15-40 \mathrm{~V}$ in steps maximum load 250 W - that is from 6 amp at 40 V to 15 amp at 15 V . This really is a high power heavy duity
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change push on leads. Silicon rectifiers and smoothing by $3,000 \mathrm{mF}$. Price $\mathbf{5 6 . 3 8}$ plus 65 p post.

A$S$ we promised a few months ago we are publishing for the first time the P.W. Buyers' Guide to Radio and Electronic Components. This has resulted from the years of experience we have of the several problems that we hear about from you, the readers.

Components form the basic requirements to building up a project and it can be argued that Practical Wireless is probably more involved in the problems of electronic component demand and supply than any other magazine of its kind. It is fitting therefore that we should launch this Buyers' Guide. It has not been possible to deal with every detail in the limited space available and certainly does not pretend to satisfy every reader's requirements. What we do aim to provide is a ready reference to component symbols used in circuit diagrams and a directory of those suppliers in the retail trade who have responded to our request for information on their trading policies and product lines. We are also pleased to welcome the assistance provided by these component suppliers who have taken space for their own personal announcements.

The fact that the response was at least up to our expectations confirms the value of such a service to the readership. We hope you will find something useful in this for your own personal needs.

We must point out that, in order to give this exercise the treatment it requires, it has been necessary to divide the Guide into sections. We do appreciate the problem that this may present to a few readers, but it would otherwise have been necessary to make it a separate book for which there would have been an additional charge. To offset this fact we have presented more than half of the Guide as extra pages, specially printed and added to the normal magazine this month; the remainder is included in the next three issues. We can now offer all this information in a form exclusive to $P . W$. readers at no extra cost to you. If you find, when you have the complete guide, that there are other aspects that you would like to have seen, related to buying components, then drop us a line and tell us.

For those readers, and that must be everyone, who are still looking for interesting projects to read about or make up, stay with us because we have more superb designs coming. This month we present a top rated project to beat other designs-an f.m. tuner. The designers said that they developed this because there were no other published do-it-yourself f.m. tuner designs that they felt were good enough. And that is certainly one way of looking at it. See us at the Audio Fair!

[^1]P.O. get PCM gear

MARCONI Communication Systems, a GEC-Marconi Electronics company, has received its largest single order for PCM equipment from the British Post Office, valued at ${£ 11_{2}}_{\mathbf{1}}$ million.

This follows a contract from the Post Office last October for $£ 1^{11_{4}}$ million worth of similar equipment and brings total PCM sales to the Post Office to $£ 141_{2}$ million.

Most of the 24 channel equipment in the latest contract is destined for the London Telecommunications Region, but some will be used in the Eastern Region and Scotland. Delivery will be in two phases during the first half of 1975.

Pulse code modulation was developed specifically as a method of increasing the capacity of existing cables. Its use makes it possible to increase the number of telephone circuits by up to 12 on a single pair of wires.

PCM has obvious advantages in built up areas as an alternative to expensive and inconvenient cable laying. It has also been proved effective in rural areas where demand for telephones and pressure on the system has increased over the past few years.

## University of Durham Radio Society

IT is proposed to start a Univer. sity Radio Society, and the callsign of G4DUR has been provisionally reserved. Anyone interested please contact Peter Whittle (G4BBU), 1 Blinco Rd., Urmston, Manchester, M31 1NF, or during term c/o St. Chad's College, South Bailey, Durham.

## "Cheesed off"

Wo Dutchmen - one in $\begin{aligned} & \text { Nijmegen, the other in } \\ & \text { Wageningen - threw their }\end{aligned}$ TV sets out of the window as the final whistle of the World Cup between Holland and West Germany blew!

# NEWS... 

Listeners please note

MALCOLM CONNAH as most of you are probably aware will not be writing the Broadcast Bands article and Simon David has ceased to write the VHF Column.
It would be appreciated however, if you have any logs for either of these two features, you send them to the Editor, Editorial offices, Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.

## Motorola FETS

L
ATEST discrete components to come from Motorola are two new dual gate FETs offering a common source power gain of $10 \mathrm{~dB}(\mathrm{~min})$ and a noise figure of 6 dB (max) at 500 MHz .

Manufactured using a silicon nitride passivation process for excellent long-term stability, the devices feature a low reverse transfer capacitance (Crss $=$ 0.03 pF max) and have built-in input protection zener diodes.

Designated types 3N209 (TO 72 package) and 3N210 (Micro-H package), the FETs are designed for a maximum drain-source voltage of 25 V and a maximum power dissipation of 300 mW (3N209 derated $1 \cdot 7 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$ ) and 350 mW ( 3 N 310 derated at $2.8 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$ ).

## TYne/Wear Local Radio

THE first Independent Local Radio station in NorthEast England, Metropolitan Broadcasting, began programmes on Monday, July 15 using the new sound radio transmitters of the I.B.A. This is the first station providing listeners in the NorthEast with stereo broadcasting.

The predicted v.h.f. service area includes Newcastle upon Tyne, Ashington, Bedlington, Sunderland, Blaydon, South Shields, Tynemouth, Morpeth, Washington, Blyth, Gateshead, Durham, Houghton-le-Spring, Stanley, Chester-le-Street, Jarrow, Hebburn, Wallsend, Longbenton and Gosforth and extends to parts of Bishop Auckland, Consett, Seaham, Spennymoor and Corbridge.

## Decca and KW

FOLLOWING their recent acquisition of KW Communications Ltd. of Dartford, Decca have formed a new firm called Decca Communications Ltd.

KW Communications-formerly KW Electronics, formed in 1955 , specialised in amateur radio gear. In recent years however, their interests have been diversified to include professional radio communications, especially mobile and point-to-point h.f. ssb systems.

The Decca policy for the new company is to develop and expand these activities.

Decca Communications Ltd., which took part in the recent Brighton Communications Exhibition, markets its products under the Decca name. Amateur radio equipment will be sold under the KW trade mark. In addition, certain equipment is being supplied to other manufacturers under contract.

## John Carter presents . . -

IN the April issue of Practical Wireless, we mentioned a Collectors' Bazaar at Alexandra Palace, Wood Green, London, N. 22 where one could buy anything from a vintage phonograph to a Victorian bottle.
Well, that one was very successful so the promoter, John Carter will be organising another one for Sunday October 20th. Once again it will be a five-bazaar event and John promises us that "Going Back" enthusiasts will probably be able to pick up quite a few bargains. There will be quite a number of stalls devoted to vintage records and radio gear.

If you want to know more about the bazaar or even want to hire a stall and sell some of your own goods, send a stamped, addressed envelope to: John Carter, "Smewins", Shottesbrooke, nr. Maidenhead, Berks, SL6 3SR (Tel Shurlock Row 539).

## Duke visits cable ship



H.R.H. THE DUKE OF KENT, member of the Council of the Institution of Electronic and Radio Engineers, on board the Cable and Wireless cableship Mercury during her stay in London. C.S. Mercury, moored in the Pool of London, was the initiation point for the inaugural call of the newest transatlantic cable, Cantat-2. She is flagship of the Cable and Wireless fleet and has laid 2,630 nautical miles of Cantat-2. Built in 1962, C.S.Mercury, with a gross tonnage of 8,962, has sailed about half a million miles, laid 16,843 nautical miles of cable, 1139 repeaters and 86 equalisers.

His Royal Highness is pictured here receiving a plaque of the ship's crest from Radio Officer Paul Money (centre), Captain Robinson (left).

THE introduction of integrated circuits into domestic products has dramatically changed the market for consumer electronic goods. Outstanding examples are, of course, the pocket calculator and the whole range of Hi Fi equipment, including FM tuners.

The integrated circuit has three main advantages for the equipment manufacturer-better performance, reduced component cost and simplified assembly and alignment. These are also of great benefit to the home constructor, especially the ease of alignment.

The PW "Sandown" tuner combines all the benefits of integrated circuits with a performance and facilities equalling those of the best commercial models. Particular attention has been given to simplifying the alignment procedure and making sure that the model can be successfully reproduced by the home constructor. A word of warning however, this is still not a project for the beginner and no one who has not successfully completed other projects should attempt this one.

## SPECIFICATIONS

Tuner specifications can be somewhat bewildering. It is worth reviewing briefly just what the various terms mean and what the desirable minimum performance figures are.

Limiting voltage: The minimum signal level from the aerial for satisfactory rejection of A.M. interference. This should be as small as possible and not greater than about $1 / \mathrm{V}$ for long-distance reception.

Quieting sensitivities: The signal level from the aerial necessary to produce the quoted signal-tonoise ratio or quieting. Preferably less than $2 \cdot 5_{\mu} \mathrm{V}$ for 30 dB on mono.

Capture ratio: The ability of an FM tuner to select the stronger of two conflicting signals. The figure quoted indicates the minimum difference in strength necessary for capture and should be not greater than about $2 \cdot 5 \mathrm{~dB}$.

Selectivity: The transmitted signal on Band II occupies a bandwidth of 200 kHz and the tuner must obviously encompass this range. At the same time it must reject interference from stations on Adjacent Channels-spaced 200 kHz away-or on Alternate Channels, spaced 400 kHz away from the wanted station.

In a superheterodyne receiver, there are a number of spurious responses, the two most serious being the Image and IF Breakthrough. Image response occurs on frequencies spaced from the wanted station by twice the IF. Intermediate Frequency breakthrough results from incoming signals from the aerial at the IF passing through the RF stages at sufficient strength to cause interference.

Both responses are minimised by adequate RF selectivity. Rejection figures should exceed 50dB for Image and 70dB for IF breakthrough.

Audio output: This figure must be compared with the input sensitivity of your amplifier to assess its compatibility.

Stereo separation: Insufficient separation between the two stereo channels will spoil the reproduced stereo image. A desirable minimum is about 30 dB .

## COMPONENTS

At this time of fast changing device technology it seems that every equipment uses some new form of circuit and device. One is sometimes tempted to ask if the changes are necessary and whether the new devices confer any real benefit.
Dual gate MOSFETs are increasingly being used as amplifiers in circuits operating between 20 and 500 MHz . They are preferred to bipolar transistors and junction FETs because they are intrinsically more linear devices so reducing spurious responses. They also have an excellent noise performance.
These advantages accrue to either the single gate or dual gate MOSFET. The inclusion of a second gate turns a good RF device into an outstanding one for uses such as this tuner. Since the voltage on the second gate controls the gain of the device it provides a simple method of applying automatic gain control to the RF stage. By the same means the local oscillator can be coupled into the mixer with very little chance that there will be any feedthrough to the aerial.
The second gate also serves to isolate the drain voltage from the first gate. This leads to a very small value of feedback capacitance so that the

## Typical Performance

| Sensitivity |  |
| :---: | :---: |
| Limiting voltage | $0.5 \mu \mathrm{~V}$ |
| 30ds quieting-mono | $1 \cdot 5 \ldots$ |
| 50 dB quieting-stereo | $12 \mu \mathrm{~V}$ |
| Capture Ratio | 2 dB |
| Selectivity |  |
| 3 dB bandwidth | 250kHz |
| Adjacent channel rejec | $25 d B$ |
| Alternate channel rejec | 65 dB |
| Image rejection | 60dB |
| 1.F. rejection | 85dB |
| Audio output (peak) | 500 mV |
| Stereo separation | 40 dB |

# funer 

maximum gain of the device can be realised without neutralisation and with a reduced possibility of instability.

The main dísadvantages of these devices are the high current consumption-about 10 mA compared with 1 mA for a bipolar device-and the delicate nature of the gate electrodes which can be damaged by static charges during handling. The devices used in this tuner overcome this by use of internal zener diodes which conduct away the charge before a dangerous voltage can build up. These diodes have a negligible effect on signal performance

## CERAMIC FILTERS

The high sensitivity and excellent noise performance of dual gate MOSFETs and integrated circuits would be of considerably less value if components of high selectivity were not available. It was of course always possible to build tuned circuit filters with a good response or to use quartz filters but the former were not easy to align and the latter were expensive. Now, however, ceramic filters are available which are preselected by the manufacturer for close frequency tolerances. They combine the good selectivity already mentioned with the linear phase response so vital to good stereo separation

## INTEGRATED CIRCUITS

There are several IF integrated circuits available from a number of manufacturers but none of them offers the complete range of functions which the RCA CA3089E performs. This IC has been designed as part of a system, and is intended to work in combination with a dual gate MOSFET front end and the CA3090AQ stereo decoder.
The circuit comprises a limiting amplifier chain followed by a quadrature detector and audio amplifier Supplementary outputs include AFC drive for the local oscillator varicap tuning diode, delayed AGC for the RF amplifier stage and Signal-strength meter drive. This last output is also used to override the stereo switching in the CA3090AQ decoder if there is insufficient signal for noise-free stereo,


Fig. 1: Circuit diagram of the RF amplifer, Mixer and Oscillator stages, The letters in brackets denote labelled


Fig. 2: Circuit diagram of the IF, Demodulator and Stereo Decoder stages. Either meter may be omitted

| Resistors (all $\frac{1}{4}$ W 5\%/0) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R101 | 39kS | R201 | $2 \cdot 2 \mathrm{k} 2$ | R218 | 4702 |
| R102 | $39 k \Omega$ | R202 | $8 \cdot 2 \mathrm{kS}$ | R219 | $120 \mathrm{k} \Omega$ |
| R103 | 47k $\Omega$ | R203 | 8.2k』 | R220 | 470 kS |
| R104 | 2200 | R204 | 3302 | R221 | 56 k 2 |
| R105 | 51.2 | R205 | $51 \Omega$ | R222 | 3900 |
| R106 | $39 \mathrm{k} \Omega$ | R206 | 3002 | R223 | $12 \mathrm{k} \Omega$ |
| R107 | 22k2 | R207 | $2 \cdot 2 \mathrm{k}$ 人 | R224 | $51 \Omega$ |
| R108 | 2.7kS | R208 | $8 \times 2 \mathrm{k} \Omega$ | R225 | 6208 |
| R109 | $120 \Omega$ | R209 | $8 \cdot 2 \mathrm{k} \Omega$ | R226 | 10kS |
| R110 | $51 \Omega$ | R210 | 3302 | R227 | 10kS |
| R111 | 39 kQ | R211 | 3309 | R228 | $27 \mathrm{k} \Omega$ |
| R112 | 39 k ¢ | R212 | $51 \Omega$ | R229 | $470 \mathrm{k} \alpha$ |
| R113 | 1.5 k 2 | R213 | $10 \mathrm{k} \Omega$ | R230 | 1502 |
| R114 | $51 \Omega$ | R214 | 3kS | R301. | $3.9 k \Omega$ |
| R115 | 10 kS | -R215 | 22kS | R302 | 52 |
| P116 | 10 kQ | R216 | 330 ka | R303 | 7.5kS |
| R117 | $51 \Omega$ | R217 | $10 \mathrm{k} \Omega$ | R304 | $7.5 \mathrm{k} \Omega$ |


| Capacitors |  |
| :---: | :---: |
| C101, C102 4.7pF 63 V | C208-C210 0.01 FF 100 V |
| C103 $0.001 \mu \mathrm{~F} 100 \mathrm{~V}$ | C 212 0.01 $\mu \mathrm{F} \mathrm{f00V}$ |
| C104 0.014F 100 V | C213 120pF 63 V |
| C105 22pF63V | C214 $1 \mu \mathrm{~F} 100 \mathrm{~V}$ MP |
| C106 4.7pF 63V | C215 0.0039 $\mathrm{F}^{\text {c } 63 \mathrm{~V}} \mathrm{PS}$ |
| C107 0.01 2 F 100 V | C216 100pF 63V |
| C108 330pF 63V | C217 $1 \mu \mathrm{~F}$ 100V MP |
| C109. $0.001 \mu \mathrm{FSMC}$ | C218 0.47 $\mu \mathrm{F} 100 \mathrm{~V}$ MP |
| C110 82pF 63V | C219 22al 16 V TM |
| C111 10pF 63V | C220 1 4 F 35V TM |
| C112 18pF 63V | C221, C222 0.0047 $\mu \mathrm{F}$ |
| C113 0.001 FF 100 V | 63 V PS |
| C114 22pF 63V | C223, C224 0.01 FF 100 V |
| C115-C119 0.01 ${ }^{\text {F }} 100 \mathrm{~V}$ | $\mathrm{C} 2250.1 \mu \mathrm{~F} 18 \mathrm{~V}$ Disc |
| C120 10pF 63 V | C226-C227 0.047 HF |
| C121-C123 0.01 F F 100 V | 30V Disc |
| C201-C204 $0.01 \mu \mathrm{~F} 100 \mathrm{~V}$ | C301 1000 $\mu \mathrm{F} 25 \mathrm{~V}$ EL |
| C205 0.047aF 30V Disc | C302 100pF 63V |
| C206 $0.01 \mu \mathrm{~F} 100 \mathrm{~V}$ | C303 0.1 $\mu \mathrm{F}$ 18V Disc |
| C207 100pF 63V |  |
| Capacitor type codes:- |  |
| SMC Sub-min tubular ceramic |  |
| Disc Dise ceramic |  |
| MP Metallized polyester |  |
| PS Polystyrene |  |
| TM Tantaum |  |
| EL Electiolytic |  |
| Remainder are miniature ceramic plate type |  |

Potentiometers
VR101-VR103 $100 \mathrm{k} \Omega$. Cermet preset
VR104 tok Cermet preset
VR105 $100 \mathrm{k} \Omega \log$ Moulded track

Semiconductors

| Tr101 | 3N201 Texas |
| :--- | :--- |
| Tr102 | 3N202 Texas |$\quad$| Tr201 | BC212L |
| :--- | :--- |
| Tr202 | BC182L |

Tr103 BCY71
D101-D108 BB104 Siemens
D109 TIV 306 Texas D301, D302 iN4001
IC201 CA3089ERCA IC301 L123B SGS
IC202 CA3090AQ RCA
LED201 Miniature LED (Red)
Inductors and filters
L101, L102, L104, L106 20 swg tinned copper wire
L103 $\frac{3}{15}$ Threaded slug, powdered iron ( 100 MHz , blue) Cambion
L105, L202 Neosid A6 assembly
1201 RF Choke, Cambion 551-7108-27
1208 Toko 87BN135BX2
Also 34 swg enamelled copper wire for L108, L105, $L 202$
CF201, CF202 Vernitron FM4 matched pair

```
Miscellaneous
M201 \(200 \mu\) A FSD M202 \(100-0-100 \mu\) A FSD
T301 \(12-0-12 \mathrm{~V} 250 \mathrm{~mA}\) secondary
X101 Push-button tuner, 6-station
F301 100 mA anti-surge
LP301, LP302 12V 100 mA max,
St01, S201, S202 SPDT Sub-min toggle
S203 SP, C/Off Sub-min toggle
Aerial socket, co-axial. Audio output socket, 5 way DIN. Lead-through insulators, 17 off: Printed circuit board. Die-cast box \(8 \frac{3}{4}^{3} \times 5 \frac{3^{\prime \prime}}{4} \times 2 \frac{4}{4}\). Tuningdrive parts (all by Jackson Bros.) \(=-\) Cord drive 4555, \(1 \frac{1}{2}^{\prime \prime}\) drum 4509, \(\frac{t^{\prime \prime}}{2}\) spring 4587, Pointer 4580
```

> Note The Push-button tuner and the pcb are available from:- F. W. Electronics, 40 Tuddenham Road, Ipswich IP4 $2 S L$

A squelch or inter-station muting facility is also incorporated. This virtually cuts off the audio output in the absence of a received signal of reasonable strength.

The CA3090AQ decoder uses the phase-locked loop principle, which offers simplified initial alignment and more stable long-term performance. Automatic mono-stereo switching and stereo beacon drive is incorporated, operated by the 19 kHz pilot tone on stereo transmissions.

## CIRCUIT DETAILS

Coupled coils L101, L102 (Fig. 1) together with their associated components form a tuneable bandpass circuit which couples the $75 \Omega$ aerial input to the dual gate MOSFET RF amplifier $\operatorname{Tr}$ 101. Delayed AGC is applied to this stage via R103. The RF signals are then passed, via a further tuned stage to the MOSFET Tr 102 where they are mixed with the output of the Colpitts oscillator, $\operatorname{Tr} 103$.

The oscillator is tuned to $10 \cdot 7 \mathrm{MHz}$ above the incoming signal frequency by L106, C111 and the tuning varicap diodes D107, D108. Varicap D109 changes the oscillator frequency in response to the AFC voltage to compensate for slight mistuning or oscillator drift. The mixer load is tuned to $10 \cdot 7 \mathrm{MHz}$ and is capacitively tapped to provide a low impedance output suitable for feeding to the IF stages.

Both the signal and oscillator circuits in this receiver are tuned by the back-to-back varicap diodes D101-D108 in Fig. 1. When operated under reverse bias conditions, the capacitance of these diodes varies with the bias voltage, decreasing as the voltage increases.

A potentiometer may be used to vary the reverse bias, and therefore the capacitance, of the diodes thus providing a simple means of tuning the receiver. The leads to this potentiometer do not carry high frequency currents so the tuning control may be mounted at some distance from the receiver. The $Q$ factor of a varicap diode falls rapidly as the reverse bias approaches zero. VR104 is adjusted

to ensure that the diodes do not approach this condition when the tuning voltage is at minimum.

For simplicity the tuning range of this receiver is determined by the oscillator, the RF circuits being adjusted to track over the same range by adjustment of L101, L102, L104 and VR101-VR103. S101 selects the source of the tuning bias voltage which may be either the manual tuning control, VR105, or the push-button unit. The selected button may be rotated to adjust the preset tuning potentiometers.

Selection of a button momentarily operates a switch which overrides the action of the AFC circuit as the tuning of the receiver changes. This prevents the receiver from locking on to strong signals whilst tuning to adjacent weak ones.

Alignment details will be given in a later part of the article. The simple alignment procedure means that no expensive equipment is needed, a voltmeter and a pair of ears being the only essential items!

The 10.7 MHz IF signal is fed to the common-base stage $\operatorname{Tr} 201$ (Fig. 2) which acts as a buffer between the low impedance output from the front end and the first ceramic filter CF201. A further buffer transistor $\operatorname{Tr} 202$ feeds a second ceramic filter which completes the IF selectivity section.

Integrated circuit IC201 contains the IF amplifier and demodulator and provides outputs for a tuning meter, signal strength meter, delayed AGC, AFC, squelch and automatic stereo inhibit as previously described. Either or both meters may be omitted if they are replaced by wire links, shown dotted in Fig. 2, and any of the switched facilities may be permanently wired, allowing the switch to be omitted if required.

Demodulated signals which appear at pin 6 are fed to the stereo decoder IC202 via R221, which ensures that IC202 cannot be overloaded by large outputs from IC201. Capacitor C216 produces a break-point at 53 kHz to reduce 'birdies' which can be produced by signals whose frequency is close to that of the required signal.

The oscillator frequency is determined by L203 and C215, whilst C217, 218 and R222 provide the filtering required for correct operation of the phase

The prototype tuner box. In the final version there are three more leadthrough insulators which carry power to the dial lamps mounted on the front panel assembly.
locked loop. Pin 4 receives the stereo defeat voltage which may be switched via S203 to automatic, to mono only, or to 'stereo lock' which causes any stereo signal to be decoded however poor the signal to noise ratio.

Left and right hand audio outputs are deemphasised by C221, C222 and provide about 500 mV peak of audio which should be connected to the radio inputs of a good quality amplifier. A light emitting diode, LED 201, is illuminated to indicate that a stereo signal is being decoded.

The power supplies to individual stages of the IF and audio sections are separately decoupled, as in the front end, to avoid unwanted coupling effects.

A conventional full-wave rectifier feeds current to a power supply regulator IC301 (Fig. 3) which produces an extremely stable output of about 13 V . A proportion of the output voltage, determined by R303 and R304, is compared with an internally generated stable reference voltage, the result being used to control the output via a high gain amplifier.

Resistors R303, R304 may be adjusted slightly to vary the output voltage, if required. R302 is used to monitor the output current, its value being chosen to limit the current to the safe value of 100 mA in the event of a short-circuit.

If a different transformer/rectifier combination is used, ensure that the input voltage of IC301 does not exceed 19 V unless it is fitted with an adequate heatsink.

Next month's article will give constructional details including printed circuit board layouts.


## Interference

With reference to your editorial "Interference". I cannot quite see why you think it surprising that the amateur who is being received on audio equipment is not responsible for curing the equipment.
Long before high fidelity equipment became popular there were well into the tens of thousands of licensed Amateur and commercial transmitting stations in the UK. Knowing this, surely the responsibility for ensuring that the equipment is protected against radio signals lies with the manufacturer. I am no lawyer, but surely at the moment under the Trades Descriptions Act, if we, as retailers sell an amplifier, the customer is entitled to receive an amplifier and not a radio receiver. Certainly with the high fidelity equipment our company has supplied, where difficulty with unwanted radio reception has arisen, we have felt it our responsibility, and with new equipment or equipment within the guarantee period, have always sorted out such difficulties without charge.
Might I also point out, that under the conditions of both receiving and transmitting licences, the Ministry of Posts and Telecommunications, is not responsible for sorting out difficulties with audio equipment. If asked nicely, they will usually assist, but they will certainly not close down any transmitter just because of its unwanted reception by audio equipment. They may of course, ask the amateur concerned to volunteer to close down temporarily, if a radio tuner unit is also involved, but strictly speaking, pure audio equipment is outside the field with which they are legally involved.

The suppression of audio equipment against unwanted radio frequency reception, is compara-
tively simple, and inexpensive at the design stage, and there is no real excuse for the present lack of attention on this point. A point which might not be so well known is that annoying "plops" and "bangs" from refrigerators and central heating thermostats disappear entirely when equipment is properly designed to prevent radio breakthrough, and that there is also evidence which would seem to point out that the elimination of these "spikes" also improves reliability. Several leading manufacturers have now incorporated components to alleviate these troubles, and it is to be hoped that with a little pressure others will soon follow suit. Harry Leeming (G3LLL)
FSERT. T.Eng. (CEI),
nical Director, Holdings Photo Audio Centre).

There appears to be some confusion arising from this article. The Secretary of the Interference Committee of the RSGB was recently quoted in a letter to the RTRA ("Dealer" Sept 1973) ". . . in the case of interference to audio equipment, strictly speaking the services of the Post Office are not available. Where breakthrough occurs on audio equip. ment, then'it is "by definition" at fault since it is not intended to act as a radio receiver.
"The RSGB has, for several years, had a Committee whose specific purpose is to deal with problems of this nature, and on average we receive about ten enquiries a month from members.
The cures for the problems are often simple, and many of these have been covered in the Society's monthly magazine "Radio Communication". Other Society publications also deal with the matter."

Thank you, Mr. Leeming, for putting the record straight.Editor.

## Dry Battery Charging

I am writing to you to express my concern over the possible consequences to any of your readers who construct and use the dry battery charger described in the March 1974 issue of Practical Wireless.
Dry batteries are of primary electrochemical type and should be used only once. Attempts to recharge them are hazardous and in extreme cases could give rise to personal injury.
The underlying reasons for the
danger are fundamental and stem from materials which are basic to the construction of dry cells. These materials do not possess the capability of reacting with the gases that are evolved on overcharge. Furthermore even on normal charge, gases are produced due to the Faradic inefficiency of attempting to drive the chemical reactions pertinent to normal useage in the reverse direction. A more insidious effect is that on charge the zinc which forms the negative electrode is not returned to its original state, which is properly inhibited to prevent corrosion but is deposited in a dendritic highly active form which corrodes steadily with the evolution of gaseous hydrogen.

Dry cells are well sealed to ensure that they reach the consumer with the minimum of deterioration and hence are not able to vent the gas resulting from the various charge effects. In consequence the outer construction of the battery ruptures. This may happen quite gradually and possibly not until the battery is in the battery using equipment, whereupon exudation of corrosive liquid is likely, or it may happen suddenly after considerable gas pressure has built up within the battery causing an explosion.
I repeat that dry cells should be used only once and attempts to recharge them are hazardous. -F. L. Tye, B.Sc., A.K.C., Ph.D., F.R.I.C. (General Manager, Central Laboratories, The Ever Ready Co. (G.B.) Ltd.).

## Stop Watch

Readers who were interested in the construction of the "Solid State Stop Watch" in February P.W., and are fortunate enough to already possess a digital multimeter may not be aware that by simply connecting a $1000 \mu \mathrm{~F}$ capacitor across the meter terminals and switching to the ohms range they can obtain a digital timer with no practical construction whatsoever.
On the $100 \mathrm{k} \Omega$ range readout will be tenths of a second, on $1 \mathrm{M} \Omega$ range readout will lie in seconds. Maximum readout will be dependent on number of digits available, accuracy depends on the tolerance of the $1000 \mu \mathrm{~F}$ capacitor and its leakage. Mode of operation depends on use of constant current source with digital voltage readout.-J. F. Latuskie (Kent).

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SQ Red Neons 250V
2 5mm8』 Earpiece
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## Mixers

The process of mixing really amounts to applying two separate signals to the FET and because the device is not totally linear (ie. the graph of $V_{G S}$ against $I_{D}$ is not a straight line) it will produce


Flg. 12: Two circuits for common source mixers, the tuned circuit L3/C3 resonating at the required output frequency.



Fig. 13 : Mixer circuit employing the common gate mode.
frequencies corresponding to the sum and difference of the original signals. A tuned circuit in the output, usually the drain, is tuned to whichever of the new frequencies is required. In superhets this is nearly always the difference signal and the tuned circuit is the primary of the first IF transformer.

Fig. 12 shows two types of common source mixer. In the first the FET is set up as a common source amplifier but two signals are applied to the gate, one in the normal way and the other, from the oscillator, is connected by a very small capacitor. Because this method is used mainly at VHF the capacitor may be two short lengths of wire twisted together. The second circuit is also very similar to the conventional RF amplifier but the oscillator signal is introduced at the source by connecting the bypassed source resistor to earth via one of the coils in the oscillator. Part of a conventional bipolar transistor oscillator is shown to illustrate how the coupling is achieved.

Note that in this circuit the received signal is applied in common source mode whereas the oscillator signal is introduced in ground gate mode, the opposite of our next example which is a common gate mixer. To prevent confusion it must be made clear that when a mixer is referred to as common gate or common source it is the mode in which RF information carrying signal is applied that is being quoted.


Fig. 14 : Simple dual-gate MOSFET mixer.

A common gate mixer is shown in Fig. 13, the main RF signal may be applied in either of the ways discussed for ordinary common gate amplifiers. Note that the capacitor coupling the oscillator signal is kept small to ensure a low level of injection.

It is in mixers that MOSFETs have made an impact. They have been made with two gates and mixing is achieved by applying a signal to each gate, Fig. 14. The MOSFET may be a depletion or enhancement type. The diagram shows a depletion type but if an enhancement type were used the gates would have a DC isolating capacitor in series and gate resistors would be introduced going to the supply line.


Fig. 15: Circuit of a JFET oscillator, the frequency of operation being determined by L2/C1.


Fig. 16 : Two more circuits of oscillators using an FET.


## Oscillators

The use of an FET oscillator below VHF is not very common because bipolar transistors give good performance. A circuit of a simple FET oscillator is shown in Fig. 15 and if commercial coils are used they should be of the type intended for use with valves. Those who are familiar with valve circuitry will see how close a resemblance it bears to a tuned grid oscillator. If the circuit fails to work try changing over the connections to one of the windings. For those who wish to experiment two other FET oscillators are shown in Fig. 16.

## The source follower

With all the reference being made to common gate and common source stages the common drain, or as it is often called, source follower, mode of operation, has been neglected. Fig. 17 shows a common drain stage and it is the equivalent of the emitter follower or common collector configuration of bipolar devices. It is used, like its bipolar counterpart, as an isolating stage. Its input impedance is very high, $10 \mathrm{M} \Omega$ in our example, and it is superior in this respect to its bipolar equivalent. The voltage gain is a little less than unity and for maximum signal handling the source resistor should be chosen to make the source voltage about half the supply voltage.


Fig. 17: Source follower isolating or buffer stage.

## Common FETs

A brief list is given of some common and inexpensive FETs.
2N3819 n-channel JFET, good general- Texas 2N3823 \} purpose types
2N3820 p-channel JFET, good general- Texas purpose type
3N141 n-channel dual-gate MOSFET, de- RCA pletion mode
40468A n-channel depletion mode MOSFET RCA
A useful publication on MOSFETs is the "MOSFET Selection Guide" which is free from RCA. Data on Texas devices may be obtained from Texas Instruments, Manton Lane, Bedford. RCA data may be obtained by writing to RCA, Sunbury-on-Thames, Middlesex, TW16 7HW.

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Alternatively the attachment will considerably improve the sensitivity of cheap 1000 ohm-per-volt multimeters and make them more suitable for electronic measurements. Either way there is a lot of potential value in such a simple device.

## Circuit

The circuit is shown in Fig. 1 and is quite clearly an emitter follower in which the emitter load is the multimeter. Any potential at the base of Trl will be presented at its emitter but it must be remembered there is an approximate 600 mV forward voltage drop across the pn junction of the transistor. Because of this a normal emitter follower will not respond to input voltages less than 600 mV . In this case, however,


Fig. 1: Simple circuit of the voltmeter attachment. A component list has not been provided on this occasion! As an alternative to the construction shown in Fig. 2 the circuit could be built in the form of a probe with a pre-set potentiometer in place of VR1, the slider being adjusted with the forefinger.
we use two forward biassed silicon diodes, D1 and D2, to give a reference potential of approximately $1 \cdot 2 \mathrm{~V}$ at the bottom end of R1. A proportion of this voltage is tapped off by VR1 and we use this to place any input voltages on a pedestal voltage set by VR1. If the forward drop of the transistor were 600 mV and we set the potential at the wiper of VR1 to exactly 600 mV any extra potential applied at the input connections is bound to be displayed accurately at the emitter.

## Limitations

The circuit has its limitations. For example, voltages of reverse polarity will not be displayed so these should not be applied to avoid exceeding the reverse breakdown of the base emitter junction. Again, the circuit will not respond to input voltages having magnitudes greater than the emitter follower's supply voltage. In actual fact it is safer to assume a level less than this, say 7 V , because of the pedestal voltage which takes up a portion of the range.

## Operation

Care has to be taken in using the attachment because its simple design does not make allowances for temperature drift and it should be correctly zeroed before each measurement. This is done by shorting the input probes together and turning VRI until a reading is seen on the meter. VR1 is then reduced until the needle on the meter JUST stops at the bottom end of its travel, but do not reduce the level beyond this point otherwise it will defeat the object of the pedestal voltage. This procedure sounds a little difficult and could cause inaccuracies but it is extremely straightforward in practice and the zero setting is very easy to determine.


Fig. 2: Layout of attachment used by author and arranged to connect directly to the voltmeter terminals or sockets.

The zeroing procedure is made easier if the voltmeter is switched to a low voltage range. When carrying out measurements set the meter to any range, below the maximum already mentioned, and if the zeroing has been done correctly the meter scale will read off the voltage directly without any conversion being necessary. Due to the rectifying action of the base emitter junction of the transistor low voltage AC signals can be detected and measured by leaving the voltmeter set to DC. However, the signal should be free of any DC component.


# $\mathfrak{A}$ great future abead of him 

MR. R. J. Halls from Penzance, Cornwall sent me a cutting from an old "Windsor Magazine" dated 1897. It tells of a young man by the name of Marconi who "may have a brilliant career ahead of him".
"Guglielmo Marconi, whose name, in connection with "telegraphy without wires," has come lately into prominence, was born in Bologna. Although his name would seem to indicate an unmistakable Italian origin, as a matter of fact he is of English descent on his mother's side. He was always, from very early in life, an ardent amateur student of

electricity. It was not, however, until two years ago, while making certain experiments on his father's estate at Bologna, that he made the great discovery of his life. This, briefly, was the transmission of signals by means of electric waves travelling in the air. Signor Marconi's invention having obtained little recognition in his native country, he decided to bring it to England. Here its value was instantly recognised by our eminent scientific experts. Committees representing the Army, Navy, and Post Office, have eagerly discussed the invention and are investigating its possibilities. As Signor Marconi has but just attained his twentysecond birthday, a brilliant career may lie before him."

> Left to right: ANAKA AAB-S of 1916
> " $N$ " type of W.E. 1918
> VT-Z of W.E. 1918

Bottom pictureweft to right: British "R" valve of 1914
French " $R$ " valve of 1916 by Métal French Fotos valve of 1916 by Grammont


## そeaders tomments

Basil D. Van Der Syde, from Poole, Dorset sent me a photograph of part of his workshop. On the bench is a Thorn 3000 colour TV chassis. Its audio section is driving a model " H " horn speaker made by S. G. Brown about 1926.

Mr. Van Der Syde says his picture caused a lot of interest at work where the speaker is a good few years older than some of the engineers! One of them even went to the management with tongue in cheek and asked if all the department could be supplied with similar loudspeakers as audio aids.
The model " $H$ " speaker contains a complex Brown type "A" mechanism of a conical metal cone connected via a reed and balanced armature magnet system. This particular unit started its life in London, found its way to New Zealand then came back to England when a N.Z. colleague sent it to Mr. Van Der Syde.

## Zetters

Don't forget to keep those letters pouring in-I hope to be able to publish some more "Readers' Comments" next month.

## Fintage walues

Vintage radio enthusiast Chris Petsikopoulos from Athens tells me that he has come across some WWI valves which are quite rare, especially the French "R" by Métal made in 1916 and the "FOTOS" by Societe Grammont.

French valves were developed by "Telegraphie Militaire" of the French army during 1914-1918 but were first made by Societe Grammont. Later the production output of the factory became insufficient for the war needs, so the "Compagnie des Lampes Metal" also began to manufacture them. All the WW1 French valves had a copper base shell.

Other valves included in Chris's collection are a 1914 British "R", a 1916 5W Japanese transmitting valve made by Anaka, a 1918 American VT-2 (Western Electric) a famous " $N$ " type or "peanut" valve. This was one of the first miniature valves to be made for the US Signal Corps in late 1918, and was also made by Western Electric.

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## by Eric Dowdeswell G4AR

SUMMER holidays are obviously taking their toll of my correspondents, judging by the few reports received so far this month. Let's hope that they return rejuvenated for the winter's stint on the amateur bands! On the other hand, they may be busy refurbishing their aerial and earth systems or getting a few more feet of wire into space!

Strange how a new aerial seems to bring in DX not heard before. Switching back to the stand-by longwire usually reveals that the DX is still there, but it's a nice feeling anyway! If at all possible do put up a vertical aerial of some sort as an alternative to the horizontal wire. Verticals are reputed to pick up more of any locally generated electrical noise but they will also really bring up the more distant signals from around 8 to 10,000 miles away. You will, of course, use an aerial tuning unit to bring the vertical to resonance on each band!

## Reporting in

Regular John Porter (Baslow, Derbys) kept at it with his Trio 9R59DS and multiband dipole and found some interesting calls on 15 and 20 m . A warm welcome to Alan Rae (Glasgow) who uses a Grundig set for SSB and an Astrad 17 for AM. On the broadcast bands, presumably! Lack of space caused Alan to try the bedsprings as an aerial! Not novel but full marks for initiative! A 50ft wire outside proved more effective even though 'it's falling down around my head'. Nasty!

Newcomer A. W. McNeill (Newbury, Berks) pleased me with a $\log$ of CW titbits heard on 20 m using old faithfull R1082 and a five valve (good lad!) TRF and 30ft of wire. He queried one or two callsigns but, as I have already suggested to him, it is a good idea to look at the ITU prefix block listing when the answer will often become apparent.
A QSL from EP2BQ confirming a reception report on 160 m CW has brought much cheer to Stan Sharred, our correspondent in B'ham. The transmitting amateur often has trouble in getting a QSL after a QSO but it is many times harder for the
listener. It is a fact that very, very few listeners reports indeed ever contain information of use to a DX station. To encourage a reply it is essential to send adequate postage in the form of IRC's and a fully addressed return envelope. Do make sure the envelope will take an average sized QSL!
Mr. B. F. Hughes (Worcester) BRS25901 sent in a list of interesting stations heard on his FR500SDX, but that's all! Welcome to the page Mr H and let's hope we shall have more details of you anon. Ken Ranger (Colchester) lists a few stations heard on his teeny-weeny three transistor reflex portable, which he is going to need as he takes off soon for Hong Kong. We hope he will keep in touch with us from VS6 land.

## Copying the DX

I've always reckoned that there are three layers of stations to be heard on a DX band. On, say, 20 m there are the Europeans and east coast W's, the weaker stations either using lower power or further away, and the real DX, weaker again but often quite readable in the absence of any QRM. It is the last category that will show a marked improvement if a vertical aerial is used instead of a horizontal one.

However good a receiver might be in terms of sensitivity and selectivity it is the ears of the operator which can provide the greatest degree of discrimination between wanted and unwanted signals and this ability comes only with experience. Using headphones of course (who has ever heard of a serious operator using a loudspeaker??) it is not difficult to train oneself to ignore the strong signals and to listen through them to the weaker signals below, whether they be SSB or CW. It is a bit easier to do this on CW where no two signals are quite the same in character, especially if hand sent. We all push or press the key in a different way in spite of the efforts of electronic keyers to iron out our differences, much to be deplored!

## Log extracts

A. Rae:-80m PY4FUS PY4IR 40m CP2SL CX1CL HC2TV KZ5JM MIC OX3LW TG8KT VX3AWU VK5PC YV2NO 9G1DY.
A. MeNeill: - 20 m A9XO FG\%XC FL8CE TJ8FE TR8PB 5T5FP.
J. Porter: - 20m CE31F EL9C FY7AE TU2EN ZD7SD ZD8HD 3B8DD 5U7BA 6Y5GB 9X5PT 9Y4VT 15m EA8HA HI8EJH SV1IM (Paros Is.)
K. Ranger: - 20m EL2AK FP8DH OJ0MA VE6AGV VU2DK 9M2CR.
B. Hughes: - 80 m FP8DH TJ1EZ ZL2IR 20 m AX6XR DUINRS FG7XL HI8XHN TR8AF VEBDC VP2DM VP9GR XW8AL ZD7SD 9M8VLC 15 m CX5BT HM4GF KS6DH VK8HA 5R8SD 9M8NK.
S. Sharred: - 160m EP2BQ VX1KE W1HGT WB8APH 80m ELLTF OY5NS ZS6ZE 40m 9GIDY PY7PO 20m FM0AZY YV9AF 9Y4HR.

All CW stations in bold, remainder are SSB.

## BROADCAST BANDS

Short Wave and VHF/FM reports by the 15th of the month to The Editor, Practical Wireless, Fleetway House, FarrIngdon Street, London, EC4A 4AD,

Medium Wave Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG.

## AMATEURBANDS

Logs covering any amateur bahd/s in band/alphabetical order by the middle of the month to Eric Dowdeswell G4AR, Sllver Firs, Leatherhead Road, Ash= tead, Surrey, KT21 2TW.

## MEDIUM WAVE BROADCASTS <br> by CHARLES MOLLOY

CLIVE BARWOOD (Grimsby) has been trying for local radio stations with his Philips transistor receiver. His log includes day time reception of Capital Radio on 557 kHz ; Radio Blackburn 854 kHz ; Radio Sheffield 1034 kHz ; Radio Leeds 1106 kHz ; Radio Derby 1115 kHz ; IBA Birmingham 1151 kHz ; Radio Humberside 1484 kHz ; Radio Notting. ham 1520 kHz ; Radio Leicester 1594 kHz and Manx Radio, Isle of Man also on 1594 kHz .

Brian Murray (Edinburgh) has been listening to London Broadcasting on 719 kHz at 0100 hrs with his GEC BC 3248 receiver and 25 ft longwire antenna. He mentions that the new IBA station Radio Forth will be on 1546 kHz ( 194 m ) when it comes on the air later this year. Radio City, Liverpool will also be on 1594 kHz and is expected to open by October 1974.

Scottish DXers (and others) will be interested to learn that a medium wave/shortwave conference is being planned to take place in Scotland with the possibility of a DX expedition. All those interested should write to Fred Dinning, South Brae Cottage, Dunlop, Ayrshire, KA3 4BP, Scotland. Fred, who is a keen medium wave DXer, has a Hammerlund SP600JX6 receiver and an HRO MX. He has three external aerials; a 6000 ft Beveridge at 10 to 15 ft above the ground pointing SE/NW, a 600 ft longwire pointing $\mathrm{S} / \mathrm{N}$, a 500 ft longwire pointing $\mathrm{SW} / \mathrm{NE}$ and a medium wave loop. With this formidable set-up the following DX was logged:- 587 kHz Riyadh, Saudi Arabia at 2215 hrs ; Kishasa, Zaire 692 kHz at 0010 hrs ; Bagdad 760 kHz at 2310 hrs ; Dakar, Senegal 764 kHz at 2324 hrs ; Acholi, Uganda 809 kHz at 0300 hrs ; Radio El Espectador, Uruguay on 810 kHz at 0300 hrs ; Radio Montecarlo, Uruguay 930 kHz at 0210 hrs ; Radio Belgrano, Buenos Aires 950 kHz at 0150 hrs ; PRE8 Rio de Janeiro 980 kHz at 2325 hrs ; Bissau, Portuguese Guinea 1070 kHz at 2330 hrs ; PRG9 Sao Paulo, Brasil 1100 kHz at 0235hrs; CB114 Radio Nacional, Chile 1140 kHz at 0310 hrs ; Radio Globo, Rio 1180 kHz at 0200 hrs ; Radio Eldorado, Rio 1220 kHz at 0210 hrs ; Radio Martinique 1310 kHz at 0245 hrs ; Enugu, Nigeria 1320 kHz at 2300 hrs ; Radio Chaco Boreal, Paraguay 1330 kHz at 0230 hrs ; all times being GMT.

Noel Green (Blackpool) has an Edystone 850 and a medium wave loop. He reports hearing the new 1200 kW station at Istanbul, Turkey on 1016 kHz in mid-evening with interference from the West German outlet on the same channel. Two other megawatters have appeared recently. On the long waves Warsaw, Poland on 227 kHz has increased power to 2000 kW with a 2000 ft mast as a radiator. Vidin, Romania is a newcomer to the band and is on 1232 kHz with a power of 1000 kW . At the other end of the power scale, the 2 kW Radio na Gaeltachta station at Connermara located on the west coast of Eire is being heard regularly by the writer from his QTH in the north west of England. Programmes are in Gaelic with Irish music, during the evening.

An unusual report comes from E. Jenkinson of Sheffield who has been hearing the sound of Yorkshire TV on the medium waves with his Vidor 393 portable receiver. A receiver fault is suspected but it might be caused by re-radiation. Has any reader had similar reception of TV sound on the medium waves?

## IN THE

OCTOBER ISSUE

## SPECIAL-IN FUIL COLOURII

One of the most useful alds to the TV expent menter or service engineef is Test Card F In tact yout test equipment is limited lifoes a long: way towards making up deficiencles:- But what you can get out of it deperids on how much you know about its abilty to show up receiver defects and give an indication of tie pefformance of the yarious parts of a recelver. A full colour supplement in the October ssue gives a detalled gulde to getting the mostifrom he test card

## DIGITAL TOUCH TUNER

There are considerable advantages to the use of touch foning- no mechanical parts of any kind, so. that optimum tuning stability is achieved. Full constructional detalls of a simple digital touch tuner will be provided in Television. The unit employs a single pair of touch contacts, switching from one channel to the next each the it is operated.

## SOLID.STATE VIDEO

A major development in TV technology is the solid-state image sensor which makes possible small, cheap TV cameras. A new semiconductor technology is employed charge coupling. A clear account of what is involved is given. Lowresolution solid-state camefas have been demonstrated and high-resolution versions are in the developnent stage.

## SERVICING TELEVISION RECEIVERS

This month Les Lawrydohns describes the common faults and the fault-fnding pracedures required, with the last of the wired chassis, the ITTTKB VC100 chassis.

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## PRODUCTION LINES colin niches

## MORE PRICE CUTS

Sinclair has announced reductions in the price of two more of its pocket calculators. The "Scientific" is cut from $£ 49$ + VAT to $£ 29 \cdot 95+$ VAT and the slim "Executive Memory" model from $£ 49+$ VAT to $£ 34.95+$ VAT. A kit version of the "Scientific" is available at $£ 19.95$ inc. VAT.

The correct price of the new "Cambridge" model is $£ 19.95$ plus VAT. The kit version is $£ 13 \cdot 59$ plus VAT and not as shown in the "NEWS . . ." feature in August P.W.

## THE RN712

I first mentioned this unit in my "ICE" article in the June issue. Since then I have had a number of enquiries from readers for more gen-so here goes:

The RN712 employs 83 semiconductors (49 transistors and 34 diodes) and an IC.

The spec. is as follows: Power supply is 12 V d.c. (-ve earth). Current consumption is 1.25 A at 14.4 V and output power $2 \times 5 \mathrm{~W}$. Wave ranges are Medium ( $185-586 \mathrm{~m}$ ); Long (11542000 m ) and f.m. ( $87 \cdot 5-104 \mathrm{MHz}$ ). The intermediate frequencies are: 470 kHz (a.m.) and 10.7 MHz (f.m.).

Controls: rotary (left-hand)-front, on/off volume; centre, tone; rear, balance; (right-hand)-Super Turnolock pre-set station selector.

Slider controls are: (left hand) fast wind, rewind and stop. (right-hand) top, radio/microphone record switch; (left-hand), bottom, stereo/mono switch and indicator.

Rear connections provide for a car aerial, automatic car aerial power supply, two $4 \Omega$ speakers, fused power supply and microphone.

Frequency response of the cassette player/recorder is quoted as 80 $10,000 \mathrm{~Hz}$ within 6 dB . Wow and flutter $\max \pm 0.3 \%$. $S / n$ ratio is quoted as being better than 45 dB . Dimensions of the unit, which fits into a normal car-radio cut-out are: $7 \frac{1}{16} \times 2 \times 6 \frac{3}{8} \mathrm{in}$.

Philips Electrical Limited, Century House, Shaftesbury Avenue, London, WC2H 8AS.

## SOLDERING IRONS



Miniscope iron (above)
The Superspeed (right)
The EGM Superspeed and Miniscope soldering irons retain the shape, size and weight advantages of conventional irons yet have the rapid heating advantage of the heavier and often clumsier soldering gun.
With heating times of around 5 seconds these irons can be run from a 6 V d.c. supply such as a car battery or from 2.5 to 6.3 V a.c. from a mains transformer. EGM supply a transformer as an optional extra, supplying 4.5 V at 20 A indicating a standard (intermittent) rating of 90 W for a single iron.

With the soaring cost of electricity it is good to see that these irons are off when not in use. Only light pressure is required on the switch ring,

## TANDY

After eight months of operation, the U.S. Tandy Corporation has opened 50 own-name franchise audio shops in Great Britain.

The first half-dozen were opened in December 1973 in the West Midlands.

For further information on Tandy, please refer to the "NEWS . . ." page of our February 1974 issue.

an automatic cut-out looking after bit temperature.

Further details from EGM Solders (PW) 3 United Road, Manchester, M16 ORJ.



## PART 2

## CONSTRUCTION (continued)

The crystal filter unit, Fig. 8, can be wired and completed on the $3 \times 2$ in box lid before installing it in the chassis but initially the lid should be placed in position and fixing holes and clearing holes for the crystal sockets drilled through the lid and chassis.
-Notches are cut in the lid flanges and in the edges of the box to clear the various leadout wires. The main tuning capacitor is fitted to the other aluminium box which is mounted vertically on the chassis providing a solid mounting but a simple stiff bracket could suffice here since there is a flexible coupling between the dial drive spindle and the tuning capacitor.

Note the correct position of the pins of the IF valveholders, Fig. 8, and ensure that the small screens, cut from thin tin plate, are correctly placed or instability could result. Each screen is soldered to a tag under a mounting bolt and to the centre spigot of the valveholder. Similarly, the anode pins of the mixer valveholder are placed for the shortest leads to the filter box, again aiming at a balanced layout as far as is possible. Another important screen is that between the RF coil sockets on top of the chassis.

The first oscillator V2 is very simple, keep wiring short and direct and components firmly mounted. Capacitor C29 should be connected with shortest possible leads from pin to earth. Fig. 9 shows the layout.

The CIO and the PD together with the IC audio stage are built up on two pieces of Veroboard as shown in Figs. 10 and 11. Spacers or extra nuts are used to keep the boards clear of the chassis. The three central earth rails on the PD board are directly earthed by the fixing bolts and nuts. Veropins provide connections to the external circuitry. The IC should be inserted only after carefully checking the wiring and, in particular, checking for solder splashes or blobs between the copper rails on the boards.

The S-meter should be fitted after all the drilling has been done, to avoid damaging the meter by excessive vibration. The components associated with the S -meter are mounted on a small piece of plain Veroboard which is held under the terminal screws of the meter. Fig. 12 shows the arrangement.

Fig. 8: Close-up of the crystal filter box and associated components. The crystal sockets shown are those used with surplus, crystals in the original experlments with the filter. The crystals and holders supplied by Senator Crystals are HC6U style.

[404022]
Fig. 9: above, gives the location of the principal components under the chassis. Figs. 10 and 11, left, show the layouts for the carrier insertion oscillator and product detector boards, actual size. Each board can be tested before being fitted into the chassis.


The various IF coils are wound as shown in Fig. 13. Turns are scramble wound and held in place by a spot of polystyrene cement similar to that used in model-making. It is a good idea to make a note of the pin numbers used for each winding on the coil formers to ensure correct positioning of the IFTs on the chassis.


Fig. 12: Layout of the components in the S-meter circuit.
Note that L6 is bifilar wound. Take a length of wire sufficient for both windings, double over at the centre and wind on the requisite number of turns keeping the wires together, winding them as one. The earth end of L5 is taken out through the base of the coil former and soldered to an earth tag.

Scrape ciean the ends of all the windings before 3 soldering to the pins on the formers. Ensure that the holes in the chassis are big enough to clear the pins or, to be quite sure, slip a short piece of insulating sleeving over each pin.

As there are several holes to be drilled for each IFT it is a good idea to take a spare coil former and remove the pins thus enabling the former to be used as a template for marking out the holes, after the central hole is drilled.

The RF tuning ganged capacitor is mounted off the chassis with washers on the mounting bolts. First fit the slow motion drive to the panel in the correct position and then adjust the number of washers until the capacitor spindle fits into the drive without difficulty. If it is misaligned the drive will bind and stick. The slow motion drive is essential as the RF tuning is quite sharp. A small metal or card disc is fitted to the flange on the drive and eventually calibrated for the three $R F$ tuning ranges. The heater wires, preferably of differing colours; are twisted together between valveholders and one side earthed at the mixer valveholder only, the corresponding wire being earthed again in the power supply unit, hence the coding. The chassis should not be used for heater earth at other valveholders. Small stand-off insulators are used to support the - otherwise free ends of resistors etc.

A slot is cut in the left hand side of the cabinet to clear the coaxial aerial socket and short leads go from the socket to the IF trap L1/Cl and from the trap to the RF tuning capacitor. The aerial socket could be mounted on the rear drop of the chassis and a short length of coaxial cable run back to the trap. This would necessitate cutting a hole in the


Fig. 13: Detalls of the windings for the filter and IF transformers and the If trap. The former length is $1 \frac{1}{2} / \mathrm{n}$, and not $1 \frac{1}{2} / \mathrm{n}$, as shown in components Ilst.
back of the cabinet to clear the aerial socket. In any case, a similar size hole is required at the back for the plug on the end of the power supply cable to pass through.

## TESTING CIO/PD

The CIO board can be tested before it is fitted into the chassis by temporarily connecting the crystal to the board (do not solder to the crystal pins!!), ignoring capacitors TC4 and C46 and feeding a low voltage supply, from a 9 V battery, to R29 and the earth line. The $5 \cdot 5 \mathrm{MHz}$ signal should be heard on a short wave receiver at this frequency if the oscillator is placed close to the receiver's aerial socket. The receiver's BFO should be on.

Similarly the audio section of the PD and audio board can be tested, connecting the phone jack, volume control and a low voltage supply to the pins on the board. A test signal from a transistor radio headphone socket can be fed to the top of the volume control.

A fiye-way terminal strip is fitted inside the chassis where the power supply cable enters. The four-way screened cable is terminated with a B7G plug, plugging into a socket on the power unit.

## POWER SUPPLY

The circuit of the power supply unit is shown in Fig. 14. All the valves in the receiver are fed from the 150 V stabilised line rather than from the more conventional unstabilised 250 V . The general result is improved frequency stability and less heat dissipation in valves and resistors. The 6.3V secondary feeding the valve heaters is also connected in series with the second 6.3 V secondary (tapped at 5 V ) to provide 18 V DC for the audio IC and CIO stage via rectifier D3 and smoothing components C2, C3 and R5.

The switch in the 150 V line is very useful when testing and making adjustments. Even this voltage can produce an unpleasant shock! Resistor R4 is more of a safety device, discharging Cl when the unit is switched off. It also imposes a minimum load on the rectifier, lowering off-load peak voltages.

POWER SUPPLY UNIT

| R1 | $33 \Omega \frac{1}{2}$ | C1 | 350pF 350V |
| :---: | :---: | :---: | :---: |
| R2 | $5 k \Omega 10 \mathrm{WWW}$ | C2 | $2000 \mu \mathrm{~F}$ F 30 V |
| R3 | 1002 FW | C3 | 2000 pF 30 V |
| 184 | 22k@ 2 W | F1 | Fuse 1A |
| R5 | $33 \Omega \frac{1}{2}$ W | F2 | Fuse 250ma |

## Miscellaneous

D1/213, 1 N4007. S1, 2 pole on-off. S2, Single pole on-off, Fuseholders (2). Valveholders B7G. (2). Cable plug B76. Panel indicator lamp 6.3V. T1, Transformer $250-0-250 \mathrm{~V} 80 \mathrm{~mA}_{4} 6.3 \mathrm{~V}+6.3 \mathrm{~V}$ (Douglas MTIAT), Case $8 \times 6 \times 6 \mathrm{in}$ (H, L. Smith \& Co. Type U). RV1, voltage stabillser OA2. Speaker $6 \times 4 \mathrm{in}$. elliptical $8 \Omega$, with cable and lack plug. Speaker grill.


$$
\begin{aligned}
& 250-0-25^{\circ} \quad 80 \mathrm{mifa} \\
& 6.3^{v}-3.5 \alpha \\
& 6.3^{v}-1 \times 7 a p+25 v 2
\end{aligned}
$$

Fig. 14: Circuil of the power supply unif which provides a slabllised 150 V line plut 18 V DC for the CIO and PD bends and 6.3 V AC for the valve hestors.

The indicator lamp could be fitted to the set itself in the form of a dial light but this has never been found necessary with the 898 dial. The $100 \Omega$ resistor in the cathode side of the OA2 stabiliser is very useful as it enables the current in the OA2 to be monitored very easily. This should be around 10 mA for best regulation which means iv drop across the resistor. The important point is that OA2 should be seen to be working, by its glow, at all times. The current may be varied by changing the value of R2. Where a lower value is needed add low wattage resistors of $20 \mathrm{k} \Omega$ or so in parallel with R2, rather than changing R2 itself. The total HT current taken by the receiver is approximately 40 mA at 150 V .

The supply to the CIO stage could be stabilised by means of a zener diode but since the stage is crystal controlled this was not thought to be necessary. The various output voltages are taken to a B7G valveholder at the rear of the unit.

## CONSTRUCTION

The particular cabinet used to house the power supply unit and speaker has a pleasing appearance but there is nothing special in the choice or in the general construction. The layout can be seen in the photographs and only one or two points need any explanation.

A common bracket is used for the B7G valveholder for the OA2, mounted on long 6BA bolts, and the B7G output socket to which the various supplies are taken. Fuses, switches and the indicator lamp are fitted to the front edge of the cabinet, with twisted flex to each from the rest of the components mounted on the base plate. Make these leads of adequate length so that the cabinet can be separated from the base plate while the unit is working, for testing and checking purposes. The existing screw holes in the side of the cabinet are made into slots to facilitate this operation. When wiring any panel type fuse-holders always connect the live side of the circuit to the rear tag on the fuseholder to prevent the accidental touching of a live circuit via the fuse if it is being inserted with the fingers.

A large rectangular hole is cut in the front left hand side of the cabinet to suit the speaker chosen. This may seem a tedious job but by drilling a ${ }_{4}{ }^{2}$ in. hole in each corner and using a Mole Supercut tool it can be done in a couple of minutes. Alternatively, drill a series of small holes round the rectangle, cut between the holes with a pair of sidecutters and file clean. Yet another way is to punch a symmetrical series of holes over the area with a chassis punch such as will probably have been used to make the holes for the valveholders in the receiver. A plastic
grille over the front of the cabinet gives a professional appearance to the unit.

Initially it was the intention to mount the speaker in the receiver cabinet but since the beam deflection valve is susceptible to external magnetic fields it was thought wiser to keep the speaker's permanent magnet well out of the way!

While in the mood punch a number of holes in the base plate and at the top edge of the back of the cabinet to provide through ventilation, assisted by fixing three rubber or plastic feet to the base


Fig. 15: If the specified transformer is used the wiring of the two $6.3 V$ windings will be as shown here, for correct phasing.
plate. Slots are required in the back of the cabinet to clear the power outlet socket at the left, the speaker lead and the mains input lead.

The unit can be tested for correct output voltages before being connected to the receiver but this should be done as quickly as possible to prevent possible damage to the OA2 voltage regulator 万y being loaded ty the rectiver: If the I 18 D DC output is very low, reverse the connections to the second 6.3 V winding. If the MTIAT transformer is used the correct connections are as shown in Fig. 15. If all is well plug in the B7G plug from the receiver and continue with the alignment procedure.

The finished power unit incorporates a loudspeaker having its own lead and plug enabling it to be used with the receiver or any other audio equipment. The supply lead from the receiver plugs into the back of the cabinet.


## ALIGNMENT PROCEDURE

While a modulated signal generator is a highly desirable piece of equipment for aligning a receiver it is possible, in this design, to get adequate results without one. A $1 \mathrm{MHz} / 100 \mathrm{kHz}$ crystal calibrator would help but failing even that it is possible to use either another short wave receiver or a domestic receiver having a short wave range covering the frequency of 8 MHz . Calibration can be carried out by reference to stations of known frequency but this is a very tedious process.

When aligning a conventional superhet receiver it is customary to align the IF stages first at, say, 455 kHz and then to feed test signals into the input stages adjusting the first oscillator until calibration is correct. The oscillator will in fact be working at signal frequency $\pm$ IF frequency, depending on the design. In this receiver the single range first oscillator is calibrated directly, initially at one frequency only, 8 MHz , the rest of the calibration being done later.
low, around zero, reverse the second of the 6.3 V windings on the transformer, as noted in the section dealing with the power supply. The valve heaters should also be seen to be glowing.

Switch on the HT and check for 150 V on the HT line in the receiver. Operation of the IF gain control should increase the background noise when near maximum, least resistance. The RF gain control will have little effect at this stage. With both gain controls at zero adjust VR4 on the S-meter panel until the meter reads zero.

IF Stages. Connect a few feet of wire directly to the signal grid, pin 6 , of the mixer valve V1, turn up the gain controls and switch to AM when a babble of stations should be heard at the IF of $5 \cdot 5 \mathrm{MHz}$, the receiver in effect becoming a straight TRF. Peak the signals with the RF tuning control which should be near minimum capacity. There may be two tuning peaks but either will do. Continue to peak the
signals by adjusting the six cores in the filter and IF stages, V3 and V4. The S-meter is used as a tuning indicator for all these adjustments aiming at maximum reading. If it should reach full scale reduce the sensitivity by means of VR3 on the S -meter panel.


The cover of the power supply cabinet is removed to show the components mounted on the baseplate. The earth wire of the mains lead at the left is taken to the baseplate and the cover.
Now remove each core, one at a time, beginning at the filter, apply a spot of core locking compound or similar and replace the core adjusting for maximum signal. The object of this exercise is to ensure that the first tuning peak encountered is used since a second and incorrect peak may be found if the core is screwed in any further. Eventually the alignment should be repeated after the set is working properily in every respect. The adjustments, especially on the IFTs, will be found to be interdependent to some extent.
Calibration. The great advantage of having an IF filter of known frequency, $5 \cdot 5 \mathrm{MHz}$, is seen when the job of calibration is begun. In this design, once the low frequency end of the oscillator tuning range is established at 8 MHz the rest of the scale calibration falls into place, more or less, for both ranges, the 8 MHz point corresponding to 2.5 MHz on one range and to $13 \cdot 5 \mathrm{MHz}$ on the other. See Fig. 16.
Fit the ECC81 valve and its screen. Make quite
sure that the tuning dial and capacitor are working smoothly from end to end of the travel, that the maximum capacity coincides with $0^{\circ}$ on the dial and that the grub screws in the flexible coupling are tight. Unscrew the core (anticlockwise) in the oscillator coil L12 for minimum inductance and set trimmer capacitor TC3 to about the mid position of its travel. Set main tuning to $5^{\circ}$ on the dial, almost maximum capacity.

It is only fair to mention at this point that signals around 2 to 3 MHz can now be heard if an aerial is connected to the set and the RF tuning peaked, if only to demonstrate that all the work and expense has been worthwhile!

If another short wave receiver is available, having reliable calibration, set it for CW reception on 8 MHz and run a short wire from its aerial terminal to the vicinity of the oscillator valve V2. Run in the core of L12 until the signal is heard on the check receiver. It is now necessary to set the upper end of the range to 18 MHz , at $175^{\circ}$ on the dial. Run the dial to this point following the signal on the check receiver and adjust TC3 to give 18 MHz at $175^{\circ}$. Return to $5^{\circ}$ and readjust L 12 for 8 MHz . This sequence should be repeated until the calibration at each end is correct, then lock the core of L12 with the nut.

Intermediate points can be filled in using the check receiver or, preferably, a $1 \mathrm{MHz} / 100 \mathrm{kHz}$ crystal calibrator in conjunction with the check receiver. Use a soft pencil for marking the dial on a blank scale remembering that this calibration is for the first oscillator frequency ouly. The proper calibration can be done later for the actual tuning ranges, simply adding or subtracting 5.5 MHz to or from the oscillator frequency. For example, when the oscillator is on 12 MHz the scales will be marked $6 \cdot 5 \mathrm{MHz}$ on one and 17.5 MHz on the other, and so on. The intermediate 1 MHz points can be filled in using the crystal calibrator at the aerial input.

All calibration should be temporary at this stage, being finalised at a later date when the receiver has been in use for a while. The initial calibration was in fact adjusted to place the 14 MHz amateur band at the end of the scale.

If all else fails a domestic type short wave receiver may be pressed into service provided it can be tuned to 8 MHz but its accuracy will be highly suspect! As before, take a wire from the set to the oscillator compartment and adjust L12 core until the signal is heard. As there is no BFO on the set the signal will be heard as a rushing noise unless there happens to be at station of some sort on 8 MHz when a heterodyne whistle will be heard. This was tried using a cheap transistor portable enabling the 14 MHz amateur band to be found a little way up the dial of the 'Epsom' without any trouble at all.

The owner of a good signal generator will presumably know how to use it to align this receiver but it should be remembered that the IF response is very sharp and to ensure that the SG is always on tune its dial should be rocked back and forth across the frequency as alignment proceeds. If the modulated CW facility of the SG is used the audio output of the receiver may be monitored at the output socket with a low range AC voltmeter but the AGC line must be temporarily shorted to earth to prevent AGC action masking the effect of alignment adjustments.


## And



## OTHER CONSTRUCTIONAL ARTICLES

 AND SPËCIAL FEATURES.ON SALE IN OCTOBER

## Section 2 ofthe P.W. BUVFFf' GUIDE



## ON RECENT DEVELOPMENTS

## MICRO TV

SOLID state replacements for things like television screens and even television camera tubes have been in the wind for some time. The latest evidence seems to bring these "dreams" very much closer. A British company has won a Queen's Award for its $64 \times 64$ scanned diode array which is used in a midget television camera. An American company displayed a tiny solid state TV camera at the Paris Components Show in April this year-it was not much bigger than a packet of 20 cigarettes. Perhaps the most significant thing about the British company is not so much the $64 \times 64$ array, but that a director of the company is quoted as saying that a "substantially larger" array is currently being developed and this could compete with conventional television cameras, in terms of resolution, within two years.

## THE THYROPTER

Looking at state-of-the-art in the other type of arrays-those which emit light, the very latest from one Northern manufacturer has some intriguing possibilities. The device (no other details available) is called a Thyropter and is a light emitting diode (LED) with a built-in memory.

The construction is quite ingenious. It consists of a photosensitive junction in series with a high resistance layer plus light emitting capability. A steady voltage (about 5 V ) is applied to the device(s) and this causes a leakage current to flow. The devices are "switched" on by sending a pulse to them (about 5 V ). Once the leakage current reaches a certain level the light emitting portion starts to emit light. Because the light sensitive part is very close to the light emitting area the light from the latter shines on the high resistance layer and lower its resistance. This in turn allows more current to flow (because the resistance is now less and is in series with the current path). More current flowing causes even lower resistance and so the device switches on. This turn-on time is only about $1 \mu$ s (one millionth of a second).

Conventional arrays in a $x-y$ matrix have to be strobed and this limits their brightness. The Thyropter avoids this problem. By simply allowing less current through the device it will switch off.

Because there is a photosensitive area, light from the outside world can affect it and, if it were strong enough, switch the device on. This light would need to be about one hundred times stronger than the light from the light emitting part of the deviceremember that the light emitting part and the photo-sensitive part are extremely close (typically 20 microns).

The Thyropter is interesting if one considers the basic things it offers. We have a device which can display information optically from an electronic input. But if the Thyropter array were fed from outside (say by scanning with a laser beam), then one could feed in the information optically and (by scanning the matrix) read out electronically.

At present, the Thyropter is only at the laboratory stage and is not obtainable in any form. However, it was felt the readers might like an insight of a device which was on the horizon.

## \$51m ORDER

Speaking of the electronics industry, many people think it's going through a terrible time world wide, yet reports of orders keep coming in. GTE Sylvania Inc. has just landed an order to work on communications equipment for the US Army. The contract is valued at nearly fifty one million dollars.

## RADIATION SPARKLERS

Ever heard that diamonds are a girl's best friend? Well they're getting quite friendly with the medical profession too. The latest application for these precious morsels is as a sensor for nuclear radiation. Apparently certain diamonds are sensitive to radiation and can be used as probes. Advantages claimed are that
they have no upper limit to the dose theycan detect (in excess of $10^{9}$ Rads.) and that they are reliable and constant. Only about one diamond in a thousand is suitable, so a company has set up manufacture for a machine which sorts these diamonds. Just shows how industries get started!

## A YEN FOR WALES

Another snippet in the field of television is that a Japanese company has bought ten acres of land in South Wales to build a factory which will produce 5,000 colour television sets per month by 1976 . Some $£ 2$ million has been invested and there is mention of a 250 work force-all this within less than two years, and the factory's not even built yet!

## TOP SECRET

The science fiction fantasy of the space-age gun fighter swaggering about the cosmos with a laser on his hip has taken a step nearer reality. A laser, about the size of a cigar, has been made which has an output of one million watts peak (and that's a lot of watts no matter where it hits you!). The horrendous follow up from the manufacturer is that by increasing its size by five times, the output can be increased 250 times. No further details coz this information is top secret anyway. The work is sponsored by the US Air Force and the US Defence Department. I don't know if the US has its own Tower of London, but after this, Ginsberg will be in it (in more ways than one!).

* Our contributor, S . Ginsberg is back with us again, after a bucket and spade holiday.


## Cimbers

The Cambridge kit is the world's largestselling calculator kit.
It's not surprising - no other calculator matches the Sinclair Cambridge in functional value for money; and buying in kit form, you make a substantial saving. Now, simplified manufacture and continuing demand mean we can reduce even the kit price by a handsome $£ 12 \cdot 50$. For under $£ 15$ you get the power to handle complex calculations in a compact, reliable package - plus the interest and entertainment of building it yourself !

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With all its calculating capability, the Cambridge still measures just $4 \frac{1}{3}{ }^{\prime \prime} \times 2^{\prime \prime} \times \frac{11^{\prime \prime}}{16^{\prime}}$. That means you can carry the Cambridge wherever you go without inconvenience - it fits in your pocket with barely a bulge. It runs on ordinary U16-type batteries which give weeks of normal use before replacement.

## Easy to assemble

All parts are supplied - all you need provide is a soldering iron and a pair of cutters. Complete step-by-step instructions are provided, and our service department will back you throughout if you've any queries or problems.

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Features of the Sinclair Cambridge
*Uniquely handy package.
$4 \frac{1}{3}^{\prime \prime} \times 2^{\prime \prime} \times \frac{11^{\prime \prime}}{}{ }^{\prime \prime}$, weight $3 \frac{1}{2}$ oz.
*Standard keyboard. All you need for complex calculations. *Clear-last-entry feature.

* Fully-floating decimal point. *Algebraic logic.
*Four operators $(+,-, x, \div)$, with constant on all four.
*Constant acts as last entry in a calculation.
*Constant and algebraic logic combine to act as a limited memory, allowing complex calculations on a calculator costing less than f 15 .
*Calculates to 8 significant digits. *Clear, bright 8-digit display.
* Operates for weeks on four U16-type batteries


## A complete kit!

The kit comes to you packaged in a heavy-duty polystyrene container, it contains all you need to assemble your Sinclair Cambridge. Assembly time is about 3 hours.
Contents:

1. Coil,
2. Large-scale integrated circuit.
3. Interface chip,
4. Thick-film resistor pack.
5. Case mouldings, with buttons, window and light-up display in position.
6. Printed circuit board.
7. Keyboard panel.
8. Electronic components pack (diodes, resistors, capacitors, transistor).
9. Battery clips and on/off switch.
10. Soft wallet.

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If you just use your Sinclair Cambridge for routine arithmetic-for shopping, conversions, percentages, accounting, tallying, and so on - then you'll get more than your money's worth.

But if you want to get even more out of it, you can go one step further and learn how to unlock the full potential of this piece of electronic technology.


How ? It's all explained in this unique booklet, written by aleading calculator design consultant. In its fact-packed 32 pages it explains, step by step, how you can use the Sinclair Cambridge to carry out complex calculations.

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THE POPULAR NEW ELECTRONIC GAME


PART4

## M. J. HUGHES M A

This month we shall describe Boards C and D which carry the top and bottom base generators, bat vertical position and height generators, the vertical and horizontal ball control circuitry and the ball control logic.

## Top and Bottom Bases

The circuitry for Board C is shown in Fig. 15 and some of the more important waveforms in Fig. 14. The top and bottom bases are generated in exactly the same manner as the left and right bases, described last month. The only differences are that they are triggered from the field sync pulse and the delays involved are somewhat larger. IC 16 , connected as a monostable, sets the position of the top base relative to the field sync pulse. Ideally it should appear somewhere near the top of the screen in the final display and hence needs a delay of about 3 mS . Plenty of latitude is built in and you can adjust the position to suit your own set by means of VR7.

The output of the monostable is inverted and the rising edge from pin 6 of IC17b is differentiated by C20 and R29 to produce a spike having a width of about $200 \mu \mathrm{~S}$ at half its maximum amplitude. This is cleaned up by the Schmitt trigger, IC $17 \mathrm{~d} / \mathrm{c}$, to give a nice rectangular $200 \mu \mathrm{~S}$ pulse. Allowing for variations in component tolerances, this gives a brightening up on the screen equivalent to about 3 or 4 lines.

To increase the base height, C20 should be increased in value. This should not be necessary, as the values throughout the project have been chosen for optimum performance. However, we are mentioning these possible variations as they may help in trouble shooting or further experimentation.

The bottom base is generated in exactly the same fashion by IC18 and IC19. The only difference is that the delay is longer-hence it appears further down the screen. Final adjustment is carried out by means of VR8. Capacitor C19 decouples spikes on the logic supply rails.

## Bat Position and Height

The rest of Board C is given over to the vertical positions and heights of the two bats. We shall describe the circuitry for the left bat only; the right bat is identical in every respect.

The vertical position of the bat has to be varied by means of the front panel slider potentiometer. In this design we use an NE555 as a voltage-controlled monostable to give the variation in position, the controlling voltage being derived from the potential divider action of the front panel control, VR13. The device which performs this variable delay function is IC20.

We must ensure that the bat can overlap the top base, so the minimum delay should be in the order of 2 mS after the field sync. This is set by the components VR9, R36. R35 and C23 when the wiper of


Fig. 14: Typical waveforms for the Top and Bottom Base and Bat Verical waveform generators on Board C. The Rlght Bat waveforms are identlcal to those shown for the Left Bat.




Fig. 16: Actual size layout of Board C and location of components.

VR13 is at the 0 V end of its track. When VR13 is set to +5 V we get our longest delay and the bat is nearest the bottom of the screen. It is possible for this delay to exceed the length of a field scan, in which case the bat would appear again at the top of every second field. To prevent this happening we have a preset maximum delay, set by VR9, which limits the extent of the voltage control. We shall describe how this is adjusted later.

The height of the bat is up to the individual reader-the smaller the bat the more difficult the game. You can see from the photographs of our game the relative size we have obtained with the specified components. In any event, the duration of brightening up must be quite large to ensure that enough lines are used to define its height. It is, perhaps, more important that the height of both bats should be the same so that there is no advantage to be gained from playing on one side.

Because of these two points we have opted to generate the bat height with another monostable, IC21, instead of the simple differentiator and trigger we have repeatedly been describing. R39 sets the dwell of the monostable; increasing this value heightens the bat and vice versa. The output from IC21 describes the bat height at its desired vertical position; this has to be combined in an AND gate with the left bat width signal generated on Board B. Reference to Fig. 12 in last month's issue will show the two signals being combined in IC15b. The right bat vertical signal is similarly combined with its width in IC15a.

## Testing Board C

Following on with our usual advice we suggest you now build Board C and wire it into the subframe. Connect the field sync input to Board A and the TOP and BOTTOM BASE signals to board A and also to a pair of the unused diode inputs to board $E$. The connections to board $A$ are for the circuitry which senses coincidence between BALL and TOP or BOTTOM BASES to give a direction change signal to the ball control circuitry. The left and right bat vertical signals have to be taken to their respective pins on Board B. Finally connect VR13 and VR14 temporarily with flying leads across the 5 V power rails and take their wipers to pins 6 and 4 on Board C. Remember, of course, to connect the +5 V and 0 V rails to this board.
Now you can check the functioning of Board C. Set VR13 and VR14 to the 0V end of their travel and set VR7 and VR8 about mid-way. Apply power and tune in the television set as before. Check that the time bases are correctly set and note that all the features described last month should be displayed, except that the top and bottom bases are present and the bats appear at the top of the screen.
First adjust the positions of the top and bottom bases with VR7 and VR8. The top base should be set to cut across the centre of the bats when they are at their highest point and the bottom base should be in a symmetrical position. Now check that you can move the bats independently with their respective control potentiometers. Start with VR13 and slowly move the bat down the screen. If the bat stops before the potentiometer has reached its limit increase the value of VR7 a little and continue doing this until the bat is bisected by the bottom base when VR13 is at the +5 V end of its track. Do the same with the right hand bat.

## components list



If any of the features do not appear as specified, check the functioning of the various delay units by taking a flying lead from their outputs to the last unused diode on Board E, as described last month. A little thought and analysis should rapidly sort out the faulty zone and the fault will almost certainly be a forgotten soldered joint, a diode the wrong way round or a short caused by a blob of solder. We ought to repeat, once more, the warning that the identification marks on the NE555 timers point in the opposite direction to these on the SN7400 devices so be careful you have put these in the right way round!

## Ball Control Circuit

We will assume all is well and proceed to the board which, although the simplest to assemble, is


Fig. 17: Circuit of Board D, including the Ball Controi ramp generators and logic. S1, S2 and S3 are all biased push-buttons.


Fig. 18: Typical waveforms for Ball Control ramp generators.
the most complex to understand as it contains all the ball control logic. The complete circuitry is shown in Fig. 17 and, as can be seen, is split between the reversible ramp generators that provide the control voltages for ball movement and the logic that triggers the ramps, starts a service and ends a game when a "miss" is detected. Let's start with the ramp generators.

## Ball Ramp Generators

Both the control voltage generators are the same so we shall describe only the vertical control unit comprising IC24, an operational amplifier connected to work as a linear integrator. When the voltage at the left hand end of the input resistors, VR11 and R49, rises in a positive direction the inverting function of the amplifier chip causes the output to fall, see Fig. 18. If a voltage step is applied to the input the output will fall with a time constant set by C32 and the combination of input resistors. The lower the input resistance the faster the rate of fall. If the input is suddenly switched into a low state the operation is reversed, whatever the output voltage happens to be, and the output will rise linearly with the same time constant.

We use the signal from pin 11 of IC8 (Board A) as the input signal. This goes to a high level when BALI is coincident with TOP BASE. When this happens the collector of Trl is pulled down to zero and the output of IC24 starts its upward-going ramp. A proportion of this is tapped off from R52 and R53 and fed back to the voltage control unit of the monostable controlling the ball's vertical position (pin 5 of IC3 on Board A ). The increasing voltage of the ramp increases the delay from the monostable and the ball will move down the screen until it hits the bottom base at which time the output from pin 11 of IC8 will fall to a low level. The ramp then starts to fall and the ball rises up the screen until it hits the top base once again. We have, in effect, a complicated form of oscillator which causes the ball to move cyclically up and down the screen. The speed at which this happens is set by VR11.

At the time of switch-on it might be that the ball occurs instantaneously above the top base. If this happens there may not be a coincidence at the top of the screen and the ball would not move away from the top. This is why we have included the shorting link across the amplifier via Sla, the Ballboy switch. When it is pressed the output voltage from the ramp generator is centred and the ball is forced to a position about halfway down the screen and hence inside the controlled area.

## Ball Control Logic

The horizontal movement of the ball is controlled by coincidence signals between the ball and the left bat or left base, or the ball and right bat or right base. The logic for sensing these conditions is embodied in IC26. For example the signal at pin 11 of IC26 is RIGHT BAT or RIGHT BASE. When this is in a high condition and BALL is at level " 1 ", the level at pin 8 of the same chip will go to " 0 ". This sets a " 1 " at pin 3 and a " 0 " at pin 6 of IC27 which is connected as an RS flip flop. The low level at pin 6 is fed to the horizontal ramp generator (identical circuitry to that just described) and the output of IC25 starts to fall linearly. This is fed back to the monostable (IC5) which controls the ball's horizontal position and the ball moves from right to left across the screen. Coincidence between BALL and LEFT BAT or LEFT BASE causes a reversal of this process.

The horizontal ball speed is set by VR12. The relative vertical and horizontal speeds should be set so that there is as large a degree of randomness as possible in the ball's trajectory. Having them set at the same speed will make the ball travel at 45 degrees across the screen and it will simply precess slowly along slightly differing paths. When the unit is completed some experimentation is worthwhile to get the best effect. Again we shall repeat ourselves by pointing out that the ball's speed should not be too great otherwise the ball might cross a base line between field scans and a coincidence may not be detected. That is one reason why it is better not to make the ball too small nor the bases too narrow! If this should happen during setting up it is only necessary to increase the speed control resistor values slightly and bring the ball back into play with the Ballboy.

The other half of IC27 is a very important part of the game, called Ball Blanking. This ensures that the ball is not visible on the screen until a service is made. You must remember that, in our system, the ball is moving across the screen all the timewhether you can see it or not. We start a service by brightening up the ball when it is in coincidence with the bat or the base of the side whose turn it is to serve. When the ball misses either bat and hits the left or right base line a blanking signal is generated at pin 8 of IC27.

Let's go through a typical game and see what happens within the logic; we shall assume that the right hand player is to serve. He presses his service button (S3a) and holds it down. This puts a "l" on pin 9 of IC28c. When a RIGHT BAT or RIGHT BASE signal occurs (from pin 11 of IC26) the output at pin 8 of IC28 goes low and pin 3 of IC29 goes high. This is fed to pin 4 of IC29 and combined with the BALL signal coming into pin 5 . If the ball and base or bat signals are coincident while the service button is pressed the signal at pin 6 of IC29


Fig. 19: Actual size layout of Board D and location of components.
goes low and this forces a " 1 " at pin 8 of the Ball Blanking flip flop. This output is combined with the ball signal in AND gate IC29d, and the output signal from pin 8 of IC29 is the true BALL signal which will brighten up on the screen.
As soon as the ball appears the right hand player takes his finger off the button and the game pro-gresses-the ball stays bright because of the latching action of the ball blanking circuit. Let's say the left hand player successfully returns the ball but the right hand player misses it. What happens?

Whenever a LEFT or RIGHT BASE signal occurs, pin 3 of IC28 goes high and this is combined with the BALL signal in IC28b. When the right hand player misses the ball there is bound to be an eventual coincidence between BALL and his end base. This shows itself by the signal at pin 6 of IC28 momentarily falling to zero (we call this the Lose signal) and this resets the ball blanking flip flop thus extinguishing the ball. It should be clear that this would also have happened had the left hand player missed because the signal at pin 3 of IC28 is RIGHT BASE or LEFT BASE.

We shall not dwell on the logic any further except to draw your attention to the two series switches in the lose line feeding pin 12 of IC27. These open circuit the lose input to Ball Blanking during a service, otherwise we could get coincident noughts at both pins 12 and 9 (IC27) if the ball happened to be bouncing off the left or right base at the time. This would cause ambiguity in the logic which has to be avoided at all costs.

We expect that the lesser experienced constructor might have some difficulty in following this brief description of a fairly complex bit of logic. Do not let this put you off constructing the project, however. It is most unlikely that you will suffer faults in this region providing you are careful with your soldering.

Part 5, next month, will deal with testing Board D, final adjustments and will include inter-connection drawing for all boards and panel.

## TECHNICROSS SOLUTION NO. 6



## PW EPSOM-continued from page 527

Mixer Stage. Again, this is just a matter of a logical sequence of adjustments, easier to perform than to describe! Fit Range 5 coils in the mixer stage (highest frequency range) and set dial to the low end of the scale, about 15 MHz . Set trimmers on RF tuning gang capacitor and VC3 to about half way and RF gain control to maximum. If a signal generator is not available choose a station in the 20 m broadcast band that is fairly steady in signal strength. Set the RF tuning to about two-thirds of maximum capacity and adjust the cores in the RF coils for maximum output, using the S-meter as before


Fig. 16: Illustrating the way in which the singie range first oscillator is used to provide the calibration of the two ranges actually marked on the dial.

To check this adjustment, rock the RF tuning back and forth when two peaks of maximum signal may be noted. The adjustment should aim at making the two peaks coincident. Tune to a station at the HF end of the band, the 13 m broadcast band will do, and adjust trimmers TC1 and TC2 for maximum signal, aiming at a single peak. Check and readjust cores at the LF end, the trimmers again at HF. Tighten core lock nuts and seal trimmers. Mark the RF tuning dial at 1 MHz points corresponding to the main dial calibration.

Repeat the above procedure with pairs of RF coils for Ranges 3 and 4 and tighten lock nut on cores. Note:- adjust the cores only on these two ranges, at the LF end of each range. Do not touch trimmers TCl and TC2 again after they are aligned for Range 5, where they have most effect. The RF tuning dial calibration can be seen in the photographs.

Carrier Insertion Oscillator. With the mode switch on SSB/CW, tune in an SSB signal, on say the 20 or 80 m amateur band, and while tuning very slowly across the signal adjust trimmer TC4 on the CIO crystal for best speech quality. Try this on several stations before finding an optimum position and then seal the trimmer.

## NOTES

The 'AE Trim' control VC3 allows the input tuned circuit to be peaked for different types of aerial and will be found to be most effective at the higher frequencies. In practice the RF tuning will be found to be very sharp and can very easily be missed when the receiver will be thought to be rather dead!

There is no reason why the first oscillator circuit should not be modified to provide amateur band coverage only or particular broadcast bands, replacing the tuning capacitor, in effect, with a fixed capacitor to find the band required plus a parallel tuning capacitor. Multiband operation merely requires a multiway bandswitch, preferably ceramic or PTFE, to bring in the various combinations of capacitors. Whatever alterations are made they do not affect the RF tuning which is just peaked to the signal frequency involved.


Tr2 acts as a squarer, bias being obtained by R4. A 1 MHz square wave is available at the collector of this transistor. Whereas most crystal calibrators have used dual crystals, locked multivibrators or step counters, the availability and price of decade counter ICs makes them the obvious choice for the task of dividing this 1 MHz output by 10 and 100 . IC1 performs the first division by 10 and the 10 kHz waveform is obtained at the output of IC2 by a further division by 10.

## THE DECADE COUNTERS

As some constructors may have yet to use these devices, a few words of description is in order. These counters consist of four JK flip-flops, wired in series. Suppose, to begin with, the four outputs are at 0000 ( 0 is OFF, 1 is 0 N ). The input pulse train is connected to the clock input of the first flip-flop, each pulse in turn turning it on, then off. Thus after 10 pulses the configuration of the four flip-flops is 0101 ("New maths" people will recognise this as the binary equivalent of 10 ). A series of gates is arranged to give an output when this configuration is reached, the flip-flops are reset, and the whole process begins again.

## * components list

 calibration and tracking of brand-new amateur bat receivers leaves a lot to be desired, with 10 kHz errors at scale ends not that uncommon. Of course, the ultimate answer is a frequency counter, but this is beyond the pockets of many (author included!), so the next best solution is a crystal marker used in conjunction with a receiver. The calibrator described in this article has been found to give a reasonable output on all ranges to well over 35 MHz at 1 MHz , 100 kHz and 10 kHz intervals. The unit is simple to construct and works with a wide range of crystals and transistor gains.
## CIRCUIT DESCRIPTION

Referring to Fig. 1 the oscillator is conventional, component values having been chosen to provide stable operation with even relatively poor crystals. The trimmer TCl will pull most crystals on the high side on to the centre frequency of 1 MHz . In the event of a crystal being on the low side, some pulling will result by reducing C 2 . The method of setting up is to listen to the output of the unit on 200 kHz beating with the Droitwich transmission on 200 kHz and adjust TCl for zero beat. an


Fig. 1: above, complete circuit diagram with details of coil. In Fig. 2, below, the PCB is shown full size together with component layout.


These devices have quite a considerable highfrequency gain so that long leads and undecoupled power supplies will almost certainly result in oscillation which can easily destroy the IC. The printed circuit layout, together with C7 and C8, soldered directly to the pins and the ground plane on the underside of the board, eliminate any chance of this happening.

The operation of these devices is such that the
output of the device is not a $1: 1$ mark/space square wave. In a perfect 1:1 square wave no even harmonics are present. The spectrum of the wave form of the output of the counters is such that multiples of the 5th harmonic are weak, every 500 kHz and every 50 kHz . When calibrating receivers this point must be borne in mind as, particularly on the highest frequencies, this harmonic is quite a lot weaker than its neighbours and could be overlooked.

MANY amateur constructors regard the alignment of receivers as one of the most difficult problems they have to meet. This is especially true in the case of FM receivers where incorrect alignment can result in distortion. The Fairchild $\mu \mathrm{A} 753$ device has been specially designed for use with $10 \cdot 7 \mathrm{MHz}$ ceramic filters which avoid all alignment problems. Besides helping the amateur constructor, this also reduces labour costs for the commercial receiver manufacturer.


Fig. 1 : Pin connections for the $\mu$ A753.
The $\mu \mathrm{A} 753$ is an eight pin dual-in-line integrated circuit with the connections shown in Fig. 1. It provides an IF gain in the range 40 to 56 dB , typically 50 dB or a voltage gain of 316 at a frequency of $10 \cdot 7 \mathrm{MHz}$.

A typical circuit for the use of the $\mu \mathrm{A} 753$ is shown in Fig. 2. The output from an FM tuner is fed to one side of a $10 \cdot 7 \mathrm{MHz}$ ceramic filter and the output
from the filter is fed into pin 1 of the $\mu \mathrm{A} 753$ device. The $\mu \mathrm{A} 753$ contains three cascaded direct coupled amplifiers using emitter coupled pairs with emitter followers between stages to provide impedance matching and voltage shifts. There is overall feedback from the output of the third stage to the input. The two ceramic filters together provide all of the selectivity required in the IF stages of the receiver.

A low-level $10 \cdot 7 \mathrm{MHz}$ output is available at pin 7 with a 330 ohm output impedance. It is intended that this shall be used to provide an AGC control voltage without interfering with the output impedance at pin 5. The device incorporates an internal voltage regulator which stabilises the performance against variations of temperature and supply voltage. In addition, the $\mu \mathrm{A} 753$ provides a regulated output at pin 6 of about $7 \cdot 8 \mathrm{~V}$ at up to 10 mA which forms a suitable power supply for most types of tuner unit.

The $\mu \mathrm{A} 753$ has been designed so that a minimum number of external components are required. It can be seen that, apart from the ceramic filters, only three decoupling capacitors are required.

The output from the second $10 \cdot 7 \mathrm{MHz}$ filter is normally fed to an integrated circuit which provides further amplification followed by demodulation.

The recommended power supply voltage range for the $\mu \mathrm{A} 753$ is 10 V to 16 V with an absolute maximum voltage rating of 18 V . The power supply current

Fig. 2: Internal circuit of the $1 /$ together with basic external components




Fig. 3: Suggested FM receiver with no tuned circuitsother than those in the tuner unit.
ranges from about 11 to 19 mA . The internal power dissipation must not exceed 310 mW . The device incorporates short circuit protection for all external connections.

## Use in receivers

In one type of circuit, the output from the second ceramic filter of Fig. 2 may be fed into a circuit using the Fairchild 3075 device comprising a $10 \cdot 7 \mathrm{MHz}$ amplifier, a differential peak detector and an audio preamplifier. One tuned circuit must be employed with this device.
The writer has employed the $\mu \mathrm{A} 753$ in a simple receiver which requires no tuned circuits other than those in the tuner unit. The circuit, shown in Fig. 3, can provide excellent linęarity. A Toko ET-703UA tuner unit was used to feed a Toko CFS $10 \cdot 7 \mathrm{MHz}$ ceramic filter. Unfortunately the tuner output impedance is not ideal for this application and R1 was therefore included.

The tuner provides a gain of at least 16 dB and, although there is a loss of 6 dB in the filter, there is a further gain in the $\mu \mathrm{A} 753$. It has been found experimentally that the low-level output of pin 7 of the $\mu \mathrm{A} 753$ is quite adequate to drive the NE561B phase locked loop detector circuit. If desired, the output may be taken from pin 5 of the $\mu \mathrm{A} 753$, but an excessively large signal fed to the NE561B will reduce the rejection of amplitude modulated signals, such as car ignition noise.

The only adjustment which must be made to the circuit involves the trimmer capacitor TCl which should be adjusted so that the centre frequency of the phase locked loop is close to $10 \cdot 7 \mathrm{MHz}$. This adjustment is easily made by altering TCl to the centre of its adjustment range at which locking occurs with any correctly tuned signal. When locking occurs with a modulated signal, an audio output is obtained. A slight "plop" noise may occur as the loop comes in or out of lock.

The writer fed the output from the loop into a Sinclair "Super IC-12" audio power amplifier which was fed from the same power supply line as the remainder of the receiver. Capacitive coupling must be employed so that the steady voltage on which the audio is superimposed does not reach the input of the power amplifier. However, the recommended
circuit for the Sinclair amplifier employs an input capacitor which serves this purpose. The whole receiver provided an output which was more than adequate to drive an 8 ohm speaker at normal domestic listening levels.
In most FM receivers two CFS filters are employed to provide adequate selectivity. In some initial experiments the writer used a second CFS filter between the output of the $\mu A 753$ and the input of the phase locked loop, with a matching resistor, but the results were no better than with the circuit shown. This occurred because the phase locked loop locked on to the desired signal and further selectivity is required only to eliminate any stronger signals to which the loop might lock.

The tuner, IC and filters are obtainable from Ambit International, 37 High Street, Brentwood, Essex.

## FREQUENCY MARKER GENERATOR

from page 541

## CONSTRUCTION

Undoubtedly the simplest method of construction is to make a printed circuit, although $0 \cdot 1 \mathrm{in}$. Veroboard could be used. The author used a piece of laminate board approximately $3 \times 2 \mathrm{in}$. and a suitable layout is shown in Fig. 2. Position the components on a piece of $0 \cdot 1 \mathrm{in}$. squared paper and mark the position of the leads. Transfer this layout to the copper laminate board, by punching through the paper into the board with a sharp tool and then paint in the pattern of Fig. 2 with an etch resistant lacquer. With the board cleaned, etched and drilled the components may be soldered into position.

## OPERATION

The outputs and the 6 V supply lines have been switched so as to conserve batteries and avoid misleading pickup of the wrong output frequency. With the unit set to 1 MHz output, strong signals should be heard on a receiver. If the ICs are functioning correctly, the oscillator can then be set by switching to the 100 kHz output and using the BBC signal on 200 kHz as previously described. Current consumption should be approximately: $1 \mathrm{MHz}, 5 \mathrm{~mA}: 100 \mathrm{kHz}$ output $40 \mathrm{~mA}: 10 \mathrm{kHz}$ output, 75 mA , from the internal 6 V battery.



THERE are many audio applications where a mixing unit is invaluable, for example, tape recording or electronic music production. This unit was built as a three channel mixer although it can readily be extended for up to ten channels if required. The 741 integrated circuit used here is a high gain operational amplifier intended for general purpose applications. The basic arrangement is shown in Fig. 1. When certain theoretical conditions are satisfied the overall gain is determined exactly by the resistors R1 and R2.

$$
\text { Overall gain }=\frac{\text { output level }}{\text { input level }}=\frac{R 2}{R 1}
$$

For our circuit the gain for each channel is about two when the input gain controls are at maximum. Input impedance is $15 \mathrm{k} \Omega$ and output impedance very low.



Fig. 3: above, gives the printed circuit board actual size together with the layout of the components. The photograph below shows the completed board.


[ $\triangle \mathrm{MO2210]}$

## CIRCUIT

The 741 can work with a supply voltage up to 30 volts. A potentiometer chain to the non-inverting input biases the circuit so that the DC voltage at the input (and output) is approximately half the supply voltage. For the 18 V supply shown in the complete diagram of Fig. 2 the output terminal will have a DC bias of 9 V .

The junction $X$ forms a virtual earth mixing point for all the signals connected here. This is in effect a current (rather than voltage) mixing arrangement where the individual input currents through R1, R2 and R3 are added and produce a resultant current through R6. This means that the signal voltage at this point is very low, a few millivolts, and cannot normally be detected.

## components list

## Resistors

R1/5 $47 \mathrm{k} \Omega$ R6 $100 \mathrm{k} \Omega \cdot \mathrm{R} 7$ see text
$\frac{1}{4}$ or $\frac{1}{3}$ W 5 or $10 \%$
VR1f3 25 kQ log. potentiometers
Capacitors


Miscellaneous
IC1 8 pin DIL 741, SN72741P or similar. PCB. Case $5 \times 4 \times 3 \mathrm{in}$. or to suit. Supply terminals (2). Knobs. D1, zener diode, see text. SK1/4, jack sockets. S1/3, single pole, change over.



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IF you happen to own a Japanese made tuner, it may surprise you to learn that it would turn out to be of little use should you ever decíde to settle in the country of its origin. A look at the Japanese FM radio frequencies will explain why: they start at 80 and do not extend beyond 90 MHz so that fourfifths of the VHF band would be outside the scope of your dial More in fact, as nominally the Japanese FM band covers $76-90 \mathrm{MHz}$,

Similarly, if you plan to take a VHF set with you on a Black Sea holiday, you should be warned that while the locals on a beach in, say, Rumania, may be enjoying music from their FM radios all that you will be able to receive on yours will be a TV sound channel. Again, the VHF band used for FM broadcasting there is not the same as the familiar Band II used in the United Kingdom and elsewhere in Western Europe.

The main cause of these differences was the hasty and unorganized allocation of VHF TV channels in the 1940 's and 1950 's; FM radio, coming a few years later, in most cases had to do with what had been left. Indeed there are countries like Australia, where almost nothing has remained of the VHF band and it is hard to see how they could ever start FM radio down there without first phasing out VHF television, In South Africa, on the other hand, an extensive FM radio network has been built up before the introduction of a TV service with the result that the interference and atmospherics-rídden medium wave broadcasting in that country is to close down entirely by the end of 1974,

## DIVISIONS

Returning to Europe, FM broadcasting here is regulated by two standards, whith divíde the continent into two groups of countries roughly along the lines separating the Eurovision and Intervision TV link systems. In member countries of the European Broadcasting Union the standard adhered to is that recommended by the International Radio Consultative Committee (CCIR) with FM radio occupying, with some variations, the $87 \cdot 5-104 \mathrm{MHz}$ band. In Bulgaria, Czechoslovakīa, Hungary, Poland, Rumania and the Soviet Union, members of OIRT (Organisation Internationale de Radiodiffusion et Télévision), FM radio is allocated the 65.73 MHz band There is at least one anomaly: the German Democratic Republic, though a member of OIRT, adopted the CCIR standard at a tïme when hope still lingered

Hiat the two parts of Germany would eventually be reunited. The reasons for the division of Burope btweet two sfanfards were actually as much politif cal as organzational and tecinologica, , buf this is ino place to examine them in detall. The small differences in technical specifcations vsüch as peak deviation frequency wable etc. are net of much signifigntes etter.

## POTENTIAL DX

Pectups more inportantis the findits that here Hes an area very little explofed by long distance FM enthusiasts, although TV DXers in Britain have for some fine been achieving interesting tresults in the recêption al television Hrom Eistern Europe (Neither ts this leme strictiy geographical. Prague, for jn stance is West of Vienna) Also, the FM sound of East Earopéan TV stations on OIRT channels R4 and RS which overlay with the CCIR Band II has been occasignally recerved here during the speradic E season oi 91 毒 and sy75MHz from plures as far as Ruramia, The onnt IM radio stathoe in turn tend to may havoc at such times with the fision of UK 405 lines TV on cliannel 5 which overlase with fueir freque hcies 24 , **
The $65-75 \mathrm{MHz}_{2}$ band should offer a good oppor tupily for long distance receation as SpE opellegs on tower, trequencies rinay take place more often than those reaching into the 90 and 100s. Ron Clam, who runs a VII "observatory ineSouthern England, has recorded as entilier of events in the oIRT band between May and Aurust 1973 involviag over four hundred stations. Enreugh, to whet anystadys appetite!

## SPORADIC E

With Sporadic E, stafions most Iikely to be recelvod in Britaid are the Rolish apd Czechoslovak ones; due to the relative proximity of the fyo countries, recip: tion could be fust póssibue during periods of vert goar tivenpheric conditions, at least for those who live in the Southeast. The Pohish FM network carries all three pros ramines of the hotue service and most of the transmitters are of considerable power
In coatrast; none of the Caechosloyak transmitters are miore than 10 kW , yef coverage maps mdicates that FM signals are effectively spread over all the country with some extensigns across the borders. The location of most trapismitters on top of hills and
mountains must be helpful: the 10 kW transmitter of Králova holá, for instance, which carries two (Slovak) programmes on 68.06 and $69 \cdot 20 \mathrm{MHz}$ respectively, is situated 6500 ft a.s.l. Czechoslovakia is ideally placed for local FM DXers, being surrounded by six countries, each within reach of a sensitive tuner. Three of them broadcast in the CCIR band (East and West Germany, Austria) the other three on OIR'T frequencies (Poland, Hungary, USSR).

## TUNERS

Small wonder that there is a demand for tuners covering both bands there (as mentioned by Simon David). The Tesla T632A features two switchable front ends and the two bands appear on the scale one above the other, much like the FM and AM bands on more common tuners. On a new tuner now advertised by Tesla, the ST 100, they are placed in line so that tuning is continuous over both European FM bands. The tuners are fitted with stereo decoders, 19 kHz pilot tone system, although the proportion of stereo programmes and stereo equipped transmitters is somewhat smaller in Eastern Europe than in Britain, Germany or France. It is mostly limited to the respective 3rd programmes, broadcast on VHF only and similar in character to BBC Radio 3.
In Hungary, stereo programmes are broadcast on $69 \cdot 38 \mathrm{MHz}$ (Budapest III); in Czechoslovakia from Vltava (Czech) and Devín (Slovak) networks including Prague on 68.96, Liberec on $69 \cdot 98$ and Bratislava on 68.84 MHz . Of the six FM programmes broadcast in the Moscow area the one on $72 \cdot 14 \mathrm{MHz}$ is in stereo. But this could well be too far for any DXing; Soviet stations heard in Britain during Sporadic E are usually those in the Baltic republics, Estonia, Lithuania and Latvia, or Leningrad on $65 \cdot 93$ and $70 \cdot 42 \mathrm{MHz}$.

## EQUIPMENT

Which brings us to the crucial problem of where to get the necessary equipment without which any attempts at long distance reception on the East European frequencies are impossible. We may yet see the day when these frequencies come into use in Britain. With the crowding of IBA and BBC local stations around 97 MHz and the rest of the band reserved for public services, voices have been heard (among them that of the Editor of PW) that the lower VHF band should be allocated to FM radio, possibly after the phasing out of 405 lines television. However, many a Sporadic E season will pass before this is seriously considered.
No two-band tuners are commercially available in this country and a VHF communications receiver may prove a bit too costly, but you can build an extra bands VHF receiver for much less ( $P W$ July 1973). A good idea is a 4 m converter; radio amateurs use them, as they have a small allocation at this frequency, and there are few designs available. It should not be too difficult to adjust the IF so that the $65-73 \mathrm{MHz}$ band appears between 108 and 100 MHz on an ordinary tuner. The author is experimenting with a miniature converter design hopefully to be published in $P W$. In the meantime, do not discard the old channels 1-5 TV aerial; it may come in handy later on!

## THREE CHANNEL AUDIO MIXER-

## CONSTRUCTION

A printed circuit board, Fig. 3, was used for the prototype but a similar layout could be done with Veroboard if required. The jack sockets have insulated bodies and it is necessary to make the chassis connection for each one. The switches S1, S2 and S 3 were added so that inputs could be switched straight in at a preset level and they may be omitted if this facility is not required.


Fig. 4: Alternative power supply circuit.
The coupling capacitors C1, C2 and C3 are polyester types rated at 250 volts. Lower voltage types may be substituted. Input components up to the volume controls are mounted on the box. Extra inputs, up to a total of ten, may be connected in parallel at point $X$ and space has been allowed on the board for any extra input resistors. Space has also been allowed for a zener diode D1 and resistor R7, as shown in Fig. 4. This enables the supply to be modified, if desired, for use with an existing supply.


View inside the finished mixer unit.

## TESTING

The DC voltage at pin 6 of ICl should be checked when the unit is first switched on. If this is found to be approximately half the supply rail then the DC conditions are correct. An AC signal should now be applied to each input and the overall performance checked.

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4
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Elegance-äll af Sinclair's designleadership has beén concentrated on producing designs of outstanding functional elegance unsurpassed for styling and simplicity clexibility-
thesize and styling of Praject 80 modules makes them * the most versatile untis ever. Combine them how you will.䍃 where you will the Project 80 System of your choice gives you the best.



## technically the world's most advanced

Project 80 gives you choice from a range of 9 different modules for combining in a variety of ways to suit your requirements. The Stereo 80 is a versatile pre-amp control unit designed to meet all domestic hi-fi requirements including tape monitoring, high sensitivity magnetic cartridge input, and of course, individual slide controls on each channel for precise output matching. By separating the F.M. tuner and stereo decoder, useful economies can be effected where stereo radio reception is not needed. Two power amplifiers - Z.40 ( 18 watts RMS continuous into 4 ohms using 35 V ) and $Z .60$ ( 25 watts RMS continuous into 8 ohms using 50 V ) are available with choice of 3 different power supply units. The PZ. 8 with its virtually indestructible circuitry is particularly recommended. For the final word in system building, the Active Filter Unit puts the finishing touch of quality to what are easily the world's most technically advanced hi-fi modules. Any further units likely to be added to Project 80 range will be compatible with those already available.

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Stereo 80 Control Unit size-260:50 $20 \mathrm{~mm}\left(10 \frac{1}{2} \cdot 2 \cdot \frac{3}{4} \mathrm{nns}\right)$ Finish - Black with white indicators and transparent sliders Inputs - Magnetic Finish - Black with white 3 mV RIAA corrected: Ceramic pick-up 350 mV Radio 100 mV . pick-up 3 mV RIAA corrected: Ceramic plck-up 35 mV Radio to 15 KV .
Tape 30 mV Signal/noise ratıo -60 db Frequency range -20 Hz to 15 Hz Tape 30 mV Signal/noise ratio - 60 db Frequency range -20 Hz to 15 KHz
$1 \mathrm{~dB}, 10 \mathrm{~Hz}$ to $25 \mathrm{KHz}, 3 \mathrm{~dB}$ Power requirements -20 to 35 volts Outputs 100 mV - AB monitonng for tape Controls - Press bution tape adio and $P U$ Shders on each channet for volume bass treble $\quad$ (add fl $19 \vee \mathrm{RAT}$.) $\mathbf{E 1 1 . 9 5}$
Project 80 FM Tuner size - $85.50 \quad 20 \mathrm{~mm}$ ( $3 \frac{1}{2} \cdot 2 \cdot \frac{3}{2}$ ns ) Tuning range Dual varicap - 87.5 to 108 MHz Detector - 1 C balanced combidence One I.C. equal to 26 transistors Distortion - $02 \%$ at 1 KHz for $30 \%$ modulation 4 pole ceramic fitter in I.F section Aerial impedance $-75 \Omega$ or $240-300 \Omega$ Sensitivity -5 microvolts for $30 \mathrm{~dB} \mathrm{~S} / \mathrm{N}$ ratio Output -300 mV for $30 \%$ modulation Power requirements -25 to 35 volts f11. 5
(R.R.R.P add E1.19val)

Project 80 Stereo Decoder size -47.50-20mm (11. - 2.
 Active Filter Unit separate controls on each channel size -
 response -40 Hz to 22 KHz controls minimum Distortion - at 1 KHz - $003 \%$ using 30 V supply H.F. cut off (scratch) -22 KHz to $55 \mathrm{KHz}, 12 \mathrm{~dB} / \mathrm{oct}$ slope

 transistors Input sensitivity -100 my Output 18 watts RMS cominuous into $4 \Omega(35 \mathrm{~V})$ Frequency response $-30 \mathrm{~Hz}-100 \mathrm{KHz}-3 \mathrm{~dB} \mathrm{~S} / \mathrm{N}$ ratio -64 dB Distortion - at 10 watts into $8 \Omega$ less than $01 \%$ Power requirements -12 to

Z. 60 Power Amplifier size-55.98 15 mm ( 2 L . $3 \frac{3}{2}, \frac{3}{4}$ nns $) 12$ trans'stors Input sensitivity - $100-250 \mathrm{miV}$ Output -25 watts RMS contrnuous into $8 \Omega(50 \mathrm{~V})$ Distortion - typically $0.03 \%$ Frequency response -15 Hz to more than $200 \mathrm{KHz} \cdot 3 \mathrm{~dB} \mathrm{~S} / \mathrm{N}$ ratio - better than 70 dB Built-in protection against transient overload and short orcuiting Load impedance f 6.95 Power Supply Units Pz. 8 Stabinsed. Re-entrant current limiting makes damage from overload or even direct shorting impossible Normal working voltage (adjustable) 50 V R R P $£ 7.98$ - 79 p V A T Without mains transformer PZ. 635 V stabilised F.R P $£ 7.98-79 p$ V A T. PZ. 530 V unstabilised R R P f4-98-49pVAT

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## PRACTICAL

## October issue 25p

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$=00$ micro ann Full Scale
$\begin{aligned} & \text { ME8 }=0 \text { to } 100 \text { micro amp Full seale．} \\ &=0 \text { to } 500 \text { micro amp Fnll scat．}\end{aligned}$
ME9 $=0$ to $1 \mathrm{~m} / \mathrm{a}$ Full Scale
ME10 $=0$ to $5 \mathrm{~m} / \mathrm{a}$ Full Scale
ME11 -0 to $10 \mathrm{~m} / \mathrm{a}$ Full Scal．
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ME14 $=0$ to $500 \mathrm{~m} / \mathrm{a}$ Full Scalc．
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ohms. Size: $205 \times 110 \times 84 \mathrm{~mm}$. Sup-
plied complete with feads, crocodile Clips and steal carrying case.
OUR PRICE $£ 8.75 \quad$ P\&P $30 p$ U4312 MULTIMETER
 60/150/600mA
 accuracy $1 \%$. AC $1.5 \%$. Knife edge pointer, mirror scale- Complete with
sturdy metai carrying case, leads and
instructions. OUR PRICE $\mathbf{£ 9 . 7 5} \quad$ P\&P50p
U91 Clamp VOLT AMMETER
For measuring AC voltbreaking cirrent without Ranges: 10/25/100/250 Current: Accuracy $4 \%$. Size 283 . $x$ $94 \times 36 \mathrm{~mm}$. Complete with carrying case, leads OUR PR


KAMODEN 360 MUL TIMETER

## 

## 

TMK MOOEL 117 FET

## ELECTRONIC VOLTMETER

 Battery operated.11 Meg input 26
 $0.3-12000 \mathrm{VmC}$
$3-300 \mathrm{D}$. 3-300V RMS
$8-800 \mathrm{P}$ P.
DC current $0.12-$
12 mA . Resistence
12mA. Resistence
up to 2000MOHms. Decibels: -20 to
+51dB. Suppliad complete


TMK IDOK LAB TESTER
100,0000pv. 6\%"
scale. Buzzer
shor circuit
chack.
 opvDC. $5 \mathrm{~K} / \mathrm{VAC}$
DC Volt: $0.5 / 25$ / 10/50/250/1000V $10 / 50 / 250 / 1000 \mathrm{~V}$
$\mathrm{AC} .3 / 10 / 50 / 250 /$ $500 / 1000 \mathrm{~V}$ DC.
current $10 / 100 \mathrm{uA} / 10 /$
$10 / 100 / 500 \mathrm{~mA} / 25 / 10 \mathrm{~A}$
$10 / 100 / 500 \mathrm{~mA} / 2.5 / 10 \mathrm{~A}$. Resistence:
$1 \mathrm{k} / 10 \mathrm{k} / 100 \mathrm{k} / 10 \mathrm{Meg} / 100$ Mas ohms. $1 \mathrm{k} / 10 \mathrm{k} / 100 \mathrm{k} / 10 \mathrm{Meg} / 100$ Mag ohms,
Decibers: -10 to +49 dB . Plastic case with carrying handle. Size: $190 \times 172$
$\times 99 \mathrm{~mm}$. $\times 99 \mathrm{~mm}$.
OUR PRICE f19.95 P\&P 30p 370WTR MULTMMETER


MODEL TE15 GRIO DIP METER Transistarised. Opp
atas as Grid Dip, Oxcillator, Absorb. tion Wave'Meter and
Oscillating Detector. Oscillating Detecto
Frequency range
$440 \mathrm{kHz}-280 \mathrm{HHz}$ in six coils. 500 u meter. 9 V battery
operation, Size: operation. Size:
$180 \times 80 \times 40 \mathrm{~mm}$. OUR PRICE E19.95 P\&P 30p TRANSISTORISED L.C.R. A.C. BR/8 MEASURIN A new portable
bridge offering excellent range and ccuracy at low cost Resistance ranges: henries $\pm 2^{\circ}$ o Capacity. 6 ranges Opf-1110 mfd $=2^{21}$ Turns Ratio 6 ranges: 1:1 1000-1 11100 ted from 9 -volt battery 100 minro amp meter indication Size $77_{7^{\prime}}$ $5^{*} \times 2^{\prime \prime}$ OUR PRICE $£ 25.00$. P\&P $30 p$ TE1GA TRANSISTORISED SIGNAL GENERATOR 5 ranges, 400 kH
to 30 MHz . An
inexpensive
instrument for instrument for
the handy-man. battery. Wide easy to read
scale. 800 kH .


Modulation.
$\begin{aligned} & \text { Size: } 149 \times 149 \times 92 \mathrm{~mm} \text {. } \\ & \text { with instructions and leads. }\end{aligned}$ OUR PRICE $\mathbf{~} 8.97$ P\&P 30p MODEL TE20 RF SIGNAL


Accuracy $\pm 2 \%$. Audio
output to 8 V . Power requisments:
$105-125 \mathrm{~V}, 220-240 \mathrm{~V}$ AC. Size: 193 $105-125 \mathrm{~V}, 220-240 \mathrm{VAC}$. Size: 193
$\times 265 \times 150 \mathrm{~mm}$. Complete with test OUR PRICE f17.50 P\&P 50p TE-20D RF SIGNAL GENERATOR


Variable R F
for calibration output, Xtal socked
Brand new with 220 V a
Size $140 \mathrm{~mm} \times 215 \mathrm{~mm} \times 170 \mathrm{~mm}$ OUR PRICE $\$ 17.50^{\circ}$ P\&P 50p TE22 SINE SQUARE WAVE AUDIO GENERATOR


AC operation. Supplied brand new and leads.
OUR PRICE $\mathbf{2} 2495$
ARF 300 AF/RF SIGNAL

$220 / 240 \mathrm{~V}$ AC operation.
with instructions and leads.
OUR PRICE £37.50 P\&P 50p MOOEL MG 100 SINE SQUARE
 220.000 Hz Sine Wave 19-100,000 Hz Square Wave
Output Sine or Square wave fov P. to Ouxput Sine or Square wave 10 V P. to
Size $180 \times 90 \times 90 \mathrm{~mm}$ Operation Size $180 \times 90 \times 90 \mathrm{~mm}$ Operation
$220 / 240 \mathrm{ov}$. C .
OUR PRICE $£ 19.95 \quad$ P\&P 50p

[^2]POWER RHEOSTATS
High quality ceramic
construction. Wind-
ings embedded in
vitreous enamet.
Heavy duty brush
wiper. Continuous
rating.
Single hole fixing. $\%$ " dameter shafts.
Single hole fixing, Y" ${ }^{1} / 2$
Bulk quantities available.
25 WATT 10 25/50/100/500/1000, 2500 ohms. $\quad £ 1.15 \mathrm{~PB}$ P 10 p 50 WATT $10 / 50 \cdot 100 / 250500$ -
1500.5000 ohms £1.62 p\&P 10 p 100 W:TT $1 / 510 / 2550250500$ f7. 34 P\&P 15p CP110 CHASSIS PUNCH SET


Carefully machined top grade steel.
Contains $1 / 2^{\prime \prime}, 5 / 8^{\prime \prime} \quad 3 / 4^{\prime \prime}{ }^{\prime \prime}$ and Contains $1 / 2^{\prime \prime}, 5 / 8^{\prime \prime}, 3 / 4^{\prime \prime} 3^{\prime \prime}$ and
$11 / 8^{\prime \prime}$ punches complete with gripper OUR PRICE $\mathbf{£ 3 . 0 0 ~ P \& p 4 0 p}$ KE630 3 Station intercom


Master and two sub-stations. Can be
used on desk or wall mounted. Compused on desk or wall mounted OUR PRICE E5.25 P\&P 50p EMI LOUDSPEAKERS Model $35013 \times 8^{\prime \prime}$ with
single tweeter/erossover, single tweeter/crossover,
$20-20,000 \mathrm{~Hz}, 15 \mathrm{watt}$
RMS. Available 8 . RMS. Available 8 or
15 ohms OUR PRICE
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 your amplifier. Volume control and
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DH02S STEREO HEADPHONES


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P\&P 30p
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HANIMEX HRC 3075
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PS200 Requlated POWER
SUPPLY UNIT
Solid state. Variable
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Beatutifully made and finished in two tone ivary buff, the LE-102A I and is sutable for use as baby alarm wallor desk mounting 57 mm speaker mic gives clear 2
way conmunication with on off way communication with on off
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OUR PRICE $\mathbf{£ 3 . 9 5 \quad P \& P 3 0 p}$ TRITON 4318 PORTABLE B TRACK CARTRIDGE
PLAYER WITH MW/LW PLAYER WITH MW/LW
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FM wave
bands Slider

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HIGH QUALITY
CONSTRUCTION CONSTRUCTION KITS WE ARE
APPOINTE STOCKISTS AT Ample outpu
Operates on $9 V$ feed most amplifiers. 108 MHz . Ready battery. Covers 88 OUR PRICE for money. OUR PRICE 88.95 P\&P 20p

All kits are complete with comprehensive easy to follow instructions and Poved by full guarantee.
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GU330 Tremolo unit.
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M191 VU Meter......
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NT10 Stabilised power supply

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to4,5/75V DC, $500 \mathrm{~mA} . . . . \quad £ 9$. Amateur Electronics by Josty-Kit, -covers the subject from basic principals to advanced electronic technig-
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| T |  |
| :---: | :---: |
| AE1 100 mW output |  |
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## AMPLIFIER

Amplifier output 8 watts per $006^{\circ}$. Silicon transistors than pick-up plus radio and tape inputs, tape output and scratel filter OUR PRICE E27.50 P\&P60p.

## 38

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Excellent selectivity and sensi Avity Twin dual-varicap tuning 4 pole ceramac filter. 19 transistor separation. Distortion $02^{\circ} \cup 0 u t p u t$. Fantastic Value.
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AMPLIFIER
complete with


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| 14.55 |
| $£ 4.94$ | Add 4 channel sound to your exist package Converter splits stereo shelf speakers handles 10 watts and has $70-18,000 \mathrm{~Hz}$ performance. OUR PRICE E15.80p\&p f 1 £3 95 p \& p 50 p Model A1018

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Cambridge Ready

Buit ListE19 95 | Buit List E1995 |
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| Our Price f17 | P\&P25p. CambridgeKit Our Free

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List £4900 Our Price
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lators AE9 Treble fitter.

TE1021] Stereo Listening Station For balancing

gain controls, speakers on-off slide
switch, stereo headphone socket. OUR PRICE $\mathbf{~} 2.25$ P\&P 15 AUDIOTRONIC

## LOW NOISE CASSETTES

| TYPE | 5 | 10 | 25 |
| :---: | :---: | :---: | :---: |
| C60 | ¢1.57 | £ 3.00 | f7. 08 |
| c90 | £2.24 | £4. 25 | f10.00 |
| C120 | £2.73 | £5.17 | £12.24 |
| AUDIOTRONIC |  |  |  |
| 8 TRACK CARTRIDGES |  |  |  |
| TYPE | Each | 5 | 10 |
| 40M | 85 | £4.00 | ¢7.50 |
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| P\&P Cassettes 3p, Cartidges 5 peach OVER 10 of either POST FREE! |  |  |  |

MP7 MIXER-PREAMPLIFIER

5 Microphone
inputs each with
inputs each with
individual gain
individual gain
controls enabling

complete mixing
facilities. Battery operated. Size: 235
$\times 127 \times 76 \mathrm{~mm}$. Inputs: Mics. $\mathbf{3 \times 3 \mathrm { mV }}$ $\times 127 \times 76 \mathrm{~mm}$. Inputs: Mics. $3 \times 3 \mathrm{mV}$
$50 \mathrm{k} ; 2 \times 3 \mathrm{mV} 600$ ohms. Phono. Mag.
$4 \mathrm{mV} 50 \mathrm{k} ;$ Phono Ceramic 100 mV . 4 mV 50k; Phano Ceramic
Meg Output 250 mV 100 k . OUR PRICE £8. 97

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Stereo Headphone Amplifier

## All silicon, transistor

amplifier oper-
ates from mag
netic, ceram
or tuner

inputs with
twin stereo headphone outputs and separate volume controls for and
channtel. Operates from 9 V battery INPUTS: 5 mV and 100 mV
OUTPUT: 50 mV per channel.
OUR PRICE E8.50 P\&P 30p

## Alsn sea prexidus page

$A$ II $\rightarrow$ B $B$ EXCLUDE VAT

CLEAR PLAS

*Items with asterisk are Moving Iron type, all others are Moving Coil
CLEAR PLASTIC MODEL SD830
Size $110 \times 83 \mathrm{~m}$

\section*{EDGWISE MODE <br> 


CLEAR PLASTIC MODEL MR 38p

## Size: $42 \times 42 \mathrm{~mm}$

| 50 A | £3:0 |  |  |
| :---: | :---: | :---: | :---: |
| 1000 A | £305 |  |  |
| 200 uA | f300 |  |  |
| 5004 A | £285 |  |  |
| 50.0504 A | £305 |  |  |
| 100.0-100uA | f300 |  |  |
| $500-0-500 \mathrm{uA}$. | f2 80 |  |  |
| 1.0 .1 mA . ${ }^{\text {a }}$ | f2 80 F280 |  |  |
| 2 mA | £2 80 |  |  |
| 5 mA | 1280 |  |  |
| 10 mA .. | E280 |  |  |
| 20 mA | f2 80 |  |  |
| 50 mA | +280 | 20 V DC | ¢280 |
| 100 mA | f2 80 | 50 V DC | f2 80 |
| 150 mA | £2,80 | 100 V DC.. | f2 80 |
| 200 mA | f2 80 | 150 V DC .. | £280 |
| 300mA | ¢280 | 300 V DC | f2.85 |
| 500 mA | ¢280 | 500 V DC | ¢285 |
| 750 mA | ¢ 280 | 750 V DC.. | ¢290 |
| 1 ADC | f280 | 15 VAC | ¢290 |
| 2 ADC | E280 | $50 \cup A C$ | E2.90 |
| 5ADC | $\pm 280$ | 150 V AC | $\pm 290$ |
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| 3 VDC | f2 80 | 500 V AC | $\pm 300$ |
| $10 \vee D C$ | f2 80 | S Meter 1 mA .. | £280 |
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| :--- | ---: |
| 27 TOTTENHAM CI. RD. | $01-6363715$ | $\begin{array}{lll}33 \text { TOTTENHAM CI. RD. } & 01-6362605 \\ 42.45 \text { TOTTENHAM CT. RD. } & 01.6360845\end{array}$

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POSTAGE \& PACKING 15p


## NEW from A.S.P. "SPLASH PROOF" <br> SAFETY TRANSFORMER

750 VA Isolation Unit (Interwinding Screen) Housed in a tough Fibreglass case, with carrying handle. Complete with Heavy Duty 3 core power cable splash proof outlet plug and socket, internal fuse. 110 Volt and 240
versions available. Price 220.20.

## $2^{\prime \prime}$ and $\mathbf{4}^{\prime \prime}$ PANEL METERS $2^{\prime \prime}$

## SIZE: 60 mm Wide SIZE: 110mm Wide

 $\times 45 \mathrm{~mm}$ High $\times \times 82 \mathrm{~mm}$ High $\times$ M0rma Deep.Movement I.R. Movenent $0-50$ micro $A$ Ohms ORS $\begin{array}{lrl}0-100 \text { micro A. } & \mathbf{1 2 5 0} & \mathbf{5 8 0} \\ 0-100 \mathrm{micro} A . & 1400 \\ 0-100\end{array}$ $\begin{array}{llll}0-500 \text { miero A. } & 170 & 0-100 \text { micro A. } & 780 \\ 0-500 \text { micro } A . & 200\end{array}$ $0-1 \mathrm{~mA} \quad 170 \quad 0-1 \mathrm{~mA}$ $\begin{array}{lrr}0-6 \mathrm{~mA} & 170 & 0-5 \mathrm{~mA} \\ 0-10 \mathrm{~mA} & 6 & 0-10 \mathrm{~mA}\end{array}$ $\begin{array}{lll}0-10 \mathrm{~mA} & 6 & 0-10 \mathrm{~mA} \\ 0-50 \mathrm{~mA} & 0.5 & 0-50 \mathrm{~mA}\end{array}$ $0-100 \mathrm{~mA}$
$0-10$
$0-500 \mathrm{~mA}$
0
$0-1$ AMP
0-2 AMP
$0-25$ Volt
$0-300$ Volt
"g" Meter
V0 Meters are com
Modern wide view.
Pr 25 Post 10p. Price $4^{\prime \prime \prime}$. $\mathbf{£ 3 . 9 5}$ Post 10 n Lamps 55 p per set.

## $\frac{1}{4}$ watt CARBON FILM RESISTORS

$\frac{1}{2}$ watt at $70^{\circ} \mathrm{C}$ E 12 range $10 \Omega-1 M \Omega 5 \%$
tol above $470 \mathrm{~K} \Omega$ 10\% tol at 95p per 100

## ELECTRONIC MAINS TIMER

A rellable unit id

## Ventilators

Stairway/
Cloakroom
Lighting etc.
Gives up to 30
mins delny before
ewitching off.
Delay
adit
Delay 1-30 mins.
resistive. White Case 3 an $^{\prime \prime} \times 3^{\prime \prime \prime} \times 2^{\prime \prime}$ ur 1000 watts instructions meluded.
Trade Price $85 \cdot 80$. Post 20 p .


## TRANSFORMERS

## SAFETY ISOLATING

Prim. 120/240V. Sec. 120/240V. Centre Tay with screen.

| VA (watts) | $\begin{aligned} & \text { Ret. } \\ & \text { No. } \end{aligned}$ | Cosed | Open | $\begin{gathered} \text { Post } \\ \dot{4} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| 60 | 149 | - | 48.74 | 0.38 |
| 100 | 150 | - | 4.16 | 0.02 |
| 200 | 151 | 48-48 | 7.48 | 0.52 |
| 250 | 152 | 18.06 | 9. 57 | 0.65 |
| 350 | 158 | 14.00 | 11-44 | 0.80 |
| 500 | 154 | 16.80 | 18.20 | $2 \cdot 00$ |
| 1000 | 156 | 80-70 | 87-46 | 1.20 |
| 2000 | 158 | 80.85 | 55.45 |  |
| 3000 | 159 | 79.88 | 78.49 |  |

12 \& 24 Volts Prim. 200-240v.

| ${ }_{12 \mathrm{~V}}^{\text {Amps }}$ | 24V | Ref. No. | Price | Post |
| :---: | :---: | :---: | :---: | :---: |
| 0.3 | 0.15 | 242 | 1.34 | 0.22 |
| 0.5 | 0.25 | 111 | 1.84 | 0.22 |
| 1 | 0.5 | 218 | 1-50 | 0.23 |
| 2 | 1 | 71 | 2.00 | 0.22 |
| 4 | 2 | 18 | 8.75 | 0.88 |
| 6 | 8 | 70 | 8.58 | 0.42 |
| 8 | 4 | 108 | $8 \cdot 98$ | 0.52 |
| 10 | 5 | 72 | 4.67 | 0.62 |
| 12 |  | 116 | 6.07 | 0.62 |
| 16 | 8 | 17 | 6.64 | 0.62 |
| 20 | 10 | 115 | 10.88 | 0.69 |
| 30 | 15 | 187 | 18.75 | 0.97 |
| 40 | 20 | 232 | 18.28 | 1.00 |
| 60 | 30 | 226 | 22.62 | $1 \cdot 10$ |
| 30 Volts |  |  |  |  |
| Prim. 200-240V. Sec. 12, 15, 20, 24, 80V. |  |  |  |  |
| Amps |  |  | Price | Post |
|  |  |  | ${ }_{1}^{1.68}$ | ${ }_{0}$ |
| 0.5 |  |  | 1.68 | 0.22 |
| 1 |  |  | $2 \cdot 20$ | 0.38 |
| 2 |  |  | 8.19 | 0.38 |
| 3 |  |  | 8.98 | 0.42 |
| 4 |  |  | 4.68 | 0.52, |
| 5 |  |  | 5.80 | 0-62 |
| 6 |  |  | 6.98 | 0.52 |
| 8 |  |  | 9.00 | $0 \cdot 67$ |
| 10 |  |  | 10.00 | 0.67 |

AUTO TRANSFORMERS
Cased vereions are 240 Volt Mains to 115 Volts, smart steel cased units coated in tough resin with power lead, above 500 VA cable entry.

| VA (Watts) | Ref. No. | Price Cased 2 | Price Open 2 | Post |
| :---: | :---: | :---: | :---: | :---: |
| Tapped at 115, 200, 220, 240 Volts |  |  |  |  |
| 20 | 113 | ¢2.52 | 1.82 | 0.30 |
| 75 | 64 |  | $2 \cdot 68$ | $0 \cdot 30$ |
| Tapped at 115, 220, 240 Volts |  |  |  |  |
| 150 | 4 |  | 3.29 | 0.39 |
| 200 | 65 | $5 \cdot 58$ | 3.96 | 0.40 |
| 300 | 66 |  | 4.64 | 0.62 |
| 500 | 67 | $9 \cdot 50$ | 8.08 | 0.67 |
| 1000 | 84 | 15.82 | 18.50 | 0.82 |
| 2000 | 95 | 29.70 | 25.30 | 1.50 |
| 3000 | 73 |  | 38-00 | 1.20 |

PLEASE ADD 8\% FOR V.A.T.

50 Volts
Prim. 200-240V.
See. 19, 25, 83, 40, 507

| Amps | Ref. | Price | Post |
| :---: | :---: | :---: | :---: |
|  | No. | $£$ | $\mathcal{L}$ |
| 0.5 | 102 | 2.11 | 0.30 |
| 1 | 103 | 3.08 | 0.38 |
| 2 | 104 | 4.29 | 0.42 |
| 3 | 105 | 5.77 | 0.52 |
| 4 | 106 | 7.48 | 0.52 |
| 6 | 107 | 11.00 | 0.67 |
| 8 | 118 | 14.19 | 0.97 |
| 10 | 119 | 17.60 | 0.97 |

MINIATURE AND EQUIPMENT

| Prim. 840V with screen. Volts |  | Milliamps |  | Ref. No. | $\begin{gathered} \text { Price } \\ \hline \end{gathered}$ | $\underset{\mathbb{E}}{\text { Post }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sec. 1 | Sec. 2 | Sec. 1 | Sec. 2 |  |  |  |
| 3-0-3 | - | 200 | - | 238 | 1.28 | $0 \cdot 10$ |
| 0-6 | 0-6 | 500 | 500 | 234 | 1.80 | $0 \cdot 10$ |
| 0-6 | 0-6 | 1000 | 1000 | 212 | 1.08 | 0.22 |
| 9-0-9 |  | 100 | , | 13 | 1.28 | 0.10 |
| 0-9 | 0-9 | 330 | 330 | 235 | 1.48 | $0 \cdot 10$ |
| 0-8-9 | 0-8-9 | 500 | 500 | 207 | 8-28 | $0 \cdot 23$ |
| 0-8-9 | 0-8-9 | 1000 | 1000 | 208 | 8.08 | 0.30 |
| 15-0-15 | - | 40 | - | 240 | 1.28 | $0 \cdot 10$. |
| 0-15 | 0-15 | 200 | 200 | 236 | 1.80 | $0 \cdot 10$ |
| 20-0-20 | - | 30 | - | 241 | 1.83 | 0.10 |
| 0-20 | 0-20 | 150 | 150 | 237 | 1.80 | 0.10 |
| 0-15-20 | 0-15-20 | 500 | 500 | 205 | 2.97 | $0 \cdot 38$ |
| 0-20 | 0-20 | 300 | 300 | 214 | 1-76 | 0.22 |
| 0-20 | - | 3500 NO | SCREEN | 1116 | 3.00 | 0.40 |
| 20-12-0-12-20 | - 0 | 700 (D/C) |  | 221 | I. 65 | $0 \cdot 30$ |
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The versatility of their design makes them ideal for use in record players, tape recorders, stereo ampliners and casette and
tape players in the car and at home.

| Farameter | Conditions | Performance |
| :---: | :---: | :---: |
| HARMONIC DISTORTION | $\mathrm{P}_{0}=3$ WATTE $\mathrm{f}=1 \mathrm{KHz}$ | 0.25\% |
| LOAD IMPEDANCE | - | 8-16 $\Omega$ |
| INPUT YMPEDANCE | $1=1 \mathrm{KHz}$ | $100 \mathrm{k} \Omega$ |
| FREQUENCY RESPONSE $\pm$ 3dB | Po=2 WATTS | $50 \mathrm{~Hz}-25 \mathrm{KHz}$ |
| SENEITIVITY for Rated O/P | $\mathrm{Vs}=25 \mathrm{~V} . \mathrm{Rl}=8 \Omega \mathrm{f}=1 \mathrm{KHz}$ | 75 mV . RMS |
| DIMEAEIONS | - . | $3^{\prime \prime} \times 2 \mathbf{2}^{\prime \prime} \times 1^{\prime \prime}$ |

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences modules. The fin their working conditions.

| Parameter | AL10 | AL20 | AL30 |
| :---: | :---: | :---: | :---: |
| Maximum Supply Yoltage | 25 | 30 | 30 |
| Power output for 2\% T.H.D. <br> (RL $=8 \Omega f=1$ K Kz) | 3 watts <br> RMS Min. | 5 watts <br> RMS Min. | 10 watts <br> RMS Min. |

## AUDIO AMPLIFIER

 MODULESAJ. 10. 8 watts
AL 20. 5 watts

## POWER SUPPLIES

Pg 12. (Use with AL20, AL20, AL30) 880 GPM 80. (Uee with AL60) FRONT PANELS SP 12 with Knob

## PRE-AMPLIFIERS

 PA 12. (Use with AL10 $\&$ AL20) $\pm 4.35$PA 100.
(Use with AL30

## TRANSFORMERS

T461 (Use with ALl0) $\$ 1.38 \mathrm{P} \& \mathrm{P}$ 15p T538 (Use with AL20, AL30)
BMT80 (Use with AL60) $£ 2.15$ P \& $\&$ P 25 P

## PA 12. PRE-A MPLIFIER SPECIFICATION

The PA 12 pre-amplifier bas been designed to match into most budget stereo systems. It is compatible with the AL 10 , AL 20 and AL 30 audio power ampliders and it can be supplied from their associated power supplies. There are two siereo inputs, one has been designed for use with *Ceramic cartridges while the auxiliary input will wuit moat †Magnetic oartridges. Full details are given in the specification table. The four controls are, from left to right: Volume and on/ofl switch, balance, bass and treble. Frequency response-
$20 \mathrm{~Hz}-60 \mathrm{~K} \mathrm{~Hz}(-3 \mathrm{~dB})$
Bas controlBass control-
Treble control*Input $\stackrel{ \pm}{\text { i. }} 14 \mathrm{dmp}$ at $14 \mathrm{KHF}_{2}$ *Input 1. Impedance Sensitivity 300my $\dagger$ Input 2. Impedance 30 K ohms
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## Treble con. $\pm 14 \mathrm{~dB}$ at 14 kBz

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OK-100K $\Omega$ Single Gang
$0 \mathrm{~K}-100 \mathrm{~K} \Omega$ Dual Gang
KNOBS for above Black or Silvered 40

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iA 100 V A 200 V
A 600 V
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MYLAR FIL CAPACITORS
$100 \mathrm{~V}: 0.001 \mu \mathrm{~F}, 0.00 \mu \mathrm{~F}, 0.005 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}$, 100V: $0.1 \mu \mathrm{FF}, 0 \cdot 2 \mu \mathrm{~F}, 50 \mathrm{~V}: 0.47 \mu \mathrm{~F}$ 6p.
PRESET POTENTIOMETERS $\begin{array}{ll}0.25 W \\ 0.1 \mathrm{kS} & 1 \mathrm{M} \Omega \text { Hor, and Vert. } \\ 0 \mathrm{p} \\ 0.1 \mathrm{MEG} \Omega & \text { Vert. only } \\ \text { ip }\end{array}$
KNOES (To fit $t^{\prime \prime}$ shaft)
KNOBS (To fity
Black Pointer Type
Black Pointer Type
Sim Silvered Aluminium
$\qquad$
RESISTORS High Stability, Iow nolse
 $\begin{array}{llll} \\ 4 W & W W & 1 \Omega R-100 \Omega & E 12 \\ \text { Type: } \\ \text { C } 5 \% & \text { carbon Film miniature sil }\end{array}$ Type: $\mathrm{C} 5 \%$ carbon Film mi
WW $10 \%$ Wire Wound SWITCHES Toggle SPST Slide $\frac{1}{5} A$ D.P. sub-min. 120 V Slide 1 A D.P. 250 V
Push Button min. P/M or P/B Rotary Wavechange 1 pole 12 way, 2p/6w, 3p/4w, 4p/3w

JACK PLUGS (chrome) SOCKE Stereo Screened 30p Stereo $\begin{array}{lll}\text { Stereo Screenad } & 30 \mathrm{p} & \text { Stereo } \\ 2.5 \mathrm{~mm} \text { Screened } & 10 \mathrm{p} & 2.5 \mathrm{~mm}\end{array}$ 3.5 mm Screened $14 \mathrm{p} \quad 3.5 \mathrm{~mm}$ DIN PLUGS, SOCKETS \& COUP Plugs, 12p; Sockets, 8p; Couplers, 10p Coaxial Plugs, 10p; Sockets, 8p PHONO PLUGS, SOCKETS \& COUPLERS Assorted Coloured Plugs: $\mathrm{sp}_{1}$ COUPLERS: ip, SOCK
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## AC/DC MULTIMETER TYPE U4324



33 ranges up to 3 Amps AC/DC; 1200 V DC, 900 V $\mathrm{AC}, 500 \mathrm{k} \Omega,+12$ db .
Sensitivity:
20k $\Omega / \mathrm{V} D C$;
$4 \mathrm{k} \Omega / \mathrm{V} A C$
Accuracy:
$\pm 2.5 \%$ DC;
$\pm 4 \%$ AC

Movement is protected by silicon diodes.
Dimensions $167 \times 98 \times 63 \mathrm{~mm}$. Weight: 1.5lb.

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## MULTIMETER TYPE U4323

Sensitivity: 20,000 $2 / \mathrm{V}$


7 D.C. Voltage ranges $0.5-1000 \mathrm{~V}$ 6 A.C. Voltage ranges $2 \cdot 5-1000 \mathrm{~V}$ 5 D.C. Current ranges $0 \cdot 05-500 \mathrm{~mA}$ 4 Resistance ranges $1 \mathrm{k} \Omega-1 \mathrm{~m} \Omega$ Built-in oscillator providing AF output of 4 kHz and I.F. output of 465 kHz with an amplitude of 1 volt minimum.
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$2^{\prime} \times 12^{\prime \prime}$ Cabinet

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PRICE \& TYPE LIST

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