#  

## THE POPULAR NEW ELECTRONIC GAME


pLayed on the television screen


ALSOR
THE SEVERYY 4-BAND PORTABLE GENERAL PURIOOE PREAMPLIFER


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| :--- | ---: | :--- | :---: | :--- | :--- |
| DY86 | 20p | PCF80 | $6 p$ | PY82 | $10 p$ |
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| application. |  |  |  | PC86 | 0.75 |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | PC88 | 0.76 |
| DM70 | 0.68 | EFP0 | 0.48 | PC97 | 0.46 |
| D 7 P1 | 0.86 | EF83 | 1.08 | PC900 | 0.58 |
| DY88/7 | 0.42 | EF85 | 0.43 | PCC84 | 0.58 |
| DY802 | 0.46 | EF88 | 0.90 | PCC88 | 0.80 |
| EABC80 | 1.00 | EF89 | 0.81 | PCC89 | 0.85 |
| EB01 | 0.83 | EY01 | 1.80 | PCC188 | 0.65 |
| [ BC 1 | 0.76 | EF92 | 1.40 | PCF80 | 0.51 |
| EBF80 | $0 \cdot 60$ | EF95 | 1.86 | PCF82 | 1.80 |
| EBF89 | 0.68 | EF183 | 0.80 | PCF86 | 0.85 |
| EBF80 | 0-58 | EF184 | 0.60 | PCF200 | 0.85 |
| EC88 | 0.75 | EH90 | 0.60 | PCF201 | 0.87 |
| EC88 | 0.77 | EL34 | 0.88 | PCF801 | 0.85 |
| ECC81 | 0.45 | EL36 | 1.08 | PCF802 | 0.71 |
| ECC82 | 0.48 | EL81 | 000 | PCF806 | 0.68 |
| ECC8s | 0.46 | EL84 | 0.47 | PCH200 | 0.88 |
| ECC84 | 0.85 | EL85 | 0.85 | PCL82 | 0.84 |
| HCCss | 0.68 | EL8 ${ }^{\text {a }}$ | 0.85 | PCL83 | 0.68 |
| ECC88 | 0.75 | EL95 | 0.70 | PCL84 | 0.68 |
| ECCl ${ }^{0}$ | 0.71 | EL91 | 1.81 | PCL85 | 083 |
| ECF80 | 056 | ELL80 | 1.80 | PCL86 | 0.68 |
| ECF82 | 0.78 | EM84 | $1 \cdot 18$ | PCL805/85 |  |
| ECF8 8 | 0.71 | EM87 | 1.18 |  | 0.88 |
| ECH81 | 1.00 | EYB1 | 0.88 | PD500 | 1.55 |
| ECH83 | 1.00 | EY86/87 | 0.42 | PFL200 | 0.80 |
| ECH86 | 0.78 | EY88 | 0.84 | PL36 | 0.88 |
| ECL80 | 0.68 | EZ80 | 0.51 | PL81 | 0.75 |
| ECL82 | 0.81 | EZ81 | 0.40 | PL81A | 0.88 |
| ECL83 | 0.88 | GY501 | 0.80 | PL82 | 0.50 |
| ECL88 | 0.68 | GZ34 | 0.78 | PL83 | 0.98 |

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Individually boxed and guaranteed but of European or other origin at greatly reduced prices. Quotations for any valve not listed. Send SAE for lists.

| ME界 ( A M E |  |  |  |  |  | BP4 11 SP61 | $\begin{aligned} & 8.00 \\ & 0.75 \end{aligned}$ | 6J6 <br> 6J7M | 0.80 0.45 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | T41 | 100 | 6J 76 | 0.40 |
| Individually boxed and |  |  |  |  |  | U14 | 1.00 0.85 | 6K6GT | 0.75 |
| guaranteed but ot Euro- |  |  |  |  |  | U25 | 0.85 0.85 | 6K7M | 0.45 0.30 |
|  |  |  |  |  |  | U191 | 0.75 | 6 K 8 M | 0.70 |
| pean or other origin at |  |  |  |  |  | UABC80 UAF49 | 0.40 0.75 | ${ }_{6}^{6 \mathrm{~K} 8 \mathrm{O}}$ | 0.45 0.75 |
| greatly reduced prices. |  |  |  |  |  | URC41 | 0.75 | ${ }^{6 \mathrm{LEGG}}$ | 0.55 |
| Quotations |  |  |  |  |  | UBCA] | 0.45 0.40 | 607M | 0.50 |
|  |  |  |  |  |  | UBF89 | 0.40 | 6 SLTGT | 0.50 0.48 |
| valve not listed. Send |  |  |  |  |  | UCC85 | 0.45 | 68N70T | 0.48 |
|  |  |  |  |  |  | UCH 42 | 0.75 | 68Q70T | 0.50 |
|  |  |  |  |  |  | UCL82 | 085 | BYBG | 0.75 040 |
|  |  |  |  |  |  | UCL83 | $0-70$ | 6V6at | 046 |
|  |  |  |  |  |  | UF41 | 0.75 | $6 \times 4$ | 0.40 |
| Az33 | 0.55 | EF85 | 0.85 | PC88 | 080 | UF89 | 0.40 | $6 \times 50$ | 0.40 |
| CBL31 | 1.20 | EF86 | 0.80 | ${ }^{P} \mathrm{C} 97$ | 0.50 | UL41 | 0.88 | 6 X 5 GT | 0.45 |
| CL33 | 1.50 | EF89 | 0.28 | PC900 | 0.48 | UL84 | 0.48 | $7 \mathrm{B6}$ | 0.75 |
| CY31 | 0.50 | EF91 | 0.87 | PCC84 | $0 \cdot 40$ | UY41 | 0.48 | $7 \mathrm{B7}$ | 0.70 |
| DAF91 | 0.80 | EF9* | 050 | PCC88 | 0.55 | ${ }^{1} \mathrm{Y} 85$ | 0.40 | $7 \mathrm{C5}$ | 1.30 |
| DAF96 | 0.50 | EF95 | 0.40 | PCC89 | 0.50 | VR105-30 | 0.40 | 7 C 6 | 0.75 |
| DCC60 | 1.85 | EF98 | 0.75 | PCC189 | 0.60 | VR150-30 | 0.40 | 7H7 | 0.70 |
| DF91 | 0.80 | EF183 | 0.80 | PCF80 | 0.80 | OA2 | 0.40 | 7 R 7 | 0.75 |
| DF96 | 0.50 | EF184 | 0.35 | PCF82 | 0.36 | OB2 | 0.40 | 787 | 2-25 |
| DK91 | 0.45 | EL32 | 0.60 | PCF86 | 0.60 | 1R5 | 0.45 | 7 Y 4 | 0.75 |
| DK92 | $0 \cdot 70$ | EL33 | 1.75 | PCF801 | 0.50 | 185 | 0.80 | 12ATE | 0.40 |
| DK96 | 0.60 | EL34 | 0.80 | PCF802 | 080 | IT4 | 080 | 12 AT 7 | 0.40 |
| DL92 | $0 \cdot 40$ | EL36 | 050 | PCF805 | 0.90 | 384 | 0.40 | 12AU6 | 0.45 |
| DL94 | 0.48 | EL37 | 2.50 | PCF806 | 0.75 | $3 \vee+$ | 070 | 12AU7 | 0.88 |
| DL96 | 0.55 | ELI | 0.00 | PCF808 | 0.90 | 8R4GY | 0.80 | 12AX7 | 0.88 |
| DY86/\% | 0.38 | EL42 | 080 | PCL82 | $0 \cdot 36$ | 5046 | 0.40 | 12BAB | 0.45 |
| DY802 | 0.87 | EL84 | 0.28 | PCL83 | 068 | 5) 4 G | 0.50 | 12BE6 | 050 |
| EABC80 | 0.88 | EL95 | 040 | PCL84 | 0.45 | 5 Y 3 CT | 0.46 | 30 Cl | 0.80 |
| EAF42 | 0.75 | ELL80 | 1.00 | PCL85 | 0.60 | 5 ZaG | 0.46 | 30 Cl 5 | 1.05 |
| EB91 | 0.28 | EM80 | 0.45 | PCL86 | 0.45 | 6/30L2 | 0.80 | 30 Cl 7 | 1.10 |
| EBC38 | 1.00 | EM81 | 0.80 | PCL805/85 |  | $6 \mathrm{AK5}$ | 0.40 | 30 Cl 18 | 0.90 |
| EBC41 | 0.75 | EM84 | 0.35 |  | 0.50 | 6AMS | 0.80 | 30 F 6 | 1.10 |
| EBC81 | 0.88 | EM85 | 1.00 | PD500 | 1.80 | 6AQS | 0.45 | 30 FL 1 | 0.80 |
| EBF80 | 0.40 | EY51 | 0.40 | PEN45 | 0.75 | 6AB7G | 085 | 30FL2 | 0.75 |
| EBF83 | 0.40 | EY86 | 0.40 | PL36 | 0.55 | 6AT6 | 0.45 | $30 \mathrm{FL14}$ | 0.80 |
| EBF89 | 0.92 | EZ40 | 0.75 | PL81 | 0.50 | 6AU6 | 0.80 | 30L15 | 1.05 |
| ECCB1 | 1-50 | EZ41 | 0.75 | PL82 | 0.45 | 6BA5 | 0.28 | 30 L 17 | 0.85 |
| ECC83 | 0.88 | GYb01 | 0.90 | PL500 | 0.75 | ${ }_{\text {6BJ6 }}^{\text {6BE6 }}$ | 0.75 | 30 P 12 | 1.05 |
| ECC84 | 0.80 | GZ30 | 0.45 | PL504 | 0.75 | 6BQ7A | 0.55 | 30P19 | 100 |
| ECC8s | 0.40 | GZ32 | 0.50 | PL608 | 0.80 | 6BR7 | 1.00 | 30PL1 | 0.85 |
| ECC88 | 0.40 | GZ34 | 0.65 | PL609 | 1.55 | 6BE7 | 1.85 |  |  |
| 6CH35 | 1-25 | GZ37 | 1.25 | PL802 | 0.95 | 6BW6 | 0.00 | $30 \mathrm{PL13}$ | 1.20 |
| ECH42 | 1.00 | HN309 | 1.50 | PX4 | 3.50 | 6BW7 | 0.00 | 30PL14 | 1.25 |
| ECE81 | 0.80 | KT61 | 1.75 | PX25 | 3.50 | 6C4 | 0.35 | 35W4 | 0.50 |
| ECH83 | 0.45 | KT66 | 2.50 | PY33 | 0.68 | 6 CDGG | $1 \cdot 30$ | 35 Z 40 T | 0.70 |
| ECL80 | 0.55 | KT81 |  | PY81 | 0.50 | 6CH6 | 1.40 | 80CD6G | 1.20 |
| ECL82 | 0.85 |  | $1 \cdot 30$ | PY82 | 0.85 | 6CW4 | 1.00 |  | 1.20 |
| ECL83 | 0.70 | KT81 | 1.75 | PY83 | 0.88 | 6F23 | 1.05 | 807 | 0.50 |
| ECL86 | 0.40 | KT88 | 2.90 | PY88 | 0.40 | 6F25 | 1.00 | 813 IT | 118 |
| ECLI 800 | 3.20 | KTW61 | 1.00 | PY500 | 1.05 | 6F28 | 0.70 | 813 UBSE |  |
| EF37A | 1.20 | MU14 | 1.00 | PY81800 | 0.50 | 6 5 M | 0.65 |  | 45.75 |
| EF39 | $1 \cdot 20$ | N 7 R | 2.75 | PYR01 | 030 | ¢J5 5 | 0.45 | Rbinat | 1.00 |


| PL84 | 0.86 | 30C15/ |  |
| :---: | :---: | :---: | :---: |
| PL504 | 0.88 | PCF800 | 1.05 |
| PLL608 | 1.05 | 30 Cl 7 | 1.00 |
| PL509 | 1.55 | 30C18 |  |
| PL802 | 0.96 | PCF805 | 0.90 |
| PY33 | 0.68 | 30F5/PF8 | 18 |
| PY81/800 | 0.50 |  | 1-10 |
| PY82 | 0.55 | $30 \mathrm{FL1} /$ |  |
| PY88 | 0.00 | PCE800 | 0.75 |
| PY500A | 1.05 | 30FL2 | 0.75 |
| PY800 | 0.80 | 30 FLL 2 | 1.05 |
| PY801 | 0.50 | $30 \mathrm{FL14}$ | 0.85 |
| U26 | 100 | 30L1/PCC84 |  |
| U191 | 100 |  | 0.58 |
| U193 | 0.50 | 30L15/PCC805 |  |
| UABC80 | 0.90 |  |  |
| UBC81 | 0.70 0.60 | 30 L 17 |  |
| UBF89 | 0.60 0.80 | $30 \mathrm{P4MA}$ | 1.30 |
| UCC85 UCH81 | 0.60 | 30P12/PC801 |  |
| UCH81 | 1.00 |  |  |
| UCL82 | 0.70 |  | 1.05 |
| UCL83 | 070 | 30P10/PC802 |  |
| UF89 | $0 \cdot 80$ | - | 1.00 |
| UI,84 | 0.95 | 30PL1/PCL801 |  |
| UY85 | 0.50 |  |  |
| 8/30L2/ | 100 |  |  |
| 6 F23jEF812 |  | PCL800 | 1.20 |
| 6F | 105 | 30PL14/ |  |
| $30 \mathrm{Cl} / \mathrm{PCF}$ | 80 | PCL88 | 1.85 |
|  | 0.51 | 30 PL 15 | 105 |

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| :---: |

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| $0 \mathrm{C16}$ | 100 | 2TX501 | 0.15 | 2N2904 | 0.20 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| OC20 | $2 \cdot 0$ | 2TX503 | 0.18 | 2N2904A | 0.25 |
| 0 O 23 | 1.25 | ZTX531 | 0.25 | 2N2905 | 0.38 |
| OC25 | 0.40 | ZTX550 | 0.18 | 2N2905A | 0.25 |
| OC28 | 0.70 | 1N914 | 0.08 | 2N2906 | 0.20 |
| OC35 | 0.55 | IN 4001 | 0.6 | 2N2926 | $0 \cdot 10$ |
| OC36 | 0.86 | 1 N 4002 | 0.7 | 2N3053 | $0 \cdot 20$ |
| $\mathrm{OC4}^{\text {2 }}$ | 0.40 | IN 4003 | 0.8 | 2N3055 | 0.60 |
| OC44 | 0.18 | IN4004 | 0.8 | 2N3525 | 0.80 |
| $0 \mathrm{Cl45}$ | 0.18 | IN 4005 | 0.10 | 2N3614 | 0.60 |
| $0 \mathrm{C71}$ | 0.15 | IN 4006 | 0.12 | 2N3615 | 0.85 |
| OC72 | 0.85 | IN 4007 | 0.12 | 2N 3702 | 0-11 |
| $0 \mathrm{C76}$ | 0.30 | 1 N 4009 | 0.06 | 2N3703 | $0-12$ |
| 0 C 77 | 0.55 | 1N 4148 | 0.08 | 2N3704 | 0.14 |
| $0 \mathrm{C81}$ | 028 | 15921 | 0.07 | $2 N 3705$ | 0.12 |
| 0C81D | $0 \cdot 28$ | 182033 | 0.20 | 2N3706 | 0.10 |
| OC817 | 0.45 | 182081A | 0.10 | 2N3707 | 0.13 |
| 0 C 83 | 0.85 | 182100A | 0.80 | 2N3708 | 0.07 |
| OC140 | 0.65 | 183010 | 4.25 | 2N3709 | 0.10 |
| OC170 | 0.85 | 2N696 | 0.15 | 2N3710 | 0.11 |
| OC171 | 0.80 | 2N697 | 0.15 | 2N3711 | 0-11 |
| OC200 | 0.55 | 2N706 | 0.10 | 2N3819 | 0.85 |
| OC201 | 0.80 | 2N706A | 0.12 | 2N3820 | 0.50 |
| OC202 | 0.80 | 2N1131 | 0.25 | 2N3823 | 0.50 |
| OC203 | 0.55 | 2N1132 | 0.25 | 2N 3903 | $0 \cdot 16$ |
| OCP71 | 100 | 2N1302 | 0.18 | 2N3904 | 0.80 |
| ORP12 | 0.55 | 2N1303 | 0.18 | 2N3905 | 0.25 |
| ORP60 | 0.45 | 2N1304 | 0.82 | 2N3906 | $0-16$ |
| T1005 | 0.80 | 2N 1305 | 0.22 | 2N4058 | 0-15 |
| TIC4 4 | 0.28 | 2N1306 | 0.28 | 2N4059 | $0-10$ |
| TIC226D | 150 | 2N1307 | 0.28 | 2N4080 | 0.13 |
| TIL209 | 0.25 | 2N1308 | 0.28 | 2 N 4081 | 0-18 |
| Tr843 | 026 | 2N1309 | 0.30 | 2N4062 | 0.14 |
| 2TX 107 | 0.12 | 2N1613 | 0.20 | 2N4289 | 0.20 |
| ZTX 108 | 0.10 | 2N1614 | 0.45 | 3N141 | 0.81 |
| ZTX300 | 0.14 | 2N2147 | 0.75 | 40380 | 0.40 |
| ETX301 | 0.14 | 2N2160 | 1.00 | 40361 | $0-45$ |
| 2TX 302 | 0.20 | 2N2369A | 0.16 | 40882 | 0.40 |
| 2TX304 | 024 | 2N2646 | 0.50 | 40430 | 0.85 |
| ZTX 500 | 0.15 |  |  |  |  |
| 8N7473 | 0.44 | 8N74107 | 0.51 | EN74157 | 1.09 |
| 8N7474 | 0.48 | SN74110 | 0.57 | 8N74170 | 2.88 |
| 8N7475 | 0.59 | BN74111 | 0.88 | EN7417 | 1.80 |
| 8N7476 | 0.45 | 8N74118 | 1.00 |  | 1.29 |
| 8N7480 | 0.80 | 8N74119 | 1.92 | 8N74176 | 1.44 |
| BN7482 | 0.87 | 8N74121 | 0.57 | 8N74190 | $2 \cdot 30$ |
| BN7483 | 120 | 8N74122 | 0.80 | GN74191 | $2 \cdot 30$ |
| 8N7484 | 100 | 8N74123 | 1.44 | SN74192 | $2 \cdot 30$ |
| BN7486 | 0.50 | 8N74141 | 100 | BN74193 | $2 \cdot 30$ |
| EN7490 | 0.75 | 8N74145 | 1.44 | BN74194 | 1.72 |
| 8N74914, |  | 8N74150 | 2.80 | BN74195 | 1.44 |
|  | 110 | 8N74151 | 1.15 | BN74196 | 1.58 |
| 8N7492 | 0.75 | 6N74154 | 2.30 | SN74197 | 1-58 |
| 8N7493 | 0.75 | 8N74155 | 115 | BN74198 | 8.16 |
| EN7494 | 0.85 | 8N74166 | 115 | SN74199 | 2-88 |
| BN7495 | 0.85 | DIL SOCKETS |  |  |  |
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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 25 | $100+$ |  |  | $\pm 3$ | $100+$ |  | 1 | 25 | 00 |
|  |  | 2 p | 2 p |  | \& ${ }^{\text {p }}$ | ${ }^{2} \mathrm{p}$ | $\varepsilon_{1} \mathrm{p}$ |  | ${ }^{1} \mathrm{D}$ | $1{ }^{1}$ |  |
| 7400 | 0.18 | 0.17 | $0 \cdot 10$ | 7448 | $1 \cdot 10$ | 1.07 | 1.05 | 74190 | 1. 50 | 1.45 | $1 \cdot 40$ |
| 7401 | 0.18 | $0 \cdot 17$ | 0.16 | 7450 | $0 \cdot 18$ | 0.17 | 0.16 | 741133 | $3 \cdot 00$ | 2.90 | 2.80 |
| 7402 | 0.18 | $0 \cdot 17$ | $0 \cdot 16$ | 7431 | 0.18 | $0 \cdot 17$ | $0 \cdot 16$ | 74141 | 0.85 | $0 \cdot 82$ | 0.79 |
| 7403 | 0.18 | $0 \cdot 17$ | 0.18 | 7453 | 0.18 | 0.17 | 0.16 | 74145 | 1.65 | 1.55 | 1.45 |
| 7404 | 0.18 | $0 \cdot 17$ | $0 \cdot 16$ | 745-4 | 0. 18 | 0.17 | 0.16 | 74150 | 2. 90 | $2 \cdot 80$ | $2 \cdot 70$ |
| 7405 | 0.18 | $0 \cdot 17$ | 0.16 | 7460 | 0.18 | 0.17 | $0 \cdot 16$ | 74151 | 1.10 | 1.05 | 1-00 |
| 7406 | 0.39 | $0 \cdot 34$ | 0.31 | 7470 | $0 \cdot 32$ | $0 \cdot 28$ | 0.27 | 74153 | 1.30 | 1.20 | 1.10 |
| 7407 | 0.38 | 0.34 | $0 \cdot 31$ | 7472 | 0.32 | 0.29 | $0 \cdot 27$ | 74134 | 1.98 | 1.90 | 178 |
| 7408 | 0.20 | $0 \cdot 19$ | 0.18 | 7473 | 0.41 | 0.39 | $0 \cdot 35$ | 74155 | 1. 50 | 1.45 | $1 \cdot 85$ |
| 7404 | $0 \cdot 20$ | 0-19 | 0.18 | 7474 | 0.41 | 0.39 | 0.35 | 7415 6 | 1.50 | 1.45 | 1.85 |
| 7410 | $0 \cdot 18$ | $0 \cdot 17$ | 018 | 7475 | 0.50 | 0.48 | $0 \cdot 46$ | 74157 | 2.00 | 1.90 | 1.80 |
| 7411 | 0.28 | 0.27 | 0.26 | 7476 | 0.44 | 0.43 | 0.42 | 74180 | $2 \cdot 10$ | 2. 00 | 1.80 |
| 7412 | 0.89 | 0-34 | $0 \cdot 31$ | 7480 | 0.74 | 0.71 | 0.64 | 74161 | $2 \cdot 10$ | 2.00 | 1.90 |
| 7413 | 0.82 | 0.21 | $0 \cdot 30$ | 7481 | $1 \cdot 30$ | 1-25 | 1.20 | 74162 | 4.40 | 4.15 | $8 \cdot 85$ |
| 7416 | 0.48 | 0.44 | 0.42 | 7482 | $0 \cdot 96$ | 0.85 | $0 \cdot 94$ | 74163 | 4.40 | $4 \cdot 15$ | 3.85 |
| 7417 | 0.48 | 0.44 | 0.42 | 7483 | 1.20 | 1.15 | 1.05 | 74164 | 2.20 | $2 \cdot 10$ | 2. 00 |
| $74: 30$ | 0.18 | 0.17 | 0.16 | 7484 | 1.10 | 1.05 | 1.00 | 74165 | $2 \cdot 20$ | $2 \cdot 10$ | 2.00 |
| 7422 | 0.55 | 0.53 | 0.50 | 7485 | 3.50 | $3 \cdot 30$ | 3. 30 | 7+186 | 3.20 | $3 \cdot 10$ | $8 \cdot 00$ |
| 7423 | 0. 55 | 0.53 | 0.50 | 7485 | 0.35 | 0.34 | 0. 33 | 74174 | $2 \cdot 50$ | 2.40 | $2 \cdot 30$ |
| 74.5 | 0.55 | 0.53 | $0 \cdot 50$ | 7484 | 4.00 | 8.75 | $3 \cdot 50$ | 74175 | 1.75 | $1 \cdot 65$ | 1.55 |
| 7426 | 0.50 | 0.46 | 0.44 | 7480 | 0.74 | 0.71 | $0 \cdot 64$ | 7417 f | 1.85 | 1.75 | $1 \cdot 85$ |
| 74:7 | 0. 50 | 0.48 | 0.44 | $7+91$ | 1.10 | 1-05 | 1.00 | 74173 | 1.85 | 1.75 | 1. 85 |
| 7428 | 0.55 | 0.53 | 0.60 | 7492 | 0.74 | 0.71 | 0.64 | 74180 | 1.50 | 1.40 | 1-30 |
| 7430 | 0.18 | $0 \cdot 17$ | 018 | 7493 | 0.74 | $0 \cdot 71$ | $0 \cdot 64$ | $7+181$ | $5 \cdot 00$ | 4.50 | $4 \cdot 00$ |
| 7432 | 0. 50 | 0.48 | 0.44 | 7494 | 0.85 | 0.82 | 075 | 7418 2 | 2.00 | 1.90 | $1 \cdot 75$ |
| 7433 | 0.75 | $0 \cdot 73$ | 0.70 | 7495 | 0.85 | 0.82 | 0.75 | 74184 | $3 \cdot 20$ | $3 \cdot 10$ | 3.00 |
| 7437 | 0.70 | $0 \cdot 68$ | 0.65 | 7496 | 0.98 | 0.83 | 0.86 | 74190 | $2 \cdot 15$ | $2 \cdot 10$ | $2 \cdot 00$ |
| 7438 | $0 \cdot 70$ | 0.68 | 0.65 | 74100 | 1. 50 | 1.45 | 1.40 | 74191 | $2 \cdot 15$ | $2 \cdot 10$ | 2-00 |
| 7440 | 0.19 | $0 \cdot 17$ | 0.18 | 74104 | 1.07 | 1.04 | 100 | 74192 | 2.15 | 2.10 | $2 \cdot 00$ |
| 7441 | 0.74 | $0 \cdot 71$ | 0.64 | 74105 | 1.07 | 1.04 | 1.00 | 74193 | $2 \cdot 15$ | $2 \cdot 10$ | $2 \cdot 00$ |
| 7442 | 0.74 | 0.71 | 0.64 | 74107 | 0.44 | 0.42 | 0.40 | 74194 | $2 \cdot 88$ | 2.88 | $2 \cdot 75$ |
| 7443 | 1.20 | 1.15 | 1.10 | 74110 | 0.60 | 0.55 | 0. 50 | 74195 | $2 \cdot 00$ | 1.95 | 1.90 |
| 7444 | $1 \cdot 20$ | 1.15 | $1 \cdot 10$ | 74111 | 138 | 1.87 | 121 | 74196 | 1.85 | 1.90 | $1 \cdot 85$ |
| 7445 | 1.98 | 1.95 | 1.90 | 74118 | 1.10 | 1.05 | 1.00 | 74197 | 1.95 | 1.90 | $1 \cdot 85$ |
| 74413 | 1.20 | 1.15 | 1.10 | 74119 | 1. 50 | 1.40 | 1.30 | 74198 | $5 \cdot 00$ | 4.75 | $4 \cdot 50$ |
| 7447 | $1 \cdot 10$ | 1.07 | 1.05 | 74121 | 0.50 | 0.48 | $0 \cdot 45$ | 7419 | $5 \cdot 00$ | 4.75 | 4.50 |



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| Q9 | 7 OU: 81 ty de transintors |  |
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U31 $2 \overline{0}$ Sillcon Planer Platic NPN Trama. Low Nolse Amp $2 \bar{N} 370$
$\overline{25}$ Zener 1) Ioden $40 \overline{0} \mathrm{~mW}$ D 0.7 cane $3-18$ volts mixed
13315 Plastic Case 1 A mp Bilicon Hectifers IN 4000 Seflen
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0.65
0.65
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0.58$\begin{array}{r}0.66 \\ 0.86 \\ \hline\end{array}$
0.68$\frac{0.65}{1.10}$$-\frac{1}{0} \frac{10}{56}$$\begin{array}{r}0.66 \\ \hline 0.66 \\ \hline\end{array}$1/82$\begin{array}{r}0.66 \\ \hline 0.86\end{array}$
$\frac{0.65}{0.86}$
$-\quad 0.56$$\frac{0.56}{0.88}$
U42 10 VHF Germanium PNI Transhatora TO-1 NKT6日7, AF117 0.8
प43 25 gll. Trans. Platic TO-18 A F. BC113/
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Odb ( 0.775 volts RMS)
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Magnetic Pick-up 3 mV (within 1 db RIAA curve)
Ceramic Pick-up up to 3 mV
Microphone 10 mV
Tuner 250 mV
Auxlliary $3-100 \mathrm{mV}$
Input impedance $47 \mathrm{k} \Omega 1 \mathrm{kHz}$
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Tape 100 mV
Main output, Odb (0.775volts)
ACTIVE TONE CONTROLS
Treble $\pm 12 \mathrm{db}$ at 10 kHz
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# YATES ELECTRONICS <br> (FLITWICK) LTD. <br> DEPT PW, ELSTOW STORAGEDEPOT KEMPSTON HARDWICK <br> dBEDORD 

C.W.O. PLEASE. POST AND PACKING PLEASE ADD 10p TO ORDERS UNDER £2. Catalogue which contains data sheets for most of the components listed will be sent free on request. 10p stamp appreciated.

Callers Weicome Mon, to Sat. 9 a.m.-5 p.m.

## PLEASE ADD 10\% VAT

RESISTORS
W iskra high stability carbon film-very low noise-capless construction W Mullard CR25 carbon film-very small body slze $7.5 \times 2.5 \mathrm{~mm}$. 1 W $2 \%$ ELECTROSIL TR5.

| Power |  |  | Values | Price |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| watts | Tolerance | Range | available | 1-99 | $400+$ |
| t | 5\% | 4. $7 \Omega-2 \cdot 2 \mathrm{M} \Omega$ | E24 | 1 3p | 1-1p |
| t | 10\% | 3. $3 \mathrm{M} \Omega-10 \mathrm{M} \Omega$ | E12 | 1.3p | $1.1 p$ |
| ! | 2\% | $10 \Omega-1 \mathrm{M} \Omega$ | E24 | 3.5p | 3p |
| , | 10\% | $1 \Omega-3 \cdot 9 \Omega$ | E12 | 1.3p | $1.1 p$ |
| t | 5\% | 4. $7 \Omega-1 \mathrm{M} \Omega$ | E12 | 1.3p | 11 p |
| 4 | 10\% | $1 \Omega-10 \Omega$ | E12 | 8 p | 7 p |

DEVELOPMENT PACK
0.5 watt $5 \%$ Iskra resistors 5 off each value $4.7 \Omega$ to $1 \mathrm{M} \Omega$.

POTENTIOMETERS
Carbon track $5 \mathrm{k} \Omega$ to $2 \mathrm{M} \Omega$, log or llnear (log $\frac{1}{6} \mathrm{~W}$. lin $\left.\frac{1}{2} \mathrm{~W}\right)$.
Single, 14p. Dual gang (stereo), 49p. Single D.P. swith 25 p
SKELETON PRESET POTENTIOMETERS
Linear: $100,250,500 \Omega$ and decades to $5 \mathrm{M} \Omega$. Horlzontal or vertlcal P.C.
Sub-miniature 0.1 W.

SMOKE AND COMBUSTIBLE GAS DETECTOR-GDI
The GDI Is the world's first semlconductor that can convert a concentration of gas or smoke into an electrical signal. The sensor decreases its electrical carbon monoxide, methane, propane, alcohol, North Sea gas, as wall as carbondust contalning atror smoke. This decreasels usually large enough to be utillzed without amplification. Full details and circuits are supplled with esch detector. Detector GDI £2. KIt of parts for mains operated detector, including GDI but excluding case. $£ 560$. Sultable case £1-50. Kit of parts for 12 or 24 V battery operation, Including GDI and P.C. Board, £770. As above for PPg battery, £6.90. NOTE: The battery operated kits Incorporate our patented circuit to minimise battery drain. Typically 90 mA for 24 V
PRINTED BOARD MARKER
Draw the planned circult onto a copper laminate board with the P.C. Pen, allow to dry, and Immerse the board In the etchant. On removal the circult remains in high rellef.

MULLARD POLYESTER CAPACITORS C296 SERIES
$400 \mathrm{~V}: 0.001 \mu \mathrm{~F}, 0.0015 \mu \mathrm{~F}, 0.0022 \mu \mathrm{~F}, 0.0033 \mu \mathrm{~F}, 0.0047 \mu \mathrm{~F}, 3 \mathrm{p} .0 .0068 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}$ $0.022 \mu \mathrm{~F}, 0.033 \mu \mathrm{~F}, 3 \frac{1}{2} \mathrm{p} .0 .047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 0.9 \mu \mathrm{~F}, 5 \mathrm{p} .0 .15 \mu \mathrm{~F}, 6 \mathrm{p} .0 .22 \mu \mathrm{~F}, 74 \mathrm{p} .0 .33 \mu \mathrm{~F}, 11 \mathrm{p}$
$160 \mathrm{~V}: 0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 0.033 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 3 \mathrm{p} .0-9 \mu \mathrm{~F}, 3 \frac{1}{2} \mathrm{p} .0 .15 \mu \mathrm{~F}$, 41p $0.22 \mu \mathrm{~F}, 5 \mathrm{p} .0 .33 \mu \mathrm{~F}, 6 \mathrm{p} .0 .47 \mu \mathrm{~F}, 7 \frac{1}{2} \mathrm{p} .0 .68 \mu \mathrm{~F}, 11 \mathrm{p}, 1.0 \mu \mathrm{~F}, 13 \mathrm{p}$.
MULLARD POLYESTER CAPACITORS C2BO SERIES
250 V P.C. mounting: $0.01 \mu \mathrm{~F}, 0 \mu 015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 3 \mathrm{p}, 0.033 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 3 \mu \mathrm{p}$ $0.1 \mu \mathrm{~F}, 4 \mathrm{p}, 0.15 \mu \mathrm{~F}, 0.22 \mu \mathrm{~F}, 5 \mathrm{p}, 0.33 \mu \mathrm{~F}, 6 \frac{1}{2} \mathrm{p} \cdot 0.47 \mu \mathrm{~F}, 81 \mathrm{p} .0 .68 \mu \mathrm{~F}, 11 \mathrm{p} .1 \cdot 0 \mu \mathrm{~F}, 13 \mathrm{p} .1 \cdot 5 \mu \mathrm{~F}$,
$20 \mathrm{p} .2 .2 \mu \mathrm{~F}, 24 \mathrm{p}$. 20p. $2 \cdot 2 \mu \mathrm{~F}, 24 \mathrm{p}$ MYLAR FILM CAPACITORS 100V CERAMIC DISC CAPACITORS
$0.001 \mu F, 0.002 \mu \mathrm{~F}, 0.005 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}$. $0.02 \mu \mathrm{~F}$ CAP $0.001 \mu \mathrm{~F}, 0.002 \mu \mathrm{~F}, 0.005 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}, 0.02 \mu \mathrm{~F}, \quad 100 \mathrm{pF}$ to $10,000 \mathrm{pF}, 2 \mathrm{p}$ each.
$3 \mathrm{p} .0 .04 \mu \mathrm{~F}, 0.05 \mathrm{~F}, 0.068 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}$. 3 p . $0.04 \mu \mathrm{~F}, \quad 0.05 \mu \mathrm{~F}, \quad 0.068 \mu \mathrm{~F}, \quad 0.1 \mu \mathrm{~F}, 4 \mathrm{p}$.

## ELECTROLYTIC CAPACITORS

( $\mu$ F/v) $1 / 63,1 \cdot 5 / 63,2 \cdot 2 / 63,3 \cdot 3 / 63,4 \cdot 7 / 63,6 \cdot 8 / 40,6 \cdot 8 / 63,10 / 25,10 / 63,15 / 16,15 / 40,15 / 63$, $22 / 10,22 / 25,22 / 63,33 / 6 \cdot 3,33 / 16,33 / 40,47 / 4,47 / 10,47 / 25,47 / 40,68 / 6 \cdot 3,68 / 46,100 / 4,100 / 10$, $100 / 25,150 / 6 \cdot 3,150 / 16,220 / 4,220 / 6 \cdot 3,220 / 16,330 / 4,6$ p. $47 / 63,100 / 40,150 / 25,220 / 25,330 / 10$, $470 / 63,7 p .68 / 63,150 / 40,220 / 40,330 / 18,1000 / 4,10 p .470 / 10,680 / 6 \cdot 3,11 \mathrm{p} .100 / 63,150 / 63$, $220 / 63,1000 / 10,12 p .470,25,680 / 16,1500 / 6 \cdot 3,13$ p. $470 / 40,680 / 25,1000 / 16,1500 / 10,2200 / 6 \cdot 3$
18 p. $330 / 63,680 / 40,100 / 25,1500 / 16,2200 / 10,3300 / 6 \cdot 3,4700 / 4,21 \mathrm{p}$. 18p. $330 / 63,680 / 40,1000 / 25,1500 / 16,2200 / 10,3300 / 6 \cdot 3,4700 / 4,21 \mathrm{p}$

| SOLID TANTAL <br> $0.1 \mu \mathrm{~F}$ <br> $0.22 \mu \mathrm{~F}$ <br> $0.47 \mu \mathrm{~F}$ <br> $1.0 \mu \mathrm{~F}$ | $U M$ 35 V 35 V 35 V 35 V | AD |
| :---: | :---: | :---: |
| VEROBOARD |  |  |
|  | 0.1 | $0 \cdot 15$ |
| 21 $\times 34$ | 24p | 20p |
| $2 \times 5$ | 28p | 28p |
| $3 \times 3$ 年 | $28 p$ | ${ }^{28} \mathrm{p}$ |
| $37 \times 5$ | 32p | 32p |
| $17 \times 2 \frac{1}{4}$ | 85 p | 67p |
| $17 \times 34$ | 120p | 108p |
| $17 \times 3 \pm$ (plain) | $76 p$ | 52p |
| $17 \times 2 \frac{1}{2}$ (plaln) | - | $41 p$ |
| $2 \frac{1}{2} \times 5$ (plain) | - | 12p |
| $2 \pm \times 37$ (plain) | $\bar{\square}$ | 11p |
| Pln insertion tool | 62 p | 62p |
| Spot face cutter | 52 p | 52p |
| Pht. 50 plns | 20p | 200 |

VEROBOARD
$21 \times 34$
21
$\times 5$
$21 \times 5$
3
$\times 34$
(plain)
$17 \times 2 \frac{2}{2}$ (plain)
$2 \frac{1}{2} \times 5$ (plain)
$2 t \times 3$ (plain)
Pln insertion tool
Spot face cutter
Pht. 50 pins

## ACITORS $2.2 \mu \mathrm{~F} \quad 35 \mathrm{~V}$

$\begin{array}{ll}2.2 \mu \mathrm{~F} & 35 \mathrm{~V} \\ 4.7 \mu \mathrm{~F} & 35 \mathrm{~V}\end{array}$
$\begin{array}{ll}22 \mu \mathrm{~F} & 16 \mathrm{~V} \\ 33 \mu \mathrm{~F} & 10 \mathrm{~V}\end{array}$
$33 \mu \mathrm{~F}$
$47 \mu \mathrm{~F}$
6.3 V
100 mF 3 V

## JACK PLUGS AND SOCKETS

## Standard screened $28 \mathrm{p} \quad 2.5 \mathrm{~mm}$ Insulated

 Standard insulated $18 \mathrm{p} \quad 3.5 \mathrm{~mm}$ insulated Stereo screened $\quad 40 \mathrm{p} \quad 3.5 \mathrm{~mm}$ screened Standard socket $\quad 20 \mathrm{p} \quad 2.5 \mathrm{~mm}$ socket Stereo socket 30p 3.5 mm socketD.I.N. PLUGS AND SOCKETS
${ }^{2}$ pin, 3 pin, 5 pin 180, 5 pin 240, 6 pin, 7 pln. Plug 12p. Socket $8 p$
4 way screened cable, 25 p/metre.
6 way screened cable. $30 \mathrm{p} /$ metre

## BATTERY ELIMINATOR

9V mains ELIMINATOR E1.70

learn how to become a radio-amateur in contact with the whole world. We give skilled preparation for the G.P.O. licence

Brochure, without obligation to

## BRITISH NATIONAL RADIO \&

 ELECTRONICS SCHOOL P.O. Box 156, JERSEY NAME

Jermyn now offer a stereo decoder module that simply and easily converts your existing mono tuner for stereo reception. Multiplex output equipped tuners simply have the module plugged in, older types need the de-emphasis capacitor disconnected.

The unit will do justice to the most expensive equipment and has the following specification.
Channel separation: Typically 40dB
Distortion: Typically $0.3 \%$ at 560 mV RMS
Stereo switching: Automatic with lighted indicator Power supply: $10-16$ volts.
Assembled and fully tested with a no-strings 12 month guarantee the module costs an astonishing £6.90. Excluding VAT. (Also available as a Kit at £4.90.) Beat that!
 164 Vestry Estate Sevenoaks Kent

I enclose cheque/postal order for $\Sigma$
Name Address
NEW TUAC POWER MODULES. Now in their second successful year
 offering more power and quality than ever before.
TP100
Illustrated 125 Watts RMS continuous sine wave output
\& RCA 150 Watt 15 Amp output transistors
\& Special layer wound driver transformer
\& Short, open, and thermal overload protection
\& Compact size: $7 \times 6 \frac{1}{2} \times 3$ in.
TL30
£9.50
$\star 30$ Watts RMS sine wave
$\star$ Full thermal overload protection $\star$ Short and open circuit proof $\star$ Rugged transformer driver


TL400 Illustrated £13:00
$\star 100$ Watts RMS sine wave $\star 2$ RCA 15 Amp output transistors $\star$ Rugged transformer driver $\star$ Full thermal overioad protection $\star$ Compact size: $5 \times 5 \times 3 \mathrm{in}$.

TL60

+ 60 Watts RMS
sine wave
Specification on all three power modules :
All output power ratings $\pm 1 \mathrm{~dB}$. Output impedance $8-15$ Ohms. THD at full power $1 \%$ typically $0.5 \%$.
Input sensitivity 60 mV into $10 \mathrm{k} \Omega$. Frequency response $10 \mathrm{~Hz}-25 \mathrm{kHz} \pm 2 \mathrm{~dB}$. Hum and noise better than -75 dB .
Power supplies vacuum impregnated Transformers with supply board incorporating pre-amp supply:
PS $125 \pm 50$ volts for one TP100 $. . \quad . . \quad . . \quad . . \quad . . \quad . . \quad$.. £11.75
PS $100+45$ volts for one TL100
£10-75
PS 60 - 40 volts for on TL100
PS $30+50$ volts for one TL30
$£ 9.50$
£ 7.00


## PRE AMPLIFIERS

Alt Tuac audlo modules are constructed on glass fibre P.C. board, are ready assembled and fully tested. Low noise silicon and FET transistors together with H.S. carbon film reslstors are used throughout. Extensive research has gone Into the various wide range tone control circults, producing superb sound quality from any signal. Previous range still available. 10 V d.c.; 60 mV o/p.
$\checkmark$ VA01, Treb, Mid and Bass Controls. HI IMP. FET I/P. Sultable Mic. Gultar. Radio, Crystal/Ceramlc
VA06 Vol, Treb and Bass Controls. 8 mV sensitlvity. Treb $+28-15 \mathrm{~dB}$ at 12 kHz , Bass $\pm 18 \mathrm{~dB}$ at 40 Hz .
¢4.25
AMF01 Tuac Auto Fade Unit fades music when you speak. Auto Mrc Over-ride for Dlsco use. Feed Deck and
30 mV operatlng level. Depth and Vol. Controls.


SIZE $6 \frac{1^{\prime \prime}}{} \times 2^{\prime \prime} \times 1^{\prime \prime}$

ALL PRICES INCLUDE V.A.T. AND POSTAGE AND PACKING
ACCESS B BARCLAY CARDS ACCEPTED. JUST SEND US YOUR NUMBER. H.P. ARRANGED THROUGH PAYBONDS.


TUAC DISCOTHEQUE MIXER WITH AUTO FADE
Designed for the discerning D.J. of professional standard.
Offering a vast variety of functions.
Controls: Mic Vol, Tone, Over-ride depth, Auto Manual Sw. Tape Vol, L \& R Deck Faders, Deck Volume. Treb, \& Bass. H. Phon Vol, Selector. Master Vol, on/off sw. Max. output 1V RMS. Specification as VA06.

PANEL SIZE $18^{\prime \prime} \times 4 \frac{1}{2}$ " DEPTH $3^{\prime \prime}$
TUAC HIGH POWER AMPLIFICATION-built to high
 standards, and bullt to last
so WATT RMS SINE WAVE ALL PURPOSE AMPLIFIER
Sultable for Disco, PA, Guitar. 4 Inputs, 2 volume controls. Master volume, treble, middle and bass controls. Rugged clrcult, rugged leather-cloth covered case, short and open circu p YA08 pre-amp FlDLLY FUSED.


WATT $54.4-10$


## NEW FROM TUAC!!

100W $2 \times 12$ Disco/Group cabs, fitted 250 W RMS super heavy duty speakers $\mathbf{£ 6 6 \cdot 0 0}$ (car. £1-00) 100W $4 \times 8$ P.A. Cols, fitted 415 W heavy duty speakers. £75.00 pair (carr. £2•00).

## TUAC MAIN DEALERS

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Tel. Canterbury 60948
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MANUFACTURERS OF ELECTRONIC AND AMPLIFICATION EQUIPMENT

## AN TUAC

 SPECIALISTS IN QUALITY TRANSISTOR EQUIPMENTOPEN 6 DAYS A WEEK. $9.30 \mathrm{a} . \mathrm{m}$. - $6.00 \mathrm{p} . \mathrm{m}$.

## 5 <br> $T-v$c FOR AUDIO ON A BUDGET

## PUSH BUTTON CAR RADIO KIT <br> The first time Motor magazine have nominated a push button car radio for their Top Ten Accessory Awards



NOTE: The ability to solder on a printed circuitboard is necessary to complete this kit succes sfully. Circuit diagram and comprehensive instructions 55 f free with kit. Car Radio Kit $\mathbf{£ 6 . 6 0}+55$ p. postage \& packing.
Speaker including baffle and fixing strips
£1.65 + 23p. postage \& packing.
Recommended Car Aerial - fully retractable and locking. f1.35 post paid.


## QUALITY-SOUND* FOR LESS THAN£19.00

Stereo 21 easy to assemble audio system kit, - no soldering required. Includes:-
BSR 3 spaed deck, automatic, manual facilities together with ceramic cartrídge.
Two speakers with cabinets.
Amplifier module. Ready built with control panel, speaker leads and full, easy to follow assembly instivections.

For the technically minded:-

## Specifications

Input sensitivity $600 \mathrm{~m} V$ : Aux. input sensitivity $120 \mathrm{~m} V$ : Power output 2.7 watts per channel: Output impedance $8-15$ ohms. Stereo headphone sockel with automàtic speaker cutout. Provision for auxiliary inputs - radio. tape, etc., and outputs for taping discs. Overall Dimensions. Speakers approx. $151^{\prime \prime} \times 8^{\prime \prime}$ " $4^{\prime \prime}$. Complete deck and cover in closed position approx. $15 \frac{1}{2}{ }^{\prime \prime} \times 12^{\prime \prime} \times 6^{\prime \prime}$. Complete only $\mathbf{£ 1 8 . 9 5}$ Extras if requirad.
Optional Diamond Stylif $1.37 \quad$ - $\mathbf{I} 1.60 \mathrm{p}$ \& $p$. Specially selected pair of stereo headphones with individual level controls and padded earpieces to give optimum performance. $\mathbf{£ 3 . 8 5}$.

Reliant Mk IV Mono Amplifier. ideal for the small disco or house parties.
Outputs 20 watts R.M.S. into 8 ohms (suitable for 15 ohms).
Inputs *5 Electrically Mixed Inputs. *3 Individual Mixing controls. *Separate bass and treble controls common to all 5 inputs. *Mixer employing F.E.T. (Field Effect Transis(ors). *Solid Stata Circuitry. *Attractive Styling INPUT SENSITIVITIES

1) Crystal Mic or Guitar 9 mV . 2) Moving coul Mic or Guitar 8 mV . 3), 4), 5) Medium output equipment (Gram. Tuner, Monitor, Organ, etc.) all 250 mV sensitivity. AC Mains 240V. operation Size adorox. $12 \frac{1}{2}$ ins $\times 6$ ins $\times 3 \frac{1}{2}$ ins $\mathbf{f 1 5 . 0 0}+\mathbf{6 0 p}$. postage $\&$ packing


45 WATT R.M.S. MONO DISCOTHEQUE AMPLIFIER Ideal for Disco Work. Output Power: 45 watts R.M.S. Frequency Response 3 dB points 30 Hz and 18 KHz . Total Distortion: less than $2 \%$ at rated output. Signal to noise ratio: better than 60 dB . Bass Control Range: 13 dB at 60 Hz . Treble Control Range: 12 dB at 10 KHz . Inputs: 4 inputs at 5 mV into 470 K . Each pair of inputs controlled by separate volume control. 2 inputs at 200 mV into 470K. Size: $19 \frac{1}{4} / 10 \frac{1}{2} \times 8$ ins. approx. Amplifier $£ 27.50+\mathbf{£ 1 . 5 0} \mathbf{p}$. \& p
Special Offer: Disco 50 plus two 15" E.M.I. speakers type 14A/780 (as illustrated on opposite page). Complete $£ 57.00+\mathbf{£ 4 . 0 0} \mathbf{p} \&$ p.

## COMPLETE STEREO SYSTEM

## f51.00 <br> 40 Watt Amplifier

Viscount III - $\mathbf{R 1 0 2}$ now 20 watts per channel. System I includes.
Viscount III amplifier - volume, bass, treble and balance controls, plus switches for mono/ stereo on/off function and bass and veble

filters. Plus headphone socket Specification
20 watts per channel into 80 hms Total distortion@10W@1kHz0.1\%.P.U.I (for ceramic cartridges) 150 mV into 3 Meg. P.U. 2 (for magnetic cartridges) 4 mV (2) 1 kHz : ito 47 K equalised within IdB R.I.A.A. Radio 150 mV into 220K. (Sensitivities given at full power). Tape out facilities : headphone socket, power out 250 mW per channel. Tone controls and fifter characteristics. Bass: +12 dB to $-17 \mathrm{~dB} @$ 60 Hz . Bass filter: 6 dB per octave cut. Treble control: treble-12d810-12d8@15kHz. Treble filter: 12 dB per octave. Signal to noise ratro: (all controls at max.) -58dB.
Crosstalk better than 35 dB on all inputs. Overload characteristics better than 26 dB on all inputs. Size approx. $13 \frac{3}{4} \times 9^{\prime \prime}{ }^{\prime} 3^{33^{\prime \prime}}$
Garrard SP25 deck, with magnetic cartridge, de luxe plinth and hinged cover.
Two Duo Type II matched speakers Enclosure size approx. 17 $\frac{1}{2}^{\prime \prime}-103^{\prime \prime} \times 6^{\prime \prime}$ in simulated teak. Drive unit $13^{\prime \prime} \times 8^{\prime \prime}$ with parasitic tweeter (10 watt handling)

Complete System £51.00

### 669.00

System II
Viscount III amplifier (As System I)
Garrard SP. 25 (As System I)
Two Duo Type IIIA matched speakersEnclosure size approx. $31^{\prime \prime} \times 13^{\prime \prime} \times 11 \frac{1^{\prime \prime}}{2}$ Finished in teak veneer. Drive units approx.
 20 watts, 8 ohms. Freq. range 20 Hz to 20 kHz .

## Complete System $£ 69.00$

PRICES: SYSTEM 1
VIScount III R 102 amplifieI, $\quad £ 24 \cdot 20+\mathrm{f} 1 \mathrm{p} \& \mathrm{p}$ 2 Duo Type I| speakers $\quad £ 14 \cdot 00+\mathbf{f 2} \cdot 20 p$ \& $p$ Garrard SP25 with
MAG. cartridge de luxe plinth
and hinged cover
$£ 21.00+£ 1.75 \mathrm{p}$ \& p.
total $\mathbf{f 5 9 . 2 0}$
Available complete for only $£ 51.00+£ 3.50 p$. \&p.
PRICES: SYSTEM 2

| Viscount R102 amplifier | \{24 20 | ¢1.00 p. 80 |
| :---: | :---: | :---: |
| 2 Duo Type IIIA speakers | ¢3900 | ¢4.00p. \& p. |
| Garrard SP25 with |  |  |
| MAG cartridge de luxe plinth and hinged cover | ¢21.00 | £1.75 p. \& p. |
| total | 184.20 |  |

Available complete for only $\mathbf{f 6 9 . 0 0}+\underline{\mathbf{f} 4}$ p- $\underline{\square}$

## EMI SPEAKERS AT FANTASTIC REDUCTIONS

THE ULTIMATE COMPLETE SPEAKER SYSTEM EMI LE 315 listed price $\mathbf{E 8 6 . 0 0}$


A piofessional standard five way speaker system with enclosure giving top quality performance
Enclosure Dimensions
approx ( $3 \mathrm{ft} \cdot 2 \mathrm{ft} \cdot 1 \mathrm{ft}$.)
Drive Units
Hand built - 15 " diameter bass with $3^{\prime \prime}$ voice coll, - iwo 5 " diameter Mid Range units, - iwo $31_{4}^{\text {" " HF units. plus matching }}$ crossover panel with two variable
potentiometers for mid and high frequency adjustment
Power Handling
Continuous rating 35 Wrms. Peak power rating 70 W
Frequency Response
20 Hz 20.000 Hz . 1 mp .8 ohms


15" 14A/780 BASS UNIT
Bass unit on a rigid diecast chassis Superior cone material handles up to 50 watts RMS, and is treated to give a smooth frequency response Resonance 30 Hz . flux density 360,000 Maxwells. Impedance at 1 kHz is 8 ohms 3 " voice coil.
Recommended retail price $£ 40.80$


Five matched speakers and crossover unit for handling up 1045 watts, frequency response from 20 to $20,000 \mathrm{~Hz}$ Huge 19" $14^{\prime \prime}($ approx.) high efficiency Bass-Speaker with 16,500 -gauss magnet built on a heavy diecast frame.
The four 10,000 gauss tweeters, each $3 \frac{1}{d}$ dia. approx, are fed by the crossover which critically adjusts signal for maximum fidelity. Impedance at ! kHz is 8 ohms. Bass coil $2^{\prime \prime}$, others $0 \cdot 5^{\prime \prime}$. Recommended list price f 44.00 OUR PRICE E19.50 $+\mathbf{£ 1 . 5 0 p}$ \& p Special Offer

# 8TRACK CARTRIDGE PLAYER ${ }^{\left({ }^{\prime \prime}\right)}$ 

For the man who wants to design his own stereo - here's your chance to star with Unisound - pre-amp. pewer amplifier and control panel. No soldering just simply screw ingether 4 watts per channel into 8 ohms. Inputs: 120 mV (for ceramic cartridye). The heart of Unisound is high efficiency I.C. monolithic power chips which ensure very low distortion over the audio spectrum 240 V . AC only.
$\mathbf{f 7 . 6 4 + 5 5 p . p \& p}$

Eleyant self selector push button playes for use with your stereo system. Compatible with Viscount III system, Unisound module and the Stereo 21 Technical specification Mains input, 240V. Output sensitivity 125 mV Comparable unit sold elsewhere at $£ 24.00$ approx Yours for only $£ 10.95+\mathbf{9 0 p} . \mathrm{p} \& \mathrm{p}$


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## SCORP1OMk inghion system tit Hew rom IT:CRO SPARE

## * 6 OR 12 VOLT <br> * + VE AND - VE GROUND

Here's the new, improved version of the original Scorpio Electronic Ignition System - with a big plus over all the other kits - the Electro Spares Kit is designed for both positive and negative ground automotive electrical systems. Not just + ve ground. Nor just - ve ground. But both! So if you change cars, you can be almost certain that you can change over your Scorpio Mk. 2 as well.
Containing all the components you need, this Electro Spares Scorpio Mk. 2 Kit is simply built, using our easy-to-follow instructions. Each component is a branded unit by a reputable manufacturer and carries the manufacturer's guarantee. Ready drilled for fast assembly. Quickly fitted to any car or motor cycle. When your Scorpio Mk. 2 is installed, you instantly benefit from all these Scorpio Mk. 2 advantages
$\star$ Easier starting from cold $\star$ Firing even with wet or oiled-up plugs $\star$ Smoother running at high speed $\star$ Fuel saving $\star$ More power from your engine $\star$ Longer spark plug life $\star$ No more contact-breaker burn.
Electro Spares prices:
Deluxe Kit only $£ 11.50$ inc. VAT and $p \& p$. Ready Made Unit f14.75 inc. VAT and p \& p. State 6 V or 12 V system.
Send SAE now for details and free list.

## FM VARICAP STEREO TUNER

As featured in the May 1973 issue of 'Practical Electronics' Superb Hi-Fituner Kit now available from Electro Spares Including cabinet and all components - pre-set Mullard modules for R.F. and I.F. circuits. Motorola I.C. Phase Lock Loop Decoder for perfect stereo reception. No alignment needed. Guaranteed first time results - or send it back, and we'Il return it in perfect order (for a nominal handling charge). Electro Spares price only $£ \mathbf{2 8 . 5 0}$ inc. VAT and $p \& p$.

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## Easy to assemble

All parts are supplied - all you need provide is a soldering iron and a pair of cutters. Complete step-by-step instructions are provided, and our service department will back you throughout if you've any queries or problems.

## Total cost? Just $£ 16.45$ !

The Sinclair Cambridge kit is supplied to you direct from the manufacturer. Ready assembled, it costs $£ 27 \cdot 45$ - so you're saving $£ 11$ ! Of course we'll be happy to supply you with one readyassembled if you prefer - it's still far and away the best calculator value on the market.

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The kit comes to you pack aged in a heavy-duty polystyrene container. It contains all you need to assemble your Sinclair Cambridge. Assembly time is about 3 hours:

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WHENEVER some new idea or application appears on the public scene, we are often asked if we are going to publish a full project design so that constructors can make one. It may be that such an application has no existing off-the-shelf version that can be purchased by anyone.

Over the past year there has been a steady growth in the appearance of slot machines that offer two games of "tennis" or "football" for 10p. In the past six months they have been popping up like mushrooms, in pubs, restaurants, hotels, clubs, discotheques, railway stations and so on. Maddening, isn't it! There you are, confronted by a television screen and this white blob drifting about at random angles across the screen. How does it work? Can we make one for domestic television sets?

We hope that most of your questions on this subject, that have been coming to us recently, will be answered now. In this issue we start a do-it-yourself project that enables a domestic television set to be used to play "tennis". The principles employed are similar to the commercial version but the circuit design detail is totally original. We have carried out considerable work on this kind of project and have come up with a straightforward design for connection direct into the aerial socket of a u.h.f. 625 -line receiver. We must however warn constructors that it is not cheap to make and it is important that the published design detail must be strictly followed to avoid problems that can occur in using digital integrated circuits.
Having said this we sincerely hope that the lesser experienced constructor will not be frightened off by the amount of hardware used, because the project is not difficult to build if you take care at every stage and avoid using unknown or doubtful alternative components.
For the more experienced constructor who wants something of a challenge, we recommend that you follow the design starting in the July issue of "Television". By following through all stages you can make a "tennis" game (not the same design as that in P.W.) then progress to football and possibly golf. In the latter, the circuitry is more involved enabling you to move the players into any position on the "field". The design in Television depends on some connections being made inside the television set and you should have some knowledge or experience in television before tackling it.

With these two designs we hope to have satisfied a great deal of curiosity that has been aroused. They represent for both magazines a significant achievement in development that, so far as we are aware, is unparalleled in any other magazine. They are original in detail and a "double-first" for do-it-yourself magazines.
M.A. COLWELL-Editor

Fuba-Goon!


Peter's aerial system.

FUBA aerials (Audio Workshops Ltd.) have been supplied to Peter Sellers in his London home.
The requirement was for a top quality u.h.f. aerial signal in both colour and black and white to supply four outlets and to provide an excellent v.h.f./f.m. signal for home and continental reception.

It was decided to fit a Fuba XC 381 B u.h.f. aerial to cater for the three London channels, and a UKA Stereo 8 array with automatic rotator to cater for the f.m. requirement. Problems were encountered with reflections from nearby power station chimneys and other high buildings, but fitting the aerials on to a $15 \mathrm{ft} x$ 2 in mast overcame the main diffculties.

The Fuba UKA 8 f.m. was fitted to a 3 ft stub mast on a rotator on top of the 15 ft mast. The u.h.f. array was sited below the rotator and set for best possible results.

Audio Workshops Ltd. of Robertsbridge, Sussex are the sole UK distributors of Fuba Aerials. Audio Workshops Ltd., 29 High Street, Robertsbridge, Sussex.

## CQ column

THE CQ column is a valuable way of obtaining back numbers from other readers, but please reimburse expenses and the price of the magazines to those who have kindly offered to help!

## MinPosTel

THE Ministry of Posts and Telecommunications has been abolished. Mr. Anthony Wedgwood Benn the Secretary for Industry, becomes responsible for the Post Office.

Those parts of the MinPosTel relating to the Wireless Telegraphy Acts are under the wing of the Home Office and Mr. Roy Jenkins.

## Queen's Award

THE BBC announces that it has received the Queen's Award to Industry for the second time in five years. The award is for technological innovation in the transmission of sound and vision signals over a single vision link and relates to an original development by engineers of the Corporation's Research and Designs Departments.

## Stars af Henry's of Harrow

PETER SELLERS ably assisted by the Wombles of Wimbledon was the star attraction at the Gala opening of Henry's Hi-Fi Centre at Harrow recently.
Thousands of people turned up to see the festivities and in particular Peter Sellers-who lapsed into inspired "goonery" for a radio interview with Douglas Cameron of London Broadcasting. The Wombles set about encouraging the audience to tidy up the streets of Harrow just as they themselves do to Wimbledon Common!
After he had cut the ceremonial tape to officially declare the Hi-Fi Centre open, Peter Sellers then drew the winning entries for the Henry's $\mathrm{Hi}-\mathrm{Fi}$ Contest in which $£ 300$ of Hanimex stereo/audio equipment was given in prizes. Lucky winner was Mrs. Joanne Courtney, of Pinner View, Harrow. She won a complete stereo outfit and four runners-up each received cassette players. The contest was run in conjunction with London Broadcasting who gave live coverage to the opening.
Delighted at the crowds who turned up for the opening Henry's Retail Director, David French remarked "You can't beat the old-time showmanship when it comes to attracting the crowds. At times it was reminiscent of Beatlemania outside the store".
He had good reason to be pleased. The new Centre opened to bumper business and after the stars had left, the people of Harrow got down to the serious business of inspecting the vast range of hi-fi equipment on display.
The $\mathrm{Hi}-\mathrm{Fi}$ Centre at Harrow is the first in a series of suburban developments by the Henry's radio group-which has hitherto had a concentration of shops in Central London.


Peter Sellers and the Wombles at Henry's.

Arthur Bulgin, O.B.E.



FOLLOWING a short illness Mr. Arthur F. Bulgin, O.B.E., died at his home in Westcliffe on the night of Friday, 29th March, aged 75 years.
He was a well-known personality not only in Barking, Essex., where A. F. Bulgin \& Co. Ltd. manufactures an extensive range of electrical and electronic component parts, but also in the electronics industry, being one of the six founders in 1932 of the Radio \& Electronic Component Manufacturers Federation. Mr. Bulgin's passing marks the end of 51 years in the industry.

The chairmanship of the company now continues with his son, Mr. Ronald Bulgin who also shares joint managing directorship with A.F.B.'s brother, Mr. Stanley Bulgin.

Mr. Ronald Bulgin, M.A., C.Eng., M.I.E.E., has been with the company for over sixteen years. At the present time he is also chairman of the Radio \& Electronic Component Manufacturers Federation.

> SORRY WE ARE LATE! We apologise for the late appearance of Practical Wireless. The delay has been caused by an industrial dispute within the printing industry.


WITH a multi-band receiver it is convenient to have a ferrite rod aerial for long and medium wave reception and a telescopic aerial for the short wave bands, with provision for connecting an external aerial when necessary. This receiver is this type and the four bands tuned are approximately as follows
(1) $160-260 \mathrm{kHz}$ long wave.
(2) $575-1450 \mathrm{kHz}$ medium wave.
(3) $1 \cdot 8 \cdot 5 \cdot 0 \mathrm{MHz}$ shipping and short wave.
(4) $5 \cdot 7-15 \mathrm{MHz}$ general short wave.

The receiver has an inexpensive but robust case with a bottom compartment for holding logs of transmissions or other records. Five tuned IF circuits give good 'selectivity while the output stage provides adequate volume for ordinary purposes.

## MIXER STAGE

Switching is used to select any of the four bands and this unavoidably results in some complication of the frequency changer circuit. Despite this, there should be no particular difficulty, especially as the receiver can be tested with coils for one band only before adding the other connections for full coverage.
Fig. 1 shows the mixer stage in which a 7 -pole 4 -way switch is used. Operation will become clear if each section is dealt with separately.
When an external aerial is used it is taken to socket A1 and in LW and MW positions of S1 is connected to the winding L 4 on the ferrite rod. For normal MW or LW reception no external aerial is needed. In the other positions, Sl takes the aerial to the coupling windings L 7 or L 10 on the SW ranges.

Section S2 of the switch transfers the aerial tuning capacitor VC1 to Ll/L2 for LW/MW reception or to L5 or L8 on SW. Aerial connection A2 is for a telescopic aerial. To ensure that there is no loss of
efficiency due to errors in alignment, when aerials are changed, the panel trimmer VC3 is provided to peak this circuit. S3 transfers the base to L3 for MW and LW reception or to the base coupling windings L6 and L9 for SW. S4 short circuits the LW coil L2 for MW reception and for LW reception, S4 brings in C2 with the trimmer TC2, for appropriate coverage of the LW/MW oscillator coil L11.
Switch section S5 selects the appropriate collector coupling winding of the oscillator coils, L12 for LW/MW and L15 or L18 for the short wave ranges. S6 similarly switches the emitter circuits. The emitter bias resistor R6 in series with the LM/MW winding L13 is different value from R5, used for both SW bands, pernitting optimum results.

Switch section S7 transfers the oscillator tuning capacitor VC2 to the appropriate windings. C6 is a padder for the LW/MW coil L11, and TC3 and TC4 are trimmers on the SW coils L14 and L17.
A socket E allows an earth to be connected which is helpful when bringing in weak signals, in the $1 \cdot 8-5 \mathrm{MHz}$ range in particular. Much general listen. ing is of course possible on all frequencies with no external aerial. But reception of weak amateur and other signals on $1 \cdot 8 \cdot 2 \cdot 0 \mathrm{MHz}, 3 \cdot 5 \cdot 3 \cdot 8 \mathrm{MHz}$ and other bands will be greatly improved by an external aerial.

## IF AMPLIFIER

This is assembled on a separate board, using the circuit in Fig. 2. IFT1 and IFT2 are double tuned, but in IFT3 only the primary is tuned. As these IFT's are pre-aligned the cores should be left as they are, pending any slight final adjustment for best results.

This circuit gives very good sensitivity and selectivity. Audio output is taken from Dl to the volume control. The positive or earth line will go to the metal panel of the receiver when the amplifier is

A. Fig. 1. Circuit of the mixer stage whth four swithed ranges covering 160 kHz ? 1075 MHz .

Fig. 2. Two stage If amplifier circuit with diode detector which defives the audio amplifier, Fig. 3.



Fig. 3. Four transistor audio amplifier circuit completes the Severn portable receiver.
mounted. Other external connections are from pin 2 of IFTl to the mixer and from pin 3 of IFTl to the negative line of the mixer section. A lead from R7 will run to a supply point provided on the audio amplifier.

## AUDIO AMPLIFIER

Fig. 3 is the circuit of this section of the receiver, assembled on a separate board. Audio signals from the volume control VRl pass to the pre-amplifier Trl. Tr2 is the driver for the complementary output stage $\operatorname{Tr} 3 / \operatorname{Tr} 4$ and direct current feedback through the network R11 and R12 stabilises working conditions of driver and output stages. R13 with C6 introduce frequency compensation in audio feedback through this circuit.

Initially the pre-set VR2 is adjusted so that current drawn by the amplifier is about 7 mA to 9 mA with no audio signal. This is not a critical adjustment and the amplifier can be expected to give adequate power output with good quality of reproduction. As is usual with circuits of this kind, current drawn depends on the volume and will rise to peaks of 20 mA to 40 mA or so when volume is adjusted to a high level. A 150 hm speaker is most suitable for this circuit but the speaker should not be under $80 h m s$. With speakers of considerably higher impedance, such as 30 ohms , volume and current consumption are somewhat reduced.

In view of the fact that the receiver may be used for amateur band or other SW listening purposes when headphones are preferred, a jack outlet can be fitted. A $150 h m$ resistor is wired across this and any high or medium impedance headset plugged in.

## PANEL

A $10 \times 4$ in flanged universal chassis member is drilled to fit the tuning capacitor 4 in from the end, as in Fig. 4. Space it back slightly with washers so that the drive can fit correctly. The cursor against which the dial is read is a strip of Perspex about $3 x^{1}{ }_{2}$ in, with a vertical line, fixed with $8 B A$ bolts.


General view from the rear of the completed set.


Fig. 4. Layout of mixer stage. Transistor Tr1 is located to the rear of switch wafer S5-7 and wired directly to the switch tags. See photograph.

Fig. 5. Wiring underneath the mixer stage board. It may be necessary to drlll holes to clear the adjust/ng screws on TC1 and TC2.


The switch and VC3 are $2^{3}{ }_{4}$ in from $\mathrm{VCl} / 2$. Drill a $6 \times 3$ in paxolin board and the lower flange so that these can be bolted together as in Figs. 4 and 5. The tags MC are for connections to the metal chassis.

## MIXER ASSEMBLY

As the full band switching results in quite a lot of wiring, this is probably the most difficult section. Referring to Fig. 4, A is the Range 4 oscillator coil and $B$ the Range 4 aerial coil, $C$ is the Range 3 oscillator coil and $D$ the aerial coil. E is the LW/MW oscillator coil and its pins are wired underneath as in Fig. 5.

Connections to the switch are shown in Fig. 6. S1, S2, S3 and S4 are on the wafer nearest the panel, seen from behind. S5, S6 and S7 are similarly the contacts of the rear wafer. As contacts for sections S3 and S4, in particular, cannot be reached when the switch is fitted, lengths of thin insulated connecting wire should be soldered on first. It is of course essential that switch connections are correct. There should be no difficulty in seeing how the switch works. If there is, check its operation with
a meter or any other means of indicating continuity, for each position in turn.

S2 and S7 are near VC1 and VC2, as in Fig. 4. All other leads should be reasonably short and direct. Place Trl near the rear wafer with collector to S 5 and emitter to S6, Fig. 6. Take the base lead down to C3, Fig. 4, and the screen lead to the positive line. It may be preferred to wire in coils A and B only, at first, and to test the receiver, adding the other bands afterwards.
Leave flying leads from Cl and Sl for aerial connections later. Also provide leads to run to the IF board.

## FERRITE AERIAL

Two small brackets are bolted as in Fig. 4, holding vertical strips of paxolin about $2^{1} 2^{2} \mathrm{I}_{2}$ in each with a notch in the top to take the aerial rod which is secured with thread or elastic through holes in the strips.

The MW winding lies over TC4, its large winding is L1 and small winding L3. The LW winding has a tapping, and it is necessary to connect this coil so that the tapping is electrically near the earthed end.




Fig. 6. Connections to switches S1-4 on the front wafer and S5-7 on the rear wafer.

Should it subsequently prove impossible to align the aerial circuit on long waves, slide the LW winding off the rod, turn it over, then replace it. The external coupling winding L4 can be anywhere near the centre of the rod and its leads are connected from S1 to MC.

## IF BOARD WIRING

The IF board is $3_{2} \times 1{ }^{3}{ }_{4}$ in and Fig. 7 shows both sides. Drill holes for the IFT pins and screening can tags not forgetting a central hole to allow the lower cores to be reached for tuning. A very small round file will be helpful if some holes are not quite exactly placed.

Two tags MC are fixed with $\mathbf{1}_{2}$ in 6BA bolts for chassis returns. Connect up according to Fig. 7, placing sleeving on any leads where this is necessary. Cl and Dl must be wired in with the correct polarity. This section is very straightforward and there is plenty of space for components.

The completed amplifier can be tested before fitting by connecting the volume control from the pin VR1 to MC and placing the lead from a signal generator near to pin 2 of IFT1. Audio output from the diode can be checked with phones or an audio amplifier. With low input from the generator the five cores can be adjusted for best results, using a correctly fitting tool (such as the TT5, available from the IFT maker). Only a very small adjustment should be necessary for any core.

The IF board is mounted by passing the one bolt through a hole in the mixer board, Fig. 5. At the other end of the IF board a strip of metal runs from the MC tag bolt to the flange of the panel, to which it is secured.

## AUDIO BOARD WIRING

This board is $3^{3}{ }_{4} \times 1^{1}$ in and is wired as in Fig. 8. Two bolts with tags again provide MC return points. Veropins are inserted for external connections to speaker, battery negative, Rl and for the negative lead from the IF board.

## components list

## MIXER BOARD

Resistors

| R1 | $10 \mathrm{k} \Omega$ | R3 | $470 \Omega$ | R5 | $1 \mathrm{k} \Omega$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R2 | $2 \cdot 2 \mathrm{k} \Omega$ | R4 | $150 \Omega$ | R6 | 3.9k $\Omega$ |
| Capacitors |  |  |  |  |  |
| C1 | 22pF | C3 | $0.01 \mu \mathrm{~F}$ | C5 | $0.01 \mu \mathrm{~F}$ |
| C2 | 150 pF | SM C4 | $0.01 \mu \mathrm{~F}$ | C6 | 200pF SM |
| VC1/2 $208+176 \mathrm{pF}$ (Jackson Type 00) |  |  |  |  |  |
| VC3 50 pF variable (Jackson Type C804) |  |  |  |  |  |
|  | /2 60pF | F preset |  | 30p | F preset |

## Inductors

Blue range $3 T$ and $4 T$. Red range $3 T$ and $4 T$ (Denco-For transistor usage)
MW/LW Oscillator coil (Denco TiOC1)
MW/LW Ferrite rod aerial (Denco)

## Miscellaneous

Tr1, AF117. Switch, 7(8) pole, 4 way on two wafers (each wafer 4 pole 4 way). Paxolin sheet, $6 \times 3 \mathrm{in}$. Slow motion drive (Jackson 4489/C).

## IF BOARD

## Resistors

| R1 | $56 k \Omega$ | R4 | $22 k \Omega$ | R7 | $560 \Omega$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R2 | $680 \Omega$ | $R 5$ | $4 \cdot 7 \mathrm{k} \Omega$ | VR1 | $5 k \Omega$ log. pot. |
| R3 | $8 \cdot 2 k \Omega$ | R6 | $1 \mathrm{k} \Omega$ |  | with switch $\mathbf{S 8}$ |

## Capacitors

| C1 | $10 \mu \mathrm{~F}$ | 6 V | C 3 | $0.047 \mu \mathrm{~F}$ | C5 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| C 2 | $0.047 \mu \mathrm{~F}$ | C 4 | $0.04 \mu \mu \mathrm{~F}$ |  |  |
|  | $0.047 \mu \mathrm{~F}$ | C6 | $0.01 \mu \mathrm{~F}$ |  |  |

## Semiconductors

Tr1 AF117 Tr2 AF117 D1 OA81

## Miscellaneous

IFT1/2 (Denco IFT18/465). IFT3 (Denco IFT14). Plain veroboard, $0 \cdot 15 \mathrm{in}$. matrix, $3 \frac{1}{2} \times 1 \frac{\mathrm{in}}{}$.

## AUDIO BOARD

## Resistors

| R1 | $\mathbf{2} \cdot 7 \mathrm{k} \Omega$ | R6 | $100 \Omega$ | R11 | $\mathbf{2} \cdot \mathbf{2 k} \Omega$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R2 | $47 \mathrm{k} \Omega$ | R7 | $680 \Omega$ | R12 | $3 \cdot 9 \mathrm{k} \Omega$ |
| R3 | $3 \cdot 3 \mathrm{k} \Omega$ | R8 | $39 \Omega$ | R13 | $390 \Omega$ |
| R4 | $150 \Omega$ | R9 | $\mathbf{5} \cdot 6 \Omega$ | VR2 | 50 |
| R5 | $1.200 \Omega$ |  |  |  |  |
| R5 | $1 \cdot 2 \mathrm{k} \Omega$ | R10 | $5 \cdot 6 \Omega$ |  | WW preset |

## Capacitors

| C1 | $2 \mu \mathrm{~F}$ | 6 V | C 3 | $8 \mu \mathrm{~F} 6 \mathrm{~V}$ | C5 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{C} 250 \mu \mathrm{~F}$ | 10 V |  |  |  |  |
|  | $100 \mu \mathrm{~F}$ | 10 V | C 4 | $100 \mu \mathrm{~F} 6 \mathrm{~V}$ | C 6 |
|  |  | $25 \mu \mathrm{~F}$ | 6 V |  |  |
|  |  | C 7 | $100 \mu \mathrm{~F}$ | 10 V |  |

## Semiconductors

Tr1 OC71 Tr2 AC128 Tr3 AC128 Tr4 AC176

## Miscellaneous

Plain veroboard, 0.15 in . matrix, $4 \times 1 \frac{1}{2} \mathrm{in}$. Speaker 15S, 3 in. (Up to $6 \times 3 \frac{1}{2}$ in. can be accommodated)

## All resistors 5 or $\mathbf{1 0 \%} \ddagger$ or $\ddagger W$

CABINET ETC.
Panel, $10 \times 4$ in., flanged universal chassis member Cabinet top, $10 \times 2 \mathrm{in}$., universal chassis member (Home Radio)
Plywood 6 mm . Sides $9 \times 37 \mathrm{in}$. (2). Baffle $10 \times 4 \mathrm{in}$. Bottom $10 \times 3 \frac{1}{2} \mathrm{in}$. Back $10 \frac{1}{\frac{1}{2}} \times 8 \frac{1}{\frac{1}{2}} \mathrm{in}$. Drawer $10 \times 1 \mathrm{in}$. and $8 t \times 3 t$ in.
Telescopic aerial. Knobs. Handle.


In this view of the Severn portable the mixer stage transistor Tr1 can be clearly seen at the rear of the wafer switch, teft. The audio board is mounted on the front panel. The If board Is below the rlght-hand end of the ferrile rod aerial.


Fig. 7. top, gives location of IFT's and remaining components of the IF amplifler. Below, wirlng of IF boaid. It is very important that the polarity of the diode DI Is correctly observed.

The completed board fits above VC3 and the volume control. To avoid drilling the receiver panel, extra nuts are put on the bolts and locked to a strip/piece of metal which is in turn held in position by the bushes of VC3 and VR1. After the amplifier has been fitted in this way, connections to the IF board, and VR1 and the on/off switch can be completed. The battery supply should not be connected until the speaker is wired to the amplifier.

With the switch set for the highest frequency band, check the coverage obtained. This can be modi-
fied at the low frequency end of the band by adjusting the core of L17 and at the high frequency end of the band by adjusting trimmer TC4. The panel trimmer VC3 should peak up signal strength throughqut the whole tuning range. Adjust the core of L8 until this is so. VC3 should not be fully open or fully closed, with or without an external aerial or with the telescopic aerial extended. If necessary, TC4 may be re-adjusted to secure this result.

The receiver is then switched to the lower SW range and TC3, L14 and L5 similarly adjusted. The


Fig. 8. The two sides of the audio amplifier board, Again, check polartty of the several electrolytic. capacitors. VR2 may be replaced by a fixed resistor whose value may be found by first wiring in a potentiometer and adjusting it as described in the text.
next switch position is for MW reception and band coverage depends on Lll and TCl. Subsequently, move Ll on the ferrite rod for maximum volume when receiving signals near the LF end of the band (VCl/2 nearly closed). With correct alignment, very little re-adjustment of VC3 will be necessary, when tuning through the range.

The final position is for LW reception and alignment is obtained by moving L2 on the rod and adjusting TC2. The windings can be fixed with adhesive, when correctly positioned and coil cores may be locked with 6BA nuts.

## CABINET

Each side of the cabinet is plywood $9 \times 33_{4}$ in and cut back to $2^{1}{ }_{4}$ in at the top to form a slope 4 in long. Two 6BA bolts each side secure the $10 \times 2 \mathrm{in}$ universal chassis flanged member which is flush with the back and $\mathrm{i}_{8}$ in from the top. This member is covered with self-adhesive material before fitting.

Secure the receiver lin from the bottom, also inset about $1_{8}$ in, with two bolts each side. A piece of plywood $10 \times 4$ in with top and bottom edges bevelled is cemented to the plywood sides only. Corner strips cemented inside will strengthen this. Cut a 3in dia speaker aperture, sandpaper and varnish this baffle before fitting. Cover the hole inside with speaker gauze. Screw on the speaker from behind, using a piece of hardboard with aperture if necessary, and checking that screws cannot penetrate the front.

The bottom is $10 \times 31_{2}$ in plywood, cemented in, with the back $10^{1}{ }_{2} \times 8^{1}{ }_{2}$ in hinged to it. Two selftapping screws through the back into the top runner hold the back closed. Screw a carrying handle to the top. The drawer is plywood, sliding between


The finished chassis before mounting in the cabinet.
strips cemented to the case sides and the case bottom and is lin deep.

A strip of scrap metal about $7 \times \operatorname{lin}$ is bent to hold the PP9 battery which is placed with its fasteners towards the wooden side. This strip is held by a screw securing the carrying handle, and screws into the side.
A black socket on the side is used for Earth and is connected to the panel by a tag held by one of the fixing nuts. A red socket for an external aerial is connected to S1. C1 may be connected to a telescopic aerial mounted on the side of the case. Alternatively, fit another socket, so that a short aerial, consisting of a few feet of flexible wire, can be plugged in here, for short wave reception. It is possible to remove the receiver without disturbance to the cabinet by unscrewing the four bolts holding the panel.



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## SGS TBA651 RADIO TUNER

DURING the past few years many new types of integrated circuits have been introduced which are specifically designed for use in radio receivers. The use of such devices enables smaller, high performance radio receivers to be produced. In addition, the reduced number of components results in the labour cost of assembling the receivers being minimised.

## Description

The TBA651 contains the RF, oscillator, mixer and IF stages of a conventional type of superheterodyne receiver in a single integrated circuit. In addition, it contains a voltage regulator which keeps the performance almost constant as the supply voltage and/or temperature vary.

It is not possible to include tuned circuits on the silicon chip so they must therefore be connected externally to the device. In addition, some decoupling capacitors are required as well as a detector and an audio amplifier.


The TBA651 can be used in high quality domestic radio receivers and in car radio receivers for amplitude modulated signals at input frequencies up to 30 MHz ( 10 metres). The device provides high gain, low noise and an excellent AGC characteristic. It is encapsulated in a 16 pin quad-in-line plastic case, the outline of which is shown in Fig. 1. IC's of this


Fig. 2. Suggested circuit for a radio receiver designed around the TBA651. A capac/tor, about $0.1 \mu F$, must be used to couple the audio output to the audio amplifier as DC is present at the output. A ferrite rod aer/al may replace $L 1$ and $L 2$. Permeability tuning could be used in car radio applications.
type have alternate pins on each side of the body bent so that their ends form four lines (as shown in the end view). Sockets for these devices are not readily available and it is generally more convenient to solder directly to the pins.

## Circuit

A typical circuit using the TBA651 is shown in Fig. 2. It includes a diode detector D1, which can feed an audio amplifier consisting of either discrete components or another integrated circuit.

The aerial signal is coupled to the input of the RF stage at pin 1 by means of Ll and the tuned circuit L2/VCl. The output signal from the RF amplifier appears at pin 2 across the tuned circuit L3/VC2. The two tuned circuits provide good image signal rejection. The capacitor connected to pin 3 provides AGC decoupling.

A signal taken from the tapping on L3 is fed to the mixer input, pin 4. The local oscillator tuned circuit is connected to pin 6 and the feedback winding to pin 7 . The three variable capacitors VCl , VC2 and VC3 are ganged together and form the tuning capacitor.

The output from the mixer stage at pin 5 appears across the tuned circuit containing L6 and then coupled into the second IF tuned circuit containing L7, then feeding into the IF amplifier input stage at pin 13. The IF output appears at pin 10 across the tuned circuit containing L8. It is coupled to the untuned circuit containing L9 and detected by D1. It is filtered by the two $4 \cdot 7 \mathrm{nF}$ capacitors and the $1.5 \mathrm{k} \Omega$ resistor to remove the IF signal before being passed to the volume control and hence to the output.

It is important to note that the audio output from the volume control contains a steady voltage in addition to the audio signal. The output must therefore be capacitively coupled to the audio amplifier. A $0 \cdot 1 \mu \mathrm{~F}$ capacitor may be used.

## Power supply

The TBA651 can be operated from a power supply voltage as low as $4 \cdot 5 \mathrm{~V}$. The normal maximum operating voltage is about 16 V but the device may be damaged if the absolute maximum permissible voltage of 18 V is exceeded. The device requires about 12 mA from a 12 V supply, but much less at lower supply voltages.

## Improvements

The simple circuit of Fig. 2 contains only three IF tuned circuits. The performance may be improved by the use of a more complex filter between pins 5 and 13 , consisting of a number of tuned circuits resonant at the IF. However, it is generally more convenient to use one of the ceramic filters which are available. For example, the Toko filters contain an input and output tuned circuit coupled by a resonant ceramic disc. Such filters can provide a selectivity curve with the desirable flat top for good quality reproduction and the very steep skirts desirable for good adjacent channel selectivity. Nevertheless, ordinary tuned circuits are also required to provide good selectivity at frequencies away from the desired signal.

Filters of this type may have a pass band at least 6 kHz wide (within the -6 dB limits) and a response over 26 dB down at 10 kHz on each side of the centre frequency.

## Performance

The gain of the RF mixer and IF stages are respectively about $20 \mathrm{~dB}, 40 \mathrm{~dB}$ and 60 dB without AGC, but the losses associated with the tuned circuits must be subtracted from these values.

Fig. 3 shows how the output voltage from the receiver varies with the input level. The upper curve is for a 1.6 MHz signal modulated at $30 \%$ at 1 kHz , whilst the lower curve is the noise output when an unmodulated signal is fed to the input. It can be seen from the upper curve that the AGC action results in the audio output increasing from 0.5 V at $20 \mu \mathrm{~V}$ input level to only 1 V at about 0.5 V input. AGC is applied to the RF and mixer stages.


Fig. 3. Graph demonstrating the AGC characteristic of the TBA651.
The vertical distance between the two curves is a measure of the signal-to-noise ratio at the input level concerned. The high gain of the RF stage is largely responsible for the good signal-to-noise ratio even at low input signal voltages. The AGC applied to the RF stage is delayed until the input voltage exceeds a certain level so that the gain of the RF stage is a maximum at low input voltages thus providing a maximum signal-to-noise ratio. The amount by which the AGC is delayed can be reduced by connecting a resistor between pins 3 and 15 or increased by connecting a resistor between pins 3 and 14.
The TBA651 is a well-known device which is equally useful to the equipment manufacturer and to the amateur experimenter. Although no band switching is shown in Fig. 2, this circuit is suitable for use from the long wave band up to the highest short wave frequency used for long distance communication.

The TBA651 is available from Ambit International Ltd., 37 High Street, Brentwood, Essex, CM14 4RH at about $£ 1 \cdot 82$ at the time of writing. This company also stocks Toko ceramic filters suitable for use with the IC.

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## understanding



## Typical Driver-output Circuits

In Fig. 12 a current source is used to drive the output transistors. A voltage gain can be provided in the output stages, which is an advantage in reducing the swing demanded from the previous stage. Another possible arrangement is shown in Fig. 13. Since this output stage has a unity gain this does give good thermal stability, but demands a high output swing from the previous circuit. Although integrated circuits are available for supplies of $\pm 40 \mathrm{~V}$ (such as the MC1536) their slew rate is inadequate and a completely discrete pre-driver stage is essential.

This circuit can be modified for a small gain


Fig. 12: A fully complementary driver-output circult, using current drive for the output transistors.
(perhaps 5 times), as in Fig. 14, but the thermal stability is reduced and care must be taken in designing the DC conditions. However this basic configuration is very popular, and several variations are found in practical circuits. It has been shown that if $\mathrm{Z}_{1}$ is inductive this can increase crossover switching spikes, but if made capacitive may reduce switching spikes. In some designs a capacitor in the order of $0 \cdot 1 \mu \mathrm{~F}$ may be connected across $\mathrm{Z}_{1}$. In addition a capacitor in the order of 1000 pF may be connected across R3 to control the frequency response of the output stage.


Fig. 13: One half of a unity gain driver-output circuit, using current drive for the output transistor.

## Complete Circuit

To illustrate this article the circuit of Fig. 15 was constructed. The required voltage gain is provided by the integrated circuit, supplemented by the output stage, while the current gain is given by the class B output stage. The BC109 small signal transistor allows the potentiometer to set the quiescent current. There is $100 \%$ overall negative feedback at DC to maintain the output close to earth potential under no signal conditions, and direct coupling to the load allows a good LF response without using a large coupling capacitor.
For this amplifier graphs of distortion against output power level are shown in Fig. 16. For a 9 kHz signal the distortion is below $0.02 \%$ for all power levels up to 4 watts, and rises to $0.1 \%$ at 30 watts.


Fig. 14: One half of a driver-output circuit which gives a small voltage gain.

The 741 integrated circuit has a gain of 60 dB at 1 kHz , falling to 40 dB at 10 kHz , a factor of 10 . This is manifest in the distortion measurements at 10 kHz , where the levels are approximately ten times that of the 1 kHz measurements. This illustrates the importance of maintaining a high loop gain throughout the audio band.

The photographs show the results on the basic amplifier under various circuit conditions.


Photograph 1 Here the output power level is 5 watts with no quiescent current in the output transistors. The upper trace shows the output of the integrated circuit (pin 6), while the lower trace shows the power amplifier output. The overall feedback is inadequate to completely reduce the crossover distortion.


Photograph 2 Here the output power level is 100 mW , with no quiescent current for the output transistors. This clearly shows the 0.3 volts step at the integrated circuit output as the loop gain attempts to 'force' the output stage through the non-linear region.


Photograph 3 Here the output power level is 100 mW , with 20 mA quiescent current for the output transistors. Neither the integrated circuit output nor the power amplifier output show any trace of crossover distortion.


Photograph 4 This shows the output of the power amplifier for an output level of $50 \mu \mathrm{~W}$. Even at this very low level there is no trace of crossover distortion.

For photographs 1,2 and 3 the oscilloscope sensitivity for the integrated circuit output (upper trace) was five times that for the power amplifier output (lower trace).

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IOE12 WW KIT: 10 of each E12 value, 22 ohms-IM, a total of 570 (CARBON FILM 5\%), $63 \cdot 65$ net 25E12 WW KIT: 25 of each E12 value, 22 ohms-IM, a total of 570 (CARBON FILM 5\%), E3. 85 net $25 E 12$ WW KIT: 25 of each El2 value, 22 ohms-IM, a total of 1425 (CARBON FILM $5 \%$ ), $68 \cdot 35$ net $20 E 12$ W KIT; 20 of each EI2 value, 22 ohms-1M, a total of 1425 (CARBON FILM $5 \%$ ), $68 \cdot 45$ net I5EI2 IW KIT: 15 of each E12 value, 10 ohms-IM, a total of 1220 (METAL FILM $5 \%$ ), $\mathrm{Cl} 1 \mathrm{I} \cdot \mathbf{0 5}$ net IOEI2 2 W KIT: 10 of each EI2 value, 10 ohms-IM, a total of 915 (METAL FILM $5 \%$, © 13 . 35 net

## MULLARD POLYESTER CAPACITORS C280 SERIES

250VP.C. Mounting: $0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 0.033 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}, 3 \frac{1}{3} \mathrm{p} .0 .068 \mu \mathrm{~F}$,

MULLARD POLYESTER CAPACITORS C296 SERIES
$400 V: 0.001 \mu \mathrm{~F}, 0.0015 \mu \mathrm{~F}, 0.0022 \mu \mathrm{~F}, 0.0033 \mu \mathrm{~F}, 0.0047 \mu \mathrm{~F}, 2 \frac{1}{2} \mathrm{p}, 0.0068 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}$, $0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 0.033 \mu \mathrm{~F}, \quad 3 \frac{1}{2} \mathrm{p} .0 .047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, ~ 4 \frac{1}{2} \mathrm{p}, 0.15 \mu \mathrm{~F}, 6 \frac{1}{2} \mathrm{p}$. 160 V : $0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{FF}, 0.022 \mu \mathrm{~F}, 3 \mathrm{p}$.
5p. $0.22 \mu \mathrm{~F}, 5 \frac{1}{2} \mathrm{p} .0-33 \mu \mathrm{~F}, 6 \frac{1}{2} \mathrm{p} .0 .47 \mu \mathrm{~F}, 8 \frac{1}{2} \mathrm{p} .0 .68 \mu \mathrm{~F}, 12 \mathrm{p}, 1 \mu \mathrm{~F}, 14 \mathrm{p} .1 \mu \mathrm{~F}, 4 \frac{1}{2} \mathrm{p} .0 \cdot 15 \mu \mathrm{~F}$, MINIATURE CERAMIC PLATE CAPACITORS
50V: (pF) 22, 27, 33, 39, 47, 56. 68, 82, 100, 120, 150, 180, 220, 270, 330, 390, 470 . $560,680,820,1 \mathrm{~K}, 1 \mathrm{~K} 5,2 \mathrm{K2}, 3 \mathrm{~K} 3,4 \mathrm{K7}, 6 \mathrm{~K} 8,(\mu \mathrm{~F}) 0.01,0 \cdot 015,0.022,0.033,0.047$, $2 \frac{1}{2} \mathrm{p}$. each. $0 \cdot 1,30 \mathrm{~V}, 4 \frac{1}{2} \mathrm{p}$.
POLYSTYRENE CAPACITORS I60V 5\%
(pF) $10,15,22,33,47,68,100,150,220,330,470,680,1000,1500,2200,3300$.
$4700,4 p .6800,10,000.4 \frac{1}{2}$.


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MINIATGRE 0.25 W Vertical or horizontal 6 p each $1 \mathrm{~K}, 2 \mathrm{~K} 2,4 \mathrm{~K} 7$, IOK, etc. SUB-MIN 0.05 W Vertical, $100 \Omega$ to $220 \mathrm{~K} \Omega 5 \mathrm{p}$ each

## B. H. COMPONENT FACTORS LTD.

Miniature Mullard Electrolytics $1.0 \mu \mathrm{~F}$ 63V 61p

 $3 \cdot 3_{\mu} \mathrm{F} 63 \mathrm{~V} 6_{2}^{2} \mathrm{P}$
$4 \cdot 0 \mu \mathrm{~F} 40 \mathrm{P}$
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$15 \mu \mathrm{~F}$
163 V
$6 \frac{1}{2} \mathrm{P}$ $\begin{array}{lll}15 \mu \mathrm{~F} & 63 \mathrm{~V} & 6 \frac{2}{2} \mathrm{P} \\ 16 \mu \mathrm{~F} & 40 \mathrm{~V} & 6 \frac{1}{2}\end{array}$ $22 \mu \mathrm{~F} \quad 25 \mathrm{~V} \quad 6 \frac{1}{2} \mathrm{P}$ $22 \mu \mathrm{~F} \quad 63 \mathrm{~V} \quad 6 \frac{1}{2} \mathrm{P}$ $32 \mu \mathrm{~F}$ 10V $6 \frac{1}{2} \mathrm{P}$ $33 \mu \mathrm{~F}$ 16V $6 \frac{1}{2} \mathrm{P}$ $33 \mu \mathrm{~F}$ 40V 6 $\frac{1}{2} \mathrm{P}$ $32 \mu \mathrm{~F} 63 \mathrm{~V}$ 6i $\frac{1}{3} \mathrm{P}$ $47 \mu \mathrm{~F} \quad 10 \mathrm{~V}$ 6 $6 \frac{1}{2} \mathrm{p}$ $47 \mu \mathrm{~F}$
$47 \mu \mathrm{~F}$ 25 V 6站 P $\begin{array}{llll}47 \mu \mathrm{~F} & 25 \mathrm{~V} & 6 \frac{1}{2} \mathrm{p} & 2200 \mu \mathrm{~F} \\ 47 \mathrm{~F} & 6 \mathrm{~V} 25 \mathrm{p} \\ 43 \mathrm{~F} & 63 \mathrm{~V} & 8 \mathrm{p} & 3300 \mu \mathrm{~F} \\ 6.426 \mathrm{p}\end{array}$ $150 \mu \mathrm{~F} \quad 16 \mathrm{~V} 6 \frac{1}{2} \mathrm{p}$ $150 \mu \mathrm{~F} \quad 63 \mathrm{~V}$ isp $220 \mu \mathrm{~F} 6.4 \mathrm{~V} 6 \frac{1}{2} \mathrm{P}$ $220 \mu \mathrm{~F}$ loV $6 \frac{1}{2} \mathrm{P}$
$220 \mu \mathrm{~F}$ $220 \mu \mathrm{~F}$
$220 \mu \mathrm{~F}$
33 V 8 p $\begin{array}{ll}220 \mu \mathrm{~F} & 63 \mathrm{~V} 21 \mathrm{p} \\ 330 \mu \mathrm{~F} & 16 \mathrm{~V} 12 \mathrm{p} \\ 330 \mu \mathrm{~F} & 63 \mathrm{~F}\end{array}$ $\begin{array}{ll}330 \mu \mathrm{~F} & 16 \mathrm{~V} 12 \mathrm{p} \\ 330, \mu \mathrm{~F} & 63 \mathrm{~V} 25 \mathrm{p} \\ 470 \mu \mathrm{~F} & 6.4 \mathrm{P}\end{array}$ $\begin{array}{ll}470 \mu \mathrm{~F} & 6-4 \mathrm{~V} 9 \mathrm{p} \\ 470 \mu \mathrm{~F} & 40 \mathrm{~V} 20 \mathrm{p}\end{array}$ $\begin{array}{ll}470 \mu \mathrm{~F} & 40 \mathrm{~V} 20 \mathrm{p} \\ 680 \mu \mathrm{~F} & 16 \mathrm{~V} 15 \mathrm{p}\end{array}$ $680 \mu \mathrm{~F} 40 \mathrm{~V} 25 \mathrm{p}$ $1000 \mu \mathrm{~F} 16 \mathrm{~V} 20 \mathrm{p}$ $1000 \mu \mathrm{~F} 25 \vee 25 \mathrm{p}$ $1500 \mu \mathrm{~F} 6.415 \mathrm{p}$
$1500 \mu \mathrm{~F}$
$16 \vee 25 \mathrm{p}$
$68 \mu \mathrm{~F} \quad 16 \mathrm{~V} 6 \mathrm{tp}_{\mathrm{p}}$ $\begin{array}{ll}100 \mu \mathrm{~F} & 25 \mathrm{~V} 6 \frac{1}{2} \mathrm{p} \\ 100 \mu \mathrm{~F} & 63 \mathrm{~V}\end{array}$

POTENTIOMETERS
Carbon Track $5 K \Omega$ to $2 \mathrm{M} \Omega$, log or tin. Single, $16 \frac{1}{2} \mathrm{p}$ Dual Gang 46p. Log Single with switch 26p p. 45 mm . 47 p. $60 \mathrm{~mm}, 55$ p.


AMBIT $=$
37A HIGH STREET BRENTWOOD ESSEX CM14 4RH (216029) New prices -*100+ applies to mixes of multiples of 10 per item.

| TYPE NUMBLR 1-19 | 20-99 | 100-999 | $\begin{array}{r} \text { MIX } \\ * 100+ \end{array}$ |
| :---: | :---: | :---: | :---: |
| AUDIO |  |  |  |
| L.M380 (2-3w amp) 1.00 | 0.90 | 0.75 | 0.80 |
| L1:381 (dual pre) 1.85 | 1.63 | 1.33 | 1.45 |
| TBA810S ( 7 w amp) 1.50 | 1.17 | 0.90 | 1.08 |
| P, 3010 |  |  |  |
| CA3089E (FM IF) 1.95 | 1.55 | 1.31 | 1.42 |
| CA3053 (IF AIP) 0.52 | 0.38 | 0.31 | 0.37 |
| TBA120 (FP:i IF) 1.00 | 0.85 | 0.52 | 0.55 |
| TEA651 (AM/FM/SSB) 1.30 | 1.46 | 1.13 | 1.25 |
| CA3123E (AM) 1.40 | 1.13 | 0.94 | 1.14 |
| uA753 (FM gain) 0.99 | 0.78 | 0.65 | 0.77 |
| STEREO |  |  |  |
| MC1310 (PLL DEC.)2.85 | 2.30 | 1.80 | 2.04 |
| CA30900 (PLL DLC.)3.75 | 3.25 | 2.55 | 2.85 |
| PLL |  |  |  |
| NE561B 3.19 | 2.75 | 2.07 | 2.24 |
| NE562B 3.19 | 2.75 | 2.07 | 2.24 |
| iJE565/LM5G5 2.75 | 1.80 | 1.50 | 1.85 |
| NE567/LMi567 2.75 | 1.80 | 1.50 | 1.85 |
| Reculaturs |  |  |  |
| LM309K 2.20 | 1.80 | 1.50 | 1.80 |
| UA7805 $\quad 1.75$ | 1.32 | 1.07 | 1.30 |
| UA7012 1.75 | 1.32 | 1.07 | 1.30 |


| Regulators (contd.) 1-19, 20-99 |  | 100-999 * 100+ |  |
| :---: | :---: | :---: | :---: |
| UA723C 0.30 | 0.66 | 0.52 | 0.66 |
| NE550A 0.80 | 0.66 | 0.42 | 0.66 |
| OP AMPS |  |  |  |
| 741CV 0.40 | 0.34 | 0.32 | 0.35 |
| LM3900 (Quad amp) 0.66 | 0.53 | 0.45 | 0.53 |
| (710 Comp.) 0.52 | 0.40 | 0.34 | 0.40 |
| OTHERS |  |  |  |
| ICL.8038CC (funct.gen)3.10 | 2.85 | 2.18 | 2.47 |
| NE555V $\quad 0.78$ | 0.66 | 0.52 | 0.66 |
| LM1496 1.02 | 0.67 | 0.55 | 0.66 |
| see our new '74 A4 size catalogue for details of our range of devices and products. |  |  |  |
| TOK0 inc. (mix price applies to TOK0 items only here) |  |  |  |
| CFS10.7 0.45 | 0.38 | 0.26 | 0.34 |
| CFT455B \& C 0.45 | 0.38 | 0.25 | 0.36 |
| CFU455 0.50 | 0.43 | 0.32 | 0.39 |
| MFFHIT or 71T 1.40 | 1.24 | 1.02 | 1.15 |
| KACS586 (FM quad. det)0.30 | 0.22 | 0.14 | 0.20 |
| BLR2011N (19\&38kHz) 1.95 | 1.67 | 1.23 | 1.45 |
| 5.1 mH \& 43 mH min . chokes 27 | 0.21 | 0.15 | 0.20 |
| 2 mH choke for CA30900 . 30 | 0.22 | 0.14 | 0.20 |
| ET703UA FM tunerhead with AM gang. |  |  |  |
| 3.50 | 3.00 | 2.35 | 2.45 |
| LP1186(FM tunerhead) 3.75 | 3.05 | 2.35 | 3.05 |
| LP1185 (FM IF) 3.90 | 3.17 | 2.45 | 3.09 |

## Trade and professional enquiries welcomed.

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CWO please. Credit accounts by prior arrangement only, payable monthly nett.
POSTAGE: Order value less than $£ 1$ : 18p
£5: 15p



Fig. 16: Total harmonic distortion measurements for the ampliffer of Fig. 15.
-continued from page 222 sink. This operational amplifier is suitable for DC servomechanisms, programmable power supplies, etc. Fig. 17 shows a 35 watts audio amplifier using two in a push-pull configuration. Similarly the RCA-HC2000 power hybrid operational amplifier can deliver 100 watts into a 4 ohm Ioad, as shown in Fig. 18.

## Conclusions

The reduction in $\beta$, the 0.6 V Vbe for each output transistor," and the other effects discussec here can cause an increase in dístortion at low and high signal levels. However the problems associated with distortion in power amplifiers can be solved, at a price. Certainly the best amplifiers are limited in perform-


Fig. 17: A 35W power amplifier using a push-pull output stage.


Fig. 18: A 100W hybrid power amplifier.
ance by the remainder of the $\mathrm{Hi}-\mathrm{Fi}$ system, the loudspeaker, microphone, tape recorder, pickup, etc., and the necessity for further distortion reduction in power amplifiers may be challenged. However there is a good case for increased power output in power amplifiers, since loudspeaker efficiency decreases with fidelity, and high power may be demanded to drive the very best loudspeakers on transients. Efficiency may be typically $0.5 \%$. At such power levels speaker and amplifier unit protection is essential, but that is another problem.


## Test Gear

I congratulate you on your decision to start a series of constructional projects on test equipment. It's a pleasant change from the unending series of amplifiers of astronomical output and everincreasing perfection that so many amateur constructional magazines publish.

Personally, I started taking "P.W." regularly in the hope that something which could be adapted for use in instruments would come up, so your series is very timely. In particular, a simple wobbulator to cover 465 kHz and $10 \cdot 7 \mathrm{MHz}$ for lining up I.F.s on a scope, a transistor voltmeter of enormous input impedence, a
gadget for tracing valve/transistor characteristics on a 'scope (which according to Mr. Scroggie can be done, but which may be too complicated) and a transistorised beam-splitting switch (as currently advertised by Chiltmead) are what I'd like.

I do, of course, totally disagree with your remarks about test equipment being uninteresting and wish you good luck in this new line.-R. G. Roberts (Herts)

## Weaned on transistors?

It was with great interest that I read your "Going Back" article about the History of Practical Wireless. Might it be possible, however, to reprint some of your articles from these earlier issues to show these transistor weaned people what proper electronics is all about?!

I have written before on this subject, and there seemed to be some success for several months but then the valve disappeared again. As one of the multitude who delight in the thermionic glow, I would like to hear what other readers think on the sub-ject!-T. G. Watton (Kingston upon Hull.

## Surplus Gear

In your "C Q" feature, there are numerous queries for information on Government Surplus Equipment. I feel it would be of assistane to the interested parties, to obtain the book on the subject, called "Govt. Surplus Wireless Equipment Handbook."

I have no connection with the publisher, but have recently purchased one from Gerald Myers, 18 Shaftesbury St., Leeds LS12 3BT.-K. F. Tunnicliffe (Leics).

## WIRELESS TELEGRAPHY ACT

Readers and advertisers are reminded of the requirements laid down by the Wireless Telegraphy Act. It is an offence in the U.K. to install or operate wireless telegraphy apparatus except under the provisions of the Act and, except in the case of broadcast sound-only receivers, a licence must be obtained.
Included within the provisions of the Act are any apparatus transmitting deliberate signals for any purpose such as "walkie-talkies", radiocontrolled models or servos and some types of metal detectors. Apparatus radiating interference signals are subject to controls which also come under the administration of the same Ministry. If you require full information, please write to Waterloo, Bridge House, Waterloo Road, SE1 8UA.

## LEEXETII

## IN THE JULY ISSUE

## TELEVISON GAMES

Most people will have seen the TV games machines installed in pubs and amusement centres and we have received many requests for information on how to adapt TV sets to operate in this way. A unit is required which will generate a video signal corresponding to the basic features of the game and the movement-under control of the players-of the ball. This month we start a series of articles which will present the basic information required. This will lead up to a football game in monochrome or colour with players which can be moved at controlled speed across the "pitch".

## AFC MUTING

When channel changing it is necessary to mute the á.f.c. applied to the tuner unit. This is generally
done by specially designed switch units which remove the a.f.c. for the required time. A simple Yaxley switch can be used if a slow-start power supply to the a.f.c. circuit is used. Details of the simple circuitry which makes this possible will be given.

## FAULT-FINDING/RENOVATING

The GEC 13in. portable Model 2015 dating from 1966 gives excellent results and is worth while renovating for use as a second set. John Law describes the set and the parts of the circuit that may require attention to bring the performance up to scratch.

## PLUS ALL THE REGULAR FEATURES

Details of the July issue are subject to the current national situation at time of going to press.


## ELEGTRO/ALIE

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## Everything ${ }^{\text {B }}$ rand ${ }^{(1)}$ New Atractive Discounts $\star$ Free Postage (U.K.)

TRANSISTORS
of many types from simple diodes to ICS photo-sensitive devices, threshold MINITRON DIGITAL INDICATORS
$3015 F$ Seven segment finament, compatible with standard logic modules. 0-9 and decimal point; 9 mm characters in 16 lead DIL (some alphabetica symbols avallable)
Suitable BCD decoder driver 7447
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DALY ELECTROLYTIC
$\begin{array}{ll}\text { in cans; plastic. } \\ 1000 \mathrm{mFF} / 25 \mathrm{~V} 28 \mathrm{p} & 1000 / 5041 \mathrm{p} \\ 5000 / 100 £ 2.91 & 2000 / 5057 \mathrm{p} \\ 5000 / 25 \mathrm{~V} 62 \mathrm{p} & 5000 / 50 \mathrm{£1} 1\end{array}$
2200/100 £1 56
POLYESTER TYPE C. 280
Radial leads for P.C.B. mounting. Working voltage
$0.01,0.015,0.022,0.033,0.047$
ea. 3p
$0.068,0.1,0.15 \mathrm{O}, 0.47 \mathrm{Bp}, 0.6811 \mathrm{p}, 1 \mathrm{ea} 14 \mathrm{p}$
1.521p; 2.2 24p

SILVERED MICA
Warking vortage 2.2 to 820 in 32 stages ea. $\mathbf{6 p}$ 1000, 1500 7p; $18008 p ; 220010 p ; 2700$, 3600 12p 4700. 5000 15p; 6800 20p; 8200, 10,000 25p

TANTALUM BEAD
$0.4,0.22,0.47,10 \mathrm{mF} / 35 \mathrm{~V}, \quad$ ea. 13 p
$2 \cdot 2 / 16 \mathrm{~V}, 2 \cdot 2 / 35 \mathrm{~V}, 4 \cdot 7 / 16 \mathrm{~V}, 10 / 6 \cdot 3 \mathrm{~V} \quad$ ea. 13p $4.7 / 35 \mathrm{~V}, 10 / 16 \mathrm{~V}, 22 / 6 \cdot 3 \mathrm{~V}$ ea. 16 p
10/25, 22/16V. $47 / 6 \cdot 3 \mathrm{~V}$ 100/3V
POLYCARBONATE
Type B42540 Working Voltage-250V
$0.0047 ; 0.0068 ; 0.0082 ; 0.01 ; 0.012 ; 0.015 \quad$ ea. 3p $0.018 ; 0.022 ; 0027 ; 0.033 ; 0.039 ; 0.047 ; 0.056$ ea. 4 p CERAMIC PLA
CERAMIC PLATE
In 26 values from 22 pf to 6800 pF, each, 2p

## POTENTIOMETERS

ROTARY, CARBON TRACK. Double wipers for good contact and long working life P. 20 SINGLE log. 4.7 Kohms megohms, ea. 14p ea. 14p JP. 20 DUAL GANG lin. $4 \cdot 7$ Kohms to $2 \cdot 2$ megohms, JP. 20 DUAL GANG $\log .4 \cdot 7$ Kohms to $2 \cdot 2$ megohms JP. 20 DUAL GANG Log/antilog 10K, 22K, 47K IP megohm ony P. 20 p ecades of 10,22 and 47 only available in ranges becad
Skeleton Carbon Presets Type PR, horizontal or ertical $6 p$ each.
SLIDER
Linear or log. 47 K to 1 meg. in all popular values
Escutcheon plates, black, white or light grey, ea. 10 p Control knobs, blk/wht/red/yel/grn/blue/dk. grey/t grey ea. 7p

## JACKS AND PLUGS

Sockets
-chrcuit unswitched S1/SS
12p
-circuit $/ 2$ break coniacts S $51 / \mathrm{BB}$
3-circuit unswitched (Not GPO) S3SSS
-circuit with 3 break contacts $\$ 3 /$ BBE 20
or grey unswitched S5/SS
with 2 break contacts S5/B
Miniature 3.5 mm 2 -circuit, (black) 2 br. cont $56 / \mathrm{BB}$
Plugs
side entry SEP1
Line socket mono 231
3 circuit unscreened, b1/grey/wh. P4 2 circuit, unscreened, bl/whi/red/b/grn/gry P2 18p 3 circuit screen top entry P3
side entry SEP3
, $3-5 \mathrm{~mm}$ 2-circult screened P5 $\quad 13$ p
Min. 3.5 mm 2-circ. unscrnd. various colours P6 10p

## EV CATALOGUE 2nd printing

## 12 pages, thousands of items; illustrations

 diagrams; much useful technical information The 2nd printing of this catalogue has been updated as much as possible on prices. costs only 25 por goods list value E5 or more.
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In moulded polypropylene, with nickel plate on rass. With insulating set, washers, tag \& nuts $15 \mathrm{~A} / 250 \mathrm{~V}$ in blk/brwn/red/yel/grn/b/gry/wh. Type TP.1, ea, 14p
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## ZENER DIODES

Full range E24 values: $400 \mathrm{~mW}: 2 \cdot 7 \mathrm{~V}$ to $33 \mathrm{~V}, 14 \mathrm{p}$ each W: 6.8 V to $82 \mathrm{~V},{ }^{21 \mathrm{p}}$ each: ${ }^{1.5 \mathrm{~W}: 4.7 \mathrm{~V} \text { to } 75 \mathrm{~V}, ~}$ 48 p e 3 ch . $20 \mathrm{~W}: 7.5 \mathrm{~V}$ to 75 V , 69 p each. Clip to

## RESISTORS

| Code Walls | Ohms | 1 to 9 | 10 to 99 | 100 up |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
|  |  |  | (see note below) |  |  |  |
| C | $1 / 3$ | $4 \cdot 7-470 \mathrm{~K}$ | 1.3 | 1.1 | 0.9 | nett |
| C | $1 / 2$ | $4.7-10 \mathrm{M}$ | 1.3 | 1.1 | 0.9 | nett |
| C | $3 / 4$ | $4.7-10 \mathrm{M}$ | 1.5 | 1.2 | 0.9 | nett |
| C | $1 / 4$ | $4 \cdot 7-10 \mathrm{M}$ | 3.2 | 2.5 | 1.9 | nett |
| MO | $1 / 2$ | $10-1 M$ | 4 | 3.3 | 2.3 | nett |
| WW | 1 | $0.22-3.9$ | 9 | 0 | 8 |  |
| WW | 3 | $1-10 \mathrm{~K}$ | 7 | 7 | 6 |  |
| WW | 7 | $1-10 \mathrm{~K}$ | 9 | 9 | 8 |  |

## Codes:

- carbon film, high stability, low noise $\mathrm{MO}=$ metal oxide, Electrosil

Values: All E12 except $C \frac{1}{3} W, C, W$, and $M O \frac{1}{2} W$. E12: $10,12,15,18,22,27,33,39,47,56,68,82$ E24; as E12 plus 11, 13, 16, 20, 24, 30, $3643,51$. $62,75,91$ and their decades

Tolerances:
$5 \%$ except WW $10 \% \pm 0.05 \Omega$ under $10 \Omega$ and MO $\frac{1}{2} W 2 \%$.
Prices are in pence each for quantities of the same ohmic value and power rating. NOT mixed values. (ifnoretor order.) Prices for 100 up in units of 100 only.

## VEROBOARD

Copper clad 0.1 matrix $-2.5 \times 3.75$ ins. $27 p: 3.75 x$ 3.75 ins. $-30 \mathrm{p}: 2.5 \times 5$ ins. $-30 \mathrm{p}: 3.75 \times 5$ ins. -33 p . Copper clad 0.15 in. matrix $2.5 \times 3.75$ ins. -20 p : $3.75 \times 3.75$
5 ins. -360

## Vero spot fa

Vero spot face cutter (any matrix) 48p. 0.052 pins (for 015 matrix) per $100-36$ p.

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BAXANDALL SPEAKER KIT
As designed by P. J. Baxandall and described originally in "Wireless World." Simple to assemble, fantastically good results and a greater money saver. Carries 10 watts RMS. 15 ohms impedance. Size $18 \mathrm{in} \times 12 \mathrm{in} \times 10 \mathrm{in}$. Complete kit including pack-flat cabinet, £1490
The size and weight of this product obliges us $t o$ charge 70 part cost of ca
Equalliser Assembly. $£ 2 \cdot 30$.
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| 124 | 0.5 | 24 |  | 0×6.7× | 6.1 | 0-24-30 | 0-40-48-60 | $2 \cdot 12$ | 36 |
| 126 | 1.0 | 34 | 8.9 | $9 \times 7.7 \times$ | $7 \cdot 7$ |  |  | 2.97 | 36 |
| 127 | $2 \cdot 0$ | 64 |  | $9 \times 9.6 \times$ | 8.6 |  |  | 4.67 | 42 |
| 125 | 3.0 | 812 |  | $1 \times 9.9 \times 10$ | 0.2 |  |  | 711 | 52 |
| 123 | 4.0 | 1312 | 12.1 | $1 \times 11.8 \times 10$ | 0.2 |  | . | $9 \cdot 20$ | 67 |
| 40 | 5.0 | 1200 | 14.0 | $0 \times 102 \times 11$ | 18 |  |  | 1083 | 87 |
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| 122 | 10.0 | 250 | 17.2 | $2 \times 12.7 \times 14$ | 4.0 |  |  | 22.10 | * |
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| 238 | 200 |  | 2 | $2.8 \times 2 \cdot 6 \times 2$ |  | 3-0-3 |  | 1.44 | 10 |
| 212 | iA IA | 1 | 4 | $6.1 \times 5 \cdot 8 \times 4$ | 8 | $0-60-$ |  | 1.67 | 22 |
| 13 | 100 |  | 4 | $3 \cdot 9 \times 2 \cdot 6 \times 2$ | . 9 | 9-0.9 |  | 1.23 | 10 |
| 235 | 330,330 |  | 4 | $4.8 \times 2 \cdot 9 \times 3$ |  | $0-9,0$ | 0.9 | 1.67 | 10 |
| 207 | 500, 5 |  | 00 | $6.1 \times 5 \cdot 4 \times 4$ | 4.8 | 0-8-9. | 9. 0-8 | $2 \cdot 23$ | 22 |
| 208 | IA, |  | 12 | $7.0 \times 6.4 \times 6$ |  | 0-8-9, | ,0-8-9 | 300 | 30 |
| 236 | 200. 20 |  | 4 | $4 \cdot 8 \times 2 \cdot 9 \times 3$ | 5 | $0-15$, | , $0-15$ | 1.67 | 10 |
| 214 | 300, 300 | 00 | 4 | $6.1 \times 5 \cdot 8 \times 4$ |  | 0-20, | 0-20 | 1.76 | 22 |
| 221 | 700 (0) | .C.) | 8 | $7.0 \times 6.1 \times 6$ |  | 20-12 | 2-0-12-20 | 1.55 | 30 |
| 206 | IA. IA | A 2 | 12 | 8. $3 \times 7$-7x7 | 0 | 0.15 | 20, 0-15-20 | 4.05 | 36 |
| 3 | 500. 50 | 002 | 4 | 8. $3 \times 7 \cdot 0 \times 7$ |  | 0-15-2 | -27, 0-15-27 | $3 \cdot 10$ | 38 |
| 204 | IA, IA | A 3 | 4 | $8 \cdot 9 \times 7 \cdot 7 \times 7$ |  | 0.15 .2 | 27, 0-15-27 | $3 \cdot 15$ | 38 |

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# LERANING BY PRAGTICAI PBODEGT STEPS <br> PART 9—POTENTIAL DIVIDER BIASING \& GROUNDED BASE AMPLIFIERS 

## (continued from the June issue)

We now move away to a different type of amplifier stage; the grounded base stage. The basic circuit is shown in Fig. 65. In many respects it looks similar to that we have just described but it has considerable differences. Signal input is at point $A$ (at the emitter) for a start. This circuit has very low input impedance and quite a high output impedance; it provides us with a very useful voltage amplification but no current gain. It is used when we have a signal source that has low resistance and very low output voltage (e.g. low impedance microphones or some guitar pick-ups). Unlike the grounded emitter stage there is no change of phase between input and output.

The resistors R3 and R4 provide a fixed bias so you can assume that the transistor is conducting on a linear portion of its characteristic and there will be a collector current flowing (ideally just sufficient to give us a mid rail output at the collector).

This collector current merges with base current within the transistor and emerges as emitter current. Most of the emitter current is made up of the original collector current. If we change the emitter current (by the application of an external signal at point A) we will-indirectly-alter the collector current. Because R2 is of small value it does not need much in the way of voltage at $A$ to create reasonable changes in current flowing through R2 (but, of course, the source of current must also have a low resistance). These changes in emitter current are converted, by the transistor, to similar changes in collector current flowing through R1 but as R1 has a high resistive value we will get much larger voltage changes across it than we applied to R 2 -hence voltage amplification. This is a very over-simplified explanation but we hope it conveys the operating method of the circuit without having to resort to complicated mathematics.

We can arrive at component values by using a similar technique to that adopted for the grounded emitter stage. The main difference is that we want to keep the quiescent potential at $\mathbf{A}$ as low as pos-sible-so that the voltages that generate our input


Fig. 65 : Basic circuil of a grounded base slage.
current are significant. In this case we have based our component calculations on the assumption that the potential at $A$ is to be approximately 200 mV . This means that the potential at $B$ will be +800 mV . It is essential that the base current we supply to the transistor is highly stable and as the bias chain is not going to create input impedance problems in this case we can arrange for a much higher standing current to flow through R3 and R4. To prevent the base potential being affected by signals we swamp any changes there might be with the large capacitor C1. Make up the circuit for Fig. 65 and measure the respective potentials and then go on to experiment with the working circuit of Fig. 66. The input signal should come from a very low impedance source but at the same time should be decoupled from the emitter of the grounded base stage as far as d.c. is concerned (Cl) otherwise we would alter our quiescent working point. We suggest an old miniature loudspeaker (any impedance from 3 to 35 ohms will do) as a microphone but you could use an ex Post Office telephone earpiece as a rough and ready microphone. Alternatively you could make up a crude form of guitar pick-up by winding about 100 turns of fine enamelled copper wire on an Eclipse button magnet. As soon as a


Fig. 66 : Using a grounded base stage to amplify a signal from a low impedence source. MIC 1 could be a $35 \Omega$ loudspeaker, a moving armature earpiece (or P.O. telephone earpiece) or a variable reluctance transducer-see Fig. 70.


Fig. 68: Changes in flux in the variable reluctance transducer cause the LED (D2) to flash. Simultaneously the potential at A drops in negative going spikes.


Fig. 67: Layout for Fig. 66.


Fig. 69 : Layout for Fig. 68.

piece of ferromagnetic material touches the magnet you should hear a loud "clunk" from the amplifier. A steel string vibrating between the poles will vary the reluctance of the magnetic circuit at the frequency of the string and this would give rise to a low a.c. output voltage from the transducer.

By modifying the circuit to that of Fig. 68 you can make the light emitting diode flash whenever a piece of iron, or steel, comes in contact with the transducer. Any low power LED will do for D2 but please take note of the connection polarity!


Tune round the exciting 2 metre VHF amateur radio band on your own short wave receiver! Converts the incoming signals to the 10 metre band. No special coils or components required and simple alignment virtually guarantees first-time operation. A small 9 V battery will operate the four transistor circuit.

## MANY OTHER CONSTRUCTIONAL ARTICLES, SPECIAL FEATURES AND REGULAR COLUMNS. AUGUST ISSUE ON SALE IN JULY

The above details are subject to the national industrial situation at the time of going to press.


IT seems an awful waste that the most sophisticated electronic instrument most houses boast should be used only to watch Bugs Bunny or Coronation Street. Already the broadcasting authorities are considering the domestic television set as the basis for a data display terminal in the proposed Oracle and Ceefax systems. Why should we not use the same equipment for exciting new indoor games, puzzles and competitions? This series describes how you can make your own version of a game that is sweeping pubs and clubs throughout America and is rapidly being introduced over here.

The game is "Television Tennis", it involves skill and coordination, can be played by two people and provides excitement which can be shared by young and old. A word of warning to the proud; the author's 6 year old son can hold his own against most competition when playing the game, so there is plenty of challenge for the adult! It is an ideal indoor pastime for rainy days, but many private clubs or social societies might find benefit to their funds in building one of these fascinating, but addictive games.

Once built, the game is simplicity to install; only two connections are required-one to a mains socket and the other via a coaxial lead to the aerial socket of a domestic television. No alterations are needed to the TV except to tune in to a fourth channel and the set can be used normally at any time. Either a colour or black and white set can be used; the only limitation is that it must be a UK standard UHF 625 line model.

Before embarking on the original design the author had some misgivings about the potential complexity of the project and whether it would be suitable for the amateur constructor. By careful design and the use of integrated circuits and printed circuit boards there is no reason why it could not be undertaken by anyone with reasonable soldering ability. The cost of the project might be a bit high for some peoplenevertheless it works out much less than a medium quality stereo amplifier. We are giving a complete list of components in this first part so that you may
judge the likely cost for yourself before embarking on the project.
Those who decide to go ahead can make use of this list to obtain best prices for quantity purchases. All the components are now commonplace devices but, as many readers will know, there is a general shortage of components and you may expect delays in delivery of some of the integrated circuits.

In this issue we will describe the general principles of the instrument. Subsequent parts will carry construction details for each of the six circuit boards used, starting with the power supply and UHF modulator. The constructor will then be able to use his domestic TV set as a setting-up instrument for the remaining circuitry thus obviating the need for an oscilloscope.

## Presentation

For those who have not yet seen the commercial version-now becoming fairly standard in most amusement arcades-Fig. l shows the appearance


Fig. 1: Appearance of the game identifying the various parts of the display.

## ECTRONIC GAME <br> 

## M. J. HUGHES M A

because some of the lines are not seen-occurring above the top of the picture. Referring to Fig. 2, the lines are made by a spot which starts scanning across the top of the tube from left to right. When it reaches the right hand side, the time taken being $64 \mu \mathrm{~S}$, it returns very rapidly to the left side (this is called the line fly back), steps down the screen a short way and repeats its left to right scan. This periodic scan continues for $1 / 50$ of a second ( 20 mS ) and each time a new line is drawn.

At the end of 20 mS you can calulate that with a line frequency of $15 \cdot 625 \mathrm{kHz}$ there will be $312^{1_{2}}$ horizontal lines drawn at successive vertical positions across the screen forming one field. In a normal television signal the spot then flies back to the top left hand corner (this is called the field fly-back) to a position in between the original scanned lines and repeats the operation. This technique is known as interlaced scanning and the 625 line picture, with which we are all familiar, is actually made up of two separate fields of $311^{1}$ 2 lines interlocking with each other. The effect of interlace is to give a very high resolution picture with an effective repetition rate of 25 Hz .

Our system is NOT fully interlaced. The picture we display on the screen is generated complete on the $312^{1}{ }_{2}$ lines of one field. We repeat the field scan at a frequency of 50 Hz so that in $1 / 25$ of a second we still build up a total of 625 lines-although they do not necessarily interlace precisely. Resolution is not a problem in our application and the use of random interlace, as it is called, considerably simplifies design.
Summarising, we have a spot that moves from left to right every $64 \mu \mathrm{~S}$ and from top to bottom in 20 mS . Electronically we can identify the start of every 20 mS field scan with an electronic pulse (a field sync pulse) and in a similar way we can "tag" the start of every line using a line sync pulse. In a single field there are $312^{1}$ lines each of which starts scanning at a precise interval of time after the field sync pulse.


Fig. 2: Elements of a TV raster showing how an object's position can be represented by times within the field and line scans.

Fig. 3: The periodic waveform required to produce the object shown in Fig. 2.

## Picture generation

Suppose, for example, we want to delineate a square block on the screen at a certain position as shown in Fig. 2. We can do this by specifying on which of the horizontal lines the block is to occur and how far along those lines the block should extend. This can be done by coordinating the block in terms of time from the start of the field (this specifies on which line the block starts to be delineated) and time from the start of the line in question. The width of the block is determined by the length of time we allow the spot to "Bright-Up" along the line and the height of it by the number of successive lines we allow to bright-up. This number of lines is equally determined by time.

The waveforms of Fig. 3 show the signals which would delineate the block shown in Fig. 2. We take +300 mV as an arbitrary zero signal level, called black level; any signals going from +300 mV in a negative direction are the sync pulses-mentioned earlier. For simplicity of circuitry, we generate a single field sync pulse rather than the train of pulses normally used in broadcast TV practice. In our case we make the field sync pulse $500 \leadsto$ S long (Fig. 3a)
and between it and the next we generate approximately 312 line sync pulses-each $5 \mu \mathrm{~S}$ long (Fig. 3b). Positive going signals above +300 mV are video levels; these control the brightness of the spot on the television tube. A standard of 700 mV above black level is taken as peak white.

To produce the block of Fig. 2 we want to make use of three lines occurring about 8 mS down the field. It takes $64 \times 3=192 \mu \mathrm{~S}$ for three adjacent lines to scan across the screen, so we can say that the height of the block is contained within a window of about $200 \mu \mathrm{~S}$ occurring 8 mS after the field sync. The horizontal position of the block is just to the right of screen centre, say $38 \mu \mathrm{~S}$ after line sync. To give the required width the duration of the video signal on each of the three lines would, in this case, be $10 \mu \mathrm{~S}$. Thus you can see that the video signal we want occurs over a very small portion of the field waveform and equally over a very small portion of the three lines.

To generate the signal in the correct time position we need a number of time delay elements, controlled by the synchronisation pulses. One sets the vertical position while another sets the height relative to the field sync. A third sets the horizontal position

and a fourth the width. We take the field and line video waveforms so produced and combine them in an AND gate to give the video signal in its correctly coordinated time position.

It is a little difficult to grasp this at first because we are dealing in times as opposed to normal vertical and horizontal dimensions. Nevertheless, after a bit of thought, one can quickly get used to thinking of vertical and horizontal times as being equivalent to dimensions across the face of the screen. What we have just described is the technique for producing the video signal for the ball in our game. The position of the ball on the screen and its apparent movements are set by the time delays after the field and line sync pulses. These delays are generated by voltage controlled timing units.

The top and bottom base lines are somewhat simpler to produce because they extend the full width of the screen. We need only define the respective vertical positions and heights (number of lines to be brightened up). These waveforms are shown in Fig. 4. Similarly the left and right bases occur on every line so we need only define their coordinates in terms of time across the screen, Fig 5.

In practice we have to prevent video information appearing in our composite waveform during field and line synchronisation pulses. This is accomplished by means of blanking pulses which, for reasons of simplicity, are made the same length as the sync pulses. In other words the front and back porches normally present on line sync pulses are missing. We use conventional TTL logic levels of +5 V and OV to generate and define all video and sync information and only in the last stage do we convert to normal television signal voltages. In the descriptions that follow a logical " 1 " or +5 V denotes that a video signal is in the state that would bright-up the spot on our screen. To simplify descriptions we have adopted a crude form of Boolean Algebra terminology to describe our waveforms. For example if we use the term "BALL" we mean the waveform that, if fed to the screen, would display the ball- $\overline{\mathrm{BALL}}$ is therefore the inverted waveform for the ball. Other terms that we use include LEFT BASE, LEFT BASE, RIGHT BASE, $\overline{\text { RIGHT BASE, LEFT BAT, } \overline{\text { LEFT BAT }} \text {, }}$ etc. We shall define other terms later.
overall components list

Resistors

| tor $+\mathrm{W}, 5 \%:-$ |  |  |  |
| :--- | :--- | ---: | :---: |
| $330 \Omega-6$ | $1 \cdot 8 \mathrm{k} \Omega-2$ | $15 \mathrm{k} \Omega-5$ |  |
| $470 \Omega-1$ | $.2 \cdot 2 \mathrm{k} \Omega-6$ | $22 \mathrm{k} \Omega-3$ |  |
| $620 \Omega-4$ | $3 \cdot 9 \mathrm{k} \Omega-1$ | $27 \mathrm{k} \Omega-2$ |  |
| $1 \mathrm{k} \Omega-10$ | $4 \cdot 7 \mathrm{k} \Omega-16$ | $68 \mathrm{k} \Omega-1$ |  |
| $1 \cdot 2 \mathrm{k} \Omega-4$ | $12 \mathrm{k} \Omega-1$ | $100 \mathrm{k} \Omega-3$ |  |
| $12 \Omega 5 \mathrm{C}-1$ | $68 \Omega 1 \mathrm{~W}-1$ |  |  |
| $220 \Omega \frac{1}{2} \mathrm{~W}-1$ |  |  |  |

Potentiometers
Linear Sliders:- $\quad 5 \mathrm{k} \Omega-2$
Submin presets, vertical mounting:-

| $5 \mathrm{k} \Omega-1$ | $25 \mathrm{k} \Omega-3$ | $250 \mathrm{k} \Omega-2$ |
| :--- | ---: | :--- |
| $10 \mathrm{k} \Omega-1$ | $100 \mathrm{k} \Omega-3$ | $1 \mathrm{M} \Omega-2$ |

Capacitors

| Polystyrene:- |  |  |
| :--- | :--- | :--- |
| 1000pF-3 | $1500 \mathrm{pF}-4$ | $2200 \mathrm{pF}-4$ |
| Polyester:- | $0 \cdot 1 \mu \mathrm{~F}-15$ | $0 \cdot 47 \mu \mathrm{~F}-1$ |
| Electrolytic:- | $0 \cdot 33 \mu \mathrm{~F}-2$ | $2 \cdot 2 \mu \mathrm{~F}-2$ |
| $1000 \mu \mathrm{~F} 12 \mathrm{~V}-1$ | $2000 \mu \mathrm{~F} 25 \mathrm{~V}-4$ | $100 \mu \mathrm{~F} 25 \mathrm{~V}-1$ |
|  |  | $3000 \mu \mathrm{~F} 25 \mathrm{~V}-1$ |

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UHF Modulator kit by Crofton Electronics,
15/17 Cambridge Road, Kingston-upon-Thames, Surrey KT1 3NG
plus PCBs, cábinet, output socket, etc.

## Notes

1. The PCBs are available to order from:-
R. Whittaker

57 Mungo Park Way
Orpington, Kent
at $\mathbf{£ 7 . 5 0}$ per set of six boards including p.p. and VAT. The boards are fully drilled and are available by mail order only.
2. An undrilled cabinet in 16 swg aluminium is available to order from:-

> H. L. Smith \& Co.
> 287 Edgware Road
> London W. 2
at $£ 3.00$ including p.p. and VAT.


Fig. 5: The left and right base lines occur on every line of the field.


## System description

A simplified block diagram of the complete system is given in Fig. 6. Note that we show basic AND and OR functions in this diagram; in practice NAND gates are used and the logic connections are rather more involved. These will be dealt with in detail in subsequent parts. It is more important at this stage to try to understand the overall system.

All operations are linked to the field and line sync generators. These feed all the delay units which generate the functions of base lines, bats, bat positions, ball and ball positions. Notice, immediately, that the left and right bat vertical positions are set by voltages from potentiometers feeding voltage controlled delay units. Similarly the ball's horizontal and vertical positions are set by the Ball Horizontal and Vertical Control units-each of which is triggered by a Horizontal and Vertical Change signal. All the other delay parameters are preset.

The AND gates just to the right of the delay units provide horizontal and vertical coordination for the left and right bats and ball. The seven waveforms emanating from the delay units are: TOP BASE, BOTTOM BASE, LEFT BAT, RIGHT BAT, LEFT BASE, RIGHT BASE and BALL.

## Ball control

Generating these waveforms utilises most of the systems circuitry; the remainder performs fairly simple logic operations on these signals. Although the ball is only seen on the screen during a game it is there all the time, bouncing around between top and bottom or left and right base lines or the bats! Between games it is blanked by the logic circuitry.

Now to deal with that circuitry. First of all the Vertical Change unit which detects when the ball "hits" the top or bottom base lines. A "hit", in reality, is coincidence of signal between the BALL and one of the base line waveforms. If we get BALL. TOP BASE (coincidence between the ball AND top base) the vertical change system detects this with an AND gate. This sets a flip flop, the output signal of which causes a ramp generator to start a voltage sweep that increases the delay in the Ball Vertical Position unit. Eventually, of course, there will be coincidence provided by BALL. BOTTOM BASE; this is detected by Vertical Change and the direction of the control ramp is reversed by the Vertical Change flip flop changing state.

To control the ball horizontally we need it to "bounce off" either the left or right base lines or the bats. Because the bats are inside the court, when they are in the correct vertical position we shall get coincidence with their signals before the respective base lines. Nevertheless it is necessary to get Horizontal Change signals from either BALL. (LEFT BAT + LEFT BASE) or BALL. (RIGHT BAT + RIGHT BASE). These signals are detected and processed by the Horizontal Change unit in exactly the same way as for the vertical operation. Provided both these systems work the ball will stay within the court, bouncing about as already stated. There is only one problem-the ball must be inside the court to start with, otherwise it can never get in. This is a switch-on ambiguity and is overcome by means of a push button on the front panel which, for want of a better name, we call the Ball Boy. This centralises the output voltages of the two ramp generators. It is not shown on this simple diagram.

## Service

To complete the system all we need is a method of brightening up the ball at the start of a service and ensuring that it stays bright until one of the players misses it. A miss is detected by coincidence between the ball and either the right or left base lines. In ideal play the ball never hits these because it would have hit a bat first. BALL is ANDED with RIGHT BASE + LEFT BASE and the LOSE signal is then fed via the push button contacts S2b and S3b to the Ball Blanking circuit. If either of these coincidences occurs, the flip flop in Ball Blanking prevents the ball waveform passing through the following AND gate. The ball will then stay blanked until the next service.

Each player has a push button which generates either a RIGHT SERVE or a LEFT SERVE signal. We arrange that if the LEFT SERVE signal is present and the BALL is coincident with either LEFT BASE or LEFT BAT it will bright-up. This logic is effected by the AND gate shown immediately below the representation of the Left Service button. A similar signal is produced if the RIGHT SERVE signal is present when the ball hits the right hand base line or the right bat. Both right and left serve control signals are fed via an OR gate into the other side of the Ball Blanking flip flop. The switches on the input to the LOSE side of this flip flop prevent coincident signals on both inputs. This could have been done by logic but it was felt more economic to use the spare contacts of the service push buttons. We have now modified our original BALL' waveform to BLANKED BALL.

## Video mixer

All the waveforms are now combined in the Video Mixer which is a simple diode OR gate. They are then blanked to prevent their occurence during field and line sync pulses and fed to the Sync-Video Mixer. This circuit algebraically adds the correct proportions of video and sync to produce the composite video output signal. The source impedance is a few hundred ohms as opposed to the normal $75 \Omega$, but the signal level is greater than the standard IV peak to peak so when loaded with $75 \Omega$ this drops to a normal amplitude. It is assumed that not many people will want to use a video monitor and so this signal is used to modulate a uhf carrier for injection into the aerial socket of a conventional television set. The modulator used was designed by the British Amateur Television Club and is offered in kit form by Crofton Electronics.

This design will only operate satisfactorily on UK
 adopted for other TV systems but some of the timing components will need different values, and radio frequences and modulation polarities will be at variance.


## GOING BACK $197060500_{\text {colw вссниs }}^{3020}$

## 

IN 1892 the British rights of the Bell-Tainter and Edison phonograph were sold to the Edison Bell Phonograph Corporation Limited.

1898 saw the re-organisation of the company as the Edison Bell Consolidated Phonograph Company. It was amalgamated with Edisona Limited, a company which had been importing machines from America.


One of the most popular cylinder playing machines manufactured by Edison was the "Gem" like that shown in the accompanying pictures. It is described as the "baby" of the Edison phonograph range and first appeared in 1899 when it was introduced to compete with other small models then on the market.

Collectors of cylinder machines will find that the "Gem" is still the smallest practical machine for regular use although most have a motor mechanism which tends to be somewhat noisy. Five models were manufactured.

The "Model A" had a simple spring motor which played one 2-minute cylinder per wind. In the very early models, the motor was fitted in the left-hand end
of the casing as viewed from the front of the machine but was, in later models, turned $180^{\circ}$ and mounted at the other end.

It is thought that this change in positioning of the motor took place around 1901 when the "Gem" was fitted into a cabinet. All "Model A Gems" were fitted with a black-japanned horn.

From 1899 to 1901, the "Gem" was supplied minus a cabinet though a "drip pan" to catch the excess oil was screwed to the base. In 1901 it was equipped with the round-topped cover and wooden base and looked rather like a mini sewing machine.

The body was cast iron finished in black enamel with gilt embellishments. The mandrel, over which the cylinder fitted was of polished nickel. Early cabinets had "Edison Gem Phonograph" branded on the lid but this soon gave way to the more familiar "banner" transfer like that on our machine.

The speed adjustment screw and starting knob were combined on the right-hand front corner of the body but in 1901 this was moved to the left-hand side. It was a knurled button which operated a cam movement.
"Model B" was basically the same as its predecessor but the winding key gave way to a crank which was wound clockwise through the inclusion of an extra gear. An aluminium horn was supplied with the "Model B" and this is thought to have been a step introduced to tide the machine over until a larger and more effective horn came into production.

The "Model C" was very similar to "Model B" but had a socket fitted on the body to enable a crane rod to be slotted. This supported a rather large horn.

The "Gem Model D" was introduced into this country in 1909


Drive belt and speed adjuster.
and was the only "Gem" designed to play both 2 - and 4 -minute cylinders. The cabinet was oak and the metal body of the. machine was finished in maroon with gilt and black lining.

1912 saw the introduction of the "Model $E$ ". It had 4 -minute gearing only but in all other res. pects was similar to "Model D".

The "Gem" range was discontinued in 1913 with the price of the "Model E" being $£ 3$ 3s.

An excellent book, if you are interested in learning more about Edison Cylinder Phonographs, is entitled, "A Guide to The Edison Cylinder Phonograph". It contains details of the spring-driven models produced from 1859-1929 and has been compiled by George L. Frow to whom I am indebted for supplying some of the information on the "Gem" machines.


Speed governor mechanism.
Mr. Frow is always on the look-out for new information on Edison machines, so if anyone would like to write to him, he can be contacted at "Salterns", Seal Hollow Road, Sevenoaks, Kent. Another useful reference for vintage "gramophone" enthusiasts is the Talking Machine Review. It is edited by Mr. Ernie Bayly and appears at regular intervals throughout the year. Further information may be obtained by sending a s.a.e. to Mr. Bayly, 19 Glendale Road, Bournemouth, BH6 4JA.

## 二

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## BR-BR, BR-BR

Have you ever wondered what is going on behind the scenes as you stand and wait for your train as accident, industrial dispute or weather strike at services. The worst part often seems to be that no-one knows what is happening. When will a train materialise and, when it does, what platform will it be on? The fact that the only visible means of communication for some station staff is one of those mahogany-cased telephones of yesteryear hardly inspires confidence.

The problem is, of course, that any industry where safety is so vital has to be very sure indeed of the reliability of equipment and systems before adopting them for general use. There have been changes - recently the more observant will have spotted the UHF pocket radiotelephones in use by senior platform staff of some regions of British Rail.

Those of you who brave the melée of London Bridge each day may well have wondered what the future holds, with all the new signalling arrangements now being installed.

In a paper presented recently to the Institution of Railway Engineers, it was revealed that a mini-computer installation with disc storage at London Bridge will form the heart of the new system. The track diagram in the signal box is divided into eighteen sections and includes CRT displays of train running and signal aspect information.

At the associated London termini, station supervisory staff will have visual display units (VDU's) which can be switched to show the situation on any of the eighteen sections. Information displayed will include the position of trains, whether moving or at platforms, identified by their alphanumeric reporting numbers. "Train ready to start" signals will appear as a flashing symbol. The station platform "Next train" indicators will also be controlled by the computer.

Trials already carried out by B.R. have proved the feasibility of
operating a computer continuously all the year round in the environment of a railway signal box equipment room. An MTBF of about 8000 hours has been achieved in these trials. Additional reliability in the London Bridge installation is provided by a standby mini-computer, whilst VDU's are available in the signal box for use in the event of failure of one of the main CRT displays.

Facilities are included for timetable changes to be fed into the system and activated automatically on the due date. A future addition may be for the computer to control routing at junctions. If that comes about, it sounds as if the system will almost run itself!

## COWSHED COMPUTERS

Latest application of data processing is in the running of dairy herds. Using a micro-computer to maintain records of feed, health and milk yield of each cow is claimed to double the number of cows which can be handled efficiently by a herdsman. The farmer will also be provided with data on operating costs and income.

## STRIKE A LIGHT

Talked about for quite a while, the light-sensitive thyristor is here at last. Announced by Motorola at the Paris Components Show are two ranges of device handling 250 and 400 mA with PIV ratings from 15 to 200 V .

Also new from Motorola are three Darlington power transistors with 15A current capability and large-signal current gains of up to 5000 . Base to emitter shunt resistors and a shunt diode between collector and emitter of the output transistor are incorporated -all this in a standard TO3 package!

## ON THE BEAM

We hear that scientists at the RCA Laboratories are working on a modulator which could put 25,000 telephone calls or 20 TV channels on a single laser beam.

The device requires very much lower modulating powers than previously necessary and is compatible with ICs. Modulating voltages are applied to metal fingers which influence the passage of light through a thin-film optical waveguide.

## OPEN SESAME!

Hitherto more or less confined to the realms of science fiction or detective novels, the voice-operated lock could become a practical proposition in a couple of years if research now under way at the Westinghouse Laboratories in New York is successful.

When we speak, air is expelled from the lungs past the vocal chords, causing them to vibrate. These vibrations chop the air stream up into a string of pulses which travel up the vocal tract to the lips, giving the basic pitch to the voice. On their way, the frequency spectrum of the pulses is modified by resonances of the tract, chiefly in the throat, mouth and nose, to produce the final sound.

These resonances, which are known as formants, are different for each person and produce "voice-print" patterns as distinctive as fingerprints.

Voice-identifying locks have been produced before, but needed complex filters and large computers and cost up to $\$ 100000$. By using a different filter system and a smaller computer, Westinghouse hope to produce their lock for under $\$ 100$.

The lock could be set to respond to several voices and the password changed as often as necessary. Besides security applications, the system could be used for "no-hands" operation of machinery.

One point worries me. What happens when you have a cold or a sore throat, or even on the morning after the night before?

Norms

P.S.COLLINS


DUE to the series arrangement of the 'start' and 'park' switches of the wiper motor on some cars, Fig. 1, the original circuit and wiring must be modified. Figure 2 shows the modified circuit. The basic circuit remains the same, but $\operatorname{Tr} 5$ drives a relay instead of the motor directly. The relay contacts effectively replace the car's wiper switch. Sl is thus rewired to provide the choice of variable delay or continuous operation, with centre 'off'.

It will be noted that in the continuous position RLl is driven by a direct earth through Slb and Sla provides the 12 V . 12 V is also present on the rest of the delay circuit but its effect is nil as $\operatorname{Tr} 5$ is short circuited.

Figure 3 shows the modified wiring arrangement. RLl may be glued to the box lid or a larger box (RS Comps. type 993) could be used to house all the components including the relay.

The circuit shown is for negative earth systems. For positive earth, D3 must be reversed.

1Fig. 1: This switching arrangement of windscreen wipers found on some vehicles will prevent the proper operation of the Quickwipe circuit described in the April issue.

Fig: 2: botiom left, is the modified circuit using a relay to drive the wipers.

Fig. 3: Rearrangement of the wiring to incorporate the new relay circuit. Unless a sealed relay is used the relay should be enclosed in a box with the rest of the components. The connections from the PC' to the terminal strip remain as in the original article.


THIS amplifier is designed for audio or measurement applications where an AC coupled amplifier of well defined gain and low noise characteristics is required. Fixed gains of 20, 30, 40, 50 and 60 dB are provided. The noise referred to the input is $0 \cdot 5 \mu \mathrm{~V}$, which is low enough for most audio requirements.

General purpose amplifiers such as the 741 types are limited in frequency response and have a relatively high input noise. For example, the 741 circuit shown in Fig. 1 will have a bandwidth of about 1 kHz when the overall gain is 60 dB . With the 741 the open loop frequency response is shaped so that the closed loop is stable under all conditions, including unity gain applications. Some amplifiers such as the 748 and 301 have external frequency compensation which can be tailored to suit the application. However the improvement is only a factor of ten, giving a bandwidth of 10 kHz when the overall gain is 60 dB . Even the less readily available amplifiers, such as the LM318, which are designed for wide bandwidths can only give a 30 kHz bandwidth when the gain is 60 dB .

## CAUSE OF LIMITED BANDWIDTH

The frequency is normally limited by the bandwidth of the lateral PNP transistors used for level shifting in the input stages and by the low collector currents which are used so that the input bias currents may be reduced and an excellent DC performance obtained. For many AC applications the DC characteristics are of secondary interest.
While special low noise integrated circuits are available the approach indicated here gives an improved performance with little added complexity and cost. In Table 1 this technique is compared with the readily available standard integrated circuits.


Fig. 1: Simple amplifier using the standard 741 integrated circuit.

TABLE 1

| AMPLIFIER | $\begin{aligned} & \text { GAIN } \\ & \text { (dB) } \end{aligned}$ | BANDWIDTH (kHz) | RELATIVE NOISE |
| :---: | :---: | :---: | :---: |
| 741 series (internal compensation) | 60 | 1 | 20 |
| LM318 wideband amplifer | 60 | 30 | 15. |
| LM381 low noise amplifier | 60 | 20 | $5 \cdot 5$ |
| 301 series (external compensation) | 60 | 10 | 16 |
| 748 series (external compensation) | 60 | 10 | 20 |
| Suggested Circuit | 60 | 400 | $2 \cdot 1$ |



Fig. 2: Simplified diagram for the 301 integrated circult.


Fig. 3: Complete circuit of the final arrangement of the wideband pre-ampllfier.

A simplified diagram of the 101, 201 and 301 family is shown in Fig. 2. The main limiting components occur in the input stages, before Tr 8 . The second stage, from the base of $\operatorname{Tr} 8$ onwards, has a high gain with good bandwidth, good current capability and short circuit protection. This section of the integrated circuit should be retained, but the input stage should be replaced. Fortunately the base of Tr 8 is accessible because this point was used for offset voltage
balancing purposes. If pins 2,3 and 5 are connected to the most negative supply point (pin 4) then the complete input stage is effectively disconnected.

## COMPLETE CIRCUIT

The construction is straightforward, Fig. 4, but the input stage is replaced by a single PNP transistor Trl in a common emitter configuration which drives the output stage via pin 1 . The gain without negative


In the finished pre-amplifier, above, the circuit board is mounted about $\frac{1}{2}$ in. off the case to clear the veropins. Fig. 4 : (below) gives the board layout and wiring.

feedback is about 80 dB which allows the gain with feedback to be well defined. This is achieved by R10 and R5 to R9, to give the switched gains shown. Capacitors C2 and C6 shape the frequency response and ensure stability for the closed loop gains allowed by S 1 .

When the unit is switched on C3 or C4 will take a little while to charge up to the operating voltage and the base-emitter junction of Trl will be reverse biased for this time. Although the breakdown current would be limited to a 'safe' value this action can increase a transistor's noise level. Any reverse baseemitter voltage is therefore limited to a safe value by the conduction of D1. Under normal operating conditions D1 is reverse biased and cannot affect the circuit's pperation.

## CONSTRUCTION

The construction is straightforward, Fig. 4, but the unit must be placed in a metal box if hum pickup is to be avoided at high gain levels. Due to the bandwidth of this circuit all wiring should be keep short and the decoupling capacitor C7 placed directly actoss the pins of ICl. In critical applications the unit should be run from batteries (inside or outside the box) to reduce hum and earth loop difficulties.


The output of the amplifier with the gain at 60 dB and a 100 kHz squarewave input.


## components list

```
Resistors
\begin{tabular}{|c|c|c|c|}
\hline R1 & 100k \(\Omega\) 5\% & R7 & 100』 2\% \\
\hline R2 & 100k \(\Omega\) \% & R8 & 33ת 2\% \\
\hline R3 & 27k \(\Omega\) 2\% & R9 & 10ת 2\% \\
\hline R4 & 6.8k \(\Omega\) \% & R10 & 10k 2 2\% \\
\hline R5 & 1-2k \(\Omega 2 \%\) & R11 & 47ת 5\% \\
\hline R6 & \(330 \Omega 2 \%\) & R12 & \(100 \mathrm{k} \Omega 5\) \\
\hline
\end{tabular}
All resistors are & watt
Capacitors.
\begin{tabular}{llll} 
C1 & \(0.47 \mu \mathrm{~F}\) polyester & C5 & \(20 \mu \mathrm{~F} 16 \mathrm{~V}\) \\
C2 & 10 pF ceramic & C6 & 22 pF ceramic \\
C3 & \(100 \mu \mathrm{~F} 16 \mathrm{~V}\) & C7 & \(0.1 \mu \mathrm{~F}\) \\
C4 & \(1000 \mu \mathrm{~F} 16 \mathrm{~V}\) & C8 & \(40 \mu \mathrm{~F} 25 \mathrm{~V}\)
\end{tabular}
Semiconductors
D1 1N914
Tr1 BCY71
IC1 LM301A, SN72301A or similar TO5 verslon
Miscellaneous
S1, 2 pole 6 way wafer switch. Terminals (2). Sockets (2). Veroboard and pins. Knob.
Case approx \(5 \times 4 \times 3 \mathrm{in}\).
```

When the unit is tested a single DC measurement at the output of IC1 (pin 6) will confirm that the circuit conditions are correct. This is a low impedance point and it does not matter if the multimeter requires a few milliamps to operate it. Although a nominal 8.8 V was measured on the prototype, variations of perhaps $\pm 1$ volt would be normal. If an oscilloscope is available R3 may be changed, by one preferred value up or down, until the output limits symmetrically.

## NOISE LEVELS

The design of a low noise amplifier is complex, depending on the source impedance, the gain and bandwidth required and the transistor parameters. For this application a collector current of $220 \mu \mathrm{~A}$ has been chosen for Tr ; which is a good compromise for general wideband applications. For all transistors the noise increases at low frequencies.

If the circuit is specifically required for audio applications, where the 400 kHz bandwidth is not necessary, the performance may be improved by reducing Trl's collector current. Experienced constructors with the necessary test equipment could redesign the circuit for a collector current of between 50 and $100 \mu \mathrm{~A}$.

## P.W. ELECTRONIC COMPONENTS BUYERS' GUIDE

Special supplement in the October issue giving details of components commonly available, followed by additional sections in succeeding issues. More details on page 116 of the June issue.

## COMPONENT SUPPLIERS

Have you sent us your catalogues or lists for use in compiling the P.W. Buyers' Guide? Closing dates: 17th June for information; 1st July for advertisers in the October supplement only.

Here the gain is st/II 60dB but the input is 1 kHz squarewave.

## A series of simple transistor projects, using not more than twenty components.

UNLIKE many simple radio receivers this one will operate first time without any messing about with regeneration. It uses a straightforward parallel tuned circuit with the coil wound on a ferrite aerial rod. This is directly coupled to the RF amplifier/detector formed by $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$; the rectified carrier is suppressed by Cl and the detected audio fed to one stage of AF amplification $\operatorname{Tr} 3$. The output goes to a crystal earpiece and when the set was operated in a notoriously bad reception area in a valley in the South East it pulled in ALL the major broadcasting stations, including London Broadcasting and Capital Radio. The output level was almost comparable with a similar circuit using a ZN414 followed by an identical amplifier!


Circuit of the TRF receiver. No external aerial is required with this set.
The secret of its excellent selectivity is the very high input impedance provided by the emitter follower action of Tr ; the loading on the tuned circuit is minimal and maximum $Q$ can thus be obtained. A warning to some constructors-the tuning is so sharp that you have to tune slowly to prevent overshooting the station. There is a high degree of RF amplification which obviates the need for regeneration. The quality is thus excellent and there are no setting up problems.

## $\star$ components list



There are only two snags. The circuit is rather sensitive to fluorescent light interference and if operated too close to mains cables a certain amount of hum is induced. As a pocket portable neither of these points should present practical problems.


The set may be built on a piece of Veroboard, with pins, as shown here
Sensitivity is so high that it is necessary to include a volume control (we really do mean this, if you have any local stations!). To achieve this we introduce a controllable amount of negative feedback by adjusting the effect of decoupling capacitor C3 with VR1. Several test models have been built and with some high gain transistors there is a tendency for the circuit to oscillate which is easily prevented simply by reducing the gain by turning down VR1. For those who can't afford a ZN414 we assure you that this circuit gives very comparable results.

## SPARE A THOUGHT...

TO what extent do you maintain your fullest interest in radio, electronics and allied practical activities? Maybe you consider it to be a winter pastime, but from evidence that we have, summer issues of P.W. are still gobbled up from the bookstalls at an incredible rate. What does seem to be the case is that often you may decide to get your copy from a different source, for example in holiday resorts or nearer your home, whereas previously you might have purchased from the station bookstall on the way to your place of work.

Regular orders through newsagents can be delivered to your door, but if it does not arrive when expected, the newsagent is the first in the firing line for questions. Occasionally, factors outside his immediate control intervene and delay publication. We cannot, unfortunately, inform all newsagents and readers quickly enough when this happens and it is regretted that these occasions ever have to occur. So please have some patience with the newsagent. It may not always be his fault!

## PART5

 techniques alanamsle
## X DEFLECTION AND TIMEBASE

In the first part of this series we considered the requirements for a timebase system, namely the generation of a linear sawtooth coincident with the recurrence of the signal under observation. There are two basic modes of timebase operation, sync or trigger. We shall consider sync timebases first.

The synchronised timebase is a free-running generator of sawtooths; when one cycle is complete the next one starts with no time gap. A portion of the $Y$ signal, derived from the $Y$ amplifier by a cathode follower, is fed to a "sensitive" part of the circuit and this keeps the timebase in step with the Y signal, Fig. 1 shows how a sine wave is traced on the screen in this manner. However, the timebase is unable to cope with the requirement of a scan of duration less than one period of the waveform being examined.


Fig. 1: Generation of a sine wave on a CRT screen
The sawtooth can be generated in a number of ways, all involving charging a capacitor linearly and producing the scan, then discharging it, producing the flyback. The flyback trace interferes with the main trace and so a means of cutting off the trace during flyback has to be found. If the capacitor charges up in a positive manner and is then discharged through a resistor, this resistor will have a positive pulse across it during flyback. If this pulse is capacitively fed to the CRT cathode the trace will blank out during retrace, as required.

## CONTROLS

The controls on a sync timebase are frequency, sync and, sometimes, width. The sync control selects the amount of $Y$ signal used to sync the timebase. If too little is applied the trace will not lock and if too much is applied the trace will "fold up". The width control is adjusted for a satisfactory image width on the screen.


The timebase facilities on a dual timebase oscilloscope

The output from the timebase is applied to an X amplifier which may have to produce 100 or 200 V deflection. The bandwidth required is only a couple of MHz and small scopes may use a simple single valve output. Usually push-pull or balanced output is used and the sawtooth can be applied to one valve and again (as in the $Y$ system) a calibrated shift control can be used to drive the other grid. Fig. 2 shows the $X$ amplifier used in the EMI WM16 scope.


Flg. 2: Clrcuit of the $X$ ampl/fier in the EMI WM16 oscilloscope

## TYPICAL X AMPLIFIER

The two valves can be seen to form a simple phase splitter. The coils and TC1 peak the HF response. The $5 \mathrm{k} \Omega$ variable pot between the cathodes is in fact a switched series of preset resistors giving calibrated $X$ expansion. Resistor $R$ in the cathode is in fact a constant-current valve. The operating point of the valve can be adjusted to vary the $X$ plate potentials and these are adjusted to be equal to the potential of the $Y$ plates with the spot central, to minimise spot distortion. The balance control is set so that the cathodes of the two valves are at the same potential when the spot is central (i.e. varying the $5 \mathrm{k} \Omega$ between cathodes has no effect on the spot when central).

## TRIGGERED TIMEBASES

Most timebases in use are of the triggered variety permitting much greater flexibility than the sync timebase. In this mode of operation a sweep length control selects the duration of the sweep, the sweep beginning when the timebase generator receives a pulse from the trigger amplifier.

Fig. 3 shows the general requirement for a trigger amplifier. The $Y$ signal is sampled from the $Y$ amplifier by a cathode follower. The signal is amplified


Fig. 3: Basic arrangements for a trigger amolifier
and "phase split". A "trig polarity" switch selects one or the other of the phase splitter outputs which is applied to a comparator and compared with a DC level set by the "set trig level" control. The comparator produces a pulse when the comparator input bears a certain relation to this DC voltage selected on the "set trig level" control. This pulse is taken to the timebase to initiate the scan process. The pulse will occur once per input cycle at the same level as shown in Fig. 4.

The trigger pulse "flips" a bistable which starts the capacitor charging process. The multivibrator will now accept no further trig pulses until it returns to its former state. The capacitor selected by the range switch is charged by a constant-current valve, the value of the current being set by variable resistors also selected by the range switch, these being the sweep calibration presets. The ramp produced by the charging of the capacitor is amplified by a cathode follower and fed to the X amplifier and also to a comparator. When the level of the ramp passes a certain level the comparator produces a pulse which initiates the discharge of the capacitor. The bistable is also triggered into its original state, but is only allowed to return at a rate comparable with $2 \%$ of the sweep length, allowing complete recovery of the circuits before trigger pulses are again accepted.


Fig. 4 : Relationship between $Y$ signal and trigger pulse

A trigger sensitivity control, "set trigger" or "stab" allows for variation of sensitivity of the bistable and when the control is fully clockwise it is usual for the bistable to "free run" with the sawtooth giving a continuous output. Any signal applied to the grid of the bistable will synchronise the timebase, rather than trigger it, and a position of the trig polarity switch usually allows for the $Y$ signal to be fed to the grid of the bistable, rather than the normal pulse.

The bistable is also used to provide bright-up for the tube. Sync timebases require only flyback blanking but as a triggered timebase may be "waiting" for a trigger pulse the tube is normally cut off and is brightened up by a bright-up pulse occurring during the scan. Fig. 5 shows the sequence of events as a time graph. Note that the bistable takes slightly longer than does the ramp to revert to its initial state. The waiting time is also clearly seen.


Fig. 5: Waveforms at different points in the triggered timebase
In use there are only about five controls. The sweep length control is set to the required sweep period (it can of course be much shorter than the period of the signal being viewed). There is usually a trigger polarity switch and a mode switch. This allows for triggering from very low frequencies, or very high frequencies or automatically. Oscilloscopes for TV use also have TV frame and line positions in which a sync separator is switched into the circuit. The trig level and stability controls have already been mentioned and operation of the timebase is very straightforward. Automatic triggering is used on simple waveforms as there is no need to set the trig level control. Operation is thus simplified.

The mode switch is set to that which seems most suitable and the "stab" or "sensitivity" or "set trigger" control is set fully clockwise and the timebase should then free run. Backing off the "stab" control and rotating the "trig level" control should give a point at which a rock steady image is obtained. The sweep length control can then be switched to any range without any other adjustments being necessary.

## DUAL TRACE PROBLEMS

When triggering from a dual trace display (produced electronically) in the "ALT" mode it is possible to lock to one trace or the other, but not both unless they are overlapping. This can be overcome by very careful adjustment but the best way is to apply external trigger pulses from one of the signals if the loading of the trig input is not too great. Other-


The two outputs of a double pulse generator shown correctly on "ALT" with external trigger. It can be seen that the lower trace dropping to logic ' 0 ' triggers the upper trace to logic ' 1 '. . .


The same pulse generator output on 'ALT' but with internal trigger. The two traces both lock on the positive going edge and the time relationship is meaningless


The same pulse generator displayed on 'CHOP' with internal trigger. The 'trig level' control is set so that the timebase triggers from one signal only. The timing relationship is correctly displayed. Unfortunately the sweep speed is such that switching transients upset the trace considerably
wise it will be necessary to allow some overlap and adjust the trig level control to trigger off the overlapping portion. Similar difficulties arise in the "chop" mode because the scope tends to lock to the beam switching waveform. Once again external triggering may be needed.

## TIMEBASE OPERATION

Most oscilloscopes provide an external $X$ input but it must be remembered that the bandwidth is only a few MHz except in XY oscilloscopes where the X

The timebase section of a laboratory oscilloscope. On the top teft is the main timebase generator. The $X$ amplifier is at the top centre and the EHT unit at top right. The lower chassis is the delay timebase and power supply regulators
and Y amplifiers are identical. Several oscilloscopes are provided with two timebases, one being the normal one, the second being a delay timebase. The second timebase can be identical with the main timebase or very much simpler, as in the Cossor 2000. The purpose of the delay timebase is, as its name implies, to delay the main timebase. It is triggered from the signal and starts its sweep. At a certain point the main timebase triggers from the sweep and scans the CRT. The operation of the delay timebase is shown in Fig. 6. The time of the delay is adjusted by selecting the point at which the delay trig pick-off produces a pulse.

In order to gain some idea as to the operating point of the main sweep most scopes arrange for the


Fig. 6: Sequence of operations in a delay timebase
delay timebase to scan the tube. Thus the triggering can be seen to be correct. No bright-up pulse (or only a small one) is produced by the delay timebase so the trace will brighten up when the main timebase runs. It is essential to ensure that the main timebase is switched to external trig and that no trig is applied so that it will only trigger off the delay pulse. As the delay pick-off control is turned the bright patch can be seen to move along the trace. When it is at the correct point the scope is switched to "main sweep delayed" and the small portion viewed. If the trace tends to jitter the main timebase controls can be set to trigger from the incoming waveform, if suitable trigger points exist. This eliminates jitter but is not such a flexible method.

## APPLICATIONS

The most obvious application of these methods is in the viewing of the test pulses inserted in lines 18 and 331 of a TV picture, or to extract the colour bars from the top of the test card. The delay sweep is locked to the field of the receiver and the main sweep set to give about one scan per two lines ( 150 usec per sweep). Rotation of the delay pick-off pot will enable the user to go through the whole picture line by line. Oscilloscopes that have simple delay circuits are usually arranged to function in this manner but the trace brightness is rather poor, even when 10 or 12 kV PDA is used.

Sometimes only a single sweep of the timebase is required, particularly when photographing traces. Most scopes provide for this by making the gating bistable need resetting manually to receive any more trig pulses. The single shot trigger can be provided by an external signal (camera shutter and battery), internally from a transient on the signal or by a button on the front panel. The method of operation varies greatly from one scope to another and so it would be pointless to outline any one method.

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| :---: | :---: | :---: |
|  | No. |  |
| $0-5$ | 102 | 2.11 |
| 1 | 103 | 8.08 |
| 2 | 104 | 4.28 |
| 3 | 105 | 6.77 |
| 4 | 106 | 7.48 |
| 6 | 107 | 11.00 |
| 8 | 118 | 14.19 |
| 10 | 119 | 1760 |

Post
e
0.30
0.38
0.42
0.52
0.52
0.67
0.97
0.97

## MINIATURE AND EQUIPMENT

| Prim. 240 V Vith with |  | Milliampr |  | Re1. No. | Price | $\begin{gathered} \text { Post } \\ \text { f } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sec. 1 | Bec. 2 | Sec. 1 | Sec. 2 |  |  |  |
| 3-0-3 | - | 200 | - | 238 | 1.88 | 0.10 |
| 0-6 | 0-8 | 800 | 500 | 234 | 1.80 | 0.10 |
| 0-6 | 0-6 | 1000 | 1000 | 212 | 1.88 | 0.22 |
| 9-0-9 | - | 100 |  | 13 | 1.28 | 0.10 |
| -9 | 0-9 | 330 | 830 | 235 | 1.48 | $0 \cdot 10$ |
| 0-89 | 0-8-9 | 500 | 500 | 207 | 2.88 | 0.22 |
| 0-8-9 | 0-8-9 | 1000 | 1000 | 208 | 8.08 | $0 \cdot 30$ |
| 15-0-15 | - | 40 | $\cdots$ | 240 | 1.88 | $0 \cdot 10$ |
| 0-15 | 0-15 | 200 | 200 | 238 | 1.80 | $0 \cdot 10$ |
| 20-0-20 | - | 30 | - | 241 | 1.28 | 0.10 |
| 0-20 | 0-20 | 150 | 150 | 237 | 1.80 | 0.10 |
| 0-15-20 | 0-15-20 | 500 | 500 | 205 | 8.97 | 0.38 |
| 0-20 | 0-20 | 300 | 300 | 214 | 1.76 | 0.22 |
| 0-20 | -- | 3500 N | BCREEN | 1116 | 8.00 | 0.40 |
| 20 12-0-12-20 | - | 700 (D/C) | - | 221 | 1.55 | $0 \cdot 30$ |
| 0-15-20 | 0-15-20 | 1000 | 1000 | 208 | 8.80 | 0.38 |
| 0-15-27 | 0-15-27 | 500 | 600 | 203 | 8.08 | 0.38 |
| 0-15-27 | 0-15-27 | 1000 | 1000 | 204 | 2-24 | 0.38 |

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## CALIBRATION

Calibration of a timebase is relatively easy providing a good marker generator is available. However for those who have not got a high accuracy generator a few useful time periods are listed below.
TV frame period Main period Line period (405) Line period (625) Radio 2 ( $1500 \mathrm{~m} / 200 \mathrm{kHz}$ )

$$
\begin{array}{r}
20 \mathrm{~ms} \\
\cdot 20 \mathrm{~ms} \\
98 \cdot 8 \mu \mathrm{~s} \\
64 \mu \mathrm{~s} \\
5 \mu \mathrm{~s}
\end{array}
$$

The gain of the output stage is set so that rotation of the calibration shift moves the spot the required distance. The sweep speeds are then set using a calibrated pulse generator and the sweep speed adjusted so that a rotation of the calibrated shift moves the correct number of markers past a point on the graticule. Calibration is easily achieved to $5 \%$ and better is possible. It is perhaps interesting to note that the timebase velocity is given in time $/ \mathrm{cm}$, not $\mathrm{cm} / \mathrm{sec}$ as would be expected. It seems to mean more the first way, which, perhaps, is why it has been retained for so long. At high sweep speeds nonlinearity of the trace becomes evident due to bandwidth limitations and often capacitors are provided to linearise the faster ranges, using a high frequency sine wave as the display. General non-linearity of the output stage does not affect calibration of the calibrated shift, but non-linearity arising from bandwidth limitations does cause accuracy to suffer.

To be continued


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Suitable for colour or monochrome television sets.
Simulate the green football pitch, red and blue players, pink touch-line. See the ball kicked hard or soft across the pitch. Move your players to any position on the screen. Simple to operate joystick control.
This project will appear in TELEVISION only, starting in the July issue. Not to be confused with TELE-TENNIS, another TV game project appearing in PRACTICAL WIRELESS. Ideal for fund raising events.

9 Opponent of current circuits? (8)
10 Not conscious of such signals? (6)
12 Shortage of a dial system? (3)
15 Reduces the volume of gale-warnings?
16 Drama Marconi's Mum got into? (4)
17 Gives some sort of reception! (5)
19 Swearing about a hot switch? (4)
20 Winners run through such recordings? (5)
21 Member needled over the gramophone? (3)
25 Sound on ears inwardly disconnected! (6)
26 They're driven from the TV chairs! $(3,5)$
27 \& 1 Down Currently going through with impure stuff? $(4,9)$
28 Handy army alternative to radio (9)

## DOWN

## See 27 Across

A bouncer needed for TV reception? (9)
Sir, a twist to correct distorted melodies! (4)
Where to find a radio part on the map? (5)
Buzzer used to jam? (4)
Old sound transmitter with strings? (4)
11 Metal dish for a separator network? (4)
12 Waste amps with non-electric radio involved?
13 They're designed for individual listeners (9)
14 Press television to cover these? $(4,5)$
18 Knock-out in wireless tuning! (4)
22 Range of arc he got into a transformer (5)
23 Appendage of sound equipment (4)
24 Broken bit of a signal from the continent (4)
25 Final receiver of what the employer makes (4)

FOR AMUSEMENT ONLY ANSWERS NEXT MONTH

THE "SECUREYE"


Here's a useful little device-it's a light dimmer (up to 500 W ) and a photo-electrically operated switch. In addition it serves as a normal on/off switch when required.

It is an immediate replacement for most existing flush-mounted wall switches and takes only a minute or two to fix.
There is a hole in the flange at the base of the control knob. This acts as a pointer so that when the "light level" switch function is required, this is rotated until the hole uncovers the "magic eye".

This very versatile unit has a myriad of uses, the first one coming to mind being that of house security. With a Secureye, you can be away on holiday for a fortnight but because your house lights are automatically switched on and off, would-be burglars would think twice before "doing a job".

Price is $£ 5 \cdot 60$ plus VAT. Rendar Instruments Ltd., Victoria Road, Burgess Hill, Sussex.

## STORAGEBOX

I'm afraid I'm one of those constructors who keeps all his components in odd tins, jars and plastic aerosol can lids and gets in a muddle whenever he wants to find a $56 \mathrm{k} \Omega$ resistor in a hurry.

Well Protocraft Products Ltd., seem to have come up with the answer to my problem, for they have introduced a neat 4 -drawer storage cabinet. Overall size is $14 \frac{1}{8} \times 11 \frac{3}{8} \times$ $9 \frac{1}{2}$ ins. It's made from plywood and has a satin-white exterior. Drawer fronts are solid beech.

Also available is a matching cupboard and an open unit. They can all be interlocked to form a stacked group arrangement.

The firm supply plastic divider trays and 35 mm photographic slide racks taking 180 slides per drawer.

- These are extras and prices may be obtained from Protocraft.


Rec. prices are: $£ 12.65$ for the drawer unit (illustrated) $£ 8.23$ for the cupboard and $£ 5 \cdot 87$ for the open unit.
Further gen. from Protocraft Products Ltd., 3 Blatchford Road, Horsham, Sussex, RH13 5QR.

## P.C.TRANSFERS

Acid resistant transfers for direct application to P.C. Board. This is a new approach to printed circuit board manufacture, giving a professional finish with all drilling positions automatically marked.

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8-10-12. T.O.5 Cans, 3-4 lead transistors, etc, etc, which only require pressing into the required positions on the p.c. board before etching.
The complete system including post and VAT £2.00. Individual sheets 22p. Sample sheet 22 p. Copper laminate (boards) size $6 \times 4 \frac{1}{2}$ in. 6 sheets 50p.
E. R. Nicholls, 46 Lowfield Road, Stockport, Cheshire.

## SINCLAIR "SCIENTIFIC"

Sinclair, announce that they are marketing a 12 -function, scientific pocket calculator at a recommended retail price of $£ 49$ plus VAT. The "Sinclair Scientific" is identical in size to the "Cambridge" model (reviewed Nov. 1973)-measuring only $4 \frac{1}{2} \times 2 \times \frac{3}{4}$ ins. deep and weighing just $3 \frac{1}{2}$ ozs.
It features an 'upper' and 'lower' case operation allowing all 12 functions to be obtained using only four function keys.
Apart from the basic four ( $+-x \div$ ) operator keys the "Scientific" incorporates the following additional functions: logarithms to base 10 , antilogarithms, sine, cosine, tangent, arcSine, arcCosine and arcTangent. These enable rapid squaring, doubling and $x^{y}$ including square and other roots. Post fixed operators give full flow calculation facility on all functions.

Entry and result are in scientific notation with a signed 5 digit mantissa and a signed 2 digit exponent giving the "Scientific" a capacity for very large or very small numbers from $10^{-99}$ to $10^{99}$.

Sinclair has managed to pack these features into a tiny chip less than $1 / 5 \mathrm{in}$. square. This results from the use of a new set of algorithms for the transcendental functions devised by Clive Sinclair, managing director, and by special programming techniques used by Dr. Nigel Searle who is also a director of the company.

The calculator is powered by four standard Mallory batteries giving around 20 hours of continuous use. Guarantee is one year. -Sinclair Radionics Limited, London Road, St. Ives Huntingdonshire PE17 4HJ. Telephone St Ives (04806) 4311



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Panel fuse holders 20m3II 20p; 1t' 35p
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12-0-12V 50ma
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| 3 pin 90 | chassis plug with |  |  | Screeneil 30p |
| 4 pin, 5 pin | line socket. Per |  |  | Operi mono socket |
|  | pair 28p | Plug plast |  | 2" 10p: Moulded |
| (240\%), \% pin 10p | SA 21903 pin 5 A | Plug bereened | 12p | mono sucket $\mathbf{a}^{\prime \prime}$ with |
|  | chassir plug 20p | Chassis socket |  | 2 break contachs |
|  | S.A 1462 line nocket |  |  | 4p . Noulded stereo |
| DIN Sockets | for above 23p |  |  |  |
| $\underline{\text { pin }}$ - 8 p |  |  |  | break contacts 18 p ; 3.5th13, plak plathe |
| $3 \mathrm{pin}, 4$ pin, ${ }^{5}$ pin | McMORDO | Std. ${ }_{\text {Plutic }}$ (nono |  | 3.5that, plig platic |
| A (180 ${ }^{\circ}$ ), b pun ${ }^{\text {a }}$ | RP8 8 way chasmis | Plantic | 18 p | open rocket 8p. |

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$8^{\prime \prime} 8$ ohm, 10 wate
12" 8 ohm, 10 watt
$8^{\prime \prime} 8 \times \mathrm{hmm}^{\prime \prime} \mathrm{C} / \mathrm{Mag}$ watt C/Mag. 5 watt

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CELESTION $8^{\prime \prime} 15$ ohm
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${ }^{5 \prime} 8$ ohm, 5 watt C/Mag
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$17 \times 10 \times 9$ with $8^{\prime \prime}$ or $13^{\prime \prime} \times 8^{\prime \prime}$.
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\begin{aligned}
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& \text { D. Diame }
\end{aligned}
$$

D. Diamond

GOLDRING G800 G850 G800E
MICROPHONES
CM70 Planet stlck metal, switch
DM160 DEnsmic omi-dir, ball UD130 $50 \mathrm{~K} / 600$ ohm, unf-dir, ball netal
TW209
CONDENSER MESE 600 CONDEN uni-dIr.
Cassette STICK MIKE with $\underset{R}{ }$
Control on/off awitch 2.5 \& 3.5 mm J/Ply).
MIKE MIXERS Mono.

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| Type | $\begin{aligned} & \text { Low } \\ & \text { nolse } \end{aligned}$ | Phil. Itps | Memorex | $A \mathrm{~m}$ |
| :---: | :---: | :---: | :---: | :---: |
| C45 |  |  | 80p | 1 |
| C60 | 85 p | 60p | 56p | p |
| C90 | 45D | 69p | 76D | 76 p |
| $\mathrm{ClO}^{2}$ | 65D | 105p | 110p | 110p |
| Cassette | Head C | eaner |  | 45 |
| 11 BP Ster | reo Teat | Cassette |  | 1.88 |
| AMPEX magne | $\begin{aligned} & \text { Heal } \\ & \text { tiser } \end{aligned}$ | Cleaner | De | 85 |
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| $5^{\prime \prime}$ | 55] | 85 p |  | 800 |
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## SHORT WAVE DX by MALCOLM CONNAH

RADIO New Zealand has been heard by our reader John Godwin of Rugeley in Staffordshire. John says this in a letter which arrived just too late for inclusion in the last article.

He reports that the best frequency for reception is 1.1780 kHz ; he hears the station just after he gets up in the morning (about 0715 GMT) until about 0800 GMT. John suggests the following method of locating the station: First he looks for Radio Australia on the 25 metre band; the strength of this signal being a good pointer to the possibility of receiving New Zealand; then he tunes very carefully up in frequency, about 20 kHz , to find Radio New Zealand.

The equipment used was a pre-war HRO and a Joystick antenna. John reports March as being the best month for reception so we will probably have to wait until next year for another chance to hear this elusive station.

## Readers' Logs

Strangely enough the first report for this month also includes a logging of New Zealand. The report in question comes from A. McIntee of Angus in Scotland who used a 120 foot long-wire antenna with a choice of three receivers; Philips 7 transistor, Codar Multi-band 6, Homebrew crystal set with transistor amplifier; to hear the following:
4985 R. Kiev noted at 1950.
6020 R. Kiev noted at 1930.
6180 BBC relay Cyprus on at 1900 .
7215 AIR, Delhi noted at 1918.
11780 R. New Zealand noted at 0700.
Trevor Enefer of Cleethorpes has been concentrating on the lower frequency bands where his Lafayette HA600 and 50 foot end-fed antenna produced the following results:
3250 SABC, South Africa in English at 2315.
4820 HRVC, Honduras in English at 0330.
4820 R. Gambia in English at 2300.
4832 R. Reloj, Costa Rica noted at 0140.
4845 R. Fides, Bolivia. Ident. at 2235.
4845 R. Bucaramanga, Colombia noted at 0340.
4875 SABC, South Africa in Afrikaans at 0400.

4880 R. Universo, Venezuela noted at 03555.
4885 Ondas del Meta, Colombia at 0400.
49725 R. Cameroon, Ident. in French at 2215.
4980 Ejura, Ghana in English at 2245.
4990 R. Nigeria, S/off in English at 2305.
5038 R. diff. Nationale Centrafricaine at 2205.
5047 R. diff. du Togo, Ident. in French at 2255.
6000 R. Inconfidencia, Brazil noted at 0130 .
6006 R. Reloj, Costa Rica noted at 0140.
Paul Broadhurst of Clevedon in the new county of Avon has added a Codar PR40 preselector to his Trio 9R-59DS, this set-up plus a 150 foot long-wire and two half wave dipoles produced the following:
6050 RAI, Italy with S/on at 2030.
6065 R. Sweden with S/on at 1600.
6160 WYFR, Family Radio noted at 2250.
6165 R . Kiev noted at 1945.
9545 Radio Accra, Ghana noted at 2215.
9550 R. Finland noted at 2046.
9735 VOA, Monrovia, Liberia at 2120.
9745 Radio Baghdad, Iraq noted at 2200.
11765 Radio Australia noted at 0800.
11880 Voice of Turkey, S/on at 2200.
15120 Voice of Nigeria noted at 1620.
15140 Radio Havana, Cuba noted at 2030.
15185 WINB, Red Lion noted at 2115.
15275 TWR, Bonaire at 2140 .
15300 HCJB, Quito, Ecuador noted at 2010.
15325 Radio Canada International at 2100.
Stephen Fletcher of Bromsgrove, Worcestershire has a homebrew Heathkit SW717 with a 60 foot endfed and a 150 wire in the loft. A Grundig Yacht Boy with internal 4 foot telescopic was also available during the compilation of the log:
6080 HCJB, Quito, Ecuador in English at 0930.
6130 R. Norway, news in Norwegian at 1100.
6160 R. Australia in English at 1459.
9525 RSA, South Africa in English 2253.
9670 Adventist World Radio, Portugal at 0845.
9770 VOA relay in Greece, English at 0729.
11740 R. Nederland via Malagasy relay at 1909.
11860 BBC, Ascencion Is. relay in English at 0730.
15012 Voice of Vietnam, news in English at 2124.
15165 R. Denmark in Danish at l'158.
15410 United Nations Radio at 1800.
15415 R. Kuwait in English at 1735.
17830 R. Pakistan in English at 0735.
The final report for this month comes from Albert
E. Ord of South Shields who used his Trio 9R-59DS with a Joystick and Hamgear Preselector to hear:
4975 R. San Topez, Peru in Spanish at 0200.
4990 R. Barquisimeto, Ven. in Sp. at 0130.
7235 R. Australia noted at 2115.
11670 R. Pakistan in Hindu at 1315.
15185 R. Finland in English at 2030.
21520 RSA, South Africa in English at 1030.

## MEDIUM WAVE BROADCASTS by CHARLES MOLLOY

INDEPENDENT Local Radio came to Manchester on April 2nd when Piccadilly Radio appeared on $1151 \mathrm{kHz}(261 \mathrm{~m})$ medium waves and 97 MHz v.h.f. A press notice from IBA gives details of the medium wave outlet which is located at Ashton Moss, three miles south of Oldham. A directional aerial consisting of four 235 ft masts beams an effective radiated power of 4 kW towards Manchester and away from Glasgow, Birmingham and London where the same frequency is alloted to independent local radio. Programmes from Manchester are on the air daily from 0500 hrs ( 0600 hrs on Sunday) until 0200 hrs .
Roy Patrick (Derby) has been listening to Africa on the medium and long waves with his National 1400 receiver. Three Algerians were heard-Tipaza on 252 kHz ( 1195 m ) in French during the daytime; Ain Beida on 533 kHz and Cran on 548 kHz , both in Arabic. From West Africa, Dakar in Senegal was logged on 746 kHz at 2325 hrs and Conakry, Guinea on 1403 kHz after 2300 hrs . Roy reports hearing the BBC Eastern Mediterranean relay station in Cyprus relaying the BBC World Service on 1322 kHz at 2300 hrs GMT. A number of medium wave outlets in Africa are audible in this country after dark. On the long waves listen on 209 kHz ( 1435 m ) for Arabic music from Azilal in Morocco while on the medium waves Bissau, Portuguese Guinea on 1070 kHz can be heard after 2300 hrs GMT, usually with pop music. Others to look for are:- Tenerife, Canary Islands in Spanish on 620 kHz ; Djedeida, Tunisia on 629 kHz ; El Gawarsha, Libya on 674 kHz ; Radio Kinshasa, Zaire on 629 kHz ; Radio Algiers on 890 kHz ; Tunis on

962 kHz ; Algiers on 980 kHz ; El Peida, Libya on 1124 kHz and Radio Tangiers on 1232 kHz .

Local Radio enthusiast Stephen Fletcher (Bromsgrove, Worcs) reports hearing BBC Radio Derby on 1115 kHz ; BBC Radio Oxford on 1484 kHz and BBC Radio Bristol on 1546 kHz , using his Grundig Yacht Boy portable receiver. Roy Patrick has heard Radio Clyde on 1151 kHz after the close down of Radio Birmingham which operates on the same channel. Local radio is now well established on the medium waves with BBC stations operating on 755 kHz (397m); 854 kHz (351m); 998 kHz (301m); 1034 kHz ( 290 m ) ; 1106 kHz ( 27 lm ); 1115 kHz (269m); 1457 kHz ( 206 m ) $; 1484 \mathrm{kHz}(202 \mathrm{~m}) ; 1502 \mathrm{kHz}(19.9 \mathrm{~m}) ; 1520 \mathrm{kHz}$ ( 197 m ) ; 1546 kHz ( 194 m ) and 1594 kHz ( 188 m ). IBA stations are found on 557 kHz ( 538 m ); 719 kHz (417m).

Ioan ab Elfed (Worcester) is a recent 'convert' to the medium waves. He has built a MW loop aerial and he would now like to join a DX club that caters for the MW Dxer as well as the short wave enthusiast. The World Wide DX Club, Postfach 1263, D-6380 Bad Homburg. West Germany has a useful medium wave section in its monthly DX Magazine and the Danish SW Club International, DK-8382 Hinnerup, Denmark publishes Short Wave News monthly which caters adequately for DXers with an interest in the long and medium wave bands. Each club has a large international membership and their bulletins are printed in English.

Robert Bonsall (Buxton) would like information about an aerial suitable for MW Dxing. The MW loop is the aerial favoured by the majority of medium wave DXers. An article giving constructional details appeared in the April 1973 Practical Wireless.

## VHF/FM DXING

## by SIMON DAVID

ONE of the aspects of f.m. DXing is that you may be lucky to get a long distance transmission (or "skip" as it is called) for about ten minutes, then never hear it again. It could quite easily come in on what seems to be the wrong frequency. For example it has been known for "communist bloc" countries, who normally broadcast sound only in the 70 MHz region and television sound in the 85 to 92 MHz and 93 to 100 MHz bands, to break through with short skips into the UK, although it is rare. However, the GDR uses the same f.m. band as the UK and should not be confused with Poland and Hungary who are on the 66 to 72 MHz band.

For the readers who have reported to me of frustrated attempts, my advice is don't give up. Earlier advice on aerials and the use of modern highly sensitive receivers will help you. If the "local" station only about 100 miles away seems tame to you, it is a start and with perseverence you will improve. If you run a portable, as so many do, take it up to some high open ground, such as the hills in Wales, Sussex, the Midlands, and Yorkshire. Take some sort of portable three- or four-element aerial that you can rig up temporarily on a telescopic mast.

It is amazing how many people will happily pay $£ 25$ to $£ 30$ for a tuner or receiver and begrudge $£ 7$ or $£ 8$ for a good aerial. Without it you cannot expect reliable results, especially if you want stereo.

A useful tip comes from David Jack of Bolton who has been DXing from 30 miles west of the Pennines. He suggests cutting out the Atlantic weather chart
from the daily paper and sticking it in your $\log$ or desk diary. Trends can be followed and rough forecasts made. He has built the Gemini tuner and has picked up Norddeutscher Rundfunk (West Germany) on $99 \cdot 8 \mathrm{MHz}$ and Roermond (Holland) on $88 \cdot 2 \mathrm{MHz}$ on 8th and 9 th April.

My thanks to all the other readers who have asked about matters related to this article, including Stephen Fletcher of Bromsgrove, Michael Suttle of Kilmacanogue, Ireland, P. Shaw of Sandbach. Unfortunately, I cannot send out details or recommendations for particular receivers as there are so many. Many of you are unsure of the stations you hear and unable to identify them. It does help if you can recognise the language; have a copy of the World Radio and TV Handbook at your elbow, or even a cassette recorder ready to go when something strange comes through. If you have any doubts and can record what you hear on a cassette, I will try to help you identify the source; of course there should be some speech. The R.S.G.B. reports propagation conditions on Sunday mornings starting at 9.30 (local time) on $3 \cdot 6 \mathrm{MHz}$. The first station in the south-east is GB2RS and repeats are made in other regions at half-hour intervals. These news bulletins cover many aspects of amateur radio and are broadcast on s.s.b. transmission.

There is a chart available that gives a summary of most of the British and European f.m. stations on the 87.5 to 103 MHz band, that are likely to be picked up over long distances. It is a very useful quick reference, especially if reception conditions are changing rapidly. Any reader who would like one should writest to me personally and enclose a 25p postal order to cover the cost of printing and postage.

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## by Eric Dowdeswell G4AR

Delays in the publication of Practical Wireless, for reasons beyond editorial control, make it a toss-up as to whether items of news included herein may be out of date by the time that you read this page.

It is hoped that most of you will be aware of the RSGB's annual National Field Day, an old and revered HF bands CW contest, when Clubs put their crack operators to work and actually invite families and friends to go along and watch (and cook and wash up, usually!). If you're not actually taking part then sit down at home and listen in to the lads working worldwide DX on CW with just 10W input. It's the better-than-at-home aerials out in the country that do the trick. Note the date, June 8/9.

Incidentally, if your listening times generally are rather limited in number then try to make them coincide with a contest, then you will be assured of some activity. There is nothing more annoying than to arrange to spend an hour on the receiver only to find that the band is seemingly dead when, in fact, it is just simply lack of activity. International contests such as those organised by the RSGB, ARRL and CQ Magazine brings to life all kinds of rare stations and countries seldom heard normally. So if you are interested in lengthening your 'countries heard' list then this is the time to do it. I once worked 99 different countries in a week-end CW contest and still have the flattened ears to prove it!

When G9ZZZ down the road is working the DX see if you can hear these stations as well. If you can't then there is something wrong, unless he is using an elaborate aerial at 60 feet against your few yards of wire in the loft.

## SSTV on 80 m

The MPT's decision to permit UK amateurs to use SSTV on 80 m has not met with much enthusiasm judging by the rude remarks heard so far from the usual inhabitants of the band. It remains to be seen whether SSTV will be a workable proposition amid all the other noises on the band.

Personally I doubt it, except for perhaps local working where the strong signals may override interference, deliberate and otherwise! Somehow I don't think that SSTV and SSB are going to mix in the few kHz at the top end of the band.

Our amateurs can often be heard airing their views on non-amateur noises on 80 m but they seem to forget that this is a shared band here and that a lovely S 9 signal from some DX station is equally just a noise to some other service sharing the band.

## Goodbye MPT!

Not many amateurs seem to be aware yet of the intention of the present Government to abolish the Ministry of Posts and Telecommunications. Among other responsibilities the Home Office will administer the Wireless Telegraphy Acts which are of immediate concern to amateurs here. The MPT, or whatever it was called at different times in the past, has always had a very close and amicable relationship with the amateur, mainly through the good offices of the RSGB, and it is to be hoped that this happy state of affairs will long continue. It will not profit our movement if we have to deal with faceless Civil Servants knowing nothing of our hobby.

- In spite of the scarcity of sunspots the HF bands are improving generally with the increasing hours of daylight which we are now enjoying. Except, of course, that it generally means a transfer of personal activity at home from the inside to the outside! So when you are ostensibly doing a bit of weeding or shooing the birds from the seedlings why not shove up a rhombic aerial or at least a nice long wire as high as possible. With copper being so pricey these days don't overlook the possibility of using aluminium wire as a substitute, preferably hard drawn to avoid stretch.


## GB2MT

The Marconi Centenary station GB2MT, operated by Ralph Barrett G2FQS, and mentioned last month, managed 235 QSO's on SSB from Marconi's old home in Bayswater, London. Unfortunately, on the great day itself, April 25th, no contact was made with II4FGM, the Italian counterpart of GB2MT, located in the mausoleum where Marconi now rests. This was in spite of a schedule and a reminder by Telex from the Marconi Company here. Plenty of other Italian stations were worked around the same time. It is understood that II4FGM will be active for the rest of the year but only on Saturday afternoons.

Apologies again for the lack of any reports from readers, which would normally form the backbone of this page. My appeal in the last issue for reports will not produce any response in time for this month's page because of the delayed publication dates. Once things get back to normal, hopefully with the July issue, it will be possible to raise matters in one issue and to deal with them in the next, said he, optimistically!

## BROADCAST BANDS

Short Wave Reports by 15 th of the month to Malcolm Connah, 27 Lismore Road, Highworth, Swindon, Wiltshire, SN6 7HU.
Medium Wave Logs to Charles Molioy, 132 Segars Lane, Southport, PR8 $3 J G$.
VHF/FM Reports to Simon Davld, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.

## AMATEURBANDS

Logs covering any amateur band/s in band/alphabetical order by the middle of the month to Eric Dowdesweli G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey, KT21 2TW.
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 $3000 \mathrm{mF} .6 \mathrm{~V} .25 \mathrm{p} ; 12 \mathrm{~V} .42 \mathrm{p} ; 26 \mathrm{~V}$. 75p; $35 \mathrm{~V} .85 \mathrm{p} ; 60 \mathrm{~V} .25 \mathrm{p}$

CRRAMIC 1pF to $0.01 \mathrm{mP}, 4 \mathrm{p} .811 \mathrm{ver}$ Mica 8 to $5000 \mathrm{pF}, 4 \mathrm{p}$ PAPER 850V-0.1 4p, $0.513 \mathrm{p} ; 1 \mathrm{mP}$ 15p; 2mF 150715 p $500 \mathrm{~V}-0.001$ to $0.054 \mathrm{p} ; 0.16 \mathrm{p} ; 0.258 \mathrm{p} ; 0.4725 \mathrm{p}$
 DF 10 p : ${ }^{8,700-6,000 \mathrm{pF}} 20 \mathrm{p} ; 6,800 \mathrm{pF}-0 \cdot 01$, mid 80 p ; each $75 \mathrm{p}: 285+885$ with $25+25 \mathrm{pr}$ slow motion drive 50 p . HORT WAVE, SINGLE 10 pF 30 p ; 25 pF 65p; 50p 56 p FERT PATEL INDICATORS. 250 V AC/DC Amber 25p. REGISTORS. IW, $1 \mathrm{~W}, 1 \mathrm{~W}, 80 \% 1 \mathrm{p} ; 8 \mathrm{FW}, 6 \mathrm{p}$. $10 \Omega$ to 10 M BIGH 8TABILITY. $w, ~$
Ditto $5 \%$ Preferred values 10 ohmin to $106 \mathrm{meg} ., 10 \mathrm{p}$. Ditto $5 \%$ Preferred values 10 ohmi to 10 meg-, $4 p$.
WIRE-WOUND RESISTORS. 5 watt, 10 watt, 16 wat WIRE-WOURD RESIBTOR
TAPhm to 100K 10p each. Valve Type 35p.

# Sinclair Project 80 



## only $\frac{3^{\prime \prime}}{}{ }^{\prime \prime}$ deep $\times 2^{\prime \prime}$ high

Living with hi-fi takes on new meaning with Sinclair Project 80. The electronics of these revolutionary new modules are all contained within elegantly designed matching cases no more than three-quarters of an inch deep. They are designed for mounting on any appropriate flat surface by means of 6 BA bolts extending from the rear of each module and which pass through suitably drilled holes. Connections are taken away out of sight in a similar manner. The possibilities opened up by Project 80 are endless - superb hi-fi systems can be installed in ways hitherto only dreamed about and never before made practical. No more cutting out and shaping to put modules in position. A few holes drilled with the aid of templates supplied and the job is done. Now you need never again be faced with problems of keeping the hi-fi from clashing with carefully thought-out furnishing schemes. (That will surely please wives!) Slider controls have been introduced in place of knobs and all modules in the range incorporate new up-dated circuitry with emphasis on performance standards and built-in protection against overload and shorting. The aim was to re-think modular construction completely - to make it infinitely more versatile, even simpler and more reliable - the result - Project 80 - another triumph for Sinclair, and the most exciting construction modules ever.

## the slimmest,most elegant hi•fi modules ever made

| System | The Units to use | Units cost |
| :---: | :---: | :---: |
| Simple battery record player | 2.40 | $\begin{aligned} & £ 5.45 \\ & 54 \mathrm{p} V . A . T . \end{aligned}$ |
| Majns powered record player | 2.40, PZ. 5 | $\begin{aligned} & \mathrm{£10.43} \\ & +£ 1.04 \text { V.A.T. } \end{aligned}$ |
| 30W. RMS continuous sine wave stereo amp. | $\begin{aligned} & 2 \times 2.40 \mathrm{~s} \text {, Stereo } \\ & 80 ; \text { PZ. } 6 \end{aligned}$ | $\begin{aligned} & £ 30.83 \\ & +£ 3.08 \text { V.A.T. } \end{aligned}$ |
| 50W ( $8 \Omega$ ) RMS continuous sine wave de luxe stereo amp. | $\begin{aligned} & 2 \times \text { Z.60s, Stereo } \\ & 80 ; \text { PZ.8 } \end{aligned}$ | $\begin{aligned} & \mathrm{£33.83} \\ & +3.38 \text { V.A.T. } \end{aligned}$ |
| Indoor P.A. | 2.60, P2.8 | $\begin{aligned} & \mathrm{£14.93} \\ & +£ 1.49 \text { V.A.T. } \\ & \hline \end{aligned}$ |



Mount Project 80 on a bookshelf, a loudspeaker. a lampshade base a false wall with two 0.16 loudspeakers ... almost anywhere.

## new thinking in modular hi.fi <br> Stereo 80 pre-amplifier and control unit <br> Z.40 \& Z.60 power amplifiers totally short-circuit proof



## - For P.U., radio and tape

 - Tape monitoring switch- Simplest ever fixing

Each channel has its own separate tone and volume controls operated by sliders, enabling ideal environmental matching to be obtaned. A virtual earth input stage forms part of the up-dated circuitry that ensures the finest possible quality from all signal sources. Generous overload margins are allowed on all inputs. Clearinstructions with template are supplied TECHNICAL SPECIFICATIONS
Size $-260 \cdot 50 \times 20 \mathrm{~mm}\left(10 \frac{1}{4} \times 2 \times 3 \mathrm{~ns}\right)$
Finish - Black with white indicators and transparent sliders
Inputs - Magnetic pick-up 3 mV RIAA corrected: Ceramic pick-up 300 mV
Radıo 300 mV : Tape 30 mV
Signal/noise ratio - 60dk
Frequency range -20 Hz to $75 \mathrm{KHz} \pm 1 \mathrm{~dB} .10 \mathrm{~Hz}$ to $25 \mathrm{KHz} \pm 3 \mathrm{~dB}$
Power requirements - 20 to 35 volts
Outputs $-100 \mathrm{mV}+\mathrm{AB}$ monitoring for tape
Controls - Press button for tape radio and P.USilders for volume, bass ( -12 dB to -14 dB at 100 Hz ) treble ( +11 dB to -12 dB at 10 KHz )

$$
\text { R.R.P. } \mathbb{1 1 . 9 5}+\underset{\text { VAT. }}{\text { V. } 19}
$$

## Proiect 80 FM tuner



- Twin dual varicsp tuning: 4 pole ceramic filter: switchable A.F.C.


On the decoder, solid
state stereo indiceting batan.

Making the Project 80 F.M. tuner and decoder available separately gives a wider choice of systems and saves monay where stereo reception may not be required. The tuner is a triumph of electronic design and assures excellent performance. The decoder gives a 40 dB channel separation with 150 mV output per channel. Both. units may be used with other than Project 80 systems.
TECHNICAL SPECIFICATIONS OF TUNER
Size $-85 \times 50 \times 20 \mathrm{~mm}$ ( $3 \frac{1}{2} \times 2 \times \frac{3}{4} \mathrm{n} \mathrm{ns}$ )
Tuning range -87.5 to 108 MHz
Detector-I.C. balanced coincidence for good A.M. rejection
One I.C. equal to 26 transistors
Distortion-0.2\% at 1 KHz for $30 \%$ modulation
4 pole ceramic filter in I.F. section
Aerial impedance - $75 \Omega$ or 240-300 $\Omega$
Sensitivity - 4 microvolts for 30 dB quieting
Output -300 mV for $30 \%$ modulation
Power requirements - 23 to 33 volts
DECODER
Size $-47 \times 50 \times 20 \mathrm{~mm}\left(1 \frac{2}{8} \times 2 \times \frac{3}{4}\right.$ ins $)$
Ones 9 transistor I.C.
R.R.P. f11.95 + £ 1.18
R.R.P. $\mathbb{C} 7.45$
V.A.
+0.74
V.A.T.

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Sinclair Radionics Ltd. London Road, St. Ives, Huntingdon PE17 4HJ Telephone St. Ives (0480) 64646


Intended for use in Project 80 installations, these modules readily adapt to an even wider range of applications. Both incorporate built-in protection against short circuiting and risk of damage from mis-use is greatly reduced.
Z. 40 TECHNICAL SPECIFICATIONS

Size $-55 \times 80 \times 20 \mathrm{~mm}(2 \mathrm{k} \times 3 \mathrm{~K} \times \mathrm{zins}) 9$ transistors
Input sensitivity -100 mV
Output - 15 watts RMS continuous into $8 \Omega$ ( 35 v )
Frequency response-10 Hz-100 $\mathrm{KHz} \pm 1 \mathrm{~dB}$
Signal/noise ratio -64 dB
Distortion - at 10 watts into $8 \Omega$ less than $0.1 \%$
Power requirements -12 to 35 volts
Z.60TECHNICAL SPECIFICATIONS

Size $-55 \times 98 \times 15 \mathrm{~mm}\left(2 \mathrm{~d} \times 3 \frac{3}{4} \times \frac{3}{3} \mathrm{~ms}\right) 12$ transistors
Input sensitivity - $100-250 \mathrm{mV}$
Output -25 watts RMS continuous into $8 \Omega(45 \mathrm{~V})$
Distortion - typically $0.03 \%$
Frequency response-10 Hz to more than $200 \mathrm{KHz} \pm 1 \mathrm{~dB}$
Signal/noiseratio - better than 70dB
Built-in protection against transient overioad and short circuiting
Load impedance - $4 \Omega \mathrm{~min}$, max safe on open circuit
Z.40 R.R P. E6.45-0.54VAT. Z.60RRP £6.96-0.69pV.A.T

## Project 80 active filter unit

Makes a highly desirable part of any worthwhile system where inputs may be from kecord, radıo or tape. As with Stereo 80. separate controls applied to each channel make it easier to obtain ideal stereo balance.
TECHNICAL SPECIFICATIONS
Size $-108 \times 50 \times 20 \mathrm{~mm}\left(4 \frac{1}{4} \times 2 \times\right.$ (ns) $)$
Voltage gain - minus 0.2dB


Frequency response -36 Hz to 22 KHz controls minimum
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    from Electrical and Hardware Shops. If unolitanable, send 10 p p 80 direct to - Rib Hi-Fi Accessories Limited, Hemel Hempstead. Herts HP2 7EP

[^3]:    ## MASSIVE CLEARANCE BARGAINS

    Bargain component parcels contain Resistors, Capacitors, Switches, Potentiometers, Knobs, IF's, Tag Strips, Drive Drums, Transistor Panels etc., etc. Save yourself $f$ s on these well selected parcels 6 lbs net weight fl-00, p.p. 40 p.
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    Colvern W/Wound Potentiometer Spindle Type 10 ohms 35p.
    Please include 10\% VAT to total cost of goods
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    I. EAST STREET, BISHOPS TAWTON, DEVON

[^4]:    WANTED. Radio and TV Servicing books from 1964 onwards. $£ 2 \cdot 00$ per copy, paid by return of post. Bell's copy, paid by return of post. Bell'
    Television Services, $190^{\circ}$ Kings Road, Television
    Harrogate,
    Services, 190 Kings Road,
    Telephone Harrogate,
    $0423-55885$.

[^5]:    TRANSISTOR AMPLIFIERS 50p. Vol/ tone pre-amps 30 p . LW-MW osc. panels tone pre-amps 50 . All with circuits. Radio cabinets, suitable ext. speakers; colours: yellow, or teak finish requires sides trimmed. Mains droppers, $76 \Omega+66 \Omega+66 \Omega$ $+25 \Omega+24 \Omega+26 \Omega 30$ p. Skeleton preset 25 assorted 50 p . Archer, 9 Pine Grove, Maidstone, Kent.

    AMTRON KITS. Your Devon Stockict. E. Wenmouth, 50 south Street, Exeter 76058.

