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#### Abstract

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1.0
2.8
4.7
10
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47
100
890
470
100
220
470
10.0

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| code | Pomer | Toteraner | Raspo |
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| c | 1/20w | 5\% | $8: \Omega-240 \mathrm{~K} \Omega$ |
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| 310 | 1/2W | 2\% | $10 \Omega-13 \Omega$ |
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Band．Ext ra Mediun，uaveband prurlden etiojer tuniws of Radio Luxembourg，etc．Bullt in ferrite rod nerini for MKW and LWW．Retractable 4 section 24 la ．chrome plated telescopic aerial for 8 W．socket ior Car Aerial． Poweriul pusb－pull output． 7 tranasistrand and tuning maring collumefonfort tuning and wave change controls．Attractivo case wlth carrying bandle slize $9 \times 7 \times$ in．approx．Eany to follow inatructlons and diagrams．Parta price list and easy build plans 25p（PREE with parts）．
Farplece with plug and awitches anket fur privatc listening 33 p extra．
Total building costs $\mathcal{H}$ \＆ 5 （Overseas P．\＆P．41．05）GF 1116.47 J ．

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 7 otage－ 5 tranaintors and 2 dlodes，ferrite rod aerias．
tunlag condenser volume control．fine tons moring coil opeaker．Attractive caso whth red apeaker grilie．Slze of $x$ if $x$ dita．Easy build platid and parte price list 10 p （FREE with parta）


ROAMER SIX

8 Tunable wave
bende：MW，LW゙． SW1，8W2．\＆W3 Trawler，bandplus
an extra Srediunı an extra Mediuni wisveband fol
emaler tuning of Luxembours etc．Senaltivo fer－ rite rod aerial and
telescople serial
for gbort Wiares．
for Sbort Wares．
3in．Speaker．
3 in．Speaker．
stagen -6 transistore and as aioucs．Attractiso black casc with red grille，dial and black knobn with pollsbed metel laserts．Size $9 \times 5 t \times 2$ ilin．approx．Eatay balld Total building costs
（Oversean l．A P． 41.05 ）


6 Tunable Wave． banda：MW，LW． and Trawier Band
Senitive ferito rod aeria！for 3．W．and L．W．Tele． Sennitive ferito roi aerial for 3in．Speaker．Bimproved type tracsintori plus 3 diodes．Attractive case in black with red grille，dial and black knobs with poltahed metal ingerts．size $0 \times 5 i \times 2 i \mathrm{in}$ ．approx．Pueb poll output．Battery economiser amitch for extended battery Hfe．Ample power to drive a larger apeaker．Parta price list and eany bulld plane 25p（FREE wlith parts） Total building costs 4.19 P．P． （Oreries：P．\＆P．©1．0゙）

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| 100 | 0.28 | 0.37 | 0.32 | 0.52 | 0.55 | 0.55 |
| 200 | 0.59 | 1.27 |  |  |  |  |





## SIL. RECTS. TESTED

PIV $300 \mathrm{~mA} 750 \mathrm{~mA} 1 \mathrm{~A} \quad 1.5 \mathrm{~A} 3 \mathrm{~A}$ 10A 30 A $\begin{array}{lllllllll}50 & 0 & 04 & 0.06 & 0.06 & 0.08 & 0.18 & 0.23 & 0.66\end{array}$ | 100 | 0.04 | 0.07 | 0.06 | 0.15 | 0.18 | 0.26 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 0.83 |  |  |  |  |  | $\begin{array}{llllllll}200 & 0.0 & 0.10 & 0.07 & 0.16 & 0.28 & 0.27 & 0.27 \\ 400 & 0.10 \\ 400 & 0.15 & 0.08 & 0.22 & 0.30 & 0.41 & 1.38\end{array}$ $\begin{array}{llllll}400 & 0.07 & 0.15 & 0.08 & 0.22 & 0.30 \\ 600.11 & 1.38 \\ 8000 & 0.08 & 0.18 & 0.11 & 0.26 & 0.38 \\ 80.50 & 0.305 \\ 0.11 & 0.19 & 0.12 & 0.28 & 0.41 & 0.61 \\ 2 & 2.20\end{array}$




| triacs |  |  |  |
| :---: | :---: | :---: | :---: |
| vbosi 2 a |  | 6 A | 10A |
| T0.5 T0.66 TO-48 |  |  |  |
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1 MHz . Suitable replaceminnt for $2 \mathrm{~N} ~$
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Descriplion


 | U 3 | 75 Germanjuin Gold Bonded Bub-MIn. like OAS. OAt | $\ldots .$. | 0.85 |
| :--- | :--- | :--- | :--- | :--- | U 440 Gernmanfun Tranaigtoralike OC81. ACl28 U $5 \quad 60200 \mathrm{~ms}$ Sub M In. Silicon Dlodes

U 630 8ill. Planar Trans. NPN like B8TuSA. IN 706 U $7 \quad 16$ Sil. Rectiflers TOP-HAT 7B0mA VL.TG. RANGE up to 10000.85
 $\overline{\mathrm{U} 9} 20$ Mlined Voltages, 1 Wett Zeaer Dlodea
U10 $20 \mathrm{BA}^{\circ} \mathrm{E} 0$ chargo atorage Dlodea DO-7 (ilans
Ull $\overline{2} \overline{5} \bar{P} \overline{\mathrm{~N} P}$ 8j1. Planer Trang. TO.5 like 2N11s2, 2N2904 $\bar{T} 122-12 \overline{8}$ ilicon Rectitera Epoxy $500 \mathrm{~mA} \overline{\text { up }}$ to 800 PI U14 $1 \overline{150}$ Mixed Bilicon and Germanjum Diodes U16 25 NPN 811. Planar Trans. TO-8 like BPY51, 2N697 U16 103 Amp Silicon Rectiders Stud Type up to l000P1V

 U19 25 slitcon NPN Tranalators Ilke IBCl08

 U24 20 Germaninm 1 Amp Rectifern GJM Berles up to 300 PIV U25 25 300 MHz NPN Billicon Transistors 2N708, B8 $\mathbf{Y} 27$. U28 30 Fant 8witching silicon Dlodes like IN914 Micro-MIn. U27 12 NPN Germanlum AP Tranalatora TO-1 llke ACl27
 U30 15 Pleatic Blicon Plenar Trana. NPN 2N0928

| U31 20 | Bliticon Planar Plastic NPN Trans. Low Nolse Amp 2N 3707 | 0.65 |
| :--- | :--- | :--- | :--- | :--- | UX2 25 Zencer Diodes 400 mW DO. 7 cane 3-18 volt inlxed U33 15 Pisatic Cano 1 Amp siticon Rectiberu 1 N 4000 Serlen U34 30 8llicon PNP Alloy Trans. TO. $\bar{B}$ BCY $2628302 / 4$ U35 25 8illicon Planar Tranalators PNP TO-18 2 N 2906 U36 $\quad 25$ 8ilicon Planar NPN Translstore TO. 5 BFYb0/61/52 U37 30 Sillicon Allo5 Tranatatora 80-2 PNP OC200, 28322. U38 20 Fast 8 witching siticon Trans. NPN 400 MHz 2 N 301 l U39 30 RP. Gerin. PNP Tranalstorn 2N1303/5 TO-5 U40 10 Dual Trans!atorn 6 lead TO.5 2N2080 U41 25 jkFDermandum Trannlatore TO-1, OC45, NKTz! U42 10 VHF゙ Gernanium PNP Translatora TO. 1 NKT667, AF117 0. U43 25 8il. Trans. Plantlc TO-18 A.F. HC113/114 U44 20 811. Trans. Plantlc TO-6 BCLIS/116 U45 7 3A BCR. TO66 up to 600PIV

Code so's. mentloned above are given as a gulde to the trpe of derlce th the pak. The devicen themaelves are normally unmarked.

QUalit

Q1
02
$\begin{array}{ll}\text { Q1 } & 20 \\ \text { Q2 } & 10 \\ \text { Q3 } & \end{array}$
2 Red apot translatora PNP
16 White apot R.P. tranalatora PNP OC 7 type tranilatora
Matchell transistors OCAi//3/81/81D ${ }_{5}$ OC 78 tranastors
AC 128 transistors PNP high galn. AC 126 transistors PN OC 81 tyve transintora
107 OC 71 type transistors
Q11 2 AC $127 / 128$ Complementary pait
Q12 3 AF 116 type tranaistors.
Q13 3 AF 117 type tranaiators
Q14 3 OC 171 H.F. type transtators
mixel coloura Epoxy transiatore
Q16 2 GET880 low nolse Germanlum
Q17 5 NPN $2 \times 8 \mathrm{PT} 141$ \& $3 \times 8 \mathrm{~T} .140 \ldots$ Q18 MADTE $2 \times$ MAT $100 \& 2 \times$ MAT Q19 3 MADT'g $2 \times$ MAT $101 \& 1 \times$ अAT Q20 4 OC 4t Germaniun trannators A.P. Q21 4 AC127 NPN Cermaniurn transiator Q23 10 OA 202 sillicon diodes aub-min. Q24 8 OA 81 diodes
Q25 15 IN914 Bllicon diover 75 PIV'75ini
 Q28 2 10A PIV silicon rectimera 18425 R. Q29 4 Billicon trataiators $2 \times 2 \mathrm{~N} 696$
 Q31 6 Sllicon wwltch translators 2N708
Q32 3 PNP Billcontransistors $2 \times 2 N i 1$ i. Q $1 \times 2 \times 1132$


Q35 3 silicon PNP TO.S. $2 \times 2 N 2904$ \&
 Q37 3 2N3053 NPN Bllicon translators


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2 N 3055
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| $5 \times 7441$ | 0.74 | 0.71 | 0.64 | 9N74107 | 0.44 0.61 | 0.42 |  | +19522.20 | £2.09 ¢1. 27 | 1.98 +1.76 |
| 8N7442 Y 74. | 0.74 ¢1.43 | 0.71 41.38 | 0.64 51.32 |  |  | 0.59 21.27 |  | c1-98 |  |  |
| $\mathrm{yN7443}$ $\mathbf{8 N 7 4 4}$ | 11.43 21.43 | $21 \cdot 38$ 21 28 | 11.32 11.32 | 8.7411 | 21.38 | 21.27 81.05 | 11.2 0.9 | - $\times 1+19721 \cdot 88$ | +1.87 |  |
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| N7447 | ¢1-10 | 21.07 | 21.05 | 8574122 | 21.54 | 21.43 | 21 | astic |  |  |
| 7448 | 21.10 | 21.07 | 11. | 8N74123 | 23-08 | 28.97 | 22.8 | . \& 12.17812 | . 11 | 8 eacb |


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| Type No. | Price |  |  |
| :---: | :---: | :---: | :---: |
| BP 201C-8L201C | C8tp | 581 p | 491 p |
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| BP 702C-8L70\%C | 681p | ${ }^{35}$ | 49.p |
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| BP709-72709 | 3810 | 3715 | ${ }^{83} \mathrm{p}$ |
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* Overall size 63 mm $105 \mathrm{~mm} \times 13 \mathrm{~mm}$
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Tallor made to the mopt stringent apeclifeations using top quallty components and Incorforatiog the latest aold atate circuitry and ALSO wan conceivel to ill the nced for all your A.F athylincatlon needr.
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## STABILISED POWER MODULE SPM80

Also is especially designed to jrower 2 of the Also Amplinern, up to 15 watt (r.tn. a.) per channel minul and circuit techniques incorporatiag complete short circuit protection. With the addition of the Mains Transcormer MT80, the unit will provide outputs of up to $1 \cdot 5$ amps at 35 volts. $81 z e: 63 \mathrm{~mm} \times 103 \mathrm{~mm} \times 30 \mathrm{~mm}$. These unlts enable you to bulld Audio syatems of the highest quality at a hitherto unobtainable price. Alwo ideal for man other application Includins:- Diaco 8ynteras. Public Address Intercom Units, etc. Handbook avalable, 10 p PRICE $£ 3-25$
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Everything needed (except plywood) for building: 1 Invisible-Beam Projector and Photocell Receiver (as illustrated). Suitable for all Photoelectric Burglar Alarms. Counterb, Door Openers, etc.
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## Stereo radio from your existing tuner. <br> A complete set of parts


 from Jermyn to build a stereo decoder module that will convert your existing monotuner for stereo reception whilst maintaining a high standard of reproduction.

The distortion is very low (typically $0.3 \%$ at 560 mV RMS composite input signal) with 40 dB channel separation.

The stereo switching is automatic and there is a light emitting diode which acts as a stereo beacon.

The kit requires no coil and there are no alignment problems
Fitting. The module requires a 10-16 volt power supply which can normaily be tapped off the existing tuner. The signal input is taken off before the de-emphasis circuit which in practice means disconnecting one, or at the most, two capacitors. Any radio engineer will be able to spot these capacitors, but if you're really stuck send the circuit with a SAE to us and one of our engineers will indicate the out put point. (This is the full extent of our involvement, no hardware please)

Of course, if you have a modern mono tuner with a multiplex out-
put our module simply plugs in.
The outputs go via a screened twin cable to the tuner inputs of your stereo amplifier.
And the cost? $£ 4.90$ for the Kit with $100 \%$ tested integrated circuit. Also available assembled and aligned. checked and ready for use at $£ 6.90$ (includes 12 month guarantee). Beat that!
To Jermyn Industries Please rush me - Kit(s), $\square$ made up Stereo decoders. 183 Vestry Estate I enclose cheque/postal order for £
Sevenoaks
Name
Address

Block Capitals Please

All prices exclusive of V.A.T.

The leakage current of the NEW $\times 25$ is only a few microamps and cannot harm the most delicate equipment even when soldered "live" Tested at $1500 v$. A.C. This 25 watt iron with it's truly remarkable heat-capacity will easily "out-solder". any conventionally made 40 and 60 watt soldering irons, due to its unique construction advantages. Fitted long-life iron-coated bit $1 / 8^{\prime \prime}$ of damage to expensive transistors and integrated circuits, when soldering? Use Antex low-leakage soldering irons

## 220-240 Volts or 100-120 Volts

 harm the most delicate equipment "Iive" other bits available $3 / 32^{\prime \prime}$ and $3 / 16^{\prime \prime}$.Totally enclosed element in ceramic and steel shaft Bits do not "freeze" and can easily be removed

PRICE: £1.75 (rec. retail)
Suitable for production work and as a general purpose iron

The 15 watt miniature model CCN also has negligible leakage. Test voltage 4000 v . A.C. Totally enclosed element in ceramic shaft. Fitted long-life iron-coated bit 3/32"
4 other bits available 1/8', 3/16" $1 / 4^{\prime \prime}$ and $1 / 16^{\prime \prime}$ PRICE: $£ 1.80$ (rec. retall) OR Fitted with triple-coated, (iron, nickel and Chromium) bit 1/8" PRICE: $£ 1.95$ (rec. retail)

A SELECTION OF OTHER SOLDERING EQUIPMENT.


MODEL CN
Miniature 15 watt soidering iron fitted $3 / 32^{\prime \prime}$ ironcoated bit. Many other bits available from $3 / 64^{\prime \prime}$ to $3 / 16^{\prime \prime}$. Voltages $240,220,110,50$ or 24
PRICE: $£ 1.70$ (rec. retail)
MODEL CN2
Miniature 15 watt soldering iron fitted with nickel plated bit $3 / 32^{\prime \prime}$. Voltages 240 or 220.
PRICE. £1.70 (rec. retail)

MODEL G
18 Watt miniature iron, fitted with long life ironcoated bit $3 / 32^{\prime \prime}$. Voltages 240,220 or 110. PRICE. £ 1.83 (rec. retail)

MODEL
SK. 1 KIT

contains 15 Watt miniature iron fitted with $3 / 16^{\prime \prime}$ bit, 2 spare bits $5 / 32^{\prime \prime}$ and $3 / 32^{\prime \prime}$, heat sink, solder, stand and "How 10 Solder" booklet.
PRICE $£ 2.75$
(Rec. retail)
MODEL SK. 2 KIT
contains 15 Watt miniature iron fitted with $3 / 16^{\prime \prime}$ bit.

2 spare bits $5 / 32^{\prime \prime}$ and $3 / 32^{\prime}$

heat sink, solder and booklet"How to Solder

## MODEL



PRICE £2.40
(Rec. retail)
MES.KIT Battery-operated 12v. 25 watt iron fitted with 15' lead and 2 heavy clips for connection to car battery. Packed in strong plastic wallet with booklet "How to Solder." PRlCEfferalr 95


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## UNISOUND FORTHENEW SOUND

AT It's the RT.VC system that screws together to save you pounds! Unisound 2 5 - comprises two superb speakers and an amplifier/record deck plinth-all beautifully finished in simulated teak. The stereo amplifier ( 4 watts per channel into 8 ohms) is based on the famous Mullard Unilex system brought up-to-date INC. by RTVC using intergrated circuits. Turntable ts the proven Garrard 2025TC VAT complete with stereo cartridge and tinted acrylic cover. Speakers are big EM Twin-cone units all ready for mounting in their elegant cabinets, which simply need screwing and glueing together. Easy step-by-step instructions. £26.12 complete plus £1-40 packing $+\boldsymbol{£ 1} \cdot \mathbf{4 0}$ post. Diamond Stylus $£ 1-25$ extra. Stereo headphones with adaptor $\mathrm{E}_{4}$ extra. Send for teaflet. For the man who wants to desion his own stereo-here's your chance to start. with Unisound-Dre-amp. power amplifier and control panel. No soldering-just simply screw together. 4 watts per channel into 8 ohms. Inputs: 120 mv (for ceramic cartridge). The heart of Unisound is high efficiency I.C. monolithic power chips which ensure very low distortion at all power levels over the audio spectrum. car radio kit It's simpleutton follow the step-by-step instructions.
 comprehensive instructions 50 p free with parts.

Fully retractable lockable car aerial £1-25 post paid.

PRICE ONLY £7.70 p. and p. 55p
Speaker with bafile and fixing strips $£ 1.50$. 25 p. \& p., post free if bought with the kit. Send for leaflet.

The Tourist PB is suitable for 12 volt working on both negative and positive earth vehicles. It covers the full medium and long wave bands. It is permeability tuned and sturdily constructed. Output is a full 2.5 watts into an 8ohms speaker. But the Tourist PB will operate into any loudspeaker from 8 to 15 ohms.
Apart from the output stage, which is an intergrated circuit, the only other electronic components that need soldering are some capacitors, resistors, etc. The kit includes a pre-built RF tuner unit, and fully modulised IF stages which are pre-aligned before despatch. As well as electronic components this kit also contains 2 diamond-spun aluminium knobs, elegant matching front panel, dial, washers, screws and wire.
The Tourist PB can be mounted in any standard size dash panel and it has an illuminated tuning scale. Chassis size is: $7^{\prime \prime}$ wide, $2^{\prime \prime}$ high and $4 t^{\prime \prime}$ deep.

## RELIANT MkIV <br> A GOOD QUALITY AMPLIFIER- 12 Watts £ $10 \cdot 50$ (inc. VAT). 20 Watts £ $13 \cdot 50$ (inc. VAT) <br> *5 Electrically Mixed inputs. *3 Individual Mixing controls. *Separate bass and treble controls common to all 5 inputs. "Mixer employing F.E.T. (Field Effect Transistors). -Solid State Circuitry. *Atractive Styling INPUTS 1. Crystal Mic or Guitar 9mV. 2. Moving coil Mic. or Guitar 8 mV Inputs, 3,4 \& 5 are suitable for a wide range of medium output equipment (Gram. Tuner, Monitor, Organ, etc.) All 250 mV sensitivity. <br> Size approx. $12 \frac{1}{4} \times 6 \times 3 \frac{1}{2} \mathrm{ins}$.



50 WATT AMPLIFIER. Output Power: 45 watts R.M.S. (Sine Wave) Frequency Response 3dB points 30 Hz and 18 KHz . Total Distortion: less than $2 \%$ at rated output. Signal to noise ratio: better than 60 dB . Bass Control Range: 13 dB at 60 Hz . Treble Control Range: 12 dB at 10 KHz . Inputs: 4 inputs at 5 mV into 470 K . Each pair of inputs conrotlled by separate volume control. 2 inputs at 200 mV into 470 K . Size: $531-35$ $\mathbf{£ 1} \cdot 50 \mathrm{p}$, and p .
(inc. VAT)


## PE TAPE LINK

 CONSTRUCTORSSuitable 3 speed tape deck, less heads. Caters up to 7ins. spools. Unused but store soiled hence no war-$-88$
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plus £1p \& $p$

Denotes VAT has been absorbed in the price without increase on VISCOUNT audio systems.
$14+14$ w. r.m.s. 40 Hz to $40 \mathrm{kHz} \pm 3 \mathrm{~dB}$. Total distortion at 10 w . at $1 \mathrm{kHz}-0.1 \%$ This is real value for money! We have designed 2 systems and the heart of them both is the Viscount III amplifier. A unit of great eye appeal with teak finished cabinet. FET's (Field effect, transistors) are incorporated on the input stages, just like top priced units. FET's give you more of the signal you want and almost none of the hiss you don't. Both units have output sockets for headphones and tape recorder.
For both systems we have chosen the famous Garrard SP25 Mk. III deck, with fitted magnetic cartridge, which comes complete with simulated teak plinth and tinted acrylic cover.
The exclusive Duo loudspeaker systems are incomparable for quality within their price range. Large speakers in extremely substantial cabinets. There's a choice of the Duo Il's for the smaller room or the big Duo
Ill's for real bass response.


PRICES: SYSTEM I
Viscount III R 101 amplifier Garrard SP25 Mk.lll with
MAG. cartridge plinth \& cover
Available complete for only $£ 52^{*}+$

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£ 3.50 \mathrm{p} . \& \mathrm{p} .
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PRICES: SYSTEM 2
Vicoune R 101 amplifier 2 Duo Type III speakers
Garrard SP25 Mk. II with rotal $\overline{\underline{E 4 \cdot 40}}$ Available complete for $\overline{£ 69^{*}}+$
$124.20+11 p{ }^{2} p$
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 AUDIO STILLONLY£52 COMPLETE

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- WHY did you buy this copy of Practical Wireless? Were you influenced by advanced publicity or advertising; are you a regular reader with a devotion to follow our activities month by month; or are you one of many thousands who pick up this magazine to seek guidance on what makes radio and electronics tick? It has been said that
- people read Practical Wireless to learn something about the subject. After all, it is a technical field that demands some education and understanding and it is really this aspect that "makes most people read.

To supplement professional career requirements there is a growing band of people who are bank clerks, clergymen, accountants, businessmen, as well as students and technicians who are seeking part time courses on the practical side of radio and electronics. Some colleges are able to offer facilities, subject to minimum class size, but we have heard of cases where they cannot find enough qualified engineers who are willing to spend extra time in the evenings to instruct these students. It is a pity because it often means that a course has to be dropped because of this.

So we come back to magazines; Practical Wireless is used in schools and colleges to a great extent because it provides an excellent support service to instructors, many of whom cannot always find sufficient time in addition to their everyday jobs to make full preparation for classes. Practical Wireless is a leader because its articles and designs are "down-to-earth" and, in spite of competition from elsewhere, we still offer the greatest constructional project support to instructors, technicians and engineers, while encouraging the confidence of newcomers.

This month we have rubber-stamped this policy by giving you for the first time a unique supplement containing eight extra straightforward constructional projects for the home, attractively presented with abundant illustrations and a full colour cover picture. To make it easier for you to find this supplement and worthwhile to keep for reference, we have printed it on a pleasant shade of "apple-green" coloured paper-another first for Practical Wireless.

Don't let this divert your curiosity too far from our other usual features because you will also find much more to interest you in this issue. For the benefit of quick and easy reference you will also find our contents list just inside the front cover, together with information on many aspects of our service. And watch out for next month's issue too for more special attractions, some of which are mentioned in this issue.
M. A. COLWELL-Editor

[^2]NEWS...

## B.R.C. change their name

BRITISH Radio Corporation Limited announced on the Ist April that it has changed its name to Thorn Consumer Electronics Limited. It continues to manufacture and market audio and TV products under the Ferguson, HMV, Ultra and Marconiphone brands and remains a wholly-owned subsidiary of Thorn Electrical Industries Ltd.

## VAT

To the best of our knowledge. the prices quoted in this issue were correct at the time of going to press.

As from April 1st, 1973, there is no purchase tax but a large number of goods carry Value Added Tax.

## The "N.F.A.C."

THE National Federation of Aerial Contractors Limited is making an attempt to "clean up" the aerial contracting industry.

The Ministry of Posts and Telecommunications listed 55,000 complaints of bad reception in their recent annual report. Out of 32 listed causes of complaints. the largest numbers were for "inefficient aerial installations" and the N.F.A.C. feels that it can help this state of affairs by alerting the consumer and all who employ aerial contractors that there are in existence a very large number of "Rooftop Racketeers".

Plans currently being considered by the Federation include random inspections of members' installations and a system whereby new companies applying for membership will have their work inspected in addition to the trade references that are already required. A special Standards Committee will hear reports of faulty workmanship.

By this system, the N.F.A.C. hopes to assist in narrowing the field of consumer complaints and possibly convince dealers that they mean to play their part in cleaning up the aerial contracting industry.

Mullard film on I.C. design

Mullard Ltd. have announ. ced a new 16 mm colour film lasting 18 minutes. It's called The Computer-Aided Design of Integrated Circuits and is available on free loan from the Mullard Film Library, 269 Kingston Road, Merton Park, London, SW19 3NR.

The film, which was shot mainly on location at the Mullard semiconductor plant at Southampton, describes in detail the use of the computer and its peripheral equipment in such functions as IC design and layout, mask-making and testing at every stage of production.

## Tandberg in the jungle

Sergeant J. Murtagh of the Royal Signals is seen in the picture using a Tandberg Series 11 portable tape recorder. This machine and a TP4-1 portable radio accompanied a recent British Trans-Americas expedition which took in 18,000 gruelling miles from Alaska to the tip of South America. The purpose of the journey was to survey a road through the uncrossed 300 miles of swamp and jungle bordering the Panama canal which blocks the Pan American highway system.

During the trip, the expedition kept in touch with the outside world with the TP4-1 receiver, picking up BBC news broadcasts and weather reports.

In the jungle and swamps, the electrical equipment was carried in man-packs or by ponies and although it was partially immersed in water, rolled on several times by the ponies and carried through thick mud, it continued to function without a fault.

## Signals "piped" through waveguide

THE core of a system which, when fully implemented, will transmit 300,000 phone conversations or 200 colour TV signals at the same time through a waveguide "pipe" is now operating at the GECMarconi works at Great Baddow.

This equipment will be used by Post Office engineers in a field trial system to be installed between the Post Office Research Station at Martlesham, Suffolk and a Post Office site at Wickham Market, 15 kilometres away.

The new "pipe" is a 50 mm diameter circular waveguide capable of supporting signals throughout the frequency band from about 32 to 110 GHz . The photograph shows 32.50 GHz channel separating filters and band-branching assembly.


## Texan reprints

REprints of the "Texan" $20+20 \mathrm{~W}$ Stereo Amplifier are available.
They may be obtained by sending $35 p(30 p+5 p)$ postage/packing to "Texan" Reprint, c/o Chief Cashier, Practical Wireless Tower House, Southampton Street, London WC2E 9QX.


Sgt. Murtagh of the Royal Signals.

## World Radio Club

FURTHER to the item on the World Radio Club in the March issue, we have been informed by the programme Producer that an extra broadcast in the BBC World Service will be made each week at 20.30 GMT on Thursdays.

The midday edition has now been moved to $13 \cdot 30$ GMT on Wednesdays. The other Friday and Sunday transmissions remain unaltered. BBC, Bush House, P.O. Box 76, Strand, London WC2B 4PH.

## Some S.E.R.T. meetings

The Society of Electronic and Radio Technicians, Faraday House, 8-10 Charing Cross Road, London, W.C.2. will be holding the following meetings:
April 11: "Test Equipment" by B. Ellison from Tektronix. Venue is The Conference Theatre, I.B.A., 70 Brompton Road, London, S.W. 3 and the lecture commences at 7.00 p.m.

April 5: "Colour TV Forum and Exhibition". This will be held in the Byng Kendrick Suite, University of Aston, Birmingham, commencing at 7.00 p.m.

April 24: "The CVC5 Colour Receiver" by A. E. Thomas from ITT. This will be held in the Cleveland Scientific Institution, Corporation Road, Middlesborough. Meeting starts at 7.30 p.m.


THIS is a self-contained receiver which may be used over the range $115 \cdot 150 \mathrm{MHz}$, or 140 . 190 MHz , according to the coil fitted. It was actually found to maintain good efficiency even up to 210 MHz . A vertical telescopic aerial or improved aerial system will provide reception on the internal speaker, an outlet being present for headphones when required. An optional preamplifier is also described.
The receiver has a superregenerative detector, which is a great advantage from the point of view of simplicity. This type of detector is highly sensitive, and it should be possible to copy a signal of under $1 \mu \mathrm{~V}$. There is also only one tuned circuit, so no alignment or ganging difficulties arise. The bands include the 2 -metre amateur band ( $144-146 \mathrm{MHz}$ ). In terms of sensitivity, most signals which can be well received with the simpler type of convertercommunications receiver combination can also be received satisfactorily with this receiver.
A disadvantage sometimes encountered with this type of receiver is tricky tuning and hand-capacity
effects. These do not arise here, due to sound construction and a metal case and so actual use of the receiver is easy.

## Circuit Details

Fig. 1 is the circuit, employing a junction f.e.t. in the first stage. The rod or other aerial is coupled by L 1 , and L2 is tuned by VCl. The network R2, C4, R3 and C5 gives a suitable quench frequency and regeneration is controlled by VR1. To modify the tuning range, 22 only need be changed.

A three-stage audio amplifier assembled on a separate circuit board follows. $\operatorname{Tr} 2$ is the first audio amplifier, $\operatorname{Tr} 3$ the driver, and $\operatorname{Tr} 4 / 5$ the output pair, operating a small speaker in the case. The outlet takes a jack plug for an external speaker or phones, if wanted, and VR2 is the volume or audio gain control. R12 is a small pre-set potentiometer, which allows working conditions for the output pair to be suitably adjusted.


Fig. 1: Circult of the main receiver. The circult of the pre-amplifier is shown in Fig. 4. The heading pholograph shows the two untts bolted together.


Fig. 2: Layout of the main components and audio ampllfier board within the cabinet. When the preamplifier is fitted the coaxial aerial socket is removed and used on the preamplifier box.

## Photograph looking into the top of the receiver which may heip when locating

 components as in Fig. 2 above.
## Cabinet Construction

Flanged universal chassis members $7 \times 3$ in form the front and back, and similar parts $5 \times 3$ in are the sides. The top and bottom are $7 \times 5$ in flat plates.

The front member is drilled for VCl, VR1 and VR2, as in Fig. 2. Also punch or drill holes for a co-axial socket on the right hand side, or for an insulated terminal or socket, if a co-axial feeder is not required here.

An opening is cut in the left member for the speaker, taking care that this will clear the amplifier and other parts. Perforated zinc or expanded metal is placed over the aperture, and the speaker is bolted on. The jack outlet is placed as shown.

The four flanged members are then assembled by bolts through the holes present in them. Four holes are drilled in one $7 \times$ 5in plate, these are marked through so that the flanges can be drilled to suit. The case bottom can then be attached. Two rubber feet were placed on the front bolts, to raise the front of the receiver slightly.

It is easier to assemble the receiver if the sides and back are left off until later. When all construction is finished, the top $7 \times 5$ 5in flat plate is fixed with four self-tapping screws.

## Detector Stage

This is wired as in Fig. 2. A 3-lead holder is used for Trl. This avoids possible damage from heating while soldering, and also allows the transistor to be changed, if necessary. The MPF102 is listed as having a top frequency of 200 MHz . Some were found to perform satisfactorily at well above this, but others, not up to specification, would only operate at relatively low frequencies.

The holder drain tag is soldered directly to the lower fixed plates pillar of VC1. The leads of C3 are cut short, and this item is soldered from the source tag, to the top pillar of VCl. A stout wire is also soldered to this pillar, projecting back about ${ }_{1}{ }_{2}$ in so that L 2 can be changed without unsoldering other items.


A stout lead from the gate tag goes to the moving plates contact of VCl , just clearing the moving plates. The tag strip holding R 1 and C 2 is raised on a long bolt, so that wires from Cl are as short as possible. A wire projects upwards about ${ }_{2}$ in to take the other end of L2.
L1 is a single turn of insulated wire. Coupling can be adjusted by rotating this small tag strip slightly on its fixing bolt, but it is not very critical.

L3 is self-supporting, and is 30 turns of 26swg enamelled wire, wound on a ${ }_{4}$ in diameter object which is afterwards removed. Turns are closewound. One end is soldered to the tag supporting R2, C4 and R3, and the other end is soldered to the source tag of Trl holder.

The potentiometers and other parts can then be wired as in Fig. 2. A lead will run from VR2 under the speaker to the input pin of the audio amplifier.

## Audio Amplifier

This is assembled on Veroboard $5 \times 1^{3} \mathrm{in}$, as in Fig. 3. First drill two holes for the chassis bolts, position the board in the case, and mark and drill
matching holes in the metal bottom. Tags held with the bolts form earthing points, Fig. 3. The bolts are ${ }_{1}{ }_{2}$ in long, so that extra nuts hold the assembly clear of the metal case, lock-nuts underneath securing the amplifier. A piece of card $5 \times 1^{3}{ }_{4}$ in may be put between the amplifier and case bottom, though shorts to the metal will not arise if joints are kept close to the board.

## Coils

These are self-supporting, wound with 18 swg, 20 swg or other stout wire, with spaced turns. A coil having 4 turns, ${ }_{2}$ in outside diameter, and $7_{8}$ in long, was found to tune $115-150 \mathrm{MHz}$. This is suitable for 2 metre reception.


Flg. 3: Diagrams of the component layout and wiring of the audio amplifier board.

Take care to fit the electrolytic capacitors as indicated. With a unit of this kind, it is helpful to place black lmm sleeving on the negative line leads, and red sleeving on positive leads. With another colour for other wiring, it will be easy to check connections if this should prove necessary.
The amplifier may be tested before fixing it. Place the slider of R12 at about the central position. Connect the speaker and a 9 V battery, negative to one of the chassis tags. Either place a meter in one battery lead and move the slider of R12 for a current of 10 mA , or adjust R12 to place just enough resistance in circuit for speech to sound normal. If R12 is at a very low value, current drawn will be small but cross-over distortion will be present.
For this test, input can be from any convenient source; a signal generator, diode tuner, pick-up, or from the first stage of the completed receiver. If VR2 is not in circuit, avoid overloading the amplifier by the test signal.

The amplifier is fitted as shown, negative return being through the metal case. Connect the speaker leads and amplifier to the jack so that the contacts which open silence the speaker, when phones or an external speaker are in use.

A coil ${ }^{1}{ }_{2}$ in long and ${ }^{7}$ in in in diameter, having three turns, tuned $192-150 \mathrm{MHz}$, while a similar coil having two turns allowed 216 MHz to be reached.
Stray circuit capacitances and the length of connecting leads influence the frequencies tuned. The frequency can be raised by reducing the number of turns, or by stretching the coil to separate turns, or by reducing the overall diameter.

## Operating notes

When VR1 is advanced, a position should be found where a strong hiss begins. This is roughly the correct setting for VR1, though it will be found that further slight adjustment may be helpful, depending on the strength of the signal tuned in.

The hiss should cease when any signal of sufficient strength is tuned in, provided VR1 has not been turned too far. VR2 adjusts volume in the usual way, and can probably be advanced about half way, for the internal speaker.
If superregeneration is impossible on some part of the band, move Ll a little further from L12. This

is not critical, but tight coupling will tend to prevent regeneration, while very loose coupling will reduce signal strength.

## Aerials

There is room for considerable experiment here. Some local transmissions (range about 10 miles) were received with about 6in of wire projecting from the socket, which shows how sensitive this type of circuit can be.


This view of the receiver shows the positioning of the internal loudspeaker and the socket for an external ioudspeaker or headphones.

With a telescopic aerial extending to three feet, a considerable number of transmissions were received, including amateurs over 50 miles away. This aerial performed poorly with the receiver and aerial near a metal window, but was better in the centre of a downstairs room, and even better in an upstairs room. Reducing the length to about two feet made almost no difference, and sliding the sections up and down did not give any notably best or critical resonant length.

Best results of all on 2 metres were obtained with a dipole made from ${ }^{\frac{1}{4} \text { in aluminium tubing, } 381_{2} \text { in }}$ overall, with a centre co-axial feeder. This aerial was mounted out of doors on a light pole. A long or lossy feeder would tend to lose much of the advantage such an aerial can give.

The angle and slope (polarisation) of all these aerials had some influence on results. No doubt an improved VHF aerial would increase signal strength, but some means of rotating it would be needed, and this was not felt justified.

## Pre-amplifier

The receiver has high sensitivity, but in some circumstances there are advantages to be obtained by adding an r.f. stage. This stage will materially reduce radiation from the superregenerative detector, and also help isolate the aerial to avoid dead spot or damping effects on some frequencies. In fact, these are the most important advantages, and much gain must not be expected from the r.f. stage at frequencies over 150 MHz or so.
Fig. 4 is the circuit, the f.e.t. being used in a grounded-gate arrangement which does not need neutralising. Ll is peaked by the small capacitor VCl. Tuning is flat, and needs no adjustment over a small band.


Fig. 4: Circuit of the pre-amplifier and connections to the input circuit of the main receiver.

The f.e.t. drain circuit is to the coupling loop L2, which was originally used for aerial coupling in the receiver. Alternatively, a broadly resonant winding can be used here, resulting in better gain over a narrow band of frequencies.

## Cabinet

The box is $3 \times 2 \times 2$ in and is bolted on the metal side of the receiver case. It is made from a flat piece of aluminium $7 \times 2$ in and one $7 \times 3$ in flanged "universal chassis" member.
The long flanges are cut 2 in from each end, a $90^{\circ}$ piece being removed. A piece of wood about


Fig. 5: Positioning of the few components within the preamplifier box.
$3 \times 2$ in and ${ }^{1} 2$ in or so thick is then placed between the flanges, and another piece of wood is placed level with this, and the whole gripped tightly in a vice. The $7 \times$ 3in member is then bent into a $3 \times 2 \times$ 2 in box, with the flanges inwards. Fig. 5 shows this part from behind. The front is drilled for VC1, and one side for the co-axial or other aerial socket. Three holes are also drilled in the other side, to match up with the holes which are exposed when the co-axial socket is removed from the receiver.

The $7 \times 2$ in piece is bent at 2 in from each end, in the same manner, so will fit on to enclose the box. It is held with a number of self-tapping screws.

## Pre-amplifier Wiring

The transistor holder (or transistor) is soldered directly to VC1, as in Fig. 5. All leads are as short as possible.

L1 is wound with 18 or 20swg copper wire, and is similar to the coil in the receiver, but will generally have to be stretched somewhat, or have

## components list

$$
\begin{aligned}
& \text { R1 } 220 \Omega \pm \mathrm{W}, 5 \% \\
& \mathrm{C} 10.0 \mu \mathrm{~F} \\
& \mathrm{C} 20.01 \mu \mathrm{~F} \\
& \text { VC1 } 10 \mathrm{FF} \text { or similar miniature variable, or pre-set. } \\
& \text { Tr1 MPF102 } \\
& \text { Universal Chassis flanged side } 7 \times 3 \text { in. (Home Radio) } \\
& \text { Aluminium 7x2in. } \\
& \text { Knob, tag-strip, etc. }
\end{aligned}
$$

The components listed above for the pre-amplifler are additional to those required for the maln receiver.
about one less turn. If maximum volume is with VC1 fully open, this shows that L1 should be changed, by removing a turn, spacing turns further apart, or winding a new coil of smaller diameter.

The position of the aerial tapping depends somewhat on the use of a co-axial fed dipole or similar aerial, or a short vertical rod type aerial. This tapping can usually be about one-quarter to one-third the total number of turns from the Cl (earthed) end.

Two bolts fix the r.f. stage to the side of the receiver, and a lead from Trl drain passes through the original aerial socket hole to L2.

## Receiver Changes

The tag strip holding L2 is replaced by one having two insulated tags. A lead from one tag is run to a positive pin on the a.f. amplifier and C2 is connected from this tag to the chassis tag, as in Fig. 5. The drain lead is taken to the other tag.

L2 is one turn of insulated wire, positioned near the detector coil. Coupling is adjusted for best regeneration, by bending the loop L2 to adjust the distance to the detector coil, as with the original circuit.


Rear view of the completed pre-amplifier bolted to the receiver.
It was found that results were better with coupling in one phase. To check for this, twist L2 $180^{\circ}$, to change its sense with relation to the detector coil.

As mentioned, L2 can be resonant over a narrow band. This increases gain, but makes it a little more troublesome to change coils or cover a wide band of frequencies. If this method is to be tried, wind L2 with one or two extra turns, compared with the detector coil, using insulated wire to avoid shorts. It is then necessary to stretch or compress L2, or change the number of turns, until it is found to peak up signals in the wanted frequency range. The resonant effect is quite flat, but these adjustments, and the degree of coupling with the detector coil, and position of the aerial tapping, can make quite a difference to reception.

[^3]

## FETRONS

THE field effect transistor (FET) is currently being used in the front end of a.f. and r.f. circuits, as well as being developed into simplified forms of logic circuitry for micro-miniature applications such as wrist watches and pocket calculators. Aside from the manufacturers of such luxury items, our attention is turned here to more domestic matters such as television receivers, radio, transmitters and receivers. Where thermionic valves are still being used, there is some reluctance to effect a total conversion to semiconductor techniques. We can have the best of both worlds because we can now replace valves in some circumstances with direct equivalent improved performance transistors. Particular areas of application also include unattended relay stations, and telecommunications terminals, as well as domestic receivers.

## TRIODE EQUIVALENT

These transistors, called "fetrons," have emerged from the military applications stable and are being made available for other applications, although very little is generally known about the performance so far. The fetron is basically an arrangement of two $n$-channel field effect transistors (Fig. 1) connected to provide the equivalent working characteristics of a triode valve but with a much better frequency response at both ends of the spectrum. This is because the fetron has an extremely low channel resistance and inter-electrode capacitance. Furthermore, since there are
no heaters, operation is immediate on switch-on.

## OTHER FEATURES

The life of the fetron is likely to be much greater than the thermionic valve under normal working conditions and the degradation of operational characteristics is minimal. Other important features include a higher amplification factor (almost ten times that of a valve) and a lower noise figure. Since no heaters are used, power requirements are simplified to just one high tension supply.

## PENTODE CHARACTERISTIC

Both the thermionic valve and the FET are voltage controlled devices, hence design equations are virtually the same. Although the pentode an ode voltage-current characteristics are similar to the drain characteristics of the fetron, the latter are more clearly defined at the cut-off region
or "knee" and exhibit stable current drain for various drive conditions (Fig. 2).
Since the main purpose of the fetron is to act as a direct replacement for the triode valve, it is essential that it should withstand high voltages and have a matched gm . The single junction FET cannot do this, but when two specially selected FETs are cascaded the problem is overcome. It is also possible to reduce the Miller (gate to source capacitance) effect by using a low capacitance, small signal, high gm FET at the input circuit, coupled with a high voltage output FET.

With the arrangement shown in Fig. 1, the output FET acts as a voltage dropper for the input FET and the Miller effect capacitance of each is in series. The output impedance is also greater than in a valve pentode, resulting in the excellent characteristics shown in Fig. 2. Since the input gate circuit is effectively a reversed bias junction, it presents a very high resistance load to the signal source.

Fig. 3 shows the transfer characteristic of a fetron which has been made

Fig. 1: Basic arrange. ment of two fleid effect transistors in one package to form a fetron, and the symbol of the 6AK5 valve.


TABLE 1:


TABLE 2

| TYPICAL TRIODE DEVICE CHARACTERISTICS |  |  |
| :--- | :--- | :--- |
| (EACH SIDE)-RK $=2-70 \Omega, E b=130 \mathrm{~V}$ |  |  |
| PARAMETER | $12 A T 7$ | TS12AT7 |
| Plate voltage breakdown | $400+\mathrm{V}$ | 350 V |
| Plate resistance | $15 \mathrm{k} \Omega$ | $250 \mathrm{k} \Omega$ |
| Transconductance | $4,000 \mu$ mhos | $3,000 \mu \mathrm{mhos}$ |
| Plate current (Rk $=240 \Omega$ ) | $5 \cdot 0 \mathrm{~mA}$ | $9 \cdot 0 \mathrm{~mA}$ |
| Grid voltage for Ib $=110 \mu \mathrm{~A}$ | $-7 \cdot 0 \mathrm{~V}$ | $-7 \cdot 0 \mathrm{~V}$ |
| Amplification factor | 60 | 750 |
| Input capacitance | $2 \cdot 2 \mathrm{pF}$ | 25 pF |
| Output capacitance | $1 \cdot 5 \mathrm{pF}$ | $3 \cdot 5 \mathrm{pF}$ |

up from selected FETs to approximate closely that of a particular valve (shown dotted) operating within the same limits. If special requirements include partial operation beyond this FET cut-off then clearly a more appropriate FET device must be selected for this, perhaps providing a higher current for the same control voltage. The gm or transconductance ratio of the fetron gives a true square law property with consequent harmonic distortion figures of an extremely low order. In fact, harmonics beyond second order are claimed to be negligible.

Although the simulation of the "screen grid" principle can be effected within the fetron package, the similarity of the transfer curves to those of a pentode must not be taken as an assumption that the fetron is an ideal replacement for the pentode, even though the noise figure may be lower. The fetron has a markedly improved performance over the triode due to square law operation.


Fig. 2: Comparison of output drain characteristics with those of the 6AK5 anode.


Fig. 3: Transfer characteristic of a fetron compared wilh a valve.
fetron for replacing the 12AT7 is TS12AT7.
The manufacturer who has announced these activities in fetrons is the American company Teledyne Semiconductors, who are selling in the U.K. via the distributors GDS Sales Ltd. of Slough. Prices are higher than for valves but this is offset by the long term performance advantages described. GDS Sales quotes $£ 8$ for the TS12AT7 and $£ 6.50$ for the TS6AK5 for orders of 1 to 99, these being the first available in the U.K. Although this price is high the long term advantages of reliability and performance are compensatory.Small orders for these devices are being handled by the subsidiary company Best Electronics(Slough) Ltd, Michaelmas House, Salt Hill, Bath Road, Slough, Bucks, SL1 3UZ.

Elsewhere in this issue we are taking a closer look at some of the valves that still have a unique role to play in radio and electronics. Look out for our special feature "Special Valves for Communications".


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## CIRCUIT

In the basic circuit, Fig. 1, the reference voltage is determined by a zener diode ZD which controls the output voltage. Trl, a power transistor, takes a small current from the zener diode, amplifies it, and feeds the resulting current to the output circuit.


Fig. 1: Basic stablifing circuits for a) negative and (b) positive "earth".

With the output circuit left open Trl remains off, but as soon as a load is connected the current will increase until the voltage at the output is a little less than that of the zener diode. If for any reason the output voltage increases the voltage across Trl's base-emitter decreases causing the collector current to drop. Conversely, if the output voltage decreases the base-emitter voltage will increase, raising the collector current. The overall effect being that the output voltage will remain constant despite varying load currents.

## OVERLOAD

Although the basic circuit will work quite satisfactory, if the output leads are accidentally shorted together a heavy current will flow which may damage the transistor before the fuse can blow. To insure against this the circuit can be modified to the form shown in Fig. 2. Here, no matter what the load, even a short circuit, no more than 330 mA will flow. Under normal loads the voltage across R2 will be less than the 500 mV or so required to start Tr 2 conducting, so the circuit will work as in Fig: 1.


Fig. 2: Protected circuits for negative or positive "earth".

However when the current exceeds 280 mA this will no longer obtain and Tr2 will start to draw current from the zener diode. At first this will have no effect, but if the voltage across R2 increases further Tr2 will draw more and more current until finally the zener will stop conducting, thus enabling the output voltage to fall to a level where no more than 330 mA flows.

| Output Voltage | 2D (400mW) | R1 ( ZW$)$ |
| :---: | :---: | :---: |
| $6 \mathrm{6V}$ | 6.2 V | $680 \Omega$ |
| 7.3 V | $7 . \mathrm{V}$ | $390 \Omega$ |
| 9 V | 9.1 V | $220 \Omega$ |

## CONSTRUCTION

The unit is built into an aluminium box approx. $3 \times 2 \times 2 \mathrm{in}$. (Type AB12) the power transistor being bolted to the box after applying silicone grease. The few components are connected directly to the pins of the power transistor. Since the quiescent current is only about 13 mA no on-off switch is fitted.

## BACK NUMBERS

We regret that the back numbers department of P.W. has now closed and consequently we are unable to supply these. Requests for specific back issues can usually be included in our 'CQ' section; there is no charge for this but it is a service between readers and P.W. is unable to meet any of these requests.

## TWO VERSATILE TRANSISTOR AMPLIFIERS

Aan independent service engineer one is often called on to repair car radios whose age, or foreign origin, make it difficult, if not impossible, to obtain spares. Quite often there is a burntout output or driver transformer which would normally result in the set involved being scrapped. To avoid this it has been possible, over a period of time, to evolve two output stages which employ no transformers or "difficult" components. The transistors used are easily obtained and cheap. In fact, one aspect of the design was to take advantage of the excomputer panels now widely on sale, which contain large numbers of suitable transistors, etc.

## CIRCUIT No. 1

The first design is intended to take the place of the relatively low-powered output stage used by several firms in hybrid car radios. A typical set employed two " 12 volt h.t." valves and three transistors, an OC81d driving a pair of OC81's. The original OC81d is retained, but with a slightly different emitter resistor, and feeds directly into a complementary pair, ACl27 and ACl28.
The actual construction is so simple that it may be done on a seven-way tag strip. It will usually be possible to use the heat sinks previously fitted to the OC81's. The sole drawback, if such it be, is that the loudspeaker has to be changed to a high impedance type.


Two transistor output stage added to existing OC81D stage in receiver.

## CIRCUIT No. 2

It was to provide more power than the AC127/128's could give, and also to avoid having to use special loudspeakers, that the second circuit was evolved. It consists of an amplifier, a driver, and a complementary stage, which in turn drives the output transistors. In this circuit the computer panels really came into their own. Those used contained mainly

## C. E. MILLER



Suggested layout of Circuil No. 1 using a tag strip.
2G302's (p.n.p.), 2N1091's (n.p.n.), OC23's (p.n.p. output) and OA10 diodes. There were also some anonymous devices which looked, and behaved, like OC81's. The alternatives for the various transistors, etc., in the design are as follows:-

Trl. ACl28, OC81, 2 G302.
Tr2. ACl27, AC176, 2N1091.
Dl. AAll9, OA10, ACl 28 with base/collector strapped.
Tr 3 , as Trl.
Tr4, as $\operatorname{Tr} 2$.
Tr5, Tr6. AD149, OC23. (Etc.-any large output type).


Higher powered output stage of Circuit 2.
As a final construction point, the output transistors should be mounted on a piece of aluminium of some 30 sq. in. This may conveniently be shaped to act as a screen for the rest of the amplifier. The prototype was deliberately mounted in the worst possible place, in a confined space close to the vehicle heater, but no overheating has been observed.


Apart from the five items shown above, there are another 195 kits to choose from in the vast AMTRON range of electronic kits.

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 185 | ． 22 | 30 C 18 | ． 57 | ER91 | －12 | ES81 | －36 | PUIB2 | －30 | UAl3C80 | ． 81 |
| 1 T4 | ． 16 | 30 F 5 | ． 84 | ERC33 | ． 40 | EN84 | －32 | PCL83 | ． 55 | VAF゙42 | ． 50 |
| 394 | ． 26 | $30 \mathrm{FL1}$ | ． 65 | EBC41 | ． 40 | EM187 | .50 | PrCL4 | ． 33 | UBC41 | 48 |
| 3 V 4 | 47 | 30 FL 12 | －69 | E13C81 | ． 30 | EY51 | ．36 | PCL85 | ． 38 | UBF80 | ． 34 |
| 5 Cl 4 | ． 31 | 30F1．14 | － 68 | ERC90 | ． 22 | EY86 | －29 | PCL86 | ． 37 | UBF89 | .82 |
| 5V4G | ． 35 | 30 L 1 | －29 | Ebrbo | ． 32 | EY87 | ． 29 | PCL． 88 | ＋80 | UCC84 | ． 39 |
| bY3GT | －30 | 30L15 | $\cdot 70$ | FiBF83 | ． 38 | EZ40 | ． 38 | PCL800 | ． 88 | ucces | －35 |
| 57.40 | － 35 | 30 L 17 | $\cdot 70$ | E17F89 | ． 29 | EZ 41 | －38 | PCL805 | ． 38 | UCF80 | －30 |
| 6／30L2 | －54 | 30P4 | －54 | ISCC81 | 17 | E280 | ． 21 | PE．NA4 | 77 | UCH42 | ． 68 |
| 6 A316 | ． 13 | 30 Pl 12 | －69 | ECcs2 | ． 20 | EZ81 | －22 | PEN36C | 70 | UCH81 | ． 80 |
| 6AQ5 | －22 | 30 Pl 19 | － 54. | ECC83 | ． 38 | E290 | .25 | PFL200 | ． 81 | 1＇CL82 | ． 32 |
| 6at6 | ． 20 | 30 PL 1 | ． 56 | ECC85 | － 84 | GZ30 | －34 | PL3G | ． 48 | UCL83 | －65 |
| 6AU6 | －20 | 30PL13 | ． 89 | ECCs04 | ． 51 | G232 | 40 | PL81 | － 43 | UF41 | ． 62 |
| 6BA6 | ． 20 | 30 PLL 4 | ． 80 | ECFP80 | ． 30 | KT41 | .77 | PL81A | ． 47 | UF89 | ． 80 |
| $6 \mathrm{BE6}$ | ． 21 | 35L6GT | ． 45 | ECFP2 | ． 26 | KT61 | ． 55 | PL82 | ． 31 | CLA1 | － 58 |
| 6BJ6 | －11 | $35 W 4$ | ． 25 | ECH35 | ． 55 | кT66 | ． 78 | PL83 | ． 33 | ＇L84 | ． 80 |
| 6BW7 | ＋ 50 | 35Z4GT | ． 25 | ECII 4 | ． 59 | L． 319 | ． 56 | PL84 | ． 30 | UM84 | ． 29 |
| 6F14 | －35 | 50CD6G | ． 88 | ECH81 | ． 29 | LN329 | ． 80 | PLs00 | ． 63 | ［＇Y41 | ． 80 |
| 6 F 23 | －68 | 807 | ． 49 | EC1183 | ． 38 | LN339 | ． 65 | PL504 | －63 | U צ＇85 | －25 |
| 6 F 25 | ． 50 | AC／VP2 | －77 | ECH84 | ． 35 | N78 | 11．05 | 1 ${ }^{1984}$ | － 30 | $\checkmark \mathrm{P}_{4} \mathrm{~B}$ | ． 77 |
| \％JEGT | ． 20 | 1349 | －70 | ECL80 | ． 30 | P61 | 40 | PX25 | ． 85 | W77 | ． 48 |
| 6J7G | .24 | B729 | ． 54 | ECL82 | ． 29 | Pancso | － 31 | PY32 | －52 | 277 | ＋28 |
| 8K7a | －12 | CCH35 | ． 87 | ECL86 | ． 35 | P＇CR6 | ． 44 | ${ }^{1} \mathrm{Y} 33$ | ． 62 | Transinto |  |
| 6 K 8 G | ． 36 | Cr31 | ＋28 | EF39 | ． 38 | $\mathrm{P}^{\mathrm{C}} \mathrm{C} 88$ | 44 | PY81 | ． 25 | AC107 | 17 |
| 6Q76 | ． 35 | DAF91 | ＋22 | EF4l | ． 37 | PC96 | 42 | PY82 | ＋25 | ACl27 | ． 18 |
| 68L7aT | ． 32 | DaF96 | $\cdot 38$ | EF80 | ． 23 | PC97 | ． 38 | ${ }^{1} \mathbf{Y} 83$ | －26 | AD140 | ． 87 |
| 6SN70T | ． 32 | br91 | ． 16 | EF85 | ． 28 | PC900 | ． 29 | PY88 | ． 33 | AFILS | ． 20 |
| $6 \mathrm{V6G}$ | －28 | が96 | ． 36 | EF86 | .30 | PCC8 4 | ． 29 | F Y800 | .31 | AFl16 | ． 20 |
| 6 VGGT | ． 28 | 1 1177 | ． 20 | EF89 | ． 26 | PCC85 | ． 23 | PY801 | ． 81 | AFl17 | 20 |
| $6 \times 4$ | ． 23 | I）K32 | ． 33 | EF91 | ． 13 | PCC88 | ． 38 | R19 | ． 30 | AFI25 | ． 17 |
| 6X57T | ＋28 | DK91 | ． 28 | Er92 | ． 27 | PCC89 | ． 43 | R20 | ． 70 | AF127 | － 17 |
| 10 Pl 13 | － 53 | 1）K92 | ． 50 | EF98 | ． 65 | 1 CCl89 | ． 48 | U25 | ． 73 | OC26 | ． 25 |
| 12AT7 | －17 | DK96 | －45 | FF183 | ． 27 | 1＇CC80s | ． 70 | －96 | ． 65 | OC44 | ． 12 |
| l2AU7 | .20 | DL35 | －40 | EF184 | ． 28 | PCF80 | ． 26 | L． 47 | .73 | OC45 | ． 12 |
| 12AX7 | ． 22 | DL93 | ． 28 | E1190 | ． 38 | PCF82 | ． 33 | U49 | ＋70 | $0 \mathrm{C7} 1$ | ． 18 |
| 198（76g | ＋75 | DL94 | .47 | EL33 | ． 55 | PCr86 | ． 46 | U52 | .31 | OC72 | $1{ }^{1}$ |
| 20 F 2 | ． 87 | D296 | ． 38 | EL．34 | ． 48 | PCF800 | 58 | U78 | ． 24 | 0 0c7s | －18 |
| 20 P 3 | ． 75 | DY 86 | ． 24 | EL41 | －51 | PCF＇801 | 28 | U191 | ． 55 | OC81 | ． 18 |
| 25L6GT | ． 19 |  |  | ELS4 | $+23$ | PCF802 | ． 38 | U193 | ． 31 | 0C817 | －18 |
| 25 U4GT | ． 57 | D ${ }^{\text {D }}$ | ． 24 | EL90 | ． 26 | PCF802 | 38 | U251 | ． 61 | OC82 | ． 12 |
| 30 Cl | ． 26 | DY802 | $\cdot 33$ | EL95 | ． 33 | PCF805． | ＋57 | U301 | －38 | OC82D | 12 |
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# practically wireless commentary by IIENKI 

WHERE wireless engineers foregather, talk inevitably veers toward: 'I remember...'
It is either a model with such idiosyncracies that a catalogue of 'common faults' would have called for an appendix to the service manual, a manufacturer whose crass perfidy extended to an invoice before the goods arrived -or worse, so long afterwards that one had to guess at the cost of the spares before one dared complete the repair-or a customer.
But my subject today is not so much the trials and tribulations of the working engineer as this 'harking back' tendency we all evince, once we converse with fellows of like mind. Go to a meeting of the RSGB, the SERT, the BARTG or even your local Gramophone Society and before the last strains of the demonstration or mutters of the lecture have died away, everybody is avidly recounting his or her personal experiences.

. . . a donkey-driven gramophone.
Watching two members of the Royal Television Society taking coffee last week reminded me of Ralph Richardson and John Gielgud in the Royal Court Theatre production of Home. Parallel tracks of reminiscence, meeting rarely at some way-station. From the few words I caught in that BBC Hospitality Room, member A was waffling on about videotape while the other had some bee in
his bonnet about phase-lock loop and pulse-code-modulation.
Henry was dying to know how Mr. B allied the two subjects, but couldn't find out because the charming production assistant he was trying to chat up with his memories of Marconi would insist on relating her opinions of Arthur Negus every time I had to pause for breath.

All this is brought on by hearing about the Fetron.

The Fetron is a genuine solid state substitute, mounted in a case like a valve, with pin formation and characteristics of the valve it is meant to replace.

You can read the ins and outs of it in the "Special Product Report" elsewhere in this issue, if it grips your curiosity like it did mine. Suffice it to say on this page that all those "everlasting" relay stations, built around valves designed to run forever, could not die without putting up a fight first.

Use of the Fetron saves major circuit modification when a valvechange is needed. Ain't science wunnerful?

Trouble is, Henry took a look at the types available and found there listed the dear old 12AT7. Now the TS12AT7 sounds a good idea until you remember some of those old 'universal' radiograms, and one or two series-heatered television sets that used them.

What happens if you plug in a Fetron? Have they made a resistive heater 'bridge', or do we have to solder a resistor across the socket? And, if we do, shouldn't there be a thermistor provided? Should we not also protect the h.t. line because the Fetron is operative immediately?

So many questions... reminds Henry of that unfortunate chap in an electronics magazine who offered a simpler way of getting over some stabiliser problems. Only snag was, somebody had to remember to turn the control back to zero after use unless the
next chap along blew the thing up-you know, the way your loudspeaker creases when you have left the amplifier gain up high and a 'friend' flicks your stylus!

Well, the upshot of this poor chap's sensible economy was that

. . . and the inevitable happened.
electronic geniuses wrote in, both calling him gormless and detailing complicated protection circuits that would automatically switch off, from any given function. I wonder if Mrs. Mary W. would like one built into every TV?

I remember one TV we could never switch 'Off' because the maker had fitted too-substantial suppressors across the contacts.

We all tend to hark back. You should see the glee with which Colin Riches unearths a donkeydriven gramophone. At the wedding of a friend's daughter, hardly out of her teens, one of the speakers, Marketing Director of a worldwide Telecommunications company, had to remind the reception that his first acquaintance with the charming Sally was when she sat in his lap-at eighteen months-and the inevitable happened.

He might, at least, have reminded them of the days when he was hawking cheap radios round the council estates. It is just as funny a story. Remind me to tell it to you, one day . . .

# Special Valves <br> <br> PART 1 COMMUNICATION TYPES <br> <br> PART 1 COMMUNICATION TYPES <br> M.K.TITMAN B. Sc(Eng), C. Eng , MIEE. 

THERMIONIC devices still have a wide range of applications in modern electronic circuits and, despite the semiconductor takeover, they remain essential components in a variety of applications from high power r.f. amplifiers to electro-optical transducers.

The requirement for valves for u.h.f. and s.h.f. has led to the development of special techniques. The following valves were all developed from the necessity to exploit new ways to enable communication systems to use the wide bandwidths available at u.h.f. and microwave frequencies. The principles used are mathematically complex but their operation can be readily understood.

## DISC SEAL VALVES

The form of construction used for both triode and tetrode configurations is illustrated in Fig. 1. The structure consists of a thimble-like cathode, spaced from a parallel wire grid further separated from a disc anode. The structures are very rigidly held by the ceramic space discs and because of the annular configuration co-axial input and output terminations can be used. The advantage of this system is that high power operation with reasonable efficiency in the GHz region is possible.
Disc seal triodes are used for amplifier and oscillator applications from 0.5 GHz to 4 GHz frequencies, at power levels of 1 W to 600 W . Typical values of $\mathrm{gm}_{\mathrm{m}}$ are $6 \mathrm{~mA} / \mathrm{V}$ to $25 \mathrm{~mA} / \mathrm{V}$. At lower power levels
$(<25 \mathrm{~W})$ the envelope is designed for convection cooling but forced air cooling is used for the higher power levels. Examples of this valve type are the ES157 at 2W, and TDO4-20 at 12W.

## KLYSTRONS

Klystrons are also essentially microwave valves which operate as oscillators in the frequency range from u.h.f. to more than 100 GHz . Generally they are available for discrete commercial frequencies such as $6,7,8$ or 9 GHz and mechanical tuning by micrometer adjustment is possible.
The klystron consists of a cavity (or for power devices, multiple cavities) through which a stream of electrons is beamed from a normal electron gun assembly, as shown in Fig. 2. The electrons are velocity modulated by a field produced by a toroidal modulating structure known as a rhumbatron. The electrons therefore become bunched in regions of high electron density and rarified in low density regions, as they travel through a further section known as the drift space. Consequently if critical frequencies are utilised the bunching allows resonant oscillation to occur in a mode controlled by the rhumbatron.

Power levels for high frequencies are in the region of 1 kW with special u.h.f. power devices operating at 460 to 1000 MHz at levels of 20 kW . The electronic tuning range for such devices is from 30 to 100 MHz ,


Fig. 1: at left, shows the general configuration of a disc seal valve. The picture shows a collection of oscillator klystrons, the centre one being used in communications relay equipment. The others are used In radar local oscillators.

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| :--- | :--- |
| $\mathrm{ACCY71}$ |  |
| $\mathrm{AC127}$ | 25 BCY |
| BC 28 |  | $\begin{array}{ll}\text { AC127 } & \text { 25p } \\ \text { AC 128 } & 24 \text { BC Y } \\ \text { AC 124 }\end{array}$ AC128

AC 128/A Cl AC151
AC152 AC 153
AC 176 AC 153/176K AC187K AC 188/188K
 27p BF 180 ACY18
ACYl 19 ABY 20
ABY 21 ACY22 AO140

 | AD162 | 49p/BFX29 |
| :--- | :--- |
| AO161 | 55 BF 84 | AO161/162 £

AF106 $\begin{array}{ll}\text { AF114 } & \text { 32p BF BF X87 } \\ \text { AF 115 } & \mathbf{2 5 p} \text { BF } 88\end{array}$ $\begin{array}{ll}\text { AF115 } & \text { 25D BF X88 } \\ \text { AF 116 }\end{array}$ AF116

| AF117 | 2 |
| :--- | :--- |
| AF118 | 44 |
| AF124 | 25 |
| AF125 | 24 |

 AF125
AF126
AF139 A.F139

 ASY26
ASY27
ASY28 ASY29 $\begin{array}{lc}\text { AA } & \text { 15p/BY100 } \\ \text { BAX 16 } & 8 \text { D/ BY } 127\end{array}$ BB103
BB104 BB104
BB105
BC107 BC107/BC177 BC108
BC 108/BC178 BC 109
$\mathrm{BC} 109 / \mathrm{BC} 17$

BC109C
BC140
BC140
BC 147
BC147
BC148
BC148
BC149
BC157
BC158
BC159
8
BC147/157
BC148/158 BC149/159
BC 167
BC 168
BC 168
BC 169
BC169
BC169C
$\mathrm{BC169C}$
BC 177
BC 177
BC 178
BC 179
BC178
BC179
BC182
BC182L
$\mathrm{BC182L}$
BC 183
BC 183 L
BC 184
BC184
BC184L
BC 212
BC 212
BC 212 L
BC 238
BC 238
$\mathrm{BC} 238 / 308$
BC 257
$\begin{array}{lr}\mathrm{BC} 238 / 308 & 20 \\ \mathrm{BC} 257 & 90 \\ \mathrm{BC} 258 & 8 \mathrm{p} \\ \mathrm{BC} 259 & 90\end{array}$
$\begin{array}{lr}\mathrm{BC} 258 & 8 \mathrm{p} \\ \mathrm{BC} 259 & \text { ep } \\ \text { BC 307 } & 12 \mathrm{p} \\ \text { BC 308 } & 10 \mathrm{p} \\ \text { BCY30 } & 25 \mathrm{p}\end{array}$
$\begin{array}{ll}\text { BCY30 } & 25 \\ \text { BY } 31 & 4 \\ \text { BEY } 32 & 5 \\ \text { BY } 33 & 20\end{array}$
BCY33
BCY34
BC

| BCY38 | 30 p |
| :--- | :--- |

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Fig. 2: Internal arrangement of a klystron valve.
whilst the mechanical range is considerably more. Typical device types are the KS6, 7, 9 family and YK1010 to 1090 . Most of these utilise waveguide outputs but some have coaxial probes. The higher power devices require forced air cooling, whilst the u.h.f. power units need a cooling water supply.

## TRAVELLING WAVE TUBES

These are microwave power amplifier valves used extensively in communication systems particularly for microwave links. The basic construction is shown in Fig. 3 and consists of an electron gun assembly, a modulating helix structure and a collector electrode. The electron gun forms a narrow electron beam focused by means of the grid and anode. The beam passes along the axis of an accurately formed helix structure and is continually focussed by a magnet system. The modulating microwave frequency is passed along the helix and travels at approximately the same speed as electrons in the beam. Thus the r.f. field produces an electric field which velocity modulates the electron beam as it travels along the helix axis. After modulation the electron beam bombards the collector electrode which is often water cooled.

For low power valves the helix is of wire but for power devices a ring bar structure is used. As the helix is in a long glass envelope, heat dissipation is by radiation and thus the power is limited, especially since the mechanical helix structure must be very accurate. For very high power devices a ring-bar helix system is used and is a development of the


Fig. 3 : Diagram to Illustrate the construction of a travelling wave tube.
cross-wound opposite band helix system. Where very high power is necessary the ring bar structure is supported by annular beryllium insulators of high thermal conductivity.

Travelling wave tubes are very efficient microwave amplifiers which produce amplitude modulated output signals. The frequency range is determined by the mechanical structure and the helix in particular and, for the simple helix, it is roughly an octave about the centre frequencies from 1 to 9 GHz .

Power levels for continuous operation are usually 1 to 10 W but kilowatts are possible while operation in pulsed modes can result in peak power levels in the megawatt region. The band-width at high power levels is usually reduced to as low at $10 \%$ or 400 MHz at 4 GHz .

Both forward and backward wound helices are used and typical gains in the X band are in the region of 30 to 40 dB , with noise factors of 20 to 28 dB . Generally they are designed to fit into special mountings which incorporate the permanent magnet systems. The input and output are usually taken directly from waveguide connections, with the forward wave tubes operating as amplifiers and the backward wave tubes as oscillators. Typical forward wave types are LB4-20 and 30 , at 4 GHz and LB6-15 to 25 at 6 GHz , with backward wave oscillators like the YH1100 and BA16.

## MAGNETRONS

These are essentially high efficiency oscillator valves and are used for producing fixed frequency, fixed amplitude oscillations and, in a pulsed mode, are widely used in radar equipment. The normal frequency is in the $X$ band ( $5 \cdot 2$ to $10 \cdot 9 \mathrm{GHz}$ ) although other bands are covered.

The magnetron, as illustrated in Fig. 4, consists of one or more very carefully machined cylindrical cavities with a cathode adjacent to the cylinder and formed of a thin wire. A permanent magnet provides



In this collection of magnetrons the large one is an L-band 2.3MW tunable pulse magnetron intended for high power survelllance radar. In the foreground is a 25 kW CW model for Industrialuse. The remalning two magnetrons are rated at 50 kW and 900 kW pulse operation in the $S$-band.
a magnetic flux at right angles to the cylinder and thus at right angles to the electric field formed by the diode. Electrons released from the cathode travel in a circular path and at a given frequency just graze the anode. The oscillation frequency is determined by the physical characteristic of the cylinder and therefore is often fixed. Slight tuning is however provided with some magnetrons.

Continuous-wave magnetrons are available in the frequency range 8 to $9 \cdot 5 \mathrm{GHz}$ at power levels of 6 W to 20 W . Typical operating conditions are $V a=1 \mathrm{kV}$, $\mathrm{Ia}=50 \mathrm{~mA}, \mathrm{Vh}=6 \cdot 3$ and Ih starting at 1 A . Typical types are JPT 9-01 and JPG 8-01.

Pulsed magnetrons are designed for short pulse durations in the region 1 to $5 \mu s$ for X band devices at approximately 9 GHz . Power outputs range from 25 W to 50 kW with devices such as JPT9-02 and YJ1050. The lower frequency $1 \cdot 25 \mathrm{GHz}$ (L Band) and $5 \cdot 5 \mathrm{GHz}$ (C Band) devices operate at higher power levels up to $1,000 \mathrm{~kW}$.


Fig. 4: General arrangement of a multipie cavily magnetron.

## FUTURE TRENDS

Although trends continue towards the use of semiconductor devices, the power transmitter valve at all frequencies cannot yet be replaced directly. Thus power valves at all frequencies are still of very considerable use and development continues to improve all these designs.

A trend which undoubtedly will continue is the replacement of high power microwave transmitters by low power solid state components such as varactor chains. This has been made possible by improved receiver and aerial design.

We are indebted to the English Electric Valve Co. of Chelmsford for permission to reproduce the photographs in this article.

## TO BE CONTINUED

## televelili

## MAY ISSUE

## THE LID OFF VARICAPS

What exactly is a varicap tuner, how does it work and what goes wrong with it? This month Keith Cummins looks at all aspects of varicap tuners and sums up the pros and cons. Including an insight into the tricky servicing problems that can arise with their use.

## TRANSISTOR IF PREAMPLIFIER

It is often worthwhile converting dualstandard sets to single-standard operation and fitting a modern transistor u.h.f. tuner. When this is done it is convenient to remove the v.h.f. tuner, but this usually means the need for extra gain between the u.h.f. tuner and the i.f. strip. A simple transistor l.f. preamplifier that has been used in converting sets such as the BRC 850 chassis is featured this month.

## ASSESSING COLOUR RECEIVER PERFORMANCE

In the concluding article in his series E. J. Hoare provides a detailed account of how to assess the colour performance of receiverspurity and convergence etc. and the operation of the colour circuits.

## SERVICE NOTEBOOK

Amongst the items in George Wilding's Service Notebook this month is a detailed procedure for tackling that common condition, lack of e.h.t.
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## device of the month ZN414



The Ferranti ZN414 is a complete a.m. radio circuit which operates from 1.1 to 1.8 volts and requires only battery, earphones and antenna plus a tuning capacitor and two decoupling capacitors. The ZN414 features: medium and long waveband, good stability on assembly, no setting up of IF coils, plus much more.
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| EF91 | 5p | PL83 | 10p | 20PI | 15p |
| EY86 | 22p | PL36 | 17p | 20P3 | 12 p |
| EFI83 | 20p | PY81 | 10p | 30F5 | 12p |
| EFI84 | 20p | PY801 | 17p | 30 FLI | 20p |
|  |  | PY800 | 17p |  | 20p |

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## SGS NE555 Precision Timer

Ahighly stable timing device, type NE555, recently released by SGS, is the topic for this month's article. It allows precision timing from microseconds to hours with a mere handful of components; its uses however are not limited solely to the timing field as it can also find wide application in such diverse spheres as pulse generation, frequency division, pulse-width modulation, etc., to mention but a few. Such versatility coupled with low cost should make it an attractive i.c. to the amateur experimenter and a few of its more interesting features and applications will be outlined in the following notes.

## Applications

A block diagram of the NE555 is shown in Fig. 1 and the first application to be considered is its use as an accurate timer, Fig. 2. The timing period is set by one additional resistor capacitor network with additional terminals allowing control over the triggering and resetting of the device. The external


Fig. 1 : Biock diagram of the NE555 timing device.
capacitor connected between pin 7 and earth is initially held discharged by the short circuit path of the saturated transistor Trl. When a negative trigger
pulse is applied to pin 2 the flip-flop changes state and biases off Trl thereby allowing Cl to charge via R1. The time constant associated with R1Cl determines the rate at which Cl charges and when its voltage reaches ${ }_{3}{ }_{3} V_{\text {i. }}$ the threshold comparator


Fig. 2: Typical application of the NE555. The values of R1 and C1 for a delay of 1 second would be $i M \Omega$ and $1 \mu F$.
resets the flip-flop and discharges Cl in addition to providing an output pulse at pin 3. One of the great advantages of this type of circuit is that the timing rate, for all practical purposes, is independent of the supply voltage. Timing periods from as short as 1 microsecond to as long as 1 hour may be obtained with this rather simple arrangement.

## Multivibrator

Another interesting application of the NE555 is obtained when pins 2 and 6 are joined together as illustrated in Fig. 3. Here the device is operated as


Flg. 3 : In this circuit the NE555 is used as a free-running multivibrator.
a free-running multivibrator with the frequency and duty-cycle set by the R3-R4-C2 arrangement. The combined value of R3 and R4 in conjunction with C2 determines the frequency while the duty cycle is set by the ratio R3/R4. As the transistors fabricated in the silicon chip are of the highest quality excellent square waves are obtained from the output at pin 3. Once again, in this arrangement the operating frequency is independent of the power supply voltage.

## Pulse-width modulator

The final application of the NE555 to be considered is its use as a pulse-width modulator. Here an external square wave generator's output is connected to pin 2 with the modulating signal applied to pin 5 as indicated in Fig. 4. (Incidentally, another NE555 operated in the astable mode will function quite well


Flg. 4: Yet another applicatlon is as a pulse-width modulator.
as the clock generator.) As the control voltage on pin 5 increases, it affects the threshold voltage of the comparator resulting in an increase of the pulse width. The exact opposite occurs as the modulating voltage decreases so the output train of pulses obtained at pin 3 has a frequency identical to the clock input frequency with the pulse width controlled by the modulating signal.

A few of the more interesting applications of the NE555 i.c. have been reviewed in this article and further uses of the device are left to the ingenuity of the experimenter. The NE555 is available from Quarndon Electronics Ltd., Slack Lane, Derby.


## Improving VHF Radio April PW

Although our information was taken from a normally reliable valve and transistor manual the connections for the BF200 transistor in Fig. 6 were incorrect. They should read, clockwise from the tag: emitter, base, collector and shield.


Aend-connected wire of random length is often used as a short wave aerial and this can, in fact, give good results if reasonably high and clear of earthed objects. At some frequencies, when the aerial length is a half wave or multiple of a half wave, the end impedance at the receiver can be very high, over 1000 ohms. At the other frequencies (a quarter wave or odd number of quarter waves) the impedance is low, probably under 50 ohms. Therefore, for an efficient transfer of energy from the aerial to the receiver at all fre.


Flg. 1: above, shows the circuit of the receiver matching unit. When switched to "Out" the two variable capac/tors should be turned to minimum capacity.
quencies, some matching device is needed. The one described here covers about $3 \cdot 5 \mathrm{MHz}$ to 30 MHz , and it is over this range that such an accessory is most likely to prove useful.

## THE PI NETWORK

In the circuit, Fig. 1, the tapped inductor L1 has a variable input capacitor VCl and variable output capacitor VC2. A 12 position rotary switch S1 allows turns to be selected as follows- $0,2,5,9,14,21,30$, and 41, the last four positions remaining unused. This switch and adjustment of VC1 and VC2 allows a wide range of aerials to be matched to the receiver.

Many communications receivers have a nominal aerial input impedance of about 75 ohms while others, and especially some popular older models, are 600 ohms. On some frequencies the aerial may chance to match the receiver. The Receiver Matching Unit will then give no improvement in signal strength, but can be left in circuit by setting VCl

and VC2 at minimum and the switch at "O".
At other frequencies the switch is progressively rotated to bring more turns into circuit, each time adjusting VC1 and VC2 for best results. This is merely a matter of peaking the matching unit controls for best volume, or best S -meter reading. Where the mis-match is bad, quite a significant improvement should be had. If peaking the signal by ear, switch off the receiver a.g.c. or choose a weak signal or adjust for maximum general noise picked up by the aerial.
capacitors. Solid dielectric components are not recommended. A value of 350 pF or so is useful for the lower frequencies, but for the h.f. bands only 200 pF or even 150 pF capacitors may be suitable, if to hand.


Fig. 2: Wiring diagram of the matching unit. Unused positions on the switch have been ignored.

Fig. 2 shows construction, the coil being supported by its leads. The plastic case used was $6 \times 4 \times 4 \mathrm{in}$. but had no removable back, so flying leads were left just long enough to reach Aerial, Receiver, and Earth terminals fitted at the rear. Communication receivers often have a 75 ohm co-axial aerial input socket when a co-axial socket can be fitted to the

The photograph, right, shows the author's protolype unit. The multiple leadouts from the coll are sufficlent to hold it firmly on the switch.


The coil is wound with 22 s.w.g. enamelled wire on a paxolin tube lin. in diameter and about 2 in . long. Anchor the wire through small holes near one end. Wind 2 turns side by side, and twist a small loop. Leave a space of about 1 rin. and wind 3 turns, making a further loop. Continue in this way, adding $4,5,7,9$ and 11 turns, with a small space between each section. Scrape all the loops and solder on leads for the switch.

Solder the leads to the switch so that the first position shorts the whole coil, subsequent positions leaving 2 turns, 5 turns, 9 turns, and so on, in circuit, position 8 having no connection so that the whole coil is in use.

VCl and VC2 are each 365 pF miniature air-spaced
back of the matching unit. The inner conductor of the co-axial lead to the receiver will be the aerial lead, and the outer braiding will act as the earth connection no earth being needed on the unit.

The switch has a scale showing the number of turns in circuit. The lowest frequency reached depends on the aerial and receiver, but can extend down to 1.5 MHz in some cases. On some ranges, the unit is useful in reducing second channel interference. If a numbered dial is fitted to each capacitor a very useful chart can be made up showing dial readings and switch positions for the various amateur and short wave broadcast bands, which will considerably shorten the time taken to tune the unit to any particular frequency.

## INNEXTMONTH'S <br> PRAGTIGAL wisiluss

## 

Listen to your stereo records and radio programmes in the comfort of your armchair, perhaps several feet away from the amplifier. Settle down and enjoy the music in the "jdeal stereo" position. You don't have to get up to adjust volume or balance controls because you have this small unit on your lap to do it remotely, with balance meter and socket for private listening on stereo phones. Easy construction details given next month.



This oscillator produces a pleasing tone, different in frequency for either of two doors. By using a suitable centre-tapped transformer T1, the collector circuit of each transistor can drive the base of the other transistor.

Assembly is on a perforated srbp board and wired as in Fig. 2. This board is fitted in the speaker cabinet or to a flat speaker panel fitted across the corner of the room.

One push-button switch is wired to $A$, and the other to $B$. The return leads of both switches go the common terminal C. When one switch is operated both R1 and R2 are in circuit, while with the second push R2 only is present. Wires A-C can run to the front door, and B-C to the back door.

The note can be altered by changing the resistance of R1 or R2 or the capacitance of C1, C2 or C3.

Connections for OC81, NKT271: collector wire nearest spot, then base, emifter.

## components

> R1 resistor $1.2 \mathrm{k} \Omega \pm 10 \% \pm W$
> R2 resistor $220 \Omega \pm 10 \% \mathrm{tw}$
> R3 resistor $47 \mathrm{k} \Omega \pm 10 \%$ tw
> R4 resistor $47 \mathrm{k} \Omega \pm 10 \%$ tw
> C1 capacitor $0.047 \mu \mathrm{~F}$ polyester
> C2 capacitor $0.047 \mu \mathrm{~F}$ polyester
> C3 capacitor $0.047 \mu \mathrm{~F}$ polyester
> Tr1 transistor OC81 or NKT271
> Tr2 transistor OC81 or NKT271
> T1 transformer 9-2:1 CT primary, type T/T7 Repanco
> Loudspeaker $3 \Omega 5 \mathrm{in}$. and wooden board 12in. $\times$ gin.
> Battery 9V type PP6 or PP9 with connectors Perforated srbp component board Nuts and bolts 6BA, soldering tags, pvc wire


Fig. 1 : Circuit diagram


Fig. 2: Component



Ready-made amplifier module used to give press-button calling and communication in both directions. Fig. 1 is the complete circuit.


S1 is the "push-to-call and push-tospeak" switch. When it is pressed, the circuit is completed in such a way as to cause an audio tone (R1 limits current in this condition). $\$ 2$ switches the unit on so that the master position may speak to the remote position, or vice versa. S3 at the remote unit causes a tone at the master unit, to gain attention.
At the master unit, press S 1 a few times to gain attention, then close S2, with S1 released to listen. Press S 1 again to speak. Switch off with S 2 when contact is finished. At the remote unit, press S3 a few times to call master unit and await reply. VR1 is set to a suitable volume level, and is ready wired to the 4-300 unit.

## componenfs

Fig. 2: Wiring of modulein the master unit on the left and partly cutaway view of remote unit

R1
resistor $150 \Omega \pm 10 \%$ t watt
VR1 potentiometer supplied with amplifier module
C1 capacitor $50 \mu \mathrm{~F} 12 \mathrm{~V}$ electrolytic
T1 transformer 9•2:1 CT primary, type T/T7 Repanco
S1 2-pole, changeover spring loaded push button, type S746 with S768 operator, or type S415 Bulgin
S2 single-pole, on-off toggle switch single-pole, on-off push button Loudspeakers $3 \Omega$ 2 $\frac{1}{2}$ in. or $3 \frac{1}{\frac{1}{2} \text { in. }}$ Battery 9V type PP6 or PP9 and connectors Amplifier module type 4-300
Component board srbp $3 \frac{1}{2} \mathrm{in} . \times 2 \frac{1}{2} \mathrm{in}$.
Case $8 \mathrm{in} . \times 6 \mathrm{in} . \times 6 \mathrm{in}$. (Master unit)
Case 4in. $\times 4 \mathrm{in} . \times 4 \mathrm{in}$. (Remote unit)
PVC connecting wire and knob
Nuts and bolts 6BA and 4BA
Soldering tags 6BA


Fig. 1: Circuit diagram showing the master unit above and the remote unit on the left

Remote unit
Numbers 1 to 4 in Fig. 1 refer to connection points 1 to 4 in Fig. 2. Fig. 2 shows the master unit. Two 6BA bolts secure the 4-300 amplifier and also the srbp board for T1 and R1. Solder coloured leads to S1 as indicated before fitting this item. Input and output circuits and T1 are continued on page three

A sensor, on the end of twin flexible lead, can be placed in a water tank, swimming pool, bath or wash-boiler. A buzzer sounds when the water level reaches the sensor.

The minimum battery current drain is about 0.3 mA ; rises to about 400 mA when water reaches the sensor.

Fig. 1 shows the circuit. The presence of water shorts the sensor probe and allows base current to flow through R1, resulting in a collector current of about $40-50 \mathrm{~mA}$ to close the relay. The buzzer sounds until the sensor is removed from the water, or the device is switched off.

Fig. 2 shows all wiring, in a case made from aluminium. The tag strip (shown detached) is mounted vertically in the adjacent corner of the case. Space is left for a flat 3-cell 4.5 volt battery.

## components

$$
\begin{array}{ll}
\text { R1 } & \text { resistor } 10 \mathrm{k} \Omega \pm 10 \% \text { 立 watt } \\
\text { Tr1 } & \text { transistor } 0 \mathrm{C} 76 \text { or any high gain pnp type } \\
\text { S1 } & \text { single-pole, on-off switch } \\
\text { RLA } \\
\text { relay } 100 \Omega \text { coil, single-pole on-off contacts, } \\
3-6 \mathrm{~V} \text { operation } \\
& \text { Battery } 4 \frac{1}{2} \text { to } 6 \mathrm{~V} \text { depending on relay obtained } \\
& \text { Buzzer } 4 \frac{1}{2} \text { to } 6 \mathrm{~V} \\
& \text { Sensor probe (see text) } \\
& \text { Case } 6 \text { in. } \times 4 \text { in. } \times 2 \text { in. aluminium box or } \\
\text { chassis with lid. }
\end{array}
$$

Fig. 1 (right) : Circuit diagram
Fig. 2 (below): Component layout and wiring


## INTERCOM AMPLIFIER

## continued from page two

positioned to avoid feedback which would cause instability. In addition to VR1, the 4-300 has a preset sensitivity control, which can be left at about the middle of its travel.

Easy connecting of a remote unit lead can be by a jack plug and socket, the outer conductor being the common positive return. Do not connect or disconnect while battery is switched on.

The equipment will operate as a baby alarm by placing the remote unit near the cot and closing S2.

Connections to the 4-300 amplifier module are shown in Fig. 2, indicating appropriate copper pads used for connections. MC indicates connection made to the metal case by soldering tags. 51 does not necessarily need to resemble that shown in Fig. 2 but can be any style with the operation as in components list.


The sensor is made in coaxial form to avoid any accidental short (and wrong indication) by metal items. It has an outer metal tube about 2in. long by ?in. diameter, with a slightly shorter internal pin (actually a length of 4BA threaded rod). The inside part is fixed by a tight binding of insulating tape, or by an insulated sleeve. The sleeve and pin must not touch. Several feet of thin twin flex are soldered on, the sensor inner part going to R1.
An alternative probe can be a coaxial plug as used for TV aerial wire, although it must be kept free from cor-


This portable medium wave tuner gives an output for a tape recorder or amplifier.

Note that the AA119 diode has a black mark to denote plus polarity; wrong polarity here will upset avc action. Components are positioned as in Fig. 2 and wired as shown in
grey. The perforated srbp board is bolted to the metal bracket carrying VR1, VC1/2 and S1. MC is the metal case connection.

A bracket, srbp strip, and strip of card wrapped round the rod and drawn tight with a


Fig. 2: Layout of components and underside wiring


Resistors

| R1 | $18 \mathrm{k} \Omega$ | R 7 | $330 \mathrm{k} \Omega$ |
| :--- | :--- | :---: | :--- |
| R2 | $15 \mathrm{k} \Omega$ | R8 | $390 \Omega$ |
| R3 | $2 \cdot 7 \mathrm{k} \Omega$ | R9 | $27 \mathrm{k} \Omega$ |
| R4 | $1 \mathrm{k} \Omega$ | R10 | $1.5 \mathrm{k} \Omega$ |
| R5 | $47 \mathrm{k} \Omega$ | R11 | $3.9 \mathrm{k} \Omega$ |
| R6 | 120 kS 2 |  |  |
| All resistors $\pm$ | $10 \%$ | watt |  |

Potentiometer Diode
VR1 10kS log. D1 AA119 or OA91

## Capacitors

C1 $0.01 \mu \mathrm{~F}$ mica or ceramic
C2 $0.02 \mu \mathrm{~F}$ mica or ceramic
C3 $180 \mu \mathrm{~F}$ mica or ceramic
C4 $2 \mu \mathrm{~F}$ electrolytic
C5 $0.01 \mu \mathrm{~F}$ mica or ceramic
C6 $0.1 \mu \mathrm{~F}$ polyester
C7 $200 \mu \mathrm{~F} 9 \mathrm{~V}$ electrolytic
C8 $0.01 \mu \mathrm{~F}$ polyester
C9 $0.5 \mu \mathrm{~F}$ polyester
(Note: C9 not required if used only with IC-12 audio amplifier)

Variable Capacitors
VC1 \& VC2 208+ 176pF with trim. mers type 00 Jackson (slow motion optional)

Preset Trimmers
TC1, TC2 fitted to VC1, 2

## Transistors

Tr1 BF194 Tr2 BF195 Tr3 BF195

## Coils

L1, L2 Medium wave ferrite rod aerial coil type MW/FR5 Denco
L3 Oscillator coil type TOC1 Denco

## Transformers

T1 I.F. transformer type IFT13 Denco
T2 I.F. transformer type IFT13 Denco
T3 I.F. transformer type IFT14 Denco

## Switch

S1 Single-pole, on-off toggle switch

## Miscellaneous

Perforated srbp, $0.15 i n$. matrix 4
Control panel and bracket $4 \underset{\text { in }}{ } \mathrm{in}$. $\times 2 \mathrm{in}$. aluminium
Nuts and bolts 6BA, pve wire
Case, insulated, of wood or plastic

This radio alarm is designed to awaken you at a preset time set on the clock movement, and to switch off automatically if required.

Use the "Tape Tuner" (page four of this supplement) with an integrated circuit audio amplifier. The synchronous clock runs from 250 V a.c. mains and is supplied with contacts which are set by a front mounted control. A second control sets the duration, then automatically switching off. (A minute timer ringer is also provided, but is not used in this circuit.)

The master or programming switch, which is arranged as in Fig. 1 and shown in two views in Fig. 2, allows the radio to be switched on irrespective of the clock settings, or switched off separately, giving complete freedom of operation without any need to change clock settings.


## components

Tape tuner as described on page four of Supplement Amplifier i.c. type "Super IC12" with heat sink (Sinclair)
Electric programmer clock as illustrated with switch contacts glass and bezel (various advertisers) Loudspeaker $8 \Omega$ to match IC12
Switch single pole, 3-way to select operation Connection block, 3 -way for mains connection Fabric or expanded aluminium speaker grille Case approx. $10 \mathrm{in} \times 7 \mathrm{in} . \times 4 \frac{1}{2} \mathrm{in}$.

A mains connector joins mains leads and clock leads.

The i.c. amplifier is mounted on brackets. The whole unit is powered by a PP9 9V battery. A mains unit could be fitted instead and several proprietary brands can be purchased or the reader can make his own. All units can be mounted in a suitable wooden case.
uitable wooden case.

## TAPE TUNER

continued from page four nut and bolt hold the ferrite rod aerial.

The i.f. transformers T1, T2, T3 are pre-aligned but the effect of slight core adjustment can be tried. Adjust TC1 and TC2 at the high frequency (200 metres) end of the band, and the core of L3 (if necesary). The position of L1/L2 on the ferrite rod is adjusted at the low frequency end of the band.

Note that the specified case is insulated material, not metal to avoid screening the ferrite rod aerial. Audio output should be heard on high impedance phones connected to the output jack socket. The output is of high impedance and should be fed into the high impedance input of a tape recorder via screened cable (but see also the Radio Alarm Clock).
Transistor connections as indicated by top view in Fig. 2.

$$
\square
$$



Fig. 1 (left): Circuit diagram
Fig. 2 (below): Component layout and wiring (the programme switch is shown twice for wiring detail)



This lamp dimmer is constructed in an electrical switch box. The 40432 triac is rated at 0.5 A without a heat sink, or 1 A with the type 5 F clip-on heat sink shown. With 240 V a.c. mains, this is suitable for lamp loads of 120 watts and 240 watts respectively. An alternative triac type 40430 can also be used.
The dimmer can be fitted in place of an ordinary lamp switch. With the portable unit shown, the dimmer box and a 13A type outlet are assembled in a larger box. A table or standard lamp can be plugged into it, or it can be used for heat control of a soldering iron. This unit is not rated for power drills and is not suitable for them nor for fluorescent lamps.
Fig. 1 is the circuit, with wiring to integral 13A type outlet. The metal box, Fig. 2, provides screening. Complete closure by a metal plate was not found necessary. The triac case is connected, via a soldering tag bolted to the heat sink or case, to VR1. It must be insulated from the box and any other metal part. Flexible leads to VR1 and S1 allow these to be positioned in the front holes.
Assure proper earthing is maintained right up to any appliance controlled by the unit. The mains plug is fitted with a 3A fuse.
Triac connections shown in diagram.



## components

R1 resistor $10 \mathrm{k} \Omega \pm 10 \% \frac{1}{2}$ watt
R2 resistor $10 \mathrm{k} \Omega \pm 10 \% \frac{1}{2}$ watt
R3 resistor $22 \Omega \pm 10 \%$ 古 watt
VR1 potentiometer $250 \mathrm{k} \Omega$ linear
C1 capacitor $0.1 \mu \mathrm{~F} 1,000 \mathrm{~V}$ d.c. or 300 V a.c.
C 2 capacitor $0.1 \mu \mathrm{~F} 1,000 \mathrm{~V}$ d.c. or 300 V a.c.
C3 capacitor $0.022 \mu \mathrm{~F} 1,000 \mathrm{~V}$ d.c. or 300 V a.c.
CSR1 triac type 40432 with heat sink clip type 5F or triac type 40430
S1 Single-pole, on-off toggle switch 250 V a.c. Metal electrical switch box $2 \mathrm{zin} . \times 2 \mathrm{in}$. $\times 17 \mathrm{in}$. or 6 tin. $\times 3$ tin. $\times 2$ in. with 13 A mains socket Tag strip 8-way,knob,pvc wire,rubber grommet


Fig. 2: Component layout and wiring

The input transducer is a small loudspeaker, followed by Tr1 and Tr2 as amplifiers. VR1 is a sensitivity control, allowing adjustment of the sound level at which the unit operates.

All components except the speaker and VR1 are mounted on the perforated srbp board in Fig. 2. Underside wiring is shown in grey. Points $\mathbf{A}, \mathrm{B}$ and C carry connecting wires to VR1. Wires $A$ and $C$ are connected so that sensitivity increases as the control knob is rotated from the "off" position in the usual way. The case is an aluminium box or chassis.
Test by connecting a meter to the output terminals. A brief pulse of current is indicated when switching on, due to C5. The reading should then remain at zero, rising to $100-250 \mathrm{~mA}$ while snapping the fingers or speaking quietly.

Place the unit adjacent to the source of sound. Where extraneous sounds may operate the unit, reduce sensitivity by turning back VR1 just enough to avoid this.

Twin bell wire or a long twin flexible lead run from the output terminals to the bell or relay. A diode 1 N4148 should also be connected across the output terminals to suppress back e.m.f. through Tr4; diode plus to collector.

Connections for OC71, OC81: Collector nearest spot, then base, emitter.


Fig. 1 : Circuit diagram of the amplifier

## components

## Resistors

| R1 | $47 \mathrm{k} \Omega$ | R5 |
| :--- | :--- | :--- |
| R2 | $10 \mathrm{k} \Omega$ |  |
| R3 | $8 \cdot 2 \mathrm{k} \Omega$ | R6 |
| $1.2 \mathrm{k} \Omega$ | R7 | $39 \Omega$ |
| R4 | $47 \mathrm{k} \Omega$ | R8 |
| $2.7 \mathrm{k} \Omega$ |  |  |

All $\pm 5 \%$ tw

## Potentiometer

VR1 $5 \mathrm{k} \Omega$ with switch $\mathbf{S} 1$ attached
Capacitors

| Capacitors |  |  |
| :--- | :--- | :--- |
| C1 | $0.5 \mu \mathrm{~F}$ polyester | $\mathrm{C4}$ |
| C | $50 \mu \mathrm{~F} 6 \mathrm{~V}$ electrolytic |  |
| C | $2 \mu \mathrm{FF} 6 \mathrm{~V}$ electrolytic | C |
| C | $50 \mu \mathrm{~F} 6 \mathrm{~V}$ electrolytic |  |
| C3 | $50 \mu \mathrm{~F} 6 \mathrm{~V}$ electrolytic | C 6 |

Transistors
Tr1 OC71 Tr3 OC81
$\begin{array}{llll}\text { Tr2 } & \text { OC71 } & \text { Tr4 } & \text { OC83 }\end{array}$

## Transformer

T1 9•2:1, CT primary, type T/T7 Repanco

## Miscellaneous

Miniature 40 ohm speaker
Perforated srbp board $4 \mathrm{in} . \times 2 \frac{1}{2} \mathrm{in}$.
Screw terminals or sockets
Case, aluminium or wood, $10 \mathrm{in} . \times 4 \mathrm{in} . \times 3 \mathrm{in}$.


This alarm gives a warning by means of a bell, buzzer or lamp, so it can be used as a baby alarm, or as an extension for a door-bell or telephone bell. As it is sound operated, no direct connection is necessary to a telephone or other equipment.


Fig. 2: Component layout and underside wiring shown grey



## components



Fig. 1: Circuit diagram


Fig. 2: Component layout and wiring

Simple regenerative receiver providing headphone reception of local medium wave stations only. Power derived from a mercury cell when energised from daylight or good artificial light. A 1.5 volt dry cell can be used instead.
Tuned circuit consists of 79 turns of $26 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. enamelled copper wire ( $A$ to $C$ ) close wound on ferrite rod in. diameter, in parallel with small tuning capacitor VC1. This coil has a tapping (B) nine turns from one end (C). Trimmer capacitor TC1 controls regeneration and is set so that oscillation is just possible with VR1 near maximum voltage setting when using a single 0.5 V solar cell.
Tuning coil is wound on thin card or thick paper tube so that it can be moved along ferrite rod for best reception. A few feet of flexible wire aerial connected at A may help reception. Phones should be high impedance 2,000 ohms or more and connected via jack socket on box. Small components are mounted on perforated srbp board and wired underneath. Keep wires short. Minimum recommended box size 3 in . $\times 2 \frac{1}{4} \mathrm{in}$. $\times \frac{3}{4} \mathrm{in}$. Connections for AF711: collector wire nearest spot, then screen, base, emitter.

## COMPONENT SUPPLIES

Components should be readily available from several of our advertisers including the following: Arrow Electronics, Chromasonic Electronics, Electrokit, Electrovalue, Henry's Radio, Home Radio (Components), A. Marshall \& Son, Trannies, J. Bull (Electrical) and others.

Sub-standard, unmarked or other components that are not as specified in components lists cannot be guaranteed as suitable substitutes. Constructors should satisfy themselves before buying.

# TRICOLOUR 

Mood Lighting System

PART TWO

JUREK BUDEK*



THE P.W. Tricolour provides a versatile but straightforward form of colour lighting effect that is much improved on earlier designs, due largely to the use of the principle of zero voltage switching. Last month's article explained how this was done so now it is time to do the construction and see the results.

## Construction

In the P.W. Tricolour lighting system, the bass frequencies are 'presented' by the red lamps, middle frequencies by the green lamps and treble frequencies by the blue lamps. The control unit referred to in the following text is the P.W. Tricolour filter and control unit.

The construction of the control unit is not complicated if care is taken to follow the drawings and assembly notes. Before connecting any mains supply to any unit, double-check all wiring against the circuit diagrams (last month) and wiring diagrams, making quite sure that all thyristors, triacs and diodes are correctly connected.

It is recommended that sockets are used for mounting the integrated circuits. Do not solder the I.C.'s directly to the printed circuit board.

Assemble the eight way socket to the back panel in such a manner that when plug is inserted the five core cable to the lamps leads horizontally away from the fuse assembly.

The lights output socket is a Bulgin type P552 and the plug to fit this (for the lamps unit lead) is a Bulgin P551.
Attach the fuse holders, rubber grommets and speaker socket to the back panel. Assemble the components on to the printed circuit board, making sure that no accidental solder bridges occur across adjacent copper pads. The heat sink for the triacs is "live" and should not be connected to, or allowed to come in contact with, any metal part except the triac mountings, which are also the connections to their "main terminal 2". For safety connect this, the "zero" voltage indicated on the mains transformer, to the neutral terminal of the mains, and connect the control unit chassis to earth on the mains plug.

Insert the rubber grommet for the l.e.d. lamp

[^4]indicator into the front panel. Switches S1, S2, S3 and S 4 are as used in the Texan amplifier.

The mains switch shown on the front panel uses detachable connecting clips, but any suitably rated mains switch is suitable. The front panel is mounted on the front of the chassis frame with spacers so that clearance of the control fixing nuts provides a neat and uncluttered appearance to the panel. The assembly


Fig. 13: The simplest arrangement in which one control unit drives three lamps, each 100 to 150 watts. E represents the earth or chassis connection via tag 1 on the Bulgin 8 pin plug/socket arrangement. The figures in parenthesis are the pin numbers. $C$ is the common lead to the lamps-which is the 240 V live lead. L1, $L 2$ and $L 3$ are the leads to the respective lamps shown as LP1, LP2 and LP3 (Flg. 12 lasi month).


Fig. 14: Three banks of lamps, each 100w maximum, driven from one control unit.


Fig. 15: Three banks of lamps, each 100 W maximum, controlled by one frequency range.
 unlts.
uses 6BA nuts and bolts.
The three triacs and their associated heat sink uses 4BA nuts and bolts.

Fuses FS1, FS2 and FS3 are in the bass (red lamp), middle (green lamp) and treble (blue lamp) circuits respectively.

## Unit Arrangement

The equipment consists of two units. One unit contains the control for the psychedelic lights, the filter circuits and the necessary power supply. It is advisable, but not essential, that this unit is located near to the 13A power socket and amplifier. The second unit is mobile and consists of three colour lamps mounted on a panel with a five core flexible cable attached to it. This unit can be hung on the wall, left on the table, or placed in some other convenient position.



Fig. 18: Component layout and wiring to the printed circuit board. It will be observed that there are two leads from the 250 V tag on T4. One lead is the live (L) lead from the mains terminal block. The other lead goes to tag 2 on the lights oulput socket.


Fig 19: Full size pattern and drilling positions of the printed circuit board.


Fig. 20: Wiring of chassis mounted components to the printed circuit board. Tag 1 on the lights output socket goes to chassis (and malns earth). The live lead (L) from the malns terminal block goes to the 250 V tag on 74 transformer.

The power control unit is capable of supplying three of these lamp units in parallel, each with its three coloured 100 watt lamps, i.e. a total power capability of $3 \times 300$ watts. Each lamp unit has a six way terminal block for interconnecting as shown in the diagrams.
Fig. 13 shows the connections for a single lamp unit. The five core cable is terminated with a plug suitable for connecting to the control unit. The figures in brackets show the pin numbers on the plug used. Connected thus, the three lamps will flash in accordance with frequency ranges present in the music.
Fig. 14 shows a triple unit arrangement, where each unit is connected in the same way as shown in Fig. 13. Here, however, the overall light level is increased and flexibility of lamp positioning is allowed, each lamp unit maintaining its three frequency range response.

A great deal of experimentation of lamp arrangement is worthwhile to achieve the best effect to suit your roon and music. Fig. 15 gives another arrangement, using three lamp units, which is basically similar to that shown in Fig. 14, except that here each lamp unit will flash according to one frequency range.
The interconnections between speaker, amplifier and control units are also straightforward. Simply connect the speaker's DIN plug into the control unit and then plug in the cable from the control unit, now terminated with a DIN plug, into the amplifier. This should be done while all power is switched off. The amplifier should be connected via the control unit to a suitable loudspeaker before switching on.

The arrangement for a stereo system is very simple. Two control units and two lamp sets are required. A three core cable from a 13A socket is connected to the terminal board of control unit 1 . From the same terminal board the second three core cable is connected to control unit 2 as shown in Fig. 16.
The advantage of this arrangement is obvious, i.e. only one 13A plug is used for both control units. If required, the power supply to the amplifier can also be taken from the terminal board of control unit 2 as shown in Fig. 16, thus achieving further simplification.
The interconnections between the control units, amplifier and speakers are similar to that described for the mono system but duplicated. Connect one speaker DIN plug into control unit 1 and then plug in the cable from it into the amplifier socket. This is repeated for the second speaker and control unit.
The effectiveness of the association of the light and music can be further improved if the lamps are placed near the speaker from which they are actuated. It is extremely effective when standing each lamp unit on or behind each speaker cabinet and projecting the lights up the walls behind.
The printed circuit board shown in this issue is for the zero voltage control version of the P.W. Tricolour only. A different printed circuit board, alternative components and slight alterations to the metalwork will be required for the version with lamp dimming facilities.


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## PRODUCTION LINES

## ADJUSTABLE SPANNER

The picture shows a self-adjusting spanner suitable for all nut sizes from $\frac{7}{16} \mathrm{in}$. to $\frac{+7}{6} \mathrm{in}$. A.F.

The end of the tool is placed over the nut and turned until the "tongue" of the spanner locks onto the nut.

It is constructed from chromevanadium steel and weighs $5 \frac{1}{2}$ ozs. Finish is either matt ( $£ 1 \cdot 49$ ) or polished (£1•79). Thunder Screw Anchors Litd., Victoria Way, Burgess Hill, Sussex, RH15 9NF.


## TUAC EQUIPMENT

Tuac Ltd., are marketing a new range of ready-assembled modules and complete units. They are a "waawaa" unit, fuzz box disco "auto fade', octave doubler and a phasesplitter.

Leaflets which are issued in conjunction with Tuac kits can be obtained on receipt of a $3 p$ stamp from: Transistor Universal Amplification, Co. Ltd., 163 Mitcham Road, London, SW17 9PG.

## AUTO GROOVE-KLEEN



If you have an autochanger record playing unit, you have not been able up to now, to use a groove-cleaning brush to remove the dust and dirt from the records.

Bib seem to have solved this problem with their model 45 unit which just sticks onto the cartridge housing. Obviously to avoid any increase in stylus weight, the tone-arm should be re-balanced or the calibration control reduced by two grammes.

Due to the design, the velvet shoe and brush will not drag across the record when the tone arm moves from the end of one record to the outside of the record stack.

After the records have been played, the velvet shoe can be lifted off for cleaning with the separate brush supplied.

The price of this unit is 98 p plus tax. Bib Sales, P.O. Box 78, Hemel Hempstead Herts.

## GUIDE TO SEMICONDUCTORS

Motorola Semiconductors Ltd. have published a "master selection guide". It includes in its 150 pages brief technical details of 17 diode families from 4-layer to zener, hybrid circuits, microwave devices, optoelectronic components, rectifiers, triacs, diodes, linear integrated circuits and much more than we can describe here. The guide, which is free of charge, may be obtained from Motorola Semiconductors Ltd., York House, Empire Way, Wembley Middlesex.

## TRANSISTOR TESTER

Transistor tester type TT169 has been announced by Avo. It is designed for GO/NO-GO in-circuit testing of p.n.p. and n.p.n. signal or power transistors. The tester is battery operated and small enough to be held in the hand. Front panel lights show whether a device is faulty or OK.

The TT169 comes with all the necessary leads and connector in a plastic case. The price is $£ 17.50$ plus VAT and readers may obtain them from the usual retailers and distributors. Avo Limited, Avocet House, Dover, Kent.


## COMPONENT HOUSING TYPE LK8

Logikontrol Ltd., announce a compact component housing. It is made from high impact polystyrene and measures $90 \times 50 \times 37 \mathrm{~m} . \mathrm{m}$. and at $\mathbf{2 5 . 4 m . m}$. to the inch, you can work it out for yourselves! The internal volume is $10 c . c$. and it has facility for 2 printed circuit boards on which the components can be mounted.

Printed circuit connections and a snap-fit lid eliminate the need for a special plug and socket.

These units which are available in five different colours may be obtained from large component suppliers or in quantities of 10 upwards from Logikontrol direct, the 10 off price being 22p each. Logikontrol Ltd., 17 Little Edward Street, London, NW1 4AT.


## R.A.PENFOLD

THIS is a simple device which is easy to construct and which when placed ahead of a medium wave receiver will enable it to cover the 80 and 160 metre amateur bands. The unit is self contained, and is housed in a diecast box measuring $4^{3}$ in $\times 3^{3}{ }_{4}$ in $\times 2^{5}$ s,in. An external long wire aerial and an earth are required.
Only two transistors are used, including a fieldeffect type in the mixer stage. Frequency stability is excellent as the oscillator is crystal controlled.

## Heterodyne Principle

What is required of the converter is to receive a signal in either the 160 or 80 metre band and change this signal to a frequency which lies in the MW band. This can be achieved by heterodyning.

This is a process in which two signals are mixed to produce at the output, (a) the original two frequencies, (b) the sum of the two, and (c) the difference between the two. By the use of tuned circuits in the output, whichever of the two new frequencies produced is required can be selected.


Fig. 1: Diagrams showing methods of converting a signal to a fixed or variable intermediate frequency.

The manner in which this process can be used in a converter is shown in Fig. l. In the type of converter shown in Fig. la, the circuit is arranged so that the frequency to which the tuned circuit at the input is tuned is different from the operating frequency of the oscillator by the i.f. The tuning capacitors for the aerial tuned circuit and the oscillator would be ganged.

An example is given in the diagram of how a 3.8 MHz signal is converted to a $1 \cdot 6 \mathrm{MHz}$ i.f. There are two oscillator frequencies which will allow this ( $3 \cdot 8-1 \cdot 6=2 \cdot 2 \mathrm{MHz}$, or $3 \cdot 8+1 \cdot 6=5 \cdot 4 \mathrm{MHz}$ ). In this type of converter the receiver is tuned to the i.f., and the tuning is carried out on the converter.

A second type of converter is shown in Fig. 1b. This type is often used in 2 and 4 metre VHF
amateur band converters. This time the tuning is carried out on the receiver, the oscillator on the converter being at a fixed frequency. The aerial tuned circuit should either be a broadband unit i.e. resonant over the entire band which is to be tuned, or should be tuneable over this range. Again there are two possible oscillator frequencies (3.8-1 = $2 \cdot 8 \mathrm{MHz}, 3.5-0.7=2 \cdot 8 \mathrm{MHz}, 3 \cdot 8+0.7=$ $4 \cdot 5 \mathrm{MHz}, 3 \cdot 5+1=4 \cdot 5 \mathrm{MHz}$ ).

This type of converter has the advantage that the oscillator can be crystal controlled, simplifying alignment and giving very good stability. This type is also very much more simple and inexpensive. The system does have drawbacks as discussed later but the author's converter, which is of this type, has proved very successful.

## Practical Circuit

A circuit diagram of the converter is shown in Fig. 2. $\operatorname{Tr} 2$ is operated as a Pierce oscillator the crystal being used on its parallel resonant frequency. The primary winding of the oscillator r.f. transformer, L5, forms the collector load for Tr 2 . R2 biases the transistor, C3-C5 produce a centre tap on the crystal, this centre tap being earthed.

Tr 1 is the f.e.t. mixer stage. Ll is the aerial input coupling winding and L2 the aerial tuned winding. This can be tuned over the range $70-230$ metres by VCl. Trl is used in the common-source mode, source bias being provided by Rl and Cl is its decoupling capacitor. Trl's source and R1 are connected via the


Fig. 2 : Complete circuit of the converter unit.
secondary winding on the transformer, L4. The voltage across L4 modulates Trl's drain and source voltages and thus mixes the oscillator signal and the input signal. A small r.f. choke, L3, forms the drain load for Trl, the mixed output being coupled to the receiver via C3.

SW1 is the on-off switch, and R3 reduces the 9 V supply to the required level. C2 is the supply decoupling capacitor.
The crystal frequency is chosen so that it can be used to convert signals in both the 80 and 160 metre bands to the MW band, the desired band being selected by tuning VC1-L2 to the correct frequency. Using a 2.8 MHz crystal the 80 metre band will be converted to $0.7-1 \mathrm{MHz}(3.8-2.8=1,3.5$ $-2 \cdot 8=0.7$ ), and the 160 metre band will be converted to $0.8-1 \mathrm{MHz}(2.8-1.8=1,2 \cdot 8$ $-2=0.8$ ).

It is not essential for the crystal to operate exactly on 2.8 MHz , as if it is a little either side of this frequency the converter will still operate but the tuning range on the receiver over which the amateur bands are covered will be slightly altered. A $2 \cdot 794 \mathrm{MHz}$ crystal was used on the prototype.

## Construction

The circuit is housed in an STC diecast box. The wiring is broken into two sections, a 5 -way tagstrip on which the oscillator is constructed, and a 6 -way tagstrip on which the mixer is built.
Diagrams illustrating the wiring of these two tagstrips are shown in Fig. 3 (mixer) and Fig. 4 (osc.). These two diagrams also show all other wiring of the converter. All the wiring is quite straightforward and should present no difficulty, even to a beginner. The only point which should be noted is that the screen lead of Trl is too short to reach to the appropriate tag unless a short piece of insulated wire is used to lengthen it.

Figure 5 shows the interior layout of the unit and also gives details of the mounting bracket of the crystal. This bracket is constructed from 18-22 swg sheet aluminium. The two tagstrips are mounted by $1_{2}$ in 6 BA bolts, a stand-off insulator $1_{4}$ to $3_{8}$ in long being used to hold them clear of the sides of the case.

The battery is held in place by being trapped between the front, and rear of the case. A pad of expanded polystyrene, foam rubber or a similar material should be glued to the rear of the case where the battery would otherwise come into contact with it. This is to make it fit more firmly and to insulate the battery terminals from the case.


Fig. 3 : Method of wiring the mixer stage components.

## $\star$ components list

Resistors
$\left.\begin{array}{ll}\text { R1 } & 820 \Omega \\ \text { R2 } & 1.5 \mathrm{M} \Omega \\ \text { R3 } & 820 \Omega\end{array}\right\} \quad$ All $\div \mathrm{W}, 5$ per cent types

## Capacitors

C1 5000pF
C2 $0.022 \mu \mathrm{~F}$ polystyrene etc.
C3 10 pF ceramic or silver mica
C4 220pF polystyrene or silver mica
C5 68 pF polystyrene or silver mica
C6 220pF polystyrene or silver mica

## Semiconductors

Tri BFW10 or similar f.e.t.
Tr2 BF115

## Miscellaneous

L1/2 Repanco RA3; L3 miniature r.f. choke, about 1.5 mH ; L4/5 Repanco RO3; SW1, on-off switch; STC diecast box, size 2 ( $42 \times 3 \frac{3}{2} \times 2 \frac{-3}{3}$ in.); HC6U crystal, about $2 \cdot 8 \mathrm{MHz}$ with holder (see text) (Henry's Radio); 1 -off each 5 -way and 6 -way tag strip; 2 -off coax sockets; Knob; Battery and clip.

As supplied, the exterior finish of the diecast box is rather rough and dirty. If the case is to be painted it will be necessary to thoroughly clean it first with a scouring pad. If preferred it can be cleaned in this way, and then polished to a bright natural finish.

## Using the Converter

An external aerial is required; this merely consists of a length of wire which is mounted as high as possible and is as long as possible. An earth of some sort is essential for the correct operation of the circuit, although this does not necessarily have to be a very efficient one. The prototype is fitted with coaxial sockets for the aerial, earth and output connections.
Ideally the converter should be used in conjunction with a broadcast receiver which requires an external aerial. The receiver and the converter are connected by a short screened cable. In this way there is a minimum of interference picked up on the MW band directly by the receiver.

It was found possible to use the converter with an


Fig. 4: Tagstrip construction of the oscillator stage.
ordinary transistor receiver. C3 should be removed, and a piece of wire connected in its place. It is then merely necessary to take a short lead from the converters output socket, and to place this alongside the receiver's ferrite aerial.

In this way it was found possible to receive a number of amateur stations on both the 80 and 160 metre bands. MW stations received directly by the receiver can prove bothersome, especially after dark.


Fig. 5: Layout of components and tagstrips inside the die-cast box.

Operating the controls on the converter is very simple, as there are only two. SW1 is the on-off switch. VCl tunes the converter to the desired band. With this control turned almost fully anti-clockwise it should be found possible to tune the 80 metre band and with it turned almost fully clockwise it should be possible to tune 160 metres.

With VCl approximately adjusted in this way, it should be possible to receive a few signals. VCl can then be peaked for maximum sensitivity. A simple dial can be marked around the control knob of VC1 showing the areas over which the amateur bands are tuned.

## Results

Using the converter with a 132 ft . longwire aerial at about 20 ft ., in conjunction with a 6 transistor MW portable receiver, a large number of amateur stations have been heard. The 160 metre band is of course used mainly for local working, and a.m. is still used to a certain extent. Stations up to about 50 miles distant have been received on this band without too much difficulty.

Due to its simplicity, the circuit does have one drawback. Top Band is not only used for amateur transmissions but also for maritime ones. These transmissions are fairly powerful and occasionally when tuning the 80 metre band transmissions from ships in the nearby Thames estuary did break through. Conversely, a local amateur using a powerful SSB transmitter on 80 metres did tend to break through on the 160 metre band.


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## SHORT WAVE RECEIVER CHOICE by MALCOLM CONNAH

By far the largest portion of my mailbag consists of lettters from readers asking my advice on the choice of a receiver. I have often said that this is a very difficult subject on which to give advice. partly because the letters give very little information and partly because "one man's meat is another man's poison".

In order to assist the less technically minded reader to select a receiver to meet his requirements I am going to devote this article to discussing the various features of receivers which are important for good short wave reception.

1. Frequency Coverage: The most common type of receiver is the General Coverage Receiver. This type of receiver usually tunes from 540 kHz to 30 MHz in four bands. One of these bands covers the medium wave band leaving three bands of short wave coverage.

Due to the number of stations on the bands it is very desirable to have a separate bandspread, or fine tuning, control. This control has the effect of expanding a small portion of the tuning scale making it much easier to tune in a particular station. The much-advertised transistor portable receivers are usually lacking in this respect.

An alternative method of frequency coverage is found in the more expensive receivers which have a number of bands each covering 500 kHz of the spectrum. These receivers usually cover the Amateur bands only but can be ordered with coverage of the Broadcast bands. The tuning of these receivers is so fine that a separate bandspread control is not required.

In general the listener must ensure that the receiver covers the bands in which he is interested and that the tuning can be finely controlled.
2. Number of Conversions: The number of conversions that a receiver has is the number of different i.f.'s (Intermediate Frequencies) that it has. The normal single conversion receiver has a single i.f. usually in the range $455-470 \mathrm{kHz}$, although 1.6 MHz is sometimes used. The double conversion receiver has two different i.f.'s. In general, the more i.f.'s a receiver has, the better the selectivity and image rejection will be.
3. RF Stages: Some of the simpler receivers available have no r.f. stage and the signal is passed from the aerial to the mixer stage directly. The addition of an r.f. stage will increase the sensitivity of the receiver and also improve the image rejection of a single conversion set. As mentioned last month this problem can be overcome by adding a preselec tor between the aerial and the receiver.
4. Operating Modes: The Broadcast Bands listener is usually only interested in amplitude modulated (a.m.) signals and this mode of operation is, therefore, essential. If the set is also to be used for reception of Amateurs provision should be made for code (c.w.) reception, this also allows reception of single sideband (s.s.b.) transmissions. However, the provision of a product detector gives much better s.s.b. reception. If the provision also exists for manual selection of the upper or lower sideband this facility can be used during the reception of a.m. signals to avoid interference and fading effects.
5. Selectivity: The selectivity of a receiver is its ability to separate stations on adjacent frequencies. It is extremely useful to have the facility of varying the selectivity of the receiver. When interference is heavy a narrow selectivity can be used to cut out the interference. Mechanical or crystal filters help to improve the selectivity of a receiver.
6. Stability: It is essential for a good receiver to be stable in operation. With some valve receivers the heating effects involved caused frequency drift and other annoying effects. The introduction of transistors and, in particular, field-effect transistors has greatly improved the situation due to the low heating effects associated with these devices.
\%. Valves vs. Transistors: Apart from improving stability, as mentioned above, transistors have many advantages in communication receivers. They have a longer life, require simpler power supplies and are low cost. The benefits of this are that transistor receivers tend to be smaller, lighter in weight, less expensive and also have the option of being operated from an external battery.
8. Automatic Volume or Gain Control (a.v.c. or a.g.c.) Almost every receiver has some form of a.v.c. or a.g.c. which adjusts the gain of the receiver to compensate for changes in signal strength. A receiver with variable a.v.c. or a.g.c. is to be preferred as the optimum setting can then be used.
9. Extras: Most receivers have various extras of which the following are the most useful. (a) The provision of a headphone socket. (b) An aerial trimmer to match the aerial to the set. (c) A signal strength meter (S-meter) to assist with tuning. (d) A crystal calibrator to check the dial accuracy. (e) A noise limiter which should be variable if possible. (f) A notch filter to reduce hetrodynes.


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COMMERCIAL RADIO by CHARLES MOLLOY

COMMERCLAL radio in the UK has come a step nearer with the start of medium wave tests in the London area by the Independent Broadcasting Authority. Kevin Peel (Hornchurch Essex) has heard the IBA on 557 kHz with transmissions of music and announcements stating that the tests were being made by the IBA for an indefinite time. The choice of frequency is a surprise as the two IBA London stations are expected to be on 1151 kHz (London News) and 1546 kHz (London Entertainment). The first regular broadcasts from the IBA are scheduled to start this year with the opening of the London stations to be followed in 1974 by others in the provinces.
Harold Emblem (Mirfield, Yorkshire) has logged a number of medium wave stations in the Persian Gulf area between 0230 hrs and 0300 hrs GMT. He reports Kuwait on 539 kHz ; Tabriz, Iran on 645 kHz ; Bagdad 760 kHz ; 'The Voice of the Arab Emirates' Dubai 1250 kHz with an Arabic religious programme followed by pop music at 0300 hrs ; Teheran 1325 kHz ; Kuwait 1345 kHz . Harold mentions that Kuwait

539 kHz can be heard during the evening under Budapest, which uses the same frequency. Baghdad on 760 kHz is also audible in the evening.

Commercial radio is well established in Spain where several chains of low power locals operate alongside the government owned Radio Nacional Espana networks. The commercial stations are allocated call signs and about 150 of these outlets can be found all over the band. Those most frequently heard in the UK are EAJ5 Radio Sevilla on 809 kHz ; EAJ1 Radio Barcelona on 827 kHz ; EAJ2 Radio Espana (Madrid) 917kHz; EAJ29 Radio Intercontinental 953 kHz ; EAJ8 R. San Sebastian 1025kHz; EFE14 La Voz de Madrid 1097 kHz ; EAJ15 Radio Reloj (Barcelona) 1124 kHz ; EFJ43 Radio Juventud Bilbao 1133 kHz ; ECS11 Radio Centro Madrid 1385 kHz ; EAJ20 Radio Sabadell 1475 kHz ; EFE25 La Voz de Calabria 1570 kHz . The common channels $1106 \mathrm{kHz}, 1133 \mathrm{kHz}, 1394 \mathrm{kHz}, 1412 \mathrm{kHz}$, $1430 \mathrm{kHz}, 1475 \mathrm{kHz}, 1502 \mathrm{kHz}, 1520 \mathrm{kHz}$ and 1570 kHz are crowded with stations. They sign-off for the night from 2300 hrs GMT onwards and at this time the DXer can hear one station after another dominate a channel only to close down and leave the frequency free for a weaker occupant. Many a rare catch can be had at this time.
L. J. Hook asks for information about the MW Command receiver. Also known as the BC946 it was part of the ARC5 aircraft communications equipment used in the last war. It performs very well on the medium waves but it does require some modification as it was designed to work from a 28 volt aircraft supply.

## IBA ON VHF

## by SIMON DAVID

THIS new v.h.f. section will be a regular feature giving news and views on transmissions usually found on the 88 to 108 MHz dial, but may be extended to include related topics. VHF is generally taken to include transmissions between 30 and 300 MHz , i.e. below 10 metres, but since this area is also covered in David Gibson's Short Wave column, this section has been specially started to provide some information more appropriate to broadcasting.

Since f.m. broadcasts began in the U.K. on a regular basis, it has been continually predicted that the medium wave band was due for banishment. This has not come about however and the medium wave is in fact still being exploited. What is expected is that the new Independent Broadcasting Authority Stations will use the upper reaches of the f.m. dial for stereo programmes, but will not necessarily use the same transmitters as the BBC. Receivers within close proximity of a BBC transmitter and collecting signals of around $100 \mu \mathrm{~V}$ may find that they will be able to pick up a 20 mV signal from the local IBA station.

One of the main headaches is expected to come from cross modulation effects due to emergency services being tuned in close to the commercial channels. This will undoubtedly result in a number of semi-redundant old tuners, although there is no fear of upsetting their present usefulness for BBC programmes. Whether politics come into this we are not too sure, but it is strange how the commercial side of broadcasting frequently has to accept second rate operational conditions.

In order to help find space for the new IBA com-
mercial radio stations, the BBC will be nudging its local stations along the v.h.f. tuning scale a little, changing the operating frequencies of Radios London, Medway, Oxford, Brighton, Bristol, Leicester, Nottingham, Stoke, Humberside, and Sheffield. These adjustments are expected later this year when the appropriate details should be given in the local Press and Radio Times.
The new station at Carlisle is still expected to "appear" on 95.6 MHz , but it looks as if Swaledale will be "lost" for want of a suitable site for a relay station.

Although some way off yet, it is not a bad idea to look into the needs and possibilities of incorporating very sharp rejection filters to suppress adjacent local transmitters. The use of a field effect transistor at the front end will also help to reduce cross modulation effects. Several tuners have automatic gain control and since this would not be helpful in this situation it is worth incorporating a switch so that it can be cut out of service as necessary.
Furthermore, the mixer stage design becomes critical and the noise generated here must be at a very low level. This will mean that the r.f. circuit will not have such a high gain as in the past but this can be made up by increasing the gain through the i.f. stages.
The use of phase-lock integrated decoders will provide tuners with lower distortion and better frequency response, both of which have become necessary for good stereo reception.
We shall always be pleased to hear of readers' experiences of v.h.f. reception, especially those who listen in to continental stations. Please be brief and confine your letters to stations received, aerial and tuner used and the effect of interfering transmissions.


SHORT WAVES by DAVID GIBSON, G3JDG

THIS month's postbag has been conspicuous by the very marked absence of 14 MHz logs. It seems that the twenty-metre-only addicts are as dead as their band these days. Meanwhile, back at the eighty-metre ranch it's been a right merry r.f. square dance. The amount of DX on eighty has been quite remarkable with west coast W stations romping in at times. In fact, stations further down the globe have also put in an almost regular appearance on this band; Mexico, Brazil and Argentine, etc. Some real goodies have put in an appearance for the persistent enthusiast. Callsigns like DU1EJ and VS6DO have shown that your reciever dial need not read above 4 MHz in order to $\log$ some rewarding DX signals both on phone and c.w.

News from VE land. An enthusiastic band of Canadian Amateurs are building a large oceangoing trimaran. Their object is to put the 40 most "wanted" countries on the air. I will pass on information about their ports of call as soon as I hear.

Great hopes that an Amateur station will be allowed on Clipperton Island. Callsign to listen for will probably be FO8C. Anyone heard the station reported to be located in the Spanish Sahara yet?

Time to pass on to some queries, curses and comments. Michael Green (Cheshire) uses a UR1A. The drawing of his antenna system bears a harrowing resemblance to the national grid. (Bet he's the only s.w. 1 who tunes topband in rubber gloves and wellies). Michael queries queer callsigns heard in the wee small hours on 80 metres s.s.b.; Rudolph, Scrooge, Virgin Mary and Snowman. Michael's problem is simply, "How do I QSL them?" (Perhaps the nearest Asylum is licensed?).

Letter from a long, long way off bears the signature of Lindsay Pennell and the post mark Hong Kong (Ah, those were the days, Chow Mein butties and cocoa on the Kowloon ferry). Lindsay wonders why so few G s.w.l.s hear the Hong Kong throng signing VS6. There are some 40 licensed Amateurs many of them being very active into Europe. Confess now, you're all logging VS6's and not telling your Auntie David.

Simon Baines (Hitchin) reports a number of W stations including W5NMA, heard on forty metres s.s.b. Gear is a five-vale receiver, transistor b.f.o. and 30 ft of wire end fed.
M. Harrison (Derby) sends in a log of numerous G stations heard on topband. Incidentally, a good non-G to listen for on 1.8 MHz is WIBB/l whose stalwart support and interest in topband is well known all over the world. It is interesting to note that PYIDVG has been heard on $1 \cdot 8 \mathrm{MHz}$.
Kevin Smith is thirteerf summers old and lives in Brighton. (Wish I was and did.) Whereas most boys of 13 are the proud possessors of pieces of string and marbles, Kevin settles for a CR100 and a 215 ft long wire end fed. His best areas on topband were: DL8PC, GI3GRD, GM4BBL, GW3ZQN all on s.s.b., and OKIATP on c.w. His $\log$ for 28 MHz reads: CN8BF, CN8CF, CR4BS, CR7AF, CR7IZ, CT2AT, ET3USF, ET3USP, KV4CF, ST2SA, VP2LAF, WB4WOI/P, ZE4JW, ZS6AD, 4Z4ME, 6W8DL, 7Q7RM, 9G1HE, 9H4D, 9J2AY, 9J2DT all s.s.b.
Best times for listening on eighty metres are from midnight to around 0300 hours according to Alan Smith (Lancs). He bemoans the Lids who test incessantly by blowing into the mike (it's unhygienic but they can't touch you for it). Alan has a JR31), 60 ft end fed and an a.t.u. Heard on eighty: EP2TW, K1UAT, K2LQA, KP4AN, KV4CI, PY4BTK, VE1ADV, VP2LI, VP7ND, W1GEY, W2BXA, W3WGH, W4AG, ZB2CF, ZSiMH, ZS3GH, 9HICW, 9VIRE. A cheap day excursion to 14 MHz s.s.b. raised: EP2ES, HZ1AB, KG6JBE, KL7HFA, KX6BQ, LUIDAC, MP4TEE, VEIASJ, VE3MO, VK3ADR, YKIAA, ZL1KN, ZL1WE, ZL2AVE, ZL2BQC, ZL3QN.
David Sharred (Birmingham) had a quick tour of eighty metres. Main listening times were "after my paper-round", and the gear is a CR150/2 with a V. shaped antenna ( 60 ft each leg). Goodies bagged on $3 \cdot 5 \mathrm{MHz}$ : CN8BF, JY1, K5PFL, KV4AM, OA6NCT, PIIROS, VE3CDP/W9, W2HCW, W4MYA, W9QLD, WA5JMK, WB4MCI/P4, ZK2BO, ZL4BT, ZL4KF, ZS3GH, 3A2EG, 5U7AX. On twenty metres David's best were VK5RN and VK6XO.
Where are all you v.h.f. types hiding? No logs at all for lonely little 70 MHz and only one for 144 MHz . Michael Prescott (Lancs.) uses a Roamer 10 receiver and a two metre dipole. He reports signals from the following: G3AHD/A, G3PVC, G3VIM, G3XIM, G3VME, G8EYO/A, G8ESU, G8GYS, G8VLE and G8XDL. Well done Michael, you've kept the v.h.f. flag flying-just.
For the contest and Rally enthusiasts, April is a busy, busy month. Jottings from my Events diary read: April 1, White Rose Mobile Rally at Leeds; 1, WAB phone contest (l.f.); 8, WAB c.w. l.f. contest; 8, eighty metre QRP (low power) contest; 15, four metre portable contest (no excuse now for not sending in a log); 21-22, Bermuda contest (phone); 29, Rugby DF qualifying round; May 5-6, two metre and 70 cm open contest (another chance for the v.h.f. s.w.ls to shine); $5-6$, Bermuda contest (c.w.); 6 , Spalding Tulip Time Mobile Rally.

## BROADCAST BANDS

Short Wave Reports by 15 th of the month to Malcolm Connah, 59 Windrush, Highworth, Swindon, Wiltshire, SN6 7DT.
Medium Waves Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG.
VHF Reports to Simon David, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4 4AD.

## AMATEURBANDS

## Short Wave/VHF

Logs in alphabetical order please by 15 th of the month to David Gibson, G3JDG, 12 Cross Way, Harpenden. Hertfordshire.

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## JULIAN ANDEESON


#### Abstract

A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.


ALTHOUGH the prices of unijunctions have not taken the normal course of falling in cost, they are cheap enough to be used in one of our circuits.
The unijunction transistor bears little resemblance to the conventional transistor; it doesn't amplify, has only limited use and doesn't even have a collector. The connections are to an emitter, base 1 and base 2. In fact the best thing that the unijunction is good for is as a relaxation oscillator, as in Fig. 1.

## Operation

When a voltage is applied to the circuit, the capacitor Cl starts to charge up through R1 and VR1. Initially the emitter of $\operatorname{Tr} 1$ will be at negative potential but as the capacitor charges, the voltage at this point rises. When it reaches a certain point, $b_{1}$ and $b_{2}$ are virtually short circuited and current will pass through R2, R3 and $\operatorname{Tr} 1$. At the same time Cl will be discharged through R3 and the device will become open circuit again. The same process will start all over again so that a series of pulses appears across R3 via C2. Since the output will be a series of pulses whose rise and fall times are very rapid, only a low value capacitor is necessary despite the low value of R3. The output will be in the form of a positivegoing pulse; if a negative-going pulse is required this capacitor should be connected to $b_{2}$. A sawtooth waveform is available from the emitter but it should only be connected to a high impedance load otherwise the operation of the relaxation oscillator will be affected.

The frequency of the pulses depends on the relationship of the resistance made up from VR1 and R1 and the capacitor C1. Resistor R1 limits the current


Fig. 1: Circult and suggested valves for the pulse generator.

## No. 48 <br> PULSE GENERATOR



Fig. 2: Practical layout of components on a piece of tagboard.
through the emitter so that it cannot be connected directly to the positive line; this would cause damage to the device.

## Experimenting

There is room for experiment here; Cl can be altered in value from $500 \mu \mathrm{~F}$ down to $0.01 \mu \mathrm{~F}$. The high value will produce pulses with very long intervals; it is difficult to say how long as the natural leakage through the electrolytic will play a major role. If a low leakage device is used the time interval can be a minute or more. Using the low value capacitors the pulses could extend to ultrasonic frequencies.

## components list

| R1 | $22 \mathrm{k} \Omega \pm$ W, 5 per cent |
| :---: | :---: |
| R2 | $2.2 \mathrm{k} \Omega$ " |
| R3 | $100 \Omega$ |
| VR1 | $1 \mathrm{M} \Omega$ linear pot |
| C1 | $10 \mu \mathrm{~F} 12 \mathrm{~V}$ |
| C2 | $0.1 \mu \mathrm{~F}$ mylar, etc. |
| Tr1 | 2N2646 |

Prices are those recently advertised and may have changed. No allowance is made for minimum order costs or for postage and packing and these points should be checked carefully before ordering.

## Modifications

The output can be taken to an amplifier to act as a metronome. In fact if only a low level output is required, a high impedance loudspeaker ( $50 \Omega$ to $80 \Omega$ ) can take the place of R3; in this case of course C2 will not be needed.

A suggested layout is shown in Fig. 2 making use of a small piece of tag board; this is far from critical and almost any layout may be used.

Do you ever have that feeling that you are being watched? Well, maybe you are at that and have been for the past 13,000 years. A theory has been put forward that we are getting intelligent messages from space. To be more precise, from an interstelar "thingy" which is buzzing round the earth-probably in an orbit which is similar to that of the moon. (Good gracious, Holmes).

## LONG WAY ROUND

Before you rush out and wave your hanky at the sky, hear what the experts have done about it. It is all tied in with things called longdelayed echoes. These were observed as far back as 1928. A transmitter using 15 kW on 9550 kHz was radiating its Morse signal which in turn was being received by a number of receiving stations. A Morse signal was being sent and received almost instantaneously. Now a signal can go two waysdirect to the receiver by the shortest route and also in the opposite direction. This latter signal can quite easily travel right round the world before it is received by our receiver. Thus two signals are heard; the direct one, and the one which goes the "long" way round. The latter takes about one seventh of a second and is heard as an "echo" of the direct signal which, because it travels direct (therefore less distance) arrives almost instantaneously i.e., with negligible delay.

So far so good. But imagine the effect on the minds of the listeners when other echoes were heard-not delayed by one seventh of a second but at various intervals varying from about three seconds to 15 seconds! These long-delayed echoes were also noticed independently at other times, on other dates, by different receiving stations listening to a different transmitter and on a different frequency.

Then, someone plotted a graph of one of these echo sequences and another piece of the intrigueing jigsaw came to light. The plotted points bore a striking likeness to the constellation Bootis. Other echo sequences were plotted and produced patterns which were clearly
identifiable with other constellations.
The hypothesis has been put that the long-delayed echoes are being returned to Earth from a space probe; a probe which arrived from the Bootis constellation 13,000 years ago. Moreover, the probe was sent to search for evidence of intelligent life in the form of radio transmissions.

People who are in doubt about the validity of all this should bear in mind that all the evidence so far corroborates this hypothesis. So closely, in fact, that EMI engineers are to set up a high-power transmitter and high gain antenna (probably around 144 MHz ) in order to put the hypothesis to the test. Are they just being starry-eyed? I do not think so.

## ERNIE

Apart from driving the fastest milk cart in the west, Ernie has achieved fame in other ways. For example, he painstakingly avoids selecting your premium bond number every month without a single complaint or grumble. To date, his selections have paid happy punters prizes amounting to some $£ 350$ million-none of which has yet reached your scribe!

So it is with ageing joy and renewed. hope that I report a new Ernie who will produce the monthly list of prizewinners in under three hours. The old Ernie used to take ten days to complete the same task.
Before we non-winners get too elated, let us examine what we are up against. Just what (or who) is Ernie and how does he choose winners?

First, Ernie comes from Ernie Harrison, Managing Director of Racal, whose idea it was. Ernie himself (the number picker) has been described as the most advanced electronic system in the world for generating numbers in a completely random fashion. How does he/it go about the task?

The first job is to monitor the noise level of a pair of zener diodes (actually, a pair for each digit). Each "pair" noise is amplified and then compared with a reference voltage. Because of the nature of noise there are peaks, and each time one of these exceeds the set reference level it is counted and used in the production of a digit.

Once a complete digit is generated it is safely entrusted to the memory of a computer. Here, it is checked to see if it is eligible. If it is, then it will be stored in the computer's memory, if it is not, it will be discarded.
Ernie presses on until the memory or store has 60 numbers in its care. These are then "written" onto magnetic tape and this is then "played" to another computer for checking and finally linking the lucky numbers to the bondholders' names and addresses.

I am already making the most careful measurement of the noise generated by a pair of zener diodeswell, you never know.

## TRANSISTORISED TED?

How about an electronic government, a big computer tucked away beneath Parliament in a Guy Fawkesproof vault? Maybe not yet, but in America the computer has managed to secure itself a small governmental foothold.

The House of Representatives is to vote by computer. Problem has been the 435 -name list of members and the time wasted in correcting attendance errors. Other little hitches like finding a vote recorded from a member who wasn't even there were also proving annoying. The mind boggles.

The new system means that each member has a small plastic "card". He can use this card to vote at any one of some 50 stations located at various points about the House. Behind the Speaker's seat is a scoreboard which gives the latest updated score on how the voting is going. Electronic voting is reckoned to save at least 50 per cent of the time previously taken for such a task. The computer will also give written records of votes simultaneously plus an instant breakdown of these into States or Parties as required.
Look out members of Parliamentyou might be replaced by a pair of zener diodes one day-they're cheaper, smaller and generate less noise!
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## TRANSISTOR EIREUITRY for beinners PART 16

## Practicalities

A BCl 09 is chosen to give an open-loop gain of 260 , with an input of about 30 mV at 1 kHz . We shall aim to keep this level constant for further tests. Connecting the two resistors of Fig. 76 to the input, we have the virtual earth type of circuitry. This has been discussed at some length in previous articles. It can now be simpified to the triangle of Fig. 77,


Fig. 77: (a) Simpllfled representation, with the symbols denoting an inverting amplifler. (b) a frequency-dependent development, and (c) the bass cut variation, with the frequency-selective portion before the feedback loop.
the input shown conventionally at the blunt end; the output at the sharp end (i.e., the 'arrow' points the way the signal is going). Fig. 77 is a simplified diagram, the letter A within its triangle denoting that it is an amplifier.

Previously you will have noted reference to an 'inverter'. By this, is meant that the input is $180^{\circ}$ antiphase to the output. In Fig. 77, we see a bar over the $A$, denoting an inverter. For the benefit of oldtimers like me, this can be regarded as exactly parallel to valve technology: a positive-going waveform at the grid produces a negative-going waveform at the anode.

If previous articles have been followed, it will be noted that the closed loop gain, which is the circuit gain calculated after feedback has been applied, is derived from the formula: $G_{c}=R_{\text {tb }} / R_{\text {fn }}$.

If we now make $R_{\text {ln }}$ equal to $10 \mathrm{k} \Omega$ and $R_{\text {fb }}$ also $10 \mathrm{k} \Omega$, the closed loop gain is unity, i.e., $10 / 10$. In practice, we shall measure 0.8 rather than 1 . If, with $R_{i n}$ at $10 \mathrm{k} \Omega$ and $R_{f b}$ at $100 \mathrm{k} \Omega$, giving a theoretical gain of 10 , we were again to measure, we should find the answer more like 7•7. Carrying this experiment a little further-and please do not merely take our word for this; try it and see for yourself-we find that with $R_{t n}$ at $100 \mathrm{k} \Omega$ and feedback resistors varying between $10 \mathrm{k} \Omega$ and $1 \mathrm{M} \Omega$, the closed loop gain varies between $0 \cdot 1$, via 0.98 (at $100 \mathrm{k} \Omega$ ) and $5 \cdot 8$. Which only goes to prove that the actual gain is always less than calculated, and, secondly, the lower the circuit impedance, the greater the error.

Practically, therefore, it would seem that our circuit was not the best. But, as it is typical of the majority of commercial designs, we make no apology. It has to be remembered that the tone control circuitry does not have to contribute a lot of gain. We do not normally need a gain at any frequency of more than 'times 10', plus a stage gain of around 4, and so a maximum gain of about 40. Refinements will be added, never fear ...

Reverting to Fig. 77 (a) and making $\mathrm{R}_{\mathrm{In}} 10 \mathrm{k} \Omega$, with a similar value for $\mathrm{R}_{\mathrm{rb}}$, we obtain a gain of 0.98 , and the virtual earth point is at the junction of the two resistors. If we insert a resistor as shown at

Fig. 77(b) we reduce the gain somewhat, $0 \cdot 96$, but let's return to that later, the important point being that we can arrange the gain that we require by choice of $R_{t n}$ and $R_{t b}$.

Here I part with Mike and assert that many modern circuits are resolved and arranged (rather than designed) by what are euphemistically called 'empirical methods'; more cynically described as 'hit or miss'. With the basis of existing circuits and a mass of mathematics that go to support them, the modern designer takes for granted the previous researches, and builds upon them. Exceptions, like John Linsley Hood, who question every fact and do their own research, are as rare as gold nuggets in a leadmine.

All of which digression leads me to Fig. 77(b). Here we have $\mathrm{R}_{\mathrm{in}}$ at $10 \mathrm{k} \Omega$ with a similar feedback resistor $\mathrm{R}_{\mathrm{tb}}$ in series with a $0.047 \mu \mathrm{~F}$ capacitor (itself, practically, paralleled by $100 \mathrm{k} \Omega$ ). The impedance of the feedback network can, if you want to be meticulous, be calculated at any point in the frequency range.

This is all very fine, but, in practice, we can say that at very high frequencies the capacitor will be an effective short-circuit. In these circumstances, the circuit becomes effectively $R_{i n} / R_{r b}$ having unity gain. Lowering the frequency raises the reactance $\mathrm{X}_{\mathrm{c}}$ until it eventually becomes an open-circuit, and, in comparison with the $100 \mathrm{k} \Omega$ previously mentioned, the gain will be nearly 11. Theory gives us 110/10, practice a little less, hence my question-begging formula. We shall settle for a gain of around 20 dB , which is ten times the input voltage.

In the frequency range that $C$ is effective we will have an impedance change in the feedback network giving us a slope of $6 \mathrm{~dB} /$ octave. At frequencies below where unity gain is produced, the slope will flatten, so that further reduction of frequency does not change the output from unity gain. At frequencies above where the effective $R_{r b}$ is $110 \mathrm{k} \Omega$, i.e., for a theoretical gain of xll, the curve again flattens. The transitions from slope to flat are not sudden and our dotted curves show the practical results obtained.

## Turnover

Reference has already been made to $\mathrm{f}_{\mathrm{t}}$, and by this we mean the turnover frequency, (in the case of Fig. 75 we have two turnover points, at 3 dB positive or negative position on the curve, depending on the way the calculations are carried out, as should become apparent).

The $\mathrm{f}_{\mathrm{t}}$ points can be calculated from the formula $f_{t}=\frac{1}{2 \pi C R}$ where the frequency is in .hertz; the


Fig. 78: The bass IIft curve in theory (solid IIne) and In practice (dotted IIne).


Fig. 79 : A combined bass IIft and cut circuit.
constant $2 \pi$ can be taken as $6 \cdot 28, \mathrm{C}$ is in farads and R in ohms. Taking the component values of Fig. 77(b), we obtain a lower frequency turnover point of $33 \cdot 9 \mathrm{~Hz}$ while the upper frequency turnover point works out to 339 Hz .
In practice, of course, the points are not definite. The plotted curve, as can be shown later, follows rather the dotted than the hard line of Fig. 78. Plotting the curve obtained from a 'hook-up' replica of Fig. 76, we get the actual curve of Fig. 78, from a generator with a $600 \Omega$ source impedance, and reading across the 'open' output with a high impedance valve-voltmeter. (Amendment, please: our habit these days is to use the battery-powered millivoltmeter so the use of the term 'valve-voltmeter' is mostly a matter of habit-although we certainly continue to use our old faithful instruments where the low value of hum and noise will not prove an embarrassment.)
One of the reasons for the smoothing of a theoretical curve is, of course, that other circuit considerations take effect. In theory, we take the two extremes, when the $0.047 \mu \mathrm{~F}$ capacitor is in parallel with the $100 \mathrm{k} \Omega$ resistor and the $10 \mathrm{k} \Omega$ resistor is not effective, and when the capacitor is in series with the $10 \mathrm{k} \Omega$ resistor, the effect of the $100 \mathrm{k} \Omega$ resistor then being ignored. In practice, of course, it cannot be ignored: its real effect is to modify our $10 \mathrm{k} \Omega$ to $9 \mathrm{k} \Omega$ under these circumstances.
Taking the worked theoretical examples:
$\mathrm{f}_{\mathrm{t}}=\frac{1}{2 \pi \mathrm{CR}}=\frac{10^{6}}{6.28 \times 0.047} \times 10 \mathrm{k} \Omega$
and $\frac{106}{6.28 \times 0.047} \times 100 \mathrm{k} \Omega$.
(1) $=339 \mathrm{~Hz}$ and (2) $=33.9 \mathrm{~Hz}$

These figures agree very nearly with our practical measurements, This, from the curve of Fig. 78., gives us our Bass Lift circuit.

## Bass cut

If we now reverse the networks $R_{i n}$ and $R_{f b}$ as depicted in Fig. 77(c), we get an inverse of the previous curve. That is to say, we get bass cut instead of bass lift, because the feedback is now resistive, while the input circuit, up to the 'virtual earth point', is frequency-dependent.
Combining both these circuits, as in Fig. 79, we get bass cut and lift according to the position of the slider of the control. With the slider on the left, Cl is effectively short-circuited and we are left with
-continued on page 76

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QUITE a large number of letters addressed to us involve queries or seek information on the date or origin of bits and pieces of old wireless equipment or valves. So this month we thought that we would try to give some very broad indications of the form of construction and appear ance of domestic wireless sets at the interesting stage of their development. This should enable readers to date a piece of apparatus, if called upon to express an opinion, or if an interesting bit of gear is found in a junkshop.

## 㞒istory

From the turn of the century when Marconi was experimenting with the first tuned spark transmitter, until 1922 when the first official broadcast was made and valve circuits had been developed to the extent that they were no longer regarded as freak, the amount of equipment produced was comparatively small and that which remains is mostly in safe hands.
Once broadcasting had begun the boom in home constructed receivers got under way very rapidly since there were few commercial receivers available at that time. It is this period from about 1922 until the mid-30's that is probably of most interest to
those who specialise in collecting vintage wireless equipment and with which we will concern ourselves here.

## Components

There were many firms supplying components such as coils and holders, tuning condensers, audio transformers and valves as well as ebonite pancls and associated hardware. Basket-wound or wave-wound coils were frequently home-made and plugged into holders which were adjustable from the panel to vary the coupling between the coils. Resistors looked like cartridge fuses and were pushed in to clips. The grid-leak was often changed to suit the 'softness" of the detector valve or it might be a panel-mounted variable resistance.
'Spaghetti' resistors had the resistance wire wound on a flexible core and looked like a piece of string with end tags. These could be connected directly between terminals of components. Most components such as audio transformers, valveholders and condensers etc. had terminals, usually 6BA, often with a soldering tag. Scts of this period were characterised by the great effort that went into the wiring up.


Square sectioned copper wire was common, always arranged with neat corners or angles and straight parallel runs and neat loops under the terminals. The need for short, direct wiring was not appreciated then, and indeed, was probably of little importance where only medium and long waves were concerned and stage gains were very low.

## Construttion

Such receivers were built on a wooden baseboard to which the components were fixed with woodscrews and an ebonite panel was fixed to one edge of the board. Along the back edge was a row of terminals, mounted on a strip of ebonite, for connecting the set to the accumulator, high tension battery, grid bias battery, aerial and earth and headphones or speakers. Incidentally, the cabinets for these sets were also given a great deal of attention and often were works of art in themselves to ensure that they fitted in with the rest of the furniture. Indeed, the receiver was often built in to an existing piece of furniture. The panels of sets of this period were a mass of knobs and controls with possibly a rheostat for each filament, variable grid-leaks, tuning condensers for each stage, coil coupling controls and reaction controls. Later, when shorter wavelengths were in use, metal panels were employed in order to prevent 'hand capacity' effects which upset the rather critical tuning.

## Gallues

Valves can be dated fairly accurately from a study of their physical characteristics. At the beginning of the period we are discussing, say 1922-24, the Marconi-Osram $R$ valve was common along with the Mullard ORA and the Cossor Pl all of which were bright emitters with tungsten filaments. Generally they had a metal sleeve base and a pinch on top of the glass envelope, formed during the evacuation process. 1924-25 saw the introduction of the dull emitter valves using oxide-coated filaments such as the MO DE5, Mullard DO6 and the Cossor WR1. These valves still had the pinch on top but the bases were the more familiar moulded type.
Between 1925 and 1927 saw the advent of the now famous Mullard PM range of valves which were dull emitters with filament voltages from two to six volts. The pinch was now concealed in the base of the valve thus eliminating a very vulnerable feature of the older valves.

The first 'mains' type valves emerged in 1927 with the heaters, usually four volts, being run from a mains transformer instead of accumulators or batteries. In the early 30 's r.f. type valves appeared with sprayed-on metallic coating for screening purposes and the glass envelopes, especially for the audio amplifier valves, developed a waisted section at the top of the envelopes intended to support the mica discs of the electrode assembly and thus reduce any tendency to microphony.

For those that are really interested in these old radios there is no finer pastime than trying to get one of them to work even if it means using equivalent modern components as replacements for faulty parts. Our CQ column is open to those readers who wish to appeal to other readers for old components if it is felt that only a $100 \%$ genuine vintage receiver is acceptable.

## TRANSISTOR CIRCUITRY FOR BEGINNERS-

the effective bass lift circuit of Fig. 77(b). With the slider to its right we get the alternative condition, with C2 short-circuited and the bass cut circuit of Fig. 77(c).

## Balance

Take the case of the slider at its middle position. Then, the input and output circuits are identical and balanced. That word, BALANCED is important. It is the basis of the Baxandall tone control circuit-one of the most elegant solutions to an audio problem yet posed, and not to be under-rated. In the full circuit, the impedance change with the slider control moved (a change in frequency-dependence, looked at in the basic way of our approach) is exactly balanced with the movement of the slider in the other


Fig. 80: The eventual network to be inserted in the feedback loop, giving bass and treble Iff and cut.
section of the ganged potentiometer. It remains only that the ganged potentiometers themselves shall be within at least 1 dB of linearity.


Fig. 81: The basic amplifier circuit over which the feedback /s app/led.

From the simple experiments we have already carried out, we know that when the input resistance, $\mathrm{R}_{1 \mathrm{n}}$ is equal to the feedback resistance $\mathrm{R}_{\mathrm{fb}}$, then the theoretical gain is unity. In practice, findings are not far removed from the theoretical. At intermediate positions of the sliders, we shall get variations from the theoretical norm, between maximum bass and maximum cut.

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|  |  | $10 \mathrm{~mA} \quad . .$. |
| 1 |  | $50 \mathrm{~mA} \quad . . .282 .50$ |
|  |  | 100 mA .... 82.50 |
|  |  | 500 min . . . 22.50 |
|  |  | $\begin{array}{ll}11 \text { amp... . . . } & \text { 82-60 } \\ 8 \text { amp... }\end{array}$ |
|  |  | 10 amp....... . 42.50 |
| S0MA | 52.75 | 5V. D.C. $\quad .8250$ |
| $50-0-50 \%$ A | 28.70 | 105. D.C. . 22.50 |
| $100 \mu \mathrm{~A}$, ${ }^{\text {a }}$ | 82.70 | 20v. D.C. . 88.50 |
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| $200 \mu \mathrm{~A}$ | 82.70 | 300 V . D.C. 28.50 |
| $800 \mu \mathrm{~A}$ | 22.65 | 1sV. A.C. . - 22.75 |
| 1 mA | 28.50 | 300 V . A.C. .. 28.75 |
| 8 ma | 22.60 | VU Meter . . 28.00 |

Type SD. $64063.5 \mathrm{~mm} \times 85 \mathrm{~mm}$ Fronts \begin{tabular}{ll|lll}
50 uA \& $\ldots .$. \& $28 \cdot 60$ \& 800 mA \& 28.85 <br>
$50-0-50 \mu \mathrm{~A}$ \& 28.55 \& $1 \mathrm{mmp} . . . .$. \& 28.85

 $100 \mu \mathrm{~A}$ 

$100-0-100 \mu i$ \& 22.55 \& 5 amp.. <br>
\hline 10 map
\end{tabular} $200 \mu \mathrm{~A} \quad 10 \mathrm{mmp}$ $500 \mu \mathrm{~A}$ $\lim _{\sin A} A$

${ }_{10 \mathrm{~m} A}^{\sin A}$
10 mA
50 mA 100 mA

| 100 mA | 22-35 | $\checkmark$ U Seter | 22.70 |
| :---: | :---: | :---: | :---: |
| Type SD. $46046 \mathrm{~mm} \times 59.5 \mathrm{~mm}$ Fronts |  |  |  |
| $50 \mu \mathrm{~A}$ | 22.40 | 1 mmp | 22.15 |
| $50-0-50 \mu \mathrm{~A}$ | E2.85 | 5 amp | 28.15 |
| $100 \mu \mathrm{~A}$ | 22-36 | 10 mbip | 22.15 |
| 100-0-100 $\mu \mathrm{A}$ | E2.85 | $5 \mathrm{~V} . \mathrm{D.C}$. | 28.15 |
| $200 \mu \mathrm{~A}$ | 22.85 | 10v. D.C. | 22.15 |
| $500 \mu \mathrm{~A}$ | 28.20 | 20 V. D.C. | 28.15 |
| 1 mA | 22.15 | 50 V . D.C. | 22.15 |
| 5 mA | 28.15 | 300 V. D.C. | 22.15 |
| 10 mA | 28.15 | 15\%. A.C. |  |
| 50 mA 100 ma | 28.15 28.15 | 300 V . A.c. | 22.80 28.80 |
| 500 ma | 28.15 | VU Meter | 22-85 |

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|  | 1 atup. A.C. 28.15 |
| 1-0-1mA . . 22.15 | B amp. A.C. * 28.15 |
| $5 \mathrm{~mA} \cdot \cdots \cdots{ }^{28.15}$ | 10 mpp A.C. 28.15 |
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| 50 mA . ${ }^{\text {c... } 28.15}$ | 30 mup . A.C. 22.15 |
| 100 mA ... 22.18 | 50 amp A.C. ${ }^{\text {e }}$ ¢ 2.15 |
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overload protection $0 / 60 / 1.200 \mathrm{~V}^{\prime}$ D.C. $0 / 8 / 30 / 120 / 600 /$ <br>
1000 A <br>
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\end{tabular} $1,200 \mathrm{~V}$ A.C. $0 / 30 \mu \mathrm{~A} / 6 \mathrm{~mA} /$

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$16 / 450 \mathrm{~V}$ \& $15 p$ \& $1000 / 50 \mathrm{~V}$ \& 47 p \& $32+88 / 450 \mathrm{~V}$ <br>
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$32 / 450 \mathrm{~V}$ \& 20 p \& $8+8 / 450 \mathrm{~V}$ \& 18 p \& $850+50 / 825 \mathrm{~V}$ \& 50 p <br>
$25 / 25 \mathrm{~V}$ \& 10 p \& $8+16 / 450 \mathrm{~V}$ \& 20 p \& $82+88+32 / 850 \mathrm{~V} 48 \mathrm{p}$
\end{tabular} $30 / 50 \mathrm{~V}$ V $10 \mathrm{D} \mid 18+16 / 450 \mathrm{~V} \quad 25 \mathrm{D}) 100+50+50 / 350 \mathrm{~V} 48 \mathrm{p}$ $100 / 25 \mathrm{~V} \quad 10 \mathrm{p} 32+32 / 850 \mathrm{~V} \quad 25 \mathrm{D}$

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Fane Crescendo $15^{m} 8$ or is ohm Fane Crescendo $15^{\prime \prime} 8$ or 15 ohm
Fane Crescendo $12^{\prime \prime} 8$ or 15 ohm Fane $8^{\prime \prime} \mathrm{d} /$ cone 808 T 8 or 15 ohm Fane $8^{\prime \prime}$ d/cone, roll surr. 807T 8 or 15 ohm
Baker Group 253.8 or 15 ohm Baker Group 35, 3, 8 or 15 ohm 8aker De Luxe $12^{\prime \prime}$ d/cone Baker Major
EMI $13 \times 8$ 3, 8 or 15 ohm
EMI $13 \times 8$ type $150 \mathrm{~d} /$ cone $3 ; 8$ or 15 ohm
EMI $13 \times 8$ cype $400 \mathrm{k} / \mathrm{tw} 3,8$ or 15 ohm
EMI $13 \times 8$ type 3508 ohm
EMI $6 \frac{1}{1}{ }^{\prime \prime} 938504$ or 8 hm
Elac $9 \times 5$ 59RMLO9 15 ohm
Elac $9 \times 5$ 59RMLL4 8 ohm
Elac 6t" d/cone 6RM220 8 ohm ...
Elac $6 \frac{1^{\prime \prime}}{}{ }^{\circ}$ d/cone, roll surr. 6RMI7I 8 ohm
Elac 4" tweeter TW4 8 or is ohm Celestion PS8 for Unilex
Celestion MFL000 25 watt horn
8 or 15 ohm
Elac $5^{\prime \prime} 3$ ohm
Elac $7^{\prime \prime} \times 4^{\prime \prime} 3$ or $\ddot{8}$ ohm
Elac $8^{\prime \prime} \times 5^{\prime \prime} 3,8$ or 15 ohm
Wharfedale Bronze 8 RS/DD
Wharfedale Super 8 RS/DD
Wharfedale Super 10 RS/DD
Wharfedale Super 10 RS/DD
Goodmans 8P 8 or 15 ohm
Goodmans 8P 8 or 15 ohm
Goodmans 10 P 8 or 15 hm
Goodmans 10P 8 or 15 ohm
Goodmans 12 P 8 or 15 ohm
Goodmans 15 P 8 or 15 hm
Goodmans 18P 8 or 15 hm
Goodmans Twinaxiom 8 .
Goodmans Twinaxiom 10
Goodmans Axent 100
Eagle DT33 dome tweeter 8 ohm
Eagle HTIS tweeter 8 ohm
Eagle MHT tweeter 8 ohm
Eagle MHIO tweeter
Eagle MHTIO tweete
Eagle CTIO tweeter
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612.26
610.17
10.17
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66.00
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66.00
87.50
67.50
69.62
69.62
67.50
67.50
62.25
42.58
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62.80
62.53 62.53
62.53
62.59
$2 \cdot 59$
63.22
61.21
$+2.16$

### 610.45

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Richard Allan $12^{\cdots "}$ d/cone 3 or
15 ohm
Richard Allan $8^{\prime \prime} 3,8$ or 15 ohm $10^{\prime \prime} \times 6^{\prime \prime} 3,8$ or 15 ohm
$8^{\prime \prime} \times 5^{\prime \prime} 3$ or 8 ohm
$7^{\prime \prime} \times 4^{\prime \prime} 3$ or 8 ohm
$3^{\prime \prime} 8 \mathrm{ohm}$ or 80 ohm
$21^{\prime \prime} 64$ ohm
peaker matching oransformer 3.
8 or 15 ohm $10 \cdots 10$ watt 8 or
dastra Hiten 10 ...
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| 2N1302 | 0.17 | ACY21 | 0.80 | BF195 | 0.14 |
| 2－1303 | 0.17 | 10Y22 | 0.10 | 13F゙196 | 0.12 |
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| 2N1309 | 0.25 |  | 1.25 | Brw9 | 0.20 |
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| 2Ni711 | 0.20 | AF115 | 0.17 | 13 FY 17 | 0.40 |
| 2N1756 | 0.75 | AFl16 | 0.17 | 13 Frl 9 | 0.25 |
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| 2）2217 | 0.25 | AF＇128 | 0.20 | Brys | 0.20 |
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| 2S2369A | 0.15 | Al－181 | 0.35 | BSY28 | 0.17 |
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| 2N3134 | 0.25 | A8Z16 | 0.70 | 0 C 36 | 0.45 |
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TE20D RF Gase 10.50 . $120 \mathrm{KHz}=500 \mathrm{MHz} \subset 15.95$. Carr 3 Sp TE22D Audio Generator $20 \mathrm{~Hz}_{\mathrm{z}} 200 \mathrm{KHz} \mathbf{1 1 7} 50$. Carr. 35p $\begin{array}{ll}\text { Cl.5 } & 3^{-} \text {Pulse } \$ c o p e ~ \\ \text { Clo Hz- } 10 \mathrm{mHz} & 639.00 \text {. Carr. } 50 \mathrm{p}\end{array}$ TE65 Valve Voltmeter 28 ranges $\mathbf{4 1 7 . 5 0 \text { . Carr. } 4 0 p}$ ALL NOMBREX MODELS IN STOCK

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A popular VHF FM Tuner for quality
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yds. Ideal remote switching yds. Cideal remote switching data and new I.C. circuits. E5-90 per pair. Post 10 p .
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${ }^{2} 7^{\prime}$ High Impedance $\quad \mathbf{~} 2.00$ $\begin{array}{lr} & 17 \text {. High Impedance } \\ \text { '18. Med. Impedance } & E 2.00 \\ & 63.50\end{array}$ ${ }^{\circ}$ 18' Med.-Low Imp. $£ 3.50$ Erase Heads for abo
$63^{\prime} 2$ track mono-
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VATPrices DO NOT include Value Added Tax. From ist April, 1973 10\% must be added and shown separately to your total order (inclusive Post/packing). Help us to help you receive your order without delay.


[^0]:    Prices shown are recommended retai excluding $V$ AT
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[^1]:    poly-planar 20-Watt Full Range Speaker Completely replaces the conventional cone speaker Super-thin construction
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[^2]:    
    The June issue, on sale May 4th, will include a new easy competition to win a Digital Multimeter, a special feature on what to look for when buying Hi-Fi Equipment, and "Special Valves in Electronics', plus the usual abundance of constructional projects.

    Further details on page 48.

[^3]:    Because superregenerative receivers are notorious for their radlation it is strongly recommended that the pre-ampllfier be fitted as an essentlal part of the recelver. Complete screening, as descrlbed by the author, is very important.

[^4]:    * texas instruments limited

[^5]:    aEmeral porpose mioh staglity
    TRANSISTOR PRE-AMPLIPIER
    For P.U. Tape, Mike, Guitar, etc. and suitable for use with ralve or transistor equipment 9-18\%. battery or from 11.T. Ine $200 / 300$. Frequency
    
    
    FANDROOK OF TRANSISTOR EQUIVALENTS AND
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    VAT.
    Prices in this advertisement (incl. $p$. and p.) will be aubl
    1st Aprij, 1973.

[^6]:    AUTOMATIC EMERGENCY SUPPLY
    250 w 50 Hz - 150 watt Inverter, Full kit of parts excluding meter. Clicult at appeared In December P.W. Complete kit-fi6. $95+80 \mathrm{p}$ P. \& P

    OTHER INVERTERS AVAILABLE IN KIT FORM
    150 Watt- $13 \cdot 50+60$ p P. \& P.
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    40 Watt- $£ 5 \cdot 20+40 \mathrm{p}$ P. \& P. 25 Watt-62 $60+20 \mathrm{p}$ P. \& P.
    All above operate from $\mathbf{1 2 v}$. battery and give $250 \mathrm{v} .-50 \mathrm{~Hz}$. Output. 24 volt types are also avallable, atternative outputs or taps can be suppiled. Transformers and/or Transistors can be supplled separately. SPECIAL OFFER
    12v. Fluorescent lights, suifable for tents, caravans, houses or secondary lohiling for factorles, hotels, ete. 12 inch- 8 watt- $\$ 3.40$ post paid. 21 Inch- 13 watt- $84 \cdot 20$ post pald. harge discounts avaliable for quantities.

[^7]:    U.K. ADD VAT TO ORDER TOTAL

    MICROCIRCU1TS: $70928 p ; 71036 p ; 72357 p$ $741{ }^{28 p}: 748$ 37p: PA230 70p; SL402A £ $1 \cdot 00$
    FET Op.Amp. 1.62 TRANSISTORS: $2 N 696$ 14p: 2N697 14p: 2N7C6A 11p; 2N1613 16p 2N1711 16p: 2N2218 19p; 2N2219 19p: 2N2219A
    19p; 2N2904 17p; 2N2926 RED 6p: ORANGE 19p; 2N2904 17p; 2N29\%6 RED 6p; ORANGE
    
     $\begin{array}{ll}\text { 2N } 3709 & \text { 8p; } \\ \text { 2N4059 3p } & \text { 2N4061 } \\ \text { 2N; }\end{array}$ 2N4059 9p: 2N4061 11p: 2N4062 11p: ACl07 28p
     AFl16 14p; AF117 14p; AF124 22p: BCl07A 7p
    BC10iB 8p; BC108A 8p; BC108B 8p; BC108C
    
    
    
     BSX20 12p: OC4 $12 \mathrm{p}:$ OC45 12p: OC71 12p
    OC72 12p: OC81 18p: OC83 240: ME SERIES AVAILAB: 12 LE RECTIFIERS: 1 AMP: 50 V 3 1 D 100 V 4p: $200 \mathrm{~V} 44 \mathrm{p} ; 400 \mathrm{~V}$ 5p: 800 V 6p: 1000 V
    $7 \mathrm{D} . \mathrm{ZENERS}$ BZ Y88 SERIES $2 \cdot 7 \mathrm{~V}$ to 33 V 8p 7p. ZENERS BZY88 SERIES $2 \cdot 7 \mathrm{~V}$ to 33 V 8 P each. DIODES 1N916 4p; OA90 6p; OA200 7p; OA202 8D. SCR IR122D (400V 5A) £1.14: LED PANEL LAMP WITH BUSH AND DATA
    400 . CARBON FILM WW $5 \%$ RESISTORS E12 values 22 to 2.2 M 10 EACH or 70 Der 10 Yalues 22 to $2 \cdot 2 \mathrm{M}$ 1p EACH or 7 D per 10 of FIBRE TIP PEN 80p. MINIATURE METAI FIBRE TIP PEN 80p. MINIATURE METAL THERMISTOR 9p. 2N3819 26p. TESTED TRANSISTOR CIRCUITS BOOKLET $40 p$
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