PRACTICAL WIRELESS

FEBRUARY 1972

20p

Hilliam Quality 88888 6

TRANSISTORISED 'SCOPE

THE SOUND

COMPLETELY NEW DESIGN FURTHER IMPROVED IN BOTH APPEARANCE and PERFORM-



OF QUALITY

REPRESENTING VALUE FAR HIGHER THAN THE PRICES SUGGEST.

SUPER 30 Mkul HI-FI STEREO AMPLIFIER

9 0

Only high grade components by leading manufacturers. COMPLETE KIT OF PARTS

Or FACTORY BUILT £33.75 with 12 months guarantee £33.75 Dep. £5.75 and 9 monthly paymnts (Total £37.25)

Or FACTORY BUILT in Teak finished case as illus. Dep. £6 and 9 monthly payments £3·86 £37·75 (Total £40·74)

PRINTED CIRCUITRY, TWENTY SILICON TRANSISTORS. FOUR DIODES, FOUR RECTIFIERS. TECHNICAL DETAILS (Applying to each channel where appropriate) CONTROLS: PUSH-BUITON SELECTOR (1) Disc (2) Radio (3) Tape (4) Mono L (5) Mono R (6) SPEAKER DIS. (7) Mains on/off. Bass, Treble, and Balance. Plus Ceramic/Mag P.U. Switch. OUTPUT: 15 watts R M.S. (Continuous) into 8 ohms. 10 watts R M.S. (Continuous) into 15 ohms.

SATIN SILVER METAL FACIA with black letter

SATIN SILVER METAL FACIA with black letter ing. Black edged knobs with bright silver centres. PUSH-BUTTON SELECTOR SWITCHING NEON INDICATOR JACK SOCKET FOR HEADPHONES. CABINETED MODEL VENEERED IN SATIN TEAK. SUITABLE FOR ANY MODERN PICK-UP CARTRIDGE CERAMIC or MAGNETIC, REGARDLESS OF PRICE.
WE RECOMMEND USE WITH THE BEST ANCILLARY EQUIPMENT THAT CAN BE AFFORDED.

HUM & NOISE — 75dB Min. Vol. —65dB Full Vol. FREQUENCY RESPONSE: —3dB 7Hz to 70kHz TREBLE CONTROL: +16dB to —12dB at 14KHz CROSS TALK —58dB SASS CONTROL: +17dB to —16dB at 40Hz CROSS TALK —58dB SENSITIVITIES: Disc Mag. 2:5mV. Ceramic 35mV. Radio 120mV. Tape 120mV. REAR PANEL SOCKETS ARE FOR 3 PAIRS OF INPUTS (1) P.U. (2) Radio. (3) Tape Amp. Plus pair for tape recorder signal take off and 2 pairs for speaker connections. connections

RSC G66 MkII 6+6 Watt HIGH QUALITY STEREO AMPLIFIER



RSC SUPER 30 M

rating I.H.F.M. Frequency range 20-20,000 c.p.s. Bass Control ± 12bB. Treble Control ± 13dB. Selector switch for P.U. or Tape/Radio. For loudspeaker output impedances of 3 to 15 ohms. For standard 300,250y. 4 C. mains operation. Attractive Black and Silver standard 200-250v A.C. mains operation. Attractive Black and Silver finished metal facia plate and matching knobs.

COMPLETE KIT OF PARTS INCLUDING FULLY WIRED PRINTED CIRCUIT Carr. 40p

£12-50

Comprehensive wiring diagrams and instructions Or FACTORY BUILT IN TEAK VENEERED CABINET as illust or dep. £3.20 and 9 mthly pymnts £1.70 (Total £18.50).

Or in Teak veneer housing £23 Dep. £3 & 9 mthly payments £2.55 (Total £25.95). Send S.A.E. for leaflet

FANE 807 HIGH FIDELITY LOUDSPEAKER

A full range 8in. 10 watt unit for excellent sound quality, in suitable enclosure. Cast chassis Roll P.V.C. cone surround and long throw voice coil to achieve very low fundamental resonance of 30 c.p.s. Tweeter cone is fitted to extend high note response. Frequency range 25 Hz to 15 KHz.

Gauss 10,000. Impedance 3 or 8-15 \(\Omega\$ Please state impedance when ordering \)

43-50





HI-FI SPEAKER ENCLOSURES

Modern design. Teak veneer finish. Acoustically lined All sizes approx. Carr. 30p. per enclosure. JE8 Size 16 x 11 x 9in. Pressurised, Gives pleasing results with any 8in. Hi-Fi speaker. SE8 For optimum performance with any 8in. Hi-Fi 'speaker. Size 22 x 15 x 9in. £6.47

Ported SE10 For outstanding results SE12 For excellent performance with 10in. Hi-Fi 'spkr £6.74 with 12in. Hi-Fi speaker £7.87 Size 24 x 15 x 10in. P'td. £6.74 and Tweeter. Size 25x16x10½



R.S.C. TA12 MKIII 6.5 + 6.5 WATT

STEREO AMPLIFIER FULLY TRANSISTORISED

SOLID STATE CONSTRUCTION HIGH FIDELITY OUTPUT OF 6.5 WATTS PER CHANNEL

Designed for optimum performance with any crystal or ceramic Gram. Designed for optimum performance with any crystal or ceramic Gram-P.U. cartridge. Radio tuner, Tape Recorder, etc. *\(3\) separate switched input sockets on each channel *\(5\) Separate Bass and Treble controls \$\) Slide Switch for mono use \$\(5\) Speaker Output 3-15 ohms \$\) For 200-250v. A.C. mains \$\(5\) Frequency Response 20-20,000 c.p.s. —2dB \$\) Harmonic Distortion 0-3% at 1,000 c.p.s. Hum and Noise —70dB \$\(5\) Sensitivities (1) 50mV (2) 400mV (3) 100mV. Output rating 1.H.F.M. Handsome finish Facia plate \$\(6\) (monotonic technique for the first WITH FULL WIRING DIAGRAMS & INSTRUCTIONS.

12 mths grarantee \$\(19\) 19-50 or Dep. \$\(23\) & 9 mthly pymts \$2-15\$ (Total \$22-85)-10 (Total \$22-85)-10 (Total \$23-85)-10 (Total \$23-85)-

AUDIOTRINE HI-FI SPEAKER SYSTEMS

Consisting of matched 12in. 11,000 line 15 Watt 15 onth high quality speaker, cross-over unit and tweeter. Smooth response and extended frequency range ensure surprisingly realistic reproduction.

OR SENIOR 15 WATT INCLUDING

66.75 Carr.
35p Consisting of matched 12in. 11,000 line 15 Watt 15 ohm HF126 15,000 LINE SPEAKER



AUDIOTRINE HIGH FIDELITY LOUDSPEAKERS



Heavy construction. Latest high efficiency ceramic magnets. Treated Cone surround. "D" indicates Tweeter Choic providing extended frequency range up to 15,000 c.p.s. Impedance 3 or 8-15 ohms. PLEASE STATE CHOICE. Excellent performance at low cost.

HF808T 8" 10W £2.88 HF120D 12" 15W £4-75 HF102D 10" 10W £3-40 HF120 12" 15W £4-25 HF126 12" 15W £5:50 HF126D 12" 15W £5-90

R.S.C. All HI-FI 12-14 WATT AMPLIFIER

PUSH-PULL OUTPUT. Two input sockets with sep. vol. cor S.A.E. for leaflet



High sensitivity, 5 valves. Bass and treble controls. Response ± 3dB 30-20,000 e s. Hum level -60dB Sensitivity 40 millivolts. For Crystal or Ceramic PUs. High Impedance mikes". For Musical Instruments etc. Std. AC mains. For 3 & 15 dbm spkrs. Complete kit. Full instructions and point-to-point £10.50 carr. wiring diagrams.

Twin handled metal cover £1.75

FACTORY **£14.75** or Dep. **£3** and 9 monthly BUILT pymts of £1.60 (Total £17.40).

FANE PRESSURE TWEETER

Model 303 Gauss 10,000. Impedance 3 ohns or 8-15

ohms ohms. Excellent £2.50 value

l'ost Free

SPECIAL

WHARFEDALE UNIT '3' SPEAKER KITS

£10·50 £12.53 Carr. 25p.

* DEMONSTRATION FACILITIES AT ALL BRANCHES



R.S.C. TA6 6 Watt HI-FI 200-250v. AC SOLID STATE AMPLIFIER operated.

Frequency Response 30-20,000 c.p.s. -2dB. Harmonic Distortion 0.3% at 1,000 c.p.s. Separate Bass and Treble lift' and 'cut' controls. 3 input sockets for Mike, Grain, Radio or Tape. Input selector switch. Output for 3-15 ohm spkrs. Max. sensitivity 5hw. Output rating 1.1F.M. Fully enclosed enamelled case, 9\frac{1}{2} \frac{1}{2} \frac{1}{2

OR FACTORY BUILT WITH 12 MONTHS' GUARANTEE £9.75

R.S.C. PLINTHS



Superior Solid Natural for Record Playing Units cut for Garrard 1025, 2025, 3000, AT60, SP25 etc.

WITH TRANSPARENT £3.15 PLASTIC COVER £6.30

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HIGH-FIDELITY STEREO PACK

Four fully wired units ready

'plug in'.

★ SUPER 30 AMPLIFIER (15 + 15) in veneered housing

watt) in veneered housing

GARRARD SP25 MK III

table on Plinth with cover

GOLDRING CS90 Ceramic Pickup Cartridge with diamond stylus

PAIR OF STANWAY II Speaker

Living

Units
Special Total Price
Carr. £1.50

Terms: Deposit £12 and 9 monthly
payments £8.55 (Total £88.95).

★ Super 30 Amplifier (15 + 15 watt)

★ Super 30 Amplifier (15 + 15 watt)
in veneered housing
Goldring GL69 II Transcription
Turntable on Plinth as illustrated
★ Goldring Magnetic P.U. Cartridge.
★ Pair of Stanway II 597.75 £1.50
Special Total Price
Terms: Deposit £15 and 9 monthly
payments £10.53 (Total £114.55).

Pair



Matching as recommended for optimum performance.

Package prices apply providing all individual units are purchased from any branch within 3 months. See leaflet.

TA12 AMPLIFIER 6.5 6.5 watt in veneered

★ GARRARD SP25 MK III Player

★ GARKARD 5725 MR III Flayer
unit on Plinth
★ GOLDRING CS90 Ceramic P.U
Cartridge with diamond stylus
★ PAIR OF DORCHESTER

Loudspeaker Units Special Total Price

Or Deposit £7.15 and 9 monthly payments £6.35 (Total £64.30). Carr. £1.25 Trans. Plastic Cover £3.15 extra.

PACKAGE AS ABOVE but with Garrard 3000 Autochanger and Sonotone 9TA Ceramic Cartridge in lieu of SP25 and CS90 Carr. £1.25

Or Deposit £6 and 9 monthly payments £5.70 (Total £57.30)

Trans. Plastic cover £3:15 extra.

HIGH FIDELITY **SPEAKER**

Cabinets latest style Satin Teak veneer. Acoustically lined or filled acoustic damping. Ported where appropriate. Credit terms available.



DORCHESTER (Illustrated) Size appr. Range 45-15,000 c.p.s. Rating 8-10 watts. Fitted High flux 13 × 8in. Dual Cone speaker. Imp. 3 or 15 ohms.

STANWAY II Size $20 \times 10^{\frac{3}{4}} \times 9^{\frac{3}{4}}$ in. approx. Rating 10 watts. Inc. 13×8 in. speaker with highly flexible cone surround, long throw voice coil and 10,000 line magnet. High flux tweeter. Handsome Scandinavian design cabinet. Range 35-20,000 c.p.s. Imp. 8 ohms. Gives \$17.85 smooth realistic sound output. See 'package offers' for above illustration

UNITS 'YORK' HIGH FIDELITY **3 SPEAKER SYSTEM**

★ Moderate size only 25×14×10in.

* Response 30-20,000 c.p.s. Impedance 15 ohms * Performance comparable with units costing

considerably more.

Considerably more.

Consists of (1) 12in. 15 watt Bass unit with cast chassis. Roll rubber cone surround for ultra low resonance, and ceramic magnet. (2) 3-way quarter section series cross-over system (3) 8 × 5in. high flux middle range speaker. (4) High efficiency tweeter. (5) Appropriate quantity acoustic damping material. (6) Handsome Teak veneered cabinet. (7) Circuit and full instructions. Terms: Dep. £4·60 and 9 monthly payments £2·47 (Total £26·83).



COMPLETE

Carr. 65p

DEMONSTRATIONS AT ALL BRANCHES

Complete kit £3.25 Assembled

AUDIOTRINE A55 HIGI

5 + 5 WATT OUTPUT

Garrard 5200 Changer with low mass pick-up arm and Stereo Cart-ridge. Controls: TREBLE, BASS, VOLUME, STEREO, BALANCE. Operation on 200-250v. A.C. mains. Output rating J.H.F.M.

Luxurious Teak Veneer Finished Cabinets. Silver finished facia plate and matching control knobs.







Transparent plastic (tinted) included for main unit.
PAIR OF LOUDSPEAKERS incorporating high flux 8in. 5in. speaker. Size approx. $13 \times 7\frac{1}{2} \times 8\frac{2}{3}$ ins. PRICE COMPLETE

ONLY

R.S.C. BATTERY/MAINS CONVERSION UNITS

Carr. £1 · 25

Terms: Deposit £5.50 and 9 monthly payments £4.50 (Total £46).

TYPE BM1. An all-dry battery eliminator. Size $5\frac{1}{2} \times 4\frac{1}{2} \times 2$ in approx. Completely replaces batteries supplying 1.5v. and 90v. to battery radio where A.C. mains 200/250v. 50c/s is available.

ready for use

A REALLY SURPRISING STANDARD OF QUALITY IS OBTAINED FROM THIS COMPACT LOW PRICED SYSTEM

LF CHOKES and RECTIFIERS RSC TRANSFORMERS. FULLY GUARANTEED. Impregnated and Interleaved where necessary Primaries 200-250v, 50c/s. Screened MIDGET CLAMPED TYPE 24×24×24in. 250v., 60mA, 6.3v. 2a 250-0-250v., 60mA 6.3v 2a 99p £1.05

230-0-250v, 60mA 6.3v 2a £1-05
PULLY SHROUDED UPRIGHT MOUNTING
250-0-250v, 60mA, 6.3v, 2a, 0-5-6.3v, 2a. £1-40
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300-0-300v, 100mA, 6.3v, 4a, 0-5-6.3v, 3a. £2-20
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FOR Mullard 510 Amplifier £2-45
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425-0-425v, 200mA, 6.3v, 4a, 0, 6.3v, 3a. £2-65
425-0-425v, 200mA, 6.3v, 4a, 6.3v, 3a, 5v, 55-10

3a 450-0-450v. 250mA, 6.3v. 4a., c.t., 5v. 3a. £5-50

FILAMENT or TRANSISTOR POWER PACK Types 6.3v. 1.5a. 49p; 6.3v. 2a. 54p; 6.3v. 3a. 76p; 6.3v. 6a. £1-30; 12v. 1a. 55p; 12v. 3a. or 24v. 1.5a.£1-35;0.9-16v. 1ja.£1-10;0-12-26-42v. 2a.£1-76 CHARGER TRANSFORMERS 0-9-15v. 1a. 99p; 24a 21-10; 3a. 21-25; 5a. 21-45; 5a. 21-05; 5a. 22-00 AUTO (Step UP/step DOWN) TRANSFORMERS 0-110/120v. 2:00-230-250v., 50-80 watta 21-10; 100 watta 21-00 250 watta 22-75; 500 watta 25-75

150 watts, £1-90 250 watts zz-70; 500 watts zc-70; 000 TPUT TRANSFORMERS Standard Pentode 5,000 Ω or 7,000 Ω to 3 Ω Push-Pull 8 watts EL84 to 3 Ω or 15 Ω . Push-Pull 10 watts 6V6, ECL86 to 3, 5, 8 or 15 Ω .

15 Ω 12 waste ave, ELLSG to 3, 5, 8 or
15 Ω 21.87
Push-Pull EL84 to 3 or 15 Ω 10-12 watts . 21.35
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Push-Pull 15-18 watts, sectionally wound
61.6, KT66, etc., for 3 or 15 Ω 21.99
Push-Pull 20 watt high quality sectionally
wound EL34, \$L6, KT66 etc. to 3 or 15 Ω 23.30

You're never very far From COCENTRE! SMOOTHING CHOKES 150mA, 7-10H, 250 Ω 70p; 100mA, 10H, 200 Ω 60p; 80mA, 10H, 350 Ω 50p; 60mA, 10H, 400 Ω 25p. SELENIUM

with diagram.

RECTIFIERS F.W. (Bridged)

All 6/12v. D.C. Output. Max. A.C. Input 18v 1a. 25p, 2a 35p, 3a. 50p, 4a. 65p, 6a. 80p.

BRADFORD BLACKPOOL (AGENT) BIRMINGHAM DARLINGTON DERBY EDINBURGH GLASGOW HULL LEICESTER LEEDS LIVERPOOL LONDON MANCHESTER MIDDLESBROUGH NEWCASTLE-ON-TYNE NOTTINGHAM SHEFFIELD

SEE NEXT PAGE FOR TERMS OF BUSINESS, ADDRESSES etc.



DISCOTHEOUE **EOUIPMENT**

SAVINGS ON **PACKAGE OFFER**

- (1) FAL FG1/2 Console
- (2) 100W Power Amplifier
- (3) Pair High Quality Headphones (4) Matching Microphone fitted to Headphones
- (5) Pair 50W Speakers black rexine covered Size approx. 18" × 18" × 8"

£132 TOTAL COST OF ALL ILLUSTRATED UNITS

Carr. £2:50 Terms: Deposit £20 and 9 month monthly payments of £14.34 (Total £149.06).

BASS REGEN



A powerful high quality allpurpose unit for lead, rhythm, bass guitar, vocalists, gram., radio, tape. Peak Output rating. Loudspeaker unit optional horizontal or vertical mounting.

Two extra heavy duty 12in.

50 watt Loudspeakers.

Tour Jack inputs and two Volume Controls for simultaneous use of up to four pick-ups or "mikes".

★ Bass and Treble controls. Send S.A.E. for leaflet.

ONLY £60
Credit Terms Deposit

£16 & 9 mthly pymts Carr.£1.50 of £5.75 (Total £67.75) SEND S.A.E. FOR LEAFLET

30 WATT HI-FI **AMPLIFIER**

FOR GUITAR, VOCAL OR INSTRUMENTAL GROUP

A 4 input, 2 volume control Hi-Fi unit with Separate Bass and Treble controls.

Current valves. Peak output rating. Strong Rexine covered cabinet with handles. Attractive black/gold P.V.C. facia. Neon indicator. For 200-250v, A.C. mains. For 3 or 15 ohm speakers.



Carr. 65p

Terms: Deposit £3.70 9 monthly pay-of £2·10 (Total and 9 ments £22.60).

HEQUE CONSOLE

SEND S.A.E. FOR LEAFLET

TWIN TURNTABLE UNIT WITH MONITORING FACILITIES

£65 Cart.

Terms: Deposit £11 and 9 monthly payments of £6.70 (Total £71.80).

DISCO/GROUP EQUIPMENT PACKAGE OFFERS

Separate Volume Controls plus Treble & Bass Controls Microphone Socket with associated Switch & Vol. Control Incorporating twin Garrard SP25 Mk. III turntables and Goldring CS90 Ceramic Cartridges with diamond stylii. Size approx. 36" × 61" × 15".

Black Rexine covered Cabinet with lid. Fitted carrying handle.

F.A.L. PHASE 50 Mk.II AMPLIFIER PACKAGE PRICE PAIR FANE POP 25/2 25W L/SPEAKERS.

F.A.L. PHASE 50 Mk.II AMPLIFIER PAIR FANE POP 50 L/SPEAKERS OR PAIR L12/25 Cabineted Speakers

F.A.L. PHASE 100 AMPLIFIER PAIR L125 50W L/Speakers in cabinets.

F.A.L. PHASE 100 AMPLIFIER 4 FANE POP 50 LOUDSPEAKERS

£44 carr.

£49.50 carr.

£118 carr.

£99 carr.

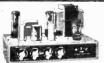
TERMS
Deposit £5.50 and 9 monthly payments of £4.72
(Total £47.98).

Deposit £10 · 50 and 9 monthly payments of £5 (Total £55-50)

Deposit £25 and 9 monthly

payments of £11-62.
(Total £129-58).
Deposit £15 and 9 monthly
payments of £10-52

(Total £109.50).



R.S.C. A10 30 WATT ULTRA LINEAR HI-FI AMPLIFIER Highly sensitive, Push-Pull high output, Hum level-70dB, Response

AUT LIFE A output, Hum level—70dB. Response
AddB 39.20,000 c/s. All high grade components, Valves BF86,
EF86, EC83, 807, 807, 6234. Separate Bass and Treble Controls.

Sensitivity 36 millivoits. For High Impedance microphones
for Clubs, Schools, Theatrest, Dance Halls, Outdoor Functions,
etc. For Electronic Organ, Guitar, String Bass, etc. Gram., Radio
or Tape. Two separate inputs with vol. controls permit such as "mike" and Pick-up etc. to be used
for mixing purposes, 200-250 v. 50 c/s A.C. mains. For 3 and 15 ohm speakers. Complete Kit of parts with wring diagram and instructions. Twin-handled perforated cover
\$1,90 Or factory built with EL34 output valves and 12 months' guarantee for £19-75

Carr, 65p

Carr, 65p TERMS: Deposit \$4 and 9 monthly payments of \$2.10 (Total \$22.90), Send 8.A.E. for leaflet.

MINIMUM 12 MONTHS GUARANTEE, LABOUR & MATERIALS (Excl. Valves) ON ADVERTISED GOODS

PHASE 50 MkI **50W AMPLIFIER**

OUTPUT Watts (Music) R.M.S

(Cont.) (Peak) 100

£33.50 65t

Terms: Deposit £6 and 9 monthly payments £3.50 (Total £37.50).

PHASE 100

100W AMPLIFIER OUTPUT 100 Watts (Music)

R.M.S (Cont.) I.H.F.M. Output rating

Terms: Deposit £12 and 9 monthly payments £6-25 (Total £68-25).

(Total 287-50). (Total 287-50). (Total 288-25). (Total 287-50). (Total 287-50). (Total 287-50). (Total 287-50). (Total 287-50). (Total 288-25). (Total 288-25

CABINET LOUDSPEAKERS

L13 8-10 WATTS

Incorporating high flux 13" × 8" 8-10 watt loudspeaker. Available with 3 or 15 ohm impedance. (State when ordering.) Cabinet finished in Teak or Afformsis Vaner ak or eneer. (Carr. 371p) £5-25 finished in Teak or Afrormosia Veneer.



L12/25 25 WATTS

12° 25 watt heavy duty loudspeaker. Impedance 15 ohms. 18° × 18° × 8° approx. Veneered or Rexine/Vynair finish. Suitable small Discotheques. Clubs, Schools (Carr. 45p).

Terms: Deposit #3 and 9 monthly payments 21 (Total 212)

B4/100 100 WATTS

Fitted four extra heavy duty 12" 14,000 Gauss 50 watt speakers for conservative rating of 100 watts. Impedance 15 ohms. Cabinet in \(\frac{2}{3}\)" ehipboard with centre reinforcement back to front. Rexine/Vynair covered. Acoustically filled and pressurised. 27" \times 27" \times 14" approx. Ideal for bass guitar or electronic organ.

Or Deposit £8 and 9 monthly payments £5.90 (Total £61.10).





Or Deposit

L125 50 WATTS

Incorporating two 12" 50 watt 14,000 Gauss extra heavy duty loudspeakers for conservative rating of 50 watts. Impedance 8-15 ohms. watts. Impedance 6-15 onms.
Sturdy pressurised cabinet
in \(\frac{q}{r} \) chipboard. Rexine/
Vynair Covered \(31^r \times 20^r \)
\(\times 16^r \) approx. Suitable
Vocal or Instrumental
Groups. Bass Guitar or
Electronic Organ, etc. For Electronic Organ, etc. For theques, Clubs, etc.

(Carr. £1.50)



FAL DUO/100

Employing two FANE
'CRESCENDO 12' 100 watt, super
efficient, high flux, high power,
full range speakers. Gauss 20,000.
ULTRA HIGH SENSITYUTI
Ideal for Vocalists and Instrumental

Ideal for Vocalisis and Instrumental Groups.
Frequency Range 30—16,000 c.p.s. Impedance 8 ohms.
Cabinet constructed in heavy \$' (chipboard and covered in black Rexine and pleasing shade of Vynair with aluminum trim.
Size 30'×19' votal.
Size 30'×19' votal.
Garriage 21-60)
and 9 monthly payments of \$8.70

COLUMN SPEAKERS

IDEAL FOR VOCALISTS AND PUBLIC ADDRESS

All types 15 Ohms covered in Rexine and Vynair TYPE C4100 IS ALSO SUITABLE FOR BASS GUITAR OR ELECTRONIC ORGAN

C48S 25-30 WATTS

Fitted four 8" high flux 8 watt speakers. Overall size approx $48" \times 10" \times 5"$. 48" × 10" × 5 Terms: Dep £3 and 9 monthly payments £2 £17.75 payments £2 (Total £21)

Carr 50p



Fitted four 12"11,000 line 15 watt speakers:
Overall size approx 56"
× 14" × 9". Terms:

\$\forall 7.\forall 5 \text{ f97-f0}\$ £27.50 \times 14" \times 9". Terms: Dep. £4 and 9 monthly payments £3 (Total £31)



C4/100 100WATTS

inc. four 12" 50 watt speakers for conservative rating. Extra heavy construction. Size approx 58" × 16" × 10" Acoustically filled and pressurised

RECOMMENDED FOR DISCOTHEQUES, OR INSTRUMENTAL GROUPS

ONLY £50-50

Terms: Dep. £7.50 and payments £5.45 (Total £56.55) and 9 monthly



FANE 'POP' 25/2 LOUDSPEAKERS Watt Dual Cone 15 \(\Omega\) (for uses other than Bass Guitar or

Electronic Organ),

or Dep. £1 and 9 mthly payments 75p (Total £7.75). **FANE**



ALL POWER RATINGS ARE R.M.S. CONTINUOUS. 2 YEARS' GUARANTEE.

HIGH FLUX CERAMIC MAGNETS. ALL CARRIAGE FREE.

'POP' 100

RATING 100 WATTS R.M.S.

monthly payments £2:15. Total £25:35 £22·50

FOR BASS GUITAR, ELECTRONIC ORGAN, ETC.

15" 'POP' 60

RATING 60 W 14,000 gauss 8/15 Ω WATTS R.M.S.

Dep. £3.30 and 9 monthly payments £1.30 (Total £15).

12" 'POP' 50

RATING 50 WATTS R.M.S. 13,000 gauss 15Ω

Dep. £2 and 9 £10·50 E1U'5U monthly payments £1:15. Total £12:35
PAIR SUITABLE ALL PURPOSES

R.S.C. Branches listed below Branches open all day Sats. BRADFORD 10 North Parade (Half-day Wed.). Tel. 25349

BRADFUKD IN TOTAL AT THE L. 2\$349
BLACKPOOL (Agent) O & C Electronics
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DERBY 26 Osmaston Rd. The Spot (Half-day Wed).
DARLINGTON 18 Priestgate (Half-day Wed).
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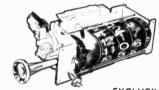
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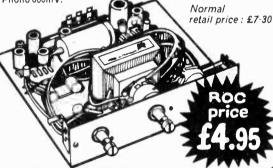
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with facility for re-

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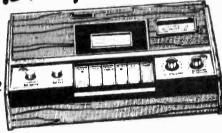
sponse, stereo headphone socket, output power:8 watts.FM frequency range 88-108 M Hz; AM frequency range 535-1605 K Hz. Inputs for turntable (ceramic cartridge) and tape. Frequency response:50-10,000 Hz ±3dB. Output:4 watts per channel @ 8 ohms. Inputs:Phono 200mV, tape 100mV.FM: Sensitivity 20µV, stereo separation 26dB, image rejection 55dB. AM: Sensitivity 300µV.

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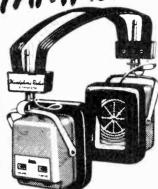
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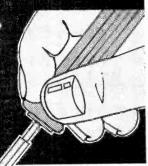
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5 A d.c 24-40	5V/50V d.c 24:65
10V d.c #4·40	

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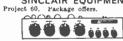
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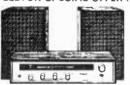
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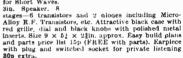
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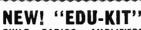


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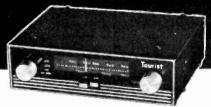
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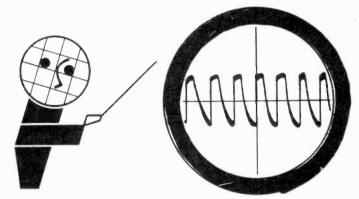
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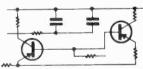
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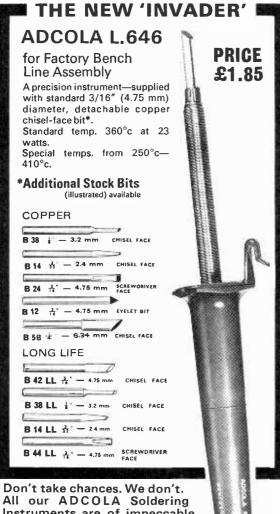
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45p BC212L 13p B8X28 27p B8X60 47p BC731 30p B8X61 27p B8X61 27p B8X61 27p B8X61 27p B8X61 27p B8X61 27p BC732 50p B8X76 47p BC732 50p B8X76 47p BC732 50p B8X76 27p BC732 50p B8X78 47p BC732 50p B8Y11 80p BC742 50p B8Y12 50p BC742 50p B8Y12 50p BC742 50p B8Y12 50p BC742 50p B8Y12 50p BC743 50p B8Y12 50p BC743 50p B8Y26 50p BC743 50p B8Y26 50p BC743 50p BSY26 50p BC743 50p B 20p 2N3404 82p 40310 20p 2N3405 65p 40311 20p 2N3415 22p 40314 30p 2N3415 22p 40314 30p 2N3415 22p 40314 30p 2N3416 37p 40320 31p 2N3417 37p 40320 31p 2N3417 37p 40320 31p 2N3417 37p 40320 31p 2N3406 22p 40347 40329 22p 22p 2N3605 27p 40324 20p 2N3605 27p 40324 20p 2N3605 22p 40347 17p 2N3702 11p 40348 20p 2N3702 12p 40347 17p 2N3702 11p 40348 20p 2N3703 10p 40380 12p 2N3704 11p 40361 12p 2N3705 10p 40380 12p 2N3706 10p 40380 12p 2N3706 10p 40380 12p 2N3706 10p 40380 12p 2N3706 10p 40380 30p 2N3706 03p 40408 30p 2N3806 27p AC126 32p 2N3806 27p AC126 32p 2N3806 32p AC126 32p AC126 32p 2N3806 32p AC126 **TRANSISTORS** NKT281 274p NKT401 874p NKT402 75p NKT404 624p NKT406 624p NKT406 624p NKT452 684p NKT452 684p NKT613F 824p NKT613F 824p NKT613F 824p NKT613F 824p NKT677F 80p NKT677F 80p 2G301 324p 824p 624p 224p 274p 274p 274p 274p 15p 174p 174p 25p 25p 25p 25p 2G302 2G303 2G306 2G308 2(1309 2G371 2G371 2G374 2G381 2N404 2N696 2N697 2N698 NKT677F 80p NKT713 25p NKT781 80p NKT10419 80p NKT10439 2N706 2N708 2N709 2N709 2N718 2N726 2N727 2N914 2N916 2N918 2N929 2002 221p
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\$ BC108 BC109 BC113 BC115 BC116A BC118 BC121 BC122 2N2926 2N2926 Green 14p Yellow 12ip Orange 12ip 2N3011 30p 2N3014 82ip 2N3053 18p 2N3054 46p 2N3055 60p BC147 BC148 BC149 BC152 BC157 BC158 BC160 BC167 BC168B BC168B BC169C BC170 BC171 BC172 46p 62p 30p 30p 25p 25p 25p 20p 17†p 15p 22†p 22†p 2N3055 2N3133 2N3134 2N3134 2N3135 2N3136 2N3390 2N3391 2N3391 A 2N3392 2N3393 2N3394 2N3402 2N3403

	TTL	. LC	OGIC I.C	:. N	IEW	PRICE	S	
	1-11	12-24		1-11	12-24		1-11	12-24
	£p	£p		£ρ	£p		£p	£p
SN7400	0.50	0.18	SN7433	0.80	0.75	SN7472	0.82	0.80
SN7401	0.20	0.18	SN7437	0.64	0.06	SN7473	0.48	0.4
SN7402	0.20	0.18	SN7438	0.64	0.60	SN7474	0.48	0.4
SN7403	0.20	0.18	SN7440	0.23	0.21	8N7475	0.45	0.4
8N7405	0-20	0.18	SN7441AN	0.87	0.83	SN7476	0.45	0-4
8N7406	0.80	0.75	SN7442	0.85	0.81	SN7480	0.70	0.6
8N7407	0.80	0.75	SN7443	2.86	2.70	SN7481	1.40	1.8
SN7408	0.20	0.18	SN7444	2.86	2.70	SN7482	0.87	0.8
SN7409	0.20	0.18	SN7445	2.50	2.40	8N7483	0.87	0.8
SN7410	0.20	0.18	8N7446	1.00	0.95	SN7484	2.00	1.8
SN7411	0.28	0.21	8N7447	1.00	0.95	SN7485	8.62	8.4
SN7412	0.48	0.46	8N7448	1.00	0.95	SN7486	0.88	0.8
SN7413	0.40	0.88	SN7449	1.00	0.95	SN7490	0.87	0.8
SN7420	0.20	0.18	SN7450	0.20	0.18	8N7491AN	1 21	1.1
SN7423	0.51	0.47	SN7451	0.20	0.18	8N7492	0.87	0.84
8N7427	0.48	0.45	SN7453	0.20	0.18	8N7493	0.87	0.84
8N7428	0.80	0.75	8N7454	0.20	0.18	SN7494	0.87	0.84
SN7430	0.28	0.15	SN7460	0.20	0.18	SN7495	0.87	0.84
BN7432	0.48	0.42	SN7470	0.40	0.88	SN7496	0.87	0.8

		SILIC	CON	REC	CTIF	ERS		
PIV	50	100	200	400	600	800	1000	1200
1 A	8p	9p	10p	11p	12p	15p	20p	_
3 A	15p		_	22 p	_	80p	_	
6 A		_	25p	80p	82 jp	35p	_	
10 A		52 ł p	57 p	65p	771p	86 ł p	971p	41.25
15 A		57 p	62 tp	77 p	90p	97 ip	£1-20	21-57
35 A	_	80p	90p	£1-00	\$1.25	£1.50	£2·50	
1 amp a	nd 8 amp	are pla	atic enc	apsulati	on.			

		DIOD	ES &	RECT	IFIER	lS	
IN34A	10p	AA119	7p	BAX16	12 i p	FST3/4	22 i p
IN914	7p	AA129	15p	BAY18	174p	OA5	17p
IN916	7p	AAZ13	12p	BAY31	7p -	OA10	20 p
IN4007	20p	AA7.15	12p	BAY38	25p	OA9	10p
1844	7p	AAZ17	10p	BY100	15p	OA47	8p
18113	15p	BA100	15p	BY103	22p	O A 70	7p
IS120	12p	BA102	25p	BY122	47 i p	OA73	10p
18121	14p	BA110	25p	BY124	15p	OA79	7p
IS130	8p	BA114	15p	BY126	15p	OA81	8p
18131	10p	BA115	7p	BY127	17p	OA85	10p
18132	12p	BA141	17p	BY164	57p	OA90	7p
18920	7p	BA142	17p	BYX10	22 p	OA91	7p
18922	8p	BA144	12p	BYZ10	35p	OA95	7p
18923	12p	BA145	17p	BYZ11	32p	OA200	7p
18940	5р	BA154	12p	BYZ12	30p	OA202	10p
	-	BAX13	5n	B ₹Z13	25p	TIV307	50p

TRIACS	BRIDGE RECTIFIERS
8C2SD 81.124 8CS1D 81.95 8C38D 21.00 40430 97;p 8C40D 21.50 40486 95;p 8C41D 21.92 40528 72;p 8C45D 21.62; 40430 21.30 8C46D 21.42; 40432 21.37 8C50D 22.05 40512 21.45	A. PIV 1 100 47 pp 4 50 60p 1.4 140 52 pp 4 100 70p 2 50 55p 4 400 85p 2 2 200 70p 6 200 87 pp 2 400 80p 4 400 \$15p

PIV 1A	25p	100 27≟p	20∂ 87∤p	300 40p	400 471p	
4 A 7 A T I C 4	7 0.6 a	mp.	92 i p 200 P	—⊈1 IV 5	l •12 i p	
	12 am; 25 at			75p		
VEROBOARD						

VEROBOAR	RD.	
	0.15	0-1
	Matrix	
21 × 31 in	17}p	20p
2	21p	24p
3∄ × 3∄in	21 p	24p
3# × 5in	27 I p	27 lp
5 × 17in (Plain)		
Vero Pins (Bag	of 36) 2 0)p
Vero Cutter 45p		
Pin Insertion T		and •15
matrix) at 55p		

HEAT SINKS	
4.8 × 4 × 1in Finned for Tw	
TO-3 Trans., 48p. $4.8 \times 2 \times 15$ Finned, for One TO-3 Trans	
83p. For 80-1, 21p. For TO-	5,
5p Finned. For TO-18, a	ŠŢ
Finned.	
0-0107000	

Finned.	, -,
RESISTORS Carbon Film	
watt 5%, 1p. watt 5%, 1p. watt 5%, 2p. watt 5%, 2p. watt 5%, 2p.	W, 1W & 2W E24 Series.
1 watt 10%, 24p. 2 watt 10%, 6p.	W & W E12 Series.

MU	LLAF	ID C2	80 M	/F	OIL
	ACIT			•	
0.01,	0.022,	0.033,	0.047	8р	each
0.068				4p	each
0.15,	0.22, 0	33		5p	each
0.47				-	9p
0.68					110
1μ F					14p
1.541	٠				21p
$2 \cdot 2 \mu I$	'				25p

WIRE-WOUND RESISTORS 2-5 watt 5% (up to 270 ohms only). 7p
5 watts 5% (up to 8-2kΩ only), 9p
10 watt 5% (up to 25kΩ only), 10p

POTENTIOMETERS

Carbon:
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and Lin., 40p.

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PREMIER STEREO SYSTEM "ONE" Consists of the new Premier 800 sll transistor stereo amplifier, Garrard 2025 T/C auto manual rerord player unit flitted stereo mono ceramic cartridge with diamond stylus and mounted in teak finish plinth with perspex cover and two matching teak finish loud-speaker systems. Absolutely complete and supplied ready to plug in and play, 800 amplifier has an output of 5 watts per channel with inputs for ceramic and magnetic pick-up, tape and tuner also tape output socket and healthone socket. Controls Bass, Treble, Volume, Balance, Selector, Power on/off. Mono/Stereo switch. Stereo Healphone socket. Black leatherette cahinet with aluminium front panel. Size: 121°× 64°× 22°. (Amplifier available separately if required £16:25. Carr. 40p).

PREMIER STEREO SYSTEM "TWO", as above but with Garrard SP25 MK III and mag-metic cartridge. ONLY

£48. Carr. £1.75.

carr. £1-75

PREMIER STEREO SYSTEM "THREE". The consists of KLINGER KC903 stereo amplifier giving 6 watts rms per channel with Bass, Treble, Volume and Balance Controls. Inputs for Magnetic consists of KLINGER KC903 stereo amplifier giving 5 watts rins per channel with Bass, Treble, Volume and Balance Controls, Inputs for Magnetic and ceramic pick-up, tuner, tape in and out. Stereo carphone socket. Carrard 8125 Mt. III in teak finish plinth with cover and fitted Sonotone 9TAHCD diamond stereo cartridge. A pair of HMF Speakers size 10½ x 10½ x 9° fitted EMI units complete the matching system. ONLY £57.75. Carr. £1-75.

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STEREO HEADPHONES

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Philips 580 £21.00 Stereo Amplifier (List £29:00) Rogers Ravensbrook II £39.50 Stereo Amplifier in teak case (List £52-50) Rogers Ravensbourne £49.00 Stereo Amplifier in teak case (List £64) Metrosound ST20E £28.50 Stereo Amplifier in teak case (List £39.50) less cartridge (List £41-61) £29-00 Garrard SP25 III with £15.50 Goldring G800 cartridge (List £28-35) Garrard AP76 £19.50 less cartridge

Garrard 3500 with Sonotone 9TA stereo cartridge (List £15-50)

£9.97 Garrard 2025 T/C with

Sonotone 9TAHC Diamond Cartridge Garrard 2025 T/C with Sonotone 9TAHC Diamond Cartridge ready wired in teak plinth with cover

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SP25 MKIII SPECIAL!



GARRARD 8P25 MK HI SINGLE RECORD PLAYER FITTED GOLDRING 800 MAG-GOLDRING 800 MAG-NETIC STEREO CAR-TRIDGE as available. COMPLETE IN TEAK PLINTH WITH RIGID PERSPEX COVER. Total list price over £34.

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HI-FI STEREO HEADPHONES

Designed to the highest possible standard, Fitted possible standard. Fitted 2¼in speaker units with soft padded ear muffs, Adjustable headband. 8 ohms impedance. Com-plete with fift lead and stereo jack plug.

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E.M.I. 13 × 8in. HI-FI SPEAKERS Fitted two 23in tweeters and

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TP3 3° 250′ P.V.C. 28p TT3 3° 450° POLYESTER 37p DT3 31° 600′ POLYESTER 57p SP6 5° 600′ P.V.C. 42p LP5 5° 900′ P.V.C. 50p DT5 5° 1200′ POLYESTER 75p E. Double wrapper-attractively boxed.

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TT7 7' 3600' POLYESTER \$250 TAPE SPOOLS 3° 5p, 5°, 51°, 7° 9p, TT7 7° 3600′ POLYESTER
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PRACTICAL WIRELESS

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FEBRUARY 1972

Preview '72

published in this country.

THIS is the first issue of P.W. to hit the bookstalls, or land on your doormat, in this brand new year of 1972. As you read these lines, the Christmas and New Year festivities will be receding into the past with, we hope, a rosy nostalgic haze. On the other hand, these notes are being written in the rather hectic period just before, as they say, the holiday breaks out. The mood at the moment of writing is perhaps more of looking back over the year that has gone, whereas a more appropriate theme for the moment of reading is 'never mind all that—we are more interested in what is to come.' Therefore, bowing to popular demand, here is a brief preview of some of the items we have in store for the coming year.

Observant readers will note that we have kicked off with a meaty start. The quality hi-fi stereo system, transistor oscilloscope (which was shown at last year's Audio Fair), a car rev-counter, a gate dip oscillator, notes on SSB reception, Take 20, IC of the Month and all the other regulars is a fair mixture. Next month is something of a special issue and will feature a novel cube radio you will all want to build, a car radio signal booster to give that extra something to your mobile radio reception and a special DX Data wall chart which incorporates information not hitherto

The line-up of interesting constructional projects jostling for publication include the digital clock which aroused such interest at the Audio Fair, a shortwave receiver covering from 1.7–30MHz, a simple wobbulator for the MW band, a THD distortion meter, a 2-metre FET converter, a transistor tester, a 160m converter, and many more, including some surprise items. Articles on installing car radios, on how to use the oscilloscope (with many waveforms) and thermionic devices in modern electronics will number among the supporting features.

The May issue will include a special extra 8-page supplement and will be of great importance as it will introduce full constructional details of a hi-fi amplifier of radical design, specially developed for P.W. Using ICs, and constructed for low-profile presentation, this new design should cause quite a stir in the world of audio.

These, then, are some of the things we have in store for the coming year and there will, of course, be others introduced into the schedule as convenient. Since we are now unfortunately unable to supply back numbers make sure you get your copy every month by placing a regular order with your newsagent or taking out a subscription. We'd hate you to be disappointed!

W. N. STEVENS—Editor

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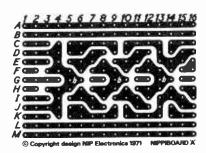
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NEWS... NEWS... NEWS...

Wiring Board



Nippiboard is a simple to use multi-purpose printed wiring board. It has a specially designed layout that can be used as a basis on which to assemble several kinds of circuit, including amplifiers, oscillators, tone circuits, switching circuits, timers, etc.

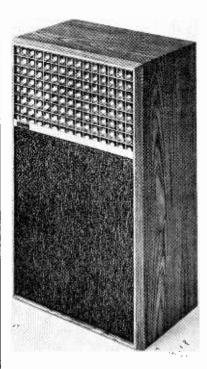
The list is formidable, but it can be done on one basic Nippi-

board pattern with up to four or five small transistors. And the amazing thing is that one Nippiboard Type 1a or 1b is little larger than a matchbox.

There are two ranges at present available: Range 'A' has an s.r.b.p. base and Range 'B' has a fibreglass base. The s.r.b.p. base is cheaper and easy to work with, but the fibreglass base overcomes some of the problems of "movement" in extreme atmospheric conditions. All Nippiboards are flux varnished to keep the copper clean and make soldering easier.

If larger circuits are multiple circuit systems or building blocks are required, Nippiboard can be obtained in nine different arrangements covering between one and ten basic patterns. Type 1a single basic pattern as shown costs 15p. NIP Electronics, P.O. Box 11, St. Albans, Herts.

Duplex 25



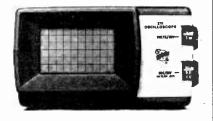
The new Duplex 25 speaker from Metrosound handles a full 25 Watts of power. It has two speaker units—one long throw cone type and the other a radically different electrostatic unit based upon an entirely new patent. The electrostatic unit is mounted behind a lenticular grille. The other is fronted by a specially woven acoustically transparent vinyl cloth. Impedance is 8 ohms. Response 40-18,000Hz. Dimensions: width 16½in., height 27½in., depth 12in.

The smaller version is also available. Called the Duplex 15 it handles 15 Watts and like its big brother it uses both cone and electrostatic units. Impedance 8 ohms. Response of the Duplex 15 is 45-17,000Hz. Dimensions: width 1814in., height 1814in., depth 812in. For both models the electrostatic unit is energised by a supply voltage of 190-250V, 50-60Hz. Prices: Duplex 15-£32. 25-£52. Metrosound Duplex Ltd., Audio Audio Products Works, Cartersfield Road, Waltham Abbey, Essex.

Mini Scope

The Tektronix Type 211 is an all solid state miniature oscilloscope with double insulation, and is designed for use in severe environments. Bandwidth is $500 \mathrm{kHz}$. Weighing only 3 pounds and measuring $3 \times 5^{1}_{4} \times 9 \mathrm{in}$, the Type 211 operates from a.c. line or up to 5 hours on internal batteries. Deflection factors are $1 \mathrm{mV/div}$ to $50 \mathrm{V/div}$. Sweep rates extend to $1 \mathrm{\mu s/div}$.

In many industrial applications it is frequently necessary to "float" an oscilloscope. The Type 211 may be elevated to 700 Volts above ground when operated from batteries, and to 250 Volts r.m.s. above ground from a.c. Trigger controls are simplified to one rotary control. A bright baseline is provided at all sweep rates, even with no signal in. When a signal is received, the oscilloscope triggers on the signal. Internal and external trigger circuits provide stable displays from about seven hertz to at least 500kHz. Price delivered in the UK is:-Type 211 Oscilloscope £262 including batteries. Duty £29.60. Further information available from: Tektronix U.K. Ltd., P.O. Box 69, Harpenden, Herts.



"Verobox"

Vero Electronics announce the introduction of the "E" Series range of cases. The basic shell is identical to the "D" Series but since no front trim is fitted, a slightly larger front panel is required. ¹4 UNF Front Panel fixing screws are included and the case is finished in R.A.F. blue grey hammertone. Vero Electronics Ltd., Industrial Estate, Chandlers Ford, Hampshire, SO5 378



NEWS... NEWS... NEWS...

Moon Laser

A group of scientists of the Moscow Physics Institute and the Crimean Astrophysical Observatory of the U.S.S.R. Academy of Sciences have carried out sessions for laser locating the angular light reflector put on the moon by the *Apollo-15* crew. Clear return signals were recorded.

The angular reflector was placed in the south-east part of the Sea of Rains in the foothills of the lunar apennines, on the dark side of the lunar surface. In order to sight the telescope on it as accurately as possible a small crater was selected on the illuminated part of the moon. Knowing the bearings of this crater and the reflector, one can calculate the angular distance between them. The calculations necessary for sighting the telescope on the light reflector were done at the Academy's Institute of Theoretical Astronomy.

One of the most important tasks of the experiment—the accurate sighting of the laser device on the target—has been solved.

The current experiment is a continuation of the work to investigate the "earth-moon" system by the laser location method. The first Soviet laser locating experiment, for spotting the French reflector mounted on *Lunokhod-1*, was carried out in December 1970 when the measuring accuracy of the distance to the reflectors was of the order of a few metres.

A distinctive feature of the present experiment is that it was possible for the first time to measure the distance to the American angular reflector.

American scientists failed to locate the French reflector mounted on *Lunokhod-1*. This was apparently due to the different methods of calculating the assumed bearings of the reflector.

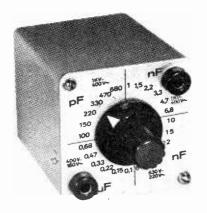
Detailed processing of the results obtained during the location sessions will make it possible to adjust thoroughly many important characteristics of the "earthmoon" system.

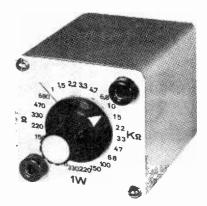
Decade Boxes

Two relatively miniature resistance and capacitance decade units are now available from Londex.

Features of Logade units include single-knob operation over the entire range of four decades, and push-fit terminal sockets accepting standard 4mm plugs.

Resistance Decade Type R1 has an overall range of 100 ohm up





to $680 \text{k}\Omega$, with a tolerance of ± 2 per cent. Maximum operating voltage is 500 V r.m.s., and the rating is 1 W continuous.

Capacitance Decade Type Cl has an overall range of 100 pF up to $0.68 \mu F$, with a tolerance of ± 10 per cent. Maximum voltage ratings are 1,000V d.c. or 400V a.c. Descriptive leaflet (List 253) is available from: Londex Limited, 207 Anerley Road, London, SE20 8EW. Telephone: 01-778-3111.

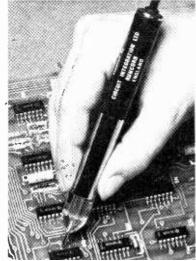
Logic Probes from C.I.

Circuit Integration have announced the introduction of a new product line—a series of Logic Probes.

These pocket-sized probes are designed for the testing of all types of equipment incorporating Integrated Circuits. The units are powered by the equipment under test, and colour-coded readout lights at the probe tip give a clear, accurate indication of "true", "zero" or "pulse" conditions.

The units can be used with virtually any DTL/TTL IC system, including calculators, business machines, numerical control equipment, computers etc., as an invaluable aid to field service engineers, and as a testing device during laboratory development and maufacture.

There are five models in the series, covering the testing and advanced testing of logic systems



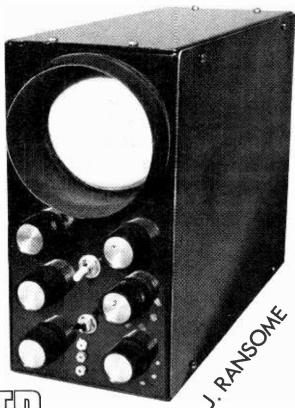
from 4.7V d.c. to 15V d.c. All models incorporate overload protection to protect the circuit under test.

Full details available from:— Circuit Integration Ltd., Davey Rd., Astmoor Industrial Estate, Runcorn, Cheshire. Tel.: Runcorn, 75973/6.

THIS oscilloscope was specifically designed for the first Project Autumn Competition. The most important rule (in the writer's opinion) of that competition was that all components should be readily available; to this the designer has added his own requirement that all circuitry should be completely proved and easily set up using simple test-gear. To the writer there is nothing more frustrating than building up a circuit exactly to the published plans only to find that it does not work because certain component values have been determined empirically and are highly specific to the valves or transistors used in the original equipment. Also, any design that calls for elaborate setting-up or requires specialised test gear for accurate calibration is bound to have an appeal limited to those having either well lined pockets or industrial contacts.

In this design, none of the components is stretched to its limits and this offers the constructor the ability to substitute a wide variety of transistor types for those shown—where transistor selection is somewhat critical this is indicated in the text. If the unit is assembled in the order described then the only test-instrument required is a milliameter capable of reading currents in the ranges 0-10mA and 0-500mA.

It was thought desirable to make the unit as portable as possible so that it could be used for field work. This, of course, requires that the unit should be capable of working from batteries. A quick calculation revealed that the power consumption



TRANSISTORISEE

PART 1

would be such that the use of dry batteries would be out of the question so it was decided that secondary cells would be used as the power source. The obvious choice of supply voltage is 12V as this is readily available from car batteries.

In order to reduce the weight of the unit, no provision for working from the mains has been incorporated, though a 12V power supply can easily be built.

The use of a 12V supply means that the use of valves in the circuit is undesirable from the point of

view of efficiency and for this reason it was decided to use transistors throughout. The employment of solid state circuitry enables both weight and power demand to be minimised.

The circuitry and construction of the oscilloscope will be described in sections starting with the power supply. A block diagram showing the relationship of these sections to the finished project is shown in Fig. 1. By tackling each section as it were in reverse, each section can be checked and will be fully functional on completion.

OSCILLOSCOPE

The complete unit is housed in a metal case, the construction of which is shown in Fig. 2. No precise drilling details are given as these will vary according to the components used.

As the layout is completely uncritical the chassis can, in fact, take any conversion form. Indeed there is no need to have a special chassis made as there are many manufacturers of standard ranges of cases and chassis who regularly advertise through the columns of this journal—any of their products will be satisfactory if made from aluminium or other

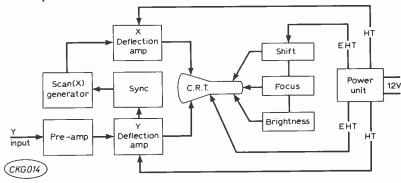


Fig. 1: Block diagram showing the relationship between the various units which will be described separately.

non-magnetic material.

Each component unit will now be described in the suggested building sequence together with the appropriate testing procedures.

POWER SUPPLY UNIT

This was the only part of the whole unit which presented problems from the design point of view. The total h.t. power demand is 3-4 watts and the e.h.t. demand is a little over 1W so that allowing for a conversion efficiency of, say, 60 per cent, the power input to the primary must be in the order of 8W. Using saturated switching circuits it is possible to obtain this sort of power from a single-ended stage but, unfortunately, all the attempts by the writer to attain this theoretical goal ended in failure or disaster!

The next type of circuit to be tried was the pushpull oscillator. Whilst this circuit worked reasonably well, the construction of a suitable transformer appeared to be beyond the scope of this constructor as either one used an inordinate number of turns to get a primary inductance that was satisfactory on the standard range of pot-cores available, or one used a pot-core which is not readily available. After much experimentation the circuit shown in Fig. 3 was developed.

The use of a multivibrator circuit does not seem to offer theoretical advantages over its competitors. Its principle disadvantages being the lower efficiency and the use of more passive components. To the practical constructor, however, it has three major advantages:

- a) it does not stall under heavy load
- b) it is a first-time starter
- c) the construction of the transformer is not critical

Of these (c) is most important in that the transformer windings do not have to be neat, tidy and accurate so long as an ade-

quate turns ratio is maintained. The writer constructed three of these units with differing transistor types and succeeded in getting all three to work first time.

The circuit operation is quite straightforward. Trl and Tr2 form a simple common emitter multivibrator. The collector load for each transistor is provided by the primary of the transformer T1. The resonant frequency of the circuit is made as high as possible so that the primary inductance can be minimised, for by reducing the primary inductance we lower the number of turns required on the primary of the transformer. This has the effect of reducing the turns-per-volt characteristic of the transformer and eases

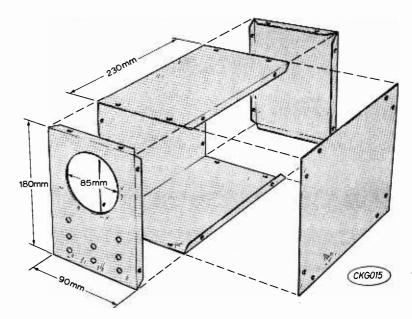


Fig. 2: The basic dimensions of the case used for the prototype and its contruction.

construction of the high voltage secondary.

For the circuit shown the total primary inductance is in the order of 1mH and the turns/volt relationship is 1.5 turns-per-volt.

The secondary of the transformer is wound to give an equivalent r.m.s. output voltage in the region of 220V. As the voltage waveform from the transformer is a peaky triangular shape rather than the more conventional sine wave, measurement of the output voltage by means of the normal a.c. voltmeter is misleading and the only valid way of checking the circuit is to measure the d.c. output from the rectifier. Thus we refer to an equivalent r.m.s. output rather than the true peak-to-peak output.

The secondary of the transformer provides power for the h.t. rail via the bridge rectifier D1-D4 and the smoothing and stabilising circuit of C3, R3, ZD1 and C4, and for the e.h.t. line via the voltage doubling circuits of C5, D5 and D6 and the associated smoothing capacitor C19. This circuitry is completely

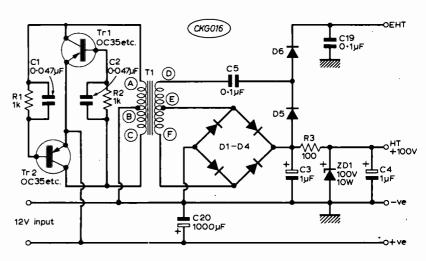


Fig. 3: The power supply circuit which provides the three different voltages necessary.

conventional and does not warrant further discussion here.

The complete power supply is built on to the back of the chassis; the siting of the main components is shown in Fig. 4.

CONSTRUCTION OF T1

Tl is wound on a Mullard LA4 pot-core which is readily available from advertisers in this magazine.

Dismantle the pot core and locate the winding bobbin. This item is fairly fragile and should be handled with care. Wind on to the bobbin 18 turns of 28 s.w.g. double cotton covered enamelled wire. This should occupy one complete layer on the bobbin. Leave several inches of wire at each end of the winding to serve as lead-out wires. Wind on a further 18 turns over the first layer and in the same direction as the previous winding and twist together the end of this winding with the end of the first winding. This is the primary centre tap. Now wrap 112 turns of p.v.c. self-adhesive tape around the windings. Next wind on 120 turns of 32 s.w.g. enamelled wire (try to be as neat as possible but don't worry about the occasional overlap). Pull off sufficient wire from the coil to form the centre tap and wind on sufficient turns to fill the bobbin (the number of turns will depend on how evenly the previous layers were wound-anything between 100-150 turns will be satisfactory). The lead-out wires forming the start, the tap and the finish of this winding should then be sleeved and the winding taped in place.

The whole unit can now be reassembled by first placing the coil inside the ferrite ring and bringing the lead-out wires through the slots cut in the ring. Now drop this assembly over the core and put on the top-plate. Bolt up the complete assembly tightly.

The transistors Tr1 and Tr2 should next be bolted on to the chassis back-plate which acts as a heat sink and Tl fixed in position together with the battery supply terminals. Note that Tr1 and Tr2 should be insulated from the chassis using mica washers. Once the primary circuit has been built up the unit may be tested. Connect the 12V supply via a milliammeter. The meter should indicate a standing current of 200-300mA. If the current is higher than this, disconnect, and check the wiring particularly on the secondary side.

If all is well connect a 250V neon across the rectifier output (- and +); the neon will light up and the current drawn from the 12V source will increase by about 80mA. If a neon lamp is not available disconnect the milliammeter from the primary circuit and connect in series with a 10kΩ resistor when, if the unit is running correctly, a current of 5-8mA will be indicated. This will rise to 15mA if a $1\mu\mathrm{F}$ 250V electrolytic capacitor is also connected across the rectifier. The second phase of the power unit construction can now be undertaken. The tagstrips holding the components are anchored at various convenient points as shown in the photograph. The zener diode must be mounted on a heat dissipating plate about 2in, square. This plate should not be anchored to the oscilloscope chassis (unless insulated electrically). Note that some zener diodes of this power rating have their mounting stud at the cathode end of the diode while on others the stud is the anode.

As the e.h.t. voltage is fairly low (about 500V) no special precautions need be taken other than to

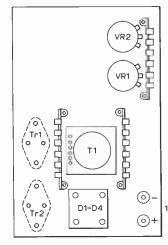
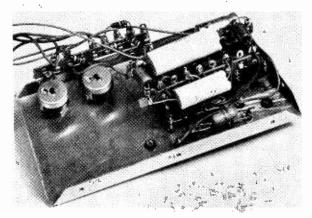


Fig. 4: The siting of the major components on the back panel.

12V Terminals



Compare this view of the back panel with Fig. 4.

ensure that there is a reasonable spacing between the components of the e.h.t. circuitry and the other low voltage items.

TESTING

Check all wiring—particularly the e.h.t. side for faults and potential short circuits. As the oscillator is capable of generating sufficient power to burn out the transformer or the transistors under short circuit conditions, this visual check is a wise precaution.

Connect the milliammeter in series with the battery supply lead and switch on. The current consumption should be about 400-500mA. If the current drain is significantly higher than this, switch off immediately and check the wiring. If all is well remove the ammeter from the battery leads and using a $10k\Omega$ resistor in series with one lead, apply this across C4. A current flow of about 10mA is correct. Remove the meter from the circuit and replace the $10k\Omega$ resistor with one of $470k\Omega$. Apply the meter and series resistance across C19 (remembering that C19 will have across it a voltage of anything up to 600V). Approximately 1mA should be taken by the meter.

The power supply is now complete and ready to connect to the next phase of construction—the Display Unit.

THE DISPLAY UNIT

The theoretical circuit of the Display Unit is shown in Fig. 5. Again the circuitry is absolutely standard and well tried. The potential divider chain of R11, VR4, VR3, R10 and R6 and R7 with VR2 and VR1 in parallel has a total resistance of $1.5M\Omega$ and draws approximately 300 µA from the e.h.t. supply. This gives a control range of 3V to 33V for VR4 and 33V to 185V for VR3. The shift controls have 100V across them and give, therefore, 50V shift either side of the mid-point voltage determined by R6 and R7.

The resistors R4, R5 and R8 and R9 serve to isolate the X and Y plates from "cross-talk" and give a measure of protection to the transistor output stage described later.

EHT 470k Inputs P4 470k R6 **R8** 10 470k VR1 VR2 470k 500k 500k X shift R9 R7 470k 5 R10 Fig. 5: The circuit details 470k of the display unit. R12 is mounted on the out-2 VR3 Focus side of the block panel on 500k1 stand-off insulators. **Brightness** VR4 1001 R12 R11 CKG017 10k 8Ω 10W

CONSTRUCTION

The shift components and X and Y bias and isolating resistors are mounted on the back plate of the chassis next to the power supplies. As the shift controls are only 500V above earth potential they can be mounted directly onto the aluminium plate without further insulation.

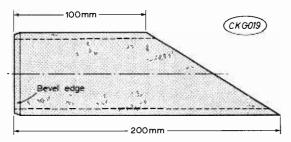
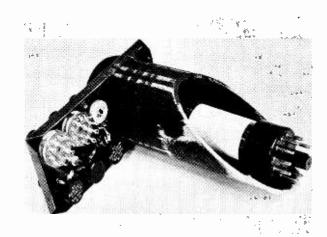


Fig. 6: The dimensions of the CRT cradle.



The front panel, showing the CRT cradle, before wiring.

The tube itself is mounted inside a cradle which also serves as a light shield. The cradle is made from 75mm dia. ABS or PVC drain-pipe (the actual pipe used by the writer was an Osman soil-pipe). About 200mm is required and this is cut and bevelled as shown in Fig. 6. After cleaning up the cut surfaces the pipe is painted matt black (alternatively use a gloss black pipe which is available from some builders rather than the more usual grey).

The cathode ray tube face rim is next padded to prevent mechanical damage if the unit is dropped. The writer used a self-adhesive foam draught excluder winding two complete turns around the tube rim. The foam should be dyed or painted black.

When the paint is dry the cradle can be pushed through the CRT hole in the front panel (push in from the front) leaving about 10mm of the bevelled edge protruding. The CRT is then pushed into the cradle from the rear and should be a snug fit inside the pipe.

TESTING

Having checked the wiring to the tube base and the e.h.t. connections, set VR4 slider to the R11 end of its travel and set VR3 to its mid-point. Switch on the power unit. Allow a minute for the tube to warm-up and adjust VR1 and VR2 until the spot is at the centre of the screen. Adjust VR4 and VR3 for minimum brightness and spot size.

If no spot can be resolved, insert the meter between R11 and VR4 and check for a current flow of about $300\mu A.$ If this current is absent, or very low, follow the e.h.t. down the chain using the meter and the $250k\Omega$ resistor until the break is found. If no break can be discovered, check to see that R11 is taken to the negative line. Inability to centre the spot and/or eliptical movement of the spot is caused by incorrect connections to the X and Y plates.

If all is well, the deflection test unit of Fig. 7 may be built up to test the circuit so far. In building the test unit, make certain that the live leg of the mains is connected to the top of the $1M\Omega$ resistor. For added safety the two neon lamps may be incorporated into the circuit. Only use the test unit when N100 is illuminated.

The high level output from the deflection test unit is first applied to the X input when a straight line about 40mm long will be produced. Turn the tube physically until this line is horizontal. When all is well apply the test unit to the Y input when a vertical line will be produced of roughly equal length

★ components list (complete unit)

Posistors			
Resistors	040 4 71/0 11	A/ D07	1700 1141
R1 1kΩ ½W	R19 4·7kΩ ‡		470Ω ½W
R2 1kΩ ¼W	R20 4·7kΩ 1	W R38	2·7MΩ ¼W 5%
R3 100Ω ½W	R21 10kΩ ¼V		MΩ 1W 5%
R4 470kΩ ¼W	R22 10kΩ ‡V	V R40	470kΩ ‡W 5%
R5 470kΩ ½W	R23 1kΩ ½W	R41	33kΩ ‡W 5%
R6 470kΩ ½W	R24 1kΩ ¼W		27kΩ ‡W
R7 470kΩ ½W	R25 10kΩ ½V		47kΩ ⅓W
R8 470kΩ ½W	R26 47kΩ ½V		lkΩ 1 W
R9 470kΩ ½W	R27 1kΩ ½W		18kΩ ‡W
R10 470kΩ ½W	R28 47Ω ‡W	R46	33kΩ ‡W
R11 10kΩ ‡W	R29 100Ω ½V	V R47	33kΩ ‡W
R12 8Ω 10W	R29 100Ω ¼V R30 47kΩ ¼V R31 47kΩ ¼V R32 1MΩ ¼V R33 82kΩ ¼V R34 10kΩ ¼V	V R48	18k17 [‡] W
R13 33kΩ ‡W	R31 4/K12 4V	V R49	1K75 4 AA
R14 10kΩ ‡W R15 2 2kΩ ‡W	M32 1M12 4V	V R50 2	22012 4 VV
	D34 4010 1V	V ROLE	3.5K75 4 AA
R16 2·2kΩ ½W	/ DOE 4700 114	V N32 2	50K77 \$ AA
R17 See text, 1V	1100 71002 4	1130 2	.2kΩ ‡W
R18 See text, 1V	4.1K75 4/	D12 +0 F	204 Inclusive
NOTE: Two off All 10% types e	cach required	hown	124 Inclusive.
VR1 500kΩ lin. p			VP7 5kO
VR2 500kΩ lin. p	of VR5 1040	lin not	
VR3 500kΩ lin. p	ot VRS 5kO =	reset	log. pot.
41/3 300K22 IIII. þ	or Aug 2427 b	eset	
Capacitors			
C1 0.047µF 150V	C8 0-14 F 10	00V C15	5 E 15\/
C2 0.047µF 150V	C9 0.1µF 10	000 V C16	1000pF
C3 1µF 250V	C10 5µF 15V		0·1µF 150V
C4 1µF 250V	C11 0·1µF 15	INV CIR	0.01E 150V
C5 0·1µF 1000V	C12 6.44 F 25	V C19	0.14F 1000V
C6 5µF 15V	C13 5µF 15V	C20	1000µF 25V
C7 5µF 15V	C14 64µF 15		1000µ1 25 ¥
NOTE: Two off			C9 inclusive.
Time base capac	itors		
CTa 1µF	CTc 0	01μF	
CTb 0·1µF	CTd 1,	00 0 pF	
Semiconductors			
Tr1 OC35, 2G2		BSX21	Tr13 2N3906
Tr2 OC35, 2G2		2N3702	Tr14 2N3906
Tr3 2N3906		2N2160	Tr15 2N3906
Tr4 2N3906		2N 3 906	Tr16 2N3906
Tr5 BSX21		2N3906	Tr17 2N3702
Tr6 2N3906		N3906	
NOTE: Two off			r7 inclusive.
D1-D4 OA202 o		idge	
D5 1000V 0-6			
	6A silicon		
D7 OA81.			
ZD1 100V, 10W	zener		
Cathode Ray Tu	ho		
ECR30 or VCR13			
ECHOU OF VCRI	AE		
Switches			
	1 nole 4 wa		
	1-pole, 4-way		
	n., 1-pole, 3-w		
	ut, on-off togg nc, 1-pole, 2-v		le .
SW4 III(EXCS)	11c, 1-pole, 2-V	way togg	i e
Miscellaneous			
B12B tube base	· 3in diam n	ine for	CRT cradle:
T1, see text, LA	4 not core 25	l nwas	CC enam
I I, SEE TEAL, LA	Por Coic, 20	2.44.A. P	J. V. C. CHaill.

wire, 32 s.w.g. enam. wire; Tag strips; Veroboard;

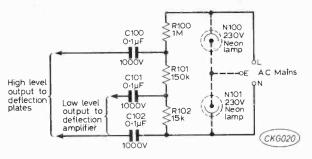


Fig. 7: The deflection test unit.

of that of the horizontal line. Next, connect the X1 and Y1 inputs together and the X2 and Y2 plates together. Apply the test voltage across the combined plates when a circle (or elipse, depending on the relative deflection sensitivity of the plates) should be produced.

The unit as it now stands can be used as a simple a.m. transmitter modulation monitor.

For this purpose a small demodulation unit will be required—this is shown in Fig. 8. Power from the transmitter is fed directly into the tuned circuit. Modulated r.f. is fed directly to the Y plates of the display unit while the X plates receive the a.f. signal from the demodulation network. The resultant trace is shown in Fig. 9. The area occupied by the

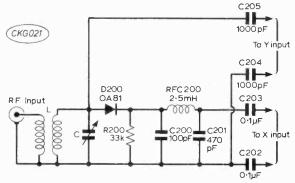
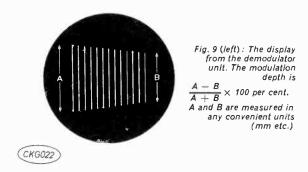


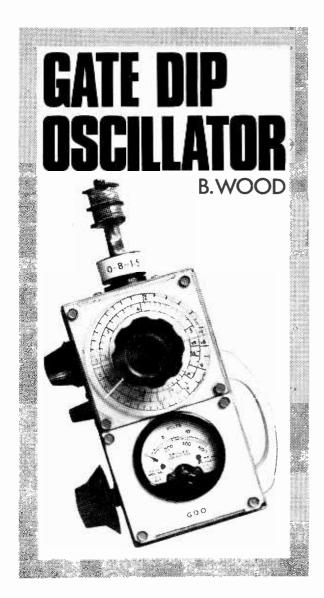
Fig. 8 (above): The circuit of the demodulator unit. L and C are chosen to resonate at the transmitter frequency.



trace is controlled by the power output of the transmitter—by making the r.f. input coil of L loose over the coil former, the coupling and thereby the power input to the demodulator may be varied.

TO BE CONTINUED

Switches, etc.



NE of the most useful and versatile of instruments, usually noticeable by its absence, is the grid or gate dip oscillator. The drawback in the pre-transistor age was that such instruments were valved and hence needed a mains power pack or bulky batteries which restricted operation. To be so restricted when measuring the resonant frequency of a whip aerial, or adjusting the traps on a dipole, is to say the least, inconvenient. The purpose of this article is to show how the author was able to construct a fairly versatile and readily portable g.d.o. almost entirely from bits and pieces found in his junk-box.

DEVELOPMENT

The original circuit is shown in Fig. 1. The f.e.t. costs under 40p, whilst the meter was taken from a No. 19 set. Acceptable results were obtained from this set up, but it was felt that the addition of a diode and an OC71 meter amplifier would increase the usefulness of the instrument. Fig. 2 shows the

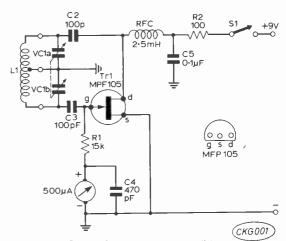


Fig. 1: Circuit of a simple gate dip oscillator

amended circuit and it will be seen that few extra components are needed. VR1 was included to enable the meter pointer to be adjusted and kept on scale when using different coils.

Fig. 3 shows the addition of a simple modulator. T1 was removed from a small pocket-type transistor set. Modulation was obtainable using several combinations of the windings, but those noted on the circuit diagram proved the best. Failure to oscillate may require the reversal of the leads to either the primary or secondary of the transformer.

The function switch provides the following modes:—
Position 1. Instrument off.

Position 2. S2 closed. Meter amplifier operative. Measurement of the frequency of coil/capacitor combinations in "hot" circuits.

Position 3. S1 and S2 closed. Operates as an unmodulated r.f. oscillator enabling:—
(a) The adjustment of "cold" coil/capacitor combinations.

- (b) Frequency measurement. Beating the g.d.o. with a station tuned in on the receiver.
- (c) As a beat frequency oscillator. Useful also for resolving s.s.b. signals.

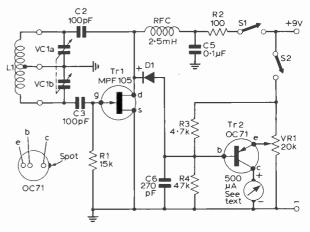


Fig. 2: G.d.o. with d.c. amplifier to permit use of less sensitive meter.

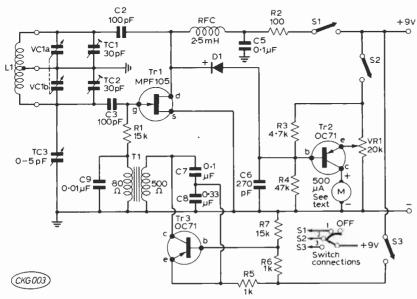
Position 4. S1, 2 and 3 closed. A modulated r.f. signal generator is available

CONSTRUCTION

Capacitor VCla-b is a twin gang 500pF variable with approximately half the rotor vanes removed. This is done by carefully bending them, one at a time, backwards and forwards until they break off. The same number of vanes is removed from each section of the capacitor.

TC1 and TC2 were added to give some measure of bandspread, the ultimate aim being to cover the required frequency range with a reasonable number of coils. TC3 was added as a fine tuner and affects the main tuning by only a few kilohertz. The original

Range MHz	Turns	Wire	Centre Tapped	Core
0-8 1-5	200+200 Pile wound each pile §" wide	28g. c.c.	Yes	Yes
1-5 3-0	130+130 Pile wound leach pile #" wide	31	Yes	Yes
3.0 6.0	100 Close wound	28g. enamel	Yes	Yes
5 · 0—10 · 0	48 Close wound	74	No.	Yes
9-5-19-0	20 Close wound	28g. c.c.	No	No
18:0-31 0		12 mm 61	No	No



▲ Winding details of coils covering 800kHz to 31MHz.

Fig. 3:

Circuit of g.d.o. incorporating meter amplifier and audio oscillator! modulator.

Some of the coils wound to the specifications given above.

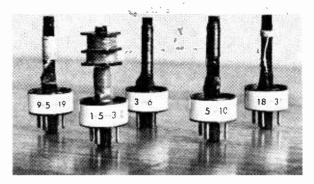
six coils covered the frequency range of $800k\mbox{Hz}$ to $31\mbox{MHz}.$

Whilst a 500 A meter was a necessity in Fig. 1, the addition of a meter amplifier permits the use of meters with full scale deflections of up to 5mA. to be used. Most of the parts were assembled on a piece of paxolin which in turn was fastened to the back of the meter by the meter retaining nuts, Fig. 4.

Whilst no attempt was made at miniaturisation, the prototype was easily constructed in a metal box which was to hand, measuring 6 x 3 x 2½in. The g.d.o. has proved itself to be an invaluable aid in the workshop and in practice no drastic change in frequency has been noted until the battery has been discharged to some 6 volts.

COILS AND CALIBRATION

The author used an octal valve holder for the coil socket and surplus valve bases for the coil holders. As only three pins are required on the coil bases all unwanted pins were removed. This facilitates insertion and withdrawal of the coils. The coil formers, 516in. diameter, are of the type to be found in the older type of TV set. The formers were stripped of all the old windings and rewound in accordance



with the coil table shown, leaving in one ferrite core, as indicated. The windings were anchored to spills soldered through the eyelets in the base of the formers. The spills in turn were used to secure the formers to the bases by passing the spills through the appropriate valve base pins and soldering them. The surplus wire was then snipped off. Small cardboard cheeks found on the formers were retained for use in the construction of the l.f. coils.

The 20 turn coil is constructed first and, with the g.d.o. switched to modulated c.w., the instrument was

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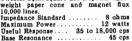
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Base Resonance ... 45 cps





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Special Offer. Aircraft Sighting Head. Comprising flexible drive, lens prism unit, Giro. Useful for model constructors, schools, etc. Condition fair. 75p. unit, Giro Carr. 75p.

Reclaimed T.V. Tubes. All with 12 months guarantee. AW43/88. £2. AW43/80. £1-50. MW43/89 £1. Special offer Brand New Brimar Tubes C17P.M. £1. Many older types in stock. Carriage and insurance on any

Breaking-up. Ferguson Model 596T. Tested L.O.P.T. £1-45. Post paid. Fireball Tuner Unit with Valves less Knobs. 75p. Post paid. S.A.E. for Price List of other spaces for this set and other types.

Valve List Ex Equipment All Valves Tested on a Mullard Valve Tester before despatched. 3 Months Guarantee on all Valves Single Valves PIP 3p. Over three Valves PIP Paid.

ARP12 EB91 EF85 EBF80 EBF89 ECC81 ECC82 ECC83 ECL80 EF80 EF91 EY86	5p 4p 12†p 12†p 12†p 12†p 12†p 7†p 7†p 4p 20p	PCC84 PCF80 PCL82 PCL82 PCL83 PCF82 PL81 PY81 PY33 PY82 PL82 PL82 PCL84	5p 5p 12+p 12+p 20p 17+p 7+p 17+p 7+p 7+p 7+p 12+p	U191 U251 6BW7 6U4 6F23 20P1 20P3 20D1 30P4 30P4 30FL1 6/30L2 30F5	20p 12½p 10p 10p 20p 20p 10p 20p 20p 20p 20p
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loosely coupled to the aerial socket of the station receiver via a short length of wire. With the g.d.o. variable capacitor vanes fully in mesh, a search is made on the receiver for the modulated signal. The search must begin at a frequency much lower than that expected, in order to ensure that one is not working on harmonics of the signal. Throughout calibration, the small variable capacitor should be kept at half mesh.

Having found the lowest frequency to which the

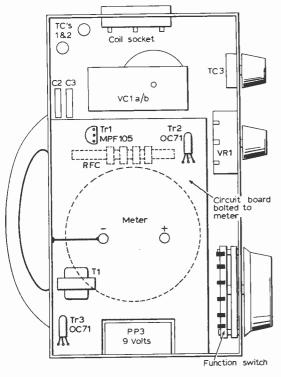


Fig. 4: Layout of main components in the g.d.o. constructed by the author.

★ components list (Fig. 3)

Resistors	_
R1 15kΩ	R5 1kΩ
R2 100Ω	R6 1kΩ
R3 4·7kΩ	R7 15kΩ
R4 47kΩ	All ‡W 10%
VR1 20kΩ lit	tear potentiometer
	į.
Capacitors	
VC1a-b 250 + 250pF	approx. See text
	C6 270pF SM
C3 100pF SM	C7 0·1μF
C4 470pF (Fig. 1)	
C5 0·1µF	C9 0.01µF
TC1/2 3-30pF trimme	
TC3 5pF trimmer.	
Miscelianeous	
Transistor MPF105(1) OC71(2). Miniature audi
transformer (T1). RF	C 2·5mH.
Meter, see text. Wa	fer switch 1 pole, 4 way,
shorting consecutive	

coil will tune, it is only necessary to open up the vanes of the g.d.o. and gradually follow the signal on the receiver up to a higher frequency, in fact to its limit. Should the desired coverage not be obtained on any range it may be necessary to add or take off a few turns of wire.

During calibration use can be made of standard frequency transmissions for checking the receiver as well as the g.d.o. Oscillation on the l.f. ranges could only be obtained if the coils were centre tapped, as indicated.

Should a crystal calibrator be available use can be made of it in the calibration procedure. Loosely couple the calibrator to the station receiver, switch the g.d.o. to c.w. and zero beat the two signals, taking care that the beat is taking place with fundamentals of the g.d.o. In the case of the Class D Wavemeter, it is switched to 1MHz, and coupled to the g.d.o. coil by a 3 turn-coil, when it is possible with the phones connected to the wavemeter, and the g.d.o. switched to c.w., to hear the 1MHz harmonics when tuning the g.d.o. Having marked these in on the dial, it is then possible to fill in the gaps with the 100kHz crystal. It is then only necessary to identify any one of these points by using the g.d.o. in conjunction with the station receiver, to complete the rest of the calibration for that coil. Calibration of the remaining coils was carried out in the same way, working down from the.h.f. to the l.f. coils.

TELEVISION

FEBRUARY ISSUE

THE DO-BE OSCILLATOR

A timebase oscillator circuit for the constructor—the double-beam oscillator, so called because it employs two valves in a blocking oscillator/discharge valve arrangement. Whilst using a double-triode and transformer the circuit is nevertheless economical in other components and has the advantage of very good locking. Field and line generator circuits are given.

SIMPLE WALL-MOUNTING UHF AERIAL

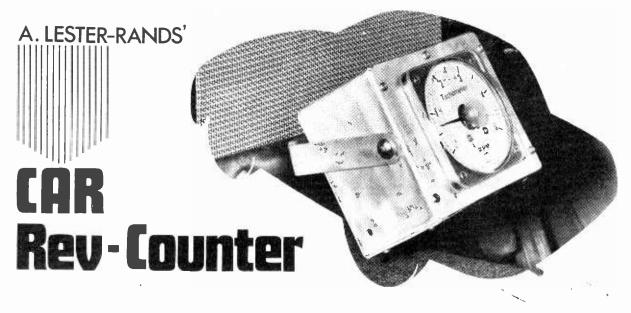
Another design for the constructor. The main advantage of this dipole-plus-sheet-reflector assembly is that it is very short and can be mounted quite unobtrusively just inside or outside a window. Dimensions are given for group A, B and C/D versions.

THE SANYO 10-T120U

A further instalment in our series on the interesting circuitry to be found in imported TV receivers. This 10in. mains/battery portable for example features a keyed a.g.c. circuit, noise-cancelled sync separator circuit, emitter-follower line output stage and other arrangements which are illustrated and described.

PLUS ALL THE REGULAR FEATURES

ON SALE JANUARY 17



ANY car owners, particularly those who have cars with high revving engines, consider an engine tachometer an essential dashboard instrument and manufacturers of some modern cars now fit a rev counter as a standard. A tachometer gives a direct reading of engine revolutions per minute which can be related to brake horsepower and torque to enable the car owner to get the best performance from the engine with the least wear and tear and at the most economical fuel consumption.

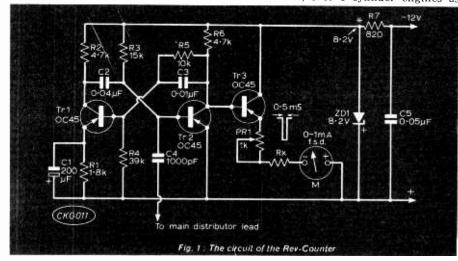
The tachometer described in this article employs a fairly simple circuit which can be adjusted for use with 4, 6 or 8 cylinder engines and calibrated for revolutions per minute of 0-5,000, 0-8,000 or 0-10,000. To give an example of this, the writer's car has a 4 cylinder engine and develops maximum brake horse power at 4,600 r.p.m.; in this case calibration was adjusted for 0-5,000 r.p.m.

The instrument will operate from the car battery regardless of which polarity of the battery is earthed to the car body and no direct electrical connection is necessary to pick up the ignition pulses. The pulse pick-up is capacitive by means of a few turns of insulated wire wrapped around the main ignition lead.

The actual r.p.m. indicator may be any lmA f.s.d. meter but for a longer calibration scale and a more pleasing appearance, a meter with a 240° scale is worth the extra cost; most of those available have a 3in. diameter scale. The meter can of course be a conventional 90° scale type or an edge scale meter which might lend itself better for dashboard mounting. If there is no room on the dashboard, the complete tachometer could be mounted in a small box of its own and secured where it can be seen at a glance.

THE CIRCUIT

The tachometer circuit is shown in Fig. 1 and is a fairly conventional arrangement using a flip-flop (Trl and Tr2) from which to derive a constant amplitude narrow square-wave. The time constant in the flipflop produces an output pulse of approximately 0.5mS. The supply voltage is held stable by the Zener Diode to 8.2V so that variations in the battery voltage do not effect the readings. The output from Tr3 is, as far as the meter is concerned, a recurrent positive-going pulse of constant amplitude and duration. The meter will read the mean positive voltage developed by the pulses so the slower the pulses the lower will be the meter reading and vice versa. However, the meter reading can be altered by increasing or decreasing the amplitude of the pulse current passing through it by inserting series resistance (PR1 and Rx). This makes it possible to adjust full scale deflection for different maximum readings. Equally the pulse amplitude to the meter can be adjusted relative to the pulse rate so that the meter can be calibrated for 4, 6 or 8 cylinder engines as



CONTROL DRILL SPEEDS

DRILL CONTROLLER NEW IKW MODEL

Electronically changes speed from approxi-mately 10 revs. to maximum. Full power at all speeds by finger-tip control. Kit includes all parts, case, everything and full instructions. £1.50 plus 13p post and insurance Made up model also avail-able, £2.25 plus 13p post & p.

MAINS OPERATED CONTACTOR

220/240v. 50 cycle solenoid with laminated core so very silent in operation. Closes 4 circuits each rated at 10 amps. Extremely well made by a German Electrical Company. Overall size 24 × 2 ×







with dashboard control switch fully extendable to 40in or fully retractable. Suitable for 12v positive or negative earth. Supplied complet-with fitting instructions and read-wired dashboard switch. 28 plus 25p post and ins.



TOGGLE SWITCH

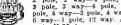
3 amp. 250v. with fixing ring 74p each, 75p doz

MICRO SWITCH



MINIATURE WAFER SWITCHES

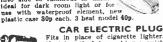
2 pole, 2 way—4 pole, 2 way—2 pole, 3 way—4 pole, 3 way—2 pole, 4 way—2 pole, 4 way—2 pole of way—1 pole, 12 way. All at 18p each, £1:80 dozen, your assortment.



WATERPROOF HEATING
ELEMENT
26 yards length 70W. Self-regulating
temperature control. 50p post free.

BLANKET SWITCH

Double pole with neon let into side so luminous in dark. ideal for dark room light or for use with waterproof element, new plastic case 30p each. 3 heat model 40p.



Fits in place of cigarette lighter. Useful method for making a quick connection into the car electrical system, 38p each or 10 for 23 42.



TREASURE TRACER

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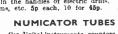
18/

QUICK CUPPA

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Mini Immersion Heater, 350v.
200/240v. Bolls full cup in about
two minutes. Use any socket or
tamp holder. Have at bedside
for tea, baby's food, etc. \$1.25, oet
and insurance 14p. 12v. car model
also available same price. Jug
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SNAP ACTION SLIDE SWITCH

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For digital instruments, counters, timers, clocks, etc. Hi-vac XN. 3, Price £1.45 each. 10 for £13,

12 WAY SUB-MINIATURE MULTI-CORE CABLE

7-0076 copper cores each core P.V.C. insulated and of different colour. P.V.C. covered overall and approx. 3/16in. thick. Price 20p per yard,



6

LIGHT CELL

Almost zero resistant in sunlight increases to 10 K Ohms
resin sealed. Size approx. In. dia. by Jin. thick.
Bated at 500 MW, wire ended. 45p with circuit.

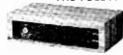
HONEYWELL PROGRAMMER

This is a furn type timing device, the drum being calibrated in equal divisions for switch setting purposes with trips which are infinitely adjustable for position. They are also arranged to allow 2 operations per switch per rotation. There are 15 changeover micro switches each of 10 amp type operated by the trips thus 15 circuits may be changed per revolution. Drive motor is smains operated 5 revs per min. Some of the many uses of this timer are Machinery control, Boiler firing, Dispensing and Vending machines, Display lighting animated and signs, Signalling, etc. Price from makers probably over £16 each. Special saip price £5.75 plus 25p post and insurance. Don't miss this terrific bargain.



Don't miss this terrific bargain

THE FULL FI STEREO SIX



sensation of the year

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Vou will be anazed at the full ness of reproduction and at the added qualifies your records or tuner will reproduce. Built into netal cabinet elegantile to blend with modern furnishings, this amplifier uses an integrated solid state circuit with an output power of 6 watts R.M.S. split over the two channels. The amplifier is ideal for use with normal pick-ups and tuners, it has a double wound mains transformer and ganged volume and tone controls—also switching for Mono to Stereo, tuner or pick-up.

UNREPEATABLE PRICE is £9 plus 38p post and insurance.

DISTRIBUTION PANELS

Just what you need for work bench or lab 4 × 13 amp sockets in metal box to take ouse wink you need no work beach or an 4 × 13 amp sockets in metal box to take standard 13 amp fused plugs and on/off switch with neon warning light. Supplied complete with 7 feet of heavy cable. Wired up ready to work, £2 less plug £2.25 with fitted 13 amp plug; £2.40 with fitted 15 amp plug plus 23 p. & 1.

THIS MONTH'S SNIP .



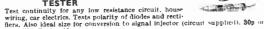
Smiths 24 hour 2 on/2 off Time Switch This is the popular model, as used in the Autoset and Morphy Richards time switches. Only needs a case and an output socket. 230° cycle. Contacts switch up to 13 smps. Price 22.75p

TANGENTIAL HEATER UNITS

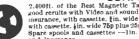
This heater unit is the very latest type, most efficient, and quiet running. Is as fitted in Hoover and blower heaters costing £15 and more. We have a few only. Comprises motor, impelier, 2kW. element and kW. element allowing switching 2 and 3kW and with thermal safety cut-out. Can be fitted into any metal line case or cablnet. Only need control switch. 23-50. 2kW. Model as above except 2 kilowatts £25. Don't miss this. Control Switch 35p. P. & P. 40p.

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Made by famous Smiths company, these have a large clear dial, size 4½ x 3½, which can be set in minutes up to 1 hour. After preset period the bell rings. Ideal for processing, a memory logger or, by adding simple lever. would operate micro-switch £115.

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These are minature relays. Size approx. 1 3/16th in. high x 14th. wide x 14th. deep. 4 change over silver/gold contacts. Contact rating lamp 1060, D.C. Fitted with a plastic cover. Coll operates approx. 250Mv. D.C. Avialable with the following



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24×31	22p	16p
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		37 i p
17 × 24 (plain)		174p
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2 m. square full vision for flush mounting. Moving iron instrument lideal for charger. Price 439 each 16 for 23-90.

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shop, 2 ft. wide × 14 in. high × 3 in. heep. Interaction is an illuminated box sign made from sheet metal hammer finish enamel with a clear plastic window You simply have your message printed or written on poster board of thick card. (Or use stick down letters available at most stationers). You will then have a box sign normally coating anything between £10-215. Humination is by a 2 ft. fluor-scent tub-with control gear enclosed, Message card can be changed quite easily from hinged top back. Price £3 each, plus 65p post. etc.

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Small ceramic magnets to operate these reed

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Dry Reed Relays. Solenoids on moulded bobbins

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D.C	Coil Resistance	Reed Switches	Price
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Multip	le Reed Relay, Re	f. 53001. Contains	13 nor-
mally	open reeds within	n a solenoid. Opera	ates on
600 70	W Cail registers	oe OK ohmy Price	£1.95

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well as for maximum r.p.m. indications mentioned previously for the different number of cylinders.

CONSTRUCTION

The circuit board and component layout is shown in Fig. 2. The board can be quite small and could be either mounted on the back of the meter as shown or installed behind the dashboard by itself but it must be clear of the direct airflow from the car heater

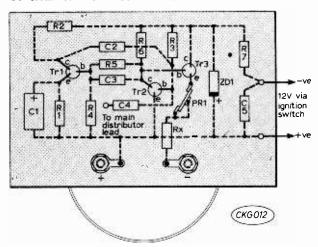
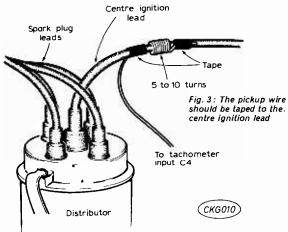


Fig. 2: A suggested component layout. The board is mounted directly on the terminal screws of the meter.

system. In the prototype the board was attached to the back of the meter by the terminal screws. The component layout is not critical and can be altered a little from that shown in Fig. 2. It is most important however, not to connect the common positive supply rail of the circuit directly to either the car body or meter case. The circuit will be effectively 'earthed' via whichever lead, positive or negative, is connected eventually to the car body i.e., via whichever side of the car battery is bonded to the car body. The 12V supply should be taken after the ignition switch.

The only other connection is a length of thin plastic covered wire from the tachometer input C4 which is taken through to the centre ignition lead on the distributor. The end of this wire is wrapped around the centre ignition lead and taped into place as shown in Fig. 3. Between 5 and 10 turns should be sufficient for ignition pulse pick up.



CALIBRATION

The ideal method of calibrating the meter is to drive the tachometer from a square-wave audio signal generator. The square-wave should have a peak amplitude of at least 2V and must be differentiated by a simple RC network as in Fig. 4. The output will

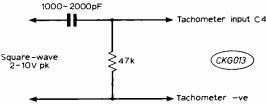


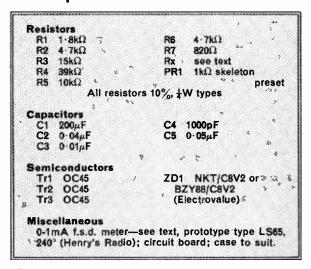
Fig. 4: The differentiating circuit for calibration.

be a series of positive and negative going pulses. The tachometer will respond to the positive going pulses only. It is essential to understand that when the tachometer is driven from a car ignition system (from the centre distributor lead) it will receive either four, six or eight pulses for *each* revolution of the engine, depending on the number of cylinders. The engine r.p.m. will therefore be the number of pulses per minute divided by the number of cylinders. For example, if the pulse frequency per minute is 10,000, the r.p.m. for a 4 cylinder engine would be 2,500. For calibration with a signal generator it is easier to work with *pulses per second*, so in order to set the tachometer scale for say 2,500 r.p.m. the generator frequency is set to

$$\frac{10,000}{60} = 166 \cdot 6$$
Hz.

It would be easier of course to set the generator to an even frequency so, for example, 200Hz would be equal to 12,000 pulses per minute (200×60) or 12,000/4 which equals 3,000 r.p.m. for a 4 cylinder engine.

* components list



Most meters, including the 240° type, will have calibration marks of 0 to 10 which is convenient for either 0-5,000 or 0-10,000 r.p.m. The meter scale can of course be taken out and new figures inscribed.

A scale of 0-8.000 would mean providing new calibration marks of 0-8 i.e., the scale must be divided into 8 equal parts. The maximum r.p.m. range must therefore be decided and the meter scale marked accordingly.

Having done this the instrument can be calibrated and to assist in this the following tables relate r.p.m. to frequency and number of cylinders.

Four Cylinder Engines

Engine R.P.M.	Pulses per	Generator
	minute from	Frequency (Hz)
1	ignition	
500	2,000	33.3
1,000	4,000	66 · 6
1,500	6,000	100
2,000	8,000	133 · 3
2,500	10,000	166 · 6
3,000	12,000	200
3,500	14,000	233 · 3
4,000	16,000	266 · 6
5,000	20,000	333 · 3
6,000	24,000	400
7,000	28,000	466 · 6
8,000	32,000	533 · 3
9,000	36,000	600
10,000	40,000	666 · 6

The suggested calibration checks for 0-5,000 r.p.m. are as follows:- Set the generator to 200Hz and adjust PR1 to obtain meter reading of 3,000 r.p.m. Set generator at 100Hz and check that meter is reading 1,500 r.p.m. If not, slightly re-adjust PR1 and check again for reading at 3,000 r.p.m. Much the same procedure is adopted for higher maximum r.p.m. readings i.e., for 8,000 r.p.m. full scale use a 400Hz test signal and set PR1 for a reading of 6,000 r.p.m. and check with 200Hz for a reading of 3.000 r.p.m. For a 10,000 r.p.m. maximum set generator to 600Hz and PR1 to obtain meter reading of 9,000 r.p.m. Recheck at 3,000 r.p.m. with 200Hz.

Six Cylinder Engines

Engine R.P.M.	Pulses per minute	Generator
	from ignition	frequency (Hz)
500	3,000	50
1,000	6,000	100
2,000	12,000	200
3,000	18,000	300
4,000	24,000	400
5,000	30,000	500
6,000	36,000	600
7,000	42,000	700
8,000	48,000	800
10,000	60,000	1,000

As the generator test frequencies all come out at even figures the calibration for six cylinder engines for any maximum r.p.m. reading of up to 10,000 is quite easy but a similar procedure i.e., the initial setting of PR1 for a high calibration reading and then check at a lower one, can be adopted.

No table is included for 8 cylinder engines as the 4 cylinder engine table can be used by simply doubling the test frequencies.

CALIBRATION WITHOUT A **GENERATOR**

With a square-wave generator a calibration accuracy of better than 1 per cent can be obtained, especially if the generator is first checked for

accuracy against the 50Hz mains frequency with an oscilloscope and Lissaiou's patterns.

Reasonable accuracy, however, can be obtained by setting the value of PRI with an ohnmeter. The table shows the values at which PR1 should be set to obtain 0-5,000, or 0-8,000 or 0-10,000 r.p.m. for a 4 or 6 cylinder engine. For 8 cylinder engines the value of PR1 will be double those of the 4 cylinder

Value of PR1 plus Rx for simple calibration

Max. Revs.	Four Cylinders	Six Cylinders
5,000	18012	500Ω
8,000	52012	1,200Ω
10,000	80012	1,500Ω

In operation the meter needle will waver slightly about the engine r.p.m. reading. Violent fluctuation or erratic indication could be due to ignition pulse pick up being too great, in which case reduce the number of turns of the pick up coil. From tick-over the needle should rise quickly as the accelerator is pressed down. Don't rev the engine just to see the tachometer read maximum r.p.m., it won't do the engine any good. For test purposes about half the engine maximum r.p.m. will be sufficient to see that the tachometer reading rises accordingly.

CQ! CQ! CQ! CQ! CQ! CQ!

INFORMATION WANTED
...any Information or circuit literature etc. on the Practical Wireless "Strand" amplifier.—G. A. Hocknell, School House, King's School, Canterbury, Kent.
...circuit designs for a car anti-theit device of the tuned circuit or capacitance type.—
R. E. Hannah, 16 Witton Way, Rainford, Nr. St. Helens, Lancashire.
...Heatinkit manual for kit EW-1. To be borrowed or bought for £1.—W. Amman.
1 Montague Avenue, London, S.E.4.
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...clrcuit diagram, alignment information and operating instructions for the Latayette KT 320 communications receiver.—A. D. Temple, 56 Wood Road, Chorlton, Man-

Chester.

Instruction books and spares for the Invicta 500 and 300 a.c.—Ralph Hamilton.
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....any lechnical Information regarding the photomultiplier tube type 931 A.—A. J.
Dickinson, 22 Kensington Place, Brighton, Sussex, BN1 4RJ.

...any Information, diagrams, etc., on Pamphonic type 601F amplifier with 2 x EL34,
one US6 and six other valves. Also any of the following issues of P.W.: June 1966,
July 1964, June and January 1963, December 1962, September 1962 or earlier.—M.
McLean, Stamford Villa, Station Avenue, Haddington, East Lothlan.

...any details of the power transformer of the Cossor scope model 1039 Mk. 2.—
David Snodley, 9 Alexandra Park Avenue, Belfast BT 153ER, N. Ireland.

...the book entitled "Oscilloscope Equipment Circuits" by Easterling (Norman Price—out of print). Will buy or borrow.—F. D. Cosgrove, Rowan Chalet, Lower Road, Postcombe, Oxford, OX9 7DU.

ISSUES FOR DISPOSAL ...P.W. for May 1969 to December 1970. Offers please to N. J. Moore, 33 Highcliffe Drive, Leliph-on-Sea, Essex.

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AF239	0 - 37	2N711	0.50
AFI86	0 - 50	2 NI302-3	0 - 20
AFI39	0 · 37	2N1304-5	0 · 25
BC154	0 · 25	2N I 306-7	0 · 30
BC107	0 · 13	2N1308-9	0.35
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BF274	0 - 15	OC20	0 - 50
BFY50	0 · 20	OC23	0 - 30
BSY25	0 · 57	OC25	0 · 25
B5Y26	0 · 13	OC26	0 - 25
BSY27	0-13	OC28	0 · 30
BSY28	0 - 13	OC35	0 - 25
BSY29	0.13	OC36	0 · 37
BSY95A	0 - 15	AD149	0 · 30
OC41	0.13	AUY10	1 - 25
OC44	0.13	25034	0 · 25
OC45	0 13	2 N3055	0 - 63
QC71	0.13		
OC72	0 - 13	Diodes AAY42	0.10
OC81	0.13		0.19
OC81D	0:13	OA95 OA79	0.09
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1-watt Zener Diodes 7.5, 24, 27, 30, 36, 43 Volts	5 p	4p	Зр
10-watt Zener Diodes 5-1, 8-2, 11, 13, 16, 24, 30, 100 Volts Micro Switches, S/P, C/O 1-amp Bridge Rec's 25-volt	20p 25p 25p	17p 20p 22p	15p 15p 20p

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Adapting for **SSB**Reception

OR amateur band reception a receiver able to resolve s.s.b. (single sideband) signals is essential. This mode of telephony transmission is used almost exclusively on many amateur frequencies.

Home-constructed or commercial receivers which have no b.f.o. (beat frequency oscillator) cannot be used at all for s.s.b. reception. Other receivers, of communications type but not of recent manufacture, will have a b.f.o., but unsuitable injection, or no product detector and as a result, s.s.b. reception may be poor, unsatisfactory, or tricky.

Fortunately it is easy to overcome these difficulties, by constructing a separate b.f.o. or product detector, and inserting it into the circuit. The older type of communications receiver is then generally able to give excellent s.s.b. reception.

TRANSMISSION MODES

Three main modes of transmission are commonly employed on the short wave bands. A receiver can only produce intelligible signals from those modes for which it is equipped to deal.

AM. Amplitude modulated signals are the usual speech and music obtainable with any domestic receiver. The presence of a carrier allows detection with a diode or other detector.

SSB. With single sideband signals the carrier and one sideband are suppressed, only the other sideband being transmitted. This allows the whole transmitter power to give useful signals, instead of power being wasted on the carrier, as in a.m. To resolve s.s.b. the receiver must provide a carrier which can be

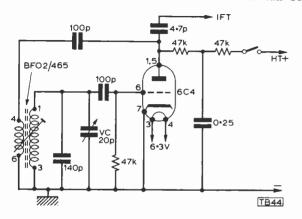


Fig. 1: Simple valve b.f.o. mainly intended to allow reception of c.w. signals.

adjusted in frequency to replace that suppressed before transmission.

CW. CW, or Morse, is a carrier only, interrupted by keying, and the presence of a beat frequency oscillator in the receiver will result in an audio tone. If the receiver has no b.f.o. the same conversion which allows s.s.b. reception will also permit c.w. reception.

BFO

Fig. 1 is a typical b.f.o. circuit for valve receivers. using readily available components. The Denco BFO2/465 b.f.o. coil is suitable for receivers having an intermediate frequency of 455-470kHz. If the circuit is constructed as an addition to a receiver having no b.f.o., the small 6C4 triode is ideal requiring only $0\cdot15A$ at $6\cdot3V$ for the heater. When more convenient, one section of a twin triode may be used instead.

The few components are readily assembled on a small chassis or plate. Variable capacitor VC has an extension spindle, or is so placed that it can be controlled by a knob on the receiver panel. The b.f.o.

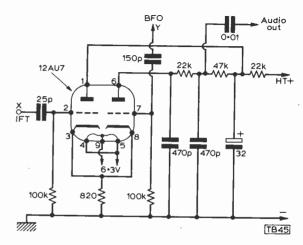


Fig. 2: Twin triode product detector. Used with the b.f.o. it permits satisfactory resolution of s.s.b. signals.

unit is bolted to the main receiver chassis close to the last i.f. transformer.

A 180-250V h.t. supply is suitable. A refinement is to use a stabilised 150V supply, but this is not essential. A switch, anywhere convenient on the panel, interrupts the h.t. supply for a.m. reception.

The circuit is adjusted by placing VC half closed, tuning in a signal, and rotating the b.f.o. coil core until the audible beat falls to zero. Turning VC slightly either way will then cause an audio note which rises in frequency.

For c.w. reception, VC is adjusted to that position which gives best results with the wanted Morse signals.

INJECTION ON SSB

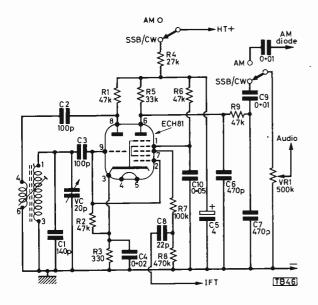
With such a b.f.o., or an older receiver having a similar b.f.o., satisfactory s.s.b. reception is only possible when the s.s.b. signal is weak at the detector. This means that the receiver r.f. gain (and possibly i.f. gain) control must be turned towards minimum

gain, the a.f. gain near maximum. The s.s.b. signal can then be resolved if the b.f.o. frequency is tuned so that it replaces the carrier removed before transmission.

One way to improve matters with the minimum of circuit change is to increase the b.f.o. injection at the final i.f.t. With some receivers, the coupling capacitor (4·7pF in Fig. 1) is of extremely low value, less than 1pF. Changing this to a 3-30pF or similar trimmer will allow increased injection. It is then possible to deal with s.s.b. signals of somewhat greater strength at the detector. The improvement is only relatively slight and insufficient carrier will be available from the b.f.o. to allow the a.m. type detector to deal satisfactorily with strong s.s.b. signals. These, if resolved, will sound like distorted, much over-modulated a.m.

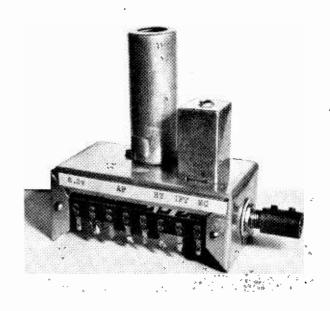
PRODUCT DETECTOR

Fig. 2 is a straightforward standard product detector using a twin triode, cathode coupled, which was found to give very good results with the minimum of difficulty.



Point X is taken directly to the secondary of the last i.f.t. This tag will have previously been wired to the a.m. detector diode. Point Y is connected to the b.f.o. stage anode. (A few commercial circuits use a tap on the b.f.o. coil for the cathode, with the anode grounded for r.f. In this case, take Y to the b.f.o. cathode.)

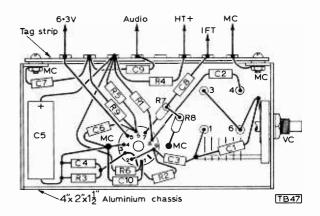
Component values were not found to be particularly critical. The $32\mu F$ capacitor is to ensure a decoupled and well smoothed h_* t supply. The audio output runs to the volume control on the first a.f. amplifier. This circuit was found to work very well indeed over a wide range of s.s.b. signal strengths, from extremely weak signals barely audible, to those giving much more loudspeaker volume than could be tolerated without reducing receiver gain.



▲ Completed product detector/b.f.o. unit using the single valve circuit of Fig. 3.

➡ Fig. 3: Circuit using an ECH81 as combined product detector/b.f.o.

▼ Fig. 4: Suggested component layout of circuit shown in Fig. 3.



PRODUCT DETECTOR WITH B.F.O.

The circuit in Fig. 3 has only one valve, an ECH81. B.f.o. injection is to grid 1 of the heptode section, with signals from the final i.f.t. to grid 3. The triode of the ECH81 acts as the b.f.o. oscillator for carrier insertion.

The main advantage of this circuit is that it needs only one valve, and a 2-pole 2-way switch provides for a.n., s.s.b. or c.w. reception. One pole applies h.t. to the ECH81 while the other pole transfers the receiver audio gain control from the usual a.m. detector to the product detector.

All the components may be assembled on a small chassis, Fig. 4 shows suggested construction and wiring. A similar method of building can be adopted with the circuits in Figs. 1 and 2.

The unit is completely wired and tested, then bolted to the receiver chassis, with VC extended

through the panel. The b.f.o. section should be adjusted in the way described for Fig. 1.

TRANSISTOR RECEIVERS

These can be adapted with equal success, and the changes are particularly useful for those receivers which cover several amateur bands.

Fig. 5 is a b.f.o. circuit using a Denco IFT14 coil, for receivers with 465kHz or similar intermediate frequency. A simple method of assembly is to fit the b.f.o. coil, transistor, Z1, resistors and capacitors on a small circuit board, which can be mounted near the 20pF variable capacitor VC, which is attached to the receiver panel. The switch in the negative line cuts the oscillator for a.m. reception and can be located anywhere convenient. The layout should provide a short, direct connection from X to the last i.f. transformer.

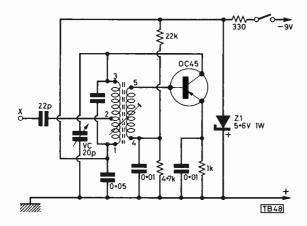


Fig. 5: Circuit of b.f.o. for use with transistorised receiver.

A zener stabilised supply is essential for the oscillator. Most receivers have an audio output stage in which the current drawn fluctuates with the audio signal level and this may cause troublesome frequency modulation effects in the oscillator. The circuit draws about 10mA.

Fig. 5 alone is satisfactory for c.w. reception. It will also provide reception of s.s.b. when the strength of the s.s.b. signal is limited in the way described for Fig. 1. An a.m. signal should first be tuned in and VC set half closed. The coil core is then adjusted as for

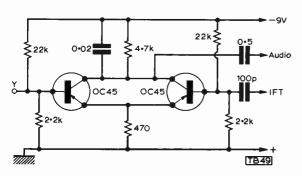


Fig. 6: Two transistor product detector used in conjunction with the b.f.o. of Fig. 5.

Fig. 1 Varying VC then allows best reception of c.w. or s.s.b. signals.

Fig. 6 is a product detector which can be used in conjunction with Fig. 5. It has the advantage of providing a.m. detection when the b.f.o. is switched off, so that no switching of audio circuits is required.

Carrier injection is at Y, from point \hat{X} in Fig. 5. Signals reach the second transistor via the 100pF isolating capacitor. This connection may be to the primary or secondary of the last i.f.t. in the receiver, according to which gives the better results.

Audio output is taken to the usual audio gain control. Other transistors of similar type may be used, and the supply to this part of the circuit need not be stabilised. With transistor receivers, a diode generally provides a.g.c. and a.m. detection, and this diode can be retained for a.g.c. purposes. In many circuits a $5k\Omega$ potentiometer serving as a.f. gain control is also the diode load resistor. As this is now not available for this purpose, a $5.6k\Omega$ resistor should be substituted.

Most transistor receivers have no manual gain control for the i.f. stages (or r.f. stage, if present) and since such a control is useful for s.s.b., it can be inserted by disconnecting the i.f. stage emitter resistors and adding a $2k\Omega$ potentiometer between this point and the positive line.

NOTES

Some receivers have a $1\cdot 6MHz$ i.f. in which case the appropriate b.f.o. coil must be used (Denco BFO2/ $1\cdot 6$).

When adjusting the variable capacitor VC, the b.f.o. must be put on the correct side of the s.s.b. transmission. Speech can then be resolved and VC carefully adjusted for the best results. If VC is altered to put the b.f.o. on the wrong side of the s.s.b. signal no possible adjustment will resolve the signals. The manner of adjusting VC, for upper or lower sideband signals as the case may be, will soon become clear in use. The standard practice is upper sideband (USB) above 10MHz and lower sideband (LSB) below 10MHz.

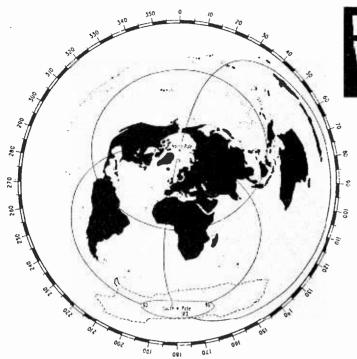
When making or altering connections to the last i.f.t., alignment may be slightly upset. So a final check should be made of this, and the i.f.t. cores re-adjusted for best results.

In some circuits, the same diode is employed to obtain a.g.c. voltage and a.m. detection. Then when a b.f.o. is added as in Fig. 1, its carrier will produce an a.g.c. voltage, reducing sensitivity. This still arises when a.g.c. is derived from a separate diode, usually with a small capacitor to the last i.f. anode. With a circuit like Fig. 2, the a.g.c. can be left in use. Otherwise a switch may be added, to short the a.g.c. line to earth for s.s.b. or c.w. reception. Communications type receivers generally have a manual control for r.f. gain, i.f. gain, or both. If this is not present in a receiver, it should be fitted. A cathode bias potentiometer is generally employed.

Bandspread tuning, or an excellent slow motion drive, will be found helpful for s.s.b. reception.

Normal circuit precautions should be taken when wiring. The i.f. leads should be short, and clear of earlier i.f. circuits. H.T. and heater leads can run against the chassis. Where a.f. circuits are extended, as for Fig. 3, the leads should be screened, or carefully placed to avoid picking up hum from heater circuits.

FREE INSIDE NEXT MONTH'S ...



WALL CHART

Next month your QSL cards will have a companion—our DX DATA WALL CHART—and it's one that you'll keep for years. Features include a P.W. Exclusive: a specially designed frequency allocation chart giving all broadcasting and amateur bands, shipping and aeronautical frequencies and a lot, lot more—much of this information has never before been published in this country. PLUS a large great circle map based on London to give true distances and bearings together with a World Time table and International Call Sign allocations.

ARTICLES INCLUDE:

the PVV CUBE RADIO 7 Transistor Superhet

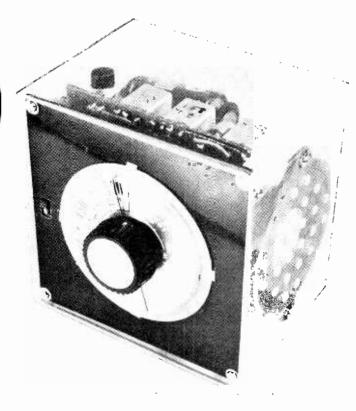
With "Novelty Radios" the emphasis is more often on the 'novelty' rather than the 'radio'; the electronics is sacrificed to the appearance. But not in ours. Built into a perspex cabinet, the **P.W. CUBE RADIO** is a full seven transistor superhet receiver giving exceptional performance for its size. Be sure not to miss this one; full details are given to build this ingenious project.

DARKROOM THERMOMETER

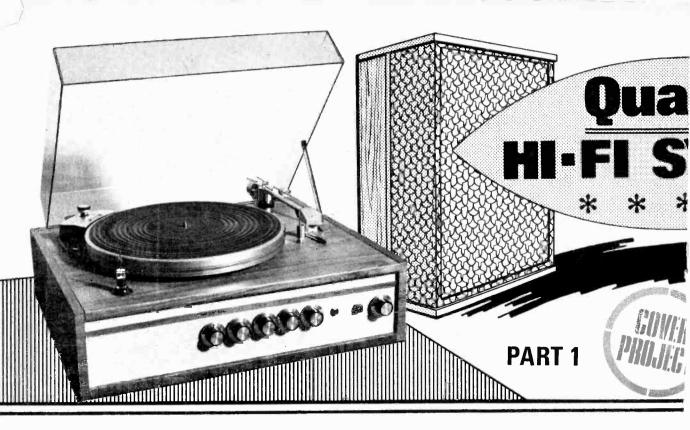
We don't want to deride conventional thermometers but from the photographers point of view they leave a lot to be desired in the darkroom. This circuit uses a thermistor and has rapid response, is very easy to read in the worst light and is accurate to within 0.25°C—and all this with a mere handful of components.

CAR RADIO SIGNAL BOOSTER

This simple amplifier gives a useful improvement in MW and LW reception on any car radio. It has the feature that it is designed for mounting at the base of the aerial to overcome interference pickup. The total cost for this project is something under 50p!



ALL IN THE MARCH ISSUE ON SALE FEB. 4th.



SELECTING the units of a hi-fi system these days is mainly an exercise in economics. The more expensive equipment from any of the many reputable makers will invariably give a good performance as the specification is the prime selling feature in this market. There is a danger not so much of getting poor value for money in the separate units (of the chain turntable-cartridge-amplifiers-loudspeakers) but of budgeting unevenly so that the performance of some links in the chain exceeds that of others. When this happens, the system's performance is somewhat below that of its worst component and the unexploited potential of the better units can be regarded as so much wasted money.

There are three basic units in the design to be described. They are:

The plinth which contains the turntable, amplifiers and controls, and two identical floor-standing loudspeaker enclosures.

Either design may be of interest for use with other equipment, but together they form a well matched system in which no performance is wasted. The three units are finished with teak veneer to match in appearance.

The Plinth

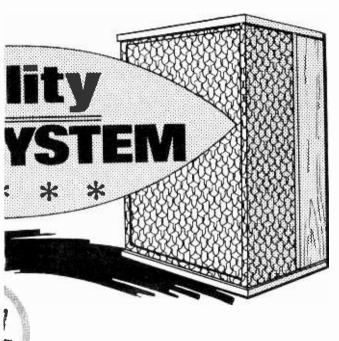
The plinth carries the turntable and separate pickup arm. These are covered by a hinged transparent tinted lid. This props in an open position for changing records and can be closed while playing. Inside the plinth is the power supply for the system, the preamplifiers which are in the form of two plugin boards, and the power amplifiers. These are a

fairly new type of hybrid Class AB module with a rating of no less than 25 watts r.m.s. each into the correct loudspeaker loads. On the front of the plinth are all the controls for the system, with space provided for future expansion. This might be the addition of an in-built f.m. multiplex tuner, or audio filters.

The Loudspeaker Enclosures

The loudspeaker enclosures are intentionally massive. The author regards their internal volumes of 8 cubic feet as essential to reproducing the full bass content of modern records. A separate woofer and tweeter, fed separately by a crossover network and brilliance control, are used in each enclosure. The enclosures are the infinite baffle type, i.e. are completely sealed. This type is only effective if it is completely airtight, and there is no flexing of the enclosure walls under low frequency sound pressure. To achieve the densest possible structure, the vertical walls are a sandwich of two sheets of hardboard with a lin. gap between, packed with fine sand. The top, bottom and speaker mounting boards are solid lin. thick chipboard. To minimise internal reflections the interior is heavily damped with carpet felt. The felt is not attached directly to the inner surfaces, but is spaced about 112 inches away from them by a layer of fibre egg-crate material for better reduction of standing waves. The internal height, width and depth are in the ratios 3:2, again to reduce standing waves. The front and the forward parts of the sides are covered with Tygan fret, other visible parts are veneered in teak.

When the walls are filled with sand, each speaker can hardly be lifted by four men! But the payoff is



C.R. BRADLEY

that with a good stereo record, the complete orchestral volume can be reproduced with a bass realism that is truly free of resonance, boxy-ness or boomy-ness. Midrange and treble performances are also very satisfactory, with no harshness. The speakers have a crisp presence which can be modified by a 6-position Brilliance control for best stereo directionality in a particular room.

Construction of the Loudspeaker Enclosures

Each identical enclosure is based on a skeleton frame made up from nominally lin. square pine, which when bought usually turns out to be nearer τ_8 in. square—see Fig. 2. Saw the lengths listed as accurately as possible with the ends square. No difficult joints are required, the pieces being simply butted together and fixed with countersunk 1^1 2in. woodscrews at the ends.

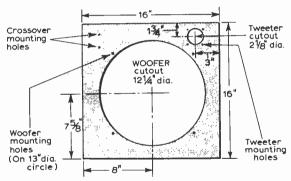


Fig. 1: Speaker mounting board, rear view.

The system to be described in this series embodies the author's ideas on the best way to spend about £130 on stereo record plaving equipment. A fair amount of carpentry is required but no special skill. Constructors may well introduce modifications to the design but if the system is built as described, one will obtain a very high standard of reproduction at a cost so far below that of equivalent commercial equipment (there is nothing sufficiently similar for a direct comparison anyway) that the saving is hard to calculate. The best assessment the author can offer of the pleasure the system provides is that he has not yet heard any commercial equipment for which he would care to swap his system.

The speaker mounting board is cut from lin. chipboard to suit the units specified—see Fig. 1. The large cutout for the woofer is easiest made with a jigsaw, or more laboriously by drilling holes around the circumference and knocking out the middle. Use wood that is perfectly flat or the woofer chassis may be irreparably distorted when it is screwed down. The board should fit snugly in the centre of its aperture in the frame. The join at the top must be airtight, which is ensured by gluing a strip of wood ('S' in Fig. 1) along the outside of the join; this piece also keeps the top edge of the fret straight.

The inner hardboard sheets can now be fitted. These must be cut accurately or there will be problems of inward sand leakage. They are screwed from the inside to the frame by screws every 6 inches approx. Their vertical edges simply butt together and these joins must be made sand-tight by a wide strip of adhesive tape (e.g. 2in. Tuftape) stuck along the outside i.e. just behind the four corner verticals. Drill the small hole for the speaker leads at the centre of the inner rear sheet.

Cut out the outer hardboard sheets, again accurately. Make an appropriate cutout in the rear sheet at bottom centre for a small aluminium panel to carry the terminals and the brilliance control; this is made up along the lines indicated in Fig. 3. Mount the panels in place, without sand, and fix with countersunk screws every 6 inches approx. Paint the entire front of the enclosure and the forward 10in. of the sides matt black so the speaker cutouts will not be visible after the fret is fitted.

Next cut out and fit the top and bottom pieces (both lin. chipboard). Screw down firmly and check that the fit is reasonably airtight, planing the surfaces if necessary.

Sand Panels

The sand filling can now begin. The sand used is fine beach sand, usually available from seed merchants. The author used 'real' beach sand but this had first to be dried thoroughly (in the kitchen oven!) and sifted free of pebbles. The filling must be done as follows to minimise the strain on the enclosure structure.

QUALITY HI-FI SYSTEM-SPECIFICATION

PLINTH SPECIFICATION

PREAMPLIFIERS (two)

General: Each preamplifier consists of a circuit using four silicon planar transistors and is wired on a piece of Veroboard which plugs into a 24-way edge connector.

Frequency response: 10Hz to 30kHz (-3dB points)
Disc equalisation: RIAA microgroove standard
Signal-to-noise ratio: Better than 80dB

Input impedances and sensitivities: (for 400mV

TUNER: 150 mV into $500 \text{k}\Omega$ DISC: 4 mV into $47 \text{k}\Omega$

AUXILIARY: 300mV into 500kΩ (Alternative sensitivities possible e.g. to suit crystal or ceramic devices)

Tape output: 3.5 mV into $10 \text{k}\Omega$, 350 mV into $2 \text{M}\Omega$ Distortion: Below 0.15% (on 400 mV output); at least 20dB overload possible (i.e.: 4 V output) without serious distortion.

Tone controls: Baxandall type giving approx. 20dB max. boost and cut at 20Hz and 20kHz

AMPLIFIERS (two)

General: Each amplifier is a Sanken SI-1020A hybrid module containing a complete single-ended push-pull Class AB amplifier on an isolated heat sink. (6 transistors).

Frequency response: 20Hz to 100kHz

Output power into 8 ohm load: 25 watts r.m.s. continuous, approx. 40 watts peak.

Distortion: Below 0.1% at usual listening levels (see graph)

Short circuit protection: Can be adequately protected by a 1 amp power fuse.

FRONT PANEL LAYOUT

RADIO - DISC - AUXILIARY, VOLUME, TREBLE, BASS, BALANCE, Stereo headphone outlet, Pilot lamp, OFF - HEADPHONE - SPEAKERS.

REAR PANEL

Stereo radio, auxiliary and spare inputs, and stereo tape recorder output (all phono sockets).

Left, right and common loudspeaker connections (screw terminals)

POWER SUPPLY

General: Unstabilised, silicon bridge rectifier.

Outputs: Separately fused 45V, 1A supplies to amplifiers; 30V (low ripple) to preamplifiers.

ENCLOSURE SPECIFICATION

TYPE: Two-way floor-standing infinite baffle, sand loaded walls.

SIZE: 38in. high x 27\fin. wide x 18\fin. deep overall approx.

TWEETER:

Type: Eagle MHT10, metal diaphragm with exponential horn type

Quoted response: 2kHz to 18kHz Flux density: 13,000 gauss Impedance: 8 ohm

WOOFER:

Type: Baker Major 12in.
Quoted response: 30Hz to 14·5kHz
Flux density: 14,000 gauss
Voice coil: 14in. diameter, 8 ohm impedance
Main cone: paper with roll surround, fitt

Main cone: paper with roll surround, fitted with concentric parasitic cone for higher frequencies Mounting requirements: 11in. diameter aperture,

four fixing holes on 13in. diameter circle.

CROSSOVER:

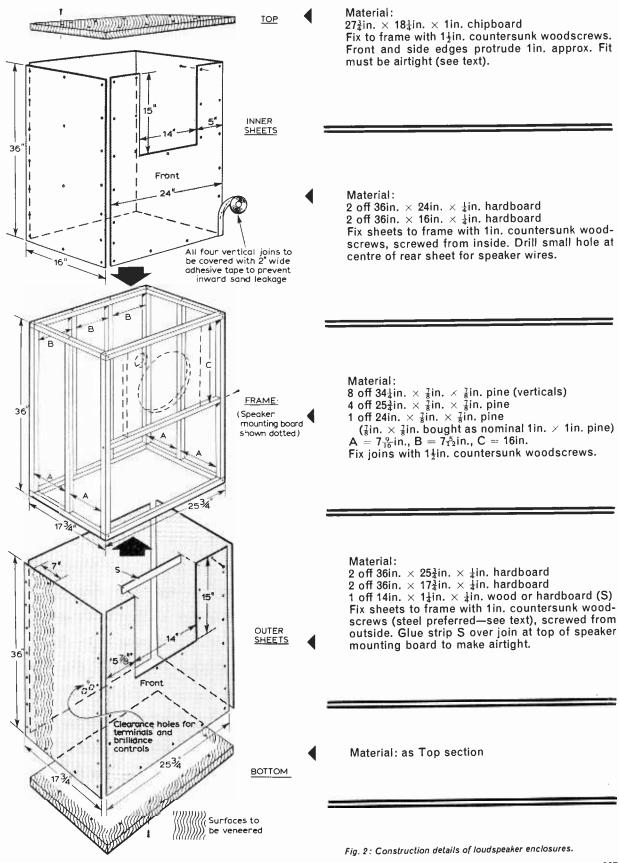
Eagle type CN28, 8 ohm series LC type Crossover frequency: 3kHz

BRILLIANCE CONTROL:

Six-position resistive attenuator, unmatched.

Lay the enclosure on one side. Remove the uppermost panel and use rubber solution or putty to seal any possible leakage points in the two sand compartments revealed. Ensure that all the other panels are screwed on firmly to give strength to the structure. Fill the compartments with fine sand and level off. Replace and screw down the outer panel checking that no sand is trapped between it and the frame to spoil the seal. Also be sure no sand enters the screw holes or the screws may break; steel screws are preferable to brass for this reason. Tip the enclosure on

its back, supporting it as necessary to avoid crushing the rear terminals and brilliance control. Remove the outer front panel and fill the compartments with sand as before. Next fill the remaining side, and lastly the back. At this stage the connecting wires can be laid through the sand from the aluminium panel to the hole in the inner rear panel, which must be sealed with rubber solution to prevent inward sand leakage. Before fitting the back, be sure that the brilliance control switch is well sealed against sand ingress by means of a polythene bag or something similar.



Mount the woofer, tweeter and crossover, and connect them as shown in Fig. 4. This is a convenient stage at which to start running the speaker since the sound vibration will help shake down the sand. For the woofer the manufacturer recommends a 'running in' period at less than full power. The sound quality will not be good until the damping material is fitted as follows.

Obtain some large corrugated fibre (not plastic) egg-crates such as most grocers throw away. Glue these over the whole inside area of the enclosure including the top and bottom pieces, but not the speaker mounting board. Allow plenty of ventilation as the glue vapour might possibly be harmful to the woofer. The egg-crate alone provides some acoustic damping but it serves mainly to space the carpet felt away from the inner walls. This felt should be the

Fig. 3: Theoretical diagram showing

loud speaker enclosure circuitry.

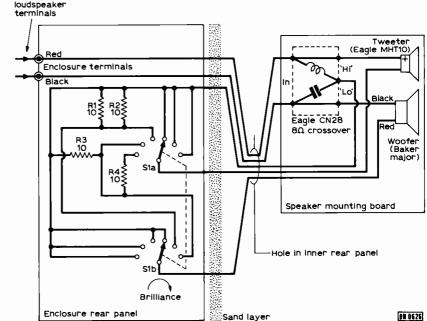
From plinth

heaviest grade obtainable and most carpet dealers will have suitable offcuts. A single piece can be used for the whole enclosure apart from the top piece. Fix the felt in place by tacking down the edges all round so the egg-crate volume is sealed off.

Again check the fit of the top and bottom pieces for airtightness. The danger here is that the weight of the sand may have warped the frame. If necessary a thin strip of expanded polystyrene or draught excluder can be used to pack any gaps. Once airtightness is ensured the enclosure is functionally complete.

The author decided to cover as much as possible of the enclosure with Tygan loudspeaker fret (maroon/gold pattern). A 36in×54in, piece of this is enough to cover the whole of the front and part of the sides. This is cut into three pieces and glued to the panels

continued on p 91



Wires passed through sand and Inner rear panel Aluminium panel fixed to rear of enclosure (rear view) (Eagle MHT10) Ήi Brilliance Eagle CN28 80 crossover Black Woofer Speaker mounting board Insulated Polythene bag to seal terminals Red(**⊚**)Black switch against sand DN 0625

Fig. 4: Wiring details of each loudspeaker enclosure. Observe polarity of woofer and tweeter connections for correct phasing.

SUPERSOUND 13 HI-FI MONO AMPLIFIER



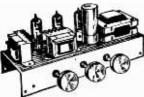
A superb solid state audio amplifier. Brand new components throughout. 5 silicon transistors

plus 2 power out-put transistors in push-pull. Full

3db. Fully integrated pre-amplifier stage with separate plume, Bass boost and Treble cut controls. Suitable for Volume, Bas 8-15 ohm sp Volume, Bass boost and Treole cut controls. Suitable for 8-16 ohm speakers. Input for ceranic or crystal cartridge. Sensitivity approx. 40mV for full output. Supplied ready built and tested, with knobs, escutcheon panel, input and output plugs. Overall size 3" high x 6" wide x 7½" deep.

PRICE £10.50. P. & P. 25p.

DE LUXE STEREO AMPLIFIER



A.C. mains 200-240 v. Using heavyduty fully isola-ted mains transform transform-er with full wave recti-fication giving ade-quate smoothing with negligible hi

Valve line up: -2 × ECL86 Triode Pentodes 1 × EZ80 as rectifier. Two dual potentionieters are provided for bass and treble control, giving bass and treble boost and cut. A dual volume control is used, lialance of the left and cut. A dual volume control is used. Instance of the left and right hand, channels can be adjusted by means of a sepa-rate. Balance' control fitted at the rear of the chassis. Input ensitivity is approximately 300mly for full peak output of 4 watts per channel (8 watts mono), into 3 ohm speakers. Pull regative feedback in a carefully calculated circuit, allows high volume levels to be used with negligible distortion. Sumplied complete with knobs chassis after distortion. Supplied complete with knobs, chassis size 11"w × 4"d. Overall height including valves 5". Ready built & tested to a high standard. PRICE 28-92 P. & P. 45p.



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All Transistor F.M funer head with twin A.M. Gang incorporated. Beautifully engineered with precision geared reduction drive. FM RF Transistor, oscillator/Mixer and first I.F. stage (10.7 Mc/s output) with optional AFC connection. Built on printed circuit panel and fully screened. Extrenely stable over range 88-108Mc/s. Brand new and pre-aligned. Size 2½ The X 1½ w X 2½ U. For 6v D.C. at 2.8m A. A. Gang fitted with trimmers which can be connected to standard A.M. aerial and oscillator circuits if required. LIMITED NUMBER. Only \$2.25 post free. Connection details supplied.

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circuit diagram and connection details. 24 each, Post Free. IFPUT MATCHING TRANSFORMER. Beautifully made in heavy Mu-metal cylindrical case for minimum hum pick-up. Size 14° high. Y 14° dia. Ratio 150 : 1 approx. Especially suitable for matching dynamic or ribbon mikes or pick up from low to high impedance or vice versa. 75p each. Post Free.

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BRAND NEW MULTI-RATIO MAINS TRANSFORMERS. Giving 13 alternatives. Primary: 0-210-240v. Secondary combinations 0-5-10-15-20-25-30-35-40-60v. half wave at 1 amp. or 10-0-10, 20-0-20, 30-0-30v. at 2 amps full wave. Size 3in. long × 3jin. wide × 3in. deep. Price 21.75 P. & P. 30p.

Price 21.73 P. & P. 30p.

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Pri 200/240v. Sec. 9-0-9 at 500mA. 70p. P. & P. 13p.

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63p. P. & P. 13p.

4 AMP BATTERY CHARGER TRANSFORMER. Brand new. For 6 or 12v. 240v. Primary. Secondary volts rms off load 10v and 16-5v. Overall size approx. $2\frac{1}{4}^{\circ} \times 2\frac{1}{4}^{\circ} \times 3^{\circ}$. Weight 3lbs. Limited number at £1-35. P. & P. 35p.

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LATEST B.S.R. C109/C129 4-SPEED AUTOCHANGER.
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Beautifully constructed in heavy gauge "Colorcoat"
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SP25 II and III, SL66B, AT60 etc. or B.S.R. C109,
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QUALITY RECORD PLAYER AMPLIFIER MK AUGUSTI RECORD FLATER ABELIEVE AT A top quality record player amplifier employing beavy duty double wound mains transformer, ECC33, ELS and rectifier. Separate Bass, Treble and Volume controls. Complete with output transformer matched for 3 ohe speaker, Size 7in, wide x 3in, deep x 6in. high. Ready built and tested. PRICE 23.76 P. & P. 409 ALSO AVAILABLE mounted on board with output

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DELUXE QUALITY PORTABLE R/P CABINET MK II. Unout motor board size 14½ × 12in. clearance 2in. below, 5½in, above. Will take above amplifier and any B.S.R. or GARRARD changer or Single Player (except A760 and SP25). Size 18 × 15 × 8in. PRICE 24.75, P. & P. 50p.

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5in, 3 ohn 80p, P. & P. 15p, 7 × sin, 3 ohn 21-05, P. & P. 20p, 10 × 6in, 3 or 15 ohn 21-90, P. & P. 30p, E.M.I. 8 × 5in, 3 ohn with high flux magnet 21-02, P. & P. 20p E.M.I. 13½ × 8in, 3 ohm with high flux ceramic magnet 22-10 (15 ohn 22-25), P. & P. 30p, E.M.I. 13 × 8in, 3 ohm with high flux ceramic magnet 22-10 (15 ohn 22-25), P. & P. 30p, E.M.I. 13 × 8in, 3, 8 or 15 ohn with two inbuilt tweeters and crossover network 24-20, P. & P. 30p, E.M.I. 13 × 8in, twin cone (parasitic tweeter) 8 ohn 22-25, P. & P. 30p.

(parasite tweezer) o olin 22:20, 7, a 1, 30p.

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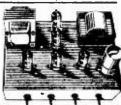
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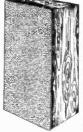
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During the first month or so of use the sand will shake down and require topping up. This can be done without removing any vertical panels if ¹4in. diameter holes are drilled through the frame at the top of each sand compartment.

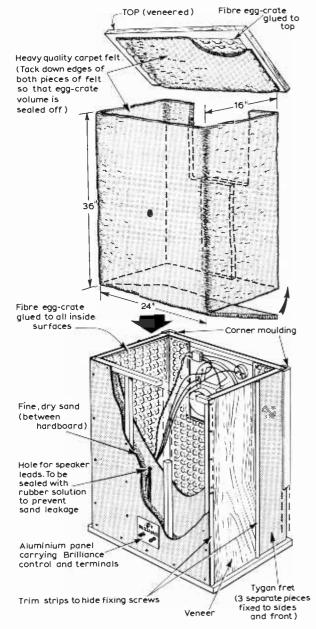
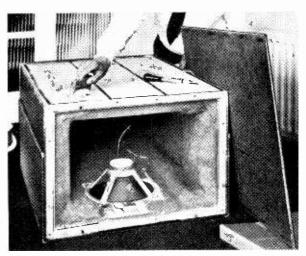


Fig. 5: Cutaway rear view of loudspeaker enclosure showing damping and external finish arrangements.

Crossover

The enclosure circuit is shown in Fig. 3. With the brilliance switch S1 in the position drawn the coil and capacitor in the ready-made crossover unit divide the incoming signal so that high frequencies pass to the tweeter and low frequencies to the woofer. The separation is not abrupt but occurs progressively above and below about 3kHz. The two frequency ranges combine again in the listener's ear so that nothing unusual should be heard. The advantage of a two-way speaker system such as this is that there is less of the intermodulation distortion which arises when a single speaker is asked to reproduce high and low frequencies simultaneously.



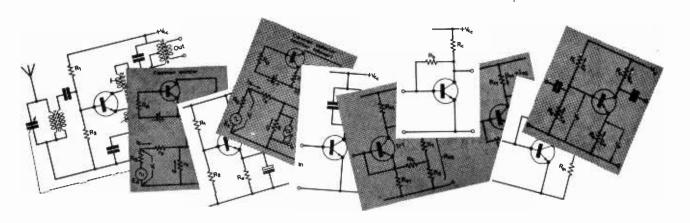
Photograph shows sand filling of a loudspeaker enclosure in progress.

Brilliance Control

The sound heard by the listener will only be satisfactory if the sound levels from the woofer and tweeter are correctly related. Several things can upset this, such as the two units having different efficiencies, the fact that the tweeter is more directional than the woofer so that the listener's position is important, and the acoustics of the room. The enclosures are therefore fitted with brilliance controls which vary the relative sound volumes from the woofer and tweeter. The subjective effect of these controls and their optimum setting for a particular room is usually quickly found. If retarded too much the sound is mellow and poorly located, if advanced too far the sound has excessive 'presence' and may seem harsh. Independent adjustment of these controls may improve the stereo 'spread' obtainable with speaker positioning which is not ideally symmetrical but dictated by the shape of the room.

It may be argued that the brilliance control must upset the action of the crossover whose component values are calculated for 8 ohm speaker loads, since it works by inserting resistance in series with the speakers. However listening tests indicated there was nothing to be gained by using a more theoretically correct version which would maintain correct matching but need many more components.

Constructional details follow for the plinth next month.



TRANSISTOR CIRCUITRY for beginners PART 5 H.W. HELLYER & MICHAEL HOLLIER

Circuit Building

Meet Mike. This month, a practical exercise in circuit building, from scratch. My friend and colleague, M. E. Hollier, is an ardent home constructor, and a gifted designer—the sort of chap who pursues a problem to the roots, even to the extent of making his own printed circuits by the photo-resist method. He has compromised to some extent this month, for our benefit, by designing and building the buffer to be described on easily obtainable Veroboard. The device is a high-to-low impedance converter. It can be used to overcome many of those difficult matching problems.

Our brief was to make transistor circuitry clear for the beginner and to be helpful to the more advanced reader. You may be surprised: I have among my correspondents an aircraft fitter who has built an electronic organ in his front room, currently valued at over seven hundred pounds, and a Ph.D. who cannot usefully wield a soldering iron. We must, as our Editor commented in his personal piece a couple of months ago, cast our nets as widely as possible.

To comply with this brief, Mike has torn a few basic circuits to bits, showing what makes them tick. This means that we shall, to some extent, be repeating some of the data I have already expounded: but repetition of salient points helps to fix them in the mind, so I'll make no excuses for that.

After digging a little into the theory, we shall construct the practical circuit, and make this the basis for future designs. The article concludes with some measurements of the constructed device, as much to illustrate the sort of deviations from pure theory that the constructor must learn to expect as to prove that the darn thing really works!

Silicon Planar Epitaxial Transistors

The most modern development in audio bipolar transistors is the silicon planar epitaxial device. We

touched briefly on these in Part 2, underlined their use in Part 3, and now come to the practical problem of using them.

Some possible troubles have been anticipated by the makers. Silicon planar epitaxial transistors such as the BC108 and BC109 that we shall be using this month, have their surfaces protected by a layer of silicon oxide which prevents contamination—which would alter the characteristics.

From the design viewpoint, working with such transistors is made easier because their collector leakage current is almost negligible. Moreover, they are easily obtainable—everybody seems to make a BC109! More about minor differences later.

Parameters

In previous articles, and in the wallchart, a choice of several parameters was given. No, let's be precise—a choice between ways of expressing transistor parameters. Our choice is determined by convenience as much as by an academic ache for accuracy. So we use, this month, the 'h' or hybrid parameter.

Hybrid, in this context, means that the symbols

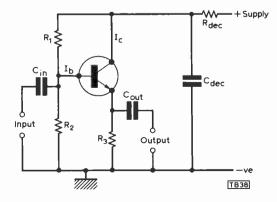


Fig. 20: Basic single stage circuit. Emitter-follower configuration.

represent a mixture of ratios, impedances and admittance values. (Admittance is impedance upsidedown; its reciprocal.)

We use the lower case 'h' as our parameter indicator, and the two subscripts after it indicate either d.c. or large-signal measurements. For example: $h_{\rm FE}$, or, small-signal, $h_{\rm fe}$. These will be explained as we need to use them.

In Fig. 20, we see an emitter follower circuit that we have met before. The emitter follower is so called because the input to the stage that comes after it FOLLOWS the emitter of the stage. Alternatively, we could call this a common collector circuit; the collector is common to both input and output signals.

The output signal is taken from $C_{\rm out}$, the live side with reference to the signal. The input is between the $C_{\rm in}$ live side and the collector. Hence, common collector. But while the earthy side of the input terminals is quite obviously connected to the negative line, we have to remember that the decoupling capacitor, $C_{\rm dec}$, presents almost a short-circuit to the frequencies we are working with. The collector line is therefore virtually connected to the earth line so far as alternating currents are concerned. Our signal is a.c.: ergo, the collector is common.

Input Impedance

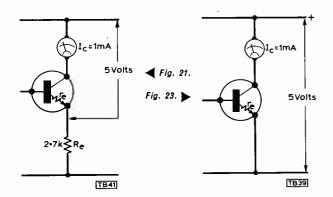
One of the constant bothers is the calculation of input impedance. It seems at first alarming, even when, as in Fig. 20, we know the component values. So we begin, as in Fig. 21, by breaking it down to fundamentals, taking the transistor with its internal resistances, r_b and r_e .

The input resistance of the transistor, looking into the base, in this grounded emitter configuration, is h_{ie} . H parameters again, but h_{ie} simply means input resistance, common emitter mode. Sometimes, we can get this easily from maker's data and there may be a graph so that h_{ie} can be plotted against collector current, Ie. Then the input resistance of the transistor can quickly be found.

If this graphical information is not immediately available, we must have recourse to a bit of simple arithmetic. The internal resistance, r_e, and h_{fe}, the small signal current gain, are what we need at first.

Whereas h_{fe} will almost invariably be specified, r_e and r_b may not. We can take r_e as around 25 ohms in a planar transistor where the collector current is about 1mA. From the known facts we obtain the formula,

$$h_{ie} = \frac{25 \text{ ohms}}{I_c \text{ (mA)}} \times h_{fe}$$



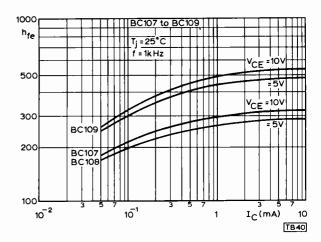


Fig. 22: Typical variation of input impedance and small signal forward current transfer ratio with collector current.

 r_b is so small in relation to the result of this formula that it can be ignored for all practical purposes.

If we take a practical example (see Fig. 21), for a BC109 operating at a collector current of 1mA, the voltage between collector and emitter ($V_{\rm CE}$) being 5 volts. From the data sheet (see Fig. 22) we find that the $h_{\rm fe}$ is 440. Putting this into the above formula, we now have:

$$h_{ie} = \frac{25}{1} \times 440$$

= 11,000 (11k \Omega input resistance).

External R.

The presence of an emitter resistor in the circuit of Fig. 21 alters the calculations. If we now look at Fig. 23 we see that the voltage reading is still across collector/emitter, but as $R_{\rm e}$ is not bypassed, the input impedance will increase by an amount equal to the resistive value of $R_{\rm e}$, multiplied by $h_{\rm fe}$. From this, we can construct a formula for input impedance, $R_{\rm in}$. Since we now have a component external to the transistor, $h_{\rm ie}$ can no longer be applied to this value of input impedance.

Let us take Re to be 2.7kΩ. Now we get:-

$$R_{in} = (R_e \times h_{fe}) + h_{ie}$$

= (2,700 × 440) + 11,000
= 1188k\Omega + 11k\Omega
= 1.2M\Omega

The input impedance can be increased by the addition of an unbypassed emitter resistor.

Base Bias

Now we develop the circuit by adding base bias resistors R_1 and R_2 in Fig. 24, and a few more voltages have to be considered. Take a collector current of 1mA. Since the base current is very small, we can say the emitter current—for practical purposes—is the same.

So 1mA through the emitter resistor, R_e , which is $2\cdot 7k\Omega$, gives us a volts drop of $2\cdot 7V$. This is the emitter voltage. To work out the required supply voltage, we take the voltage across the transistor.

 V_{CE} and add to it the 2·7 volts across $R_{\text{E}}.$ Answer: $7 \cdot 7 V.$

There is an irreducible voltage between base and emitter of a transistor and in the case of silicon transistors, this is generally 0.6V. Simple addition gives us a base voltage of 0.6+2.7=3.3 volts. The base to collector voltage must therefore be 7.7-3.3=4.4 volts.

In this form of potential divider biasing, to maintain stabilisation of the circuit, it is normal to have five times as much current flowing through the biasing resistors as the base current of the transistor.

The base current, IB, is found from the formula

$$I_B = \frac{I_C}{H_{FE}}$$

where H_{FE} is the d.c. current gain of the transistor.

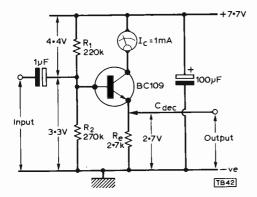


Fig. 24: The final circuit. Component values are worked out and explained in the text.

For the BC109, with an I_c of 1mA, this is typically 380.

So
$$I_B = \frac{1mA}{380} = 2.6$$
 microamps.

Taking a value of five times this we get 13 microamps. So the voltage drop across R_2 is $3\cdot 3V$, the current 13 microamps and the ohmic value of R_2 must be:—

$$\frac{3\cdot 3}{0\cdot 000013}$$
 or $\frac{3\cdot 3\times 10^6}{13}=254k\Omega$.

The nearest preferred value resistor would be $270k\Omega.$ A 5% component will do.

A different condition obtains with R_1 , which has the base current of the transistor flowing through it as well as the $5\times I_B$ which flows through R_2 . So we have a total current of six times I_B . The formula for R_1 is:—

$$R_1 = \frac{4.4}{0.000156} = \frac{44 \times 10^6}{156} = 211k\Omega$$

The nearest preferred value is $220k\Omega$, at 5%.

Stage Resistance

Now that we have the component values, we can calculate stage resistance. Input resistance is what we are interested in here. Remember that as far as

alternating currents are concerned, the top end of R_1 is joined to the lower end of R_2 by the very low impedance of $C_{\rm dec.}$ So the input resistance is effectively $R_1,\ R_2$ and $R_{\rm in},$ all in parallel. Again applying Ohm's Law:—

$$\frac{1}{R_{IN}} = \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_{in}}$$
$$= \frac{1}{220k\Omega} + \frac{1}{270k\Omega} + \frac{1}{1 \cdot 2M\Omega}$$
$$= 110k\Omega$$

Output resistance is calculated from a combination of $R_{\rm E}$, the total input resistance of the transistor and $r_{\rm e}$.

Total input resistance presented to the base of the transistor is the parallel combination of R_1 , R_2 and the output impedance of the device which is feeding the input of our considered circuit. The effect of this lumped resistance (R_8) on the emitter circuit is reduced by the $h_{\rm fe}$ of the transistor, i.e. the lumped resistance is divided by $h_{\rm fe}$.

If the source resistance is one-fifth of $R_{\rm IN},$ say $20k\Omega,$ then R_s is $R_1,~R_2$ and the external source resistance, all in parallel, or

$$\frac{1}{R_s} = \frac{1}{220k\Omega} + \frac{1}{270k\Omega} + \frac{1}{20k\Omega}$$
$$= 17.2k\Omega$$

This resistance when looked at by the emitter seems smaller, due to h_{fe} :—

$$\frac{R_s}{h_{fe}} = \frac{17 \cdot 2k \Omega}{440} = 39 \text{ ohms.}$$

This is in parallel with $R_{\rm E}$ and any external load. If we consider an external load of a minimum value of $20k\Omega$ (and these 'taken' values, throughout, are not just dreamed up; they are 'from life'), then the minimum output resistance would be:—

$$\frac{1}{R_{out (min)}} = \frac{1}{39} + \frac{1}{2.7k\Omega} + \frac{1}{20k\Omega}$$

In other words, for an input of $100k\Omega$, our stage has given us an impedance reduction of around 2,500:1.

Coupling Capacitors

A stumbling block to many would-be circuit designers. . . . the value of the capacitor which joins two stages is very important and must be calculated in the following way for optimum performance.

This input capacitor, C_{iu} , must have a reactance that is small in relation to the input resistance of the stage, at the lowest frequency we want the stage to handle.

Taking a practical example, if C_{in} was made $0\cdot02\mu f$, its reactance at little under a 100Hz would be $100k\Omega$. Since this is the same as the input resistance of the stage, which we have already worked out, a 2:1 attenuator would be formed at the critical frequency, actually 90Hz. In fact, the voltage drop would be 6dB, around half this would fall with decreasing frequency at the rate of 6dB per octave.

If we made C_{out} as low as $0.02\mu f$ and then fed our

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emitter follower into a $100k\Omega$ input, we would have a 12dB drop at the critical frequency with a falling off equal to 12dB per octave.

Normally, with a circuit of this type, acting simply as a buffer, the low-frequency roll-off will have been determined by associated circuitry.

A value of $C_{in}=1\mu f$ and C_{out} 10 μf are adequate down to a few hertz, even if the load into which the circuit if feeding is as low as 20 $k\Omega$.

The load on the circuit should be at least 5 times greater than the output impedance: preferably, ten times.

Decoupling Components

We must consider the practical matter of the available supply voltage and what we have calculated as being desirable. For convenience, a 9-volt battery will do. This could be a PP6, for the current being drawn by this device does not demand a battery of large capacity.

Our circuit calls for a supply voltage of 7·7 volts, so the difference will have to be dropped by a resistor, $R_{\rm dec}.$ The current flowing through this resistor will be the collector current, $I_{\rm c},$ which is 1mA, plus the $6\times I_{\rm B}$ current in the base bias network. This gives us a total current of 1·0156mA, not significantly far from 1mA to matter.

So, again having recourse to Ohm's Law, we say that: --

$$R_{dec} = \frac{1.3}{1 \times 10^{-3}} = 1,300 \text{ or } 1.3 \text{k} \Omega.$$

For our purpose, $1\cdot 2k\Omega$ at 5% is enough, but it so happens that $1\cdot 3k\Omega$ is a standard value in the E24 resistor series, so if you have one of these available, so much the better.

The decoupling capacitor has to have a low reactance for us to maintain good low frequency response. Another function C_{deo} performs is to bypass any signal currents which may have crept into the supply line from other sections of circuitry. A value ten times greater than C_{out} is desirable.

From this, without further calculation, we make $C_{\text{den}}\,100\mu\text{f}$. This gives us a reactance at 20Hz of around 80ohms, which will be quite small in comparison with the minimum a.c. load on the circuit of $20k\Omega$.

Construction

Fig. 25 should be self-explanatory. Mike chose Veroboard, cutting a portion of a group board to make a 13-way section,. This type of board has three copper strips at each outer line, leaving the centre clear. Holes can be cleared with a No. 33 drill (6BA clearance), and relating to the grid of our Fig. 25 holes are first drilled at 2F and 12F for mounting. Next stage is to fit the links, 3B to 4B and 4B to 6B, going around 5B. Link 7B to 8B, and 7B to 6I, using sleeved wire, and the same for 5B to 10B. Link 4I to 5I and 5I to 8I and 9I.

Battery connections are red, positive, to 7J and black, negative, to 5J. Input lead, 'live', 3J with the earthy braid to 4J: output live to 10J, earthy braid to 9J. Finally the BC109 transistor, which should be fitted as shown, to 5A (emitter), 6A (base), and 7A (collector). Components are mounted as shown.

Results

Measurements on the prototype built from this circuit gave an output of 1.85 volts r.m.s. at the onset of clipping. This is equivalent to 2.6 volts peak, the measured emitter voltage on the prototype. A glance at the circuit shows that the emitter voltage, when driven by a sinewave, can swing down to the negative line. This represents a peak negative swing of 2.7 volts

The positive swing, however, can push the emitter voltage up near collector voltage of 7.7 volts, a peak swing of 5 volts. Since this circuit would only be called upon to handle a few hundred millivolts, this unbalance is only academic—but the point is worth making.

Input impedance measured $105k\Omega$, output impedance $78\cdot 5$ ohms with $20k\Omega$ source. Deviations from the calculated value can easily occur due to the spreads in h_{fe} . For example: the h_{fe} spread for a BC109 operating at a collector current of lmA is from 240 to 960, a ratio of very nearly four to one. Frequency response was within $0\cdot 1dB$ of reference (lkHz) from 10Hz to 100kHz.

The upper limit frequency will be determined by the source resistance of the device being fed into our circuit, and the capacity of the interconnecting cables.

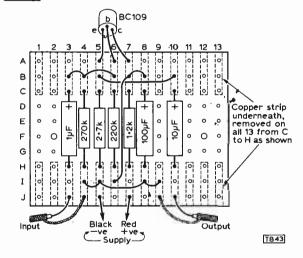


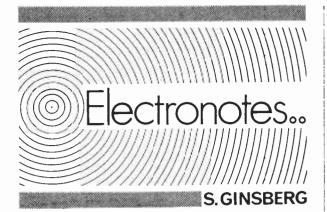
Fig. 25: Practical layout using 0-15in. matrix Veroboard. Approximately to scale.

Gain, between input and output, is less than unity, a measured 0.98. The object of the exercise is not to get gain but to convert impedances—very often, when doing this, one is also concerned to attenuate, but this is done externally.

Total harmonic distortion is almost too low for measurement with normal workshop instruments. In fact, the figures were as follows:—

Output level	20Hz	1kHz	20kHz
300mV 500mV 750mV 1V	0.008%	0·007 % 0·01 % 0·06 % 0·08 %	0.005%

TO BE CONTINUED



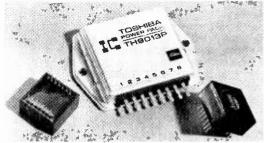
T seems that there are very few areas where electronics has not penetrated in one way or another. The automobile industry is a natural market for electronics but it seems to be slow in getting off the ground. The home constructor and "amateur" has not been slow to appreciate the benefits, however, and items like windscreen wiper speed controls have appeared in the popular construction journals. For the do-it-yourself man there is a good opportunity to get electronics into his car and to increase the comfort and efficiency. Transistorised ignition is one example and one company, Transmetrix (Research & Development) Ltd., have just launched a tiny transistorised ignition unit which sells for just over £10. It was tested, along with those from other manufacturers, by a leading motor magazine and came out number one. At this sort of price. one wonders how long it will be before the motor car manufacturer fits transistorised ignition as a standard or at least an available option on all models.

Another thing which has a great deal to offer is thick film technology but again it is a thing which has been slow to catch on. Thick film circuitry is achieved by taking an insulating substrate and printing the wiring pattern on it with a special conducting ink using silk screen printing techniques. The circuit is then put on a belt which passes through a special oven which fuses the ink and bakes it.

The inks are composed mainly of glass together with a conductive element. By reducing the amount of conductive material in the ink, the pattern will have a greater and greater resistance dependent upon the amount of conductive material remaining. Thus resistors can be "printed" down in the same way as the wiring. Usually, these resistors have a tolerance of around 15%—good enough for some circuits.

For closer tolerance, down below 1 per cent for example, the circuit is put in a jig and probes measure the actual value of resistance. This is fed to a circuit which compares this actual resistance against the value required. A jet of air plus an abrasive is then fired at the resistor through a tiny nozzle. This erodes away tiny parts of the resistor pattern, gradually reducing the resistance value. When the actual value reaches the required value set up on the resistance bridge, the air/abrasive is automatically switched off.

Capacitors, transistors and integrated circuits may be bonded onto the thick film substrate once the initial pattern has been layed down. By laying down an insulating layer, another pattern may be printed over the top of the first and thus a multilayer circuit can be built up. Joshiba HI-FI
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We are now supplying a printed circuit board (for the pre-amplifier circuit) to achieve instant success with this fabulous amplifier kit.



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Buv British

I recently asked at a local radio shop for an OC44 transistor and was offered one marked "Mullard, Foreign Made" and when I asked the price I was told it would be 70p. When I protested at the price I was informed that others I said I could obtain cheaper could only be "seconds".

I tried another radio shop a few miles away and obtained an OC44 marked "Mullard, British Made" for 41p, which the dealer assured me was the correct price according to his list.

Since then, I have had occasion to purchase a volume control, tone control/switch for a wellknown continental radio and the price in this case was £1.90 plus 10p purchase tax. A comparable British-made component would certainly not have been more than 50p and apart from this, the printed circuit was in my opinion inferior in workmanship to many Hong Kong made sets costing a fraction of the price this one did. -R. J. Hall (Penzance, Cornwall).

All in the mind

I would be grateful if anyone could assist me in a little private research. What I need is an authoritative assertion or denial as to whether it is possible by the use of radio equipment to transmit any messages that can be received by people without any receiving equipment at all. In other words, can messages be transmitted directly to a person's mind?

I have heard this claimed on several occasions—the first time being from a Gendarmee Commissionier in France in 1946 and although he was a learned man, he was not familiar with radio technology. From that time, I had heard nothing more about it until three years ago.

In a district I left two years ago, a great deal of talk centred around this subject under the name of "telemetering" and I do know that a number of people had radio transmitters which they claimed they were using for this purpose and I do know they were tried on me with this intention.

Whether they worked or not is obscured by other issues-but none of the people using them had any radio knowledge at all and I am wondering how many of their claims belong to the realm of legends.

I am aware that some years ago, there were reports of odd individuals who claimed that they could receive BBC transmissions without receiving apparatus, but whether such claims have been substantiated, I do not know.

If however, telemetering is a reality, would anyone be kind enough to give me in brief, the principles on which it is accomplished?

I am highly suspicious about claims that I have heard made: particularly since the accepted sense of the word "telemetering" is in connection with recording instruments being read at a distance.-V. D. Butler (Kirkstall Hill, Leeds).

has been unmarked or otherwise of surplus origin, and in several cases your name has heen mentioned as the supplier. In addition the diagram I saw shows D5 connected in reverse.

It is imperative that any modification to a car ignition system be as reliable as possible since sudden failure could, in certain circumstances, cause an accident situation. For this reason I must condemn the use of unmarked or otherwise low grade components.

Unfortunately many constructors have become disillusioned with the results and have laid the blame at my door saying that it is a design fault. This has caused me a lot of unnecessary work and expense in replying to this type of complaint, and has delayed the writing of a follow up article since I feel I must in future recommend specific types and sources of all components.

Yours faithfully,

S. Soar."

Ignition!

This is a copy of a letter sent to one of our advertisers by Mr. S. Soar, author of the Electronic Ignition article published in P.W. June 1971. We do not feel that any further comment by us is needed.—Editor.

"Dear Sirs,

With reference to the electronic ignition article. I have one or two comments which I would like to raise.

As the author of the original article I have received several hundreds of letters from constructors, in the main these have been very encouraging and I estimate that the unit has now covered an aggregate distance in excess of one million miles.

However, several constructors writing to me have disappointed with the results, and in general they fall into two catagories, circuit construction faults and component failure, the latter accounting for something like 90 per cent of all problems encountered. In almost every case of component failure or malfunction the component in question

WHO MAKES WHAT?

In the October 1971 issue, the Editor expressed his concern at the winding up of the Merchandise Marks Act as from November 30th last, after which it was no longer obligatory for imported goods to bear a "country of origin" mark. One aspect of concern was the fact that some goods bearing well-established UK trade names are, in fact, made in lowcost labour countries and that after the ending of the Act there would be no way of telling where, the goods were actually manufactured.

While it appears that there is little hope of reversing the decision to end the Act, one ray of hope is that the Government is likely to support a Private Member's Bill which will provide that if a UK company's name or trade mark or any UK place name appears on imported goods it will have to be accompanied by a statement of where the goods were actually made.

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A SELECTION FROM OUR LIST AAY30 10p | BD115 75p | OC16 50p | 2N1303 18p

AA 130	TOD	BDII 7	OP	LOCH6	50p	2N 1303	ISD
AAY42	15p	BD123 8	5p	OC20	85p	2N1304	22 p
AAY42 AAZ13	10p	BD124 8	0p	OC22	50p		
AAZ15	10p	BD131 7	5p	OCUS	60p	2N1305	22p
AAZ17	10p		Op	OC23 OC24	000	2N1306	25p
			υp	0024	60p	2N1307	25p
AC107	35p	BDY11		OC25	40p		
AC126	30p	£1.	50	OC25 OC26	25p	2N1308	25p
AC127	25p	BDY17		OC28	60p	2N1309	25p
AC127Z	50p	£1.	50	OC29	60p	2N1613	20p
AC128	20p		5p	OC35	50p	2N2147	75p
		BDY60	o p	OC36	80p	2N2160	739
AC176	20p				60p		60p
AC187	25p	£1.	υυ	OC42	40p	2N2217	25p
AC188	25p			OC43	50p	2N2218	20p
ACY17	30p	BF115 2	5p	OC44	15p	2N2218.	A
ACY18	25p	BF154 2	Op	OC45	12p		25p
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ACY21	20p	BF180 3	5p	OC72	20p		25p
ACY22	10p	BF194 1	5p	OC75	25p	2N2220	25p
ACY39	55n	BF195 1	5p	OC76	25p	2N2221	20p
ACY40	20p		5p	OC77	40p	2N2221	4
ACY41	200	BF197 1	5p	OC81	200	21122211	``^-
ACX41	15p	DF 197 1	op		20p		25p
ACY44	25p	BFX13 2	5p	OC81D	20p	2N2222	20p
AD140	50p	BFX29 2	5p	OC81Z	40p	2N2222.	A
AD149	50p	BFX30 2	5p	OC83	25p		25p
AD161	35p		5p	OC84	25p	2N2369	15p
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AD162	35p	BFX85 3		OC139	25p	2N2369	٦
AF114	25p	BFX86 2	5p	OC140	40p		15p
AF115	25p		5p	OC141	60p	2N2646	40p
AF116	25p	BFX88 2	0p	OC170	25p	2N2904	20p
AF117	20p	BFY18 2	5p	OC171	30p	2N2904	4
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AF124	25p	BFY51 2	0p	OC201	75p	2N 2905	25p
AF125	20p	BFY52 2	0p	OC202	80p	2N 2905	4
AF126	20n	BFY53 1	5p	OC206	95p		25p
AF127	20p	BFY90 6	5p	OCP71	97p	2N2906	20p
AF139	30p		5p	ORP12	2 / P	2N 2906	
	aup				50p	214 29001	
AF180	50p	B8X21 2	0p	ORP60	40p		25p
AF181	45p	B8Y27 1	5p	ST140	15p	2N2907	28p
AF185	50p	BST95A 1	2p	ST141	20p	2N2907	١ ١
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BA110	25p	BYZ13 2	5p	T1850	12p	2N3614	55p
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BAY31	7p	GET103 2:	5p 5p	TIS52 TIS60 TIS61	10p 10p 18p 20p	2N3703 2N3704 2N3705	10p 10p 12p 10p
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BC107 BC108 BC109 BC109C BC113 BC114 BC115 BC116 BC116A BC117 BC118 BC119 BC134	7p 7p 15p 10p 10p 12p 10p 20p 20p 20p 20p 20p 20p 20p 20p 20p	GET103 2: GET111 4: GET114 2: GET114 5: GET116 5: GET880 4: GET880	5p 5p 5p 0p 5p 5p 5p 5p 5p	T1852 T1860 T1861 T1862 V405A VR525 WO1 WO6 ZTX107 ZTX108 ZTX300 ZTX300 ZTX302 ZTX303 ZTX303 ZTX303	10p 10p 18p 20p 25p 25p 30p 45p 12p 12p 12p 12p 20p 25p 15p	2N3703 2N3704 2N3705 2N3707 2N3708 2N3715 2N3715 2N3716 2N3771 2N37772 2N3772	10p 10p 12p 10p 12p 10p 2 00 2 20 2 85 2 00
BC107 BC108 BC109 BC109C BC113 BC114 BC115 BC116 BC116A BC117 BC118 BC119 BC134 BC135	7p 7p 15p 10p 10p 12p 10p 20p 20p 20p 20p 20p 20p 20p 20p 20p 2	GET103 2: GET111 4: GET1113 2: GET114 5: GET116 5: GET880 4: GET880 3: GEX66 21: GM378A 5: MAT101 2: MAT121 2: MAT121 2: MC724P 6: MJ420 8: MJ421 8: MJ2801	5p 5p 0p 0p 5p 0p 5p 0p 5p 0p 0p	T1852 T1860 T1861 T1862 V405A VR525 WO1 WO6 ZTX107 ZTX108 ZTX300 ZTX300 ZTX302 ZTX303 ZTX303 ZTX303	10p 10p 18p 20p 25p 25p 25p 35p 45p 15p 12p 15p 12p 15p 20p 25p 15p	2N3703 2N3704 2N3705 2N3707 2N3707 2N3714 2N3715 2N3716 2N37716 2N3772 2N3772 2N3772 2N3773	10p 10p 12p 10p 12p 10p 200 2 20 2 85 2 00 2 35
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BC107 BC108 BC109 BC109C BC113 BC114 BC115 BC116 BC116A BC117 BC118 BC119 BC134 BC136 BC136 BC136	7p 7p 15p 10p 10p 10p 20p 20p 20p 20p 20p 20p 20p 20p 20p 2	GET103 2: GET111 4: GET113 2: GET114 5: GET116 5: GET880 4: GET880 3: GET880 4: GET882 3: GEX66 21: GM378A 5: MAT1012: MC724P 6: MJ420 8: MJ421 8: MJ420 8:	5p 5p 0p 0p 5p 0p 5p 0p 5p 0p 0p	T1852 T1860 T1861 T1862 V405A VR525 WO1 WO6 ZTX107 ZTX108 ZTX300 ZTX300 ZTX302 ZTX303 ZTX303 ZTX303	10p 10p 18p 20p 25p 25p 35p 30p 45p 12p 15p 12p 15p 20p 25p 15p 20p 25p	2N3703 2N3704 2N3705 2N3707 2N3708 2N3711 2 2N3716 2 2N3771 2 2N3771 2 2N3772 2 2N3791	10p 10p 12p 10p 10p 200 200 285 200 285 205 235 275
BC107 BC108 BC109 BC109C BC113 BC114 BC115 BC116 BC116A BC117 BC118 BC119 BC134 BC136 BC136 BC136	7p 7p 15p 10p 10p 10p 20p 20p 20p 20p 20p 20p 20p 20p 20p 2	GET103 2: GET111 4: GET113 2: GET114 5: GET116 5: GET880 4: GET880 4: GET882 3: GEX66 21: GM378A 5: MAT101 2: MAT121 2: MAT121 2: MJ420 8: MJ421 8: MJ421 8: MJ2801 21:	5p 5p 6p 0p 0p 5p 5p 5p 5p 0p 0p 0p	T1852 T1860 T1861 T1862 V405A VR525 WO1 WO6 ZTX107 ZTX108 ZTX300 ZTX300 ZTX302 ZTX303 ZTX303 ZTX303	10p 10p 18p 20p 25p 25p 30p 45p 15p 12p 15p 12p 15p 15p 12p 15p 15p 15p 15p 15p 15p	2N3703 2N3704 2N3705 2N3705 2N3715 2N3716 2N3716 2N3771 2N3772 2N3773 2N3773 2N3791 2N3791	10p 10p 12p 10p 12p 10p 2 00 2 20 2 85 2 00 2 05 2 35 2 75 35p
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BC107 BC108 BC109 BC109 BC113 BC114 BC115 BC116 BC116 BC117 BC118 BC119 BC135 BC136 BC137 BC138 BC138	7p 7p 15p 10p 10p 10p 20p 20p 20p 25p 20p 25p 20p 20p 20p 20p 20p 20p 20p 20p	GET103 2: GET111 4: GET113 2: GET114 2: GET116 5: GET880 4: GET880 4: GET882 3: GEX66 21: GM378A 5: MAT101 2: MAT121 2: MAT121 2: MAT121 2: MJ420 8: MJ420 8: MJ2801 21: MJ2801 21: MJ2801 21:	5p 5p 5p 0p 0p 55p 0p 55p 0p 55p 0p 10	T1852 T1861 T1861 T1862 V405A VR525 WO1 WO6 ZTX107 ZTX108 ZTX300 ZTX300 ZTX301 ZTX302 ZTX302 ZTX302 ZTX302 ZTX501 ZTX501 ZTX503 ZTX504 ZTX503	10p 10p 18p 20p 25p 25p 30p 45p 112p 115p 12p 12p 15p 20p 20p 20p 14p 20p 20p 20p 20p 20p 20p 20p 20p 20p 20	2N3703 2N3704 2N3705 2N3707 2N3708 2N3714 2N3716 2N3716 2N3771 2N3772 2N3773 2N3773 2N3791 2N3819 2N3820 2N3820 2N3820	10p 10p 12p 10p 12p 10p 2 00 2 20 2 85 2 00 2 35 2 35 2 75 35p 55p
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BC107 BC108 BC109 BC109C BC113 BC114 BC115 BC116 BC116 BC116 BC119 BC134 BC135 BC135 BC135 BC135 BC136 BC137 BC138 BC147 BC148	7p 7p 15p 10p 10p 10p 20p 20p 20p 20p 20p 20p 20p 20p 20p 2	GET110 2: GET111 4: GET111 5: GET111 5: GET116 5: GET116 5: GET116 5: GET1882 3: GEX66 MAT101 2: MAT121 2: MAT121 2: MJ290 8: MJ2901 4: MJ2901 MJ2901 MJ2307 3: MJ2307	5p 5p 5p 0p 0p 5p 5p 0p 5p 5p 0p 0p 10	T1852 T1860 T1861 T1862 V405A V8525 WO1 WO6 ZTX109 ZTX300 ZTX300 ZTX301 ZTX302 ZTX302 ZTX302 ZTX304 ZTX501 ZTX501 ZTX501 ZTX501 ZTX501 ZTX501 ZTX501 ZTX501 ZTX501	10p 10p 18p 25p 25p 25p 30p 45p 115p 115p 115p 12p 20p 25p 115p 20p 25p 115p 20p 20p 20p 20p 20p 20p 20p 20p 20p 20	2N3703 2N3704 2N3705 2N3707 2N3708 2N3708 2N3714 2N3715 2N3715 2N3715 2N3771 2N3772 2N3771 2N3772 2N37819 2N3829 2N3820 2N3823 2N3824 2N3903	10p 10p 12p 10p 12p 10p 2 00 2 20 2 85 2 00 2 05 2 35 2 75 35p 50p 95p
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BC153 20p BC154 20p BC167 15p BC169 12p BC169C 15p BC177 20p BC178 20p BC178 20p BC182 10p

BC179 20p BC182L 10p BC183L 10p BC184L 12p BC212L 12p BC213L 12p BC214L 15p BCY30 35p BCY31 40p BCY32 60n

BCY34 35p BCY38 45p

BCY39 £1.00 BCY40 50p BCY70 15p

MJE521 ... MJE2955 £1:10

18922 2G301 2G302 2G303 2N404 2N696 2N697

2N697 2N698 2N706 2N706 A 2N708 2N930 2N987 2N1131

2N1132

2N1302 18p

20p 15p 15p

30p 10p 12p 15p 20p 40p 25p 25p

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ш	7400	Quadruple 2-input NAND gates	20p	18p	14p	14p	12p
	7401	Quad 2-input open collector NAND gates	20p	18p	16p	14p	12p
	7402	Quad 2-input NOR gates	20p	18p	16p	14p	12p
ш	7403	Quad 2-input open collector NAND gates	20p	18p	16p	14p	12p
ч	7404	Hextuple inverters	20p	18p	16p	14p	12p
	7405		0.0	18p	16p	14p	12p
п	7410	Triple 3-input NAND gates Dual 4-input NAND gates Dual 4-input NAND gates	20p	18p	16p	14p	12p
ш	7413	Dual 4-input Schmitt triggers	30p	27p	25p	220	20p
н	7420	Dual 4 input NAND cates	20p	18p	16p	14p	12p
	7430	Cingle 9 input NAMD gates	20p	18p	16p	14p	12p
	7440	Dual 4 invest N 4 ND buffer notes	20p	18p	16p	14p	12p
	7441	Dual 4-input NAND gates Single 8-input NAND gates Dual 4-input NAND buffer gates BCD-Decimal decoder/Nixie driver	75p	72 p	70p	60p	55p
-	7442	BCD-Decimal decoder/Nixe driver BCD-Decimal decoder (4-10-line) TTL O/P	75p	72p	70p	60p	55p
-		DCD-Decimal decoder (4-10-fille) III O/F	#1 00	95p	90p	80p	70p
	7443	Excess 3-Decimal decoder TTL outputs	21 00	£1 · 60	£1 45	£1 · 80	£1 · 15
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	7448	BCD-Decimal 7 seg. decoder/driver TTL O/P	£1 · 75	£1 · 60			
	7450	Expand dual 2-input AND-OR-INVERT gates		18p	16p	14p	12p
	7451	Dual 2-wide 2-input AND-OR-INVERT gates	20p	18p	16p	14p	12p
-	7453	Quad 2-input expand AND-OR-INVERT gates		18p	16p	14p	12p
	7454	4-wide 2-input AND-OR-INVERT gates	20p	18p	16p	14p	12p
	7460	Dual 4-input expanders Single J-K flip-flop (gated inputs) Single J-K flip flop (gated inputs)	20p	18p	16p	14p	12p
	7470	Single J-K flip-flop (gated inputs)	30p	27p	25p	22p	20p
в	7472	Bingle J-K flip flop (gated inputs)	30p	27p	25p	22p	20 p
-1	7473	Dual J-K flip flop Dual D flip flop Quadruple bistable latch	40p	87p	35p	38p	30p
1	7474	Dual D flip flop	40p	37p	35p	33p	30p
	7475	Quadruple bistable latch	45p	42p	40p	38p	35p
1	7476	Dual J-K flip-flops with Preset and Clear	40p	37p	34p	31p	28p
	7480	Gated Full Adder	80p	72p	67p	59p	55p
	7491	16-bit read/write memory	41 25	£1-15	£1:10	£1-00	90p
	7400	9 hit binary Full Adder	87p	80p	70p	65p	60p
	7482	4-bit binary Full Adder	#1 · 00	90p	85p	80p	78p
8	7404	16 hit DAN with geted write inputs	905	85p	80p	75p	71p
	7402	Our Imple 9 input Freductive OP gates	450	41p	38p	35p	33p
	7100	DCD decade country	750	70p	65p	60p	55 p
	7490	9 bit shift aggister	#1.00	95p	90p	80p	70p
	7491	8-Dit shift register	755	70p	65p	60p	55p
	7492	Divide twelve counter	750	70p	65p	60p	55p
	7493	4-bit binary counter	700	75p	70p	65p	60p
	7494	Dual entry 4-bit shift register	80p	75p	70p	65p	60p
	7495	Dual J-K flip-flops with Preset and Clear Gated Full Adder 16-bit read/write memory 2-bit binary Full Adder 4-bit binary Full Adder 4-bit binary Full Adder 4-bit binary Full Adder 16-bit RAN with gated write inputs . Quadruple 2-input Exclusive OR gates BCD decade counter 8-bit shift register 1-bivide twelve counter 4-bit binary counter 1-bual entry 4-bit shift register 4-bit up-down shift register 5-bit parallel/serial in/out shift register 8-bit bistable latch 1-lextuple Set-Reset latches 1-bit bistable latch 1-bit data electro/multiplexer 1-bit bit data elector/multiplexer 1-bit bit data elector/multiplexer	8UP	97 p	95p	90p	83p
	7496	5-bit parallel/serial in/out shift register	21.00			£1.75	£1 · 50
	74100	8-bit bistable latch	22 00	#2.30	£2:00	80p	70p
	74118	Hextuple Set-Reset latches	\$1.00	95p	90p		41p
	74121	Monostable multivibrators	вор	55p	50p	46p	
	74141	BCD-Decimal decoder/Nixie driver	£1 · 00	95p	90p	80p	70p
	74145	BCD-Decimal decoder (1-4-line) TTL O/P	£1 50	£1 · 40	£1 · 30	£1·10	£1 · 00
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	75151	8-bit data selector/multiplexer	£1 · 10	95p	90p	80р	70p
1	74153	Dual 4-line to 1-line data selector multiplexer	£1 35	21.27	£1 · 20	£1 · 15	£1·10
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1	Comple	ete data on the above in booklet 20 pages, Ref. 29,	issue 2 a	t 15p post	paid.		

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THE BROADCAST BANDS Malcolm Connah

Frequencies in kHz Times in GMT

NEWS FOR DX LISTENERS

EW ZEALAND is one of the countries that can only be heard for a few months in each year. The transmitter power is only 7.5kW and the aerials are beamed to Australia and the Pacific Islands, Propagation conditions only allow reception in this country in the last few months of the year and possibly in January as well.

Our first reporter this month is David Watters of Edinburgh. The equipment consists of an old Philips domestic superhet and a six foot whip antenna fixed on the roof. David's reports of Radio New Zealand should prove useful to all those trying to catch this

rare country.

6010 R.T. Belge, Belgium in Dutch at 1430.

7105 CBC, Canada in Russian at 0330.

9520 New Zealand in English at 0900.

9525 RSA, South Africa in English at 0500.

9540 New Zealand in English at 0600.

9550 Finland in English at 1800.

9560 ABC, Australia in English at 0645.

9625 CBC, Canada in English at 0715.

9755 New Zealand in English at 1700.

Jean A. Meghriche of Elstree has again concentrated on the 60 metre band and produced the following results:

4920 R. Caracas, Venezuela at 0620.

4945 R. Colosal, Colombia at 0610.

4955 R. Nacional, Colombia, s/off at 0505.

4965 R. Santa Fe, Colombia at 0605. 4970 R. Rumbos, Venezuela at 0450.

4980 Radio Accra, Ghana at 1815.

4980 Ecos del Torbes, Venezuela at 2320.

4990 R. Barquisimeto, Venezuela at 0305.

5010 R. Cristal, Dominican Republic at 0525. .

5025 R. Clube de Huila, Angola at 2010.

5035 R. Bangui, Cent. African Rep. at 2000.

5047 R. Lome, Togo at 0630.

9535 ETLF, Ethiopia at 1830.

11920 R. Abidjan, Ivory Coast at 1750.

11925 R. Bandeirantes, Brazil at 2050.

11865 R. Clube de Pernambuco, Brazil at 2015.

Alexander Morton of Framlington, Suffolk has a VEF-204 receiver and a 20 foot long-wire in the loft. This combination produced a very long log of which the following is an extract:-

5875 HCJB, Quito, Ecuador in English at 0810.

6025 Radio Sweden in English at 1600.

9770 R. Sofia, Bulgaria in English at 1930.

11860 R. Portugal in English at 1900.

15225 RSA, South Africa, news at 1600.

15380 CBC, Canada at 1120.

17787 WINB, Red Lion, U.S.A. at 1820.

17840 HCJB, Quito Ecuador at 2030.

17885 R. Lebanon in English at 1840.

17970 R. Pakistan, news in English at 1350.

21560 RSA, South Africa at 1400.

21582 Radio Accra, Ghana at 1445.

21800 Radio Norway, in English at 1800.

Steve Mathews of Hull has used his Trio 9R-59DS and 90 foot long-wire to hear the following:

3265 R. Clube Mozambique in English at 2100.

4833 Bamako, Mali in French at 2130.

5010 R. Cristal, Dominican Republic at 0245.

6040 Voice of the Coast, Dubai at 0410.

6055 ABC, Australia (Darwin relay) at 1715.

6120 R. El Mundo, Argentina at 0200.

15430 KBS, Korea in Spanish at 0205.

15440 FEBC, Philippines at 1545. 21500 R. Brazzaville, Congo, French at 0845.

D. A. Hairon of St. Clement, Jersey is now using a Codar CR70A, a PR30 preselector, a 19 metre band dipole and a 100 foot long-wire. His log for this month included:-

9560 RSA, South Africa in English at 0230.

9710 HCJB, Quito, Ecuador in English at 0245.

11710 AIR, Delhi in English at 2330.

11765 R. Dif. Sao Paulo, football at 0100.

11775 VOA, Philippines, s/off at 1700.

11785 TWR, Bonaire in English at 0115. 11885 R. Maua, Brazil in Portuguese at 0000.

11925 R. Bandeirantes, Brazil at 2030.

15185 R. Havana, Cuba in English at 2010.

21570 NHK, Japan in English at 0800.

Craig Tyson of Wembley, Western Australia has concentrated on 19 metres and his log includes:-

15105 R.T. Belge, Belgium at 1600.

15120 Radio Ceylon in English at 0320.

15155 RSA, South Africa in English at 1810.

15165 R. Damascus, Syria in French at 1950.

15175 R. Norway in English at 0800.

15190 R. Brazzaville, Congo, French at 1810.

15235 NHK, Japan in English at 0930.

15285 R. Accra, Ghana in English at 1820.

15345 VOA, Philippines in English at 1100.

15355 R. Lebanon at 2300.

Stephen Hillman of Warley has a Teleton 136F4 receiver connected to a 50 foot long-wire enabling him to hear: -

4970 R. Rumbos in Spanish at 0200.

5960 HCJB, Quito, Ecuador in English at 0800.

11795 WINB, Red Lion, USA in English at 2000.

11805 R. Globo, Brazil in Portuguese at 2030.

Reports should arrive by the 15th of the month and be addressed to me at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex.

ON THE



ANDS up all those who got a new receiver from Santa. Just think of all those exotic callsigns you'll be hearing—or perhaps you've heard them already in which case how about sending in a log?

What antennas are you going to try this year? Now is the time to start planning and doing all the paperwork. If '3JDG's experience is anything to go by then this definitely is the time. After you've changed your mind half a dozen times and bought lengths of wire you find you don't need after all it works out a bit expensive in both time and money. Much better to work out everything while you're sitting by the fire in the cold months. You'd be surprised how much time you can save by planning well in advance. How about an all-band automatically-switched vertical for the loft?

"The most exciting band for me this month was two metres," says **Stefan Kaye** (Witney). Gear is a 4-over-4 in the loft, Space Mark converter and an AR88D tuning 12-14MHz. Ears are the Kaye, MK1 types and were stimulated to the tunes of the following on 144MHz; DC2JN, DC6EQ, DJ4AX, DJ4EU/P, DK4TP, DL0ER, DL0WU, DL1XG, F1KCG, G8ABP, G8EJH, ON5NY, PA0QX, PA0WCH.

Some peope have written in asking how a receiver tunes in 144MHz signals since the frequency given for the receiver tuning is never anywhere near 144MHz. Idea is that you use a converter between the main station receiver and the aerial. The converter "converts" (surprise, surprise) the 144MHz incoming signals and lowers the frequency down to a range which can be covered by the main receiver. Popular converter output frequencies are 12-14MHz and 28-30MHz. The converter doesn't need tuning, you just plug the antenna in one end and the receiver into the other.

But I digress! **R. Gillon** uses a Wein Flight 4 on 144MHz. Signals received from: DM0ER, DL0PT, EI2BY, F6AP, GW8ASA, GM3NYY/P, OL6OL, ON5NY, PA0LM. QTH is Richmond.

Brian Lucas (Gillingham) has an RBX-2 Hallicrafter and describes the antenna as "chopped down v.h.f. dipole loitering on the end of a 3ft beam under the eaves." (Bet he only listens in the eavenings! Squeaks of r.f. on 144MHz from: DL0ER, F0YT/M, F1PD, F1AXI, F1BMF, F1BCD, F5ID, F6HWH plus 12 G3s, a G4 and 18 Gs.

A 46 (forty-six) element Multibeam, converter and 9R59DE tuning 28-30MHz is N. Richardson's visiting card on 70cm. Goodies arriving at Aylesbury at this rarified frequency include: DC8AMA, DC8UA, PA0DGH, PA0JNH, PA0EZ, PA0OX.

Down on 144MHz, Nicholas and 8-element yagi, converter plus 9R59DE, did a bit of eavesdropping on: DC0QA, DJ8SW, DJ8VRA, DJ9UXA, DK2T/P, DK4TP, DL0ER, DL1XG, F1AEX, F2XO, F5DA, F6BBA, F6BOM, F9QW, GC8AWE, GC8BMO, ON4OR, ON5QW, ON5VU, PA0APE, PA0HWB, PA0CML, PA0ELL, PA0HAG.

THE AMATEUR BANDS David Gibson, G3JDG

Frequencies in kHz • Times in GMT

All this v.h.f. is a bit too rich for the old '3JDG blood, let's flick the bandswitch to 28MHz and see who heard what. Ten metre addict M. Shields (Abergavenny), JR500-SE, 70ft long wire end fed running NS, sends in a mouth-watering log of callsigns. Pages from an immaculate log read: CE3EZ, CE7TJ, CR4BS, CR6IK, CR6TP, CR7LE, CR7IA, CP6FG, CT3AS, CX7BF, CX8BE, CN8HD, DJ4OI, EL8I, FY7AD, F9XF, G3MUL/CE3, HK4AFT, HR1JA, KV4FD, KP4CQB, K4AVD, LU6ECE, PY3BNJ. VP9DC, RA3AFL, VP8MM, W6JIF/4, W3FXG, ZP5AQ, XX6FL, YN2OM, ZC4AVU, ZE1BP, ZEIGDS, ZS2AG, ZS4UCC, ZS5KS, ZS6ATA, 4Z4HF, 5N5ABG, 8RIG, 9G1DY, 9H1AQ, 9J2DT, 905ELA.

Letter from Karl Muller (Swaziland) informs that ZD5 stations are now all 3D6A stations. Karl says that forty metres has been disappointing in the evenings mainly because of QRM from BC stations. How about all transmitting amateurs having a 1972 40-metre activity year, I'm sure we could make some of these pests QSY out of our band? It would make forty a greater attraction for the s.w.l. and would dissuade greedy eyes from pilfering our last (in the UK) 100kHz. How about it, r.f. makers?

Robert Ferguson (near Birmingham), has an HRO plus a "... one element rotatable beam." (Good gracious, Holmes!). Ten metres yielded: CX8BE, CR6TP, CX8BE, LU5DTA, VK9XK, ZS1JA, 7Q7BC, 9G1DY, 9J2DT, 9Y4VU plus hoards of JAs.

Best from Martin Evans (Colwyn Bay) on 3.5MHz using a three-transistor t.r.f. with 150ft end fed plus a.t.u. were: CT1BH/P, OX3RA, OY400, TF5TP, T12GI, VE1AM/VP9, VP7NH, ZS6DW, 4U1ITU, 4X4YM, 4Z4HF.

Keith Monham (Feltham) bagged these on phone on 160 metres; DJ4SS, DK2JX DL0WU, EI9ONE, GM3NVU, GM3YCB, GM4NR/P, GW3AAC, GW4AJ/A. OH1VR, OH5GM, OH5SM, PA0PN. Cor, think what was about on c.w. Gear is a 60ft. end fed with a.t.u. plus a B40 receiver which draws sparks between earth wire and chassis. (Shocking state of affairs!).

Nicholas Minns (Letchworth), CR300, 110ft. end fed, sends in this list of topband hearings; DK0WA, DK2WA, HB9CM, OH1VR, OH5SM, PA0PN, E19ONE.

On 3.5MHz, the same set up raised: FM7WN, HR1WSG, OY2X, PJ2CW, PZ1CU, TI2CAP, WA6EGL/P/TF, VP2VAG, ZB2AV. While the dreaded forty metres surrendered signals from: CN8CS, EP2BQ, FL7ZX, JA6BSM, 4X4LNJ, 6W8DY.

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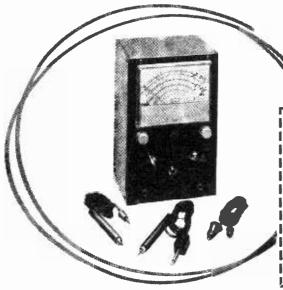
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No. 87

Milk Teeth

practically wireless commentary by

T IS ALL TOO EASY to blame lack of foresight on teething troubles. That, after all, is what happens when car doors fall off, when vacuum cleaners shed belts, when 'fridges go up in smoke—or when radio gear develops a case of the twitches only weeks after delivery.

"Teething troubles," if I may quote John Pudney, "is an indulgent phrase which has become a blanket term for incompetence."

Ralph Nader may have a lot to say about the automobile industry and its tendency to blanket its failings with next year's model draped with nudes, or not. Henry cannot cap his quotes, perhaps because he has had to manage with a succession of second-hand cars—and you know what the public thinks of their advertisements. . . But on the subject of newly-sold radios and associated gear, your correspondent speaks with some authority.

And bitterness! I often wish some fully-equipped Nader would rise and berate the manufacturers of our domestic electronic equipment. And not only our homegrown makers, for at least we must give them a Beta-minus for trying, but also the importers.

However elegant the drawn circuit, reality will always have rough edges. Any constructor will verify that. Even with the



Buzzing around like bluebottles.

mollycoddling given to us by such redoubtables as Heathkit, it is possible to make mistakes. Human error enters into Fate's formula and reductio ad absurdum is the result.

Absurd as the contretemps Henry observed when working as a "tester" in a radio factoryinstructions were given to those doing routine alignment: "twiddle until the needle on the meter reaches maximum, then seal the screw." Nobody considered that there were two alternative peaks when the mixer circuit was tuned in-so, of a batch of well over a thousand sets, boxed and despatched, a goodly proportion were completely misaligned—and nobody noticed till the complaints came rolling in!

Teething troubles were blamed for many of the television set assininities that kept field engineers buzzing about like bluebottles when ITV first opened, when dual-standard receivers became the vogue, and harass them now, when colour is the order of the day.

Teething troubles are given as the reason why quite famous hifi makers foist amplifiers on the public with an inherent rumble and noisome hiss and then announce a Mark II model with alternative front-end transistors.

There will always be teething troubles while makers, greedy for profit without the responsibility that once pervaded our industry, market gear that is not in any way backed with a spares service or even the vital information the retailer's engineer will need.

Ask half the agents that are pushing their newest models, and you'll get the answer: "Our service manual's being prepared." And by that time, the poor old dealer has had to rip half a dozen of the units to bits to find why sundry minor ailments were apparently missed on final test.

A reviewer, not a hundred miles from where I sit, refuses pointblank to accept equipment



My largest pair of pliers.

for appraisal unless it is accompanied by the service information that was available to the factory engineers. He has bitter memories of putting a mediocre system through its paces, according to British Standards, only to be hauled over the coals because he had not tested it the way originally laid down. The fact that their way was a palpable con trick (resetting tone controls to fiddle a flat response curve) made but little difference-he should have waited for the gen. So now he does, and the panting manufacturer can whistle for his review.

But I don't know whether that is preferable to those who launch a new radio in a blaze of publicity, then proceed to Mark II, III and IV during a twelvemonth without a word to anyone. Which becomes embarrassing, when a customer toddles into one's shop with a request for a "volume control for the Superstar, please." How does one explain that there have been a veritable constellation of models bearing that name, and the clue is in the suffix to the number on the back?

I'd like to solve some of those makers' teething troubles with my largest pair of pliers.



Books reviewed on this page are normally obtainable through any retail bookshop. In this instance, the information printed in heavy type should be quoted.

FOUNDATIONS OF WIRELESS AND ELECTRONICS
By M. G. Scroggie
Published by Iliffe Books,
521 pages, 9 × 6in. £3.00 (hard cover)

OW do you start to review a book that will without doubt become a classic? Do you try to pick holes in it to fill out the copy? That would be unfair and very difficult so all there is left to do is to praise it as strongly as you can and thoroughly recommend it to all and sundry.

I don't know how old Mr. Scroggie is; we are told on the flyleaf that he graduated in 1922 and has been writing ever since. Here he has produced a book that radiates freshness and originality and is far more up-to-date than any book I have seen for several years.

The author appears to recognise that the semiconductor is here to stay and now forms the basis of electronics and he has started from scratch with this new edition to take this into account—what a contrast to authors half his age who still regard semiconductors as upstarts!

In future, whenever I am asked to recommend a book for beginners, I shall quote this one; it doesn't give circuits or constructional details of course—it isn't that sort of book—but the explanations are clear, complete and logical.

Congratulations Mr. Scroggie and Iliffe—a fine book!—*H.W.M.*

SIMPLE SHORT WAVE RECEIVERS By F. A. Baldwin Published by Data Publications. 140 pages, $8\frac{1}{2} \times 5\frac{1}{2}$ in. Price 80p.

RANK Baldwin is an author who certainly knows what he's talking about when it comes to shortwave listening and it is a name that crops up frequently as the author of articles in Radio Constructor and amongst the short wave listening fraternity. This book is a collection of simple short wave circuits—four in all—and they are all good stuff and I have no doubts that they all work—and work well. Drawings, circuits and descriptions are all very clear and well presented and these in themselves should give the reader a certain amount of confidence.

Having said that, some less kind comments must follow. All circuits use valves—and some are very old types indeed. The date is 1971—transistors rule the day, yet there is not one mention of them in the whole book. A title such as "Simple Short-Wave Receivers" must surely be aimed at beginners and wouldn't circuits using semiconductors have been far, far better? Still this is a criticism that can be levelled at nearly all books of this type and it is a reflection on all authors and publishers rather than on this book.

For what the book sets out to do, it is excellent. Without actually building the circuits it is difficult to judge the performance but they are all well tried and tested circuits and are described in great detail. It is tempting to find fault with the length—it is very long for only four circuits—but that would be unfair for the price is very reasonable at 80p and for that you do not feel cheated and the extra space has at least been used to detail the construction thoroughly.

ABC's OF THERMISTORS
By Rufus P. Turner
Published by Foulsham-Sams
96 pages, 8½×5¼in. Price £1.10.

NE'S first reaction to this book is to wonder how nearly one hundred pages can have been written on such a simple device as the thermistor. Knowing that "thermistor" derives from "thermally sensitive resistor" and that it's temperature coefficient can be positive but is usually negative, what else is there to say?

After the "specially written chapter for the guidance of the English reader" the rest of the book, printed in the United States, does give an adequate description of the characteristics of the thermistor and its many applications, in a non-mathematical way.

It was pleasant to see a reference to the fact that our own Michael Faraday observed the negative temperature coefficient of silver sulphide as long ago as 1833.

Circuits show the thermistor in its basic role as a temperature measuring device as well as its derived use as an anemometer, flowmeter, vacuum gauge etc. and as an altimeter. This last application is based on the fact that the boiling point of a liquid decreases with altitude but it is hoped that expeditions to the Himalayas have something more sophisticated to determine their altitude than a thermistor in a pot of boiling liquid as shown in this book!

A most useful application of the thermistor in the electronics field is the measurement of r.f. power levels well into the microwave region by means of a small bead type thermistor mounted within a waveguide; others include audio compressors/expanders, c.r.t. deflection circuitry, a.g.c. systems and oscillators where the thermistor is used to control negative feedback.

Unfortunately all the circuits shown are purely theoretical, no thermistor type numbers are indicated or values given for other components. The introductory chapter "for the English reader" does admit that the circuits are basic and not for the d.i.y. types and that values of small components etc. are not stated. In fact no values are given anywhere in the book for any component, large or small.

A pity, because the book could have been so good.—AED.

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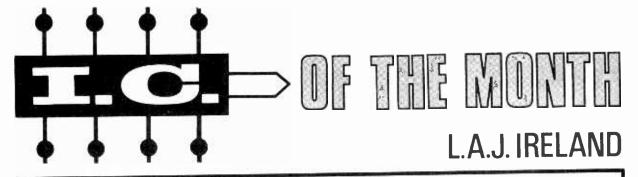
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Number 26

S.G.S. TBA631 TV Audio Detector/Amplifier

N modern times, after-sales service in the electronics industry is proving to be far too costly so any advance which limits this service to simply plugging in replacement units will be enthusiastically welcomed by both manufacturer and consumer alike. Lately the way has been paved for the introduction of a complete modular TV consisting of plug-in type i.c. sub-systems thereby providing enormous savings in production costs and after-sales service.

In addition to the obvious advantages of lower cost and greater reliability, inexperienced or semi-skilled technicians can perform repairs on a trial and error basis by simply plugging in replacement i.c's.

until the set functions.

Over the past few years great strides have been made particularly in the TV industry in this regard and today practically every i.c. manufacturer has on offer an integrated form of the i.f. sound amplifier and detector. In fact some firms included an audio preamp on the same chip as the i.f. strip and so it was only a logical step from here that eventually the complete audio power amplifier and i.f. sound section should appear in integrated form.

S.G.S. have recently released a new i.c. device capable of performing just these functions (TBA631), with the very attractive feature of having a price tag less than £3 and an audio power

output in excess of 2.5 watts.

As far back as Dec. 1967 PW published a design for an i.c. f.m. tuner using an RCA type CA3014. Other manufacturers quickly followed with remarkably similar versions of this i.c. and in fact the wide band limiting section of the TBA631 is almost identical with it. However, the similarity ends there as a coincidence type detector, low frequency separator and low frequency preamp follows before the recovered audio signal enters the more or less separate power amplifier, on the silicon chip.

Specification

The electrical specifications of the TBA631 are quite good. It gives an almost flat frequency response from 50Hz to 10MHz with an input threshold limiting voltage of 100 microvolts at 5MHz rising to 230 microvolts at 10MHz. Total harmonic distortion at an output power of 2 watts is less than 1% and this provides adequate volume for most domestic purposes.

A separate power supply is used for the r.f. and demodulation part of the circuit and this is designed

to operate at any voltage between 4.5 and 15V. Up to 24 volts can be applied to the power amplifier and with a quiescent current of a mere 18mA with a 12 volt supply, the i.c. should prove particularly useful for inclusion in portable tv systems.

The i.c. consists of an i.f. limiting amplifier section following the well established differential amplifier patterns. A phase shift network applied between pins 10 and 11 allows for the demodulation of the inter-carrier signal and, electrically isolated from the i.f. stages, follows a typical i.c. power output stage.

Applications

Fig. 1 shows a practical application of the TBA631 in the sound section of a TV receiver. Overall savings in components and simplification of alignment is fairly obvious and of course a similar circuit with a rearrangement of coil values can be made to function admirably as the i.f. and output stages of an f.m. tuner. The drop in gain of 4dB in the i.f. stage as compared to its operation at 5.5MHz will hardly be noticed.

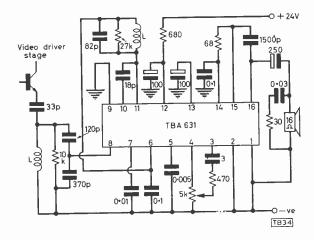


Fig. 1: In this practical application, inductors L may consist of 55 turn of 36g. enamel wire on a 1/2 in former, for 5.5MHz.

At its price and specification the TBA631 is a good buy and no doubt its appearance will shortly be felt in the consumer TV market. It is available from any S.G.S. distributor or from Neltronics, 14 Wellington Park, Belfast, BT9 6DJ.

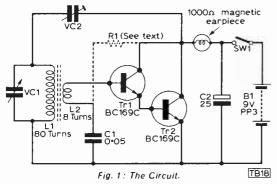
TAKE 2 (3)

JULIAN ANDERSON

A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

CONFESS that I don't know very much about Mr. Darlington but his name has been given to a transistor circuit configuration which has many uses in many fields of electronics. Some months ago we featured an ultra simple audio amplifier using two transistors, a resistor, a loudspeaker, a capacitor and a volume control and from the reaction of readers, it was a highly popular little circuit.

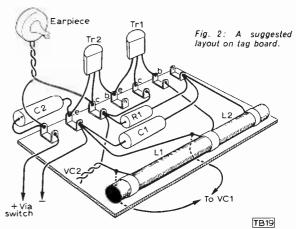
This month we are using basically the same circuit configuration but this time it is for a simple medium wave radio. It is the aim of this column to get the best possible use out of the minimum number of components and this circuit certainly achieves that. No external aerial or earth are required and reception may be expected of all local and some more powerful distant stations. The circuit operates from a PP3 battery and the small size of this and the other components means that the circuit lends itself to miniaturisation.



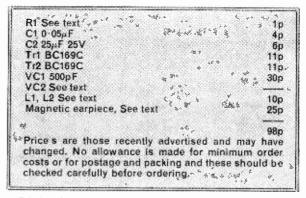
The magic of the Darlington Pair lies in the massive amplification available; the gain of the combined pair is equal to the product of the individual transistor gains. So, taking the best case, where both transistors have a gain of 900 (the maximum quoted for a BC169C), the circuit gain will be a massive 810,000. We are unlikely, however, to have two such high gain transistors but even with the minimum gain versions we shall have plenty of amplification in what is effectively a single stage.

The r.f. signals are induced into the tuned circuit comprising VC1 and L1 and are transformed by L2 and fed to the base of Tr1. This feeds directly to Tr2 where the signal is further amplified and applied to the magnetic earpiece. Astute readers will note that there is no obvious way in which the r.f. signals are detected and smoothed. Detection takes place in two ways: a circuit of this simplicity is hardly likely to amplify completely linearly and this means that there is a degree of detection. Alternatively there is a small degree of regeneration applied to the tuned circuit via VC2 and this aids detection. The self-capacity of the earpiece has been found sufficient to smooth the r.f. to allow it to be heard.

No. 33 Two transistor radio



★ components list



R1 is shown dotted in the circuit. The value of this resistor will depend entirely on the individual transistors used and it is not possible to give an absolute value for all types—indeed with several combinations of transistors used in the prototype it was not even found necessary; the gain is so high that the tiny leakage currents were sufficient to apply the bias. However a resistor will normally be required and the value may lie anywhere between $470 \mathrm{k}\Omega$ and $10 \mathrm{M}\Omega$.

The aerial comprises 80 turns of enamelled copper wire (about 30 s.w.g. but this is not critical) wound on a 3in. length of ³8in. diameter ferrite rod. L2 comprises a further 8 turns. VC2, as shown is made up from two short lengths of insulated wire, twisted together for optimum performance over the complete band.

The magnetic earpiece is shown in the circuit as 1000Ω impedance; this is the ideal but any type between 250Ω and $2,000\Omega$ will suffice. Low impedance types (usually 8Ω) and crystal types will not work in this circuit.

A suggested layout is shown in Fig. 2 on a short piece of tagboard with the tags along one side removed. If, by twisting VC2 together, there is no improvement or tendency to oscillation, then the connections to L2 should be reversed.

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1N5399	20p	AC176K	17p	BD136 BDY20	92p
1N5402	28p	AC187K	17p	BF115	23p
1844	9p	ACY17 ACY18	31p	BF167	18p
18940	5p		19p 23p	BF173 BF177	19p 25p
2N696 2N697	17p 18p	ACV20	20p	BF177 BF194	14p
2N706	12p	ACY21	21 p	BF195	15p
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2N1309	36p	AD161	330	BFY51	20p
2N 1613	23p	AD162	36p	BFY52	23p
2N1711	26p	AF114 AF115	24p 24p	B8X20	16p
2N1893 2N2147	54p 95p	AF116	22p	BY164 BY238 BYX38-300 BYX38-300	18p
2N2218	34p	AF116 AF117	22p	BYX38-300	38p
2N2218A	44n	A F118	82p	BYX 38-300	R 38p
2N2219 2N2270	38p	AF124 AF125	24p 24p	C407 C762	17p 19p
2N2369A	62p 19p	AF126		EA403	10p
2N2483	35p	AF126 AF127 AF139	22p 33p	EA403 EB383	10p
2N2484	4.20	AF139	331	EC401 EC402	18p
2N2646 2N2904	47p 38p	AF239 ASY26	36p 27p	EC402 NKT911	17p 25p
2N2905	44p	ASY27	360	NKT211 NKT212 NKT213	25p
2N2905A	47p	ASY27 ASY28	27p	NKT213	25p
2N2924	20p	ASY29	36p	NKT214 NKT217	23p
2N2925 2N2926	22p 11p	AU111 B30C250	97p 24p	NKT217 NKT961	50p 21p
2N3053	27p	B1912	66p	N K T271	18p
2N3054	60p	B5041	72p	NKT274	18p
2N3702	13p	BA102	25p 22p	NKT261 NKT261 NKT271 NKT274 NKT403 NKT405	65p 79p
2N3703	13p 13p	BA130 BA145	27p	NKT613F	30p
2N3704 2N3705 2N3706	13p 13p	BA156	13p	NKT613F NKT674F	24p
2N3706	13p	BB103/B	16p	OA47	8p
2N3708 2N3709	10p 11p	BB103/G BC108	16p	OA90 OA91	6p 5p
2N3710	130	BC109 BC122 BC125	120	OA95	6p
2N3711	13p 13p	BC122	21p	OA200 OA202	9p
2N3794 2N3819	15p 23p	BC125 BC126	15p 22p	OA202 OC19	10p 50p
2N3820	53p	BC140	30p	OC25	42p
2N3904	35p	BC140 BC147 BC148	30p 10p	OC25 OC29	76p
2N3906	35 p	BC148 BC149	9p 10p	OC35 OC36	60p 65p
2N 4036 2N 4058	55p 13p	BC149	19p	0C36	42p
2N4059	10p	BC153 BC169 BC177 BC178	11p	0C41 0C44 0C70 0C71	42p
2N4060	110	BC177	14p 13p	OC70	21p
2N4061 2N4124	11p 18p	BC178	13p 14p	OC71 OC75	38p 40p
2N4124 2N4126	27p	BC178 BC179 BC182L BC183L BC184L BC186	11p	OC81	25p
2N4284	15p	BC183L	10p	OC81 OC81D	25 p
2N4286	15p	BC184L	11p 42p	OC83 OC84	25p 25p
2N4289 2N4291	15p 15p	BC212L	16p	P346A	26p
2N4410	24p	BC213L	16p	82CN1	10p
2N4991	62p	BC214L	16p	8D1	10p 12p
2N5062 2N5457	61p 49p	RC259	9p 9p	8D4 V763	28p
2N5459	49p	BC267	17p	W106B1 W02	45p
40250	71p	BC268	15p	W02	40p
40251 40361	89p 55p	BC267 BC268 BC269 BC300	17p 49p	WP02 ZTX 300	95p 14p
40361 40362	55p 68p	1 BC301	37p	ZTX300 ZTX301 ZTX302	16p
40602	52p	BC303	60p	ZTX302	22p
AC107 AC126	4fir	BCY30	60 p	ZTX303	22p
AC197	20p 20p		75p 18p	DIAGON	27p
AC128	20p	BCY71	33p	ZIASSU	23p
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č	1/2W	5%	4:7-10M	E24	1.2	1	0.9
č	1 W	5%	4·7-10M	E12	2.5	2	1.9
MO	1/2W	2%	10-1M	E24	4	3.5	3
ww	1W	$10\% \pm 1/20 \Omega$	0.22-3.9	E12	7	7	6
ww	3 W	5%	12-10K	E12	7	7	6
ww	7 W	5%	12-10K	E12	9	9	8
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with ordinary electronic organs that simply blow air over mouth-organ type reads etc. Fully transistorized. SELF CORTAINED LOUDSPEAKER. Fifteen separate keys span two full octaete—play the "Yellow Rose of Texar", play "Stient Night", play "Aud Long Syne" etc. etc. You have the thrill and excitement of building it together with the pleasure of playing a real, live, portable electronic organ. NO FREVIOUS KNOW-LEDGE OF ELECTRONICS NEEDED. NO soldering necessary, simple as ABC to make. Anyone over nine years can build it easily in one short ecening following the fully illustrated step-by-step, simple instructions. OMLY 22.75 + 23p p. 4p. for kit, including case, nuts, screws, simple instructions, etc. Uses standard battery (parts available separately). Have all the pleasure of making it yourself, finish with an exciting gift for someone.

Find buried treasure with this READY BUILT & TESTED TREASURE LOCATOR **MODULE**

ONLY £4.95 FULLY TRANSIS-TORISED PRIN-

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TOR MODULE. Ready built
and tested—just plug in a PP3 battery and
'phones and it's working. Put it in a case,
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PORTABLE TREASURE LOCATOR EASILY
WORTH AROUT 2601. Extremely sensitive. PORTARE TREASURE LOCATOR EASILY WORTH ABOUT \$20 ! Extremely sensitive — penetrates through earth, sand, rock, water, etc.—EASILY LOCATES COINS, GOLD, SILVER, JEWELLERY, HISTORICAL RELICS, BURIED PIPES, ETC. Signals exact location by "beep" pitch increasing as you near buried metallic objects, So sensitive it will dried certain objects buried SEVERAL FEET BELOW GROUND: GIVES CLEAR SIGNAL ON ONE COIN! \$4.85 + 30p carr. etc. (High quality Danieh Stethoscope headphones \$2.75 extra if required.) EXAMINS AT HOME FOR 7 DAYS. YOUR MONEY REFUNDED IN FULLIF NOT 100%

BUILD 5 RADIO AND ELECTRONIC PROJECTS only £1.97



all transistors, loudspeaker. personal phone, knobs, screws, etc. all you need. Presentation box 37p extra as illus. (if required) (parts available eparately) no soldering necessary. Send £1.97 + 23p p. & p.

SOOTHE YOUR NERVES, RELAX WITH THIS AMAZING RELAXATRON

CUTS OUT NOISE POL-LUTION—SOOTHES YOUR NERVES! Don't under-NERVES! Don't under-estimate the uses of this fan-tastic new design—the RELAXATRON is basically a



RELAXATRON is basically a pink noise generator. Besides being able to mask out extraneous unwanted sounds, it has other very interesting properties. For instance, many people find a rainstorm mysteriously relaxing, a large part of this feeling of well-being can be directly traced to the sound of falling rain-trops!—a well known type of pink noise. IF YOU WORK IN NOISY OR DISTRACTING SURROUNDINGS, IF YOU HAVE TROUBLE CONCENTRATING, IF YOU FEEL TENSED, UNABLE TO RELAX—then build this fantastic Relaxatron, once used you will never want to be without it—TAKE IT ANYWHERE. Uses standard PP3 batterles (current used so small that battery life is almost shelf-life). CAN BE EASILY BUILT BY ANYONE OVER 12 YEARS OF AGE using our unique, step-bystep, fully illustrated plans. No soldering necessary. All parts including case, a pair of crystal phones. Components, nuts, servers, wire, etc. no soldering servers, wire, etc. no soldering engressed. stal phones. Components, nuts, wire, etc. no soldering. \$2.25 + 25p p. & p. Parts available separately

CONCORD ELECTRONICS LTD. (PW3) 8 Westbourne Grove, London, W.2. Callers welcome 9 a.m.-6 p.m. inc. Saturday

separately).

Transistorised Stereophonic High Fidelity AM/FM Tuner Amplifier System.



This system includes this elegantly styled solid state Teak finished cabinet tuner/amplifier. Covering VHF/FM. Short, medium and long wavebands. The latest 4 Speed B.S.R. Mono/Stereo record changer with 2-10in, x 6in matching elliptical speakers. A complete Hi-Fi Stereo Radiogram The latest 4 Speed B.S.N. Floriolistic Level Color Library Marching elliptical speakers. A complete Hi-Fi Stereo Radiogram at less than half normal price. SPECIAL OFFER £44

Easily fitted no technical

knowledge necessary. Credit Terms available First monthly payment of £5-83 followed by 9 monthly payments of £4.95. Total Credit Sale Price £49.50. Send £5.83 today,



FABULOUS VALUE

Hi-Fi stereo at a new low. System Ten-Ten; 4 speed BSR autochanger with cue and pause control plus solid state amplifier, 20 watt total output. Frequency response 20-20,000 Hz.
ONLY

CREDIT SALE TERMS: Send £4-93 (being the first of TEN monthly payments of £4-05 plus 88p. Carriage and Packing). To be followed by NINE monthly payments of £4-05 (Total Credit Sale Price £40-50).

EASY TO INSTALL NO TECHNICAL KNOWLEDGE REQUIRED. PLEASE SEND ME FREE DETAILS OF YOUR RANGE ost coupe NOW for PEE LEWIS Fradio 100, Chase Side London N.14 Tel: 01 - 886 3733/9666 teaflets

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SETS 1R5, 185, 1T4, 384, 3V4, DAF91, DF91, DK91, DL92, DL94, Set of 4 for \$1.02, DAF96, DF96, DK96, DL96, 4 for \$1.48.

_	_						_		_	_	
1R5	-28	130C17	-76	EABC80	-32	EM81	-41	PCL84	-34	UBC41	-52
185	-22	30C18	-61	EAF42	-50	EM84	-32	PCL85	-38	UBF80	
1T4	-16	30F5	-64		-40	EM87		PCL86	-38	UBF89	
384	-26	30FL1	-61	EB91	-10	EV51	-83	PCL88	-65	UCC84	
3V4	-87	30FL12	-69	EBC33	-40	EY86	.29	PCL800	.75	UCC85	
5U4G	-31	30FL14	-68	EBC41	-54	EZ40	-43	PENA4	.77	UCF80	
5V4G	-35	30L1	-29	EBC90	-22	EZ41	+43	PEN36C		UCH42	
5Y3GT	-26		-57	EBF80	-32	EZ80	-22	PFL200	-52	UCH81	
5Z4G	.85		-67	EBF89	.29	E281	.23	PL36	-49	UCL82	
6/30L2	-54	30P4	-57	ECC81	-17	GZ30	-34	PL81	-44	UCL83	-55
6AL5	-11	30P12	-72	ECC82	-20	GZ32	-40	PL81A	-47	UF41	-56
6AM6	·18	30P19	-57	ECC83	-25	GZ34	-48	PL82	·31	UF89	-80
6AQ5	-22	30PL1	-60	ECC85	-34	KT41	-77	PL83	-33	UL41	-57
6AT6	.20	30PL13	.75	ECC804	-54	KT61	-55	PL84	-30	UL44	£1.00
6AU6	-20	30PL14	-65	ECF80	.27	KT66	.78	PL500	-68	UL84	-80
6BA6	-20	30PL15	-90	ECF82	-26	LN319	-63	PL504	-63	UM84	-22
6BE6	-21	35L6GT	-45	ECH35	.80	LN329	.72	PM84	.33	UY41	-42
6BJ6	-41		-25	ECH42	-61	LN339	-63	PX 25	.95	UY85	-25
6BW7	.52		.25	ECH81	-29	N78	-87	P¥32	- 55	VP4B	.77
6F14	-40		-45	ECH83	-40	P61	-40	PY33	-55	X78	£2.75
6F23	-68	6063	-62	ECH84	-36	PABC80	-34	PY81	-25	X79	£2.75
6F25	- 53	AC/VP2	.77	ECL80	-30	PC86	.47	PY82	.25	277	-22
6K70	-12		-65	ECL82	-81	PC88	-47	PY83	-28	Transi	
6K8G		B729	-62	ECL86	-85	PC96	-42	PY88	-88	AC107	-17
6Q7G	- 85	CCH35	-67	EF39	-88	PC97	-89	PY800	.34	AC127	-18
68N7OT	-80	CY31	-80	EF41	-60	PC900	-81	PY801	-34	AD146	-37
6V6GT	·28	DAF91 DAF96	-22		.23	PCC84	-29	R19	-30	AF115	-20
6X4		DF33	-36	EF85	-28	PCC85	-25	R20	-56	AF116	-20
6X5GT	-23	DF91	-38		-80	PCC88	-40	U25	-64	AF117	-20
10P13	-28 -58	DF96	·16		-26	PCC89	-45	U26	-56	AF118	-48
12AT7	-17	DH77	.20	EF91 EF98	-13	PCC189	-48	U47	-64	AF125	-17
12AU6	.20	DK32	-33		·65 ·28	PCC805 PCF80	• 56	1149	.56	AF127	-17
12AU7	.20	DK91	.28	EF184	-31	PCF82	-28	U50		OC26	-25
12AX7	.22	DK92	-28	EH90	-35	PCF82 PCF86	-81	U52 U78		OC44	-12
19BG6G	-87	DK96	-38	EL33	-55	PCF800	·45	U191	·24	OC45	-12
20F2	-87	DL35	-40	EL34	-45	PCF801	-28			OC71	-12
20P3	-77	DL92	-26	EL41	-54	PCF801		U193 U251	·42	OC72 OC73	-12
20P4	-92	DL94	-37	EL84	-23	PCF802	-61	U301		OC81	-12
25L6GT	-20	DL96	-38	EL90	-26	PCF806	-56	U329	-88	OC81D	·12 ·12
25U4GT	-57	DY86	.24	EL95	-33	PCF808	-68	U801	-80	OC82	-12
30C1	-28	DY87	.24		-62	PCL82	-32	UABC80		OC82D	.12
30C15		DY802	-33	EM80		PCL83		UAF42		OC170	
	-00	2 1 302	- 30	2000	.41	LONG	-07	CAP42	.DI	00110	-23

READERS RADIO

85 TORQUAY GARDENS, REDBRIDGE, ILFORD, ESSEX. Tel. 01-550 7441,

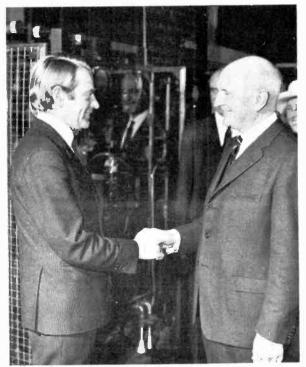
Post/Packing on 1 valve 6p, on 2 or more valves 3p per valve extra.

Any parcel insured against damage in transit 3p extra.

GOING BACK... 1970 60 50 40 30 20 COLIN RICHES ARTHUR DOWN

UITE a few of our readers, interested in the history of wireless, will have paid a visit to the Science Museum in South Kensington, London, and seen the collection of the old and not so old equipment on view there. The old gallery has now been moved to the third floor and on October 26th last a new and resplendent Telecommunications Gallery was formally declared open by the Minister for Posts and Telecommunications, the Minister, accompanied by Sir Harold Bishop, Chairman of the Museum's Advisory Council, toured the gallery with other distinguished visitors.

The North side of the gallery is devoted to the development of telegraph and telephone systems and many pieces of equipment from the early 1800's are displayed. The South side of the gallery is perhaps of more interest to our readers since it covers



The Minister for Posts and Telecommunications (left) is greeted by Sir David Follett, Director of the Science Museum.



The spacious nature of the new gallery is illustrated in this view of part of the collection of Army equipment.

radar and radio communications as well as broadcasting. Many examples of equipment, both civil and military, are exhibited in well-lit spacious showcases with detailed descriptive explanations.

Many were the oo's and ah's among us older visitors as we spied transmitters and receivers from the early days of the last war! Memories were stirred as thoughts went back to the problems of getting that last watt from a transmitter in a bouncing aircraft or bumping tank!

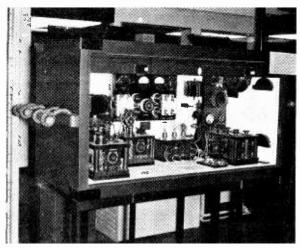
The equipment on view traces the history of wireless from the late 1800's and the discovery of the existence of electromagnetic waves by Hertz, who, although proving that the waves could pass through solid objects, took the matter no further. This aspect was left to Marconi who developed a practical wireless telegraphy system despite the very crude equipment of the time and the scorn of the "line-of-sight only" scientists of the day.

Great progress was made when shipping companies accepted the idea of ship-borne wireless realising its value from the commercial point of view and its potential as a means of getting assistance for their ships when they ran into trouble.

The next great push forward came with the 1914-18 war when rapid developments provided radio telegraphy and telephony facilities for the forces on on land, sea and in the air. The crude spark and arc

days were over and valves came into their own. Following the early experimental work of the radio amateurs long distance commercial circuits were established on short waves.

Subsequent discoveries are hardly "vintage" having taken place in the lifetime of many of us but even so the early radar equipment and certainly the Army's communication gear of that time looks crude beyond belief.



A complete 120watt field wireless station of 1918.

Broadcasting and TV have not been forgotten in the new gallery which, inevitably, includes Baird's 30-line television receiver. A visit to the exhibition is a must and after spending a while in the gallery one can return to the present day by visiting the amateur radio station GB2SM now re-sited adjacent to the new gallery.

MAXWELL

by G8DSH



"You're biased!"

CHARLES MOLLOY

edium ave Column

"MPOSSIBLE," I thought, writes Ian Rennison of Horsham, Sussex, when he read reports in Practical Wireless of American and Canadian stations being heard in UK on the medium waves. Ian now has a Trio 9R59D and he sends an impressive list of stations heard using a medium wave loop antenna in his bedroom.

CBNA 600kHz St. Anthony Nfld; CKCM 620 Grand Falls Nfld; CBN 640 St. John's Nfld; WNBC 660 New York; WOR 710 New York; CJOX 710 Grand Bank Nfld; WSB 750 Atlanta Georgia; WJR 760 Detroit Michigan (The Great Voice of the Great Lakes); WABC 770 New York; WCBS 880 New York; CJON 930 St. John's; CBM 940 Montreal; CHER 950 Sydney N.S.; CHNS 960 Halifax N.S.; WINS 1010 New York (All-news all the time); CFRB 1010 Toronto; WHN 1050 New York; CBA 1070 Moncton N.B.; WBAL 1090 Baltimore; WNEW 1130 New York; WHAM 1180 Rochester N.Y.; WOWO 1190 Ft. Wayne, Indiana; WCAU 1210 Philadelphia; WLOB 1310 Portland, Maine (5kW); WKLX 1350 Portsmouth, Virginia (5kW); WMYR 1410 Fort Myers, Florida (1kW at night); WTOP 1500 Washington D.C.; WMEX 1510 Boston; CJRS 1510 Sherbrook, Quebec; WKBW 1520 Buffalo, N.Y.; WCKY 1530 Cincinnati, Ohio.

Hugh Martin (G3XCD) of Wallasey, Cheshire, abandoned the Amateur Bands temporarily and connected his 20m dipole with 30ft downlead, to a BC946 medium wave 'Command' receiver. The time was 2340 hrs and he heard WINS 1010kHz New York and CBA 1070kHz Moncton N.B. This one-band receiver covers 520kHz to 1530kHz and only requires to be modified to convert from 28V to mains working. The MW Command receiver is not often available from commercial sources these days, but one can often be obtained, suitably modified, from private hands, for quite a modest sum.

George Harpur of Brentwood, Essex, logged 4 North American medium wave stations between 2300hrs and 2330hrs, the first time he tried out his new Eddystone 680X. George raises some interesting questions on operating techniques. Always turn OFF the a.v.c. when DXing on the medium waves. Set the l.f. (audio) gain control to a comfortable level and control the incoming signal with the r.f. gain. If the a.v.c. is left ON and an attempt is made to listen to a weak station only a kHz or two from a strong one, then the strong signal will operate the a.v.c., reduce the receiver gain and the weak station will be missed.

Conditions on the medium waves are better now than for several years and will continue to improve as we approach the minimum of the current sunspot cycle. Many North Americans can be heard before midnight, WINS 1010 New York being particularly prominent.

Send logs and information about the Medium Waves to:
132 SEGERS LANE, SOUTHPORT
PR8 3JG



High fidelity Monolithic Integrated

Two years ago Sinclair Radionics announced the World's first monolithic integrated circuit Hi-Fi amplifier, the IC.10. Now we are delighted to be able to introduce its successor, the Super IC.12. This 22 transistor unit has all the virtues of the original IC.10 plus the following advantages:

- 1. Higher power.
- 2. Fewer external components.
- 3. Lower quiescent consumption.
- 4. Compatible with Project 60 modules.
- Specially designed built-in heat sink.
 No other heat sink needed.
- 6. Full output into 3, 4, 5 or 8 ohms.
- Works on any voltage from 6 to 28 volts without adjustment.
- 8. NEW 22 transistor circuit.

SINCLAIR GENERAL GUARANTEE

Should you not be completely satisfield with your purchase when you receive it from us, return the goods without delay and your money will be refunded in full, including cost of return postage, at once and without question. Full service facilities are available to all Sinclair customers.

Output power 6 watts RMS continuous (12 watts peak).

Frequency Response 5 Hz to 100KHz \pm 1 dB.

Total Harmonic Distortion Less than 1%. (Typical 0.1%) at all output powers and all frequencies in the audio band.

Load Impedance 3 to 15 ohms.

Power Gain 90dB (1,000,000.000 times) after feedback.

Supply Voltage 6 to 28 volts (Sinclair PZ-5 or PZ-6 power supplies ideal).

Size 22 x 45 x 28 mm including pins and heat sink.

Input Impedance 250 Kohms nominal.

Quiescent current 8mA at 28 volts

Integrated Circuit Amplifier

With the addition of only a very few external resistors and capacitors the Super IC.12 makes a complete high fidelity audio amplifier suitable for use with pick-up, F.M. tuner etc. Alternatively, for more elaborate systems, modules in the Project-60 range such as the Stereo 60 and A.F.U. may be added. The comprehensive manual supplied with each unit gives full circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include car radios, oscillators etc. The very low quiescent consumption makes the Super IC.12 ideal for battery operation.



Price, inc. FREE printed circuit board for mounting.

£2.98 Post free

Sinclair Radionics Ltd, London Rd, St. Ives Huntingdonshire PE17 4HJ Telephone St Ives (048 06) 4311



Sinclair Project 60

The World's leading range of high fidelity modules







The easy way to buy and build **Project 60**

605



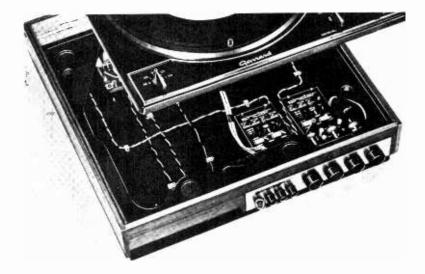
Project 605 is one pack containing: one PZ5, two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules. Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting.

Complete Project 605 pack with comprehensive manual, post free £29.95

All you need for a superb 30 watt high fidelity stereo amplifier.

Sinclair Radionics Limited, London Road, St. Ives, Huntingdonshire PE17 4HJ. Tel: St. Ives (048 06) 4311





Project 60 offers more advantage to the constructor and user of high fidelity equipment than any other system in the world.

Performance characteristics are so good they hold their own with any other available system irrespective of price or size.

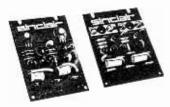
Project 60 modules are more versatile — using them you can have anything from a simple record player or car radio amplifier to a sophisticated and powerful stereo tuner-amplifier. Either power amplifier can be used in a wide variety of applications as well as high fidelity. The Stereo 60 pre-amplifier control unit may also be used with any other power amplifier system, as can the AFU filter unit. The stereo FM tuner operates on the unique phase lock loop principle to provide the best ever standards of sensitivity and audio quality. Project 60 modules are very easily connected together by following the 48 page manual supplied free with all Project 60 equipment. The modules are great space savers too and are sold individually boxed in distinctive white and black cartons. With all these wonderful advantages, there remains the most attractive of all — price. When you choose Project 60 you know you are going to get the best high fidelity in the world, yet thanks to Sinclair's vast manufacturing resources (the largest in Europe) prices are fantastically low and everything you buy is covered by the famous Sinclair guarantee of reliability and satisfaction.

Typical Project 60 applications

The Units to use	together with	Cost of Units	
Z.30	Crystal P.U., 12V battery volume control	£4.48	
Z.30, PZ.5	Crystal or ceramic P.U. volume control etc.	£9.45	
2 x Z.30s, Stereo 60, PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£23.90	
2 x Z.30s, Stereo 60, PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc	£26.90	
2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr	As above	£34.88	
Z.50, PZ.8, mains transformer	Mic, guitar, speakers, etc., controls	£19.43	
	Z.30, PZ.5 2 x Z.30s, Stereo 60, PZ.5 2 x Z.30s, Stereo 60, PZ.6 2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr Z.50, PZ.8, mains	Z.30 Crystal P.U., 12V battery volume control Z.30, PZ.5 Crystal or ceramic P.U. volume control etc. 2 x Z.30s, Stereo 60, P.U., F.M. Tuner, etc. 2 x Z.30s, Stereo 60, PZ.6 High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc 2 x Z.50s, Stereo 60 As above Z.50, PZ.8, mains trsfrmr Z.50, PZ.8, mains Mic., guitar, speakers, etc.,	

from a simple amplifier to a complete stereo tuner amplifier with Project 60 modules

Z.30 & Z.50 power amplifiers



The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well.

SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications). **Power Outputs**

Z.30 15 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M.S. into 3 ohms using 30 volts. **Z.50** 40 watts R.M.S. into 3 ohms using 40 volts: 30 watts R.M.S. into 8 ohms using 50 volts Frequency response: 30 to 300,000 Hz ± 1dB. Distortion: 0.02% into 8 ohms.

Signal to noise ratio: better than 70dB unweighted. Input sensitivity: 250mV into 100 Kohms. For speakers from 3 to 15 ohms impedance Size: 14 x 80 x 57 mm.

Built, tested and guaranteed with circuits and instructions manual £4.48

Built, tested and guaranteed with circuits and instruc-£5.48

Power Supply

Designed special for use with the Project 60 system of your choice. Use PZ 5 for normal Z.30 assemblies and PZ.6 where a stabilised supply is essential.

PZ.5 30 volts unstabilised £4.98 PZ.635 volts stabilised £7.98
PZ.845 volts stabilised ess mains transformer) £7.98



The Sinclair Guarantee

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail. Air-mail charged at cost.

Project 60 Stereo F.M. Tuner





First in the world to use the phase lock loop principle

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other original features include varicap diode tuning. printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. Good reception is possible in difficult areas, and often a few inches of wire are enough for an aerial. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system

SPECIFICATIONS—Number of transistors: 16 plus 20 in i.C. Tuning range: 87.5 to 108 MHz. Capture ratio: 1.5dB Sensitivity: 2μV for 30dB quieting: 7μV for lock-in over full deviation. Squelch level: 20μV. A.F.C. range: ±200 KHz. Signal to noise ratio: > 65dB. Audio frequency response: 10 Hz - 15 KHz (±1dB). Total harmonic distortion: 0.15% for 30% modulation. Stereo decoder operating level: 2μV. Cross talk: 40dB. Output voltage: 2 x 150mV R.M.S. Operating voltage: 25-30 VDC Indicators: Power on/tuning/stereo. Size: 93 x 40 x 207 mm.

Built and tested. Post free.

£25

Stereo 60 Pre-amp/control unit



Designed for Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

SPECIFICATIONS—Input sensitivities: Radio – up to 3mV. Mag. p.u. 3mV. correct to R.1.A.A curve ±1d8.20 to 25,000 Hz. Ceramic p.u. – up to 3mV: Alix – up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE + 15 to —15dB at 10 KHz: BASS ± 15 to —15dB at 100Hz.

Front panel: brushed aluminium with black knobs and controls. Size: 66 x 40 x 207mm. **£9.98** Built tested and guaranteed.

A.F.U. High & Low Pass Filter Unit



For use between Stereo 60 unit and two Z 30s or Z.50s. and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less

loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. Two filter stages – rumble (high pass) and scratch (low pass). Supply voltage – 15 to 35V. Current – 3mA. H.F. cut-off (–3dB) variable from 28KHz to 5KHz. L.F. cut-off (–3dB) variable from 25Hz to 100Hz. Distortion at 1 KHz (35V. supply (0.02% at rated Built tested and guaranteed. output. Size: 66 x 40 x 90 mm

To: SINCLAIR RADIONICS LTD LONDON ROAD	ST. IVES HUNTINGDONSHIRE PE17 4HJ
Please send	Name
	Address
l enclose cash/cheque/money order.	PW272

Sinclair Q16/Micromatic

Q16 High fidelity loudspeaker

The O16 employs the well proven acoustic principles specially developed by Sinclair in which a special driver assembly is meticulously matched to the characteristics of the uniquely designed cabinet. In reviewing this exclusive Sinclair design, technical journals have justly compared the Q16 with much more expensive loudspeakers. Its shape enables the Q16 to be positioned and matched to its environment to much better effect than is the case with conventionally styled enclosures. A solid teak surround with a special all-over cellular foam front is used as much for appearance as its ability to pass all audio frequencies without loss.

This elegantly designed shelf mounting speaker brings genuine high fidelity within reach of every music lover.

Specifications:

Construction: Special sealed seamless sound or pressure chamber with internal haffle

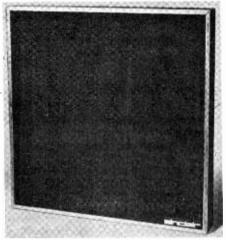
Loading: up to 14 watts RMS. Input Impedance: 8 ohms.

Frequency response: From 60 to 16,000 Hz. confirmed by independently plotted B and K curve.

Driver unit: Special high compliance unit having massive ceramic magnet of 11,000 gauss, aluminium speech coil and special cone suspension for excellent transient response.

Size and styling: 93 in. square on face x 43 in. deep with neat pedestal base. Black all over cellular foam front with natural solid teak surround

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Size: $36 \times 33 \times 13$ mm (1.8 x 1.3 x 0.5 in.) Weight: including batteries, ,28.4 gm (1 oz.)

Case: Black plastic with anodised aluminium front panel and spun aluminium dial.

Tuning: medium wave band with bandspread at higher frequencies (550 to 1,600 KHz)

Earpiece: Magnetic type.

On/off switching: By inserting and withdrawing earpiece plug.

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BP70 = 7470 BP72 = 7472	Master slave J-K flip-flop	0.29	0.26	0.24
BP73 = 7473	Dual Master slave J-K flip-flop	0.87	0.85	0.82
BP74 = 7474	Dual D type flip-flop	0.87	0 · 85 0 · 45	0.32
BP75 = 7475	Quad latch	0.49	0.40	0·42 0·88
$BP76 = 7476 \\ BP80 = 7490$	Cated full adoers	0.67	0.64	0.58
BP81 = 7481	16-bit read/write memory	0.97	0.94	0.88
BP89 - 7489	2-bit binary full adders	0.97	0.94 0.94 1.05	0.88
BP83 = 7483	Quad full adder	1.10	1.05	0.95
BP83 = 7483 BP86 = 7486 BP90 = 7490	Invert 4-wide 2-input and-or-invert gates Duai 4-Input expander Bingle-phase J-K filo-flop Master slave J-K filo-flop Dual Master slave J-K filo-flop Dual D type filo-flop Dual D type filo-flop Dual J-K with pre-set and clear Gated full adders 16-bit read/write memory 2-bit binary full adders Quad-2-input exclusive NOR gates BCD decade counter. 8-bit shift registers Dual entry 4-bit shift register 4-bit up-ilown shift register 4-bit up-ilown shift register 4-bit up-ilown shift register 4-bit inpule in parallel out shift- register 8-bit farallel in parallel out shift- register 8-bit stable latenes	0.82	0.80	0.28
BP90 = 7490 BP91 = 7491	BCD decade counter	0.07	0-64 0-84	0.58 0.78
BP92 = 7491	Divide-by-twelve counters	0.67	0.64	0.58
BP92 = 7492 BP93 = 7493 BP94 = 7494	4-bit binary counters	0.67	0.64	0.58
BP94 == 7494	Dual entry 4-bit shift register	0.77	0.74	0.68
BP95 = 7495	4-bit up-down shift register	0.77	0.74	0.68
$\mathbf{BP96} = 9496$	5-bit parallel in parallel out shift-	0.00	0-77	0-68
BP100 = 74100	register 8-bit bistable latenes Single L-V din den aggivelent 9000	1.75	1.65	1.55
BP104 = 74104	Cin-l- 7 77 61- 6 a-uluslant 0000			
	series	0.97	9-94	0.88
BP105 = 74105	Single J-K flip flop equivalent 9001			
	series	0.97	0.94	0-88
BP107 == 74107	Dual Master slave flip-flops	0.40	0·88 0·58	0·86 0·50
BP110 = 74110 BP111 = 74111	Dual data lock-out fin-flop	1.95	1.15	1.00
BP118 = 74118	Hex set-reset latches	1.00	1 15 0 95 1 25	0.90
BP119 = 74119	Hex set-reset latches, 24-pfn	1.85	1.25	1.10
BP121 = 74121	Monostable multivibrators	0.87	0.64	0.58
BP141 = 74141	BCD-to-decimal decoder/driver	0.67	0 64 1 40 1 70	0.58
BP145 = 74145 BP150 = 74150	BCD-to-decimal decoder/driver U/C	1.00	1.70	1·30 1·60
BP151 = 74150 BP151 = 74151	8-bit data selectors (with stroke)	1.00	0.95	0.80
BP153 = 74153	Dual 4-line-to-1-line data	1.20	1.10	0.95
BP154 = 74154	4- to 16-line decoder	1.80	1.70	1.60
BP155 = 74155 BP156 = 74156	Dual 2- to 4 line decoder	1.40	1.80	1.20
BP156 = 74156	Dual 2- to 4-line decoder O/C	1.40	1.80	1·20 1·60
BP160 = 74160 BP161 = 74161	series Single J-K fip flop equivalent 9001 series Single J-K fip flop equivalent 9001 series Dual Master slave fip-flops Gates master-slave fip-flops Dual data lock-out flip-flop Hex set-reset latches Hex set-reset latches Hex set-reset latches SCD-to-decimal decoder/driver BCD-to-decimal decoder/driver BCD-to-decimal decoder/driver O/C 16-bit data selector S-bit data selector (with strobe) Dual 4-line-to-1-line data 4-to 16-line decoder Dual 2- to 4-line decoder Dual 2- to 4-line decoder Dual 2- to 4-line decoder Sync, decade counter Sync, up-down BCD counter Sync, bright sync y-lown counter (single	1.80	1 70 1 70	1.60
BP190 = 74190	Sync. up-down BCD counter	8-50	8-25	8.00
BP190 = 74190 BP191 = 74191	Sync, up-down counter (single			
	clock line)	0.00		8.00
BP192 = 74192		2.10	1.95	1.75
BP193 = 74193	Sync. binary up-down counter (tow	0.10	1.05	1.66
RP196 - 74108	Pre-setable 50M Hz decade counter	1.80	1.70	1.60
BP197 = 74197	Pre-setable 50MHz binary counter	1.80	1.70	1 60
BP198 = 74198	8-bit parrallel L-R shift register	5.50	5.00	4.00
BP199 = 74199	8-bit parrallel access shift register	5.50	5.00	4.00
Devices may be m	Sync. binary up-down counter (tow clock lines). Pre-setable 50MHz decade counter Pre-setable 50MHz binary counter. 8-bit parrallel L-R shift register 8-bit parrallel access shift register lxel to quality for quantity price. Larg	er quan	tities—pr	ices on

Devices may be mixed to qualify for quantity price. Larger quantities—prices on application (TTL 74 Series only).

Data is available for the above series of I.C's in booklet form. Price 13p.

Owing to the ever increasing range of TTL 74 Series: please check with us for supplies of any devices not listed above, as it is probably now in stock.

BRAN	D NEW	LIN	EAR I.C's-FULL	SPEC		
					Price	
Type No.	Case	Leads	Description	1-24	25-99 1	00 up
BP 201C-8L201C	TO-5	8	G.P. Amp	68p	58p	45p
BP 701C-8L701C	TO-5	8	OP Amp	68p	50p	45p
BP 702C-8L702C	TO-5	8	OP Amp Direct OP	63p	50p	45p
BP 702-72702	D.I.L.	14	G.P. OP Amp Wide	-	-	
			Band)	58p	45p	40p
BP 709-72709	D.I.L.	14	High OP Amp	58p	45p	40p
BP 709P-4A709C	TO-5	- 8	High Gain OP Amp	58p	45p	40p
BP 710-72710	D.I.L.	14	Differential comparato	r 53p	45p	40p
BP 711-4A711	TO-5	10	Dual comparator	58p	50p	45p
BP 741-72741	D.I.L.	14	High Gain OP Amp			
			(Protected)	75p	60p	50p
μΑ 703C-μΑ703C	TO-5	6	R.F.—I.F. Amp	43p	85 p	27p
TAA 263-	TO-72	4	A.F. Amp	70p	60p	55p
TAA 293-	TO-74	10	G.P. Amp	90p	75p	70p
TAA 350	TO5	8	Wide band limiting	-		

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	NOTE	THESE	PRIC	ES!				
	I.C's DTL	930 S	ERIE	S		LO	GIC	
Type							Price	
No.		Function				1-24 2	25-99 10	0 up
BP930	Expandable duel 4-inpu	at NAND		. 17		23p	20p	15p
BP932	Expandable dual 4-inpu					25p	23p	20p
BP933	Dual 4-input expander					25p	23p	20p
BP935	Expandable Hex Inver					25 p	23p	20p
BP936						25p	23p	20p
BP944	Dual 4-input NAND ex							
D1 344	pull-up		, , ,			25p	23p	20p
BP945	Master-slave JK or RS					35p	32p	29 p
	Quad, 2 input NAND					23p	20p	15p
RP946						25p	82p	290
BP948	Master-slave JK or RS		2. 1					80p
BP951	Monostable	2.2			5.15	90p	85p	
BP962	Triple 3 input NAND		8.7		***	23p	20p	15p
BP9093	Dual Master-slave JK w	ith separ	ate cloc	k		80p	75p	70p
BP9094	Dual Master-slave JK	with sepa	rate clo	ek		80p	75p	70p
BP9097	Dual Master-slave JK	with Com	mon Cl	ock		80p	75p	70p
TOOOOO	Due I Wester slave IV (ROn	75n	70n

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UIC936 = 12 × µA 936	50p	U1C9094 = 5		50p
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50p	$UIC47 = 5 \times 7447N$	50p		50p
50p	$UIC48 = 5 \times 7448N$	50p		50p
50p	$UIC50 = 12 \times 7450N$	50p	$UIC86 = 5 \times 7486N$	50p
	$UIC51 = 12 \times 7451N$	50p	$UIC90 = 5 \times 7490N$	50p
	UIC53 = 12 × 7453N	50p	UIC91 - 5×7491N	50p
	$UIC54 = 12 \times 7454N$	50p	$UIC92 = 5 \times 7492N$	50p
	$UIC60 = 12 \times 7460N$	50p	$UIC93 = 5 \times 7493N$	50p
	$UIC70 = 8 \times 7470N$	50p	$UIC94 = 5 \times 7494N$	50p
	$UIC72 = 8 \times 7472N$	50p	$UIC95 = 5 \times 7495N$	50p
	$UIC73 = 8 \times 7473N$		UIC96 = 5×7496N	50p
	UIC74 = 8 x 7474N		$UIC121 = 5 \times 74121N$	50p
			UICX 1 = 25 × Asst'd	
				1.50
50p		50p		
	50p 50p 50p 50p 50p 50p 50p 50p 50p 50p	50p UIC46 = 5 × 7446N 50p UIC47 = 5 × 7447N 50p UIC48 = 5 × 7447N 50p UIC50 = 12 × 7461N 50p UIC50 = 12 × 7461N 50p UIC50 = 12 × 7461N 50p UIC30 = 12 × 7461N 50p UIC40 = 12 × 7461N 50p UIC70 = 8 × 7470N 50p UIC72 = 8 × 7470N 50p UIC73 = 8 × 747N 50p UIC74 = 8 × 747N 50p UIC74 = 8 × 7474N 50p UIC74 = 8 × 7474N 50p UIC76 = 8 × 7478N 50p UIC76 = 8 × 7478N	\$\begin{array}{l} 50\begin{array}{l} 50array	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

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For single outputs, 6v, 9v, 12v, 18v, £2.00. For two separate outputs, 4½v + 4½v, 6v + 6v, 9v + 9v, £2.50. P. & P. 15p. per unit. (Please state outputs read).

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*Goldring G850 Dia. *Goldring G800 Dia. *Shure M44.7 Dia. *Goldring G800E Dia. *Shure M55E Dia.	£3.75 £6.27 £12.55 £9.84 £18.16 £12.52 £20.57	£2 00 £4 00 £6 50 £7 50 £11 00 £9 50 £14 00
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	7.16	4 - 75
	11.63	8 70
	10 · 73	8 05
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SHURE M44-5	10.73	7 19
SHURE M44-7	9.84	7 · 15
SHURE M-44C	9 - 84	7 · 15
SHURE M44E	11:63	7 - 95
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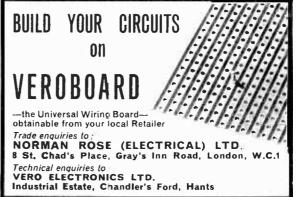
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1B3GT		6A87G	0.85	6F6G	0.85	10C2	0.50
1L4	0.20	6AT6	0.35	6F11	0.40	10D1	0.55
1R4	0.45	6AU6	0.25	6F13	0.45	10D2	0.50
1R5	0.40	6AV6	0.80	6F14	0.70	10F1	0.75
184	0.30	6AW8A		6F15	0.65	10F9	0.60
185	0.80	6AX4G		6F18	0.50	10F18	0.50
1T4 1U4	0.30	6AW8A	0.60	6F23 6F24	0.85	10L1	0.50
1U5	0.60	6BA6	0.00		0.75	10LD11	
1V2	0.50	6BE6	0.30	6F25 6F26	1.00	10P13	0.60
1X2B	0.50	6BF5	1.00	6F28	0.35	10P14	1.10
2A3	0.50	6BF6	0.55	6GK6	0.60	12AB5 12AC6	0.70
2CW4	0.70	6BH6	0.75	6J4	0.50	12AC6 12AD6	0.50
2D21	0.38	6BJ6	0.50	6J5GT	0.30	12AE6	0.55
3A4	0.40	6BK7A		6J6	0.20	12 A L 5	0.50
3BP1	3.00	6BN5	0.43	6J7	0.45	12AQ5	0.50
3B28	2.50	6BN6	0.45	6K6GT		12AT6	0.30
384	0.35	6BQ5	0.25	6K7	0.85	12AT7	0.35
3V4	0.48	6BR8	0.70	6K8G	0.40	12AU6	0.35
5R4GY	0.75	6387	1.80	6K25	0.75	12AU7	0.30
5U4(1	0.35	6BW6	0.85	6L6GT	0.45	12AV6	0.40
5 V 4 G	0.45	6BW7	0.80	6L7	0.40	12AV7	0.65
5 Y 3 G T	0.40		0.25	6L18	0.45	12AX7	0.80
5Z3	0.60		0.40	6LD20	0.50	12AY7	0.75
5Z4G	0.40		0.33	6N7GT	0.45	12B4A	0.60
6/30L2	0.80		0.40	6P1	0.60	12BA6	0.40
6AB4	0.35	6CB6	0.35	6P28	0.65	12BA7	0.40
6AF4A	0.55	6CD6GA		6Q7	0.40	12BE6	0.40
6AG5 6AG7	0.22		0.55	68A7 68G7	0.40	12BH7	0.45
6AH6	0.50		0.55	68K7	0.40	12BY7 12K5	0.60
6AJ8	0.30		0.65	68L7G1		12K7G	
6AK5	0.35		0.45	68N7G7		12Q7G7	
6AK6	0,60		0.70	6807	0.40	128R7	0.40
			0.50	68R7	0.40	20D1	0.50
6AL3	0.48		0.80	6T8	0.35	20L1	1.10
6AL5	0.20		0.50	6U4GT		20P1	0.50
6AM5	0.35		0.70	6U8A	0.40	20P4	1.10
0 4 350	0.00	41144	0.75	CUCCIT	0.40	OADE	1.00

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EF92 0.35 GZ31 GZ32

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į	2516GT 0.50	50B5 0.50	DK92 0.55	ECC88 0.40
I	25Z4G 0.80	50C5 0,50	DL96 0.45	ECC89 0.50
ı	25Z6GT 0.65	50CD6G1.20	DM160 0.65	ECC91 0.20
ı	30 A 5 0.50	50L6GT 0.55	DY86 0.32	ECC189 0.65
ı	30AE3 0.40	85A2 0,50	DY87 0.33	ECF80 0.35
ı	30C1 0.80	90 AG 2.40	DY802 0.35	ECF82 0.85
ı	30C15 0.80	90AV 2.50	E88CC 0.65	ECF86 0.85
ı	30C17 0.90	90C1 0.65	E180F 1.00	ECF8041.65
ı	30C18 0.80	90CV 2.40	E810F 2.90	ECH42 0.75
ı	30F5 0.85	807 0.50	EABC800,35	ECH81 0.80
ı	30FL1 0.75	813 8.75	EAF42 0.55	ECH83 0.45
I	30FL12 1.20	866A 0.75	EBC33 0.50	ECH84 0.45
ı	30FL14 0.85	5642 0.70	EBC41 0.55	ECL80 0.45
1	30L1 0.40	6080 1.60	EBC81 0.80	ECL81 0.50
1	30L15 0.85	6146 1.60	EBF80 0.40	ECL82 0.35
1	30L17 0.80	5360 1.25	EBF83 0.40	ECL83 0.70
ı	30P12 0.80	6939 2.25	EBF89 0.80	ECL84 0.55
ı	30P19 0.85	7199 0.80	EC53 0.50	ECL85 0.55
ı	30PL1 0.75	7360 2.00	EC86 0.60	ECL86 0.40
ı	30PL13 0.98	7586 1.25	EC88 0.60	EF40 0.50
ı	30PL14 0.90	7895 1.25	EC90 0.33	EF41 0.85
ı	35A3 0.55	9002 0.40	EC91 0.60	EF42 0,70
ı	35A5 0.75	9003 0.50	EC92 0.85	EF80 0.25
ı	35B5 0.65	AZ1 0.55	EC93 0.55	EF83 0.55
Į	35C5 0.50	AZ31 0.55	EC8010 2,25	EF85 0.35
1	35D5 0.75	CBL1 0.90	ECC35 1.00	EF86 0.30
i	35L6GT 0.50	CBL31 1.00	ECC40 0.65	EF89 0.38
ł	35 W 4 0.85	CY31 0.35	ECC81 0.85	
i	35Z3 0.70	DAF96 0.45	ECC82 0.80	EF91 0.88
ı	35Z4G 0.35	DF96 0.45	ECC83 0.80	EF92 0.35
1	35Z5GT 0.60	DK96 0.50	ECC84 0.80	EF95 0.35

- 1	EF183	0.80	HABC800.45	PL82 0.45	U301 0.40
	EF184	0.85	HK90 0.40	PL83 0.45	U403 0.60
	EF800	1.00	KT66 2.05	PL84 0.40	U404 0.60
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	EL34	0.50	PABC800.40	PL508 0.90	0.40
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1	EL42	0.65	PC900 0.48	PM84 0.60	UBC41 0.50
·	EL51	0.55	PABC800-40	PY31 0.30	UBC81 0.40
0	EL83	0.42	PCC84 0.40	PY33 0.63	UBF80 0.40
0	EL84	0.25	PCC85 0.40	PY80 0.40	UBF89 0.85
0	EL83	0.48	PCC88 0.55	PY81 0.30	UBL1 0.60
0	EL86	0.40	PCC89 0.55	PY82 0.85	UBL21 0.65
5	EL90	0.38	PCC189 0.55	PY83 0.38	UC92 0.40
5	EL95	0.35	PCC805 0.85	PY88 0.40	UCC85 0,40
5	EL821	0.60	PCC806 0,80	PY500 1.00	UCF80 0.55
5	EL822	1.30	PCF80 0.80	PY800 0,40	UCH21 0.60
5	ELL80	0.75	PCF82 0.85	PY801 0.50	UCH42 0.70
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0	EM71	0.80	PCF86 0.60	QQVO2-6	UCL81 0.60
5	EM80	0.45	PCF87 0.90	2.25	UCL82 0.85
5	EM81	0.60	PCF801 0.50	QQVO3-10	UCL83 0.60
5	EM84	0.35	PCF802 0.50	1.25	UF9 0:60
0	EM85	1.00	PCF805 0.80	QQV03-20A	UF11 0.50
5	EM87	0.70	PCF806 0.70	5.25	UF41 0.60
0	EN91	0.88	PCF808 0.85	QQV06-40 A	UF42 0.60
5	EY51	0.40	PCH2000.70	5,50	UF43 0,60
5	EY80	0.55	PCL81 0.50	TT21 8.00	UF80 0.35
0	EY81	0.40	PCL82 0.85	TT22 8.20	UF85 0.40
0	EY83	0.55	PCL83 0.65	TY2-125	UF89 0.40
5	EY86	0.40	PCL84 0.45	10.00	UL41 0.65
0	EY87	0.48	PCL85 0.40	U18/20 0.75	UL84 0.40
5	EY88	0.48	PCL86 0.45	U25 0.80	UM84 0.25
5	EZ40	0.50	PCL88 0.90	U26 0.80	UY1N 0.50
5	EZ41	0.50	PCL800 0.93	U31 0.60	UY11 1.00
0	EZ80	0.27	PCL801 0.75	U37 2.10	UY41 0.48
8	EZ81	0.29	PD500 1.80	U52 0.85	UY82 0.50
8	GY501	0.80	PF86 0.65	U76 0.85	UY85 0.40
5	GZ30	0.40	PF818 0.85	U78 0.35	W729 0.75
	GZ31	0.85	PFL200 0.65	U191 0.75	Z759 2.00
5	GZ32	0.48	PL33 0.85	U201 0.35	Z803U 1.20
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0.70 PL36 0.60 PL81

0.70 6U8A 0.40 0.75 6V6GT 0.40

0.40 0.50 1.10 0.50 1.10 1.20

20D1 20L1 20P1 20P4 20P5

6CD6G, 6CG7 6CH6 6CL6 6CW4 6CY5 6CY7 6D3 6DC6 6DK6 6DK6 6D84

6AM6

	TR	ANSI	STO	RS	
2N696	0.17	AC127	0.20	BD123	0.80
2N697	0.17	AC128	0.15	BD131	0.85
2N698	0.80	AC132	0.85	BD132	0.85
2N705	0.70	AC153	0.20	BF115	0.20
2N706	0.10	AC154	0.15	BF167	0.18
2N708	0.15	AC157	0.20	BF173	0.20
2N753	0.25	AC169	0.10	BF179	0.30
2N929	0.22	AC176	0.25	BF180	0.85
2N930	0.25	AC187	0.80	BF181	0.25
2N987	0.30	AC188	0.80	BF184	0.25
2N1131	0.25	ACY17	0.275	BF185	0.20
2N1132	0.25	ACY18	0.20	BF194	0.15
2N1184	1.25	ACY19	0.25	BF195	0.15
2N 1301	0.40	ACY20	0.20	BF196	0.20
2N1802	0.75	ACY21	0.20	BF197	0.20
2N1304	0.25	ACY22	0.15	BF200	0.35
2N1305	0.25	AD140	0.50	BFW87	0.25
2N1306	0.25	AD149	0.50	BFW88	0.23
2N1307	0.80	AD161	0.85	BFW89	0.20
2N1308	0.25	AD162	0.35	BFW91	0.20
2N1309	0.80	ADZ11	1.25	BFX88	0.25
2N1613	0.22	ADZ12	1.25	BFY17	0.40
2N1711	0.25	AF114	0.20	BFY19	0.60
2N1756	0.75	AF115	0.20	BFY50	0.25
2N2147	0.75	AF116	0.20	BFY51	0.20
2N2160	0.65	AF117	0.20	BFY52	0.25
2N2217	0.30	AF118	0.45	BSY26	0.20
2N2218	0.80	AF125	0.25	BSY27	0.20
2N2219	0.85	AF127	0.20	B8Y28	0.20
2N2369A	0.20	AF180	0.35	B8Y65	0.20
2N2477	0.65	AF181	0.85	BSY95A	0.15
2N2646	0.60	AF186	0.40	OC16	0.50
2N2905	0.85	AF239	0.40	OC22	0.50
2N2923	0.15	AFZ11	0.45	OC23	0.60
2N2924	0.15	A8 Y 26	0.25	OC24	0.60
2N2926	0.125	ASY27 ASY28	0.80	OC25	0.85
2N3053	0.25		0.25	OC26	0.25
2N3054	0.60	ASY29 ASY54	0.30 0.25	OC28	0.80
2N3055	0.75	A8Z15	0.20	OC29	0.60
2N3133	0.80	A8Z16	0.70	OC30	0.75
2N3134 2N3391	0.30	A8Z17	0.75	OC35	0.50
	0.20	ASZ18	0.75	OC36	
2N3392 2N3393	0.15 0.15	A8Z20	0.25	OC42 OC44	0.20
2N3394	0.15	A8Z21	0.40	OC44	0.15
2N 3395	0.20	BC107	0.125	OC70	0.10
2N3402	0.15	BC108	0.125	OC71	0.12
2N3403	0.15	BC109	0.125	OC72	0.25
2N3404	0.85	BC113	0.25	OC73	0.80
2N3414	0.20	BC118	0.80	OC75	0.20
2N3415	0.15	BC134	0.30	OC76	0.20
2N3416	0.25	BC147	0.175	OC78	0.25
2N3417	0.25	BC148	0.15	OC78D	0.20
2N3702	0.12	BC149	0.15	OC81	0.25
2N3703	0.12	BC152	0.15	OC81D	0.15
2N3704	0.17	BC158	0.15	OC83	0.20
2N3707	0.15	BC175	0.20	OC139	0.80
2N3709	0.12	BC186	0.25	OC140	0.85
2N3710	0.12	BCY30	0.25	OC141	0.60
2N3819	0.85	BCY31	0.40	OC170	0.25
2N3906	0.20	BCY33	0.25	OC171	0.25
28702	0.50	BCY34	0.80	OC200	0.80
28746	0.25	BCY72	0.20	OC201	0.60
AC113	0.15	BCZ10	0.80	OC202	0.65

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TYPE U4313. High sensitivity 20 Kohms/voit DC and 2 Kohms/voit AC. Accuracy 1.5% DC and 2.5% AC. 8 DC current ranges 604A to 1.5A. 6 AC current ranges 60-60M to 1.5A. 9 AC and DC Voltage ranges 1.5 to 500V. Resistance ranges 0-5-500 Kohms.

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