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LEAK 200 Spks. (pr.)
C49.90
LEAK Truspeed TIT system...........69.50
Total Rec. Retail Price ............194-40
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PEAK ST 30 Plus (cased)
EAK ST 30 Plus (cased) LEAK 200 Spks. (pr.)... LEAK Truspeed T/T system EAK Truspeed TIT system ... 649.90 Total Rec. Retail Price ............ $\mathbf{2 5 1 \cdot 7 0}$ LASKY'S PRICE G160. C. BP. ©3.00

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…...E15. 20 AD76K magnetic cartrldge ............E4. 35 Total Ree. Retail Price............. 126.70 IASKY'S PRICE EPZ C. P. E2.190 Package F LEAK ST70 Wharf............655.00 Gerr. (pr.)......E59.90 Garrard AP76 Garrard base and cover................. 11 Total Ree. Retail Price............. $484 \cdot 13$ LASKY'S PRICE $\mathbb{C l 2 9 .}$ C. . P. $63 \cdot 20$

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| 5ZAC； | ． 35 | 30LI | ． 29 | EBC90 | ． 22 | EZ41 | $\cdot 43$ | PEN36C | ． 70 | UCB42 | ． 58 |
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| 6AQ3 | －22 | 30P1를 | .72 | ECus： | ． 20 | （123？ | ． 40 | PL8A | ． 40 | UF゙41 | 56 |
| 6AT6 | ． 20 | 30P19 | ． 57 | ECC83 | ． 35 | （1234 | .48 | PL8： | 31 | U F8y | －30 |
| 6．1U6 | ． 20 | 30PL1 | ． 63 | FCCOs | ． 26 | KT41 | ． 77 | PL83 | －33 | UL4 | 57 |
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| 6 BW 7 | ． 52 | 35L64T | 45 | ECH3 ${ }^{\text {\％}}$ | ． 30 | LN329 | ． 72 | PM84 | 35 | UY41 | 42 |
| 6CD64 | 11.07 | 351 | ． 25 | ECH ${ }^{\text {a }}$ ？ | ． 61 | LN339 | －63 | Px23 | E1－00 | UY85 | 25 |
| 6 Fl 4 | ． 42 | 35744T | ． 25 | ECH81 | ． 29 | N78 | ． 87 | PY3－ | 55 | VP4B | ． 77 |
| 6 F 28 | －68 | 807 | ． 45 | ECH83 | 40 | P61 | $\cdot 45$ | PY33 | ． 55 | 77 | ． 22 |
| 6 F 25 | － 57 | 6063 | ． 62 | ECH84 | ． 36 | Pancro | ． 34 | PY8 6 | －25 | Tranti | r |
| 6K7 ${ }^{\text {\％}}$ | －12 | AC／VP？ | .77 | ECLBO | .30 | PC86 | ． 47 | PY8： | ． 25 | ACl0i | 17 |
| 6 K 8 4 | $\cdot 17$ | 13349 | ． 65 | ECL8： | ． 31 | PC88 | 47 | PY88 | －28 | ACl27 | ． 18 |
| 6Q74 | ． 27 | 13729 | －62 | ECL86 | ． 38 | PC96） | .42 | PY8＊ | － 33 | AD140 | ． 37 |
| 6SNTIT | － 30 | $\mathrm{CCH}^{\text {3＇}}$ | ． 87 | EF39 | ． 38 | PC97 | ． 39 | PY800 | －34 | AF115 | ． 20 |
| 6 VGG | ． 23 | CY31 | ． 30 | EF41 | ． 60 | P6900 | －33 | PY＊01 | －34 | AFl16 | 20 |
| 6V66； | －31 | DAF91 | ． 22 | EFPO | －23 | PCC84 | ． 29 | R1！ | －30 | AF117 | －20 |
| 6X4 | －23 | DAF゙ot | ． 36 | EF83 | ． 28 | PUC85 | ． 27 | R：0 | ． 56 | AF118 | ． 48 |
| 6X5：10 | ． 28 | DF33 | ． 38 | EF86 | .30 | PCC88 | － 42 | L | －64 | AFt25 | ． 17 |
| 737 | －33 | D P 91 | ． 18 | EF89 | －26 | PCC89 | －45 | U26 | －56 | AF127 | ． 17 |
| $10 \mathrm{P13}$ | － 58 | DF゙9 | ． 36 | E101 | .13 | PCCI89 | ． 48 | V4 | －64 | OC24 | ． 25 |
| 12AT | ． 17 | DH\％ | ． 20 | EF98 | －85 | PCC805 | － 56 | U4 4 | －56 | $0 \mathrm{OC4} 4$ | ． 12 |
| 12AU6 | ． 20 | DK3 ${ }^{\text {2 }}$ | ． 33 | EF183 | ． 28 | PCF＇80 | ． 28 | C50 | ． 26 | OC4à | ． 12 |
| 12AUT | ． 20 | DK91 | ． 28 | EF184 | ． 31 | PCF゙82 | ． 31 | Uう | －31 | 0 C 71 | －12 |
| 12AX7 | －22 | DK94 | ． 38 | EH90 | ． 37 | PCF＇86 | ． 45 | U＇7 | －24 | $\mathrm{OC}^{2} 2$ | －12 |
| 1913664： | ． 87 | DK96 | ． 38 | ELi3 | ． 55 | PCF800 | － 58 | U191 | －59 | OC75 | ． 12 |
| 20F： | ． 67 | DL33） | 40 | EL34 | .45 | PCF801 | ． 30 | 11193 | ． 42 | $0 \mathrm{C8} 1$ | 12 |
| 20 P 3 | ． 80 | DL9： | ． 26 | EL4 1 | ． 54 | PCFPO＇ | ． 40 | Uとら1 | －66 | OC81D | 12 |
| 20P4 | ． 92 | DL94 | ． 37 | EL84 | ． 23 | PCF805 | ． 61 | U301 | － 38 | 0082 | 12 |
| 25Lbict | ． 20 | DL96 | ． 38 | EL90 | ． 28 | PCF＇806 | ． 58 | U3＊9 | ． 66 | 0C82D | 12 |
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## NOVEMBER ISSUE

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DORCHESTER (Illustrated) Size $16 \times 11 \times 9 \mathrm{in}$. appr. Range 45-15,000 c.p.s. Rating 8-10 watts. Fitted High fux $13 \times 8 \mathrm{in}$. Dual Cone speaker. Imp. 3 or 15 ohms.
$\mathbf{1 9 \cdot 4 5} \begin{gathered}\text { Carr. } \\ 40 \mathrm{p} .\end{gathered}$
STANWAY II Size $20 \times 10 \frac{3}{2} \times 9 \frac{3}{4}$ in. approx. Rating 10 watts. Inc. $13 \times 8 \mathrm{in}$, speaker with highly flexible cone surround, long throw voice coil and 10,000 line magnet. High flux tweeter. Handsome Scandinavian design cabinet. Range $\mathbf{3 5 - 2 0 , 0 0 0}$ c.p.s. Imp. 8 ohms. Gives smooth realistic sound output. See 'package 117.85

## 'YORK' HIGH FIDELITY

 3 SPEAKER SYSTEM$\star$ Moderate size only $25 \times 14 \times 10 \mathrm{in}$.
$\star$ Response $\mathbf{3 0 - 2 0 , 0 0 0}$ c.p.s. Impedance 15 ohms $\star$ Performance comparable with units costing considerably more.
Consists of (1) 12 in . 15 watt Bass unit with cast chassis. Roll rubber cone surround for ultra low resonance, and ceramic magnet. (2) 3-way quarter section series cross-over system (3) $8 \times 5 \mathrm{in}$. high flux
middle range speaker. (4) High efficiency weeter middle range speaker. (4) High efficiency tweeter. Com
(5) Appropriate quantity acoustic damping material. km (5) Appropriate quantity acoustic damping material.
(6) Handsome Teak veneered cabinet. (7) Circuit and full instructions. Terms: Dep. $£ 4.50$ and 9 monthly payments $£ 2.25$ (Total £24.75).

DEMONSTRATIONS AT ALL BRANCHES

## AUDIOTRINE A55 HIGH QUALITY STEREO SYSTEM

$5+5$ WATT OUTPUT
Garrard 5200 Changer with low masas pick-up arm and Stereo Cartridge. Controls: TREBLE, BASS VOLUME, STEREO, BALANCE Operation on $200-250 \mathrm{v}$. A.C. mains Output rating I.H.F.M.
Luxurious Teak Vencer Finished Cabinets. Transparent plastic (tinted) cover included for main unit. Silver finished facia plate and matching control knobs.


## PAIR OF LOUDSPEAKER UNITS <br> incorporating high flux 8 in . 5 in .

 speaker. Size approx. $13 \times 71 \times$ 83 zins.PRICE COMPLETE
ONLY ONLY

Carr. $11 \cdot 25$ Terms: Deposit $£ 5.50$ and 9 monthly payments $£ 4 \cdot 50$ (Total $£ 46$ )

A REALLY SURPRISING STANDARD OF QUALITYIS OBTAINED FROM THIS COMPACT LOW PRICED SYSTEM RSC TRANSFORMERS LF CHOKES and RECTIFIERS


Where necessary
$350-0-350 \mathrm{v} .80 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a}, 0 \cdot 5-6.3 \mathrm{v} .2 \mathrm{a}$. 11.05 $260-0-250 \mathrm{v}, 100 \mathrm{siA}, 6.3 \mathrm{v}, 4 \mathrm{a}, 0-5 \mathrm{~b} .3 \mathrm{y}, 3 \mathrm{a} 8.86$
 $\$ 00-0-300 \mathrm{v} .130 \mathrm{~mA}, 6.3 \mathrm{v}$. $4 \mathrm{a} ., 0-5-6.3 \mathrm{v}$. 1 a
Suitable for Mniliard 610 A mplifier .... se 80 $350-0-350 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}, 0-5-6.3 \mathrm{v} .3 \mathrm{~s} .22 \cdot 20$
$350-0-350 \mathrm{v} .150 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{~m}, 0-5-6.3 \mathrm{v} .3 \mathrm{~s}$. 22.60 FILAMERT or TRAM 18 ISOR POWER PACK Types 6.3v, 1.5a. 490; 6.3v. 2s. 54p; 6.8v. 3a. 76p 6.8 v . $6 \mathrm{a} .81 \cdot 80 ; 12 \mathrm{v}$. 1a, 55 p ; 12 v .3 s . or 24 v . 1.5a CHARGER TRAMRFORMERS $0.8-15 \mathrm{v}$. $1 \ddagger \mathrm{a}$. 90 p ;
 AUTO (Step UP/itep DOWN) TRANSFORMERS
 OUTPUT TRAMEFORIERR
8tandard Pentodo $5,000 \Omega$ or $7,000 \Omega$ to $9 \Omega 50 \mathrm{p}$ Puh-Pull 8 watt ELS4 tor 3 or $10 \Omega \ldots \quad 88$ Puah-Pull 10 watts 6V6, ECL8 8 to $3,5,8$ or
$15 \Omega$
Puab-Pull ELis to 3 or 15 ® $10-12$ watts .. 81.86 Puah-Pull Ultra Linear for Mullard 510, etc. $28 \cdot 20$
 Push-Pull 20 witt htgh quality sectionally

## R.S.C. BATTERY/MAINS CONVERSION UNITS

 CYPE BM1. An all-dry battery eliminator. Size $51 \times 4 \frac{1}{2} \times 2 \mathrm{in}$ approx. Completely replaces bat teries supplying 1.5 v . and 90 v . where A.C. mains $200 / 250 \mathrm{v}$. $50 \mathrm{c} / \mathrm{s}$ is available.

Complete


Assembled ready for use

## SHOOTHITG OEOKRE

 $150 \mathrm{~mA}, 7-10 \mathrm{E}, 250 \Omega 70 \mathrm{p}$ $100 \mathrm{~mA}, 10 \mathrm{H}, 200 \Omega 80 \mathrm{p}$ : 60 mA 10H 400 ค
## BELEITVA

RECTIHISRS
F.W. (BrIdged)

Al o/12v. D.C.
Output. Max.
A.C. Input 18:

1a. 25p, 2a 85 p , 6a. 80p.

## BRADFORD BLACKPOOL (AGENT) BIRMINGHAM DARLINGTON DERBY <br> EDINBURGH GLASGOW HULL LEICESTER LEEDS LIVERPOOL LONDON MANCHESTER MIDDLESBROUGH NEWCASTLE-ON-TYNE NOTTINGHAM SHEFFIELD

SEE NEXT PAGE FOR TERMS OF BUSINESS, ADDRESSES etc.

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OF QUALITY

SEPARATE VOLUME CONTROLS PLUS TREBLE \& BASS CONTROLS MICROPHONE SOCKET WITH ASSOCIATED SWITCH \& VOL. CONTROL
TWIN TURNTABLE UNIT
WITH MONITORING FACILITIES
HI-FI CENTRES


## BASS REGENT

 50 WATT AMPLIFIER A powerful high quality allA powerful high quality all-
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for lead. riny bass guitar, vocalists, gram, radio, tape. Peak Output rating. Loudspeaker unit optional horizontal or vertical mounting. * Two extra heavy duty 12 in . Loudspeakers.
$\star$ Four Jack inputs and two Volume Controls for simultaneous use of up, to four pick-ups or "mikes"
Base and Treble controls. Send S.A.E. for leaflet. Credit Terms Deposit $£ 16$ and 9 monthly
of
payments
(Total
5 ${ }_{\mathbf{\Sigma 6}} \mathbf{6 7} .75$ )

30 WAT T HI-FI AMPLIFIER
FOR GUITAR, VOCAL or INSTRUMENTAL GROUP A 2 or 4 input, 2 vol. control Hi-Fi unit with Separate Bass and Treble controls. Cư̌rent valves. Peak output rating. Strong Rexine covered cabinet with handles.
ered cabinet witth handles. Attractive black/gold P.V.C. facia. Neon indicator. For
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Cart. 1.50

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## PHASE 50 MkII FRLD PHASE 100

50W AMPLIFIER 100 W AMPLIFIER OUTPUT


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 £14.34 (Total £149.06).

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F.A.L. PHASE 50 Mk.II AMPLIFIER PAIR PANE POP $45 / 226 \mathrm{~W}$ L/SPEAKERS.
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F.A.L. PHASE 100 AMPLIFIER PAIR L125 50W L/8 in cabinete.

## F.A.L. PHASE 100 AMPLIFIER

 4 FANE POP 50 L/GPEAKERSTerma: Deposit E 5.50 and 9
monthly paymenta of $\mathbf{8 4} \cdot 72$ (Total 447.98 ).
Terma: Deposit 210.50 and 9 monthly payments of 85 (Total $255 \cdot 50$ )
Terms: Deposit tas and $\theta$
 (Total 8129.58 ).
Terms: Deposit 215 and 9 monthly payments of $\$ 10.52$ (Total Elog 50).
package price 244 ${ }_{\text {cart }}^{\text {carr }}$ PACKAGE PRICE $\mathbf{4} 49-50{ }_{51}^{\text {car }}$
package price
 Package peice $199 \begin{gathered}\text { cart. } \\ \text { f1.50 }\end{gathered}$

R.S.C. AIO 30 WATT ULTRA LINEAR

HI-FI AMPLIFIER $\begin{gathered}\text { Higbly senaltive. Pusb-Pull high } \\ \text { nutput, Hum level-7odB Reaponse }\end{gathered}$ $\pm 3 \mathrm{~dB} 30-20,000 \mathrm{c} / \mathrm{s}$. All high grade components. Valves EFB6,
 EF86, ECC83, 807, 807, GZ3s. Separate Hass and Treble Controls.
Sensitlvity 36 millivolta. For Iligh Impedance microphones. Sensitivity 36 millitolta. For IIIgh Impedance microphones. For Clubs, 8choole, Theatres, Dance Balla, Ontdoor Functions,
ete. For Electronio Organ, Guitar. String Baza, etc. Gram. Radici or Tape. Two separate inputg with vol. controls permit such sa "mike" and Pick-up etc. to be used

 TRREMS: Deposit 24 and 9 monthly paymente of $88 \cdot 10$ (Total $282 \cdot 90$ ). Bend 8.A.E. tor leailet.

L13 8-10 WATTS
Incorporating high flux $13^{\prime \prime} \times 8^{\prime \prime} 8-10$ watt loudspeaker. Available with 3 or
15 ohm. impedance. (State when ordering.) Cabinet finished in Teak or
Afrormosia Veneer.
fR: 0


## L12/25 25 WATTS

120 watt heavy duty fomikpenker. Imper l-
 cotheques, Clubs, ashnols

monthly

## B4/100 100 WATTS

Fitted four extra heavy duty $12^{\prime \prime} 14,000$ Gauss 50 watt speakers for conservative rating of 100 watts. Impedance 15 ohms. Cabinet in ?" chipboard with centre reinforcement back to front. Rexine/Vynair covered. Acoustically filled and pressurised $27^{\prime \prime}$ y $27^{\prime \prime} \times 14^{\prime \prime}$ approx Ideal for base guitar or Electronic organ. Or Deposit $£ 8$ and 9 monthly payments $£ 5.90$ (Total £6s 10)

$L 12550$ WATTS


Or Deposit £4 and 9 monthly payments $£ 3 \cdot 35$ (Total £34-15)

## ALL FANE LOUDSPEAKERS GUARANTEED 2 YEARS

 [FANE 'POP' 25/2 LOUDSPEAKERSFAL DUO /100


C412S 50 WATTS
Fitted four $12^{\prime \prime} 11,000$ line 15 Overall size approx $56^{\prime \prime}$ Dep. 84 and 9 monthly payments $£ 3$ (Total £31)


## C4/100 100W

inc. four $12^{\prime \prime} 50$ watt speakers for conservative rating. Extra heavy construction; Size approx $58^{\prime \prime} \times 16^{\prime \prime} \times 10^{\prime \prime}$ Acoustically filled and pressurised. Terms: Dep. $\$ 7.50$ and 9 monthly payments 55.45 (Total $£ 56.55$ )

Carr. \&1

## £50.50

## SPEAKERS

IDEAL FOR VOCALISTS AND PUBLIC ADDRESS
All types 15 Ohms covered in Rexine anti Vynair
TYPE C4100 IS ALSO SUITABLE FOR BASS GUITAR OR ELECTRONIC ORGAN
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Fitted four $8^{\prime \prime}$ high flux 8 watt speakers. Overall size approx Terms: Dep is n $T$ T Terms: Dep £3
and 9 monthly
payments $£ 2$


18" 'POP' 100 15" 'POP' 60 RATING 100 WATTS R.M.S. 14,000 gauss $8 / 15 \Omega$ f79.5 Dep. 56 and 9


RATING 60 WATTS R.M.S
14,000 gauss $8 / 15 \Omega$ Dep. $£ 3.30$ and 9
\&1?.! $\quad \begin{aligned} & \text { Dep. } £ 3-30 \text { and } 9 \\ & \text { monthly payments } \\ & \text { £1.30 (Total } £ 15 \text { ). }\end{aligned}$ AN, ETC

12" 'POP' 50
RATING 50 WATTS R.M.S. 13.000 gauss $15 \Omega$ f10.50 ${ }^{\text {Den }}$ E2 and monthly payments \& ['15. Total $\mathbf{2 1 2} 35$
R.S.C. Branches listed below
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## TECHNICAL DETAILS

Bass Control $\pm 12 \mathrm{~dB}$ at 40 Hz . Treble Control $\pm 12 \mathrm{~dB}$ at 14 KHz .
Sensitivitles Mag. P.U. 3.5 m.v Pu 45 K ohm Amp. $100 \mathrm{~m} . \mathrm{v}$. into 100 K .
Radio Tuner $400 \mathrm{~m} . \mathrm{v}$. Into 400 K ohm, Crosstalk 53 dB .
Hum and Noise-75 dB min. vol. -65 dB max. vol
Total Harmonle Distortion 0.1 pe cent at 1 watt into 15 ohms.

* A modestly priced solid state unit.
* The Silver Facia with black lettering enhanced by matching control knobs, provides a high standard of appearance.
* Suitable for crystal or ceramic Gram. Pick-up cartridges, and Radio input.
$\star$ A wide range of tone variation is provided by the separate Bass and Treble 'lift' and 'cut' controls.
* A selector switch permits instantaneous selection of Gram. or Radio.
Speaker impedances between suitable.


## TECHNICAL DETAILS

Frequency Range $20 \mathrm{~Hz}^{\text {to }}$ 20 KHz Output (per channel) 4 watts I.H.F.M.

Bass Control $\pm 12 \mathrm{~dB}$ at 60 Hz Treble Control $\pm 14 \mathrm{~dB}$. at 14 KHz.

$0-200-250 v .50 \mathrm{~Hz}$ A.C. mains operation

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Price: Standard klt .. $\mathbf{E 7 . 2 5}$ post tree De-luxe initad.." © $\quad$ Mall order only
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* Individual Bass and Treble Controls.
$\star$ Frequency Response $\pm 1 \frac{d B}{}$ 27 Hz to 65 KHz .
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* Input Selector Switch.
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$\star$ Attractive silver finished metal facia and matching control knobs.
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Please add 50p carr. amplifier. Other Amplifiers - Tuners - Tape Recorders etc. Prices on application.

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Stereo headphones
Complete Complete wilh spare ear muffs.
 ${ }_{p .4}^{+23 p}$ Avaliable only from us at this price. Due to entire purchase of manufacturer's remaining stock this fantastic offer ls oden only whlle stocks last.

* High-fidelity reproductlon due to broad frequency response ( $20-20,000 \mathrm{~Hz}$ ) * Substantlally Increased stereo effect * Headphones fit the head gently and do not shift * Earpleces fit eare snugly (Cardanic suspension) t Tone quality superior to conventional loudspeakers. $\hbar$ Only expensive studio loud-
speakers can match the reproductlon quality of the K50. speakers can match the reproduction quality of the reproduced at concert hall volume (I). Preserving the lower base notes and reproduced at concert hall volume (1). preserving the lower basa
briflant freble tones without causing any strain to the lletener


GARRARD SP25 mk III £12.50 ${ }^{\text {Plus }}$ cailige Normal price $\mathbf{5 1 5 . 5 7}$ Wired with malns cable and 5 ft . twin screened stereo cable, 5 pin din plug. 53 p extra.
Ap75 Complete with base and cover $\mathbf{2} 25$ plus 75p carrlage. PLINTH AND COVER SUITABLE FOR GARRARD RANGE

Replacement Stered
DIAMOND STYLI BTA 9TA 9TAHC
GP91 ST4 ST9 GP91 ST4 ST9 EV26 GC8 75p others on requast +13 p p. \& p . Countdown SPEAKER Teak Cabinet

E12 plus 38p
A peaker of outstandling specifications and technical merlt. Solld teak cublnet size. 14 Teak cablilet size: $14^{-7} \times 10^{+} \times 6^{-}$ Orionnally designed for use with our Countdown stereo budget sytem but now avallable separately.

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Today's value $£ 6$
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Ronette 105 Stereo cartridge (Sapplat

## PLUGS <br> 

Pack 107 5-PIn DIn 20p
Pack 1083. Pin Din
Pack 135 d" Jack $^{\text {P }}$
Pack 130 "" Jack Sitereo
Pack 103 Loudspeaker Plug
Pack 100 Phono Plug
Pack 230 3-Pin Socket
Pack 234 Loudspeaker Socket
Ready-made Leads
3 -pin to 3-pin Din
3-pin to open end
5-pin to 5-pln Din
5 -pin to open end
5 -pin to 4 phono pluge Speaker lead Din to $\ldots p$... 93 p Extenslon 121165 p
All feads approx. 6ff. In length. Post
EMI 20w matched loudspeaker set 350
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Our price $£ 3.75$ plus 25p. D. \& p
$13 \frac{1}{2}$ " $\times 8 x^{\prime \prime}$ elliptlcal loud-
speaker and Indepen-
dent high frequency
units with assoclated
crossover network. Fre-
13000 Hz . The cone of
the bass unlt has a sur-
round desloned for hloh
travel glving freedom
when operated at low frem distortion
EMI 14A/770C \& 14.50 plus. 50 D
C- $x^{2}$ SONOTONE Cartridge ... (Fitted Dlamond Styll) (Ceramic) //st price et.10
Senslitivity:
9TAHC $55 \mathrm{mV} / \mathrm{cm} / \mathrm{sec}$
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rms minimum at $45^{\circ}$ a
$1,000 \mathrm{~Hz}$ measured on
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LEAK Delfa 30 （cased）
LEAK Delta 70 （cased）
METROSOUND ST20E
PHILIPS RH 591
PHILIPS RH 590
PHILIPS RH 580
PIONEER SA500
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ROGERS Ravensbourne
ROGERS Ravensbourne（cased）
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8 electronically mixe Discotheque．
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All the above take both ceramic 60.00
TUNERS
ARMSTRONG 523 AM／FM
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ARMSTRONG M8
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LEAK Delta FM
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PHILIPS RH 890
PHILIPS RH 691 ：$\because$ MIFM
IONEER TX 900 AM／FN
RANK ROTEL 320
ROGERS Ravensbourne chassis ROGERS Ravensbrook OGERS Ravens brook（cased） ROGEFS Ravensbourne In teak case sinclalr proje ELETON GT 101 tuner（stereo）

All above Tuners are complete Stereo Decoder except where with MPX
TUNER／AMPLIFIERS
AKAI AA 8500
AKAI 8300
AKA 6200.
ARENA 2600
ARENA 2700
ARENA T9000
ARMSTRONG M8 Decoder
ARMSTRONG 525
GOODMANS Mod．80．35w．R．M．S． GOODMANS Mod．80，35w．R．M．S．
GOODMANS MOdel 110 FM／MWi LW／SW 100W R．M．S．
LEAK Delta 75
PHILIPS 882 wlth stereo cassett PHILIPS RH 790 PIONEER S X770 AM／FM PIONEER SX9
 ROGERS Ravensbrook（cased） TANDBEAG 1171 comp．with TANDEERG TR200 without decoder ＊TELETON F2000
TELETON TAT 20
TELETON 10AT1 150w．RMS
TELETON TFSSO
TELETON TFS50 LA M $\mathbf{M} \mathbf{W} / \mathrm{L} W / F M$
TELETON CR55
WHARFEDALE $100-1$


## 54

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All the above Tuners and Tuner／Amplifiers take both ceramic and magnetic cartrldges except Teleton F2000 which takes ceramic only．All include MPX Stereo Decoder with the exception of Armstrong where decoder is extra as listed

Rec．Retail Comet
CARTRIDGES
GOLDRING 800
GOLDRING 800 E
GOLDRING 800 E
GOLDRING 800 Super E
－GOLDRING CS90 Stere。
＊GOLDRING CS91／E
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EMPIRE 999TE／X
EMPIRE 999SE／X
EMPIRE 999E／X
EMPIRE 999／X
EMPIRE 909E／X
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## But Why?

0NE of the most difficult tasks to face a technical journalist is to write an article for the absolute beginner. It is comparatively easy to prepare something for the advanced reader, for the author is aiming at those generally a little below his own standard. An article beamed at middle-of-the-road readers is, perhaps, the least troublesome because the author does not have to dwell on fundamentals or to go too deeply into advanced theory.
But the snags come when a writer has to do something for "the beginner"-a term full of pitfalls, for there are various degrees of that species. The main difficulty for the writer is to put himself in the position of his potential readership and to anticipate questions which might arise in the mind of a newcomer to the subject. A point which is to the author perfectly obvious may cause a beginner to feel perplexed and form questions in his mind. Taken to its extreme;' the author must, as far as possible, assume that the newcomer knows virtually nothing-an impossibility in practical terms, for some sort of mental line has to be drawn.
In P.W., we have to cater for all grades of experience. In general, a constructional article is geared to provide sufficient information for a constructor who has reached a stage at which he should reasonably be expected to be able to tackle the particular project. Since levels vary so widely, some readers complain that articles are too elementary while others think they are too advanced. This is the perpetual dilemma of trying to please everyone!
We do feel, however, that it is not a bad thing to err on the side of simplicity, for if the beginner is the one who wants to ask the most questions it is obvious that he is the one who needs greater attention. This is one reason why we have periodic bursts of special features for the beginner, such as the new series on transistor circuitry started in October and the extra 8 -page supplement included with this issue aimed at providing some basic guidance on the main components likely to be encountered by the home constructor.
Author Hellyer said in the October issue, "... any beginner worth his salt is going to say 'But Why???' We would go further, for the path of progress of any enthusiast will be travelled faster if he makes a point of always asking 'But Why?'-and finding the answer-when confronted with an aspect not fully understood.
W. N. STEVENS-Editor.

## NEWS AND COMMENT

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SUPPLEMENT:Components Dictionary by S. Yeatman
JANUARY ISSUE WILL BE PUBLISHED ON DECEMBER 3rd

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# MEWS... NEWS... <br> Wews... 

BSR Transcription


I'SR's new unit, the McDonald 810, priced at $£ 45 \cdot 51$ for the basic unit, was shown at the Audio Fair for the first time. Features include push button operation, a pitch control for absolute accuracy of turntable speed and a virtual friction free pick up arm movement which is gyroscopically controlled with a concentric gimbal mount.

Twelve months ago, BSR Limited launched the BSR McDonald consumer range. The 810 is the culmination of design expertise and production efficiency which has successfully produced in succession the wide selling MP 60 and HT 70 units.

The technical data for the 810 is impressive. It is a two speed player, $331_{3}$ and 45 rpm , utilising as its heart a 4 pole dynamically balanced synchronous motor driving a $7^{1}{ }_{4} \mathrm{lb}$. diecast balanced turntable. A stroboscopic centre plate when coupled with the pitch control ensures absolute turntable accuracy. A low mass pick up arm, over $8^{1}{ }_{2} \mathrm{in}$. in length has less than $0.5^{\circ}$ per inch tracking error.

Although primarily a single play unit, versatility comes with an interchangeable umbrella spindle giving true automatic function if required.

## "Sonex 72"

The Third International Exhibition of Audio Equipment, operated by British Audio Promotions Ltd, on behalf of the members of The Federation of British Audio will be mounted at the Skyway Hotel, Bath Road, Hayes, Middx (near London Airport) over the period from Wednesday, March 22, 1972, to Sunday, March 26, 1972.

## Hacker RP73

This newly-designed successor to the famous Hacker Autocrat RP33 home/car portable radio incorporates an integrated circuit and ceramic filter in its design.

In common with its predecessor the Autocrat Mark 2 Model RP73 offers extreme portability for use in the home, and a special changeover aerial circuit for inter-ference-free reception in a car. Price is $£ 25 \cdot 25$ including Purchase Tax. Hacker Radio Ltd, Norreys Drive, Cox Green, Maidenhear. Berks.


## Meteronic Scope



The MSB 101 oscilloscope has a bandwidth of d.c.- 8 MHz ; vertical sensitivity of $100 \mathrm{mV} / \mathrm{cm}-50 \mathrm{~V} / \mathrm{cm}$; sweep speed range of $100 \mathrm{nSec} / \mathrm{cm}$ $150 \mathrm{mSec} / \mathrm{cm}$; and a unique signal locking circuit which by means of a single control enables the user to select through 'Free Run', 'Internal Signal Sync' to 'Triggered. Also provided is switch slope selection. Fibreglass P.C. boards are fitted as standard. The MSB 101 size is $8 \times 6 \times 4 i n$. and weighs 51 lb . Price: $£ 69$. Meteronic, 114/116 Shipbourne Road, Tonbridge, Kent. Tel. Tonbridge 61448.

## Daystrom Throw It Around

Daystrom has introduced a 660 series drop-proofed multimeter. These precision meters are warranted to operate within specification after being dropped from a height of five feet. The meter mechanism floats inside a sealed, high-impact plastic case. These multimeters also have temperature compensation, with shielded and electrically protected meter movement. The meter maintains accuracy in extreme environments and will not be damaged if, as sometimes happens, the user accidentally connects it to a high voltage source. Daystrom salesmen sometimes demonstrate the 660 series by throwing the meter on the customer's floor. So far, customers have had a worse shock than the meter! So, if you feel like chucking a $£ 29$-85 meter about, contact Daystrom (Schlumberger), Bristol Road, Gloucester GL2 6EE.


## WEWS... <br> WEWS... MEWS...

## Litesold System

The Litesold ETC/1 Soldering System consists of a lightweight soldering iron which is fed from a solid state power/control unit giving fully automatic electronic control of the temperature of the front of the bit.

Operating temperature is fully adjustable by means of a calibrated dial on the power unit over a wide range from $150 / 400^{\circ} \mathrm{C}$. Thus there is no need to change bits for different settings which can be altered and read-off instantly.

The most important feature is the total avoidance of electrical disturbance and R.F.I. generation


## A New Iron From Antex



The element of this new Antex soldering iron is totally enclosed within a ceramic shaft. (Aluminium oxide.)

Near perfect insulation has been achieved; as a result there is no measurable leakage and live transistors can be soldered without risk of damage.

The 15 watt element generates a temperature of up to $450^{\circ} \mathrm{C}$. at the tip to facilitate high speed sol-
by the control unit which allows the iron to be used on ultra-sensitive equipment and components.

The plug-in soldering iron contains no control components except the temperature sensor and is as cheap and simple to repair as an ordinary iron.

Long-life bits slip over the heating element and are available in a range of tip sizes. Price is £19.80. Light Soldering Developments Ltd., 28 Sydenham Road, Croydon, CR9 2LL.
dering. A choice of four iron coated bits and one special bit plated with iron, nickel and chrome is available: all designed to ensure long bit-life.

The complete iron has passed a test of 4,000 volts a.c. and each production model is tested at 2,000 volts a.c. Further details from: Antex Limited, Mayflower House, Plymouth, Devon.

## Eagle International

Eagle International will add a quadraphonic synthesiser to its range in January 1972. Designated AA10, it enables a conventional stereo system to be turned into a quadraphonic system by dividing the 2 -channel output from a stereo amplifier into 3 or 4 channels based on sum and difference signals.

## Fver Ready Co's Rechargeable Cells

These cells, marketed by the Ever Ready Co. are sealed Nickel Cadmium types and have been used for some time now as the rechargeable power units in small portable appliances where the charging unit is integral. Now they are available to the home constructor and prices vary with quantity and capacity but typically a U2 size replacement would cost something over $£ 2$ for a single cell but would be proportionately reduced for larger quantities.

Button cells are more normally supplied as higher voltage prepacked batteries and typically a $4 \cdot 8 \mathrm{~V} 550 \mathrm{mAh}$ battery as used in radio controlled models, would cost around $£ 3 \cdot 30$.

Cells and battery packs are available direct from the manufacturer and the smaller button cell packs from reputable suppliers to the radio controlled model field. The Ever Ready Company (Gt. Britain) Ltd., Special Battery Division, Hockley, Essex.


TYPACAL CYLINDRICAL CELL CONSTRUCTION


TYPACAL BUTTON CELL CONSTRUCTION


ANY means of spreading the great number of short wave transmissions which can be heard over an increased tuning range is helpful, simplifying and easing tuning. When several ranges are needed it becomes difficult to use separate inductors for each range, involving a large number of coils, with all the associated switching.

In the receiver described here, only two coils are required band-changing being achieved by bringing in pairs of fixed capacitors. This breaks up the full tuning range into a number of smaller divisions.

## CIRCUIT

Fig. 1 is the mixer stage circuit the wiring being very much simplified by using this switching arrangement. L1 is the aerial coil, tuned by VCl, and L2 the oscillator coil, tuned by VC2. VCl and VC2 are sections of a small ganged capacitor, operated through a cord drive.

The 2 -pole 9 -way rotary switch S2/S3 selects the required band. With the switch in position $1, \mathrm{VCl} / 2$ alone are in use, for the highest frequency band. When the switch is in position 2, C2 and C10 are in circuit. Each of these capacitors is 50 pF , so the next range runs on from the frequency reached when $\mathrm{S} 2 / 3$ was in position 1 , and VCl/2 fully closed. In a similar manner, position 3 of the switch brings in C3 and CII, each of 100 pF . The next lower frequency band employs $C 4$ and $C 12$, each of 150 pF , with the switch in position 4. This continues for the nine ranges, each pair of capacitors being 50 pF larger in value than the previous pair.
$\mathrm{VCl} / 2$ has a swing of a little over 50 pF , so that ranges overlap. VC3 is a panel trimmer, which can be set for best volume on any band, or when altering the aerial. Sl is an aerial switch, used for the attached telescopic aerial or an external aerial.

The capacitors C 2 to C 9 for the aerial circuit, and C 10 to Cl 7 for the oscillator, are $1 \%$ or $2 \%$ silvermica, and any variation in the exact capacitances of the components used is easily cancelled out by VC3.

## IF AMPLIFIER

A conventional high gain intermediate frequency amplifier is used, Fig. 2. This has two double-tuned i.f.t.'s, and one single tuned i.f.t. resulting in good selectivity.

The i.f. amplifier is wired as a separate unit, on


The complete clrcuit of the 9 Band Recelver is made up of Fig. 1, (left) mixer stage; Fig. 2, i.f. stages and Fig. 3 the audlo output stage. The constructor only need assemble the mixer and i.f. stages since the audlo stage is a packaged module.

686
a small insulated board. Input from the mixer stage is to pin 2 of i.f.t. 1 and audio output is from D1 and C26. VR1 is the usual audio volume control.

## AUDIO AMPLIFIER

This provides high gain and 330 mW output into a 15 ohm speaker. Fig. 3 is the circuit and $\operatorname{Tr} 4$ is the first a.f. amplifier stage, stabilised by R14. Output from Tr4 collector is via C30 to the base of Tr5, which with Tr6 forms a Darlington pair driver for the output transistors $\operatorname{Tr} 7$ and $\operatorname{Tr} 8$. These form a push-pull complementary-symmetry stage, working in Class B, with diode D2 for thermal stabilisation. Feedback through R17 maintains operating
conditions for the four directly-coupled transistors Tr 5 to Tr8.
This circuit has plenty of amplification and volume. In order to simplify construction of the whole receiver, the audio amplifier is obtained as a printed circuit package, ready for use, and incorporating matched transistors.
A is the common positive line, and D the negative line. Point C is for audio input. The resistor R13 is included in the amplifier. R12, which is in series with R13, was found to be necessary for stable working in this particular receiver.
Leads from D (battery negative line) and E run to the 15 ohm speaker. The circuit is of the transformerless type and a speaker of other than 15 ohm impedance should not be used.


Fig. 2. The circuit of the i.f. stages, constructed as a separate unh on a paxolln panel (See Fig. 6). The input comes from oln 8 on 22 in the mixer stage.

Fig. 3. Since the audio stages are contained within a packaged module this circuil of the 5 transistor unlt is given for interest only. Input from the lif. assembly goes to pin C, the loudspeaker to pins $D$ and $E$ and the earth line to the onloff switch S3. (Note: C23 should read C32.)


## MIXER STAGE ASSEMBLY

A 10 in . x 4 in . flanged plate (universal chassis member) serves as panel for the controls and the top of the case. The controls are placed lin. from the botton of this plate, VC3 and the cord drive spindle being $1^{3} 4 \mathrm{in}$. from the plate ends and $\mathrm{S} 2 / 3$ and VR1-equally spaced between these.
$\mathrm{VCl} / 2$ is fixed as in Fig. 4 sq that the top of the drum is about ${ }^{1}{ }_{8}$. below the top of the plate. One pulley is above the cord drive spindle, to keep the cord parallel with the plate. The second pulley guides the cord clear of the bushes of S2/3 and VR1. The pulleys are on bolts fixed with lock nuts to the plate. The cord is given one complete turn round the drive spindle, then passes round the wheels and


Flg. 4. Layout of the mixer assembly built on an aluminium plate.
drum. It is taken through the drum slot, and tied so that it is under tension from the spring.

Fig. 4 shows wiring, etc., for this stage. L1, L2 and the other items are mounted on a piece of paxolin 5 in. $x{ }^{21}{ }_{2}$ in., which has a cut-out section to clear $\mathrm{S} 2 / 3 . \mathrm{VCl} / 2$ is bolted to the 10 in . x 4 in . plate, and the paxolin is in turn bolted to the underside of the ganged capacitor. Additional support is given by a bracket attached to the paxolin and rear of the 9 -way switch.

Transistor Tr has three leads soldered directly


Fig. 5. Detalls of the wiring of the bandswitch S2/S3.

## $\star$ components list



VR1 $5 \mathrm{k} \Omega$ potentiometer, log, with switch (S3).

## Capacitors:

|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | 150 pF | C10 | 50 pF | C19 | 0.01.1 F |
| C2 | 50 pF | C11 | 100pF | C20 | 0.01/дF |
| C3 | 100pF | C12 | 150pF | C21 | 10/4F 6 V |
| C4 | 150 pF | C13 | 200pF | C22 | 0.04 1 F F |
| C5 | 200pF | C14 | 250pF | C23 | 0.04/1F |
| C6 | 250pF | C15 | 300 pF | C24 | 0.0411F |
| C7 | 300pF | C16 | 350pF | C25 | 0.5/f F |
| C8 | 350pF | C17 | 400pF | C26 | $0.01 \mu \mathrm{~F}$ |
| C9 | 400pF | C18 | $0.01 \mu \mathrm{~F}$ |  |  |
| Cap mic VC | acitors | to C1 | 7 inc . a 75 pF | 1\% | 2\% silv |
| $\checkmark$ | $12 \begin{aligned} & 2 \mathrm{~g} \\ & 50 \mathrm{p} \\ & \end{aligned}$ | r-spa | ced vari |  |  |
| TC | 30p | e-set |  |  |  |

Semiconductors:

| Tr1 | OC170 | Tr3 | AF117 |
| :--- | :--- | :--- | :--- |
| Tr2 | AF117 | D1 | OA81 |

## Inductors:

| IFT1 | IFT18/465 (Denco) | L1 | Range 4 Blue |
| :--- | :--- | :--- | :---: |
| IFT2 | IFT18/465 (Denco) |  | (Transistor) |
| IFT3 | IFT14/465 (Denco) | L2 | Range 4 Red |

(Transistor)

## Audio Amplifier:

PC3 Packaged circuit (Newmarket).

## Miscellaneous:

Cabinet: 2 off, $10 \mathrm{in} . \times 4$ in. Universal chassis flanged member (Home Radio). 2 off, 7 tin $\times$ $4 \frac{\mathrm{i}}{2} \mathrm{in}$. plywood. 2 off, $10 \mathrm{in} \times 7 \mathrm{in}$. hardboard. Tuning drive: Drum, ${ }_{2} 3 \mathrm{in}$. dia., DL34 drive spindle, spring, cord, pulleys (Home Radio). Speaker, 7in. $\times 3 \frac{1}{2}$ in., $15 \Omega$. Telescopic aerial. Aerial socket, knobs, rubber feet.
to the pins of L2. The base lead B is extended by soldering on connecting wire, to run to C18. Connections in this stage should be reasonably short and direct. R3, C19 and C20 are wired to a tag under the paxolin, in contact with the metal frame of $\mathrm{VCl} / 2$.

VC3 is mounted directly under VCl/ 2 and is connected in parallel with it by short leads.
The bandswitch occupies the position shown in Fig. 4, and is wired as in Fig. 5. The switch has separate single-pole 9 -way wafers connected directly to VC1 and VC2 by short leads. No extra connection is made to position 1. Position 2 has the pair of capacitors C2 and Cl 0 ( 50 pF each). Position 3 has equal capacitors C 3 and Cll ( 100 pF each), and so on.
The capacitors are best arranged to lie partly over the wafers, in the manner giving shortest leads to a stout wire which returns to the frame tag of the ganged capacitor.

## GANGED CAPACITOR BAND SWITCH

S2/3 introduces fixed capacitor increments of 50 pF at each position. There is a certain amount of stray circuit capacitance, to which is added the
minimum capacitance of $\mathrm{VCl} / 2$. This means that a ganged capacitor having a maximum capacitance of 50 pF each section is not quite sufficient and results in small gaps in the tuning range.

A ganged capacitor with a capacitance swing of just over 50 pF (say from 10 pF to 70 pF ) would be ideal. To obtain a little overlap, and allow for variations of C2 to C17, the nearest standard value is 75 pF , which is satisfactory.

When this tuning arrangement was first used, a $2 \times 100 \mathrm{pF}$ capacitor was fitted and some plates pulled off, but this resulted in too many being removed. A new capacitor thus had to be fitted. Caution is therefore required, if a capacitor is modified in this way. With a 2 -gang 100 pF capacitor, the effective value can be reduced to about 75 pF by placing a 300 pF fixed capacitor (silver mica) in series with each section. The lead from L 1 to VCl must then run over VCl so that it can join the lead from S2.

## IF AMPLIFIER ASSEMBLY

This is assembled and wired on a paxolin panel $3^{3_{4}} \mathrm{in}^{2} \times{ }^{1}{ }^{3_{4} \mathrm{in} \text {. All components are mounted on one }}$ side and wiring is on the reverse, as in Fig. 6. Note that the different spacing of the pins of the i.f.t.'s enable these to be identified. Remember to drill holes for adjustment of the cores.

Small holes are drilled for the leads of the other components. Note the polarity of C21 and diode D1. Connections underneath are made by bending over the wires and snipping off the ends and by using thin connecting wire where required. Insulated sleeving is put on all leads where necessary. Two bolts holding the tags MC, locked on, will mount the finished amplifier and provide a positive return circuit.



Fig. 7. The i.f. and audio stages are mounted on a common panel.

Solder a lead to pin 2 of i.f.t.1. This is later soldered to pin 8 of the oscillator coil L2.
Take a black lead from R11, to use as negative. Solder a wire to the junction of R11 and C25, as shown, which will later run to R 4 . The remaining external connection is from R7, C26 and D1, and goes to the volume control VR1.
Both i.f. and a.f. amplifiers are mounted on a piece of paxolin $5^{1}{ }_{2} \mathrm{in}$. x ${ }^{2}{ }^{1}{ }_{2} \mathrm{in}$. which is supported by the bracket mentioned earlier, and by a further bracket bolted to the $10 \mathrm{in} . \mathrm{x} 4 \mathrm{in}$. aluminium plate. Extra nuts are put on the bolts holding the tags MC, Fig. 6. The bolts pass through the $5^{1}{ }_{2}$ in. $\times{ }^{2}{ }_{2}$ in. paxolin. Further tags are then put on fixed with nuts. The tags are wired to the volume control and metal plate (positive line).

The audio amplifier package is mounted in a similar way, Fig. 7. R12 is soldered to point C. A black lead for battery negative is taken to point D , and white leads for speaker connections to points D and E. A red lead from point A runs to the positive line at VR1 and the on-off switch.

## ALIGNMENT

The complete assembly on the 10in. x 4in. flanged plate is aligned and tested before fitting it in the cabinet. A speaker of the correct type ( 15 ohms) must be connected.

The five cores of the i.f.t.'s are rotated with a suitable tool, such as the Denco TT5, for best results. A weak signal is most suitable from a signal generator, or from a transmission, a short wire aerial being temporarily

Fig. 6. Layout and wiring diagram of the i.f. assembly built on a paxolin panel, 3 in $x$ 17\%.
connected to tag 8 of Ll. VR1 should be near maximum volume, but a strong signal should be avoided because the automatic gain control circuit will then make critical adjustment of the cores difficult.

Once the i.f.t. cores have been correctly peaked for best sensitivity, they should be left alone. A meter placed in one battery lead should show a current of under 15 mA with weak signals, rising to peaks of 50 mA or more with signals giving good volume.

The cores of L1 and L2 are then rotated until about ${ }_{8} \mathrm{in}$. of threaded brass projects. Set VC3 and TCl at about half capacitance. Open $\mathrm{VCl} / 2$, set the bandswitch at Position 1, and rotate TCl as necessary to tune to about 15 MHz .

Leave VC3 and TCl, switch to Position 9, and close $\mathrm{VCl} / 2$. Rotate the core of L 2 as necessary to tune to approximately $3 \cdot 6 \mathrm{MHz}$. Switch to Position 8 , tune in a transmission, and rotate the core of L1 for best results.

It should then be found that with the bandswitch in any position, and a transmission tuned in, VC3 can be peaked for best reception. Should VC3 need to be either fully open or fully closed with the switch in Positions 1 or 2, re-adjust TCl as required. If VC3 is either fully open or fully closed to give best results with the switch in positions near the low frequency end of the coverage provided (especially Position 8 or 9 ) then the core of Ll needs slight readjustment to avoid this.

It should be found that VC3 generally only needs one adjustment for each band and that often even this will not be necessary. VC3 can be peaked up for best reception of weak signals at any time, when changing the aerial, or switching Sl.

If it is found that almost uninterrupted whistles arise at the extreme h.f. end of the coverage provided, include a resistor at $X$ in Fig. 1, between collector and pin 9 of L2. Its value should be the lowest which prevents oscillation and will generally be around 47 ohms to 470 ohms or so. This depends qn the individual transistor and other factors.

## CABINET ASSEMBLY

Fig. 8 will help to clarify assembly of the case. Cut two pieces of hardboard 10 in . x 7 in . and with a pad saw or keyhole saw cut a hole to match the


A view inside the 'works' shows the three units forming the complete receiver.
speaker cone. Clean up all edges with glasspaper and wipe off any dust. Fabric is then stretched over the haraboard, brought round the edges, and glued on the inside.
The sides are 3 -ply, each $7^{1}$ in $x 4^{1}{ }_{2}$ in., sanded and varnished. The $10 \mathrm{in} \times 4 \mathrm{in}$. flanged plate forming the case bottom is placed on a flat surface, and the sides are positioned as in Fig. 8. Mark through the flange holes, drill the sides to match, and fix them with bolts.

Drill the hardboard front for speaker and front flange, and bolt this as in Fig. 8, with the speaker in position.

The receiver panel should then be finished. Cut a piece of plywood or other thin wood about 5 in . $x 2 \mathrm{in}$. and fix this with small screws through the 10 in x 4 in. plate, to bring the tuning scale about level with the drive cord. Clip a small piece of tinplate on the cord, and solder a straight wire pointer on this, so that it moves along the scale.

A piece of perspex is cut 10 in . $x 4 \mathrm{in}$., and drilled to match the four control spindles and for 6BA bolts in line with the four holes which are in the universal chassis flanged plate. A piece of coloured card is also cut this size, and a window about $51_{4} \mathrm{in} . \times{ }^{1{ }^{1}} 4 \mathrm{in}$. is cut in it with a sharp blade, to lie over the tuning scale.


Fig. 8. Detalls of the construction of the receiver cabinet.
Four lin. long 6BA bolts are put through the holes in the perspex and card. A washer and nut is put on each bolt, and the nuts are tightened. An extra nut is then put on each bolt, and the whole is fixed in place with further nuts behind the flanged plate. The nuts are adjusted to give about $l_{2}$ in. clearance, to take the drum, cord and pointer.

The assembly is then put in the top of the case, so that the flanged plate is about ${ }^{1}$ in. down, as in Fig. 8, and the perspex is flush with the case front. Drilling positions are then marked through the holes punched in the flanges. The sides are drilled, and the receiver bolted in place. The receiver case front is also bolted to the front flange of the $10 \mathrm{in} . \times 4 \mathrm{in}$. plate.




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THE power supply described uses the same feedback principles as in closed loop control systems and is capable of delivering 1 A at any voltage between 4 V and 20 V . A separate 45 V d.c. output is also available making the power supply particularly suitable for audio amplifier work where good regulation is required for the low voltage preamplifier stages and a higher d.c. supply required for the power output stage, generally of the order of 45 V , the regulation of this not being so critical.

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Variable current limiting from 0.2 A to 1 A is included making the power supply particularly suitable for development work and also giving it protection from short-circuit surges.

## Principle

The principle of negative feedback is used in systems where accurate control is required. The system could be a positional servo as used in rudder


TB20
Fig. 1 : Block diagram showlng function of slages in the power unit.
control of a model aircraft, speed control of an electric motor, temperature control of a blast furnace or cooker or as in this example, voltage stabilisation. In each case a sample is taken of the final output, a comparison made with some reference, then corrective adjustments made to reduce the error.

The block diagram of Fig. 1 illustrates the principle of voltage control where the controlling device is in series with the output current. The output is monitored by a sampler and the sample voltage compared to a reference voltage by a differential amplifier.

The differential amplifier amplifies the difference such as to starve the output stage of base current if the sample voltage is greater than the reference. As a transistor is basically a current amplifying device complete control of the output current can be achieved by controlling the base current of the current output transistor.

## Current Output Stage

Transistors are current amplifying devices and in general the more current they are capable of handling the less gain they have. A power transistor capable of passing 1 A can have a typical $\beta$ (current gain) of only 10 which would mean that the base current would still be rather high for the differential amplifier to handle, being in the region of 100 mA . The current output stage is simply a configuration of two transistors, $\operatorname{Tr} 3$ and Tr4, Fig. 2, to give high output current capability with high current gain.

## Constant Current Generator

The output current of this circuit, $\operatorname{Tr} 2$, is constant and sufficient to supply the maximum base current of the current output stage with a little extra for the differential amplifier.
The circuit uses the principle that as the baseemitter junction of a transistor is a forward biased diode then it will present a low voltage drop 0.7 V in the case of silicon transistors). The zener diode potential will therefore be applied almost completely across R6. The resulting current through R6:-

$$
\mathrm{I}=\left(\mathrm{V}_{\mathrm{z}}-0 \cdot 7\right) / \mathrm{R} 6
$$

will pass through the transistor without loading the zener diode.


Fig. दे : Circuit of power unit. The diodes D1-4 may be replaced by a single bridge rectifier unit.

Bias current for the zener diode will be supplied by R6. A constant current output of 4 mA was sufficient to supply the output stage and the differential amplifier.

## Differential Amplifier

The differential amplifier, Tr 1 and Tr , is coupled to the base current circuitry of the current output

stage. It takes current surplus to that required to maintain the correct amount of output current.

The amplifier amplifies the difference between its two inputs hence the term "differential amplifier." In this case it is used as a current control device.

## Reference Voltage

This is obtained from a zener diode, D5, an attempt being made to keep the diode current constant by connecting a capacitor across it. This is necessary as low wattage zener diodes have a high series internal resistance resulting in their output voltage varying with current.
The regulated output voltage of the power supply would normally be preferred to supply bias current to the zener but as this will be switched over wide ranges in this case, bias current has been supplied from the unregulated input through a $4 \cdot 7 \mathrm{k} \Omega$ resistor R 2 giving a bias current of 10 mA .

Fig. 3. Layout of unit constructed by the author. See Flg. 4: for details of the component board.

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| 1N1763s. | 44 p | АС163K | 24 p | BD135 | 38 p |
| 1N3754 | 20 p | AC176 | 16 p | H1136 | ${ }^{44} \mathrm{p}$ |
| 1N5399 | 21) | AC176K | 17 P | BDY20 | 92p |
| 1N5402 | 28p | $\mathrm{ACl}^{\text {cis }}$ | 17p | BFI15 | 23p |
| 1844 | 9 | ACY 17 | 31 p | BF167 | 18p |
| 18940 | 5 p | ACY18 | 19p | BFiT3 | 19 p |
| 2N696 | 17 p | ACY 19 | 23p | BF 177 | 25 p |
| $2 \mathrm{~N}^{697}$ | 18p | ACy20 | $\stackrel{0}{0}$ | BF194 | 145 |
| 2N706 | 12 p , | ACY21 | 21 p | BF195 | 154 |
| 2 N 930 | 29p | ACY22 | 211 | 13F254 | 14 p |
| EN1132 | 29p | ACY 39 | ${ }^{63 p}$ | ${ }^{352505}$ | 15 p |
| 2 N 1302 | 19p | ACE40 | 17 p | BFX29 | ${ }^{31 p}$ |
| 2N1303 | 1931 | ACY41 | 18p | HFX84 | 25 p |
| 2 N 1304 | 26p | ACY44 | ${ }^{31 p}$ | 13FX85 | 32 D |
| ${ }^{2} \mathrm{~N} 1305$ | 20 p | AD142 | 50 p | BFX87 | 291 |
| ${ }^{2} \times 1306$ | 33 p | AD149 | 58 p | BFX 88 | 2 pp |
| 2N1307 | 33p | AD150 | 50 p | Bry | ${ }^{239}$ |
| 2N1309 | 3 p | A 1 161 | 33 b | BFY51 | 20 p |
| ${ }^{2}$ 2 1813 | 23p | AD162 | 36 y | 3FY52 | 23p |
| 2N1711 | $22^{21}$ | AF114 | 24p | B8X20 | ${ }_{4}^{6 p}$ |
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| 2N2147 | 95 p | AF116 | 22 p | ${ }^{\text {BYY }}$ | ${ }_{380}^{18 p}$ |
| 2N2218 | 344 | AF117 | 23 p | BYX 38.300 | ${ }_{8}^{38 p}$ |
| 2 N 2218 A | 44 p | AF'18 | 8 P P | BY 38.300 |  |
| 2N2219 | 38 p | AF124 | 24. | ${ }^{\text {C40 }}{ }^{\text {a }}$ | 17 p |
| 2N2270 | 62 y | $\mathrm{AF}^{125}$ | 24 p | $\mathrm{C}_{762}$ | 19 p |
| 2 N 2369 A | 19p | AF126 | 22p | EA403 | 10p |
| $2 \mathrm{~N}^{2483}$ | 35 p | AF 127 | ${ }_{3}^{22}$ | E13383 | 10p |
| 2N2484 | 42p | AF139 | ${ }^{33 \mathrm{p}}$ | EC401 | 18p |
| 2 N 2646 | 47 p | AF239 | ${ }^{3671}$ | EC402 | ${ }^{178}$ |
| 2 N 2004 | 38p | A8Y26 | 27 p | NKT211 | ${ }^{25 p}$ |
| $2 \mathrm{~N}^{2905}$ | 44 p | AsY27 | ${ }^{367}$ | NKT21\% | ${ }^{25 p}$ |
| $2 \mathrm{~N} \cdot 2905 \mathrm{~A}$ | 47 p | AsY\%8 | 270 | NKT213 | 25 p |
| 2 N 2904 | 20 p | AsY'29 | 370 | NKT214 | 231 |
| 2 N 2925 | 22 p | AU111 | 974 | NkT217 | 50 p |
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| 2 N 3702 | 13p | bal0? | 25 p | NKT403 | ${ }_{650}{ }^{\text {P }}$ |
| ${ }_{2}{ }^{\text {N }} 3703$ | 13 p | BA130 | 22 p | ${ }^{\text {NKT }} 405$ | 79 p |
| $2 \mathrm{N3704}$ | 13 p | BA145 | 27p | NKTG13F | 30 p |
| 2 N 3705 | 131) | B4156 | 13 p | NK T674F | ${ }^{24 p}$ |
| 2N3706 | 13 p | ${ }^{8 B 103 / B}$ | 16 p | OA47 | 81 |
| 2 N 3708 | 10 D | BB103/4: | 161 | OA90 | 6 m |
| 2N3709 | 10 | BC108 | 11 p | OA91 | 5 p |
| 2 N 3710 | ${ }^{13} \mathrm{p}$ p | $\mathrm{BCl}_{1} 109$ | 12 p | 0495 | ${ }_{9} \mathrm{p}^{\text {p }}$ |
| $2 \mathrm{~N}^{3711}$ | 13. | ${ }^{\text {BC }} 122$ | 219 | Oa200 | 9 p |
| 2 N 379.4 | 15p. | BC125 | 159 | OA20:2 | 10p |
| 2N3819 | 23 p | $\mathrm{BCl}^{2} 26$ | ${ }^{221}$ | OC19 | 50 p |
| 2 N 3820 | ${ }^{53} \mathrm{p}$ | 1 Cl 10 | 30 p | ${ }^{\circ} \mathrm{C} 25$ | 42 p |
| 2 N 3904 | 35. | ${ }^{\text {BC1 }} 47$ | 10 p | $\mathrm{OC} 29^{\text {O }}$ | 76 B |
| - 2 N 4930 H | 350 | ${ }^{\mathrm{BCH}} \mathrm{BC148}$ | ${ }^{10 \mathrm{p}}$ | OC31 | 80 |
| 2N 403 H | $\mathrm{SFP}_{13 \mathrm{p}}$ | 13 C 153 | 19 p | OCl | 42 p |
| 2N 4059 | 10p | 8C169 | 1 p | OC44 | 42p |
| 2 N 40 fio | 11p | ${ }^{1} \mathrm{C} 178$ | $1 \pm 1$ | Orio | 219 |
| $2 \mathrm{~N}^{2} 061$ | $11 \mathbf{p}$ | 13 C 178 | 13p | Or'1 | 38 p |
| $2 \mathrm{~N}+124$ | 18p | $1 \mathrm{BC179}$ | 14 p | Oc75 | 4013 |
| 2 N 412 6 | 2 L | ${ }_{3 C 182}$ | 11 p | OC81 | ${ }^{25 p}$ |
| 2 N 4284 | $15 p$ | 13C183L | 10 p | OC81D | 25p |
| 2 N 4286 | 15p | BC1841. | 110 | OC83 | 255 |
| 2 N 4289 | 15p | BC189 | 42 y | $\mathrm{OCR}^{\text {P3 }}$ | $25 p$ |
| $2 \mathrm{~N}+291$ | 15 | BC2 2 L | 16 p | P346. | 20p |
| 2 N 4410 | 24 p | BC21314 | 1 hp | 82CN 1 | 10p |
| 2 N 499 | 621 | $\mathrm{BC} 214 .^{\text {d }}$ | ${ }^{16 p}$ | SD1 | 10 p |
| 2N5062 | 61. | 3C257 |  | $\mathrm{SO}_{4}$ | 12p |
| 2 N 5457 | 49 p | 13C259 | 9 | $\checkmark 763$ | 88. |
| 2N5459 | 49 p | ${ }_{11 \mathrm{C} 287}$ | 17 p | W106bi | 45 p |
| 40250 | 71. | ${ }^{\text {BC2288 }}$ | 15 p | W02 | 40 p |
| 40351 | 89, | BC269 | 17 p | W1.02 | 95 p |
| 40361 | 55 p | BC300 | ${ }^{49 \mathrm{p}}$ | ZTX 300 | 14 p |
| 40362 | ${ }^{68 p}$ | 1 C 301 | ${ }^{37} \mathrm{p}$ | ZTX301 | 169 |
| 400:02 | 52 p | ${ }^{13 C 303}$ | 60 p | 7TK302 | 22 J |
| AC107 | 46 p | BCY30 | ${ }^{60 \mathrm{p}}$ | zTX 303 | 22 p |
| AC126 | 20p | ncy 31 |  | zTX304 | 270 |
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## Output Sampler

The resistor chain is strapped across the output voltage and the tapping point will always be at $3 \cdot 9 \mathrm{~V}$. There are three separate resistor chains in order to reduce the sensitivity of VR1.

It is worth mentioning that the output of this power supply can never be less than the reference voltage generated by D5. If 3.9 V is not low enough then a $2 \cdot 7 \mathrm{~V}$ zener may be used for D5 and if necessary, the sampling chain recalculated.

## Construction

Not much information need be given on the construction of this unit since much will depend upon the dimensions of the components used. Fig. 4 shows the layout of the component board and the interconnections with the remaining components.

Fig. 3 illustrates the general layout of the power unit as built by the author. Note that the transistor case of Tr3 forms the collector connection and must be insulated from the heat sink with the mica insulation kit generally supplied with the transistor. Check after assembling the transistor and heat sink that there is no conducting path between the transistor case and the heat sink.

The heat sink used here is made from aluminium sheet $4^{1}{ }_{2} \times 2^{3}{ }_{4} \mathrm{in}$. bolted to the main chassis.

It is worth adding that where wire-wound resistors are used there is always a tendency for oscillation to occur. These resistors, from the nature of their construction, are slightly inductive. Often this effect can

## * components list



## Semiconductors

Tr1 2N706 or BC107, 2N930 or 2N2484
Tr2 2N3250 or BCY30, 31, 32 or 2N3250
Tr3 2N3055 or BDY 38, with insulating washer etc.
Tr4 BFY50 or $2 \mathrm{~N} 1711,1613$ or BFY51
Tr5 2N706 or BC107, 2N930 or 2N2484
$\begin{array}{llll}\text { D1 } & \text { 1N645 } & \text { D4 } & \text { 1N645 } \\ \text { D2 } & \text { 1N645 } & \text { D5 } & \text { ZF3.9 }(400 \mathrm{~mW}) \\ \text { D3 } & \text { 1N645 } & \text { D6 } & \text { FF4.7 }(400 \mathrm{~mW})\end{array}$
Miscellaneous
Transformer 30V 2A (Type MT3AT). S1, 2 pole way toggle switch. S2, 4 pole 3 way, make before break wafer switch, used as 2 por equivalent: some equivalents have built-in resistor -if so delete R18. Fuse holder with 1 A fuse. Vevoboard, plain, $3 \frac{1}{2} \times 3 \frac{1}{2} \mathrm{in}$., 0.1 in . matrix. Aluminium $2 \frac{3}{3} \mathrm{in}$. Voltmeter 20 V , ammeter 1 A , if required.


Fig. 4 : Layout of component board.
be corrected by the addition of a small capacitor of 20 to 100 pF coupled across the resistor to tune out the effect of the inductance.

## TELEVISION

## DECEMBER ISSUE

## A CLOSER LOOK AT PAL

The basic principles of the PAL system are now generally understood. There is however a good deal more than meets the eye to the system. So this month we are starting a new series in which we shall be investigating the system in greater detail than previously. The account will be descriptive, not a fog of formulae!

## CONSTRUCTORS' CIRCUITS

This month we turn to the line timebase. A choice of transistor or valve line oscillator circuits, both with flywheel synchronisation, and a line output stage with optional stabilisation and optional solid-state e.h.t. and boost rectifier circuits is given.

## THE TELDEC SYSTEM

With the first demonstration of the Teldec system in colour at the recent international Berlin Radio Exhibition this remarkable disc videorecording system is again in the news. A full account of the mechanics of the system.

## RUSSIAN TV RECEIVERS

There are many novel and unusual features in the Temp single-standard receivers manufactured in the USSR and now being widely distributed in the UK. For example, an external definition control varies the vision i.f. response by means of a varicap diode, the line blocking oscillator transformer has an adjustable feed-in point for optimum a.f.c., automatic brightness control is incorporated in the video output stage and amplified negative feedback is used in the field output stage. We are taking a detailed look at this interesting chassis.
plus all the regular features

deliberate effort has to be made to roll-off this response to avoid r.f. pickup in the high gain amplifier and also to prevent the bias oscillator signal from being a problem.

It should be pointed out that this circuit is only suitable for the Marriott XRP18 or XRP36 record playback heads and the XESll erase head. The amplifier will play back from other heads but, on record, other heads need much higher bias voltages than this circuit will produce.
All the transistors specified are common types and inexpensive and the total cost of the semiconductors is unlikely to be more than about $£ 1 \cdot 50$ including the output pair.
The circuit is very largely based on one published by Mullard's and no originality is claimed. There are however certain differences incorporated for various reasons.
The switching necessary in a tape recorder circuit tends to make the understanding of the circuit difficult and so Fig. 1 shows the effective circuit on playback. Fig. 2 shows it in on record. The component numbers are shown and if the values given in the main circuit are used these will work perfectly well by themselves without switching if for instance only a tape playback amplifier is needed.

## PLAYBACK

From Fig. 1 it will be seen that Tr 1 and Tr 2 are coupled as a pretty conventional preamplifier to boost the signal from the tape head. R7, the emitter resistor of $\operatorname{Tr} 2$, is not decoupled, this provides a measure of feedback to the whole stage as the bias

# Transistor TAPE RECO RDER W. LANGLEY 

In January we published full details for a stereo tape recorder and at the time we promised an article describing a mono version. The amplifier described here can be used with any type of tape deck, though the tape heads specified must be used.

THE design of a transistor tape recorder has its own special problems. High gain is necessary since the output from a tape head on playback is very low but at the other end, in the circuits feeding the loudspeaker, high currents are passed and it is vital to ensure that earth loops do not create instability. Readers who wish to build this circuit should not deviate from the general layout unless they are absolutely certain that they know exactly what they are doing.

The problems of earth loops are not helped by the necessity for including fairly complex switching to alter the function of the amplifier from record to playback. An early prototype of this project was violently unstable due to the voltage drop in only a 2 in . length of wire; this may give some indication of how important careful layout is.

Care has also to be taken in another field. Modern transistors of the type used here have frequency responses reaching to several Megahertz and a
to Tr 1 is taken from the emitter of $\operatorname{Tr} 2$ via R 5 . This feedback improves the stability of the amplifier. C , a low value capacitor, has little effect at audio frequencies but effectively cuts out the r.f. signals, which may have been picked up, from later stages. Tone control is achieved by coupling feedback from Tr2 collector to Trl emitter via C6 and VR2. To


Fig. 1: The effective circuit on playback.
ensure quiet and stable operation, the supply to Tri collector must be adequately decoupled, this being achieved through R6 and C2.

After the volume control, the output is fed to a fairly conventional transformerless complementary pair output stage. It is d.c. coupled throughout with a variety of feedback and stability circuits. Conventional connections would take the junction of C10-R15 to the junction of R24 and R25 instead of the base of Tr6; the reason for deviating from this will become apparent from the record stage.

TH1, a VA1077 32s thermistor, holds the bases of the output pair close together, as far as potential is concerned, while the trimmer VR3 linearises the operation and sets the output current. R10 applies a degree of negative feedback to the first part of the output stage.

## RECORD

On record the input to Tr is connected to the input sockets, the first of which is unattenuated, the second which is severely attenuated for inputs of up to 2 V . The input impedance of both is fairly high, about $100 \mathrm{k} \Omega$.

The preamplifier and the first two stages of the main amplifier operate identically except that the tone control is disconnected and the volume control becomes the record level control. TH1 and VR3 are included but in fact their low value means that they can be ignored in the record position; R16 goes directly to chassis and acts as the collector load. Output to the tape head is taken from the collector of $\operatorname{Tr} 4$ (effective) via C11, C12 and R21. The VU meter is connected via R22, the actual value of which should be selected later.
In the record mode, transistors $\operatorname{Tr} 5$ and $\operatorname{Tr} 6$ are coupled as an oscillator with the erase head, the potential divider chain R17, R18, R19 and R20 providing the correct bias voltages. This arrangement


Fig. 2: The effective circuit on record.
gives a high voltage swing across the erase head. The a.c. bias necessary for correct operation is applied to the record head via C16.

## SWITCHING

To alter the function of the amplifier from record to playback an eight-pole, two-way switch is needed. The various functions can be studied in the complete circuit diagram shown in Fig. 3. The VU meter is only operational on record and serves as a level indicator.

The type of switch used is not important but may be hard to obtain. That used in the prototype is made up from "Make-a-Switch" parts with two six-pole, two-way wafers.

## EQUALISATION

For the best signal-to-noise ratio, on record, treble boost should be applied to the signal and on playback, bass boost should be applied. In fact these tend to be self-cancelling if a slightly worse signal-to-noise ratio can be accepted (and it is only very slight with


Fig. 3: The compiete circuit. SW1 is shown in the record position. The connections for Tr5 and Tr6 are shown in Fig. 6.
modern tape). The author has a number of professionally recorded tapes and recordings, made without equalisation using this amplifier, were hardly different from these. On playback the tone control gives a wide control over the frequency response and this compensates somewhat for the lack of equalisation.

## HEAD SWITCHING

The tape heads specified are both four-track and it is of course necessary to switch from one to the other. This is simply accomplished by fitting a slide switch near the heads, the siting will depend on the

## components list




Fig. 4 : Details of the melalwork.
deck used. Alternatively, this switch could be incorporated on the main chassis.

## CONSTRUCTION

A very simple chassis arrangement is used for the amplifier, the dimensions are shown in Fig. 4. The input sockets and loudspeaker socket are at one end with the VU meter at the other; the function switch, the volume control and the tone control lie in between. The majority of the components are mounted on a piece of Veroboard $5 \mathrm{in} . \times 2^{1}{ }_{2} \mathrm{in}$. (a standard size). Four holes are drilled in this for later mounting to the chassis.
The power transistors, AD161 and AD162, need to be heat-sunk and these are fitted at one end of the Veroboard near the switch. A small tag-strip holds the large capacitor C 17 and acts as an anchoring point for the output pair emitter resistors, R24 and R25. R1 and R2 are mounted directly on the input sockets.

Building the Veroboard panel should be straightforward, the layout is shown in Fig. 5. The necessary connections to the board are made with Veropins at


Fig. 5: The main component layout on Veroboard.


|  | 1-11 12-24 |  |  | 1-11 12-24 |  |  | 1-11 12-84 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| gN7400 | 0.20 | ${ }_{0}^{2.18}$ | SN7433 | 0.80 | 0.75 | SN7472 | 0.82 | 0.80 |
| GN7401 | 0.20 | 0.18 | sN7437 | 0.64 | 0-06 | SN7473 | 0.48 | 0.41 |
| SN7402 | 0.20 | 0.18 | gN7438 | 0.64 | 0.60 | 8N7474 | 0.48 | 0.41 |
| SN7403 | 0.20 | 0.18 | SN7440 | $0 \cdot 28$ | 0.21 | 8N7475 | 0.45 | 0.44 |
| SN7405 | 0.20 | 0.18 | SN7441AN | 0.87 | 0.83 | 8N7476 |  |  |
| 8N7406 | 0.80 | 0.75 | 8N7442 | 0.85 | 0.81 | 8N7480 | 0.70 | 0.66 |
| SN7407 | 0-20 | 0.18 | SN7443 | 2.88 | 2.70 | 8N7481 | ${ }^{1.40}$ |  |
| gN7408 | 0.20 | 0.18 | SN7444 | 2.86 | 8.70 | 8N7482 | ${ }_{0}^{0.87}$ | 0.82 |
| SN7409 | 0.20 | 0.18 | 8N7445 | 8.50 | $2 \cdot 40$ |  |  |  |
| SN7410 | 0.20 | 0.18 | SN7446 | 1.00 | 0.95 0.95 | SN7484 | ${ }_{8.68}^{2.60}$ | 40 |
| 8N7411 | 0.48 | ${ }_{0}^{0.48}$ | 8N\% 448 | 1.00 | 0.95 | 8N7486 | 0.88 | 0.80 |
| SN7413 | $0 \cdot 40$ | 0.88 | SN7449 | 1.00 | 0.95 | 8N7490 | 0.87 | 0.84 |
| SN7420 | 0.20 | 0.18 | SN7450 | 0.20 | 0.18 | SN7491AN | 1.21 | 4 |
| 8N7423 | 0.51 | 0.47 | SN7451 | 0.20 | 0.18 | 8N7492 | ${ }_{0}^{0.87}$ | 84 |
| SN7427 | 0.48 | 0.45 | 8N7453 | 0.20 | 0.18 | 8N7493 | 0.87 0.87 |  |
| ${ }^{\text {SNF7428 }}$ | 0.80 0.83 | 0.75 0.15 | SN7454 SN7460 | 0.20 0.20 | 0.18 0.18 | -8N7494 | 0.87 0.87 |  |
| $8 \mathrm{SN7432}$ | 0.48 | 0.42 | -1740 | 0.40 | 0.38 | SN7496 | 0.87 | 0.84 |

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Yalues: $(\mu \mathrm{F} / \mathrm{V}):$ : $0.64 / 64 ; 1 / 40 ; 1 \cdot 6 / 25 ; ~ 2.5 / 16 ; 2.5 / 64 ; 4 / 10 ; 4 / 40 ; 1 / 64 ;$ 6.4/6.4: ( $4 \mathrm{~F} / \mathrm{V}$ ): $0 \cdot 64 / 64$; $1 / 40$ : $10 / 64$; $12 \cdot 5 / 25$; $16 / 40$; $20 / 16$; 20/64; $25 / 6 \cdot 4$; $\begin{aligned} & 25 / 25 ; 32 / 10 ; ~ \\ & 80 / 16 ; 30 / 25 ; 100 / 6 \cdot 4 ; 125 / 10 ; 126 / 16: 20 / 6 \cdot 4 ; 200 / 10 ; 320 / 6.4 .\end{aligned}$

## SILICON RECTIFIERS

| PIV | 50 | 1002 | 00 | 400 | 600 | 800 | 1000 | 1200 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 A | 10 p | 121p | 15p | 16p | 171p | 19p | 209 |  |
| 3A | 15p |  |  | 221p |  | 80 p |  |  |
| 6A |  |  | 5 p | 80 p | $82 \pm p$ | 850 |  |  |
| 10A |  | 52¢p 5 | 3718 | 65p | 7719 | $88 \pm p$ | 9710 81.80 | $\begin{aligned} & \text { 韹 } 1.2572 \end{aligned}$ |
| 17A |  | $57 \%$ 6 | 3210 | 771p | ${ }^{90}$ | $9715$ $\text { 害 } 1 \cdot 50$ | $\begin{gathered} 81 \cdot 20 \\ \hline 98-60 \end{gathered}$ | 31.67 |
| 35A |  | 80 p | 90 p | 31-00 | 21.25 | E1.50 |  |  |
| 1 amp and 8 amp are plastic encspsulation. |  |  |  |  |  |  |  |  |
| DIODES \& RECTIFIERS |  |  |  |  |  |  |  |  |
| IN34A | 10p | AA119 | 10 p |  | BAX16 | 12tp | BYZ13 | ${ }_{\text {20]p }}$ |
| IN914 | 07 p | AA129 | 10 p |  | BAY18 | 17\% ${ }^{7}$ | FST3/4 |  |
| IN916 | 0710 | AAZ13 | 100 |  | BAY31 | ${ }^{0710}$ | OA5 | 1710 |
| IN 4007 | 22jp | AA7,15 | 121p |  | BAY38 | $25 p$ | OA10 |  |
| I844 | 10 p | AAZ17 | 12tp |  | BY100 | 17\%p | OA9 | 107 |
| IS113 | 15 p | BA100 | $15 p$ |  | BY103 | $221 p$ | OA47 | 078 |
| 18120 | $15 p$ | BA102 | ${ }^{29}+p$ |  | BY122 | 4740 | OA70 | 07 p |
| 18121 | 171p | 13A110 | 321p |  | BY124 | ${ }^{16 p}$ | OA73 | 109 |
| 18130 | 12+p | BA114 | Rels |  | BY126 | 18 p | OA79 | 09 p |
| 18131 | 121p | BA115 | 07¢D |  | BY127 | 1718 | OA81 | 078 |
| 18132 | 15p | BA141 | $881 p$ |  | BY164 | ${ }^{5718}$ | OA | 07 |
| 18920 | 071P | BA142 | 8819 |  | BYX 10 | 22\%p | OA90 | 07 D |
| 18922 | 07 07p | BA144 | 1810 |  | BYZ10 | 88 p | OA95 | 07 |
| 18923 | 071p | BA145 | 20 p |  | BYZ11 | $32+\mathrm{p}$ | OA9200 | 10 p |
| 18940 | 07 f | BA154 BAX13 | $\begin{aligned} & 121 p \\ & 12 ? \mathrm{p} \end{aligned}$ |  | BYZ12 | 30 p | OA202 | 10p |


| TRIACS |  |  |  |
| :---: | :---: | :---: | :---: |
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| 8 C 36 D | 21.00 | 40430 | 97 p |
| SC40D | 81.50 | 40486 | ${ }^{985}$ |
| SC41D | 21.20 | 40528 | $72 \pm \mathrm{p}$ |
| SC45D | 21-62 ${ }^{\text {2 }}$ | 40430 | 21.30 |
| $8{ }^{\text {84 }} 46 \mathrm{D}$ | 21.42\% | 40432 | 81.87k |
| 8C30D | \$2.05 | 40512 | 81-45 |

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821p. For 80.1, 8\& TO-18, 5p
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W $2 \%$ M/O 4 p .


BRIDGE RECTIFIERS

| A. PIV |  | A. PIV |  |
| :---: | :---: | :---: | :---: |
| 1100 | 471 | 450 | 80 p |
| 1.4140 | 52 p | 4100 | 70p |
| 250 | 85p | 4400 | 95 |
| 2200 | 70p | ${ }_{6} 6200$ | 871 |
| - 400 | 80p | 4400 | 21-12 |

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The Veroboard panel-compare this with Fig. 5.
both ends of the board and much work will be saved later if these are fitted at the same time as the main components and soldered in.
. There are a number of breaks in the copper conducting strip and these are shown clearly on the diagram.

There is a reasonable amount of room on the board but care should be taken to ensure that extra large components are not selected. The ${ }^{1} \mathrm{BW}$ resistors specified will fit neatly as shown. The skeleton preset VR3 will also fit neatly into $0 \cdot 15 \mathrm{in}$. matrix Veroboard if fitted at an angle as shown.

Naturally the output transistors have to be

fig. 7: The record!playback switch wiring.
insulated from the chassis and this applies to $\operatorname{Tr} 6$ as well, even though the collector is at chassis potential. It is this sort of thing that can cause earth loop problems.

One connection on the small tag strip is the common earthing point and all wires which carry any appreciable current are earthed directly to this. A second earthing point is on the input DIN sockets but as these wires are taking no current to speak of, no problem arises. When finally connected to the tape deck, be sure that the metal body of the deck is connected to the main earthing point of the amplifier. Certain wires need to be screened, these are indicated on the diagrams.

The switch wiring is shown in Fig. 7. A logical sequency in wiring this up is essential. It is easier to mount the completed Veroboard panel and the other components to the chassis and then proceed with the wiring. A heavy gauge piece of copper wire can be mounted alongside the switch to act as an earth bus bar, this being connected to the common earth point. If the tape deck used has incorporated switch wafers these could be used but this entails a lot of additional wire and could result in instability.


The power supply should be built separately and fixed some distance both from the main amplifier and the tape heads to avoid hum induction. The circuit for a suitable power supply is shown in Fig. 8.
There are only two items that need to be set up. One is VR3; for this a meter should be inserted in the emitter leads of one of the output pair and the quiescent current should be adjusted, using VR3, to read about 20 mA . The value of the resistor feeding the VU meter has to be found by trial and error. In use the correct recording level can be found simply by listening for high level distortion caused by over modulation of the tape. When the correct level has been found, the resistor R 22 should be selected to read zero level on peaks.

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# CDMPREHENSME~ MULTI-BANDN~M  PART 2 

## RF AMPLIFIER

The circuit for this stage is shown in Fig. 5. The 6BA6 is to the right of the ganged capacitor, Fig. 3, and Ll is to the left, near the panel. In Fig. $5, \mathrm{Ll}$ is a "Blue" coil, and L2 the existing mixer "Yellow" coil.
Leads run from VC6 and VC7 through the chassis as in Fig. 3. The aerial trimmer VC8 is fixed to the panel in the position shown in Fig. 4, near the holder for L1. Arrange the valve and coil holders to allow short leads, with separation of grid and anode circuits, and earth the central spigot of the valveholder to the chassis.

The primary of L2 was originally earthed. Pin 8 is now disconnected from the chassis and wired to Cl , Fig. 4, shown as C4 in the r.f. stage circuit Fig. 5. Pin 9 is disconnected from the aerial socket and connected to pin 5, V1, Fig. 5.

A piece of co-axial cable is now used for the aerial circuit. Its inner conductor runs from the aerial socket to pin 8 of Ll . The outer conductor is connected to the earth socket, chassis, and also to the chassis near Ll.
Add the r.f. gain control in the position shown, and disconnect R7 of the i.f. amplifier from the chassis, wiring it to VR1 and R4, Fig. 5.

## RF AMPLIFIER ALIGNMENT

Insert a set of three coils. VC8 should peak quite sharply near the h.f. end of each band, unless the aerial is very long. Adjust the core of L1, in the way already described for L2, so that little or no adjustment of VC8 is required near the l.f. end of the band.
There is no loss of efficiency if VC8 and VC3 can
both be used to peak up signals throughout each band, and are not fully open or fully closed. But correct adjustment of the cores will make it unnecessary to adjust these trimmers frequently, except to peak up weak signals, or when changing the aerial or coils.
When dealing with the highest frequency range, note that it is possible to tune Ll or L 2 to the wrong side of the oscillator frequency, at the h.f. end of the band. This effect is possible when trimming any circuit of this type, with an i.f. near 465 kHz . Ll and L2 should be tuned 1.f. of the oscillator frequency, and the second channel, or unwanted response, will be about 930 kHz h.f. of this, and will be found as a weaker signal, if a generator is used for alignment.

On the lower frequencies it is not possible to set L 1 or L2 to the wrong side of the oscillator frequency.

## CARRIER OSCILLATOR/PRODUCT DETECTOR

Fig. 6 shows the circuit of these sections. The product detector Vl occupies the position near the last i.f.t. as in Fig. 3. The carrier oscillator is constructed completely in the box which is later bolted to the left of the chassis, Fig. 3. It is possible to use the carrier oscillator for the reception of both c.w. and s.s.b. using the diode detector Dl but reception is much improved by switching it out and bringing in the product detector V1.
The 3-way rotary switch controls operation of the receiver. Section Sl allows the diode detector D1 to supply signals for a.m. reception, or switches to C5 for s.s.b., c.w. and "Calibrate." Section Slb applies h.t. to both stages in the s.s.b./c.w. and "Calibrate" positions.

A $7 \times 2$ in "universal chassis" flanged side is taken and its flanges cut away 2 in from each end. It is then given right-angle bends 2 in from each end, to make an open box 2 in high, 3 in wide, and 2 in deep. A plate $3 \times 2$ in is cut and bolted to the front flanges.

The valveholder and CO coil are located as in Fig. 3, and all components in the box in Fig. 6 are assembled and wired, with tag strips to anchor h.t. circuits and other

Fig. 5: Circult of the r.f. amplifier, to give increased sensilivily.

components. A blue lead is run out from pin 4 for heater, a yellow lead from tag 1 for $C 6$, and a red lead from C7 for h.t. circuits.

A back plate $3 \times 2$ in with a ${ }_{2}$ in flange to bolt to the chassis is bent up, or cut from a spare 3 in wide "universal chassis" member. It is drilled so that it can be attached to the back of the CO box with four self-tapping screws into the flanges of the latter.

The CO box is placed so that the bush and spindle of VCl , Fig. 6, project through a clearance hole in the receiver panel. It is fixed here by two bolts through the lower flanges of the box and chassis. The back plate described is then screwed on from behind, and is bolted to the receiver chassis.

When VCl is half closed the knob pointer or mark should be vertical.

The function switch is put in the position shown, and h.t. and heater circuits connected.
Most of the small components for the product detector are supported by the valveholder pins. and an adacent tag strip. The lead from C5 to Sl runs


This photograph of the underneath of the receiver can be compared with Fig. 4 (Part 1).

Fig. 6: Circult of the carrier osciivator and product detector to permit reception of s.s.b. and c.w. signais. against the chassis. Keep grid circuits away from leads carrying heater current.

After connecting Cl realign the last i.f.t. in the way explained. Tune in any transmission, with the switch at the "AM" position and place VCl in the central position, as mentioned earlier.

Switch to SSB/CW and rotate the core of the CO coil until a strong heterodyne is produced. This is an audio tone which falls in frequency as the correct core position is reached. Passing this position results in the tone beginning again and rising in frequency. The correct core setting is the central, zero beat setting. An audio tone which rises in pitch can then be produced by rotating VC1 either way.

When receiving s.s.b. the carrier oscillator has to replace the suppressed carrier, being adjusted slightly one way or the other, as necessary by VC1. The sideband normally employed depends on the amateur band in use, but the adjustment of VCl will soon become clear.

For c.w. reception, use VCl to obtain the most suitable pitch, placing the CO either above or below the c.w. as found to give least interference.

## CRYSTAL FILTER

This incorporates an extra stage of i.f. amplification, 3-position selectivity switch, and variable phasing control using the circuit in Fig. 7. It provides


Fig. 7: For increased gain and selectivity this crystal filter unit can be fitted.

## components list

```
RFSTAGE:-
    R1 1MS ! W R R = 100k\Omega iW R5 150k\Omega 1W W
    R2 47kS2 IW R4 68S2 &W All 10% tolerance
```

VR. 10 kS wire wolnd potentiometer, linear.
C1 100 pF SM
C3 $0.1, \mathrm{~F}$
C2 $0.02 \mu \mathrm{~F}$ disc
C4 (C1, Fig. 4)

VC6 Front sectiono bandset capacitor
$\vee C 7$ Front section of bandspread capacitor
VC8 50 pF va-iable
$L 1$ From bas c recaiver (L2)
L2 Miniature plug-in coils (Denco 'Yellow' Ranges 2. 3, 4 ane 5)

## Miscelianeous:

V1, SBA6. Valvelolders B7G (1) with screen, B9A (1).

## CARRIER OSC/P.DETECTOR:

| R | 100kS 1 W | R4 | $22 \mathrm{k} \Omega+\mathrm{W}$ | R7 | 47k』 iW |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R | B20: 2 in | R5 | 33ks2 IW | R8 | $47 \mathrm{kS}+\mathrm{W}$ |
| R3 | 47ko iw | R6 | 100ks $+\frac{\mathrm{W}}{}$ | R9 | $47 \mathrm{k} \Omega+W$ |


| C1 | 56 pF SM | C6 47 pF SM |  |
| :--- | :--- | :--- | :--- |
| C2 | $4 \mu$ F $350 . /$ | C7 | $0.25 \mu$ F 350 V |
| C3 | 470 pF | C8 $100 \mu \mathrm{~F}$ SM |  |
| C4 | 470 pF | C9 100 pF SM |  |
| C5 2000 pF | C10 140 pF SM |  |  |

$\vee \mathrm{C} 1 \quad 15 \mathrm{pF}$ variable
$\begin{array}{ll}V_{1} & 12 A U 7\end{array}$
$\mathrm{V} 2 \quad 6 \mathrm{C} 4$

## Miscellaneols

Valveholders, B9.A :1), B7G (1) with screen. S1a/b/c 3 pole 3 way wafe switch (S1c is for crystal marker). Universal chass s flanged members $7 \times 2$ in (1) $4 \times \operatorname{3in}$ (Home Rasio). L1, BFO2/465 (Denco).

CRVSTAL FILTER:

| $R 1$ | $2.7 \mathrm{k} \Omega$ | W | $R 3$ | $68 \mathrm{k} \Omega$ | $\frac{1}{2} \mathrm{~W}$ | $R 5$ | $68 \Omega$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| F 2 | $100 \mathrm{k} \Omega$ | W | $R 4$ | $47 \mathrm{k} \Omega$ | $\frac{1}{2} \mathrm{~W}$ |  |  |
| C1 | $0.02 \mu \mathrm{~F}$ | C 2 | $0.05 \mu \mathrm{~F}$ | C3 | $0.02 \mu \mathrm{~F}$ |  |  |
| VC1 | 25 pF varlable |  |  |  |  |  |  |

## Miscellaneans:

V1, 6BA6. Crys al, 465 kHz (see text). IFT, IFT11/ 465/CT (Dencol, S1, 1 pole 3 way wafer switch. Valveholder 875 and screen. Bushes (2) DL52C, couplings 12) DL60, $\frac{1}{2}$ in dia. polystyrene rod (Denco). Universal zhassis side $7 \times 2$ in (1), $4 \times 3$ in (1) (Home Radio).

## CRYSTAL MARKER:

| R1 | $470 \mathrm{k} \Omega$ i W | R3 | $100 \mathrm{k} \Omega$ |
| :--- | :--- | :--- | :--- |
| R2 | $10 \mathrm{k} \Omega+\mathrm{W}$ | W | R4 |
|  | $22 \mathrm{k} \Omega$ | $\frac{1}{2} \mathrm{~W}$ |  |
| C1 | 220 pF SM | C3 | $0.02 \mu \mathrm{~F}$ disc |
| C2 | $0.02 \mu \mathrm{~F}$ disc | C4 | 100 pF SM |

VC1 100 F veriable

## Miscellantous :

Crystal, 1 MH . Valve, EF91. Valveholder, B7G. Universal châssis side $4 \times 3$ in (Home Radio). Crystal holder.
additional gain, and a very great increase in selectivity.

The i.f.t. has a centre-tapped secondary, and VCl can be adjusted to balance stray capacitance in the crystal and wiring, or to give a rejection notch either side of the crystal frequency. With the switch in position 1, the crystal is out of circuit, and selectivity is that provided by the three i.f.t.'s. With position 2, the crystal is in use working into the relatively high impedance of R3. For position 3, the crystal provides maximum selectivity. Position 1 is suitable for general reception and position 2 is used for other signals except when severe interference from adjacent transmissions is troublesome.

A $3 \times 2 \times 2$ in box is made in the same way as described for the carrier oscillator. The circuit in Fig. 7 is built entirely in this box, which is then bolted to the chassis, and closed by a plate fixed to the back with self-tapping screws.

The i.f. transformer is situated above a hole in the main chassis, so that its lower core can be adjusted.

VC1 must be insulated from the front of the box, and it is also mounted so as to avoid unnecessary

stray capacitance to the metal. This was done by punching a lin hole in the box and bolting a rim strip of paxolin across inside, with a hole to take the capacitor bush. The spindle is extended by using a small coupling and length of ${ }_{4}$ in diameter insulated rod, which runs through a bush at the panel.
The 3 -way switch is situated immediately under the box, on a chassis bracket and an extension spindle is also fitted.

The exact frequency of the crystal is not too important, provided it falls near the frequency of the i.f.t.'s ( 465 kHz ). A 464 kHz surplus crystal was used and a 455 kHz crystal, available as a spare for a wellknown communications receiver, also tried. No difficulty arose in adjusting the i.f.t.'s to 455 kHz .

A wire-ended crystal can be supported between pin 4 and VC1. Other crystals may need fixing to an insulated strip or bracket.

Coloured leads pass down through the chassis to identify heater and other circuits. R2 runs to the common a.g.c. line, R5 is connected to the r.f. gain control, which now adjusts the bias of all i.f. stages.

RF leakage round the filter will degrade the very high selectivity so the lead from the f.c. anode to i.f.t. primary is screened from the valveholder right up to the pin of the i.f.t. The anode lead of V1, Fig. 7 , is similarly screened.

## ALIGNMENT WITH FILTER

Alignment should be checked with a meter, such as used earlier when adjusting the i.f.t. cores. A multi-range meter clipped in to read cathode current of one of the stages receiving a.g.c. is suitable, adjustments being directed towards securing minimum current.

Set the phasing control about half open and the selectivity switch at 1 . Tune in a strong transmission. Switch to position 2 and tune slowly across the signal, observing the tuning meter. There will probably be one normal response on the meter, observed as a steady rise and fall while tuning through the signal. A second response should be found, very much sharper, and probably giving only a small dip on the meter. This is the crystal frequency. Leave the tuning at this frequency, and adjust all the i.f.t. cores for best results (lowest meter reading). Switching from 1 to 2 and tuning should show that the i.f.t.'s are now virtually on the crystal frequency.

The phasing control is now adjusted slowly to find the exact point where selectivity is greatest and the


Fig. 8: As a finishing touch this 1 MHz crystal marker will provide calibration points throughout the range of the receiver.
response peak (or meter movement) approximately symmetrical a each side of the signal. Repeat this with the switch at 3 , and adjust all the i.f.t. cores slightly, if necessary, with a signal tuned in precisely. Adjust the pointer of the phasing control so that it is vertical without moving the control itself.

With the switch at 2 or 3 , slight adjustments of VCl one way or the other will produce a rejection notch which can be moved across the i.f. passband. This should be found to eliminate any interfering signal which is so near the wanted signal that it produces a heterodyne.

## CRYSTAL MARKER

Fig. 8 is the circuit of the harmonic marker, which provides crystal-controlled "pips" from 1 MHz to 30 MHz . TCl allows a slight shift in crystal frequency, so that the unit can be set to zero beat with MSF on 5 MHz . HT is applied to the EF91 only when the function switch is in the "Calibrate" position.

The marker is assembled on a sub-chassis which
is $1^{3}{ }_{4} \mathrm{in}$. high, 4 in . wide, and $1^{1}{ }_{4} \mathrm{in}$. deep made from a single "universal chassis" member $4 \times 3$ in cut to leave two pieces, one $4 \times 1^{3} 4 \mathrm{in}$ and the other $4 \times 1^{1}{ }_{4}$ in. The flange of the smaller piece is bolted to the straight edge of the larger piece, which can later be attached to the chassis by its flange. After wiring, it is bolted ${ }^{31}{ }_{2}$ in from the rear edge of the chassis, behind the bandspread capacitor.

The EF91, TC1, and crystal holder are mounted in line on the top of the sub-chassis with TCl insulated from the metal. This may be done by punching a hole which adequately clears the bush, and using two washers of $\mathrm{t}_{16}$ in paxolin.

A small tag strip anchors C2, R3 and R4, and a flexible lead to pass to the function switch. C4 is similarly anchored, and a rigid insulated wire a few inches long is soldered here and runs near the ganged tuning capacitor. This was found to give adequate coupling into the receiver.

A blue lead from pin 4 passes to the heater circuit. The chassis return is formed by bolting the marker to the receiver chassis.

Initially place TCl about half closed. With the function switch at "Calibrate" the 5th harmonic at 5 MHz can be located with the appropriate coils in place. Switch off the marker and tune in MSF, which will probably be found on almost exactly the same frequency. If necessary, TCl is rotated so that the marker harmonic is on the same frequency. Turning TCl either way from this position will cause a flutter, rising to a low pitched growl or audio tone, the correct setting for VC1 being the central, zero position.

The marker can be used for calibration, enabling the 1 MHz tuning points to be marked in, from 1 MHz to 30 MHz .

It also allows exact positioning of the bandset capacitor, so that frequencies in a narrow band can be read with the bandspread tuner. To do this, turn the bandspread pointer to the nearest MHz reading, and adjust the bandset capacitor for zero beat. This assures exact reading on the bandspread dial, which is not possible if the bandset capacitor is adjusted visually. This procedure is used at $4 \mathrm{MHz}, 7 \mathrm{MHz}$, $14 \mathrm{MHz}, 21 \mathrm{MHz}$ and 28 MHz , for the $80,40,20,15$ and 10 metre amateur bands.

## GENERAL NOTES

A piece of thin perspex $8{ }_{4} \times 3{ }_{2}$ in is used to cover the scales, held with chrome bolts. The perspex was held slightly clear of the panel by $1_{2}$ in wide strips of card at the bottom and each side. This allows slightly thinner card to be slid in, so that a separate pair of scales can be used with each set af coils. There is sufficient space to take all the four ranges on a single permanent card, if preferred.

The case top was cut to give an opening lid about $111_{2} \times 7 \mathrm{in}$. A line scribed $3_{4}$ in from the back, $1^{1}{ }_{2}$ in from the front, and $13_{4}$ in from each side. A small drill is used to start a metal saw, to remove this piece. Strips about lin wide are bolted on inside the cabinet, for the piece removed to close upon, and it is secured along the back with a piano type hinge.

Several $1_{2}$ in holes are punched in the case bottom, and along the back, for ventilation. Openings $3_{2} \times 1^{1}{ }_{2}$ in are cut for the aerial and other connections and the mains cord. This can be done by punching pairs of $1^{1}{ }_{2}$ in diameter holes, and sawing between them.


This dictionary has been compiled to assist the reader in identifying the more common components that he will come across when constructing electronic equipment. It will also enable him to choose the correct component for a particular purpose.

## AERIALS, ferrite

Ferrite rod aerials are universal in transistor radios and many other receivers, obviating the need for an external aerial. Inductors suitable for the medium and/or long wave ranges are wound on formers on a flat slab or round rod of ferrite material, the formers being movable on the rod for alignment purposes. These inductors take the place of the conventional inductors in the input circuit of the first stage of the receiver.

Ferrite rod aerials have very pronounced directional characteristics having minimum pick-up off the ends of the rod and maximum pick-up at right angles to the line of the rod. This feature can be used to increase the strength of a signal or to null out an interfering signal if its direction is substantially different to that of the wanted signal.

Ferrite aerials are obtainable for use in either valve or transistor circuits.

## CAPACITORS, fixed

Any two metal objects (plates) separated by an insulator (dielectric) possess capacitance, or the ability to hold an electrical charge. Introduction of a solid dielectric in place of air increases the value of a capacitor by several times.

Practical Units: The microfarad ( $\mu \mathrm{F}$ ) and the picofarad ( $\mathrm{pF}=1 / 1,000,000 \mu \mathrm{~F}$ ).
Electrolytic capacitors basically consist of two lengths of metal foil separated by a length of insulating material, the whole rolled up and sealed in a tubular container. During the process an electrolyte is introduced often in the form of a jelly. The foil may be aluminium or tantalum which may be etched in ofder to increase the effective area and thus the capacitance. The insulating material will be as thin as possible consistent with the working voltage of the capacitor. All these measures are aimed at getting the maximum capacitance into the minimum of space.

Electrolytic capacitors are generally polarised, one side (or electrode) always being connected to the positive side of the supply and the other electrode to negative. Generally, the outer case, usually of aluminium, is connected to the negative side although occasionally it is isolated. If the voltage is applied in reverse polarity the capacitor will almost certainly be badly damaged. Plus and minus signs or red and black markings are usually boldly marked on polarised electrolytic capacitors.

It should be noted that non-polarised electrolytics are

also obtainable but they are the exception rather than the rule. Electrolytic capacitors with as many as four sections are available such as $8+8+16+16 \mu \mathrm{~F}$ usually with a common negative connection, with the one unit being used for smoothing and decoupling purposes. Values of electrolytic capacitors range from $0 \cdot 25 \mu \mathrm{~F}$ to $10000 \mu \mathrm{~F}$ at working voltages from 2.5 V to 600 V . Tolerances on nominal capacity are not "symmetrical" as with resistors ( $\pm 5 \%$ ) but may be given as " $-10 \%+50 \%$ " or " $-10 \%+100 \%$ ".
Electrolytic capacitors are used in electronic equipment for smoothing purposes in mains rectifier circuits and as decoupling capacitors on h.t. and cathode circuits in valve radios, amplifiers etc. and as decoupling and coupling components in transistorised equipment.

Fixed Capacitors (non-electrolytic) have several different forms of construction, each with its own special characteristics, which must be taken into account when selecting a capacitor for a particular application, so each type will be described separately.

Silver Mica capacitors are considered very stable with a low temperature co-efficient and thus eminently suitable for use in tuned circuits. The working voltage is generally 350 V and capacity tolerance 1 or $2 \%$ with values available from $2 \cdot 2$ to $12000 \mathrm{pF}(0 \cdot 012 \mu \mathrm{~F})$.


Polystyrene capacitors are cylindrical in form with the plastic film forming the dielectric. Possessing high insulation resistance, stability is fair and a negative temperature co-efficient makes these capacitors suitable for temperature compensation purposes in oscillator circuits. Also suitable for coupling and decoupling at radio frequencies. Capacitances available from $2 \cdot 2 \mathrm{pF}$ to $0 \cdot 1 \mu \mathrm{~F}$ with tolerances of $2 \frac{1}{2}$ to $5 \%$ and working voltages of 125 V or 250 V .
Polyester capacitors are also tubular, the dielectric this time being polyester plastic foil, again providing high insulation resistance and thus much superior to paper insulation in every respect. Stability is good and performance at r.f. fair. These capacitors can be used to replace paper ones in all non-critical applications. The range of capacitance is $0.01 \mu \mathrm{~F}$ to $0.5 \mu \mathrm{~F}$ with a tolerance of $10 \%$ and working voltages of 125 V or 250 V .
Polycarbonate capacitors are somewhat similar to paper capacitors in performance, having poor stability and only fair capabilities from the point of view of r.f. performance.
Ceramic, tubular capacitors have good stability characteristics together with known temperature coefficients which may be positive or negative and sometimes
included in the colour code marking. Hence these capacitors may be used to effect temperature compensation of funed circuits with a fair amount of precision. Care must be taken not to confuse these capacitors with the ceramic "High K" types which have a very high temperature co-efficient and are not particularly stable, being more suited for use as r.f. coupling and bypass capacitors. See table for colour coding.

## CAPACITORS, variable

Variable capacitors, like their fixed counterparts, come in a wide variety of sizes and values from the simplest two plate (vane) trimmer to the multi-section tuning capacitor with a total of perhaps 120 vanes.
The moving plates or rotor are usually electrically part of the capacitor framework, the fixed vanes or stator being mounted in the framework on ceramic stand-off insulators to ensure minimum losses. Capacitors intended for use in oscillator circuits, where stability is most important, will have a rotor bearing at each end of the framework while a single front bearing is adequate for other uses.

The spacing between the vanes may only be a few thousandths of an inch in the case of miniature variable capacitors such as are used in transistor radios while those used in small transmitters may have an air gap of a $\ddagger \mathrm{in}$. depending upon the d.c. and r.f. voltages existing across the capacitor. In the process of miniaturisation the air dielectric is replaced by a plastic film considerably reducing the physical size of the unit for a given capacltance.


Ganged capacitors may have several sections mounted on a common spindle otten with an end section of lower capacitance than the others, for use in the oscillator circuit of a superhet receiver. Each section will have a built-in compression type trimmer for alignment purposes. These trimmers are not generally shown on circuit diagrams. Typical values for a two-gang unit are $176 \mathrm{pF}+208 \mathrm{pF}$ and, for a four-gang unit, $15 p F+15 p F+500 p F+500 p F$, the latter being intended for use in an a.m./f.m. receiver.

Differential capacitors have two stators arranged about a common rotor so that the capacitance of one is increasing while decreasing on the other, being, in effect, a capacitative potentiometer.
The "law" of a capacitor relates the change in capacity with angular movement of the rotor, common ones being SLF (straight line frequency) and SLW (straight line wavelength). In each case the dial calibration will be approximately linear. The law is determined by the shape of the rotor vanes.
It is possible to obtain capacitors with integral slowmotion gearing obviating the need for a separate dial mechanism.
Trimmer capacitors are generally similar in construction to variable capacitors except that the spindle is short and slotted to take a screwdriver. Air spaced trimmers are not generally available in values greater than 150 pF . Ceramic trimmers are two plate capacitors with the plates in the form of silver deposited on the ceramic base and ceramic disc rotor. The maximum value of this type of trimmer is mostly under 50 pF .

Compression type trimmers utilise mica or plastic film for the dielectric between a stack of plates the capacity being adjusted by means of a central screw altering the pressure on the plates. The minimum capacitance of this type of trimmer tends to be high but the maximum capacitance can be as much as 2000 pF . Typical ranges are $10-$ 80 pF and $500-2000 \mathrm{pF}$. These trimmers are commonly known as "padders" and are mainly used in the oscillator circuit of receivers.

## CIRCUIT BOARDS

These are flat boards of insulating material on which components may be mounted and wired together to form electronic circuits. The insulation may be s.r.b.p. (synthetic resin bonded paper) or fibreglass. Boards may have the circuit printed on one side by depositing copper by chemical means, the components being interconnected with the circuit through small holes in the board. Copper clad boards having one side covered in copper can be used to form printed circuit boards by etching away the unwanted copper.

Other boards (Veroboard) have a series of copper strips on one side with a matrix of holes, usually of $0 \cdot 10^{\prime \prime}$ or $0.15^{\prime \prime}$ spacing, along the strips thus enabling components to be wired between the strips to form a circuit. Plain Veroboard is also available having the matrix of holes but no copper strips. Special pins are used with this board to which components and wiring may be connected.

Edge connector sockets can be fitted to electronic equipment enabling circuit boards to be rapidly inserted or removed for servicing.

## DIODES

A diode is a simple rectifier capable of passing current essentially in one direction only and hence may be used to rectify a.c.


Thermionic diodes consist of a filament or heater, constituting the cathode, surrounded by a metal cylinder or anode, all enclosed in an evacuated glass envelope. The diode may be a single unit or one or more may be incorporated with a triode or other valve. Power rectifiers consisting of two diodes, often with a common heater, are used in radio receivers and similar equipment to provide d.c. from an a.c. supply. Thermionic diodes or rectifiers are rapidly being replaced by silicon diodes which do not require a heater and are more efficient.

Semiconductor diodes are generally of silicon or germanium with a point contact or a junction of semiconductor materials. The smallest, a fraction of an inch long, are used for signal rectification and similar small signal purposes while the largest used in power supplies єañ pass several hundred amperes. Vast quantities of s.c. diodes are used in computers as high speed switches usually as part of integrated circuits. In a silicon diode the resistance in the forward direction is very low and high in the reverse direction. In a germanium diode the resistance in the reverse direction is appreciably lower
than that of a silicon diode.
Semiconductor diodes are marked with a spot or a band or a plus sign indicating the end of the diode that will show a positive voltage when an a.c. voltage is applied to the diode. This end corresponds to the cathode in a thermionic rectifier.
A characteristic of diodes, quoted in maker's data, is the "peak inverse voltage" (PIV). This is the maximum peak voltage allowable across the diode during the nonconducting part of its operating cycle. In practice the p.i.v. will vary between 1.4 and 2.8 times the applied r.m.s. voltage depending upon the type of rectifier circuit employed.

## INDUCTORS

While a straight wire possesses "inductance" the value of this inductance will be considerably increased if the wire is formed into a coil or inductor. An iron dust core inserted into the inductor will further increase this inductance.

Practical Units: The henry ( H ), the millihenry ( $\mathrm{mH}=$ $1 / 1000 \mathrm{H}$ ) and the microhenry ( $\mu \mathrm{H}=1 / 1,000,000 \mathrm{H}$ ).

LF Inductors, or chokes, are a single winding on an insulating former having a laminated core (see Transformers). The inductance will range from one or two henrys to around 50 henrys or so. These chokes offer high impedance to low frequencies and are used in audio amplifiers and filters, loudspeaker networks and as smoothing chokes in mains rectifier circuits.

RF Inductors, or coils, have a single winding, either layer or pile wound, on a low-loss former and may include an adjustable iron dust core for varying the inductance. If the coil is wound with heavy gauge wire the turns may be self-supporting. Windings of comparatively few turns may be added to the inductor to couple it to other circuits or to provide a feedback winding for use in oscillators.

Such inductors, with associated tuning capacitors, are found in r.f. amplifier, mixer and oscillator stages of receivers as well as in transmitters and signal generators and other test equipment. Although they are usually permanently wired into circuit they can be obtained mounted on a plug-in base for rapid coil changing.

The "goodness" or "Q" of an inductor may be enhanced by enclosing it in a ferrite "pot" with or without an adjustable iron dust core.


RF Chokes are inductors having a single winding, sometimes on a ferrite core, and of sufficiently large inductance to present a high impedance to specified radio frequencies. The winding may also be in the form of several separated pile wound sections in order to reduce the self-capacitance of the choke.

Values of inductance range from a few microhenrys for v.h.f. work to 30 millihenrys for the lower radio frequencies.

## NTEGRATED CIRCUITS

The integrated circuit is produced by methods similar to those used in transistor manufacture and combines a number of discrete components on the one silicon chip. Apart from the transistors or diodes, resistors, capacitors

and inductors can be formed as well as the necessary interconnections.

Linear i.c.'s include wideband, audio and operational amplifiers while digital i.c.'s are used in frequency counters, digital clocks, computers etc.

Integrated circuits may be encapsulated or mounted in metal cases. Lead-out wires or tags enable the device to be directly wired into a circuit board or plugged into a suitable holder.

## PHOTOCONDUCTIVE CELLS

These devices are sensitive to light, either producing a voltage when subjected to sunlight as in the case of selenium and silicon photocells, or varying their internal resistance as with cadmium sulphide photocells. The latter are also known as light-dependent resistors (LDR).

The silicon and selenium cells will deliver enough power to operate a transistorised radio or even a small electric motor, a single silicon cell providing nearly half a volt at a current of 15 mA .


With LDR's the effect of the varying resistance with changes of incident light can be amplified and used to actuate an alarm or counter or similar device. A typical LDR is the ORP12 which has a "dark resistance" of several megohms falling to a few hundred ohms with full illumination.

## RESISTORS, fixed

Every electrical circuit possesses "resistance" which limits the current flowing in the circuit. Resistors of known value are used to introduce resistance into circuits, usually to a pre-arranged design.
Practical Units: The ohm ( $\Omega$ ), kilohm ( $k \Omega=1000 \Omega$ ) and the megohm ( $M \Omega=1,000,000 \Omega$ ).

Fixed resistors (carbon) are moulded from a special carbon composition, the connections to the resistor being in the form of wire ends. Resistors are given a wattage rating by the makers which represents the maximum power that the resistor may safely dissipate. Wattages generally available range from $\frac{1}{8}$ watt to 2 watts in values from 1 ohm to 22 megohms.

The tolerances available on the nominal value are usually plus or minus ( $\pm$ ) 5 and $10 \%$ although $20 \%$ was common in the recent past.

The stability of composition resistors is poor but their performance at radio frequencies can be considered fair while their change of value with change in temperature
(temp. co-efficient) is poor being about ten times worse than a wire-wound resistor. Such resistors should only be used in non-critical applications.

High wattage carbon resistors, 25 W or more, are often used as non-inductive loads for transmitters and amplifiers although they are somewhat difficult to obtain. Constructors can improvise by series/paralleling lower wattage resistors until the required value is obtained.

Fixed resistors (metal oxide/carbon film) are formed by deposition on to a ceramic tube or rod, their main advantage being that of high stability. Tolerances are generally 1 or $2 \%$.

Their performance at r.f. is good although care should be taken in using them at v.h.f. or u.h.f. slnce the metal film is often in the form of a spiral which can introduce appreciable inductance at these frequencies. These resistors are particularly suitable for audio amplifiers and circuits where a low noise level is essential.

Fixed resistors (wire-wound) are composed of a layer of resistance wire on a ceramic tube or rod, with clips or wire ends, and generally having a coating of vitreous enamel or something similar. Some versions have one or more movable clips so that intermediate values of resistance can be had.

Wire-wound resistors must not be used in r.f. circuits since by the very nature of their construction they are highly inductive. Those with special windings and termed "noninductive" should also be treated with some suspicion at r.f. On the credit side these resistors have a very low noise characteristic and low temperature co-efficient compared to carbon resistors.


Wire-wound resistors are available to the constructor in ratings from 1 W to around 50 W and in values from $0.22 \Omega$ to $100 \mathrm{k} \Omega$ usually with a tolerance of $5 \%$. Mains "dropper" resistors are a special breed of wire-wound resistor used in transformerless radios and TV sets and fitted in series with the valve heater chain. They may have adjustable clips or tapped sections.
Resistor values, for carbon resistors, are indicated by a colour coding, details of which are given in the accompanying table. If a tip or spot colour appears to be missing it can be assumed to have the same colour as the body of the resistor. For example, a resistor which is red all over has a value of $2 \cdot 2 \mathrm{k} \Omega$ and one with an orange body and a yellow spot only is $330 \mathrm{k} \Omega$.

The actual values of resistors in common use conform to the "E12 Series" of twelve values and their decades (see table) but there is also the "E24 Series" with a further twelve values intermediate with the E12 series. These are: $1 \cdot 1,1 \cdot 3,1 \cdot 6,2 \cdot 0,2 \cdot 4,3 \cdot 0,3 \cdot 6,4 \cdot 3,5 \cdot 1,6 \cdot 2,7 \cdot 5$ and $9 \cdot 1$ and their decades.

Wirewound resistors usually have their value marked in plain numbers.

## RESISTORS, variable

Like fixed resistors, these use either carbon composition or resistance wire for the resistance element. The moving arm or rotor moves over the element thus enabling any value between virtually zero and the value of the variable resistor to be selected. The rotor spindle is extended to take a control knob where frequent adjustment is required, such as with a volume control, or may be short and slotted for adjustment with a screwdriver as a preset control. Potentiometer or "pot" is the general name given to such variable resistors.

Carbon potentiometers have a moulded composition track or a carbon deposit on an insulating ring. The rotor contact, generally with two or more "fingers" to ensure continuous pressure on the track, is usually isolated from the spindle.

The amount of resistance in circuit relative to the angular movement of the rotor constitutes the "law" of the potentiometer. If equal resistance change results from equal angular movement of the rotor the potentiometer is said to be "linear". If the change is logarithmic the potentiometer is "log" law. If checked on a test meter such a potentiometer would show little change in resistance at the beginning of the movement (clockwise) and a very rapid change towards the end of the movement. An "anti-log" potentiometer will show the reverse effect.
Log potentiometers are generally used as volumes controls on radios and audio amplifiers since the human ear responds to sound levels on a logarithmic basis, Such a volume control will appear to give equal changes in sound level for equal movement of the control.

Potentiometers can be obtained ganged together with a common spindle or with concentric spindles for independent operation. On stereo amplifiers ganged potentiometers are used for volume controls, filter adjustments, balancing and similar circuits where both amplifiers must be adjusfed simultaneously. It is common practice to fit a volume control with a single or double pole mains on/off switch operated by the rotor of the potentiometer at the beginning of its travel.


Values of carbon potentiometers go from around $100 \Omega$ to about $2 \mathrm{M} \Omega$. Wattage ratings are not always quoted since these controls are not usually called upon to pass any appreciable current.

Pre-set carbon potentiometers may be of completely enclosed construction or open skeleton type. The latter generally have wire lead-outs or tags suitable for direct mounting on circuit boards.


Wirewound potentiometers are similar in most respects to the carbon ones except that the resistance element consists of resistance wire wound on to a flat insulating strip which is then formed into a ring, the rotor generally moving round one edge of the ring.

Values of these potentiometers of interest to the constructor run from $10 \Omega$ to $100 \mathrm{k} \Omega$ in ratings from 1 to 3 W . Again, mains on/off switches can be fitted if required.

Precision wirewound potentiometers have the winding in helical form needing perhaps ten or more turns of the control spindle to cover the whole winding. A turns counter is fitted to the spindle. Preset wirewound potentiometers for use on circuit boards have a straight winding with a sliding contact operated by a screw thread, the whole enclosed in a plastic moulding. For use in adverse conditions of dirt or moisture both carbon and wirewound potentiometers can be had as hermetically sealed units.

## SWITCHES

The simplest device for making or breaking a circuit is the on/off switch and from this devolves a multiplicity of types.

COLOUR CODE FOR CAPACITORS AND RESISTORS

|  | First Figure ' ${ }^{\prime}$ ' | Sec'd Figure 'B' | Multiplier$' C^{\prime}$ |  | Tolerance 'D' |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Res | $\begin{aligned} & \text { Cerami } \\ & \text { to } 10 \mathrm{pF} \end{aligned}$ | Capacitors over 10pF |
|  |  |  | Resistors | Caps pF |  |  |  |
| Black | - | 0 | 10 | 1 | -1 | 2pF <br> 0.1 pF | $\begin{array}{r}  \pm 20 \% \\ \pm 1 \% \end{array}$ |
| Brown | 1 | 1 | 10 | 10 | $\pm 1 \%$ | $0 \cdot 1 \mathrm{pF}$ | $\begin{aligned} & \pm 1 \% \\ & \pm 2 \% \end{aligned}$ |
| Red | 2 | 2 | 100 | 100 | $\pm 2 \%$ | - | $\pm 2 \%$ |
| Orange | 3 | 3 | 1,000 | 1,000 | - | - | $\pm 2-\%$ |
| Yellow | 4 | 4 | 10,000 | 10,000 | - | 0.5 pF | $\pm 5 \%$ |
| Green | 5 | 5 | 100,000 | - | - | $0 \cdot 5 \mathrm{pF}$ | $\pm 5 \%$ |
| Blue | 6 | 6 | 1,000,000 | - | - | - |  |
| Violet | 7 | 7 | 10,000,000 | $0.01 \mu \mathrm{~F}$ | - | $0 . \overline{25 p F}$ | - |
| Grey | 8 | 8 | $100,000,000$ $1,000,000,000$ | $0.01 \mu \mathrm{~F}$ $0.1 \mu \mathrm{~F}$ | - | $0.25 p F$ 1 pF | $\pm \overline{10 \%}$ |
| White | 9 | 9 | 1,000,000,000 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm \overline{20} \%$ | 1pF | $\pm$ - |
| No colour Silver | - | - | - | - | $\pm 10 \%$ | - | - |
| Gold | - | - | - | - | $\pm 5 \%$ | - | - |

A salmon-pink fifth ring or body colour denotes a Grade 1 high-stability composition resistor. There are variations in the code for capacitors other than ceramic tubular types.


Toggle switches have a laminated or moulded body with a metal or insulated dolly or operating lever. Switch contact combinations include single pole, single throw, (s.p.s.t.), double pole, single or double throw (d.p.s.t. and d.p.d.t.) and double pole change-over. Some types are obtainable with a centre off position. The dolly may be slotted for operation from a cam on an associated control. Other variations include biasing in one position, terminal or tag connections and instrument type toggles which are designed to have very low contact resistance for instrument use.

The ordinary toggle is designed to carry 3 A at 250 V a.c. with other ratings up to 10A.

Other switches performing the same function as toggle switches include rotary toggle switches, miniature slide switches and press button switches although these are generally s.p.s.t. only.


Microswitches are button operated switches capable of operation with pressures as low as 1 ounce usually by means of a lever or similar attachment. Contact arrangements are fairly simple, on/off or s.p.d.t. the contacts themselves handling 6 A at 12 V a.c. or 3 A at 250 V a.c. although models are obtainable for up to 10A.

Wafer rotary switches consist of a flat ring of paxolin insulating material with fixed contacts riveted around the periphery. A disc in the centre of the ring carries the rotor contacts, the disc being rotated by a spindle attached to an index plate. The maximum number of fixed contacts is generally 12 with a maximum of four on the rotor giving various combinations such as 1 pole, 12 way to 4 pole, 3 way.

Since the wafers are very thin several may be mounted on one spindle, sometimes with metal screens between sections to reduce unwanted coupling. These switches are widely used as wavechange switches on radios, audio filters and tone control circuits as well as in meters and test equipment.

Mains switches are available for use with wafer switch assemblies since the wafers themselves should not be used for this purpose. The contacts are not designed to
carry any appreciable current. Wafers in ceramic or other low-loss materials are available for switching r.f. circuits. The switches can be bought as complete units or the individual wafers and parts obtained and assembled to suit particular requirements.

## THERMISTORS

Thermistors are a special kind of resistor having a pronounced negative temperature co-efficient. They are used in circuits, such as valve heater chains, to restrict initial current surges when first switching on. The initial high resistance of the thermistor drops logarithmically as the protected device warms up.
Neg. temp co-effic.

$$
\operatorname{Hos} \text { temn co-eftic. }
$$

The thermistor is also used to protect photo flood lamps from current surges and in temperature sensitive fire alarm systems. Audio signal generators and oscillators utilise the thermistor in feedback circuits to provide a constant output. Bead type thermistors are used in these circuits since their reaction time to current changes is comparatively short. Bead types can also be employed in measuring r.f. power especially at very high frequencies.
Thermistors in general use have current ratings ranging from 2 mA to 2 A .

## THYRISTORS

Also known as silicon controlled rectifiers (SCR) the thyristor is basically a silicon diode rectifier with an additional electrode or "gate" which is used to control the current flowing through the thyristor. A pulse applied to the gate can switch the thyristor on or off. Once the thyristor is conducting a minimum current is required to maintain conduction.


Thyristors used by the constructor will have current ratings between 1 and 10A and peak voltage ratings up to 600 V . The p.i.v. figure required for a particular application will be approximately $1 \frac{1}{2}$ times the applied r.m.s. voltage.

The gate trigger circuit will need to provide a voltage of the order of 3 V at a current of up to 20 mA . Small current thyristors are generally contained in a TO5 type metal case with wire lead-outs while the larger thyristors have a stud mounting and tag connectors.

## TRANSFILTERS

Transfilters are ceramic filters having somewhat similar characteristics to those of the conventional i.f. transformer. Several transfilters may be combined with capacitors to provide specified bandpass filter features. Several types of transfilter are available around 455 kHz as well as for $10 \cdot 7 \mathrm{MHz}$ for use in the i.f. stages of f.m. receivers. Since transfilters do not require any alignment in a receiver they are gradually replacing the tuned i.f. transformers in commercial receivers.


## TRANSFORMERS

Basically two coils coupled together so that an alternating current in one coil, the primary, will induce an alternating current in the second coil, the secondary. The ratio of the input voltage, producing the current in the primary, to the voltage at the secondary is directly proportional to the turns ratio of the two coils.
In this way the transformer can be used to match one impedance to another.

LF Transformers are wound on a laminated core of ferromagnetic material, the laminations being electrically insulated from each other. Mains transformers may have extra windings for valve heaters, pilot lamps etc. as well as taps on the primary winding to accommodate variations in mains supply voltages.


RF Transformers have coils wound in layer or pilewound form, or air-spaced, on insulating formers often with iron dust cores or slugs to enable each winding to be separately tuned.
IF Transformers are similar to r.f. transformers, being designed to work at the fixed intermediate frequency in superhet receivers, usually between 450 to 475 kHz or around 1.6 MHz . As well as dust cores each winding generally has a fixed capacitor across it in order to obtain the optimum inductance to capacitance ratio.


Autotransformers have a single tapped winding the ratio of the turns each side of the tap providing the required transformation ratio. One winding may be common to both circuits providing an alternative ratio. Note that an autotransformer does not provide the isolation obtainable with a double wound transformer. A common form of autotransformer is the Variac used for compensating changes in mains supply voltages.


Power



Toroid

Toroid transformers have the windings wound on an annular ferrite core. The separate wires comprising the windings are laid or twisted together and then wound round the ferrite ring. On the circuit symbol the start of each winding is marked with a dot to assist in identification.

## TRANSISTORS

The transistor is a three electrode semiconductor device capable of amplifying an electrical signal. The semi-
conductor materials used in making transistors are either silicon or germanium although there are others such as selenium.

The pure silicon or germanium is treated with either of two impurities in minute quantities to produce ' $p$ ' and ' $n$ ' type silicon and germanium. A junction of silicon $p$ and $n$ material will show a high resistance in one direction and a low resistance in the other thus forming a diode. A germanium diode similarly formed will not show such a wide change in resistance.

A p-n-p transistor is formed from a thin slice of $n$ material sandwiched between two pieces of $p$ material, the slice being known as the base and the p material as the emitter and collector respectively. An n-p-n transistor has a slice of $p$ material between two pieces of $n$ material.

With an n-p-n transistor the emitter voltage must always be negative with respect to the collector and the emitter of a $\mathrm{p}-\mathrm{n}-\mathrm{p}$ transistor positive with respect to the collector. N-P-N and p-n-p transistors can have very similar characteristics in which case they are said to be "complementary".

Many different processes are used in the manufacture of transistors producing devices of widely varying characteristics and types:

Alloy transistors were among the earliest types produced. The germanium alloy transistors are cheap to produce but do not have a very good performance at high frequencies. They are widely used as power transistors since their low resistance permits the maximum current to be passed at low voltages. Silicon alloy transistors are used mainly because of their ability to operate at high temperatures.


 insul, gate

n-channel
junction gate


Alloy-diffused transistors have improved performance with a cut-off frequency of the order of 100 MHz and being cheap to produce are widely used in radio receivers.

Mesa transistors with a cut-off frequency of over 1000 MHz are among the best at high frequencies.

Planar and epitaxial planar transistors have been developed to reduce the collector leakage current and also to include a shield to reduce the capacitance existing between the collector and base electrodes.

Field effect transistors are unipolar as distinct from those listed above which are bi-polar. F.E.T.'s are more akin to the thermionic valve than any previous transistors. While bi-polar transistors are essentially current operated devices and have a low input resistance f.e.t.'s are voltage controlled and consequently have a very high input resistance. The controlling "gate" may be either a junction type (j.u.g.f.e.t.) or insulated type gate (i.g.f.e.t.) either type being obtainable as p-channel or n-channel f.e.t. The i.g.f.e.t. is also known as the metal oxide silicon f.e.t. (m.o.s.f.e.t.).


## VALVES

Thermionic valves contain a filament or heater/cathode which emits electrons, with one or more other electrodes. all contained in an evacuated glass envelope. The four basic types of valve are the diode, triode, tetrode/pentode and frequency changer or mixer.


The Diode comprises the cathode and a metal plate or cylinder called the anode. Small single or double diode units are used for signal rectification in detectors and a.g.c. circuits. Larger single or double units are employed in half and full wave power rectifier circuits. A special use for diodes is in the line scanning circuits of TV sets where they are known as "efficiency diodes".

One or more diodes are frequently found in a common structure with triodes and pentodes where they are associated with the signal circuits.

The Triode has a wire mesh, the signal grid, placed between the cathode and the anode. A negative voltage on the grid controls the anode current enabling the triode to be used as an a.f. amplifier or oscillator at a.f. or r.f. A triode is commonly incorporated with a pentode where it acts as a preamplifier.

The Tetrode has a second grid placed between the signal grid and the anode. This "screen grid" reduces inter-electrode capacitance and overcomes a deficiency of the triode known as the "space charge effect".

The Pentode has yet another grid, the suppressor grid, between the screen grid and the anode, which eliminates
the kink in the characteristic curve of the tetrode caused by secondary emission. In "beam" tetrodes this third grid is omitted but its effect is simulated by the careful placement of the anode with respect to the other electrodes. Tetrodes and pentodes are used for both r.f. and a.f. work.

Frequency changers, or mixers, are used in superhets to produce the intermediate frequency (i.f.) from the input signal and the local oscillator signal. The mixer valve takes the form of a pentode or tetrode with additional grids to which these signals are applied. Some frequency changers incorporate a separate triode for the local oscillator feeding internally or externally into the mixer section.

Battery type valves have 1.4 V filaments for operation from a single cell, taking a current of 25 or 50 mA . The maximum anode voltage is generally 90 V . Valves fed from a mains supply may have 6.3 V heaters which are connected in parallel each heater taking anything from 200 to 600 mA . Dual section valves sometimes have heaters with a centre tap allowing operation in series on 12.6 V or in parallel on $6 \cdot 3 \mathrm{~V}$.

Other mains operated valves have the heaters in series based on a common current of 100,150 or 300 mA with individual heater voltages of 4 up to 50 V . In a.c./d.c. receivers and TV sets the heater chain may be connected across the mains, the difference between the sum of the heater voltages and the mains voltage being taken up by a "dropper" resistor (see Resistors, fixed).

## VARICAP DIODES

Varicap Diodes, sometimes known as varactors, are similar to semiconductor p-n junction diodes in that the capacity existing between the regions varies with the applied reverse voltage. Varicap diodes provide known changes of capacity over a given range of reverse voltage, typically 50 to 10 pF for a range of 1 to 20 volts.


These diodes can thus be used to tune r.f. circuits by means of a potentiometer controlling the applied reverse voltage. They are useful up to frequencies of several hundred MHz and are currently being employed commercially in v.h.f. receivers and t.v. tuners.

## ZENER DIODES

The zener diode is a semiconductor diode which breaks down and conducts when a voltage applied in the reverse direction reaches a predetermined value. The action is somewhat similar to that of a gas filled voltage stabiliser.

The external circuitry of a zener diode must be designed so that its rated power dissipation is not exceeded.

[Tㅏㄹㄱ
Zener diodes of interest to the constructor are available with nominal zener voltages ranging from 2.4 V to 200 V with tolerances from 5 to $20 \%$ and dissipations from 200 mW to 20 W . These diodes are used as voltage stabilisers, voltage reference sources, limiters etc.

The end of a zener diode intended to be connected to the positive side of a supply is usually marked with a spot or band or a plus sign.

## * IN NEXT MONTHS MiAGFIGAL

 EXTRA EXPERIMENTERS
## CIRCUITS SUPPLEMENT

Here is a mine of information for anyone who can work from a circuit. Feast your eyes on some of the items which are included: several audio amps, ranging from 50 mW to 10W: radio circuits from a crystal set to an all band receiver-plus test gear, novelty circuits, etc., etc. Heaps of circuits with all the necessary information and notesyou'll want to keep it for years!


## stereo decoder

Most of us have been endowed with two ears; why? Surely because we were meant to listen to stereol Plans are being made by the BBC to increase their output of stereo material and you'll soon want to fit a decoder to your f.m. set if you haven't one already. Why not settle for our high quality design-complete with easy-to-follow plans.



## TRANSISTOR CIRCUITRY formeginers <br> PART 3

## Circuits and Parameters

That ugly word 'parameters' frightens many new-comers-and really, it need not, for it is only the guideline along which we can walk as we follow the curious path of transistor development. There have to be some hard-and-fast rules, and these are the parameters.

Transistors can be of p.n.p. or n.p.n configuration, the essential difference, in practice, being polarity of the supply voltage. The three basic modes are common-base, common emitter and common-collector. The last is more conveniently referred to as emitter follower, for reasons we shall explain. Some of our circuits show p.n.p. transistors, some n.p.n.-we must get it into our heads at the outset that the essential difference is polarity, and this makes it easy to combine the two types in one circuit.

The common-base circuit is a good introduction to transistor technology. Here, a small change in emitter current brings about a small change in collector current. The ratio between the two is the current transfer ratio, alpha (x).

$$
\text { In symbolic form : } \alpha=\frac{\delta I_{C}}{\delta I_{E}}
$$

where delta ( $(\mathrm{r})$ denotes change, in this case, increase. In some formulae, the symbol $\triangle$ may be used instead of $\delta$.

Figures for alpha are very near, but not quite, unity. For a germanium device, typically 0.98 .

Take Fig. 9, a proving circuit to demonstrate the above formula. Here we have a common-base transistor connected so that the emitter current flows, around 0.5 mA . Voltage $\mathrm{V}_{\mathrm{E}}$ establishes this. The emitter junction for an average transistor will be around 100 ohms. The collector current, $\mathrm{I}_{\mathrm{C}}$, flowing through the load $\mathrm{R}_{\mathrm{L}}$, will be slightly lower than the emitter current. Between base and emitter-the base being earthed, or common, a 1.5 volt battery biases the emitter positively.

The input voltage, $\mathrm{V}_{\mathrm{II}}$, depends on the setting of the variable resistance, $\mathrm{R}_{\mathrm{I}}$, which has a further $\mathbf{1} \cdot 5$
volt battery across it, again biasing the emitter positively. The proportion of voltage across the base/ emitter junction aided by the position of $\mathrm{R}_{\mathrm{IS}}$ in series with $\mathrm{V}_{\mathrm{E}}$ represents the increase $\delta \mathrm{I}_{\mathrm{E}}$.

The emitter junction resistance of a typical small signal transistor is about 100 ohms, and let us suppose that the load resistor is 10000 ohms. Thus the change at the input is $10 \mu \mathrm{~A}$ through a resistance of 100 ohms, but the change at the output is $9 \cdot 8 \mu \mathrm{~A}$ through a resistor of 10000 ohms. The result, from Ohm's Law, is a voltage change across $R_{L}$ of 98 mV for a change in voltage at the input of 1 mV . This gives us a voltage gain of 98 times in spite of a slight loss of current flowing out through the base contact.


Fig. 9: The common-base circuit arranged to demonstrate change in emitter current causing change in collector current.
With the more frequently used common-emitter circuit, the current transfer ratio is the ratio of current change at the base to current change at the collector, and is designated $\beta$ (beta) (or sometimes $x^{\prime}$ ). These parameters, $\beta$ and $x$, are mathematically related, the relationships, for those wishing to look further into this being:

$$
\beta=\frac{\alpha}{(1-\alpha)} \text { and } \alpha=\frac{\beta}{(1+\beta)}
$$

The figures quoted by manufacturers are for smallsignal operation unless otherwise stated.

Another commonly seen transistor parameter is the transition frequency, designated $\mathbf{f}_{\mathrm{T}}$. This is the frequency at which the common-emitter current gain falls to unity, and gives an indication of the frequency limits of the transistor.

## Hybrid Parameters

Hybrid parameters are widely used in the semiconductor industry to specify transistor characteristics. They are a set of resistance, admittance and voltage and current ratios for given conditions (hence the term hybrid). In the case of the common-emitter circuit these $h$ parameters are:
$\mathbf{h}_{\mathrm{ie}}$ : - input resistance, common emitter, output short-circuited.
$h_{r e}$ :- reverse voltage feedback ratio, common emitter, input open circuit.
$\mathbf{h}_{\mathrm{fe}}$ : - forward current gain, common emitter, output short-circuited.
$\mathbf{h}_{0 \mathrm{e}}$ :- output admittance, common emitter, input open circuit.
If one group of parameters is known, for one circuit configuration, it is possible to work out the others. In practice, however, such information is more useful to the designer than to the engineer or constructor, who chooses replacement transistors on more empirical lines than a comparison of detailed parameters.

## Characteristics of Basic Configurations

Approximate characteristics of the three basic circuit configurations are summarised in Table 1. These must be taken as a guide only, not as accurate conditions for a particular transistor. The table indicates the orders of magnitude of the main parameters with the three configurations: actual figures will of course vary considerably with different types of transistor.

TABLE 1 Features of Circuit Configurations for Comparison

| Characteristic | Common Base | Common Emitter | Common Collector |
| :---: | :---: | :---: | :---: |
| Input to | Emitter | Base | Base |
| Output from | Collector | Collector | Emitter |
| Current Gain | Less than unity | About 50 | About 50 |
| Voltage Gain | $\begin{aligned} & \text { High (approx. } \\ & 250 \text { ) } \end{aligned}$ | High (approx. 250) | Low (approx. <br> 1) |
| Input Impedance | Low (2002) | Medium (1000 $\Omega$ ) | High ( $100 \mathrm{k} \Omega$ ) |
| Output Impedance | High (200k $\Omega$ ) | Medium ( $40 \mathrm{k} \Omega$ ) | Low (1000, ) |
| Power Gain | Medium $(30 \mathrm{~dB})$ | High (40dB) | Low (16dB) |
| H.F. Response (Power ... 3dB down) | High ( 400 kHz ) | Low ( 12 kHz ) | Dependent on source and load resistances |
| Phase Shift | $0^{\circ}$-Output and input in phase | $\begin{aligned} & 180^{\circ} \\ & \text { (inverse) } \end{aligned}$ | (in phase) |

It will be noted that the details given in Table 1 include power gain and phase shift, the latter stated to show the effect of the different configurations on the polarity of the signal. This last factor is too often overlooked when experiments are made. Another important factor, not given in the table, but necessary for the designer, is the comparison of collector leakage current with the three configurations: except in the common base configuration, this is dependent on the resistance in the base circuit.

## Output Characteristics

As can be seen from the output characteristic set of curves of Fig. 10, circuit configuration makes quite
a difference to collector voltage and current relationships (compare these characteristics with the basic pn junction characteristic shown in Fig. 6, Part 1). When considering the choice of a replacement transistor or working out a design it is necessary to take a set of output characteristics, i.e., a family of curves for different base currents-and plot a load line as shown in Fig. 11. It can be seen that with a common emitter circuit when the base current is zero the voltage between emitter and collector is almost the full supply volts, i.e. collector current is very small. (It is actually the reverse leakage current of the collector junction.)


Fig. 10: Typical characteristics showing how circuit configuration drastically alters collector voltage and current relationships.

Increasing base current causes an increase of collector current; the voltage across the load resistance increases and the voltage across the transistor decreases. Eventually, as the base current is increased to a state when the collector current causes a voltage across the load almost equal to the supply


Fig. 11: Constructing a load line for a transistor gives its case history for design purposes.
voltage, the voltage across the transistor drops to practically zero. Any increase of base current beyond this point gives no further increase in collector cur-rent-the transistor is saturated. This, for a transistor of given characteristics, is at point B in Fig. 11. The load line, drawn through points X to Y passes through this point $B$. Point $X$ is the maximum supply voltage and point $Y$ the current resulting from dividing the supply voltage by the load resistance. In the example, a supply voltage of 12 volts and a load resistor of 6000 ohms gives a collector current at $Y$ of 2 mA .

From this load line, the transistor operating point can be chosen by adjusting the base current to a value between the two extremes of $A$ and $B$. The
best choice is midway along the load line, i.e. at $P$, where collector current is $\operatorname{lm} A$ and collector volts 6 . Since the current gain of our example is 50 , the base current must be adjusted for $20 \mu \mathrm{~A}$. This will allow an input signal for linear amplification to produce a base current variation of $\pm 20 \mu \mathrm{~A}$, giving a collector current variation of almost $\pm 1 \mathrm{~mA}$ between saturation and cut-off (at upper and lower ends of the curve respectively).

Correct choice of operating point is important; input and output impedances of a common emitter amplifier stage vary with collector current and so performance depends on the value of the d.c. rollector current.

## Bias Stabilisation

To set the operating point, a simple method is to arrange that a d.c. base current flows which (when multiplied by the current gain of the particular transistor) gives the required value of collector current. A resistor from the negative supply to the base provides this, but is not really effective, because of collector leakage current and variation with temperature change. For stable operation, bias stabilisation is required, and the two circuits of Fig. 12 are methods of ensuring this.


Fig. 12(a): Base bias current feedback and (b) voltage bias.
In Fig. $12(\mathrm{a})$ a resistor $\mathrm{R}_{\mathrm{B}}$ is coupled back from collector to base so that if the collector current increases, collector voltage falls and this fall is reflected back to base via $R_{B}$, reducing base current. This tends to reduce collector current and oppose the change. However, this method does not allow control with zero base current and slight variations between transistors do not allow replacements to be made without reconsideration of the value of $R_{B}$. A further point is that a.c. negative feedback is introduced by this method, and this may not be wanted. Splitting the bias resistor and bypassing the centre point to chassis with a suitable capacitor can reduce this feedback.

A better method is shown in Fig. 12(b). The bias voltage $\mathrm{V}_{\mathrm{b}}$ applied to the base is obtained from a potentiometer R1 and R2 across the supply. A further resistor $R_{F}$, is put in the emitter circuit. The voltage across $R_{E}$ is equal to $V_{b}$ less the voltage dropped across the emitter-base junction of the transistor. If $\mathrm{V}_{\mathrm{b}}$ is made large with respect to this junction voltage, the emitter current will depend only on $V_{b}$ and $R_{E}$. Thus if $V_{b}$ is held constant, $I_{E}$ and therefore $I_{C}$ will be independent of temperature and transistor gain.

A comparatively low value of R 2 will not cause a significant change in $\mathrm{V}_{\mathrm{b}}$. Actual values can be seen in
later circuits, and it will be noted that R1 is four or five times the value of $R 2 . R_{E}$ depends on the transistor to be employed, and it will usually be bypassed by a large value capacitor ( C , shown dotted) to avoid loss of gain with an a.c. signal.

## Practical Circuits

Two low frequency amplifier circuits using this method of base bias stabilisation are depicted in Fig. 13. In the first, transformer coupling is used between stages, and in the second RC coupling is employed (note the polarity of the electrolytic coupling capacitors: in p.n.p. transistor circuits the succeeding base will generally be positive with respect to the preceding collector). Because a more precise impedance match between stages can be made with a transformer, and thus the greatest energy transfer effected, this type of coupling is widely used.


Fig. 13: Circuits demonstrating base bias voltage stabilisation, (a) transformer coupling and (b) RC coupling.

As with valve-operated receivers intermediate frequency stages use transformer coupling, with the windings tuned to the appropriate frequency, as we shall see later. But for audiofrequency purposes coupling transformers are not so economical as resistor-capacitor combinations, and some efficiency is sacrificed to save costs.

Having laid the ground and, it is hoped, taken some of the fearsomeness from formulae, we shall proceed to a breakdown of some of the circuitry likely to be met in radio and audio gear, with a few notes on constructing both the simple circuits themselves in practical form and test devices that can help us handle transistors with more confidence.

## TO BE CONTINUED

> We regret that, due to shortage of space, several regular features have had to be held over. These will be resumed as soon as possible.


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The Modular Audio Mixing System is designed to allow any combination of signals to be mixed. The previous two parts have described some of the preamp. circuits and this final part concludes these and describes the final mixing and level monitoring arrangement

## MICROPHONE PREAMP (MIC Hi ZT)

This circuit shown in Fig. 19 is for microphones with built-in transformers or can be used with a microphone transformer at the input. The input impedance is about $100 \mathrm{k} \Omega$ and is suitable for microphone transformer secondaries, usually classified as medium to high impedance. The amplifier is a direct coupled BC109 pair with d.c. stabilization and negative feedback between the output and the emitter of Tr to set the gain. The circuit board layout is given in Fig. 20.

## PREAMP FOR CRYSTAL PICK-UPS

The requirements are a high input impedance and a sensitivity between 500 mV and 1 V r.m.s. The large


[^2] buill-in transformers.


Fig. 20: Layout for the circuit shown in Fig. 19.


Fig. 21 : Preamp. circuit for use with high output crystal pickups.
value series resistor and emitter follower input provide the high impedance input and the gain, and therefore input sensitivity, is set by negative feedback from the amplifier (Tr2) output to the circuit input. The nominal input sensitivity is 850 mV . The output network VR1 and R10 is again as common to all the preamplifiers. The circuit board layout is given in Fig. 22.

## PREAMPLIFIER FOR GUITAR (G)

Some guitar pick-up units have a high output and


Fig. 22: Layout for the crystal pickup preamplifier.


Fig. 23: The preamplifier circuit for use with low output guitar pickups.


Fig. 24 : The component layout for the guitar pickup preamplifier.
these could be connected to a line level input which, in conjunction with the line amplifier, has an input sensitivity of approximately 200 mV . Low output, medium impedance guitar pick-ups may provide signal levels from around 20 mV to perhaps 100 mV and require some amplification. The circuit given in Fig. 23 is quite a conventional arrangement originally due to Mullards and has provision for setting the

## components list

| Mic Pre-amp (Mic Hi ZT) |  |  |  |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| VR1 | 10k $\Omega$ | Car | log. pot. |
| Resistors |  |  |  |
| R1 | $220 \mathrm{k} \Omega$ | R5 | 220k $\Omega$ |
| R2 | $680 \Omega$ | R6 | 10k $\Omega$ |
| R3 | $1 \mathrm{k} \Omega$ | R7 | 22 k , |
| R4 | 39k $\Omega$ |  |  |
|  |  | All | \% types |


| Capacitors |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | $1.5 \mu \mathrm{~F}$ | 25 V | C 4 | $100 \mu \mathrm{~F}$ | 25 V |  |  |  |  |  |  |
| C 2 | $2.5 \mu \mathrm{~F}$ | 25 V | C 5 | $10 \mu \mathrm{~F}$ | 25 V |  |  |  |  |  |  |
| C3 | 100 pF |  | C6 | $1.5 \mu \mathrm{~F}$ | 25 V |  |  |  |  |  |  |

$\underset{T r 1, T r 2}{\text { Crystal }} \underset{\text { BCi09 }}{\text { p.u. }}$ Pre-amp (P.U. Xtal) VR1 $10 \mathrm{k} \Omega$ Carbon log. pot.
Resistors

| R1 | $470 \mathrm{k} \Omega$ | R5 | $1.5 \mathrm{k} \Omega$ | R9 | $820 \Omega$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R2 | $120 \mathrm{k} \Omega$ | R6 | $120 \mathrm{k} \Omega$ | R10 | $22 \mathrm{k} \Omega$ |
| R3 | $150 \mathrm{k} \Omega$ | R7 | $12 \mathrm{k} \Omega$ |  |  |
| R4 | $100 \mathrm{k} \Omega$ | R8 | $10 \mathrm{k} \Omega$ |  |  |
| All $4 \mathrm{~W}, 10 \%$ types |  |  |  |  |  |
|  |  |  |  |  |  |


| C 1 | $0.1 \mu \mathrm{~F}$ |  | C 4 | $100 \mu \mathrm{~F}$ |
| :--- | :--- | :--- | :--- | :--- |
| C 2 | $0.1 \mu \mathrm{~F}$ |  | C 5 | $1 \mu \mathrm{~F}$ |
| C 3 | $2.5 \mu \mathrm{~F}$ | $25 V$ |  |  |

Guitar Pre-amp

| Tr1, Tr2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| VR1 | $10 \mathrm{k} \Omega$ | BC109 <br> Carbon log. pot. |
| PR1 | $10 \mathrm{k} \Omega$ |  | | Carbon preset |
| :--- |

## Line Input

| VR1 | $10 \mathrm{k} \Omega$ |
| :--- | :--- |
| R1 | $22 \mathrm{k} \Omega\left(\frac{1}{2} \mathrm{~W}, 10 \%\right.$ type $)$ |

## VU Meter

 Type V403
## Henry's Radio

Insulated input jack or phono sockets as required.
overall gain from about 12 to 40 dB . This is controlled by PR1 which sets the amount of negative feedback between Tr2 collector and Trl emitter. With PR1 at maximum resistance the gain will be at 12 to 13 dB and about 40 dB with PR1 at minimum. The input impedance is typically $100 \mathrm{k} \Omega$ and suitable for the majority of medium to high impedance guitar pickups. PR1 should be adjusted so as to provide not more than the requisite 100 mV or so output between R8 and earth with VRl at maximum. The circuit board layout is given in Fig. 24.

## LINE LEVEL SIGNAL INPUTS

Line level usually refers to signals of over 100 mV or so which are linear i.e., requiring no equalization and no preamplification other than that necessary to bring the level to the requirements of the system output, in this case to a uniform 1V r.m.s. As no preamplifier is required, line level signals, such as from a radio tuner, tape recorder external amplifier output, etc., could be coupled directly to the line amplifier but as the outputs from other sources i.e., preamplifiers and/or other line inputs are also to be connected, the passive mixing component must be included to prevent any one signal source loading the others. Line level inputs are therefore connected to the line amolifier via a gain control and series resistor ( $22 \mathrm{k} \Omega$ ) in the same way as the output from each preamplifier is connected. This method is commonly used in signal mixing circuits so that any one signal source can be controlled independently of any other. The series passive component has been made high ( $22 \mathrm{k} \Omega$ ) compared with the gain controls, each of which are $10 \mathrm{k} \Omega$. The insertion loss is a little higher but the higher value series resistor ensures complete fadeout of the signal when a gain control is at minimum and that no loading is imposed on other mixing circuits. The circuit for the line inputs, as


Fig. 25: The resistive arrangement for the line inputs.
shown in Fig. 25 consists simply of the gain control and series resistor. Up to half a dozen line inputs can be used but more than this number could cause loading. If say, four or five preamplifiers were used, then the number of line inputs should be limited to three or four. Much the same applies to the total number of preamplifiers e.g., six should be about the limit with two line inputs.

## VU LEVEL METERS

VU meters with built-in rectifiers are readily available and most of these will read well over full scale with a lV r.m.s. signal. This allows a VU meter to be connected across the line amplifier output with a series variable resistor so that the meter can be adjusted for a maximum signal indication of 1 V r.m:s. equals 0 dB . The meter could also be adjusted to read in conjunction with a tape recorder level meter in cases where the mixer is remote from the recorder. The connection is simple enough as shown in Fig. 26 but note that the meter must be one with a built-in rectifier and provide full scale deflection for at least 600 mV of signal.

## GENERAL APPLICATIONS

As already mentioned in Part 1, the various preamplifiers, tone control unit and line amplifier can be connected together to provide signal mixing facilities for sound recording, public address and


Fig. 26: (left) The VU meter arrangement.
Fig. 27: (right) The arrangement for feeding more than one amplifier.
discotheque or music amplification systems. The high signal output of around IV r.m.s. is sufficient to directly drive many power amplifier modules now available so in fact a complete multi-channel amplifier system is perfectly feasible. The various combinations given in the block diagram in Part 1 are but a few of the possibilities and any combination can be extended for stereo operation simply by duplication. For stereo mixing systems ganged gain and tone controls are not necessary, in fact separate controls are advisable, as they allow much more control over stereo balance. The output from the line amplifier can be coupled to more than one amplifier or tape recorder simultaneously or for example to a tape recorder and an amplifier for simultaneous recording and monitoring. As the input impedance of external equipment may yary, external equipment connections should be made via series resistors as shown in Fig. 27. Normally each resistor can be $47 \mathrm{k} \Omega$ but this may be reduced to as little as $10 \mathrm{k} \Omega$ if the higher value reduces the output signal too much as it may do if external equipment has a very low input impedance.

## LAYOUT IN CABINETS

The photos shown in the previous parts are of a small mixing system which would be ideal for tape recording enthusiasts and, as can be seen, each of the preamplifiers are simply mounted side by side. The built-in screens prevent crosstalk and shield the boards from hum pick-up. Nevertheless a metal cabinet should be used for any system derived from the various modules. The mains power supply should be situated away from the preamps and preferably in a screened compartment.


Last month's Fig. 12 (page 619) showed the incorrect layout. The correct layout for the crystal mic. preamp. circult Is shown above.


THE completed keyboard is mounted in a tilted position as in Fig. 9b on a hardboard base that fits into the top of the organ. This base also carries the circuit board and battery etc. The piece of hardboard is cut as in Fig. 9a and the keyboard mounted as in Fig. 9b so that the keys themselves are


Fig. 9: Details of the keyboard mounting.



Fig. 10: A front view of the keyboard mounting and the siting of the upper front panel.
level. It is important that when the completed keyboard is fitted in the top of the case that the front of the keys are aligned with the top of the upper front panel as shown in Fig. 9c and also in Fig. 10 so that when a key is depressed the top does not come below the upper edge of the panel. When the keyboard has been correctly aligned it can be secured in the organ cabinet.

The lid of the organ is made up as shown in Fig. 11 and in the photo. Appropriate dimensions for the lid are best derived from the inside measurements of the top of the case and the height of the keys but the lid must be made so that the centre portion drops directly behind the black keys. The whole of the lid is hinged on the rail at the rear of the cabinet. Figure 11 also shows more detail concerned with the expression pedal system. Ensure that when the lid is closed down it does not foul the keys and that all the keys can be depressed and will return to their rest position.

At this stage the painting might well be done but first the keyboard and the main front panel should be removed. If a music stand is to be included this should be fitted and can be made from a piece of hardboard about $12 \times 7 \mathrm{in}$. attached to the lid by a

short length of $1_{2} \times{ }^{1}$ in. batten. The original organ was finished with a bright red gloss paint over an undercoat of emulsion paint.

When the decor is complete the loudspeaker can be installed and the expression pedal (if used) adjusted. The on/off, vibrato and voice switches can be fitted to the left hand portion of the lid and a back cover made up of hardboard to close in the rear of the organ. Two small wood blocks should be fitted inside, one either side of the keyboard, and flush with the upper front panel. These act as stops when the lid is closed down and take a screw through each side of the lid so that it can be secured against opening by small hands. These blocks are just visible in the photograph.

The component board is mounted just behind the key contact frame as shown last month - and allows for convenient short connections between the tuning pre-sets and the key contact wires. A rear view of the completed organ with the circuit board in position is shown.

## TUNING

First adjust all the pre-sets, including PR1, to midway travel and set Sl, the vibrato switch, and S2, the voice switch, so that both are open. Tuning is best done with a piano and should be commenced with the pre-set for the F key (No. 25) at midway. Now tune the $F$ note to pitch at $698 \cdot 4 \mathrm{~Hz}$ with PR1, the initial pitch control. The remainder of the presets from E No. 24 down to F No. 1 at $174 \cdot 6 \mathrm{~Hz}$ can now all be tuned one after the other.

The vibrato should produce a pleasant pitch variation, not too pronounced, at about 6 to 8 Hz . The intensity of the vibrato can be increased by reducing R14 to $100 \mathrm{k} \Omega$ or decreased by making R14 about $150 \mathrm{k} \Omega$. The vibrato frequency can be altered by slightly increasing or decreasing the value of R 2 . With the voice switch S 2 closed, the tone should be flutelike and somewhat softer.

The expression pedal will reduce the sound level somewhat but if moved up and down quickly whilst


A rear view of the completec project with the back removed.
a note is sustained will produce a pronounced "wahwah" effect which will no doubt intrigue the junior player.

The organ will stay in good tune for a long time, or until the battery voltage falls and the two octave range allows for the playing of a wide range of tunes. Like the author's grandson who inas become the final owner of the prototype, any youngster will get a great deal of enjoyment from it.

In the circuit of the 2-octave minialure organ published last month (Fig. 1, page 594) there is an error in the multivibrator circuit. C6 should connect between the collector of Tr2 and the base of Tr3 and not between the bases as shown. In Fig. 2 the resistor next to R1 should read R14 and not R13 as shown.

## DIGITAL FREDUENGY COUNTER/TIMER



## PART 4 (continued from the November issue)

Frequency measurement is the primary purpose of the instrument and although, on low and medium frequency signals of a reasonable amplitude, it is sufficient to connect the signal and read away, better results may be obtained particularly on the higher frequencies if the controls are set correctly.

It should be remembered that the purpose of the input clipping stage is to provide, from the input signal, a clean squarewave suitable for driving the signal gate and decade counters.

With the input switch in the "AC" position the input a.c. signal can be "slid up and down" the input characteristic of $\operatorname{Tr} 1$ by rotating the LEVEL control, so that symmetrical clipping takes place.

The smaller the input signal and the higher the input frequency the more important it is to set the LEVEL control correctly.

With the signal applied to the input and the function control set to a low frequency range, the LEVEL control should be carefully rotated from one end to the other and the range noted over which a steady reading is obtained. The correct setting is in the centre of this range (see Fig. 19).

The actual physical position of the control depends to a large extent on the individual characteristics of Trl. (It may be possible to substitute other types of f.e.t. in place of the 2 N 3823 but the spread of characteristics may make the LEVEL control inoperative.)

It is assumed that normally the signal to be measured will be clean and free from hum and noise. However, if a large amount of hum (mains ripple) is present on the signal to be measured this may cause errors due to the clipper stage being saturated for periods of the hum waveform, as shown in Fig. 20.

A solution to this problem is to use a simple high pass filter, as shown, which will effectively remove the low frequencies whilst allowing the r.f. signal to pass through.

## IIIII IIIII <br> IIIIIII <br>  J.THORNTON-LAWRENCE GW3JGA

Assuming that the LEVEL control has been set to its optimum position, the function switch should then be rotated to a position where the first digit of the displayed reading appears on the left hand tube.

Suppose that a signal of $7 \cdot 054321 \mathrm{MHz}$ is being measured, the reading of frequency should be 7.054 MHz . Setting the function switch to the highest frequency range will cause a reading of $07 \cdot 05 \mathrm{MHz}$ to be displayed and obviously the frequency is not being measured as accurately as it can be.

Conversely, by moving the function switch the other way to a lower frequency range, the 7 disappears off to the left and a reading of 0543 is displayed.

This procedure may be repeated until in the Hz position the reading will be 4321 , the right hand figure indicating cycles per second and the left hand figure indicating kHz .


Fig. 19 : Waveforms showing correct and incorrect settings of the LEVEL control.


Fig. 20 : Effects of hum and noise on the input signal. A simple high pass filter is shown on the right.

This is a useful facility for measuring small changes in frequency, e.g. checking variable frequency oscillators, frequency modulation systems, and monitoring the frequency of a signal generator when aligning the i.f. stages of a receiver and checking crystal filters.
It is important to remember that whilst this measurement gives very high discrimination it is only a relative measurement of frequency and is not an absolute measurement to this accuracy. The stability of the internal crystal oscillator is insufficient for this to be so.

## Calibration Outputs

The $100 \mathrm{kHz}, 10 \mathrm{kHz}$ and 1 kHz outputs at the rear of the instrument may be used for calibrating receivers. This can be done by loosely coupling the appropriate output to the input of the receiver. A series coupling capacitor and resistor of about $1,000 \mathrm{pF}$ in series with $1 \mathrm{k} \Omega$ should be used as each output is directly connected to the divider circuits and an accidental short to earth or worse still to a high voltage would upset the operation of the divider and may cause permanent damage.

## Time and Period Measurement

The simplest time measurement for the instrument to make is in measuring the time of one cycle of a repetilive waveform. This is useful for frequencies below 100 Hz as greater accuracy can be obtained.

On the time ranges of the instrument, the counting is initiated by the negative going part of a signal and slopped by the next negative going signal. The operation on various waveforms is shown in Fig. 21a, b and c.


Fig. 21: Operation of various timing waveforms. Circuit on the right provides a fast negative going pulse when S1 is closed.

For the timing of events, as an electronic stop watch, it is necessary to provide a circuit which will generate a fast negative going pulse when a button is pressed. A suitable circuit is shown in Fig. 21d.

The luF capacitor Cl is normally charged to +5 volts through Rl. When the microswitch is pressed a sharp negative going voltage step is pro-
duced which starts the timer counting time. The switch is released and R1 recharges C1. When the switch is pressed for the second time the negative pulse stops the count and the total time between the two operations is displayed in mS or seconds depending on the setting of the function switch. The purpose of Cl is to prevent the contact bounce in SI from causing false triggering of the instrument.
For actomatic operation, two photocells may be used and a suitable circuit for timing the duration between two events is shown in Fig. 22.


Fig. 22 : Circuit shown above is suitable for automatically timing the duration belween two events.

An extension of this system with more powerful light sources may be used for race timing, horse trial events, etc.

In the above applications of start-stop pulses it is suggested that the input switch is set to the "AC" position and that the LEVEL control is adjusted to the position which gives reliable operation, this is usually slightly higher (clockwise) than the centre operating point used in frequency measurements.

## Very Low Frequency Input Signals

For very low frequency signals where the input coupling capacitor may attenuate the signal severely the input switch may be used in the "DC" position. This may result in the LEVEL control having little or no effect. However, if the input signal has an amplitude of about 10 volts peak to peak about earth potential, reliable operation of the instrument should be obtained.

The integrated circuits used in the Digital Frequency Counter Timer are the 74 series of TTL (Transistor-Transistor Logic) in the 14 and 16 pin DIL (dual in line) package. The device operates from a supply of +5 volts ( $4 \cdot 5 \mathrm{~V}$ min., $5 \cdot 5 \mathrm{~V}$ max.).

In the operation of the logic only two states are possible, 0 and 1 .
logic $0=$ "low" $=$ less than $+0 \cdot 8$ volts.
$\operatorname{logic} 1=$ "high" = greater than $+2 \cdot 0 \mathrm{volts}$.

## 7400N Quadruple 2 Input Nand Gate

This device contains four separate identical two input NAND (NOT AND) gates, as shown in Fig. 23.

| 2 inpart NAND gate | Truth tabie |  |  |
| :---: | :---: | :---: | :---: |
|  | Input 1 | Input 2 | Output |
|  | Low | Low | High |
| tput | High | Low | High |
| nut | Low | High | High |
| 1105] | High | High | Low |



Each gate has two inputs and one output and the operation is shown in the truth table. It can be seen that only when input 1 AND input 2 are high will the output NOT be high, i.e. low. In the circuit of the instrument some gates are shown with only one input and here the other input is left disconnected. This is equivalent to connecting it to a high input. In this condition the gate becomes an invertor, the output condition is the inverse of the input.

## 7473N Dual Master-Slave J.K. Flip Flops

The SN7473N contains two Master-Slave J.K. Flip Flops, each flip flop contains a large number of gates all internally connected to form a bi-stable or flip-flop in which the state of the outputs for specific input conditions is clearly defined. This is shown in the truth table in Fig. 24. What this means is that if $J$ and $K$ are both low, no change takes place during the clock pulse. But if K is high and $J$ is low the clock pulse will cause Q to go low and conversely if J is high and K is low the clock pulse will cause $Q$ to go high. And finally if $J$ and $K$ are both high $Q$ will change state at each appearance of the clock pulse. With $J$ and $K$ both high the circuit makes a divide by two divider stage, the output from $Q$ being half the frequency applied to CP.


| Truth table |  |  |
| :---: | :---: | :---: |
| $t_{n}$ |  | $t_{n}+1$ |
| $J$ | $K$ | 0 |
| Low | Low | $Q_{n}$ |
| High | Low | High |
| High | High | $\bar{Q}_{n}$ |

$t_{n}=$ bit time betore clock pulse $t_{n}+1=$ bit time atter clock pulse
Clock input waveform
01031


Fig. 24 : SN7473N integrated circuit and truth table. The sequence of operation relative to the clock waveform is also shown.

In the master-slave JK flip flop, the input to the master section is controlled by gates operated by the clock pulse. The clock pulse also regulates the state of more gates which connect the master and slave sections. The sequence of operation, relative to the clock waveform shown in Fig. 24, is as follows:

1. Isolate slave from master.
2. Enter JK input information into master.
3. Disable input gates.
4. Transfer information from master to slave.

The input C is a direct clear input which restores Q to low irrespective of any other input signals., opposite logic condition to $Q$.
instrument is in storing information and transferring this on the application of a pulse to the clock pulse
$\bar{Q}$ is the reciprocal of $Q$ and always has the
The use of the Master-Slave JK Flip Flop in the input.

## 7490N Decade Counter

The SN7490N contains 4 flip-flops and 3 gates forming a divide by 2 stage and a divide by 5 stage.

When used as a binary coded decimal counter, the signal input goes to the divide by 2 stage and from the output of this to the divide by 5 stage. The binary coded decimal output is then available as shown in Fig. 25.

When used as a frequency divider, as in the Crystal Oscillator divider panel, it is more convenient to feed the signal into the divide by 5 stage hrst and then the divide by 2 stage, this ensures a $1: 1$ square wave output which has certain advantages when used as a calibrator output. The other arrangement


Fig. 25 : SN7490N integrated circuit used as a binary coded decimal counter.
will of course also divide by 10 but the output waveform is far from symmetrical. The SN7490N has input connections for resetting to " 9 " or " 0 " and in the instrument only the reset to " 0 " is used.

## 74141N B.C.D. to Decimal Decoder Driver

This device contains a complex arrangement of gates terminating in ten high voltage transistors for driving the numeral indicator tube. The operation of this device was illustrated in Part II of this series (Fig. 9, page 480, October 1971 issue).

A number of queries have been received regarding the use of a SN7441AN device in place of the SN74141N. The SN7441AN was in fact used in the prototype and whilst a number of these functioned satisfactorily a few gave trouble by loading the decade counter excessively and causing an incorrect count.

The SN74141N is an improved version of the original SN7441AN.

B.B.C. RADIO LONDON<br>Sunday, November 7th at 3 p.m. on $95 \cdot 3 \mathrm{MHz}$.<br>"Don't call us 'hams'!"<br>featuring radio amateurs of London, with Sylvia Margolis, past P.R.O. of the Radio Society of Great Britain NE of the attractions of medium wave DXing is its unpredictability, a feature which is very apparent when the listener searches for North American DX. Although reception conditions can vary considerably from night to night, there is also a long term trend which follows the sunspot cycle; the best medium wave DX occurring in years of low sunspot activity. We are now well past the maximum of the current sunspot cycle and can expect an allround improvement in long range reception on ni.w.

Last month it was suggested that the newfomer to MW DXing should listen on 1070 kHz after 2300 hrs for the Canadian CBA located at Moncton, New Brunswick. Other North Americans that are frequently heard in this country during the early part of the night are CNB 640 kHz in St. John's, Newfoundland; WNBC 660 kHz in New York City; WABC 770 also in NYC; WHDH 850 in Boston; CBH 860 in Halifax, Nova Scotia; WABI 910 in Bangor, Maine; CJCH 920 Halifax, N.S.; CJON 930 St. John's; CHER 950 Sydney, N.S.; WINS 1010 NYC; WBZ 1030 Boston; WBT 1010 Charlotte, North Carolina. An unusual catch is Radio St. Pierre 1375 kHz situated at St. Pierre, the capital of the French islands of St. Pierre et Miquelon, located to the south of Newfoundland. When conditions are favourable R. St. Pierre will cause a heterodyne on Lille 1376 kHz before the latter closes down for the night at 2300 hrs .

Harold Emblem, of Mirfield, Yorkshire, has received a verification from the new station at Kinshasha ( 692 kHz ). This is a difficult country to verify and the address for reception reports is Chef des Services Techniques, Radiodiffusion Nationale Congolaise, Kinshasha, Republique Democratique du Congo.

Reception of Far Eastern medium wave stations is possible in the U.K. during the afternoon in winter time. Stations fade-in about one hour before sunset and are audible either until they sign-off or they become submerged in interference from Europeans, which increases as darkness approaches. The $1,000 \mathrm{~kW}$ All India Radio outlet at Calcutta on 1130 kHz which broadcasts in English from 1530 until 1600 hrs was heard frequently last winter. It is easy to pass over this station as it suffers from slow cyclic fading, so it is worth while pausing on the frequency for a few minutes. The Voice of America, Okinawa 1178 kHz is another megawatter that is often heard in this country, usually as a background to the Swedish broadcaster on the same channel. Programmes from Okinawa are in local languages but identification is on the hour and half hour usually in English and is accompanied by the Yankee Doodle signature tune. Sign-off is at 1700 hrs . Peking has been logged on $1,000 \mathrm{kHz}, 1230 \mathrm{kHz}$ and 1290 kHz ; Taiwan (Formosa) has been heard on 750 kHz and 1200 kHz with programmes of westernised Chinese music while Kabul, Afghanistan 1280 kHz is a regular until close down at 1830 hrs .

Reports to 132 Segars Lane, Southport PR8 3JG.


## NEWS FOR

 DX LISTENERSDURING the past few months I have received many letters asking the correct way of converting metres into kilohertz. It would appear that many readers have receivers which are calibrated in metres only.

The conversion is performed as follows: In order to obtain the frequency in kHz divide 300,000 by the wavelength in metres. This formula also works in reverse, that is: wavelength in metres can be obtained by dividing 300,000 by the frequency in kHz .

The first report this month comes from Paul Benton of Hednesford who has an Astrad-Nova receiver. Paul's aerial system consists of a 75 foot long-wire, a 14 -element television aerial and a copper grid. Items from his log include:
4783 Radio Mali, in French at 2145.
4800 Radio Lara, Venezuela, music at 2330.
4900 R. Juventud, Venezuela, music at 0000.
4900 R. Conakry, Guinea, news in French at 2300.
4940 R. Abidjan, Ivory Coast, French at 2250.
5015 Windward Islands B.S., English at 2345.
5035 R. Bangui, Cent. Afr. Rep., English at 2045.
5047 R. Lome, Togo, African music at 2100.
11652 R. Pakistan, Karachi in English at 2030.
11815 HCJB, Quito, Ecuador in English at 0040.
11855 Saudi Arabia in English at 0430.
Stephen John Mathews of Hull has a new receiver, the Trio 9R-59DS, but having broken his leg playing football he has to be content with his 90 foot loft aerial instead of the new one which he was going to erect. The combination yielded some interesting stations including:
2326 S. African B.C. in English at 0030.
4777 R.T. Gabonaise in French at 0000.
4800 R. Lara, Venezuela in Spanish at 0400.
4880 R. Universo, Venezuela, Spanish at 0045.
4955 R. Nacional, Colombia in Spanish at 0315.
5960 Voz de Angola in Portuguese at 2015.
15170 ELW A, Liberia in French at 2020.
15200 NBC, Lagos, Nigeria, English at 1830.
15280 4VEH, Haiti in English from 2330 to 0200.
15415 FEBA, Seychelles, testing at 1855.
15485 R. Portugal Libre, clandestine at 1922.
Peter Reed of Brighton has used his R1155N receiver in conjunction with his Joystick antenna to log some interesting stations which include:
3380 Malawi B.C. in English at 2000.
4805 Voice of Kenya, Nairobi, 1800-1845.
4875 R. La Cruz del Sur, Bolivia, Spanish at 1100.
5040 R. Burma noted at 1445.
9520 R. La Cronica, Peru, Eng. and Sp. at 1200.
11825 Papeete, Tahiti in French at 0755.
21685 Kuwait B.S. in Arabic at 1300-1330.
Ross Pullen of Crawley has sent in a log which includes the following interesting stations:
5970 R. El Sol, Peru in Spanish at 0200.
9670 Saudi Arabia in Arabic at 2215.

## THE BROADCAST BANDS Malcolm Connah

## Frequencies in kHz - Times in GMT

## 9725 R. Burma in English at 0700.

11715 R. Republik Indonesia in English at 0900.
11875 R. dif. Nacional, Nicaragua at 0200.
Julian V. Moss of Rayleigh, Essex has just purchased a Meridian receiver and a 50 foot long-wire enabling him to hear:
6050 HCJB, Quito, Ecuador in German at 0615.
6080 R. Berlin Int. in French at 2100.
7280 R. Berlin Int. in English at 2045.
9530 AIR, Delhi in English at 2100.
9550 R. Warsaw, Poland in English at 2030.
9700 R. Sofia, Bulgaria in English at 1935.
9765 Deutschewelle in English at 2150.
11620 AIR, Delhi in English at 2030.
11672 R. Pakistan, news in English at 1900.
11700 R. Kiev, Ukraine in English at 1945.
11740 R. Australia in English at 1610.
11755 Finnish B.C. in English at 1000.
11765 R. Australia in English at 0800.
11800 RAI, Rome in English at 1940.
11910 Radio Budapest in German at 2010.
Fred Wall of Walthamstow, London E. 17 used his homebrew 4 -valve superhet and a 20 foot long-wire aerial to hear the following stations:
7290 TWR, Monte Carlo at 1600.
9555 Finnish B.C. at 1815.
9620 R. Belgrade, Yugoslavia, English at 1942.
11745 HCJB, Quito, Ecuador at 0015.
11765 R. Australia with news at 0900.
11790 R. Afghanistan, news in English at 1800.
15345 Kuwait B.S. with news at 1830.
17820 RSA, S. Africa with news at 1845.
21640 NHK, Japan with music at 1518.
25900 R. Norway in Eng./Nor. at 1820.
Robert C. Hanstock of Sheffield has a Colombia 5 -valve superhet and a 50 foot long-wire which enabled him to hear:
5980 RSA, S. Africa in English at 1815.
7205 R. Australia in English at 1600.
9010 R. Peking in English at 2045.
9740 Radio Portugal in French at 0700.
Robert also reports that Radio Nederland is to open a new relay station at Tananarive, Malagasy in November. Programmes will be beamed to Africa and S. Asia. The station will also be changing the frequencies of its evening transmission in English to Europe; the new frequencies being 17830,6085 and 6020 from 1830 to 1950 .
D. A. Hairon of St. Clement, Jersey is now using a 100 foot long-wire with his other equipment and reports hearing:
9740 R. Cairo in English, 2245-2300.
11730 R. Nederland, Bonaire in Eng. at 0630.
11795 R. Nacional, Rio de Janeiro at 0055.
11865 R. Clube, Brazil at 0200.
21705 R. Mexico in Spanish at 2205.
Reports should arrive by the 15th of the month and be addressed to me at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex.

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IRST letter out of the hat this month is from Peter Short (ZS2HT). He remarks on comments made in an earlier Amateur Bands regarding ZS1MH. Peter says that the latter station has managed over 1,000 contacts on $3 \cdot 5 \mathrm{MHz}$ notching up 115 countries. Gear is a KW Atlanta and a G8KW antenna at 175 ft . Apparently ZS1MH will be using a 66 ft . loaded vertical early next year and has plans to have a 2 -element beam for 3.5 MHz up by next March. Peter says also that there is intense ZS activity on both $3 \cdot 5$ and 7 MHz between 0400 and 0600 g.m.t. Listen 7090 to 7100 kHz and from 3730 kHz upwards.

A shout from Des Walsh (EI5CD) of Co. Tipperary. He asks for s.w.l's who can QRX on 2 metres to listen out for his a.m./f.m. sigs on the following freqs.: $144 \cdot 7,144 \cdot 9,145 \cdot 35$ and $145 \cdot 96$. Des runs 8 W output to a 6 -over- 6 and is on most weekends beaming eastwards.

The aerial is 67 ft . wrapped neatly around a first floor flat in Cambridge. The receiver is a "modded" HRO-MX and the log from M. Wallace is for 3.5 MHz s.s.b.; HA0KHT, WA80BG, ZB2CC, ZL3LE, ZL4JW.

Listen after 0100 b.s.t. around $7 \cdot 2 \mathrm{MHz}$ for KP4GL who m.c's the Caribbean net, advises Paul Edwards (Penge). Paul's antenna is. 120 ft . "bent round the garden" and the Rx is a homebrew 1-V-1. Log for 7 MHz reads; CN8HD, CT1GQ, CT2AK, EA7EU, FM7WN, K4UAS, KP4DHD, KP4GL, KZ5JF, PJ2CW, PY3APH, PY7BIH, VP7DL, W1YNQ, W2RGV, W3LTU, WA2BVU/4X, YV1BI, YV5BPG, ZL2BT, 4Z4JT, 8P6AJ.

John Brockett (Hemel Hempstead) has a homebrew transistor superhet which is working on 160 and 80 metres. Best on 160 to date is GM3SVK/A in the Shetlands. On 80, John bagged many EUs plus JY9DX, OD5BA, VE10W, VO1FG, 3V8ZK and 5H3LV.

Peter West (Leigh, Lancs), reckons midnight to 0700 for 7 MHz DX. Proof of the pudding comes from Peter's $\log$ for that band gained with the aid of a TCS -9 receiver and 132 ft . end-fed (all s.s.b.); CM3LN, EA3LP, EA6BH, K4ELK, K4PTK, PY2ASY, PY7AJB, PZ1CV, W1EEF, W2BMK, W3WGH, W4CVS, YV4BE.

Talk about UX logs, I gotta DX letter. Epistle from Karl Muller of Mbabane, Swaziland, uses a Philips domestic portable and the oscillating detector of a homebrew t.r.f. as a b.f.o. Karl stalks 40 metres with this little lot and reports squeaks of activity from: CR7FM, CR7BN, DK2EQ, DJ9JF, EI8H, ET3ZU/A, G8NV (that's DX to Karl!), GM3JDR, HA3GR, HB9AGN, IT9FG, JA0BCO, JA1BK, JA2BUX, JA3LU, JA4IWD, JA5BLH/MM, JA6FT, JA7DCK, JA9YBA, JH1EDB, JW1EE, K4THA, K6DC, K6DV, KH6RS, LZ1KVV, OK2BM, OH5UQ, SM5EXE, thousands of "U" stations.

David Lawley (Gravesend) CR100, a wide variety of antennas, has been doing a spot of all-band listening. Topband $\log$ includes; GI3ZIA, GM3WDF and GW3UMB. Up to $3 \cdot 5 \mathrm{MHz}$ and a QRX revealed; C'Г1BT, EI3S, GC3MDX, OY7JD, PY7AF, VO1FX,

# THE AMATEUR BANDS David Gibson, G3JDG Frequencies in kHz - Times in GMT 

V01FG and YK1AA. On 40 metres, David's best were; OZ9HG (Langeland Island) and TI2IT.

Without doubt the award for the best kept log of the year goes to Adrian Barnes of Abingdon, Berks. This was laid out neatly and ledgibly in columns making it easy to read. All the information was included; callsign, mode, frequency, date, time, country etc. No local stations were listed, no Eu stations either, just some 175 DX stations. A sample from this superb 14 MHz s.s.b. $\log$ reads; AP2AD, CE3FM, CN8BB, CP1BG, CR5SP, CT1BT, EL2BA, EP2JA, ET3ZU, HC1M, HI1AGS, JY9DK, KH6CD, KP4FS, KZ5JW, LU2AGE, OA1BU, OA6BGI, PJ0PM, PY2FIQ, TI2FKB, VA2UN (special station in Montreal), fourteen VEs, VK1BT, VK2APK, VK3BCM, VK4CZ, VK4PV/P, VK5GX, VK60V, VK7RX, VK9CD, seventy Ws, XE1IIJ, YB5BFK, YN2OM, YV1ACI/P5, YV4YC, YV5CKR, YV6EE, ZA2BE, ZB2A, ZC4LC, ZE1CW, ZL2BGV, ZL3GO, ZL4AW, 3A0FX, 3V8ZK, 4X4JL, 4Z4DZ, 5Z4LW, 6Y5GA, 7X2BK, 9H1BG, 9M2LP, 9Q5RN, 9V1QJ, 9Y4CP.

Irwin Brown (Co. Antrim), has a JR-310 and a dipole at 30 ft . Log of s.s.b. from 14 MHz which was heard in the Emerald Isle includes; AP5HQ, EA6BM/ M, ET3ZU/A, HI8LA, VE1CW/M, VQ9YL, YA2DD, YB3AAY, ZK1CD, ZM7AG, 5K5LR, 5Z5KL.

Philip Cross (Preston) has an HRO-MX and a dipole cut for 14 MHz . Log of s.s.b. reads; CN8GC, CR5SP, CR6IC, ET3ZU/A, FP9AR/M, HP9ARZ, HV3SJ, JA6YUV, JX1AK, JY1, LU2ECO, M1B, MP4TDM, OD5GC, PZ1DR, VQ9XX, VP9BN, ZE1CY, ZS3KC, 3A2CP, 3V8ZK, 7X2BK, 7Z3AB, 9K2BG, 9J2ED, 9X5AA, 9Y4VV.
"I'm now working hard trying to learn c.w," says Alan Smith (Nelson). "Good lad," says David Gibson (Harpenden). Alan uses a Koyo KTR 1662 receiver and 25 ft . of wire. Not an elaborate set up, but enough to hear some 14 MHz s.s.b. from; EA6BU, HC1KH, HK3BN, KZ5IK, KP4BJD, PJ9AD, PZ1AY, VE3CNE, YB5FB, YV5AXT, 6Y5SR, 9Y4VV.

An ECC83 and ECL82 (leaky grid detector and a.f. amp), is the homebrew receiver of John Runchman (South Norwood). On 20 metres, with the aid of a dipole, John bagged; HK3UY, sixteen Ks, LU4ECO, PY2CAQ, VE1IJ, VP2LY, thirty Ws, YN1ABD, YV4UA, ZP5AN, ZL3AA, 4X4AE, 4Z4QAM, 6Y5GA, 9 HlM , which is pretty good going for two valves.
P. Harris (Surbiton) RA-1, dipole, got these on 28 MHz ; LU3DTV, LU6DRB, PY2HT.

Goings on for contest-types at this time of the year includes: November $6-7,144 / 432 \mathrm{MHz}$ c.w. contest; 6-7, 40 metre phone contest; 6-8, CHC/FHC phone/ c.w. contest; 13-14, topband contest; 14, OK contest; 27-28, CQ WW d.x. c.w. contest. December 5, 2 metre contest.

Logs, in alphabetical order please, to arrive by the 15th of the month to:

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$4 / 350 \mathrm{~V}$ \& 14 p \& $500 / 25 \mathrm{~V}$ \& $\cdots$ \& 20 p \& $50+50 / 350 \mathrm{~V}$ <br>
$8 / 450 \mathrm{~V}$ \& 14 p \& $1000 / 25 \mathrm{~V} .$. \& 35 p \& $60+100 / 350 \mathrm{~V}$

 

$1 / 450 \mathrm{~V}$ \& 14 p \& $1000 / 25 \mathrm{~V} \ldots$ \& 35 p \& $60+100 / 350 \mathrm{~V}$

 

$16 / 450 \mathrm{~V}$ \& 1 p \& $1000 / 50 \mathrm{~V}$ \& 47 p \& $32+32 / 250 \mathrm{~V}$ <br>
$32 / 450 \mathrm{~V}$ \& 20 p \& $8+8 / 450 \mathrm{~V}$ \& 18 p \& $32+32 / 450 \mathrm{~V}$

 

\& $8+8 / 450 \mathrm{~V}$ \& 18 p \& $32+32 / 450 \mathrm{~V}$ \& 33 p <br>
$25 / 25 \mathrm{~V}$ \& 10 p \& $8+16 / 450 \mathrm{~V}$ \& 20 p \& $350+50 / 325 \mathrm{~V}$ \& 50 p

 

$25 / 25 \mathrm{~V}$ \& 10 p \& $8+16 / 450 \mathrm{~V}$ \& 20 p \& $350+500 / 325 \mathrm{~V}$ <br>
$50 / 50 \mathrm{~V}$ \& 10 p \& $16+18 / 450 \mathrm{~V}$ \& 25 p \& $82+32+32 / 350 \mathrm{~V}$ <br>
\hline 13 p
\end{tabular} $100 / 25 \mathrm{~V} \quad 10 \mathrm{p} \quad 32+32 / 350 \mathrm{~V} \quad 25 \mathrm{p}: 100+50+50 / 350 \mathrm{~V} 48 \mathrm{p}$ SUB-MIN. ELECTROLYTICS. $1,2,4,5,8,16,25,30,50,100$, $200 \mathrm{mF} 15 \mathrm{~V} 10 \mathrm{p} ; 500,1000 \mathrm{mF} 12 \mathrm{~V}$ 18p; 2000mF 25 F 35p. CERAMIC 1 pF to 0.01 mF .4 p . Silver Mics 2 to $5000 \mathrm{pF}, 4 \mathrm{p}$ PAPER $350 \mathrm{~V}-0.14 \mathrm{p}, 0.513 \mathrm{p} ; 1 \mathrm{mF}$ 15p; 2 mF 150 V 15 p . $500 \mathrm{~V}-0.001$ to $0.054 \mathrm{p} ; 0.15 \mathrm{p}, 0.258 \mathrm{p} ; 0.4725 \mathrm{p}$. SILVER MICA. Close tolerance $1 \% 2 \cdot 2-500 \mathrm{pF} 8 \mathrm{p}$; $500-2 \cdot 200$ pF 10p; 2,700-5,600pF 20p; 6,800pF-0.01, mid 30p; each. TWIN GANG. "0-0"' 208pF +176 pF , 65p; Slow motion drive $365+365$ With $25+25 \mathrm{pF}, 50 \mathrm{p}$ 500pF slow motion, standard

$45 \mathrm{p} ; \operatorname{small} 3$-gank 500 pF \&i $\cdot 60$. SHORT WAVE. Single 25 pF 55 p SHROME TELESCOPIC AERIAL, swivel base, 23in. 20p. CHROME TELESCORIC AERIAL, sWivel bsac, 23in. 20p TRIMMERS. Compression $30,50,70 \mathrm{pF}, \mathrm{Sp}_{\mathrm{p}} ; 100 \mathrm{pF}, 150 \mathrm{pF}$. $8 \mathrm{p} ; 250 \mathrm{pF}, 10 \mathrm{p} ; 600 \mathrm{pF}, 10 \mathrm{p} ; 750 \mathrm{pF} 10 \mathrm{p} ; 1250 \mathrm{pF} 10 \mathrm{p}$. SILICON REC. 40 -LUCAS 2DS500 Bridge 70 V 5 amp 81 RECTIFIERS CONTACT COOLED + wave 60 mA 38 p 85 mA 48 p . SILICON BYZ13 30p; BY1 00 30p; BY187 30p. EX-GOVERNMENT RECTIFIERS $250 \mathrm{v}, 200 \mathrm{~mA}, 30 \mathrm{p}$. NEON PANEL INDICATORS 250V AC/DC Red or Amber 20p RESISTORS, $\frac{1}{2}$ W., $W$., $20 \% 1 \mathrm{p}: 2 \mathrm{w} .5 \mathrm{p} 10 \Omega$ to 10 M . IIGH STABILITY. W. $2 \%$ ohms to 10 meg-, 10 p Ditto $5 \%$ Preferred values 10 ohms to 10 meg., 4 p ,
WIRE-WOUND RESISTORS 5 watt, 10 watt, 15 watt, 10 ohms to $100 \mathrm{~K}, 10 \mathrm{peach} ; 2 t$ watt, 1 ohm to 8 ohms 10 p


## MAINS TRANSFORMERS ${ }^{\text {ALL PosT }}$

 $250-0-25080 \mathrm{~mA} .6 .3$ จ. $4 \mathrm{smp} . . . . . . . . . . .$. $250-0-25080 \mathrm{~mA} .8 .3$ v. 3.5 a .8 .3 F .1 a. or $5 \mathrm{\nabla} .2 \mathrm{a}$. 82.00 $350-0-35080 \mathrm{~mA} .6 .3$ จ. 3.5 a. 6.3 \%. 1 a. or 5 F. 2 a . 82.00 MINIATURE $200 \% .20 \mathrm{~mA}, 6.3$ v. $1 \mathrm{a} .21 \times 21 \times 2 \mathrm{in}$. P.E. ADRORA TRANS. $12+12 \mathrm{~V}_{\text {; }} 500 \mathrm{~mA}$ MINI-MAINS $20 \mathrm{v}, 100 \mathrm{~mA}$. 1in. HEATER TRANS. 6.3v. 3

4, 5, 8.3 v. 11 amp 55p GENERAL PURPOSE LOW VOLTAGE. Tepped Outputs at 2 amp. 3. 4, 5, 6, 8, 9, 10, 12, 15, 18, 24 and 30 v. 82.00
 2 amp. B, $8,10,12,16,18,20,24,34,88,40,48.80 . £ 3.00$
AUTO TRANSFORMERS 115 v . to 230 v . or 230 v . to 115 z . AUTO TRANSFORMERS 115v. to 230v, or 230 v . to 115 v . Inpnt/Output, 150 w. E2-00; $^{5}$ 500w. e5; 1000
CHARGER TRANSFORMERS. Input 200/250v. Cor 6 or 12 p . FOLL WAVE BRIDGE CHARGER RECTIFIERS. 8 or 12 v. outputs, 11 amp. $40 \mathrm{p} ; 2 \mathrm{amp} .55 \mathrm{p} ; 4 \mathrm{amp} .85 \mathrm{p}$.
All tranaformers Postege 25 p extra.

E.M I. $13 \frac{1}{2} \times 8 \mathrm{in}$. LOUDSPEAKERS
 State 3 or 8 or 15 ohm . Post 15p With fiared tweeter cone and ceramic
 Flax 10.000 gauss. State 8 or 8 or 15 ohm. Post 15p Recommended Teak Cabinet
Size $18 \times 10 \times 9$ in. Post 25 p . $\mathbf{S 5}$

## IOW MINI-MODULE $£ 3 \cdot 25$ LOUDSPEAKER KIT

 Triple speaker system combining on read cat batile.in. chipboard $15 \mathrm{in}, \times 81 \mathrm{in}$. Separate Bass, Middle and Treble loudapeakert and crossover condenser. The heavy duty 5 in. Bass Woofer unit has a low resonance cone. The mid-Range unit is apecially designed to add drive to the middie register and the tweeter recreates the $20-15,000$ eps. Fall inatructions tor 3 or 15 ohm TEAK VENEERED BOOKSHELF ENCLOSORE. $164 \times 101 \times 6 \mathrm{in}$. Modern Design, dark grey Trgan covered baffie or with fiuted wood front $16 \times 10 \times 9 \mathrm{in}$.


## GOODMANS HI-FI WOOFER

8 ohm, 10 watt. Large ceramic magnet Special Cambric cone surround. Frequency esponse $80-12,000 \mathrm{cps}$. Ideal P. A. Colnm
Hi-Fi Enclosures Systems, etc. 64


## ELAC CONE TWEETER

The moving coil diaphragm sives 2 good radiation pattern to the higher frequenciea and a smooth extension of total response from $1,000 \mathrm{cps}$ to $18,000 \mathrm{cps}$. Size $3 \frac{3}{2} \times$
$3 \uparrow \times 2 \mathrm{~m}$. deep. Rating 10 watte. 3 ohm or 15 ohm models. $\leq 1.90$

Horn Tweeters 2-18kc/i, 10 W 8 ohm or 15 ohm De Luxe Horn Tweeters $9-18 \mathrm{Kc} / \mathrm{a}, 15 \mathrm{w}, 8$ ohm 83 TWOWWAY 3000eps CROSSOVERS 3 or 8 or 15 ohm 95 p . SPECAAL OFFER! 80 ohm, 2 inin. dia.; $35 \mathrm{ohm}, 2 \mathrm{Zn}$.; 3in $25 \mathrm{ohm}, 8 \mathrm{in}$. dia.; 3 in . dia.; $8 \times 4 \mathrm{in} . ; 8 \times 5 \mathrm{in}$. $\mid$ EACH $15 \mathrm{ohm}, 3$ in. dia.; $7 \times 4 \mathrm{in}$.: $8 \times 5 \mathrm{in}$. II TYPE $8 \mathrm{ohm}, 6 \times 4 \mathrm{in} .3 \mathrm{ohm}, 81 \mathrm{in}$. 3 in . 5in. $5 \times 3 \mathrm{in} .7 \times 4 \mathrm{in}$ LOUDSPEAKERS P.M. 3 OEMS. $61 \mathrm{in} .21 .10 ; 8 \times 5 \mathrm{in} .21-25$; $8 \times 2 \nmid \mathrm{in} .90 \mathrm{p} ; 8 \mathrm{in}$. $81.75 ; 10 \times 6 \mathrm{in}$. 11.90 . 5 in . WOOFER 8 watts max. $20-10,000 \mathrm{cps} .8$ or 15 ohm .41 .80. ELAC 8 in. De Luxe Ceramic 3 ohm or 15 ohm fRe 50.
RICEARD ALLAN TWIN CONE LOUDSPEAKERS. 8 in. dia. 4 watt; $10 i n$. dia. 5 watt; 12in. dia. 6 watt 3 or 8 or 15 ohm models 21.95 each. Post 15 p . OUTPUT TRANS. ELB4 etc. 25p; MIKE TRANS. $50: 125 \mathrm{p}$. SPEAKER COVERING MATERIALS. Sgmples Large S.A.E. GOODMAN'S OUTPUT TRANSFORMER 5 watt punh-pull for valves EL84 etc., 8,8 and 15 ohme 85 p , Polt 20 p . BAKER 100 WATT ALL PURPOSE POWER AMPLIFIER
4 inputs speech and music Mixing facilities. Response $10-30,000$ cpi. Matches 200/250v. Treble and Bass control., Guaranteed.


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 BARGAIN AM TUNER. Medium Wave. $\leq 4$ Trannistor Superhet. Ferrite aerial. 8 volt.Add musical highlights and sound effects to recordings.
Will mix Microphone, records, tape and tuner Will mix Microphone, records, tape and tuner
with separste controls into sing le outpnt. 9 volt. BARGAIN FM TUNER 88-108 Mc/s Six Transiator. 9 vol Printed Circuit. Calibrated alide dial tuning t.10

BARGAIM FM TUNER as above lesa cabinet
$£ 7.50$
BARGAIN 3 WATT AMPLIFIER. 4 Transistor $\mathbf{4 3 . 5 0}$
COAXIAL PLUG 6p. PANEL SOCEETS 6p. LINE 18p
OUTLET BOXES, SURFACE OR FLUSH 25p.
BALANCED TWIN FEEDERS $5 p$ yd. 80 ohms or $\mathbf{8 0 0}$ ohms JACE SOCKET Std. open-circuit $14 \mathrm{p}_{\text {. }}$ closed circuit 23 p ; Chrome head Socket 45p. Phono Plugs 5p. Phono Socket Sp, JACK PLUGS $\$$ th, Chrome $15 \mathrm{p} ; 3.5 \mathrm{~mm}$. Chrome 14 p . DIN $3_{3-\text { pin }} 18 \mathrm{p}$; 5 -pin 25 p . DIN PLUGS 3 -pin 18 p ; 5 -pin 25 p . 3-pin 18p; 5-pin 25p. DIN PLUGS 3-pin 18p; 5-pid 20p

E.M.I, TAPE MOTORSPoat 16 p . 120 v . or 240 v . AC. 1,200 r.p.m. 4 pole 135 mA . Spindle $0.187 \times 0.75 \mathrm{in} . \quad$ \&|.25 BALFOUR GRAM MOTORS 120 v . or 240 v . A.C. 1.200 r.p.m. 4 pole


## Fully guaranteed Individually packed VALVES

\section*{B12स 81．75p} $\begin{array}{ll}\text { CY31 } & 35 \mathrm{p} \\ \text { DAF96 } & \text { ECL } 80 \\ \mathbf{8 8} & \mathbf{4 5} 5 \mathrm{p} \\ \text { OB2 }\end{array}$ | DAF96 | 88p | FCL89 | $\mathbf{3 2 p}$ | PABC80 |
| :--- | :--- | :--- | :--- | :--- |
| DF96 | 87p | ECL83 | $\mathbf{6 5 p}$ | PC97 | | DF96 | 87p | ECL83 | 65p | PC97 |
| :--- | :--- | :--- | :--- | :--- |
| DK96 | 41p | ECL86 | 48p | PC900 | | DK96 | 41p | ECL866 | 48p | PC900 |
| :--- | :--- | :--- | :--- | :--- |
| DL92 | 32p | EF36 | 45p | PCC84 |禺苞

TRANSISTORS，ZENER DIODES etc．


 | 28 | $25 p$ | OC201 | 6 |
| :--- | :--- | :--- | :--- |
| 29 | $62 p$ | OC206 | 8 |
| 35 | $50 p$ | IN21 | 1 |
| 38 | $48 p$ | IN 21 | 2 |
| 44 | $17 p$ | IN 43 | 6 |



 | EF83 | $55 p$ | PCF84 | 46p | OA210 | 25p |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| OA211 | 37p | 0 |  |  |  |
| EF85 | $38 p$ | PCF86 | 57p | 0 |  |


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 29／a1ft．AERIALS each consisting of ten 3 ft ． in ．dia． tubular screw－in sections． 11 ft ．（6－section）whip aerial
with adaptor to fit the 7 in ．rod，insulated base，stay plate and stay assemblies，pegs，reamer，hammer，etc． Absolutely brand new and complete ready to erect．

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 \begin{tabular}{r|ll|l}
£1．05 \& FF92 \& 37p \& PCF802 <br>
EF95 \& $30 p$ \& PCF805

 

EABC80 \& 32 p \& EF183 \& 32 p \& PCF806 <br>
EAF42 \& 50 p \& EF184 \& $\mathbf{3 5 p}$ \& PCF808 <br>
EB91 \& $\mathbf{1 5 p}$ \& EFL 200 \& $\mathbf{7 5 p}$ \& PCH200
\end{tabular}



| EBFP80 | 80 p | EL42 | 58 | PCLs 3 |
| :---: | :---: | :---: | :---: | :---: |
| EBFa |  | EL8 | 2 p | PCL84 |
| EBF83 | 42p | FL85 | 40p | PCL85 |
| EBF89 | 30p | EL86 | 40p | PCL86 |
| ECC81 | 30p | EL90 | 3 pp | PFL200 |
| ECC82 | 28p | EL95 | 35p | PL36 |
| ECC83 | 80p | EL500 | 85p | PLS 1 |
| ECC84 | 20 p | EM31 | 25p | PL82 |
| ECC85 | 40 p | EM80 | 40p | PL83 |
| ECC86 | 50p | EM84 | 35p | PL84 |
| ECC88 | 37p | EM87 | 55 p | PL500 |
| ECC189 | 52p | EY51 | 40p | PL504 |
| ECF80 | 35 p | FY86 | 35p | PY33 |
| ECFR2 | 33 p | EY81 | 35p | PY80 |
| ECF83 | 75p | EY88 | 40p | PY81 |
| FCF801 | 62p | EZ41 | 42p | PY89 |
| ECFRO2 | 62p | EZ80 | 25p | PY83 |
| ECH35 | 80p | E781 | 27p | PY88 |
| ECH42 | 65 p | GZ34 | 52 p | PY800 |
| ECH81 | 28p | KT6 | 21．60p | PY801 |
| ECH83 | 42p | KT88 | 22．16p | QQVO3 |

METERS

ALL valves guaranteed

（＇omplete set of parts for this MW／LW Transistor Radio．Originaily sold by world－famous company as a set for more $\begin{array}{ll}\text { than } \\ 1870 \mathrm{~m} . & \text { ．} 917 \text { ．Coverage } 192-555 \mathrm{~m}+1070- \\ 6\end{array}$ naing 3 AFll7 in RF and IF stages powered by a two atage AV＇amplifler naing powered by \＆two atage ap amplifier nising
$8 \times \mathrm{AC128}$ ．Output approx． 500 MW ． Also works lof car－merial．Full in－ Rtruction book 18ip free with parts． Red only，ply case，rexine covered． $3 \ddagger$ in hlgh－quality speaker．Price $\$ 6$ plns 31 in hlgh －qua
40 p,

STEREO AMPLIFIER Type SHV－2 $\times 3$ watts Fully built．Separate vol．，base and treble controls each channel； $12 \times 4!\times 6$ hin high．EZRO and Double wound mains trans．Snitable for crystal， masn．cartridge，tuner，etc．with monn－stereo switch．200－250V a．c．Inains． $27 \cdot 25$ ，50p P．\＆P．


A．M．／F．M．（V．H．F．）tuning gang $/ 3 \times 2 \times 1$ in
plus bindle plas opindle $\operatorname{tin}$（ 1 in dia．） $400+180+20+$ 20pi；geared slow motion drive $6: 1$ ； no back lash ：cast frame；Brand new； German； $3 \times 4 \mathrm{~b}$ ．a．fixings． 35 p poat pd．
less $10 \%$ for 6 ．

## MAINS TRANSFORMERS（ $240-250 \mathrm{~V}$ input）

Postage in brackets
$6-3 \mathrm{~V}$ at $2 \neq \mathrm{A}, 40 \mathrm{p}$（ 15 p ）
250 V at 50 AliA and 6.3 V at $1 \nmid \mathrm{~A}, 50 \mathrm{p}(20 \mathrm{p})$
22 V at $1 \mathrm{~A}, 6 \cdot 3 \mathrm{~V}$ at 2 A and 250 V at 50 mA ， 75 p （ 25 p ）．
90 V at 2013 A and 1.4 V at $250 \mathrm{~mA}, 50 \mathrm{p}$（ 15 p ）．
Deduct 10 per cent from total bill for more than one transformer．

 dust cover ：Plessey． 250 post pd．，less $10 \%$ for 6 ．

## GLADSTONE RADIO

66 ELMS ROAD，ALDERSHOT．Hants
（2 mins．from Station and Buaes）．FULL GUARANTEE．Alderghot 22240 CLOSED WEDNESDAY．S．A．E．for enquiries please．

Selections from FELSTEAD ELECTRONICS＇List
（Sent free for atamped addrensed envelope to address below）
（Sent free for atamped addreased envelope to address below）
Traneintors etc．AC12 $121 p$ ．AF115 20p．AF116 15 p ．AF117 20p．OA5 7pp．OA10 7pp
 12p．OC170 20p．OC171 12 $\ddagger$ p．Many more in list．S．D．R．BY100 800piv 14p．Charges 64 p up to 11 ．paid for 12 and over）．\＆ab－Min Tranformers：OUTPUT $3 \Omega$ for OC72 etc．） 14p．DRIVER $15 p$（up to 6，6ip）．SOLDERING IRON．Slim，modern，British highsped 81 ． all parts replaceable，highest qualify，full guarantee： 81.071 （ 10 p）．DIAMOND 8TYLII Re－
placements for BSR TC8／LP，TC8／S，TC8LP／STE REO：COLLARO＇O＇：RONETTE placements for BSR TC8／LP，TC8／S，TC8LP／BTEREO：COLLARO＇O＇：RONETTE BF 40LP：Garrard GC2／LP and GC8／LP：ACOB GP65／67，all at 40p（6p）．ACOS GP73，
（7P91，GP918C，GP104－BSR ST4（ST3，ST5），ST8（ST9）；RONOTONE $8 T A$ ． 9 TA，9TAHC； （P91，GP918C，GP104－BSR ST4（ST3，ST5），ST8（ST9）；RONOTONE 8TA．9TA，9TAHC；
PHILIPS AG3306， $3060(3063,3066,3301,3302.3304$ ）；Gartard GKS25，GCM21，GCS23 DOUBLE DIAMOND．ST4（ST3 GP92，GP93，GP94 cartridges）：GP91－SC for all GP91－SC Cartridges All at 91.50 each（ $6 p$ ） SAPPHIRE STYLII．Ali tbose types shown above under＇Diamond Styll at 40p＇also GP3 at 171 peach （ 5 p ）and GP91 and GP918C at 40 p （ 5 p ）．No others．PICK－UP CARTRIDGES． All Standard fittings and atylii．Mono GP67／2 80p．STEREO－COMPATIBLE（MONO） GP91／8C E1－10 STEREO GP93 21.80 STEREO CERAMIC GP94 81.95 SONOTONE
 $57^{*} 1200$ ft． $56 \mathrm{p} .7^{\circ} 1800 \mathrm{tt}$ ． 90 p ．（ 7 fp on $5^{\circ}$ and $57^{\circ}$ ， 9 p on $7^{*}$ ）．Other sizes of Tapes，als metal hand－grip $81-00$ ．CM21 Grey hand desk 821 pic hand／desk 81p．M1C45．Curved
 （all 9p）．LAPEL（or hand）with clip 32 $\ddagger \mathrm{p}$（ 6 p ）．All are fitted with leads．DYNAMIC Type 209 Cardioid ball， $50 \mathrm{~K} / 600 \Omega$ ，omni－dir．，built－in vol．control，on／oft switch，special lead，handle（as goorl as money can buy）26－30．UD180 Uni－Dir．Ball．mesh， $50 \mathrm{~K} / 600 \Omega$ Adap．，cable，jack plug 24.80 ．（20p）．DM160，onni－dir．，Ball，50K Cable adaptor 88.87 （all at 271p）．WICROPKONE IN8ERT8．Dia．， $1-75^{*}$ OR $0-9^{\prime}$ elther aize 27 ip（ 6 p ）．EAR－ PIECES with lead and min．jack plug（ 2.5 or 3.5 mm ．，state which）．Magnetie 9p Crybtal
（ 3.5 only）24p（Up to 3 for 6 p on any）．HEADPHONS De－luxe STEREO $8-16$ Ohm $22 \cdot 47$ ．Bame，fitted vol．control each earpiece 24．20．Both have lead and stereo jack plug（ 171 p ）．High Res． 2000 ohm ．Adjustable 92 pp （ 71 p ）．SPEAKERS $12^{\circ}$ ROUND fitted
 with two tweeters and crossover network $15 \Omega 88.75$（25p）．YIBPATORS 12 V ． non－synch． $121 \mathrm{HD} 4,2 \mathrm{~m}^{\prime}$ ex．ping．271p． 12 V 7 －pin gynch．（12SR7）68łp．（Both types 6｜p per vibrator）．COMVECTING WIRE．Packs of 5 coils asotd．cols．ea．coil $5 y$ yis．Solid core 14 p （ 6 p ）．Fiexible 16p（ 7 p ）．Super thin for transist or wiring 16p（6p）．PICK－UP WIRE．Super thin，twin tlex，screened and aheathed 6p yd．（6p up to 6yds，over free）． RETRACTABLE Flex．Leads．（Curlies）Phonoplug each end li2ft．39p．6ft phono plug／ phono socket other end $25 \mathrm{p} .12 f t$ 421p（6p per lead alf types）．BATTERY ELIMINATOR．
 light，adaptor to auit most transistorised sets and cassette recorders $33 \cdot 15$（ 25 p ）．8END able），electrolytics，vol．controls，more microphones，transiators，thyristors and SDRs and other devices，盺itches of many types，rotary，toggle min．and sub－min．slide types， croc．clips，terminals，valve holders also Goldring G800 series cartridges etc．etc．＇gpecial Offer＊linea at very low prices．

## FELSTEAD ELECTRONICS（PW 5I）

LONGLEY LANE，GATLEY，CHEADLE，CHES．SK8 4EE
Cash with order only．No COD or Caller Service．Charges（Min．6p）in brackets after all tems．Regret Orders under 25p excluding postage，unacceptable．SAE please for enquiries or cannot be replied to．Charges apply G．B．and Eire only．Overseas orders welcomed
（lists free overieas）．

## Electronic Vandals

As an amateur archaeologist and also as a reader of your journal for nearly 20 years, I would like to applaud your editorial on "Electronic Vandals."

We as archaeologists do not want to deprive folk of their pleasures, but in return we ask that they in turn do not deprive us of vital information.

A coin or a metal brooch, so badly corroded as to be almost worthless as a coin may, in expert hands of conservationists at museums, tell us the date when Roman forces were active in a fort or when a Roman villa was last occupied.

We may have worked for many years patiently working out the size, shape and function of a structure; but if our dating evidence has been removed all our work becomes fruitless.

If some of your readers honestly wish to help in furthering human knowledge then I suggest they contact their local archaeological society through their museum. It may be that they would be grateful for their help. Please remember that archaeology is a study of people and not a treasure hunt. -J. L. Cole, (Sutton Coldfield).

## Beginners' Licence

Although there are many Amateurs, who have worked hard to acquire their radio licence, and are now fully fledged Amateurs, I fail to see why the G.P.O. have, as yet, not introduced a "beginners" "licence. Such a licence could not fail to please all, as it would undoubtedly benefit the amateur radio movement, would encourage enthusiastic people to join, and would not clash with the activities of the fully licensed Amateur.

I feel that a "beginners" licence is necessary as there are lots of potential Amateurs, who either don't have the facilities or don't have the time. I am sixteen years old, a keen SWL, but am in the middle of my ' $O$ ' Levels, and $I$ will be continuing my studies for the next two years, and have therefore no time with which to study for the R.A.E. I am sure that there are many others, who
are in a similar position. A limited licence would sow a good grounding and this would enable one to acquire a licence at a later date.

Such a licence could be based on the following terms, and conditions:
(1) A written exam comprising: (a) Section one of the present exam;
(b) Frequency control and measurement;
(c) Interference, the causes and suppression of it;
(d) Full operating procedure (this should relieve many qualified "Hams");
(2) The G.P.O. morse test;
(3) (a) Only able to use a small allotted section of the band;
(b) Limited to two watts power output;
(c) C.W. transmission only;
(d) The allocation of a "beginners" prefix.
These conditions would, by their very nature, urge the willing and genuine Amateur on to the full licence while the lazy, and unenthusiastic would fall by the wayside.-M. S. Lerner, (Hendon, London).

## Take-20 Dollars

Recently I started to construct one of the "Take 20 " projects and I was horrified at some of the local prices for parts. These prices may be of interest to you: $5 \mu \mathrm{~F} 12 \mathrm{~V}$ capacitor, 20 cents; $1.5 \mathrm{M} \Omega \quad{ }^{1}{ }_{4} \mathrm{~W}$ resistor 10 cents; BC109 transistor, $\$ 1 \cdot 85 \mathrm{c}$; BC169C transistor $\$ 2 \cdot 25 \mathrm{c}$. Ten New Zealand cents is equal to 5 p.

It is actually cheaper to have these parts air-freighted from Britain than to buy them from the local shop.-K. B. Moore (Tokoroa, New Zealand).

## A Protest

Radio components are clearly inferior to the previous designed ones, when silk covered windings of transformers were impregnated with quality varnish. Modern methods use enamelled wire impregnated with wax resulting in what I think is an inferior com-
ponent which cannot be relied upon.

Oil insulated windings are inferior, especially when mains voltages are used in primary windings of transformers. Enamelled wires are clearly inferior and unreliable. More so when wax impregnated.

We are progressing in the wrong direction. When will the proven system return, so that quality returns? I refer to transformers only but other components are quite often just as bad.-R. Wibberley, Nottingham.

## Such a D.I.N.

I would like to say a few words, aimed at manufacturers and suppliers: Now that "D.I.N." connectors are becoming more popular and standard on most equipment nowadays, how about making 5 -core cables readily available, and 4-core individually screened cables at least available, if not readily available?-R. Williams (St. Albans, Herts)

## Treasure Traced

We have been using a metal locator manufactured by a wellknown company for some time now and recently our Town Hall called upon us to help search for a very expensive diamond and sapphire ring which had been lost on the beach.

We tried a manufactured metal locator which proved useless near salt. When we used the P.W. Treasure Tracer, we found the ring after one hour. The P.W. locator was not affected by water at all and the ring was in salt water when located.

This was the first time we had put the P.W. Treasure Tracer to work and since the ring we located was worth about $£ 200$ it proves how good it is. Needless to say, the lady to whom the ring belonged is very grateful and I hope other readers will have as much success.

The cost to build the Treasure Tracer is so low for such performance that the P.W. circuitry gives.

I must add that we also found about a dozen coins before finding the ring.-R. Miller (Brightlingsea, Essex).

## SERVIOING

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## PART 7

GORDON KING CONTINUES THE SERIES DISCUSSING TUNER-AMPLIFIERS AND THEIR PROBLEMS, PICKUPS AND THEIR ASSOCIATED CORRECTION NETWORKS AND ENDS WITH A BRIEF RESUME OF HI-FI AMPLIFIER SPECIFICATIONS.

Iwant to begin this month with the hi-fi type of radio receiver, called the tuner-amplifier. This is an integration of a stereo (two channel) amplifier and a radio receiver always tuning the f.m. band (Band II) and sometimes a.m. bands as well, and invariably embodying a stereo decoder. This type of equipment is ousting the ordinary radiogram in certain areas of application, for, coupled to a pair of good speaker systems and a record playing unit the tuner-amplifier constitutes the 'heart' of a music system of significantly greater quality potential than the average radiogram.

Real hi-fi radio reproduction is not possible from the a.m. bands owing to the necessary restriction of the i.f. passband to avoid interference between adjacent stations. Sadly, even such passband restriction is unable to keep unwanted stations from the wanted in the medium waveband after dark, and as a consequence we get an annoying background of whistles and monkey chatter. Moreover, the passband restriction deletes the higher-order sidebands of the modulated signal and hence impairs the treble output.

With f.m. things are not like this because in Band II each channel is allotted 200 kHz of 'elbow room', thereby permitting full expansion of all the sidebands without restriction.

The f.m. system has attractive attributes over and above the a.m. system, including enhanced signal-tonoise performance, the ability to reject a.m. signals and interference and a parameter known as the 'capture ratio'.

The capture ratio stems from the nature of f .m. demodulation and from the amplitude limiting engineered into the i.f. channel of the receiver. It means that when two signals are present in the same channel (or close together in the receiver's passband) the weaker one is almost completely rejected and only the stronger of the two gives an output, free from interference.

A capture ratio of two or three decibels ensures that a co-channel signal is muted when the wanted signal is only about 10 dB above it. Nothing like this degree of rejection is possible on a.m. All this boils down to the fact that the f.m. radio system is truly hi-fi, and that a.m. cannot be regarded in this light at all.

## DEVELOPMENTS

Contemporary radio tuners and the tuner sections of tuner-amplifiers are fast taking in the latest devices, including field effect transistors (f.e.t's.), integrated circuits (i.c's.), crystal and ceramic i.f. filters supplementing the bandpass transformer couplings. F.e.t's. are used mostly in the front-end as the r.f. amplifier and, sometimes, the mixer (With a bipolar local oscillator). Since their transfer characteristics exhibit second-order components they yield fewer third-order intermodulation components at high signal level than bipolar counterparts, whose characteristics contain an abundance of third-order components.

This means that unwanted spurious signals are minimised, particularly at locations close to a powerful station group. They also provide other attributes, including relatively low noise working and good 'mixing' properties. Thus a tuner section (f.m.) containing an f.e.t. r.f. amplifier and an f.e.t. mixer is likely to out-perform an 'equivalent' incorporating bipolar devices in these stages under a wide range of operating conditions.

## THIRD ORDER INTERMODULATION

One problem with simple f.m. front-ends is thirdorder intermodulation when operated in a strong, locally derived signal field. One symptom of this is a spurious signal at Radio 3 frequency (from $f_{2}+f_{4}-f_{3}$, where $f_{2}, f_{3}$ and $f_{4}$ are the frequencies of Radios 2, 3 and 4 respectively). This can result in 'burbles' and similar sort of interference on Radio 3, and possibly 'birdies' inteference when Radio 3 is stereo encoded.


Fig. 1: Simple altenuator for reducing intermodulation problems.

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Fig. 2 : Circuit of the "front-end" of a typical British tuner-amplifier.


Fig. 3: The f.m. i.f. channel of the tuner-amplifier shown above.

One solution lies in attenuating the signal from the aerial to the set. Belling Lee make plug-in attenuators over a range of values; alternatively a simple resistive pad can be made up as shown in Fig. 1.

## FM FRONT-END

The f.m. front-end of a typical British tuneramplifier is shown in Fig. 2. Here VT1 is a dual-gate f.e.t. with the input signal applied to one gate and an a.g.c. potential to the other. The mixer is bipolar VT2 and the local oscillator bipolar VT3.

Aerial coupling is by Tl primary, and since this is centre-tapped 300 ohms balanced feeder can be connected across terminals 1-2 or 75 ohms coaxial (unbalanced) across $2-3$. Not all input circuits permit this dual mode of feeder connection, and if the design is essentially for 300 ohms balanced (or 240 ohms European DIN) the best coupling from coaxial is obtained through a 'balun' transformer.
A.f.c. is applied to the local oscillator from a varactor diode (MR601), and this receives its control bias from the f.m. detector. The varactor is in parallel with the oscillator tuned circuit, so the frequency of this is altered by the control bias which appears in appropriate polarity from the f.m. detector when the tuned carrier is displaced from the centre of the i.f. passband.

The i.f. signal is developed across T2, and is coupled to the f.m. i.f. channel from the capacitance tap on circuit No. 8.

## FM IF CHANNEL

The f.m. i.f. channel is shown in Fig. 3, and the input goes to circuit No. 503 and thence to the base of VT501.
The channel includes two ceramic filters of the kind already mentioned (X501/X502) and a couple of i.c's. (VT503/VT504). The ceramic filters take the place of the usual i.f. transformers and because they exhibit steeply rising and falling response sides extremely good i.f. selectivity is secured. The only alignment required is of the ratio detector transformer T501.

The i.f. signal at VT501 collector is fed to the first filter and from this to the first i.c. The second filter couples the two i.c's., while VT505 bipolar transistor drives the ratio detector, composed of diodes D1/D2, etc. This circuit is balanced, and preset RV501 allows this to be optimised, one mode for adjustment being for the least response to an a.m. signal.

It will be noticed that the ratio detector yields potential for the tuning meter as well as for the varactor diode on circuits 506 and 505 respectively. Demodulated audio (or multiplex signal in the case of stereo) from circuit 507 is coupled to the stereo decoder.

VT506 is concerned with the muting, etc., while VT502 amplifies i.f. signal at VT501 collector and passes it to the rectifier MR501. The resulting filtered d.c. constitutes the a.g.c. potential for the f.e.t. r.f. amplifier (Fig. 2).

## FAULT FINDING

Fault finding in a circuit of this kind is best carried out by feeding a modulated $10 \cdot 7 \mathrm{MHz}$ (or a signal at the i.f.) into the strip, starting at the final transistor (VT505 in this case), then working forward until the point of inactivity is located.

To find the actual component which is in trouble, after locating the faulty area or stage, might well require the testing of voltages, etc. at the electrodes of the various devices, and to help in this respect the voltage references in Fig. 3 have been retained.

Servicing of f.m. front-ends is not recommended —apart, possibly, from the replacement of transistors -and trouble in this area is best left to the maker or distributor to clear. This applies to professional service organisations as well as to the amateur repairer.

A word about the replacement of f.e.t's. would not be amiss. The insulated gate types in particular are vulnerable to static discharges, and when making a replacement always retain the shorting clip (fitted by the maker) until the device has been completely soldered into the circuit.

From the testing, adjusting and servicing aspects, the BBC's stereo test sequence at the close-down of Radio 3 can be of a great help in determining such parameters as stereo separation (e.g., degree of crosstalk), signal-to-noise, frequency response, etc.

## SOURCE INPUTS

When a radio tuner is used with a hi-fi amplifier a 'flat' response is required since the de-emphasis is performed in the tuner. Inputs with 'flat' responses thus include radio, high-level tape replay and auxiliary. If an amplifier is equipped with an input for the signal direct from a tape head, then equalisation will be included to cater for the replay response. The only equalising then required is that pertaining to the gramophone pickup, and a good starting point is the pickup (cartridge) itself.

## PICKUPS

There are two versions. One the magnetic which works rather like a generator, and the piezo, using either a natural crystal or processed ceramic, which works on the transducer principle.

When a gramophone record is made the modulation is imparted to the groove from a cutting head via a special electrical filter having a specific


Fig. 4: Graph showing the standard RIAA recording characteristic
recording characteristic. The bass end of the spectrum is attenuated and the treble end is boosted. On replay, therefore, the bass needs to be boosted and the treble attenuated to secure a 'flat' audio output.

The standard recording characteristic is given in Fig. 4. This has an 'average' slope of about 4 dB /

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octave, but the RIAA equalising, as it is called, is very carefully engineered into the magnetic pickup input circuits of hi-fi amplifiers and good quality radiograms, etc., so that the response is exactly the reciprocal of that shown in Fig. 4. The net result is that a 'flat' output from the preamplifier which, of course, is the signal requirement of the control section and power amplifiers.

Now, it is the velocity of the imparted modulation which follows Fig. 4 curve, and because magnetic pickups yield an output proportional to the velocity of stylus deflection the output from the pickup applied to the equalised preamplifier is thus after the style of that in Fig. 4. Hence the reciprocal equalisation just referred to.

A piezo pickup, on the other hand, produces an output which is proportional to the amplitude of stylus deflection (not velocity). This implies that a piezo pickup playing a record cut to the standard RIAA response produces an almost 'flat' output without equalisation.

All piezo cartridges need to be loaded into a very high resistance of not less than $1 \mathrm{M} \Omega$ and for the best results and to secure full advantage of the inbuilt equalisation and thus obtain a 'flat' output from a disc recorded to the RIAA standard.

A magnetic cartridge (whose source is inductive), however, is commonly designed to work best into a load of round $50 \mathrm{k} \Omega$. If it is loaded lower the treble tends to fall, while too high a loading can lift the treble end of the spectrum and incite undue 'ringing'. Conversely, a piezo cartridge (because its source is capacitive) exhibits falling bass and rising treble when loaded into a resistance significantly below 1MS! or so.

The signal yield from a piezo cartridge, even when loaded low, is significantly in excess of that from a magnetic cartridge when playing modulation of a given velocity. This means, therefore, that the piezo signal might well have to be attenuated before being fed to the magnetic input, to avoid preamplifier overload.


Fig. 5: Circuit of a pre-amplifier incorporating RIAA equalisation

The peaks of signal can be clipped when the pickup signal veers towards the overload level. However, when an 'equalising' pad is included a degree of attenuation is automatic, so additional attenuation may not be necessary.

## RIAA EQUALISED PREAMPLIFIER

Shown in Fig. 5 is the circuit of a fairly conventional RIAA equalised preamplifier. It is common to employ two transistors, at least, and in the circuit shown, R306/R310/C303/C304 network provides the frequency selective network, giving the necessary response characteristic inversely to correspond with the recording characteristic (Fig. 4). The overall effect is that the feedback increases with rising frequency and decreases with reducing frequency, thereby giving the required treble cut and bass boost.

R303 provides a 'flat' control of gain, and in some amplifiers the frequency selective network is switched out of circuit when the programme input signal requires a 'flat' response, a resistor such as R303 then being used to provide the appropriate input sensitivity voltage. Stereo equipment embodies two such preamplifiers, one for each channel.

The RC network C306/R311 provides a low-pass. characteristic, preventing the response from extending too far above the audio spectrum. The 100 pF capacitor (C308) connected directly across the base/ emitter electrodes of the input transistor cuts the input response to radio frequencies and thus prevents the breakthrough of radio and television interference during low-level record replay.

## RADIO/TV BREAKTHROUGH

Not all amplifiers are equipped with radio and TV filtering like this, and since the response of transistor stages can embrace the radio and TV spectrums, a symptom becoming increasingly common is, in fact, radio and TV breakthrough. This mostly happens when the equipment is switched to magnetic pickup and when it is operated relatively close to a powerful radio or TV station. It is encouraged by (i) the high sensitivity of the amplifier under this mode of operation and (ii) the relative ease at which the RIAA preamplifier can be pushed into non-linearity.

A filter which nearly always clears the trouble is given in Fig. 6. The circuit to the base should be broken and the $2 \cdot 2 k \Omega$ resistor inserted in series.


Fig. 6: A simple filter to prevent radio and TV signals interfering with audio amplifiers.
while the 100 pF capacitor should be connected right across the base/emitter electrodes, as close as possible to the input transistor. Both channels should be so treated.
The RIAA preamplifier signals can get into trouble so if one channel of a stereo amplifier appears to be lacking in bass, with excessive treble output, when operating from a magnetic cartridge, then attention should be given to the preamplifier department of the affected channel. Excessive noise on the magnetic
input is commonly caused by a defective preamplifier transistor or a 'noisy' collector resistor.

## HI-FI SPECS

It is impossible to detail all the specifications relating to hi-fi equipment (further information on this score is given in "Tuners and Amplifiers" by John Earl, published by Fountain Press), but comment on a few of the more important ones would not be amiss.

Power Capacity. This is the maximum power that an audio section is capable of delivering with both channels running, the maximum being defined either to the level of sinewave clipping or to a specified value of distortion when the output is loaded by pure resistance of appropriate value in place of the speaker. The 'standard frequency' is 1 kHz , but to obtain the power bandwidth the measurement is repeated at low and high frequencies.

Standard Output Power. This is $50 \mathrm{~mW}(17 \mathrm{~dB} / \mathrm{mW})$. However, in some instances values of 500 mW ( $27 \mathrm{~dB} / \mathrm{mW}$ ) and $5 \mathrm{~mW}(7 \mathrm{~dB} / \mathrm{mW})$ might be used, but the power to which any parameter (such as sensitivity) refers should be stated in the specification.

Input Sensitivity Voltage. This is the input signal at 1 kHz required to yield the rated output power when the volume control is fully advanced, all filters 'out' and tone controls 'flat'.

Signal/Noise Ratio. This refers to the voltage due to components of hum and noise across the output load in terms of dB ratio to the rated output power and within the full noise bandwidth of the equipment. The volume control is generally fully advanced and the selected source input is either short-circuit or open-circuit (the former preferred since it avoids the pickup of spurious hum and noise components).

A ratio of 60 dB , for example, implies that the power of the summed hum and noise in the output load is one million times below the full power of the amplifier.

Total Harmonic Distortion (THD). This is commonly measured through a distortion factor meter, in which a very sharply tuned filter 'notches out' the fundamental frequency, leaving only the harmonic components.

Intermodulation Distortion (IMD). Like THD, IMD is a function of amplifier non-linearity. This is commonly measured in terms of the amplitude of intermodulation components resulting from the introduction of two signals to the amplifier, so as to produce sum and difference frequencies.

S/N Ratio (FM). This refers to hum and noise relative to a stated modulation level ( $100 \%$ or $30 \%$ ). Measurement is similar to that of $S / N$ ratio of an amplifier, and the usable sensitivity of an f.m. tuner is commonly given as the input required for a $\mathrm{S} / \mathrm{N}$ ratio of 45 dB .

Owing to the wider passband involved and the action of decoding, a stereo receiver has a $\mathrm{S} / \mathrm{N}$ performance below that on mono, particularly at the lower signal input levels, which is the reason why stereo receivers should always be operated with the best possible f.m. aerial system, consistent with the location and prevailing signal field on Radio 3.

END OF SERIES

## NINE BAND RECEIVER-continued from page 690

## AERIALS

The telescopic type aerial has a bracket, so that it can be bolted directly on the left hand side of the case, about lin. from the back. An insulated socket is fitted on the side of the case for an external aerial. Many transmissions can be received at ample volume with the telescopic aerial alone but an external aerial will greatly improve the reception of weak signals.


## DIAL SCALE

Because each of the nine bands covers a relatively small frequency range, the main tuning scale is fitted with a card marked 0 to 50.

The bandswitch has nine positions, and the card scale under it has ten frequency markings. The bandswitch pointer comes to rest between these markings, which thus show the approximate frequency coverage of that particular range. For example, if the pointer rests between $4 \cdot 6$ and $5 \cdot 0$, the range is $4 \cdot 6-5 \cdot 0 \mathrm{MHz}$, while if it is between $5 \cdot 0$ and $5 \cdot 6$ the range is $5 \cdot 0 \cdot 5 \cdot 6 \mathrm{MHz}$, covered with the normal tuning control.

The full markings are as follows: $3 \cdot 6-3 \cdot 8-4 \cdot 3$ $4 \cdot 6-5 \cdot 0-5 \cdot 6-6 \cdot 3-7 \cdot 4-10-15$. This scale is best put under the perspex.



## High fidelity Monolithic Integrated

Two years ago Sinclair Riadionics announced the World's first monolithic integrated circuit $\mathrm{Hi}-\mathrm{Fi}$ amplifier, the 1C. 10 . Now we are delighted to be able to intraduce its successor, the Super IC. 12. This 22 transistor unit hes all the virtues of the original IC. 10 plus the following advantages:

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Input Impedance 250 Kohms nominal.
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With the addition of only a very few externat resistors and capacitors the Super IC. 12 make: a complete high fidelity audio amplifier suitable for use with pick-up. F.M. tuner eic. Alternatively, for more elaborate systems, modules in the Project-60 range such as the Stereo 60 and A.F.U. may be added. The comprehensive manual supplied with each unit gives full circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include car radios, oscillators etc. The very low quiescent consumption makes the Super IC. 12 ideal for battery operation.


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Project 60 offers more advantage to the constructor and user of high fidelity equipment than any other system in the world.
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[^3]
# from a simple amplifier to a complete stereo tuner amplifier with Project 60 modules 

## Z. 30 \& Z. 50 power amplifiers



The $Z .30$ and $Z .50$ are of advanced design using silicon epıtaxial planar transıstors to achieve unsurpassed standards of performance Total harmonic distortion is an incredibly low 0.02\% at full output and all lower outputs. Whether you use $Z .30$ or $Z .50$ amplifiers in your Project 60 system will depend an persanal preference, but they are the same size and may be used with other units in the Project 60 range equally well. SPECIFICATIONS ( 2.50 units are interchangeable with 2.30 s in all applicatlons). Power Outputs
Z. 3015 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M.S. into 3 chms using 30 volts. Z.50 40 watts R.M.S. into 3 ohms using 40 volts 30 watts R.M.S. in to 8 ohms usirg 50 volts. Frequency response: 30 to $300.000 \mathrm{~Hz} \pm 1 \mathrm{~dB}$. Distortion : $0.02 \%$ intc 8 ohms.
Signal to noise ratio; better than 70 dB unweighted. Input sensitivity: 250 mv into 100 Kohms
For speakers from 3 to 15 ohms impedance.
Size: $14 \times 80 \times 57 \mathrm{~mm}$.
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Bull, tested and guaranteed whth circuits and instruc tions manual.
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## Project 60 Stereo F.M. Tuner



First in the world to use the phase lock loop principla

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratı. Now. Sinclar have applied the principle to an F.M. tuner with fantastically good results. Other original features include varicap dıode tuning. printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. Good reception is possible in difficult areas, and often a few inches of wire are enough for an aertal. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in This tuner can also be used to advantage with any other high fidelity system.
SPECIFICATIONS-Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108 MHz . Capture ratio: 1.5 dB . Sensitivity: $2 \mu \mathrm{~V}$ for 30 dB quieting: $7 \mu \mathrm{~V}$ for lock-in over full deviation. Squelch level: $20 \mu \mathrm{~V}$. A.F.C. range: $\pm 200 \mathrm{KHz}$. Signal to noise ratio: $>65 \mathrm{~dB}$. Audio frequency response: $10 \mathrm{~Hz}-15 \mathrm{KHz}$ ( $\pm 1 \mathrm{~dB}$ ). Total harmonic distortion: $0.15 \%$ for $30 \%$ modulation. Stereo decoder operating level: $2 \mu \mathrm{~V}$. Cross talk: 40 dB . Output voltage: $2 \times 150 \mathrm{mV}$ R.M.S. Operating voltage: 25-30 VDC. Indicators: Power on/tuning/stereo. Size: $93 \times 40 \times 207 \mathrm{~mm}$.
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## Stereo 60 Pre-amp/control unit



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SPECIFICATIONS-Input sensitivities: Radio-up to 3 mV . Mag. p.u. 3 mV : correct to R.I.A.A curve $\pm 1 \mathrm{~dB}: 20$ to $25,000 \mathrm{~Hz}$. Ceramic p.u. -up to 3 mV : Alx-up to 3 mV . Output: 250 mV . Signal to noise ratio: better than 70 dB . Channel matching: within 1 dB . Tone controls: TREBLE +15 to -15 dB at $10 \mathrm{KHz}:$ BASS $\overline{+} \overline{1} 5$ to -15 dB at 100 Hz . Front panel: brushed aluminium with black knobs and controls. Size: $66 \times 40 \times 207 \mathrm{~mm}$. Built tested and guaranteed.
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For use between Stereo 60 unit and two 2.30 s or $Z .50 \mathrm{~s}$, and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid ( $12 \mathrm{~dB} / o c t a v e$ ). there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. Two filter stages - rumble (high pass) and scratch (low pass). Supply voltage -15 to 35 V . Current -3 mA . H.F. cut-off $(-3 \mathrm{~dB})$ variable from 28 KHz to 5 KHz . L.F. cut-off ( -3 dB ) varıable from 25 Hz to 100 Hz . Distortion at 1 KHz ( 35 V . supply ( $0.02 \%$ at rated
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## Sinclair Q16/Micromatic

## Q16 High fidelity loudspeaker

The 016 employs the well proven acoustic principles specially developed by Sinclair in which a special driver assembly is meticulously matched to the characteristics of the uniquely designed cabinet. In reviewing this excluslve Sinclair design, technical journals have justly compared the Q16 with much more expensive loudspeakers. Its shape enables the Q16 to be positioned and matched to its environment to much better effect than is the case with conventionally styled enctosures. A solid teak surround with a special all-over cellular foam front is used as much for appearance as its ability to pass all audio frequencies without loss

This elegantly designed shelf mounting speaker brings genuine high fidelity within reach of every music lover.

## Specifications:

Construction: Special sealed seamless sound or pressure chamber with internal baffle.

Loading: up to 14 watts RMS.
Input Impedance: 8 ohms.
Frequency response: From 60 to 16.000 Hz . confirmed by independently plotted B and $K$ curve.
Driver unit: Special high compliance unit having massive ceramic magnet of 11,000 gauss, aluminium speech coil and special cone suspension for excellent transient response.

Size and styling: $9 \frac{3}{4}$ in. square on face $x$ $4 \frac{3}{4} \mathrm{in}$. deep with neat pedestal base. Black all over cellular foam front with natural solid teak surround.


Price £8.98.

## Britain's smallest radio

Considerably smaller than an ordinary box of matches. this is a multi-stage AM receiver brilliantly designed to provide remarkable standards of selectivity, power and quality for its size. Powerful AGC counteracts fading from distant stations; bandspread at higher frequencies makes reception of Radio 1 easy. The plug-in magnetic earpiece provided, matches the Micromatic's output to give wonderful standards of reproduction. Everything including the special ferrite rod aerial and batteries is contaned within the minute attractively designed case. Whether you build a Micromatic kit or buy this amazing receiver ready built and tested. you will find it as easy to take with you as your wrist watch, and dependable under the severest listening conditions

## Specifications:

Size: $36 \times 33 \times 13 \mathrm{~mm}(1.8 \times 1.3 \times 0.5 \mathrm{in}$.)
Weight: including batteries., 28.4 gm (1 oz.)
Case: Black plastic with anodised aluminium front panel and spun aluminium dial.
Tuning: medium wave band with bandspread at higher frequencies (550 to 1.600 KHz ).

Earpiece: Magnetic type
On/off switching: By inserting and withdrawing earpiece plug.
Kit in pack with earpiece. case, instructions and solder £2.48.

Ready built, tested and guaranteed, with earpiece £2.98.
Two Mallory Mercury batteries type RM675 required from radio shops. chemists, etc.


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## The largest selection

NEW LOW PRICE TESTED S.C.R.'s PIV

| PIV | $\mathrm{TO}_{1 / 5}$ | $3 A$ TO-66 | 7. T0-66 | 10 A | TO | 48 T | $\begin{array}{r} 30 A \\ \text { TO-48 } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8. | ep | \%p | $e^{2}$ |  | ep | $\mathrm{Ef}^{\text {p }}$ |
| 50 | 0.88 | 0.25 | - 0.47 | 0.80 |  | . 68 | 1-18 |
| 100 | 0.25 | 0.38 | 8 0.5s | 0.38 |  | -88 | 1.40 |
| 200 | 0.85 | 0.87 | 70.57 | 0.61 |  | -75 | 1.60 |
| 400 | 0.48 | 0.47 | $7 \quad 0.67$ | 0.75 |  | -88 | 1.75 |
| 600 | 0.50 | 0.67 | 7 0.77 | 0.97 |  | -28 |  |
| 800 | 0.88 | 0.70 | 0 0.90 | 1.80 |  | . 40 | 4.00 |
| SIL. RECTS. TESTED |  |  |  |  |  |  |  |
| PIV | 300 mA |  | $\begin{aligned} & \text { A } \\ & \hline \end{aligned}$ | 1-JA | $\begin{aligned} & 3.1 \\ & i p \end{aligned}$ | 10 A | 30A |
|  | 19 |  |  | Ep |  | \& | \&p |
| ¢0 | 0.04 | 0-05 | 0.05 | 0.070 | 0.14 | 0.21 | 0.47 |
| 100 | 0.04 | 0.00 , | - 0.05 | 0.180 | 0.16 | . 23 | -0.75 |
| 200 | 0.05 | 0.09 | 0.08 | 0-14 0 | 0.20 | 24 | 1.00 |
| 400 | 0.08 | 0.18 | 0.07 | 0.80 | 0.27 | . 37 | 1.25 |
| 600 | 0.07 | $0 \cdot 16$ | 0.10 | 0.28 | 0.84 | -48 | 51.85 |
| 800 | 0.10 | 0.17 | 0.18 | 0.25 | 0.87 | . 85 | 2-00 |
| 1000 | 0.11 | $\begin{aligned} & 0.25 \\ & 0.83 \end{aligned}$ | $0.15$ | 0.30 | 0.46 | -6.78 | 8-50 |
| 1200 | - |  |  | $\begin{array}{lll}0.33 & 0.57\end{array}$ |  |  |  |
| TRIACS |  |  |  | LUCAS SILICON RECTIFIERS |  |  |  |
| VBO | M 2A | 6A | 10A |  |  |  |  |  |  |  |
|  | T0-1 | T0-66 T | TO.88 | 35 amp, 400 p.l.v. stul type. 810p each. |  |  |  |
|  |  | ep | ep ${ }^{1}$ |  |  |  |  |  |  |  |
| 100 | 0.80 | 0.88 | 1.00 | DIACs |  |  |  |
| 200 | 0.70 | 0.80 | 1.25 | FORTRIACg | U |  | WITH |
| 400 | 0.90 | 1.00 | 1.60 ! |  |  | 87 p | 7p each |

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oII, 89 esch; 1,000 off,
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75 Gerinanlum gold bonded diodes sim. OĀ̄, OA47 40 Germanhum transiators like OC81. AC128 60200 mA mb-min. sil. diodes.
30 silicon planar translistors NPN sim. BSYOJA, 2N706 16 sillcon rectiflera Top-Hat 750 InA up to $1,000 \mathrm{~V}$
508 gil . planar diodea $250 \mathrm{~m} / \mathrm{A}, 0 \times / 200 / 202$
¿20 Mired volte I Watt Zener diodes
U11 30 PNP sillicon planar tranaistora TO-j nim. 2N113\% U13 30 PNP-NPN sil. translators $0 \mathrm{C} 200 \& 28104$
U14 100 Nlxed ailicon aod germanium diodes
UI5 25 NPN Silicon planar transistors TO-j bim. 2N697
U16 103 -Amp silicon rectifiers stud fype up to 1000 PIV U17 30 Germanium PNP AF tranaistors TO-5 like ACY 17-22 U18 86-Amp silicon rectifiers BYZI3 type up to f00 PIV U19 25 8ilicon NPN tranaiators like BC108
U20 $121 \cdot \mathrm{~J}$-Amp ailicon rectlifers Top-Hat up to I,000 PIV U21 30 A.F. germanium slloy transistors $2 G 300$ series \& OC7I U23 30 Madt's like MAT series PNR translators
U24 20 Germanium 1-Amp rectifers GJM up to 300 PIV. U25 $25300 \mathrm{Mc} / \mathrm{m}$ NPN silicon transistors 2 N 708 , B8Y27.
U26 30 Fast awitching billcon dioles ifke IN914 micro-min

## U28 Experimenters assortment of Integrated circuits, untested

Gates, Bip-flops, registers, etc., 8 assorted pieces
U29 10 1-Amp BCR's TO. 5 cm up to 600 PIV CRE1/2j-600 U31 20 8il. Planar NPN trans. low nolse amp 2N3707
U32 25 Zener dioden 400 mW D07 cese mixed volts, $3-18$
U33 15 Plantic cese 1 amp silicon rectifers IN 4000 ser les.
U34 30 8ill. PNP ailoy trans. TO-5 BCY26, 28302/4
U35̈ 25 Sll. planar trans. PNP TO-18 2N 2906
U36 25 sil planar NPN trans. TO-5 BFY $0 / / 51 / \overline{5} 2$
U37 30 gil. alloy trans. 80-2 PNP, OC200 28322
U38 20 Fast switching ail. trans. NPN, 400Mc/s 2 N 3011
U39. 30 RF germ. PNP trans. 2N1303/5 TO-5
U $00-10$ Dual trans. 6 lead TO.5 2N2060
U41 20 RF germ. trans. TO-1 0C4j NKT72
U42 10 VHF germ. PNP trans. TO.1 NKT667 AF117.
Code Nos, mentioned above are given guide to the tape of device in Code Nos. mentioned above are given a gunce to the ty
the Pak. The devices themselies are normally unmarked. the Pak. The devices themselves are normally unmarked.

## GENERAL PURPOSE GERM, PNP POWER TRANSISTORS

Coded OP100. BRAND NEW TO-3 CAgE. POS8. REPLACEMENTS FOR:-OC2J 28-29-30-3.j-36. NKT REPLACEMENTS FOR-404-40j-406-430-4vi-4 $22-453$. TI3027-3028, $2 \mathrm{~N}^{2} 50 \mathrm{~A}, 2 \mathrm{~N} 45 \mathrm{~J} / 4-47 \mathrm{~A}-488 \mathrm{~A}, 2 \mathrm{~N} 511 \mathrm{~A}$ \&. 2 G 220 222, ETC.
BPECIFICATION
VCBO 80V VCEO 00 V IC 10A PT. 30 WATTS Hie $30-170$.
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\text { 48p each } & 405 \text { each } & 38 p \text { each }
\end{array}
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GENERAL PURPOSE SILICON NPN POWER TRANSISTORS
Coded GP300. BRAND NEW TO-3 CABE. POBBIBLE REPLACEMENT FOR:-2N3050, BDY20, BDY11 BPECIFICATION
VCBO 100 V , VCEO 60 V , IC $15 A \mathrm{MPS}$, PT. 115 WATTS. Hfe 20-100. FTI MHZ
PRICE ${ }^{51}-24 \quad 100 \mathrm{up}$
GEITERAL PURPOSE YPA SIWCON SWITCRILG TRAES. TO-18 SIM. TO 23706/8, B8Y $27 / 28 / 95 A$. All uasble devices no open or short clrcult. A LSO AVAILABLE in PNP Bim. to 2 N 2906 , BCY70. When ordering plesse atate preference NPN or PNP.

$$
\begin{array}{llllll} 
& & \text { Ip } & 100 & \text { For } & 1.76 \\
20 & \text { For } & 0.80 & 600 & \text { For } & 7.50 \\
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\end{array}
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AILICON PHOTO TRATSIRTOR. TO-18 Lens end NPN $8 i m$, to BP $\times 25$ and P 21 . BRAND NEW. Full date available. Fuily gumenteed.
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 Data and Clrcuite Booklet for I.C's Price 7p.

|  | Description |
| :---: | :---: |
| Q1 | 20 Red bpot trans. PNP A |
| Q2 | 16 White spot R.E. trans. PNP |
| Q3 | $40 \mathrm{C7} 7$ tspe trans. |
| Q4 | 6 Matched trans. OC44/4v/81/81 |
| Qu | $40 \mathrm{O} \mathrm{S}_{5}$ transiators |
| Q6 | 4 OC72 transiators |
| Q7 | 4 ACl28 trans. PNP high gain |
| Q8 | 4 AC126 trans. PNP |
| Q9 | 7 OC81 type trans. |
| Q10 | $70 \mathrm{C7r}$ type trans. |
| Q11 | $\because$ AC127/128 comp. pairs PNP |
| Q12 | 3 AF116 type trans. |
| Q13 | 3 AFl17 type trana. |
| Q14 | 3 OCl71 H.F. typetrans. |
| Q15 | 52 N 2926 sil. epoxy trans. |
| Q16 | $2 \mathrm{GET880}$ low noise germ, trans. |
| Q17 | 3 NPN 1 ST141 \& 2 ST140 |
| Q18 | 4 Mantes 2 Mat 100 A 2 MAT 120 |
| Q19 | 3 Madtes 2 MAT 101 al MAT 121 |
| Q20 | 4 OC44 merm, trans. A.F. |
| Q21 | 3 AC127 NPN germ. tran |
| QP2 | 20 NKT trans. A.F. R.F. coded |
| Q23 | 10 OA2202 sil. dioder sub-min |
| Q24 | 80.881 diodes |
| Q25 | 6 IN914 sil. dioder 75 PIV 70 mA |
| Q26 | 8 OA9j germ. diodes sub-min. IN69 |
| Q27 | 2104600 PIV sil. rectas. I845R |
| Q28 | 2 Sil. power rects. BYZ13 |
| Q29 | 4 Bil. trans. $2 \times 2 N 696,1 \times 2$ N697. <br> $1 \times 2 \mathrm{~N} 698$ |
| Q30 | 7 8hl. switch trans. 2 N 706 NPN |
| Q3I | 6 8il. switch trans. 2 N 708 NPN |
| Q32 |  |
| Q33 | 3815. NPN trane. 2N1711 |
| Q34 | 78 il . NPN trans. $2 \mathrm{~N} 2369,500 \mathrm{MHZ}$. |
| Q35 |  |
| Q38 | 7 2N3646 TO. 18 plastic 300 MH 2 NPN |
| Q37 | 3 2N3003 ${ }^{\text {N PN ail. trans. }}$ |
| Q38 | 7 PNP trans. $4 \times 2 \mathrm{~N} 3703,3 \times 2 \mathrm{~N} 3702$ |
| Q39 | 7 NPN trans. $4 \times 2 \mathrm{~N} 3704,3 \times 2 \mathrm{~N} 3705$ |
| Q40 | 7 NPN amp. $4 \times 2 \mathrm{~N} 3707,3 \times 3 \mathrm{~N} 3708$. |
| Q41 | 3 Plastic NPN TO.18 2N 3904 |
| Q4'3 | 6 NPN trana. 2 Nil7 |
| Q43 | 7 BC107 NPN trans. |
| Q44 | 7 NPN trans. $4 \times \mathrm{BCl108} .3 \times \mathrm{B}$ |
| Q4J | 3 BCLI3 NPN TO-18 trane. |
| Q46 | 3 BCL15 NPN TO-5 trans. |
| Q47 | 6 NPN high esin $3 \times$ BCl67, $3 \times$ BC168 |
| Q48 | 4 RCYTO NPN trans. TO. 18 |
| Q49 | 4 NPN trams. $2 \times$ BFY51, $2 \times$ BFY 52 |
| Q50 | 7 BEY 28 NPN switch TO. 18 |
| Q51 | 7 BRY90A NPN trans. $300 \mathrm{MH2}$ |
| Q32 | 8 BY100 type sil. rect. |
| Q53 | 25 gil. \& germ. trans. mixed all marked new |

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| :---: | :---: | :---: | :---: |
| OC\%O | 50p | OC29 | 400 |
| OC2\% | 30p | $0 \mathrm{C} 3 \overline{\mathrm{~J}}$ | 389 |
| OC23 | 88 p | 0 C 36 | 40p |
| 0 C 2 J | 250 | AD140 | 400 |
| OC26 | 25p | AD142 | 40p |
| 0028 | 40\% | ADI49 | 48p |

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$\mathrm{BPOS}=740{ }^{\circ}$
$\mathrm{BP10}=7410$
$\mathrm{BP13}=7413$
$B P 20=7420$
$\mathrm{BP} 40=7440$
$\mathrm{BP} 41=7441$
$\mathrm{BP} 42=744 \mathrm{z}$
$\mathrm{HP46}=7446$
$\mathrm{BP47}=7447$
BP4
HPS
$=7448$
BP51 $=7451$
AP53 $=7453$
BP60 $=746$
$\mathrm{HP70}=7470$
$\mathrm{BP72}=747$
$\mathrm{HP73}=7 \mathrm{7l}$
$\mathrm{BP74}=747$
$\mathrm{BP75}$
$=7475$

| BP 75 |
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| BP 76 |
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$\mathrm{BPP6}=7480$
BP
$\mathrm{BPP}=7$
$\mathrm{BPS}=748$
$\mathrm{BPP1}=7881$
BP82
$=7482$
$\mathrm{BPP}=7483$
$\mathrm{BPB6}=748 \mathrm{~B}$
$\mathrm{BP90}=7490$
$\underset{B P 91}{\mathbf{B P}}=7491$
$\mathrm{BP92}=749$
$\mathrm{BP93}$
$\mathrm{BP94}$
$=7493$
$\mathrm{BP94}$
$\mathrm{HP9}$
$=749$
$\begin{aligned} \mathrm{BP9G} & =7490\end{aligned}$
$13 P 100=: 4104$ RP104 $=7+104$
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$\mathrm{BP192}=7419$ $\mathrm{BP} 193=7419:$ BP196 $=74196$
BP197
$=74197$ BP197 $=74197$
BP198
$=74194$ $\mathrm{BP199}=74199$

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| :---: | :---: | :---: | :---: |
|  |  |  |  |
|  |  |  |  |
| Quad "input pos. NANI) gate |  |  |  |
| (with open collector output) | 0.15 |  |  |
| (eay |  |  |  |
|  |  |  |  |
| (with open collector output) | 0.18 |  |  |
| Hex Inverters |  |  |  |
| Hex Invetter (xith inpen-collector |  |  |  |
|  |  |  |  |
| Triple 3-inpu | - |  |  |
| IJual 4 -- ${ }^{\text {aput Schuitt trigger }}$ | 0.29 | 0.2 | 0.2 |
| Dual 4 -input pos. NANI) gat | 0.15 | 0.14 | 0.12 |
| input pos. NANI gates | 0.15 | 0.14 | 0.12 |
| Dual 4 -fnput pos. NAND in | 0.15 | 0.1 | 0. |
| RCD to decimal nixie driver |  |  |  |
| BCO to decimal decoter ( $4-10$ lines. |  |  |  |
|  |  |  |  |
| BCD-to-seven-segment dec |  |  |  |
| BCD-seven-segment decoder/Uriver* |  |  |  |
| (15V outputs) |  |  |  |
| Expandable dual $\%$-input andror- |  |  |  |
|  |  |  |  |
|  |  |  |  |
| Dialit-wide 2 -input and-ot-incert |  |  |  |
|  |  |  |  |
| Quad 2 -input expardatle and-ur- |  |  |  |
|  |  |  |  |
| wial 4-input expander |  |  |  |
|  |  |  |  |
| Mingle-phase J-K Hip-rlop | 0.29 | 0.26 | 0.2 |
| Master slave J-K flip-Hop, $\quad . \quad 0 \quad 0.29 \quad 0.26$ |  |  |  |
| Dusil Master alave J-K Hip-H!p | $0 \cdot 37$ | 0.35 | 0.32 |
| $\begin{array}{llllllll}\text { Lual D type flip-Hos } & \cdots & \cdots & \cdots & 0.37 & 0.35 & 0.32 \\ \text { Quadt latch }\end{array}$ |  |  |  |
|  |  |  |  |
| 13ual J-K with pre-set amid clear $\quad 0.43$ 0.40 0.38 |  |  |  |
|  |  |  |  |
| 2 bit binary full auders .- .o 0.97 0.94 |  |  |  |
|  |  |  |  |
| Quall full adder | 1.10 | 1.05 |  |
|  |  |  |  |
| BLD decade counter | 0.87 | 0.64 | 0.58 |
|  |  |  |  |
|  |  |  |  |
| \$-bit binary counters | 0.87 | 0.64 | 0.68 |
| bual entry 4 -bit ahitt register | 0.77 | 0.7 | 0.6 |
| $\pm$-hit up-down shift register. |  |  |  |
| - - -hit parallel in parallel out whiftregiater |  |  |  |
|  |  |  |  |
| single $J \cdot \mathrm{~K}$ Hip-flop equivalent ! 000 |  |  |  |
|  |  |  |  |
| single J. K flip fup equivalent 9001 |  |  |  |
|  |  |  |  |
|  | 0.40 | 0.2 |  |
| fisteg master-slave fip-ilopm $\quad \therefore \quad 0.55$ | 0.55 | 0.53 |  |
| Dual dats lock-out flip-fop - $\quad 1.25$ 1.16 |  |  |  |
| Hex net-reset latches | 1.00 | 0.9 |  |
| Hex set-reset latcher, ${ }^{24}$-pin $\quad 1.85$ 1-25 |  |  |  |
|  |  |  |  |
|  |  |  |  |
| BCD-to-decimal decoler/driser o/t 1.50 1.4 |  |  |  |
|  |  |  |  |
| 8 -bit data selectors (with ntrobe) |  |  | 0.8 |
| Dual 4-line-to-1-line data ... $\quad 1.20 \quad 1.10 \quad 0.95$ |  |  |  |
|  |  |  |  |
|  |  |  |  |
| Dual 2 - to 4 -line decrader O/C $\quad \therefore \quad 1-40 \quad 1-30 \quad 1-20$ |  |  |  |
| Syuc. decade counter | 1.80 | 1.70 | 1.60 |
| \&ync. 4-bit binary cound | 1.80 | 1.70 |  |
| sync. up-doum BCD counter $\quad \begin{array}{llll}\mathbf{3} .50 & 3.25\end{array}$ |  |  |  |
| Sync. binary up-thutt counter (wingle clock line) |  |  |  |
|  |  |  |  |
| Sync. up-down lecale counter <br> Sync. binary up-down counter (low |  |  |  |
|  |  |  |  |
|  | 2.10 | 1.8 |  |
|  | 1.80 | 1.70 | 1-60 |
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| 13D | 12p | 11. |
| 18p | 12p | 110 |
| 25p | 240 | 22p |
| 12p | 11 p | 10p |
| 250 | 240 | 229 |
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| Tra |  |  |
| $60 \mu \mathrm{~A}$ | 觡37 | 10V．D．C．．．880 |
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 protection 0／8／30／60／300／600／3000 DC． $0 / 6 / 60 / 120 / 600 / 1200$ V AC $0 / 60 \mathrm{~K} / 6 \mathrm{MEG}$ ． s4．50．P．A P． 18 p ． MODEL TE－18
20，000 O．P．V．0／0．8／6／80／120／ $600 / 1,200 / 3,000 / 6,000 \mathrm{~V}$ ．D．C． $0 / 6 / 30 / 120 / 600 / 1,200$ v．A．C． $600 \mathrm{~K} / 6 \mathrm{Meg} / 60 \mathrm{Meg}$ ． S 5 pF ． 0.2 mFd ． $\mathrm{m}_{5}$ ．071．P．\＆P． 17 ip． TME MODEL TW－50E 46 ranges，mirror scale， $50 \mathrm{~K} / \mathrm{Vol}$ ．
 Volts $125,-25,1 \cdot 25,2-5,5,10$ ． $25,50,125,250,500,1000 \mathrm{~V}$. $50,125.250,500,1000 \mathrm{~V} . \mathrm{D} . \mathrm{C}$ ． Current： $25,500 \mathrm{~A}, 2-5,5,25$. $50,950,500 \mathrm{~mA}, 5,10 \mathrm{amp}$ ．
Realstance： $10 \mathrm{~K}, 100 \mathrm{~K}, 1 \mathrm{MEG}$ Realstance： $10 \mathrm{~K}, 100 \mathrm{~K}, 1$ MEG，
$10 \mathrm{MEG} \Omega$ ．Decibels：-20 to


## HT100BA HOLTI

Features A．C．Current ranges． 100,000 o．p．v． Mirror Scale，Overload protection．
$0 / \cdot 5 / 2 \cdot 5 / 10 / 50 / 250 / 500 /$ 0／2． $5 / 10 / 50 / 25$ AC． 0／10／250 $\mathrm{DA} / 2 \cdot 6 / 26 / 250$ MA／10 A $0 / 20 \mathrm{~K} / 200 \mathrm{~K} / 2 \mathrm{MEG} / 20$
 MEG．
$-20+6$.

## $-20+62 \mathrm{db}$ ．

218．60，P．\＆P．25p．
RUSSIAN 22 RANGE MULTIMETER Model U437 10，000 o．p．v． A frat class verastile In U．S．g．R．to the highest U．S．8．R．to the highest
Btandards．Rances： $2 \cdot 6 / 10 /$ $50 / 250 / 600 / 1000 \mathrm{v}$ D．C． 2.6 10／50／250／500／100v／
DC Gurrent． 100 wA／1／10／
$100 \mathrm{~mA} / 1 \mathrm{~A}$ ．Resiatance
300 ohms $/ 3 / 30 / 300 \mathrm{~K} / 3 \mathrm{M} \Omega$ ． Complete with batteries． test leads，instractions and sturdy steel carrying case． 25p．
$\qquad$ 3 in．tube．Y mp．Benstt Nopist wity $0 \cdot 1 \mathrm{p} p \cdot \mathrm{p} / \mathrm{CM}$ ，Band Fidth 1.5 cps－1．5 MRX Input imp． 2 meg $\Omega 25 \mathrm{pF}$ p．p／CM．Bendwidith 1.5 eps p．p／CM．Bendwidit 1.5 cp
－800K Hz．Input imp． 2 meg $\Omega 20 \mathrm{pF}$ ．Time base 6 ranges $10 \mathrm{cps}-300 \mathrm{KHz}$ Synchronization．Interna external．Illuminated scale $140 \times 215 \times 880$ mm．Weight 151 lb．220／240V．A．C．Supplted brand new with handbook．287－60，Cart． 50 p HOMETWEKL DOLTHETER VT． 100


Can be panel or bench mounted．Basic meter measures I volt D．C．but can be ured to messure a wide range of AC and DC volt， Spectication：Accuracy： $\pm 0.2, \pm 1$ carde． Resolution： 1 mV ．Number of digits： 3 plus fourth overrange digit．Overrange： $100 \%$ （up to 1－999）Inpuit impedance： 1000 Meg ohm．Measuring cycle： 1 per second．Adjust－ ment：Automatic zeroing，full scale adjust－ ment against an internal reference voltage． Overload：to 100 v ．D．C．Input：Fully floating
（ 3 polea）．Input power： （3 poles）．Input power：110－230v．AtC． $\times 83 / 16 \mathrm{fm}$ ．
AVAILABLE BRAND NEW AND FULLY GUARANTEED AT APPROX．HALF £49．97⿺辶 t Carr．50p．

G．W．SMITH
\＆CO（RADIO）LTD． Also see next two pages

## SENI-CONOUGTRS/VAMVES

ALL DEVICES BRAND NEWAND FULLY EUARANTEED

\begin{abstract}

| Transistors |  | 203415 | 22p | 2xucim | ${ }^{35 p}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2N3416 | 27p | 2N5459 | 40p | 16 |
| 20301 | 20] | 2N3417 | 37p | 28102 | 25p | BC116 |
| $2 G 302$ | 20 D | 2 N 3439 | 130p | 28103 | 25p | BC118 |
| $2 \mathrm{G303}$ | 20p | $2 \mathrm{~N}^{3440}$ | 97p | 28104 | 5 | BC119 |
| 269306209308 | 80 p | $2{ }^{2} 3564$ | 17p | 28301 | 60p | BC121 |
|  | 80 D | 2N3565 | 15p | 28302 |  | 8C12z |
| 20309 | 30p | 2N3668 | $22 p$ | 28303 | 60 | BC125 |
| 20371 | 15 | 2N3568 | 25 D | 28304 |  | BC126 |
|  | 20 p | 2N3569 | 25 p | 28501 | 38 | BC134 |
| $\begin{aligned} & 29374 \\ & 29381 \end{aligned}$ | 22p | 2N3570 | 125p |  | 97 | ${ }^{\text {RC135 }}$ |
| 2N388A | 48p | 2N3572 | 97 p | 28.503 | 27p | BC136 |
| 2 N 404 | 20 D | 2N3605 | 27] | 3N8 |  | BC137 |
| 2N696 | 15p | 2N3806 | 97p | 3N128 | 70 | ${ }^{\text {BCl }} 38$ |
| 2N697 | 150 | 2N3607 | 22 D | 3N140 |  |  |
|  | 25 p | 2N3638 | 18p | 3N141 | 72. |  |
| $\text { 2N } 699$ | 30p | 2N3638 | 20p | 3N142 |  |  |
|  | 10p | 2 N 3841 | 18p | 3N143 | 67 |  |
| $\begin{array}{ll} 2 N 706 & 1 \\ 2 N 706 A & 1 \end{array}$ | 12D | 2N3642 | 18p | 3N152 | 87 |  |
| $2 \mathrm{N708}$ | 12 p | 2N 3643 | 20p | 40050 | 55 | BC152 |
| 2N709 | 45p | 2N3644 | 250 | 40250 |  | BC153 |
| 2N718 | 25 p | 2N3645 | 25p | 40251 | 32p | BC154 |
| ${ }_{2}^{2 N 7184}$ | 30p | 2N3691 | 15p | 40309 | 32p | HC157 |
|  | 25 p | 2N3692 | 18p | 40310 | 45 p | BC158 |
| $2 \mathrm{~N}^{2} 727$ | 250 | 2N3693 | 15 p | 40311 | 85p | BC159 |
| 2N914 | 170 | 2N3694 | 18p | 40312 | 47p |  |
|  | 170 | 2N3702 | 10p | 40314 | 87 p | BC |
| 2 N 918 | 30p | 2N3709 | 10p | 40315 | 87 p | BClbsB |
| 2N929 | 22. | 2N3704 | 12D | 40316 | 470 | ${ }_{8 C 1}$ |
| 2N930 | 20p | 2N3705 | 100 | 40317 | 37 p | BC |
|  | , | 2N3706 | 10 p | 40319 | 55p | BC |
| $\begin{aligned} & \text { 2N937 } \\ & 2 \mathrm{~N} 1090 \end{aligned}$ | 22p | 2N3707 | 12p | 4032 | 47 p | BC |
| $\begin{aligned} & \text { 2N1091 } \\ & \text { 2N1181 } \end{aligned}$ | $2{ }^{2}$ | 2N3708 | 10p | 40323 | 38. | BC171 |
|  | 25 b | 2N3709 | ${ }^{10} \mathrm{p}$ |  |  |  |
| 2 N 1132 | 25 | 2N3710 | 109 | 40328 | 37 D | BC |
| ${ }_{2}^{2 N 1302}$ | 17. | 2N3711 | 10p | 40329 |  | $\mathrm{BCl}^{\text {d }}$ |
|  | 17. | 2N3713 | 187p | 40344 | 570 |  |
| 2 N 13042 N 1305 | 28D | 2N3714 | 200p | 40347 | 578 | ${ }_{\text {BC }} \mathrm{BC}$ |
|  | 82p | 2N 3715 | ${ }^{820} \mathrm{D}^{28}$ | 40348 | ${ }^{62 \mathrm{p}}$ | ${ }_{\text {BC182 }}$ |
| ${ }^{2} \mathrm{~N} 131306$ | \% 25 | 2N3716 | ${ }_{2400}^{285 p}$ | 40360 40361 | 40 p | $\begin{aligned} & \mathrm{BC} 182 \mathrm{~L} \\ & \mathrm{BCl} 88 \end{aligned}$ |
| 2N1307 2 | 25 p 250 | $\begin{aligned} & \text { 2N3773 } \\ & 2 N 3791 \end{aligned}$ | 875p | ${ }_{40362}$ | 50 p | BC183L |
| 2N1309 | 25 p | 2N3819 | 34D | 40370 | 38 p | BC184 |
| $\begin{aligned} & 2 \mathrm{~N} 1507 \\ & 2 \mathrm{~N} 1613 \end{aligned}$ | 17D | 2N3820 | 55 | 40406 | 57 p | BC184L |
|  | 20 D | 2N3823 | 50 D | 40407 | 40 D |  |
| 2 N 1631 2N1632 | 35p | 2N3854 | 270 | 10408 | 68 p | ${ }^{\text {BC }}$ |
|  | 300 | 2N3854A | 27\% | 40408 | 55 p | ${ }_{\text {BC212L }}$ |
| 2 N 1837 | 80 p | 2N3855 | 270 | 40410 | 82p | BC213L |
| 2N1838 | 87) | 2N 3855 A | 30p | 40412 | 50D | ${ }^{\text {BC2 }}$ B 145 |
|  | D | 2N3856 | 80D | 4046 | 57 D |  |
| ${ }_{2}^{2 N 17011} 10$ | 162 D | 2 3858 | 35p | 40468 | 35 D | BCY |
|  | 849 | 2N 3858 | 25 p | 40528 | 72p |  |
| 2N1889 | 82p | 2N3858A | 80 | 40800 | 578 | BCY32 |
| ${ }_{2} 2 \mathrm{~N} 18147$ | 37p | 2N3859 | 27D | 40603 | 50 p | BCY 33 |
|  | 72p | 2N3859A | 32p | AC107 | 80 p | BCY34 |
| 2 N 2160 | 87 D | 2N3860 | 30 D | AC126 | 20 P |  |
| $\begin{aligned} & 2 \mathrm{~N} 2193 \\ & 2 \mathrm{~N} 2193 \mathrm{~A} \end{aligned}$ | 40 p | 2N3866 | 150 p | AC127 | 24D | BCY39 |
|  | 42p | 2N3877 | 40 D | AC128 | 80p | BCY |
| $\begin{array}{ll} 2 N 2194 \\ 2 \\ 2 N 2194 A \\ 8 \end{array}$ | 27p | 2N 3877 A | 400 | ${ }^{\text {AC151 }}$ | 18p | BCY41 |
|  | 80 | 2N3900 | 87 P | ${ }^{\text {AC152 }}$ | 28 p | BCY |
| $\begin{aligned} & 2 N 2217 \\ & 2 N_{2218} \end{aligned}$ | 25p | 2N3900A | 40D | AC154 | 22 p | BCY43 |
|  | 20 D | 2N3901 | ${ }^{978}$ | ${ }^{\text {AC176 }}$ | 20 p | ${ }^{\text {BCY54 }}$ |
| $2 \mathrm{~N}^{2} 219$ | 20 p | 2N3903 | 80 p | AC187 | 25 D |  |
| ${ }_{2} 2 \mathrm{~N} 2222018$ | 25 p | 2N3904 | 25p | AC188 | 25p | BCY59 |
|  | 25p | 2N3905 | 80 D | ACY17 | 27p |  |
|  | 20 p | 2N3906 | 25 p | ACY18 | 24p | BC |
|  | 25 p | 2N4058 | 12 D | ACY19 | 24 p | BCY71 |
| ${ }^{2} 2 \mathrm{~N} 22978$ | 30 p | 2N4059 | 10p | ACY20 | 20p | BCY72 |
|  | 15p | 2N 4060 | 12p | ACY21 | 20p | ${ }^{\text {BCY78 }}$ |
| $\begin{array}{ll} 2 \mathrm{~N} 2369 \\ 2 \mathrm{~N} 2369 \mathrm{~A} \\ 1 \end{array}$ | 15 p | 2N4061 | 12 D | ACY2 | 10p | BCY79 |
|  | 15 p | 2 N 4062 | 12p | ACY | 17p | BCZ10 |
| ${ }^{2} \mathrm{~N} 2410$ | 42p | 2N4244 | 47 D | ACY 39 | 47p | BCZ11 |
|  | 27p | 2N4248 | 15p | ACY40 | 14p | BD112 |
|  | 32p | 2N 4249 | 15p | ACY41 | $15 p$ | BD116 |
|  | 22p | 2N4250 | 18p | ACY44 | 2 | BD121 |
| $2 N 2540$ | 22 | 2N4254 | 42D | AD140 | 47 p | BD123 |
| 2N2613 | 35p | 2N4255 | 42 D | AD149 | 47p | BD124 |
|  | 30 p | 2M 4284 | 17 D | AD150 | 62 p | BD131 |
| ${ }^{2 N} 2 \mathrm{~N} 2614$ | 47p | 2N4285 | 17 p | AD161 | ${ }^{35}$ p | BD132 |
| 2 N 2711 | 25p | 2N4288 | 178 | AD162 | 45 | BDY 10 |
| ${ }_{2}^{2 N^{2} 2712}$ | 25p | 2N4287 | 17p | A F109 | 45p | BDY20 |
|  | 27 | 2N4288 | 15 p | AF114 | 5 | BDY81 |
| 2N2714 | 30 p 20p | 2N4289 | 12p | AF115 |  | BDY62 |
| $\begin{aligned} & 2 N 2904 \\ & 2 N 2904 \mathrm{~A} \end{aligned}$ |  | 2N4290 | ${ }^{12} \mathrm{p}$ p | AF116 | $25 p$ $20 p$ | ${ }_{\text {BF115 }}$ |
| 2 N 2905 A | 25p | 2N4292 | 15 p | AF18 | 44 p | BF152 |
| ${ }_{2 \mathrm{~N}} \mathbf{N} 290068$ | 20p | 2N4294 | 17D | AF121 | $80 p$ | BF154 |
|  | 20 p | 2N4303 | 47p | AF124 | 29p | BF158 |
| $2 \mathrm{~V}^{29064} 45 \mathrm{D}$ |  | 2N4964 | 15p | AF125 | 19p | BF159 |
|  |  | 2N4965 | 18p | AF128 | 16p | BF163 |
|  |  | 2N5027 | 52 D | AF127 | 88 | BF167 |
| 2 N 2924 | 15p | 2N5028 | 57p | AF139 | ${ }^{28 p}$ | BFi70 |
| 2 N 2925 | 15p | 2N5020 | 47p | AF178 | 42p | BF173 |
| 2 N 2926 G |  | 2N5030 | 42p | AF179 | 450 | Br177 |
|  |  | 2N5172 | 12p | AF180 | ${ }^{50} \mathrm{p}$ | BF178 |
| 2 N 2926 Y | 12p | 2N5174 | ${ }^{68} \mathrm{~s}$ p | AF181 | 401 | BF179 |
|  | 20p | 2N5175 | 52 D | AF188 | 89 D | BF180 |
| 2 N 3014 | 25 p | 2N5176 | 450 | A F239 | ${ }^{30}$ | BF181 |
| 2 N 3003 | 20 p | 2N5232 | 30 | AF279 | 479 | ${ }^{\text {BF }} 182$ |
| N3054 | 49p | 2N5245 | 45p | AF280 | 47p | ${ }_{\text {PF184 }}$ |
|  | 72 p | 2N5246 | 48 y | AFZ11 | 32 p | ${ }_{\text {BF1 }} \mathrm{BF185}$ |
| 2 N 3133 | 250 | 2N5249 | ${ }^{77 \%}$ | A8YY2 | 25 | BF194 |
| N3134 | 80 D | 2N5265 | 225p | A8Y27 | ${ }^{30 p}$ | ${ }_{\text {BF196 }}$ |
| N3138 | 25p | 2N5305 | ${ }^{37} \mathrm{D}$ | A8Y28 | 24 p | BF196 |
|  | 25 p | 2 N 6306 | 40 D | A8Y49 | 27p | BF197 |
| 2N3990 | 25p | 2N5307 | 87 p | AsY50 | 25 p | BF198 |
| 2N3391 | 800 | 2 N 5308 | 37 D | AAY 61 | 32 p | Br200 |
| 2 N 3391 A | 80 p | 2 N 5309 | 82p | AsY54 | 25 | BF224 |
| 2N3392 | 170 | 2N5310 | 420 | ASY67 | 45 | BF225 |
|  | 15p | 2N6354 | 27 p | A8Y86 |  | BF297 |
| 2 N 3398 | 15p | 2N5355 | 27p | A8Z21 | 51 | $\mathrm{BF}^{\text {BF238 }}$ |
| $\begin{aligned} & 2 N 3402 \\ & 2 N 4403 \end{aligned}$ |  | 2N5356 | 82 D | AUY10 | 50 p | 8F244 |
|  |  | 2N5368 | 47p | BC107 | 10 D | BFW61 |
| $\begin{aligned} & 2 N 3404 \\ & 2 N 3400 \end{aligned}$ |  | 2N 5366 | 38D | BC1 | 1 | BFW87 |
|  |  |  |  |  |  |  |



| integrated Circuits |  |  |  | ${ }^{20 p}$ |
| :---: | :---: | :---: | :---: | :---: |
|  | FJH111 | 70p | SN7440 | D |
|  | PJH121 | 250 | SN7441AN |  |
| CA3000 180D | PJH131 | 25p |  | 750 |
| C.A3005 1170 | FJH141 | $25 p$ | SN7442 | 750 |
| CA3007 282p | FJH151 | 250 | 8N7446 | 00D |
| CA3011 750 | FJH161 | 70 D | SN 7447 | 186 |
| CA3012 88p | FJH 171 | 85 D | 8N7448 | 1250 |
| CA3013 105D | FJH181 | 250 | SN7450 | 20p |
| CA3014 124D | FJH221 | 25p | BN7451 | 20p |
| CA3018 84p | FJH231 | 25. | SN7453 | , |
| CA3018A | FJH241 | 25. | SN74 | 80 p |
|  | PJH251 | 85D | ENT 7460 | 20 p |
| Ca3019 84D | FJJ 101 | 80 p | SN74 | 30 p |
| CA3020 128p | FJJ111 | \$0p | SN747 | 40 p |
| CA3020A | FJJ121 | 60 p | 8N747 | 40 p |
|  | FJJ131 | 60 p | SN747 | 5 p |
| CA3021 156p | FJJ141 | 125 p | 8N7478 | 45p |
| CA3022 180p | FJJ 181 | 750 | 8N7483 | 87 |
| A3023 126p | FJJ 191 | 65 p | GN7486 | 83p |
| A3026 100p | FJJ 211 | 125p | SN7490 | $87{ }^{\circ}$ |
| CA3028A 74p | FJJ251 | 125 | SN7492 | 7p |
| CA3028B ${ }^{\text {cosp }}$ | FJL101 | 125 p | gN7498 | 7 |
|  | FJ Y 101 | $25 p$ | SN7495 | 87 |
| CA3029 87p | IC10 | 250 p | 8N | 87p |
| $\mathrm{CA} 3029 \mathrm{~A}_{105 \mathrm{p}}$ | $1 \mathrm{Cl2}$ | 250 p | gN74107 |  |
|  | L900 | 40 p | EN 74153 140p |  |
| CA3030 137 p | L914 | 40p |  |  |
| CA3036 128p | L923 | 40p | EN74164 |  |
| CA3036 72p | MC724 ${ }^{\text {P }}$ | 60p |  | 220p |
| A3039 82p | MC780P | 247p | SN 74160 |  |
| 43041 109p | MC788P | 148p |  | 180p |
| A3042 109p | MC790P | 124 p | SN 74161 |  |
| CA3043 187p | MC792P | -66p | 8N74164 |  |
| CA3044 120p | MC799P | -88p |  |  |
| CA3045 198p | MC1303L |  |  | p |
| CA3046 81p |  | 100p | SN74165 |  |
| CA3047 1879 | M |  |  |  |
| CA 3048 204p |  | 225p | SN 74192 |  |
| CA3049 1805 |  |  |  | 175p |
| CAS050 185p |  | 886 | SN74193 |  |
| 3051 134D |  |  | TAA241 |  |
| A3053 46p | MCl435 |  |  | 182. |
| CA3054 1090 |  | 8450 | TAA242 |  |
| CA3055 840p | MC15520 |  |  | 425p |
| CA3059 165D |  | 461p | TAA243 | 00 |
| CA3064 180p | MC17000 |  | TAA263 | 750 |
| FCH101 850 |  | ${ }^{94} \mathrm{p}$ | TAA293 | p |
| FCH 1111050 | MFC400 |  | TAAS00 | 1750 |
| FCH121 1050 |  | 75 p | TAA310 | 125 p |
| FCH131 50p | PA222 | 260 D | TAA320 | 72p |
| FCH141 1050 | PA230 | 140 p | TAA360 | 175p |
| FCH 1611050 | PA234 | 98 D | TAA435 | 7 p |
| FCH161 500 | PA237 | 210 D | TAA621 | 88D |
| FCH171 105p | PA246 | 1600 | TAA522 | 860p |
| FCH181 105p | PA424 | 2850 | TAA530 | 495p |
| FCH191 1050 | PA264 | 1900 | TAA811 | 45p |
| FCH201 180p | PA265 | 200 D | TAB101 | 97 D |
| FCH211 180D | gN7400 | 20p | TAD10 | 150p |
| FCH221 130p | SN7401 | 200 | TAD110 | 150 p |
| FCH231 1500 | SN7402 | 20 p | 8L408D | 150p |
| FCJ 101 180p | SN7403 | 20 p | 8L702C | 147p |
| FCJ111 1500 | EN7404 | 20 p | UA702 | 280p |
| FCJ121 875p | 8N7405 | 20 p | UA7020 | 77p |
| FCJ131 8750 | SN7406 | 80p | UA703C | 187p |
| FCJI41 525p | SN7408 | 20 D | UA709 | 125 p |
| FCJ201 100p | 8N7409 | 20p | UA710C | 185p |
| FCJ211 8750 | SN7410 | 800 | UA716 | 187p |
| FCK 101480 p | 8N7411 | 23p | UA723 | 162p |
| FCL101 230p | 8N7413 | 30 p | UA7 | 80p |
| FCY101 102p |  | 20p | A7 | 87 |
| BRIDGE |  | 50 PIV 4A |  | 80p |
| RECTIFIERS |  | 100 PIV 4A |  | 70p |
| PLASTIC |  | 200 PlV 4 4 |  |  |
| ENCAPSULATED |  | 400 PIV 4A |  | 750 |
| b00 PIV 1A | 50 p | 50 PI | V6A | 62p |
| 50 PIV 2A | 55p | 100 PI | V 6A | 75 D |
| 100 PIV 2A | 80 p | 200 PI | IV 6A | 75p |
| 200 PIV 2A | ${ }^{65} \mathrm{p}$ | 400 PI | IV 6A | 100p |
| 400 PIV 2A | 750 |  |  |  |

SILICOR RECTIPIERS
MINIATURE WIEE ENDED PLASTIC SERIES SERIES SEREIES
400150 PIV
4002100 PIV
4004400 PIV
4005600 PIV
4006800 PIV
40071000 PIV
BILCON RECTIFIER
BTUD MOUNTING


VALVES

| OA2 | 38p | 25 Z | 80p | EL93 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| OB2 | 46 p | 2525 | 42D | EM80 |  |
| OZ4 | 30 p | $25 z 6$ | 85p | EM81 | 60p |
| L4 | 20p | 30C15 | 80 p | EM84 |  |
| LR5 | 40 p | 30 C 17 | 90 p | EM8 | . 00 |
| 185 | 80 p | 30 Cl 18 | ${ }^{80 p}$ | EM87 | ${ }^{70}$ |
| IT4 | 25p | 30 Fs | 85p | EY5 |  |
| IU4 | 30p | 30 FL | ${ }^{75}$ | EY8 | 40D |
| 1 U |  | 30FL12 | 120p | EY87 | P |
| 2 D 2 | D | $30 \mathrm{FL14}$ | 95p | EZ40 |  |
| 3 Q 4 | 50p | $30 \mathrm{L15}$ | 85 p | EZ41 |  |
| 384 | 85 D | 30 L 17 | 80 p | Ez80 |  |
| 3 V 4 | 480 | 30 Pl 12 | 80 | Ez81 |  |
| 6R4 | 759 | $30 \mathrm{P19}$ | 85 D | az32 | 8D |
| 5 U 4 | 85 | 30 PLl | 750 | Oz34 |  |
| 5 V 4 | 45 D | $30 \mathrm{PL13}$ | 98p | K T60 | 22.05 |
| 5 Y 3 | , | $30 \mathrm{PL14}$ | 90 | K 78 |  |
| za | 40 p | 35 L 6 | 50p | MU14 |  |
| 8/30L2 | 80 p | 35 W 4 | 35p | Pabcs | 40 D |
| 6AC ${ }^{\text {a }}$ | 40 p | 35 Z 4 | 85D | PC8 |  |
| 6 6AG7 | 900 | $33 \mathrm{z5}$ | , | PC8 | 0 |
| 6AKb | . | 50 B 5 | 0 D | PC97 | 5p |
| 6AK6 | p | 50Cit | D | PC900 | D |
| 6aL5 | 0 D | 80 | $55^{\text {d }}$ | PCCA 4 | 0 p |
| 6AM6 |  | 85 A |  | PCC85 | 0 |
| 6 AQ | 88D | 807 | 50 D | PCC88 |  |
| ${ }^{8186}$ | 40 D | 1625 | 50 p | PUC8 | O |
| 8AT8 | 850 | 5763 | 70 p | PCC188 |  |
| 8AU6 | 25 p | 6146 | 160 | PCF80 | 0 D |
| 6AV6 | 30p | Az3! | p | PCF82 | 4p |
| 6BA6 | 259 | CY31 | d | PCF84 |  |
| 6BE6 | 30 p | Daf9 | 30p | PCF |  |
| ${ }^{68 \mathrm{BH}} 6$ | 750 | DAF9 | 45 | PCP80 | 0p |
| 6BJ6 | 50p | DF91 | 22p | PCF801 | 50 D |
| 6BQ7 | 40p | DF96 | 45p | PCP802 | 50p |
| 6BR7 |  | DK91 | 40p | PCF805 | 80 |
| $6 \mathrm{BR8}$ | 70p | DK92 | 55p | PCF808 |  |
| 6BW6 | 85p | DK9 | 50 p | PCH808 | 75 |
| 6BW7 |  | DL92 | 855 | PCL82 |  |
| ${ }^{8 B Z 8}$ | 40 p | DL94 | 48p | PCL83 | D |
| 6 C 4 | 33p | DL96 | 45 p | PCLS 4 | 5 D |
| bcidi | 125p | DM70 | 40D | PCL | D |
| 6 CL 6 | 50p | DY86 | 32 y | PCL86 | D |
| 8CW | 65p | DY87 | 33p | PFL20 | D |
| ${ }_{6} \mathrm{Pr}^{1}$ |  | E88CC | 100 p | PL36 | 5 |
| 3FGO | 35p | E180F | 100p | PLs1 | 0 |
| 8 F 13 | 45p | EABC80 | 95p | PLS2 | 5 |
| $\mathrm{BFP}^{4}$ | 70p | EAF42 | 35p | PL83 | 5 |
| 6 F 15 | 5p | Eb91 | 20p | PLS4 |  |
| 6 F18 | 50 p | EBC41 | 55D | PL500 | 5 |
| $\mathrm{BPF}_{23}$ | 85p | EbC81 | 30p | PL504 | D |
| 6H6 | 17p | EbF80 | 40 | PY32 | 5 |
| 6J4 | ${ }^{50} \mathrm{p}$ | EbF83 | 0 D | PY33 |  |
| 6 J 5 | 25 D | EBF89 | 82p | PY80 | , |
| 6.50 | 30 p | EBL21 | 80 p | PY81 | D |
| 6 J 6 | 20 D | EC86 | 60 D | PY82 | 5 |
| 6.J7 | 45p | EC88 | 60 D | PY83 | 8 D |
| $6 \mathrm{K89}$ | 40 D | ECC40 | 65p | PY88 | 0 |
| 6L6GT | 45 p | ECCS4 | 301 | PY800 | D |
| 6LD2 | 50 p | ECC85 | 40 p | PY801 | OTo |
| 687 | 40 p | ECC88 | 40 D | U25 | D |
| 69A7 | 40p | ECF80 | 85 p | U26 | 0 |
| 6897 | 40 p | ECF82 | 85 y | U50 | D |
| J7 | 40 p | ECF86 | 85 | U52 | 5 |
| $6 \mathrm{sk7}$ | 40p | ECH21 | 578 | U191 | d |
| 68.7 | 350 | ECH35 | 100p | U281 | 40 |
| $6 \mathrm{6N7}$ | 研 | ECH42 | 750 | U282 |  |
| 68 Q 7 | 40 p | ECH81 | s0p | U301 |  |
| BU4 | A | ECH83 | 45 D | U801 |  |
| 9V69 | 25 D | ECL80 | 45p | UABC80 | 0 |
| ${ }^{8} \mathbf{V} 6 \mathrm{G}$ | 82p | ECL82 | 85 D | UAF42 | 55 |
| $6 \times 4$ | 85D | ECL83 |  | UBC41 |  |
| 6x5c | 800 | ECL86 | 40 D | UBC81 | \% |
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| 10 P 13 |  | EF41 | 5 p | Ucc8s | 0 |
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| $12 \mathrm{AT7}$ | d | EF85 | 85 p | UCH42 | 70 |
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$\begin{array}{ll} \pm 1.75 & \text { PA7 } 6 T R \quad 16 \mathrm{~V} 7 \mathrm{~W} \\ £ 2.12 & 608\end{array}$ 4TR $£ 2.47 \quad 4104 \mathrm{TR} 28 \mathrm{~V}$ loW MPAI2/15 6TR MPV 12 W 6TR I8V I2W 64.50 OPTIONAL POWER SUPPLIES $5 \cdot 25$ Post, etc. 20p P500 (1 or 2) for 104, 304
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PROJECT 60
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[^1]:    Importers and Distributors
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[^2]:    Fig. 19: Circuit of the preamplifier for use with microphones with

[^3]:    F.M. Stereo Tuner ( $\mathbf{I 2 5}$ ) \& A.F.U. Filter Unit (E5.98) may be added as required

[^4]:    20 WATT I.C. AMPLIFIER Toshiba 20
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