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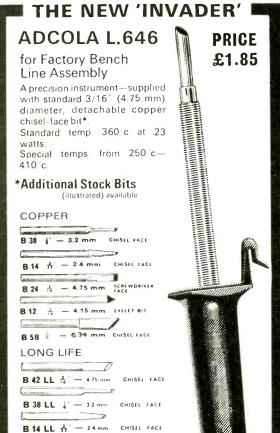
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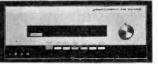
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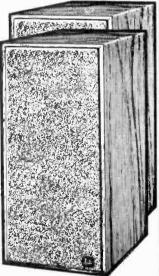
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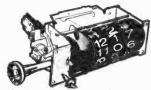
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Ready built and tested—just plug in a PP3 battery and 'phones and it's working. Put it in a case,

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384	-26	30C18	-61	EAF42	-50	EM84	.32	PCL85	.38	UBF80	.34
3 V 4	-37	30F5	-69	EB41	-40	EM87	-36		-39	UBF89	-32
5U4G	-26	30FL1	-61	EB91	-11	EY51	.33		-65	UCC84	-33
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5 Y3GT	-26	30FL14	-88	EBC41	.54	EZ40	-43		-77	UCF80	-33
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6/30L2	-54	30L15	-57	EBF80	-32	EZ80		PFL20t		UCH81	-32
6AL5	.11	30L17	-71	EBF89	-29	EZ81	.23	PL36	.49	UCL82	.32
6AM6	-13	30P4	-57	ECC81	.17	GZ30	.35	PL81	-44	UCL83	-55
6AQ5	.22	30P12	.72	ECC82	-20	(1Z32	.40		-49	UF41	-56
6AT6	.20	30P19	.57	ECC83	.35	GZ34	-48	PL82	-31	UF89	-30
6AU6	.20	30PL1	.63	ECC85	-26	KT41	.77	PL83	-33	UL41	-57
6BA6	-20	30PL13	.75	ECC804	-54	KT61	.55	PL84	.30	1"L44	£1.00
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6BW7	.52	35L6GT	-45	ECH35	.30	LN329	-72	PM84	-35	UY41	.42
6CD60 #		35 W 4	-25	ECH42	-61	LN339	.63	PX25	£1-00	UY85	-25
6F14	-42	35Z4(1T	.25	ECH81	.29	N78	-87	PY32	- 55	VP4B	-77
6F23	-68	807	-45	ECH83	-40	P61	.45	PY33	.55	277	-22
6F25	- 57	6063	-62	ECH84	-36	PARC80	-34	PY8L	-25	Transi	
6K7G	-12	AC/VP2	-77	ECL80	.30	PC86	.47	PY82	.25	ACI07	-17
6K8G	.17	B349	-65	ECL82	.31	PC88	.47	PY83	+28	AC127	-18
6Q7G	.27	B729	-62	ECL86	-36	PC96	.42	PY88	.33	AD140	-37
68N7GT	-30	CCH35	-67	EF39	-38	PC97	.39	PY800	-34	AF115	-20
6V6G	.23	CY31	.30	EF41	-60	PC900	- 33	PY801	.34	AF116	-20
6V6GT	.31	DAF91	.22	EF80	-23	POC84	-29	R19	-30	AF117	-20
6X4	-23	DAF96	-36	EF85	-28	PCC85	.27	R20	.56	AF118	-48
6X5GT	.28	DF33	-38	EF86	.30	PCC88	-42	U25	-64		-17
7B7	-33	DF91	-16	EF89	-26		-45	U26	-56	AF127	-17
10P13	.58	DF96	-36	EF91	.13	PCC189	-48	U47	-64	OC26	-25
12AT7	.17	DH77	-20	EF98	-65		- 56	U49	-56	OC44	-12
12AU6	.20	DK 32	.33	EF183	-28	PCF80	-28	U50	- 26	OC45	.12
12AU7	-20	DK91	.28	EF184	.31	PCF82	.31	U52	-31	OC71	-12
12AX7	.22	DK92	.38	EH90	-37	PCF86	.45	U78	-24		-12
19BG60	-87	DK96	.38	EL33	-55	PCF800	-58	U191	-59		.12
20F2	-67	DL35	-40	EL34	.45	PCF801		U193	.42	OC81	-12
20P3	-80	DL92	-26	EL41	.54		-40	U251	.66	0C81D	.12
20P4	.92	DL94	-37	EL84	.23	PCF805	.61	U301	-38	OC82	-12
25LaGT	-20	DL96	-38	EL90	-26	PCF806	.58	U329	-66	OC82D	-12
25U4GT	.57	DY86	.25	EL95	.33	PCF808	-68	U801	-98	OC170	.22

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Gaivometer 20-0-20 f.s.d. moving coil precision laboratory instrument of extremely high sensitivity (3 × 10·7 A per division), Bize approx 6½ × 2½ × 2in. Price 35.

Acos. 49 Meters. For use with Acos transducers and accelerometers or others of any make provided they have a sensitivity of not less than 17:5mV. per g² and a linear output over the frequency range under investigation.

This is a precision instrument. It measures g² in three steps, 0-10, 0-100 and 0-1000 directly on a large clear meter scale 0-1. We have two models. Standard Model (ID001). Price 312 and: Auto cutout model (ID001) which has an inbulit circuit with relay to trip the external circuit (trip level is adjustable by a control which is virtually linear with the meter scale). The tripload may be up 2a. Once the circuit has been tripped it can be restored by a reset button. Price of this model is 318. Please note also we have Acos Transducers ref. no. ID1001 in stock. Price 34 each.

Parmeko Meptune Beries C. Core Transformers and accessed, stove enamelled black, upright mounting. All have normal 50eps. primary 230/240v. with primary screen and as two and unuses collows: Model 86, 100 of 100 o

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Price per each
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1 Watt 1p 8p 6p 8p
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7 transistor Keychain Radio in very pretty case, size 2½×2½×1½in.—complete with soft leather zipped bag. 7 transistor, ferrite rod. Loudspeaker.

Loudspeaker.
In transit from the East these sets suffered corroeion as the batteries were left in them but when this corrosion is cleared away they should work—offered without guarantee except that they are new. Price only \$1.25 cless batteries plus 18p. poat 6 for 87 post free. Pair of rechargeable batteries and charger \$5p.





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You will be amased at the
fullness of reproduction and at
the added qualities your records
or tuner will reproduce. Built
into metal cabinet elegantly
to blend with modern furnishings, this amplifier uses
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controls—also switching for Mono to Stereo, tuner or pick-up. Other controls
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UNREPEATABLE PRICE is £9 plus 38p post and insurance.

_ THIS MONTH'S SNIP .



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Test continuity for any low resistance circuit, house wiring, car electrics. Tests polarity of diodes and rectifiers. Also ideal size for conversion to signal injector (circuit supplied) 30p or 2 for 50p Post paid.

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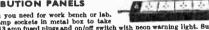
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This heater unit is the very latest type, most
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be fitted into any fietal line case or cabinet. Only
need control switch. \$2.50. 2kw. Model as above
except 2 kilowatis \$25.0. 2kw. Model as above
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Control Switch \$55. P. & P. 40p.

CENTRIFUGAL FAN



Mains operated, turbo-blower type. Pressed steel Housing contains motor and aluminium impeller. Motor is 1/10th hp giving considerable air flow but virtually no noise. Approx. dimensions 101" wide by 12" dia. Outlet into trunking 104" × 44". 44.95 + 41.

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Just what you need for work bench or lab.

4 × 13 amp sockets in metal box to take
standard 13 amp fused plugs and on/off switch with neon warning light. Suppled
complete with 7 feet of heavy cable. Wired up ready to work. 32 less plug
\$2.25 with fitted 13 amp plug; \$2.40 with fitted 15 amp plug, plus \$23p P. & I.

CAPACITOR DISCHARGE CAR IGNITION



This system which has proved to be amazinefficient and reliable was first described in the W emercht and reliable was met described in the wise less World about a year ago. We can supply kit of parts for improved and even more efficient version, price \$4.95. When ordering please state whether for positive or negative systems. Plus 30p post.

15 WATT 12in. HI-FI SPEAKER

15 WATT 12in HI-FI SPEAKER. Is undoubtedly one of the finest loudspeakers that we have ever offered, produced by one of the country's most famous makers. It has a die-cast metal frame and is strongly recommended for Hi-Fi and public address. Handling 15W R.M.S.—Cone moulded fibre—Freq, response 30

10,000 c.p.s.—specify 3 or 15 ohms. Chassis diam. 12in—12in over mounting lugs. Overall height 5in. A £10 speaker offered this month for £3.75 plus 30p. post and ins.

2 OCTAVE MINI ORGAN

As featured in this issue. Send S.A.E. for list of parts.

J. BULL (ELECTRICAL) LTD.



Numbestor Tubes. For digital instruments, counters timers, clooks, etc. Hi-vao XN, S. Price \$1.46 each. 10 for \$1.8.

Pressure Switch (Containing a 15 amp. change over switch operated by a disparan which in turn is operated by air pressure through a small metal tube. The operating pressure is adjustable but is set to operate in approx. 10 in. of water. These are quite low pressure devices and can in fact be operated simply by blowing into the inlet tube. Original use was for washing machines to turn off water when tub has reached correct level but no doubt has many other applications. Sup each. 10 or \$4.45 times Extractor Fans. Beautifully made again and the second correct level but no doubt has many other applications. Sup each. 10 of \$4.45 times Extractor Fans. Beautifully made again and the second computers but suitable for any equipment. Size \$4 in. square and 1\frac{1}{2} in. thick. Frice \$3 each. Post and insurance 20p.

Commutator Motor. Small. Size approx. Sin. plus 110. of \$4.45. Sin. high \times \ti 10 for \$18.

Snap Action Slide Switch, Rated 5a. 240v. Made by Arrow. Type fitted in the handles of electric drills, vacuums, etc. 5p each, 10 for 45p. Numicator Tubes. For digital instruments, counters

ocks, etc. Hi-vac XN, 3. Price #1-45 each.

Insurance 284 kr. Glock Switch. In metal case with 13 amp. 284 kr. Glock Switch. In metal case with 13 amp. socket Smiths movement, 2 ons and 2 offs per 24 hours. Very neatly made and finished. Original retail price 27 cach. Few only, new and perfect.

hours. Very nestly made and dnished. Original retail price \$7 each. Few only, new and perfect. \$4.00 each.

F.E. Gemini Amplifier. This amplifier is a \$0 × 30 wait stereo amplifier and pre-amplifier of exceptionally high performance. The performance is certainly equal to anything one can buy no matter what the cost. The P.E. Gemini has been designed for both hid applications and for use with discotheques and forthis reason, has a microphone input that can be mixed with any other input. The amplifier is designed and is thus capable of driving two Quad electrostatic speakers and is thus capable of driving any other speakers and is thus capable of driving any other speakers and is thus capable of the correct impedance. We offer the complete kit cabinets at \$45\$. Price list including reprint of that. \$59 poet paid.

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Condensers. Another addition to our range. 500uF at 50v. 159 each. 10 for \$1.25.

Thermistor Bead Type. For instruments, medical applications, etc. ITT No. GLOS, 759 each. 10 for \$6.75.

Core Mains Leads. Special offer this month is a 5tt. lead with 23/36 cores and coloured according to the new code i.e. Brown—live; Yellow/Green—earth; Blue—neutral. Price \$9 each or 10 for \$59.

P.W. Constructor Projects

As described in this and past issues. We can probably supply components. Send S.A.E. for list, naming project.

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Complete Kit (except wooden battens) to make the metal detector as the circuit in Practical Wireless August issue. \$2.95 plus 20p post and insurance.

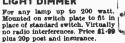
MAINS RELAY BARGAIN

MAINS RELAY BARGAIN
Special this month are some single,
double and treble pole changeover
relays. Contacts rated at 18 amps.
Operating coil wound for 240v A.C.
Good British Make. Ex-unused equipment. Size approx. 1½ × 1².
Open construction
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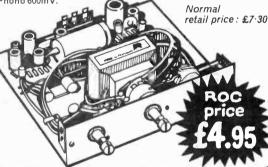


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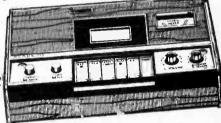
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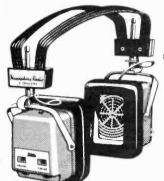
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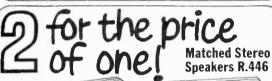
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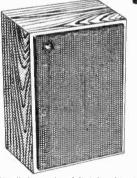


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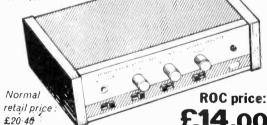
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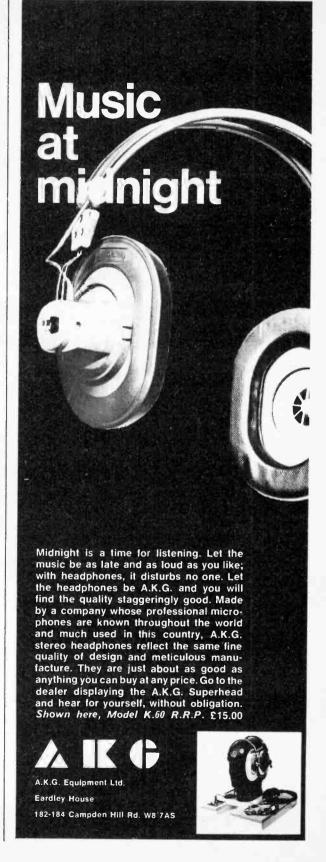
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Or Deposit £7-15 and 9 monthly payments £6.35 (Total £64.30). Carr. £1.25 Plastic Cover £3-15 extra.

PACKAGE AS ABOVE but Garrard 3000 Autochanger and Sono-tone 9TA Ceramic Car-tridge in lieu of SP25

and CS90

Carr. £1.25

Or Deposit £6 and 9 monthly payments £5.70 (Total £57.30)

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FIDELITY **SPEAKER** UNITS



Cabinets latest style Satin Teak veneer. Acoustically lined for filled acoustic damping. Ported where appropriate. Credit terms available.

DORCHESTER (Illustrated) Size appr. Range 45-15,000 c.p.s. Rating 8-10 watts. Fitted High flux 13-x8 in. Dual Cone speaker. Imp. 3 or 15 ohms.

£9.45 Carr.

STANWAY II Size 20×102×92in. approx. Rating 10 watts. Inc. 13×8in. speaker with highly flexible cone surround, long throw voice coil and 10,000 line magnet. High flux tweeter. Handsome Scandinavian design cabinet. Range 35-20,000 c.p.s. Imp. 8 ohms. Gives smooth realistic sound output. See 'package £17-85 offers' for illustration.

'YORK' HIGH FIDELITY 3 SPEAKER SYSTEM

Moderate size only 25×14×10in.

Response 30-20,000 c.p.s. Impedance 15 ohms

Performance comparable with units costing considerably more.

considerably more.

Consists of (1) 12in. 15 watt Bass unit with cast chassis. Roll rubber cone surround for ultra low resonance, and ceramic magnet. (2) 3-way quarter section series cross-over system (3) 8 × 5in. high flux middle range speaker. (4) High efficiency tweeter. (5) Appropriate quantity acoustic damping material kir (6) Handsome Teak veneered cabinet. (7) Circuit and [22] full instructions. Terms: Dep. £4.50 and 9 monthly payments £2.25 (Total £24.75).



DEMONSTRATIONS AT ALL BRANCHES

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5 + 5 WATT OUTPUT Garrard 5200 Changer with low mass pick-up arm and Stereo Car-tridge. Controls: TREBLE, BASS. VOLUME, STEREO, BALANCE. Operation on 200-250v. A.C. mains. Output rating I.H.F.M. Finished Luxurious Teak Veneer

Cabinets. Transparent plastic (tinted) cover included for main unit. Silver finished facia plate and matching control knobs







PAIR OF LOUD-SPEAKER UNITS

incorporating high flux 8in. 5in. speaker. Size approx. 13 × 71 × 83ins. PRICE COMPLETE 442

Carr. £1.25
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A REALLY SURPRISING STANDARD OF QUALITY IS OBTAINED FROM THIS COMPACT LOW PRICED SYSTEM

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Primaries 200-250v. 50c/s. Screened MIDGET CLAMPED TYPE 21×21×21 in. 99p £1.05 60mA, 6.3v. 2a ... 250v., 60mA 6.3v 2a 250-0-250w, 60mA 6.3 v. 2a. 11-05
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300-0-300w, 100mA, 6.3 v. 4a., 0-5-6.3 v. 3a. £2-80
300-0-300w, 130mA, 6.3 v. 4a., 0-5-6.3 v. 3a. £2-80
300-0-300w, 100mA, 6.3 v. 4a., 0-5-6.3 v. 3a. £2-85
300-0-350w, 100mA, 6.3 v. 4a., 0-5-6.3 v. 3a. £2-65
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TYPE BM1. An all-dry battery eliminator. Size 5½ × 4½ × 2in. approx. Completely replaces batteries supplying 1-5v. and 90v. where A.C. mains 200/250v. 50c/s is available. available.

Complete kit with £3 diagram.

Assembled ready for use

SMOOTHING CHOKES

 $\begin{array}{l} 150 \mathrm{mA, 7-10H, } 250 \ \Omega \ \textbf{70p;} \\ 100 \mathrm{mA, } 10 \mathrm{H, } 200 \ \Omega \ \textbf{60p;} \\ 80 \mathrm{mA, } 10 \mathrm{H, } 350 \ \Omega \ \textbf{50p;} \\ 60 \mathrm{mA, } 10 \mathrm{H, } 400 \ \Omega \ \textbf{25p.} \end{array}$

SELENIUM RECTIFIERS F.W. (Bridged)

All 6/12v. D.C. Output. Max. A.C. Input 18v 1a. 25p, 2a 35p, 3a. 50p, 4a. 65p, 6a. 80p.

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SEPARATE VOLUME CONTROLS PLUS TREBLE & BASS CONTROLS MICROPHONE SOCKET WITH ASSOCIATED SWITCH & VOL. CONTROL

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Terms: Deposit £11 and 9 monthly payments of £6.70 (Total £71.80)

Incorporating twin Garrard SP25 Mk. III turntables and Goldring CS90 Ceramic Cartridges with diamond stylii.

Size approx, $36'' \times 64'' \times 15''$

Black Rexine covered Cabinet with lid.

39BASS REGE

50 WATT AMPLIFIER



30 WATT HI-FI

FOR GUITAR, VOCAL or INSTRUMENTAL GROUP

A 2 or 4 input, 2 vol. control Hi-Fi unit with Separate Bass and Treble controls.

Current valves, Peak output rating. Strong Rexine cov-Attractive black/gold P.V.C. fac 200-250v. A.C. mains. For 3 Send S.A.E. for leaflet.

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A powerful high quality all-purpose unit for lead, rhythm, bass guitar, vocalists, gram, bass guitar, vocalists, gram, radio, tape. Peak Output rating Loudspeaker unit optional horizontal or vertical mounting.

**Two extra heavy duty 12in.

Two extra heavy duty 12111.
Loudspeakers.

★ Four Jack inputs and two
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Base and Treble controls.
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> £19.95 Carr. 65p

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Carr. £1:50

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H/PHONES MICROPHONE MAIN THRATARIE

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(3) Pair High quality Headphones

Matching Microphone fitted to H/phones.

Pair 50W Speakers cabinets black rexine covered

TOTAL COST OF ALL
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DISCO/GROUP EQUIPMENT PACKAGE **OFFERS** PACKAGE PRICE

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F.A.L. PHASE 50 Mk.II AMPLIFIER PAIR FANE POP 25/2 25W L/SPEAKERS.

F.A.L. PHASE 50 Mk.II AMPLIFIER PAIR FANE POP 50 L/SPEAKERS OR PAIR L12/25 Cabineted Speakers.

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F.A.L. PHASE 100 AMPLIFIER FANE POP 50 L/SPEAKERS.

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£44 carr. PACKAGE PRICE

£49.50 carr. PACKAGE PRICE

£118 carr.

PACKAGE PRICE 299 CAIT.



R.S.C. A10 30 WATT ULTRA LINEAR

H-FI AMPLIFIER Highly sensitive, Push-Pull high output, Hum level—70dB. Response 13d 30-20,000 c/s. All high grade components. Value EP86, EC83, 807, 807, 0234. Separate Bass and Treble Controls. Sensitivity 36 millivoits. For High Impedance microphones or Tape. Two separate inputs with vol. controls permit such as "mike" and Pick-up etc. to be used for mixing purposes, 200-250 v. 50 c/s A.C mains. For 3 and 15 ohm speakers. Complete Kit of parts with wring diagram and instructions. Twin-handled perforated cover 21,90 or factory built with E L34 output valves and 12 months' guarantee for 219-75

TERMS: Dengit 44 and 9 months, payments of 25:10 Cross, 429-200. Send S.A.E. for leader. TERMS: Deposit 24 and 9 monthly payments of 22-10 (Total 222-90), Send S.A.E. for leaflet.

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PHASE 50 MkII

50W AMPLIFIER OUTPUT

50 Watts (Music) R.M.S. (Cont.) (Peak)

£33.50

Сагт. 65р

Terms: Deposit £6 monthly payments Total £87.50.

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100W AMPLIFIER OUTPUT

PHASE 100

100 Watts (MUSIC) R.M.S. (Cont.) 70 , R.M.S. (Co I.H.M.F. Output rating.

£61·95

Сагт. 75р

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★ Individual Bass and Treble Controls.
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(Carr. £1-50)



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Groups.
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Cabinet constructed in heavy 3° Chipbiard and pleasing shade of Vynair with a duminium trim.
Attractive design.
Size 30° × 195° × 151° 503
at 100 watts.

FANE LOUDSPEAKERS GUARANTEED 2 YEARS

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Incorporating two 12" 50 watt 14,000 Gauss extra

heavy duty loudspeakers for

conservative rating of 50 watts. Impedance 8-15 ohms.

watts. Impedance 8-15 ohms. Sturdy pressurised cabinet in 4" chipboard. Rexine- Vynair Covered 31" × 20" × 16" approx. Suitable Vocal or Instrumental Groups. Bass Guitar or Electronic Organ, etc. For use in Discotheques, Clubs,

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C48S 25-30 WATTS

Fitted four 8" high flux 8 watt speakers. Overall size approx 48" × 10" × 5".

48"× 10" × 5".
Terms: Dep £3
and 9 monthly
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Carr 50p

C412S 50 WATTS

Fitted four 12" 11,000 line 15 watt speakers Overall size approx 56' × 14" × 9". Terms

 \times 14" \times 9". Terms: Dep. £4 and 9 monthly payments £3 (Total £31)

Carr 75p



C4/100 100W

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ULTRA HIGH FANE power ratings are R.M.S. continuous. 2 YEARS' GUARANTEE High flux ceramic magnets, Heavy cast chassis. All carr. free



18" 'POP' 100

FOR BASS GUITAR, ELECTRONIC ORGAN, ETC.

RATING 100 WATTS R.M.S. 14,000 gauss 8/15Ω

Dep. £6 and 9 14,000 gauss 8/15Ω

Dep. £6 and 9 14,000 gauss 8/15Ω

Dep. £3-30 and 9 monthly payments £1:35. Total £25:35 monthly payments £1:30 (Total £15).

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RATING 50 WATTS R.M.S. 13.000 gauss 15 \(\Omega_{-} \) Den.

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Pair suitable all purposes

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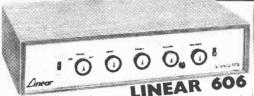
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6+6 WATTS I.H.F.M. Recommended Retail Price

TECHNICAL DETAILS

Bass Control ± 12 dB at 40 Hz. Treble Control ± 12 dB at 14 KHz.

Sensitivities Mag. P.U. 3:5 m.v. into 47K ohm R.I.A.A. Ceramic P.U. 35 m.v. Into 100K ohm. Tape Amp. 100 m.v. into 100K.

Radio Tuner 400 m.v. into 400K ohm, Crosstalk 53 dB.

Hum and Noise-75 dB min. vol. -65 dB max, vol.

Total Harmonic cent at 1 watt into 15 ohms.

- ★ Individual Bass and Treble Controls.
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- ★ Stereo/Mono Switch.
- * Input Selector Switch.
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- A modestly priced solid state unit.
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- A wide range of tone variation is provided by the separate Bass and Treble 'lift' and 'cut' controls.
- A selector switch permits instantaneous selection of Gram. or Radio.
- suitable.

TECHNICAL DETAILS

Frequency Range 20 Hz to 20 KHz

Output (per channel) 4 watts I.H.É.M.

Bass Control ± 12 dB at 60 Hz Treble Control ± 14 dB. at 14 KHz.

Speaker impedances between 3 and 15 ohms are PRINTED CIRCUIT CONSTRUCTION EMPLOYING 10 TRANSISTORS



Recommended Retail Price

0-200-250v. 50 Hz A.C. mains operation

Wholesale and Retail enquires to the Manufacturers

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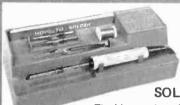
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VOL 47 NO 8

Issue 778

DECEMBER 1971

But Why?

ONE of the most difficult tasks to face a technical journalist is to write an article for the absolute beginner. It is comparatively easy to prepare something for the advanced reader, for the author is aiming at those generally a little below his own standard. An article beamed at middle-of-the-road readers is, perhaps, the least troublesome because the author does not have to dwell on fundamentals or to go too deeply into advanced theory.

But the snags come when a writer has to do something for "the beginner"—a term full of pitfalls, for there are various degrees of that species. The main difficulty for the writer is to put himself in the position of his potential readership and to anticipate questions which might arise in the mind of a newcomer to the subject. A point which is to the author perfectly obvious may cause a beginner to feel perplexed and form questions in his mind. Taken to its extreme, the author must, as far as possible, assume that the newcomer knows virtually nothing—an impossibility in practical terms, for some sort of mental line has to be drawn.

In P.W., we have to cater for all grades of experience. In general, a constructional article is geared to provide sufficient information for a constructor who has reached a stage at which he should reasonably be expected to be able to tackle the particular project. Since levels vary so widely, some readers complain that articles are too elementary while others think they are too advanced. This is the perpetual dilemma of trying to please everyone!

We do feel, however, that it is not a bad thing to err on the side of simplicity, for if the beginner is the one who wants to ask the most questions it is obvious that he is the one who needs greater attention. This is one reason why we have periodic bursts of special features for the beginner, such as the new series on transistor circuitry started in October and the extra 8-page supplement included with this issue aimed at providing some basic guidance on the main components likely to be encountered by the home constructor.

Author Hellyer said in the October issue, "... any beginner worth his salt is going to say 'But Why???' We would go further, for the path of progress of any enthusiast will be travelled faster if he makes a point of always asking 'But Why?'—and finding the answer—when confronted with an aspect not fully understood.

W. N. STEVENS-Editor.

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JANUARY ISSUE WILL BE PUBLISHED ON DECEMBER 3rd

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NEWS... NEWS... NEWS...

BSR Transcription



BSR's new unit, the McDonald 810, priced at £45.51 for the basic unit, was shown at the Audio Fair for the first time. Features include push button operation, a pitch control for absolute accuracy of turntable speed and a virtual friction free pick up arm movement which is gyroscopically controlled with a concentric gimbal mount.

Twelve months ago, BSR Limited launched the BSR McDonald consumer range. The 810 is the culmination of design expertise and production efficiency which has successfully produced in succession the wide selling MP 60 and HT 70 units.

The technical data for the 810 is impressive. It is a two speed player, 33^1_3 and 45 rpm, utilising as its heart a 4 pole dynamically balanced synchronous motor driving a 7^1_4 lb. diecast balanced turntable. A stroboscopic centre plate when coupled with the pitch control ensures absolute turntable accuracy. A low mass pick up arm, over 8^1_2 in. in length has less than 0.5° per inch tracking error.

Although primarily a single play unit, versatility comes with an interchangeable umbrella spindle giving true automatic function if required.

"Sonex 72"

The Third International Exhibition of Audio Equipment, operated by British Audio Promotions Ltd, on behalf of the members of The Federation of British Audio will be mounted at the Skyway Hotel, Bath Road, Hayes, Middx (near London Airport) over the period from Wednesday, March 22, 1972, to Sunday, March 26, 1972.

Hacker RP73

This newly-designed successor to the famous Hacker Autocrat RP33 home/car portable radio incorporates an integrated circuit and ceramic filter in its design.

In common with its predecessor the Autocrat Mark 2 Model RP73 offers extreme portability for use in the home, and a special change-over aerial circuit for interference-free reception in a car. Price is £25·25 including Purchase Tax. Hacker Radio Ltd, Norreys Drive, Cox Green, Maidenhead. Berks.



Meteronic Scope



The MSB 101 oscilloscope has a bandwidth of d.c.-8MHz; vertical sensitivity of 100mV/cm-50V/cm; sweep speed range of 100nSec/cm-150mSec/cm; and a unique signal locking circuit which by means of a single control enables the user to select through 'Free Run', 'Internal Signal Sync' to 'Triggered. Also provided is switch slope selection. Fibreglass P.C. boards are fitted as standard. The MSB 101 size is 8 x 6 x 4in. and weighs 51b. Price: £69. Meteronic, 114/116 Shipbourne Road, Tonbridge, Kent. Tel. Tonbridge 61448.

Daystrom Throw It Around

Daystrom has introduced a 660 series drop-proofed multimeter. These precision meters are warranted to operate within specification after being dropped from a height of five feet. The meter mechanism floats inside a sealed. high-impact plastic case. These multimeters also have temperature compensation, with shielded and electrically protected meter movement. The meter maintains accuracy in extreme environments and will not be damaged if, as sometimes happens, the user accidentally connects it to a high voltage source. Daystrom salesmen sometimes demonstrate the 660 series by throwing the meter on the customer's floor. So far. customers have had a worse shock than the meter! So, if you feel like chucking a £29.85 meter about, contact Daystrom (Schlumberger), Bristol Road, Gloucester GL2 6EE.



NEWS... NEWS... NEWS...

Litesold System

The Litesold ETC/1 Soldering System consists of a lightweight soldering iron which is fed from a solid state power/control unit giving fully automatic electronic control of the temperature of the front of the bit.

Operating temperature is fully adjustable by means of a calibrated dial on the power unit over a wide range from 150/400°C. Thus there is no need to change bits for different settings which can be altered and read-off instantly.

The most important feature is the total avoidance of electrical disturbance and R.F.I. generation



A New Iron From Antex



The element of this new Antex soldering iron is totally enclosed within a ceramic shaft. (Aluminium oxide.)

Near perfect insulation has been achieved; as a result there is no measurable leakage and live transistors can be soldered without risk of damage.

The 15 watt element generates a temperature of up to 450°C. at the tip to facilitate high speed sol-

by the control unit which allows the iron to be used on ultra-sensitive equipment and components.

The plug-in soldering iron contains no control components except the temperature sensor and is as cheap and simple to repair as an ordinary iron.

Long-life bits slip over the heating element and are available in a range of tip sizes. Price is £19.80. Light Soldering Developments Ltd., 28 Sydenham Road, Croydon, CR9 2LL.

dering. A choice of four iron coated bits and one special bit plated with iron, nickel and chrome is available: all designed to ensure long bit-life.

The complete iron has passed a test of 4,000 volts a.c. and each production model is tested at 2,000 volts a.c. Further details from: Antex Limited, Mayflower House, Plymouth, Devon.

Eagle International

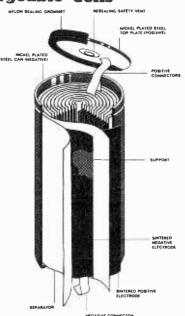
Eagle International will add a quadraphonic synthesiser to its range in January 1972. Designated AA10, it enables a conventional stereo system to be turned into a quadraphonic system by dividing the 2-channel output from a stereo amplifier into 3 or 4 channels based on sum and difference signals.

Ever Ready Co's Rechargeable Cells

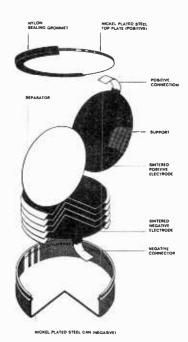
These cells, marketed by the Ever Ready Co. are sealed Nickel Cadmium types and have been used for some time now as the rechargeable power units in small portable appliances where the charging unit is integral. Now they are available to the home constructor and prices vary with quantity and capacity but typically a U2 size replacement would cost something over £2 for a single cell but would be proportionately reduced for larger quantities.

Button cells are more normally supplied as higher voltage prepacked batteries and typically a 4.8V 550mAh battery as used in radio controlled models, would cost around £3.30.

Cells and battery packs are available direct from the manufacturer and the smaller button cell packs from reputable suppliers to the radio controlled model field. The Ever Ready Company (Gt. Britain) Ltd., Special Battery Division, Hockley, Essex.



TYPICAL CYLINDRICAL CELL CONSTRUCTION



TYPICAL BUTTON CELL CONSTRUCTION



A NY means of spreading the great number of short wave transmissions which can be heard over an increased tuning range is helpful, simplifying and easing tuning. When several ranges are needed it becomes difficult to use separate inductors for each range, involving a large number of coils, with all the associated switching.

In the receiver described here, only two coils are required band-changing being achieved by bringing in pairs of fixed capacitors. This breaks up the full tuning range into a number of smaller divisions.

CIRCUIT

Fig. 1 is the mixer stage circuit the wiring being very much simplified by using this switching arrangement. L1 is the aerial coil, tuned by VC1, and L2 the oscillator coil, tuned by VC2. VC1 and VC2 are sections of a small ganged capacitor, operated through a cord drive.

The 2-pole 9-way rotary switch S2/S3 selects the required band. With the switch in position 1, VC1/2 alone are in use, for the highest frequency band. When the switch is in position 2, C2 and C10 are in circuit. Each of these capacitors is 50pF, so the next range runs on from the frequency reached when S2/3 was in position 1, and VC1/2 fully closed. In a similar manner, position 3 of the switch brings in C3 and C11, each of 100pF. The next lower frequency band employs C4 and C12, each of 150pF, with the switch in position 4. This continues for the nine ranges, each pair of capacitors being 50pF larger in value than the previous pair.

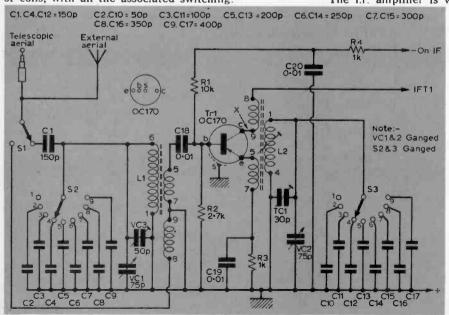
VC1/2 has a swing of a little over 50pF, so that ranges overlap. VC3 is a panel trimmer, which can be set for best volume on any band, or when altering the aerial. S1 is an aerial switch, used for the attached telescopic aerial or an external aerial.

The capacitors C2 to C9 for the aerial circuit, and C10 to C17 for the oscillator, are 1% or 2% silvermica, and any variation in the exact capacitances of the components used is easily cancelled out by VC3.

IF AMPLIFIER

A conventional high gain intermediate frequency amplifier is used, Fig. 2. This has two double-tuned i.f.t.'s, and one single tuned i.f.t. resulting in good selectivity.

The i.f. amplifier is wired as a separate unit, on



The complete circuit of the 9 Band Receiver Is made up of Fig. 1, (left) mixer stage; Fig. 2, i.f. stages and Fig. 3 the audio output stage. The constructor only need assemble the mixer and i.f. stages since the audio stage is a packaged module. a small insulated board. Input from the mixer stage is to pin 2 of i.f.t.1 and audio output is from D1 and C26. VR1 is the usual audio volume control.

AUDIO AMPLIFIER

This provides high gain and 330mW output into a 15 ohm speaker. Fig. 3 is the circuit and Tr4 is the first a.f. amplifier stage, stabilised by R14. Output from Tr4 collector is via C30 to the base of Tr5, which with Tr6 forms a Darlington pair driver for the output transistors Tr7 and Tr8. These form a push-pull complementary-symmetry stage, working in Class B, with diode D2 for thermal stabilisation. Feedback through R17 maintains operating

conditions for the four directly-coupled transistors Tr5 to Tr8.

This circuit has plenty of amplification and volume. In order to simplify construction of the whole receiver, the audio amplifier is obtained as a printed circuit package, ready for use, and incorporating matched transistors.

A is the common positive line, and D the negative line. Point C is for audio input. The resistor R13 is included in the amplifier. R12, which is in series with R13, was found to be necessary for stable working in this particular receiver.

Leads from D (battery negative line) and E run to the 15 ohm speaker. The circuit is of the transformerless type and a speaker of other than 15 ohm impedance should not be used.

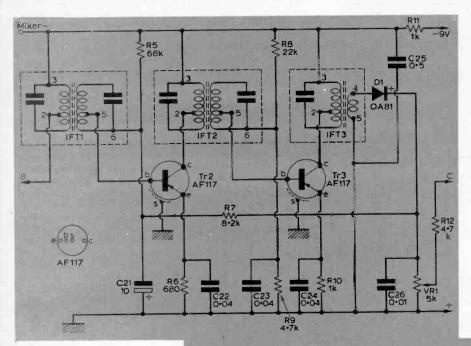
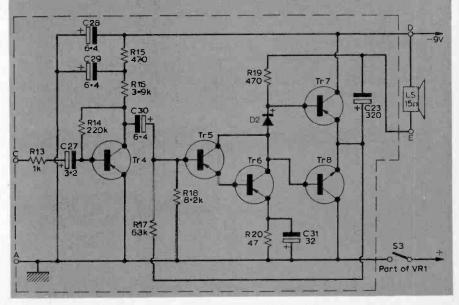


Fig. 2. The circuit of the i.f. stages, constructed as a separate unit on a paxolin panel (See Fig. 6). The input comes from pln 8 on L2 in the mixer stage.

Fig. 3. Since the audio stages are contained within a packaged module this circuit of the 5 transistor unit is given for interest only. Input from the I.f. assembly goes to pin C, the loudspeaker to pins D and E and the earth line to the onloff switch S3. (Note: C23 should read C32.)



MIXER STAGE ASSEMBLY

A 10in. x 4in. flanged plate (universal chassis member) serves as panel for the controls and the top of the case. The controls are placed lin. from the bottom of this plate, VC3 and the cord drive spindle being 154in. from the plate ends and S2/3 and VR1-equally spaced between these.

VC1/2 is fixed as in Fig. 4 so that the top of the drum is about ¹8 in. below the top of the plate. One pulley is above the cord drive spindle, to keep the cord parallel with the plate. The second pulley guides the cord clear of the bushes of S2/3 and VR1. The pulleys are on bolts fixed with lock nuts to the plate. The cord is given one complete turn round the drive spindle, then passes round the wheels and

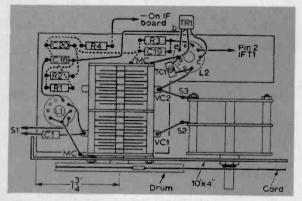


Fig. 4. Layout of the mixer assembly built on an aluminium plate.

drum. It is taken through the drum slot, and tied so that it is under tension from the spring.

Fig. 4 shows wiring, etc., for this stage. L1, L2 and the other items are mounted on a piece of paxolin 5in. x $2^{1}2$ in., which has a cut-out section to clear S2/3. VC1/2 is bolted to the 10in. x 4in. plate, and the paxolin is in turn bolted to the underside of the ganged capacitor. Additional support is given by a bracket attached to the paxolin and rear of the 9-way switch.

Transistor Trl has three leads soldered directly

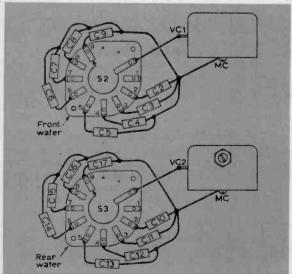


Fig. 5. Details of the wiring of the bandswitch \$2/\$3.

* components list

, comp	oneng	1130			
Resistors					
R1	10kΩ	R5	68kΩ	R9	4.71.63
R2	2·7kΩ	R6	680Ω	R10	4·7kΩ 1kΩ
R3	1kΩ	R7		R11	
R4	1kΩ	R8	22kΩ		1kΩ
114	11/22			R12	4·7kΩ
VR	1 Elianot	All 2	W 10%.	741	'4 L (CO)
		entiom	eter, log	, with s	witch (S3).
Capacito					
C1	150pF	C10	50pF	C19	0.01µF
C2	50pF	C11	100pF	C20	0-01/4F
C3	100pF	C12	150pF	C21	10/1F 6V
C4	150pF	C13	200pF	C22	0.04#F
C5	200pF	C14	250pF	C23	0.04/1F
C6	250pF	C15	300pF	C24	0.04µF
	300pF	C16	350pF	C25	0.5uF
C8	350pF	C17	400pF	C26	0.01 <i>u</i> F
C9	400pF	C18	0.01µF	C20	σοιμα
			7 inc ar	0 10/ n	r 2% silver
mic	a	10 01	i iiic. ai	6 1/0 0	1 2 % Sliver
VC		75 4	75 nF a	nnrov	See text.
VC			ced varia		See text.
TC		re-set	ceu varia	Die.	
	i Johi i	ne-set			
Semicon	ductors:				
Tr1	OC170		Tr3	AF117	
Tr2	AF117		D1	OA81	
				OP(O)	
Inductors					
IFT				1 Ran	ge 4 Blue
IFT:				(Transistor)
IFT	3 IFT14/46	65 (Der	ico) L	2 Ran	ge 4 Red
				(7	Transistor)
	-1:6-				
Audio Ar				10.0.	
PC3 Packaged circuit (Newmarket).					
Miscellan	eous:				
	inet: 2 off	10in	y Ain I	Inivers	al chassis
flan	ged memb	OF CH	me Bad	io) o	off 7lin v
Alin	. plywood.	2 0#	10in v 7:	n bost	board
4- <u>7</u> 111	ing driver	2 011,	10111 X /1	n. nard	DOATU.
i UII	ing drive:	חטוע	1, 25111.	uia., L	L34 drive
Spin	dle, spring	g, core	, pulley	s (Mon	ne Radio).
Spe	aker, 7in.	C 3½In.	, 15 12.	elesco	pic aerial.

to the pins of L2. The base lead B is extended by soldering on connecting wire, to run to C18. Connections in this stage should be reasonably short and direct. R3, C19 and C20 are wired to a tag under the paxolin, in contact with the metal frame of VC1/2.

Aerial socket, knobs, rubber feet.

VC3 is mounted directly under VC1/2 and is connected in parallel with it by short leads.

The bandswitch occupies the position shown in Fig. 4, and is wired as in Fig. 5. The switch has separate single-pole 9-way wafers connected directly to VC1 and VC2 by short leads. No extra connection is made to position 1. Position 2 has the pair of capacitors C2 and C10 (50pF each). Position 3 has equal capacitors C3 and C11 (100pF each), and so on.

The capacitors are best arranged to lie partly over the wafers, in the manner giving shortest leads to a stout wire which returns to the frame tag of the ganged capacitor.

GANGED CAPACITOR BAND SWITCH

S2/3 introduces fixed capacitor increments of 50pF at each position. There is a certain amount of stray circuit capacitance, to which is added the

minimum capacitance of VC1/2. This means that a ganged capacitor having a maximum capacitance of 50pF each section is not quite sufficient and results in small gaps in the tuning range.

A ganged capacitor with a capacitance swing of just over 50pF (say from 10pF to 70pF) would be ideal. To obtain a little overlap, and allow for variations of C2 to C17, the nearest standard value is

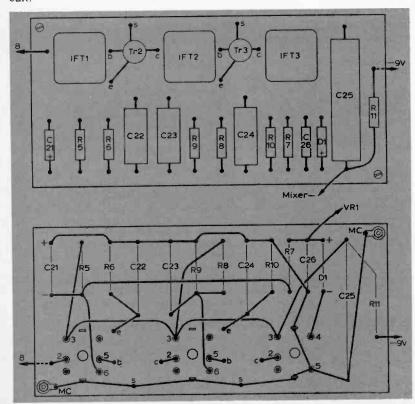
75pF, which is satisfactory.

When this tuning arrangement was first used, a 2 x 100pF capacitor was fitted and some plates pulled off, but this resulted in too many being removed. A new capacitor thus had to be fitted. Caution is therefore required, if a capacitor is modified in this way. With a 2-gang 100pF capacitor, the effective value can be reduced to about 75pF by placing a 300pF fixed capacitor (silver mica) in series with each section. The lead from L1 to VC1 must then run over VC1 so that it can join the lead from S2.

IF AMPLIFIER ASSEMBLY

This is assembled and wired on a paxolin panel 3^3_4 in. x 1^3_4 in. All components are mounted on one side and wiring is on the reverse, as in Fig. 6. Note that the different spacing of the pins of the i.f.t.'s enable these to be identified. Remember to drill holes for adjustment of the cores.

Small holes are drilled for the leads of the other components. Note the polarity of C21 and diode D1. Connections underneath are made by bending over the wires and snipping off the ends and by using thin connecting wire where required. Insulated sleeving is put on all leads where necessary. Two bolts holding the tags MC, locked on, will mount the finished amplifier and provide a positive return circuit.



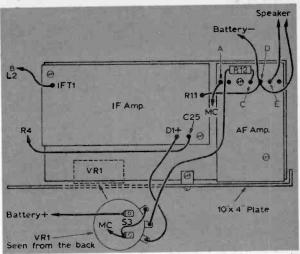


Fig. 7. The i.f. and audio stages are mounted on a common panel.

Solder a lead to pin 2 of i.f.t.1. This is later soldered to pin 8 of the oscillator coil L2.

Take a black lead from R11, to use as negative. Solder a wire to the junction of R11 and C25, as shown, which will later run to R4. The remaining external connection is from R7, C26 and D1, and goes to the volume control VR1.

Both i.f. and a.f. amplifiers are mounted on a piece of paxolin 5^1_2 in. x 2^1_2 in. which is supported by the bracket mentioned earlier, and by a further bracket bolted to the 10in. x 4in. aluminium plate. Extra nuts are put on the bolts holding the tags MC, Fig. 6. The bolts pass through the 5^1_2 in. x 2^1_2 in. paxolin. Further tags are then put on fixed with nuts. The tags are wired to the volume control and metal plate (positive line).

The audio amplifier package is mounted in a similar way, Fig. 7. R12 is soldered to point C. A black lead for battery negative is taken to point D, and white leads for speaker connections to points D and E. A red lead from point A runs to the positive line at VR1 and the on-off switch.

ALIGNMENT

The complete assembly on the 10in. x 4in. flanged plate is aligned and tested before fitting it in the cabinet. A speaker of the correct type (15 ohms) must be connected.

The five cores of the i.f.t.'s are rotated with a suitable tool, such as the Denco TT5, for best results. A weak signal is most suitable from a signal generator, or from a transmission, a short wire aerial being temporarily

Fig. 6. Layout and wiring diagram of the i.f. assembly built on a paxolin panel, 3½in x 1½in

connected to tag 8 of L1. VR1 should be near maximum volume, but a strong signal should be avoided because the automatic gain control circuit will then make critical adjustment of the cores difficult.

Once the i.f.t. cores have been correctly peaked for best sensitivity, they should be left alone. A meter placed in one battery lead should show a current of under 15mA with weak signals, rising to peaks of 50mA or more with signals giving good volume.

The cores of L1 and L2 are then rotated until about $^{3}_{8}$ in. of threaded brass projects. Set VC3 and TC1 at about half capacitance. Open VC1/2, set the bandswitch at Position 1, and rotate TC1 as necessary to tune to about 15MHz.

Leave VC3 and TC1, switch to Position 9, and close VC1/2. Rotate the core of L2 as necessary to tune to approximately 3.6MHz. Switch to Position 8, tune in a transmission, and rotate the core of L1 for best results.

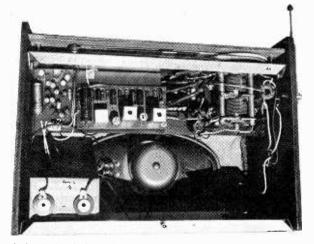
It should then be found that with the bandswitch in any position, and a transmission tuned in, VC3 can be peaked for best reception. Should VC3 need to be either fully open or fully closed with the switch in Positions 1 or 2, re-adjust TC1 as required. If VC3 is either fully open or fully closed to give best results with the switch in positions near the low frequency end of the coverage provided (especially Position 8 or 9) then the core of L1 needs slight readjustment to avoid this.

It should be found that VC3 generally only needs one adjustment for each band and that often even this will not be necessary. VC3 can be peaked up for best reception of weak signals at any time, when changing the aerial, or switching S1.

If it is found that almost uninterrupted whistles arise at the extreme h.f. end of the coverage provided, include a resistor at X in Fig. 1, between collector and pin 9 of L2. Its value should be the lowest which prevents oscillation and will generally be around 47 ohms to 470 ohms or so. This depends on the individual transistor and other factors.

CABINET ASSEMBLY

Fig. 8 will help to clarify assembly of the case. Cut two pieces of hardboard 10in. x 7in. and with a pad saw or keyhole saw cut a hole to match the



A view inside the 'works' shows the three units forming the complete receiver.

speaker cone. Clean up all edges with glasspaper and wipe off any dust. Fabric is then stretched over the hardboard, brought round the edges, and glued on the inside.

The sides are 3-ply, each 7^12 in x 4^12 in., sanded and varnished. The 10in x 4 in. flanged plate forming the case bottom is placed on a flat surface, and the sides are positioned as in Fig. 8. Mark through the flange holes, drill the sides to match, and fix them with bolts.

Drill the hardboard front for speaker and front flange, and bolt this as in Fig. 8, with the speaker in position.

The receiver panel should then be finished. Cut a piece of plywood or other thin wood about 5in. x 2in. and fix this with small screws through the 10in x 4in. plate, to bring the tuning scale about level with the drive cord. Clip a small piece of tinplate on the cord, and solder a straight wire pointer on this, so that it moves along the scale.

A piece of perspex is cut 10in. x 4in., and drilled to match the four control spindles and for 6BA bolts in line with the four holes which are in the universal chassis flanged plate. A piece of coloured card is also cut this size, and a window about 5^1_4 in. x 1^1_4 in. is cut in it with a sharp blade, to lie over the tuning scale.

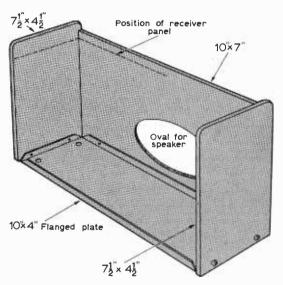


Fig. 8. Details of the construction of the receiver cabinet.

Four lin. long 6BA bolts are put through the holes in the perspex and card. A washer and nut is put on each bolt, and the nuts are tightened. An extra nut is then put on each bolt, and the whole is fixed in place with further nuts behind the flanged plate. The nuts are adjusted to give about 12 in. clearance, to take the drum, cord and pointer.

The assembly is then put in the top of the case, so that the flanged plate is about ¹2in. down, as in Fig. 8, and the perspex is flush with the case front. Drilling positions are then marked through the holes punched in the flanges. The sides are drilled, and the receiver bolted in place. The receiver case front is also bolted to the front flange of the 10in. x 4in. plate.



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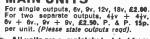
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Variable current limiting from 0.2A to 1A is included making the power supply particularly suitable for development work and also giving it protec-

tion from short-circuit surges.

Principle

The principle of negative feedback is used in systems where accurate control is required. The system could be a positional servo as used in rudder

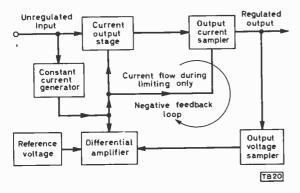


Fig. 1: Block diagram showing function of stages in the power unit.

control of a model aircraft, speed control of an electric motor, temperature control of a blast furnace or cooker or as in this example, voltage stabilisation. In each case a sample is taken of the final output, a comparison made with some reference, then corrective adjustments made to reduce the error.

A. BURNFTT

The block diagram of Fig. 1 illustrates the principle of voltage control where the controlling device is in series with the output current. The output is monitored by a sampler and the sample voltage compared to a reference voltage by a differential amplifier.

The differential amplifier amplifies the difference such as to starve the output stage of base current if the sample voltage is greater than the reference. As a transistor is basically a current amplifying device complete control of the output current can be achieved by controlling the base current of the current output transistor.

Current Output Stage

Transistors are current amplifying devices and in general the more current they are capable of handling the less gain they have. A power transistor capable of passing 1A can have a typical β (current gain) of only 10 which would mean that the base current would still be rather high for the differential amplifier to handle, being in the region of 100mA. The current output stage is simply a configuration of two transistors, Tr3 and Tr4, Fig. 2, to give high output current capability with high current gain.

Constant Current Generator

The output current of this circuit, Tr2, is constant and sufficient to supply the maximum base current of the current output stage with a little extra for the differential amplifier.

The circuit uses the principle that as the baseemitter junction of a transistor is a forward biased diode then it will present a low voltage drop (0.7V in the case of silicon transistors). The zener diode potential will therefore be applied almost completely across R6. The resulting current through R6: -

 $I = (V_z - 0.7)/R6$

will pass through the transistor without loading the zener diode.

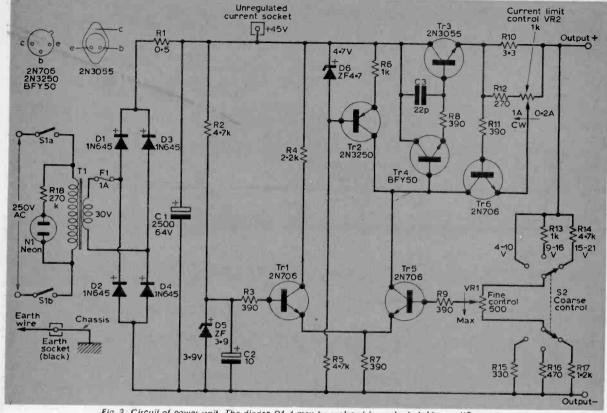


Fig. 2: Circuit of power unit. The diodes D1-4 may be replaced by a single bridge rectifier unit.

Bias current for the zener diode will be supplied by R6. A constant current output of 4mA was sufficient to supply the output stage and the differential amplifier.

Differential Amplifier

The differential amplifier, Trl and Tr6, is coupled to the base current circuitry of the current output

Voltmeter Current Voltage Volta ge limit (coarse) Neon (fine) Ammeter VR2 VR1 SI To earth R18 0 Earth Component board T1 CI Tr 3

stage. It takes current surplus to that required to maintain the correct amount of output current.

The amplifier amplifies the difference between its two inputs hence the term "differential amplifier." In this case it is used as a current control device.

Reference Voltage

This is obtained from a zener diode, D5, an attempt being made to keep the diode current constant by connecting a capacitor across it. This is necessary as low wattage zener diodes have a high series internal resistance resulting in their output voltage varying with current.

The regulated output voltage of the power supply would normally be preferred to supply bias current to the zener but as this will be switched over wide ranges in this case, bias current has supplied from the unregulated input through a 4.7kΩ resistor R2 giving a bias current of 10mA.

Fig. 3. Layout of unit constructed by the author. See Flg. 4: for details of the component board.

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2N1303	19b	ACY40 ACY41 ACY44 AD142	18p	BFX84	25p
2N1304	26p	ACY44	31p	BFX85	32p
2N1305 2N1306	26p 33p	AD142	50p 58p	BFX87 BFX88	29p 26p
2N 1306	33p 33p	AD149 AD150	50p	BFY50	23p
2N 1307 2N 1309	36p	AD161	33 b	BFY50 BFY51 BFY52	20p
2N1613	23p	AD162	3611	BFY52	23p
2N1711	26 p	AD162 AF114 AF115 AF116	24p	B8X20	16p
2N1893	54p	AF115	24p	BY164 BV228	4 Km
2N2147	95n	AF116 AF117	22p 22p	BY238 BYX38-300 BYX38-300	19b
2N2218 2N2218A	34p 44p	AF117 AF118	82p	BYX38.300	R 38n
2N2218A 2N2219	38p	AF124	240	C407	14P
2N2270	62p	AF124 AF125 AF126	24p	C407 C762	19p
2N2369A	19p	AF126	22p	EA403 EB383	10p
2N2483	35p	AF127 AF139	22p	EB383	10p
2N2484	42p	V F-550	33p 36p	EC401	18p 17p
2N2646	47p	AF239 ASV26	36p 27p	EC402 NKT211 NKT212	17p 25p
2N2904 2N2905	38p 44p	A8Y26 A8Y27 A8Y28	36p	NKT212	25P
2N 2905 A	47 p	A8Y28	27p	NKT213 NKT214	25 P
2N2924	20p	ABY29	36p	NKT214	231)
2N2925	22p	AUIII	97 p	NKT217	50p
2N2926	110	B30C250	24p 66p	NKT261	21p 18p
2N 3053	27p	B1912 B5041	72p	NKT271 NKT274 NKT403	18p 18p
2N3054 2N3702	60p	BA102	25p	NKT402	65P
2N3702 2N3703 2N3704	13p 13p	BA130	22p	N K T 405	79P 30p
2N3704	13p 13p	BA145	27p	N K T 6 13 F	30p
203705	13b	BA156	13p	NKT674F	24p
2N 3706	13p	BB103/B	16p 16p	OA47 OA90	8ր 6 ր
203708	10p	B(1108	11p	OA91	5p
2N3708 2N3709 2N3710	13p	BC108 BC109	12p	OA95	6p
2N3711	13p 13p	BC122	21p	OA200	9p
2N3794	1011	BC125	15D	OA202	10p
2N3819	23p	BC122 BC125 BC126 BC140 BC147 BC148	22p 30p	OC19 OC25	50p 42p
9N 3890	53p 35p	BC147	10p	OC90	42p 76p
2N3904 2N3906	35p	BC148	9p	OC35	60p
2N4036	55p	BC149	10p	OC36	ศิรีษ
2N4058	13p	BC153	190	OC41	42p
2N4059	100	BC169	11p	OC44 OC70	42p
2N 4060 2N 4061	11p	BC177	14p 13p	FF0C70	21p 38p
2N4061 2N4124	11p 18p	BC170	14p	OC75	38p 40p
2N4124 2N4126	270	BC182L	11p	OC81	25p
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2N4289	150	BC186	420	OC84	25p
2N4291 9N4410	16p	RC9191	161 161	P346A S2CN1	26p 10p
2N4410 2N4991	24p 62p	BC213L BC214L	16r	SDI	10p
2N4991 2N5062	611	BC213L BC214L BC257 BC259 BC268 BC268 BC269 BC300 BC300 BC301 BC303 BC303 BC303	91	NO S DA	12p
2N5457	491	BC259	91	V763	28p
2N5459	49p	BC267	171	W106BI	45 p
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40602	521	BC303	601	P ZTX 302	220
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EY86	4p	PL82	7∳p	30FL1	20p
E 100	20 p	PL83 PCL84	7+p	6/30L2	20p

Output Sampler

The resistor chain is strapped across the output voltage and the tapping point will always be at 3.9V. There are three separate resistor chains in order to reduce the sensitivity of VR1.

It is worth mentioning that the output of this power supply can never be less than the reference voltage generated by D5. If 3.9V is not low enough then a 2.7V zener may be used for D5 and if necessary, the sampling chain recalculated.

Construction

Not much information need be given on the construction of this unit since much will depend upon the dimensions of the components used. Fig. 4 shows the layout of the component board and the interconnections with the remaining components.

Fig. 3 illustrates the general layout of the power unit as built by the author. Note that the transistor case of Tr3 forms the collector connection and must be insulated from the heat sink with the mica insulation kit generally supplied with the transistor. Check after assembling the transistor and heat sink that there is no conducting path between the transistor case and the heat sink.

The heat sink used here is made from aluminium sheet $4^{1}_{2} \times 2^{3}_{4}$ in. bolted to the main chassis.

It is worth adding that where wire-wound resistors are used there is always a tendency for oscillation to occur. These resistors, from the nature of their construction, are slightly inductive. Often this effect can

* components list

1kΩ
4·7kΩ
330Ω
470Ω
1-2kΩ
270kΩ

Capacitors

2500µF 64V C2 10µF 25V 22pF polystyrene

Semiconductors

Tr1 2N706 or BC107, 2N930 or 2N2484 Tr2 2N3250 or BCY30, 31, 32 or 2N3250

Tr3 2N3055 or BDY 38, with insulating washer etc.
Tr4 BFY50 or 2N1711, 1613 or BFY51

Tr5 2N706 or BC107, 2N930 or 2N2484

Tr6 2N706 or BC107, 2N930 or 2N2484

1N645 D1

D5 ZF3-9 (400mW) 1N645 D2

D6 ZF4-7 (400mW) 1N645

Miscellaneous

Transformer 30V 2A (Type MT3AT). S1, 2 pole 2 way toggle switch. S2, 4 pole 3 way, make before break wafer switch, used as 2 pole 3 way. Sockets, red (4), black (5). Neon lamp, Q1332 (Bulgin) or equivalent; some equivalents have built-in resistor -if so delete R18. Fuse holder with 1A fuse. Vevoboard, plain, 3½ x 3½ in., 0.1 in. matrix. Aluminium chassis, 10½ x 9 in., panel 12 x 9 in., heat sink 4½ x 2½ in. Voltmeter 20V, ammeter 1A, if required.

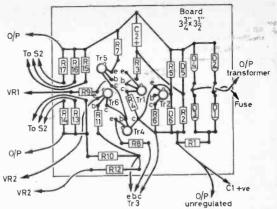


Fig. 4: Layout of component board.

be corrected by the addition of a small capacitor of 20 to 100pF coupled across the resistor to tune out the effect of the inductance.

TELEVISION

DECEMBER ISSUE

A CLOSER LOOK AT PAL

The basic principles of the PAL system are now generally understood. There is however a good deal more than meets the eye to the system. So this month we are starting a new series in which we shall be investigating the system in greater detail than previously. The account will be descriptive, not a fog of formulae!

CONSTRUCTORS' CIRCUITS

This month we turn to the line timebase. A choice of transistor or valve line oscillator circuits, both with flywheel synchronisation, and a line output stage with optional stabilisation and optional solid-state e.h.t. and boost rectifier circuits is given.

THE TELDEC SYSTEM

With the first demonstration of the Teldec system in colour at the recent international Berlin Radio Exhibition this remarkable disc videorecording system is again in the news. A full account of the mechanics of the system.

RUSSIAN TV RECEIVERS

There are many novel and unusual features in the Temp single-standard receivers manufactured in the USSR and now being widely distributed in the UK. For example, an external definition control varies the vision i.f. response by means of a varicap diode, the line blocking oscillator transformer has an adjustable feed-in point for optimum a.f.c., automatic brightness control is incorporated in the video output stage and amplified negative feedback is used in the field output stage. We are taking a detailed look at this interesting chassis.

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deliberate effort has to be made to roll-off this response to avoid r.f. pickup in the high gain amplifier and also to prevent the bias oscillator signal from being a problem.

It should be pointed out that this circuit is only suitable for the Marriott XRP18 or XRP36 record playback heads and the XES11 erase head. The amplifier will play back from other heads but, on record, other heads need much higher bias voltages than this circuit will produce.

All the transistors specified are common types and inexpensive and the total cost of the semiconductors is unlikely to be more than about £1.50 including the output pair.

The circuit is very largely based on one published by Mullard's and no originality is claimed. There are however certain differences incorporated for various reasons

The switching necessary in a tape recorder circuit tends to make the understanding of the circuit difficult and so Fig. 1 shows the effective circuit on playback. Fig. 2 shows it in on record. The component numbers are shown and if the values given in the main circuit are used these will work perfectly well by themselves without switching if for instance only a tape playback amplifier is needed.

PLAYBACK

From Fig. 1 it will be seen that Tr1 and Tr2 are coupled as a pretty conventional preamplifier to boost the signal from the tape head. R7, the emitter resistor of Tr2, is not decoupled, this provides a measure of feedback to the whole stage as the bias

Fransistor PE RECORDER W. LANGLEY

In January we published full details for a stereo tape recorder and at the time we promised an article describing a mono version. The amplifier described here can be used with any type of tape deck, though the tape heads specified must be used.

THE design of a transistor tape recorder has its own special problems. High gain is necessary since the output from a tape head on playback is very low but at the other end, in the circuits feeding the loudspeaker, high currents are passed and it is vital to ensure that earth loops do not create instability. Readers who wish to build this circuit should not deviate from the general layout unless they are absolutely certain that they know exactly what they are doing.

The problems of earth loops are not helped by the necessity for including fairly complex switching to alter the function of the amplifier from record to playback. An early prototype of this project was violently unstable due to the voltage drop in only a 2in. length of wire; this may give some indication of how important careful layout is.

Care has also to be taken in another field. Modern transistors of the type used here have frequency responses reaching to several Megahertz and a

to Trl is taken from the emitter of Tr2 via R5. This feedback improves the stability of the amplifier. C3, a low value capacitor, has little effect at audio frequencies but effectively cuts out the r.f. signals, which may have been picked up, from later stages. Tone control is achieved by coupling feedback from Tr2 collector to Tr1 emitter via C6 and VR2. To

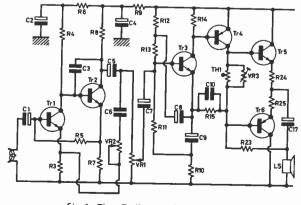


Fig. 1: The effective circuit on playback.

ensure quiet and stable operation, the supply to Trl collector must be adequately decoupled, this being achieved through R6 and C2.

After the volume control, the output is fed to a fairly conventional transformerless complementary pair output stage. It is d.c. coupled throughout with a variety of feedback and stability circuits. Conventional connections would take the junction of C10-R15 to the junction of R24 and R25 instead of the base of Tr6; the reason for deviating from this will become apparent from the record stage.

TH1, a VA1077 320 thermistor, holds the bases of the output pair close together, as far as potential is concerned, while the trimmer VR3 linearises the operation and sets the output current. R10 applies a degree of negative feedback to the first part of the output stage.

RECORD

On record the input to Trl is connected to the input sockets, the first of which is unattenuated, the second which is severely attenuated for inputs of up to 2V. The input impedance of both is fairly high, about $100 \mathrm{k}\Omega$.

The preamplifier and the first two stages of the main amplifier operate identically except that the tone control is disconnected and the volume control becomes the record level control. TH1 and VR3 are included but in fact their low value means that they can be ignored in the record position; R16 goes directly to chassis and acts as the collector load. Output to the tape head is taken from the collector of Tr4 (effective) via C11, C12 and R21. The VU meter is connected via R22, the actual value of which should be selected later.

In the record mode, transistors Tr5 and Tr6 are coupled as an oscillator with the erase head, the potential divider chain R17, R18, R19 and R20 providing the correct bias voltages. This arrangement

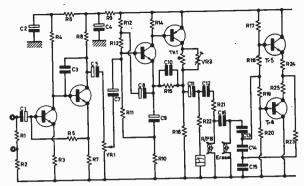


Fig. 2: The effective circuit on record.

gives a high voltage swing across the erase head. The a.c. bias necessary for correct operation is applied to the record head via C16.

SWITCHING

To alter the function of the amplifier from record to playback an eight-pole, two-way switch is needed. The various functions can be studied in the complete circuit diagram shown in Fig. 3. The VU meter is only operational on record and serves as a level indicator.

The type of switch used is not important but may be hard to obtain. That used in the prototype is made up from "Make-a-Switch" parts with two six-pole, two-way wafers.

EQUALISATION

For the best signal-to-noise ratio, on record, treble boost should be applied to the signal and on playback, bass boost should be applied. In fact these tend to be self-cancelling if a slightly worse signal-to-noise ratio can be accepted (and it is only very slight with

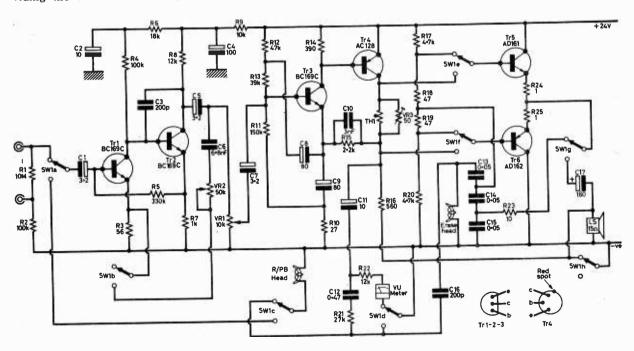


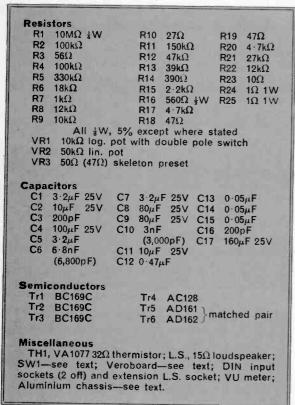
Fig. 3: The complete circuit. SW1 is shown in the record position. The connections for Tr5 and Tr6 are shown in Fig. 6.

modern tape). The author has a number of professionally recorded tapes and recordings, made without equalisation using this amplifier, were hardly different from these. On playback the tone control gives a wide control over the frequency response and this compensates somewhat for the lack of equalisation.

HEAD SWITCHING

The tape heads specified are both four-track and it is of course necessary to switch from one to the other. This is simply accomplished by fitting a slide switch near the heads, the siting will depend on the

* components list



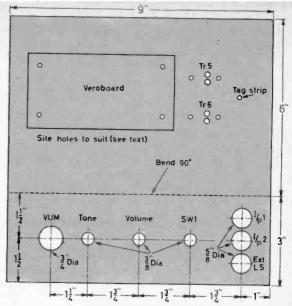


Fig. 4: Details of the metalwork.

deck used. Alternatively, this switch could be incorporated on the main chassis.

CONSTRUCTION

A very simple chassis arrangement is used for the amplifier, the dimensions are shown in Fig. 4. The input sockets and loudspeaker socket are at one end with the VU meter at the other; the function switch, the volume control and the tone control lie in between. The majority of the components are mounted on a piece of Veroboard $5in.\times 2^12in$. (a standard size). Four holes are drilled in this for later mounting to the chassis.

The power transistors, AD161 and AD162, need to be heat-sunk and these are fitted at one end of the Veroboard near the switch. A small tag-strip holds the large capacitor C17 and acts as an anchoring point for the output pair emitter resistors, R24 and R25. R1 and R2 are mounted directly on the input sockets.

Building the Veroboard panel should be straightforward, the layout is shown in Fig. 5. The necessary connections to the board are made with Veropins at

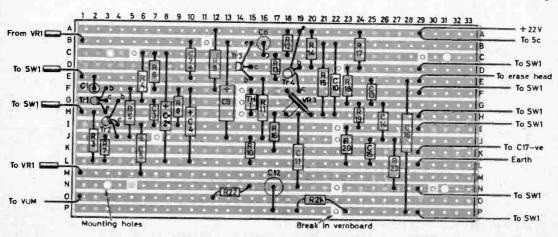


Fig. 5: The main component layout on Veroboard.

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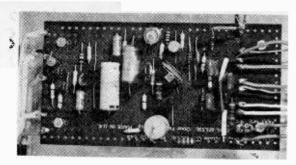
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2Ny923 15p 2N3366 32†p BC 2Ny924 15p 2N5366 32†p BC 2Ny925 15p 2N3366 32†p BC 2Ny925 32†p 2Ny925 32	102 20p BFY20 50p KFY214 2819 T1843 279	2½ × 3½ in 17½ 20°p 2½ × 5 in 21°p 24°p 3½ × 5 in 21°p 24°p 3½ × 5 in 21°p 27½°p 5 × 17 in (Plain) 65°p — Vero Pins (Bag of 36) 20°p Vero Cutter 45°p Pin Insertion Tools (·1 and ·15 matrix) at 55°p.	2-5 watt 5% (up to 270 ohms only).7½p 5 watts 5% (up to 8-2kΩ only), 10p 10 watt 5% (up to 25kΩ only), 13½p POTENTIOMETERS Carbon: Log. and Lin., less switch, 16p. Log. and Lin., with switch, 25p.
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The Veroboard panel—compare this with Fig. 5.

both ends of the board and much work will be saved later if these are fitted at the same time as the main components and soldered in.

There are a number of breaks in the copper conducting strip and these are shown clearly on the diagram.

There is a reasonable amount of room on the board but care should be taken to ensure that extra large components are not selected. The $^{1}{}_{8}W$ resistors specified will fit neatly as shown. The skeleton preset VR3 will also fit neatly into $0\cdot 15$ in. matrix Veroboard if fitted at an angle as shown.

Naturally the output transistors have to be

A29

Power supply -ve

Tr6

R24

Fig. 6: The wiring around the tag strip and the output transistors have to be

sistors.

To SW1

To SW1

To SW1

To LS and

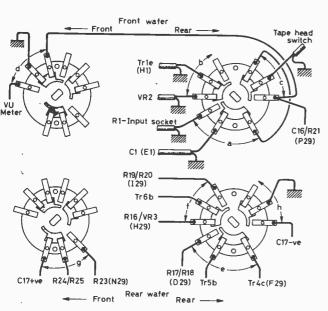
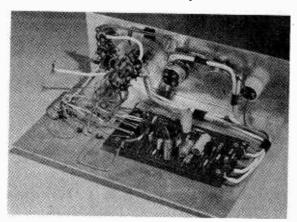


Fig. 7: The record/playback switch wiring.

insulated from the chassis and this applies to Tr6 as well, even though the collector is at chassis potential. It is this sort of thing that can cause earth loop problems.

One connection on the small tag strip is the common earthing point and all wires which carry any appreciable current are earthed directly to this. A second earthing point is on the input DIN sockets but as these wires are taking no current to speak of, no problem arises. When finally connected to the tape deck, be sure that the metal body of the deck is connected to the main earthing point of the amplifier. Certain wires need to be screened, these are indicated on the diagrams.

The switch wiring is shown in Fig. 7. A logical sequency in wiring this up is essential. It is easier to mount the completed Veroboard panel and the other components to the chassis and then proceed with the wiring. A heavy gauge piece of copper wire can be mounted alongside the switch to act as an earth bus bar, this being connected to the common earth point. If the tape deck used has incorporated switch wafers these could be used but this entails a lot of additional wire and could result in instability.



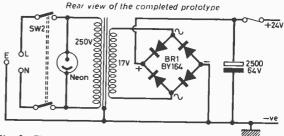


Fig. 8: The circuit of a suitable power supply.

The power supply should be built separately and fixed some distance both from the main amplifier and the tape heads to avoid hum induction. The circuit for a suitable power supply is shown in Fig. 8.

There are only two items that need to be set up. One is VR3; for this a meter should be inserted in the emitter leads of one of the output pair and the quiescent current should be adjusted, using VR3, to read about 20mA. The value of the resistor feeding the VU meter has to be found by trial and error. In use the correct recording level can be found simply by listening for high level distortion caused by over modulation of the tape. When the correct level has been found, the resistor R22 should be selected to read zero level on peaks.

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RF AMPLIFIER

The circuit for this stage is shown in Fig. 5. The 6BA6 is to the right of the ganged capacitor, Fig. 3, and L1 is to the left, near the panel. In Fig. 5, L1 is a "Blue" coil, and L2 the existing mixer "Yellow" coil.

Leads run from VC6 and VC7 through the chassis as in Fig. 3. The aerial trimmer VC8 is fixed to the panel in the position shown in Fig. 4, near the holder for L1. Arrange the valve and coil holders to allow short leads, with separation of grid and anode circuits, and earth the central spigot of the valveholder to the chassis.

The primary of L2 was originally earthed. Pin 8 is now disconnected from the chassis and wired to C1, Fig. 4, shown as C4 in the r.f. stage circuit Fig. 5. Pin 9 is disconnected from the aerial socket and connected to pin 5, V1, Fig. 5.

A piece of co-axial cable is now used for the aerial circuit. Its inner conductor runs from the aerial socket to pin 8 of L1. The outer conductor is connected to the earth socket, chassis, and also to the chassis near L1.

Add the r.f. gain control in the position shown, and disconnect R7 of the i.f. amplifier from the chassis, wiring it to VR1 and R4, Fig. 5.

RF AMPLIFIER ALIGNMENT

Insert a set of three coils. VC8 should peak quite sharply near the h.f. end of each band, unless the aerial is very long. Adjust the core of L1, in the way already described for L2, so that little or no adjustment of VC8 is required near the l.f. end of the band.

There is no loss of efficiency if VC8 and VC3 can

both be used to peak up signals throughout each band, and are not fully open or fully closed. But correct adjustment of the cores will make it unnecessary to adjust these trimmers frequently, except to peak up weak signals, or when changing the aerial or coils.

When dealing with the highest frequency range, note that it is possible to tune L1 or L2 to the wrong side of the oscillator frequency, at the h.f. end of the band. This effect is possible when trimming any circuit of this type, with an i.f. near 465kHz. L1 and L2 should be tuned l.f. of the oscillator frequency, and the second channel, or unwanted response, will be about 930kHz h.f. of this, and will be found as a weaker signal, if a generator is used for alignment.

On the lower frequencies it is not possible to set L1 or L2 to the wrong side of the oscillator frequency.

CARRIER OSCILLATOR/PRODUCT DETECTOR

Fig. 6 shows the circuit of these sections. The product detector V1 occupies the position near the last i.f.t. as in Fig. 3. The carrier oscillator is constructed completely in the box which is later bolted to the left of the chassis, Fig. 3. It is possible to use the carrier oscillator for the reception of both c.w. and s.s.b. using the diode detector D1 but reception is much improved by switching it out and bringing in the product detector V1.

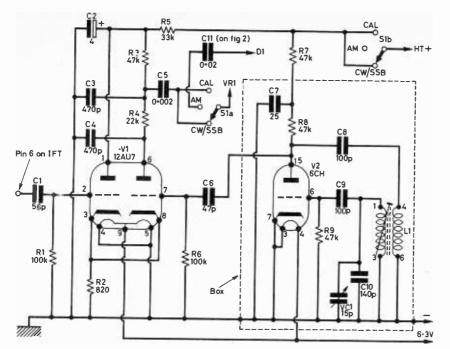
The 3-way rotary switch controls operation of the receiver. Section S1 allows the diode detector D1 to supply signals for a.m. reception, or switches to C5

for s.s.b., c.w. and "Calibrate." Section S1b applies h.t. to both stages in the s.s.b./c.w. and "Calibrate" positions.

A 7×2in "universal chassis" flanged side is taken and its flanges cut away 2in from each end. It is then given right-angle bends 2in from each end, to make an open box 2in high, 3in wide, and 2in deep. A plate 3×2in is cut and bolted to the front flanges.

The valveholder and CO coil are located as in Fig. 3, and all components in the box in Fig. 6 are assembled and wired, with tag strips to anchor h.t. circuits and other

Fig. 5: Circuit of the r.f. amplifier, to give increased sensitivity.



lator and product detector to permit reception of s.s.b. and c.w. signals.

against the chassis. Keep grid circuits away from leads carrying heater current.

After connecting C1 realign the last i.f.t. in the

Fig. 6: Circuit of the carrier oscil-

After connecting C1 realign the last i.f.t. in the way explained. Tune in any transmission, with the switch at the "AM" position and place VC1 in the central position, as mentioned earlier.

Switch to SSB/CW and rotate the core of the CO coil until a strong heterodyne is produced. This is an audio tone which falls in frequency as the correct core position is reached. Passing this position results in the tone beginning a gain and rising in frequency. The correct core setting is the central, zero beat setting.

An audio tone which rises in pitch can then be produced by rotating VC1 either way.

When receiving s.s.b. the carrier oscillator has to replace the suppressed carrier, being adjusted slightly one way or the other, as necessary by VC1. The sideband normally employed depends on the amateur band in use, but the adjustment of VC1 will soon become clear.

For c.w. reception, use VC1 to obtain the most suitable pitch, placing the CO either above or below the c.w. as found to give least interference.

components. A blue lead is run out from pin 4 for heater, a yellow lead from tag 1 for C6, and a red lead from C7 for h.t. circuits.

A back plate 3×2 in with a 12 in flange to bolt to the chassis is bent up, or cut from a spare 3in wide "universal chassis" member. It is drilled so that it can be attached to the back of the CO box with four self-tapping screws into the flanges of the latter.

The CO box is placed so that the bush and spindle of VC1, Fig. 6, project through a clearance hole in the receiver panel. It is fixed here by two bolts through the lower flanges of the box and chassis. The back plate described is then screwed on from behind, and is bolted to the receiver chassis.

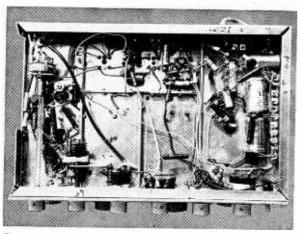
When VC1 is half closed the knob pointer or mark should be vertical.

The function switch is put in the position shown, and h.t. and heater circuits connected.

Most of the small components for the product detector are supported by the valveholder pins, and an adacent tag strip. The lead from C5 to S1 runs

CRYSTAL FILTER

This incorporates an extra stage of i.f. amplification, 3-position selectivity switch, and variable phasing control using the circuit in Fig. 7. It provides



This photograph of the underneath of the receiver can be compared with Fig. 4 (Part 1).

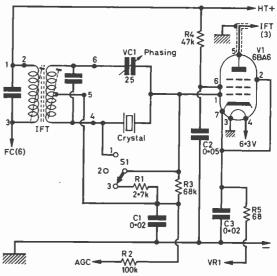


Fig. 7: For increased gain and selectivity this crystal filter unit can be fitted.

* components list

RF STAGE:-

R3 = 100kΩ IW R5 150kΩ 1W R1 1MΩ ½W R4 68Ω 4W All 10% tolerance R2 47kΩ 1W

VR1 10kΩ wire wound potentiometer, linear.

C1 100pF SM

C3 0.1µF

C2 0.02 F disc

C4 (C1, Fig. 4)

VC6 Front section o bandset capacitor

VC7 Front section of bandspread capacitor VC8 50pF variable

L1 From basic receiver (L2)

L2 Miniature plug-in coils (Denco 'Yellow' Ranges 2, 3, 4 and 5)

Miscellaneous:

V1, 5BA6. Valveholders B7G (1) with screen, B9A (1).

CARRIER OSC/P. DETECTOR:

R4 22kΩ ½W R7 47ks 1W R1 100kΩ 1W R8 47kΩ ½W 33kΩ 1W 82012 JW R5 R6 100kΩ ±W R9 47kΩ ±W R3 47kΩ 1W

C1 56pF SM C2 4µF 3507 C3 470pF C4 470pF C5 2000pF

C6 47pF SM C7 0.25 F 350V C8 100µF SM

C9 100pF SM C10 140pF SM

VC1 15pF variable

V1 12AU7

V2 6C4

Miscellaneous:

Valveholders, B9.A [1), B7G (1) with screen. S1a/b/c 3 pole 3 way wafe switch (S1c is for crystal marker). Universal chass s flanged members 7 x 2in (1) 4×3in (Home Radio). L1, BFO2/465 (Denco).

CRYSTAL FILTER:

R5 68Ω 3W R1 2.7kΩ W R3 68kΩ ½W R2 100kΩ ±W R4 47kΩ 1W

C3 0.02µF C1 0.02µF C2 0.05µF

VC1 25pF variable

V1, 6BA6. Crys.al, 465kHz (see text). IFT, IFT11/ 465/CT (Denco). S1, 1 pole 3 way wafer switch. Valveholder B7S and screen. Bushes (2) DL52C, couplings (2) DL60, {in dia. polystyrene rod (Denco). Universal chassis side 7 × 2in (1), 4 × 3in (1) (Home Radio).

CRYSTAL MARKER:

R3 100kΩ {W R1 470k0 JW R2 10kΩ +W R4 22kΩ ½W

220pF SM C3 0.02µF disc C2 0.02µF disc C4 100pF SM VC1 100pF variable

Miscellaneous:

Crystal, 1MH2. Valve, EF91. Valveholder, B7G. Universal chassis side 4×3in (Home Radio). Crystal holder.

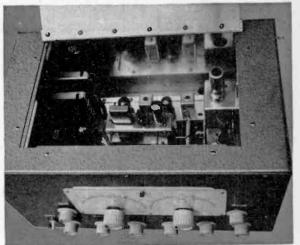
additional gain, and a very great increase in selectivity.

The i.f.t. has a centre-tapped secondary, and VC1 can be adjusted to balance stray capacitance in the crystal and wiring, or to give a rejection notch either side of the crystal frequency. With the switch in position 1, the crystal is out of circuit, and selectivity is that provided by the three i.f.t.'s. With position 2, the crystal is in use working into the relatively high impedance of R3. For position 3, the crystal provides maximum selectivity. Position 1 is suitable for general reception and position 2 is used for other signals except when severe interference from adjacent transmissions is troublesome.

A 3×2×2in box is made in the same way as described for the carrier oscillator. The circuit in Fig. 7 is built entirely in this box, which is then bolted to the chassis, and closed by a plate fixed to the back with self-tapping screws.

The i.f. transformer is situated above a hole in the main chassis, so that its lower core can be adjusted.

VC1 must be insulated from the front of the box, and it is also mounted so as to avoid unnecessary



stray capacitance to the metal. This was done by punching a lin hole in the box and bolting a tein strip of paxolin across inside, with a hole to take the capacitor bush. The spindle is extended by using a small coupling and length of 14in diameter insulated rod, which runs through a bush at the panel.

The 3-way switch is situated immediately under the box, on a chassis bracket and an extension

spindle is also fitted.

The exact frequency of the crystal is not too important, provided it falls near the frequency of the i.f.t.'s (465kHz). A 464kHz surplus crystal was used and a 455kHz crystal, available as a spare for a wellknown communications receiver, also tried. No difficulty arose in adjusting the i.f.t.'s to 455kHz.

A wire-ended crystal can be supported between pin 4 and VC1. Other crystals may need fixing to an

insulated strip or bracket.

Coloured leads pass down through the chassis to identify heater and other circuits. R2 runs to the common a.g.c. line. R5 is connected to the r.f. gain control, which now adjusts the bias of all i.f. stages.

RF leakage round the filter will degrade the very high selectivity so the lead from the f.c. anode to i.f.t. primary is screened from the valveholder right up to the pin of the i.f.t. The anode lead of V1, Fig. 7, is similarly screened.

ALIGNMENT WITH FILTER

Alignment should be checked with a meter, such as used earlier when adjusting the i.f.t. cores. A multi-range meter clipped in to read cathode current of one of the stages receiving a.g.c. is suitable, adjustments being directed towards securing minimum current.

Set the phasing control about half open and the selectivity switch at 1. Tune in a strong transmission. Switch to position 2 and tune slowly across the signal, observing the tuning meter. There will probably be one normal response on the meter, observed as a steady rise and fall while tuning through the signal. A second response should be found, very much sharper, and probably giving only a small dip on the meter. This is the crystal frequency. Leave the tuning at this frequency, and adjust all the i.f.t. cores for best results (lowest meter reading). Switching from 1 to 2 and tuning should show that the i.f.t.'s are now virtually on the crystal frequency.

The phasing control is now adjusted slowly to find the exact point where selectivity is greatest and the

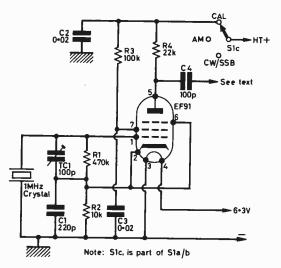


Fig. 8: As a finishing touch this 1MHz crystal marker will provide calibration points throughout the range of the receiver.

response peak (or meter movement) approximately symmetrical a each side of the signal. Repeat this with the switch at 3, and adjust all the i.f.t. cores slightly, if necessary, with a signal tuned in precisely. Adjust the pointer of the phasing control so that it is vertical without moving the control itself.

With the switch at 2 or 3, slight adjustments of VC1 one way or the other will produce a rejection notch which can be moved across the i.f. passband. This should be found to eliminate any interfering signal which is so near the wanted signal that it produces a heterodyne.

CRYSTAL MARKER

Fig. 8 is the circuit of the harmonic marker, which provides crystal-controlled "pips" from 1MHz to 30MHz. TCl allows a slight shift in crystal frequency, so that the unit can be set to zero beat with MSF on 5MHz. HT is applied to the EF91 only when the function switch is in the "Calibrate" position.

The marker is assembled on a sub-chassis which

is 1^3_4 in. high, 4in. wide, and 1^1_4 in. deep made from a single "universal chassis" member 4×3 in cut to leave two pieces, one 4×1^3_4 in and the other 4×1^1_4 in. The flange of the smaller piece is bolted to the straight edge of the larger piece, which can later be attached to the chassis by its flange. After wiring, it is bolted 3^1_2 in from the rear edge of the chassis, behind the bandspread capacitor.

The EF91, TC1, and crystal holder are mounted in line on the top of the sub-chassis with TC1 insulated from the metal. This may be done by punching a hole which adequately clears the bush, and using two washers of \$^1\text{lein}\$ paxolin.

A small tag strip anchors C2, R3 and R4, and a flexible lead to pass to the function switch. C4 is similarly anchored, and a rigid insulated wire a few inches long is soldered here and runs near the ganged tuning capacitor. This was found to give adequate coupling into the receiver.

A blue lead from pin 4 passes to the heater circuit. The chassis return is formed by bolting the marker to the receiver chassis.

Initially place TC1 about half closed. With the function switch at "Calibrate" the 5th harmonic at 5MHz can be located with the appropriate coils in place. Switch off the marker and tune in MSF, which will probably be found on almost exactly the same frequency. If necessary, TC1 is rotated so that the marker harmonic is on the same frequency. Turning TC1 either way from this position will cause a flutter, rising to a low pitched growl or audio tone, the correct setting for VC1 being the central, zero position.

The marker can be used for calibration, enabling the 1MHz tuning points to be marked in, from 1MHz to 30MHz.

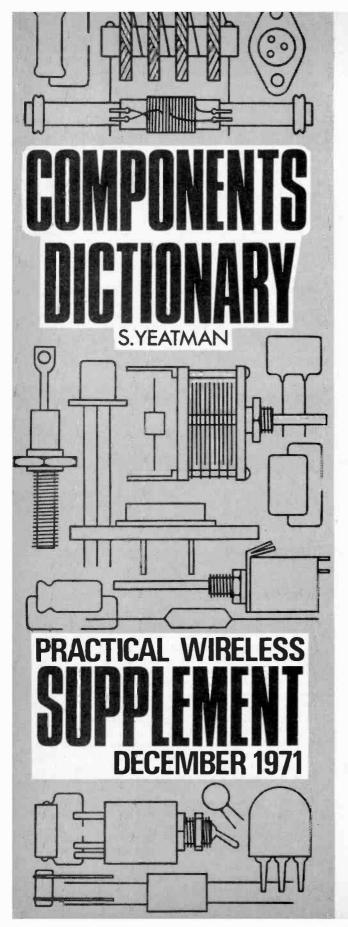
It also allows exact positioning of the bandset capacitor, so that frequencies in a narrow band can be read with the bandspread tuner. To do this, turn the bandspread pointer to the nearest MHz reading, and adjust the bandset capacitor for zero beat. This assures exact reading on the bandspread dial, which is not possible if the bandset capacitor is adjusted visually. This procedure is used at 4MHz, 7MHz, 14MHz, 21MHz and 28MHz, for the 80, 40, 20, 15 and 10 metre amateur bands.

GENERAL NOTES

A piece of thin perspex $8^1_4 \times 3^1_2$ in is used to cover the scales, held with chrome bolts. The perspex was held slightly clear of the panel by 1_2 in wide strips of card at the bottom and each side. This allows slightly thinner card to be slid in, so that a separate pair of scales can be used with each set af coils. There is sufficient space to take all the four ranges on a single permanent card, if preferred.

The case top was cut to give an opening lid about $11^{1}{}_{2} \times 7$ in. A line scribed ${}^{3}{}_{4}$ in from the back, $1^{1}{}_{2}$ in from the front, and $1^{3}{}_{4}$ in from each side. A small drill is used to start a metal saw, to remove this piece. Strips about 1in wide are bolted on inside the cabinet, for the piece removed to close upon, and it is secured along the back with a piano type hinge.

Several $^{1}2$ in holes are punched in the case bottom, and along the back, for ventilation. Openings $3^{1}2 \times 1^{1}2$ in are cut for the aerial and other connections and the mains cord. This can be done by punching pairs of $1^{1}2$ in diameter holes, and sawing between them.



This dictionary has been compiled to assist the reader in identifying the more common components that he will come across when constructing electronic equipment. It will also enable him to choose the correct component for a particular purpose.

AERIALS, ferrite

Ferrite rod aerials are universal in transistor radios and many other receivers, obviating the need for an external aerial. Inductors suitable for the medium and/or long wave ranges are wound on formers on a flat slab or round rod of ferrite material, the formers being movable on the rod for alignment purposes. These inductors take the place of the conventional inductors in the input circuit of the first stage of the receiver.

Ferrite rod aerials have very pronounced directional characteristics having minimum pick-up off the ends of the rod and maximum pick-up at right angles to the line of the rod. This feature can be used to increase the strength of a signal or to null out an interfering signal if its direction is substantially different to that of the wanted

Ferrite aerials are obtainable for use in either valve or transistor circuits.

CAPACITORS, fixed

Any two metal objects (plates) separated by an insulator (dielectric) possess capacitance, or the ability to hold an electrical charge. Introduction of a solid dielectric in place of air increases the value of a capacitor by several

Practical Units: The microfarad (μ F) and the picofarad

 $(pF=1/1,000,000\mu F)$.

Electrolytic capacitors basically consist of two lengths of metal foil separated by a length of insulating material, the whole rolled up and sealed in a tubular container. During the process an electrolyte is introduced often in the form of a jelly. The foil may be aluminium or tantalum which may be etched in order to increase the effective area and thus the capacitance. The insulating material will be as thin as possible consistent with the working voltage of the capacitor. All these measures are aimed at getting the maximum capacitance into the minimum of space.

Electrolytic capacitors are generally polarised, one side (or electrode) always being connected to the positive side of the supply and the other electrode to negative. Generally, the outer case, usually of aluminium, is connected to the negative side although occasionally it is isolated. If the voltage is applied in reverse polarity the capacitor will almost certainly be badly damaged. Plus and minus signs or red and black markings are usually boldly marked on

polarised electrolytic capacitors.

It should be noted that non-polarised electrolytics are

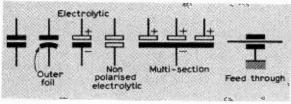


also obtainable but they are the exception rather than the rule. Electrolytic capacitors with as many as four sections are available such as $8+8+16+16\mu F$ usually with a common negative connection, with the one unit being used for smoothing and desoupling purposes. Values of electrolytic capacitors range from $0.25\mu F$ to $10000\mu F$ at working voltages from 2.5V to 600V. Tolerances on nominal capacity are not "symmetrical" as with resistors $(\pm 5\%)$ but may be given as "-10% +50%" or "-10% +100%".

Electrolytic capacitors are used in electronic equipment for smoothing purposes in mains rectifier circuits and as decoupling capacitors on h.t. and cathode circuits in valve radios, amplifiers etc. and as decoupling and coupling components in transistorised equipment.

Fixed Capacitors (non-electrolytic) have several different forms of construction, each with its own special characteristics, which must be taken into account when selecting a capacitor for a particular application, so each type will be described separately.

Silver Mica capacitors are considered very stable with a low temperature co-efficient and thus eminently suitable for use in tuned circuits. The working voltage is generally 350V and capacity tolerance 1 or 2% with values available from $2 \cdot 2$ to 12000 pF ($0 \cdot 012 \mu F$).



Polystyrene capacitors are cylindrical in form with the plastic film forming the dielectric. Possessing high insulation resistance, stability is fair and a negative temperature co-efficient makes these capacitors suitable for temperature compensation purposes in oscillator circuits. Also suitable for coupling and decoupling at radio frequencies. Capacitances available from $2 \cdot 2pF$ to $0 \cdot 1\mu F$ with tolerances of $2\frac{1}{2}$ to 5% and working voltages of 125V or 250V.

Polyester capacitors are also tubular, the dielectric this time being polyester plastic foil, again providing high insulation resistance and thus much superior to paper insulation in every respect. Stability is good and performance at r.f. fair. These capacitors can be used to replace paper ones in all non-critical applications. The range of capacitance is $0.01\mu\mathrm{F}$ to $0.5\mu\mathrm{F}$ with a tolerance of 10% and working voltages of 125V or 250V.

Polycarbonate capacitors are somewhat similar to paper capacitors in performance, having poor stability and only fair capabilities from the point of view of r.f. performance.

Ceramic, tubular capacitors have good stability characteristics together with known temperature coefficients which may be positive or negative and sometimes

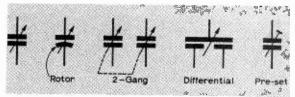
included in the colour code marking. Hence these capacitors may be used to effect temperature compensation of tuned circuits with a fair amount of precision. Care must be taken not to confuse these capacitors with the ceramic "High K" types which have a very high temperature co-efficient and are not particularly stable, being more suited for use as r.f. coupling and bypass capacitors. See table for colour coding.

CAPACITORS, variable

Variable capacitors, like their fixed counterparts, come in a wide variety of sizes and values from the simplest two plate (vane) trimmer to the multi-section tuning capacitor with a total of perhaps 120 vanes.

The moving plates or rotor are usually electrically part of the capacitor framework, the fixed vanes or stator being mounted in the framework on ceramic stand-off insulators to ensure minimum losses. Capacitors intended for use in oscillator circuits, where stability is most important, will have a rotor bearing at each end of the framework while a single front bearing is adequate for other uses.

The spacing between the vanes may only be a few thousandths of an inch in the case of miniature variable capacitors such as are used in transistor radios while those used in small transmitters may have an air gap of a \(\frac{1}{4}\)in. depending upon the d.c. and r.f. voltages existing across the capacitor. In the process of miniaturisation the air dielectric is replaced by a plastic film considerably reducing the physical size of the unit for a given capacitance.



Ganged capacitors may have several sections mounted on a common spindle often with an end section of lower capacitance than the others, for use in the oscillator circuit of a superhet receiver. Each section will have a built-in compression type trimmer for alignment purposes. These trimmers are not generally shown on circuit diagrams. Typical values for a two-gang unit are 176pF+208pF and, for a four-gang unit, 15pF+15pF+500pF+500pF, the latter being intended for use in an a.m./f.m. receiver.

Differential capacitors have two stators arranged about a common rotor so that the capacitance of one is increasing while decreasing on the other, being, in effect, a capacitative potentiometer.

The "law" of a capacitor relates the change in capacity with angular movement of the rotor, common ones being SLF (straight line frequency) and SLW (straight line wavelength). In each case the dial calibration will be approximately linear. The law is determined by the shape of the rotor vanes.

It is possible to obtain capacitors with integral slowmotion gearing obviating the need for a separate dial mechanism.

Trimmer capacitors are generally similar in construction to variable capacitors except that the spindle is short and slotted to take a screwdriver. Air spaced trimmers are not generally available in values greater than 150pF. Ceramic trimmers are two plate capacitors with the plates in the form of silver deposited on the ceramic base and ceramic disc rotor. The maximum value of this type of trimmer is mostly under 50pF.

Compression type trimmers utilise mica or plastic film for the dielectric between a stack of plates the capacity being adjusted by means of a central screw altering the pressure on the plates. The minimum capacitance of this type of trimmer tends to be high but the maximum capacitance can be as much as 2000pF. Typical ranges are 10–80pF and 500–2000pF. These trimmers are commonly known as "padders" and are mainly used in the oscillator circuit of receivers.

CIRCUIT BOARDS

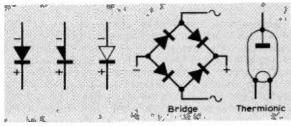
These are flat boards of insulating material on which components may be mounted and wired together to form electronic circuits. The insulation may be s.r.b.p. (synthetic resin bonded paper) or fibreglass. Boards may have the circuit printed on one side by depositing copper by chemical means, the components being interconnected with the circuit through small holes in the board. Copper clad boards having one side covered in copper can be used to form printed circuit boards by etching away the unwanted copper.

Other boards (Veroboard) have a series of copper strips on one side with a matrix of holes, usually of 0·10" or 0·15" spacing, along the strips thus enabling components to be wired between the strips to form a circuit. Plain Veroboard is also available having the matrix of holes but no copper strips. Special pins are used with this board to which components and wiring may be connected.

Edge connector sockets can be fitted to electronic equipment enabling circuit boards to be rapidly inserted or removed for servicing.

DIODES

A diode is a simple rectifier capable of passing current essentially in one direction only and hence may be used to rectify a.c.



Thermionic diodes consist of a filament or heater, constituting the cathode, surrounded by a metal cylinder or anode, all enclosed in an evacuated glass envelope. The diode may be a single unit or one or more may be incorporated with a triode or other valve. Power rectifiers consisting of two diodes, often with a common heater, are used in radio receivers and similar equipment to provide d.c. from an a.c. supply. Thermionic diodes or rectifiers are rapidly being replaced by silicon diodes which do not require a heater and are more efficient.

Semiconductor diodes are generally of silicon or germanium with a point contact or a junction of semiconductor materials. The smallest, a fraction of an inch long, are used for signal rectification and similar small signal purposes while the largest used in power supplies can pass several hundred amperes. Vast quantities of s.c. diodes are used in computers as high speed switches usually as part of integrated circuits. In a silicon diode the resistance in the forward direction is very low and high in the reverse direction. In a germanium diode the resistance in the reverse direction is appreciably lower

than that of a silicon diode.

Semiconductor diodes are marked with a spot or a band or a plus sign indicating the end of the diode that will show a positive voltage when an a.c. voltage is applied to the diode. This end corresponds to the cathode in a thermionic rectifier.

A characteristic of diodes, quoted in maker's data, is the "peak inverse voltage" (PIV). This is the maximum peak voltage allowable across the diode during the nonconducting part of its operating cycle. In practice the p.i.v. will vary between 1·4 and 2·8 times the applied r.m.s. voltage depending upon the type of rectifier circuit employed.

INDUCTORS

While a straight wire possesses "inductance" the value of this inductance will be considerably increased if the wire is formed into a coil or inductor. An iron dust core inserted into the inductor will further increase this inductance.

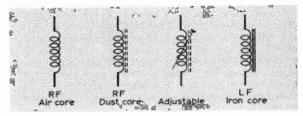
Practical Units: The henry (H), the millihenry (mH= 1/1000H) and the microhenry (μ H=1/1,000,000H).

LF Inductors, or chokes, are a single winding on an insulating former having a laminated core (see Transformers). The inductance will range from one or two henrys to around 50 henrys or so. These chokes offer high impedance to low frequencies and are used in audio amplifiers and filters, loudspeaker networks and as smoothing chokes in mains rectifier circuits.

RF Inductors, or coils, have a single winding, either layer or pile wound, on a low-loss former and may include an adjustable iron dust core for varying the inductance. If the coil is wound with heavy gauge wire the turns may be self-supporting. Windings of comparatively few turns may be added to the inductor to couple it to other circuits or to provide a feedback winding for use in oscillators.

Such inductors, with associated tuning capacitors, are found in r.f. amplifier, mixer and oscillator stages of receivers as well as in transmitters and signal generators and other test equipment. Although they are usually permanently wired into circuit they can be obtained mounted on a plug-in base for rapid coil changing.

The "goodness" or "Q" of an inductor may be enhanced by enclosing it in a ferrite "pot" with or without an adjustable iron dust core.

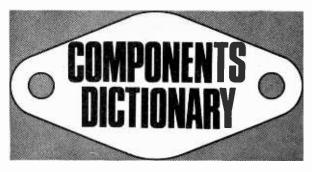


RF Chokes are inductors having a single winding, sometimes on a ferrite core, and of sufficiently large inductance to present a high impedance to specified radio frequencies. The winding may also be in the form of several separated pile wound sections in order to reduce the self-capacitance of the choke.

Values of inductance range from a few microhenrys for v.h.f. work to 30 millihenrys for the lower radio frequencies.

INTEGRATED CIRCUITS

The integrated circuit is produced by methods similar to those used in transistor manufacture and combines a number of discrete components on the one silicon chip. Apart from the transistors or diodes, resistors, capacitors



and inductors can be formed as well as the necessary interconnections.

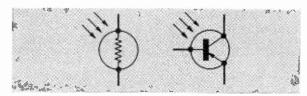
Linear i.c.'s include wideband, audio and operational amplifiers while digital i.c.'s are used in frequency counters, digital clocks, computers etc.

Integrated circuits may be encapsulated or mounted in metal cases. Lead-out wires or tags enable the device to be directly wired into a circuit board or plugged into a suitable holder.

PHOTOCONDUCTIVE CELLS

These devices are sensitive to light, either producing a voltage when subjected to sunlight as in the case of selenium and silicon photocells, or varying their internal resistance as with cadmium sulphide photocells. The latter are also known as light-dependent resistors (LDR).

The silicon and selenium cells will deliver enough power to operate a transistorised radio or even a small electric motor, a single silicon cell providing nearly half a volt at a current of 15mA.



With LDR's the effect of the varying resistance with changes of incident light can be amplified and used to actuate an alarm or counter or similar device. A typical LDR is the ORP12 which has a "dark resistance" of several megohms falling to a few hundred ohms with full illumination.

RESISTORS, fixed

Every electrical circuit possesses "resistance" which limits the current flowing in the circuit. Resistors of known value are used to introduce resistance into circuits, usually to a pre-arranged design.

Practical Units: The ohm (Ω) , kilohm $(k\Omega=1000\Omega)$ and the megohm $(M\Omega=1,000,000\Omega)$.

Fixed resistors (carbon) are moulded from a special carbon composition, the connections to the resistor being in the form of wire ends. Resistors are given a wattage rating by the makers which represents the maximum power that the resistor may safely dissipate. Wattages generally available range from $\frac{1}{8}$ watt to 2 watts in values from 1 ohm to 22 megohms.

The tolerances available on the nominal value are usually plus or minus (\pm) 5 and 10% although 20% was common in the recent past.

The stability of composition resistors is poor but their performance at radio frequencies can be considered fair while their change of value with change in temperature (temp. co-efficient) is poor being about ten times worse than a wire-wound resistor. Such resistors should only be used in non-critical applications.

High wattage carbon resistors, 25W or more, are often used as non-inductive loads for transmitters and amplifiers although they are somewhat difficult to obtain. Constructors can improvise by series/paralleling lower wattage resistors until the required value is obtained.

Fixed resistors (metal oxide/carbon film) are formed by deposition on to a ceramic tube or rod, their main advantage being that of high stability. Tolerances are generally 1 or 2%.

Their performance at r.f. is good although care should be taken in using them at v.h.f. or u.h.f. slnce the metal film is often in the form of a spiral which can introduce appreciable inductance at these frequencies. These resistors are particularly suitable for audio amplifiers and circuits where a low noise level is essential.

Fixed resistors (wire-wound) are composed of a layer of resistance wire on a ceramic tube or rod, with clips or wire ends, and generally having a coating of vitreous enamel or something similar. Some versions have one or more movable clips so that intermediate values of resistance can be had.

Wire-wound resistors must not be used in r.f. circuits since by the very nature of their construction they are highly inductive. Those with special windings and termed "non-inductive" should also be treated with some suspicion at r.f. On the credit side these resistors have a very low noise characteristic and low temperature co-efficient compared to carbon resistors.



Wire-wound resistors are available to the constructor in ratings from 1W to around 50W and in values from $0\cdot 22\Omega$ to $100k\Omega$ usually with a tolerance of 5%. Mains "dropper" resistors are a special breed of wire-wound resistor used in transformerless radios and TV sets and fitted in series with the valve heater chain. They may have adjustable clips or tapped sections.

Resistor values, for carbon resistors, are indicated by a colour coding, details of which are given in the accompanying table. If a tip or spot colour appears to be missing it can be assumed to have the same colour as the body of the resistor. For example, a resistor which is red all over has a value of $2\cdot 2k\Omega$ and one with an orange body and a yellow spot only is $330k\Omega.$

The actual values of resistors in common use conform to the "E12 Series" of twelve values and their decades (see table) but there is also the "E24 Series" with a further twelve values intermediate with the E12 series. These are: $1\cdot1$, $1\cdot3$, $1\cdot6$, $2\cdot0$, $2\cdot4$, $3\cdot0$, $3\cdot6$, $4\cdot3$, $5\cdot1$, $6\cdot2$, $7\cdot5$ and $9\cdot1$ and their decades.

Wirewound resistors usually have their value marked in plain numbers.

RESISTORS, variable

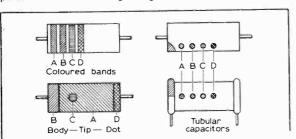
Like fixed resistors, these use either carbon composition or resistance wire for the resistance element. The moving arm or rotor moves over the element thus enabling any value between virtually zero and the value of the variable resistor to be selected. The rotor spindle is extended to take a control knob where frequent adjustment is required, such as with a volume control, or may be short and slotted for adjustment with a screwdriver as a preset control. Potentiometer or "pot" is the general name given to such variable resistors.

Carbon potentiometers have a moulded composition track or a carbon deposit on an insulating ring. The rotor contact, generally with two or more "fingers" to ensure continuous pressure on the track, is usually isolated from the spindle.

The amount of resistance in circuit relative to the angular movement of the rotor constitutes the "law" of the potentiometer, If equal resistance change results from equal angular movement of the rotor the potentiometer is said to be "linear". If the change is logarithmic the potentiometer is "log" law. If checked on a test meter such a potentiometer would show little change in resistance at the beginning of the movement (clockwise) and a very rapid change towards the end of the movement. An "anti-log" potentiometer will show the reverse effect.

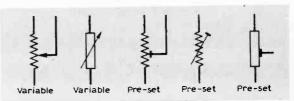
Log potentiometers are generally used as volumes controls on radios and audio amplifiers since the human ear responds to sound levels on a logarithmic basis. Such a volume control will appear to give equal changes in sound level for equal movement of the control.

Potentiometers can be obtained ganged together with a common spindle or with concentric spindles for independent operation. On stereo amplifiers ganged potentiometers are used for volume controls, filter adjustments, balancing and similar circuits where both amplifiers must be adjusted simultaneously. It is common practice to fit a volume control with a single or double pole mains on/off switch operated by the rotor of the potentiometer at the beginning of its travel.



Values of carbon potentiometers go from around 100Ω to about $2M\Omega$. Wattage ratings are not always quoted since these controls are not usually called upon to pass any appreciable current.

Pre-set carbon potentiometers may be of completely enclosed construction or open skeleton type. The latter generally have wire lead-outs or tags suitable for direct mounting on circuit boards.



Wirewound potentiometers are similar in most respects to the carbon ones except that the resistance element consists of resistance wire wound on to a flat insulating strip which is then formed into a ring, the rotor generally moving round one edge of the ring.

Values of these potentiometers of interest to the constructor run from 10Ω to $100k\Omega$ in ratings from 1 to 3W. Again, mains on/off switches can be fitted if required.

Precision wirewound potentiometers have the winding in helical form needing perhaps ten or more turns of the control spindle to cover the whole winding. A turns counter is fitted to the spindle. Preset wirewound potentiometers for use on circuit boards have a straight winding with a sliding contact operated by a screw thread, the whole enclosed in a plastic moulding. For use in adverse conditions of dirt or moisture both carbon and wirewound potentiometers can be had as hermetically sealed units.

SWITCHES

The simplest device for making or breaking a circuit is the on/off switch and from this devolves a multiplicity of types.

COLOUR CODE FOR CAPACITORS AND RESISTORS

	First	Sec'd	Multip	Multiplier		Tolerance 'D'		
	Figure	Figure	'C'			Ceramic	Capacitors	
	'A'	'B'	Resistors	Caps pF	Res	to 10pF	over 10pF	
Disali		0	1	1		2pF	±20%	
Black	1	1	10	10	±1%	0·1pF	±1%	
Brown Red	2	2	100	100	±2%	—	±2%	
Orange	3	3	1,000	1,000	_	- "	±2-%	
Yellow	4	4	10,000	10,000	-		-	
Green	5	5	100,000		_	0·5pF	±5%	
Blue	6	6	1,000,000	_	_	_	_	
Violet	7	7	10,000,000	-			_	
Grev	8	8	100,000,000	0·01µF	_	0·25pF	1	
White	9	9	1,000,000,000	0·1µF		1pF	±10%	
No colour	_	_		-	±20%	_	_	
Silver	-	-	100	-	±10%		_	
Gold	_	_		_	±5%	-		

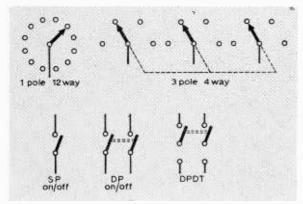
A salmon-pink fifth ring or body colour denotes a Grade 1 high-stability composition resistor. There are variations in the code for capacitors other than ceramic tubular types.



Toggle switches have a laminated or moulded body with a metal or insulated dolly or operating lever. Switch contact combinations include single pole, single throw, (s.p.s.t.), double pole, single or double throw (d.p.s.t. and d.p.d.t.) and double pole change-over. Some types are obtainable with a centre off position. The dolly may be slotted for operation from a cam on an associated control. Other variations include biasing in one position, terminal or tag connections and instrument type toggles which are designed to have very low contact resistance for instrument use.

The ordinary toggle is designed to carry 3A at 250V a.c. with other ratings up to 10A.

Other switches performing the same function as toggle switches include rotary toggle switches, miniature slide switches and press button switches although these are generally s.p.s.t. only.



Microswitches are button operated switches capable of operation with pressures as low as 1 ounce usually by means of a lever or similar attachment. Contact arrangements are fairly simple, on/off or s.p.d.t. the contacts themselves handling 6A at 12V a.c. or 3A at 250V a.c. although models are obtainable for up to 10A.

Wafer rotary switches consist of a flat ring of paxolin insulating material with fixed contacts riveted around the periphery. A disc in the centre of the ring carries the rotor contacts, the disc being rotated by a spindle attached to an index plate. The maximum number of fixed contacts is generally 12 with a maximum of four on the rotor giving various combinations such as 1 pole, 12 way to 4 pole, 3 way.

Since the wafers are very thin several may be mounted on one spindle, sometimes with metal screens between sections to reduce unwanted coupling. These switches are widely used as wavechange switches on radios, audio filters and tone control circuits as well as in meters and test equipment.

Mains switches are available for use with wafer switch assemblies since the wafers themselves should not be used for this purpose. The contacts are not designed to

carry any appreciable current. Wafers in ceramic or other low-loss materials are available for switching r.f. circuits. The switches can be bought as complete units or the individual wafers and parts obtained and assembled to suit particular requirements.

THERMISTORS

Thermistors are a special kind of resistor having a pronounced negative temperature co-efficient. They are used in circuits, such as valve heater chains, to restrict initial current surges when first switching on. The initial high resistance of the thermistor drops logarithmically as the protected device warms up.

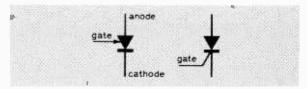


The thermistor is also used to protect photo flood lamps from current surges and in temperature sensitive fire alarm systems. Audio signal generators and oscillators utilise the thermistor in feedback circuits to provide a constant output. Bead type thermistors are used in these circuits since their reaction time to current changes is comparatively short. Bead types can also be employed in measuring r.f. power especially at very high frequencies.

Thermistors in general use have current ratings ranging from 2mA to 2A.

THYRISTORS

Also known as silicon controlled rectifiers (SCR) the thyristor is basically a silicon diode rectifier with an additional electrode or "gate" which is used to control the current flowing through the thyristor. A pulse applied to the gate can switch the thyristor on or off. Once the thyristor is conducting a minimum current is required to maintain conduction.

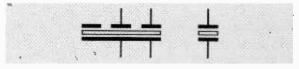


Thyristors used by the constructor will have current ratings between 1 and 10A and peak voltage ratings up to 600V. The p.i.v. figure required for a particular application will be approximately $1\frac{1}{2}$ times the applied r.m.s. voltage.

The gate trigger circuit will need to provide a voltage of the order of 3V at a current of up to 20mA. Small current thyristors are generally contained in a TO5 type metal case with wire lead-outs while the larger thyristors have a stud mounting and tag connectors.

TRANSFILTERS

Transfilters are ceramic filters having somewhat similar characteristics to those of the conventional i.f. transformer. Several transfilters may be combined with capacitors to provide specified bandpass filter features. Several types of transfilter are available around 455kHz as well as for 10·7MHz for use in the i.f. stages of f.m. receivers. Since transfilters do not require any alignment in a receiver they are gradually replacing the tuned i.f. transformers in commercial receivers.

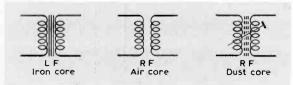


TRANSFORMERS

Basically two coils coupled together so that an alternating current in one coil, the primary, will induce an alternating current in the second coil, the secondary. The ratio of the input voltage, producing the current in the primary, to the voltage at the secondary is directly proportional to the turns ratio of the two coils.

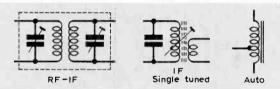
In this way the transformer can be used to match one impedance to another

LF Transformers are wound on a laminated core of ferromagnetic material, the laminations being electrically insulated from each other. Mains transformers may have extra windings for valve heaters, pilot lamps etc. as well as taps on the primary winding to accommodate variations in mains supply voltages.

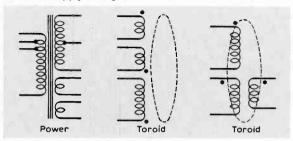


RF Transformers have coils wound in layer or pilewound form, or air-spaced, on insulating formers often with iron dust cores or slugs to enable each winding to be separately tuned.

IF Transformers are similar to r.f. transformers, being designed to work at the fixed intermediate frequency in superhet receivers, usually between 450 to 475kHz or around 1.6MHz. As well as dust cores each winding generally has a fixed capacitor across it in order to obtain the optimum inductance to capacitance ratio.



Autotransformers have a single tapped winding the ratio of the turns each side of the tap providing the required transformation ratio. One winding may be common to both circuits providing an alternative ratio. Note that an autotransformer does not provide the isolation obtainable with a double wound transformer. A common form of autotransformer is the Variac used for compensating changes in mains supply voltages.



Toroid transformers have the windings wound on an annular ferrite core. The separate wires comprising the windings are laid or twisted together and then wound round the ferrite ring. On the circuit symbol the start of each winding is marked with a dot to assist in identification.

TRANSISTORS

The transistor is a three electrode semiconductor device capable of amplifying an electrical signal. The semi-

conductor materials used in making transistors are either silicon or germanium although there are others such as selenium.

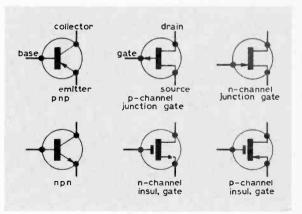
The pure silicon or germanium is treated with either of two impurities in minute quantities to produce 'p' and 'n' type silicon and germanium. A junction of silicon p and n material will show a high resistance in one direction and a low resistance in the other thus forming a diode. A germanium diode similarly formed will not show such a wide change in resistance.

A p-n-p transistor is formed from a thin slice of n material sandwiched between two pieces of p material, the slice being known as the base and the p material as the emitter and collector respectively. An n-p-n transistor has a slice of p material between two pieces of n material.

With an n-p-n transistor the emitter voltage must always be negative with respect to the collector and the emitter of a p-n-p transistor positive with respect to the collector. N-P-N and p-n-p transistors can have very similar characteristics in which case they are said to be "complementary".

Many different processes are used in the manufacture of transistors producing devices of widely varying characteristics and types:

Alloy transistors were among the earliest types produced. The germanium alloy transistors are cheap to produce but do not have a very good performance at high frequencies. They are widely used as power transistors since their low resistance permits the maximum current to be passed at low voltages. Silicon alloy transistors are used mainly because of their ability to operate at high temperatures.



Alloy-diffused transistors have improved performance with a cut-off frequency of the order of 100MHz and being cheap to produce are widely used in radio receivers.

Mesa transistors with a cut-off frequency of over 1000MHz are among the best at high frequencies.

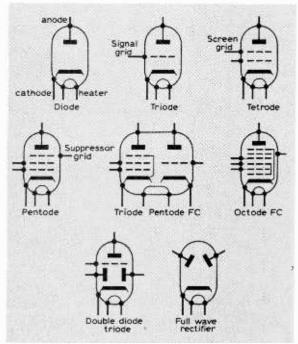
Planar and epitaxial planar transistors have been developed to reduce the collector leakage current and also to include a shield to reduce the capacitance existing between the collector and base electrodes.

Field effect transistors are unipolar as distinct from those listed above which are bi-polar. F.E.T.'s are more akin to the thermionic valve than any previous transistors. While bi-polar transistors are essentially current operated devices and have a low input resistance f.e.t.'s are voltage controlled and consequently have a very high input resistance. The controlling "gate" may be either a junction type (j.u.g.f.e.t.) or insulated type gate (i.g.f.e.t.) either type being obtainable as p-channel or n-channel f.e.t. The i.g.f.e.t. is also known as the metal oxide silicon f.e.t. (m.o.s.f.e.t.).



VALVES

Thermionic valves contain a filament or heater/cathode which emits electrons, with one or more other electrodes. all contained in an evacuated glass envelope. The four basic types of valve are the diode, triode, tetrode/pentode and frequency changer or mixer.



The Diode comprises the cathode and a metal plate or cylinder called the anode. Small single or double diode units are used for signal rectification in detectors and a.g.c. circuits. Larger single or double units are employed in half and full wave power rectifier circuits. A special use for diodes is in the line scanning circuits of TV sets where they are known as "efficiency diodes".

One or more diodes are frequently found in a common structure with triodes and pentodes where they are associated with the signal circuits.

The Triode has a wire mesh, the signal grid, placed between the cathode and the anode. A negative voltage on the grid controls the anode current enabling the triode to be used as an a.f. amplifier or oscillator at a.f. or r.f. A triode is commonly incorporated with a pentode where it acts as a preamplifier.

The Tetrode has a second grid placed between the signal grid and the anode. This "screen grid" reduces inter-electrode capacitance and overcomes a deficiency of the triode known as the "space charge effect".

The Pentode has yet another grid, the suppressor grid, between the screen grid and the anode, which eliminates

the kink in the characteristic curve of the tetrode caused by secondary emission. In "beam" tetrodes this third grid is omitted but its effect is simulated by the careful placement of the anode with respect to the other electrodes. Tetrodes and pentodes are used for both r.f. and a.f. work.

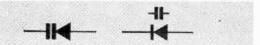
Frequency changers, or mixers, are used in superhets to produce the intermediate frequency (i.f.) from the input signal and the local oscillator signal. The mixer valve takes the form of a pentode or tetrode with additional grids to which these signals are applied. Some frequency changers incorporate a separate triode for the local oscillator feeding internally or externally into the mixer section.

Battery type valves have 1·4V filaments for operation from a single cell, taking a current of 25 or 50mA. The maximum anode voltage is generally 90V. Valves fed from a mains supply may have $6\cdot3V$ heaters which are connected in parallel each heater taking anything from 200 to 600mA. Dual section valves sometimes have heaters with a centre tap allowing operation in series on $12\cdot6V$ or in parallel on $6\cdot3V$.

Other mains operated valves have the heaters in series based on a common current of 100, 150 or 300mA with individual heater voltages of 4 up to 50V. In a.c./d.c. receivers and TV sets the heater chain may be connected across the mains, the difference between the sum of the heater voltages and the mains voltage being taken up by a "dropper" resistor (see Resistors, fixed).

VARICAP DIODES

Varicap Diodes, sometimes known as varactors, are similar to semiconductor p-n junction diodes in that the capacity existing between the regions varies with the applied reverse voltage. Varicap diodes provide known changes of capacity over a given range of reverse voltage, typically 50 to 10pF for a range of 1 to 20 volts.



These diodes can thus be used to tune r.f. circuits by means of a potentiometer controlling the applied reverse voltage. They are useful up to frequencies of several hundred MHz and are currently being employed commercially in v.h.f. receivers and t.v. tuners.

ZENER DIODES

The zener diode is a semiconductor diode which breaks down and conducts when a voltage applied in the reverse direction reaches a predetermined value. The action is somewhat similar to that of a gas filled voltage stabiliser.

The external circuitry of a zener diode must be designed so that its rated power dissipation is not exceeded.



Zener diodes of interest to the constructor are available with nominal zener voltages ranging from 2.4V to 200V with tolerances from 5 to 20% and dissipations from 200mW to 20W. These diodes are used as voltage stabilisers, voltage reference sources, limiters etc.

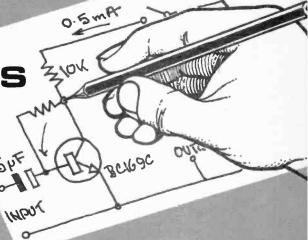
The end of a zener diode intended to be connected to the positive side of a supply is usually marked with a spot or band or a plus sign.

IN NEXT MONTH'S

EXTRA EXPERIMENTERS CIRCUITS

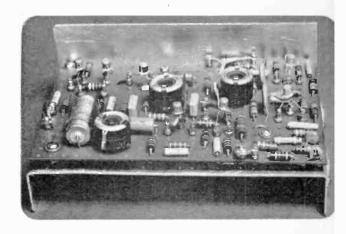
SUPPLEN

Here is a mine of information for anyone who can work from a circuit. Feast your eyes on some of the items which are included; several audio amps, ranging from 50mW to 10W; radio circuits from a crystal set to an all band receiver—plus test gear, novelty circuits, etc., etc. Heapsof circuits with all the necessary information and notes—you'll want to keep it for years!



stereo

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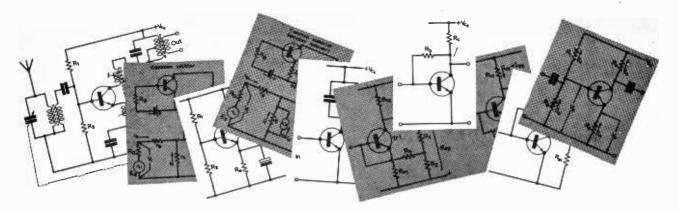


Just think of the photographs you could take if you you could. Now you you could to the photographs you could. Now you you go the could freeze an action for a split second in the could freeze an action for a split shots for a very small could freeze and operated flash trigger unit enables could freeze and operated flash trigger could freeze and operated shots for a very small shots for a outlay and with no additional expensive equipment.

Outlay and with no additional expensitive and ultration is highly sensitive and service to select the service and an SCR.
This circuit, which transistors and an SCR.
Teliable, uses three transistors and an SCR.

This fist-full of probe uses just two transistors and is completely portable. Typical receiver and audio amplifier circuits are illustrated with invaluable hints and tips on how to go about trouble-shooting that faulty set.

ALL IN THE JANUARY ISSUE ON SALE DEC. 3rd.



TRANSISTOR CIRCUITRY for beginners PART 3 H.W.HELLYER

Circuits and Parameters

That ugly word 'parameters' frightens many new-comers—and really, it need not, for it is only the guideline along which we can walk as we follow the curious path of transistor development. There have to be some hard-and-fast rules, and these are the parameters.

Transistors can be of p.n.p. or n.p.n configuration, the essential difference, in practice, being polarity of the supply voltage. The three basic modes are common-base, common emitter and common-collector. The last is more conveniently referred to as emitter follower, for reasons we shall explain. Some of our circuits show p.n.p. transistors, some n.p.n.—we must get it into our heads at the outset that the essential difference is polarity, and this makes it easy to combine the two types in one circuit.

The common-base circuit is a good introduction to transistor technology. Here, a small change in emitter current brings about a small change in collector current. The ratio between the two is the current transfer ratio, alpha (α) .

In symbolic form:
$$\alpha = \frac{\delta l_C}{\delta l_E}$$

where delta (δ) denotes change, in this case, increase. In some formulae, the symbol \triangle may be used instead of δ .

Figures for alpha are very near, but not quite, unity. For a germanium device, typically 0.98.

Take Fig. 9, a proving circuit to demonstrate the above formula. Here we have a common-base transistor connected so that the emitter current flows, around $0\cdot5\text{mA}.$ Voltage $V_{\rm E}$ establishes this. The emitter junction for an average transistor will be around 100 ohms. The collector current, $I_{\rm C},$ flowing through the load $R_{\rm L},$ will be slightly lower than the emitter current. Between base and emitter—the base being earthed, or common, a $1\cdot5$ volt battery biases the emitter positively.

The input voltage, $V_{\rm IN}$, depends on the setting of the variable resistance, $R_{\rm IN}$, which has a further 1.5

volt battery across it, again biasing the emitter positively. The proportion of voltage across the base/emitter junction aided by the position of $R_{\rm IN}$ in series with $V_{\rm E}$ represents the increase $\delta I_{\rm E}.$

The emitter junction resistance of a typical small signal transistor is about 100 ohms, and let us suppose that the load resistor is 10000 ohms. Thus the change at the input is $10\mu A$ through a resistance of 100 ohms, but the change at the output is $9 \cdot 8\mu A$ through a resistor of 10000 ohms. The result, from Ohm's Law, is a voltage change across R_L of 98mV for a change in voltage at the input of 1mV. This gives us a voltage gain of 98 times in spite of a slight loss of current flowing out through the base contact.

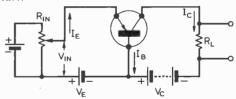


Fig. 9: The common-base circuit arranged to demonstrate change in emitter current causing change in collector current.

With the more frequently used common-emitter circuit, the current transfer ratio is the ratio of current change at the base to current change at the collector, and is designated β (beta) (or sometimes α ?). These parameters, β and α , are mathematically related, the relationships, for those wishing to look further into this being:

$$\beta = \frac{\alpha}{(1-\alpha)}$$
 and $\alpha = \frac{\beta}{(1+\beta)}$

The figures quoted by manufacturers are for small-signal operation unless otherwise stated.

Another commonly seen transistor parameter is the transition frequency, designated f_T . This is the frequency at which the common-emitter current gain falls to unity, and gives an indication of the frequency limits of the transistor.

Hybrid Parameters

Hybrid parameters are widely used in the semiconductor industry to specify transistor characteristics. They are a set of resistance, admittance and voltage and current ratios for given conditions (hence the term hybrid). In the case of the common-emitter circuit these h parameters are:

- h_{ie} :— input resistance, common emitter, output short-circuited.
- $h_{\rm re}$:— reverse voltage feedback ratio, common emitter, input open circuit.
- h_{fe}:— forward current gain, common emitter, output short-circuited.
- h_{oe} :— output admittance, common emitter, input open circuit.

If one group of parameters is known, for one circuit configuration, it is possible to work out the others. In practice, however, such information is more useful to the designer than to the engineer or constructor, who chooses replacement transistors on more empirical lines than a comparison of detailed parameters.

Characteristics of Basic Configurations

Approximate characteristics of the three basic circuit configurations are summarised in Table 1. These must be taken as a guide only, not as accurate conditions for a particular transistor. The table indicates the orders of magnitude of the main parameters with the three configurations: actual figures will of course vary considerably with different types of transistor.

TABLE 1 Features of Circuit Configurations for Comparison

Characteristic	Common	Common	Common
	Base	Emitter	Collector
Input to	Emitter	Base	Base
Output from	Collector	Collector	Emitter
Current Gain	Lessthan unity	About 50	About 50
Voltage Gain	High (approx.	High (approx.	Low (approx.
Input Imped- ance Output Imped-	$250)$ Low (200Ω) High (200 k Ω)	250) Medium (1000Ω) Medium	1) High (100kΩ) Low (1000Ω)
ance	Medium	(40kΩ)	Low (16dB)
Power Gain	(30dB)	High (40dB)	
H.F. Response (Power 3dB down)	High (400kHz)	Low (12kHz)	Dependent on source and load resis- tances
Phase Shift	0°—Output and input in phase	180° (inverse)	0° (in phase)

It will be noted that the details given in Table 1 include power gain and phase shift, the latter stated to show the effect of the different configurations on the polarity of the signal. This last factor is too often overlooked when experiments are made. Another important factor, not given in the table, but necessary for the designer, is the comparison of collector leakage current with the three configurations: except in the common base configuration, this is dependent on the resistance in the base circuit.

Output Characteristics

As can be seen from the output characteristic set of curves of Fig. 10, circuit configuration makes quite

a difference to collector voltage and current relationships (compare these characteristics with the basic pn junction characteristic shown in Fig. 6, Part 1). When considering the choice of a replacement transistor or working out a design it is necessary to take a set of output characteristics, i.e., a family of curves for different base currents—and plot a load line as shown in Fig. 11. It can be seen that with a common emitter circuit when the base current is zero the voltage between emitter and collector is almost the full supply volts, i.e. collector current is very small. (It is actually the reverse leakage current of the collector junction.)

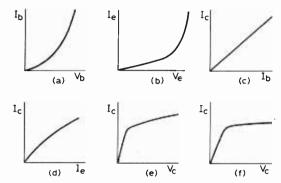


Fig. 10: Typical characteristics showing how circuit configuration drastically alters collector voltage and current relationships.

Increasing base current causes an increase of collector current; the voltage across the load resistance increases and the voltage across the transistor decreases. Eventually, as the base current is increased to a state when the collector current causes a voltage across the load almost equal to the supply

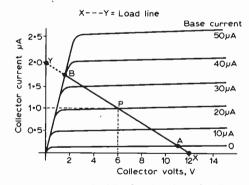


Fig. 11: Constructing a load line for a transistor gives its case history for design purposes.

voltage, the voltage across the transistor drops to practically zero. Any increase of base current beyond this point gives no further increase in collector current—the transistor is saturated. This, for a transistor of given characteristics, is at point B in Fig. 11. The load line, drawn through points X to Y passes through this point B. Point X is the maximum supply voltage and point Y the current resulting from dividing the supply voltage by the load resistance. In the example, a supply voltage of 12 volts and a load resistor of 6000 ohms gives a collector current at Y of 2 mA.

From this load line, the transistor operating point can be chosen by adjusting the base current to a value between the two extremes of A and B. The

best choice is midway along the load line, i.e. at P, where collector current is 1mA and collector volts 6. Since the current gain of our example is 50, the base current must be adjusted for $20\mu A$. This will allow an input signal for linear amplification to produce a base current variation of $\pm 20\mu A$, giving a collector current variation of almost $\pm 1mA$ between saturation and cut-off (at upper and lower ends of the curve respectively).

Correct choice of operating point is important; input and output impedances of a common emitter amplifier stage vary with collector current and so performance depends on the value of the d.c. col-

lector current.

Bias Stabilisation

To set the operating point, a simple method is to arrange that a d.c. base current flows which (when multiplied by the current gain of the particular transistor) gives the required value of collector current. A resistor from the negative supply to the base provides this, but is not really effective, because of collector leakage current and variation with temperature change. For stable operation, bias stabilisation is required, and the two circuits of Fig. 12 are methods of ensuring this.

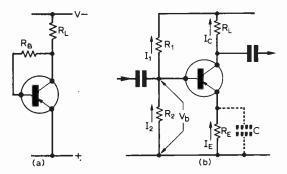


Fig. 12(a): Base bias current feedback and (b) voltage bias.

In Fig. 12(a) a resistor R_B is coupled back from collector to base so that if the collector current increases, collector voltage falls and this fall is reflected back to base via R_B, reducing base current. This tends to reduce collector current and oppose the change. However, this method does not allow control with zero base current and slight variations between transistors do not allow replacements to be made without reconsideration of the value of R_B. A further point is that a.c. negative feedback is introduced by this method, and this may not be wanted. Splitting the bias resistor and bypassing the centre point to chassis with a suitable capacitor can reduce this feedback.

A better method is shown in Fig. 12(b). The bias voltage V_b applied to the base is obtained from a potentiometer R1 and R2 across the supply. A further resistor $R_{\rm L}$ is put in the emitter circuit. The voltage across $R_{\rm E}$ is equal to V_b less the voltage dropped across the emitter-base junction of the transistor. If V_b is made large with respect to this junction voltage, the emitter current will depend only on V_b and $R_{\rm E}$. Thus if V_b is held constant, I_E and therefore I_C will be independent of temperature and transistor gain.

A comparatively low value of R2 will not cause a significant change in $V_{\text{b}}.$ Actual values can be seen in

later circuits, and it will be noted that R1 is four or five times the value of R2. $R_{\rm E}$ depends on the transistor to be employed, and it will usually be bypassed by a large value capacitor (C, shown dotted) to avoid loss of gain with an a.c. signal.

Practical Circuits

Two low frequency amplifier circuits using this method of base bias stabilisation are depicted in Fig. 13. In the first, transformer coupling is used between stages, and in the second RC coupling is employed (note the polarity of the electrolytic coupling capacitors: in p.n.p. transistor circuits the succeeding base will generally be positive with respect to the preceding collector). Because a more precise impedance match between stages can be made with a transformer, and thus the greatest energy transfer effected, this type of coupling is widely used.

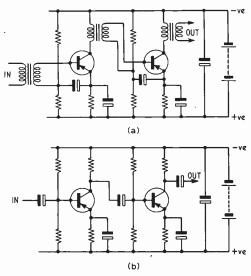


Fig. 13: Circuits demonstrating base bias voltage stabilisation, (a) transformer coupling and (b) RC coupling.

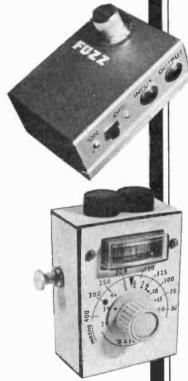
As with valve-operated receivers intermediate frequency stages use transformer coupling, with the windings tuned to the appropriate frequency, as we shall see later. But for audiofrequency purposes coupling transformers are not so economical as resistor-capacitor combinations, and some efficiency is sacrificed to save costs.

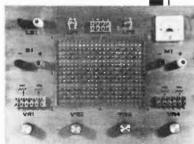
Having laid the ground and, it is hoped, taken some of the fearsomeness from formulae, we shall proceed to a breakdown of some of the circuitry likely to be met in radio and audio gear, with a few notes on constructing both the simple circuits themselves in practical form and test devices that can help us handle transistors with more confidence.

TO BE CONTINUED

We regret that, due to shortage of space, several regular features have had to be held over. These will be resumed as soon as possible.







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H. SUPPLIES



The Modular Audio Mixing System is designed to allow any combination of signals to be mixed. The previous two parts have described some of the preamp. circuits and this final part concludes these and describes the final mixing and level monitoring arrangement

MICROPHONE PREAMP (MIC Hi ZT)

This circuit shown in Fig. 19 is for microphones with built-in transformers or can be used with a microphone transformer at the input. The input impedance is about $100 \mathrm{k}\Omega$ and is suitable for microphone transformer secondaries, usually classified as medium to high impedance. The amplifier is a direct coupled BC109 pair with d.c. stabilization and negative feedback between the output and the emitter of Tr1 to set the gain. The circuit board layout is given in Fig. 20.

PREAMP FOR CRYSTAL PICK-UPS

The requirements are a high input impedance and a sensitivity between 500mV and 1V r.m.s. The large

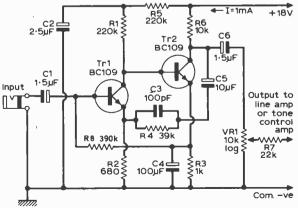


Fig. 19: Circuit of the preamplifier for use with microphones with built-in transformers.

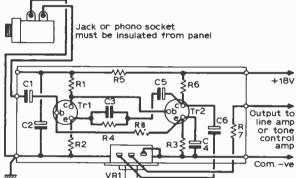


Fig. 20: Layout for the circuit shown in Fig. 19.

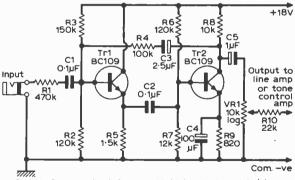


Fig. 21: Preamp. circuit for use with high output crystal pickups.

value series resistor and emitter follower input provide the high impedance input and the gain, and therefore input sensitivity, is set by negative feedback from the amplifier (Tr2) output to the circuit input. The nominal input sensitivity is 850mV. The output network VR1 and R10 is again as common to all the preamplifiers. The circuit board layout is given in Fig. 22.

PREAMPLIFIER FOR GUITAR (G)

Some guitar pick-up units have a high output and

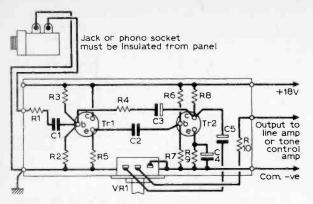


Fig. 22: Layout for the crystal pickup preamplifier.

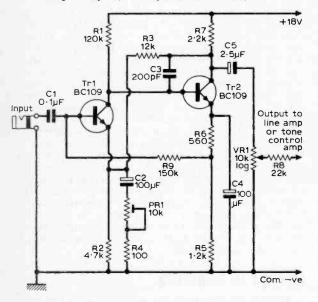


Fig. 23: The preamplifier circuit for use with low output guitar pickups.

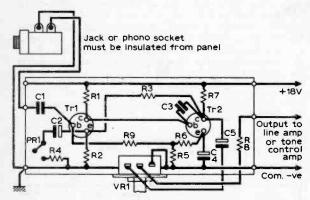


Fig. 24: The component layout for the guitar pickup preamplifier.

these could be connected to a line level input which, in conjunction with the line amplifier, has an input sensitivity of approximately 200mV. Low output, medium impedance guitar pick-ups may provide signal levels from around 20mV to perhaps 100mV and require some amplification. The circuit given in Fig. 23 is quite a conventional arrangement originally due to Mullards and has provision for setting the

* components list

			-		
BALL D		/B#!-	11: 77		
Mic Pre-amp (Mic Hi ZT)					
Tr1, Tr					
VR1	10kΩ	Carbor	log. pot.		
Resistors					
Resisto R1	rs 220kΩ	R5	220kΩ		
R2	680Ω	R6	10kΩ		
R3	1kΩ	R7	22kΩ		
R4	39kΩ	R8	390kΩ		
			% types		
Capacitors					
C1	1.5µF	25 V	C4	100µF	25V
C2	2 5μF	25V	C5	10μF	25 V
C3	100pF		C6	1.5µF	25V
	- 4	24 -	-		
Crystal p.u. Pre-amp (P.U. Xtal)					
	r2 BC109				
VR1	10kΩ	Carbor	log. pot.		
Resisto R1	7S 470kΩ	R5	1.5kΩ	R9	820Ω
R2	120kΩ	R6	120kΩ	R10	22kΩ
R3	150kΩ	R7	12kΩ	1/10	ZZRSZ
R4	100kΩ	R8	10kΩ		
	All	±W, 10%	types		
Capacit	ors				
C1	0·1μF		C4	100μF	25V
C2	0.1µF		C5	1μF	25 V
C3	2.5µF	25 V			
Guitar Pre-amp					
Tr1, T					
VR1	10kΩ		n log. pot.		
PR1	10kΩ	Carbo	n preset		
Resisto	rs				
R1	120kΩ	R4	100Ω	R7	2·2kΩ
R2	4·7kΩ	R5	1·2kΩ	R8	22kΩ
R3	12kΩ	R6	560Ω	R9	150kΩ
		All & VV, I	0% types		
Capacit			CA	100 F	051/
C1 C2	0·1μF 100μF	25V	C4 C5	100μF 2·5μF	25 V 25 V
C3	200pF	25 4	Co	2.5με	23 4
	Loop.				
Line Innut					
Line Input					
VR1 10kΩ carbon log. pot.					
R1 22kΩ (‡W, 10% type)					
VII Motor					
VU Meter Type V403 Henry's Radio					
Type	V403	Henry'	s Radio		
Insulated input jack or phono sockets as required.					
misulated input jack of phono sockers as required.					

overall gain from about 12 to 40dB. This is controlled by PR1 which sets the amount of negative feedback between Tr2 collector and Tr1 emitter. With PR1 at maximum resistance the gain will be at 12 to 13dB and about 40dB with PR1 at minimum. The input impedance is typically $100k\Omega$ and suitable for the majority of medium to high impedance guitar pickups. PR1 should be adjusted so as to provide not more than the requisite 100mV or so output between R8 and earth with VR1 at maximum. The circuit board layout is given in Fig. 24.

LINE LEVEL SIGNAL INPUTS

Line level usually refers to signals of over 100mV or so which are linear i.e., requiring no equalization and no preamplification other than that necessary to bring the level to the requirements of the system output, in this case to a uniform 1V r.m.s. As no preamplifier is required, line level signals, such as from a radio tuner, tape recorder external amplifier output, etc., could be coupled directly to the line amplifier but as the outputs from other sources i.e., preamplifiers and/or other line inputs are also to be connected, the passive mixing component must be included to prevent any one signal source loading the others. Line level inputs are therefore connected to the line amplifier via a gain control and series resistor $(22k\Omega)$ in the same way as the output from each preamplifier is connected. This method is commonly used in signal mixing circuits so that any one signal source can be controlled independently of any other. The series passive component has been made high $(22k\Omega)$ compared with the gain controls. each of which are $10k\Omega$. The insertion loss is a little higher but the higher value series resistor ensures complete fadeout of the signal when a gain control is at minimum and that no loading is imposed on other mixing circuits. The circuit for the line inputs, as

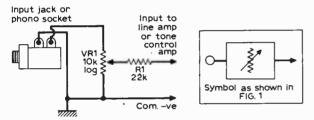


Fig. 25: The resistive arrangement for the line inputs.

shown in Fig. 25 consists simply of the gain control and series resistor. Up to half a dozen line inputs can be used but more than this number could cause loading. If say, four or five preamplifiers were used, then the number of line inputs should be limited to three or four. Much the same applies to the total number of preamplifiers e.g., six should be about the limit with two line inputs.

VU LEVEL METERS

VU meters with built-in rectifiers are readily available and most of these will read well over full scale with a 1V r.m.s. signal. This allows a VU meter to be connected across the line amplifier output with a series variable resistor so that the meter can be adjusted for a maximum signal indication of 1V r.m.s. equals 0dB. The meter could also be adjusted to read in conjunction with a tape recorder level meter in cases where the mixer is remote from the recorder. The connection is simple enough as shown in Fig. 26 but note that the meter must be one with a built-in rectifier and provide full scale deflection for at least 600mV of signal.

GENERAL APPLICATIONS

As already mentioned in Part 1, the various preamplifiers, tone control unit and line amplifier can be connected together to provide signal mixing facilities for sound recording, public address and

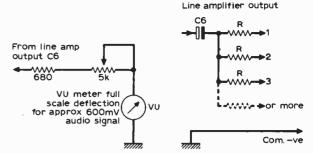
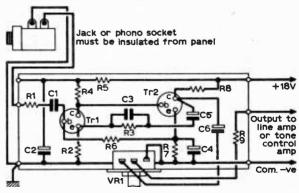


Fig. 26: (left) The VU meter arrangement.
Fig. 27: (right) The arrangement for feeding more than one amplifier.

discotheque or music amplification systems. The high signal output of around 1V r.m.s. is sufficient to directly drive many power amplifier modules now available so in fact a complete multi-channel amplifier system is perfectly feasible. The various combinations given in the block diagram in Part 1 are but a few of the possibilities and any combination can be extended for stereo operation simply by duplication. For stereo mixing systems ganged gain and tone controls are not necessary, in fact separate controls are advisable, as they allow much more control over stereo balance. The output from the line amplifier can be coupled to more than one amplifier or tape recorder simultaneously or for example to a tape recorder and an amplifier for simultaneous recording and monitoring. As the input impedance of external equipment may vary, external equipment connections should be made via series resistors as shown in Fig. 27. Normally each resistor can be $47k\Omega$ but this may be reduced to as little as $10k\Omega$ if the higher value reduces the output signal too much as it may do if external equipment has a very low input impedance.

LAYOUT IN CABINETS

The photos shown in the previous parts are of a small mixing system which would be ideal for tape recording enthusiasts and, as can be seen, each of the preamplifiers are simply mounted side by side. The built-in screens prevent crosstalk and shield the boards from hum pick-up. Nevertheless a metal cabinet should be used for any system derived from the various modules. The mains power supply should be situated away from the preamps and preferably in a screened compartment.



Last month's Fig. 12 (page 619) showed the incorrect layout. The correct layout for the crystal mic. preamp. circuit is shown above.



III II III III 2-Octave

niature Organ

F. C.JUDD

PART 2

THE completed keyboard is mounted in a tilted position as in Fig. 9b on a hardboard base that fits into the top of the organ. This base also carries the circuit board and battery etc. The piece of hardboard is cut as in Fig. 9a and the keyboard mounted as in Fig. 9b so that the keys themselves are

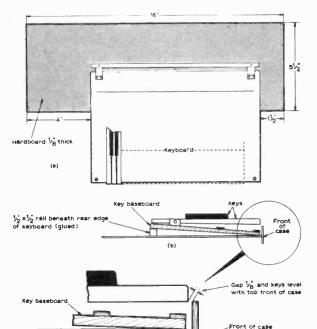
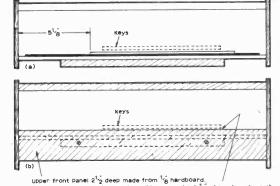


Fig. 9: Details of the keyboard mounting.



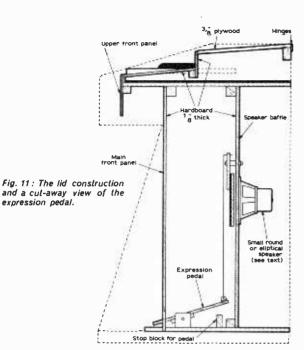
(secure panel so that lower edges of keys are about ${}^{1}8$ above top of panel)

Fig. 10: A front view of the keyboard mounting and the siting of the upper front panel.

level. It is important that when the completed keyboard is fitted in the top of the case that the front of the keys are aligned with the top of the upper front panel as shown in Fig. 9c and also in Fig. 10 so that when a key is depressed the top does not come below the upper edge of the panel. When the keyboard has been correctly aligned it can be secured in the organ cabinet.

The lid of the organ is made up as shown in Fig. 11 and in the photo. Appropriate dimensions for the lid are best derived from the inside measurements of the top of the case and the height of the keys but the lid must be made so that the centre portion drops directly behind the black keys. The whole of the lid is hinged on the rail at the rear of the cabinet. Figure 11 also shows more detail concerned with the expression pedal system. Ensure that when the lid is closed down it does not foul the keys and that all the keys can be depressed and will return to their rest position.

At this stage the painting might well be done but first the keyboard and the main front panel should be removed. If a music stand is to be included this should be fitted and can be made from a piece of hardboard about 12 x 7in. attached to the lid by a



short length of 12 x 12in. batten. The original organ was finished with a bright red gloss paint over an undercoat of emulsion paint.

When the decor is complete the loudspeaker can be installed and the expression pedal (if used) adjusted. The on/off, vibrato and voice switches can be fitted to the left hand portion of the lid and a back cover made up of hardboard to close in the rear of the organ. Two small wood blocks should be fitted inside, one either side of the keyboard, and flush with the upper front panel. These act as stops when the lid is closed down and take a screw through each side of the lid so that it can be secured against opening by small hands. These blocks are just visible in the photograph.

The component board is mounted just behind the key contact frame as shown last month - and allows for convenient short connections between the tuning pre-sets and the key contact wires. A rear view of the completed organ with the circuit board in position is shown.

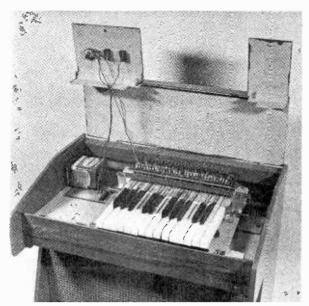
TUNING

expression pedal.

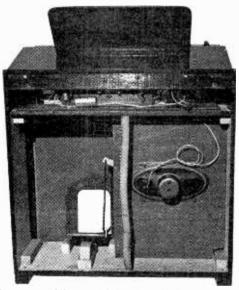
First adjust all the pre-sets, including PR1, to midway travel and set S1, the vibrato switch, and S2, the voice switch, so that both are open. Tuning is best done with a piano and should be commenced with the pre-set for the F key (No. 25) at midway. Now tune the F note to pitch at 698.4Hz with PR1, the initial pitch control. The remainder of the presets from E No. 24 down to F No. 1 at 174.6Hz can now all be tuned one after the other.

The vibrato should produce a pleasant pitch variation, not too pronounced, at about 6 to 8Hz. The intensity of the vibrato can be increased by reducing R14 to 100kΩ or decreased by making R14 about $150k\Omega$. The vibrato frequency can be altered by slightly increasing or decreasing the value of R2. With the voice switch S2 closed, the tone should be flutelike and somewhat softer.

The expression pedal will reduce the sound level somewhat but if moved up and down quickly whilst



A view of the keyboard with the lid raised.



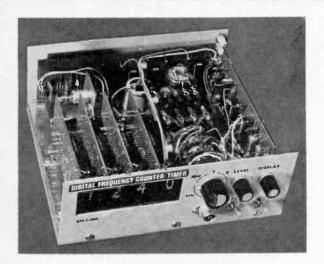
A rear view of the completed project with the back removed.

a note is sustained will produce a pronounced "wahwah" effect which will no doubt intrigue the junior player.

The organ will stay in good tune for a long time, or until the battery voltage falls and the two octave range allows for the playing of a wide range of tunes. Like the author's grandson who has become the final owner of the prototype, any youngster will get a great deal of enjoyment from it.

In the circuit of the 2-octave miniature organ published last month (Fig. 1, page 594) there is an error in the multivibrator circuit. C6 should connect between the collector of Tr2 and the base of Tr3 and not between the bases as shown. In Fig. 2 the resistor next to R1 should read R14 and not R13 as shown.

DIGITAL FREQUENCY COUNTER/TIMER



PART 4 (continued from the November issue)

Frequency measurement is the primary purpose of the instrument and although, on low and medium frequency signals of a reasonable amplitude, it is sufficient to connect the signal and read away, better results may be obtained particularly on the higher frequencies if the controls are set correctly.

It should be remembered that the purpose of the input clipping stage is to provide, from the input signal, a clean squarewave suitable for driving the

signal gate and decade counters.

With the input switch in the "AC" position the input a.c. signal can be "slid up and down" the input characteristic of Trl by rotating the LEVEL control, so that symmetrical clipping takes place.

The smaller the input signal and the higher the input frequency the more important it is to set the

LEVEL control correctly.

With the signal applied to the input and the function control set to a low frequency range, the LEVEL control should be carefully rotated from one end to the other and the range noted over which a steady reading is obtained. The correct setting is in the centre of this range (see Fig. 19).

The actual physical position of the control depends to a large extent on the individual characteristics of Trl. (It may be possible to substitute other types of f.e.t. in place of the 2N3823 but the spread of characteristics may make the LEVEL control in-

operative.)

It is assumed that normally the signal to be measured will be clean and free from hum and noise. However, if a large amount of hum (mains ripple) is present on the signal to be measured this may cause errors due to the clipper stage being saturated for periods of the hum waveform, as shown in

A solution to this problem is to use a simple high pass filter, as shown, which will effectively remove the low frequencies whilst allowing the r.f. signal to pass through.

J THORNTON-LAWRENCE GW3JGA

Assuming that the LEVEL control has been set to its optimum position, the function switch should then be rotated to a position where the first digit of the displayed reading appears on the left hand tube.

Suppose that a signal of 7.054321MHz is being measured, the reading of frequency should be 7.054MHz. Setting the function switch to the highest frequency range will cause a reading of 07.05MHz to be displayed and obviously the frequency is not being measured as accurately as it can be.

Conversely, by moving the function switch the other way to a lower frequency range, the 7 disappears off to the left and a reading of 0543 is dis-

played.

This procedure may be repeated until in the Hz position the reading will be 4321, the right hand figure indicating cycles per second and the left hand figure indicating kHz.

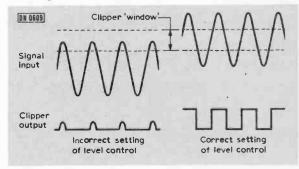


Fig. 19: Waveforms showing correct and incorrect settings of the LEVEL control.

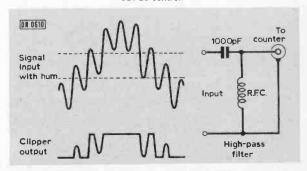


Fig. 20 : Effects of hum and noise on the input signal. A simple high pass filter is shown on the right.

This is a useful facility for measuring small changes in frequency, e.g. checking variable frequency oscillators, frequency modulation systems, and monitoring the frequency of a signal generator when aligning the i.f. stages of a receiver and checking crystal filters.

It is important to remember that whilst this measurement gives very high discrimination it is only a relative measurement of frequency and is not an absolute measurement to this accuracy. The stability of the internal crystal oscillator is insufficient for this to be so.

Calibration Outputs

The 100kHz, 10kHz and 1kHz outputs at the rear of the instrument may be used for calibrating receivers. This can be done by loosely coupling the appropriate output to the input of the receiver. A series coupling capacitor and resistor of about 1,000pF in series with 1k Ω should be used as each output is directly connected to the divider circuits and an accidental short to earth or worse still to a high voltage would upset the operation of the divider and may cause permanent damage.

Time and Period Measurement

The simplest time measurement for the instrument to make is in measuring the time of one cycle of a repetitive waveform. This is useful for frequencies below 100Hz as greater accuracy can be obtained.

On the time ranges of the instrument, the counting is initiated by the negative going part of a signal and stopped by the next negative going signal. The operation on various waveforms is shown in Fig. 21a, b and c.

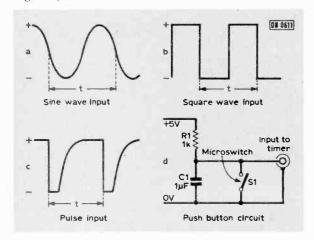


Fig. 21: Operation of various timing waveforms. Circuit on the right provides a fast negative going pulse when S1 is closed.

For the timing of events, as an electronic stop watch, it is necessary to provide a circuit which will generate a fast negative going pulse when a button is pressed. A suitable circuit is shown in Fig. 21d.

The $1\mu F$ capacitor C1 is normally charged to +5 volts through R1. When the microswitch is pressed a sharp negative going voltage step is pro-

duced which starts the timer counting time. The switch is released and R1 recharges C1. When the switch is pressed for the second time the negative pulse stops the count and the total time between the two operations is displayed in mS or seconds depending on the setting of the function switch. The purpose of C1 is to prevent the contact bounce in S1 from causing false triggering of the instrument.

For automatic operation, two photocells may be used and a suitable circuit for timing the duration between two events is shown in Fig. 22.

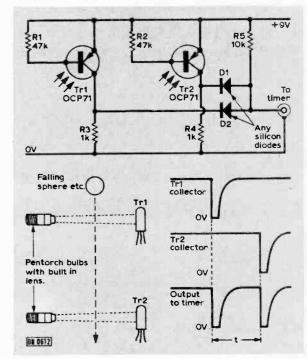


Fig. 22: Circuit shown above is suitable for automatically timing the duration between two events.

An extension of this system with more powerful light sources may be used for race timing, horse trial events, etc.

In the above applications of start-stop pulses it is suggested that the input switch is set to the "AC" position and that the LEVEL control is adjusted to the position which gives reliable operation, this is usually slightly higher (clockwise) than the centre operating point used in frequency measurements.

Very Low Frequency Input Signals

For very low frequency signals where the input coupling capacitor may attenuate the signal severely the input switch may be used in the "DC" position. This may result in the LEVEL control having little or no effect. However, if the input signal has an amplitude of about 10 volts peak to peak about earth potential, reliable operation of the instrument should be obtained.

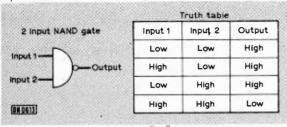
The integrated circuits used in the Digital Frequency Counter Timer are the 74 series of TTL (Transistor-Transistor Logic) in the 14 and 16 pin DIL (dual in line) package. The device operates from a supply of +5 volts (4.5V min., 5.5V max.).

In the operation of the logic only two states are possible, 0 and 1.

logic 0="low" = less than +0.8volts. logic 1="high" = greater than +2.0volts.

7400N Quadruple 2 Input Nand Gate

This device contains four separate identical two input NAND (NOT AND) gates, as shown in Fig. 23.



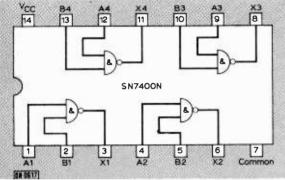
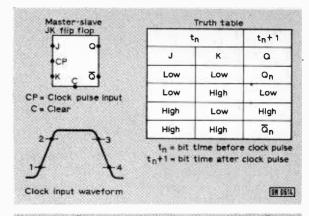


Fig. 23: SN7400N integrated circuit and truth table.

Each gate has two inputs and one output and the operation is shown in the truth table. It can be seen that only when input 1 AND input 2 are high will the output NOT be high, i.e. low. In the circuit of the instrument some gates are shown with only one input and here the other input is left disconnected. This is equivalent to connecting it to a high input. In this condition the gate becomes an invertor, the output condition is the inverse of the input.

7473N Dual Master-Slave J.K. Flip Flops

The SN7473N contains two Master-Slave J.K. Flip Flops, each flip flop contains a large number of gates all internally connected to form a bi-stable or flip-flop in which the state of the outputs for specific input conditions is clearly defined. This is shown in the truth table in Fig. 24. What this means is that if J and K are both low, no change takes place during the clock pulse. But if K is high and J is low the clock pulse will cause Q to go low and conversely if J is high and K is low the clock pulse will cause Q to go high. And finally if J and K are both high O will change state at each appearance of the clock pulse. With J and K both high the circuit makes a divide by two divider stage, the output from Q being half the frequency applied to CP.



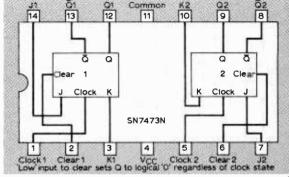


Fig. 24 : SN7473N integrated circuit and truth table. The sequence of operation relative to the clock waveform is also shown.

In the master-slave JK flip flop, the input to the master section is controlled by gates operated by the clock pulse. The clock pulse also regulates the state of more gates which connect the master and slave sections. The sequence of operation, relative to the clock waveform shown in Fig. 24, is as follows:

- 1. Isolate slave from master.
- 2. Enter JK input information into master.
- 3. Disable input gates.

4. Transfer information from master to slave. The input C is a direct clear input which restores Q to low irrespective of any other input signals., opposite logic condition to Q.

instrument is in storing information and transferring this on the application of a pulse to the clock pulse

 \overline{Q} is the reciprocal of Q and always has the The use of the Master-Slave JK Flip Flop in the input.

7490N Decade Counter

The SN7490N contains 4 flip-flops and 3 gates forming a divide by 2 stage and a divide by 5 stage.

When used as a binary coded decimal counter, the signal input goes to the divide by 2 stage and from the output of this to the divide by 5 stage. The binary coded decimal output is then available as shown in Fig. 25.

When used as a frequency divider, as in the Crystal Oscillator divider panel, it is more convenient to feed the signal into the divide by 5 stage first and then the divide by 2 stage, this ensures a 1:1 square wave output which has certain advantages when used as a calibrator output. The other arrangement

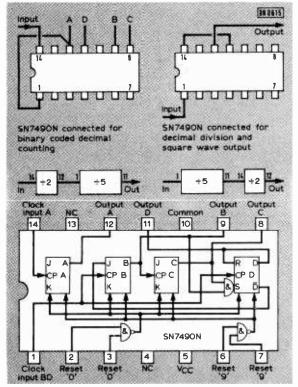


Fig. 25 : SN7490N integrated circuit used as a binary coded decimal counter.

will of course also divide by 10 but the output waveform is far from symmetrical. The SN7490N has input connections for resetting to "9" or "0" and in the instrument only the reset to "0" is used.

74141N B.C.D. to Decimal Decoder Driver

This device contains a complex arrangement of gates terminating in ten high voltage transistors for driving the numeral indicator tube. The operation of this device was illustrated in Part II of this series (Fig. 9, page 480, October 1971 issue).

A number of queries have been received regarding the use of a SN7441AN device in place of the SN74141N. The SN7441AN was in fact used in the prototype and whilst a number of these functioned satisfactorily a few gave trouble by loading the decade counter excessively and causing an incorrect count.

The SN74141N is an improved version of the original SN7441AN.

B.B.C. RADIO LONDON

Sunday, November 7th at 3 p.m. on 95.3 MHz.

"Don't call us 'hams'!"

featuring radio amateurs of London, with Sylvia Margolis, past P.R.O. of the Radio Society of Great Britain



NE of the attractions of medium wave DXing is its unpredictability, a feature which is very apparent when the listener searches for North American DX. Although reception conditions can vary considerably from night to night, there is also a long term trend which follows the sunspot cycle; the best medium wave DX occurring in years of low sunspot activity. We are now well past the maximum of the current sunspot cycle and can expect an allround improvement in long range reception on m.w.

Last month it was suggested that the newcomer to MW DXing should listen on 1070kHz after 2300hrs for the Canadian CBA located at Moncton, New Brunswick. Other North Americans that are frequently heard in this country during the early part of the night are CNB 640kHz in St. John's, Newfoundland; WNBC 660kHz in New York City; WABC 770 also in NYC; WHDH 850 in Boston; CBH 860 in Halifax, Nova Scotia; WABI 910 in Bangor, Maine; CJCH 920 Halifax, N.S.; CJON 930 St. John's; CHER 950 Sydney, N.S.; WINS 1010 NYC; WBZ 1030 Boston; WBT 1010 Charlotte, North Carolina. An unusual catch is Radio St. Pierre 1375kHz situated at St. Pierre, the capital of the French islands of St. Pierre et Miquelon, located to the south of Newfoundland. When conditions are favourable R. St. Pierre will cause a heterodyne on Lille 1376kHz before the latter closes down for the night at 2300hrs.

Harold Emblem, of Mirfield, Yorkshire, has received a verification from the new station at Kinshasha (692kHz). This is a difficult country to verify and the address for reception reports is Chef des Services Techniques, Radiodiffusion Nationale Congolaise, Kinshasha, Republique Democratique du Congo.

Reception of Far Eastern medium wave stations is possible in the U.K. during the afternoon in winter time. Stations fade-in about one hour before sunset and are audible either until they sign-off or they become submerged in interference from Europeans, which increases as darkness approaches. The 1,000kW All India Radio outlet at Calcutta on 1130kHz which broadcasts in English from 1530 until 1600hrs was heard frequently last winter. It is easy to pass over this station as it suffers from slow cyclic fading, so it is worth while pausing on the frequency for a few minutes. The Voice of America, Okinawa 1178kHz is another megawatter that is often heard in this country, usually as a background to the Swedish broadcaster on the same channel. Programmes from Okinawa are in local languages but identification is on the hour and half hour usually in English and is accompanied by the Yankee Doodle signature tune. Sign-off is at 1700hrs. Peking has been logged on 1,000kHz, 1230kHz and 1290kHz; Taiwan (Formosa) has been heard on 750kHz and 1200kHz with programmes of westernised Chinese music while Kabul, Afghanistan 1280kHz is a regular until close down at 1830hrs.

Reports to 132 Segars Lane, Southport PR8 3JG.

URING the past few months I have received many letters asking the correct way of converting metres into kilohertz. It would appear that many readers have receivers which are calibrated in metres only.

DX LISTENERS

The conversion is performed as follows: In order to obtain the frequency in kHz divide 300,000 by the wavelength in metres. This formula also works in reverse, that is: wavelength in metres can be obtained by dividing 300,000 by the frequency in kHz.

The first report this month comes from Paul Benton of Hednesford who has an Astrad-Nova receiver. Paul's aerial system consists of a 75 foot long-wire, a 14-element television aerial and a copper grid. Items from his log include:

4783 Radio Mali, in French at 2145.

NEWS FOR

4800 Radio Lara, Venezuela, music at 2330.

4900 R. Juventud. Venezuela, music at 0000.

4900 R. Conakry, Guinea, news in French at 2300.

4940 R. Abidjan, Ivory Coast, French at 2250.

5015 Windward Islands B.S., English at 2345.

5035 R. Bangui, Cent. Afr. Rep., English at 2045.

5047 R. Lome, Togo, African music at 2100.

11652 R. Pakistan, Karachi in English at 2030.

11815 HCJB, Quito, Ecuador in English at 0040.

11855 Saudi Arabia in English at 0430.

Stephen John Mathews of Hull has a new receiver, the Trio 9R-59DS, but having broken his leg playing football he has to be content with his 90 foot loft aerial instead of the new one which he was going to erect. The combination yielded some interesting stations including:

2326 S. African B.C. in English at 0030.

4777 R.T. Gabonaise in French at 0000.

4800 R. Lara, Venezuela in Spanish at 0400.

4880 R. Universo, Venezuela, Spanish at 0045.

4955 R. Nacional, Colombia in Spanish at 0315.

5960 Voz de Angola in Portuguese at 2015.

15170 ELWA, Liberia in French at 2020.

15200 NBC, Lagos, Nigeria, English at 1830.

15280 4VEH, Haiti in English from 2330 to 0200.

15415 FEBA, Seychelles, testing at 1855.

15485 R. Portugal Libre, clandestine at 1922.

Peter Reed of Brighton has used his R1155N receiver in conjunction with his Joystick antenna to log some interesting stations which include:

3380 Malawi B.C. in English at 2000.

4805 Voice of Kenya, Nairobi, 1800-1845.

4875 R. La Cruz del Sur, Bolivia, Spanish at 1100.

5040 R. Burma noted at 1445.

9520 R. La Cronica, Peru, Eng. and Sp. at 1200.

11825 Papeete, Tahiti in French at 0755.

21685 Kuwait B.S. in Arabic at 1300-1330.

Ross Pullen of Crawley has sent in a log which includes the following interesting stations: 5970 R. El Sol, Peru in Spanish at 0200.

9670 Saudi Arabia in Arabic at 2215.

THE BROADCAST BANDS

Malcolm Connah

Frequencies in kHz Times in GMT

9725 R. Burma in English at 0700.

11715 R. Republik Indonesia in English at 0900.

11875 R. dif. Nacional, Nicaragua at 0200.

Julian V. Moss of Rayleigh, Essex has just purchased a Meridian receiver and a 50 foot long-wire enabling him to hear:

6050 HCJB, Quito, Ecuador in German at 0615.

6080 R. Berlin Int. in French at 2100.

7280 R. Berlin Int. in English at 2045.

9530 AIR, Delhi in English at 2100.

9550 R. Warsaw, Poland in English at 2030.

9700 R. Sofia, Bulgaria in English at 1935.

9765 Deutschewelle in English at 2150.

11620 AIR, Delhi in English at 2030. 11672 R. Pakistan, news in English at 1900.

11700 R. Kiev, Ukraine in English at 1945.

11740 R. Australia in English at 1610.

11755 Finnish B.C. in English at 1000.

11765 R. Australia in English at 0800.

11800 RAI, Rome in English at 1940. 11910 Radio Budapest in German at 2010.

Fred Wall of Walthamstow, London E.17 used his homebrew 4-valve superhet and a 20 foot long-wire aerial to hear the following stations:

7290 TWR, Monte Carlo at 1600.

9555 Finnish B.C. at 1815.

9620 R. Belgrade, Yugoslavia, English at 1942.

11745 HCJB, Quito, Ecuador at 0015.

11765 R. Australia with news at 0900.

11790 R. Afghanistan, news in English at 1800.

15345 Kuwait B.S. with news at 1830.

17820 RSA, S. Africa with news at 1845.

21640 NHK, Japan with music at 1518.

25900 R. Norway in Eng./Nor. at 1820.

Robert C. Hanstock of Sheffield has a Colombia 5-valve superhet and a 50 foot long-wire which enabled him to hear:

5980 RSA, S. Africa in English at 1815.

7205 R. Australia in English at 1600.

9010 R. Peking in English at 2045.

9740 Radio Portugal in French at 0700.

Robert also reports that Radio Nederland is to open a new relay station at Tananarive, Malagasy in November, Programmes will be beamed to Africa and S. Asia. The station will also be changing the frequencies of its evening transmission in English to Europe; the new frequencies being 17830, 6085 and 6020 from 1830 to 1950.

D. A. Hairon of St. Clement, Jersey is now using a 100 foot long-wire with his other equipment and reports hearing:

9740 R. Cairo in English, 2245-2300.

11730 R. Nederland, Bonaire in Eng. at 0630.

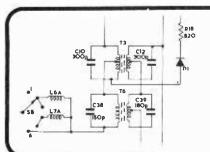
11795 R. Nacional, Rio de Janeiro at 0055.

11865 R. Clube, Brazil at 0200.

21705 R. Mexico in Spanish at 2205.

Reports should arrive by the 15th of the month and be addressed to me at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex.

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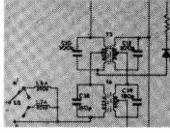


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- - · Electronic switch · Simple transmitter
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 - · d.c. experiments
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Peter Short (ZS2HT). He remarks on comments made in an earlier Amateur Bands regarding ZS1MH. Peter says that the latter station has managed over 1,000 contacts on 3.5MHz notching up 115 countries. Gear is a KW Atlanta and a G8KW antenna at 175ft. Apparently ZS1MH will be using a 66ft. loaded vertical early next year and has plans to have a 2-element beam for 3.5MHz up by next March. Peter says also that there is intense ZS activity on both 3.5 and 7MHz between 0400 and 0600 g.m.t. Listen 7090 to 7100kHz and from 3730kHz upwards.

A shout from **Des Walsh** (EI5CD) of Co. Tipperary. He asks for s.w.l's who can QRX on 2 metres to listen out for his a.m./f.m. sigs on the following freqs.: 144·7, 144·9, 145·35 and 145·96. Des runs 8W output to a 6-over-6 and is on most weekends beaming eastwards.

The aerial is 67ft. wrapped neatly around a first floor flat in Cambridge. The receiver is a "modded" HRO-MX and the log from M. Wallace is for 3.5MHz s.s.b.; HA0KHT, WA8OBG, ZB2CC, ZL3LE, ZL4JW.

Listen after 0100 b.s.t. around 7·2MHz for KP4GL who m.c's the Caribbean net, advises **Paul Edwards** (Penge). Paul's antenna is 120ft. "bent round the garden" and the Rx is a homebrew 1-V-1. Log for 7MHz reads; CN8HD, CT1GQ, CT2AK, EA7EU, FM7WN, K4UAS, KP4DHD, KP4GL, KZ5JF, PJ2CW, PY3APH, PY7BIH, VP7DL, W1YNQ, W2RGV, W3LTU, WA2BVU/4X, YV1BI, YV5BPG, ZL2BT, 4Z4JT, 8P6AJ.

John Brockett (Hemel Hempstead) has a homebrew transistor superhet which is working on 160 and 80 metres. Best on 160 to date is GM3SVK/A in the Shetlands. On 80, John bagged many EUs plus JY9DX, OD5BA, VE1OW, VO1FG, 3V8ZK and 5H3LV.

Peter West (Leigh, Lancs), reckons midnight to 0700 for 7MHz DX. Proof of the pudding comes from Peter's log for that band gained with the aid of a TCS-9 receiver and 132ft. end-fed (all s.s.b.); CM3LN, EA3LP, EA6BH, K4ELK, K4PTK, PY2ASY, PY7AJB, PZ1CV, W1EEF, W2BMK, W3WGH, W4CVS, YV4BE.

Talk about DX logs, I gotta DX letter. Epistle from Karl Muller of Mbabane, Swaziland, uses a Philips domestic portable and the oscillating detector of a homebrew t.r.f. as a b.f.o. Karl stalks 40 metres with this little lot and reports squeaks of activity from: CR7FM, CR7BN, DK2EQ, DJ9JF, E18H, ET3ZU/A, G8NV (that's DX to Karl!), GM3JDR, HA3GR, HB9AGN, IT9FG, JA0BCO, JA1BK, JA2BUX, JA3LU, JA4IWD, JA5BLH/MM, JA6FT, JA7DCK, JA9YBA, JH1EDB, JW1EE, K4THA, K6DC, K6DV, KH6RS, LZ1KVV, OK2BM, OH5UQ, SM5EXE, thousands of "U" stations.

David Lawley (Gravesend) CR100, a wide variety of antennas, has been doing a spot of all-band listening. Topband log includes; GI3ZIA, GM3WDF and GW3UMB. Up to 3.5MHz and a QRX revealed; CT1BT, EI3S, GC3MDX, OY7JD, PY7AF, VO1FX,

THE AMATEUR BANDS David Gibson, G3JDG

Frequencies in kHz • Times in GMT

VO1FG and YK1AA. On 40 metres, David's best were; OZ9HG (Langeland Island) and TI2IT.

Without doubt the award for the best kept log of the year goes to Adrian Barnes of Abingdon, Berks. This was laid out neatly and ledgibly in columns making it easy to read. All the information was included; callsign, mode, frequency, date, time, country etc. No local stations were listed, no Eu stations either, just some 175 DX stations. A sample from this superb 14MHz s.s.b. log reads; AP2AD, CE3FM, CN8BB, CP1BG, CR5SP, CT1BT, EL2BA, EP2JA, ET3ZU, HC1M, HI1AGS, JY9DK, KH6CD, KP4FS, KZ5JW, LU2AGE, OA1BU, OA6BGI, PJ0PM, PY2FIQ, T12FKB, VA2UN (special station in Montreal), fourteen VEs, VK1BT, VK2APK, VK3BCM, VK4CZ, VK4PV/P, VK5GX, VK6OV, VK7RX, VK9CD, seventy Ws, XE1IIJ, YB5BFK, YN2OM, YV1ACI/P5, YV4YC, YV5CKR, YV6EE, ZA2BE, ZB2A, ZC4LC, ZE1CW, ZL2BGV, ZL3GO, ZL4AW, 3A0FX, 3V8ZK, 4X4JL, 4Z4DZ, 5Z4LW, 6Y5GA, 7X2BK, 9H1BG, 9M2LP, 9Q5RN, 9V1QJ, 9Y4CP.

Irwin Brown (Co. Antrim), has a JR-310 and a dipole at 30ft. Log of s.s.b. from 14MHz which was heard in the Emerald Isle includes; AP5HQ, EA6BM/M, ET3ZU/A, HI8LA, VE1CW/M, VQ9YL, YA2DD, YB3AAY, ZK1CD, ZM7AG, 5K5LR, 5Z5KL.

Philip Cross (Preston) has an HRO-MX and a dipole cut for 14MHz. Log of s.s.b. reads; CN8GC, CR5SP, CR6IC, ET3ZU/A, FP9AR/M, HP9ARZ, HV3SJ, JA6YUV, JX1AK, JY1, LU2ECO, M1B, MP4TDM, OD5GC, PZ1DR, VQ9XX, VP9BN, ZE1CY, ZS3KC, 3A2CP, 3V8ZK, 7X2BK, 7Z3AB, 9K2BG, 9J2ED, 9X5AA, 9Y4VV.

"I'm now working hard trying to learn c.w," says Alan Smith (Nelson). "Good lad," says David Gibson (Harpenden). Alan uses a Koyo KTR 1662 receiver and 25ft. of wire. Not an elaborate set up, but enough to hear some 14MHz s.s.b. from; EA6BU, HC1KH, HK3BN, KZ5IK, KP4BJD, PJ9AD, PZ1AY, VE3CNE, YB5FB, YV5AXT, 6Y5SR, 9Y4VV.

An ECC83 and ECL82 (leaky grid detector and a.f. amp), is the homebrew receiver of **John Runchman** (South Norwood). On 20 metres, with the aid of a dipole, John bagged; HK3UY, sixteen Ks, LU4ECO, PY2CAQ, VE1IJ, VP2LY, thirty Ws, YN1ABD, YV4UA, ZP5AN, ZL3AA, 4X4AE, 4Z4QAM, 6Y5GA, 9H1M, which is pretty good going for two valves.

P. Harris (Surbiton) RA-1, dipole, got these on 28MHz; LU3DTV, LU6DRB, PY2HT.

Goings on for contest-types at this time of the year includes: November 6-7, 144/432MHz c.w. contest; 6-7, 40 metre phone contest; 6-8, CHC/FHC phone/c.w. contest; 13-14, topband contest; 14, OK contest; 27-28, CQ WW d.x. c.w. contest. December 5, 2 metre contest.

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	·80p	EF86	31p	PCF200	77;
E180CC	42p	EF89	26p	PCF201	771
E181CC	90p	EF91	15p	PCF801	485
E182CC		EF92	37p	PCF802	481
	1.05	EF95	30p	PCF805	72;
EABC80	32p	EF183	32p	PCF806	65p
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EB91	15p	EFL20		PCH200	701
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EBF80	42p	EL84	23p	PCL84	421
EBF83	42p	FL85	40p	PCL85	42p
EBF89	30p	EL86	40p	PCL86	42p
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ECC85	40p	EM80	40p	PL83	42
FCC86	50p	EM84	35p	PL84	351
ECC88	37p	EM87	55p	PL500	731
ECC189	52p		40p	PL504	75;
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77p	OAZ200	55
77p	OAZ201	50
77 p	OAZ202	to
18p	OAZ206	42
18p 72p	OAZ207	47
/2p	OAZ208	to
35p	OAZ213	
2р	OAZ223	to
0p	OAZ225	
17р	OC16	50
7p	OC22	50
35p.	0022	

OA5	20p	OC35	50p	IN21B		40362		AF127	17p	CRS1/30
01AC	25 p	OC38	42p	IN25	60p	82303	50p	AF139	30p	CRS1/35
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Electronic Vandals

As an amateur archaeologist and also as a reader of your journal for nearly 20 years, I would like to applaud your editorial on "Electronic Vandals."

We as archaeologists do not want to deprive folk of their pleasures, but in return we ask that they in turn do not deprive us of vital information.

A coin or a metal brooch, so badly corroded as to be almost worthless as a coin may, in expert hands of conservationists at museums, tell us the date when Roman forces were active in a fort or when a Roman villa was last occupied.

We may have worked for many years patiently working out the size, shape and function of a structure; but if our dating evidence has been removed all our work becomes fruitless.

If some of your readers honestly wish to help in furthering human knowledge then I suggest they contact their local archaeological society through their museum. It may be that they would be grateful for their help. Please remember that archaeology is a study of people and not a treasure hunt.

—J. L. Cole, (Sutton Coldfield).

Beginners' Licence

Although there are many Amateurs, who have worked hard to acquire their radio licence, and are now fully fledged Amateurs, I fail to see why the G.P.O. have, as yet, not introduced a "beginners'" licence. Such a licence could not fail to please all, as it would undoubtedly benefit the amateur radio movement, would encourage enthusiastic people to join, and would not clash with the activities of the fully licensed Amateur.

I feel that a "beginners" licence is necessary as there are lots of potential Amateurs, who either don't have the facilities or don't have the time. I am sixteen years old, a keen SWL, but am in the middle of my 'O' Levels, and I will be continuing my studies for the next two years, and have therefore no time with which to study for the R.A.E. I am sure that there are many others, who

are in a similar position. A limited licence would sow a good grounding and this would enable one to acquire a licence at a later date.

Such a licence could be based on the following terms, and conditions:

- A written exam comprising:

 (a) Section one of the present exam;
 - (b) Frequency control and measurement;
 - (c) Interference, the causes and suppression of it;
 - (d) Full operating procedure (this should relieve many qualified "Hams");
- (2) The G.P.O. morse test;
- (3) (a) Only able to use a small allotted section of the band;
 - (b) Limited to two watts power output;
 - (c) C.W. transmission only; (d) The allocation of a "beginners" prefix.

These conditions would, by their very nature, urge the willing and genuine Amateur on to the full licence while the lazy, and unenthusiastic would fall by the wayside.—M. S. Lerner, (Hendon, London).

Take-20 Dollars

Recently I started to construct one of the "Take 20" projects and I was horrified at some of the local prices for parts. These prices may be of interest to you: $5\mu F$ 12V capacitor, 20 cents; $1\cdot 5M\Omega$ $^{1}_{4}W$ resistor 10 cents; BC109 transistor, \$1\cdot85c; BC169C transistor \$2\cdot25c. Ten New Zealand cents is equal to 5p.

It is actually cheaper to have these parts air-freighted from Britain than to buy them from the local shop.—K. B. Moore (Tokoroa, New Zealand).

A Protest

Radio components are clearly inferior to the previous designed ones, when silk covered windings of transformers were impregnated with quality varnish. Modern methods use enamelled wire impregnated with wax resulting in what I think is an inferior com-

ponent which cannot be relied upon.

Oil insulated windings are inferior, especially when mains voltages are used in primary windings of transformers. Enamelled wires are clearly inferior and unreliable. More so when wax impregnated.

We are progressing in the wrong direction. When will the proven system return, so that quality returns? I refer to transformers only but other components are quite often just as bad.—R. Wibberley, Nottingham.

Such a D.I.N.

I would like to say a few words, aimed at manufacturers and suppliers: Now that "D.I.N." connectors are becoming more popular and standard on most equipment nowadays, how about making 5-core cables readily available, and 4-core individually screened cables at least available, if not readily available?—R. Williams (St. Albans, Herts)

Treasure Traced

We have been using a metal locator manufactured by a well-known company for some time now and recently our Town Hall called upon us to help search for a very expensive diamond and sapphire ring which had been lost on the beach.

We tried a manufactured metal locator which proved useless near salt. When we used the P.W. Treasure Tracer, we found the ring after one hour. The P.W. locator was not affected by water at all and the ring was in salt water when located.

This was the first time we had put the P.W. Treasure Tracer to work and since the ring we located was worth about £200 it proves how good it is. Needless to say, the lady to whom the ring belonged is very grateful and I hope other readers will have as much success.

The cost to build the Treasure Tracer is so low for such performance that the P.W. circuitry gives.

I must add that we also found about a dozen coins before finding the ring.—R. Miller (Brightlingsea, Essex).

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PART 7 G. J. KING

GORDON KING CONTINUES THE SERIES DISCUSSING TUNER-AMPLIFIERS AND THEIR PROBLEMS, PICKUPS AND THEIR ASSOCIATED CORRECTION NETWORKS AND ENDS WITH A BRIEF RESUME OF $H\cite{t}$ -Fi amplifier specifications.

want to begin this month with the hi-fi type of radio receiver, called the tuner-amplifier. This is an integration of a stereo (two channel) amplifier and a radio receiver always tuning the f.m. band (Band II) and sometimes a.m. bands as well, and invariably embodying a stereo decoder. This type of equipment is ousting the ordinary radiogram in certain areas of application, for, coupled to a pair of good speaker systems and a record playing unit the tuner-amplifier constitutes the 'heart' of a music system of significantly greater quality potential than the average radiogram.

Real hi-fi radio reproduction is not possible from the a.m. bands owing to the necessary restriction of the i.f. passband to avoid interference between adjacent stations. Sadly, even such passband restriction is unable to keep unwanted stations from the wanted in the medium waveband after dark, and as a consequence we get an annoying background of whistles and monkey chatter. Moreover, the passband restriction deletes the higher-order sidebands of the modulated signal and hence impairs the treble output.

With f.m. things are not like this because in Band II each channel is allotted 200 kHz of 'elbow room', thereby permitting full expansion of all the sidebands without restriction.

The f.m. system has attractive attributes over and above the a.m. system, including enhanced signal-to-noise performance, the ability to reject a.m. signals and interference and a parameter known as the 'capture ratio'.

The capture ratio stems from the nature of f.m. demodulation and from the amplitude limiting engineered into the i.f. channel of the receiver. It means that when two signals are present in the same channel (or close together in the receiver's passband) the weaker one is almost completely rejected and only the stronger of the two gives an output, free from interference.

A capture ratio of two or three decibels ensures that a co-channel signal is muted when the wanted signal is only about 10dB above it. Nothing like this degree of rejection is possible on a.m. All this boils down to the fact that the f.m. radio system is truly hi-fi, and that a.m. cannot be regarded in this light at all.

DEVELOPMENTS

Contemporary radio tuners and the tuner sections of tuner-amplifiers are fast taking in the latest devices, including field effect transistors (f.e.t's.), integrated circuits (i.c's.), crystal and ceramic i.f. filters supplementing the bandpass transformer couplings. F.e.t's. are used mostly in the front-end as the r.f. amplifier and, sometimes, the mixer (with a bipolar local oscillator). Since their transfer characteristics exhibit second-order components they yield fewer third-order intermodulation components at high signal level than bipolar counterparts, whose characteristics contain an abundance of third-order components.

This means that unwanted spurious signals are minimised, particularly at locations close to a powerful station group. They also provide other attributes, including relatively low noise working and good 'mixing' properties. Thus a tuner section (f.m.) containing an f.e.t. r.f. amplifier and an f.e.t. mixer is likely to out-perform an 'equivalent' incorporating bipolar devices in these stages under a wide range of operating conditions.

THIRD ORDER INTERMODULATION

One problem with simple f.m. front-ends is third-order intermodulation when operated in a strong, locally derived signal field. One symptom of this is a spurious signal at Radio 3 frequency (from $f_2+f_4-f_3$, where f_2 , f_3 and f_4 are the frequencies of Radios 2, 3 and 4 respectively). This can result in 'burbles' and similar sort of interference on Radio 3, and possibly 'birdies' inteference when Radio 3 is stereo encoded.

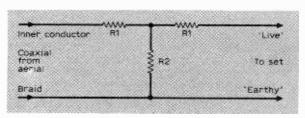


Fig. 1: Simple attenuator for reducing intermodulation problems.

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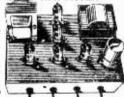
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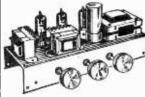
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0	EH90	.36		.63	PL82 .80	UCL83	.48	AC128	. 20	BF159	.25	OC24	.38
8	EL32	.18		.50	PL83 .32	UF41	.50	ACI54	.25	BF163	.20	OC25	. 38
₽∣	EL34	.44	MHLD6	. 75	PL84 .30	UF42	. 60	AC156	.20	BF173	.88	OC26	.24
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3	EL37	.74	N 339	.44	PL505 1.80	UF86		ACI68	. 38	BF185	.40	OC35	. 32
5١	EL42	. 53		. 44	PL50M .90		.27		.55	BF194	.15	OC36	. 43
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	EM80	. 38		. 26	PY81 .24	T12/14	.38	ACY28		BY127	.18	0C72	.11
31		. 89	PCC88	.41	PY82 .24	U18/20	.75		.18	BYZIO	.25		.23
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Ы	EZ40	.40		. 57	R10 .75	U403	. 33	AF124	. 25		. 20	OC84	. 24
)	EZ41	.42		. 68	R11 .98	U404	. 38	AF126	.18	(1ET573		OC123	. 23
3 Ì	EZSO	.21		. 62	R16 1.75	11801	. 98	AF139	. 65	GET387	.48	OC139	. 23
) [EZ81	.22	PCL83 .	. 32	R17 .88	U4020	. 38	AF178	. 68	GET873	.15	OC140	. 95
7	EZ90	. 20		.58	R19 .80	VP23	. 40	AF180	. 48	GET887	. 28	OC169	. 23
	FW4/500			. 34	8P42 .75	VP41	.38	AF186	. 55	GET897	. 23	OC172	. 35
И	FW4/800		PCL805/8		RP61 .33	VT61A	.35	AF239	. 38	GET898	. 28	OC200	. 22
	(4Z30	.34		. 40	TH4B .50		.44	BA102	. 45	MI	.15	OC201	.38
	GZ32	.41		.38	TH233 .98	VU120	. 60	BATIS	.14	MS	.15	OC202	. 43
	GZ33	.70		. 65	TP2620 .98	VU1202		BA116	. 25	OAS	. 28	OC203	.80
	GZ34	.48	PD500 1.	44	UABC80.30	VU133	. 35	BA129	.13	OA9	. 13	OC204	.80
	GZ37	.67	PEN4DD		UAF42 .49		.34	BA130	.10	OA10	. 43	OC205	. 48
51	HABC80			. 38	UBC41 .45	W107	. 50	BA153	.15	OA47	.10	ORP12	.58
3	HL23DD	.40	PEN36C	.75	UBCst .40	W729		BC107		OA70	.15	i	
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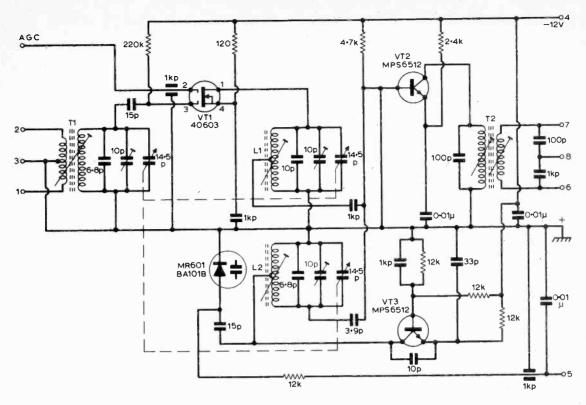


Fig. 2: Circuit of the "front-end" of a typical British tuner-amplifier.

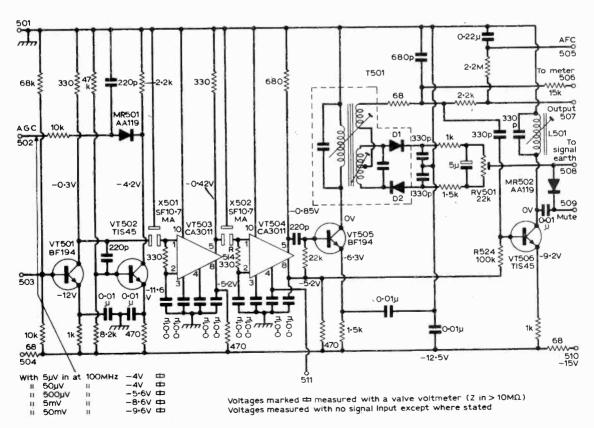


Fig. 3: The f.m. i.f. channel of the tuner-amplifier shown above.

One solution lies in attenuating the signal from the aerial to the set. Belling Lee make plug-in attenuators over a range of values; alternatively a simple resistive pad can be made up as shown in Fig. 1.

FM FRONT-END

The f.m. front-end of a typical British tuneramplifier is shown in Fig. 2. Here VT1 is a dual-gate f.e.t. with the input signal applied to one gate and an a.g.c. potential to the other. The mixer is bipolar VT2 and the local oscillator bipolar VT3.

Aerial coupling is by T1 primary, and since this is centre-tapped 300 ohms balanced feeder can be connected across terminals 1-2 or 75 ohms coaxial (unbalanced) across 2-3. Not all input circuits permit this dual mode of feeder connection, and if the design is essentially for 300 ohms balanced (or 240 ohms European DIN) the best coupling from coaxial is obtained through a 'balun' transformer.

A.f.c. is applied to the local oscillator from a varactor diode (MR601), and this receives its control bias from the f.m. detector. The varactor is in parallel with the oscillator tuned circuit, so the frequency of this is altered by the control bias which appears in appropriate polarity from the f.m. detector when the tuned carrier is displaced from the centre of the i.f. passband.

The i.f. signal is developed across T2, and is coupled to the f.m. i.f. channel from the capacitance tap on circuit No. 8.

FM IF CHANNEL

The f.m. i.f. channel is shown in Fig. 3, and the input goes to circuit No. 503 and thence to the base of VT501.

The channel includes two ceramic filters of the kind already mentioned (X501/X502) and a couple of i.c's. (VT503/VT504). The ceramic filters take the place of the usual i.f. transformers and because they exhibit steeply rising and falling response sides extremely good i.f. selectivity is secured. The only alignment required is of the ratio detector transformer T501.

The i.f. signal at VT501 collector is fed to the first filter and from this to the first i.c. The second filter couples the two i.c's., while VT505 bipolar transistor drives the ratio detector, composed of diodes D1/D2, etc. This circuit is balanced, and preset RV501 allows this to be optimised, one mode for adjustment being for the least response to an a.m. signal.

It will be noticed that the ratio detector yields potential for the tuning meter as well as for the varactor diode on circuits 506 and 505 respectively. Demodulated audio (or multiplex signal in the case of stereo) from circuit 507 is coupled to the stereo decoder.

VT506 is concerned with the muting, etc., while VT502 amplifies i.f. signal at VT501 collector and passes it to the rectifier MR501. The resulting filtered d.c. constitutes the a.g.c. potential for the f.e.t. r.f. amplifier (Fig. 2).

FAULT FINDING

Fault finding in a circuit of this kind is best carried out by feeding a modulated 10·7MHz (or a signal at the i.f.) into the strip, starting at the final transistor (VT505 in this case), then working forward until the point of inactivity is located.

To find the actual component which is in trouble, after locating the faulty area or stage, might well require the testing of voltages, etc. at the electrodes of the various devices, and to help in this respect the voltage references in Fig. 3 have been retained.

Servicing of f.m. front-ends is not recommended —apart, possibly, from the replacement of transistors —and trouble in this area is best left to the maker or distributor to clear. This applies to professional service organisations as well as to the amateur repairer.

A word about the replacement of f.e.t's. would not be amiss. The insulated gate types in particular are vulnerable to static discharges, and when making a replacement always retain the shorting clip (fitted by the maker) until the device has been completely soldered into the circuit.

From the testing, adjusting and servicing aspects, the BBC's stereo test sequence at the close-down of Radio 3 can be of a great help in determining such parameters as stereo separation (e.g., degree of crosstalk), signal-to-noise, frequency response, etc.

SOURCE INPUTS

When a radio tuner is used with a hi-fi amplifier a 'flat' response is required since the de-emphasis is performed in the tuner. Inputs with 'flat' responses thus include radio, high-level tape replay and auxiliary. If an amplifier is equipped with an input for the signal direct from a tape head, then equalisation will be included to cater for the replay response. The only equalising then required is that pertaining to the gramophone pickup, and a good starting point is the pickup (cartridge) itself.

PICKUPS

There are two versions. One the magnetic which works rather like a generator, and the piezo, using either a natural crystal or processed ceramic, which works on the transducer principle.

When a gramophone record is made the modulation is imparted to the groove from a cutting head via a special electrical filter having a specific

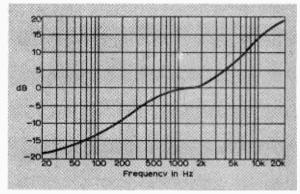


Fig. 4: Graph showing the standard RIAA recording characteristic

recording characteristic. The bass end of the spectrum is attenuated and the treble end is boosted. On replay, therefore, the bass needs to be boosted and the treble attenuated to secure a 'flat' audio output.

The standard recording characteristic is given in Fig. 4. This has an 'average' slope of about 4dB/

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7in.	1,200ft.	62 i p	7in.	1,800ft.	921p
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	7478	Dual J-K filp flop	40p	87p .	85p	38p	30p
	7474	Dual J-K filp flop Dual D flip flop Quadruple bistable latch	40p	87p	85p	83p	80p
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octave, but the RIAA equalising, as it is called, is very carefully engineered into the magnetic pickup input circuits of hi-fi amplifiers and good quality radiograms, etc., so that the response is exactly the reciprocal of that shown in Fig. 4. The net result is that a 'flat' output from the preamplifier which, of course, is the signal requirement of the control section and power amplifiers.

Now, it is the **velocity** of the imparted modulation which follows Fig. 4 curve, and because magnetic pickups yield an output proportional to the velocity of stylus deflection the output from the pickup applied to the equalised preamplifier is thus after the style of that in Fig. 4. Hence the reciprocal equalisation

just referred to.

A piezo pickup, on the other hand, produces an output which is proportional to the amplitude of stylus deflection (not velocity). This implies that a piezo pickup playing a record cut to the standard RIAA response produces an almost 'flat' output without equalisation.

All piezo cartridges need to be loaded into a very high resistance of not less than $1M\Omega$ and for the best results and to secure full advantage of the inbuilt equalisation and thus obtain a 'flat' output from a

disc recorded to the RIAA standard.

A magnetic cartridge (whose source is inductive), however, is commonly designed to work best into a load of round $50k\Omega$. If it is loaded lower the treble tends to fall, while too high a loading can lift the treble end of the spectrum and incite undue 'ringing'. Conversely, a piezo cartridge (because its source is capacitive) exhibits falling bass and rising treble when loaded into a resistance significantly below $1M\Omega$ or so.

The signal yield from a piezo cartridge, even when loaded low, is significantly in excess of that from a magnetic cartridge when playing modulation of a given velocity. This means, therefore, that the piezo signal might well have to be attenuated before being fed to the magnetic input, to avoid preamplifier overload.

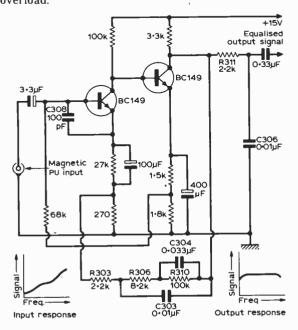


Fig. 5: Circuit of a pre-amplifier incorporating RIAA equalisation.

The peaks of signal can be clipped when the pickup signal veers towards the overload level. However, when an 'equalising' pad is included a degree of attenuation is automatic, so additional attenuation may not be necessary.

RIAA EQUALISED PREAMPLIFIER

Shown in Fig. 5 is the circuit of a fairly conventional RIAA equalised preamplifier. It is common to employ two transistors, at least, and in the circuit shown, R306/R310/C303/C304 network provides the frequency selective network, giving the necessary response characteristic inversely to correspond with the recording characteristic (Fig. 4). The overall effect is that the feedback increases with rising frequency and decreases with reducing frequency, thereby giving the required treble cut and bass boost.

R303 provides a 'flat' control of gain, and in some amplifiers the frequency selective network is switched out of circuit when the programme input signal requires a 'flat' response, a resistor such as R303 then being used to provide the appropriate input sensitivity voltage. Stereo equipment embodies two such preamplifiers, one for each channel.

The RC network C306/R311 provides a low-pass characteristic, preventing the response from extending too far above the audio spectrum. The 100pF capacitor (C308) connected directly across the base/emitter electrodes of the input transistor cuts the input response to radio frequencies and thus prevents the breakthrough of radio and television interference during low-level record replay.

RADIO/TV BREAKTHROUGH

Not all amplifiers are equipped with radio and TV filtering like this, and since the response of transistor stages can embrace the radio and TV spectrums, a symptom becoming increasingly common is, in fact, radio and TV breakthrough. This mostly happens when the equipment is switched to magnetic pickup and when it is operated relatively close to a powerful radio or TV station. It is encouraged by (i) the high sensitivity of the amplifier under this mode of operation and (ii) the relative ease at which the RIAA preamplifier can be pushed into non-linearity.

A filter which nearly always clears the trouble is given in Fig. 6. The circuit to the base should be broken and the $2.2k\Omega$ resistor inserted in series.

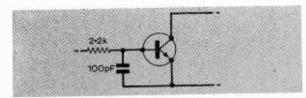


Fig. 6: A simple filter to prevent radio and TV signals interfering with audio amplifiers.

while the 100pF capacitor should be connected right across the base/emitter electrodes, as close as possible to the input transistor. Both channels should be so treated.

The RIAA preamplifier signals can get into trouble so if one channel of a stereo amplifier appears to be lacking in bass, with excessive treble output, when operating from a magnetic cartridge, then attention should be given to the preamplifier department of the affected channel. Excessive noise on the magnetic

input is commonly caused by a defective preamplifier transistor or a 'noisy' collector resistor.

HI-FI SPECS

It is impossible to detail all the specifications relating to hi-fi equipment (further information on this score is given in "Tuners and Amplifiers" by John Earl, published by Fountain Press), but comment on a few of the more important ones would not be amiss.

Power Capacity. This is the maximum power that an audio section is capable of delivering with both channels running, the maximum being defined either to the level of sinewave clipping or to a specified value of distortion when the output is loaded by pure resistance of appropriate value in place of the speaker. The 'standard frequency' is IkHz, but to obtain the power bandwidth the measurement is repeated at low and high frequencies.

Standard Output Power. This is 50mW (17dB/mW). However, in some instances values of 500mW (27dB/mW) and 5mW (7dB/mW) might be used, but the power to which any parameter (such as sensitivity) refers should be stated in the specification.

Input Sensitivity Voltage. This is the input signal at 1kHz required to yield the rated output power when the volume control is fully advanced, all filters 'out' and tone controls 'flat'.

Signal/Noise Ratio. This refers to the voltage due to components of hum and noise across the output load in terms of dB ratio to the rated output power and within the full noise bandwidth of the equipment. The volume control is generally fully advanced and the selected source input is either short-circuit or open-circuit (the former preferred since it avoids the pickup of spurious hum and noise components).

A ratio of 60dB, for example, implies that the **power** of the summed hum and noise in the output load is one million times below the full power of the amplifier.

Total Harmonic Distortion (THD). This is commonly measured through a distortion factor meter, in which a very sharply tuned filter 'notches out' the fundamental frequency, leaving only the harmonic components.

Intermodulation Distortion (IMD). Like THD, IMD is a function of amplifier non-linearity. This is commonly measured in terms of the amplitude of intermodulation components resulting from the introduction of two signals to the amplifier, so as to produce sum and difference frequencies.

S/N Ratio (FM). This refers to hum and noise relative to a stated modulation level (100% or 30%). Measurement is similar to that of S/N ratio of an amplifier, and the usable sensitivity of an f.m. tuner is commonly given as the input required for a S/N ratio of 45dB.

Owing to the wider passband involved and the action of decoding, a stereo receiver has a S/N performance below that on mono, particularly at the lower signal input levels, which is the reason why stereo receivers should always be operated with the best possible f.m. aerial system, consistent with the location and prevailing signal field on Radio 3.

END OF SERIES

NINE BAND RECEIVER—continued from page 690

AERIALS

The telescopic type aerial has a bracket, so that it can be bolted directly on the left hand side of the case, about lin. from the back. An insulated socket is fitted on the side of the case for an external aerial. Many transmissions can be received at ample volume with the telescopic aerial alone but an external aerial will greatly improve the reception of weak signals.

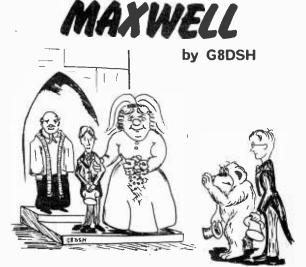


DIAL SCALE

Because each of the nine bands covers a relatively small frequency range, the main tuning scale is fitted with a card marked 0 to 50.

The bandswitch has nine positions, and the card scale under it has ten frequency markings. The bandswitch pointer comes to rest **between** these markings, which thus show the approximate frequency coverage of that particular range. For example, if the pointer rests between 4.6 and 5.0, the range is 4.6-5.0MHz, while if it is between 5.0 and 5.6 the range is 5.0-5.6MHz, covered with the normal tuning control.

The full markings are as follows: 3.6—3.8—4.3—4.6—5.0—5.6—6.3—7.4—10—15. This scale is best put under the perspex.



"—a bit of a mismatch somewhere!"



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Two years ago Sinclair Radionics announced the World's first monolithic integrated circuit Hi-Fi amplifier, the IC.10. Now we are delighted to be able to introduce its successor, the Super IC.12. This 22 transistor unit has all the virtues of the original IC.10 plus the following advantages:

- 1. Higher power.
- 2. Fewer external components.
- 3. Lower quiescent consumption.
- 4. Compatible with Project 60 modules.
- 5. Specially designed built-in heat sink. No other heat sink needed.
- 7. Works on any voltage from 6 to 28 volts without adjustment.

6. Full cutput into 3, 4, 5 or 8 ohms.

8. NEW 22 transistor circuit.

SINCLAIR GENERAL GUARANTEE

Should you not be completely satisfield with your purchase when you receive it from us, return the goods without delay and your money will be refunded in full, including cost of return postage, at once and without question. Full service facilities are, available to all Sinclair customers.

Output power 6 watts RMS continuous (12 watts peak).

Frequency Response 5 Hz to 100KHz ± 1 dB

Total Harmonic Distortion Less than 1%, (Typical 0.1%) at all output powers and all frequencies in the audio hand.

Load Impedance 3 to 15 ohms.

Power Gain 90dB (1,000,000,000 times) after feedback

Supply Voltage 6 to 28 volts (Sinclair PZ-5 or PZ-6 power supplies ideal).

Size 22 x 45 x 28 mm including pins and heat sink.

Input Impedance 250 Kohms nominal.

Quiescent current 8mA at 28 volts.

With the addition of only a very few external resistors and capacitors the Super IC.12 makes a complete high fidelity audio amplifier suitable for use with pick-up, F.M. tuner etc. Alternatively, for more elaborate systems, modules in the Project-60 range such as the Stereo 60 and A.F.U. may be added. The comprehensive manual supplied with each unit gives full circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include car radios, oscillators etc. The very low quiescent consumption makes the Super IC.12 ideal for battery operation.



Price, inc. FREE printed circuit board for mounting.

£2.98 Fost free

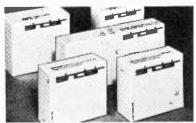
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Sinclair Project 60

The World's leading range of high fidelity modules







Project 605

The easy way to buy and build **Project 60**



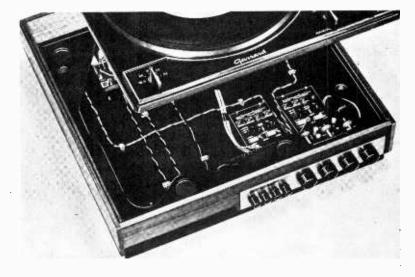
Project 605 is one pack containing: one PZ5, two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all incessary leads cut to length and fitted with neat little clips to plug straight on to the modules. Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting.

Complete Project 605 pack with comprehensive manual, post free £29.95

All you need for a superb 30 watt high fidelity stereo amplifier.

Sinclair Radionics Limited, London Road, St. Ives, Huntingdonshire PE17 4HJ, Tel: St. Ives (048 06) 4311





Project 60 offers more advantage to the constructor and user of high fidelity equipment than any other system in the world.

Performance characteristics are so good they hold their own with any other available system irrespective of price or size.

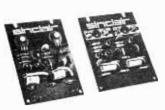
Project 60 modules are more versatile — using them you can have anything from a simple record player or car radio amplifier to a sophisticated and powerful stereo tuner-amplifier. Either power amplifier can be used in a wide variety of applications as well as high fidelity. The Stereo 60 pre-amplifier control unit may also be used with any other power amplifier system, as can the AFU filter unit. The stereo FM tuner operates on the unique phase lock loop principle to provide the best ever standards of sensitivity and audio quality. Project 60 modules are very easily connected together by following the 48 page manual supplied free with all Project 60 equipment. The modules are great space savers too and are sold individually boxed in distinctive white and black cartons. With all these wonderful advantages, there remains the most attractive of all — price. When you choose Project 60 you know you are going to get the best high fidelity in the world, yet thanks to Sinclair's vast manufacturing resources (the largest in Europe) prices are fantastically low and everything you buy is covered by the famous Sinclair guarantee of reliability and satisfaction.

Typical Project 60 applications

The Units to use	together with	Cost of Units
Z.30	Crystal P.U., 12V battery volume control	£4.48
Z.30, PZ.5	Crystal or ceramic P.U. volume control etc.	£9.45
2 x Z.30s, Stereo 60, PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£23.90
2 x Z.30s, Stereo 60, PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90
2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr	As above	£34.88
Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43
	Z.30, PZ.5 2 x Z.30s, Stereo 60, PZ.5 2 x Z.30s, Stereo 60, PZ.6 2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr Z.50, PZ.8, mains	Z.30 Crystal P.U., 12V battery volume control Z.30, PZ.5 Crystal or ceramic P.U. volume control etc. 2 x Z.30s, Stereo 60, PZ.6 P.U., F.M. Tuner, etc. 2 x Z.30s, Stereo 60, PZ.6 As above Z x Z.50s, Stereo 60 As above Z x Z.50s, Stereo 60 As above Z.50, PZ.8, mains Mic., guitar, speakers, etc

from a simple amplifier to a complete stereo tuner amplifier with Project 60 modules

Z.30 & Z.50 power amplifiers



The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well.

SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications). Power Outputs

Z.30 15 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M.S. into 3 ohms using 30 volts. Z.50 40 watts R.M.S. into 3 ohms using 40 volts: 30 watts R.M.S. into 8 ohms using 50 volts. Frequency response: 30 to 300.000Hz ±1dB. Distortion: 0.02% into 8 ohms. Signal to noise ratio: better than 70dB unweighted. Input sensitivity: 250mV into 100 Kohms For speakers from 3 to 15 ohms impedance Size: 14 x 80 x 57 mm.

Z.30 Built, tested and guaranteed with circuits and instruc-

tions manual

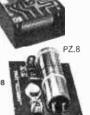
Built, tested and guaranteed with circuits and instruc-**F5 48**

f4 48

Power Supply

Designed special for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ.6 where a stabilised supply is essential.

PZ.5 30 volts unstabilised £4,98 PZ.6 35 volts stabilised £7.98 PZ.8 45 volts stabilised less mains transformer) £7.98 PZ.8 mains transformer £5.98



P7 5

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail, Air-mail charged at cost

The Sinclair Guarantee

Project 60 Stereo F.M. Tuner





First in the world to use the phase lock loop principle

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. Good reception is possible in difficult areas, and often a few inches of wire are enough for an aerial. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system.

SPECIFICATIONS-Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108 MHz. SPECIFICATIONS—Number of transacors: 10 pius 2011 1.0. Tuning range: 07.50 ti 08 MTZ. Capture ratio: 1.568. Sensitivity: 2µV for 30dB quieting: 7µV for lock-in over full deviation. Squelch level: 20µV. A.F.C. range: ±200 KHz. Signal to noise ratio: > 65dB. Audio frequency response: 10 Hz – 15 KHz (±1dB). Total harmonic distortion: 0.15% for 30% modulation. Stereo decoder operating level: 2µV. Cross talk; 40dB. Output voltage: 2 x 150mV R.M.S. Operating voltage: 25-30 VDC. Indicators: Power on /tuning/stereo. Size: 93 x 40 x 207 mm

Built and tested. Post free.

£25

Stereo 60 Pre-amp/control unit



Designed for Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

SPECIFICATIONS-Input sensitivities: Radio - up to 3mV. Mag. p.u. 3mV: correct to R.I.A.A SPECIFICATIONS—Input sensitivities: nation—up to 3mV, mag. p.u. 5mV. Correct on 1,A,A curve ±1dB:20 to 25,000 Hz. Ceramic p.u.—up to 3mV. Aux—up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE ± 15 to —15dB at 10 KHz: BASS ± 15 to —15dB at 100Hz. Front panel: brushed aluminium with black knobs and controls. Size: 66 x 40 x 207mm. £9.98 Built tested and guaranteed. Built tested and quaranteed.

A.F.U. High & Low Pass Filter Unit



For use between Stereo 60 unit and two Z.30s or Z.50s, and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less

loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. Two filter stages - rumble (high pass) and scratch (low pass). Supply voltage - 15 to 35V. Current – 3mA. H.F. cut-off (–3dB) variable from 28KHz to 5KHz. L.F. cut-off (–3dB) variable from 25Hz to 100Hz. Distortion at 1 KHz (35V. supply (0.02% at rated output. Size: 66 x 40 x 90 mm. Built tested and quaranteed.

To: SINCLAIR RADIONICS LTD LONDON ROA	ST. IVES HUNTINGDONSHIRE PE17 4HJ
Please send	Name
	Address
I enclose cash/cheque/money order.	PW 12

Sinclair Q16/Micromatic

Q16 High fidelity loudspeaker

The Q16 employs the well proven acoustic principles specially developed by Sinclair in which a special driver assembly is meticulously matched to the characteristics of the uniquely designed cabinet. In reviewing this exclusive Sinclair design, technical journals have justly compared the Q16 with much more expensive loudspeakers. Its shape enables the Q16 to be positioned and matched to its environment to much better effect than is the case with conventionally styled enclosures. A solid teak surround with a special all-over cellular foam front is used as much for appearance as its ability to pass all audio frequencies without loss.

This elegantly designed shelf mounting speaker brings genuine high fidelity within reach of every music lover.

Specifications:

Construction: Special sealed seamless sound or pressure chamber with internal baffle.

Loading: up to 14 watts RMS. Input Impedance: 8 ohms.

Frequency response: From 60 to 16,000 Hz. confirmed by independently plotted B

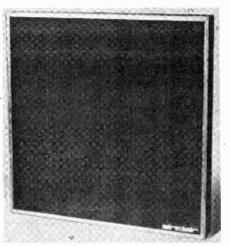
and K curve.

Driver unit: Special high compliance unit having massive ceramic magnet of 11,000 gauss, aluminium speech coil and special

cone suspension for excellent transient response.

Size and styling: 93 in. square on face x 43 in. deep with neat pedestal base. Black all over cellular foam front with natural solid teak surround.

Price £8.98.



Britain's smallest radio

Considerably smaller than an ordinary box of matches, this is a multi-stage AM receiver brilliantly designed to provide remarkable standards of selectivity, power and quality for its size. Powerful AGC counteracts fading from distant stations; bandspread at higher frequencies makes reception of Radio 1 easy. The plug-in magnetic earpiece provided, matches the Micromatic's output to give wonderful standards of reproduction. Everything including the special ferrite rod aerial and batteries is contained within the minute attractively designed case. Whether you build a Micromatic kit or buy this amazing receiver ready built and tested, you will find it as easy to take with you as your wrist watch, and dependable under the severest listening conditions.

Specifications:

Size: $36 \times 33 \times 13$ mm (1.8 x 1.3 x 0.5 in.) Weight: including batteries., 28.4 gm (1 oz.)

Case: Black plastic with anodised aluminium front panel and spun aluminium dial

Tuning: medium wave band with bandspread at higher frequencies (550 to 1,600 KHz).

Earpiece: Magnetic type.

On/off switching: By inserting and withdrawing earpiece plug.

Kit in pack with earpiece, case, instructions and solder £2.48.

Ready built, tested and guaranteed, with earpiece £2.98.

Two Mallory Mercury batteries type RM675 required from radio shops, chemists, etc.



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BARGAIN COMPUTER BUMPER BOARDS



Many Resistors, Con-densers, Diodes and Transistors (minimum of 4 transistors on each board).

5 BOARDS FOR 120n.



BLACK TERMINALS

Length as indicated 1 inch 10p per pair P. & P. 3p.

BATTERY ELIMINATOR

Plug your Transistor Radio, Amplifier, Cassette, etc., into the a.c. mains through this compact eliminator, $2\frac{1}{2}\ln \times 2\ln \times 3\ln$ approx. 41×21.50 , 61×21.50 , 61×21.50 , 91×210 ,



SEND S.A.E. FOR GREAT BARGAINS IN MICROPHONES, AMPS, DECKS, COMPLETE DISCOTHEQUE CONSOLS SPEAKERS AND MANY OTHER ITEMS

LIGHT DIMMER

The unit comes complete with MK Ivory Front Plate and Control Knob, when used in place of Light Switch it will control your room lighting from off to full brightness. Power—up to 300 watts interference.

£2.75 P. & P. 8p



SOLID STATE BLOCK MODULES

Phono pre-amp E1311 input 100k: gain 28dB max out 3 volt: max input 50mV. 3 voit: max input 50mv.
Tape pre-amp as above E1313.
Power amp E1314 input 1,000
ohms gain 20dB 30mw.
Organ tone ose E1315 tone
freq. 200-1k. Hz output 80mW. All above modules 9
voit. Dual flasher E1318 flash time 1-4 secs power 6
voit. Lamp 6v 150mA. All at £1.25 P. & P. 16



D.P.D.T. SLIDE SWITCH



SIZE 13p each 3p Postage

Transformer Scoop

Primary 220, 250 v. fused. Secondary 220 v. at 50mA, 6.3v. at 1 amp. Overall size 2% x 2" x 2% high. 63p each. P. & P. 15p.

COMPONENT CENTRE

COMPO	N	L	١,	Λ		1			,	٠	۰	E	_	U	V	ı	1	- 5	(E
8 x 6 Printed circult	bot	ar.	d							~							1	LO _D	each
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2; 8 ohm speaker		4 .															. 3	3 p	11
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100HM W/W Pots																	.1	2p	
OC81 Heat clips (dou	ble) .				ï												an.	**
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DISPLAY
This compact unit (size 8½" × 5½" ×
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light display 1600 water light output
each colour). Send S.A.E. for
further details or call in at any
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P. 4 P. 38p

POWER





peak output

Open and short circuit proof Sensitivity 10mV for full output Frequency Response 10-25,000Hz Safe with all loudspeaker systems 4 to 16 ohms

Silicon transistors used throughout F.E.T. Front end Send S.A.E. for further details

▲ £42.00 If purchased with light unit above £40.00 Post and Insurance £1.00

GUARANTEED 12 MONTHS

DWELL TIME UNIT
These small units contain the following components: 760 ohm
DPDT relay with base, 1µF
250v. paper, 0.01µF 400v. paper,
50µF 35v. electrolytic, 3 diodes
OC200 transistor, a 2N2926
type transistor unmarked, a skeleton pre-set pot, 4 pin din
plug & skt., 4 foot of 4 core
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43p P. & P. & p. & p.



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Two separate Tuning Dials, Calibrated Mhz and Degrees. Electrical Bandspread on all bands.

Bandspread on all bands

Bandspread on all bands.
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This is a quality CODAR-KIT with full 12 months guarantee. No technical knowledge required, printed circuit construction, Instruction Manual with pictorial drawings backed by friendly Help-U After Sales Service if you have any queries.

Complete Kit (even to the resin-cored solder)
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Available NOW. NEW ATS MK 2, 12 WATT. Transmitter 160-80 |
metres. Also NEW PR40 FET Pre-Selector. Stamp brings illustrated





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The CODAR CR 70A is an outstanding general coverage communication receiver, ideal for the keen S.W.L.

It tunes from 540 metres medium through to 10 metres with no gaps. Covers shipping, coastguard and distress frequencies, all six amateur bands 160-10 metres, international broadcast, Met. stations etc. etc. giving world-wide reception. Exclusive features include Air-spaced CODAR-COIL Hi-"Q" Aerial input, Illuminated "S" Meter and Slide Rule Scale, Two Speed vernier tuning, Separate B.F.O. for CW/SSB signals, 5 valves inc. two twin triodes giving 7 valve line-up, separate output for Tape recorder.

Ready to plug in to 200/240 volts A.C. it only needs your aerial and a 2/3 ohm loudspeaker to bring the world to your finger tips. |2 months full guarantee.

Complete ready built £24.50, Carriage 50p.

Ask the chap who's got one, there's lots of them !

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	TO-5	TO-66	TO-66		TO-48	TO-48
	£9	£p	£p	£p	£р	£p
50	0.28	0.25	0.47	0.60	0.58	1-15
100	0.25	0-33	0-58	0.58	0-68	1.40
200	0-25	0.27	0-57	0.61	0.75	1.60
400	0-43	0-47	0.67	0.75	0.98	1.75
600	0-53	0.57	0.77	0.97	1-25	_
800	0.68	0.70	0-90	1.20	1.50	4.00

		SIL. R	ECIS	. TES	IEU		
PIV	300mA ⊈p	750mA	1A £p	1.5A £p	3.A £p	10 A	30 A
50	0.04	0-05	0.05	0.07	0-14	0-21	0-4
100	0-04	0.06	0-05	0.18	0.16	0.23	0.7
200	0-05	0-09	0.06	0.14	0-20	0.24	1.0
400	0.06	0.13	0.07	0-20	0.27	0.37	1.2
600	0.07	0.18	0.10	0.23	0.34	0.45	1.8
800	0-10	0-17	0.13	0.25	0.87	0.55	2-0
1000	0.11	0.25	0.15	0.30	0.46	0.68	2.5
1200		0.88	_	0.33	0.57	0.75	_

	M 2A	EACS 6A	10A	LUCAS SILICON RECTIFIERS 35 amp, 400 p.l.v. stud
	TO-1 ?	r0-66 £ p	£p	type. £1-10p each.
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MPM SILICON PLAMAR BC107/8/9, 10p each; 50-99, 9p; 100 up, 50-99, each; 1,000 off, 7p each. Fully-tested and coded TO-18 case.

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One 50p Pak of your own choice free with orders valued \$4 or over.

AF239 PNP GERM, SIEMENS VHF TRANSISTORS. RF MIXER & OSC. UP TO 900 MHZ. USE AS REPLACEMENT FOR AF139.47168 & 100's OF OTHER USES IN VHF. OUR SPECIAL LOW PRICE:—1-24 87p each, 25-99 \$4p each 100 + \$0p each.

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PHOTO TRANS. OCP71 Type, 43p

SIL. G.P. DIODES \$9 300mW 30 ... 0-50 40PIV (Min.) 100 ...1-50 Sub-Min. 500 ...5-00 Full Tested 1,000 ... 9-00 Ideal for Organ Builders.

D13D1 Silicon Unilateral switch 50p each. A Silicon Planar, mono-

lithic integrated circuit having thyristor electrical characteristics, but with an anode gate and a built-in "Zener" diode between gate and between gate and cathode. Full data and application circuits available on request.

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For mains driven output stage of Amplifiers and Radio receivers.
OUR LOWEST PRICE OF 63p PER PAIR

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ZULL RARGE OF ZENER DIODES VOLTAGE RARGE 2-23V. 400mV (DO-7 Case) 13p ea. 1jW (Top-Hat) 13p ea. 10W (80-10 Stud) 25p ea. All full tested 5% tol. and marked. State voltage required.

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T3 8 2G374A OC81D
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120 VCB BIXIE DRIVER TRANSISTOR. Sim

Sil. trans. suitable for P.E. Organ. Metal TO-18 Eqvt. ZTX300 5p each.

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AF117 transistors. Large
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real value at 15 for 50p.

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Satis	faction GUARANTEED in Every Pak, or money back.	
Pak !	No.	£p 0.50
U1 U2	120 Glass sub-min, general purpose germanium diodes	0-50
	60 Mixed germanium transistors AF/RF	0.50
U3	75 Germanium gold bonded diodes sim. OA5, OA47	0.50
U4	40 Germanium translators like OC81, AC128	0.50
U5	80 200mA sub-min. Sil. diodes	
U6	30 Silicon planar transistors NPN sim. BSY95A, 2N706	0-50
U7	16 Sillcon rectifiers Top-Hat 750inA up to 1,000V	
UB	50 Sil. planar diodes 250mA, OA/200/202	0-50
U9	20 Mixed volts I watt Zener diodes	0-50
Ull	30 PNP silicon planar transistors TO-5 sim. 2N1132	0.50
U13	30 PNP-NPN sil. translators OC200 & 28104	0-50
U14	150 Mixed silicon and germanium diodes	0-50
U15	25 NPN Silicon planar transistors TO-5 slm. 2N697	0.50
U16	10 3-Amp silicon rectifiers stud type up to 1000 PIV	0-50
U17	30 Germanium PNP AF transistors TO-5 like ACY 17-22	0-50
U18	8 6-Amp silicon rectifiers BYZ13 type up to 600 PIV	0-50
U19	25 Silicon NPN translators like BC108	0.50
U20	12 1.5-Amp silicon rectifiers Top-Hat up to 1,000 PIV	0.50
U21	30 A.F. germanium alloy transistors 2G300 series & OC71	0-50
U23	30 Madt's like MAT series PNP translators	0.50
U24	20 Germanium 1-Amp rectifiers GJM up to 300 PIV	0-50
U25	25 300Mc/s NPN silicon transistors 2N708, BSY27	0-50
U26	30 Fast switching silicon diodes like IN914 micro-min	0.50
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U33	15 Plastic case 1 amp silicon rectifiers IN 4000 series	0-50
U34	30 Sil. PNP ailoy trans. TO-5 BCY26, 28302/4	0.50
U35	25 Sil. planar trans. PNP TO-18 2N2906	0-50
U36	25 Sil. planar NPN trans. TO-5 BFY 50/51/52	0-5
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U38	20 Fast switching sil. trans. NPN, 400Mc/s 2N3011	0-5
U39	30 RF germ. PNP trans. 2N1303/5 TO-5	0.50
U40	10 Dual trans. 6 lead TO-5 2N2060	0.5
U41	25 RF germ. trans. TO-1 OC45 NKT72	0.54
U42	10 VHF germ. PNP trans. TO-1 NKT667 AF117	0-5

Code Nos. mentioned above are given as a guide to the type of device in the Pak. The devices themselves are normally unmarked.

1	Pak	Description	Price
1			£p
4	01	20 Red spot trans. PNP AF 16 White spot R.F. trans. PNP 4 OC77 type trans.	0-50
и	Q2	16 White spot R.F. trans. PNP	0-50
1	Q3	4 OC77 type trans.	0-50
1	Q4	6 Matched trans. OC44/45/81/81D	0-50
)	Q5	4 OC75 transistors	0.50
	Q6	4 OC72 transistors	0-50
	Q7	4 AC128 trans. PNP high gain	0.50
١	Q8	4 AC126 trans. PNP	0.50
il	Q9	7 OC81 type trans	0.50
٠I	Q10 Q11	7 OC7r type trans. 2 AC127/128 comp. pairs PNP/NPN.	0.50
1	Q12	2 AF118 twee trans	0.50
il	013	3 AF116 type trans. 3 AF117 type trans.	0.50
	Q14	3 OC171 H.F. type trans	
i	Q15	5 9N9996 sil. epoxy trans	0.50
5	Q16	2 GET880 low noise germ, trans	0-50
	Q17	3 NPN 1 8T141 & 2 8T140	0.50
i	Q18	4 Madt's 2 MAT 100 & 2 MAT 120	
١	Q19	3 Madt s 2 MAT 101 & 1 MAT 121	0.50
	Q20	4 OC44 gerni, trans. A.F.	0.50
3	Q21	3 AC127 NPN germ. trans	0.50
0	Q22	20 NKT trans. A.F. R.F. coded 10 OA202 sil. diodes sub-min.	0-50
- 1	Q23 Q24	9 OA91 diodes	0.50
0	025	8 OA81 diodes	0-50
0	Q26	8 OA95 germ. diodes sub-min. 1N69 . 2 10A 600PIV sil. rects. IS45R	0.50
0	Q27	2 10 A 800PIV sil. rects. I845R	0.50
	Q28	2 Sil. power rects. BYZ13	0-50
0	Q29	2 8il. power rects. BYZ13 4 8il. trans. 2 × 2N696, 1 × 2N697, 1 × 2N698	
0		1 × 2N698	0.50
	Q30 Q31	7 Sil, switch trans. 2N706 NPN 6 Sil, switch trans. 2N708 NPN	0.50
0	032	3 PNP all trans 2 x 2N1131.	0.00
0	905	3 PNP sll. trans. 2 x 2N1131, 1 x 2N1132	0-50
0	033		
	Q34	7 Sil. NPN trans. 2N2369, 500MHZ	0-50
0	Q35	7 Sil. NPN trans. 2N2369, 500MHZ 3 Sil. PNP TO-5 2 × 2N2904 &	
0			
	Q36	7 2N3646 TO-18 plastic 300MH2 NPN	0.50
0	Q37	3 2N3053 NPN sil. trans.	0.50
	Q38	7 PNP trans. 4×2N3703, 3×2N3702	
0	039	7 NPN trans 4 × 9N3704 3 × 9N3705	0.60
_	040	7 NPN amp. 4×2N3707, 3×3N3708. 3 Plastic NPN TO-18 2N3904	0.50
0	Q41	3 Plastic NPN TO-18 2N 3904	0.80
0	Q42	6 NPN trans. 2N5172	0-50
0	Q43	7 BC107 NPN trans. 7 NPN trans. 4 × BC108, 3 × BC109.	0.50
	Q44	7 NPN trans. 4 x BC108, 3 x BC109 3 BC113 NPN TO-18 trans	0-50
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0	047	3 BC115 NPN TO-5 trans	0.50
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0	Q49	4 NPN trans. 2 x BFY51, 2 x BFY52	0.50
0	Q50	7 BSY28 NPN switch TO-18	0.50
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0μΑ Αμ0
0-0-50µA \$8 10
00µA #3-16
00 88 Au(001-0-00
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00 88 Au
00-0-500µA \$8 80
mA An
-0-1mA \$2.80
mA £2:80
0mA #2:80

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100µ

500µ. 1mA

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VU Meter. 48-60
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	ov amp. A.c. as o
pa MR.52P. 2}	in. square fronts.
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504A 82-60	20V. D.C 82-00
- 08-ER A	50V. D.C 42.00
-100µA #\$-50	300 V. D.C. 48.00
4 42 30 .	15 V. A.C 42-10
49-00	300V. A.C. #8-1
#2-00	B Meter 1mA #8-1
42:00	VU Meter £3.2
##-00	1 amp. A.C. * 22.0
A AS-00	5 amp. A.C.* \$2.0
A \$29-00	10 amp. A.C. *\$2.00
p £E-00	20 amp. A.C. \$2 0
P #2:00	30 amp. A.C.*#2:00

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50-0-50µA #8.75	20V. D.C 43-20
100µA \$8.75	50V. D.C 48-80
100-0-100µA#8-65	150V.D.C \$8-20
200μA \$2 65	300V. D.C. #2-20
500µA 43-40	15V. A.C \$2:30
500-0-500µA \$2:80	50V. A.C \$8-80
lmA #2 20	150V. A.C. 22.80
5mA #2-20	300V. A.C. #8-80
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50mA #\$ 20	8 Meter 1mA \$2.87
100mA #2-20	VU Meter #3-87
500mA #3-20	50mA A.C. *23.20
1 amp #3-20	100mA A.C.*#8:20
5 amp £2:20	200mA A.C.*#2-20
10 amp: #8:20	500mA A.C.*88-20
15 amp £2.20	1 amp. A.C.* #2:20
20 amp £3-20	5 amp. A.C.* #2-20
30 amp \$2.80	10 amp. A.C.*22.20
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5V. D.C #2:20	30 amp. A.C.*#2-26

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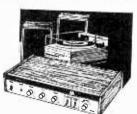
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DB3GT	OB3	0.60	68R7	0.40	E180F 0	95	PCC805	0.85
IBS 100 80		0.88		0.85	ESTOF Z	-35	PCF80	
11A4	1 B3(4T	0.88	6U8A	0.40	EAF42 0	-55	PCF82	
1RA			6V6GT	0.88	EBC33 0	-50	PCF86	0.90
184	1 R4	0.85	6X5GT	0.85	EBC81 0	-30	PCF87	0.85
174		0.85	6X8			-40	PCF801	0.50
11	185	0.25	7Y4	0.60	EBF89 0	-80	PCF805	0.75
11		0.25	9BW6	0.50	EC53 0		PCF806	0.70
1728	1 U 5	0.50			EC88 0	-60	PCH200	0.70
2001 304	172		10D2	0.40	EC90 0	.33	PCL81	0.50
324		0.82		0.50	EC92 0	-35	PCL83	0.65
Section	3A4	0.85	10F18	0.45	EC93 0	-50	PCL84	0.45
384	3B28 3BP1	2.15	10LD11	0.60	EC8010 2	-60	PCL86	0.45
3V4 0.45 12AB5 6.00 ECCS4 0.30 PCL801 0.70 5Y4G 0.32 12AL6 6.40 ECCS4 0.30 PD500 1.70 61V4G 0.42 12AG 6.43 ECCS8 0.40 PF86 0.80 67Y3GT 0.50 12AT7 0.30 ECCS8 0.40 PF818 0.83 67SAG 0.50 12AU7 0.30 ECCB9 0.35 PLB2 0.45 6AB4 0.35 12AV7 0.30 ECCB9 0.35 PLB3 0.45 6AB4 0.35 12AV7 0.30 ECP80 0.35 PLB4 0.40 6AB5 0.50 12BA6 0.35 ECH81 0.30 PLB4 0.40 6AB5 0.50 12BA7 0.30 ECR90 0.35 PLB4 0.40 6AB5 0.31 12BA7 0.35 ECH81 0.30 PLB4 0.45 6AB5 0.32 12B	3Q4	0.40	10P13	0.55	ECC81 0	-38	PCL88	0.90
5Y4G 0 -80 12ACB 0 -40 ECC84 -80 PP560 -80 -80 6U4GB 0 -42 12AG 0 -43 ECC88 0 -40 PF581 0 -85 -80 6U4GB 0 -42 12AT 6 -83 ECC88 0 -40 FF581 0 -85 -80 6U4GB 0 -42 12AT 6 -83 ECC89 0 -50 -91 133 0-85 12AU 9 -83 ECC89 0 -50 -91 133 0-85 12AU 9 -83 ECC89 0 -80 PF581 0 -85 68 12AU 9 -83 ECC99 0 -85 PL33 0 -85 68 68 12AU 9 -83 ECC99 0 -85 PL33 0 -85 68	384 3V4	0.85	10Pl4		ECC82 0	-80	PCL800	0.20
6 V4G 0-42 12 AG5 6-43 ECC89 0-50 PFL30 0-55 6 Y3G 0-70 0-82 12 AT7 -38 ECC99 0-50 PFL30 0-55 5 Z4G 0-40 12 AU7 0-30 ECC89 0-50 PL30 0-55 6 AB4 0-85 12 AV7 0-50 ECP80 0-35 PLB3 0-56 6 AB4 0-80 12 AY7 0-50 ECP80 -85 PLB3 0-46 6 AH6 0-80 12 BA7 0-30 ECP80 -85 PLB3 0-46 6 AH6 0-80 12 BA7 0-35 ECH81 0-30 PLB40 -80 6 AK6 0-80 12 BA7 0-35 ECH81 0-30 PLB40 -80 6 AK6 0-83 12 K7 0-56 ECL81 0-35 PLB3 0-80 6 AK7 0-83 12 K7 0-56 ECL89 0-35 PY31 0-80 6 AM6 0-32 12	5R4GY	0.60	12AC6	0.40	ECC84 0	-80	PD500	1'50
6 Y43G 042 12AT6 0-30 ECCS9 0-50 PPL200 0-70 6 Y3GT 050 12AU7 0-30 ECCS9 0-20 PL33 0-55 5 Z3G 040 12AU7 0-30 ECCB9 0-35 PLB1 0-56 6 ABA 055 12AV7 0-50 ECP80 0-35 PLB2 0-56 6 ABA 056 12AV7 0-50 ECP80 0-35 PLB2 0-46 6 AH4 050 12AX7 0-50 ECH80 0-67 PLB2 0-46 6 AH5 0-80 12BA6 0-35 ECH81 0-30 PLB04 0-86 6 AKB 300 12BA7 0-35 ECH81 0-30 PLB04 0-86 6 AL3 301 12BA7 0-35 ECL80 0-40 PL509 0-80 6 AM5 032 12EV5 0-55 ECL81 0-45 PL509 0-98 6 AM6 033		0.83	12AL5		ECC85 0	-40	PF86 PF818	
5Z4G	5 V 4 G	0.42	12AT6	0·80	ECC89 0	-50	PFL200	0.70
12AUT 0.85 CCP80 0.85 CP80 0.85 6.AB4 0.85 12AV7 0.80 CCP80 0.85 6.AB4 0.85 12AV7 0.80 CCP80 0.85 6.AB4 0.85 12AV7 0.80 CCP80 0.85 6.AB6 0.85 12AV7 0.80 CCP80 1.50 6.AB6 0.80 12BA7 0.85 CCH82 0.70 6.AL3 0.81 12BA6 0.85 CCH83 0.80 6.AL3 0.81 12BA6 0.85 CCH83 0.80 6.AL3 0.81 12BA6 0.85 CCL83 0.85 6.AB6 0.82 12K5 0.85 CCL83 0.85 6.AB7 0.80 0.90 0.45 6.AB8 0.85 0.90 0.90 6.AB7 0.80 0.90 0.	5Y3GT	0.82	12AT7	0.88	ECC91 0	20	PL33	0.85
6AB4		0.40	12AU7		ECF80 0	-85	PL81	0.50
6AP4A 0-50 12AX7 0-30 ECF804 1-50 PL84 0-40 CAP7 0-70 CAH6 0-50 12B4A 0-55 ECH81 0-30 PL804 0-80 CAP8 0-30 12BA5 0-35 ECH81 0-30 PL804 0-80 PL804 0-80 CAP8 0-80 PL804 0-8	6/30L2	0.75	12AV6	0.83	ECF82 0	-35	PL82	0.45
SAMS		0.85	12 A X 7		ECF804 1	50	PL84	0.40
6AAK6 0-30 12BAG 0-35 ECH83 0-40 PL508 0-90 30 6AK6 0-57 12BEG 0-35 ECH84 0-45 PL509 1-30 PAL901 0-80 6AL3 0-40 12BY7 0-55 ECH84 0-45 PL509 1-30 PAL901 0-80 PAL901 0-	6AG7	0.40	12AY7	0.70	ECH42 0	-70	PL302	0.80
6AK6 0-30 12BA7 0-35 ECH84 0-45 PL509 1-30 0-80 6ALJ 0-80 PS PBES 0-35 ECL81 0-45 PM84 0-50 CBPT 0-55 ECL81 0-45 PM84 0-50 CBPT 0-80 PASA 0-80	6AJ8	0.80	12BA6	0.35	ECH83 0	-40	PL508	
6ALD 0-20 12817 0-56 ECLB2 0-35 PY31 0-80 6AM6 0-32 12877 0-56 ECLB2 0-35 PY31 0-80 6AM6 0-32 12877 0-56 ECLB3 0-65 6AM6 0-32 12877 0-56 ECLB3 0-65 6AM6 0-32 12877 0-36 ECLB3 0-65 6AQ6 0-35 12977 0-36 ECLB3 0-65 6AQ6 0-35 14877 0-36 ECLB3 0-65 6AR8 0-35 14877 0-36 ECLB3 0-65 6AR8 0-36 1487 0-36 ECLB3 0-65 6AR8 0-38 20P1 0-45 EF377 0-40 6AR3 0-30 20P5 1-10 EF40 0-65 6AV6 0-30 20P5 1-20 EF41 0-65 6AV6 0-30 20P5 1-20 EF41 0-65 6AV6 0-30 25C5 0-50 6AV6 0-30 25C5 0-50 6AV6 0-30 25C5 0-50 6AV6 0-30 25C5 0-50 6BF6 0-30 30AC5 0-45 EF30 0-35 6BF6 0-30 30AC5 0-45 EF30 0-35 6BF6 0-30 30AC5 0-45 EF68 0-35 6BF6 0-30 30AC5 0-45 EF68 0-35 6BF6 0-30 30AC5 0-45 EF68 0-35 6BF6 0-30 30AC5 0-45 EF68 0-35 6BF6 0-30 30AC5 0-45 EF68 0-35 6BF6 0-30 30AC5 0-45 EF69 0-28 6BF7 0-30 30L17 0-80 EF99 0-85 6BK6 0-45 30C17 0-85 EF99 0-85 6BK7 0-45 30FL1 0-70 EF99 0-85 6BK8 0-45 30FL1 0-70 EF99 0-85 6BK8 0-45 30FL1 0-80 EF90 0-100 6BK8 0-25 30FL1 0-80 EF90 0-100 6BK8 0-25 30FL1 0-80 EF90 0-100 6BK8 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35 30FL1 0-80 EF90 0-100 6BK9 0-35	6AK5	0.80	12BA7	0.85	ECH84 0	45	PL509	1.30
6AM6 0-38 12K76T 0-35 ECL83 0-65 PY80 0-38 A6AM6 0-38 12Q76 0-30 ECL84 0-55 PY80 0-38 PY80 0-38 A6AM6 0-38 12Q76 0-30 ECL85 0-55 PY81 0-30 A6AM6 0-55 12Q76 0-30 ECL85 0-55 PY81 0-30 A6AM6 0-40 20D1 0-45 ECL86 0-65 PY80 0-30 PY82 0-30 PY82 0-30 PY82 0-30 PY83 0-38 A6AM6 0-40 20D1 0-45 EF39 0-40 PY80 0-50 PY80 0-50 A6AM6 0-32 20P1 1-10 EF40 0-60 PY80 0-50 A6AM6 0-30 20P4 1-10 EF40 0-60 PY80 0-50 A6AM6 0-30 20P4 1-10 EF40 0-60 PY80 0-50 PY80 0-50 A6AW6 0-30 28L6GT 0-45 EF42 0-70 QV2-2-8 120 A6AW6 0-52 25C5 0-60 EF42 0-70 QV2-2-8 120 A6AW6 0-52 25C2GT 0-65 EF42 0-70 QV2-2-8 120 A6AW6 0-52 25C2GT 0-65 EF86 0-36 A6AW6 0-52 25Z4G 0-60 EF86 0-36 A6AW6 0-52 25Z4G 0-60 EF86 0-36 A6AW6 0-52 25Z4G 0-60 EF86 0-36 A6AW6 0-55 A6AW6	6AL3	0.57	12BE6 12BH7	0.40	ECL81 0	45	PM84	0.50
6AM6 0-38 12KTGT 0-30 ECL36 0-55 Y860 0-38 6AQ6 0-58 12BR7 0-30 6AR5 0-38 12BR7 0-30 6AR6 0-40 20D1 0-45 6CL36 0-40 P780 0-38 6AR6 0-40 20D1 0-45 6CL36 0-40 P780 0-38 6AR6 0-40 20D1 1-10 EF37 0-60 P780 0-38 P780 0-	6AL5	0.20	12BY7	0.55	ECL82 0	85	PY31	0.80
6AQ6 0-35 12Q76 0-30 ECL86 0-45 PY81 0-30 6AQ6 0-55 12B7 0-35 (ECL86 0-45 PY82 0-30 PY81 0-36 6AR6 0-45 1487 0-35 (ECL86 0-45 PY82 0-30 PY83 0-38 6AR6 0-40 20D1 0-45 ECL86 0-46 PY83 0-38 PY88 0-40 PY83 0-38 PY88 0-40 PY85 0-35 (ECL86 0-46 PY85 0-35 PY88 0-40 PY85 0-35 (ECL86 0-46 PY85 0-35 PY88 0-40 PY85 0-35 (ECL86 0-46 PY85 0-45 PY8		0.88	12K5 12K7GT	0.85	ECL83 0	55	PV80	0.85
6ARS 0.36 1487 0.80 ECLL800 PY88 0.38 0.40 20D1 0.45 6ARI1 1.25 20L1 1.10 EF37 0.60 PY80 0.40 0.60 PY80 0.50 EF39 0.40 PY80 0.50 PY80 0.50 PY80 0.50 PY80 0.50 PY80 0.50 PY80 0.50 PS2 0.50 EF41 0.60 PY80 0.50 PS2 0.50 0.50 PS3 0.80 PS8 0.80 0.50 PS3 0.80 QQV03-2.10 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 <td>6AQ5</td> <td>0.85</td> <td>12Q7G</td> <td>0.80</td> <td>ECL85 0</td> <td>-55</td> <td>PY81</td> <td>0.80</td>	6AQ5	0.85	12Q7G	0.80	ECL85 0	-55	PY81	0.80
6ARRIG 0-40 20DJ 0-45 1-50 PY88 0-40 6ARSI 1-25 20L1 1-0 EF37A 0-40 PY800 1-00 6ARTG 0-80 20P4 1-10 EF30 0-40 PY800 0-50 6ATG 0-80 20P4 1-10 EF40 0-65 PY801 0-60 6ATG 0-30 22DS 0-50 EF41 0-65 PY801 0-50 6AW8A 0-55 25Z6G 0-80 EF83 0-85 QQV02-6 2:15 6BE6 0-80 30AES 0-40 EF86 0-35 QQV03-20A 6BF6 0-80 30CIS 0-80 EF98 0-80 QQV03-20A 6BB76 0-80 30CIS 0-80 EF99 0-80 TT22 2-80 6BB76 0-80 30CIS 0-75 EF91 0-80 TT22 2-80 6BB76 0-45 30CIS 0-80 EF93 <t< td=""><td>6AQ6</td><td>0.55 0.25</td><td></td><td>0.80</td><td>ECLL800</td><td>40</td><td>PY83</td><td></td></t<>	6AQ6	0.55 0.25		0.80	ECLL800	40	PY83	
8ABS 0.36 29P1 1-0 EF39 0-40 PY800 0.50 8ABTG 0.80 20P4 1-10 EF40 0-65 PY800 0-50 6ATG 0.30 20P5 1-20 EF41 0-65 PY800 0-50 6AV8 0.30 255 CSCG 0-50 EF42 0-70 CAC PY800 0-85 6BAB 0.55 25276 T 0-85 EF83 0-85 QQV0-6 255 QQV0-6 256 QQV0-6 255 QQV0-6 256 QQV0-6 251 QQV0-6 251 QQV0-6 251 QQV0-6 251 QQV0-6 251 QQV0-6 251 QQV0-6 248 QPV8-0 285 QQV0-6 248 QPV8-0 285 QQV0-6 251	6AR6	0.40	20D1	0.45	1		P¥88	
SABTG 0-80 20P4 1-10 EF40 0-60 PX801 0-50 CAV6 0-30 25L5GT 0-65 EF41 0-65 PX30 0-85 CAV6 0-30 25L5GT 0-65 EF42 0-70 0-66 PX30 0-85 CAV6 0-30 25L5GT 0-65 EF42 0-70 0-66 PX30 0-85 CAV6 0-80 0-85 CAV6 0-80 0-85 CAV6 0-80 0-85 CAV6 0-85 CAV6 0-80 CAV6 CAV6 0-80 CAV6 CAV6 0-80 CAV6 CAV6 0-80 CAV6			20L1	1.10	EF37A 0	-60	PY500 PY800	1.00
6AV6 0-30 25L56 T 0-45 EF80 0-36 QQV03-10 6AW8A 0-55 25Z4G 0-30 EF83 0-35 6BA6 0-25 25Z6G 1-655 EF85 0-30 6BB6 0-30 30AB 0-40 EF85 0-30 6BF6 0-30 30AB 0-40 EF89 0-38 6BB6 0-30 30AB 0-40 EF89 0-38 6BB6 0-56 30C1 0-80 EF91 0-33 6BB6 0-45 30C1 0-80 EF91 0-33 6BB6 0-45 30C1 0-80 EF92 0-40 6BB7 0-45 30C1 0-80 EF92 0-40 6BB7 0-45 30C1 0-70 EF92 0-40 6BB7 0-40 30F1 0-70 EF183 0-30 6BB7 0-55 30F1 0-80 EF80 0-30 6BB7 0-70 30L1 0-80 EF80 0-30 6CGG 0-40 30P1 0-80 EL33 1-25 6CGG 0-40 30P1 0-80 EL34 0-50 6CGG 0-55 35E5 0-65 EL33 0-42 6CGG 0-60 35C5 0-40 EL35 0-60 6CW4 0-83 35D8 0-70 EL37 0-25 6CW4 0-83 35D8 0-70 EL37 0-75 6CW4 0-83 35D8 0-70 EL38 0-40 6CW4 0-83 35D8 0-70 EL38 0-70 6FF0 0-90 0-85 65A2 0-85 6FF1 0-70 0-85 66A2 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75 6360 0-75 ER89 0-85 6FF3 0-75	6A87G	0.80	20P4	1.10	EF40 0	-50	PY801	0.50
6AW8A 0-30 281.6GT 0-45 EF80 0-25 6BA6 0-25 625 6B 26 0-25 0-2	6AT6				EF41 0	-85	PZ30	9.15
6B M8	6AV6	0.30		0.45	EF80 0	-25	QQVO3-	10
6BEE 0-30 30 AB 0-45 EFS8 0-30 6 Dec of the control of the co	6AW8A	0.55	25Z4G	0.80			00003-9	
6BF6 0-80 30AE3 0-40 EF99 0-28 38 6BH6 0-55 30C16 0-30 EF99 0-38 6BH6 0-46 30C17 0-85 EF99 0-40 TT21 2-55 6BB76 0-45 30C17 0-85 EF95 0-30 TT22 2-80 6BB76 0-45 30C18 0-75 EF95 0-30 TT22 2-80 6BB76 0-42 30F16 0-70 EF96 0-85 U25 0-75 U25 0-		0.80	30 A 5	0.45	EF86 0	-80	-	5.25
6BH6 0-45 30C15 0-80 EF92 0-40 TT21 2-66 6BK7A 0-45 30C17 0-86 EF95 0-80 TT22 2-80 CBBK5 0-45 30C18 0-75 EF97 0-85 U18/20 0-75 6BK8 0-85 30C18 0-75 EF98 0-85 U26 0-75 U26 0-80 U26 0-75 U26 0-80 U26 0-80 U26 0-80 U27 0-80 U27 0-80 U27 0-80 U27 0-80 U28 0-80 U29 0-80 U26 0-80 U26 0-80 U26 0-80 U26 0-80 U26 0-80 U26 0	6BF5	0.80	30AE3	0.40			QQ V06-4	A 8.50
6BBK7 A 0-54 30C18 0-75 EP98 0-65 U18/20 0-75 6BN6 0-40 30Fb1 0-85 EP98 0-65 U26 0-76 6BN6 0-40 30Fb1 0-85 EP183 0-80 U26 0-75 6BR8 0-65 30Fb1 0-80 EP183 0-80 U26 0-75 6BR7 1-30 30L1 0-40 EF804 1-25 U26 0-85 6BW7 0-70 1-30L17 0-80 EE594 1-25 U22 0-82 6BX6 0-25 30P12 0-80 EL33 1-25 U78 0-80 6CAG 0-35 30P12 0-80 EL34 0-50 U291 0-80 6CBG 0-30 30P114 0-70 EL37 1-26 U291 0-80 6CBG 0-30 30P114 0-80 EL33 0-50 U291 0-80 6CCBG 0-35 36191		0.45	30C15	0.80	EF92 0	40	TT21	2-65
6BRNS 0-480 30FFD 0-85 EP98 0-65 U25 0-75 6BRS 0-40 30FFLI 0-70 EF183 0-85 U25 0-75 6BRS 0-65 30FLI2 0-88 EF184 0-85 U231 0-45 6BBRS 0-65 30FLI4 0-76 EF804 1-25 U562 0-38 6BW6 0-75 30L17 0-80 EF804 1-25 U562 0-38 6BX6 0-25 30F12 0-80 EL33 1-25 U78 0-80 6BZ6 0-25 30F12 0-80 EL33 1-25 U291 0-36 6CGA 0-33 0-711 0-70 EL36 0-50 U201 0-35 6CGB 0-33 0-711 0-73 EL37 1-25 U282 0-40 6CBA 0-30 30F14 0-90 EL42 0-58 U301 0-40 6CBA 0-55 355A	6BJ6	0.45	30C17	0.85	EF95 0	-80	TT22	2.80
6BNG 0-40 30FLI 0-70 EFIS3 0-30 U29 0-75 6BRS 0-65 30FLI 0-76 EFIS4 0-35 U31 1-50 6BRS 0-65 30FLI 0-76 EFR04 1-25 U29 0-38 6BRS 0-65 30FLI 0-76 EFR04 1-25 U62 0-38 6BRS 0-65 30FLI 0-80 EER04 1-25 U76 0-38 6BRS 0-65 30LI 0-80 EER04 1-25 U76 0-38 6BRS 0-65 30LI 0-80 EER04 1-25 U77 0-38 6BRS 0-65 30LI 0-80 EES 0-30 U77 0-38 6BRS 0-25 30FLI 0-80 EL33 1-25 U77 0-38 6CG 0-25 30FLI 0-80 EL33 1-25 U77 0-38 6CG 0-36 0-38 0-70 EL3 1-25 U291 0-32 6CG 0-36 0-35 35BS 0-55 EL3 1-25 U403 0-50 6CG 0-55 35BS 0-75 EL42 0-85 6CG 0-60 0-55 35BS 0-75 EL33 0-85 6CCY 0-43 35L6GT 0-50 EL36 0-40 UAF41 0-50 6DRS 0-43 35L6GT 0-50 EL39 0-33 UAB080 0-35 6CCY 0-43 35L6GT 0-50 EL39 0-35 UBC41 0-50 6DRS 0-48 352GT 0-40 EL392 0-90 6DRS 0-48 352GT 0-40 EL392 0-90 6DRS 0-48 352GT 0-40 EL392 0-90 6BRS 0-55 50L6GT 0-50 EM31 0-50 6ERH 0-70 90AG 2-40 EM54 0-90 6ERH 0-70 90AG 2-50 EM58 0-60 UCH32 0-70 6ERH 0	6BN5	0.48	30F5		EPOR A		U25	0.75
6BBRS 0-65 30PL14 0-75 EP800 1-90 U37 1-50 081 0-60 0-85 EP804 1-25 U02 0-83 6BW6 0-55 30L15 0-85 EK90 0-30 U76 0-80 6BW7 0-70 0-30L17 0-80 EK90 0-30 U76 0-80 6BX6 0-25 30P12 0-80 EK90 0-80 U201 0-80 6BX6 0-25 30P12 0-80 EL34 0-50 U201 0-80 6C4 0-80 0-80 0-80 6C4 0-80	6BN6	0.40	30FL1	0.70	EF183 0	80		
6BW6 0-55 30L15 0-85 EK90 0-30 U76 0-80 6BW6 0-70 10L17 0-80 EL33 1-25 U78 0-80 6BZ6 0-25 30P12 0-80 EL34 0-50 U191 0-70 6C4 0-33 30P11 0-80 EL34 0-50 U201 0-86 6C4 0-33 30P11 0-90 EL37 1-25 U281 0-40 6CB6G 1-15 35A3 0-55 EL42 0-58 U301 0-40 6CB6G 1-55 35A3 0-55 EL53 0-50 U301 0-40 6CB6 0-55 35A3 0-55 EL54 0-25 U404 0-40 6CH6 0-50 35C3 0-40 EL58 0-42 U404 0-40 6CW4 0-83 35L9 0-70 EL58 0-40 UAF41 0-50 6CY7 0-85 35W4 0-8	6BR8	0.65	30FL12	0.75	EF800 1	·00	U37	1.50
6BW7 0.70 30L17 0.80 EL33 1.25 U78 0.80 6BX6 0.25 30P19 0.80 EL34 0.50 U191 0.76 6BZ6 0.33 30P19 0.80 EL36 0.50 U201 0.36 6CG6 0.43 0.7011 0.70 EL36 0.50 U201 0.36 6CG6 0.40 3PL13 0.93 EL41 0.55 U203 0.40 6CG7 0.50 30 30P14 0.90 EL42 0.55 U403 0.50 6CG7 0.50 35AS 0.55 EL83 0.42 U404 0.40 6CH6 0.55 35BS 0.65 EL84 0.25 U801 0.40 6CH6 0.55 35BS 0.65 EL84 0.25 U801 1.00 6CV5 0.43 35DB 0.70 EL88 0.40 UAF41 0.56 6D2 0.45 35Z49 <	6B87	1.80	30L1	0.40	EF804 1	25	U52	
6BX6 0-25 30P12 0-80 EL34 0-50 U91 0-786 6BZ6 0-25 30P12 0-70 EL37 1-25 U221 0-40 0-86 6C4 0-83 30PL1 0-90 EL34 0-50 U201 0-35 0-60 0-60 0-70 EL37 1-25 U222 0-40 0-60 0-60 0-70 EL37 1-25 U222 0-40 0-60 0-60 0-70 EL37 1-25 U222 0-40 0-60 0-60 0-75 0-75 EL37 0-75 U223 0-40 0-60 0-60 0-75 0-75 EL37 0-75 U223 0-40 0-60 0-75 0-75 EL37 0-75 U231 0-93 0-75 EL37 0-75 U231 0-93 0-75 EL37 0-75 U231 0-93 0-75 EL37 0-75 U231 0-93 0-75 EL37 0-75 U331 0-93 0-75 EL37 0-75 U331 0-93 0-75 U331 0-93 0-75 U331 0-93 0-75 U331 0-75		0.70	30L15	0.80	EL33 1	25	U78	0.80
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Color Colo	6CG7	0.50	35A5	0.75	EL83 0	42		0.40
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28 watts, r.m.s. 40Hz to 40kHz ± 3dB



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SPEAKERS Duo Type II Size approx $17'' \times 10\frac{3}{4}'' \times 6\frac{3}{4}''$. Drive unit $13'' \times 8''$ with parasitic tweeter. Max. power 10 watts. 3 ohms. Simulated Teak cabinet. £14 pair+£2 p&p.

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SPECIFICATION RIOI

14 watts per channel into 3 to 4 ohms. Total distortion @ 10W @ |kHz 0.1%. P.U.1 (for ceramic cartridges) (@) 10VV (@) 18/12 0 17/6 r. O. 1 (Go Castridges) 150mV into 3 Meg. P.U.2 (for magnetic cartridges) 4mV (@) 18/Hz into 47K. equalised within ± 1dB R.I.A.A. Radio 150mV into 220K. (Sensitivities given at full power). Tape out facilities; headphone socket, power out 250mW per channel. Tone controls and filter characteristics. Bass: +12dB to -17dB @ 60Hz. Bass filter: 6dB per octave cut. Treble control: treble +12dB to -12dB @ 15kHz. Treble filter: 12dB per octave. Signal to noise ratio: (all controls at max) R101-P.U.1 and radio-65dB. P.U.2. -58dB. R100 same as R101 but P.U.2 (for crystal cartridges) 450mV into 3 Meg. Cross talk better than -35dB on all inputs. Overload characteristics better than 26dB on all inputs. Size approx 133" x 9" x 33".



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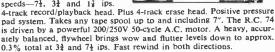


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VAL	VFS 6	BE6		6J7M	45	7C6		14H7	50			DAF96		EC90		EL42		N108		PL508		U801 UABC8	
IAL	6	BH6	75	6J7G	30	7D5	55	19AQ5		50B5				ECC81		EL84		OA2		PL509		UAF42	55
1A7GT			50	6J7GT	45	7H7		20D1		50C5		DF33		ECC82		EL95		OC3		PL802		UBC41	50
1CP31	\$6.00 6		45	6K6GT	60	7 R7		20F2		50CD6G			45	ECC83		ELL80			50	PX4		UBC81	40
1 D5	40 6	BR7	90	6K7M	35	787	£2.25	20L1		50L6GT		DF91		ECC84		EM34		PC86	60	PX25 PY33		UBF80	40
1H5	50 6	BR8	70	6K7G	20	7¥4		20P4	£1.10			DF92		ECC85		EM80		PC88		PY81		UBF89	35
INSGT	55 6	B87		6K7GT		9BW6		20P5	£1-20			DF96		ECC88		EM81		PC97	20	PY82		UCC84	43
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3A4		C6		6L6G		10F18		25Z5G		801		DK92 DK96		ECL80	45	EZ41		PCF84		R2		UCL82	35
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BU4G	35 6 45 6			68H7M		12AU6		30FL1		5763	70	DL96		EF9	75	GZ34		PCF80		STV28		UM80	28
5V4G	32 6			68J7GT		12AX7		30FL12		7193		DM70		EF37A		HN309	£1.50	PCL82	85		£10.00		£1.05
5Y3GT 5Z4G	40 6			68K7GT		12BA6		30FL14		7475		DY86		EF39		KT36		PCL83		SU25	£1.00	UU7	£1.05
6/30L2	80 6			68L7GT		12BE6		30L15		A61		DY87	83	EF41		KT61		PCL84		SU215		UU8	£1.05
6A7	75 6			68N7GT		12C8G7		30L17		ATP4		E88CC	65	EF50	25	KT66		PCL85		T41	£1.00		45
	40 6		70	68Q7GT		12E1	£1.80			ATP5	60	EA50		EF80		KT81		PCL86		TDD4		UY21	50
6A8G		F23		6U4GT		12J5G7		30P12		ATP7	50	EABC8		EF85		KT81(7	7C5)	PD500		TH41		UY41	48
6AK5	99 6	F24		6U5G		12J7G7		30P19		AU2	£4.00	EAF42		EF86	30			PENA				UY85	40
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6AT6		H6		6X5G		128G7	35	35L6		CCH35		EBF80		EF183	30	ML6	40	PL81		U191		VU120	
		J5M		6X5GT		128117	35	35W4	35	CL33		EBF83		EF184	35 30	MSP4	50	PL82 PL83		U251			£2.50
6AU6										CY30		EBF89		EL32	01 06	MU14		PL84		U301		W81M	63
6B4G		J5G		7B6		128J7	40	35Z4G	r 50	CY31	43	EBLI		EL33 EL34	\$1.20	MX40		PL500		U403		Y63	50
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Iran	sisto	rs		2N2219		AAZ12		AD161	37	BF898		GJ7M		NKT2		OAZ20		0C44		OC82D		ZTX 10	
				2N2369A		AC126		AF115		BFY50		KS100		NKT71		OAZ20		OC45 OC57		OC821		ZTX 10	
1N914		N697		2N2646		AC127		AF117		BFY51	20	MJE52		OA70	10	OAZ21 OAZ22		OC57		OC170		ZTX30	
18113		N706		2N2904	20	AC128		ASY26		BY100		MJE29		0A71	10	OAZ22	4 45	OC58		OC171		ZTX 30	
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OC3	0.38	6AR11 1.25	6F1 0.75	7Y4 0.65		COM				0.30	KT88 2.00	PL302 Q.85	U801 0.80
OD3	0.35	6AS5 0.45	6F5 0.75	9BW6 0.60						1.25	N78 1.50	PL504 0.80	UABC80
1B3GT	0.40	6A87G 0.85	6F6G 0.35	10C2 0.50	//		BR/	IND	EL34	0.50	PABC800.40	PL508 0.90	0.40
1 1L4	,0.20	6AT6 0.35	6F11 0.40	10D1 0.55		-				0.50	PC86 0.60	PL509 1.10	UAF41 0.50
1R4 -	0.45	6AU6 0.25	6F13 0.45	10D2 0.50	Lane S	(3)				1.60	PC88 0.80	PL801 0.80	UAF42 0.55
1R5	0.40	6AV6 0.80	6F14 0.70	10F1 0.75						0.60	PC97 0.50	PL802 0.95	UB41 0.60
184	0.30	6AW8A 0.60	6F15 0.65	10F9 0.60	FIFC	TRON	IC VA	LVES		0.65	PC900 0.48	PM84 0.60	UBC41 0.50
185	0.30	6AX4GTB	6F18 0.50	10F18 0.50		INUN	IC VA	FAFO	EL81	0.55	PABC800-40	PY31 0.30	UBC81 0.46
1T4	0.30	0.60	6F23 0.85	10L1 0.50						0.42	PCC84 0.40	PY33 0.68	UBF80 0.40
1U4	0.80	6AW8A 0.60	6F24 0.75	10LD110.65	2505 0.50	50A5 0.75	DK92 0.56	ECC89 0.50	EL84	0.25	PCC85 0.40	PY80 0.40	UBF89 0.35
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1 V 2	0.50	6BE6 0.30	6F26 0.35	10P14 1.10	25Z4G 0.30	50C5 0.50	DM160 0.65	ECC189 0.85		0.40	PCC89 0.55	PY82 0.35	UBL21 0.65
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2A3	0.50	6BF6 0.55	6GK6 0.60	12AC6 0.50	30 A5 0.50	50L6GT 0.55	DY87 0.83	ECF82 0.85		0.85	PCC805 0.85	PY88 0.40	UCC85 0.40
2CW4	0.70	6BH6 0.75	6J4 0.50	12 A D6 0.55	30AE3 0.40	85A2 0.50	DY802 0.35	ECF86 0.65	EL821		PCC806 0.80	PY500 1.00	UCF80 0.55
2D21	0.38	6BJ6 0.50	6J5GT 0.30	12AE6 0.55	30C1 0.80	90AG 2.40	E88CC 0.85	ECF8041,65	EL822		PCF80 0.30	PY800 0.40	UCH21 0.60
3A4	0.40	6BK7A 0.60	6J6 0.20	12AL5 0.50	30C15 0.80	90AV 2.50	E180F 1.00	ECH42 0.75	ELL80		PCF82 0.35	PY801 0.50	UCH42 0.70
3BP1	8.00	6BN5 0.43	6J7 0.45	12AQ5 0.50	30C17 0.90	90C1 0.65	E810F 2.90	ECH81 0.30		1.00	PCF84 0.60	PZ30 0.85	UCH81 0.40
384	0.35	6BN6 0.45	6K6GT 0.60	12AT6 0.80	30C18 0.80	90CV 2.40	EABC800.35	ECH83 0.45		0.80	PCF86 0.60	QQV02-6	UCL81 0.60
3V4 5R4GY	0.48	6BQ5 0.25 6BR8 0.70	6K7 0.35 6K8G 0.40	12AT7 0.35	30F5 0.85	807 0.50	EAF42 0.55	ECH84 0.45		0.45	PCF87 0.90	2.25	UCL82 0.35
5U4G	0.75	6BR8 0.70	6K25 0.75	12AU6 0.35	30FL1 0.75 30FL12 1.20	813 3.75	EBC33 0.50	ECL80 0.45		0.60	PCF801 0.50	QQV03-10	UCL83 0.60
	0.45	6BW6 0.85	6K25 0.75 6L6GT 0.45	12AU7 0.30	30FL12 1.20	866A 0.75 5642 0.70	EBC41 0.55 EBC81 0.30	ECL81 0.50		0.85	PCF802 0.50	1.25	UF9 0.60
	0.40	6BW7 0.80	6L7 0.40	12AV6 0.40 12AV7 0.65	30L1 0.40	6080 1.60	EBF80 0.40	ECL82 0.85 ECL83 0.70		1.00	PCF805 0.80	QQV03-20A	UF11 0-50
523	0.80	6BX6 0.25	6L18 0.45	12AX7 0.30	30L15 0.85	6146 1.60	EBF83 0.40	ECL83 0.70		0.70	PCF806 0.70	5.25	UF41 0.60
	0.40	6BZ6 0.40	6LD20 0.50	12AY7 0.75	30L17 0.80	6360 1.25	EBF89 0.30	ECL85 0.55		0.88	PCF808 0.85	QQV06-40 A	UF42 0.60
	0.80	6C4 0.33	6N7GT 0.45	12B4A 0.60	30P12 0.80	6939 2.25	EC53 0.50	ECL86 0.40		0.40	PCH2000.70 PCL81 0.50	TT21 8.00	UF43 0.60 UF80 0.85
	0.35	6C5GT 0.40	6P1 0.60	12BA6 0.40	30P19 0.85	7199 0.80	EC86 0.80	ECLL800		0.40	PCL82 0.35	TT22 8.20	UF85 0.40
6AF4A		6CB6 0.35	6P28 0.65	12BA7 0.40	30PL1 0.75	7360 2,00	EC88 0.60	1.65		0.55	PCL83 0.65	TY2-125	UF89 0.40
	0.22	6CD6GA1.25	6Q7 0.40	12BE6 0.40	30PL13 0.93	7586 1.25	EC90 0.38	EF40 0.50		0.40	PCL84 0.45	10.00	UL41 0.65
	0.40	6CG7 0.55	68A7 0.40	12BH7 0.45	30PL14 0.90	7895 1.25	EC91 0.60	EF41 0.65		0.48	PCL85 0.40	U18/20 0.75	UL84 0.40
	0.50	6CH6 0.60	68G7 0.40	12BY7 0.60	35 A3 0.55	9002 0.40	EC92 0.35	EF42 0.70	EY88	0.43	PCL86 0.45	U25 0.80	UM84 0.25
	0.30	6CL6 0.55	68K7 0.40	12K5 0.70	35 A 5 0.75	9003 0.50	EC93 0.65	EF80 0.25		0.50	PCL88 0.90	U26 0.80	UU8 0.60
	0.35	6CW4 0.65 6CY5 0.45	68L7GT0.35 68N7GT0.35	12K7GT0.40 12Q7GT0.40	35B5 0.65 35C5 0.50	AZ1 0.55 AZ31 0.55	EC8010 2.25 ECC40 0.65	EF83 0.55 EF85 0.35		0.50	PCL800 0.93	U31 0.60	UYIN 0.50
	0.60	6CY7 0.70	68Q7 0.40	128R7 0.40	35D5 0.75	CBL1 0.90	ECC40 0.85	EF86 0.30		0.27	PCL801 0.75 PD500 1.80	U37 2.10 U52 0.35	UY11 1.00 UY41 0.48
G. K. Z. G		6D3 0.50	68R7 0.40	20D1 0.50	35L6GT 0.50	CBL31 1.00	ECC82 0.80	EF89 0.28		0.80	PF86 0.65	U76 0.85	UY82 0.50
	0.43	6DC6 0.80	6T8 0.35	20L1 1.10	35W4 0.85	CY31 0 35	ECC83 0.30	EF91 0.38		0.40	PF818 0.85	U78 0.35	UY85 0.40
	0.20	6DK6 0.50	6U4GT 0.65	20P1 0.50	35Z3 0.70	DAF96 0.45	ECC84 0.30	EF92 0.35		0.35	PFL200 0.65	U191 0.75	W729 0.75
	0.35	6DQ6B 0.70	6U8A 0.40	20P4 1.10	35Z4G 0.35	DF96 0.45	ECC85 0.40	EF95 0.35	GZ32	0.48	PL33 0.85	U201 0.35	Z759 2.00
6AM6	0.33	6D84 0.75	6V6GT 0.40	20P5 1.20	35 Z5GT 0.60	DK 40 0.60	ECC88 0.40	EF97 0.65		0.70	PL36 0.55	U281 0.40	Z803U 1.20
	_									-			

	_	_	_			_
TO		8.2	0	100	-0	DC

		TR	ANSI	STO	RS	
	2N696	0.17	AC127	0.20	BD123	0.80
	2N697	0.17	AC128	0.15	BD131	0.85
	2N698	0.30	AC132	0.35	BD132	0.85
	2N705	0.70	ACI53	0.20	BF115	0.20
	2N706 2N708	0.10	AC154 AC157	0.13	BF167 BF173	0.18
	2N753	0.15	AC169	0.10	BF179	0.80
	2N929	0.22	AC176	0.25	BF180	0.85
	2N930	0.25	AC187	0.80	BF181	0.25
	2N987	0.30	ACI88	0.30	BF184	0.25
	2N1131	0.25	ACY17	0.275	BF185	0.20
	2N1132	0.25	ACY18	0.20	BF194	0.15
	2N1184 2N1301	1.25	ACY19 ACY20	0.25	BF195 BF196	0.15
	2N1302	0.75	ACY21	0.20	BF197	0.20
	2N1304	0.25	ACY22	0.15	BF200	0.35
	2N1305	0.25	AD140	0.50	BFW87	0.25
	2N1306	0.25	AD149	0.50	BFW88	0.23
	2N1307	0.30	AD161	0.35	BFW89	0.20
	2N1308	0.25	AD162 ADZ11	0.35	BFW91	0.20
	2N1309	0.30	ADZ12	1.25	BFX88 BFY17	0.25
	2N1613 2N1711	0.25	AF114	0.20	BFY19	0.60
	2N1756	0.75	AF115	0.20	BFY50	0.25
	2N2147	0.75	AF116	0.20	BFY51	0.20
	2N2160	0.65	AF117	0.20	BFY52	0.25
	2N2217	0.30	AF118	0.45	B8Y26	0.20
	2N2218	0.30	AF125	0.25	BSY27	0.20
	2N2219	0.85	AF127 AF180	0.20	BSY28	0.20
	2N2369A 2N2477	0.20	AF181	0.35	BSY65 BSY95A	0.20
	2N2646	0.60	AF186	0.40	OC16	0.50
	2N2905	0.35	AF239	0.40	OC22	0.50
	2N2923	0.15	AFZ11	0.45	OC23	0.60
	2N2924	0.15	A8Y26	0.25	OC24	0.60
	2N2926	0.125	A8Y27	0.30	OC25	0.35
	2N3053	0.25	A8Y28	0.25	OC26	0.25
	2N3054 2N3055	0.60	ASY29 ASY54	0.25	OC28	0.60
	2N3035 2N3133	0.30	A8Z15	0.70	OC29 OC30	0.60
	2N3134	0.80	ASZ16	0.70	OC35	0.50
	2N3391	0.20	A8Z17	0.75	OC36	0.60
	2N3392	0.15	ASZ18	0.75	OC42	0.20
	2N3393	0.15	A8Z20	0.25	OC44	0.20
	2N3394	0.15	ASZ21	0.40	OC45	0.15
	2N3395 2N3402	0.20 0.15	BC107 BC108	0.125 0.125	OC70 OC71	0.10 0.12
	2N3402	0.15	BC109	0.125	OC72	0.12
	2N3404	0.35	BC113	0.25	OC73	0.30
	2N3414	0.20	BC118	0.30	OC75	0.20
	2N3415	0.15	BC134	0.30	OC76	0.20
	2N3416	0.25	BC147	0.175	OC78	0.25
	2N3417	0.25	BC148	0.15	OC78D	0.20
	2N3702 2N3703	0.12	BC149 BC152	0.15 0.15	OC81	0.25
	2N3703	0.17	BC158	0.15	OC81 D OC83	0.15
	2N3707	0.15	BC175	0.20	OC139	0.30
	2N3709	0.12	BC186	0.25	OC140	0.35
	2N3710	0.12	BCY30	0.25	OC141	0.60
	2N3819	0.35	BCY31	0.40	OC170	0.25
	2N3906	0.20	BCY33	0.25	OC171	0.25
	28702 28746	0.50	BCY34	0.30	OC200	0.30
	28746 AC113	0.25	BCY72 BCZ10	0.20	OC202	0.65
	AC125	0.30	BCZ10	0.30		
	AC126	0.20	BD121	0.65		
i	-					

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3-in tube fitted with telescopic viewing hood, giving bright display in full daylight. Sensitivity 10mV/mm (narrow band) to 30mV/mm (wide band). Bandwidth 10 c/s=-10 mc/s. Triggered sweep pre-set at 1-2-5-10-30-100-300-100-3000 µsec per stroke. Free-tunning time base 20 c/s to 2000kc/s with built-in crystal calibrator providing timing marks at .05-.2-1-5-20-100 µsec + 5%. Amptitude calibrator directly calibrated in volts. Input attenuator 1-10-100. Power supplies 127/230v AC.

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TO72 outline TAA293. Medium frequency amplifier up to 600kc. Supply voltage 6V. output 10mW TO74	0.75
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GAS Light emitting dloge type MV10B	£1-05
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required to bulld a comple				£1.95
PHOTO-EMISSIV	E DEV	TCES		
GAS Light emitting dione type	MVI	0 B		£1-05
Photo-transistor OCP71				0.90
Photo-conductive cell ORP12				0.50
Photo-conductive cell ORP60				0.50
Photo-conductive cell ORP61				0.32
Photo conductive cell ORP90				1.10
Photo-conductive cell ORP91				1.10
GAS Photocells 90AG			N .	2.40
90CG	2.5		4000	2.40
Vacuum Photocells 90AV		2.0		2.50
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