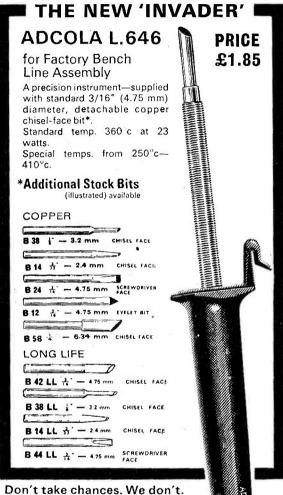
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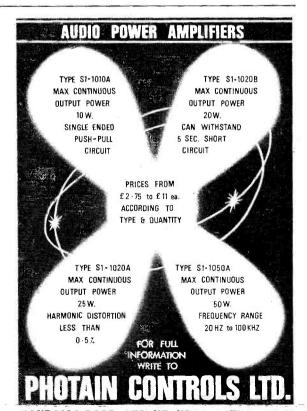
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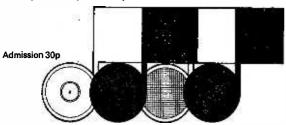


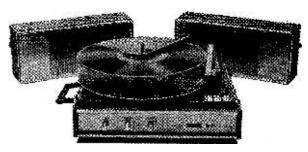
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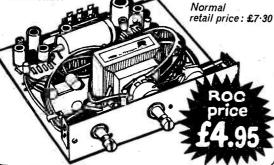


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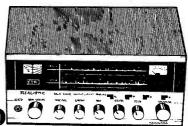
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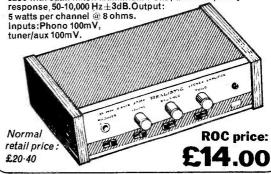
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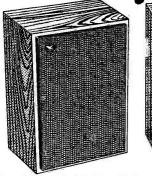
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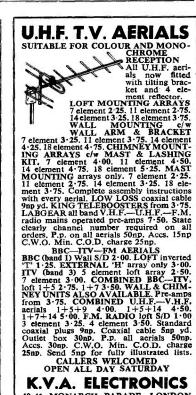
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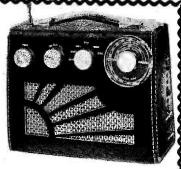
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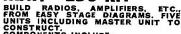
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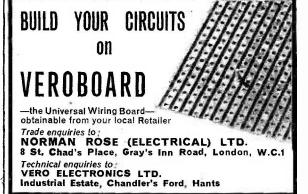
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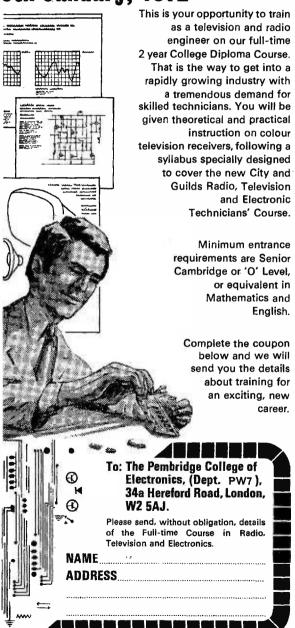
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High precision low-mass counterbalanced pick-up arm, heavy blanced turntable, simple to operate controls, viscous cueing device, slide in cartridge carrier, 4 pole

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MP. 60	11.20	15.50	19.00	19 - 25	22
HT.70	15.90	20.00	23.50	24.50	27
610	14 50	18 - 57	22 00	23.00	25
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SONY 8FC 59WA SCOOP

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Digital Alarm Clock Radio.
The digital clock shows you the time minute by minute with matchles accuracy and once set the Digital will wake you up at the same time every morning without having to be re-set. The radio section features Sony's unique sleep button, you fall gently to sleep lulled by the sweet tone of the radio, which switches itself off at a predetermined time. Available in either black or white. Frequency range 530-1,605/KHz (AM); 87-108MHz (FM). Uses 8 transistors and 8 semi-conductors, built-in ferrite aerial and 3fin loudspeaker. Power requirements: 230V AC 50Hz. Dimensions: (2½in x 3½in. x 5½in.

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KATONE AM/AIRCRAFT PORTABLE RADIO

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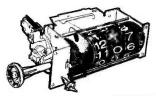
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A combined battery and mains portable of exceptionally attractive design. Housed in a leatherette covered case, size 8½in. x 5½in. x 3½in., fitted with an 8-section external telescopic aerial for FM and internal ferrite rod for MW wave bands, and clear easy-to-read dial with logging scale. Wave band coverage is FM 88-108MHz, AM 535-1,600KHz. A highly selective circuit using 9 transistors and 9 semi-conductors operating from either 4 x 1-5 volt torch batteries or direct from 230 volts 50Hz AC house mains, from a built-in mains unit. A socket is fitted for a personal earphone. Easy-to-use silver colour knobs, with "woodgrain" panel enhances the appearance of this fine radio.

LASKY'S PRICE 49.95 Post 15p



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EXCLUSIVELY FROM LASKY'S

for you to mount into any housing.
The clock measures 4% W x 1% H x 3% D (overall from front of drum to back of switch). SPEC.: 2101/240V a.c., 50Hz operation; switch rating 200, 3A. Complete with instructions, HUNDREDS OF APPLICATIONS. COMPLETE WITH KNOBS.

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Models HS-I and HS-2. Both these sets by TRIO offer really superb stereo reproduction in a lightweight, fully adjustable headset designed for optiadjustable headet designed for optimum comfet. Listening fatigue is unknown with headphones. Brief spec, both modes I flour imp. BQ nominal (matching is: Input imp. BQ nominal (matching is: Input imp. BQ nominal (matching is: Input imp. Sow); frequency response 20-19 kHz; output sensitivity may models are finished in ivory with contrasting foam filled ear pads and head band. LIST PRICE £8-40

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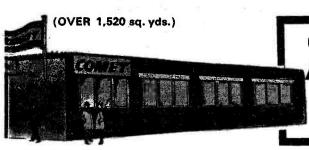
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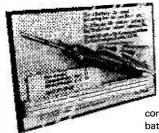
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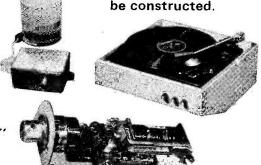
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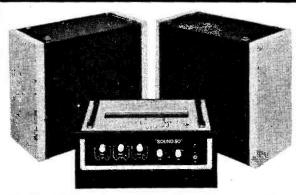
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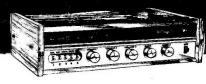
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PRACTICAL WIRELESS

VOL 47 NO 7

Issue 777

NOVEMBER 1971

Evolution of Audio

Thas been a long haul since the days when a pair of PX4's in push-pull represented the last word in "quality". Although the search for greater realism continues, and is reflected in the steady flow of improved products, the industry itself and its approach to marketing is undergoing fundamental changes.

For some years, hi-fi has revolved around a kind of cottage industry, the highest quality products coming from small, highly specialised companies. More recently, however, the big boys have been getting into the act. Generally speaking they had previously been unable to compete because mass production is incompatible with the "luxury trade" associated with products for the connoisseur.

Things, however, are changing. In the first place, the minnows are being swallowed by the whales so that high specification equipment can still be made but with the backing and resources of the bigger parent company. Secondly, hi-fi is now no longer the sole province of the more affluent and this has led to a huge market in so-called mid-fi—not the equipment for the more fastidious but representing a very fair sound at a reasonable price. And, thirdly, developing techniques and new devices such as ICs are making it more feasible to produce equipment of quality in greater quantity and within narrower tolerances.

But although there is now a vast selection of audio products to suit all pockets, there is a potential danger. The phenomenal boom in hi-fi is probably past its peak, although the industry as a whole continues to grow, and a slowing down seems to be inevitable. This will again put the pressure on reducing costs as the market cools down.

Largs of Holborn, a paradise for audio types, with a large auditorium and their famous £5,000 comparator, is already a casualty. David A. Larg says that a combination of overheads and competition from undercutting competitors "who offer neither the listening and demonstration facilities nor the installation advice and after sales service of Largs" have forced the company to close down.

The specialist dealer offering the kind of service and facilities expected by the discerning enthusiast is, of course, at a disadvantage when facing dealers offering discounted goods albeit with little service. But this is the trend and if manufacturers are also forced to keep their eyes more on the ledgers than the quality then customers are in for a leaner time.

Let us hope, therefore, that in its evolution, audio will not retreat from its present pinnacle and degenerate into the cheap-and-nasty take-it-or-leave it standards which have been the fate of other modern industries.

W. N. STEVENS-Editor.

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DECEMBER ISSUE WILL BE PUBLISHED ON NOVEMBER 5th

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NEWS... NEWS... NEWS...

Project 605

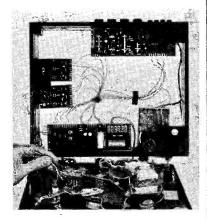
Sinclair Radionics Limited, announce the introduction of Project 605, a stereo system designed for the do-it-yourself enthusiast who does not have any special audio or electrical knowledge.

Based on four of the Sinclair Project 60 modules, Project 605 has an additional unit—Masterlink—through which all internal connections are routed by means of push-on tags already fitted to wires of the correct length—soldering is completely eliminated.

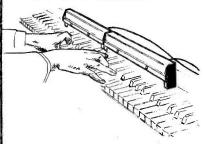
In the very comprehensive and extensively illustrated twelve page instruction book which is included in every Project 605 pack there are full details of tested installations in plinths of some of the major manufacturers of record players.

The Project 605 pack contains:
—two Z.30 power amplifiers; one
Stereo 60 pre-amplifier and control unit; one PZ5 power supply;
one Masterlink connector unit
with all necessary inter-connecting wires tagged at each end;
twelve page Instruction Book. The
suggested retail price is £29.95.

Project 605 and all other Sinclair products are available from retailers in all parts of the Country or direct from the Company. The guarantee which extends over two years is direct with Sinclair who perform all service and repair work in their own large Service Department. Sinclair Radionics Limited, London Road, St. Ives, Huntingdonshire, PE17 4HJ.



The PianoMate



This device transforms any piano, whatever its age or condition into four octaves of blending electronic chords.

There are two double octave units that are simply placed onto the back of the piano keyboard without any permanent fixing.

These keyboard units (A) are then plugged into the 'Master control Unit' (B) which in turn is plugged into a power socket.

A Tone Selector Switch provides three different tone colours which include a 'Flute' sound which is ideal for standard tunes or ballads. A second tone is that of a Church Organ, the third has a 'Jazz Band' sound which is suitable for Latin American or Pop Music.

A two speed Vibrato Control provides a further variation of tone colours.

There is a Level Control giving predominance to either the Bass or Treble keyboard unit.

An Input Socket is also provided for those wishing to plug in a microphone or other instrument, or to amplify the piano itself.

A further socket is provided for a foot volume or Waa Waa pedal.

The PianoMate is completely tuneable via a single control for pianos which may be out of pitch by as much as a semi-tone.

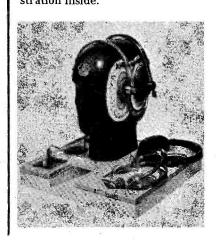
It is possible to play the Piano-Mate without a piano at all. One would do this by using a dummy or practice keyboard. This would provide all the electronic variations, without of course the blending qualities of the piano.

The price of the PianoMate complete with Foot Volume Control will be £69·00, and it will be in production January 1972. Dubreq Studios Limited, 249/289 Cricklewood Broadway, London NW2 6NX Tel: 01-450 5475.



A.K.G. Superhead

A.K.G. announce the introduction of their 'Superhead'. This is a novel demonstration unit which will be found at many A.K.G. retail stockists. It comprises a large life size black robot-like head with two faces, mounted on an orange coloured base. On this 'Superhead' unit are three or four different types of A.K.G. headphones which can be listened to instantly and judged for personal preference. This most unusual yet very helpful device will be found at dealers displaying an orange and black poster announcing that they have an A.K.G. 'Superhead' on demonstration inside.



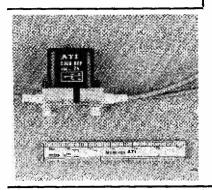
NEWS... NEWS... NEWS...

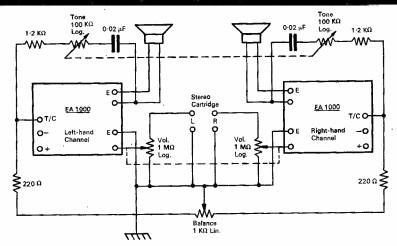
SGS Module

SGS have entered the module market for the first time with their EA1000 unit. A compact solid - state a u d i o amplifier assembled on a printed-circuit board, it is capable of delivering a minimum output power of 3W into a 16Ω load from a 24V supply.

The amplifier has been designed around the proven TAA621 monolithic silicon integrated circuit which contains all the active stages. The careful choice of associated components and of layout has given the unit considerable flexibility making it suitable for a wide range of applications at various supply voltages, load impedances and power outputs. Provision has also been made to alter the negative feedback and to vary the frequency response.

As a guide to obtaining the highest possible standards of performance from the EA1000 module, a 12 page handbook has been prepared which includes detailed information on its function, characteristics, and a number of applications. It includes a scheme for a stereophonic record player complete with volume, tone and balance controls. This publication immediately available, price 10p. SGS (United Kingdom) Ltd. Planar House, Walton Street, Aylesbury, Bucks.





A typical application of the EA1000 in a stereophonic record player.

Co-Axial Relays

McMurdo are extending their range of components, marketed under arrangement with Alliance Technique Industrielle of France, by the introduction of a miniature co-axial relay.

For frequencies up to 500MHz there are versions for PCB or chassis mounting. Three types are available—Type R has fixings, inputs and outputs on a 2.5 mm grid for PCB mounting. In Type RC the fixings and supply are PCB mounted whilst the h.f. circuits are fed via a co-axial cable.

For the chassis mounted version Type RCP (illustrated) the supply connections are by solder tags and those to the h.f. circuits by co-axial cable.

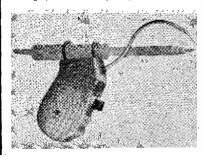
Supply voltage is either 12 or 24V d.c. at 1 Watt. The impedance is 50 ohms, VSWR is less than 1·15 and the cross talk at 300MHz is 45dB. Dimensions are length 26·8 mm (1·06in), height 24·8 mm (0·98in), width 10 mm (0·39 in). Further information from: McMurdo, Rodney Road, Portsmouth, PO4 8SG.

Solder Feed

Leaving one hand free to hold the job, Anextra Solder Feed fits the majority of soldering irons and carries up to 4oz. reels of flux cored solder. Saves time on soldering in production, construction and repairs.

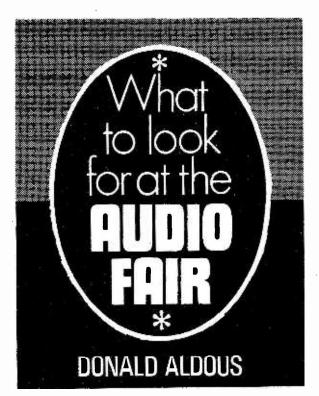
Injection moulded in tough, high impact polystyrene, with a life tested simple mechanism, easily reloaded, light weight, with comfort grip, suitable for right or left hand users, the Anextra provides an adjustable solder feed, for 22 to 18s.w.g. solder, which is fed onto the job.

Designed and made in England, the Anextra Solder Feed, with initial loz. reel of 60/40 cored 22s.w.g. solder, and detailed instructions is obtainable direct from the makers at £4·25, spare loz. reels at £0·25, post free, c.w.o. S.a.e. for leaflet, Anextra Ltd., Chiltern Works, Rear of 77/78 Chiltern View Road, Uxbridge, Middlesex, England.



International Audio Festival & Fair 1971

Come and visit us on stand 3 at Olympia, London, from October 26th to 30th.



ENTION of the title to this feature to a rather jaded audio trade friend evoked the reply "find the exit or the nearest bar!" Having been associated with audio fairs and like jamborees before there were any—if that isn't too paradoxical—I know what my friend meant. Tired feet allied to noise do not make for the best appreciation of high fidelity sound reproduction, which is presumably what such gatherings of the hi-fi clans should be all about.

Having made that point, I must go on to say that audiophiles with discerning eyes and ears can glean a lot of useful information about products to come. the latest technical developments in hi-fi, and by a discriminating choice of demonstrations to attend, gain a very helpful overall impression of what's happening in the home electronics entertainment world. Then after your visit to the 1971 International Audio Festival and Fair, Olympia, October 26 to 30th inclusive, 10 a.m. to 9.0 p.m. daily, admission 30p, go along to your local hi-fi dealer and have another session there or, if he will co-operate, have the equipment on test in your home. Reputable and well-organized hi-fi stores, many of which are members of the High Fidelity Dealers' Associationlook for the HFDA sign-have demonstration showrooms or theatres, and facilities for A-B direct comparisons of systems or components.

At the last count, which may well have been increased by the time you visit Olympia, 66 exhibitors have stands at this year's exhibition, excluding the consumer and trade papers' stands. And, of course, these exhibits cover many brand names of products manufactured, imported and distributed, so a representative cross section of the world's hi-fi equipment and accessories is on display and demonstration.

This is not all you get for your admission fee, as four times a day for five days, an impressive lecture/recital programme is presented in the specially built theatre. Speakers taking part include H. W. Hellyer

(Tape Troubles), Professor Tristram Cary (Musical Value of Synthesizers), J. L. Linsley Hood (Amplifiers), Loudspeakers (Dr. A. Bailey), W. Woyda (Tape Cassettes/Cartridges), A. C. Griffith (Record Rejuvenation), R. Auger (Multi-Channel Sound), Howard Souther (Headphones), and two panel sessions, one on 'Women and Hi-Fi', and under the title 'Feed-Back-Chat' a number of well known audio personalities will tackle technical questions from the floor. This occasion will be recorded on the spot by BBC Radio London, and broadcast in November on their 'Sounds Good' programme.

Under the umbrella title 'home electronics entertainment media'—this is the new term at present in vogue—audiovisual recording systems are coming more and more into prominence, with applications extending into many areas from education to industry. At least five systems are now being promoted—VCR (video-cassette), EVR (electronic video recording), VTR (videotape recording), Super-8 film, and the Teldec bildplatte (picture-disc) from AEG-Telefunken-Decca. A colour version of this last disc technique was recently demonstrated in Berlin, at the big international radio and TV show.

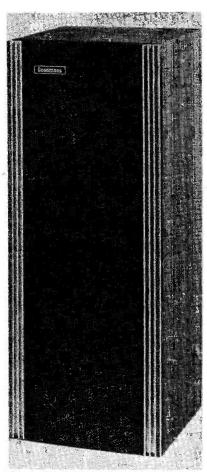
Whilst a few of the firms participating in the audio exhibition at Olympia have one or other of these systems, they are not really eligible for presentation at a strictly audio assembly.

So let's turn our attention to techniques and products that immediately concern the audio enthusiast. Topics that are the talking points for engineers and the knowledgeable public are quadraphonic sound systems, noise reduction methods, cassette and cartridge tape recorders, headphones, and that hardy perennial—loudspeakers.

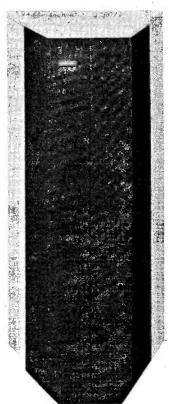
Starting with loudspeakers, the hundreds of models available in all shapes and sizes and prices do present a problem for the potential purchaser. The perfect loundspeaker does not exist and, although some families of transducers do have a 'household' sound—in most instances each system sounds a little different from the next and, so, ultimately, you must make your final choice by listening. The more experienced your ear is the better, naturally, and most audio purists would agree that regular ear purification by listening to 'live' music at concert halls is necessary to serve as a reference standard. A few audiophiles do exist still who tolerate the music to hear the equipment, but for the music loveraudiophile 'natural sound' is the goal for his domestic listening.

Home constructors will find several examples of D-I-Y loudspeaker enclosure kits at the show, ranging from Heathkit models to the latest Units 3, 4 and 5 from Wharfedale. Goodmans have now entered this field with their DIN 20 kit, as well as launching several new loudspeaker designs at Olympia.

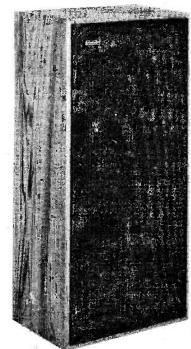
The two new bookcase models from Goodmans are both three-way systems, but here the similarity ceases. The DoubleMaxim is intended for those with limited space. The bass and middle registers are shared between two small cone l.f. units and an h.f. dome unit handles the higher frequencies. The system will accept up to 30 watts (DIN). By employing three drive units—a bass model, a new mid-range and an h.f. dome radiator—Goodmans' engineers claim the division of the frequency range in the Havant model ensures a balanced natural sound. The DoubleMaxim is an IB design and the Havant is a reflex, and both models meet the DIN standards



Goodmans Double Maxim speaker system.



Goodmans Dimension 8 bi-directional speakers.

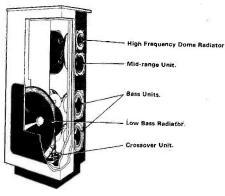


Rola Celestion Ditton 44 Monitor

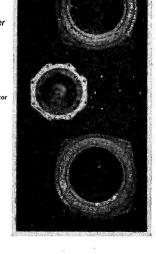
ALCOHOLD THE TOTAL

(right) B & O Beovox 4700 speaker enclosure.

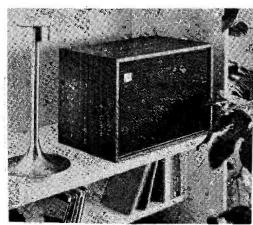




(above) Units and functions in a Dimension 8 enclosure.



(right) Wharfedale Denton 2 speaker for bookshelf mounting.



45:500 and 45:573.

The outstanding product in the new Goodmans' range is undoubtedly the Dimension-8 loudspeaker system. Described as bi-directional, to distinguish it from the traditional uni-directional and omnidirectional systems, the designers believe it to be the first system planned to meet the twin requirements for ideal stereo—namely, radiating direct sound over a large listening area for accurate stereo placing and providing a controlled amount of indirect sound for natural stereo ambience (reflection and reverberation).

This effect is achieved by having one set of four drive units vertically arranged on each side of the cabinet so that the inward facing drive units (of a stereo pair) radiate direct sound over an appreciable listening area, whilst the outward facing units give indirect sound reflected off the side walls of the room.

The design philosophy of the Dimension-8 embraces the 'small cone concept' with a number of units which are carefully selected to match and so complement each other's output. The 'small cone' approach simply means using small diameter units working within their range, so avoiding cone break-up distortion. Four bass units handle the considerable rated input power of 60 watts nominal, or 35 watts r.m.s. Two new mid-range units, two dome h.f. radiators, and a 12in. 'sympathetic' low bass resonator complete the assembly. The output of these nine units is integrated by a crossover network using eight close tolerance components. The interior volume is 40 litres and its weight is 44lbs. The crossover frequencies are 80.800 and 4.000Hz. Its frequency response covers 30 to 22,000Hz within ±5dB. Physical dimensions: $30^{3}_{8} \times 14 \times 12^{1}_{2}$ ins.

After a short period of listening to the Dimension-8s at the recent Berlin Radio and TV exhibition, I was impressed by their spacious and smooth sounding performance, so don't miss this demonstration at Olympia.

The radiation characteristics of loudspeakers are attracting interest lately, with the upsurge of enthusiasm by some designers-notably Stig Carlsson of Sweden-for an omni-directional pattern. The Sonab loudspeaker of this type disperses the sound in all directions so that all reflecting surfaces of a listening room are integrated, and the listening position for stereo sources is not critical, although room dependent to some extent. Yet another realisation of this concept are the omni-radial speakers from Sony. These have six acoustic-suspension drivers, and an individual dispersion dome over each cone distributes the highest frequencies evenly throughout a full 360° and from floor to ceiling. These speakers are housed in a barrel-shaped compound curved cabinet. Lastly, in this category of multi-directional loudspeakers, Arthur Radford, well known for his

amplifier and other loudspeaker designs, has created an unusual loudspeaker of special dispersion characteristics, which will be released shortly, I understand, by Radford Audio Ltd. of Bristol.

At this point, it must be mentioned that neither Sonab nor Radford is exhibiting at the Olympia audio exhibition, and Sony may not be showing their Omni-Radials, which have only lately come on to the market in Japan and in the USA. Sonab, however, did demonstrate their OA speaker range at the Northern Audio show in Harrogate in September. But enthusiasts will wish to know what developments are afoot in this controversial area of electro-acoustic transducer design.

Mention of kits, reminds me that Sinclair Radionics will show for the first time their new Project 605 at the Audio Fair, Olympia. Using modules, it is a novel extension of their popular Project 60 and sells for £29.95. The complete system can be assembled by any handyman without any soldering at all, as the printed circuit boards, etc. are all interconnected to inputs, outputs, through leads with push-fit tags. A fully illustrated instruction manual is supplied with the Project 605 system, which is certainly good value for outlay. The modules supplied include two Z.30 (15 watts r.m.s. per channel) power amplifiers, a pre-amp/control unit, and the PZ-5 power supply unit. (See "News...")

Audio fairs throughout the world seem to be using headsets as a practical means of reducing the bedlam of such conclaves and providing the audiophiles with a personal intimate sound demonstration. The latest designs of stereo headsets will be displayed and available for listening on the stands of such firms as AKG (75 on first floor), Dynatron Radio (47, first floor), Grundig (62, first floor), Sony (51 and 93), T. M. Distributors (Koss) on 68, first floor, and Wilmex (Stax), 24 on ground floor, where six pairs of 'phones will be fed from disc/tape signals.

Many other manufacturers will have earphones on show, and my advice is not to miss the demonstrations of the latest Koss electrostatic ESP-9 studio monitor headset, and the Japanese Stax SR-3 so-called Ear Speakers. The ESP-9 model costs £69 and the Stax headset, with its SRD-5 adaptor, retails at £45.40. Once you have become used to listening via a headset, which fits comfortably and is non-fatiguing even after an hour or so's wearing, the experience can only be described as a sonic delight. Fed from a good source, the sound quality is clinically clean and undistorted. If you consider solo listening is anti-social in the home, Koss and other manufacturers produce connector boxes to permit attaching two or more pairs of headphones! Koss also offer among their collection of accessories, a stereo/mono adaptor cable, which simply switches from stereo to mono reproduction, as required, on the particular headphones. By the way, highly acceptable performance

International Audio Festival & Fair 1971

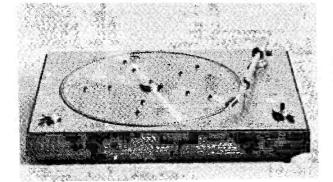
All the big names of the Hi-Fi industry will be there in strength and there will be nearly 100 specially constructed audio studios where one can hear and compare sophisticated equipment spanning the whole price spectrum.

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Buses passing Olympia are 9, 27, 28, 49, 73. Green Line coaches are 701, 702, 704, 716. Underground train to Kensington, Olympia.

BEING HELD AT OLYMPIA, LONDON, OCTOBER 26-30 IS OPEN FROM 10 A.M. TO 9 P.M.



B & O Beogram 1200 turntable on plinth.



New Sony PSE 4000 turntable.

(below) Akai X2000 SD which accepts open reel, 8-track cartridge and Philips' type cassettes.



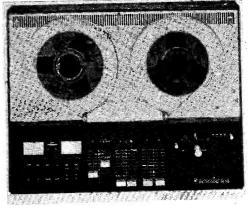


Goodmans Model 80 fitted with Goldring Lenco G800E and Module 80 stereo f.m. tuner/amplifier.

Philips N4450 recorder/amplifier with auto reverse.



Beocord 1600 4-track recorder.



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headphones are available for far less than the prices quoted of these 'state of the art' designs.

Peter Merrick, of Wilmex, tells me that there is a good chance that he will be able to show the latest Stax UA-7 pick-up arm, a sophisticated design, but it depends whether the samples from Japan reach our shores in time. Don't miss it, if it is on display. Before leaving headphones, we have just been told of the stereophonic 2-way, 4-speaker headphones, type DD1 from Wharfedale. These have dynamic elements, with separate bass and treble units, plus a crossover network, and a frequency response specified as from 16Hz to 22,000Hz but no tolerances given. Distortion less than 1 per cent and sensitivity (at 600Hz) is 100dB for 1mW input. Price: £11.

Wharfedale are showing, in addition to their well known Super 10/RS/DD, Super 8/RS/DD and 8in Bronze RS/DD units, their Dovedale 3 and Rosedale loudspeakers (both 3-unit systems) and the three Unit kits referred to earlier, will also introduce the Linton stereo amplifier (15+15 watts into 8 ohms) at 0·1 per cent distortion at all power levels up to 10 watts each channel driven at 1kHz into 8 ohm speakers, at £60. Another innovation from Wharfedale is the Linton 4-speed disc turtable, fitted with Shure M44-7 cartridge, and selling for £35, including PT. Rumble is quoted as better than 35dB and wow better than 0·2 per cent, with flutter down to less than 0·06 per cent.

One wag has observed that the cassette revolution is not red but fully coloured these days. However, we are not dealing with video-cassette systems here, but the audio cassette revolution does concern us. In about six years, the fuss-free cassette has made tape recording more popular than ever, with modest recorders available at reasonable prices and **Philips** report that since the launch of the portable cassette recorder some five years ago, more than 6 million units have been sold in Western Europe.

Philips are marketing their new Cassettophone battery model, type N2000, styled in green polystyrene and weighing only 2lbs. It has one central control for playing, rewinding and fast forward, plus sockets for the addition of a mains supply unit and an earphone. Price is £13. A mains stereo cassette deck, N2503, is also now released from Philips. This design has one neat sliding control for setting the recording level and a 3-digit counter to give tape position. Another feature is that the motor stops automatically at the end of each cassette. This model sells for £52·05.

What might be called the 'home studio class' has been catered for in another new model from the Philips organization. Known as Model N4450, it is a 3-speed quarter-track recorder for vertical or horizontal operation with automatic and manual reverse. This facility means that the direction of the tape transport can be reversed at will or at the end of the tape, when it will automatically play in the other direction. The machine can accept up to $10^1{}_2$ in reels and the built-in stereo amplifier develops 2×25 watts, and can be employed as a straight amplifier, with the motors and transport switched off.

Features in this advanced design include six heads, levers for cueing during fast forward and rewind, a tape tension comparator for constant winding torque, and a synchronous clock with built-in timing device for starting and stopping the recorder at any predetermined time. Following a trend, the volume, balance and treble/bass tone controls are

sliding potentiometers. Having played with an advance model of this N4450 I can vouch for its flexibility, and so don't miss examining this machine. It costs £280, including PT and will not be available till November.

We learn that Philips are engaged in producing hi-fi cassette machines, due for release in 1972, and this vast organization will take the initiative in proposing standards for this category of hi-fi cassette machine, but the standards will be reached—so they say—that the advantages of compact cassette systems, namely compatability and ease of operation, will not be affected. Be it noted, however, that the prices of these models will be higher than existing equipment! These developments have been made possible by the release of tapes with high coercivity and improved magnetic heads on commercial recorders.

If you are a tape recordist, you will make special visits to the stands of Agfa-Gevaert, BASF, 3Ms (Scotch) to find out about the latest chrome-dioxide tapes now manufactured by these companies. These are low noise tapes and the BASF cassettes have a new form of internal construction for even more reliable foolproof operation.

It will be evident now that this preview is highly selective, and, of course, cassette tape models (including new radio-recorders, with built-in radio tuners) incorporating various refinements can be seen on stands other than those mentioned. For example, Sony have several outstanding designs, as has Sanyo, Grundig, Akai, Sharp, National Panasonic, not forgetting the **Revox** open-reel tape machines.

Uher (Bosch) have a real innovation for them in their latest Compact Report Stereo 124 model, a mono-stereo cassette machine, which will accept Philips' type cassettes, work from all power sources, and has a built-in capacitor microphone, auto-reverse, remote controls and a power output of 1·3 watts r.m.s. per channel.

So we come to the noise bugaboo. Reams have been written about the brilliantly conceived Dolby noise reduction system, which in its professional A-type is widely used by all the major recording companies of the world, resulting in quieter surface commercial pressings. A simplified B-type Dolby system designed for home tape recorders is now available and used by more than 30 manufacturers of hi-fi equipment. Hundreds of cassettes processed for domestic playback with units having the Dolby system are already available from such firms as Columbia (USA), RCA (UK), Decca/London, Ampex Stereo Tapes (USA), Pye Precision Tapes, and others.

The Dolby technique works in two stages. During recording, the Dolby circuit automatically analyses the sounds of the music and makes appropriate changes in the level of the programme. The same circuit, operating in reverse, removes these changes during replay, and with them most of the intrusive noise produced by the tape. For the first time Ferrograph, that much respected name in the tape recorder world, has launched one of their machines incorporating Dolby B circuitry, which must not be overlooked at the show. Cassette machines fitted with Dolby noise-reduction circuit include Harman-Kardon (Highgate Acoustics), a Rank-Wharfedale model, and Bell & Howell also market such a unit.

Although it will not be seen in a production model, so far as I know, at Olympia, Philips have developed

-continued on page 589

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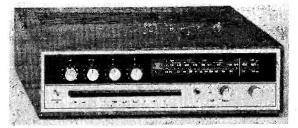
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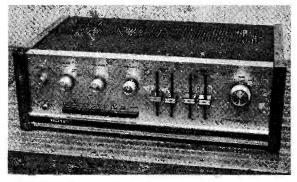
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WHAT TO LOOK FOR AT THE AUDIO FAIR

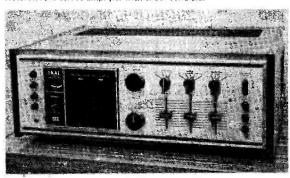
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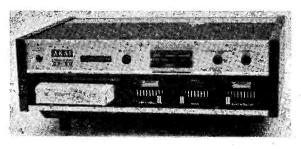
Armstrong 526 a.m./f.m. stereo tuner/amplifier.



Rotel RA 610 stereo amplifier with slider controls.

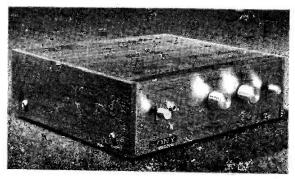


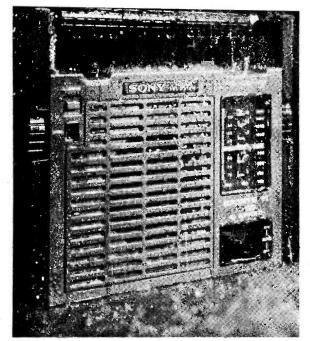
Akai a.m./f.m. solid state stereo receiver AA 8500.



Akai CR 80 8-track cartridge record and player.

(below) Sony SQD-1000 Quadphonic Decoder.

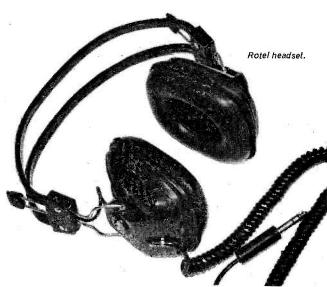




Sony Sports 11 waterproof portable.



Stax electrostatic headset SR3/SRD5 "ear speakers".



WHAT TO LOOK FOR AT THE AUDIO FAIR —continued

their DNL circuitry (which means Dynamic Noise Limiter) as an alternative system to the Dolby method. It operates as a steep low-pass filter in the absence of high signal frequencies, and it is tripped by high frequencies only, in such a way that the presence of high frequency signals above a certain level will by pass the filter action. It is claimed that unweighted measurements show an S/N ratio improvement of more than 10dB at 6kHz and 20dB at 10kHz. A prototype Philips cassette recorder with the DNL circuit incorporated was shown at Berlin, which has push buttons ready for all types of tape, from the newer chrome grades to standard hi-fi formulations. Perhaps next year production models will be available, but the news of this development indicates the importance attached to noise reduction systems for upgrading domestic sound recorders.

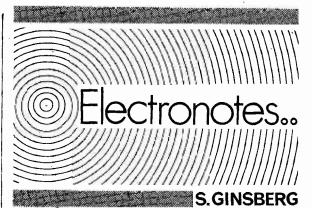
Denham & Morley's stand 65 (on first floor) will display and demonstrate JVC-Nivico equipment, and among this range is their ANRS circuit, meaning Automatic Noise Reduction System, another technique that seems to bear some resemblance to the

Dolby method.

A lot of money and effort is being spent developing and promoting spatial sound systems, which are being given such names as quadraphonic, quadrasonic, surround sound, tetrahedral sound, even multisound, and some of the competing 4-channel systems for the home environment include Sansui, E-V (Electro-voice), JVC-Nivico, Dyna (Hafler) and the CBS.SQ technique. In the last instance, Sony is manufacturing the hardware for reproducing these SO (meaning stereo quadraphonic) discs. Benjamin Bauer (Vice President, CBS Laboratories), who led the team responsible for the system, has given some most impressive demonstrations of the method on the Continent and in London, at a recent Audio Engineering Society meeting. A specially prepared sampler LP, with David Frost as narrator, was used for this purpose, and it is promised that about 50 SO processed discs will be produced in the coming months, so providing the needed software.

At the time of writing, no details are available of any company participating in the Audio Fair here that will be demonstrating a 4-channel disc system, although multi-channel tape systems will undoubtedly be heard. Propagandists for quadraphonic sound which recreates sound from four different source points, permitting a 360° sound perception, regard the technique as the most important advance in hi-fi sound recording since the advent of the stereo disc. This is not a universally held viewpoint, and some critics consider it rather gimmicky at this stage, offering all-round sound at the price of maximum fidelity for a given outlay. No standards exist yet, and only time will show which system will win, if at all in the UK, where the extra cost of decoder, amplifier and loudspeakers, linked to limited room size and problems of siting additional loudspeakers, may weigh more heavily than technical advances.

Lastly, BSR will show their attractive transcription hi-fi record playing deck, BSR McDonald 810 with many refinements, including push button control, and I hear that our old faithful Quad electrostatic loud-speaker will now be available in black finish, as an alternative to the long familiar bronze. Leak, too, have a new series of Delta equipment, including amplifiers, speakers, turntables, and a.m. f.m. tuner.



POWER supplies have long followed fairly standard rules. In the days of the valve, it resolved itself to a mains transformer, rectifier(s) and some form of smoothing, usually comparatively high value capacitors and a fairly hefty iron-cored choke.

With the advent of the transistor, much the same rules applied, except that whereas before it was a case of high voltage and low current the reverse was true. This was particularly so in the case of industrial applications such as computers. In many forms of instrumentation today, many logic chips are employed, all requiring some 5V and, since there can be many, needing quite a few amps of current.

An improvement came with active regulation, the use of large transistors as series regulators with some form of feedback sensing circuit to control variations

in the final supply to within certain limits.

A snag is that the power supply has become, in many instances, the largest part of the equipment—and the heaviest. The two major offenders in space and weight considerations are the mains transformer and the series regulator heat sinks. In a series regulator, the total current passes through the device which also has a voltage dropped across it. This means heat, mainly because of inefficiency, and thus the heat sinks become vital to get rid of the heat and prevent the regulators from overheatining and becoming ruined.

A new technique has now been launched which gets rid of both the big 50Hz mains transformer and the heat sinks all in one go. It uses switching techniques. The mains is taken and rectified. It is then applied to an inverter which is a form of oscillator using semiconductors. The oscillator has a working frequency of between 20 and 40kHz. The output is fed to a small ferrite torroid transformer and the output rectified by Schottky barrier diodes in a full wave rectifier circuit. The Schottky diodes have barely one third the voltage drop across them compared to conventional high-speed silicon rectifiers and they do not have the problems of reverse recovery. This means very much smaller heat sinks.

A 5V 20A unit, using these techniques, is so small it can be easily stood on the palm of one's hand. The power packing density, just for the mathematicians, works out at around 0.75in.3/W. Using conventional techniques to build a similarly rated unit would mean that the 50Hz mains transformer alone would be both bigger and heavier, than the whole power supply using switching techniques. Because the switching frequency is high (compared to 50Hz) and because it is effectively doubled by using full wave rectification, the smoothing components can be made extremely small.

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S a "one off" project, the simple electronic organ described here is not a difficult one and actually involves more carpentry than electronics. Moreover, a half scale version of the real thing has tremendous appeal to young children and if you have junior members in the family, there could be a large demand for a project of this type. The prototype, shown on the front cover, was in fact patterned on a full size electronic organ and is approximately a half scale version.

The circuit employs only four transistors and it comprises a multi-vibrator tone generator, a vibrato oscillator and an amplifier stage providing quite a reasonable output. The organ has a two octave keyboard with a range from F at 174.6Hz to F at 698 · 4Hz. The vibrato can be switched on or off and there is a choice of two 'voices', one being slightly reedy and the other a softer flute-like sound. There is also an "expression" pedal which, although mechanical, provides the young player with some control over loudness. The organ uses a standard 9V battery from which the total current drain is about 20mA.

THE ELECTRONICS

The circuit for the tone generator, vibrato oscillator and amplifier is shown in Fig. 1. Tr1 is a phase shift oscillator and runs at about 6 to 8Hz, the output from the junction of C2/R1 being taken to the base of Tr2 which is one half of the multi-vibrator tone generator. The output from Tr2/Tr3 is a typical multi-vibrator waveform and the frequency range is governed by the series connected 10kΩ preset potentiometers marked F1, F#2, G3 etc., between the base of Tr3 and the negative supply rail. The $50k\Omega$ pre-set, PR1, is for adjustment of initial pitch. The output from Tr2/Tr3 is taken directly to the amplifier-cumtone forming circuit, Tr4, and with a 25-400 small loudspeaker the nominal output is about 0.5W. The voicing is a very simple arrangement by means of

* components list

	eres to the		A STATE OF THE STA	and the second
Resisto				
RI	8 2kQ	R8	3-9kΩ	
R2	8-2kΩ	R9	4-7kΩ	
	8-2kΩ	R10	18kΩ	4.0
R4	1-5kΩ	R11	6 8kΩ	
R5	-5 6kΩ	R12's	56Ω	
R6	2·7kΩ	R13	58kΩ	4.3=0
R7 /**	≈47kΩ			
Allto	r &W/10% to	/pes	1977	
100	77			2926
Capacit		SALAR	O.OF.E	13.50
C1	250μF	C6	0·05μF 0·01μF	
C2	1.5uF	C7 C8	10µF	
- C3	1.5µF	Č	0-14F	$r_{i,j}(T_i)$
C5	1·5μF 400μF	C10	0.47µF	
		least 10V wor		
	cirotytics ac			
Semico	nductors			
ATH W	OC7L or NK	T213 Tr3	OC71 or NK	T213
Tr2	OC71 or NK	T218 T/4	OC81	
Miscella		the section of	DECEMBER 1	
		skeleton po	te miniative	type
4 AFE	WO preset el	eleton pot, in	Injeture tyne	small
louden	eaker rour	d or eliptic	al 25-400:	2-off
ewitch	es niess on	off types; or	off toogle	witch.
2111.011				4

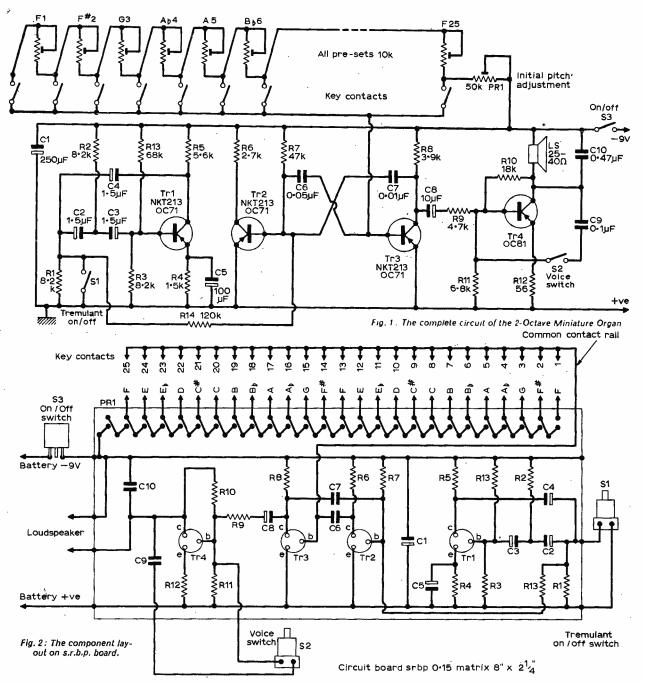
* materials list

Plywood and hardboard to sizes in diagrams. \(\frac{1}{2}\) x \(\frac{1}{2}\) p planed batten for keys, approx. 9ft.

Felt or foam plastic \(\frac{1}{2}\) to \(\frac{1}{2}\) in wide approx. 20in.

\(\frac{1}{2}\) x \(\frac{1}{2}\) aluminium angle, 10in.

16s.w.g. aluminium for brackets. Thin countersunk head woodscrews for key springs and contact guides. 75 off. (these should not be more than in long) Material for main front panel (speaker pull material). Sundry screws and give. Tagstrip, 9in long. Gold clad wire (organ contact wire) 6ft (Henry's Radio Limited): Light tension springs approx. In long. 25 off.



negative feedback and gives two voices, one with a 'reed' sound and the other a 'flute' sound.

All the components, including the 25 miniature pre-sets, can be mounted on a piece of plain Veroboard 8 x 2^1 4in. which is secured to the key baseboard with a short strip of 3 8 x 3 8in. aluminium angle or a small bracket either end. The component layout and wiring for the circuit board is shown in Fig. 2.

CONSTRUCTION

The various diagrams show the dimensions used for the original, but these can be varied so long as similar space is provided for the keyboard and the electronics. A supply of assorted sizes of woodscrews and some glue are required for assembly and these, together with the pieces of plywood, hardboard and planed batten etc., should be readily available from timber merchants or d.i.y. shops.

The main case should be built first, as shown in Fig. 3 and assembled complete with the inside shelf (for the keyboard etc.) and the rail at the rear on which the lid is hinged. The batten under the front edge of the inside shelf is used to support the upper front panel. An inside speaker baffle is necessary if the expression pedal feature is to be incorporated, otherwise the speaker can be mounted directly on the main front panel. In this case the speaker opening will be appropriate to the loudspeaker used and the cut out for the expression pedal will not be required.

The expression pedal is a simple mechanical

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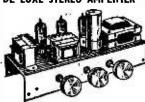
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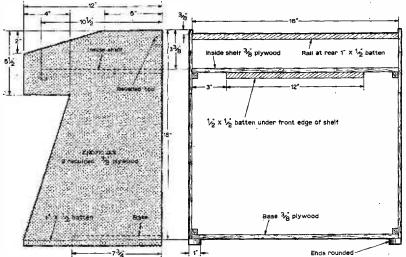


Fig. 3: Cutting dimensions for the main cabinet.

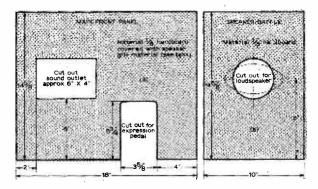


Fig. 4: Cutting details of the main front panel and speaker baffle.

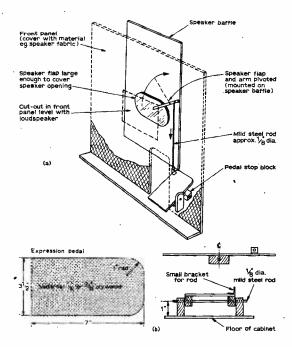


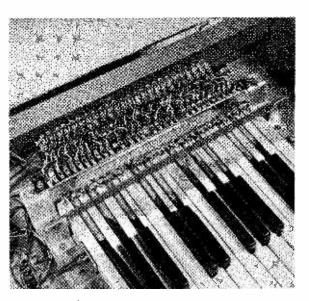
Fig. 5: Arrangement of the expression pedal.

arrangement that lifts a flap over the loudspeaker when the pedal is pressed downward. Although this only provides a small degree of change in loudness it is worthwhile including as it does at least simulate the use of an expression pedal. The general mechanical arrangement used for the prototype is shown in Fig. 5a. As the size of the speaker flap and the length of the arm attached to it may depend somewhat on the shape and size of the loudspeaker, no detailed dimensions have been given. All that is necessary however, is to ensure that the flap over the loudspeaker moves upward and clear of the speaker opening in the direction shown

when the pedal is pressed downward. The arm on the flap, the position of the pivot and the length of the operating rod should be adjusted so that the flap just covers the speaker opening when the pedal is lifted. The position of the pedal stop block will help facilitate the correct amount of pedal movement.

THE KEYBOARD

This is the most difficult part because normally piano keyboards are cut from one piece so that they fit together precisely when reassembled on the frame. The keys for the children's electronic organ are slightly larger than half scale and are made separately. The general layout of the keyboard and the size of the white and black keys is shown in Fig. 6. The base is made from ³8 in. thick plywood and the 'frame' consists of two end brackets and a length of ³16 in. dia. mild steel rod. The best procedure is first to make the baseboard and the two end brackets (see Fig. 7b) and secure the left hand bracket in position as in Fig. 6. The spacers between each key are single turns of 22 s.w.g. wire, or if you



The completed keyboard of the prototype. The contact wires and the presets can be seen.

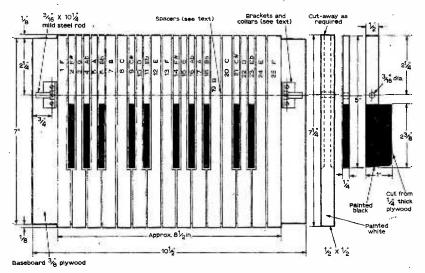


Fig. 6: Plan view of the keyboard with key dimensions given on the right.

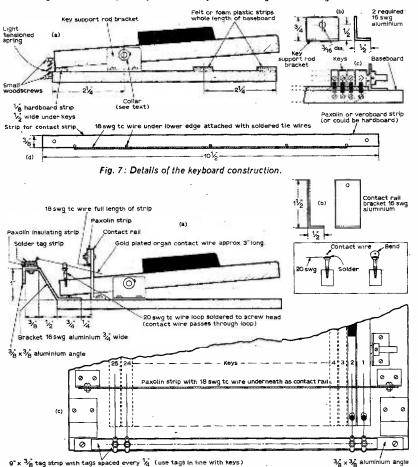


Fig. 8: Arrangement of the keying contacts—see text for explanation.

can get them, 3 ₁₆in. washers of similar thickness e.g. 1 ₂₉in. It will be seen from Fig. 6 that the cut-away portions on each of the white keys varies according to its position. For instance, key No. 1 is cut-away only on one side to fit with the black key No. 2. Key No. 3 and also keys 5, 10, 15, 17 and 22 have cut-aways on both sides. Keys No. 8, 13 and 20 are similar

to No. 1 with the right hand side only cut-away whilst keys No. 7, 12, 19 and 24 have only the left-hand side cut-away. The remaining key No. 25 has no cut-away.

First the 10¹4in. long mild steel rod should be ready to take the keys. Then make up the first half dozen keys, black and white, from No. 1 to No. 6. Cut and file the cut-away portions of the white keys until each fits snugly with its associated black key. Then proceed on the same lines until all the keys are made and fitted and, most important, numbered and marked as in Fig. 6.

Temporarily fit the remaining end bracket and ensure that the keys move up and down freely on the rod. They can now be removed and painted. Before re-fitting the keys secure the strip of hardboard along the rear of the key baseboard and the strips of felt under the keys as shown in Fig. 7a. When the keys have been re-assembled the rod can be secured with small brass collars each end as in Fig. 6 and 7a. Meccano collars were used originally but could be made quite easily from 38in. dia. brass rod. Before fitting the tension springs as in Fig. 7a, make sure that each key moves freely up and down. The springs, which must not be too highly tensioned, are secured by small woodscrews as shown in Fig. 7c. When the springs have been fitted, make sure that each key moves freely downward with a light touch and returns to its upward position.

KEYING CONTACTS

The keying contact system is a simple but effective one and the general assembly details for this are given in Fig. 8. The main contact rail as shown in Fig. 7d consists of a strip of insulating material such as paxolin (or hardboard would do) to which is secured a length of 18 s.w.g. tinned copper wire. This strip is fitted over the keys as in Fig. 8a by means of two brackets

(Fig. 8b). The gold wire contacts, one for each key, are fitted as shown in Fig. 8 to a solder tag strip mounted on a length of ³₆in. aluminium angle which is secured on two brackets projecting over the end of the baseboard as in Fig. 8a. Before fitting this assembly to the baseboard, small countersunk woodscrews are fitted one to each key and about

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2N697	18p	2N2925	22p	AC126	20p	BC154	20p	BFY51	20p
2N706	12p	2N2926	11p	AC127	20p	BC157	12p	BFY52	28p
2N930	29p	2N3053	27p	AC128	20p	BC158	11p	BSX 20	16p
2N1131	29p	2N3055	60p	AC153K	22p	BC159	12p	C407	17p
2N132	29p	2N3702	13p	AC176	16p	BC167	11p	MC140	25p
2N1302	19p	2N3703	13p	ACY20	20p	BC168	10p	MP86531	35p
2N1308	19p	2N3704	13p	ACY22	16p	BC169	11p	MPS6534	30p
2N1304	26p	2N3705	13p	AD140	63p	BC177	14p	NKT211	25p
2N1305	26p	2N3706	13p	AD142	50p	BC178	13p	NKT212	25p
2N1306	33p	2N3707	13p	AD149	58p	BC179	14p	NKT214	23p
2N1307	33p	2N3708	10p	AD161	83p	BC182L	11p	NKT274	18p
2N1308	36p	2N3709	11p	AD162	36p	BC183L	10p	NKT403	65p
2N1309	36p	2N3710	13p	AF114	24p	BC184L	11p	NKT405	79p
2N1613	23p	2N3711	13p	AF115	24p	BC212L	16p	OC71	38p
2N1711	26p	2N3819	23p	AF117	22p	BC213L	16p	OC81	25p
2N1893	54p	2N3904	35p	AF124	24p	BC214L	16p	OC81D	25p
2N2147	95p	2N3906	35p	AF127	22p	BCY70	18p	ZTX 300	14p
2N2218	34p	2N4058	13p	AF139	33p	BCY71	83p	ZTX301	16p
2N2218A	44p	2N4059	10p	AF239	36p	BCY72	15p	ZTX302	22p
2N2219	38p	2N4060	11p	ASY26	27p	BF115	23p	ZTX 303	22p
2N2219A	53p	2N4061	11p	ASY28	27p	BF167	18p	ZTX304	27p
2N2270	62p	2N4062	12p	BC107	12p	BF173	19p	ZTX 500	18p
2N2369A	19p	2N4124	18p	BC108	11p	BF194	14p	ZTX501	21p
2N2483	35p	2N4126	27p	BC109	12p	BF195	15p	ZTX 502	25p
2N2484	42p	2N4284	15p	BC125	15p	BFX29	31p	ZTX 503	22p
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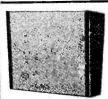


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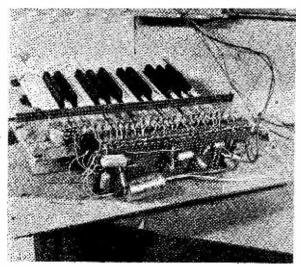
P.W. COMMUNICATIONS RECEIVER

(P.W. DEC. '70-FEB. '71)

Was built entirely from parts supplied by us. 2nd Convertor/I.F. kit..... £7.90 Product Det. (with vol. control) £2.90 £1.80 Audio Amp £5.50 Pre-Sel./1st Con. Power Supply ... COMPLETE KIT all of above plus sub chassis material (formed tinplate) and F/T caps £20-00 P.W. F.M. TUNER (Feb.-Mar. '69) COMPLETE KIT inc. drilled chassis, scale etc. £8.20 P.W. STEREO DECODER (June '70) £4.80 COMPLETE KIT inc. chassis Post and Packing per order, 15p

C & D ELECTRONICS 1, Neville Road, St. Lukes Cross, Sunderland ³gin. back from the rear end of the key. Solder about ¹2in. to ³4in. of 20 to 22 s.w.g. tinned copper wire to each screw head as in the inset in Fig. 8. These wires are wrapped loosely around the gold contact wires when the contact frame is finally placed in position.

The final stage of the keying assembly is to ensure that when the keys are at rest, the gold contact



A rear view of the keyboard showing the component board fixed in place

wires are each about 18 in. clear of the main contact rail but do not touch the keys themselves. Check each contact with a continuity meter. The finished keyboard is shown in the photograph.

TO BE CONTINUED

P.W. at the Fair

The 2-Octave Miniature Organ, described above, will be just one of the constructional projects which can be seen at the International Audio and Music Fair which is to be held at Olympia, London, from October 26th to 30th.

This year Practical Wireless and Television will be showing more projects than ever before and there will often be someone from the technical staff to explain and answer questions.

Among the items that we are planning to show are the Digital Frequency Counter/Timer, The Modular Audio Mixer, The P.W. Treasure Tracer, The P.W. Workshop Oscilloscope as well as many other constructional projects.

P.W. is your magazine and we shall be at your service at Olympia on the dates mentioned. Be sure to visit us on Stand 3—right by the main entrance.

PRACTICAL WIRELESS AND TELEVISION STAND 3

INTERNATIONAL AUDIO AND MUSIC FAIR OLYMPIA, LONDON OCTOBER 26th—30th

10 a.m. to 9 p.m.

(Press preview and Trade day Oct. 25th)

lium e Column

AMADAM starts on the 21st October this year and lasts until the 19th November. During this period Arabic speaking stations will be on extended schedule, many remaining on the air all night. From 2200hrs GMT onwards, listen for Algiers on 980kHz and 890kHz; Tunis on 962kHz and 629kHz; Libya with El Beida on 1123kHz and Tripoli on 1250kHz; Tangiers on 1232kHz; Batra Egypt on 620kHz. Among the less conspicuous are Riyadh, Saudi Arabia, 588kHz; Aleppo, Syria, 647; Bagdad, 760 (also on 908 after BBC4 closes down); Beirut, Lebanon, 876; Omdurman, Sudan, 960; Diyabakir, Turkey, 1061; Tel Aviv, Israel, (in Arabic) 1286; Teheran, Iran, 1325; Kuwait, 1345; Ahwaz, Iran, 1390.

M. Noctor of South Norwood has had difficulty using his MW loop aerial with a transistor portable. A loop should not be connected to a receiver that has an interial aerial as the latter will mask the 'null' of the loop. Dr. H. S. Brodribb of St Leonardson-Sea has solved this problem by mounting the receiver *inside* the loop so that the two rotate together. Coupling is between the turns of the loop and the windings on the ferrite rod inside the receiver and care should be taken that the nulls of both the loop and receiver are pointing in the same direction.

Medium Wave DXers will welcome the return of GMT this winter. Many European stations will close down at 2300hrs, clearing the band for North American DX before midnight. Paris 1070kHz signs off at 2300hrs GMT and, if the North American path is open, the 50kW Canadian at Moncton, New Brunswick, also on 1070kHz, should be audible after the Paris carrier is switched off. This station is a main outlet of the Canadian Broadcasting Corporation; it belongs to the "CBC Radio Network" and identifies on the hour and the half hour with the call letters CBA. Other Canadians that can be heard before midnight are CHER in Sydney, Nova Scotia, on 950kHz and CJON, St. John's, Newfoundland, on 930kHz. As midnight approaches look for WINS, 1010kHz, the all-news station in New York City; WNEW, 1130kHz, also in NYC; WBZ 1030kHz in Boston and WHN 1050kHz, NYC (After BBC4 signs

Newcomers to the medium waves are sometimes disappointed if North America is not heard at the first attempt. Propagation on this path is variable, with occasional fadeouts that last several days, so if you are unsuccessful the first time, try again a few days later. On a good night, many trans-atlantic stations peak-up by 0100hrs GMT. They can be logged on any communications receiver that covers the medium waves (the writer uses a CR100).

All reports and information concerning Medium Wave DXing should be sent to me at 132 Segars Lane, Southport PR8 3JG.

T REASURE RACED

T the end of the article describing the P.W. Treasure Tracer, we offered a small prize for the reader who sent in the most interesting letter mentioning items that had been found using the project.

Well, this article seems to have hit the jackpot. We know that several thousands have been built, so many in fact that for several weeks some components which were specified were in very short supply; we hope this did not put off some potential constructors.

The prize for the most interesting letter goes to 13-year-old Mark Read of Benfleet, Essex, who, on his first trip, found a ·38 Smith and Wesson revolver in some nearby woods. Young Mark made the front page of his local evening newspaper with his find after he had done the sensible thing and handed it over to the police.

Mark admits to having had a little help with the building but he is a keen constructor and is tackling further P.W. projects by himself. His skill in using the Treasure Tracer must be very high as other finds include a .303 bullet and an iron axe head.

Competition for the most interesting finds was fierce. Mr. Peter Hope of West London found a total of £3 4s $3^{1}2^{1}$ in his first week after building the project, enough he says to cover the cost of the Treasure Tracer—with a bit over.

Another reader found several transistors on the beach; how they got there we will probably never know but one has to admit that it is unusual.

Several letters mentioned sums of money that have been found and the total of all of them is nearly £20.

One point must be emphasised again and again. A lot of people complained that their results were poor compared to ours; when asked if they had spent much time trying, in nearly all cases they had done very little practice and were expecting good results immediately. You will not become good with the Treasure Tracer without considerable practice. One or two of those politely asked to put in more practice actually contacted us again saying that all was now fine and finds had been made.

Correspondence on the Treasure Tracer has been considerable but the points raised have all been very similar and answers are given below to the most common queries.

There are no mistakes in the article which will affect the operation, suspect your construction as a likely cause. Any type of 2N2926 transistor will do though the G (or green) may be better in the audio stages. Many readers felt that the volume was a little low and want to fit a louder amplifier. Any transistor amplifier capable of being run from a PP3



Mark Read with his Treasure Tracer and the revolver he found.

battery can be used instead of the amplifier of the prototype. Connections for this should be taken from the junction of D1 and C6, C5 may not be necessary. Experimenting with the value of R6 may help in some cases.

A lot of readers mentioned a Faraday shield, since these are fitted to most commercial types. The amount of information on metal locators is not very extensive. Experiments have shown that a Faraday shield is only useful or necessary if the frequency is a lot higher. The ground capacity effect on the Treasure Tracer is very small indeed and fitting a Faraday shield made no difference. However, another design was tried working on 700kHz; on this frequency the ground capacity effect was marked even with a Faraday shield.

There is room for experimenting with different coils. A larger diameter with fewer turns to obtain the same inductance will find large objects much deeper in the ground but it will not pick up small items, even on the surface; the size of the prototype seems to be the best operational size for general use.

Recent experiments have been carried out on encapsulating the coil in epoxy resin to hold the windings rigid. This works well and is an improvement but it does increase the weight of the head to an uncomfortable degree. Lacquering the search coil with a coil cement definitely helps.

And please, many letters were from readers who had not read the article through, they could have saved themselves a lot of trouble and time by reading the text as we had already anticipated their queries.

We hope that the above will help some readers and answer their queries. We regret that no back numbers are available at all.



9-Band Short Wave Radin

The world at your finger-tips" has become almost a cliche when advertising short wave receivers—but it's certainly true with this project. The frae bands means no dial cramping, enabling you to tune into stations with ease in the range 3:6 to 15 MHz. Worried by visions of lots of coils?—don't worry, there are only two, band selection is made by switching in pairs of fixed capacitors, greatly simplifying the construction.

COMPONENTS

Aerials to Zeners-that's the field covered in this extra supplement featured in the December issue. A detailed explanation is given of most of the important components used in today's electronics.

ALL IN THE DECEMBER ISSUE ON SALE NOV. 5th ALSO

4-20V REGULATED POWER UNIT • TRANSISTOR TAPE RECORDER

Fed up with using a whole variety of batteries for your experiments? You'll be able to throw them away if you build our stabilised power supply covering 4V to 20V. The whole unit builds up into a smart, compact unit.

Earlier this year we promised you a mono tape recorder project. Well, it's in the December issue. Six transistors are used in this 4W circuit which combines both record and playback facilities. Constructional details and layout are given in full.

THIS receiver, intended for use in the 550kHz to 30MHz range, has electrical bandspread for all frequencies and is capable of very good general short wave reception. For the builder who is particularly interested in the amateur bands a crystal filter is incorporated and a product detector for the reception of single-sideband. For calibration purposes a harmonic crystal marker is included.

The circuit has the advantage that the receiver can be started in much simplified form, the crystal filter, carrier oscillator and other features being added later, as required. In any case, it will be found convenient to proceed in this way rather than to build the complete circuit before anything can be used or tested.

Miniature plug-in coils are used which enormously simplifies wiring and construction. These coils have to be changed by hand, but in practice this is often not so much of a disadvantage as may be supposed. For example, if most interest is in the h.f. amateur bands, 14, 21 and 28MHz, all these fall in the range of one set of coils. Again, both the l.f. amateur bands (1·8 and 3·5MHz) are tuned with another set of coils while for general s.w. listening, the range which falls between these will cover many of the useful broadcast frequencies.

Approximate coverage of the four ranges is as follows:

Range 2. 550-1550kHz. Range 3. 1·5·4·8MHz. Range 4. 4·8·12·0MHz. Range 5. 12·0-30MHz.

These ranges are the maker's coil numbers. Range 1 is for long waves and may be employed if a high-performance receiver is wanted for these low frequencies.

DESIGN

Fig. 1 shows the receiver stages in block diagram form. (1) is the r.f. amplifier, with r.f. gain control and panel aerial trimmer, allowing best results with any aerial. (2) is the frequency changer stage. (3) is the crystal filter and (4) the 1st i.f. amplifier. As selectivity with the filter adjusted for maximum

F.G.RAYERVVV G3OGRWW

sharpness is much too narrow for a.m. reception a selectivity switch is incorporated, together with a phasing control which allows a rejection notch to be moved across the i.f. passband.

(5) is the 2nd i.f. amplifier and (6) a diode, for a.m. detection and a.g.c. (7) is the carrier oscillator, used for s.s.b. and as a beat frequency oscillator for c.w. reception, in conjunction with the double-triode product detector (8). (9) is a triode-pentode, for a.f. amplification and output, feeding the speaker. (10) is the crystal marker, a 1MHz crystal giving calibration points up to 30MHz.

For the beginner in particular, it is recommended that the receiver is built in the following order:

Stages (2), (5), (6) and (9). This is a straightforward superhet with three valves and one diode, capable of good results on any band.

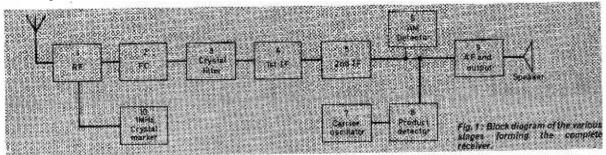
The r.f. stage (1) is then added, improving sensitivity, and giving much more freedom from second channel interference on the h.f. ranges.

Stages (7) and (8) may then be added, allowing reception of s.s.b. and c.w. signals. The crystal filter (3) and its extra i.f. amplifier (4) can then be incorporated which are primarily intended to bring about the increased selectivity which proves so useful with crowded amateur and other bands.

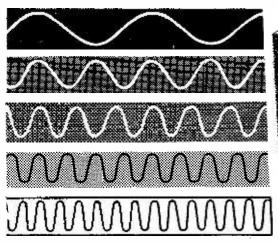
The marker (10) plays no part in actual reception, but is a convenience for accurate calibration and accurate setting of the bandset ganged capacitor, when it is necessary to read frequencies from the bandspread dial.

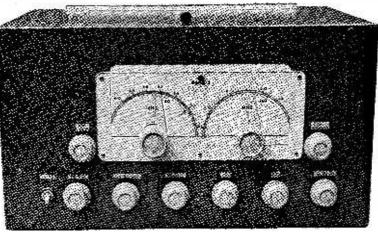
It is, of course, not necessary that the extra or optional stages are added in the order given, as this depends to some extent on the requirements of the user.

It is recommended that the "basic circuit" is built first, for the following reasons:



604





(1) This consists only of stages 2, 5, 6 and 9, Fig. 1, so there is less chance of wiring or other errors.

(2) The "building time" until a useful receiver is produced is much smaller.

(3) If a fault should be present at this stage it will be much easier to locate.

(4) The whole construction can be spread over a period, without the feeling that it will never be finished.

(5) In some cases a simpler receiver will be adequate, so that some stages need not be built.

METHOD OF CONSTRUCTION

The carrier oscillator, crystal frequency marker, and crystal filter (with i.f. stage and phasing capacitor) are built as three separate units on boxes readily made from "universal chassis" flanged members. When wired, they are bolted on to the main chassis, and connected to the receiver circuit.

The main chassis is 13×8 in. To allow experimentation, and the easy changing of some parts of the circuit, the chassis was made from five "universal chassis" members, bolted together by the flanges to

form one assembly 13×8 in. To the left, the power supply and a.f. amplifier occupy a 8×4 in member, with space near the front for the carrier oscillator box, when required.

To the right, a 8×3 in member takes the mixer section, with space for the crystal filter, when added. Between these, two 5×3 in members accommodate the bandspread and bandset capacitors, and aerial coil.

At the back, a 6×3 in member forms the i.f. and product detector strip. All make a chassis by bolting on a 13×2 in member at the back and 8×2 in sides.

If this method of construction is employed, place the five flanged members together with their flanges upwards, and mark and drill the flanges for two 6BA bolts between each member and those adjacent. Also drill and fit the back and sides. It is then possible to remove the bolts and take out any section, without much disturbance to other members.

If this method of construction is not favoured, it is in order to use a conventional chassis $13\times 8in$. This would simplify preparation and metalwork to some extent.

The completed receiver is enclosed in a readymade metal cabinet, the speaker being an external

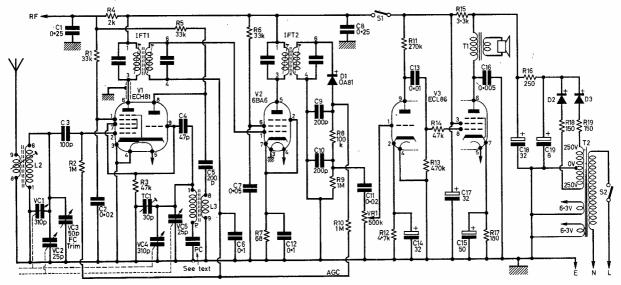


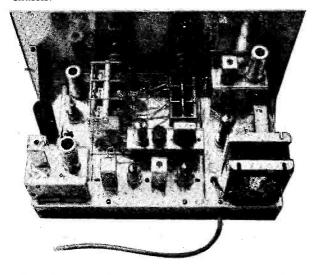
Fig. 2: Circuit diagram of the 3-valve basic receiver. The unused sections of the two 3-gang capacitors will be used for the r.f. stage added later.

unit. No reasonably-priced cabinet with a lifting lid could be obtained, so the top was sawn and hinged to allow access to the interior and changing of plug-in coils. If the receiver is later modified to include band-switching, this is still a useful feature.

BASIC RECEIVER

Fig. 2 is the circuit of the basic receiver. The miniature plug-in coils are "Blue" for the aerial circuit, "Yellow" for the mixer grid (L2 in Fig. 2) and "Red" for the oscillator circuit (L3 in Fig. 2). With Fig. 2, it is necessary to have a pair of coils, one Blue and one Red, for each waveband. When the r.f. stage is included, a set of three coils is necessary for each waveband—Blue for aerial, Yellow for mixer, and Red for oscillator. Yellow coils will thus be placed in the L2 holder, Fig. 2, when this stage is reached.

Padder capacitors PC are of separate value for each Red coil, using a different pin for this purpose on each range. So all the padders are permanently wired to the holder and the correct value is automatically in circuit for any coil which is inserted. PC is 350pF to tag 2 for Range 2, 1000pF to tag 3 for Range 3, and 3000pF to tag 4 for Range 4. Range 5 has no padder and tag 6 must be connected to the chassis



VC1/VC4 is the ganged tuning or bandsetting capacitor, and a 3-gang unit is fitted to allow tuning the r.f. stage when fitted. VC2/VC5 is of low value, so that its full movement covers only a narrow range of frequencies, for bandspreading (easy and more accurate short wave tuning). This unit is also 3-gang. Both variable ganged capacitors have ball drives.

The oscillator trimmer TCl is left at the same setting for all coils, and VC3 is a panel aerial trimmer for peaking up signals.

V2 is the i.f. amplifier, and the two transformers IFT1 and IFT2 give a good degree of selectivity. When the crystal i.f. filter and extra i.f. stage are added, these come between V1 and IFT1. D1 is the a.m. detector which also gives automatic gain control voltage. When the product detector is provided, D1 is retained for a.g.c. and a function switch selects the appropriate mode of operation for a.m. or c.w./s.s.b. reception.

V3 is a 2-stage a.f. amplifier giving adequate output into a loudspeaker. Additional h.t. smoothing is

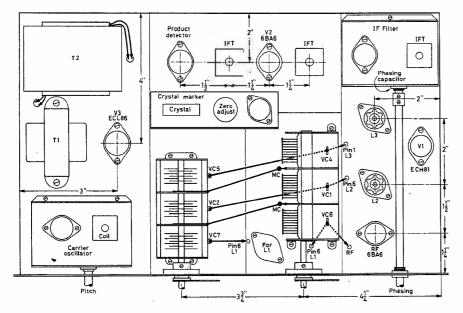
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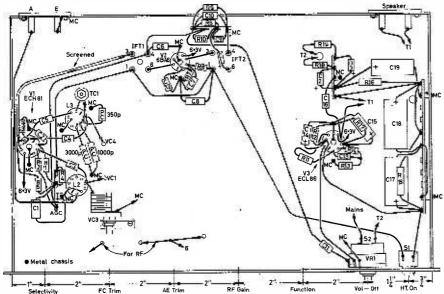
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Resistors:	
R1* 33kΩ 1W	R8 TOXEL WITH HILLS SALL SWIT
R2 1MQ TW	R9 1M: W R16 250Ω 3W
RO 47KQ/4W	RIO 1MI2 JW RIT 1800 1W .
PA OKC TWEE	# R11 270kQ TW R18 750U 1W
. 185 . 33kΩ 4W ≤	710 4:7KO JW: .: R19 1500 1W
'R6, 33k() 1W	* PLA 470kΩ 1W
PF 690 MM	RIC 47KS TW. All loss tolerance
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C1 0 25µF 3601 C2 0 02µF 350	V CH PROM INDV V CHS G-LF (20V -1 CRS (0.01) F 250V
C3 100pF SM	Part of the Control
C1 - 47pF SM -	CIVILLY W
CM 47pF SM CS 200pF SM	
CD EMPT SM	C15 50/FT 25V C16 0054F 500V C17 32/F 450V
C6 0 1 F : 150V	CID O'DUDAL DRAW
F CT & 0 CC F 250	C17 - 32AF , 400V.
C8 0.25µF (E)0	
C9 200pF	C19 8µF : 450V
C10 MupF	×3(0pF (Jackson Type E3-9 gang)
VCI-VCI-VC63	(x310pF-(Jackson Type E3-8 gang) s
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Range 8	1000pB to pin a
Range 4	3000pF to pin 4
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one screen, S1.	on/off totale switch. Ball drives (2)
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Cabinet 15x9	8in with senel (M.L. Smith Tene
(LW) Chassis 13	x 8in aluminium plate with tax bear
(2) and 8 your to) flanged members (Home Radio)
23.50	

provided for early stages by R15 and C17. S1 is a "Standby" switch, leaving heaters on but h.t. on V3 only. This allows immediate on/off switching, as may be required when using the receiver with a transmitter.

CONSTRUCTION

Fig. 3 shows the layout of the completed receiver, but the i.f. filter, carrier oscillator, marker, product detector and r.f. stage are added later in the way described. Punch chassis holes for the r.f. stage, aerial coil holder L1, and product detector holder, as this is awkward later if sections are not removable





in the way explained.

Punch holes in the front 13×2 in runner as in Fig. 4. Place this on the panel with 1_2 in of the panel projecting below, and punch matching holes in the panel. The panel is held to the chassis by component bushes and a vertical bracket each side.

Mount the variable capacitors with their spindles at the same height, so that the ball drives fit in clearance holes, with the drive lugs bolted to the panel. Take insulated leads from the lower tags of the bandsetting capacitor, down through holes as in Fig. 3. Connect the bandspread capacitor with stout leads clear of the chassis. The rotor tags are wired to tags bolted to the chassis.

Fig. 4 shows connections and components under the chassis to assemble the circuit in Fig. 2. The absence of bandswitching simplifies this part of the

Anchor the mains cord at a tag strip. Leads from

Fig. 3: (left) shows the disposition of the major components and units on top of the chassis while Fig. 4: (below) illustrates the wiring beneath.

the transformers T1 and T2 pass down through rubber grommets. Smoothing capacitors and other items are anchored by tagstrips.

Later, h.t. for the r.f. stage is taken from the tag holding C1, while the "a.g.c." tag supporting R2 is the a.g.c. connection for the r.f. stage.

Leads carrying r.f. are stout and run clear of the chassis. AF circuits, such as to C11, are run against the chassis, as are heater and h.t. connections.

VC3 is mounted on a bracket near the holder for L2, as in Fig. 4, and its spindle is extended through the panel. This allows short leads and separation of r.f. and mixer circuits.

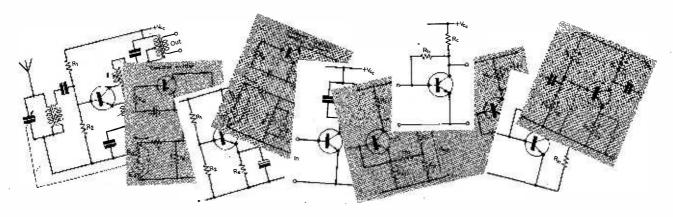
ALIGNMENT

With the circuit of the basic receiver completed, insert a correct pair of coils, such as those for Range 2. Clip a test-meter, set for 10mA, across R7 with negative to chassis. Tune in any local BBC or other stable transmission.

The four cores of the two i.f.t.'s are then adjusted, with the correct type of core tool, for minimum meter reading. Each core should have quite a definite peak.

TC1 is set at about half capacitance and rotating VC3 with any pair of coils in use, and the bandset capacitor nearly fully open, should peak up signals. The receiver is then tuned towards the low-frequency end of the band, and if coverage is unsuitable, the core of L3 is adjusted to correct this. The core of L2 is then adjusted for best results (minimum meter reading). Set the core of L2 so that when tuning from the h.f. end of the band, to the l.f. end, the minimum re-adjustment of VC3 is required. Deal with each pair of coils separately, and lock the cores with 6BA nuts.

PART 2 NEXT MONTH WILL CONTAIN FULL DETAILS OF THE ADD-ON UNITS TO COMPLETE THE RECEIVER



RANSISTOR CIRCUITRY for beginners H.W.HELLYER

PART 2

Properties of Germanium and Silicon

The silicon diode has a more sharply defined 'knee' in the reverse characteristic than the germanium type. At a certain point, as the reverse voltage is increased, the current suddenly increases very rapidly. At the breakdown point the current can suddenly increase from a few microamps to many milliamps, and even amperes in some specially constructed devices. Advantage is taken of this characteristic which all semiconductors exhibit to some extent, in the development and application of a Zener diode.

History of the Transistor

Although it was as recently as 1947 that Bardeen and Brattain of the Bell Telephone Laboratories earned themselves a Nobel prize with the development of the transistor from the types of semiconductor devices we have been discussing, it should not be imagined that the whole family of semiconductors has so short a history. The main research impetus, it is true, came during World War II, but as long ago as 1835 the rectifying properties of certain substances had been noted by Rosenshold. F. Braun revived interest in 1874 and Willoughby Smith Co. testing underwater telegraph lines, had already noted a variation of resistance according to the amount of light shining on the material some un-named technical assistant was using-which happened to be selenium. In Victorian times, the selenium cell, in rather primitive form, was a scientific curiosity, and its rectifying property was observed in 1876.

Even as Fleming was experimenting with his thermionic diode in 1904, J. C. Bose patented a semiconductor crystal diode, and in the early years of broadcasting, the crystal detector was much used. A silicon detector was invented in 1906 by Pickardfamiliar to early experimenters under the name of the 'Perikon detector'. A patent for the improved version of this device was taken out in 1909.

Earlier devices-until 1941, anyway-were pointcontact. Then a junction diode was brought out. Six years later came the first transistor. Bardeen

and Brattain developed a 'crystal diode' and the name 'Transistor' came from 'Transfer-resistor'.

There is nothing new under the sun. Many years before, the diode had been used as an oscillator, and in 1924, Wireless World carried an article by Victor Gabel, which dealt with the Russian Lossev's experiments with crystals as generators and amplifiers. To undermine our easy belief in progress yet further, we note that Eccles used a crystal diode as an oscillator way back in 1909!

The original work on point contact devices at Bell Telephone Laboratories brought the first transistors. Shockley was a leader among those, who, realising the limitations-high noise factor, relatively high production costs, lack of durability and the difficulty of manufacture-researched the junction device and eventually came up with a 'junction transistor'. This is the basis of most modern semiconductor devices.

A variety of techniques has developed: grown junction, alloying, surface barrier, alloy-diffused, diffused mesa, epitaxial diffused mesa, planar, epitaxial planer, diffused field effect, etc. Let's take a look at the more important among them.

Development

It was during an investigation into the rectifying properties of surface potentials around a point contact that the scientists at Bell Telephone Laboratories used a second contact to prove the field. At spacings between the two probes of less than a couple of thousandths of an inch they noted a change in current in the main contact influenced the current flow in the other. From this, the germanium point contact transistor was developed.

Two springy wires with pointed ends about a thousandth of an inch apart, pressed on a flat piece of germanium, each having rectifying characteristics. The emitter has a forward bias and thus a low resistance while the collector is reverse biased, giving it a high resistance. A change in forward current through the emitter contact produces a change in the collector contact, and because of the difference in the resistances, power amplification takes place.

This is the important, noteworthy, fact about

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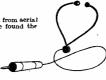
This system which has proved to be amazingly efficient and reliable was first described in the Wireless World about a year ago. We can supply kit of parts for improved and even more efficient version, (P.W. June), price \$4.95. When ordering please state whether for positive or negative systems.

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1 poie	40p	40p	40p	40p	4 8 p	40p	40p		40p
2 poles	40p	40p	40p	40p	40p	40p	40p		70p
3 poles	40p	40p	40p	40p	70p	70p	70p		95p
4 poles	40p	40p	40p	70p	70p	70p	70p		£1.20
5 poles	40p	40p	70p	70p	95p	95p	95p		£1·45
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as described in this issue and in past issues. We can probably supply components. Send S.A.E. for list naming the project.

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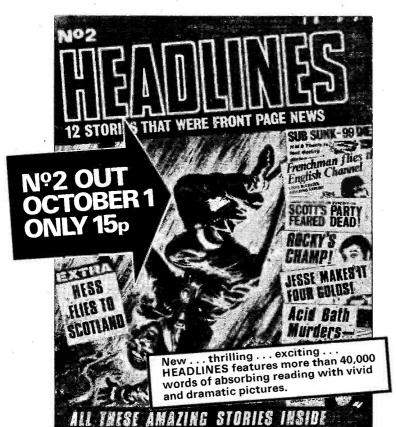
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that was Beria-Head of Russia's Secret Police and responsible for the callous murder of thousands of 'anti-communists'.

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the heavyweight champion with the iron punch that no man on earth could withstand.

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that was the name given to the factory in Crawley where John Haigh destroyed the 6 bodies of his victims in a tank of acid! THESE AND OTHER GREAT FRONT-PAGE STORIES OF THE TWENTIETH CENTURY ARE ALL IN NO. 2 ISSUE

the transistor, that it is essentially a currentoperated device. However, it is the difference in input and output resistance that is the vital means of securing amplification. Hence the name—the process being basically one of transferring a current from a low to a high resistance, using a solid-state device. The advantage is reduced size and weight and no need for a heater supply as with a thermionic valve.

As development goes on, some of the disadvantages, power handling limitation, frequency characteristics, etc., will be overcome. Solid-state devices have almost completely ousted valves from portable equipment, have invaded the domestic entertainment field for table radios and record players, and most tape recorders, are already into high fidelity amplifiers and are now used for nearly all stereo radiograms, while television circuitry has been the subject of much experiment with transistors taking the place of valves in almost every stage. Transistor television receivers have been marketed and are gaining in popularity as prices level off.

In the commercial and industrial field, solid-state devices are imperative for many applications, where the number of switch-gates and amplifiers in a unit would militate against valves on the grounds of space alone, even if power consumption and heat dissipation were not important considerations. Transistors, allied to micro-electronics, modules, integrated circuits and other developments, have led to the production of computers with a wide range of facilities, yet no larger than an old-style adding machine.

Operation

In considering the operation of the junction transistor, we must revert to the properties of the p-n junction. If two of these junctions are formed, back to back, in a single piece of semiconductor, and lead wires taken from the p and n sections, a transistor is formed. This formation can be either p.n.p. or n.p.n., with roughly opposite characteristics, as we shall observe. The first p region, called the emitter, emits holes into the base, the centre n region. The second p region, the collector, collects holes from the base and is negatively biased. This is the p.n.p. transistor, which we shall now consider.

Fig. 7 shows the p.n.p. transistor connected as an

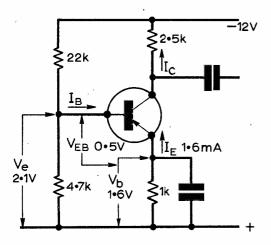


Fig. 7: A silicon p.n.p. transistor connected as a common-emitter amplifier.

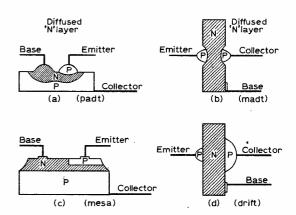


Fig. 8: Typical construction of some transistors.

amplifier, with appropriate supply voltages. In passing through the base region, the emitter current $I_{\rm E}$ decreases slightly by some holes recombining with electrons. To take the place of these 'lost' electrons, more flow in from the base contact, the current thus produced being equal to the difference between the emitter current and the collector current, or $I_{\rm B}\!=\!I_{\rm E}\!-\!I_{\rm C}$.

Some actual constructions of p.n.p. transistors are shown in diagrammatic form in Fig. 8. These are (a) post alloy diffused, (b) microalloy diffused, (c) mesa type, and (d) 'drift' type. In the construction of transistors, a number of very delicate refining processes take place, and the following notes are only a brief look at production techniques.

Production Techniques

Germanium occurs in certain coal formations and as an impurity in zinc and copper ores. It can be extracted from the flue dust of coal-burning power stations. It is chemically extracted from its source, converted to germanium dioxide and heated in hydrogen to reduce to the metal. Impurities at this stage are as low as one part in a million. To purify further, zone refining is carried out by concentrating power in one part of the ingot, producing a narrow molten zone and moving this to the end of the ingot, which tends to move the impurities toward the end, which may be cut off and rejected. Refinement to reduce impurities to as little as one part in 10¹⁰ can be carried out in this way.

The selected donor or acceptor impurity is added in similarly small controlled amounts. This is done during the same process as seeding, when a small 'seed' of the metal is lowered into contact with molten germanium in a crucible heated a little above the melting point and raised very slowly so that a crystal solidifies on the seed.

This process of 'pulling from the melt' is also used in manufacture of silicon transistors. Silicon is a common substance (sand is mainly silicon dioxide) and chemical extraction is employed to refine it. A floating zone process is often used both to complete refining and to produce the correct crystal, whereby a rod of polycrystalline silicon is held vertically and a molten zone, narrow enough to be held in position by surface tension is passed up, from a single crystal seed at the bottom, to the top. As the zone passes up, silicon melts into it at

the top and boron and other impurities are taken to the top while the silicon solidifies out into single crystal form at the bottom.

After refinement and preparation, the single crystal material is sawn into slices about fifteen-thousandths of an inch thick, using diamond impregnated wheels. The slices are lapped to a thickness of about eight to ten thou' by carborundum and finally surface irregularity is removed by etching in an acid mixture. For some diffused types the whole subsequent process is carried out on the whole slice, which is then scribed and cut to size, but for many other applications the processing is done separately.

The junctions between the p and n type materials may be 'grown' during the process of pulling from the melt, or formed by other methods. These include alloying, diffusion and epitaxy. Epitaxial junctions are formed on a substrate wafer by growing a thin film of the same semiconductor on to it, hence the term 'epitaxial', meaning, on the same axis. Again, heating is the key to the process, and very precise methods of temperature control have been developed by transistor manufacturers.

Alloy diffused transistors are made by a combination of diffusion and alloying techniques. This gives a narrower base width and a better high frequency performance. They have a high current gain and an upper cut-off around 100 MHz.

Diffusion transistors of both germanium and silicon types have much better characteristics because of the more rigid control of dimensions of the elements during construction. In general, germanium offers higher frequency possibilities than silicon and germanium diffused transistors operating up to several thousand MHz are available. The method of construction gives rise to the term 'mesa'. whereby an area of the diffused collector junction is defined by masking over the emitter and base stripes (evaporated gold contacts being used) and the wafer etched to leave a raised 'mesa' containing the active part of the transistor—a process that greatly aids mass production.

Silicon diffused transistors can be sub-divided into several types but most variations are the result of research into closer production control. Some forms similar to mesa etching are employed, and diffused mesa transistors are generally of the silicon type.

Planar Transistors

A development of manufacturing processes to overcome instability caused by contamination at the surface of the mesa led to the planar type of silicon transistor. The process is quite involved, including the use of photo-etching techniques, deposition and diffusion, but the great advantage is the protection of the collector-base junction, resulting in very low collector leakage current. Very thin base layers are possible giving good high frequency performance, up to several thousands of MHz. Manufacturing techniques can be modified to easily make different size transistors and a whole range of types, from small signal high frequency, to high power medium frequency (typically 50 watts at 10 MHz) can be produced.

One disadvantage of the diffused transistor is the series resistance between the collector junction and the contact at the bottom of the wafer. This sets up an internal voltage drop when collector current

flows. To improve upon this, the epitaxial planar transistor has been developed. This is perhaps the most versatile transistor to date, with good, allround characteristics. Manufacture includes the previous processes, but a composite slice of very low resistance substrate on which a thin epitaxial layer has been formed is now employed and the epitaxial structure can be developed by depositing alternate p and n layers on a suitable substrate.

Field-effect Transistors

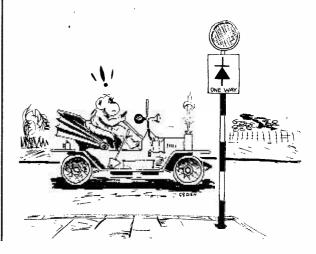
One very important development of this process is the construction of the field-effect transistor. Its special properties are likely to lead to a rapid increase in applications. In particular, its high input impedance makes it suitable for a number of circuit configurations where other types of transistor are not appropriate. Another important feature is that only one type of carrier is involved—the majority carrier in the basic bar of semiconductor. This is in contrast to the normal type of junction transistor, which depends for its action on the flow of minority carriers through the base region and majority carriers in the emitter and collector regions. A high impedance linked with a low noise factor makes this device eminently suitable for small-signal input stages. The most significant difference for the designer, is that the f.e.t. is a voltage-controlled device but more about f.e.t.'s later.

The zener diode is essentially a specially constructed diode designed to work in reverse, employing what would be regarded as the 'failure' part of the characteristic of an ordinary silicon diode. The silicon controlled diode or thyristor is a further device which finds special uses. Normally, this rectifier blocks current both ways, but when triggered by a pulse fed to a gate electrode, current is allowed to flow in the forward direction only. As this is basically a three-junction device, more detailed explanation will be left until later.

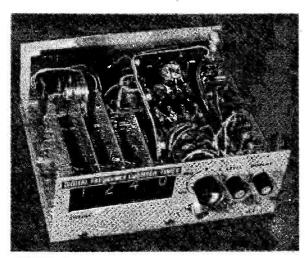
TO BE CONTINUED

MAXWELL

by G8DSH



DIGITAL FREQUENCY COUNTER/TIMER



PART 3 (continued from the October issue)

The cutting and drilling of the panels is shown in Fig. 15 and the drilling and position of the components on the chassis is shown in Fig. 16.

The top cover consists of a simple drop-over inverted 'U' shape. It is $^{1}2$ in longer front to back than

the chassis and overhangs the front panel by about 38 in to produce a 'visor' effect. The top cover is fastened by two 6BA screws on each side.

To conceal the screws which protrude through the chassis underneath, a snugly fitting base cover is fitted inside the underside of the chassis and the top cover screws pass through the sides of the chassis into the base cover. The base cover is drilled and tapped 6BA for this purpose, but 6BA self-tapping screws would be equally suitable. The base cover is fitted with four stick-on plastic feet.

To avoid any bending of metalwork, it would be possible to use a piece of 3 8 in plywood for the chassis and plastic covered hardboard for the cover. It would still be desirable to make the front and rear panels of aluminium.

The window cut-out for the indicator tubes can be made either by drilling a line of holes and then join-



J. THORNTON-LAWRENCE GW3JGA

ing these by filing through, or more simply by using an Abrafile in a hacksaw frame and finally finishing off with a flat file.

The front and rear panels are sprayed with car touch-up enamel and lettered with Letraset. The cover may also be sprayed or alternatively it may be covered with Contact or Fablon self-adhesive plastic material.

Assembly and Wiring

The various sections of the Digital Frequency Counter/Timer are built separately and then assembled and wired to each other and to the supplies and controls on the main chassis and panels.

The operation of the complete working instrument

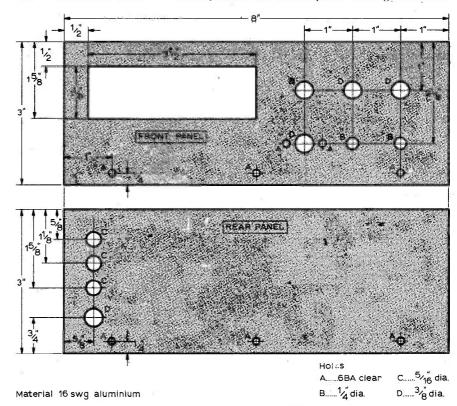


Fig. 15: Front and rear panel metalwork.

is not in itself very complicated, but should any part malfunction due to a wiring error or faulty component, the locating of the fault could prove to be very time consuming. This is mainly due to the fact that the cycle of operation depends on several stages operating in sequence. If the sequence is broken due to a fault condition, all stages become suspect and it may be quite difficult to locate the section containing the fault.

The operation of most of the panels can be checked before being assembled on the chassis and by doing this the possibility of building-in a fault is greatly reduced.

In any case it is always important to try to prevent wiring errors right from the outset and although, to some constructors, the following suggestions on wiring the Veroboard panels may be rather trivial, it is hoped that they will help to produce an instrument which will work first time.

Main Chassis and Power Supply

It is suggested that this is constructed first as it will provide the various voltages required to test the other parts of the instrument.

The component positions and wiring are shown in Fig. 17.

Testing

When operated without a load, the h.t. section of the power supply will develop an h.t. voltage of about +350 volts. The -5 volt section will not operate correctly until the h.t. section is loaded, but some negative voltage should be detected across D9, depending on the current drawn by the meter (approximately -5 volts on a 20,000 ohm/volt meter). All voltages are with respect to chassis.

The +5 volt section is regulated and here the noload voltage will be about $+5\cdot2$ volts. The voltage across C14 is about +8 volts.

Crystal Clock and Divider (Panel B)

This panel is built and tested next, as it is needed to provide a test signal for testing the other panels. The components, links and pins are fitted in the manner suggested previously.

Connect the crystal and trimmer to the appropriate pins and, with temporary wires, connect the panel to the chassis earth and the +5 volt supply.

Testing

The oscillator transistors Tr8 and Tr9 operate in class A and the voltage of $+2\cdot3$ volts on each collector remains about the same whether the crystal circuit is oscillating or not.

However, the clipper stage Tr10 has a normal operating collector voltage of about +2 volts but if the oscillator is not functioning this voltage will rise to nearly +5 volts. The oscillator circuit has adequate gain for most crystals but for very stubborn surplus types which may refuse to oscillate, C8 may be reduced in value to 220pF. Any further reduction of C8 may cause the circuit to oscillate at some spurious frequency controlled by the not crystal.

With the oscillator and each stage of the divider chain functioning, the voltage af each output point will be approximately +1.6 volts d.c. with the oscillator not functioning the voltage at each point could be +3.5 volts or +0.1 volts depending on the state of the output of the decade counter.

The waveform at any of the divider outlets should be a square-wave of 1:1 mark-space ratio and 3.4 volts peak to peak amplitude and of the appro-

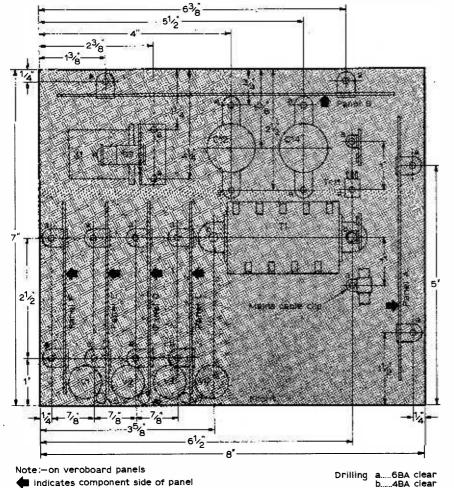
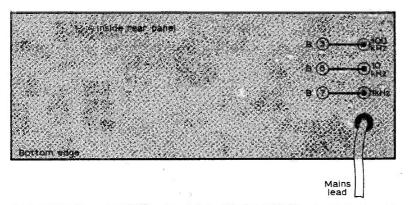


Fig. 16: Chassis metalwork and main component layout.

priate frequency. The 100kHz output at Tr10 collector should be about 4.7 volts peak to peak. The frequency of the 100kHz oscillator can be checked and set exactly by beating its second harmonic with the 200kHz signal from Droitwich (BBC Radio 2).

cast receiver to Radio 2 on 200kHz and by connecting

A simple way of doing this is by tuning a broad-



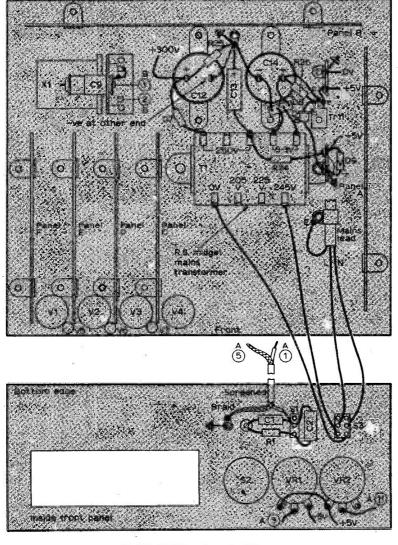


Fig. 17: Chassis and panel wiring.

a length of insulated wire to the 100kHz output, B(3), to provide coupling. The wire is placed close to or around the receiver to cause a beat note or whistle to be heard. The trimmer capacitor C9 is then carefully adjusted so that the beat reduces to zero. If the 200kHz signal is very strong it will be necessary to reduce the pick-up of this signal by removing the

> external aerial or by rotating the set if it has an inbuilt ferrite rod aerial, to obtain a weak reception of the 200kHz transmission.

> Near zero beat the difference frequency will be heard as a cyclic variation of the background noise rather than a 'note'. The final setting of the oscillator frequency should be made when the instrument is complete.

Gounter and Display Panels, C, D, E and F

The components, links and pins are fitted to the panel in the usual way.

The numeral indicator tube is fitted to the panel and held in place by the glass pip which fits snugly into a 18in×14in grommet. The grommet is supported by a crossed loop of 20 s.w.g. wire fitted in holes Al and A4.

The numbers must face the correct direction, the top of the glass pip should be in line with the top of the panel and the straight surface of the glass envelope should extend about 18in beyond the end of the panel.

Wiring should commence with the low numbers and the lead-out wires sleeved using small diameter sleeving. The last few wires to be connected should pass over the previous wires. The wires, when soldered, effectively support the base end of the tube.

Testing

Each panel should be tested separately by connecting it with temporary wiring to the +300 volt, +5 volt and earth, 0 volt, connec-

Connect the crystal clock and divider panel to the same +5 volt supply and using a croc-clip 'jumper' lead join the input of the counter panel (7) to the 1Hz output of the divider B(10).

As the reset input (4) is not connected to 0 volt the counter is continually in the reset condition and the numeral tube should indicate '0'. With another jumper lead join the reset input (4) to 0 volt (6). The numeral tube should now display continuous counting 0-9 at one digit per second.

Disconnecting the jumper lead between (4) and (6) at any time should reset the count to zero, '0'. Counting should recommence when the connection is remade.

The neon 'decimal point' may be checked by connecting a $220 \mathrm{k}\Omega$ resistor between the decimal point connection (1) and 0 volt (6). A wrong sequence of numbers probably indicates a fault in the wiring of the numeral tube. Two numbers being on together is probably caused by a solder blob short circuiting two strips on the Veroboard, but also could be due to a faulty decoder-driver integrated circuit.

I.C's. can be checked by substitution and as four panels are required for the complete instrument a faulty panel can be easily checked against the other three.

When testing counter and display panels it is advisable to insulate the +300 volt connection to the panel in case a jumper lead going to an i.c. accidentally strays on to the +300 volt connection.

Each panel should be checked individually for correct operation and then mounted on the chassis and linked together as shown in Fig. 6. (Part 1. September issue.)

The counting and 'carry' operation of the complete counter and display section may be checked by applying the 1Hz output B(10) from the divider to the signal input C(7) and checking that the carry to the next higher decade is made on the transition from 9 to 0.

The previous remarks about the reset line now apply to all the panels simultaneously.

Input Stage, Control Oscillator and Gate (Panel A)

To test this panel, it is necessary to have all the other panels installed on the chassis and connected to the appropriate supplies. This applies particularly to the ± 300 volt supply to the numeral tubes as without the normal loading on this supply the ± 5 volt supply will not regulate correctly under load. It is not necessary to have S2 connected in circuit when testing the operation of Panel A, and it is advisable to check the operation of all the sections before connecting S2 into circuit.

Input Stage

With all the supplies connected to panel A, and to VR1 and VR2, connect A(3) to the slider of VR1 and monitor the output of Tr5 A(6) with a voltmeter. Slowly rotate VR1 until a point is found where the voltage at A(6) flips between +4·0 volts and +0·1 volt. Dual voltages are given at various points in the circuit diagram of the input stage and these may be checked if faulty operation is suspected. The actual position of VR1 at which the circuit operates depends on the individual gate characteristic of Tr1.

An oscilloscope check may be made by connecting the input components and S1 to A(1) and A(5) as shown in the circuit diagram and feeding in a 100mV r.m.s. audio frequency signal to the input socket. Switch S1 should be in the a.c. position and the output should be monitored at the output A(6).

The square-wave output should vary in mark-space ratio as VR1 is adjusted and the operating point is moved over the amplitude range of the input signal voltage.

Control Oscillator

For the control oscillator to function, A(11) must be connected to VR2 as shown in the diagram. Depending on circuit conditions the oscillator circuit may be held in the clamped condition by D4 and D4

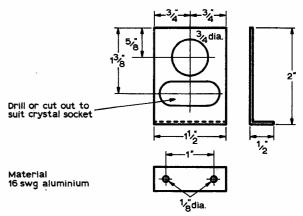


Fig. 18: Crystal mounting bracket.

should be temporarily disconnected by unsoldering one end to stop any clamping action.

The control oscillator should now free-run at a speed determined by the setting of VR2. The slowest speed is one cycle in about 4 seconds.

The square-wave output at Tr6 and Tr7 collectors should have a voltage swing from $0\cdot 1$ volt to nearly +5 volts. An oscilloscope test may be made at A(8) to check the presence of the positive-going 200μ S pulse which performs the resetting of the counter and the setting of ICla. However, due to the short duration of the pulse and the low repetition rate it may be difficult to observe this pulse on a simple oscilloscope.

The diode D4 should be reconnected after this test.

If the oscillator refuses to run, check the collector voltages of Tr6 and Tr7, if either of these are low, about +0.1 volt, check the coupling capacitors for open circuit. If either is +0.6 volt, check the coupling capacitor for short circuit. If either collector voltage is about +5 volts check the appropriate base feed resistor circuit.

Gate

The testing of the gate is most easily carried out with all the remaining sections of the instrument operational. The function switch S2 should be left disconnected and temporary wire links used to connect between the various sections.

All supplies should be connected to all panels. Temporary wire connections should be made as follows: Clock divider 1Hz output B(10) to clock period input A(7). Clock divider 1kHz output B(7) to signal input A(9). Gate output A(10) to signal input C(7). Reset output A(8) to reset input C(4).

With these connections made, the instrument should count the 1kHz output for a period of one second and display a reading of 1000. The counter should then reset to 0000 and then commence counting again. This is equivalent to the "TEST" position on the function switch, position 6.

The time that the reading is displayed before resetting is determined by VR2.

With the exception of wiring errors, it is unlikely that a fault will exist in the gate circuit but in any event the sequence of operations can be followed through from the circuit description given previously and the fault diagnosed from the point in the sequence at which the operation ceased.

With all sections operating correctly the function

-continued on page 634

No. 85

practically wireless HENRY commentary by

Made in Where?

ILTED soldiers march across the sea to be sold in Aberdeen. It's enough to make a haggis weep. But until now, November 1971, there had to be, somewhere, a label denoting the country of origin. Or, at least, a tiny ticket under the sporran that said, unequivocally, 'Foreign'.

Parliament, proud of British prowess, demanded that goods should be so marked way back in 1926. It has taken forty-two years for us to bring in the Trades Descriptions Act, and one of the things written in when this became law, in 1968, was that by November 1971 the need for declaring a country of origin would end.

Philips introduction of the *Popmaster* radio woke up some of us stick-in-the-muds. Now, we have come to accept the flair of the Italians, the inventiveness of the Scandinavians, the engineering efficiency of the Germans. It is the idea of Oriental precocity that still fails to sink in.

Yet, as I write, the hold on the television market is being tightened by Far East competition. BREMA figures tell us that in the first quarter of this year British-made TV sets dropped from 484,000 to 401,000, i.e., a 16 per cent loss. The increase, taken up by importers, was



Kilted soldiers march across the seas.

practically a total invasion from Japan. In the radio receiver market, we came down from 342,000 to 323,000. I dread to think what a survey of the audio market would reveal.

Henry gets rather hot under the collar when he hears of the 'rationalisation' that the big boys impose on a taken-over small concern. In no time, the special position that made the back-alley company worth taking-over has been flattened and stultified, making its products part of the bland image that the parent company projects.

In the name of 'efficiency' the economies imposed rob the product of all its individuality. It becomes just another wireless set, tape recorder, gramophone . . .

There is an ironically apt story in an American publication just out: 'Welcome to our conglomerate—you're fired!' Large concern takes over small, specialist company and sacks the boss. A little later, sales begin to slump and the whizz-kids search around for a reason. Can't be the absent boss—after all, he spent most of his time playing poker with the salesmen.

Then it comes out: the poker games were the breeding ground for ideas, and the way the boss instilled his very individual flair in his team.

We have seen the loss of the personal touch more than once in the audio world. A notable case has recently been exemplified by some facelifted models. A small firm with an international reputation is merged into a large group. Almost overnight its keen service fades; models are restyled and, basically similar, with no progressive modification, have a posher faceplate. The companion tuner-amplifier, however, is an imported model.

What's wrong with that? Oh, nothing, except that the *implied* 'Made in England' is held in the brand name. The imported geardoes not even have its gramo-



"Welcome to our conglomerate—you're fired!"

phone pickup input equalised to the standards of the records we, in this country, are going to be able to buy. But to the unsuspecting public, this is a new (and by implication, better) product from the famous stable.

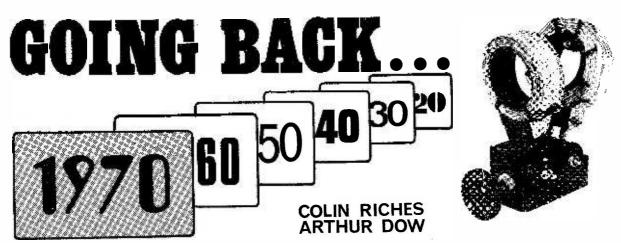
Many electronic goodies masquerade under strange flags. Home-grown labels mean little when the bits have been imported, needing only assembly, boxing and test.

Perhaps that is why the Government have said 'Drop it.'

Do you remember how Max Grundig started? Back in the days when the Germans were not allowed to purchase a complete radio, he brought out a radio, constructed except for the plugging in of a valve, sold the valve separately, circumvented the regulations and laid the basis of a fortune.

Using the Henry method—what artistic circle call aleatory technique of random connections and accidental parallels —I present to you the following information. G.E.C. propose closing the Marconi-Elliott Microelectronics factories at Witham, Essex and at Glenrothes. The first was especially built as recently as 1968. The second has a prospective new neighbour-a microcircuit factory to be built at East Kilbride, Lanarkshire, for the American great concern. Motorola.

Will *their* chips be marked 'Made in Britain'?

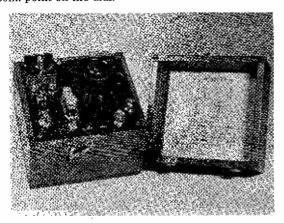


UR request for information on the little buzzer unit shown in our September issue met with little response. However, Mr. F. Kirkby of Ruislip, Middlesex, came to the rescue in no uncertain way by producing what appears to be a more sophisticated version of the unit.

Recently Mr. Kirkby had the task of clearing out the house of an elderly relative and amongst the 'junk', some of which is thought to be over 100 years old, was found the wavemeter shown in the accompanying photograph. The circuit, mounted inside the lid of the teak case, is still perfectly clear and shows a parallel tuned circuit which, in the "receive" position of the changeover switch, is connected to an adjustable carborundum detector and to the telephone terminals at the front. In the "send" position the tuned circuit is connected to the buzzer and cell. The cell in the equipment appears to be the original Siemen's 'S' type cell.

The circuit notes that "the inductance is a 5-turn rectangular coil 3^1_2 in. \times 2in. lying close against the front face of the case" presumably to allow the wavemeter to be closely coupled to the external equipment under test.

The dial is finely engraved in steps from '45' to '95' and this is presumed to be the range covered, in metres. Anyway, a new cell was fitted to the wave-meter and the buzzer adjusted on "send" and the unit placed a few feet from a communications receiver tuned to 5MHz (60 metres) and sure enough the signal, if it can be called that, did peak when the dial of the wavemeter was tuned through the 60m, point on the dial.

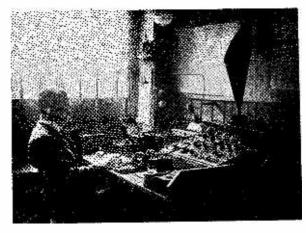


Since no aerial terminal is provided it is presumed that the "receiver" was used as a monitor for a local transmitter and used to set the transmitter to a particular wavelength.

Unfortunately there is no indication of the maker's name or the year of manufacture so once again we must ask our readers to help in identifying this bit of vintage equipment.

Mr. Kirkby is to be congratulated on his vigilance and for rescuing this piece of ancient equipment. We make no excuse for again reminding readers of the thousands of pieces of similar equipment that must be hidden away in sheds, attics and storerooms and which must not be allowed to finish up in some dustcart. There are collectors in the UK who will see that such equipment gets the attention it deserves.

Since writing the above we have heard further from Mr. Kirkby. He has now discovered some old documents including the photograph we show of an amateur radio station operating in 1922. The actual wavemeter under discussion can be seen at the left hand end of the operating desk. Mr. Kirkby now believes that the wavemeter dates from 1916 and that it was obtained as "Ordnance Disposal" or "Government Surplus" as we would call it today.



Incidentally, the two wall charts to the right of the speaker were issued by the Marconi Company and represent the movement of ships equipped with wireless. Presumably listeners could estimate the "range" of their receivers by listening for these ships over varying distances.



etc., were given in Part 1.

We continue now with more circuits for preamplifier stages beginning with one for crystal microphones (Code: Mic Hi-ZX). This is given in Fig. 11 and the circuit board layout is shown in Fig. 12. Crystal microphones have a high output impedance. hence the need for the high series input resistance, R1, to the base of Tr1. The circuit is conventional with d.c. stabilization and negative feedback which also sets the amplifier gain by the feedback network C5 and R3. The 100pF capacitor across R3 produces a roll-off in frequency response above about 30kHz to prevent pick up of r.f. signals as is often the case with preamplifiers having a high frequency response. As with all the preamplifier stages, the output is taken to the gain control VR1 and thence to the line amplifier (or tone control unit) via the passive mixing component R9. Details of the circuit board and screen construction for all the preamps and the tone control were given in Part 1.

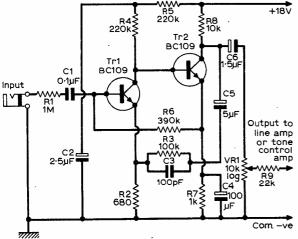


Fig. 11: The crystal microphone preamp circuit.

Fig. 12: The component layout for the crystal mic. preamp. PREAMPLIFIER FOR MAGNETIC PICK-UPS

The circuit is given in Fig. 13 and its code is PU Mag. Again a conventional BC109 pair is used with d.c. stabilization and a negative feedback equalization network between Tr2 collector and Tal emitter to obtain the correct R.I.A.A. response for magnetic cartridges. The actual response curve was

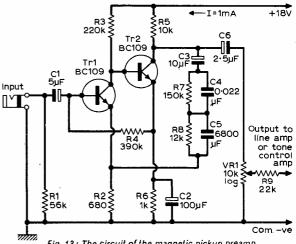
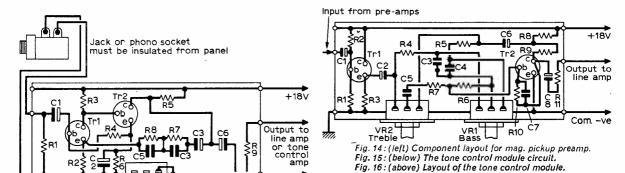


Fig. 13: The circuit of the magnetic pickup preamp.

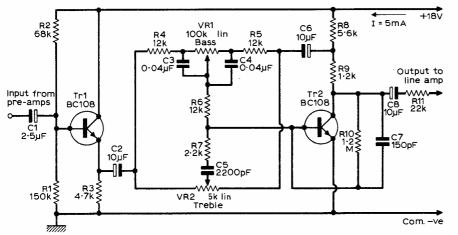
+18V

Output to line amp

or tone



Com. --ve



given in Part 1. The output, via VR1 and R9, is again as common to all the preamps. The input sensitivity is approximately 5mV and the overload margin at least 10 times this. The circuit board layout and wiring is given in Fig. 14.

THE TONE CONTROL UNIT

This has unity gain and an input sensitivity of 100mV so the output is therefore 100mV. The tone control unit will accept the outputs from any of the preamps and one or more may be connected to its

★ components list

	Carbon lin. pot. Carbon lin. pot. Carbo
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	earbon lin. pot. R9 1·2kΩ R10 1·2MΩ Ω R11 22kΩ
Resistors R1 $1 M \Omega$ R6 $390 k \Omega$ Resistors R2 680Ω R7 $1 k \Omega$ R1 $150 k \Omega$ R5 $12 k \Omega$ R3 $100 k \Omega$ R8 $10 k \Omega$ R2 $68 k \Omega$ R6 $12 k \Omega$ R4 $220 k \Omega$ R9 $22 k \Omega$ R3 $4.7 k \Omega$ R7 $2.2 k \Omega$ R5 $220 k \Omega$ R9 $22 k \Omega$ R4 $12 k \Omega$ R8 $5.6 k \Omega$ All $\frac{1}{2} W$, 10% types Capacitors C1 $2.5 \mu F$ $25 V$ C3 $2.0 k \Omega$ R8 $5.6 k \Omega$ C2 $2.5 \mu F$ $25 V$ C5 $5 \mu F$ $25 V$ C2 $10 \mu F$ $25 V$ C5 $200 \mu F$ C2 $10 \mu F$ $25 V$ C3 $0.04 \mu F$ C6 $10 \mu F$ $25 V$ C3 $0.04 \mu F$ C6 $10 \mu F$	R9 1·2kΩ 2 R10 1·2MΩ 2 R11 22kΩ
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R5 $220k\Omega$ All $\frac{1}{4}$ W, 10% types R4 $12k\Omega$ R8 $5\cdot 6k$ All $\frac{1}{4}$ W, 10% types Capacitors C1 $0\cdot 1\mu$ F C4 100μ F 25 V C3 C2 $2\cdot 5\mu$ F 25 V C4 $0\cdot 04\mu$ C C2 $2\cdot 5\mu$ F 25 V C5 5μ F 25 V C2 10μ F 25 V C5 2200μ C C3 100μ F C6 $1\cdot 5\mu$ F 25 V C2 10μ F 25 V C5 2200μ C Magnetic p.u. pre-amp (PU Mag) Ceramic p.u. amp (P Tr1, Tr2 BC109 VR1 $10k\Omega$ Carbon log. pot. Resistors R1 $56k\Omega$ R6 $1k\Omega$ Resistors R1 $56k\Omega$ R6 $1k\Omega$ R2 $470k\Omega$ R5 1.5 R2 680Ω R7 $150k\Omega$ R2 $120k\Omega$ R6 12 R4 $330k\Omega$ R9 $22k\Omega$ R3 $150k\Omega$ R4 $1.5k\Omega$ R8 $100k$ R5 $10k\Omega$ R8 $10k$ $10k$	2
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Magnetic p.u. pre-amp (PU Mag) Ceramic p.u. amp (P Tr1, Tr2 BC109 VR1 10kΩ Carbon log. pot. Tr1, Tr2 BC109 VR1 10kΩ Carbon log. pot. Resistors R1 56kΩ R6 1kΩ Resistors R2 680Ω R7 150kΩ R1 470kΩ R5 1-5 R3 220kΩ R8 12kΩ R2 120kΩ R6 12l R4 390kΩ R9 22kΩ R3 150kΩ R7 12C R5 10kΩ R4 1.5kΩ R8 10k	
Resistors R1 $56k\Omega$ R6 $1k\Omega$ Resistors R2 680Ω R7 $150k\Omega$ R1 $470k\Omega$ R5 1.5 R3 $220k\Omega$ R8 $12k\Omega$ R2 $120k\Omega$ R6 $12k$ R4 $390k\Omega$ R9 $22k\Omega$ R3 $150k\Omega$ R7 $10k\Omega$ R5 $10k\Omega$ R4 $1.5k\Omega$ R8 $10k$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	g. pot.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
R2 680Ω R7 150 Ω 2 R2 120 Ω R6 12I R3 220 Ω R3 150 Ω R7 12 R4 390 Ω R9 22 Ω R4 1.5 Ω R8 10 R5 10 Ω R4 1.5 Ω R8 10	Μ Ω R9 820 Ω
R3 220kΩ R8 12kΩ R3 150kΩ R7 120 R4 390kΩ R9 22kΩ R3 150kΩ R7 120 R5 10kΩ R4 1.5kΩ R8 10kΩ	
R4 390 kΩ R9 22 kΩ R4 1.5 kΩ R8 10 kR5 10 kΩ R8 10 kΩ R8 10 kΩ R8 10 kΩ R9 $\frac{1}{2}$ R9 $\frac{1}{$	
R5 10K12	
All ‡W, 10% types	
	•
Capacitors Capacitors	
Capacitors $C1 = 5\mu F = 25V = C4 = 0.022\mu F = C1 = 0.1\mu F = C4$	
$C2 100\mu\text{F} 25\text{V} C5 6800\text{pF} C2 0.1\mu\text{F} C5$	100μF 25V
C2 100 μ F 25V C3 0000 β F 25V C3 2.5 μ F 25V C3 2.5 μ F 25V	100μF 25V 2·5μF 25V

input. The output from the tone control unit is taken via the passive mixing component R11 so it may, in turn, be connected to the line amplifier together with any one or more preamps. Equally two or more tone control units each accepting a number of preamps may be simultaneously connected to the line amplifier. The circuit for the tone control unit is shown in Fig. 15. (Note that BC108 transistors are used) and the board layout in Fig. 16. The input is taken to the active (negative feedback) network via the emitter follower Tr1. The insertion loss of the tone control network is recovered by the amplifier stage Tr2 but amplification is controlled to obtain unity gain. The frequency response curves for the unit were given in Part 1 but it provides approximately 15dB cut and lift at 40 and 20,000Hz respectively.

PREAMPLIFIER FOR CERAMIC PICK-UP **CARTRIDGES**

The requirements for the preamplifier input are generally similar to those for a crystal pick-up cartridge except that the input sensitivity is higher. The circuit in Fig. 17 provides a high input impedance and a sensitivity of about 60mV. Tr1 is an emitter follower and Tr2 the amplifier with negative

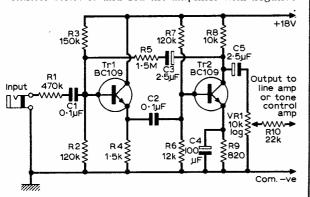


Fig. 17: The ceramic pickup cartridge circuit.

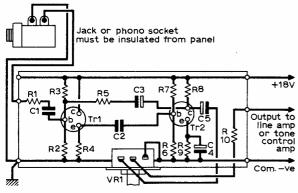


Fig. 18: The layout of the ceramic pickup preamp.

feedback between output and input to obtain the correct gain and wide frequency response. The output is taken via the gain control VR1 and the passive mixing component R10. The circuit board layout is shown in Fig. 18.

TO BE CONTINUED

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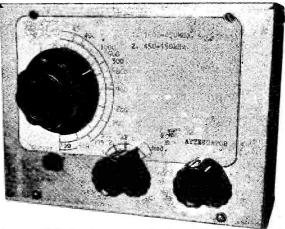
BASID signal generator

R.H.LONGDEN

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- 3. Audio tone.
- 4. Unmodulated signal in the range 150-450kHz. 5. Unmodulated signal in the range 450-1600kHz.
- 1 and 2 are used for the general alignment and testing of receivers, and includes the 455-470kHz i.f. frequencies. 4 and 5 are used for similar purposes



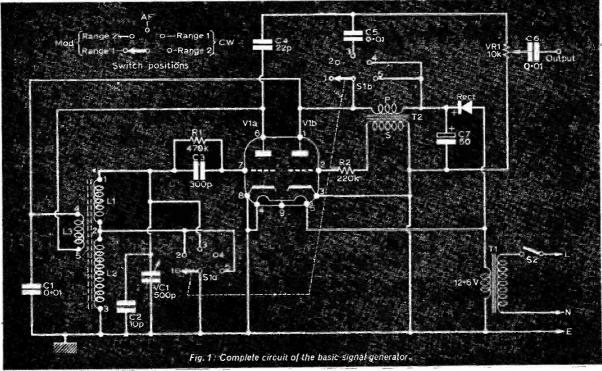
when modulation is not required. 3 allows testing of a.f. stages and amplifiers.

THE CIRCUIT

Figure 1 shows the circuit and uses a single double-triode valve, one section performing as a tunable r.f. oscillator and the other section as an a.f. oscillator. Power is derived from a small $12\cdot 6V$ heater transformer and this also gives a little over 20V d.c. across C7 for the anode supply voltage.

V1a is the r.f. oscillator, tuned by VC1. With S1a in position 1, L1 and L2 are in series, for Range 1 (450-150kHz). With position 2, L2 is shorted, L1 covering about 450-1600kHz, for Range 2. V1b is the a.f. oscillator. Both valve anodes draw h.t. through the primary of T2, thus modulating the r.f. output.

R.F. is taken through C4 to the attenuator or output control VR1. With S1 in position 3, S1a shorts VC1 so that no r.f. is produced, and S1b brings in the larger capacitor C5, the a.f. output of V1b passing to VR1.





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00/28V . 10p | 16+16/450V 25p | 38+28-32/350V 35p 100/28V - 10p | 32+32/350V 25p | 100+56+56/350V439 SUB-MIN. ELECTROLYTICS. 1, 2, 4, 5, 8, 16, 25, 30, 50, 100, 200mF 15V 10p; 500, 1000mF 15V 18p; 2000mP 28V 35p, CERAMIC 1pF to 0-01 mF, 4p, Silver Mine 2 to 5000pF, 4p-APER 3850V-01 4p, 0-8 13p; 1mF 15p; 2mF 150V 15p. 500V-0-001 to 0-05 4p; 0-1 5p; 0-25 5p; 0-47 25p. SILVER MICA Close tolerance 19, 22-500pF 8p; 500-2-200 pF 10p; 2,700-5,600pF 20p; 6,800pF-0-01, mid 30p; each. TWIN GARG. (4-0.0" 208pF+176pF, 65p; Slow motion drive 365+365 with 28+25pF, 50p 500pF dlow motion, standard 45p; small 2-squp 550pF, 21:10. STORT WAVE. Single 25pF 55p CHROME TELESCOPIC AERIAL, swived base, 23in. 20p. TINING. 512-28pF 50p 20pF, 10p; 100pF, 10pF, 50pF, 35p 280pF, 10p; 300pF, 10p; 750pF 10p; 1250pF 10p. TINING SILVERS CONTACTOLOLED 1 wave 60mA 38 p; SSMA 48p, SILICON BYZIS 30p; BY100 30p; BY127 30p. EX-GOVERNMENT RECTIFIERS CONTACT COOLED 1 wave 60mA, 30p. REON PANEL INDICATORS 250V, 200mA, 30p. REON PANEL INDICATORS 250V, 200mA, 30p. HIGH STABILITY. 1 w. 2% 10 ohms to 1 mes., 10p. WIRE-WOUND RESISTORS 5 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 100K. 10p each; 2 watt, 10 watt, 15 watt, 10 ohms to 10

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2N1305 25p BC135 20p MJE2955 2N1306 25p BC136 22p £1:37	7403 Quadruple 2-input Positive NAND Gates (with open collector output) 7404 Hex Inverters 20p 18p 15p 13p 20p 18p 15p 13p	100 + 17p 100 + 17p 500 + 15p 500 + 15p
2N1307 25p BC137 25p MJE305587p 2N1308 25p BC138 25p MPF102 42p 2N1309 25p BC147 17p MPF103 35p	7405 Hex Inverter with open collector 20p 18p 15p 13p 7410 Triple 3-input Positive NAND Gates 20p 18p 15p 13p	2N3055 75p 2N3819 Texas 35p
2N1613 22p BC148 12p MPF104 37p 2N1711 25p BC149 20p MPF105 40p	7420 Dual 4-input Positive NAND Gates 20p 18p 15p 13p 7430 8-input Positive NAND Gates 20p 18p 15p 13p	Mullard 115watt 25 + 30p Silicon Power 100 + 25p
2N2160 60p BC157 20p NKT27720p 2N2218 20p BC158 17p NKT40375p	7440 Dual 4-input Positive NAND Buffers 20p 18p 15p 13p 7441 BCD to decimal nixte driver 87p 77p 66p 60p	25 + 65p 100 + 50p 1000 + 18p
2N2219 20p BC159 20p NKT40462p 2N2222 20p BC169C 15p OA5 20p	7447 BCD-Seven-Segment Decoder/Drivers (15-V Outputs) £1.40 £1.30 £1.20 £1.05	BFY90 65p 2N2646 40p 1000 MC/S Motorola
2N2369 20p BC178 25p OA10 25p 2N2484 35p BC179 27p OA47 10p	7450 Expandable dual 2-input AND-OR-INVERT 20p 18p 15p 13p 7451 Dual 2-wide 2-input AND-OR-INVERT GATES 20p 18p 15p 13p 7493 Quad 2-input Expandable AND-OR-INVERT 20p 18p 15p 15p 18p	25 + 60p Unitunction 100 + 55p 25 + 35p 500 + 50p 100 + 30p
2N2646 50p BC182L 12p OA70 10p 2N2904 20p BC183L 12p OA73 10p 2N2904A25p BC184L 15p OA79 10p	7454 4-wide 2-input AND-OR-INVERT Gates 20p 18p 15p 12p 7460 Dual 4-input Expander 20p 18p 15p 12p	500 + 25p
2N2905 25p BC212 12p OA81 10p 2N2906 20p BCV30 25p OA85 12p	7470 Single-phase J-K Flip-Flop 35p 32p 25p 25p 25p 7472 Master-slave J-K Flip-Flop 35p 32b 25p 25p 25p 7473 Dual Master slave J-K Flip-Flop 43p 40p 37p 33p	AF139 30p Siemens V.H.F. AF186 40p
2N2906A25p BCY31 30p OA90 10p 2N2907 23p BCY32 50p OA91 7p 2N2926 10p BCY33 25p OA95 7p	7474 Dual O type Flip-Flop 43p 40p 37p 33p 7475 Quad latch 47p 45p 43p 40p	25 + 25p Mullard V.H.F. 100 + 22p 25 + 35p 500 + 19p 100 + 30p
2N3011 25p BCY34 80p OA200 7p 2N3053 20p BCY38 40p OA202 10p 2N3084 50p BCY39 55p OCL8 50p	7480 Gated Full Adders 87p 77p 67p 60p 7481 16-bit read/write memory £1.35 £1.25 £1.15 £1.00	OC170 Mullard 25p
2N3055 75p BCY40 50p OC20 97p 2N3525 BCY58 25p OC22 50p	7482 2-5R Binary Full Adders £1:30 £1:20 £1:00 85p 7483 Quad Full Adder 87p 77p 67p 60p 7486 Quad 2 input Exclusive OR Gates 80p 70p 60p 50p	25 + 21p BYZI3 25p 100 + 17p ByZI3 25p Mullard 6a 200v
\$1.10 BCY59 25p OC23 80p 2N3702 10p BCY70 15p OC24 80p 2N3703 10p BCY71 20p OC25 37p	7490 BCD decade counter 87p 77p 67p 60p 7491 8-bit Shift Registers £1:21 £1:00 87p 75p	500 + 15p 100 + 17p 100 + 17p 500 + 15p
2N3704 15p BCY72 15p OC26 25p 2N3705 15p BCY78 30p OC28 60p 2N3707 15p BCY79 30p OC29 60p	7493 4-bit Binary Counters 87p 77p 67p 60p 7494 Dual entry 4-bit shift register 87p 77p 67p 60p 60p	OCI71 Mullard 30p 500 + 15p 25 + 27p 100 + 22p BCI07, BCI08,
2N3709 10p BCZ10 35p OC35 50p 2N3710 10p BCZ11 45p OC36 60p	7496 5-bit Parallel in parallel out Shift Begister 87p 77p 67p 60p 74100 8-bit Blatable Laiches 91-25 41-65 91-65 90p	BCI09 12p each
2N3819 35p BD112 50p OC41 25p 2N3820 60p BD121 65p OC42 30p 2N4058 15p BD123 80p OC43 40p	74118 Hex Set-Reset Latches £1:30 £1:20 £1:00 85p 74121 Monostable Multivibrators 87p 77p 67p 60p	BY (27 Mullard 20p I.T.T. Planars 1000v I amp Plastic 25 + 11p 25 + 17p 100 + 10p
2N4061 15p BD124 75p OC44 17p 2N5457 35p BD125 50p OC45 15p	74145 BCD-to-Decimal Decoder/Drivers £1.80 £1.70 £1.60 £1.50 74151 8-bit Data Selectors (with Strobe)	100 + 15p 500 + 8p 500 + 13p
2N5458 37p BD131 75p OC76 12p 2N5459 50p BD132 85p OC71 15p 28301 50p BD153 62p OC72 25p	74153 Dual 4-Line-to-1-Line Data Selectors/Multiplexers 21-40 21-30 21-20 21-05 74191 Binary Counter reversible £2:50 £2:50 £2:50 £2:00 £1:50 Devices may be mixed to qualify for quantity price.	BC113 SGS 15p Mullard Photo
28302 50p BD156 57p OC73 30p 28303 60p BDY10£1:25 OC74 30p 28304 75p BDY11£1:62 OC75 25p	Devices may be mixed to quality for quantity price 10p. (Ref No. 30). Larger quantity prices Extn. 4. Dual Inline 14 Pin Socket 30p each 16 Pin 35p each.	25 + 13p 25 + 85p 100 + 11p 100 + 80p 500 + 9p 500 + 75p
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AF180 52p BFY51 20p ZTX301 15p F AF181 42p KFY52 22p ZTX302 20p (SILICON) SIZE 1 x 1 x 1 ins. SC35D 400 3 amps 41.00 85p 75p	0C44 Mullard 17p 100 + 17p 500 + 15p 1000 + 13p
ASY26 25p BSX20 17p ZTA 300 20p 1	Cur- Vpe P.I.V. ren 1-49 50+ 100+ 500+ Street 1-49 50+ 100+ 500+ SC40A 100 6 amps \$1.00 85p 75p SC40B 200 6 amps \$1.20 £1.00 85p SC40D 400 6 amps \$1.20 £1.00 85p SC40D 400 6 amps \$1.20 £1.00 85p	100 + 13p 500 + 11p 1000 + 10p 0C84 25p
A8Y27 32p B8X21 20p ZTX501 25p A8Y28 25p B8X76 15p ZTX502 25p 4	002 200 2 amps 70p 65p 60p 55p SC45A 100 10 amps £1.25 £1.10 £1.00 ** 002 400 2 amps 80p 75p 70p 65p SC45B 200 10 amps £1.35 £1.20 £1.10 (25 + 20p 0Cl39 Mullard 25p 100 + 17p
ASY67 47p BSY95A 15p ZTX504 40p ASZ21 42p BY100 15p ZTX531 30p 4	004 100 4 amps 70p 60p 55p 50p 8CG9A 400 10 amps ±1:50 ±1:58 ±1:20 004 200 4 amps 75p 70p 65p 60p 8CG9A 100 15 amps ±1:50 ±1:5	25 + 20p 100 + 17p 500 + 15p
BA164 10p BY127 20p DISCOUNTS 6	002 600 2 amps 90p 80p 75p 70p 8C30D 400 18 amps £2:00 £1:75 £1:60 004 600 4 amps 90p 80p 75p 70p 8C40E 500 6 amps £1:50 £1:25 £1:10 006 100 6 amps £1:50 £1:25 £1:40 €1:25 £00 £1 amps £1:50 £1:25 £1:40 €1:25 £00 £1 amps £1:50 £1:25 £1:40 €1:25 £1	AF239 42p OC81 Mullard 25p 25 + 35p
BAX16 7p BYZ10 40p 15% 25+ 2 BAY31 7p BYZ11 35p 20% 100+ 4	006 200 6 amps 80p 75p 70p 65p SC50E 500 15 amps £2.25 £2.00 £1.75	25 + 20p 100 + 30p 100 + 17p 500 + 25p
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Positions 4 and 5 of S1 give r.f. coverage as for positions 1 and 2, but S1b shorts the primary of T2, so that an audio tone is no longer present to modulate the output. C6 is an isolating capacitor for external circuits.

THE R.F. COIL

This is wound on a ferrite rod about 5in. long and ${}^3{}_8$ in. in diameter, which gives a higher Q and requires fewer turns than an air-cored inductor. All windings are of 32 or 34s.w.g. enamelled wire and are wound on thin tubes made by winding paper round the rod. L1 and L2 can then be slid along to adjust band coverage if necessary.

* components list

Rt	470ks) FW, 10%
R2	298k7 [W, 10%
VRt	10kQ pot with switch
	0-01uF 250V disc ceramic
C)	
C2	10pF silver mice
C5	500pF silver mica
C4	22pF sliver mica
C5	0.01µF 250V disc ceramic
CB	0-01µF 350V disc ceramic
C7	50 ₄ F.60V electrolytic
VC1	500nF Jackson variable
51	2-pole, 8-way rotary switch
71	240V, 12 6V, 0 5A or similar heater frana- former
7/4	ECC82
RSA	valve holder: Rectifier, GJSM or symbar (BY100
	o): T2: Radiospares intervalve, 8mA / 3 ratio;
	e rod, enamelled wire, tag strips, knobs, etc.;
	Two 5 x 2m and two 7 x 2m, universal chassis
	od members, two 5 x 7m, flat plates (Home
Radio	

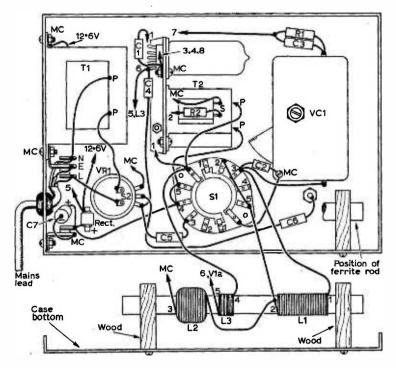
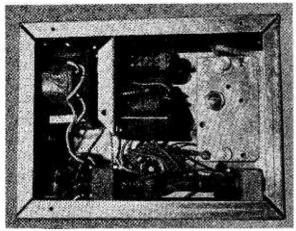


Fig. 2: Wiring details and the construction of the r.f. inductor.



An internal view of the completed prototype; compare this with Fig. 2.

The ends of the windings can be secured with cotton or adhesive tape. After construction is finished, and coverage has been checked, windings and ends are secured using clear *Bostik*, as any movement here will upset dial calibration.

A space of about ${}^{3}4$ in. is left to the end of the rod, and L1 is commenced at point 1. Seventy turns are wound on, side by side, and the wire is fixed at point 2. The beginning of L2 is about ${}^{13}4$ in. from the other end of the rod. L2 is wound in a compact pile about ${}^{5}8$ in. long, and has 140 turns. End 3 of L2 will thus come about ${}^{11}8$ in. from this end of the rod. L3 has 25 turns side by side and is about ${}^{1}4$ in. from L2.

The end of L1 and beginning of L2 are soldered together to form point 2. Windings must be in the same direction, as shown. Leads to L3 must not be reversed or feedback will be in the wrong phase.

A.F. INDUCTOR

The transformer listed can easily carry the required primary current but other transformers could probably be used, though not transistor types. When the generator is first tested, set S1 at position 3, and listen for an audio output, either with phones or by taking a lead to an amplifier. If no tone is heard, reverse secondary connections to T2.

R2 raises the pitch of the tone produced and may be changed in value if necessary. Should an available transformer produce a tone of too high a pitch, this can be altered by connecting a capacitor of about $0.01\mu\text{F}$ (or as found necessary) across the primary or secondary.

CONSTRUCTION POINTS

The complete generator occupies a case $7\times5\times2in$. deep, made by assembling $7\times2in$. and $5\times2in$. "universal chassis" flanged members. The panel is a $7\times5in$. plate, and most of the construction is upon this, and on a $2^1_2\times2in$. chassis bolted to the panel. The chassis is most easily made by cutting a 2^1_2in . length from a 2in. wide flanged universal chassis member.

Mount components on the panel in the positions shown in Fig. 2. Countersunk screws hold VC1 to the panel. Fit the valveholder and T2 to the small chassis, and bolt this to the panel, also with countersunk screws

All wiring except for the r.f. inductor, mains transformer T1, rectifier, and C7 can now be done.

One 5×2 in. flanged member is then drilled to take T1, and a grommet for the 3-core mains lead. The lead is anchored at a 3-tag strip. Equip the lead with a 13A type 3-pin plug having a 2A or 3A fuse. Use brown (or red) for L, which runs to S2, and blue (or black) for N, which is connected to the primary of T1. Yellow-green (or green) is for the earth or metal box connection.

The rectifier is supported on an insulated tag. When this part of the wiring is finished, assemble the top, bottom and sides of the case, securing them with bolts through the perforated flanges provided. The panel is then fitted in place and fixed with four bolts.

The leads from the tag-strip to S2, T1 to S2, and other circuit points can now be soldered on. All wiring is finished except for the r.f. inductor.

The ferrite rod is mounted by drilling two pieces of wood to take it and when in position it should be about 58 in. clear of the bottom of the case. Screws pass up through the bottom member into the wooden mounts. Insulated sleeving is fitted onto the wire ends of the windings, which are scraped and soldered to the various connecting points.

Coverage can be checked by taking a lead from the output socket and placing this near a receiver, or near a short wire connected to the receiver aerial terminal. Note that the two bands obtained should overlap, giving continuous coverage from about 1600kHz to 150kHz. This means that with S1 in position 2, and VC1 fully closed, the signal should be heard at the high frequency end of the long wave band of the receiver, or that with the generator switch in position 1, and VC1 fully open, the signal should be tuned in at the low frequency end of the receiver medium wave band. If necessary, slide L1 or L2 along the rod to achieve this, then cement the windings in place.

C2 in parallel with VC1 enables dial readings at the extreme minimum position of VC1 to be rather less crowded, so that frequencies around 1600-1400kHz can be more easily read.

All connections should be quite short and rigid. The flanged top and sides of the case allow a 5×7 in. plate to be fixed on using self-tapping screws.

SCALES

VC1 can have a fairly large knob with a pointer, or with a hair-line or cursor. Frequencies are read on two semi-circular scales drawn on thin card which can be cemented to the front of the case. The scales may be covered with transparent material for protection after calibration, or a piece of thin perspex, 7×5 in., can be bolted on to cover the whole front.

CALIBRATION'

The simplest method of calibration is to plug a lead into the generator output socket and place this near a receiver, or its aerial or aerial lead. The receiver is then tuned to known frequencies, the generator is tuned to the same frequency and its scales are suitably marked. Alternatively, if a calibrated generator is available, tune both generators to the same frequency, by means of the receiver, and calibrate the scales.

A very good guide to markings can also be made by temporarily fitting a 0-100 scale, and preparing a graph with the aid of stations of known frequency. Round figures for the generator can then be read from the graph, and marked on the scales.

HARMONICS

It is also possible to secure good calibration of the generator with an ordinary long and medium wave band receiver, using harmonics. This depends on the fact that if the generator is set to some particular frequency F, harmonics of this frequency will be heard on the receiver, at Fx2, Fx3, and other multiples. These grow weaker as the multiplier increases, the upper limit depending on receiver sensitivity. For this method, the following steps should be followed:—

- 1. Tune receiver (R) to 200kHz (BBC Radio 2).
- 2. Tune signal generator (SG) to this and mark scale 200kHz.
- 3. Leave SG untouched. Tune R to find Fx3, or 600kHz.
- Leave R untouched. Tune SG to 600kHz and mark scale.
- 5. Tune SG to 300kHz and mark scale. (R is at Fx2.)
- 6. Leave SG tuning untouched. Tune R to 300kHz.
- 7. Tune SG to 150kHz and mark scale. (R is at Fx2.)
- 8. Tune R to 200kHz and SG to 200kHz.
- 9. Tune R to Fx3, or 600kHz.
- 10. Tune SG to 600kHz.
- 11. Leave SG untouched and tune R to Fx2, or 1200kHz.
- 12. Leave R untouched and tune SG to 1200kHz. Mark scale.
- 13. Leave R untouched and tune SG to 400kHz. Mark scale. (R is at Fx3.)
- Tune SG to 200kHz and receiver to Fx5, or 1000kHz.
- Leave R untouched. Tune SG to 500kHz. Mark scale. (R is at Fx2.)

By proceeding in this way, calibration points can be found through both bands, including frequencies outside the normal coverage of the usual 2-band receiver. For accuracy, obtain all reference points by tuning originally to zero beat with BBC Radio 2 on 200kHz, as at (8) not relying on visual readings of the 200kHz mark or other signal generator or receiver calibration markings.

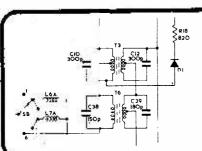
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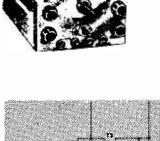
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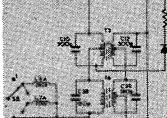


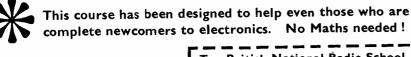
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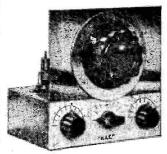
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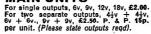
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MONTHLY NEWS FOR DX LISTENERS

HE first reporter this month is **Terry Gibbs** of Swindon who uses a Murphy 'Overlander' receiver and a long-wire which he has recently extended to 500 feet. This equipment enabled him to hear:—

3905 New Hebrides B.C. in broken English at 0700.

4895 Mauritius B.C. in English at 1800.

4895 R. Malaysia in vernacular at 1240.

4926 R. Bata, Guinea (Equat.) at 2300.

4975 R. Timbira, Brazil in English at 2330.

6055 R. Continental, Peru at 0600.

9610 VLX9, R. Perth, Australia at 1200.

11835 4VEH, R. Haiti in English at 2345.

Philip Nichols of Longlevens, Gloucester has an Eddystone 830 receiver and a 50 foot long-wire at 19 feet helping him to hear:—

6010 RT Belge, in French at 1506.

9630 R. Sweden with sign-on at 1100.

9555 CBC, Canada in French at 1830.

9582 R. Australia in English at 1832.

10530 Alma Ata in German at 1740.

11620 AIR, Delhi in English at 1820.

15200 Nigeria noted at 1835.

15265 R. Afghanistan in English at 1815.

15345 R. Kuwait in English at 1730.

21460 HCJB, Quito, Ecuador in English at 1900.

21495 R. Portugal in English at 0840.

21690 WIBS, Windward Is. at 2124.

A new reporter this time is Ian Alexander Kelly of Bulawayo, Rhodesia. Ian's equipment is best described in his own words: "My equipment comprises of two radio receivers, a 5-band a.m./f.m. supersonic PR127 (11 transistor) and a 6-transistor, 3-band home-made regeneration receiver. There are four different types of antenna systems which I use, there is a 100 foot inverted 'L' aerial; a 200 foot centre-top aerial; a 9 foot telescopic aerial and the internal telescopic aerial on the 5-band set." That impressive line-up enabled him to hear:—

2306 RSA, South Africa at 2045.

3250 Lourenco Marques, Mozambique at 2100.

3295 R. Lusaka, Zambia with news at 2105.

9410 BBC World Service to Europe at 2056.

9505 R. Belgrade, Yugoslavia at 2010.

11815 NHK, Japan in English at 1600.

11935 R. Portugal in Portuguese at 1830.

11980 R. Prague, Czechoslovakia at 1815.

15350 ORTF relay from Brazzaville (Congo), 2028.

15400 Ulan Bator, Mongolia at 2345.

15600 Manila, Philippines at 1335.

21501 R. Accra, Ghana at 1500.

21520 SBC, Berne, Switzerland at 1900.

Another new reporter is Ronald L. J. Winson of Reading whose equipment consists of a Codar CR70A and an 80 foot long-wire antenna.

6020 R. Nederland in Spanish at 2130.

11970 R. Bucharest, News in Spanish at 2130.

15295 Sweden Calling DXers at 0000.

15325 CBC, Canada in English at 2115.

21700 Vatican Radio with News at 1245.

Ross Pullen of Crawley has added an 18 foot vertical aerial and had his Murphy A72 re-aligned giving the following results:—

THE BROADCAST BANDS

Malcolm Connah

9510 RTA, Algeria in French at 1215.

9575 Gronlands Radio (Greenland) in Danish at 2207.

11735 R.T.V. Morocco in English at 1720.

15018 Hanoi Radio in English at 2000.

15115 KBS, Seaul in English at 0630.

15115 R. diff. de Sao Paulo, Brazil at 2335.

15170 ELWA, Liberia in French at 2040.

15200 Nigeria in English at 0735.

Neil Smith of Sutton Coldfield used his Unica UNR-30 receiver and a 170 foot long-wire to hear the following stations:—

7100 RSA, South Africa in English at 1900.

7108 R. Budapest in English at 1900.

9620 R. Belgrade, Yugoslavia in English at 2312.

9615 Vatican Radio in English at 2154.

9770 Austrian Radio in English at 1130.

Tony Alcock of Bath has a Codar CR70A receiver and a Joystick antenna which helped him to hear:—9620 Radio Belgrade, Yugoslavia at 2200.

9805 R. Cairo, U.A.R. noted at 2235.

9833 R. Budapest, Hungary.

11060 Radio Vilnius, Lithuanian SSR. at 2240.

11740 Vatican Radio noted at 2045.

11765 Radio Australia noted at 0845.

15345 Kuwait B.S. at 1723.

17810 R. Nederland, Bonaire relay at 2230.

17825 Radio Sofia, Bulgaria at 1920.

News

Peter Reed of Brighton has a R1155N receiver and a Joystick antenna. Peter used his equipment to send in several items of news including:—

Finland: Radio Finland can be heard from 2000 to 2100 on the following frequencies: 9530, 11755 and

15185.

Ceylon: The Ceylon Broadcasting Corporation transmits to Asia at 0212 on 15120 but the broadcast can be heard in this country.

can be neard in this country. **Tahiti:** Faint signals have been picked up from

Radio Tahiti on 11825 at 1630.

Turkey: Radio Ankara has been heard broadcasting at 2300 on a frequency of 15160.

Reports should arrive by the 15th of the month and be addressed to the author at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex.

T'S happened! A log has been received for 70cm. Honours for being first go to Nick Richardson (Wendover, Bucks) who has a 46-element multibeam at 33ft. Receiving line-up is a BF180 preamp, AF239 converter, i.f. amp. and a Trio 9R59DE tuning 28-30MHz. The log shows the great majority of stations using a.m. on 70cm. Callsigns logged include: G2RD, G2FNW, G3BNL/P, G3COJ, G3DAH, G3EHM, G3HAZ, G3HXS, G3KEQ, G3KMS, G3LQR, G3LTN, G3ZYC, G5QA, G5UM, G6GN, G8ACN, G8AMG, G8ANZ, G8ARC, G8ATS, G8AZU/P, G8BBB, G8BGC, G8BII, G8BQH, G8BSH, G8CIT, G8DDC/P, G8DXJ/P, G8EFX/P, G8ERW, G8APZ/P (Merionethshire), GW8AWS/P (Flintshire).

Down on 144MHz, Nick uses an 8-element Yagi at 28ft. feeding an f.e.t. preamp, Garex converter, i.f. amp into the 9R59DE. Goodies on 2 metres were: DL1XJ, ON5NY, GW3GIZ, PA0BDH, PA0CBN, PA0DTC, PA0RLS, PA0TLX, PA0UVP all s.s.b. On a.m., 144MHz sigs. were received from: DL0DD, DK1OV, F1AOY, F1BCI, F3LP, ON5UI, PA0DMS.

"I am 12 years old," claims **Paul Dumpleton** of Dunstable. Paul uses a Cossor domestic receiver and a television aerial "mounted on the chimney." The log shows plenty of EU activity on 14MHz such as DJ, DK, DL, DM, EI, F, HA, HB9, I1, LA, OH, OK, ON, OZ, SM, UA and YU. From further afield: DU4CC, ET9SPI, KANKI, K6YRD, VU1HH, VK3AP, WA6EGL, 4U1ITU, 9HIBG, 9K2AM, which is pretty good going no matter how old you are.

Stephen Hopkins (Gloucester), admits that "... this is the first report I have sent." Receiver is a H.A.C. DX Mk2 with a "slight modification." Antenna is 40ft. end-fed and raised EI9Q on 3·5MHz, F6ARC on 7MHz and HB9XUM/M, K1NJE, ON8WF/A, and W2BLQ on 14MHz s.s.b.

Stephen Terry writes from Banbury to take me to task for my remarks about the l.f. bands and DX. He includes the following callsigns as evidence of 80 metre activity: FP8CT, JY1/B, LU7AAC, OY7JD, PJ2CW, PY3APH, PY7AF, VE1AM, VE1ZZ, VE2XD, VE3FXT, VO1FG, ZS1MH.

Even dreaded 7MHz was persuaded to reveal signals from: CX7AP, HK3LT, PZ1AX, TF5TP, UW9AF, VP2AA, YV1BI, YV5CYA. All are s.s.b. and received on a Lasky's Skyrover MkII with a 120ft. end-fed.

Alan Newman, G8CXC (Portsmouth) used an HW17 transceiver on 144MHz to work PA0—RKS, PVC, CSL, ON5RE. Antenna is a 14-element Parabeam at 21ft. although Alan says he is at zero feet a.s.l. On 80 metres s.s.b. using 9R59DS, Alan logged CT2AK, FP8CT, FP0CA, KP4AN, KV4FZ, LU7AAC, PJ2CW, PZ1AX, PY1HA, PY3CIQ, PY7AF, PY0PK, TF3EB, WA6EGL/P/TF, VE1AAN, VO1AR, WA1KK, WA3WFJ, ZB2CC, ZP3AQ. Having received these (plus a long list of others) in some 3 hours of listening time, Alan is sold on 80 as a DX band and

THE AMATEUR BANDS David Gibson, G3JDG

Frequencies in kHz • Times in GMT

is now polishing up his c.w.

Another first-timer with a log for this column is **David Bettington** (Upton) who has a CR150 which, he claims, "... is older than I am." A 20 metre dipole just fits into the loft-shack and gave s.s.b. messages from: JH10MS, KP4DEY, OX3OJ, VP2MF, WA2OYP/MM. 4X4OH.

Richard Mortimore (Cardiff) can now receive c.w. at 20w.p.m. His log for 21MHz (c.w., of course) reads: CO2FC, EL2CB, JA4ONC, JA5FQU/MM, JH1WKS, JH1YCW, K9YXA, LU9FAN, PY1KEK, WB6VVZ/MM, YV4AQ, 3A0ML, 4Z4KKI. Receiver is a 9R59DS and antenna is a 60ft. long wire.

Tom Brosnan (tnx QSL OM) uses a Windom antenna on 20 metres to feed his JR3LO receiver. Signals received (s.s.b.) include: AP5HP, EQ2BQ, ET3USA, JA1HBC, JA1JTH, JA6YG, KR6JX, T12JU, VU2NH, ZE1DP, 9M8DEA. Fifteen metres s.s.b. revealed: CR6IY, JA6BSM, VQ9R, WB4BFZ, ZS5OV, 5Z4MW, 3V8ZK. QTH is Tadworth in Surrey.

The Modular Three featured in P.W. is the receiver used by M. Evans (Good Evans!) The antenna system consists of unspecified lengths of wire "tangled round the garden and fed to an a.t.u. with a coil former made from a drain pipe," Eighty metre sigs received from: CR7IC, CT1IPS, CT2HK, EA4LH, EL9LS, F0HH/M, JY1, OY2R, OY7JD, PY7AF, VE1IE, VP5KG, VP9GQ, WA6EGL/TF, ZB2CC, ZL3LE, ZL4JFA, ZS1MH, ZS5LB, 3V8ZK, 5Z4KL, 9K2AL.

Good samaritan of the month is G3ZRD who resurrected an ailing B40 belonging to a sad **Crispin Henderson**. Just to show how well things are going now, Crispin sends in a multiband, multimode log. On 160 c.w.: EI8H, EI9J. Signals on 80 s.s.b.: CT1MK, K4QM, VE1IE, W3EFX, W5SZ, W8KEX. Best on 40 c.w. were VK3CC and YV5DRN. Twenty c.w. raised: EA8FE, GM3UYF, HC8GG, HP7KAL, OX3HU, PY7GV, SM0FY, W7HBQ, ZC4CB, ZL2IR, 7Q7AA, 9H1BB. While s.s.b. on the same band was received from: CE3OE, HK1BQR/P7, KZ5OD, OY9LV, VK7MB, 4X4KM, 9K2AM, 9Y4VV. Fifteen c.w.: CR7FM, PY2YCC, Y06KBM, and s.s.b.—KP4AOW, LU5MAO, LU8LH, PY5DI, YV6JB, 4X4GB, 5Z4GK.

Many happenings in October for the keen contest enthusiast. October 9-10, 21-28MHz telephony contest; 9-10, VK/ZL Oceana c.w. contest; 13 (and 27), 70MHz contest; 23-24, 7MHz c.w. contest—well worth a listen; 30-31, 432MHz contest; 30-31, CQ WW phone contest; November 6-7, 144/432MHz c.w. contest; 6-7, 7MHz phone contest; 6-8, CHC/FHC—both phone and c.w.; 7, OK contest.

Logs, in alphabetical order please, to arrive by the 15th of the month to:

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AD 108D MARCONI COMMUNICATION RECEIVER. 9 miniature valves plus Xtal filter and tunable BFO covering 260 to 510 Kc/s and 2 to 18.5 Mc/s in 4 switched bands. Slow motion deal with logging scale. Originally intended for 24v DC operation but supplied with details for conversion to mains. In very clean tested condition. £15 50

12v INVERTER TRANSFORMERS. Complete with circuit build inverter to give 350v output at 300 m/a. £2.20

GEIGER COUNTERS. Well-known contamination meter comprising main unit fitted with meter marked in Milli Rontgens hour, probe lead and carrying case. Audio output available from socket on front panel. Supplied new or as-new condition. Model I fitted with vibrator PSU using 5 pen cell batteries.

MB2/20A TWO METRE TRANSCEIVER. Rx tunable over 2 metre band. 20 watts RF output AM modulated. Ideal for mobile or fixed station. Only requires connection to speaker, aerial and 12v DC supply to become fully operational. Full details on our lists. £50.00

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AMPLIFIERS

TAKE 2®

JULIAN ANDERSON

A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

THE term "general purpose" amplifier is rather a sweeping one; a design suitable for one function may be poor for another. However, the characteristics of the one described here will allow it to fulfil a variety of needs.

The output is in the order of 750mW, peanuts perhaps when compared with the modern day "blockbusters" but still quite sufficient for most purposes. For those who find it hard to relate output in watts to actual loudness, 750mW is the sort of level produced by a large portable transistor radio at full volume, which, of course, is adequate for most purposes. The input impedance of the amplifier is high which gives it far more versatility than low impedance types. It is perfectly O.K. to feed a low impedance source into a high impedance amplifier, though not the other way around. The cheaper sorts of transducers are usually high impedance, such as crystal pickups and microphones.

I hope that no one thinks that I am cheating, for our £1 limit does not include the battery, loudspeaker or the on-off switch; the latter should preferably be incorporated with the volume

control.

THE CIRCUIT

The first stage of the amplifier, represented by Trl, is an emitter follower. This configuration has a very high input impedance, here it is likely to be at least $1M\Omega$ though the actual figure depends on the gain of the transistor used. The volume control, a 5kΩ potentiometer, is directly in the emitter of the first transistor. If you do not require the high impedance input, this complete stage, to-

gether with C1 and R2, can be omitted, coupling the input directly across the volume control, however, although no gain will be sacrificed, it means that the input impedance will only be $5k\Omega$ and this makes it rather less versatile.

The output from the volume control feeds into a fairly conventional driver/complimentary pair audio output stage. Tr2 operates as a conventional amplifier with a collector potential equal to half the supply potential. When the signal swings negative with respect to this potential, Tr4 conducts and Tr3 is held off; when the signal swings positive, Tr3 conducts and Tr4 is held off.

The output appears at the emitters of the two transistors and is coupled via C3 to the loudspeaker.

No. 31

GENERAL PURPOSE AUDIO AMPLIFIER

* components list

Tr1 EN2926 (any colour)	11p
Tr2 2N2926 (any colour)	110
Tra AC176	36p
TH AC128	20p
RI 1MC FW, 5% type	1p
R2 2 2kD	1p
R3 220k()	1p
R4 47hQ	
R5 4702 R6 47002	1p
200 270 VF 407 (200 O CONAY MINER ASSOCIATION ASSOCIAT	. 1p
C1 52F 12V	4p
C2 5µF 12V	4p
C3 180µF 12V	4p
C4 100µF 12V	4p
C5 0 1µF	4p
VR1 5kΩ log. pot.	12p
And the second second second second	00-
Prices are those recently adve	96p
Wireless and may have change	No allowance is
made for minimum order costs or	for nont and nach
ing; these should be checked be	in hear and back-

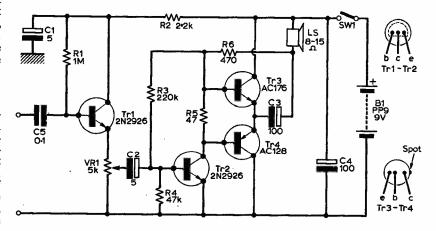


Fig. 1: The circuit of the amplifier.

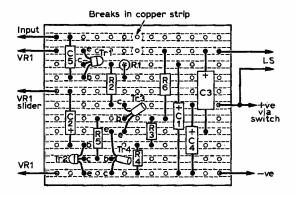


Fig. 2: A suggested layout on Veroboard.

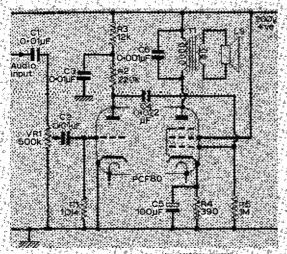
Negative feedback is applied via R6 which is coupled to the "live" side of the speaker. Circuits of this type usually include resistors of 1Ω or 2Ω in the emitters of the output transistors but if the battery supply does not exceed 9V these are not really necessary. If the supply voltage is increased greater output is achieved but the output pair will overheat and eventually blow.

CONSTRUCTION

A suggested layout for the amplifier is shown in Fig. 2, but this is not critical. One point must be carefully checked. If R5 is not connected properly the output transistors will blow instantly, so be especially careful here with regard to dry joints etc. The speaker impedance can vary over a wide range and even 3Ω types work perfectly well though it is better not to go this low and 8Ω is the lowest that should be used for any length of time.



SERVICING-Part 6. October Issue We apologise for the wrong circuit being given in Fig. 1. The correct circuit is shown below.



TESTING SURPLUS PRANSISTORS, October issue. The battery polarity is shown reversed in Fig. 4b.

BINDERS

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Digital Frequency Counter— continued from page 616 switch S2 can now be connected. The temporary wires should be removed.

Overall Check

The crystal oscillator should be allowed to run for about 20 minutes and then the frequency should be checked and set against Droitwich as previously described.

Using an audio oscillator and then an r.f. signal generator check the operation of the counter on signals of various frequencies and amplitudes. The 'LEVEL' control should be adjusted carefully so that the input signal operates the input clipping stage correctly and ensures reliable operation of the counter and display.

The top operating frequency should be in excess of 15MHz and may be as high as 25MHz depending on the integrated circuits used. The time measurement may be checked by measuring the duration of one cycle of the 50Hz mains. A few volts from a mains stepdown transformer is suitable for this. With the function switch in the 'mS' positions, the time of one cycle will be very close to 20mS, depending on the true frequency.

In common with all digital frequency timer/ counters of this type there is always the possibility of an error of one least significant digit. This is due to the input signal not being synchronised with the crystal oscillator from which the counting period is derived. For example, during one counting period n cycles of the input signal may be counted. The next counting period may be very slightly shifted in time with respect to the input signal so that this time n+1 cycles are counted. This error is not present in the internal check, position 6, as here the signal being counted is synchronised with the gate period, one having been divided from the other.

TO BE CONTINUED

TELEVISION

SIMPLE UHF AERIAL PREAMP

A recent transistor, the BF272, is used in a simple circuit housed in a 35mm. film can. The emphasis has been placed on simple construction and minimum expense. The earlier AF139 can be used as an alternative, reducing the cost still further.

SERVICING TV RECEIVERS

Continuing our coverage of chassis widely used in the rental trade, next month we deal with the Plessey/Defiant 9A50-9A52 series.

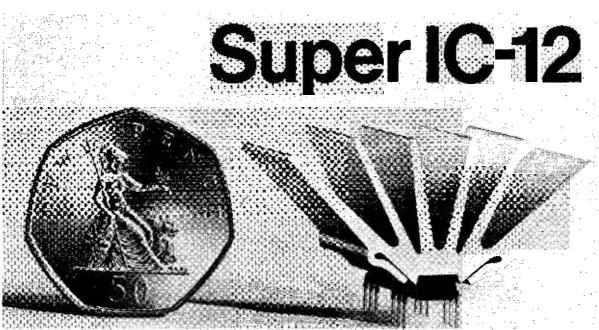
PANORAMIC MONITOR

. . Or things you can do with varicap tuners! These are now readily available and are very versatile. One application highlighted is as a Band monitor-the tuner is swept across the Band and the output monitored on an oscilloscope.

NOVEMBER ISSUE on sale OCTOBER 22nd

We regret that, due to shortage of space. I.C. of the Month and Servicing, Part 7 have had to be held over until next month.





fidelity Monolithic Integrated Circuit **Amplifier**

Two years ago Sinclair Radionics announced the World's first monolithic integrated circuit Hi-Fi amplifier, the IC.10. Now we are delighted to be able to introduce its successor, the Super IC.12. This 22 transistor unit has all the virtues of the original IC.10 plus the following advantages:

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- 3. Lower quiescent consumption.
- 4. Compatible with Project 60 modules.
- 5. Specially designed built-in heat sink. No other heat sink needed
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- 7. Works on any voltage from 6 to 28 volts without adjustment.
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Frequency Response 5 Hz to 100KHz ± 1 dB.

Total Harmonic Distortion Less than 1%. (Typical 0.1%) at all output powers and all frequencies in the audio band.

Load Impedance 3 to 15 ohms.

Power Gain 90dB (1,000,000,000 times) after feedback.

Supply Voltage 6 to 28 volts (Sinclair PZ-5 or PZ-6 power supplies ideal).

Size 22 x 45 x 28 mm including pins and heat sink.

Input Impedance 250 Kohms nominal. Quiescent current 8mA at 28 volts.

With the addition of only a very few external resistors and capacitors the Super IC.12 makes a complete high fidelity audio amplifier suitable for use with pick-up, F.M. tuner etc. Alternatively, for more elaborate systems, modules in the Project-60 range such as the Stereo 60 and A.F.U. may be added. The comprehensive manual supplied with each unit gives full circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include car radios, oscillators etc. The very low quiescent consumption makes the Super IC.12 ideal for battery operation.



Price, inc. FREE printed circuit board for mounting.

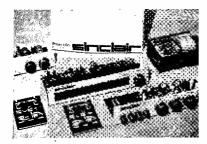
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Project 60



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Project 60 offers more advantage to the constructor and user of high fidelity equipment than any other system in the world.

Performance characteristics are so good they hold their own with any other available system irrespective of price or size.

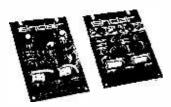
Project 60 modules are more versatile — using them you can have anything from a simple record player or car radio amplifier to a sophisticated and powerful stereo tuner-amplifier. Either power amplifier can be used in a wide variety of applications as well as high fidelity. The Stereo 60 pre-amplifier control unit may also be used with any other power amplifier system, as can the AFU filter unit. The stereo FM tuner operates on the unique phase lock loop principle to provide the best ever standards of sensitivity and audio quality. Project 60 modules are very easily connected together by following the 48 page manual supplied free with all Project 60 equipment. The modules are great space savers too and are sold individually boxed in distinctive white and black cartons. With all these wonderful advantages, there remains the most attractive of all — price. When you choose Project 60 you know you are going to get the best high fidelity in the world, yet thanks to Sinclair's vast manufacturing resources (the largest in Europe) prices are fantastically low and everything you buy is covered by the famous Sinclair guarantee of reliability and satisfaction.

Typical Project 60 applications

System The Units to use together with		together with	Cost of Units
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20 + 20 W. stereo amplifier with high performance spkrs.	2 x Z.30s, Stereo 60, PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90
40 + 40 W. R.M.S. de-luxe stereo amplifier	2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr	As above	£34.88
Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43

from a simple amplifier to a complete stereo tuner amplifier with Project 60 modules

Z.30 & Z.50 power amplifiers



The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well.

SPECIFICATIONS (Z.50 units are inter-changeable with Z.30s in all applications).

Power Outputs

Z.30 15 watts R.M.S. into 8 ohms using 35 volts: 2.30 watts R.M.S. into 3 ohms using 30 volts. 2.50 40 watts R.M.S. into 3 ohms using 40 volts: 30 watts R.M.S. into 8 ohms using 50 volts. Frequency response: 30 to 300.000Hz±1dB.

Distortion: 0.02% into 8 ohms. Signal to noise ratio: better than 70dB unweighted. Input sensitivity: 250mV into 100 Kohms.

For speakers from 3 to 15 ohms impedance. Size: 14 x 80 x 57 mm.

Z.30

Built, tested and guaranteed with circuits and instructions manual. £4.48

Built, tested and guaranteed with circuits and instruc-£5.48

Power Supply Units

Designed special for use with the Project 60 system of your choice. Use PZ 5 for normal Z.30 assemblies and PZ.6 where a stabilised supply is essential.

PZ.530 volts unstabilised £4.98 PZ.6 35 volts stabilised £7.98
PZ.8 45 volts stabilised ss mains transformer) £7.98 PZ.8 mains transformer £5.98



PZ.5

The Sinclair Guarantee

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail. Air-mail charged at cost.

Project 60 Stereo F.M. Tuner





First in the world to use the phase lock loop principle

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. Good reception is possible in difficult areas, and often a few inches of wire are enough for an aerial. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system

SPECIFICATIONS-Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108 MHz. Capture ratio: 1.5dB. Sensitivity: 2µV for 30dB quieting: 7µV for 10ck-in over full deviation. Squelch level: 20µV. A.F.C. range: ±200 KHz. Signal to noise ratio: > 65dB. Audio frequency response: 10 Hz – 15 KHz (±1dB). Total harmonic distortion: 0.15% for 30% modulation. Stereo decoder operating level: 2µV. Cross talk: 40dB. Output voltage: 2 x 150mV R.M.S. Operating voltage: 25-30 VDC. Indicators: Power on/tuning/stereo. Size: 93 x 40 x 207 mm.

Built and tested. Post free.

£25

Stereo 60 Pre-amp/control unit



Designed for Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

SPECIFICATIONS—Input sensitivities: Radio—up to 3mV. Mag. p.u. 3mV: correct to R.I.A.A curve ±1dB:20 to 25,000 Hz. Ceramic p.u.—up to 3mV: Atx—up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE + 15 to —15dB at 10 KHz: BASS + 15 to —15dB at 100Hz.

Front panel: brushed aluminium with black knobs and controls. Size: $66 \times 40 \times 207$ mm. Built tested and güaranteed.

A.F.U. High & Low Pass Filter Unit



For use between Stereo 60 unit and two Z.30s or Z.50s. and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation

in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. Two filter stages – rumble (high pass) and scratch (low pass). Supply voltage – 15 to 35V. Current – 3mA. H.F. cut-off (–3dB) variable from 28KHz to 5KHz. L.F. cut-off (–3dB) variable from 25Hz to 100Hz. Distortion at 1KHz (35V. supply (0.02% at rated output. Size: 66 x 40 x 90 mm. Built tested and guaranteed.

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This elegantly designed shelf mounting speaker brings genuine high fidelity within reach of every music lover.

Specifications:

Construction: Special sealed seamless sound or pressure chamber with internal baffle.

Loading: up to 14 watts RMS. Input Impedance: 8 ohms.

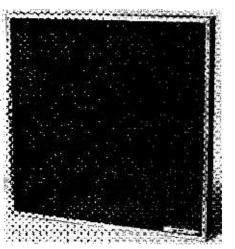
Frequency response: From 60 to 16,000 Hz. confirmed by independently plotted B

and K curve.

Driver unit: Special high compliance unit having massive ceramic magnet of 11,000 gauss, aluminium speech coil and special cone suspension for excellent transient response.

Size and styling: 93 in. square on face x 43 in. deep with neat pedestal base. Black all over cellular foam front with natural solid teak surround.

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Specifications:

Size: $36 \times 33 \times 13$ mm (1.8 x 1.3 x 0.5 in.) Weight: including batteries, , 28.4 gm (1.0z.)

Case: Black plastic with anodised aluminium front panel and spun aluminium dial

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Earpiece: Magnetic type.

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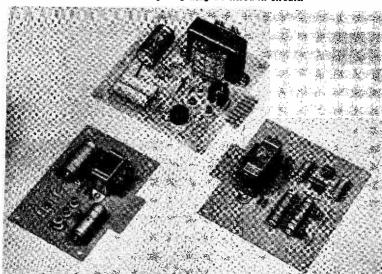
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All units are completely assembled and tested and may be used by plugging in using the edge contact provided. Alternatively they may be wired in circuit.



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400 600	0-48 0-58	0·47 0·57	0-87 0-77	0·75 0·97	0.93 1.25	1.75
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200	0.05	0.09	0.06	0.14	0.20	0.24	1.00		
400	0.08	0.13	0.07	0.20	0.27	0.87	1.25		
600	0.07	0.16	0.10	0.23	0.84	0.45	1.85		
800	0.10	0.17	0.13	0-25	0.37	0.55	2.00		
1000	0.11	0.25	0.15	0.80	0.46	0.68	2.50		

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Code Nos. mentioned above are given as a guide to the type of device in the Pak. The devices themselves are normally unmarked.

Pak	Description	Price
01	00 Pel met trans DNP 4 P	£p
Q1 Q2	20 Red spot trans. PNP AF	0.50
Q3	4 OC77 type trans	
Q4	6 Matched trans. OC44/45/81/81D	
Q5	4 OC75 transistors	0-50
Q6	4 OC72 transistors 4 AC128 trans. PNP high gain	0.50
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Q14 Q15	3 OC171 H.F. type trans	0.50
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Q23	10 OA202 sil. diodes aub-min	0-50
Q 24	8 OA81 diodes	0.50
Q25	6 IN914 sil. diodes 75PlV 75mA	0.50
Q26 Q27	8 OA95 germ. diodes sub-min. 1N69 . 2 10A 600PIV sil. rects. IS45R	0.50
028	2 Sil. power rects. BYZ13	0.50
Q29	4 Sil. trans. 2 × 2N696, 1 × 2N697, 1 × 2N698	
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Q31 Q32	2 DATE all trans 0 V 9N1131	0-50
402	1 × 2N1132	0.50
Q33	3 Sil. NPN trans, 2N1711	0.50
Q34	7 Sil. NPN trans. 2N2369, 500MHZ	0.50
Q35	1 × 2N1132 3 Sil. NPN trans, 2N1711 7 Sil. NPN trans, 2N2369, 500MHZ. 3 Sil. PNP TO-5 2 × 2N2904 & 1 × 2905	0-50
Q36	7 2N3646 TO-18 plastic 300MH2	
400	NPN	0.50
Q37	NPN 3 2N3053 NPN sil. trans.	0.50
Q38	7 PNP trans. 4×2N3703, 3×2N3702	0.50
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Q42	6 NPN trans, 2N5172	0.50
Q43	7 BC107 NPN trans	0.50
Q44	7 BC107 NPN trans. 7 NPN trans. 4×BC108, 3×BC109. 3 BC113 NPN TO-18 trans.	0.50
Q45 Q46	2 BC115 NPN TO-18 trans.	0.50
047	3 BC115 NPN TO-5 trans. 6 NPN high gain 3 × BC167, 3 × BC168	0.50
Q 48	4 BCY70 NPN trans. TO-18	0.50
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BP03 = 7403	Quad 2-input pos. NAND gates			
	(with open collector output)	0-15	0.14	0.12
BP04 = 7404	Hex Inverters	0.15	0.14	0.12
BP05 = 7405	Hex Inverter (with open-collector		·	*
	output)	0.15	0.14	0.12
BP10 = 7410	Triple 3-input pos. NAND gates	0-15	0-14	0.12
BP13 = 7413	Dual 4-input Schnitt trigger	0.29	0.28	0.24
BP20 = 7420	Dual 4-input pos. NAND gates	0-15	0.14	0.12
BP30 = 7430 BP40 = 7440	8-input pos. NAND gates Dual 4-input pos. NAND buffers	0-15	0-14	0.12
BP40 = 7440	Dual 4-input pos. NAND buffers	0-15	0-14	0.12
BP41 = 7441	BCD to decimal nixie driver	0-67	0.64	0-58
BP42 = 7442	BCD to decimal decoder (4-10 lines.			
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D1 00 - 1400	invert	0.15	0.14	0.12
BP51 = 7451	Dual 2-wide 2-input and-or-invert	0-10	0.74	0.75
131 01 - 1401		0.15	0.14	0.12
BP53 = 7453	Quad 2-input expandable and-or-	0.10	0.74	A. TW
DI 00 - 7400	invert	0.15	0.14	0-12
BP54 = 7454				
BP60 = 7460	4-wide 2-input and-or-invert gates	0-15 0-15	0·14 0·14	0-12 0-12
BP70 = 7470	Dual 4-input expander Single-phase J-K flip-flop		0.26	0.24
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BP72 = 7472	Master slave J-K flip-flop	0.29	0-26	0.24
BP73 = 7473 BP74 = 7474	Dual Master slave J-K flip-flop	0.37	0.85	0.82
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BP76 = 7476	Dual J-K with pre-set and clear	0.43	0.40	
BP80 = 7480	Gated full adders	0-67	0.64	0.58
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BP91 = 7491	8-bit shift registers	0.87	0-84	0.78
BP92 = 7492	Divide-by-twelve counters	0.67	0.64	0-58
BP93 = 7493	4-bit binary counters	0-67	0-64	0.58
BP92 = 7492 BP93 = 7493 BP94 = 7494	Dual entry 4.bit shift register	0.77	0.74	0.68
BP95 = 7495	4-bit up-down shift register	0-77	0.74	0.68
BP96 = 7496	5-bit parallel in parallel out shift-			
	register	0.77	0.74	0.68
BP100 = 74100	8-bit bistable latches	1.75	1.65	1.55
BP104 = 74104	Single J-K flip-flop equivalent 9000			
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BP155 = 74155	Dual 2- to 4-line decoder	1.40	1.30	1.20
BP156 = 74156	Dual 2- to 4-line decoder O/C	1.40	1.80	1.20
BP160 = 74160	Sync. decade counter	1.80	1.70	1.60
BP161 = 74161	Sync. 4-bit binary counter	1.80	1.70	1.60
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~~	clock line)	3.50	8-25	3.00
		2.10	1.95	1.75
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BP192 = 74192 BP192 = 74199	Sync, up-down decade counter			
BP192 = 74192 BP193 = 74193	Sync. binary up-down counter (tow		1.05	1.75
BP193 = 74193	Sync. binary up-down counter (tow clock lines)	2.10	1-95	1.75
BP193 = 74193 $BP196 = 74196$	Sync. binary up-down counter (tow clock lines)	2·10 1·80	1-95 1-70	1.60
BP197 = 74197	Sync. binary up-down counter (tow clock lines) Pre-setable 50MHz decade counter Pre-setable 50MHz binary counter	2·10 1·80 1·80	1·70 1·70	1.60 1.60
BP193 = 74193 BP196 = 74196 BP197 = 74197 BP198 = 74198	Sync. binary up-down counter (tow clock lines) Pre-setable 50MHz decade counter Pre-setable 50MHz binary counter S-bit parallel L-R shift register	2·10 1·80 1·80 5·50	1.70 1.70 5.00	1.60 1.60 4.00
BP193 = 74193 BP196 = 74196 BP197 = 74197 BP198 = 74198 BP199 = 74199	Sync. binary up-down counter (tow clock lines) Pre-setable 50MHz decade counter Pre-setable 50MHz binary counter A-bit parallel L-R shift register 8-bit parallel access shift register	2·10 1·80 1·80 5·50 5·50	1.70 1.70 5.00 5.00	1.60 1.60 4.00 4.00
BP193 = 74193 BP196 = 74196 BP197 = 74197 BP198 = 74198 BP199 = 74199 D evices may be m	Sync. binary up-down counter (tow clock lines). Pre-setable 50MHz decade counter. Pre-setable 50MHz binary counter. 8-bit parallel L-R shift register 8-bit parallel access shift register inted to qualify for quantity price. Lars	2·10 1·80 1·80 5·50 5·50	1.70 1.70 5.00 5.00	1.60 1.60 4.00 4.00
BP193 = 74193 BP196 = 74196 BP197 = 74197 BP198 = 74199 BP199 = 74199 D evices may be mapplication (TTL 7	Sync. binary up-down counter (tow clock lines). Pre-setable 50MHz decade counter. Pre-setable 50MHz binary counter. 8-bit parallel L-R shift register 8-bit parallel access shift register inted to qualify for quantity price. Lars	2·10 1·80 1·80 5·50 5·50 ger quan	1.70 1.70 5.00 5.00 tities—pr	1.60 1.60 4.00 4.00

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$UIC03 = 12 \times 7403N$	50p UIC60 = 12 x 7460N	$50p$ UIC86 = $5 \times 7486N$ $50p$
$UIC04 = 12 \times 7404N$	$50p UIC70 = 8 \times 7470N$	$50p$ UIC90 = $5 \times 7490N$ $50p$
$UIC05 = 12 \times 7495N$	$50p UIC72 = 8 \times 7472N$	$50p U1C92 = 5 \times 7492N 50p$
$UIC10 = 12 \times 7410N$	$50p \ UIC73 = 8 \times 7473N$	$50p$ UIC93 = 5×7493 N $50p$
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$UIC40 = 12 \times 7440N$	$50p$ UIC75 = $8 \times 7475N$	50p U1C95 = 5 x 7495N 50p
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BP935	Expandable Hex Inverter				13p	12p	11
BP936	Hex Inverter				13p	12p	11
BP944	Dual 4-input NAND expan-						~
01 011	pull-up				13p	12p	111
BP945	Master-slave JK or RS				25p	240	22
BP946	Quad, 2-input NAND.			***	12p	îin	10
BP948	Master-slave JK or RS				25p	24p	22
BP951	Monostable		• •	4/4	65p	600	55
BP962	Triple 3-input NAND			::	12p	115	10
3 P9 093	Dual Master-slave JK with				40p	38p	35
BP9094	Dual Master-slave JK with				40p	38p	35
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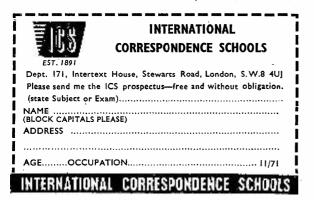
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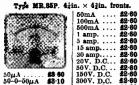
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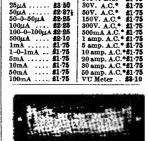
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2N718 25p 2N3645 25p 40251 2N718A 30p 2N3691 15p 40309 2N726 25p 2N3692 18p 40310	82p BC154 85p BFY29 40p NKT281 27p 82p BC157 15p BFY30 40p NKT401 87p 45p BC158 15p BFY41 50p NKT402 90p	CA3028A 74p FJJ251 125p SN7492 87p CA3028B FJL101 125p SN7493 87p 105p FJY101 25p SN7495 87p	6AC7 25p 35Z4 30p PC86 60p 6AG7 40p 35Z5 40p PC88 60p 6AK5 30p 50B5 45p PC97 45p
2N727 25p 2N3693 15p 40311 2N914 17p 2N3694 18p 40312 2N916 17p 2N3702 10p 40314	35p BC159 15p BFY43 68p MKT403 75p 47p BC160 35p BFY50 22p NKT404 62p 37p BC167 15p BFY51 20p NKT405 75p	CA3029 87 IC10 250p SN7496 87p CA3029A IC12 250p SN74107 48p 165p L900 40p SN74153	6AK6 57# 50C5 409 PC900 43p 6AL5 20p 80 50p PCC84 40p 6AM6 83p 85A2 45p PCC85 40p
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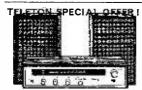
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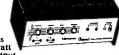
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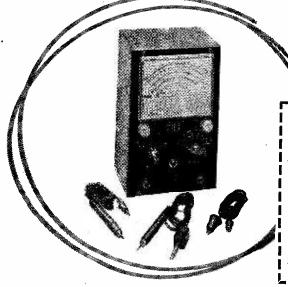
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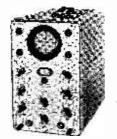
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184	0.30	6BH6 0.75	6J5GT 0.80	12AE6 0.55		TRON	IC VA	LVES	EL81	0.55	PABC800-40	PY31 0.30	UBC81 0.40
185	0.30	6BJ6 0.50	6J6 0.20	12AL5 0.50	ELEV	INVI	10 17		EL83	0.42	PCC84 0.40	PY33 0.68	UBF80 0.40
1T4	0.80	6BK7A 0.60	6J7 0.45	12AQ5 0.50					EL84	0.25	PCC85 0.40	PY80 0.40	UBF89 0.85
104	0.80	6BN5 0.48	6K6GT 0.60	12AT6 0.30					EL85	0.43	PCC88 0.55	PY81 0.30	UBL1 0.60
		6BN6 0.45	6K7 0.85	12AT7 0.35	30C17 0.90	90AG 2.40	DY87 0.83	ECC189 0.65	EL86	0.40	PCC89 0.55	PY82 0.85	UBL21 0.65
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3BP1	8.00	6BW7 0.80	6L18 0.45	12AX7 0.30	30FL14 0.85	813 8.75	EABC800.35	ECH42 0.75	ELL80	0.75	PCF82 0.35	PY801 0.50	UCH42 0.70
384	0.85	6BX6 0.25	6LD20 0.50	12AY7 0.75	30L1 0.40	866A 0.75	EAF42 0.55	ECH81 0.30	EM34	1.00	PCF84 0.60	PZ30 0.35	UCH81 0.40
3V4	0.48	6BZ6 0.40	6N7GT 0.45	12B4A 0.60	30L15 0.85	5642 0.70	EBC33 0.50	ECH83 0.45	EM71	0.80	PCF86 0.60	QQV02-6	UCL81 0.60
		6C4 0.88	6P1 0.60	12BA6 0.40	30L17 0.80	6080 1.60	EBC41 0.55	ECH84 0.45	EM80	0.45	PCF87 0.90	Ž.25	UCL82 0.85
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	0.85	6C5GT 0.40						ECL81 0.50	EM84		PCF802 0.50		UF9 0.60
	0.45	6CB6 0.85	6Q7 0.40	12BE6 0.40	30P19 0.85	6360 1.25	EBF80 0.40			0.35		1.25	
5Y3GT	0.40	6CD6GA1.25	68A7 0.40	12BH7 0.45	30PL1 0.75	6939 2.25	EBF83 0.40	ECL82 0.35	EM85	1.00	PCF805 0.80	QQV03-20A	UF11 0.50
5Z3	0.60	6CG7 0.55	68G7 0.40	12BY7 0.60	30PL13 0.98	7199 0.80	EBF89 0.80	ECL83 0.70	EM87	0.70	PCF806 0.70	5.25	UF41 0.80
6Z4G	0.40	6CH6 0.60	68K7 0.40	12K5 0.70	30PL14 0.90	7360 2.00	EC53 0.50	ECL84 0.55	EN91	0.88	PCF808 0.85	QQV06-40A	UF42 0.60
	0.80	6CL6 0.55	68L7GT0.35	12K7GT0.40	35A3 0.55	7586 1.25	EC86 0.60	ECL85 0.55	EY51	0.40	PCH2000.70	5.50	UF43 0.60
	0.85	6CW4 0.65	68N7GT0.85	1207GT 0.40	35A5 0.75	7895 1.25	EC88 0.60	ECL86 0.40	EY80	0.55	PCL81 0.50	TT21 8.00	UF80 0.85
6AF4A		6CY5 0.45	68Q7 0.40	128R7 0.40	35B5 0.65	9002 0.40	EC90 0.88	ECLL800	EY81	0.40	PCL82 0.35	TT22 3.20	UF85 0.40
			68R7 0.40	20D1 0.50	35C5 0.50	9003 0.50	EC91 0.60	1.65	EY83	0.55	PCL83 0.65	TY2-125	UF89 0.40
	0.40					AZ1 0.55	EC92 0.85	EF40 0.50	EY86	0.40	PCL84 0.45	10.00	UL41 0.65
	0.50	6D3 0.50	6T8 0.85	20L1 1.10	35D5 0.75								
	0.30	6DC6 0.80	6U4GT 0.65	20P1 0.50	35L6GT 0.50	AZ31 0.55	EC93 0.55	EF41 0.65	EY87	0.48	PCL85 0.40	U18/20 0.75	UL84 0.40
6AK5	0.85	6DK6 0.50	6U8A 0.40	20P4 1.10	35W4 0.85	CBL1 0.90	EC8010 2.25	EF42 0.70	EY88	0.48	PCL86 0.45	U25 0.80	UM84 0.25
	0.60	6DQ6B 0.70	6V6GT 0.40	20P5 1.20	35Z3 0.70	CBL31 1.00	ECC40 0.65	EF80 0.25	EZ40	0.50	PCL88 0.90	U26 0.80	UU8 0.60
	0.48	6DS4 0.75	6X4 0.35	25C5 0.50	35Z4G 0.85	CY31 0.85	ECC81 0.85	EF83 0.55	EZ41	0.50	PCL800 0.93	U31 0.60	UY1N 0.50
	0.20	6EA8 0.60	6X5GT 0.40	25L6GT 0.50	35Z5GT 0.60	DAF96 0.45	ECC82 0.30	EF85 0.35	EZ80	0.27	PCL801 0.75	U37 2.10	UY11 1.00
	0.85	6EH7 0.30	6X8 0.60	25Z4G 0.30	50A5 0.75	DF96 0.45	ECC83 0.80	EF86 0.30	EZ81	0.29	PD500 1.30	U52 0.85	UY41 0.48
		6EJ7 0.35	6Y6G 0.70	25Z6GT 0.65	50B5 0.50	DK40 0.60	ECC84 0.30	EF89 0.28	GY501	0.80	PF86 0.65	U76 0.35	UY82 0.50
	0.88					DK92 0.55	ECC85 0.40	EF91 0.38	GZ30	0.40	PF818 0.85	U78 0.35	UY85 0.40
	0.38	6EW6 0.70	7Y4 0.65	30A5 0.50									
6AQ6	0.65	6F1 0.75	9BW6 0.60	30AE3 0.40	50CD6G1.20	DL96 0.45	ECC88 0.40	EF92 0.35	GZ31	0.85	PFL200 0.65	U191 0.75	W729 0.75
6AR5	0.45	6F5 0.75	10C2 0.50	30C1 0.80	50L6GT 0.55	DM160 0.65	ECC89 0.50	EF95 0.35	GZ32	0.48	PL33 0.85	U201 0.35	Z759 2.00
6AR6	0.55	6F6G 0.35	10D1 0.55	30C15 0.80	85A2 0.50	DY86 0.82	ECC91 0.20	EF97 0.65	GZ33	0.70	PL36 0.55	U281 0.40	Z803U 1.20
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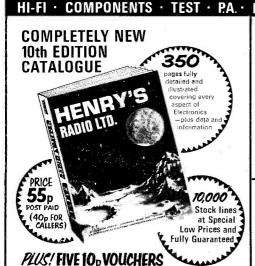
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