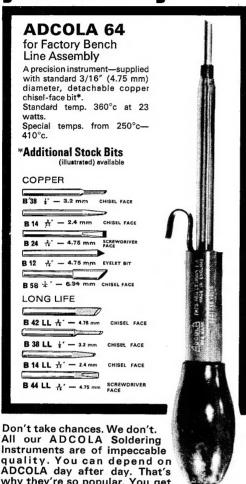
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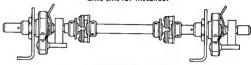
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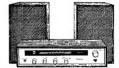
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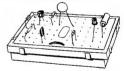
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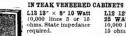
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R.S.C. TAI2 MKIII 6-5 + 6-5 WATT STEREO AMPLIFIER FULLY TRANSISTORISED, SOLID STATE CONSTRUCTION HIGH FIDELITY OUTPUT OF 6.5 WATTS PER CHANNEL

HIGH FIDELITY OUTPUT OF 6.5 WATTS PER CHANNEL.

Designed for optimum performance with any crystal or ceramic fram. P.U. cartridge, Radio tuner, Tape recorder etc. * 3 separate switched input sockets on each channel * Separate Bass and Treble controls * Slide Switch for mono use * Speaker Output 3-15 Johns * For 200-250v. A.C. mains * Frequency Response 20-26,000 c.p.s. — 24B * Harman * Frequency Response 20-26,000 c.p.s. — 24B * Harman * Frequency Response 20-26,000 c.p.s. — 24B * Harman * Separate Distortion 3.9% at 1,000 c.p.s. Hum and Noise 10 Johns * Sensitivities (1) 50mV (2) 10mV (3) 10mV (4) 10mV (2) 10mV (4) 10mV (5) 10mV (6) 10mV (7) 10mV (7)

AUDIOTRINE A55 HIGH QUALITY 5 + 5 WATT OUTPUT

GARRARD 5200 Changer with low mass pick-up arm and Stereo Cartridge. CONTROLS: TREBLE, BASS, VOLUME, STEREO, BALANCE. Operation on 200 200 500

Operation on 200-250v.
A.C. mains.
Output rating. I.H.F.M
A REALLY SURPRISING STANDARD OF QUALITY IS OBTAINABLE FROM THIS COMPACT LOW PRICED SYSTEM

incorporating high flux 8×5 ins. speaker. Size approx. $13 \times 7\frac{1}{2} \times 8\frac{3}{4}$ ins. Price complete £42

STEREO SYSTEM | LOW DEPOSIT **CREDIT TERMS** PAIR OF LOUDSPEAKER UNITS **AVAILABLE ON PURCHASES OVER**

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WITH VISCOUNT FIELD EFFECT TRANSISTORS



This superb stereo system is a real price break through. It comprises the VISCOUNT F.E.T. Mk I amplifier on which full details are given below, the famous Garrard SP 25 Mk III (including teak veneer base and transparent cover) with diamond cartridge or 2025 TC and the very successful DUO type 2 speakers. Measuring 17½in x 10½in x 6½in, the Duo type 2 speakers are teak finished with matching Vynair grills. They incorporate a 3 ohm. 13in x 8in drive unit and Parasitic tweeter. Max. power handling 10 watts. Price £13·50 per pair plus p. &p. £1·50.

Complete stereo system £43 plus £2·50 p. & p. or with Mk II Amplifier and Magnetic Cartridge £48 &£2·50 p. & p.

The Viscount

F.E.T. MkI £14.25 - 50p. p. & p.

High fidelity transistor stereo amplifier employing field effect transistors. With this feature and accompanying guaranteed specifications below, the Viscount F.E.T. vastly surpasses amplifiers costing far more.

Specification-Output per channel 10 watts Specification—Output per channel to watts r.m.s. into 3 ohms Frequency bandwidth 20 Hz to 20 kHz + 1db at 1 watt. Total distortion at 1 kHz at 9 watts 0.5% Input sensitivities CER. P.U. 100mV into 3 meg ohms. Tuner 100mV into 100K ohms. Tape 100mV into 100K ohms. Overload Factor Better, then 26dh Better than 26db.

The £25 Stereo system

The Duetto is a good quality stereo amplifier, attractively styled and finished. It gives superb reproduction previously associated with amplifiers costing far more.

SPECIFICATION ...

R.M.S. power output 3 watts per channel into 10 ohms speakers.

INPUT SENSITIVITY. Suitable formedium or high output crystal cartridges and tuners. Cross-talk better than 30dB at 1Kc/s.

CONTROLS: 4-position selector switch (2 pos. mono and 2 pos stereo) dual ganged volume control. Signal to noise ratio—70db on all inputs (with vol. max). Controls—6 position selector switch (3 pos. stereo and 3 pos. mono). Separate volume controls for left and right channels. Bass \pm 14db at 60 Hz. Treble (with D.P.S. on off) \pm 12 db at 10 KHz. Tape recording output sockets on each channel. Size 12 \pm in. 6in. 2 \pm in. in simulated teak case. BUILT & TESTED.

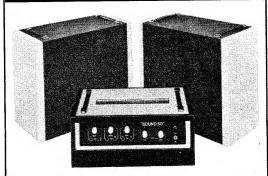
MkII (MAG P.U.) £15.75 plus 50p. p. & p. Specification same as Mk. 1, but with the following inputs. Mag. P.U. CER. P.U. Tuner. Spec. on Mag. P.U. 3mV at 1 kHz input impedance 47K. Fully equalised to within ±1db RIAA. Signal to noise ratio-65db (vol. max).



TONE CONTROL Treble lift and cut Separate on off switch. A preset balance control. Duetto integrated transistor stereo Amp £9.50 50p Garrard Changer from £7.97 50p Cover and teak finish plinth £4.75 50p Duo Type I speakers (see opp. page) £4.20 50p The above items purchased together £25.00 £2.00

SOUND 50

50 WATT AMPLIFIER & SPEAKER SYSTEM



The Sound Fifty valve amplifier and speakers are sturdily constructed with smart housings and thoroughly tested electronics. They are designed to last—to withstand the knocks and bumps of life on the road. Built for the small and medium sized gig, they are easy to handle and quick to set up and can be relied upon to come over with all the quality and power you need.

the quality and power you need.

Output Power: 45 watts R.M.S. (Sine wave drive). Frequency response:

-3dB points 30Hz at 18KHz. Total distortion: less than 2% at rated output. Signal to noise ratio: better than 60dB.

Speaker Impedance: 3, 8 or 15 ohms. Bass Control Range: ± 13dB at 60Hz. Treble Control Range: ± 12dB at 10 KHz. Inputs: 4 inputs at 5mV into 470K. Each pair of inputs controlled by separate volume control. 2 inputs at 200mV into 470K.

To protect the output valves, the incorporated fail safe circuit will enable the amplifier to be used at half power.

SPEAKERS! Size 20° × 20° × 10° incorporating Baker's 12° heavy duty 25 watt high flux, quality loudspeaker with cast frame. Cabinets attractively finished in two tone colour scheme—Black and grey.

£50 Plus P. & P. COMPLETE SYSTEM

Sound 50 amp and 2 speakers

or available separately.

Amplifier £28.50 plus £1.50 P. & P.

Speakers £12.50 each plus £1.75 P. & P

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The ELEGANT SEVEN Mk. III (350m W Output)

7 transistor fully-tunable M.W.—L.W. superhet portable. Set of parts. Complete with all components, including ready etched and drilled printed circuit board—back printed for foolproof

construction.
MAINS POWER PACK KIT: 47p extra.

Price £5.25 plus 50p. P. & P. Circuit 13p FREE WITH PARTS.

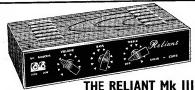


DORSET (600m W Output)

Price £5.25 plus 50p P. & P. Circuit 13p FREE WITH PARTS

7-transistor fully tunable M.W.—L.W. superhet portable—with baby alarm facility. Set of parts. The latest modulised and pre-alignment techniques makes this simple to build. Sizes: 12 x 8 x 3in.

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SOLID-STATE GENERAL PURPOSE AMPLIFIER

in simulated teak case £7.25 plus P. & P. 50p

SPECIFICATIONS

Output ± 10 watts. Output impedance—3 to 4 ohms. Inputs 1. -xtal mic 10mV Tone Controls—Treble control range ± 12dB at 10KHz, 2. -gram/radio 250mV. Bass control range ± 13dB at 100Hz.

120B at 100Hz. 2. -gramhtand 250hrv. Bass controls range at 100Hz.
Frequency Response—(with tone controls central) Minus 3dB points at 20Hz and 40KHz. Signal to Noise Ratio—better than -60dB.
Transistors—4 silicon Planar type and 3 Germanium type. Mains input—220/250V. A.C. Size of chassis—104in. x 4\frac{1}{2}\text{in.} x 2\frac{1}{2}\text{in.} For use with Std. or L.P. records, musical instruments, all makes of pick-ups and mikes. Built and tested.

THE DUO SPEAKER SYSTEM

Similar in design to those on the previous page the 2-way speaker system is beautifully finished in polished teak veneer. It is ideal for wall or shelf mounting either upright or horizontally.

Type 1 SPECIFICATION:—
Impedance 8 or 10 ohms (please state requirement). It incorporates high flux 7in. x 34in. speaker and 24in. speaker. Teak finish 11½in. x 6in. x 52in. £4.20 each. 50p P. & P.

ALL TRANSISTOR

Beautifully designed to blend with the interiors of all cars. Permeability tuning and long wave loading coils ensure excellent tracking, sensitivity and selectivity on both wave bands. R.F. sensitivity at 1 MHz is better than 8 micro volts. Power output into 3 ohm speaker is 3 watts.

Originally sold completely built for £15.4.6 (£15.23) Pre-aligned I.F. module and tuner together with comprehensive instructions guarantees success first time. 12 volts negative or positive earth. Size 7in x 2in x 41in deep.

See top of previous page for address



SET OF PARTS

plus P. & P. 50p.

Circuit diagram 13p. Free with parts Speaker, baffle and fixing kit £1.25 extra plus 25p. p. & p. Postage free when ordered with parts.



NEW FROM TRS

This money saving STEREO 8+8 AMPLIFIER in a new PRE-ASSEMBLED MODULAR PRESENTATION

nception in modular assembly which makes construction even easier than ever and results even better. Two pre-amp even easter than ever and results even better, Iwo pre-amp and two power amp modules, factory built, tested and guaranteed by a world famous maker come to you ready mounted with mains power unit on chassis forming part of the attractive TRS cabinat which simply need wiring for immediate use. A generous 8 watt RMS output per channel into 3-5 ohms is assured. Cabinet with aluminium front, charcoal grey top and wood sides measures 12in × 8±in × 23in.

- Frequency resp.: 50Hz-l6kHz ±3dB.
 Input: 110mV per P.U., radio 240mV.
 Output: 8VV per channel. RMS into 3-50. Slightly less
 Record and playback facilities
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 Extra bay so install.



Complete kit assembled ready to wire up with mains lead and instructions.
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FOR YOUR STEREO 8 + 8 OR OTHER HI-FI SYSTEMS

PLINTH AND MOTOR ASSEMBLY comprising modern style teak finished plinth cut to take famous Garrard AT6 auto/single playing unit wired for stereo, with hard smoke grey perspex lid, Plinth and AT6 less cartridge (Carr. and packing 53p).

SPECIAL CARTRIDGE OFFER TO PURCHASERS OF ABOVE ONLY

Acos stereo 6P93-1 (sapphire) £1·25. Sonotone 9TA/HC (diamond) £2. Various magnetic types from £3·50.

TRS SPEAKER BARGAIN

Ready now—Speaker and cabinet assembly comprising 8" unit (4 ohms) and easy to put together flat-pack cabinet, ported and lined, size 18in×12in×9in. £5:50 (carr. 40p).

Ar ruggedly built unit in ventilated steel case with carrying handles: size 12in×8in×8in. Two input channels mixable (10mV and 150mV) bass and treble controls. EL. 34's output (mono) in push-pull, with fixed bias. Excellent for P.A., musical group work, etc. Brand new and guaranteed £30. Carriage 75p. RADIO COMPONENT SPECIALISTS

MORE AMPLIFIERS FROM TRS **MULLARD VALVES AMPLIFIERS** 5-10 basic kit (mono) £10.99. Carr. 28p. 2 valve mono pre-amp basic kit for above £7.65. Carr. 28p.

TRS 50 WATT VALVE AMPLIFIER

10-10 stereo amplifier kit £18-99. Carr. 63p.

BONDACOUST speaker wadding ! in thick, 18in wide per yard 42½p.

COMPONENTS CORNER VYNAIR speaker and cabinet covering by iCl. Send 5p for samples—refundable on purchase. 12½p per sq. ft. £1:38 per yd. 48in wide.

VEROBOARD in all latest sizes and forms. inc. $2\frac{1}{2}$ in $\times 3\frac{3}{2}$ in, 16 p; $2\frac{1}{2}$ in $\times 5$ in or $3\frac{3}{4}$ in, 23 p; $3\frac{3}{2}$ in $\times 5$ in, 26 p; 17 in $\times 3\frac{3}{4}$ in, 75 p.

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Twin ganged stereo, 5K to 2meg. less switch, 48p; with switch 100K to 2meg. 52p.

STEREO BALANCE CONTROLS. Log/ Anti-log 5K, 10K, ½, 1 or 2meg., 55p.

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Fully built and street, where you are.
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garden, park, home, office, school, etc.
The super sensitive 6 transistor circuit is
fully tunneable over both long and
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battery, either mercury or nickel cadmium, for long life and economical running cost. The output is via a crystal-type
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COMPLETE WITH EARPIECE ONLY POST RECHARGEABLE BATTERY £1.48 18p POCKET CARRYING CASE

Spare battery 18p extra-post FREE with radio.

GARRARD SP25 Mkill



The SP2's arrier record duck has proved to be none of the most oppular of its rype in the world. Styled in black and silver, this moderately priced three-spaed unit complies with the Din 45-800 Hi-Fi performance standard-up arm is counter-balanced by a resiliently mounted weight. Stylis force is adjusted by an optical-type knurled knob, finely calibrated from 0.5 gm. in steps of 1 gm. Bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. Bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. Bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. Bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. Bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. Bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. Bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. Bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. bias compensation is set with a finger-tip from 0.5 gm. in steps of 1 gm. bias compensation is set with a finger-tip from 0.5 gm. in set with a finger-tip from 0.5 gm.

TM₅

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MODEL IM-1 1000 ohms/y

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The first of Lasky's new-look top value maters, the TM-1
is a really timp pocket multimeter providing "big" meter
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Complete with tets leads, battery and instructions.

LASKY'S PRICE £1.95 Post 13p Size Only Size Only Size Only



MODEL TM-5 5,000 OHMS/V POCKET MULTIMETER

MODEL TM-5 5,000 OHMS/V POCKET A
Another new look pocket multimeter from Lasky's
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instrument for servicing transistorised equipment.
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MP.60 McDONALD PROFESSIONAL SPEED SINGLE PROFESSIONAL PLAY UNIT

High-precision low-mass fully counterbalanced pick-up arm, heavy balanced turntable, simply operated controls, viscous cueing device, slide-in cartridge carrier, four pole motor.

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Same specifications as the MP60 but with synchronous four pole motor and full automatic change facilities.

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Counterbalanced pick-up arm, pressed steel turntable, bias compensator, viscous curing and synchronous four pole motor. LASKY'S PRICE £13.45 Post 35p

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ow-mass square section pick-up arm, cue and pause lever, visual stylus ressure indicator, slide-in cartridge carrier, four pole motor. LASKY'S PRICE £9.95 Post 35p

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PACKAGE No. 1 Recommended retail price£30,00

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ADD 50p if BSR Ceramic Cartridge is preferred

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This revolutionary idea in sound reproduction functions in a similar manner to the cone loudspeaker system. In place of the conventional paper cone is a flat, rigid plastic panel only a fraction of the depth of the equivalent cone structure. With a flat exctangular panel a larger piston area an equivalent cone loudspeaker.

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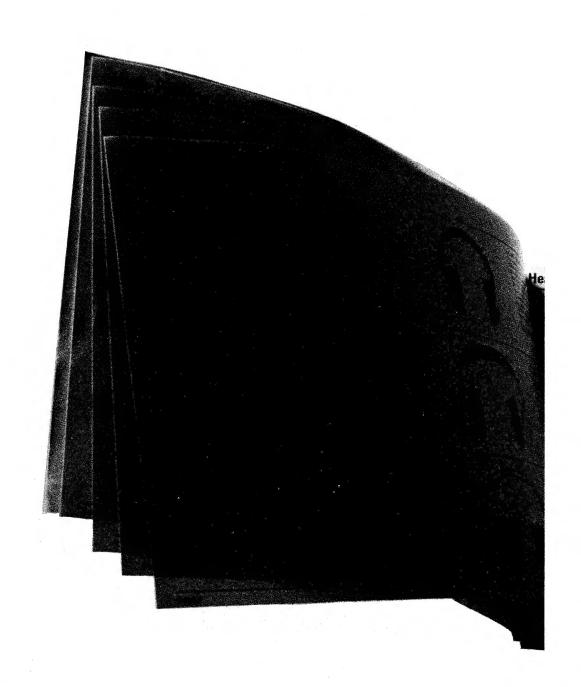
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The Eagle Annual.

Sorry, no Dan Dare, Digby or P.C. 49. Because this is the new Eagle annual catalogue. And it's packed with interesting things. Like the new TSA 151 stereo amplifier: it uses a new block construction silicon output device for absolute reliability. It's got low noise silicon transistors throughout. Its output is 15 Watts per channel. That's 15 Watts RMS, not an exaggerated figure for maximum music power.

The price? A very reasonable £36. And for people who like to listen to stereo undisturbed, we've got the new SE 100 headphones.

Dual cone transducers are used throughout, and to keep the weight down, the independent volume controls are

mounted on a separate unit with a pocket clip. £16.00.

Every item in the annual has been specified or selected by Gerry Adler. Eagle is Gerry's baby, and he's very fussy about what goes out under the Eagle banner. He gets very twitchy at the thought of a duff diode. A bit like the Mekon in fact.

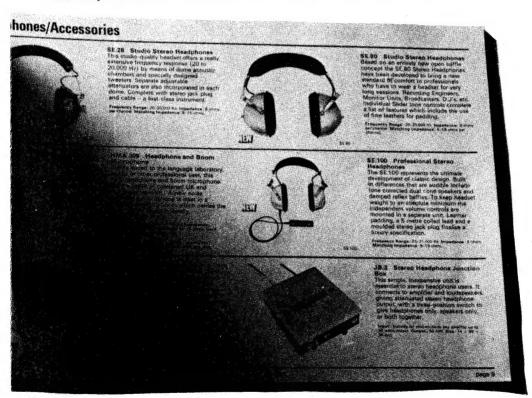
But he does it for a reason. He believes that if the first Eagle product you buy is O.K., you'll come back for more.

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ready to play

LEWIS AUDIO SYSTEMS comprise ready built equipment designed and built to advanced technical standards of efficiency and styling. Their prices make true hi-fi available to a wider public than ever. Based on the excellent Lewis Audio SA. 55 stereo amplifier in which FETS are used in the pre-amp to ensure better quality throughout, the range offers choice of free-standing amplifler with separate playing unit in plinth with plastic hard top or the Compact assembly in which the amplifier is built into the base of the plinth and motor assembly. Separate matched speakers are available for either system. Illustrated above is the Lewis S.55 Mk. Il Compact System.

LEWIS AUDIO SYSTEMS

S.A.S STEREO AMPLIFIER—6 watts RMS output per ch. into 15 ohm speakers Controls— Input selector/Vol/Bass/ Treble/Balance/ On-Off. Tape Record and replay facilities. DIN socket connections. Modern teak finished cabinet. R.R.P £18-90

PLINTHS WITH HARD TOPS & FITTED GARRARD UNITS

Garrard 2025TC with Sonotone 9TA/HC R.R.P. £16-50

Garrard 40B with Sonotone 9TA/HC R.R.P. £20-16

Garrard SP.25 Mk. III less cartridge R.R.P. £20-16

SC.55 Mk. II 'Compact' with Garrard 2025TC and SA.55 amplifier built into plinth R.R.P. £40-32

LOUDSPEAKERS
LS. 16 'Major'—13' x 8" three way system in American Walnut finished cabinet. 8 ohms R.R.P. £11-70

LS.17 6" three way system in teak or Am. walnut finish. 15 or 8 ohms R.R.P. £10-80

LS.18 8" three way system in teak or Am. walnutfinish 15 or 8 ohms. R.R.P. £12-50

• TRADE ENQUIRIES WELCOME

for the constructor

MARTIN AUDIOKITS were first to make modular unit construction available to the hi-fi enthusiast keen to save by building his own assembly. AUDIOKITS were first to feature "add-on-ability" by which a simple system could be expanded to high performance stereo equipment by the addition of easily added on units. Many who built with MARTIN AUDIOKITS years ago continue to enjoy unsurpassed quality and reliability from them to this day. NOW YOU CAN BUY AUDIORITS AGAIN to allow you to build a high fidelity system to your personal choice and which will satisfy completely on performance, simplicity of assembly, robustness and reliability. These units are beautifully engineered and solidly built for a lifetime of trouble-free service. You can start with mono and add on units to make stereo, or build with stereo throughout.

TYPICAL MARTIN ASSEMBLIES

1478E Five stage matched input selector unit; controls and pre-amp; power amp. (10 watts RMS into 15 ohms) powersupply; front escutcheon plate (mono) total price £17-58 Similar to above but for stereo. Total price £29-54 Siereo assembly for use with high grade ceramic and low power map. plocks.

All units are obtainable separately. State pick-up when outering.



- EACH MARTIN AUDIOKIT MODULE IS COMPLETE IN ITSELF AND REQUIRES THE ADDITION OF NO FURTHER COMPONENTS TO IT.
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Front escutcheon panel of assembly 1458SE

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PRACTICAL WIRELESS

VOL 47 NO 1

Issue 771

MAY 1971

TOPIC OF THE MONTH

★ components list!

THE ready supply of components is, of course, the life-line of the radio constructor, even if in these days they are sometimes crammed together to form integrated circuits or grouped and encapsulated as modules. But despite the existence of a vast multitude of components, we still hear of people unhappy about not getting what they want from their local suppliers or via mail order.

Undoubtedly, the supply position forms a different pattern these days; stocks of some items become exhausted quicker than they used to do; new versions appear as alternatives which are not always direct replacements. Years ago, a particular component would stay in a catalogue for a decade, but today's constructors cannot rely on an item staying in stock for even a year. Very often it is a case of 'take it or leave it—while it's there!'

Why, then, should this be so? Well, at the International London Electronic Component Show, opening at Olympia on May 18th, 358. British component manufacturers will be displaying their wares; these companies representing an industry with annual sales of more than £190 million. But despite this huge turnover, there is concern in the trade balance due to increasing imports of components. The exhibition will be a showplace for these competitors, from the USA, France, Russia, Israel, Hungary, India, Japan, Yugoslavia and other countries.

Components, then, are big business—big international business—and the competition is hot. To stay in the race demands investment, production and marketing of a very high level in the teeth of flercely contesting rivals. Consider, then, this feverish background the next time you call in at your local dealer for a batch of 22k resistors, six 100 puffs and a couple of AF117's!

For the facts of economic life today mean that to many component makers the home constructor either does not exist or is very small fry indeed. In fact, if it were not for manufacturers' spin-offs and end-of-run oddments we would be in a very sad state. So next time you feel like complaining about components, be thankful that we are served as well as we are. Things could be far worse.

W. N. STEVENS-Editor

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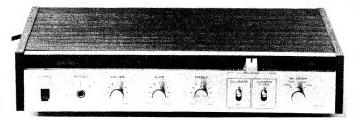
JUNE ISSUE WILL BE PUBLISHED ON MAY 7th

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NEWS... NEWS... NEWS...

Stereo from Teleton



A new stereo amplifier with 26 semiconductors and 18 silicon transistors has been launched by Teleton Electro (UK) Ltd. The new amplifier, known as the SAQ 206, has an output power of 6 watts continuous at 1% distortion and a frequency response of 40-15,000Hz. It is equipped with inputs for magnetic and crystal

pick-up plus tape playback. Output from speakers and headphones is 8Ω and the model is equipped with both scratch filter and loudness control. The amplifier has a brushed aluminium front and matt walnut cabinet. The SAQ 206 operates at 110/240 volts, 50 Hz. Retail price of the SAQ 206 is £32-50.

The "S.S.S."



Diary Dates

Apr 19-22. Physics Exhibition, Alexandra Palace, London.

Apr 20-21. Electromation Exhibition, Royal Station Hotel. Newcastle.

Apr 20-23. Technicom '71 — Conference and Exhibition, Hotel Technical Communication for Industry and the Professions, Hotel Metropole, Brighton.

Apr 22-23. Electromation Exhibition, Grand Hotel, West Hartlepool.

Apr 23. Colloquium on Railway Automation (IEE), Savoy Place, London. Briefly explained, this device consists of an electronic synthesiser which when placed between a mono programme source and a stereo amplifier will create a very realistic stereo effect from all forms of music. Whilst quality components are used throughout to give performance consistent with the most expensive high-fidelity equipment, the recommended retail price is just £10.

The most obvious uses to which the simulator might be put are: between tuner and stereo amplifier for the effect of stereo radio from mono transmissions; between a mono/stereo pickup and stereo amplifier to give simulated stereo with mono records; and between tape recorder and stereo amplifier to give the effect of stereo replay with tapes recorded on a mono machine.

Whilst normal retailer outlets, will be used, in order to enable the customer to more easily obtain this product during the early stages of production the company's fullest attentions will be concentrated upon mail order sales (p&p 20p). Their broadsheet on this product is available on receipt of a stamped addressed envelope. Kampel Electronics Ltd., 99 Old Christchurch Road, Bournemouth BH1 1EP (Tel. Bournemouth 28998).

Eton Computer

Boys at Eton College, the famous English public school, are learning the language and concepts of computers with the assistance of a Marconi-Elliott machine. A "903" computer is now in operation at the school and pupils are using it to learn what computers are, what they do, and how one makes them do it. By operating the 903 themselves, the boys are picking up the 'jargon' of the computer world, gaining knowledge of order and instruction codes and probing the intricacies of program writing.

The 903 is also being used more directly as a functional 'tool' by senior boys and members of the Eton staff to help them in the work that they are carrying out. For example, a teacher of Astronomy is using the processor to perform many of his more complex calculations.

Cassette Cleaner



The Bib Division of Multicore Solders Limited, Hemel Hempstead, Hertfordshire, announce the introduction of their new Cassette Tape Head Cleaning Tape, suitable for all compact cassette type recorders and car playing units.

The unit comprises a cassette tape container in which high quality cleaning tape has been incorporated to clean tape heads, capstan and pinch wheel. It is very simple to use, in the same manner as a tape cassette it is placed in the machine and operated in the play-back position. The whole operation takes only about a minute. A plastic container is provided in which to keep the cleaning tape cassette. This accessory retails at 10s. 7d./53p including p.t. and is available from leading Hi-Fi shops.

NEWS... NEWS... NEWS...

Mr. Fillmore



After a brief illness Mr. Leonard Walter Fillmore, Managing Director of Jackson Brothers (London) Limited died on the morning of Saturday, January 30th, aged 67. With his father and brother he founded Jackson Brothers in the early twenties and pioneered the development of Variable Capacitors and associated Drive Mechanisms. His inventive genius led to many patents in Components for communications equipments over a span of nearly 50 years.

During the war years he was very active on Ministry Standardisation Panels. From then right up to the time of his death he worked on Panel 'F', the Variable Capacitor Standardisation Panel of R.E.C.M.F. He was Chairman of Panel 'F' from September 1951 to January 1965. On relinquishing the Chairmanship he continued as Vice Chairman. Thus for nearly 30 years he devoted considerable time and energy to the Establishments of Standards both National and International for Variable Capacitors. His earlier work on the production of R.I.C. and R.C.S. Specifications has had great influence on the evolution of current International Specifications (I.E.C.).

In recent years he was deeply involved in the preparation of detailed Common Standards under the present Burghard System. His death is not only a great personal loss to his many friends but also to the entire Electronic Industry.

Group One

About a year ago, Home Radio (Components) Ltd., formed a buying group with about 15 other dealers in the London area, which they provisionally called "Group One". Its primary object was to buy components at the best prices in reasonable quantities. There are several secondary aims such as exchange of surplus stock and information.

In a letter to PRACTICAL WIRELESS, Mr. A. Sproxton, a Director of Home Radio, says, "To some extent this has been forced on us because we wished to buy certain items that wholesalers do not wish to handle and the manufacturers will only sell in quantities that are beyond the pocket of one dealer to buy. But I would like to stress the fact that this is not aimed at distributors or wholesalers (I for one have always believed that they do a useful job and earn their money) in fact any small wholesaler or manufacturer would be welcome to join. I feel sure that you will agree this is a desirable scheme as ultimately it means we can offer readers a greater range of goods at the lowest prices. Initially we are going to limit it to about 20 dealers (not on account of any closed shop principle, but because we thought - quite wrongly - that we could not handle the administration of a larger number). Now we would like to offer membership to any Bona Fide trader in the U.K. and I would be very grateful if you could make this generally known through your columns. At the moment there is no entrance fee or subscription, if anyone is interested please write to me. Home Radio (Components) Ltd., 234-240 London Road, Mitcham, Surrey, CR4 3HD.

U.K.-Finland

The United Kingdom — Finnish trade deficit of over £72m appears to be set for a £10m reduction as a result of the British Trade Drive in Finland. Britain is now the third in the list of suppliers to Finland.

Camera catch

A camera which not only photographs a traffic offence at the moment it happens, but also simultaneously records the time and the date on the same negative, may soon be used by police forces in the U.K.

It has been developed by a South African company and is already in use by the police in that country.

Known as the Trafficam, the camera can be powered by either the car battery or the built-in power pack of eight Mallory Manganese Alkaline Mn1500 penlight size batteries for fully automatic instant use.

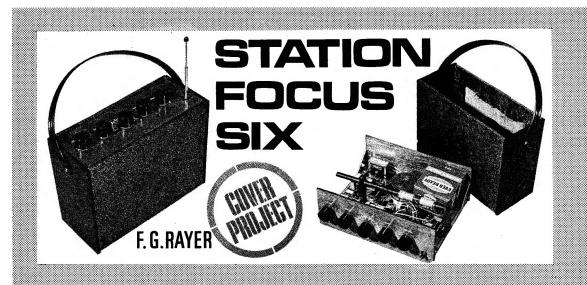
Spanish appliances

Fabrelec, one of Spain's biggest manufacturers of electrical appliances, and Westinghouse Electric Corporation, have signed patent licences, technical assistance agreements and trademark agreements for the manufacture of electrical appliances.

Powerful

The new range of seven zinc carbon batteries now being marketed by Mallory Batteries for general electrical and radio appliances. These are in addition to the mercury and alkaline batteries marketed under the company's Duracell brand name. Mallory Batteries Ltd., Gatwick Rd., Crawley, Sussex.





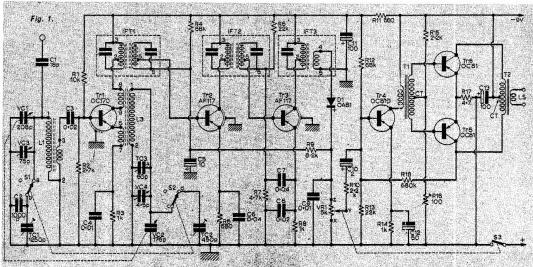
ITH many transistor portables, tuning is somewhat sharp and possibly tricky, especially at the high-frequency end of the medium wave band. The receiver described here overcomes this by using "station focus"—a control which allows oscillator tuning to be shifted slightly, for easy and exact tuning of a signal.

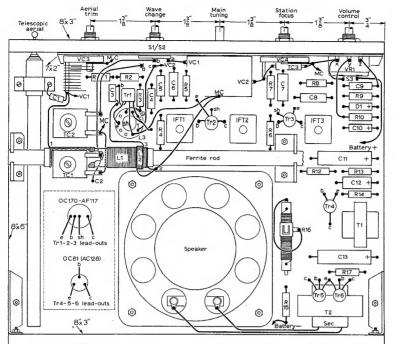
The circuit is shown in Fig. 1, and a ferrite rod aerial is used for normal reception. This gives sufficient signal strength from most transmissions likely to be required. For weaker signals, or during those times of day when reception is less good, a telescopic aerial can be extended. This is coupled to the tuned winding of the ferrite rod, L1, by the small capacitor C1. VC3 is an aerial circuit trimmer, allowing L1 to be peaked for maximum possible efficiency on all frequencies, with the aerial closed or extended.

Normal medium wave coverage is about 550-1600kHz. In the interests of easy switching, full long wave frequency coverage is not provided. However, switch S1 places TC1 and C2 across L1, and S2 puts TC2 across the oscillator coil L3. This allows a narrow band around 200kHz to be tuned for BBC Radio 2 transmissions on this frequency.

Tr1 is an OC170, followed by two double-tuned i.f.t.'s with AF117 transistors, and this combination gives good sensitivity and selectivity. The OA81 diode D1 used with i.f.t.3 provides automatic gain control bias in the usual way, through R9, and VR1 is the audio volume control.

The driver stage Tr4, OC81D, and output pair Tr5/6, $2 \times OC81$, are straightforward and give ample volume. R18 is for negative feedback over these stages, while R16 is adjustable, so that base operating conditions for Tr5/6 can be set for best results.





General Construction

The way in which the receiver is assembled is very convenient for wiring, testing and adjusting. The loudspeaker and all small components are on an 8 x 6in. perspex panel. A 7 x 2in. flanged aluminium

plate ("universal chassis" ready-formed side) bolted to the top of this panel, and carries the variable capacitors, switch and volume control. A threeply panel 8 x 3in. is secured with the bush nuts of these items, and projects about 38in. over the wiring side of the 8 x 6in. panel. At the bottom of the 8 x 6in. panel, a further piece of three-ply also 8 x 3in. is fixed with brackets.

With this form of construction, the receiver will rest in any position, to insert and wire components and will stand vertically in a normal working position, without a cabinet. The bottom piece 8 x 3in. carries the battery. The controls are on the top, so the whole receiver can be lowered into the case which clears 8 x 612 x 3in, inside and has apertures opposite the speaker.

The 8 x 6in. panel is

¹gin. perspex, so that all components and connections can be seen from either side. If this feature is not required, the receiver can be built on a paxolin panel.

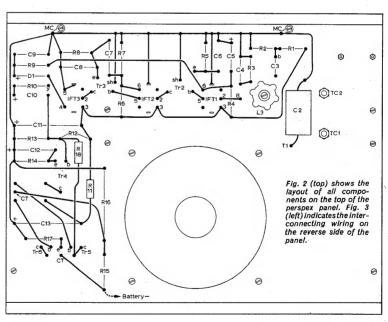
Perspex is usually supplied covered on both sides with paper, which is left in place until cutting and drilling are finished. The panel is marked out to take components as in Fig. 2. A ¹₁₆in. drill was used for the wire ends of resistors, etc., and ¹₈in. for bolts which hold the speaker, brackets, etc.

Drilling positions for the i.f.t. pins can be found by pressing paper on pins, then locating the paper on the panel, and marking through with a sharply pointed tool. A central hole is necessary under i.f.t.1 and i.f.t.2, to take a trimming tool.

The speaker aperture is most readily cut with an adjustable washer or tank

cutter, but can be made with a fine toothed saw.

Check the holes against Fig. 3. Drilling is much easier before any components are mounted, but if any holes are missed, they can be drilled later. Drill the 7×2 in. flanged plate and panel, so that they can be secured together with the two bolts



marked MC in Fig. 3. This plate is to the right in Fig. 2, to clear the extending aerial.

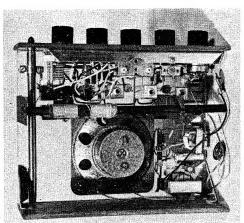
Fig. 2 also shows the spacing for the variable capacitors the holes for which are most readily made with a punch. VCI is held with three bolts which run into tapped holes in the front plate. These bolts must be very short, or washers must be added, so that the ends do not foul the moving or fixed plates of the capacitor.

The ferrite rod and speaker are left off until last.

Wiring Tips

Place tags under the bolt heads and nuts of both bolts MC, Fig. 3. A 20 s.w.g. bare tinned copper wire is soldered from tag to tag, as shown, as a positive or "earth" return and VC1/2 is connected to this circuit through the metal plate. Connect VC3 and VC4 to the adjacent tags this side, Fig. 2, and also X on VR1, and S3.

All other wiring is carried out with 26 s.w.g. tinned copper wire, with 1mm. insulated sleeving. It is convenient to use red for all "earth" or positive circuits, black for negative circuits, and some other colour for other connections.



Compare this view of the completed receiver with Fig. 2.

I.F.T.'s 1 and 2 have slightly closer spacing between pins 1 and 2, and 5 and 6, as in Fig. 3 and must be inserted and wired this way. The cans of all i.f.t.'s are earthed.

As a check, each component can be marked with coloured pencil on the diagrams as it is inserted and each connection can be similarly marked, as it is made. If this is done systematically, it is unlikely that anything will be omitted.

Electrolytic capacitors must be inserted with the polarity as shown. Trimmers TC1 and TC2 are of a type which can be secured with nuts (Fig. 3). The small trimmer TC3 can be soldered across VC4, or supported on a small bracket from the flange.

The telescopic aerial is fixed so that it can be drawn up through a hole in the top panel. Wire VR1 to MC, C9 and R10 as shown, and run red flex from the switch on this control, S3, soldering on a positive battery clip. The battery negative lead comes from R15.

Connect a flexible lead from the slider of R16, to one end, as in Fig. 2.

Transistors

These are best added after the resistors and capacitors. Fig. 2 shows the four leads of Tr1, Tr2 and Tr3, which are for emitter, base, shield and collector.

Transistors Tr4, Tr5 and Tr6 have three leads, for emitter, base and collector, as shown in Fig. 2. If Tr4 is an OC81D and Tr5/6 are OC81's, with leads in line, then a red spot indicates the collector.

Shape the leads so that they are clear of each other, and will pass down through the correct holes. The transistors can be about ¹2in. clear of the panel, but leads should not be unnecessarily long in the i.f. stages. They are then soldered as in Fig. 3, and snipped off.

Form the leads of Tr1 as in Fig. 2, and put sleeving on them before soldering. With Tr5 and Tr6, both emitter wires go through a single hole, to R17. Place D1 with its polarity as shown.

Heat shunts are not generally required if the connections are soldered rapidly with a properly heated iron. The iron is removed immediately the joint is made.

★ components list

-	
	R13 22kΩ R14 1kΩ R15 2·2kΩ R16 100Ω* R17 4·7Ω R18 680kΩ tre-set (Home Radio ot. (log) with switch.
Capacitors: C1 18pF C6 0.04µl C2 1000pF SM5% C7 0.04µl C3 0.02µF C9 0.02µl C4 0.01µF C9 0.01µl C5 10µF 6V C10 2µF 6	F C12 50μF 6V F C13 100μF 12V F
fure	riable, miniature. ced variable, minia- me Radio VC29SA)
Semi-conductors: Tri OC170 Tr4 OC81 Tr2 AF117 Tr5 OC81 Tr3 AF117 Tr6 OC81 D1 OA81	(or AC 128)
Inductors: L1/L2 Ferrite rod aerial (M.W. IFT3 IFT18/465 (Denco) IFT IFT3 IFT14/465 (Denco L3 Range 2T Red (Denco)	2 IFT18/465 (Denco)
Miscellaneous: Speaker, $3\frac{1}{2}$ in 3Ω . T1, Driver Radio TR64). T2, Output Radio TR65A). S1/S2, 2 pole scopic aerial with bracket member 7 x 2in. (Home Radi Perspex (or paxolin) 8 x 6 x (2 off). "Radio Constructor"	transformer (Home 2 way switch. Tele- . Universal chassis o CU136). Knobs (5).

TAKE 2®

JULIAN ANDERSON

A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

T is the aim of this page to give circuits and explain the operation of the simplest type of circuits and we are of course limited to £1.00 and twenty components and obviously this places certain restrictions on the quality of the finished articles. Nevertheless simplicity also leads to a lesser likelihood of mistakes and the circuits usually have a wide range of uses in many fields. This month's project fits into this category; it is an audio amplifier which may be used to boost the output of an earphone type radio, as a pickup amplifier or an intercom. It is extremely simple and, to my knowledge, has never been published before.

THE CIRCUIT

The secret of the simplicity of the circuit shown in Fig. 1 is the directly coupled Darlington Pair of transistors, Tr1 and Tr2. This configuration, which is also known as a super-alpha pair, acts rather like a single transistor with very high gain, the base being represented by the base of Tr1, the emitter by the emitter of Tr2 and the collector by the common collector connections. The gain of this combination is roughly equal to the products of the gains of the individual transistors. With the specified transistors the minimum gain should be no less than 8,000 using the green version of the 2N2926 (highest gain grouping) or a maximum of over 20,000!

With gains of this sort of order it's not surprising that few components are needed.

If one looks upon a transistor as a resistor whose value between the emitter and collector alters, depending on the base bias applied, it can quickly be seen how the circuit operates—and why the gain is so high. Regarding the operation in this way, Tr1 becomes a variable bias resistor for Tr2 so that the higher the input signal, the greater the bias.

The quiescent current through the transistor pair depends on the value of R1 and although the value shown— $1.8M\Omega$ —worked well with several transistors used for Tr1 and Tr2, the value does depend on the gain of the pair and may have to be selected from a range between $680k\Omega$ and $3.9M\Omega$.

The quiescent current through Tr2 is fairly high—20mA or so—and it is for this reason that we are using a BFY51 rather than a transistor with a lower current handling capacity.

C1, VR1 and C2 simply act as d.c. blocking capacitors and as a volume control. The input impedance of this type of circuit is high and this allows for the use of low value blocking capacitors in conjunction with a high value volume control—here a $1 M\Omega$ type is used. It is not recommended to substitute an 8Ω or a 3Ω speaker directly into the collector circuit, though the use of a transformer with a ratio of about 5:1 would allow these to be used.

No. 25 AUDIO AMPLIFIER

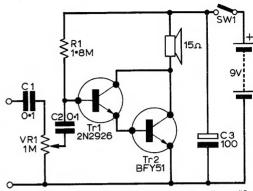


Fig. 1. The circuit of the "Take 20" Darlington pair audio amplifier

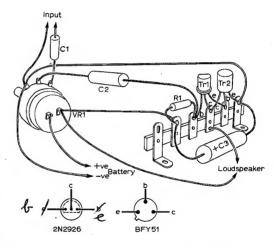
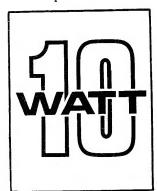


Fig. 2. A suggested layout for the amplifier using a small tag-strip; the transistor lead connections are shown below, viewed from the lead ends.

A suggested layout on a short tag-strip is shown in Fig. 2, though as the circuit is published as a general purpose type, it will normally be built as part of some other circuit.

A PP9 battery should be sufficient for this circuit; the smaller PP3 type will be unable to supply the necessary current as the power output of the amplifier will be about 200mW. This output level is quite adequate for most uses.

The final quality is surprisingly good and all-in-all the circuit will be found to be a very useful one.





AUDIO AMPLIFIER

HALVOR MOORSHEAD

T is difficult to fit the amplifier described in this article into any normal category. By the DIN specification it is probably Hi-Fi but by current accepted standards of Hi-Fi it leaves a little to be desired.

The ten watt output is far higher than normal record player amplifiers, yet is well below the usual 25W which now seems to be the lowest power acceptable.

It is neither as cheap to build as the amplifiers featured in "Take 20" but neither does the cost approach that of commercial amplifiers. So this amplifier is in the "Mid-Fi" field. The quality is good—laboratory tests show a flat output from 40Hz to 20kHz with harmonic distortion below 1% at 1kHz at 5W output. This distortion level is high by prevalent standards but since the human ear cannot distinguish even 2% of harmonic distortion, it hardly matters.

The cost of the project is low. The amplifier by itself should be rather less than £5 and the cost of the separate power supply will probably add another £3—these prices do not, of course, include the loudspeakers.

The circuit and the construction details cover a mono version but naturally when doubled up, using dual pots for the volume and tone controls, and fitted with a balance control, it would be perfectly satisfactory for stereo.

Since the amplifier as described does have limitations in performance, it is not intended for use with expensive magnetic pickups and it is assumed that it will be used with ceramic or crystal types. If a magnetic pickup facility was to be incorporated, correction would also have to be applied.

No great originality is claimed for the circuit—it is largely based on Mullard designs though slight modifications have been incorporated. The output transistors are the common AD161-AD162 complementary pair and closely matched pairs of these are currently available for as little as 50p though they are more commonly sold for 80p.

The finished amplifier, in the monophonic version, is small, though not so small that construction is difficult and it was designed to this size so that it can fit into almost any record player cabinet. If the amplifier is to stand on its own a wooden surround

would improve appearances. The power supply is built separately and this can be mounted quite a distance from the amplifier—if fitted into a record player this can be fitted at the back.

Loudspeakers are not dealt with as this is a completely different field but the impedance can be anything between 5Ω and 15Ω . The amplifier has been tested running for several hours at full output on a 3Ω speaker system but this low impedance cannot be recommended in all cases, though no harm came to the prototype.

The hum and noise level are extremely low; at full output they were only just audible with an ear inside the speaker cone and at a foot away, nonexistent.

One of the problems with home built amplifiers of this type is instability, the author has often come across this and knows of others who have experienced the same problems.

The design shown should be unconditionally stable and two features are incorporated in the circuit to increase stability, even though without them the stability was good; this means that anyone building the amplifier can be sure that these problems will not arise even if the layout chosen would tend to oscillation.

THE CIRCUIT

The complete circuit, apart from the power supply, is shown in Fig. 1 and this comprises three main sections: the preamp., the tone control and filter stage and the output amplifier.

It has already been mentioned that the amplifier is designed for use with ceramic or crystal pickups. Although these have got a very high output—at the very least 80mV and often ten times that level, the inherent impedance of these types is high and unless they are coupled to a high input impedance, the frequency response will suffer. Transistors in the common emitter mode have typical input impedances of about $20k\Omega$, far too low to mate the pickup to, so for this reason the inputs are connected directly to a $1M\Omega$ resistor in series with the input and this, of course, determines that the input impedance is at

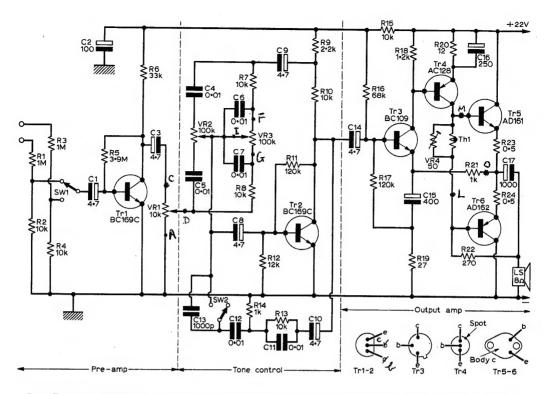


Fig. 1: The complete circuit of the 10W amplifier. A full description of the operation and function of the components is given in the text.

* components list

	4-7μF 15V 0-01μF	C12	0·01µF 1000pF	Ver	oboard	0.15in matrix,	4in x 2in type for AC128
	100µF 25V		4·7μF 15V 0·01μF	Tag	strip	Type 2-way	
	4-7µF 15V	~~		500	kets		IIN, Output, DIN L.S
Cana	citors			Met	al Chassis	7in x 4in x 1ii	, H. L. Smith Ltd.
VRS	! 100k(3 lin.	VR4	50Ω skeleton preset.	Fus	e	With fusehold	ler. 1A
VR1	10kΩ log.	VR3	100kΩ lin.	Tra	nsformer	250V pri., 17 o	r 18V secondary, 1.5A
All	resistors #W, 5%	excep	t where stated				ngeover slide switche:
R12	12kΩ	R24	0.47Ω (or 0.5Ω) 2W	Misc	ellaneous		
	120kΩ		0·47Ω (or 0·5Ω) 2W	Tr5	AD161		r—see text
	10kΩ		270Ω ↓ W		AC128		Silicon Bridge Recti
	10kΩ 2·2kΩ		12Ω 1kΩ		BC109		ue)
R7 R8	10kΩ		27Ω		BC169C	DATE: NOTE: THE PARTY OF	VA1077 (32Ω) (Electro
R6	33kΩ		1·2kΩ		conducto BC169C		AD162
R5	3·9MΩ	R17	120kΩ				
R4	10kΩ		68kΩ		4-7µF 15		2500µF 50V
R3	1MΩ—see text		10kΩ		4-7µF 151		1000µF 25V
R2	10kΩ		1kΩ		0.01µF		250µF 6V
R1	1MΩ—see text	D12	10kΩ		0·01μF 0·01μF		4-7μF 15V 400μF 15V

least this high.

Two inputs are provided and as shown are for similar levels and impedances. One is provided for the pickup, the other for a radio tuner. Radio tuners have outputs which vary from about 50mV to 1V and R3 (if the tuner is to be connected to this section)

may well have to be varied from the given value to match the tuner used. The value shown is suitable for 500mV.

For a 1V output it should be $2M\Omega$ while for 50mV it should be $100k\Omega.$ Since the output impedance of tuners is rarely high it doesn't matter if the input

impedance is lower for this side. In any case the value should be chosen so that the levels at the input to Tr1 are similar for both tuner and pickup.

Therefore R1 and R2, R3 and R4 act as the input attenuators and matchers. The output for the attenuators go directly to the input select switch and the output from this goes to the base of Tr1 via the blocking capacitor C1.

The function of Tr1 is to raise the level of the signal to a suitable level to feed the tone control network and overcome the necessary attenuation brought about by the input resistors. Tr1 is a BC169C, a plastic version of the low noise BC109. R5 provides the base bias and is of this high value because of the high gain of the transistor.

The output of the preamplifier connects via the blocking capacitor C3 to the volume control, a $10 \mathrm{k}\Omega$ log, potentiometer. If a stereo version is to be built the only additional component necessary would be a balance control which fits at this point in the circuit. This should be a $25 \mathrm{k}\Omega$ linear pot., the outer tags connecting to the sliders of the two volume controls with its own slider going to chassis.

The output from the volume control goes to one side of the tone control network comprising VR2, VR3, C4 to C7 and R7 and R8. The other side of the tone control network is connected to a negative phase signal so that the output of the network can be varied from minimum bass and treble to maximums of the same signals.

The output of the network connects to the base of Tr2 which is baised by R11 and R12. The feedback to the tone control network is taken from the potential divider R9 and R10 which between them form the load for Tr2.

Another output from the collector of Tr2 is taken via blocking capacitor Cl0 to the "Hi-Cut" filter which is designed to couple back to the base as little of the frequencies below 7kHz as possible and as much of the higher frequencies as possible. As the filter is connected in the negative feedback mode

this has the effect of giving a very steep cut above 7kHz and acts very effectively as a scratch filter for poorly treated or old records.

In addition when used to amplify radio signals it will help to get rid of the higher frequency heterodynes present on many a.m. signals after dark.

A filter of this sort should not be confused with a tone control which is designed to gradually slope the high or low frequencies. The "Hi-Cut" filter is designed to have little effect below 7kHz and a lot above it.

The filter is switched in or out by SW2 but C13 is arranged to couple at all times. This is included so that even with the filter out there is a very steep cut at a much higher frequency—about 40kHz—and signals much above this are completely eliminated. Since this is well outside the audio range it in no way impairs the quality but it does serve two other functions.

The fantastic frequency response of the silicon transistors used in modern audio amplifiers leads to the amplification of any r.f. signals picked up in the wiring which tend to be detected at some point

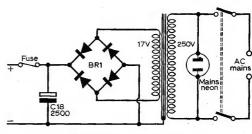


Fig. 2: The power supply circuit.

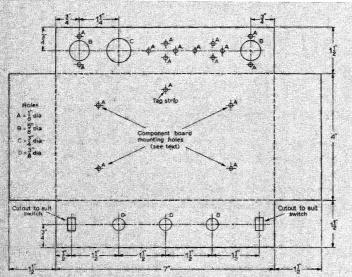


Fig. 3: The drilling of the chassis. A suitable inexpensive one, as used in the prototype is available from H. L. Smith Ltd., 287 Edgware Rd., London W.2.

in the circuit. The high input impedances included in the earlier stages do nothing to help this. The filter completely eliminates these problems.

For similar reasons it is quite common for instability to become a problem, output signals of a high level being capacitively coupled to the input circuitry. The filter greatly reduces the likelihood of this.

The output of the tone control couples to the output stage and is first amplified by Tr3 whose emitter is held at half the supply volts which appear at the junction of R23-R24 and is smoothed by C15. The inclusion of R19 incorporates a degree of negative feedback and thus improves the quality and stability of the output stage.

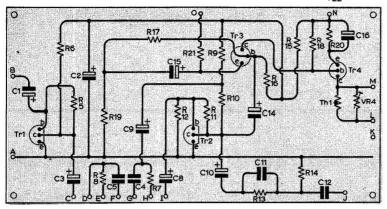
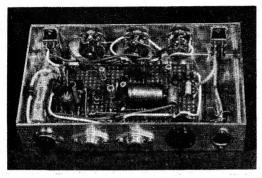
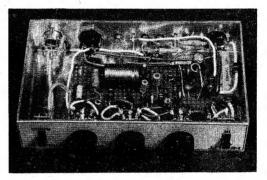


Fig. 4: The component layout on plain veroboard.

The output from Tr3 is directly coupled to the driver transistor Tr4, a p-n-p germanium type, which, because of the high currents it is passing must be protected from runaway by R20, decoupled by C16.

The output from Tr4 is coupled to the bases of the output pair Tr5 and Tr6, the slight bias necessary between them provided by the thermistor TH1 whose slope is made linear by paralleling it with a 50Ω preset whose setting also determines the quiescent





Two internal views of the 10W amplifier showing the general layout. Compare these with Figs. 4 and 5.

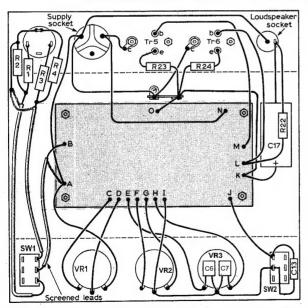


Fig. 5: The wiring between the component board and those components mounted directly on the chassis.

current in the output stage.

A degree of feedback is applied by connecting the load resistor of Tr4 (R22) through the loudspeaker.

The output of the complementary pair provides the low impedance output via C17 which has to be high in value to effectively couple the bass notes to the loudspeaker.

Amplifiers of this type require a low impedance power supply—batteries will be no good. The current drawn varies between a few milliamps and an amp. The transformer has a primary winding of 250V with a 17V, 1A secondary which connects to the Bridge Rectifier BR1. Various types are suitable and some inexpensive plastic encapsulated types such as the Mullard BY164 are highly suitable. However any type with a voltage and current rating of 30V, 1A should be satisfactory.

To keep the hum level down to an acceptable level, the reservoir capacitor has to be of a high value. Some protection to both the power supply and the amplifier is provided by the 1A fuse in the line.

Careful smoothing of the supply voltage is necessary in the earlier stages and this is catered for by C2; any value lower than this may lead to low frequency instability. If motor-boating does occur the value of C2 should be increased.

CONSTRUCTION

The amplifier is built inside a small aluminium chassis $7\times4\times1^{1}$ ₂in. with one long side holding the controls with the inputs, outputs and power transistors sited on the back. The drilling of the prototype chassis is shown in Fig. 3.

Small slide switches are used for SW1 and SW2 and rectangular holes have to be cut at each end of the control panel for these. Slide switches are designed to be bolted to the chassis but a much smarter and easier job is made by gluing these on using Araldite

The holes for the power transistor leads and mounting screws are most easily made by using the mica washers, which should be provided with the transistors, as a template.

On the prototype the supply is arranged to plug in using a Bulgin connector, but of course a simple hole fitted with a rubber grommet would be just as good to feed the two wires to the power supply.

To make the wiring short, a small tag strip should be mounted near the output transistors to hold R23 and R24.

The majority of the components are mounted on a piece of plain Veroboard, 0.15in matrix, sized 434× 212in. The siting of the components on this is shown in Fig. 4. C15 is a bulky component and has to be sited as shown in order to fit in.

Tr4 will be warm in operation and it is important that a heatsink is fitted to avoid thermal runaway. The output transistors also need a heatsink and this is provided for by bolting these to the back. Even though the body of Tr6 is at chassis potential (the body being the collector) do not be tempted to leave off the mica insulating washer that is also needed for Tr5. Hum may be introduced due to earth loops if it is left off.

The output capacitor is connected directly between the output socket and a mounting pin fitted on the component board, so is R22.

The wiring between the board and the components mounted on the chassis is shown in Fig. 5.

No wiring is shown for the power supply as this will depend on the transformer and bridge rectifier used, but it is so simple that it can easily be worked out.

If a switch is needed for this it should be mounted on the power supply chassis.

Only one input socket is provided—a DIN 3-pin type and both inputs should be wired to it, the attenuator resistors are also mounted on it.

If the slide switches are glued to the chassis as suggested, a sheet of white card can be fitted over the front panel, as there will be no screws to stop it from laying flat, and a very acceptable face plate can be achieved as shown.

TESTING

Once the wiring is completed and thoroughly checked it is worthwhile measuring with an ohmmeter the resistance between the bases of the output transistors. The resistance should be low and the preset VR4 adjusted for minimum resistance. (This means that there should be a short between them.) Also check that the collector of Tr5 is insulated from the chassis. If all is well with these tests it is unlikely that harm will befall your newly completed project.

If two PP9 batteries are available, these can be



The small size of the amplifier can be judged by the matchbox on the left yet the photographs on the previous page show that layout is not crowded.

used to supply 18V for initial testing. The noise level, even on full output, should be very low, but the dabbing of a finger on the input should produce a high hum level.

If all seems well a pickup can be connected. On full output there will be severe distortion due to the use of batteries but the use of these lessens the likelihood of destroying the transistors if there are any mistakes in wiring, etc.

With all these points checked, the power supply can be connected. There may still be distortion due to the setting of VR4 and this should then be backed off until the audible distortion just disappears while ensuring that Tr4, Tr5 and Tr6 do not get hot.

The effectiveness of the tone controls and the Hi-Cut filter should be considerable and the output be more than adequate.



INFORMATION WANTED
... details of the makers of the stereo amplifier marketed by Electronic Sales (Victoria)
Life was led to understand that this was covered by maker's guarantee but have no
Life was led to understand that the was covered by maker's guarantee but have no
A. E. Webb, 25 Heather Road, Milton, Abvicthed on without speakers connected.—
A. E. Webb, 25 Heather Road, Milton, Abvicthed in the content of the was a considerable on the content of the content of

Park, Middlesox.

... horrow manual of —or acquire constructional information on Heathkit battery portable UXRI—A. Pitt, Rendcomb College, Nr. Cirencester, Gloucestershire, ... any information, or the loan of a circuit for a Selmer Type "C" Clavioline with the transistor line-up 4 x SSB178, SSB178B and 25B1788.—J. M. Newby, 27 St. Johns Road, Shildon, Co. Durham.

—any information on the Standard Radio SAH transmitter. Also, where can I get a BA114 Mullard diode and has it an equivalent?—P. Gladwin, Westfield Farm, Towersey, Thame, Oxon. OX9 3QB.

...any information on modifications to, and the handbook and circuit diagram of the R 209 Mk. 2 receiver.—P. Reeves, 2 Hunts Mead, Billericay, Essex.

ISSUES WANTED
Practical Wireless dated October 1967 containing the Music Box article. Tenshillings, 16 for same.—"The Occupier", 3 Lawrence Close, White City Estate, London, Vt.2.
...the March 1970 issue of Practical Television.—J. Barin, 7 Eastside Road, London, N.W.;11 OAY.

N.V., II UAY.

...January to September 1968 copies of P.E.—M. Duxbury, 2 Jefferson Drive, Ulverston, Lancashire.

ISSUES FOR DISPOSAL

ISSUES FOR DISPOSAL
...copies of Practical Wireless for 1963/4/5/6. Anyone can have them FREE.—
S. J. Wells, 34 Brockman Rise, Bromley, Ken.
...Practical Electronics from the start (November 1964) to December 1968. Practical
Wireless from May, 1965 to April, 1965. All are complete and in binders. Any offers
considered.—N. J. Moore, Flat 5, 7 Cortion Road, Ealing, London, W.5.

EQUIPMENT WANTED and dual I.i.t. numbered "L8" for a Jason Argonaut f.m./a.m. tuner.—A. Kenway, 16 Hilliers Lane, Beddington, Surrey.

LITERATURE WANTEDcopy of Mullard Circuits for Audio Amplifiers, second edition (1962). The price at the time was 8s. 6d. Please state price and postage.—G. W. Saunders, 26 Rowan Crescent, Streatham, London, S.W.16.

practically wireless commentary by HENRY

ESPITE the fact that there were only eight entries for last year's John Rouse Trophy (RSGB constructional entry for under-sixteens), and our disgruntled Editor found it necessary to bemoan (September 1970) that few radio amateurs now build their own main station gear, we feel encouraged by the response to Project Autumn 1970, to recommend those bright young sparks about to cast off the shackles of school to think about the radio servicing busi-

Henry recently enjoyed a talk with a bunch of school-leavers. Many of them were captivated by the glittering world of electronics. Bemused by the button-pressing magic of *Dr. Who* and *Star-Trek*, bedazzled by the multimillion flash of instrumentation in the Space-age-for-real, they imagine that radio and television engineers in the entertainment industry must hold the key to perpetual interest.

Henry is amazed at the blurred occupational edges. These young-sters imagine that the lucrative and glamour-ridden world of the television 'star' is gained via the cabled chaos of the studio floor, or, at best, the hallowed hush of the control room.

Hush! Have you ever been in a control room when the producer is shouting at three camera-



The continuity girl dissolved into tears.

men at once, when the sotto voce of the floor director's talkback is rattling the monitor loudspeakers, when the continuity girl has dissolved into tears over a lost page four and the musical arrangements depend on the cueconsciousness of a half-drunk tape recorder operator?

Very few performers come up from these ranks. To begin with, a few weeks behind the cameras, or abaft the mikes, soon disillusion any would-be entertainer. There's Harold Williamson, of course, but he is not exactly an entertainer. And there's 'Professor' Stanley Unwin, whose prowess should convince us that a spell in the camera crew would make anyone talk gobbledygook. One or two disc jockeys know a little of what goes on beneath the platter. But those who fancy that job may not have any notion of the sweat and toil that can go into sorting out, helping to edit and presenting 'a favourite toon for Mrs. Pettifer of Lower Peckham Rye.'

Sometimes, the yearning is genuine. The lure of electronics really fascinates youth. Some of the mystery has been peeled away by a keen science master, revealing even greater depths. Space-age phenomena make much that was wonderful seem mundane—when we hear a gravelly op-check from many thousands of miles away, we are now more likely to carp at its roughness than marvel we can get it at all!

But Miss Today and Master Tomorrow take miracles in their stride. Perhaps I should have told them about the openings in Tero-technology, a word the Min-Tech boys coined for Maintenance Engineers. These maligned gentlemen are fast becoming an élite. They work for large engineering companies, daily waving their magic wands over the fallible products of systems designers.

They are expected to instal, commission and maintain any-

The Tero-Technologist



Leaving behind a trail of modified machinery.

thing from an air-drying purifier to a fully automated oilfield. Electronics is only part of the game to them—building blocks are what we should consider factory-sized projects.

I know one of these gents. He came out of redbrick with a poor degree, entered industry as an assistant to an assistant of an assistant designer. Moved from firm to firm, absorbing knowledge like a sponge and leaving behind a trail of modified machinery. He graduated to his present job simply because nobody else dared take it. And now he picks up all the bricks that scatter-brained designers have dropped besides acting as consultant for half-a-dozen international concerns.

From whence came his qualifications? Well, despite our modern technicological age and the outmoded place for an amateur, I suggest he received his impetus and his capacity for a quirky open mind from his younger love of amateur radio, constructional hi-fi and continual dissatisfaction with marketed products. He is a gadget man' and proud of it, even if his present job of 'panel-changing' involves him in king-sized modules.

If anyone tells you, young shaver, that the day of the dabbler has gone, just point to the tero-technologist and be thankful.

SERVIGING

PART 1 H. W. HELLYER

THIS SERIES, WRITTEN BY H. W. HELLYER AND G. J. KING, BEGINS WITH A DISCUSSION OF THE BASIC COMPONENTS OF ANY PIECE OF ELECTRONIC EQUIPMENT, THE RESISTOR, CAPACITOR AND INDUCTOR, WITH SOME NOTES ON THE VALVE AND TRANSISTOR.

BEFORE we can repair a radio receiver, audio amplifier or any other piece of electronic equipment, we must understand something about the fundamental parts of the circuit. Any circuit can eventually be broken down into its component parts or combinations of parts, just as any whole circuit will separate, for convenience, into a number of 'building bricks', as we shall see when my colleague Gordon J. King takes over the next part of this series.

My job, this month, is to lay the ground, describe the 'bones' which form the skeleton circuits and give a few hints about their testing.

Description of components and their functions must needs be brief. We haven't the space for a detailed exposition or for more than a quick look at the three main classes of circuit bones—resistors, capacitors and inductors.

RESISTORS

Sub-dividing the first class, we have fixed, variable and non-linear resistors.

Fixed types may be of carbon, of composition, metal-oxide film on a glass rod or any of several proprietary substances. Values of these components will vary between a fraction of an ohm and several million.

Tolerances are important to the designer and to the engineer who follows in his footsteps by maintaining the equipment. For resistors the tolerances fall into groups, from 1% to as much as 20%. The current a resistor can safely carry is important also for this determines the choice of wattage of the component we may need, to replace a damaged one in a circuit.

The wattage (W) is equal to the product of the current (I) through the resistor (R) and the voltage developed across it (V). By Ohm's Law, $W=I^2R$ or V^2/R or $V\times I$.

Resistors of more than about 2 or 3 watts will usually be wirewound. These are generally bulkier and often consist of a ceramic tube with resistive wire wound on it anchored to stiff wire ends.

Non-inductive wirewound resistors are very necessary for some positions in the circuit and these are

made by winding the resistive element in such a way that the two legs of the 'coil' lie together and magnetic fields tend to cancel each other. Such bifilar winding, as it is called, will also be met with in coil construction, where it is used for the same purpose of cancellation of unwanted magnetic fields.

Practical points: composition resistors are easily damaged by heat. Discolouration of the coding or body paint is an indication that excess current has passed. Do not ignore the warning, look for the reason. Metal-oxide components (and some of the older composition types) had end caps clamped on, relying on physical pressure for their resistive contact.

A loose clamp, or a badly connected lead wire to a cap, is the possible cause of a 'high resistance' joint. As these types are often painted over, with the poor joint beneath the coating of paint, the end cap may not appear to be loose at all.

Colour coding has been standardised pretty well by now, although there are always awkward exceptions. Dirt, heat and age may discolour components and obscure or alter colours, so the rule should be: 'When in doubt—check.' A table of colour codes, including tolerances, etc., is given for resistors.

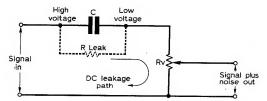
To some extent, the same code can be used for capacitors, as can the abbreviated method of indicating component values. Despite attempts at standardisation, values may be expressed in several different ways. A 4700 ohms resistor, for example, may be designated 4.7k, or 4k7, or given its full title.

Variable resistors come in a number of varieties, from the common, three-tag 'volume control' we know so well, to multi-section, tapped sliders, often ganged mechanically as well. Basically, the variable resistor can be sub-divided into carbon-track and wirewound types, and a further classification must specify whether the 'law' of the resistor is logarithmic or linear, i.e. log. or lin.

Linear types are self-evident; the resistance in circuit varies in proportion to the angular rotation of the spindle to which the wiper is attached (or the lengthwise travel of 'slider' types). Log. types have a track whose resistance increases logarithmically

as the spindle moves, so that for a great proportion of travel there is little change in resistance, then as the rotation continues, the resistance increases more and more rapidly, i.e., the scale of resistance is cramped toward the upper end. As this conforms more with the physical nature of hearing, such a control is more often used for a volume control, whereas lin. types will usually be found in tone and balance control circuits.

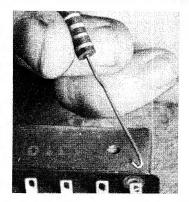
Practical points: noisy volume controls are a frequent complaint—not always justifiable. Very often, the real trouble lies in stages prior to the control, with the fault revealed as the control 'opens up'. An example here is a leaky coupling capacitor in a valved circuit, where the coupling is from the anode of the preceding stage to the 'top end' of the volume control, the potential across the capacitor being nearly that of the h.t. line. This causes a small current to flow through the variable resistor, with resultant noise.



Reported "noisy" volume controls can be due to a leaky coupling capacitor.

Similar faults occur in transistorised equipment, where electrolytic capacitors are needed to maintain the time constants of the interstage circuits.

Noisy controls can be caused by poor connection between spindle and main body, or to wiper support. Where there is a divided section of the control casing, poor clamping or corrosion between surfaces can also be an unsuspected cause of noise, as can inefficient earthing. A composition track volume control already damaged by current flow, caused by a leaking capacitor, may have a 'hot spot', a portion of the track pitted or burned. This will never succumb successfully to treatment. Replacement is the only cure. But carbon track variable resistors that have simply aged, which can be opened easily, could be treated by rubbing over the track with a soft lead pencil. If the damage is not too far gone, the crackle can sometimes be cured by injection of switch-cleaning fluid; several aerosol preparations are available.



Even in black and white the colour bands on this 1-watt composition resistor are clearly seen.

Personally, I do not favour this method. It is, at best, a temporary solution. Replacement of the offending control is always best. But though the professional in me must advocate the fitting of new parts, the practical wireless hobbyist in me says 'what about cost and availability?' If you are prepared to spend infinite pains in rejuvenating an outworn part, then good luck to you.

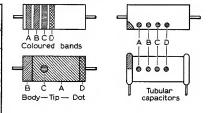
Small variable resistors, used as preset controls

COLOUR CODE FOR CAPACITORS AND RESISTORS

·	First Figure 'A'	Sec'd. Figure 'B'	Multiplier 'C' Resistors Caps pF			Tolerance 'D' Ceramic Capacitors to 10pF over 10pF		
Black Brown Red Orange Yellow Green Blue Violet Grey White No colour Silver Gold	1 2 3 4 5 6 7 8 9	0 1 2 3 4 5 6 7 8 9 	1 10 1,000 1,000 10,000 100,000 10,000,00	1 10 100 1,000 10,000 — — — 0.01µF 0.1µF	±1% ±2% ±20% ±10% ± 5%	2pF 0·1pF 	±20% ±1% ±2% ±2½% — ±5% — ±10% —	

A salmon-pink fifth ring or body colour denotes a Grade 1 high-stability composition resistor. There are variations in the code for capacitors other than ceramic tubular types.

The "preferred" series of values is as follows:—
1.0 1.2 1.5 1.8 2.2 2.7 3.3 3.9 4.7 5.6 6.8 8.2 and their decades.

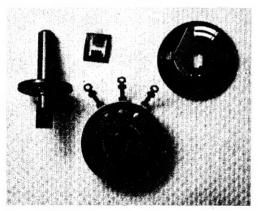


Above, left, shows two ways of indicating the value of a fixed resistor; coloured bands and the body-tip-dot method. Above, right, shows how coloured dots are used for the same purpose with tubular ceramic capacitors. However capacitor coding has not followed the same standard pattern as resistor coding there being national and even manufacturers' variations. The code shown in the table is the common one. Manufacturers often use plain marking for the value, tolerance etc. on the body of a capacitor.

in many circuits, are vulnerable to damage by a heavy hand. The usual trouble is strain of the wiper portion from its open rivet attachment to the body of the control. These controls are not intended to carry much current. They will burn out easily and the burn is sometimes invisible—the usual place being adiacent to the end contact. If the control is used as a simple variable resistor and the track is damaged, a simple solution is to reverse the end connection, thus using the other terminal of the track. It is best, when connecting simple variable resistors into circuit, to bridge the slider to the 'common' end. Similar remarks apply to the potentiometer, or the larger variable control.

A final class, the dual concentric control, is being met very often in stereo equipment, needing another special point of attention to be noted. This is the possibility of noise due to imperfect contact between the sections of the control. Sliding metal surfaces tend to generate electrical as well as mechanical noise and this can sometimes be picked up and amplified. A cleaning and greasing regime for such controls will help-but really this is a design problem, and the root cause may be that the control is 'too early' in the circuit. I feel sure my colleague will have a few remarks to offer about such circuitry in a later part.

Non-linear resistors: Final mention has to be made of the special resistors increasingly being encountered: such things as temperature and voltage-dependent resistors, thermistors, varistors, etc. The thermistor at one time performed a voltage dropping function as part of the series chain in the heater line of an ac/dc receiver. As the component warmed, its resistance decreased and from a cold value of several thousand ohms reached an eventual value of one or two ohms (in some cases up to about



A dismantled potentiometer showing, top left, the spindle; top centre, the fixing spring; bottom centre, the carbon track with rivetted tags. At top right, the wiper with split spring for flexibility.

40 ohms) when at operating temperature. This regulated the current flow, preventing damage to cold valve heaters and obviating cathode stripping which can be caused by excessive emission. H.T. applied quickly, when semiconductor rectifiers are associated with valved circuits is a common cause of cathode stripping.

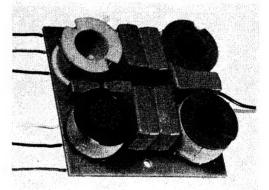
Practical points: such components must be allowed to dissipate their heat. They should be mounted in

a ventilating flow of air, if the repairer or constructor has any choice in this matter. Care must be taken to dress wires away from the hot thermistor, and to keep other components out of its heat field.

Smaller temperature-dependent resistors will be found in power output stages, near or attached to the heat sinks of power transistors. Their purpose is to regulate the bias circuits so that an increase in heat causes a reduction in current. More will be said later about these protection devices.

Varistors are resistors which change their value according to the voltage across them. Again, they are met in many modern circuits where electronic control is needed, and some of the stabilising circuits in which they are employed will be dealt with in succeeding articles.

Light-dependent resistors have a special function, their resistance decreasing as the light falling on their target area increases. There are a number of



Inductors and polyester capacitors in a speaker crossover network.

special types with special applications and only a few of them will concern us here. A practical point arises from this: when these 'variable' or non-linear components are met, take great care that any replacement made shall be exact. There are seldom effective substitutes, and the designer may have chosen a particular component with parameters in mind which may not strike us immediately. The range of variation, the voltage rating and the current rating should be studied.

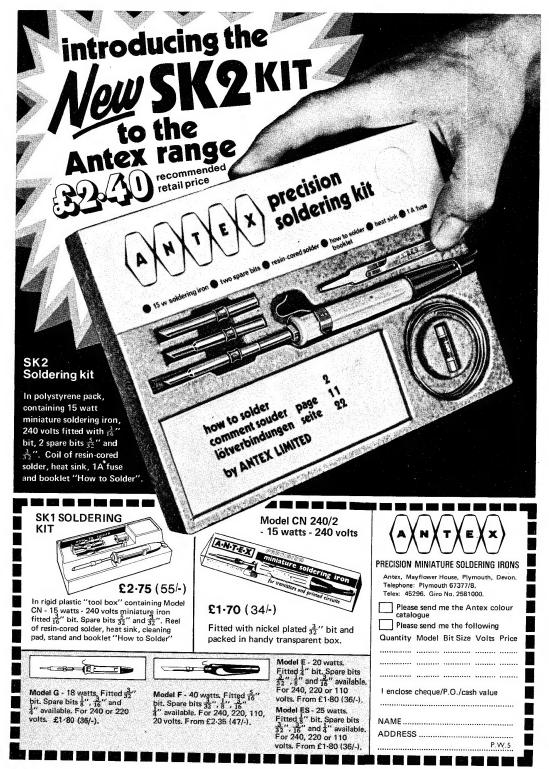
CAPACITORS

Capacitors sub-divide into three main groups: fixed, variable and electrolytic. Within these groups, there are many more divisions.

Fixed capacitors have various dielectrics and there are various methods of constructing and laying the foil or plates, giving all manner of special characteristics. It would be futile to attempt to explain these in detail, but a few salient points should be explained.

As with resistors, choice must be made according to capacitive value, tolerance, working voltage, peak voltage, temperature variation and in some special cases, frequency characteristics. For variable components, especially presets, the range of variation and its law must be taken into account.

Negative temperature coefficient components are widely used nowadays. There are many ways of



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NEW 6 VALVES 6 VALVES 6 147 46 6 1105 40 6 110	BBT 41.50 6KT. BW6 58 6KT. BW7 70 6KKS. BW7 80 6KKS. B	1	14H7 50 42 56 19Ag 56	DACS2 42 BLL21 6 DACF91 25 BBL31 4.3 DAF96 42 BCB21 4.3 DAF96 42 BCB20 DAF96 42 BC90 DF93 48 BC082 3 DF93 48 BC082 3 DF93 48 BC082 3 DF93 49 BC083 3 DF94 45 BC083 4 DF94 45 BC083 4 DF96 42 BC083 4 DH99 42 BC083 4 DH99 43 BC083 4 DH99 45 BCM14 3 DK96 47 BCM14 3 DK96 47 BCM14 3 DK96 47 BCM14 3 DK96 48 BCM14 3 DK96 48 BCM14 3 DK96 49 BCM14 3 DK96 49 BCM14 3 DK96 40 BCM14 3 DK9	18	\$\text{\$\texit{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\text{\$\
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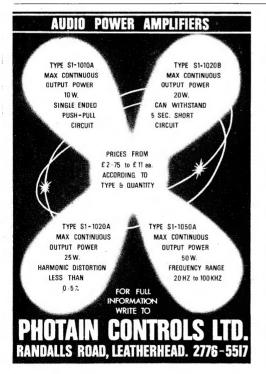
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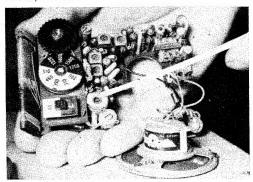
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stabilising tuned circuits but undoubtedly one of the easiest is to counter the drift due to warming up of the receiver by alteration to the tuning itself. This is done by the inclusion of a capacitor whose value decreases as the temperature increases. Important practical point here is, of course, to ensure that replacement shall always be with the same type.

Standard tubular capacitors are generally ceramic but there are variations such as the high voltage varicaps, made with barrier dielectric techniques, used widely with transistorised circuitry. These are junction-diodes chosen to take advantage of the capacitance effect: they will concern us later.

Variable capacitors may be the simple compression types found atop the small sealed ganged tuning capacitors in modern transistorised radios, or larger, more precise versions with fine thread screws and several interleaved layers of dielectric. Beehive capacitors, with concentric barrels and a coarse thread, are often found in older sets.



A small pot-core inductor, used here as the tuned circuit of the frequency-changer stage.

Electrolytics have an additional factor in their leakage current. In power supply circuits, where electrolytics are used to filter alternating currents from a supply that should be essentially d.c., we often come across the device of an additional, smaller, decoupling component across the main decoupler. This is to bypass the higher frequency currents that may be present in the ripple current.

Ripple current, in power supply circuits, is an important factor. It bears a direct relationship to the direct current drawn by the equipment, the load. For full-wave rectification, ripple current is about 1½ times the d.c., but a half wave circuit needs a reservoir capacitor in its filter circuit with a ripple current rating of three times the d.c.—a point to be watched when making replacements.

Excessive ripple current will cause overheating—application of "raw a.c." across an electrolytic can cause a spectacular but dangerous explosion. A point to be watched is the relationship of frequency and capacity. If high frequency ripple is present, the impedance of the capacitor, which may have been sufficiently low at its filter frequencies, rises dramatically and the heating effect increases.

The inductive element of electrolytic capacitors may have to be taken into account. This also will be mentioned later, when we come to practical circuitry.

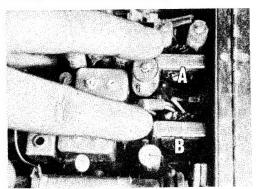
Polyester capacitors are being increasingly used in radio work because their method of construction decreases the inductive element. The tantalum capacitor, with some special virtues and few drawbacks except cost, has been used in many circuits, its advantage being a relatively large capacitance (albeit at low working voltage) for small physical size.

INDUCTORS

Inductors will be found in all sorts of applications, from the small ferrite beads with a single turn of wire around them to the multi-layer, tapped transformer of the modern stereo radio receiver. From the servicing point of view, inductance is either there or not—one seldom has to make up inductors, and we shall not waste space by talking about the factors determining inductance, permeability and so on. Instead, let's concentrate on the practical aspect of core variation, and the ways to overcome core breakage.

Iron dust cores are the usual way to change inductance of coils, these being threaded into the coil former. The individual particles of iron dust are insulated from each other, although closely packed, affording low loss and high permeability and so a miniaturisation of the whole inductor. But, for this reason, the cores themselves are more fragile.

It is not uncommon for wireless workshops to hold in stock large quantities of replacement iron dust cores. Instead of wasting time fiddling—often ineffectually—with painted, varnished, waxed or lacquered cores which crumble when torsional pressure is applied, the technique is to shatter the core, carefully remove the bits and clean the thread with a metal runner (of the same thread pitch), finally inserting a new core and aligning.



Interstage transformers A and B of a small transistor radio, with transistors between them wired directly into the circuit. Also to be seen are vertically mounted electrolytic capacitors and screened tuned circuits.

OTHER CIRCUIT ELEMENTS

A mention will have to be made of the alternative to the conventional inductor, the ceramic filter. The tuned circuit resonates at a frequency to which the crystal (usually a man-made crystal, a ceramic) is carefully cut and shaped. The actual arrangement is not straightforward as a simple crystal so used would have far too sharp a tuning response.

A pass-band of 180kHz is needed for the handling of the 15kHz audio signals at low distortion which we now require from our f.m. receivers. So two ceramic elements are used, with bandpass coupling. This gives the required bandwidth but retains the advantage of a sharp "skirt" at the extremes of the filter response curve.

Later we shall consider integrated circuits which are revolutionising receiver design in the same way as the innovation of transistors did some time ago. Also the use of various special semiconductors must be discussed. Field effect transistors (f.e.t.'s) have brought new opportunities to circuit designers, especially in the input circuits of v.h.f. receivers as well as to tape recording circuitry.

THERMIONIC VALVES

Valves are on the way out—thus runs the creed of some authorities. So they may well be, for there is little in the domestic field that is done by thermionic devices that can not be done as well or better by semiconductors. For a while, the barriers of high power meant that valves were still needed for certain applications. Now, with the improved silicon semiconductors available, even this barrier has broken down and the only remaining market for domestic valved circuitry appears to be in some television receivers, although a number of these are already fully transistorised.

But from the servicing aspect, valves are still very much with us. Not only do we need to know what they will do and how the circuits work but also what substitutes are available. Such information is not always convenient to come by—the best method of determining replacement suitability, of both valves and transistors, is a study of the relevant parameters.

Taking a simple case—nevertheless, not an uncommon case, for the triode amplifier stage is very often met with, especially in the low-signal sections of tape recorders—we have to consider first the operating conditions, i.e., heater voltage and current, circuit suitability, etc., and after that we can look at the Ia/Va curves, the Ia/Vg curves and the mutual conductance.

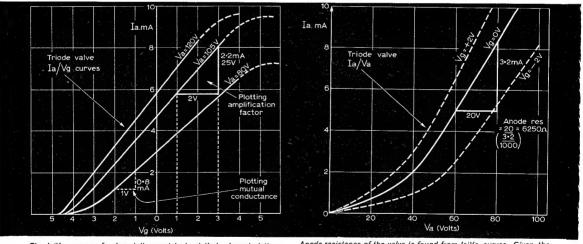
For any particular anode voltage there will be a curve which slopes up and then tails off when the anode current increases to and beyond a certain point, for a given grid voltage. There is a cut-off point where negative grid volts reduce anode current to zero and a saturation point where further positive grid volts cannot affect anode current. If we know the valve bias, cathode or grid, we can work out whether our alternative will do what we want.

If there is any further doubt, we can tackle the mutual conductance curves and the a.c. resistance. Amplification factor can be obtained from the results we already have, thus from the various factors already at our disposal we should be able to build up as good a picture about the valve we have as we are likely to need. Nine times out of ten we shall not need it: we shall be able to turn up our tables, select a replacement and go ahead. The tenth time could baffle us and this extra little bit of knowledge could save pounds.

SEMICONDUCTORS

Semiconductors can nowadays be divided into three sections: diodes, bipolar devices and others (which includes f.e.t.'s etc.). We are concerned with diodes very much indeed, as we shall see; there are plain rectifiers, diodes used as blocking devices, diodes used as circuit guide lines and finally variable capacitance diodes which can play an important part in the tuning of circuits.

The bipolar transistor (so called because it has two types of current carrier) has a few fundamental parameters that will enable us more easily to identify it and choose a possible substitute. Understanding of these parameters will also help us in the solution of some teasing circuit faults.



The Ia/Vg curves of valves tell us a lot about their characteristics. Three curves shown are plotted at different anode voltages. By comparing anode current change with grid voltage change causing it, we obtain the mutual conductance, gm, in mA/volt. Comparing curves we get the amplification factor, μ .

Anode resistance of the valve is found from la/Va curves. Given the anode load, the stage gain = $\mu \times Ra$ Ra + ra

Where Ra=anode load, ra= anode resistance and $\mu=$ amplification factor,

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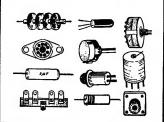
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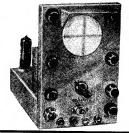
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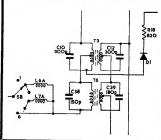
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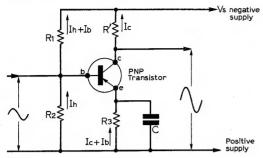


Fig. 1: Common-emitter PNP amplifier stage with arrows indicating "hole" conduction. Base voltage is stabilised by R1 and R2 with additional bias provided by R3.

It is to be assumed that the designer has done his homework. Table 1 gives the more important things we need to know about a transistor and a specimen set of figures for a general purpose n.p.n. silicon transistor has been quoted, to show the way these figures are expressed.

As an example of the use of these terms, Fig. 1 shows a p.n.p. transistor in common-emitter mode, as would be used for a simple amplifier. In this mode, we need to know the ratio of change of collector current for a change in base current, i.e., the current gain, β or α o' (beta or alpha nought dash). The subscript nought means that the current gain applies to d.c., the dash indicates the signal input is applied to the base. A plain α (alpha), without the dash is the symbol for current transfer ratio, and we usually see this written in a statement showing increase, this $\Delta \alpha$ or $\delta \alpha$.

The relationship between alpha and alpha-dash is important, and the formula

$$\alpha' = \frac{\alpha}{(1-\alpha)}$$

will be encountered. In Fig. 1 we see the various currents and voltages outlined with the arrows denoting hole conduction.

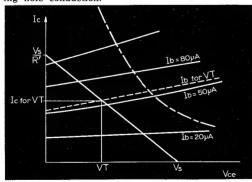


Fig. 2: A load-line drawn on the output characteristic curve of the transistor in Fig. 1. This depends on supply voltage Vs and value of R'. Chain-dotted line is power limitation and VT the working voltage.

TABLE 1

Max. Collector-Base Voltage	V _{СВО}	25V
Max. Collector-Emitter		
Voltage	VCEO	25V
Max. Emitter-Base Voltage	VEBO	5V
Max. Peak Collector Current	Icm	500mA
Max. Dissipation		
(at T _{emb} =25° C.)		300mW
Max. operating temp.	55 to 12	5°C
Characteristics	i desert	
Max. Collector-Base Reverse	and California	
Current	Ісво	0-2µA
Max. Emitter-Base Reverse		
current	1 _{EBO}	0-2μA
Max. Collector-Emitter	VCEO (sus)	96V/
sustaining voltage Max. Collector-Emitter	Y CEO (sus)	
saturation voltage	VCE (sat)	0·35V
Base-Emitter saturation	40.00	
voltage	VBE (sat)	0.65-1.0V
DC current gain	h _{FE}	50-300
Min. Gain-Bandwidth Product	fr	150
Max, output capacitance	Cab	6pf
Typical Noise Figure	N	7dB

Characteristic curves. From what we already know, we can draw up a similar family of curves to those we used for valves. Fig. 2 shows just such a series of curves used to determine the static collector current for various output characteristic curves. Values in the simple diagram we saw before can be calculated from this load-line graph, thus:

At cut-off, Vce = supply voltage.

At maximum current, all the voltage is dropped across R' and maximum current is V_{supply}/R'. If we choose a suitable voltage, call it VT for the collector, the base and collector currents can be determined from the load-line.

Volts drop across R' is $I_o \times R'$. Value of

$$R3 = V_s - \left[(I_c \times R') + VT. \right]$$

We get the static value of V_{be} from the input characteristic and know that the voltage drop across R2=drop across R3 minus V_{be} .

Then
$$V_{R2} = \left[R3 \times (I_c + I_b) \right] - V_{be}$$

If we now choose a suitable value of $I_{\mathtt{L}}$ we get the value of R2, thus:

$$\frac{\left[R3\times (I_c+I_b)\right]-V_{be}}{I_L}$$

and the voltage across R1 is the difference between V_s and $V_{\rm R2},$ or as calculated from the value of I_b (Ohms Law) taken from the load-line.

Dynamic considerations differ and the conditions for different kinds of transistor differ. These we shall tackle as they arise. The foregoing has been intended as an example—a way of laying the ground for Mr. King to launch into servicing techniques and circuitry without having to waste his time explaining every detail as he goes along.

END OF PART ONE

THE

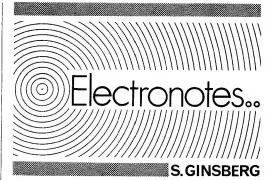
MW COLUMN

THE proposal to start local commercial radio on the medium waves has focused attention on two international common frequencies-1484kHz and 1594kHz. Many low power stations in Europe and parts of Africa occupy these channels. the only restriction being that there should not be interference between them. The BBC uses both frequencies for 2kW relays, so DXing on these channels will, in some parts of the country be limited to times when these locals are off the air. Manx Radio is on 1594kHz from sunset until 2015hrs while BBC3 broadcasts from Bournemouth and Dundee until 2230hrs. Look for CSB4 Emissoras Associadas de Lisboa; the US Air Force station in Athens; Marrakesh in Morocco and possibly Nova Lisboa in Angola; all on 1594kHz. The other channel-1484kHz-is more popular and is used by BBC4 in Kent, Lancashire and Norfolk; BBC2 in Scotland and BBC1 in Bournemouth. During the summer, the USAF base at Kenitra in Morocco has been heard on 1484 on several occasions while the USN 250-watter at Keflavik, Iceland, has also been logged. Radio Gibraltar is on this channel from 0655hrs to 2300hrs but has so far eluded the writer. Others to search for on 1484 are CSB90 in Funchal Maderia; Volos, a regional station in Greece; Riga in Latvia; Limassol in Cyprus; Ankara Turkey; Jeddah in Saudia Arabia.

A recent note by David Gibson referred light-heartedly to a DXer using the PW medium wave loop on the 10m amateur band. A MW loop will not, of course, function properly on 30MHz but it is quite easy to modify one to cover the Top Band. Remove one turn from the main winding; the range will now extend to 2MHz and the loop can be used for nulling-out Loran or other QRM. Useful results can be obtained in daylight with a modified MW loop to 3MHz but as frequency increases the directional properties gradually disappear.

As winter approaches in the southern hemisphere Latin Americans become prominent and can be heard in Europe from midnight until daybreak. Two high power stations in Buenos Aires Argentina are nearly always audible; LR1 1070kHz and LR3 950kHz. They are commercially owned and identify frequently between jingles. LR3 has the call Radio Belgrano and LR1 is Radio el Mundo. Others to look for include LR4 910kHz Radio Splendid Buenos Aires; LT2 1230kHz R. Splendid Rosario; LS6 1350kHz R. America Buenos Aires. From nearby Montevideo in Uruguay CX14 Radio Espectador is on 810kHz; CX28 R. Imparcial is on 1090kHz and CX16 850kHz has the unusual identification 'Radio Carve.' Venezuela is on a direct sea path across the Atlantic and can be logged on all parts of the band. Listen for YVLH 650kHz Radio Giradot in Maracay; YVKS 750kHz Radio Caracas; YVNM 1000kHz R. Mil in Moron; YVRS 1020kHz R. Margarita La Asuncion; YVQJ 1080kHz R. Barcelona; YVQT 1110kHz R. Carupano; YVOZ 1200kHz R. Tiempo Caracas; YVOH 1230kHz R. Valera.

CHARLES MOLLOY



Solid-state devices are slowly but surely advancing in areas which were previously held by the valve. But there are some applications where transistors find it hard to compete. This is highlighted in places where high power coupled with high frequency are required. To produce kilowatts at microwave frequencies is still the prerogative of the valve.

An application which illustrates this is that of cooking. Microwave ovens are becoming a reality as various types of sustenance are bronzed to culinary perfection by very high frequency energy.

Strange things happen when one uses radar-type frequencies to cook. An egg, for example, can be "boiled" by placing it in the oven and setting the timer for some 25 seconds. Thirty-five seconds will supply the article hard-boiled. Funny thing is that at around the 45 second mark the egg goes off with a bang. This is because the microwave energy concentrates at the centre of the unfortunate egg.

Small tea cakes, made from a proprietary brand of cake mix, take barely 35 seconds to cook and it is amusing to watch a lifeless paper cup full of gooey cake mix suddenly spring into life and fill the container. The weekend joint is reckoned to take around the eight-minute mark. No washing up of pots if you put the food on a paper container.

Digital techniques are still gaining popularity in electronic circles. More and more voltmeters and multimeters are boasting a digital readout. But the readouts are now commonly becoming available by themselves and there is an increasing number of modules being launched. These usually take the form of a small oblong package which houses a number of readout devices and often all the necessary logic circuitry for driving the solid-state readouts themselves. The whole package is offered as a single unit which can be fitted on to a front panel. Thus instead of fitting a meter, it is now possible to fit a solid state direct digital readout device. One of the advantages of direct readout is that parallax is avoided—the difference in absolute reading which is dependant upon whether the eye is directly over the needle of a conventional meter or slightly to one

Perhaps the most advanced digital meter available is one which automatically checks its own accuracy against a standard cell between readings. The circuitry switches from the measurement at the probes to the standard cell and back again. It does this repetitively and any slight difference between the standard cell and what the meter should read is immediately corrected by a fast-acting feedback loop.

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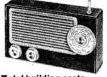
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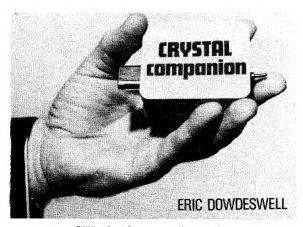
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ITH the large numbers of crystals now available at low prices it is not unusual to go into a components shop and find a large box full of assorted crystals being continually churned over by eager hands in search of some peculiar frequency.

While the old 10X type of crystal can probably stand up to such rough usage the more delicate HC6U type is liable to succumb to such barbaric

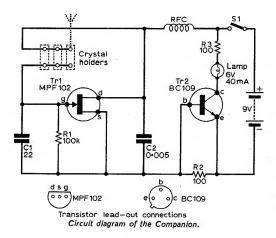
treatment.

The older "surplus" types can be over 25 years old and although well wrapped and apparently "as new" will often be found to have electrodes that have oxidised making the crystal useless. Having bought such a crystal and got it home it is a little annoying to discover that the wretched thing won't work!

This little crystal checker was designed to slip into the pocket so that it can be used to check almost any type of crystal before it is bought. It has worked with crystals from 100kHz to over 10MHz without any trouble.

Operation

The circuit is very simple but a little different from those usually found in this particular application



insofar as the operation is "fail-safe". That is, the indicator lamp is on when the crystal is not oscillating thus providing a check on the working of the lamp. If the lamp came on only when the crystal was oscillating failure of the lamp to light could be due to either a faulty crystal or dud lamp.

The oscillator circuit itself uses an MPF102 f.e.t. transistor and just four other components plus three crystal holders. The lamp control circuit has a BC109 silicon transistor which acts as a switch for

the lamp circuit.

In the non-oscillating state the MPF102 draws about 10mA current through resistor R2 which switches the BC109 "on" the lamp circuit being completed through the current limiting resistor R3 to the 9V supply. In this condition the lamp will light.

With a good crystal plugged in to one of the holders the MPF102 current drops to less than lmA, depending on the activity of the crystal used, the BC109 is switched "off" and the lamp goes out.

Since the lamp draws around 30mA the unit should not be left switched on longer than is required to check a crystal in order to prevent the early demise of the PP3 battery.

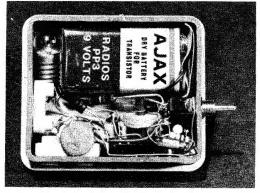
Constructing the "Companion"

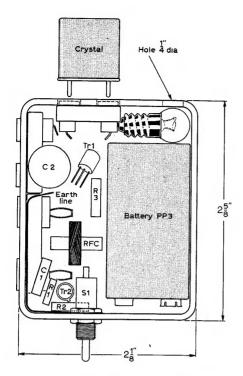
The checker can be built in any small box that will slip into the pocket and may be of metal or plastic or wood. The one used in the prototype is made up of a $^5\!\!\!_{\rm 4in}$ long section of plastic tube, rectangular in section, $2^5\!\!_{\rm 8}$ x $2^1\!\!_{\rm 8in}$ similar to that used in the construction of the popular Dewbox cabinets. Two Dewbox endcaps provide a handsome finish to the case.

Holes are drilled around the centre section to accommodate the three crystal holders to take 10X, HC6U and FT241/3 crystals so as to make the checker as versatile as possible. The holders are bolted on or fixed with Araldite. A ¹4in. diameter hole is drilled so that the indicator lamp is easily seen.

The simple wiring is mainly direct between components but a short busbar of thin tinned copper wire is run round one corner of the box to act as an "earth" return, one end of which is held under the locknut of the miniature on/off switch. Before doing this check that the dolly of the switch is isolated from the contacts.

After fitting the crystal holders, wire them in parallel, then fit one end cap and lay the PP3 battery



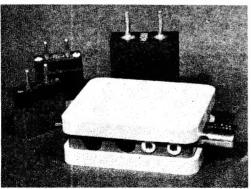


This actual size drawing of the Companion may be compared with the photograph on the previous page.

in position after which the remaining components can be soldered in place.

Because of the small size of this version of the checker a lamp holder was dispensed with and the connections soldered directly to the lamp. If a larger box is used a lampholder should be fitted.

The two transistors are wired into the circuit after everything else has been done. Especial care should be taken with the MPF102 transistor. Holding all three lead-out wires firmly in the jaws of a pair of longnosed pliers the wire ends should be tinned quickly and then soldered into the circuit without releasing the pliers. The BC109 is not so "touchy" but there is no harm in providing a heatsink when soldering it into place using the pliers as before.



* components list

Resistors:
R1 100kΩ ¼W R2 100Ω ¼W R3 100Ω ¼W

Capacitors:
C1 22pF Polystyrene C2 0·005μF disc

Semiconductors:
Tr1 MPF102 Tr2 BC109

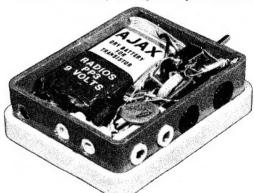
Miscellaneous:
Lamp 6V 40mA. Crystal holders (3) for HC6U, FT241/3 and 10X. S1, miniature on/off switch. Battery 9V PP3 and terminal clip. RFC, 2·5mH miniature. Dewbox ¾n. long with end caps or similar.

When the checker is completed the end caps can be pushed on leaving enough gap between them to accommodate an HC6U type crystal.

Checking Out

After double checking the wiring, paying particular attention to the transistor lead out connections, the unit can be switched on. Without a crystal plugged in the indicator lamp should light. Inserting a known good crystal should cause the lamp to go out.

The relative activity of a crystal may be estimated



This view clearly shows the hole for the indicator lamp.

by watching the lamp when the unit is switched on with a crystal in place. With an active crystal the lamp will go out immediately but if the crystal is reluctant to start the lamp will flash momentarily before going out. With a poor crystal the lamp may stay on but dimly.

With a really dud crystal the lamp will come on at full brilliance as if the crystal was not plugged in.

The "Companion" can be used on the workbench as a signal source for alignment purposes using crystals such as 470kHz or 1.6MHz for i.f. alignment or 100kHz or 1MHz for calibration work. A crystal on say 5MHz is very useful for calibration on the h.f. bands as well as for alignment.

If the checker is built into a plastic box there should be enough radiation for all the above purposes. If a metal box has been used it may be necessary to plug a short stiff piece of wire into any one of the unused crystal holder sockets to increase the radiation. A miniature telescopic aerial as supplied with some transistor radios is ideal for this purpose.

PRACTICAL WIRELESS

ALL IN THE JUNE ISSUE, ON SALE MAY 7th

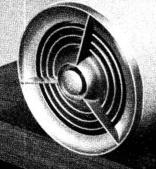
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CROSSWORD COMPETITION No.2

THE CARLONI RECEIVER

A 5-RANGE RF SIGNAL GENERATOR

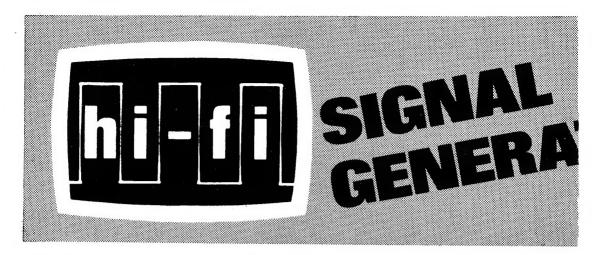
This simple signal generator uses an FET in the oscillator which covers 150kHz to 30MHz. The audio modulation is separately available for testing of audio amplifiers and circuits. The only power requirement is a 9 volt battery contained within the unit.



PLUS THE REGULAR "TAKE 20" AND "I.C. OF THE MONTH" SERIES AND OTHER CONSTRUCTIONAL ARTICLES AND FEATURES—ON SALE MAY 7th—PRICE 20p

SIMPLE IGNITION SYSTEM

You have seen advertisements for all kinds of gadgets that will reputedly save you many pounds a year in the running of your car. Here is one device, easily and quickly constructed, that will really carry out that promise. To try it is to keep it ... electronic timing for your car's ignition system. Circuits for positive or negative earth systems and all details in next month's issue of PW.



THE audio frequency signal generator described here was designed and built to fill the need for a high quality, wide range instrument, capable of permitting accurate and reliable distortion, gain and frequency response measurements to be carried out on a wide range of audio equipment.

For an a.f. generator to be really useful, it must be accurate in respect of frequency and voltage output calibration, and it must maintain this degree of accuracy under widely varying conditions of use.

The initial calibration accuracy will depend on the frequency and voltage standards available at the time of calibration, plus the time and care taken over the calibration process. Also accuracy will be dependent upon the quality of the components used and, to a lesser extent, upon the workmanship involved. The basic design will, of course, also influence both factors.

On the present design, much thought has been expended, plus not a little experimental work, in producing a design that fulfils most adequately all the requirements of a very high quality instrument. Good quality components, used well within their ratings, ensure that initial calibration accuracy will be maintained almost indefinitely. The mechanical design also, has been aimed at producing a robust, easily assembled unit.

CIRCUIT

The generator is based, in common with virtually all available a.f. generators, upon the well known, and proven Wein Bridge. The three transistors Tr1, Tr2 and Tr3 form a high gain amplifier with d.c. coupling throughout, with the exceptions of the frequency determining capacitors. This has the twin advantages of being sparing of coupling capacitors, which lessens expense, and relieves the designer of solving unwanted phase shift problems.

The frequency of oscillation is dependent on the setting of VR1 and the capacitors selected by SW1. For oscillation to occur there must be adequate gain and there must be positive feedback, i.e. there must be a phase shift of 360° between the input and the output of the amplifier. For the Wein Bridge to oscillate, the gain requirement is very modest, being only 10db or three times. Since the gain of the

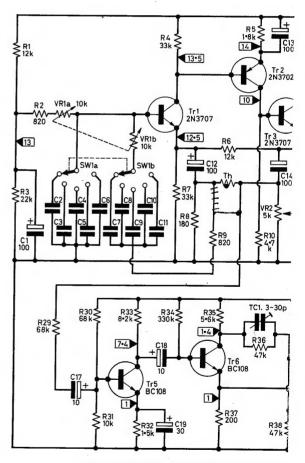
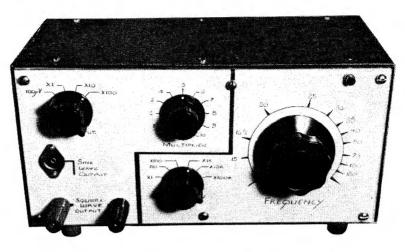
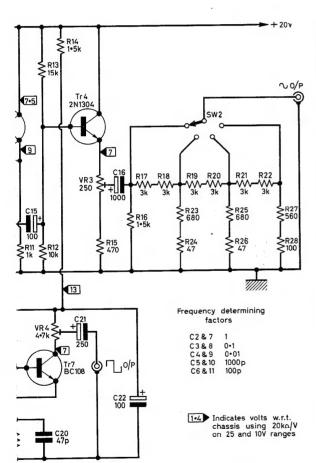


Fig. 1: The circuit of the HI-Fi Signal Generator, an expla







nation of the operation of the various sections is given in the text.

★ components list

Resis					
R1	12kΩ		470Ω		68kΩ
R2	820Ω	R16	1.5kΩ		68kΩ
R3	22kΩ	R17	3kΩ	R31	
R4	33kΩ		3kΩ		1.5kΩ
R5	1⋅8kΩ		3kΩ		8·2kΩ
R6	12kΩ		3kΩ		330kΩ
R7	33kΩ		3kΩ		5·6kΩ
R8	180Ω	R22	3kΩ		47kΩ
R9	820Ω		680Ω		200Ω
R10	4·7kΩ	R24			47kΩ
R11			680Ω		4·7kΩ
	10kΩ		47Ω	R40	2·2kΩ
R13	15kΩ		560Ω		1-5kΩ
	1.5kΩ		100Ω	All !	5%
	10kΩ±10k				
	5kΩ Lin. (
VR	250Ω skel	eton pr	eset		
VR	5kΩ skele	ton pre	set (can be	e 4·7ks	2)
Capa	citors				40 F 4834
	100µF 15V	C10	1000pF 17	"LCIA	10µF 15 V
C2	1μF 1%†	C11	100pF 1%	T C19	30μF 15V
C3	0·1μF 1%	C12	100μF 15\	/ C20	4/pr 1%
C4					250µF 15V
C5	1000pF 1 2	6† C14	100μF 15\	/ C22	100µF 15V
C6	100pF 1%	† C15	100µF 151	CZS	100µF 15V 1000µF 25V 8µF 25V
C7					
C8			10µF 15 V	C25	100µF 50V
C9	0·01μF 1%	6T	ulmmar +	ena to	av4
	3-30pF B		immer i	SCC II	
	iconducto	S To	BC108		
Tr1			2N3053		
Tr2		119	E.6\/ #00	m\M 7	ener Diode
	2N3707	711	S.T.C. R	33 The	ermistor
Tr4	2N1304 BC108	20	Bridge R	ectifie	r. silicon
		, Br	BY164 or	simil	ar
Tr6	BC108		B 1 104 01	3111111	
Misc	ellaneous /1 2-pole, 6-		nly 5 positi	one II	sed)
SV	/ 2-pole, b	way (U	my a positi	J113 U	
	/2 2-pole, 4- /3 Mains or	ΛĦ			
T1	Maine 4	onefor	mer 240V	pri	12-0-12 sec
11	Wains U	0.94)	OSmA He	me R	adio Cat. No.
	TRAKATA				
A 1	I WINITO	d nere	nex for ra	se: In	dicator neon
All	animum at	n heis	hav (a) on		THE THE STATE OF

transistors used is considerably higher than this, no problem exists here. The phase shift requirements are also met, since the trio introduce a phase shift of 180°, and the frequency network introduces further 180°. Since these phase shifts are effectively in series, the requisite 360° phase shift is produced.

Stability of the output voltage is important and to this end a thermistor is used. Since it has a negative temperature coefficient, it must be connected in the negative feedback mode. In Fig 1, it is in series with C12 and C14 and controls the a.c. negative feedback from Tr3 emitter to Tr1 emitter. The correct part of its coefficient slope is selected by the value of R8, under which conditions it will hold the output constant to better than $\pm 1 \mathrm{dB}$.

Although the a.c. gain is controlled by the negative feedback via the thermistor, the d.c. gain is still high. Although the silicon transistors chosen have very stable gain and leakage characteristics, the high overall gain does mean that any change in Tr1's characteristics, and to a lesser extent in Tr2's, will disturb the operating point of Tr3 to the detriment, if not complete failure, of the complete circuit. D.C. negative feedback via R6 provides a high degree of stability against any such changes.

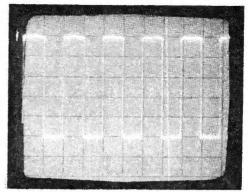
In Fig. 1 five pairs of capacitors, C2-C6 and C7-C11, provide five frequency ranges, selected by SWI, with VR1 (a and b) providing continuous coverage with some slight overlap at either end. The degree of overlap is dependent on the values of R2 and R9, increasing them decreases the overlap, the converse also applying.

The output voltage from the oscillator is taken from the wiper of VR2, which acts as an infinitely variable control, in conjunction with the decade attenuator which follows later in the circuit. This feeds into an emitter follower, Tr4, which has a high input and low output impedance and effectively isolates the oscillator from any load which may be connected across its output. Tr4 is biased at 10mA emitter current by R12 and R13, permitting resistive loads as low as 1500 to be connected across the output without altering the output voltage by any significant amount.

The coarse attenuator comprises SW2 and range resistors R16 to R28. It is a constant impedance type, with a characteristic impedance of 600Ω, and provides four decade voltage outputs of IV, 100mV, 10mV and 1mV. This is somewhat more complex, and requires more resistors than the simple potential divider type of attenuator. It is preferred because of the near constant resistance it offers to the load on its four ranges. The resistance values as calculated are odd but the series connection of the range resistors enables preferred value resistors to be used with very little loss of accuracy. If an accurate a.c. millivoltmeter is available, the series connections enables individual resistors, i.e. R24, R26 or R28, to be changed to enable true decade switching to be achieved. The change in value should not be great; the next preferred value should prove satisfactory.

Although sine wave testing of audio equipment can reveal a great deal of information about it, it does not always tell the full story and needs to be complimented by another wave form.

The most commonly used such waveform is a square wave, and this is produced by the two transistors Tr6 and Tr7, with the assistance of Tr5. Tr5 is an overdriven amplifying stage, fed with the sine wave via R29 and C17. The output of Tr5 is



Actual photograph of the square wave at 1kHz.

partially squared and fed via C18 to Tr6, which in conjunction with Tr7, forms the well known Schmitt Trigger configuration. The component values were chosen for a very fast rise time. TC1 is a "speed up" capacitor, and is used in conjunction with R36, to form a time constant that exactly matches the parallel RC combination of the input impedance of Tr7 base. When these are equal, the coupling from Tr6 collector to Tr7 base is truly aperiodic, and extremely rapid rise times result.

The collector load of Tr7 is a preset resistor, VR4, so that the output of the square wave can be preset to any desired level, up to a maximum of approx 12V peak-to-peak. The coupling capacitor C2I must be as high in value as possible in order to maintain the tops of low frequency square waves as horizontal as possible.

POWER SUPPLIES

The question of power supplies will depend on the length of time the equipment is in use. For short, intermittent periods of use, batteries can be used. However, the current consumption of 25mA at 20v means four series connected 6V batteries of reasonably high capacity in conjunction with a 20V zener diode for stabilisation purposes. Four such batteries will be somewhat bulky, and the use of mains supplies is therefore an attraction. The circuit of the mains voltage power supply used on the prototype is shown in Fig. 2. The transformer used was rated at 50mA at 12-0-12V, used as 0-24. This is then rectified by the bridge BR1 to provide a voltage across the reservoir capacitor C25 of about 30V. This is then applied to the collector of the series regulator transistor Tr9, and to R41 which is the collector load of the error amplifier Tr8, the emitter voltage of which is held at a constant 5.6V by the zener diode ZD1. The current drawn by ZD1 is about 5mA.

COMPONENTS

For optimum performance and maximum long-term reliability, all the components used in the construction of the generator must be of good quality.

The semiconductors used were carefully selected, and should not be changed unless the individual knows what he is doing and why. Whilst comparable semiconductors do exist, their use has not been investigated, and no advice on this score is therefore offered.

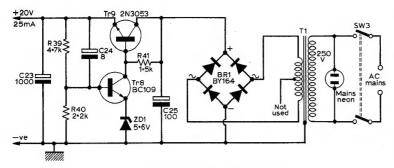


Fig. 2: The circuit of the stabilised power supply.

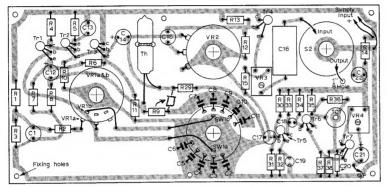


Fig. 3: The component layout and details of the printed circuit board,

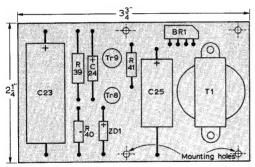
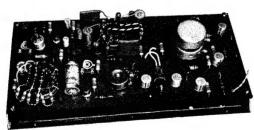


Fig. 4: The component layout of the power supply.



The neat construction using a printed circuit board can clearly be seen here.

With the availability, freely and cheaply, of high quality 5% carbon film resistors, there seems little point in using the inferior carbon composition types, unless these are to hand and cost is of paramount importance.

The majority of the electrolytic capacitors used are of the single ended, or P.C.B. type, as these assist in the conservation of space. The only radial ended electrolytics are those combining high capacity with a relatively high working voltage.

The capacitors used in the frequency determining network of the Wein Bridge should preferably be of 1% tolerance, as this means a single frequency scale can be used on the front panel. It must be admitted that 1% high value capacitors are somewhat expensive and wider tolerance capacitors can be used in the interests of economy. This then requires either the careful selection of capacitors, or the adoption of

a multiple frequency dial calibration if accuracy is not to be sacrificed to cost. Readers wishing to use 1% capacitors can purchase WIMA capacitors, as used on the prototype, from WAYCOM LTD., WORKINGHAM ROAD, BRACKNELL, BERKS.

CONSTRUCTION

For this type of circuit, a circuit board of some type is almost mandatory. The prototype was built on to an etched circuit board, measuring 9½in×4¾in, shown in Fig. 3. The fully completed board is supported behind the front panel, and parallel to it, by means of lin long insulated pillars drilled and tapped 4BA at either end. This allows ¼in 4BA bolts to be used for securing the circuit board, whilst the perspex and metal panel are secured by ½in 4BA bolts

The power supply is built upon a piece of plain Veroboard, 2^1_{4} in $\times 3^3_{4}$ in shown in Fig. 4 with the component siting.

The supply board is mounted on the rear of the cabinet. That on the prototype was backed by a piece of ¹₁₅in perspex to preclude any danger of short circuits between the component leads and the cabinet.

The front panel of the instrument was made of white card which is clamped to the front of the cabinet behind a protecting piece of 1 ₁₈in perspex.

The cabinet for the prototype was made from 20s.w.g. aluminium to the sizes in Fig. 5. The easiest way of ensuring that the circuit board, cabinet front and perspex all line up accurately, essential if the control spindles are to pass without fouling through the front panels, is to make up the cabinet first. Then the circuit board and perspex are cut slightly smaller

so that they drop into the recess behind the front panel, formed by the top, bottom, and sides. The required holes are then scribed through, using the metal front panel as a template, and carefully drilled out. The holes for the controls in the circuit board will need to be of $^3\mathrm{ein}$ diameter, the corresponding holes in the front panel can be $^1\mathrm{_{4}in}$ if accuracy in alignment is achieved. The holes for the output terminals will depend on the components actually used.

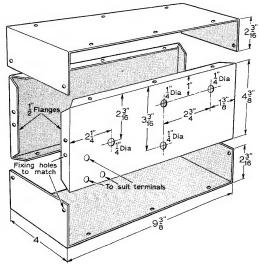


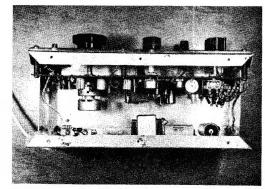
Fig. 5: The details of the case.

SETTING UP

After completing both circuit boards, they should be carefully inspected for soldering and for wiring errors. Then the power supply can be connected to the mains, its output disconnected from the generator board. The output should be monitored and either R39 or R40 altered if necessary to set the output voltage at 20V. The generator board can then be connected and further tests made. A meter capable of reading up to 25mA should be connected in series with one of the supply leads; a reading $\pm 10\%$ of this should be obtained. The meter can then be removed from circuit. Voltage tests using a $20 \mathrm{K}\Omega/\mathrm{V}$ meter should provide readings substantially in agreement with those given in Fig. 1.

In order to ensure that the generator is correctly calibrated in respect of frequency and voltage, an accurate, wide range oscilloscope and a.c. millivoltmeter are required. Another a.f. generator of known accuracy is a useful aid, but is not indispensible. It is only really necessary if wide tolerance capacitors are used in the frequency network.

The oscilloscope and meter should be connected to the sine wave output, and a check made for oscillation throughout all ranges. The sine wave should "look good"; however a visual check for distortion does not reveal it unless it is really severe. Should this prove to be the case, transistor "spreads" may be responsible, in which a change in Tr1 bias effected by changing R1 or R3 may help. If it is due to a thermistor "spread," variation in R8 may help.



Components should not be varied unless really necessary, and even then variations should be in small steps.

If all seems well, attention can be turned to frequency calibration. Here two courses are possible. If 1% capacitors are used for C2-C6 and C7-C11, one frequency scale will suffice. If wide tolerance capacitors are used, a different scale for each range will be necessary, unless some accuracy can be sacrified in the interest of simplification and one scale. Another a.f. generator will be necessary if different frequency scales are to be provided. The use of Lissajous figures for frequency calibration is well known and need not be repeated here.

Lissajous figures are used, using the mains as a frequency standard. VR1 is used on Range 1, and points plotted at 15Hz, 16·6Hz, 20Hz, 25Hz, 30Hz, 35Hz, 40Hz, 50Hz, 75Hz, 100Hz and 150Hz. Range 2 will be these frequencies x10, Range 3 will be x100 and so on.

The next step is to set the output voltage. VR2 should be at maximum, with SW2 on the 1V position. Using a frequency of 1kHz, VR3 is set to give a reading on the meter of precisely 1V. SW2 is then set at 100mV, and the output checked, similarly at 10mV and 1mV, if the meter will read as low as this R24, R26 and R28 can then be changed if necessary.

The frequency response can then be checked if required, and should be constant to $\pm 1 db$ from 15Hz to 150kHz, falling to -2.5 db at 1.5 MHz.

For setting the Schmitt trigger, the ideal 'scope would be a d.c. coupled one, with the h.f. response extending to 10MHz or higher. On an a.c. coupled 'scope, considerable sloping of the tops of the low frequency square waves can be expected.

Similarly, unless the 'scope has a first class h.f. response, rounding off the shoulders of the leading edges of the square waves can be expected at high frequencies. The measured rise time of the prototype square wave at 1kHz was 250nS (nanoseconds).

The effect of TC1 is only apparent at the higher frequencies, where it should be adjusted so that the shoulders of the leading edges of the square waves have neither "overshoot" or "sag."

VR4 can be adjusted to provide a square wave output of up to 12V peak-to-peak, Designing an attenuator that does not degrade a fast square wave is not too easy and was not attempted.

The mark-space ratio should be one-to-one, and is dependent upon Tr5 providing a symmetrical output to the trigger. Any variation of this ratio from the required 1:1 can be corrected by variation in the value of R29.



MONTHLY NEWS FOR DX LISTENERS

DUE to the postal dispute no reports have reached me in time for inclusion in this issue. The following news items were obtained from Radio Sweden's DX programme: 'Sweden Calling DXers' and from my own log.

GERMANY. DRM23, Radio Bremen on 6190kHz has announced that it plans to increase its power from the present 10kW in the near future.

GUATEMALA. Radio Cultural has been reported at 1205 on 9505kHz with a strong signal.

NEW CALEDONIA. Radio Noumea is reported to be using the new frequency of 9510kHz. The times of the broadcasts are 0600-1100 and 2330-0200, the language used is French.

NORWAY. Radio Norway now broadcasts a DX programme called 'DX Radio Norway' on the first Sunday of every month. The first programme was scheduled to be broadcast on March 7th. The programmes are transmitted at 0800, 1000 and at two-hourly intervals throughout the day. Radio Norway has also reported that it hopes to have transmitters with power in the region of 500 to 1000kW in operation before the end of 1974.

PERU. Radio Nacional, Lima, Peru, has been heard broadcasting at 0300 on a frequency of 6082kHz. The programme consisted of Peruvian music.

Choosing a receiver

Since I started writing this column I have had many queries from readers, the most common being about the choice of equipment. In the following paragraphs I list the most important features for a DXer's receiver. Each DXer requires a slightly different receiver and the following is my own order of importance.

An adequate short-wave range. Before purchasing a receiver the listener should decide which bands he is interested in. Some listeners may require coverage of the 49m to 13m bands only, whereas others may have a special interest in the tropical bands (120 to 60 metres). Most listeners will probably settle for a general-coverage receiver (540kHz to 32MHz).

An external aerial connection. This is a very important point which can easily be overlooked. No short-wave receiver can give DX performance unless a good aerial is used.

Bandspread frequency control. With the present crowded state of the bands it is essential to have a receiver with this feature to enable adjacent stations to be separated. The receiver should also have a logging scale so that the setting can be noted and returned to at a later date.

Adequate selectivity. Selectivity is a measure of

THE BROADCAST BANDS

Malcolm Connah

Frequencies in kHz Times in GMT

the ability of the receiver to separate two adjacent stations. Some receivers have a variable selectivity control and this can be very useful.

Adequate sensitivity. Sensitivity is a measure of the receiver's ability to pick-up and amplify weak signals. A DXer's receiver must be sensitive as he is mainly interested in weak signals.

An aerial matching device. Sometimes called an antenna trimmer this very useful control allows the aerial to be correctly matched to the receiver. A very small mis-match can cause a serious loss of signal.

A crystal calibrator. This gives signals at intervals of 100kHz and is an invaluable aid to determining the exact frequency of any station.

A signal-strength indicator. Usually in the form of a magic-eye indicator or an S-meter. These indicators enable the relative strengths of incoming signals to be determined.

An r.f. gain control. Most receivers have an audio gain control only, the addition of a separate r.f. control can greatly assist in the reception of difficult signals.

An automatic gain control switch. All receivers incorporate some form of automatic gain control which adjusts the gain of the receiver to compensate for sudden fluctuations in the input signal. The a.g.c. switch enables the circuit to be disconnected, with the circuit out of action weak signals can be greatly amplified.

A noise limiter. Sensitive receivers are susceptible to noise interference. The noise limiter clips the tops of the noise signals and stops them from reaching the output of the receiver.

I hope that the above paragraphs have been of interest to those of you who are thinking of buying a receiver, I look forward to receiving reports from you in the near future.

All reports please to me at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex, by the 15th of the month.

1971 WORLD RADIO-TV HANDBOOK Published by Billboard A.G. and available from Fountain Press, 46 Chancery Lane, London, W.C.2. 372 pages, 9 × 6in. Price £2.30

POR those not familiar with this publication it lists virtually every radio and television station in the world and provides all the information you are ever likely to need for DXing—in fact I don't know of a short wave listener who doesn't regard it as a sort of "bible".

Every year we look forward to the new edition and we have not been disappointed with this one. The introductory articles that used to take up the first part have been dropped and published separately for the first time under the title "How to Listen 1971".

We could hardly do without it at the P.W. offices and we are sure you will be in the same position if you are interested in any form of DXing.—H.W.M.

ACH month, letters arrive which raise various queries. Some contain the usual questions which crop up again and again, others are peculiar to a person or piece of equipment. Over the years numerous questions have been answered but it seems obvious that more and more newcomers are reading this page and are, therefore, repeating the same questions which others before them raised. So for once, let's have a session of answers to some of the problems which have arrived over a period of months.

First query is usually a "By the way" enquiry and asks what gear does G3JDG use and on what bands can emission from your scribe be detected. Gear permits 120W of a.m./c.w. from 3.5MHz to 30MHz and 10W on topband. Main interests are the h.f. DX bands and an unashamed preference for c.w. Phone is used on topband and then, usually, mobile. The receiver is a valve type with r.f., mixer, two i.f., det. and one audio plus b.f.o. and Q-multiplier. An a.t.u. is always used since aerials are a source of much experimentation. Antenna for the past six months has been a solitary slither of wire some 60ft. long at about 18ft. Current move into a "new" house should see activity on 14MHz c.w. and on topband a.m. at first. A modified Pye reporter transceiver allows 18W on 70MHz.

Two questions which occur more often than any others. Where can I get a list of callsigns and countries, and what is the "best" aerial to use? A country's list can be obtained from the R.S.G.B., 35 Doughty Street, London, WC1N 2AE, price is 612p Incidentally, those who are not members of the R.S.G.B. might like to send for a free specimen copy of the Society's monthly publication Radio Communication.

The short answer to the question, "What is the best aerial to use", is simply "There is no such animal". An aerial which is excellent for a particular band will not necessarily be any good on another frequency. Again, the particular physical location can affect the performance. Aerials are often largely a matter of suck it and see.

The only aerial which might be considered an "all frequency" affair (speaking now of 1·8 to 30MHz) is simply a length of wire as long as possible, as high as possible and as far from earthed objects as possible. The wire is then fed to the receiver via an a.t.u. (aerial tuner unit). This is, in fact, the system in use at G3JDG at the moment. It is essentially a compromise system and there are other set-ups which could quite easily out-perform it. Aerials, or antennas, are a subject in themselves and there are numerous textbooks which discuss the relative merits of each type to which interested readers are respectfully referred.

A common question from newcomers is simply where to start, what receiver, etc. If the receiver is to be home-built, then much will depend upon individual skills in construction. For the absolute beginner it might be easier to purchase a simple kit,

THE AMATEUR BANDS David Gibson, G3JDG

Frequencies in kHz • Times in GMT

the only real alternative being to buy a ready-made unit.

Headphones are a must and aerials have already been dealt with as has a country's list. Armed with these basic essentials one is all set to start the initiation of becoming a short wave listener (s.w.l.). Amateur bands to listen on (up to 30MHz) are: 1.8—2.0MHz; 3.5—4.0MHz; 7.0—7.1MHz; 14.0—14.35MHz; 21.0—21.45MHz; 28.0—29.7MHz.

A good wall map of the world is useful and a packet of coloured drawing pins will permit stations logged to be located on the map. Incidentally, this procedure, besides adding interest, will also provide a surprisingly good working knowledge of geography over a short period of time.

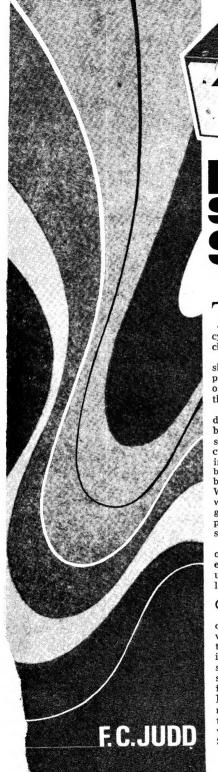
A point which often appears to baffle the beginner is the disappearance of signals from a particular band or bands. There are many causes of fluctation in communications. For example, the height of the ionised layers above the earth which reflect the radio waves back has a marked affect. Again, the activity of the sun plays an important role as does the season or time of year. As an example, at the time of writing, the 14MHz or twenty metre band is mainly active from around 0700 to 2200hrs although some signals might be heard occasionally outside these times. The 21MHz band is mainly active between 0700 and 2000hrs while up on 28MHz the signals are in evidence between 0800 and 1800hrs.

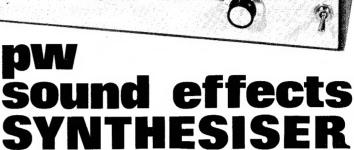
Another favourite query is how to get a transmitting licence and what is involved. The licencing body in the U.K. is the Post Office. In order to obtain a licence the Post Office need to be satisfied of a persons technical competence to operate transmitting equipment.

There are two types of licence. For a full "A" licence, which permits the holder to transmit on all amateur bands from 1 ·8MHz upwards, it is necessary to pass a written technical examination. The other test is that the candidate is required to send and receive Morse at the rate of 12 words per minute. A pass in the technical paper is essential for either licence.

If the Morse test is not taken it is still possible to obtain a licence but in this case transmission is restricted to the amateur frequencies from 144MHz (two meters) and higher. Thus all the h.f. DX band would be "out of bounds" as regards transmission. This licence is called a "B" licence and holders are distinguishable by a callsign which begins "G8" followed by three letters. Some holders of full licences have a G8 callsign but these are followed by only two letters. Note that in Scotland callsigns begin "GM" and in Wales with "GW". GI (Northern Ireland), GC (Channel Islands), GD (Isle of Man). Thus a G8 licence issued to a Scottish amateur would begin GM8, etc.

Logs for the Amateur Bands must arrive before the 15th of each month. The address is: 14 Manland Avenue, Harpenden, Herts





PART 3

THREE more circuit boards and the power supply complete the electronic percussion and sound effects synthesiser for which general constructional details and the circuits etc. for castanets, cymbal, snare drum, triangle, woodblock, taxi horn, train whistle and bell chime were given in parts 1 and 2.

The remaining two generator circuits Nos. 9 and 10, are those for a ship's siren and the sound of the sea (surf). Details are also given in this part for the mixer amplifier and power supply etc. However, before going on to these circuits it would be as well to deal with the small modification

that must be carried out on the organ key switch assembly.

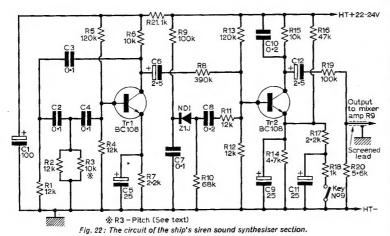
There are 10 keys on this and when either one is pressed it will stay down until pressed again. This action is facilitated by small phosphorbronze clips, one to each key and the function of each clip is to hold a small brass pin within the key guide frame. The operation of all the circuits 1 to 9 is that they must produce the sound when the key is pressed and instantly released, or pressed and held under pressure, i.e., the keys must behave like a piano key. All that is necessary is to remove the phosphorbronze clips on keys 1 to 9 only and shake or pull out the small brass pins. When the keys are now pressed they will immediately return to normal when pressure is released. Key No. 10 which actuates the sea sound generator (circuit No. 10) must be left to work as intended i.e., when pressed down it must stay down until pressed again. This allows the sea sound to be run continuously without having to hold the key down.

The contact system on each key is simply a pair of single pole changeover switches and one or both can be used for the make and break of each keying circuit. The writer simply paralleled both sets of contacts but used them as a single make/break switch. This will be referred to again

later.

Circuit for Ship's Siren-No. 9

This circuit is given in Fig. 22 and employs a phase shift oscillator (Tr1) operating at a frequency of about 120Hz and which can be adjusted by variation of R3. The output from Tr1 is attenuated by R8 and fed directly to Tr2 which is biased to cut-off by R16. The noise content for the sound is produced by the noise diode ND1, the output signal from this being slightly attenuated by R11. The sine-wave signal from Tr1 and the noise signal are combined in Tr2 which is keyed on by key No. 9. The output from Tr2 is attenuated to a level suitable for the mixer amplifier by R19/R20. The circuit board layout is given in Fig. 23. The circuit should require little or no adjustment except for pitch but the noise content of the sound, which should not be too predominant, can be regulated by variation of R11. Waveforms for this circuit are shown in Fig. 26 (Ship Siren circuit, A and B).



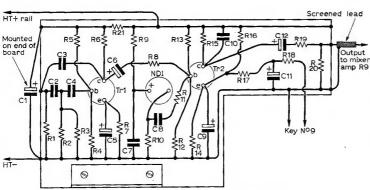
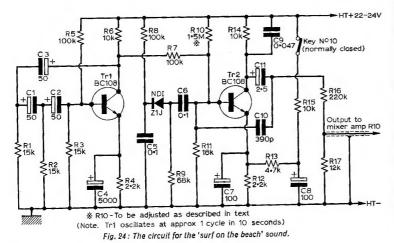


Fig. 23: The component layout for the ship's siren synthesiser.



Surf on the Beach—No. 10

Surf rolling up on the beach and receding is a fairly slow movement and the sound itself, which is mainly random noise, rises and falls in amplitude at the same rate as the movement of the water. Here we need a slow but sinusoidal rate of change in signal level. The noise diode ND1 provides the white noise but to be effective a slight change of pitch in the noise is needed as well as the amplitude variation.

The noise signal is fed directly to Tr2 which is rendered almost non-conducting because of the large value resistor $(1.5M\Omega)$ between the base and positive rail. .The base is however, directly coupled (via R7) to the collector of the slow running phase shift oscillator Trl. As the potential at Trl collector rises and falls Tr2 will become fully conductive and/or quiescent at the same rate. The noise output signal from Tr2 will rise and fall accordingly. The phase-shift oscillator runs at approximately 1 complete cycle in 10 seconds. The change in pitch of the noise output is produced by feedback via C10. In operation, key No. 10 is pressed down and stays down (see above) so that the sound continues until the key is again pressed and released. The sound must not cut off completely as the amplitude falls but simply fall to a low level. Adjustment to the value of R10 $(1.5M\Omega)$ may therefore, be necessary, i.e., the value may have to be reduced to $1.2M\Omega$ or increased to 1.8MΩ. The sound produced by the circuit is quite realistic but should not be too loud when used as a background effect for desert island type tunes. Note that the key for this circuit (No. 10) is wired so that the key contacts are "on" whilst the circuit is nonoperational. When key No. 10 is closed as shown in the circuit, Tr2 is biased to cut off. The circuit board layout is shown in Fig. 25 and relevant waveforms in Fig. 26 (Surf on Beach Circuit A and B).

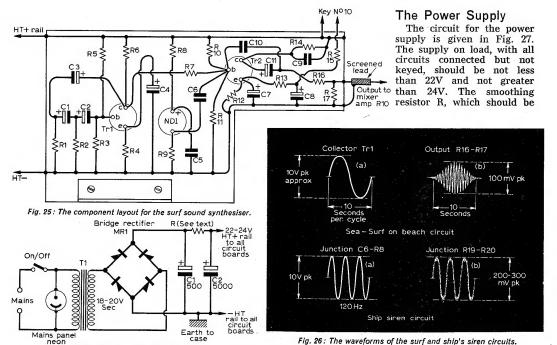


Fig. 27: The power supply circuit.

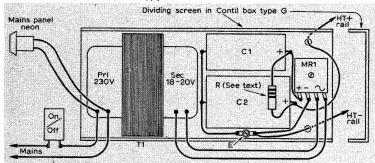


Fig. 28: The construction of the power supply section which is built on the dividing panel supplied with the case.

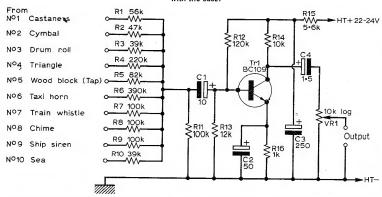


Fig. 29 : The circuit of the mixer amplifier. The values of R1-R10 may have to be varied as mentioned in the text.

about $1k\Omega$, may therefore require adjustment to value. The total current drawn by the generator circuits (not keyed) and the mixer amplifier should be approximately 20mA. The layout for the power supply as used on the dividing chassis of the Contil Mod 2 case employed for the prototype unit, is shown in Fig. 28.

Mixer Amplifier

This is a single stage signal amplifier with input attenuation to reduce the signals from each of the generator circuits to a level appropriate to each of the sounds. The input attenuation resistors R1 to R10 also serve to prevent impedance loading by each circuit and also signal overloading of the amplifier itself. The values chosen for R1 to R10 may require slight adjustment one way or the other in value so that the levels of the various sounds are relative for any setting of the volume control. The volume control has been provided simply to control the overall output from the unit.

* components list - part three

Transis					
Tr1,		BC	108 Mullar	d	
Noise (ND1		see pa	art 1) Semi	tron	
Resisto	a province of the province				
R1	12kΩ	R8	390k Ω		10k Ω
R2 R3	12kΩ 10kΩ	R9 R10	100k Ω 68k Ω	R16 R17	47k Ω 2·2k Ω
R4	12k Ω	R11	12k Ω	R18	1kΩ
R5 R6	120k Ω 10k Ω	R12 R13	12k Ω 120k Ω	R19	100k Ω 5·6k Ω
R7	2·2kΩ		4·7k Ω		1kΩ
		II I W,	10% types		
Capaci C1	tors 100μF		C7	0·1μF	
C2	0-1μF		C8	0.2µF	
C3 C4	0·1μF 0·1μF		C9 C10	25μF 0·2μF	
C5 .	25μF		C11	25μF	
C6	2·5μF		C12	2·5μF	
Sea (Surf on E	3eac	h) Circu	it No.	10
Transis	tors		:108 Mullai		
Tr1, Noise l		٦٥	ivo munal	Year o	
ND1	Z1J (see pa	art 1) Semi	tron	
Resisto R1	ors 15kΩ	R7	100k Ω	R13	4·7k Ω
R1 R2	15k Ω	R8	100k Ω	R14	10k Ω
R3	15k Ω	R9	68k Ω		10kΩ
R4 R5	2·2k Ω 100k Ω	R10 R11	1·5M Ω 18k Ω	R16 R17	220k Ω 12k Ω
	10k Ω	R12	2·2k Ω		
		II ‡W	10% type:	•	
Capaci C1	tors 50μF		C6 0	·1μF	
C2	50μF		C7 1	00μF	
C3 C4	50μF 5000μF			00μF ·047μF	
Č5	0·1μF •			90pF	
Mixe	Amplifi	er			
Transi	itors				
Tr1,	BC109 Mt	mard			
Resisto R1	56k Ω	R7	100k Ω	R13	12k Ω
R2	47k Ω	R8	100k Ω	R14	10kΩ
R3 R4	39k Ω 220k Ω	R9 R10	100k Ω 39k Ω	R15 R16	5·6kΩ 1kΩ
R5	82k Ω	R11	100kΩ		
R6	390kΩ 4	R12	120k Ω , 10% type		
Capaci	tors				
C1 C2			250μF 1·5μF		
		M 8			
	r Supply		230V., Sec	19_00\	/ /TSHOP
ırans	former TI		nry's Radio		(10)10)
Resis		1 Wa	tt (see text)	
Capa	citors	C2 50)0μF 30v wk)00μF 25-30	v wka.	
Recti	ner MR1	Brid	ge type I	T120	or LT119
		(H	enry's Radi	0)	
1505 2476	llaneou				
	ne Control	VR1	l0kΩ log.		
	ut socket	40.5	Jack or Ph	опо тур	e.
	on/off swi	tch '	Toggle typ	e	

The layout for the mixer-amplifier circuit is given in Fig. 30.

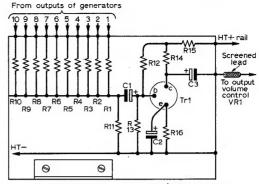


Fig. 30: The component layout of the mixer amplifier.

The Keying Contacts

The modification required to allow the keys to be pressed and instantly released, i.e., the removal of the phosphor bronze clips, was dealt with earlier. The switches attached to these keys are a pair for single pole changeover. Both sets can be used for keys 1 to 9 as shown in Fig. 31, i.e., both pairs are wired to provide a paralleled pair of on-off contacts. The same applies to key No. 10 (sea circuit) except that the rear pair as in Fig. 31b are used as the contacts are normally closed.

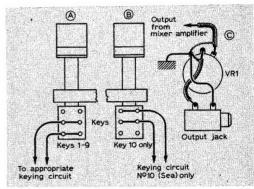


Fig. 31: The wiring of the keying contacts and the level control.

Final Assembly

If the specified case has been used, the final assembly should appear as shown in the photograph which shows the unit as seen from beneath, i.e., with the base panel removed. As explained in part 1 the circuit boards are assembled on what is really the top of the case so that when it is turned over the keys are all at the top as shown. Whatever type of case is used the assembly should follow this pattern, particularly if the unit is to be used with an electronic organ.

Operation

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12 diodes, 2 varistors,
14 diodes, 2 varistors,
15 diodes, 2 varistors,
12 diodes, 2 dio

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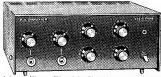
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A. LESTER-RANDS



THE circuit and other technical details of the P.W. oscilloscope were given in part 1. The prototype, as shown in the photographs, was constructed in a Mod-Contil case type Q which has overall dimensions of $13\times9\times7$ in. Any case of similar size could be used but the layout of the components should follow that given as closely as possible. Details for the front panel drilling are given in Fig. 2 and these apply of course to the panel of the Mod-Contil type Q case. The general assembly of the two end panels and the chassis and the

panels and the chassis and the positions of the c.r.t., the component tagboards and mains transformer are shown in Fig. 3. This layout is important even if a different case is used. The transformer TI must be situated below and to the rear of the c.r.t. and as close to the end of the chassis as possible as shown in Fig. 4.

SUB-ASSEMBLIES

These include the main tagboard mounting screen, the panel for the c.r.t. base and the panels for the focus and brilliance controls and the X amplifier gain control. Details for the main tagboard mounting screen are given in Fig. 5 and on this are fitted the miniature tagboards as shown in Fig. 3 with insulating material beneath them to prevent short circuits. The panel and clamp material for the c.r.t. base are shown in Fig. 6 but note the slotted holes in the panel to allow the height of the c.r.t. to be adjusted relative to the front panel. The c.r.t. holder is not mounted on this panel but simply pushed on to the c.r.t. connecting pins.

Details for the focus (VR9) and brilliance (VR8) controls panel are given in Fig. 7b. The panel may be made from perspex or paxolin, 18 in. thick. Both controls are at high potential with respect to chassis and for this reason must not only be mounted on a panel of insulating material but must also be coupled to the front panel control knobs via insulating spindle

couplers as shown in the photo. The remaining panel is that for the X amplifier gain control VR1 as shown in Fig. 7c and which is secured to the side of the chassis as in Fig. 7a. The spindle of this control must be cut very short (to about \(^1_8\mu)\), and slotted as shown as adjustment is made, when required, by screwdriver. To facilitate this a hole is cut in the side panel exactly in line with the control i.e., on the right when facing the front panel.

The three small tagboards E, F and G are located

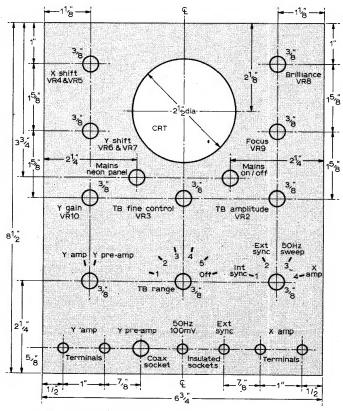
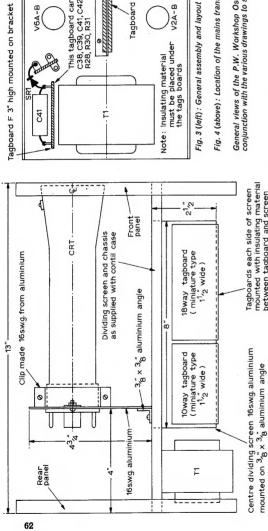


Fig. 2: The drilling of the front panel and location of the controls.



Tagboards each side of screen mounted with insulating material between tagboard and screen

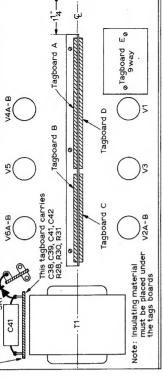
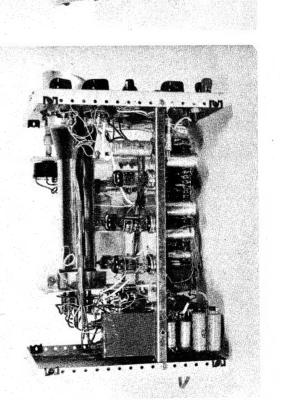


Fig. 3 (left): General assembly and layout using the specified case.

Fig. 4 (above): Location of the mains transformer, the centre screen and the tagboards.

General views of the P.W. Workshop Oscilloscope are shown below and these should be used in conjunction with the various drawings to site the main components.



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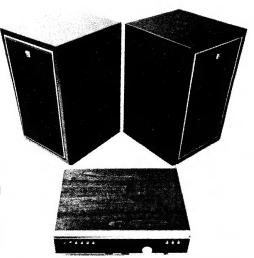
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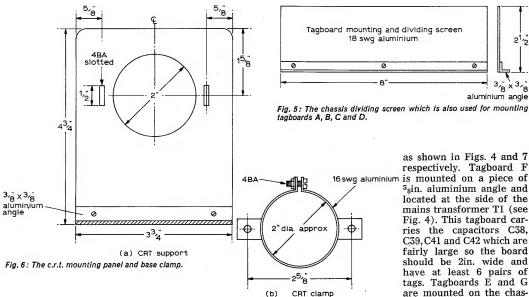
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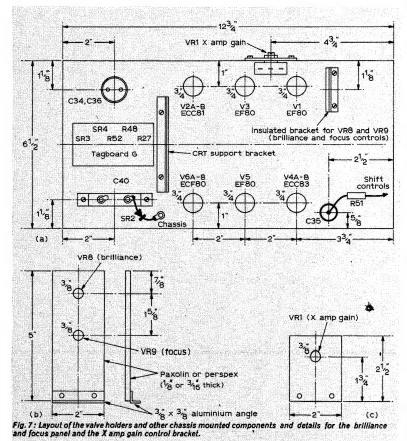
40361			55p	AFI 14			30p
	• • • •	•••	68p	AF115			30p
40362	•••	•••	oop	AF113			28p
2N696	• • • •	***	20p	AF117	• • • •		
2N697		***	22p	AF124	•••		30p
2N706			12p	AF127	• • •		28p
2N930			29p	AF139	***		48p
2N1131			36p	AF239		***	49p
2N1132	•••		40p	ASY26			27p
2N1302			19p	ASY28			27p
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2N1303	•••	•••	130	BC107 BC108			12p
2N1304		• • •	23p 23p	BC100		• • •	14p
2N1305			23P	BC109			
2N1306			33p	BC125		***	15p
2N1307	***		33p	BC126			22p
2N1308			36p	BC147	***		15p
2N1309			36p	BC148			14p
2N1613			23p	BC126 BC147 BC148 BC149			15p
2N1711			26p	BC153			19p
2N1893			54p	BC154			28p
2N2147			95p	BC153 BC154 BC157 BC158 BC159			19p
2N2218	• • • •		34p	BC158			17p
	• • • •		43p	BC I FO			18p
2N2218A		• • • •	38p	BC167			13p
2N2219		•••	30p	BC168	• • • •		lip
2N2219A			53p	BC100		• • • •	13p
2N2270		•••	62p	BC169	* *,*		13P
2N2369A	• • • •		19p	BC177		• • • •	17p
2N2483			35p	BC178			15p
2N2484			42p	BC179			17p
2N2646			54p	BC182L			13p
2N2904A			42p	BC183L			Hp
2N2905			44p	BC184L			13p
2N2905A			47p	BC212L	***		25p
			20p	BC213L			25p
2N2924	•••	• • •	22p	BC214L			25p
2N2925	• • • •	• • • •	lip	BCY70			19p
2N2926		***	27-	BC170	•••		33p
2N3053		***	27p	BCY71 BCY72		***	15p
2N3055	• • •	***	75p	BCY/2	•••		
2N3702			13p	BF115	• • •	***	23p
2N3703			13p	BF167			27p
2N3704			I3p	BF173			31p
2N3705			13p	BF194			17p
2N3706			13p	BF195			18p
2N3707			13p	BFX29			31p
2N3708			I3p	BFX84			25p
2N3709			13p	BFX85		***	34p
			13p	BFX87			29p
2N3710	•••	• • •	13p				26p
2N3711	• • •			BFX88			23p
2N3819			35p	BFY50			20p
2N3904			35p	BFY51			23p
2N3906		***	35p	BFY52 BSX20	***		
2N4058			20p	BSX20			l6p
2N4059			20p	C407			17p
2N4060		• • • •	20p	MC140	• • •		25p
2N4061			20p	MPS6531	• • • •		35p
2N4062			20p	MPS6534	• • • •		30p
2N4124			18p	NKT211			25p
2N4126			27p	NKT212			25p
2N4284			15p	NKT214			23p
2N4286			15p	NKT274			18p
2N4289			15p	NKT403			65p
2N4291	***		I5p	NKT405			79p
			15p	OC71			29p
2N4292	• • •		46p	OC81			25p
AC107	• • • •	• • • •	300			•••	25p
AC126			20p	OCSID	•••		
ACI27			20p	ZTX300	•••		17p
ACI28	•••		20p	ZTX301			12p
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as shown in Figs. 4 and 7 respectively. Tagboard F 16 swg aluminium is mounted on a piece of 38in. aluminium angle and located at the side of the mains transformer T1 (see Fig. 4). This tagboard carries the capacitors C38, C39, C41 and C42 which are fairly large so the board should be 2in. wide and have at least 6 pairs of tags. Tagboards E and G are mounted on the chassis with spacers or insulating material underneath so that the tag eyelets do not touch the chassis. These boards may be miniature (112in. wide), each with 10 pairs of tags. The location of the valveholders and other chassis mounted components such as C34, C35, C36 and C40, etc., are shown in Fig. 7.

21/2

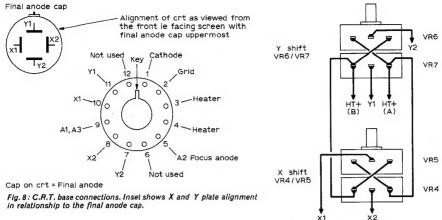
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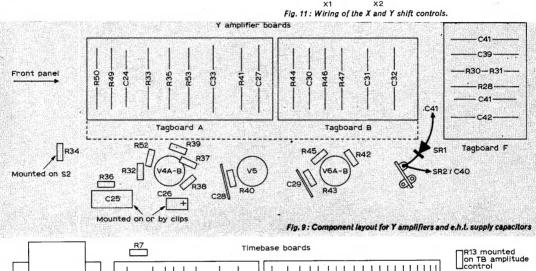
aluminium angle

CONSTRUCTION AND WIRING

These photos show the construction and layout as seen from both sides and above and below the chassis (see also photos in Part 1). The c.r.t. is mounted so that the final anode cap is uppermost as shown in Fig. 8. This will bring the 'key' on the c.r.t. base to the vertical position and ensure that the trace is horizontal when displayed. Fig. 8 also shows the c.r.t. connections. The lead to the final anode cap can be directly soldered to the projecting pin.

The layout for the Y amplifier, the 'timebase and the X amplifier tagboards is shown in Figs. 9 and 10 respectively. The tagboard pairs A and B, and C and D should each be regarded as one long





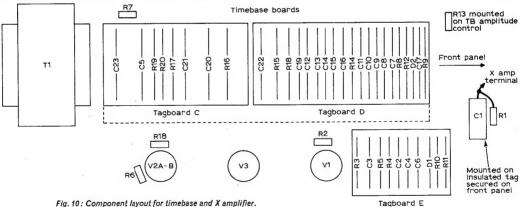


Fig. 10: Component layout for timebase and X amplifier.

board and the components spread out, each accordingly to the space required. For this reason some pairs of tags will not be used but there will be more than enough for all the components. Much the same applies to tagboards E and G. The wiring for the X and Y shift controls is given in Fig. 11. Clockwise movement of the X shift control moves the c.r.t. trace upwards, and clockwise movement of the Y shift control moves the trace to the right and vice versa in both cases.

The only rule as far as wiring is concerned is to keep all wires short as possible and do not take wires



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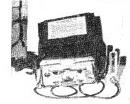
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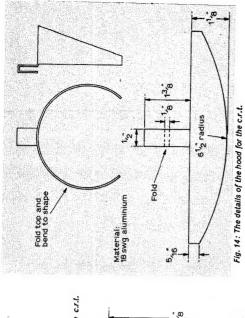
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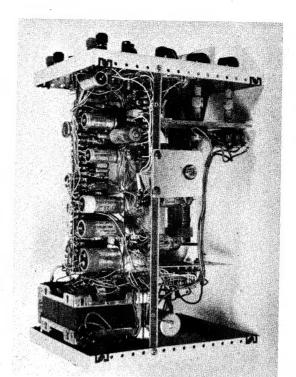
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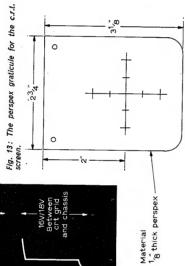
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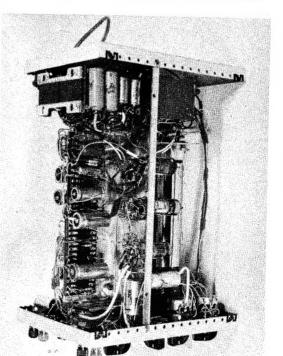
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Two views of the underside of the completed Oscilloscope are shown below.

Fig. 12: Timebase and flyback suppression waveforms. associated with the timebase and its controls too close to the Y amplifier wiring, that is try to keep the timebase and Y amplifier wiring to the respective sides of the centre screen.

TESTING AND PERFORMANCE

It is most important that the various potentials as shown on the circuit are obtained but note that the voltmeter used must be at least 20,000 ohms per volt, otherwise the readings obtained will be inaccurate. The measured potentials should be within 3% of those listed. (Example-for a reading of 600V the measured potential should be not less than 580V and not more than 620V.)

If another oscilloscope is available the timebase waveforms and flyback suppression pulse can be checked quite easily and should appear as in Fig. 12. Failing this, set the timebase range switch to position 1 and the fine control to about midway travel. Set the timebase amplitude control to about one third travel and the X and Y shift controls to midway. Set the Y amplitude control to zero. Adjust brilliance and focus to obtain a bright but sharp trace which should be extended fully across the screen. Check that it remains fully extended on all timebase switch positions. Now turn the timebase switch to the 'off' position in which case only the c.r.t. spot should be displayed and this should be completely round and about 1mm, in diameter. Reduce brilliance a little for this test. Check that the spot can be centred on the c.r.t. screen by means of the X and Y shift controls the setting for these being almost exactly midrange.

With either control it should be possible to move the spot up or down, or from left to right, completely off the screen. With the timebase range switch still at the 'off' position turn the sync switch (S1 AB) to position 3, 50Hz sweep. The trace displayed should be about 1.5cm. long.

The Y amplifiers can be checked next by first setting the timebase range to position 1 and the fine control to approximately half-way. Connect the 100mV 50Hz calibration signal to the 'live' Y amplifier terminal and make sure the Y amplifier switch is to 'Y amp' and not 'Y pre-amp'. With the Y gain control at almost maximum the 50Hz sine-wave displayed should be about 2cm. peak-to-peak and there should be at least 3 or 4 complete cycles. Now switch to 'Y pre-amp' and connect the 50Hz calibration signal to the co-axial Y input and set the Y gain to 1,0th of its travel. The 50Hz sine-wave displayed should again be about 2cm. peak-to-peak. Turn the Y gain a little higher so that the peaks of the test signal extend to the top and bottom of the screen. At this point the sine-wave should show no sign of clipping.

Further tests which include timebase synchronization, and the X amplifier gain etc., require the use of an audio signal generator. For the X amplifier test set the sync switch (S1 AB) to 'X amp' and turn the X amp pre-set gain control fully clockwise. Set the timebase range switch to 'off'. With a sine-wave signal of 1.5V r.m.s. to the X amp input the trace should deflect vertically to approximately 4cm. long.

Return the timebase range switch to position 2 or 3 and then set the sync switch to 'internal sync'. Inject a 1000Hz sine-wave of approximately 500mV to the 'Y amp' input and adjust the Y gain for a 4cm. display. Adjust the timebase fine control until the trace locks. Now run through the rest of the timebase ranges using input signals of appropriate frequency to ensure that each range is functioning and that synchronization can be obtained on each.

The screen graticule on the prototype was made from 18in. thick perspex to the size shown in Fig. 13. The calibration marks were as shown, in centimetres and were produced by scoring the perspex on the side facing the c.r.t. screen. The scored lines and marks were filled with Chinagraph (soft wax pencil). The graticule can be fixed over the screen by two screws at the top which go into the front panel but with spacers on them to keep the graticule just off the tube face.

The c.r.t. hood can be made from 18s.w.g. aluminium as shown in Fig. 14. The tab at the top is folded as shown and this holds the hood on to the top of the graticule. The hood can be pained matt black inside if desired.

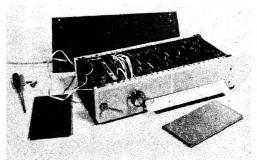
In the main circuit of the oscilloscope on page 1009 of the April issue the secondary of the mains transformer was marked 250-0-250V. This should have read 350-0-350V and is as the components list which gave it correctly.

P.W. SOUND EFFECTS SYNTHESISER

continued from page 58

could be tested separately with a 24V battery supply and the output coupled to an amplifier for aural checks. The output signal level from each generator is over 100mV. This is the best way of ensuring that each circuit is operating properly and producing the right sound and may well save time and trouble when the final assembly stage is reached.

The amplifier and loudspeaker used with the completed synthesiser should be capable of good quality reproduction and have a fairly wide frequency range. The power output will depend on how loud the sounds are to be produced but should be comparable with the power output of the organ. A minimum of 10W



The completed synthesiser with the bottom and side panels removed. The power supply can be seen on the left.

might be suitable for the majority of domestic electronic organs. It may be possible, of course, to couple the unit directly to the organ main amplifier but care should be taken with regard to required signal level and impedance matching.

A little gremlin seems to have been at work regarding the castanets circuit on page 914 of the March issue. C1 and C2 should be 0.2µF and not 0.02µF as given. In the text of the same the section near the middle should read "The waveform from Tr1 and Tr2 is applied to the base circuit of Tr3..." and not "emitter circuit."

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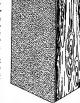
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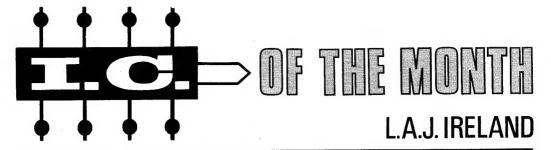
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Number 19

G.E. PA494 Precision Voltage Detector

EFORE going on to consider the technical details of this month's circuit, it would be well to indicate some of the answers to the obvious question as to why the electronics enthusiast should be interested in a new high performance precision voltage detector such as the G.E. type PA 494. It was designed principally for applications requiring the logic function of a Schmitt trigger. In other words, the output of the i.c. would switch states very rapidly once the input threshold voltage had been exceeded. Applications for such a unit are obvious in circuits requiring pulse control, in that a trigger which has lost its shape can produce an accurate square wave output. In radio control of models for instance, this is a valuable feature permitting correction for signal degradation in propagation from the control transmitter to the model receiver. Of more general interest, however, are its uses in such systems as time delays, square wave generators, overvoltage and over-current protection systems, photoelectric controls, etc., some of these applications of the unit being considered in greater detail later on.

Operation

The PA494 itself comes as a four pin device mounted in a T0-5 package. The complete circuit diagram is shown in Fig. 1. Provided the input

(Bottom view)

Fig. 1: Circuit of the PA494 with transistors circled for clarity.

voltage at pin 1 does not exceed the reference voltage set by the resistor pair R1, R2 then Tr2 and Tr4 will be biased on causing Tr7 to saturate and an output current of up to 250 mA may be drawn from pin 3. On the other hand once the reference voltage is exceeded at the input, Tr1 and Tr3 will conduct in addition to Tr5 resulting in positive feedback to the base of Tr2. This reduces the reference voltage and at the same time turns Tr2 off. Consequently the differential amplifier will have changed states and no output current will be available at pin 3 as Tr7 will have been biased off.

Due to the Darlington input configuration of the unit an exceptionally high input impedance is achieved with a mere 100 nanoamps needed to saturate Tr1. This makes the PA494 ideally suited for high impedance sources as a result of the low input current drawn. It combines many of the features of a f.e.t. in a bi-polar device; yet it does not suffer from failure due to static discharge as is sometimes the case with the f.e.t.

Practical Uses

Now let us consider some uses to which we can put the device. Fig. 2 shows a simple bridge configuration using a photoelectric cell or a thermistor

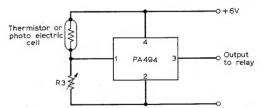
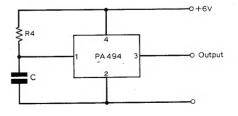


Fig. 2: (above) the PA494 in an alarm or warning system; and Fig. 3 (below), in a timing circuit.



in one arm. The coil of a relay can act as the load for Tr7 thereby providing simple photoelectric control systems or on the other hand if preferred a discrete p.n.p. power transistor may be inserted for direct control of currents up to several amperes.

The PA494 also lends itself to very neat timing circuits of intervals of up to 1 minute, by a simple r.c. network. As can be seen from Fig. 3 a d.c. output is obtained when the threshold voltage is reached in contrast to the unijunction which generates a pulse.

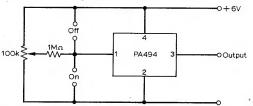


Fig. 4: Another application of the PA494. A switching or shaping circuit.

By biasing Tr1 midway between saturation and cut-off a number of interesting uses may be obtained. The same circuit as shown in Fig. 4 may be utilised as either an on-off touch switch, sine to square wave converter or pulse shaper.

No doubt further uses for the PA494 will spring to mind; a few designs have been given here in the hope that further innovations will be realised on the part of the individual constructor.

U.K. distributors for the PA494 are: — Jermyn Industries Ltd., Vestry Estate, Sevenoaks, Kent.

Caleb Bradley receiving the P.W. Designer's Trophy from Norman Stevens.

TELEVISION

USING THE 'SCOPE

The oscilloscope is an increasingly important servicing tool with the number of colour sets rapidly increasing and a whole range of videocassette devices soon to appear on the market. Yet many enthusiasts and engineers are uncertain about its capabilities and use. Hence this new series by Keith Cummins—starting next month—to clear up exactly what can be done with the oscilloscope and how to do it.

DYNAMIC TV PICTURES

The video circuits in most sets are something of a compromise and do not do full justice to the contrast range of the transmitted picture. Norman McLeod presents a circuit for the experimenter to try which overcomes these defects and provides dynamic TV pictures.

LOGBOOK OF VAN 13

As you might suppose, Van 13 is on the colour run! Harold Peters in this feature provides details of common—and some not so common—faults found in colour receivers.

APRIL ISSUE-OUT NOW

P.W. DESIGNER'S TROPHY

Presented at Film Show

Although the postal strike prevented the despatch of the usual invitation cards, a reasonable number of readers turned out to see the filmshow at the Caxton Hall, Westminster, London, on 5th. March, run as usual by Practical Wireless and Television magazines in conjunction with Mullard Ltd.

The first part of the evening was devoted to the showing of two films, "Now and Then" featuring John Pertwee and "The Electrons Tale", a lighthearted look at the story of the electron.

Following the films, the Editor, Norman Stevens, presented the Practical Wireless "Designer's Trophy 1970" awarded for the most meritorious article submitted for the Project Autumn Competition. The reader was Caleb Bradley and his article "A High Impedance Voltmeter" was featured in the April issue of PW.

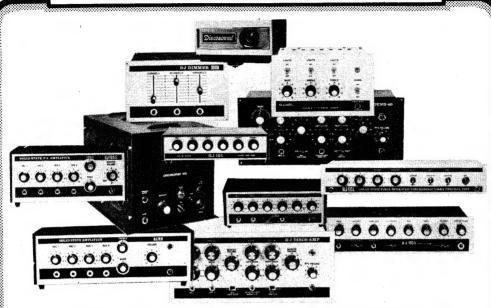
Following refreshments the rest of the evening was given over to a talk by Philip Hunt of Mullards. Entitled "I.C. Story-Continued" it was a continuation of the "Introduction to the I.C." lecture given at last year's Filmshow. This time the theme was the application and servicing problems of I.C.'s.

This year's show was the last to be run in conjunction with Mullard. The company have decided to make cuts in the film and lecture department but Mr. Stevens assured those present that every effort would be made to continue the Filmshows in the years to come.

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	clear			671
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ı			7410N		50p	UIC83 = $5 \times 7483N$ 50p	
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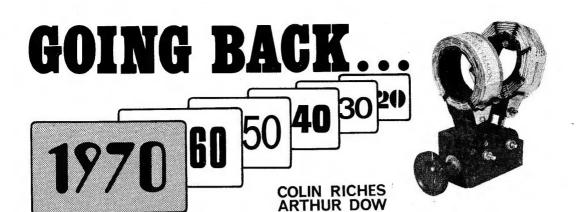
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BP70972709	D.I.L. 1	High OP Amp	58p 45p 40p
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NE reads nowadays of the extremely high power stations that are being used on the very low frequencies for maintaining communication with nuclear submarines even when they are submerged. Megawatts on frequencies at the top end of the audio range are not, unusual.

It was a similar combination of power and long wavelengths that opened up radio communication in the first decade of this century, but it would be invidious to compare the efficiency of those old transmitters and their aerial systems with those in use today.

We recently came across an article, written in 1912, that endeavoured to correlate power, distance and wavelength. At that time it was known that

TABLE 1

	Working Distance		Extreme Distance	
Aerial Current	Day	Night (zero absorption)	Day	Night (zero absorption)
amps. 1 2 3 5 7 10 15 20 25 30 40	miles 75 135 180 235 280 345 420 475 525 665	miles 90 180 270 450 630 900 1,350 1,350 2,250 2,700 3,600	miles 200 300 375 475 550 630 725 790 840 900 970	miles 360 720 1,080 1,800 2,520 3,600 5,400 7,200 9,000 10,800 14,400
50 60	685 725	4,500 5,400	1,025 1,150	18,000 21,600

received signal strengths in the daytime were roughly inversely proportional to distance but the rule only seemed to work up to about 150 to 200 miles after which signal strength dropped off quite rapidly. This was reception by ground wave, as we know it today.

Attempts to formulate some kind of law for signals travelling over a night path came to grief as it was observed that such signals were very irregular in strength and generally stronger than the signals received over the day path. The attenuation of signals was thought to be due to their "absorption" in the upper layers of the atmosphere but assuming no absorption at all the signals over the night path were still stronger than the calculated values.

Apparent changes in the degree of absorption between summer and winter had also been noted and it was thought that the conductivity of the upper atmosphere was increased by the action of the sun's rays.

Table 1 shows the calculated relationship between the aerial current at the transmitter and two ranges, 'working range' and 'extreme distance of audibility'. The first range produced $40\mu A$ in the 'receiver resistance' of 25 ohms and the second range $10\mu A$, corresponding to $1000\mu V$ and $250\mu V$.

These ranges were between two ships each having aerials at 130 feet so presumably the transmitter aerial current was measured in what was the base

TABLE 2

Nautical	λ=	λ=	λ=	λ=
Miles	1,000 m.	2,500 m.	3,750 m.	6,000 m.
1,000 1,250 1,500 1,750 2,000 2,250 2,500 2,750 3,000	amps	amps. 13·5 27 49 95 155 245 470 —	amps. 15 27 44 77 122 314 414 500 775	amps. 17 30 46 74 105 160 235 335 500

of a top loaded vertical over an almost perfect ground plane. The wavelength in use for these experiments was $1000\ metres\ (300kHz)$.

However our mathematician seems to have gone astray by overlooking the impracticability of a 21000-mile night path; perhaps he was already thinking of going into orbit!

At this time, 1912, no one doubted the great advantages of long waves for communicating with distant stations and Table 2 was published to prove the point. This was based on two stations with aerials 450 high and again the distance quoted is working

It seems strange, in this scientific age, that brute

force and long waves are still needed to establish solid communication at a distance regardless of conditions. One would think that an entirely new method of communication would have been dreamed up by now.

Ship Shack 1912

It is somewhat difficult for us, even the old-timers, to realise that in 1912 only the largest passenger ships were fitted with wireless telegraphy apparatus of a sort, that smaller ships, particularly cargo ships, were virtually lost to the rest of the world for weeks or even months on end once they had left our shores.

They did of course make visual signals to other ships and to coast stations en route so that owners had some idea of what was going on. Nevertheless ships, passengers and crews were lost at sea in circumstances where a brief radio call, had it been possible, would have brought other ships hurrying to their aid.



A typical ship's wireless cabin of 1912 fitted with the Marconi "½kW cargo set". The cabinet contains the vertical rotary converter with the disc discharger on top.

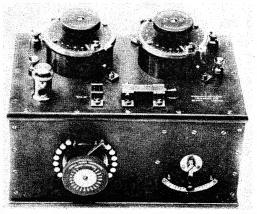
A dock labour dispute in 1911 did a lot to accelerate the equipping of the smaller ships with wireless telegraphy especially as owners realised that this would enable them to re-direct ships at a moment's notice which was particularly important with perishable cargoes. It was left to the Marconi company to produce a wireless installation that was small enough and cheap enough to be suitable for the smaller ships.

Called the "1₂kW cargo set" it could transmit spark signals between 200 and 600 metres wavelength and receive signals between 200 and 1600 metres. The ship's d.c. mains supply energised a rotary converter which gave a 1₂kW of a.c. at "a spark frequency of 300 per second." A disc discharger on top of the converter was adjustable so that the discharge took place at the peak voltage output of the converter.

Tapped inductors were wound with copper strip

on ebonite formers and these in conjunction with capacitors made from glass and zinc plates formed the "oscillation transformer".

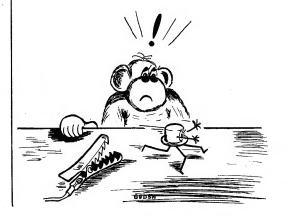
It is interesting to note that the receiver, a "magnetic detector", was permanently connected to the aerial but was shorted out by an auxiliary pair of contacts on the key, "thus enabling the receiving operator to 'break-in' on the transmission in the event of erroneous reception and thus avoid waste of time". Even today very few amateur c.w. stations



A close-up of the "magnetic detector" receiver that can also be seen in the general view of the equipment

have proper "break-in" facilities, although they may have a fast changeover system, but that is not the same thing at all. Those that have true break-in do not use it to its best advantage but it must be admitted that the licence regulations governing the use of call signs does nothing to encourage the use of break-in!

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2N1307 25p 2N1308 30p 2N1309 25p	BC135 30p BC136 35p BC137 40p	BYZ11 35p BYZ12 30p BYZ13 25p	7441 BCD to Decimal Decoder and NIX I 7442 BCD to Decimal Decode (TTL)	£1.00 90p 80p 75p	Mullard II5watt Silicon Power	25 + 30p 100 + 25p 500 + 23p 1000 + 20p
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AD149 50p AD161 37p AD162 87p	BF180 37p BF181 37p BF182 32p	OC77 40p OC81 25p OC82 25p	PL4007 1000 20p 17p 15p 13p 11p	ZENER DIODES ZENER DIODES 3 Watt Plastic 7 Watt Stud	25 + 21p 100 + 17p 500 + 15p 1000 + 13p	OC72 Mullard 25p
AF114 25p AF115 25p	BF184 25p BF185 25p	OC83 25p OC84 25p	3 AMP PLASTIC WIRE ENDED RECTIFIERS Type P.I.V. 1-49 50+ 100+ 500+1000+ PL7001 50 20p 18p 17p 16p 14p	Wire Ends 5% Mounting 5% All voltages 5.1-	0C20 97p	25 + 20p 100 + 17p 500 + 15p 1000 + 13p
AF116 25p AF117 25p AF118 62p	BF194 17p BF195 15p BF196 15p	OC139 25p OC140 37p OC141 62p	PL7002 100 20p 19p 18p 17p 15p PL7003 200 22p 20p 19p 18p 16p	-100 Volts. 30p 100 Volts. 40p each. 25 + 27p 25 + 35p	Mullard 100v	500 + 15p 1000 + 13p
AF124 25p AF125 20p	BF197 15p BF200 37p	OC170 25p OC171 30p	PL7004 400 25p 23p 21p 20p 18p PL7005 600 26p 24p 23p 22p 20p	100 + 25p 100 + 30p 500 + 23p Any one type.	25 + 85p 100 + 80p 500 + 75p	OC83 25p
AF126 17p AF127 17p AF139 30p	BF274 87p BFW87 25p BFW88 23p	OC200 40p OC201 60p OC202 75p	PL7006 800 27p 25p 24p 23p 21p PL7007 1000 30p 28p 26p 24p 22p	1000 + 21p Any one type.	OC44 Mullard 17p	25 + 20p 100 + 17p 500 + 15p
AF178 47p AF179 47p	BFW89 20p BFW90 22p	OC203 40p OC204 40p	MINIATURE POTTED BRIDGE RECTIFIERS (SILICON) SIZE ½ x ½ x ‡ins.	POWER RECTIFIERS	25 + 15p 100 + 13p 500 + 11p	500 + 15p 1000 + 13p
AF180 52p AF181 42p AF186 40p	BFW91 20p BFX13 25p BFX29 30p	OC205 75p OC206 90p	Cur- Type P.I.V. rent 1-49 50+ 100+ 500+ 1902 100 2 amps 60p 55p 50p 45p	SILICON RECTIFIERS STUD MOUNTING 6AMP RANGE P.I.V. 1-49 50+ 100+	500 + 11p 1000 + 10p	OC84 25p
AF239 42p ASY26 25p	BFX30 32p BFX37 32p	OC207 90p OCP71 97p ORP12 50p	2002 200 2 amps 70p 65p 60p 55p 4002 400 2 amps 80p 75p 70p 65p	BYZ10 800 40p 35p 30p BYZ11 600 35p 30p 25p	OCI39 Muliard 25p	25 + 20p 100 + 17p 500 + 15p 1000 + 13p
ASY27 32p ASY28 25p	BFX84 30p BFX85 40p	ORP60 40p ORP61 42p	6002 600 2 amps 90p 80p 75p 70p 1004 100 4 amps 70p 60p 55p 50p	BYZ12 400 30p 25p 20p BYZ13 200 25p 20p 17p	25 + 20p 100 + 17p 500 + 15p	1000 + 13p
ASY29 30p ASY67 47p ASZ21 42p	BFX86 32p BFX87 32p BFX88 30p	Discounts	4004 400 4 amps 80p 75p 70p 65p 6004 600 4 amps 90p 80p 75p 70p	10AMP RECTIFIERS P.I.V. 1-49 50+ 100+ SK103 100 45p 40p 37p	00 + 13p	AF239 42p
BA115 7p BA164 10p	BFY18 30p BFY50 22p	10% 12+ 15% 25+ 20% 100+	1006 100 6 amps 75p 70p 65p 60p 2006 200 6 amps 80p 75p 70p 65p	SK203 200 50p 45p 42p SK403 400 55p 50p 45p	25 + 20p 100 + 17p	25 + 35p 100 + 30p 500 + 25p 1000 + 20p
BAX13 6p BAX16 7p	BFY51 20p BFY52 22p	Any one type Tel. Extn 4.	4006 400 6 amps £1:10 £1:00 90p 80p 6006 600 6 amps £1:25 £1:10 £1:00 90p	SK803 800 75p 70p 65p	500 + 15p	1000 + 20 p
			-CONDUCTOR DEPARTME		UNTS Wet	espectfully ask

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Sinclair Project 60



the world's most advanced high fidelity modules

Sinclair Project 60 presents high fidelity in such a way that it meets every requirement of performance, design, quality and value and now that the remarkable phase lock loop stereo FM tuner is available, it becomes the most versatile of high fidelity systems. With Project 60, it is possible to start with a

The Units to use

Stereo F. M. Tuner

Z.30, PZ.5

modest mono record reproducer and expand it to a sophisticated stereophonic radio and record reproducing system of fantastically good quality to hold its own with any other equipment, no matter how expensive. Project 60 is a unique high fidelity module system where compactness and ease of assembly are combined with

with any other equipment, no matter how expensive. Project 60 is a unique high fidelity module system where compactness and ease of assembly are combined with together with Cost of Units Crystal P.U., 12V battery volume control

Crystal or ceramic P.U. £9.45 volume control etc.

Crystal, ceramic or mag. P.U., most dynamic

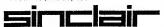
£25.00

c	20+20 W. R.M.S. stereo amplifier for most needs		Crystal, ceramic or mag. P.U., most dynamic speakers, F.M. tuner etc.	£23.90
D	20+20 W. R.M.S. stereo amplifier with high performance spkrs.	2 x Z.30s, Stereo 60, PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner. Tape Deck, etc.	£26.90
E	40+40W. R.M.S. de- luxe stereo amplifier	2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr	As for D	£34.88
F	Outdoor P.A. system	Z.50	Mic., up to 4 P.A. speakers controls, etc.	£5.48
G	Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43
Н	High pass and low pass	A.F.U.	C. D or F	£5.98

C. D or E

circuitry that is far in advance of any other manufacturer in the world. Thus it is extraordinarily easy to assemble any combination of modules using nothing more complicated than the simplest of tools, and you certainly do not have to be experienced to build with complete confidence. The 48 page manual free with Project 60 equipment makes everything easy and you can house your assembly in an existing cabinet, motor plinth, free standing cabinet or virtually any arrangement you wish. Once you have completed your assembly you will have superlatively good equipment to give you years of service and enjoyment. You will have obtained superb value for money because Project 60 is the best selling modular system in Europe and can therefore be produced at extremely competitive prices and with excellent quality control.

Sinclair Radionics Ltd., London Road, St. Ives, Huntingdonshire PE17 4HJ. Tel: St. Ives (048 06) 4311



filters J Radio

System

player

Simple battery

Mains powered record

record player

Sinclair Project 60

Z.30 & Z.50 power amplifiers



The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well.

SPECIFICATIONS (Z50 units are inter-changeable with Z.30s in all applications), Power Outputs
Z.30 15 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M.S. into 8 ohms using 30 volts. Z.50 40 watts R.M.S. into 3 ohms using 40 volts: 30 watts R.M.S. into 3 ohms, using 60 volts. Frequency response: 30 to 300 000 Hz ±1d8. Distortion: 0.02% into 8 ohms. Signal to noise ratio: better than 70d8 un-

Weighted. Input sensitivity: 250mV into 100 Kohms. For speakers from 3 to 15 ohms impedance. Size $3\frac{1}{2} \times 2\frac{1}{4} \times \frac{1}{2}$ in.

Built tested and guaranteed with circuits and instructions manual £4.48

Built, tested and guaranteed with circuits and instructions manual. £5.48

Power Supply Units





Designed specially for use with the Project 60 system of your choice.

Illustration shows PZ.5 to left and PZ.8 (for use with Z.50s) to the right. Use PZ.5 for normal Z.30 assemblies and PZ.6 where a stablised supply is essential.

PZ-5 30 volts unstabilised £4.98 PZ-6 35 volts stabilised £7.98 PZ-8 45 volts stabilised (less mains transformer) £7.98 PZ-8 mains transformer £5.98

Guarantee

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work pe fectly and should anounce is guaranteed to work pe fectify and should any defect sitse in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail. Air-mail charged at cost.

Stereo 60 pre-amp/control unit



Designed for the Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

SPECIFICATIONS

Input sensitivities: Radio-up to 3mV. Mag. p.u. 3mV: correct to R.I.A.A. curve ± 1dB:20 to 25,000 Hz. Ceramic p.u.-up to 3mV: Aux-up to 3mV. Output: 250mV

Signal-to-noise ratio: better than 70dB.

Signal-to-noise ratio: better than 70db.
Channel matching: within 1dB.
Tone controls: TREBLE + 15 to —15dB at 10KHz: BASS + 15 to—15dB at 100Hz.
Front panel: brushed aluminium with black knobs

Size: 81 x 11 x 4 ins.

Ruilt tested and guaranteed.

£9.98

Active Filter Unit



For use between Stereo 60 unit and two Z.30s or Z.50s, and is easily mounted. It is unique in the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. suitable for use with any other ampline system. Two stages of filtering are incorporated – rumble (high pass) and scratch (low pass). Supply voltage – 15 to 35V. Current – 3mA. H.F. cut-off (–3dB) variable from 28kHz to 5kHz. LF. cut-off (–3dB) variable from 25kHz to 100Hz. Distortion at 1kHz (35V. supply) 0.02% at rated output.

Built, tested and guaranteed

£5.98

Stereo FM Tuner



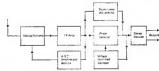
phase lock loop principle
Before production of this tuner, the phase lock
loop principle was used for receiving signals
from space craft because of its vastly improved signal to noise ratio over other systems. Now, for the first time, the principle has been applied to an FM tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch specially designed stereo decoder and squelch circuit for silent tuning between stations. Sensitivity is such that good reception becomes possible in difficult areas. Foreign stations can be tunad in suitable conditions and often a few inches of wire are enough for an aerial. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system.

SPECIFICATIONS:

Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108 MHz Capture ratio: 1.5dB Sensitivity: 2µV for 30dB quieting: 7µV for full Sensitivity: ∠µν του σωσε με mining.
Squelch level: 20μV.
A.F.C. range: ±200 KHz
Signal to noise ratio: ⊃65dB
Audio frequency response: 10Hz—15KHz^b

Audio frequency response: 1UHz—IDKΠz-(±1dB)

Total harmonic distortion: 0.15% for 30% modulation
Stereo decoder operating level: 2μV
Pilot tone suppression: 30dB
Cross talk: 40dB
I.F. frequency: 10.7 MHz
Output voltage: 2 x 150mV R.M.S.
Aerial Impedance: 75 Ohms
Indicators: Mains on: Stereo on; tuning indicator Operating voltage: 2.25-30 VDC Operating voltage: 25-30 VDC Size: 3.6 x 1.6 x 8.15 inches: 91.5 x 40 x 207 mm



Price: £25 built and tested. Post free

To: SINCLAIR RADIONICS LTD LONDON RO	AD ST. IVES HUNTINGDONSHIRE PE17 4HJ
Please send	Name
	Address
for which I enclose cash/cheque/money order.	

Sinclair IC10/Q16/Micromatic



The world's most advanced high fidelity amplifier

This is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself is a chip of silicon only a twentieth of an inch square by one hundredth of an inch thick, having 5 watts RMS output (10 watts peak). It contains 13 transistors (including two power types), 2 diodes, 1 zener diode and 18 resistors, and is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins This exciting device is more rugged and has considerable performance advantages, including complete freedom from runaway and a very low level of distortion. The IC10 is primarily intended as a full performance high fidelity power and preamplifier, for which application it only requires the addition of such components as tone and volume controls and a battery or mains power supply. It may also be used in other applications including car radios, electronic organs, servo amplifiers (it is do coupled throughout) etc.

Circuit Description

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of temperature. There is generous negative feedback round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory. Each IC10 is sold with a comprehensive

manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include oscillators, etc. The pre-amp section can be used as an RF or IF, amplifier without any additional transistors.

Specifications

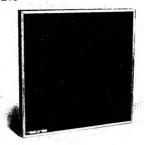
Output: 10 watts peak, 5 watts RMS continuous. Frequency response: 5Hz to 100kHz 1± dB. Total harmonic distortion: Less than 1% at full

output. Load impedance: 3 to 15 ohms. Power gain: 110 dB (100,000,000,000 times)

total.

Supply voltage: 8 to 18 volts. (A Sinclair power unit, PZ,7 is available for mains operation).

Size: 1 x 0.4 x 0.2 in, plus heat sink and tags. Sensitivity 5 mV. Input impedance: Adjustable externally up to 2.5 Mohms.



High fidelity loudspeaker

The Q16 employs the well proven acoustic principles specially developed by Sinclair in which a special driver assembly is meticulously matched to the characteristics of the uniquely designed cabinet. In reviewing this exclusive Sinclair design, technical journals have justly compared the Q16 with much more expensive loudspeakers. Its shape enables the Q16 to be positioned and matched to its environment to much better effect than is the case with conventionally styled enclosures. A solid teak surround with a special all-over cellular foam front is used as much for appearance as its ability to pass all audio frequencies

elegantly designed shelf mounting speaker brings genuine high fidelity within reach of every music lover.

Specifications:
Construction: Special sealed seamless sound or Construction: Special sealines seamless sound of pressure chamber with internal baffle.

Loading: up to 14 watts TMS.
Input impedance: 8 ohms.
Frequency response: From 60 to 16,000 Hz.
confirmed by independently plotted B and K curve.

confirmed by independently plotted B and K curve. Driver unit: Special high compliance unit having massive ceramic magnet of 11,000 gauss, aluminium speech coil and a special cone suspension for excellent transient response. Size and styling: 9½ in square on face x4½ in, deep with neat pedestal base, Black all-over cellular foam

front with natural solid teak surround

Micromatic



Britain's smallest radio

Considerably smaller than an ordinary box of matches, this is a multi-stage AM receiver brilliantly designed to provide remarkable unificative designed to provide remarkable standards of selectivity, power and quality for its size. Powerful AGC counteracts fading from distant stations; bandspread at higher frequencies makes reception of Radio 1 easy. plug-in magnetic earpiece provided ches the Micromatic's output to give wonderful standards of reproduction. Every-thing including the special ferrite rod aerial and batteries is contained within the minute and attractively designed case. Whether you build a Micromatic kit or buy this amazing receiver ready built and tested, you will find it as easy to take with you as your wrist watch, and dependable under the severest listening conditions.

Specifications: Size: $36 \times 33 \times 13$ mm ($1^4/5 \times 1^3/10 \times \frac{1}{2}$ in.) Weight: including batteries, 28.4 gm (1 oz.). Case: Black plastic with anodised aluminium front Case: Jacks pleast with a motivate administration panel and spun aluminium dial.

Tuning: medium wave band higher frequencies. (550 to 1,800 Hz).

Earpiece: Magnetic type.

On/off switching: By inserting, and withdrawing

earpiece plug.

Kit in pack with earpiece, case, instructions and solder £2.48.

Ready built, tested and guaranteed, with earpiece

Two Mallory Mercury batteries type RM675 required From radio shops, chemists, etc.

Price (with manual): £2.98 post free.	
To: SINCLAIR RADIONICS LTD LONDON RO	AD ST. IVES HUNTINGDONSHIRE PE17 4HJ
Please send	Name
	Address
for which I enclose cash/cheque/money order.	PWari

Sinclair Radionics Ltd., London Road, . St. Ives, Huntingdonshire PE17 4HJ. Tel: St. Ives (048 06) 4311



Fully guaranteed	TRANSIS	TORS, ZENE	R DIODES etc.	COLOMOR ALL valves
Individually packed	SPECIAL OC25	37p OC200 37p 2N3054	95p AD149 55p BYZ13 20p	quaranteed
VALVES	OFFER OC26 O9J tube OC28	25p OC201 47p 2N3055 62p OC206 50p 2N3730£	75p AD161 35p BYZ16 62p 1.25p AD162 35p CRS1/10 25p	5Y4G 35p 12K8GT 87p 5933 £1.12p
VALVES	£1.75 OC29	62p IN21 17p 2N3731£	1.25p AF118 32p CRS1/20 37p	5Y3GT 35p 12Q7GT 27p 6057 50p
B12H £1.75p ECH200 62p OA2 35p		50p IN21B 25p 2N5109£ 42p IN25 60p 40362	67p AF139 37p CRS1/35 42p	5Z4 70p 12SG7 35p 6060 37p 5Z4GT 60p 14S7 75p 6064 35p
CY31 35p ECL80 45p OB2 35p DAF96 38p ECL82 32p PABC80 37p	1 OA70 100 OC44	20p IN43 10p S2303	50p AF178 47p CRS1/40 47p	5Z4GT 60p 1487 75p 6064 35p 6AB7 20p 19AQ5 38p 6065 65p
DF96 37p ECL83 65p PC97 40r		12p IN70 7p 3F100 12p IN702-72586p 3FR5	67p AF186 45p CRS3/05 80p 32p AFY19£1-12p CRS3/20 37p	6AC7 15p 19G3 £3.50p 6080 £1.37p
DK96 41p ECL86 40p PC900 47p DL92 32p EF36 17p PCC84 37p	OA74 10p OC71	15p IN746A 3N128	87p ASY26 27p CRS3/30 42p	6AH6 57p 19G6 £1.00p 6146 £1.40p 6AK5 25p 19H4 £4.50p 8020 £1.75p
DL94 40p EF37A 45p PCC89 45p	0.491 75 0072	25p series 26p 3N139 £ 30p IN821A £1.05 3N140	1.75p ASY28 27p CRS25/025 95p ASY67 47p 75p	6AK8 32p 20P4 87p 9001 15p
DL96 41p EF39 40p PCC189 55p	OA91 6p OC75	22p IN823A £1.30 3N154	90p BAW19 27p CRS3/40 50p	6AL5 10p 25L6GT 36p 9002 22p 6AL5W 35p 30C15 75p 9003 50p
DM70 30p EF40 50p PCE800 75p DY86 45p EF41 62p PCF80 30p	OA200 8p OC76	25p IZMT5 35p 3N159 £	1.45p BC107 15p GET103 20p	6AL5W 35p 30C15 75p 9003 50p 6AM6 15p 30C17 80p 9004 12p
DY87 55p EF80 25p PCF82 33p		25p IZMT10 33p 6FR5 20p IZT5 67p 12FR60	45p BCf08 1op GET115 45p 73p BC113 30p GET116 50p	6AN8 50p 30C18 75p 9006 12p
DY802 48p EF83 47p PCF84 48p E88CC/01 EF85 32p PCF86 57p	OA211 37p QC81DM	1 20p IZT10 63p 10D1	16p BC118 37p GEX66 75p	6AQ5 30p 30F5 83p C.R. Tubes 6SC7GT 25p 30FL1 75p VCR97
£1.35p EF86 31p PCF200 77p	OAZZOU SON OCCOZ	25p 2G385 51p 40594 £ 1 15p 2G403 15p 40595 £	1.37p BCY72 37p NKT222 20p 1.37p BF115 25p NKT304 35p	6SG7 30p 30FL12 92p £4.50p
E180CC 45p EF89 26p PCF201 771	OAZ202 to OC83	22p IN4785 55p 40636 £	1.45p BF173 30p SD91S 26p	68J7 87p 30FL13 46p VCR517B 68J7GT 32p 30FL14 77p #3.50p
E181CC 45p EF91 15p PCF801 48p E182CC EF92 37p PCF802 48p	UAZZUO AZP UCOSB	15p 2N277 50p 40668 #	1.35p BF187 50p SD928 31p	68K7 35p 30L15 85p VCR517C
£1-15 EF95 25p PCF805 72p	OAZ207 47p OC84 OAZ208 to OC122	25p 2N918 37p 40669 £ 50p 2N1304 25p AC126	1.45p BFY51 22p SD93S 32p 21p BFY52 22p SD94 21p	68L7GT 82p 30L17 80p 47.50p 68N7GT 85p 30P12 80p 5FP7 41.32p
EABC80 32p EF183 32p PCF806 65p EAF42 50p EF184 35p PCF808 72p	OAZ213 32p OC139	25p 2N1306 25p AC127	21p BSO5 37p SD98S 46p	68N7GT 35p 30P12 80p 5FF7 £1.32p 68Q7 38p 30P19 70p 88D £9.00p
EB91 10p EFL200 77p PCH200 70p	042225 to 00140	37p 2N1307 25p AC128 25p 2N2147 75p AC176	20p BS 45p V405A 38p 25p BS2 46p CRS3/30 42p	6SQ7GT 38p 30PL1 65p 88J #9-00p
EBC33 50p EL34 52p PCL81 47p EBC41 52p EL41 57p PCL82 87p	OC16 42p OC171	30p 2N2904A 37p ACY17	25p BSY29 17p CRS25/025	6V6G 17p 30PL13 90p 88L £9.00p 6V6GT 31p 30PL14 85p Photo Tubes
ECC81 20p EL42 52p PCL83 65p	OC22 42p OC172	37p 2N3053 25p ACY28	20p BU100 £1 80p 75p	6X4 23p 35L6GT 47p CMG25
EBF80 37p EL84 23p PCL84 42p		22p 6CH6 55p UL41	60p 6J7M 40p 184 25p	6X5G 25p 35W4 25p £1.25p
EBF83 30p EL85 36p PCL85 42p EBF89 30p EL86 40p PCL86 42p	£5.25p 6AU6 R17 40p 6AX4	25p U801 £1 UL84 40p UABC80 85p UU5	80p 5K6GT 40p 185 22p 85p 6K7 32p IT4 15p	6X5GT 27p 35Z4GT 45p 931A 23·12p 6Y6G 55p 42 35p 6097C
ECC81 20p EL90 80p PFL200 57p	R19 37p 6AX5GT	65p UAF42 52p UY41	42p 6K7G 10p 1X2A 37p	6-30L2 70p 50C5 35p £17-50p
ECC82 28p EL95 35p PL36 53p ECC83 27p EL500 85p PL81 50p	STV280/40 6B7	27p UBC41 47p UY85	28p 6K8GT 36p 1X2B 37p	6Z4 25p 50CD6G30 Special Vivs 7B7 35p £1.50p CV1031
ECC84 20p EM31 25p PL82 4up		40p UBF80 35p 6CL6 22p UBF89 35p 6D6	48p 6K25 70p 3A4 20p 15p 6SA7 35p 3D6 15p	7C5 72n 50EH5 60n £5.00p
ECC85 60p EM80 40p PL83 42p	£9.00p 6BE6	25p UCC85 40p 6EA8	55p 68A7GT 32p 3Q4 37p	7C6 30p 75 27p CV2339
ECC86 37p EM84 35p PL84 35p ECC88 35p EM87 55p PL500 73p		55p UCF80 50p 6F23 42p UCH42 62p 6F33	75p VR105/30 30 384 33p £1 VR150/30 30p 3V4 40p	7H7 27p 76 30p £20-00p 7Y4 60p 78 25p JP9/7D
ECC189 48p EY51 40p PL504 68p	U26 72p 6BQ7A	33p UCH81 30p 6H6M	15p Z759 \$1.75p 5B254M £1.80	9D6 37p 80 45p £37-50p
ECF80 32p EY86 35p PY33 60p ECF82 32p EY81 35p PY80 35p		80p UCL82 35p 6J4WA 80p UCL83 60p 6J5	70p Z801U £1.25p 5B/255M 35p Z803A £1.25p £1.75	11E2 £1.50p 803 £8.00p K301 £5.00p 12AT6 22p 805 £8.00p K305 £12.00p
ECF83 77p EY88 40p PY81 27p		80p UCL83 60p 6J5 65p UF41 50p 6J5GT	35p Z803A £1.25p £1.75 25p Z900T 60p 5R4GY 52p	12AT7 20p 807 45p K308 £16.00p
ECF801 62p EZ41 42p PY82 27p ECF802 62p EZ80 25p PY83 35p	6AS6 30p 6C4	28p UF80 36p 6J6	17p IL4 12p 5U4G 27p	12AU7 28p 813 £3.75p K337 £12.00 p 12AV6 27p 832A £2.75p
ECF802 62p EZ80 25p PY83 35p ECH35 60p EZ81 27p PY88 37p		20p UF89 33p 6J7G	25p IR5 30p 5V4G 37p	12AV6 27p 832A \$2.75p 12AX7 27p 866A 75p
ECH42 65p GZ34 52p PY800 52p	P & P un to Son Sp. to	El 10n: over £1 10n in £1. over	Tubes and Special Valves. U.K. er £3 post free, C.O.D. 20p extra.	12BA6 30p 954 22p
ECH81 28p KT66 21-60p PY801 52p ECH83 42p KT88 21-75p QQVO3-10		GRATED CIRCUITS-MANY		12BE6 30p 955 20p 12BH7 17p 956 10p
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THE FULL-FI STEREO SIX
The amplifier
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UNREFEATABLE PRICE is \$9 plus 38 post and insurance.

STANDARD WAFER SWITCHES

all brown	Standard Size 11 wafer—silver-plated 5 amp								
			dard		11 wa	iter—si	iver-pi	ated :	
42.5					₹″ spir	ndie 2"	. long-	-with .	ocking
3633			her and	i nut.					
No. of	2	3	4	5	6	8	9	10	12
Poles	way	way	way	way	way	way	way	way	way
1 pole	33p	33p	33p	33p	33p	33p	33p	33р	33p
2 poles	33p	33p	33p	83p	33p	33p	33p	55p	55p
3 poles	33р	33p	33p	33p	55p	55p	55p	75p	75p
4 poles	33p	33p	33p	55p	55p	55p	55p	95p	95p
5 poles	33p	33p	55p	55p	750	75p	750	£1.15	£1.15
6 poles	33p	55p	55p	55p	75p	75p	75p	£1.35	£1.35
7 poles	55p	55p	55p	75p	95p	95p	95p	£1.55	£1.55
8 poles	55p	55p	55p	75p	95p	95p	95p	£1.75	£1.75
9 poles	55p	55p	75p	75p	£1.15	£1.15	£1.15	£1.95	£1.95
10 poles	55p	55p	75p	95p	£1.15	£1.15	£1.15	£2·15	£2·15
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1 than usual speaker giving
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Zim. diameter, 5im. long. Frice 90p plus 23p,
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BLANKET SIMMERSIAI
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Glass encased, switches operated by external
magnet—gold welded contacts. We can now offer
3 types:

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This is a drum type timing device, the forum being calibrated in equal divisions for switch setting purposes with trips which are infinitely adjustable for position. They are also arranged to allow 2 operations per switch per rotation. There are 15 changeover micro switches each of 10 amp type operated by the trips thus 10 servations per type operated by the trips thus 10 servations of the many uses of this timer are Machinery control, Boiler firing, Dispensing and Vending machines, Display lighting animated and signs, Signalling, etc. Price from makers probably over £10 each. Special snip price £5.75 plus 25p post and insurance. Don't miss this terrific bargain.

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CONTROLLER
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R.M.S	95.00	75 - 00
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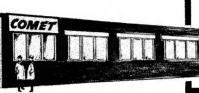
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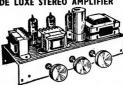
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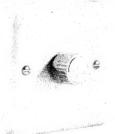
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2D21 3A4	0.35 6BQ5 0.25 0.35 6BR8 0.65	6K7 0.35 6K8G 0.35 6K25 0.75	12AV6 0.38 12AV7 0.50	30F5 0.85 30FL1 0.70	90C1 0.60 90CV 1.25	DY86 0.33 DY87 0.35	ECC91 0.20	EL42 0.5 EL81 0.5	PC88 0.60 PC97 0.50	PL801 0.80 PM84 0.50	UBL21 0.60 UC92 0.35
3BP1 3Q4	2.75 6BW6 0.85 0.40 6BW7 0.70	6L6GT 0.45 6L7 0.40	12AX7 0.30 12AY7 0.70 12B44 A0,55	30FL12 0.93 30FL14 0.75 30L1 0.40	807 0.50 812A 3.50 813 3.75	DY802 0.50 E88CC 0.65 E130L 5.00	ECC189 0.60 ECF80 0.35 ECF82 0.35	EL83 0.43 EL84 0.23 EL85 0.43	PCC84 0,40	PY31 0.80 PY33 0.63 PY80 0.85	UCC85 0.40 UCF80 0.55 UCH21 0.60
3S4 3V4 5R4GY	0.35 6BX6 0.25 0.45 6BZ6 0.35 0.60 6C4 0.33	6L18 0.45 6LD20 0.40 6N7GT 0.40	12BA6 0.35 12BA7 0.35 12BE6 0.35	30L15 0.85 30L17 0.80 30P12 0.80	866A 0.75 5642 0.65 6080 1.50	E180F 0.95 EABC80 0.35	ECF86 0.65 ECF8041.50 ECH42 0.70	EL86 0.40 EL90 0.30 EL95 0.30	PCC89 0.50	PY81 0.30 PY82 0.30 PY83 0.38	UCH42 0.70 UCH43 0.75 UCH81 0.35
5U4G (5U4GB (0.33 6C5GT 0.40 0.42 6CA4 0.28	6P1 0.60 6P28 0.65	12BH7 0.40 12BY7 0.55	30P19 0.80 30PL1 0.70	6146 1.50 6146B 2.50	EAF42 0.55 EBC33 0.50	ECH81 0.30 ECH83 0.40	EL360 1.1 EL803 1.0	PCC805 0.85 PCC806 0.80	PY88 0.40 PY500 1.00	UCL81 0.60 UCL82 0.35
5Y3GT (0.42 6CA7 0.50 0.32 6CB6 0.30 0.50 6CD6GA1.15	6Q7 0.40 6SA7 0.40 6SG7 0.35	12K5 0.55 12K7GT0.35 12Q7G 0.30	30PL13 0.93 30PL14 0.90 35A3 0.55	6360 1.25 6939 2.15 7199 0.75	EBC41 0.55 EBC81 0.30 EBF80 0.40	ECH84 0.45 ECL80 0.40 ECL81 0.45	EL821 0.5 EL822 0.9 ELL80 0.7	PCF82 0.35	PY800 0.50 PY801 0.50 PZ30 0.35	UCL83 0.60 UF41 0.60 UF42 0.60
5Z4G 0 6/30L2 0	0.40 6CG7 0.50 0.75 6CH6 0.55	6SK7 0.35 6SL7GT0.35	128R7 0.35 1487 0.80	35A5 0.75 35B5 0.65	7360 1.80 7586 1.25	EBF83 0.40 EBF89 0.30	ECL82 0.35 ECL83 0.65	EM34 0.90 EM71 0.74	PCF86 0.60 PCF87 0.85	QQV2-6 2.15 QQV03-10	UF43 0.60 UF80 0.35
6AF4A (0.35 6CL6 0.50 0.50 6CW4 0.63 0.40 6CY5 0.43	68N7GT0.35 68Q7 0.40 68R7 0.40	20D1 0.45 20L1 1.10 20P1 0.50	35C5 0.40 35D5 0.70 35L6GT 0.50	7895 1.25 9002 0.35 9003 0.50	EC53 0.50 EC86 0.60 EC88 0.60	ECL84 0.55 ECL85 0.55 ECL86 0.40	EM80 0.40 EM81 0.60 EM84 0.30	PCF802 0.50	QQV03-20A 5.25	UF85 0.40 UF89 0.35 UL41 0.65
6AJ8 (0.50 6CY7 0.65 0.30 6D3 0.45 0.30 6DC6 0.75	6T8 0.35 6U4GT 0.60 6U8A 0.40	20P4 1.10 20P5 1.20 25C5 0.50	35W4 0.30 35Z3 0.60 35Z4G 0.30	AZ1 0.48 AZ31 0.55 CBL1 0.80	EC90 0.33 EC91 0.50 EC92 0.35	ECLL800 1.50	EM85 1.00 EM87 0.56 EN91 0.36	PCF808 0.75	TT21 2.65 TT22 2.80	UL84 0.30 UM84 0.20 UY1N 0.50
6AK6 C	0.57 6DK6 0.48 0.48 6DQ6B 0.68	6X4 0.30 6X5GT 0.35	25L6GT 0.45 25Z4G 0.30	35Z5GT 0.40 50A5 0.70	CBL31 0.90 CY31 0.35	EC93 0.50 EC8010 2.25	EF37A 0.60 EF39 0.40 EF40 0.50	EY51 0.40 EY80 0.40	PCL81 0.50 PCL82 0.35	U18/20 0.75 U25 0.75 U26 0.75	UY11 0.65 UY41 0.45
6AM5 C	0.20 6DS4 0.75 0.32 6EA8 0.58 0.33 6EH7 0.30	6X8 0.55 6Y6G 0.65 7Y4 0.60	25Z6GT 0.65 30A5 0.45 30AE3 0.40	50B5 0.45 50C5 0.40 50CD6G1.65	DAF96 0.42 DF96 0.42 DK40 0.55	ECC40 0.60 ECC81 0.33 ECC82 0.30	EF41 0.65 EF42 0.70 EF80 0.25	EY81 0.40 EY83 0.50 EY86 0.40	PCL84 0.45	U31 0.45 U37 1.50 U52 0.33	UY82 0.50 UY85 0.30 W729 0.60
	0.35 6EJ7 0.35	9BW6 0.50	30C1 0.30	50L6GT 0.50	DK92 0.50	ECC83 0.30	EF83 0.55	EY87 0.4		U76 0.30	Z803U 0.90

TRANSISTORS

NAME						
2N4444	ONT404	0.15	1 09094	1 00	PCIES	0.15
2N866 0.50 28104 0.50 BCY30 3.8 2N867 22.8 28701 0.50 BCY33 0.25 2N968 0.40 28702 0.50 BCY34 0.25 2N709 0.70 28746 0.35 BCY72 0.20 2N709 0.10 AC125 0.13 BCY72 0.20 2N709 0.20 AC125 0.25 BD113 0.65 2N793 0.35 AC125 0.29 BP115 0.20 2N890 0.35 AC126 0.35 BF173 0.35 2N891 0.35 AC132 0.35 BF173 0.35 2N131 0.40 AC146 0.15 BF184 0.35 2N132 0.40 AC167 0.35 BF184 0.35 2N1302 0.25 AC167 0.36 BF184 0.35 2N1302 0.25 AC167 0.35 BF184 0.35 2N1307				0.40	BC175	0.10
2N987 0.32 28701 0.50 BCY33 0.30		0.20				0.25
2NO98 0.40 28702 0.50 BCY34 0.80 2N706 0.70 28746 0.30 BCY72 0.20 2N706 0.15 ACI13 0.15 BCX11 0.80 2N706 0.21 ACI23 0.80 BD113 0.80 2N930 0.30 ACI22 0.90 BP115 0.20 2N937 0.35 ACI23 0.35 BF177 0.35 2N937 0.35 ACI32 0.35 BF177 0.25 2N1131 0.40 ACI46 0.15 BF181 0.25 2N1132 0.45 ACI36 0.23 BF187 0.25 2N1302 0.25 ACI37 0.01 BF184 0.25 2N1302 0.25 ACI37 0.01 BF184 0.25 2N1303 0.25 ACI37 0.01 BF194 0.20 2N1303 0.25 ACI37 0.03 BF196 0.20 2N1303						
2N766 0.76		0.20				0.20
2N708						
2N708				0.15		
2N753 0.25 AC126 0.26 BD123 0.26 2N929 0.30 AC127 0.20 BF155 0.20 2N939 0.36 AC126 0.20 BF155 0.20 2N939 0.36 AC126 0.20 BF155 0.20 2N939 0.36 AC126 0.20 BF156 0.20 AC126 0.20 BF157 0.20 AC126 0.20 BF157 0.20 AC126 0.20 BF157 0.20 AC126 0.20 BF158 0.20 AC126 0.20 BF159 0.20 AC126 0.20		0.20				
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2 N9390 0.85 AC132 0.38 BF167 0.30 SF167 0.3		0.30		0.20	BF115	
2NP397	2N930	0.35			BF167	0.25
2 N1131		0.35	AC153	0.25		0.30
2N11914 1.25			AC154	0.15		0.25
2N1301		0.45				0.25
2N1304 0.25 AC176 0.25 BF195 0.20 2N1304 0.25 AC187 0.30 BF196 0.20 2N1306 0.35 AC187 0.30 BF197 0.20 2N1306 0.35 AC187 0.30 BF197 0.20 2N1307 0.35 AC790 0.20 BFW89 0.25 2N1308 0.40 ACV19 0.25 BFW89 0.20 2N1307 0.35 AC790 0.20 BFW89 0.20 2N1313 0.25 ACV21 0.20 BFX88 0.25 2N1711 0.30 ACY22 0.20 BFX88 0.25 2N1711 0.37 AD140 0.36 BFY97 0.40 2N1717 0.75 AD140 0.36 BFY97 0.40 2N1717 0.75 AD140 0.36 BFY97 0.40 2N1717 0.75 AD140 0.38 BFY91 0.20 2N2127 0.30 AP128 0.38 BFY91 0.20 2N2129 0.40 AF114 0.25 BFY36 0.25 2N2128 0.40 AF114 0.25 BFY36 0.25 2N21314 0.30 AF113 0.25 BFX68 0.35 2N2137 0.50 AF116 0.25 BFX68 0.30 2N2137 0.50 AF116 0.25 BFX68 0.30 2N2131 0.50 AF117 0.25 BFX68 0.30 2N2132 0.50 AF116 0.30 BFX68 0.30 2N21334 0.50 AF128 0.35 CC24 0.50 2N21334 0.50 AF128 0.55 CC25 0.60 2N21334 0.50 AF128 0.50 CC24 0.50 2N2134 0.50 AF128 0.50 CC25 0.60 2N21334 0.50 AF128 0.50 CC24 0.50 2N2134 0.50 AF128 0.50 CC26 0.50 2N2134 0.50 AF12			AC157	0.20		0.20
2N1360 0.25 AC187 0.30 BF1967 0.20 2N1360 0.25 AC188 0.30 BF1967 0.20 2N1360 0.25 AC188 0.30 BF1967 0.20 2N1360 0.25 AC188 0.30 BFW87 0.20 2N1360 0.25 AC188 0.20 BFW88 0.25 2N1360 0.25 AC781 0.20 BFW88 0.25 2N1360 0.25 AC781 0.20 BFW88 0.25 2N1361 0.25 AC7821 0.20 BFW88 0.25 2N1613 0.25 AC7821 0.20 BFW88 0.25 2N1613 0.25 AC7821 0.20 BFW88 0.25 2N1761 0.75 AD140 0.80 BFY19 0.60 2N2147 0.75 AD140 0.80 BFY19 0.60 2N2147 0.75 AD140 0.55 BFY50 0.20 2N2147 0.75 AD140 0.55 BFY50 0.20 2N2160 0.4 AD142 0.35 BFY50 0.20 2N2180 0.4 AD142 0.35 BFY50 0.20 2N22180 0.5 AP115 0.25 OC16 0.75 2N2223 0.15 AP118 0.45 BFY50 0.20 2N2360 0.50 AF125 0.25 OC16 0.75 2N2223 0.15 AF180 0.35 OC25 0.40 2N2363 0.30 AF125 0.25 OC16 0.75 2N2363 0.30 AF125 0.25 OC16 0.75 2N2363 0.30 AF125 0.25 OC16 0.75 2N2383 0.35 AF211 0.35 OC25 0.30 2N2383 0.35 AF211 0.35 OC25 0.30 2N2383 0.35 AF211 0.35 OC25 0.30 2N2383 0.36 AF211 0.55 OC36 0.30 2N2383 0.36 AF211 0.55 OC37 0.20 2N23840 0.36 AF210 0.55			AC169	0.10	BF194	
2N1306 0.25 AC188 0.30 BF197 0.30 C.30 L.30 C.30 L.30 C.30 C.30 C.30 C.30 C.30 C.30 C.30 C	2N1302	0.20	AC176	0.25	DF199	0.19
2N1366 0.25 ACV17 0.30 BFW87 0.30		0.25		0.80		0.20
2N1307 0.30						0.20
2N1308 0.40 ACV19 0.20 BFW99 0.20 2N1303 0.35 ACV29 0.20 BFW89 0.20 2N1313 0.25 ACV29 0.20 BFX88 0.20 2N1311 0.35 ACV29 0.20 BFX88 0.20 2N241 0.35 ACV29 0.35 BFY77 0.40 2N241 0.35 BFY30 0.20 2N2417 0.30 AP114 0.50 BFY30 0.20 2N2417 0.30 AP115 0.30 BFY30 0.20 2N2418 0.40 AP114 0.25 BFY31 0.20 2N2418 0.40 AP115 0.30 BFY30 0.20 2N2418 0.40 AP115 0.30 BFY30 0.20 2N2418 0.40 AP118 0.45 BFY30 0.30 2N2418 0.50 AP128 0.45 CC24 0.60 2N2428 0.15 AP178 0.45 CC24 0.60 2N2428 0.15 AP178 0.45 CC24 0.60 2N2431 0.30 AP181 0.45 CC29 0.65 2N3431 0.30 AP181 0.45 CC29 0.65 2N3433 0.35 AF229 0.40 CC29 0.65 2N3434 0.50 AP121 0.45 CC29 0.65 2N3434 0.50 AP121 0.45 CC29 0.65 2N3434 0.50 AP121 0.45 CC29 0.65 2N3434 0.51 AFY30 0.35 CC24 0.00 2N3434 0.51 AFY30 0.35 CC24 0.00 2N3434 0.51 AFY30 0.35 CC24 0.00 2N3434 0.51 AFY30 0.35 CC29 0.65 2N3434 0.30 AP181 0.45 CC29 0.65 2N3434 0.50 AP181 0.45 CC29 0.65 2N3434 0.30 AP181 0.45 CC29 0.65 2N3446 0.50 AP181 0.50 CC39 0.60 2N3460 0.50 AP181 0.50 CC39 0.60 2N346 0.50 AP181 0.60 CC39 0.60 2N346				0.00		0.95
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2N1610				0.20		
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2N1766 0.75 AD149 0.80 BFY19 0.25 2N2147 0.75 AD149 0.50 BFY50 0.25 2N2161 1.25 AD161 0.35 BFY50 0.25 2N2161 1.25 AD161 0.35 BFY50 0.25 2N2161 0.45 AD161 0.35 BFY50 0.25 2N2219 0.45 AP116 0.30 BFY50 0.25 2N2219 0.45 AP116 0.30 BFY50 0.25 2N2219 0.45 AP116 0.30 BFY50 0.25 2N2217 0.85 AP116 0.30 BFY50 0.25 2N2217 0.85 AP116 0.30 BFY50 0.25 2N24046 0.86 AP118 0.35 CC24 0.30 2N24046 0.80 AP118 0.45 SFY90 0.20 2N24046 0.80 AP18 0.45 CC24 0.30 2N2924 0.15 AP178 0.25 CC24 0.30 2N2926 0.15 AP178 0.25 CC24 0.30 2N2928 0.15 AP180 0.35 CC24 0.30 2N2928 0.15 AP180 0.35 CC24 0.30 2N2939 0.30 AP181 0.35 CC25 0.40 2N2393 0.45 AP232 0.40 CC30 C.25 0.40 2N2393 0.45 AP232 0.50 CC30 0.55 2N2393 0.55 AP232 0.30 CC30 0.55 2N2393 0.55 AP322 0.55 CC30 0.55 2N2393 0.55 AP3	2N1711	0.30	ACY22	0.15	BFY17	0.40
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2N1756	0.75	AD140			0.60
287160 1.25 AD161 0.35 BFYY51 0.25 2.85 2.87 2.87 2.87 2.87 2.87 2.87 2.87 2.87	2N2147	0.75	AD149			0.25
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		1.25	AD161	0.35		0.20
2N2919 0.45 AP115 0.30 BSY27 0.30 2N2917 0.65 AP116 0.25 BSY28 0.30 2N2917 0.66 AP117 0.29 BSY28 0.30 2N2917 0.66 AP117 0.29 BSY28 0.30 2N2917 0.66 AP117 0.29 BSY28 0.30 2N2918 0.50 AP128 0.55 CC22 0.65 2N2928 0.15 AP127 0.25 CC22 0.65 2N2928 0.15 AP128 0.25 CC24 0.60 2N2928 0.15 AP128 0.25 CC24 0.60 2N2928 0.15 AP128 0.25 CC24 0.60 2N2928 0.15 AP128 0.55 CC24 0.60 2N2928 0.15 AP128 0.55 CC24 0.60 2N2928 0.15 AP128 0.55 CC24 0.60 2N2939 0.15 AP128 0.55 CC24 0.60 2N2939 0.16 AP21 0.45 CC29 0.66 2N2939 0.15 AP228 0.55 CC30 0.55 C.50 2N2939 0.15 AP228 0.25 CC30 0.55 C.50 2N2939 0.15 AP228 0.20 CC71 0.25 2N2940 0.25 AP228 0.25 CC728		0.30	AD162	0.35	BFY52	0.25
2N3269A 0.25 AP116 0.25 BSY28 0.20 2N3264 0.60 AP113 0.45 BSY28 0.20 2N3264 0.60 AP125 0.25 Col.6 0.75 2N3264 0.60 AP125 0.25 Col.6 0.75 2N3262 0.11 AP127 0.25 Col.2 0.25 2N3262 0.13 AP127 0.25 Col.6 0.20 2N3263 0.30 AP121 0.25 Col.6 0.30 2N3263 0.30 AP121 0.35 Col.2 0.36 2N3263 0.30 AP121 0.35 Col.2 0.30 2N3263 0.30 AP121 0.35 Col.2 0.30 2N3333 0.35 AP181 0.35 Col.2 0.30 2N3333 0.35 AP181 0.35 Col.2 0.30 2N3334 0.30 AP211 0.45 Col.9 0.65 2N3335 0.30 AP211 0.45 Col.9 0.65 2N3334 0.51 AP136 0.35 Col.9 0.30 2N3346 0.51 AP136 0.30 Col.9 0.30 2N3346 0.51 AP136 0.30 Col.9 0.30 2N3346 0.51 AP136 0.30 Col.9 0.30 2N3464 0.35 AP136 0.30 Col.9 0.30 2N3466 0.30 BC018 0.15 Col.9 0.30 2N346				0.25		
28N2477 0.65 AP117 0.90 BSY855 0.20 28N2466 0.60 AP118 0.45 BSY85A 0.20 28N2466 0.50 AP18 0.45 BSY85A 0.20 28N2508 0.55 AP125 0.25 COL6 0.55 28N2508 0.55 AP125 0.25 COL6 0.55 28N2508 0.55 AP128 0.25 COL6 0.55 28N2508 0.55 AP128 0.35 COC24 0.60 28N2505 0.75 AP180 0.35 COC25 0.40 28N2505 0.75 AP180 0.35 COC25 0.40 28N2503 0.30 AP181 0.35 COC25 0.40 28N2503 0.30 AP181 0.45 COC25 0.40 28N2503 0.30 AP181 0.45 COC25 0.40 28N2503 0.30 AP181 0.45 COC25 0.50 28N2503 0.30 AP181 0.45 COC25 0.50 28N2503 0.25 AP180 0.55 COC25 0.50 28N2503 0.25 AP180 0.55 COC25 0.50 28N2503 0.25 AP180 0.55 COC25 0.50 28N2503 0.25 AP180 0.25 COC30 0.55 28N2503 0.25 AP180 0.25 COC30 0.50 28N2504 0.25 AP180 0.25 COC30 0.25 28N2504 0.25 AP180 0.25 COC30 0.25 28N2504 0.25 AP180 0.25 COC30 0.25 28N2504 0.20 AP180 0.25 COC30 0.25 28N2504 0.20 AP180 0.20 COC30 0.25 28N2505 0.15 BC107 0.15 COC30 0.20 28N2507 0.15 BC107 0.20 COC30 0.20 28N2500 0.15 BC108 0.15 COC30 0.20 28N2500 0.15 BC108 0.15 COC30 0.20 28N2500 0.16 BC108 0.15 COC10 0.25		0.45	AF115	0.30		
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28X2905 0.50 AF128 0.25 OC16 0.20 C.55 C.40 C.20 AF128 0.40 OC23 0.65 C.40 AF128 0.45 C.40 AF128		0.65		0.20		
28X2928 0.15 AP1297 0.25 OC22 0.85 C22 0.85 C22 0.85 C22 0.85 C22 0.85 C22 0.85 C22 0.85 C23						
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287396 0.15 APP180 0.35 OC24 0.50 OC24 0.80 OC25 OC25 OC25 OC25 OC25 OC25 OC25 OC25		0.15		0.25		
283693 0.30 AFF81 0.35 OC25 0.40 283133 0.35 AF231 0.50 OC25 0.30 283133 0.35 AF239 0.40 OC28 0.60 283134 0.5 AF231 0.45 OC25 0.60 283134 0.5 AF231 0.45 OC25 0.65 28323 0.30 AF71 0.45 OC25 0.65 28323 0.15 AF231 0.30 OC25 0.65 28323 0.15 AF231 0.30 OC25 0.65 28323 0.15 AF232 0.30 OC25 0.60 28323 0.15 AF232 0.30 OC25 0.60 28323 0.15 AF232 0.30 OC25 0.60 28323 0.15 AF232 0.30 OC24 0.30 28324 0.15 AF232 0.30 OC25 0.60 28324 0.15 AF232 0.30 OC25 0.20 28324 0.15 AF232 0.50 OC45 0.20 28324 0.30 AF54 0.50 OC45 0.20 28324 0.30 AF54 0.50 OC45 0.20 28324 0.30 AF52 0.50 OC71 0.12 28324 0.30 AF52 0.50 OC75 0.25 28324 0.30 AF52 0.50 OC75 0.25 28324 0.50 OC75 0.25 28325 0.50 OC75 0.25 28326 0.50 OC75 0.25 28327		0.15		0.40		
283655 0.75 AF186 0.50 0.628 0.80 283134 0.58 AP239 0.40 0.28 0.60 283134 0.59 AP211 0.45 0.629 0.65 283134 0.59 AP211 0.45 0.629 0.65 28323 1.5 ASY21 0.30 0.628 0.50 283393 0.15 ASY29 0.30 0.628 0.50 283393 0.15 ASY29 0.30 0.624 0.80 283492 0.1 ASY34 0.26 0.64 0.20 283402 0.1 ASY46 0.26 0.60 0.22 283410 0.3 ASY34 0.65 0.64 0.20 283414 0.35 ASY85 0.20 0.77 0.72 283414 0.35 ASY85 0.20 0.77 0.72 0.25 283414 0.15 ASZ17 0.75 0.77 0.72 0.25 <td></td> <td>0.20</td> <td></td> <td>0.00</td> <td></td> <td></td>		0.20		0.00		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		0.75	AF186	0.50	OC26	0.30
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2N3391 0.20 ASY26 0.25 OC30 C.75 C.82 C.83 C.83 C.84 C.84 C.84 C.84 C.84 C.84 C.84 C.84	2N3134	0.50				
283893 0.15 ASP28 0.30 OC36 0.60 0.80 0.80 0.80 0.80 0.80 0.80 0.8	2N3391		ASY26	0.25		0.75
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1 Amp 1 Amp 425mA

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