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opv． AC volts $10,50,250$ ， $1,000 \mathrm{v} . \mathrm{DC}$ volts $5-25,125,500$ ． $0-50 \mathrm{uA}, 0-250 \mathrm{~mA}$ ． $0-6$ Keg ohm．Deci－ Aize of meter $4 \lambda \times 3 \frac{\text { bels }}{} \times 20$ to $+2 d \mathrm{in}$ ．Complete
with case．
£4－25．P．\＆P． $17 \frac{1}{2} p$

C． 1050 MULTI－TESTER
 10，000 opy
RANGES： DC Voltage：0－3－15－ $150,600-1200$
Volt
10,00
per Volt）． hms per Volt BC Current： $0-120$ uA，ohms per $0-300 \mathrm{~mA}$ ． Resistance： $0-50 \mathrm{~K}, 0-5 \mathrm{Meg}(\mathrm{R} \times 10)$ Decibels：-20 to $+17 a \mathrm{~B}$ ． £5．97⿺辶 $\frac{1}{2}$ P．\＆P．17 $\frac{1}{2} p$

C． 1052 MULTI－TESTER


$$
\begin{aligned}
& \text { RANGES: } \\
& \text { AG Voltage: } 6,30, \\
& 120,300,1200 \\
& 115,000 \mathrm{hm} / \mathrm{V}) \\
& \text { 10 Voltare: } 0.6 .3
\end{aligned}
$$

DC Foltage：0．6， 3,
$15,60,300,1200$ $(30,000 \mathrm{lhm} /$
$30,300 \mathrm{~mA}$ Mr Curremt： $0,067,3,30,300 \mathrm{~mA}$
Resistance： $0,6 \mathrm{k}, 60 \mathrm{k}, 60 \mathrm{k}, 6 \mathrm{M}$ ohms玉7．35．P．\＆P． $17 \frac{1}{2} p$

SM－370 MULTI－TESTER 20，000 opv
RANGES： DC Voltage： $0-5-25-100$－ $500-1000 \mathrm{~V}$（ 20,000 ohms $/$

AC Voltage： $0-5-25-100-$ $500-1000 \mathrm{~V}(20,000$ ohms $)$ nc Current： $0-50 \mathrm{uA}, 0-250 \mathrm{~mA}$ Resistance：RX10，RX．1K（ 300 ohms and 30 K ohms at centre scale）．
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plastic (tinted ) cover included for main. unit.
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Better than 26 db.

## The $£ 25$

## Stereo system

The Duetto is a good quality stereo amplifier, attractively styled and finished. It gives superb reproduction previously associated with amplifiers costing far more.

## SPECIFICATION-

R.M.S. power output 3 watts per channel into 10 ohms speakers.
INPUT SENSITIVITY. Suitable for medium or high output crystal cartridges and tuners. Cross-talk better than 30 dB at $1 \mathrm{Kc} / \mathrm{s}$.
CONTROLS: 4-position selector switch (2 pos, mono and 2 pos stereo) dual ganged volume control.

Signal to noise ratio-70db on all inputs (with vol. max). Controls- 6 position selector switch (3 pos. stereo and 3 pos. mono) Separate volume controls for left and right channels. Bass $\pm 14 \mathrm{db}$ at 60 Hz . Treble (with D.P.S. on off) $\pm 12 \mathrm{db}$ at 10 KHz . Tape recording output sockets on each channel. Size $12 \pm \mathrm{in}$. 6 in . $2 \frac{2}{3} \mathrm{in}$. in simulated teak case. BUILT \& TESTED.

MkII (MAG P.U.) $£ 15.75$ plus 50p. p. \& p. Specification same as Mk. 1, but with the following inputs. Mag. P.U. CER. P.U. Tuner. Spec. on Mag. P.U. 3 mV at 1 kHz input impedance 47 K . Fully equalised to within $\pm 1 \mathrm{db}$ RIAA. Signal to noise ratio$65 d b$ (vol. max).


## SOUND 50 <br> 50 WATT AMPLIFIER \& SPEAKER SYSTEM



The Sound Fifty valve amplifier and speakers are sturdily constructed with smart housings and thoroughly tested electronics. They are designed to last-to withstand the knocks and bumps of life on the road. Built for the small and medium sized gig, they are easy to handle and quick to set up and can be relied upon to come over with all the quality and power you need.
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To protect the output valves, the incorporated fail safe circuit will enable the amplifier to be used at half power.
SPEAKERS! Size $20^{\prime \prime} \times 20^{\prime \prime} \times 10^{\prime \prime}$ incorporating Baker's $12^{\prime \prime}$ heavy duty 25 watt high flux, quality loudspeaker with cast frame. Cabinets attractively finished in two tone colour scheme-Black and grey.

## COMPLETE SYSTEM $-50 \underset{\substack{\text { Pus } \\ \pm 4}}{\substack{\text { ins }}}$ <br> Sound 50 amp and 2 speakers <br> £50

or available separately.
Amplifier $£ 28.50$ plus $£ 1.50$ P. \& P.
Speakers $£ 12.50$ each plus $£ 1.75$ P. \& P.

## The ELEGANT SEVEN MK. 111 (350m W Output) <br> 7 transistor fully-tunable M.W.-L.W. superhet portable. Set of parts. Complete with all components, including ready etched and drilled printed circuit board-back printed for foolproof MAINS POWER PACK KIT : 47p extra. <br> Price $\mathbf{\$ 5 . 2 5}$ plus 50p. P. \& P. Circuit 13p FREE WITH PARTS. <br>  <br> The <br> DORSET <br> (600m W Output) <br> Price £5.25 plus 50 p P. \& P. <br> -transistor fully tunabie M, W het portable-with baby alarm facility. Set of parts. The latest modulised and pre-alignment parcnigues makes this simple to build. Sizes : $12 \times 8 \times 3$ in. <br> MAINS POWER PACK KIT : 47p extra. <br>  <br> SOLID-STATE GENERAL PURPOSE AMPLIFIER

in simulated teak case $£ 7.25$ plus P. \& P. 50p

## SPECIFICATIONS

Output $\pm 10$ watts.
Output impedance- 3 to 4 ohms.
Inputs 1. -xtal mic 10 mV Tone Controls-Treble control range $\pm$ 12 dB at 10 KHz . $2 .-\mathrm{gram} /$ radio 250 mV . Bass control range $\pm 13 \mathrm{~dB}$ at 100 Hz .
Frequency Response-(with tone controls central) Minus 3 dB points at 20 Hz and 40 KHz . Signal to Noise Ratio-better than - 60 dB .
 with Std. or L.P. records, musical instruments, all makes of pick-ups and mikes. Built and tested.

## THE DUO SPEAKER SYSTEM

Similar in design to those on the previous page the 2-way speaker system is beautifully finished in polished teak veneer. It is ideal for wall or shelf mounting either upright or horizontally.
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Impedance 8 or 10 ohms (please state requirement). It incorporates mpedance 8 or 10 ohms (please 7 in . $3 \frac{1}{\mathrm{in}}$. speaker and 2 in . speaker. Teak finish $11 \frac{1}{2} \mathrm{in}$. $x 6$ in. $x 5$ sin. $£ 4.20$ each. 50 p P. \& $P$.


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See top of previous page for address

STOCK


## SET OF PARTS


plus P. \& P. 50p.
Circuit diagram 13p, Free with parts Speaker, baffle and fixing kit £1.25 extra plus 25p. p. \& p. Postage free when ordered with parts.


## NEW FROM TRS

This money saving STEREO 8+8 AMPLIFIER in a new PRE-ASSEMBLED MODULAR PRESENTATION

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TRS 50 WATT VALVE AMPLIFIER
A ruggedly built unit in ventilated steel case with carrying handles: size 12 in $\times$ $8 \mathrm{in} \times 8 \mathrm{in}$. Two input channels mixable ( 10 mV and 150 mV ) bass and treble controls. EL. 34's output (mono) in push-pull, with fixed bias. Excellent for P.A., musical group work, etc. Brand new and guaranteed
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## The Eagle Annual.

Sorry, no Dan Dare, Digby or P.C. 49. Because this is the new Eagle annual catalogue. And it's packed with interesting things. Like the new TSA 151 stereo amplifier: it uses a new block construction silicon output device for absolute reliability. It's got low noise silicon transistors throughout.Its output is 15 Watts per channel. That's 15 Watts RMS, not an exaggerated figure for maximum music power.

The price? A very reasonable $£ 36$.
And for people who like to listen to stereo undisturbed,we've got the new SE 100 headphones.

Dual cone transducers are used throughout,and, to keep the weight down, the independent volume controls are
mounted on a separate unit with a pocket clip. £16.00.

Every item in the annual has been specified or selected by Gerry Adler. Eagle is Gerry's baby, and he's very fussy about what goes out under the Eagle banner. He gets very twitchy at the thought of a duff diode. A bit like the Mekon in fact.

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# Which ever way you choose 

## LEWIS <br> AUDIO SYSTEMS <br> Fine equipment

## MARTIN AUDIOKITS

For the do-it-yourself enthusiast, the return of a

## You are going to enjoy better listening for

great range of hi-fi modules


## less cost and greater reliability

## ready to play

LEWIS AUDIO SYSTEMS comprise ready built equipment designed and built to advanced technical standards of efficiency and styling. Their prices make true hi-fi available to a wider public than ever. Based on the excellent Lewis Audio SA. 55 stereo amplifier in which FETS are used in the pre-amp to ensure better quality throughout, the range offers choice of free-standing amplifier with separate playing unit in plinth with plastic hard top or the Compact assembly in which the amplifier is built into the base of the plinth and motor assembly. Separate matched speakers are available for either system. Illustrated above is the Lewis S.55 Mk. II Compact System.

## LEWIS AUDIO SYSTEMS

SA.55 STEREO AMPLIFIER-6 watt RMS output per ch, into 15 ohm speaker Controls- Input selector/Vol/Bass and replay facilities. DIN socket connections. Modern teak finished cabinet.

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Garrard 2025TC with Sonotone 9TA HC R.R.P. $£ 16.50$

Garrard 40B with Sonotone 9TA/HC
Garrard SP. 25 Mk. III less cartridge

SC. 55 Mk. II 'Compact' with Garrard 2025TC and SA. 55 amplifier built int plinth

## LOUDSPEAKERS

LS. 16 'Major'-13" $\times 8^{\prime \prime}$ three way system in American Walnut finished cabinet. 8 ohms R.R.P. £11.7 Ls. $176^{\prime \prime}$ three way system in teak of Am. walnut finish. 15 or 80 hms
$5.188^{\prime \prime}$ three or Am. walnutfinish system in teak or Am. walnutfinish 15 or 8 ohms.

- TRADE ENQUIRIES WELCOME


## for the constructor

MARTIN AUDIOKITS were first to make modular unit construction available to the hi-fi enthusiast keen to save by building his own assembly. AUDIOKITS were first to feature "add-on-ability" by which a simple system could be expanded to high performance stereo equipment by the addition of easily added on units. Many who built with MARTIN AUDIOKITS years ago continue to enjoy unsurpassed quality and reliability from them to this day. NOW YOU CAN BUY AUDIOKITS AGAIN to allow you to build a high fidelity system to your personal choice and which will satisfy completely on performance, simplicity of assembly, robustness and reliability. These units are beautifully engineered and solidly built for a lifetime of trouble-free service. You can start with mono and add on units to make stereo, or build with stereo throughout.

## TYPICAL MARTIN ASSEMBLIES

1478E Five stage matched input selector unit; controls and pre-amp; power amp. ( 10 watts RMS into 15 ohms ) powertsupply; front escutcheon plate (mono) $1478 \mathrm{SE} \quad$ Similar to above but for stereo. $\quad$ Total price $\quad$ T17.5 9748 SE Stereo assembly for use with high grade ceramic and low power mag. All units are obtainable separately. State pick-up when ordering.


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## PRAGTIGAL WIRELLSS

## TOPIC OF THE MONTH

## components list!

THE ready supply of components is, of course, the life-line of the radio constructor, even if in these days they are sometimes crammed together to form integrated circuits or grouped and encapsulated as modules. But despite the existence of a vast multitude of components, we still hear of people unhappy about not getting what they want from their local suppliers or via mail order.

Undoubtedly, the supply position forms a different pattern these days; stocks of some items become exhausted quicker than they used to do; new versions appear as alternatives which are not always direct replacements. Years ago, a particular component would stay in a catalogue for a decade, but today's constructors cannot rely on an item staying in stock for even a year. Very often it is a case of 'take it or leave it-while it's there!'

Why, then, should this be so? Well, at the International London Electronic Component Show, opening at Olympia on May 18th, 358 . British component manufacturers will be displaying their wares; these companies representing an industry with annual sales of more than $£ 190$ million. But despite this huge turnover, there is concern in the trade balance due to increasing imports of components. The exhibition will be a showplace for these competitors, from the USA, France, Russia, Israel, Hungary, India, Japan, Yugoslavia and other countries.
Components, then, are big business-big international business-and the competition is hot. To stay in the race demands investment, production and marketing of a very high level in the teeth of fiercely contesting rivals. Consider, then, this feverish background the next time you call in at your local dealer for a batch of 22 k resistors, six 100 puffs and a couple of AF117's!
For the facts of economic life today mean that to many component makers the home constructor either does not exist or is very small fry indeed. In fact, if it were not for manufacturers' spin-offs and end-of-run oddments we would be in a very sad state. So next time you feel like complaining about components, be thankful that we are served as well as we are. Things could be far worse.
W. N. STEVENS-Editor

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## NEWS... <br> NEWS...

## Stereo from Teleton



A new stereo amplifier with 26 semiconductors and 18 silicon transistors has been launched by Teleton Electro (UK) Ltd. The new amplifier, known as the SAQ 206, has an output power of 6 watts continuous at $1 \%$ distortion and a frequency response of $40-15,000 \mathrm{~Hz}$. It is equipped with inputs for magnetic and crystal
pick-up plus tape playback. Output from speakers and headphones is $8 \Omega$ and the model is equipped with both scratch filter and loudness control. The amplifier has a brushed aluminium front and matt walnut cabinet. The SAQ 206 operates at $110 /$ 240 volts, 50 Hz . Retail price of the SAQ 206 is $£ 32 \cdot 50$.

The "S.S.S."


## Diary Dates

Apr 19-22. Physics Exhibition, Alexandra Palace, London.
Apr 20-21. Electromation Exhibition, Royal Station Hotel. Newcastle.
Apr 20-23. Technicom '71 - Conference and Exhibition, Hotel Technical Communication for Industry and the Professions, Hotel Metropole, Brighton.
Apr 22-23. Electromation Exhibition, Grand Hotel, West Hartlepool.
Apr 23. Colloquium on Railway Automation (IEE), Savoy Place, London.

Briefly explained, this device consists of an electronic synthesiser which when placed between a mono programme source and a stereo amplifier will create a very realistic stereo effect from all forms of music. Whilst quality components are used throughout to give performance consistent with the most expensive highfidelity equipment, the recommended retail price is just $£ 10$.
The most obvious uses to which the simulator might be put are: between tuner and stereo amplifier for the effect of stereo radio from mono transmissions; between a mono/stereo pickup and stereo amplifier to give simulated stereo with mono records; and between tape recorder and stereo amplifier to give the effect of stereo replay with tapes recorded on a mono machine.

Whilst normal retailer outlets, will be used, in order to enable the customer to more easily obtain this product during the early stages of production the company's fullest attentions will be concentrated upon mail order sales ( $p \&$ p 20p). Their broadsheet on this product is available on receipt of a stamped addressed envelope. Kampel Electronics Ltd., 99 Old Christchurch Road, Bournemouth BH1 1EP (Tel. Bournemouth 28998).

## Eton Computer

Boys at Eton College, the famous English public school, are learning the language and concepts of computers with the assistance of a Marconi-Elliott machine. A " 903 " computer is now in operation at the school and pupils are using it to learn what computers are, what they do, and how one makes them do it. By operating the 903 themselves, the boys are picking up the 'jargon' of the computer world, gaining knowledge of order and instruction codes and probing the intricacies of program writing.
The 903 is also being used more directly as a functional 'tool' by senior boys and members of the Eton staff to help them in the work that they are carrying out. For example, a teacher of Astronomy is using the processor to perform many of his more complex calculations.

## Cassette Cleaner



The Bib Division of Multicore Solders Limited, Hemel Hempstead, Hertfordshire, announce the introduction of their new Cassette Tape Head Cleaning Tape, suitable for all compact cassette type recorders and car playing units.

The unit comprises a cassette tape container in which high quality cleaning tape has been incorporated to clean tape heads, capstan and pinch wheel. It is very simple to use, in the same manner as a tape cassette it is placed in the machine and operated in the play-back position. The whole operation takes only about a minute. A plastic container is provided in which to keep the cleaning tape cassette. This accessory retails at 10 s . 7d././ 53 p including p.t. and is available from leading Hi-Fi shops.

## NAWS...

## NEWS...

## NEWS...

## Mr. Fillmore



After a brief illness Mr. Leonard Walter Fillmore, Managing Director of Jackson Brothers (London) Limited died on the morning of Saturday, January 30th, aged 67. With his father and brother he founded Jackson Brothers in the early twenties and pioneered the development of Variable Capacitors and associated Drive Mechanisms. His inventive genius led to many patents in Components for communications equipments over a span of nearly 50 years.

During the war years he was very active on Ministry Standardisation Panels. From then right up to the time of his death he worked on Panel ' $F$ ', the Variable Capacitor Standardisation Panel of R.E.C.M.F. He was Chairman of Panel ' $F$ ' from September 1951 to January 1965. On relinquishing the Chairmanship he continued as Vice Chairman. Thus for nearly 30 years he devoted considerable time and energy to the Establishments of Standards both National and International for Variable Capacitors. His earlier work on the production of R.I.C. and R.C.S. Specifications has had great influence on the evolution of current International Specifications (I.E.C.).

In recent years he was deeply involved in the preparation of detailed Common Standards under the present Burghard System. His death is not only a great personal loss to his many friends but also to the entire Electronic Industry.

## Group One

About a year ago, Home Radio (Components) Ltd., formed a buying group with about 15 other dealers in the London area, which they provisionally called "Group One". Its primary object was to buy components at the best prices in reasonable quantities. There are several secondary aims such as exchange of surplus stock and information.

In a letter to PRACTICAL WIRELESS, Mr. A. Sproxton, a Director of Home Radio, says, "To some extent this has been forced on us because we wished to buy certain items that wholesalers do not wish to handle and the manufacturers will only sell in quantities that are beyond the pocket of one dealer to buy. But I would like to stress the fact that this is not aimed at distributors or wholesalers (I for one have always believed that they do a useful job and earn their money) in fact any small wholesaler or manufacturer would be welcome to join. I feel sure that you will agree this is a desirable scheme as ultimately it means we can offer readers a greater range of goods at the lowest prices. Initially we are going to limit it to about 20 dealers (not on account of any closed shop principle, but because we thought - quite wrongly - that we could not handle the administration of a larger number). Now we would like to offer membership to any Bona Fide trader in the U.K. and 1 would be very grateful if you could make this generally known through your columns. At the moment there is no entrance fee or subscription, if anyone is interested please write to me. Home Radio (Components) Ltd., 234-240 London Road, Mitcham, Surrey, CR4 3HD.

## U.K.-Finland

The United Kingdom - Finnish trade deficit of over $£ 72 \mathrm{~m}$ appears to be set for a $£ 10 \mathrm{~m}$ reduction as a result of the British Trade Drive in Finland. Britain is now the third in the list of suppliers to Finland.

## Camera catch

A camera which not only photographs a traffic offence at the moment it happens, but also simultaneously records the time and the date on the same negative, may soon be used by police forces in the U.K.
It has been developed by a South African company and is already in use by the police in that country.
Known as the Trafficam, the camera can be powered by either the car battery or the built-in power pack of eight Mallory Manganese Alkaline Mn1500 penlight size batteries for fully automatic instant use.

## Spanish appliances

Fabrelec, one of Spain's biggest manufacturers of electrical appliances, and Westinghouse Electric Corporation, have signed patent licences, technical assistance agreements and trademark agreements for the manufacture of electrical appliances.

## Powerful

The new range of seven zinc carbon batteries now being marketed by Mallory Batteries for general electrical and radio appliances. These are in addition to the mercury and alkaline batteries marketed under the company's Duracell brand name. Mallory Batteries Ltd., Gatwick Rd., Crawley, Sussex.



WITH many transistor portables, tuning is somewhat sharp and possibly tricky, especially at the high-frequency end of the medium wave band. The receiver described here overcomes this by using "station focus"-a control which allows oscillator tuning to be shifted slightly, for easy and exact tuning of a signal.
The circuit is shown in Fig. 1, and a ferrite rod aerial is used for normal reception. This gives sufficient signal strength from most transmissions likely to be required. For weaker signals, or during those times of day when reception is less good, a telescopic aerial can be extended. This is coupled to the tuned winding of the ferrite rod, Ll, by the small capacitor C1. VC3 is an aerial circuit trimmer, allowing Ll to be peaked for maximum possible efficiency on all frequencies, with the aerial closed or extended.

Normal medium wave coverage is about 5501600 kHz . In the interests of easy switching, full long wave frequency coverage is not provided. However, switch S1 places TC1 and C2 across L1, and S2 puts TC2 across the oscillator coil L3. This allows a narrow band around 200 kHz to be tuned for BBC Radio 2 transmissions on this frequency.
$\operatorname{Tr} 1$ is an OC170, followed by two double-tuned i.f.t.'s with AF117 transistors, and this combination gives good sensitivity and selectivity. The oA81 diode D1 used with i.f.t. 3 provides automatic gain control bias in the usual way, through R9, and VR1 is the audio volume control.

The driver stage Tr4, OC81D, and output pair $\operatorname{Tr} 5 / 6,2 \times 0 \mathrm{C} 81$, are straightforward and give ample volume. R18 is for negative feedback over these stages, while R16 is adjustable, so that base operating conditions for Tr5/6 can be set for best results.


${ }_{1}$ in. perspex, so that all components and connections can be seen from either side. If this feature is not required, the receiver can be built on a paxolin panel.

Perspex is usually supplied covered on both sides with paper, which is left in place until cutting and drilling are finished. The panel is marked out to take components as in Fig. 2. A ${ }_{16}{ }^{\mathrm{in}}$. drill was used for the wire ends of resistors, etc., and ${ }^{1}$ in. for bolts which hold the speaker, brackets, etc.

Drilling positions for the i.f.t. pins can be found by pressing paper on pins, then locating the paper on the panel, and marking through with a sharply pointed tool. A central hole is necessary under i.f.t. 1 and i.f.t.2, to take a trimming tool.

The speaker aperture is most readily cut with an adjustable washer or tank

## General Construction

The way in which the receiver is assembled is very convenient for wiring, testing and adjusting. The loudspeaker and all small components are on an $8 \times 6 \mathrm{in}$. perspex panel. A $7 \times 2 \mathrm{in}$. flanged aluminium plate ("universal chassis" ready-formed side) is bolted to the top of this panel, and carries the variable capacitors, switch and volume control. A threeply panel $8 \times 3 \mathrm{in}$. is secured with the bush nuts of these items, and projects about ${ }^{{ }_{8} \text { in. }}$. over the wiring side of the 8 x 6 in. panel. At the bottom of the $8 \times 6 \mathrm{in}$. panel, a further piece of three-ply also $8 \times 3 \mathrm{in}$. is fixed with brackets.
With this form of construction, the receiver will rest in any position, to insert and wire components and will stand vertically in a normal working position, without a cabinet. The bottom piece $8 \times 3 \mathrm{in}$. carries the battery. The controls are on the top, so the whole receiver can be lowered into the case which clears $8 \times 6{ }^{1}{ }_{2} \times 3$ in. inside and has apertures opposite the speaker.
The $8 \times 6 \mathrm{in}$. panel is
cutter, but can be made with a fine toothed saw.

Check the holes against Fig. 3. Drilling is much easier before any components are mounted, but if any holes are missed, they can be drilled later. Drill the 7 x 2 in . flanged plate and panel, so that they can be secured together with the two bolts

marked MC in Fig. 3. This plate is to the right in Fig. 2, to clear the extending aerial.
Fig. 2 also shows the spacing for the variable capacitors the holes for which are most readily made with a punch. VCl is held with three bolts which run into tapped holes in the front plate. These bolts must be very short, or washers must be added, so that the ends do not foul the moving or fixed plates of the capacitor.

The ferrite rod and speaker are left off until last.

## Wiring Tips

Place tags under the bolt heads and nuts of both bolts MC, Fig. 3. A 20 s.w.g. bare tinned copper wire is soldered from tag to tag, as shown, as a positive or "earth" return and VC1/2 is connected to this circuit through the metal plate. Connect VC3 and VC4 to the adjacent tags this side, Fig. 2, and also X on VR1, and S3.

All other wiring is carried out with 26 s.w.g. tinned copper wire, with 1 mm . insulated sleeving. It is convenient to use red for all "earth" or positive circuits, black for negative circuits, and some other colour for other connections.


Compare this view of the completed receiver with Fig. 2.
I.F.T.'s 1 and 2 have slightly closer spacing between pins 1 and 2, and 5 and 6, as in Fig. 3 and must be inserted and wired this way. The cans of all i.f.t.'s are earthed.
As a check, each component can be marked with coloured pencil on the diagrams as it is inserted and each connection can be similarly marked, as it is made. If this is done systematically, it is unlikely that anything will be omitted.
Electrolytic capacitors must be inserted with the polarity as shown. Trimmers TC1 and TC2 are of a type which can be secured with nuts (Fig. 3). The small trimmer TC3 can be soldered across VC4, or supported on a small bracket from the flange.
The telescopic aerial is" fixed so that it can be drawn up through a hole in the top panel. Wire VR1 to MC, C9 and R10 as shown, and run red flex from the switch on this control, S3, soldering on a positive battery clip. The battery negative lead comes from R15.

Connect a flexible lead from the slider of R16, to one end, as in Fig. 2.

## Transistors

These are best added after the resistors and capacitors. Fig. 2 shows the four leads of $\operatorname{Tr} 1, \operatorname{Tr} 2$ and $\operatorname{Tr} 3$, which are for emitter, base, shield and collector.

Transistors $\operatorname{Tr} 4, \operatorname{Tr} 5$ and $\operatorname{Tr} 6$ have three leads, for emitter, base and collector, as shown in Fig. 2. If $\operatorname{Tr} 4$ is an OC81D and $\operatorname{Tr} 5 / 6$ are OC81's, with leads in line, then a red spot indicates the collector.
Shape the leads so that they are clear of each other, and will pass down through the correct holes. The transistors can be about ${ }_{2} \mathrm{in}$. clear of the panel, but leads should not be unnecessarily long in the i.f. stages. They are then soldered as in Fig. 3, and snipped off.
Form the leads of TrI as in Fig. 2, and put sleeving on them before soldering. With Tr5 and Tr6, both emitter wires go through a single hole, to R17. Place Dl with its polarity as shown.
Heat shunts are not generally required if the connections are soldered rapidly with a properly heated iron. The iron is removed immediately the joint is made.

## $\star$ components list



TO BE CONTINUED

# TAKE <br> $2 ه$ 

 JULIAN ANDERSON
## A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

IT is the aim of this page to give circuits and explain the operation of the simplest type of circuits and we are of course limited to $£ 1 \cdot 00$ and twenty components and obviously this places certain restrictions on the quality of the finished articles. Nevertheless simplicity also leads to a lesser likelihood of mistakes and the circuits usually have a wide range of uses in many fields. This month's project fits into this category; it is an audio amplifier which may be used to boost the output of an earphone type radio, as a pickup amplifier or an intercom. It is extremely simple and, to my knowledge, has never been published before.

## THE CIRCUIT

The secret of the simplicity of the circuit shown in Fig. 1 is the directly coupled Darlington Pair of transistors, $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$. This configuration, which is also known as a super-alpha pair, acts rather like a single transistor with very high gain, the base being represented by the base of Tr1, the emitter by the emitter of $\operatorname{Tr} 2$ and the collector by the common collector connections. The gain of this combination is roughly equal to the products of the gains of the individual transistors. With the specified transistors the minimum gain should be no less than 8,000 using the green version of the 2N2926 (highest gain grouping) or a maximum of over 20,000 !

With gains of this sort of order it's not surprising that few components are needed.

If one looks upon a transistor as a resistor whose value between the emitter and collector alters, depending on the base bias applied, it can quickly be seen how the circuit operates-and why the gain is so high. Regarding the operation in this way, Trl becomes a variable bias resistor for Tr 2 so that the higher the input signal, the greater the bias.

The quiescent current through the transistor pair depends on the value of R1 and although the value shown-1 $\cdot 8 \mathrm{M} \Omega$-worked well with several transistors used for $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$, the value does depend on the gain of the pair and may have to be selected from a range between $680 \mathrm{k} \Omega$ and $3 \cdot 9 \mathrm{M} \Omega$.

The quiescent current through Tr2 is fairly high20 mA or so-and it is for this reason that we are using a BFY51 rather than a transistor with a lower current handling capacity.

C1, VR1 and C2 simply act as d.c. blocking capacitors and as a volume control. The input impedance of this type of circuit is high and this allows for the use of low value blocking capacitors in conjunction with a high value volume control-here a $1 \mathrm{M} \Omega$ type is used. It is not recommended to substitute an $8 \Omega$ or a $3 \Omega$ speaker directly into the collector circuit, though the use of a transformer with a ratio of about $5: 1$ would allow these to be used.

No. 25 AUDIO AMPLIFIER


Fig. 1. The circuit of the "Take 20" Darlington pair audio amplifier"


Fig. 2: A suggested layout for the amplifier using a small tag-strip; the transistor lead connections are shown below, viewed from the lead ends.

A suggested layout on a short tag-strip is shown in Fig. 2, though as the circuit is published as a general purpose type, it will normally be built as part of some other circuit.

A PP9 battery should be sufficient for this circuit; the smaller PP3 type will be unable to supply the necessary current as the power output of the amplifier will be about 200 mW . This output level is quite adequate for most uses.

The final quality is surprisingly good and all-in-all the circuit will be found to be a very useful one.


IT is difficult to fit the amplifier described in this article into any normal category. By the DIN specification it is probably Hi-Fi but by current accepted standards of Hi-Fi it leaves a little to be desired.
The ten watt output is far higher than normal record player amplifiers, yet is well below the usual 25 W which now seems to be the lowest power acceptable.
It is neither as cheap to build as the amplifiers featured in "Take 20 " but neither does the cost approach that of commercial amplifiers. So this amplifier is in the "Mid-Fi" field. The quality is goodlaboratory tests show a flat output from 40 Hz to 20 kHz with harmonic distortion below $1 \%$ at 1 kHz at 5 W output. This distortion level is high by prevalent standards but since the human ear cannot distinguish even $2 \%$ of harmonic distortion, it hardly matters.

The cost of the project is low. The amplifier by itself should be rather less than $£ 5$ and the cost of the separate power supply will probably add another $£ 3$-these prices do not, of course, include the loudspeakers.

The circuit and the construction details cover a mono version but naturally when doubled up, using dual pots for the volume and tone controls, and fitted with a balance control, it would be perfectly satisfactory for stereo.

Since the amplifier as described does have limitations in performance, it is not intended for use with expensive magnetic pickups and it is assumed that it will be used with ceramic or crystal types. If a magnetic pickup facility was to be incorporated, correction would also have to be applied.

No great originality is claimed for the circuit-it is largely based on Mullard designs though slight modifications have been incorporated. The output transistors are the common AD161-AD162 complementary pair and closely matched pairs of these are currently available for as little as 50 p though they are more commonly sold for 80 p.

The finished amplifier, in the monophonic version, is small, though not so small that construction is difficult and it was designed to this size so that it can fit into almost any record player cabinet. If the amplifier is to stand on its own a wooden surround
would improve appearances. The power supply is built separately and this can be mounted quite a distance from the amplifier-if fitted into a record player this can be fitted at the back.
Loudspeakers are not dealt with as this is a completely different field but the impedance can be anything between $5 \Omega$ and $15 \Omega$. The amplifier has been tested running for several hours at full output on a $3 \Omega$ speaker system but this low impedance cannot be recommended in all cases, though no harm came to the prototype.
The hum and noise level are extremely low; at full output they were only just audible with an ear inside the speaker cone and at a foot away, nonexistent.
One of the probiems with home built amplifiers of this type is instability, the author has often come across this and knows of others who have experienced the same problems.
The design shown should be unconditionally stable and two features are incorporated in the circuit to increase stability, even though without them the stability was good; this means that anyone building the amplifier can be sure that these problems will not arise even if the layout chosen would tend to oscillation.

## THE CIRCUIT

The complete circuit, apart from the power supply, is shown in Fig. 1 and this comprises three main sections: the preamp., the tone control and filter stage and the output amplifier.
It has already been mentioned that the amplifier is designed for use with ceramic or crystal pickups. Although these have got a very high output-at the very least 80 mV and often ten times that level, the inherent impedance of these types is high and unless they are coupled to a high input impedance, the frequency response will suffer. Transistors in the common emitter mode have typical input impedances of about $20 \mathrm{k} \Omega$, far too low to mate the pickup to, so for this reason the inputs are connected directly to a $1 \mathrm{M} \Omega$ resistor in series with the input and this, of course, determines that the input impedance is at


Fig. 1 : The complete circuit of the 10 W amplifier. A full description of the operation and function of the components is given in the text.

## $\star$ components list


least this high.
Two inputs are provided and as shown are for similar levels and impedances. One is provided for the pickup, the other for a radio tuner. Radio tuners have outputs which vary from about 50 mV to 1 V and R3 (if the tuner is to be connected to this section)
may well have to be varied from the given value to match the tuner used. The value shown is suitable for 500 mV .
For a 1 V output it should be $2 \mathrm{M} \Omega$ while for 50 mV it should be $100 \mathrm{k} \Omega$. Since the output impedance of tuners is rarely high it doesn't matter if the input
impedance is lower for this side. In any case the value should be chosen so that the levels at the input to Tr 1 are similar for both tuner and pickup.

Therefore R1 and R2, R3 and R4 act as the input attenuators and matchers. The output for the attenuators go directly to the input select switch and the output from this goes to the base of $\operatorname{Tr} 1$ via the blocking capacitor Cl .
The function of Trl is to raise the level of the signal to a suitable level to feed the tone control network and overcome the necessary attenuation brought about by the input resistors. Tr 1 is a $\mathrm{BC169C}$, a plastic version of the low noise BC109. R5 provides the base bias and is of this high value because of the high gain of the transistor.

The output of the preamplifier connects via the blocking capacitor C 3 to the volume control, a $10 \mathrm{k} \Omega$ $\log$. potentiometer. If a stereo version is to be built the only additional component necessary would be a balance control which fits at this point in the circuit. This should be a $25 \mathrm{k} \Omega$ linear pot., the outer tags connecting to the sliders of the two volume controls with its own slider going to chassis.
The output from the volume control goes to one side of the tone control network comprising VR2, VR3, C4 to C7 and R7 and R8. The other side of the tone control network is connected to a negative phase signal so that the output of the network can be varied from minimum bass and treble to maximums of the same signals.

The output of the network connects to the base of $\operatorname{Tr} 2$ which is baised by R11 and R12. The feedback to the tone control network is taken from the potential divider R9 and R10 which between them form the load for Tr2.

Another output from the collector of Tr 2 is taken via blocking capacitor Cl0 to the "Hi-Cut" filter which is designed to couple back to the base as little of the frequencies below 7 kHz as possible and as much of the higher frequencies as possible. As the filter is connected in the negative feedback mode
this has the effect of giving a very steep cut above 7 kHz and acts very effectively as a scratch filter for poorly treated or old records.

In addition when used to amplify radio signals it will help to get rid of the higher frequency heterodynes present on many a.m. signals after dark.

A filter of this sort should not be confused with a tone control which is designed to gradually slope the high or low frequencies. The "Hi-Cut" filter is designed to have little effect below 7 kHz and a lot above it.

The filter is switched in or out by SW2 but C 13 is arranged to couple at all times. This is included so that even with the filter out there is a very steep cut at a much higher frequency-about 40 kHz -and signals much above this are completely eliminated. Since this is well outside the audio range it in no way impairs the quality but it does serve two other functions.

The fantastic frequency response of the silicon transistors used in modern audio amplifiers leads to the amplification of any r.f. signals picked up in the wiring which tend to be detected at some point


Fig. 2: The power supply circuit.


Fig. 3: The driling of the chassis. A sulfable Inexpensive one, as used in the prototype is available from H. L. Smith Lid, 287 Edgware Rd, London W. 2


Fig. 4: The component layout on plain veroboard.


Two internal views of the 10 W amplifier showing the general layout. Compare these with Figs. 4 and 5.


Fig. 5: The wiring between the component board and those components mounted directly on the chassis.
current in the output stage.
A degree of feedback is applied by connecting the load resistor of Tr4 (R22) through the loudspeaker.

The output of the complementary pair provides the low impedance output via C17 which has to be high in value to effectively couple the bass notes to the loudspeaker.

Amplifiers of this type require a low impedance power supply-batteries will be no good. The current drawn varies between a few milliamps and an amp. The transformer has a primary winding of 250 V with a 17 V , 1A secondary which connects to the Bridge Rectifier BRI. Various types are suitable and some inexpensive plastic encapsulated types such as the Mullard BY164 are highly suitable. However any type with a voltage and current rating of $30 \mathrm{~V}, 1 \mathrm{~A}$ should be satisfactory.
To keep the hum level down to an acceptable level, the reservoir capacitor has to be of a high value. Some protection to both the power supply and the amplifier is provided by the 1 A fuse in the line.

Careful smoothing of the supply voltage is necessary in the earlier stages and this is catered for by C2; any value lower than this may lead to low frequency instability. If motor-boating does occur the value of C2 should be increased.

## CONSTRUCTION

The amplifier is built inside a small aluminium chassis $7 \times 4 \times 1^{1}{ }_{2}$ in. with one long side holding the controls with the inputs, outputs and power transistors sited on the back. The drilling of the prototype chassis is shown in Fig. 3.

Small slide switches are used for SW1 and SW2 and rectangular holes have to be cut at each end of the control panel for these. Slide switches are designed to be bolted to the chassis but a much smarter and easier job is made by gluing these on using Araldite.
The holes for the power transistor leads and mounting screws are most easily made by using the mica washers, which should be provided with the transistors, as a template.
On the prototype the supply is arranged to plug in using a Bulgin connector, but of course a simple hole fitted with a rubber grommet would be just as good to feed the two wires to the power supply.
To make the wiring short, a small tag strip should be mounted near the output transistors to hold R23 and R24.
The majority of the components are mounted on a piece of plain Veroboard, $0 \cdot 15$ in matrix, sized $4^{3}{ }_{4} \times$ ${ }_{2}^{1}{ }^{1}$ in. The siting of the components on this is shown in Fig. 4. C15 is a bulky component and has to be sited as shown in order to fit in.
$\operatorname{Tr} 4$ will be warm in operation and it is important that a heatsink is fitted to avoid thermal runaway. The output transistors also need a heatsink and this is provided for by bolting these to the back. Even though the body of $\operatorname{Tr} 6$ is at chassis potential (the body being the collector) do not be tempted to leave off the mica insulating washer that is also needed for Tr5. Hum may be introduced due to earth loops if it is left off.
The output capacitor is connected directly between the output socket and a mounting pin fitted on the component board, so is R22.
The wiring between the board and the components mounted on the chassis is shown in Fig. 5.
No wiring is shown for the power supply as this will depend on the transformer and bridge rectifier used, but it is so simple that it can easily be worked out.
If a switch is needed for this it should be mounted on the power supply chassis.

Only one input socket is provided-a DIN 3-pin type and both inputs should be wired to it, the attenuator resistors are also mounted on it.

If the slide switches are glued to the chassis as suggested, a sheet of white card can be fitted over the front panel, as there will be no screws to stop it from laying flat, and a very acceptable face plate can be achieved as shown.

## TESTING

Once the wiring is completed and thoroughly checked it is worthwhile measuring with an ohmmeter the resistance between the bases of the output transistors. The resistance should be low and the preset VR4 adjusted for minimum resistance. (This means that there should be a short between them.) Also check that the collector of $\operatorname{Tr} 5$ is insulated from the chassis. If all is well with these tests it is unlikely that harm will befall your newly completed project.

If two PP9 batteries are available, these can be


The small size of the amplifier can be judged by the matchbox on the left yet the photographs on the previous page show that layout is not crowded.
used to supply 18 V for initial testing. The noise level, even on full output, should be very low, but the dabbing of a finger on the input should produce a high hum level.
If all seems well a pickup can be connected. On full output there will be severe distortion due to the use of batteries but the use of these lessens the likelihood of destroying the transistors if there are any mistakes in wiring, etc.
With all these points checked, the power supply can be connected. There may still be distortion due to the setting of VR4 and this should then be backed off until the audible distortion just disappears while ensuring that $\operatorname{Tr} 4, \operatorname{Tr} 5$ and $\operatorname{Tr} 6$ do not get hot.
The effectiveness of the tone controls and the Hi-Cut filter should be considerable and the output be more than adequate.


INFORMATION WANTED
INFORMATION WANTED
Ladetails of the makers of the stereo amplifier marketed by Electronic Sales (Victoria) LTd. I was led to understand that this was covered by maker's guarantee but have no
idea who they were. The faul is that I switched on without speakers conne A. E. Webb, 25 Here. The fault is that I switched on without, Milton, Abingdon, Berkshire.
...any information on the Fi-Cord 1A tape recorder. I wish to modify this machine to one with a more modern specification.-M. A. Amstell, 37 Basing Hill, Wembley Park, Middiesex.
ortable UXR1-A Pitt or acquire constructional information on Heathkit battery ...any information, or the lond College, Nr. Cirencester, Gloucestershire. the transistor IIRe-up $4 \times 2$ 2SB176, 2SB175B and $2 S B 1738$.-J. M. Newby, 27 St. Johns

- any information on the Standard Radio 5AH transmitter. Also, where can I get a BA114 Mullard diode and has it an equivalent?-P. Gladwin, Westfeld Farm,
Towersey, Thame, Oxon. OX9 3 BB. Towersey, Thame, Oxon. OX9 3QB the $R 209$ Mk. 2 receiver.-P. Reeves, 2 Hunts Mead, Billericay, Esseuit diagram of


## ISSUES WANTED

.7illactical Wireless dated October 1957 containing the Music Box article. Ten shillings paid for same.-"The Occupier", 3 Lawrence Close, White City Estate, N. the March 1970 issue of Practical Television,-J. Barin, 7 Easiside Road, London, N.W. 11 OAY. ston, Lancashire.

## ISSUES FOR DISPOSAL

S...coples of Practical Wireless for 1963/4/5/6. Anyone can have them FREE.
S. J. Wells, 34 Brockman Rise, Bromley, Kent.

Wireless from May, 965 to April, 1966 (November 1964) to December 1968. Practica considered.-N. J. Moore, to April, 1966. All are complete and in binders. Any offers

EQUIPMENT WANTED
16 Hilliers Lane, Beddington, Surrey. Jason Argonaut f.m./a.m. tuner.-A. Kenway, 16 Hilliers Lane, Beddington, Surrey.

## LITERATURE WANTED

...copy of Mullard Circuits for Audio Amplifiers, second edition (1962). The price
at the time was 8 s . 6 d . Please state price and postage.-G. W. Saunders, 26 Rowan
Crescent, Streatham, London, S.W.f6.

D
ESPITE the fact that there were only eight entries for last year's John Rouse Trophy (RSGB constructional entry for under-sixteens), and our disgruntled Editor found it necessary to bemoan (September 1970) that few radio amateurs now build their own main station gear, we feel encouraged by the response to Project Autumn 1970, to recommend those bright young sparks about to cast off the shackles of school to think about the radio servicing business.

Henry recently enjoyed a talk with a bunch of school-leavers. Many of them were captivated by the glittering world of electronics. Bemused by the buttonpressing magic of $D r$. Who and Star-Trek, bedazzled by the multimillion flash of instrumentation in the Space-age-for-real, they imagine that radio and television engineers in the entertainment industry must hold the key to perpetual interest.

Henry is amazed at the blurred occupational edges. These youngsters imagine that the lucrative and glamour-ridden world of the television 'star' is gained via the cabled chaos of the studio floor, or, at best, the hallowed hush of the control room.

Hush! Have you ever been in a control room when the producer is shouting at three camera-


The continuity girl dissolved into tears.
men at once, when the sotto voce of the floor director's talkback is rattling the monitor loudspeakers, when the continuity girl has dissolved into tears over a lost page four and the musical arrangements depend on the cueconsciousness of a half-drunk tape recorder operator?

Very few performers come up from these ranks. To begin with, a few weeks behind the cameras, or abaft the mikes, soon disillusion any would-be entertainer. There's Harold Williamson, of course, but he is not exactly an entertainer. And there's 'Professor' Stanley Unwin, whose prowess should convince us that a spell in the camera crew would make anyone talk gobbledygook. One or two disc jockeys know a little of what goes on beneath the platter. But those who fancy that job may not have any notion of the sweat and toil that can go into sorting out, helping to edit and presenting ' $a$ favourite toon for Mrs. Pettifer of Lower Peckham Rye.'

Sometimes, the yearning is genuine. The lure of electronics really fascinates youth. Some of the mystery has been peeled away by a keen science master, revealing even greater depths. Space-age phenomena make much that was wonderful seem mun-dane-when we hear a gravelly op-check from many thousands of miles away, we are now more likely to carp at its roughness than marvel we can get it at all!

But Miss Today and Master Tomorrow take miracles in their stride. Perhaps I should have told them about the openings in Tero-technology, a word the MinTech boys coined for Maintenance Engineers. These maligned gentlemen are fast becoming an élite. They work for large engineering companies, daily waving their magic wands over the fallible products of systems designers.

They are expected to instal, commission and maintain any-


Leaving behind a trail of modified machinery.
thing from an air-drying purifier to a fully automated oilfield. Electronics is only part of the game to them-building blocks are what we should consider factory-sized projects.

I know one of these gents. He came out of redbrick with a poor degree, entered industry as an assistant to an assistant of an assistant designer. Moved from firm to firm, absorbing knowledge like a sponge and leaving behind a trail of modified machinery. He graduated to his present job simply because nobody else dared take it. And now he picks up all the bricks that scatter-brained designers have dropped besides acting as consultant for half-a-dozen international concerns.

From whence came his qualifications? Well, despite our modern technicological age and the outmoded place for an amateur, I suggest he received his impetus and his capacity for a quirky open mind from his younger love of amateur radio, constructional hi-fi and continual dissatisfaction with marketed products. He is a gadget man' and proud of it, even if his present job of 'panelchanging' involves him in king. sized modules.

If anyone tells you, young shaver, that the day of the dabbler has gone, just point to the tero-technologist and be thankful.

# SERVICN 

PART 1
H. W. HELLYER

## THIS SERIES, WRITTEN BY H. W. HELLYER AND G. J. KING, BEGINS WITH A DISCUSSION OF THE BASIC COMPONENTS OF ANY PIECE OF ELECTRONIC EQUIPMENT, THE RESISTOR, CAPACITOR AND INDUCTOR, WITH SOME NOTES ON THE VALVE AND TRANSISTOR.

BEFORE we can repair a radio receiver, audio amplifier or any other piece of electronic equipment, we must understand something about the fundamental parts of the circuit. Any circuit can eventually be broken down into its component parts or combinations of parts, just as any whole circuit will separate, for convenience, into a number of 'building bricks', as we shall see when my colleague Gordon J. King takes over the next part of this series.
My job, this month, is to lay the ground, describe the 'bones' which form the skeleton circuits and give a few hints about their testing.
Description of components and their functions must needs be brief. We haven't the space for a detailed exposition or for more than a quick look at the three main classes of circuit bones-resistors, capacitors and inductors.

## RESISTORS

Sub-dividing the first class, we have fixed, variable and non-linear resistors.

Fixed types may be of carbon, of composition, metal-oxide film on a glass rod or any of several proprietary substances. Values of these components will vary between a fraction of an ohm and several million.

Tolerances are important to the designer and to the engineer who follows in his footsteps by maintaining the equipment. For resistors the tolerances fall into groups, from $1 \%$ to as much as $20 \%$. The current a resistor can safely carry is important also for this determines the choice of wattage of the component we may need, to replace a damaged one in a circuit.

The wattage (W) is equal to the product of the current (I) through the resistor (R) and the voltage developed across it (V). By Ohm's Law, $W=I^{2} R$ or $\mathrm{V}^{2} / \mathrm{R}$ or $\mathrm{V} \times \mathrm{I}$.

Resistors of more than about 2 or 3 watts will usually be wirewound. These are generally bulkier and often consist of a ceramic tube with resistive wire wound on it anchored to stiff wire ends.

Non-inductive wirewound resistors are very necessary for some positions in the circuit and these are
made by winding the resistive element in such a way that the two legs of the 'coil' lie together and magnetic fields tend to cancel each other. Such bifilar winding, as it is called, will also be met with in coil construction, where it is used for the same purpose of cancellation of unwanted magnetic fields.

Practical points: composition resistors are easily damaged by heat. Discolouration of the coding or body paint is an indication that excess current has passed. Do not ignore the warning, look for the reason. Metal-oxide components (and some of the older composition types) had end caps clamped on, relying on physical pressure for their resistive contact.

A loose clamp, or a badly connected lead wire to a cap, is the possible cause of a 'high resistance' joint. As these types are often painted over, with the poor joint beneath the coating of paint, the end cap may not appear to be loose at all.

Colour coding has been standardised pretty well by now, although there are always awkward exceptions. Dirt, heat and age may discolour components and obscure or alter colours, so the rule should be: 'When in doubt-check.' A table of colour codes, including tolerances, etc., is given for resistors.

To some extent, the same code can be used for capacitors, as can the abbreviated method of indicating component values. Despite attempts at standardisation, values may be expressed in several different ways. A 4700 ohms resistor, for example, may be designated $4 \cdot 7 \mathrm{k}$, or 4 k 7 , or given its full title.

Variable resistors come in a number of varieties, from the common, three-tag 'volume control' we know so well, to multi-section, tapped sliders, often ganged mechanically as well. Basically, the variable resistor can be sub-divided into carbon-track and wirewound types, and a further classification must specify whether the 'law' of the resistor is logarithmic or linear, i.e. log. or lin.

Linear types are self-evident; the resistance in circuit varies in proportion to the angular rotation of the spindle to which the wiper is attached (or the lengthwise travel of 'slider' types). Log. types have a track whose resistance increases logarithmically
as the spindle moves, so that for a great proportion of travel there is little change in resistance, then as the rotation continues, the resistance increases more and more rapidly, i.e., the scale of resistance is cramped toward the upper end. As this conforms more with the physical nature of hearing, such a control is more often used for a volume control, whereas lin. types will usually be found in tone and balance control circuits.

Practical points: noisy volume controls are a frequent complaint-not always justifiable. Very often, the real trouble lies in stages prior to the control, with the fault revealed as the control 'opens up'. An example here is a leaky coupling capacitor in a valved circuit, where the coupling is from the anode of the preceding stage to the 'top end' of the volume control, the potential across the capacitor being nearly that of the h.t. line. This causes a small current to flow through the variable resistor, with resultant noise.


Reported "noisy" volume controls can be due to a leaky coupling capacitor.

Similar faults occur in transistorised equipment, where electrolytic capacitors are needed to maintain the time constants of the interstage circuits.

Noisy controls can be caused by poor connection between spindle and main body, or to wiper support. Where there is a divided section of the control casing, poor clamping or corrosion between surfaces can also be an unsuspected cause of noise, as can inefficient earthing.

A composition track volume control already damaged by current flow, caused by a leaking capacitor, may have a 'hot spot', a portion of the track pitted or burned. This will never succumb successfully to treatment. Replacement is the only cure. But carbon track variable resistors that have simply aged, which can be opened easily, could be treated by rubbing over the track with a soft lead pencil. If the damage is not too far gone, the crackle can sometimes be cured by injection of switch-cleaning fluid; several aerosol preparations are available.


Even in black and white the colour bands on this 1-watt composition resistor are clearly seen.

Personally, I do not favour this method. It is, at best, a temporary solution. Replacement of the offending control is always best. But though the professional in me must advocate the fitting of new parts, the practical wireless hobbyist in me says 'what about cost and availability?' If you are prepared to spend infinite pains in rejuvenating an outworn part, then good luck to you.

Small variable resistors, used as preset controls

COLOUR CODE FOR CAPACITORS AND RESISTORS

|  | First Figure ' A ' | Sec'd Figure 'B' | Multiplier ' C ' |  | Tolerance 'D' |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Ceramic | Capacitors |
|  |  |  | Resistors | Caps pF | Res | to 10 pF | over 10pF |
| Black | - | 0 | 1 | 1 | - | 2pF | $\pm 20 \%$ |
| Brown | 1 | 1 | 10 | 10 | $\pm 1 \%$ | $0 \cdot 1 \mathrm{pF}$ | $\pm 1 \%$ |
| Red | 2 | 2 | 100 | 100 | $\pm 2 \%$ | - | $\pm 2 \%$ |
| Orange | 3 | 3 | 1,000 | 1,000 | - | - | $\pm 2 \frac{1}{2} \%$ |
| Yellow | 4 | 4 | 10,000 | 10,000 | - | - | - |
| Green | 5 | 5 | 100,000 | , | - | 0.5 pF | $\pm 5 \%$ |
| Blue | 6 | 6 | 1,000,000 | - | - | - | - |
| Violet | 7 | 7 | 10,000,000 | - | - | - | - |
| Grey White | 8 9 | 8 | 100,000,000 | $0.01 \mu \mathrm{~F}$ | - | 0.25pF | - |
| White No colour | 9 | 9 | 1,000,000,000 | $0.1 \mu \mathrm{~F}$ | + $20 \%$ | 1 pF | $\pm 10 \%$ |
| Silver | - | - | - | 一 | $\pm$ | - | - |
| Gold | - | - | - | - | $\pm 5 \%$ | - | - |



A salmon-pink fifth ring or body colour denotes a Grade 1 high-stability composition resistor. There are variations in the code for capacitors other than ceramic tubular types.

The "preferred" series of values is as follows:-

in many circuits, are vulnerable to damage by a heavy hand. The usual trouble is strain of the wiper portion from its open rivet attachment to the body of the control. These controls are not intended to carry much current. They will burn out easily and the burn is sometimes invisible-the usual place being adjacent to the end contact. If the control is used as a simple variable resistor and the track is damaged, a simple solution is to reverse the end connection, thus using the other terminal of the track. It is best, when connecting simple variable resistors into circuit, to bridge the slider to the 'common' end. Similar remarks apply to the potentiometer, or the larger variable control.

A final class, the dual concentric control, is being met very often in stereo equipment, needing another special point of attention to be noted. This is the possibility of noise due to imperfect contact between the sections of the control. Sliding metal surfaces tend to generate electrical as well as mechanical noise and this can sometimes be picked up and amplified. A cleaning and greasing regime for such controls will help-but really this is a design problem, and the root cause may be that the control is 'too early' in the circuit. I feel sure my colleague will have a few remarks to offer about such circuitry in a later part.

Non-linear resistors: Final mention has to be made of the special resistors increasingly being encountered: such things as temperature and voltagedependent resistors, thermistors, varistors, etc. The thermistor at one time performed a voltage dropping function as part of the series chain in the heater line of an ac/dc receiver. As the component warmed, its resistance decreased and from a cold value of several thousand ohms reached an eventual value of one or two ohms (in some cases up to about


A dismantled potentiometer showing, top left, the spindle; top centre, the fixing spring; bottom centre, the carbon track with rivetted tags. At top right, the wiper with split spring for flexibility.
40 ohms) when at operating temperature. This regulated the current flow, preventing damage to cold valve heaters and obviating cathode stripping which can be caused by excessive emission. H.T. applied quickly, when semiconductor rectifiers are associated with valved circuits is a common cause of cathode stripping.

Practical points: such components must be allowed to dissipate their heat. They should be mounted in
a ventilating flow of air, if the repairer or constructor has any choice in this matter. Care must be taken to dress wires away from the hot thermistor, and to keep other components out of its heat field.

Smaller temperature-dependent resistors will be found in power output stages, near or attached to the heat sinks of power transistors. Their purpose is to regulate the bias circuits so that an increase in heat causes a reduction in current. More will be said later about these protection devices.

Varistors are resistors which change their value according to the voltage across them. Again, they are met in many modern circuits where electronic control is needed, and some of the stabilising circuits in which they are employed will be dealt with in succeeding articles.
Light-dependent resistors have a special function, their resistance decreasing as the light falling on their target area increases. There are a number of


Inductors and polyester capacitors in a speaker crossover network.
special types with special applications and only a few of them will concern us here. A practical point arises from this: when these 'variable' or non-linear components are met, take great care that any replacement made shall be exact. There are seldom effective substitutes, and the designer may have chosen a particular component with parameters in mind which may not strike us immediately. The range of variation, the voltage rating and the current rating should be studied.

## CAPACITORS

Capacitors sub-divide into three main groups: fixed, variable and electrolytic. Within these groups, there are many more divisions.

Fixed capacitors have various dielectrics and there are various methods of constructing and laying the foil or plates, giving all manner of special characteristics. It would be futile to attempt to explain these in detail, but a few salient points should be explained.

As with resistors, choice must be made according to capacitive value, tolerance, working voltage, peak voltage, temperature variation and in some special cases, frequency characteristics. For variable components, especially presets, the range of variation and its law must be taken into account.
Negative temperature coefficient components are widely used nowadays. There are many ways of




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stabilising tumed circuits but undoubtedly one of the easiest is to counter the drift due to warming up of the receiver by alteration to the tuning itself. This is done by the inclusion of a capacitor whose value decreases as the temperature increases. Important practical point here is, of course, to ensure that replacement shall always be with the same type.
Standard tubular capacitors are generally ceramic but there are variations such as the high voltage varicaps, made with barrier dielectric techniques, used widely with transistorised circuitry. These are junction-diodes chosen to take advantage of the capacitance effect: they will concern us later.
Variable capacitors may be the simple compression types found atop the small sealed ganged tuning capacitors in modern transistorised radios, or larger, more precise versions with fine thread screws and several interleaved layers of dielectric. Beehive capacitors, with concentric barrels and a coarse thread, are often found in older sets.


A small pot-core inductor, used here as the tuned circuit of the frequency-changer stage.

Electrolytics have an additional factor in their leakage current. In power supply circuits, where electrolytics are used to filter alternating currents from a supply that should be essentially d.c., we often come across the device of an additional, smaller, decoupling component across the main decoupler. This is to bypass the higher frequency currents that may be present in the ripple current.
Ripple current, in power supply circuits, is an important factor. It bears a direct relationship to the direct current drawn by the equipment, the load. For full-wave rectification, ripple current is about $1^{1}{ }_{2}$ times the d.c., but a half wave circuit needs a reservoir capacitor in its filter circuit with a ripple current rating of three times the d.c.-a point to be watched when making replacements.

Excessive ripple current will cause overheating -application of "raw a.c." across an electrolytic can cause a spectacular but dangerous explosion. A point to be watched is the relationship of frequency and capacity. If high frequency ripple is present, the impedance of the capacitor, which may have been sufficiently low at its filter frequencies, rises dramatically and the heating effect increases.
The inductive element of electrolytic capacitors may have to be taken into account. This also will be mentioned later, when we come to practical circuitry.

Polyester capacitors are being increasingly used in radio work because their method of construction decreases the inductive element. The tantalum capacitor, with some special virtues and few drawbacks except cost, has been used in many circuits, its advantage being a relatively large capacitance (albeit at low working voltage) for small physical size.

## INDUCTORS

Inductors will be found in all sorts of applications, from the small ferrite beads with a single turn of wire around them to the multi-layer, tapped transformer of the modern stereo radio receiver. From the servicing point of view, inductance is either there or not-one seldom has to make up inductors, and we shall not waste space by talking about the factors determining inductance, permeability and so on. Instead, let's concentrate on the practical aspect of core variation, and the ways to overcome core breakage.

Iron dust cores are the usual way to change inductance of coils, these being threaded into the coil former. The individual particles of iron dust are insulated from each other, although closely packed, affording low loss and high permeability and so a miniaturisation of the whole inductor. But, for this reason, the cores themselves are more fragile.

It is not uncommon for wireless workshops to hold in stock large quantities of replacement iron dust cores. Instead of wasting time fiddling-often ineffec-tually-with painted, varnished, waxed or lacquered cores which crumble when torsional pressure is applied, the technique is to shatter the core, carefully remove the bits and clean the thread with a metal runner (of the same thread pitch), finally inserting a new core and aligning.


Interstage transformers $A$ and $B$ of a small transistor radio, with transistors between them wired directly into the circuit. Also to be seen are vertically mounted electrolytic capacitors and screened tuned circuits.

## OTHER CIRCUIT ELEMENTS

A mention will have to be made of the alternative to the conventional inductor, the ceramic filter. The tuned circuit resonates at a frequency to which the crystal (usually a man-made crystal, a ceramic) is carefully cut and shaped. The actual arrangement is not straightforward as a simple crystal so used would have far too sharp a tuning response.

A pass-band of 180 kHz is needed for the handling of the 15 kHz audio signals at low distortion which we now require from our f.m. receivers. So two ceramic elements are used, with bandpass coupling. This gives the required bandwidth but retains the advantage of a sharp "skirt" at the extremes of the filter response curve.

Later we shall consider integrated circuits which are revolutionising receiver design in the same way as the innovation of transistors did some time ago. Also the use of various special semiconductors must be discussed. Field effect transistors (f.e.t.'s) have brought new opportunities to circuit designers, especially in the input circuits of v.h.f. receivers as well as to tape recording circuitry.

## THERMIONIC VALVES

Valves are on the way out-thus runs the creed of some authorities. So they may well be, for there is little in the domestic field that is done by thermionic devices that can not be done as well or better by semiconductors. For a while, the barriers of high power meant that valves were still needed for certain applications. Now, with the improved silicon semiconductors available, even this barrier has broken down and the only remaining market for domestic valved circuitry appears to be in some television receivers, although a number of these are already fully transistorised.

But from the servicing aspect, valves are still very much with us. Not only do we need to know what they will do and how the circuits work but also what substitutes are available. Such information is not always convenient to come by-the best method of determining replacement suitability, of both valves and transistors, is a study of the relevant parameters.

Taking a simple case-nevertheless, not an uncommon case, for the triode amplifier stage is very often met with, especially in the low-signal sections of tape recorders-we have to consider first the
operating conditions, i.e., heater voltage and current, circuit suitability, etc., and after that we can look at the Ia/Va curves, the Ia/Vg curves and the mutual conductance.

For any particular anode voltage there will be a curve which slopes up and then tails off when the anode current increases to and beyond a certain point, for a given grid voltage. There is a cut-off point where negative grid volts reduce anode current to zero and a saturation point where further positive grid volts cannot affect anode current. If we know the valve bias, cathode or grid, we can work out whether our alternative will do what we want.

If there is any further doubt, we can tackle the mutual conductance curves and the a.c. resistance. Amplification factor can be obtained from the results we already have, thus from the various factors already at our disposal we should be able to build up as good a picture about the valve we have as we are likely to need. Nine times out of ten we shall not need it: we shall be able to turn up our tables, select a replacement and go ahead. The tenth time could baffle us and this extra little bit of knowledge could save pounds.

## SEMICONDUCTORS

Semiconductors can nowadays be divided into three sections: diodes, bipolar devices and others (which includes f.e.t.'s etc.). We are concerned with diodes very much indeed, as we shall see; there are plain rectifiers, diodes used as blocking devices, diodes used as circuit guide lines and finally variable capacitance diodes which can play an important part in the tuning of circuits.

The bipolar transistor (so called because it has two types of current carrier) has a few fundamental parameters that will enable us more easily to identify it and choose a possible substitute. Understanding of these parameters will also help us in the solution of some teasing circuit faults.


The laivg curves of valves tell us a lot about their characteristics. Three curves shown are plotted at different anode voltages. By comparing anode current change with grid voltage change causing it, we obtain the mutual conductance, gm, in mA/volt. Comparing curves we get the amplification factor, $\mu$.


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The stated parameters will always depend on operating temperature, a typical mean figure being $25^{\circ} \mathrm{C}$. If the operating conditions vary, it is important that the parameters be corrected accordingly, but this is not generally the province of the chap who is doing the repairs.


Fig. 1; Common-emitter PNP amplifier stage with arrows indicating "hole" conduction. Base voltage is stabilised by R1 and R2 with additional blas provided by R3.

It is to be assumed that the designer has done his homework. Table 1 gives the more important things we need to know about a transistor and a specimen set of figures for a general purpose n.p.n. silicon transistor has been quoted, to show the way these figures are expressed.
As an example of the use of these terms, Fig. 1 shows a p.n.p. transistor in common-emitter mode, as would be used for a simple amplifier. In this mode, we need to know the ratio of change of collector current for a change in base current, i.e., the current gain, $\beta$ or $\alpha_{0}{ }^{\prime}$ (beta or alpha nought dash). The subscript nought means that the current gain applies to d.c., the dash indicates the signal input is applied to the base. A plain $\alpha$ (alpha), without the dash is the symbol for current transfer ratio, and we usually see this written in a statement showing increase, this $\Delta \alpha$ or $\delta \alpha$.
The relationship between alpha and alpha-dash is important, and the formula

$$
\alpha^{\prime}=\frac{\alpha}{(1-\alpha)}
$$

will be encountered. In Fig. 1 we see the various currents and voltages outlined with the arrows denoting hole conduction.


Fig. 2: A load-line drawn on the output characteristic curve of the transistor in Fig. 1. This depends on supply voltage Vs and value of $R^{\prime}$. Chain-dotted line is power limitation and VT the working voltage.

TABLE 1


Characteristic curves. From what we already know, we can draw up a similar family of curves to those we used for valves. Fig. 2 shows just such a series of curves used to determine the static collector current for various output characteristic curves. Values in the simple diagram we saw before can be calculated from this load-line graph, thus:

At cut-off, $\mathrm{V}_{\mathrm{oe}}=$ supply voltage.
At maximum current, all the voltage is dropped across $R^{\prime}$ and maximum current is $V_{\text {supply }} / R^{\prime}$. If we choose a suitable voltage, call it VT for the collector, the base and collector currents can be determined from the load-line.

Volts drop across $R^{\prime}$ is $I_{0} \times R^{\prime}$. Value of

$$
\mathrm{R} 3=\mathrm{V}_{\mathrm{s}}-\left[\left(\mathrm{I}_{\mathrm{c}} \times \mathrm{R}^{\prime}\right)+\mathrm{VT} .\right]
$$

We get the static value of $\mathrm{V}_{\mathrm{be}}$ from the input characteristic and know that the voltage drop across $\mathrm{R} 2=$ drop across R 3 minus $\mathrm{V}_{\text {be }}$.

Then $V_{R 2}=\left[R 3 \times\left(I_{c}+I_{b}\right)\right]-V_{b e}$
If we now choose a suitable value of $\mathrm{I}_{\mathrm{L}}$ we get the value of R2, thus:

$$
\frac{\left[\mathrm{R} 3 \times\left(\mathrm{I}_{\mathrm{c}}+\mathrm{l}_{\mathrm{b}}\right)\right]-\mathrm{V}_{\mathrm{be}}}{\mathrm{I}_{\mathrm{L}}}
$$

and the voltage across R1 is the difference between $\mathrm{V}_{\mathrm{s}}$ and $\mathrm{V}_{\mathrm{R} 2}$, or as calculated from the value of $\mathrm{I}_{\mathrm{b}}$ (Ohms Law) taken from the load-line.

Dynamic considerations differ and the conditions for different kinds of transistor differ. These we shall tackle as they arise. The foregoing has been intended as an example-a way of laying the ground for Mr. King to launch into servicing techniques and circuitry without having to waste his time explaining every detail as he goes along.

END OF PART ONE

## THE <br> MW COLUMN



THE proposal to start local commercial radio on the medium waves has focused attention on two international common frequencies1484 kHz and 1594 kHz . Many low power stations in Europe and parts of Africa occupy these channels, the only restriction being that there should not be interference between them. The BBC uses both frequencies for 2 kW relays, so DXing on these channels will, in some parts of the country be limited to times when these locals are off the air. Manx Radio is on 1594 kHz from sunset until 2015 hrs while BBC3 broadcasts from Bournemouth and Dundee until 2230hrs. Look for CSB4 Emissoras Associadas de Lisboa; the US Air Force station in Athens; Marrakesh in Morocco and possibly Nova Lisboa in Angola; all on 1594 kHz . The other channel- 1484 kHz -is more popular and is used by BBC4 in Kent, Lancashire and Norfolk; BBC2 in Scotland and BBCI in Bournemouth. During the summer, the USAF base at Kenitra in Morocco has been heard on 1484 on several occasions while the USN 250-watter at Keflavik, Iceland, has also been logged. Radio Gibraltar is on this channel from 0655 hrs to 2300 hrs but has so far eluded the writer. Others to search for on 1484 are CSB90 in Funchal Maderia; Volos, a regional station in Greece; Riga in Latvia; Limassol in Cyprus; Ankara Turkey; Jeddah in Saudia Arabia.
A recent note by David Gibson referred lightheartedly to a DXer using the PW medium wave loop on the 10 m amateur band. A MW loop will not, of course, function properly on 30 MHz but it is quite easy to modify one to cover the Top Band. Remove one turn from the main winding; the range will now extend to 2 MHz and the loop can be used for nulling-out Loran or other QRM. Useful results can be obtained in daylight with a modified MW loop to 3 MHz but as frequency increases the directional properties gradually disappear.

As winter approaches in the southern hemisphere Latin Americans become prominent and can be heard in Europe from midnight until daybreak. Two high power stations in Buenos Aires Argentina are nearly always audible; LR1 1070 kHz and LR3 950 kHz . They are commercially owned and identify frequently between jingles. LR3 has the call Radio Belgrano and LR1 is Radio el Mundo. Others to look for include LR4 910 kHz Radio Splendid Buenos Aires; LT2 1230 kHz R. Splendid Rosario; LS6 1350 kHz R. America Buenos Aires. From nearby Montevideo in Uruguay CX14 Radio Espectador is on 810 kHz ; CX28 R. Imparcial is on 1090 kHz and CX16 850 kHz has the unusual identification 'Radio Carve.' Venezuela is on a direct sea path across the Atlantic and can be logged on all parts of the band. Listen for YVLH 650 kHz Radio Giradot in Maracay; YVKS 750 kHz Radio Caracas; YVNM 1000 kHz R. Mil in Moron; YVRS 1020 kHz R. Margarita La Asuncion; YVQJ 1080 kHz R. Barcelona; YVQT 1110 kHz R. Carupano; YVOZ 1200 kHz R. Tiempo Caracas; YVOH 1230 kHz R. Valera.

CHARLES MOLLOY


Solid-state devices are slowly but surely advancing in areas which were previously held by the valve. But there are some applications where transistors find it hard to compete. This is highlighted in places where high power coupled with high frequency are required. To produce kilowatts at microwave frequencies is still the prerogative of the valve.

An application which illustrates this is that of cooking. Microwave ovens are becoming a reality as various types of sustenance are bronzed to culinary perfection by very high frequency energy.

Strange things happen when one uses radar-type frequencies to cook. An egg, for example, can be "boiled" by placing it in the oven and setting the timer for some 25 seconds. Thirty-five seconds will supply the article hard-boiled. Funny thing is that at around the 45 second mark the egg goes off with a bang. This is because the microwave energy concentrates at the centre of the unfortunate egg.
Small tea cakes, made from a proprietary brand of cake mix, take barely 35 seconds to cook and it is amusing to watch a lifeless paper cup full of gooey cake mix suddenly spring into life and fill the container. The weekend joint is reckoned to take around the eight-minute mark. No washing up of pots if you put the food on a paper container.

Digital techniques are still gaining popularity in electronic circles. More and more voltmeters and multimeters are boasting a digital readout. But the readouts are now commonly becoming available by themselves and there is an increasing number of modules being launched. These usually take the form of a small oblong package which houses a number of readout devices and often all the necessary logic circuitry for driving the solid-state readouts themselves. The whole package is offered as a single unit which can be fitted on to a front panel. Thus instead of fitting a meter, it is now possible to fit a solid state direct digital readout device. One of the advantages of direct readout is that parallax is avoided-the difference in absolute reading which is dependant upon whether the eye is directly over the needle of a conventional meter or slightly to one side.

Perhaps the most advanced digital meter available is one which automatically checks its own accuracy against a standard cell between readings. The circuitry switches from the measurement at the probes to the standard cell and back again. It does this repetitively and any slight difference between the standard cell and what the meter should read is immediately corrected by a fast-acting feedback loop.

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retractable chrome plated Telescopic aerial for Short Waves for maximum perfor
$\begin{aligned} & \text { mance. Push pull output using } 600 \mathrm{~mW} \text { trankistors. Socket for car aerial. Tape record } \\ & \text { socket. Selectivity switch, Switched earpiece socket cornplete with earpiece for private listen- }\end{aligned}$
ing. Eight transistors plus 3 diodes. Famous make 7in. $x$ 4in. Speaker. Air spaced ganged tuning
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volume coantrol fine tone moving coil speakier. volume coatrol, fine tone moving coil speaker.
Easy buid plans and parts price list 8p ${ }_{\text {EFREE widith parts). }}$
Earpiece with plug and switched socket for private listening 20 pextra


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| 1A7GT |  | 25U4GT | . 57 | DL92 |  | EL500 |  | PCL83 | -60 | BC41 | . 52 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1H5GT | $\cdot 36$ | 30 Cl | . 30 | DL94 | . 37 | EM80 | . 41 | PCL84 | . 37 | UBF80 |  |
| 1N5C | . 38 | 30 Cl 5 | -63 | DL96 | $\cdot 36$ | EM81 | . 41 | PCL85 | -45 | UBF89 | - 83 |
| 1 R 5 | -28 | 30 Cl 7 | -80 | DY86 | . 28 | EM84 | $\cdot 38$ | PCL86 | - 41 | UCC84 | -35 |
| 1s5 | . 21 | 30 Cl 8 | . 67 | DY87 | . 28 | EM87 | $\cdot 37$ | PCL 88 | $\cdot 72$ | UCC8 | -36 |
| 1 T 4 | . 16 | 30F5 | . 76 | Eabc80 | . 32 | EY51 | -38 | PCL800 | -77 | UCF80 | . 36 |
| 384 | -28 | $30 \mathrm{FL1}$ | -68 | EAF42 | . 50 | Ex86 | -32 | PENA4 | - 42 | UCH4 | -62 |
| 3 V 4 | $\cdot 87$ | 30FL12 | $\cdot 72$ | EB91 | $\cdot 11$ | EZ40 | -43 | PEN360 | $\cdot 70$ | UCH8 | -32 |
| $5 \mathrm{Y3G}$ | . 30 | $30 \mathrm{FLI4}$ | . 72 | EbC33 | . 40 | FZZ41 | -43 | PFL200 | -58 | UCL8 | . 35 |
| 5Z4G | $\cdot 37$ | 30L1 | -32 | ERC41 | -52 | Ez80 | -23 | PL36 | -48 | OCL8 | - 55 |
| 6/30L2 | . 58 | 30 L 15 | -62 | EBC90 | . 22 | Ez81 | -24 | PL8I | 48 | UF41 | . 62 |
| 6ALS | - 11 | 30 LL 7 | .78 | EBF80 | -33 | Gz32 | -43 | PL81 | -51 | UF89 | -38 |
| 6am6 | -13 | 30P4 | -85 | EBF89 | . 31 | GZ34 | -48 | PL82 | - 32 | UL41 | . 60 |
| 8 825 | -28 | 30 Pl 2 | . 77 | ECC81 | . 18 | KT41 | .77 | PL83 | . 35 | UL44 | .00 |
| 6AT6 | . 22 | 30 P 19 | . 65 | ${ }^{\text {ECC82 }}$ | . 23 | KT61 | . 48 | PL8 ${ }^{\text {d }}$ | -33 | UL84 | . 35 |
| 6AU0 | -28 | 30PLI | . 68 | ECC83 | -35 | KT60 | . 83 | PL500 | -65 | TM8 | -25 |
| 6 Ba 6 | ,22 | 30 PL 13 | . 88 | \#CC85 | . 28 | LN319 | -63 | PL504 | $\cdot 67$ | UM8 | . 22 |
| 6BE6 | -23 | 30PL14 | . 70 | ECC80 | . 80 | LN329 | $\cdot 72$ | PL508 | 81.17 | UY41 | 41 |
| 6BJ6 | 42 | 30PL15 | -62 | ECF80 | $\cdot 30$ | LN33 | -63 | PM84 | $\cdot 37$ | VY85 | 28 |
| 6BW7 | -60 | 35L6GT | . 43 | ECF82 | . 30 | N78 | -87 | PX25 | 21.17 | VP4B | .77 |
| 6CD6G | 1.10 | 35W4 | .24 | ECH35 | . 30 | P61 | -50 | PY32 | - 55 | W119 | . 35 |
| $6 \mathrm{~F}_{14}$ | . 45 | $35 \mathrm{Z4G}$ | . 25 | ECE42 | . 88 | PABC | -35 | PY33 | $\cdot 55$ | Z77 | . 22 |
| 6 F 23 | .78 | 807 | - 45 | ECH81 | . 28 | PC86 | -51 | PY81 | -26 | Trans |  |
| $6 \mathrm{FP25}$ | -62 | 6063 | .62 | ECE8 ${ }^{\text {a }}$ | . 41 | PC88 | -51 | PY82 | -26 | AC107 | -17 |
| 6K7G | . 12 | AC/VP2 | $\cdot 77$ | ECH84 | . 37 | PC96 | -42 | PY8 | -28 | AC127 | 18 |
| 6K8G | $\cdot 17$ | AZ31 | . 47 | ECL80 | . 35 | PC97 | . 40 | PY88 | $\cdot 34$ | AD140 | $\cdot 37$ |
| 6sL7a | . 27 | B349 | . 65 | ECL82 | 33 | PC90 | -37 | PY800 | $-37$ | AF115 | 20 |
| 6 V 6 G | . 17 | ${ }^{\text {B729 }}$ | -62 | ECL86 | . 40 | PCC84 | -32 | PY80 | - 37 | AF116 | -20 |
| 6VgGT | . 32 | CCH3 | . 67 | EF39 | . 23 | PCC85 | $\cdot 30$ | R19 | . 38 | AF117 | 0 |
| $6 \times 4$ | . 23 | $\mathrm{CLS3}^{\text {CY3 }}$ | . 02 | EF41 | . 58 | PCC88 | -45 | R20 | . 65 | AF118 | . 48 |
| $6 \times 5 \mathrm{~T}$ | . 28 | CY31 | . 38 | EF80 | 24 | PCC89 | -47 | -25 | . 68 | AF125 | 17 |
| 10 Fl 8 | . 35 | DAC32 | . 36 | EF85 | . 31 | PCC189 | . 51 | U26 | . 65 | AF127 | -17 |
| $10 \mathrm{P13}$ | -60 | DaF91 | . 21 | EF86 | $\cdot 31$ | PCC805 | . 65 | V47 | -68 | OC26 | 25 |
| 12AH8 82 | 2.25 | DAF96 | . 36 | EF89 | . 26 | PCF80 | -30 | U49 | -65 | 0044 | . 12 |
| $12 \mathrm{AT7}$ | . 18 | DF33 | . 38 | EF91 | $\cdot 13$ | PCF82 | -32 | U78 | . 24 | OC45 | 12 |
| $12 \mathrm{AU6}$ | . 28 | DF91 | .18. | EF183 | . 28 | PCF86 | . 47 | U191 | . 62 | OC71 | . 12 |
| 12 AUF | . 23 | DF96 | . 36 | EF184 | . 32 | PCF800 | -67 | U193 | . 42 | - $\mathrm{C}_{7} \mathbf{2}$ | 12 |
| 12 AX 7 | . 23 | DH77 | . 22 | EH90 | . 42 | PCF801 | -33 | U251 | -72 | 0075 | . 12 |
| 19BG6G | .87 | DK32 | -37 | ELs3 | . 48 | PCF802 | . 45 | U301 | . 52 | OC81 | 12 |
| 20 F 2 | -67 | DK91 | . 28 | EL34 | . 47 | PCF805 | -67 | U329 | -72 | OC81D | $\cdot 12$ |
| 20P3 | -85 | DK92 | . 42 | EL41 | . 55 | PCE806 | -60 | U801 | . 98 | OC82 | . 12 |
| 20 P 4 | . 92 | DK96 |  | EL84 | $\cdot 24$ | PCF8 | . 72 | UABC80 | . 32 | OC82D | . 12 |
| 25L6GT | . 25 | DJ | . 25 | - | . 26 | PCL82 | . 38 | UAF4 | . 51 | 0 Cl 70 | . 22 |

## READERS RADIO

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WITH the large numbers of crystals now available at low prices it is not unusual to go into a components shop and find a large box full of assorted crystals being continually churned over by eager hands in search of some peculiar frequency.

While the old 10 X type of crystal can probably stand up to such rough usage the more delicate HC6U type is liable to succumb to such barbaric treatment.
The older "surplus" types can be over 25 years old and although well wrapped and apparently "as new" will often be found to have electrodes that have oxidised making the crystal useless. Having bought such a crystal and got it home it is a little annoying to discover that the wretched thing won't work!
This little crystal checker was designed to slip into the pocket so that it can be used to check almost any type of crystal before it is bought. It has worked with crystals from 100 kHz to over 10 MHz without any trouble.

## Operation

The circuit is very simple but a little different from those usually found in this particular application

insofar as the operation is "fail-safe". That is, the indicator lamp is on when the crystal is not oscillating thus providing a check on the working of the lamp. If the lamp came on only when the crystal was oscillating failure of the lamp to light could be due to either a faulty crystal or dud lamp.
The oscillator circuit itself uses an MPF102 f.e.t. transistor and just four other components plus three crystal holders. The lamp control circuit has a BCl09 silicon transistor which acts as a switch for the lamp circuit.
In the non-oscillating state the MPF102 draws about 10 mA current through resistor R2 which switches the BC109 "on" the lamp circuit being completed through the current limiting resistor R3 to the 9 V supply. In this condition the lamp will light.
With a good crystal plugged in to one of the holders the MPF102 current drops to less than $\operatorname{ImA}$, depending on the activity of the crystal used, the BC109 is switched "off" and the lamp goes out.
Since the lamp draws around 30 mA the unit should not be left switched on longer than is required to check a crystal in order to prevent the early demise of the PP3 battery.

## Constructing the "Companion"

The checker can be built in any small box that will slip into the pocket and may be of metal or plastic or wood. The one used in the prototype is made up of a ${ }^{3} \mathrm{in}$. long section of plastic tube, rectangular in section, $2^{5}$ a $\times 2^{1}{ }_{8}$ in. similar to that used in the construction of the popular Dewbox cabinets. Two Dewbox endcaps provide a handsome finish to the case.

Holes are drilled around the centre section to accommodate the three crystal holders to take 10x, HC6U and FT241/3 crystals so as to make the checker as versatile as possible. The holders are bolted on or fixed with Araldite. A ${ }^{1} 4 \mathrm{in}$. diameter hole is drilled so that the indicator lamp is easily seen.
The simple wiring is mainly direct between components but a short busbar of thin tinned copper wire is run round one corner of the box to act as an "earth" return, one end of which is held under the locknut of the miniature on/off switch. Before doing this check that the dolly of the switch is isolated from the contacts.
After fitting the crystal holders, wire them in parallel, then fit one end cap and lay the PP3 battery



This actual size drawing of the Companion may be compared with the photograph on the previous page.
in position after which the remaining components can be soldered in place.

Because of the small size of this version of the checker a lamp holder was dispensed with and the connections soldered directly to the lamp. If a larger box is used a lampholder should be fitted.

The two transistors are wired into the circuit after everything else has been done. Especial care should be taken with the MPF102 transistor. Holding all three lead-out wires firmly in the jaws of a pair of longnosed pliers the wire ends should be tinned quickly and then soldered into the circuit without releasing the pliers. The BC109 is not so "touchy" but there is no harm in providing a heatsink when soldering it into place using the pliers as before.


## components list



When the checker is completed the end caps can be pushed on leaving enough gap between them to accommodate an HC6U type crystal.

## Checking Out

After double checking the wiring, paying particular attention to the transistor lead out connections, the unit can be switched on. Without a crystal plugged in the indicator lamp should light. Inserting a known good crystal should cause the lamp to go out.

The relative activity of a crystal may be estimated


This view clearly shows the hole for the indicator lamp.
by watching the lamp when the unit is switched on with a crystal in place. With an active crystal the lamp will go out immediately but if the crystal is reluctant to start the lamp will flash momentarily before going out. With a poor crystal the lamp may stay on but dimly.

With a really dud crystal the lamp will come on at full brilliance as if the crystal was not plugged in.

The "Companion" can be used on the workbench as a signal source for alignment purposes using crystals such as 470 kHz or 1.6 MHz for i.f. alignment or 100 kHz or 1 MHz for calibration work. A crystal on say 5 MHz is very useful for calibration on the h.f. bands as well as for alignment.

If the checker is built into a plastic box there should be enough radiation for all the above purposes. If a metal box has been used it may be necessary to plug a short stiff piece of wire into any one of the unused crystal holder sockets to increase the radiation. A miniature telescopic aerial as supplied with some transistor radios is ideal for this purpose.

## practical Wililliss

 No.z

## CROSSWORD COMPETITION

## ALL IN THE

 JUNE ISSUE, ON SALE MAY 7th
## A 5-RANGE RF SIGNAL GENERATOR

This simple signal generator uses an FET in the oscillator which covers 150 kHz to 30 MHz . The audio modulation is separately available for testing of audio amplifiers and circuits. The only power requirement is a 9 volt battery contained within the unit.



THE audio frequency signal generator described here was designed and built to fill the need for a high quality, wide range instrument, capable of permitting accurate and reliable distortion, gain and frequency response measurements to be carried out on a wide range of audio equipment.
For an a.f. generator to be really useful, it must be accurate in respect of frequency and voltage output calibration, and it must maintain this degree of accuracy under widely varying conditions of use.
The initial calibration accuracy will depend on the frequency and voltage standards available at the time of calibration, plus the time and care taken over the calibration process. Also accuracy will be dependent upon the quality of the components used and, to a lesser extent, upon the workmanship involved. The basic design will, of course, also influence both factors.
On the present design, much thought has been expended, plus not a little experimental work, in producing a design that fulfils most adequately all the requirements of a very high quality instrument. Good quality components, used well within their ratings, ensure that initial calibration accuracy will be maintained almost indefinitely. The mechanical design also, has been aimed at producing a robust, easily assembled unit.

## CIRCUIT

The generator is based, in common with virtually all available a.f. generators, upon the well known, and proven Wein Bridge. The three transistors Tri, $\operatorname{Tr} 2$ and $\operatorname{Tr} 3$ form a high gain amplifier with d.c. coupling throughout, with the exceptions of the frequency determining capacitors. This has the twin advantages of being sparing of coupling capacitors, which lessens expense, and relieves the designer of solving unwanted phase shift problems.

The frequency of oscillation is dependent on the setting of VR1 and the capacitors selected by SW1. For oscillation to occur there must be adequate gain and there must be positive feedback, i.e. there must be a phase shift of $360^{\circ}$ between the input and the output of the amplifier. For the Wein Bridge to oscillate, the gain requirement is very modest, being only 10 db or three times. Since the gain of the


Fig. 1 : The circuit of the Hi-Fi Signal Generator, an expla


## $\star$ components list



[^1]

## Capacitors

C1 $100 \mu \mathrm{~F} 15 \mathrm{~V}$ C10 $1000 \mathrm{pF} 1 \%$ +C18 $10 \mu \mathrm{~F} 15 \mathrm{~V}$ C2 $1 \mu \mathrm{~F} 1 \% \mathrm{t} \quad \mathrm{C} 11 \quad 100 \mathrm{pF} 1 \%$ C19 30 $\mu \mathrm{F} 15 \mathrm{~V}$ C3 $0 \cdot 1 \mu \mathrm{~F} 1 \% \mathrm{C} \quad \mathrm{C} 12 \quad 100 \mu \mathrm{~F} 15 \mathrm{~V}$ C20 $47 \mathrm{pF} 1 \%$
C4 $0.01 \mu \mathrm{~F} 1 \% \mathrm{f}$ C13 $100 \mu \mathrm{~F} 15 \mathrm{~V}$ C21 $250 \mu \mathrm{~F} 15 \mathrm{~V}$
$1000 \mathrm{pF} 1 \%+\mathrm{C} 14 \quad 100 \mu \mathrm{~F} 15 \mathrm{~V}$ C22 $100 \mu \mathrm{~F} 15 \mathrm{~V}$
$100 \mathrm{pF} 1 \%$ \& C15 $100 \mu \mathrm{~F} 15 \mathrm{~V}$ C23 1000 F F 25 V C7 $1 \mu \mathrm{~F} 1 \% \mathrm{t}, \quad \mathrm{C} 161000 \mu \mathrm{~F} 10 \mathrm{~V}$ C24 $8 \mu \mathrm{~F} 25 \mathrm{~V}$ C8 $0.1 \mu \mathrm{~F} 1 \%$ t C17 10 $\mu \mathrm{F} 15 \mathrm{~V}$ C25 100 $\mu$ F 50 V C9 $0.01 \mu \mathrm{~F} 1 \% t$
TC1 $3-30 \mathrm{pF}$ Beehive frimmer t see text
Semiconductors

| Tr1 | 2 N 3707 | Tr8 | BC108 |
| :--- | :--- | :--- | :--- |
| Tr2 | 2 N 3702 | Tr9 | 2 N 3053 |
| Tr | $2 N 3707$ | ZD1 | $5.6 \mathrm{~V}, 400 \mathrm{~mW}$ Zener Diode |
| Tr4 | 2N1304 | TH | S.T.C. R53 Thermistor |
| Tr5 | BC108 | BR1 | Bridge Rectifler, silicon |
| Tr6 | BC108 | BY164 or similar |  |
| Tr7 | BC108 |  |  |

## Miscellaneous

SW1 2-pole, 6 -way (only 5 positions used)
SW2 2-pole, 4-way
SW3 Mains on-of
T1 Mains transformer, 240 V pri, $12-0-12 \mathrm{sec}$ (used as $0-24$ ) 0.05 mA , Home Radio Cat. No. TMM13.
Aluminium and perspex for case; Indicator neon; knobs etc.
transistors used is considerably higher than this, no problem exists here. The phase shift requirements are also met, since the trio introduce a phase shift of $180^{\circ}$, and the frequency network introduces a further $180^{\circ}$. Since these phase shifts are effectively in series, the requisite $360^{\circ}$ phase shift is produced.

Stability of the output voltage is important and to this end a thermistor is used. Since it has a negative temperature coefficient, it must be connected in the negative feedback mode. In Fig 1, it is in series with C12 and C14 and controls the a.c. negative feedback from $\operatorname{Tr} 3$ emitter to $\operatorname{Trl}$ emitter. The correct part of its coefficient slope is selected by the value of R8, under which conditions it will hold the output constant to better than $\pm 1 \mathrm{~dB}$.
Although the a.c. gain is controlled by the negative feedback via the thermistor, the d.c. gain is still high. Although the silicon transistors chosen have very stable gain and leakage characteristics, the high overall gain does mean that any change in $\operatorname{Tr} 1$ 's characteristics, and to a lesser extent in Tr2's, will disturb the operating point of $\operatorname{Tr} 3$ to the detriment, if not complete failure, of the complete circuit. D.C. negative feedback via $\mathbf{R 6}$ provides a high degree of stability against any such changes.
In Fig. 1 five pairs of capacitors; C2-C6 and C7-C11, provide five frequency ranges, selected by SWl, with VRI (a and b) providing continuous coverage with some slight overlap at either end. The degree of overlap is dependent on the values of R2 and R9, increasing them decreases the overlap, the converse also applying.
The output voltage from the oscillator is taken from the wiper of VR2, which acts as an infinitely variable control, in conjunction with the decade attenuator which follows later in the circuit. This feeds into an emitter follower, Tr4, which has a high input and low output impedance and effectively isolates the oscillator from any load which may be connected across its output. Tr4 is biased at 10 mA emitter current by R12 and R13, permitting resistive loads as low as $150 \Omega$ to be connected across the output without altering the output voltage by any significant amount.
The coarse attenuator comprises SW2 and range resistors R16 to R28. It is a constant impedance type, with a characteristic impedance of $600 \Omega$, and provides four decade voltage outputs of $1 \mathrm{~V}, 100 \mathrm{mV}, 10 \mathrm{mV}$ and 1 mV . This is somewhat more complex, and requires more resistors than the simple potential divider type of attenuator. It is preferred because of the near constant resistance it offers to the load on its four ranges. The resistance values as calculated are odd but the series connection of the range resistors enables preferred value resistors to be used with very little loss of accuracy. If an accurate a.c. millivoltmeter is available, the series connections enables individual resistors, i.e. R24, R26 or R28, to be changed to enable true decade switching to be achieved. The change in value should not be great; the next preferred value should prove satisfactory.
Although sine wave testing of audio equipment can reveal a great deal of information about it, it does not always tell the full story and needs to be complimented by another wave form.
The most commonly used such waveform is a square wave, and this is produced by the two transistors $\operatorname{Tr} 6$ and $\operatorname{Tr} 7$, with the assistance of $\operatorname{Tr} 5$. Tr 5 is an overdriven amplifying stage, fed with the sine wave via R29 and C17. The output of Tr5 is

partially squared and fed via C18 to Tr6, which in conjunction with Tr7, forms the well known Schmitt Trigger configuration. The component values were chosen for a very fast rise time. TC1 is a "speed up" capacitor, and is used in conjunction with R36, to form a time constant that exactly matches the parallel RC combination of the input impedance of $\operatorname{Tr} 7$ base. When these are equal, the coupling from Tr6 collector to $\operatorname{Tr} 7$ base is truly aperiodic, and extremely rapid rise times result.

The collector load of $\operatorname{Tr} 7$ is a preset resistor, VR4. so that the output of the square wave can be preset to any desired level, up to a maximum of approx 12 V peak-to-peak. The coupling capacitor C21 must be as high in value as possible in order to maintain the tops of low frequency square waves as horizontal as possible.

## POWER SUPPLIES

The question of power supplies will depend on the length of time the equipment is in use. For short, intermittent periods of use, batteries can be used. However, the current consumption of 25 mA at 20 v means four series connected 6 V batteries of reasonably high capacity in conjunction with a 20 V zener diode for stabilisation purposes. Four such batteries will be somewhat bulky, and the use of mains supplies is therefore an attraction. The circuit of the mains voltage power supply used on the prototype is shown in Fig. 2. The transformer used was rated at 50 mA at $12-0-12 \mathrm{~V}$, used as $0-24$. This is then rectified by the bridge BR1 to provide a voltage across the reservoir capacitor C25 of about 30 V . This is then applied to the collector of the series regulator transistor $\operatorname{Tr} 9$, and to R41 which is the collector load of the error amplifier $\operatorname{Tr} 8$, the emitter voltage of which is held at a constant $5 \cdot 6 \mathrm{~V}$ by the zener diode ZD1. The current drawn by ZD1 is about 5 mA .

## COMPONENTS

For optimum performance and maximum longterm reliability, all the components used in the construction of the generator must be of good quality.
The semiconductors used were carefully selected, and should not be changed unless the individual knows what he is doing and why. Whilst comparable semiconductors do exist, their use has not been investigated, and no advice on this score is therefore offered.


Fig. 2: The circuit of the stabilised power supply.


With the availability, freely and cheaply, of high quality $5 \%$ carbon film resistors, there seems little point in using the inferior carbon composition types, unless these are to hand and cost is of paramount importance.

The majority of the electrolytic capacitors used are of the single ended, or P.C.B. type, as these assist in the conservation of space. The only radial ended electrolytics are those combining high capacity with a relatively high working voltage.

The capacitors used in the frequency determining network of the Wein Bridge should preferably be of $1 \%$ tolerance, as this means a single frequency scale can be used on the front panel. It must be admitted that $1 \%$ high value capacitors are somewhat expensive and wider tolerance capacitors can be used in the interests of economy. This then requires either the careful selection of capacitors, or the adoption of

Fig. 3: The component layout and details of the printed circuit board.


Fig. 4: The component layout of the power supply.


The neat construction using a printed circuit board can clearly be seen here.
a multiple frequency dial calibration if accuracy is not to be sacrificed to cost. Readers wishing to use $1 \%$ capacitors can purchase WIMA capacitors, as used on the prototype, from WAYCOM LTD., WORKINGHAM ROAD, BRACKNELL, BERKS.

## CONSTRUCTION

For this type of circuit, a circuit board of some type is almost mandatory. The prototype was built on to an etched circuit board, measuring $9^{1}{ }_{4} \mathrm{in} \times 4^{1} 1_{4} \mathrm{in}$, shown in Fig. 3. The fully completed board is supported behind the front panel, and parallel to it, by means of lin long insulated pillars drilled and tapped 4BA at either end. This allows ${ }^{1} 4$ in 4 BA bolts to be used for securing the circuit board, whilst the perspex and metal panel are secured by ${ }_{2}$ in 4BA bolts.

The power supply is built upon a piece of plain Veroboard, $2^{1}{ }_{4}$ in $\times 3^{3}{ }_{4}$ in shown in Fig. 4 with the component siting.

The supply board is mounted on the rear of the cabinet. That on the prototype was backed by a piece of $1_{16}$ in perspex to preclude any danger of short circuits between the component leads and the cabinet.

The front panel of the instrument was made of white card which is clamped to the front of the cabinet behind a protecting piece of $1_{16 i n}$ perspex.

The cabinet for the prototype was made from 20s.w.g. aluminium to the sizes in Fig. 5. The easiest way of ensuring that the circuit board, cabinet front and perspex all line up accurately, essential if the control spindles are to pass without fouling through the front panels, is to make up the cabinet first. Then the circuit board and perspex are cut slightly smaller
so that they drop into the recess behind the front panel, formed by the top, bottom, and sides. The required holes are then scribed through, using the metal front panel as a template, and carefully drilled out. The holes for the controls in the circuit board will need to be of $3_{8}$ in diameter, the corresponding holes in the front panel can be ${ }^{1}{ }_{4}$ in if accuracy in alignment is achieved. The holes for the output terminals will depend on the components actually used.


Fig. 5: The details of the case.

## SETTING UP

After completing both circuit boards, they should be carefully inspected for soldering and for wiring errors. Then the power supply can be connected to the mains, its output disconnected from the generator board. The output should be monitored and either R39 or R40 altered if necessary to set the output voltage at 20 V . The generator board can then be connected and further tests made. A meter capable of reading up to 25 mA should be connected in series with one of the supply leads; a reading $\pm 10 \%$ of this should be obtained. The meter can then be removed from circuit. Voltage tests using a $20 \mathrm{~K} \Omega / \mathrm{V}$ meter should provide readings substantially in agreement with those given in Fig. 1.

In order to ensure that the generator is correctly 'calibrated in respect of frequency and voltage, an accurate, wide range oscilloscope and a.c. millivoltmeter are required. Another a.f. generator of known accuracy is a useful aid, but is not indispensible. It is only really necessary if wide tolerance capacitors are used in the frequency network.
The oscilloscope and meter should be connected to the sine wave output, and a check made for oscillation throughout all ranges. The sine wave should "look good"; however a visual check for distortion does not reveal it unless it is really severe. Should this prove to be the case, transistor "spreads" may be responsible, in which a change in Trl bias effected by changing R1 or R3 may help. If it is due to a thermistor "spread," variation in R8 may help.


Components should not be varied unless really necessary, and even then variations should be in small steps.

If all seems well, attention can be turned to frequency calibration. Here two courses are possible. If $1 \%$ capacitors are used for C2-C6 and C7-C11, one frequency scale will suffice. If wide tolerance capacitors are used, a different scale for each range will be necessary, unless some accuracy can be sacrified in the interest of simplification and one scale. Another a.f. generator will be necessary if different frequency scales are to be provided. The use of Lissajous figures for frequency calibration is well known and need not be repeated here.

Lissajous figures are used, using the mains as a frequency standard. VR1 is used on Range 1, and points plotted at $15 \mathrm{~Hz}, 16 \cdot 6 \mathrm{~Hz}, 20 \mathrm{~Hz}, 25 \mathrm{~Hz}, 30 \mathrm{~Hz}$, $35 \mathrm{~Hz}, 40 \mathrm{~Hz}, 50 \mathrm{~Hz}, 75 \mathrm{~Hz}, 100 \mathrm{~Hz}$ and 150 Hz . Range 2 will be these frequencies x10, Range 3 will be x100 and so on.

The next step is to set the output voltage. VR2 should be at maximum, with SW2 on the 1V position. Using a frequency of 1 kHz , VR3 is set to give a reading on the meter of precisely IV. SW2 is then set at 100 mV , and the output checked, similarly at 10 mV and 1 mV , if the meter will read as low as this R24, R26 and R28 can then be changed if necessary.

The frequency response can then be checked if required, and should be constant to $\pm 1 \mathrm{db}$ from 15 Hz to 150 kHz , falling to $-2 \cdot 5 \mathrm{db}$ at $1 \cdot 5 \mathrm{MHz}$.

For setting the Schmitt trigger, the ideal 'scope would be a d.c. coupled one, with the h.f. response extending to 10 MHz or higher. On an a.c. coupled 'scope, considerable sloping of the tops of the low frequency square waves can be expected.

Similarly, unless the 'scope has a first class h.f. response, rounding off the shoulders of the leading edges of the square waves can be expected at high frequencies. The measured rise time of the prototype square wave at 1 kHz was 250 nS (nanoseconds).

The effect of TCI is only apparent at the higher frequencies, where it should be adjusted so that the shoulders of the leading edges of the square waves have neither "overshoot" or "sag."

VR4 can be adjusted to provide a square wave output of up to 12 V peak-to-peak. Designing an attenuator that does not degrade a fast square wave is not too easy and was not attempted.

The mark-space ratio should be one-to-one, and is dependent upon $\operatorname{Tr} 5$ providing a symmetrical output to the trigger. Any variation of this ratio from the required $1: 1$ can be corrected by variation in the value of R29.


## MONTHLY

## NEWS FOR

 DX LISTENERS UE to the postal dispute no reports have reached me in time for inclusion in this issue. The following news items were obtained from Radio Sweden's DX programme: 'Sweden Calling DXers' and from my own log.GERMANY. DRM23, Radio Bremen on 6190 kHz has announced that it plans to increase its power from the present 10 kW in the near future.

GUATEMALA. Radio Cultural has been reported at 1205 on 9505 kHz with a strong signal.

NEW CALEDONIA. Radio Noumea is reported to be using the new frequency of 9510 kHz . The times of the broadcasts are $0600-1100$ and 2330-0200, the language used is French.

NORWAY. Radio Norway now broadcasts a DX programme called 'DX Radio Norway' on the first Sunday of every month. The first programme was scheduled to be broadcast on March 7th. The programmes are transmitted at 0800, 1000 and at twohourly intervals throughout the day. Radio Norway has also reported that it hopes to have transmitters with power in the region of 500 to 1000 kW in operation before the end of 1974.

PERU. Radio Nacional, Lima, Peru, has been heard broadcasting at 0300 on a frequency of 6082 kHz . The programme consisted of Peruvian music.

## Choosing a receiver

Since I started writing this column I have had many queries from readers, the most common being about the choice of equipment. In the following paragraphs I list the most important features for a DXer's receiver. Each DXer requires a slightly different receiver and the following is my own order of importance.

An adequate short-wave range. Before purchasing a receiver the listener should decide which bands he is interested in. Some listeners may require coverage of the 49 m to 13 m bands only, whereas others may have a special interest in the tropical bands ( 120 to 60 metres). Most listeners will probably settle for a general-coverage receiver $(540 \mathrm{kHz}$ to 32 MHz ).

An external aerial connection. This is a very important point which can easily be overlooked. No short-wave receiver can give DX performance unless a good aerial is used.

Bandspread frequency control. With the present crowded state of the bands it is essential to have a receiver with this feature to enable adjacent stations to be separated. The receiver should also have a logging scale so that the setting can be noted and returned to at a later date.

Adequate selectivity. Selectivity is a measure of

# THE BROADCAST BANDS Malcolm Connah Frequencies in kHz - Times in GMT 

the ability of the receiver to separate two adjacent stations. Some receivers have a variable selectivity control and this can be very useful.

Adequate sensitivity. Sensitivity is a measure of the receiver's ability to pick-up and amplify weak signals. A DXer's receiver must be sensitive as he is mainly interested in weak signals.

An aerial matching device. Sometimes called an antenna trimmer this very useful control allows the aerial to be correctly matched to the receiver. A very small mis-match can cause a serious loss of signal.

A crystal calibrator. This gives signals at intervals of 100 kHz and is an invaluable aid to determining the exact frequency of any station.

A signal-strength indicator. Usually in the form of a magic-eye indicator or an S-meter. These indicators enable the relative strengths of incoming signals to be determined.

An r.f. gain control. Most receivers have an audio gain control only, the addition of a separate r.f. control can greatly assist in the reception of difficult signals.

An automatic gain control switch. All receivers incorporate some form of automatic gain control which adjusts the gain of the receiver to compensate for sudden fluctuations in the input signal. The a.g.c. switch enables the circuit to be disconnected, with the circuit out of action weak signals çan be greatly amplified.

A noise limiter. Sensitive receivers are susceptible to noise interference. The noise limiter clips the tops of the noise signals and stops them from reaching the output of the receiver.
I hope that the above paragraphs have been of interest to those of you who are thinking of buying a receiver, I look forward to receiving reports from you in the near future.

All reports please to me at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex, by the 15 th of the month.

F
1971 WORLD RADIO-TV HANDBOOK
Published by Billboard A.G. and available from Fountain Press, 46 Chancery Lane, London, W.C.2. $\mathbf{3 7 2}$ pages, $9 \times 6$ in. Price $\mathbf{2} \mathbf{2} \mathbf{3 0}$ OR those not familiar with this publication it lists virtually every radio and television station in the world and provides all the information you are ever likely to need for DXing-in fact I don't know of a short wave listener who doesn't regard it as a sort of "bible".

Every year we look forward to the new edition and we have not been disappointed with this one. The introductory articles that used to take up the first part have been dropped and published separately for the first time under the title "How to Listen 1971".

We could hardly do without it at the P.W. offices and we are sure you will be in the same position if you are interested in any form of DXing.-H.W.M.
 ACH month, letters arrive which raise various queries. Some contain the usual questions which crop up again and again, others are peculiar to a person or piece of equipment. Over the years numerous questions have been answered but it seems obvious that more and more newcomers are reading this page and are, therefore, repeating the same questions which others before them raised. So for once, let's have a session of answers to some of the problems which have arrived over a period of months.

First query is usually a "By the way" enquiry and asks what gear does G3JDG use and on what bands can emission from your scribe be detected. Gear permits 120 W of a.m./c.w. from $3 \cdot 5 \mathrm{MHz}$ to 30 MHz and 10 W on topband. Main interests are the h.f. DX bands and an unashamed preference for c.w. Phone is used on topband and then, usually, mobile. The receiver is a valve type with r.f., mixer, two i.f., det. and one audio plus b.f.o. and Q-multiplier. An a.t.u. is always used since aerials are a source of much experimentation. Antenna for the past six months has been a solitary slither of wire some 60 ft . long at about 18 ft . Current move into a "new" house should see activity on 14 MHz c.w. and on topband a.m. at first. A modified Pye reporter transceiver allows 18 W on 70 MHz .

Two questions which occur more often than any others. Where can I get a list of callsigns and countries, and what is the "best" aerial to use? A country's list can be obtained from the R.S.G.B., 35 Doughty Street, London, WC1N 2AE, price is $6{ }_{2}$ p Incidentally, those who are not members of the R.S.G.B. might like to send for a free specimen copy of the Society's monthly publication Radio Communication.

The short answer to the question, "What is the best aerial to use", is simply "There is no such animal". An aerial which is excellent for a particular band will not necessarily be any good on another frequency. Again, the particular physical location can affect the performance. Aerials are often largely a matter of suck it and see.

The only aerial which might be considered an "all frequency" affair (speaking now of 1.8 to 30 MHz ) is simply a length of wire as long as possible, as high as possible and as far from earthed objects as possible. The wire is then fed to the receiver via an a.t.u. (aerial tuner unit). This is, in fact, the system in use at G3JDG at the moment. It is essentially a compromise system and there are other set-ups which could quite easily out-perform it. Aerials, or antennas, are a subject in themselves and there are numerous textbooks which discuss the relative merits of each type to which interested readers are respectfully referred.

A common question from newcomers is simply where to start, what receiver, etc. If the receiver is to be homebuilt, then much will depend upon individual skills in construction. For the absolute beginner it might be easier to purchase a simple kit,

## THE AMATEUR BANDS <br> David Gibson, G3JJG

## Frequencies in kHz - Times in GMT

the only real alternative being to buy a ready-made unit.

Headphones are a must and aerials have already been dealt with as has a country's list. Armed with these basic essentials one is all set to start the initiation of becoming a short wave listener (s.w.l.). Amateur bands to listen on (up to 30 MHz ) are: $1 \cdot 8-2 \cdot 0 \mathrm{MHz} ; 3 \cdot 5-4 \cdot 0 \mathrm{MHz} ; 7 \cdot 0-7 \cdot 1 \mathrm{MHz} ; 14 \cdot 0-$ $14 \cdot 35 \mathrm{MHz} ; 21 \cdot 0-21 \cdot 45 \mathrm{MHz} ; 28 \cdot 0-29 \cdot 7 \mathrm{MHz}$.

A good wall map of the world is useful and a packet of coloured drawing pins will permit stations logged to be located on the map. Incidentally, this procedure, besides adding interest, will also provide a surprisingly good working knowledge of geography over a short period of time.

A point which often appears to baffle the beginner is the disappearance of signals from a particular band or bands. There are many causes of fluctation in communications. For example, the height of the ionised layers above the earth which reflect the radio waves back has a marked affect. Again, the activity of the sun plays an important role as does the season or time of year. As an example, at the time of writing, the 14 MHz or twenty metre band is mainly active from around 0700 to 2200 hrs although some signals might be heard occasionally outside these times. The 21 MHz band is mainly active between 0700 and 2000 hrs while up on 28 MHz the signals are in evidence between 0800 and 1800 hrs .

Another favourite query is how to get a transmitting licence and what is involved. The licencing body in the U.K. is the Post Office. In order to obtain a licence the Post Office need to be satisfied of a persons technical competence to operate transmitting equipment.

There are two types of licence. For a full "A" licence, which permits the holder to transmit on all amateur bands from $1 \cdot 8 \mathrm{MHz}$ upwards, it is necessary to pass a written technical examination. The other test is that the candidate is required to send and receive Morse at the rate of 12 words per minute. A pass in the technical paper is essential for either licence.

If the Morse test is not taken it is still possible to obtain a licence but in this case transmission is restricted to the amateur frequencies from 144 MHz (two meters) and higher. Thus all the h.f. DX band would be "out of bounds" as regards transmission. This licence is called a " $B$ " licence and holders are distinguishable by a callsign which begins "G8" followed by three letters. Some holders of full licences have a G8 callsign but these are followed by only two letters. Note that in Scotland callsigns begin "GM" and in Wales with "GW". GI (Northern Ireland), GC (Channel Islands), GD (Isle of Man). Thus a G8 licence issued to a Scottish amateur would begin GM8, etc.

[^2] general constructional details and the circuits etc. for castanets, cymbal, snare drum, triangle, woodblock, taxi horn, train whistle and bell chime were given in parts 1 and 2.
The remaining two generator circuits Nos. 9 and 10, are those for a ship's siren and the sound of the sea (surf). Details are also given in this part for the mixer amplifier and power supply etc. However, before going on to these circuits it would be as well to deal with the small modification that must be carried out on the organ key switch assembly.

There are 10 keys on this and when either one is pressed it will stay down until pressed again. This action is facilitated by small phosphorbronze clips, one to each key and the function of each clip is to hold a small brass pin within the key guide frame. The operation of all the circuits 1 to 9 is that they must produce the sound when the key is pressed and instantly released, or pressed and held under pressure, i.e., the keys must behave like a piano key. All that is necessary is to remove the phosphorbronze clips on keys 1 to 9 only and shake or pull out the small brass pins. When the keys are now pressed they will immediately return to normal when pressure is released. Key No. 10 which actuates the sea sound generator (circuit No. 10) must be left to work as intended i.e., when pressed down it must stay down until pressed again. This allows the sea sound to be run continuously without having to hold the key down.

The contact system on each key is simply a pair of single pole changeover switches and one or both can be used for the make and break of each keying circuit. The writer simply paralleled both sets of contacts but used them as a single make/break switch. This will be referred to again later.

Circuit for Ship's Siren-No. 9
This circuit is given in Fig. 22 and employs a phase shift oscillator ( Tr 1 ) operating at a frequency of about 120 Hz and which can be adjusted by variation of R3. The output from Tr1 is attenuated by R8 and fed directly to Tr2 which is biased to cut-off by R16. The noise content for the sound is produced by the noise diode ND1, the output signal from this being slightly attenuated by R11. The sine-wave signal from Tr1 and the noise signal are combined in $\operatorname{Tr} 2$ which is keyed on by key No. 9. The output from $\operatorname{Tr} 2$ is attenuated to a level suitable for the mixer amplifier by R19/R20. The circuit board layout is given in Fig. 23. The circuit should require little or no adjustment except for pitch but the noise content of the sound, which should not be too predominant, can be regulated by variation of R11. Waveforms for this circuit are shown in Fig. 26 (Ship Siren circuit, A and B).


Fig. 23: The component layout for the ship's siren synthesiser.


Fig. 24: The circuit for the 'surf on the beach' sound.

## Surf on the Beach-

No. 10
Surf rolling up on the beach and receding is a fairly slow movement and the sound itself, which is mainly random noise, rises and falls in amplitude at the same rate as the movement of the water. Here we need a slow but sinusoidal rate of change in signal level. The noise diode ND1 provides the white noise but to be effective a slight change of pitch in the noise is needed as well as the amplitude variation.
The noise signal is fed directly to $\operatorname{Tr} 2$ which is rendered almost non-conducting because of the large value resistor ( $1 \cdot 5 \mathrm{M} \Omega$ ) between the base and positive rail. The base is however, directly coupled (via R7) to the collector of the slow running phase shift oscillator Trl. As the potential at $\operatorname{Tr} 1$ collector rises and falls Tr2 will become fully conductive and/or quiescent at the same rate. The noise output signal from Tr2 will rise and fall accordingly. The phase-shift oscillator runs at approximately 1 complete cycle in 10 seconds. The change in pitch of the noise output is produced by feedback via Cl0. In operation, key No. 10 is pressed down and stays down (see above) so that the sound continues until the key is again pressed and released. The sound must not cut off completely as the amplitude falls but simply fall to a low level. Adjustment to the value of R10 ( $1 \cdot 5 \mathrm{M} \Omega$ ) may therefore, be necessary, i.e., the value may have to be reduced to $1 \cdot 2 \mathrm{M} \Omega$ or increased to $1 \cdot 8 \mathrm{M} \Omega$. The sound produced by the circuit is quite realistic but should not be too loud when used as a background effect for desert island type tunes. Note that the key for this circuit (No. 10) is wired so that the key contacts are "on" whilst the circuit is nonoperational. When key No. 10 is closed as shown in the circuit, $\operatorname{Tr} 2$ is biased to cut off. The circuit board layout is shown in Fig. 25 and relevant waveforms in Fig. 26 (Surf on Beach Circuit A and B).

fig. 27 : The power supply circuit.


Fig. 28: The construction of the power supply section which is built on the dividing panel supplied with the case.


Fig. 29 : The circuit of the mixer amplifier. The values of R1-R10 may have to be varied as mentioned in the text.
about $1 \mathrm{k} \Omega$, may therefore require adjustment to value. The total current drawn by the generator circuits (not keyed) and the mixer amplifier should be approximately 20 mA . The layout for the power supply as used on the dividing chassis of the Contil Mod 2 case employed for the prototype unit, is shown in Fig. 28.

## Mixer Amplifier

This is a single stage signal amplifier with input attenuation to reduce the signals from each of the generator circuits to a level appropriate to each of the sounds. The imput attenuation resistors R1 to R10 also serve to prevent impedance loading by each circuit and also signal overloading of the amplifier itself. The values chosen for R1 to R10 may require slight adjustment one way or the other in value so that the levels of the various sounds are relative for any setting of the volume control. The volume control has been provided simply to control the overall output from the unit.

## components list - part three

| Ship Siren Circuit No. 9 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Transistors Tr1, Tr2 |  | BC108 Mullard |  |  |
| Noise Diode <br> NDt Z1J (see part 1) Semitron |  |  |  |  |
| Resistors |  |  |  |  |
| R1 | $12 \mathrm{k} \Omega$ | R8 | $390 \mathrm{k} \Omega$ | R15 |
| R2 | $12 \mathrm{k} \Omega$ | R9 | $100 \mathrm{k} \Omega$ | R16 |
| R3 | $10 \mathrm{k} \Omega$ | R10 | $68 \mathrm{k} \Omega$ | R17 |
| R4 | $12 \mathrm{k} \Omega$ | R11 | $12 \mathrm{k} \Omega$ | R18 |
| R5 | $120 \mathrm{k} \Omega$ | R12 | $12 \mathrm{k} \Omega$ | R19 |
| R6 | $10 \mathrm{k} \Omega$ | R13 | $120 \mathrm{k} \Omega$ | R20 |
| R7 | $2.2 \mathrm{k} \Omega$ | R14 | $4.7 \mathrm{k} \Omega$ | R21 |
| All 1 W, 10\% types |  |  |  |  |
| Capacitors |  |  |  |  |
| C1 | $100 \mu \mathrm{~F}$ |  | C7 | 0.14 F |
| C2 | $0.1 \mu \mathrm{~F}$ |  | C8 | $0.2 \mu \mathrm{~F}$ |
| C3 | $0.1 \mu \mathrm{~F}$ |  | C9 | $25 \mu \mathrm{~F}$ |
| C4 | $0.1 \mu \mathrm{~F}$ |  | C10 | $0.2 \mu \mathrm{~F}$ |
| C5 | $25 \mu \mathrm{~F}$ |  | C11 | $25 \mu \mathrm{~F}$ |
| C6 | $2.5 \mu \mathrm{~F}$ |  | C12 | $2.5 \mu \mathrm{~F}$ |

$0.1 \mu \mathrm{~F}$
$0.2 \mu \mathrm{~F}$
$25 \mu \mathrm{~F}$
$0.2 \mu \mathrm{~F}$
$25 \mu \mathrm{~F}$
$2.5 \mu \mathrm{~F}$

| Mixer Amplifier Transistors Tri, BCiog Mullard |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Resistors |  |  |  |  |  |
| $R 1$ | $56 \mathrm{k} \Omega$ | R7 $100 k \Omega$ |  | R13 | 12k $\Omega$ |
| R2 | $47 \mathrm{k} \Omega$ | R8 | $100 \mathrm{k} \Omega$ | R14 | 10k $\Omega$ |
| R3 | $39 \mathrm{k} \Omega$ | R9 | 100k $\Omega$ | R15 | $5.6 \mathrm{k} \Omega$ |
| R4 | $220 \mathrm{k} \Omega$ | R10 | 39k $\Omega$ | R16 | $1 \mathrm{k} \Omega$ |
| R5 | 82k $\Omega$ | R10 | $100 \mathrm{k} \Omega$ |  |  |
| R6 | 390k $\Omega$ | R12 | $120 \mathrm{k} \Omega$ |  |  |
|  |  | All $\frac{1}{4}$ W | , 10\% types |  |  |
| Capacitors |  |  |  |  |  |
| C1 | 10 $\mu \mathrm{F}$ | $\begin{aligned} & \mathrm{C} 3 \\ & \mathrm{C} 4 \end{aligned}$ | $\begin{aligned} & 250 \mu \mathrm{~F} \\ & 1.5 \mu \mathrm{~F} \end{aligned}$ |  |  |
| C2 | 50 $\mu \mathrm{F}$ |  |  |  |  |

## Power Supply

Transformer TI Pri, 230V., Sec 18-20V (TS/18/2, Henry's Radio)

## Resistor R

Capacitors
Rectifier MR1

1 Watt (see text)
C1 $500 \mu \mathrm{~F} 30 \mathrm{v}$ wkg.
C2 $5000 \mu \mathrm{~F} 25-30 \mathrm{v}$ wkg.
Bridge type LT120 or LT119 (Henry's Radio)

## Miscellaneous

Volume Control VR1 $10 \mathrm{k} \Omega \mathrm{log}$.

Output socket
Mains on/off switch
Jack or Phono type.
Toggle type
230 V mains type


Sea (Surf on Beach) Circuit No. 10

## Transistors

| Tri. | Tr2 | BC108 Mullard |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Noise Diode |  |  |  | J (see part 1) Semitron |
| Resistors |  |  |  |  |
| R1 | 15k $\Omega$ | R7 | $100 \mathrm{k} \Omega$ | R13 |
| R2 | 15k $\Omega$ | R8 | $100 \mathrm{k} \Omega$ | R14 |
| R3 | $15 k \Omega$ | R9 | $68 \mathrm{k} \Omega$ | R15 |
| R4 | $2 \cdot 2 \mathrm{k} \Omega$ | R10 | $1.5 \mathrm{M} \Omega$ | $\Omega$ R16 |
| R5 | 100k $\Omega$ | R11 | $18 \mathrm{k} \Omega$ | R17 |
| R6 | $10 \mathrm{k} \Omega$ | R12 | $2.2 \mathrm{k} \Omega$ |  |
|  |  | All $1 \mathrm{~W}, 10 \%$ types. |  |  |
| Capacitors |  |  |  |  |
| C1 | $50 \mu \mathrm{~F}$ |  | C6 | $0.1 \mu \mathrm{~F}$ |
| C2 | 50 $\mu \mathrm{F}$ |  | C7 | $100 \mu \mathrm{~F}$ |
| C3 | 50 $\mu \mathrm{F}$ |  | C8 | $100 \mu \mathrm{~F}$ |
| C4 | . $5000 \mu \mathrm{~F}$ |  | C9 | $0.047 \mu \mathrm{~F}$ |
| C5 | $0 \cdot 1 \mu \mathrm{~F}$ |  | C10 | 390pF |

BC108 Mullard
Noise Diode
ND1 Z1J (see part 1) Semitron

$$
\begin{aligned}
& 47 \mathrm{k} \Omega \\
& 10 \mathrm{k} \Omega \\
& 10 \mathrm{k} \Omega \\
& 220 \mathrm{k} \Omega \\
& 12 \mathrm{k} \Omega
\end{aligned}
$$




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THE circuit and other technical details of the P.W. oscilloscope were given in part 1. The prototype, as shown in the photographs, was constructed in a Mod-Contil case type $Q$ which has overall dimensions of $13 \times 9 \times 7 \mathrm{in}$. Any case of similar size could be used but the layout of the components should follow that given as closely as possible. Details for the front panel drilling are given in Fig. 2 and these apply of course to the panel of the Mod-Contil type $Q$ case. The general assembly of the two end panels and the chassis and the positions of the c.r.t., the component tagboards and mains transformer are shown in Fig. 3. This layout is important even if a different case is used. The transformer T1 must be situated below and to the rear of the c.r.t. and as close to the end of the chassis as possible as shown in Fig. 4.

## SUB-ASSEMBLIES

These include the main tagboard mounting screen, the panel for the c.r.t. base and the panels for the focus and brilliance controls and the X amplifier gain control. Details for the main tagboard mounting screen are given in Fig. 5 and on this are fitted the miniature tagboards as shown in Fig. 3 with insulating material beneath them to prevent short circuits. The panel and clamp material for the c.r.t. base are shown in Fig. 6 but note the slotted holes in the panel to allow the height of the c.r.t. to be adjusted relative to the front panel. The c.r.t. holder is not mounted on this panel but simply pushed on to the c.r.t. connecting pins.

Details for the focus (VR9) and brilliance (VR8) controls panel are given in Fig. 7b. The panel may be made from perspex or paxolin, $1_{8}{ }_{8}$. thick. Both controls are at high potential with respect to chassis and for this reason must not only be mounted on a panel of insulating material but must also be coupled to the front panel control knobs via insulating spindle
couplers as shown in the photo. The remaining panel is that for the X amplifier gain control VRI as shown in Fig. 7c and which is secured to the side of the chassis as in Fig. 7a. The spindle of this control must be cut very short (to about ${ }_{8}$ in.) and slotted as shown as adjustment is made, when required, by screwdriver. To facilitate this a hole is cut in the side panel exactly in line with the control i.e., on the right when facing the front panel.
The three small tagboards E, F and G are located


Fig. 2: The drilfing of the front panel and location of the controls.

$\begin{array}{ll}\text { Centre dividing screen } 16 \mathrm{sw.g} \text {, aluminium } & \text { Tagboards each side of screen } \\ \text { mounted on } 3,8_{8}^{\prime \prime} \times 3,8_{8}^{\prime} \text { aluminium angle } & \text { mounted with insulating material } \\ \text { between tagboard and screen }\end{array}$ $\rightarrow$


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Fig. 6: The c.r.t. mounting panel and base clamp.


Flo, 7 : Layout of the valve holders and other chassis mounted components and detalls for the brilliance and focus panel and the $X$ amp gain control bracket.
as shown in Figs. 4 and 7 respectively. Tagboard F is mounted on a piece of $3_{8}$ in. aluminium angle and located at the side of the mains transformer T1 (see Fig. 4). This tagboard carries the capacitors C38, C39, C41 and C42 which are fairly large so the board should be 2 in . wide and have at least 6 pairs of tags. Tagboards E and G are mounted on the chassis with spacers or insulating material underneath so that the tag eyelets do not touch the chassis. These boards may be miniature ( $1^{1}{ }_{2} \mathrm{in}$. wide), each with 10 pairs of tags. The location of the valveholders and other chassis mounted components such as C34, C35, C36 and C40, etc., are shown in Fig. 7.

## CONSTRUCTION AND WIRING

These photos show the construction and layout as seen from both sides and above and below the chassis (see also photos in Part 1). The c.r.t. is mounted so that the final anode cap is uppermost as shown in Fig. 8. This will bring the 'key' on the c.r.t. base to the vertical position and ensure that the trace is horizontal when displayed. Fig. 8 also shows the c.r.t. connections. The lead to the final anode cap can be directly soldered to the projecting pin.
The layout for the Y amplifier, the 'timebase and the X amplifier tagboards is shown in Figs. 9 and 10 respectively. The tagboard pairs A and B , and $C$ and $D$ should each be regarded as one long


Cap on crt $=$ Final anode
Fig. 8: C.R.T, base connections. Inset shows $X$ and $Y$ plate alignment in relationship to the final anode cap.


Fig. 11: Wiring of the $X$ and $Y$ shift controls.


Fho. 9 : Component layout for Y amplliers and e.h.t. supply capactiors

board and the components spread out, each accordingly to the space required. For this reason some pairs of tags will not be used but there will be more than enough for all the components. Much the same applies to tagboards $E$ and $G$. The wiring for the $X$ and Y shift controls is given in Fig. 11. Clockwise
movement of the X shift control moves the c.r.t. trace upwards, and clockwise movement of the $Y$ shift control moves the trace to the right and vice versa in both cases.

The only rule as far as wiring is concerned is to keep all wires short as possible and do not take wires


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Fig. 13: The perspex graticule for the c.r.t.
screen.


Two views of the underside of the completed
Oscilloscope are shown below.
Fig. 12: Timebase and flyback suppression wave-
forms.

associated with the timebase and its controls too close to the $Y$ amplifier wiring, that is try to keep the timebase and $Y$ amplifier wiring to the respective sides of the centre screen.

## TESTING AND PERFORMANCE

It is most important that the various potentials as shown on the circuit are obtained but note that the voltmeter used must be at least 20,000 ohms per volt, otherwise the readings obtained will be inaccurate. The measured potentials should be within $3 \%$ of those listed. (Example-for a reading of 600 V the measured potential should be not less than 580 V and not more than 620 V .)

If another oscilloscope is available the timebase waveforms and flyback suppression pulse can be checked quite easily and should appear as in Fig. 12 Failing this, set the timebase range switch to position 1 and the fine control to about midway travel Set the timebase amplitude control to about one third travel and the $X$ and $Y$ shift controls to midway. Set the $Y$ amplitude control to zero. Adjust brilliance and focus to obtain a bright but sharp trace which should be extended fully across the screen. Check that it remains fully extended on all timebase switch positions. Now turn the timebase switch to the 'off' position in which case only the c.r.t. spot should be displayed and this should be completely round and about 1mm, in diameter. Reduce brilliance a little for this test. Check that the spot can be centred on the c.r.t. screen by means of the $X$ and $Y$ shift controls the setting for these being almost exactly midrange.

With either control it should be possible to move the spot up or down, or from left to right, completely off the screen. With the timebase range switch still at the 'off' position turn the sync switch (S1 AB) to position $3,50 \mathrm{~Hz}$ sweep. The trace dis played should be about 1.5 cm . long.

The $Y$ amplifiers can be checked next by first setting the timebase range to position 1 and the fine control to approximately half-way. Connect the 100 mV 50 Hz calibration signal to the 'live' Y amplifier terminal and make sure the $Y$ amplifier switch is to 'Y amp' and not 'Y pre-amp'. With the Y gain control at almost maximum the 50 Hz sine-wave displayed should be about 2 cm . peak-to-peak and there should be at least 3 or 4 complete cycles. Now switch to 'Y pre-amp' and connect the 50 Hz calibration signal to the co-axial $Y$ input and set the $Y$ gain to ${ }_{10}$ th of its travel. The 50 Hz sine-wave dis played should again be about 2 cm . peak-to-peak. Turn the $Y$ gain a little higher so that the peaks of the test signal extend to the top and bottom of the screen. At this point the sine-wave should show no sign of clipping.
Further tests which include timebase synchronization, and the X amplifier gain etc., require the use of an audio signal generator. For the $X$ amplifier test set the sync switch ( Sl 1 AB ) to ' X amp' and turn the X amp pre-set gain control fully clockwise. Set the timebase range switch to 'off'. With a sine-wave signal of 1.5 V r.m.s. to the X amp input the trace should deflect vertically to approximately 4 cm . long,

Return the timebase range switch to position 2 or 3 and then set the sync switch to 'internal sync'. Inject a 1000 Hz sine-wave of approximately 500 mV to the ' $Y$ amp' input and adjust the $Y$ gain for a 4 cm . display. Adjust the timebase fine control until the trace locks. Now run through the rest of the timebase
ranges using input signals of appropriate frequency to ensure that each range is functioning and that synchronization can be obtained on each

The screen graticule on the prototype was made from ${ }^{1}$ gin. thick perspex to the size shown in Fig. 13. The calibration marks were as shown, in centimetres and were produced by scoring the perspex on the side facing the c.r.t. screen. The scored lines and marks were filled with Chinagraph (soft wax pencil). The graticule can be fixed over the screen by two screws at the top which go into the front panel but with spacers on them to keep the graticule just off the tube face.

The c.r.t. hood can be made from 18s.w.g. aluminium as shown in Fig, 14. The tab at the top is folded as shown and this holds the hood on to the top of the graticule. The hood can be pained matt black inside if desired.

> In the main circuit of the oscilloscope on page 1009 of the April issue the secondary of the mains transformer was marked $250-0-250 \mathrm{~V}$. This should have read $350-0-350 \mathrm{~V}$ and is as the components list which gave it correctly.

## P.W. SOUND EFFECTS SYNTHESISER

continued from page 58
could be tested separately with a 24 V battery supply and the output coupled to an amplifier for aural checks. The output signal level from each generator is over 100 mV . This is the best way of ensuring that each circuit is operating properly and producing the right sound and may well save time and trouble when the final assembly stage is reached.
The amplifier and loudspeaker used with the completed synthesiser should be capable of good quality reproduction and have a fairly wide frequency range. The power output will depend on how loud the sounds are to be produced but should be comparable with the power output of the organ. A minimum of 10 W


The completed synthesiser with the bottom and side paneis removed. The power supply can be seen on the left.
might be suitable for the majority of domestic electronic organs. It may be possible, of course, to couple the unit directly to the organ main amplifier but care should be taken with regard to required signal level and impedance matching.

[^3]


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| T41/3T | B.F.O. Coil | $\ldots$.... 57p |

Details of these and our other components are given in an illustrated folder which will be supplied on request with postage please.


Number 19

G.E. PA494 Precision Voltage Detector

BEFORE going on to consider the technical details of this month's circuit, it would be well to indicate some of the answers to the obvious question as to why the electronics enthusiast should be interested in a new high performance precision voltage detector such as the G.E. type PA 494. It was designed principally for applications requiring the logic function of a Schmitt trigger. In other words, the output of the i.c. would switch states very rapidly once the input threshold voltage had been exceeded. Applications for such a unit are obvious in circuits requiring pulse control, in that a trigger which has lost its shape can produce an accurate square wave output. In radio control of models for instance, this is a valuable feature permitting correction for signal degradation in propagation from the control transmitter to the model receiver. Of more general interest, however, are its uses in such systems as time delays, square wave generators, overvoltage and over-current protection systems, photoelectric controls, etc., some of these applications of the unit being considered in greater detail later on.

## Operation

The PA494 itself comes as a four pin device mounted in a TO-5 package. The complete circuit diagram is shown in Fig. 1. Provided the input


TO-5 package outine
(Bottom view)
Fig. 1: Circuit of the PA494 with transistors circled for clarity.
voltage at pin 1 does not exceed the reference voltage set by the resistor pair R1, R2 then $\operatorname{Tr} 2$ and $\operatorname{Tr} 4$ will be biased on causing $\operatorname{Tr} 7$ to saturate and an output current of up to 250 mA may be drawn from pin 3. On the other hand once the reference voltage is exceeded at the input, $\operatorname{Tr} 1$ and $\operatorname{Tr} 3$ will conduct in addition to $\operatorname{Tr} 5$ resulting in positive feedback to the base of $\operatorname{Tr} 2$. This reduces the reference voltage and at the same time turns Tr2 off. Consequently the differential amplifier will have changed states and no output current will be available at pin 3 as Tr7 will have been biased off.

Due to the Darlington input configuration of the unit an exceptionally high input impedance is achieved with a mere 100 nanoamps needed to saturate Trl. This makes the PA494 ideally suited for high impedance sources as a result of the low input current drawn. It combines many of the features of a f.e.t. in a bi-polar device; yet it does not suffer from failure due to static discharge as is sometimes the case with the f.e.t.

## Practical Uses

Now let us consider some uses to which we can put the device. Fig. 2 shows a simple bridge configuration using a photoelectric cell or a thermistor


Fig. 2: (above) the PA494 in an alarm or warning system; and Fig. 3 (below), in a timing circuit.

in one arm. The coil of a relay can act as the load for Tr 7 thereby providing simple photoelectric control systems or on the other hand if preferred a discrete p.n.p. power transistor may be inserted for direct control of currents up to several amperes.
The PA494 also lends itself to very neat timing circuits of intervals of up to 1 minute, by a simple r.c. network. As can be seen from Fig. 3 a d.c. output is obtained when the threshold voltage is reached in contrast to the unijunction which generates a pulse.


Fig. 4: Another application of the PA494. A switching or shaping circuit.

By biasing Trl midway between saturation and cut-off a number of interesting uses may be obtained. The same circuit as shown in Fig. 4 may be utilised as either an on-off touch switch, sine to square wave converter or pulse shaper.
No doubt further uses for the PA494 will spring to mind; a few designs have been given here in the hope that further innovations will be realised on the part of the individual constructor.
U.K. distributors for the PA494 are:- Jermyn Industries Ltd., Vestry Estate, Sevenoaks, Kent.
television

## USING THE 'SCOPE

The oscilloscope is an increasingly important servicing tool with the number of colour sets rapidly increasing and a whole range of videocassette devices soon to appear on the market. Yet many enthusiasts and engineers are uncertain about its capabilities and use. Hence this new series by Keith Cummins-starting next monthto clear up exactly what can be done with the oscilloscope and how to do it.

## DYNAMIC TV PICTURES

The video circuits in most sets are something of a compromise and do not do full justice to the contrast range of the transmitted picture. Norman McLeod presents a circuit for the experimenter to try which overcomes these defects and provides dynamic TV pictures.

## LOGBOOK OF VAN 13

As you might suppose, Van 13 is on the colour run! Harold Peters in this feature provides details of common-and some not so common-faults found in colour receivers.

## APRIL ISSUE-OUT NOW

## P.W. <br> DESIGNEIES TROPHY

## Presented at Film Show

Although the postal strike prevented the despatch of the usual invitation cards, a reasonable number of readers turned out to see the filmshow at the Caxton Hall, Westminster, London, on 5th. March, run as usual by Practical Wireless and Television magazines in conjunction with Mullard Ltd.
The first part of the evening was devoted to the showing of two films, "Now and Then" featuring John Pertwee and "The Electrons Tale", a lighthearted look at the story of the electron.
Following the films, the Editor, Norman Stevens, presented the Practical Wireless "Designer's Trophy 1970 " awarded for the most meritorious article submitted for the Project Autumn Competition. The reader was Caleb Bradley and his article "A High Impedance Voltmeter" was featured in the April issue of PW.
Following refreshments the rest of the evening was given over to a talk by Philip Hunt of Mullards. Entitled "I.C. Story-Continued" it was a continuation of the "Introduction to the I.C." lecture given at last year's Filmshow. This time the theme was the application and servicing problems of I.C.'s.
This year's show was the last to be run in conjunction with Mullard. The company have decided to make cuts in the film and lecture department but Mr. Stevens assured those present that every effort would be made to continue the Filmshows in the years to come.

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ONE reads nowadays of the extremely high power stations that are being used on the very low frequencies for maintaining communication with nuclear submarines even when they are submerged. Megawatts on frequencies at the top end of the audio range are not, unusual.
It was a similar combination of power and long wavelengths that opened up radio communication in the first decade of this century, but it would be invidious to compare the efficiency of those old transmitters and their aerial systems with those in use today.
We recently came across an article, written in 1912, that endeavoured to correlate power, distance and wavelength. At that time it was known that

TABLE 1

| Aerial <br> Current | Working Distance |  | Extreme Distance |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Day | Night <br> (zero <br> absorption) | Day | Night <br> (zero <br> absorption) |
| amps. | miles | miles | miles | miles |
| 1 | 75 | 90 | 200 | 360 |
| 2 | 135 | 180 | 300 | 720 |
| 3 | 180 | 270 | 375 | 1,080 |
| 5 | 235 | 450 | 475 | 1,800 |
| 7 | 280 | 630 | 550 | 2,520 |
| 10 | 345 | 900 | 630 | 3,600 |
| 15 | 420 | 1,350 | 725 | 5,400 |
| 20 | 475 | 1,800 | 790 | 7,200 |
| 25 | 525 | 2,250 | 840 | 9,000 |
| 30 | 565 | 2,700 | 900 | 10,800 |
| 40 | 630 | 3,600 | 970 | 14,400 |
| 50 | 685 | 4,500 | 1,025 | 18,000 |
| 60 | 725 | 5,400 | 1,150 | 21,600 |

received signal strengths in the daytime were roughly inversely proportional to distance but the rule only seemed to work up to about 150 to 200 miles after which signal strength dropped off quite rapidly. This was reception by ground wave, as we know it today.
Attempts to formulate some kind of law for signals travelling over a night path came to grief as it was observed that such signals were very irregular in strength and generally stronger than the signals received over the day path. The attenuation of
signals was thought to be due to their "absorption" in the upper layers of the atmosphere but assuming no absorption at all the signals over the night path were still stronger than the calculated values.
Apparent changes in the degree of absorption between summer and winter had also been noted and it was thought that the conductivity of the upper atmosphere was increased by the action of the sun's rays.
Table 1 shows the calculated relationship between the aerial current at the transmitter and two ranges, 'working range' and 'extreme distance of audibility'. The first range produced $40 \mu \mathrm{~A}$ in the 'receiver resistance' of 25 ohms and the second range $10 \mu \mathrm{~A}$, corresponding to $1000 \mu \mathrm{~V}$ and $250 \mu \mathrm{~V}$.
These ranges were between two ships each having aerials at 130 feet so presumably the transmitter aerial current was measured in what was the base

TABLE 2

| Nautical <br> Miles | $\lambda=$ <br> $1,000 \mathrm{~m}$. | $\lambda==$ <br> $2,500 \mathrm{~m}$. | $\lambda=$ <br> $3,750 \mathrm{~m}$. | $\lambda=$ <br> $6,000 \mathrm{~m}$. |
| :---: | :---: | :---: | :---: | :---: |
|  | amps. | amps. | amps. | amps. |
| 1,000 | 15 | $13 \cdot 5$ | 15 | 17 |
| 1,250 | 38 | 27 | 27 | 30 |
| 1,500 | 91 | 49 | 44 | 46 |
| 1,750 | 200 | 95 | 77 | 74 |
| 2,000 | 490 | 155 | 122 | 105 |
| 2,250 | - | 245 | 314 | 160 |
| 2,500 | - | 470 | 414 | 235 |
| 2,750 | - | - | 500 | 335 |
| 3,000 | - | - | 775 | 500 |

of a top loaded vertical over an almost perfect ground plane. The wavelength in use for these experiments was 1000 metres ( 300 kHz ).

However our mathematician seems to have gone astray by overlooking the impracticability of a 21000 -mile night path; perhaps he was already thinking of going into orbit!

At this time, 1912, no one doubted the great advantages of long waves for communicating with distant stations and Table 2 was published to prove the point. This was based on two stations with aerials 450 high and again the distance quoted is working range.

It seems strange, in this scientific age, that brute
force and long waves are still needed to establish solid communication at a distance regardless of conditions. One would think that an entirely new method of communication would have been dreamed up by now.

## Shí Shatk 1912

It is somewhat difficult for us, even the old-timers, to realise that in 1912 only the largest passenger ships were fitted with wireless telegraphy apparatus of a sort, that smaller ships, particularly cargo ships, were virtually lost to the rest of the world for weeks or even months on end once they had left our shores.
They did of course make visual signals to other ships and to coast stations en route so that owners had some idea of what was going on. Nevertheless ships, passengers and crews were lost at sea in circumstances where a brief radio call, had it been possible, would have brought other ships hurrying to their aid.


A typical ship's wireless cabin of 1912 fitted with the Marconi " $\frac{1}{2} k W$ cargo set". The cabinet contains the vertical rotary converter with the disc discharger on top.

A dock labour dispute in 1911 did a lot to accelerate the equipping of the smaller ships with wireless telegraphy especially as owners realised that this would enable them to re-direct ships at a moment's notice which was particlularly important with perishable cargoes. It was left to the Marconi company to produce a wireless installation that was small enough and cheap enough to be suitable for the smaller ships.

Called the " ${ }_{2} \mathrm{~kW}$ cargo set" it could transmit spark signals between 200 and 600 metres wavelength and receive signals between 200 and 1600 metres. The ship's d.c. mains supply energised a rotary converter which gave a $\mathrm{l}_{2} \mathrm{~kW}$ of a.c. at "a spark frequency of 300 per second." A disc discharger on top of the converter was adjustable so that the discharge took place at the peak voltage output of the converter.
Tapped inductors were wound with copper strip
on ebonite formers and these in conjunction with capacitors made from glass and zinc plates formed the "oscillation transformer".
It is interesting to note that the receiver, a "magnetic detector", was permanently connected to the aerial but was shorted out by an auxiliary pair of contacts on the key, "thus enabling the receiving operator to 'break-in' on the transmission in the event of erroneous reception and thus avoid waste of time". Even today very few amateur c.w. stations


A close-up of the "magnetic detector" receiver that can also be seen in the general view of the equipment
have proper "break-in" facilities, although they may have a fast changeover system, but that is not the same thing at all. Those that have true break-in do not use it to its best advantage but it must be admitted that the licence regulations governing the use of call signs does nothing to encourage the use of break-in!



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## Power Supply Units



Designed specially for use with the Project 60 system of your choice.
Illustration shows PZ. 5 to left and PZ. 8 (for use with 2.50 s) to the right. Use PZ. 5 for normal Z.30 assemblies and PZ. 6 where a stablised supply is essential.
$\mathbf{P Z - 5} 30$ volts unstabilised $\mathbf{£ 4 . 9 8}$
PZ-6 35 volts stablised $£ 7.98$
PZ-8 45 volts stabilised
(less mains transformer) $£ 7.98$

## Guarantee

If within 3 months of purchasing Proiect - 60 modules direct/y from us, you are dissatisfied with them. we will refund your money at once. Each module is guaranteed to work pe fectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever purchase datie. There will be a small charge for service thereafter. No charge for postage by surface mail. Air-mall charged at cost.

Stereo 60 pre-amp/control unit


Designed for the Project 60 range but suitable for use with any high quality power amplifier Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

## SPECIFICATIONS

Input sensitivities: Radio-up to 3 mV . Mag. p.u mV -correct to R.I.A.A. curve $\pm 1 \mathrm{~dB}: 20$ to $25,000 \mathrm{~Hz}$ Ceramic p.u. $\sim$ up to 3 mV : Aux-up to 3 mV .
Output: 250 mV
Signal-to-noise ratio: better than 70 dB .
Signal-to-noise ratio: better than
Channel matching: within 1 dB .
Tone controls: TREBLE +15 to -15 dB at OKHz: BASS +15 to -15 dB at 100 Hz .
Front panel: brushed aluminium with black knobs .
ize: $8 \frac{1}{4} \times 1 \frac{1}{2} \times 4$ ins
Built, tested

## Active Filter Unit



For use between Stereo 60 unit and two Z.30s or $Z .50$ s, and is easily mounted. It is unique in hat the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid ( $12 \mathrm{~dB} /$ octave), there is ess loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negigible. The A.F.U. is suitable for use with any other amplifier system. Two stages of filtering are incorporatedumble (high pass) and scratch (low pass) Supply voltage 15 to 35 V Current - 3 mA SF ly voltage -- 15 to 3 . Curn 30 ki 5 kHz . L.F cut-off ( -3 dB ) variable from 25 Hz 5 kHz . L. cut-off ( -3 dB ) variable from 25 Hz
to 100 Hz . Distortion at $1 \mathrm{kHz}(35 \mathrm{~V}$. supply) to 100 Hz . Distortion at
$0.02 \%$ at rated output.
Built, tested
and'guaranteed
£5.98

## Stereo FM Tuner


first in the world to use the
phase lock loop principle
Before production of this tuner, the phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio over other systems. Now. for the first time. the principle has been applied to an FM tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. Sensitivity is such that good reception becomes possible in difficult areas Foreign stations can be tuned in suitable conditions and often a few inches of wire are enoug for an aerial In terms of a high fidelity this for a low lon listion then tuner has a lower level of distortion than an kow. Stereo broadcasts ar received automatically as the tuning control is rotated. a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system.
SPECIFICATIONS:
Number of transistors: 16 plus 20 in I.C.
Tuning range: 87.5 to 108 MHz
Capture ratio: 1.5 dB
Sensitivity: $2 \mu \mathrm{~V}$ for 30 dB quieting: $7 \mu \mathrm{~V}$ for full limiting.
Squelch level: $20 \mu \mathrm{~V}$
A.F.C. range: $\pm 200 \mathrm{KHz}$

Signal to noíse ratio: $>65 \mathrm{~dB}$
Audio frequency response: $10 \mathrm{~Hz}-15 \mathrm{KHz}^{3}$
Total harmonic distortion: $0.15 \%$ for $30 \%$ Total harm
Stereo decoder operating level: $2 \mu$
Pilot tone suppression: 30 dB
Cross talk: 40 dB
I.F. frequency: 10.7 MHz

Output voltage: $2 \times 150 \mathrm{mV}$ R.M.S.
Aerial Impedance: 75 Ohms
Indicators: Mains on: Stereo on; tuning indicator Operating voltage: $25-30 \mathrm{VDC}$
Size: $3.6 \times 1.6 \times 8.15$ inches: $91.5 \times 40 \times 207 \mathrm{~mm}$


Price: $\mathbf{£ 2 5}$ built and tested. Post free

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Address
for which $i$ enclose cash/cheque/money order

## Sinclair IC10/016/Micromatic

IC10


The world's most advanced high fidelity amplifier
This is the world's first monolithic integrated circuit high fidelity power amplifier and preamplifier. The circuit itself is a chip of silicon only a twentieth of an inch square by one hundredth of an inch thick, having 5 watts RMS output ( 10 watts peak). It contains 13 transistors (including two power types), 2 diodes. 1 zener diode and 18 resistors. and is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is more rugged and has considerable performance advantages, including complete freedom from thermal runaway and a very low level of distortion. The IC10 is primarily intended as a full performance high fidelity power and preamplifier, for which application it only requires the addition of such components as tone and volume controls and a battery or tone and volume controls and a battery or mains power supply. It may also be used in
other applications including car radios, other applications including car radios,
electronic organs, servo amplifiers (it is dc electronic organs, servo amplifiers (it is dc coupled throughout) etc.
Circuit Description
The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier, Class $A B$ output is used with cosely controlled quiescent.current which is independent of temperature. There is generous negative feedback round both sections and negative feedback round both sections and distortion at all supply voltages, making battery operation eminently satisfactory,
Each IC10 is sold with a comprehensive Each IC10 is sold with a comprehensive manual giving circuit and wiring diagrams for a arge number of applications in addition to
high fidelity. These include oscillators. etc. high fidelity. These include osciliators. etc.
The preamp section can be used as an RF or The pre-amp section can be used as an RF or
IF, amplifier without any additional transistors. IF, amplifier with

## Specifications:

Output: 10 watts peak, 5 watts RMS continuous. requency response : 5 Hz to $100 \mathrm{kHz} 1 \neq \mathrm{dB}$. Total harmonic distortion: Less than $1 \%$ at full output.
oad impedance: 3 to 15 ohms.
Power gain: 110 dB ( $100,000,000,000$ times) total.
Supply voltage: 8 to 18 voits. (A Sinclair power unit, $\mathrm{PZ}, 7$ is available for mains operation)
ize: $1 \times 0.4 \times 0.2$ in, plus heat sink and tags.
Sensitivity 5 mv .
nput impedance: Adjustable externally up to 2.5 Mohms.

Price (with manual): 玉2,98 post free.

016


## High fidelity loudspeaker

The 016 employs the well proven acoustic principles specially developed by Sinclair in which a special driver assembly is meticulously matched to the cher assembics of the uniqu designed cabinet. In reviewing this exclusive Sinclair design, technical journals have justly compared the 016 with much more expensive loudspeakers. Its shape enables the 016 to be positioned and matched to its environment to much better effect than is the case with conventionally styled enclosures. A solid teak conventionally styled enclosures. A solid teak surround with a special all-over cellular foam
front is used as much for appearance as its front is used as much for appearan
ability to pass all audio frequencies.

This elegantly designed shelf mounting seaker brings genuine high fidelity within reach of every music lover.

## Specifications

Construction: Special sealed seamless sound or pessure chamber with internal baffle.
oading : up to 14 watts TMS
nput impedance: 8 ohms.
Frequency response: From 60 to $16,000 \mathrm{~Hz}$ confirmed by independently plotted B and K curve, Driver unit: Special high compliance unit having massive ceramic magnet of 11,000 gauss, aluminium speech coil and a special cone suspension for excellent transient response.
size and styling: 97 in square on face $x 4 t$ in. deep with near pedestal base, Black all-over cellular foam ront with natural solid teak surround. Price $\boldsymbol{q}^{8-98}$.

Micromatic


## Britain's smallest radio

Considerably smaller than an ordinary box of matches, this is a multi-stage AM receiver brilliantly designed to provide remarkable standards of selectivity, power and quality for its size. Powerful AGC counteracts fading its size. Powerful AGC counteracts fading
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Specifications:
Size: $36 \times 33 \times 13 \mathrm{~mm}\left(14 / 5 \times 13 / 10 \times \frac{1}{2} \mathrm{in}\right)$
Weight: including batteries, 28.4 gm ( 1 oz .).
Case: Black plastic with anodised aluminium front panel and spun aluminium dial
Tuning; medium wave band with bandspread at higher frequencies, ( 550 to $1,600 \mathrm{~Hz}$ ).
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[^1]:    nation of the operation of the various sections is given in the text.

[^2]:    Logs for the Amateur Bands must arrive before the 15th of each month. The address is: 14 Manland Avenue, Harpenden, Herts

[^3]:    A little gremlin seems to have been at work regarding the castanets circuit on page 914 of the March issue, C1 and C2 should be $0.2 \mu \mathrm{~F}$ and not $0.02 \mu \mathrm{~F}$ as given. In the text of the same the section near the middle should read "The waveform from Tr1 and Tr2 is applied to the base circuit of Tr3 .. "" and not "emitter circuit."

[^4]:    Published approximately on the 7th of each month by IPC Magazines Limited, Fleetway House, Farringdon Street, London, E.C.4. Tel: 01-634 4444. Printed in England by Index Printers, Dunstable, Beds. Sole Agents for Australia, and New Zealand-Gordon and Gotch (A) sia) Ltd.; South Africa Central News Agency Ltd.; Rhodesia and Zambia-Kingston Ltd.; East Africa-Stationery and Office supplies Letd. Subscription rate (including postage); For one year to any part of the world e2.65 (e2 18s od.) otherwise disposed of by way of Trade at more than the recommended selling price shown on the cover, and that it shall not be lent, resald or hired out or otherwise disposed of in a muti lated condition or any unauthorised cover by way of Trade, or affixed to as part of any pubication or advertising, literary or pictorial matter whatsoever.

