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Complete stereo system $£ 41$ plus $£ 2.10$, p. \& p.

## F.E.T. MkI $£ 14.5$ plus $7 / 6$ p. \& p. High fidelity transistor stereo amplifier employlng field effect transistors. With this feature and accompanying guaranteed specifications below, the Viscount F.E.T. vastly surpasses amplifiers costing far more.

Specification-Output per channel 10 watts r.m.s. Frequency bandwidth 20 Hz to 20 $\mathrm{kHz}+1 \mathrm{db}$ at 1 watt. Total distortion at 1 kHz at 9 watts $0.5 \%$ Input sensitivities CER. P.U. 100 mV into 3 meg ohms. Tuner 100 mV into 100 K ohms. Tape 100 mV into 100 K ohms. Overload Factor Better than 26 db .

Signal to noise ratio-70db on all inputs (with vol. max). Controls- 6 position selector switch (3 pos. stereo and 3 pos. mono). Separate volume controls for left and right channels. Bass $\pm 14 \mathrm{db}$ at 60 Hz . Treble (with D.P.S. on off) $\pm 12 \mathrm{db}$ at 10 KHz . Tape recording output sockets on each channel. Size $12 \frac{1}{4} \mathrm{in}$. 6 in . $2 \frac{2}{3} \mathrm{in}$. in teak-
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## The f29-10-0 Stereo system

The Duetto is a good quality stereo amplifier, attractively styled and finished. It gives superb reproduction previously associated with amplifiers costing far more.

## SPECIFICATION-

R.M.S. power output 3 watts per channel into 10 ohms speakers.
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## THE DUO SPEAKER SYSTEM

Bimilar in debign to those on the previous page the 2way speaker system is beautifully duished in polished teak veneer, with matching vynair grille. It is ideal for wall or shelf mounting either upright or horizontally.

Type 1 APECIFICATION:-
Impedance 3,8 or 10 ohms (please state requirement). It incorporates Goodmans high flux 6 in x 41 in speaker

4 guineas each. $7 / 6 \mathrm{p} . \& \mathrm{p}$.

## 50 WATT AMPLIFIER

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An extiemely reliable general purpose valve amplifier. Its rugged conatruction yet space age styling and design makes it by far the best value for money.
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3 electronically mixed channels, with 2 inputs per chavnel, enables the use of 6 separate ingtzuments at are located directly above the corresponding input sockets. SENBITIVITIES AND INPUT IMPEDANOES Channels 1 aud 24 mV at 470 K . These 2 channels (4 inputs) are suitable tor microphone or guitars. Channels 3 and 4300 mv at lm . Suitable for most high output instruments (gram, tuner, organ, etc). Input


## EXTRACTOR FAN

A.C. mains $230 / 450 \mathrm{v}$, conplete with pull switch. Size: $6 \times 6 \times 4 \mathrm{jn}$.

Price 27/6
plus 7/6 P. \& P.


8PECIPICATIONS
Output-10 watts. Output impedance- 3 to 4 ohme Inputs-1. -xtal mic 10 mV Toue Controls-Treble control range $\pm 12 \mathrm{~dB}$ at 10 KHz . 2. - $\mathrm{kram} /$ radio 250 mV . Bass control range $\pm 13 \mathrm{~dB}$ at 100 Hz . Frequency Response-(with toue controls central) Minus 3dB points at 20 Hz and $40 \mathrm{KHz}$. Bignas to Noise Ratio-better than Mains input-220/250V. A.C. Size of chassis $101 \mathrm{in} \leq 4 \frac{1}{\mathrm{i}} \mathrm{in} \mathrm{x}$ 2 inin. For use with Std. or L. $\mathbf{P}$. records, nuasical instruments, all 2xin. For use with sta. or il.P. recorus, nusical makes of pick-ups and mikes. Separate bass and treble litt control. Two inputs with control from gram. and mike. Built and tested.
RELIANT Mk. 1
As above less teak case
£6.10 plus $7 / 6 \mathrm{P}$. \& P
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Tuning Heart


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Mk. III
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$\overline{7}$ trantistor fullg-tunable M.W.-L.W. superhei portable Net of parts. Complite with all components, including ready etched and drilled printed circuit board-back printed for foolproor construction

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# DISCOSOUND 

## DJ DISCO-AMP



The DJ Disco-amp has been designed specifically for use with discotheques and has many exclusive features not normally found on P.A. amplifiers. The unit will be of use to the professional D.J. as well as in clubs and mobile discotheques.

The pre-amp section features independent inputs and volume controls for two mics with separate bass, treble and master volume, plus two independent inputs and volume controls for turntables, again with separate bass, treble and master volume controls.

A complete Pre-fade listen (P.F.L.) cueing monitor section is also featured with separate input for headphones (either stereo or mono) with an independent volume control for headphone monitoring, and a P.F.L. switch, so that either turntable can be monitored fcr accurate cueing up of records. A mic over-ride switch is also added which cuts the music volume by half so that mic announcements may be made over the music without altering the volume controls.

The power amplifier section has an output of 70 watts R.M.S. into 8 ohms and has elaborate protection against thermal, short or open circuit. The unit is designed for panel mounting.

## SPECIFICATION

Output power
Frequency response
Harmonic distortion
Signal/noise ratio
Speaker impedance
Headphone impedance
Bass control
Treble control
Inputs:
turntable

70 watts R.M.S. $\pm 1 \mathrm{db}$ at 8 ohms $30-20,000 \mathrm{~Hz} \pm 3 \mathrm{db}$. Less than $1 \%$ at full output. Better than -65 db .
$8-16$ ohms.
8-16 ohms.
Variable 20 db at 100 Hz .
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50 ohm or 600 ohm mic inputs may be ordered at extra cost. Size: Front Panel $16 \mathbf{t}^{\prime \prime} \times 7^{\prime \prime}$. Cut out $15 \frac{1^{\prime \prime}}{} \times 6^{\prime \prime}$. Fuses: A.C. 1.5 amp (B.S.) mounted on back panel.

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This is a four channel fully mixable prc-amp, with separate treble, bass and master volume controls. and is completely self powered. All four inputs are by standard jack socket on the front panel with the addition of inputs 3 and 4 being duplicated on the back panel, with, two paralleled outputs also featured for versatility in use. Frequency
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## DJ 705 <br> INTEGRATED MIXERAMPLIFIER



One of the finest units available on the market today, regardles of price. The front end of the unit consists of a four channel mixer with separate inputs and volume controls, plus a separate bass, treble and master volume control. One of the main features of this remarkable amplifier is its elaborate protection against short and open circuit and we can guarantee that it is virtually indestructable. Allied to this is its very high power output ( 70 watts R.M.S.) a frequency response $(30-20,000 \mathrm{~Hz} \pm 3 \mathrm{db})$ that is superb, and distortion that is well below $1 \%$ even at full output. The unit is suitable for use with discotheques, groups, P.A.. clubs etc., or anywhere that high quality high output is required. Size: 1512 in $\times 5$ in $\times 6 \mathrm{in}$.
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Cabinets lateat style Satin Teak or Atrormosia veneer.
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Cone spkr. Imp. 3 or 15 ohuss. $E 8.19 .9$
STANWAY II Size $20 \times 10$ In $\times$ Catin. approx.
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c.p.s. -21 Bi . Harnouic Distorc.p.s. -2013 . Harlionics Distor-
tlon o.3\% at 1,000 c.p.eSeparate Bas and Treble
input sockets for Mike, (iran, - lift' and 'cut' contrula. 3 input sockets for Mike, (ram, Radio or I'ape. Input selector switch. Output for $3-15$ ohm spkrs. Max. sensiticits bunV. Ontput rating 1.H.F.M. Fully enclosed enamelled case, $9 \frac{1}{2} \times 2$ yōtia. Attractive lorushed sllver faish facia plate 10 x 3 inn. and maiching knibs.
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high fux nidule range speaker. (4) High effiency tweeter. (0) Approhigh flux nididle range speaker, (4) High effciency tweeter. (5) Appro priate quantity acolstic damping material (6) Teak veneered cabinet. (7) Circuit and

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High Grade Componento
Specifications comparable with units costing considerably more. trasisistors 9 high quality typen in each channel.
OUTPUT 10 Watts R.M.S. continuous
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TREBLE CONTROL +17 dB to -14 dB at $10 \mathrm{Kc} / \mathrm{s}$.
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HARMONIC DISTORTION $0.1 \%$ at 10 ratt 1,000 c.p.s.
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ROSS TALE 52 dB at 1,000 c.p. CROSS TALK 52 dB at 1, $100 \mathrm{c} . \mathrm{p}$. CONTROLS 5 Position Input Eelector'. Bbss, Treble, Vol., Bal. Stereo/Mono
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Approx. $12 \times 3 \times 8$

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Polnt to point wiring diagranis 22 gis. Polnt to point wiring diagranis
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HI-FI SPEAKER ENCLOSURES Teak or Afrormosia
reneer finish. Modern derign. Aconsticaliy lined
$\begin{aligned} & \text { All wizes spprox. Carr. } \\ & \text { JEs Size } 16 \text { I } \\ & \text { I } \\ & \text { gin. Pressurised. Give }\end{aligned}$
Es Bize 16 I 11 I 9in. Pressurised. Gives f4.|4.6
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FOR GUTTAR，vocal or mstrumental group A 4 input， 2 volume control Hi －Fi unit with geparate Bass and Treble controls．B．V．A．ralves．Peak output rating．Strong Rexine covered cabinet with handles． attractive black／gold facia panel．Neou indicator．For


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FANE ULTRA HIGH POWER LOUDSPEAKERS All power ratings are R．M．S．continuous． 9 years＇

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| WHARFFEDALE Unit 3 | ¢11, 19 | E47 15 | SME 3012 with S2 shell | ¢ 33 | 62619 |
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| GOLDRING GL69 | ¢25 16 | <19 19 |  |   <br> 5 17 | 4410 |
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4

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## TOPIC OF THE MONTH

## Showtime

TEMPUS, as they say, certainly fugits. And here we are once again in that fag-end of the British summer which has become known traditionally as "show time". To add emphasis to this exhibition oriented season, the annual RSGB show has, thls year, moved up from its usual October date to August, finishing at the time the round of annual radio trade shows begin. It is hoped that regular visitors to the RSGB show (known officially as the International Radio Engineering and Communications Exhibi-tion-or Radiocom 70-) have taken note of this change of date; it is now August 19-22. For full details please refer to page 360. We hope many readers will be there; Practical Wireless will have the usual display of constructional projects on show.
After all this activity, the Audio Fair follows on in October. Once again Practical Wireless will be supporting the exhibition with displays and demonstrations of a range of audio projects, plus a special competition for the occasion. It is all a little feverish for those intimately connected with the trade and the technical press.
With the RSGB exhibition, so far as P.W. is concerned, our participation is very largely a matter of preaching to the converted, yet we think it well worthwhile to take part. Anything that encourages a greater interest in home construction meets with our approval and the RSGB exhibition has always stressed this side of the hobby. This year we are pleased to learn that small stands will be available to non-trade members of the Society to display and sell pieces of equipment.

Until fairly recent times, most radio amateurs built all their station gear. Nowadays the more general thing is to use commercially built transmitters and receivers. Whether this is due to that mysterious phenomena of having more leisure time than ever but less time to spare for building, or merely to being more affluent is hard to calculate.
But if amateurs cannot or will not build their own main equipment, then they can learn one lesson from the P.W. stand. That is, that there are very many auxiliary pieces of equipment that anyone can find the time to build, not only directly connected with the radio amateur station but in the various allied fields of radio, audio and electronics.
W. N. STEVENS-Editor.

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## OCTOBER ISSUE WILL BE PUBLISHED ON SEPTEMBER 4

[^4]
## MEWS... <br> NEWS...

## Dixons Stereo



When Dixons Photographic entered the Audio HiFi field in depth, their first units were updated versions of existing record reproducing systems, restyled for marketing through the Company's 100-plus Branches under the "PRINZ" label.
Now they are marketing their own Prinz Stereo System 6. Specific points in the system's specification are detailed. Amplifier; Solid state- 12 transistors-a.c. Mains $220 / 250 \mathrm{~V}$. 50 Hz . Frequency Range $50-18,000 \mathrm{~Hz}$. Noise level- 55 dB . Controls: On/Off and Volume, Bass, Treble and Stereo Balance. Output 5 watts Music Power per Channel. Turntable is a Garrard 4 -speed Auto 2025TC, fitted with Acos GP93/1 stereo crystal cartridge with sapphire styli. Speakers are two sealed enclosures each containing one 8 in. $x$ 5in. loudspeaker, 10,000 lines, and complete with 8 ft . of lead per enclosure, terminating in a 2 -pin DIN plug. Cabinets are as in photograph, with teak veneer finish. Price is £55 complete.

## Two Metre Vertical

Two metre mobile enthusiasts will be pleased to hear of a new antenna manufactured by the American company Antenna Specialists Co., and available from KW Electronics Ltd., 1 Heath Street, Dartford, Kent.

This is a vertical whip, the ASP 629, which offers a gain of 2.5 dB relative to a quarter wave antenna. It consists of a stainless steel whip and matching transformer assembly and may be tuned up anywhere in the range $130-174 \mathrm{MHz}$.

The interference suppression ratio, relative to a quarter wave antenna, is better than 6 dB . The mounting hole required is $\frac{3}{4}$ in. in diameter and no access is needed from the inside of the vehicle.
The antenna could also prove suitable for a home station and would be extremely useful where space was at a premium. The cost of the ASP 629 is $£ 3$ 10s. Antenna Specialists also manufacture vertical whip antennas suitable for 4 metres and 70 cms .

## New Inverter

A new range of Inverter Modules introduce a new service by Gardners Transformers Limited, of Christchurch, Hampshire, England.

The new range, known as the M48 E.H.S. Series, are the product of a development and manufacturing service which has been set up to cater for individual requirements and special applications.


They offer power ratings up to 30 watts stabilised or 50 watts unstabilised in a standard mechanical assembly which will meet a wide variety of electrical parameters. The assembly incorporates a single power stabiliser which would be fitted in the d.c. output line for single output inverters or in the input to the inverter where multiple outputs are specified.
Finished dimensions for the power ratings quoted are 4 in . $\times$ 3.3 in . $\times 2 \mathrm{in}$., and the weight is 24ozs. Fixing is by 4BA tapped bushes in the base of the unit.

Full details of the new range and the new service may be obtained from Gardners Transformers Limited, Christchurch, Hampshire BH23 3PN.

## Bi-Pak I.C.'s

A complete range of Digital T.T.L. Integrated Circuits is to be launched by Bi-Pak Semiconductors to cover the popular 74 N series of logic units. These will be available in the dual-inline plastic package at approximately half the normal distribution price. The range includes gates, flip-flops and complex units such as divide by 164 -bit binary counters, shift registers and decimal decoders plus nixie tube drivers.
It is hoped that with the low price and guaranteed supply which Bi-Pak have arranged with the manufacturers the teaching and experimental use of Integrated Circuits which up to now have been almost non-existent for most amateur concerns will at last become a reality.

Bi-Pak hope to publish in the near future enough circuitry for building computers, calculators, etc., using the Integrated Circuits mentioned. Bi-Pak say their aim is to further reduce the cost for amateur electronics and at the same time make it the most interesting hobby of this day and age.

Full details and prices are available from: Bi-Pak Semiconductors, P.O. Box 6, Ware, Herts.

## Going Metric

A new leafiet 'Going MetricEveryday Units' is now available free from the Metrication Board. The leaflet sets out the more common metric units and correct symbols for 14 everyday quantities including length, area, capacity, temperature and weight.

In the United Kingdom the basis for the metric system now coming into use is the International System of Units, known in all countries by the abbreviation SI. The units contained within this system are sufficient for all present needs of technology, science, industry, commerce and daily life.

Copies of the leaflet can be obtained without charge from Information Division, Dept. 4, Metrication Board, 22 Kingsway, London, W.C.2.

## WEWS... NEWS... <br> NEWS...

## Quick on the draw



No, it's not a new kind of space gun-it's an Ersa Sprint soldering iron. Made in West Germany, the retailer in this country is Home Radio Ltd.

The interesting thing about this iron is that it weighs only 7ozs. and heats up in only 10 seconds. The technique used is different from usual quick heat irons because this switch is released once the operating temperature has been reached. Current consumption is 150 W during heat-up period, dropping to 80 W when operating temperature is reached. Working voltage is $200-250 \mathrm{~V}$ a.c.
Home Radio stress that they supply a guarantee with these irons and they also stock a complete set of spare parts any of which can be changed in a matter of seconds.
The retail price of the Ersa Sprint is $£ 319 \mathrm{~s}$. 6d. and the only retail supplier is: Home Radio (Components) Limited, $234-240$ London Road, Mitcham, Surrey, CR4.3HD.

## Preston R.R.C.

The P.A.R.S. are again holding a Mobile Rally. The venue, as in previous years is: Kimberley Barracks, Deepdale Road, Preston (next to Preston North End Football Ground).
The date is August 30th and a talk-in station will be active on 160 m . Refreshments, both tea and the "hard stuff" will be available. Numerous trade stands will be in evidence. Further information may be obtained from (s.a.e. please): G. Wright, G3YOT, 56 Queensway, Bamber Bridge, Preston, PR5.6UD.

## R.A.I.B.C.

The Radio Amateur Invalid and Bedfast Club will have a corner of their stand at the Radio Engineering and Communication Exhibition devoted to the collection of unwanted foreign stamps. So, if you have any stamps please take them along to the Exhibition and leave them at the R.A.I.B.C. stand. Also, on this stand, visitors will be able to see at firsthand the kind of good work the Club does.

Both the Hon. Sec. of the Club (Mrs. Woolley), G3LWY and Allan Herridge, G3IDG, will be present throughout the exhibition and look forward to meeting Practical Wireless and Practical Television readers.

## I.C. Amplifiers

Motorola Semiconductors have announced a range of low-cost integrated circuits for the con-sumer-equipment field. Known as MFC units, these plastic-encapsulated devices use smaller chips and contain fewer circuit elements than the professional-equipment of i.c's. These new i.c's also have wider pin spacing to make them suitable for the printed-circuit boards used in consumer products.

The first two devices in the range to be introduced are a lowpower audio amplifier and a wide-band amplifier. The former, Type MFC 4000 , is a 250 mW a.f. amplifier with a low total harmonic distortion (typically, $0.7 \%$ at 50 mW output) and is designed for pocket radios. Contained in a four-lead package, it includes six transistors, three diodes and five resistors and requires no output transformer to match to a $16 \Omega$ load. The input sensitivity is 15 mV r.m.s. for 50 mW output. It requires a 9 V d.c. supply and the quiescent current is 3.5 mA .
The latter unit, Type MFC 4010 , is a high gain ( 60 dB ) wideband $(100 \mathrm{~Hz}$ to $4 \mathrm{MHz},-6 \mathrm{~dB}$ points) amplifier that could be used either as a general-purpose a.f. amplifier or as an i.f. amplifier at 465 kHz . Typical output noise is 1 mV r.m.s. Maximum power supply potential is 18 V and typical current drain is 3 mA .

## Hugh Greatorex

The retirement was recently announced of Hugh Greatorex who for 37 years has been with the BBC Engineering Information Department. For the last 16 years he has been Assistant Head of that department. During this time his responsibilities included the organisation and management of the BBC technical enquiry stands at exhibitions and conferences. He made significant contributions to the promotion of new BBC services, in particular the v.h.f. radio service and latterly the u.h.f. and colour TV services.

Hugh has been a great friend of the Press for many years and we at Practical Wireless would like to wish him all good luck in his retirement.

## Do il yourself

A new, inexpensive, educational aid to learning and teaching elements of logic, Boolean algebra and fundamentals of digital computers, COMPUKIT 1, has been announced by Limrose Electronics. It is supplied in kit form ready to be assembled on a specially designed printed circuit board. Logic circuits are constructed by making soldered, or solderless, connections to the terminal pins mounted on the p.c. board. Logic levels are indicated by miniature wire-ended bulbs on the board which is powered by a $4 \frac{1}{2}$ volt battery. The gates in the kit use transistors, diodes and resistors, and can be used not only for performing elementary logic functions, but also for wired-or, bistable and polyflop circuits and counters. The kit is complete and requires only a small soldering iron and a pair of cutting pliers to assemble. These can be purchased from the manufacturers as optional extras. The Instruction Book is written by a Fellow of the British Computer Society and avoids the use of jargon.

The basic kit costs only 7 Gns, and can be supplied in assembled form ready for use for an extra 27s. 6d. Further details from Limrose Electronics, Lymm, Cheshire.

## PW 2. F.JUDD Part 1

FOR TREBLE OR BASS GUITAR, ORGAN AND MICROPHONE WITH NEW "TONE TREMULANT" SYSTEM, BUILT-IN MIXING, VISUAL TREMULANT INDICATOR. MAX 50 WATTS R.M.S. POWER. COMPLETELY SELF CONTAINED. OPTIONAL FOOT CONTROLLED TREMULANT AND WAH-WAH.

SELF-CONTAINED high power guitar amplifiers with facilities similar to those of the PW 25-50, and which will be fully dealt with in this and following articles, do not come cheaply. A commercially made equivalent would cost in the region of $£ 150$ or more. All the components, including the power module, its power supply, the cabinet materials and the two special Goodmans power loudspeakers specified, can be obtained for approximately half this price.

The finished 50 watt amplifier is neither small nor light in weight because of the twin heavy duty loudspeakers and the very necessary rugged cabinet construction which is essential for power reproduction of guitar bass at the full 50 watts r.m.s. output. The cabinet is constructed from $\frac{3}{4} i n$. thick Weyroc compressed chipboard.
There is, however, an alternative arrangement with regard to the loudspeakers and power output. For those who require the amplifier for treble guitar only with less power, a single type 12P 8 ohm Goodmans power speaker can be used and with this the PA50 power output module will deliver 25 watts r.m.s.

If the full 50 watts should be required at a later date, it will only be necessary to fit the additional loudspeaker. With a pair of type 12P Goodmans 12 -inch 8 ohm loudspeakers used in parallel, the power module load becomes 4 ohms across which the module will deliver 50 watts (r.m.s.) power.

These Goodmans loudspeakers are a new range recently released by the manufacturers and have been specially designed for musical instrument amplifiers. Note that the use of loudspeakers, other than those specified, would in all probability spoil the performance of the amplifier. Under no circumstances must the power module output load be less than 3 ohms.

## Amplifier Facilities

One of the special features of this amplifier is the 'tone tremulant' system which produces a tremulant effect similar to that obtained from the rotating loudspeaker systems used in electronic organs (Leslie speakers). The tone tremulant can be varied to any degree but when turned off leaves normal amplitude tremulant as found on most guitar amplifiers. The
amplifier can, of course, be used without either of the tremulants.

Two inputs are provided for guitars, i.e., two instruments, bass or treble, can be plugged in and for which independent volume controls are provided. There is also an input for a microphone which may be high or low impedance, depending on whether a microphone transformer is used. The microphone channel has its own volume control and being quite separate from the guitar channels is not affected by the tremulant system. A master volume control is provided for all channels.


The completed Vibrasonic amplifier which utilises two 12in. speakers to handle the output of 50 watts (r.m.s.)

The function of the tremulant system is visually indicated by a front panel lamp which shows the tremulant speed and depth. However, when the tremulant is switched off the tone networks of the tremulant amplifier can still be used as a tone control. There is also a separate treble lift control in the guitar input pre-amplifier which together with the tremulant tone control can provide the very sharp tonal quality favoured by pop guitarists.

There are two optional facilities. One is a foot switch on-off control for the tremulant and the other a foot pedal-controlled wah-wah effect. Foot switch control of the tremulant simply requires an extra jack socket and a foot switch with a press 'on' and press again 'off' function. The wah-wah


Fig. 1. Block diagram illustrating the function of each stage of the amplifier.
effect can be obtained with a pedal-operated potentiometer which can also be plug and socket connected to the guitar pre-amplifier.

## Power Amplifier Module and Power Supply

To facilitate construction for those with little experience in building and testing transistor power amplifiers, modules and regulated power supplies, the new Henelec 50 watt power amplifier module type PA50 and its matching power supply Henelec type MU442 have been chosen for the power output end of the PW25-50.
As previously mentioned the Henelec PA50 module will deliver 50 watts r.m.s. into a 4 ohm load or 25 watts to an 8 ohm load. Hence the reason for the designation PW25-50 and the use of either one or a pair of 8 ohm loudspeakers.

The Henelec PA50 module and its power supply are supplied complete with connecting cables, ready wired to the connectors, DIN loudspeaker plugs, a DIN signal input plug and a 3 -pin mains input connector. To mount these units it is only necessary to drill the appropriate fixing holes on the PW25-50 chassis. The Henelec power module and power supply are tested before despatch so that no circuit adjustment whatever is necessary.

## Pre-amplifier and Control Circuit

The block diagram in Fig 1 may help to clarify the various functions of the pre-amplifier and tremulant control stages. The two guitar inputs can be mixed, i.e., each can be adjusted for volume independently of the other. The inputs are suitable for all medium to high impedance guitar pick-ups and the sensitivity of each input is 40 mV for maximum rated power output.

Signal levels of 1 volt or more can be taken to these inputs and with the tremulant switched off they can be used for signals from other sources such as the output from a portable electronic organ, a tape recorder or high output gramophone pick-up, etc.

The guitar pre-amplifier also has a treble control which provides approximately 15 dB lift at $10,000 \mathrm{~Hz}$. This has been included as many guitarists favour a tone with a strong upper harmonic content.

## New Tremulant System

The signal output from the guitar pre-amplifier is passed to a network which routes the signal via the tremulant l.d.r. (Light Dependent Resistor) to the tone tremulant amplifier and also directly to the input of the mixing pre-amplifier. The 1.d.r. is controlled by means of a lamp, the brilliance of which is made to vary sinusoidally.

When the phase shift oscillator is running the amplitude of the छuitar signals is varied at the requisite tremulant rate, between 5 and 10 Hz as required. The signals that pass through the tone tremulant circuit are modified and the harmonic structure changed by means of the primary inductance of T3 and its RC network. The signals are phased reversed at the primary and therefore appear at the output of the tone tremulant amplifier 'in phase' with signals direct from the guitar pre-amplifier. The result is a complex variation (at tremulant rate) of the higher harmonics produced by the guitar, the aural effect being akin to that obtained with a rotating loudspeaker tremulant system (Leslie speaker).

The effect is much more pleasing than the usual straight amplitude variation tremulant used in commercially made amplifiers. The tonal quality of the tremulant is continuously variable and when turned off leaves a normal amplitude tremulant only, the tone of the guitar remaining unaffected.

This too can be switched off but the tone tremulant control can still be used as a tone control for the guitar providing even stronger upper harmonic sounds than those produced by the treble lift control.

The mixed outputs from the guitar pre-amplifier and the tone tremulant circuit are then taken to the mixing pre-amplifier together with the output from the microphone pre-amplifier. The mixing preamplifier output is then connected to the power amplifier module via the master volume control.

## Tremulant Control System

The tremulant control circuit consists of a phase shift oscillator with variable frequency control (approximately 5 to 10 Hz ), the signal from which is used to drive the 1.d.r. control amplifier. There are two 6 V 0.04 A lamps in series with the collector of this transistor, one of which is used to control the


Figs. 2. (above) and 3 (right) give full details for the construction of the cabinel.
1.d.r. and the other as a visual tremulant indicator for the front panel.
The tremulant depth can be controlled so that a full or light tremulant can be obtained but the system is so arranged that the playing volume does not sharply increase when the tremulant is switched off. The l.d.r. control lamp remains alight when the tremulant is switched off, thus restoring the volume to a mean level. The rise and fall of the tremulant is rather like that of Class A modulation in a transmitter.
The 1.d.r. system of control is completely free of the low frequency thump that is common with the usual combination of a phase shift oscillator and signal amplifier. The tremulant variation is perfectly sinusoidal.

## Construction (Cabinet)

The cabinet dimensions given in Fig 2 are in accordance with the enclosure space required by the loudspeakers for proper loading and for full


Fig. 4. Constructional and drilling details for the amplifier chassis and panel. Note that the aluminium angle plece at the rear of the chassis is turned downwards while the side and front angle pieces are facing upwards. The sizes of the component mounting holes shown in the front panel may need to be altered to suit the components aclually used. Check before drilling panel.

bass response down to about 40 Hz . It is made from $\frac{3}{4}$ in. thick Weyroc chipboard with joints strengthened by $2 \times 1 \mathrm{in}$. planed battens.
All joints must be screwed as the cabinet is carrying a fair weight when the speakers and amplifiers are installed and because strong joints will prevent cabinet buzz at very low frequencies.

Weyroc is hard to cut but most local timber dealers with a power saw will cut the pieces exactly to size as in Fig. 2. One may then only have to cut the holes for the speaker(s). Fig 2A, B and C give all the cabinet assembly details.

Note the recessed beading around the front and back of the amplifier compartment and the recessed batten around the speaker compartment. It is not absolutely necessary to line the speaker compartment with felt but this may be worth doing to ensure no resonance effects whatsoever from the cabinet. Half-inch thick carpet felt glued around the inside and on the back panel would be sufficient.
The cabinet must have strong carrying handles, one each side, as these will be the only means of carrying it with ease. The base of the cabinet can
be fitted with rubber feet or two battens crosswise as can be seen in the photos or with roller castors. The actual finish of the cabinet can be left to the constructor's choice, but the prototype shown on the front cover was covered with plastic material as used for home decorating, the cabinet being finally edged at the front with $\frac{3}{4} \times \frac{3}{4}$ in. aluminium angle fixed with chromed instrument head screws.
The loudspeaker cut-outs are as shown in Fig 3. If the 25 watt version is to be constructed only one speaker will be used but if the second speaker and, therefore, higher output power is anticipated for a later date, then cut one hole for the single speaker in the top left-hand corner as in Fig 3. Otherwise a single speaker may be mounted centrally if desired.

## Construction (Amplifier Chassis)

The amplifier chassis occupies most of the area of the amplifier compartment and allows plenty of room for the three circuit boards, the pre-amplifier


Fig. 5. Circuit of the complete pre-amplifer and its power supply.

View of the complete
amplifier with the three
circuit boards of the pre-ampliffer
(see Fig. 5) at the left. The power ampli-
fler module is in the centre with its own
power supply unit to the right. Behind the seem-
ingly blank hole in the very centre of the panel is the tremulant visual indicator lamp.
power supply, the power output module and its power supply. The chassis and front panel dimensions with drilling and assembly details are given in Fig 4. Note how the finished chassis fits into and is secured in the amplifier compartment as shown in Fig 2D.

## Pre-amplifier Circuit

The full pre-amplifier and tremulant control circuit is shown in Fig 5. This is assembled on three s.r.b.p. circuit boards, the three sections being marked round by the dotted lines. The circuit function has
already been explained by means of the block diagram Fig 1, but the following general circuit description may prove useful.

The microphone pre-amplifier Tr 1 and Tr 2 has a microphone transformer included in the input circuit which should be used if the microphone is low impedance ( 25 to 30 ohm type). Microphones of 200 ohms impedance can be used without a transformer as also can other microphones with a high impedance output i.e., with a built-in low to high impedance transformer.

## components list

Resistors:

| R1 | $4.7 \mathrm{k} \Omega$ |
| :--- | :--- |
| R2 | $1.5 \mathrm{k} \Omega$ |
| R3 | $12 \mathrm{k} \Omega$ |
| R4 | $12 \mathrm{k} \Omega$ |
| R5 | $560 \Omega$ |
| R6 | $1.2 \mathrm{k} \Omega$ |
| R7 | $2.2 \mathrm{k} \Omega$ |
| R8 | $1 \mathrm{k} \Omega$ |
| R9 | $150 \mathrm{k} \Omega$ |
| R10 | $8.2 \mathrm{k} \Omega$ |
| R11 | $1.5 \mathrm{k} \Omega$ |
| R12 | $68 \mathrm{k} \Omega$ |


| R13 | $8.2 \mathrm{k} \Omega$ | R25 | $150 \mathrm{k} \Omega$ | R37 | $47 \mathrm{k} \Omega$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R14 | $2 \cdot 2 \mathrm{k} \Omega$ | R26 | $1.8 \mathrm{k} \Omega$ | R38 | $47 \mathrm{k} \Omega$ |
| R15 | 56k $\Omega$ | R27 | $470 \Omega$ | R39 | $120 \mathrm{k} \Omega$ |
| R16 | $10 \mathrm{k} \Omega$ | R28 | $1 \cdot 2 \mathrm{k} \Omega$ | R40 | $4 \cdot 7 \mathrm{k} \Omega$ |
| R17 | 18k $\Omega$ | R29 | $1 \mathrm{k} \Omega$ | R41 | $100 \Omega$ |
| R18 | $270 \Omega$ | R30 | $4.7 \mathrm{k} \Omega$ | R42 | $12 \mathrm{k} \Omega$ |
| R19 | $47 \mathrm{k} \Omega$ | R31 | $22 \mathrm{k} \Omega$ | R43 | $560 \Omega$ |
| R20 | $47 \mathrm{k} \Omega$ | R32 | $100 \mathrm{k} \Omega$ | R44 | $1.5 \mathrm{k} \Omega$ |
| R21 | $470 \Omega$ | R33 | $18 \mathrm{k} \Omega$ | R45 | $2 \cdot 2 \mathrm{k} \Omega$ |
| R22 | $4.7 \mathrm{k} \Omega$ | R34 | $10 \mathrm{k} \Omega$ | R46 | $560 \Omega$ |
| R23 | 120k $\Omega$ | R35 | $2 \cdot 2 \mathrm{k} \Omega$ |  |  |
| R24 | $12 \mathrm{k} \Omega$ | R36 | $47 \mathrm{k} \Omega$ |  |  |

All resistors $\frac{1}{2} \mathrm{~W} 10 \%$ miniature

| VR1 (Microphone Volume) | $100 \mathrm{k} \Omega$ log. |
| :--- | :---: |
| VR2 (Tremulant Speed) | $50 \mathrm{k} \Omega$ linear |
| VR3 (Tremulant Depth) | $10 \mathrm{k} \Omega$ linear |
| VR4 (Gultar 1 Volume) | $100 \mathrm{k} \Omega$ log. |
| VR5 (Guitar 2 Volume) | $100 \mathrm{k} \Omega$ log. |
| VR6 (Treble Control) | $50 \mathrm{k} \Omega$ linear |
| VR7 (Tremulant Tone) | $100 \mathrm{k} \Omega$ log. |
| VR8 (Master Volume) | $100 \mathrm{k} \Omega$ log. |
| VR9 (Wah-wah Control) | $100 \mathrm{k} \Omega$ linear |

## Capacitors:

| C1 | $0.02 \mu \mathrm{~F}$ polyester | C11 | $0.1 \mu \mathrm{~F}$ polyester | C21 | $2.5 \mu \mathrm{~F} 25 \mathrm{VW}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C2 | $100 \mu \mathrm{~F} 12 \mathrm{VW}$ | C12 | 100 $\mu \mathrm{F}$ 12VW | C22 | $0.05 \mu \mathrm{~F}$ polyester |
| C3 | 200pF | C13 | $0 \cdot 1 \mu \mathrm{~F}$ polyester | C23 | $100 \mu \mathrm{~F} 12 \mathrm{VW}$ |
| C4 | $100 \mu \mathrm{~F} 12 \mathrm{VW}$ | C14 | 200pF | C24 | 200pF |
| C5 | $2.5 \mu \mathrm{~F} 25 \mathrm{VW}$ | C15 | $100 \mu \mathrm{~F} 12 \mathrm{VW}$ | C25 | $100 \mu \mathrm{~F} 12 \mathrm{VW}$ |
| C6 | $500 \mu \mathrm{~F} 25 \mathrm{VW}$ | C16 | $2.5 \mu \mathrm{~F} 25 \mathrm{VW}$ | C26 | $2.5 \mu \mathrm{~F} 25 \mathrm{VW}$ |
| C7 | $1 \mu \mathrm{~F}$ polyester | C17 | $250 \mu \mathrm{~F} 25 \mathrm{VW}$ | C 27 | $250 \mu \mathrm{~F} 25 \mathrm{VW}$ |
| C8 | $1 \mu \mathrm{~F}$ polyester | C18 | $0.015 \mu \mathrm{~F}$ polyester | C28 | $5000 \mu \mathrm{~F} 30 \mathrm{VW}$ |
| C9 | $1 \mu \mathrm{~F}$ polyester | C19 | $10 \mu \mathrm{~F} 12 \mathrm{VW}$ | C29 | $0.25 \mu \mathrm{~F}$ polyester |
| C10 | $500 \mu \mathrm{~F}$ 12VW | C20 | $25 \mu \mathrm{~F}$ 12VW |  |  |

Semi-conductors:

| Tr1 BC109 | Tr4 AD161 | Tr7 BC108 |
| :--- | :--- | :--- |
| Tr2 BC108 | Tr5 BC109 | Tr8 BC108 |
| Tr3 BC108 | Tr6 BC108 | Tr9 BC108 |
|  | All Mullard |  |

## Loudspeakers:

50W Amplifier. 2 Goodmans Type 12P-50watt (12in. 8 ohm)
25W Amplifier. 1 Goodmans Type 12P-50watt (12in. 8 ohm)

Power Module and Supply:
Power amplifier module, Henelec Type PA50 (Henrys Radlo Ltd)
Mains power unit, Henelec Type MU422 (Henrys Radio Ltd)

## Miscellaneous:

Transformer T3 Type CP6713/2 (Henrys Radio Ltd)
Transformer T2 $240 \mathrm{~V} / 17 \mathrm{~V}$ Type CT1 (Henrys Radlo Ltd)
Light Dependent Resistor LDR (Mullard ORP12). Lamps 6V, 0.04A, (2). Batten lampholder MES.
Dial lampholder MES. Neon panel indicator 240V.
Bridge rectifier MR1, 30 V (Henrys Radio Ltd. Type LT 119 or 1H3). Jack sockets (3).
Switch S1, 1 pole 2 way, (Henrys Radio Ltd. Wafer type A)
Switch, 2 pole 2 way, mains toggle.
Plug and socket, 3 pin, mains input (Henrys Radio Ltd. type 373).
Knobs (4), (Henrys Radio Ltd. type NK2)
Knobs (5), (Henrys Radio Ltd. type 7)
Veroboards ( 3 ) $7 \times 5 \mathrm{in}$., $5 \times 4 \mathrm{in}$.; $5 \times 4 \mathrm{in}$. plain, 0.1 in . matrix. Screened connecting cable.
Mains lead, 3 -core cable.

## materials list

## Chassis and Panel:

Aluminium 18 s.w.g. Pieces as in Fig. 4.
Aluminium angle, $\frac{3}{4} \times \frac{3}{4} \mathrm{in}$. Approx. 6 ft .
Aluminium angle $\frac{7}{8} \times \frac{8}{8} \mathrm{in}$. Approx 2 ft .
Nuts and screws various, 4 BA.

## Cabinet:

Weyroc chipboard $\frac{3}{4}$ in. Pieces as in Fig. 2.
Planed batten, $2 \times 1 \mathrm{in}$. Approx 16 ft .
Square beading, $\frac{1}{2} \times \frac{1}{2} \mathrm{in}$. Approx 10 ft
Carrying handles (2). Sundry woodscrews.
Covering material. Felt, $\frac{1}{2}$ in, thick if required.

If the microphone transformer is not required (it is not included in the pictorial diagrams to follow later) then simply connect the input jack to Cl as shown at the starred points. Note that the impedance of the microphone input without a transformer is approximately $100 \mathrm{k} \Omega$ and is not suitable for crystal microphones.

The guitar pre-amplifier $\operatorname{Tr} 4$ and $\operatorname{Tr} 5$ is similar to the microphone pre-amplifier except that a treble lift control (VR6) has been incorporated which provides approximately 15 dB lift at $10,000 \mathrm{~Hz}$. The output from the guitar pre-amplifier is divided across R31 and the l.d.r. and routed to the tone tremulant ciricuit input transformer T3 and on to the mixing pre-amplifier Tr 8 and Tr 9 via R38.

The transformer T3 must be the one specified in the components list and connected exactly as shown. The circuitry drawn in dotted line (C29-VR9) is for the optional wah-wah effect, further details of which will be given later.

The phase shift oscillator $\operatorname{Tr} 3$ is quite straightforward but note the optional dotted line circuitry for a foot control tremulant on-off switch which can be connected via a jack socket on the front panel. The tremulant control amplifier Tr4, which is an AD161, must be mounted on a small heatsink as will be shown in Part 2.
The mixing pre-amplifier $\operatorname{Tr} 8$ and $\operatorname{Tr} 9$ completes the pre-amplifier section and the output from this is taken via VR8, the master volume control, to the power output module. The pre-amplifier power supply T2, the bridge rectifier MR1 and the smoothing capacitor C28 are mounted directly on the main chassis.

More detailed information concerning the preamplifier and tremulant circuitry, its function and performance, will be given in a later article. Next month will deal with the layout of the three circuit boards, the front panel controls and the power module and its supply.

TO BE CONTINUED


## NEXT MONH IN

## Minitics

## TRANSISTOR AND DIODE TESTER

This unit is the first of a new range of test equipment, full constructional details of which will appear from time to time in PW. Simplicity of construction is the key-note of this tester which will measure the basic characteristics of most PNP or NPN transistors. All the components are mounted on the cover of a die-cast aluminium box which itself provides an elegant finish.

## SIMPLE MINI-ORGAN

This interesting project, which can be built in a few hours, will provide many more hours of entertainment for the constructor and family alike. The circuit uses four cheap transistors to produce a musical range of two octaves the notes being selected by a "magic wand".

## ELECTRONIC DIGITAL COMBINATION LOCK

A device which began life as a "gadget" to raise funds at a coffee party was developed into this sophisticated version which, although amusing, could have commercial possibilities. The two transistor circuit employing digital techniques need hold no fears for the average constructor.

PLUS THE REGULAR "TAKE 20" AND "IIC. OF THE MONTH" FEATURES AND OTHER CONSTRUCTIONAL ARTICLES AND FEATURES

Don't miss your copy of the October issue of Practical Wireless-on sale 4th September-price 3s. 6d.


THE simple transistorised preselector to be described can be constructed and got working in a single evening. It costs approximately $£ 2$ to build and is a worth-while project for listeners who like to search out DX on the h.f. amateur bands.

Some of the communications-type receivers in use function well on the low frequency bands but do tend to become insensitive at higher frequencies of say 21 MHz or so. Some operators aware of the problem have gone so far as to replace the older octal-based valves used in some such receivers with more modern types-but not always with complete success!
Some of the more up-to-date receivers too are by no means faultless in this respect; generally speaking the replacement of certain valves with more modern
types should be attempted only by experienced persons who have access to reliable test and alignment apparatus; without such test gear results obtained are likely to be problematical.

When first class results are required on the higher frequency bands attention should first be paid to the aerial and its aerial matching unit after which the use of a preselector can be considered, which can make the best possible use of such signals that are available from the aerial system.

## CIRCUIT

Reference to Fig. 1 shows the final preselector circuit adopted. The components associated with Tr 1 confer the required degree of r.f. amplification. Transistor Trl operating in common-emitter mode with the necessary tuned circuit L1/VC1 tied to the base element which allows continuous coverage over the frequency range of $13-30 \mathrm{MHz}$. The three principal amateur bands used for DX. 10, 15 and 20 metres, are thus taken care of; in the prototype they appear on the dial pointer at approximately the 10,1 and 2.30 o'clock positions.

Due to the damping effect of the aerial, preselector tuning tends to be broad and there is thus no need to fit a reduction drive to the peaking control VCl .

Amplified signals appear at the collector of Tr 1 and go via capacitor C3 to transistor $\operatorname{Tr} 2$ operating as an emitter-follower stage; signals pass via C 5 and the screened cable to the receiver aerial socket.
In order that the preselector can be switched off when the user wishes to listen on other bands-say 18.3 .5 or 7.0 MHz -a combined In/Out/By-pass switch, S1a/b is provided. This disconnects the battery and at the same time allows the aerial to be fed through to the receiver.
The switch can also be used for checking the effectiveness of the unit by comparing receiver ' S ' meter readings with the device alternatively 'In' and 'Out'. An increase of at least $2 \frac{1}{2}$ ' $S$ ' points has been noted on the meter of an Eddystone 888A on the 21 MHz band with the signal peaked correctly by means of VCl. This means that the unit is of particular value when copying weak c.w. or a.m. signals.


Fig. 1. Circuit of preselector. (Note:-the capacitor between Tr1 and Tr2 is C3, 100pF).

## CONSTRUCTION

A 6 -in square of 18 -s.w.g. aluminium sheet bent centrally into an ' $L$ ' shape is used as a combined panel and chassis. As may be seen from the wiring and layout plan of Fig. 2 the battery can also be accommodated on the chassis. Two simple 'Lektrokit' tag strips act as small component anchors; the transistors are soldered in last of all. The coil is fixed to the base-plate in the position shown, its brass-stemmed dust core being removed completely. In connection with the coil, care should be taken when soldering for excessive heat application will cause the polystyrene former to melt.

The length of screened cable to the receiver should be made no longer than required and it should be clamped firmly to the preselector base-plate. It is also necessary to fabricate a small metal bracket to carry the aerial socket SK1. Wiring associated with the slide switch Sla/b is shown inset in the interests of clarity.

## TESTING

Initially a test meter set to read $0-10 \mathrm{~mA}$ may be inserted in series with the battery and S1. When the switch is moved to 'In' a current of approximately 2 mA should be noted. Subsequently the test meter is' removed and the preselector can be connected to the receiver and aerial with which it is to be used.
With the preselector switch at 'Out' a reasonably steady, but weak, signal should be sought on the receiver on the 14 MHz amateur band and the ' S '


Fig. 2. Layout of the completed pre-selector.

## components list

```
Resistors:
    R1 15k\Omega
    R2. 2.7k\Omega
    R3 1k\Omega
    R4 270k\Omega
    R5 3.3k\Omega
Capacitors:
    C1 0.01 }\mu\mathrm{ F ceramic
    C2 0.04\mu\textrm{F}\mathrm{ tubular}
    C3 100pF ceramic
    C4 0.01\muF ceramic
    C5 100pF ceramic
    VC1 100pF variable
Semi-conductors:
```


## Tr 1 AF 117 or AF 115

```
Tr 2 AF 117 or AF 115
```


## Inductors:

```
\(L 1\) Miniature transistor type Denco Range 4 (blue) RFC 1 Miniature ferrite cored choke 1.5 mH .
```


## Miscellaneous:

```
Miniature switch, 2P 2W slide type K.
\(6 x\) 6in aluminium sheet. 6 V battery.
Coaxial socket. Tag strips etc.
```

meter reading noted. If $S 1$ is next moved to its 'In' position the amplifying effect of the preselector will be soon noted as VC1 is tuned to peak the transmission. The preselector can then be similarly tested on the 21 and 28 MHz bands and thereafter finalized as required to suit the particular location.

Should it be found that the 21 MHz band peaks when the vanes of VC1 are almost fully disengaged it will not be possible to achieve signal peaking on 28 MHz ; in such cases three turns may be removed from the tuned winding of coil L1. To do this, carefully snip the winding clear where it terminates at pin No. 6, unwind the necessary number of turns slowly, snip off the unwanted wire and re-make the connection to the vacated pin.

Advantages the simple preselector described has over a valved version are a physically small size plus the fact that it is completely independent of any mains connection and is thus safe. On the debit side noise generated by the transistorised preselector tends to be higher than that developed by a good valved specimen. Since to some extent noise - to - signal ratio changes with d.c. potentials supplied the lowest possible battery voltage should be applied to the transistorised unit compatable with adequate amplification.


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THIS month seems to have been a bumper one for Broadcast Bands listeners and I have been swamped with reports and letters.
C. R. S. Stacey of Tunbridge Wells who regularly uses his Lafayette HA-700 and Joystick to send in excellent reports like the following:

5047 Radio Togo, Eng. news at 1950
15165 Syria, Overseas Service, English, 1930
15300 NHK, Japan, Eng. 1800-1815
15435 DW, Kigali relay in Amharic 1415
15440 FEBC, Philippines in English at 1530.
Glyn Morgan of Tredegar has an impressive lineup of equipment including a Lafayette HA-230, an Eddystone-EC10 and a Hallicrafters SX130 and a 50 ft . long-wire aerial. This equipment enabled him to send in a report which included:
3232 R. Brazzaville, Congo in French at 2205
3376 CR6RP, Angola, English music at 2205
4765 R. TV Congolaise, French at 2155
4815 Upper Volta, talk in French at 2220
4835 R. Mali, play in French at 2210
4850 R. Mauritania at 2050
4880 Kinshasa, Congo, African music at 2245
4885 Nairobi, Kenya, pop music at 1845
4905 R. Relogio, Brazil, Port. at 2145
4915 Nairobi, Kenya often heard at 1900
4926 R. Ecuatorial, Guinea, Spanish at 2140
4940 R. Abidjan, Ivory Coast, music at 2225
4976 Kampala, Uganda, music at 2025
4990 R. Barquisimeto, Ven., music at 0745
4995 R. Brazil Central with football at 2250
5026 Kampala, Uganda in vernacular at 1850
6045 R. Clube Paranaense, Brazil, 2300
6055 R. Panamericana, Brazil, at 2235
6250 Santa Isabel, Guinea, Spanish at 1930.
John Trewick of London Colney has a Perdio six transistor portable receiver with a telescopic antenna and a log which includes:

6145 Deutsche Welle to the USA a 0435-0555
7210 Oslo, Norway on Sundays at 1200 to 1235
11735 Rabat, Morocco with news at 1715
11740 ABC, Australia with news at 1700.
John also reports that a new station is TransEurope, Portugal at $0900-1000$ on 9650 and 11720 and at 1345-1415 on 9625 and 11865. The first programme is in English from the Tourist Radio and the second is a relay of Deutsche Welle in English.

Geoffrey Gilham of London S.E.12. is a regular reporter to the column and his log includes:

4835 R. Mali with talk in French at 2045
4855 R. C. Mozambique, music at 2102
4923 Radio Quito with classical music at 0250
4967 R. Kuwait with pop music at 2052
6090 R. Belgrano, Argentina with talk at 0203
6160 Emis. Nueva Grenada, Col. at 0420.

## THE BROADCAST BANDS

Regular reporter Roy Patrick of Derby has sent in some more, very interesting, news items:

FINLAND Radio Finland has announced that it intends to drop its DX programme.
IRAQ Radio Baghdad has been logged on 9610 at 1930 with a programme in English.
MONACO Radio Monte Carlo is now broadeasting twelve hours a day in Italian on 1466 and the shortwave frequencies of 6035 and 7135. The latter frequency provides very good reception.
Philip Batt of Littleborough in Lancashire has a PCR3 receiver and a 60 ft . long-wire antenna which enabled him to hear the following stations:

4920 YVKR, Caracas, Venezuela, 0600
15060 Radio Peking in English at 0930
15140 Radio Vilnius, Lithuania, sign-off at 2300
15160 ABC. Australia in English to Asia at 0700
15275 R. Afghanistan in English at 1800
15370 R. Tamoio and Tupi, Rio at 2200
17785 Tentative logging of Radio New Zealand with English news at 0700
17855 Radio Japan with English news at 0800
21505 R. Accra, Ghana in English at 1554.
V. P. Hill of Cwmbran owns a 5 -valve domestic superhet. and an 80 ft . long-wire and his log included:

9560 ABC, Australia in English at 0645
15160 Voice of Turkey at 2220
17445 Radio Havana, Cuba at 2042
17448 WINB, United States of America at 1956
17650 Trans World Radio, Bonaire at 2155.
Stephen Wainwright of St. Helens used his Skyrover Mark II receiver and 100 ft . long-wire to hear the following:

9465 R. Pakistan in English at 1945-2030
11815 Bonaire, Neth. Antilles in English at 00300130
15013 Voice of Vietnam in English at 2000-2030
17740 VOA, Monrovia, Liberia in English at 0800
21690 Windward Islands Broadcasting Service, Grenada in English from 1945-2200.
Raymond Peart of Worcestershire used his Spidola transistor receiver and 100 ft . long-wire to $\log$ :
6145 Deutsche Welle in English at 0500-0555
9650 ABC, Australia in English at 0645-0915
9770 Austrian Radio in German at 0730
9833 Radio Budapest in German at 1330
21495 Radio Portugal in English at 1345-1430.
Due to the ever increasing number of reporters to this column I will, in the future, only be able to use those reports which contain accurate details of frequency and time and the name of the station.

All reports should arrive at 58 Kensington Gardens, Cranbrook, Ilford, Essex by the 17th of the month.

## THE AMATEUR BANDS <br> David Gibson, G3JDG

LOTS of interesting things happening this last month both on and off the Amateur Bands. For the c.w. versus a.m. versus s.s.b. addicts you've got a nasty shock coming from the professionals. At a recent conference in London a very strong case indeed was put up for double side band diminished carrier. On tests carried out in the field, a 6 W d.s.b. transmitter consistently outdistanced a 25W a.m. transmission. The police force are seriously considering using d.s.b. and data transmissions at around $2 \cdot 4$ kilobits/second.

Yet another seminar discussed interference. One point which came out here was that of earthing. It was agreed that any interference problem (and earthing system) was very much an individual thing and that no one simple solution or set of rules existed. Makes you think about t.v.i. and that tiny splinter of copper you call an earth, doesn't it!
Lots of inquisitive ears have been flapping about this month and despite the warm weather many people sent in multiple logs. My thanks to all those owners of hot, swetty little lugs who persisted and perspired. You're doing a grand job slaves.
More mighty magnificence from the majestic Master Moore. John, who lives in Leicester bagged GM and GW on topband. On 14 MHz , the CR100/2. a.t.u. and 130 ft . long wire reported signals fromAX5LC, AX HK4AD, HR1KAS, HR2WTA. KH6BX, YN2EC, YV4YC, 8 P 6 AH .

A quick pilfer round the pertinent portions of 21 MHz raised-CN8AH, EL1B, EL2BZ, FDRT/ FC/P, JA1EOD, JA2NPC, JA6YSS, TF3BV, VP9BY, VU2OLK, YA1EXZ, YA1GNT, 5H3KA, 5Z4DW, 9E3USA, 9H1BE, 9V1PA. Ten metres a.m. was heard from LU6DRB, and on s.s.b.-HK3AVA, KV4AD, VU2BEO, ZE2JA, ZS6AUD, 5Z4LS.

John is hoping to listen on 432 MHz soon when he gets a homebrew converter perking and takes delivery of a 14 -element skybeam. (Cor, think of the pleasure all those little prongs will give the birds.)

Roger Boyd is located in Victoria Park, Western Australia and has the distinction of sending the most $\mathrm{DX} \log$ received this month. The rig is a Trio $9 \mathrm{R}-59 \mathrm{DE}$ and choice of 20 metre dipole or a 25 ft . vertical. His $\log$ for 7 MHz reads-DJ DJE, DK1CU, DL6WE, DL8MM, EA4KY, G3VYF/P, HB9ADQ, IIBAF, JA2VGQ, JA8TL, OZ5MV, PY7BPD, SP6DVB, UA1IG, UY5YS, YT1BCD. So, if the path from Europe to Australia is open, why don't more of us hear VK/AX stations on forty? Perhaps it's still the operator that counts and not so much the equipment.

Malcolm Monro (Cumberland) writes a sad tale of holding a G8 licence but the transistor transmitter won't work. Two metre fans will be pleased to hear of the latest Fairchild transistor, the MSA8506 which gives 25 watts at 175 MHz from a 12 V line. Twist in the tail is the price, which is around the $£ 15$ mark. However, the MSA8507 gives 8 W for the same parameters and costs around $£ 6$. With luck the price should drop as production quantities build up. These devices will, however, withstand any non-oscillatory load from an open to a short circuit at full rated power.

Back to logland again. Andy Crooks (Leicester) RA1, PR3O and 45 ft . end fed prowled 21 MHz to find sigs from-CP5PD, CR6BF, CR6FP, EL2L, EP2BQ, HP1RC, JA1DJL, JA2QUQ, JA3QKU, JA4DGG, JA8BMK, JH1ECU, LJ2L (special prefix for Norwegian schools), LU2CF, LU4DM, OD5BZ, PY2CRN, PY5ATL, PY7GAH, TG9GF, VE7DG, VP2VI, VQ9RK (Seychelles), W5DL, W5GंC, W7RI, ZP5GS, ZS3HX, 3V8AL, 5Z4CK, 9J2PV, 9Q5WV. All these using s.s.b.
D. Browning (Herts), CR7OA, PR30X, 37ft. of bent wire in the loft shows what's been about on 3.5 MHz . Heiroglyphics scribed in his $\log$ readAX6HD, CT1BH, CT1GD, CT2AK, DL5YA/MM, FORT/FC, PY1HA, 4U1TTU, 9H1K, 9H1CC, 9 VIPP.

On 14 MHz , Douglas bagged-AXOLD, CN8HL, CN8MJ, HV3SJ, HK4AD, KL7BJW, LU5NA, OJDDX (Market Reef), OA4UY, TR8MC, XE1AE, XE1TX, YN2OM, YV5CQM, 3V8AV, 6W8BD, $7 \times 2 \mathrm{AL}, 9 \mathrm{X} 5 \mathrm{AA}$. Listening on 21 MHz , Douglas had the distinction of hearing King Hussein of Jordan, callsign JY1.
N. Richardson (Bucks.) sent in a $144 \mathrm{MHz} \log$ obtained using earholes backed by a Garex converter into a PR30 and CR7OA tuning $28-30 \mathrm{MHz}$. The antenna is an eight-element Yagi at 28 ft . Signals received from-EI2AX/P, G3JQA/P, G8BCL, G8BEU, G8BMC, G8CAF, G8CIL, G8CSJ, G8CVK/P, GW3GIZ/P, GW3SRT/P, GW8ACG/P GW8BIP, GD2HDZ (Isle of Man). Nicholas will have a rotator on the Yagi by the time you read this which will put the antenna clear of the chimney and roof.
G3QG is located at Luton Hoo and is active on 144.68 MHz . Bill would appreciate any DX reports on his signals and will QSL for worthwhile details of his signals. How about it all you 2 metre sleuths?
A reminder to listen for GB3WRA operating 160-10 from the 24th. Annual Wycombe Show on Saturday, September 6th. If you can get along, visitors, s.w.ls and licensed amateurs will be welcome. Perhaps a chance to go mobile?

Another one to listen for is G2DRT who will be operating as EI2VCL from September 5th. to 22nd. from Fenit County Kerry. Operation will be on 2 metres.
Happenings in August include: August 9th., D/F qualifying even at Chelmsford; 10th., 2 metre s.s.b. contest; 15 th. and 16 th., 4 metre c.w. contest; September 5th. and 6th., v.h.f. NFD.

Mobile Rallies: August 9th., Woburn Abbey; 9th., Stratford upon Avon Mobile Picnic; 16th., Torbay A.R.S. rally at Newton Abbot; 16th., Mobile Rally at Derby; 23rd., Wroughton Aerodrome near Swindon.

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# 27Tility FIEID STRENGTH METER 

## RICHARD COLLINS

IN radio control work, it is often useful to use a field strength meter; it should not be regarded as a superfluous piece of equipment. It is a very simple circuit (see Fig. 1), easy to build and provides a very convenient way of checking that a transmitter is working correctly. Also, the field strength meter is handy for comparing the output power of different transmitters.

## THE CIRCUIT

Refering to Fig. 1, L1 and VC1 comprise the tuned circuit. The aerial, which should be a small telescopic type, connects to one side of the tuned circuit. The signal is tapped off from the tuned circuit, rectified by D1 and smoothed by Cl . The voltage appearing across C 1 will, for most applications, be enough to give a decent reading on a meter placed across it, but for further sensitivity this voltage is made to bias the base of $\operatorname{Tr} 1$; where this is done the meter is of course not required across C1.

VR1, R1, R2 and Tr1 form a bridge circuit and before taking any readings should be adjusted for zero current. The r.f. signal after being rectified will bias the transistor causing the bridge to unbalance and the meter will show a reading. It will quickly be seen that the higher the r.f. signal, the greater will be the unbalance of the circuit and so


Fig. 1: The circuit of the field strength meter. Components to the right of the dotted line are only needed where the extra sensitivity version is required and here the meter is across the bridge circuit.
the reading on the meter will bear a direct relationship to the strength of the signal received at the tuned circuit.
The on/off switch is incorporated with VR1 but care should be taken to ensure that it is wired as shown. The battery used is a 1.5 V pencell.

## CONSTRUCTION

The only component to be constructed is L1, the coil. This is wound on $\frac{3}{4} \mathrm{in}$. dowelling or anything of similar diameter, which may be later removed. Starting at one end of the former, using $16 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. enamelled wire, (leaving about $2 \frac{1}{2} \mathrm{in}$. spare) wind on 8 turns, close wound. A small portion of the wire
should then be bared of enamel so that a tapping can be soldered on later. Another 4 turns are now wound making a 12 turn coil tapped at 8 turns. The coil can then be slipped off the former and stretched to a length of $1 \frac{1}{4} \mathrm{in}$.

Although the wiring is simple (Fig. 2.), it should be carried out with care. Every wire should be as straight as possible. Stiff wire is best as it is less likely to vibrate and cause slight variations in meter readings.
The unit may be housed in a small box measuring about $2 \frac{1}{2} \times 3 \times 6 \mathrm{in}$. and the 25 pF capacitor should preferably be of the ceramic base type with silverplated plates.

$\star$ components list

| VC1 | $25 \mathrm{pF}-$ see text |
| :--- | :--- |
| C1 | 100 pF |
| D1 | OA70 |
| L1 | see text |
| M1 | $0-1 \mathrm{~mA}$ moving coil meter |
| Tr1 | $0 C 71$ |
| VR1 | $10 \mathrm{k} \Omega$ pot with switch |
| R1 | $680 \Omega$ |
| R2 | $680 \Omega$ |
| B1 | 1.5 V battery |
| Five way tag strip, case, telescopic aerial, 16 s.w.g. |  |
| enamelled copper wire. |  |

## CALIBRATING AND TESTING

To test the unit, it should be held with its aerial about 18 in . from the transmitter aerial. The field strength meter tuning control should then be turned slowly until a reading appears on the meter. It is advisable to get the field strength meter calibrated approximately and the easiest way of doing this is to use a signal generator, the earth of which should be connected to the positive rail. The output lead from
continued on page 365


THE need for this amplifier became apparent because of the reduction in signal strength when operating a portable radio in a car. Listening was made practically impossible, particularly to B.B.C. Radio 2. Although the set has a socket for a car aerial which is connected to a loop winding on the ferrite rod and a proper wing mounted car aerial was used. A large amount of interference was picked up even though the sparking plug leads were suppressed, the car generator output terminal had a $1 \mu \mathrm{~F}$ capacitor to chassis and the coil


Fig. 1 : The circuil of the signal booster.
switch terminal a $1 \mu \mathrm{~F}$ capacitor to chassis. This was due to the small signal producing practically no a.g.c. voltage, therefore the sensitivity of the set was maximum, making the set acutely responsive to electrical interference. The addition of this small r.f. amplifier made a vast improvement. The increased signal input to the ferrite rod pushes the set hard into a.g.c., cutting out the interference and making listening a pleasure once more.


The signal booster may be mounted inside the existing cabinet as shown.


Fig. 2: The component layout on Veroboard.

## CIRCUIT DETAILS

The circuit uses an AF117 transistor in the common emitter mode. The base bias is set by the negative voltage at the junction of R1 and R2 and by the voltage across the emitter resistor R4. C 2 , the emitter by-pass capacitor is to prevent the emitter resistor affecting the signal. The signal is applied to the base via C1, R3 is the collector load and the output is taken from C3. The total current drain from the nine volt battery is under 1 mA .

All the components except the switch are mounted on a piece of Veroboard $2 \frac{5}{8} \times 1 \frac{3}{8}$ ins. Only one break in the Veroboard is required, the hole for mounting is also drilled at this point. Component layout is shown in Fig. 2.

Two methods of housing the amplifier are possible. The authors method was to mount the amplifier inside the case of the radio with which it is going to be used. A small bracket was made on which a double pole switch is mounted, together with the amplifier. A thin piece of insulating material is put behind the Veroboard to insulate it from the


Alternative method of using the slgnal booster is to bulld It into a thn as shown above.
bracket. This method of housing can be used when there is sufficient space.
The second method, should it prove impossible to find sufficient space, is to build the amplifier into a small case as shown in the photograph with its own battery. A short length of co-axial cable is used to connect the amplifier to the radio via the aerial socket.

## 27MHz FIELD STRENGTH METER

-continued from page 363
the generator should then be held near the field strength meter aerial. The signal generator should then be set to 27 MHz and the field strength meter control VC1 tuned slowly for the maximum meter reading.
The dial reading on the field strength meter should then be noted and marked. This operation should then be repeated, with spot frequencies each side of 27 MHz until the full coverage has been calibrated. It should be stressed that the coil should not be bent or touched at all after calibration as this will certainly alter the readings.

## USING THE INSTRUMENT

When used to check a transmitter, the field strength meter should be held about 18 in . from the transmitter and adjusted for maximum meter reading. The dial setting can be compared with that obtained during calibration and this will indicate the transmitter's approximate frequency.

> See you at the R.S.G.B. Show August 19th-22nd

## THE

MW COLUMN


AUGUST marks the end of the summer season on the medium waves, the effect of the longer hours of darkness being apparent, even at the beginning of the month. North American stations are usually audible as early as 0030 hrs GMT. Canadians appearing first. Look for CBN 640 kHz St. John's Newfoundland; CBH 860 Halifax Nova Scotia; CJON 930 St. John's; CHER 950 Sydney N.S.; CHNS 960 Halifax; CKBW 1000 Bridgewater N.S.; CBA 1070 Moncton New Brunswick; CKEC 1320 New Glasgow N.S. Stations from the East Coast of the United States appear a little later, the more prominent being WNBC 660 kHz , WOR 710, WABC 770, WCBS 880, WINS 1010 all in New York City; WHDH 850 in Boston; WBAL 1090 Baltimore; WCAU 1210 Philadelphia; WKBW 1520 Buffailo N.Y. By 0230 hrs stations further inland may be heard:- WJR 760 kHz 'The Great Voice of the Great Lakes' in Detroit; WBBM 780, WLS 890, WCFL 1000, in Chicago; WHO Des Moines Iowa on 1040;' KMOX 1120 'The Voice of St. Louis'; WOAI 1200 San Antonio Texas. By the end of the month reception of the West Coast becomes possible from 0400 hrs GMT until sunrise. This is a favourable time of year for the West Coast since European QRM is light just before dawn while locals have not yet signed on. Last year the following stations were logged during the first week in September; KOMO 1000 kHz and KING 1090 kHz both in Seattle; KNX 1070 Los Angeles, KFBK 1530 Sacramento California. Others that might be heard are KSL 1160 in Salt Lake City Utah and KEX 1190 in Portland Oregon.

The recent interest in Vintage Radio brings to mind that early broadcast receivers operated mainly on the medium and long waves. Many of them could pull-in DX from North America, for in the mid-twenties it was not unusual to read of reception of stations such as 'WGY Schenectady N.Y. on 380 metres' by DXers using straight receivers and indoor aerials. The state of the MW band was more favourable for DX then, as there was little QRM while transmitters used flat-topped aerials which radiate lots of sky wave. Vintage receivers would hardly be successful on the medium waves today (though it would be intriguing to try one out), but many of the early stations are still broadcasting and are often logged by the DXer. WGY is currently on 810 kHz ; it was heard by the writey as recently as the 13 th of June this year. Older DXers may care to look for CBO 910 kHz in Ottawa; CBM 940 Montreal; KDKA 1020 Pittsburg; WBZ 1030 Boston; WBT 1110 Charlotte North Carolina; WHAM 1180 Rochester N.Y. A few old-timers have changed callsign. WEAF New York City is still on $660 \mathrm{kHz}(454 \mathrm{~m})$ but is now called WNBC. WLWL Cincinatti, which once had a power of 500 kW is now WLW 700 kHz with a modest 50 kW . It is interesting to note that a new 50 kW transmitter installed at WOR New York City ( 710 kHz ) during 1968 replaced one which had been in service continuously since 1922.

CHARLES MOLLOY


ALTHOUGH surplus crystals are readily available, cheaply and in large quantities, many of them are not marked with their frequencies or at best are marked with a code or 'channel' number.

While it is possible to get information to decode these numbers it is far simpler in the long run to make a direct check on the crystal to determine its fundamental frequency.

In some cases the frequency indicated on the crystal holder is an operating harmonic frequency and not the fundamental. So once again the necessity arises to find the fundamental by direct means.

It is possible to build a simple transistorised oscillator using the Pierce circuit so that just about any crystal plugged into it will oscillate.

But to determine the fundamental frequency of this crystal with a receiver can lead to false answers because of the several spurious signals that can be generated due to the beating together of oscillators in the receiver and the fundamental and harmonics of the crystal under test.

Fortunately there is a simple way by which the fundamental frequency of any crystal can be found quite accurately before a final precise measurement is made.

## Conventional use of GDO

All that is required is a Grid-dip Oscillator or g.d.o. This will normally have plug-in coils and a roughly calibrated scale for each range. It should be stressed that this calibration is really quite rough since the coil is subject to outside influences that can seriously affect the frequency at which the g.d.o. will oscillate.

In normal use the g.d.o. is loosely coupled to the tuned circuit being investigated and then tuned until grid current shown on its meter suddenly dips. Fig. 1.

The g.d.o. is then moved away from the tuned circuit to reduce the coupling until a good clean sharp dip is obtained on the meter. The g.d.o. should, if possible, be placed with respect to the tuned circuit, so that it does not have to be held in the hand.

It is at this point that the signal from the g.d.o.
can be picked up by a nearby receiver and its frequency determined. This is only an approximate answer since the frequency of the g.d.o. is being measured and not that of the tuned circuit itself.


Fig. 1: Conventional use of a g.d.o. to invesligate the resonant frequency of a tuned circuit.

It is no use getting a dip on a hand-held g.d.o. and then taking the g.d.o. across the room to a receiver and expecting the frequency to remain constant.

## Checking Crystals

When the g.d.o. is used to check the fundamental frequency of a crystal a slightly different technique is used. A few turns of wire are wound on a former which is slightly larger in internal diameter than the g.d.o. coils. The ends of the coil are connected to a suitable holder for the crystal, Fig. 2, but if it is


Fig. 2. Using a g.d.o. to "excite" a crystal at its fundamental frequency.
expected that a large number of crystals having different size pins and spacings are to be checked it is suggested that a permanent board be made up with a number of different holders, all connected in parallel.

The lowest frequency range of the g d.o. is chosen to begin with and its coil inserted into the crystal coil. Tuning from the low end to the high end of the range very slowly a dip will occur as soon as the g.d.o. passes the frequency of the crystal. At this point the crystal is absorbing power from the g.d.o. and it should begin to oscillate at its own natural frequency provided that the coupling between the coils is sufficient.

When the g.d.o. is used to check a conventional tuned circuit the dip in grid current takes the form shown in Fig. 3(a) but when it is used to check a crystal the form changes to that of Fig. 3(b). This is because the g.d.o. frequency becomes locked to that of the crystal once the crystal is oscillating and the tuning of the g.d.o. is ineffective over a small range and its frequency is precisely that of the crystal.


Fig. 3. (a) Grid current of g.d.o. when used conventionally as in Fig. 1. (b) grid current when used to "excite" crystal.

The g.d.o. frequency and hence that of the crystal can now be measured on a receiver in the conventional manner. Depending on the degree of accuracy of measurement required the calibration of the receiver should be cross checked against a standard crystal calibrator with $1 \mathrm{MHz}, 100 \mathrm{kHz}, 10 \mathrm{kHz}$ and possibly 1 kHz check points.
It should be remembered that in practice the precise operating frequency of the crystal will depend upon the type of circuit in which it is used. If it is necessary to order a crystal for a specific frequency from a manufacturer the type of circuit to be employed should be stated.

## Notes

The 'locking' effect, mentioned above, between the g.d.o. and the crystal is very marked but if it is not obtained during the initial tests the coupling between the coils should be increased by sliding the g.d.o. coil further into the crystal coil.

It is important to begin with the g.d.o. on its lowest frequency range, probably about $115-4 \mathrm{MHz}$, so that the crystal will oscillate initially on its fundamental frequency rather than on an overtone mode. If it should work on such a mode further confusion will arise if an attempt is made to measure the crystal frequency, because of the fact that overtone frequencies are not integral multiples of the fundamental frequency. On, say, the fifth overtone
the measured frequency may be several kilohertz different from the fundamental frequency multiplied five times.

## Alternative method

If a g.d.o. is not available a signal generator or a frequency meter may be used using the set-up shown in Fig. 4. The voltmeter should have a high resistance of about $10,000 \Omega$ /volt or a general purpose meter may be used on a low voltage range. A valve voltmeter will be more sensitive and should be used in preference to a conventional test meter.

The procedure is to tune the signal generator from its lowest frequency, about 1 MHz , upwards until a deflection is noted on the meter. In this case the peak indication is the point at which the crystal is resonant with the applied signal.

If the calibration of the signal generator is not to be relied upon then an external receiver can be used to measure the frequency as before. The author has found in practice that much too much faith is placed on the calibration of signal generators which do not have their own internal calibration facilities.

fig. 4. Use of a signal generator instead of a g.d.o. to determine frequency of crystal.

If the output of the signal generator has a calibrated attenuator the 'goodness' of the various crystals can be estimated by keeping the input voltage to the crystals constant and noting the relative deflection on the meter when the signal generator is tuned to the frequency of the crystal under test.
Once the fundamental frequency of a crystal has been found its performance in the overtone mode can be judged by applying signal voltages from the g.d.o. or the signal generator at the third, fifth or higher harmonics. The dip shown on the g.d.o. will be less than that obtained on the fundamental of the crystal and in the same way the output indication using a signal generator will be less, as the order of the harmonic is increased.
Crystals designed especially for operation on the overtone mode will naturally perform better in this test than those that are not, but after testing a number of crystals, the good and the bad will be obvious.

## "Praject autumn"

camp.te for the Practical Wireless

## "Designer's Jraphy"

see page 390

T
HIS is a self contained 13 note (single octave) organ pedal bass unit that can be used with any portable or domestic electronic organ having no bass note pedals of its own. It can be tuned to pitch without having to alter the tuning of the individual notes i.e., the pitch of the whole octave can be raised or lowered by approximately one full note.

It features a drum brush accompaniment that sounds each time a pedal is pressed regardless of whether the pedal is pressed and released quickly for a bass note of short duration, or the pedal held down to sustain the bass note. The drum brush sound begins with an attack and decays of its own accord.

The output signal level is sufficient for any external amplifier requiring not more than 1 volt r.m.s. signal input.

The pitch available is 16 ft . or 8 ft ., or 16 and 8 ft . combined. The 16 ft . octave is C to $\mathrm{C}(32$ to 65 Hz approx) and the 8 ft C to C ( 65 to 130 Hz approx). These two pitches are combined in equal proportions of amplitude when the $16+8 \mathrm{ft}$. pitch is used. The voicing is flute or clarinet which is fairly conventional for domestic electronic organs.

## Circuit



The block diagram (Fig.1) shows the general circuit arrangement which employs a total of nine OC71 transistors. The consumption is quite low so that operation from a PP9 ( 9 V ) battery is economical. There is little point, therefore, in making the


Fig. 1: Diagram showing the function of each slage of the Pedal Bass unit.


Rear view of unit shows, above, the circuit boards with the battery compartment to the right, and, below, the spring mounting of the pedals.

unit mains powered but there is no reason why this should not be done.

The main note generator is a multi-vibrator the output of which provides the 8 ft . pitch notes. The pitch for 16 ft . is obtained from a divider driven from the multi-vibrator. Then follows the voicing circuitry, the output of which is taken through a buffer amplifier and via a volume control to the output socket. The maximum signal level available at the
output is approximately 1 V r.m.s.
The drum brush circuit consists of a three stage white noise generator and filter, the output being controlled by a special attack-decay circuit (control amplifier). The drum brush signal is then attenuated to balance with the pedal bass output and passed to the buffer amplifier.

## Pedal Frame and Case

The basic pedal frame complete with the thirteen pedals mounted and sprung can be obtained readymade from Henrys Radio Limited (see materials list). The frame has a plywood top cover which is not required as a case to house the circuit boards and battery etc. has to be built up onto the frame itself. This top cover is $\frac{3}{8} \mathrm{in}$. plywood and can be used for making the end pieces of the case.

Those who wish to make the pedal frame and pedals will find the dimensions etc., in the various diagrams. The main frame is shown in Fig. 2 (A and B) and made from soft planed wood. Note that the rear member of the frame (the pedal support rail) is bevelled to the dimensions given in Fig.2B. The front main member of the pedal frame is fitted with guide posts for the pedals as shown in Fig.3. These posts are made from $\frac{5}{16}$ in. diameter dowel and are glued in so that they just clear the upper pedal stop rail (see inset Fig.3).

Next, the pedals themselves should be made and checked for fitting within the frame but not secured until the case frame work has been completed. Details of the pedals ( 8 white and 5 black) are given in Fig.4. Note the soft leather or plastic binder around each pedal, a couple of turns of adhesive plastic insulating tape will do, and also the small hardboard pads which press on the keying contacts.
Each pedal is secured to the rear member of the main frame by means of a flat phosphor bronze spring, details of which are given in Fig.5. Do not bend these strips, they will bend themselves (Fig.6) when the pedals are finally fitted, and the springs secured to the rear pedal support rail.


Fig. 2 : Constructional details of the wooden pedal frame of the unit.


Fig. 3: Positioning of the pedals on the frame. Compare with the heading photograph of the completed unit.


Fig. 4 : Details for making the key pedals.


Pedal spring - one on each pedal - underside
Fig. 5: Details of the phosphor bronze springs and their fitment to the pedals.


Fig. 6: Fitting of the springs to the pedal frame unit.


Fig. 7: Construction of the framework for the case.

Before fitting the pedals the case must be completed by first making and assembling the two end pieces (Fig.7C) and then by building up the framework. (Figs.7A and Fig.8). Note the shape of the upper pedal stop rail (Fig.7A). Wood of this shape can be obtained from most D.I.Y. decorating materials shops.
The alternative would be to use a rail $1 \downarrow \times \frac{1}{\ddagger}$. and drop the front panel accordingly. The frame members, (Fig.8) can be glued in place with Evostik. Leave the 'lower rear member' (Fig.8) until the pedals have been secured in place.
Pieces of hardboard cut to appropriate size can be glued to the frame members to form a box for the PP9 battery at the right hand end of the frame (looking from the rear) as shown in the photograph.

## Contact Rail and Keying Contacts

The contact support rail is ' $U$ ' shaped aluminium channelling and fits underneath the pedal frame in the slots at the sides (Figs. 2A, 3, 7A and 9). Dimensions and drilling details for the rail are given (Fig.10). Note that the fixing holes for the contact assemblies must be $3 / 32 \mathrm{in}$. in diameter to take the self tapping screws supplied with them.

The contact assemblies have two pairs of contacts -one pair make as the other pair break and each pair is isolated. The press-to-make pair are used for keying the pedal bass notes and the press-tobreak pair are used for actuating the drum bush sound.

The thirteen contact assemblies are mounted on the rail (Fig.10, inset) and the rail is then attached to the pedal frame so that the contact sets are uppermost beneath each pedal (Fig.9). Note the clearance for the downward movement of the pedal. To obtain the requisite spacing between the contact actuating buttons and the pads on, the pedals small spacers can be fitted between the contact rail and the slots in the pedal frame.

## materials list

Planed wood for pedal frame and pedais. (The frame and pedais may be obtained, ready-made, from Henrys Radio Ltd. Type 13/2).
Pedal contact set (13 off), Leaf type, 1 pair make, 1 pair break. (Henrys Radio Ltd.) Aluminium U channelling, $\frac{1}{2} \times \frac{1}{2} \times \frac{1}{2}$ in, $20 \frac{3}{3}$ in. long.
Aluminium sheet, 18 s.w.g. for output socket panel. Plywood, woodscrews, etc.


Fig. 9 (below): Final assembly of the pedals and their positioning



# OW BAND VIF GONVERTER 

CONSIDERABLE importance is attached by the author to the reception in this country of 'paging' stations operating in the United States on frequencies around 35 MHz . Not from any 'eavesdropping' aspect but as a check on the upward movement of the m.u.f. and the possibilities of reception of signals via the F2 layer.

The writer's interest lies with v.h.f. propagation, 30 MHz and above, so with the increased activity in the low v.h.f. band over the past few years, due to maximum sunspot activity, need was felt to cover this part of the spectrum with something better than a modified RF25 unit. The RF25 unit, having switched positions, gave only limited coverage. It had been set to the main paging station frequencies, so coverage was inefficient at frequencies removed further than 500 kHz from the preset position. Accordingly, a simple converter was made, using commerciailly available coils, giving fully tunable coverage from 26 MHz to 53 MHz .

## Circuit

Basically the unit (Fig. 1) contains an r.f. stage using an EF80 or EF184 pentode, feeding into an ECF80 frequency changer. Internal coupling between the triode oscillator and pentode mixer is sufficient for frequency conversion to the i.f. of 5 MHz . The output from the frequency changer feeds into an i.f. amplifier, prior to feeding into the main receiver. By using an i.f. of 5 MHz , the main receiver can be accurately set to 5 MHz on a standard frequency station, before inserting the converter output. An alternative circuit is given (Fig. 2) for using an ECC84 cascode stage. No r.f. gain control is fitted, but those readers living adjacent to a channel B1 transmitter may find one necessary to prevent overload (Fig. 3).

## Construction

The layout of the various components can be seen from the photographs. The usual precautions of short, direct wiring and single earthing points for each stage should be observed.



Fig. 2. Alternative r.f. stage using the cascode circuit.
The five coils are mounted on a sub-panel with shields between the coils. The power supply is fed into the unit via a four pin socket but constructors may wish to make their own arrangements in this respect. Likewise a suitable dial can be fitted and calibrated after the alignment of the unit has been finished.

## Alignment

The alignment of the converter is simple. Inject a low level modulated signal at 5 MHz to pin 2 Valve 3. Adjust the core of L5 to give maximum reading on the main receiver ' $S$ ' meter, or for maximum sound output with the a.g.c. switched off. Now shortcircuit the oscillator section tuning gang to


Fig. 3. Modified circuil incorporating an r.f. gain control.
chassis, and inject the 5 MHz signal to pin 2 of Valve 2. Adjust the core of L4 to give maximum readings as before. Remove the shortcircuit and adjust C 11 to approximately one third value. Find a signal such as Crystal Palace sound on 41.5 MHz , and align L2 to give maximum signal. Alternatively inject low level signals from a signal generator at about 40 MHz and adjust the core of L2. Check that the range $30-50 \mathrm{MHz}$ is covered, then seal C 11 with wax to prevent movement.

Denco recommend that 50 pF tuning capacitors are used, but at the time of construction a 3 -gang unit of these values was not available, hence the use of a Jackson 3 -gang 75 pF unit was necessary, which tends to increase the l.f. coverage below 30 MHz . It may be found that performance falls off below 26 MHz , due to the low value of C 11 . Increasing its value to improve the l.f. coverage tends to deteriorate the h.f. performance at 50 MHz . So C 11 should be set for optimum v.h.f. reception.

## General Notes

During the daytime, particularly in winter at sunspot maximum, a considerable number of signals may be heard, often above the m.u.f. listings and predictions. From the east, forward - scatter networks and r.t.t.y. may be heard from the USSR. The most spectacular reception may be heard from the west, particularly from the United States. A large number of domestic services, such as waterworks undertakings, gas suppliers, private individuals and shops have 2-way communication circuits between 30 and 45 MHz , and both base stations and mobiles can be heard in communication.
The most important frequencies are $35 \cdot 22,35 \cdot 58$, $43 \cdot 22,43 \cdot 58 \mathrm{MHz}$. Paging stations are situated in most towns, and in some cities there may be three or more. A subscriber carries a small radio receiver,
tuned to the paging station. If the subscriber leaves his office or home, and is wanted urgently, he is paged by the transmitter. Each transmitter will repeat the message on a tape loop, interspersed with its identification. Consequently it is extremely easy to identify and locate these transmitters by the call sign, and in most cases, the name of the town is given.

## components list

## Resistors:

| R1 |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | $100 \Omega \frac{1}{}$ | R6 | $10 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ |
| R2 | $100 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R7 | 150 $\frac{1}{2}$ W |
| R3 | $120 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R8 | $2 \cdot 2 \mathrm{k} \Omega 5 \mathrm{~W}$ |
| R4 | $470 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R9 | $2 \mathrm{k} \Omega 3 \mathrm{~W}$ |
| R5 | 39k $\Omega 1 \mathrm{~W}$ | R10 | $270 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ |
| VR1 | 5K WW pot | R11 | $270 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ |
|  |  | istor | S $\pm 20 \%$ |

## Capacitors:

| C1 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc | C13 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |
| :---: | :---: | :---: | :---: |
| C2 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc | C14 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |
| C3 | 100pF 500 V | C15 | $35 \mathrm{pF} 500 \mathrm{~V} 1 \%$ S.M. |
| C4 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc | C16 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |
| C5 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc | C17 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |
| C6 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc | C18 | $0.05 \mu \mathrm{~F} 500 \mathrm{~V}$ |
| C7 | $0.05 \mu \mathrm{~F} 500 \mathrm{~V}$ | C19 | 1500 pF 500 V |
| C8 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc | C20 | 1500 pF 500 V |
| C9 | 100 pF 500 V | C21 | 1500 pF 500 V |
| C10 | 35 pF 500 V | C22 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |
| C11 | 10 pF trimmer | C23 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |
| C12 | 500pF 500V 1\% | C24 | $0.005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |

VC1-2-3 3 gang 75pF per section (Jackson E3)
Inductors:
\(\left.\begin{array}{ll}L1 \& Blue -Range 6 <br>
L2 \& Yellow-Range 6 <br>
L3 \& Red —Range 6 <br>
L4 \& Yellow-Range 3 <br>

L5 \& Yellow-Range 3\end{array}\right\}\)|  |
| :--- |
| Denco, miniature dual |
| purpose |

Valves:
V1, 3 Ef80 (or EF184)
V2 ECF80
V4 ECC84
Miscellaneous:
Chassis $9 \times 5 \times 2 \frac{1}{2}$ in. Slow motion drive and knob. 3 B9A Valve holders and screens. 2 co-axial sockets. Tag strips. 4 pin socket.

A number of paging stations is given, but this is only a few of the many presently transmitting, those listed having been received by the author.

|  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| KIF | 651 | Ft. Lauderdale | Fla. | $35 \cdot 58$ | MHz |
| KIY | 508 | Orlando | Fla. | $35 \cdot 22$ |  |
| KEC | 519 | Rochester | NY | $35 \cdot 58$ |  |
| KCC | 482 | Pembroke | N. Hamp. $35 \cdot 22$ |  |  |
| KQQ | 303 | Detroit | Mich. | $35 \cdot 22$ |  |
| KIQ | 510 | Jacksonville | Fla. | $35 \cdot 58$ |  |
| KIM | 905 | Charlotte | N.C. | $35 \cdot 22$ |  |
| KGC | 400 | Scranton | Penn. | $35 \cdot 58$ |  |
| KGC | 266 | Allentown | Penn. |  |  |
| KGC | 223 | Philadelphia | Penn. | $35 \cdot 22$ |  |
| KKI | 445 | Houston | Tex. | $35 \cdot 58$ |  |
| WWA. 335 | San Juan. | P. Rico | $35 \cdot 22$ |  |  |
| KKM | 248 | Oklahoma City | OkI. | $35 \cdot 58$ |  |
| KGC | 397 | Wilkes Barrie |  |  |  |
| KIF | 650 | Birmingham | Ala. | $35 \cdot 58$ |  |
| KIE | 953 | Atlanta | Ga. | $35 \cdot 58$ |  |

During good conditions in the winter of 1969 , stations as far west as KKI 445 Houston and KKM 248 Oklahoma City, both on $35 \cdot 58 \mathrm{MHz}$ were heard. Usually reception is easiest from the east coast, and especially down to KIY 508 Orlando, Fla. One rare pager, only heard twice here is WWA 335 San Juan, P . Rico on $35 \cdot 22 \mathrm{MHz}$. The aerial in use for these various signals in the lower v.h.f. band has been a vertical 12 foot whip. Activity in the west is usually from 1300-1800 b.s.t.
The Worldwide TV-FM DX Association often publishes articles and lists on activity within the $30-40 \mathrm{MHz}$ spectrum, in addition io their normal coverage of t.v. and f.m. DX proper. Information on this club may be obtained from W.TV.FM. DX Assoc., P.O. Box 5001. Harbor Sta., Milwaukee. Wis., 53204 U.S.A. For a sample bulletin enclose 2 IRC.

It should be pointed out that reception upon these high frequencies of ionospheric signals is dependent on sunspot activity (other than sporadic E). Consequently, there may be periods during which little or no activity is heard. However conditions can improve over the space of a few days. During January, 1970, the highest frequency noted was $39 \cdot 8 \mathrm{MHz}$, after which conditions deteriorated.

It must be stressed at this point, that NO ATTEMPT MUST BE MADE TO VIEW THE SUN DIRECTLY, to observe sunspot activity. One second is sufficient to damage the eye. A telescope on a tripod may be used to project the sun on to a card, and spots can then be observed upon the card, indicating sunspot activity.

Never look at the sun through a telescope, even though it may be supplied with a special filter to fit over the lens. These filters can fracture under concentrated heat. Even when the sun is setting, no attempt must be made to view the sun directly.

## "PROJECT AUTUMN"

Are you entering for the competition?
Are you stuck for ideas?
What about designing:-
A cassette tape recorder?
A general purpose oscilloscope?
A car radio/tape player?
An intercom system for the home?
A wavemeter to comply with the amateur transmitting service regulations?

See page 390 for details of
"PROJECT AUTUMN"

JULIAN ANDERSON
A series of simple transistor projects, each using less than twenty components and costing less than twenty shillings to build.

THERE is one piece of equipment that all of us own (if we take the hobby at all seriously) and that is a multimeter. These cost anything from under $£ 2$ to over $£ 30$ though the majority fall in the $£ 3$ to $£ 7$ range. Although all of them will measure voltage, current and resistance the ranges are often inadequate, especially on the cheaper types. For a few bob several additional features can be added to the cheaper and simpler testmeters. We shall describe four circuits but with a little imagination and application of Ohms law it will be seen that still further ranges can be added.

## TRANSISTOR TESTER

Many readers will occasionally wish to test transistors but do not feel that the construction of a separate piece of equipment is justified. For these people a separate and simple circuit can be kept for the odd occasions on which it is needed-the cost should be no more than a few shillings as it uses only a three-pole four-way switch and a $100 \mathrm{k} \Omega$ resistor.

Although this tester only measures the transistor using the internal battery (almost universally 1.5 V in the cheaper range on multimeters) it will give an


Fig. 1: The clrcuitry necessary for converting a multimeter to a transistor tester.
indication of leakage and gain. In position A the meter's battery negative is applied to the collector and the positive to the emitter, the resistor connected between the collector and the base applying a bias of about $10 \mu \mathrm{~A}$. A good device should show quite a deflection on the scale. In position B the bias is removed and the meter indicates the leakage. Positions C and D do the same for NPN transistors. Note that there is not a mistake in the circuit; the positive connection to the meter is in fact connected to the battery negative.

## LOW VOLTAGE RANGE

The base bias voltage on transistors is usually

No. 17
MULTIMETER EXTRAS


Fig. 2: Adding a $1 V$ range is a simple matter but refer to the text for the value of $R x$
between 0.3 V and 0.8 V but only a few meters have a 1 V range. However this can be added simply by the addition of a resistor. With the meter on its lowest current range and a resistor equal to the meters sensitivity a 1 V range is added. Thus a $1,000 \Omega / \mathrm{V}$ meter would need a $1 \mathrm{k} \Omega$ and a $20,000 \Omega / \mathrm{V}$ meter a $20 \mathrm{k} \Omega$ resistor. Unfortunately the internal resistance of the meter has to be subtracted from this. The simplest way to find the correct value is to fix a $100 \Omega$ pot across a 1.5 V battery and adjust so that a 1 V reading is obtained on your testmeter. This should be done with care as the accuracy of the scale will depend upon it. Then change over to the lowest current range and select a resistor that will give full scale deflection from the 1V supply. This will probably mean using two or even three resistors in series; once the exact value has been found the resistors can be soldered together.

## A.C. CURRENT RANGE

Only the most expensive multimeters include an a.c. current range and although this is rarely needed it is sometimes necessary to measure mains current. If a $1 \Omega$ resistor is inserted in the line a 1 A current will drop 1 V and a $10 \Omega$ resistor will drop 10 V and of course we can measure a.c. volts. We won't attempt to describe this further but make sure that the resistor is a high wattage type and if used on the mains that careful insulation is used (we don't want to lose too many Take 20 readers!).

## HIGH RESISTANCE RANGE

Many of the cheaper meters have very inadequate resistance ranges-the centre scale reading is usually only $3 \mathrm{k} \Omega$ and it is practically impossible to get an accurate reading over $50 \mathrm{k} \Omega$. The additional com-


Fig. 3: A high resistance range can be added to nearly all test meters by using the above arrangement on the lowest current range.
ponents in Fig. 3 will improve the best resistance range by a factor of 10 . Again we use the meter on it's lowest current range and instead of the integral 1.5 V battery we use an external 15 V one (B154 or similar). The combined resistance of VR1 and $\mathrm{R}_{y}$ should be $15 \mathrm{k} \Omega$ for a $1,000 \Omega / \mathrm{V}$ type and $300 \mathrm{k} \Omega$ for a $20,000 \Omega / \mathrm{V}$ meter so for the former type a $12 \mathrm{k} \Omega$ resistor and a $5 \mathrm{k} \Omega$ pot should be used.

#  

IN presenting this month's integrated circuit there is the question of whether or not it would fit more appropriately in the "Take 20 " slot, since the unit in question, the Motorola MFC4000P, costs little more than $£ 1$, and to date is probably the simplest unit to use. In a package occupying less than 1/100th of a cube inch it provides a $\frac{1}{4}$ watt audio amplifier, matching a 16 ohm loudspeaker.

To add to the simplicity, only four leads connect the silicon monolithic chip to the outside world, d.c. power supply, signal input and output, and a common earth. The unit is the first of a series of "consumer" circuits, intended for the amateur constructor and for manufacturers of utility equipment such as portable radios and baby alarm or intercom units.


Fig. 1. Equivalent circuit of the MFC 4000P
As such, it does not match the G.E series of audio integrated circuits introduced to our readers in March 1970 "P.W.", or the increasingly familiar Plessey SL403, which are essentially hi-fi devices with internal noise levels 65 dB . or more down, or with less than $0.5 \%$ total harmonic distortion.

On the other hand, those devices require feedback and decoupling connections to the chip, with multiple pins and an external metallic heat sink. Further, previous audio units required a d.c. supply
higher than the 9 volt battery which powers the standard pocket radio or domestic transistor device: the MFC 4000 P on the other hand, will operate at full rating down to 6 volts d.c., though with the harmonic distortion raised to $4 \%$ due to crossover difficulties. At a nominal 9 volts a harmonic distortion figure of $0.7 \%$ is attained, a better performance than is common in the standard pocket radio preamplifier, driver and class B output lineup.


Actual size of the MFC 4000P. The dot identifies pin 1 , the numbering going clockwise

Finally, the device is used in a completely transformerless circuit, enabling a degree of compactness to be achieved previously unobtainable in home built equipment. In use, the slightly higher noise and distortion figures are not significantly reflected in the output sound, since in the type of equipment for which this unit is intended, quality is inevitably loudspeaker limited, and there is no advantage to be attained by incorporating more expensive semiconductor complements.

## Circuit

Now for a brief consideration of the circuit itself, Fig. 1. It is a six transistor unit, with Tr1 acting as a stabilising element across the input, and therefore controlling all stages of the direct-coupled circuit. The preamplifier transistor, $\operatorname{Tr} 2$, is in an orthodox common emitter configuration and biased by d.c. feedback from the output stage of the circuit (shunted, as mentioned already, by the regulator Trl. which however, does not affect the signal appearing at the base of $\operatorname{Tr} 2$ since the collector circuit of a transistor has a high impedance to applied signals).

It will be noted also that there is also a frequencydependent element (the $0.003 \mu \mathrm{~F}$ capacitor) in this negative feedback loop to determine the frequency response of the complete amplifier, Fig. 2.

The driver transistors, Tr3 and Tr5, are a complementary pair, as indicated by the direction
indications on the emitter symbols. Therefore, although the same signal is applied to each from the collector of $\operatorname{Tr} 2$, there is $180^{\circ}$ phase difference between the signals passed on to the output pair, since $\operatorname{Tr} 3$ may be regarded as an emitter follower while $\operatorname{Tr} 5$ is common emitter and therefore signal inverting. Tr4 and Tr6, then, act as class B push-pull output transistors.

However, due to the presence of the diodes and small resistance between the bases of $\operatorname{Tr} 3$ and $\operatorname{Tr} 5$,


Fig. 2. Circuit of an audio stage suitable for a pocket radio
there is a small standing current in the output pair even in the no-signal or quiescent condition, to minimise the crossover distortion sometimes found in class B systems.
In practice, the current drain of the circuit rises from an average of 3.5 mA in the quiescent condition to 60 mA on full load. The advantage of class B operation, with battery drain highly dependent on output, is evident. Sensitivity is high, with a power output of 50 mW (average pocket radio listening level) a vailable on an input signal of only 15 mV , but Fig. 3 indicates the use of an external preamplifier should one be desired for special low-signal applications, such as operation from a tape head. Otherwise the circuit shown in Fig. 2 should be fully satisfactory.


Fig. 3. Alternative circuit using a discrete pre-amplifier
It is hoped to introduce shortly the Motorola MFC4010P, as the next element in this series of sub-miniature 4 -pin i.c.'s (it is a general purpose direct coupled amplifier, for a.f. or i.f. applications); until then, this attractive little unit should provide food for thought and work for the soldering iron! The unit is available from Jermyn Industries, Vestry Estate, Sevenoaks, Kent or Henrys Radio Ltd. who can also supply the transistor MPS A70.

## RADIO ENGINEERING AND COMMUNICATIONS EXHIBITION

If you're in Town Aug. 19-22, pop along to the above exhibition and see our latest designs. Venue is Royal Horticultural Society's New Hall, Greycoat Street, Westminster, London, S.W.1.
Exhibits include: Light Beam Phone; Vibrasonic Guitar Amp.; Organ Pedal Bass Unit.

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## COLOUR TELEVISION

Two features next month on colour television. First a detailed look at burst and automatic chrominance control circuitry, including a pulse generator stage of a type which has not previously been used in domestic TV equipment.

Secondly an account of the various types of tubes that can be used to display colour pictures, beam masking, deflection and indexing types, their advantages and disadvantages. Includes a description of the Sony Trinitron and the "Essex" tube which could lead to big changes in TV receivers.

## ELECTRONIC VIDEO RECORDING

EVR is due to be with us soon and brings with it many new techniques. Next month we publish a detailed account of the system with a block schematic and description of a colour EVR teleplayer.

## LOG-PERIODIC AERIAL

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NOW that the name of Hertz has come into everyday use in the jargon of the electronic engineer it is perhaps opportune to look back at the work of that early pioneer in radio communication, Professor Heinrich Hertz, and to consider whether or not the perpetuation of his name as a technical term is really justified.

Heinrich Hertz, born in 1857, became a pupil of the famous physicist von Helmholtz and received a good grounding in electricity as far as the "state of the art" permitted at that time.

Although dying in 1894 at the early age of 36 Hertz was able to carry out many experiments that had the most far reaching effect on man's attempt to communicate at a distance.

In 1888 Hertz had progressed enough to be able to demonstrate the propagation of electromagnetic waves, or Hertzian waves as they were then known, thus confirming the earlier theoretical work of Maxwell.

Hertz showed that the waves conformed to the same laws as applied to the propagation of light namely that they could be bent and reflected.
Earlier experimenters had noticed spurious effects in the vicinity of large spark coils, when they were operating, such as secondary sparking between metal objects completely isolated from the coil.

Among those experimenters was Edison who coined the phrase "etheric force" to explain away the effect of secondary sparking at a distance.

Hertz's "receiver" consisted of nothing more than a length of wire formed into a circle leaving a minute gap at the ends across which a spark would jump when Hertzian waves were induced into the loop from the nearby spark coil "transmitter".

Hertz found that he could increase the effective range of his equipment by adding metal spheres and plates to the spark gap on the transmitter and to the ends of the receiver loop. He was in fact using what we now call "dipoles" and towards the end of his experiments Hertz was able to "resonate" his transmitter and receiver to approximately the same wavelength. The frequencies involved were in fact what we would now term v.h.f.!

As if these incredible experiments were not enough Hertz then demonstrated the phenomenon of "standing waves" using a long cage of wires strongly resembling the present-day Lecher wire system of measuring wavelength.
Using sheet metal reflectors and reflectors made of wire stretched on wooden frames Hertz showed that his Hertzian waves could be treated as light waves and bent or reflected at will. Little did Hertz realise that he was really demonstrating the basic principle of radar!

"Crown Copyright, Science Museum, London'"

Since many modern v.h.f. and u.h.f. aerial systems strongly resemble the equipment used by Hertz in his famous experiments it would not be ungenerous if he were to be regarded as the "father" of v.h.f. communication. It is surely little enough reward for his name to be associated with the basic unit of frequency, the cycle per second, or Hertz (Hz), since he was the first to devise a method of measuring the frequency or perhaps the wavelength of electromagnetic waves.

## fltobile 1922

IN 1922 experiments were being made with radio receivers in cars and there follows a description of one of the first car radios: "The receiving apparatus used is a Marconiphone 6 -valve set, five of the valves being high-frequency amplifiers and the other a rectifier. The valves are of the special lowcurrent consumption type. The aerial is fitted on the roof of the car and is so constructed that it can be raised and lowered at will by means of a hand-wheel.
"The receiver is bedded in spongy rubber and mounted in a compartment under the floor boards immediately in front of the rear seats. Control is effected by means of three levers in the car interior


## Hintage $\mathbb{C O}$

Should readers wish to have a "Vintage CQ" published, we will be prepared to accept letters for inclusion. They will of course be inserted in the magazine when space permits and will be dealt with

Therefore, if you have any queries on old gear, want to exchange or obtain vintage equipment, books, etc., drop us a line and we'll put a note in
and on the control panel there is an indicating 'pilot' bulb which shows the intensity of the filament lighting of the valves. The valve filament lighting is effected from the starting and lighting battery of the car. High-tension batteries of the usual type are fitted in the same compartment as the receiver. In order to prevent interference from the ignition and lighting equipment of the car, the magneto and generator are screened.

Two pairs of double earpieces and two single earpieces may be employed, so that four persons can listen in at once.

The effective receiving range of the equipment is approximately fifty miles radial distance from a broadcasting centre when used with the frame aerial fitted to the car roof. When all the broadcasting stations are in operation a car fitted with this apparatus, will, therefore, practically be within range of broadcast."

This pholograph shows a Daimler car equipped with a Marconiphone receiver and frame aerial. A similar car was used in the Lord Mayor of London's procession 1922.

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## FURTHER

 NOTESSince the appearance of the LF bands transmitter/ receiver in the June/July 1970 issues of "Practical Wireless" it is apparent that the v.f.o. coil unit is no longer available. There has also been interest in 2 -band switching for the equipment. This has been employed for some time with excellent results, and results on 80 m have been surprisingly good.

## The VFO

Fig. 1 is the circuit of a v.f.o. which can be built in the original v.f.o. box, using easily obtainable components, and giving correct coverage for both 160 m and 80 m , with the minimum of difficulty.
There are three $1 \%$ silver mica capacitors, and the coil is a Denco (Clacton) Ltd. "Yellow" Range 3. It is mounted inside the box, with the threaded rod protruding. So that all circuits can be screened, the holder for the EF91 was mounted on the box, and thus encloses all the components in Fig.1. The r.f. choke is a miniature cored type (as used in transistor receivers).

It is only necessary to adjust the core of L1 until coverage is from 1.75 MHz to 2.0 MHz , with a little to spare at the extreme settings of the v.f.o. tuning capacitor.

For 160 m , the dial is calibrated from $1 \cdot 8-2 \cdot 0 \mathrm{MHz}$. For the 80 m band, frequencies from $1.75-1.9 \mathrm{MHz}$ are doubled, giving coverage of 3.5 MHz to 3.8 MHz .

## Buffer and PA

Fig. 2 shows the switching of the buffer amplifier and p.a. circuits. S1 is a single pole 2 -way rotary wafer switch, mounted under the chassis, below the v.f.o. tuning control. L2 is for 160 m , and is a Denco "Blue" Range 2 coil, with the small coupling winding wholly removed. L3 is for 80 m , and is a Denco "Red" Range 2 coil the small winding being removed, and 28 turns taken off the tuned winding.

These coils are under the chassis, with the threaded rods above. The switch S 1 is set for 160 m , the v.f.o. tuned to about 1.9 MHz , and L2 core peaked for best p.a. grid current. With the v.f.o. tuned to about 3.7 MHz , and S 1 at $80 \mathrm{~m}, \mathrm{~L} 3$ is similarly adjusted.



Fig. 1. (above) shows the circuit of the modified v.f.o. stage using readily aval/able components.
The photograph (left) will assist in identifying the additional components required for 2-band operation. The receiver bandswltch is below the receiver tuning dial at the left of the panel. The b.a. bandswitch S1 is below the v.f.o. d/al, centre. The p.a. bandswitch is located in the top right hand corner of the panel.

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# practically wireless commentary by ILIIII 

THE paths of progress are many and devious. Woe betide the inventive gambler who stakes his all on a technical dead-end. Pitying, progress watches the John Logie Bairds picking up the shards of mirror from a dusty floor, and sweeps on to electronic miracles that we unfeeling fellows take in our stride.

The rewards of progress come closer home. Henry is inspired this month by a recent visit to a Mullard Film Show, where Ian Nicholson was in fine form. chiding his audience because they dared to query the reliability of integrated circuits, and were so reactionary as to want plug-in devices.

Plugs and sockets are a technological cul-de-sac, we were given to understand. Despite the arguments of some industrial electronics boys who were slumming in Bristol that night, the signposts decidedly pointed to a 'solder-in, de-solder out' future, with aspirated soldering irons and a ruined 'chip'. 'What does it matter, if you have to break it to take it out?' said Mr. N., 'If you test intelligently, you will know it is faulty before you get to that stage. The emphasis must be upon logical diagnosis.'

But, of course, the implication was that things never went wrong


He can be a tongue-tied mug.
with Mullard chips, and when one chap persisted he was asked in what sphere these plug-in whatsits were to be found. It turned out that he was a shipboard electronics engineer. 'Oh, that explains it,' said Mr. Nicholson, 'I-Cs on the 'igh seas.'

Henry often wishes he had the gift of turning away the awkward question and dissolving his audience in friendly laughter. When things go wrong at one of his lectures, he can be a tonguetied mug. Only last week there was the most appalling faux pas.

The occasion was a lecture on recording, and a number of musical illustrations had been taped. For the purposes of demonstration these were at different speeds and as is usual with one of Henry's lectures, time had us all by the forelock. A complicated chart had to be drawn on a rickety blackboard, demanding the utmost concentration, both to prevent the latter falling and the former degenerating into illegible graffiti. Henry craftily set the trusty 2000 in motion as he drew . . . and drew. . . .

Minutes later, as a man dredges up his consciousness from dreamland, Henry became aware of something vaguely wrong. The horns of the New York Philharmonic had never sounded like that, no, not even in Mahler's day.

I am ashamed to say that, without blinking an eyelid, our villain said: 'Let's go on to the third movement,' and while winding the tape forward, slyly switched the tape recorder to its higher, correct speed. And none of the class protested, although one did telephone the next day to say: 'What was that piece you played just after the interval?'


Such a contretemps can happen to anybody. In the wireless world it happens even to the boffins. A little while ago, the British engineers at the Gloucester factory of Bang \& Olufsen were instructed by their parent factory in Denmark to make one or two modifications to a stereo tuneramplifier to cure 'viups'. Their radio wizard made the changes and noted an improvement in stability, especially at the top of the medium wave band.

A message went off to Denmark: 'Viups cured-what are they please?' And the answer returned from the Danes: 'Isn't it obvious? That's the sound the receiver makes when the fault is present!' And it was.

By the same token, Henry's new FET-IC tuner has a fault best described as Fizzz-crick-Hhbh!

But the trouble there is very simple; largely mechanical. Henry is patiently waiting for Gordon King or one of his colleagues to publish another of those revealing articles in Practical Wireless which show how an effective loft FM aerial for stereo multiplex FM reception 80 miles from the transmitter in the shadow of a hill can be constructed from a bale of chicken wire and a few lengths of wood batten.


## RULES.

1. Articles submitted for the competition should conform to the general style of material publlshed in Practical Wireless and must describe the operation and construction of a piece of radio, audio or test equipment that has been designed and built by the author.
2. Articles should, preferably, be typed using double spacing, leaving wide margins, and on one side only of each sheet. Circuit diagrams and any other drawings should be on separate sheets and numbered to agree with the text. Author's roughs must be clear enough to permit re-drawing. Component liste must also be separate and laid out to the standard PW format.
3. Photographs of the equipment are desirable and should be in black and white, sharp and clear. Each photograph should be identified by sticking a piece of paper on the back rather than by writing on the photograph itself.
4. Components used in the design must be readily available from retail sources.
5. An entry form, properly completed, must accompany each article submitted. There is no limit to the number of articles submitted by any one author.
6. Articles must reach the Editor, Practical Wireless, Old Fleetway House, Farringdon Street, London, E.C.4. by the first post on Monday, November 2nd 1970 with the envelope and title sheet clearly marked "Project Autumn". A stamped, self-addressed envelope must accompany each entry.
7. All entries submitted will be considered by a panel of judges and the Edltor's decision on all matters arising will be final. The Editor will require authors of winning entries to submit the equlpment to him immediately on request for final assessment by the panel.
8. Employees and staff of Practical Wireless are not eligible for entry to this competition.
9. The winner of the competition will receive and retain outright the Practical Wireless "Designer's Trophy $1970^{\prime \prime}$. Other prizes will be awarded to the best pun-ners-up. Any article published will be paid for at normal rates.


Fig. 2. Switching arrangements for 2-band operation of the b.a. and p.a. stages.

Lock v.f.o. and buffer/doubler cores with 6BA nuts. On 80 m S 2 shorts out one-half of the tank coil and is a toggle switch, fitted to the panel immediately behind the coil.

## Receiver Coils

Readily-available Denco coils are used for 160 m and 80 m , in the receiver section, Range 2 coils for 160 m , and Range 3 coils for 80 m . "Blue" coils are required for the aerial circuit, "Yellow" coils for the mixer grid, and "Red" coils for the oscillator.
The Range 2 "Blue" and "Yellow" coils each have 32 turns removed from the tuned winding.

Count these as they are unwound, and re-solder the wire to the pin. The "Red" coil for this band has 20 turns removed from the tuned winding.

A rotary wafer switch with three wafers, each having 2 -pole 2 -way seotions, is fitted under the chassis below the ganged tuning capacitor. Connections for the coils are as follows:

Blue. 1 and 9 to chassis. 8 to aerial, via switch. 6 to r.f. grid, via switch.
Yellow. 8 to h.t. positive. 1 to chassis. 9 to r.f. anode via switch; 6 to mixer grid via switch.
Red. Range 2: 9 to chassis. 2 to 300 pF padder, returned to chassis. 8 to oscillator anode capacitor via switch. 1 to oscillator grid capacitor via switch. Range 3: As Range 2, but no padder and pin 3 wired directly to chassis.
An individual 60 pF trimmer is wired across the tuned section of "Yellow" and "Red" coils. Aerial coils are peaked with the panel trimmer. Coverage is of the 160 m and 80 m bands, with a little to spare, and the cores and trimmers are adjusted in the usual way.

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# A <br> TWO-TONE <br>  

## A.S.CARPENTER G3TYJ

THERE is nothing unique in the circuitry presented here being rather a practical presentation of a transistorised device very useful in the modern amateur radio station. The device may also be used in other ways as will be mentioned later. It is easily copied and can be constructed in a few hours and will cost approximately 35 s . even if every item has to be purchased. As the illustration shows the finalised unit is attractive in appearance and ruggedly built.


Fig. 1. Circuit of the Two-Tone Tester.
The use of a two-tone audio oscillator unit in conjunction with a suitable oscilloscope is the accepted way of adjusting a single-sideband transmitter and it is convenient if the tones used approximate to 1000 and 2000 Hz .
The phase-shift type oscillator employing a ladder network is one of the simplest ways of producing a sine wave in conjunction with a single transistor. The required degree of phase-shift between input and output circuits necessary to ensure reliable oscillations at audio frequency can be obtained by using a transformer as the feedback element.

Control of the operating frequency is not easily achieved in this way however and it is preferable

to dispense with the transformer and to use capacitors connected in series between input and output. Resistors associated with the feedback capacitors complete the RC network.

## Circuit

The complete circuit of the two-tone oscillator is given in Fig. 1 and will be seen to comprise two separate phase-shift audio oscillators. Resistor values used in each are identical but capacitors differ. The output is fed via a crude attenuator to outlet socket SK1, blocking capacitors C4 and C5 being chosen to offer similar reactance at the differing output frequencies.

Switch S1 offers four alternatives and when at position ' 1 ' the unit is ' Off '. At position ' 2 ' the output should approximate to 1000 Hz whilst at position ' 3 ' 2000 Hz signals are available. Both tones are available when position ' 4 ' is selected. The output amplitudes are equalised by preset potentiometer VR1. If necessary resistor R11 may also be a preset potentiometer but this has not been found necessary.

The purist might consider it an advantage however to make both VR1 and R11 $2 \mathrm{k} \Omega$ preset potentiometers with capacitors C5 and C10 connected to the respective sliders thereby introducing a degree of waveshaping. Dissimilar output amplitudes can also be equalized by making either R4 or R9 partially variable.


A very useful instrument in a very small space!

## Construction

The oscillators can be accommodated on a piece of Veroboard measuring approximately $3 \frac{3}{4} \times 1 \frac{7}{8} \mathrm{in}$. with 0.1 in . matrix and ten conductor strips are required. Considerable thought has been given to the layout and, due to this, little preparation of the Veroboard is required.

Looking at Fig. 2 it is seen that after cutting a piece of the board to suit it is only necessary to cut the strips in six places, indicated by ' X ', along strips $D, E, F, G, I$ and $J$.


Fig. 2. Circuit board showing breaks required in conductor strips.
The Veroboard is then turned over and with the conductor strips on the underside the various small components are positioned as shown in Fig. 3. It is desirable to use modern high grade miniature resistors and capacitors and to test them prior to soldering them into position.

A piece of $18 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. aluminium, $5 \times 2 \frac{3}{4} \mathrm{in}$., is required for the panel and the Veroboard is fixed to this using a small L-bracket with tin. sides and approximately 2 in . in length. The panel is connected to earth by the link wire indicated in Fig. 3. The panel also carries the function switch, attenuator and outlet socket; these components together with essential dimensions and the remainder of the wiring can be seen in Fig. 4.


Veroboard $3^{\frac{1}{4}} \times 1^{\frac{7}{8}}$ in approx. -0.1 in matrix
fig. 3. Component layout on top of circuil board.

## * components list

| Resistors: |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | $6.8 \mathrm{k} \Omega$ | R7 | $6.8 \mathrm{k} \Omega$ |
| R2 | $6.8 \mathrm{k} \Omega$ | R8 | $10 \mathrm{k} \Omega$ |
| R3 | $10 \mathrm{k} \Omega$ | R9 | $100 \mathrm{k} \Omega$ |
| R4 | $100 \mathrm{k} \Omega$ | R10 | $3.9 \mathrm{k} \Omega$ |
| R5 | 3.9k $\Omega$ | R11 | $1 \cdot 2 \mathrm{k} \Omega$ |
| R6 | $6 \cdot 8 \mathrm{k} \Omega$ | R12 | $8 \cdot 2 \mathrm{k} \Omega$ |
| All $\ddagger$ W 10\% |  |  |  |
| $\begin{array}{ll}\text { VR1 } & 5 \mathrm{k} \Omega \text { skeleton pot. } \\ \text { VR2 } & 50 \mathrm{k} \Omega \text { miniature po }\end{array}$ |  |  |  |
|  |  |  |  |
| Capacitors: |  |  |  |
| C1 | 5000pF ceràmic | C6 | $0.01 \mu \mathrm{~F}$ ceramic |
| C2 | 5000 pF ceramic | C7 | $0.01 \mu \mathrm{~F}$ ceramic |
| C3 | 5000 pF ceramic | C8 | $0.01 \mu \mathrm{~F}$ ceramic |
| C4 | 75 pF ceramic | C9 | 150 pF ceramic |
| C5 | $10 \mu \mathrm{~F} 12 \mathrm{VW}$ elec. | C10 | $10 \mu \mathrm{~F} 12 \mathrm{VW}$ elec. |

Semiconductors:
Tri/2 BC109

## Miscellaneous:

Switch, 2 pole 4 way wafer. Veroboard $3 \frac{3}{2} \times 1 \frac{7}{8} \mathrm{in}$, $0 \cdot 1 \mathrm{in}$. matrix. Panel, $5 \times 2$ isin., $18 \mathrm{~s} . \mathrm{w} . g$. aluminium. Output socket. Knobs. Case.

## Testing

The prototype was tested by connecting the output to an oscilloscope which showed a satisfactory waveform when the Tr2 circuit was functioning. The other oscillator was switched in and adjusted for amplitude by means of VR1. This waveform was also found satisfactory. When both oscillators were operating simultaneously it was found necessary to make a small re-adjustment to VR1, which also had an effect on the operating frequency. The outputs were checked for frequency and found to be 950 and 1900 Hz respectively.


Fig. 4. Mounting of circuit board, function switch, attenuator and output socket on panel.

## Conclusion

Although intended mainly for use when adjusting s.s.b. transmitters other uses for the unit are possible and some will doubtless spring to mind! If preferred only one half of the unit, a single sine-wave oscillator, may be constructed. Recording enthusiasts may find the device useful as a 'Tape Tailer' and if its signal is introduced as the recording nears the end of the tape, on playback the warning note will save much re-threading on to an empty spool!



## theworld's most advanced high fidelity amplifier

The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by a hundredth of an inch thick, has an output of 5 watts R.M.S. ( 10 watts peak). It contains 13 transistors (including two power types), 2 diodes, 1 Zener diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.
The IC-10 is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of such components as tone and volume controls and a battery or mains power supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs, servo amplifiers (it is d.c. coupled throughout) etc. The photographic masks required as part of the process of producing monolithic I.Cs are expensive but once made, the circuits can be produced with complete uniformity and at very low cost. This enables us to cover every IC-10 with the Sinclair guarantee of reliability.

## SPECIFICATIONS

Output 10 Watts peak, 5 Watts R.M.S. continuous. Frequency response otal harmonic distortion Less than $1 \%$ at full output. Load impedance 3 to 15 ohms. Power gain $110 \mathrm{~dB}(100,000,000,000$ times ) total.

Supply voltage
Size
Sensitivity
Input impedance

Adjustable externally up to
2.5 M ohms.

## CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

## APPLICATIONS

Eaich IC-1.0 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transistors.

SINCLAIR
IC. $10=59 / 6$

# Project 60 

## laboratory-standard high fidelity modules

Sinclair Project 60 comprises a range of modules which connect together simply to form a compact stereo amplifier with really excellent performance. So good, in fact, that only 2 or 3 amplifiers in the world can compare in overall performance. Now with the addition of three new modules to the range, the constructor has choice of assemblies with either 20 or 40 watts output per channel, with or without filter facilities.

The modules are: 1. The Z-30 and Z-50 high gain power amplifiers, each of which is an immensely flexible unit in its own right. 2. The Stereo 60 pre-amplifier and control unit. 3. The Active Filter unit with both high and low audio frequency cut-offs. 4. The PZ-5 and PZ-6 power supplies. A complete system could comprise, for example, two Z-30's, one Stereo-60, and a PZ-5. The PZ-6 is stabilised and should be used where the highest possible continuous sine wave rating is required. An A.F.U. may be added as required. In a normal domestic application, there will be no significant difference between using a PZ-5 or PZ-6 unless loudspeakers of very low efficiency are being used, in which case the PZ-6 will be required. For assemblies using two Z-50's there is the
new PZ-8 stabilised supply unit to ensure maximum performance from these more powerful amplifiers.
All you need to assemble your Project 60 system is a screwdriver and soldering iron. No technical skill or knowledge whatsoever is required and, in the unlikely event of you hitting a problem, our customer service and advice department will put the matter right promptly and willingly. Project 60 modules have been carefully designed to fit into virtually all modern plinth or cabinets and only holes need be drilled into the wood of the plinth to mount the control unit and the A.F.U. Any slight slip here will be covered by the aluminium front panels of these two units.
The Project 60 manual gives all the building and operating instructions you can possibly want, clearly and concisely. Perhaps the greatest beauty of the system Is that it is not only flexible now but will remain so in the future as the latest additions to the range show. A stereo F.M. tuner is next to come. These and all other modules we introduce will be compatible with those already available and may be added to your system at any time. And because Sinclair are the largest producers of constructor modules in Europe, Project 60 prices are remarkably low.


Z. 3020 WATT R.M.S: POWER AMPLIFIER (40 WATTS PEAK)

The Z. 30 together with the higher powered Z.50 are both of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low $0.02 \%$ at full output and all lower outputs. Whether you use the $\mathbf{Z . 3 0}$ or $\mathbf{Z . 5 0}$ power amplifiers in your Project 60 system will depend on personal preference, but they are both the same physical size and may be used with other units in the Project 60 range equally well. The $\mathbf{Z . 3 0}$ is unique in that it may be used with any power source between 8 and 35 volts without need for adjustment and may thus be driven from a car battery for example. For operating from mains, for the $\mathbf{Z . 3 0}$ use PZ. 5 power supply unit for most domestic requirements, or PZ. 6 if you have very low efficiency loudspeakers. For $Z .50$, use the PZ.5, PZ. 6 or the PZ. 8 described below.

## SPECIFICATIONS

## Power Outputs

Z. 3015 watts R.M.S. into 8 ohms, using 35 V : 20 watts R.M.S. into 3 ohms using 30 volts.
$\mathbf{Z . 5 0} 40$ watts R.M.S. into 3 ohms: 30 watts R.M.S. into 8 ohms, both continuous, using 50 V .
Frequency response 30 to $300,000 \mathrm{~Hz} \pm 1 \mathrm{~dB}$
Distortion $0.02 \%$ into 8 ohms
Signal to noise ratio better than 70 dB unweighted
Input sensitivity 250 mV into 100 Kohms
For speakers from 3 to 15 ohms impedance
Size $3 \frac{1^{\prime \prime}}{} \times 2 \frac{1}{\prime \prime}^{\prime \prime} \times \frac{1^{\prime \prime}}{}$

z.50
40 WATT R.M.S. POWER AMPLIFIER (80 WATT PEAK)
APPLICATIONS
Hi-fl amplifier: car radio amplifier; record player amplifler fed directly fröm pick-upi intercom; electronlc music and instruments; P.A.; laboratory work etc. Full details for these and many other applications are given In the manual supplied with the Z.30.


The Z. 50 is completely interchangeable with the $\mathbf{Z . 3 0}$ and can be used in all Z. 30 applications
Z. 30

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## STEREO 60 Pre-amplifier and tone control unit

The Stereo 60 is a stereo preamplifier and control unit designed for the Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout and great attention has been paid to achieving a really high signal-tonoise ratio and excellent tracking between the two channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs. The tone controls are also very carefully designed and tested.

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to 3 mV .
Output-250mv
Signal-to-noise ratio-better than 70 dB .


Channel matching-within 1dB. Tone controls-TREBLE +15 to $-15 d B$ at 100 Hz . - Power consumption 5 mA . Front panel-brushed aluminium with black knobs and controis. - Size $8 \pm \times 1 \frac{1}{2} \times 4 \mathrm{ins}$.

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