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3 electronkeally intred olvarinels, with 2 uputa per chanocl, cnabiles the une of $a$ seppata instroments at the same the. The volurve ocatralif for each shannel are located directjy above the eorresponding input Booketh. SENAITIYITIES AND INP 2 IMPEDANOES. (4 inputa) are aultable for mikraphode or guitarn Channels 3 and 4300 ml Et Irah Brdtahic for most high contput, inatruments faram, tomer, organ, etc). Input


GENERAL PURPOSE AMPLIFIER

## SPECIFICATRONS

Output- 10 watts. Outpnt impedance- -3 to 4 ohms Inputa-l. -xtal mile 10m5 Tour Controig-Trable contril frag.

Frequews Eeaponat Bass coalral range $\pm 13 \mathrm{~dB}$ at 100 Hz Frequeiky Eeaponst-(With tume contmala central) Minus 3ubs -findR Trasuatory- 4 silkent Planar type and 3 Jtaramalme type.


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As above less teak case
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 muste 50 watty sma 100 watha peak. For antatned monda 45 witta ras. 90 watis Deas Yor sloc ware 38 .h watto ran. Nearly 80 waita peak. Total Uintorthon it rated output $3.2 \%$ at 1 KHz .


 located at the rear of the unit Output-impedarice 3,8 and 15 ohms.


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- $10-30.000 \mathrm{Kz}$ (9) 10 Watts $\pm 108$
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VARIABLE TRANSFORMERS Input 290\％A．C．50／60
Output wariable 0－960t．

|  |  | EENOH | MOUNTINA |  |
| :---: | :---: | :---: | :---: | :---: |
| 1 | anp | \＄5．10．0． | 8 gmp | 814．10．0． |
| 24 | amp | 28．15．0． | 10 amp | E18．10．0． |
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$125 \mathrm{KHz}-20 \mathrm{MHz}$
Excellent condition
Fully tested and checked and
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4 band teceives covering 550 Kels to $30 \mathrm{Mc} / \mathrm{B}$ continuous and eleetrical bandspresd on 10,15 ． 20 40 and 80 metres 8 valve plus 7 diode cifcnit，

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 An excellent general pur－ pose
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 Operating voltage 0／110 Operating voltage ondor
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in excelfent porking conl． dition．\＆22．10．0．
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vity $0 \cdot l \mathrm{lv}$ p－p／CM．Band

 X gmp．Rensitivity $0 \cdot \mathrm{gr}$ ．
p－p／CM．Bandwidth 1.0 cps
 meg $\Omega$ ropF．Time liase． 0 rangea 10 ePs－ 300 KHz
Gynchronizatrori．Internal Gynchronizatwon Internal
ngted grale $140 \times 215 \times 380$ exterial，Humbinfed geale $140 \times 215 \times 330$ bracd new with handbook．f87．10．6．Carr． bracd

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 A new portable brudgeoffering ex－ cellent range and
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$+11101 \mathrm{Fd} . \quad 6$ Ranges $\pm 2 \%$ ．TURNS RATIO $1: 1 / 1000^{6}$ 1：11100． 6 Ranges $\pm 1 \%$ ．Bridge voltage at 1，000 cps．Operated from 9 voits． $100 \mu \mathrm{~A}$ ．








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> TRIO TS 510 AMATEUR TRANG:CEIYER with speaker and maine P.B.U. sel2. IN STOCE!


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A new model from Teleton． 31 golld昭保e devicer． $4+4$ watt output． Frequency tange AM $540-1600 \mathrm{KHz}$ Frequency range AM $540-1600 \mathrm{EHz}$
FHM $88-105 M H z$ Automatic FM FM 8B－108MHz．Automatie FM Stereo reception－Stereo Indipator． Controls： Tona and f \＆ L ．volume contros， AFC wwitch，stereo beadphone socket．



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First grade quality Moving Coil panel metera．Type MR asf． likin．square fronts．

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| :---: | :---: | :---: |
| Lund ．．．．．． $97 / 8$ | 100ma＋．． $87 / 6$ | 300V．J．C．． $27 / 6$ |
| 1－0－1md ．．．${ }^{\text {2 }} / 6$ | 150ma,$-\ldots .27 / 8$ | 500V．D．C．．．87／6 |
| 2mA ．．．．．． $27 / 6$ | 200mA ．．．． $27 / 6$ | 750V．D．C．．27／6 |
| JnA ．．．．．． $87 / 6$ | 300mA ．．．． 878 | 15V．A．C．．． $27 / 6$ |
| 10ms ．．．．． $87 / 6$ | 500mA ．．．． $27 / 6$ | 50V．A．C．． $27 / 6$ |
| 750］n4．．．． $27 / 6$ | 3V．D．C．．．87／6 | 150V．A．C．． $87 / 6$ |
| $1 \mathrm{mmp} . . . . .9 .9810$ | H0V．D．C．．．2F／6 | 300 V ．A．C．． $87 / 8$ |
| 4 amp ．．．． $27 / 6$ | 15V．D．C．．97／6 | 500 V ．A．C．$+2 / 1 / 6$ |
|  | $20 \mathrm{~V}, \mathrm{D} . \mathrm{C} .4 .876$ | Stmeter lma $30 /$ |
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TE－40 HIGH SENSITIVITY A．C．VOLTMETER 10 mes．input 10 ranges． $01 /+003 /+1 / \cdot 3 / 1 / 3 j 10 / 30 / 100$ sonv．R．N．S． $4 \mathrm{cps}-\mathrm{I}-\mathrm{-}$ Mer ． gupplied brand refor completr with leads and ingtructions Operation 230F，A．C． $81 \% .10 .0$ Catr．${ }^{1 /-}$


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 FREQUENCY OSCILLATORS Frequency o－zo Kefa．of 2 ranges．Output sispplied in perfect order，sid． $10 . \mathfrak{C a r r}$ 10i－
## TE－65 VALVE VOLTMETER

 High quality instrument with 28 ratiges．B．C．volt
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COSSOR 1049 DOUBLE BEAM OSCILLOSCOPES D．C．coupled．Band width $1 \mathrm{Ke} / \mathrm{s}$ ．Perfert order． $2 \$ 5$. Carr． 801


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5 MHz Prass Band．Separate Y1，Ya ampli flers．Cahbrated trigeterd surtep from 2 ved to 100 milli segfern．
notructians es\％（the with all sucessories pud netructions es．Carr．yard TE－1．6A Trataistornsed Signsi Generator． $\mathbf{0}$ rauges
 $\$ 00 \mathrm{HHz-30mHz}$ An for the handrman oper ates ou 0v battery．Wide easy to read scale
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TF, $800 \quad 20,000$ R/VOLT GIANT MULTINFTER nutrot reqle and operlogd
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 $=1000 \mathrm{~V}$. A.C. volts $1.3 Y$
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 $300 \mathrm{~mA} / 600 \mathrm{~mA} 008 \mathrm{k} / 50 \mathrm{~K}$ $800 \mathrm{~K} / 8 \mathrm{meg} .20$ to +68 db
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20,000 O.P.V. $0,0.6 / 6 / 30 / 120 /$ $600 / 1,300 / 3,000 / 6,600 v$ D.C
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| 284 | 612 | 6Es | 7／6 | 6SC7 | $7 /$ | 12AUG | 519 | 30 PLL 12 |
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| 5 F 4 G | $8{ }^{-}$ | 6Frag | $5 / 6$ | 6SK7GT | $4 / 9$ | 128E6 | $0 \cdot 3$ | 30 P 4 |
| 6Y3GT | $6 /$ | 6F11 | $8 / 6$ | 68L7GT | B／－ | 1208GT | bi－ | 30F12 |
| 5 EdCa | 7 － | 6F13 | $6 / 6$ | 6aN7GT | $5 / 6$ | 12E1 | 201－ | 30F19 |
| 1／30L2 | 15／ | 8F14 | 1216 | 6897 | \％／8 | 12U5GT | 2／6 | 30 PL 1 |
| 6 AT | 151－ | 6 F 23 | 161－ | 6U4GT | 12. | 12JTGT | $8 / 6$ | 30PL13 |
| －489 | 12／6 | 6F24 | 14／－ | 6UsG | $7 / 8$ | 12E7GT | 71 | $30 \mathrm{PL14}$ |
| GACT | 4／－ | 6F26 | $15 /-$ | 6V6M | 121－ | 12F8GT | 81 | 35 A 0 |
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| dAP7G | 151－ | 6．554 | 9－ | 6xbGT | B／ | 123.17 | 3／9 | 35Z5． |
| 6AT6 | $4 / 8$ | 6J5G | 4 | 7 P 6 | 11／6 | 129 K 7 | 49 | 37 |
| \％AU6 | 5／－ | 6J5GT | $5 / 6$ | 787 | 7／6 | 128n7 | $5{ }^{5}$ |  |
| 6E4 4 | 20，－ | 656 | 3／6 | 7 CJ | 22／6 | 14H7 | 8／6 | 2085 |
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|  | 8／6 | 5／6 | 4／6 |
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 UTC01 $=5 \times 7401 \mathrm{~N}$ UICOS $=5 \times 7403 \mathrm{~N}$ UIC04－5 $\times 7404 \mathrm{~N}$ $\mathrm{UIC05}=5 \times 7405 \mathrm{~N}$ $T \mathrm{Cl} 10=5 \times 7410 \mathrm{~N}$ $\mathrm{UIC} 40=5 \times 7440 \mathrm{~N}$ UIC41 $=5 \times 7441$ A
$\begin{array}{ll} & \text { PAKE NO．} \\ 10 /-\quad \text { UIC4 }=5 \times 7442 \mathrm{~N} \\ 10 & \text { UTC } 50-5 \times 7450 \mathrm{~N}\end{array}$
$10 /-\mathrm{CIC50}=5 \times 7442 \mathrm{~N}$ UIC51 $=5 \times 7450 \mathrm{~N}$ UIC60 $=5 \times 7451 \mathrm{~N}$ UIC70 $=5 \times 7460 \mathrm{~N}$ UIC72 $=6 \times 7470 \mathrm{~N}$ UIO73 $=5 \times 7472 \mathrm{~N}$
$\times 7473 \mathrm{~N}$ $\begin{array}{ll}\mathrm{UIC7} \\ \mathrm{UI} & =5 \times 7473 \mathrm{~N} \\ =5 \times 747 \mathrm{~N}\end{array}$ UIC75 $=$ 万 $\times 7475 \mathrm{~N}$ UIC76 $=5 \times .7476 \mathrm{~N}$


PAK No．
UIC $80=5 \times 7480 \mathrm{~N} \ldots 10 /-1$ UIC82 $=5 \times 7482 \mathrm{~N} \cdots 101-$ UIC88 $=5 \times 7483 \mathrm{~N} \cdots 10 /-$ UIC86 $=5 \times 7486 \mathrm{~N} . .101$ OIC90 $=5 \times 7490 \mathrm{~N} . .101-$ $\begin{aligned} & \text { UIC92 } \\ & \text { UTC9 } \\ & =5\end{aligned}=7492 \mathrm{~N}$ UIC93 $=5 \times 7493 \mathrm{~N} \ldots 101-$
$=5494 \mathrm{~N} . .101-$ $\mathrm{UIC} 95=5 \times 7495 \mathrm{~N} \cdots 10 /-$ URC96 $=5 \times 7496 \mathrm{~N}^{\circ} \mathrm{C} .10 /-$

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# PRACTICAL Wireliss 

## NEWS AND COMMENT

## Learn while you build

EXPERT gardeners are said to have 'green fingers' which E implies that they have some magic touch. In the same way, there are service technicians who, seemingly by some sort of telepathy, have an uncanny knack of quickly looking over a faulty piece of equipment, then pointing an accusing finger and saying "C5 has gone down".
The same kind of thing happens in the area of amateur home construction. Some seem to have it, others do not. But although it is obvious that some constructors are neater and cleverer than others, and some people can "de-bug" a project quicker and more effectively than others, it would be wrong to put this down to fate or any other ethereal influence.
Real success in such realms as radio construction is rarely accidental; it is usually achieved only by a combination of common sense and thoughtful application. An enthusiast passes the barrier between the absolute novice and competent constructor when he begins not only to build equipment but starts to puzzle out exactly what each component does and what effect each component has on others. Only by acquiring a solid working knowledge of each individual item will the enthusiast be able to get the optimum performance from his project and to clear up any troubles which may subsequently arise.

One often hears that certain pieces of equipment, such as portable transistor radio receivers, use "standard circuits". This may appear to be superficially true, but in actual practice, variations are legion. These may be minor in character, the basic "blocks" being almost identical, but it is these minor variations which (if fully understood) will give the enquiring hobbyist a much better insight into the whys and wherefores of circuit design.
Basic circuitry can be learnt from text books, but no amount of reading will substitute for practical work; on the other hand practical work will not advance the constructor's knowledge unless he takes the trouble to work out what a circuit is, what it is supposed to do, and how. He should want to know why a certain component is where it is, and why it has a certain value. He should also want to know what might happen should that component become faulty.
W. N. STEVENS-Editor.

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[^2]
## WEWS... MEWS... MEWS...

## Listeners Club Ceases

Now in its fourth year of service, the Listeners' Club of Radio New York Worldwide has ceased operation.
Irwin Belofsky, the President of the Club, says that they have found it impossible to continue publishing Radio Worldwide, their magazine, without a tremendous financial loss. It is a loss incurred through rising costs in postage, print, etc., and these could not be covered through membership dues or advertising.
All Listeners Club members with unexpired subscriptions will, however, receive the balance of their membership in issues of a new publication, Radio Today.

## Vero Strip



Vero Electronics Ltd., of Chandler's Ford, Hampshire, have recently introduced a new type of terminal board which has been designed as a simple and inexpensive mounting strip for discrete components. These can be mounted across the width of the board or alternatively along its length to effect cross-connection.

The mechanical and electrical specifications of the materials used enable the board to withstand a maximum working voltage of 2 kV , whilst still maintaining an insulation resistance of one hundred thousand megohms between adjacent copper pads. These features make the board suitable for all applications where a conventional tag strip or group board might be used.

The dimensions of the strip are such that they can be mounted in standard die-cast boxes.

A number of terminal pins are also available which can be used in conjunction with the Vero strip where such additional facilities are required. Vero Electronics Limited, Industrial Estate, Chandler's Ford, Hampshire, SO5 3ZR.
B.B.C. Radio Birmingham


This v.h.f. service transmits on $95 \cdot 6 \mathrm{MHz}$, horizontal polarisation. Maximum e.r.p. is 5.5 kW with a directional aerial.

The transmitter is sited at BBC Sutton Coldfield. Inner and outer service area boundaries correspond to average field-strength contours of 60 and 52 dB (relative to 1 microvolt per metre) respectively for a receiving aerial height of 30 feet. The field strength at a particular site may differ by as much as 10 dB from that indicated.

## Otley Radio Society

The Chairman of the Otley Radio Society, M. T. George-Powell, G3NNO, informs us that the membership has increased and the Society recently moved to larger premises so that they will bei able to hold lectures, slide shows etc. The Society meets every Tuesday evening and on March 19th members visited the Yorkshire TV studios in Leeds. Further details about the meetings may be obtained from: The Chairman, 82 Forest Avenue, Harrogate, York.

## Loudspeaker Eils

Richard Allan Ltd. announce details of three loudspeaker kits. They have made a special study of the needs of the D.I.Y. individual and believe that they have met all the requirements.

The kits are complete in every
sense and contain B.A.F. wadding and foam underlay cut to size and a postcard giving a choice of any three Vynairs. Receipt by Richard Allan of the card giving the user's choice enables them to post him the Vynair by return post. Shown in the photograph is the "Twin Assembly".

For further details contact Richard Allan Ltd., Bradford Road, Gomersal, Cleckheaton, Yorkshire.


## MEWS... NEWS...

## MEWS...

## Keeping Track



A new useful accessory for record collectors is a unique system for cataloguing and locating gramophone records easily. The system comprises:- luxury padded simulated pigskin book containing 12 clear P.V.C. slip-in pockets in which are kept specially preprinted index records which can be completed by the user. The index is provided in pad form, each set comprises:- 25 preprinted Index Pages, 3 Records Wanted Pages and 3 Contents

Pages; pairs of self-adhesive circular labels numbered 1-100 for attaching to record sleeves; 40 plain self-adhesive labels enabling printed headings of the Index Pages to be covered neatly to provide for hand or typewritten headings. The system can be expanded to 999 records and can also be used for recorded tape.

Made by the Bib Division, Multicore Works, Hemel Hempstead, Herts. retail price, including tax, is 34 s.

## Stereo Rmplifier from F.S. Electronics



This amplifier has been designed as an optimum between the simple and sophisticated units presently available, to give performance and looks required by present day living rooms at a moderate cost. This unit is due for export to Czechoslovakia as a solid British product housed in a $\frac{3}{4} \mathrm{in}$. polished cabinet with a choice of woods and front panel colours. Inputs are available for Ceramic/Crystal and Magnetic cartridges, with an Auxiliary input for Radio Tuner or Tape Replay.

Outputs consist of a low impedance Tape Record and Twin
speakers.
Specification is as follows: Ceramic Input: 50 mV sensitivity, velocity loaded, R.I.A.A. corrected.
Magnetic Input: 2.5 mV sensitivity, velocity loaded, R.I.A.A. corrected.
Auxiliary Input: 100 mV into 110 K , flat response, ie $20 \mathrm{~Hz}-$ $20 \mathrm{kHz} \pm 2 \mathrm{~dB}$.
Tape Output: 150 mV flat response.
Speaker Output: 6 watts Music Power into 4 ohms per channel. Tone Controls: Base $\pm 10 \mathrm{~dB}$ at $20 \mathrm{~Hz}-20 \mathrm{kHz}$. Treble $\pm 15 \mathrm{~dB}$ at 20 kHz .
Signal/Noise: Better than 50 dB on all inputs. Aux. input 60dB. Overall Distortion: $1.5 \%$.
The amplifier retails at $£ 32$ 10s and the power output modules can be supplied seperately at £3 16s each.
F.S. Electronics Ltd., 93A Balderton Gate, Newark, Notts.

## Club Nofes

. Meetings of the Chester \& District Amateur Radio Society are held at the Y.M.C.A., Chester at 8 p.m. every Tuesday except the first Tuesday of each month which is Nett Night. Recent meetings included lectures on Short Wave Listening and Aerials, visit to BBC, junk sale, and talk entitled On to Square Two by G3ATZ. Further gen from: Alan S. Warne, G8AYW, 113 Queens Road, Vicars Cross, Chester.
... Derby \& District Amateur Radio Society are holding their Mobile Rally on Sunday, August 16th. at Rykneld School, Bedford Street, Derby. There will be talkin stations from $10 \mathrm{a} . \mathrm{m}$. to $3 \mathrm{p} . \mathrm{m}$. G3ERD/A on 160 m ., G2DJ/A on 4 m . and G8DBY/A on 2 m . Further gen from: T. Darn, G3FGY, Sandham Lodge, Sandham Lane, Ripley, Derby.
. . . Stourbridge \& District Amateur Radio Society, in collaboration with the LlanfairWelshpool railway set up a radio station at the Llanfair-Caereinion terminal station on July 4th. They operated between 12 noon and 6 p.m. on 80 m . using the call GW601/P. Further gen on the Society from: Sheila Clift, G8BYE, Manorways, 49 Manor Lane, Halesowen, Worcs.

## Radio \& TV Course

The Stonebridge Evening Institute, Brentfield Road, London, N.W.10. are holding a Radio \& TV Course. It will be held on Tuesdays and Thursdays (7p.m.-9p.m.) commencing 22nd and 24th. September 1970. Fees for a course lasting 30 weeks for two evenings per week are $£ 4$. Session ends on 28th. May 1971. The course covers theory and some practical work. Enrolment will take place during the week 14th. to 17 th. September 1970 or readers may enrol now by writing to: 44 Worcester Crescent, Mill Hill, London, N.W.7. Cheques and P.O.'s should be made payable to "The Brent Borough Treasurer".


## A USEFUL AID <br> TO SPEEDY FAULT FINDING

WHAT the serviceman requires is some quick method of "seeing" (or hearing) what is actually happening to the signal passing through any part of equipment under investigation. The sophisticated approach to this requirement is to use an oscilloscope, on the screen of which the actual signal at the test point can be displayed.

But few radio enthusiasts possess such an instrument and the necessary ancillary items such as a wobbulator and calibrated signal generator, which are required to utilise the full potential of an oscilloscope.
A very effective substitute is the use of the procedure known as "signal tracing". Basically, this can be approached in two ways, either an artificial signal can be injected into the equipment under test, at any given point, and the result listened to on the equipment's own speaker, or, alternatively, a sensitive signal tracer can be connected to any suitable point in the equipment being tested, and the signal at that point "picked off" by the tracer,

demodulated if necessary (r.f. or i.f. signals), and given sufficient a.f. amplification to produce an audible signal in the speaker built into the tracer itself.
Both systems have their merits and the instrument about to be described combines both functions. If the output socket be connected, preferably by a short length of coaxial cable, to the equipment under test, a wideband signal extending from r.f. to a.f. frequencies can be injected at any desired level by adjustment of the output gain control, and a steady audio note (of about 1 kHz ) will be heard from the speaker of the equipment being tested, if all is in order onwards from the point of injection.
Alternatively, if the input socket is connected to the equipment being tested, the tracer will reproduce in its own speaker, a faithful rendering of the signal existing at the test point. It is in fact possible, indeed often useful, to utilise both functions simultaneously.


Fig. 1 : Circuit of the Genetracer. The "generator" and the "tracer" are built on separate circuit boards

For example, a signal can be injected at the grid of a valve, and the amplified signal "heard" on the tracer's speaker by connecting the input socket to the anode circuit of the same valve. Thus absence of signal, lack of gain, or distortion arising within the stage under investigation, can be quickly discerned.

Once the faulty stage has been located in this way, voltage and/or resistance checks of all components directly connected thereto will usually show what is amiss.

## Circuit

Referring to Fig. 1, it will be seen that the "generator" portion of the instrument comprises the familiar cross-coupled multivibrator circuit, using Tr1 and Tr2. The "tracer" function is carried out by the $\mathrm{D} 1, \operatorname{Tr} 3$ and $\operatorname{Tr} 4$ circuitry.

The instrument is in fact constructed as two separate units, on paxolin component boards, powered from a common 9 V battery (type PP3 or similar). The full 9 V is not necessary for the multivibrator "generator" and so this part of the circuit is fed from a potential divider network (R6 and R5) giving about 6 V .

This has all the advantages of printed circuit wiring, yet is much easier for the amateur constructor to reproduce.

For those who have not previously used this material, it comprises a thin strip of pure copper, protected when bought by a plastic backing which when peeled away leaves the adhesive copper strip ready for fixing to any smooth insulating surface. The copper strip is easily cut, bent, or otherwise shaped, to meet circuit needs.

It is already prepared for soldering, and the leads of the various components are bent over and soldered on with a quick application of hot iron and cored solder in the usual way.

Figures 2 and 3 show the component layouts used in the prototype, and it is recommended that these should be adhered to. The drawings are actual size and, for ease of construction, it is suggested that tracings of these be made. A tracing can then be temporarily fixed to the surface of a paxolin panel, and the drilling of all connecting points (shown by a black dot), and component mounting holes made, using the tracing as a template. Holes, $\frac{3}{8}$ in. diameter, are required for the mounting of the gain controls VR1 and VR2.

All other holes should be small enough to just accommodate the lead out wires from the various


Fig. 2 : Full scale layout of the "generator" circuit board

The circuits of both units are entirely conventional, and standard readily obtainable transistors and components are used throughout. A simple Class A single-ended transistor output stage is used in the "tracer" as a large output is not required.

## Construction

For ease of construction and general neatness of the completed units, the popular method of mounting all components on one side of a $\frac{1}{10} \mathrm{in}$. thick paxolin panel, with their connecting wires protruding through holes to the other side of the panel, and there connecting them to adhesive "Cir-Kit" copper wiring strips, has been adopted.
resistors, capacitors, etc. Note that the coaxial input and output sockets are mounted on the front control panel (also of paxolin) of the instrument, not on the component panels. Connection to these sockets is thus delayed until the panels have been completed, and fixed to the $\frac{3}{3}$ in. thick wooden spacers glued to the rear surface of the control panel.

The speaker is also mounted on the control panel and, for neatness, is provided with a small square of "fret" fabric.

The Cir-Kit strips are shown in Figs. 2 and 3 as actually lying on top of the component lead out holes, done for the sake of clarity. Actually, the strips should be affixed so that they run just clear of the holes, the component wires then being bent over at right angles (which helps to anchor them in position) and soldered to the appropriate strips.


Fig. 3: Layout of the "tracer" circuit board, also full scale

Take care to ensure that the electrolytic capacitors are correctly placed with regard to polarity markings. The transistors should not be soldered into place until all other wiring has been completed on the panels. When soldering the transistor and diode leads take care to use an effective heat sink.
It helps if coloured sleeving is slipped over the transistor leads before connecting them into circuit, a suitable colour code being red for collector, yellow for emitter, and blue for base. Note especially that in the case of $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$, the relative positions of " $b$ ", " $c$ " and " $e$ " are not identical on the component board.

When the two panels have been completed, and checked for correct assembly and wiring, they may be fixed to the spacing strips secured to the control panel by small wood screws. The photograph of the completed assembly shows what is required.

Connect the speaker to the output transformer secondary T1, and connect the input and output sockets to the respective gain controls as shown in Fig. 4.

The battery leads, terminating in a suitable press stud connector to fit the PP3 battery, and composed of red and blue flexible wire, can now be connected. The diagonal interconnection between the tracer and generator panels should also be completed at this stage.

The completed unit is housed in a simple rectangular box of a size to suit the front panel, and about 4in. deep from front to rear. This depth is not required to house the instrument, but rather to provide stability when stood upright on the bench. It is a good plan to fix four small rubber feet at the corners of the base. The actual method of construction and the materials used are left to the discretion of the constructor.

Two lengths of test lead should now be prepared comprising some 12 in . to 18 in . of TV type coaxial. cable, one end of each lead being terminated in a coaxial plug. The other ends should have outer braiding and inner conductor separated for about 6 in., and crocodile clips fitted. These form the most convenient means of connecting the instrument leads to the equipment under test.

## Testing

To test the completed instrument, plug the test leads into the input and output sockets, and connect the ends of the test leads together, i.e., braiding to braiding and inner to inner. Switch on both the generator and tracer units and, by adjusting the gain controls, the output from the generator can be clearly heard in the tracer's speaker.

Fig. 4 : Interconnection of the circuit boards after mounting in cabinet.


Full Name
If my article does not win a prize I should like it:-

## Address

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(b) to be returned to me.*

Title of Article


THIS transmitter is VFO controlled, and operates on the $80,40,20,15$ and 10 m amateur bands. A power input of about 40 to 60 watts, according to the h.t. supply, proves very useful, and a single switch selects any band.

Fig. 1 shows the circuit, and the following details should help when checking operation and tuning up.

## VARIABLE FREQUENCY OSCILLATOR

V1, a 6CH6, is a Clapp type oscillator, with the voltage stabilised screen grid acting as a virtual anode for the oscillator circuit. L1 tunes 1.751.9 MHz , and is selected by $S 1$ and $S 2$, output frequency being doubled for the $3 \cdot 5 \cdot 3 \cdot 8 \mathrm{MHz}$ band. C 1 , with TC 1 and the core of L 1 , allow adjustment of band coverage. The anode circuit of V1 is electron coupled, and is untuned on this band, R4 being the anode load.

For the higher frequency bands, S 1 and S 2 select L2, which has TC2 and C2, VC1 being the main variable tuning capacitor as before. The fundamental range is now approximately $7-7 \cdot 3 \mathrm{MHz}$, and this with harmonics allows complete coverage of the 7,14 and 21 MHz bands, and coverage from $28-29 \cdot 2 \mathrm{MHz}$ on 10 metres. As all these ranges are direct harmonics, calibration is simplified.

For $7 \mathrm{MHz}, \mathrm{R} 4$ provides an untuned anode load. L 3 is resonant at about $7 \cdot 1 \mathrm{MHz}$, and is brought in by S 3 , for the 14 and 21 MHz bands. For 28 MHz , L 4 is in circuit, and is tuned to about 14.5 MHz , so that the output from the anode of V1 is doubled in frequency.

## POWER AMPLIFIER

This is a v.h.f. type power beam tetrode, a 6146, operated at 100 mA anode current. This corresponds to 40 watts input with a 400 V supply, 50 watts with 500 V , and 60 watts with 600 V . It has also been used with 300 V ( 30 watts) with excellent results.

Bias is obtained by grid current through R8. Here, 2 mA grid current provides 44 V bias and normal operation is with about 2 mA to 2.5 mA grid current. Since lack of grid current can rapidly damage the 6146 the grid meter is permanently in circuit.

When changing frequency, h.t. is applied to V1 and V2 by closing the "Tune" switch, and VC2 is then adjusted for suitable grid current. When this has been done, the 2-pole transmit/receive switch applies h.t. to all stages.
R.F.C. 3 with R10 forms a parasitic suppressor. Anode current is shown by the 150 mA meter. The switch S5 and tapped coil L10 allow 5-band coverage. VC3 is for anode tuning, and VC4/5 is the output capacitor of the pi-network, and allows the p.a. to be loaded by a range of impedances.

TC3 with L11 forms a series tuned harmonic trap, which in certain circumstances will be useful when interference is being caused to t.v. reception.

## MODES OF OPERATION

The transmitter was built for use with a 30 watt modulator, which permits modulation of V3 anode and screen grid. This is a very trouble-free and satisfactory method, and one which will give excellent results without any special care in adjustment.


Fig. 1: Complete circuit diagram of the 5-band transmitter.

The connection to R9 can be broken, and screen grid modulation used. This has the advantage that an ordinary audio amplifier, giving about 2-4 watts output, will readily modulate the transmitter but r.f. output is reduced, so correct and full aerial loading is essential, to avoid distortion.
Though the transmitter was intended for telephony working on all bands, cathode and other forms of keying have been found satisfactory for c.w. It is also possible to substitute an inexpensive 807 for the 6146 .

## CONSTRUCTION

$\mathrm{VC1}, \mathrm{C} 1, \mathrm{C} 2, \mathrm{TC} 1$ and TC 2 , with L 1 and L 2 , occupy an enclosed box on top of the chassis, Fig. 2. To simplify metal work, the front and both sides of this box are formed from an $8 \times 2 \mathrm{in}$. universal chassis runner. Segments are cut from each flange $2 \frac{1}{2}$ in. from the end.

The runner is then bent at right angles at these points, to form a member $3 \times 2 \frac{1}{2} \mathrm{in}$. L 1 and L 2 are mounted, and also the ball-drive for $\mathrm{VCl} . \mathrm{VC1}$ is fitted to a bracket bolted to the runner.

This assembly is then bolted to the chassis in the position shown in Fig. 2, and is completely wired. Leads pass down through the chassis from L1 and L 2 , to S 1 and S 2 . VC1 is also wired to S 2 .

TC1 and TC2 are ceramic trimmers, on brackets bolted to the chassis. A piece of aluminium $4 \frac{3}{4} \times 3 \mathrm{in}$. is bent to form the coil box top and back, $\frac{1}{4}$ in. forming a flange to bolt to the chassis. This part is attached to the box flanges by self-tapping screws. Holes allow TC1 and TC2 to be reached.


Fig. 2 : Plan view of transmitter chassis.

## VFO ANODE CIRCUIT

A universal chassis runner $11 \times 2 \mathrm{in}$. has its flanges cut $3 \frac{3}{4}$ in. from the ends, so that it can be bent into a box $3 \frac{3}{4} \times 3 \frac{1}{2} \mathrm{in}$. This is bolted to the chassis and chassis front in the position in Fig. 3, and contains V1 holder, L3, L4, etc.
R.F.C. 1 is supported on a tag strip. All wiring associated with S1/S2, C3, C4, C5 and V1 should be stout and rigid. A tag strip also anchors R2 and R5. S3 is wired to select R4, L3 or L4.

C10 is inside this box, and a lead passes through the box to tag 8 of V2. This and R7 are positioned as in Fig. 3. The box is closed by cutting a plate $3 \frac{1}{2} \times 3 \frac{3}{4} \mathrm{in}$. and fixing it to the flanges with self-tapping screws.

## BA ANODE CIRCUIT

Coils L5/L6/L7/L8 and L9 are selected by the wafer S4, and are tuned by VC2. C7 should be on short leads from VC2 to L9, while C13 is directly connected from S4 to V3, with a short wire to VC2. A coupler and long shaft operate VC2.

S4 is arranged so that very short leads are possible to the h.f. range coils, especially L8 and L9. All other wiring needs to be reasonably short and direct.

## POWER AMPLIFIER STAGE

Cathode and r.f. circuits in this stage should be wired with 16 s.w.g. or stouter conductors. Tags 1, 4, 6, 7 and 8 are well earthed, see Fig. 3. A tag strip supports R8 and C14, a lead passing from here to the grid current meter. A tag strip near the rear of the chassis is used for h.t. and other connections, and allows easy disconnection of R 9 for screen grid modulation.

The p.a. and anode circuit components occupy a box $8 \frac{1}{2} \times 4 \frac{1}{2} \times 4$ in. high, Fig. 2. This was purchased ready made (see component list). A number of holes are punched in the chassis around the holder for the 6146. The box is finally closed with perforated metal or similar material, holes being punched in this for TC3 and the co-axial output socket.

VC3 and VC4/5 are joined by a stout lead, and earthed to the chassis. R.F.C. 3 is 5 turns of 18 s.w.g. wire, wound to $\frac{3}{8} \mathrm{in}$. diameter, and stretched to occupy about $\frac{5}{8} \mathrm{in}$. R10 is in the centre of R.F.C.3, and both are soldered directly to the anode cap clip of the 6146. All leads to VC3, C18 and L10 should be very stout and short.
A tag strip holds R.F.C.3. The output socket is bolted to a bracket in contact with the chassis, and is wired to VC4/5. TC3 is held with a small bracket and L11 is fitted directly between TC3 and the output socket, as shown.

## INDUCTORS

L1 is a medium wave type dipped coil with unwanted windings and some turns removed until 1.75 MHz is reached with VC1 closed. L2 is 11 turns of 24 s.w.g. enamelled wire close-wound on a $\frac{1}{2} \mathrm{in}$. diameter former. L3 is 50 turns of 32 s.w.g. enamelled wire, and L4 is 17 turns, both on $\frac{1}{2}$ in. diameter formers.


Fig. 3: Underneath the chassis showing main wiring.
L5 has 65 turns of 34 s.w.g. enamelled wire, and L7 has 14 turns of 32 s.w.g. all closewound on $\frac{1}{2} \mathrm{in}$. diameter cored formers. L8 has nine turns of 26 s.w.g., spaced by the wire diameter, and L9 has eight turns of 26 s.w.g., also spaced by the wire diameter. Both formers are $\frac{1}{2} \mathrm{in}$. diameter, and L8 has a core, but not L9. If necessary, the inductance of $L 9$ can be reduced by spreading the turns.

L1 should tune from $1 \cdot 75-1 \cdot 9 \mathrm{MHz}$, with a trifle to spare, and L 2 from about $7-7 \cdot 3 \mathrm{MHz}$. This can be checked by applying h.t. to V1 only, with R4 in circuit, and listening for the v.f.o. signal with a receiver. Final calibration is by adjusting the cores of L1 and L2, in conjunction with trimmers TC1 and TC2. The y.f.o. should be adjusted in conjunction with the 100 kHz harmonics from a crystal marker when all construction is finished.
L3, with stray circuit capacitances, should be tunable to 7 MHz . This can be shown by grid current through R7 or R8, or by using a wavemeter. L4 is similarly tunable to 14 MHz . When the transmitter is tested, the cores of L3 and L4 can be rotated slightly for maximum p.a. grid current around the middle of the respective bands.
L5 should tune to about 3.6 MHz with VC2 about half closed. L6 is resonant at about 7 MHz with VC2 about one-third closed.

The cores of both L7 and L8 are adjusted so that 14 MHz and 21 MHz can be tuned with VC2 only slightly closed. No core was used with L9, and the winding is adjusted so that VC2 is almost at minimum capacitance at 29 MHz .

If L8 and L9 have insufficient inductance, and resonance on 21 and 28 MHz bands is only obtained with VC 2 near maximum, grid current will be reduced. If the coils are adjusted as explained, it will not be possible to tune to wrong harmonics with VC2.

A grid-dip meter should be used to check that each anode coil L5 to L9 operates on the correct harmonic, when first aligning the buffer-amplifier, with h.t. off. Since V1 provides 7 MHz output for 14 MHz and 21 MHz , and 14 MHz output for 28 MHz , wrong tuning of the anode circuit of V 2 is unlikely.

Final adjustments to the cores of these coils must be made by observing grid current on the grid current meter, V3 being in position, but anode and screen grid voltages being removed from this stage.

## TANK COIL

This is wound on a paxolin tube $3 \frac{1}{2} \mathrm{in}$. long and $1 \frac{1}{2}$ in. in diameter subsequently mounted on 6BA bolts with extra nuts, to be $\frac{3}{4} \mathrm{in}$. clear of the chassis. The ends A and F, and tappings B, C, D, and E, Fig. 2, are on the underside of the coil, so that leads to wafer S5, Fig. 3, are short.

Some 16 s.w.g. wire is anchored at A, and four turns are wound with a pitch of 8 turns-per-inch. The wire is taken along to allow a $\frac{1}{4}$ in. space, and two more turns are wound. After another $\frac{1}{4} \mathrm{in}$. space, three turns are wound, and the wire is anchored at D. Stout leads are securely soldered at B and C. The coil is finished by winding 22 turns of 20 s.w.g. wire from $D$ to $F$, these turns occupying $1 \frac{1}{4} \mathrm{in}$. Tapping E is a short loop seven turns from D .

F is connected directly to $\mathrm{S5}$ rotor tag. B, C, D and $E$ are connected so that turns in circuit are as follows : 10 metres, $4 ; 15 \mathrm{~m}, 6 ; 20 \mathrm{~m}, 9 ; 40 \mathrm{~m}, 16$; 80 m , whole coil.

## POWER SUPPLIES

V1 and V2 draw current from a separate h.t. supply of around $250 / 300 \mathrm{~V}$. A 230 V supply was found to give a minimum grid current of 3 mA on all bands, with R6 reduced to $10 \mathrm{k} \Omega$. The supply should be able to provide 60 mA , so a receiver-type power pack is thus generally suitable.

The h.t. for V3 can depend somewhat on the modulator power or available supplies. For highlevel modulation, an audio output of about onehalf the p.a. input is required. Modulator circuits actually used had $2 \times 6 \mathrm{~V} 6$ for 15 W of audio, $2 \times 6 \mathrm{~L} 6$ for 20 W , and $2 \times 807$ for 30 W .

For screen grid modulation, R9 is disconnected from the positive line, and receives modulated h.f. from a small amplifier. A single 6BW6 or similar output stage is quite adequate. The p.a. anode is then supplied from a higher voltage source-preferably $500 / 600 \mathrm{~V}$.

## BANDSWITCH

S1/S2 is a 2-pole 5 -way wafer and S3, S4 and S5 are each single-pole 5 -way wafers. S3 and S4 are mounted on the box, Fig. 3, with long bolts and spacers. S5 is fixed to a bracket near V3 and immediately under L10.

The shaft is a long insulated $\frac{1}{4} \mathrm{in}$. diameter rod (see component list) with flats filed to engage with the holes in the rotating part of the wafers. A hole in the rear of the chassis allows this rod to be pushed in from the back, and through each wafer. A coupler connects it with the metal shaft of $\mathrm{S} 1 / \mathrm{S} 2$.


Fig. 4 : View of p.a. compartment at rear of chassis.

A switch in which tags are progressively shorted all round is often used for a pi-tank of the type shown in Fig. 1. R.F. output was measured on all bands with such a wafer, and again with an ordinary single-pole 5 -way wafer, and no measurable difference could be observed. In view of this, the ordinary 5 -way wafer seems suitable.

## FUNCTION SWITCHING

The "Tune" switch applies h.t. to V1/V2 only, to allow adjusting transmitter frequency, and tuning for grid current. The 2 -way $\mathrm{T} / \mathrm{R}$ switch applies h.t. to both V1/V2 and to V3. This was arranged by having the $T / R$ switch on the power-pack/modulator.

Should the high voltage supply be from a separate h.t. transformer, h.t. may be taken off the p.a. and modulator valves by placing an h.t. on/off toggle switch in the mains supply to this transformer. (The transformer must then be for h.t. supply only, and not include rectifier, heater or other supplies.)

The actual method of h.t. switching is not important, provided h.t. can be applied to V1 and V2 separately, with V3 off. It should not be possible to apply h.t. to V3, with V1 and V2 inoperative.

If the $T / R$ switch has extra poles, these may be used to operate an aerial change-over relay, or to switch the aerial directly from receiver to transmitter. With the latter method, switch wiring should be done with co-axial cable, and the receiver aerial input should be earthed on transmit, to reduce stray r.f. at the receiver.

## OPERATION

V3 anode circuit must always be tuned to resonance, by VC3, as shown by a dip in anode current. A check is most readily made on 80 m , with an artificial load such as a 60 watt domestic lamp plugged
into the output socket or connected across VC4/5.
With h.t. on V1/V2 only, VC2 is rotated for about 2.5 mA grid current. VC4/5 is at maximum capacity. H.T. is applied to V3, and VC3 at once adjusted for minimum anode current. This minimum is raised by reducing VC4/5, simultaneously readjusting VC3 for minimum current. When this minimum has reached 100 mA the lamp should light brightly.
Working on the other bands is similar, except that tuning becomes more critical. For the h.f. bands, VC3 should be at almost minimum capacity.
R.F. output for screen grid modulation will be much less than with high level modulation, and the p.a. must be loaded in the manner described until the anode current dip found with VC3 is very flat.

## components list

## Resistors:

| R1 | $100 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R7 | $100 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ |
| :---: | :---: | :---: | :---: |
| R2 | $2 \cdot 2 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R8 | 22k $\Omega 1$ W |
| R3 | 22kS 2W | R9 | 22kS 2W* |
| R4 | $4 \cdot 7 \mathrm{k} \Omega \mathrm{WW}$ |  | 27k $\Omega 2 \mathrm{~W}$ * |
| R5 | $1 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ |  | $33 \mathrm{k} \Omega 3 \mathrm{E}$ |
| R6 | $33 \mathrm{k} \Omega 1 \mathrm{~W}$ | R10 | $47 \Omega 1 \mathrm{~W}$ |
| ( $10 \mathrm{k} \Omega$ for 250 V ) |  |  | * see text |
| Capacitors: |  |  |  |
| C1 | 100pF $1 \%$ S.M. | C10 | 100pF mica |
| C2 | 300pF 1\% S.M. | C11 | $0.002 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |
| C3 | 1000pF 1\% S.M. | C12 | $0.002 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |
| C4 | 1000pF 1\% S.M. | C13 | 100pF mica |
| C5 | 100pF 1\% S.M. | C14 | $0.002 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |
| C6 | $0.01 \mu \mathrm{~F} 500 \mathrm{~V}$ disc | C15 | $0.002 \mu \mathrm{~F} 1.5 \mathrm{kV}$ |
| C7 | $0.01 \mu \mathrm{~F} 500 \mathrm{~V}$ disc | C16 | $0.002 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |
| C8 | $0.01 \mu \mathrm{~F} 500 \mathrm{~V}$ disc | C17 | $0.002 \mu \mathrm{~F} 500 \mathrm{~V}$ disc |
| C9 | $0 \cdot 005 \mu \mathrm{~F} 500 \mathrm{~V}$ disc | C18 | $0 \cdot 005 \mu \mathrm{~F} 1.5 \mathrm{kV}$ |
| TC1 | 40pF ceramic trim | nmer |  |
| TC2 | 40 pF ceramic trim | mer |  |
| TC3 | 25pF double spac | ced va | riable |
| VC1 | 50 pF air spaced | variab |  |
| VC2 | 50pF air spaced | variab |  |
| VC3 | 150pF double spa | aced | variable |
| VC4/5 | $2 \times 500 \mathrm{pF}$ gange | d var | ble |

Switches:
$\left.\begin{array}{l}\begin{array}{l}\text { S } 1 / 2 \\ \text { S } 3 / 4 / 51 \text { pole } 5 \\ 5\end{array} \text { way wafer wafer }\end{array}\right\}$ 'Bandswitch'
S6 Single pole single throw rotary. 'Tune'
S7/8 2 pole 2 way "T/R Switch"
Vaives:
V1 6CH6 with B9A holder and screen.
V2 5763 with B9A holder and screen.
V3 6146 with octal holder, low-loss or ceramic.
V4 OA2 with B7G holder.

## Metalwork:

Chassis $10 \frac{1}{2} \times 9 \times 2 \frac{1}{2} \mathrm{in}$. Type K (H. L. Smith \& Co.) Chassis $8 \frac{1}{2} \times 4 \frac{1}{2} \times 4$ in. Type $P$ (H. L. Smith \& Co.)
2 Panel brackets $4 \times 4$ in. Type C (H. L. Smith \& Co.)
Panel, $10 \times 7$ in. (H. L. Smith \& Co.)
Universal chassis runner $8 \times 2 \mathrm{in}$. (Home Radio)
Universal chassis runner $11 \times 2 \mathrm{in}$. (Home Radio)
Perforated metal $9 \times 8 \frac{1}{2} \mathrm{in}$.
Sheet metal for covers, etc.

## Miscellaneous:

R.F.C.1. $\mathbf{2 . 5} \mathbf{~ m H}$ midget cored choke.
R.F.C.2. 2.6 mH choke, (Denco RFC9).
R.F.C.3. and L.1-11 see text.

Panel meters, $0-5 \mathrm{~mA}$ and $0-150 \mathrm{~mA}$.
Slow motion drive, knobs, 3 panel bushes, 3 shaft couplers, $\frac{1}{4} \mathrm{in}$. insulated rod.
Tag strips, co-axial socket.

Switching should be so arranged that screen voltage cannot be applied to the 6146 unless anode voltage is also present.

It is essential that the power amplifier is not left operating off-tune, or with insufficient grid current, as this will rapidly damage the valve.

The transmitter is best operated into a low impedance load, such as a multiband dipole with 75 ohm feeder, or a tuner feeding an all-band aerial.

## HARMONIC TRAP

This is a series-tuned acceptor, using L11 and TC3. A very closely spaced midget capacitor is not suitable except when working into low impedances.
L11 is best adjusted with a grid-drip meter, so that TC3 gives resonance on the particular channel required. L11 will usually be from about 5 turns $\frac{3}{8}$ in. in diameter and $\frac{1}{2} \mathrm{in}$. or so long, up to 14 turns close-wound $\frac{1}{2}$ in. in diameter. It can be 16 s.w.g. wire, self-supporting.
The best method of adjustment is to operate the transmitter into a dipole or 75 ohm non-reactive load, adjusting VC4/5 for the correct p.a. input. With power off and TC3 about half closed, check the resonant frequency with the grid dip meter, and adjust Ll1 as required. Then with power on, rotate TC3 while observing any interference to t.v. reception. Actual trouble in this direction depends on the siting and type of aerials, efficiency of earthing, strength of the t.v. signal, and other factors.

## CALIBRATION

The ball drive is fitted with a transparent cursor and hair-line. Calibration on $3 \cdot 5-3 \cdot 8 \mathrm{MHz}$ is for the 80 m band only. The $5.5,6 \cdot 5$ and 7.5 MHz points can be found by listening to the second harmonic of the y.f.o. on the receiver, beating with 100 kHz harmonics from a 100 kHz crystal.
Calibration on the 20,15 and 10 m bands is obtained by direct multiplication from 40 m , so these four bands are marked simultaneously. L2 core and TC2 are adjusted for suitable coverage, with 7 MHz obtained when VCl is almost fully closed. This is also 14,21 and 28 MHz . In the same way, $7 \cdot 1 \mathrm{MHz}$ corresponds to $14 \cdot 2 \mathrm{HMz}, 21 \cdot 3 \mathrm{MHz}$, and $28 \cdot 4 \mathrm{MHz}$.

## LATE PUBLICATION OF PRACTICAL TELEVISION

We apologise to readers of our sister magazine Practical Television for the late appearance of the June and July issues, due to a dispute at the printers. We are doing our best to publish the August issue on time but this may also be a little late.


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THE project described here has a number of uses. First, it will operate as a conventional metronome, that is it can be used to provide the time for playing musical instruments. It may also be used as a, short-duration timer or in a situation when using a clock is impractical such as in a darkroom. A similar circuit has been used by the author as a bird scarer; after two years of being without a single ripe cherry from a tree in the garden, a more powerful version was waterproofed and placed at the foot of the tree. A healthy click every few seconds succeeded in keeping the crop intact.

It is possible to build a cheaper metronome than the one described here using one PNP and one NPN transistor (such a circuit was described in Take 20 No. 3, Practical Wireless, July 1969) but this type, although it has several uses, suffers from inaccuracy due to the beat being dependent on the supply voltage and to a lesser extent on the ambient temperature. The circuit used here is very stable and overcomes these inaccuracies by using a unijunction transistor.

The metronome may be calibrated very accurately and once this is done the settings can be relied upon. When the battery voltage falls the output level drops but the beat timing is unaffected.

## THE CIRCUIT

The circuit for the metronome is shown in Fig. 1 and consists of a 2N2646 unijunction transistor operating as a relaxation oscillator. The second transistor, a BC108 in the prototype, simply boosts the output though it is being operated more as a switch rather than as an amplifier.

The operation of the unijunction has been described in past issues of the magazine and for those interested in its operation these should be consulted.

When no voltage is applied to the circuit the emitter junction of the u.j.t. will be at earth potential as the capacitor has no charge on it, but as the unit is switched on


Fig. 2: The component layout and transistor base connections


Internal view of the completed metronome
and the voltage at $b_{1}$ rises.
However, as C 1 has discharged the unijunction is switched off and the voltage rapidly falls. All this takes place very quickly and all you actually get is a series of pulses across R3.
$\operatorname{Tr} 2$ is connected with its emitter grounded, its base directly connected to $\operatorname{Tr} 1 \mathrm{~b}_{1}$ and the loudspeaker acting as the collector load. When Tr1 is not conducting the base of $\operatorname{Tr} 2$ is negative so no current flows but when $\operatorname{Tr} 1$ is producing the pulses Tr 2 is switched on and the pulse is transferred to the loudspeaker, giving a healthy click.

The timing of the beats depends on the time constant of VR1 plus R1 and C1 and a wide range of frequencies are possible by altering VR1. The values in the circuit cover beats from 4 per second to one every 4 seconds and this should cover most music and timing requirements. For other ranges C1 can be changed-for faster beats reduce Cl , for longer ones increase the value.

It is an easy matter to set the control accurately and this has been done on the prototype at the one second setting, this being very useful for timing applications.
VR1 can be either a linear or logarithmic type, but to give more control over the faster beats a log. type was chosen.

Almost any silicon NPN transistor can be used for Tr 2 , including the cheap surplus types.

The output volume is almost entirely dependent upon battery voltage, but a PP3 delivering 9V gives a pretty healthy click.

## CONSTRUCTION

The prototype was built in a transistor radio case and many readers will recognise it. Several kits were based on this case and they are still advertised separately from time to time. If this type is not available local component suppliers often have surplus transistor radio cases and most of these should be suitable. The advantage of using such a case is that it will have a speaker grill and mounting facilities for the circuit board.
Apart from the loudspeaker and the battery, all components are mounted on a drilled paxolin board. Figure 2 shows the component layout and this should be fairly easy to follow.

## 

## THE 'VIBRASONIC' PW25-50 GUITAR AMPLIFIER

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1N4002 2/3 AAZ12 $1 N 4003 \quad 2 / 6$ AAZ17


AS long ago as December 1967 "P.W." carried a report, with full assembly details, on an f.m. tuner incorporating a special-purpose linear integrated circuit, the R.C.A. type CA3014, as the i.f. amplifier stage. Since then other manufacturers have introduced competing f.m. i.f. amplifier i.c.s, and now there are also available units to perform the other functions required in a hi-fi audio system. This month two of them are considered, a stereo decoder and the audio preamplifier to follow it.

## MC1304 Stereo Decoder

First, the stereo decoder, a Motorola unit type MC1304. With a handful of resistors, capacitors and coils this unit takes a "pilot tone" type multiplex stereo signal from the discriminator stage of an f.m. tuner and sorts out the separate right and left
the extent to which right and left channels differ at any given moment.

The difference is actually transmitted in the form of an amplitude modulation of a subcarrier at 38 kHz , and therefore a decoder is analogous to a t.r.f. receiver tuned to this frequency, followed by a matrix which produces the separate channels from the now known sum and difference signals. There is one final complicating factor; to conserve bandwidth the sidebands only of the 38 kHz a.m. subcarrier are allowed to contribute to the frequency modulation. The "suppressed carrier" must be provided if a conventional a.m. detector is to function, and this is in fact produced in the decoder with the assistance of a 19 kHz "pilot tone" accompanying the sum signal.

To these essential functions the MC1304 adds a few "optional extras" in the form of a lamp driver output activated by the pilot tone to indicate the


Left: The external circuitry required for full stereo decoder facifities using the MC1304. The righthand side of the indicator lamp goes to the 12 V supply. Lefthand channel output is between pin 11 and earth and righthand channef output between pln 12 and earth. With a supply voltage of 12 V the resistor at pin 8 should be changed to $2 \cdot 7 \mathrm{k} \Omega$.
channels to feed the audio stages of the receiver system. As many readers will know, the pilot tone system of stereo f.m. transmission was chosen by the broadcasting networks since it is "compatible," i.e. can be received as a mono signal on a standard f.m. receiver. This is because the primary signal is the average of the two stereo channels. However, the demodulated stereo signal also contains components at a frequency beyond the limits of aural sensitivity which carry the difference information, determining
presence of a stereo signal, together with stereo suppression allowing comparison of stereo and mono reception at the touch of a switch. A similar system allows complete audio muting, switching the receiver into a stand-by mode. Like the stereo preamp type MC1303, described below, the MC1304 is supplied in a standard 14 lead dual in-line epoxy package, and the circuit and application diagrams should enable the experienced constructor to achieve success with this unit. Layout of the decoder system is not critical, as the highest frequency occurring is the upper sideband of the 38 kHz suppressed carrier a.m. signal. In regard to matching this unit to the circuitry of the f.m. tuner, the input impedance is typically $12 \mathrm{k} \Omega$,


(b)

Left : Circuit of MC1303, stereo preamplifier unit. Right: Simplified diagram of the preamplifier.
and with this light loading of the discriminator stage of the tuner, no difficulty should be experienced. (One point, however, the satisfactory operation of a stereo decoder presupposes that the tuner had the specified bandwidth for f.m. reception, which must allow for a 75 kHz frequency deviation. This is assured in conventional circuits with 10.7 MHz i.f. and discriminator circuits, but may not be available in pulse-counting type tuners, with their very low i.f. frequencies, even though a particular specimen appears fully satisfactory in its mono performance.)

The output for each channel of the decoder is taken from the collector of a common emitter transistor stage, so that the only constraint on the audio amplifier following it is that its input impedance should not be too low. However, any standard stereo preamp will have an input impedance of $50 \mathrm{k} \Omega$ or greater, so again no difficulty in matching should be experienced. For standard applications elegant and effective output stages to follow the decoder, with power levels in the range of 0.5 to 2 watts per channel, can be provided with i.c.s already mentioned in the pages of this magazine, such as the R.C.A. CA3020 or the General Electric (USA) PA237.

## MC1303 Stereo Preamplifier

Motorola intend their MC1303 preamp to drive an output stage using discrete power transistors to a level of ten watts per channel or greater. The circuit is a development of an industrial dual operational amplifier, the MC1535, and as such provision is made for operation from a dual power supply, which gives both positive and negative inputs to the unit as well as an earth reference. For single source
operation, as would be provided in the amateur circuit and for compatibility with the decoder, the base bias to the input transistors is drawn from a potential divider. The output level will then also be approximately one-half of the supply voltage, and correct for direct coupling to the bases of a complementary output transistor pair of the appropriate power rating.


Typical circuit of one channel of a stereo preamplifier built around the MC1303.

The power supply unit will be a standard system chosen with regard to the requirements of the output stage, with suitable decoupling for the preamp and decoder. Neither this nor the tone control circuits, also conventional, should provide any difficulty for the competent constructor.

## Very interesting

Your correspondent J. B. Jobe (Feb. 1970) describes a phenomenom which I remember witnessing a couple of years ago when servicing a receiver.

I cannot remember the make of the set, though I know it was of foreign manufacture. Its owner had complained of no response from the volume control, although the sound was of reasonable quality and at a reasonable level.

Upon dismantling the set, I immediately noticed that one of the loudspeaker leads had come adrift, though at the time I thought this had occurred during dismantling.

However, after having duly fitted a new potentiometer, I switched the set on before I had connected the speaker and music miraculously emanated from . . . somewhere!

Unfortunately pressure of work precluded me from pursuing the matter at the time, so I wired up the L.S. and forget about it until I read Mr. Jobe's letter.

In retrospect, I know that the sound could not have come from the speaker transformer and I seem to remember suspecting the transistors at the time, though I do not remember whether they were "canned" or not.

As for explaining the phenomenom, I'm afraid I cannot! I am in the process of experimenting with various makes and types of transistors in an effort to reproduce the effect but so far without success. Dare we hope for speaker-less radios in the future? David A. Evered, (Roath Park, Cardiff).

## Some views

I write first to say how much I agree with your Editorial comment in the April 1970 issue of P.W.

The recent decisions by the broadcasting authorities have all been negative to a high degree, and it has always been my opinion that they seem intent on filling up m.w. channels, especially since the outrageous affair of the "pirates" being kicked off the air (although I am by no means a whole-hearted supporter of piracy!).

It seems that an important part of our cultural and entertainment facilities are being used as a political and financial pawn in the hands of the authorities.

My second point is entirely removed from the first and concerns the availability of components and the shops that supply them.

I recently decided to build the "Injectrace" in the Dec. 1969 issue and as I was anxious to get optimum performance from it, I decided to buy new components throughout instead of consulting my "odd-box". Having made a special journey to London to obtain the components for this, you can imagine my dismay and outrage when half the bits were as obtainable as Moondust! In one shop I was informed with great authority that the capacitors (Mylar) were no longer available as the firm called Mylar had "gone bust" six months ago. In another shop I was asked what circuit the capacitors were for and when I showed them the circuit in P.W. I was treated to a long tirade of abuse directed at P.W. and its staff who 'didn't ought to specify fings cos the manufacturer sent em a free sample or two", (or words to that effect). In a very well-known shop I stood for $7 \frac{1}{2}$ minutes awaiting service whilst the assistants discussed in great detail the latest pop music.

The assistants in one wellknown shop have the annoying habit of putting all one's purchases in a paper bag and not showing to one before doing so. This resulted in my coming away one or two items short. One could of course check them at the counter but this would be after paying as they are so quick to take the money.

Several other minor things happened all adding up to a very frustrating day, after which I resolved firmly to shop from the excellent small men who advertise in P.W., by post.-Paul Newman (Aylesbury, Buckinghamshire).

## Oldest in the world?

South Africa may claim to have the oldest ham net in the world in the Early Morning Gang (sic),
which is international in character and has been in existence since 1935. It is also one of the most informal, and although $I$ as an associate and short wave listener have known it for 12 years, I have not sounded the depths of its traditions, customs and "deep mysteries".

From the chairman, affable $\mathbf{O}$. M. Ted (ZS6 William Ida), Johannesburg, I learn that the only founder member is $\mathbf{O}$. M. Bill (Horizontal Willie) who resides symbolically enough in Vereeniging, Transvaal, where the Treaty of Vereeniging was signed in 1902 restoring full peace to South Africa and establishing the Union.

Bill Yapp sets the pace for the amusing mimicry of the EMG (which must never be called a group) by claiming to reside in "the depths of the River Vaal" from which he emerges with a gurgling of water (recorded on a tape recorder) to give his matinal greeting.

The Early Morning Gang is only heard in the mornings between 0400 GMT and 0600 on the 40 -metre band ( $7056 \cdot 3 \mathrm{kHz}$ ), on a.m., and migrates to 3600 kHz during the South African winter. It is a very far flung gang and has members in Cape Town ( 1,000 miles from Johannesburg) Bulawayo, Rhodesia, East London, C. Province, Lesotho, Botswana and Swaziland. Among its members are farmers, a retired hotel keeper, a pharmaceutical expert, a retired mining official, and one nursing sister, who is the only YL. Most of the members put out a pretty good signal, and the gang has been heard in many parts of Africa, and sometimes in Australia and South America. On Christmas mornings as many as 42 hams in Southern Africa have exchanged greetings within the EMG, and passing of the "over" has been expertly handled by the chairman assisted by veterans with more than 20 years membership.

It has dozens of faithful listeners each morning and has officially awarded Five Star Listener status to two for their services in sending in reports.

I'm one, so that's why I've written this.-Hector Watt (Johannesburg).

THE arrival of spring always seems to drag DXers out of their shacks and put them to work in the garden or around the house. One DXer who remained in his shack was J. G. Sowerby of Stranraer and he was suitably rewarded when he heard Radio New Zealand. His equipment is a Lafayette HA600 with either a Joystick or an external long-wire.

This is a case of the early bird catching the worm as reception occurred at 0500 GMT with news followed by music and talks until close-down at 0545. The broadcast is beamed to the Pacific Islands on several frequencies but only 15280 is audible in this country.

Geoffrey Gilham of London S.E. 12 has, once again, used his Eddystone EC10 and Trio 9R59D to good effect and sent in the following $\log$ :

4935 Radio Poti, Brazil with light music at 0220
4835 Radio Mali with news in French at 2015
4870 Dahomey with radio play at 1939
4890 Radio Baré, Brazil at 2315
15125 BED60, Taiwan in English at 1802
15440 DZF8, FEBC in English at 1530
A new reponter this month is. Mervyn Winters of County Antrim whose equipment consists of an AR88D and a 12 foot whip aerial. His list of two dozen stations has been severely pruned by your scribe but among the better catches were:

6095 Radio Baghdad, Iraq in English at 2000
9545 Accra, Ghana in English at 2045
11730 R. Nederland, Bonair in English at 0625
$11915 H C J B$, Ecuador in English at 0900
15020 Radio Hanoi, Vietnam in English at 2000
15160 Radio Ankara, Turkey in English at 2200
15165 Radio Damascus, Syria in English at 1930
15345 Radio Kuwait in English at 1830
21480 RSA, South Africa in English at 1750
21485 Radio Australia in English at 2310
Another regular reporter is T. R. Gibbs of Swindon. His report this month contained the following loggings :

3322 Radio New Guinea at 1200
7135 Radio Peking in German from 2000 to 2030

9715 Cyprus B.C. from 1900 to 2000
$11855 R T A$, Algeria at 1600
15270 Radio Sudan (// with 11835) from 1715 to 1800

Philip Batt of Littleborough, Lancashire is another new reporter, his equipment is a PCR3 receiver and a 92 foot long-wire at 15 feet elevation. His log included:

7105 Radio Tirana, Albania at 0015
7110 All India Radio at 2115
11995 Teheran, Iran at 2010
15335 Deutsche Welle, Kigali relay at 0659
15365 R.N. Espana, Canary Is. in Spanish at 1910

# THE BROADCAST BANDS Malcolm Connah 

15400 Radio Kiev at 1935
15405 Voice of Nigeria at 1815
17750 Radio Pakistan in English at 0900
17825 NHK, Tokio, Japan in English at 0900 21600 Radio Australia at 0620
Raymond Peart of Worcestershire used his Spidola transistor receiver and 100 foot long-wire to send in his first report to the column:

6135 Radio Warsaw, Poland at 1830-1900
7210 Radio Norway, English news, 1200-1230
7219 Radio Nederland, Happy Station at 0930
9605 Radio Prague in English at 1730-1830
9665 Radio Switzerland Calling at 1830
9770 Austrian Radio with news in English, 13001400

17705 Radio Havana, Cuba in English at 20102138

Roy Patrick of Derby has sent in some very interesting items of news including:

Radio Pyongyang has been heard by Roy at 1900 in a frequency of 6540 with programmes in English.

Radio Mexico is now using two frequencies, according to Roy these are 9745 and 15135 kHz .

Malcolm Robinson of Liverpool sent me the schedule of Radio RSA, South Africa which reads as follows:

English: Daily Transmission to:-
U.K. and Ireland from 1756 to 1850 still using the 21480 and 15250 outlets.

Africa General from 1056. Heard at good strength on 25790 and 21535 also with unheard outlet of 15220; and from 1450 to 1550 heard on 21535 and unheard on 15220. An additional outlet on Saturdays and Sundays on 11900 is in use from 1056 to 1450.

Monday-Saturday Transmissions to:-
North-West Africa from 0645 to 0658 heard on 21535 and 17805 and unheard on 15220 and 11900.

Afrikaans: Monday-Saturday Transmissions to:-
Rhodesia, Malawi and Zamibia from 0600 to 0613 heard on 17805 and 15220 , also broadcasting on 11900 and 9525.
Sundays to:-
East and Central Africa from 0656 to 0950. Heard on 25790 also broadcasting on 15220 .

French: Monday-Saturday to:-
Central and North Africa from 0630 to 0643 heard on 21535 and 17805 also outlets on 15220 and 11900 .

Potuguese: Monday-Saturday to:-
Angola from 0615 to 0628 heard on 17805 also with outlets on 15220,11900 and 9525.

We have been asked to point out that in the report on page 57 in the May 1970 issue, the reference to the Codar CR70A was not intended to be detrimental. It was not intended as a report on the receiver and reception was of course governed by conditions.

## THE AMATEUR BANDS David Gihson, G3JDG

READ all about it. Who is GB3WRA? Why are strange callsigns coming from PY land? Who has a 21-mile antenna buried in ice?
Listen out on all bands $160-10$ metres on Saturday, September 5, for GB3WRA. This will be a special station located at High Wycombe, Bucks, for the annual Wycombe show. Visiting amateurs and s.w.ls welcome.

Brazilian stations apparently used the prefixes ZV, ZW, ZX, ZY and ZZ for the CQ WW contest because the contest was for prefixes. You begin to wonder if a countries list or a callbook is really of much use these days.

John Moore (Leicester), relates the strange saga of KC4AAD who is located near the U.S. base "Byrd" some 650 miles from the South Pole at $120^{\circ} 30^{\prime} \mathrm{W}, 79^{\circ} 54^{\prime} \mathrm{S}$. Are you sitting comfortably? Then I'll begin. This station has a 21 -mile dipole which is resonant at just under 1 kHz and is used on 3 kHz for experimental purposes. Quick, get the hi-fi out, you might log him. Apparently some five years ago the antenna, all 21 lovely, dangly miles of it, was lying on the ice. Now, it is four feet below the surface. Anyone at the North Pole is advised to be on the lookout for a long piece of wire which should be through in about another seven million years' time.
J. Leaver (Lancs), home brew s/het, 100ft wire wound round the loft, a.t.u., has sent in a fantastic topband $\log$ which is $99 \cdot 893 \%$ c.w. Among the stations heard, which includes 30 OK and 13 OL stations are: DL9KRA, EI9BG, GI3JEX, GI6TK (s.s.b.), GM3BGW, GM3LQI/P, GM3SVK, GW3TUG, GW3ZEY, OK1ABK, OK2BMR, OK3TCA, OK5TOL, OL1AUL, OL2ANK, OL4AMF, OL5AMA, OL6AKP, OL8ANL, PAØPN, 5B4NZ, 9H1BL. Would-be c.w. sleuths are advised to QRX 1.85 MHz down to band-edge.

Steve Ireland (Kent), PW Clubman, 19-set variometer, 67 ft end fed, says best time to listen for DX on 80 is 2130 , especially the net on 3.795 MHz . Steve's best on the band are: CN8HD, CT2AK, CR6IV, EP2DX, HBØLL, OY2X, OD5BA, PY1HA, PY7BFN, PZ1AH, SM6CNS/MM, TA2E, W4RDD / P/VP9, W2NIN, K3JH, XE7KS, YVØAI, ZC4CB, ZM2BCG, 4X4KT, 4X4YM.

I've heard of "A little bird" whispering in someone's ear, but when it comes to 14 MHz , the PCR3 Jelonging to P. Batt (Lancs), takes a lot of beating. The $22 \mathrm{ft} 45^{\circ}$ "vertical" is connected via a 70 ft single wire feeder and an a.t.u. Proof of this r.f. pudiding is: AX2AYE, AX3AD, AX3LAF, AX4SD, CE3OE, EP4OE, HP1MD, K4ZL, KP4CM, KV4AB, LU5B, PY1BSC, PY7ARM, VK5RFJ, VK7WH, VP2DOE, VP2VO, VR1IC, VE3CU, VE4SK, YV3US.

Messrs Anderson, Roberts and Apperley have confessed! Their chemistry master is none other than G3XMM. Heard on 21 MHz on the guv's HRO and 80ft end fed: AX3DCR, DU1CH, EL2AI, EP2KB, G3PAC/W9, HR2HHP, HV1CN, JA6MDD, JA8DGR, KR6HR, LU5XE, MP4MBB, MP4TDR, PY2EIR, SV1CZ, VE3EQA, VP7CG, VP9GE, VU2DK, YV1SA, ZM1AIX, ZS6AL, ZX1MB, ZX2DVH, 9Y4MM all on s.s.b.
A. Crooks (Leicester), RA1 plus PR30, 45 ft end
fed also reports a series of interesting squeaks on 21 MHz s.s.b. Andy's $\log$ reads: CR4BC, CR6GA, CR7IZ, EA8GZ, EL2BZ, EP2DX, HS3ACP, JA1SQI, JAIYGM, JA4AOF/MM (near the Phillipines), JA5ARU, JẢ6MS, JA9IL, JH1BLX, JW7UH, KP4ES, OA4LM, OI3NY PY4BLH, TG9RR, TJlAR, UA0SU, VO1FX, VU2KV, VU2OLK, ZS2PX, 4X4BR, 6W8BD, 9H1CB.

Gear-CR100/2, 60 ft end fed. Listener-J. Moore (Leicester). Log: AX3VK, CR6GA, CR6MH, CR7BB, CX7BF, DU1FH, FG7XL, FL8MB, HK3VA, HS5ABD, HT1HSM, JA1HTM, JA2EQ, JA4FRB, KV4AD, KZ5JW, LU2DEK, LU5DDM, LU9NA, OA4LM, OD5BZ, PJ9JR, PY2HT, PY8II, UH8BX, UL7GAW., VE3MR/4X4, ZE1AA, ZE3JO, ZS6AL, ZV2CK, ZY2RZ, ZZ1CAD, 4S7PB, 4Z4HF, 5J3WO, 5Z4LS, 7Q7LZ, 9H1BA, 9J2PV all on ten metres s.s.b.

It's all happening on two metres. N. Richardson sends in an impressive $\log$ which included F1BCI/P located some 10 km south of Calais. Nicholas is in Bucks, and uses an 8-element Yagi, Garex converter, PR30 and CR7OA tuning $28-30 \mathrm{MHz}$.
"Keep up the good work in printing 2 metre logs in PW," says S. Carter (Staffs), while Glyn Richards (Isle of Wight), admits to riding his trusty 4 -over-4 slot fed on the 144 MHz trail. The JXK converter and GC-1U got these a.m. stations which are between 120 and 180 miles away: G3GZJ (c.w.), G3PWJ, G8CSU/P, GW3CBY, GW3ITZ/P, GW3OXD/P, GW3NWR, GW3VKL/P.

From France, Glyn logged: F1AAD/A, F1TE/P (both in Cherbourg), F1BCI/P (Calais), F3LP (Le Havre), and from further afield-HB9AEN/P.

Mobile rallies in July include: July 5th, Cornish ARC rally at St. Ives; 5th, ARMS rally at RAF/ USAF air base, Alconbury (highly recommended); 12th, Upton Mobile Rally, Upton-upon-Severn, Worcs; 19th, Mobile Rally at Scarborough; 26th, White Rose rally at Leeds; 26th, Saltash rally; August 2nd, Mobile picnic at Bristol; August 9th, Woburn Abbey mobile rally; August 9, Mobile picnic at Stratford-upon-Avon.

Deadline for logs for The Amateur Bands this month is the 15 th.

## RSGB EXHIBITION 1970 <br> PRACTICAL WIRELESS PRACTICAL TELEVISION

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## WHEN?

Wednesday Aug. 19th to Saturday Aug. 22nd 10 a.m. to 9 p.m. daily
WHERE?
The Royal Horticultural Society's New Hall, Greycoat Street, Westminster, London, S.W. 1 (Nearest Station-Victoria)

## be CAREFUL ... !!! NOTE THE DATE THE SHOW'S EARLY THIS YEAR!



A$S$ is well known, a t.r.f. type receiver is capable of surprisingly good results, when correctly operated and circuit design is very much simpler than with a superhet.
The receiver described here covers approximately 1.3 MHz to 20 MHz or 230 to 15 metres, in three switch selected wavebands. The OC81D output stage gives very good headphone volume, from a large number of transmissions. Coverage includes the 160 m and 80 m amateur bands, ship and other frequencies, as well as the more usual short wave bands.

A push-pull output stage can be added to boost
volume for loudspeaker reception. This stage is in the form of an optional module which can be plugged into the receiver output socket.

## Circuit

This is shown in Fig. 1, with the coil for one band only. The remaining two coils are wired in the same way as that shown.

VC1 is the main tuning or band-setting capacitor and the small capacitor VC 2 is for bandspreading.


Fig. 1 : Circuit of receiver. The circuit of the additional audio module is shown in Fig. 7.


Its full rotation covers only a narrow band of frequencies. In use, VC1 is set for a band required, such as the 25 m or 31 m band, and this is tuned with VC2. The tuning "rate" with VC2 is about the same as that which would be obtained with a $20: 1$ reduction drive on VC1, and this method is inexpensive, convenient, and easy from the building point of view. These capacitors need not have the exact values shown.

Each inductor has a tuned section $C$ to $E$, base coupling $E$ to $B$, and aerial coupling $A$ to $E$ and 3-pole 3-way switch brings in the coil required. Alternative aerial sockets are fitted, A1 is better with a reasonably long aerial and when an earth is available. A2 is used in other circumstances, and has a small series capacitor TC1.

An OCl 170 , Tr 1 , is used as a regenerative detector, with feedback through TC2 and regeneration control


Fig. 2 : Top view of circuit board and identification of transistor connections.

VR1. For proper results with a t.r.f. receiver, proper regeneration on all frequencies is absolutely essential, and this circuit was found to perform well.

The output of the detector is coupled to an OC71, Tr 2 , first audio amplifier, and VR2 is the audio gain control. Tr3, an OC81D, is intended for use with medium impedance ( $500 \Omega$ ) headphones. A single earpiece or miniature personal earphone not being very suitable for regular s.w. listening.

## Circuit Board Module

Most of the components are assembled upon a ready perforated insulated board about $4 \frac{3}{4} \times 2 \frac{1}{4} \mathrm{in}$. which is later fixed to the chassis by three bolts, two of which provide earth returns.

Fig. 2 is the top of the board. The easiest method is probably to insert the resistors and capacitors a few at a time, spreading the wire ends so that they do not fall out. The boand is then turned over, and the leads are cut to suitable length, and soldered. Check all component values as they are fitted, and note that the larger canacitors have their polarity indicated, as shown.

Fig. 3 is the underside of the board. Where wire connections are necessary, some 22 s.w.g. tinned copper or similar wire is used. Insulated sleeving is put on all leads which may touch other bare wires or joints. Two tags are placed as in Fig. 3, and are common to the positive or earth circuit and chassis. These tags are tightly held by nuts or $\frac{1}{2} \mathrm{in}$. long bolts.

When the circuit board is fixed to the chassis, put an extra nut on each bolt, so that the board is about $\frac{1}{4}$ in. clear of the chassis. The bolts then pass through holes in the chassis, and further nuts are put on and locked tight. Bare joints and wires should be clear of the metal chassis, but a piece of card can be put under the circuit board, to avoid any possible short circuit.

Transistor connections are shown in Fig. 2, and it may be found helpful to put thin coloured sleeving on the wires to help identify them. Red may be used for the collector, black for the base, and some other colour for emitter leads. The wires are left at such a length that the transistors are about $\frac{1}{2} \mathrm{in}$. clear of the circuit board.

A number of flexible leads run from the circuit board, for connections to the volume control and elsewhere. It is helpful to identify these wires by using coloured sleeving, or by employing thin coloured flex.

A lead from C1 passes directly down through the chassis to the bandswitch, Fig. 4. Leads from VR1 go down through a common hole, as do leads from VR2. Take a flexible lead from C9, for battery negative, and solder on a negative battery fastener. Run leads from C9 and OC81D collector which go to the headphones socket.


Fig. 4 : Top view of chassis and circuit board.


Fig. 3: Bottom view of circuit board showing interconnection of components.

## Chassis

The chassis has flanges to which the panel is bolted as in Fig. 5, and Fig. 4 shows how the circuit board is fitted. The rotor connections for both VCl and VC2 run to a tag MC, in Fig. 4. A further tag, under the chassis on this bolt, is the earth return point for the coils, Fig. 5.

TC1 is soldered to the insulated tags of a tag-strip, Fig. 4, and TC2 is soldered directly to one of the stator tags of VC1. A lead from the other stator tag passes directly down through the chassis to the bandswitch.

The tags of VR1 and VR2 are lettered, and must, of course, be correctly connected to the circuit board. The metal chassis is the common positive or earth return. A lead with a positive battery fastener is soldered to the switch incorporated in VR2, as in Fig. 5.


Fig. 5: Bottom vlew of chassis and wiring of colls and controls.
The cabinet listed has an inner flange, so the chassis has to be mounted a little high, as in Fig. 6, to clear this. With a receiver of this kind, a metal case is helpful in avoiding hand-capacity effects.

## Coils and Calibration

The three coils are wound in the same way, except for the numbers of turns. L1 and L2 are on $\frac{1}{2} \mathrm{in}$. diameter insulated formers, $1 \frac{1}{2} \mathrm{in}$. long, and L3 is wound on a ferrite rod 2 in . long and $\frac{3}{8} \mathrm{in}$. in diameter. Paxolin tubes can be mounted by cutting dises of insulating material, and cementing these in one end. A small bolt will then fix the coil to the chassis.

All windings for L2 are of 32 s.w.g. enamelled wire, turns wound side by side. Fix the wire at C, Fig. 5, near one end of the tube, by passing it through small holes, or cementing it. Wind on 34 turns. Bare the wire and form a loop E, continue for a further 4 turns in the same direction, and finish at B . Leave the wire ends long enough to reach the switch. Solder the wire on at E , leave about $\frac{1}{8} \mathrm{in}$. space, and wind 7 turns, finishing at A .

With all coils C goes to VC1 (via switch), E to chassis and earth line, B to transistor base (via switch and C 1 ), and A to aerial, again via the switch.

The highest frequency coil L1 has 15 turns from $C$ to $E$, and 3 turns from $E$ to $B$, of 22 s.w.g. enamelled wire. E to A is 4 turns.

The lower frequency coil L3 is wound on a ferrite rod to reduce the number of turns required. C to E is 27 turns, and E to B is $1 \frac{1}{2}$ turns, of 24 s.w.g. double


Fig. 6: Position of chassis relative to panel and bandswitch connections
cotton-covered wire. E to A is 7 turns of 32 s.w.g. enamelled wire. The end of the ferrite rod is a tight push fit in a hole in a strip of paxolin, and is cemented here. It is then mounted with two bolts, as in Fig. 5.

Fig. 6 shows the rotary switch connections, as seen from behind. (This is actually a 4 -pole switch, with one pole unused. To avoid any chance of a mistake here, L2 only can be wired in, and the receiver tested with the switch in its central position. If the wrong tags are used for any coil or connection, the receiver cannot function.
$\mathrm{VC1}$ and $\mathrm{VC2}$ are fitted with large knobs and dials calibrated $0-100$. VC1 is secured with three bolts, which must be very short to avoid fouling the plates. A small bolt was fitted above each dial, with its slot vertical and filled with paint, so that the dial numbers can be logged. Dial readings of VCl for the various bands are given below. These are only a guide, because the home-wound coils and other factors will influence coverage.

|  | Freq. | Dial |
| :---: | :---: | :---: |
| Band 1. | 20 MHz | 10 |
|  | 15 | 20 |
|  | 10 | 38 |
|  | 8 | 55 |
|  | 6 | 90 |
| Band 2. | 8 MHz | 12 |
|  | 6 | 20 |
|  | 4 | 40 |
|  | 3 | 70 |
| Band 3. | 4 MHz | 15 |
|  | 3 | 25 |
|  | 2 | 50 |
|  | $1 \cdot 6$ | 68 |
|  | $1 \cdot 3$ | 95 |

## Operation

With a t.r.f. receiver, adjustment of the regeneration is of the greatest importance. If there is little or no regeneration, almost no signals will be heard, and tuning will be very flat, but as regeneration is
increased, a point is reached where sensitivity and selectivity improve enormously. This shows that the detector is approaching the point where it will begin to oscillate. Optimum results are with regeneration so adjusted that the receiver is just failing to oscillate. Advancing regeneration further will cause whistles when tuning through signals, and an almost complete loss of signals.

Initially, TC2 is almost wholly unscrewed. When VR1 is rotated slowly in a clockwise direction, background noise should begin to increase, and signals heard. If oscillation occurs when tuning through a signal back off VR1 very slightly. If regeneration up to the oscillating point cannot be obtained on some frequencies, screw down TC2 a little.

TCl should normally be fairly well open, except for a very short aerial. If TC1 is screwed down, and a long aerial attached, the damping introduced may prevent regeneration, and mäy cause flat tuning.

Current drain is about $6-8 \mathrm{~mA}$ or so, and any 9 V battery is satisfactory.

## Push-pull Amplifier Module

This amplifier, Fig. 7, can be plugged into the t.r.f. short wave receiver, to obtain speaker reception. No changes are needed to the receiver. The jack plug is put in the receiver headphones socket, audio signals being taken to the primary of the driver transformer T1. The plug also provides the supply voltage for the output stage.

## $\star$ components list



R12 and R13 set the base operating conditions for the pair of output transistors, and R13 is a miniature pre-set resistor. This allows easy adjustment for best results with any pair of output transistors of the type shown, or similar type.

The amplifier module is mounted on two small brackets which form the positive or chassis return. This connection is essential. If the amplifier is not fixed to the chassis in this way, a lead must be provided here to complete the circuit. In this case, the amplifier could be in the speaker cabinet.

fig. 7 : Circuit of amplifier moduie.

The components are mounted on an insulated board about $3 \times 2 \frac{1}{4} \mathrm{in}$., Fig. 8. Provide a short flexible lead from the slider of R13, to one end, as shown. One tag of the driver transformer T 1 is identified by a green dot, and this should be placed as in Fig. 8. Flexible leads run from the primary to the jack plug. Connect the plug is such a way that the negative circuit is correctly made when it is inserted.


Flg. 8: Vlews of amplifer clrcuit board. Care must be taken to ensure correct wifing of jackplug.

Flexible leads from T2 run to the speaker, which should be a reasonably large $2 \Omega$ or $3 \Omega$ model, fitted in a cabinet, or attached to a baffle board. The amplifier is attached to the receiver by the two brackets, and stands vertically behind the receiver circuit board.

When the amplifier is in use, a PP9 or similar large 9 V battery is more suitable. Temporarily, place a 100 mA or similar meter in series with one battery lead. Set R13 to minimum resistance and plug the amplifier plug into the receiver headphones socket. When the receiver is switched on, the meter should show about $8-10 \mathrm{~mA}$. Move the slider of R13 to increase its resistance until the current rises about 2 mA to 4 mA above the original figure.

Subsequently R 13 may be re-adjusted, if necessary, for best results with a signal tuned in. Current should not be over 15 mA or so with no signal, rising to $30-40 \mathrm{~mA}$ with good volume. The best setting for R13 depends somewhat on the individual transistors.

Headphones can be used as before, when wanted, by withdrawing the amplifier plug, and inserting the headphone plug. This puts the push-pull amplifier completely out of use.

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THE
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MEDIUM-WAVE stations in Europe operate on channels spaced 9 kHz apart as laid down in the Copenhagen Plan. There are a number of African and Asiatic stations in the gaps between these channels and these can be heard during the evening before the majority of Europeans close down. A selective receiver of communications standard is an advantage for this type of DX while a loop aerial is helpful in cutting down splash from adjacent channels. Baghdad Iraq 760 kHz can be located between West Germany on 755 and Sottons 764. The programming is in Arabic though it sometimes broadcasts western music before closedown at 22.30 GMT. Occasionally there is a 1 kHz heterodyne on this station caused by $C Q A 759 \mathrm{kHz}$ in the Portuguese island of Sao Tome West Africa. Sandwiched between USSR on 890 and Milan on 899 is EFJ57 Radio Juventud de Canarias Tenerife on 895 kHz . This station relays news from Radio Nacional Espana and specialises in serious music until sign-off at midnight. Deir el Zor 959 kHz Syria has Arabic programmes until 2230 hrs and can be found just below Paris 962 kHz . Other stations to look for on these 'split' frequencies include Riyadh Saudi Arabia on 588; Jerusalem 677; Kermanshah Iran 985; Kuwait 1345; BBC Eastern Relay in the Persian Gulf on 1410. Urumchi in western China is a regular on 1525 with Russian propaganda and jamming. Two long wave Asiatics logged recently are Tselinograd in Kazakstan behind Warsaw 227 kHz and Ashkhabad 375 kHz , both at 2200 hrs .

A mystery Greek-speaking station has been heard just out-of-band on 1610 kHz . It was first reported to Sweden Calling DXers by a listener in Austria and further information has just come to hand in a letter from Angelo Coppola of Naples who has logged it several times after sunset. The programmes are mainly Greek folk music and the identification sounds like Radiophonikos Stathmos Chidas. Has anyone heard this station? There is nothing listed on 1610, the highest MW channel being 1603.

Stations along the east coast of North America can be logged for about one hour before sunrise during July. European interference is light at this time owing to the aproaching daylight from the east while QRM from inland North America is absent, enabling stations that would be classed as 'difficult' in winter, to be heard. Look for WHAM Rochester NY on 1180; WLIB New York City 1190; CKCW Moncton N.B. 1220; WSYB Rutland Vermont 1380; $W N J R$, the all-negro station in Newark N.J. 1430; CBG Gander Newfoundland 1450; WHEC Rochester NY 1460; WPTR Albany NY 1540 mixed with ZNSI Nassau Bahamas. Those right on the top of the band are usually prominent, such as WSFR Ft. Lauderdale Florida 1580; WSMN Nashua N.H. and WAKR Akron Ohio, both on 1590 and CJRN Niagara Falls Ontario 1600. Nearer home on the periphery of Europe are three A.F.R.T.S. stations not normally heard except at sunrise in summer. These are Kenitra Morocco 1484; Lajes Terceira Azores 1500 and Tripoli 1594.

CHARLES MOLLOY

# OEPPAMDER COMPRESSOR C.R.Bradley 

ALMOST every audio source can benefit from a degree of compression or expansion of the volume range. The unit described here provides a variable amount of compression or expansion with low distortion and can be added to almost any sound system. It can be an additional 'luxury' control (like the tone controls) in a hi-fi system, or it can have more important uses in tape recording, pop music and radio communication as will be described. It can also be used to sustain notes played on an electric guitar, or give a tape recorder automatic level control.

## PRINCIPLE

The level of an audio signal may be controlled by passing it through a stage with variable gain. A simple example is the volume control in a radio receiver, if we can regard it as a stage on its ownsee Fig. 1a. When the slider is at the bottom end of the track, the gain of the stage is zero and the output signal is zero. When the slider is at the top end of the track, the gain is unity (disregarding loading effects) and the output signal is maximum. The range of gain is 0 to 1 and it is controlled by mechanical action on the control spindle. Note that if the slider is left in a certain position, say half way along the track (gain $=\frac{1}{2}$ ), the dynamic range (volume range) of the signal is not affected. Thus if the input level doubles the output level doubles also, regardless of the control setting (except at zero of course).

Now suppose the volume control in Fig. 1a could be turned up when the input level is low and turned down when the level is high, all this to be done automatically without noticeable delay. The output level could then be held constant in spite of wide variations in the input level. This would be volume compression or reduction of the dynamic range. Conversely, if the volume control could be turned

down when the input level is low and turned up when the level is high we would get volume expansion or exaggeration of the dynamic range.

Either of these processes can properly be called a.v.c. (automatic volume control). The circuit in a radio receiver which maintains a constant r.f. input to the detector is sometimes misnamed the a.v.c. circuit; it is more correctly a.g.c. (automatic gain control) applied to an r.f. stage, whereas a.v.c. is


Fig. 1: A standard volume control and a simple method of audio expansion or compression using an L.D.R.
a.g.c. applied to an a.f. stage.

It might be thought possible to obtain volume compression or expansion by driving the volume control in Fig. 1a with a servo motor. Unfortunately, any practical mechanical linkages would have significant inertia and friction and the system would be too slow to keep up with fast volume changes. Therefore it is necessary to design a stage whose gain can be controlled electrically. But before considering all-electric stages, the circuit in Fig. 1b provides an interesting use of light for a.v.c. $\mathbf{X}$ is a cadmium sulphide photocell and $L$ is a lamp mounted close to it. The lamp brilliance depends on the control voltage. When the control voltage is high the lamp shines brightly and the resistance of


Fig. 2: Radio receiver a.g.c circuit and graphs showing effect of a.g.c on gain.


X is low, resulting in a high output level. When the control voltage is low the lamp shines dimly and the resistance of $\mathbf{X}$ is high, resulting in a low output level. This arrangement is often used in remote volume control applications and in some audio compressor and expander circuits. The lamp and photocell can be bought as a single sealed unit for this use. After experiment, this circuit was discarded in favour of the circuit to be described because the power consumption of the lamp is high and the relation between the control voltage and the output level is very non-linear. Also the heat mass of the lamp filament and the photocell characteristics introduce a delay in response.

## VARIABLE GAIN STAGES

The gain of a class A amplifier stage can be varied by moving the bias toward cut-off. This is a type of gain control used in radio a.g.c. circuits-see Fig. 2. This circuit has the disadvantage of severe distortion of the output waveform when the stage is near cut-off. In a tuned r.f. stage this distortion is tolerable as the next tuned circuit will eliminate harmonics and restore the sine waveform. But the distortion is excessive for a full range a.f. stage, particularly in an audio compressor where the stage would be biased near cut-off when the input signal was at maximum.

Another circuit which was investigated is shown in Fig. 3. This is a long tailed pair where the audio signal is passed through one of the transistors (Tr2). When the control voltage swings negative, Trl turns


Fig. 3: Two transistors connected as a long tailed pair can control dynamic range but only at low input levels.
on. As $\operatorname{Tr} 2$ base is held at constant potential, the increased voltage drop across $\mathbf{R}$ biases $\operatorname{Tr} 2$ toward cut-off and the audio signal is attenuated. This circuit gives a good performance but the input signal must be small to avoid distortion.

The final choice of circuit is shown in Fig. 4. It


Fig. 4: The basic control circuit used in the final circuit.
is a conventional common emitter amplifier with a field effect transistor placed in series with the emitter bypass capacitor. The f.e.t. is used as a variable resistor controlled by the gate voltage. When the gate voltage is zero, the source-to-drain resistance is low and Trl emitter is fully decoupled by C. When the gate voltage swings negative, the resistance rises so that the decoupling action of C on Tr 1 emitter is reduced. The gain of the stage is now reduced by negative feedback from the unbypassed emitter resistor $\mathbf{R}$.
It will be noticed that the f.e.t. is being used to control alternating current. The circuit was first tried with an additional resistor from h.t. positive to the f.e.t. source to give a steady d.c. bias. This was discarded when it was found that as the f.e.t. is basically a symmetrical device, it can be used on a.c. In this circuit the source and drain leads can be swapped with no great effect on performance, althought one arrangement is slightly better with the low cost f.e.t. specified-which is not specified as a symmetrical type in any case.

The main advantage of this circuit is the low distortion over a wide range of signal level. The transistor is always biased in class $\AA$ where distortion is minimum. Unlike any of the previous circuits, the distortion reduces as the gain is reduced; this is due to the increased negative feedback from $R$. This makes it particularly suitable for an audio compressor. The transistor and the f.e.t. also provide useful amplification of the audio signal and the control voltage respectively.

## COMPRESSOR CIRCUIT

The arrangement for audio compression is shown in Fig. 5. The output signal is sampled by a single stage amplifier A. This provides a signal across R1 which is rectified by $D$ to give a negative-going voltage across the diode load R2. Audio frequency components are smoothed by Cl to produce the steady control voltage which is fed to the f.e.t. gate. Since the gate impedance of the f.e.t. is very high, the attack/decay time of the compressor is determined by the values of R3 and C2. The graph in Fig. 6 illustrates the action of compression. When the input signal is low, the f.e.t. gate voltage $V_{g}$ is between 0 V and -2 V and the transistor gives a high gain.


Fig. 5: The compressor circuit principle.

When the input signal level rises so that the gate voltage passes from -2 V to -3 V the gain is progressively reduced. Higher signal levels cannot be further compressed as the f.e.t. has already blocked all the emitter decoupling. However, distortion due to clipping only sets in with very high signal levels.

The flattish portion of the solid curve in Fig. 6

Although squelch has its own uses it is not the kind of volume expansion required.

The same arrangement is more workable if the signal sampled by $A$ is the unexpanded input signal; this removes the positive feedback loop. However, a very high gain is requred in A and the expansion proves to be very non-linear (Fig. 7b).

level

(a) different f.e.t gate voltages for the circuit in Fig. 5.
shows the range of compression. The higher the gain of amplifier A the flatter it will be and the greater will be the degree of compression. As A samples the compressed output and not the input signal, the circuit cannot 'over compress' strong signals no matter how high the gain of A, i.e. it is impossible for the curve to slope downwards from left to right.

It must be understood that the non-linearity of the curve in Fig. 6 does not cause harmonic distortion in the output signal as it represents a nonlinear volume response, not instantaneous response. The time constant $\mathrm{R} 3 / \mathrm{C} 2$ is chosen so that the gate voltage does not change appreciably during even the longest (bass) audio cycles. The instantaneous response curve at any time is one of the dashed lines in Fig. 6, and these are linear.

## EXPANDER CIRCUIT

Although audio expansion has simply the reverse effect of audio compression, the circuit design is not as simple as this might suggest. We might try to use the circuit in Fig. 5 but with a negative bias on the f.e.t. gate and the diode $D$ reversed. The transistor would then give a low gain on weak signals and a high gain on strong signals, as desired. Unfortunately a positive feedback loop exists. A strong signal causes the gate voltage to swing towards zero which increases the gain; this increases the signal sampled by A which drive the gate voltage further towards zero and so on. The arrangement gives a squelch action illustrated in Fig. 7a i.e.: signals below a threshold level are amplified with low gain and signals above the threshold level are amplified with high gain.



Fig. 8: (left) Expansion circuit principle. Fig. 9 : (above) The arrows on the graph show how a small range of volume in the input is expanded to a wider range.

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is amplified by Tr 3 and fed via C 7 and VR3 to Tr6 which is the amplifier A in Fig. 4. The degree of compression (or expansion) is controlled by VR3. The signal at Tr6 collector is rectified by D1, smoothed by C15 and fed to the f.e.t. gate via one of the sets of time constant components selected by S2.

For compression, the signal at Tr 3 collector is also taken directly to the base of emitter follower Tr5 which provides a low impedance output on JK2; in this mode Tr4 has no function.

For expansion, the signal at Tr 1 emitter is used as described in Fig. 8. This signal is taken through VR2 and C 8 to Tr4 base. The signal at Tr 4 collector is taken directly to the base of output stage $\operatorname{Tr} 5$. The potentiometer VR2 works only on expansion; its resistance forms a potential divider with the varying source-to-drain resistance of the f.e.t. and it is used to set the range of expansion. All the transistors are working as $\operatorname{Tr} 3$ is still delivering a compressed signal to Tr6.

Base bias for both Tr 3 and Tr 4 is provided via R14 from $\operatorname{Tr} 5$ emitter; $\operatorname{Tr} 5$ forms a d.c. feedback pair with either $\operatorname{Tr} 3$ or $\operatorname{Tr} 4$ on compression or expansion respectively.

It is possible to experiment with the time constant components selected by S 2 to obtain any desired
attack/decay characteristic; some quite complex networks might be used here to obtain a particular result. The values of R22 to R24 shown in Fig. 10 have been chosen to give the following choice of characteristics in conjunction with C16. In position 1 of S2, C16 can rapidly charge and discharge through R22. The compressor/expander therefore has as fast a response to volume changes as is possible without feedback arising from audio frequencies reaching $\operatorname{Tr} 2$ gate. In position 2 of S2, R22 is replaced by a higher value R23 resulting in a slower response. Position 3 of S 2 gives a special attack/decay characteristic intended for automatic level control use with a tape recorder (S1 switched to compression).
The compressor responds very quickly to an increase in signal volume when forward current flows in D2 to charge C16 negatively, but C16 can only discharge very slowly through R24 as the leakage current of the f.e.t. gate is negligible. Hence the f.e.t. gate voltage depends on the peak volume level. This characteristic is ideal for the purpose since volume peaks are quickly brought down to a constant level to avoid over-modulating the tape, but the gain does not increase much during lower level sound passages. Thus the dynamic range of the material recorded is not greatly affected.

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Fnll wave Bridge $75 \mathrm{~mA} 10 /-; 150 \mathrm{~mA} 19 / 6$ ；TV recta． $10 /-$ NEON PANEL INDICATORS 250V AC／DC Red，Amber $4 /-$ RESISTORS．Preferred walues， 10 ohms to 10 meg．
 Ditto $5 \%$ Prelerred values 10 ohmit to 22 meg 0 ．， WIRE－WOUND RESISTORS 5 watt， 10 watt， 16 watt 10 ohms to 100K．2／－each；2t watt．Iohm to 8.2 ohms 2／－

## Q MAX CHASSIS CUTTER

## Complete：a die，a punch，an Allen sorem and key


 TRANGISTOR MAINS POWER PACKS．FULL WAVE 9 volt 500 mA ．Size $4 t \times 24 \times 2$ 2in．Metal case．$\times 49 / 6$
Crackle finish．Outpul terminala．On／off switch． Crackle fnish．Output terminala．On／off awitch．
Half Wave 9 volt 50 mA ．Size $2 \frac{1}{2} \times 1$ in．Snap terminale $82 / 6$

## MAINS TRANSFORMERS

$250-0-25050 \mathrm{~mA} .6 .3$ v． 2 zmps ，centre tapped Post
$5 /=$ each $250-0-25080 \mathrm{~mA} .6 .3$
$250-0-25080 \mathrm{~mA} .4 \mathrm{mmp}$.


 HEATER TRAMS．6．8v． $1+\mathrm{A}, 10 / 6 ; 6.3 \mathrm{v} 4 \mathrm{amp}$ ． Ditto tappad sec． 1.4 V．， $2,3,4,5,6.8$ v． $1 \frac{1}{2} \mathrm{gmp}$ GENERAL PURPOSE LOW VOLTAGE．Outputs 8，4，5 8，8， $8,10,12,15,18,24$ and 80 ．at 2 amp ． AUTO TRANSFORMERS $0-115-220$ ．
 lor 6 or 12v．1t amp．，24／－； 4 amp．， 88 FULL WAVE BRIDGE GFARGER REOTLPIERS 6 or 12 \％．outpute，1t amp．8／－； 2 amp ．11／－； $4 \mathrm{amp} .17 /-$ ． OOAXIAL PLUG 1／8，PANEL SOOKETS 1／8．LINE 8／6． BALANCED TWIM FEEDERS 1／－Yd． 80 ohm or 300 ohma． JACE SOCKET Std．open－circuit 2／B，closed eifcait 4／6； Chrome Lead Socket 7／6．Fhono Plugi $1 /-$ ．Phono Socket $1 /-$ ； JACX PLUGS Sta．Ohtome 8／－； 8.5 mm Chrome 2／6．DIN SOCKETS Chastis 3－yin 1／6；5－pin 2／－．DLS \＆Ockers Lead



## E．MI． $13 \frac{1}{2} \times 8 \mathrm{in}$ ． LOUDSPEAKERS With flared tweater cone and corsmi magnet． 10 watts． Bata rea． $45-60 \mathrm{cpa}$ ． Speech coil， 8 or 16 ohm ． Fith with twin tweeteri．Complote ohms． 10 watt． <br> Hecommended Teak Size $16 \times 10 \times$ Din．

## MINI－MODULE LOUDSPEAKER KIT

## 10 watt 65／－carriage 5 －

Triple speaker syatem combining on ready cut baflle． $\frac{1}{2}$ in．chiphoard $15 \mathrm{in} . \times 8 \frac{1}{\mathrm{in}}$ ．Separate Bass，Middio and rreble Loudapeakers and cronsovar condenser．The heavy duty 5 in．Basll Wooter unit has a low reanonance
cone．The mid－Range nnil is apacially designed to add drive to the middle register and the tweeter recreates the top ond of the musical spectrum．Total response 20－15，000 cpu．Full instructions for 3 or 8 ohm． TEAK FENEERED BOOKSHELY ERCLOSURE． $16 \times 10 \times 9 \mathrm{in}$ ．Modern Scandinavian $\boldsymbol{\$ 5}$ Post 5 －
fluted front design tor Zini－module．

ALL MODELS＂BAKER SPEAKERS＂I STOCE


30－14，500 c．p．s．，18in． donble cone，woofer and tweeter cone tosether with a BAKER ceramic magnet assembly having a flux density of 14,000 grusg and a total fiuz of 145，000 Maxwella．Basa resonance 45 c．p．s．Rated 20 watts．Voice coill 3 os 8 or 15 ohms． Module kit， $80-17,000$ e．p． ． with tweeter，eronsover， baffe and
instractions．
al｜ 10.0 instractions． BAKER＂GROUP SOUND＂SPEAKERS－POST FREG ＇Group 25＇＇Group 35＇＇Group 50＇

TEAK EI－FI SPEAKER CABINETS．Fluted wood front． For $18 \times 8$ or 12 in ．round Loudspeaker

Horn Tweeter $2-16 \mathrm{kc} / \mathrm{s}, 10 \mathrm{~W} 8$ ohm $29 / 6$
De Luxe Horn Tweeters $2-18 \mathrm{Kc} / \mathrm{s}$ ， $15 \mathrm{~W}, 16$ ohm 59／6．
MOVING COIE cone tweeter 8 ohm 19／－

 $8 \mathrm{ohm}, 6 \times 4 \mathrm{in} ., 8 \mathrm{ohm}, 24 \mathrm{in}, 8 \mathrm{in}$ ， $5 \mathrm{in} .5 \times 8 \mathrm{in} .7 \times 4 \mathrm{in}$ LOUDSPEAKERS P．M． 3 OHMS．6tin．28／6； $8 \times$ Sin， $81 /-$ $8 \times 2 \operatorname{in} .21 /-8 \operatorname{in} .35 /-; 10 \times 6 \mathrm{in} .30 /-$
Sin．Weofer 8 watt max． $20-10,000 \mathrm{cps}$.8 or $150 \mathrm{hm} .89 / 6$ ELAC 8 in．De Luxe Ceramic 3 ohm or 15 ohm $50 /-$ 8in LOUDSPEAKER．TWIN CONE 15 ohm $35 /$ ． RICH／ALLAN 8 or 10 or 12in Twin cone 3 or 16 ohm $39 / 6$ ． SPEAKER COVERING MATERIALS．SA mples Latre S．A．E


ALL．EAGLE PRODUCTS

BARGAM AM TUPER．Medium Wave．$\quad 79 / 6$
Trandistor superhet．Ferrite aerial． 8 volt．
BARGAIK DE LUXE TAPE SPLICGR．Cuts，
trimg，joins ior editing and repairs．With a bladea $22 / 6$ rana BARGAN 4 CRANAEL TRANSISTOR MIXER Add musical highlighty and sound effects to recordings Will mir microphone，records，tape and tnner
with soparate eontrols into single ontput． 9 volt． $59 / 6$
BARGAIM FM TUNER 88－108 Me／s Six Transistor． 9 volt Printed Circall．Calibrated alide dial tuning． $\mathbf{E 9 . 1 0 . 0}$
Wainut Cabinet． $8 i z a 7 \times \frac{1}{5} \times$ in． ditto lese cabinet 47.10 .0 FM STEREO MULTIPLEX ADAPTOR．For above of
general une．Beady made with 4 tranistorn． $99 / 6$ genersi uis．Ready made with 4 tranistorn，
8 diodes．
BARGAIM 3 WATT AMPLIFEIR． 4 Tranaintor
69／6
$\frac{\text { Push－Pull Ready built，with volume control．日v．}}{\text { tRADIO EOOKS }+ \text {（Poutage 9d．）}}$
Practical Radio Inside Out
Practical Stereo Handbook
Supersensitive Tranaistor Pocket Rsadio
Radio Valve Guide，Booki $1,2, \mathrm{z}$ or 4 es． $5 /-\mathrm{Flo} .6 \mathrm{es}$ ．
T．V．Fanlt Finding 405／625 lines
Tranistor Communication Sets
Wircless World Radio Valve Data
Trantistor Cirenits for Radio Controlled Model：
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22 Circuits for Micro Alloy transibtors
Practical Car Radio installation
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MAINS ELECTRIC MOTORS

（120v．ar 240\％．AC）．Sire $2 t \times 2 t \times 1$ in． civis 4 pole 50 mA ．Spindle i $\times 8 / 20$
 （ Lor sol－；o 102 PO／ CUSTOMERS FREE CAR PARK，CALLERS WELCOME，
337 YHITEHORSE ROAD，CROYDOM 337 MHITEHORSE ROAD，CROYDON Opan 9－5 p．m．（Wadnasdays 9－i p．mn，Saturdays 9－s pim．）
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Supplement and a Bookmark giving electronic abbreviations.
Post the Coupon today, with 12/6

The price of 1216 applies only to catalogues purchased by customers residing in the U.K.


The value of R24 can be increased to give an even longer discharge time for C16. The combination of R24 and silicon diode D2 (low leakage) can be replaced by a germanium diode (higher leakage) but this prevents any experimentation with R24.

## CONSTRUCTION

Most of the components are carried on a printed circuit board shown in Fig. 11. The board and the controls are mounted in a two piece aluminium box (see Fig. 12) for effective screening. The author used a separate component for the ON/OFF switch S3; this results in a rather large number of knobs on the front of the unit and it might be preferable to have a third 'OFF' position on S1. In this case S1 would need to be a 4-pole 3-way type.

Arrangements have been made for readers to obtain the printed board ready made and drilled
from the suppliers listed in the parts list. If making the board oneself, the pattern of conductors shown in Fig. 11 should be traced and the resist painted on the copper in a mirror image of the pattern.

The transistor types used, viz: 2N2926 (popular plastic silicon planar) and 2N3819 (general purpose f.e.t.) are available cheaply from advertisers in the magazine. Ensure that the electrolytic capacitors and the semiconductors are wired with correct polarity as indicated in Fig. 11. All components should be soldered quickly and with short leads. The germanium diode D1 is the only component where particular care should be taken to avoid heat damage. The wiring between the board and the controls should be short and the indicated leads screened as shown. All earth connections are made to a common point, the body of VR1.

The inclusion of Cl 1 should be sufficient to en-


Fig. 11 : The component layout. Using the recommended P.C. board makes for easy construction and a neat final layout.
 sure stability if the layout is followed. If instability arises due to poor layout or the use of higher gain transistors. a 100 pF capacitor C6 can be added between earth and $\operatorname{Tr} 5$ base (connect at S1) or in the position shown on the printed circuit (normally unoccupied). The compressor/expander should remain stable even with an overload input.

Two links are shown on the printed circuit. When the link between C 2 negative and R3/R4 is made, the gain of the unit is reduced slightly but the range of compression or expansion is increased. The link between Tr 5 collector and the positive line may be opened to measure Tr5 collector current. This should be around 3.5 mA in both compress and expand positions of S 1 .

Under some conditions, it may be possible to drive the circuit into low frequency oscillation when VR3 is fully on (clockwise). Some improvement in this, and in the circuit's recovery time from an extreme overload, can be found by wiring a lowwattage 2.7 V zener diode across C16 (positive to positive).

## USE

For compression, the unit is set up as follows. Start with S1 at COMPRESS, VR1 (LEVEL) anticlockwise and VR3 anticlockwise. Feed the


Fig. 12: The cutting and drilling details of the two piece aluminium cabinet.
signal input to JK1. The unit can be driven by a dynamic microphone, electric guitar, magnetic pickup, tuner, etc. A crystal microphone or pickup can also be used but a resistor of $47 \mathrm{k} \Omega$ to $220 \mathrm{k} \Omega$ should be put in series with JK1 to reduce distortion. The output at JK2 may be fed to any valve or transistor amplifier. Advance VR1 (LEVEL) until the lowest level sound passages are reproduced at the desired volume. Then advance VR3 until the louder passages are sufficiently compressed.

Expansion is a little harder to set up as VR1, VR2 and VR3 have interdependent effects. With S1 at EXPAND and VR3 anticlockwise, set VR2 for the desired range of expansion, from slight (anticlockwise) to extreme or 'squelch-like' (clockwise). Advance VR1 until the lowest level sound passages are just audible. Then advance VR3 until the louder passages are sufficiently expanded.


If a voltmeter is available, the voltage across C16 can be monitored. Note that the internal resistance of a moving coil voltmeter will affect the attack/decay times. A change in signal level is expanded or compressed when it causes a voltage change in the range 1.8 V to $2 \cdot 5 \mathrm{~V}$ d.c.

## APPLICATIONS

Volume compression can be applied usefully to almost any audio signal where full, reproduction of the dynamic range is not essential. Compression reduces the demands made on audio equipment and on the listener. In the extremes, 'loud' sounds are prevented from causing overload distortion while 'quiet' sounds are not lost. The use of compression for tape recorders has already been mentioned and is a great help when recording 'wild' sounds out of doors. Some further applications are described below.

Compression is useful in a public address system as it compensates for poor microphone technique. Intelligibility is improved and this may enable the amplifier to be used at lower gain with consequently less risk of feedback howls.

Compression can be used in radio communication to increase 'talk power' (intelligibility) over a noisy channel. It is preferable to speech clipping as it does not introduce harmonic distortion. A combination of compression and clipping would give excellent intelligibility over a poor quality speech link.

Compression can be useful to the hard of hearing who may need to listen to radio or television at an uncomfortably high volume (to others) in order to hear everything. If the dynamic range of the material is compressed, the annoyance caused to others by peak sound levels is reduced.

Compression is used in commercial record making where the dynamic range of the material to be recorded exceeds the range that can be cut on the record. Pop music often employs a high degree of compression; in this way the 'backing' sound can be recorded at full level without drowning out the singer. Even the most idolised groups usually provide live performances which seem 'weak' compared with their recorded offerings; compression can provide

## DISCOSOUND

## DJ DISCO-AMP



The DI Disco-amp has been designed specifically for use with discotheques and has many exclusive features not normally found on P.A. amplifiers. The unit will be of use to the professional D.J. as well as in clubs and mobile discotheques.

The pre-amp section features independent inputs and volume controls for two mics with separate bass. treble and master volume, plus two independent inputs and volume controls for turntables, again with separate bass, treble and master volume controls.

A complete Pre-fade listen (P.F.L.) cueing monitor section is also featured with separate input for headphones (either stereo or mono) with an independent volume control for headphone monitoring, and a P.F.L. switch, so that either turntable can be monitored for accurate cueing up of records. A mic over-ride switch is also added which cuts the music volume by half so that mic announcements may be made over the music without altering the volume controls.

The power amplifier section has an output of 70 watts R.M.S. into 8 ohms and has elaborate protection against thermal, short or open circuit. The unit is designed for panel mounting.

## SPECIFICATION

Output power
Frequency response
Harmonic distortion
Signal/noise ratio
Speaker impedance Headphone impedance Bass control
Treble control Inputs: turntable

70 watts R.M.S. $\pm 1 \mathrm{db}$ at 8 ohms. $30-20,000 \mathrm{~Hz} \pm 3 \mathrm{db}$. Less than $1 \%$ at full output. Better than - 65db.
8-16 ohms.
$8-16$ ohms.
Variable 20 db at 100 Hz .
Variable 20 db at 10 kHz .
Mic $1 \& 25 \mathrm{mV}$ at 50 K ohms. 1 \& 2100 mV at 1 meg ohm.

50 ohm or 600 ohm mic inputs may be ordered at extra cost. Size: Front Panel $16 \frac{1}{2}{ }^{\prime \prime} \times 7^{\prime \prime}$. Cut out $15 \frac{1}{2}$ " x $6^{\prime \prime}$. Fuses: A.C. 1.5 amp (B.S.) mounted on back panel.

PRICE $£ 85.0 .0$ inc. $P \& P$.

## DISCOSOUND PRE-4

This is a four channel fully mixable pre-amp, with separate treble, bass and master is completely self powered. All four inputs are by standard jack socket on the front panel with the addition of inputs 3 and 4 being duplicated on the back peing duplicated on the back panel, with two paraleled outputs also featured for versatiity in use. Frequency . Signal/Noise Ratio: - 65 db . Size: front panel $12 \frac{1}{2} \times 5 \frac{1}{2}$ cut out required $11 \frac{1}{2} \times 4 \frac{1}{2}$. Completely built and tested.

## PRICE £18.0.0 inc. P \& P.

## DJ 30L PSYCHEDELIC LIGHT CONTROL UNIT

3 channel light control unit that handles up to 1,000 watts per channel. Separate bass, middle and treble controls for full frequency separation.
Completely built and tested


PRICE £37.10.0 inc. P \& P.

## DJ 70 S <br> INTEGRATED MIXERAMPLIFIER



One of the finest units available on the market today, regardless of price. The front end of the unit consists of a four channel mixer with separate inputs and volume controls, plus a separate bass treble and master volume control. One of the main features of this remarkable amplifier is its elaborate protection against short and open circuit and we can guarantee that it is virtually indestructable. Allied to this is its very high power outDut ( 70 watts R.M.S.) a frequency response $(30-20,000 \mathrm{~Hz} \pm 3 \mathrm{db})$ that is superb, and dis tortion that is well below $1 \%$ even at full output. The unit is suitable for use with discotheques. groups. P.A.. clubs etc., or anywhere that high quality high output is required. Size: $15 \frac{1}{2}$ in $\times 5 \mathrm{in} \times 6 \mathrm{in}$.
PRICE 555.0 .0 inc. $\mathbf{P} \& \mathbf{P}$.
Also available DJ105S 30 watt P.A. Amplifier. Similar specification to above.

## PRICE £35.0.0 inc. P \& P.

## DISCOSOUND 70 MAIN AMPLIFIER

A 70 watts RMS ( 8 Ohms ) High Fidelity power Ampliffer which utilises all silicon transistors of modular construction and features full automatic overload protection against short or open circuits. Frequency response: $20-20,000 \mathrm{~Hz} \pm 2 \mathrm{db}$. The High output is Frequency response: $20-20,000 \mathrm{~Hz} \pm 2 \mathrm{db}$. The High output is ideally suited for discotheques, groups, clubs, eic., or anywhere where reliability and quality are required. This unit is the companion model for use with our control pre-amp Discosound PRE-4, or can be used with
Completely built, and tested on steel Chassis.
PRICE £30.0.0 inc. P \& P.

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# ELECTROVILUE 

## EVERYTHING BRAND NEW \& TO SPECIFICATION • LARGE STOCKS


some improvement here. The usual technique seems to be to overload amplifiers and speakers to a ludicrous extent, presumably to achieve volume compression by extreme clipping! A local pop group has been experimenting with a prototype of the compressor/expander and are enthusiastic about it. The effect of extreme compression on the sound of an electric guitar is to sustain the notes played; the

## components list

| Resistors: |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | 270k $\Omega$ | R13 | $2 \cdot 2 \mathrm{k} \Omega$ |
| R2 | $27 \mathrm{k} \Omega$ | R14 | 3.3k $\Omega$ |
| R3 | 15k $\Omega$ | R15 | $1.8 \mathrm{k} \Omega$ |
| R4 | 12k $\Omega$ | R16 | 270k $\Omega$ |
| R5 | $2 \cdot 7 \mathrm{k} \Omega$ | R17 | 27k $\Omega$ |
| R6 | 27k $\Omega$ | R18 | 27k $\Omega$ |
| R7 | $4 \cdot 7 \mathrm{k} \Omega$ | R19 | $2 \cdot 7 \mathrm{k} \Omega$ |
| R8 | 27k $\Omega$ | R20 | 82k $\Omega$ |
| R9 | $2.2 \mathrm{k} \Omega$ | R21 | 82k $\Omega$ |
| R10 | 27k $\Omega$ | R22 | $8.2 \mathrm{k} \Omega$ |
| R11 | 4.7k $\Omega$ | R23 | 270k $\Omega$ |
| R12 | 27k $\Omega$ | R24 | $3 \cdot 3 \mathrm{M} \Omega$ |
| All resistors $\frac{3}{4}$ watt, $10 \%$ tolerance. |  |  |  |
| VR1 $50 \mathrm{k} \Omega$ 1og. |  |  |  |
| VR2 | $10 \mathrm{k} \Omega$ 1og. |  |  |
| VR3 $50 \mathrm{k} \Omega$ 10g. |  |  |  |
| Capacitors: |  |  |  |
| C1 | $50 \mu \mathrm{~F} 6 \mathrm{~V}$ | C9 | $100 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C2 | $50 \mu \mathrm{~F} 10 \mathrm{~V}$ | C10 | $100 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C3 | $100 \mu \mathrm{~F} 6 \mathrm{~V}$ | C11 | $100 \mu \mathrm{~F}$ ceramic |
| C4 | $50 \mu \mathrm{~F} 10 \mathrm{~V}$ | C12 | $100 \mu \mathrm{~F} 10 \mathrm{~V}$ |
| C5 | $100 \mu \mathrm{~F} 6 \mathrm{~V}$ | C13 | $50 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C6 | 100pF ceramic | C14 | $50 \mu \mathrm{~F} 10 \mathrm{~V}$ |
|  | -see text | C15 | $1 \mu \mathrm{~F}$ paper |
| C7 | $4 \mu \mathrm{~F} 15 \mathrm{~V}$ | C16 | $2 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C8 | $50 \mu \mathrm{~F} 10 \mathrm{~V}$ | C17 | $250 \mu \mathrm{~F} 20 \mathrm{~V}$ |
| Switches: |  |  |  |
| S1 | 3-pole 2-way ro |  |  |
| S2 | 2-pole 3-way ro |  |  |
| S3 | Single pole on | (or se | text) |
| Semiconductors: |  |  |  |
| Tr1 2N2926G (green) |  |  |  |
| Tr2 Texas 2N3819 (f.e.t.) |  |  |  |
| Tr3 2N2926Y (yellow) |  |  |  |
| Tr4 2N2926Y (yellow) |  |  |  |
| Tr5 2N2926Y (yellow) |  |  |  |
| Tr6 2N2926Y (yellow) |  |  |  |
| D1 OA70, OA91 or any germanium diode. |  |  |  |
| D2 | 1 N914 or any si | dio |  |

## Miscellaneous

JK1, JK2, jack sockets; B1, B2, PP3 9V batteries; printed circuit board*; knobs; battery clips etc.

* The printed wiring board is available from: Walsall Timing Developments Ltd., Hall Lane, Walsall Wood, Staffis for $10 s$. post paid. Delivery $\mathbf{7 - 1 0}$ days.
result is more like an organ than a guitar. Compression also removes the need to change the amplifier gain between playing accompaniment and single note solos.

Compression has a side effect of worsening the apparent signal to noise ratio of an audio system. This happens because hum and noise are amplified at high gain during silent passages when they are most noticeable.

Volume expansion is not quite as useful as compression as most audio material already has a wide
dynamic range. It can be used to counteract previous volume compression when replaying records or tapes. Expansion has a remarkable side effect of improving the apparent signal to noise ratio of an audio system. This is because the gain is only high when the signall level is high, and hum and noise are not very noticeable at this time. This effect reduces the fatigue of listening to short wave signals against a noisy background, although any fading will be exaggerated.

If VR2 is set for the maximum degree of expansion, the circuit behaves similarly to a squelch. The usefulness of squelch in muting radio receiver noise when no signal is present has already been described in Practical Wireless October 1969.

## GENETRACER-continued from page 270

It is recommended that the instrument be tested on a radio receiver in known working order, first injecting a signal from the "generator" at the control grid (valve receivers) or base (transistor receivers) at each stage in turn, listening to the resultant response in the receiver's speaker.

## $\star$ components list

| Resistors: ${ }^{\text {c }}$ |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | $1.5 \mathrm{k} \Omega$ | R7 | $33 \mathrm{k} \Omega$ |
| R2 | $270 \mathrm{k} \Omega$ | R8 | 10 k , |
| R3 | $150 \mathrm{k} \Omega$ | R9 | $2 \cdot 7 \mathrm{k} \Omega$ |
| R4 | $1.5 \mathrm{k} \Omega$ | R10 | $470 \Omega$ |
| R5 | 47k $\Omega$ | R11 | $12 \mathrm{k} \Omega$ |
| R6 | $4 \cdot 7 \mathrm{k} \Omega$ | R12 | $2 \cdot 2 \mathrm{k} \Omega$ |
|  |  | R13 | $39 \Omega$ |
| All $\frac{1}{4}$ W 10\% |  |  |  |
| VR1/SW1 1M VR2/SW2 100k $\Omega$ pot. with switch |  |  |  |
| Capacitors: |  |  |  |
| C1 | $0 \cdot 002 \mu \mathrm{~F} 500 \mathrm{VW}$ mica |  |  |
| C2 | $0.01 \mu \mathrm{~F} 150 \mathrm{VW}$ ceramic |  |  |
| C3 | $0.005 \mu \mathrm{~F} 150 \mathrm{VW}$ ceramic |  |  |
| C4 | $10 \mu \mathrm{~F} 15 \mathrm{VW}$ electrolytic |  |  |
| C5 | $0 \cdot 001 \mu \mathrm{~F} 500 \mathrm{VW}$ mica |  |  |
| C6 | $2 \mu \mathrm{~F} 15 \mathrm{VW}$ electrolytic |  |  |
| C7 | $30 \mu \mathrm{~F} 15 \mathrm{VW}$ electrolytic |  |  |
| C8 | $8 \mu \mathrm{~F} 15 \mathrm{VW}$ electrolytic |  |  |
| C9 | $50 \mu \mathrm{~F} 15 \mathrm{VW}$ electrolytic |  |  |
| C10 | $100 \mu \mathrm{~F} 25 \mathrm{VW}$ electrolytic |  |  |

## Semi-conductors:

| Tr1, 2, 3 | OC71 |
| :--- | :--- |
| Tr4 | OC72 |
| D1 | OA81 |

## Miscellaneous:

Paxolin panels: 1 off $10 \times \sin \times \frac{7}{16}$ in. 2 off $6 \times 2 \frac{3}{4}$ in. $x$ $\frac{1}{16}$ in. Reel of "Cir-Kit" adhesive connector strip. T1-Transistor output transformer OC72 to $3 \Omega$ speaker. Speaker, $3 \Omega$ impedance. PP3 battery and connector. 2 control knobs. 2 Coaxial sockets, chassis mounting. 2 Coaxial plugs. 2 lengths TV coaxial cable about 12 to 18 in long. 4 crocodile clips.

Now, switch off the "generator", switch on the "tracer", and listen to the signal at the input and output of each stage in the receiver, on the tracer's own speaker. Finally, try the effect of injecting a signal from the "generator" at the input side of a receiver stage, simultaneously listening to the output in the "tracer's" speaker.

## FEEDBACK

THE operation of amplifying circuits with feedback can be analysed quite simply using a few basic principles. Figure 5.1 shows an amplifier of gain ' $A$ ' with a feedback network which has a gain, or attentuation, of ' $B$ '.
Because most amplifiers have negative feedback we will assume that the voltage fed back will be subtracted from the input voltage, and by algebraic manipulation we arrive at the formula.

$$
\begin{equation*}
\mathrm{V}=\mathrm{V}_{\mathrm{IN}}-\mathbf{B} \times \mathrm{V}_{\mathrm{O}} \tag{1}
\end{equation*}
$$

This means that the voltage actually fed into the amplifier is less than the voltage supplied.

We can say that because the amplifier has a gain of A,

$$
\begin{equation*}
\mathrm{V}_{\mathrm{O}}=\mathrm{A} \times \mathrm{V} \tag{2}
\end{equation*}
$$



Fig, 5.1. Basic circuit of a feedback network
As we require a relationship between the output, $\mathrm{V}_{\mathrm{O}}$, and input, $\mathrm{V}_{\text {IN }}$, we must manipulate the terms in equations (1) and (2) to contain only constants and variables $V_{I N}$ and $V_{0}$.

From equation ( 2 ). V. $=\frac{V_{0}}{A}$
and substituting equation (3) into equation (1) gives:

$$
\frac{V_{O}}{A}=V_{I N}-B \times V_{O}
$$

rewriting

$$
\begin{aligned}
& V_{O}\left(\frac{1}{A}+B\right)=V_{I N} \\
& \therefore V_{O}\left(\frac{1+A B}{A}\right)=V_{I N} \\
& \therefore V_{O} \\
& V_{I N} \frac{A}{1+A B}=\text { gain with negative feedback }
\end{aligned}
$$

From this formula it would appear that the application of negative feedback would reduce gain.

$$
\begin{aligned}
& \text { e.g. if } A=100, B=\frac{1}{100} \\
& \qquad \frac{V_{C}}{V_{I N}}=\frac{100}{1+1}=50
\end{aligned}
$$

This is a disadvantage. However, a very important advantage of applying negative feedback can be demonstrated quite easily.

Bandwidth was defined as the frequency range between the half power points. Suppose at the 3 dB point of an amplifier the power gain was 50

$$
\begin{aligned}
\text { or } & =10 \log _{10} 100-10 \log _{10} 2 \\
& =20-3 \mathrm{~dB}
\end{aligned}
$$

Now at the same frequency with negative feedback applied, the amplifier gain would be

$$
\text { Gain }=10 \log _{10} \frac{A / 2}{1+A / 2 B}
$$

If $\mathbf{B}=\frac{1}{100}$ then gain with feedback becomes:-

$$
\begin{aligned}
& 10 \log _{10} 50-10 \log _{10}\left(1+\frac{1}{2}\right) \\
& =16.99-1.76 \mathrm{~dB}
\end{aligned}
$$

It can be seen by comparing the amplifier gains at the same frequency, the reduction of gain with feedback applied is only 1.76 dB , indicating that the -3 dB point occurs at a higher frequency at the upper half power point and a lower frequency at the lower half power point. Therefore, although the mid-band gain has been reduced, bandwidth has been increased.

It would seem logical that by applying positive feedback gain would increase and bandwidth reduce. This is so, in fact if sufficient positive feedback is applied to an amplifier, gain would be so far increased and bandwidth reduced that the amplifier would become unstable and produce oscillations. This is not a particularly good way of producing oscillations' of predetermined sigrials-there are numerous' other more reliable methods.

## Oscillators

Oscillators which produce sinusoidal waveforms, can, in general, be simplified to an amplifer and feedback network as shown in Fig 5.2.

Usually the amplifier will produce an output voltage $180^{\circ}$ out of phase with an input voltage. For oscillations to be self sustaining the feedback network should produce the amplifier's input voltage from its output voltage, therefore the feedback network should also produce a $180^{\circ}$ phase shift to compensate for amplifier phase shift. Another governing factor is that any losses which are present in the feedback network must be compensated for by the amplifier gain.

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Fig. 5.2. Feedback network employed to produce an oscillator
Figure 5.3 shows the circuit diagram of a CR feedback network oscillator which can be analysed as follows.

R at the input of the amplifier should include the transistor input resistor and the biasing resistors in parallel. This circuit consists of a single stage amplifier providing a $180^{\circ}$ phase shift and a 3 -stage CR feedback network.


Fig. 5.3. Typical oscillator circuit utilising a CR feedback network
Neglecting the effects of the individual CR networks loading each other, each CR network will produce a $60^{\circ}$ phase change as indicated by the vector diagram in Fig 5.4.

$$
\begin{aligned}
\text { Tangent } 60^{\circ} & =\frac{\sqrt{3}}{1}=\frac{\mathbf{V}_{\mathbf{C}}}{\bar{V}_{\mathbf{R}}}=\frac{\mathbf{X}_{\mathrm{C}}}{\mathbf{R}} \\
\text { but } \mathrm{X}_{\mathrm{C}} & =\frac{1}{2 \pi \mathrm{fC}} \\
\therefore \sqrt{ } \mathbf{3} & =\frac{1}{2 \pi \mathrm{fCR}}
\end{aligned}
$$

therefore the frequency of oscillation,

$$
\mathrm{f}=\frac{1}{2 \sqrt{3} \pi \mathrm{CR}}
$$



For this circuit it can be shown that the amplifier must have a gain of slightly more than 29 to compensate for losses in the network.

The Wien bridge oscillator shown in Fig 5.5 is perhaps the most widely used for frequency generator circuits in test equipment as a wide range of frequencies can be generated by varying $C$ and $R$ values.


Fig. 5.5. Basic circuit of the Wien bridge oscillator
It can be shown by making the appropriate circuit assumptions that frequency of oscillation is given by:

$$
\mathrm{f}=\frac{1}{2 \pi \mathrm{CR}}
$$

## Relaxation Oscillators

These are circuits which again involve feedback in amplifiers, but here switching of current flow is obtained by CR network feedback rather than by producing sinusoidal oscillations. Fig 5.6 shows the basic circuit.


Fig. 5.6. Relaxation oscillator using two feedback networks C1R1 and C2R2

The time taken for switching is half the periodic time of the waveform. This time can be obtained from the equations discussed in the last article.

Periodic time $=2 \times 0.693 \times \mathrm{CR}=1.386 \mathrm{CR}$ or approximately $1 \cdot 4 \mathrm{CR}$

$$
\therefore \text { frequency }=\frac{1}{1 \cdot 4 C R}
$$

This type of circuit, although used in logic circuits in the main, is often used in electronic organs, the keyboard used to switch different values of $\mathbf{C}_{1}$ and $\mathbf{R}_{1}$ into the circuit thus providing the different notes. Filter circuits are sometimes used to filter out some of the higher harmonics to give a purer sound.
So far these articles have shown that mathematics applied to electronics can remove all the guesswork normally encountered in circuit designing and building. It is now up to the reader to put these principles into practice not only in the workshop but in understanding radio and electronics a little more clearly.

# T/AK 

E

## A series of simple transistor projects, each using less than twenty components and costing less than twenty shillings to build.

ONCE a piece of equipment has been built, it is often necessary to provide some form of signal input with which to test it. I am sure many of you use the trick of tapping the audio from either the loudspeaker or the volume control of a transistor radio. This is fine where an audio signal is required but will not help where r.f. is needed. For this type of equipment radio broadcasts can often be used but if this does not work you will not know if something is wrong or if the equipment is just not sensitive enough.
It is however very easy to build a signal injector which produces a basic audio signal which is so distorted that the harmonics reach way up into the r.f. spectrum.

Various types of oscillator will do this but the one described here will achieve all the others do and the cost will be under 10s.

## THE CIRCUIT

The transistor is connected in the common emitter mode with base bias being provided by R1. The collector load comprises a radio frequency choke which has two capacitors, themselves in series, connected across it. C 1 and C 2 are $0 \cdot 1 \mu \mathrm{~F}$ each so that the effective capacitance across the choke will be $0.05 \mu \mathrm{~F}$. The junction of these capacitors is connected to the base via a $1,000 \mathrm{pF}$ capacitor which starts and maintains the oscillation.

By coupling far too much positive feedback to the input, a grossly distorted waveform is achieved, this being necessary to produce the harmonics.

In operation for radio frequency usage, the choke itself will radiate the harmonics to be picked up on any tuned circuit and it is only necessary to place the injector near the equipment. For audio purposes C4 taps off the output and this can be coupled to the equipment under test via some form of probe.

A huge variety of transistors can be used for Tr1, we are using a 2 N 2926 here only for economy; the frequency response should be over 10 MHz otherwise the higher harmonics will not be produced. PNP transistors, if used, of course require that the battery polarities be reversed.

Component layout should prove to be easy, a small piece of Veroboard will take all the components and make the finished article neat.

Just a few lines on test equipment. Many beginners seem to ignore this feeling that, since it is rarely used, it is a waste of time and money. I am sure that many constructors who are frustrated by early failures drop the hobby for this reason. If they had

## No. 16 SIGNAL INJECTOR



Fig. 1 : The circuit diagram of the signal injector.

## * components list

| R1 | $470 \mathrm{k} \Omega \frac{1}{4}$ watt $10 \%$ |
| :--- | :--- |
| C1 | $0 \cdot 1 \mu \mathrm{~F}$ |
| C2 | $0 \cdot 1 \mu \mathrm{~F}$ |
| C3 | 1000 pF |
| C4 | 1000 pF |
| R.F.C. | $2 \cdot 5 \mathrm{mH}$ radio frequency choke |
| Tri | 2 N 2926 |

paid proper attention to it and realised that test equipment will often sort out troubles in seconds that would otherwise take hours they would still be with us. Good test equipment enables one to churn out projects quickly and of a high standard but even the simplest types, such as that described here, is very useful.

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## Zintage ładio Gotiety

In connection with our previous notes on the possible formation of a VRS we have had an offer from a reader to compile a list of those people who have a genuine interest in the collection and preservation of "vintage" radio equipment. All communications direct to: Mr. K. Lancaster, 40 Great Gardens Road, Hornchurch, Essex.

It is of interest at this point to raise the question as to just what constitutes "vinage" radio equipment. In our view the term should apply to equipment produced prior to 1930 by which time broadcasting had become firmly established in this country and the basic design of radio receivers more or less stabilised.

However, would readers care to express their own views on this matter?

## hadíograms

"According to the latest reports Captain Amundsen, at present en route to survey the Arctic region, will broadcast Eskimo music to the world.". . . 1922 . . . possibly more pleasing to the ear than some of today's pop!!
"One of the simplest ways of cutting down atmospherics is to lower the aerial.". . . 1932.
"Increasing the height of the aerial is often as effective as adding another valve.". . . 1932. . . . your move!
"America promises us a new method of waging war in her promised production of a giant airship capable of carrying large numbers of pilotless gliders laden with bombs. These gliders would be guided to the spot at which it was desired to drop bombs by means of a wireless ray." . . . 1922 . . . but what about anti-missile missiles??
"How Germany does it . . . in Germany the listening tax is paid monthly and its collection from setowners is made by the postman on his rounds. The annual cost is approximately 30 s . Radio pirates are discovered by the municipal chimney-sweeps who in the course of their daily duties visit all houses, flats and apartments. It is their duty to notify all wireless receivers to the local authorities." . . .!! . . . . 1932. $\therefore M$ of $P \& T$ to note.$:$ using postmen that is. not chimney sweeps!
. . . in addition to the Post Office Licence it is also
necessary to have a licence from Marconi's Wireless Telegraphy Co., for the use of their patents. The home constructor is not immune from this levy . . . if you construct a receiver for your own use and make use of any of the above company's patents you should write to them for a licence plate which will be supplied on payment of the royalty. If in doubt send them a wiring diagram of the receiver. The Post Office Licence is 10 s. per annum, the Home Constructors Marconi Licence is 12 s . 6 d . and Manufacturers Licence is 5 s . per valve!! . . . 1932 . . . we should be grateful that this at least has been dropped!!


In 1922 the first broadcasts, as we know them today, took place from Marconi House in the Strand in London. Initially the power used was only 100 watts but this was soon increased to 1.5 kW . The British Broadcasting Company came into being in December the same year and in a matter of months a network of eight 1.5 kW stations, similar to 2LO, were operational around the country.


A first glance at the transmitter hall of 2LO gives the impression of many mighty kilowatts but in fact it was only 1.5 kW . On the right are the early audio stages and modulator with the master oscillator in the centre background. The power supply with its transformers and valve rectifiers is on the left.

## 鼠eaders $\mathbb{C o m m e n t}$

. . . Recently I sorted out one of the old 2 V triodes and made a single valve reaction set. The coil was home-wound on a former made from a toilet roll. The results were fantastic. (J. Taylor, Lancashire.)
... I got the wireless "bug" in 1920 when I was given some odd pieces of World War 1 surplus equipment. (F. H. Osborn, G2CVO, London, E.4.)
...I constructed a John Scott Taggart design delivering 12 W of audio and had the police hammering on the door at 2 a.m. (B. Richardson, Nottingham.)
...I clearly remember several of your crystal receiver designs. (Raymond A. Hounslow, Carlton, Bedford.)
... I collect old wireless components and still have the Vol. 1, No. 1 issue of Practical Wireless. (Alan Barnes, Yorkshire.)
$\ldots$ The years which P.W. has survived are clear proof of quality. I have many fond memories of its earlier days. (Maurice Dean, Sheffield.)
... Wireless has been the No. 1 all-devouring interest for me since I was 11 in 1932. I collect books, magazines and components from the much earlier days of wireless. (Basil D. Van Der Syde, M.S.E.R.T., Dorset.)
.. I still have many magazines dating back to the early days and would not part with them for all the world. (B. Richardson, Nottingham.)

I built my first wireless receiver at the end of the First World War. (Norman Gilbertson, Southampton.)
... My first receiving licence was a Constructor's Licence issued in 1924. (E. C. Parker, Middlesex.)
...I have taken P.W. since the first issue, and would like to see some early designs of transmitters. (John R. Davidson, G3FG, Surrey.)

These are but just extracts from some of the many letters we have received on the subject of the early days of radio.

## $\mathbb{U r s t i n g}$ '3phones

Back in 1922, this was an inexpensive way to test your earphones: "The two leads from the earphones are connected to the two terminals of an ordinary electric bell. No battery whatever is put in the circuit. The clapper is pressed forward to the bell and then quickly released. It will vibrate several times before coming to rest. A similar vibration will take place and will be plainly heard in the phones. The explanation of the action is that there is a small amount of magnetism in the magnet of the bell when it is not connected to the battery which usually works it. When you cause the armature of the bell to vibrate the magnetism is disturbed and sets up currents in the coils of the magnet core. These currents work the diaphragms of your phones, and you hear a sound agreeing with the vibration of the armature of the bell."

## 

"Various means have been designed for the purpose of operating the 'change-over' switch automatically. de Forest used an electromagnet which was energised by a delicate contact inserted in the microphone mouthpiece.
"This contact was closed by the actual air pulses from the mouth and the electromagnet thereupon moved a pivoted switch so as to break the receiving circuit and couple the transmitter to the aerial." . . . VOX 1923!
"In response to a query from a reader concerning the operation of station 5 HY the owner of the station, Mr. Baynham Honri, writes to say that his station is licensed for 10 watts but that he actually uses from 4 to 6 watts only on 440 and 200 metres."
. . . January 1923. . . . Readers may be interested to know that Mr. Honri is still very much alive and is the author of the monthly feature "Underneath the Dipole" in our "sister" magazine Practical Television.


## MONOLITHIC INTEGRATED CIRCUIT HIGH FIDELITY AMPLIFIER AND PRE-AMP



## theworld's most advanced high fidelity amplifier

The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by a hundredth of an inch thick, has an output of 5 watts R.M.S. ( 10 watts peak). It contains 13 transistors (including two power types), 2 diodes, 1 Zener diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.
The $1 \mathrm{C}-10$ is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of such components as tone and volume controls and a battery or mains power supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs, servo amplifiers (it is d.c. coupled throughout) etc. The photographic masks required as part of the process of producing monolithic l.Cs are expensive but once made, the circuits can be produced with complete uniformity and at very low cost. This enables us to cover every IC-10 with the Sinclair guarantee of reliability.

## SPECIFICATIONS

Output<br>10 Watts peak, 5 Watts R.M.S. continuous. Frequency response 5 Hz to $100 \mathrm{KHz} \pm 1 \mathrm{~dB}$. Total harmonic distortion Less than $1 \%$ at full output. Load impedance<br>Power gain Supply voltage Size<br>Sensitivity<br>Input impedance<br>$110 \mathrm{~dB}(100,000,000,000$ times) total.<br>8 to 18 volts.<br>$1 \times 0.4 \times 0.2$ inches.<br>Adjustable externally up to<br>2.5 M ohms.

## - CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class $A B$ output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

## APPLICATIONS

Each $1 C-10$ is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transisters.

## SINCLAIR

IC. 10with
IC.10
manual

# Project 60 

## laboratory-standard high fidelity modules

Sinclair Project 60 comprises a range of modules which connect together simply to form a complete stereo amplifier with really excellent performance. So good, in fact, that only 2 or 3 amplifiers in the wofld can compare in overall performance. Now with the addition of three new modules to the range, the constructor has choice of assemblies with either 20 or 40 watts output per channel, with or without filter facilities.

The modules are: 1. The $Z-30$ and $Z-50$ high gain power amplifiers, each of which is an immensely flexible unit in its own right. 2. The Stereo 60 pre-amplifier and control unit. 3. The Active Filter unit with both high and low audio frequency cut-offs. 4. The PZ-5 and PZ-6 power supplies. A complete system could comprise, for example, two $\mathrm{Z}-30$ 's, one Stereo-60, and a PZ-5. The PZ-6 is stabilised and should be used where the highest possible continuous sine wave rating is required. An A.F.U. may be added as required. In a normal domestic application, there will be no significant difference between using a PZ-5 or PZ-6 unless loudspeakers of very low efficiency are being used, in which case the PZ-6 will be required. For assemblies using two Z-50's there is the
new PZ-8 stabilised supply unit to ensure maximum performance from these more powerful amplifiers.
All you need to assemble your Project 60 system is a screwdriver and soldering iron. No technical skill or knowledge whatsoever is required and, in the unlikely event of you hitting a problem, our customer service and advice department will put the matter right promptly and willingly. Project 60 modules have been carefully designed to fit into virtually all modern plinth or cabinets and only holes need be drilled into the wood of the plinth to mount the control unit and the A.F.U. Any slight slip here will be covered by the aluminium front panels of these two units.
The Project 60 manual gives all the building and operating instructions you can possibly want, clearly and concisely. Perhaps the greatest beauty of the system is that it is not only flexible now but will remain so in the future as the latest additions to the range show. A stereo F.M. tuner is next to come. These and all other modules we introduce will be compatible with those already available and may be added to your system at any time. And because Sinclair are the largest producers of constructor modules in Europe, Project 60 prices are remarkably low.


# Z. 30 <br> 20 WATT R.M.S. POWER AMPLIFIER (40 WATTS PEAK) 

The $Z .30$ together with the higher powered $Z .50$ are both of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low $0.02 \%$ at full output and all lower outputs. Whether you use the $\mathbf{Z . 3 0}$ or $\mathbf{Z . 5 0}$ power amplifiers in your Project 60 system will depend on personal preference, but they are both the same physical size and may be used with other units in the Project 60 range equally well. The Z.30 Is unique in that it may be used with any power source between 8 and 35 volts without need for adjustment and may thus be driven from a car battery for example. For operating from mains, for the Z. 30 use PZ. 5 power supply unit for most domestic requirements, or PZ. 6 if you have very low efficiency loudspeakers. For Z.50, use the PZ.5, PZ. 6 or the PZ. 8 described below.

## SPECIFICATIONS

Power Outputs
The Z. 50 is completely interchangeable with the $\mathbf{Z . 3 0}$ and can be used in all Z.30 applications
Z. 3015 watts R.M.S. into 8 ohms, using 35 V : 20 watts R.M.S. into 3 ohms using 30 volts.
Z. 5040 watts R.M.S. into 3 ohms: 30 watts R.M.S. into 8 ohms, both continuous, using 50 V .
Frequency response 30 to $300,000 \mathrm{~Hz} \pm 1 \mathrm{~dB}$
Distortion $0.02 \%$ into 8 ohms
Signal to noise ratio better than 70 dB unweighted
Input sensitivity 250 mV into 100 Kohms
For speakers from 3 to 15 ohms impedance
Size $3 \frac{1}{2}{ }^{\prime \prime} \times 2 \frac{1^{\prime \prime}}{} \times \frac{\frac{1}{2}^{\prime \prime}}{}$

## APPLICATIONS

Hi-fl amplifier; car radio amplifier; record player amplifier fed directly from plck-up; intercem; electronic music and instruments; P.A.; laboratory work etc. Full details for these and many other applications are given in the manual supplied with the Z.30.

of Sinclair Z.30 and Z. 50
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2.30
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with circuits and instructions manual

## STEREO 60 Pre-amplifier and tone control unit

The Stereo 60 is a stereo preamplifier and control unit designed for the Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout and great attention has been paid to achieving a really high signal-tonoise ratio and excellent tracking between the two channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs. The tone controls are also very carefully designed and tested.

## ACTIVE FILTER UNIT

High Pass and Low Pass
For use between Stereo 60 unit and to Z.30s or Z.50s, the Active Filter Unit matches the Stereo 60 in styling and is as easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible by reason of the careful design and generous negative feed back employed.
Supply voltage- 15 to 35 V . Current- 3 mA
H.F cut-off ( -3 dB ) variable from 28 kHz to 5 kHz .
L.F cut-off ( -3 dB ) variable from 25 Hz to 100 Hz .

Filter slope, both sections 12 dB per octave
Distortion at 1 kHz ( 35 V supply) $0.02 \%$ at rated output

## SINCLAIR POWER SUPPLY UNITS



PZ-5 30 volts unstabilised £4.19.6
PZ-6 35 volts stabilised $£ 7.19 .6$
PZ-8 45 volts stabilised
(less mains transformer) £5.19.6
PZ-8 Mains transformer
£5.19.6

- Input senslitivities-Radio-up to 3 mV Mag. p.u. 3 mV : correct to R.I.A.A. curve $\pm 1 \mathrm{~dB}: 20$ to $25,000 \mathrm{~Hz}$. Ceramic p.u, -up to 3 mV ; Aux.-up to 3 mV ,
Output- 250 mV
Signal-to-noise ratio-better than 70 dB .


Chan nei matching-within IdB Tone controls-TREBLE + 15 to Tone controls-TREBLE +15 to -15 dB at 100 Hz .

- Power consumption 5 mA .

Front panel-brushed aluminium with black knobs and controls. Size $8 \frac{4}{4} \times 1 \frac{1}{2} \times 4$ ins.
Bult, tested
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£5.19.6 60 ASSEMBLY

The illustration here shows quite clearly how easily Project 60 can be contained in one of today's slim, modern piinths. Very little space is required to house these Sinclair units, and within the space of the motor plinth, you can install a stereo amplifier of the very highest quality. If, for example you have already put together an assembly as ilius= trated here, adding the Active Filter Unit would be very easy.

## GUARANTEE

If at any time within 3 months of purchasing Project 60 modules from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for services thereafter. No charge for postage by surface mail. Air-mai charged at cost.


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## SINCLAIR 0.16 <br> new elegance in an outstanding loudspeaker

All the superb features which went to make the Sinclair Q. 14 have been incoporated in the new Q. 16 which gives an exciting new opportunity for you to match your Sinclair equipment with modern decor. Employing the same well proven acoustic system in which materials, processing and styling are used in such a radical and successful departure from conventional design. This speaker presents an entirely new appearance with its attractive teak surround and all-over special cellular foam front chosen as much for its appearance as for its ability to pass all audio frequencies without loss. The Q. 16 is compact and slim. Its new styling makes it eminently suitable for shelf mounting, but it is no less versatile than its famous predecessor. Listen to a pair of Q.16s in stereo and marvel at the standards of quality and clarity they give. At the price this Sinclair speaker represents outstanding value as you will discover the moment you see and hear it.


The 0.16 will handle loading up to 14 watts R.M.S. and presents an 8 ohm impedance to the amplifier output. Frequency response extends from 60 to $16,000 \mathrm{~Hz}$ with exceptional smoothness. A specially designed driver system is used in a sealed and contoured pressure chamber to ensure good transient response at all frequencies. Size: $9 \frac{3}{4}$ " square $\times 4 \frac{3}{4}$ " deep from front to back.

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Should you not be completely satisfied with your purchase when you receive it from us, return the goods without delay and your money will be refunded in full, including cost of return postage, at once and without question. Full service facilities are available to all Sinclair customers.


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| 2N930 | 68 | 析 | 4 | TFF19 | $4 / 6$ |  |  |  |  |
| ${ }^{2 N T}$ | 8；／6 | ${ }_{\text {achri }}$ |  |  |  | D242 190p．t．v． 104 A 6 6 － |  |  |  |
| \％NTH2 | ${ }_{9}^{8,9}$ | －${ }^{\text {ACM }}$ | 6－ |  | ${ }_{5}^{8 / 6}$ | D202B |  |  |  |
|  | $7{ }^{7}$ |  |  |  | 5\％－ | KD202E 2009 |  |  | PAZ34 Audto Amplifer providing a max ourtint of 1 wats |
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| ${ }_{2}^{2 N 1305}$ | ${ }_{4}^{4 / 8}$ | ${ }^{\text {a }}$ | ${ }_{3 / 218}^{318}$ | ${ }_{\text {BFF }}^{\text {Bra }}$ | ${ }_{4}^{4 / 10}$ | ${ }_{\text {KDD2021 }}$ S009．iv． | 1A | 818 | PA237 2 watts Audio Amplifier <br> The abore threc I．C＇s are in epoxy moulded double fout－ $40 /$ in－line package． <br> MC1709CG General Purpose operational amplieer in TO |
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| ${ }^{2 \mathrm{~N} 1388}$ | 76 | ${ }^{\text {ADP161 }}$ | 9，－ | ${ }^{\text {BSY } 28}$ | $5 \cdot$ |  |  |  |  |
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| 150 |  | ${ }^{\text {AF17 }}$ | ${ }^{516}$ | OC23 | 12／6 |  |  |  |  |
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| 込 | ${ }^{8 /}$ | Asym | 6／6 | Of32 | 6；－ |  |  |  | Please note that certatin exterral components like revishors． capacitors，etc．are required to buld complete amplifiers－ but are charge at $1 /-$ each if supplied separateig． |
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