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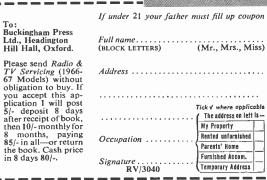


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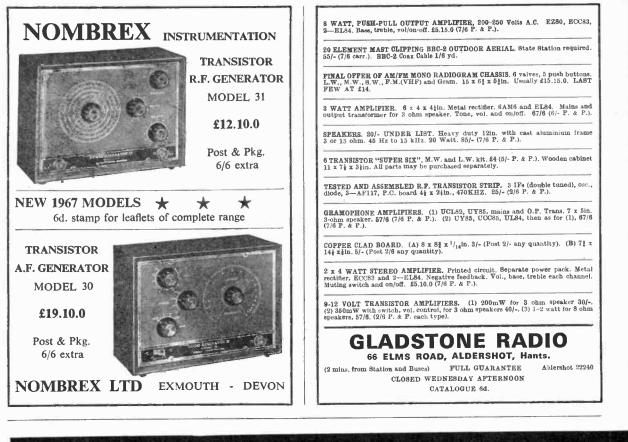
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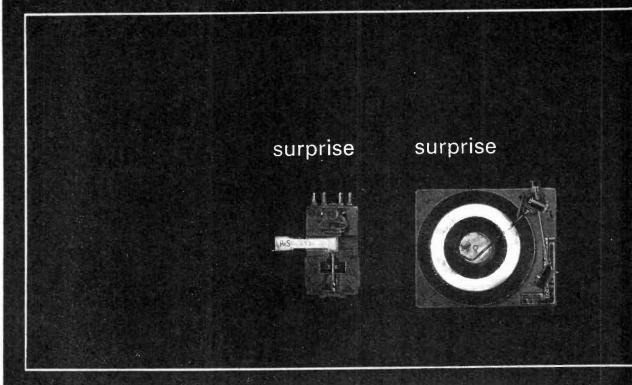
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5in. Long play, 900ft. Acetate				Long play, 1800ft. Mylar		
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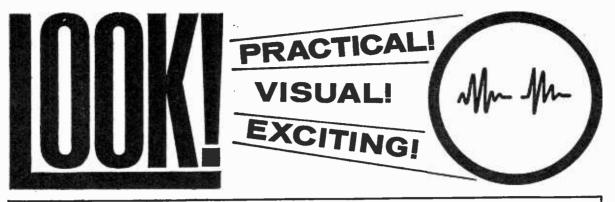
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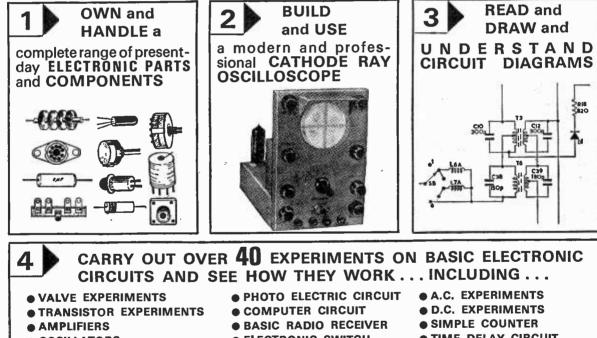
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VOL 43 No 5

issue 727

SEPTEMBER 1967

TOPIC OF THE MONTH

Keeping In Touch

T RADITIONALLY this space should be devoted to the burning issues of the day. In fact it is normally used not only as a platform for editorial policy but also to air subjects open to controversy.

RACTICAL

One objective is to provide the raw material for further discussion and to this end comments sometimes scarcely disguise the tongue in cheek. This policy sometimes backfires, as witness the overseas reader whose faith in the British character sank when we spoke of sending a gunboat down the Rhine in protest against the Hertz! Then there was the reader who darkly hinted at a despotic editor campaigning against poppirates against the will of the otherwise 100% pro-pirate staff. So there must be no mention here of the rhino whip used to control this mutinous bunch of editorial personnel otherwise there will be a protest march on Tower House. Down you dogs!

A lesson to learn here is that it matters not only what you say—but how you say it. The only certain thing is that you will not please everyone. And the same applies, on an extended scale, to the contents of the magazine. Not only the editor, but his browbeaten staff are constantly striving for the impossibility of pleasing everyone.

How, for instance, does one cater for minority tastes without incurring the rage of those with more mundane appetites? How does one devise a succulent menu to leave most readers happily gorged? We can only hope to succeed by supplementing our own judgment with the reactions of readers. Constructive criticism, comment and suggestion are always welcome; indeed are vital. Interests and tastes change from time to time and only by keeping a finger on the pulse of our readers can we gauge our progress. That is why we value your letters.

Judging from the continued high circulation of P.W. we seem to be doing nicely—but don't let us get complacent as we sit back polishing our haloes! In the end it all comes back to the wellworn truism, that by and large you get the magazine you deserve!

W. N. STEVENS---Editor

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OCTOBER ISSUE WILL BE PUBLISHED ON SEPTEMBER 8th

All correspondence intended for the Editor should be addressed to : The Editor, "Practical Wireless", George Newnes Ltd., Tower House, Southampton Street, London, W.C.2. Phone: TEMple Bar 4363. Telegrams: Newnes London, W.C.2. Subscription rates, including postage: 36s. per year to any part of the world. © George Newnes Ltd., 1967. Copyright in all drawings, photographs and articles published in "Practical Wireless" is specifically reserved throughout the countries signatory to the Berne Convention and the U.S.A. Reproductions or imitations of any of these are therefore expressly forbidden.

NEWS AND COMMENT...

FIRST AID KIT FOR THE WORKSHOP



Ever burned yourself on the soldering iron or jabbed the screwdriver into your hand? Even if you are lucky and have not, it doesn't hurt to have a first-aid kit in the workshop or shack.

Illustrated above is a compact kit measuring $6\frac{3}{4} \times 4\frac{3}{4} \times 1\frac{1}{2}$ in. (shown closed on the left). It contains $\frac{1}{2}$ oz. cotton wool, burn dressings, lint dressings, adhesive plaster, bandages, antiseptic cream, Elastoplast and a pair of scissors.

It's a good idea to slip it into your pocket if you're going mobile too, so that it doubles up as a car first-aid kit!

Price is £1, postage is free and kits are obtainable from George Bros. & Mott, Gothic Works, 1 Hainault Road, London, E.11.

TRANSISTOR PROBES AID VETS.

A transistorised instrument to detect metal objects which accidentally get eaten by cows with fodder, has been designed at the Yerevan Veterinary Research Centre in Russia.

The portable device locates the object precisely and measures its size. The foreign body is then promptly extracted with a flexible magnetic probe. It operates on a flashlight battery lasting for 200 hours, long enough to treat over 2,500 cows.

VHF SOUND SERVICE FROM MADDYBENNY MORE

The v.h.f. sound service from the relay station at Maddybenny More, between Coleraine and Portrush, Northern Ireland, started on June 26. The three sound programmes are transmitted on v.h.f., horizontally polarized, on the following frequencies: Northern Ireland Home Service 93.1 Mc/s; Light Programme 88.7 Mc/s; Third Network 90.9 Mc/s.

OSCILLATOR IN TRANSISTOR CAN



A micro-oscillator, type F3185, has been developed by The Marconi Company. Completely sealed inside a tiny transistor can, this unit is the smallest in the Marconi range of oscillators.

The photograph shows the micro-oscillator with the cover removed. The deposited gold electrodes on the circular crystal have been left out in order to show the micro-circuit underneath.

ELECTRONIC REFLEX CAMERA

A miniature reflex camera with electronically controlled shutter speeds, said to be the first of its kind in the world market, has gone into serial production at the Pentacon camera and cine works of Dresden, East Germany.

Trade-named Praktica Electronic, the SLR camera is equipped with an electronic plane shutter speeded from 30 full seconds to 1/500th sec., with individual settings arranged in a geometrical series. The single shutter-speed setting does not rotate during exposure and positive-action settings are provided for each speed.

The electronic circuitry is powered by a Mallory PX 21 alkali-manganese cell. A change-over switch permits the adjustment of a mechanically controlled shutter speed of 1/60th second.

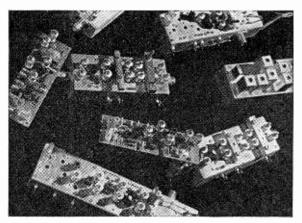
HALLICRAFTERS FROM ELECTRONIQUES

Electroniques (proprietors STC Limited) has augmented the 11,350 products it offers to radio and electronic hobbyists with a complete range of high-grade communications equipment.

An agreement has been concluded with the Hallicrafters Company of Chicago, whereby Electroniques will market the complete range of Hallicrafters radio communications products for amateur and commercial use. The agreement applies to the United Kingdom and is exclusive.

Hallicrafters amateur equipment includes high-performance receivers, transmitters and transceivers, and covers frequencies up to and including the v.h.f. bands. All apparatus is of compact, lightweight design offering the optimum performance and ease of use.

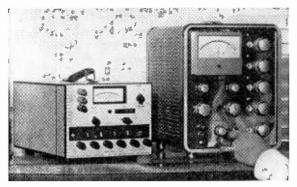
DESIGNS FOR VHF TRANSMITTERS



These v.h.f. transmitters have been designed by Mullard Applications engineers around two high-power silicon planar transistors, types BLY33 and BLY35. The circuits available are 8W, 80Mc/s a.m. transmitter; 7, 11 and 15W, 170Mc/s a.m. transmitter; 15W, 80Mc/s f.m. transmitter; 25-30W, 170Mc/s f.m. transmitter. The supply voltage for the 25-30W transmitter is 28V. All the other designs operate from a 13:8V supply.

NEWS AND COMMENT...

ALL-GOLD INSTRUMENT INSURED FOR £4,000



One of the most expensive electronic instruments — \pounds for Ib. — at this year's RECMF was this portable differential voltmeter (right) with a gleaming 24-carat polished front panel and gold plating throughout.

The golden instrument weighs only 24lb. but is insured for over £4,000. It was the 10,000th of its type produced by the American specialists John Fluke and took pride of place on the stand of Livingston Laboratories Ltd. of Watford, where it is being displayed alongside the first British-made equivalent off the production line (left). The home produced version is lighter and more compact than its golden U.S. forerunner, has an accuracy of 0.02% and is solid-state throughout. It is also cheaper because it attracts no duty.

MONO PICKUP DESIGN

Following the announcement by EMI Records Limited of their intention to introduce stereo-only classical LPs from July next, the following statement has been issued jointly by BREMA and the RECMF:—

It is not practicable to specify any clear-cut performance figures for pickups and their cartridges which will be suitable for playing stereo records, but satisfactory results should be obtained if the pickup used is either one which has been designed for stereo reproduction (though it may be wired for mono) or is a type which has good vertical compliance, low mechanical resistance and a low tip-mass. Many mono pickups produced in the past will be satisfactory although they were not designed specifically for stereo; in future it is expected that most mono pickups will be suitable, and these will be identified: — 'This mono pickup will play stereo records'.

Although some high-output pickups used with singlestage amplifiers may not fully meet these conditions, they may still be acceptable if it is desired only to play the record monophonically and on that particular piece of equipment. The manufacturers of the equipment should be consulted if it is desired to know whether a particular type is suitable.

THE WRONG RAY

In the caption to the photograph in Club Spot on page 219 in July issue the two Rays were transposed. Ray, the SWL is on the extreme left and Ray, G3MWF is pictured fourth from the left. Our sincere apologies to both Rays.

INTERNATIONAL MOBILE RALLY

"Keep going straight on and you can't miss us". The congenial voice boomed out of the loudspeaker in the car. The time around 1045, frequency—1950kc/s and the voice was John—GB3USA. Fifteen minutes later we were at the entrance to the United States Air Force Base, R.A.F. Alconbury and we had arrived at the Eighth International Mobile Rally organised by the Amateur Radio Mobile Society and the Third United States Air Force.

What a day. The sun blazed down and the people flocked in. Estimates reckoned some 5000 people attended and certainly by 2 p.m. the huge runway was crammed with cars six deep.

Couldn't make it? Want to know what you missed? Well the big hanger looked like the annual RSGB Exhibition, with over 70 trade stands displaying just about everything from surplus equipment sales to commercial Amateur stations. Then there was the giant tombola, the numerous competitions—even one for the children, the Mid-Anglia police who demonstrated a radar trap, and a superb demonstration of radio controlled model aircraft which did just about everything except serve hot lunches on board. A popular event with the ladies was the demonstration by Helena Rubinstein beauty experts.

Perhaps the most significant factor in the tremendous success of the Rally was the wonderful hospitality of the Americans. There was "Bob" who served the most delicious hot-dogs direct from an open barbacue; and the man in sun-glasses smoking a cigar who drove a gaily decorated "train" round the base all afternoon to give rides to the children. The "train" by the way, was brought all the way over from Mildenhall. Out on the runways and roads round the Base men in uniform with white hats and gloves gave clear directions to all newcomers and directed them to the parking runway. They were still out there when we left at 5.30 p.m. The "Talking Bird", a huge aircraft which, inside, looked like a "baddies" communications centre in a James Bond film. Special buses were laid on to take us to see the Police dog display and for those who got thirsty, there was a nice long cool drink which had been kept in huge bins crammed with ice. With so much going on no wonder we were all so reluctant to leave. The weather was superb, and at half past five the sun was still blazing to attention patiently waiting for "permission to set Sir". If you missed the rally then-"like man you goofed". See you next year?

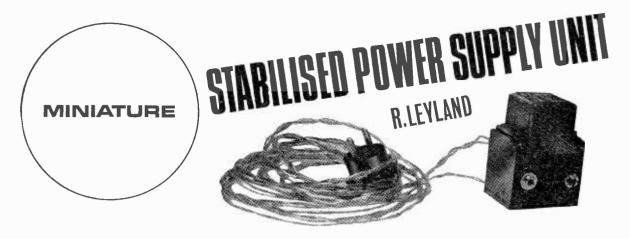
IRISH POLICE ON THE AIR

Ultra Electronics have received an initial order worth £19,000 from the Garda Siochana (Irish Police) for their new "Cub" Pocketset.

The purchase of the "Cub" by the Irish Police follows their declared policy to provide their force with the most efficient and up-to-date equipment currently available.

The equipment is already in quantity production for the Home Office and many industrial users.

Designed to meet the ever growing need for personal lightweight, 2-way radio communications equipment, the f.m. "Cub" weighs only 25ozs. It is the latest edition to the Vigilant range of portable equipment which is already used in large quantities by Police, Fire Services, public utilities and many commercial users throughout the United Kingdom and overseas.



URRENTS can be provided from this 9-volt supply of up to 100mA to work radio or other transistorised circuits. The output is kept in the region of 9 volts throughout the normal current range by a series stabiliser consisting of a power transistor and a 250mW zener diode. Beyond the stabilised range, a steep fall in voltage limits the short-circuit current to about 300mA. The steeplyfalling characteristic belongs to the voltage-doubler rectifier system and is levelled out initially by the action of the transistor regulator, to give an output impedance of approximately 5 Ω over its linear range.

Unlike most other types of power supply, it is not immediately damaged by overloads, but a shortcircuit lasting for half-an-hour or more would cause the transformer to overheat. A midget bell transformer, it has an unusually large voltage drop on load. On open circuit, the secondary voltages are 50% above the nominal values obtained at the rated 3 volt-amperes output. Choosing the 5V section, about 18 volts appears across the voltage-doubling capacitors when no load is connected to the power unit. The excess voltage is dropped across the transistor, and only about 9 volts appears at the output. This is clearly shown in the graphs, Fig. 3, of the power unit before and after stabilisation.

Zener diode

The power dissipation in the transistor is low, and the small temperature rise in normal working is confined mainly to the transformer. The zener diode also works at well below its 250mW rating. The maximum zener current (approximately 17mA) occurs when there is no load on the power unit. At output currents above 100mA, the current in the zener diode decreases to zero, stabilising action ceases, and the voltage falls.

There is an appreciable production spread in zener diodes, e.g. \pm 5% or more. The nominal voltage of an OAZ207 is 9.1V, and the output should not exceed 10 volts with a diode at the upper end of the production spread. It would in fact be rather less, possibly 9.8V, owing to the base-emitter drop. A lower voltage than this could be guaranteed, if necessary, by using an OAZ206 with a nominal voltage of 8.2V.

The characteristic of any good quality zener diode shows hardly any current at voltages below the

stabilised voltage, but when the stabilised voltage is reached, any further slight increase of voltage causes a large current to flow. This current is passed through a resistance in series with the diode, causing any surplus voltage to be dropped across the resistance, leaving the voltage across the zener diode almost unchanged, and only slightly higher. The zener diode is thus enabled to preserve an almost constant voltage despite large changes in the supply voltage, and in the face of variable loading. The constancy of stabilised voltage depends on the amount of resistance into which the zener diode works. Here it is a 470Ω resistance, together with the input resistance of the transistor.

The base-emitter potential difference of the transistor will be between 0.2 and 0.3V according to the emitter current. Connecting the base of the transistor to the zener diode ensures that the emitter voltage will be within a fraction of a volt of the voltage across the zener diode. As long as the zener voltage is maintained, the output will be stabilised, and when with heavier loading, the zener current approaches zero, the voltage across the zener diode and the output voltage will both fall. The transistor functions as an emitter-follower, tying the output to the reference voltage, acting as a control amplifier to minimize the difference between them. The transistor handles a heavier current than the zener diode, a low wattage type, is able to control directly, and permits some improvement in stabilisation. by enabling the resistance in series with the zener diode to have a value as high as 470Ω .

A highly stabilised supply would have an output impedance that is only a small fraction of an ohm,

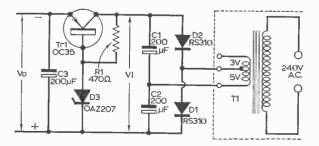
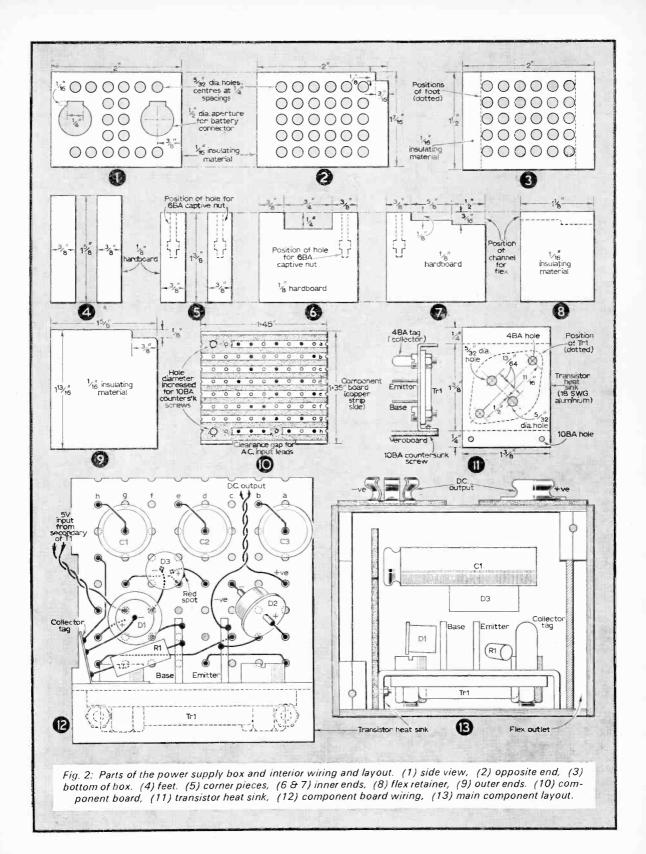


Fig. 1: Circuit diagram of the complete unit.



but this requires a multi-stage amplifier with temperature compensation. An output impedance of 5Ω compares quite well with that of a transistor radio battery.

Performance

After continuous working at 100mA for a long period, the only noticeable change is a small decrease in output voltage, less than 2%, due to warming up. The low output impedance and freedom from ripple make it a suitable power unit for Class B amplifiers with outputs up to 1 watt (see Fig. 3).

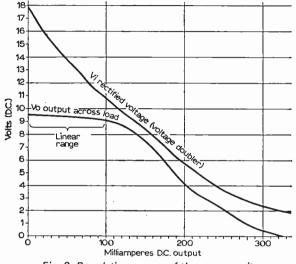


Fig. 3: Regulation curves of the power unit.

Construction

An all-insulated construction was considered necessary, with complete separation of the primary and secondary circuits. The transformer itself meets this requirement, and the other components are housed under the transformer in a box made from $r_{\rm sin.}$ insulating material, perforated with $\frac{1}{3}$ in. dia. holes for ventilation. To prevent the holes in the bottom from being blocked, it is raised on feet consisting of two hardboard strips. Hardboard is also used for the inner end pieces to provide thicker edges for gluing. An impact adhesive should be used that gives strong joints without becoming brittle.

The outer ends of the box overlap the connector blocks of the transformer and at one end a flex channel is provided in the simplest manner by shaping the top of the hardboard and adding a piece of $r_{\rm b}$ in. material on the inside to form the other wall of the channel.

Twisted plastic-covered flex, with the leads separated and uncrossed, fits into this channel, and the two leads are retained individually by the bends into the connector blocks.

At the other end of the transformer, fine plasticcovered stranded wire brings the input from the 5V secondary into the box, and similar wire is used for the d.c. output connections. These connecting leads are several inches in length to enable the component assembly to be inserted easily into the box.

The output connectors are a pair of large type transistor battery press studs, glued in position over the two apertures at the front. The tags are bent back on the inside so as to remain clear of the component assembly. The d.c. leads are soldered to these bent tags in the interior.

A pair of 6BA bolts 1in. long secure the transformer on top of the box containing the other components. These screw into 6BA nuts that are imbedded in the hardboard, $\frac{1}{2}$ in. from the top. To make this possible, the hardboard is thickened to $\frac{1}{4}$ in. by additional corner pieces glued on the inside. The vertical holes for the 6BA bolts occur at the joins, but with care, the holes can be drilled satisfactorily. If splitting occurs, this can be remedied with further gluing.

Before the outer $\frac{1}{16}$ in. material is glued on over the ends, holes are made at right angles through the doubled hardboard, $\frac{1}{2}$ in. from the top, for the 6BA nuts. These holes can be made rectangular by inserting a needle file after drilling. The 6BA nut is pushed in and positioned by screwing the 6BA bolt through it from the top. The nut is then fixed with plastic wood. Finally the outer pieces are glued on.

Component assembly

The earlier type of OC35 is thicker and will not fit into this power supply, although it is otherwise suitable.

The more recent type is only $\frac{1}{4}$ in. in depth (excluding the soldering pins).

The transistor is bolted on a small heat sink with 4BA nuts and bolts. A tag is fitted under the head of one of these bolts for the collection connection. The heat sink, of 18 s.w.g. aluminium, has two 4in. flanges. To one of these a small square of Veroboard is fastened at right angles to the heat sink by a pair of 10BA countersunk bolts with nuts.

The Veroboard measures 1.45 by 1.35in. and is sawn from a larger piece. If necessary it can be filed a little at the edges to allow it to be fitted easily into the box when attached to the heat sink. A small gap is filed at the top edge to leave sufficient room for the leads to the transformer secondary.

Three breaks are made in the copper strips. Two of these are necessary to avoid contact through the 10BA bolts with the heat sink. Three jumper links of 24 s.w.g. tinned copper are added. These are inserted from the other side of the Veroboard and soldered to the respective copper strips.

Wiring the power unit presents no difficulty if the proper sequence is followed. The resistor R1 is connected between the collector tag and the base pin of the transistor. A wire is taken from the base pin to an adjacent point on the board as shown. A heat sink should be applied on the transistor pin when soldering. The emitter pin also connects to the components board, and a flying lead is taken from it for the negative d.c. output. The other leads are taken from the points on the board shown, and must be of fine flexible plastic-insulated wire to

-continued on page 343



Transistor lead indentification is given with the respective pictorial diagrams. The 2N2926 has a central collector lead as shown in Fig. 8 (sketch A) and this must be bent (sketch B) to suit connections for Tr5, Tr6 and (sketch C) for Tr7. Sleeving should be fitted to all transistor leads.

After careful checking the tuner may be tuned without the lid on the screened compartments. Connect dipole, 9V battery and crystal earpiece or amplifier. A rushing noise is normal in the absence of a signal and should disappear as a switched-in preset (TC1-TC3) is adjusted. If the entire capacitor range fails to bring in all three programmes adjust L4 by slight extension or compression to shift the resonant range. L1 and L2 are very broadly resonant and will not need adjustment at this stage, if at all, but L3 core should be adjusted half a turn at a time for every sweep with the tuning pre-set. When the three programmes have been located switch and tune all three pre-sets, then adjust L3 core for optimum performance over the band. Some adjustment of L2 (by slight extension or compression) may be necessary. Fit the screen lid and note the effect upon tuning. Adjust L4 to restore the range, a matter of a few trials before the lid is permanently attached by spot soldering in four or five places. Final adjustment is best achieved with a poor signal-from a split-flex indoor dipole, for example-so that you can tune L4 through the screen hole, and the pre-sets, for minimum background noise.

The excellent results obtained with a crystal earpiece suggest that the tuner can be used for 'personal" listening, a far more enjoyable experience than plugging the earpiece into most transistor receivers. The audio output is more than ample and drives the author's 5-watt transistor amplifier (without pre-amplifier) and should therefore be enough for most fidelity needs. An output capacitor will be necessary if this protection does not exist at the input of the amplifier or pre-amplifier-up to $50\mu F$ and an appropriate working voltage for transistor equipment. The tuner requires a 9V, 11mA power supply and this can be supplied from other equipment provided the correct polarity is observed. A 12V supply (maximum) will increase the sensitivity, frequency stability and output if this is necessary. The frequency stability of the oscillator will tolerate some supply variations but cannot be expected to offset the effects of very poor regulation.

Although a single-pole three-way switch is sufficient the photographs show a three-pole type with the unused tags earthed. There seems to be a tendency for dealers to stock only three-pole types on

Second and final part — by W. GROOME

the grounds that these will do for one-, two- or three-pole use. Again, although dealers' stocks have become largely representative of the transistor era it is by no means easy to obtain switches smaller than those that have done service in valve circuits ever since the war. Because of this supply difficulty a standard-sized component has been specified. Despite all this, the tuner is small enough to fit into most fidelity housings very easily. Perhaps, when the required small components are readily available, I will cram the entire tuner into a fag-packet!

Note. Throughout this article the term "earth" means the positive line of the tuner.

CONSTRUCTION

Divide conductors as in Fig. 2, drill screw fixing holes in first (unused) conductor and through S21. Restore continuity here with bare-wire soldered connection S20 to S22. Drill hole at P30 to pass switch bush and fit platform with pre-set capacitors, secured by fitting switch. Connect insulated wire from midpoint of Q18 and Q19 to V32. Black connection from mid-point Z21 Z22 to mid-point M25 M26 and from there to M11. Make bare connection from T to S near hole 2. Make bare connection T25 U26 V27. Turn panel plain side upwards so that M1 is top left and switch is on right, then proceed as in Table 1.

	TABL	E I R.F. STAGE (FIG. 4)
M2	N2 C1	
S2	Q2 R2	
S3	Q3 C3	
	$\left\{ \begin{array}{c} N1\\ 01 \end{array} \right\}$ L1	See Fig. 3
M5	P5 R3	
S5	— R4	wire-to-wire with R3
S6	— C4	wire-to-wire with R4
	N3 Tr1	emitter
	N5 Tr1	collector
	P4 Tr1	base
	S4 Tr1	screen
S7	M7 C2	wire sleeved, flat on panel
	M6] 2	Fig. 3 Equi-distant from
	N8 ∫ ⊑	other components and panel edge
M10	M8 R1	Wire sleeved, bent close to resistor and panel
—	$\left. \begin{array}{c} N9 \\ P9 \end{array} \right\} C5$	
T1		This screen support wire can be left until screen is fitted

Check work already done with circuit and pictorial diagrams, then turn panel, again plain side upwards, so that switch is on left and M1 is lower right. Work then proceeds generally in the direction left to right as before.

Check work thoroughly before fitting screens. The shorter screen should lie along row T. Trial fit first to mark positions of small partitions—R.F. partition to stand between rows 9 and 10 with C5 on one side

TAB	LE II	osci	LLATOR STAGE (FIGS. 5 AND 6)
M13	P13	R6	
S13		R7	wire-to-wire with R6
I —		L3	short stiff wire connection from one
			tag to top wire of R6. C7 aids support;
			no further support needed
S12	—	C7	connect to second tag on L3
M14		C6	negative
- 1	S14	C6	positive. Wire sleeved, flat on panel
M16	N16	R8	1
Q16	S16	C8	
P17		. —	wire partition support, similar to T1
-	N17	C1	0 to right of P17
	017	{ ···	
1 -	Q18	>C9	
	S18)	
S19	Q19	R9	
	N15		collector
- 1	P15	Tr2	base
I I	Q15 S15		emitter
	Q24	Tr2	
	S24	> C1	1
-	524	ر 	Connect unused switch tags together
			and earth to S28
1 -	025		Insulated lead to switch selector tag.
1			Press wire flat on panel and bend
			C11 clear of L4 area
M25	M23	R5	
- 1	N21	314	Trial fit and bend ends to make coil
	Q21	54	stand about $3/16$ in. above panel, $\frac{1}{4}$ in.
			clear of panel edge and equi-
			distant from other components. Refer
1-01			to Fig. 3, Fig. 6 and photograph
T24			Partition support wire
			~ ²¹ ²⁰
			23 22 BB
			25 24 3 123
			27 20 0 0 0 0 0
	26	29 28	
20	31 30	\searrow	· R13U €14 · 16 B _ 2 C15
32		5 .	

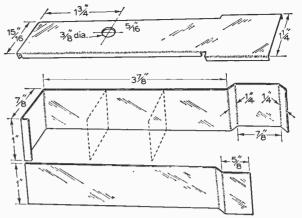
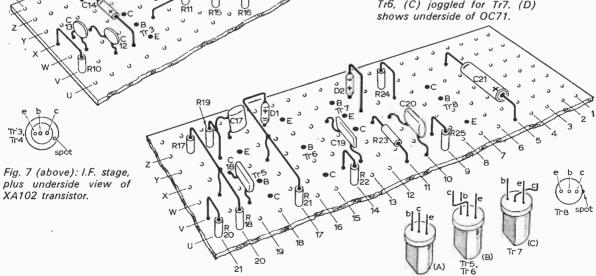


Fig. 9: Details of tinplate screens.

TABLE III I.F. STAGE (FIG. 7)								
V3	3	X33	R10		—	X29	Tr3	collector
-	_	X32	} C1	2	V25	W25	R15	
I I		W32	٢٠	3	U24	V24	_R16	
-	_	X31	} C1	2	—	U23	}C1	5
1		V31	J			V23	J	-
I -	_	Z30		negative	Z22	Z24	_R12	
-		V30	C14	positive		Y22	}c1	6
Z2	7	X27	R13			W22	<u>ر</u> م	0
Z2	6	Y26	R14			W24	Tr4	emitter
W:	26	W28	R11			X24	Tr4	base
-	_	V29	Tr3	emitter		Y24	Tr4	collector
- 1		W29	Tr3	base				

Fig. 8 (below): Discriminator and output. Sketches of 2N2926 show underside (A) as pur-chased, (B) joggled for Tr5 Tr6, (C) joggled for Tr7. (D) shows underside of OC71.



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Tr': Tr

	IINATOR AND OUTPUT ES (FIG. 8)
Z19 Y19 R19 wire-to Z18 — C17 wire-to — X19 V19 C18	o-wire with R18 o-wire with R18 o-wire with R19
 Y18 Tr5 emitter W18 Tr5 base V18 Tr5 collect 	
in Fig.	o-wire with R21. Note polarity 8
U14 V14 R22 — V13 Y13 — Z15 Tr6 emitter	
— X15 Tr6 base — V15 Tr6 collect	
$ \begin{array}{c} - & 13 \\ - & 011 \\ X11 \end{array} \right\} R23 $	
$- U10 \\ X10 \\ C20$	
 V7 Tr8 emitter X7 Tr8 base Y7 Tr8 collect Y7 Tr8 collect Z5 C21 negative U5 C21 positive 	or /e

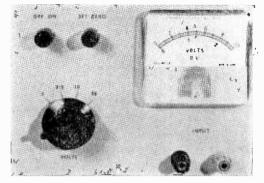
and R1 the other, oscillator partition between rows 16 and 17 with C8 R8 on one side and C10 the other. After soldering partitions to screen attach plastic adhesive tape to areas likely to touch components when fitted, then fit screen to panel by soldering to wire supports T1 T24 F17. Attach the other (long) screen by soldering lap joint, partitions (hot iron outside, cored solder to joint inside) and a spot joint to tinplate platform near switch. Lid to be spot soldered after final tuning adjustment, or may be omitted if tuner is eventually to be fitted in a screened housing.

Connect the following leads as in Fig. 2:

- Z1 negative, black flex. -9V.
- S1 or T1 positive, red flex. OV.
- core \uparrow to socket attached to braid \int housing. M1 co-ax cable, core
- S1
- Y1 a.f. output, via capacitor if this is not present in a.f. equipment input.

IMPORTANT. Observe polarity when connecting to other equipment. On no account must the positive line, the screens or the aerial be allowed to contact the earth or chassis of "negative earth" equipment. Next to a battery the simplest supply is a smooth, well-regulated -9V from transistor equipment with positive earth. With negative-earth equipment connect Z1 to equipment negative line and S1 (or T1) to +9V obtained by dropper resistor or bleeder from equipment positive line.

two voltmeters for the workshop



The comparatively recent inclusion of silicon devices into electronic circuitry has brought one of the most simple measurement problems into the foreground. This article describes the construction of a modern a.c. millivoltmeter and a d.c. voltmeter incorporating silicon transistors.

the music box a simple pre-set portable

Make this easy-to-build transistor portable receiver. Only three transistor stages to wire up. Utilises a cheap pre-wired audio strip with push-pull output stage. Tunes in the stations of your choice at the flick of a switch. Tagstrip wiring for ease of construction and only two controls. Full constructional details of case included.

economical speaker enclosure

The weakest link in many audio set-ups is the loudspeaker-or, to be more exact, its housing. Here is a simple and easy-to-build corner enclosure which should help to obtain better results from existing speakers.



October issue — on sale September 8th

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THE BROADCAST BANDS

by JOHN GUTTRIDGE

Times in GMT Frequencies in kc/s

MIDDLE EAST

Egypt: Cairo Radio (U.A.R. Broadcasting and TV, P.O. Box 1186, Cairo) uses the new frequency of 15,050 in parallel 15,475 to carry its main Arabic programme.

Iran: Radio Iran (Ministry of Information, Meidan Ark, Tehran) is again using 3,780 for its home service and giving an excellent signal around 1,800. The regional station Radio Isfahan gives a fair signal at 1715 on 7,890.

Iraq: *Radio Baghdad* (Salihiya, Baghdad) using additional frequencies to relay home service: On 15,400 from 0930–1200 and on 11,785 0530–0700 and 1200–2200.

Lebanon: *Radio Lebanon* (Ministry of Information, Beirut) transmits in its external service as follows: 1830–2030 on 17,750; 2300–0100 17,765; 0130–0400 11,965. Some reports give this last frequency as 11,760.

Syria: Radio Damascus (Ommayad Square, Damascus) is relaying its home service on 17,860 at 1300-2300 and on 15,165 1900-2300. English is beamed to Europe at 1600-1700 over 15,165.

AFRICA

Algeria: Radiodiffusion-Television Algerienne (21 Boulevard des Martyrs, Algiers) is to start shortly using a 1,000kW long wave transmitter. This will be the first long wave transmitter in Africa.

Ghana: Radio Ghana (Broadcasting House, P.O. Box 1633, Accra) is actually using 9,755 instead of the announced 9,760 for its 2000-2100 English transmission.

Nigeria: *Radio Nigeria* (Broadcasting House, Lagos) is now carrying its external service over 21,645/15,255/11,715/7,275. English is at 1500–1600, 1700–1900, 2100–2200.

South Africa: *Radio South Africa* (P.O. Box 8606, Johannesburg) is once again using the 11m.b. The transmission concerned is at 1000–1455 and frequencies are 25,730/21,495/17,805/15,200. Careful tuning will bring in the home programme around 2100 on 3,250.

ASIA

Afghanistan: Radio Afghanistan (Ansari Watt, Kabul) has a new transmission beamed to Europe at 1100–1200 over 17,825/15,340.

China (Taiwan): Voice of Free China (Taipei, Taiwan) now uses 17,890/17,780/17,720/15,345/15,125/11,825/ 7,130 for its 0200–0350 English transmission.

India: All India Radio (P.O. Box 500, New Delhi) has English as follows: 2245–0015 7,235/9,615; 2245– 0115 9,740/11,760; 0030–0115 11,710/15,105; 1000–1200 15,105/15,165/17,705/17,890/21,615; 1330–1500 15,375/ 16m.b.; 1745–2230 7,215; 1745–2030 11,620; 1745– 1945 15,230; 1945–2045 9,690/11,775; 1945–2230

9,912; 2045-2230 11,755.

Indonesia: Radio Republik Indonesia (P.O. Box 157, Djakarta) has English as follows 1900-2000; 2330-2400 9,865; 0900-0930 11,770; 1100-1200 9,865/11,770. A new home service outlet has been noted around 1100 on 5,065.

Japan: N.H.K. (Tokyo) frequency usage for English and Japanese service is 0100–0730 15,105/15,195/ 15,300; 0800–0930 15,300/15,195/9,505; 1000–1330 9,505/11,815/15,300; 1400–1630 9,505/9,560/11,815; 1700–2130 9,560/11,815/15,105; 2200–0030 15,195/ 15,300/17,785. Transmissions are every hour on the hour and last 30 minutes except for those at 1000, 1400 and 2300 which last 90 minutes.

Pakistan: Radio Pakistan (Broadcasting House, Bunder Road, Karachi) has a dictation speed English news broadcast at 1335–1350 on 15,100/17,812. The U.K. English TX at 1945–2030 is now on 11,672/15,365.

NORTH AMERICA

Canada: C.B.C. (P.O. Box 6000, Montreal) has replaced 21,460 by 21,595 at 1100–1215 and 1345–2152 and has replaced 15,365 by 15,320 between 1100 and 1830.

CENTRAL AND SOUTH AMERICA

Bolivia: La Cruz de Sur (Cajon 1408, La Paz) is reported fair at 0200 over CP75 on 4,985.

Brazil: Radio Exelcior (Rua Wenceslaut Brazil 78, Sao Paula) gives fair reception at 0100 on 9,585.

Costa Rica: Radio Popular (Apartado 341, San José) is now using the additional frequency of 4,784.

Uruguay: Radio Oriental (Olimar 1364, Montevideo) is fair at 0030 on 11,735 (CXA7).

Venezuela: *Radio Maturin* (Maturin). YVQH has been noted on 5,040 with fair signals around 0100.

EUROPE

Germany: Deutsche Welle (Bruederstrasse 1, Postfach 344, 5 Koln) has made frequency changes in the following English TX: 1550–1620 15,275/17,880; 1900–1910 15,405/17,785.

Greece: Voice of America (Washington, U.S.A.) has closed its G8 Thessaloniki and Rhodes relays to avoid censorship.

U.S.S.R.: *Radio Moscow* (Moscow) now has the following European English schedule: 0700–0730 9,700/9,710/11,830/11,890/15,300/15,360; 1200–1230 11,700/11,740/11,830/15,300/17,760; 1900–1930 1,322/ 9,710/9,770/11,830/15,170; 2000–2030 1,383/9,710/9,770 11,830/15,170; 2100–2200 1,443/9,710/9,770/11,830/ 12,060; 2200–2230 1,322/1,383/1,443/9,710/9,770/11,830

Thanks go this month to G. Coyne, M. E. Terry, R. J. Warner, the International Short Wave Club, and the Swiss Broadcasting Corporation. A SOMEWHAT controversial month with some claiming things were so bad they were going to take up chess, while others lamented that there were not enough hours on the clock to log all the DX. At '3JDG things were about half and half, but most s.w.l.'s logged my best ones anyway and threw a few more in for good measure.

From letters received it is now certain that 8R is the new prefix for VP3. I reckon all people issuing a Countries List should give away a free pen with it for all the alterations that will arise while the darn thing is still in the post. I can hardly wait for instructions to change my call to VXY7JDG. (Many a true word!)

One or two have written in to ask about a competition or a table of some sort. If there are enough takers we might try this, any suggestions as to what form it should take?

Quite a heavy postbag this month so I'll replace my muzzle and press on with what others have heard.

LOW

Nothing extra special reported on topband other than hordes of G's and quite a large number of mobiles. Eighty fared a little better but surprise surprise—forty has been given a going over. John Wresdell (Yorks), logged ZL3IJ and ZL4LM on 80 s.s.b. so the DX is about on this band. John is 13 and takes the RAE in December. (Good luck OM).

R. Iball (Notts), AR88D, 80 ft. end-fed with 35 ft. 72 Ω co-ax managed these on 7Mc/s c.w.—HI7JMP, HK4AOY, KZ5FX, PY2AXZ, 3C2ATD, 6Y5RM.

Paul Baker (S. Wales), HE30, 100 ft. end-fed 30 ft. up snapped this little lot up on 7Mc/s s.s.b.— CN8AW, CN8BV, CR6IV, DJ, DL, DK, DM, EA4JV, F, HA, HB9, I1, MP4BEU, MP4TBO, OD5AR, OHØNI, OY7S, PY4FLR, PY7APS, PY7VKG, PY8QA, PZ1CF, TF2WKM, UA1KBX, UQ2KAJ, UW9AF, ZC4MO, ZD7CI, ZD8CX, 3A2CQ, 4X4VE, 9G1BF, 9H1AM, 9Q5SS. These were all received 2200-2400 GMT.

F. Simpson (Yorks), no rig quoted, must be pretty good headphones, got these on 7Mc/s phone— HK3BHV, K1GZL, K2ZKA, K4LYW, KP4CQY, PY4ND, PY7AKG, W3ADO, W4YWX, WA4MZI, WA9OIN, WB4FRL. Why is it all these stations never seem to be on forty when I listen. ('Tiz a conspiracy Jim Lad, Har that's what 'tiz).

A number of s.w.l's commented on the dozens of G stations who are about these days (and nights) on forty, so perhaps that 100kc/s will begin to buzz again. Why not give it a try this month?

HIGH

It looks like twenty is still top DX dog with fifteen and ten a close second.

David Henbry (Sussex) roamed twenty with that O-V-O of his. This is coupled into a "Joymatch" No. 2 and the antenna is a 7 ft. vertical at 30 ft. David logged these on s.s.b.-CR4BC, CR6HI, EL2AJ, HK5AZA, KG4AM, KL7EBK, KP4AXC, LU2DGO, LU9DM, MP4BEU, MP4TBO, MP4MAX, OA4MX, UWØIE, XW8CC, VP6WR, VP2AA, VP8IU. PZICF. ZD3I. ZD8RD, YS1CPI, VS9ARS. 5H3JR, 6O1GB, 6W8DX, 6Y5GG, 8R1S, 9G1GA, 9U5BB, 9Y4VT.

D. Fry (Glos) 52 set. $\lambda/4$ dipole (coo!), reports twenty lively especially late evenings. He scooped— HV3SJ, JA4DJO, KP4CRD, K70EW/MM, PY1CAD, SVØWL, T12PZ, UA3KND, UB5KIW, UWV3T, VQ9HJB, VS9MB, XW8CC, YV4QG, YV5ANF, 5A4TR, 6W8DX.

Is your name Philip, and do you live in the Langley Mill area of Nottingham? You've got an RX60 receiver and a 20 metre dipole in the loft, but you haven't got a second name! Anyway, on 20 a.m. and s.s.b. you logged—CE1AQ, CN8CS, CR4BC, CR6IV, CR7CH, EA8OG, EP2KW, HC1DX, HM5BF, HV3SJ, JA2BV, K8VWM/P/KG6, KA3FU, KA9LLE, KP4AST, KR6AB, KR6QG, KV4UA, LU3IQ, MP4BE, OD5EU, OY9IN, PY1CRI, PY7SM, TF2WKI, VE1AFY, VP9CP, VQ9HJB, VU2DKZ, VK7RÉ, VKØTO, WB2BWW, WB4BII, XW8BJ, YV3LA, ZC4TK, ZD3DM, ZD8RD, ZD9BI, ZP5OG, ZS6AYI, 3A2CP. ZE1AE, 5R8AS, 5A1TV, 5A4TV, 5N2AB, 5Z4KL, 707LZ, 8R1C, 8R1S, 9H1AB, 905BIG. Take a bow Philip—whoever you are.

B. Hughes (Worcs), AR88D, dipole, listened on 15 for—HK1KS, JA9BXL, KZ5AO, KV4CX, 4S7PB (Ceylon), 5R8AS, 9M2PO, 9V1NP, WAØDVT.

L. Rowland (Cheshire), 9R-59, 150ft. end-fed, switched in the b.f.o. on 15 and heard these on s.s.b. CE3DM, CN8FC, CP6GC (Bolivia), CR4BC, EL2AI, EL9A, HC1MW, HI8LAL, HK1OI, HKØAI (San Andres Is.), HP3PJ, HR1CN, IS1VAZ, JA1AEH, JA2ADH, JA3JEJ, JA4ABS, JA8BIU, KG4AN, KG6FAE (Guam), KH6BFU, KL7WAH, KR6GF (Okinawa), KP4CP, KV4CX, KZ5FW, LU1DAB, MP4MAW, OA4JR, OD5DJ, PY1TX, PY2SD, PY5BK, PY6NG, SVØWV, TI2JH, TJ1AG, TU2AY (Ivory Coast), VK4QM. VK9XI (Christmas Island), VR1AT, VS9ARS, W5PBH, W6CCP, W7MSI, YA1DAN, YN1BKC, ZB2AM, ZC4JU, ZD8CX, ZP5JB, ZS1BD, ZS4LI, ZS5NX, ZS6PZ, ZS8L, 4S7PB, 4X4BL, 5A1TV, 5A2TR, 5A3TG, 5A4TR, 5A5TV, 5H3JL, 5N2AAJ, 5Z4KK, 8R1S, 9H1AG, 9J2AB, 9L1JW, 9M2NF, 9Q5BD, 9V1FF. This is only three-quarters of the log too!

K. Jeeves (Yorks) CR70A, PC30, 80 ft. long wire, doesn't say what mode but heard these on 10— CN8BB, IT1ALG, UG6ARO, VE3FUG, VS9APW, ZE2JA, 3C3GCO, 5A1TK, 9H1X.

Signalman G. Gibson writes from Germany. He has an EC10, 50 ft. long wire, and a sharp pair of ears. On 10 a.m. he got—CT3AM, CX6AD, LU5DRC, PY2CK, PY8SV, UB5GUS, UL7OB, ZE1CS, ZE2JA, ZS2OM, 9J2DF, while on s.s.b.—CR6IV, CR7BF, EP2GI, OH2TI, PY2OY, ZD8CX, 4X4BL, 9J2VX, 9Q5DD.

D. Goodhall (Rugby), HE30, 40 ft. long wire hooked these in on ten, mostly s.s.b.—EA4JN, HG5CZ, LU3IAG, OZ6HP, PAØBK, PY2AFL, UA6JP, ZC4TY.

CONTESTS/RALLIES

2

This month the list includes—August 13th, Derby Mobile Rally, at Rykneld School, Derby. That's it, sorry, can't find any contest, and no sign of anything else for August. On September 2nd - 3rd is the V.H.F./IARU contest. Deadline for logs is, as usual, the 20th.

LETTERS....

John Arminson Rouse — A Tribute

May I express, as a reader of PRACTICAL WIRELESS, the shock and sorrow at hearing the news of the death of Mr. John Rouse, G2AHL, who was General Manager and Editor of the RSGB. I am sure I speak for many readers, RSGB members or not, because John had a high regard for 'PW' and he and I often spoke about articles and readers' letters in it.

The much improved RSGB Bulletin, and the very fine Third Edition of 'The Amateur Radio Handbook' is seen, I know, by many more people than just RSGB members. Mr. Rouse made both these developments possible with his tremendous devotion.

We have lost a much loved worker in the field of Amateur Radio, and I for one and the small band of boys in the Radio Club I run, have lost a personal friend. We will miss his cheerful anecdotes and great encouragement.—Ken Smith, G3JIX (Walthamstow, E.17).

[I am sure that all readers will join with myself and the PW staff in Ken Smith's tribute to the memory of John Rouse. Many of us have lost a personal friend and PW, the RSGB and amateur radio in general will sadly miss his devotion and loyalty to the cause of amateur radio. We must spare a thought, too, for the wife and daughter he left, for John was still only a young man. Amateur radio can ill-afford such tragic losses.]—W. N. Stevens.

Why not tape them?

Whilst attempting to wind a coil on a cotton-reel which became very tedious, I sought after a faster method. I tried a sewing machine but was unsuccessful then in despair tried using a portable tape recorder. The cotton reel fitted on the rewind spool perfectly and by using a screwdriver I was able to guide the wire on to the cotton-reel while the recorder was on rewind. After a little experimenting this was found to be very much quicker and neater than winding by hand .--- S. Cooke-Willis (Auckland, New Zealand).

No more excuses, please

When are these types going to run out of excuses as to why they should be exempt from the RAE and the morse test? I refer to Mr. T. Hawker's letter in the July issue, who seems to think that just because he uses radio telephones he should be given an amateur licence.

Let's put this in its right perspective, this equipment is all commercial gear which is approved by the GPO and is also crystal controlled. The only qualification to operate it being, the ability to press a button and speak the appropriate language. A child of five could do it.

He asks where is the sense in it? Maybe this question is the answer to why he failed the RAE, he may not have enough enthusiasm. After all the RAE and the morse tests are the only way in which we can weed out the person who just wants a new toy to play with, from the real enthusiast who would be a competent amateur.

When I look around at some of the Bedfast Club members, I thank God that I have got all my human faculties as I don't think I would have the drive of these less fortunate types, there are no exemptions from the rule.

I have no time at all for the anti-RAE, the anti-morse, and the citizen band brigades, if these chaps were to spend a bit more time studying for these things and less time thinking up reasons whey they should be exempt, in no time at all they would be on the air saying how easy it was.

No hard feelings old man, best of luck for the next RAE.— **R. T. A. Brown**, G3TOF, Hon. Secretary Harlow & District Radio Society (*Harlow*, *Essex*).

Fault-finding on a "dead" receiver

I would like to comment on the series of articles "Repairing Radio Sets" by Messrs. Hellyer and King. I was trained in HM Forces and although the equipment we use may be a lot more sophisticated, the basic principles surely still apply.

The way I was taught to fault-

find on a "dead" set disagrees with the method shown in the series. I was taught to start at the a.f. end and work towards the r.f. end, by applying a suitable signal to first the speaker and then to the a.f. stages, i.f. stages and back to the r.f. stages and aerial input. The output should then be heard after each step.

If no input signal is heard, then the section in which the fault lies is the first one you have applied the signal to and obtained no output from the speaker.—J. F. May (Gosport, Hampshire).

The Author Replies:

The stage responsible for complete failure of a radio set can be located quickly by adopting one of three methods: (i) applying suitable signal in turn to the stages starting from the aerial input, (ii) as in (i) but starting from the loudspeaker and (iii) applying a modulated signal at the aerial and then tracing the signal in the set from input to output.

Methods (i) and (ii) can be discussed at length in terms of relative merit! If the trouble is open-circuit of the aerial coupling coil, for instance, method (ii) would take as long as method (i) would take to find an open-circuit in the loudspeaker. It is well known that HM Forces recommend method (ii); but this does not mean that the other methods are less effective. Forces equipment has to be maintained to a higher level than ordinary domestic radios, and technicians are often surrounded with test equipment designed for matching the equipment to be serviced; and each repair usually demands a stage-by-stage performance check in terms of voltage sensitivity and so forth and, as stated by Mr. May, if a common output meter is employed, then each input can immediately be translated into input sensitivity voltage.

The various methods of faultystage locating have not yet, in fact, been dealt with at length in the articles These are in hand for Part II, when the transistor set as a whole is put under the service microscope. The series commenced at the first stages, working to the audio section, because this is the normal direction of the signal. There was no other motive!

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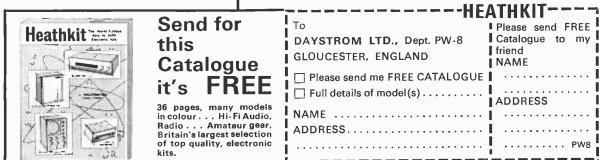
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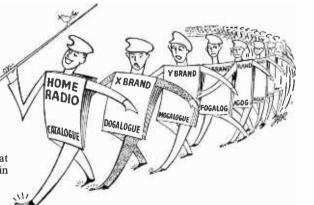
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repairing radio sets

PART 6 H. W. HELLYER

printed circuits

OPING with printed circuits is partly a matter of common sense, partly a matter of knowing how these aids to construction are designed, formed and used.

Contrary to idealist opinion, the printed circuit has not been employed—in many receivers—to eliminate the wiring. In some sets it seems to have further confused the issue. Certainly, printed circuits can make fault-finding much more difficult unless one unlearns the old procedures and gets acquainted with the new. In too many designs, the aim of printed circuit boards has been to reduce production costs, with no regard for servicing. In short they can be a mixed blessing.

However, like the poor, they are with us—if not to stay, at least, for a very long time to come. So it behoves us to find out as much as we can about them.

★ BASIC PRINCIPLES

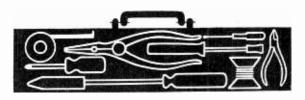
The technique of forming interconnecting wiring flat on a piece of insulating material began with guided missile research toward the end of World War II. Some of the insulating materials then in use were bulky, expensive and less effective than those available to us now. The principle remains the same, though the processes of manufacture have developed.

Basically, the printed circuit is a board or laminate of high quality insulant with the wiring between components and test points or connections to other parts of the equipment laid out in a pattern of thin copper strips. This copper, the foil, is bonded to the laminate and the component leads are inserted through holes and soldered to the foil. We thus have the three basic ingredients of the system, the board, the foil and the bond, to consider.

A common type of board for rigid mounting is phenolic paper laminate. This is made in various thicknesses. Alternative materials are used, particularly where some flexibility is needed, or higher voltages have to be handled, or higher currents passed than those with which we are at present concerned. Most interesting of the recent developments has been a film type of printed circuit, completely flexible, very thin and almost transparent!

A copper foil, perhaps as thin as one and a half thousandths of an inch, is bonded to the board. The method of bonding is often a trade secret, as jealously guarded as a Whitehall file, so that, after processing, the very fine lines of copper that form the circuit will not lift away from the board, especially as components are fixed and soldered.

Heat is the great enemy, and for this reason, con-



siderably more care must be taken when dealing with printed circuits than when soldering conventional wiring. There are two danger points; first, the foil itself can lift when the bond is destroyed by heat, leaving a weak portion that may later fail; and, second, the method of construction means that components will generally be affixed by much shorter lead-out wires than with conventional wiring, and excess heat can damage small components. This last factor applies especially to transistors, of course.

*** РНОТО-ЕТСН МЕТНОД**

Perhaps the most popular way of making a printed circuit is the "photo-etch" method. The design for the print is carefully made—this being the foundation on which the whole process is built. Components are laid out so that the "wiring" takes the desired path, with inter-connections taking the shortest path possible, and no leads crossing where they should not!

This last apparently elementary point is vital in high frequency work to avoid instability and other undesirable effects. Anybody who doubts the importance of this preliminary planning may gain a new respect for the "back-room boys" of the electronic industry by doodling out a few simple drawings of printed circuits for his own amusement!

It is no easy matter to compress a dozen or so components in a couple of square inches, make sure that there is room to bend leads and mount them, and ensure that transistor leads do not have to cross, then draw out the maze that will eventually be the print without allowing adjacent connectors to encroach too closely. I speak with feeling!

However, assuming someone else is carrying out this tedious task, after the doodle is perfected a master drawing is prepared. This is drawn to scale, much larger than the required board, and all the details are put in, including the holes for the component wires (which appear as white circles on the black lines of the print). This "black-and-white" master drawing is photographed and the negative brought down to the actual size of the required board.

The copper foil which covers the whole board is emulsified and the negative is "printed" on to the plate by light exposure. The holes are drilled where indicated on the pattern and the printing is treated with an acid resistant chemical.

★ FIXING COMPONENTS

Then the treated board is placed in an etching bath whose solution of iron perchloride dissolves the surplus copper and leaves the printed wiring untouched. The acid resist is then cleaned away and the board made ready for soldering.

Components are fixed to the board and soldered into place—again a highly specialised process, often individual to the manufacturer. The principal methods are dipping or wave soldering. In the first method, the board, with the ends of the components crimped into place, is briefly dipped into a bath of molten solder and all the joints are made in one go. Surplus solder is shaken off and the cooled board treated with protective shellac.

The alternative method moves the board along the surface of a bath of molten solder which is made to "wave", so that the copper foil and component wires skim through the wave.

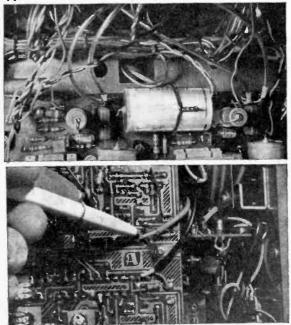
There are other techniques, such as plating of circuits, silk-screen printing, double-sided bonding, where the print is made on both sides of the board, inter-connections being achieved by soldered "collars" that go through holes in the board, and spot-soldering methods that protect the wiring and solder only the joints. The details are extremely interesting but must not concern us here, as the treatment of such circuits, for fault-finding and repair, follows much the same general pattern.

★ TRACING FAULTS

Tracing faults on printed circuit boards can be difficult. Slight cracks, invisible to the naked eye, or dry joints that present a high resistance to the lowvoltage, low-current circuit and are hidden under respectable looking mounds of solder, are common troubles.

One device that can be useful is a simple length of wire terminated at each end by a sharp probe and used as a temporary shunt to "prove" suspected wiring on certain ranges of transistorised radio and tape recorders where experience had taught us open circuits through flexing could be found.

Because it is not easy to remove or disconnect components to make proving tests, a different approach to fault-finding has to be made when deal-



ing with printed circuits. My colleague, Gordon J. King, has already had something to say on this subject, and will be underlining this point when we come to the servicing of transistorised equipment and all the special care that this entails.

For the present, let me make a few purely practical remarks about the removal and replacement of components and the treatment of printed circuits, just to lay the ground.

First, and most important, point is to keep the heat applied to the minimum. The maker of the printed circuit went to a lot of trouble to get a good bond of foil to laminate. No use our ruining this by leaving a hot iron too long at a crucial junction.

★ REMOVING COMPONENTS

The practice of digging away at a joint to remove the end of a component wire, or the tag of a control, is one of the worst P-C offences. When removing a component whose wire end has been bent over, crimped or twisted, snip the lead *above* the board and allow the twisted end to drop away with the minimum of melting.

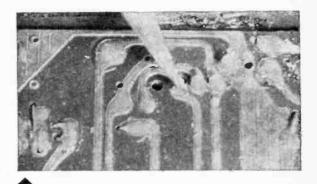
In many cases, even if the component is cut short, this technique will still allow enough wire end for a quick "straight-through" reconnection. If not —well, remember that the best way is to test and prove your fault first—then start hacking away at components.

If it is essential to make proving tests at component junction points, but then by doing so the presence of the component affects the meter reading —as when a test for a leaky capacitor is spoiled by the shunting effect of a resistor—then it may be legitimate to break the circuit.

This can be done by cutting through the foil with a sharp blade, and lifting it slightly at the cut. Do not scrape and scratch a path wide enough to drive a bus through, and avoid making this type of test unless no other method avails.

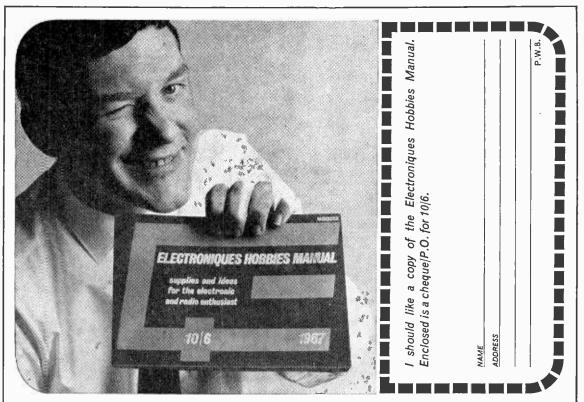
After each test, remake the broken foil with a 'bridge' of solder. (Hence the need to avoid wide

Printed circuits do not necessarily eliminate conventional wiring!



Poor joint, where tag of potentiometer or switch is strained away from the print. Note proximity of fixing screws with printed foil; always check that insulating washers are refitted.

Look for joints of flyleads with printed circuit.



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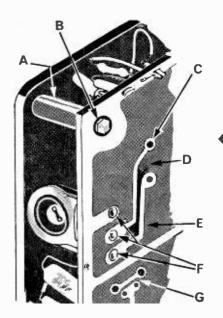
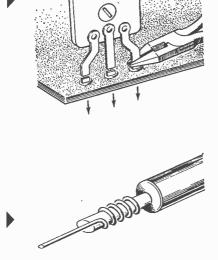


Fig. 4: Cut off lug ends and clean out holes to refit component.

Fig. 1: Printed circuit danger spots. A—strained board where large components are fitted; B—poor return path at fixing bolt; C—end of soldered part (dry joint); D—charred board between conductors; E—lifted foil; F—control mounting; G narrow gap between conductors. Also hairline cracks.

Fig. 5: Make extension "bit" to reach awkward spots. Wire can also be looped around a meter probe to gain access to remote points.



breaks—the joint is always the weakest link in the circuit.)

★ BREAKS IN PRINT

Where there are breaks in the print, as can happen when a board is flexed or a component strained, these mst be bridged strongly. If the break is the most common type, a hairline, simply scraping the foil clean at each side and soldering over the break should be sufficient. Try to avoid lifting the foil while doing so and do not apply the heat for too long. But where the break is more awkward, as, for example, when a burnout has charred adjacent regions of the board, other methods are needed.

A charred board may provide a conducting path for current, no matter how well you try to clean it. In this case, open circuit the print path at each side of the charred portion so that no current reaches it, then provide a wire link. These 'jumpers' are best fitted from existing joint to joint, rather than soldered to stretches of the foil, where the weight of the new wire may tend to lift the thin foil and break the bond.

A common place for breaks to occur is at the anchor post of a large component, such as a potentiometer or switch. The more physical movement that is applied to this portion of the circuit, the more it should receive close attention—no matter how good the print appears to the naked eye. This

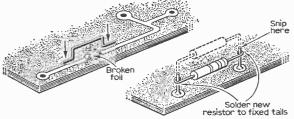


Fig. 2: Bridge joint with new section of wire. Avoid loose ends of foil and apply as little heat as possible to prevent broken ends from lifting.

Fig. 3: Solder new component to existing tail ends to avoid disturbing print.

is where the watchmaker's glass advocated in Part 2 comes in handy.

Fitting a new component can be awkward, especially in the last-mentioned case. Even the removal of the faulty part presents a problem. The technique with multi-tagged components is to melt the solder around the tag and, as it begins to cool, brush it away.

★ SOLDER TECHNIQUE

The trick is to catch it at just the right heat when the solder brushes away in a crystalline form that will not stick to other parts of the circuit. Let it get too hot—and you will have a short-circuiting streak across adjacent foil paths; not hot enough — it merely makes an unsightly mess around the tag.

When the surplus solder has been removed, the tags may be eased gently as heat is applied until the bond on all is broken. Then it should be possible to remove the component.

Of course, the correct way is to remove this surplus solder by the proper device, such as an aspirated solder gun, which Philips patented a few years ago, and which has proved such a boon to professional service engineers. But the average chap can hardly justify the expense for the odd occasion he may need it. In this case, he should weigh the cost of a new component, make sure the part he is removing is not needed again, and destroy it to make for easy removal!

This is not so daft as it sounds. It is far easier to remove the tail end of a resistor or capacitor, or the spade end of a switch or potentiometer lug, by first cutting the component away close to the top of the board, then melting the solder at the joint and withdrawing what is left. A good pair of pointed-nosed pliers or strong tweezers aid this operation.

When replacing a component on a congested board, it may be easier to fix the new one to the existing tail ends than to clean out joint holes and perhaps have force the new part in place.

An example is the larger resistor that takes the place of the maker's special miniature type that has been proved faulty. Cut off this time with a slightly longer tail, twist the ends of the new component into anchor loops and quickly solder these to the tails.

It helps to tin the loops first, and perhaps scrape the tails to remove varnish or oxidisation. Do not apply heat too long, or the joint where the tail is fixed may be weakened. This method is especially handy where it is difficult to get at the rear of the printed circuit board.

★ REPLACING COMPONENTS

Where there is insufficient room to mount the new component, consider the ruse of standing it vertically, with one end through the nearest convenient hole from which the old one has been taken, and the other end insulated by a short length of sleeving if necessary and bent to enter the other hole. Make sure there is enough 'headroom' for the board to be remounted—it is very easy to get caught in this way.

When it is possible to get at the anchor points and completely remove the old component, the next problem is in cleaning out the holes for the new one. Again, remove as much surplus solder as possible. Remember that solder once heated, cooled and reheated is much weaker than new.

Then sharpen a match-stick or, better still, an orange-stick from her ladyship's manicure set. Use the point to delve into the hole while heat is applied. As the solder cools, it will not stick to the wood, and a good, clear hole is left.

Refitting the component is a matter of convenience and taste. It may be found helpful to bend over the ends to make a more solid joint with the foil, but usually it is better to let the solder 'dome' over the tinned end of the lead-out wire. If removal ever becomes necessary again, you can save yourself a lot of snipping and avoid ruining components by adopting this method.

Ideally, the printed circuit joints, when remade, should be treated again with varnish to prevent corrosion, oxidisation, etc, but this is a counsel of perfection—necessary on professional equipment; an added refinement at home.

★ VALVE BASES

Previously, we mentioned the device of easing out multi-tagged components by clearance of old solder.

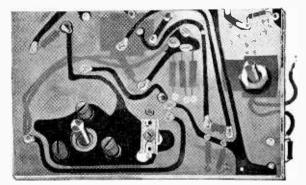


Fig. 6: A bench light can be used to aid circuit tracing wired components will be seen "through" the panel. But avoid overheating components.

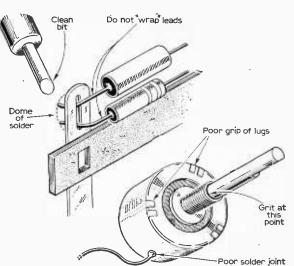


Fig. 7: Make straight joint through lug and allow solder to run on cleanly from a well-shaped iron bit.

Fig. 8: Look for poor jointing of potentiometer cases and, if necessary, make fresh chassis returns.

This may prove extremely difficult in—for example —the case of a damaged valve-base.

Here, a soldering iron that would melt all the tags simultaneously and allow us to lift the base clean away would be ideal. But as sizes of parts vary so much, marketing such a device would not be likely to excite great sales. Nevertheless, somewhat similar devices *are* on the market—but we can make our own for the odd occasion.

Use a fairly heavy gauge copper wire, bend it carefully to form a loop that touches the required joints, then bring up the end to loop in a coil around the bit of the soldering iron.

Heat is transferred from the bit to the copper wire loop and with a little practice, quite good clean removal jobs can be done. Similarly, where it is necessary to get between closely confined components, where the bit of the iron is likely to damage them, use a coiled length of copper wire, 16 or 18 s.w.g., and straighten the end to form a thin auxiliary bit.

★ SEE-THROUGH BOARD

When fault tracing, the tedious business of following twisting lines of print and identifying the components on the other side of the board, can be eased by using a light at the opposite side of the board and getting a kind of X-ray picture of the layout. Many boards of laminated phenolic construction lend themselves admirably to this practice. Older types are usually too opaque.

Often, when wiring in new components, the unavoidable difference in size and shape prevents us from following the set-maker's original layout. In these cases it is quite legitimate to make a 'suspended joint', where two components meet and are connected together. This, despite the cry of 'botchers' from so many practicing servicemen, who have been brought up on the method of ordering the exact replacement from some far-distant manufacturer and keeping the customer waiting while it is obtained.

No wonder some far-sighted firms make fortunes

by marketing "general replacement" parts. (Readers who have not seen the *Electroniques* manual may perhaps be surprised to know what a very wide range is covered.)

★ ANCHOR POINTS

Making soldered joints to tags, lugs and anchor points can be difficult, and the practice of wrapping lead-out wires twice around the gasworks and home before soldering is to be deprecated. Anyone who has had to dismantle many of these joints in congested equipment, where sleeving unravels like snow in the sunshine, will sympathise with this point of view.

A wire end put through the lug and perhaps bent over slightly to aid keeping it still while soldering is all that is needed. A good soldered connection *is* a good mechanical joint. The secret is to keep your iron clean, apply the right heat for the right length of time, and use a good resin-cored solder. Not please not—the corrosive tinman's flux that dad left in the potting shed. Solder is cheap enough, and the little extra time and care at the preparation stage saves hours of fretting later.

★ CLEANING

Other odd chemicals that are to be shunned are the solvents and cleaning fluids that some folk appear to have used on printed circuits. Even carbontetra-chloride, which has a great many cleaning and degreasing uses, and was once the standby of all who wanted to 'lubricate' a volume control, can be dangerous. Apart from its toxic effect—fumes should *never* be inhaled—it can cause many types of plastic to soften and run.

For cleaning plastics, methylated spirit is safer, and in some instances an impregnated wadding (again borrowed from her ladyship's silver or brasscleaning cache) will give a good burnish.

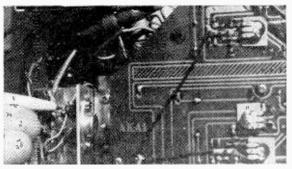
But for degritting controls and for cleaning switches, the proprietary chemicals that were mentioned in Part 2 simply cannot be beaten. If they will not do the job, the control is due for replacement anyway!

Sometimes, it is difficult to get at the inside of a potentiometer to apply the cleaner. Many plastic edge-type controls, for example, appear to be completely sealed. In these cases it is quite legitimate to drill a small hole in the side casing and inject through this. After allowing the necessary evaporation time, the hole could be resealed to prevent dust entering.

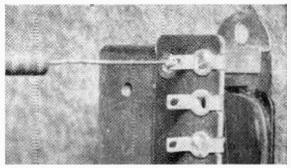
***** NOISE FAULTS

A popular place for noise faults is at the junction of spindle and bush of a 'conventional' volume control. One tape recorder manufacturer realised this very early on and provided a spring clip that separately earthed the spindle. Where movement noise is bothersome, a drop of switchcleaner run down the spindle at this point may help. Remember, only a drop—don't drown it.

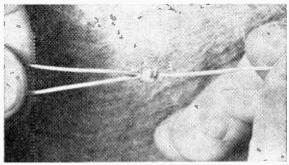
Another popular place for noise to originate is



Example of typical printed circuit layout, where the output transistors are mounted on a separate sub-chassis, which acts as a heat sink. Note the use of a jumper wire for interconnection of sections of the main printed circuit.



A simple hook is often more effective than a bulky, wrapped joint.

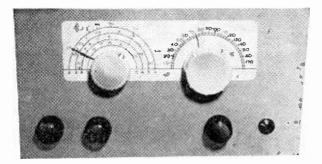


Wire ends of components can be joined firmly by inserting them in a twist or coil, where size of replacements precludes exact fitting.

at the 'earthing' point on the body of a control. This applies also to some types of switch. The connection may be firmly soldered, but if you inspect the control closely you will note that this is to a shell, and the shell makes contact with the bush by a bent-over clamp. And time and heat may have worked its insidious depredations at this point.

So clean off the control at the junction of parts and solder the contraption together. It is surprising how many hum troubles in audio equipment have been cured by this ruse.

This article concludes the first section of this series by H. W. Hellyer and Gordon J. King. The second section will begin publication in about three months time, when the emphasis will be on transistor equipment.





HIS superhet receiver tunes approximately 10-600 metres in four bands. It has only three valves—frequency changer, regenerative 1.6 Mc/s i.f. amplifier and detector, and output stage. This, and the use of a panel aerial trimmer, practically removes any alignment or trimming difficulty, while providing good sensitivity. Tested at 14Mc/s, a 3μ V signal at the aerial was just audible in the loudspeaker. Due to the relatively high intermediate frequency, there is good freedom from second channel interference from unwanted transmissions.

Fig. 1 is the circuit and a few points should be noted. VC1/VC2 is the ganged tuning capacitor, and though a value of about 315pF is specified a someat about half capacity. The panel trimmer VC3 is then adjusted as necessary for maximum signal strength. VC4 is for bandspreading, and useful for amateur and other congested bands. A 10pF, 15pF or 20pF capacitor is most suitable. Should a 2-gang capacitor be to hand, its sections can be connected in parallel with VC1/VC2.

OSCILLATOR PADDER

Each oscillator coil requires its own padder. Range 2 is approximately 515-1545kc/s and has a 100pF padder connected to tag 2 of the holder, range 3 is about 1.67-5'3Mc/s with 350pF padder to tag 3, range 4 is 5-15Mc/s with a 1000pF padder to tag 4,

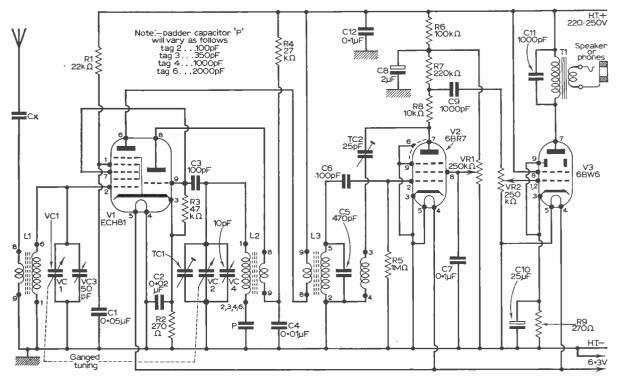


Fig. 1: Complete circuit of the receiver. The capacitor Cx is optional and is discussed in the text.

what larger value can be fitted with no loss of efficiency. The one fitted had an integral ball drive, but a separate drive and scale would be in order. Trimmer TC1 serves for all oscillator coils and is left and range 5 10.5-31.5 Mc/s with a 2000pF padder connected to tag 6. These values are easily obtained and not exactly as specified for the coils, but are suitable with TC1 and VC3 adjusted as explained.



AHAM

REGENERATIVE I.F.

The grid circuit of V2 is permanently tuned to about 1.6Mc/s. Regenerative feedback is applied through TC2, and controlled by VR1, and as the grid circuit is not variable tuned, frequent adjustment of VR1 is not required.

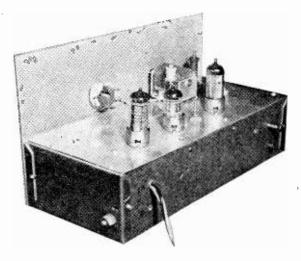
With V2 somewhat below the critical point at which oscillation nearly arises, the receiver has good general sensitivity and selectivity. As VR1 is advanced a point is reached where both selectivity and sensitivity to weak signals greatly increase—this is the optimum setting of VR1 for speech and music (telephony). Turning VR1 further causes a heterodyne, and allows reception of Morse (c.w.), single sideband (s.s.b) transmissions can also be resolved with some adjustment of VR1, unless rather powerful. If too strong, reducing sensitivity with VC3 helps.

VR2 is an audio gain control, and either speaker or phones can be plugged into the panel jack. The ratio of Tr1 is not correct for phones, but as V3 can provide much more power than wanted this does not seem important. Low or medium impedance headsets are best, but high impedance phones can be approximately matched by using a second output transformer (same ratio as T1), with low impedance winding connected to the jack plug, and high impedance winding to the phones.

The receiver runs from a separate power pack. Heaters require 6.3V at 0.9A and the bt drain is about 50.6

h.t. drain is about 50-60mA, at 220 to 250V (max). The power pack must have a mains transformer which provides h.t. and l.t., so that the receiver is completely isolated from the mains.

Positions of valveholders and other items can be seen from Fig. 2. Chassis dimensions could be modified somewhat. The large holes are best made by drilling a small pilot hole, and using a valve-holder punch. Mark through valveholder lugs and drill $\frac{1}{8}$ in. holes for 6BA bolts.



THE I.F. COIL

This is screened by the aluminium can in which it is supplied, and screening is essential. The bottom of the can is drilled to clear the threaded portion of the coil, and five small holes are also drilled $1\frac{1}{4}$ in. from the bottom, so that leads may pass through as in Fig. 3. Capacitor C5 is wired across the pins inside the can.

The i.f. coil tunes about 1.4-1.7Mc/s by adjusting its core, and the best frequency is around 1.6Mc/s. A nut locks the core, as moving it alters tuning

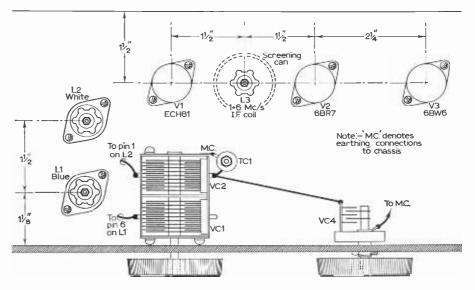
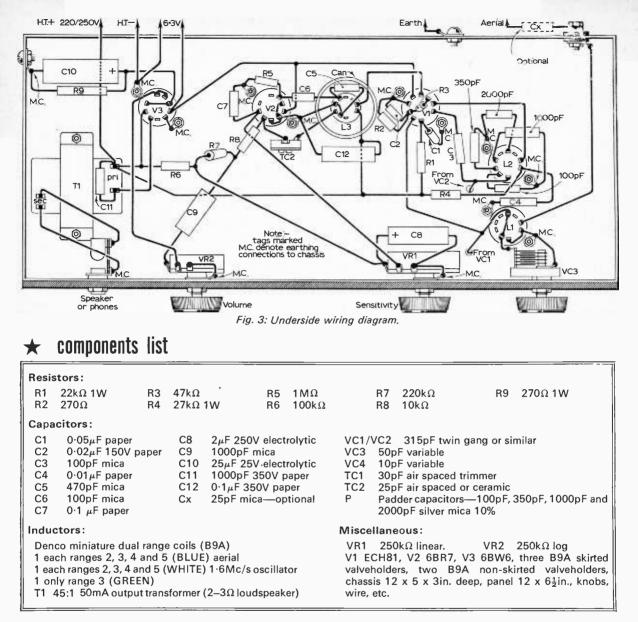


Fig. 2: Above-chassis layout and main drilling dimensions.

calibration. TC2 may be suspended by wiring if short, stiff leads are used.

For best results on range 5 (10.5-31.5Mc/s), leads to variable capacitors, V1, coil holders and the padder capacitor should be short and direct. The aerial socket must of course be insulated from the chassis, or an insulated flexible lead can be taken directly from tag 8.

By-pass capacitors C1, C2, C4, C7 and C12 could be modified somewhat, and the voltage rating is



unimportant, provided it is higher than the voltage present. C8 could be 8μ F and C10 50 μ F if to hand. C9 can be 1000pF (0.001 μ F) to 0.01 μ F, but should be mica. VR2 may be 500k Ω , C11 may be 5000pF (0.005 μ F) or even 0.01 μ F.

Connections from tag 2 of V2 to C6 and R5 must be as short as possible and clear of heater wiring or hum may arise. Components and wiring associated with V2 and V3 are best close against the chassis.

ADJUSTMENTS

Insert V2 and V3 and VR2 at its maximum clockwise position. Temporarily place the aerial lead near the connection from pin 8 of the i.f. coil. Open TC2 fully, and adjust VR1 for maximum sensitivity. This is *not* the fully clockwise position, but an intermediate one giving the most suitable G2 voltage, and will be shown by maximum background noise, or possibly reception of a transmission which can be tuned in by rotating the i.f. coil core. Close TC2 until oscillation just begins, which can be prevented by turning back VR1 slightly.

If TC2 is at too high capacity, oscillation arises with a much lower G2 voltage than optimum, so sensitivity is reduced. Rotate the i.f. coil core to find a spot where no transmission is received. If a signal generator is available, this can be found near 16Mc/s. Otherwise adjust the core so that all the brass thread is above the chassis, then slowly screw it down until a position is found which gives no direct reception at the intermediate frequency. Such reception is untunable during normal operation of the receiver, but is avoided by screening as described, and by keeping the aerial away from C6 and associated wiring.

VR1 and VR2 should be turned back somewhat, VI and a pair of coils inserted, with TC1 set about half closed. Any transmission tuned in should peak up for maximum volume when VC3 is rotated. VC3 should be neither fully open, nor fully closed, this giving maximum efficiency on all frequencies. If it is found that the required trimming adjust-

ment falls outside that available by means of VC3, towards the low frequency end of any band (VC1/ VC2 closed) adjust the coil cores until this is prevented. The best position is that which allows tuning from one end of the band to the other without any need to re-adjust VC3, except for optimum possible reception of weak signals.

If a signal generator is available, band coverage can be set by rotating the cores of the oscillator (white) coils. The aerial (blue) coils are then ad-justed for best results. Should VC3 need to be fully open at the high frequency end of any band, this can be corrected by slightly screwing down TC1.

If the aerial is very long, results may be improved by placing a small capacitor (Cx) in series. A 25pF or 50pF pre-set capacitor should be satisfactory, or a small fixed component can be tried. This allows the aerial circuit to tune more sharply, and avoids overloading V1 or V2 with strong signals.

For normal reception, VR1 can be placed so as to give good results, and tuning carried out with VC1/ VC2. But for weak signals it will be found that critical adjustment of VC3 and VR1 makes a considerable difference.

For general short wave reception range 4 is most suitable. Range 3 includes the 1.8-2.0 and 3.5-3.8 Mc/s amateur bands, and other transmissions. Range 5 covers frequencies often capable of long distance results. Range 2 permits usual medium wave cover-age, if wanted. A good earth improves reception, though long distance reception is possible without an earth.

PRACTICAL ELECTRONICS

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SEPTEMBER ISSUE on sale AUGUST 11-2/6

MINIATURE STABILISED POWER SUPPLY

—continued from page 324

enable the component assembly to drop easily into place.

\star components list

- R1 470Ω ±10% ±W
- C1 200µF 16V electrolytic
- 200µF 16V electrolytic C2
- 200µF 16V electrolytic **C**3 Tr1
- OC35 (recent manufacture) D1
- RS310 S.T.C. or similar silicon rectifiers D2
- OAZ207 9.1V 250mW silicon zener diode D3 (Mullard)
- Small bell transformer with 5V tap (Friedland T1 Lilliput)

Veroboard, battery connectors, etc.

One of the silicon rectifiers connects at its negative side to the collector tag. The flange on each rectifier corresponds to the cathode in a thermonic rectifier and is the positive end.

A red spot on the zener diode indicates the lead that is to be connected to the positive side of the supply.

The 200µF capacitors are mounted in line with the zener diode and rectifiers on the inside between them and the power transistor. The negative lead of each capacitor is bent over and brought down the side of the capacitor so that the two leads can be inserted into adjacent holes on the board. The capacitors should be insulated with plastic sleeves.

AN ANNOUNCEMENT

The field of television is an interesting and varied one. For enthusiasts with an inquiring mind, and this will include almost all our readers, we recommend the next issue of Practical Television which is on sale August 18th.

Practical Television features articles on aerials. signal boosters, test equipment and in fact just about everything in the field of television.

A current series of articles discusses colour television in down-to-earth terms. Articles in line for publication include a study of interference, reports on the latest colour TV receivers, and even how to connect headphones safely to vour TV.

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CONNECTOR BLOCK CIRCUITRY

A PROBLEM which is very often encountered when assembling a radio receiver, amplifier or other piece of equipment, is that of quickly substituting differing values of resistors or capacitors, or making wiring alterations to one or more sections of the apparatus under construction in order to observe the effect and to achieve optimum working conditions. In the "Good Old Days" (actually a little before the writer was old enough to pursue this fascinating hobby of radio) when all components had large brass terminals and were connected up by means of thick chunks of copper wire, it was a simple matter to carry out alterations to components or wiring.

There is available to the constructor now a very suitable alternative form of "terminal" in the form of polythene connector blocks. These are available in various forms, the most popular being of 2 amp current carrying capacity, obtainable as blocks containing 2, 3, or 12 connections. Each connector comprises a small brass "coupling" into which wires can be pushed from either end, with two small grub screws provided to secure the wires. The whole is embedded in solid polythene, screw holes are provided in the polythene by means of which the blocks can be secured to any mounting surface, and as the polythene is an excellent insulator, these blocks can be secured directly to an aluminium chassis without any risk of short circuits. The "12 section" blocks can be cut with a sharp knife or razor blade to any desired length and hence the number of connector points adjusted to suit the constructor's needs of the moment.

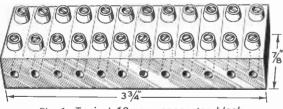
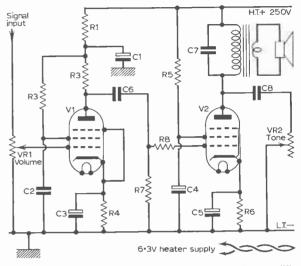


Fig 1: Typical 12-way connector block.

The obvious use for connector blocks is, of course, as a ready means of quickly connecting together the various separate units of a receiver or amplifier (where unit construction is adopted) such as the power supply unit and amplifier; provided the connections are plainly labelled on the chassis adjacent to the connector block, a ready means of feeding in heater and h.t. supplies from a power unit is provided.

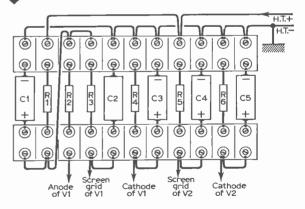
A more novel use for connector blocks has

J. B. WILLMOTT, A.I.P.R.E.



🔺 Fig 2: Theoretical circuit of simple audio amplifier

Fig 3: Suggested connector block layout of Fig 2. R7, R8, C6, C7 & C8 are not mounted on tagboard—see text.



recently been adopted by the author when constructing experimental gear; instead of using paxolin tagstrips or tagboards for securing resistors and capacitors, a double line of polythene connector blocks spaced some $1\frac{1}{4}$ in. apart forms a very effective substitute (see Fig. 3). The measurements of a 12-section connector block are $3\frac{1}{4}$ in. long by $\frac{7}{4}$ in. wide, thus it is possible to place the two parallel blocks with $1\frac{1}{4}$ in. clearance between them in an overall space of $2\frac{1}{4}$ in., which in turn means that they can be mounted on the $2\frac{1}{2}$ in. deep side runner of the popular range of aluminium chassis, and leave just enough room for the external connections to the blocks without protruding above the level of the chassis walls.

Before attempting to wire up a piece of home designed equipment, work out carefully from the theoretical circuit diagram which components can be conveniently mounted on "tagboards" and hence the number of "ways" required on the tagboard(s). Remember, intervalve coupling components, grid resistors, grid stoppers and other similar signal carrying portions of a circuit should not normally be mounted on tagboards, as this introduces longer connecting leads and more risk of instability and interaction between wiring than can be tolerated. Such components should always be wired up by the shortest possible leads between the valveholders, etc. Decoupling components, bias resistors and by-pass capacitors can nearly always be mounted in groups without ill effect. A typical example is given in Fig. 2 of the circuit of a simple two-stage a.f. amplifier (no component values are given as obviously these will depend on the types of valves involved and the h.t. voltage supply available), and in Fig. 3 a suggested arrangement for mounting resistors and capacitors on a connector block "tagboard" of the type described, which it will be noted requires the use of an 11-way "board".

When the project has been completed, and found

Book Review

MATHEMATICS FOR RADIO AND ELECTRONIC TECHNICIANS By Dr. -Ing Fritz Bergtold. Published by George Newnes Ltd. 304 pages. 8½ x 5½in. Hard Covers. Price 50s.

HE title is no idle boast. Too often, books on mathematics are the stale, rehashed collections of formula.... three men working for seventeen hours dig a trench twelve feet long by ... This book aims squarely at the radio and electronic technician and hits bang on target. Every example, description of method, formula or fact has a bearing on the subject.

This second edition has been re-written in consultation with practising engineers and mathematicians, particularly in semiconductor development. Thus, we find technical terms relevant to our subject continually cropping up, being explained and subsequently worked into the text. Much hard cogitation has obviously gone into such styling.

Beginning with simple equations and the technique

IN-LINE AUDIO A.G.C. UNIT

Two of the illustrations in the article describing an in-line audio a.g.c. unit, published in the July issue, were incorrect. In the circuit diagram (Fig. 2) on page 204 the emitter and collector symbols for Tr2 are reversed. The emitter should be towards the negative line as this is an n-p-n transistor, with the transformer as the collector load. The other error concerns the same transistor, but on the component layout (Fig. 3): the diagram is correct, but the letters identifying the collector and emitter are reversed. to be in working order, experiments to find the optimum value of resistors (or capacitors) can be readily carried out, changing one component at a time. For example, if one started off with R1 a 1M Ω component, the effect of altering this "up" to $1.2M\Omega$ or $1.5M\Omega$, or "down" to $68k\Omega$ or $470k\Omega$ for example, can be tried out. It is surprising what a difference in overall performance can be made in quite a simple piece of equipment by experimenting on these lines.

The connector blocks referred to can be obtained from several component suppliers advertising in this magazine, and also in good D.I.Y. shops and some chain stores.

Lastly, whilst the remarks in this article have been primarily concerned with valve circuits, there is no reason why similar principles should not be adopted in experimental transistor work (provided space is not of prime consideration). A very quick means of "hooking up" transistors and their associated components is afforded.

One final word, whilst it is not really intended that these connector blocks should replace tagboards, etc., in permanent equipment, the author has found that provided the grub screws securing the component wires, etc., are tightened firmly home, there has been no noticeable deterioration in performance as compared to equipment wired by conventional means with 100% soldered joints, even after long periods of use.

of numbers and the use of symbols, the 24 chapters work through basic algebra, powers, curves and their uses, more detailed functions of x, logarithms, trigonometry, Fourier and other series, differentiation and integration, series, polar co-ordinates, vectors and complex calculus.

Right in the middle we find a brief refresher. Ch. 9 deals with "Some Peculiarities"—wise words of advice on the need for accuracy and the use of approximation, with handy notes on signs. The next chapter is a beautifully concise work on powers, exponents and the slide rule.

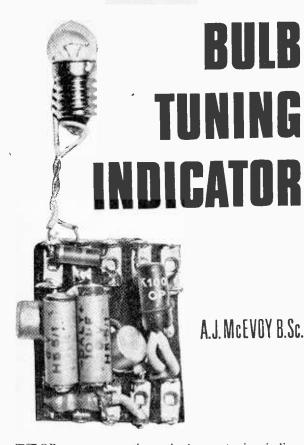
Intended as a supplement to the deeper textbooks in electronic technology, no specialist knowledge is needed. Taking the book as a course and reading for an average of a half-an-hour a day, the technician who has grown stale can refresh himself and should undoubtedly advance his knowledge at the same time.

The emphasis is on worked examples and these are directly aimed toward the student's chosen field. For the reader who thinks mathematics a dull and difficult subject, this book will come as a welcome relief.—H.W.H.

Practical Wireless Binders

A first class magazine deserves first class treatment. Store your copies of *Practical Wireless* with a new Easi-binder, specially designed to hold 12 copies of the new large size. It has a special pocket for storing those blueprints and data sheets too. Yours for 14s. 6d. from: Binding Dept., George Newnes Ltd., Tower House, Southampton Street London, W.C.2.

Note. Please state the volume number required otherwise a blank cover will be sent.



Ror many years the cathode ray tuning indicator has been the accepted way of presenting visually the amplitude of signals in valve circuits. The constructor will be familiar with its use in radio sets to indicate tuning accuracy, and in tape recorders where it provides a clear warning of any overmodulation of the tape by too strong a recording signal.

The device relies on the deviation of an electron stream by a grid whose voltage depends on the strength of the signal, with the result that the pattern of the glow produced when the stream falls on a phosphor like that of a TV tube, is shifted in proportion to the signal. Such a device is obviously unsuitable for applications in transistorised circuitry, where there is no heater supply available for a filament to emit the electrons, and no high voltages to focus them into a beam. Admittedly, a few transistorised tape recorders have obtained sufficient h.t. to operate a miniature cathode ray indicator (the DM70), most manufacturers have fallen back on the use of small meters.

The circuit to be described was developed to supply the need for a low-voltage low-current visual display of signal strength without resorting to a moving-coil meter. Since any system involving cathode rays is excluded by power requirements, some other light source is necessary. Photoemissive diodes are still too expensive, though very attractive from the point of view of circuitry, so the only possibility was the old-fashioned filament bulb. A system which merely varied the brightness of a bulb would not be a definite, or even attractive, indicator, and there is the additional disadvantage that the current drawn by a bulb would be twice that of the radio or tape amplifier for which it served as indicator! It was therefore decided to develop a circuit in which the bulb would flash on and off at a rate depending on the signal strength. This holds the extra advantage that the current is reduced to a fraction of that of a continuously-glowing lamp. The familiar multivibrator circuit can be set up to switch the bulb on and off at a suitable rate, this frequency being controlled by the time constants of the R-C circuits in each leg of the device.

Circuit description

The circuit finally evolved is shown in Fig. 1. Tr2 and Tr3 will be recognised as the transistors forming the multivibrator, and it will also be noted that they are n-p-n types. Trl, a p-n-p type, forms the resistive element in an R-C timing network with C2. The resistance to which Trl is equivalent, depends on the biasing current supplied at its base, which in turn is set by the input voltage applied through R1. In operation, therefore, the current available to charge C2 is the product of the bias current and the common-emitter current gain of Tr1. Therefore, the higher the bias current, the higher the charging current, and as a consequence, the shorter the time required to charge C2, and therefore the higher the repetition frequency of the multivibrator. Tr1 also functions as a buffer between the multivibrator and the signal source; otherwise there would be some direct connection between these, and as well as the reference voltage being supplied to the multivibrator, high harmonics of the multivibrator frequency, extending into and beyond the audio range, would be forced back into the reference circuit.

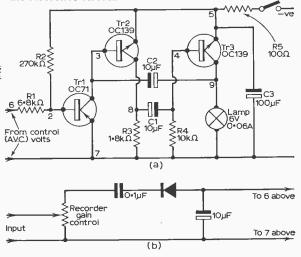


Fig. 1(a): Basic circuit of the tuning indicator unit (numbers denote tags on groupboard—see Fig. 2). Fig. 1(b): Extra circuitry to obtain control d.c. in a tape recorder.

Most transistorised apparatus as yet available relies on germanium p-n-p transistors, and it is the positive line which is chosen conventionally as the earth line. This is the reason for the otherwise unusual choice of transistor polarities for the multivibrator transistors. The signal to be indicated will usually be small and close to the potential of the earth line of the set. It will therefore be able to control directly the bias level of Tr1 only if this is a p-n-p device. Similarly, acting as a current amplifier, Tr1 can give Tr2 the necessary forward bias only if the latter is an n-p-n unit.

Control voltage

In the above remarks and in Fig. 1, it is assumed that the signal is applied to Tr1 in the form of a d.c. voltage proportional to the strength of the audio component in the circuit. This is the case in a radio set, in which the appropriate voltage to indicate is that of the a.v.c. line. This is obtained from the d.c. component of the output from the detector diode, which is arranged to be positive-going, beyond the potential of the earth line. The first i.f. amplifier, receiving its bias current from a potential divider connected to this line, is then biased back and its gain reduced. If Tr1 is then connected through R1 to this line, it follows that, when the set tunes in a signal and the a.v.c voltage builds up, its base will go more positive, and its bias current will fall. Between collector and emitter it will then be equivalent to a larger resistor, since there is a lower current for the same applied voltage. The time constant is increased, and the frequency reduced. Visually, this means that, as a station is tuned in, the bulb will flash more slowly; if the constructor wishes, R1 may be reduced until it stops completely on the strongest local stations.

Audio equipment

It was also mentioned that the circuit is a suitable indicator for audio equipment and tape rerecorders; in these, however, there is not usually a convenient d.c. potential proportional to the volume level, analogous to the radio set's a.v.c. Fig. 1b shows the modification to the circuit of Tr1 to operate off the signal as it appears on the volume control of the recorder. According to the sense of the diode D1, the rate of flashing may be either increased or decreased. It is convenient with tape recorders to use for R1 a value of resistor which just suppresses flashing at the onset of overloading of the amplifier. This can be as clear and definite an indication as the closing of the display of a cathode ray device on a mains recorder. The constructor might choose to replace R1 with a preset potentiometer in order to achieve best results. Finally, should it happen that an indicator is required for a radio or amplifier using n-p-n transistors and a negative earth, it is only necessary to change Tr1 for n-p-n, and Tr2 and Tr3 for p-n-p types.

Construction

Construction of the indicator is simplicity itself, even for the beginner. Fig. 2 shows the arrangement of one prototype, on a ten-way group board. Even without miniature capacitors it measures only $1.5 \times 1.2 \times 0.5$ inches. A decoupling resistor and capacitor are added in the supply line to prevent

\star components list

Resistors

R1	6·8kΩ	R4	10kΩ
R2	2 70kΩ	R5	100Ω
R3	1·8kΩ		
All 1	0% 1 W		

Capacitors:

C1 10µF 9V electrolytic

- C2 10µF 9V electrolytic
- C3 100µF 9V electrolytic

Semiconductors:

- Tr1 OC71 general purpose p-n-p
- Tr2 OC139 audio n-p-n
- Tr3 OC139 audio n-p-n

Miscellaneous:

Lamp 6V 0.06A, miniature 5-way tag board, wire, etc.

any noise from the multivibrator, blocked by the buffer action of Tr1, from entering the audio amplifier through its power supply.

The circuit diagram is numbered corresponding to the tags on the board to assist in identification of the components during construction.

One final point deserves consideration-the

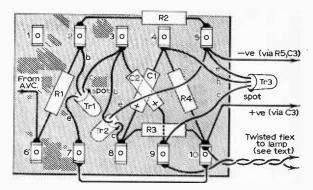


Fig. 2: Groupboard showing layout of components—note that C5/R3 are mounted externally but, this is not essential if a larger (ie. 12 or 14 way) groupboard is utilised.

mounting of the indicator in the set. The lampholder-a standard m.e.s. type-is fixed at some convenient position on the front of the set, so that the bulb is visible through an aperture which, for appearance's sake, may be covered with a coloured plastic disc. However, the leads from the unit to the lamp should be twisted, in the same way as heater leads in valve amplifiers, and for the same reason, namely to prevent noise being induced into signal circuits. The location of the group board is not critical, but should clicks be heard in the speaker as the lamp flashes, the cause is probably the proximity of the multivibrator to a tuned circuit, and relocation will solve the problem. For battery economy a switch may be built in to save the 15mA. of the indicator circuit when listening for long periods to a single station. At other times the circuit is switched in, if only to serve as a dial light.



No. 36

l'll Warrant You !

HERE is something impressively legal about the usual form of guarantee. With its archaic script, pretty red seal and clauses of small print, it is more suited to frame and hang on the wall than file in the bureau. And for all the good most of them are, they might just as well be used for decoration.

Nowadays, we are conditioned to want some sort of assurance that goods are better than we should deserve. The goggle-box nightly churns out these assurances. "Splosh washes cleaner", "Use Rubbit for the Deep-Down-Glow", "Pablum is better than ordinary bread". But . . . Cleaner than what—sand and pebbles? What if we only want a common surface shine? And, surely, this is ordinary bread?

We find the same thing in the press. The cleverer copy-writers cash in quickly with those intriguing advertisements that begin: "Well, perhaps we DON'T make the fastest petrol" or the intellectual ones that waffle on for half a page about something apparently irrelevant so that one congratulates oneself at the end for discovering the business of the advertiser.

So it is with guarantees. This week I broke my trusty electric shaver—trying to save the cost



Cropping the back-growth.

of a visit to the barber by cropping some of that back-growth, my wife said. She brought me a packet of emergency wet-shaving blades and stark across the inevitable plastic cocoon was the glaring red slogan, "Guaranteed".

What would happen if I sent one of the treacherous things back because my pampered beard refused to succumb and supplied bloodstained skin shavings as evidence? Would the guarantee be honoured? Or would I be referred to some obscure item of small print that I had carelessly cast away with the wrapper?

This, roughly, is the position when one buys a bit of radio equipment. Twelve Months Guarantee, says the dealer, and we go off all unsuspecting. Then discover, if things go wrong, that the small print has absolved the maker from practically every hazard except an act of God.

Guarantees do not cover service charges. Time, trouble, labour, S.E.T. and other evils, make the dealer unduly avaricious. When we take our faulty radio back to his shop, he is perfectly entitled to charge a normal fee. Often he does not.

He has no hope of recouping losses from the manufacturer. Even the brand new models he has had to repair before he dare put them in his window carry no extra bonus for his service. Some makers talk airily about "discounts covering the cost of minor adjustment," and we can guess what our radio repair man says about that. Small wonder he sometimes describes himself as the manufacturer's final inspection department.

The contractual element enters more strongly when we buy our equipment directly from source.

"Provided the card is filled in and returned within seven days." Did we remember to date it correctly? Dare we update it, or will they check? Can they check?

Supposing we did remember to



Unfortunate experience with the cat.

post the darn thing off. "The Superspecial shall have been used strictly in accordance with the instructions." Does that exclude the time we lent it to Aunt Mabel who had that unfortunate experience with the cat? "The Superspecial must not have been tampered with, dismantled or subjected to misuse."

And, to cap it, we are solely responsible for packing charges and insurance, it seems. We remember what happened to that Christmas parcel; the forms we had to fill in to convince the GPO that we had not been sending contraband. We recall the tales of hijacked goods wagons, of large-scale pilfering, the Great Train Robbery, flood damage, fire . . In the end, we probably settle for a quick repair by the little man around the corner.

But fate still dogs us. When the set comes back it bears a label: "Three Months Repairs Guarantee." We congratulate ourselves on a new lease of life and when the thing goes wrong a week later march back with confidence oozing from our ears.

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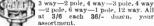
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With Capstan control. This unit is extremely well made and imeasures approx. 6 x 5 x 2in. deep. Has three piano key type controls for Record, Playback and Rewind Motor is a special neary duity type intended for operation off 4/5 volts. Supplied complete with 2 spools ready to install. Record, Replay head is the sensitive M4 type intended for use with transistor amplifier. Price 44.15.0, Post and insurance 4/6.

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1μF	10 volt	4μF	4 volt	16µ.F	30 volt	64µ.F	10 volt
1μF 1μF	15 volt 40 volt	4μF 4μF	12 volt 25 volt	16μ.F 20μ.F	150 volt 3 volt	64μF 100μF	40 volt 3 volt
1μ.F	50 volt	4μF	100 volt	20µF	6 volt	100µF	6 volt
1μF	350 volt	5µF	6 volt	20µF	9 volt	100µ.F	10 volt
1-25µ.F	16 volt	5µF	25 volt	20µ.F	15 volt	100µF	12 voit
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2µ.F	15 volt	6μF	15 volt	25µF	30 volt	200µF	3 volt
2µF	70 volt	6-4µ.F	40 volt	30µ.F	6 volt	200µF	4 volt
2µF	150 volt	8µ.F	3 volt	30µF	10 volt	200µ.F	16 volt
2.5μF	16 volt	8µF	6 volt	30µ.F	15 volt	250µ.F	2-5 volt
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3μF	12 volt	10µ.F	10 volt	40µF	3 volt	320µF	2.5 volt
3µF	25 volt	10µF	12 volt	40µ.F	6-4 volt	500µF	4 volt
3-2µ.F	6 volt	10µ.F	25 volt	50 µ.F	6 volt	640µF	2-5 volt
3-2µF	6-4 volt	12-5µF		50µF	9 volt	750µF	18 volt
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50 for 10, FCF80 FCF80 FCF80 FCL84 FL36 SILICOP organs.1 SILICOP organs.1 SILICOP SIGNAL S	(- Light-sc Televis Trice 7/6 9/- 6/6 7/6 9/- 8/7/6 9/- 9/6 9/7/6 9/- 9/2 9/2 9/2 9/2 9/2 9/2 9/2 9/2 9/2 9/2	Analysis of the second se	ALVES, B PCC24 PY61 PCC29 PCL82 PY81 Accellent detr N H-T. RE Itilve resisto FELMINA F ELIMINA F BUDERING SUBJERS OLDERING SUBJERSUBERS SUBJERSUBJERSUBJERSUBJERS SUBJERS SUBJERS SUBJERSUBJERS	RAND N 6/6 6/- 9/- 7/6 6/- ectors, als CTIFIER rs 9/- eacl TORSs and fuse. oldering 1 5 GUN, 5 ery uselul) £7.10.0 p it to make to comake 16 s 1mA me AND CIR D SCRA' nents and ding lates HALFPFR 10- Ac needles1 S. Fantast crystal S. Fantast crystal an s. 1/-; 100 an 37/6, 12 ch. 8 x 21 ach.	EW AND So suitable S. SPECI/ iame size a 4 amp. 5/1 (rons 25/- e 7/6. assorted f alr. 10/- only. 0/- only. 0/- only. 10/- only. 10/- only. 10/- only. 10/- only. 10/- only. 10/- assorted f is version c CES. All 10/- each. 11c value at 4 dynamic yds. 7/6; 5 11n. Bakers n. 12/6. 2ir 	BOXED PCL83 PCL85 ECC82 PY33 for keying e AL PRICE s PP930/-; 2 volt 55/- ach. Dacks, 6/- e and circuli convert in FER (for i MICRO-6 types below. S Stereo L cos Stereo 12/- each. in stock. 00yds. 25/- Guitar £5.5. B0 ohm 7/	7/6 6/6 9/- ilectronic 5/- each, PP6 20/ each. ach. it to make mproving . World's rat 3/6 ea. P: Studio Sapphire post 4/6; i.0. 6. 50 for 3/7/3
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TUO METRE TRANSMITTER E.G. BAYER G30GR

The I44Mc/s amateur band covers a very wide frequency range compared with the low frequency bands, and crystal control is quite often used offering a simple means of obtaining good frequency stability. In addition to its obvious use on the I44Mc/s band, a transmitter of the kind described here may be adapted for use as a driver, with its output frequency multiplied into the 420M/cs band. The new Class B licence permits operating on frequencies above 420Mc/s without any need to pass the Morse test, call-signs being allocated in the G8 (followed by three letters) series.

Figure 1 is the circuit, V1 using an 8Mc/s 3rd overtone type crystal so that output is obtained directly on 24Mc/s. If the tuned circuit L1/VC1 is tuned for maximum output, oscillation may not recommence after switching on and off, and VC1 is adjusted slightly as necessary to correct this.

V2 triples to 72Mc/s, while V3 doubles to 144Mc/s driving the power amplifier V4 at 144Mc/s ensuring reasonable efficiency. As grid current is very important, VC2 is panel operated, and a grid current meter is included. It is possible to omit this meter, fitting a jack for an external test-meter or similar instrument. If a grid dip oscillator is available this will be very useful to check the frequencies of the various circuits before applying power. Should a g.d.o. not be to hand, tuning up can be accomplished by means of the indicating wavemeter described. Initial adjustments should be made stage by stage, and no h.t. must be applied to h.t.2 until the circuits are correctly tuned. If the coil details given are followed carefully, this should avoid any serious error such as working on the wrong harmonic. The coil details are given exactly as a guide, and this does not mean that somewhat dissimilar coils would not be satisfactory if a g.d.o. can be brought into use to adjust their frequency.

CONSTRUCTION

This is quite straightforward, with all circuits except the p.a. anode and output below the chassis. A piece of aluminium $4\frac{1}{4}$ in. x $9\frac{3}{4}$ in. has $\frac{1}{4}$ in. flanges bent on it, and is shaped to fit as in Fig. 2. The positions of valveholders and other items on the chassis can be judged from Figs. 2 and 3.

Figure 3 is the underside of the chassis. Heater and h.t. leads run close against the chassis. All bypass capacitors are connected with very short leads.

OVERTONE OSCILLATOR

The oscillator is intended for 3rd overtone type crystals, and other crystals may not be satisfactory. With the 8Mc/s overtone crystal, the lowest frequency present is the overtone, or 24Mc/s. The output frequency of the transmitter is approximately x18 the crystal frequency, and crystals can be chosen on this basis.

The position of the tapping T on L1 considerably influences results, and will probably have to be

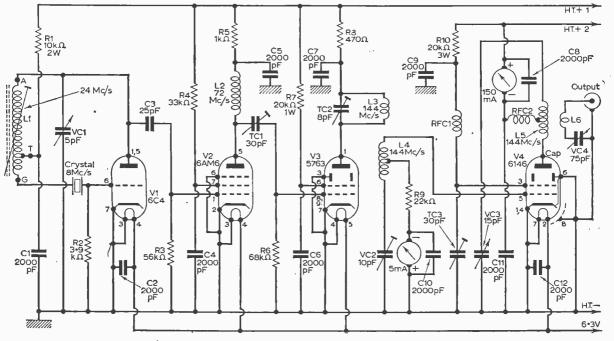


Fig. 1: Circuit diagram of the two metre transmitter.

adjusted to suit the particular operating conditions. If the tapping is too near the grid end G of L1, no oscillation will be obtained. But if the tapping is too near the anode end A, oscillation will continue at all frequencies to which L1 may be tuned. When the tapping is correctly placed oscillation arises only at the crystal overtone.

L1 is wound with 24s.w.g. enamelled wire, on a 9/32in. diameter cored former. There are 18 turns in all, with the tapping 5 turns from the grid or crystal

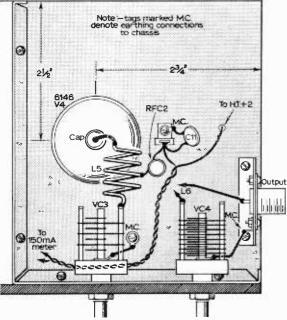


Fig. 2: Layout of the components in the p.a. compartment above chassis.

end, Fig. 4. Some adjustment of the ease with which the circuit oscillates can be made by modifying the position of the core, and restoring tuning by VC1. If a g.d.o. is available, place V1 and V2 in, and set L1 core and VC1 to give resonance on 24Mc/s. Include a meter between R1 and the h.t. line, and apply about 250-300V. Current may be around 10mA off tune, falling to 8-9mA on tune. If adjustments of VC1 and L1 core do not produce a dip in current, the circuit may not be oscillating. A receiver or sensitive wavemeter tuned to 24Mc/s will show this. Alternatively, there will be a sharp rise in current if L1 is shorted, if the circuit was oscillating. If oscillation is not obtained, tapping T may need to be a turn or so nearer A. Should these tests show the circuit oscillates, but that the frequency can be tuned by VC1, tapping T needs to be a turn or so nearer G. If a g.d.o. is not handy, use a receiver or wavemeter to make sure that L1 is not tuned to 16Mc/s or 32Mc/s in error. Some 3rd overtone type crystals will oscillate at multiples other than the one required.

When adjustment is correct, adjusting L1 or VC1 will only slightly change the frequency, due to pulling the crystal, and if L1 is put very far off resonance, oscillation will cease, as shown by a rise in anode current.

Coil L2 has 6 turns of 16s.w.g. wire, spaced to occupy $\frac{3}{4}$ in., with an outside diameter of $\frac{4}{5}$ in. The

shortest possible connections are used from the coil to tag 5, and from C5 to the coil and chassis.

Insert V3. Temporarily insert a meter between R6 and chassis (positive to chassis). If a g.d.o. is available, adjust TC1 until L2 is resonant at 72Mc/s. If no g.d.o. is to hand, adjust TC1 for maximum grid current through R6, this should be over 0.5mA. Check with the wavemeter that L2 is tuned to 72Mc/s, and not some other multiple. Adjustments of TC1 may seem quite flat, because it is in series with V3 grid capacity. TC1 should be at least half closed. Should L2 not tune to 72Mc/s, it must be stretched or compressed slightly.

The driver coil L3 is adjusted to 144Mc/s with the parallel trimmer TC2. L3 is 2 turns of 16s.w.g. wire, with an outside diameter of $\frac{5}{8}$ in. and turns separated to occupy 5/16in. With grid current obtained through R6 as mentioned, rotate TC2 for maximum output, as shown by a wavemeter or lamp loop. The latter can be 1 turn of insulated wire, soldered directly to a 0.06 ampere bulb. The trimmer, L3, and C7 have the shortest possible leads. If L3 does not tune to 144Mc/s, it will have to be compressed or stretched slightly.

PA GRID COIL

As stray capacity is otherwise too great for efficient working, this is series tuned by VC2. It has $5\frac{3}{4}$ turns of 16s.w.g. wire, and is $\frac{1}{2}$ in. long, with an outside diameter of $\frac{1}{2}$ in. Wire V4 holder with stout conductors (16s.w.g.) and the shortest leads possible. Take by-pass capacitor and other connections to the tags adjacent to the sockets, not to the ends of the tags. A paxolin holder of the thin type, with little solid material, was found satisfactory, and the moulded type of holder with embedded sockets should not be used. A ceramic or other low-loss holder is preferable.

Connect L4 directly from tag 5 to VC2. Cut one lead of R9 very short, and solder this to the centre of L4. Put V4 in, but be sure no h.t. is applied to anode or screen grid. L3 and L4 are closely coupled as in Fig. 3. Adjustments in all stages can now be directed towards obtaining maximum grid current. With VC2 correctly adjusted, grid current should be 2mA to 3mA. If maximum grid current is with VC2 open, stretch L4 slightly. Should maximum grid current be obtained with VC2 closed, press the turns of L4 slightly together.

All the previous trimming adjustments can be checked now, to get maximum grid current on the meter. Although L3 and L4 need to be close together, on no account must they touch. The adjustments of TC2 and VC2 to some extent depend on each other, but after these are peaked VC2 should allow ample adjustment of grid current on the meter.

PA ANODE COIL

The p.a. anode coil L5 has $4\frac{1}{2}$ turns of 14s.w.g. wire wound to an outside diameter of 11/16in. The coil is $\frac{1}{4}$ in. long and a $\frac{1}{2}$ in. flexible lead is soldered to the anode end. This can be a piece of co-axial cable outer braiding, or a number of pieces of bared flex twisted together. The other end goes directly to VC3. A 14s.w.g. wire runs from VC3 moving plates tag to chassis.

RFC2 is self-supporting and has 30 turns close wound of 22s.w.g. enamelled wire on a $\frac{1}{4}$ in. diameter rod. Straighten a piece of wire and fix one

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end to some object. Wind by rotating the rod, keeping tension on the wire. Then when the rod is removed the turns will not spring out, but will remain as a solenoid. The actual tapping point is slightly off centre on the coil, as shown.

With no h.t. applied to V4 rotate VC2. A dip in grid current should be found indicating resonance for L5. If this is not found, compress or stretch L5, or check its frequency with a g.d.o. L6 is a single turn of 14s.w.g. wire, covered in stout sleeving. The co-axial socket is fixed to a bracket, and the ends of L6 go directly from this to VC4. A lead from VC4 moving plates tag runs to the socket outer member at a soldering tag.

NEUTRALISING

Series tuned screen neutralising is used, adjusted by TC3. The choke r.f.c.1 is 90 turns of 38s.w.g. wire on a 3/16in. diameter former. With TC3 fully closed, and no h.t. applied to V4, tune VC3 so that the dip in grid current mentioned is seen. Unscrew TC3 while VC3 is swung from side to side. A point should be found when the dip in grid current is much smaller, or absent and TC3 is left in this position.

PA TUNING

As a 6146 may readily draw a destructive anode current, a first test at reduced voltage is wise. Take h.t.2 to a 250V or similar supply, with a switch in circuit. A domestic lamp can be used as an artificial load. This is not ideal at 144Mc/s, and will present a much higher impedance than the usual load. A temporary loop having 2 or 3 turns of insulated wire should be made and connected by short leads to the lampholder terminals. Put this loop near L5, switch on the h.t.l supply, and adjust VC2 for about 2mA grid current. Switch on h.t.2, and immediately rotate VC3 for a dip in anode current. If this is under about 100mA, bring the lamp loop nearer L5. With 25 watts input (100mA at 250V) a 15W lamp should light fairly brightly.

Efficiency is much higher with increased voltages. VC2 may need slight re-adjustment after

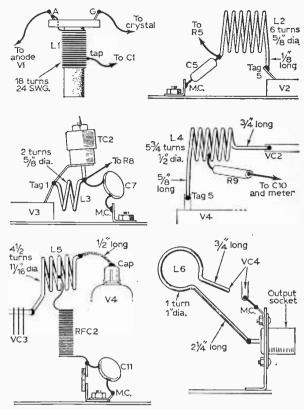


Fig. 4: Coil details. For winding instructions see text.

applying h.t. to V4. A 275V or 300V supply is recommended for h.t.l. When a lamp or other artificial load is connected to the output socket, closing VC4 from zero increases loading, but a 200/250V lamp is too high an impedance for this to be sufficient for full p.a. input.

C.W. ratings of the 6146 at 175Mc/s, are given as 140mA anode current at 320V. At 60Mc/s, ratings are 112mA at 600V. Telephony ratings are

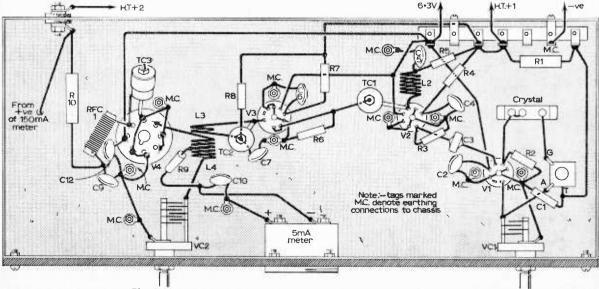


Fig. 3: Under chassis wiring diagram showing layout of components.

normally somewhat lower. In addition, the highest input ratings need ample grid drive, or full output is not obtained. In view of this, the amplifier has been operated at about 100mA anode current, from a 320V supply.

PA BIAS

The p.a. must not be operated without sufficient grid current (bias) or off resonance, or in conditions where the output obtained is so low that the anode dissipation is exceeded. With normal care, this should not be difficult. For increased output, R10 may be reduced to $16k\Omega$.

Point h.t.2 is supplied with modulated h.t. from the secondary of a modulation transformer. The modulator can be of normal type with a pair of 6L6 or 807 valves or similar stage delivering power about equal to half the p.a. input.

Note that the h.t. *must* be removed when changing crystals, if this is not done the valves could be permanently damaged.

WAVEMETER

★ components list

If a g.d.o. or wavemeter is not available, a simple indicating wavemeter can be constructed as in Fig. 5. Provided the inductance and other details are exactly as shown, accuracy should be high enough for the various harmonic multiples to be identified. The output from the diode is taken to a test-meter or other instrument with a ImA or similar range. The variable capacitor is fitted to a piece of

		· · · · · · · · · · · · · · · · · · ·		
ſ	Capac	itors:	Variat	le Capacitors:
Į	eib IIA	sc ceramic except C3	TC1	30pF Beehive
	C1	2000pF	TC2	8pF Beehive
1	C2	2000pF	TC3	
	C3	25pF mica	VC1	
1	C4	2000pF	VC2	
	C5	2000pF	VC3	
	C6	2000pF	VC4	75pF variables
	C7	2000pF		
	C8	2000pF		
	C9	2000pF	Induct	tors:
	C10	•	RFC1)
	C11		RFC1	
1	C12	2000pF	L1	•
			L2	See text and
	Resist	tors:	L2 L3	Fig. 4
1	R1	10kΩ 2W	L4	1 19. 4
ł	R2	3·9kΩ	L5	
	R3	56kΩ	L6	l l
	R4	33kΩ	LU)
	R5	1kΩ		
	R6	68kΩ	Valve	e •
	R7	20kΩ 1W		6C4
	R8	470Ω		6AM6
	R9	22 kΩ		5763
	R10	20kΩ 3W		6146
		20144 011	• •	01-10

Miscellaneous:

Crystal (8Mc/s 3rd overtone); two B7G skirted valve holders with cans; one B9A skirted holder with can; one octal holder; 5mA meter; 150mA meter; chassis $12 \times 5 \times 3in.$; crystal holder; co-ax socket; four knobs; tagstrip; wire; solder etc.

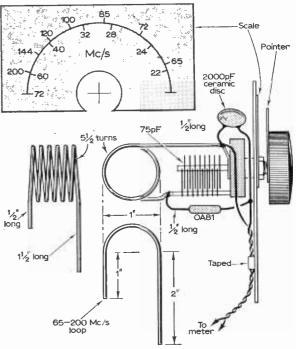


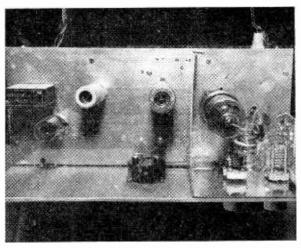
Fig. 5: Details and layout of suitable wavemeter.

insulating material, to serve as a handle and carry a card scale.

For the 22-72Mc/s band, take $17\frac{1}{2}$ in. of 16s.w.g. wire, and straighten it. Wind $5\frac{1}{2}$ turns so that the coil has an outside diameter of 9/10in. and is $\frac{1}{2}$ in. long, with the ends going directly to the tuning capacitor. For the 65-200Mc/s band, use 4in. of 16 s.w.g. wire. Bend this round a suitable object to form the loop as shown, and solder it to the capacitor. To cover both bands, it is necessary either to make two wavemeters, or to unsolder the unwanted coil. The wavemeter coil is loosely coupled to the appropriate transmitter coil, and tuned for maximum reading on the milliammeter.

Fixed capacitors should be of high-frequency by-

-continued on page 360



Top view of the chassis showing p.a. screening.

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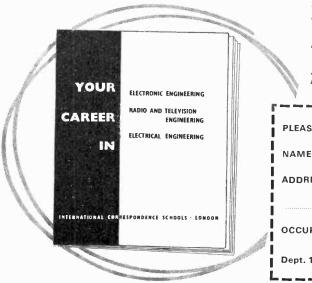
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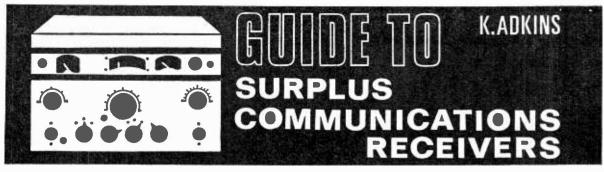
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PART 2

AR-8516L

This outstanding receiver, manufactured by R.C.A., is probably the last word in valve receivers. It was designed only a few years ago for marine communications, and a few of them have since become available on the amateur market. The receiver covers 80kc/s to 30Mc/s continuously, in 18 bands as follows:

1	80kc/s-200kc/s	10	12—14Mc/s
2	200kc/s—520kc/s	11	14-16Mc/s
3	520kc/s-1300kc/s	12	16—18Mc/s
4	1.09Mc/s-3.09Mc/s	13	18—20Mc/s
5	24Mc/s	14	20-22Mc/s
6	46Mc/s	15	22—24Mc/s
7	6—8Mc/s	16	24—26Mc/s
8	8—10Mc/s	17	26-28Mc/s
9	10-12Mc/s	18	28—30Mc/s

On bands 1 and 2, the receiver operates as a single superhet with an i.f. of 45kc/s. On bands 3, 4 and 5 operation is as a double superhet with i.f.'s of 455kc/s and 45kc/s. On bands 6 to 18 the receiver is a triple superhet with 2nd and 3rd i.f.'s of 455kc/s and 45kc/s respectively, and the first i.f. tunable from either 2-4Mc/s, or from 1.09-3.09Mc/s.

The valve line-up is as follows:

3BZ6	(Bands 6–18) R.F. Amplifier.
3CB6	(Bands 6-18) 1st Mixer to 2-4Mc/s or
	1.09-3.09Mc/s.
3CB6	(Bands 6–18) Oscillator.
3BZ6	(Bands 6–18) 1.F. Amplifier.
or	(Bands 1-5) R.F. Amplifier.
3CB6	(Bands 1–2) 1st Mixer to 45kc/s.
or	(Bands 3—5) 1st Mixer to 455kc/s.
or	(Bands 6–18) 2nd Mixer to 455kc/s.
7AU7	(Bands I—3) V.F.O.
3CB6	(Bands 4—18) V.F.O.
3BZ6	455kc/s I.F. Amplifier.
3BZ6	455kc/s I.F. Amplifier.
3BZ6	455kc/s I.F. Amplifier.
3BE6	(Bands 3—5) 2nd Mixer to 45kc/s.
or	(Bands 6-18) 3rd Mixer to 45kc/s.
7AU7	Oscillator and crystal calibrator.
5U8	455kc/s B.F.O.
3 1 1 5	155kc/s Detector and A C C

- 3AL5 455kc/s Detector and A.G.C.
- 5U8 45kc/s I.F. Amplifier.
- 7AU7 45kc/s B.F.O.
- 3AL5 45kc/s A.G.C.
- 1N34A 45kc/s crystal detector.
- 3AL5 Noise Limiter.
- 7AU7 A.F. Amplifier.
- 7AU7 Feedback Amplifier.
- 12CU5 A.F. Output.

Some of the valves serve more than one function. Five positions of selectivity are available: 6kc/s, 3kc/s, 1.5kc/s, 0.8kc/s and 0.1kc/s. The 6kc/s and 3kc/s bandwidths are available only on the 455kc/s i.f. system. A mechanical filter is operative on bands 3—18. A noise limiter is included, and the a.g.c. has both fast and slow positions. An "S" meter is incorporated. C.W. receiver sensitivity for a 6dB signal plus noise-to-noise ratio is as follows:

Bands	12	3	microvolts
Bands	3—5	2	microvolts
Bands	6—18	1	microvolt.

Frequency drift due to changes in external environment or supply voltage is extremely low, and there is no long-term drift. The horizontal tuning scale has frequency markings at 50kc/s intervals, and a circular logging scale enables frequencies to be read to 1kc/s.

Output is arranged for high impedance phones, 3Ω speaker or 600Ω line. An output is also available at 455kc/s for FSK adaptors, etc. The receiver may be operated either from 115V a.c. or d.c., or from 230V a.c. The complete receiver weighs 91 lb, due mainly to the heavy gauge metalwork.

Modifications: It is unlikely that the performance could be improved.

Availability: As only a few of these receivers were ever released, a certain amount of difficulty may be encountered in obtaining one. Second-hand prices would probably run into three figures, although this is still a fraction of the original price. Manuals were available with the receivers.

BC453 BC454 BC455

These sets are popularly known as "Command Receivers", and were used in aircraft of the US Army. They are of totally shielded, all-aluminium, construction and are very light and compact. They were originally designed to operate from the 28 volt d.c. aircraft supply. The three receivers are identical except for their frequency coverage and i.f. frequencies, which are given below:

BC453	190-550kc/s.	I.F.	85kc/s.	
BC454	3-6Mc/s.	I.F.	1415kc/s.	
BC455	6-9·1Mc/s.	I.F.	2830kc/s.	
M.C.	and the standard of the	41		

Minor variations of these receivers are denoted by a suffix letter, e.g. BC453A.

These three receivers originate from a piece of equipment known as the SCR274. Another series, known as the ARC-5, contains an almost identical set of command receivers.

The command receiver has 6 valves, as follows:

Three 12SK7, one 12SR7, one 12A6, one 12K8. The circuitry includes one r.f. stage, two i.f. stages, mixer, detector, b.f.o. and audio. A 28 volt dynamotor power supply is incorporated. In its original form, the command receiver has output for 300 or $4,000\Omega$ headphones. The circuitry does not usually incorporate a.g.c., but it is believed that a few command sets in the ARC-5 series do have this feature.

The size of the command receiver is 5in. x 8in. x 12in., and its weight is only about 6 lb.

Modifications. The command receiver has become very popular both in the USA and in this country, mainly because of its cheapness and small size. It is not normally used on its own as a communications receiver, but is used in conjunction with v.h.f. coverters, or as a second i.f. channel for another communications receiver. It is admirably suited for both of these functions, after a certain amount of modification.

The first and obvious modification is to replace the 28 volt dynamotor with an a.c. power supply. It is possible to mount an a.c. power supply on the chassis in the position formerly occupied by the dynamotor, although reasonably small components must be used. The unit must supply 250V at 50mA. The valve heaters were originally wired for 25.2 volts, and must be rewired for operation from the more usual heater voltage supplies.

For loudspeaker operation, the output transformer must be changed, and it will probably be necessary to provide more audio power.

Few controls are provided and it will be necessary to modify the panel in order to allow for the mounting of the additional controls provided by the electrical modifications.

Other popular modifications include the addition of a noise limiter; and the replacement of the 12SK7 valves with 12SG7's in order to improve gain.

The BC453 version is normally employed as a second i.f. channel. It is set up to receive the i.f. signal from the main receiver, and then amplifies this signal at 85kc/s, at which frequency it is possible to obtain adequate selectivity for operation in the most crowded of bands.

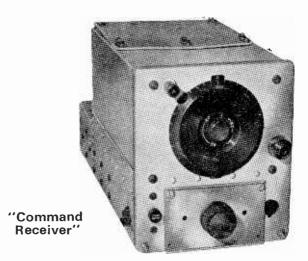
The BC454 and BC455 versions are normally employed as single i.f. channels v.h.f. converters.

TWO METRE TRANSMITTER

—continued from page 356

pass type, and sufficient voltage rating. When the p.a. is operated from a modulator, Cl1 should be rated at more than *twice* the h.t. voltage. A 1kV disc ceramic capacitor is ideal, but a mica capacitor can be used, and the value may be reduced to 1,000pF. The variable capacitors VC1, VC2 and VC3 can be modified somewhat, to use 7.5pF, 10pF, or similar components. Much larger values, such as 25pF or 50pF, are not suitable. The minimum capacity is too great, and adjustment too difficult. The capacity of some surplus miniature short wave tuning capacitors can easily be reduced by taking off plates. VC should be rated at twice the h.t. voltage or more, so needs double plate spacing.

Various combinations of inductance and capacity will reach the resonant frequency required in each stage. But with L3 in particular, output rises when



Availability. Unlike the majority of the other receivers dealt with in this guide, the command receiver seems to come on to the surplus market in a steady trickle, rather than in batches. They are doubtless much more readily available in the United States. It is usually possible to hunt one down in the West End, as most retailers seem to hold a small supply of them at one time or another. The position is almost certain to become more difficult in the future.

Prices range up to a maximum of £4 or £5, depending on condition. The writer was lucky enough to obtain two of them, two or three years ago, for 2s. 6d. each! (In grade 3 condition, of course).

Command receivers can quite easily be obtained on the second-hand market, and here one has the advantage that the receiver has probably already been modified, although perhaps not to the purchaser's satisfaction.

Command receiver manuals are not widely available, and indeed are not generally considered necessary owing to the numerous modifications to this receiver published in the amateur radio press in the last ten years or so.

To be continued

TC2 is at quite low capacity, so the coil may be compressed slightly if needed.

CW WORKING

Cathode keying of V4, suitable for lower frequencies, cannot be used. However, the screen grid supply to V3 can be keyed, and bias applied through L4 so that the input to V4 does not exceed 20 watts during key up intervals. In this case R9 should be reduced to $2.2k\Omega$, and the negative bias taken to positive on the 5mA meter. Bias from a small power pack delivering some 40V or so is most convenient, with a potentiometer to allow voltage adjustment. A check should then be made with no drive so that V4 d.c. input (voltage x current) is not over 20W for the anode and 3W for the screen grid.

During phone or c.w. working, the p.a. must be so coupled and loaded that the d.c. input does not exceed by more than 20W the r.f. output obtained. In the absence of bias from a power pack or battery, R9 must be $22k\Omega$.

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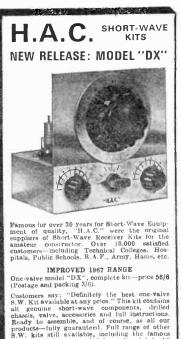
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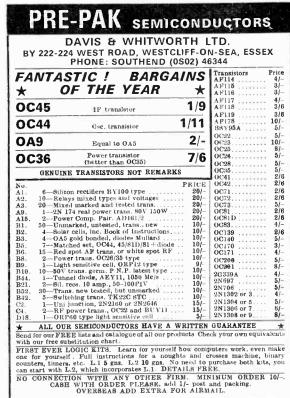
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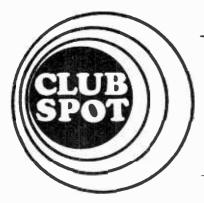


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No. 17 CRAY VALLEY RADIO SOCIETY C

HE Cray Valley Radio Society was founded in 1946 to provide a focal point for Radio Amateurs and Short Wave Listeners living in the vicinity of Cray Valley, a district covering Eltham, Sidcup, Bromley, Orpington and the Crays. Membership now consists of over 40 licensed operators and nearly 20 Short Wave Listeners drawn from a wide variety of trades, professions and students.

Early licences

The Society is proud to include among its members, four operators, G2HP, G2MI (who is President and a member of the RSGB Council), G2WI and G2ZI, all licensed in the earliest days of Amateur Radio.

There is no doubt that QUA, the Society's newsletter, does a great deal to keep members in touch. This is published regularly each month, the present editor being G3DNC. Contributions from members are always welcome and usually make up a satisfactory proportion of the contents, varying from technical articles to miniature masterpieces of doggerel.

Meetings

The Society meets twice monthly. On the first Thursday in the month at the Congregational Church Hall. Court Road, Eltham, London S.E.9 the meeting is usually devoted to a technical lecture or feature. The second meeting, held a fortnight later at All Saints Church Hall, Bercta Road, New Eltham, London S.E.9 is usually a "natter-nite" because past experience has shown that members seldom have enough opportunity at the principal meeting to say all that they want to in the limited time available for conversation. It is hoped to alter the meeting night for this event in due course so that those members who find Thursdays inconvenient will at least be able to attend some of the meetings.

Until a few years ago there was little or no interest in contest operating but in the last three years, the Society has participated in both h.f. and v.h.f. contests with varying degrees of success. In an attempt to co-ordinate the efforts of individual members, G3VLT has taken on the job of Liaison Officer and hopes to produce improved results.

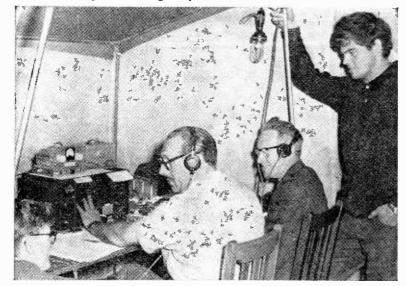
Balance of activities

One problem which must be common to many Societies is that of getting a reasonable balance of activities. This particular aspect has recently engaged the attention of the Cray Valley management committee to the extent of sending a questionnaire to all members and it is hoped that the future programmes based on suggestions received will be to their liking.

Society net

The Society runs a net on Top Band on Fridays at 21.00 hours and there is also a rival, though none the less popular, net on four metres at 20.00 hours on Tuesdays. The Top Band net has proved a valuable source of publicity for attracting new members who, by this means, often first learn of the club's existence.

Activity weekends are held at intervals, mainly with the object of giving other amateurs an opportunity of qualifying for the Cray Valley Award. Particulars of this are obtainable by sending a stamped addressed envelope to G3MCA.



Members at the 1966 NFD. From the left they are: Chris, G3VLT; Alan, G3ANK; Bill, G2AQB; and Dave, G3RGS.

No permanent QTH

One big handicap that has not yet been overcome is the lack of a permanent headquarters where gear can be installed and aerials erected. The Society looks forward to the day when this object can be achieved.

WVC award

The Society award a certificate to any licensed amateur who can give proof of two-way communi-



cation, any mode, any band. To gain the number of points pertaining to his locality, e.g., G stations require, 15 points, Euro pean stations require 10 points and DX stations require 5 points.

One point is given for contacting each Society member and three points for contacting the Society Station, G3RCV. Net QSO's are void. Log extract, certified by two other licensed amateurs, or QSL's and 5 I.R.C. (or 2s. 6d.) to G3MCA. To gain the required points, G3RCV need not be QSO'd. GM, GD, GC, GI and GW stations count as European.

The present committee includes G3JJC (Chairman) G3VLX (Secretary) and G3TCC (Treasurer). Anyone interested in joining will be welcome at any meeting: alternatively they can contact the secretary at 850-6945, evenings or weekends, or write to G3VLX, 234 Halfway Street, Sidcup, Kent.

A book reviewed

The notice of Donald Smith's ABC's of Electronic Test Equipment by "HWH" in the June number conveys so little of interest that one wonders why the work was noticed at all; the space might well have been given to better use. What does "HWH" expect for 16/- — a tome covering the entire field of test instrumentation in such detail that low-grade technicians can make their own in their garden sheds, from parts bought at "junk shops"? Has "HWH" spent a whole day at, say, the recent **RECMF** show at Olympia. Has he examined the shelves of books on electronics in his local public library? Above all, has he himself written any books on electronics. and is he really familiar with the problems of publishers to-day? If "yes" to all queries, I am surprised and annoyed by his notice of this unimportant but harmless enough book, which may be best left for technicians to discover for themselves without his hostile remarks. For my part, I want information about more important practical books .-- W. H. Cazalv.

[We, too, would love to see more useful books, but can only review those sent. To ignore those that dissatisfy makes a mockery of the task reviewers set themselves.

ABC's of Electronic Test Equipment falls awkwardly between two stools. It would have been more interesting (though even less useful) if it merely listed the available test gear seen at the recent RECMF Exhibition. It would have been more useful if it had continued as it began and developed its theme of basic design. But to omit so much fundamental information that even we "low-grade technicians" could not use it to work in our garden sheds certainly merited some adverse comment.

There are indeed many books on the public library shelves—this reviewer has written a few himself, Mr. C., and is aware of the blood and sweat they entail. The few that deal with test instruments are either very expensive or narrowly specialised. I feel sure the Editor would be delighted to give space to a review of any work that deserved the attention of his faithful band of practical readers]—H.W.H.

Infinite baffle mods

I note with interest G. R. Fletcher's article "Idea for an Infinite Baffle" published in the April edition of P.W.

Whilst commending the scheme from the technical (and domestic) point of view, I should like to suggest certain slight modifications: (1) the chimney can resonate like a closed organ pipe. Although the fundamental will almost certainly be too low in pitch to be noticeable (18c.p.s. for a 30-foot chimney), the even harmonics emitted could produce devastating coloration.

(2) Front-to-back standing waves, reflected by hard materials such as firebrick, could present problems.

(3) The presence of a large lintel close to the rear face of the speaker cone causes "tunnel effect"—i.e. more coloration.

These effects can be remedied in the following ways:

(1) The chimney should be blocked above the speaker to make a rigid airtight seal. The height of the chamber so formed is not critical, but should not be made a multiple of either major horizontal dimension. Mr. G. A. Briggs recommends ratios of -1 : 1.25 : 1.6 or 1 : 1.6 : 2.5—to minimise coloration.

The roof of the chamber should ideally be brick or concrete, but wood at least $\frac{1}{2}$ in. or preferably lin. thick could be substituted. Wood faced on the upper side with heavy unglazed ceramic tiles would be a good compromise.

(2) The whole cabinet should be lined on the inside with absorbent: a good thick layer of fluffy soot would help considerably.

(3) Bricks close to the speaker should be bevelled away:

The author's precaution of pushing newspaper wads up the chimney has probably saved him from the worst effects of column resonance—the pads will form an acoustic filter.

In conclusion—Good luck, Mr. Fletcher—an excellent idea.—W. S. Lymath, Engineer, Rank Wharfedale Ltd. (*Bradford, Yorkshire*).

Veteran valve identity

I wonder if you or your Correspondent P. J. Plater, of Wallington, Surrey (June '66) can help me with the valve line up of a veteran Burndpept 285.

As he says the valve identity marks do get lost, and this veteran was doing nicely, when it spluttered and stopped. I found that the ancient electrolitic was leaking and had evidently eaten through a lead to earth, but I cannot decide which of two tags it belongs to, till I know the identity of the output valve.—W. M. Mackenzie (Gosport, Hampshire).



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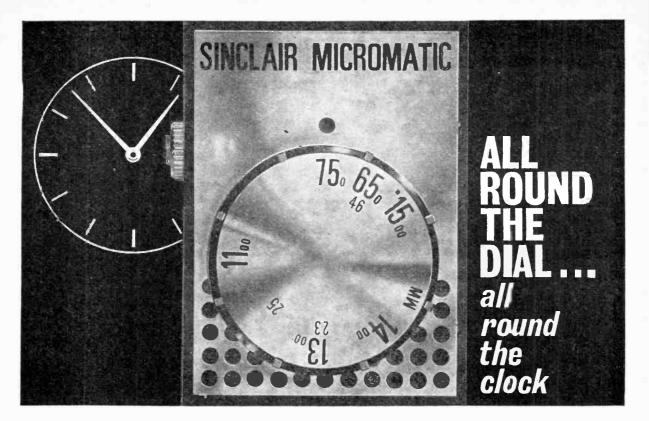
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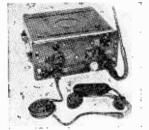
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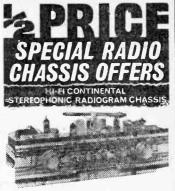
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