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HFW-1


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RA. 1

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"Home, Light. A,F.N., Lux. all at good volume. 7 stages-5 transistors and 2 diodes
Fully tunable over Medium and Long Waves. Incorporates Ferrite rod aerial. funing condenser volume control, new type Attractive case. Size \(6 \frac{1}{5}\) x \(4 \frac{1}{3} \times\) lifin. with red speaker grille. (Uses 1289 battery, avallable anywhere.) - Extended M.W. band for easier tuning of Luxembourg etc. \(\begin{array}{llll}\text { Total cost of all } & 42 / 6 & \text { P.-\& P. } & \begin{array}{l}\text { Parts Price List and easy bulld } \\ \text { plans } 2 /-\end{array} \\ \text { (Free with kit) }\end{array}\) POCMET EMVE Now with 3in - 7 stages- 5 transistors \(\& 2\) diodes Covers Medium and Long Waves. On test Home, Light, Luxembourg and many Continental stations were recelved loud and clear. Designed round supersensitive Ferrite Rod Aerial and
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Pocket \(\delta\) med. and long wave \(29 / 6\) P. E.P.

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- 8 stages-6 transistors and 2 diodes A top performance receiver covering full Medium and Long Waves. High-grade 3in. speaker makes istening a pleasure. Push-pull output. Ferrite rod aerial. Many stations listed in one evening includgrey with red grille. Size \(61 \times 41 \times 1\) inctin. Uses PP4 battery available anywhere). Carrying strap 1/- extra.
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\section*{Clause 7-No person shall make equipment undesirable to Government if new Act becomes law.}

AT first glance, the changes to the Wireless Telegraphy Act outlined in the recently published Bill appear to be a bold attempt to remedy some long outstanding ills. Strong measures are suggested for dealing with TV licence dodgers and evaders of car radio licences. But the section dealing with illegal radio transmitting merits a much closer investigation.

This journal has long campaigned for action to resolve the ludicrous situation whereby it is perfectly legal to import, offer for sale and buy \(27 \mathrm{Mc} / \mathrm{s}\) walkie talkies and yet impossible to use them without breaking the law. The Board of Trade, the GPO and radio dealers have for years shrugged off responsibility with some agility.

In the new Bill, the PMG introduces provisions presumably to deal with this situation and that of radio bugging devices. Presumably, we say, because in the potentially explosive Clause 7 it states that "where it appears to the PMG to be expedient", the provisions should "apply to wireless telegraphy apparatus of any class or description" and that "no persons shall manufacture any apparatus of that class or description whether or not for sale".

This loose phraseology could be interpreted to cover any form of radio apparatus deemed to be "undesirable" and amounts virtually to a blanket control over the manufacture, importation, sale and construction of radio equipment of any type which the Government considers undesirable.

We do not say that the PMG intends to use the sweeping powers implicit in the seven sub-sections of Clause 7, nor even that he has considered them in detail, but the fact remains that if this Bill becomes law as it stands, these powers will not only be available to the present administration but to all future PMGs.

In seeking to deal with specific problems the PMG has wielded a bludgeon. If classification is difficult it would have been better to isolate the real objectives by making it illegal to sell or buy any transmitting equipment except on the production of a suitable transmitting licence. This way, innocent bystanders would not get involved. Unless, of course, the PMG has more sinister motives.
W. N. STEVENS—Editor

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All correspondence Intended for the Editor should be addressed to : The Editor, "Practical Wireless", George Newnes Ltd., Tower House, Southampton Streef, London, W.C.2. Phone: TEMple Bar 4363. Telegrams: Newnes London, W.C.2. Subscription rates, Including postage: 36 s . per year to any part of the world. (C) George Newnes Ltd., 1967. Copyright in all drawings, photographs and articles published in "Practical Wireless" Is specifically reserved throughout the countifes signatory to the Berne Convention and the U.S.A. Reproductions or Imitations of any of these are therefore expressly forbidden.
}

\section*{Kits a success}

During the past eight years I have built kits supplied by seven of your regular advertisers and I cannot fault one of them. In all cases the instructions were clear and easy to follow.

I think those who make claims that their kits can be built in an hour are not helping their own cause. Who wants to build a kit in an hour anyway? It is a hobby and how much better to make the interest last for a few days at least. There are sure to be setbacks, then out comes the test-meter and the interest is extended further.

Most early efforts fail because of poor soldering, through getting resistor values mixed up and switch and coil connections wrong.

I do not grudge the charge of 6d. per valve, bearing in mind the cost to the retailer of cartons, corrugated paper, packer's wages, etc. I would give a vote of thanks to the firms who send me good valves promptly, cheaply and beautifully packed.
P. J. Plater.
\(\star \quad \star \quad\)\begin{tabular}{l} 
Wallington. \\
Surrey.
\end{tabular}

Mr. A. H. Brough of Staffordshire (P.W. May issue) will probably find that most firms specify P. \& P., and packing involves corrugated card, cartons 'and often stout cardboard boxes, also employment of a packer and checker, all of which has to be paid for to ensure adequate protection in transit.
A. Deverell.

Rickmansworth, Hertfordshire.

\section*{U.S. Citizens' Band}

After reading the column "Amateur Bands" in the May 1967 issue, it appears to me that there is some confusion concerning Citizens' Band licences in the United States. As an American now living in England, perhaps I can straighten out the situation.

A Citizens' Band licence may be issued to any U.S. citizen over the age of 18 with no exam. required. A fee of \(\$ 8.00\) ( \(£ 217 \mathrm{~s}\). 2d.) is charged, and the licence allows the bearer to transmit on the \(27 \mathrm{Mc} / \mathrm{s}\) band with a power not exceeding 5 watts. A callsign is assigned which usually consists of a three letter prefix followed by four numbers.

Any person, regardless of age, may use Citizen Band frequencies so long as the transmitter power does not exceed 100 mW , and a vertical antenna of not more than 60 inches in length is used No callsigns are issued to these people, as they are not required to register with the Federal Communications Commission.

> D. L. Potash.

Ambleside, Westmorland.

\section*{NEWV AND}

\section*{VHF STEREO TRANSMISSIONS}


Work is in hand to extend the BBC stereophonic transmissions, at present radiated from Wrotham, Swingate and Brighton, to Sutton Coldfield and Holme Moss and certain relay stations fed from them, early in 1968. The unshaded part of the map indicates the areas in which satisfactory stereophonic reception should normally be obtained. In places where the field-strength is low, increased background noise may be heard on stereophonic programmes; improvements to the receiving aerial enable the noise level to be reduced.

\section*{ELECTRONICS CONFERENCE IN GREAT BRITAIN}

A Technical Conference and Exhibition devoted to the engineers who build and produce electronic equipment will be held at Brighton in October 1968. This is the first such conference and exhibition ever to be held in this country or Europe.

Called NEP/CON-INTERNATIONAL it has for some time been held twice-yearly in the U.S., and will present a wide-ranging international technical programme. It will cover the most recently developed techniques such as printed circuitry, microminiaturisation, component and equipment manufacture etc. Talks will be given by leading engineers from the U.S., U.K. and Western Europe. Also there will be an exhibition where the latest components materials and machines will be on display.

SUB-MINIATURE METER


Sifam Electrical Instrument Co. Ltd., Woodland Road, Torquay, Devon, have introduced a new sub-miniature instrument in the "Director" series of moving-coil instruments.

The new "Director 14" is exceptionally compact, having an overall size of 1.92 in . by 1.65 in . with a scale length of 1.34 in . It is flush mounting requiring a panel cutout of \(1 \cdot 5\) in. diameter.
The company emphasises that, despite its size, the instrument is a glazed-front, quality unit built to BS89: 1954 accuracies (i.e. \(\pm 2.5\) per cent of full-scale deflection). The case is made from a special reinforced plastic with a matt black finish, resulting in an elegant yet highly practical case style, which blends well with modern equipment panels.

\title{
...CDMIMENT
}

\section*{PANEL LIGHTS TO ELECTRIC ORGANS}

From Henry's Radio Ltd. comes the 1967 Electronic Components, Equipment and High Fidelity Catalogue. This edition-now over 200 pages-is more comprehensive than those published in previous years and includes details of many new items supplied by Henry's, including their Mayfair Portable Electronic Organ.

Included in this issue are five free discount vouchers which when used enable the customer to obtain \(2 s\) s. in the pound discount. It is also interesting to note that further discounts are allowed for equipment in the Hi-Fi section of the catalogue.

The price of the catalogue is 7 s .6 d . plus 1 s . postage and copies may be obtained from Henry's Radio Ltd., 303 Edgware Road, London, W2.

\section*{PIRATES-ALL OR NOTHING}

Discussing the Marine and Broadcasting (Offences) Bill in the House of Commons recently, Mr. Ian Gilmour unsuccessfully suggested that the Government should restrict the scope and impact of some offences covered by the Bill. He maintained there was no reason why penalties should be imposed on scriptwriters and others who provided material for the pirates. He had not, however any objection to imposing penalties on those who ran the pirate stations. Answering, the Postmaster General, Mr. Edward Short, said to omit the clause from the Bill would enable the pirates to continue receiving advertising revenue, records and tapes, etc., from which they made up their programmes and attracted an audience. It would make the legislation almost ineffective. Publication of information about future programmes of the pirate stations is to be prohibited.

The Bill had been carefully drafted, Mr. Short told the House, to catch only things which served as advertisements. References to past broadcasts would not be affected by the Bill but references to future broadcasts would be. Also anybody in this country giving assistance to the pirates will be liable when the Bill becomes an Act.

Referring to Clause 6 of the Bill (Penalties and Legal Proceedings) Mr. Short moved an amendment to increase the maximum penalty for unlicenced transmitting from \(£ 100\) to £400. He maintained that \(£ 100\) was nothing more than petty cash to a successful pirate broadcaster.


From Philips comes a new four waveband portable costing \(19 \frac{1}{2}\) guineas. Included in the features is an "electric eye" tuning guide which doubles up as a battery condition tester. Another feature is a separate battery cartridge holding four U11 batteries which is released from the radio at the touch of a button. Wavebands covered are long, medium, short and f.m. Output is 380 mW , and a telescopic aerial is provided for reception on v.h.f. and s.w. Cabinet measures \(9 \frac{3}{4} \times 5 \times 1\) 膏in. and is finished in black polystyrene with silver grille.

\section*{New members wanted}

I am writing on behalf of the Sheffield Amateur Radio Club which urgently needs new members. Anyone interested in any aspect of radio, especially amateur radio and short wave listening would be most welcome at any of our meetings. These are held every. Friday evening at 8.00 p.m. at 8 Sandbeck Place, Sheffield 11.

Anyone requiring further information or details on how to reach the club H.Q. should contact me at the address below. G. Watson.

25 Underwood Road, Woodseats,
Sheffield 8,
Yorkshire.

\section*{Well done Sirs}

I am writing this letter to express admiration of two 60-year-old gentlemen whose letters appeared during 1965 stating that they had obtained their Amateur licences. These gentlemen fired my enthusiasm and I started to study for the RAE in October 1965 and passed in May 1966. I then started Morse practice and received my Pass slip recently.

I hope that this letter will encourage others, as I myself am 47 years of age. All study was done at home from library books and guidance obtained from the RSGB Radio Amateurs' Examination Manual and a study of five years' examination papers. The Morse code was also self-taught by means of an oscillator and a tape recorder.
F. Woolliscroft.

> Whitley Bay, Northumberland.

\section*{The spirit of readers}

You printed a request in your "CQ" column for me in the May issue of this journal and within hours of Practical Wireless being on sale I had a satisfactory reply. In fact, someone personally brought around the "wanted" magazines and many other readers wrote to me.
I. Nicholls.

Kilburn,
London, N.W. 6.

\section*{U.K. Police State?}

I would like to bring to the attention of other readers that if the Government gets its own way on the amendments to the Wireless Telegraphy Act, we shall be told what we can build and what we cannot. This is very wrong and I suggest readers in agreement with me write to the P.M.G. personally - Edward Shont, M.P., House of Commons.
C. Rolls.

Highgate,
London, N.6.
[We are not very keen on the Government's proposals, for it covers virtually anything: see the Leader page for our views.]-Editor
More News and Comment on Page 122
 not required for local station reception. Both coarse reaction and tone are pre-set but could be brought out to separate controls on the front panel if desired. With a three foot piece of flex as an aerial the sensitivity is comparable to the average transistor portable, and in Northern Scotland the prototype receives Radio Luxembourg very well after dark.
The receiver contains very few components most of which are not critical, the circuit is thus ideal for experimentation. Both long and shortwave coverage can easily be added by the addition of


Fig. 2 (below): Suggested power supply circuit.

suitable coils and a wavechange switch. This modification is described later in detail. Although two modern miniature valves are specified using B9A valveholders, the older octal-based types such as the 6SL7 and 6 V 6 should function equally well. If these older valves are used then the valvebases should be wired accordingly, since the pin connections are different to the B9A base wiring shown in the circuit and layout diagrams.

\section*{CIRCUIT DESCRIPTION}

The two-valve circuit contains three stagesdetector, a.f. amplifier and output. The power supply unit (p.s.u.) is built on a separate chassis which enables it to be used to power other equipment.

The regenerative detector (V1A) has unusual input circuitry. The signal from the aerial is fed to a capacitive potential divider consisting of \(\mathrm{Cl} / \mathrm{C} 2\), through the tuning coil L1 to the grid of V1A. The d.c. continuity between grid and chassis is established by the grid leak R2, and resistor R1 is wired between aerial and earth to prevent a charge building up on the aerial. Feedback is effected by L2 and TC1, the fine control being made by adjustment of VR1. Note that TC1 is insulated from the chassis. Slight detuning is evident because VCl is across the valve grid-to-cathode capacitance which alters slightly as the valve warms up. Detuning is also affected to some slight degree as the reaction is varied, but these effects are small and are thus ignored. The value of the anode load resistor R 4 may be adjusted if regeneration cannot be readily obtained. Other methods of obtaining regeneration


Fig. 3: Layout of the power supply shown in fig. 2.
are possible, however the method used works out very well. For those who like to experiment, the different "textbook" methods could be tried out.
From the junction of R3/R4 the detected signal passes via C3 and VR2 to the grid of the audio frequency (a.f.) amplifier V1B. This is an a.f. stage of conventional design other than the omission of the cathode by-pass capacitor usually wired in parallel with R6. In order to cut down the bass response when a miniature speaker is used, the cathode decoupling capacitor C5 may be reduced to \(2 \mu \mathrm{~F}\). This will help prevent undue damage to the small speaker due to bass overloading. This step will not be necessary with the larger type of speaker. When using a small speaker, R8 could be increased to \(1 \mathrm{k} \Omega\), this will limit the output and effect some economy.

\section*{POWER SUPPLY}

The power unit is straightforward, using two contact-cooled metal rectifiers in a full-wave circuit. A valve, such as the EZ80, could be fitted in place of D1/D2, but this would require to be fed with 6.3 volts and would also contribute considerable heat. A double-wound mains transformer is strongly recommended and suitable types are readily obtainable from advertisers in this journal. It would be possible to make use of a miniature 220 volt \(20 / 25 \mathrm{~mA}\) mains transformer of the type used in tuners and preamps. In this case R8 should be increased to \(1 \mathrm{k} \Omega\) in order to reduce the current consumption.

\section*{MODIFICATIONS}

Although the tuning capacitor VC1 gives satisfactory station separation on the medium and long wavebands, crowding occurs on the short waves. To combat this it is suggested that the s.w. band be split into two sections, and that the effective


Fig. 6: Rear view of the wavechange switch for three-band coverage.
capacitance of VC1 be reduced. This latter suggestion can be easily performed by interposing a capacitor between VCl and the junction of terminal \(a\) on L1, and pin 2 of V1A. By placing a fixed capacitor in series with VC1 in this way, the effective swing or tuning range of VC1 is restricted to a portion of the band. However, since this small portion of the band is now spread out over the entire \(180^{\circ}\) swing of VCl instead of a few degrees, the stations received will be easier to tune. If the extra capacitor is made 300 pF to start with, the constructor can experiment from there.
If band switching is required then a suggested method is shown in Fig. 6. As shown, the switch will give three-waveband coverage, the actual wavelenths covered depending on the coils used. Details for suitable coils are given later on.
Other worth-while modifications are a tone control and a socket for headphone reception. The simple top-cut control shown in Fig. 5 works well. The voltage rating of the capacitor between the anode and the headphone socket must be at least 1.5 times the nominal h.t. voltage. Do not fit a

Fig. 5 (below): Suggestions for the inclusion of a tone control. and for using headphones. It would be unwise to use a capacitor of less than 400 V working in the phones lead to the anode of the valve.



Fig. 4: Layout of components and wiring below chassis. Note that TC1 must be insulated from the chassis. This is essential for the circuit to function properly.
"normally closed" jack socket or this will short the signal to earth when the phones are removed.

\section*{CONSTRUCTION}

The following procedure is recommended when all the parts, including the chassis have been obtained. Drill the chassis and mount all components securely. Wire up the power unit starting with the mains transformer. Wire the heaters of the valves with twisted leads and plug in both valves. After a careful check of the wiring switch on and note that the heaters inside the valves light up. If they do not, switch off immediately and re-check the wiring.

Switch off, unplug the valves and disconnect the power supply unit from the mains. Proceed with the wiring up of V2 starting with the output transformer working back to R7. Keep all leads as short as possible. Fit one end of C4 to pin 2 of V2
\begin{tabular}{|l|c|c|}
\hline COIL & NO. OF TURNS & WAVEBAND \\
\hline L1 & 45 & \(\}\) \\
L2 & 5 & MW \\
L1a & 12 & \(\left\{\begin{array}{l}\text { SW1 } \\
\text { L2a }\end{array}\right.\) \\
L1b & \(1-2\) & \(\left\{\begin{array}{l}\text { SW } \\
\text { L2b }\end{array}\right.\) \\
\hline
\end{tabular}

The table shows details of the coils. The type of wire and former diameter are mentioned in the text.
and temporarily solder a wire to the other end. After checking the wiring plug in V2 only, connect the loudspeaker and switch on. After the valve has warmed up there should be a slight hum from the speaker, this should increase as the wire on C4 is touched. There should be no whistling or clicking nor any instability. If the stage is functioning properly switch off, remove the wire from C4 and unplug the valve.

Wire up V1B and fit one end of C3 to the volume control VR2. Check the wiring and plug in both valves. Repeat the test for V2. As the wire from C3 is approached a loud hum should be heard. If all is satisfactory switch off, unplug the valves.

Wire up V1A taking every care to keep connections short and direct. Unscrew TC1 to minimum capacitance and set VR1 to maximum resistance. Now check all wiring very carefully as this last stage is more complex. Plug in the valves and the aerial ( 2 or 3 yards of flex), then switch on. There should be no howling or whistling, if there is reduce the coupling i.e. the distance between L1 and L2. If preferred the number of turns on L2 may be reduced instead. Now screw up TCI to the point where howling or whistling just commences. Tune in a station, backing down VR1 until oscillation has just stopped. This is the most sensitive position for the set. Retune VCl if necessary and set the volume control to a convenient level. Switch off taking care not to touch the h.t. line without first discharging the capacitors C6a and C6b to chassis. Check all components to ensure that there has been no overheating. The receiver may now be enclosed in its cabinet.

\section*{COILS}

The medium wave coil on the prototype consisted of 45 turns of 22 s.w.g. enamelled copper

\section*{components list}

\section*{Resistors:}
\begin{tabular}{clll} 
Resistors & R5 & \(100 \mathrm{k} \Omega\) \\
R1 & \(22 \mathrm{k} \Omega\) & R6 & \(2 \cdot 2 \mathrm{k} \Omega 10 \%\) \\
R2 & \(1 \mathrm{M} \Omega\) & \(R 7\) & \(390 \mathrm{k} \Omega\) \\
R3 & \(22 \mathrm{k} \Omega\) & R8 & \(330 \Omega\) \\
R4 & \(1 \mathrm{M} \Omega \frac{1}{2}\) watt & &
\end{tabular}

Capacitors:
\begin{tabular}{|c|c|c|c|}
\hline C1 & 150pF & C5 \(25 \mu \mathrm{~F} 25 \mathrm{~V}\) & \\
\hline C2 & 1000 pF & C6A \(\}_{16+16 \mu \mathrm{~F}}\) & ectrolytics \\
\hline C3 & \(0.01 \mu \mathrm{~F}\) & C6B \(\} 16+16 \mu \mathrm{~F}\) & \\
\hline C4 & \(0.01 \mu \mathrm{~F}\) & & \\
\hline TC1 & 250pF & ssion trimmer & \\
\hline VC1 & 300 pF & , solid dielectric & \\
\hline
\end{tabular}

\section*{Valves:}

V1 ECC83 V2 6BW6

Diodes:

Potentiometers:

\section*{VR1 \(500 \Omega\)}

D1 \(\}\) Contact-cooled metal D2 \(\}\) rectifiers 250 V 60 mA

\section*{Inductors:}
\(\left.\begin{array}{l}\text { L1 } \\ \text { L2 }\end{array}\right\}\) see text
L.F. Choke 10 H 60 mA

T1 Output transformer ratio 40:1 suitable for mains pentode.
T2 Mains transformer \(\mathbf{2 5 0} \mathbf{- 0}-250 \mathrm{~V} 60 \mathrm{~mA}, 6.3 \mathrm{~V} 3 \mathrm{~A}\).

\section*{Miscellaneous:}

Two B9A valveholders, tagstrip, \(\frac{1}{2} \mathrm{in}\). coil former, chassis, nuts, bolts, solder, wire, 1 Pole 2 Way on/off switch, wire for coils.
\begin{tabular}{lc}
\hline \multicolumn{1}{c}{ COMPONENTS } & FOR MODIFICATIONS \\
Tone Control: & Headphone Reception: \\
\(25 \mathrm{k} \Omega\) potentiometer & Normally open jack socket \\
\(0.02 \mu \mathrm{~F}\) capacitor & \(0 \cdot 1 \mu \mathrm{~F} 400 \mathrm{~V}\) capacitor \\
Wavechange: & \\
3 Pole 3 Way rotary switch, Extra coil formers, Wire \\
for coils, Two 300pF capacitors \\
\hline
\end{tabular}
wire pile wound, with L2, five turns, wound over the top. The former was \(\frac{1}{2}\) in. diameter fitted with an adjustable dust core. The former size is not critical except that the number of turns will need to be adjusted if the former is a different diameter to that specified. A long wave coil would require 140 turns for L1 and around 13 turns for L2. For short wave coverage less turns will be needed and if the wire used is thick enough no former will be required since the turns can be self-supporting. If the diameter is about one inch and the wire 16-20s.w.g. then between \(5-12\) turns for L1 and 1 or 2 turns for L2 will give coverage of 19-49 metres. These turns should be wound side by side on the same axis.
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Double the usefulness of the neat little rig described in the January, 1967 issue

DURING the time this transmitter has been on the air many pleasing and surprising reports have been received on both "Top Band" and " 80 " metres running but 9 W and working into a G5RV multi-band dipole antenna at 28 ft . through a Z-match coupling unit. In all fairness, however, it should be stated that results and reports do depend to a great extent on band conditions at any given time. The modest power available can hardly be expected to combat or flatten heavy QRM often prevalent-particularly at week-ends-but under fair conditions the transmitter performs surprisingly well and enables one to enjoy many interesting QSO's.

As originally described the transmitter is a phone rig (A3 emission) only, suitable for Fixed station or / M working, but the versatility can be increased beneficially to include keying thus enabling the user to work c.w. (Al emission) when necessary.

It is not difficult to include keying facilities in the transmitter; only small changes are required which consist of fitting a voltage stabiliser to the v.f.o. section, adding a suitable key jack socket and adding a switch to disable the modulator.

\section*{Modifications}

Fitting a voltage stabiliser. The inclusion of a type OA2 voltage stabiliser tube to the v.f.o. is obligatory but necessary if "chirp" is to be avoided; chirp is most likely to be found when the transmitter is working "straight through", viz. on "Top Band". The stabiliser chosen has a B7G base and a holder can be fitted between the v.f.o. valve proper and the front panel.

Theoretically, it would seem sufficient to apply a stabilised voltage to the triode section of the


Fig. 1: Skeleton circuity showing position of extra stabilising components.


Fig. 2: This shows the Phone/C.W. switching and key circuitry.

ECF80 valve only and this may be tried by connecting the stabiliser to point "Y" of the original circuit. In practice however, it has been found most beneficial to include both sections of the valve.

The modified "bare bones" circuitry is given here in Fig. 1 and as may be seen three additional components are needed, viz. \(\mathrm{Ry}-3.3 \mathrm{k} \Omega, \mathrm{Cz}-0.1 \mu \mathrm{~F}\) and Vstab. Drive is diminished slightly when these items are added but 1 mA is available and this is adequate.

Adding a key jack socket. By re-positioning the panel lamp and lens, a standard normally closedcircuit type jack socket may be fitted in the vacated hole. It should be connected between the negative terminal of the \(0-50 \mathrm{~mA}\) meter and the chassis; a \(100 \mathrm{k} \Omega\) fixed resistor is also connected across the key jack sockets.

Disabling the internal modulator. Since the internal modulator is not required for c.w. working an additional switch is needed. Referring to Fig. 2 the added switch, SZA/B, and its conneotions may be seen; the key jack socket and its resistor are also shown. Other items are identical with the original circuitry with the exception that R6 is reduced in value to \(3.3 \mathrm{k} \Omega\).

Switch \(S Z\) is a DPDT toggle-type item and is easily located at the rear of the chassis above socket Sk4; it may be mounted on a small L-shaped aluminium bracket.

Provided that all wiring is correct lift the connection from pin 7 of the OA2 voltage regulator clear of the chassis and insert a testmeter set to read \(0-50 \mathrm{~mA}\) in series with the stabiliser. Switch to
—continued on page 146


IN this field the steady migration towards semiconductors continues. Some years ago, H. J. Leak, in his presidential address to the B.S.R.A. observed, that for power outputs of up to 15 watts per channel the valve could no longer compete with the transistor. At the Fair, transistor amplifiers in the hi-fi class were commonly offered with outputs of up to 110 watts, and although it is difficult to appreciate listening to this output in the average living room, it does indicate the advances in transistors. Most manufacturers were not content to state that the equipment was "fully transistorised" but plugged that they were silicon types. So it looks like the trend this year for amplifier enthusiasts is to acquire a "Silicon Solid Status".

The complexity of the units seems to grow each year. One can remember not so long ago being content witht volume, treble and bass. Now one sees miniature Jodrell Bank-type front panels with Low-filter; High-filter; Equalisation; Input selector; Balance; Stereo reverse (should be interesting); Stereo left; Stereo right; Stereo left + right etc.

Stereo was very much in evidence and mostly solid state. The trend here was split right down the middle as regards units. Some were complete with amplifier, preamp and both speakers all in one package. Others had one or both speakers floating. Many speakers and indeed amplitiers were of the "bookshelf" type, usually in a matt wood. Listening to "Uranus" from the Planet Suite on stereo with large enclosures some 3 ft . cube, and then on a couple of the small twelve inch bookshelf cabinets gave a vivid demonstration of the efficiency of the

The Armstrong 426 is an example of the growing complexity of audio units and the tendency towards "integration".
smaller units. They did lack the roundness in the bass, but the reproduction nevertheless was exceptionally good.

Prices varied, but on the whole were high, some very high. Perhaps the common-sense way in buying would be to say-if I'm satisfied with the performance of cheaper equipment then it's pointless to spend more, but if I want the ultimate in quality and my ears can appreciate the difference, then I will pay for quality.

All things considered there was nothing really startling at this year's Audio Fair. Most of the units on show are already displayed in the dealers' windows and have been for some time. Summing it all up: Transistors now outnumbered valves. Stereo is becoming commonplace and trends indicate that before long it could well be stereo only, since the units can receive and/or play mono too. Prices are high but then so is performance, and there are more knobs to twiddle. Bookshelf units are advancing with the advance in the frequency response of smaller speakers.

Perhaps next year we will have vest pocket stereo, but we wonder how they'll fit all those controls in!


\section*{Tape Recorders}

New trends this year in the tape recorder field were hard to find. The most noticeable was that more machines were making use of cassette loading. Also, we noticed fewer low-priced machines and more with comprehensive mixing and dubbing facilities. More are becoming available for vertical operation.

Philips, who pioneered the cassette-loading recorder market in the UK, released another battery-operated machine at the show-the EL 3302. Similar to its predecessors, it has almost double the audio output at 400 mW , and an external loudspeaker socket. The price remains 27 gns . Also from Philips come two mains-operated cassetteloading tape recorders-one stereo and one mono.

The range of Philips pre-recorded "Musicassettes" can be used on all of their cassette-loaded machines, and there are over 100 different mono/ stereo Musicassettes available from the repertoires of EMI, Philips and Pye records.

Grundig's latest cassette-loading tape recorder, the C110, is also a mains-operated machine. Although it measures only \(13 \frac{7}{8} \times 9 \times 4 \frac{5}{8}\) in., it has a two-watt push-pull amplifier and seven-inch eliptical speaker. Using the half-track recording system, it has a recording and play-back time (for DC90 tape) of approximately \(1 \frac{1}{2}\) hours. The technical specification gives a wow and flutter figure of better than \(\pm 0.4 \%\), a frequency range of \(50 \mathrm{c} / \mathrm{s}\) to \(10 \mathrm{kc} / \mathrm{s}\), and a signal-to-noise ratio of better than 45 dB . Grundig claim this machine to be virtually foolproof - click-in cassette loading, simple press-button controls, a green light to indicate the machine is switched on and a red warning light when the recording button is depressed. The price is 48 gns .

Most of the four-track machines shown this year have comprehensive mixing facilities, permitting one to record on one channel while listening to the other. To permit this, three tape heads and independent and play-back amplifiers are necessary. An example is the Truvox R104 at 89 gns . This machine, which has been on the market for some time now, has the facility aptly labelled duo-play.

The Fidela range of four-track tape desks and recorders from the Waltham Electronics Company of Geneva (handled in this country by Denham and Morley Ltd.) attracted a lot of attention for they were on show for the first time in this country. All of these are suitable for vertical or horizontal operation. The recorders have solid-state amplifiers and attractive specifications along with appropriate price tags -75 and 138 gns . The tape decks are also expensive; Model 707 costs 119 gns , but it comes complete with separate record and play-back amplifiers having a \(30 \mathrm{c} / \mathrm{s}\) to \(22 \mathrm{kc} / \mathrm{s}\) frequency response. The other deck, Model 780 at 145 gns. also features adjustable bias for optimum performance with different types of tape.

Among the Telefunken exhibits were the Magnetophon 200 series of vertical and horizontal recorders. The 204 E is a two-speed ( \(3 \frac{3}{4}\) and \(7 \frac{1}{2} \mathrm{in}\).) stereo machine with a frequency range extending up to \(18 \mathrm{kc} / \mathrm{s}\) on the higher speed. This 106 gn . machine has comprehensive mixing facilities.
Another semi-professional performance/stereo machine is the Tandberg Series 6 x . This ' x ' series is similar to earlier models, but incorporate an additional bias head, improved frequency response and


One of the Fidela vertical tape recorders shown for the first time at the Audio Fair.
signal-to-noise ratio-within 2 dB from \(20 \mathrm{c} / \mathrm{s}\) to \(25 \mathrm{kc} / \mathrm{s}\) and a 62 dB signal-to-noise figure on the fastest speed of \(7 \frac{1}{2} \mathrm{in} . / \mathrm{sec}\). Wow is less than \(0.1 \%\) and crosstalk rejection is better than 60 dB . Two and four-track recorders using this deck are offered at 115 gns .
The newest model in the Uher range of professional recorders is the 1000 Report Pilot. .With this machine, one can synchronise sound with film as well as reporting under professional conditions. Features of this \(£ 243\) portable recorder include

Latest in the range of BSR popular tape decks-_The TD20, available with a wide range of stereo or mono head arrangements.


One of the growing range of cassette tape recorders-the new Philips Model EL3302.
stroboscopic tape speed control and switchable equalisation. It has only one tape speed- \(7 \frac{1}{2}\) in./sec.

BSR's latest three-speed tape deck, the TD20, introduced at the end of last year, was prominently displayed. It is available in both stereo and mono versions with two or four-track heads. The control linkage has been improved and only requires the lightest pressure to operate the direct-action keys. Wow and flutter is claimed to be better than \(0 \cdot 15 \%\) on \(7 \frac{1}{2} \mathrm{in}\). \(/ \mathrm{sec}\)., \(0.25 \%\) on \(3 \frac{3}{4} \mathrm{in} . / \mathrm{sec}\)., and better than \(0.35 \%\) on \(1 \frac{1}{8} \mathrm{in} . / \mathrm{sec}\). It will take up to seven-inch reels and there is provision for a third head.

Tape Recorder Developments Ltd., who announced their first tape deck just over a year ago had on show seven variations of their TRD 1 deck, and silicon semiconductor electronic units to complete a hi-fi system-with any of the deck variations. As an indication to the type of deck, the wow and flutter specification is as follows: \(0.04 \%\) at \(30 \mathrm{in} . / \mathrm{sec}\).; \(0.05 \%\) at 15 in . \(/ \mathrm{sec}\).; \(0.08 \%\) at \(7 \frac{1}{2} \mathrm{in}\). \(/ \mathrm{sec}\).; \(0.13 \%\) at \(3 \frac{3}{4} \mathrm{in} . / \mathrm{sec}\).; \(0.2 \%\) at \(1 \frac{7}{8} \mathrm{in} . / \mathrm{sec}\).; and \(0.35 \%\) at \(\frac{15}{7} \mathrm{in} . / \mathrm{sec}\).

Tape Recorder Spares Limited had their usual wide range of pre-packed leads, plugs and accessories. Often it is not realised that this company deals with more than tape recorder accessories. In fact, they have a very wide range of connectors that could well solve many problems of the hi-fi and audio enthusiasts.

\section*{Microphones and Pickups}

It is a very far cry from the carbon granules of yesteryear to the array of sophisticated microphones now available on the market; microphones of range and diversity to meet all requirements and depths of pocket.

One of the new developments noted at the Fair was a dynamic unit by AKG which combines two moving coil capsules, one covering high frequencies, one covering low frequencies. Philips also


A trend in speaker enclosures-the Celestion Ditton 3-element 15 -watt system for bookshelf mounting.
had a unit with two moving coil units; this was a stereo type (Model EL179) in which the two m.c. units are detachable.

Another interesting model was the Sennheiser unit which combines the directional properties of the gun microphone and the high performance of a condenser (or should we say capacitor?) micro-


Parmeko stereo record reproducer incorporating the latest in pickups-the Miniconic transistor cartridge.
phone. It is in fact, a transistorised r.f. condenser type.
It is impossible in this space to detail the many mentionable microphones on show, but those which attracted our attention included the new series of subminiature ribbon units by Lustraphone, the new Unisphere models by Shure which are based on the Unidyne dynamic cardioid type, the three new dynamic models from M.B. Mikrofonbau and the latest high-quality cardioid microphone from STC -who also showed for the first time the 4119 hyper-cardioid ribbon microphone.
Pickups, cartridges and gramophone decks, as to be expected, showed a general tendency to higher efficiency and slicker presentation. The most unusual exhibit was the new semiconductor stereo pickup introduced by Miniconic.

Insensitive to hum fields and turntable noise, the pickup is claimed to have a power output 40 dB greater than a magnetic cartridge, 20 dB greater than a ceramic cartridge. It functions by modulating the flow of d.c. provided by the amplifier power supply through a semiconductor strain gauge element (the resistance of which varies as the stylus is flexed) to produce signal current variations. In other words, energy is provided by an external source and not, as conventionally, by the record groove. The makers claim a frequency response of an octave below and two octaves above audible range, reduced record wear and chatter, a cleaner signal with increased dynamic range. The inrst British stereo equipment to incorporate this revolutionary pickup is the System 22 system marketed by Parmeko.

Also new at the Fair was the range of moving magnet stereo cartridges by Audio Technica, the new Studio 1000 range of amplifiers, tuners and speaker units by Braun and the ffss Mark 4 heads and cartridges by Decca. Focus of interest on the Garrard stand was their new Model 50 automatic turntable unit which incorporates pause and cue control, tubular pickup arm and calibrated force adjustment.

\title{
repairing radio sets
}

\section*{PART 3}

\author{
GORDON J. KING
}

Having heard from H. W. Hellyer (last month) on the use and choice of tools and service equipment we now continue with fault symptoms in the "electronics" of the animal and thence to their diagnosis.

Part 1 investigated the first two or three stages of a typical valved receiver. These stages collectively are often referred to as front ends, being composed of r.f. amplifier (if the set has one), mixer and local oscillater. Modern a.m./f.m. sets have two front-ends, one for medium-frequency (and possible short-wave) a.m. and another for v.h.f./f.m.

\section*{FRONT-END NORMAL}

Assuming that first tests failed to reveal any conclusive defect in the front-end, we can conclude that the mixer, or that section of the frequency changer, is delivering off-the-air signals converted to i.f. as they are tuned in by the set's dial. Something, then, is preventing these signals from reaching the detector and later stages. That is, assuming the symptom is the easy one of "no signals" or "set dead".
The best plan under these circumstances is to apply a modulated signal at the set's i.f. to the input of the first i.f. amplifier. A straightforward valved set usually has a single i.f. amplifier stage, a typical circuit being shown in Fig. 3-1.

Here the control (first) grid of the i.f. amplifier valve receives an i.f. signal from the secondary winding of the first i.f. transformer, whose primary


Fig. 3-1: Typical a.m.-only i.t. stage, showing three prime tests.

is loaded into the anode circuit of the mixer or frequency-changer valve. It should be understood that the nature of this testing for a "dead set" starts at the aerial input, works through to the frequencychanger, checks the local oscillator (as in Part 1) and then goes on to the i.f. stages, commencing at the input of the first i.f. amplifier valve (Fig. 3-1).

Assume that we have a signal generator and tune it to the set's i.f. (recent models \(470 \mathrm{kc} / \mathrm{s}\), earlier models \(465 \mathrm{kc} / \mathrm{s}\) ), then switch on the audio modulation and apply the signal to the control grid of the first i.f. valve. Signal continuity from this grid to the loudspeaker should give a modulated tone output. If there is no response the next move is to check the i.f. stage up to the detector input. If discontinuity remains, then the trouble is either in the detector or audio stages (to be considered in Part 5).

Useful first-action tests are (i) check that the i.f. valve heater is alight (change valve and/or check heater supply circuit if not) (ii) check the valve envelope for temperature with a hand (a "cold" valve-with heater alight-could indicate lack of anode and screen grid current) and (iii) try tapping the valve with the set running to establish the possible presence of internal inter-electrode shorts or open-circuits.

\section*{BASIC D.C. TEST}

If these tests give no clues to the fault, a more scientific approach will be necessary. A good test for valve emission is to measure the voltage across the cathode resistor (see Test 1). A valve normally operating will yield about 2.2 volts d.c. across this resistor. A test voltage appears because the sum of the anode and screen-grid current passes through the cathode resistor, and this develops a voltage drop across it of magnitude depending (a) on the value of the resistor and (b) on the current value.

It is easy to find the cathode current (in mA) by dividing the voltage measured (in volts) by the value of resistance in kilohms (thousands of ohms). For example, 4 volts measured across \(500 \Omega(0.5 \mathrm{k} \Omega)\) signifies a current of 8 mA .

If this first basic or "key" test indicates cathode current, we are sure that: (i) the valve has emission, (ii) its heater is aglow, (iii) the valve has both anode and screen grid voltage and (iv) the general d.c. conditions of the stage are reasonable-if not normal. A more exacting indication on the d.c. conditions can be obtained from a knowledge of the anode and screen grid (i.e., cathode) current of the valve in the circuit. Such operating parameters are
usually given in the service sheet, manual, or valve data book.

Abnormally low cathode current could mean (a) low emission valve, (b) low screen grid voltage, (c) low anode voltage or (d) reduced heater current. (This is often overlooked.)

To establish (a), Tests 2 and 3 (see Fig. 3-1) would be made, and if the anode and screen grid voltages are reasonable (refer to service sheet, if possible), check the valve either by substitution (often the best way) or with a valvetester. Typical values are anode 225 volts and screen grid 100 volts.
So far we have established that the i.f. signal cannot be passed through the set from the control grid of the i.f. amplifier valve and, assuming Tests 1,2 and 3 to be positive, that the d.c. conditions of the stage are reasonable.

There is a remote chance that the valve has some internal short or open-circuit which is failing to affect the d.c. conditions yet preventing the passage of signal. A sharp tap on the envelope of the valve with a screwdriver handle may prove something here; but valve substitution is much more conclusive a test in a case like this.

Some enthusiasts may not possess a signal generator or other equipment, yet may wish to try their hands at radio repairs. Where possible, therefore, suggestions based on instrument-less testing will be included. One instrument, however, is indispensable and that is a good quality multirange testmeter with a d.c. sensitivity not less that 10,000 ohms/volt (bearing in mind that low voltage and current readings may have to be made in transistor equipment).

Signal continuity in the i.f. stage can sometimes be proved by conneoting an aerial to the control grid. This should pick up random signals in the i.f. band and reproduce them in the loudspeaker. Another dodge is connecting the contact points of a lowvoltage electric buzzer between chassis and the control grid via a 100 pF capacitor. The impulsive "signal" produced by the working buzzer contains many harmonic components well into the i.f. band, and signal continuity is revealed by a harsh buzz in the speaker. This, of course, also proves the detector and audio stages at the same time. Special transistor, pulse generating signal continuity test instruments are also available commercially, but there is nothing to beat a good modulated signal generator.
I.F. stage continuity can also be vaguely assessed by rubbing the tip of a screwdriver blade on the control grid pin of the i.f. valve while holding a finger in contact with the metal blade. Good response in the i.f. channel is then indicated by fairly loud crackles from the speaker when the test is performed.

\section*{DYNAMIC TROUBLE}

We now assume that the d.c. conditions are normal, yet the signal fails to pass through the stage. This is often called "dynamic trouble", signal rather than d.c. A prime factor here is misalignment of the i.f. transformers. These are best checkedand aligned-by a modulated signal generator, as explained in Part 1 (April issue).
It will be recalled that the signal is applied to the signal grid of the frequency-changer valve (at fairly high level if the cincuits are well out of
alignment) and then the second and first i.f. transformers adjusted-secondary and then primaryaiming for maximum output at the detector or audio stage.

\section*{ALIGNING THE I.F.'s WITHOUT INSTRUMENTS}

It is possible to align the i.f's. without a signal generator, assuming that the front-end circuits are in alignment. The technique is first to bring the i.f. windings to exactly the same frequency, irrespective of the actual frequency. This can be done by "clicking" the screwdriver blade on the frequencychanger signal grid or by the use of a buzzer (as already explained) or other pulse-type harmonic generator and adjusting the i.f. trimmers or cores, one after the other, until maximum output is attained. The circuits will all be tuned to the same frequency, not necessarily the correct one.
Next, apply an aerial signal with the set tuned to the longwave Light Programme. Since the i.f's. will most likely not be tuned to their correct frequency, the Light Programme will come in well off tune and possibly weakly, so full volume setting must be used.
The i.f's. can then be tuned nearer to the correct frequency by adjusting the main tuning so that the Light Programme can still be heard yet may still be off tune although closer to the actual 1,500 metre mark on the dial. The i.f's. should again be peaked in turn for maximum signal output and the process repeated until the i.f's. can be peaked with the tuning spot-on the station setting on the main dial. The i.f's. should then be in fairly reasonable alignment.
A dynamic fault can exist due to a short-circuit across one (or more) of the i.f. transformer windings. Note that an open-circuit, at least in the primary, would be brought to light by the d.c. testing earlier described. Typical trouble is a short across a trimmer (if used) or fixed parallel tuning capacitor (i.e., \(\mathrm{Cl} / 2 / 3 / 4\) in Fig. 3-1). A short can also occur across an internal tag panel, and such possibilities can only be examined by taking the screening can from the transformer. Incidentally, an open-circuit capacitor across a winding will be revealed during the alignment process by that particular tuned circuit failing to peak at the correct frequency.
If tuning is by a trimmer capacitor, the tendency towards maximum output will occur with the trimmer fully compressed (assuming that there is also a fixed trimmer), while if tuning is by dustiron slug, the slug will be fully in the core and still not tuning the winding properly. Incorrect i.f. \(\star 2\) alignment aggravates adjacent channel interference effects, and these will be recognised from Symptom 2 on the record issued free with the April issue.

A fault typical of i.f. transformers is intermittency in the winding(s) or parallel capacitor. The primary winding (carrying h.t. current) is the one that often goes down in this way, but on some transformers leakage between primary and secondary is possible. Symptom 5 on the record typifies the noises \(\star 5\) that can be expected from this trouble. To see whether the fault is in the first or second i.f. transformer, the control grid of the i.f. valve


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can be shorted direct to chassis. If the symptom persists, it is definitely not in the first i.f. transformer or in the front-end sections.

It may be a good idea to short out the secondary of the second i.f. transformer at this juncture to prove the audio section. If the noise effects cease, then the second i.f. transformer is almost certainly responsible. If they persist, the audio stages should be investigated (dealt with in Part 5).

If intermittency in the primary winding is responsible, it is often possible to "see" this in terms of a flickering pointer when the voltmeter is connected as for Test 2.

\section*{I.F. INSTABILITY}

Oscillation in an i.f. stage can be brought about by incorrect i.f. alignment. Some sets are sensitive when the windings are peaked, and if they are the \(\star 1\) amplifier could change into an oscillator and produce the effect of Symptom 1 on the record. This kind of set requires so-called staggertuning in which one winding is detuned relative to the other on each transformer, but not sufficiently to reduce the sensitivity or to encourage adjacent channel interference.
Instability can also result from a bad valve (old valves with sprayed-on gold-coloured conductive coating were troublesome in this respect, but there are very few of these about now!) and from an open-circuit screen grid capacitor (C5 in' Fig. 3-1).

An open-circuit in the cathode bypass capacitor (C6 in Fig. 3-1) will usually result in reduced sensitivity rather than instability owing to negative feedback effects. A set with an electrolytic in position C7 in the circuit could also go low-gain due to its open-circuit.
Other troubles that occur in the i.f. stage are (a) noise (Symptom 5) due to badly seating valves and/or dirty valve pins and faulty sockets, (b) burn\(\star 5\) ing resistors due to a shorting bypass capacitor (i.e., R1 would overheat due to C5 shorting, or R2 due to C7 shorting), (c) overloading due to \(\star 4\) an a.g.c. fault (Symptom 4) to be considered later and (d) intermittent operation due to a badly soldered connection, bad valve and poor connection of valve pins with its holder sockets. Valve bad seating can often be brought to light by wriggling the valve in its holder while the set is running.

\section*{A.M./F.M. I.F. STAGE}

All that has so far been said applies equally to the i.f. stage employed in a.m./ f.m. sets. From Part 1 it will be recalled that sets of this mode employ two i.f. transformers in series, one tuned to \(470 \mathrm{kc} / \mathrm{s}\) for a.m. and the other to \(10.7 \mathrm{Mc} / \mathrm{s}\) for f.m.

An i.f. stage typical in this respect is shown in Fig. 3-2. This shows that the basic d.c. parts of the circuit are almost identical to those in Fig. 3-1. The valve is a more modern version since it has to provide reasonable gain at \(10.7 \mathrm{Mc} / \mathrm{s}\) as well as at \(470 \mathrm{kc} / \mathrm{s}\), and the voltages to be expected on a valve of this kind are shown on the diagram. Alignment of the a.m. transformers is performed first, and
these then present the correct impedance to the much higher frequency f.m. transformers, allowing their subsequent alignment.

The control grid of the valve is fed from the secondary windings of the first set of i.f. transformers (which are also in series with each other), and in some sets there is a switch to short out the primary of the first f.m. transformer when the set is set to a.m. working.

It may be remembered from Part 1 that on f.m. the a.m. mixer section of this kind of set works as an additional i.f. amplifier with


Fig. 3-2: This kind of i.f. stage is foundin a.m. /f.m. receivers. the local oscillator section switched off. This gives another f.m. transformer, which is usually located in the v.h.f. tuner section (f.m. front-end).

Dynamic testing through this dual-type of i.f. amplifier follows the practices already described, and the fact that the circuit is normally responsive to two widely differing i.f. signals means that failure of one channel only cannot be caused by a valve fault or incorrect d.c. conditions. The reason is often related to misalignment of the affected channel or trouble in the appropriate i.f. transformer section.

\section*{DETECTOR AND A.G.C.}

Now let us look at the detectors, starting with a.m. circuits. A detector a.g.c. circuit in common use is shown in Fig. 3-3. This employs a double diode-triode valve, but only the two diodes interest us at this time; the triode is used in the audio stages and will be considered in Part 5.

The detector is nothing more complex than a diode connected in series with the secondary winding of the second i.f. transformer, along with its


Fig. 3-3: An a.m. detector and a.g.c. circuit, showing a test for a.g.c.
load. It looks much more involved, however, when tied up in a complete circuit Fig. 3-3).

The detector diode is D1 and its load is R1 and R2 in series, with the bottom end returned to valve cathode instead of chassis. This is to avoid biasing the diode by the voltage dropped across the cathode resistor R3 when the triode is passing current. The audio signal thus appears across R1 and R2, and it is tapped-off at their junction. C 1 and C2 are i.f. filter capacitors, taking away the residual i.f. signal, leaving only the audio component.

The i.f. signal from the anode of the final i.f. amplifier valve is passed to the second (a.g.c.) diode (D2) through the coupling capacitor C3. Rectified i.f. current thus flows through R4 and R5 and a d.c. voltage is developed across these resistors of a magnitude governed by the strength of the i.f. signal applied to the diode. This represents the a.g.c. bias, and since its full strength is not required a suitable level is tapped off the potential-divider R4/R5. This charges C4 and a time-constant is formed with R5. Residual i.f. signal is also bypassed by C4.

On the a.g.c. line therefore, is a negative potential (with respect to chassis) which is used as extra grid bias for the i.f. amplifier and frequencychanger (mixer section) valves. As the mutualconductance (and hence stage gain) is determined by the amount of grid bias-the greater the bias the less the gain-the overall amplification of the signal circuits is automatically regulated by the strength of the signal. Rapid fading is also combated by the time-constant on the a.g.c. line.

\section*{FAULTY A.G.C.}

One fault which can develop in the detector/a.g.c. stages, and cause bad overloading, is open-circuit of \(\star 4\) C3. This effect is clearly illustrated in Symptom 4 of the record and, apart from distortion due to "envelope distortion", intermodulation troubles can occur on strong signals giving a background whistle accompaniment.

A conclusive a.g.c. test is shown in Fig. 3-3 at Test 4. Here a voltmeter is used to measure the actual a.g.c. voltage produced by the signal. There is no point in attempting this test with a voltmeter of less than \(10,000 \Omega / \mathrm{V}\) sensitivity, however, for the meter would swamp the circuit and give virtually no reading even on a very strong signal. A reading up towards 5 volts should be obtained at the point indicated on the circuit on a strong signal.

In some sets the a.g.c. voltage is transferred to the control grids through very high (order of megohms) resistors, so even a highly sensitive meter would give very little reading at these points. A valve voltmeter or equivalent transistor instrument would, however, be suitable.
A noteworthy point of the a.g.c. circuit is that it is delayed. This comes about by the biasing given to the a.g.c. diode due to triode current flowing through the cathode resistor. Thus, the cathode is at some voltage positive with respect to D2 (since in this case D2 is returned to chassis through R4/5), and this means that D2 will not conduct until the signal reaches the delay level given by the bias. This means that the set's gain is always at maximum on weak signals.
The detector itself rarely develops faults except perhaps when an i.f. filter capacitor goes open-


Fig. 3-4: The ratio-detector formed by two isolated diodes in a triple-diode-triode valve. A ratio detector test is shown.
circuit. This can aggravate instability and introduce whistles. Since the diodes are working at very low power they rarely fail, even though the triode may go low emission.

\section*{RATIO-DETECTOR}

In a.m./f.m. sets, the detector valve is usually a triode (for audio) with three diodes, one with its own cathode and two using the common triode cathode. One of the diodes common to the triode cathode is used as an a.m. detector, which is often arranged to provide a.g.c. as well, while the other diode, in conjunction with that with its own cathode, is used in a ratio-detector for f.m., as shown in Fig. 3-4.

Here D1 has its own cathode and D2 a shared cathode. The ratio-detector circuit is formed by D2 anode going to one side of the ratio-detector transformer secondary and DI cathode to the other side. D1 anode and D2 cathode are then connected across the d.c. load of the detector (as is conventional practice) comprising R1/C1. The audio is developed across \(C 2\) connecting to the third winding on the transformer. This looks a bit messy in this form but if it is worked out into a different pattern it will be found to conform to the ordinary ratiodetector circuit.
A good test for this kind of detector is to measure the voltage across the d.c. load, as shown by Test 5 in the circuit. With a correctly working circuit, up to 20 volts will be measured across the load when the f.m. set is tuned to a strong transmission.

Difficult tuning and poor interference suppression is often caused by Cl of the load going down or becoming open-circuit. This would not be indicated by the test across the load and a new capacitor (about \(4 \mu \mathrm{~F}\) electrolytic) should be hooked on as a trial. Shorting Cl would, of course, prevent a voltage reading and certainly kill normal working of the detector.
If R1 goes high in value the effect is a sort of "overhang" on the f.m. tuning, it being difficult to establish quickly the correct tuning point.

This triple-diode-triode valve can cause a hum or buzz on f.m. only under certain fault conditions \(\star 3\) (not unlike the first interference effect in Symp3 tom 3 of the record). The valve may not immediately be suspected since a.m. is invariably unaffected, but a substitution test soon shows that the valve is to blame.

To be continued

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\title{
dual function sicmat cenerator \\ 
}

NEXT to the multi-range testmeter probably one of the most useful items of equipment in the amateur workshop is a generator of signals covering a wide frequency spectrum. While such an instrument can be quite complex and costly, for most amateur requirements a simple, stable, modulated oscillator is sufficient for most purposes. With the aid of such an oscillator, alignment of receivers is easily carried out and the degree of uncertainty associated with trial and error methods eliminated. Apart from this prime function the signal generator is an invaluable aid to fault tracing in receivers.

The basic requirements of an oscillator suitable for alignment purposes are as follows. It should be stable and not require recalibration at frequent intervals. Changes in supply voltage should not have an adverse effect on the oscillator frequency. Radiation of energy other than by the output socket should be reduced to a minimum. Finally, the output of the oscillator should be controllable. Although none of these desirable features is easy to obtain and
is reflected in the relatively high cost of commercial instruments, nevertheless, by careful attention to screening and suitable choice of oscillator, it is possible to construct a generator which approaches these ideals.

The signal generator described in this article has been designed with these features in mind. As well as performing all the usual functions of the normal oscillator, a further valuable feature enables the experimenter to extend the scope of the instrument to inductance and capacitance testing. Tbis aspect of the design will be dealt with briefly in the latter part of the article.

\section*{CIRCUIT DESCRIPTION}

An examination of the circuit given in Fig. 1 will show that both the radio and audio frequency oscillators are of the "two terminal" type. In each case a double triode is employed, one section being used as a cathode follower and the other as a grounded grid amplifier. Energy in the correct phase is fed

Fig. 1: Circuit diagram of the signal generator including the power supply unit. The coupling capacitor C2 may require slight adjustment as described in the text.


\section*{Dual function signal generator.} Figure 2
A: Dimensions for a suitable cabinet.
B: Chassis drilling details.
C: Cardboard template for mounting coils.
D: Front panel drilling details.


Hotes \(A 3 / 4\) diameter Holes B \(1 / 4^{2}\) diameter Holes C 4 BA clearance Holes D 6BA clearance



Holes A \(1 / 8^{\prime \prime}\) diameter
Holes \(B \quad 1 / 4^{\prime \prime}\) diameter
Template \(13 / 8\) diameter


\section*{0}

Hole A 7/8 diameter
Holes \(B \%_{8}^{\prime \prime}\) diameter.
Holes C 4 BA clearance
Holes D 6 BA clearance
back from the second section of each triode into the grid circuit in such a way that continuous oscillation is maintained. The coupling capacitor, C 2 , between the anode of the section triode section of V1 and the grid of V1 is rather critical. Since valve and component tolerances vary somewhat, it may be found that some experiment is necessary to achieve optimum results. Generally a value between 10 and 50 pF will be adequate. An indication that the value is too high will be shown by violent squegging.

Anode modulation of V1 is achieved by connecting the h.t. supply to V 1 in series with the primary of the audio transformer T1. The audio component developed in the secondary of T1 is inductively transferred to the primary winding of the transformer. An audio signal for amplifier testing is taken from the cathode of V2. Selection of the desired signal, whether r.f., modulated r.f. or a.f. is by means of switch S 2 .
The frequency span of the generator is from \(200 \mathrm{kc} / \mathrm{s}\) to \(30 \mathrm{Mc} / \mathrm{s}\). This range is covered using five inductors, L1 to L5, taken from the Denco range of iron cored coils. The screening cans supplied with these coils have been retained since they help materially in reducing extraneous radiation. Power requirements for the unit are quite modest and any small transformer with an output of 200-250 volts
at 20 mA and 6.3 volts at 1 ampere is adequate. The specified audio transformer in the modulating section has a primary rated at 8 mA and if any other type of transformer is substituted it must have a similar rating.

Although in the interests of compactness, miniature type valves have been specified, there is no reason why older types such as the octal based 6SN7 or 6SL7 should not be used. These two valves function perfectly satisfactorily in this circuit without any alteration in component valves. Naturally the use of the larger octal valve holders will necessitate some chassis dimensions changes.

\section*{CONSTRUCTIONAL DETAILS}

The generator is built on a 9in. x 5 in . universal chassis. Full drilling and mounting details are given in Fig. 2. The front panel drilling dimensions given in Fig. 2D are applicable to the specified Eddystone dial. A flexible coupler is used to connect the epicyclic drive mechanism to the variable capacitor. When fitting the drive to the capacitor spindle care must be exercised in the alignment of the spindle and drive mechanism since slight misalignment will mar the smoothness of the drive system. Although many generators, both amateur and commercial, use a direct drive system, the use of a slow motion drive


Fig. 3: Under chassis layout and wiring diagram. Note, tags marked MC are bolted directly to chassis.
enables more precise settings to be obtained.

The inductors, L1 to L5, together with the screening can lids are mounted ensuring that the holes in the chassis and can bases coincide. The cardboard template shown in Fig. 2C may be used to facilitate drilling of the chassis and can bases. Since the coil formers and associated plastic securing nuts are of polystyrene it is important that overtightening of the securing nuts is avoided.

When mounting the two valve holders, make sure that they are correctly orientated as shown in Figs. 3 and 4. The completely wired chassis is also shown in the same figures. On all coil ranges the primary windings are shorted out and connected via the earthy end of the grid coil to earth. It may be found on ranges 4 and 5 that the coils have wire ended terminations. If this is the case the grid wire must be insulated with a short length of sleeving before passing it through the chassis.

Wiring of the unit is straightforward although care must be exercised when soldering connections to the coil pins. Excessive and prolonged heating of the pins will lead to distortion of the polystyrene


Fig. 4: Layout of components above chassis.
rear of the box is covered with a nominal 11 in. \(x\) 8in. aluminium top plate taken from the universal chassis range. When covering the interior of the box with foil make sure sufficient overlap is allowed at the edges so that intimate contact between the front panel and back plate is obtained. This method of construction was adopted in the interests of cheapness, and a metal box would be preferable.

Calibration based on comparison with signals of known frequency has been given many times in Practical Wireless and although no attempt

TABLE 1
\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline \multicolumn{2}{|l|}{Range 1} & \multicolumn{2}{|c|}{Range 2} & \multicolumn{2}{|r|}{Range 3} & \multicolumn{2}{|r|}{Range 4} & \multicolumn{2}{|r|}{Range 5} \\
\hline \(f \mathrm{kc} / \mathrm{s}\) & Dial & \(f \mathrm{Mc} / \mathrm{s}\) & Dial & \(f \mathrm{Mc} / \mathrm{s}\) & Dial & \(f \mathrm{Mc} / \mathrm{s}\) & Dial & \(f \mathrm{Mc} / \mathrm{s}\) & Dial \\
\hline 200 & 98 & 0.6 & 98 & \(1 \cdot 8\) & 98 & \(5 \cdot 5\) & 98 & 9 & 93 \\
\hline 250 & 72 & 0.7 & 80 & \(2 \cdot 0\) & 85 & 6.0 & 85 & 10 & 79 \\
\hline 300 & 54 & 0.8 & 65 & \(2 \cdot 5\) & 62 & 7.0 & 69 & 12 & 62 \\
\hline 350 & 41 & 0.9 & 54 & \(3 \cdot 0\) & 45 & 8.0 & 57 & 14 & 49 \\
\hline 400 & 30 & 1.0 & 45 & \(3 \cdot 5\) & 31 & 9.0 & 47 & 16 & 38 \\
\hline 450 & 21 & \(1 \cdot 1\) & 37 & \(4 \cdot 0\) & 22 & \(10 \cdot 0\) & 39 & 18 & 30 \\
\hline 460 & 19 & \(1 \cdot 2\) & 31 & \(4 \cdot 5\) & 14 & 11.0 & 32 & 20 & 23 \\
\hline 470 & 18 & \(1 \cdot 3\) & 25 & \(5 \cdot 0\) & 8 & \(12 \cdot 0\) & 26 & 22 & 18 \\
\hline 500 & 14 & \(1 \cdot 4\) & 20 & \(5 \cdot 5\) & 4 & 13.0 & 21 & 24 & 13 \\
\hline 550 & 8 & 1.5 & 15 & - & - & 14.0 & 17 & 26 & 9 \\
\hline 600 & 3 & \(1 \cdot 6\) & 11 & - & - & \(15 \cdot 0\) & 13 & 28 & 5 \\
\hline - & - & 1.7 & 7 & - & - & 16.0 & 10 & 30 & 2 \\
\hline - & \(\stackrel{-}{-}\) & \(1 \cdot 8\) & 4 & - & - & \(17 \cdot 0\) & 7 & - & - \\
\hline
\end{tabular}

The table shows approximate dial readings against frequency. The coils should be adjusted as advised in the text in conjunction with Table 2.
formers. On completion of the wiring check the resistance between the h.t. line and chassis. A reading of approximately \(500 \mathrm{k} \Omega\) should be obtained. A much lower reading should be investigated and any obvious faults remedied.
The writer housed the instrument in a wooden box lined with aluminium foil. Constructional details are given in Fig. 2A and are self explanatory. The
will be made to give exhaustive details a brief description is given for the benefit of the newcomer.

The method requires a receiver, not necessarily accurately calibrated, covering a wide frequency range. After setting the receiver to a transmission of known frequency, the generator is adjusted to zero beat with the known frequency. By choosing an adequate number of frequencies for each band, a
graph may be drawn of frequency versus dial readings. Care must be exercised during this procedure since it is quite easy to confuse harmonics with the fundamental frequency. If a superhet receiver is used for calibration purposes, additional difficulties may arise, particularly on frequencies above approximately \(10 \mathrm{Mc} / \mathrm{s}\). Simple superhets with an intermediate frequency of \(450 \mathrm{kc} / \mathrm{s}\) and without adequate selectivity prior to the mixer, will almost certainly suffar from second channel interference. As an example, consider a receiver of this type tuned to a known frequency of \(15 \mathrm{Mc} / \mathrm{s}\). If, as is generally the case, the receiver oscillator is tuned to the higher frequency side of \(15 \mathrm{Mc} / \mathrm{s}\), then in order to give an intermediate frequency of \(450 \mathrm{kc} / \mathrm{s}\) the receiver oscillator will be set at \(15 \cdot 45 \mathrm{Mc} / \mathrm{s}\). A little thought will show that a transmission on \(15.90 \mathrm{Mc} / \mathrm{s}\)

TABLE 2
\begin{tabular}{|c|c|c|}
\hline Range & \begin{tabular}{c} 
Frequency Range \\
\(\mathbf{M c / s}\)
\end{tabular} & Core Turns \\
\hline 1 & \(0.2-0.6\) & \(5 \frac{1}{2}\) \\
2 & \(0.6-1.8\) & 6 \\
3 & \(1.8-5.5\) & \(12 \frac{1}{2}\) \\
4 & \(5.5-17.0\) & 12 \\
5 & \(9.0-30.0\) & 20 \\
\hline
\end{tabular}

For approximate calibration the coil cores are unscrewed to their fullest extent and then screwed in. The number of revolutions is shown in the table.
will equally give rise to an i.f. of \(450 \mathrm{kc} / \mathrm{s}\). In terms of the generator calibration this means that when the generator is tuned from the low frequency end a first response will be obtained at \(15 \mathrm{Mc} / \mathrm{s}\). Further tuning of the generator will give a further response when the generator frequency is \(15 \cdot 9 \mathrm{Mc} / \mathrm{s}\). In general terms, for each receiver setting on the high frequency ranges, two generator responses will be evident, one when the generator is set to the actual frequency, and a second in which the generator is set to this frequency plus twice the i.f. of the receiver. Although all this may appear rather formidable, in practice the actual calibration of the higher frequency ranges is quite simple and provided the foregoing is borne in mind, no real difficulty should arise. In any case, a graphical check will reveal any errors.

\section*{APPROXIMATE CALIBRATION}

For those constructors who feel hesitant about this procedure and have no receiver covering the whole gamut of frequencies the following approximate calibration will enable them to make a start. The iron cores of each coil are gently unscrewed to their fullest extent. Do not apply undue force. The cores are then screwed back into the formers the number of complete turns shown in Table 2. The calibration chart shown in Table 1 is applicable to this procedure. If this method is adopted it is imperative that the specified coils are used and the wiring lay-out of Figs. 3 and 4 followed as closely as possible. It must be stressed that the foregoing method is of an approximate nature and is only intended as a preliminary aid to calibration and as a help to the constructor who has no suitable

Resistors:
\begin{tabular}{ll} 
R1 \(1 \cdot 2 \mathrm{k} \Omega\) & R5 \(5 \mathrm{k} \Omega 5\) watt \\
R2 \(22 \mathrm{k} \Omega\) & R6 \(400 \Omega\) \\
R3 \(2 \cdot 2 \mathrm{k} \Omega\) & R7 \(400 \Omega\) \\
R4 \(47 \mathrm{k} \Omega\) & VR1 \(10 \mathrm{k} \Omega\) carbon pot \\
All fixed resistors 1 & watt except where otherwise \\
specified &
\end{tabular}

Capacitors:
\begin{tabular}{llcccc} 
C1 & 10pF & C4 & \(0.01 \mu \mathrm{~F}\) & C7 & \(32 \mu \mathrm{~F}\) \\
C2 & 20 pF & C5 & \(0.01 \mu \mathrm{~F}\) & C8 & 200 pF \\
C3 & \(0.0015 \mu \mathrm{~F}\) & C6 & \(32 \mu \mathrm{~F}\) & C9 & 400 pF
\end{tabular}

\section*{Variable Capacitor:}

VC1 300pF Jackson E1
Valves:
V1 ECC82 V2 ECC82

Inductors:
Chassis mounting types
L1 Denco Maxi 0 Yellow Range 1
L2 Denco Maxi \(Q\) Yellow Range 2
L3 Denco Maxi 0 Yellow Range 3
L4 Denco Maxi 0 Yellow Range 4
L5 Denco Maxi \(Q\) Yellow Range 5
RFC: See text
T1 Intervalve type 3:1 ratio
Radiospares 8 mA rating

\section*{Mains Transformer}

T2 Osmabet 230v 45mA 6.3v 1 A

\section*{Miscellaneous:}

MR Metal rectifier contact cooled 250 V 50 mA B9A Skirted valve holders (2), B9A screens (2), Coax sockets (4), 2P 6W switch S1a, b; 2P 3W switch S2a, b; SPST switch S3, Universal chassis \(9 \times 5 \times 3\), Home Radio Aluminium panel \(10 \frac{3}{4} \times 7 \frac{1}{8}\) (2), DialEddystone 598 (Stratton), Flexible shaft coupler; knobs, sleeving, coaxial cable, etc.
reference standard. More accurate calibration may be carried out at a later stage. When the finalised calibration has been completed the five scales of the dial may be marked in with indian ink.

\section*{DUMMY AERIAL}

A suitable dummy aerial for use in conjunction with the signal generator during receiver alignment is given in Figs. 5 and 6. This dummy aerial is satisfactory for frequencies between \(150 \mathrm{kc} / \mathrm{s}\) and \(2 \mathrm{Mc} / \mathrm{s}\). For the higher frequencies up to \(30 \mathrm{Mc} / \mathrm{s}\) the simple form shown in Fig. 7 is recommended.

In each case the dummy aerial may be mounted inside a discarded tobacco tin as shown in Fig. 5. The \(20 \mu \mathrm{H}\) choke used in the medium frequency version consists of 70 turns of 34 gauge enamelled wire close wound on a \(\frac{z}{8} \mathrm{in}\). diameter former. The remaining details given in Fig. 5 are self explanatory.

A feature of the generator not generally available
-continued on page 142


THIS design offers simplicity coupled with versatility. The tester will check p-n-p or \(n-p-n\) transistors for leakage (I'co), a.c. and d.c. gain. The circuit has been arranged to minimise the switching and consequently enables the cheaper and more easily available types of switch to be used. By careful perusal of the advertisements in this magazine it could, at the time of writing, be built for about thirty shillings.

\section*{Circuit details}

Having now discussed what it does and how much it will cost, let us turn to the question of how it works. Basically, a measured d.c. current is fed into the base of the transistor under test, and then the collector current is measured. The resistance of VR1 controls the base current, while R2 performs the function of preventing this current from


Fig. 1 (above): Basic circuit of the tester.


Fig. 2 (left)s Modification for testing n-p-n transistors.
Fig. 3 (right): Calibration of the unit.

\section*{SIMPLE TRAM!}

Transistors are now readily available from variou manufacturers' surplus units, and some of these ar here enables some of the more useful transistor provide constructors with a very useful piece of
becoming excessive when VR1 is at its minimum value.

With the function switch S1 in the "Set Ib" position, the meter is connected in series with R2 and VR1, and thus measures the base current set by VRI. In the "Ic" position SI switches R3 across the meter terminals to give it a full scale deflection (f.s.d.) of 10 mA , thus enabling it to measure the collector current. In order to perform a leakage test, i.e., measure I'co, S 1 connects the meter in series with the transistor across the supply voltage, with the base open-circuit.

To enable the tester to be used for both n-p-n and \(p-n-p\) transistors, the circuit of Fig. 1 is modified slightly by the addition of Fig. 2. The meter is


Fig. 4: Layout of the prototype tester. Compare this with the photograph in the heading on the right.
connected to points \(A\) and \(Z\) on Fig. 1 via the p-n-p/n-p-n switch \(S 2\). This enables both the meter and the supply to be reversed for testing \(n-p-n\) transistors (see Fig. 2).

\section*{Calculations}

Resistor RI should be equal to the meter's d.c. resistance, \(\pm 20\) per cent will be satisfactory, while R3 the 10 mA shunt resistor must be made very accurate. Its precise value will depend on the meter used and its value may be calculated as follows:
\(R=\frac{\text { Meter's f.s.d. }}{\text { f.s.d. required }- \text { Meter's f.s.d. }} \times\) Meter's resistance.

\title{
ISTOR TESTER BY G.A.BOBKER
}

\section*{;ources quite cheaply. Others are obtainable in} nmarked. The simple but efficient unit described haracteristics to be measured and it will thus st gear at low cost. Construction is uncritical.

Example: Supposing we are using a meter having a f.s.d. of \(500 \mu \mathrm{~A}\) and a resistance of \(250 \Omega\). In order to give a f.s.d. of 10 mA it would require a shunt resistor whose value will be:
\[
\mathrm{R}=\frac{500}{10,000-500} \times 250
\]

This equation gives the value of R3 as approximately \(13 \cdot 1 \Omega\), therefore a preset potentiometer of some \(25 \Omega\) will be ideal. To calibrate accurately, the meter is placed in series with another meter of known accuracy as shown in Fig. 3. As the shunt has to be very accurate it is switched in the tester by two of the switch contacts wired in parallel, Slc and Sid. This has the advantage of reducing the contact resistance of the switch.

As the leakage current of some a.f. output transistors can be as high as \(450 \mu \mathrm{~A}\), if a more sensitive meter is used then \(\mathrm{S} 1 \mathrm{c} / \mathrm{S} 1 \mathrm{~d}\) should be arranged to switch in a \(500 \mu \mathrm{~A}\) shunt in the "I'co" position. The switch S 1 should be the normal 4 -pole 3 -way type. If fancy switches, or switches to hand are used, difficulty might be experienced if they are not of the "Break-before-make" type.

\section*{Construction}

The cabinet was made from plywood fixed together with glue and panel pins, the finished case being covered with "Fablon" or "Contact". The final size of the case will be determined by the size of the meter used. The clips to hold the batteries were made from strips of brass pilfered from a defunct cycle-lamp battery, and these were fixed to the cabinet with Araldite. This is very easily achieved and is far superior to soldering wires direct to the battery cases.

The terminals used in the prototype were of the spring loaded variety and were obtained from surplus equipment. Alternative terminals can be

\section*{\(\star\) components list}

\section*{Resistors:}

R1 see text
R2 \(4 \cdot 7 \mathrm{k} \Omega-10 \mathrm{k} \Omega\) see text
4 pole 3 way
S2 3 pole 2 way
R3 \(1 M \Omega\) potentiometer

\section*{Meter:}

R4 see text
\(500 \mu \mathrm{~A}\) f.s.d.

\section*{Miscellaneous:}

Terminals, Batteries-2 penlight 1.5 V , Materials for case, solder, wire etc.

made either from bolts or from three crocodile clips as shown in Fig. 5. Constructors may use their ingenuity as to terminals but whichever type is used they must provide good positive action holding the wires tightly. They should also be kept clean.


Fig. 5: Suggested approach to the problem of making suitable terminals, these may be modified bolts, or made from crocodile clips.

\section*{Using the tester}

Set the \(\mathrm{p}-\mathrm{n}-\mathrm{p} / \mathrm{n}-\mathrm{p}-\mathrm{n}\) switch to the appropriate position and turn the function switch to the off position. (1) Connect the transistor to the terminals, switch to "I'co" and note the reading. 12) Switch to "Ib" and adjust "Set Ib" to give \(20 / 4 \mathrm{~A}\) reading. (3) Switch to "Ic" and note the reading. Repeat (2) and (3) but this time using \(\mathrm{lb}=40 \mu \mathrm{~A}\). The d.c. gain is simply Ic divided by Ib. The small signal or a.c. gain is obtained from the readings noted in steps (2) and (3);
\[
\text { A.C. gain }=\frac{\text { Change in Ic in } \mu \mathrm{A}}{\text { Change in Ib in } \mu \mathrm{A}}
\]

Example: If \(20 \mu \mathrm{~A}\) gave 1.2 mA , and \(40 \mu \mathrm{~A}\) gave 2.6 mA then gain \(=\frac{2600-1200}{40-20}=\frac{1400}{20}=70\)

If the meter scale is marked at the \(20 \mu \mathrm{~A}\) and \(40 \mu \mathrm{~A}\) positions then steps (2) and (3) are made very simple.

\section*{Let's Keep the Pirates}

You have published many letters and articles in your pages against Pirate radio stations. One of the more recent letters dealt with the shortage of medium-wave channels. Has anyone ever looked to see how many channels are allocated to this country and how efficiently they are being used? It seems to me that using nine channels for the Home Service alone, is not doing things efficiently. Surely by using synchronised transmitters on one channel, we could release eight channels at once for other services. Any regional variations, few and short-lived as they are, could be accommodated on v.h.f.

The public has proved the demand for what the Pirates are providing. Why not let them provide it from landbased stations using channels already allocated to the UK?

\section*{R. E. Tinson.}

Wilford, Nottingham.

\section*{Comments from New Zealand}

This is a somewhat belated reply to H. C. Pryse who wrote in the December issue of Practical Wireless, concerning his inability to obtain spares for his H.E. 30 receiver. The Lafayette brand name is only one of many names used on this receiver which is made by the Trio Corporation, 6-5 Ichome Shibuya, Shibuya-KU, Tokyo, Japan, to which he may care to write.

Many amplifiers and receivers which are sold in the USA with American names on them are made in Japan and as to Mr. Pryse's inability to receive a reply from the Lafayette Co. I am in full sympathy with him. I find there are quite \(a\) few British firms including advertisers in Practical Wireless who do not answer my letters when I request information or catalogues. I get the impression that British firms are not interested in overseas orders!

\section*{S. Burrage.}

Auckland, New Zealand.

\section*{Ease of Pronunciation}

There has been a certain amount of controversy over the last few months on the subject of changing cycles to Hertz. I personally do not care one way or the other since it is just as easy to write MHz as it is to write \(\mathrm{Mc} / \mathrm{s}\).

The point that seems to be overlooked is the pronunciation of the new term. For example, \(\mathrm{Mc} / \mathrm{s}\) and \(\mathrm{kc} / \mathrm{s}\) are usually pronounced "Megs and and Kaycees". The new terms MHz and kHz will now, I suppose, be pronounced "Megger hurts and Killer hurts."

Redditch,
V. E. Green.

Worcestershire.

\title{
NEWS AND..
}


The Eddystone Lighthouse has been presented with a transistorised receiver by Eddystone Radio Limited. This new receiver type EB35 will provide the lighthouse keepers with high quality reception on all the broadcasting frequencies in the long, medium, short and f.m. wave bands.

The receiver was presented at the lighthouse by Mr. A. C. Edwards, Director of Eddystone Radio Limited, and accepted, on behalf of Trinity House, by Principal Keeper Emerson. Mr. Edwards is seen here with Principal Keeper Emerson (centre) on the afterdeck of the Trinity House vessel Stella as the receiver was being delivered to the lighthouse. The Eddystone lighthouse and Smeaton's Stump can be seen in the background.
"CONTACT" FOR THE SWL
We have recently received a copy of "Contact", the monthly journal of the World Communication Club of Great Britain. It gives useful information for the SWL and contains articles of a nature that would also appeal to Hams.

The aims of the Club are: to interest more people in the international aspect of radio; to provide fellowship to all interested; to encourage and help DXers in their hobby and to learn more about the world we live in through the medium of short wave radio.

If anyone would like further information and details of membership of the Club, contact Mr. S. Green, 26 Tolhouse Street, Great Yarmouth, Norfolk.

\section*{ST. DUNSTAN'S CALLING}

On Saturday, 8th April, a new callsign was heard on the amateur bands, GB3STD. This was the temporary callsign allocated to St. Dunstan's Holiday Home and Training Centre for men and women blinded on war service, when they held a weekend reunion of war-blinded radio Hams at their centre at Ovingdean near Brighton. The station was equipped with the very latest in amateur radio equipment. They had as their host, Lord Fraser of Lonsdale, St. Dunstan's Chairman who, despite his blindness, was one of the pioneers of amateur radio.

\section*{Dah Di Dah Dit Dah Dah Di Dah}

I think it ought to be publicised that the Postmaster-General will do all he can to assist in making alternative arrangements for the place and time for sitting the GPO Radio Amateurs' Morse Test for those who, because of their location, have a long way to travel to any of the officially designated centres.

From my own home in Workington, the nearest designated centres are Whitley Bay and Glasgow, 220 and 270 mile journeys respectively. Alternative arrangements were however made to take the test at Ambleside, 40 miles away, with the further suggestion that it could be taken in Workington but only at very short notice.

All readers working for the Morse Test, living in places remote from named Test centres should write to the GPO Radio Services Headquarters, where I have no doubt they will be given courteous consideration, and some easier-reached centre arranged.
A. G. Thorburn, G3WBT. Workington, Cumberland.

\section*{Useful Lists}

I would like to congratulate Mr . H. W. Hellyer on his Repairing Radio Sets article in the May issue of Practical Wireless. The lists of Test Gear and Bench Aids that he gives on pages 38 and 39 are an invaluable aid and certainly save hunting through lots of old issues of the three "Practicals" for the article that you know is there but for the life of you, just cannot find! Many thanks H.W.H.
P. Keeling.

> Woodford Bridge, Essex.

\section*{Oh Henry!}

I read with interest Henry's remarks on page 27 of the May issue of Practical Wireless regarding Retail Price Maintenance. I do not know how Henry can possibly say servicing will suffer because dealers may have to bring prices down to compete with the "big boys".

It is a fairly common fact that from manufacturer to consumer, the price of a product is nearly doubled. Part of this is taken by the wholesaler-about \(10 \%\)-so where does the rest go? Why, to the retailer who cannot cut his prices to the man in the street because it will affect his servicing organisation. Already most servicing facilities are rather shoddy, so what have we got to lose?
A. Read.

Walthamstow,
London, E.17.

\title{
UNITS
}

\author{
by A. J. Bassett
}

LET us begin with a definition. "Tremolo" is a sound effect caused by rhythmic variations in the amplitude of a musical note or notes.
Another, radically different, effect is often confused with tremolo. This is "vibrato" i.e. rhythmic variations in the pitch of a musical note. Various amplitude-modulation devices now on the market are wrongly described as "vibrato" units. This is a gross inexactitude for a true vibrato effect can be achieved only by frequency modulation of the note.

Acoustic vibrato units are based upon the wellknown "Doppler" effect; a note emitted at frequency " n " \(\mathrm{c} / \mathrm{s}\) by a moving object will have an apparent frequency " \(f\) " \(\mathrm{c} / \mathrm{s}\) when received by a moving or stationary auditor (e.g. listener or microphone).

The difference between " n " and " f " is the apparent shift in note frequency. This shift depends upon the velocity and direction of movement of both source and auditor. Similarly an apparent frequency-shift can be produced when a note from a stationary source is reflected from a moving object and the reflected sound waves received by a stationary auditor.

Thus arising from the "Doppler" effect we have three main acoustic means to an apparent change in pitch of a musical note radiated at a fixed frequency:
(1) Moving source of sound
(2) Moving auditor
(3) Moving reflector of sound waves.
in a single installation and the paddles run at different speeds to produce an exhilarating "chorus" effect.

Best speed of rotation is in the region 100 to 300 r.p.m. for average use. The effect is best applied to the high and middle response speakers, large brass speakers being left alone.

Four main output loudspeakers are mounted in a "pitch" circle on a plywood wheel, which acts as a baffle. The wheel is driven silently round at about 80 r.p.m. Slip rings with multiple phosphor bronze brushes are used to make connections to the loudspeakers. Sound waves are guided outwards by means of a stout wooden panel as shown in Fig. 2. Destructive interference between waves of opposing phase contributes toward a tremolo effect, in addition to the vibrato effect which is the main feature of this device.

\section*{Echo Device}

Here a real echo chamber is used. Once again, both vibrato and tremolo are produced, with the addition of echo and reverberation. In Fig. 3 a corner mounted loudspeaker (L) operating at a low level produces a complex pattern of direct and reflected sound-waves in the chamber. The sound is picked up by a rotating high-quality directional microphone (M). Because of the varying path-


Fig. 1 (left): Rotating paddle method. The paddle may be polished or felt covered (see text).

Fig. 2 (right): Rotating loudspeaker device producing vibrato and tremolo effect.


The "loudspeaker paddle" method is shown in Fig. 1 where a wooden or metal paddle is rotated in front of the loudspeaker, producing a cyclic change in both pitch and amplitude. To enhance the tremolo effect, the paddle should be smooth and polished, thus promoting reflection of sound waves. If only vibrato is required, the paddle may be covered with felt.

There is no reason why several units should not function simultaneously at different speeds. Thus several loudspeakers may be fitted with paddles
lengths of the reflected and direct waves, a phaseshift effect emerges, which is sampled at various, angles by the microphone to produce a more or less intense vibrato effect. Tremolo is produced because some of the sound waves are stronger at different angles.
The degree of echo produced by such a chamber may be undesirable for certain types of music. This echo is determined by the length ( S ) of the chamber, which could be only 4 ft . for minimum echo, though a length of 12 ft . might be acceptable in
other instances. This is a subjective matter, and much depends upon the size and character of the main room or hall.

The chamber itself may be constructed in an unused passage or cellar from which extraneous noise is excluded. The walls are best constructed of concrete, brick, stone or heavy galvanised iron. The microphone is driven at about 300 r.p.m. from a silent-running electric motor using plastic or

Fig. 5. V1, a double-triode valve (ECC83) and its associated network form a low-frequency Wienbridge oscillator, whose output is fed to the screengrid of V2 via C3 and depth control VR4. The gain of V2 varies in sympathy with the changes in the voltage on its screen-grid, thus providing amplitude-modulation of the audio signal. VR5 is a gain control, which may be adjusted until the


Fig. 3 (left): Echo chamber containing loudspeaker and micro-phone-only the microphone rotates.

Fig. 4 (right): Block schematic of complete system when using an echo chamber

mean gain of the unit approximates unity. The output may contain, in addition to the input frequencies, traces of the tremolo frequency, but these are small and are usually not objectionable. This unit could not possibly produce frequencymodulation of any note it might receive from the pre-amp. A different approach is clearly needed.

We will now discuss a unit which does not rely upon acoustics; can be built fairly small, and which will produce a true vibrato effect; the basis of operation is a phase shift ladder network, whose theoretical diagram is shown in Fig. 6 together with associated amplifier circuits.

To each stage of the ladder is connected a capacitor plate P1, P2, - - P6, these plates being arranged in a ring in the order given. Above this ring is placed a ring of thin sheet dielectric (e.g. perspex) pressed flat against the plates. A sliding pick-up plate P7 is arranged to run round on the dielectric, thus providing capacitive pickup of the audio signal, from each of the plates in the ring, in turn.

Because the phase of the signal is different at each stage of the ladder network, the output waveform derived from P7 is alternatively "compressed" and "expanded" with regard to the time axis. If the device is correctly adjusted by extra pads or dielectric where need be, amplitude-modulation is rendered negligible. The result is a frequencymodulated output derived from a constant frequency input.

Fig. 7 shows a rough sketch of a printed circuit board, showing arrangement of the capacitor plates P1-P6. It will be noticed that plates P2-P5 are split into different positions in the ring as shown. This aids in the production of a smooth output. An electric motor (not shown) drives the wiper plate P7 (not shown) over these plates to pick up the signal via the dielectric. Signal pickup from P7 is effected by a phosphor-bronze sliding contact. Speed of rotation of P7 is adjusted to about 300 r.p.m. for average use. The ladder network components shown are on the other side of the board. The paired capacitor plates are connected together by wires. The size of the printed circuit, etc., may be left to individual choice, but a pitch circle of 4 to 6 in. should be adequate for plates P1-P6, the

larger plates producing a better quality. The wiper plate P7 may be big enough to just cover one of these plates, or possibly a little shorter. This may be determined by subjective listening, or by the use of an oscilloscope to obtain good output waveform.


Fig. 7: Suggested layout of printed circuit board showing arrangement of the capacitor plates P1-P6.

Almost any small electric motor may be used provided the power is adequate to drive P7 against the small friction involved; however, a synchronous or regulated type is to be preferred. The motor should be geared down by non-metallic gears to avoid hum pick-up. Several modellers' motors are
available with suitable plastic multi-speed gearboxes, and these should be tested in the shop to ensure that they are reasonably silent-running.

The whole unit should be well shielded against external capacitive pick-up; special care being taken to shield the motor leads (use shielded twin cable), and the valves in separate compartments to avoid audio feedback.

V1 of Fig. 6 forms a preamplifier with high and low sensitivity inputs, and volume controls VR1, VR2. The top-cut tone control VR3 operates in conjunction with low-pass filter network R7, C7, R9. This is necessary to compensate for bass attentuation in the phase-shift network. The output from V1b is fed to the ladder network, and having passed to P7, is amplified by V2. VR4 is a gain control, which cuts down the voltage gain of V2, and will help combat any tendency to a.f. oscillation in this high-gain circuit. Output from V2 is fed to the main amplifier through C20.

The values of C11-C15 and R13-R18 may be varied to suit individual taste and the type of instrument to be used. Thus for bass instruments, a higher value of capacitor may be preferred.

With regard to the mechanical section of this unit, the constructor is not bound to use a printed circuit at all; thus the capacitor plates may be assembled in the form of a cylinder, inside which is a film of dielectric round which runs plate P7. In fact the whole design is quite flexible, and with care the construotor may build a vibrato and/or tremolo unit more suited to his purpose than many on the markets of today.

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1LBANIA: Radio Tirana (Rue Ismail Quemal, Tirana) European English schedule is 0630-0700 6,157 plus possibly 7,\(120 ; 1500-15301,214\) (some reports say \(7,265 / 1,277\) ); 2000-2030 7,265 ; \(2200-2230\) 7,265 (plus 1,310 in some reports). Non European English TX believed to be 0200-0300 9,715/7,265 and 0400-0430 7,265/9,390/1,310.

Radio Shkodra (Drejtoria e Radio Shkodres Shkoder) may just be heard at 1700-1930 on 8,217.

Andorra: Radio Andorra (c/o 82 Chelsea Manor Street, London, S.W.3) has been testing on 719 at 1800-0100 with a view to starting an external service beamed to the U.K.

Bulgaria: Radio Sofia (4 Boulevard Dragan Tsankov, Sofia) reported with new frequencies \(11,930 / 11,955\) for African English TX at 2105-2130.

France: O.R.T.F. (Maison de l'O.R.T.F., 116 Avenue du President Kennedy, Paris 16) has English 0515-0530 9,500/11,960; 1100-1115 17,850/21,650; 1300-1330 15,245/17,740/21,580; 1915-1930 15,245/ 9,700.

Germany: Deutsche Welle (Bruederstrasse 1, Postfach 344, 5 Koln) has made following changes in English TX: 1550-1620 11,765/15,435; 1100-1115 11,930/ 15,275/17,875; 1900-1910 11,925/15,380.

Westdeutschen Rundfunk Wallrafplatz 5, Koln) is to increase the power of its 1,586 TX to 800 kW .

Radio Free Europe (1 Englisches Garten, Munchen) shows the new frequencies of 7,215 and 21,575 in its latest schedule.

Great Britain: BBC (CEXB, Bush House, London, W.C.2) using 25,750 for \(1200-1300\) Chinese TX.

Holland: Radio Nederland (P.O. Box 222, Hilversum) using 25,610 for some programmes. The 1600-1720 Sunday Happy Station session has been reported on \(17,765 / 11,730\) A special QSL is to be issued from April 28 to October 7 to commemorate the Canadian Expo 67 exhibition. A new picture series will then follow.

Hungary: Radio Budapest (Brody Sandor-S.U. 5-7, Budapest VIII) now uses 3,995/6,234/7,100/7,220/ 9,833 for the 2200-2230 English session.

Italy: R.A.I. (Viale Mazzini 14, Rome) has completely revised schedule. English is now aired as follows: 2135-2155 9,710/7,275/6,050; 0100-0120 11,810/9,575; 2200-2255 11,905/9,540/6,095; 0350-0410 17,770/ 15,310/11,905; 0425-0504 7,275/6,050; 2025-2045 9,575/ 7,235/6,130.

Monaco: Trans World Radio (Rue de la Poste 5, P.O. Box 141, Monte Carlo) has English 0630-0730; 7,295; 0730-0815 9,655/7,295. 0815-1000 Sunday, 1200-\(1245,1430-15309,655\). Frequencies are subject to confirmation.

Poland: Radio Warsaw (Warsaw). Revised European English schedule is: 1830-1857, 2130-2155 9,525/7,125;

1930-2000 9,525/7,285/7,125/1,502; 2030-2100 9,675/ 9,540; 2230-2300 9,540/7,285/1,502; 2303-2330 818.

Rumania: Radio Bucharest has new English transmission at 1200-1230 on 11,920/15,250 and 1300-1330 \(11,920 / 15,250 / 15,318\). The \(1500-1530\) is now on \(11,885 /\) 11,920/15,250.

Spain: Radio Nacional de Espana (General Yague 1, Madrid) has a new Hungarian TX at 1300 on \(9,760\).

Sweden: Gothenburg Radio (Omsala) reported testing at 0700,1223 and 1715 on 11,820 . Does anyone know anything about this station?

Radio Sweden (Box 955, Stockholm 1) now has English: 0900-0930 9,625/21,585; 1100-1130 9,625/ 15,240; 2015-2045 9,625/11,705; 1900-1930 11,705/ 17,\(840 ; 1230-1300 \quad 15,240 / 21,690 ; 2245-2315\) 9,620/ 11,705; 1400-1430 21,585/17,840; 0515-1545 17,840; 1600-1630 17,840/15,240; 0200-0230, 0030-0100 11,805; 0330-0400 11,705; 2330-2400 1,178.

Switzerland: Swiss Broadcasting Corporation CH 3000, Bern 16). The summer English schedule is: 0130-0315 6,120/9,535/11,715; 0515-0700 9,695/11,715; 0700-0900 (not Sundays) 6, 135/9,535; 0700-0900 9,590/ 11,775/17,890; 0915-1030 15,305/21,520/17,830; 11151300 9,665/11,865; 1315-1500 15,235/17,775/21,520; 1515-1700 15,305/17,830/21,540; 1900-2045 9,665/ 11,865. Available transmitter powers are now 25/100/ \(150 / 250 \mathrm{~kW}\).
U.S.S.R.: Radio Moscow (Moscow) now broadcasts 24 hours a day in Chinese to China.

Radio Kiev (Ukrainiske Radio, Radio Centre, ul Khreshchatik 24, Kiev, Ukrainian SSR) has English to Europe Mondays, Thursdays and Saturdays at 19001930 6,020/6,040/9,640; 2230-2300 1,241. To North America on the same days \(0030-0100\) 7,120/7,280/ 7,290/7,330/9,680; 0430-0500 7,250/7,290/7,330/9,600.

Yugoslavia: Radio Belgrade ( 70 Borisa Kidrica, Belgrade) has English 1530-1600 11,735/15,240/9,505; 1830-1900 6,100/7,200; 2200-2215 1,268/6100/7,200/ 9,505.

Clandestine: Radiofonicas Stamos \(i\) Foni. This is a communist station with Greek programmes produced in East Germany and probably transmitted from Bulgaria. It can be heard 0510-0545 on 6,215 and 1730-1800 on 8,065 .

Radio Portugal Libre transmits at 0700-0730 on 12,008; 1200-1230 11,510;1900-1930 and 2115-2145 9,445.

Radio Espana Indepentiente transmits 0600-0700 6,950; 1300-1400 15,365; \(1615-1800 \quad 9,430 / 10,130\); 1800-2230 6,950/7,005/9,430.

Contributions came this month from Radio Sweden, R. J. Warner, A. E. Roxburgh, R. Severn, J. McDonald, J. W. Smith, D. S. Abbott, K. Proctor, W. E. Bartlett, D. Owen, J. Fitzgerald, and the Swiss Broadcasting Corporation.

WE will spend two minutes with heads reverently bowed in silence before pressing on. This token of mute sympathy is for the G3JDG receiver which passed peacefully away-just as ten metres was beginning to get interesting too. The mains "trany" has shorted itself out so it looks like I'm stuck with the t.r.f. until after Easter. Have you ever noticed how things always break down on a Sunday or a bank-holiday, when all the shops, are shut? Prior to being struck "mains tranyless" however, things were going great guns and most bands appeared to be very busy. Ten metres has yielded VK stations at 5 and 7 on a.m. phone; fifteen has gone literally potty with signals at times and seems more consistently open these days; twenty has been, well twenty, lots of DX and quite good openings to the Pacific and Oceana. On seven megs lots of noise, commercials and DX too if you can stand the pace and have the skill to winkle them out. Eighty metres, well I didn't do too well this month but others have sent in some very fine logs for \(3 \cdot 5\) so it must be me. (More exciting confessions next month.)

\section*{LOW FREQUENCIES}

Still very few people send logs for the l.f. bands. Everyone seems to stick h.f. where DX falls like ripe plums into the ears of anyone who cares to listen out. Some people are persistent however.
N. Henbry (Sussex), EA12, 20 metre dipole for \(7 \mathrm{mc} / \mathrm{s}, 7 \mathrm{ft}\). vertical copper rod at 30 ft . for all other bands. Norman really goes to town on the l.f. segments. On 80 s.s.b. he logged-F \(-\mathrm{FAO} / \mathrm{M}, \mathrm{K} \operatorname{ISLZ}\), K2DPA, K3UQU, K4SXT, K7UIT/9A1, KP4AST, TF3EA, TI2NA, VE1AHP, VE2BTS, VS9ALV, WIZBT, W2ZPO, W3BMS, WA3DCG, W4SIB, 3A2MJC, \(3 \mathrm{~A} \varnothing \mathrm{AE}, 3 \mathrm{~B} 1 \mathrm{FG}, 3 \mathrm{ClUA}, 3 \mathrm{C} 2 \mathrm{WM}\), 3C3FJZ/SU, 9H1AB. Up higher on \(7 \mathrm{Mc} / \mathrm{s}\) the \(\log\) reads - CN8AW, CN8BV, GC8HT, K5OSH, PZ1CF, WB2CKS, W4OMW. It's no good, I shall have to lay a long lead from Norman's shack to my place to plug in a spare pair of phones.
L. Smith (Glasgow), 19 set (modified), 66 ft . long wire went s.s.b'ing on forty and hooked-CN8AW, CN8BB, DJ4AX, DJ7QV, DL9ME, EP3AM, IlBAF, OE2EGL, PY6NW, UA3KBO, UB5KIW, YU3LB. Nearly all the reports this month were for the h.f. bands, so let's turn the bandswitch to 20/15/10 and see what's about.

\section*{HIGH FREQUENCIES}
A. Darragh, QTH not stated so we'll put him down as no fixed abode, GC1U, 100 ft . long wire running N/S. On 20 s.s.b.-AC4AK, CE1FC, CE3TS, CP8OS, CT1BK, EP1BP, EP2BI, HI8LAL, HK4KL, HV3SJ, ISIKW, JA-1AEA, EZT, 4TRV, KC6BW, KH6BT, KL7BZ, KR5CUN, KR6UL, KS6BT, LU5AH, OX3LY, OX4AA, OY7S, PXIPA, TF3EA, TG2IA, TG8IA, TI2PAS, TU2DC, UA7JA, UA9FC, UF6KPA, UJ8KAA, UNICC, U5ARTEK, VK-2ID, 3AUP, 4KS, 5LT, 6KK, 7SS, W4EFB/P/KH6, XE1FFA, XF1KB, YSIAG, ZL-1AI, 3BE, 3QH, ZS-2PD, 3FT, 6AJL, 6RA, VU2BX, 3A- \(\varnothing A E, 2 B S, 2 M J, 2 R J C\), 3B-1GL, 3C-3BVE, 5SV, 6ALX, 7ZU, 8AD,

4UISU, 4X4MO, 5A1TV, 5A5TV, 5H3TG, 6Y5MJ, 9G1ND, 9H1A, 9M2DX, 9X5PB.
S. Porter (Surrey), has an R1155 with a 20 metre dipole. He reckons the best time to listen is around sunrise, and from 1800 onwards. His log for twenty includes - EL3D, KA6BFU, KP4CSV, KP4AXC, VK2NI, VK2ID, VL9UC, XEICE, YV5BSL, 3A2KO, 4X4BL, 5A5TV, 7XØAH, 9X5A.
D. Clark (Bucks), progressive s/het plus PR30, 60ft. NW/SE, 20 s.s.b.-ISIDMN, K1EPG, K2AGZ, K3FGO, K4LZU, K5ZSX/MM, KG6AQG, KL7EBK, KP4ID, KR6UL, OD5FA, OX4VT, SV \(\varnothing\) WII, TF3HS, VE1ACD, VE1AGH, VE3DJE, VK2AFD, VK3SX, W-1/2/3/4/5/9/ \(\varnothing\), WA8CH/ MM, YN1JW, YV4AZ, ZE1AE, ZF1GC, ZL3UY, ZSIJM, 3A2CP, 5A1TG.
P. Baker (S. Wales), HE30, 120ft. l.w., heard these on 15 metres, mostly s.s.b. the rest a.m.CN8FT, CR3KD, CR4BA, CR7BO, CR8AL, CT2AP, EA6BG, EA9EJ, EL6B, EP2RT, EP3AM, HC2SW, JA-1OYY, ITTL, 4AXW, 9JX, K6PIZ, KP4CQV, KV4CX, MP4-BBA, BGM, BGL, OA4TF, OD5BU, OX5AR, PY9AI, VE6QG/SU, SV \(\varnothing W L, ~ T F 2 W K E, ~ T I 2 R L J, ~ U A 9 D T, ~ V E 7 P V, ~\) VK5HT, VS9ALV, WB2FBQ/MM, W6ITA, W7VSM, YS1TF, ZE6JL, ZL-3KA, 4JI, 4MZ, ZBIYR, 3C5HV, 3C6AJY, 4X4LL, 5A1TV, 5N2ABB, 7X \(\varnothing W W, 9 G 1 E Z, 9 H I X, 9 U 5 B B\).
J. Preece (Cheshire), PCR3, 60 ft . l.w., 15 metres all a.m. - CN8CF, CO8RA, CR4EJ, CR6AU, CR7FM, EA9EJ, EP2RT, FG7XE, FM7WQ, HC2SW, HI8BGA, KG6AAY, LU5DZ, MP4BGL, OD5ET, PY1MGW, ST2SA, SV1DL, TF5TP, TJ8AC, VP6BW, WA5QQF, W6QBA, YV4ON, ZE6JE, 3C3GCO.
P. Knowles (Cheshire), CR 45 plus PR30, 70ft. l.w., listened on ten metres a.m. for-CT1JW, EA3HL, K1ZFP, LA2XK, MP4BGM, UA3AWK, UB5EVW, VP7NP, W1DT, WB2QEH, ZS6RQ.
G. Taylor (Staffs), HE30, 135ft. l.w., ten metres a.m.-PJ3CL, VP6UN, XE1CT, 9Y4BS, on s.s.b.CR7ER, DUIFH, EP2GI, FG7XL, HCIMF, JA2BVY, KV4EY, VK4TT, VP2MK, XW8AL, YVIEJ, ZE4JS, 5R8AS, 9LITL.
P. Allsop (Derby), GCIU, 66ft. l.w. all a.m. on ten metres - K1ZKD, K2BJR, K3HTZ, KøQMU/P, VE3CKM, W1UHY, W2BFZ, W3DJW, W5WS, W9MZM, XE2CJ, ZC4MO.
P. Elliott (S. Africa), 5 valve s/het, 105 ft . I.w. logged these on phone on \(10-\mathrm{CE} 6 \mathrm{E} Z, \mathrm{HB} \varnothing\) WEE, KR6BF, KV4CX, KV4EY, MP4BBA, OD5EC, PY2PA, SVøWFF, VE6ALA, WA6UEK, YA5RG, YV1PP, YV3FBP, 3C3FDZ/P/SU, 4Z4AO, 5N2ABA, 5R8AS, 9H1HR, 9M2LO, 9V1NY.

\section*{WHERE AND WHEN}

Contests and rallies are on the increase now that the warmer months are coming. In May there's quite a few and my diary reads-7th, Thanet Mobile Rally at Ramsgate; 7th, 2 metre portable contest; \(20 \mathrm{th}-21 \mathrm{st}, 1296 \mathrm{Mc} / \mathrm{s}\) contest; \(27 \mathrm{th}-28 \mathrm{th}, 432 \mathrm{Mc} / \mathrm{s}\) contest; 29th, Redbourne Fair (Herts) listen on 160 ; June 3rd-4th, National Field Day. Deadline for this month is 20th. The deadline for all logs in future will be the 20th of each month.

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7 transintor plus 2 diode superhet, \(f\) waveband portable receiver covering the ful. Medlum Waveband and Bhort Wavehand spread ranges, 13 M , 16 M , 19 M and 55 M whin Band Spresd Tuning for acourate Station Selection. The coil pack and tuning heart is completely factory assembled, wired and tested. The remaining assembly can be campleted in under three hours from our easy to follow, stage by atage instructions. Superhet, \(470 \mathrm{Kc} / \mathrm{s}\). All Mullard Translators and Diodes. Uses 4 U2 batteries. Sin. Ceramic Magnet P.M. Speaker. 500 MW Tone Circuit with separate Tone Control. Volume Control. Tuning Control and Waveband Selector. In wood cabinet, sixe \(11_{1} \pm 6 \frac{1}{5}\) 3in. covered with washable material, plastic trim and carrying handle. Car aerial socket Etted.

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Four 02 batteries \(3 / 4\) extra.

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SPECIAL PURCHASE-UHF/VHF TV TUNERS Well known British makers surplus stocks. Now available for the first time to the Home Constructors. Add 2/6 Post and Packing on each. VALVE UHF MODEL (illustrated)
In metal case size 4 6 1th. Fully tunable-complete with PCS6 and PC88 valves. LASKY'S PRICE \(29 / 6\) Without valves 12/6 TRANSISTORISED VHF TUNER
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Fully tunable-range 88 to \(108 \mathrm{Mc} / \mathrm{s}\). Completely wired on printed circuit. \(10.3 \mathrm{Mc} / \mathrm{s}\). IF, 6 transistors and 3 diodes. Slow motion tuning drive. 8 ize \(6 f\) I \(4 \times 2\) in. Operates from any 0v, D.C. Bource. Full data and circult aupplied.


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\(1 \times 1 \mathrm{n}\). \\
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\section*{practically Wirieless
conmentar by HENRY}

T1 HE price of newsprint is going up. Space must not be wasted. It is Henry's duty to utilise this column in a forthright, serious, progressive way. This was underlined by a letter on Page 821 of the March Practical Wireless. I.N.R.W. Newport accused the Editor of wasting space in comment; space that could have been better used for constructional articles. The sting of Mr. Newport's letter came in the tail. "A far better policy would be to refuse advertised non-convertible \(27 \mathrm{Mc} / \mathrm{s}\) walkie-talkie spreads unless boldly indicated as such.'

The key-word is boldly. Our correspondent expects the advertisers to proclaim: "Buy it NOW-but use it NEVER." He may be right. It is scandalous that potentially illegal apparatus should be blatantly peddled for the innocent reader to be corrupted. What about those radio tuners for the front end of your hi-fi kit, feeding a tape recorder aren't they just a little naughty? Even the impeccable Mr. Molloy released the secret (Page 839, same issue) that the phone output of the R1155 was suitable to load a tape recorder. Shame on him!

We must draw the Editor's attention to another article that appeared in the same issue. A top-band transceiver is described by T. Simon.

Here the felony is compounded by an attractive cover picture
that even includes communications in foreign languages, aye, whisper it, from behind the Iron Curtain. What a gift to some potential George Blake.

The article bristles with lawbreaking possibilities. In the first place, for only \(£ 15\), our innocent is tempted to transmit. Or is it simply that the Editor is fanning another controversy on hamlicences and the anachronistic need to learn the Morse Code?

Let us look a little deeper at the article. Near the bottom of column 1, Mr. Simon tells us that in his area ". . . there is a strong break-through from the BBC at Brookmans Park ( \(908 \mathrm{kc} / \mathrm{s}\) 2nd harmonic)". Who knows what else may break through, even using a well-peaked tank circuit. We may find ourselves clandestinely eavesdropping on the police, fire service, ambulances, even taxis. In a south-coast town even the dust-carts have two-way radio.

Further on we see two stages of modulation defended with the statement ". . . the QSO can be conducted in a confidential whisper with the mike gain half-way up." We have roamed the amateur bands and heard a few of those confidential whispers, thank you. It's a good job Mrs. Whitehead is only bothered about professional TV. What a fine hunting ground the hambands would provide for someone with a prurient mind.

True, Mr. Simon cares about


The dust carts have two-way radios
v.f.o. swishers and does his best to eliminate the beat note. He also uses frequency modulation the better to avoid t.v.i. Perhaps Mr. Newport would wonder darkly whether he has some ulterior motive - perhaps the family has demanded uninterrupted Coronation Street.

Yet the constructor still has to put 100 pF across the mike to avoid BBC re-radiation. Tape recorder owners will recognise the phenomenon. Free radio programmes, lightly veiled in an innocent text. It's anarchy, that's what!

But Mr . N is more concerned with the advertisers. He worries about Swish not washing whiter than white noise. He forgets that we are conditioned to the blandishments of the adman and don't believe half of what we read, hear and see. Has he thought of the awful possibilities -the unsuspecting reader who buys and builds a kit that doesn't work, then offends the local litter-laws by throwing it out of the window? Or the student who chucks up his butcher's apron for a correspondence course and electrocutes himself with a 9 V battery.

Somewhere a heart beats more strongly because Messrs. SuperFi have advertised their home video tape link. What a prospect this conjures up! All your favourite programmes canned while you are out shopping, for a paltry ten quid an hour-or, as the advertisers say piously, much less when the demand steps up. To follow the argument through, we ought to ask for video tapers to apply for some kind of licence.

Henry stands aghast. The thought of such electronic sins being committed all round appalls him. Perhaps it is as well the price of newsprint is risingthere will be less room per issue for policy-bending letters.


ADESIRABLE item in any audio enthusiast's list of "accessories" is a good quality mixer, to enable a number of inputs to be added together to give a single, complex, output signal. This four-channel mixer contains a 500 mW power amplifier and makes the device very versatile and suitable for use either on its own as a multi-input, general purpose, power amplifier, or as a fairly conventional mixer capable of driving a speaker or a low impedance feeder line. Semiconductors are used in this high gain unit, which features good stability and quality with low noise and low inter-channel interaction.

\section*{BASIC DESIGN PRINCIPLES}

A conventional "mixer" consists of some kind of combining circuit, followed by an amplifier which compensates for any attenuation which takes place in the adding process. In the unit we are considering here, an additional power amplifier "block" is provided so that the simplified block diagram of our unit is as shown in Fig. 1a.

Dealing first with the "mixer" part of the unit, a passive adder type is used, and is shown in basic form in Fig. 1b. Here, only two channels are shown; each input is applied across a variable resistor and a proportion of the input signal is tapped off at the slider and applied to a series circuit comprising either R1/R3 or R2/R3. Thus, the two input currents flow in the common resistor, R3. The output voltage developed across this resistor is proportional to the sum of the input signals. R3 may be made common to as many input signals as are required.

When this basic "mixer" circuit is redrawn as in Fig. 1c, it can be seen to be nothing more than a couple of potential divider circuits. The approximate values of input impedance, input-to-output attenuation, and inter-channel interaction can be established at a glance. Note that "worst case" values are shown, with VR1 and VR2 set for maximum sensitivity and with input 2 open circuit. In this case, the input impedance to input 1 is approximately \(55 \mathrm{k} \Omega\), and, if 1 volt is applied, the attenuation will be such that 55 mV will appear at the output, and inter-channel interaction will be such that 25 mV will appear across input 2. Input impedance will vary with the setting of VR1, and will be at maximum ( \(100 \mathrm{k} \Omega\) ) when VR1 is set for minimum sensitivity. The attenuation factor between VR1 slider and the output will be virtually constant.

The most important factor, as far as quality is

\section*{4-CHANNEL Miver/amnifitian}
concerned, is the inter-channel interaction factor, as this will cause distortion between the inputs if it is high. In practice, this factor will depend on the setting of VR2 and the source impedance of the signal connected to input 2. Typically, when 1 volt is applied to input 1 and zero input is applied across input 2 , from a \(1 \mathrm{k} \Omega\) source, and both VR1 and VR2 are set for maximum sensitivity, only 0.22 mV will appear across input 2 and interaction



(c)


Fig. 1: 'a' block schematic of the mixer/ampliffer; 'b' basic two-channel mixer; ' \(c\) ' basic mixer re-drawn to show potential divider effect, with worst-case values; "d" basic circuit of the amplifier section of the unit.



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If you're between 17 and 25 you can join the Army as a trainee technician . . . and take an r8-month technical training course. Soon you'll be up to City and Guilds standard. Six months after you've successfully completed your course you will be promoted to Corporal. From then on, it's up to you!
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\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline \multicolumn{9}{|c|}{ELECTROLYTIC CONDENSERS} \\
\hline -25 \(\mu \mathrm{F}\) & . & 3 volt & \({ }_{5}^{5} \mu \mathrm{~F}\) & & 50 volt & \(32 \mu \mathrm{~F}\) & & 25 volt \\
\hline \(1 \mu \mathrm{~F}\) & & 10 volt & \(5 \mu \mathrm{~F}\) & & 70 volt & \(40 \mu \mathrm{~F}\) & & 3 volt \\
\hline \(\underline{I} \mu \mathrm{~F}\) & & 15 volt & \({ }^{6} \mu \mathrm{~F}\) & & 12 volt & \(40 \mu \mathrm{~F}\) & & \(0 \cdot 4\) volt \\
\hline \(1 \mu \mathrm{~F}\) & & 40 volt & \(6 \mu \mathrm{~F}\) & & 15 volt & 50, F & & 6 volt \\
\hline \(1 \mu \mathrm{~F}\) & & 50 volt & \(6.4 \mu F\) & & 40 volt & \(50 \mu \mathrm{~F}\) & & 9 volt \\
\hline \(1 \mu \mathrm{~F}\) & & 850 volt & \(8 \mu \mathrm{~F}\) & & 3 volt & \(64 \mu \mathrm{~F}\) & & 2.5 volt \\
\hline \(1 \cdot 25 \mu \mathrm{~F}\) & & 16 volt & \(8 \mu \mathrm{~F}\) & & 6 volt & \(64 \mu \mathrm{~F}\) & & 9 volt \\
\hline \(2 \mu \mathrm{~F}\) & & 3 volt & \(8 \mu \mathrm{~F}\) & & 50 volt & \(64 \mu \mathrm{~F}\) & & 10 volt \\
\hline \(2 \mu \mathrm{~F}\) & & 9 volt & \(10 \mu \mathrm{~F}\) & & 6 volt & \(64 \mu \mathrm{~F}\) & & 16 volt \\
\hline \(2 \mu \mathrm{~F}\) & & 10 volt & \({ }^{10 \mu \mathrm{~F}}\) & & 10 volt & \({ }^{64} \mu \mathrm{~F}\) & & 40 volt \\
\hline \(2 \mu \mathrm{~F}\) & - & 15 volt & \(10 \mu \mathrm{~F}\)
\(10 \mu \mathrm{~F}\) & & 12 volt & \(100 \mu \mathrm{~F}\) & & 3 volt \\
\hline \(2 \mu \mathrm{~F}\) & . & 70 volt & \(10 \mu \mathrm{~F}\)
\(12.5 \mu \mathrm{~F}\) & & 25 volt
4 volt & \(100 \mu F\)
\(100 \mu F\) & & 6 volt \\
\hline \(2 \mu \mathrm{~F}\) & & 150 volt & \(12 \cdot 5 \mu \mathrm{~F}\) & & 4 volt
40 volt & \(100 \mu \mathrm{~F}\)
\(100 \mu \mathrm{~F}\) & \(\cdots\) & 10 volt
12 volt \\
\hline \(2 \cdot 5 \mu \mathrm{~F}\) & \(\ldots\) & 16 volt & \(12.5 \mu \mathrm{~F}\)
\(16 \mu \mathrm{~F}\) & & 40 volt
16 volt & \(100 \mu \mathrm{~F}\)
\(100 \mu \mathrm{~F}\) & \(\cdots\) & 12 volt \\
\hline \(2 \cdot 5 \mu \mathrm{~F}\) & & 25 volt & \(16 \mu \mathrm{~F}\)
\(16 \mu \mathrm{~F}\) & \(\ldots\) & 16 volt & \(100 \mu \mathrm{~F}\)
\(150 \mu \mathrm{~F}\) & \(\cdots\) & 15 volt \\
\hline \(3 \mu \mathrm{~F}\) & . & 3 volt & \(16 \mu \mathrm{~F}\)
\(16 \mu \mathrm{~F}\) & ". & 30 volt & \(150 \mu \mathrm{~F}\)
\(160 \mu \mathrm{~F}\) & . & 12 volt \\
\hline \(3 \mu \mathrm{~F}\) & . & 12 volt & \(20 \mu \mathrm{~F}\) & -. & 3 volt & \(200 \mu \mathrm{~F}\) & ". & 25
3
3 \\
\hline \(3 \mu \mathrm{~F}\) & . & 25 volt & \(20 \mu \mathrm{~F}\) & & 6 volt & \(200 \mu \mathrm{~F}\) & : & 4 volt \\
\hline \(\frac{3 \cdot 2 \mu \mathrm{~F}}{3.2 \mu \mathrm{~F}}\) & & 6.4 volt & \(20 \mu \mathrm{~F}\) & .. & 9 volt & \(200 \mu \mathrm{~F}\) & & 16 volt \\
\hline \(3.2 \mu \mathrm{~F}\) & & 40 volt & \({ }^{20 \mu \mathrm{~F}}\) & & 15 volt & \(250 \mu \mathrm{~F}\) & , & 2.5 volt \\
\hline \(3 \cdot 2 \mu \mathrm{~F}\) & & 64 volt & \({ }_{25}^{25 \mu \mathrm{~F}}\) & \(\ldots\) & 6 volt & \(250 \mu \mathrm{~F}\) & . & 9 volt \\
\hline \(4 \mu \mathrm{~F}\) & - & 4 volt & \({ }_{2}^{25 \mu \mathrm{~F}}\) & & \(\underline{12}\) & \({ }^{250 \mu \mathrm{~F}}\) & \(\because\) & \({ }_{2}^{15} 5\) volt \\
\hline 4رF & . & 12 volt & \(2.5 \mu \mathrm{~F}\) & & 30 volt & \(500 \mu \mathrm{~F}\) & \(\because\) & 4 volt \\
\hline \(4 \mu \mathrm{~F}\) & . & 25 volt & \(30 \mu \mathrm{~F}\) & & 6 volt & \(500 \mu \mathrm{~F}\) & - & 25 volt \\
\hline \({ }^{4} \mu \mathrm{~F}\) & . & 100 volt & \(30 \mu \mathrm{~F}\) & & 10 volt & \(640 \mu \mathrm{~F}\) & & 2.5 volt \\
\hline \(5 \mu \mathrm{~F}\) & . & 6 volt & \(30{ }^{2} \mathrm{~F}\) & & 15 volt & \(750 \mu \mathrm{~F}\) & & 18 volt \\
\hline \(5 \mu \mathrm{~F}\) & - & 25 volt & \(32 \mu \mathrm{~F}\) & . & 1.5 volt & \(1000 \mu \mathrm{~F}\) & & 6 volt \\
\hline
\end{tabular} All at \(1 /\) each \(9 /\) - per dozen. Mixed packet (our selection) 20 for \(10 /-200 / 100 \mu \mathrm{~F}\) 275 volt; \(200 / 200 \mu \mathrm{~F} 275\) volt; \(125 / 300 / 50 \mu \mathrm{~F} 275\) volt, \(6 /\) - each or 3 for \(10 /-\)
\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline \multicolumn{8}{|c|}{PAPER CONDENSERS} \\
\hline \({ }^{0} 001 \mu \mathrm{~F}\) & 500 volt & -02 \(\mu \mathrm{F}\) & & 600 A C & -25 \(\mu \mathrm{F}\) & & 350 volt \\
\hline -001 \(\mu \mathrm{F}\) & 1000 volt & -02 \(\mu \mathrm{F}\) & & 350 volt & - \(5 \mu \mathrm{~L}\) F & & 180 volt \\
\hline -002 2 F & 500 volt & -1 \(\mu \mathrm{F}\) & & 350 volt & -5 \(\mu \mathrm{F}\) & \(\because\) & 350 volt \\
\hline -005 \(\mu \mathrm{F}\) & 750 volt & -1 \(\mu \mathrm{F}\) & & 780 volt & \(\cdot 5 \mu \mathrm{~F}\) & & 500 volt \\
\hline
\end{tabular}

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Fig. 2: Complete circuit of the four-channel mixer/amplifier. Note: the two diodes may be made from old p-n-p germanium transistors, see the inset in the top-right corner for connections.
will be negligible. The performance of this simple type of circuit can thus be seen to be "adequate", so the basic principles of the amplifier circuitry can now be considered.

The basic design requirements of the unit call for an amplifier with a very high degree of gain but with good stability and low distortion. Such an amplifier is, of necessity, rather complex; the basic principles of the amplifier are therefore best understood by first referring to the simplified circuit diagram shown in Fig. Id. Here, the input signal (from the mixer) is connected via Cl to the base of Trl , which is connected as a common emitter amplifier with its collector load split into two parts, R3 and R4. If the output from Trl collector
were fed in the normal way to a following amplifier stage, the input impedance of this second stage would be effectively in parallel with Trl collector load and would thus reduce its effective value and hence lower the gain of Trl. In Fig. 1d this problem is overcome by using emitter follower \(\operatorname{Tr} 2\) as a buffer between Trl collector and the following stages, the amplified output from this "pair" being taken from Tr 2 emitter. Since Tr 2 has a high input impedance, Trl can be given a very high value of collector load, with consequent high overall gain.

In practice, the maximum usable value of Tr collector load is dictated by the d.c. and temperature stabilisation requirements of the circuit, and, in this particular application, the maximum usable


Fig. 3: Constructional data for the Veroboard panel. Care must be taken not to short the individual copper strips when soldering-in components.

(b)


Fig. 4: Metal-work data. 'A' shows the main chassis; ' \(B\) ' the front panel; and 'C' the battery holder. Two battery holders are needed for this unit.
value is set at about \(10 \mathrm{k} \Omega\). It is possible to increase the effective value of the collector load without changing its real or d.c. value; referring to Fig. 1d, the signal at the emitter of Tr 2 is of the same form and phase as the signal at Trl collector, but these two signals are effectively isolated from one another by the impedance transformation action of the emitter follower. In the diagram, Trl collector load is split into two parts, R3 and R4, and the signal appearing at Tr 2 emitter is fed via C3 to the R3-R4 junction. Thus, when an input signal is applied to Trl, similar a.c. signals appear at both ends of R3 and very little signal current flows in this resistor, which reacts as a high impedance, even though its resistive value is fairly low. In practice, the effective value of R3 may be increased to ten times its real value, giving consequent high gain. This technique of increasing the effective value of a resistance is known as "Bootstrapping".

The output signal at \(\operatorname{Tr} 2\) emitter is direct coupled to the bases of Tr 3 and Tr 4 , which are wired as a compound connected \(p-n-p / n-p-n\) emitter follower pair, giving unity voltage gain but a very low (virtually earth) output impedance, which is fed to the external speaker via C6. As in the case of Tr 2 , the \(\mathrm{Tr} 3-\mathrm{Tr} 4\) emitter followers give an output that is of the same phase and form as their input signal (from Tr 2 emitter), but the two signals are effectively isolated from one another by impedance transformation; the output signal from \(\mathrm{Tr} 3-\mathrm{Tr} 4\) is
therefore used to Bootstrap the R7-R8 emitter load of \(\operatorname{Tr} 2\), and to increase the effective input impedance of \(\operatorname{Tr} 2\) and indirectly further increase the effective value of the collector bad of TrI.

The input impedance of an emitter follower is given (approximately) as the emitter load, \(\mathrm{R}_{\mathrm{L}}\), times the \(\beta\) of the transistor, so that, in Fig. 1d, the effective value of the emitter load of Tr 2 is dictated by the Bs of \(\operatorname{Tr} 3\) and \(\operatorname{Tr} 4\) and the impedance of the speaker. The effective value of Trl collector load is dictated by this value times the \(\beta\) of \(\operatorname{Tr} 2\). Since all impedance levels are interdependent throughout the circuit, the design automatically gives an optimum performance with whatever transistors are used.

The output transistors can be given a very high 13 by replacing the two individual transistors by Darlington or Super-Alpha-Pair connected transistors, in which case the effective collector load of Trl becomes so high that, on the prototype, voltage gains of 500 to 1,000 times are obtained when using a \(15 \Omega\) speaker.

Note that direct coupling is used throughout the amplifier, and that the base-bias to Tr is obtained from the \(\operatorname{Tr} 3-\operatorname{Tr} 4\) output via R1, R2, R5, so that a d.c. negative feedback loop is set up which fully stabilises the working points of all transistors used in the circuit. Also note that all signals from TrI collector onwards are in anti-phase with the input signal, so that any stray feedback will be degenera-

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tive, rather than regenerative, and very good circuit stability is thus obtained. Having cleared up the main details of the circuit, the final version of the completed unit can now be considered.

\section*{HOW THE CIRCUIT WORKS}

The full circuit diagram of the completed unit is shown in Fig. 2. Here, the four inputs are applied to the variable resistors, VR1-VR4 via the coaxial sockets Sk1-Sk4 and the blocking capacitors \(\mathrm{C} 1-\mathrm{C} 4\), and the input currents are added in R5 via RI-R4. If the output of the mixer, taken from across R5, were fed directly to the input of a common emitter amplifier the comparatively high input capacitance of the transistor would be effectively in parallel with \(R 5\) and would result in an increase in attentuation at the higher frequencies. This is overcome by feeding the output of the mixer to the base of emitter follower Trl, which has a very low input capacitance.

The signal tapped off from the slider of VR5, the volume control, is fed, via C7, to the base of the common emitter amplifier, \(\operatorname{Tr} 2\), which has its collector load, R10-R11, "Bootstrapped" from the emitter of \(\operatorname{Tr} 3\) via C10. The amplified signal at the emitter of \(\operatorname{Tr} 3\) is fed to the base of the p-n-p Dar-lington-connected emitter follower pair \(\operatorname{Tr} 4 / \mathrm{Tr} 7\) and to the base of the similarly connected \(n-p-n\) pair, Tr5/Tr6. Diodes D1 and D2, and VR6, in the emitter of Tr3, are used to apply a degree of temperature compensated base-bias to the output transistors and so minimise any cross-over distortion which might otherwise occur. The very low impedance output at the emitters of \(\operatorname{Tr} 6 / \operatorname{Tr} 7\) is fed to the output socket, Sk5, and thence on to the external speaker, via C13. Bootstrapping is applied from Tr6/Tr7 emitters to the R14-R15 emitter loads of Tr3 via C12. Overall d.c. negative feedback is achieved via R8, R9, R19; decoupled via C11.

A 12 volt battery supply is used, and an output power of well over 0.5 watt is available when feeding a \(15 \Omega\) speaker.

\section*{CONSTRUCTION}

For ease of construction, the major part of the circuitry is wired up on a small piece of Veroboard. Start construction by cutting the panel to size, as shown in Fig. 3a, and breaking the copper strips where indicated. Now drill the two small mounting holes, to clear 6BA screws, where shown, and cut back the copper around them to eliminate risk of short circuits when the panel is secured to the main chassis.

Now solder all components, shorting links, and leads in position on the panel as shown in Fig. 3b. Note that all components, other than R7 and R13, are mounted vertically. Insulated sleeving should be used where there is any danger of short circuits occurring. Before attempting to fit VR1 in olace, reduce the width of the three mounting legs, with the aid of a small file, so that they fit easily in the holes in the Veroboard. Particular care should be taken to ensure that all electrolytic capacitors are connected with the polarities shown. Heat shunts should be used when soldering all semiconductors in place.

(a)


Fig. 5: 'a' shows the wiring details and ' \(b\) ' cabinet details.
If preferred, D1 and D2 can be made from any scrap p-n-p germanium transistors, providing that the base-emitter junctions are intact, by cutting off the collector leads and soldering the resulting "diode" in place as shown.

When the assembly of the Veroboard panel is complete, double-check all wiring and make sure that no short circuits are occurring between the copper strips. If satisfactory, the circuit can now be given a functional check. Temporarily connect VR5 in place, set VR6 for minimum resistance, short the input to ground, and connect a 12 volt supply to the unit, taking care to monitor the supply current; the unit should draw about 8 mA . Now connect a \(15 \Omega\) speaker to the output, and check that there is no appreciable increase in mean current. If satisfactory, an input can be connected from a tuner, etc., and a functional check carried out; VR6 should be adjusted to give negligible crossover distortion consistent with a low no-signal mean current, which should work out at about 10 to 12 mA .

If the performance of the circuit is satisfactory, it should be run at fairly high volume for a few minutes, to make sure there is no tendency to thermal runaway. If there is any tendency to run-
away, the two output transistors (Tr6 and Tr 7 ) should be fitted with heat sinks. Once these tests have been completed, the rest of the unit can be constructed.

Make up the main chassis, from light gauge aluminium, as shown in Fig. 4a, and cut and drill the front panel, from a medium gauge aluminium, as shown in Fig. 4b. If a battery supply is to be used, cut and drill and bend the two battery holders, from light gauge aluminium, as shown in Fig. 4c; the batteries are held in place by friction. Before assembling these components, carefully cover the outer face of the front panel with Fablon or a similar self-adhesive decorative plastic material; a material with a light wood-grained finish was used on the prototype. Cut away the surplus Fablon with a sharp knife. Now secure the five sockets, Sk1 to Sk5, and the five variable resistors, VR1 to VR5, in place on the front panel. Next, bolt the front panel to the main chassis, and wire up as shown in Fig. 5a. When wiring up is complete, secure the Veroboard panel to the main chassis by passing two 6BA screws through the Veroboard and the chassis, using the mounting holes provided, and interpose two small rubber grommets between the chassis and the panel to act as spacers/insulators.

The main construction can now be completed by bolting the two battery holders in place. The two batteries should now be fitted in place and the unit given a final and complete functional check. The cabinet can now be made up, as shown in Fig. 5b. This is an easy assembly to make, the sides, top, base, and rear being simply cut from hardboard and screwed or nailed to four short lengths of wood which hold the unit in a box shape. When the cabinet has been assembled, smooth off all rough spots with a file or sandpaper, and then cover the complete job with Fablon or a similar self-adhesive decorative plastic. Finally

\section*{DUAL FUNCTION SIGNAL GENERATOR}
—continued from page 119
in other types is the provision of an external socket to which the grid of the r.f. oscillator may be directly switched. Since the oscillator is of the two terminal type, oscillations may be set up in external coils without the use of tappings or separate feedback coils. What is perhaps more important is that


Fig. 5 (left): Layout of dummy aerial.
Fig. 6 (top right): Circuit of dummy aerial.
Fig. 7 (bottom right): Simplified dummy aerial.

\section*{components list}
\begin{tabular}{|c|c|}
\hline Resistors: & Capacitors: \\
\hline All \(\frac{1}{2}\) watt, \(10 \%\) carbon, except where otherwise stated. & All sub-min. 15 VW electrolytics C1 \(8 \mu \mathrm{~F}\) \\
\hline R1-R4 120k \(\Omega\), \(5 \%\) hi-stab & C2 \(8 \mu \mathrm{~F}\) \\
\hline R5 \(8 \cdot 2 \mathrm{k} \Omega\) & C3 \(8 \mu \mathrm{~F}\) \\
\hline R6 \(47 \mathrm{k} \Omega\) & C4 \(8 \mu \mathrm{~F}\) \\
\hline R7 \(56 \mathrm{k} \Omega\) & C5 \(16 \mu \mathrm{~F}\) \\
\hline R8 \(10 \mathrm{k} \Omega\) & C6 \(\quad 16 \mu \mathrm{~F}\) \\
\hline R9 \(22 \mathrm{k} \Omega\) & C7 \(50 \mu \mathrm{~F}\) \\
\hline R10 \(2 \cdot 2 \mathrm{k} \Omega\) & C8 \(160 \mu \mathrm{~F}\) \\
\hline R11 8-2k \(\Omega\) & C9 \(16 \mu \mathrm{~F}\) \\
\hline \(\mathrm{R} 121 \mathrm{k} \Omega\) & C10 16 \(\mu \mathrm{F}\) \\
\hline R13 1 k ת & C11 \(50 \mu \mathrm{~F}\) \\
\hline R14 1-2k \(\Omega\) & C12 \(160 \mu \mathrm{~F}\) \\
\hline .R15 \(1.2 \mathrm{k} \Omega\) & C13 1000 \(\mu \mathrm{F}\) \\
\hline R16 \(470 \Omega\) & Semiconductors: \\
\hline \(R 17470 \Omega\) & \\
\hline R18 \(470 \Omega\) & Tr1 2G403 or NKT675 \\
\hline R19 33k \(\Omega\) & Tr2 2G403 or NKT675 \\
\hline VR1-VR4 \(100 \mathrm{k} \Omega\) variable & Tr3 2G374 or NKT274 \\
\hline VR5 \(5 \mathrm{k} \Omega\) variable with & Tr4 2G374 or NKT274 \\
\hline built-in on/off & Tr5 2N1304 or NKT713 \\
\hline switch (S1) & Tr6 2N1304 or 2N1306 \\
\hline RV6 \(500 \Omega\) skeleton preset & \begin{tabular}{l}
Tr7 2N1305 or 2N1307 \\
D1, D2 OA70
\end{tabular} \\
\hline \multicolumn{2}{|l|}{Miscellaneous:} \\
\hline \multicolumn{2}{|l|}{Sk1-Sk5=Coaxial sockets. B1-B2=6 volt, type} \\
\hline \multicolumn{2}{|l|}{DT1 batteries. Veroboard, wire, sleeving, screened} \\
\hline Fablon, etc. 15 ohm speak & er. \\
\hline
\end{tabular}
secure the mixer/amplifier chassis in place with the aid of four small wood screws passed through the holes in the corners of the front panel, then mark the front panel with transfers or pressure sensitive lettering.
oscillations may be set up in screened coils. Generally the presence of a screening can precludes the use of the more conventional grid dip oscillator technique. The author has found this facility to be of particular value when the resonance frequency of an unknown i.f. coil is required.

Let us suppose that an i.f. transformer in a receiver is suspect. The transformer is temporarily disconnected and one section connected via a short length of cable to the external socket of the generator. After switching the generator to this external coil, the signal emitted by the generator is picked up on a receiver. Let us assume that the i.f. transformer has a nominal resonant frequency of \(470 \mathrm{kc} / \mathrm{s}\). A receiver set to the medium waveband will give a response in the neighbourhood of \(940 \mathrm{kc} / \mathrm{s}\) \((319 \mathrm{~m})\), which is the second harmonic of \(470 \mathrm{kc} / \mathrm{s}\). Although no account has been taken of the inevitable stray circuit capacitances, a response in this region is almost certain proof that at least one section of the transformer is functioning satisfactorily. The remaining section may be tested similarly. In the foregoing example it has of course been assumed that the i.f. transformer has its own built-in tuning capacitors. Further valuable uses to which the generator may be applied are coil matching and capacitor testing, details of which are given in the October 1964 issue of Practical Wireless.


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HOW TO LISTEN TO THE WORLD
Published by World Publications.
E 184 pages. \(84 \times 5 \frac{1}{4} \times\) Price \(26 s\).

THIS is a new edition of a well established favourite. For those who have the previous edition there is little extra to be gained from purchasing this one. However, if you are a beginner and have had your appetite whetted by "PSE QSL" in the March Practical Wireless you will be helped considerably by this book.

Every aspect of DXing is covered both in theory and practice, and there are separate chapters on listening to various continents. For those with specialised interests there are chapters on learning languages by radio, listening to satellites and television DXing.

A good feature of the book is that every chapter is written by either a leading DXer or member of a short wave station's staff with the result that some good down-to-earth facts emerge. One slight disadvantage stems from this though in that inevitably there is a certain amount of overlap between chapters.

One disappointing feature is that the section How to write a report in Portuguese or Spanish is not in the latest edition. Even so a good buy for the beginner.-JMG.

\footnotetext{
三 HANDBOOK OF APPLIED MATHEMATICS
By E. E. Grazda, M. E. Jansson and W. R. Minrath.
Published by D. Van Nostrand Co. Lid., 46 Victoria Street, London, S.W.1. 1,119 pages. Size \(7 \frac{1}{4} \times 5 \frac{1}{4} i n\). Price 80s.
}

THERE can be no doubt that the authors of this book have given value for money. In over a thousand pages they have covered a wide variety of fields. The problem is that if one recommends this book, to precisely whom can it fairly be offered. Starting with a general treatment of the various sections of mathematics the authors continue for the remaining 800 -odd pages with the application of mathematics to various professions. For example, separate chapters are devoted to-Plumbing, Carpentry and Building, Brickwork, Print Shop, Accounting just to mention a few. For the layman it's a bit high up. The table headed "Coefficients of Transmission (U) of Pitched Roofs" might well prove too much for a layhandyman. On the other hand for the expert in a particular field, when he has read his chapter he will have another eight or nine hundred pages which are not applicable to his work.

As a person interested in mathematics as a whole, I found this book extremely interesting, and for those whose interests are parallel it would be a very useful addition to the bookshelf. Perhaps a better title would be "Applied Mathematician's Delight".-DLG.

\section*{三 NEWS FROM AROUND THE WORLD 1967 \\ Published by \(O\). Lund Johansen Ltd. \\ 36 pages. \(8 \frac{3}{4} \times 6 \frac{1}{2} \mathrm{in}\). Price \(15 s\).}

0NE of the fascinations of owning a short wave receiver is that when a new world trouble spot appears one can listen to the news from the spot. Alternatively you can hear the news from the various power centres and compare. To do this you need to know quickly when the country concerned has a news broadcast in a language you can understand and this is where this publication from the World Radio TV Handbook stable comes in with its listings of news broadcasts by both country and language.

For the DXer the book has a second use as an aid to the identification of stations. Whatever the language you can always tell the news broadcast. Reference to this book will show the stations transmitting news at the time concerned with ihe result that a process of elimination will enable the station to be identified.

One word of warning; although the times of news broadcasts are unlikely to vary greatly during the currency of this book the frequencies will. So don't pay too much attention to the frequency listings given.-JMG.

\section*{킁 ABC's OF ELECTRONIC TEST EQUIPMENT \\ By Donald A. Smith. Published by Foulsham-Sams Technical \(\equiv\) Books. 96 pages. \(8 \frac{1}{2} \times 5 \frac{1}{2} \mathrm{in}\). Hard covers. Price 168.}

IF you buy your instruments ready-made, a book on applications will appeal more than this slim volume. If you are a kit-building enthusiast, the information given by a reputable kit firm should be more than adequate for your needs. There is little here to augment it, despite a neat plug for Heathkit in the preface. To whom then, should this book appeal? Perhaps the best way to expound is to describe its contents and leave readers to judge.

Chapter 1, predictably, describes the meter movement. Chapter 2 explains the Volt-Ohm-Milliameter, and the following chapter the basic design of the valve voltmeter. There is no mention of the later types of transistor millivolter or high impedance meters and it seems obvious that this book has not been revised since the original publication in 1963. Transistor testers receive a very perfunctory treatment and valve testers are hastily skated over.

Perhaps the greatest disappointment is Chapter 6, where a description of signal tracers does not include a single buildable circuit, nor any sensible details of the use of this very handy instrument. The chapter on oscilloscopes is longer, and more fundamental, but reveals very little practical circuitry and virtually no practical application.

\section*{new books-continued}

Vital specifications are hardly mentioned at all.
Of all things to find in a purported instrument book, we find Battery Eliminators in Chapter 8. With modern regulated and transistorised power supply units, this chapter is something of an anachronism, just as the final chapter, on signal generators, has not reached the state of considering f.m. generators, wavemeters and other modern necessities.

The author is an electronics development engineer in instrumentation and his aim has been to give those intending to service electronic equipment a 'thorough understanding of test and measuring instruments'. It is a mystery why the publishers did not allow him the space to do so.HWH.

\section*{Catalogue Received}
G. W. Smith \& Co. (Radio) Ltd., 3-34 Lisle Street, London, W.C. 2 have just published their first comprehensive Catalogue of Electronic Components and Equipments. It contains over 150 fully illustrated pages and lists items ranging from relays to table lamps and communications receivers to zener diodes and amateur equipment.

The cost of the Catalogue is 5 s. plus 1 s . postage, but discount coupons included in the Catalogue enable the cost to be retrieved with purchases.
G. W. Smith carry the complete Lafayette range and are agents for Codar, Partridge Aerials, TW Electronics, Green, and Contactor Switchgear. They offer after-sales service and spares for all imported radio equipment shown in their Catalogue.

\section*{KEYING THE TEN-FIVE TX}
—continued from page 103
"C.W." and apply power to the transmitter. After a suitable warming up period has elapsed rotate the Function switch to "Net" whereupon the stabiliser should glow. Check the current as monitored by the externally connected testmeter; this should be in the range of \(15-20 \mathrm{~mA}\). Check that V1 is oscillating and that drive is available.
Connect a dummy load to the transmitter aerial socket (Sk3) and rotate the Function switch to "Transmit". Load up to approximately 8W. Check the current reading monitored by the external meter and compare it with the earlier reading; if the two readings differ adjust the value of R9 slightly in an attempt to make them equal each other. In the prototype this necessitated making \(\mathrm{R} 9=4 \cdot 7 \mathrm{k} \Omega\).
Later, the external meter may be removed and pin 7 of the OA2 tube returned direct to chassis. The meter should then be set to read \(0-250 \mathrm{~V}\) d.c. when a reading taken from between the R4/Ry junction and chassis should be 150 V at both the "Net" and "Transmit" positions of the transmitter Function switch.

When these tests have been satisfactorily' carried out the dummy load may be replaced with the station aerial and after adjusting the transmitter in the usual way a call may be put out in either c.w. or phone modes. It will then be found that the 10 W maximum input available under phone conditions can be increased to approximately 15 W of c.w. on " 80 " metres.

\title{
MAKE THIS TRANSFILTER PORTABLE
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FULL DETAILS IN NEXT MONTH'S ISSUE It's a 7 -transistor receiver just right for the experimenter. Uses transfilters for the i.f. inter-stage couplings. Provides higher " Q ", greater selectivity and more efficient matching than conventional i.f. transformers.

\section*{ALSO}

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PRE-SET 100 K b
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25E POT-METER Standard size with double pole switch by Egan with f
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\multicolumn{5}{c|}{ Number of Positions } \\
\multicolumn{6}{c|}{} \\
1 pole & 2 & 3 & 4 & 6 & 12 \\
2 pole & \(3 / 6\) & \(3 / 6\) & \(3 / 6\) & \(3 / 6\) & \(3 / 6\) \\
3 pole & \(3 / 6\) & \(3 / 6\) & \(3 / 6\) & \(3 / 6\) & \\
4 pole & \(3 / 6\) & \(3 / 6\) & \(3 / 6\) & & \\
Any 12 switches ordered together \(40 /-\) \\
\hline
\end{tabular}

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\begin{tabular}{|c|c|c|c|c|c|}
\hline Type & & Tupe & & Type & \\
\hline No. & Prica & No. & Price & No. & Pric \\
\hline 2N1727 & 15/- & Matiol & \(8 / 6\) & \(0 \mathrm{C71}\) & \(3 /\) \\
\hline 2N1728 & 10/- & MAT120 & \(7 / 9\) & \(0 \mathrm{C7} 2\) & b/ \\
\hline 2N 1742 & 251- & MAT121 & 8/6 & 0075 & 6 \\
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\hline 2N1748 & 10/- & OA10 & 6/- & \(0 \mathrm{C77}\) & \\
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\hline ACY19 & 6/6 & OA85 & \(2 / 6\) & \(0 \mathrm{C82}\) & \\
\hline ACY20 & 5/6 & OA90 & 216 & \(0 \mathrm{C83}\) & d \\
\hline ACY'21 & 6/- & OA91 & \(2 / 6\) & \(0 \mathrm{C8} 4\) & 61 \\
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\hline MAT 100 & 7/9 & \(0 \mathrm{C70}\) & 4/- & EB251 & 10 \\
\hline
\end{tabular}

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Teated
\begin{tabular}{lllll}
100 v. & \(1 / 3\) & 1 Amp. & 100 v. & 8 \\
200 v. & \(1 / 8\) & & 200 v & 4 \\
400 v & \(8 / 6\) & & 400 v. & 0 \\
100 v. & \(3 / 8\) & & 10 Amp. & 100 v \\
200 v. & \(5 /-\) & 8 \\
400 v & \(7 / 6\) & & 200 v. & 12 \\
600 v. & \(9 / 8\) & & 400 v. & \(14 / 8\)
\end{tabular}

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Designed to operate transistor sete and smpliflers. Adjustable output \(8 v ., 9 \mathrm{~V}\)., 12 volts for up to 600 mA (claca B working). Trkes the place of any of the following battertes: PI', PP3, PP4, PP6, PP7. rectian others. Kit comprises: maina transinimer 600 mfd . condengers Z load resistor, \(, 0,000\) and Real snip at only \(14 / 6\), plus \(3 / 6\) postage

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12 WATTS R.M.S. OUTPUT CONTINUOUS SINE WAVE (24 W. PEAK)

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The embodiment of power, efficiency and reliability, there has never been an amplifier to touch the \(\mathbf{Z . 1 2}\) for adaptability and compactness. Nothing could be better than this fine amplifier for use with space-saving plinth-mounted motor and pick-up assemblies. Equally, the light weight of the \(\mathbf{Z . 1 2}\) makes it the ideal guitar amplifier, particularly since it operates efficiently on any power supply between 6 and 20 V.D.C. The pre-amp of this 8 -transistor masterpiece will accept the outputs of pick-up, radio and microphone, etc. Full details for matching, control and selector switching circuits are in the manual supplied with each unit. The \(\mathbf{Z . 1 2}\) is now in use all over the world and is the accepted standard for all hi-fi needs.
\end{abstract}

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H.A. (Consulting gineer), London, N6.

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PRE-AMP AND CONTROL UNIT
FOR USE WITH TWO Z.12s OR OTHER STEREO AMP

THE SINCLAIR STEREO 25 has been designed specially to ensure the highest possible standards of reproduction when used with two Z.12s or any other first class stereo power amplifier, Best possible components are used in the construction of this superb unit, whilst its appearance reflects the professional elegance characteristic of all Sinclair designs. The front panel of the Stereo 25 is in solid brushed and polished aluminium with beautifully styled solid aluminium control knobs. Mounting the unit is simple, and power is conveniently obtainable from the Sinclair PZ. 3 which can also be used to supply two Z.12s to make a complete stereo assembly. Hi -fi enthusiasts seeking the ultimate in domestic listening will find all they want from this combination of Sinclair units. With a Micro-FM for tuner, they will have an installation to compare favourably with anything costing from four to five times as much.

Performance figures obtained using Stereo 25 , two Z.12s and a PZ.3.
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SINCLAIR PZ. 3 Transistorised A.C. mains power supply unit for two Z.12s with Stereo 25.
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\title{
The most remarkable letter we have so far received
}
P.O. Box 43, PAEKAKARIKI, New Zealand.
27th February, 1967. Thank you very much for the new Micromatic which arrived safely by Airmail. Our 13 -year-old son is highly delighted. On the first evening he logged several New Zealand stations. These included our one and only "pirate", Radio Hauraki, stationed in the gulf of that name well over 400 miles north of here.
His biggest surprise was when 2CY, Canberra (10Kw) identified itself. Australia is more than 1,200 miles away! I tested the receiver within half a mile of 2 YA and 22 B (just north of Wellington). Selectivity remained perfect. Neither station swamped the other and the customary nul was evident when the ferrite aerial was end on to the transmitters.
In the metal coach of an electric train, the receiver functioned normally even under such noise producing conditions.
You have produced a radio receiver which has no equal. Its design size and performance are such that even you will not easily evolve a successor
(Signed) Arnold S. Long
The original of this and countless other letters which enthusiasts send us can ahways be seen at our Cambridge offices.

\title{
SINCLIAR MICROMAIIC THE SMALLEST SET IN THE WORLD
}
- \(14 / 5{ }^{\prime \prime} \times 13 / 10^{\prime \prime} \times 1 / 2^{\prime \prime}\)
- NEW 6 STAGE CIRCUITRY
- AMAZING POWER AND RANGE
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Guarantee
Should you not be completely satisfied with your purchase when you receive it from us, your money will be refunded in full at once and without question.

This British-made six stage transistor receiver is a fully fledged radio with all the features essential to reliable listening. It is smaller than anything you have ever used before, yet it gives good choice of programmes anywhere, is selective, powerful, dependable. When, after two or three months or so, the two batteries need replacing, new ones are easily obtainable from radio shops, Boots Chemists, etc. Good listening works out to under a halfpenny an hour. Whether you buy the

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