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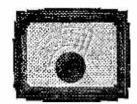
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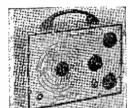
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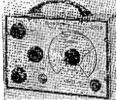
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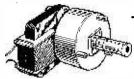
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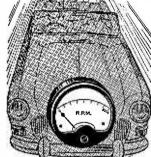




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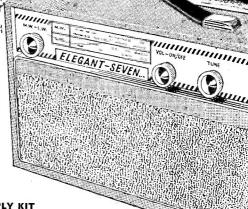


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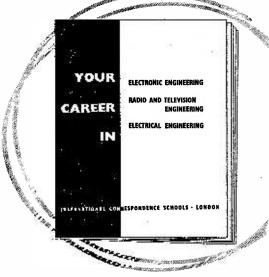
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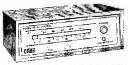
R.S.C. STEREO/20 HIGH FIDELITY AMPLIFIER

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PROVIDING 19/14 WATT ULTRA LINEAR PUSH-PULL OUTPUT ON
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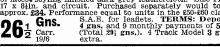
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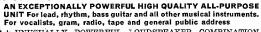
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Highly sensitive. Push-Pull high output, with Pre-amp./Tone Control
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To vocalists, gram, radio, tape and general public address

★ UNUSURALLY POWERFUL LOUDSPEAKER COMBINATION consisting of a FANE HIGH FLUX 15in. 30 watt unit PLUS a FANE 12in. 20 watt unit with extended frequency response. ★ 4 Jack Inputs and two Volume Controls for simultaneous use of up to 4 pick-ups or "mikes".

★ Cabinets covered in two-tone Rexine/Vynair with gold trimming. Fitted carrying handles. ★ Separate Bass and Treble Controls giving "lift" and "cut".

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Consisting Mains Transformer, Metal Rectifier, Electrolytics, smoothing choke, chassis and circuit. 200/250v. A.C. mains. Output 250v. 60mA, 6.3v. 2a or with case in lieu of chassis 260s.

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G15 15 WATT AMPLIFIER for Lead or Rhythm Guitar, Mike, Gram or Radio

High-fidelity output. Separate bass and treble controls. Twin separately controlled inputs so that two instruments or "mike" and pickups can be used at the same time. Heavy Duty 12in. 20 watt Speaker. Cabinet covered in attractive Rexine/Vynair. Size 18 x 18 x 18 in. 19½ Gns. Ordeposit 3 gns. and 9 monthly payments of 43/7? (Total Carr. 15/- £22.15.3). S.A.E. for leaflet.

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Flux Density 17,000 lines. Fully Guaranteed.

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FANE HEAVY DUTY HI-FI SPEAKERS 12in. 20 watt. Type 122/10.

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R.S.C. COLUMN SPEAKERS Covered in two-tone Rexine/Vynair. Ideal for vocalists and Public Address. 15 ohm matching Type C58, 15-20 watts. Fitted five 8in. high flux speakers. Overall size approx. 121 Gns. 22 x 10 x 5in. Or Deposit 22 and 9mthlypmis28/-(Total£14.12.0)
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for Guitar, Vocal or Instrumental Group



A Four Input, two volume control Hi-Fi unit with separate Bass and Treble "cut" and "boost" controls. Latest type valves. Housed in strong Rexine covered cabine carrying handles. Attr

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For 200-250v. A.C. mains. Output for
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12in. HIGH QUALITY LOUDSPEAKERS

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In walnut veneered cabinet. 10 Watt
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Speech coli 3 or 15 ohms.
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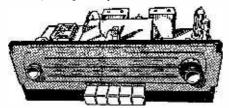
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250-0-250v. 100mA, 6.3v. 2a, 0.5-6.3v. 2a.
250-0-250v. 100mA, 6.3v. 4a, 0.5-6.3v. 3a.
300-0-300v. 100mA, 6.3v. 4a, 0.5-6.3v. 3a.
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39/9 39/11 27/9

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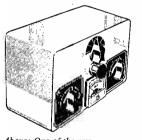


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- (f) 4.5 v. A.C. amp. common earth.
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5 valves, 7 silicon rectifiers, 4 Selenium HV rectifiers. Brand new, £9.10.0. Carriage 12/-.

PHASE MONITOR ME-63/U. Manufactured recently by Control Electronics Inc. Measures directly and displays on a panel meter the phase angle between two applied audio frequency signals within the range from 20-20,000 cps to an accuracy of ±1.0°. Input signals can be sinusoidal or non-sinusoidal between 2 and 30v peak. In excellent condition together with handbook and necessary connector £45. Carriage 30/-

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0-3 amp RF	2in.square		• •	• •	20/-
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2 KW ULTRASONIC GENERATOR together with power supply unit for 200-250 v. A.C. Complete two chassis with interconnecting cables. Frequency 37 to 43 kc/s adjusted by fine control. Peak output 2 kw., average output 500 w Completely new with valves and manual £65, carriage paid U.K.

LARGE SELECTION of mains and Heavy Duty L.F. TRANSFORMERS.

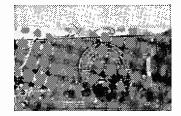
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MARCONI SIGNAL GENERATOR TYPE TF 801B/3/S. Frequency range 12-485 Mc/s. in five ranges. Directly calibrated frequency dial. Output waveform: C.W. sinewave A.M., pulse A.M. (from ext. source only). Internal modulation frequency 1,000 c/s. Output: a, normal—continuously variable directly calibrated from 0.1µ v.—0.5 v. b, high: up to 1 v. modulated or 2 v. unmodulated, output impedance 50 ohms. Fine frequency tuning control, carrier on/off switch, built-in crystal calibration for 2 Mc/s and 10 Mc/s. Stabilised voltage supply. In excellent "as new" condition. Fully checked and guaranteed. Including necessary connectors, plugs and instruction manual.

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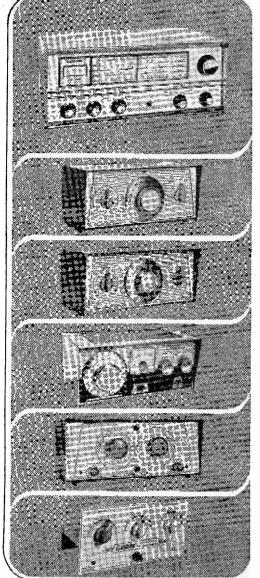
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4in. Triple play, 900ft. Mylar 1	17 6 7in. Standard play, 1200ft. Acet. 12 6 15 0 7in. Standard play, 1200ft. Mylar 12 6
5in. Double play, 1200ft. Mylar 1 5in. Long play, 900ft. Acetate 1	
5in. Standard play, 600ft. PVC	8 6 7in. Double play, 2400ft. Mylar 25 0
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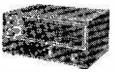
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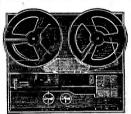
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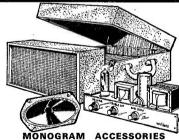
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PRACTICAL WIRELESS

VOL 42 No 6

issue 716

OCTOBER 1966

TOPIC OF THE MONTH

THE LONG WAIT

AFTER many false starts, promises and delays, the Government has fired a preliminary salvo across the bows of the pirate radio ships. This was in the form of a Bill, presented by Mr. Edward Short, Postmaster General, and published on July 27th.

The Marine, &c., Broadcasting (Offences) Bill enacts that it shall be unlawful for a broadcast to be made from a ship, aircraft or any other structure within U.K. territorial limits. It also prohibits U.K. and colonial citizens from operating broadcasting stations on non-U.K. ships or aircraft on or over the high seas or on other structures.

Clause 4 makes it an offence to furnish ships or aircraft, supply goods and materials or to supply and maintain radio equipment or otherwise assist in their physical maintenance. Further clauses make it an offence to supply programme material or advertising and lay down that a person guilty of an offence under the Act shall be liable on summary conviction to a fine of £100, imprisonment for a term not exceeding three months, or both. This Bill, of course, has still to receive the approval of Parliament and the Queen.

There is already considerable pressure against this Bill. The listening millions who, if you believe all the claims, will not like it. Nor will the organisations running these stations; Radio Caroline alone is reputed to be making a profit of something like £1,000,000 a year.

Legislation is, of course, long overdue. The present proliferation of pop-music stations is ridiculous and their *modus operandi* is irresponsible. The whole situation must clearly be rationalised in a re-think of the whole broadcasting set-up to bring it into line with today's demands and requirements. The key factor is local broadcasting—its place in modern society, its shape, objectives and how it can slot into the existing national networks.

This problem, however, remains in the melting pot. For it is one of the subjects to be covered in the long awaited White Paper on Broadcasting—which has been promised, and postponed, so often that we can only assume that it has been absentmindedly filed in the Historic Documents Archives of the Post Office.

At the time of going to press, several newspapers carried reports that the Cabinet has agreed to set up a chain of v.h.f. stations to broadcast pop-music.

W. N. STEVENS, Editor

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NOVEMBER ISSUE WILL BE PUBLISHED ON OCTOBER 6th

All correspondence intended for the Editor should be addressed to: The Editor, "Practical Wireless", George Newnes Ltd., Tower House, Southampton Street, London, W.C.2. Phone: TEMple Bar 4363. Telegrams: Newnes Rand London. Subscription rates, including postage: 36s. per year to any part of the world. © George Newnes Ltd., 1966. Copyright in all drawings, photoapphs and articles published in "Practical Wireless" is specifically reserved throughout the countries signatory to the Berne Convention and the U.S.A. Reproductions or imitations of any of these are therefore expressly forbidden.

Closed Shop!

WHILE I agree with you, the editor, that attendance figures for recent Radio Shows have been falling, I do not think the public should be barred from the Show. The reason for the poor attendance can clearly be put at the foot of the organisers' door.

At the last Radio Show—you cannot count last year's fiasco—I wasted 3/6d. going to Earls Court. Without doubt, I could have seen almost as much walking down my own High Street. As far as new developments were concerned, I saw few. Several of the major manufacturers—particularly the component boys—had large stands, but large portions were cordoned off for the "trade".

Many of the new developments were displayed within these private enclosures. I know, I falsely stated that I worked for J. Bloggs and Co. and "that we use your components". With this, a smiling representative shook my hand and gladly showed me all the latest developments. On others, I indicated that I was an amateur and received polite rebuffs.

So if we are allowed to see another Radio Show, please can we have a chance of seeing the "works"? Remember, the dealer is only a gobetween; we are the real customers.

Also, is it not possible to popularise the Radio Show? In the good old days the radio and television organisations used to put on first-class entertainments. If the radio industry realised that these organisations are not so wealthy as everyone thinks, and was prepared to support them with "brass", I am sure something could be worked out. One can, of course, let the radio and television industry strangle itself. If present trends continue, it is only a matter of time.

Edward Salter, B.Sc. London, W.1.

Burglar Alarms

I AGREE with McNair's letter published in the July issue (concerning the Simple Proximity Detector, March 1966), but with the following reservations: It is indeed the responsibility of the Police to protect one's property and they will do so if they are informed. However, as McNair himself writes, the Police cannot work miracles, but they will make sure that premises are regularly inspected. It is the inbetween times when the burglar strikes. I know, it has happened to me.

Another point I wish to make is that electricity supplies can easily be disconnected from houses without the burglar having to enter the premises. Thus, it is important to operate any burglar device from separate supplies; transistor equipment has much to offer when compared with valve gear, since the current drain is nowhere near as high.

H. A. L. Wagner.

Kuala Lumpur.

NEWS AND..

RADIO COMMUNICATIONS EXHIBITION

The Exhibition will again take place at the Seymour Hall, Seymour Place, London W.1., from Wednesday October 26 to Saturday October 29, 1966, and will be open from 10 a.m. to 9 p.m. daily. Admission 3s.

The Stage Presentation will be a display by the Royal Signals who are taking part for the first time. The Post Office will also be showing and the Royal Navy. All space for Exhibitors has been taken and the largest Exhibitor is a newcomer to this Hall: Standard Telephones and Cables Ltd., Components Group, who will display a comprehensive range of radio components. The return of the Company S.V.S. Aerials and Towers will assist many with their range of masts and fittings.

The RSGB Stand will be a longer stand with a book and information service, live transmitting stations on several frequencies including v.h.f.

Meetings of all Radio Groups and Armed Forces' Clubs will also be held in the Lecture Hall and Overseas Guests' Night will be held in the restaurant on Friday evening, October 28, 1966, when the attendance is expected to break last year's record. CCTV will be used to announce all overseas visitors.

The Exhibition Awards for Home Construction and Manufacturers' Equipment will again take place; silver plaques being presented to the winners. Many new ideas on developments of home and overseas transmitters, transceivers and receivers particularly on s.s.b. and v.h.f. will be seen. Also the latest technical books will be available for inspection or purchase.

A famous £200 world coverage communication receiver will again be presented to the lucky entry ballot card holder.

SUB-MINIATURE BATTERY CHARGER



Lexor announce a sub-miniature battery charger. Known as the "MilliQ", the unit is intended for incorporation into equipment employing rechargeable batteries or cells. Typical applications are with portable transistorised instruments, radio sets and tape recorders operating from nickel-cadmium accumulators. The inclusion of a "MilliQ" charger can enable the equipment to operate from either its internal battery or the mains supply, and in the latter case, the battery will be automatically recharged.

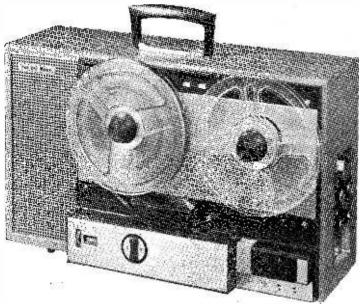
The unit measures $1\frac{1}{4}$ in. $x \frac{3}{4}$ in. diameter and is in the form of a sealed aluminium can. Two versions are available: one with flying lead connections for orthodox mounting and one designed for direct application to a printed circuit. Input voltages may range from 110 to 240V a.c., with resulting charge currents from 8mA at 110V input to 18mA at 240V input. Charging currents are constant for cells between 1-4V and 25V total. The unit is completely unharmed by short or prolonged overload or short circuit and may be disconnected from the battery without damage.

Prices can be as low as 8s. each in production quantities and the unit is offered on short delivery. The address of Lexor Electronics Ltd. is 25/31

Allesley Old Road, Coventry.

... COMMENT

VAN DER MOLEN TAPE RECORDER



Van Der Molen, 42 Mawney Road, Romford, Essex, announce Model VR7, a high performance tape recorder using a new 3-speed 4-track vertical deck mechanism. It is fully transistorised, has 5 watts output, recording level meter, mixing, bass and treble controls, an 8in. round speaker and facilities for listening on record and stereo output. It has a polished teak cabinet, moving coil microphone and 7in. spool of tape. Price is 39 guineas.

BICC MICROWAVE TOWERS FOR IRAN

British Insulated Callender's Construction Company Ltd., has received an order from G.E.C. (Telecommunications) Ltd. for the supply and erection of three microwave towers in Iran. The towers will be sited at oil pumping stations at Abadan, Bandur Mashur, and Khor-doraq and will form part of a telecommunications network linking the pumping stations.

Two of the towers are 275ft, high and the other is 110ft. These have recently been added to the BICC range of standard towers.

MULLARD SERVICE DEPARTMENT

With effect from August 8, 1966, the Mullard Service Department at 294 Purley Way, Croydon, Surrey, moved to premises at the Mullard plant at Mitcham.

All enquiries should be directed to the new address: Mullard Limited, Service Department, P.O. Box 142, New Road, Mitcham Junction, Surrey. Telephone Mitcham 3471.

ECHO SOUNDERS FROM FERROGRAPH

The Ferrograph Company Ltd., announce three echo sounders. The "Offshore 500" at £108, the Inshore Sounder at £52 and the Graphic Sounder at £66. A leaflet describing these units and giving brief specifications may be obtained from The Ferrograph Company Ltd., Ferrograph House, 84 Blackfriars Road, London, S.E.1.

New Thinking Needed for Sound Broadcasting

On the subject of pirates, Mr Dobbs stated (July issue of PRACTICAL WIRE-LESS) that "our offshore buccaneers have probably indicated to the BBC that there is a healthy demand for 'Wallpaper' music throughout the day " Undoubtedly there is such a demand but the BBC seems to ignore this fact. Only recently, the Director General of the BBC (in Middlesbrough for a BBC Week) was reported in a local newspaper as saving something to the effect that the audiences claimed by pirates were excessive, that they (the pirates) must have tapped an entirely new kind of audience - because the audience measurements for the BBC sound services were constant. (In all fairness I must stress that these were not his exact words but it is a fair indication of what he was reported as saving.)

The recently published proposals for extending the BBC sound service does not take into account the demand for "non-stop pop". The objections of the Musicians' Union are cited as examples of obstacles but I have not noticed any detrimental effects on musicians since the first pirate went on the air—which is now some time ago.

I suppose that the numbers who listen to the BBC could decrease still further by the satisfaction with the present audience and the refusal to tap the socalled "new" audience. Objectors to the proposals to create a fourth radio channel serving the same purpose as pirates have pointed out the lack of available wavelengths as allocated to Britain at the last conference in Geneva on frequency allocations. They wish to preserve the European medium-wave band as it is at present—an intricatelyarranged system of stations. But the pirates are playing havoc with this system; and as other countries extend their broadcasting facilities I very much doubt whether they will take much more notice than the pirates; for example, Mr. Dobbs mentioned the new Peking transmitter on 1,525 kc/s.

The obvious conclusion one can draw from the briefest summary of facts is that it is high time that a new conference be called to discuss the entire rearrangement of the wavebands, making use of new inventions and discoveries in the field of broadcasting, and making allowances for further expansion by each country of its existing broadcasting facilities. Then the BBC can follow the Swedish model and create a new channel for canned sound.

P. Charlton.

Yorks.

More News and Comment on Page 420



Very few serious amateurs or s.w.l's these days would dream of using a t.r.f. in fact the majority would probably laugh at the idea. Yet in the past these receivers were extremely popular and one reads of simple circuits giving truly amazing results.

reads of simple circuits giving truly amazing results. The writer wished to use "double" valves for a particular application, but not having had a great deal of experience with them, decided to try the idea out first in a simple application in order to investigate the possibilities and the various snags which would doubtless arise. The result of this experiment is the unit about to be described.

Standard Circuitry

The "standard" circuit of a t.r.f. receiver is usually offered as a three valve unit. This comprising three stages with one valve to each stage; r.f. amplifier, detector and audio amplifier. It was decided to duplicate this "standard" but with the proviso that the three valves should be "double" valves. This arrangement gives, on the face of it, a three valve t.r.f., but since these valves are "doubles" then the project becomes a six-stage circuit. By this means it has been possible to design a t.r.f. receiver giving above average performance

and having features which place it in the communications class.

The valves chosen are all the same type—ECF82/6U8. These are triode-pentodes whose normal function in life is in the role of a frequency changer up to 200 odd Mc/s. These are freely available both from manufacturers' sources and the surplus market.

Having now a chassis with three innocent looking valves perched on it, the problem resolves itself into fixing a function for each stage since in effect we have a six-valve circuit comprising three pentodes and three triodes.

The main drawbacks or "bugbears" of t.r.f.'s are (a) radiation of interference by the reacting detector stage; (b) lack of selectivity; (c) tricky reaction, often due to variations from the aerial circuit affecting the detector. In this design these difficulties are not so much reduced as annihilated!

The Circuit

Commencing with the aerial, the first valve in Fig. 1, the triode of V1 is connected in a grounded

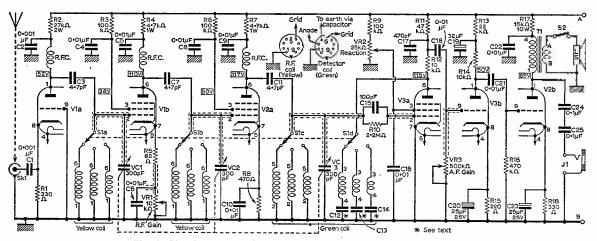


Fig. 1: Circuit diagram of the receiver, less power unit. (See Fig. 2)

grid configuration noted for its ability to isolate one stage from another and also present a low impedance input to the aerial. This stage is capacity coupled to the first tuned r.f. amplifier, the pentode section

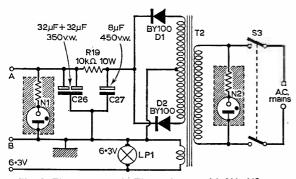


Fig. 2: The power unit. The resistors with N1, N2, are an integral part of the neon units.

of V1. This stage in turn is again top capacity coupled to V2a pentode wired as another tuned r.f. amplifier. V3a pentode is a reacting detector using the variation of screen potential as a reaction control.

At this point it will be realised that any spurious radiation from the detector has to fight its way through two tuned r.f. stages plus the grounded grid in order to reach the aerial. In the prototype it proved too much for this particular gremlin and no such radiation could be detected. The whole receiver is installed in an earthed aluminium case to ensure minimum radiation from the actual circuitry and components. Selectivity is extremely good since there are three tuned circuits plus an a.t.u. used by the writer. Also, variations in aerial loading affecting

To grid (pin 2) of V1b

To grid (pin 2) of V2a

To grid (pin 2) of V3a via

R10 and C15

To anode of V3a

To chassis

o chassis

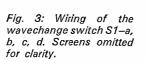
To chassis

To chassis

the regenerative detector stage are minimised by the three stages between detector and aerial, but more on this point later.

The high value of screen resistors was found imperative in the interests of stability. In the writer's model was possible it reduce these values to around $82k\Omega$ before instability set in. Since this "threshold" vary with different constructors it was thought best to use the values marked.

The voltages at various strategic points in the circuit are marked in fig. 1 and should act as a guide only and not be interpreted as a b s o lute



values. Similarly, for those who wish to experiment, the values of R13 and R17 may be varied for more gain on the audio side.

The remaining two triodes, V3b, V2b, are used as audio amplifier and output stage respectively, providing ample volume on local signals to drive the small loudspeaker used.

Construction

There is a great deal of gain in this receiver, and if due care is not taken in construction the end result will always be the same—instability. Careless wiring or a dry joint will practically guarantee this so watch these points carefully.

Each valve is screened from its neighbours with a strip of tinplate to help eliminate interaction between stages. Note also the extra screen across V1 which shields the triode section and its components from the pentode section. We don't want our hard won selectivity and isolation ruined by signal leaking round by various alternative paths.

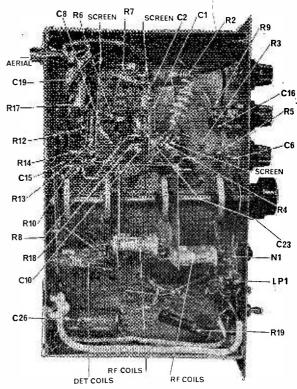


Fig. 4: Under chassis layout showing positions of some of the main components. Note small screen across V1.

Although there is more to this one than the average t.r.f. it is really no more difficult to wire up. If you can wire up a simple one valve circuit, then all you have to do is just that—six times! The obvious rules apply and are no different from any other unit construction. Heater leads twisted and kept away from the grids and associated components, wire these first, tuck the leads out of the way and wire $0.01\mu F$ disc ceramics across the heater pins at each valve base using the shortest possible leads. Keep anode and grid wiring as far apart as possible and make sure, very sure, that all soldered joints are "good uns".

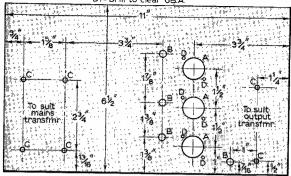


Fig. 5: Top chassis layout of the valves and two transformers.

The main tuning capacitor has a 10:1 reduction drive fitted. On the H.F. bands a greater reduction would be an asset due to the dozens of stations receivable. The dial pointer was made from a piece of thick celluloid and locked in position with the locking nut on the slow motion drive.

Bandswitching

As shown, the receiver covers approximately 1.5 to 30Mc/s in three switched bands. There is no reason at all why plug in coils should not be used and this would only require three B9A valveholders in place of the bandswitch. By this means the tuning range of the receiver could be extended to cover M.W. and L.W. Details of the bandswitch and coil unit are given in Fig. 3. Your scribe must confess to an oversight here in that when the unit was finished it was thought impossible to adjust the cores of the coils in order to align the receiver. However, by drilling holes in the screens to allow a fret saw blade through in line with the coil slugs this disaster was avoided.

To obtain peak performance the cores of the coils should be adjusted for maximum signal. The r.f. coil cores should be fixed before the unit is installed, the second r.f. stage and detector coils can then be peaked after the coil pack is fitted in position.

The reaction feedback capacitors C12, C13, C14, will require a value between 50-200pF. The best idea is to use a 200pF trimmer in these positions and adjust for the set to just oscillate when VR2 is at minimum. Alternatively various fixed values might be substituted until a satisfactory value is found.

There are no trimmers across the coils, if there were then these could be peaked instead of the coil cores. Would-be constructors might care to think along these lines before commencing construction. Dimensions are given but these will depend on the actual components used. An underchassis layout photograph is given in Fig. 4. Purchase all components first, lay them out on the chassis and then, only then, start drilling.

The loudspeaker in/out switch is optional if phones only are to be used. Also the power indicators, N1, N2, LP1, might be dispensed with since it is rather a luxury to have visual indication of mains, h.t., and heaters, perhaps fuses would be more useful. Certainly the inclusion of a fuse in the lead from the centre tap of the mains transformer to earth would be a wise precaution.

There is room beneath the chassis to install a smoothing choke for those who prefer this type of circuitry. If this is adopted then choke input is strongly recommended.

The mains transformer shown is a standard item although 80 mA is a very generous rating since the set only draws some 15-20 mA. Any transformer rated from 30 mA upwards at 20 volts will serve. Similarly almost any choke which will pass 30 mA may be used for the choke input circuit suggested.

The dials and wording are all hand-made to suit

-continued on page 401

★ components list

Resistors: R1 330 Ω R2 27k Ω 2 watt R3 100k Ω R4 4·7k Ω 1 watt R5 82 Ω R6 100k Ω R7 4·7k Ω 1 watt R8 470 Ω R9 100k Ω R10 2·2M Ω	R11 $47k\Omega$ R12 $10k\Omega$ R13 $22k\Omega$ R14 $10k\Omega$ R15 220Ω R16 $470k\Omega$ R17 $15k\Omega$ 10 watt R18 330Ω R19 $10k\Omega$ 10 watt
$ \begin{array}{c} \textbf{Capacitors:} \\ \textbf{C1} & 0.001 \mu \textbf{F} \\ \textbf{C2} & 0.001 \mu \textbf{F} \\ \textbf{C3} & 4.7 \textbf{p} \textbf{F} \\ \textbf{C4} & 0.01 \mu \textbf{F} \\ \textbf{C5} & 0.01 \mu \textbf{F} \\ \textbf{C6} & 0.01 \mu \textbf{F} \\ \textbf{C7} & 4.7 \textbf{p} \textbf{F} \\ \textbf{C8} & 0.01 \mu \textbf{F} \\ \textbf{C9} & 0.01 \mu \textbf{F} \\ \textbf{C10} & 0.01 \mu \textbf{F} \\ \textbf{C11} & 4.7 \textbf{p} \textbf{F} \\ \textbf{C12} \\ \textbf{C13} \\ \textbf{See text} \\ \textbf{C14} \end{array} $	C15 $100 \mathrm{pF}$ C16 $0.01 \mu \mathrm{F}$ C17 $470 \mathrm{pF}$ C18 $0.01 \mu \mathrm{F}$ C19 $32 \mu \mathrm{F}$ 250V. electrolytic C20 $25 \mu \mathrm{F}$ 25V. electrolytic C21 $0.01 \mu \mathrm{F}$ C22 $0.01 \mu \mathrm{F}$ C23 $25 \mu \mathrm{F}$ 25V. electrolytic C24 $0.1 \mu \mathrm{F}$ C25 $0.1 \mu \mathrm{F}$ C26 $32 + 32 \mu \mathrm{F}$ 350V. electrolytic C27 $8 \mu \mathrm{F}$ 450V. electrolytic
Valves: V1 ECF82/6U8 V2 ECF82/6U8 V3 ECF82/6U8	
3 Coils Green Range 3 Switch 1P 3W 4B Coo	de SS/666 Specialist Switches London, W2. (24/- inc. p. & p.)

LOW VOLTAGE

POWER SUPPLY UNIT

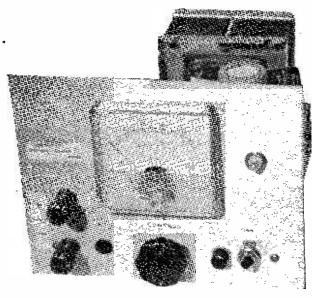
by C. J. Mitchell

HIS design is for a simple stabilised voltage power supply suitable for running transistorised equipment, low voltage motors etc. It uses two low power transistors and one power transistor as well as a bridge rectifier assembly.

The voltage range is from 0.5 to 30 volts and the maximum current obtainable varies from 100mA at 30 volts output to 400mA at 0.5 volts output. It has been designed so that a short circuit across the output will not damage the supply. The short circuit current is about 450mA in order to protect the diodes in the bridge rectifier. If higher current rated diodes are available then the short circuit current and hence the maximum current can be increased. The design is relatively inefficient as far as power transfer is concerned as it uses a large ballast resistor. All components are readily obtainable and layout is not critical except for the ballast resistor which should be kept clear from other components particularly the semiconductors as it could dissipate a lot of heat under certain conditions.

Circuit Description

A Douglas MT104AT transformer which has a 50 volt 2 amp winding tapped at various voltages was used by the author. The 33 volt tap is used in this circuit. The primary has the usual adjustments for 200-250V



input. If not obtainable then the MT103AT (1 Amp) or MT105 (3 Amp) transformers are also suitable, or for that matter any similar one by a different maker.

The bridge rectifier contains four OA210 semiconductors. Any higher current rated diodes can be used (i.e. BYZ12). The minimum rating required is 50 volts p.i.v. and 500mA mean rectified current. Do not omit the fuse in one side between the transformer and the bridge as if one diode goes short circuit the mains transformer will be subjected to an excessive load and possibly be damaged. A delay fuse or a resettable trip type might be a good idea in this position. The 2000µF capacitor is a simple reservoir/smoothing capacitor.

The Zener diode determines the maximum voltage and so a 30 or 33 volt diode is required. There are some 30 volt zeners on the market but three 10 or 11 volt zeners connected in series will do just as well. The $1.5 \mathrm{k}\Omega$ resistor is a limiting resistor to limit the current through the zener to a reasonable value. The $10 \mathrm{k}\Omega$ potentiometer is the output voltage control and should be a good quality linear wire wound pot. if possible. This taps off a voltage from the zener reference and passes it to the first transistor, then to the second transistor and finally to the OC29 power output transistor. The transistors act as current amplifiers

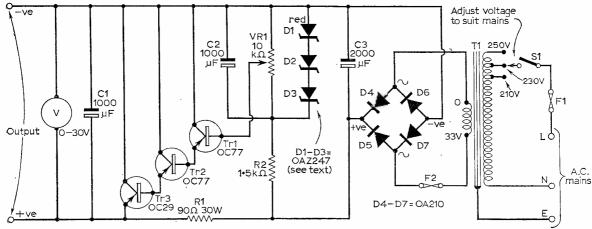
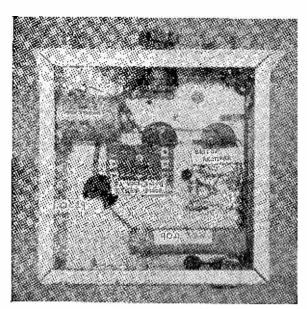


Fig. 1: Circuit diagram of the low voltage power supply unit.



i.e. even though the load current is say 100 mA the current drawn from the zener is a few microamps, thus the voltage delivered from the reference does not alter.

Excess voltage, i.e. the voltage difference between required output as set by the zener diode and the output voltage from the bridge rectifier is dissipated by the ballast resistor. This resistor also determines the short circuit current of the supply and thus, has a fairly high wattage rating.

Almost any voltmeter 0-30V is suitable for the power supply unit. The cheaper Japanese ones on the market are ideal.

Construction

The prototype was built on a chassis 7 x 7 x 2 in. with a small front panel, but any available chassis will suffice. If the supply is to be built into a case then make sure that there is adequate ventilation over the ballast resistor. The OC29 transistor should be bolted to the chassis using a mica washer and insulating bushes so that the case of the transistor is electrically isolated from the chassis but maintains good thermal contact. Doing this ensures that the output is floating i.e. neither rail is earthed so that the supply can be used with equipment needing either connection (i.e. positive or negative earth). The OC77 transistors are best used with cooling clips bolted directly to the

Note:—'A' and 'B' mounting plates are of Aluminium or Tin (16-18 s.w.g.) Do not let' the B' plates touch each other

-ve line

Plates

Plates

Anodes

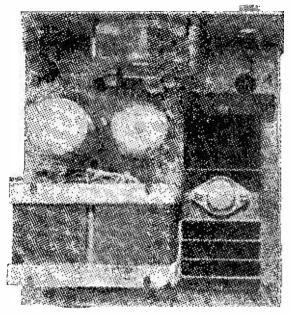
D5

D7

D7

D7

Fig. 2: Constructional details for the bridge rectifier.



Various views of the power supply unit.

chassis but this is not essential. The 90Ω ballast resistor should be soldered to two tag strips mounted above the chassis. The capacitors should be fixed using the normal clips making sure that the cases are isolated from the clips by the plastic case of the capacitors or by insulating tape. The polarity of these capacitors must be closely followed. The bridge rectifier is best assembled on three small pieces of metal as a heat sink (see Fig. 2), and mounted away from other components. The choice of mains input socket, output terminals etc., is up to the individual and will depend

continued overleaf

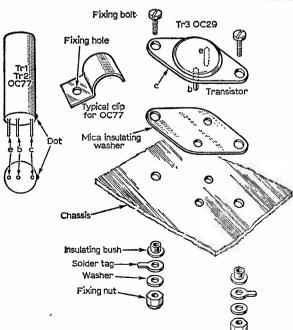


Fig. 3: Mounting data for the transistors.

on the case used etc. A neon to indicate when the supply is on would also be useful. It is important that all joints are properly soldered as a poor contact will decrease the stabilisation of the supply. Critical values are that of the 90Ω resistor and the transformer output voltage. If these are wrong the unit may not function or F2 may blow. If BYZ12 diodes are used then the 90Ω resistor may be replaced by a lower value and the max. output current is then higher i.e. $(33\Omega, 1.5A)$ fuse), but care must be taken not to over-dissipate the ballast resistor. Alternative transistors which can be used are OC76 or OC77X in place of OC77. OC28 or OC35 in place of OC29. It should be possible to use only one OC77 taking the emitter of Tr1 to the base of the OC29 directly but this has not been tried.

* components list

$\begin{array}{ll} \textbf{Resistors:} \\ \textbf{R1} & 90\Omega \ 30W \ (\textbf{Radiospares}) \\ \textbf{R2} & \textbf{1.5} \textbf{k} \Omega \end{array}$	VR1	10kΩ linear wirewound
Capacitors: C1, C2 1000μF 50V	СЗ	2000μF 50V
Semiconductors: Tr1 & 2 OC77 Tr3 OC29	D1 D4	
Miscellaneous: T1 Douglas MT104 or similar; F1 SW S.P. on/off; Meter 030V.	1A fuse	; F2 500mA;

A COMMUNICATIONS t.r.f. receiver—continued from page 398

using scraper board, while the case is a standard item but with its front panel re-sprayed. Almost any output transformer will suit for Til if phones only are envisaged. Incidentally, if phones and speaker are to be used together then the phones

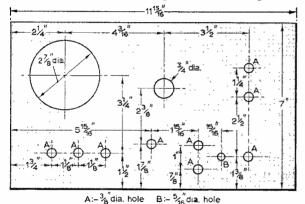


Fig. 6: Front panel drilling diagram.

must be high resistance, say, $2000-4000\Omega$. Using low resistance phones will result in a drastic reduction in volume from the speaker.

Panel Controls

These controls are fairly straightforward but, due to the very high sensitivity, the setting of the r.f. gain does affect the reaction control to some slight degree. However, the r.f. gain pot. is extremely useful on strong signals, particularly the Light Programme, Luxembourg, pop pirates, etc., as it prevents the detector from being overloaded.

The input circuit is designed to accept a low

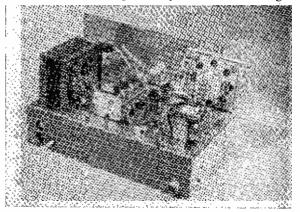
The input circuit is designed to accept a low impedance input but any length of wire plugged in will receive signals.

The prototype was fed from a 100ft. long wire via an aerial tuner unit. This method is strongly advised not merely for this receiver but for all those which cover the short waves. In this way it is possible to cover almost any sector of the short waves spectrum and still present a nicely matched 80 ohms to the input of the receiver. As will be appreciated, the impedance at the end of a random

length of wire will vary, its exact value depending upon the frequency in use. Since the receiver is designed to accept an 80Ω input, any value other than this will present a mismatch, and thus the efficiency of the unit will be impaired. A dipole cut to a particular band, will automatically present this 80Ω impedance but the dipole is essentially a one-band device. (A dipole cut for the 7Mc/s amateur band, will present around 90Ω 's on the 21Mc/s amateur band, which can be tolerated.)

The reduction drive of 10:1 is quite adequate on the lower and middle range. However on the 10-30Mc/s range, crowding of stations is noticeable and an even greater reduction is desirable. Constructors who like to experiment might consider putting a 3-gang variable capacitor of say 25pF per section in parallel with the main tuning capacitor. However if this idea is adopted due allowance should be made in the layout.

Set r.f. gain, a.f. gain and reaction to half way and tune in the signal. Adjust the r.f. control for max. signal, then turn up the reaction. The r.f. gain may now need a slight



adjustment. If greater volume is now required turn up the a.f. gain.

For reception of a.m. signals and B.C. stations the reaction should be advanced to the point just before it commences to oscillate. For c.w. reception it should be adjusted to just on the point of oscillation.

THE BROADCAST BANDS

by JOHN GUTTRIDGE

Albania: Radio Tirana (Rue Ismail Quemal, Tirana) now has an English transmission at 1500—1530 on 7,090.

Ascenion Island: BBC South Atlantic Relay (C.E.X.B., Bush House, London, W.C.2) has started transmissions with first of its four 250kw transmitters. It has been heard on 15,350 with the following scheduule: 1735—1830 World Service; 1830—1930 French; 1930—1945 Hausa; 1945—2245 close down World Service.

Clandestine: A further report on Radio Scari says this station's full title is La Voz de Resistenzia Basque. A new station reported is Radio Cassanova which has been heard with an Italian programme at 1800 in the 31 m.b.

Radio Portugal Libre has now been heard at 0700—0730 on 12,008.

Denmark: Radio Denmark (Radio House, Copenhagen V) introduced a brand-new schedule on September 4, the main feature of which is daily broadcasts to all transmission areas. English transmissions will be at 0145—0215 on 9,520 and 0745—0815, 1245—1315, 1445—1515 and 1915—1945 on 15,165. In addition, the Saturday test transmission at 1015—1100 on 9,520 will continue.

Egypt: Cairo Radio (U.A.R. Broadcasting and Television, P.O. Box 1186, Cairo) has English as follows: 0130—0300 9,580; 0130—0230 11,710; 1200—1430 17,690; 2045—2215 15,135; 1930—2015 17,690; 2145—2315 9,475/11,915.

Ethiopia: Radio Voice of the Gospel ETLF (P.O. Box 654, Addis Ababa) can be heard until 1455 with an Arabic programme 21,690. Severe interference is caused by a Hindi programme relayed by the Voice of America, Tangier, on the same frequency. The 1830—1945 Hausa and English transmission is now on 15,295.

Gabon: Radiodiffusion Television Gabonaise (P.B. 150, Libreville) can be heard at 2055 on 4,777 with news in French. Full verification is given.

Greece: An unidentified Greek station has been heard at various times between 1500—2015 on 6,915 through heavy interference.

Liberia: Voice of America Monrovia relay (Washington 25, D.C., U.S.A.) can be heard on with Urdu at 1500—1530 and a special Swahili, English and Arabic transmission at 1530—1600 on 21,670. The same outlet carries Arabic at 1830. The higher frequency bands have been good recently with very little interference.

Portugal: Radio Lisbon (Rua do Quelhas 2, Lisbon) broadcasts in English at 2015—2100 on 6,025 and a 41 m.b. outlet variously reported as 7,130 or 7,225. There is a new French transmission at 0615—0745 on 6,185/7,130. A new series of Portuguese by radio is to be broadcast shortly and those wishing to take part should send their names and addresses to the station by September 30. DX vocabularies and Portuguese and Spanish specimen report letters are available on application to the station.

Spain: La Voz de Andalucia (Cordoba) now has a shortwave outlet on 6,280, which is on the air from 0645—1000 and 1600—2200. Morning transmissions include language lessons.

Sweden: Radio Sweden (Box 955, Stockholm) is now reported to air its DX programme on Wednesdays instead of Tuesdays as previously.

Switzerland: S.B.C. (CH 3000, Bern 16) now uses 15,235 instead of 15,305 in its 1330—1500 English transmission. Other frequencies used remain 15,395/11,855/17,830.

U.S.S.R.: *R. Moscow* from September 1 transmits to Europe in English as follows: 0700—0730 11,830 / 9,710 / 9,480 / 5,980; 1200—1230 15,480 / 11,930 / 11,830 / 11,740 / 11,700; 1900—1930 9,590 / 7,340 / 7,280 / 6,050 / 5,980 / 1,320; 2000—2030 9,590 / 7,340 / 7,280 / 7,160 / 6,050 / 1,380; 2100—2200 9,750 / 7,280 / 7,260 / 6,050 / 1,490; 2200—2230 7,280 / 6,050 / 5,960 / 1,490 / 1,380 / 1,320.

Radio Yerevan (Armenian Radio, Mravian Street 5, Yerevan 25) has Armenian at 0900 and French at 0950—1000 on 11,830 / 11,790 / 11,745 / 9,800. Full QSL verification is given.

Radio Kiev (Ukrainske Radio, Radio Centre, ul Khreshchatik 24, Kiev, Ukrainian SSR) has English Monday, Thursday and Saturday at 1900—1930 on 7,210/11,730 and 2230—2300 on 1,241. Also on Tuesdays, Fridays and Sundays at 0030—0100 on 9,610/9,670/9,690/9,710/9,810 and 0430—0600 on 9,610/9,630/9,670/9,690.

Radio Vilnius: (Lietuvas TSR Radijas, ulkanarskio 49, Vilnius) has English on Sundays and Fridays at 2100 and 2230 over 665/6,200/7,180.

Help this month came from S. Ormerod, M. O. Donnelly, Des Walsh, J. F. French, D. Torbell, R. Patrick, I. Patterson, A. B. Thompson, G. Roberts, I. Perry, T. Davis, International Short Wave Club, "Swiss Shortwave Merry-Go-Round."

EGRETTABLY we kick off this month with a serious plea. Better logs! A large number of LUs.w.l.'s take the trouble to write and send in a log which is of very little value. Others omit important details which really are necessary and not just needed to satisfy a whim on the part of yours truly. As an example the following log was received yesterday. It reads—receiver HE-30—CN8AA, CR6AN, EA8EA, JA4BU, KZ5MC, OD5BU, PY1AGB, SVØWO, VO1AQ, VP6BW, W6JRY, YV5NSZ, ZS1MW, 4X4HI, JA1TK, 5N2FEL, 9J2DL. Name and address were supplied and that was it. The big question is now—what aerial, what band? On 10 metres this is very good, on 15 and 20 average to good, on the l.f. bands really excellent. This insistance on a good standard should, in the long run, help the s.w.l. since the cultivated habit of well kept and complete log keeping is a decided asset. Briefly then, please, date; time g.m.t.; r.s.t.; frequency; a.m./c.w./s.s.b.; and last but not least, alphabetical order does help a great deal. Of course, we need the receiver and aerial gen., too.

Vive la l.f.

Confess at once! Some of you have been having sneaky listen on the l.f. segments. **David Douglas** (Dundee), reports 1·8—F5DP, HB9T, OE5CD, SP9LP, XE2OK, 7·0—CE1ED, VS6FF. David offers to QRX for ZS stations on 160. How about a sked from some of you r.f. generating ZS gentlemen? I will pass on any sked news as and when I hear, and perhaps we can all QRX. "Very noisy but good if you can stick it." This is 40 according to **Chris Peel** (Stoke-on-Trent), S750, PR30, 20m dipole. He claims best times are late night and early mornings. Proof of this is CN8AW, EL2A, W1FZI/KP4, PY7APS, PY1CAD, UC2BF, UT5DZ, UB5UN, ZD8ARP, ZS1JA, all on 40 s.s.b.

Another 40-metre listener, Paul Baker (Pontypool), HE30, 45 ft. l.w. logged CN8AC, HK4ECM, KØWOO, OX3TI, PY1MEN, PY7LAK, W1PZB, W3JAL, W4TL, W6AP, plus 16 separate EU prefixes. No other logs down the l.f. end this month, but by now some might have read last month's "dare" and next month we might have more l.f. than h.f. reports. (Will the man who laughed please

leave the tent!)

20 and 15

The terrible twins 14 and 21, they never fail to produce the exotic stuff. J. Currie (Kirkintilloch), HA-230, 40 ft., end fed, 21Mc/s—CR6BC, CR7FM, PY1BOL, VE8BZ (Baffin Island, "expecting snow any minute"), WA4JWT, ZC4MO/P, 5A1TK, 5H3JL, 5X5JK, 9Q5DL, 9H1AM, all a.m.

If you have an Eddystone S750 with a PR30 pre-selector and a 20-metre dipole in the loft, you have the same set up as **Chris Peel** (see 40-metre log). Did you hear the same stations on 20 too? BV1USA, CE—1HU, 3CR, 3QB, CP1PE, CR5EB, CR6HF, CR7GF, CO8MN, CX9AAK, W6FHM/DU1, DU1FA, DU1AA, EL2AR, EP—2AX, 2TR, 2GF, 3AM, ET3AC, FO8AB (Tahiti), FY7AJ, HC1PB, HC8JG (Galapagos Is.), HC5NW, HK3KR, HP3MC, H17PB, HL—1CP—9CH (Korea), HR1SO, HZ1AB, JA—1CA, 1BZF, 1HER, 1BTR, 2AEV, 2ADH,

4BJO, 6DCE, 6MV, 7GY, 8AA, KA1KFH, KC6BO, KJ6AJ, KG6IG, KR6—DI, SR, BB, UL, LL, KS6BR, KX6BQ, KW6EB, KH6—BJ, ACC, BVS, EJM, UDR, CHU, OR, KL7—FIL, IFX, ESA, EBK, KV4EQ, KP4COS, KZ5PW, LA8FG/P (Jan Meyen Is.), LU—1DTL, 8BC, 8CZ, 8MIB, MP4BCC, OA—4PF, 6BL, OX3—AU, WX, GL, PY 1, 2, 3, 7, PZ1BW, PJ4AC, SU1DL (United Arab Republic), UA9—HA, CV, EU, VE—4TQ, 4IG, 5LY, 5RN, 6UM, 7AEZ, 8MA, VE8RCS (Ellesmere Is.), VK—1AL, 2PP, 2WB, 2ASP, 2AVA, 3AUP, 4FJ, 5FM, 5GG, 6XX, 6RL, 7CK, 7PW, 8KK, 9MK, VP2MW, VP3JR, VP5EC, VP6WR, VP7NS, VP8CW, VP9FK, VQ9HB, VS9AJC, VU2FN, W1, 2, 3, 4, 5, 6, 7, 8, 9, Ø, XE1YO, XW8AX, YA1AC, YS1JSM, ZF1GT (Grand Caymen), W9WNV/ZK1 (Don Miller on Manahiki Is.), ZL—1AUR, 2AFM, 5AA, ZP5KT, ZD8ES, ZD9BE (Tristan Da Cuhna), ZS 1, 2, 3, 3A2BF (Monaco), 5H3JR, 5N2AAE, 5U7AG (Niger), 5Z4FB, 601GB, 6Y5AR, 7Q7PS, 7X2CK, 9J2FF, 9L1AX, 9M4VP, 9V1MT, 9U5BB (Burundi), 9Y4VP. All s.s.b. and in alphabetical order, too.

John Farrer (Bishop's Stortford), Mini-clipper plus 2 transistor amp. and 20m. dipole heard on. 20 BV1USA, CN8BB, CR6HG, CT1PE, CX1YR, EL2AT, EP2AX, ET3MEN, HB9DL, HK3RQ, HM2BD, HP1JC, HR1RP, HS1HC, JA2CTC, JA6CZD, JA8CKC, KA2HQ, K6DJZ, KB6CZ, KG4AN, KL7DRZ, KP4AXC, KR6CL, MP4BDP, OD5BZ, OY2BE, PR1AQ, VE2BUJ/SU, VE7BV, VP2LS, VQ9DC, VS9AJC, WA6FPB, XE3JG, XW8AZ, YN1CML, YV1LA, YS1AD, ZD8JK, ZP5OG, 4X4BC, 5A1TM, 5N2AAW, 7Q7BN, 9H1AB, 9J2JC, 9K2AF, 9M2CP, 9Q5CZ, 9V1MX, 9X5CE. On 15 metres Paul Baker (see 40-metre log), netted CE3IY, CP5ET, CR4BC, CR5SP (Sao Thome), CR6—AR, JT, LA, CR7GJ, CT2AG, CT3AM, CX5AAM, EA6BG, EP2—AX, RJ, ET3USA, JA9AVK, KP4CRT, MP4BBA, OA4OS, OD5—CS, ET, ST2SA, SVØWU, VE8BZ, VO1EX, VP2AZ, W10RD/MM, XE1DW, ZB2AS, ZC4—KF, MO, ZS1BV, 4X4VB, 5A1TK, 5H3JL, 5X5JK, 9G1FL, 9Q5—QR, QV, RW, 9U5KU.

On ten metres C. Clarke (Farnham), 12 v. s/het, ground plane, logged DL2BU, G—3PQF, 3OUF, 8MY, GB3LER (Beacon in the Shetland Is.), GI3OZW, I1CGV, OE3GSA, OH2TI, OZ3Y, SM5DTK, SMØCQR, UP2ADZ, UQ2KKD, 5N2AAF, 9J2DT. John Farrer (see 20-metre log) managed to hear DL2CM, G3NMH, I1HC, LA3II, OH2TI, OZ1VR, OZ8PK, SM4AIQ, SM7XV, ZD8RB, 7Q7RM, 9J2DT. Chris Peel (see 20-metre log) logged only the a.m. signals which came in—CE3RC, CR6AT, EA8AE, EL2AK, KP4BJM, PY1AGP, PY7AC, SVØWF, ZE2KL, ZS1BK, 5N2AAM, 5H3JR, 7Q7RN, 9J2WR, 9J2DT, 9Q5BH.

News and Contests

Known to be lurking top band CX3BH (Uruguay). Contests for September include 10th—11th WAE (C.W.) contest. 11th—VHF—NFD. 18th—D/F National Final. Don't forget the RSGB mobile rally at Woburn Abbey, Beds., on September 11th. Your scribe will be loitering at this one, personal audio QSO's welcomed. Deadline for this month is September 25th.

INIATURE transistorised tape recorders are nowadays offered in a wide variety of models, the simpler of which make no attempt to maintain constant motor speed, or even constant tape speed irrespective of the position on a reel. Indeed, the motor speed is often manually variable on such machines, which means that recordings made on one instrument cannot in general be played back on a different one or even on the same one if the speed has in the meantime changed. Reasonable speech and dictation performance may be achieved even under such conditions, but musical recordings are not possible.

Without even making any claims towards true high fidelity, a tape recorder with constant tape speed is essential for all serious musical recordings and preferably for good speech recordings too. This means that a tape drive capstan must be driven from a constant-speed motor, and not the tape take-up reel. Even if the motor runs at constant speed on a take-up reel drive, the tape speed will vary with the diameter to which tape is wound on to the reel at any time. The recording will then run at incorrect pitch if the tape is at any subsequent time spooled on to a reel of different diameter.

It is the aim of this article to discuss and explain



SPEED STABILISATION for BATTERY MOTORS

what manufacturers and designers have consequently undertaken in the meantime to improve low-power battery motors. The situation has now changed and motors are available with a reliability at least equal to that of other parts of the tape recorders or record players, so that at any rate these instruments incorporating the new Bühler RF-Stabilised Motor, and many using simpler switch-transistor stabilised systems are to be recommended.

STABILISER SYSTEMS

It is obviously a prime requirement for any automatic speed control arrangement to provide some means of deriving an electrical signal as indication of the actual motor speed at any time. Furthermore, this "actual speed" signal must be compared with a reference standard and the discrepancy, i.e. error, detected by the circuit must be used to correct the motor speed, preferably after amplification of the error signal, so that the locking action is very rigid.

This is the skeleton principle of any automatic regulator system, including non-electrical systems in purely mechanical or hydraulic machinery. The other electrical example probably familiar to the reader, the electronically stabilised h.t. supply is thus of exactly the same construction. A portion of the actual h.t. output voltage at any moment is applied to the grid of an amplifier valve, to whose cathode is tied a fixed reference voltage from a neon tube. The detected error voltage thus appears between the grid and cathode of the valve, is amplified by it, and thereafter regulates the principal series control valve(s) to correct the h.t. output voltage.

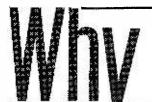
BY M.L. MICHAELIS, M.A.

OBTAINING A SPEED SIGNAL

Now there are, in principle, several possible methods of deriving an electrical signal as a measure or indication of the actual speed of a motor. A tiny alternator (a.c. generator) can be coupled to the shaft, when the output frequency thereof is a measure of the motor speed. Such an arrangement requires an external frequency meter (ratemeter) circuit, a reference oscillator of known and constant frequency and an error detection discriminator, quite apart from the amplifier and actual regulator circuit then operated off the finally derived speed error signal. Such a circuit would be rather complicated so we must look for simpler, more elegant solutions. If the motor shaft carries a small rotating radial obstruction at one end and this interrupts a beam of light impinging on a photocell or other photoelectric device, once every revolution of the motor shaft, the output waveform of the photocell will contain a pulse component whose repetition frequency is equal to the actual speed of the motor at all times.

REFERENCE OSCILLATOR

All that this arrangement brings in the way of improvement over the slaved alternator is that no sliprings are required to take the speed signal from the rotating part of the motor to the stationary part of the circuit. Sliprings and brushes are a constant source of trouble, so any way of avoiding them is certainly an advantage. But they could in fact be obviated even in a tacho-alternator if the coil is made the stator and a small permanent magnet is rotated on the motor shaft within this coil. There is



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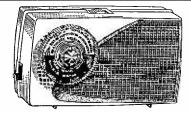
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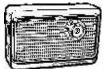
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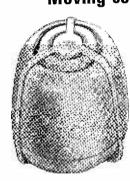
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thus hardly any point in going to the extra trouble of employing photocells and light beams. In any case all such systems, whether employing tachoalternator or photoelectric pick-up, require the external reference frequency oscillator, ratemeter discriminator and error amplifier/regulator circuit. Such designs are not simple and the stabilisation factor can never be any better than the inherent stability of the reference oscillator of such a circuit, which is generally insufficient in the face of the large range of battery voltages encountered.

It is as well to consider what degree of stability is actually required for good musical tape recordings. Taking the most sensitive region of the response curve of the human ear, say 1kc/s, a change of motor speed such that the originally recorded 1kc/s note shifts by about $\pm 50c/s$ will move the whole recording one whole musical key either way. Any residual changes for the average music lover should be less than a fifth of this and even better for the specialist. A motor speed stability of better than ±1% is therefore definitely essential for even reasonably good musical recordings or record disc reproduction. A reference oscillator in a frequency discriminating stabiliser circuit should thus be stable to better than 0.25% to allow a margin for other influences without exceeding the total permissible limit.

A free-running oscillator can be made to achieve this order of frequency stability only at the price of some considerable compensatory measures and circuit complications. A short-term stability of this order during any one period of operation is very much easier to achieve than a long-term stability of this order between various times of operation in winter or summer, indoors or outdoors, with new and exhausted batteries in any of these instances.

OPTIMUM REQUIREMENTS

The optimum system of deriving a speed indication signal from the motor shaft should be such as to transmit that signal to the external stationary circuit without any need for sliprings and brushes subject to rapid wear. In other words, some system of radiation or induction into a stationary pick-up element is called for. There is no objection at all to the use of commutator segments or sliprings and brushes to take the main motor running current to the armature, since any effects of wear on these components are then corrected by the speed stabiliser

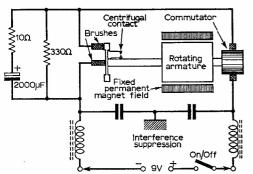


Fig. 1: The earliest method of stabilising the speed of a battery motor, using a centrifugal contact to break the main current through the motor when the desired speed has been reached.

loop, which does not include them and thus is not influenced in its accuracy by them. Any sliprings and brushes within the speed stabiliser loop will affect the speed indicator signal to a greater or lesser extent and will thus affect the accuracy of the entire stabilisation. It is found that changes of contact resistance of any sliprings and brushes within a speed regulator circuit are the chief detrimental factors and these resistance fluctuations affect the speed signal the more the greater the current flowing in the circuit needs to be. The input of the regulator electronics should therefore be of very high impedance especially in simpler systems which do need to use sliprings after all.

The circuit should also be able to operate without any form of external reference standard. This requirement was satisfied as soon as it had been realised that there is in fact no need at all to transmit a continuous signal of actual motor speed at all times. It is quite sufficient for all but the most exacting professional purposes if the motor can be made to transmit a simple binary signal, i.e. merely either one of two possible states, "too slow" or "too fast". This is provided in the simplest practical manner imaginable by a centrifugal contact.

CENTRIFUGAL CONTACTS

A centrifugal contact is simply a spring-loaded contact very similar to the type found on conventional relays but mounted on and rotating with the motor shaft in such a manner that at the desired speed of rotation the outward centrifugal force just balances in inward spring pressure and the contact consequently then open. The closed centrifugal contact thus signifies "motor running too slow' and the opened centrifugal contact "motor running too fast". The speed at which the contact opens, which is the speed at which the electronics then stabilises the motor can be set over a wide range with a small grubscrew bearing down upon the contract spring. This is normally preset to the correct value for a particular motor at the factory and then sealed, but adjustments on the part of the service engineer are certainly possible when necessary.

The "reference" in this system is the effective stiffness of the contact spring and its physical geometry. The accuracy of the entire stabiliser system is as good as the constancy of these mechanical parameters of the centrifugal contact provided that the regulator circuit is designed (a) in such a manner that contact

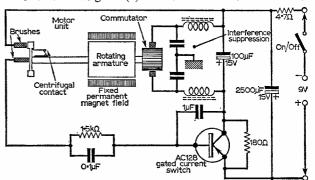


Fig. 2: An improved method with a centrifugal contact. The loading on the contact is reduced, by using it only to gate a switch transistor which in turn interrupts the main motor current.

wear in the electrical sense is minimised and (b) any such wear and resulting fluctuations of electrical resistance are unable to affect the circuit to any significant extent. Virtually all modern speed stabilised motors in battery operated equipment, at least in the domestic range, now employ centrifugal contacts as speed indicators. The external electrical circuits all involve some means of choking back the full motor drive current when the centrifugal contact opens and restoring the full motor current as soon as the motor has slowed down again sufficiently to close the contact. The better the particular circuit the lower the electrical loading imposed upon the centrifugal contact.

DIRECT SWITCHING

Fig. 1 depicts the simplest form of speed stabiliser circuit with a centrifugal contact which, however, meets none of the requirements already discussed for achieving good reliability. The centrifugal contact switches the full motor current directly and is thus heavily loaded and it is necessarily connected by sliprings and brushes under these conditions. The earliest speed-regulated tape recorders and record players nearly all employed this circuit, which turned out to be notoriously unreliable and led to the bad reputation of such equipment mentioned earlier in this article. The very cheapest recorders without any form of stabiliser, which merely employed a manually variable resistor in series with the motor, gave superior reliability.

In the arrangement of Fig. 1 the centrifugal contact rapidly burns up, in some cases after only 20 to 50 running hours of a new motor. Resulting changes of contact and slipring resistance reflects greatly as speed fluctuations, in some cases to a greater extent than the fluctuations encountered in simple unstabilised motors. The arrangement of Fig. 1 was thus largely a commercial failure as it stands, although many machines were marketed using it.

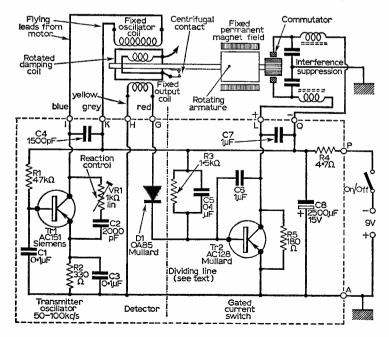
The chief root of the trouble was the heavy and continuous arcing at the centrifugal contact because

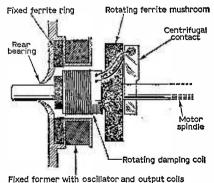
this contact hovers close to the make/break state, never getting really far away from it. The 10Ω resistor and 2,000 µF capacitor shown in Fig. 1 were added to make the action more sluggish in an attempt to reduce this "hover arcing". When the contact opens, the charge stored in the capacitor keeps the motor running at the higher speed for a moment to allow the contact to open fully before speed falls and it closes again, whereupon it remains closed properly for a moment until the capacitor has recharged and the motor can gather speed again. This innovation was not really successful either because any increase of the time-constant of the resistor/capacitor combination sufficient to kill the arcing led to an intolerably high level of motor hunting, i.e. wow and flutter in the recorder or record player. Moreover such measures are in direct contradiction to the purpose of the drive capstan flywheel of a tape recorder (or the turntable mass of a record player). It is not the charge stored in the capacitor of Fig. 1 that is the decisive factor, but rather the time-constant of the motor speed variation, which is largely dictated by the flywheel, i.e. the mechanical inertia of the system. This leads to a vicious circle in trying to reach any satisfactory compromise along these lines. A much better approach is to reduce the current loading of the centrifugal contact, which will reduce arcing without any contradictory side effects.

SWITCH-TRANSISTOR CONTROL

The better machines of past years thus resorted to the circuit arrangement shown in Fig. 2 where the centrifugal contact is used merely to switch the base bias of a gating transistor which in turn controls the full motor drive current. Loading and wear of the centrifugal contact were therefore much reduced and any fluctuations of contact or slipring resistance in this circuit of much higher impedance led to far smaller speed fluctuations. Such circuits were reasonably successful and found widespread application.

If any reader possesses a tape recorder or record player with the arrangement of Fig. 1 he is well

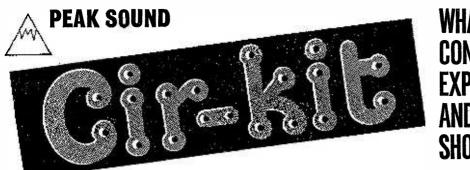




Pixed for their with oscillator and output cons

Fig. 3a (left): The final design used by the author utilising a centrifugal contact. Note the centrifugal contact (or switch) is connected to the rotating damping coil.

Fig. 3b (above): Construction of the Bühler motor.



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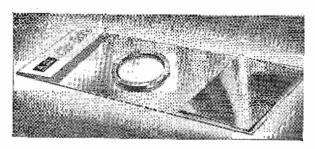
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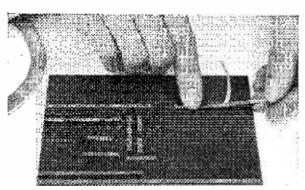
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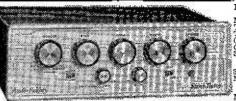
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advised to convert this to that of Fig. 2. This is very straightforward, layout is non-critical and the AC128 (or equivalent) switching transistor and its few associated components can be tucked into any available free corner of the equipment. Before replacing a seriously fluctuating motor in a recorder using the arrangement of Fig. 1, try conversion to Fig. 2. This is simpler and cheaper than a motor replacement in many cases and very often leads to good performance for a long spell of continued operation with a centrifugal contact already too burnt to operate correctly in the circuit of Fig. 1. If a motor is so far damaged in Fig. 1 as to need definite replacement on all accounts, simultaneous conversion to Fig. 2 (which is always possible) is strongly recommended or even replacement with the new Bühler r.f.-stabilised motor (if mechanically practicable in the particular instrument).

If a centrifugal contact has already been burnt so badly in Fig. 1 that performance in Fig. 2 is still not quite as desired, it is possible to add a second transistor as emitter-follower in order to reduce contact loading still more. Any small a.f. type with a current gain of 20 to 30 in the grounded emitter circuit is satisfactory. The R-C combination of $1.5 \text{k}\Omega$ and $0.1 \mu\text{F}$ from the centrifugal contact shown in Fig. 2 must then go to the base of this second transistor. whose emitter is taken to the base of the AC128. The collector of the additional transistor is taken to the negative end of the 2.500 µF electrolytic shown in Fig. 2. No other changes are necessary. If even this two-stage cascade circuit fails to operate stably then the motor is definitely too far gone and needs replacement. The two-stage circuit, although actually adopted by a few commercial recorders, is hardly necessary with the new replacement motor, with which the single-stage circuit of Fig. 2 is normally quite adequate.

Even the circuit of Fig. 2 proved to be much more prone to trouble than the motor itself, i.e. the life of the centrifugal contact system was nearly always much shorter than that of the motor bearings, commutator and armature.

CONTACT BURN-UP

Troubles were still merely ones of gradual burn-up of the contact and wear on the sliprings. Even the slightest interrupted current—as little as a few microamps-suffices to burn up the contact gradually to the extent of forming a minute surface film of oxidation. It was thereupon realised that an ultimately reliable motor (in the sense that the service life of the centrifugal contact system is at least as great as that of the motor itself) is possible only if the centrifugal contact never interrupts any current whatsoever, i.e. if no voltage at all is ever present across it at the moment it opens (conditions at the moment of closing are unimportant since there can then be no significant arcing). Also complete obviation of any sliprings is essential, i.e. a radiative or inductive method of transfer for the signal is highly desirable.

These conditions led to the ingenious and surprisingly simple solution adopted in the highly successful Bühler r.f.-stabilised motor whose full operating circuit is shown in Fig. 3a. These motors, developed by Messrs. Bühler Motors, of Nuremberg, West Germany, are now used in the better quality portable tape recorders of Messrs. Grundig and all

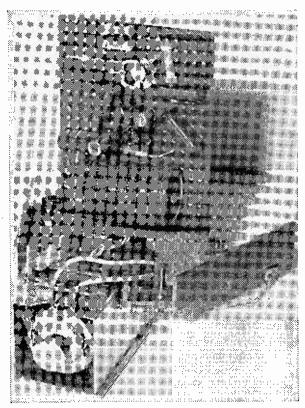


Fig. 4: Demonstration unit using the circuit of Fig. 3a. The motor supplied stabilises at 3,000 r.p.m. within the limits shown in Fig. 5.

other leading manufacturers. They have proved highly successful and are apparently free at last from all the shortcomings of previous arrangements. Fig. 5 shows some performance data of this novel motor which is seen to be really excellent. The useful life of all parts of this motor is very long, the motor runs exceptionally quietly and smoothly and the power conversion efficiency is so good that rugged mechanisms can be driven without uneconomical battery consumption.

THE BÜHLER MOTOR

The front end, i.e. drive mechanism, of the motor is conventional, using an ordinary d.c. arrangement of wound armature and commutator with a permanent magnet field as heretofore. All battery motors for this type of equipment should use permanent magnet fields to save expensive battery power otherwise uselessly wasted in energising a solenoid field.

The rear end of the motor shaft carries the same type of centrifugal switch as previously but this is now connected across a rotating coil of many turns of fine wire wound on a ferrite mushroom rigidly attached to the motor shaft and rotating with it Fig. 3a. There are no external connections to this system, which rotates within a fixed bobbin near the rear bearing of the motor shaft, carrying a stationary oscillator and pick-up sensing winding as well as a stationary ferrite ring around the bearing to complete the magnetic path. The larger winding of the stationary coil is connected as oscillator coil in a conventional transistor oscillator circuit around Tra

in Fig. 3a. The pick-up sensing coil of fewer turns is connected to a detector diode D1 which develops a positive rectified output at its cathode (applied to the base of Tr2) whenever the oscillator is actually oscillating and no output when it is muted.

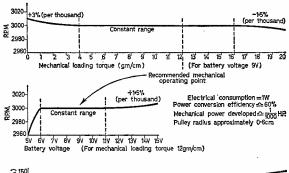
As long as the motor is still running too slow the large rotating coil is shorted out by the centrifugal contact. Provided that the reaction control is set correctly (VR1) the oscillator is therewith damped so heavily that it is unable to oscillate at all. The base of Tr2 receives sufficient bias via R3 under these conditions to fully open the emitter collector path of Tr2 and allow the motor to draw full current and gather speed. As soon as it reaches the correct speed the centrifugal contact opens. Since the oscillator is still dead at this moment the contact breaks neither voltage nor current, so that there is no spark whatsoever developed and electrical wear is nil. But the damping of the oscillator is therewith removed and it bursts into oscillation at once. The oscillation picked up by the sensing coil is immediately rectified by D1 to give a positive backing bias cutting Tr2 off at its base. The motor current is therefore reduced to a low value magnitude. When the motor has lost sufficient speed again for the centrifugal contact to close, the oscillator ceases to oscillate abruptly (if not, reaction applied via VR1 is excessive and must be reduced accordingly.

The cut-off bias developed by D1 vanishes, Tr2 can open again and restore full motor current so that the motor can gather speed again. It is necessary to give slight additional delay above that imposed on the motor speed response by the mechanical inertia (flywheel or turntable mass) so that centrifugal contact can fully open and fully close on each action cycle without fluttering in order to provide clear-cut keying of the oscillator Tr1, leading to a positive action. This is achieved largely with C6, which multiplies itself by the familiar Miller effect as a virtual capacitor β times as large between the base of Tr2 and chassis, where β is the current gain of Tr2. This virtual large capacitor acts as time-delay reservoir for the control bias developed by D1.

ADJUSTMENTS

If the motor is heard to "sing", i.e. to run up to an excessively high speed, and an oscilloscope connected to the anode of D1 (use a probe) reveals no oscillation, check the transistor connections and all other wiring. If this leads to no cure, the current gain of Tr1 may be too low. Select a transistor with a higher current gain after first trying an increase of C2 and reduction of C3 (say 50% or even 100% in each case). Check that the coils blue/grey and yellow/red have not been confused, although individual coils may be connected any way round.

Once oscillation is evident at the anode of D1 stop the motor pulley with the fingers and adjust reaction with VR1 such that residual oscillation just vanishes. Then release the motor pulley and allow the motor to run up to full speed until the centrifugal contact intermittently opens and observe the 100% arbitrary interval square wave amplitude modulation of the oscillation on the slowest timebase speed available on the oscilloscope. Observe that the oscillation is absent only for very brief intervals, and present most of the time, when the motor is running light off load. Then apply increasing friction with



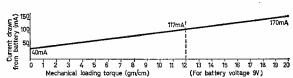


Fig. 5: The performance characteristics of the Bühler r.f. stabilised motor in the circuit of Fig. 3a.

a finger held against the rim of the pulley and note that the oscillation gaps progressively increase until finally only very brief bursts of oscillation remain and very long intervals. If these brief bursts are of lower amplitude than the longer ones, or of variable amplitude reaction is insufficient. If the modulation is not 100%, i.e. if the oscillator commutates between a low and a high level without ever muting completely, reaction is excessive.

Once the oscillator gating is correct in the manner described make a recording of a fixed sinewave of, say, 1 kc/s from an a.f. signal generator with the motor driving the tape desk mechanism in the machine with which it is to be used (or play a standard frequency record if a record player is involved). Study the effect of changes of value of C6 and R5 upon wow and flutter in the output aurally or, if available, with special test equipment. As an intermediate between these extremes jitter of the playback display may be observed empirically on a weakly synchronised oscilloscope (sync control near minimum). Make sure that C6 is definitely smaller and R5 definitely greater than those values for which serious wow and flutter commences.

The oscillator frequency should lie between 50kc/s and 100kc/s. If strange interferences or distortion in conjunction with inversion beating with higher audio frequencies in the a.f. signal being recorded or replayed with the instrument are observed, shift the oscillator frequency to a higher value than that prevailing by reducing C4 until such interference disappears. Before undertaking such measures carry out some experiments to determine the best position for the Veroboard. If necessary interpose an aluminium screen or surround the Veroboard completely with a metal can grounded to the main chassis.

Further possibilities of beat frequency interference can arise in a tape recorder if the difference between the bias and erase oscillator frequency on the one hand and the motor control on the other hand lies within the audio passband of the machine. Good mutual screening may already effect a cure and, if not, suitable increase of motor control oscillator frequency (reduce C4) will again remove the trouble.

5-WATT AMPLIFIER

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THIS amplifier has no transformers and gives an output of up to approximately 5 watts into a 3 ohm loudspeaker. The amplifier is sufficiently versatile to be able to feed into almost any speaker impedance, without the use of a matching transformer, but with the higher impedance speakers, the maximum available output is less. The amplifier built by the author measures $3\frac{1}{2} \times 2\frac{1}{4} \times 2\frac{1}{4}$ in, but these dimensions could be reduced with little difficulty, if required. Total building costs should be less than £3.

Although the unit is designed to work from a 12V supply. it will work perfectly well within the range of 9 to 18V without need for any component value changes.

Circuit Description

A circuit diagram of this five transistor unit is shown below in Fig.1. Tr1 is wired as a conventional common emitter amplifier, with collector load R4. The input signal is connected to Tr1 base via C1, and R1-R2 are the base-bias resistors. The collector circuit of Tr1 is directly coupled to the bases of Tr2 and Tr3. Tr2 can also be regarded as a conventional emitter follower, operating from approximately half supply potential, the lower end of R6 will therefore be approximately 6V negative. Being an emitter follower it gives a high input and low output impedance, and gives unity voltage gain with zero

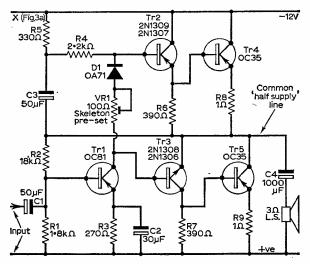
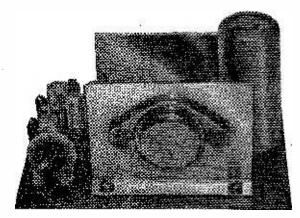


Fig. 1: Circuit diagram of the amplifier.



phase shift between input and output.

Tr3 is wired as an n.p.n. common emitter amplifier with 100% (voltage) negative feedback; in this case the circuit gives a high input and low output impedance.

The circuit again gives unity voltage gain, but in this case 180° phase shift occurs between the base and output collector. Thus, when a common input signal is applied to the bases of Tr2 and Tr3, the output signals at Tr2 emitter and Tr3 collector are of similar form but are of opposing phase.

Both of these transistors operate at approximately half supply potential, and the input signal from Tr1 collector operates at the same mean level, so that, when negative going inputs are applied, Tr2 conducts and Tr3 is cut off, and vice versa.

conducts and Tr3 is cut off, and vice versa.

The signal at the emitter of Tr2 is directly coupled to the base of Tr4, an emitter follower, so that the signal at Tr4 emitter, and thus at the common "half supply" line, follows the signal at Tr1 collector.

The signal at the collector of Tr3 which is in antiphase to that at Tr1 collector, is directly coupled to the base of Tr5; being connected as a common emitter amplifier, with 100% (voltage) negative feedback, giving unity voltage gain between base and collector but 180° phase change, so that Tr5 collector, and the common "half supply" line, again follows the signal at Tr1 collector.

When negative going signals are available at Tr1 collector, Tr2 and Tr4 conduct and Tr3 and Tr5 are cut off. When positive going signals appear at Tr1 collector, Tr2 and Tr4 are cut off and Tr3 and Tr5 conduct. The common "half supply" line follows the signal at Tr1 collector, but at a very low impedance level signals fed to the external speaker via C4. Thus, the circuit acts as a single ended Class-B push-pull amplifier.

To minimise cross-over distortion in the amplifier, a small bias voltage is applied between the bases of Tr2 and Tr3. This bias voltage should be compensated against changes in temperature and diode D1 and variable resistor RV1, in the collector line of Tr1, are used for this purpose. Ideally, a special compensating diode should be used, but since are quite expensive, a semiconductor diode OC70 and variable resistor have been used instead to give results that, although not perfect, are quite acceptable.

Resistors R8 and R9 give a degree of stabilisation to the two power transistors, Tr4 and Tr5.

It is important to the operation of the circuit

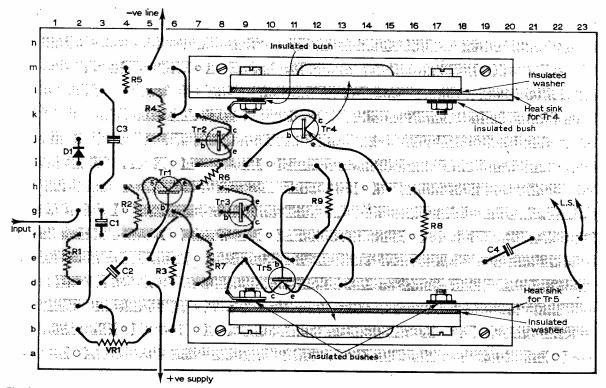


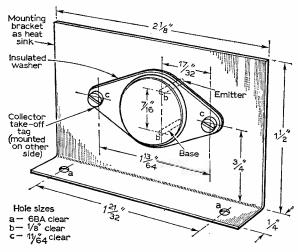
Fig. 2: Constructional details. Above is a component layout and wiring diagram of the Veroboard panel. The illustration below gives drilling and mounting details for the heat sinks.

that the common "half supply" line be kept at approximately half the supply line voltage, and with this in mind the circuit is d.c. stabilised by feeding the Tr1 base-bias resistor, R2, from the common line.

To obtain the maximum possible voltage gain from Tr1, the collector load should be as large as possible, but unfortunately the d.c. requirements limit the value of the load to about $2.5 \mathrm{k}\Omega$. Fortunately, it is possible to increase the *effective* value of the collector load without increasing the *actual* value. This is achieved by inserting R5 between the negative supply line and the main collector load, R4, and feeding the full a.c. signal from the common "half supply" line to the R4-R5 junction via C3. Thus, when a signal appears at Tr1 collector, almost identical signals appear at *both* ends of R4, and therefore only a small signal flows in this resistor, which thus appears to the a.c. signal to be of a far greater resistance than it really is. This technique is known as "bootstrapping" and has many applications.

Construction

The unit is built up on a single piece of Veroboard measuring $3\frac{1}{2} \times 2\frac{1}{4}$ in. with 0·15in. hole spacing. Start construction by cutting out two heat sinks from 18 s.w.g. aluminium sheet for the power transistors, Tr4 and Tr5. Bend and drill the sinks as shown in Fig. 2a. When the heat sinks are completed, bolt the two power transistors in place, using insulated washers and spacers which should be supplied with the transistors. A small solder tag should be secured behind one of the nuts that is used to



hold the transistor in place, this solder tag being insulated from the heat sink, but in electrical contact with the body of the transistor to give a collector take-off point. Cut the Veroboard panel to size shown in Fig. 2, and break the copper strips where indicated. Eight small holes should now be drilled in the panel; four of which will be used for securing the heat sinks. The others are for mounting the completed amplifier.

Turn the panel over and start fitting the components and wiring up as shown in Fig. 2. If space is at a premium it is best to mount all the components vertically. Before attempting to fit VR1 in place, the diameter of its mounting legs should be filed so that they fit easily into the holes

in the Veroboard panel.

When complete, the wiring should be double checked, and if satisfactory, the unit can then be checked as follows: with no external speaker connected, connect a 12V supply to the unit, taking care to monitor the current taken from the supply, and adjust VR1 to give a reading of 8 to 15mA. This reading should remain steady over a test period of a few minutes. Now connect an external speaker. There should be no appreciable increase in the mean current, apart from a small "flick" that may occur at the instant that the connection is made.

If these tests are satisfactory, an input can be connected to the unit and a functional check carried out. The amplifier should be run at fairly high volume; the current will fluctuate considerably with volume level, but should fall back to the 8—15mA level whenever the input signal falls to zero. The final value of the zero signal current should be adjusted to give minimum cross-over distortion, but should be within the limits set above.

The unit is now complete and ready for use.

Adding a Pre-Amp

The sensitivity of the unit should be adequate for most purposes at it but, should stands, extra sensitivity be required, the pre-amplifier shown in Fig. 3 may be used. that the polarity of C1, shown in Fig.1, should be reversed if the preamplifier is to be used. C7 and R14 act as a decoupling network between the main amplifier and the pre-amplifier, and prevent instability.

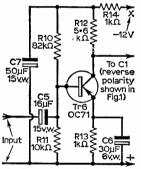


Fig. 3: Pre-amplifier designed to work with main amplifier.

onity.

If required, this pre-amplifier can be built into

★ components list

Resi	stors:		
R1	1·8kΩ	R6	390Ω
R2	18kΩ	R7	390Ω
R3	270Ω	R8	1Ω 3W 5%
R4	2·2kΩ	R9	1Ω 3W 5%
R5	330Ω		
All re	sistors 10% ½W unless	otherv	vise stated.
Capa	citors:		
	50μF 15V	C 3	50μF 15V
C2		C4	1000μF 15V
Semiconductors:			
Tr1	OC81	Tr4	OC35
Tr2	2N1309, 2N1307	Tr5	OC35
	2N1308, 2N1306	D1	OA71
Misc	ellaneous:		
Insul	ated mica washer a	ind sp	pacers for OC35's.
3Ω loudspeaker, Veroboard 3½ x 2¼ in., 18 s.w.g.			
aluminium sheet for heat sinks, wire, sleeving, etc.			

the main amplifier by slightly increasing the size of the basic Veroboard panel.

Power Supply

A suitable mains power supply unit (12V output) for use with the amplifier, is shown in Fig. 4. The 2.5A fuse is fitted to protect the power unit should a fault occur.

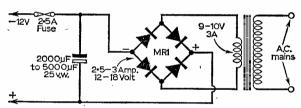


Fig. 4: A power supply suitable to drive the main amplifier and the pre-amp.

If alternative power supply voltages are to be used with the amplifier, VR1 should be adjusted to give the no signal currents already stipulated.

EXPERIMENTERS' CORNER

in small quantities to the bath.

-continued from page 425

Fehling's-Formaldehyde Copper Bath.
Rochelle Salt (Sodium Potassium Tartrate)
..225 gms./litre.
Sodium Hydroxide (DANGER-CAUSTIC!)

Copper Nitrate, Cu(NO₅)₂, 3H₂O 125 gms./litre. This solution is made up, filtered, and added to an equal volume of 37% formaldehyde solution just before use. It deposits at about the same rate as the nickel solution and is fairly stable, as copper baths go, over a period of several hours. It can be replenished by adding the first mixture

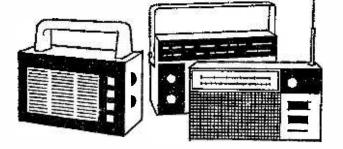
Finally the most important part of the process is the initial catalysing operation. The board must be cleaned and degreased, and washed well with water, finishing up with demineralised water. One popular catalyst is Gold Chloride, 0·1% AuCl₃ by weight. As this is not a solution to throw around in experiments, a less reliable alternative is;

Stannous Chloride SnCl₂

5 oms

These solutions are made up with thickening agents as inks, one useful thickener is "Polycell", and you can always paper the room after plating your circuits! Easier still, if you can get hold of finely powdered metals, is to make up thick "inks" of the appropriate metal, stirring well before use. The metal powder should be of 200 mesh or finer.

Important: Hands should be washed immediately after handling any chemicals. All liquids, particularly those containing caustic, should be poured gently to avoid splashing. A bowl of clean water should be to hand. If any chemical splashes into the eyes, plunge the head immediately into the water and blink rapidly.



IMPROVING F

ANY of the smaller transistor radios are designed and built down to a price. They contain the minimum number of components assembled around the simplest basic circuit. Results can be quite satisfactory but it is possible in many cases to improve on the original design. Modifications can range from simple improvements to a.g.c. circuits, to methods of battery economy and adding r.f. and a.f. stages.

Before making any alterations, it is advisable to study the circuit and familiarise oneself with the physical layout. A typical circuit for a six transistor superhet is shown in Fig. 1. The components in this type of receiver are often assembled on both sides

of a printed panel.

Difficulty may be experienced in locating the connections to individual parts. Holding the panel before a bright light can help to outline the wiring. If this method fails, one can mark the component terminal wires with coloured spots of paint. Quick drying aero-model dope in a wide range of bright colours is available from model shops in ninepenny tins.

Begin by identifying the output transistor terminal solder blobs on the underside of the printed panel. Using a pointed match stick drop a spot of red paint on each collector blob, yellow on each base terminal and blue on each emitter. Repeat this colour code on the remaining transistors. Locate the i.f. transformers and enclose the terminals in squares of white dope. Repeat this code on the driver and out-

put transformer, where fitted, using green dope. This speeds up the actual time spent on modifications and helps later when service may be required.

★ IMPROVING A.G.C.

In the circuit shown in Fig. 1 a.g.c. is fed back from the top of the volume control through an $8.2k\Omega$ resistor to the secondary winding of i.f.t. 1 as a control voltage for the base of the following i.f. transistor. This provides for normal signal variations such as night fading but is insufficient to deal with strong transmissions. Additional control can be added as in Fig. 3. To incorporate this modification the primary winding of i.f.t. 2 is disconnected from the negative h.t. line. Cutting the metal on the printed panel may be necessary in order to isolate the relevant i.f.t. terminal. Having isolated the transformer, add a $1.8k\Omega$ resistor between the former earth terminal and the negative line and by-pass the resistor with an $8\mu F$ capacitor to the positive line. Next connect an 820Ω resistor in series with an OA91 diode from the same terminal on i.f.t. 2 to the oscillator tapping on i.f.t. 1. Note the diode polarity.

In operation bias across the $1.8k\Omega$ resistor keeps the diode from conducting until a strong signal is tuned in. On strong signals, the diode conducts and feeds back part of the signal to reduce the gain of the second i.f. transistor. The effect is best appreciated when the set is used travelling in a car.

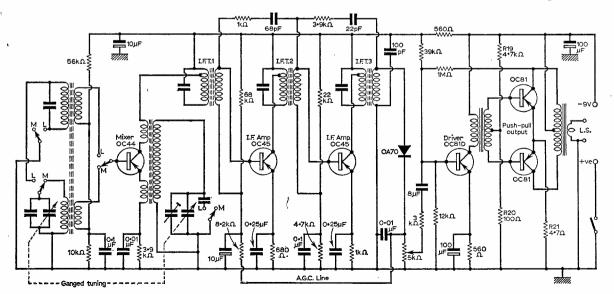
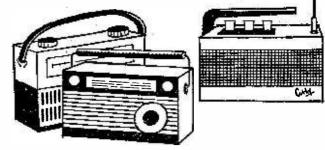


Fig. 1: Circuit diagram of a typical six transistor superhet.

RANSISTOR ORTABLES



by John Law

* ADDITIONAL AERIAL SOCKET

When operating a portable receiver in a car the internal ferrite rod aerial is not always satisfactory. Provision for a car aerial can be made relatively simply by adding an aerial coupling coil to the ferrite rod. Wrap six turns of gummed paper round the centre of the rod to make a former for the extra turns; avoid sticking the former to the rod. Now wind about forty turns of coil wire on to the former and secure with a quick drying adhesive. The aerial socket will depend on the plug on the aerial lead but, assuming it is a standard coaxial type, mount it on to the back or side of the cabinet, whichever is most convenient. Solder the leads from the aerial coil to the centre and body of the socket leaving a little spare wire. With the aerial connected and a weak signal tuned in, move the coil along the ferrite rod for maximum volume. If the receiver covers more than one waveband it may be necessary to find a compromise position for the coil. Finally, cement the former to the ferrite rod. See Fig. 2.

★ DIODE OUTPUT SOCKET

Since most small portables are fitted with small loudspeakers and have a fair amount of distortion in the output stages, output from the loudspeaker jack socket (where fitted) is not all that suitable for feeding tape recorders and the like. The output from the detector diode, however, is relatively pure and provides an ideal take-off point (see Fig. 4). As with the aerial socket modification, a miniature jack socket can be fitted to the rear or side of the cabinet. The circuit arrangement is such that plugging in the jack plug will mute the internal speaker. This is useful if the output is being fed to an amplifier; most tape recorders today have facilities for monitoring the input.

★ ADDITIONAL AUDIO STAGE

In a few cases the output from the diode detector may not be sufficient to load an external amplifier or tape recorder. To overcome this difficulty an additional amplifier stage will have to be added. Fig. 5 shows a low noise audio stage that will meet most requirements.

★ ADDITIONAL R.F. AMPLIFIER

An additional tuned r.f. amplifying stage for a transistor radio is complicated by the need for tuned circuits and separate controls. An untuned aperiodic stage is, however, capable of giving useful amplification. A circuit is given in Fig. 6. In

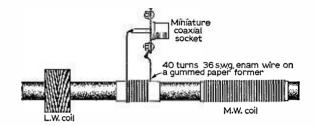


Fig. 2: Details of a car aerial coupling coil on the ferrite rod.

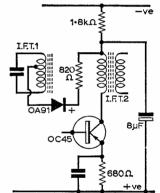


Fig. 3: Improving a.g.c. by the addition of an a.g.c. clamp diode.

Fig. 4: Adding a tape recorder output facility with muting jack socket.

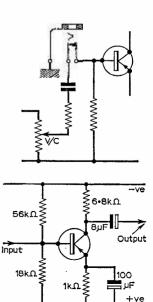


Fig. 5: Circuit of a suggested low-noise audio stage.

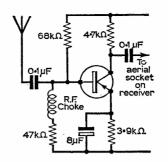
conjunction with an external aerial it can enable satisfactory signals to be picked up from weak stations.

★ BATTERY ECONOMY CIRCUIT

With push pull output stages it should be remembered that the greater the volume the greater the current and, hence, the larger the drain on the battery. It is surprising how much longer the battery will last with careful use of the volume control at all times. The ear is very tolerant and quite a small signal satisfies its requirements. Louder noises are tolerated, as it were, by the ear's own a.g.c. control.

A system of automatically biasing the push pull output stage which enables the battery to be used beyond the period when distortion would appear was introduced by one of the major manufacturers some years ago. This circuit is shown in Fig. 7. R19 in Fig. 1 is replaced by a variable $15 \mathrm{k}\Omega$ resistor and R20 with a diode shunted by a 560Ω resistor. The diode used by the author was, in fact, the base and emitter of a NKT259 transistor. To set up the circuit for use it was necessary to connect a meter in series with the centre tap of the output transformer primary and battery negative, and adjust the variable resistor to give a reading of 4mA with no signal input.

Battery economies are associated mainly with the driver and output stages in transistor radios since the current drawn by the r.f. stages is only a few milliamps. If heavy current drain is suspected it is advisable to check the values of all resistors in the



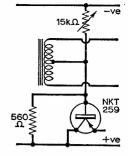


Fig. 6 (left): Periodic r.f. stage.

Fig. 7 (right): A battery economy circuit. The $15k\Omega$ resistor replaces R19 and the diode replaces R20 in the circuit of Fig. 1.

audio stages. For example, R21 has a critical value of 4.7Ω . Some of the cheaper sets omit this resistor with the result that the current is needlessly high. The presence of R21 also ensures a measure of thermal stability keeping the output transistors within their current and heat ratings.

Resistors R19 and R20 determine the biasing of the output transistors. Any change in their ratio will alter the bias and therefore the current consumption of the transistors. Should R19 drop in value or R20 increase in value the battery drain will be increased. An increase in the value of R19 or decrease in R20 can result in distortion and an increase in battery consumption.

SPEED STABILISATION

-continued from page 412

It is thus seen that all possible sources of interference are avoided by assuring that the motor control oscillator frequency is sufficiently high, preferably double that of the erase oscillator. In general do not change the frequency of the erase oscillator, since this would bring dangers of audio distortion. The bias and erase circuits are critically adjusted in good commercial tape recorders and should not be tampered with unless one has some experience and the necessary test equipment to hand—or at least the maker's instructions for the particular model. All necessary adjustments of frequency to avoid spurious beat interference should be made to the motor control oscillator or to the screening.

CONVERSION

Whilst conversions from Fig. 1 to Fig. 2 are normally possible in any tape recorder or record player without mechanical changes, conversion from Fig. 2 to Fig. 3a requires a change to a different motor, with accompanying problems of mechanical accommodation, and possibly a change of reduction ratio is necessary if the new motor pulley speed (3.000 r.p.m. at about 6mm radius) differs from that of the former motor. This will require some skill and ingenuity on the part of the experimenter.

It is possible to convert a motor of the type used in Figs. 1 and 2 for r.f. speed stabilisation without resorting to the new motor with integrated coils. This may in some practical cases be more feasible

than the mechanical complications of changing the motor type. A complete three-winding coil in a completely enclosed miniature "ferrite pot" core should then be mounted additionally on the spare copper strips of the Veroboard card with the damping coil connections taken out through the Veroboard socket to the centrifugal contact sliprings of the existing motor. About 100 turns of fine wire for the oscillator coil, 30 turns for the pick-up coil and 100 to 300 turns for the damping coil should be tried. Some experiments are required according to type and size of pot core, varying the relative and absolute number of turns until smooth action is obtained. Such a system will give very long contact life because the contact loading is nil, but the sliprings may continue to be a source of trouble. However, since these now carry only very small high-frequency a.c. currents instead of d.c., their life is improved, so that experiments along these lines to obtain r.f. speed control of conventional motors are well worthwhile.

Finally, on the subject of commercial conversion kits, these usually comprise a new Bühler motor, a set of mechanical fittings for installing this motor in place of the former one and a "partial" circuit card containing the part of Fig. 3a to the left of the dotted dividing line. This is in keeping with the fact that most recorders are already fitted with the motor current switch transistor Tr2 operated from the centrifugal contact in the arrangement of Fig. 2, and the conversion to the Bühler r.f. system merely needs Tr1 and D1 circuitry of Fig 3a to change control of Tr2 over to the oscillator sensing coil instead of directly from the centrifugal contact of the rejected motor.

practically wireless HENRY commentary by

Intelectronics

TEWS items come in complementary pairs. Right after the report that the vicar has not been in his customary pew for a fortnight we find a noncommittal mention of Miss Golightly's surprise holiday in Majorca, coupled with some difficulty in tracing the Death-Watch Beetle Fund that was in her keeping.

Right beside an uncaptioned pin-up, some malignant subeditor pastes a story with the headline: 'Cows run wild on Slopcomb beach.' And with almost inevitable certainty, after reading a sensational report from America (well, where did you think?) about electronic brainwashing of animals, and the prospect (more Orwellian than 1984) of induced personality changes in human beings being 'necessary to counter-effect the unchained use of atoms if the human race is going to survive', we come across its exact opposite.



Cows run wild on Slopcomb beach.

This is a forecast by the British International Worldwide Information Network (BIWIN—why didn't they call it Brit. Int. Knowledge & Inf. Net. Inc.? and form a more familiar title?) They say that by 1980 computers will have taken over the vast 'middle range' of human activity. Machines will make all routine decisions, take and put out tele-

phone calls, make business appointments and so on.

More important, a new race of computers will develop. These will be programmed to 'learn' in the same way that we acquire skills, by instruction, trial and error. The fantastically rapid assessment of the possibilities means that Black Box 'X' will knock up a constructakit in less time than it takes us to decipher the title page of the instruction manual.

A more sophisticated group of machines will be employed on design work, using past methods as launching pads, and ironing out all the snags before production is more than a gleam in the managing director's eye. Happy accidents, like the discovery of penicillin, are strictly for the history books, it would appear.

Henry has his doubts. Experience of the thin end of the electronic wedge engenders a healthy scepticism in any engineer.

Most of us have met the set with an inbuilt intelligence—usually directed, like a fallen angel's, to dastardly ends.

The field engineer regards such equipment as a normal part of his work. The customer has telephoned seven times while the girl in the shop feverishly tried to contact old Joe and re-organise his priorities. Each call became more desperate, each description of symptoms more alarming. It was not certain whether an engineer or a midwife would be more appropriate in this emergency.

Eventually Joe turns up, is re-routed, and casually slides back into his sagging van-seat. He reaches the customer as she slams the telephone on its rest for the eighth time, follows her into the lounge and—yes, you have guessed it—there is the receiver, an innocent smirk all over its gilt-trimmed fascia, belting forth Radio Concubine as if it had never had an intermittent

pain in its intestines.

The constructor is even more familiar with the phenomenon. He takes up his copy of the latest *Practical*——, roots in his spares box for the parts the author blithely assumes every enthusiast has been saving for just this occasion, and begins to build his Taj Mahal.



An innocent smirk.

No matter how assiduously he follows the instructions, something is not quite right, and he casts the attempt to one side to pen a 'Disgusted' letter to the Editor. Then some well-meaning Mr. B. type comes to borrow a piece of insulating tape, says: 'That looks interesting', plugs it in and gets perfect results.

Henry would not want to be thought a stick-in-the-mud. Progress is inevitable. But he is convinced that the glittering new world of the future will also spawn a new breed of computers—the electro-neurologist machines, adapted to doctor the temperamental monster we have attempted to mould after our own fashion.

Dr. Jose Delgado, of Yale, facing a charging bull, armed only with a small transmitter which sent impulses that diverted the beast by 'twitching' its brain is not so far removed from Spallazini, trying to trap bats in his tangle of wires.

The logical outcome is the computer which experiments on us!

Details on the 1155

I REFER to Mr. R. E. Robinson's cry for mods on the 1155. A great deal has been said about this receiver in the past.

In the July 1946 issue of "Wireless World," there were full circuit details of this set, together with an a.c. power pack and output stage. In the November 1947 issue of "Short Wave Listener," there was a noise limiter for it and in April 1949 "S.W.L.," a 10 meter converter. The April 1965 issue of PRACTICAL WIRELESS gave a s.s.b. detector for the 1155, and the November 1961 issue of "P.W." gave details of a "Q" multiplier which could be used on same.

John Tye.

Dereham, Norfolk.

An Exchange

In the July issue of Practical Wire-Less, reader R. E. Robinson, of Darlington congratulates contributor S. Simpson on his modifications to the No. 19 Set. If he would be interested in obtaining a Mk. III 19 set in exchange for the 1155, would he please contact me at the address below.

A. G. Ward.

Collingwood, Blackwater, Truro, Cornwall.

Can anyone help?

I HAVE a Taylor Valve Tester model No. 45b, and although I have written to the makers to try to obtain a copy of the manual and instruction book, they tell me that they are out of print. I wonder, therefore if any readers would have a copy that I could purchase or borrow to make a copy from.

H. C. Evans.

70 Seaforth Road, Seaforth, Liverpool, 21.

Tapespondent wanted

I would like to tapespond with anyone of my own age (14-15 years) living in Europe or Australasia who has an interest in Short Wave Listening and Pop Music. I have a two track $3\frac{3}{4}$ i.p.s. recorder taking up to 5in. spools.

R Baker.

488b Lady Margaret Road, Southall, Middlesex.

NEWS AND..

WORLD'S SMALLEST POCKET MICROPHONE?

What is believed to be the world's smallest single unit pocket radio telephone is now being manufactured at the Welwyn Garden City factory of Bush Murphy Electronics. Including its slide-on battery it is about the size of a medium packet of five cigars or little bigger than a pocket diary.

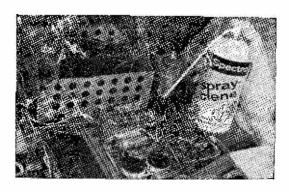
The Mitre, as it is known (derived from Miniature Individual Transmitter-Receiver Equipment) offers four channels of f.m. communication in the 68–100Mc/s or 145–174Mc/s bands. Channel spacing is 25kc/s.

Completely transistorised, the device gives half a watt of r.f. output and 100mW of audio. Designed to slip into a uniform pocket, it has a thickness of only $\frac{13}{6}$ in. (2·48 cms). The height is $5\frac{3}{16}$ in. (13·18 cms) and the width $3\frac{3}{4}$ in. (9·53 cms). These dimensions include the slide-on battery.

A sealed nickel-cadmium battery supplies power for the transciever. This is rechargeable and may be instantly changed by means of a quick-action slide. A specially designed mains operated charger is available which will accommodate up to twelve batteries simultaneously.

A miniature loudspeaker-microphone unit fitted with "press-to-talk" is used which can be clipped to the inside pocket enabling the operator to hear incoming calls. Alternative ancillary equipment is also available.

NEW CLEANER/LUBRICANT



Spectra Chemicals Limited of Caterham, Surrey, are now offering two new grades of Spray-Clene safety solvent containing lubricant. While the original Spray-Clene cleans and degreases, the new grades clean and lubricate in one operation.

Besides cleaning all electrical switches and relays without fire risk from the ignition of flammable vapours by arcing, Spectra Spray-Clene with Switch Lubricant prevents tarnish and corrosion and provides excellent mechanical lubrication. It is harmless to most commonly used insulating materials.

Spectra Spray-Clene with Instrument Lubricant will clean precision mechanisms down to watch size leaving a fine film of highly refined colourless, odourless oil to lubricate moving parts and protect from corrosion.

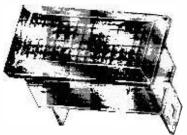
All grades are supplied in 12 oz. aerosols fitted with angled extension tubes giving "one hand reach anywhere" action at full pressure. This facilitates cleaning without dismantling, while low toxicity and non-inflammability permits use in most situations. Price: Standard Spray-Clene 7/6d. each. Spray-Clene with either lubricant 8/- each.

...COMMENT

ARCOLECTRIC NEON INDICATOR

Recent additions to Arcolectric's range of neon indicators include Cat. No. SL.59.

This is designed for snap in fixing, having integral spring clips in the polycarbonate lensbody. Colours available are red amber, clear or green. The indicator can be fitted with either tab terminals (SL.59) or flexible leads (SL.59/WL).



PRESENTATION TO BICC BY LORD DERBY

The emblem of the Queen's Award to Industry, together with a Grant of Appointment bearing the signatures of H.M. The Queen and the Prime Minister, were presented on July 18 by the Earl of Derby, M.C., Lord Lieutenant of Lancaster, to Lord McFadzean, Chairman of British Insulated Callender's Cables Limited.

From among nearly 1000 concerns who applied BICC are one of 115 organisations to win the distinction. This is conferred for outstanding export achievement or technological innovation or both. BICC were among the select few—18 firms in all—who won Queen's Awards in both categories.

In direct exports BICC's figures in 1965 reached a record level of £40 million—an increase of 47% over 1964. At £77 million sales by overseas companies in 1965 showed an increase of 25% over 1964. From many examples of BICC technological innovation, three were submitted under the terms of the Queen's Award. These were: bulk power transmission by both land and submarine cables; railway electrification; and magnet wires and strips.

NEW HEATHKIT CATALOGUE

Daystrom Ltd., Gloucester, announce their new Heathkit catalogue No. 86/3. It covers their range of kits and includes some new models, such as the model EC-1U Analogue Computer Kit, and De-luxe Transistor f.m. Tuner Kit.

WIREWOUND POTENTIOMETERS FOR PRINTED CIRCUITS

W. Greenwood (London) Ltd., 21 Germain St., Chesham, Bucks., introduce a new wirewound adjustment potentiometer specifically designed for direct mounting on to printed circuit boards.

This precision component is a single turn potentiometer with outstanding humidity performance. It has a power rating of $1\frac{1}{2}$ watts at 50°C, and is available in a resistance range from 10Ω to $50k\Omega$. The solder pins are gold plated.

The potentiometer is one of a comprehensive range manufactured by Contelec of Switzerland. It is a competitively priced component and

It is a competitively priced compo delivery is ex stock.



RADIO CLEARANCE UNDER NEW MANAGEMENT

Radio Clearance (1965) Ltd. (retail sales of radio-electronic and electrical components) 27 Tottenham Court Rd., W.1, are now under completely new management. All items as previously advertised will be available plus a much wider range of items. Shop hours are 9-6 Monday to Friday, 9-1 Saturday (MUS 9188).

Great Circle Calculations

USERS of the formula 2b for Azimuth of bearing should be warned that the formula is a classic example of the "ambiguous sine". The value of the sine C so calculated applies equally to two angles, C and 180-C, and there is nothing to show which is the right one for the case being worked. It will be seen in Fig. 1, page 261, August, 1966, that a circle of radius a and centre C will cut the meridian of B in two places. Hence the two values of C. A further point is that it is unnecessary to limit the calculations to places in the same hemisphere. For myself, I prefer to use the fundamental formula 1, using the polar distances 90—lat for b and c or, otherhemisphere, 90+lat. F Hilton.

> Cranmore, Isle of Wight.

Any ideas?

I HAVE a unit—presumably a receiver—with the following details on the case: R-89/ARN 5 A. 24V D.C. CRO 0825 DAY 44. PL 284. There is a two pin input socket and a ten pin socket below this. There are three crystals marked KC6497.9, KC6522.9, and KC6547.9.

I would be very pleased to hear from anyone who could give me any help at all on this, especially a circuit or instruction book.

Roger Sheppard.

122 Gloucester Avenue, Regent's Park, London, N.W.1.

Letter of thanks

I would like to thank all those who replied to my letter "Can anyone Help?" in the August issue of Practical Wireless. I have had 50 replies and now have the set working.

I could not agree more with H. S. Barkin's letter "Save the Grand Old Sets" and the saying "they don't make 'em like they used to" applies more than ever these days.

G. Wright.

East Lothian, Scotland.

Issues for disposal

DUE to storage problems, I am obliged to sell March 1965—July 1966 issue of Practical Wireless with blueprints, etc. If anyone is interested, I will be pleased to let them know any further details.

B. Wilson.

37 Gladys Street, Clifton, Rotherham, Yorkshire.

MW-DX

by Ken Brownless

OME of us who do not devote much time to short wave listening find that there is a different kind of Ochallenge in looking for and listening to DX on the medium waves, which makes an interesting change from what can be heard on short wave. It is most fascinating to be able to eavesdrop on the domestic radio stations of other countries. challenge lies in the fact that medium wave DX is much harder than that on short waves, calling for considerably more patience, care and accuracy when listening.

Receivers and aerials

The choice of receiver is often governed by the amount of cash available. The most frequently used surplus receivers are the AR88, CR100 and R1155, all of which give satisfactory results. Commercial communications receivers will also give excellent The good class valve domestic receivers will give fair results, as will the better transistor receivers. In all cases some form of antenna is a definite advantage for medium wave DX'ing, the most useful type being a loop, details of which will appear next month.

If a "long wire" aerial is preferred, a length of 50 feet or more of wire is recommended, but even a length of wire strung round a picture rail can be of some help. However, the loop, with its excellent signal-to-noise ratio and directional properties, is the superior antenna for medium wave DX. The use of an earth is also to be recommended.

What to expect

The last two seasons (autumn to spring 1964/5 and 1965/6) have given us interesting reception from coast-to-coast of North America and South America (mainly the northern part). We had indications of this during the spring of 1966 and we can expect this pattern of reception to continue with a gradual decrease in the number of North American loggings as we approach the next sunspot maximum. last two seasons produced excellent Asiatic reception in the afternoons and evenings, which should continue during this autumn, winter and spring.

Recommended time for North America is from 01.00 G.M.T. when there is less European QRM.

The following are easy ones: CBA (1070 kc/s), Sackville, N.B., often heard under Paris and then in the clear after Paris signs off at 23.00; CJCB (1270 kc/s), Sydney, N.S., often the first North American audible in the U.K. from 20.00; both the aforementioned stations have also been heard at

Some frequently heard North Americans are CBN (640 kc/s), St. John's, Nfld.; WNBC (660), New York City; WOR (710), N.Y. City; WHDH (850), Boston; WCBS (880), N.Y. City; CJON (930), St. John's, Nfld.; WINS, N.Y. City and CFRB, Toronto, both on 1010; WNEW (1130), N.Y. City; WCALL (1210). WCAU (1210), Philadelphia, best heard after the B.B.C. Light Programme signs off at 02.02.

The H.F. end is also productive: WMEX (1510), Boston; WKBW (1520), Buffalo; WCKY (1530), Cincinnati, and WQXR (1560), New York, which is often the best in this range.

Easy South Americans are Radio Americas, Swan Island (1157); YVNZ (1020), Radio Calendario, Maracaibo, and LR1 (1070). Radio El Mundo, Buenos Aires, often heard under CBA.

Easy Asiatics include the 1,000 kW V.O.A. stations on Okinawa (1178) heard afternoons up to 16.30 sign off; also the high powered Western China relay of Peking's Russian Service (1525) between 15.00 and 22.00. Another interesting channel is 1250 where two Asiatic signals have been heard around 15.30, the dominant signal is Vladivostok and All India Radio, Sangli, has been heard with news in English at 15.30.

Useful guides

Three useful helps to medium wave listening are published by World Publications in Hellerup, Denmark, and may be obtained through local booksellers. These are (1) "World Medium Wave Guide" which includes a listing of North American stations by frequency, call-letters and also by location, (2) "World Radio and TV Handbook" and (3) "How to Listen to the World."

Genuinely interested M.W. DX'ers will also be interested in the newsletter edited by the author. Details from: K. Brownless, 7 The Avenue, Clifton, York.

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AUTOCATALÝTIC PLATING

K. T. WILSON

LECTROPLATING is such a widespread and well-known method of producing a metal coating on a conducting surface that we tend to forget the much more ancient and delicate art of "Immersion", or, more correctly, Autocatalytic plating.

In principle, the process is remarkably simple. The object to be coated may be metallic (with certain exceptions) or non-metallic. The coating is uniform, irrespective of the shape of the object, and well bonded, and plating is carried out simply by immersing the object in the plating solution. The earliest known process of this type is the technique of silvering mirrors; a process familiar to any schoolboy who has added ammonia solution dropwise to silver nitrate solution until the precipitate which forms has just redissolved, then warmed gently with formaldehyde (about three drops of 2% solution) until a bright mirror of silver appears on the test-tube.

What is fortunately not so familiar is that the by-products of the reaction are explosive if allowed to dry; they should be washed off immediately plating is complete.

Autocatalytic Reduction

Chemically, the reaction is known as an "Autocatalytic Reduction". The reduction part of it is the conversion from metal ions in solution to solid metal, the Autocatalytic part implies that the reaction requires a catalyst to start it and keep it going, and that the catalyst for such a reaction is the metal which it produces. This raises the very reasonable question: "How does such a reaction start in the first place?"

This depends on the object being plated. Many metals other than the one being plated may act as catalysts for the process. Even if only the slightest reaction is promoted, this will be sufficient to start autocatalysis. In other cases a thin film of the autocatalytic metal may be deposited by displacement, the process by which iron filings placed in a copper sulphate solution acquire a coating of copper; note that this process stops whenever the iron is fully covered, whereas the autocatalytic process goes on until the solution is exhausted.

Printed Circuits

Non-metals must be primed, that is, coated with a readily reduced salt of a metal which will catalyse the main reaction. Since this implies that the metal will not be deposited at any point not properly primed, the process has an obvious application to printed circuits.

Suppose we have a clean grease-free board of Paxolin or similar material. We then print or draw on this board a circuit, using as our ink, a solution of suitable primer. We then immerse the board in the autocatalytic plating solution to deposit metal over the drawn lines.

In practice, of course, it is not quite so easy as it sounds. The surface of the board must be chemically clean and absolutely free from grease. The containers for the solutions must also be scrupulously clean. One of the most annoying experiences of autocatalytic plating, and one which haunts the worker who uses insufficiently cleaned glassware, is to find that a plating solution which perversely refuses to deposit on a well-primed board will instantly react on a beaker which has one minute speck of dirt on it.

Temperature is critical for some solutions. Some can be regenerated, with care, almost indefinitely, others last only a few hours.

Plating Solutions

The best-known chemical plating solutions are those for nickel and copper. The nickel solution actually deposits an alloy of nickel and phosphorus. Virtually every workable solution and variation thereon has at some time been patented, and no immunity from patent restrictions can be guaranteed for the formulations given, but this should not be any barrier to experimenters; firms wishing to use such processes can sort out the patent situation for themselves.

ACID NICKEL BATH

Nickel Chloride, NiC₂, 6H₂O 30 gms./litre Sodium Hypophosphite, NaH₂PO₂, H₂O 10 gms./litre Sodium Hydroxyacetate, NaC₂H₂O₃ . . 10 gms./litre

Used at a temperature of 210°F., 99°C., this bath deposits at a rate of 0.0005" per hour. Heating up to the working temperature should be done slowly and the solution should be thoroughly filtered before heating. Soft or demineralised water is recommended for making up solutions.

It is possible to preserve this solution, like so many other nickel solutions, by cooling rapidly after use and filtering into a clean bottle. Loss of active ingredients can be compensated by adding small quantities of the first two ingredients in solution to the cold mixture. Never add powdered ingredients or the bath will at once shed all its nickel.

---continued on page 415

GETTING GOING

Py international definition the v.h.f. (very high frequency) bands extend from 30Mc/s to 300Mc/s (10 metres wavelength to 1 metre). These include Band I and Band III television as well as Band II f.m. broadcasting. Also in this part of the radio spectrum there are four bands allocated to amateur radio. These are known as 6, 4, 2 and 1½ metres. Of these, only 4 metres and 2 metres may be used for transmission in the United Kingdom and Eire. The details of the British licensing conditions are given in Table I.

TARIFI	Rritish	Licensina	Conditions	for v h f	
IADLE	DITUSII	Licensina	Conditions	IUI V.II.I.	

Band	4m	2m
Frequencies Mc/s	70·1—70·7	144–146
Maximum D.C. Power Watts	50	150

Types of emission allowed: CW MCW AM SSB DSB NBFM FSK

Special notes

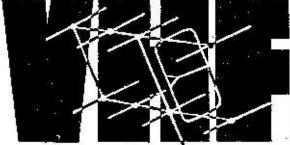
4m The section 70·35—70·4 Mc/s. only can be used for emergency purposes. North West of the line from the Firth of Lorne to the Moray Firth only the frequencies 70·3—70·5 Mc/s. may be used.

2m The frequencies 144·0 144·09 144·18 144·27 144·36 144·45 144·54, 144·63, 144·72, 144·81 and 144·9 Mc/s. must be avoided.

It is generally thought that v.h.f. communication is limited to line of sight. In other words, the two stations in contact must be able to see each other. This is not strictly true, although the range is limited. However, unless there is a large amount of intervening high ground, stations with medium power and modest aerials can maintain regular contact up the about 30 to 40 miles. Contacts over much larger distances can be made as explained in later paragraphs.

Although communication is somewhat restricted, the v.h.f. bands have several advantages. Among these are: much greater bandwidth (hence less congestion); virtually no atmospheric noise; virtually no interference from non-amateur stations; minimal t.v.i. problems; ease of making and erecting good aerials due to their small size.

The days have gone when the amateur wishing to go on to v.h.f. had to improvise and to use unsuitable equipment. The components from any television set capable of receiving Band III (ITV)



J.P. BILLINGHAM G8AAC

signals are suitable, and since so many are made, are now no more expensive than the components used for medium wave broadcast reception.

Six Metres

The six metre band extends from 50Mc/s to 54Mc/s and is used mainly on the American and African continents, although there are a few other places where operation is permitted.

Like the other v.h.f. bands, use is mainly confined to a limited radius. However, in some respects 6 metres is similar to 10 (28Mc/s-29·7Mc/s).

During periods of sunspot activity parts of the 'E' layer of the ionosphere become very highly ionised This causes it to reflect radiation of a much higher frequency than normal. This effect is usually short-lived and is known as "sporadic 'E'." Spordadic 'E' usually occurs during midmorning or late afternoon in the summer, and quite often over the equator. This means that African stations may be heard in Europe quite often.

Transatlantic contacts have been made by the cross-band technique, that is, American stations have transmitted on 6 metres and the British stations on 10 metres.

Four Metres

The 4 metre band extends from 70·1 to 70·7Mc/s and is a British and Irish only band. Consequently, the true DX properties are not really known, although it is hoped that 4 metre/6 metre QSO's will be achieved nearer the sunspot maximum.

This band is becoming more popular for local "nets" and in some areas has replaced top band for popularity. It is also very popular for mobile working since many commercial car radio aerials can be used as a quarter wave ground plane aerial.

Two Metres

The 2 metre band extends from 144-148Mc/s, although in Europe the range 144-146Mc/s only is used. This is the only world-wide v.h.f. amateur band, and tends therefore to be the band on which there is the greatest concentration on DX.

As with 4m, 2m is used mainly for local working. Since the level of activity is relatively high, a



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1mA 22/6	750mA	22/6	500V D.0	3	22/6
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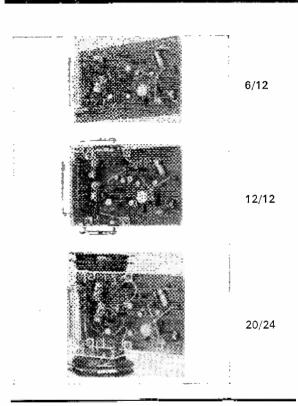
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voluntary band plan has been drawn up by the RSGB (Table II) and amateurs in Britain in general

keep to this.

Various methods of propagation are used for long distance QSO's on two. Probably the most imaginative to date is Earth-Moon-Earth (E-M-E, or more popularly "Moonbounce"). The enormous problems involved have been overcome to a large extent by a few dedicated amateurs, and intercontinental DX has been achieved.

Transatlantic QSO's were made using the Oscar III satellite, and some of these were reported in PRACTICAL WIRELESS. Since Oscar, there have been some translator balloon tests in Europe. Some amateurs regard these as cheating, though, since they involve retransmission of signals.

Another exotic "space-age" method used is known as "meteor-scatter". Signals are reflected from

TABLE II RSGB Voluntary Band Plans **4 METRES**

70·1—70·175 Mc/s	Northern England, North Wales.
70·175—70·3 Mc/s	Free.
70·26 Mc/s	Mobile calling frequency.
70:370:35 Mc/s	Isle of Man Northern

Ireland, Scotland 70·35—70·4 Mc/s Free (R.A.E.N. Priority).

70·4-70·45 Mc/s S.W. England, South Wales, Channel Islands.

70·45-70·625 Mc/s Free 70.625--70.7 Mc/s South and S.E. England.

2 METRES

144·0-144·1 Mc/s	Nationwide CW only.
144·1—144·25 Mc/s	Cornwall, Devon, Somerset, Berks, Dorset, Hants, Wilts and the Channel Islands.

144·25—144·5 Mc/s Brecon, Cardiganshire, Carmarthenshire, Glam, Glos, Herefordshire, Mon, Pembrokeshire, Radnor, Worcs.

144·5--144·7 Mc/s Kent, Surrey and Sussex. Beds, Bucks, Essex, Herts, 144·7-145·1 Mc/s London and Middlesex.

145·1--145·3 Mc/s Cambs, Hunts, Leics, Norfolk, Northants, Oxon, Rutland, Suffolk and Warwickshire.

Anglesey, Caernarvonshire, 145·3-145·5 Mc/s Ches, Denbighshire, Flints, Merionethshire, Montgomeryshire, Salop and Staffs.

Nationwide SSB spot fre-145-41 Mc/s quency.

145·5-145·8 Mc/s Derbys, Lancs, Lincs, Notts and Yorkshire.

145·8-146 Mc/s

Scotland, N. Ireland, Isle of Man, Cumberland, Co. Durham, Northumberland, Westmorland.

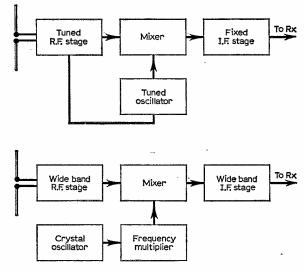


Fig. 1: Top-Tuneable converter producing fixed i.f. Fig. 2: Bottom—Crystal controlled converter tuned i.f.

ionised meteor trails in the upper atmosphere. As these occur at about 60 miles up, this gives an average maximum range of about 1,400 miles. The best time of day for this activity is at about 6 a.m. Signals have also been bounced off aurorae. However, all of these methods, so far, have used c.w. only as a means of contact.

Tropospheric Refraction

The most common method of DX propagation is by tropospheric refraction. This occurs rarely at frequencies below 100Mc/s. The mechanism involved is similar to that by which mirages are seen. The radiation path is bent by the lower layers of the atmosphere, and in some cases can be "ducted" above the ground for a considerable distance before it is bent back again. This way, two-way contacts of over 1,000 miles have been achieved. Tropospheric refraction normally occurs when the pressure and humidity are high. The usual indications of this are fine muggy weather.

"Sporadic E" propagation rarely occurs on this band, but an outstanding opening occurred over Europe on the morning of July 4, 1965, when British and Irish stations were able to work as far as Italy and Yugoslavia.

There are several beacon stations on 2 metres which give indications of openings. Some of these are listed in Table III.

1월 Metres

The $1\frac{1}{2}$ metre band extends from 220-225Mc/s and is used in America. The characteristics of this band are very similar to 2 metres.

Techniques

The v.h.f. bands, from the technical point of view, can be divided into two sections: 30-100Mc/s and 100-300Mc/s.

In the first of these, h.f. techniques can still be

used, and the majority of valves and many transistors will function effectively. However, the section from 100-300Mc/s represents a transition from "normal" circuit techniques to the specialised techniques of v.h.f. and microwave work. Components have to be selected with great care. Consideration will now be given to the various pieces of equipment used.

Aerials

Although on 6m. and 4m., and occasionally on 2m., scaled down versions of h.f. aerials are used, by far the most popular aerial is the Yagi array, the familiar TV aerial.

Horizontal polarisation is almost universal on

6m., 2m. and $1\frac{1}{2}$ m., but there is a tendency to use vertical polarisation on 4m. This has come about because of the availability of surplus transceivers (the B44). These run on 12V d.c. and are compact and thus are ideal for mobile use.

Receivers

In the early days of v.h.f. the super regenerative receiver was the most popular. However, since this type of receiver is notorious for re-radiation, and since the 2m. band is also used by aircraft, it has dropped out of favour. Most amateurs nowadays use a converter, the output from which feeds into a short wave or communications receiver. There are also receivers which tune the v.h.f. bands, such

F	REQUENC Mc/s			III VHF BEAC			R.F. Power		.
Band	7,-	Call Sign	Approximate Location	Operating Peri	od¹	Mode	(W)	Aerial	Direction
6m	50.046	ZE1AZC	Salisbury, Rhodesia	Continuous ²		Not known	40	Ground Plane	All
						Call sign A1	15	4 element Yagi	S
4m	70.100	GB3ANG	Dundee, Angus	Continuous ³		each minute Call sign A1		_	
	70.305	GB3LER	Lerwick, Shetland	Continuous		each minute Call sign A1	15	Two 4 ele Yagis	NNE, S
	70-695	9H1MB	Malta	Continuous ⁸		each minute	15	4 ele Yagi	Towards London
				Daily		Call sign A1		•	
2m	144.005	OE5THL	Linz, Austria	0700—1900 GN All times, except		30 per minute ⁴ A1/A2/A3	0.4	Ground Plane	All
	144.010	SP7VHF	Kielce, Poland⁵	Monday		"de SP7VHF"	50	Dipole ⁶	Not known
		220070	D. Joseph Comparell	Continuous		Call sign A1 each minute	25	6 over 6 Yagi	ENE
		GB3CTC	Redruth, Cornwall Innsbruck, Austria	Continuous ²		Not known	25 5	Vertical	All
		OE7IB/P GB3GW	Swansea, Glamorgan	Continuous*		Not known Call sign F1		Not known	Not known
	144 500	GB3VHF	Wrotham, Kent	Continuous		each minute	50	5 ele Yagi	N
		OH3VHF	Tampere, Finland	Continuous Daily		Not known	80	Six 4 over 4 Yagis	
	145.000	SM4UKV	Orebro, Sweden	0600-2400 GN	/T10	Not known	90		All
		LA1VHF	Riukan, Norway	Continuous	-	Not known	= 20	Crossed Dipole	All
		LA2VHF	Trondheim, Norway	Continuous		Not known	20	Crossed Dipole	All
		LA3VHF	Harstad, Norway	Continuous		Not known	20	Crossed Dipole	All
		LA4VHF	Bergen, Norway Straubing, Niederbayern,	Continuous		Not known	20	Crossed Dipole	All
	145-900	DL0SG	Germany	Not known ¹¹		Not known Call sign A1	12	Not known	All
	145-985	GB3ANG	Dundee, Angus	Continuous Daily		each minute	15	5 ele Yagi	S
	145-987	OZ7IGY	Copenhagen, Denmark	1100—2300 GA	ΛT²	Not known		Not known	All
	145.990	GB3GI	Strabane, Co. Down	Continuous		Not known	15	Two 5 ele Yagis	Not known NW, W,
	145-990	YU1VHF	Yugoslavia	Continuous		Not known Call sign A1	50 12	Four 4 ele Yagis	
	145-995	GB3LER	Lerwick, Shetland	Continuous Daily		each minute Call sign A1	15	6 over 6 Yagi	S
	145-995	OE5THL	Linz, Austria	0700—1900 GN	ΛT	30 per minute ⁴	0.4	Ground Plane	All
		YU2VHF	Yugoslavia	Continuous		Not known	50 12	Four 4 ele Yagis	NW, SW, NE, SE
	In the	1021111	i ugosiavia	Continuous		Unmodulated call sign A2	arrier,		,
	range 145:95	OE1XAA	Wein, Austria ⁵	Continuous		each minute	1	Halo	All
	146 Not known	OH8VHF	Oulu, Finland	Continuous13		Not known	Not known	Not known	Not known
to the	operating p times when erational.	period refe	rs 2 These beacons of	ogramme. It in nether they	These	e beacons await	:	This beacon to 30 seconds on on the QSY's to the	ne frequenc
	se beacons a ed to better					e beacons are I yet operationa		9 400 c/s shift	
	mporarily Ω hoped to be				2 Fina	l D.C. input p		l3 During test o call sign used is	





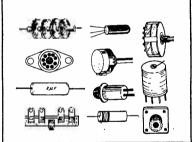
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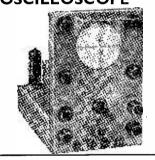
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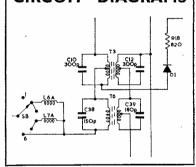


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0-2.500v.	D.C. 20,000	ohms per volt. 0-	1,000v. A.C.	99/6
	to 6 mag			77/0

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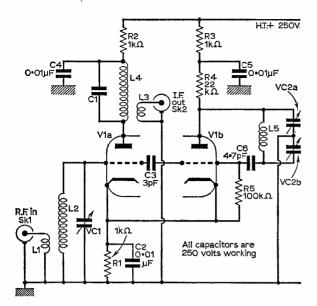


Fig. 3: Example of a typical simple tunable converter. The tuned circuits VC1/L2 and VC2a—VC2b/L5 are arranged to produce the desired intermediate frequency.

as the surplus R1392.

There are basically two types of converter. There is the tunable converter which produces fixed i.f. The RF24, 25, 26 and 27 units are examples of these. There are also converters which have a fixed frequency oscillator, usually crystal controlled, where the i.f. is tuned by the receiver.

Block diagrams of the two types of converter are

35Mc/s

shown in Figures 1 and 2, and typical circuits are shown in Figures 3 and 4.

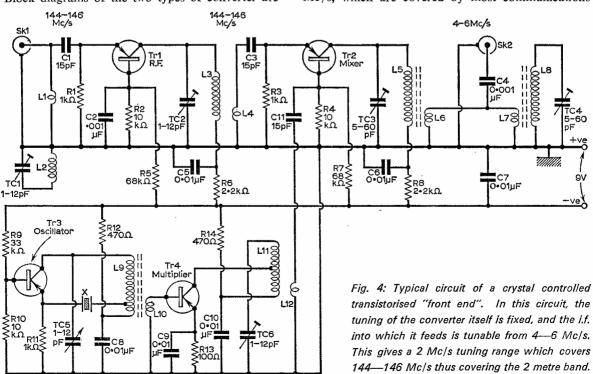
The best converters always include a stage of r.f. amplification and a stage of i.f. amplification. Although the tunable converter is the simpler to build, the crystal controller converter is more popular because of its advantages. These are: It is easier to tune to a specific frequency accurately; signals on adjacent channels can be separated more easily; stability is adequate for s.s.b. and c.w. signals to be read; a long warming-up period is not necessary.

Receiver noise is a serious problem, and a low noise front end is essential for receiving weak signals. Consequently, for the best results, special valves are used. These are almost all triodes. Examples of these are Nuvistors such as the 6CW4 and 6DS4, double triodes designed for cascode operation such as the ECC88, and special valves for grounded grid operation such as the A2521, EC88 and 6AM4.

Semiconductors

Now that v.h.f. transistors are at reasonable prices, these are tending to replace valves as they have lower noise figures. The AF139, AF186 and GMO290 are very popular, all priced about £1. Because of noise considerations the first mixer is usually a triode rather than a multigrid valve, although once again transistors are proving advantageous.

Choice of a suitable i.f. is important, as it is desirable to avoid powerful broadcasting stations, since these may break through. The most popular ranges for i.f.'s are: 2-5Mc/s, 12-14Mc/s, 24-30 Mc/s, which are covered by most communications



140Mc/s

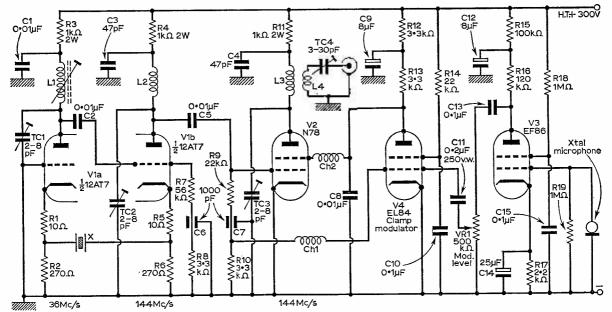


Fig. 5: Circuitry for a simple two metre transmitter. This is a typical circuit, V1, V2 forming the r.f. section and V3, V4 the modulator.

receivers. There is no doubt, though, that the range 30-40Mc/s is the best as there is very little activity in this region, and there are some surplus receivers, the R1466 (34-40Mc/s) available at almost give away prices.

Too low an i.f. should be avoided since this may give rise to poor image response and increased noise. In general, the minimum i.f. for 6m. and 4m. should be 1Mc/s, for 2m. 2Mc/s, and for 1½m. 3Mc/s.

In some areas, television receivers can be used. When conditions allow, and there is not a local transmitter on the channel, 6m. signals may be heard on channel 2 and possibly channel 3, if a horizontally polarised aerial is used. Also some receivers, when tuned off channel 5, will pick up 4m. signals.

Transmitters

Transmitters are almost universally crystal controlled, since v.f.o. stability is not good enough. (A drift of one part in 10,000 [0.01%] on 2m. is over 14kc/s.). Consequently the operating technique is to call on one's own frequency and then

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to tune the band for replies. This technique simplifies construction to some extent since the complication of a v.f.o. and tuning the power stages does not occur.

On 6 and 4m. most available transmitting valves can be used, even the 807, although its efficiency is well down and many receiving valves are suitable. For instance, the ECL82 is often used in the p.a. of a 4m. transmitter.

On 2m. some receiving valves can be used, but generally special valves are required. Double-beam tetrodes such as the 832, QQVO3-10 and the QQVO6-40 are very popular for medium and high power rigs.

Figure 5 shows a circuit for a typical simple low-powered crystal controlled transmitter.

Throughout the v.h.f. bands, tuned circuits may be made, using capacitively tuned coils. However, for frequencies above 100Mc/s tuned transmission lines can be used, and usually are in high-power stages. The use of non-inductive capacitors and resistors is advisable. Insulators should be ceramic or p.t.f.e., although losses in Paxolin are not serious up to 150Mc/s.

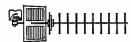
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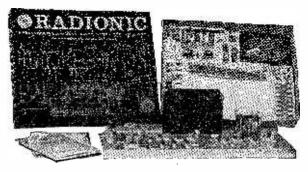
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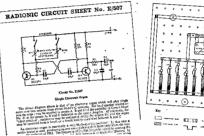
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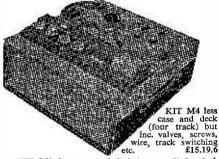
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NETWORK ANALYSIS FOR TELECOMMUNICATIONS AND ELECTRONICS

By R. A. Lampitt, M.Brit, I.R.E. Published by Iliffe Books Ltd. = 263 pages. $8\frac{1}{2}$ ins. x $5\frac{1}{4}$ in. Price 63s.

THIS book is intended to be used as a text for advanced students of Telecommunication and Electronic Engineering and aims at the fourth and fifth year level of the appropriate courses in preparation for entry to the Graduateship Examina-tion of the Institution of Electronic and Radio Engineers and the City and Guilds of London Institute supplementary studies in Advanced Telecommunications and Electronic Principles.

It is envisaged that the book is appropriate to students holding H.N.C. or equivalent and is thus not suitable for beginners or novices. Briefly the volume deals with the mathematical treatment of the principles involved in the field of telecommunications and electronics and forms firm ground on which to base further studies of the many special

applications of the subject.

The first chapter offers useful revision and introduction to the subject. This leads to the chapter on basic networks and thence to transmission properties of four-terminal networks. Further chapters on tuned circuits and wave filters, followed by transmission lines and an introduction to the Fourier analysis of waveforms, completes what is thought to be a useful contribution towards providing the student with essential material for study.—LSA.

TRANSISTOR ELECTRONIC ORGANS FOR THE AMATEUR By Alan Douglas and A. Astley. Published by Sir Isaac Pitman & Sons Ltd. 70 pages. Size 8½in. x 5½in. Price 18s.

NO those interested in electronic organs the name of Alan Douglas will be well known. In this L book, in conjunction with A. Astley, the accent

is entirely on solid state construction.

Chapters include: Organs and Their Terminology, Introduction to Transistors, Transistorised Organ Circuits, All-transistor Amplifiers and Supplies, and Semi-conductor Keying and Special Effects. In addition there is a complete chapter devoted to the design and construction of a transistorised two-manual pedal organ.

An extremely useful book for the practical enthusiast, it commences with a discussion on transistors and how they work, including characteristic curves, etc., and even contains a circuit for a simple transistor tester. The chapter on the two-manual organ depicts chassis layouts, wiring layouts, diagrams of commercial and home-made contact blocks and photographs of the various sections. For those building an organ of this type the book is a good buy for this one chapter alone.

The remainder of the book is liberally endowed with circuits, nearly all with values. These useful diagrams include such things as a light-operated volume control, tone filters, vibrato oscillators and

frequency dividers.—DLG.

HAM ANTENNA CONSTRUCTION PROJECTS By J. A. Stanley. Published by W. Foulsham & Co. Ltd. 160 pages. Size 8½in. x 5¼in. Price 24s.

ASSENTIALLY this is a book for the practical man. It concerns itself, as the title implies, with the numerous aerials suitable for use on the amateur bands. It is perhaps somewhat refreshing to find a book almost devoid of mathematics

on a subject which can be quite complex.

In place of "pi" and log_e Mr. Stanley offers "length of wire", "number of turns" and "tuning up procedures". Let's look through this tome of down-to-earth, uncomplicated collection of aerials. Briefly there are chapters on Verticals, Horizontals, Multi-element Beams, Vertical Beams, Long Wires
—Short Wires, Indoor Antennas, V.H.F. and Special Purpose Aerials. As an added attraction an entire chapter is devoted to using antenna test equipment -g.d.o's, s.w.r. bridges, etc.

If you wish to erect an aerial which will receive and/or transmit signals efficiently without the mathematical analysis of why, then this 24 shilling

work is an investment.-DLG.

KNOW YOUR SIGNAL GENERATORS 144 pages. Size $8_2^{\rm sin}$, x $5_2^{\rm lin}$. Price 20s. KNOW YOUR SQUARE-WAVE AND PULSE GENERATORS 144 pages. Size 8¾in. x 5½in. Price 21s. Both by Robert G. Middleton. Published by Foulsham-Sams Ltd.

HESE two both deal at some length with the design, application and employment of particular pieces of test equipment. The author bases his work firmly on a practical knowledge of servicing. There are many "throwaway" hints and tips in these pages, and the illustrations are lavish, including many photographs of oscilloscope traces.

SIGNAL GENERATORS starts by defining the instrument and describing the various types, discusses accuracy and calibration and the various methods of modulation. Descriptions of specialised generators include u.h.f. and audio generators, analysers and transistor instruments and something we will all need to know about soon - the F.M. Stereo

Multiplex generator.

PULSE GENERATORS the technique square-wave testing, extremely useful in audio work, is fully discussed, with a wealth of diagrams. As a departure from the usual method, Mr. Middleton describes the circuit and construction of many of the instruments he is discussing, and adds the bonus of a final chapter focused entirely on a laboratory-type pulse generator, going through its circuit and application step-by-step. One learns more by this spotlight method than in volumes of generalised description.

It goes without saying that this author wastes no words. The text remains readable, although its information content is formidable. Even if one should never run to the type of test gear he is describing, the circuits on which it is used become much more familiar after a careful study of this recommended bench-side reading.—HWH.

* SENSITIVE baby alarm

BY F. GATE

HIS device consists of an extension amplifier, complete with loudspeaker and should be suitable for most homes, since it has an output in excess of 200mW. A moving coil loudspeaker may be used as a microphone and can be coupled to the amplifier with unscreened cable.

A view of the interior of the amplifier is shown below (Fig. 1) and the circuit diagram is illustrated

opposite (Fig. 2).

Circuit Description

Signals are picked up by the 3Ω moving coil loud-speaker, which is used as a microphone, and fed directly to the emitter of Trl, a grounded-base amplifier. The collector load Rl of the first transistor is in series with the emitter load—the microphone. Now, although R1 and the speaker are effectively in series as far as the current is concerned, the internal characteristics of the transistor change the apparent values of these two components, effectively increasing the values of both, but increasing the apparent value of the emitter load to a greater degree than it increases the apparent value of the collector load. The voltage gain of the circuit is thus lower than might at first be expected. Actual voltage gain is approx. 120 times

One of the snags with transistor circuitry is that, when a number of stages are used, the low impedance input of the following stage effectively shunts the collector load of the preceding stage, so that, although a collector load of (say) $5.6k\Omega$ may be used, the *effective* value of the load is reduced to less than $1k\Omega$, and gain is thus reduced. In this amplifier it is overcome by direct coupling the collector of Tr1 to the base of Tr2, which is wired as an emitter follower. This gives a high input

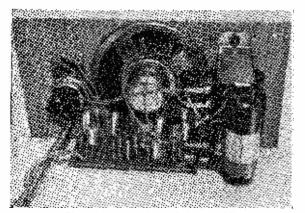


Fig. 1: Interior view of the amplifier.

impedance and a low output impedance, and is thus able to feed following stages with minimum loss of signal, while at the same time placing a negligible load on the preceding circuit.

D.C. negative feedback is applied to Tr1-Tr2 to stabilise the operating points, Tr1 base-bias being derived from Tr2 emitter. The major part of the emitter load of Tr2 is made up by VR1, which is used as a volume control in the completed unit.

The amplified signal appearing at the slider of VR1 is fed, via C3, to the base of Tr3; as a conventional common emitter amplifier, with collector load R6, base-bias network R4-R5, and emitter load R7 decoupled by C4. Again an emitter follower, (Tr4), is used as a buffer between Tr3 and Tr5.

The amplified signal appearing at the emitter of Tr4 is applied, via C6, to the power amplifier stage. Here, three transistors are used, Tr6 (p-n-p) and Tr7 (n-p-n) being the actual output transistors, and Tr5 being the driver. For all practical purposes, Tr5 can be considered as conventional common emitter amplifier. Tr6 can be regarded as an emitter follower, with its base directly coupled to the collector of Tr5, and with Tr7 as its emitter load. Similarly, Tr7 can be regarded as an n-p-n emitter follower, but in this case with Tr6 as its emitter load. Thus, the junction of the two emitters is at low impedance, and feeds the 25Ω speaker via C8. This common junction is at roughly half supply volts, and when a positive going signal from Tr5 collector is fed to both Tr6 and Tr7 bases, Tr6 is cut off and Tr7 conducts; when the applied signal is negative going, it is the n-p-n transistor, Tr7, which is cut off and Tr6 that conducts. Thus, the circuit acts as a class-B push-pull amplifier. With this circuit, it is essential that the potential at the junction of the Tr6 and Tr7 emitters stays at a mean level of approx. half the supply potential, and with this in mind the base-bias to Tr5 is stabilised by the d.c. feed-back loop from the Tr5 collector junction to R13. R11 is used to give a degree of base-bias to Tr6 and Tr7, to minimise cross-over distortion.

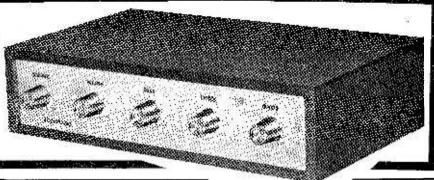
To prevent instability, decoupling networks R3-C2 and R9-C5 are interposed in the supply line between the major sections of the amplifier.

Construction

Start by cutting the Veroboard to size as shown in Fig. 3, and break the copper strips where indicated. Now drill the two mounting holes in the panel, drilling through from the copper side.

Next, wire up the components on the panel, and connect all leads where indicated. Note that all components are mounted vertically. Assembly is best carried out progressively, starting at the left

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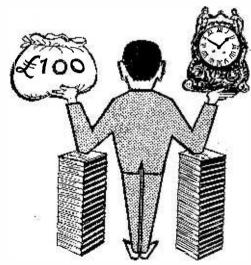
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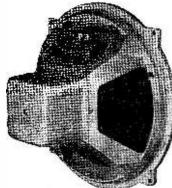
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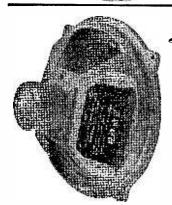


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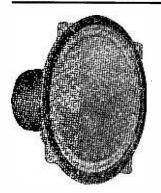


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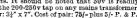
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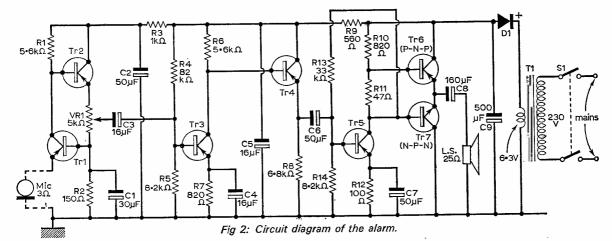
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R2	150 Ω	R7	820 Ω		Ω 100 Ω	
R3	$Ik\Omega$	R8	6-8kΩ		3 33k Ω	
R4	82k Ω	R9	560Ω	R14	4 8⋅2kΩ	
R5	8·2kΩ	RI0	820 Ω			
(all -	W 10% carb	on)				
) VRI	5kΩ log wi	th D.P	. switch			
Capac	itors:					
ČI	30μF 6V 50μF 12V	C4	16μF 12V	C7	50μF 12V	
C2	50μF 12V	C5	16μF 12V	C8	160μF 12V	
C3	16μF 12V	C6	50μF I2V	C9	500μF 25V	
	sub-min elect	rolytic	:)			
Semic	onductors:					
	Tr5 OC71					
	OC81					
	NKT774 or	simila	r n-p-n typ	e		
DI	Any small 🕹	-wave s	silicon rect	ifier capa	ble of passing	
	current up	to 200	mA at 20 p	o.i.v.		
	llaneous:	_				
6.3√	/ heater tran:	sforme	r; 3Ω m o vi	ng coil s	peaker; 25 Ω ,	
3in.	round, mo	ving c	oil speake	er; Vero	board; wire;	
sleeving; speaker gauze; nuts; screws; control knob; etc.						

hand side of the board and working through to the right. Heat shunts should be used when soldering transistors in place.

Once all wiring has been completed and a functional check carried out, drill the front panel to take the Veroboard, T1, VR1, etc. Drill the Veroboard at points 'A' and attach it to the front panel with a length of angle bracket. The front face of the front panel can be covered with a speaker gauze, securing it in place with Copydex. Bolt VR1 to the panel, and wire up as indicated. The speaker can be secured in place with Bostik, and then wired up. Finally, bolt mains transformer T1 in place, wire C9 and D1 in place and complete the rest of the wiring.

Since a low impedance 'microphone' is used, a very long and un-screened input lead may be used; a 20 yard input lead was used on the prototype.

The cabinet may be built from wood or metal, as preferred, but in either case corner brackets should be provided so that the front panel can be secured in place. When complete, the case can be covered with Fablon or a similar self-adhesive decorative plastic; a material with a dark wood grained finish was used on the prototype.

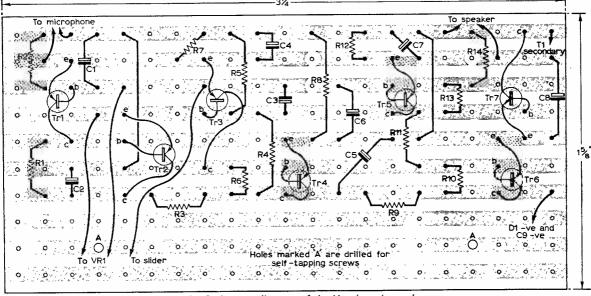


Fig. 3: Layout diagram of the Veroboard panel.



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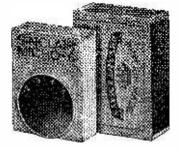
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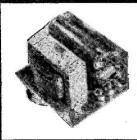
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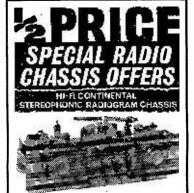
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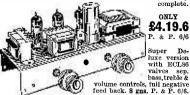
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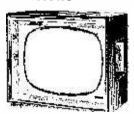
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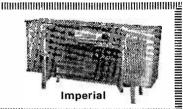
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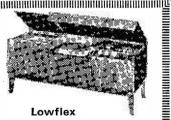
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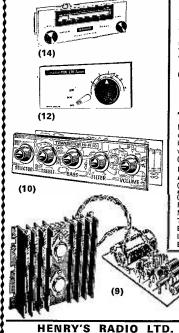
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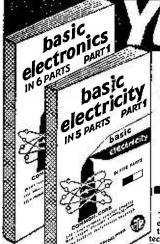












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PRACTICAL WIRELESS, OCTOBER 1966

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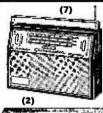
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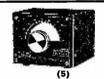
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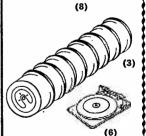
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