# PRACTICAL WIRELESS <br> AUGUST 1966 



## SOLDERING INSTRUMENTS AND EQUIPMENT



DESIGNED FOR THE AMATEUR'S RADIO STATION

## ILLUSTRATED

List No. $70 \frac{17}{8 \prime}$ BIT IN

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SHIELD
List No. 68
for catalogue apply direct to:-

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## the big name in PRECISION components

## MINIATURE AIR TRIMMER

Jackson type CI6 is a robust air di-electric trimmer of very small size. Suitable for use in high grade equipment. The standard component is designed for mounting on its base by two 10 BA (.07in.) clearance holes; two other forms provide for printed-
circuit mounting.

> Price $9 / 6$ each

Actual Size
$\star$ Capacitances: $2 \cdot 7-7 \cdot 5 \mathrm{pF}, 3-8 \mathrm{pF}, 3-11 \cdot 5 \mathrm{pF}$.

* Air gap 0.0075in.
$\star$ Length back to front 0.4 in . to 0.58 in .
$\star$ End area 0.375 in. square.
$\star$ Silver-plated brass vanes
$\star$ Siliconed ceramic insulation
$\star$ Beryllium copper rotor spring
* Temperature coefficient plus 50 p.p.m. per deg. C.

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| C. R. Bridge 62 | .. | $£ 9.6 .9$ |
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WIDE RANGE TRANSISTORISED AUDIO GENERATOR 63
$\star$ Range $10 \mathrm{c} / \mathrm{s}-100 \mathrm{Kc} / \mathrm{s}$
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$\star$ Accuracy \& Low Dist.

* Calibrated Output £17.1.9


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Valut III VALVES
GUARANTEED 3 MONTHS BY RETURN OF POST

Satisfaction or Money Back guarantee on goods if returned unused within 14 days. INSURANCE. POSTAGE 1 valve 9d., 2-11 6d. per valve. Free over i2.

| 1 L 4 | 2/3 | 6L6G | $7 /=$ | 30 F 5 | 8/3 | ECF80 | $7 / 6$ | KT61 | 11 | TDD4 | '7/ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1R5 | 4/9 | 6L18 | 7/9 | 30FL1 | 9/6 | ECFS2 | $7 / 6$ | KT63 | 5/9 | U18 | 7/6 |
| 1S4 | 4/9 | 6LD20 | 8/6 | 30L15 | 9/6 | ECH21 | 10/= | KT66 | 14/= | U22 | $6 / 9$ |
| 155 | $4 / 6$ | 6P25 | 11/- | 30P4 | $9 / 6$ | ECH35 | 11/- | KT88 | 21/- | U25 | $8 / 6$ |
| 1 T 4 | 3/- | 6P28 | $91-$ | 30P12 | $7 /$ | ECH42 | 8/6 | KTW61 | $5 / 9$ | U26 | 8/9 |
| 2D21 | $5 / 6$ | 6Q7G | 5/6 | 30PL1 | $9 / 3$ | ECH81 | 6/9 | KTW63 | 5/- | U35 | 12/6 |
| 3A5 | 6/- | 6Q'VGT | 8/9 | 3505 | 8/6 | ECH83 | 7/3 | KTZ63 | 7/- | U3'\% | $11 /$ - |
| 3Q4 | $5 / 3$ | 6SL7GT | 5/6 | 35LBGT | $81-$ | ECL80 | $5 / 9$ | MU14 | $7 /$ | U107 | 12/6 |
| 5U4G | 4/6 | 6SN7GT | 4/6 | 35 W 4 | 6/\% | ECL82 | $7 / 6$ | N37 | $9 / 6$ | U191 | $9 / 6$ |
| 5Y3 GT | $4 / 9$ | 6U4GT | 9/6 | 35Z4GT | 5/6 | ECL83 | $9 / 6$ | N78 | 13/- | U281 | $8 / 6$ |
| 5Z4G | $8 / 9$ | 6V6G | 4/6 | 50L6GT | 8/6 | ECL88 | $9 / 6$ | N108 | 13/- | U282 | 15/- |
| 5Z4GT | $9 / 6$ | 6V6GT | 5/9 | 80 | $5 /-$ | EF38 | $3 / 3$ | PC86 | 10/- | U329 | $15 / 6$ |
| 6/30L2 | $8 / 9$ $7 / 9$ | ${ }_{6 \times 4}^{6 \times 4}$ | 4/6 | 185BT | 9/6 | EF39 | 5/- | Pc97 | $7 / 6$ | U801 | 19/- |
| 6AK5 | $7 /$ | 6X5G | 5/- | 807 | 8/- | EF40 | 10/- | PCC84 | 6/6 | UABC8 | 6/6 |
| $6 \mathrm{AQ5}$ | 5/- | ${ }_{7 B 6}^{\text {6x5GT }}$ | 6/- | 955 958 | $2 / 6$ | EF41 | 8/- | PCC85 |  | UAF42 | $7 / 9$ |
| BAT6 | $5 /$ |  | 6/6 | AZ31 | 2/9 | EF50 | $3 / 8$ $4 / 3$ | PCC89 | 11/9 | UB41 | $8 / 6$ |
| 6BA6 | $5 / 6$ | $7{ }^{7} 5$ | $7 / 9$ | CBL31 | 19/- | EF85 | 6/3 | PCC189 | 11/= | UBC41 | $7 / 6$ |
| 68E6 | $5 / 6$ | ${ }^{7} \mathrm{C} 6$ | $6 / 9$ | CL33 | 9/- | EF86 | $7 / 6$ | PCF80 | 6/9 | UBC81 | $6 / 3$ $7 / 6$ |
| 6 BH 6 | 5/4 | ${ }^{7 \% \%}$ | 51. | CY31 | 7/6 | EF889 | $6 / 6$ | ${ }^{\text {PCF }} 82$ | $6 /-$ | UBF80 | 7/6 |
| 6 BJ 6 | 5/9 | ${ }^{7 / 5}$ | 14/6 | DAF96 | $7 / 3$ | EF991 | $6 / 6$ $3 /-$ | PCE86 | $8 / 3$ | UBFB | 7/6 |
| ${ }^{\text {BRR7 }}$ | 876 | ${ }^{\text {rY4 }}$ | $5 / \mathrm{m}$ | DF92 | 3/- | EF91 | $3 /-$ $3 /-$ | PCL82 | $7 / 9$ | UBL21 | $9 / 9$ |
| 6BW6 | 7/6 | 1001 | 11/- | DF96 | $7 / 3$ | EFP183 | 3/- | PCL83 | $8 / 9$ | UC92 | 6/9 |
| BBW 7 | 5/- | 10c2 | 12/6 | DK92 | \%/- | EF184 | 8/- | PCL84 | $8 / 3$ | UCC85 | $7 / 3$ |
|  | 5 | 10F1 | 7/6 | DK96 | $7 / 3$ | EL32 | $8 / 9$ | PCL85 | $8 / 6$ | UCF80 | 8/6 |
|  | 5/6 | 10LD11 | 14/6 | DL92 | 5/\% | EL33 | 11/- | PCL8 6 | 9/6 | UCH21 | $9 / 3$ |
| 6 69 | 11/\% | 10P18 | 8/6 | DL94 | 6/6 | EL34 | 11/- | PL38 | $8 / 6$ | UCE42 | $8 / 6$ $7 /$ |
| 60D6G | 17/3 | 10P14 | $9 / 6$ $4 / 9$ | DL96 ${ }^{\text {EAB80 }}$ | 7/3 | EL35 | 6/4 | PL36 | $8 / 9$ | UCL82 | 7/- |
| 6D6 | 3/- | 12AU' ${ }^{\text {12 }}$ | $4 / 9$ $4 / 9$ | EAB42 | $6 / 6$ $7 / 6$ | EL38 | 15/- | PL38 | 12/6 | UCL88 | 8/- |
| BF1 | 6/6 | 12AX ${ }^{\text {ch }}$ | 6/9-1 | EAF41 | 4/6 | EL41 | 8/6 | PL81 | 7/9 | UF41 | $10 /-$ $7 / 9$ |
| ${ }^{6 F 6 G}$ | $4 / 6$ | 12J7GT | 8/- | EB41 | 4/- | EL424 | $8 / 6$ $6 / 6$ | PL82 | 5/9 | UF42 | $6 / 9$ $6 / 9$ |
| 6 F 13 6 F 14 | 4/6 | 12K7GT | 8/- | EBC33 | 2/\% | EL84 | $6 / 6$ $7 / 1$ | PL88 | 6/- | UF85 | 7/6 |
| 6 F 15 | 9/6 | 12K8GT | $9 / 6$ | EBC41 | 6/6 | EM81 | $7 / 3$ | PY31 | \%/6 | UF89 | 5/9 |
| 6 F 23 | $8 / 6$ | 12Q7GT | 5/- | EBC81 | ${ }^{6 / 6}$ | EMP4 | 7/9 | PY32 | 9/- | UL41 | 8/6 |
| 6J5G | $3 / 4$ | 14 S 7 | 14/6 | EBF80 | 7/6 | EY51 | $7 / 6$ | PY33 | $91=$ | UL44 | 14/- |
| 6J5GT | 4/6 | 19AQ | 5/- | EBF89 | $7 /$ | EY86 | $7 / 3$ | PY80 | 5/9 | UL46 | $8 / 8$ |
| 6 J 6 | $3 / 3$ | 2001 | 819 | EBL21 | 10/6 | EY88 | $8 / 6$ | PY81 | 5/8 | UL84 | $6 / 9$ |
| 687G | 4/9 | 20F2 | $9 / 6$ | ECC40 | $6 / 8$ | EZ40 | 6/6 | PY82 | $5 / 6$ | UM80 | $9 / 6$ |
| 6J7GT | 7/9 | 20L1 | 16/- | ECC81 | 4/9 | EZ41 | 6/6 | PY83 | $5 / 9$ | UY21 | $8 / 9$ |
| $6 \mathrm{~K}^{\text {\% }}$ G | 1/6 | 20P1 | $9 / 6$ | ECC82 | 4/9 | EZ80 | $5 / 6$ | PY88 | 8/6 | UY41 | 6/- |
| 6K\%GT | 4/9 | 20P3 | 9/6 | ECC83 | 5/9 | EZ81 | $6 /-$ | PY800 | $8 / 6$ | UY85 | 5/6 |
| 6K8G | 3/- | 20P4 | $1{ }^{\text {r// }}$ | ECC84 | 7/- | FC4 | 8/- | PZ30 | $9 / 6$ | VR105 | $5 /-$ |
| 6 K 8 GT | 8/- | 25L6GT | $7 / 9$ | ECC85 | 5/6 | GZ32 | $9 / 6$ | SP61 | 2/- | VR150 | 5/- |
| 6 L 1 | 9/6 | 25Z4G | 6/6 | ECC88 | 9/- | GZ34 | 10/6 | T41 | $6 / 9$ | X66 | 7/9 |

## GRAM KITs

atochanger portable conzisting new 4 peed 10record BER UA14, superior quality ally fitted portable cabinet with BSR cutout, hes. gan 2 valve amplinex, Ho 10 speaker, knobs, cable nothing $\mathbf{8 9 . 1 0}$
else to buy normally 16 gns.
RADIOGRAM KITS-Modernise your old sram.

AM MONO New super all wave de luxe Amper heavy chassis. 4 speed VA14 $10^{\prime \prime}$ speaker.

2 AM/FM MONO. as above but $\quad \mathbf{~} 19$
AM STEREO as above with 2 H Flux $10^{r}$ speakers, stereo 819,19

FM STEREO as 3 but with FM band de-luxe push button controls. $\mathbf{2 2 5}$

## ELPICO MONO PREAMPS

DPA15. Latest black/satin chrome finish multiple input channels selector, base and reble controls. Matches all pickups and mikes. Provision tape record- 5 Gins.
ng. Normally 10 gns, our price

CAR RADIOS 8 Gns.
Latest Autolux fully transistorised complete with speaker and fittings. Large purchase enables us to sell these 14 gns.) at the amazing price of 8 Cns.

## ENORMOUS PURCHASE. GUARANTEED. APPROX, HALF PRICE.

## $\rightarrow$ TAPE $t$

We offeryou lully terisilised polyester/ mylar and F.V.G. tapes of identical quality hi-fi, wide range recording characteristics as top grade tapes. Quality control manufacture. They are truly worth a few more coppers than acetate, subustandard, jointed or cheap iznports. TRY ONE AND
Standard Plas
Standard Play Double Play $\begin{array}{lllll} & 150 \mathrm{ft} .2 / 8 & 3 \text { in. } & 300 \mathrm{ft} . & 4 / \pi \\ 4 \mathrm{in} . & 300 \mathrm{ft} . & 4 / 6 & 4 \mathrm{in} . & 600 \mathrm{ft} . \\ 8 /\end{array}$ 5in. $600 \mathrm{ft} 7 / 6$ 5im. $1,200 \mathrm{ft}$ 15/ $5 \frac{1}{2} \mathrm{in}$. $900 \mathrm{ft} .10 / 6 \quad 5$ in. $1,800 \mathrm{tt} .19 / 6$ 7in. 1,200it.12/6 7.n. 2.400ft. 27/m Long Play Triple Play $3 \mathrm{in} . \quad 625 \mathrm{ft} .2 / 9 \quad 4 \mathrm{in} .900 \mathrm{ft}, \quad 13 /-$ $4 i n . \quad 450 \mathrm{ft} .5 / 65 \mathrm{in} .1,800 \mathrm{it} .25 / \mathrm{F}$ 5in, $900 \mathrm{ft.10/6} \quad 5 \frac{3}{4} \mathrm{in} .2,400 \mathrm{ft} . \quad 34 / \mathrm{m}$ $5 \frac{3}{4}$ in $1,200 \mathrm{ft} .13 /=7 \mathrm{in} .3,600 \mathrm{ft} .44 /=$ 7in. 1,800ft. $18 / 6$
Postage 1/- reel 3 Quadruple Play Rost Free less $5 \%$ on three reels.

SPEAKER FABRIC
Superior Gold/Brown Yynide with smal। perforations, gift at $2 / 6 \mathrm{sq}$. ft. or $\quad 19$

1. sq . $\mathrm{It} .(4 \times 3)$ for only
100 HI-STABS ${ }_{100}^{10 \% \text { to } 5 \%} 9$ C0-AX. low lass, 6d. yd., 25 yds. 11/6; 100 RESISTORS SIZES 6/6 MICROPHONE CABLE. Highest quality black, grey, white, 9d. per yard.
100 CONDENSERS
$9 / 6$
Miniature Ceramic, Silver Mica. etc.
30 F to $1 \mu \mathrm{~F}$. LIST VALUE OVER \&勺े


Reproduction stands favourable comparison with tuners costing 3 times as much. Come and hear it (and compare it) at any of our branches or send to Brighton without delay as ze'e anticipate a very heavy denand.
This beautifully compact 6 transistor +3 diodes machine (size 6in. x $4 \mathrm{in} . \mathrm{x} 2 \frac{1}{2} \mathrm{in}$.) will give quieter, more interference-free reception. Frequency Range $88-108 \mathrm{~m} / \mathrm{cs}$. I.F. $10.7 \mathrm{~m} / \mathrm{cs}$. Sensitivity $10 \mu \mathrm{~V}$. imput for 10 mV output. Months of use from a standard 9 volt battery or its small power requirements can be drawn from any amplifier. Low noise frequency changer with smooth 2 gang tuning feeding no fess than three I.F. stages coupled to a double-tuned discriminator terminating in an L.F. stage giving ample output for all quality amplifiers.

## 15 Watt TUNERAMPLIFIER KIT

consisting of FMT41 tuner and the exceilent Sinclair zom (buit) together with it consisting oomplete vol on/off, treble and base component sets with complete connecting instructions and circuits.

## t13 19s.

or complete with AC mains power pack f1\%.18.6. Complete control kit only witb cirouits 25/-.

## avoid disappointment <br> ORDER NOW 88-10

## BARGAIN 71b. PARCELS

Including variable condensers, 1.f. coils, loudspeaker plugs/sockets, knobs, pots, condensers, resistors, nuts, boits, cabine nectics, switches, transiormer choke rectiner. transistors. List value $17 / 6$

Stockists of Leak, Quad, Chapman, Goodman, Armstrong, Tripletone, Linear, Rodgers, Trwox, Ferrograph, Wharfedale, eic., etc.
Post: $11 \mathrm{~b} .1 / 6,1 \frac{1}{2} 1 \mathrm{~b} .2 / 6,21 \mathrm{lb} .2 / 9,41 \mathrm{lb} .3 / 3,61 \mathrm{~b} .4 /-$ 14Lb. $5 / 6$.

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TRANSISTOR PLAYERS UA2588 Autochanger, 2 external inputs with hi-flux External exper socket controls, really de-luxe portable, large satin chrome control panel. 17 Gns. Normal price 25 gns.

## TRANSISTORS

$\begin{array}{llll}\text { Mullard Matched } & \text { Output } & 9 / 6\end{array}$ R.F. Kits OC44, OC45 (2) $9 / 6$

## GERMANIUM DIODES

General Purpose miniature Gold Bonded highest quality Individually tested $9 / 6$ doz.

## SILICON RECTIFIERS

Guaranteed performance. Top makes Tested 250 v , working.
 BRANDS ONLY, AND SUBJECT TO MAKERS' FULL GUARANTEE, PLEASE NOTE THAT WE DO NOT SELL ITEMS FROM USED EQUIPMENT NOR MANUFACTURERS' SECONDS \& REJECTS, WHICH ARE OFTEN DESCRIBED AS "NEW AND TESTED" BUT HAVE A SHORT AND UNreliable life. all valves are individually boxed and branded


## WE REQUIRE FOR PROMPT CASH SETTLEMENT ALL TYPES OF VALVES, LOOSE OR BOXED, BUT MUST BE NEW

ELECTROLYTICS. Can types: $8 \times 8 / 500 \mathrm{v} .616 ; 8 \times 16 / 500 \mathrm{v} .71$; $16 / 500 \mathrm{v}$. 51 -; $16 \times 16 / 500 \mathrm{v}$. $716 ; 16 \times 32 / 450 \mathrm{v}, 819 ; 32 / 500 \mathrm{v} .616 ; 32 \times 32 / 450 \mathrm{v} .61 /$;
 $100 / 275 \mathrm{v} .316 ; 100 \times 200 / 275 \mathrm{v} .816 ; 100 \times 200 / 350 \mathrm{v}$. $1616 ; 100 \times 200 \times 60 / 300 \mathrm{v}, 1616 ; 100 \times 300 \times 100 \times 16 / 275 \mathrm{v} .24 \mathrm{I} ; 100 \times 400 / 275 \mathrm{v} .1216 ; 100 \times 400 \times 16 / 275 \mathrm{v}$.

 Specials: $16 \times 16 \times 16 / 275 \mathrm{v} .6 / 2 ; 50 \times 50 \times 50 / 350 \mathrm{v}$. $1016 ; 2 / 150 \mathrm{v}, \times 500 / 25 \mathrm{v}$. $5 / 9 ; 8 / 600 \mathrm{v}, 8 / 9 ; 16 / 600 \mathrm{v} .12 /-; 47 / 450 \mathrm{v} .6 / 6$.


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## PE

Famous war-time "cats eye" used for seeing in the dark. This is an infra-red image converter cell with a silver caesium shereer which lights up
(like a cathode (like a cathode
ray tube) when the electrons re. the electrons re-infra-red strike it. A golden opportumity for some interesting experiments. 5/- each, post $2 /-$

## MAINS POWER PACK

MAINS POWER PACK designed to operate transistor sets and amplifiers. Adjustable output $6 \mathrm{~F} .-9$ to 12 volts for up to 500 mA (class B working). Takes the place of any of the following batteries. PR1, PP3, PP4, PP6, PP', PP9, and others. Kit and load resistor, 5,000 and 500 mfi . condensers, zener diode and instructions. Real snip at only 14/6, plus $3 / 6$ post.

SPEAKER BARGAIN
12in. High fidelity Iux flux permanent magnet type with either 3 or 15 ohm
speech coil. Will speech eoil.
handle up t
watts. Brand watts. Brand new Price $29 / 6$, built in tweeter $35 /$ plus $3 / 6$ post and

## ARDENTE HEARING AID

If not wanted as hearing aid these could be the
basis of radio control units-mocket uransmitterbasis of radio control units-pocket uransmitterunits and they contain many subminiature parts volume control with on/oft switch-inter-stage transformer-Mullard valves types DE 66 and DF 64 ( 2 of). All parts in good order, in fact hearing aids believed to be in working order but not guaranteed so-complete in plastic case with pocket clip only $2 \% / 6$ (earphone not included). MEDRESCO HEARING AIDS Also available similar condition to
believed working, only $18 /$ - each.

## THERMOSTATS

TYPE 'A' 15 amp for controlling room heaters, greenhouse, airing cupboard. Has spindle for
pointer knob quickly adjustable from $30^{\circ}-80^{\circ} \mathrm{F}$. pointer knob quickly adjustable from $30^{\circ}-80$. ${ }^{9} / 6$ plus $1 /$ post. Suitable box for wall mounting, TYPE ' ${ }^{\text {B }}$ ' $\mathbf{P}$. 15 amp. This is a 17 in . long rod type made by the famous Sunvic Co. Spindle adjusts this from $50-550^{\circ} \mathrm{F}$. Internal screw alters the setting so this could be adjustable over $30^{\circ}$ to $1,000^{\circ} \mathrm{F}$. Suitable for controlling furnace, oven, fire alarm, $8 / 6$ plus $2 / 9$ post and insurance. fire alarm, 8/6 plus $2 / 9$ post and insurance. and out at around freezing point. $2 / 3$ amps. Has many uses, one of which would be to keep the loft pipes from freezing if a length of our blanket
wire (16 yds. 10/-) is wound round the pipes. $/ 6, P . \&$ P. $1 / 1$.
TYPE ' 'E' This is a standard refrigerator thermostat. Spindle adjustments cover normal refrigeraor temperature, $\% / 6$ plus $1 /-\mathrm{P} . \& \mathrm{P}$.
TYPE 'F' Glass encased cor controlling the temp. of liquids-particularly those in glass tanks, vats
or sinks-thermostat is held (half stbmerged) by or sinks-thermostat is held (hali submerged) by developers and chemical baths of all types. developers and chemical baths of all types.
Adjustable over range $50^{\circ}$ to $150^{\circ} \mathrm{F}$ - price 18/plus $2 /-$ post and ins.

## TWO WAY RADIOS

 Give communication over $\frac{1}{4}$ mile. $\int$ controlled, built-in telescopic $;$ aerial-press button operationPP3 batteries-pair instruments complete and ready to use $£ 7.9 .6$ lus $5 /-$ post and insu, 4.
-Three Unusual Items-m OZONE OUTFIT-for removing smells and generally improving any oppressive atmos-
phere. Kit consists of Philips Ożone Lamp phere. Kit consists of Philips Ożone Lamp
and mains unit, only needs box, 19/6 plus 6/6 carr. and ins.
BLACK LIGHT UNIT. BLACK LIGHT UNIT, 40 watt intensity,
comprises lamp, lamp holder and 40 watt comprises lamp, lamp holder and 40 watt
choke. Only $19 / 6$ plus $6 / 6$ carr, and choke. Only 19/6 plus $6 / 6$ carr. and ins.
TIMER KIT. Special oiter of all components TIMER KIT. Special oiter of all components interval timer for photography etc. 12/6 plus post $2 / 6$.

[^1]
## STUPENDOUS OFFER-£II for $\mathbb{E}$

The Princess superhet described below is a very fine little set that has been carefnly designed for
high periormance. Only recently
(under another name of course) this was on offer in many radio hops, for $£ 10.19 .6$, but we hare been fortunate in obtaining the parts at a very low price and now pass this saving on to you. If you act quickly you can pur-
chase this tor only $39 / 6$ plus $3 / 6$ chase this for only $39 / 6$ plus $3 / 6$
post and insurance. Note these post and insurance. Note these
features: $\theta$ Long and Medium Wave Long clear dial with traveling pointer and slow mo-
tion drive Push pull output approx mately $350 \mathrm{~m} . \mathrm{w}$. A.V.C. and feed back
 Wigh colectivity ferrite. transiormers
For fool-proof assembly Eerial Sily tested transistors Printed circuit board or Aconomy output circuit gives long life from PPs You get over 100 parts (list value over $£ 10$ ). In fact everything you need and easy to follow wring and aligning instructions. Don't miss this wonderiul offer, Make up several while you have the chance. Use them as presents and you'dl
be Ioved for ever. Made up chassis $10 /$. extra. Battery $1 / 9$ extra. Data be Ioved for ever. Made
purchased separately $2 / 6$.


## 750 mW TRANSISTOR AMPLIFIER

4 transistors including two in push-pull input for crystal pick-up-feed back loops-

Price 19/6
Post and insurance $2 / 6$.
Speakers 3in. 12/6; 5in. 13/6; Bin. $\times 4$ in. $14 / 6$.
THIS MONTH'S SNIP

## A MOVING COIL METER BARGAIN

Panel meters are always being needed and they are jolly costly when you have to buy them in a hurry so you should take advantage of this offer: 2 in. moving coil tlush mounting meters onty $5 / 6$ each or $48 /-$ a dozen unused and in makers
boxes. These are actually R.F. meters and oost about $£ 3$ each but if you don't want them for R.F. then all you have to do is to remove the thermo couple and You will have a $2-3 \mathrm{~m}$. . meter which you can rake into almost anything by adding shunts or series resistor. These are ex-government, of course.


## CORONET PARCEL

Here's a bargain for you-parcel comprises: plastic case, printed circuit earphone socket and plastic carrying case all for $8 / 6$ plus $1 / 6$ post.


## SELF REPAIRING FUSES

Sounds good doesn't it-we can't offer quite that but we can offer a fast acting overioad trip which will save you having to repair fuses every time you do would instal this on or near your bench all you do is to switch on again. Thyis is made by Westinghouse. Regular price about $£ 10$ each. We offer them this month at 29/6, plus $5 /-$ post and insurance. Not many in stock so hurry or you will be too late.

## Your last chance to buy one of these

## 125 watt MERCURY VAPOUR

SPOT LAMP In addition to the normal uses in photography and lighting generally you will find that a spot light shining over your shoulder is a circuits. This month due to a fortunate purchase we are able to ofier a complete "Philips" outfit for about one fifth of its proper price thus showing you a saving of $80 \%$. The outfit comprises 125 watt $8 P O T$
LAMP (gives approx. samelight as an watt ordinary lamp) LAMP (Gives approx. same light as 000 watt ordinary lamp)
-Polyester filled choke-starter and adjustable mounting -Polyester filled choke-starter and adjustable mounting soiled only $37 / 6$ plus $6 / 6$ post and insurance.

## SUMMER SALE

## BARGAINS UNLIMITED

TAPE DECK BARGAIN. 240v. Maing motor with capstan and heavy flywheel to drive the tape at a very steady $3 \frac{3}{4}$ i.p.s. Mounted on deck with high 2 tape head - the deok is shaped to taire \& Redi spindles to take normal suols enclosed in a metal box, with carrying handle mains neon indicator, voltage adjustment panel and various input and output sockets. Size of the box is $11 \frac{1}{2} \times 10 \frac{1}{2} \times 7 \mathrm{in}$. and there is plenty o room for an amplifier-this looks just the right unit for anyone wanting to make a playback machine, telephone aniswerer etc. A limited quantity oniy of these, price $37 / 6$ plus $7 / 6$ post and insurance.
MINIATURE RELAYS with removable covers Fery sensitive (will close on only 20 mA ). Goil triple set for change over pair to open circuit and the third pair to close circuit--perfect order unused (removed from equipment), $\geqslant / 6$ each MAINS TRANSFORMER. Upright mmunting wit primary tapped $200,220,240 \mathrm{v}$. H.T. secondary secondaries of 6.3 v . 1) $\frac{1}{2}$ amp-unused removed from equipment $)$, $15 /-$ plus $3 / 6$ post and insurance
MOLLARD SILICON RECTIFIER. 350 v .100 mA Removed from unused equipment, perfect. Ref BY100, $4 / 6$ each.
SOUND POWERED INSERTS. These are very delicately made units and work well either as microphones or loudspeakers-mount them on suitable boxes and you will be amazed how maintenance. Cost from need no batteries or Our price while stocks last is $5 / 6$ each.
REED SWITCHES. A pair of contacts sealed into a glass tube. When a magnet comes clese the contacts close immediately and the circuit is switohed. For burglar alarms on doors or win-dows-moving displays for advertisiag-rev. or batch counting-relay ciroults. New end perfect, price is $6 / 6$ each
MEG POTS.
$\frac{1}{2}$ MEG POTS. By Erie, standard $\frac{1}{4} \mathrm{in}$. spindle, lin. long. Md. each in doz. lots otherwise 10d. $\frac{1}{2}$ MEG POTS WITH D.P. SWITCH. Again by
Erie. Standard size spindle lin. length. 10d, each
in doz. lots otherwise $1 / 3$ each.
MINIATURE PICK-VP. For pop records-this is made by Cosmocord-has a crystal cartridge and long piay sapphire stylus-offered for less than 3/9 each or $36 /-$ doz
SYNCHRONOUS METER MOTOR. This is self starting and has a cog ended spindle-add a train of gears and you have a clock or hours elapsed meter, or it would drive a fittle fan to keep equipment cool or similar job. Brand new and periect $5 / 6$ each BUI-per doz
delicate thermostats or other low curro switches, delicate thermostats or other low current devices
to control up to 30 amps ideal to switch thermal storage heaters-motors etc., made by the famous A.E.I. group these are listed at e25 each-yon can buy if you hurry at a rery keen price of $39 / 6$ each and we will include diagrams and data. Mounted on panel size approximately $6 \times 7 \times 2 \mathrm{in}$. deep. MAINS FROM CAR BATTERY. Rotary genera. tors 12 v . imput, 240 v . output, $110 \mathrm{~mA}, 40 /$ H.R.O. POWER PACK
H.R.O. POWER PACK, Suitable 240 or 115 volt mains give 250 v. H.T. and $6.3 \nabla$. L.T. Unused OU DD. AMMETER A.C./D.C. AMMETER.
0.9 amps. but external shunt easily removed. Offered at silly price, $8 / 6$ each, 15 doz. 'C' CORE POTTED OUTPUT TRANSFORMER. Made by the famons "Parmeko" company these are the best money can buy-we can offer a bargain 15 watt rating, centre tapped primary with secondary for 3 ohm speaker. Potted and in black stove enamelled case for upright mounting these will make your amplifier or rig look perfect at only $12 / 6$ plus $3 / 6$ carriage and insurance' $\mathbf{c}$ ' CORE MAINS TRANSFORMER.

We hare " "arly Bid" Companion to be a case of the "Early Bird". Companion to the with 5 v . adjustments and tapped at 115 v . -the secondary is rated at $625-0.625-250 \mathrm{~mA}$ with a tapping for $3 \cdot 25-0-325$ at 150 mA —so it's a big 8410 s . each plus $10 /$ carriage and insurance. 6.3 v . HEATER TRANSFORMERS, $1 \frac{1}{2}$ amps, $5 / 6$. FLEX CABLE 14/86. Twin figure 8 -brownideal for most mains leads and flex extensions, COMPLETE FLDORESGENT FITTINGS. These are nicely made in white enamelled metal and are complete with tube ready ior immediate use. 2 it. 20 watt $37 / 6$ plus $6 / 6$ post and insurance.
3 ft. 40 watt $38 / 6$ plus $8 / 6$ post and insurance. 4 ft .40 watt $39 / 6$. 5ft. 80 watt $55 / \mathrm{m}$. These last two unfortunately we cannot dispatch-they are only for callers. This is due to the difficulty we have in packing these so that they do not get FLmashed up in trans
amphold 20 watt 19 , 0 wat $10 / 6$ plus 3.6 post and insurance.
80 watt 22/6 plus $4 ; 6$ post and insurance.


TRANSISTOR MIXER, Model TM-1. A must for the tape enthusiast. Four channels. Battery operated. Similar styling to Model AA-22U Amplifier. Kit £11.16.6 Assembled £16.17.6

20+20W TRANSISTOR STEREO AMPLIFIER. Model AA22U. Outstanding performance and appearance. Kit £39.10.0 (less cabinet). Attractive walnut veneered cabınet £2.5.0 extra. Assembled £59.15.0

GARRARD AUTO/RECORD PLAYER. Model AT-60, less cartridge £13.1.7. With Decca Deram pick-up £17.16.1 incl. P.T, Many other Garrard models available, ask for Lists.

HI-FI MONO AMPLIFIER. ModeI MA-5. A general purpose 5W Amplifier, with inputs for Gram., Radio. Modern functional appearance. Kit £11.9.6 Assembled £15.15.0

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HI-FI MONO AMPLIFIER. Model MA-12. 10W output, wide freq. range, low distortion. Use with control unit. Kit £12.18.0 Assembled £16.18.0 3+3W STEREO AMPLIFIER. Model S-33. An easy-to-build, low cost unit. 2 inputs per channel. Kit £13.7.6 Assembled £18.18.0
DE LUXE STEREO AMPLIFIER. Model S-33H. De luxe version of the S-33 with two-tone grey perspex panel, and high sensitivity necessary to accept the Decca Deram pick-up. Kit £15.17.6 Assembled £21.7.6
HI-FI STEREO AMPLIFIER. Model S-99. $9+9$ W output. Ganged controls. Stereo/Mono gram, radio and tape inputs. Push-button selection. Printed circuit construction. Kit £28.9.6 Assembled £38.9.6
POWER SUPPLY UNIT. ModeI MGP-1. Input 100/120V, 200/250V, $40-60 \mathrm{c} / \mathrm{s}$. Output $6.3 \mathrm{~V}, 25 \mathrm{~F}$ A.C. $200,250,270 \mathrm{~V}, 120 \mathrm{~mA}$ max. D.C.

Kit £5.12.6 Assembled £7.2.6

## FOR THE INSTRUMENTALIST

TRANSISTOR PA/GUITAR


PA-2 AMPLIFIER, PA-2. 20 Watt amplifier. Two heavy duty speakers. Four inputs. Two channels. Variable tremolo. Speed and depth controls. Weight 51 lb .
$18^{\prime \prime}$ high $\times 29^{\prime \prime}$ wide $\times 10^{\prime \prime}$ deep.
Kit £44.19.0 Assembled £59.10.0
VALVE PA/GUITAR AMPLIFIER, PA-1. 50 Watt amplifier.

Kit £54.15.0 Assembled £74.0.0
Castors or legs available as extras.
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## TRANSISTOR RECEIVERS


"OXFORD" LUXURY PORTABLE Model UXR-2. Specially designed for use as a domestic or personal portable receiver. Many features, including solid leather case. Kit £14.18.0 incl. P.T.

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"MOHICAN" GENERAL COV. RE= CEIVER for Amateur or Short Wave listening. Send for leaflet.

Kit £37.17.6 Assembled £45.17.6

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Kit £23.18.0 Assembled £31.18.0 5" GEN.-PURPOSE OSCILLOSCOPE. Model 10-12U. An outstanding model with professional specification and styling. " $Y$ " bandwidth $3 \mathrm{c} / \mathrm{s}-4.5 \mathrm{Mc} / \mathrm{s} \pm 3 \mathrm{~dB}$. T/B $10 \mathrm{c} / \mathrm{s}-$ $500 \mathrm{kc} / \mathrm{s}$. Kit £35.17.6 Assembled £45.15.0
DE LUXE LARGE-SCALE VALVE VOLTMETER. Model IM-13U. Circuit and specification based on the well-known model V-7A but with many worth-while refinements. $6^{\prime \prime}$ Ernest Turner meter. Unique gimbal bracket allows operation of instrument in many positions. Modern styling.

Kit £18.18.0 Assembled £26.18.0


OS-2

M, IM-13U

AUDIO SIGNAL GENERATOR. Model AG-gU. $10 \mathrm{c} / \mathrm{s}$ to $100 \mathrm{kc} / \mathrm{s}$, switch selected. Distortion less than $0.1 \%, 10 \mathrm{~V}$ sine wave output metered in volts and dB's.

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VALVE VOLTMETER. Model V7-A. 7 voltage ranges d.c. volts to 1,500 . A.C. to 1,500 r.m.s. and 4,000 peak to peak. Resistance $0.1 \Omega$ to $1,000 \mathrm{M} \Omega$ with internal battery. D.C. input resistance $11 \mathrm{M} \Omega$. dB measurement, has centre-zero scale. Complete with test prods, leads and standardising battery.

Kit £13.18.6 Assembled £19.18.6
MULTIMETER. ModeI MM-1U. Ranges $0-1.5 \mathrm{~V}$ to $1,500 \mathrm{~V}$ a.c. and d.c.; $150 \mu \mathrm{~A}$ to 15 A d.c. $; 0.2 \Omega$ to $20 \mathrm{M} \Omega$ $4 \frac{1^{\prime \prime}}{} 50 \mu \mathrm{~A}$ meter, Kit £12.18.0 Assembled £18.11.6 R.F. SIGNAL GENERATOR. ModeI RF. 1U. Up to $100 \mathrm{Mc} / \mathrm{s}$ fundamental and 200 $\mathrm{Mc} / \mathrm{s}$ on harmonics. Up to 100 mV output.

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SINE/SQUARE GENERATOR ModeI 1G-82U. Freq. range $20 \mathrm{c} / \mathrm{s}-1 \mathrm{Mc} / \mathrm{s}$ in 5 bands less than $0.5 \%$ sine wave dist. less than $0.15 \mu \mathrm{sec}$. sq. wave rise time.

Kit £25.15.0 Assembled £37.15.0


IG-82U
Prices and specifications subject to change without notice


HI-FI FM TUNER. Model FM-4U. Available in two units, R.F. tuning unit (£2.15.0 incl. P.T.) with I.F. output of $10.7 \mathrm{Mc} / \mathrm{s}$ and I.F. amplifier unit, with power supply and valves (£13.13.0). Total Kit £16.8.0

STUDIOMATIC "363"' TAPE DECK. The finest buy in its price range. Operating speed: $1 \frac{77^{\prime \prime}}{}, 3 \frac{34^{\prime \prime}}{}$ and $7 \frac{1}{3}^{\prime \prime}$ p.s. Two tracks, "wow" and "flutter" not greater than $0.15 \%$ at $7 \frac{1}{2}$ " p.s. £13.10.0 With TA-1M Tape Pre-amplifier kit £31.5.6

HI-FI AM/FM TUNER. Model AFM-1. Available in two units which, for your convenience, are sold'separately. Tuning heart (AFM-T1-£4.13.6 incl. P.T.) and I.F. amplifier (AFM-A1£22.11.6). Printed circuit board, 8 valves. Covers L.W., M.W., S.W., and F.M. Built-in power supply.

Total Kit £27.5.0


TRUVOX D-93 TAPE DECKS. High quality stereo/mono tape decks. D93/2, $\frac{1}{2}$ track, £36.15.0 D93/4, $\frac{1}{4}$ track, £36.15.0

TAPE RECORDING/PLAYBACK AMPLIFIER. Thermometer type recording indicators, press-button speed compensation and input selection.
Mono Model TA-1M. Kit £19.18.0 Assembled £28.18.0 Stereo Model TA-1S. Kit £25.10.0 Assembled £35.18.0

MONO CONTROL UNIT. Model UMC-1. Designed to work with the MA-12 or similar amplifier requiring 0.25 V or less for full output. 5 inputs. Baxandall type controls. Kit £9.2.6 Assembled £14.2.6

STEREO CONTROL UNIT. Model USC-1. Push-button selection, accurately matched ganged controls to $\pm 1 \mathrm{~dB}$. Rumble and variable lowpass filters. Printed circuit boards. Kit £19.19.0 Assembled £27.5.0


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HI-FI SPEAKER SYSTEM. Model SSU-1. Ducted-port bass reflex cabinet "in the white". Two speakers. Vertical horizontal models with legs, Kit £12.12.0, without legs, Kit £11.17.6 incl, P.T.

The BERKELEY SLIM-LINE SPEAKER SYSTEM, fully finished walnut veneered cabinet for faster construction. Special $12^{\prime \prime}$ bass unit and $4^{\prime \prime} \mathrm{mid} / \mathrm{high}$ frequency unit. Range $30-17,000 \mathrm{c} / \mathrm{s}$. Size $26^{\prime \prime} \times 17^{\prime \prime}$ only $7 \frac{a}{a}^{\prime \prime}$ deep. Modern attractive styling. Excellent value. Kit £19.10.0 Assembled £24.0.0

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Kit £25.12.0 Assembled £33.17.0
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A wide range available including kits, ready assembled cabinets or assembled and fully finished cabinets, for example:
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Malvern


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## "AMATEUR" EQUIPMENT

$\mathbf{8 0 - 1 0 m}$ TRANSMITTER, DX-40U. Power inputs 75 W . C.W., 60 W peak CC phone. Output 40 W to aerial. Provision for VFO.

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DX-40U


RA-1

## COMMUNICATIONS TYPE RECEIVER. ModeI

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## TO H

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THE SKYROVER De Luxe
7 transistor plus 2 diode superhet， 6 wave－ Mandium Wortable receiver covering the full $3 I-94 \mathrm{M}$ and also 4 separate switched band spread ranges． 13 M ．， 16 M ．， 19 M ．，and 25 M ．， with Band spread Tuning for accurate Station Selection．The coil pack and twing heart is completely factory assembled， wired and tested．The remaining assembly can be completed in under three hours from our easy to follow，stage by stage instruc－ Transistors and Diode．Uses．AI T2 Mullard Transistors and Diode．Uses 4 U2 batteries． bin．Ceramic Magnet P．M．Speaker．Easy to Aerial and Ferrite Road Aerial．Tone Circuit is incorporated，with separate Tone Control in adaition to Folume Control． Tuning Control and Waveband Selector． In a wood cabinet，size 11⿱⿻丷木女⿱⿰㇒一乂心，$x 6 \frac{1}{2} \times 3$ in． covered with a washable material，with plastic trim and carrying handle．Car aerial socket fitted．
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Permeability tuned－covering 87 to $108 \mathrm{Mc} / \mathrm{s}$ ．For use with one ECC8 case，size $3 \times 2 \frac{1}{2} \times 1 \frac{1}{2}$ in．Circuit supplied．
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LASKY＇S PRICE 291

## THE NEW GARRARD STEREO DECK

Now available from stock－superb specifi－ cation：three $\frac{1}{4}$ track stereo／mono heads； 3 speeds－1委， $3 \frac{3}{4}, 7 \frac{1}{2}$ i．p．s．；takes 7in．spools； fast forward and rewind；tape position indicator；pause control；separate record， replay and erase heads－4 tracka；piano key start can be remotely controlled；anto，tape－ start can be remotely controlled；auto，tape－ and rua，large dynamically balanced fy－ wheel．Deck finished in grey plastic，size： $14 \frac{1}{2} \times 12 \times 6$ in．，depth below plinth $4 i n$ ．For 110 v ． 00 c．p．s．Mains operation．Auto－ transformer for $200 / 250 \mathrm{v}$ ．included tree． GNS．

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## 363 TAPE DECKS

The very latest 3 speed model－ $1 \frac{7}{8}, 3 \frac{3}{4}, 7 \frac{1}{2}$ ips，available with either $\frac{1}{2}$ track or $\frac{1}{2}$ trol；digital counter；fast forward and re－ wind；new 4 pole fuily screened induction motor，interlocking keys．Size of top plate $13 \frac{1}{2} \times 11 \mathrm{in}$ ． $5 \frac{1}{1} \mathrm{in}$ ．deep below unit plate． For $200 / 250 \mathrm{v}$ ．A．C．mains， 50 cps operation New，unused and fully guaranteed．
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## SPECIAL BARGAIN－＂THE ARROW＂ PORTABLE DICTATION／TAPE RECORDER



High Quality British Manufacture：Fully transistorised single control lever feassette takes 3in．spools giving $2 \times 22$ mins．twin track recording and 31 in ．spools giving up to $2 \times 30$ mins．）Volume control －Accidental erasure safety device Fast rewind －Operates on 4 U2 type batte．Strong two－ tone plastic case size $9 \mathrm{in} . \times 6 \mathrm{in} . \times 3 \frac{1}{2} \mathrm{in}$ ．，with trans－ parent cover．Fully guranteed ©omplete with all these accessories：＊．Gassette with 3in．spools and tape．＊．Microphone with lapel clip and remote pause control（doublea as speaker on replay）．＊． ＊．Foot Switch．＊．Desk speaker．＊Reference pad． List price $£ 3$ ．
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Carriage 5／－． 4 long ］ife Rayovac Batt．6／－extra．


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HIGH QUALITY EQUIPMENT CABINETS
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LATEST MULLARD TRANSISTORS, AD149. ADIU, EQUALISATION to Standard R.I.A.A. and C.C.I.R Characteristics for Gram and Tape Heads.
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Head 2.5 mV . Radio/Aux or Ceramic P.U. 10 mV . FREQUENCY RESPONSE: $20-20,000$ c.p.s
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NEGATIVE FEEDBACK: 52dB.
Complete Kit of parts with full constructional Complete Kit of parts with full constructional
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Both types post and pucking 1/-per reel. Four or more Spaze spools, SPECLAL OFFER Internationally branded acetate tape, Fin. reel, 1200 ft giving 80 minutes per track at $3 \frac{3}{4}$ i.p.s.
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A really versatile instrument that makes a handy pocket-size tool. Measures AC or DC voltage in three ranges of $0-15-150-1000 \mathrm{~F}$. Resistance 0-1000,000 ohms and Current $0-150 \mathrm{~mA}$. DC. Size only 3; x $21 \times 1$ in. with ingenious dial design providing a clear, easily read scale. Complete with battery and test leads.

## Dah Dit Dah!

MENEVER you hear the cry "Down with Morse" you can be sure that within arm's reach is a frustrated character with an RAE pass wondering if N is dit-dah or dah-dit and proclaiming that the Morse Test is a creaking anachronism maintained simply to thwart would-be radio amateurs.

Superficially there may be a case for confining the Morse Test to limbo, for many prospective amateurs feel no affinity with c.w. It is understandably galling for an enthusiast who wants to use 'phone to find that if he is unwilling to reach his 12 w.p.m. he must be restricted to the nether regions of the $440 \mathrm{Mc} / \mathrm{s}$ band.

And the existence of a reserve of amateur c.w. operators who could be called in for emergency duties (and which proved so valuable in 1939) is no longer important owing to the shift in military communications techniques and practices.

Even so, we not only support the continuance of the Morse Test but positively encourage a wider use of c.w. even to the extent of desiring every amateur station to devote some time to it.

The simplest way to get on the air is via a small c.w.-only transmitter and the surest path to success is to learn the rudiments with small gear and progress step by step to more complex rigs. Also, the range of c.w. is much greater than telephony and simple gear can give satisfactory results for the probationary ham.

Furthermore, letting a newcomer loose with a microphone is like throwing a Christian to the lions! Exposed to the ponderous drivel that passes for conversation on some sections of the amateur bands, he will start off on the wrong foot. But on c.w., he will better learn how to operate a station efficiently. Morse demands economy of message information, encourages snappier communications-and the language barrier does not exist. He will also be spared such delights as having Aunt Maude rip off a few gems on the weather conditions in Scunthorpe on the EL-key!

To mix a metaphor or two, the amateur with his L-plates up will find that a good long baptism of key bashing wins hands down. And so, to those inventing elaborate curses for the shade of Samuel Morse we say: keep at it-you may even, like Dr. Strangelove, learn to stop worrying and love the Code!
W. N. STEVENS, Editor
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[^3]
## Save the Grand Old Sets

I Was interested in P. J. Plater's letter in the News and Comment of the June issue of Practical Wireless. I, myself, have restored many of these sets, with very little trouble and expense, which in the normal course of events would have found their way to the rubbish dump.

One in particular which I came by some three years ago is still going well and has earned me QSL Cards from all over the world, and apart from its performance, is a lovely piece of furniture and the tone quality is outstanding. I do most of commercial DX'ing on the "old faithful" as I have named it. It compares exceptionally well with the modern outfit I must -say. A new valve and variable resistor were the only requirements to restore it to perfect working order
H. S. Barker.

## Dalton-in-Furness, <br> Lancashire.

## The Radio Collector

I FOUND the article "The Radio Collector" in the June issue of Practical Wireless extremely interesting, as I took up radio as a hobby in the early 1920's.

I now have many copies of various wireless magazines, including Practical Wireless of the 1920's and 1930's for disposal. I also have valves, components, catalogues, etc., of that period.

If any readers are interested, please would they send me a stamped, addressed envelope and I will let them have further details.
E. Latham.

45, Beech Road,<br>Radstock,<br>Bath, Somerset.

## Tape Exchange

I will be pleased to exchange tapes with any of the old timers among Practical Wireless readers, who are still active short wave listeners, no matter what types of receivers are in use. Should there be any H.R.O. users, their tapes will be very welcome. My tape recorders are four track, $5 \frac{3}{4}$ in. spools with speeds of $3 \frac{3}{4}$ i.p.s. and $1 \frac{7}{8}$ i.p.s. Let me know receivers used, aerials, results on amateur 'phone and short wave broadcast bands, and the extent of Loran QRM on top band if any. Three-inch letter tapes only, please. A. W. Маид.

## 62, Costa Street, Middlesborough.



The latest in the Advance range of five voltmeters is the Advance VM76 which extends the range of voltmeters to include a.c. frequencies in excess of $1000 \mathrm{Mc} / \mathrm{s}$ and d.c. measurements up to 1000 V with accuracies of $\pm 2 \%$ up to 100 V .
Push-button selection of the various functions is a natable feature of this instrument. In d.c. operation this method can be used to select centre-zero readings and either positive or negative polarity. Resistance measurements between $0.02 \Omega$ and $500 \mathrm{M} \Omega$ to an accuracy of $\pm 5 \%$ at midscale can be selected in a similar way. The VM76 is available from Advance Electronics Ltd., Roebuck Rd., Hainault, llford, Essex, at a price of $\mathbf{E 9 0}$.

## SUBMINIATURE 300mW AMPLIFIER

Messrs. L.S.T. Components have informed us that due to import difficulties the GA02 is not available, but they are able to supply the following specified devices:
TrI, Tr2, OC45 (Mullard) 5s. 2G374 (Texas) 3s. Id. 2G374 (not coded) 1s. Tr3, 2 N 1305 (Texas) 6s. 9d. 2NI305 (not coded) 2s. 6d. Tr4, 2 N1304 (Texas) 6s. 9d. 2 N 1304 (not coded) 2s. 6d.

One shilling post and packing should be added, unless all four devices are ordered, when postage is free.

All enquiries are to be forwarded to the company's new address, 23 New Road, Brentwood, Essex, AND NOT to Benfleet.

## ULTRASONIC Tx/Rx

From Beulah Electronics Ltd., 126 Hamilton Road, London, S.E.27, comes the Nuray Ultrasonic Transmitter/Receiver. It consists of two units; an ultrasonic transmitter and a receiver. The range of the equipment is up to 30 feet. Uses include batch counting, burglar alarm, garage door opening and electronic control systems. The units measure $4 \frac{1}{2} \mathrm{in} . \times 2 \frac{1}{2} \mathrm{in} . \times 3 \mathrm{in}$. and the price of the battery-operated model Bo/l (set of transmitter and receiver) is $£ 19$ 19s. There is a mains-operated model, Mo/l which costs $£ 26$ for the set of transmitter and receiver.

# ...COMMENT 

## SWITCHES AND COMPONENTS MADE TO ORDER

Elmbridge Instruments Ltd., West Molesey Trading Estate, Surrey, have started a comprehensive component service for the home constructor.

This service makes available small quantity packs of professional electronic components, including carbon film resistors, polyester capacitors, rechargeable nickel-cadmium cells, pushbutton and rotary switches, to home constructors who have found it difficult in the past to obtain direct from the component industry.

The photograph shows a DEAC Ni-Cad cell, of which Elmbridge Instruments Ltd., market the PP3, U2, U7 and UII equivalents.


EMI HELPS TO TRAIN POLARIS CREWS
EMI Electronics Limited is taking an active part in the Royal Navy's Polaris project. The company is responsible for part of the electronic equipment used for crew training at the Submarine Base at Faslane in Scotland.

EMI engineers spent some time studying the design of training simulators at the California factory of the Hughes Aircraft Corporation, after which, they tuned the equipment at Faslane and are now training Naval personnel in its use and maintenance.

## WELLER "MARKSMAN" SOLDERING IRON

Shown in the photograph below is the latest addition to the Weller range of soldering irons. It is the "Marksman", a small light-weight model that fits easily in the hand and can be used for hours without fatigue. It is rated at 25 W and takes a variety of screw-in tips made of nickel-plated copper. Voltage rating is 240V. The "Marksman" is supplied in a vinyl pouch and costs El 9 s. A "Marksman" kit, containing iron, 60/40 solder, two spare bits, and a soldering aid, is available ot tl 18 s .


## Who Wants To Sell?

As a regular reader now of Practical Wireless, I should like to purchase back-numbers, bound or otherwise, of Practical Wireless, "Practical Electronics" and "Radio Constructor" for a reasonable sum. Freight will be paid and all letters of offer will be answered. A cheque from a British bank (Westminster) will be sent to the seller.
John Lawn.

Shek Kwu Chau,<br>c/o Cheung Chau Post Office,<br>New Territories,<br>Hong Kong.

## Can Anyone Help?

Can any reader help me in finding the number of a four-pin base rectifier valve used in an old Pilot 7 -valve set (the type with a magic eye, model number possibly H.G. 56263, covering l.w., m.w. and s.w.) and possibly the heater voltage. The other valve numbers are as follows: Brimar 6D6, 6D6, Pilot 6A7, 42, Mullard 75 and the magic eye 6G5.
G. Wright.

Bankhead House, Tranent,
East Lothian, Scotland.

## Congratulations

Congratulations on your "new look" magazine also the idea of the free booklets which I have found very useful indeed.

I have taken Practical Wireless from the first issue and I am now 62 years old. I may be one of your oldest readers, but I still look forward each month to my issue.

I have Practical Wireless going back to 1958 and if any of your readers require back-numbers and send a post card first, I will reply.
E. Brown.

## Tiptree Hall Annexe,

 Tiptree,Near Colchester.

## Tapespondent Wanted

I would like to tapespond or correspond with anyone anywhere in the world. I am 23 and my interests are short wave listening and radio.

I have a 2 -track, $3 \frac{3}{4}$ i.p.p. recorder with maximum spool size of 5 in .
Allen Green.
22A Okahu Road, Kaitaia, Northland, New Zealand

More News and Comment on Page 272

# HUIIIIIPT  

THIS multipurpose instrument combines a comprehensive twenty-seven range multimeter and an L.C.R. bridge and should provide the radio constructor with sufficient test gear to build and test a host of electronic equipment. A complete list of multimeter and bridge ranges is given in Fig. 2.

Signal injection and signal tracing facilities, and an insulation test facility capable of measuring up
to $400 \mathrm{M} \Omega$ are also provided to assist in fault finding.
Realising that some constructors may already have a bridge or a comprehensive multimeter, the author has split the circuit into two distinct sections. There are, of course, minor problems if one decides to build only part of the complete instrument. For instance, the high voltage supply for the insulation test facility is derived from the bridge section, while


Fig. I: Circuit diagram of the multimeter section of the multitest. The bridge section of this instrument will be included in next month's issue in part II.

## MULTIMETER RANGES



Fig. 2: List of ranges


Fig. 3: Front panel view of the multitest, showing author's layout.
the associated meter components are in the multimeter section.

All the circuitry for signal injection and tracing is contained in the bridge section, which will be described in the next issue.

## THE METER MOVEMENT

A moving coil type of meter movement having a full scale deflection sensitivity of $60 \mu \mathrm{~A}$ and an internal resistance of $1667 \Omega$ was used by the author. Other movements can be used so long as the sensitivity is at least equal to the original and the internal resistance is similar.

If a different movement is used, the internal resistance should be made up by inserting a series resistor in the meter circuit (shown dotted in the circuit diagram). To reduce the sensitivity a shunt should be placed across the terminals of the meter movement.

An internal resistance of $1667 \Omega$ was chosen as it requires exactly $0 \cdot 1 \mathrm{~V}$ for full-scale deflection.

## MULTIMETER

A circuit diagram of the multimeter section of this instrument is illustrated in Fig 1. Although the switching looks complicated at first glance, it is really quite simple.

Switch S3 (double-pole, three-way) is the a.c./d.c. changeover. In the a.c. position it knocks out the step-up transformer $T 1$ and two of the bridge rectifiers, D3 and D6. The other two switches S1 and S2 (double-pole, twelve-way) are used to put the correct shunt or load resistor into the meter circuit.

Reference to the circuit diagram will show that there are five resistor banks in the multimeter. Resistors R1 to R5 are for the direct current ranges; R6 to R11 for d.c. voltage; R12 to R15 and R32 for a.c. voltage; R18 to R24 for alternating current; and R26 to R28 for the resistance ranges.

All the shunt and load resistors used are
dependent on the internal resistance of the meter, so it is important to know how to check its value should it not be marked on the movement.

## FINDING THE METER RESISTANCE

It is a relatively easy matter to determine the internal resistance of a meter if the full-scale sensitivity of the movement is known. (The majority of movements of this order of sensitivity are marked.)

The first step is to get the meter to indicate fullscale deflection by hooking it across a battery, but take care not to damage the movement by inserting a high value variable resistor in series with the meter. Another variable resistor should then be placed across the meter terminals and adjusted to back-off the reading to half full-scale deflection. Then carefully disconnect the shunt resistor (the one across the meter terminals) and measure its value. The answer will give the value of the internal resistance, as it will be the same as the movement.
If a quality ohmmeter is not at hand, the shunt can be made up with high tolerance $1 \%$ fixed resistors.

## DIRECT CURRENT SHUNTS

Values for the resistors making up the pad to shunt the meter on the direct current ranges are included on the circuit diagram. There should be no difficulty in obtaining R3 to R5 "over-thecounter," but you will have to make the two lower values. Wire tables should be consulted to obtain the resistivity characteristics.

The values for the resistance pad can be calculated mathematically, remembering whatever the range, the voltage across the meter remains constant at full scale deflection. The actual voltage drop across the meter can be found by Ohms law:

$$
\begin{aligned}
\mathrm{V} & =\mathrm{I} \times \mathrm{R} \\
& =\left(60 \times 10^{-6}\right) \times 1667 \\
\therefore \quad \mathrm{~V} & =0.10002
\end{aligned}
$$

For all practical purposes the voltage drop can be considered as $0 \cdot 1 \mathrm{~V}$. The ohmic value of the complete shunt can now be found by the following:

$$
\mathrm{Rs}=-\frac{\mathrm{V}}{\mathrm{It}-\mathrm{Im}}
$$

where Rs is the shunt resistance, $V$ the volts drop, It the total current for full scale deflection and Im the current through the meter. Maximum resistance is in circut on the $0 \cdot 1 \mathrm{~mA}(100 \mu \mathrm{~A})$ range and thus:

$$
\begin{aligned}
\mathrm{Rs} & =\frac{0 \cdot 1 \mathrm{~V}}{100 \mu \mathrm{~A}-60 \mu \mathrm{~A}} \\
& =0 \cdot 1 \mathrm{~V} \times \frac{1,000,000}{40} \\
& =\frac{10,000}{4} \\
\therefore \quad \mathrm{Rs} & =2,500 \Omega
\end{aligned}
$$

One cannot use the same formula to calculate the tappings as the switch arrangement is such that part of the pad is put in series with the meter on some ranges. However, as the current through the meter is so small, compared with that through the shunt on the higher ranges, the value of the shunts can be divided by the increase factor in range. Thus, as the 1 mA range is ten times larger than the 0.1 mA range, the shunt should be one-tenth the size, i.e. $225 \Omega$.

## D.C. AND A.C. VOLTS

The load resistors for the d.c. and a.c. volts ranges are quite straightforward. The lowest d.c. volts range $(100 \mathrm{mV})$ has no load resistor as the potential can be safely developed across the internal resistance of the meter. On the other ranges a resistor is brought into circuit each time the voltage range is increased to limit maximum current through the meter movement to $60 \mu \mathrm{~A}$.
To determine the values of the load resistors, one uses a form of Ohms law. The example that follows is for the 10 volt d.c. range.

$$
\mathrm{R} 1-\mathrm{Rm}=\frac{\mathrm{Vt}}{\mathrm{Im}}
$$

where R1 is the load resistor, Rm is the internal resistance of the meter, Vt the maximum voltage drop and $\operatorname{Im}$ is the current required for f.s.d.

$$
\begin{aligned}
\text { Thus: } & \mathrm{R} 1-1667 \Omega=\frac{10 \mathrm{~V}}{60 \mu \mathrm{~A}} \\
& \mathrm{Rl}-1667 \Omega=166667 \\
\therefore \quad & \mathrm{R} 1 \_165 \mathrm{k} \Omega
\end{aligned}
$$

## RESISTANCE SHUNTS

The values of the shunts for the resistance ranges ( R 26 to R 28 ) are given on the circuit diagram. They effectively shunt the meter to $10 \mathrm{~mA}, 0.1 \mathrm{~mA}$ and $75 \mu \mathrm{~A}$ respectively.

The resistor R33 on the multimeter circuit diagram is for the insulation test facility and the value given is only suitable when taking power from the h.t. rail of the bridge section.

Should one wish to build only the multimeter section and retain the insulation test facility, a d.c. source of about 200 to 300 volts is required. The ohmic value of the series resistor R33 should be of sufficient size to prevent excessive current to pass through the meter movement when the terminals are shorted. A simple way to find the correct value is to place a variable resistor in series with the fixed resistor R33 and, with the terminals shorted, adjust for full-scale deflection. Always start off with a large resistor and work down; to do it the other way, can result in permanent damage to the meter movement.

## ALTERNATING CURRENT SHUNTS

Calculating the shunt resistors for the alternating current ranges is a little more difficult as one has to take transformer T1 into consideration. This transformer is used to step up the alternating current (voltage wise, to at least 5 V ) to overcome the non-linearity of the rectifier diodes in the meter
circuit.

The type of transformer is not all that important so long as it has a turns ratio somewhere between 50 and 100 to 1 . It is necessary to measure the d.c. resistance of the primary and secondary windings as they are needed for the shunt calculations.

In circuit, the secondary winding (the one with the higher d.c. resistance) should be shunted for impedance matching. The value of this shunt resistor R17 must be about three times the impedance value of Rsec (d.c. resistance in the secondary winding of T1). Impedance, as resistance, is found by dividing current into voltage.

The approximate value of the series limiting resistor R16, linking the meter with transformer T 1 , can be found from the following formula:

$$
\text { R16 }=\frac{\text { Vsec }}{1 \cdot 1 \times \operatorname{Im}}-\text { Rsec }
$$

where Vsec is the voltage across the secondary of T1, Rsec is the resistance of the secondary of T1 and Im is the meter current for full-scale deffection. The factor 1.1 is introduced to reduce the r.m.s. (root mean square) value to an average value, which is the value indicated by the meter.

The exact value of R16 is determined after the current and power shunts have been completed.

The current in the low impedance side of T1 (that connected to the shunts) can be found from the formula:

$$
\mathrm{Ip}=\frac{\mathrm{n} \times \mathrm{Vsec}}{\text { Rsec }+\mathrm{R} 17}
$$

where Ip is the primary winding current, n is the turns ratio of the transformer, Vsec is the voltage across the secondary of T 1 and Rsec is the d.c. resistance of the secondary winding.

One must consider the impedance of the primary winding in much the same way as the internal resistance of the meter when calculating the a.c. and a.c. power shunts. In fact, the same technique as


Fig. 4: Specimen chart for the power range.


Fig. 5: Under chassis view showing the position of the main components in the multitest. Layout is not critical, but reference should be made to the frent ponel view for switch and meter positioning.
used for calculating the d.c. shunts is employed for selecting the a.c. shunts-substituting the primary winding current for 10 volts in the secondary for full-scale deffection current.

$$
\text { Thus } \quad \mathrm{Rs}=\frac{\mathrm{Vp}}{\mathrm{It}-\mathrm{Ip}}
$$

where Rs is the shunt resistance, Vp the voltage across the primary windings of T 1 , It is the total current and $I p$ the current in the primary windings.

The shunts for the a.c. ranges are most easily made from copper or eureka wire. Reference to wire tables will give sufficient information on resistivity. Take care to ensure that the current carrying capacity of the wire used is suitable.

## POWER RANGES

The a.c. power ranges are, in fact, alternating current ranges with f.s.d. coinciding with power levels at 3 or $5 \Omega$. The ratio of increase of deflection with power is logarithmic ( $1=\sqrt{\mathrm{P} / \mathrm{R}}$ ) and the author found it easier to produce a calibration chart in preference to another scale on the face of the meter. Since f.s.d. occurs at either 2.5 W or 10 W only one graph need be drawn; see Fig. 4.

## NEXT MONTH

Brief constructional details on the multimeter and comprehensive details on the associated bridge will be in next month's issue.


CORRECTLY applied negative feedback can considerably improve the quality of an audio amplifier or a complete receiver. Care should, however, be taken to select the correct component values as one can easily introduce more distortion through phase changing. In this brief article on the subject, ten different ways of applying negative feedback are touched upon. This is by no means exhaustive, but should give the serious amateur ideas for experimentation.

The values in the examples that follow should be considered as a kicking-off point rather than fixed values. It is, of course, possible to select the values mathematically, but this involves complicated calculations. Trial and error methods are perfectly satisfactory, as one can select component values for optimum personal listening.

Before going into the various methods, one should realise that only a small amount of feedback is necessary to improve the overall response of an audio amplifier or a receiver. Also, it should be noted that negative feedback loops are often frequency conscious and thus, the beginner should be careful of the capacitive elements of a feedback loop as they can introduce phase distortion.

## Split Cathode Resistor

One of the simplest methods of introducing negative feedback is to disconnect a cathode de-coupling capacitor. This produces quite a high level of feedback and can often cause too much, causing the output to fall to an unacceptable level.

As there is no capacitance in this method, the feedback is almost entirely independent of frequency. One can control the amount of

feedback by splitting the cathode resistor and de-coupling the lower half as shown in Fig. 1. The component values have not been included as they do not have to be changed from the original circuit.

A simple way to split the cathode resistor is to use a potentiometer which has an end-to-end value equal to the resistor it replaces. Then the de-coupling capacitor can be attached to the wiper arm and the potentiometer adjusted for optimum performance. This potentiometer can either be left in circuit so that the feedback level can be changed at will or replaced with two fixed resistors.

It is unwise to play around with the size of the de-coupling capacitor, as one can easily upset the overall frequency response.

## Anode-to-Anode

Another very simple and extremely efficient method of obtaining negative feedback is to couple a pair of anodes with a high-value resistor as shown in Fig. 2. The value of this coupling resistor is not critical and a $2 \cdot 2 \mathrm{M} \Omega$ should provide a good starting point. To increase the amount of feedback and thus reduce the overall gain. the size of the resistor should be reduced.

A capacitor can be connected in series with the coupling resistor to make the feedback loop frequency conscious. Inserting one having a value somewhere between 0.001 and $0.01 \mu \mathrm{~F}$ will increase the limiting effect at the higher end of the frequency band in much the same way as the conventional treble-cut tone control.

Another variation of the anode-to-anode coupling is shown in Fig. 3. This makes use of a potential divider hooked across the primary

windings of the audio output transformer, which lies between the anode of the output valve and the h.t. line. The amount of feedback can be varied by adjusting the ratio of the two resistors forming the potential divider.
One can use the potentiometer method again to determine the best ratio. If one does this, it is advisable to use a potentiometer having a value of at least $250 \mathrm{k} \Omega$.

## Treble Controls

A further refinement of the feedback loop is illustrated in Fig. 4. This circuit has been specially made frequency conscious to give limiting control of the high frequencies. Again the series capacitor and resistor arrangement is used, but this time the feedback loop is from the anode to grid in the same valve stage.
Although the components are differently arranged in the following circuit (Fig. 5), the feedback loop has the same characteristics of limiting the upper frequencies. Values for the two circuits appear on the relevant diagrams.

## Cathode-to-Cathode

An example of cathode-tocathode coupling is shown in Fig. 6. This type of feedback is used in many Philips television receivers and is quite interesting. One should be careful in adopting this method of feedback for other circuits as value of the resistors is tied to the valve characteristics. The values given on the circuit diagram (Fig. 6) only apply to the PCL83 triodepentode.
Calculating the values for another valve can be done, but one must know the current and voltage levels in the triode and pentode sections. The common cathode resistor value can then be deter-

mined by dividing the total current through the two sections into the triode section voltage. The other value can be found by dividing the current through the pentode section into the pentode voltage minus the triode voltage.

## Commonly used Feedback Circuits

The more usual forms of negative feedback found in audio amplifiers and radio receivers are shown in Figs. 7 to 10. As you can see, the circuits differ from one another; the first (7) feeding back part of the output to an uncoupled cathode resistor in the driver stage, the second (8) to a potential divider in the control grid of the driver, the third (9) to a potentiometer in the grid circuit of the final amplifier and the final illustration (10) shows a loop terminating at a fixed resistor in the grid circuit of the audio amplifier.

All four circuit arrangements are straightforward, but one must be careful not to reverse the polarity when making connections to the secondary of the output transformer. If it is connected the wrong way round, you will get positive feedback which will increase overall amplification and cause instability.
When you examine the circuit in illustration 7 you will see that there are two feedback paths, one through the cathode resistor and another from the output transformer. The level of feedback can be adjusted by changing the ratio of the two feedback resistors.
The only circuit that is frequency conscious in this group of four is the one illustrated in Fig. 9. In fact, the potentiometer in the feedback loop makes a very good treble-cut tone control.


Clandestine: Radio Scali is probably Radio Scari, a station operated by the exiled Spanish Communist Party. Announcements in Spanish call the station the "Voice of the Resistance" and state that transmissions are in the 23 and 26 m.b. An address believed to be B.P. 59, somewhere in France, is given. Has now been heard between 2100 and 2230 on 11,280.

Dahomey: Radiodiffusion du Dahomey (Boite Postale 366 Cotonou) has QSC giving date and time. Transmits on 4,870 Monday-Friday 05150715, 1130-1300, 1630-2200. Longer transmission periods are utilised at weekends.

Egypt: Cairo Radio (Propagation and Monitoring Department, U.A.R. Broadcasting and TV, P.O. Box 1186, Cairo) now uses for $7,075 / 11,915$ for the dictation speed news at $0630-0700$.

Guinea: Radiodiffusion Nationale (Boite Postale 617, Conakay) has been heard around 1945 on 4,910.

Guinea (Portuguese): Emissora Provincial da Guine (Avenue da Republica, Bissau) has been heard signing off at 2400 on 5,017.

Guinea (Spanish): Emissora de Radiodiffusion Santa Isabel (Apartmento 195, Santa Isabel, Fernando Poo ) is reported to be using an outlet in the $31 \mathrm{~m} . \mathrm{b}$. in the early evening. Full QSL is given.
Libya: Libyan Broadcasting Service (P.O. Box 333, Tripoli) has been heard on 674 at 2205.
Sudan: Sudan Broadcasting service (P.O. Box 572, Omdurman) has English 0530-0600 on 4,394/9,508. These frequencies carry Arabic during the day. Some reports say the frequencies are $4,994 / 9,508$.

Tanzania: Radio Tanzania (Box 9191, Dar Es Salaam) has been heard at 1900 on 5,050 .
China: Radio Peking (Broadcasting Administration, Fu Hsin Men, Pekin) has English 1800-1900 on $6,825 / 7,006 / 7,075 / 9,457$ and 2000-2100 6,825/ 6,890/9,860. There is an Arabic transmission on 9,520 at 1830 which suffers from bad QRM.

Cyprus: BBC East Mediterranean relay (Bush House, London, W.C.2) has been heard signing off at 1915 on the new frequency of 9,558 .
India: All India Radio (Post Box 500, New Delhi) has introduced a general Overseas Service in English. Transmissions are 1000-1100 in 19-2516 m.b.; 1330-1500 19-25; 1745-2230 41-2531 ( 7,210 is believed to be the $41 \mathrm{~m} . \mathrm{b}$. outlet); $2245-011575-49-41-31-25$ (9,740 is believed to be the $31 \mathrm{~m} . \mathrm{b}$. outlet).

Iran: Radio Iran (Ministry of Information, Meydan Ark, Tehran) reported to be using 11,795 for the Foreign Service between 1730-2130 but still announces 11,730

Japan: N.H.K. (Tokyo) now uses $17,875 / 15,135$ for the $2345-0045$ transmission. The following frequency usage is now used for general service transmissions: At $0200,0300,0400,0500,0600,0700$ and 0800 on $15,105 / 15,195 / 15,300$; at $0900,9,505 /$ $15,195 / 15,300$; at $1000,1100,1200,1300,9,505 /$ $11,815 / 15,300$; at $1400,1500,1600,1700,1800,1900$, $9,505 / 9,560 / 11,815 ; 2000,9,560 / 11,815 / 15,195 ;$ at $2100,2200,9,700 / 11,815 / 15,195$; at 2300,2400 , 9,700/15,105/15,425.
Korea (Peoples' Democratic Republic): Radio Pyongyang (Korean Central Broadcasting Committee, Pyongyang) has English on 7,580/13,780 at $0800-0900,1100-1200$ and $1400-1500$.

Korea (Republic): Korean Broadcasting System (Yejangdong 8, Chung-Ku, Seoul) has English 0830 - 0900 on 9,640 .

Lebanon: Radio Lebanon (Ministry of Orientation, Information and Tourism, Beirut) transmits as follows 1830-2030, 11,955; $2300-0100,11,760$; $0130-0400,9,575$. English is at 1830 and 0230 .

Philippines: Far East Broadcasting Company (P.O. Box 2041, Manila) has been heard identifying in English at 1000 on 11,855 (DZH8) with good signal.

Singapore: Radio Singapore (Broadcasting Division, Ministry of Culture, P.O. Box 1902, Singapore) has been reported with English at 1100 on 15,010 .

Vietnam (Democratic Republic): The Voice of Vietnam (No. 58 Quan-Su Street, Hanoi) reported in English at 1300 on new frequency of 11,760 . A pennant is sent by this station to those sending in reception reports.
U.S.A.: Voice of America (U.S. Information Agency, 330 Independence Avenue, S.W., Washington 25, D.C.) appears to have made major schedule changes. The Thessaloniki relay is now using 5,995 where there is severe interference with Radio Warsaw. The 1500 Estonian transmission is being relayed by the BBC on 11,760 . Also at 1500 there is an Urdu transmission over 17,805 Tangier and 21,675.

Armed Forces Radio and TV Service. Schedules are sent out on application only. Requests for them to Det 102, 7122 Spt. Sq. (AFRTS-USAFE), APO U.S. Forces, 09755, Europe. New schedules are issued in March, May, September and November.

Reporters this month were S. Shaw, J. D. Ashworth, P. Watts, Roy Patrick, G. Roberts, G. Lamb, I. Perry, J. W. Smith, I. Taylor, Middlesbrough High School S.W. Club, A. B. Thompson, International Short Wave Club and Sweden calling DXers.

THE AMATEUR BANDS
by DAVID GIBSON, G3JDG

YOUR scribe has been taken to task again by indignant l.f. band of specialists. Peter Short, ZS6HL says that there is quite a gang of ZS stations on 80 in the evenings. In particular he quotes ZS8M and ZS9H who are quite happy to arrange skeds with any G's interested.

Opinions seem to vary as to the state of the various bands. "I have tried listening for any amateurs on 40 but the QRM is astounding," writes D. Harvey (Salop). "Eighty metres is again very constant with the usual W's and VE's on s.s.b. Ten metres is beginning to open with a lot of European (EU's) signals coming in," observes the SWL/YL team of Messrs Singleton and YL Longbone. At '3JDG things are about as one would expect. The six bands are all humming at one time or another but 160 has been noticeably quieter. Look out l.f. bands-the sunspots is a-coming. Many people have queried the changing prefixes of some countries, so to answer a few and let you amend those countries' lists, here's the queries to date. 9Y4 is a new one for VP4, 9J2 is Zambia and 9V1 is the new one for 9 M 4 .

## Mains to $7,000,000 \mathrm{c} / \mathrm{s}$.

Michael Olsen (Gateshead), Star SR550, 35ft. wire plus 2 coat-hangers (that's what the man said)$3.5 \mathrm{Mc} / \mathrm{s}$; CN8FV, ET3AC, LA1CH, OZ, OH, ON4, PAD, SM6, LX1BW, FM7DOE, VP2AX, W2PZO, VO1GG, James Brown (Cardiff), 19 set, dipole, 80 s.s.b. CT1SQ, I1RV, KøJDA, SL2YI, VE1IE, VE8ML, VO1DM, W3PHZ, YV5BTS, ZB2AO. On 40 F. Simpson (Hull), RX80, 1.w., beheld the wonderment of-IS1DMN, K1GZL, K3UEN, PY4ND, PY7AOT, UW9AF, WA4PNC, W2AZ, W3VP, YV5BZX. David Avis (Christchurch), writes: "Sacrilege!! that's what I call it. No news on 40 for two months." He offers the following duly unearthed on the dreaded r.f. segment-CN8AW, HA9OZ, OD5EJ, PY-1CAD, $1 \mathrm{CPE}, 1 \mathrm{MIN}$, 2DUE, 70 OU , VP2SJ, VP6KL, 9H1IA. All on a 4 -valve 18 set with a half-wave dipole 12 ft . high - cor! Chris Peel (Stoke-on-Trent), waved a critical ear complete with $\mathrm{S} 750,45 \mathrm{ft}$. l.w., and headphones, the results-EL2AX, KP4, LA7RS MM (Arabian Sea) OX3LP, PY-4ND, 2AUC, 7APN, 7APS, UA1CK, UB5KB, UR2KAA, VE8ML (c.w.), W3MSK, YV5CBM, 9H1IA, 9M20V all s.s.b.

## 14, 21 and 28

So much activity that even the '3JDG t.r.f. is pulling them in on 20 and 15 with 130ft. 1.w. to an a.t.u. (plus the t.r.f. of course, they're not that strong) the three valves glowed to the rhythm of CO, CX, EL, ET3, KZ5, with the best ones UL7HB, VS9AMD, 6W8BL, 9K2AD. Colin Morris (Worcs.), homebrew s/het, joystick, 20 metres: CR5SP (Säo Thome) CO8MN, CP5AD, GC8HT, HL9KH, HM2BD, "thousands of JA's", KA7AB, KG6AAY, KH6FMG, KJ6DA, KX6BQ, DU1BA, W6FHM DU1, OA4EE, PJ2CE, VE1AED/P/SU, PZ1BW, TI2EVA (Costa Rica) TU2BA, TY3ATB, VP-1HC, 2KD, 3AA, 6WR, 8CW (Falkland Is.) VK9XI, XP1AA, XW8AX (Laos), W3KXD/VO2, YA1FV, YN1CML, YS1MA, YK1AA (Syria), ZL-1ARY,

2BE, ZS8L, ZF1GC (Grand Cayman), 6Y5AR, 9M2CP, 9M6AP, 9V1MT, 9K2AM, 9Y4VP. L. Cox (West Ham), Mohican, 21ft. vertical, 20 metres s.s.b. -CN3JC, CT1JJ, EA3JE, EP2TR, ET3AC, FB8YY, FG7XX, FM5XM, HB9QK, HZ1AB, JA-4CNS, 4XW, 6CZD, K3TUV/MM, K6JXS/MM, KP4AXC, KR6LL, LA4FG/P, MP4BZO, PY1BAR, UG6AW, UL7GL, VE3CT, VE8MD, VO1FB, VP2AX, VQ2UJ, VK-1FH, 3BG, W2ZXM/MM, W4QCM /M, W5YSM/Fix P/VU1, YQ5RF, 'YV5ACO, ZS5JM, ZC4SS, 4X4BL, 5A1TZ, 5A3TY, 5N2TWS. John Farrer (Bishop's Stortford), Mini - clipper, dipole: EP2GF, ET3AC, HC1SM, JA7ARZ, KH6GAA/MM, KP4AMI, OX1QW, TF3EA, VK3 ADR, VP2MW, VP6JC, VQ8AI, VS9AJC, VU2CK, VE1AED/SU, WA6PMG, W7RII, W5YSM/P DU1, YK1AA, YA3TNC, YV5BNW, ZC4CI, ZL5AA, 5X5GT, 5Z4KW, 7X2AH, 9M6AP, 9V1ND. Not bad for a one-valve plus two transistor amplifier, Wait till he adds an r.f. stage! R. Adair (Co. Down), R107, 30ft. 1.w. 20: CN8FS, KJ60A, KL7IEY, PY7AN, VK-3ID, 5DS, 6XX, VP2QP, VS9ARV, ZB2AM, ZL1AIX, 4U1ITU, 5A1TS, $9 \mathrm{H} 1 \mathrm{AB}, 9 \mathrm{X} 5 \mathrm{GG}$. For 15 -metre sleuths the following offerings from headphone-clad enthusiasts. $\mathbf{F}$. Simpson (Hull), RX80, 1.w., CX8AAW, HC1GB, HK3APC, JA-1DDZ, 1LPZ, 3COX, 4DLP, 6DCE, KV4TX, LU6AJ, YV1QB, ZS6AX, 4X4AS, $5 \mathrm{~N} 2 \mathrm{AAE}, ~ 5 \mathrm{Z} 4 \mathrm{AC}, 7 \mathrm{Q} 7 \mathrm{BN}, 9 \mathrm{Q} 5 \mathrm{FV}, 9 \mathrm{~V} 1 \mathrm{MX}$. A mystic signature informing that a $9 \mathrm{v} . \mathrm{s} / \mathrm{het}$. in Cardiff is worked by $\mathbf{4 4 3 7 8}$ in conjunction with a 96 ft . 1.w.: CP8GC, EL2A, HC1SM, HR2GK, KøSVT, KH6FBJ/3, PY1AXP, VK6UP, VP6KL, VS9AJC, ZC4JU, ZF1GC, ZS2NV, 5A4TO, 5H3JR.

## On its own No. 10

Two reports of activity on $28 \mathrm{Mc} / \mathrm{s}$ come from Staffs. and Notts. In Stoke-on-Trent, S750, 45 ft . 1.w. in the loft, and Chris Peel hooked CE3RC, CR6GO, CT2JA, CX1AV, EA8AE, IT1ALC, LU1DAB, PY1AGP, UP2ADJ, VS9AJC, ZE2JA, ZC4CN, ZS1JA, ZS6AW, 5X5JK, 5Z4JW, 7Q7RN, 9J2WR, 9Q5JG. R. Iball (Worksop), SX28 plus PR30, 80ft. 1.w.: CR7IZ, PY5ACN, SM2CEK, ZS6BMD, 5Z4JX, 7Q7RM, 9Q5LJ, these on c.w., while on a.m. CR6AT, CR6LAS, CX1AA, EL2O, PY2EQ, ZS1BV, s.s.b. CR4OI, EL2AK, ZD8HR, 5H3JJ.

## News and Contests

9M2FI, on Penang Island, 300 miles N.W. of Singapore: VE8BZ at Frobisher Bay, Baffin Island -these two on 15. VEØMB (20) on a lightship off the coast of Yarmouth, Nova Scotia (tnx Paul Baker) WB6QOE/VP9 on 40 c.w. The USNS Eltanin signs, KC4AAA/MM or CEØZI/MM, depending where they are. Heard on $28 \mathrm{Mc} / \mathrm{s}$ YN1AA, CR6EI, YN1MAV, ZL2PI. For the contest and rally types the following are worth a listen in July. $3 \mathrm{rd}, 144 \mathrm{Mc} / \mathrm{s}$, portable contest. $9-10 \mathrm{th}$. $1.8 \mathrm{Mc} / \mathrm{s}$ summer contest. 10th, Hurn Airport Mobile Rally. 10th, South Shields Mobile Rally. 17 th, D/F qualifying event. $24 \mathrm{th}, 70 \mathrm{Mc} / \mathrm{s}$ portable contest. 31st, D/F qualifying event Deadline this month is July 24th.

THE reception of the maximum energy from a given signal, or the transmission of the greatest energy in a particular direction, necessitates the correct orientation of the aerial in order to realise the optimum. Elementary antenna theory indicates that the simple half-wave dipole, as an example, both transmits and receives in a direction $90^{\circ}$ with the plane of the antenna. With the exception of a few odd types this fact is applicable to the majority of aerials. The essential requirement then is that the antenna, whether rotary or fixed, should be correctly aligned for some specific direction.

## Straight Lines?

It is generally satisfactory to accept a straight line as the track of radio waves over distances of a few hundreds of miles, although in marine direction finding, as an instance, bearings of radio beacons ascertained by ships at distances exceeding 70 miles are corrected. This correction, known as "half convergency ", is necessary in the interests of precise navigation, the tendency of radiated waves being to adhere strictly to the curvature of the earth. The corrected bearings can then be drawn by the navigator on the plane surface of a mercator chart as a rhumb (straight) line.
A fact with which radio men are well conversant is that the shortest distance between any two spots on the earth's surface is not necessarily a straight line but actually the arc of a great-circle passing through both of them. Great-circles are those whose planes pass through the centre of the earth, possessing a radius equal to that of the globe. The meridians of longitude and the equator are greatcircles but the parallels of latitude are not since, as they progress north and south of the equator, their radii decrease.
And so if radio signals are to be transmitted or received between London and Buenos Aires, New York and Sydney, or Cape Town and Hong Kong the radiated waves will, without exception, follow the arcs of great-circles.

It is therefore very useful in both radio transmission and reception to be able to ascertain the
direction and distance of any spot on the earth's surface from one's own backyard.

There are in existence, based upon a number of the principal cities of the world, great-circle maps (sometimes termed azimuthal maps), enabling the true bearing of any place to be read off a circumferential scale of degrees. These maps, specially calculated and drawn, provide an unusual view of the world and are useful only when used in the areas on which they are based. A great-circle map based on London is quite useless in Cape Town, Hong Kong or elsewhere.
Formulae exist facilitating the calculation of direction and distance. The Fundamental or Cosine Formula is straightforward enough but possesses an inherent disadvantage for logarithmic calculation because the cosine of any angle between 90 and 180 is negative, and if a large number of distances and directions are to be calculated the task becomes onerous. Logarithms, on the other hand, speed and simplify calculation, rendering error less likely.

## Haversine Formula

A more convenient formula used by ocean navigators is the Haversine Formula in which the Fundamental is expressed in haversines or half versine. And since the versine of any angle (A) $=$ $1-\cos$ A the haversine $=\frac{1-\cos A}{2}$. As an example the cosine of, say, 110 (being between 90 and 180) is -3420 , thus negative. Now the haversines of $110=1-\frac{(-.3420)}{2}=\frac{1+\cdot 3420}{2}=6710$. The haversine, then, is always positive, a distinct advantage, avoiding the awkward negative characteristic.

But there is a snag! How many radio enthusiasts can nonchalantly reach up to their technical bookshelves and extract a set of Haversines? The "Seaman's Bible" (Norie's Nautical Tables), a sturdy volume of more than 700 pages, contains 104 pages of natural and logarithmic haversines. We can, of course, calculate haversines as most radio manuals contain trigonometrical tables, but the advantage is lost in the tedium. But it is possible that in the

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larger cities reference libraries may be able to supply nautical tables including haversines.

There is, however, a comparatively simple solution to the problem of ascertaining great-circle bearings within a reasonable degree of accuracy, but distances must be calculated or measured on a globe. For very many years an ingenious graphical method of determining the azimuth of a celestial body has been available to ocean navigators; and a little juggling with the essential factors can quickly transform it into a handy means of finding greatcircle bearings. Should one desire extreme accuracy then the only solution is to worry a little spherical trigonometry!

## Graphical Method

Basically this graphical method comprises a diagram of hour-angle hyperbolas and latitude ellipses, with a semi-circular azimuth scale. Since the astronomical triangle of the celestial sphere is analogous to the spherical triangle of the terrestrial sphere, the hour-angle, zenith distance and azimuth in one can be taken as corresponding to the difference of longitude, great-circle distance and bearing in the other. Thus it is feasible to adapt the diagram for radio use.
In radio work it is fortunate that in order to transmit the maximum energy, or to receive the maximum signal from a given place, we need only find the initial direction. The navigator on the other hand requires to find not only the initial and final courses, but also a number of in-between courses since great-circles cross the meridians of longtitude at constantly changing angles, together with the vertex of the great-circle he proposes the ship should follow, ensuring that the highest latitude attained by the are does not pass over land, ships displaying a


Fig. 1: Illustrating the arcs of three great-circles forming the spherical triangle, $A B C$. Where, $A=$ Difference of longitude between B and C . $\mathrm{B}-\mathrm{BI}=$ latitude of $\mathrm{B} . \mathrm{C}-\mathrm{CI}=$ latitude of C . $c=$ Co-lat. of $B(90-l a t . B) . b=C o-l a t$. of $C(90$-Lat. C). $a=$ Great-circle distance. NOTE: If a latitude is in the opposite hemisphere, the co-lot. will be $90+$ Lat.
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## The Cosine Formula

Cosine Formula for Distance: (Fig 1).
$\operatorname{Cos} a=\cos b \cos c+\sin b \sin c \cos A \ldots \ldots \ldots .1$ This then becomes:
$\operatorname{Cos} a=\cos b(90-$ Lat $B) \cos c(90-$ Lat C) $+\sin b$ ( $90-$ Lat B)
$\sin \mathrm{c}(90-$ Lat C$) \cos \mathrm{A}$ (Difference of longitude between B \& C).


Fig. 2: Illustrating the Yokohama-San Francisco problem.
(At this point it might be well to state that where a latitude is located in the opposite hemisphere it will be $(90+\mathrm{Lat})$. Longitudes on the opposite of the Prime Meridian are added together to find the difference of longitude, but when of like sign are subtracted. Where a great-circle crosses the 180th Meridian, with the places on opposite sides, the difference of longitude is the sum of the differences between the individual longitudes and $180^{\circ}$ ).
Now, since $\cos (90-\mathrm{Lat})=\sin$ Lat, and $\sin (90-$ Lat) $=\cos$ Lat, we can simplify the Cosine Formula for places in the same hemisphere, re-writing it:
$\operatorname{Cos} \mathrm{a}=\sin ($ Lat B) $\sin (\operatorname{Lat} \mathrm{C})+\cos ($ Lat B) $\cos$
(Lat C) $\cos$ A..........................a
$=$ distance in nautical miles between $B \& C$.
To find the bearing of B from C :-
$\operatorname{Sin} C=\sin (90-$ Lat B) $\sin A$ (Diff. Long.)
But since dividing by sine a is the same as multiplying by cosecant a, the formula can be re-written: Sin $\mathrm{C}=\sin (90-\mathrm{Lat} \mathrm{B}) \sin \mathrm{A} \operatorname{cosec} \mathrm{a} \ldots \ldots \ldots . .2 \mathrm{a}$ Or $\sin \mathrm{C}=\cos ($ Lat B) $\sin \mathrm{A} \operatorname{cosec} \mathrm{a} \ldots \ldots \ldots \ldots 2 \mathrm{a}$
It will be obvious, of course, that to find the bearing of $C$ from $B$ merely calls for a slight re-arrangement of the factors in the formula.

## Example

Find the great-circle distance from San Francisco ( $37^{\circ} 49^{\prime}$ N., $122^{\circ} 29^{\prime} \mathrm{W}$.) to Yokohama ( $35^{\circ} 26^{\prime} \mathrm{N}$.,
$139^{\circ} 39^{\prime}$ E.), and the bearing of Yokohama. Refering to Fig 2:
$B A C=$ Difference of longitude between San Francisco and Yokohama.
$\mathrm{BC}=$ Great-circle distance.
$\mathrm{ABC}=$ Bearing of San Francisco from Yokohama. $\mathrm{ACB}=$ Bearing of Yokohama from San Francisco.

TO FIND THE DISTANCE (Both places in the same hemisphere):
Using Formula la:
$\operatorname{Cos} \mathrm{a}=\sin 35^{\circ} 26^{\prime} \sin 37^{\circ} 49^{\prime}+\cos 35^{\circ} 26^{\prime} \cos 37^{\circ} 49^{\prime}$

$$
\cos 97^{\circ} 52^{\prime}
$$

$$
=.5795 \times \cdot 6131+\cdot 8153 \times \cdot 7904 \times-\cdot 1380
$$

$$
=.3553+-.0889
$$

$$
=2664
$$

$$
=74^{\circ} 33^{\prime}
$$

$$
=74^{\circ} 33^{\prime} \times 60=4,473 \text { nautical miles. }
$$

(To convert nautical miles to statute miles multiply by $1 \cdot 152$, although the land mile, purely an arbitrary unit introduced during the First Elizabethan Age, bears no relationship to the physical dimensions of the earth, whereas the nautical mile does).

## TO FIND THE BEARING YOKOHAMA:

Using Formula 2 b :
$\sin \mathrm{C}=\cos 35^{\circ} 26^{\prime} \sin 97^{\circ} 52^{\prime} \operatorname{cosec} 74^{\circ} 33^{\prime}$
$=.8153 \times .9906 \times 1.0374$
$=.8378$
$=56^{\circ} 54^{\prime}\left(\mathrm{N} .57^{\circ} \mathrm{W}\right.$., or $\left.303^{\circ}\right)$.


Fig. 3: Great-circle bearing graph. (Weir). The difference of longitude scale is marked in both directions.

From the formula and examples given it should be possible for any distance and direction on the earth's surface to be calculated without any great difficulty; and reference to a world map-or better still, a globe-will dispel any doubt as to whether a bearing is say, west of north or east of north. However, a word of warning!

World maps are often drawn on Mercator's projection, the meridians of longitude being parallel
and the parallels of latitude "stretched out" towards the Poles, providing a completely distorted view. A line drawn from San Francisco to Yokohama on such a map will indicate the bearing of Yokohama as approximately S. $89^{\circ}$ W., or $269^{\circ}$, whereas we already know from the results of our worked example that the bearing is $\mathrm{N} .57^{\circ} \mathrm{W}$., of $303^{\circ}$, a difference of no less than $34^{\circ}$.

A ship leaving San Francisco on a true course $\therefore$ of S. $89^{\circ} \mathrm{W}$. would reach Japanese waters, but the route would be considerably further than on the great-circle course. Yet a signal radiated by a directional aerial on the same bearing ( $\mathrm{S} .89^{\circ} \mathrm{W}$.) would result in the maximum energy passing over the northern part of Australia, some 3,000 miles south of Japan, adhering to the inflexible rule that radio waves confine themselves to great-circle tracks.

## Graphical Method

The diagram provides a graphical means of finding the azimuth of a celestial body. The mathematical analysis is rather complex and of no interest to us, but by varying the factors involved we are able to utilise the diagram for determining greatcircle bearings of places on the earth. Fig. 3 illustrates the diagram in the form adapted for radio use. The rules are simple. To determine the bearing of a distant place or transmitter:

1. Reverse the names of the latitudes of the two places, marking them on the Latitude Scale.
2. From the latitude of the observer (the place from which the bearing is to be ascertained) follow the latitude ellipse until it intersects the hyperbola corresponding to the difference of longitude between the places.
3. Join the latitude of the distant place to the point of intersection.
4. Transfer this line (by means of parallel-rulers or set-squares) to the centre of the Latitude Scale ( $0^{\circ}$ ), extending it to cut the Bearing Scale.
A couple of examples should make the procedure quite clear.

What is the great-circle bearing of Yokohama from San Francisco? (Factors given in the worked example).

1. Mark off the latitudes of both places, reversing the signs. They will now be South.
2. Trace the San Francisco latitude ellipse until it cuts the difference of longitude $97^{\circ} 52^{\prime}$-almost $98^{\circ}$ ).
3. Join the latitude of Yokohama to this spot.
4. Transfer the line to zero on the Latitude Scale, extending it to the bearing Scale, reading off the bearing as $57^{\circ}$.

Since the elevated pole in this example is that in the North, the bearing is measured from the North towards the West, thus N. $57^{\circ}$ W., Yokohama being

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# A Contemporary Case 

by E. V. KING

MANY amateurs build excellent transistor radios but often spoil them by obviously home made cases. The writer hopes to show readers a method of making very attractive cases which cost little in time and money. The method is not suitable for mains receivers which generate heat, but for small battery operated ones.

The example described in this article was designed specifically for a 5 -transistor receiver but the idea can be adapted to suit individual requirements.

## Materials to use

Although plastics such as Perspex and Formica may be used the writer considers that good planed softwood is best. Use $\frac{1}{2} \mathrm{in}$. deal planed down (by the shop) to $\frac{3}{8} \mathrm{in}$. The front and back panels may be thin plywood, but for ease of cutting, hardboard is difficult to beat. Later p.v.c. quilting will cover all the woodwork so great dexterity is not required.

## Making the case

A rectangle is made up to the correct size (Fig. 1b) so that the receiver chassis will fit internally into it. The rectangle is carefully squared up and the back and front pieces of hardboard are then marked to size and cut out. Fixing holes are then drilled and the front and back temporarily fixed to the case with $\frac{1}{2}$ in. round-headed japanned wood screws. The back is then removed.

## Marking the control holes

A little dab of vaseline is placed on the longest control spindle and the chassis carefully placed in the cabinet until an oily mark has been made on the front panel. This hole ( $\frac{3}{8} \mathrm{in}$.) is then drilled out. The next longest spindle is then dealt with, and so on. In this way no measuring is required to get the holes in exactly the right place.



Fig. 3: The transistor receiver fitted into the cabinet. Note the Fablon quilting overlap round the edges.

The loudspeaker hole is then planned. In most cases any artistically designed hole may be cut in the panel as in Fig. 1a, so that when the receiver is placed in the case the appearance will be as in Fig. 2. Round holes are generally to be avoided as they make difficult the use of plastic quilting later. Small radii, such as in Fig. 1a, have some artistic merit, but square corners are easier to deal with.

The loudspeaker hole may be cut with a coping or fret saw, or may be chiselled very easily on a flat piece of waste wood. The receiver is now mounted in the cabinet and the back is put on to make sure everything is satisfactory. Leave the spindles long at this stage. Small wooden blocks screwed to the sides will hold the chassis in position (Fig. 3). Remove the receiver and both front and back panels.

## Fablon quilting

The main consideration in making the cabinet quilting cover is that no joins must be visible. To


Fig. 4: Using the Fablon quilting.
A. How the main frame is covered.
B. How the front and speaker aperture is dealt with.
C. Making the carrying strap.

## D. Fixing the strap.

$E, F, G$. and $H$. Dimensions of the Fablon quilting required for the cabinet.
overcome this difficulty and to make sure the Fablon does stay stuck down at the edges the writer has found it best to cover the three pieces separately. When screwed together, the effect is very pleasing, no joins are visible and the Fablon is tightly clamped in situ. Fablon is self-adhesive and needs no sticking medium.

Fig. $4 \mathrm{E}, \mathrm{F}$ and G shows the pieces of Fablon quilting necessary, but it is easier to cut these to size on the actual pieces of wood rather than premeasure them. The long piece that goes right round the cabinet is fixed on so that the join is underneath and overlaps. A razor blade then cuts through the overlap to give a perfect butt joint. The edges are bent down both sides as in Fig 4A, making sure that there is no double thickness of quilting at the corners.

The back and front are similarly covered, the speaker hole being the most difficult part. Fig. 4B shows how the Fablon is bent round the hardboard; small thin radial cuts are made where a curve is present. If black quilting is used, any slight visibility of white form is camouflaged with a touch of black enamel, and in fact becomes almost invisible.

The front panel is now fitted. Tygan is the most suitable speaker material and can be obtained from any radio dealer. It is sold in various designs and is strong enough to protect the speaker without any metal grille. The Tygan may be fitted with adhesive, or fixed with shortened drawing pins, or made big enough to cover the whole front panel so that it is clamped in place as the front is fixed to the case.

Make sure the Tygan is fixed so that the lines on it are in the desired direction and are straight. In the case of a speaker fixed separately to the front the speaker itself will usually clamp the


Fig. 5: A completed cabinet made by the incorporation of the ideas given in the article.

## PARTS REQUIRED

3 ft . $6 \mathrm{in} . \times 2 \frac{1}{4} \mathrm{in} . \times \frac{1}{2} \mathrm{in}$. in planed deal.
$2 \frac{1}{2} \mathrm{sq}$. ft. ordinary $\frac{1}{8} \mathrm{in}$. hardboard.
$\frac{1}{2}$ sq. $y d$. Tygan speaker material.
1 yd. Fablon quilting (ironmongers and decorating shops).
Panel pins, touching-up paint, round-headed, thin wood screws.


Fig. 6: Diagram showing how small light batteries such as the PP4 may be held in place by fixing the battery clips to the wooden casing. Two PP4's are shown in parallel.
material. For the example described, the writer takes the Tygan over the complete panel.

The front is now refitted on the case, the radio is inserted and fixed, and the spindles are carefully cut to the correct length to take the knobs required.

Fig. 5 shows the completed cabinet made by the author.

The back is similarly covered and a plastics carrying handle is easily made from some of the same material as shown in Fig. 4C, D and H.

## Fixing batteries

Batteries may be fixed in large Terry clips, or the battery connectors may be fixed to the wood with small wood screws so that the battery simply clips in place (Fig. 6). Otherwise rubber bands, or separate wooden compartments may be constructed.

The only places on the cabinet thus constructed where any join may show is for $\frac{1}{8} \mathrm{in}$. at the corner of each piece of hardboard. This can be obviated by fitting metal corner covers, but if the visible white foam is carefully painted it will be quite invisible in ordinary use. Scores of cabinets have been made in this manner and have proved entirely reliable, even outdoors in wet weather.

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Light Programme can easily be obtained by adding a parallel capacitor and switch, described later.

## Components

The components listed are those recommended, but in some cases items to hand may be used. Notes on fitting alternative transistors and other parts are given later. Many other transistors are satisfactory, particularly in the audio and output stages, but it is important to remember that if alternative transistors are fitted it will often be necessary to change some resistor values as well. This is essential in the output stage, where R6 and R7 are chosen to suit the transistors.

## Panel

This measures $5 \frac{1}{2} \mathrm{in}$. x 6 in . cut from $1 / 16$ th in. thick paxolin, with an opening the same diameter as the speaker cone. Holes for the resistor leads and other wires are made with a $1 / 16$ th in. drill. It is is advisable to drill as many holes as possible before mounting any parts.

At.r.f. receiver of the type described here can normally give good loudspeaker reception of quite a number of stations, and all the difficulties of superhet alignment and ganging are avoided. If each stage is tested as described, when wired, no difficulty should be encountered. If a wiring or other fault is made, only a portion of the receiver will have to be examined.

Construction is very easy. All components are on one side of an insulated panel, and most of the wiring is on the other side. Here, matters are so arranged that no leads cross, so connecting up should be particularly straightforward.
The circuit (Fig. 1) uses $\operatorname{Tr} 1$ as r.f. and a.f. amplifier, in a reflex arrangement which is capable of very good results. Regeneration and gain are controlled by VR1. The ferrite rod aerial tunes medium waves. Reception of the 1500 m . long wave

The speaker is mounted with 6BA bolts. Screw holes for the aerial supports will also be required. $\mathrm{VC1}$ is shown as 300 pF , but may be anything from 208 pF to 350 pF or so, preferably of the air-spaced variety. The capacitor may be fitted with a lock-nut, or by short 4BA bolts, according to type. If bolts are used, see they do not penetrate so far as to short circuit the capacitor or bend its plates.

T1 is the driver transformer, coloured leads emerging as in Fig. 3 for the component listed. If a different transformer is used, the tag or lead connections must be as specified for it. T2 is the output transformer, for use with a $2-3 \Omega$ speaker.

## Ferrite Aerial

This uses a 6 in. $x \frac{3}{8} \mathrm{in}$. diameter rod, the winding being 26 s.w.g. enamelled wire, turns side by side. Two wooden supports are cut to the shape in Fig. 4,


Fig. I: Complete circuit of the TRF4 receiver.
with screws holding them to the panel. Place a layer of paper on the rod, and fix the wire at A with tape or adhesive. Wind on 76 turns, and make a small loop $B$. Then continue winding in the same direction for a further 11 turns, and fix the wire at C.

Other rods and wires can be equally satisfactory, though a small rod is likely to give slightly less volume. If no means of checking band coverage is available, the simplest method is to adjust the number of turns until a station around 200 metres (say Radio Luxembourg, 208 m ) is tuned in with VCl nearly fully open. Coverage can also be adjusted by sliding the whole winding along the rod.
The tag in Fig. 3 is in contact with the tuning capacitor frame, and forms the moving plates connection. VCl fixed plates go to TCl and A on the aerial, Fig. 2.

## Wiring

Components are inserted in the position in Fig. 2. Spread the wire ends of resistors and capacitors so

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that parts do not fall out when the panel is turned over. After soldering, snip off excess wire. All connections on the front of the panel are shown in Fig. 3.

To avoid any difficulty with identifying transistor leads, cut 1 in . pieces of 1 mm . red, blue and yellow sleeving, placing red over each collector wire, blue over each base wire, and yellow over the emitter leads. There is no need to cut the transistor leads short, so no damage should arise with normal
soldering, providing the iron is removed as soon as joints are made.
Note positive and negative ends of the diodes. Each wire can be made into a small loop before passing through the panel, so that the heat of soldering does not easily reach the diode itself.

## First Stage

It is easy to test each stage as it is wired. Trl operating alone should give good headphone volume. Connect medium or high impedance phones from X on C5 (Fig. 1) to earth line. Unscrew TC1 fully. Connect a $4 \frac{1}{2} \mathrm{~V}, 6 \mathrm{~V}$ or similar battery, positive to earth line (via switch).

When VR1 is turned up about one-quarter to one-half way, some stations should be tuned in by rotating VC1. Note that VR1 does not have to be turned the whole way, as this does not give maximum volume. Adjust VR1 for best volume, then slowly screw down TC1 until oscillation just begins. Oscillation should cease when VR1 is turned back slightly, and sensitivity should be high.
At this stage, tuning coverage can be adjusted as already described, if necessary. C3 may be anything from about $0.25 \mu \mathrm{~F}$ to $8 \mu \mathrm{~F}$. Capacitors larger than about $8 \mu \mathrm{~F}$ give an unpleasant delayed effect on the control of regeneration.
Many good quality r.f. transistors with a cut-off frequency of several megacycles will function well in the $\operatorname{Tr} 1$ position. Other diodes than the OA81 have also proved suitable. However, the base voltage of Tr 1 depends on the transistor, diodes, and R2. Therefore with a different transistor and diodes, it may be necessary to change R2. The best value will generally lie between about $82 \mathrm{k} \Omega$ and $680 \mathrm{k} \Omega$.
Lack of sensitivity and overloading causing audio distortion shows R2 is too high in value. Violent regeneration and a high background noise indicates that R2 is too low in value. Two or three resistors

Fig. 2: Back-of-panel view showing layout of components.

The completely assembled receiver out of the cabinet.



Fig. 3: Front of the paxolin panel showing connections.

Fig. 4: Details of the ferrite rod aerial assembly and method of mounting.

of about $100 \mathrm{k} \Omega .220 \Omega$, and $470 \mathrm{k} \Omega$ can easily be tried, singly and in series or parallel.

## Second Stage

This is the audio amplifier and driver $\operatorname{Tr} 2$. The values given suit most other similar transistors. If the phones are connected across the primary of T1, signals should be much stronger, and free from distortion.

If results are now poor, R3 and R4 should be checked, and also $\operatorname{Tr} 2$, if suspected. As reputable transistors are inexpensive, there is little point in using very cheap surplus ones of doubtful merit.

## Output Stage

R6 and R7 must be correct for Tr3 and Tr4. For OC81's, change R7 to $82 \Omega$. Alternatively, use $2 \cdot 2 \mathrm{k} \Omega$ for R 6 and $33 \Omega$ for R7.
The resistors R6 and R7 should be 5 per cent tolerance. To check operation with unknown transistors or normal 10 per cent resistors insert a milliammeter in the battery circuit. Distortion
(often sounding like a faulty speaker) and a low current with no signal tuned in shows that R7 is slightly too low in value, or R6 a little too high.

On the other hand, lack of amplification, and a high current with no signal, shows that R6' is too low in value, and R7 is too high. The current of $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$ combined should normally be around 3 mA to 5 mA , with no signal, rising to peaks of 15 mA to 40 mA or more, as volume is increased

Changes made to R6 or R7 should be small. On no account switch on with R7 disconnected. You can use a new matched pair of transistors with the 5 per-cent resistors required for them, or a small pre-set resistor may be used for R6 or R7, and adjusted for proper working. Alternatively, find the value by using an ordinary potentiometer, then select a fixed resistor of the same resistance. Or shunt a resistor whose value is to be lowered by a second resistor. In all cases guard against making the base voltage very negative, as this may cause a destructive current.
In general, a midget output transformer and speaker will not give quite such good results as a somewhat larger transformer and speaker.

Cabinet, etc.
TC1 must not be screwed down very far, for if oscillation begins with VR1 nearly at zero (slider at positive end) volume will be poor. With a solid dielectric capacitor at VCl oscillation may not be sustained towards the high wavelength end of the band.

It was found that the long wave Light Programme was well received by shunting extra capacitance across VCl . About $1,500 \mathrm{pF}$ is required, depending on the position of the winding on the rod.

If the capacitor is fixed, slide the winding along the rod to tune to 1500 m . This should have little important effect on medium wave coverage. Alternatively, use a 500 pF or larger pre-set, with a $1,200 \mathrm{pF}$ or similar fixed capacitor in parallel, and adjust the pre-set capacitor for 1500 m .

The receiver can be operated from a $6 \mathrm{~V}, 7 \frac{1}{2} \mathrm{~V}$ or 9 V battery.

The author's simple cabinet is shown in the photograph. The receiver is held by screws inserted from behind. The pieces are coated with adhesive, and fixed together with small panel pins. When the adhesive is dry, glasspaper the cabinet thoroughly. It can then be finished with varnish, coloured paint to choice, or one of the self-sticking covering materials.

Stretch a piece of silk over the speaker opening inside, and glue it. A plastic drawer type handle may be screwed to the top. The back can be hinged at the bottom and have a top clip, or may be held with four small screws.

## components list

## Resistors:

| R1 | $4.7 \mathrm{k} \Omega$ | R5 | $1 \mathrm{k} \Omega$ |
| :--- | :--- | :--- | :--- |
| R2 | $470 \mathrm{k} \Omega$ | R6 | $4.7 \mathrm{k} \Omega 5 \%$ |
| R3 | $47 \mathrm{k} \Omega$ | R7 | $100 \Omega 5 \%$ |
| R4 | $10 \mathrm{k} \Omega$ | R8 | $4.7 \Omega$ |

All fixed resistors $\frac{1}{4} \mathrm{~W}, 10 \%$ except where otherwise stated.
VRI $25 \mathrm{k} \Omega$ potentiometer with switch.

## Capacitors:

| Cl | $0.01 \mu \mathrm{~F} 150 \mathrm{~V}$ | C 5 | $0.25 \mu \mathrm{~F} 150 \mathrm{~V}$ |
| :--- | :--- | :--- | :--- |
| C 2 | $330 \mathrm{pF} \mathrm{I50V}$ | C | $50 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C 3 | $2 \mu \mathrm{~F} 12 \mathrm{~V}$ | C | $100 \mu \mathrm{~F} \mathrm{I} 2 \mathrm{~V}$ |
| C 4 | $0.04 \mu \mathrm{~F} \mathrm{I50V}$ |  |  |
| VCl | 208 pF to 350 pF variable |  |  |
| TCI | 30 pF trimmer |  |  |

Transistors and Diodes:

| Tr1 | OC44 | D1 | OA8I |
| :--- | :--- | ---: | ---: |
| Tr2 | OC71 | D2 | OA8l |
| Tr3/4 | NKT251 matched pair |  |  |

## Transformers:

T1 Osmor QXD1 T2 Osmor QX02

## Other parts:

Ferrite rod, $6 \times \frac{3^{\prime \prime}}{8}$ diameter.
3 -ohm, $3^{\prime \prime}$ diameter loudspeaker.
Paxolin sheet, $6 \times 5 \frac{1}{2} \times \frac{1^{\prime \prime}}{16}$.
Battery clips, 26s.w.g. enamelled wire, connecting wire,
Imm. sleeving, two $2^{\prime \prime}$ diameter control knobs.


## 三 Electric guitar amplifier handbook

트․ By Jack Darr. Published by W. Foulsham \& Co., Ltd., Slough, Bucks. 144 pages. Size $8 \frac{1}{2} \mathrm{in}$. $\times 5 \frac{1}{4} \mathrm{in}$. Price 24 s .

IT is rather difficult to see who would benefit by paying 24 s . for this book. For the novice who plays a guitar it is perhaps rather technical. For the service engineer it is doubtful if very much would be of interest. Apparently the book has been written to " dispel any qualms the service man may have about entering a strange field".

Your reviewer is unaware of the standard of servicemen in the U.S.A. (from whence this book originated). However to seriously suggest that this be offered as a handbook to service engineers in this country is laughable if not actually insulting. To be told that low-frequency oscillation in a.f. amplifiers is called motor-boating would scarcely bring a gasp of astonishment even from the most junior apprentice who makes the tea!

The book is liberally sprinkled with such sparkling examples as being instructed to turn the amplifier upside down to get at the bottom. For the uninitiated-see this one before you buy. For the service man-stick to reading Punch.-DLG.

## 三 MICROWAYE PRIMER <br> By Albert Camps and Joseph A. Markum. Published by W Foulsham \& Co., Ltd., Slough, Bucks. 192 pages. Size $8 \frac{1}{2}$ in. $x$

FOR those readers who have a knowledge of radio and/or electronics but who fight shy of those mysterious and strange happenings high up in the microwaves then this book offers a chance to peep over the fence and find out, quite painlessly, just what is on the other side.

Although split into only four chapters the division is very effective in grouping together all the relevant facts in a particular section. Transmission lines, r.f. components and Measurement Techniques are very fully covered, while the first chapter affords an introduction to microwaves. Particularly useful is the thorough treatment given to Smith Chart techniques.

One annoying thing which for your reviewer nagged throughout the entire book and that was the question and answer technique used all the way through. Had the questions all been taken out the amount of useful information could have been doubled. Most students can supply their own questions without the help of text $!-L S A$.

## Sell or Loans

the circuit, instructions and any other information on the Bendix TA-12C transmitter.-R. C. Beckett, 275, Goldington Road, Bedford.
any information whatsoever on receiver No. 18 Mark 3.-J. Myers, 4, Pollard Street, Middlesbrough, Yorks. any information on the Army receiver R109A and modern equivalents of the valves AR8 and AR12.-P. Chatham, 58, Longrood Road, Bitton, Rugby, Warwickshire.
the issue of Practical Wireless which contains the instructions for building an Echo Unit. I have almost completely built this unit, but the book was accidentally burned. - T. J. Harrigan, "Holly Villa," 49, Trench Road, Trench, Near Wellington, Salop.
... the circuit diagram and any other information on the v.h.f. transceiver P/SU type RLP2; Tx RLS 4.1; Rx RLS 4.3. The separate numbering on each is unfortunately necessary as overall the unit is not named and it is in three separate chassis as assembled. It is made by A. T. and E. Bridgnorth. - James Whitaker, Suetts Farm, Bishops Waltham, Hampshire.
$\ldots$ a circuit diagram and any information on Ex-Government receiver R3673 Ref. No. 100/16876.-D Mines, 41, Sandringham Road, Bitterne Farm, ... a technical information manual concerning three 8 -transistor superhet model KT-1000 made by the Kobe Kogyo Radio Corp.-P. D. Winder, Elizabeth College, The Grange, St. Peter Port, Guernsey, Channel Islands.
the official handbook for the ExArmy No. 12 set transmitter.-B. King, 17 Windermere Ave., Eastcote, Ruislip, Middlesex.

## Transistors Fight Back!

Witu reference to Mr. Biddlecombe's letter in the May issue, I would suggest that he makes certain of his facts before making sweeping statements ". . .the transistor is an inferior substitute for a valve as far as the matter of music reproduction is concerned".

He obviously has never listened to a high quality transistor amplifier. It can produce results of equal quality to many valve amplifiers I have heard, with, if anything a slightly lower noise level. Added to this is the fact that one does not have to wait for the valves to warm up and there is very little heat rise and greater reliability (estimated at 500 per cent).
R. C. Bean.

London, N.W.10.

# NEWS AND 

NEW RANGE OF TRANSISTOR RADIOS

E. R. (Factors) Ltd., of 374-378 Harrow Road, London, W.9, announce the introduction of three new models, the "Fantavox" range. These sets are manufactured in Japan, by Novel Dempa Co. Ltd.
Model TA-8009 (lower left) is an 8 transistor receiver covering medium waves and costing 5 guineas. Size: $2 \frac{5}{16} \mathrm{in} . \times 2 \frac{3}{4} \mathrm{in} . x \frac{7}{8} \mathrm{in}$.
Model TM-I213 (left) is a 12 transistor four waveband a.m./f.m./s.w./l.w. receiver costing $2 / \frac{1}{2}$ guineas and measuring $6 \frac{1}{4} \mathrm{in}$. x $9 \frac{1}{2} \mathrm{in}$. $x 3 \frac{1}{2} \mathrm{in}$.
Model TM-1015 (right) is a 10 transistor three-band a.m./f.m./l.w. receiver costing 15 guineas and measuring $6 \frac{1}{4} \mathrm{in}$. $x 7 \frac{1}{2} \mathrm{i}$. $x 2 \frac{7}{8} \mathrm{in}$. Further details on any
of these models may be obtained from E of these models may be obtained from E.R. (Factors) Ltd., address as above.

## MODULAR COMMUNICATIONS RECEIVER



Racal introduce a new modular and flexible communications system based upon their RA. 217 h.f. Communications Receiver.
The basic RA. 217 is a fully transistorised receiver covering a frequency range of 1 to $30 \mathrm{Mc} / \mathrm{s}$, with continuous tuning, using the well-tried Wadley loop principle. It is designed for the reception of SSB, AM, and CW signals, and suitable IF bandwidths and AVC constants are provided for all modes of reception. The receiver may be operated from AC mains or batteries.

New modules of the system allow the basic RA. 217 to be adapted or extended into a fully flexible modular communications receiving system which can also receive ISB, FSK and LF signals and can operate either in a single or dual-diversity role. A panoramic adaptor is available together with units for synthesizer control, and extended or remote control.

# COMMENT 

## MORE POLICE RADAR TRAPS

Thirty-five more Marconi speed-measuring radar sets have been ordered by the Home Office. This will bring the total number of sets available to the British Police Forces for setting-up speed traps to 200. The basic accuracy of this speed measuring equipment is better than $\pm 2 \%$ over the entire operating range which extends from zero to $80 \mathrm{~m} . \mathrm{p} . \mathrm{h}$. This is considerably better than the normal speedometer which has an accuracy of $-0 \%,+10 \%$. Speedometers fitted to police vehicles for checking the speed of other vehicles have accuracies of $-5 \%,+0 \%$.

Most magistrates accept evidence based upon figures derived from these electronic devices, which are extremely accurate so long as they are correctly set-up and correctly operated.

The official line (Marconi) on this gear is "to provide an accurate and safe method of measuring traffic speeds, in an effort to reduce the accident rate due to speeding on busy roads."

PHILIPS TRANSWORLD DE-LUXE


The ultimate in radio luxury is provided by Philips with the Transworld de Luxe Portable radio, model 638T. It features long, mediumand v.h.f. wavebands together with four short wavebands. When the top flap opens to reveal the tuning scale the lidshows a map of theworld divided into sections for calculating the time in each area. Twin telescopic aerials serve for f.m. and s.w. reception. Price is 100 gns.

## ELECTRONICS ADVISORY COMMITTEE

A Technical Advisory Committee on electronics has been set up by the Ministry of Technology under the Chairmanship of I. Maddock, a deputy controller in the Ministry.

The Committee's terms of reference are: to identify within the field of electronics both research and development projects relating to systems, equipments, components and production technologies, the exploitation of which is important industrially and commercially. Also to identify areas where effort and available facilities in relation to these projects are considered to be too fragmented or on too small a scale. The Committee will, of course, make recommendations to Ministry of Technology and review progress on electronics projects in the Department's authorised programme.

The following have been elected Committee members: R. J. Clayton, G.E.C. Electronics; P. D. Hall, International Computers \& Tabulators; D. S. Ridler, Standard Telephones \& Cables; P. E. Trier, Mullard; A. J. Young, English Electric Valve; Dr. G. G. MacFarlane, Royal Radar Establishment; W. Makinson, National Research Development Corporation; J. H. Merriman, General Post Office; J. R. Mills, Ministry of Technology; Dr. W. H. Penley, Ministry of Aviation; A. W. Ross, Ministry of Defence (Naval); Mrs A. W. Swaffield, Ministry of Technology; and Dr. J. R. M. Granville, Royal Radar Establishment, who has been appointed secretary.

## Circuit Boards

IT was good to have an authoritative statement from L. Allen of Arborite Ltd.

I've been using off-cuts of this stuff for quite a few years . . . for two reasons; one, as I happen to have a relative who is the Managing Director of the firm importing Arborite; two, it seemed to me to be just as good as the usual Paxolin.

Both, however, suffer from one slightly annoying feature; they cannot be conveniently cut with metal shears, and I must confess that I love using metal shears. In this heat, the amount of energy expended on cutting and shaping is quite an important factor in the hobby, and shears get me less hotted up than a fret saw.

There is one other type of chassis that might interest readers, and one that I am tending to use more and more. It is vinyl floor tiling off-cuts. The delightful thing about this is its flexibility in one plane and its rigidity in the other. Thus a neat little superhet strip plus audio can be bent around the corners of some old fancy cabinet, and all the space used.

I realise that "building round bends" is going to get me dubbed the "obvious", but we all have our particular brand of bends; the diver, the high flier, and the man who constructs a radio in a plastic sphere representing the World. H. Wagner.

## Kuala Lumpur, Malaya.

## Transistors Fight Back!

Surely Mr. Biddlecombe must be joking, when he calls transistors inferior!

Mind you, he spoils his case a bit, when he uses a pre-war 8 in . speaker as a source of "Hi-Fi".

I have been making, assembling and modifying radio gear for over 35 years, but I haven't touched any new valve apparatus for two years-so convinced am I that they are now back numbers! (Except for high-voltage applications, like TV).

Transistors hiss? Only if badly designed-or chosen. After all, you wouldn't use a 6L6 in a preamp!

Yet that is the kind of thing that I have seen done in "hissy" transistorised amplifiers.

It will shock Mr. B. to hear that I use transistors because they are so noisefree! (My latest being a 20 dB TV u.h.f. booster.)

In my categorical opinion, a welldesigned (note!) bit of transistor apparatus is always superior to its valve equivalent in reliability, stability, coolness of running and quality of reproduction, even when using the best of modern speakers on f.m. / v.h.f.
R. G. Young.

Peacehaven,
Sussex.

# THE 'IMPERIAL' 3-band transmitter F.G.RAYER G3OGR 

Part III

## KEYING THE TRANSMITTER

The usual methods of keying a transmitter for c.w. (continuous wave) operation are perfectly satisfactory for the Imperial. The first to be described is extremely simple and requires few additional components. In fact, it involves disconnecting the cathode and beam plate connections (pins 1, 4 and 6) to the power amplifier and keying its cathode. It is then necessary to insert a 2000 pF disc ceramic capacitor between each of the three valve pins and chassis, keeping the leads as short as possible.

One must also disconnect the h.t. to the screen grids in the modulator and isolate the modulation transformer by shorting the primary winding. It is also advisable to put a $47 \mathrm{k} \Omega$ resistor across the key in the cathode circuit of the power amplifier.

All of these alterations (not including the 2000 pF de-coupling capacitors)


Fig. 8: Switch connections for the simple c.w. modification.

Fig. 9: Circuit showing the clamp valve 6AQ5 connections. Only the basic outlines are included of the driver and the final power amplifier stages.
switching away from the cathode switching. The illustration Fig. 8 shows the actual connections.
Should one wish to avoid keying the final power amplifier, an alternative method is illustrated in Fig. 9, using a clamp valve 6AQ5. In the original layout a hole was shown for this valve between the tank circuit and the modulator transformer.

The grid circuit of the power amplitier has to be altered so that bias obtained from grid rectification can be applied to the clamp valve 6AQ5. A similar switching arrangement to that of the simpler keying circuit, described earlier, is employed in this circuit. The main difference being that the key is in the cathode circuit of the driver and not in the final p.a. No alternations have to be made to the anode or cathode circuits of the final p.a. A cathode de-coupling capacitor does, however, have to be included in the driver 6CH6.

The three-pole, two-way c.w./phone can be
mounted on the rear chassis runner.
should be dwitch beug a ganged switch, being careful to keep the h.t.


When grid drive is available from the p.a. driver, bias developed across the $22 \mathrm{k} \Omega$ resistor almost wholly cuts off the anode current of the clamp valve. No bias is developed when the key is open. This permits the clamp valve to conduct heavily which, in turn, reduces the screen grid voltage and the anode current of the final p.a. and thus kills the r.f. output.

The anode load of the clamp valve (R1) may have to be modified to suit the h.t. voltage; $40 \mathrm{k} \Omega$ is suggested as a starting point. Before setting-up the $500 \mathrm{k} \Omega$ potentiometer in the grid circuit of the clamp valve, adjust the slider arm for minimum voltage on the grid. Then tune up the transmitter; with about 2 to $2 \frac{1}{2} \mathrm{~mA}$ grid current and 80 mA anode current. Now adjust the potentiometer until the anode current on the final p.a. just begins to fall.

With the key open, the screen grid potential of the final p.a. should fall to about 25 V and the anode current to about 40 mA . Using a 400 V supply, this represents an anode input of 16 watts, which is well within the anode dissipation rating of 20 watts. Resistor R1 can be reduced to raise the input with drive, if wanted.

The clamp value is left permanently in circuit, and has no effect on phone working, except to keep the p.a. anode current down if grid drive ceases through a fault. If the maximum possible c.w. output is wanted, fixed bias can be obtained from a battery or a small power supply connected to the positive side of the 5 mA meter. The voltage is not critical (between 20 and 60 volts), but the $500 \mathrm{k} \Omega$ clamp control potentiometer should be adjusted as previously described. The effect of fixed bias reduces the p.a. anode current under no drive conditions.

## H.F. BANDSPREAD

As only part of the 3.5 to $3.8 \mathrm{Mc} / \mathrm{s}$ v.f.o. range is used when operating in the 7 and $14 \mathrm{Mc} / \mathrm{s}$ bands, it is possible to bandspread. A method found to be very successful with the author is shown in Fig. 10. A twin-gang tuning capacitor having a value of


Fig. 10: The bandspread tuning modification for the 7 and $14 \mathrm{Mc} / \mathrm{s}$ bands.
about 80 pF per section and trimmers with about 50 pF are perfectly satisfactory. All the capacitors should, however, have a fairly high stability.

The adjustment procedure is quite straightforward. Adjust range $A$ and $B$ for correct coverage using the trimmers and then switch to the 20 metre band and calibrate range $B$ at $0.1 \mathrm{Mc} / \mathrm{s}$ intervals with a $100 \mathrm{kc} / \mathrm{s}$ crystal marker or other generator which may be at hand. Now the v.f.o. range 14 to $15 \cdot 2 \mathrm{Mc} / \mathrm{s}$ covers $14 \cdot 0$ to $14 \cdot 4 \mathrm{Mc} / \mathrm{s}$.

The additional components for this modification can be mounted in the v.f.o. box.


## 4-CHANNEL TRANSISTORISED MIXER

An essential unit for audio enthusiasts, enabling various sound sources to be mixed for single composite output. 7 transistors. Separate volume controls for each channel. Veroboard construction, simplifying layout and assembly.

## GRYSTAL CONTROLLED OSCILLATORS AND TRANSMITTERS

How-to-make details of an easy-to-build $3.5-28 \mathrm{Mc} / \mathrm{s}$., using crystal control for simplified design and construction.

## MODIFICATIONS TO THE TEN-FIVE RECEIVER

Improvements to this popular all-transistor doubleconversion communications receiver fully described.

## BEGINNERS' SHORT WAVE TWO

How to build a simple 2-valve t.r.f. for loudspeaker or headphone operation. Operates from a.c. mains with built-in power unit. 5-15 Mc/s


SEPTEMBER ISSUE ON SALE AUGUST 4th MAKE SURE OF YOUR COPY!

# practically  

W$E$ are no longer a nation of shopkeepers: merely suppliers and demanders, says a pundit. As far as the marketing of wireless spares goes Henry would amend that to "non-suppliers and pleaders".
We enter the nearest radio shop and an immaculately attired gent appears. He receives our request with a lifted eyebrow and disappears in the back premises. In no time at


With lifted eyebrows
all he returns to shake his head sadly, regretting that supplies of spares are restricted to their own agency models.
Recognising the brush-off technique, we toddle along to a branch of one of our betterknown multiples, even more resplendent than the last emporium-and even less likely to bother with our one-andninepenny item.

There was a heartrending letter in a trade journal recently asking why the "multiples" should be regarded in such a bad light. The writer worked in the usual crack about the " man in a dirty coat in a little room above every store" and the dead flies in the independent dealer's window.

We could have told him one reason why the multiples have a bad image-so seldom is there
anyone on the premises that knows anything about the technicalities of the equipment they are trying so hard to sell! The man in the little room, dirty coat notwithstanding, would treat us with more sympathy. We would put up with a few dead flies, and even a dozing cat, to be sure of a modicum of real service.

The pattern is repeated in all the radio supermarkets of the High Street. The aristocrats advance, kneading their knuckles at the prospect of a hundredpound sale, then retire, crestfallen, when it turns out that all we need is an insignificant spare part.

We are forced to try the little chap around the corner, where the proprietor has himself gone through the mill and is now elevated to chief salesman-cumsweeper - cum - cashier - cummechanic's aide - cum-anything else that's needed.

Have you, dear reader, ever tried asking a large manufacturer for a small spare part? Either one is completely ignored or referred to the "nearest agent". And as he is probably the first of the well-swept emporia we tackled the problem is back in our laps.

Let me offer a few crumbs of comfort. We are not alone in our nail-biting frustration. Even

the so-called agents have their troubles when ordering spares. To cite a recent example . . .

Wanted: A spool carrier for a well-known make of tape recorder under guarantee. To remove the faulty part was to leave a welter of loose belts and pulleys, so we ordered an advance replacement, quoting the full details of the machine, the owner and the date of sale.
Back.came a carrier, minus the tyre-which was the specific part that was causing the trouble. We searched the manual for a separate parts number for the tyre, found none, so wrote to the maker, quoting our previous order number and asking for the missing bit pronto.
By return of post a complimentary slip saying: "Please quote model, etc.". We played safe and sent the dud part this time with explanatory cover note. Back came the wrong replacement with invoice. Three letters later we received four replacements with tyres but minus a small bush. We packed the lot' off with an acid note, quoting again our original order, and this time received a fresh carrier with bush but minus tyre. And in the following post invoices for the other, unwanted, returned, spares.

So far I calculate we have spent nearly as much on postage as it would have cost to order a new part COD, which would probably have turned up correctly by return!

Perhaps it is understandable after all when the dealer balks like a frightened horse at the sight of our sorry spare part. Practical Wireless readers who pride themselves on being what Percy Wilson graciously calls "the dawn of a new dispensation" would be better advised to make the darn gubbins themselves!

## AIIAR - QUALITY



SEND 6d. IN STAMPS FOR ILLUS. LEAFLETS OF THE CODAR RANGE

## ANOTHER GODAB TRUUMPH!

THE NEW 1966 CR. $\%$ A COMMUNICATION RECEIVER.
This completely new receiver sets a new high standard for performance and finish unequalled at the price, and is a worthy ddition to the outstanding range of CODAR quality communication equipment. Frequency range: $560 \mathrm{Kc} / \mathrm{s}-30 \mathrm{Mc} / \mathrm{s} 2 \mathrm{M} / \mathrm{s}$ $4.2 \mathrm{Mc} / \mathrm{s}-11.5 \mathrm{Mc} / \mathrm{s}: 11.5 \mathrm{Mc} / \mathrm{s}-30 \mathrm{Mc} / \mathrm{s}$. Slide rule scales for each band calibrated in frequencies plus an additional logging cale in degrees. Two speed vernier tuning control with reverse slow tune action. Unique aerial input stage exclusive to the CR.70A employing High 'Q' Air-spaced CODAR-QOIL Inductor giving extremely high gain with 1ow noise level. Panel aerial trimmer for peaking weak signals, Double tuned I.F. Iron cored transformers. 47 . Kols winh mise frame grid valve for triodes) giving 7 yalveline-up Separate F . SSB reception Calibrated signal strenth 's', meter illumin ated. Automatic Yolume control. Panel phone iack for 'private listening. $2-3$ ohm output for external speaker. (Matching unit optional extra,) Superb styling metal cabinet in the new Organasol Satin lustre finish Size: $13^{\circ} \times 52^{\prime \prime} \times 73^{\prime}$. For A.C. $200 / 250 \mathrm{v}$. Ready built. Not a Kit at the fantastic low price of 19.10.0. Carr. 7/6.

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ASIMPLE, inexpensive audio amplifier that can be fitted to an experimental chassis in a few minutes is described in this article. Two easily obtainable valves are used in the amplifier, which incorporates a three-inch round loudspeaker and has an output of about two watts. This should be sufficient for an experimenter to line-up i.f. and r.f. circuits that have no audio stages. A jack socket is also provided to permit the output to be reproduced by a larger speaker or displayed on an oscilloscope.
The circuit, shown in Fig. 1, is extremely simple and functional; a high-gain EF91 being used as a preamplifier and an EL91 as a single-ended output amplifier. The output of the preamplifier is capacitively coupled by C3 to the grid of the EL91 which, with a 13 volt swing on the grid will give a $1 \frac{1}{2}$ watt output.

Loading of the output stage is not critical in a circuit of this type. Optimum loading is 16,000 ohms and thus, to match the $3 \Omega$ loudspeaker, one should try to obtain an output transformer with a ratio of about 75 : 1.

A little negative feedback from the output transformer is applied to the cathode of the preamplifier


# SIMPLE AUDIO AMPLIFIER 

for the radio experimenter's workshop

by V. E. Holley

to prevent microphony. One should, however, be careful in wiring the feedback loop, as it is easy to reverse the polarity and put positive feedback on to the cathode of the first stage which will cause instability. Decoupling between the two stages has not been found to be necessary.

The power requirements for the amplifier are quite nominal; 15 to 20 mA at a potential of 200 to 250 V d.c. for the h.t. rail and 500 mA at 6.3 V a.c. for the heaters. Often this can be taken from the equipment with which it is working.

## * components list



## Construction

The main chassis and the shelf that supports the two valves is constructed out of 18 s.w.g. aluminium sheet; bending and drilling details are given in Fig. 2. Probaby the most difficult hole to cut will be that for the loudspeaker. If no suitable tool is available to cut the $2 \frac{5}{8}$ in. hole in the faceplate, a neat and simple alternative is to drill a large number of one-eighth holes just inside the circumference. It


Fig. 1: Circuit of the amplifier module.
is then a simple matter to break the centre out and clean up the ragged edges with a file.

Once the metalwork has been drilled and bent, check that there is sufficient clearance for the loudspeaker before the holes necessary for securing the shelf to the main chassis are drilled. Before making


Fig. 2: Drilling and bending data for the main chassis and for the valve shelf.
a permanent fixing, it is best to wire the valve bases as it 'is difficult to reach these with the shelf in posi-s tion.

## Components and Wiring

Component layout, which is not critical, and the associated wiring information is given in Fig. 3. All the components are standard other than the output transformer which has been fitted with an additional (isolated) tag. This has been done to provide a convenient point for the heater input. The high tension


Fig. 3: Wiring diagram of the amplifier. The amplifier is shown laid face down and to simplify the diagram, the valve shelf has been up-ended, so that the under-side can be seen, ond the sides of the main chassis are shown "un-bent".
input connection is also made on the output transformer tagboard; on the "hot end" of the primary winding. The only other external connection, the signal input, is made direct to the volume control. Thus, only three soldered connections are necessary when the completed amplifier is fitted to an experimental chassis.

The internal wiring is quite straightforward. Tinned copper wire, covered with sleeving, is suitable for all connections. One should, however, be careful to use tubular ceramics in the C3 and C4 positions and miniature electrolytics in the C2 and C5 positions.

## Testing

When the amplifier wiring has been completed, the normal resistance checks should be made before applying power. Should there be any instability, check that the connections to the primary and secondary windings on the output transformer are the right way round.

## great circle calculations

## -continued from page 262

west of San Francisco. This agrees with our worked example.
Find the bearing of Sydney, Australia ( $34^{\circ} \mathrm{S}$., $151^{\circ}$ E.) from Luanshya ( $13^{\circ} \mathrm{S}$., $29^{\circ} \mathrm{E}$.)
Proceed as in the previous example, reversing the names of the latitudes. Then trace the Luanshya latitude ellipse (now $13^{\circ} \mathrm{N}$.) to the difference of longitude, which is $122^{\circ}$. Join the latitude of Sydney (now $34^{\circ} \mathrm{N}$.) to the intersection, and transfer this line to zero on the Latitude Scale, reading the bearing on the outer scale as $47^{\circ}$. The elevated (nearest) Pole is the South, thus the bearing will be S. $47^{\circ}$ E., Sydney being Eastwards of Luanshya.

Of course, if a simple transmitting dipole, correctly oriented, were in use in the preceding example a signal of equal strength would be radiated towards Sydney on the reciprocal course-N. $47^{\circ}$ W., or $313^{\circ}$. The short route to Sydney from Luanshya, about 6,400 miles, is south of Madagascar towards the Antarctic, within approximately 40 degrees of the South Pole, whereas the long route spans West Africa and the North Atlantic to Canada, curving south-westwards over the U.S.A., skirting the Hawaiian Islands to Sydney, a distance of about 15,200 nautical miles; and it will be observed that the combined distances of the two routes equal 21,600 nautical miles, the circumference of the earth, thus a great-circle.
The use of a directional beam aerial would obviate the wastage of energy radiated over the abnormally long route, although the time of day and the prevailing conditions must always be borne in mind when considering the transmission and reception of signals over very long distances.

## Captain Weir

The Azimuthal Diagram, from which the Graphical Method was adapted, was originally devised by Captain Weir for the use of seamen as an aid in celestial navigation.

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | D | $L$ | C | 3V. | 6 V . | 9V. | 12V. | I5V. | 25 V . |
| CE. 2 'V' or 'H' |  | $\frac{1}{8}$ | $\frac{1}{2}$ | 0.07 | 8 | 6 | 4 | 3 | 3 | - |
| CE. 3 | " | $\frac{3}{16}$ | $\frac{7}{16}$ | 0.1 | 25 | 20 | 15 | 10 | 6 | 4 |
| CE. 4 | " | $\frac{3}{16}$ | $\frac{1}{2}$ | 0.1 | 40 | 30 | 20 | 15 | 8 | 6 |
| CE. 5 | " | $\frac{1}{4}$ | $\frac{7}{16}$ | 0.14 | 50 | 40 | 25 | 20 | 10 | 8 |
| CE. 6 | " | $\frac{1}{4}$ | $\frac{1}{2}$ | 0.14 | 80 | 60 | 40 | 30 | 15 | 12 |
| CE. 7 | ".. | $\frac{5}{16}$ | $\frac{1}{2}$ | 0.18 | 100 | 75 | 50 | 40 | 20 | 15 |
|  |  | D | $L$ | C | 3V. | 6V. | 10V. | 15 V. | 25 V. | $\underline{50 \mathrm{~V} .}$ |
| CE. 8 | " | $\frac{1}{4}$ | $\frac{3}{4}$ | 0.14 | 100 | 80 | 60 | 40 | 25 | 8 |
| CE. 9 | " | $\frac{3}{8}$ | $\frac{3}{4}$ | 0.2 | 250 | 200 | 160 | 100 | 60 | 20 |

$\mathrm{V}=$ Vertical Mounting $\quad \mathrm{H}=$ Horizontal Mounting

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THE simplest method of comparing two frequencies is by applying one to the $\mathbf{X}$ amplifier (or $\mathbf{X}$ plates) of an oscilloscope, and the other to the $Y$ amplifier. When the two frequencies are equal, an ellipse is obtained, which at a $90^{\circ}$ phase difference between them can be adjusted into a circle by means of the oscilloscope gain controls.

Other recognisable Lissajous figures are obtained when one frequency is at an exact multiple of the other, and it is easy to tell when one frequency is $2,3,4, \ldots$ times the other frequency. Stationary patterns are also produced at intermediate frequency ratios such as $3: 2$, but like the higher multiples, are difficult to interpret.

An oscilloscope is thus the most likely means to be used in calibrating an a.f. oscillator in the absence of specialised instruments such as frequency bridges and frequency meters, and the standard frequency will probably be $50 \mathrm{c} / \mathrm{s}$ from a low voltage mains transformer. Alternative frequency standards are not so easy to use. Examples are BBC tuning signals and television line frequency. Although it is not impossible to work downwards from a $100 \mathrm{kc} / \mathrm{s}$ crystal oscillator, or even the Long Wave Light Programme, this would require special and very stable apparatus.

If only one or two standards of frequency are available in calibrating an a.f. signal generator, an auxiliary oscillator is necessary to fill in the gaps. Starting with $50 \mathrm{c} / \mathrm{s}$ mains frequency, the signal generator can be calibrated upwards at $50 \mathrm{c} / \mathrm{s}$ intervals. The auxiliary oscillator is then brought in and set to a multiple of $50 \mathrm{c} / \mathrm{s}$, which enables the process to be continued to higher frequencies, the frequency of the auxiliary oscillator being increased whenever the ratio is too large.

Below $50 \mathrm{c} / \mathrm{s}$, the auxiliary oscillator is equally necessary, and setting it at $10 \mathrm{c} / \mathrm{s}$ one-fifth of mains frequency, allows the signal generator scale to be marked at multiples of $10 \mathrm{c} / \mathrm{s}$. It has been found

just possible to calibrate down to $5 \mathrm{c} / \mathrm{s}$, although at these low frequencies, changes in the pattern occur very slowly and the moving spot is seen, persistence of vision no longer working to produce the effect of a continuous line.

At high frequencies, the reverse is true, and the voltages are changing so rapidly that it becomes increasingly difficult to hold a stationary pattern. It was found that in the wide range a.f. oscillator, the output potentiometer had a very slight effect on the frequency, which could be utilised to produce the very slight frequency adjustment necessary. At frequencies well above the audio range, however, it may only prove possible to hold a pattern momentarily.

It would be possible to introduce a very small amount of synchronisation between the two oscillators, to assist in making the pattern stationary, but the wide range a.f. oscillator was calibrated successfully up to $75 \mathrm{kc} / \mathrm{s}$ without doing this, although the


Fig. 2: Top view of the completed unit.
signal. The basic trace is then an ellipse on which the higher frequency is superimposed as a ripple. It is only necessary to count the number of peaks along the ellipse to establish the frequency ratio. Each peak denotes a cycle since the negative (i.e. inverted) peaks are not counted. If the pattern is quite stationary, since the top and bottom of the ellipse have a similar appearance, it is possible to count the peaks in pairs along the ellipse.

A number of photographs have been taken of


Fig. 3: Layout of components showing jumper links above panel and the external leads.


Fig. 4: Underside view showing the cross-links and breaks in the copper strips.
adjustment is very critical at the higher frequencies. The disadvantage of any degree of synchronising is that there will be some inaccuracy due to one oscillator being "pulled into step" by the oscillator at the higher frequency, and consequently shifted slightly from its true frequency.

## Elliptical Trace

The main source of confusion with Lissajous figures is that the forward and return traces are superimposed on each other so that it is not always possible to distinguish which is which. A separation of the two wave traces will make the patterns much clearer and enable larger ratios of frequency to be compared. This separation can be made by applying a phase-shifted version of the $X$ signal to the $\mathbf{Y}$ amplifier in addition to the higher frequency
the types of oscillogram produced by this method. When the two oscillators have the same frequency, the pattern is simply an ellipse, but its tilt and shape will be seen to alter with adjustment of the superimposed signal. When the higher frequency is an exact multiple of the ellipse frequency, the "wavy ellipse", described, is obtained. The other patterns shown (J.K.L.) are intermediate ones or produced from having the ellipse frequency higher than the other frequency. Although interesting, these patterns need not be considered for calibration purposes, since the simple wave patterns will provide all the frequency ratios needed.
To produce the ellipse, a phase-shifting circuit is required in addition to an auxiliary oscillator. This sounds rather complicated, although it can be a temporary set-up, using, for example, Veropins as


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junction points, well-spaced out on a panel of plain Veroboard. The auxiliary oscillator must be sufficiently stable in performance, but it need not be calibrated, and automatic amplitude control is dispensed with, although this necessitates readjustment of an extra potentiometer every time the frequency of the auxiliary oscillator is changed. A simple form of auxiliary oscillator may be preferable, but a twophase oscillator can be constructed which produces an ellipse without any additional phase-shifting circuit.
to adjust them separately. Separate adjustment would enable a perfect circle to be obtained, if necessary, by compensating with one network for minor phase-shifts in the transistors. Only an ellipse is required, however, for frequency comparison, so the phase shift in the networks need not be precisely $90^{\circ}$.

Direct coupling throughout the oscillator circuit makes electrolytic capacitors unnecessary and $=$ enables oscillation to be obtained down to a very low frequency. Apart from the relatively bulky


Ideally of course the unit should be completely independent of any influences or variables which might affect its ultimate performance. Unfortunately the frequency of the two-phase oscillator is not as completely independent of the transistor characteristics as could be desired for precision, and it could probably be improved in this respect, but it does enable consistent frequency checks to be made, starting from $50 \mathrm{c} / \mathrm{s}$ as the standard frequency, and enables a useful calibration to be made on another oscillator.

## Circuit Description

The circuit diagram, Fig. 1, shows that the oscillator contains two phase-shifting networks separated by transistor stages, an arrangement more common in thermionic circuits. Each network produces a $90^{\circ}$ phase shift. At the frequency of oscillation, the overall phase shift around the loop is effectively zero, consisting of the two $90^{\circ}$ phase shifts cancelled by the phase inversion of Tr5. The networks are supplied from phase-splitter stages Trl and Tr 3 . The two outputs from each phase-splitter resemble those of a centre tapped transformer winding, the zero volts line being equivalent to the centre-tap. This arrangement enables $90^{\circ}$ phase shifts to be produced from networks which normally would yield only phase shifts of $45^{\circ}$.

Loading on the networks is avoided by the insertion of the high input impedance stages $\operatorname{Tr} 2$ and Tr4. The oscillator thus consists largely of emitterfollower stages, with $\operatorname{Tr} 5$ as the amplifying stage. Tr 3 also provides some amplification of the output for the X axis, but functions only as a phasesplitter in the oscillator loop. Variable resistances, VR1a and b are ganged together, as it is awkward

Typical oscillograms obtained with the two-phase oscillator when another frequency is superimposed on the elliptical trace. Readers may note these oscillograms have been redrawn from the photographs illustrating the wide range oscillator described last month.
components of the phase-shifting networks, the rest of the oscillator is extremely compact and was constructed on a small piece of Veroboard (Figs. 3 and 4): actually, part of 2.5 in . x 3.75 in . panel sawn in half. Veropins are used as anchoring points for the external leads. This miniaturisation is not essential, however, as the ellipse generator is only a temporary aid to calibration, and it can be connected up more quickly if well spaced out, by simply following the layout of the circuit diagram.

The potential divider formed by R12 and VR2 is necessary to reduce the direct voltage to the base of Tr1. Prefixing Tr1 by another emitter-follower would improve the performance, but the number of transistors would be increased to six. The inclusion of C9 extends the frequency coverage, but the waveform deteriorates above the a.f. range, even when r.f. transistors are used.

## Adjustment of VR2

The pre-set amplitude control VR2, is used to adjust the loop gain in the absence of a thermistor. With too low a setting, oscillation does not occur, while with too high a setting, the ellipse that appears on the oscilloscope screen will be flattened at one end. Suitable adjustment produces a good ellipse, but readjustment is needed as the frequency is changed.

A two-phase oscillator has the special advantage


Fig. 5: Interior of the unit. The components are omitted from the components panel in order to show the underneath wiring (dotted).


Fig. 6: Elliptical trace produced on oscilloscope screen by applying part of the $X$-signal, shifted by $90^{\circ}$ in phase, to the $Y$-plates. (Expanding the $Y$-deflection will produce a circle). At phase differences other than $90^{\circ}$ the ellipse is tilted and cannot be adjusted into a perfect circle.

## components list


that it readily produces an ellipse or circle on the screen of an oscilloscope at any audio frequency. The outputs from the collectors of $\operatorname{Tr} 3$ and $\operatorname{Tr} 5$ are of similar magnitude and can be used to produce a circle. A reduced $Y$ output is available from the junction of R13 and R14 for the ellipse, whose height and width will depend also upon how far the gain controls of the oscilloscope amplifiers are increased. The higher frequency to be compared is applied to the socket marked "Input" from which it is superimposed on the $Y$ output via R14. The resistances R13 and R14 may be high in value, taking advantage of the high input impedance of the oscilloscope $Y$ amplifier, and this avoids any interaction between the oscillators, which might produce synchronising.

## Construction

After some temporary set-ups, the oscillator was assembled in a box made from 22 s.w.g. tinplate by soldering. This is in an upper and a lower portion which fit together and there are two coaxial sockets on each side with a small label under each to indicate its function. As an auxiliary oscillator, the ellipse generator does not require calibration, and its frequency scale is too much influenced by adjustment of the amplitude control to be more than an approximate guide.

The interior of the oscillator, Fig. 5, is traversed by sleeved leads from the Veroboard components panel in the centre. This is supported in the wiring by using wires of a stouter gauge from the four coaxial sockets. If VR2 is a metal-cased potentiometer, insulation will be required under the components panel unless there is sufficient clearance to make this unnecessary. The two sets of network capacitors are mounted around the miniature wavechange switch, the common junctions being to insulated tags whose brackets are soldered to the case.

The battery leads pass through a $\frac{1}{4} \mathrm{in}$. grommet at one end of the case and as the 9 volt battery is external, it can easily be disconnected, so an onoff switch is unnecessary.

This unit is eminently suited for use with the Wide Range Audio Oscillator described in last month's issue.
-(Ed)


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Left to right: Club chairman Bill Sheppard G3JBS, club secretary Jim Bunce, Bill Patten G3PAT, Robbin Powell G30GP, David Penny G3PEN, Martin Railton G8AB, club treasurer Bob Stevens, Jack Atkinson G3OPA and John Stuart G3TUM.

THE Loughton and District Radio Society was formed just over four years ago by John Kay G3AAE and Cliff Waterman G3NKX. Like so many other amateur radio clubs, this was started by circularising local licensed amateurs and known shortwave listeners.
About 30 came to the inaugural meeting, which was held in John Kay's front room. Everyone was enthusiastic and a working committee was formed; Cliff Waterman being elected honorary chairman, Jack Atkinson G3OPA club secretary and Bill Patten G3PAT treasurer. John Kay had to decline office owing to business commitments.
Accommodation was one of the club's biggest headaches until the local Community Association came to the rescue, with a room at Loughton Hall at a most reasonable fee. The club does not have exclusive use of the room-occupying it every other Friday evening-and thus, cannot have its own

station. All the facilities of Loughton Hall, which stands in spacious, well-kept grounds, are made available to club members, including the wellstocked bar. Ken Jones, chief warden of the hall, has been of immense help to the club and has done a lot to publicise the activities of the club.

Exhibitions, mobile rallies and social functions laid-on by the club have always been well attended and the revenue raised from these activities has enabled the club to make several purchases. A typewriter and duplicating machine were among the first purchases and are now in regular use producing the club's "Newsletter." One of the more recent acquisitions is a 16 mm sound projector.

A lot of the credit for the success of the social side of the club must go to the club's first entertainments officer Bob Stevens and public relations officer Jack Atkinson. Jack is now the club's entertainments officer and Bob has charge of the club's purse.

Meetings are held at Loughton Hall every other Friday evening, starting at 8 o'clock and include lectures and film shows on a host of subjects. The evening Practical Wireless visited the club, a lecture was given on the London Post Office Tower, by club member David Penny G3PEN, who actually works "in-the-tower"

Like all good clubs, most of the "seniors" adjourn to one of the local taverns afterwards to sample the ale and talk "shop." The youngest licensed club member is Stephen Alderton G3UXV, who was 15 last birthday. He got his licence last year and already has quite a selection of QSL cards from countries all over the world. He even has one from Japan.

The club does not run instructional classes for the unlicensed members as there are two first-class evening institutes within easy reach of Loughton. Some of the club-night lectures and film shows are,

Club member Bill Patten G3PAT uses an HRO receiver and a home-built top-band transmitter. He has ten coil packs for the receiver which covers the medium waveband and all the amateur bands up to $30 \mathrm{Mc} / \mathrm{s}$. Some of these coil packs are band-spread. To change the frequency of the transmitter, Bill has to solder in different coils.


Club chairmon Bill Sheppard G3JBS is extremely proud of his home-built 280-watt linear amplifier, shown on the left. It cost him under $£ 4$ to build. As you can see from the other illustration, Bill has gone "part commercial" with a KW2000 1.8 to $30 \mathrm{Mc} / \mathrm{s}$ transceiver.
of course, of an instructional nature.
Like many other clubs up and down the country, Loughton is affiliated with the Radio Society of Great Britain and holds an annual field day. Most members participate and all have the time of their lives, whatever the weather conditions. Each year field day takes place in the grounds of the Rainbow and Dove public house, Hastingwood, which is between Epping and Harlow. Wing-Commander Martin Railton's G8AB call sign is always used on field day. Although the weather for this year's event -held on 4th and 5th June-was the best ever, the portable generator failed and it took nine hours to put it right. Only one hundred and forty-six calls were logged in the twenty-four hours.

Last November the club was involved with the Television Viewer's Council and the British Amateur Television Club in a closed-circuit television exercise to demonstrate the potential of television in education and community life. This demonstration took place at Loughton Hall, with the B.A.T.C. driving the vision equipment and club members operating the sound gear.

Full three-camera productions were put "on-the-

air" under the direction of a professional producer from one of the independent television companies. Other professionals, from the Independent and BBC television organisations, had a hand in the productions and all in all more than 100 people were involved. Club chairman Bill Sheppard G3JBS and club member Jim Brett G6MJZ/T worked extremely hard to make the experiment the success it was. Jim, who is also a member of the B.A.T.C., frequently rigs up his closed-circuit television apparatus at Loughton Hall for club exhibitions and mobile rallies.

The camera outputs were used to feed large-screen monitors in the public viewing rooms in Loughton Hall and to a video recorder. An edited version of the three days' transmissions was shown to members of the Television Viewers' Council, whose annual conference at Loughton Hall coincided with the closed-circuit television experiment.

If you live in or around Loughton-or for that matter only visiting the area-do call in on clubnight. Club secretary Jim Bunce will be only too pleased to let you know the times and dates; his address is 60, Deepdene Road, Loughton, Essex.

Jack Atkinson G3OPA is another "part commercial" man with a KW2000 transceiver. He is building a 190-watt linear amplifier (shown left) to go with this outfit and has several home-built items, including a Practical Wireless grid dip oscillator.


Practical Wireless invites club secretaries to send details of their own club to the editor.


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太 Powse counting diseriminator
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