# PRACTICAL 

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saves wear on soldering iron bits

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## THE MOST ATTRACTIVE COMPETITIVE VALVE

 LIST IN THE COUNTRYAll valves are new and unused unless otherwise advised

| 1 Valive Bd．，2－11 1／－． FREE for 12 or more valves． | 3 MONTHs GUARANTEE <br> in writing with every valve． |  |
| :---: | :---: | :---: |


| OZ4 | $4 / 6$ | ${ }^{6 /-2}$ | 18j－DL32 |  | EZ80 | $5 / 9$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{17}$ | $8 / 36$ | 5／9 20 | ${ }^{9 / 6}$ DL | 5／－ | EZ8 | － | U24 |  |
| $1{ }^{\text {ch }}$ | 7／－6 | 2／－201 | 12／6 DL | $6 / 6$ | FC4 | ${ }_{81}$ | 0 |  |
| $1{ }^{105}$ | 71－6K7 | 4／9，20P | 1／／－DL | 7／3 |  |  | U2 |  |
| 1 DB | 9／9 6K8 | 5－20P5 | 15 | 1／3 |  | 6 | U31 |  |
| ${ }^{1} 1$ | 8 8－8 | 25 | $8 /$ EA | 6／9 |  | 16 | U33 |  |
| 1 L | 3／－8K | 8／6 25 LbGT | EA | 4／－ | GZ | 16 | U3 |  |
| 11. | 4／36L1 | ${ }_{9 / 6} 23 \mathrm{Y} 5 \mathrm{G}$ | 8／－EAF42 | $8 / 3$ | HK |  | U3 |  |
| $1 \mathrm{LN5}$ | $4 / 6 \mathrm{cLb}$ |  |  | 1／3 |  |  | U5 |  |
|  | $8 / 96 \mathrm{LL8}$ | \％ | Eb |  |  |  | U5 |  |
| 1 R 5 | 5／6 $6 \mathrm{LL18}$ | 11／625 |  | 3 3－ |  | － | 1 |  |
| $1{ }^{105}$ | 5136 LD | 7 | $1 \% 6 \mathrm{~EB}$ | $4 / 9$ |  | 819 | U1 |  |
|  |  |  |  |  |  | － |  |  |
|  |  |  | EB |  |  |  |  |  |
| ${ }_{2}{ }^{\text {2 } 21}$ | ${ }_{5 / 6} / 6.6$ | 3JF | 16 EBF | 9／6 | KT55 | 17／8 |  | － |
| 3 A |  | 816 | 6 E | 析 | KT\％1 |  |  |  |
|  | 81968 |  | 9／9 EBL | $10 / 9$ | KT63 | 4／6 |  |  |
|  | ${ }_{7}^{4 / 9} 68$ |  | 9／6 | $4 / 9$ |  | 3／6 |  |  |
| ${ }_{3} 54$ | 5／－${ }^{\text {B }}$ | $5 / 933$ | ${ }_{13 / 6}^{7 / 6 C 9}$ | $8 / 6$ | KT38 | 19 1－ |  | 16 |
| $3 \mathrm{3V} 4$ | ${ }^{8 / 6.65}$ | $4 / 930 \mathrm{P}$ | $9 / 3$ E | ${ }_{4}^{7 / 6}$ |  |  |  |  |
|  | ${ }_{81}^{9 / 6} 68 \mathrm{BH}$ | $3 /$ 30PL13 | ${ }^{9 / 6} \mathbf{6 C L}$ |  |  |  |  |  |
|  | ${ }_{568685}$ |  | ${ }_{8 /-\mathrm{ECC3}}$ |  | KTZ | 11／－ |  |  |
|  |  |  | ${ }_{8 /-}^{81}$ ECC | 519 |  | 3 － |  |  |
|  | ${ }^{4 / 9} 9685$ | ${ }_{4 / 9}{ }^{\text {8／35 }}$ |  | ${ }^{9 / 8}$ | LN152 | ${ }^{176}$ |  |  |
|  |  | ${ }_{59}{ }^{1 / 351}$ |  | 81／ |  |  |  |  |
| 6Y49 |  |  |  | ${ }^{6 / 8}$ |  | 17 |  |  |
| $58 \mathrm{5z4}$ | ${ }^{9 / 18}$ |  | ${ }_{719}^{8 / 8.1}$ |  | N108 |  | UB |  |
| ${ }_{6}^{624}$ | ${ }^{7 / 6}$ |  | ${ }_{8 / 6}{ }^{\text {E EC }}$ | 7／6 | N152 | $8 / 8$ |  |  |
|  | 9 | $4 / 950$ | $7 / 6$ | ${ }_{8 / 8}^{9 / 8}$ |  |  |  |  |
|  |  |  | 9／6 | $8 / 3$ | Pabc |  |  |  |
|  | 9／9 $9 \times 5$ | ${ }^{81}$－618 ${ }_{61}$ | ${ }_{11 / 5}^{176}$ | 1019 |  |  |  |  |
|  |  | 62 B | 13／6 |  |  | ／6 |  |  |
|  |  |  |  | $\stackrel{816}{7}$ |  |  | UCL |  |
|  | 2919 | $7_{78} 8^{78}$ |  | $8 / 6$ |  | 1 |  |  |
|  | ${ }_{51-7}$ |  |  | $8 / 6$ |  | ， |  |  |
| ALL5 | 3／3，744 |  |  |  |  |  |  |  |
|  | 3－724 | 185 |  | ${ }_{12 /}^{10 / 6}$ |  | ${ }_{7}{ }^{6 / 8}$ |  |  |
| ${ }_{8 \text { BATE }}$ | ${ }_{10 c 1}^{81}$ | 11／6 | 491－ | 10／3 |  | 2／－ |  |  |
| 8 A | 7 |  | 14／－ | $3 / 3$ | PC | 1－ |  |  |
|  | ${ }_{8 / 6,10 \mathrm{~F}}^{5}$ | $10 / 6$ | 319 |  |  |  |  |  |
|  | 3／－10F18 | 10f－ |  | 716 |  |  |  |  |
| bas | $5 / 61010$ | 14／6 |  | 81 | PCL | $10 / 6$ |  |  |
|  | 5／8－108 | ${ }_{9 / 6}$ | ${ }_{7}^{\text {\％／6 EF4 }}$ | $6 / 9$ |  | 3／9 |  |  |
|  | 8／6 10 P | 7／－ 6 | $9 / 6$ |  |  |  |  |  |
|  | 5／912A | ${ }^{2 / 3} 13^{3} 6$ | 9／8 EF5 | 3／ | PL33 | ／6 |  |  |
| ${ }^{88}$ |  |  | ${ }^{7 / 6}$ EF30 | 4／8 | ${ }_{\text {PL }}$ | $9 / 6$ |  |  |
|  |  | ${ }_{5 / 6}$ | ${ }_{4}^{3 / 9} 1 \mathrm{EPF}^{\text {EF }}$ |  | PL33 |  | UY |  |
|  | 71912 A | 91－9 | ${ }_{5 / 9}{ }^{\text {E EF }}$ |  | ${ }_{\text {PL88 }}$ |  |  |  |
|  | $5 \cdot 12 \mathrm{~A}$ | ${ }^{81-97 P}$ | $2 / 6 \mathrm{EF9}$ | 3 ／． | ${ }_{\text {PL83 }}$ |  |  |  |
| ${ }_{605}^{60}$ |  | ${ }_{87}^{87}$ | ${ }^{7 / 8}$ EE | 3 － | $\mathrm{PLL}_{184}$ |  |  |  |
| ${ }_{6} 6$ | ${ }^{3 / 8128}$ | 7 | ${ }_{69} / 9^{\text {EFF }} 184$ | ${ }_{9 / 8}^{9 / 8}$ | PM84 | 8 8－ |  |  |
|  | 11－128 |  | 8／－EK32 | $7 / 8$ | PX4 | 12／6 |  |  |
|  | 1 | $5 / 8$ | ${ }_{13 / 6}$ | 319 |  |  |  |  |
| ${ }^{6 D 2}$ | 3／812 | 171 | ${ }_{7 / 6} 16 \mathrm{EL3}$ | 11／6 | ${ }_{\text {P }}^{3} 39$ | 101－ | 33 |  |
| ${ }^{\text {ad6 }}$ | ${ }_{3 /-12}$ | $1 / 9$ D7 | ${ }^{3 / 3}$ |  | y33 | 10／6 | X85 |  |
|  | 419125 |  | 1／6 EL3 |  | Y8 |  |  |  |
| 速 | $7 / 612 \mathrm{~L} 7$ | DA | $4 / 8 \mathrm{EL}$ | \％ | ${ }_{\text {PY82 }}$ | $5 / 9$ |  |  |
| b88G | 4／612K | ${ }^{19}$ | $7 / 3 \mathrm{EL}$ | $8 / 9$ | PY83 | $8 / 9$ |  |  |
| ${ }^{8 F 13}$ | ${ }^{4 / 9} 1112$ |  | 8／9 ELS4 | $8 / 8$ | Y8 |  |  |  |
| ${ }_{6 F 15}$ | ${ }_{8 / 6}^{9 / 8} 12$ | ${ }_{7}$ | \％／3EL91 | 8／9 |  |  |  |  |
| $8{ }^{19}$ | 8／－12807 | ${ }^{4 / 6}{ }^{\text {D }}$ D | \％／6ELS |  | $\mathrm{PzZ30}^{\text {a }}$ | 9／8 |  |  |
| ${ }_{\text {8F32 }}$ | ${ }_{4}^{4 / 91-128537}$ | 5／6 ${ }^{3 / 6 . \mathrm{DH}}$ | $5 / 8 \mathrm{EM3}$ | 878 |  |  | 288 |  |
|  | $1 / 81 / 28 \mathrm{E} 7$ | ${ }_{4} / 6{ }^{\text {DK33 }}$ | ${ }_{9 / 8}$ EM | ${ }_{8 / 9}$ |  |  |  |  |
|  | 4／3 128N7GT |  | 5／6 | 16 | SP | － | ${ }_{\text {TYPES }}^{\text {Le＇s }}$ |  |
|  | 3／－12887 | 8／6 DK92 | $7 /$ EN31 | 181 |  |  |  |  |
|  |  |  |  |  |  |  | LISTED |  |
|  | ${ }^{6} 818$ |  |  |  |  |  |  |  |
|  | 818198 GB | 147－DL35 |  |  |  | $8 / 6$ |  |  |
| ${ }_{80}{ }^{\text {dig }}$ | ${ }_{7619}$ | 6 DL／5 | 8－－EZ41 |  | 118 |  |  |  |

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| $\begin{aligned} & \text { PROFESSIONAL TAPE } \\ & \text { RECORDER } \end{aligned}$ |  |
| MayFAIR FT157．Six Trangitor， |  |
| Push hut ton Costrols，Tape，Ideal |  |
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| Fruish with Mike，jim．Tape，Telephone |  |
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| CONNECTING WIRE |  |
| Pr，M，Bright Coloura．Five |  |
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MAINS TRANSFORMERS Excellent Quslity Guar
1pright mounting $250-0-250 \mathrm{~V}$
tif） $\mathrm{mA}, 6.3$ V $3 \mathrm{~A}(80 \mathrm{~mA} 12 / 6)$ Ditto semi－ghronded $9 / 6$ ． 9／6

13 CHANNEL T．V．s
Table Modele．Famons Makes．Abso－ exthat led in value due to huge purchase ：rect frum source．They are untested
ind hul kuaranteed to be in worling nd mind uaranteed to be in working
14in．£2．19．0 17in．£4．19．6

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Exxeluent．Bizes i－3 watt．
100 CONDENSER8 $9 / 6$ Mimiature Ceramic and Bilver Mica
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GUARANTEED TOP QUALITY Huge reduction．Red Spos
standard L．F．type now only Whit Spot P F 2／－
Mullard Matched Qutpat Kits $12 / 6$ R．F．Kits OC44，OC45（2）． $12 / 6$ 3 transistors．

| AF114 | $8 / 6$ | $0 C 44$ | $5 / 6$ |
| :--- | :--- | :--- | :--- |
| AF115 | $7 / 6$ | $0 C 45$ | $5 / 6$ |


| AF110 | $7 / 6$ | $0 \mathrm{OC} \%$ | $5 / 6$ |
| :--- | :--- | :--- | :--- |
| AF11\％ | $7 /-$ | 0 O 81 | $\mathrm{~B} / 6$ |


| AF11\％ | $71-$ | $0 \mathrm{c81}$ | 6 |
| :---: | :---: | :---: | :---: |
| AF12\％ | 9／6 | OC810 | $6 / 6$ |
| 0C28 | 12／6 | $0 \mathrm{C82}$ | 81／ |

$\begin{array}{llll}0<36 & 14 /- & 0 C 170 & 8 / 6\end{array}$
GERMANIUM DIODES
General Purpose miniature detector， A．V．L．etc．
Gold Bonded highent arabis． Gold Bonded highen rasily．Indi－ idualy teated．
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Guaranteed periormance Top Makw Tested 250 V working．
$\underset{(3 \text { for } 8 / 6)}{100 \mathrm{~mA}} 3 / 9 \quad \underset{(3 \text { for } 19 / 6)}{250 \mathrm{~mA}} 7 / 6$ VALVE HOLDERS，Bī6，Gd．es．，with Screen 8d，ea．，B9A 6d．e3．，with Screes 8d．es．Int．Gctal 6d．，Mavds Octal 4d BA Bd，（tess $15^{\circ}$ o la dozens）．

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| ELECTRIC MOTORS． ACIDC 3－8 volts．Totally enclosed standard mountang，powerful v pnileys， $7 / 6$spare jrushes，2in．x 2ix． |  |  |  |  |  |  |
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## ELECTROSTATIC

## SPEAKERS

Type LSH\％5．Orikinally $25 / \mathrm{F}$ ．Ae fitted to tierman Hi－Fi Radios．Bargain 5／－～，

ACCUMULATORS
Bmall 2 volt $3 \mathrm{amp} / \mathrm{hour}, 3 / 6$ each．

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 $20012 \overline{\text { लि }} 0 \mathrm{~V}$ a．c． $350.0-350 \mathrm{~V} 150 \mathrm{~m}$ m． 6.3 V 5 amp， 5 V 3 amp ．Gift $27 / 6$ ．
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F．M．agang $15+15 \mathrm{pf}$ gtandard wh slow motion．3／9．AM／FMS 500 pi and 15 pf ． 2 gang wilh slow motion，$/ \mathrm{g}$
Standard .0005 g gang， $4 / 6$ ， .00052 gang， $4 / 6$ ．

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For 230 V a．c．Powerful，celi－atarthe weight $11 \mathrm{lb} ., 12 / \mathrm{B}$ ．

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HIFI 10 WATT AMPLIFIER Brand New Complete $\begin{aligned} & \text { Units } \\ & \text { E7.19.6 } \\ & \text { Carr. }\end{aligned}$ Manufacturer's discontinued Model. Pushpull output. Latest high efficlency valves 'Mual separately controlled Inputs for Controls. HIgh Sensitivity. Output for 3 or 15 ohm speaker, Guaranteed tested and in perfect working order.

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A highly sensitive Push-Pưl hish output unit with self-contained Pre-amp. Tone Control Stages. Certlfied performance flgures compare equally with most expensive amplifiers avallable. Hum level 70 dB down. Frequency response $\pm 3 \mathrm{~dB}$ $30-20.000 \mathrm{c} / \mathrm{s}$. A speclally designed sectionally wound ultra linear output transformer is used with 807 output valyes. All components are chosen for reliablity, S1x balver are used Eras. Separate Bass and Treble Conbo7, Gzz34. Separate Bass and reble con trois are provided. Minimum mput required ANY KIND OF MLCROPHONE OK AICK-UP IS SUITABEE The unit is designed for CLCBS, SCHIOOLS: DOOR FUNCTIONs. etc. For use with Electronic ORGAN: MASA, LEAD OR etc, For standard or long-playing records. OUTPUT SOCKET PROVIDES
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In walnut veneered cabinet. Gauss 12.000 Ines. Speech coll 3 ohms or 16 ohms. Snly e4.19.6. Carr. $11 / 3$ and 9 monthly payments of $11 / 3$. H0 WATT MIFI IN CABINETS. SIZ $18 \times 18 \times 101 \mathrm{n}$. Finlsh as above. Only 87.19 .6 . Terms: Deposit $17 / 9$ and 9 monthly payFor larger types see page 2 .
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High-fldelity push-pull output. Separate bass and controls. Twin separately controlled inputs so that and plek-ups can be used at and pick-ups can be used at speaker is a heavy duty high flux $121 n$. 20 watt model with cast chassis. Sturdy cabinet is covered in pleasing shades of Rexine/V ynair. Model Size approx. $18 \times 18 \times$ 8in. Only 19 EnS. Cair
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A hishly efficient unit incorporating massive 15 in . high flux loudspeaker specially constructed to withstand heaviest load conditions. Rating 25 watts. Individual bass and treble controls give ample "Boost" and cut Two high impedance jack socket inputs are separately con-
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approx. $24 \times 21 \times 13$ ynair. Size
Operation approx $24 \times 21 \times$ x
from $200-250$
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TYPE BGI
Suitable for Bass Guitar. Speaker Flux. 15 inin HIISI Flux, 15 ohms. 30 watts. Cabinet size approx. $24 x$ $19 \frac{1}{2}$ Eins. Or $43 /$ and 12 monthit

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| EnS. |
| $7 / 6$ |

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Based on a current Mullard design and eraploying valves ECC8s, ECCB3, ECLB6, ECL86. ZOL86, EC1.86, ERB1. Ontput transformers are hbly quality sectionally wound to required specificution. Output matchinge for 3 and 15 ohm speakers on each channcl.
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SENSITTVITY: 15 millivolts maximum
HARMONLO DIBTORTION (each channel)
For operation on $200 / 250 \mathrm{v}$. A. O. Mains.
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arles $200-230-250$
 $250-0-250 \mathrm{y}$ $350-0-350 \mathrm{v} . ~ 80 \mathrm{~mA} .6 .3 \mathrm{v} .2 \mathrm{a}, 0-5-6.3 \mathrm{v} .2 \mathrm{a}$ 19/9 $250-0-250 \mathrm{v}, 100 \mathrm{~mA}, 6.3 \mathrm{v}, 2 \mathrm{a}, 6.3 \mathrm{v}, 1 \mathrm{~s}$.. $21 / 9$ $250-0-250 \mathrm{v}, 100 \mathrm{~mA}, 6.3 \mathrm{v}, 3.5 \mathrm{a}$, С.Т. $250-0-250 \mathrm{v} .100 \mathrm{~mA}, \quad 19 / 9$ $250-0-250 \mathrm{v} .100 \mathrm{~mA} .6 .3 \mathrm{v} .4 \mathrm{a}, 0-5-6.3 \mathrm{v} .3 \mathrm{a}$ $300-0-300 \mathrm{v} .130 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}, 6.3 \mathrm{v}, 1 \mathrm{a}$, for
Mullard 510 Amplifier Mullard 510 Amplifies $300-0-300 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v}$. 4a, 0-5-6.3v. 3a $27 / 9$ $350-05 v .100 \mathrm{~mA}, 6.3 v, 4 a, 0-5-6.3 v .3 \mathrm{a} 2 \% / 8$ $350-0-350 \mathrm{v}$. $150 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}, 0-5-6.3 \mathrm{v} .3 \mathrm{a} 35 / 9$ FULIT SHROUDED UPRIGHT 250-0-250v. $60 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a} .0-5-6.3 \mathrm{v} .2 \mathrm{a}$ Midget type 2t x $3 \times 3 i n$. $250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, 0-5-6.3 \mathrm{v} .3 \mathrm{a} 28 / 9$ $300-0-300 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}, 5 \mathrm{v} .3 \mathrm{a} \ldots 2 \mathrm{a}$ $300-0-300 \mathrm{v} .130 \mathrm{~mA}, 6.3 \mathrm{v}$. 4a, С.T. 6.3 v . la, for Mullard Amplifier $\begin{array}{cccc}\text { la, for Mullard Amplifier } & 3 \\ 350-0-350 \mathrm{v} . & 100 \mathrm{~mA}, 6.3 \mathrm{v} \text {. 4a, 0-5-6.3v. 3a } & 28 / 9 \\ 350-0-350 \mathrm{v} . & 150 \mathrm{~mA}, 6.3 \mathrm{v} \text {. 4a, } 0-5-6.3 \mathrm{v} .3 \mathrm{a} & 37 / 9\end{array}$
$4 \mathrm{a}, \mathrm{C} . \mathrm{T} .5 \mathrm{~V} .3 \mathrm{a}$
$450-0-450 \mathrm{v} .250 \mathrm{~mA}$ $450-0-450$ Y. $250 \mathrm{~mA}, 6.3 v, 4 a, \mathrm{C} . \mathrm{T}, 5 \mathrm{v} .3$ 3a $69 / 9$ MUT] UT TRANSFORNIERS
Midget Battery Pentode 66:1 for 3S4, Small
Small Pentode, 5.0000 to 30
Small Pentode. 7/8,000 2 to $3 \Omega$. Standard Pentode $5.000 \Omega$ to $3 \Omega$ $10,000 \Omega$ to $3 \Omega$
Push-Pull 8 watts, $\dot{\text { E }}$ L84, or 6V6 to $3 \ddot{\square}$ or matched to $15 \Omega$
Push-Pull 10-12 watts to match' 6 V6 or EL84 to 3-5-8 to $15 \Omega$
Following types for 3 and $15 \Omega$ speakers Push-Pull 10-12 watts 6V6 or EL84 Push-Pull 15-18 watts, 6L6, KT66 Push-Pull Muhard 510 Ultra Linear Push-Pull 20 watts, sectionally wound 6L, KT66, EL34, etc.

MIDGET MAINS Primarles $200-250 \mathrm{v}$ $50 \mathrm{c} / \mathrm{s} .250 \mathrm{v} .60 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a} \quad . \quad . \quad 11 /$

FILA MENT TRA NSFOREMERS
All with $200-250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$ primaries $6 / 3 \mathrm{z}$. $1.5 \mathrm{a} .5 / 9 ; 6.3 \mathrm{v}$. $28,7 / 6 ; 12 \mathrm{v} .1 \mathrm{a}, 7 / 11 ; 6.3 \mathrm{p}$ 3a., 8/11: 6.3v. ba, 17/6; 12v. 1.5a twlce $17 / 6$.
SAIOTIIENG CHOKES
$150 \mathrm{~mA} .7-10 \mathrm{H} .250 \mathrm{ohms}$
$100 \mathrm{~mA}, 10 \mathrm{H} .200 \mathrm{ohms}$
$80 \mathrm{~mA}, 10 \mathrm{H}, 3500 \mathrm{hms}$
$11 / 9$
$8 / 9$ CHARGER TRANSFORMERS All with 200 -230-250v. 50 c/s Primaries; $0-9-15 \mathrm{v}, 11 \mathrm{~s}, 12 / 9 ; 0-9-15 \mathrm{v}, 2 \mathrm{a}, 14 / 9 ; 0-9-15 \mathrm{v}$. 3a. 16/9; 0-9 15v. $52,19 / 9 ; 0-9-15 \mathrm{v} .6 \mathrm{a}, 23 / 5 ;$ 0-9-15v. 82, 28/9.
ALTO (Ntep up/Step down) TIRANS. $0-110 / 120-230 / 250 \mathrm{v}$. $50-80$ watts, $13 / 9: 250$ watts. $49 / 9 ; 150$ watts. $27 / 9$.
MICROPHONE, TRANSFORMERE
i20:1 high grade, clamped, 819 .

## bentley acoustic corporation ltd．

Suppliers to H．M．Government． 38 CHALCOT ROAD，LONDON，N．W．I Telephone：PR！MROSE 9093

## NEAREST UNDERGROUND：CHALK FARM． <br> ALL GOODS LISTED BELOW ACTUALLY IN STOCK ALL GOODS ARE NEW，BEST QUALITY BRANDS ONLY，AND SUBJECT TO MAKERS＇FULL GUARANTEE，PLEASE NOTE THAT WEDO NOT SELLITEMSFROM USEDEQUIPMENT NOR MANUFACTURERS＇SECONDS \＆REJECTS

| OAZ | $4 / 6$ | til38 | 251－ | 7Ai 12／6 | $25 \mathrm{Y} 5 \quad 7 / 9$ |  | KAEO 1／6＇ | EL35 10／－ | KTwne 5／6 | Q1－2．5 5／－ | 147， $8 / 6$ | AFled 11／ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 St 2 | $61 /$ |  | $8 / 0$ | 7 Bi 12／6 | －559 $7 / 9$ | 11）12，6 | F．．17\％8／9 | F1．36 8／9 | КTWrs 5； | 25\％520 10／6 | 1＂20＇ $4 / 9$ | AFles 10／8 |
| OZ4i？ | 4，3 |  | 5／－ | $7157 \quad y / 6$ | 25loti $71-$ | ACJPEN／ | EADC80 $3 / 9$ | N1．3i $12 / 3$ | KTZ41 5／0 | QS130／159／6 | $15 \pm 4 / 6$ | A F126 10／－ |
| 1 A 3 | $2 / 6$ | bilisit | 4／－ | Itis $8 / 0$ | 2．う\％$\quad 1 / 3$ | （1） $23 / 8$ | EAt＇91 3／3 | ELil $/ 18$ | $1.6331-$ | R14 15／－ | L＇ti $4 / 6$ | AFl27 9／6 |
| 1 A 4 | 12／4 | 1 m ¢ | 2／3 | 7 CH 13／9 | ご\％fite 81－ |  | 18AF42 \％／6 | EL4， 716 | $1{ }^{1+150 \%}$ bi＝ | R12 | 3／5 | FYZ13 11／6 |
| 1．45 | $55^{-}$ | 皆交 | 4／－ | 7\％5／－ | 27 2il 23.3 | ACIMES | E1334 1／－ | EL\1 8／3 | LN302 7／9 | K1尔 291－ | 11 | （ill 3 5／6 |
| 1A7BT | $7 / 9$ | HC\％ | 3／－ | I113 15／－ |  | （i） $17 / 6$ | EBH1 4／9 | FLSA $6 / 9$ | LN319 8／6 | 1317 17／6 | $1 \begin{array}{ll}101 & 19 / 6\end{array}$ | （114i 5／6 |
| 161 | 41－1 | $\mathrm{SC}^{4}$ | 3／－ | 7W，14／6 | 3n土 1 6／6 |  | Firal $2 / 3$ | EL84 4／6 | L．P？0／8 | 114 9／6 | U1い 17／6 | （illy 10\％ |
| 163 | 8／－ |  | 1019 | －15 $14 / 8$ | 3410 | （7）17\％－ | Wist＇3 20／8 | F．LW3 $\quad 7 / 6$ | LZ319 6／8 | R1H $6 / 6$ | E191 $0 / 6$ | 4ETlos 7\％ |
| 103 | 6／6 | 1tc 10 | 8／－ | $7147 \quad 5 / 9$ | 216－14 10／8 | AC／40 $22 / 6$ | E．3193 b／－ | Elum $7 / 3$ | L7．329 $\quad 8 / 6$ | R6：7／8 | $\underline{1271}$ | OFT16410／－ |
| 105 | $5 \%$ | ＇t＇t？ | 6／－ | 7に7 12／6 | S11F $5 / 9$ | AU／GG／VA1 | EHETL 616 | EL91 2／6 | ME4L 13／－ | HG1／240A | $\begin{array}{ll}\mathrm{U} \times 21 & 8 / 9\end{array}$ | GET $10 \% 17 / 6$ |
| 106 | 10／6 | fieljeg | 18\％－ | $7 \mathrm{~V} 7 \quad 5 /-$ | 析FL1 9／3 | 12\％－ |  | EL9．3 $5 / 6$ | MEy 12／6 | 54／－ | 12\％2 12／3 | \＃ETい112／－ |
| 155 | 6／8 | 6CHt | 5／－ | 7 Y 4 5／－ | 3141.15 | Ar＇TH1 15／－ | E BC90 3／2 | EL350 2\％－ | MH\％3／6 | RK34 18 | $1130111 / 6$ | （FFT118 8／9 |
| 1 DH | $8 / 8$ | tic＇W4． | 24／－ | 4112 $2 / 6$ | ：311：15 9／3 | A $1 / \mathrm{TP}$ 181－ | F．bcy $5 / 6$ | E1．N：0 16／4 | MH［4 $7 / 6$ | 8130 2216 | V＊29 0／－ | （1）T114 6／8 |
| 1－1）1 | 8／－ | 1］1 | $1 / 8$ | \＄136\％9／8 | （101） $412 / 3$ | A ${ }^{\prime \prime}$ I＇1 12\％ | FRF40 5／9 | EJx： 1810 | MFILDO12／6 | SP1S 1916 | $\begin{array}{ll}\text { U33y } & 8 / 6\end{array}$ | HEX3S 3／－ |
| 1 Fis9 | 3／6 | 6103 | $9 / 1$ | 913 $31=$ | 3世1）7／8 | A＇Y＇P $291-$ | FBrFx ${ }^{\text {a }}$ | F1， 180 | MLib $\quad 5 / 8$ | sulse 12／e | 174038 | （1）EX3t 10\％－ |
| 16 | $81-$ | HIDH | 3／－ | 9127 7／6 | 301P14 5／3 | － $5142 / 3$ | FiBFs： $6 / 3$ | EM4 17／9 | M3413 20／5 | \＄P41 2／－ | 1704 6；－ |  |
| 1HouT | $7 / 9$ |  | 9／6 | 11018 | い11＇9 12／3 | $\begin{array}{ll}4 \% 1 & 5 / .\end{array}$ | FMLSL 10／P | EM34 11／6 | MSP4 12／－ | $\begin{array}{ll}\text { N1，} & 1216\end{array}$ | Usul $18 / 8$ |  |
| 1L4 | $2 / 3$ |  | 9／6 | 1062 $12 / 3$ | 31PL1 8／8 | A 231 6／6 | W65） $4 / 8$ | EMM35 12\％ | st12／144／6 |  | प4020 6／6 | GEXGR 15／\％ |
| 11.44 | 17／6 | Cipig | $3 / 9$ | 11191 | 301PL！${ }^{\text {a／8 }}$ | 47.416 | V053 1216 | EM71 15／a | M X $40 \quad 8 / 9$ | SU25 27／2 | $V M P 9$ 11／9 | \＄AT100 7／8 |
| 1LA！ | 16／10 | birdit | $7 / 6$ | l012 $11 / 8$ | 201＇L14 $12 / 6$ | $\begin{array}{ll}13 i 1 ; & 4 / 8\end{array}$ | FCot 6f－ | Evin $6 / 3$ | \＄37 $23 / 3$ | 「41 | $\because \mathrm{Ms} 4 \mathrm{~B}$ 12j－ | MAT101 $8 / 8$ |
| 1 L .15 | 4／＝ | fiF7 | 5／－ | InFi 101－ | 3.3 12／8 | 1 Lff $10 / 8$ | E（27）4／8 | EMAI \％ | ＊i4 28／6 | Tul2 12／6 | VP\％ $3 / 6$ | MA＇1120 $7 / 9$ |
| 1LN5 | 4／6 | firs | $5 /$－ | lurs 9／9 | ：35151 12／6 | $\cdots 1012 / 8$ | Er90 $2 / 3$ | EM44 6／8 | 108 28／2 | T13134 $7 / 6$ | $\checkmark \mathrm{VP} 213 \quad$ O／6 | MAT121 8／8 |
| 1N54T | $8 / 6$ | HFll | 17／0 | l1\％14 9／9 | 3．4． $20 / 9$ | （1）${ }^{195} 12 / 8$ | Ereyl $4 /$－ | EMs5 8／9 | इ349 15／－ | TH4B 15／－ | V1！14／6 | OAS 8／－ |
| 1 Pl | 8／－1 | til＇ie | $3 /-$ | 101．1） $6 / 3$ |  | －hinat 8／8 | Et＇y］6／6 | EM＜2 7／8 | P41 3／8 | TH：LU 10／6 | VriA $14 / 6$ | OA10 8／6 |
| 1 Pl 10 | 4／6 | 6113 ${ }^{\text {d }}$ | $3 / 9$ | 101．111 ¢／f | 浱W＋4／9 | CL4 19／6 | E（－31 7／3 | EN31 10\％ | P61 2／6 | 1H41 10／－ | VP4B 29／－ | vaig 2\％ |
| 11＇11 | 5／3 | 61－14 | 23／8 | 10P1：3 8／3 | （1，\％ 131612 | （1，a3s 11／6 | Frrse $41-$ | ENW1 5／6 | PABC80 6／9 | TH233 619 | VPs．80 7／－ | UAF：3／－ |
| 1 RS | 4／－ | 61F15 | 819 | 111114 11／6 | （1，\％W WT 4／4 | （＇1）2／6 | E1＂33 29／1 | EXil 5／9 | PU＇si 10／3 | Tド2 5 － | $\because 1+36$ | \＃A79 3／－ |
| 14．1 | 5／－ | 11\％ 17 | 12／6 | I110．i $17 / 6$ | 35\％ら心T 5／コ | （－1．3 10／6 | Fu－3 ${ }^{\text {Fu }}$ 21\％ | EY゙－／3 | $\begin{array}{ll}\text { PC＇ss } & 9 / 8\end{array}$ | TP？5 5／－ | VP41 5／－ | UAS1 3／－ |
| 185 | $3 / 6$ | iff 18 | $13 / 5$ | 116.1 17／8 | ：31 12／6 | けrj $14 / 6$ | E1 $13551-$ | ESQ3 9／3 | P4：15 11／3 | Tr゙2h20 716 | $\square 5133819$ | UA85 3／－ |
| 1＇T3＇ | 29／＊ | if：${ }^{\text {a }}$ | 618 | IIE゙ 15／－ | ．9 2／t， | $1 \begin{array}{ll}1-12 / 6\end{array}$ | WCry\％\％1－ | EYy 9／6 | 1047 7／9 | TY4tip $11 / 8$ |  | ＂A＊）4／J－ |
| 1T4 | $2 / 3$ | RFet | $8 / 6$ | 11183 | 403CA 6／6 | （V42\％10／－ | EMrめ3 3／6 |  | PCisal $5 / 6$ | 1．－1134 $405 /-$ | VRIus 5／6 | 0． 210030 |
| 104 | $5 / 6$ | HF3 | 8！－ | 12A； 213 | 41NTL 8f－ | $\begin{array}{lll}1-11 & 16 / 4\end{array}$ | Rucys 4／6 | Eどヶ\％8／9 | Peters 6／b | リAF゙せ $71-$ | VR150 4／8 | 0．a！ $31 /$ |
| 145 | $5 / 3$ | セドア3 | $8 / 6$ | 10 AX 16／6 | 41．3＇山 15\％ | IVJC $6 / 0$ | Etcs3 4／6 | EYyl 3／0 | PCMs 10／6 | UB41 10／E | VTiciA 7／－ | GAYD 3／6 |
| 2 A 7 | 12／8 | biti | $2 / 6$ | 12AC6 8／6 | 425 51－ | 以゙31 5／9 | ECCSy 5／6 | EZ35 4／6 | $\underline{P}(x \times x y 816$ | UBE＇41 8／3 | VT501 3／－ | UAD10 9／8 |
| 2026 | $2 / 9$ | ${ }_{6} \mathrm{H}^{5}$ | 1／6 | TVA106 9／6 | $4310 \%$ | 01 1／3 | ECcs3 $5 / 9$ | E／740 5／3 | PCClsy 10／6 | UBi＇81 $8 / 3$ | V1111 5j－ | OAZP10 7／6 |
| 21130 | $7 /=$ | $6 J 5 \mathrm{C}$ | 31. | 1－2E6 81. | $4517 / 0$ | 1） $1.513 / 8$ | －EuC88 810 | EZ41 8／－ | PCFs0 6／6 | UBF80 $5 / 9$ | VU120 10\％ | OA211 13／6 |
| $2 \mathrm{2D} 21$ | 5／6 | 655 GT | $4 / 3$ | 12AH7 5／－ | 4526GT 15／－ | $1) 42$ 10／6 | ECC18911／6 | F280 8／8 | PeFsz $6 / 8$ | UBF89 6／9 | VU120A101－ | UCl6W 35／－ |
| ${ }_{2 P}$ | 23／3 | 6．J3 | 310 | 12AH8 $10 / 9$ | 50As $21 / 10$ | I川33 5\％－ | Eicsor 15／－ | EZ81 4／－ | PCFS4 8／6 | U3Lis 10／9 | VU133 7／－ | OC13 25／． |
| 2 x 2 | 3／2 | $6 \mathrm{~J} 7 \mathrm{a}$ | $4 / 6$ | 12．T＇9 4／6 | $\begin{array}{ll}31135 & 6 / 6\end{array}$ | $15: 7$ 2／3 | ECFso $6 / 6$ | EZ90 3／8 | PCF86 7／8 | VC9\％ 613 | What $6 / \%$ | $\mathrm{OC}^{22}$ 83／． |
| 3A4 | $3 / 9$ | 6J7GT | 71 | 12＋T7 3／6 | 5以年 8／8 | JaC32 7／9 | ECFS2 6／3 | FCL $14 / 6$ | PCFs01 101－ | UCC84 819 | $\mathrm{W}^{\mathbf{W}+2}$ 29／－－ | OC23 57／－ |
| 3A5 | 6／9 | 6．13 | 12／6 | l2Al＇6 5／日 | 30CDEG40／9 | Hapy 3／8 | ECFR 11／3 | 4819 | PUF゙S（1） $10 \%$ | VCress 616 | Wh1M 24／6 | UC25 12／ |
| 8 B 7 | $5 /$. | 6K9GT | $5 / 8$ | $1 \because A リ 74 / 6$ | 50h，ita＇ $6 / 3$ | bargo 8／－ | EC＇F404 24／－ | FC13 14／6 | PC＇Fsus 10／6 | CCF＇s 818 | Wh3 $10 / 8$ | OC26 85\％ |
| 314 | $3 / 9$ | 施ご； | 1／3 | 12AV＇r 6／6 | 52kU 14／6 | 以く¢0 6／9 | ECH3 28／3 | FC13C 17／－ | PCL8： 616 | LCH21 81－ | W－7 $3 / 6$ | Or28 23／－ |
| 3Q4 | 5／3 | 6K7ct | 4／－ | $\begin{array}{ll}12 \mathrm{~A} & 4 / 6\end{array}$ | J3EU 14／8 | 1）94 12／8 | ECHO1 91－ | FW4／5008／6 | Prise3 710 | $\mathrm{I}^{\prime} \mathrm{GH} 428 \mathrm{l}$ | $\begin{array}{ll}W 77 & 2 / 8\end{array}$ | （1） $16 / 8$ |
| 3Q6GT | $7 /$ | 6K8G | $3 / 3$ | 1：1年7919 | 72 6／6 | 1141 10／8 | E1＂H3： $22 / 8$ | FW＋／4008／6 | Pe1，44 718 | 1＇thul $8 / 6$ | Wsim 5／9 | 9／8 |
| 384 | 4／6 | 1Fを硣 | 1816 | 1こBA3） $6 / 9$ | 77 5／－ | 1）15 7／8 | EGH3 $6 / 6$ | （1TH 919 |  | Uじいいこ 719 | W101 $26 / 2$ | O6：36 21／6 |
| 3 Y 4 | 5／31 | 1ik\％3 | 241－ | 1：8EA 4／ | $4 / 9$ | 1）ETM． 710 | Eutits 81－ | G［「3）55／－ | PしLst 819 | リ＂1，¢3 9\％ | W107 10／6 | OC41 8／－ |
| 411 | $3 / 9$ | 61． 1 | 101－ | 1213F7 $81-$ | 5／3 | 13F33 8／8 | ECHE1 5／9 | 1234 7／6 | PCLBS 12／6 | 1F4 $6 / 9$ | W729 17／6 | OC4\％5／－ |
| SR4GY | 8／8 | 5Lat | 12／6 | 12EL 16／9 | $22 / 8$ | UF6t 15\％ | Echis3 6／8 | 1／332 8／－ | PEN 4 D ${ }^{\text {d }}$ | 1F゙4 419 | $\underset{14}{7 / 9}$ |  |
| 5 T 4 | T／ | aldiat | 71－ | 1－HHATT $1 / 3$ | 53 V 81－ | $11 F \%$ | ECH84 $9 / 6$ | GZ33 17／8 | 85／－ | LF80 8／3 | X18 8／－ | OCL4 813 |
| $8[46$ | 4／6 | 5L－（a＇ | $5 / 6$ | 1：559T $2 / 8$ | \＄5A2 6／6 | $1{ }^{109} 4$ | ECLA $61-$ | c234 10／－ | PEN4010 | tFs5 6／9 | $\begin{array}{ll}\mathrm{X} 94 & 18 / 6\end{array}$ | UC44PM11／－ |
| 6V417 |  | 6 L 18 | 10／－ | 12JJuT $7 / 3$ | Prat 67／B | DF9\％8\％－ | ECLRO2 6／B | ${ }_{13} 123714 / 6$ | 84／－ | 1゙「83 9\％－ | X 41 15／． | OC4\％8／－ |
| 5Y3uT | 4／9 | （ 61.14 | 19／－ | 1りk．10\％ |  | LFY7 101－ | ECls $9 / 6$ | H30 ${ }^{\text {H }}$ | PEN45 7\％－ | UF89 8／－ | $\begin{array}{ll}\mathrm{X} 61 & 8 / 3 \\ \mathrm{X} 61 & 5 / 9\end{array}$ |  |
| 5 CH | 9／8 | 61.103 | $6 / 6$ | 1K7ヵ1 $3 / 6$ | yodu 421－ | $11113015 / 8$ | ECL86 818 | HabC80 9／3 | PEN45D | Llal 718 | X63 $\quad 5 / 9$ | OC6J 28.6 |
| 573 |  | 6L．D13 | 7\％ | 1：2れなT 9\％ | 30¢ $42 /-$ | 1） 1 Litis 4／6． | Ectl． 800 | HL2 $7 / 6$ | 12／－ | V144 $28 / 3$ | x 4  <br> x 45 $5 / 6$ | $\begin{array}{ll}\text { OCti } & 25 / 6 \\ \text { Un＇70 } & 6 / 6\end{array}$ |
| $5 \% 4$ | $7 / 6$ | 6L1520 | $5 / 6$ | 120才い 3／0 | 914 16\％ | 19H74 3／6 | $26 / 2$ | 11.130 | PES $464 / 6$ | LL46 8／6 |  | $\begin{array}{ll}\text { Ue＇70 } & 6 / 6 \\ 0.71 & 6 / 8\end{array}$ |
| ${ }^{4} 301.2$ | 9／－ | HSTUT | 71 | 1ザ ！6／9 | 1303： $16 / 8$ | $1) 1178$ | EFr $20 / 6$ | If İ3 $12 / 6$ | E12N38310／3 | ULN4 6／－ | $\mathrm{X}^{631} 57 / 3$ | $\begin{array}{ll}\text { Ue71，} & 6 / 8 \\ \text { Ur＇\％} & 8 /\end{array}$ |
| ，Ansis： | $3 / 9$ |  | 9／3 | 1？N木： $4 /=$ | 13 ¢ $4 / 8$ | 1）154 23／3 | Firy 20／E | H1．23DD $51-$ | PEStu3bl | C34 15／5 | $\begin{array}{ll}\text { xibu } & 9 /- \\ \times 8\end{array}$ | Ur7\％8\％ |
| 持ち1； | 6／9 | $1 i^{1}+5$ | 8／！ | $\begin{array}{ll}1 \pm 4: i & 31 \\ 14\end{array}$ | 1＂1 13－ | 1H1い！25／－ | E＇ド 6 6／3 | 111 110 | 101－ | $13134816 / 18$ | $\begin{array}{lll} \\ 874 & 20 / 6\end{array}$ | U＇73 181－ |
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| 1，46 ； |  | 1际い | 11／6 | 1－3．1： $5 /-$ | －1 ist b／l | いにち，－19 |  |  | 1＇ENilob | LK10 6／6 | Anlm 24，1 | Wc7．81－ |
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| tiadz | 5／9 | とりう心 | 7／9 | 1き以下 81－ | Sul 20\％ | 1） 41 4／－ | E゙tu 8／9 | $9 / 8$ | $\mathrm{l}^{1} \mathrm{Las3}$ 9／－ | UU6 11／－ | Xlus 28／－ | O桨 18／－ |
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| diARt | $201-1$ | 10817 | $5 / 3$ | $4.10 / 6$ | 1tise $12 / \%$ | ！15\％4／8 | H1P80 6／8 | K13） $11 / 6$ | PTis 10／－ | 1：1： $18 /-$ | $\begin{array}{ll}7729 & 6 / 9 \\ 7740 & 6 / 3\end{array}$ | UCLIO $18 /-$ <br> UC170  |
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## Compactly buitt to be carried by one rasn．This has a range of approx． erystal controlided，tuntog irystal controued，tuntrg Le amoided，and operation phoes Frequency phoce Frequency 3.60 atetion compriciong so ofver／tranmmitter，rod marlel．One set of head－ phanes and mike，in can－ vas omarying bag．Gryetal ool unit available for Pree．Prand new in makerre beajed cartons Por sutborised ube only． Price per station <br> Sale Price <br> S3．0．0 ${ }_{10 \%}^{P}=P$ ． Two atations for <br>  86．0．0 ${ }^{\text {Porm }}$ <br> Ansessin

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Fully thterlocking copper rails．One foot sectlone． Ideal for car or mocoter acrials．Will makc excellent dipoles．Six sections complete with canvas carrying case．3／6．P．\＆P．1／6．Additional sections 6d，each． Plesse send sufficient postage．
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Atrong，Migh quality paxolin sheete size 10$\}$ x 84 I 1／10in．， 3 for 5／－．P．do P．1／－． 6 for 10／r．Post free． 4 S人A

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Housed to complact metai case．200／250 F．A．C． mains．Ontput 250 v． 50 ma A．Fully smoothed D．C． slmost any pre－amp．or radio tuner．Prioe 39／6． P．\＆P．2／6．

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R．A．F．SHORT WAVE RECEIVER
35 to $40 \mathrm{Mc} / \mathrm{a}$ ．Power supplies 12 volts and 250 volts D．C．，in excellent condition with exceptionaly tine slow－motion tuning and clean component s人 NEW WALK ROUND STORE OPEN IN LA MBERTS ARCADE LOWER BRIGGAT CYCLE SHOP．OPEN ALL DAY SATURDAY．S．A．E．WITHAAL CNGUILIES．

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| BUHLD YOUR RECORD PLAYER |  |
| :---: | :---: |
| 4 Speed Autochange 2－tone |  |
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| built．Quality outpat．Vol－ |  |
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| AJTOCHANGE EITS |  |
| Compitte－al sbove． |  |
| B．S．R．Monerch | \＄10．19．6 P．P． $51-$ |
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Complete：die，punch，Allen screw and key

| $14 / 6$ | $1{ }^{1} / \mathrm{l}$ | 181－ | lin． | $22^{16}$ |
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| Sin． 1416 | $1 \frac{1}{1 / i n}$ ． | $18{ }^{1}-$ | 2 in ． | 34／3 |
| tin． 1516 | 1发的． | 1816 | $2{ }^{\frac{3}{2} \text { in }}$ ． | 3719 |
| 1519 | 1 者in． | $20^{\prime}$ | $2 \frac{1}{2} \mathrm{in}$ ． | 4419 |
| n．18\％ | $1 \frac{1}{2} \mathrm{in}$ ． | 2016 | lin．sq． | 3116 |


FOLL WAVE BRIDGE SELENIUM RECTIFIER： 2， 8 or 12 P．， 14 smp．， $8 / 8 ; 2$ \＆．， $11 / 8 ; 4$ a．， $17 / 6$ ． CHARGRR TRANSFORHERS．Tapped input 200／250 F．for oharting at 2,6 or 12 v．＂ $1 \frac{1}{2}$ ampa．，15／6； 2 emps．，17／6； 4 amps ．，22／8．Cirenlt inelnded．


VALVE HOLDERS．Int．Oct．or Mazda Oct．6d B7G，B8A．B8G，BCA．9d．；B7G with can $1 / \theta_{\text {．}}$ B9A with can I／9．Ceramic EF50，B7G，B9A，Int Ook $1 / \%$ Valve pluse B7G．B9A，Int．Oct． $2 / 3$ ．


NEW ELECTROLYTICS FAMOUS MAKES


 \begin{tabular}{ll|ll|lr}
$2 / 350 \mathrm{~V}$ \& $8 / 3$ \& $200 / 25 \mathrm{~V}$ \& $2 / 8$ \& $10 / 600 \mathrm{~V}$ \& $1 / 500 \mathrm{~V}$ <br>
$4 / 350 \mathrm{~V}$ \& $1 / 3$ \& $400 / 12 \mathrm{~V}$ \& $3 /-$ \& $16+18 / 6$ <br>
$8 / 450 \mathrm{~V}$ \& $2 / 3$ \& $1,000 / 1, \mathrm{~V}$ \& $3 /-$ \& $34+32 / 350 \mathrm{~V}$ \& $3 / 6$

 

$8 / 400 \mathrm{~V}$ \& $2 / 3$ \& $1,000 / 4 \sim \mathrm{~V}$ \& $3 /-$ \& $32+32 / 350 \mathrm{~V}$ \& $6 / 6$ <br>
$18 / 460 \mathrm{~V}$ \& $3 /-$ \& $8+6 / 450 \mathrm{~V}$ \& $3 / 6$ \& $32+32 / 450 \mathrm{~V}$ \& $6 /-$

 

$38 / 480 \mathrm{~V}$ \& $3 / 9$ \& $5+16 / 450 \mathrm{~V}$ \& $3 / 0$ \& $50+50 / 3,0 \mathrm{~V}$ \& $7 /-$ <br>
$20 / 25 \mathrm{~V}$ \& $1 / 9$ \& $16+16 / 450 \mathrm{~V}$ \& $4 / 3$ \& $64+280 / 350 \mathrm{~V}$ \& $11 / 6$
\end{tabular}

 CONDENSERS． $0.001 \mathrm{mld.} .7 \mathrm{kV} . \mathrm{B} 0 / 6 ; 20 \mathrm{kV} ., 1016$ ； $0.1 \mathrm{mld} ., 7 \mathrm{kV} .$. 9／6；Tubular 500 v． 0.001 to 0.05 ．Ad；


 $1 \mathrm{pF} . \mathrm{J}, 2.2$ to $47 \mathrm{pF} ., 1 /-$ d dito $1 \% 50$ to $815 \mathrm{pF} . .1 /-$ ； 1 pF.$)$ ． 8.2 to 47 pF ． $1 / /$ ；ditto $1 \% 50$ to $815 \mathrm{pF} . .1 /-$ ；
1,000 to $8,000 \mathrm{pF}, 1 / \theta$.
 pF．miniature， $10 /-; 500$ pF．atandard with trimmers．
0／－；midget， $7 / 6 ;$ midgat with trimmers． $9 /-; 500 \mathrm{pF}$ ， slow motion，ntandard， $9 /-\mathrm{i}$ smal 3－gang 500 pF ．
 $5 / 6$ each Can be ganged together， 100 pF．． 300 pF. TUNING AND REACTION． 100 PF．． 300 PF．： $500 \mathrm{pF} ., 8 / 8$ each．nolid dielectric．TRIMMERS．
 MAINS TRANSFORMER $200 / 250$ v，A．C．

 MINLATURE ： 200 v． $201 \operatorname{lnA}$ ．ti． 3 v． 1 a． $10 / 6$


 HEATER TRANS． 6.3 v．， 14 a．
Ditto tapped $1.4,2,3,4,5$, ti．3
ilito，нei， 6.3 v． 4 zmp


GENERAL PORPOSE LOW VOLTTAGE $10 / 6$ $3.4,5.6,8,9,10,12,15,1 \mathrm{~m} .24,30 \mathrm{v} .28 / 6$ AUTO TRANSFORMERS． 130 w．
 $28 / 6$
$22 / 6$ Transformers，Rectiters，Condeusers，providing Transiormers， H．T．and 2 m ．

4250 v． 80 mA ．D．e． 1.3 .3 v． $3 . \overline{6}$ a．tapped 4 v

TELEPCOPIC CHROME AERIALS， 13 to a3in．． $8 / 6$ TRIPLEXERS EAnds I，II，II，12／6．COAX PLUGS $1 /=$ LEAD SOCKETS．I／，PANEL SOCKETS， $1 /$－ OUTLET BOXES（Surface or flush）， $4 /-$ Pach． BALANCED TWIN FEEDER yd．6d．， 8 n or 300 ohms． TWIN SCREENED per yd． $1 /$ ．， 80 ohme only

THE＂INSTANT＂BULK TAPE ERASER AND RECORD HEAD DEMAGNETIZER． $200 / 250$ v．A．C． 35／－
＂THE POWER MITE＂45＇－
PM9 Majns Joit 9 volt for Transistor Radios． Same vize as P．P． 9 （200／250 v．）

## 4 TRANSISTOR AMPLIFIER

Rendy bailt． $8 i z e 3 \times 1 \ddagger \times$ fin．With transformers 8 and 8 ohms output．Ideal lor hase with record plasers，intorooms．，BABY ALARMS．Complete plith instractions and oirouit．

Price $47 / 6$
NEW MULLARD TRANSISTOKS OC71，8／－；OC72．7／6；OC81D，7／8；OC81，7／8； AF11s，10／6；AF114，11／－；0C44，8／－；OC45． 8／Fi OC171，9／－；OC170，8／6：AF117，9／6； OAB1，3／－；OG86，12／6；Holders， $1 / 3$ ．Sub Min， Condensers $0.1 \mathrm{mFd}, 30$ ₹．．1 $1 / 3 ; 1,2,4,5.8,16$ ． 25，30，50， 100 mFd. ． 15 volt．2／6．
Volume Controls $80 \mathrm{chm}_{\mathrm{chbLe}}$ Coax Linear or log Tracks Semi－air spaced tin．




## B．T．H．TAPE MOTORS 115 v．A．C．

 28 w ． 12.6 pair，for $200 / 250 \mathrm{v}$ ．（in series）．
## BAKERS <br> ＇Selhurst＇ <br> 25 WATT 5 Gns． HEAVY DUTY <br> 15 OHE VOICE COLLs Renponse 20－10，000 cps Basp Remonanoo 80 epa <br> Gonuine Musical In－ <br> 

BAKERS 12in．STALWART 15w． 5 kns 3 or 15 ohms voice coils．Unlimited applications．
 BAKERS 12in．STANDARD 20w．${ }^{7}$ gns． More powerfu！magnet 14,000 lines special sus－ pension． $40-14,500$ ops．Recommended．
BAKERS 121n．BASS 25 w ．Aluminium coil Now 1965 high power model．Aluminium coil

BAKERA 15 in ．AUDITORIUM 36 w .18 mD ．
LOUDSPEAKERS P．M． 3 OHM FAMOUS MAKES． 2 in．．3in．， 4 in ．， 5 nn．， $7 \times 4 \mathrm{in}$ ．． $15 / 6$ each； $8 \mathrm{jn.} 17 /$.6 ．

WAVE－CHANGE SWITCHES，B／G each．
2 p．2－way or 2 p．G－way； 3 p． 4 －way or 1 p． 12 －why 4 p .2 －way or $4-\mathrm{p}$ ． 3 －way．
Wavechange＂MAKITS＂evallable； 1 p .12 －way，\＆ 2 6－wag． 3 p．4－way 4 p．3－way． 6 p． 2 －was．Kit pricen 1 wafor $8 / 6$ ； 2 wafer， $12 / B ; 3$ wher． $16 /-$ ．Extre walers， $3 / 6$ each．
TOGGLE SWITCHES，s．p．，2／－；d．D．，3／6；d．p．d．b．，4／m
BOOKS pleasq add postace
Bnya＇Thook of Crystal sets．

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RHillo Talve（inde，Books 1．2．3．
$\begin{array}{ll}4 \text { or } 5 \text { eitral Rindioinsidienut } & . .3 / 6 \\ 1 / 6\end{array}$
Mastir Colour code Chart．
$1 / 6$
$7 / 6$
$0 / 6$
Transistor controlied Nindels
$2 / 6$
JACKS．Standard open－circuit 2／G，olosed oironit 4／6 Grundig type 3－pin 1／3i Grundig Lead Type 3／6 Phono Plugs 1／－．Socket 1／－．Banana Plays 1／a JACK PLUGS．Soreened $3 /$ G．Grundig 3 －pin $8 / 6$ BULGIN NON－REV PLUGS and SOCKETS．P7 2－pin $4 / 3 ;$ P7s 3 －pin 4／6；P184 $6-$ pin $0 / 6 ;$ P468 $12 / 6$.
RESISTOR8．Pralerred valnes， 10 ohms to 10 mer RESISTORS．Pralerred valnes， 10 ohims to 10 mes W．：
HIGH STABLLTEY．
St 10 obms to 10 meg ．Ditto $\mathrm{o}^{\circ} \mathrm{o}, 10$ ohing to R2 mog．． 9 d ．
$\left.\begin{array}{r}5 \text { Watt } \\ 10 \text { wart }\end{array}\right\}$ WIRE－WOUND RESISTORS
15 watt $\} \quad 10$ ohms－6，800 ohms
10 K．， 15 K．， 20 K．， 25 K． 10 W．
MAINS DROPPERE．Midget．With slidera 0. she $1 \mathrm{~K} ., 0.2 \mathrm{a} ., 1.2 \mathrm{~K} ., 0.15 \mathrm{a} ., 1.5 \mathrm{~K} ., 0.1$ R．， $2 \mathrm{~K} ., 6 \mathrm{j}$ each．Line Cord 100 ohms it．S－way， $1 /-$ ． 35 日 $8 / 8$. Wirewand Ext．Spasker control，WAT．Jre－set Mid TV Typps．All whlice up in 10 ohres to $25 \mathrm{~K} ., 8 /-$ en TV Typms．All inher up to 40 K to meg．，8／－）． WIRE－WOUND 4 WATTS Pots．Imag spladie Value， 50 ohms to $50 \mathrm{~K} ., 8 / 8: 100 \mathrm{~K} . \mathrm{c} 7 / 6$.
SPEAKER FREM．Tygan various dolourn．58in，wit

EXPANDED METAL，Gold 12 I 1 Rin． $6 /-$ ．
ARDENTE 1 Pushopull to 3 ohras output $11 /$
D8084，1．6：1 C．E．Push－pull Driver
D8058，11．5：1 Output to 3 ohms，to．
D830． $4.5: 1$ Drlver
D239，i．5：1 Drjper：D240，8．5：1 Driver
TRANSISTOR POTS 5 K Switohed

| TUANSISTOR PIOTS 5 | $11 / 6$ |
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| K SWitched | $11 / 8$ |

IR－MIN EARPIECE Xtal or magnetie $7 / 6$ gIB－MLN．JACK AND PLUG 2.5 or 3.5 mm ． $3 / 6 \mathrm{mF}$ ． Blank Aluminium chassis， 18 A．w．g． 4 sides．riveted corners，latrice fixing holes， $24 n$, sides， 7 x $41 n . .4 / 9: 9 \times 71 n$. 5／9： $11 \times 7 \mathrm{in}$. ． $8 / 9 ; 13 \times 9 \mathrm{id} ., 8 / 6 ; 14 \mathrm{x} 11 \mathrm{n}$. $10 / 61.15 \times 141 n . .12 / 6$ ．

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| :---: | :---: |
| 8 Mathematics | 8 - SERVO-MECHANISMS |
| - transistors | radar \& NAVIGational |



Yol. XL No. 697 MARCH, 1965



## Diversified Interests

WE have all, no doubt, at some time or another been subjected to the frustrating boredom of the man with a one-track mind. There are countless versions: he (or she, come to that!) may be a football fanatic, a motor car maniac, a prattling philatelist, a rabid racing addict. His tastes may be low or high, academic, athletic, scientific, active or sedentary. He lives for only his chosen subject to the exclusion of all else. his pet interest has become an obsession.

Such a person suffers from the sad delusion that everyone else is equally interested, or should be, and he succeeds only in being devastatingly boring and infuriating. He is usually magnificently unloved. Even his best friends won't tell him. And among this population of over-zealous enthusiasts there must bc, if only on the law of averages, one or two radio bores!

Many hobbies, and ours is no exception, present limitless opportunities for exploration and exploitation. There are so many basic activities, so many possible diversions, so much to do in so short a-time, that the really keen enthusiast can easily find himself so inextricably involved that the hobby becomes the master. The dividing line between a Fan and a Fanatic may be extremely thin!

Most of us, of course, keep a reasonable sense of proportion but the line of thought being pursued does suggest some selfinterrogation that might be applied at times.

Unless one is engaged professionally, it is probably better not to become too highly specialised-or too narrow minded. Don't get into a rut by building only valve or only transistor equipment, or only receivers, or only amplifiers. Try something different, even if only occasionally.
"Jack of all trades, master of none" may be a justifiable slur in industry, but surely not in amateur radio, where a diversity of interests is the best way to get the most from the hobby and to avoid becoming a radio bore even to other radio enthusiasts!

A sense of proportion is also advisable in our general approach. Since the hobby is a technical one, it is inevitable (and desirable) that equipment is appraised in a technical manner. But the time to take stock is when you listen to recordings and hear not music but only frequency response, harmonic distortion, wow and flutter percentages. Or when you watch a TV programme in misery because the raster is slightly non-linear or there is a fraction too much overshoot. Or when you are impelled to switch off a radio in the middle of a programme to change a coupling capacitor. Or when you mentally read advertisement posters in morse code!

The search for improvement, if not perfection, is highly commendable, but the place to do this is on the work bench when the equipment is being designed, constructed, aligned or serviced.

It should always be remembered that equipment is built to be used and to be enjoyed. And if it is in the living room, no doubt other members of the family will be only too pleased to point this out!


## NEWS AT HOME AND ABROAD

## RADIO MASTS FOR ATLANTIC ISLAND

BBRITAIN'S Ascension Island in the South Atlantic Ocean is shortly to have nine radio masts erected on it. An order valued at over $£ 90.000$ for the masts from the Marconi Company Limited has been received by British Insulated Callender's Construction Company Limited.

Under the contract BICC will supply one 250 ft . and eight 325 ft . radio masts for use on the island.

## Miniature Resistors Protect Motors

NEW protection devices for electric motors recently introduced by Mullard are designed to be incorporated directly in the windings of the motor. The new devices-positive temperature coefficient resistors-will provide cheaper and more effective protection of electric motors than conventional methods.

The miniature resistors (see illustration) are made from doped barim titanate ceramics. In operation they exhibit a high positive temparture coefficient which causes a large and rapid increase in value when an excessive increase in the temperature of the motor windings (above about $110^{\circ} \mathrm{C}$ ) occurs, and this will cut-off the power supply.

A number of special advantages are presented by the introduction of these resistors and applications in transistor circuits are foreseen.


## AIRCRAFT NAVIGATION BEACONS FOR U.S.S.R.

RADIO navigation beacons for aircraft, of the type now covering the Western European air lanes, will shortly be installed in the U.S.S.R. under a contract signed recently in London.

The contract. which is for two high-power long-range VOR beacons (one is shown on the right), is the first ever Soviet order for this type of equipment. Standard Telephone and Cables Limited are to supply the beacons which will be installed on the airway between Moscow and the Baltic coast.

During the negotiations for the contract, which also includes STC airborne equipment, Soviet representatives witnessed the operational procedures of the VOR receiver equipment during a demonstration flight in the Company's aircraft


## RADAR REFLECTORS FOR HIGH-FLYING GLIDERS

A
T Ipswich airport, home of the London Gliding Club, the Marconi Company, on behalf of the Ministry of Aviation, are currently carrying out a series of experiments aimed at reducing the danger of collision between gliders and high-speed aircraft.

Because of their very light construction, gliders do not register on the radar screens of air-traffic control centres and as the modern high-performance glider can easily reach the airways of civil and military aircraft, this danger of collision is increasing.

The experiments carried out by the Marconi Company will investigate possible methods of improving the radar reflective properties of gliders by such means as cheap, light-weight radar reflectors that could be easily fitted in a glider to make it visible to radar. without being in any way detrimental to the performance of the glider.

After a series of experiments using scale models at the Marconi Research Laboratories. Great Baddow, a number of radar reflectors have been designed and tested in flight. For these trials a glider with a tug aircraft has been operated by members of the London Gliding Club.

At the Marconi Rivenhal! Establishment in Essex, Marconi research engineers have observed these flights and recorded the strength of the reflected radar signals received by three separate radar systems.


Marconi engineers recording the radar signals received from a glider fitted with experimental reflectors.

## Ionosphere Sounders for U.S. Navy

EQUUIPMENT which will be used by the United States Navy to ascertain the best operational frequency for long range h.f. radio communications, is to be developed under a contract awarded to EMI-Cossor Electronics Lid. of Canada, subsidiary of EMI.
The equipment-an ionospheric oblique sounder-will be a sophisticated version of the company's Ionosonde 8000, which is currently being evaluated by several NATO nations.
Due to the physical structure of the ionosphere, quality of reception of short wave radio transmissions varies considerably between one frequency and another. The new sounder will enable the U.S. Navy to detect the best possible wavelength for communications without relying on possibly incorrect forecasts or lengthy trial and error methods.

## Telegraph System in North Sea

DNING the intensive search for oil and natural gas under the North Sea, a G.P.O. radio telegraph system will be used to provide communications between the many mobile drilling rigs and one of two shore stations at Humber, on the Lincolnshire coast, and Stonehaven, near Aberdeen.

Both shore stations will be fitted entirely with Marconi multichannel telegraph transmitting and receiving systems and will provide up to 30 individual communication channels.
This order was placed by the General Post Office. An accompanying order from the Marconi International Marine Company will provide radio equipment on one of the drilling rigs.

## NEW AERIALS FOR RADIO ASTRONOMY


'1'HE contribution of the
Commonwealth to the study of radio sources throughout the universe, has advanced on two accounts recently by the installation of a new 15 ft . radio telescope at Coxtie Green, near Brentwood. Essex, and the erection at Parkes, New South Wales, Australia of a 60 ft . inferometer.

The Coxtie Green telescope (above) has been produced by the Marconi Company Limited for research scientists from Queen Mary College, London University, to examine the brighter planets and radio scources in tho sky. The telescope, which operates at wavelengths in the region of one millimetre, has the unusual feature of being monlded in glass fibre reinforced plastic.

The New South Wales inferometer (below) joins a 210 ft . radio telescope on the same site. On occasions these two instruments will be used in conjunction for the accurate position fixing of radio sources.



MODER $N$ electronics practice makes increasing use of small circuit bricks comprising circuitry which can be used in virtually the came form for the most diverse applications. Such arrangements are all the more valuable on account of the tendency to miniaturisation on small circuit boards, using transistorised circuitry. The particu*ar "brick" which is the subject of this article oomprises a versatile keyed audio oscillator which bas been devised and thoroughly tested by the tuthor. It is built-up on a 4 in . $\times 2.5 \mathrm{in}$. Veroboard
(small paxolin sheet with regular rows of holes for affixing components, as described in Practical Wireless. May 1964) and has seven terminals for external connections (Fig. 1).

The basic function of this circuit is to provide an audio output signal, of almost pure sine-waveform, whenever and only as long as the d.c. current or voltage injected at P1 exceeds a certain threshold limit which can be set over a wide range in each case with the help of the sensitivity control VR1 (or VR1ia). The three n.p.n. silicon epitaxial


Fig. 1: The oseillator circuit. The output frequency is determined by the capacity of the four (equal) capacitors Cl-C4. (4) 100 pF , the frequency is about $5 \mathrm{kc} / \mathrm{s}$, ot $250 \mathrm{pF} 2 \mathrm{kc} / \mathrm{s}$, at $500 \mathrm{pF} / \mathrm{kc} / \mathrm{s}$, ot $1000 \mathrm{pF} 500 \mathrm{c} / \mathrm{s}$, ot $0.01 \mu \mathrm{~F} 50 \mathrm{c} / \mathrm{s}$, ot $0.1 \mu \mathrm{~F}$ $5 \mathrm{c} / \mathrm{s}$ and at $0.5 \mu \mathrm{~F} / \mathrm{c} / \mathrm{s}$. The relationship is thus strictly linear.

Input circuit for voltage keying (see text)

transistors are basically in a threestage emilter follower cascade arrangement and are normally cut-off because the bias appled to the base of Trl is just less than the threshold voltage of such an arrangement. A very emall current injected va Pl ta fraction of a microamp in the most sensitive setting of VR1) cuts the cascade of thre transistors on. whereupon the latt two. Tris and Trs. immediately commence to oscillate as a phase-shoft oscillator through the feedback networh (1-C+1 R15-RI7.

Fig. 2: The PI input of the circuit of Fig. I modifed for voltage keying.

## Uses

This circuit can be used for any purpose requiring thes function. The input circuit at PI is, for example, more than adequately sensilive to operate directly from a vacumm photocell of the 90AV type, whose cathode is then connected directly to P1 and anode to the appropriate positive voltage needed to operate the photocell (in fact. the same +40 V line as needed to uperate the Veroboard elreuit will generally dol. Whenever the photocell is illuminated. it draks a tiny current in mroportion io the intensity of the illumination. With the sensitivity control VRI. the current at which the transstors "switch on" and the audio oscillation thereupon appears at the output socket. can be adiusted between about 0.5 and $12 \mu \mathrm{~A}$. this being the normal current operating range for most photocells. The sonsitivity control VR1 will. in such applications, normally be set so that the photocell current dae to the ambent illumination just does not "swith" the oscillator on, response then being obtained only to any "wanted" additional light signal.

Regarding the output circuit. this may be connected via a simple bloching capacitor and volume control (Fig. 3) hetween terminak 6 and 7 to the input of any audio amplifier. transmitter modulator amplifier of to the record-player input sockets on the recording amplifier of any conventional domestic tape recorder. However, if you wish to record the bursts of atodio oscellation (in response to the d.c. voltage or current pulses applied at the input) on tape, an additional recording amplifier is
not absolutely essential. Fig. 4 shows how a normal type of recording head can be fed directly from the output terminals 5, 6 and 7. R23 here gives d.c. bias for the head in place of the otherwise (for musical recordings) more usual r.f. bias. This is quite satisfactory here, particularly if erase is performed with a powerful permanent magnet over the pole of which the tape passes. which also has the advantage of completely avoiding the need for any form of electronic bias and erase oscillator for such a technical pulse-recording tapedeck, therewith greatly simplifying circuitry. The erase magne will saturate the tape: the d.c. bias passed into the recording head via R 23 must be of opposite polarity, i.e. such as to move the magnetisation of the tape away from saturation again, to the recording operating point on the hysteresis curve. The playback head will function normally, using a normal playback amplifier.

When deciding to build a special tapedeck from scratch the characteristics of the recording head KHI chasen should be obtained from the makers. These will normally state an (r.m.s.) r.f. bias colrent and a signal current required for correct operation. Satisfactory performance is obtained, in most cases, with the value of R 23 chosen such that the d.ce current obtained as bias is some two-


Fig. 3: Input and output connections for m.c.w. telegraphy and model control transmitters, as well as for electronic organs and tremolo insertion on guitar amplifiers.


Fig. 4: Output connections for direct tape-recording, without an additional recording amplifier being required
thirds of the specified r.m.s. value for r.f. bias. The transformer L2 must have a step-down ratio approximately equal to the number of mA signal current specified for the particular recording head. The sub-miniature types sold for interstage coupling in transistorised audio amplifiers will in most cases be found satisfactory; conditions are not very critical.

## Practical Uses Requiring Tape Recording of the Output

Apart from numerous applications in the control of industrial machinery which are beyond the scope of this article there are several interesting amateur applications, particularly in the field of remote control of model ships and aircraft. These involve the prerecording of a sequence of pulses tapped in with a Morse key at the input so that, on playback of the tape into the modulator of the model control transmitter, the model can be made to respond to the particular sequence of commands automatically without further manual attention. If a closed loop of tape is used the sequence of commands can be repeated indefinitely as the tape goes round and round until stopped. There is a wide field here for model control experimenters.

A transmitted signal using modulation of the carrier with various audio frequencies is best used here, the receiver on the model employing audio tuned circuits of resonant reed relays to select the individual frequencies and thereupon cause the appropriate responses in the correct control circuits of the model. All necessary components for building such model control receivers, together with profuse technical information, are stocked by good modelmakers' shops and are made by such firms of world repute as, for example, Messrs. Grundig.

The advantage of this method of model control is that as many different commands can be sent simultaneously as different audio frequency "channels" are available. Several of the Veroboard circuits described in this article (Fig. 1) can be made, differing solely in the value chosen for the four capacitors (all must be equal) C1 to C4, which determines the frequency of oscillation. Alternatively a two-pole, multi-way wafer switch -or a set of push-buttons-may be used to select various similar networks with different $C$ values between the collector of $\operatorname{Tr} 3$ and the base of $\operatorname{Tr} 2$ on a single circuit. The different "channels" are then merely no longer available simultaneously but only suçcessively in any order.
lt is in fact possible to use this Veroboard circuit as a virtually complete multi-channel modelcontrol transmitter, the output signal at terminal 6 generally being of ample power to grid-modulate a conventional transistorised p.a. stage, which is all that will be required in addition on the r.f. side, no additional modulation amplifier being necessary. If a row of suitable press-buttons are used, each having two contacts selecting and connecting different networks between the collector and base of $\operatorname{Tr} 3$ and $\operatorname{Tr} 2$ respectively, and a third contact in the function of Morse tapper (Fig. 3), then by pressing the appropriate button it will cause the transmitter to send out the associated selective command in each case.

With a tapedeck connected to the output, as shown in Fig. 4, the programme of commands "tapped in" with the buttons can be recorded for suesequent automatic operation of the model according to the predetermined programme on playback into the transmitter modulation input. The great advantage of the d.c. bias shown in Fig. 4 for the recording head and of being able to dispense entirely with an erase oscillator, using a permanent magnet, lies in the extraordinary simplicity of the tapedeck thereby rendered possible. The playback amplifier need only be a perfectly straightforward audio amplifier with an input sensitivity in the region of 1 mV , almost any microphone amplifier advertised ready built or as a kit in these pages (e.g. baby alarms) being satisfactory. It is consequently possible to accommodate the sub-miniature tapedeck into the model-control transmitter casing (hand-carried

## COMPONENTS LIST

Resistors:

| Resistors: |  |  |  |
| :---: | :---: | :---: | :---: |
| RI | 180kS | R13 | 22k! |
| R2 | IMS | R14 | 2703, |
| R3 | IMS2 | R15 | 220k! |
| R4 | 100kS | R16 | 220k! |
| R5 | 5.6 k g | R17 | 220ks |
| R6 | 220 k , | R18 | 100 k g |
| R7 | 1 MS | R19 | 47 k S |
| R8 | J0MS | R20 | 1MS2 |
| R9 | 470 k S | R21 | 1MS2 |
| R10 | 4.7 k @ | R22 | $3 \cdot 3 \mathrm{k} \Omega 2 \mathrm{~W}$ |
| RII | 4.7 k S 2 | R23 | $6.8 \mathrm{k} \Omega$ |
| R12 | 10kS |  |  |

All $10 \% \frac{1}{2} \mathrm{~W}$ carbon, unless otherwise stated
Capacitors:

| Cl | $100 \mathrm{pF}-0.5 \mu \mathrm{~F}$ |  |
| :---: | :---: | :---: |
| C2 | $100 \mathrm{pF}-0.5 \mu \mathrm{~F}$ | To suit desired frequency |
| C3 | $100 \mathrm{pF}-0.5 \mu \mathrm{~F}$ | See caption Fig. 1 |
| C4 | $100 \mathrm{pF}-0.5 \mu \mathrm{~F}$ |  |
| C5 | 10 times $\mathrm{Cl} /$ | value |
| C6 | $0.1 \mu \mathrm{~F}$ paper |  |
| C7 | $100 \mu \mathrm{~F}$ electroly | c 125 V |
| C8 | $100 \mu \mathrm{~F}$ electro | c 125V |
| C9 | $250 \mu \mathrm{~F}$ electrol | c 9 V |

Semiconductors:
DI S36 diode Brush Crystal Co.,
$\left.\begin{array}{ll}\text { D2 S36 diode } \\ \text { D3 ZL39 zener diode }\end{array}\right\}$ Hythe, Southampton
D4 $200 / 250 \mathrm{~V}$ silicon h.t. rectifier
D5 $200 / 250 \mathrm{~V}$ silicon h.t. rectifier
D6 $200 / 250 \mathrm{~V}$ silicon h.t. rectifier
Trl 2 N 1613 transistor?
Tr2 2N1613 transistor $\}$ Brush Crystal Co. Tr3 2Ni613 transistor)
Potentiometers:
VR1 5 MS log. VRIa $250 \mathrm{k} \Omega$ log.
VR2 $100 \mathrm{k} \Omega$ lin. preset sub-miniature
VR3 $500 \mathrm{k} \Omega$ log.
Miscellaneous:
TI Mains transformer. Secondaries: 50 V 30 mA (heater transformer with rewound secondary)
T2 Transistor interstage transformer with 5:1 ratio, or to suit recording head (see text)
SI Mains toggle on/off switch
FI $\quad 250 \mathrm{~mA}$ mains fuse
Plugs, sockets, wire, piece of Veroboard 4 in . $\times 2 \frac{1}{2} \mathrm{in} .$,
etc.
portable) with a switch on the panel "auto/direct" being included. In the auto setting the transmitter is modulated with a prerecorded sequence of commands from the tape; in the direct setting the transmitter is modulated directly by the commands. Various combinations are possible, e.g. commands can be recorded simultaneously to direct transmission so that if some hand-controlled acrobatic antic of the model proved particularly pleasing it can immediately or at any later time be repeated by playing back the tape.
lt is, of course, immaterial whether several Veroboard circuits are used so that commands such as throttle and rudder control can be given simultaneously or whether only one switchedfrequency circuit is used for successive commands as far as the tapedeck and receiver function is concerned. The tape can record all frequencies simultaneously if necessary and the receiver audio tuned circuits will sort them out. There is only one important practical condition, namely that the various audio frequencies associated with the different channels should bear no harmonic relationships, i.e. they should not be simple multiples or other simple ratios of each other but rather as "odd" as possible. This is to avoid the harmonics $g$.nerated upon distortion of the waveform in any one channel causing spurious responses in one or more other channels. The receiver audio tuned circuits will already be staggered appropriately and it is then merely necessary to trim the Veroboard circuit networks to proper resonance (if necessary wire small trimmers in parallel with C 1 to C 4 ).

## Geiger Counters

A somewhat more specialised but nevertheless interesting and practical use of the circuit concerns Geiger counters, this also requiring tape recording of the output pulses. In Practical Wireless, December, 1962/January, 1963, an article was published on an advanced Geiger head, followed by a digital register in the April to June, 1963, issues. Finally in the December, 1963, issue, a description was given of the many experiments possible with this equipment which. as readers will remember. involved among other things a study of the natural radium-product activity in rain or snow. This can reach enormous intensities and decay within some three to five hours. The study of these activities in relation to season, location and weather patterns, as explained in the lastnamed article, can be a most instructive line of experiment for schools and clubs but it is often rather time consuming since the counter must be read off every few minutes after as many rains as possible. More troublesome still is the fact that many of the most interesting rains and thunderstorms occur deep in the night and it is bad enough having to get up and switch the apparatus on then -but having to sit by it for the rest of the night reading off the counter every few minutes is the last straw! A second almost insurmountable problem is involved with the fact that many of the most interesting studies concern quick successions of many showers in a row. A study of the changes of radioactivity with the progress of such weather patterns is particularly interesting but quite
impossible with the design already published unless one duplicates the whole set-up as many times as the number of showers in a row to be studied. However, the problem here is that whilst one shower is still being studied to follow the decay of its activity over three to five hours, the next will maybe many more will arrive and the counter will be "engaged". Having come up against this problem the author hit upon the idea of tape recording the signals from the successive showers so that these can be counted out at any later time by replaying the tape through a suitable circuit into the digital register. The circuit described in this article was first designed for this particular application, it is only necessary to duplicate the Geiger head the necessary number of times and associate each head with a Veroboard circuit giving output pulses of a particular (in each case different) audio frequency. All signals can be fed on to one single continuously running tape track, using a perfectly ordinary domestic tape recorder. The Geiger counters will be "started up" one after the other as the successive showers occur and their samples are ready. It is not absolutely necessary even to keep checks of the clock because the relative timing will automatically be indicated later on the tape counter of the recorder! Upon subsequent playback at any later time a tunable audio resonant circuit (choke-coil and switched parallel capacitors to bring it to resonance at the various channel frequencies) is fed from the extension speaker terminals of the tape recorder and in turn feeds a simple rectifier circuit, much the same as an ordinary diode detector arrangement, for reconstituting the original Geiger counter pulses. Each channel, i.e. each shower, can then be played back and registered in detail in the digital register by tuning to each channel frequency on successive runs. Only a single digital register unit, running correspondingly longer, is thereby required. Furthermore, rains and snows occurring at night, even if only single, can be recorded and analysed on the digital register the next day. It is only necessary to get up in the middle of the night to switch the Geiger counter and the tape recorder on!

A different solution would be to use a digital register with facilities for printing out the count at predetermined regular intervals on an automatic basis. This will solve problems of work at night but still not help in the matter of recording many showers whose radioactive overlap in time. Short of duplicating the whole equipment several times there is no other sensible solution apart from the use of the Veroboard circuits described in this article in conjunction with an ordinary domestic tape recorder.

## Modulated Continuous Wave (MCW) Telegraphy for "Ham" Transmitters

A useful incorporation for the Veroboard circuit is shown in Fig. 3 which itself again has a variety of specific uses. Bursts of the characteristic audio frequency are obtained at an amplitude which is adjustable with VR3 (as volume control) in rhythm with the tapping of the Morse key. R20, C5 and R21 serve as key-click filter in this

#  <br> How to Align a Receiver Without Test Equipment <br> BY GORDON J. KING 

II often happens that the enthusast linds himself in a spot when it comes to the alignment or realignment of home constructed receivers and receivers in for repair. This ss because the service sheet or building instructions stipulate the use of a signal generator for this exercise, such an instrument not always being in the possesston of the enthusiast. Indeed, the radio beginner may yet have been able to acquire only the essential mulurange test meter.

Nevertheless. it is possible successfully to align and realign radios, including a.m. and f.m. sets and transistor portables, without an! instruments at all, and this article tells how it is done.

## Misalignment Symptoms

The term alignment implies the trimming and tuning of the various radio-frequency (r.f.),


Fig. 1: Block diagram of tuned radio-frequency receiver.
oscillator and intermediate-frequency (i.f.) circuits for optimum tracking, sensitivity and response. A set which is completely out of alignment will not usually function at all, while a set whose alignment is not right will exhibit various symptons.

One is an inaccuracy of scalc calibration. That is, for example the Light Programme may tune on Radio Luxembourg instead of the correct 1,500 metres. Moreover, the "tracking " may be wrong, giving the correct calibration on stations, say. at the high frequency end of the medium wave band and incorrect calibration on stations at the other end of the band.

Another misalignment symptom is poor sensitivity, the set working only on powerful local
stations and being dead to more distant stations and weak signals. Misal.gnment can also callse poor reproduction owing to a restricted or distorted response. while the breakthrough of adjacent stations can prove troublesome of the response of the luned circuits is too wide.

## Trimming

Let us look first at the tuned radio-frequency (t.r.f.) receiver. which is the simplest of all types so far as alignment is concerned. Such a receiver is shown in the form of a block diagram in Fig. 1. From the tuning aspect we have two stages. the tuned r.f. amplifier and the detector. The detector produces the atalio signals which are amplified and applied to the loudspeaker.
it is the purpos? of the r.f. amplifier to receive the very weak aerial signals, to amplify these and then pass them on to the detector. The aerial is supplying the r.f. stage with hundreds of signals. so it is essential for that stage to select or tune the required signal. Likewise the detector stage must tune to the required signal. Thus. buth the r.f. amplifier and the detector must tune to the same frequency simalianeously.

Tuning in most cases is accomplished by tuning capacitors. In the early days of radio separate luning capacitors were used for the r.f. amplifier and detector, the exercise being first to tune the detector to pick up the signal and then tune the r.f. amplifier for maximum sensitivity (to get the signal as loud as possible).

Modern receivers, of course, feature ganged tun.ng capacitors, as Fig. 1 shows, and it is important that each section of the gang funes to exactly the same frequency over the whole tuning range.

The design of the ganged capacitor and associated tuning coils ensures that this happens reasonably well but final trimming is necessary for correct dial calibration and optimum sensitivity over the bands. It should be noted that with tr.f. sets the dia: calibration is established by the detector tuning and the sensitivity by the r.f. amplitier tuning.


Fig. 2: At (a) trimming is effected by a preset capacitor across the tuning gang and padding by on adjustable dust-Iron core in the tuning coil, while at (b) a preset capacitor across the coil serves for trimming and a similar type of capacitor, though larger value, in series with the tuning coil for padding.

## Padding

While it is relatively easy to arrange for the two circuits to tune to the same frequency (or wavelength) at one point on the dial it is not quite so easy to arrange for the tuning to be accurately maintained over the whole of the dial. The simaltaneous and accurate tuning of more than one tuned circuit is called " tracking ".

To secure good tracking most t.r.f. sets fand all sunerhet sets) embody what is called a "padding adiustment". This consists either of a smatl trimmertype capacitor or an adjustable dust-iron core in the tuning coil.

In addition there are " trimming capacione" on each circuit. In mexpensive t.r.f. sets the trimmers consist simply of compression type prese capacitors on cach section of the tuning gang, while more expensive versions have separate trimmers (and padders) for each band.

The important points to remember are that the trimmers have the greatest effect on the tuned freouency at the high frequency (low wavelength) end of the hand. while the padders have the greatcst influence at the low frequency (high waveleneth) end of the band. Fxamnles of padders and trimmers are shown a! (a) and (b) in Fig. 2.
The idea of trimming and naddine then is to adiust the trimmers for correct calibration and ontimum sensitivity at a frequency at the high frequency end of the tuning and the padders for like conditions at the low frequency end of the tuning.

## T.R.F. Examble

Now let us suppose that we have a t.r.f. set that is in need of trimming and no instruments at all. The set should be switched on and allowed thoroughly to warm up. A good aerial should be connected and the volume control turned to maximum. The first thing to do is to get the circuits into anproximate alignment. This can be done by carefully listening at the speaker while tuning the set over the band. When the local station is heard the r.f. trimmer should be adjusted for maximum output.

Next the calibration should be attended to. Say the local station is the long wave Light Programme and that this is coming in at 1.600 m instead of the correct 1.500 m . It his means that more capacitance is requited on the detector trimmer. A compression type should be screwed in and the station followed by tuning the set as the trimmer is adjusted until the correct calibration is established. The r.f. trimmer should then be readjusted for maximum output at the correct tuning point on the dial

For final adjustment the set should be tuned to a station (say Radio Luxembourg) at the top end of the medium wave band, trmmed first detector and then r.f. wise and then tuned to a station at the bottom end of the band and then padded detector and r.f. wise.

It is generally necessary to repeat these adjustments until no further improvement can be obtained at both ends of the band-both for calibration and sensitivity. It will then be found that stations between the two alignment points will tune correctly on the dial and that the sensitivity is maintained over the band.

If the station is tuning too low on the dial, say 1.400 m for the Light Programme instead of 1.500 m , the detector trimmer should be screwed out. In some cascs the trimmer on a completely misaligned set may not give the correct calibration over its range. In that case the trimmer should be set to its approximate mid-setting and the padder adjusted to give the correct tuning point. After this, of course, the process as detanled above should be carried out.

For a delicate setting of sensitivity, when the r.f. adjustments are being made, the aerial should be very loosely coupled to the set by winding a few turns of the aerial wire round the aerial socket or lead of the set. This will ensure that the r.f. circuits are not swamped by aerial capacitance.

It is generally best first to align the medium wave band, followed by the long wave band and then the short wave band if fitted.

## Superhet Principle

A sunerhet type recciver is a little more difficult to handle but. once the basic princinle is understood, there should be no undue problem. Fig. 3 shows the block diagram of this type of set. Here the signals in the aerial are apolied to the mixer alneg with a signal from the local oscillator. The aerial and oscillator signals are effectively "mixed" in the mixer and the output is either the sum or the difference in terms of frequency of the two signals.

As an examole, sunnose that the incoming signal is at a frequency of $150 \mathrm{kc} / \mathrm{s}$ (that is 1.500 m -the wavelength of the light Programme) and the oscillator is producing a signal at $320 \mathrm{kc} / \mathrm{s}$. In the mixer these two signals bsat together and their sum gives a fremiency of $470 \mathrm{kc} / \mathrm{s}$. while their difference gives a freouency of $170 \mathrm{kc} / \mathrm{s}$.

In practice either the sum or the difference frequency is selected and tuned by the intermediate frequency (i.f.) tuned circuits. The standard a.m. i.f. these days is $470 \mathrm{kc} / \mathrm{s}$, so the sum frequency of the example given above would be selected.

If the difference frequency is selected as the i.t. then the oscillator would produce a signal of $620 \mathrm{ke} / \mathrm{s}$ to beat with the $150 \mathrm{ke} / \mathrm{s}$ of the Light Programme (1.e. 620 minus 150 equals 470).

Clearly then the muxer and oscillator tuning must always be out of step with each other over the whole tuning range by an amount equal to the i.f. This is one thing that the alignment process has to ensure. It also has to ensure that the i.f. tuning is correct and that each i.f. transformer winding is tuned to the same frequency.

Let us assume that we have a completely misaligned set to deal with. What we want is breakthrough of some sort of signal just to get a start on tuning the i.f.s. for as these come into tune so the sensitivity of the whole set rises and the remaining alignment becomes possible using off-air signals.

## Peaking the I.F.s

One way found by the author that can be adopted to peak the i.f.s somewhere within their tuning range is to connect the screen of the television aerial's downlead, via a 100 pF capacitor. to the signal grid of the mixer section of the frequency changer valve (note that the frequency changer is the valve that performs both functions of mixing and producing a local oscillator signal. Communications type sets and certain domestic models employ separate valves for mixer and oscillator).

When this connection is made and the ser's volume control turned fully up, slight clicks and a hiss can be heard in the speaker. If the i.f.s are miles off tune the noise output will be very weak. but as the transformers are brought into tune so the output will increase and a Continental station may be heard in the background.

The idea then is carefully to adjust the i.f. cores in turn, starting from that nearest to the detector (see Fig. 3) and working back towards the mixer (frequency changer) until the background disturbances are at their loudest. When this has been achieved one can rest assured that the i.f. windings are all tuned to the same frequency.
This may not be the exact i.f. frequency but it will not be a long way out if the noise peak is arranged to occur when the trimmers are approximately halfway within their range of adjustment.


An adjustment of greater accuracy can be made later of necessary.

Having estabished a setting for the i.f. tuning the next step ts to adjust the local oscillator and mixer tuning on a local station. This time the long wave should be adjusted first and, since the Lignt Programme puts a strong signal into most areas, this is a good station to work with.

With the television downlead connected still to the mixer signal grid the set should be switched to long wave and the tuning carefully adjusted until the Light Programme is heard. It may be very weak and well off calibration, but if the set is without fault, apart from being misaligned, then it will be found somewhere on the dial.

When it is found the long wave local oscillator trimmer should be adjusted step by step to put the light Programme nearer and nearer the correct point on the tuning dal until eventually the correct tuning foint is established. Tests will have to be made to see which way the oscillator trimmer needs to be turncd to move the station tuning in the required direction.

The programme should now be coming in very loud, though interference and whistles may be troublesome. At this stage the television downlead should be disconnected and the correct aerial plugged into the proper aerial socket (if fitted). The signal will now be weakened again but it will soon be brought back to its correct volume by adjusting the mixer trimmer. The interference and whistle should then disappear.

## Snags

The set is now in approximate alignment on the long wave band but to arrive at that condition several snags may be encountered. It may be found. for instance, that the Light Programme cannot be tuned at the correct position on the dial at any setting of the oscillator trimmer. In that event a check should be made to ensure that the dial drive is working properly and that the cursor (or diall corresponds to the high frequency llow wavelength) end of the scale when the gang is fully open and to the low frequency (high wavelength) end when fully closed. A check should also be made to ensure that the gang spindle or dial drive is tightly secured and not slipping in any way.

If all is well here a badly misadjusted long wave padder may be responsible. Initially this should be set to the centre of its adjustment. If this is correct then the i.f. is too far away from its correct frequency.

To correct for this the long wave oscillator trimmer should be adjusted as far as possible to bring the tuning as close as possible to the Light Programme $(1,500 \mathrm{~m})$ on the dial. It will either be wide open or very tightly compressed. If wide open it should be closed up several turns or if tightly compressed it should be opened a little to give scope for eventual further adjustment. The Light Programme should then be retuned on the dial, the tuning error being a little greater than previously of course.

The idea now is to adjust the i.f. tuning to correct the tuning error. This is not difficult. The core of the winding connected to the detector
locate the adjustments for specific bands.
The oscillator trimmers and padders, however, can be discovered by touching the " live " side of the component with the blade of a screwdriver while a finger is resting on the blade (keep the other hand clear of the chassis to avoid shock). If, for instance, the set is receiving a medium wave signal, contacting the medium wave oscillator component in the manner described will detune the signal.

The adjusting components for the mixer or r.f. stage (note that some superhets also feature an r.f. stage with a three-gang tuning capacitor) when contacted in a like manner will give rise to loud clicks from the speaker. The trimmer or padder which is not in circuit at the time will result in zero response.

Sets using ferrite rod aerials need no special attention and the instrument-less alignment procedures outlined in the foregoing can be adopted with them also.

## F.M. Sets

F.M. sets utilise the superhet principle and basically the alignment information already given applies also to this type of set. There are now plenty of f.m. stations on the air and very strong sugnals are delivered by local stations via correctly cut f.n. (Band II) aerials.

Frequencies of local stations are given in the Radio Times. The Light Programme has the lowest frequency and the Home Service the highest frequency. This is easy to remember taking the L of Light for low and the H of Home for high. The Third Programme has a frequency between the Light and Home.

The ratio detector or discriminator may need special attention after the basic alignment process. This should be adjusted for the best quality reception. ensuring that each tuning point has only a single major peak. Two or three peak tuning means that the i.f. response is faulty.

Magic eye tuning indicators can be of considerable assistance for instrument-less alignment. Such indicators increase in deflection for increase in signal strength. Thus they can be used as an output indicator to reveal when, say, the i.f. transformers are tuned to optimum frequency or when the tuned circuits are peaked.
I.F. transformers peaking in f.m. sets may not be desirable, for a sharp response (Fig. 4a) can suppress the higher order sidebands and impair the treble response. After peaking as a preliminary adjustment. slight detuning may be warranted to give a flatter top to the response as shown at Fig. 4b. Insufficient bandwidth can also aggravate oscillator or tuning drift effects on f.m. sets.


BY F. L. THURSTON

CABINETS for radio or test gear can be made from a number of different materials and in a range of styles. The principal materials for amateur use are aluminium, wood, and synthetics.

## Aluminium Cabinets

The general hints given in Part 1 for making aluminium chassis also apply when making aluminium cabinets, i.e. drilling methods.

Sheet aluminium is best cut with the aid of a hacksaw, large holes with a fret saw using metal cutting blades. When marking out prior to bending, if the drawing shows external dimensions of chassis of cabinet, the score lines along which the bends are to be made must be marked short of the overall dimensions by the thickness of the metal for each bend.

When bending the metal, if a special bending machine is not available, a normal vice can be used. But if a depth of bend greater than about 3 in . is required, as it will be for most cabinet making jobs, a carpenter's vice may be used, using a bending technique similar to that already outlined.

If no carpenter's vice is available, use pieces of wood, of suitable size, clamped to the metal with a pair of carpenter's clamps, the wooden blocks
being used in a similar fashion to the jaws of the carpenter's vice. The wood used should be of a fairly hard type if a good sharp bend is to be obtained.

Failing all of these alternatives, the bending operation can be performed at reasonable cost by one of the many firms that specialise in this kind of work, some of whom advertise in this magazine.

Several basic cabinet styles are available, and Fig. 7 shows a type made from a single sheet of metal forming an open-ended box into which a complete chassis and front panel assembly may be fitted. The front panel is bolted to the cabinet by means of "clinch" nuts secured into flanges at the front of the cabinet.

Clinch nuts are similar to normal nuts but have a tubular extension on one side which is drilled out to give clearance of the bolt. When the clinch nut is bolted to a piece of metal a hole is drilled of such a size as to just give clearance to the outside diameter of the tube and the hole is then countersunk. ${ }^{\text {. }}$

The nut is then pushed into the hole from the blank side of the metal and the fube is peened over into the countersink, securing the nut to the metal panel: 'The' inset of Fig. 7 shows the principle involved. If a suitable peening punch is not available a ball bearing can be used as a substitute.


Fig. 7: An open-ended aluminium cobinet, made from a single sheet of metal.

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Fig. 8 (above): Another method of constructing a cabinet on the lines of that of Fig. 7, and Fig. 9 (below): an easier method of achieving the same result.


A method of construction which involves no bending of sheet metal at all is shown in Fig. 11. A skeleton frame, made from steel or aluminium angle, is assembled and individual top, bottom, front, rear and side panels bolted to it, using clinch nuts secured to the trame.

An advantage of this method, which is widely used for large commercial equipment, is that the frame can be used as a basic part of the chassis assembly, separate sub-units being bolted to it. Strengthening struts are added where required. When cutting the panels care should be taken to ensure that a good final fit is obtained. i.e., some panels may have to be made larger than the basic frame if unsightly cracks in the finished cabinet are to be avoided.

A variation on this theme is shown in Fig. 12, which shows a close up detail of a frame unit made from a composite assembly of $\frac{1}{2} \mathrm{in}$. and 1 in . angle. The complete frame assembled in the same way as that of Fig. 11, but

The cabiner of Fig. 7 is very robust but difficult to bend. The same final shape can be obtained by using a number of different methods of construction, as shown in Figs. 8 and 9.

A different style of construction is shown in Fig. 10. The front and rear panels are bolted directly to the chassis and a separate bottom plate and cover unit are used. A pair of clinch nuts are bolted to each side of the chassis and holes drilled in the side of the top cover to line up with them.

Four clamp plates, drilled out and tapped, are secured to the top cover with countersunk screws and line-up holes drilled in the front panel, enabling the whole assembly to be fitted together. the finished article now gives a number of recess areas, available between the $\frac{1}{2}$ in. angle, to take each of the main panels, which may be bolted to the lin. frame.

The advantage of this system is that the panels can be cut to the dimensions of the recesses, without the danger of making expensive mis-calculations when allowing for overlap. Any slight errors will be masked by the recesses, and the complete assembly, when painted, has an attractive appearance, the $\frac{1}{2}$ in. framework standing proud of the panels.

If ventilation holes are to be provided in the cabinet, the easiest method is to provide a cut out and bolt one of the commercially available grilles over it. Alterna-


Fig. 10: Another approach to the problem of cabinet construction. tively, a large number of drill holes can be provided as long as great care is taken in positioning them.

Ventilation louvres can be made by two methods. Fig. 13a shows a "handle" type and the " mould" required for making them. To make the mould, cut out a piece of steel plate, the same thickness as the depth of the louvres, the cut-out being " negative ", and, after case hardening, bolt down to a hardwood base. Cut a slot in the panel to be formed, and press the metal slightly outward under finger pressure, then locate the

"lip" that results in the lower edge of the recessed mould. A soft mallet is used to force the panel into the shape of the mould.

When making the mould, keep the overall width only slightly greater than that of the louvre, otherwise it will not be possible to space the individual louvres reasonably close together.

The "venetian blind" type of slot (Fig. 13b) required no mould. The positions are marked out and cut, using a metal cutting fret saw after drilling a small pilot hole. Cut only as far as shown, and then, using either finger pressure or a pair of pliers, bend as shown.

Both of the above methods require a certain amount of practice before really good results are

Fig. 11: This method of construction requires no bending of metal.


Fig. 12: $\frac{1}{2}$ in. and lin. angled metal bolted together with countersunk bolts can be used to make a cabinet frame.
obtained, and a few test runs should be made on a piece of scrap aluminium first.

## Plastics and Insulating Materials

Most plastics materials can be bent under the application of heat and thus may be used for some forms of cabinet construction. If sulficient heat is applied the material can be melted. Fittings such as nuts, bolts, hinges, etc., may therefore be heated and moulded permanently into the plastics if needed.

Most plastics are easily worked, and special glues are available for fitting plastics to plastics or to other materials. If only two-dimensional bends are required, the plastics can be heated locally and bent around a wooden former to obtain the required shape. If three dimensional shapes are required, it will be necessary to make a male or female mould and apply heat over a large area when shaping the material on the mould.

Most non-plastics insulating materials are non-malleable but can be cut and drilled fairly easily. Both of the materials mentioned above are best suited for use in the type of construction shown in Fig. 11, where simple panels are used.

Part Three Next Month
Fig. 13: Methods of forming louvres for ventilation purposes.

# Preventing Accidental Tape Erasure 

TWERE is no perfect system of preventing accidental erasure of wanted recordings and many recorders have mechanical or electrical "reminders" that the instrument is switched to "record" and, therefore, will erase any previous recording.

An additional precaution which will prevent erasure, unless a microphone plug or other signal source plug is plugged in the appropriate socket, is described below.

Using sockets of the Bulgin J14 type. the arid of the r.f. erase and bias oscillator valve is earthed until a plug is inserted and, of course, with the grid shorted to chassis erasure is impossible. even though the instrument is switched to "record".

This feature is well worth incorporating because if the instrument is being used for playback only and a microphone is not available for plugging-in, then the recordings are safe.

A single screened and insulated lead is taken from the oscillator valve grid pin to the jack socket (see diagram). The outer screen should be taken to the nearest chassis point at the valve socket.

This system cannot be used with recorder anplifiers which use a common output/oscillator valve. however the erase head feed or winding can he shorted via the jack socket but it will be found that the bias current will partially erase. This is better than losing the recording.

## BY J. SCOTT



Fig. I: The input circuit arrangement for the recorder with a single socket.


Fig. 2: The arrangement for recorders with two input sockets.

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ANYBODY who watched Prof. Colin Cherry expounding on the telly about Science and Communications, will have been struck by the idea that our boxes of electronic tricks were no more than links between the mysterious forces that direct our existence and the puny grey cells that fill the space between our ears.

The conception of information theory does not concern us here -which is just as well. for my ignorance of the subject is just as remarkable. But the implicit assumption that the means are infallible, given enough time for development. and only the ends matter, is rather alarming.

A recent report from the Equipment Reliability, Committee of the Electronic Engineering Association only serves to confirm my view that the boffins are overlooking one vital point in their assessment of the electronic situation.

This report, for example, shows a graph failure rate of electronic equipment against time. As one might have expected, the curve starts high, swoops rapidly, levels out. then creeps up at an ever-increasing rate. Which means that the gear breaks down


Moybe one of the girls was mooning. . .
more frequently, just after it is thrown together, settles to a comparatively trouble-free level for a while, then begins to break down again as it ages.

To some extent, we go along with that view. Ton often, brand new sets conk out and investigations prove that the faults could -nay, should-have been foreseen in production. Things like dry joints, wrong components, carly mechanical wear, and so on.
You and I. concerned mainly with our own little box of hombs, tend to give the bencfit of the doubt to the manufacturer. Maybe one of the girls on the production line was mooning as our set went by and forgot to apply the solder gun. What we overlook is the fact that her lovesick lapse will have affected half a hundred other prospective owners, too.

So, in this report. the committee advocate the manufacturer delivering his product "only after the constant failure rate period has commenced. . .".

Doesn't that phrase strike a cold chill? The constant failure rate, mate, is the time you and me are going to be proud users of the equipment.
They have even worked out the probable frequency of breakdown, and computed a "Mean Time Between Failure", which they cleverly abbreviate to MГВF. From this. they work out a formula for reliability, saying, the MTBF over $t$ hours being
$\overline{\mathrm{T}}$, then $\mathrm{P}_{\mathrm{s}}=\frac{\mathrm{e}^{-\mathrm{t}}}{\overline{\mathrm{T}}}$
This gives the frightening calculation that for a chance of successful operation for various multiples of T , the MTBF required to give a 90 per cent chance of fulfilling a two hour mission successfully must be $2 / 0 \cdot 1$, or twenty hours. It makes you wonder how they ever got


A tendency to give off wild puffs of smoke...
Telstar up there, let alone working.

My point is that the boffins have overlooked a vital factor. This elusive parameter, the "H" factor- (H for Henry, I'm after a Nobel Prize)-must be inserted in any formula that attempts to assess reliability. It is the tendency of a piece of electronic gear to give off wild puffs of smoke, or horrid noises. or sudden bouts of unbearable silence. at the most embarrassing moments.

Just at the moment when the Director of the Electronological Institute is passing through. or when those political purseholders who haunt the men at R3 pay a visit, or when Aunt Mabel comes to tea, the "H" factor comes into play.

We have laboriously built the hi-fi rig. planed and glued the cabinetry, tackled all the wires out of sight, assembled our friends and neighbours for the preview and-presto-comes a power cut. Small use citing the Reliability Committee or quoting MTBF then. As your wife passes the coffee and makes with the small talk. you can muse on the " H " factor, and write another failure up to experience.

H. WEBSTER

## FOR THE BEGINNER'S S.W.SUPERHET

CONTINUED FROM PAGE 968 OF THE FEBRUARY ISSUE

IN a c.w. frequency transmission the carrier wave is unmodulated and means must therefore be provided to render the signal intelligible at the receiver. In the simplest type of receiver such as the detector and l.f. type this is often accomplished by making the detector oscillate at a frequency slightly removed from the incoming frequency.

The difference in the two frequencies is equal to the frequency of the beat note. This process whereby the detector itself provides the local frequency is known as the autodyne method. Another and more general method employed in the superheterodyne receiver is to use a separate oscillator. This oscillator, known as the beat


Fig. 7: The one-valve circuit of the b.f.o. unit.

## COMPONENTS LIST

Resistors:

| RI | $47 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R3 | $47 \mathrm{k} \Omega$ IW |
| :---: | :---: | :---: | :---: |
| R2 | $47 \mathrm{k} \Omega$ IW |  |  |

## Capacitors:

| C | 100 pF silver mica |
| :--- | :--- |
| C 2 | 100 pF silver mica |
| C 3 | 100 pF silver mica |
| C4 | $0.1 \mu \mathrm{~F}$ tubular |
| VCI | 15 pF variable (Jackson C804) |

Miscellaneous:
VI 615
SI S.P.S.T. switch
L. L, L2 1.6Mc/s b.f.o. coil. Denco BF02

International octal ceramic valveholder. Chassis top plate $4 \mathrm{in} . \times 7 \mathrm{in}$. (Home Radio). Knob, wire, etc.


Fig. 8: Details of the b.f.o. chassis which is eventually attached to the main receiver chassis. This arrangement may be seen in one of the heading photographs on page 1055.
frequency oscillator, injects an unmodulated signal into the second detector circuit. The frequency of this oscillation can be varied over several kilocycles each side of the receiver intermediate frequency.

A further and important use for a b.f.o. is in the reception of single side band (s.s.b.) transmissions. Since these signals are generally transmitted with little carrier, means must be provided to insert the carrier at the receiver. A description of this technique will be given later in the article.

## Circuit

The b.f.o. is built round a $6 \mathbf{J 5}$ medium impedance triode. The circuit diagram is shown in Fig. 7. L1, L2 is a Denco $1 \cdot 6 \mathrm{Mc} / \mathrm{s}$ beat frequency oscillator coil. The frequency of the oscillator can be varied a few kilocycles each side of the $1.6 \mathrm{Mc} / \mathrm{s}$ i.f. by means of a panel-operated control VCl . Screening of the unit is of importance since harmonics of the b.f.o. may find their way into the front end of the receiver. Although the author did not find this troublesome it may be necessary to screen the 6 J 5 to reduce the b.f.o. injection.

## Constructional Details

The b.f.o. unit is built on a small sub-chassis which is mounted on the main receiver chassis. Sufficient space is available between the output valve ( 6 V 6 ) and the gang capacitor. The subchassis is cut from a 7 in . x 4 in . piece of aluminium
to the dimensions given in Fig. 8. The method for mounting on the receiver chassis is given in Fig. 9. Since the unit is comparatively small care must be exercised in wiring the components. It will be


A rear view of the completed preselector described in last month's issue.

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Fig. 9 (above): The position of the b.f.o. unit on the moin chossis. The shaded parts indicate components on the original receiver.

Fig. 10 (for left): Underchassis wiring of the b.f.o. unit.

Fig. 11 (left): Additional wiring from the power input socket of the main receiver, to provide for the b.f.o.
noted that no fixing details are given for the b.f.o. coil unit. Fitting is best done using the unit itself as the template.

A point-to-point wiring diagram is shown in Fig. 10. When wiring is complete the usual routine chack is made of the resistance between h.t. positive and chassis. If this is satisfactory the unit may be bolted to the receiver chassis and the heater and h.t. leads taken through the hole in the receiver chassis. The power leads are soldered to the tags of the octal innut socket at the rear of the receiver. The relevant details are shown in Fig. 11.

## Adjustment and Operation of B.F.O.

Adiustment of the b.f.o. is best done with the aid of a signal generator such as was described in the original article. Inject an unmodulated signal of $1 \cdot 6 \mathrm{Mc} / \mathrm{s}$ via the top cap of the frequency changer. Set the b.f.o. panel trimmer to midcapacity and then carefully adjust the dust core of
the b.f.o. coil until zero beat is obtained. The setting is now correct.

If no signal generator is available the coupling between the. grid and anode of the i.f. stage pentode can he increased to the point where the stage breaks into oscillation. A gentle hissing noise will be heard at this point. The b.f.o. is adjusted until zero beat is again obtained.

## Single Side Band Reception

S.S.B. signals can be rendered intelligible by the following procedure. The signal is accurately centred on the main receiver. If the preamplifier is used the gain control is set to minimum and the receiver volume control turned to maximum. VR1 is now adiusted until a weak signal is heard. Switch on the b.f.o. and adjust the pitch control until intelligible speech is obtained. A little practice may be needed before the correct setting is obtained. THE variable frequency oscillator described here may be used to control the two-band speech transmitter (January. 1965. P.W.) so that no crystals are needed. It enables the transmitter to be tuned to any frequency in the 1.8 or $3.5 \mathrm{Mc} / \mathrm{s}$ amateur bands.

The v.f.o. may be employed with other transmitters. The fundamental operating frequency is $1 \cdot 75-2 \mathrm{Mc} / \mathrm{s}$ but output may be taken at $3.5-$ $3.8 \mathrm{Mc} / \mathrm{s}$ if a different transmitter requires this.

Fig. 1 shows the circuit and the VR 150 regulates the anode and screen supply for the 6AG7. I.1, the oscillator coil. is tuned by VC1 from $1.75-$ $2 \mathrm{Mc} / \mathrm{s}$. There is good isolation between I. 1 and the anode circuit and 1.2 is tuned to about $1-9 \mathrm{Mc} / \mathrm{s}$ and needs no further adjustment. A coaxial lead takes r.f. to the transmitter.

Heater and h.t. currents are drawn from the companion transmitter. Heater drain is 0.65 A , plus 0.3 A for the indicator lamp. For h.t. about 25 mA will be needed at $200-500 \mathrm{~V}$.


BYF.G. RAYER G30GR

## CONSTRUCTION

As the v.f.o, replaces the crystals. rigid construction is needed. An aluminium box about 7 in . $x$ $5 \mathrm{in} . \mathrm{x} 3 \mathrm{in}$. is used, completely enclosed, and with a 7 in . $x 3 \mathrm{in}$. shelf bolted 2 in . from the case top. The panel is screwed to this shelf and the box to increase rigidity. L1, TC1. C1 and VC1 are below the shelf with other components in the top compartment.

The valve and voltage regulator stand clear on top of the v.f.o. so that their heat does not cause unnecessary frequency. drift in the circuit L1. All components are securely held. with short leads and tag strips where needed. With these precautions the general stability of the unit was found satisfactory.

Fig. 2 shows all internal wiring. including the underside of the box top, to clarify valveholder connections. Stout wire such as 18 s.w.g. is used throughout. Two leads pass through the shelf. These go to B on Ll and to R1 and C2. These wires are in thick insulated sleeving which is a push fit in the holes.


Fig. 1: The v.f.o. circuit. The operation of this simple circuit is described in the text.

It will be seen that $I$ ? is at right-angles 10 L .1. I2 is atlached to a bracket on the shelf and is horizontal. All construction must be perfectly solid to avoid randon changes in frequency.

## V.F.O. COIL

L. 1 is wound on a strong paxolin tube in . in diameter and about $2 \frac{1}{2} \mathrm{in}$. long. Drill two small
holes at A (Fig. 2). About lin. away drill two further holes for end $C$.

A length of $265 . w . g$. enamelled wire is anchored to some convenient point and threaded through the holes at A . The centre lin. of the tube is smeared thinly with an adhesive cement. The coil can then be wound by rotating the tube, walking slowly forwards and keeping the wire under


Fig. 2: The complete :. ring diagram of the finished unit.
tension. Turns are side by side. After winding 25 turns make the small loop B, then continue for a further ten turns, finishing at C. Scrape and tin B and the winding ends. A dise of wood is cemented in the tube and drilled for a fixing bolt.

## ANODE COIL

L2 was a small medium wave coil of unknown manufacture. Coils of this kind with adjustable cores can be tuned to about $19 \mathrm{Mc} / \mathrm{s}$. Tuning is by adjusting the core to suit stray circuit capacity.

The correct tuning of L2 can be found by placing a wavemeter near the coil or by observing grid current in the transmitter. For the latter purpose a $0-5 \mathrm{~mA}$ meter is convenient. After calibrating the v.f.o. set it to about the middle of the band. When the core of L 2 is rotated a broadly resonant peak will be found corresponding to maximum grid current. There is little change in grid drive when tuning the v.f.o. across the band, so L2 can be left peaked at about the middle of the band.

If a different transmitter requires an input in the 80 m band L2 should be adjusted to about $3.65 \mathrm{Mc} / \mathrm{s}$. A suitable coil can be 65 turns of

## COMPONENTS LIST

## Resistors:

| R1 | $4.7 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ |
| :--- | :--- |
| R2 | $6.8 \mathrm{k} \Omega$ |
| $l$ |  |

## Capacitors:

| CI | 200 pF silver mica |
| :--- | :--- |
| C2 | 100 pF silver mica |
| C3 | $2,000 \mathrm{pF}$ silver mica |
| C4 | 200 pF silver mica |
| C5 | $2,000 \mathrm{pF}$ silver mica |
| TCl | $50,60,75$ or 100 pF air-spaced trimmer |
| VCI | 100 pF s.w. variable; high quality |

## Miscellaneous:

| V1 | 6AG7 | V2 | VRI50 |
| :--- | :--- | ---: | ---: |
| LI, L2 See text for details |  |  |  |

Two octal valveholders and indicator lamp holder. Two insulated tags and tag strip. Universal chassis $5 \mathrm{in} . \times 7 \mathrm{in} . \times 3 \mathrm{in}$. with $5 \mathrm{in} . \times$ 7 in . plate and extra $7 \mathrm{in} . \times 3 \mathrm{in}$. runner (Home Radio). Paxolin tube, dial drive, wire, etc.

32s.w.g. enamelled wire side by side on a 1 in. diameter dust-cored former. For the $160 / 80 \mathrm{~m}$ speech transmitter the v.f.o. output is $1.8-2 \mathrm{Mc} / \mathrm{s}$ for 160 m and $1 \cdot 75 \cdot 1 \cdot 9 \mathrm{Mc} / \mathrm{s}$ for $3 \cdot 5 \cdot 3 \cdot 8 \mathrm{Mc} / \mathrm{s}(80 \mathrm{~m}$ band).

Should the v.f.o. be employed with a different transmitter it is generally best to have the v.f.o. output on one-half the frequency of the first stage of the transmitter as this avoids instability. The 160 m output is then used for 80 m , but a 80 m output would be handy for doubling to 40 m . If a two-way switch is fitted in place of the lamp both 160 m and 80 m anode coils may be used to give output on either band.

## POWER SUPPLIES

These are drawn from the transmitter, h.t. being required at net and transmit positions of the function switch but not at receive. To arrange this take the h.t. connection from S 1 as in Fig. 3.

For easy interconnection a valveholder or threeway socket is fixed to the transmitter panel. A matching plug or old valve base wired to the tag strip in Fig. 2 allows the v.f.o. to be brought into use at once.

The coaxial cable is fitted with a plug which is inserted in the crystal socket going to R1 (Fig. 3). The other crystal socket is unused.

## RESISTOR R3

For the $160 / 80 \mathrm{~m}$ transmitter with a $250 / 0 / 250 \mathrm{~V}$ transformer R3 is $4.7 \mathrm{k} \Omega, 2 \mathrm{~W}$. This gives a regulator current of about 20 mA . In other transmitters the h.t. voltage may be greater and R3 must then be increased. This is readily done by taking 150 V from the actual potential available, then using Ohm's Law to find R3 for this voltage drop with about $25-30 \mathrm{~m}$ A flowing, e.g. $7 \mathrm{k} \Omega$ would do for 350 V supply, etc. Alternatively connect a


A rear view of the completed prototype v.f.o. unit.
meter in serics with the voltage regulator and adjust R 3 until the regulator draws about 25 mA .

## TRANSMITTER DOUBLER

When operating on 160 m the onginal crystal oscillator valve acts as an untuncd buffer. No changes at all are needed except to plug the v.f.o. in instead of a crystal.

When working in the 80 m band the first transmitter stage must operate as a doubler. This is donc by fitting an on/ofl switch on the chassis and panel near the crystal socket and wiring it to a $3 \cdot 65 \mathrm{Mc} / \mathrm{s}$ coil as in Fig. 3. This coil can be 65 turns of 3Is.w.g. enamelled wire, side by side. on a $\frac{1}{2}$ in. diameter former provided with an adiustable dust core.

For 160 m the switch is left open. For 80 m set


Fig. 4: Connections for a two-pole, three-way switch to be incorporated in the transmitter meter circuit to provide indications of grid and anode currents.
the v.f.o. to roughly $1.8 \mathrm{Mc} / \mathrm{s}$ and adjuṣt the new coil core for maximum grid current with the switch closed. The switch must be open if crystals are inserted.

## GRID/ANODE SWITCH

For the above adjustments a fairly accurate indication of small changes in grid current will be necessary. It may thus be felt worth while to change the transmitter meter circuit to show grid and anode currents at will.

A three-way, two-pole rotary switch can be mounted on the transmitter panel near the meter and wired as in Fig. 4. With the switch in the position shown, grid current is read. The $470 \Omega$ resistor is only to complete the grid circuit when reading anode currents. The most convenient neter is a $0-5 \mathrm{~m} \mathrm{~A}$ model.

With the switch fully turned 10 its other position the meter reads anode current, the shunt changing the range to $0-100 \mathrm{~mA}$. It is necessary to use a threc-way switch so that the contacts clear the grid circuit before completing the anode circuit. But if a break-hefore-make two-way switch is to hand this is perfectly suitable.

In use grid current is checked as necessary and the meter is then used to show anode current as previously described.

## V.F.O. CALIBRATION

VC1 has a large knob with dial, a reduction drive being optional. It is only necessary to calibrate for one band as 80 m coverage is obtained by the second harmonic.

A crystal calibrator or marker is ideal for calibration. Open VC1, tuace a receiver to $2 \mathrm{Mc} / \mathrm{s}$ from the marker and adjust TC. until the v.f.o. is at zcro beat. Mark the dial $2 \mathrm{Mc} / \mathrm{s}$. The process can then be repeated at 1.95, 1.9, 1.85, 1.8 and $1.75 \mathrm{Mc} / \mathrm{s}$.

Divisions are filled in between the calibrated points. The 160 m hand is indicated from 1.8 $2 \mathrm{Mc} / \mathrm{s}$ on one scale. Each frequency is then multiplied by two and placed on a second scale for 80 m . Only frequencies from $3 \cdot 5-3 \cdot 8 \mathrm{Mc} / \mathrm{s}$ ( $1.75-1.9 \mathrm{Mc} / \mathrm{s}$ fundamental) should be shown on the 80 m range.

## V.F.O. WORKING

The method of loading up and tuning the transmitter for crystal operation has already been described. V.F.O. working is similar except that any required frequency can be selected.

If a $C Q$ call is to be made find a vacant channel with the recciver and tune the v.f.o. to this, using the net position of the switch. Then switch to transmit and tune the p.a. as described.

If a CQ is to be answered the v.f.o. is tumed to zero beat with the transmission heard, again using the net position. The p.a. is then quickly tuncd with the function switch at transmit. The switch is then returned to receive until the calling station stands by for replies. The switch is then turned to transmit and a reply made.


T|HE amplifier to be described was built to fulfil the requirements of a medium power amplifier at the lowest possible cost. Although it could not be placed in the hi-fi class by any stretch of the imagination, it gives a good output for a wide range of inputs.

When originally designed, careful consideration was given to parts available from the junk box, and many constructors will probably find that they already have the majority of the parts. There are no critical values in the amplifier at all. and even starting from scratch, with careful buying from the columns of this magazine it should be possible to make the amplifier for about $£ 210$ s. (excluding case).

The original amplifier had two low level inputs (actually for two guitar pick-ups) and a treble cut control but it can easily be modified to give up to ten low level inputs, with or without the treble cut control, and also a socket can be brought out to give a high level input (i.e. from a gramophonc or carbon microphone). It can therefore be built for virtually any application which requires a maximum output of approximately 7W.

## CIRCUIT DESCRIPTION (FIG. I)

The amplifier is a hybrid design: that is, it uses transistors for low level amplification, and valves for the driver and the output stage. Both valves and transistors derive their power from a mains power pack.
This arrangement was decided on because modern transistors are well suited to low level
amplification and are also cheaper than their valve counterparts: a wholly transistorised amplifier could have been designed, but transformers for transistorised amplifiers are still quite expensive items.

Direct coupling is possible. but can be difficult to set up properly without an oscilloscope. A hybrid amplitier offers the best compromise between cost and simplicity compatible with performance.

## TRANSISTOR PREAMPLIFIER

The transistor preamplificr uses two OC71 Mullard transistors (or equivalents) in a conventional $\mathrm{R}-\mathrm{C}$ coupled circuit. The two inputs are wired so that the operation of one control does not effect the other control. RI and R2 in series with the inputs ensures that the microphone or pick-up is not completely short circuited when the associated volume control is turned down to its minimum position.

The volume controls are coupled to the base of the first transistor by C1; R3 and R4 determine the base bias for the transistor. R5 and R6 are chosen to give a collector current of approximately 1 mA in the first stage, and R9 and R10 give a


Fig. 1: The basic hybrid circuit - 5 the "Codet", complete with preamplifer stage and power supply.

coilector current of approximately 1.5 mA in the second stage.

The preamplifier will work satisfactorily with a supply voltage between 4.5 and 15 V . though a certain ameunt of gain will be lost at the lower voltages. and the circuit may be rather noisy at the higher supply voltages (depending on the transistors used).

A nominal supply voltage of 9 V was chosen. obtained by using two 6.3 V windings on the mains transformer, and the voltage is set for optimum performance when the amplifier is tested by means of a 5 ks : peset potentiometer (VR4) in the power supply.

## MAIN AMPLIFIER

The output from the preamplifier is taken via C4 to the grid of a 655 triode. This feeds a 6L6 beam tetrode operating in class" A". A treble cat circuit is provided between the two valves. The h.t. for the valves is approximately 275 V with the values specified.

As with the preamplifier, the main amplifier was tested with voltages between $180-400 \mathrm{~V}$, and again, the ouput was somewhat lower with the lower voltages and a bit noisier at 400 V .

One side of the secondary of the output transformer should be eathed, not only from a safety point of view, but also to prevent parasitic oscolla-
tions which can occur when a long lead is used to the speaker.

## THE POWER SUPPLY

The power supply uses a full wave transformer and modern silicon rectifiers which are available at at reasonable price through the columns of this magazine. These are very efficient and have a very low voltage drop across them: but because they have such a low impedance they can be destroyed by switching-on surges.

Some suppliers suggest that a resistance of approximately $50 \Omega$ is connezted in series with the rectifier. However, most, if not all, of the resistance is supplied by the windings of the transformer, so the series resistors have not been included in this design, but 2W 479 resistors may be wired between the rectifier and the transformer for safety if required. Alternatively, metal rectifiers may be used if they are to hand or more easily obtainable.

The negative 9 V supply is obtained by wiring two of the low voltage secondaries of the transformer together, and using a simple half-wave rectifier circult with a smoothing consisting of $5 \mathrm{k} \Omega$ preset potentiometer and two $100 \mu \mathrm{~F} 25 \mathrm{VW}$ electrolytics. Most transformers have at least two 6.3 V windings,

## COMPONENTS LIST

Resistors:

| R1 | $4.7 \mathrm{k} \Omega$ | R 10 | $1 \mathrm{k} \Omega$ |
| :--- | :--- | :--- | :--- |
| R2 | $4.7 \mathrm{k} \Omega$ | R 11 | $270 \mathrm{k} \Omega$ |
| R3 | $56 \mathrm{k} \Omega$ | R 12 | $56 \mathrm{k} \Omega$ |
| R4 | $10 \mathrm{k} \Omega$ | R 13 | $1 \mathrm{k} \Omega 2$ |
| R5 | $3.9 \mathrm{k} \Omega$ | R 14 | $270 \mathrm{k} \Omega$ |
| R6 | $1 \mathrm{k} \Omega$ | R 15 | $180 \Omega 1 \mathrm{~W}$ |
| R7 | $39 \mathrm{k} \Omega$ | R 16 | $1 \mathrm{k} \Omega 5 \mathrm{~W}$ |
| R8 | $10 \mathrm{k} \Omega$ | R17 | $100 \mathrm{k} \Omega 2$ (for neon) |
| R9 | $2.7 \mathrm{k} \Omega$ |  |  |

All $10 \% \frac{1}{2} \mathrm{~W}$ carbon unless otherwise stated
Potentiometers:

| VR1 | $100 \mathrm{k} \Omega$ | VR3 | $1 M \Omega$ |
| :--- | :--- | :--- | :--- |
| VR2 | 100k $\Omega$ | VR4 | $5 \mathrm{k} \Omega$ |

- R2


## Capacitors:

$\mathrm{Cl} \quad 8 \mu \mathrm{~F}$ electrolytic 25 V
C2 $8 \mu \mathrm{~F}$ electrolytic 25 V
C3 $\quad 25 \mu \mathrm{~F}$ electrolytic 25 V
C4 $\quad 0 \cdot 1 \mu \mathrm{~F}$ paper 350 V
C5 $25 \mu \mathrm{~F}$ electrolytic 25 V
C6 $\quad 25 \mu \mathrm{~F}$ electrolytic 25 V

| C7 | $0.02 \mu \mathrm{~F}$ paper 350 V |
| :--- | :--- |
| C8 | $0.1 \mu \mathrm{~F}$ paper 350 V |
| C 9 | $25 \mu \mathrm{~F}$ electrolytic 25 V |
| C10 | $32 \mu \mathrm{~F}$ electrolytic 450 V |
| C11 | $32 \mu \mathrm{~F}$ electrolytic 450 V |
| C12 | $32 \mu$ electrolytic 450 V |
| C13 | $100 \mu \mathrm{~F}$ electrolytic 25 V |
| C14 | $100 \mu \mathrm{~F}$ electrolytic 25 V |

Valves and Semiconductors:
V1 6J5 V2 6L6

Trl, Tr2 OC7l or equivalent
D1,D2 $\quad 400$ p.i.v. 100 mA silicon rectifiers (see text)
30 V 5 mA surplus diode (see text)

## D3

Miscellaneous:
T1 Output transformer: ratio $3 \cdot 5 \mathrm{k} \Omega: 3 \Omega 8 \mathrm{~W}$
T2 Mainstransformer. Secondaries:250-0-250V, $80 \mathrm{~mA} ; 6.3 \mathrm{~V}, 3 \mathrm{~A} ; 6.3 \mathrm{~V}, 1 \mathrm{~A}$ (see text)
LI $10 \mathrm{H}, 100 \mathrm{~mA}$ choke (see text)
FI 2A fuse
70 '90V neon, tag strips, aluminium, etc.


Fig. 2: The modification to the VI circuitry to provide a high level input. This allows for the use of record player, carbon microphone and similor inputs with the amplifier.


Fig. 3: Using this modification up to ten inputs to the preamp. may be provided. with the addition of a master volume control ( $10 \mathrm{k} \Omega$ potentiometer).


Fig. 4: Complete wiring details of the main amplifier and power pack chossis.
or one 6.3 V winding and a 5 V winding for the rectifier.

The 6.3 V winding (with the larger current capacity if there is more than onc winding) has one side connected to the chassis: this also supplies the heaters of the valves. The other winding is connected in series with the first winding.

It must be connected the right way round otherwise the two windings will be $18^{\circ}$ out of phase and the total output voltage will be zero. To check the sense of the connections, connect the transformer to the mains, and connect the two low voltage windings together and measure the output voltage.

A 12 V bulb can be used for this purpose if no a.c. meter is available. The bulb will glow brightly with the windings connected one way round. and the windings should be connected in this sense when building the amplifier.

Virtually any diode can be used for the 9 V supply since it is only required to supply about 2.5 mA . One of the diodes obtainable at about $1 \mathrm{~s}, 6 \mathrm{~d}$. will be adequate. Note that the black end goes to the smoothing circuit and the red end goes to the transformer.

The 250 V supply is smoothed Fig. 5: Construction details of the preamplifier chassis which is built separately by a choke-resistor-capacitor arrangement: this was found to be more than adequate. If required, the choke could be replaced by a $1,000 \Omega 10 \mathrm{~W}$ resistor with consequent economy but slight degradation of performance.

## MODIFICATIONS

As has been previously stated, a number of modifications can be introduced in to the amplifier to increase its usefulness while it is being built. The treble cut control may be omitted by removing C7 and VR3.

A high level input socket may be added simply by bringing out the grid of VI via a length of screened cable to a suitable socket. It is not very simple to provide a volume control at this point however, because the output impedance of the transistor amplifier will effect the use of such a control.

However, the circuit of Fig. 2 would work since the volume control has been "turned round". RI is made a variable component, and the slide is taken to the grid of VI.

The real limit to the number of channels is the layout. since the more channels there are, the greater the problems of hum pick-up and control interaction become. There is no reason why 10 channels should not be possible so long as efficient screening and the shortest possible lead between the input socket and the potentiometer are used. A master volume control may be built in between the two transistors by making R 8 a variable component.

## CONSTRUCTION

The author's original amplifier was constructed to fit in a case 17 in . $\times 5 \mathrm{in}$. $x 5 \mathrm{in}$. This gave plenty of room (except that a 6 L 6 M had to be used instead of 6L6G, since the 6L6G was taller than 5in.!!. The layout is by no means critical providing the usual rules are followed such as wiring the heaters first of all and keeping the leads carrying a signal as short as possible.
The output transformer, smoothing choke and mains transformer should have their cores in opposite planes to avoid interaction. No wiring carrying $50 \mathrm{c} / \mathrm{s}$ (such as mains or heater supplies) should pass anywhere near the preamplifier.

It is suggested that the main amplifier and the power pack are constructed on the same chassis and the preamplifier is constructed on a tag board and fixed under the main amplifier chassis. It is a good idea to use transistor sockets so that different transistors can be tried to select one for good noise characteristics.

The cabinet is left to the constructor's ingenuity (don't forget that the 6L6 gets fairly hot in operation). If required the cabinet can be dispensed with and the amplifier left as a plain chassis with the controls on the front. A neon bulb was used as a pilot light; a low voltage bulb wired across the heater winding would be equally sufficient. A mains fuse of 1 A should be included in the live mains lead.

## TESTING

When the amplifier has been completed and the wiring checked the amplifier should he connected to the mains supply. The chassis should always be earthed when the amplifier is in use, not only because this is safer but it also cuts down hum and noise.

The preamplifier should be left disconnected at this stage. When the main amplifier has warmed up and a loudspeaker has been connected a pronounced hum should be heard when the grids of the valves are touched with a screwdriver.


Fig. 6: Basic details of a suggested cabinet for the loudspeaker.

Assuming that the main amplifier works, check that the transistor supply is giving a negative output and turn the preset potentiometer down to its minimum voltage setting. This voltage may be quite high. since there is no load connected across it.

Switch off the mains and connect the preamplifier. Turn on the mains and adjust the preset potentiometer to give approximately 9 V . (If no meter is available set it for minimum noise.) An input, such as a low impedance microphone, can now be connected and the whole amplifier tested.

## LOUDSPEAKER AND ENCLOSURE

An 8 in. 10W loudspeaker was used with the original amplifier. This was mounted in a shallow box with the dimensions shown in Fig. 6. A single piece of wood (say) 20 in . x 16 in . would have been just as efficient acoustically but it is well worth the trouble involved in making the baffle board into a shallow box. since it not only makes it more convenient to stand up hut it also protects the speaker from accidental damage to the back of the cone.

Finish of the case depends on how much money and time the constructor is prepared to allow. The box itself should be solidiy made $\frac{1}{2} \mathrm{in}$. ply or chiphoard to avoid resonances at the lower frequencies to be handled. If the box does resonate it may be necessary to include one or more braces to increase the rigidity.

The dimensions given should serve as a guide: actual measurements can be decided by the individual. If required the main amplifier and power pack chassis could be mounted at the bottom of the box and the preamplifier and controls could be mounted at the top.

## KEYED AUDIO OSCILLATOR

## -continued from page 1043

arrangement, causing the audio oscillation to rise and fall at the beginning and end of each pulse respectively, smoothly over about one cycle. The capacitor C5 should have ten times the capacity of the capacitors Cl to C 4 determining the andio frequency to realise this condition correctly. Since the audio output has an amplitude of some 4 V r.m.s. with VR3 turned full up, only simple audio amplifiers are required for even the most powerful transmitters met with in amateur transmitters. The output can alternatively be plugged in in place of the mike of an existing telephony transmitter, giving immediate conversion to m.c.w. operation without any other alterations of any kind.

A few words about the advantages of m.e.w., for which the carrier runs uninterrupted as in telephony, the Morse characters being impressed as corresponding bursts of a.f. modulation as if these were music or speech signals. Apart from the fact that no b.f.o. is required in the receiver and some loss of signal-to-noise ratio the greatest outstanding advantage is the available multiplicity. Several Morse operators at the one transmitter can
each key their own Veroboard circuit with thell own particular audio frequency output. All outputs are used to modulate the one transmitter simultaneously. At the receiver each receiving operator interposes a tuned circuit resonant to the audio frequency of his intended signal in front of his phones. Alternatively the entire signal can he tape recorded and a single receiving operator can read each message successively on successive playbacks with his audio resonant circuit tuned to the m.c.w. channcls one after the other. Ordinary carrier-keyed c.w. cannot transmit more than one message per r.f. channel. When it is remembered that with the m.c.w. technique single sideband (s.s.b.) modulation techniques can be combined therewith. the upper and lower sidebands containing completely different sets of multiplex m.c.w. signals, it is clear that the total information which can be modulated on to a single r.f. carrier frequency without exceeding the conventional bandwidth is quite enormous. It is little wonder that these types of communications systems are very popular with the GPO nowadays! They provide some measure of solution to the increasing congestion of the communications wavebands.

# BUILDING A TRANSISTOR SOLO organ 

CONTINUED FROM PAGE 945 OF THE FEBRUARY ISSUE

TIHE layout of the three panels-the wiring of which was detailed last month-the controls. batteries and sockets viewed from underneath the cabinet. is shown in Fig. 8.

## Keyboard Switches

For ease of manipulation from the keyboard it was decided to adapt the three-way switches so that they are moved by levers instead of knobs.

The levers were made from $\frac{1}{2}$ in. wide strips of brass about $\frac{1}{6}$ in. thick and 2 in . long. For half the length. width is reduced to $\frac{1}{4} \mathrm{in}$. At the end of the wide portion a $\frac{1}{4}$ in. clearance hole is drilled and the surface adjacent to this hole tinned.

We now need bosses (with gitub serew's) to which the levers can be soldered. A brass $\frac{1}{4} i n$. spindle coupler sawn in half will provide us with two. The circular ends are tunned and ptaced on the tinned portion of the levers. with holes correctly aligned, and heat with pressure applied with a large solderıng iron, when they should unite.

The case under the keys is recessed back $\frac{3}{3} \mathrm{in}$. The switches are fixed so that the ends of the levers project out $1 \frac{3}{4}$ in. from centre of spindles and come level with front of keyboard.

Coloured plastic adhesive tape is now bound around the ends of levers to form a neat handle.

## The Keyboard and Case

Assuming the constructor has an accordion keyboard, and the rest of the instrument has been dismantled. we should now have the keyboard with its keys sticking up in the front and at the end of each a spike with leather covered pallets attached.

Care must be taken now as we cannot level the keys until a baseboard has been fitted. This should be of plywood the width of the keyboard plus 1 in. and 12 in . from back to front and about $\frac{1}{4} \mathrm{in}$. thick.

Any plastic covering should be removed and the keyboard now placed so as to be level with the front of the baseboard, $\frac{1}{2} \mathrm{in}$. spacing either side, and fixed to it with countersunk screws.

As the front of the keys are sticking up it can be seen that under them is a shallow compartment containing key guides and springs. It is the bottom of this compartment which is fixed to the baseboard and any screws coming through from baseboard will need to be carefully positioned or kept short. The strongest fixing will be into the key blocks at each end.

Having fixed the keyboard we can attend to the keys. The pallets should be removed and the malleable spike on each key carefully pressed back and downwards to form an extension of the key whilst the front of key is held down firmly.

The spikes should now rest on a felt-covered piece of wood the length of the 29 keys. Height of wood is by experiment (see Fig. 9). The keys can now be levelled and adjusted to give a tin. deep touch at the front.

The idea now is to build up a compartment at the back of the keys and another under the baseboard. The bottom compartment need only be $1 \frac{1}{4}$ in. deep and will accommodate all the panels, batteries and switches (Figs. 8 and 9).

Planed wood $1 \frac{1}{4} \mathrm{in}$. $x \frac{3}{4} \mathrm{in}$. is cut to length and mitred or butt-jointed in the form of a frame and fixed with countersunk screws level with back and sides of baseboard. The front part of the frame should be fixed $\frac{3}{4}$ in. from the front of baseboard. A piece of hardboard cut to the size of the frame and fixed with countersunk screws will form a cover.

The top compartment is built up in a similar manner with $\frac{1}{2}$ in. wood. Depth must be obtained by measuring from top of highest spike and, with the key down, adding $1 \frac{s}{3}$ in. for hopper and another


Fig. 8: The layout of the bottom compartment which accommodates the three panels, batteries and controls.
tin. for clearance; this height to the baseboard is the width of wood required.
The planed wood is now fixed on the baseboard level with the back and two sides. The sides, which finish level with the front of the keyboard, are shaped and levelled down to the original key blocks, to which a fixing can be made.

Fig. 10 shows the author's meihod of fixing the panels to the interior casework. The screws remain captive and wiring always held clear.

## Using Piano Keys

These can often be obtained from a piano dealer as old instruments taken in part exchange are always being broken up. They are slightly larger than accordion keys and for the same
compass of 29 keys would need another $2 \frac{1}{2} \mathrm{in}$. or one could make do with 25 notes (two octaves).

They would need to be shortened from the back and each one fitted with a coil tension spring. The upward thrust of the keys would be taken by a felt-covered wooden bar situated over the keys just at the back of the black notes. From then on they could be adapted as later described for accordion keys.

## Making Action for Key Contacts

The action to be described uses spring brass sliding contacts which are self-cleaning and found

Fig. 9: This drawing illustrates how keys, hoppers, distribution strips, etc., are arranged within the cabinet.


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Fig. 10: The method of fixing the panels to the case-work.

reliable in use. Twenty-nine vertical strips of $\frac{1}{16} \mathrm{in}$. paxolin $\frac{1}{4} \mathrm{in}$. wide and $1 \frac{3}{4} \mathrm{in}$. long will now be required as drawn in Fig. 11.

These will now be referred to as hoppers and each one is drilled with a holc just large enough to go on the key spike. The holes should only have very slight clearance in the direction required in keeping the hoppers upright throughout the movement of the key.

A $\frac{1}{4}$ in. length of cycle valve rubber tubing is pushed on to each spike, followed by the hoppers and another piece of rubber tubing. The hoppers can now be lined up level by adjustment of the tubing. which also prevents undue movement of the hoppers. These can now be roughly checked by moving each key while holding the hopper vertically between the fingers

Paxolin ( $\frac{1}{16}$ in. thick) is used throughout and if two pieces are laid side by side on a flat surface it is possible to feel if one is slightly thicker than the other. A small piece of the thicker should be put aside for guide pieces and will save having to stick on gummed paper to allow hoppers to work freely.

Two strips of paxolin are now required, one $\frac{9}{1 g}$ in. wide and one $\frac{11}{16} \mathrm{in}$. wide: length is a clearance fit between the two checks of the top compartment and in line with the hoppers.

Place the two strips together with edges level on a flat surface, clamp together with both ends level. Measure $\frac{1}{4}$ in. from each end on the narrow strip and mark for drilling a 4 BA . hole centrally.

Drill the two holes, turn the assembly so that the level edges are top and overlapping edge bottom back, unclamp and mark each one on the front for identification and right way up.
The action supports should now be made from $\frac{1}{16}$ in. aluminium angle (see Fig. 11). Drill with two
holes each so that they can be fixed, one on each key block, after being lined up exactly with the hoppers.

From now on it will be easier to work with the organ case on its back and the hoppers straightened out. The widest long strip is placed under the tops of the hoppers and brought up to the underside of action supports. The other, narrower, long strip is now placed on top of the hoppers and action supports.

Spring paper grips or clothes pegs will be found useful here to temporarily hold things together. The exact spot can now be marked for drilling a hole in each support. One 4BA. bolt and nut each end will be sufficient.

Correct height is ascertained by seeing that none of the hoppers project beyond the top of the two long strips when keys are held down. Drill the 4BA. holes in each support. bolt together and check that everything is in line. Procceding, with organ still on its back. the guides can now be made -from the thicker paxolin if any.

From now on each note is treated individually. Guides may vary from $\frac{3}{3}$ in. to $\frac{1}{4}$ in.: the main concern now is that each hopper will be truly vertical when playing.

Each part, including the hoppers, must be numbered on the front. Start by making the first guide against the metal support, filing down where necessary so that adjoining hopper would be truly vertical. Fach one is now cut down to $\frac{11}{10} \mathrm{in}$., numbered on front and reinserted, and process repeated throughout.

It will facilitate later assembly if the bottom corners of each guide are slightly rounded. also tops of hoppers.

A supporting piece of wood along the wide strip and wedged up from back of case would now help. Check that each guide is in place and level with top edges, mark for drilling on strip dead centre between hoppers and $\frac{1}{8}$ in. down from top of strip. Mark bottom of each guide $\frac{1}{15}$ in. up.

While the guides are in place mark off where the short contact strips are to be fixed on the front paxolin strip as in Fig. 11. Take out guides,


The finished instrument comblete with the expression bedal.
numbering if not already done, place aside in order. Unbolt and remove long strips and bolt them together.

## Drilling Guides and Strips

All holes are $\frac{1}{82}$ in. diameter. Care must be taken with this small drill and all work should be clamped or weighted down to ease withdrawal.

An archimedean drill is best but if a hand machine drill is used it may be necessary to pad out the stem of drill so it can be gripped in the chuck.

A sharp-pointed awl pushed down hard on the work will assist in starting the drill at the correct point. Drill holes through the two long strips while bolted together and clamped down. Drill. one hole at bottom of each guide (Fig. 11).

With organ again on its back reassemble as before and with each guide correctly in place mark each through the holes in top strip. Drill these holes and lay guides aside. Remove strips from supports.

Thoroughly clean and cut one strip of phosphorbronze, as used in draught excluders, 13 in . long and in. wide for rear contact strip. For front strip 15 pieces tin. wide are needed. They are measured off as in Fig. 9, allowing for bending each end at rightangles to fit into saw cuts. Remove and trim ends to just under $\frac{1}{16}$ in. so as not to project inside. Put aside in order.

Drill holes to take $\frac{\pi}{\text { litin. }} \mathrm{x}$ No. 1 brass countersunk screws where the centre of each short strip will come. Countersink so that the screw head is level with paxolin, cut off threaded end, make a slight countersink at the back, put screws in from
front, place and hold firmly on a piece of flat iron, tap end of screw until it is tight, finally see none project at back. Lightly tin each screw head.

Fit contact strips into saw cuts, hold down near centre with a screwdriver and correct if not laying flat. Still holding down firmly, apply a hot iron just over the screw head and hold down with screwdriver for a moment to cool.

The 13 in . long bronze strip can now be fitted to the rear paxolin strip. Scratch a line $\frac{3}{8} \mathrm{in}$. from the top-this will give position of the bronze strip working edge (see Fig. 11). Fixings can be made as before with a tinned screw positioned over each guide.

## Assembly of Action

Wire staples are made from copper wire, a good fit in the holes. Bend at right-angles to match length between each pair of holes, commencing with guide against the metal support. Push through the two strips and guide, bend over to fasten.

When completed place assembly on the two supports and gradually push down whilst inserting the hoppers between their guides.

This done check that all work freely and, if necessary, remove any guide by undoing the staple and easing or packing as required.

The hottom holes in guides are drilled through into the wide strip. With care it is possible to do this without removing the assembly. A thinner wire is pushed through each drilling, given one twist and snipped off. It is an advantage that there should be a little sideplay here.

CONCLUDED NEXT MONTH


Fig. II: lllustrating the making action of the key contacts and their construction details.



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## The Broadcast Bands-by John Guttridge

1ITHOUGH this feature is called "On the Short Waves", it is interested in DX (long distance) reception news of all sorts. News is given therefore this month of some recent loggings in the medium waveband.

For the beginner to medium wave DX the best station to try for is the Trans World Radio-Radio Nederland transmitter at Bonaire in the Netherlands Antilles. From 2330-0020 it carries the Spanish programme of Radio Nederland followed by the English programme from $0040-0130$. From 0130 the programmes of Trans World Radio can be heard. The frequency is $800 \mathrm{kc} / \mathrm{s}$. In London a SINPO rating of 34343 was recorded at 0130 recently. Another very reliable one is the Canadian CBA (Maritime) on $1070 \mathrm{kc} / \mathrm{s}$.
Two listeners who have been " working" North America on medium waves between 2200 and 0200 are J. Fitzgerald (Great Missenden) and D. Walsh (Ballylynch, Ireland). Some of those logged were640 CBN St. John's. Newfoundland: 660 WNBC New York: 710 WOR New York: 860 CJBC Halifax, Nova Scotia: 880 WCBS New York: 930 CJON St. John's. Newfoundland; 940 CBM Montreal: 960 CHNS Halifax, Nova Scotia; 1.010 WINS New York: 1.010 CFRB Toronto; 1.050 WHN New York: 1,090 WBAL Baltimore; 1,130 WNEW New York: WMEX 1,510 Boston; 1,520 WK BW Buffalo; 1.560 WQXR New York.*
Now let's take a look at changes in the Short Wavebands. First comes news from E. H. Conduit (Wolverhampton) of the introduction of English and Spanish transmissions by Radio Alocrie. They are aired from 2200-2230 and 2230-2300 respectively on 11.835.

According to R. Coates, of Burton-on-Trent, the schedule of AFRS New York is now 1430-1900 on 15.225: 1430-1800 21,645: 1430-2245 15,280; 1815-2245 11.920; 1900-2245 11.905. The transmitters used are those of the Voice of America at Bound Brook (WBOU) and Greenville. Reception in London is usually good on most frequencies. Mailing address of the station is Armed Forces Press, Radio and Television Service, 250 West 57th Street, New York 19, U.S.A.

[^2]News of test transmissions by Saudi Arabia Broadcasting comes from Roy Patrick (Derby) who says reports are wanted and should be sent to the Deputy Minister, Ministry of Information, Jeddah, Saudi Arabia. He has heard the transmissions from 1500-1700 on 9,670. Frequencies of 7,170 and 11,890 are also used according to the International Short Wave Club.

Radio Nacional de Espana now has a 50 kW transmitter at Teneriffe in the Canary Islands, says Roy Patrick. Transmissions are from 1400-1600 on 9,660 . This frequency is given as 9,640 by the ISWC which also mentions a transmission from $0000-0300$ on 11,800

This year the Far East Broadcasting Company, Box 2041, Manila, Philippines, hopes to put the first of several new high power transmitters into operation. At present English programmes are aired at the following times. $2200-2330$ on $15,300 / 17,810$; $0330-0100$ on $11,850 / 15,380 / 17,810 ; 0100-0200$ on 15.380: 0230-0300 on $9,710 / 11,740 / 15,380 /$ 17.810 (also $0300-0830$ Sundays plus 15.300): 0830 - 0900 on $9.710 / 11,920 / 15,380 / 17,810$; $0900-$ 1200 on 15,380/17,810; 1200-1430 on 15,300; 1230 - 1300 on $9.505 / 15,300: 1330-1400$ and $1530-$ 1630 on 9,505 . There is also an 0900-1000 transmission on 11,850 .

On March 7, 9,520 replaces 15,165 for the 0630 -0700 and 0900-1000 transmissions from Radio Denmark. At the same time 15,165 replaces 9,520 for the $1600-1630$ transmission.

Special English language programmes for the Caribbean are carried by the B.B.C. from $2230-$ 2245 on Mondays to Fridays. The frequencies used are $6,110 / 9.580 / 11,750$.

English language programmes are now transmitted as follows by Radio New York Worldwide, 4 West 58th Street, New York 19. N.Y.. U.S.A. From 1200-1615 on $17,760 / 15,440 / 15,135 / 11,940$; 1615-1730 $\quad 17.760 / 15,440 / 15,135 / 11,940 / 11,840 ;$ 1730-1745 17.760/15.440/11.840; $1745-2000$ 17.760/15.440/11,840/9.640; 2000-2015 15.440/ 9.640: 2015-2140 15,440/11,940/11,855/9,640; $2140-2200$ 11,940; 2200-2400 6.015/11,940. The transmissions are beamed to Northern South America, the Caribbean, Africa, Continental Europe, the British Isles and Scandinavia.

Radio Moscow announces that the following frequencies are being used for its English transmission to North America starting at 2300: 9,660/9,620/ $9.570 / 7.360 / 7.310 / 7,290 / 7,250 / 7,200 / 7,150$. Reception in London is good.
At present one of the most frequently heard 19 metre band transmitters is that of the Voice of America at Greenville.

From 1300-1400 15.235 can be heard with Spanish for Latin America. At 1400 the beam switches to Europe with a consequent jump in signal strength and a programme in Georgian begins. The signal is good and programmes include Ukranian at 1530, Armenian at 1600 and Latvian at 1900. The Europe English outlet of 15,205 has
been heard at gond strength at 1600 and 1900. CW interference spoils the 15.250 outlet which is beamed to Africa. Swahili is carried at 1830 with Arabic from 1900-1930. One of the last channels to fade out in the evenings is 15,415 which carries French and English to Africa. At close down at 2215 it returns SINPO 35333.

## The Amateur Bands-by David Gibson G3JDG

SUCCESS, success!! At last my ageing eardrums have been stimulated by signals heard on $21 \mathrm{Mc} / \mathrm{s}$. At 1140 G.M.T. on the 16 th December I heard G3TMA OHIWF, SMSLH, SM5BKY, EL8AF and. 6W8BL, all on c.w. Now an important point: readers sending in reports must make clear whether the stations logged were on 'phone or c.w. In order to avoid confusion 'phone stations can be given a two digit signal report, and c.w. three digits. These digits are, of course, the standard amateur Readability, Signal strength, and Tone. For instance: G3TMA (579)-R5 S7 T9. Therefore, the station was c.w. Or G3TMA (57), i.e. R5 S7, the station was on 'phone. Better still, keep 'phone and c.w. separate.

## Top Band

160 metres is going like a bomb! G-DX is about almost nightly and many Europeans are popping up. December 10th raised VO1FR (Newfoundland) 459, GM3FXM. GW3TOW. GW3HUM GW3DRV, GW3PMR and GW3SPA, all between 2300-2330 G.M.T. December 16th gave 9L1TL (Sierra Leone) 569. VO1BD 459, VOIFB 559, OK 100579.
It may not be generally appreciated, but at the moment the 160 metre Transatlantic and Worldwide DX tests are being held. Accepting a kind invitation from SWL Frank Videan I went along to his QTH to listen in on one of these test dates (December 20). The receiver was an Eddystone 888 A , but the antenna was only 30 ft of wire running from the bedroom window to the fence. We heard all these:

DJ8GR, DL7AA. PAØPN. 9L1TL, OK1AFN, OK1KLX, OK1AGB. VOIBD, GW3CW, GW3SPA, PA V VB, OK1IQO, VO1FB. GM3TMK OK1KIT, W1BB/1, W2IU, W1WY, DL1FF, W2GGL, W1HGT, VE3DDR, W1BU, VE2UQ, W8HRV, GI3PDN, VE3AGX, W2UWD, W1BHQ, VE2LI.

The next test dates are February 7th and 21st from 0500 to 0730 . I would be interested to know what you hear.

## Other Bands

This month ten metres has been very dead, and twenty, usually good for some DX, failed to oblige. At the time of writing, it dies a natural death around 1900 . Forty metres, however, is quite lively now and again. On December 13th most of Europe was there on c.w., including DJISQ, OK2KHF, LZ1KPG, SP8AJK, UA6CP, IT1AGA, YU1LM, YO5THY.

And at 1845 two real pieces of DX came out of nowhere.- VK2EO (449) and VK7SM (459) in QSO with YO8KAE. Just goes to show that besides sharp ears the magical gifts of patience and persis-
tence are a requirement for DX winkling. Two virtues not possessed by your scribe!

Eighty was disappointing. Early evenings produced Europeans only, but later around 2330 the best that came in was W1PKW.

## Readers' Reports

From Renfrewshire, Gillies Wylie sends in the following report:
$21 \mathrm{Mc} / \mathrm{s}$. SSB:-9M4LX, ZE4JZ, MP4TBJ, ZS7R, XEIFSV.
A.M. - VK6QL, VK3AZY, CR4AJ, CR7GM, 9JZMI, 9L1WN, VE3CQG, CT2AL. C.W.ZD3TJ. W8AMO, WA1AGO, all between 1005 and 1830 hrs .
$14 \mathrm{Mc} / \mathrm{s}$. $\quad$ SSB:-ZB2AK, FM7WQ, VK6MK, HC1MX, HK5ACI, VE1AJR/SU, W6MWF, VE6CJ.
$3.5 \mathrm{Mc} / \mathrm{s}$. SSB:-WA2EVH. W1ONK. A.M.VE2SX. VOIFX, SM7BSE/MM.
SWL Coull in Littlestone. Kent. has a recently acquired HRO with an end fed 60 ft. antenna. This set up is working extremely well as the following list shows:-
$3.5 \mathrm{Mc} / \mathrm{s}$ - VEIIE (57), W1FRR (58), KIKDA (54/5). W2ZDL (56/7) all round 2200 and all SSB.
$14 \mathrm{Mc} / \mathrm{s}$ :-VE8ML (59). VE8RG (48). OX3MN - (58). TG9RJ (57). all SSB from 1500-2000.
$2 / \mathrm{Mc} / \mathrm{s}:-\mathrm{VK} 2 \mathrm{NN}(57)$. VK3AZY (58), ZC4TJ (56). 9J2W (58). 9J2DT (58). ZS1AB (56), WøYDB (58), KøFPZ (56). ZS6U (57).
R Collins writes in to query Z6AP/KC4 heard on 20 metres at 2330 and claiming the QTH as Queen Maud Land, Antarctica. Anyone else heard this one?

Maurice Curtis in Sheffield with an EA12 receiver found the following on $14 \mathrm{Mc} / \mathrm{s}$ 'phone between 1345 and 1845 :-
K5ZVP, W2RNV, W2RAV, UO2GC, W2ONV, W4SHP, UH8BO. HB9JO. W2BLF, W4RJO, VO8AF, K8AIR, W4FZE. K1DRE, W5AZI/MM (Marine Mobile) 11 FW , W8TF, W4BHU, WIKJ, W9DPI, DJ5JI.

## News in General

People puzzled by the prefix SPØ will be pleased to note that the $\varnothing$ prefix was issued to SP stations instead of their numeral i.e. 9 and was authorised for the duration of the International Marathon DX scheme which was in operation from May to September last year. VK3TL reported loose on Norfolk Island with s.s.b. and c.w. while CEØAG also s.s.b. and c.w. is keeping Easter Island on the radio map. In case you think its cold at your QTH, spare a thought for KC4USN who is in Antarctica. He runs s.s.b. into a Rhombic antenna pointed at
-continued on page 1093

## New list of Bargains

## Transistor ferrite rod aerial with th lony wave woils with ciroult， $7 / 6$ ．

 Ogcillator Coill sud set of 3 I．F．trsnstormert tor transistor set with circuit， $1 \% / \mathrm{\theta}$ ．Tuning Condenser to suit alr－apaced with trimmers garg Coudensers to suit， $8 / 8$（requesi sub imith，circirit）．Midzet 3in＿P．M．Lontspeaker 3 ohm 12／0． 80 ohm 18／8．
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other gear． $10 / 6$ each．Pont $3 /$ ．
Battery Charger Kit．Comprisea 5 amp．trann－ former， 8 amp．rectller，metal case and moter to charge 8 or 12 volt batterles up to $B$ armpe． With variable aharge rate， $80 / 6$ esch Poat and insuranoe， $3 / 8$ ．
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## Transistor Set Inductive Amplifier

${ }^{\top}$ ROM Design Engineering Wokingham Lid., comes the "Dewtron" Wave Trap, designed to improve reception on medium wave stations when used in conjunction with any transistor or portable radio.

Basically the circuit comprises an r.f. stage. which contains a ferrite tuned circuit capable of receiving m.w. signals. The amplification of this stage is very high, and its output is fed into an inductive element on the end of a length of screened cable. This element is termed the "injector", because when placed near to the ferrite rod in the portable radio. its output is injected into the aerial by direct induction.

On distant stations, the Wave Trap injects a boosted signal in such a way that the mean level of received signal at the set is of sufficient order to ensure that the a.v.e. circuit operates, and will then ensure that any variations in the mean received signal level will not be noticed in the loudspeaker. When used in place of a car aerial on reasonably local stations. the high factor of amplification afforded by the Wave Trapis circuit makes sure that the inherent directional characteristic of the Wave Trap receiving ferrite aerial is cancelled. since the receiver is once again fed with a signal of sufficient strength to make it operate well beyond the a.v.c. threshold. even when the vehicle turns so that the Wave Trap aerial is in the "null" position. Battery voltage is 9 V and the current drain is 4 m A. Price is 39 s . 6d.. p. and p .1 s .6 d . Desigh Engineering (Wokingham) Lud., "Caledon"', Ringwood Road, Ferndown, Dorset.


## SSB Transmitter/Receiver

' 'HE Hanmarlund Manufacturing Company, a Giannini Scientific Company, has announced the CSB-125C s.s.b. transmitter/receiver. The power output of this unit is 125 W s.s.b.-p.e.p., and six channels can be provided (two of these suppled and the other four optional), to cover the frequency range 2 to $30 \mathrm{Mc} / \mathrm{s}$.

The CSB-125C features sensitivity of less than $0.5 \mu \mathrm{~V}$ for s.s.b. $/ \mathrm{c} . \mathrm{w}$. and $1 \mu \mathrm{~V}$ for 10 dB s.n. $/ \mathrm{n}$ ratio. $30 \%$ modulation on a.m. The separately houstd power supply is designed for $115 / 230 \mathrm{~V}$, $50 / 6 \mathrm{c} / \mathrm{s}$ operation.

The U.K. agents for this range of equipment are K.W. Electronics Lid., Vanguard Works, I Heath Street. Darlford, Kent.


Hammarlund's CSB-125C s.s.b. tronsmitter/receiver.

## Mains/Battery/Table Radio

A
NEW model in the Bang and Olufsen range is the Beo Box battery operated transistor table radio. having a separate power unit for mains operation. It covers v.h.f., medium, long and two short wave bands $(1.45-4 \mathrm{Mc} / \mathrm{s}$ and $7-16 \mathrm{Mc} / \mathrm{s})$. and has 14 transistors and 8 diodes. Weighing 161 b ., and measuring $19 \frac{3}{3} \mathrm{in}$. $x 8 \frac{3}{1} \mathrm{in}$. $x$ in.. this receiver has the feature of providing a high standard of reproduction without a mains supply. The output is 2 W when operating from the mains and 1 W when working from batteries. There is an 11 in . $x$ 7in. elliptical speaker, and separate treble and bass controls are provided. A 500 1 . moving coil indicator gives visual indication of accurate tuning, and the aerial is detachable and rotatable and can be used for the improvement of v.h.f. and short wave reception. Finished in teak. the Beo Rox retails at 39 guineas. St. Aldate Warehonse Limited, Innsworth Lane, Gloucester.

Above: The "Dewtron" Wave Trap inductive amplifier.

Right: The BEO BOX fully tronsistorised bottery, mains table radio.


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## 5: THERMIONIC VALVES

### 5.1 The Emission of Electrons from a Filament

WTHEN a hut wire or FIIAMENT is enclosed in an evacuated glass bulb it will gave off "paricles". These particles are called ELEECTRONS. If a plate of metal is introduced into the bulb it will be found that electrons from the filament will strike the plate. Many more electrons will be attracted to the plate if a POSITIVE potential is applied to it as this will attract the negatively charged electrons. The higher the positive potential appled to the plate the greater will be the electron flow from the filament to the plate. In the diagrams shown in Fig. 38 the electrons emitted by the filament are represented by arrows.

As we saw when dealing with simple d.c. circuits a current can only flow in a circuit when the circuit is complete. Therefore to show the current flowing from the flament to the plate a millammeter must be connected between the filament and the plate.


Fig. 38: A heated filament in an evacuated bulb emits electrons (a), some of which strike the metal plate (b). When a positive potential is applied to the plate, more electrons are attracted to it (c) and the greater the potential, the greater the electron flow (d).

The flow of electrons from the filament to the plate or ANODE is the principle on which the operation of the radio valve is based. The valve is so called because it will allow electrons, which enable a current to flow, to travel in one direction only-i.e. towards the plate or anode. If a negative potential were applied to the anode no current would flow as this would only repel the negatively charged electrons.

### 5.2 The Diode

This is the simplest type of valve and it has only two ELECTRODES, the FILAMENT or CATHODE and the PLATE or ANODE. The two electrodes are generally arranged concentrically so as to increase the area of the anode.


Fig. 39: The diode: (a) practical representation: (b) theoretical representation.

In the diagrams shown in Fig. 39 the type of diode shown is called a directly heated diode. This is because the electrons which travel to the anodo come directly from the filament. However, the surface area of the filament is very small and the current which could be drawn from it would also be snlall. The current could be increased by increasing the temperature of the filament but an easicr way is to encase it in a sheath of metal which will emit many electrons at a low temperature. In this case the filament now becomes the HEATER (i.e. it heats the sheath) and the sheath is called the CATHODE. This type of valve, which has the heater enclosed by the cathode, is called an INDIRECTLY HEATED type as the electrons come from the cathode and not the heater.


Fig. 40: The indirectly heated diode, proctical construction (a) and theoretical representation (b).

Practical and theoretical representations of an mdirectly heated diode are given in Fig. 40 (N.B.: The cathode in an indirectly heated valve is generally made of a base metal with a coating of barium oxide, strontium oxide, etc.).
?

### 5.3 Characteristic Curve of the Diode



Fig. 41: Circuit to determine the characteristic curve of a diode.

If the circuit shown in Fig. 41 is set up the anode voltage can be varied and for each value of anode voltage the corresponding value of the anode current can be found. It would be suitable to start the anode voltage at 0 and increase this in 10 V steps until no further increase in anode current is noted.

Typical results obtained using the circuit shown in Fig. 41 are shown in Fig. 42 and the graph which results when these are plotted is shown in Fig. 43..

It can be seen from the graph that there is a fairly long, STRAIGHT LINE portion and the valve is generally operated within the limits of this portion


Fig. 42: (inset table): Typical values obtained using the circuit in Fig. 41.

Fig. 43: Graph obtained by plotting Va against la.
of the graph-e.g. in this case the valve would be operated with anode voltages between 20 and 50 V and anode currents of between 3 and 13 mA . It can be seen that on the graph the anode current has been represented by la and the anode voltage by Va. This type of graph is therefore usually called an la/Va graph and, as its name suggests, it shows the relationship between anode current and anode voltage.
If the graph shown in Fig. 43 is studied it can be seen that after a certain value of anode current is reached any further increase in anode voltage will not cause it to rise any furtber. When this occurs the value of anode current noted is called the SATURATION CURRENT and the valve is said to be SATURATED. The point on the graph where saturation first occurs is called the SATURATION POINT.


Fig. 44: Choracteristic curves using different heoter voltoges.

If the characteristic curve for a diode were taken with heater voltages less than the recommended value the curve(s) woukd be of the type shown in Fig. 44.

### 5.4 The A.C. Resistance or Impedance of a Diode <br> We know from Ohm's Law that $R=\frac{E}{I}$

therefore if we find the limits of the straight line portion of the characteristic curve of a diode we could express the SLOPE of this portion of the graph as being from, say, $20-50 \mathrm{~V}$ and from $3-13 \mathrm{~mA}$. This is represented on Fig. 45. We can see that the line AB extends over 30 V and the line $B C$ extends over 10 mA . Knowing that $R=-$ the a.c. resistance of the valve could be expressed as being

## 30 <br> 001 ("I " must be in AMPS) or $3,000 \Omega$.

Therefore the a.c. resistance of this particular diode would be expressed as being 3,000 . The a.c. resistance of a valve is sometimes called the IMPEDANCE or DIFFERENTIAL RESISTANCE of the valve. The valve used as an example

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in the above calculation would normally be operated with anode voltages of $20-50 \mathrm{~V}$ and anode currents of $3-13 \mathrm{~mA}$.


Fig. 45: Determination of the a.c. resistance of the diode.

### 5.5 The Diode as a Rectifier

From the section which dealt with a.c. theory it will be remembered that an alternating current could be represented graphically in the form shown in Fig. 48; this would also. of course, be the same shape as a graph of an alternating voltage (both graphs being drawn with respect to time, of course). However, it can be seen that the current (or voltage) starts at zero, reaches a maximum positive value, returns to zero, reaches a maximum negative value and returns to zero once more. This is a complete CYCLE for an alternating current or voltage.


Fig. 46: Typical a.c. waveform.

The mains supply in most areas is an alternating supply and if d.c. is required for any particular purpose then this a.c. has to be changed to d.c. or, to use the correct term, it has to be rectified.

We already know that a diode will allow a current to pass through it only when a positive voltage is applied to the anode, therefore if an alternating voltage were applisd to the anode of a diode a current would only flow on the POSITIVE HALF-CYCLE. The current flowing in the circuit would therefore be no longer a.c. as it would now not have a negative component.
The current could be said to be an UNSMOOTHED DIRECT CURRENT. The diode has then changed the a.c. shown in Fig. 46 into the type of d.c. shown in Fig. 47, i.e. the diode has acted as a RECTIFIER.


Fig. 47: Current flowing in the anode circuit of a simple diode rectifier.

In the diagram shown in Fig. 48 it will be seen that the alternating current has been supplied by a TRANSFORMER and that the D.C. OUTPUT of the rectifier has been connected to a LOAD which has been represented by " $R$ ".


Fig. 48: Typical circuit using a diode as a simple rectifier.

### 5.6. Smoothing the Output from a Simple Diode Rectifier

Where a steady current of the d.c. type is required it is obvious that a current of the type shown in Fig. 47 will be unsuitable. This current has then to be SMOOTHED. We know that a CAPACITANCE is an electrical device which can be used to "store" a current. If we were to connect a large capacitor across the load R in Fig. 48 what would be the effect? Well, between A and B the capacitor would be charging and between B and C


Fig. 49: The a.c. waveform: (a) before rectification; (b) after rectification and (c) with smoothing capacitor.
the capacitor would be discharging. Thus the capacitor would be a current to the circuit where previously no current had been flowing. The capacitor would in fact be acting as a RESERVOIR for the current and is in fact called a RESERVOIR CAPACITOR. The larger the value of the capacitor the greater the smoothing effect. The three stages mentioned in the rectification of a.c. by a simple diode circuit are shown in Fig. 49. (It is often said that a SMOOTHING CAPACITOR "absorbs the peaks and fills in the troughs " of the type of waveform shown in Fig. 47.)

The type of rectifier which only rectifies one half of the a.c. cycle, i.e. a single diode, is called a HALF-WAVE RECTIFIER.

## Question

Attempt to answer the following questions which relate to the graph given in Fig. 50.

1. Mark with an " $X$ " the point where saturation occurs.
2. Between what values of Va and Ia would the valve be normally operated?
3. Using the graph, calculate the a.c. resistance of the valve.
4. In practice would you expect the graph to pass through the points $V a=0, I a=0$ ?


Fig. 50: The graph relating to this month's problems.

## Answer to last month's question

$$
\begin{aligned}
\mathrm{f} & =\frac{10^{6}}{2 \pi \sqrt{\mathrm{LC}}} \\
& =\frac{10^{6}}{6.28 \sqrt{ } 10 \times 100} \\
& =\frac{10^{\circ}}{198.6} \\
& =5,035 \mathrm{kc} / \mathrm{s} \text { or } 5.035 \mathrm{Mc} / \mathrm{s} .
\end{aligned}
$$

New frequency is $2,517 \mathrm{kc} / \mathrm{s}$.

$$
\begin{aligned}
& \therefore \quad 2517=\frac{10^{6}}{6.28 \sqrt{ } 10 \times \mathrm{C}} \\
& \sqrt{ } 10 \mathrm{C}=\frac{10^{8}}{6 \cdot 28 \times 2517} \\
&=\frac{10^{\circ}}{15810} \\
& \begin{aligned}
\therefore \sqrt{ } 10 \mathrm{C} & =63.25 \\
\therefore \sqrt{ } 10 \mathrm{C} & =63.25^{2} \\
& =4000 \\
C & =\frac{4000}{10} \\
& =400 \mathrm{pF}
\end{aligned}
\end{aligned}
$$

## Part 6 Next Month

SEE ALSO PAGE IO94 THIS MONTH

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SIR,-I think that you and many readers of
Practical Wireless and Practical Television may be interested in the response to my letter in the October issue of P.W. (page 577) in which I offered free all my past issues of the two magazines.

1 had 256 letters requesting copies. and in order to be as fair as possible I selected letters at random; within ten days I had dispatched all my copies to 88 readers by post and the half dozen local ones 1 delivered personally.

1 had (in my simple way). expected about six requests and was staggered, to say the least, by the amount of mail that descended on me. On three days there were as many as 60 letters per day!

The pleasant task of reading so many friendly letters was enjoyable. I am so sorry to have had to disappoint many, many readers, but I could easily have distributed 50 copies of each issue had they been available.

The one unpleasant aspect of my "give-away" scheme was the out-of-pocket expense it caused me, principally by the thoughtlessness of so many people who enclosed crossed P.O.'s, loose cash, stamps, cheques and paper money etc., and in some cases not even a threepenny stamp!

Only twelve readers enclosed an s.a.e.; to them many thanks, they were a great help in what proved to be a gigantic task of replying to everyone.

Incidentally, only ten readers out of nearly 90 to whom I sent copies, bothered to send a word of thanks.

So may I warn any other reader who might be considering the same offer as mine, that my out-of-pocket expenses have been:- 212 threepenny stamps-(£2 13s.), 136 P.O.'s (3d. poundage)( $£ 1$ 14s.) and 200 envelopes. writing paner, wravpers etc.-(9s. 3d.) totalling $£ 4$ 16s. 3d. - J. F. Hitchcock (Sutton, Surrey).

## UNUSUAL MICROPHONE



IR,-Having built my tape recorder from a kit, I was very dissatisfied with the peaky result from my crystal mike. This led me to thinking that a more expensive one such as a ribbon type may be the answer to my problem but the price of such an instrument stopped my progressive thoughts. It was then that I decided to experiment with a small $2 \frac{1}{4}$ in. loudspeaker with an $80 \Omega$ voice coil, but alas,

Whilst wo are always pleased to assist raaders with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commarcial or surplus equipment. We cannot supply alternative dotails for receivers deacribed in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELEPHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iii of the cover.
The Editor does not necessarily agree with the opinions expressed by his correspondents
my junk box did not reveal a matching output transformer. All that could be found was an old 230 V in $230+6.3 \mathrm{~V}$ out mains transformer removed from an old TV converter. Nevertheless, it was all that was available and I subsequently connected my speaker (now to be called microphone) to the 6.3 V winding. feeding the 230 V winding to my tape recorder input.

The result was most surprising, a very fair allround response and my " lapespondent" friend feels certain that I am using an expensive ribbontype mike!

Should any other readers be interested in similar experiments they may care to bear in mind the fact that the actual cone diameter of the speaker should be no less than $2 \frac{1}{4} i n$., as this would probsbly resalt in loss of bass response.-Jorn B. Cox (Brighton).

## CORRESPONDENTS WANTED

SIR,-I am interested in transistor circuitry and radio in general. I would like to correspond with anyone who is interested in radio and who is about my own age (16). - Donald Gabried (43 Oliver Plunkett Street, Blandon, Co, Cork, Ireland).

## ON THE SHORT WAVES

-continued from page 1078
America, and you never know he may spray a little r.f. in your direction (listen at the high end of 20 m band).

Part One of the 1965 ARRL DX contests are scheduled for February and could provide something interesting. There are two sections: 'phone a.m. and s.s.b. and c.w. In February there is one section of each with another in March. The full list of contest dates this month is as follows:-

6th—7th QCWA Party.
13th-14th ARRL DX Contest, 'Phone section.
14 th $70 \mathrm{Mc} / \mathrm{s}$ Contest.
20th-21st BERU Contest.
20th-21st YL/OM 'Phone Contest.
27th-28th ARRL DX Contest, c.w. section.
27th-28th REF Contest, 'Phone section.
The ARRL contest by the way, starts at 0001 G.M.T. Saturdays and ends 2400 Sundays.

My thanks to listeners who sent in logs. We are hoping to provide report forms to make it easier to send in a log. If you would like to send in a regular report drop me a line with your address (printed please) and I'll forward them if and when they become available.


ACTON, BRENTFORD AND CHISWICK RADIO CLUB Hon. Sec.: W. G. Dyer, G3GEH, 188 Gunnersbury Avenue, Acton, London, W. 3.

At the meeting to be held on 16th February at 8 p.m. at 66 High Road, Chiswick, the Club will be having a show of mixed films, to which all those interested in amateur radio are invited.
CHESTER AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: P. J. Holland, Field House, 19 Kingsley Road. Great Boughton Chester.

The only function arranged for January by the outgoing committee was the A.G.M. held in the Y.M.C.A. hall. Chester
CLIFTON AMATEUR RADIO SOCIETY
Hon. Sec.: J. Rose, G30GE, 63 Broomfield Road, Beckenham, Kent.

Winner of the 1964 Constructional Contest was SWL Dave Reed, with a $430 \mathrm{Mc} / \mathrm{s}$. transistor convertor.
COVENTRY AMATEUR RADIO SOCIETY
Hon. Sec.: E. E. Snow G3TKO, 11 Lupton Avenue, Coventry.
On Ilth lanuary there was an evening of construction on the Club top band transmitter, and on the 18th there was a Frequency Measurement symposium. On 25th January there was a lecture aimed at SWLs, entitled H.F. Bands Convertor.
DERBY AND DISTRICT AMATEUR RADIO SOCIETY
Hon. Sec.: F. C. Ward, G2CVV, 5 Uplands Avenue, Littleover, Derby.
The R.S.G.B. Affiliated Sociaties' Contest was held on 23rd and 24th January, and on 3rd February the Annual General Meeting took place.
DURHAM CITY AMATEUR RADIO SOCIETY
Hon. Sec.: M. Allenson, G3TGD, Physics Department, University of Durham, South Road, Durham.
The Society is now one year old and can look back on a prosperous year with average attendances of thirty or more members. Meetings are held every alternate Thursday at 7 p.m. at the Bridge Hotel, North Road, Durham.
Hotel, North Road, Durham.
FAREHAM AMATEUR RADIO CLUB
FAREHAM AMATEUR RADIO CLUB
Hon. Sec.: C. A. Gledhill, G3LGX, li3 Oak Road, Fareham, Hampshiro.
Meetings of this club take place formighty at 39 Nicholas Crescent, Fareham, and full details can be obtained by writing or telephoning the Hon. Secretary at the above address.
telephoning the Hon. Secretary at the above address. Hon. Sec.: J. Ingram, G3RMQ, Lambert House, Greetiand, Halifax, Yorkshire.
The speaker on 26th January was J. J. Platt, G2VO, whose topic was "Radio a long time Ago". On the 30th and the 31 st January, there was the CO Worldwide 160 meter Contest.
MID-WARWICKSHIRE AMATEUR RADIO SOCIETY
MID-WARWICRSHIRE Inkester, 13 Dormer Place, Leamington Spa Warwickshire.

The New Year activities commenced on Monday, Ilth January with an Open Meeting. The meeting on 25 th January was devoted to a filmshow, and will be followed on 8th February by the Annual General Meeting.
Anrual General Meeting. NORTHERN HEIGHTS AMATEUR RADIO SOCIETY NORTHERN HEIGHTS AMATE
Hon. Sec.: A. Robinson, G3MDW, Candy Cabin, Ogden. Halifax, Yorkshire.

With the permission of Stew WIBB, a copy of his tape-recorded talk entitled "Top Band DXing", along with slides has been made and any club wishing to borrow it may do so, provided that the club concerned agrees to registered postage both ways. Application should be made to G3MDW.
READING AMATEUR RADIO SOCIETY
Hon. Sec.: R. G. Nash, G3EJA, 'Peacehaven', 9 Holybrook Road, Reading Berkshire.

The Annual General Meeting was held on 30 th January at the Palmer Hall, West Street, Reading, and new officers were appointed to take over from those retiring this year.
SLADE RADIO SOCIETY
Hon. Sec.: D. T, Wilson, 177 Dower Road, Four Oake, Surton Coldfield, Warwickshire.

On 8th January there was a General Discussion on d.f. arrangements for 1965 with special reference to Harcourt, rules and technical organisation. A talk entitled "The Early Days" was given tochnical organisation. A talk ent
by H. Wilson, on 22nd January. RADIO SOCIETY
Hon. Sec.: N. Pride, 100 Raikes Lane, Birstall, Near Leeds.
The subject under discussion on 2lst January was, "Aerials for


Radio Astronomy". On 4th February, there was an evening for Model Control enthusiasts.
UNIVERSITY OF SHEFFIELD AMATEUR RADIO SOCIETY
Hon. Sec.: J. P. Billingham, G8AAC: 2 St. Andrew's Way, Ardsley, Barnsley, Yorkhira.

On 8th December, Messrs. G. Harris and M. Taylor of Whitley Electrical Radio Co. Led., gave a demonstration of High Quality Sound Reproduction Seven of the Club's members sat the R.A.E. at the University on 10th December
WELLINGBOROUGH RADIO CLUB
Hon. Sec.: J. Baker, 34 Essex Road, Rushden, Northamptonshire.

At the meeting held on 14th January. P. Elderkin gave a talk on Home Made Gadgets. On 21st January there was a junk sale and on the 28th G. Abrams gave a talk on Transistors. The General Meeting was held on 4th February.
WEST KENT AMATEUR RADIO SOCIETY
Hon. Sec.: H. F. Richards, 17 Reynolds Lane, Tunbridge Wells, Kent.

On 8th January there was a Gossip Group in which the AFS Contest arrangements came under discussion. At the meeting on the 22 nd G6SSE/T and friends gave a lecture and demonstration on Colour Television.

## Preparing for the R.A.E.

The loudspeaker diagram of Fig. 12 (page 740, December ' 64 issue) was considered, by some readers, over-simplified and ambiguous. Below we reproduce a more explanatory diagram.


Also in this issue. the meter coil of Fig. 14 was shown in the mid-deflection position, and therefore the pointer also should have been set mid-way on a linear scale. Fig. 17 should have shown the two coils wound in opposite directions, so as to produce one North and onc South pole uppermost, for maximum attraction.

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