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former．F．W．Bridge．Metal Rectifer．weli ventilatod Meted case．Fuses．Fuse－holders Gase．Fuses．Fuse－holdors Clips．circult．Cart． $3 / 6$ extra 6v．or $12 \mathrm{v} .1 \mathrm{amp} . . . . . . . .22 / 9$ As above with Ammeter．．
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R．S．C．MAINS TRANSFORMERS（GURUKNY

## Interleaved and Impregnated． <br> \section*{FULLY SHiROUDED（continued）－ $425-0-425 \mathrm{v} .200 \mathrm{~mA} .6 .3 \mathrm{v} .4 \mathrm{a}, \mathrm{C} . \mathrm{T} .5 \mathrm{v} .3 \mathrm{a}$

}aries $200-230-250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$ ．Screened TOP SHROUDED DROP THROUGH
 $250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v}$ ． $2 \mathrm{a}, 0-3.5 \mathrm{v} .1 \mathrm{~s}$. $250-0-250 \mathrm{v}, 100 \mathrm{~mA} .6 .3 \mathrm{v}, 3.5 \mathrm{a}$ ．С．T． $2500-0-250 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, 0-5-6.3 \mathrm{v} .3 \mathrm{a}$ $300-0-300 \mathrm{v} .130 \mathrm{~mA}, 6.3 \mathrm{v}$ ． 4 a
Mullard 510 Amplifier
$300-0-300 \mathrm{v}, 100 \mathrm{~mA} .6 .3 \mathrm{v} .4 \ddot{\mathrm{a}}, 0-5-6.3 \mathrm{v} . \ddot{3}$ $350-0-350 \mathrm{v} .100 \mathrm{~mA} .6 .3 \mathrm{v} .4 \mathrm{a}, 0-5-6.3 \mathrm{v}$ ． 3 a $350-0-350 \mathrm{v}, 150 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, 0-5-6.3 \mathrm{v}, 3 \mathrm{a}$ FULLY SHROUDED UPRI Midget type $2 申 \times 3 \times 31 n$ ．
$250-0-250 \mathrm{v}, 100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}, 0-5-6.3 \mathrm{v} .3 \mathrm{a}$ $500-0-300 \mathrm{v}, 100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}, 5 \mathrm{v} .3 \mathrm{a}$. $200-0-300 \mathrm{v}$ ． 130 mA A． 6.3 v ． $4 \mathrm{~m}^{\prime}$
1a．for Mullard Amplifer
$850-0-350 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}, 0-5-6.3 \mathrm{v} .3 \mathrm{a}$
$350-0-350 \mathrm{v} .150 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, 0-5-6.3 \mathrm{v}, 3 \mathrm{a}$
 $450-0.450 \mathrm{v} .5 \mathrm{~V} 5 \mathrm{~mA} . \ddot{\mathrm{ma}} .4 \ddot{\mathrm{a}}, \mathrm{C}, \mathrm{T} .5 \mathrm{v} . \ddot{3}$ OUTPUT TRANSFORMERS Midget
etc．
Smali Péntode， 5,0000 to 3 a
Small Pentode，7／8，000 a to 30
Standard Pentode $5,000 \Omega$ to 3 a
10,000 a to 30
Push－Pull 8 watts，ËL84，or 6V6＂to 3＂̈ or matched to $15 \Omega$
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Following types for 3 and 15 a speakers Push－Pull 10－12 watts 6V6 or ELS8 Push－Pull 15－18 watts，6L6，KT66 Push－Pull Mullard 510 Ultra Linear． Push－Pull 20 watts，sectionally wound

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| $250-0-250 \mathrm{v}$. | 60 mA .6 .3 th |  | Both above size $2 f$ x 24 x $2 t t^{2}$ ．

FILAMENT TRANSFORMER All with $200-250 \mathrm{v}$ ． $50 \mathrm{c} / \mathrm{s}$ primariea 8.8 ．5a，5／8： $6.3 \mathrm{~V} 29.7 / 6 ; 12 \mathrm{v}, 1 \mathrm{a}, 7 / 11=8.38$ $3 \mathrm{a}, 8 / 11 ; 6.3 \mathrm{v} .6 \mathrm{a}, 17 / 6 ; 12 \mathrm{v}$ ． 1.5 a ，7ndion 17／人 SHOOTHING CHOKES $\begin{aligned} & 150 \mathrm{~mA}, 7-10 \mathrm{H}, 250 \mathrm{ohms} \\ & 100 \mathrm{~mA}, 10 \mathrm{H}, 200 \text { ohms }\end{aligned} \quad . \quad 11 / 9$ $100 \mathrm{~mA}, 10 \mathrm{H}, 200$ ohms ．． $60 \mathrm{~mA}, 10 \mathrm{H}, 400$ ohms
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 $0-9-15 \mathrm{v}$ ．Ba，28／9．
AUTO（Step up／Step cown）Trang watts，38／8； 150 watts，2\％／日． 120：1 high grade，clamped． $8 / 9$

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$6 / 12 \mathrm{v}$ 4a．．． $12 / 3250 \mathrm{~V}$ ． 50 mA
612 v ．Ga．$\cdot-15 / 3$ 250 v ． 60 mA $6 / 12$ v．10a． $\begin{array}{lll}26 / 9 & 250 & \text { V．} \\ 2519 & 201 \mathrm{~mA} \\ \text { v．} 250 \mathrm{~mA}\end{array}$
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 Bu：lt－in＇${ }^{2}$＇multiplier aevial trimmer plec trical bandspread noist 1 im ter．controls are：Function switch． aulio sam，seloctivits． rrequency（B．F．O．）． band selector，A．V．F．i N．V．C．Sunch．A．N．switeh，muin tuming bandepread tuning．butput for H／Phones or standend speaker．provides 1 ．Whatts put－
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| 105 | 6／6 7B7 | 81. | Dr＊91 | 2／6 | EP4： $4 / 6$ | 80 | 6／9 | 178 | $3 / 8$ |
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| 185 | 3／91ix | 19／6． |  | 12／6 | EFra 4／3 | 1＇CLES | 6／0 | ［isul | $15 / 9$ |
| ＋ | $2 / \mathrm{6}$ ） f | 5／－1 | bKi3 | 81－ | トド91 $2 / 9$ | PCLM3 | $9 /-$ | 114020 | 5／9 |
| SA， | 6／8 1：AT6 | 4／3 |  | 4／9 | ヒ1「42 2／8 | Pl： 1.84 | 7／6 | 1 A Bise | 5／9 |
| 1 | 4／10 12．${ }^{\text {a }} 7$ | $3 / 8$ | JR92 | 6／9 | よド95 5\％ | Pt＇1．85 | 8／6 | ＇AF゙42 | 81 |
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| 6 $\mathrm{BH}_{6}$ | 5／0，301，${ }^{\text {a }}$ | 8／8 | Fi B ${ }^{\text {c }}$＋1 | 7／3． | E\％$\% 1 \quad 2 / 6$ | PLs： | 5／6． | V1083 | 8／3 |
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| $8 \mathrm{~K} ⿳ 亠 丷 厂 犬$ | 1／6｜35L6id＇T | 6／3 | HCa ${ }^{\text {da }}$ | 4／9 | K＇se $5 /-$ | P：33 | $9 /-$ | U1，44 | 151－ |
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| 114 | 2／3 | ${ }^{\text {8FP1 }}$ | 9／6 | 10 Cl 818 | 30P19 12／8 | AZ1 $5 / 9$ | RBFP9 6／3 | 8M4 1719 | MSP4 12／． | 8Pbl ril | U4020 6／6 | GEX36 10\％ |
| 1．LA4 | $17 / 8$ | AP6G | $3 / 9$ | $100212 / 8$ | $30 \mathrm{PL} 18 \mathrm{~B} / 6$ | AZ31 6／6 | FBL21 $10 / 6$ | EM34 11／6 | MU19／144／6 | sU36 27／2 | VMP4G11／9 | QEX46 6／6 |
| luan 1 | 16／10 | 9F6GT | $7 / 8$ | 1001 \％／－ | $30 \mathrm{PL}_{1} 13$ 9／6 | AZ41 6／6 | ECst 4／4 | EMS3 12／－ | M $\times 40819$ | T41 9／－ | VM84B 12／－ | CEX64 11／6 |
| ILDS | 4／－ | BF7G | $5 /$. | $100211 / 8$ | 30 PL14 12／6 | B38 $\quad 1 / 9$ | i 5 5 $519 / 6$ | FM71 13／6 | N 37 23／3 | TDD2 12／6 | VP2 $\quad 3 / 6$ | GEX $3615 / 5$ |
| lLNJ | 4／6 | f F\％ | $51-$ | 10F1 101－ | $3312 / 6$ | B319 5／6 | $\therefore 654$ 6／－ | EM80 6／3 | N74 28／－ | 2lob4 7／6 | VP2B 016 | MATl00 7／8 |
| 1 W50r | 8／6 | i $\mathrm{F}^{1}$ | 17／9 | $10 ヶ 980$ | $35 / 51$ 12／6 | $\begin{array}{ll}\mathrm{BIA3} & 10 / 6\end{array}$ | EC70 1／8 | EM81 7／－ | $\cdots$ | TH4B 15／－ | VP4 $14 / \mathrm{C}$ | MAT1018／6 |
| 1 Pl | 5／9 | 13F12 | 21 | 10F゙14 9／9 | 31； $12 / 6$ | C1 $12 / 6$ | ECan $\quad$ 2／3 | Fand $6 / 0$ | ㅊ339 15／－ | TH21C 10／6 | VPLA $14 / 6$ | MAT1207／8 |
| 1 P 19 | $4 / 8$ | 6F13 | $3 / 8$ | 10 LDB 6／3 | 35 A5 14／8 | COH35 12／6 | Ef91 8／－ | EM85 8／0 | 1＇41 8／6 | TH30C 14／6 | VP4B 2015 | MAT121 8／6 |
| $1 \mathrm{P11}$ | $5 / 3$ | $6 \mathrm{Fl4}$ | 23／8 | 10LDI1 9／8 | 35LBGT 8／9 | CK506 6／8 | HC92 $6 / 8$ | EM87 7／6 | P61 8／6 | TH233 6／9 | VP130 7／－ | OAS O／－ |
| 1 RS | $4 /-$ | 6F゙15 | 6／8 | 10P13 8／5 | 35W4 4／9 | CLA 19／6 | ECC31 $2 / 8$ | EN31 10／\％ | PABC80 6／8 | TP2 $5 /-$ | VPes 2／6 | 0.1080 |
| 154 | 51. | $6 \mathrm{Fl7}$ | 12／6 | 10 Pl 4 11／6 | 8573 14／6 | CL38 11／6 | ECC32 4／－ | EN91 5／6 | PC4 $10 / 8$ | TP25 5］－ | VP41 5／－ | OA70 3／6 |
| 185 | $8 / 6$ | ${ }^{3} \mathrm{~F} 18$ | 13／5 | $110317 / 6$ | 35Z4GT 4／6 | CV6 2／6 | ECC3s 29／1 | EY61 5／6 | PC88 9／6 | TP－2620 17／6 | VP13s 9／9 | 0478 8／－ |
| 172 | $91-$ | $8 \mathrm{~F}^{\mathbf{2} 28}$ | $6 / 8$ | 11D5 17／8 | 3575GT 5／9 | CV6 $10 / 8$ | ECCO4 $21 / 7$ | EY81 7／8 | PC95 11／8 | TY88F $11 / 8$ | VR75 处／ | 0479 8／m |
| 1 T 4 | $2 / 8$ | $6 \mathrm{~F}^{2} 24$ | $9 / 6$ | $11 \mathrm{El} 15 /=$ | 39 ［ $2 / 6$ | CV85 14／8 | BCC38 $6 /-$ | EY83 9／8 | PC97 $7 / 3$ | UABC80 $5 / \mathrm{m}$ | VR105 5／6 | OA81 8／m |
| 104 | $5 / 8$ | $6 \mathrm{~F}^{3} 3$ | $8 /$ | $11 \mathrm{E} 317 /$ | 408UA $6 / 6$ | CV271 12／6 | HCC40 7／－ | EY84 9／6 | POC84 5／6 | UAF42 7／－ | VR150 $1 / 9$ | 0486 8\％ |
| 105 | 5／3 | $6 \mathrm{F3} 3$ | \＄／8 | 1246 2／8 | 41 MTL 8：－ | CV428 19／－ | ［CC81 3／6 | EY86 $\quad 6 / 8$ | PCC85 $6 / 9$ | $\begin{array}{lll}\text { UB41 } & 10 / 6\end{array}$ | VTriEA F／－ | 0486 4／5 |
| 247 | $12 / 6$ | 6¢ ${ }^{\text {c }}$ | $2 / 6$ | 1243 16／6 | $418 T \mathrm{C}$ 15／－ | CY1 16／4 | ECCOR2 4／6 | EY88 819 | PCCA8 $10 / 6$ | UBCA1 6／8 | VT501 8／－ | OA90 8\％ |
| 2098 | $2 / 8$ | AFAR | 1／8 | 12ACB 8／8 | 42510 | CY 10 6／6 | ECO8S $\quad 1 / 6$ | EY91 8／－1 | PCC89 $7 / 9$ | $\begin{array}{ll}\text { UBC81 } & 6 / 8\end{array}$ | VU111 6／－ | 0491 3／E |
| 2 2180 | 7／－ | 9J5C | $81-$ | 12AD6 $0 / 6$ | 43 10／－ | CY31 $\quad 1 / 9$ | HCC84 $5 / 6$ | $\begin{array}{ll}\text { EZ35 } & 4 / 6 \\ \text { EV }\end{array}$ | PCC189 10／6 | UBFPRO $8 / 9$ | VU120 10/- | OA95 8／6 |
| 2 ap 21 | \＄／6 | 8．559T | $4 / 3$ | 12AF688／\％ | $45817 / 6$ | D1 1／3 | Ecces $5 / 9$ | $\begin{array}{ll}\text { EZ40 } & 5 / 3\end{array}$ | $\begin{array}{ll} \mathrm{PCF} 80 & 5 / 6 \\ \hline \end{array}$ | UBFAS 6／9 | VU120410／－ | OA810 9／6 |
| ${ }_{9} \mathrm{P}$ | $28 / 8$ | 6．5］ | $3 / 6$ | $13 A H 7 \quad 5 /-$ | $4578151=$ | D15 13／6 | $\mathrm{ECOC88}^{818}$ | EZ41 6／－ | $\begin{array}{ll}\text { PCF82 } & 6 / 3\end{array}$ | UBL21 10／ | サ133 \％－ | 0 O211 $18 / 6$ |
| $2 \times 2$ | －81／ | 6．J7C | $4 / 6$ | 12AA8 1018 | 50A5 $21 / 10$ | D42 10／6 | ECC189 11／6 | EZ80 3／9 | PCF84 8／6 | UC92 6／8 | W21 $5 /=$ | OCl67 80／－ |
| 3 As ． | 8／9 | 8J7GT | 719 | 12AT6 4／6 | $\begin{array}{ll}50 \mathrm{~B} 5 & 6 / 8 \\ \text { 500 } & 6 / 8\end{array}$ | D63 0／－ | ECC807 15／－ | EZ81 4／－ | PCF86 $7 / 6$ | UCo84 8／9 | W42 \％0／5 | OC19 86／ |
| 3A5 | $8 / 9$ $8 \%$ | 6J8 | $12 / 6$ $5 / 6$ | $\begin{array}{ll}12 A T 7 & 2 / 6\end{array}$ | 5005 $6 / 6$ | D77 2／8 | ECF80 6／－ | EZG90 $\quad 8 / 9$ | PCF502 10／－ | UC085 5／6 | W614 84／6 | 0 Caz 98\％． |
| 887 | $81 /$ | 6K6GT | $5 / 6$ | 12AUG $5 / 8$ | 500D6G40／8 | DACs2 $7 / 9$ | ECF83 6／8 | $\mathrm{FC} \quad 14 / 8$ | PCF806 10／6 | UCF80 $8 / 0$ | W63 10／6 | 0083 5\％ |
| 3D6 | $8 / 9$ | 6K7 | 1／8 | 12AU7 4／8 | 60LbGT 6／8 | Dar91 816 | ECF80 11／6 | FCA 819 | PCL82 $6 / 8$ | UCEP1 8／－ | W76 8／6 | 008519 |
| 3Q4 $806 G T$ | 813 | 8K7GT |  | 12AV6 $6 / 8$ | 52KU 14／6 | DAF96 5／9 | ECF804 84/ | $\begin{array}{ll}\text { FC13 } & 14 / 6\end{array}$ | PCL83 $7 / 9$ | DCE49 7／w | WT7 2／6 | 0020 31－ |
| $8 Q 6 G T$ 384 | 7／6 | 6K8G BK8GT | 818 | $\begin{array}{ll}12 \mathrm{AX7} & 4 / 6 \\ 12 \mathrm{AY} 7 & 9 / 9\end{array}$ | 63 KU 14／6 | DCC90 6／8 | ECH8 $98 / 8$ | FCISO 17／－ | PCL84 $7 / \mathrm{L}$ | DCHE81 6／6 | W81／E\％ | 0028 樶f |
| 384 | $1 / 6$ $5 / 8$ |  | 84／9 | $\begin{array}{ll}12 A Y 7 & 9 / 9 \\ 12 B A 6 & 5 / 9\end{array}$ | $\begin{array}{ll}72 & 6 / 6 \\ 77\end{array}$ | DD4 $18 / 6$ | RCER 21 9／－ | FW4／600 6／6 | PCL85 716 | DCL82 70 | W101 80／9 | 0029 |
| 374 | $5 / 8$ $3 / 8$ | 8K25 | 24／\％ | 12BA6 $5 / 9$ | 77 5／6 | DD41 $10 / 6$ | DCH38 $28 / 8$ | FW4／8008／6 | PCL86 818 | UOL83 818 | W107 $10 / 6$ | OCA5 |
| 4 DL | $3 / 8$ | ${ }^{81} 101$ | 10／6 | 12BRE $4 / 9$ | 7318 | DDT4 7／6 | ECL35 $6 / 8$ | GT10 9／8 | PCI 88 <br> $18 / 6$ | UF41 6／9 | W790 17／6 | OC36 5ij |
| ${ }_{5} \mathrm{R} 4 \mathrm{Ciz}$ | $8 / 6$ | 6L5G | 12／8 | 12BH7 8／m | $80 \quad 5 / 3$ | DET25 7／6 |  | GU50 55／－ | PEN4DD | UP42 $1 / 9$ | F14 7／9 | OC4 8／－ |
| ${ }_{5} \mathrm{~S}^{\text {T }} 4$ | $7 / 8$ | 6L8G | 6／8 | 12E1 18／9 | 83 802／6 | DF33 8／6 | ECH81 $5 / 9$ | G230 7／－ | 25／－ | UF80 6／8 | X18 6／8 | 00485 |
| ${ }_{5} 5 \mathrm{U} 4 \mathrm{G}$ | 4／6 | ${ }_{6} \mathrm{LLTGT}$ | 4／8 | 12H6GT 1／6 | $830 \quad 8 /-$ | I）Find 15／－ | ECHE3 616 | G232 7／6 | PEN40DD | UF85 $61 / 8$ | $\times 2416 / 6$ | OC43 18\％ |
| $5 V 40$ | $7 / 6$ $4 / 9$ | 6 L 18 | 10／6 | 12J56T 2／6 | 8542810 | 10772 80／－ | ECHB4 $8 / 6$ | ${ }^{12233} 51776$ | PEN45 84／－ | UF86 9／－ | X 41 15／－ | OC4 81 |
| $5 \text { Y3GT }$ | － $4 / 8$ | ${ }^{6} \mathrm{~L} 19$ | 9／9 | 12J76T 7／3 | 90AG 67／B | DF91 $2 / 3$ | NClsisu | Q234 10／＝ | PEN45 \％／－ | UF89 6／－ | X 8181 |  |
| $3 \hat{Y} 4$ | $9 / 8$ | ${ }_{6} \mathrm{~L}$ L113 | $6 / 8$ | 12k5 10／－ | 90AV 67／6 | DF96 $5 / 9$ | FCCL8y 818 | 9237 14／6 | PEN45DD | UL41 6／9 | X 88 619 | $0 \mathrm{C45}$ 8／－ |
| 573 | $7 /-$ | 6LD13 | 7／8 | 12K7GT 3／6 | 900G 42／\％ | DFY\％10／－ | ECLS3 916 | H30 5／m | 12／－ | UL44 28／3 | X64 4／6 | OC45 8 8 |
| $5 \mathrm{Z4}$ | 71－ | 6LD30 | 5／6 | $12 \mathrm{KBCT} 91$ | 50 CV 49／－ | DH30 15／8 | ECL． 86819 | HABC80 8／3 | PEN49 4／\％ | ULA6 8／6 | X 65 5／6 | $0 \mathrm{C65}$ 80／ |
| 6／30L2 | 8／3 | 8N7GT | $5 /$. | 12Q79T 3／6 | $90 \mathrm{Cl} 16 /-$ | DH63 4／－ | ECLL800 | HL2 716 | PEN38310／8 | UL84 6／\％ | X 66 7／3 | 0c68 80／ |
| 6ABC | $8 / 8$ | ${ }_{8} 8 \mathrm{P} 1$ | $9 / 8$ | 128A7 6／8 | $150 \mathrm{~B} 811 / 9$ | $\begin{array}{ll}\text { DH76 } & 8 / 6\end{array}$ | 2a／8 | HL130 4／－ | PEN 453 DD | UM4 15／2 | X76M 9\％ | 0070 |
| 6ABG | $8 / 9$ | ${ }_{6 P 25}$ | 6／9 | 12 sc 7 4／－ | 15002 4／6 | ${ }^{\text {D } \mathrm{H}^{7} 7} \quad 8 / \mathrm{C}$ | EF6 $20 / 6$ | HL23DD $51-$ | 10／＝ | UM34 16／10 | X78 50／8 | 0071 3／0 |
| 6AB7 | 4／2 | ${ }^{\text {RP38 }}$ | $91 /$ | $12 \mathrm{SG7}$ 8\％ | 161 13／－ | ${ }_{\text {DH81 }} \mathrm{DH}$ 88／8 | EIFS 20／6 | HL41 3／9 | PENA4 \％ | UM80 8／8 | $\times 70$ 871－ | $0 \mathrm{OC73} 81-$ |
| $6 \mathrm{AC7}$ | 8／－ | ${ }^{81}$ P288 | $11 / 6$ | 12847 3／\％ | 185 BT 34／11 | D H101 25／－ | ，EY゙22 6／6 | HLA1DD8／6 | PEN／DD | UR10＇6／8 | X81M 89／1 | $0 \mathrm{OC73}$ 16／－ |
| 6AG5 | $2 / 6$ | 6Q7G | 4／－ | 12857 5／－ | 215BG $8 / 6$ | DH10716／11 | EP36 8／8 | HL42DD8／6 | $402017 / 6$ | UU5 7\％ | X 101 88／6 | OC7 81－ |
| 6A（77 | 「／9 | 6Q70T | 718 | $12 \mathrm{SK} 781-$ | 22041016 | DK 32 7／9 | LF37A 6／－ | HL133DD | PLu3 9／－ | UU6 9\％－ | X 100 86／－ | OC75 8／＝ |
| 6AJS | $8 / 6$ | 6R7\％ | 5／3 | 128Q7 8／－ | 3018 | $\begin{array}{lll}\text { DK } 40 & 15 / 6\end{array}$ | EF39 8／8 | 9／6 | PL36 8\％ | UU7 7／8 | X118 8／9 | OC7\％ 818 |
| DAK5 | $4 / 9$ | 6R7UT | 11／－ | $12 \mathrm{sk7}$ 5／－ | $30.210 / 6$ | DK91 4／－ | EF40 819 | HN309 25／－ | PL38 16／\％ | UU8 11／6 | X119 6／a | 0077 12／－ |
| 6AK6 | 61－ | 6BA7 | 5／9 | $12 \mathrm{UFG} 7 /-$ | 303 15／－ | 15K92 $6 / 9$ | E1゙41 6／8 | HVR2 $8 / 3$ | PLS1 $6 / 8$ | UU9 5／8 | $X 142$ 7－ | 0c73 8／－ |
| bAk 4 | $5 / 6$ | $6 \mathrm{SC7}$ | $4 / 9$ | $13 \mathrm{DL} 5 /$ | $30415 /=$ | $1{ }^{1} \mathrm{~K} 96 \quad 6 / 3$ | EF42 819 | HVR2A 8／9 | P1，82 5／3 | UU12 $4 / 6$ | Y63 5／＝ | $0 \mathrm{CB1}$ 4／－ |
| 6A15 | $9 / 8$ | 6SG7 | 4／9 | $13 \mathrm{D} 3 \quad 5 / 6$ | $30.181-$ | 0133 7\％ | EF50 $2 / 8$ | 1 W 3 5／6 | PL83 613 | UY1N $10 / 8$ | Y65 5／－ | 0C81D \％／m |
| 6AM5 | $2 / 6$ | 6817 | 3／6 | 14 BA 20／9 | 306 18／－ | DLa35 5／－ | EF54 8／： | ［W4／350 5／6 | PL84 5／6 | UY21 $7 / 8$ | Z63 | OC81M 8／－ |
| GAMB | $3 /-$ | 68J77 | $4 / 8$ | $14 \mathrm{H7} 9816$ | $866412 / 6$ | $\begin{array}{ll}\text { D1．63 } & 6 / 8\end{array}$ | EF＇73 6／－ | TW4／500 8／－ | PL500 $15 / 9$ | UY41 $4 / 8$ | z66 7／8 | 0082 10／－ |
| 6 645 | $5 / 9$ | 6sk7 | $4 / 6$ | 10．${ }^{1}$ | 956 2j－ | D1．68 15／－ | EF＇s0 8／9 |  | $\begin{array}{ll}\text { PM84 } & \text { 9／3 }\end{array}$ | UY85 | 277 8／－ | 0083 6／－ |
| 6AR6 | 201／ | 6 LL 7 | 5／3 | 181818 | $12034 \quad 7 / 5$ | $\mathrm{DL72}^{15} \mathrm{j}-$ | EF88 9／9 | KF35 12／8 | PT15 10／． | U10 $9 /$ | 2720 8／－ | $0 \mathrm{C8} 4$ 81－ |
| 6ATG | $8 / 9$ | $68 \mathrm{N7}$ | 4／－ | $1910 / 6$ | 1624 1：76 | DL75 30／－ | EF86 4／6 | KL35 $11 / 6$ | PX4 9／－ | U12／14 7／6 | Z749 6／8 | OC199 18／m |
| 6AUS | 5／8 | 68Q7 | 5／－ | 19AQ5 7／3 | 2101 12／6 | WL92 $4 / 6$ | EFF86 E／－ | K LL3 $3281 / 7$ | PX25 8／6 | U16 15\％ | 二750 88／－ | OC140 10／－ |
| GAVG | $5 / 6$ | 6sL7 | $12 / 6$ | 19B46020／5 | 4033 15／m | DLO4 $\quad 1 / 3$ | EF89 4／m | K T2 5／\％ | PY31 6／－ | U17 ¢／－ | Tramafotore | 00170816 |
| $6 \mathrm{B5G}$ | 12／6 | 6387 | 2／－ | 19 H 16 | 4687 71／－ | DL96 5／9 | EFG1 3／－ | KT8 15／－ | PY32 $\quad 8 / 6$ | $\begin{array}{ll}\text { U18／20 } & 6 / 6\end{array}$ | and diodes | 0 Cl 71 \％ |
| $6 \mathrm{B8G}$ | 216 | GU4GT | $8 / 6$ | 201） $10 /-$ | $8763 \quad 7 / 6$ | DLB10 10／6 | Eh92 2／6 | KT32 4／9 | PY33 819 | 119 48／6 | AA129 1／6 | 0 C 2000167 |
| ${ }^{6} \mathrm{BAB}$ | $4 / 6$ | 15U5G | 51－ | 20122 21／－ | 6067 10／－ | DM70 5／－ | E1997 101－ | KT33C 4／－ | PY80 5／－ | 1228 | $\triangle C 107$ 14／6 | OC2201 89／－ |
| CBE ${ }^{\text {d }}$ | $4 / 9$ | 6U74 | 71－ | －1）${ }^{\circ} \mathrm{l}$ | $71931 / 6$ | DM71 9／8 | HF＇ys 1u／－ | КT36 29／1 | PY81 $4 / 8$ | $\begin{array}{ll}\mathrm{U} 24 & 12 / 6\end{array}$ | $\triangle \mathrm{AC127}$ 9／6 | $00203 \text { 1/ }$ |
| 6 BCBG | 13／6 | 6V6G | 319 | 20L1－12／6 | $7475 \quad 2 / 9$ | 1）W4／3508／6 | EF183 \％－ | Kリ41 7／6 | PY82 $\quad 1 / 8$ | U45 8／6 | AD140 25／－ | $\text { OCP71 } 17 / 6$ |
| 68HG | 5／3 | 6＊64T | 5／6 | 201P1－12／6 | 9002 416 | LW4／5008／6 | EF184 \％ | KT44 J／－ | PY83 5／9 | $1{ }^{190} 37 / 6$ | AF102 27／6 | ORP12 18／6 |
| 6 BJJ ¢ | $5 / 8$ | $11 \times 4$ | $3 / 9$ | $30 \mathrm{P} 312 / \mathrm{c}$ | 3006 2／6 | DY86 1／8 | E1190 \％／－ | KT61 6／8 | PY 48 \％$/ 8$ | U31 819 | AFll4 11／－ | $8 \times 641$ 10／－ |
| 6BQ5 | $4 / 6$ | $6 \times 5$ | $4 / 6$ | 20P4 13／6 | Al×34 21－ | DY87 81－ | EK2 25／11 | KT6 $31 / 8$ | PY800 6\％＊ | $\begin{array}{ll}\text { U33 } & 13 / 6\end{array}$ | AF115 10／6 | T82 18／8 |
| 6BQ7A | －7／6 | 6 Y7G | $12 / 6$ | $30 \mathrm{P} \quad 12 / 3$ | ACO42 28／3 | E80F 24／－ | EK32 $\begin{array}{lr}\text { t／9 }\end{array}$ | KT66 12／3 | PY801 $6 / 3$ | $\begin{array}{ll}\text { U3）} & 18 / 6\end{array}$ | AF116 10／－ | Ts3 16/ |
| 6BR7 | $8 / 3$ | 67\％ 4 | 5／－ | $25 \mathrm{~A} 6 \mathrm{G} \quad 7 / 6$ | ACO44 9／－ | E83F 24／－ | ELi $19 / 6$ | KT74 12／6 | QP＋1 5 | U37 29\％ | ${ }^{\text {APP17 }}$ 5／8 | V10/15419/= |
| 6BRS | 8／－ | 6859 | 15／－ | 25 L 6618 | AC2HL 10／6 | Es80C 10／－ | EL32 3／6 | KT88 88／－ | QP22B 12／6 | U45 15／6 | AF118 90／＝ | XA103 15／－ |

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[^2]

L 6 VALVE 15 WATT POSH-PULL AMPLIFER, $15 \times 7$ I Lin A.C. Mains $200 \cdot \div 50$ volt.s. 4 inputs mith controls for ame and bape anil treble tift controls. Tapped for 3 and 15 ohm speakers. Enir P. \& ll. $12 / 6$.
2. CYLDON A.M. F,M, PERMEABILITY TUNER FOR ALL TRANSISTOE OPERATION. SIze 2i 2 in approx. By famous manufacturer. A, A,
 Kc/a. F.M. corerage 108 Mc r-88 Mc/a Circuit dagrame 2/6. F R.M with Tumer. 18t, end. 3rd. A.M. I.F.g. hat, 2nd. 3rd and A.F. 115 All the above are the R.F゙. end of au A.M./F.M. recciver car radio etc The above sar items, e2.10.0.
3. AMPLIFIER KIT
4. TRANSISTOR INVERTOR. 50 v. D.C. Input. Outpat 340 r. A.C. 40

 fanturer, 19/6. pius b/- 民. \& [".
5. FLUORESCENT LIGHT FITTING. Twin 40 watt $200 / 200 \mathrm{v}$. Iess tubes 59/6. P. \& P. fi/.
6. SIGNAL GENERATORS: Cash 27.5 .0 . T. \& P. 6/6. Coverage $10 n \mathrm{Kc} / \mathrm{f}$ Lo lof Mc/s on fundamentala and $100 \mathrm{Mc} / \mathrm{s}$ to $200 \mathrm{Mc} / \mathrm{s}$ on harmonice Came $10 \times 5 \frac{k}{2} \times \bar{n} \frac{1}{2} u$. Three mimature valver and Metal Fectifier A.C. maine $2\left(10 r^{2} 2011 \mathrm{x}\right.$, lnternal modnation of 400 c.p.s. to a depth of 3t per cent. Moftulaled or unmolulated R.F. output contibuously Fariable 110 moltwolls. C.W. and mod. vwiteh, variable A.F. output. Alagicere as output indicator. Accuracy - 2 per celit.
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| CV:7 | 8)- | ECC84 | $5 / 6$ $8 / 6$ | EVY41 | $3 /-$ $5 / \mathrm{l}$ | $\begin{array}{ll}\text { PEN25 } & 4 / 8 \\ \text { PEN46 } & 3 /-\end{array}$ | $\begin{array}{ll}\text { UABC80 } & 4 / 6 \\ \text { UBC4l } & 8 /-\end{array}$ | IT4 $2 A 3$ | 2/- | 6B7 7 6BAA | 8/- | f8.17GT f\&. 76 | $5 / 6$ $8 / 8$ | 19 Ml | 13/\% | R17 AM 808 | 8/6 | Photo | Tnhes |
| CT102 CYIn | 1/- | ECCs | $6 / 6$ $4 /-$ | E741 | 6/6 | PEN46 3/- PEN200A3/- | $\begin{array}{ll}\text { UBPCR0 } & 5 / 6 \\ \text { URPa }\end{array}$ | 243 $2 A 5$ | 6/- | 6BAB | $4 / 6$ | f*K7 | 6/6 | 2186 | 18/- | 811 | $17 / 6$ | G816 | 12/6 |
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3－VALVE AUDIO AMPLIFIER MODEL HA34


Deslgned for $\mathrm{H} \mid-\mathrm{F}$ reproduction Mains operation．Ready built on plated beary gauge metal chasgis，mize 7 ll в． $w x 4 i n . d x t y i n . h$ ． Incorporates ECC83． ELS4，EZ80 valves， heary duty double－ mound mains tranformer and output tranaformoer matched for 3 ohm spesker．separate BasB， Treble and volume controle．Negative feedback line．Output $4 \ddagger$ watts．Front pasuel can be dehached and leads extended for remote mounting of controle．
The HA34 has been quecially designed for ue and our quantily order enablea us to noter them omplett＂with knohs，walver．\＆4．5．0 P．\＆P． $\mathrm{I}^{\mathrm{P}}$ tic．wired and tested for ondy
collaro studio deck a motors， 3 speeds． push tutiton control．Up to 7 iin spools．siv．10．0． B．S．R．MONARDECK．Single apeed， 8 \％in．per ec．，simple control uses 5 sin．apools．80．15．0 plu s／8 carr，and ins．TTajes nxtra on both）．

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Incorporating a ECL，siz and I EZ80 heavy duty double－wound mains transformer．Ontpint 4 watt Absolutely complote．


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A Aret－clasa 2 wavebands transistor superbet －Printed clrcult panel（slze $8 \ddagger x 2\{i n$.$) ． 3$ pre allgned I．F．transformers．－High－grain Ferrite rod meral．All Flrat－grade translistors．o Cor aerial wiading．－puhh－pull output．All parts supplied With simple instructions．All parta eold eeparatoly Set of parts if putchased at ore time．
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P．\＆P． $1 / 6$ per epeaker．

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ALSO AVALABLE．Mounted on board with output trangormer and bin．ppeaker，ready to tit into cablnet below．PR1CE 80／8．P．\＆P．4／8． QUALITY PORTABLE R／PLAYER CABINET Uncut motor board．WIII take alove amplifer and B．s．R．or GARRARD Autochanger or single Record Playyer Unit．Rlze $18 \times 14 \times 8$ in

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Cumfomers are invited to see and hear this amplifier at our shop premises in Tedinhert＇s Arcaule．Send S．A．E．for leaftet．

A high ghanty bo watit ampliter developed for hae in large halls and cintse etic．Irieal for hasa lear or shythm gnitars，schoole，dance halls，theal res and puble adilrese suitable for any tppe of mike or pickup．
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10 watt 10 watt 10 ohrus－ 10,000 ohma
12.5 K to 25 K 10 F.
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|  | $1 / 6$ |  |  | HEATER TRANS．， 8.14 v．， $1 \frac{1}{2}$ a． Ditto，tapped 1．4，2，3，4，5，6．3 v．．．8／6 G｜t to．sec．6．3 \％．4 amp． $3,4,5,6,8,9,10,12,15,18,24,30$ v． $22 / 6$ $3,4,5.6 .8,9,10,12,15,18,24,30$ v． $22 / 6$

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 MULLARD＂510＂Mains Transiormer ．． $33 / 6$ MAINS POWER PACKS．Rebly huilt with Tranaformers，Rectiliers，Condensers，providing H．T．and L．T．outputs．
200 v． 20 LAA．D．C． 6.3 v． 1 a．A．C．． $25 / 6$ 2220 v． 50 mA ．D．C． 1.3 v．32．A．C．＊ $85 / 6$ and 6.3 v． 1 a．tapped 5 v．， 4 v．， 2 a． $45 / 6$ NTERVALVE TRANSFORMERS． $3: 1$ or $5: 1,9 /$ O．P．TRANSFORMERS．Heavy Duty，b／f．Multi ratio， 76 ．Multiratir heavy dinty push－pull，in w 15／6．Battery，4／6．Sub，min．DL96．3V4，etc．，5／8 10 w ．O．P．matehing tratus． $3,7,15 \Omega$ ． $12 / 6$ ． L．F．CHOKES． $15 / 10 \mathrm{H}, 60 / 65 \mathrm{~mA}, 5 /=101 \mathrm{I}, 8 \mathrm{a} \mathrm{mA}$ $10 / 8 ; 10 \mathrm{II}, 150 \mathrm{~mA}$ ． $14 /$－．

C．R．T．BOOSTHER T＇IR ANSHOKRMEIRS for heater cathode short circuit or tubes with failing emission．Full instructions supplied，mains input．

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FULL WAVE BRIDOE SELENIUM RECTIFIERS： 2,6 or 12 v．． 14 amp．， $8 / 9 ;{ }^{2}$ a．． $11 / 3 ; 4$ a．， $17 / 6$,
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three wavebands
FIVE VALVES 8．W． 16 m － 50 m ．LATEST MULLAIED，etc． M．W．21014－050 mL ECH81，EF89，EBC\＆1． L．W． $800 \mathrm{~m}-2,000 \mathrm{~m}$ ． EL84．EZ80 1－2－nouth Gnarantee
A．C． $200 / 250$ v．Short－Medium Long／Grarn． Fertite Acrial A．C．V．？ohin outpat 5 watta． Tape Sockets．Glass diu，horizontal woriling size 13 x in．Aligmed alld caribrated，isulated Chasgis suce $13 \mathrm{fin} \times 7 \mathrm{in}$ ．high $\mathbf{x} 5 \mathrm{jin}$ ．deep． 89．15．6 Carr．\＆Ina．4／6．

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## Contents



## Pirate Saboteurs

PRE-WAR amateurs were obliged to call "Test" on each transmission; today they call "CQ" like amateurs in other countries. This neatly illustrates a changing of attitude. Before the war, the amateur was encouraged as an experimenter and a potential radio operator in times of National emergency; today he is operating on sufferance. He is grudgingly tolerated, but is liable to be pushed around, his scope restricted.

Our national radio society, the RSGB, has fought long and tough battles to resist encroachments into amateur territory. lt has struggled to retain frequencies, to get more. With other national societies it has done what it can to resist strong pressures for chunks of amateur bands from broadcasting, commercial and military services. The RSGB has done yeoman service in keeping so much for the amateur, but even so we have lost valuable (and irreplaceable) air space since the war.

It is manifestly obvious that in the incessant fight to retain the privileges of the radio amateur (for they are privileges and not rights, as many fail to grasp) it is incumbent on each individual amateur operator to conduct himself on the air in a manner, if not exemplary, at least not provocative.

It hardly needs stating that the continual efforts of national societies and responsible operators can be placed in jeopardy by the irresponsible behaviour of a few. Pirates notably sabotage and mar not only the good name of amateur radio but proffer, on a plate, strong arguments to those who wish to reduce even further the still reasonable freedom of licensed amateurs.

Dealers can help clean up the current situation by refusing to sell transmitting equipment to all-comers. The fact that a licence is necessary (or that certain equipment is not operable on licensed frequencies) is never pointed out to customers. And it must be patently obvious to store assistants that they frequently sell such equipment to unsuspecting youngsters who thereafter run the risk of fines and confiscation, not to mention possible disruption of existing radio services.

Ideally, of course, it should be illegal for anyone to purchase transmitting equipment except on the production of a transmitting licence-as it should be for any shop to sell such equipment to non-licensed customers.

From the would-be operator's point of view the remedy is simple. The Radio Amateur Examination requires only a basic knowledge unlikely to strain the abilities of the genuine enthusiast. It covers only subjects which any active amateur must know to operate his station.

The cold fact is that anyone incapable of passing the RAE cannot really expect the privilege of putting a transnitter on the air. It has never stopped the real enthusiast.

A good deal of literature, including sample papers from previous examinations, is readily available. Our own new series on the RAE, too, we hope, will be of help to those aspiring to a "ticket".
Taking it all round, it seems that there is no real justification, or excuse, for amateur radio piracy.

Our next issue dated January will be published on December 4 th
 in the Caribbean. preparatory to the installation of internal and external communications equipment in these Islands. Precise details of the equipment and circuits to be operated has not yet become available. However, a fully automatic telephone exchange is planned for Georgetown, the principal town, which will

## NEWS AT HOME AND ABROAD

## Miniaturisation in Hearing Aids

FOR many years Mullard developments have contributed to the gradual improvement and miniaturisation of hearing aid devices, and at the recent London convention of the Society of Hearing Aid Audiologists, the company demonstrated circuits which may soon be introduced to continue the trend toward smaller aids.

With devices such as those shown at the Convention, hearing aid manufacturers are advancing from the "behind-the-ear" instruments, once considered tiny, to "in-the-ear" types. The kind of device which is making the transition possible is the integrated circuit module on show by Mullard, measuring only $2 \mathrm{~mm} \times 2.5 \mathrm{~mm} \times 1 \mathrm{~mm}$. This plastic encapsulation contains what is effectively. a three-stage d.c. coupled amplifier made from a single slice of silicon.

Other components exhibited,

hiere o Mullard integratea d.c, coupled omplifier (lower right) and an epitaxial transistor are compared to a pin.
were silicon planar expitaxial transistors measuring only 1.5 mm round by 1.8 mm long, and pinhead resistors only 1.7 mm in diameter. initially provide for 400 lines. A new wireless station is :Iso planned which will link Grand Cayman with Jamaica by an h.f. circuit.

The Georgetown telephone exchange will also serve West Bay. Boddentown, North Side and East End.

The Cayman-Jamaica link will provide the islands' external communications by carrying composite teleprinter and radio telephone circuits. The latter facility will be made capable of being linked over the JamaicaFlorida cable into the international telephone system.

The two islands Grand Cayman and Cayman Brac will be connected by another radio telephone link, which will give the latter access to the international services as well.
These plans were announced after the Islands had accepted Cable and Wireless' offer to install, maintain and operate all their internal and external commurications.

## Photo-electric Equipment will Detect Fog

MODULATED photo-electric equipment supplied by Lancashire Dynamo Electronic Products Limited (part of the M.I. Group), is to be installed at the Haulbowline Lighthouse in the Irish Republic, to detect fog and mist.

The equipment in the lighthouse,
which is situated at the entrance to Carlingford Lough, will span the 1.300 yards to the north bank of the estuary with a light beam. Once this beam is broken by poor visibility, i.e. fog, mist, snow, rain, an integral relay system automatically brings into operation a large Swedish-made fog
horn which ceases operation when visibility clears.

The equipment consists of a light projector unit and a light receiver unit, each fitted with a 6in. lens, precision optical viewing sights, and a sensitivity control on the receiver unit for adjustment of the operating level.

## BBC RESEARCH SCHOLARSHIPS

THE Engineering Division of the BBC provides a number of research scholarships at United Kingdom Universitiec, intended to provide selected honours graduates with the opportunity to work for a higher degree, the subject chosen for post-graduate study being within those fields of physics or engineering that have an application to sound or television broadcasting. Scholarships this year have been awarded to G. Brown of Durham University, R. W. Smith of Trinity College, Cambridge, and B. J. Vieri of Birmingham University.
Mr. Brown's research will be on the microwave spectroscopy of maser materials, while Mr. Smith will be concerned with photo-electronic image delay and storage tubes.

Mr. Vieri will, under his scholarship, continue and complete the research he has been conducting for the past three years on the automatic bandwidth reduction of television and facsimile channels by statistical encoding.

## New Cable Factory in Scotland

THE demand for high voltage oil filled cables has increased so rapidly. that Scottich Cables I imited are to huild a new factory at Renfrew for their manufacture.

This was announced recently by Sir William MsFadzear. Chairman of the BICC Group, whose research organisation has been at the dispocal of Scotioh Cables during the planning of a $\mathfrak{f z}$ million expansion programme, of which the new factory is part.

The factory, with a floor area of approximately 160.000 sq . ft., will be equipped with a highly specialised nlant for the manufacture and teating of single core and 3 -core oil iilled cables for voltages up to 130.000 .

## NEW RECEIVERS ARE AUTOMATICALLY TUNED

RADIO receiving system in which the receiver performs all tuning operations entirely automatically, has recently been introduced by the Marconi Company Limited.
The system has been designed to cut both capital and running costs for high-grade h.f. communications by taking advantage of new techniques and methods of construction. These include transistorication throughout and the use of printed circuit techniques and modular construction.
The result has been more reliable, more stable and smaller equipment (the overall size has been reduced to a third of that of previous designs) automatic operation as far as possible. and very rapid frequency changing. The valve and the telegraph retay have heen eliminated completelv.
A Marconi Self-Tuning (MST) h.f. communications system enables one man. at a central point. to control every receiver. Simply by setting decade dials on a frequency sythesizer unit to the required frequency, and pressing a button. he initiates the self tuning action of the equipment and within 24 seconds all stages of the receiver are accurately tuned to the new frequency.

The MST communications system includes three separate
receivers; a dual-diversity telegraph recciver, suitable for diversity reception of f.s.k. or four frequency diplex signals: a dualdiversity i.s.h./5.s.h. receiver, and a single path i.s.b./s.s.b. receiver.

The associated units making up the complete system include the frequency synthesizer, a display and control unit, and a master frequency source.

The fully transistorised synthesizer provides the high-stability firat oscillator input to any of the MST receivers and a $100 \mathrm{kc} / \mathrm{s}$ signal used for carrier reinsertion and for generating the second
oscillator signal where a.f.c. is not used. Its coverage is from 3.0000 to $30-9999 \mathrm{Mc} / \mathrm{s}$. in steps of $100 \mathrm{c} / \mathrm{s}$, permitting any one of 250,000 frequencies to be selected.

This synthesizer requires a 1Mc/s master frequency signal of a high accuracy and stability and this can be provided by the master frequency source.

In creating this new communications system, Marconi's have achieved reductions in size and cost of equipment: staff and cost of both operation and maintenance.


The control panel of a Marconi Self-Tuning receiver.



## FIG. 9 - $2 \frac{1 n_{2}^{\prime \prime} \longrightarrow}{\longrightarrow}$

 COMPONENTS LISTInductors:
Inductors:
TI Pentode-type output
TI Pentode-type output trans-

 ( $\forall 9 \mathrm{Lj} /$ OJuag) transformer (Denco IFT6A) Menco Maxi-Q Aerial coil (Denco Maxi-Q
blue coil, ranges 3, 4, 5-
 white coil, ranges 3, 4, 5-
plug-in octal type) plug-in octal type)
10 H I.f. choke $80-100 \mathrm{~mA}$ Miscellaneous: 'чग्य!мs ग 8802 Ho/uo d'a IS



 Side plate (screen) 3 in . $x$ IOin.
(Home Radio). Full vision dial





COMPONENTS LIST FOR צOLVาTIJSO LNヨWNDITV 6SN7
$1.5 \mathrm{k} \Omega$ IW R2 68k $\mathrm{IW}_{\text {I }}$ IW
500 p VI 500 pF variable capacitor


 One I.O. valveholder. Knobs, dial,
etc.

 Resistors:
 33
aca
and


## 


FIG.II

ટા•શ1」


## A NEW RECEIVER FOR THE S.W.L.



## WAVE

SUPERHET and simple Alignment Oscillator

## by H. Webster

IIANY constructors make their introduction to short wave radio either by way of the familiar detector and l.f. receiver or alternatively via the tr.f. receiver in which a stage of radio frequency amplitication is interposed between the aerial and the detector stage.

These combinations have long been a favourite with the amateur, and although receivers of this type can be quite sensitive, particularly on the lower frequencies, they suffer from several serious defects. The most important of these are lack of selectivity, blocking by strong signals and the occurrence of dead spots when the aerial is directly coupled to the detector stage. A further, though possibly minor defect, is the element of skill required for the reception of weak signals.

Although the superhet receiver offers greater gain and selectivity, many beginners are deterred by the apparent complexity and the alignment of such a receiver.

It is true that a superhet receiver can be quite complex when one considers multi-tuned stages, automatic volume control systems, noise limiters and the like, in actual fact a good basic superhet
receiver can give an extremely good performance on the shoit liave ranges. Even without the foregaing items the performance is vastly superior to that of the t.r.f. type of receiver.

The receiver described in this article is intended to bridge the gap between the usual t.r.f. receiver and the more ambitious type of communications receiver. Although the receiver is basically quite simple and devoid of frills it gives an extremely good performance on all wave ranges. Careful ittention has been paid to screening and to the use of good quality. Low loss components in the receiver. Plug-in coils are used. the slight inconvenience entailed in band changing being outweighed by the gain in efficiency and ease of wiring.

Utilising Denco Maxi-Q coils, ranges 3, 4 and 5 , the receiver covers $1.67-31.5 \mathrm{Mc} / \mathrm{s}$, but the range can be extended to cover the medium and lung wave band by the use of the appropriate plugin coils. Slight modification may be necessary if such coverage is desired. The modifications are quite simple and entail the substitution of $\mathrm{C} 1, \mathrm{C} 2$, C 3 with $0 \cdot 1 \mu \mathrm{~F}$ capacitors. The appropriate padding capacitors Cpl and Cp2 are also required in the oscillator section. As an aid to alignment, a simple alignment oscillator is also described.

## CIRCUIT DESCRIPTION

The circuit diagram is shown in Fig. 1. The incoming radio frequency signal is fed via the combination of L1, L2, VC1, TC1 to the signal grid of V1 which is a triode hexode frequency changer. The oscillator section of V1 injects a signal whose frequency is determined by L3 and the associated capacitors. This signal is such that it is always higher than the signal frequency by $1.6 \mathrm{Mc} / \mathrm{s}$. Mixing of this higher frequency with the signal frequency produces an intermediale frequency of $1.6 \mathrm{Mc} / \mathrm{s}$ in the anode circuit of V 1 ,

The intermediate frequency transformer i.f.t. 1 after rejecting unwanted frequency components produced in the mixing process, passes the i.f. signal to the grid of $V 2$ which is a variable mu pentode. After further amplitication by $V 2$ the i.f, signal passes to the grid of $V 3$ which is a medium impedance triode.

The detector V3 is of the so called infinite impedance type in which the load resistance is in the cathode circuit. Since considerable negative current feedback occurs. distortion is reduced to a very low level. At the same time the input impedance is extremely high and little loading of the grid tuned circuit occurs. In other words the selectivity is increased. Because some radio frequency component is invariably present in the output almost complete elimination is affected by C 10 and C12. These capacitors have low reactances at radio frequencies and high reactances at audio frequencies. The resulting audio signal is fed via C11 to the volume control VR1 and then on to the grid of the first audio valve V4, which, like the detector valve is a medium impedance triode. V4 is resistance capacity coupled to the output valve $V 5$ which is a beam power tetrode. Provision has been made for headphones by the insertion of a jack socket in the grid circuit of $V 5$. When phones are used the output stage is rendered inoperative.

## DESIGN CONSIDERATIONS

The intermediate frequency of $1.6 \mathrm{Mc} / \mathrm{s}$ was chosen in preference to the more ustal value of $470 \mathrm{kc} / \mathrm{s}$ for two reasons. First. to avoid second channel interference and secondly, to avoid pulling. For newcomers to the field an explanation may not be amiss. The first effect arises because there are always two frequencies which when combined with a third frequency. in this case the oscillator frequency, produce the same intermediate frequency. Consider an example in which a receiver has an intermediate frequency of $100 \mathrm{kc} / \mathrm{s}$. If the frequency of the incoming signal is $1.000 \mathrm{kc} / \mathrm{s}$ the oscillator must be tuned to $1,100 \mathrm{kc} / \mathrm{s}$ in order that the difference or intermediate frequency of $100 \mathrm{ke} / \mathrm{s}$ may be produced. Consider further a signal of frequency $1.200 \mathrm{ke} / \mathrm{s}$. This will again beat with the $1.100 \mathrm{hc} / \mathrm{s}$ oscillator frequency to produce an i.f. of $100 \mathrm{kc} / \mathrm{s}$. Now since the i.f. transformer is tuned to $100 \mathrm{kc} / \mathrm{s}$ it will accept this i.f. irrespective of the method of origin of this i.f.. In other words the i.f. transformer cannot discriminate between a station on $1.200 \mathrm{kc} / \mathrm{s}$ and one on $1.000 \mathrm{kc} / \mathrm{s}$. The way to eliminate this so-called second channe! interference is by adequate preselection ahead of the mixer stage. When one considers frequencies of the order of $5-30 \mathrm{Mc} / \mathrm{s}$ this interference can be very troublesome, particularly when the i.f. is only a small fraction of the signal frequency. With an i.f. of $470 \mathrm{kc} / \mathrm{s}$ at least two stages ahead of the mixer are required to give reasonable second channel rejection. An i.f. of $1.6 \mathrm{Mc} / \mathrm{s}$ considerably reduces this interference and even without a tuned r.f. stage the effect only begins to show up at round about $20 \mathrm{Mc} / \mathrm{s}$. However, like all good things, this virtue must be paid for in other ways. As the i.f. is raised the selectivity and gain decrease. Although this loss can be compensated by further i.f. stages this would add unnecessary complication to the basic receiver. The selectivity and gain of the receiver described in this article were improved in two wavs. First, by the selection of an infinite impedance detector and secondly by the introduction of regeneration in the i.f. stage. Regeneration is effected by loose coupling between the anode and grid of the i.f. stage pentode. The stability of the receiver is such that excellent control of regeneration can be made by this simple expedient.
The second effect is known as pulling. This effect is due to changes in oscillator frequency caused by the signal frequency. Pulling is caused by coupling of the input and the oscillator by means other than the ideal of pure electronic coupling in the mixer. The phenomenon can be alleviated by the use of a high i.f. and by adequate screening of the mixer and oscillator stages. These foregoing effects have been reduced to a minimum in the receiver by careful attention to screening and component layout.

Although a double triode such as the 6SN7 could have been used in place of the two separate triodes used in the detector and first audio stages, it was felt that the slight decrease in cost of the 6SN7 was hardly warranted by the increased complexity of wiring. The atuthor offers no apologies for using the international octal series of valves in preference to miniature types. These valves were chosen because of their availability and cheapness.

At the same time they are robust and the comparatively large valve holders lend themselves to simplified wiring.

The power pack has been chosen for multipurpose application since it was felt that the experimenter would have other uses for this unit. The cost of separate power units for each receiver and instrument that the experimenter is likely to use can be quite considerable and is, in many cases. needless duplication. The unit described in this article has a nominal output of 250 V at 100 mA which is in excess of that required by the receiver. The large reserve of power results in "cold running" of the power unit. A further advantage is that the excess current can be usefully employed if additional units such as converters are used with the receiver.

Considerable latitude is permissible in the choice of transformer for the power unit. Provided the transformer delivers $60-70 \mathrm{~mA}$ at 250 V this will be adeopuate for the needs of the set. However, if additional units are envisaged for use with the set, it would be wise to choose a transformer with a more generous rating.

It will be noted that a specific list of parts for the receiver proper has been made. Considerable thought weat into the design and layont of the receiver and the author feels that adherence to this specified list is essential, particularly to the beginner in the field. The use of dubious surplus capacitors and resistors is to be deprecated.
A good dial drive is essential for tuning on the short wave bands. Many inferior drives suffer from backlash, their reset stability being poor. For this reason an Eddystone slow motion dial was chosen. The dial has five ranges in addition to the $0-100^{\circ}$ scale and can be calibrated by the individual constructor.
The importance of the mechanieal side of a receiver such as this cannot be stressed too highly. The chassis, screens and pancl must be rigid to avoid undesirable capacitive changes. These changes can affect the frequency stability of the receiver. Attention to this aspect of receiver construction will be well repaid by a stable, good looking job. It is the author's experience that many constructors, somewhat understandably, tend to neglect the purely mechanical side of construction.
Two under chassis screens bolted together in a composite unit are used in the receiver. Apart from screening the oscillator and aerial sections they also serve as mounting brackets for the volume control and aerial trimmer. In addition a degree of rigidity is given to the chassis.
A word concerning alignment of a superhet may not be amiss at this point. The alignneent of a superhet has probably deterred and disappointed so many constructors that either they have given up the attempt or have been unduly critizal of the superhet. Generally, such constructors have been unable to avail themselves of the services of a signal generator. Now while it is possible to align a superhet receiver by trial and error the process is extremely tedious, particularly with a new receiver where the inductances are often well away from their required values. Even after such an alignment procedure the constructor is left with the thought that the receiver could be improved upon. In other words a considerable element of
doubt exists. The time taken up in such an attempt can often be spent more profitably in the construction of a signal source. Such a source need not be complex and for these reasons the construction of a single valve oscillator is described for the benefit of constructors without such an aid.

## CONSTRUCTIONAL DETAILS-RECEIVER

The receiver is mounted on a universal 7in. x $13 \mathrm{in} . x 3 \mathrm{in}$. chassis. The relevant dimensions and drilling details are given in Figs. 3, 8, 9 and 10. Note that the top panel supplied with the chassis is slightly less than the nominal 7 in . $x 13 \mathrm{in}$. In the case of the author's receiver the actual size was $6 \frac{7}{8} \mathrm{in} . x{ }^{12 \frac{7}{8}} \mathrm{in}$. The drilling is best performed with the chassis unassembled. No mounting points for the twin gang capacitor have been indicated because it is easier to mount this unit when the panel and dial have been assembled.

The next stage is the marking out and drilling of the front panel. This panel is a nominal 9in. $x$ 14 in . chassis top plate. The actual dimensions are $8 \frac{7}{7} \mathrm{in} . x{ }^{13} \frac{1}{\mathrm{~B}} \mathrm{in}$. On completion of the panel the dial and associated epicyclic drive are temporarily bolted to the panel. The chassis is then assembled and the panel and drive offered up to the chassis. The three holes in the panel should coincide with the three holes in the chassis front plate. Slight reaming of the holes may be necessary if the drilling has not been too accurate. Note that a slight overlap of the front panel occurs between the base and sides of the chassis. The height of the dial centre spindle above the chassis top should now be carefully measured. Two brackets to support the gang capacitor are then constructed as shown in Fig. 3. The mounting holes are slightly larger than the nominal 4BA clearance to allow some measure of flexibility in the final alignment of the gang capacitor shaft and the dial spindle. The two brackets are then bolted to the gang capacitor and a flexible coupler inserted on the shaft

The length of the capacitor shaft should be $\frac{1}{2}$ in. If the shaft is longer than $\frac{1}{2}$ in., the excess should be removed. Great care is essential during this operation. It is recommended that the end of the shaft be held in a vice and gang capacitor covered with a cloth.

The gang capacitor with attached brackets is then offered up to the dial spindle making sure that the shaft is in exact alignment with the dial spindle. The chassis is then marked by inserting a sharppointed tool through the bracket base holes. The gang capacitor unit is then removed and the chassis drilled at the points indicated. The front panel may now be removed from the chassis.

## UNDERCHASSIS SCREENING

The main chassis screen is constructed from a 3 in . $\times 10 \mathrm{in}$. chassis side plate. Cut away $2 \frac{1}{2} \mathrm{in}$. and cut and bend the remaining piece to the shape shown in Fig. 9. The subsidiary screen is constructed from a $2 \frac{7}{8} \mathrm{in}$. $x$ Sin. piece of aluminium. Although it is possible by prior measurement to mark out the holes for the aerial trimmer capacitor TC1 and volume control VR1 the method calls for great accuracy. A better method utilises the following dodge. The main and subsidiary screens
are bolted together making sure that the bottom flanges sit neatly on a flat surface. The unit is then bolted to the chassis. Two spindle bushes are then inserted in the holes in the chassis front plate. The holding nuts are tightened and a 6 in . length of $\frac{1}{4} \mathrm{in}$. diameter rod inserted through one of the bushes. A smear of paint is placed on the end of the rod which is then eased gently through the bush until the painted end makes contact with the screen. The process is repeated for the other hole. The screen unit is removed from the chassis and drilled in the positions indicated by the paint spots. Although the process of construction may appear tedious, care spent at this stage of the work is well worth while.

## GENERAL ASSEMBLY AND WIRING OF RECEIVER

Wiring of the receiver is facilitated by working with the chassis dismantled. Remove the chassis top plate and bolt the screen in its original position. The valve holders are mounted noting that the holders for V1 and V2 are of the ceramic type. The remainder are standard moulded amphenol type. Before mounting the coil holders

in position the lids supplied with the coil screens are cut to the dimensions shown in Fig. 6a. The slots in the lids are best cut with a single edged razor blade. The gauge of metal is sufficiently thin to allow this procedure to be adopted. This method gives a neater hole than that obtained by punching or shearing. Two lids are required and are held in position by the valve holders. The author found that distortion of the lids was avoided if the ceramic holders were dismantled before fixing.
Solder tags are placed under the fixing bolts of each valve and coil holder. Note that a tag is placed on the fixing bolt of each coil holder above the chassis and near to the gang capacitor. It is important that the holders are mounted correctly orientated with the locating holes in the correct positions.

The intermediate frequency transformers are then mounted, ensuring that the access holes to the iron cores face to the rear of the chassis. This is important when the alignment process is carried out. The tag strips are then mounted. Four tag
strips are required, noting that two small strips are mounted, one adjacent to the oscillator coil holder, the other adjacent to V1 holder. The two small tag strips are obtained by removing the appropriate amount from 7 -way strips.

The volume control and aerial trimming capacitor TC 1 are mounted on the screening unit. Wiring of the receiver can now commence. Run the heater wiring round the perimeter of the base to minimise hum and interaction with other parts of the circuit. Note that the correct method of heater wiring is shown in Fig. 4. The remainder of the wiring is quite straightforward and no difficulties should be experienced. Wherever possible, short, stiff wiring should be employed, particularly in the signal frequency and oscillator sections. When the main wiring on the chassis plate is completed there remains the wiring of the oscillator trimmer TC2, output transformer T1, power input socket, phone jack and gang capacitor VC1/VC2.

The chassis side members are attached followed by the panel. Two spindle bushes for the volume control and aerial trimmer are screwed in position and the oscillator trimmer inserted in the remaining hole. Two wires are soldered to the tags on the gang capacitor stators and ater bolting it to the chassis, are passed through the holes in the chassis. The two wires are then soldered to their appropriate points on the coil holders.

The frame of the gang capacitor is earthed by two heavy wires, outer braiding from screened cable being suitable. The two leads are taken to the fixing tags on the coil holders as shown in Fig. 3. Ensure that the dial movement is free and rotates smoothly over the entire range of travel. As a point of interest the gang capacitor is mounted on its side to facilitate coil changing.

## GENERAL DETAILS OF COILS USED IN RECEIVER

The well known range of Denco " Maxi $Q$ " plug-in coils is used in the receiver. Note that the blue type coils are used in the aerial section while the white type coils are used in the oscillator section. Automatic selection of the appropriate padding capacitors $\mathrm{Cpl}-\mathrm{Cp} 5$ is made when the oscillator coil for a given range is plugged into the octal holder. To avoid confusion on the theoretical (Fig. 1) and main wiring diagram (Fig. 4) only one padding capacitor ( Cp ) has been indicated. This has been shown connected to pin 6 on L3/L4 coil holder. In fact, Cp5 will be wired in this position and the diagram below shows all the padding capacitors fitted. Cp 1 and Cp 2 may be ignored if long and medium wave reception is not contemplated. The underside pin connections for the aerial and oscillator coils for the various ranges are given below.


Aerial coils LI/L2 all ranges


To avoid confusion the Denco range numbers for the various ranges in the receiver have been retained. For example. Range $31.67-5 \cdot 3 \mathrm{Mc} / \mathrm{s}$. Range $450-15 \mathrm{Mc} / \mathrm{s}$. Range $510-31 \varsigma \mathrm{Mc} / \mathrm{s}$.
The remainder of the wiring is now completed as shown in Fig. 4.

Now that the wiring of the receiver is complete a check on the recciver is made. A careful examination of the wiring against Fig. 4 should be made and any obvious mistakes renseded. Using a multirange meter the resistance between the h.t. line and earth is measured. A reading of approximately $300 \mathrm{~h} \Omega$ should be obtained. Initially a somewhat lower reading will he observed due to the charging up of C9. After a short time the resistance will rise to the steady value indicated previously.

## POWER UNIT

The author's unit was built on a $7 \mathrm{in} . \mathrm{x} 4 \dot{\mathrm{in}} . \mathrm{x}$ 3in. aluminium chassis. Since it was felt that manv constructors would possess a mains transformer or suitable power unit no hard and fast rules have been laid down for the construction of this unit. Provided the unit delivers $200-250 \mathrm{~V}$ at $60-100 \mathrm{~mA}$, this is adequate for the needs of ;he set. A wiring diagram is given in Fig. 5. Power from the unit is taken from an octal socket mounted adjacent to the rectifier.

## VOLTAGE CHECK ON RECEIVER

The loudspeaker is connected and a set of coils inserted in their sackets. The power unit is plugged into the octal socket at the rear of the receiver. When the unit is switched on any obvions signs of overheating should be noted; the power switched off and the fault remedied. With the receiver working correctly the following voltage readings should be obtained. The author used a $10,000 \Omega / \mathrm{V}$ meter set to the 1.000 V range for h.t. measurements and the 10 V range for bias voltage measurements. With a less sensitive instrument lower readings will be obtained.

| Valve | Anode | Screen | Cathode | $\underset{\substack{\text { H.T. } \\ \text { line }}}{ }$ |
| :---: | :---: | :---: | :---: | :---: |
| VI | $\left.\begin{array}{c}\text { Hexode } \\ 210 \\ \text { Triode } \\ 100\end{array}\right\}$ | 100 | 3.7 |  |
| V2 | 205 | 105 | 3.5 | 220 |
| V3 | 210 | 105 | 3. | $\checkmark$ |
| V4 | 55 |  | 1.6 |  |
| V5 | 200 | 220 | 10.0 |  |

## ALIGNMENT PROCEDURE

The following notes are given for the benefit of constructors who have access to a signal generator. Insert a set of coils for the $1.67-5 \cdot 3 \mathrm{Mc} / \mathrm{s}$ range, noting that the blue coil is inserted in the aerial coil holder and the white coil in the oscillator coil holder. Connect the signal generator lead via a $0.1 \mu \mathrm{~F}$ capacitor to the top grid cap of VI. Inject a modulated $1.6 \mathrm{Mc} / \mathrm{s}$ signal and peak the cores of the i.f. transformers, starting with i.f.t.2. Gradually reduce the generator signal as the circuits come into line. This completes i.f. aligament.

Set the receiver dial to 100 and adjust the aerial and oscillator trimmers to approximately one third capacity. Inject a $1.67 \mathrm{Mc} / \mathrm{s}$ signal via the top grid cap of VI and peak the oscillator core until maximum response is obtained. Set the receiver dial to 0 and inject a $5 \cdot 3 \mathrm{Mc} / \mathrm{s}$ signal. Peak the oscillator trimmer on this signal. Repeat this procedure until no further adjustment is required.

Remove the coupling lead from V1 and inject a $1.835 \mathrm{Mc} / \mathrm{s}$ signal via a dummy aerial or 400 s resistor into the aerial socket. Set the receiver dial to 100 and slowly tune to the high frequency end of the band. The signal should be picked up at a dial reading of approximately 87. Peak the core of the aerial coil on this signal. Inject a signal of $4.5 \mathrm{Mc} / \mathrm{s}$ and tune the receiver to this signal. (Dial approximately 9.) Peak the acrial trimmer on this signal. Repeat the process until no further adjustment is required. A check on the tracking can now be carried out. Inject a signal of $2 \cdot 64 \mathrm{Mc} / \mathrm{s}$ and tune the receiver to this signal. Tracking is satisfactory if no further increase in signal strength is obtained.

Range $4 \quad(5-15 \mathrm{Mc} / \mathrm{s})$ and Range 5 ( $10.5-31.5 \mathrm{Mc} / \mathrm{s}$ ) can be aligned in a similar fashion. The alignment frequencies for these two ranges are given in the accompanying table.

Comprehensive details of these coils are given in the Denco Technical Bulletin DTB1.

Alignment points. Ranges 4 and 5

\begin{tabular}{|c|c|c|c|c|c|}
\hline \& \multicolumn{2}{|c|}{Oscillator} \& \multicolumn{3}{|c|}{Aerial} <br>
\hline Range

4

5 \& $$
\begin{gathered}
\text { Cores } \\
\mathrm{Mc} / \mathrm{s} \\
5.0 \\
10.5
\end{gathered}
$$ \& \[

$$
\begin{gathered}
\text { Trimmer } \\
\mathrm{Mc} / \mathrm{s} \\
15.0 \\
31.5
\end{gathered}
$$

\] \& Cores Mc/s $5 \cdot 5$ 11.55 \& Trimmer Mc/s $13 \cdot 5$ 16.65 \& \[

$$
\begin{gathered}
\text { Tracking check } \\
\text { Mc/s } \\
7.93 \\
28.36
\end{gathered}
$$
\] <br>

\hline
\end{tabular}

When alignment is complete regeneration can be introduced into the i.f. amplifier in the following manner. Solder a short length of wire to the anode pin of V2 pin 8). A lin. length is ample. Slowly bend the wire towards the grid pin (pin 4). This
capacitor is indicated by Cs in Fig. 1. The point at bend the wire towards the grid pin (pin 4). This
capacitor is indicated by Cs in Fig. 1. The point at which oscillation commences is easily heard as a which oscillation commences is easily heard as a
sudden increase in signal hiss. Redace the coupling slightly until stable conditions are obtained. A use-
ful increase in selectivity and sensitivity is slightly until stable conditions are obtained. A use-
ful inerease in selectivity and sensitivity is obtained by this method.

## ALIGNMENT OSCILLATOR

The oscillator used for alignment of the beginner"s short wave superhet comprises a double triode valve arranged in a simple feedback circuit. triode valve arranged in a simple feedback circuit.
Feedback from one triode section is fed back in the correct phase to the other triode section. The the correct phase to the other triode section. The
circuit diagram is shown in Fig. 14. This particular method of feedback permits the use of a two
terminal coil in the grid circuit. The necessity for method of feedback permits the use of a two
terminal coil in the grid circuit. The necessity for tapping or separate feedback coils is thus avoided. To avoid the complication of a modulating section the anodes of the double triode are fed with raw a.c. The $50 \mathrm{c} / \mathrm{s}$ modulation was found to be very effective and no difficulty has been experienced in identification of the signal. A small transformer capable of supplying $150-200 \mathrm{~V}$ a.c. for the anodes Whoduced into the i.f. amplifier in the following pping or separate feedback coils is thus avoided.
and 6.3 V for the heater is adequate. Only a small current is demanded by the instrument.

Three ranges are covered by the instrument. 700 $-2.000 \mathrm{kc} / \mathrm{s}, \quad 1.8-5.8 \mathrm{Mc} / \mathrm{s}$ and $5-15 \mathrm{Mc} / \mathrm{s}$. These three ranges are sufficient for alignment of the receiver. The range of the oscillator can be extended either way if a fuller coverage is desired.
The oscillator is constructed on a small aluminium chassis 5 in . x 3 in . $x 2 \frac{1}{2} \mathrm{in}$. The coils, switch and associated capacitors and resistors are mounted below chassis while the variable capacitor is mounted above chassis. The wiring of the oscillator is not critical. A diagram of the prototype is given in Figs. 11 and 13.

The inductances for the three ranges were wound on $\frac{1}{2}$ in. diameter formers, the relevant winding details being given in the accompanying table.

| LI | 700 to <br> $2000 \mathrm{kc} / \mathrm{s}$ | 105 turns, pile wound to occupy <br> a length of $\frac{1}{2}$ in. |
| :---: | :---: | :--- |
| L 2 | 1.8 to <br> $5.8 \mathrm{Mc} / \mathrm{s}$. | 50 turns, close wound, length <br> $\frac{7}{3 i n}$. |
| L 3 | 5.0 to <br> $15 \mathrm{Mc} / \mathrm{s}$. | 19 turns, spaced to occupy lin. |

All coils wound with 28s.w.g. enamelled wire on $\frac{1}{2}$ in. diameter formers.

## THE DIAL DRIVE

A direct drive dial calibrated from $0-100$ was used in the prototype. The accuracy of this dial was found to be more than adequate for alignment purposes.

## CALIBRATION OF OSCILLATOR

Range 1. For the calibration of this range a domestic receiver covering the medium wave band is required. Switch on the oscillator and allow a few minutes to elapse so that steady running conditions may be attained. Tune the domestic receiver to the medium wave band and select a station of known frequency near to $700 \mathrm{kc} / \mathrm{s}$. The BBC North programme on $962 \mathrm{kc} / \mathrm{s}$ is suitable. Place the generator near the receiver and slowly rotate the generator dial until zero beat is obtained. By adjusting the coupling between the oscillator and receiver the zero point can easily be obtained by observing the throbbing note which slowly falls in frequency as the null point is neared. Note the generator dial setting and the frequency of the station. Repeat this procedure with other
frequencies until the remainder of the medium wave band down to about $1,550 \mathrm{kc} / \mathrm{s}$ is covered. In this way a complete set of readings can be obtained. The generator readings are next plotted against frequency on a sheet of graph paper. A curve will be obtained from which any frequency between 700 and $1.550 \mathrm{kc} / \mathrm{s}$ can be obtained. For frequencies between 1,550 and $2.000 \mathrm{kc} / \mathrm{s}$ the line may be extrapolated. Since the plot of frequency against dial readings is a curve the extrapolation procedure is subject to error. A better method for obtaining the 1.6 and $1.67 \mathrm{Mc} / \mathrm{s}$ points, which are required for receiver alignment, is to plot wavelength againct generator dial readings. A straight line is obtained which can be safely extrapolated. The accuracies of the 1.6 and $1.67 \mathrm{Mc} / \mathrm{s}$ points are more than sufficient for receiver alignment. The relationship between frequency and wavelength is

$$
300,000
$$

$W=-\quad$ where $W$ is in metres and $f$ is in kilocycles.

An actual plot obtained by the author is shown in Fig. 7. Note that some points may be slightly off the line. This is caused by several factors of which the most important are observer error and inaccuracies in the variable capacitor. When the points are made on the graph the straight line is drawn to give the best possible fit. The dotted line is the extrapolated portion of the line. From this dotted line are read off $1.6 \mathrm{Mc} / \mathrm{s}$, the i.f. and $1.67 \mathrm{Mc} / \mathrm{s}$ required for range 3 alignment.

## AlIGNMENT OF RECEIVER I.F. SECTION

Now that a $1.6 \mathrm{Mc} / \mathrm{s}$ signal is available the i.f. section may he aligned as described in the receiver construction. Set the generator to $1.6 \mathrm{Mc} / \mathrm{s}$ and wrap a piece of wire loosely round the top cap of V1. Run this lead near the generator. Coupling may be reduced by shortening the lead. Peak the cores of i.f.t. 2 and i.f.t. 1 for maximum noise and working with the smallest possible i.f. signal. I.F. alignment is now complete and on no account must the iron cores be disturbed.

## ALIGNMENT OF $1.67 \mathrm{Mc} / \mathrm{s}-5.3 \mathrm{Mc} / \mathrm{s}$ RANGE OF RECEIVER

A set of coils to cover this frequency should have already been plugged in during i.f. alignment. Set the receiver dial to 100 and adjust the aerial and oscillator trimmers to roughly half capacity. From the graph find the generator reading corresponding to $1.67 \mathrm{Mc} / \mathrm{s}(180 \mathrm{~m})$. Inject this signal via the top cap of $V 1$ and peak the oscillator for maximum response. From the graph ascertain the generator reading corresponding to $1.325 \mathrm{Mc} / \mathrm{s}(226.4 \mathrm{~m})$. Set the generator to this reading and slowly tune the receiver to the h.f. end of the band. Harmonics should be heard at 2.65 .3 .975 and $5.3 \mathrm{Mc} / \mathrm{s}$. The oscillator trimmer is peaked on the $5 \cdot 3 \mathrm{Mc} / \mathrm{s}$ harmonic with the receiver dial at 0 . Return to the I.f. end of the band and repeat the process until optimum results are obtained.
The coupling lead is taken from the top cap of V1 and inserted in the aerial socket. The core of the aerial coil is adjusted on a $1.67 \mathrm{Mc} / \mathrm{s}$ signal
while the aerial trimmer is adjusted on the $5 \cdot 3 \mathrm{Mc} / \mathrm{s}$ harmonic of $1.325 \mathrm{Mc} / \mathrm{s}$. The exact procedure is as before. This completes the alignment of Range 3. Note the position of the pointer knob of the oscillator trimmer and mark this position on the panel.

A partial calibration of the receiver dial may now be carried out. From the graph determine the $1 \mathrm{Mc} / \mathrm{s}$ point and inject this signal via the aerial socket. Tune the receiver from the I.f. to the h.f. end of the band. Four peaks corresponding to 2, 3, 4 and $5 \mathrm{Mc} / \mathrm{s}$ should be heard. From the receiver dial read oft the points corresponding to these frequencies. A record of these readings should be retained for future use. The $1 \cdot 3-5 \cdot 8 \mathrm{Me} / \mathrm{s}$ range of the generator may now be calibrated against range 3 of the receiver.

## CALIBRATION OF THE $1.8-5.8 \mathrm{Mc} /:$ RANGE OF GENERATOR

Switch the generator to this range and set the receiver dial to the point corresponding to $2 \mathrm{Mc} / \mathrm{s}$. Adjust the generator dial until a signal is heard. Repeat for the 3,4 and $5 \mathrm{Mc} / \mathrm{s}$ points. This simple calibration is sufficient for aligament of range 4 of the receiver. Note the generator dimp reading corresponding to the above points.

## ALIGNMENT OF RECEIVER RANGE 4. $5-15 \mathrm{Mc} / \mathrm{s}$

The procedure is exactly the same as for that employed on Range 3 except that a $5 \mathrm{Mc} / \mathrm{s}$ signal is injected for adjustment at the 1.f. end of band. The $15 \mathrm{Mc} / \mathrm{s}$ harmonic of $5 \mathrm{Mc} / \mathrm{s}$ is used for alignment at the h.f. end of the band. Note that when $5 \mathrm{Mc} / \mathrm{s}$ is injected peaks will be heard at 5,10 and $15 \mathrm{Mc} / \mathrm{s}$. When alignment is satisfactory note the positions of these frequencies on the receiver dial. The $5-16 \mathrm{Mc} / \mathrm{s}$ range of the generator may now be calibrated against these three points.

## ALIGNMENT OF RECEIVER RANGE 5. $10.5-31.5 \mathrm{Mc} / \mathrm{s}$

On this range switch the generator to Range 3. At the l.f. end of band inject a $10 \mathrm{Mc} / \mathrm{s}$ signal with the receiver dial set to $96^{\circ}$. The h.f. end of the band is peaked on the $30 \mathrm{Mc} / \mathrm{s}$ harmonic of $15 \mathrm{Mc} / \mathrm{s}$ with the receiver dial set at $5^{\circ}$. Note that at the h.f. end of this band two peaks will be heard on adjusting the oscillator trimner. Select the peak requiring least trimmer capacity.

A fuller calibration of the receiver dial may now be carried out. Points for 2, 3, 4 and $5 \mathrm{Mc} / \mathrm{s}$ will have already been noted for Range 3. Inject a $1 \mathrm{Mc} / \mathrm{s}$ signal into the aerial socket and note the positions on the dial at which the harmonics of $1 \mathrm{Mc} / \mathrm{s}$ are received on Ranges 4 and 5. For example, on Range 4 calibration points at $5-15 \mathrm{Mc} / \mathrm{s}$ will be obtained separated by $1 \mathrm{Mc} / \mathrm{s}$ intervals. The points between the $1 \mathrm{Mc} / \mathrm{s}$ intervals may be obtained as follows:

A glance at Fig. 13-14 will show that a blank position has been left on the switch. A long wave coil is inserted in this position and the coil can be conveniently placed above chassis. The aerial coupling winding on the coil may be ignored. Switch the generator to this range and place a
-continued on page 758

# invertel $\mathbf{V}$ aerbal <br> by R. F. Graham 

FOR ALL-BAND RECEPTION AND TRANSMISSION<br>ON 160, 80, 40, 20, 15 AND 10 METRES

T1HIS aerial can be used for reception only, over the range $10-200$ metres ( $30-1.5 \mathrm{kc}$ ), or for both receiving and transmitting, on 160,80 , $40,20,15$ and 10 metre bands. It is particularly intended for locations where only one pole or other high support is available.

The aerial is shown in Fig. 1. and the high anchor point needs to be about 38 ft . above ground level. A pole may be secured to a chimney with TV-type lashings, or may be held with strong
pass through the insulators. An insulator is fitted each end.

If cords pass down to ground pegs, a total width of about 76 ft . is required. If a building, fence, tree. or other convenient anchor point is avallable, this reduces the total space necessary for the aerial. Cord or polythene line is used between aerial insulators and anchor points. If the aerial is employed for transmitting, its ends. should be out of reach of children.


Fig. 1: The construction of the aerial.
brackets, or with spikes securing it in an angle between chimney and house. The aerial wires act as halyards, helping to prevent sideways movement.

A piece of $2 \times 3 \mathrm{in}$. timber, free from knots, makes a good pole. A "ladder pole", available from large timber suppliers, is also inexpensive. If the supporting point is a little under 38 ft . high, the lower ends of the aerial can be spread out more, or may be 6 or 7 ft . above ground.

Each element of the aerial is 14s.w.g. hard drawn copper wire, or $7 / 26$ s.w.g. aerial wire. Each piece is $41 \frac{1}{2} \mathrm{ft}$., to allow 3in. each end to

The apex of the aerial is most easily raised by threading a long line through an insulator or strong evebolt at the pole top. before fixing the pole. The aerial can then be hoisted up, when ready.

## Feeder

The aerial is designed to operate with an openwire twin feeder, which has negligible losses at all the frequencies covered. The feeder is made from $7 / 26 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. aerial wire, with 5 in . or 6 in . spreaders.

Ceramic spreaders of this kind can be purchased, or spreaders can be cut from insulating material. If the feeder is reasonably taut, one spreader every $4 f t$. to 5 ft . will do.

If the aerial is to be used for reception and transmission on 3.5 .7 , and $14 \mathrm{Mc} / \mathrm{s}$ (80. 40 and 20 m ) bands only, then 300 ohm flat twin ribbon may be used for the feeder. The efficiency with this type of feeder is less than with an open wire feeder.

Each feeder wire is soldered to one of the 41 ft . aerial elements. The open wire feeder should not touch the roof, pole, or walls. An extra insulator or two can be attached to the feeder, with a cord to any suitable point, to keep the feeder in position.

## Coupling

There are several different ways in which the twin feeders can be coupled to the receiver or transmitter. The one chosen depends to some extent on the receiver or transmitter, and the purpose in view,

Receiver Dipole Input. Communications type receivers generally have a dipole or twin feeder input. There are then two aerial terminals for this purpose. One feeder wire is taken to each terminal. This method is simple, and can be used on all bands without adjustment. It is often employed with twin feeders, despite the fact that the best impedance match between feeder and receiver (and thus best signal strength) is only obtained on some frequencies.

Receiver Timer. A tuner allows the aerial to be tuned to resonance, and also provides an impedance match. it thus gives best possible signal strength at all frequencies.

The tuner can be made as described for a transmitter tuner (Fig. 2) except that a widespace tuning capacitor is not required. for reception. If the receiver has a $75 \Omega$ or similar aerial input, it is best to use a piece of 75!? coaxial cable between tuner and receiver. with a coupling loop exactly as described for transmitting.

Some receivers have an input for $300-600 \Omega$. If so, signal strength is improved by taking the receiver feeder to a tapping some turns out from the coil centre tap.


Fig. 2: The method of coupling a twin feeder.

With a receiver tuner. the tuner variable capacitor is adjusted for best signal strength, as shown by the tuning meter, signal strength meter. or by maximum volume. The increase in signal strength obtained from the tuner will be important, on those frequencies where a bad impedance match would otherwise exist between feeder and receiver.

Transmitter Pi-Output. Twin feeder svstems are sometimes operated directly from a transmitter pi-output circuit, one feeder wire being earthed at the transmitter. This method can be used when the feeder impedance falls within the range of impedances to which the transmiter output circuit can be adjusted.

In this case, the transmitter is loaded up into the aerial in exactly the same way as if an endfed wire were in use.

Transinuter Tuner. This is the most satisfactory way of all-band operation. and the same tuner may be used for both receiver and transmitter. A suitab.e tuner circuit is shown in Fig. 2. The variable capacitor needs to have spacing about equal to that in the anode circuit of the transmitter P.A., to avoid sparking over.

A coil for 10-80 meters can be made by winding 26 turns of 18 s.w.g. wire on a $2 \frac{1}{\frac{1}{i n} \text {. diameter }}$ or similar former, turns being spaced to occupy about 3 in . in all. The loop can be 3 turns of well insulated wire, over the centre of the 26 turn coil.

Any convenient length of $75 \Omega$ co-axial cable passes from the tuner to the transmister pi-output socket.

In use, taps $\mathrm{Y}-\mathrm{Y}$ are clipped on the coil at equal distances from the centre tap, to obtain resonance on the required band. This is most eacily done by observing signal strength on the receiver, while tuning to some transmission in the required band. Clips X-X are placed at equal distances from the centre tap, until the transmitter can be loaded to the required input.

If a dipole or Zepp tuner is to hand, this may be used instead, with series tuning for low feeder impedances, and parallel tuning for high feeder impedances. The tuner is best housed in a case near the receiver or transmitter, so that it can be adjusted as required.

During tests. the aerial was found to give good results, for both receiving and transmitting. This was also so on Top Band ( 160 m ) where the performance exceeded that expected.


\title{

PREPARING DoA. <br> <br> BRIAN ROBINSON. <br> <br> BRIAN ROBINSON.

## 

## 

 Fig. 12: In a loudspeaker, a paper cone is connected to a coil suspended between the poles of a magnet.

### 2.3 The Moving Coil Meter

This also uses the same principle as the loudspeaker. A constant current is. however, passed through the coil, which is connected to a pointer, and an indication is given which is proportional to the strength of the current. Moving coil meters can only be used to measure d.c. current but voltages can be measured by connecting a resistance in series with the meter. The formula used to convert a milliammeter into a voltmeter is:

$$
\mathrm{R}=\frac{\mathrm{E} \times 1000}{\mathrm{I}}-\mathrm{Rm} .
$$

Where $R$ is the desired series resistance $E$ is the


Fig. 13: The basic arrangement of the component parts of a moving coil meter.
decired full-scale reading of the voltmeter. $I$ is the current drawn by the meter (in milliamps) and $\mathbb{R}$ is the resistance of the meter. A circuit and typical values are given in Fig. 14.


Fig. 14: A circuit for making voltage measurements.

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To convert a milliammeter into an ammeter or a milliammeter having a higher full-scale deffection a shunt resistance nust be used. The formula used to find the value of the shunt is:

$$
R=\frac{R m}{n-1}
$$

where $R$ is the shunt resistance,
$\mathrm{Rm}_{\mathrm{m}}$ is the meter resistance and n is the factor by which the original f.s.d. has been multiplied. A typical example is shown in Fig. 15.


Fig. 15: Inclusion of the shunt resistor $(11.1 \Omega)$ gives the milliammeter a higher full-scole deflection.

### 2.4 The Electromagnet

When a coil of wire is wound round a piece of soft iron and a current is passed through the coil the soft iron will become magnetised. When the current is switched off the soft iron immediately loses its magnetism. This type of magnet is called an electromagnes. Electromagnets are generally used in electric bells and buzzers and relays, all three of which are really switching devices. See if you can work out how the relay switches on the current in a separate circuit in Fig. 16 and how the electric bell in Fig. 17 rings continuously.


Fig. 16: Here an electromagnet is used to operate a relay for switching on the lamp.

### 2.5 Self-Inductance

If a wire is wound into a coil and a current is passed through the coil the coil will oppose any change in the value of the current passing through it. This property of opposing a change in current is called inductance and is due to the fact that a second current is itiduced in the coil which opposes the change in current. The amount of inductance possessed by a coil depends on the number of turns. the area of cross-section of the coil, the length of the winding and the material


Fig. 17: The circuit of an electric bell.
on which the coil is wound. If a current passes through a coil the current does not at once rise to its maximum value because of the inductance of the coil. This is shown in Fig. 18.


Fig. 18: The rise of current with time in the coll shown on the left, is illustrated graphically on the right.

Inductances are measured in Henrys. The Henry is a large unit and in radio frequency coils the inductance is generally measured in microhenrys $\left(\frac{1}{1,000,000}\right)$ of a Henry. The inductance which acts when a current passes through a single coil is called self-inductance.

### 2.6 Mutual Inductance

When current flows through a coil a magnetic field is set up round the coil as shown in Fig. 19.


Fig. 19: The magnetic field set up around a cail of wire.

If a second coil is now brought near to the coil shown in Fig. 19 so that the lines of magnetic force " cut through" it a current will be produced in the second coil. This current is produced as a result of a mutual inductance between the two
coils. This is shown in Fig. 20, a milliammeter being used to demonstrate the induced current in the coil. The coil connected to the cell is called the primary coil and that in which the current flows is called the secondary coil.

Two coils such as those in Fig. 20 are said to be coupled and the coupling effect is greatest when the two coils are on the same axis and close together.


Fig. 20: The effect of placing one coil in close proximity to another.

### 2.7 Inductances used in Receiving and Transmitting Circuits

Adding an iron core (generally powdered iron) to a coil increases the inductance considerably and therefore for receiving purposes coils can be made very small. Also the inductance of a coil can be reduced by adding a core of a metal such as brass. As will be seen later when a.c. theory is dealt with the inductance of a coil varies according to the frequency of the current which passes through it. Generally, in transmitting circuits where there is considerable radio frequency power, the inductances used in the circuit will be self-supporting (i.e. not wound on a "former"), will be made of stout wire and will have an air core.

### 2.8 Capacitance

If two metal plates are separated by a small distance and connected to a battery and switch, as shown in Fig. 21, the instant the switch is closed


Fig. 21: How electrical capacitance is obtained.
electrons will travel from the upper plate towards the positive terminal of the battery and electrons will leave the negative terminal of the battery and travel to the lower plate. The plates are now said to be charget. The switch can now be opened but the plates will retain their new charge. The charges can be neutratised by short-circuiting the plates, a spark often resulting.

Two plates as shown can therefore be used to store an electrical charge and a device which can do this is called a capacitor or condenser. The capacity or storing power of a capacitor is dependent on the area of the plates, the number of plates, the distance between the plates and the material (dielectric) between the plates.

The unit of capacitance is the farad. This is too large for most radio applications and the microfarad $\frac{1}{1.000 .000}$ of a Farad and the
picofarad or micromicrofarad

$$
\frac{1}{1,000,000} \text { of a microfarad }
$$ are more commonly used.

Capacitors fall into two main types, fixed capacitors which have a fixed capacity and variable capacitors which have a variable capacity. The symbols for these two types are g =nerally represented as shown in Fig. 22. Fixed capacitors are physically usually small and may


Fig. 22: The circuit symbols of capacitors fixed and variable.
often be made of metal foil with a thin layer of dielectric, such as waxed paper, between the plates. The capacitor may also be made of two long lengths of foil separated by waxed paper and the whole being wound cylindrically so as to occupy a small space only. A special type of fixed capacitor is called an electrolytic capacitor but this will be dealt with later.

Variable capacitors have two sets of plates, one set variable and the other fixed; moving the position of the variable plates alters the capacity of the arrangement. The two sets of plates are almost always separated by air but occasionally mica may be used.

The voltage which can be applied to a capacitor depends upon the distance between the plates and the material separating the plates. If too high a voltage is applied sparking will occur between the plates and the breakdown voltage of the capacitor will have been exceeded.

## Question-

A meter has a full-scale deflection of 10 mA and an internal resistance of 502 . Calculate, using Ohm's Law, the following:
a. The value of the series resistance required to convert it into a voltmeter reading up to 250 V .
b. The value of the shunt resistance required to convert it into an anmeter reading to 2 A .
Use the formulae given in the article to check your answers. Answers to Question 1 last month are given on page 790.

Part 3 Next Month

# A MODEL CONTROL TRANSMITTER 

TTHE circuit shown here is extremely simple, and has proved to be very useful. When experimenting with radio control equipment indoors, power can be drawn from a small nains unit. This unit should deliver 6.3 V a.c. for the 6C4 heater, and 10 mA at 150 V h.t. supply. When mains are not available, the mains unit is removed, and the iransmitter operated from batteries. As O.15A is drawn from the 6 V supply, reasonable battery life is obtained.

Fig. 1 shows the transmitter circuit and battery conrections. Any home-built or ready-made c.w. type receiver may be used. The transmitter is not suitable for controlling tone receivers. The unit is tuned to the required frequency by TCI and the control switch or key used to control the model is connected in the 6C4 cathode.

The transmitter is built on a pioce of thin paxolin 4 in . $x$ 4in. Drilling positions can be taken from Fig. 2. The valveholder requires a sin. dianeter hole. Short 6BA or similar bolts are provided with tags and fitted in the positions indicated. for battery, coil and key connections.

An extra tag is fitted at point 1. Fig. 2. and one projecting tag of TCl is soldered to this. A stout lead passes from the centre tag of the trimmer, through a small hole, and to tag 3 in Fig. 3.

All underneath wiring is shown in Fig. 3, and leads and parts should be positioned approxinnately as illustrated. Wires are short and direct, and insulated sleeving is used on all leads. The wire ends of resistors and capacitors are cut down as necessary. Connections should be rigid, so 20 s.w.g. tinned copper wire, with $1 \mathrm{~m} . \mathrm{m}$. sleeving, will be satisfactory. A lead passes from h.t. positive to tag 2, as in Fig. 2.

## Coil LI/L2

This need not be wound exactly as described, provided it can be tuned to $27 \mathrm{Mc} / \mathrm{s}$ with TCI trimmer about half closed. For this type of circuit, a selfsupporting coil is not recommended. A smooth pavolin tube can be used as a former. though a former with notched ribs is better as turns are then evenly spaced and cannot move.

The former actually used was approximately $\frac{3}{3}$ in. acrose the ribs and $1 \frac{1}{4} \mathrm{in}$. lone. 1.2 consish of 10 turns of 205.w.g. tinned copper wire, the winding oceupy-


Fig. 1: The 27 Mc s transmitter circuit.
ing 1 in . A short lead is soldered on the centre turn, this being the tapping 2 in Fig. 1. The ends of 1 ? coil are soldered to tags 1 and 3 in Fig. 2, and the tapping is soldered to tag 2.

Two turns of insulated wire are used for the arrial coupling winding L1. These are wound round the centre of L2 coil, the ends being twisted togeiher, and taken to tags 4 and 5. In Fig. 2,
this winding and its connections are shown with broken lines.

A former which would hold 10 turns, $\frac{5}{8}$ in. in diameter, was tried, and was also satisfactory. A $\frac{7}{8} \mathrm{in}$. diameter former would also do well. Formers smaller than $\frac{s}{8}$ in. diameter are not recommended. The wire gauge and spacing between turns are not critical, provided the finished coil can be tuned around $27 \mathrm{Mc} / \mathrm{s}$. The finished coil was - mounted with a ${ }^{f}$ in. bolt, spacer and bracket, as in Fig. 2.

## Tuning and Aerial

The heater may be run from a.c. or d.c., the polarity with d.c. being unimportant. The h.t. supply is 90 V to 150 V according -to power required or the supply available.

The transmitter must be tuned to a frequency in the Model Control band (26.96-27.28 $\mathrm{Mc} / \mathrm{s}$ ) before the aerial is attached. If desired, a test for r.f. can be made by soldering a 6 V 0.06 A bulb to a 2 -turn loop,
$\therefore$ and bringing the loop near the transmitter coil. The bulb should light at reasonable brilliance.

To tune the transmitter, a calibrated wavemeter is required. The wavemeter is set to a frequency near the middle of the band (say about $27 \cdot 1 \mathrm{Mc} / \mathrm{s}$ ) and is coupled to the transmitter coil. If the wavemeter has a bulb indicator, the wavemeter coil will need to be in line with the transmitter coil, with an inch or so hetween coils. Coupling should be loose (coils as far apart as possible, provided sufficient power is transferred to light the, bulb). TC1 trimmer is then rotated until the wavemeter bulb lights best. A 9 in . length of insu-
*. lated tube, filed to engage- the trimmer, is handy for tuning.

If the wavemeter has a selisitive moving-coil meter indicator,

- coupling between transmitter and wavemeter can be small, the units being separated by such distance as will give a satisfactory deflection of the meter.

If the coil has been wound to dimensions other than those given, the tuning range ohtained may be unsuitable. If $27 \mathrm{Mc} / \mathrm{s}$ is approached with TC1 trimmer


Fig. 2: Layout on top side of the chassis panel.


Fig. 3: Wiring on the underside.

## COMPONENTS LIST

RI 10k $\Omega$ IW
CI 1000 pF 250 V or similar
C2 25 pF mica or ceramic
C3 1000 pF 250 V or similar
VI 6C4
One B7G valveholder. $1 \frac{1}{4} \mathrm{in}$. $x$ in. diameter coil former. $4 i n . \times 4 \mathrm{in} . \times \frac{1}{15} \mathrm{in}$. paxolin panel. 20s.w.g. wire, 6BA nuts, bolts, connecting wire, etc.

## monitoring a BIG

## A RAPID FAULT-FINDING SYSTEM FOR COMMUNICATIONS RECEIVERS

## Receiver

by S. Simpson

ANY item of electronic equipment is liable to break down but, in the case of communications receivers, such "down time" must be kept to a minimum if communication schedules are to be maintained. Rapid maintenance of the receiver when the fault has been found is very largely tied up with the design and layout of the receiver, but rapid fault finding can be greatly helped by a comprehensive monitoring system.

Monitoring a receiver such as that shown in Fig. 1 can be a very extensive arrangement if all possible points are to be covered. Obviously h.t. lines have a priority and one could feasibly monitor all h.t.-carrying electrodes at all valves.

One could also check all bias voltages where such are developed.

All this could lead to a monitoring system so complex that it might itself require monitoring to ensure its serviceability, to say nothing of the risk of malfunctioning of the receiver caused by interaction in the numerous monitor leads!

A compromise can, however, be obtained and is described in the following paragraphs. It leaves several gaps in information but does narrow the field such that the operator should be able, firstly, to say with fair certainty what has happened and, secondly. by using normal metering and tools to quickly clear the fault.


Fig. 1: A block diogram indicating the monitoring system in a typical communications receiver.

## Monitoring Points

H.T. supplies must be known, thus the rough h.t. and smoothed supply are monitored. One thus has a check on the filter system, also a check on serious breakdown of decoupling capacitors. Working backward through the receiver the next useful point is the a.f. output signal (for a reason explained shortly). This signal is taken from the output transformer secondary, rectilied, smoothed and passed as a fluctuating d.c. voltage to the monitor switch.

The a.f. output valve is a "hard" worker and a check on its bias condition is desirable. The paralleled resistance of the meter will temporarily alter the actual operational bias but a reading taken during normal operations gives a figure for comparison when abnormal operation is sus* pected.)
(4) The stabilised voltage applied to the local oscillator in the frequency changer; a voltage can be present even if the stabiliser valve has failed but will differ appreciably from normal.
With these facilities the operation of the entire receiver can be checked as follows:
(1) The crystal calibrator is switched in.
(2) The r.f. gain control is turned to maximum and the receiver tuned to a known harmonic on, say, the medium wave band if a $100 \mathrm{kc} / \mathrm{s}$ crystal is in use.
(3) A.G.C. is switched in, also b.f.o. at $1 \mathrm{kc} / \mathrm{s}$.
(4) The monitor circuit is switched to i.f. cathode bias and the receiver carefully retuncd to maximum signal (minimum bias reading). This should coincide with a previously logged dial setting of the tuning capacitors.


Fig. 2: A 'tone-test' arrangement for checking the a.f. amplifier stage of the receiver.

In the recciver shown amplificd a.g.c. is used. The full output of the a.g.c. diode is monitored, also the cathode bias of the last controlled i.f. valve. Drift in tuning of that i.f. amplifier, which is part of the amplified a.g.c. system, is thus shown by a fall in dinde output: a fault or drift in the main i.f. amplifier is also made apparent by comparing a known diode output against the effect of a.g.c. in the i.f. amplifier.

The question arises: How does one know that the a.g.c. i.f. amplifier is receiving a normal signal to cause it to produce a known diode output? This doubt is settled by further monitoring at the points listed below:
(1) The r.f. output of the calibration oscillator, rectified by a diode, to show that r.f. is indeed coupled to the receiver input.
(2) The cathode bias of the calibration oscillator to show whether the valve is oscillating normally (weak oscillation shows up as an increased voltage).
(3) The cathode bias of the frequency changer (again weak or non-oscillation gives a noticeable rise above a normal operation figure).
(5) The monitor circuit is now switched to a.f. output.
(6) The a.f. gain control is set to a predetermined position (gained from experience).
(7) If the receiver is behaving normally a known figure of a.f. output is shown on the monitor.
The above procedure has proved satisfactory in checking the receiver diagrammed in Fig. 1 but will. of course, be modified to suit individual cases.

So far the monitor has covered the complete front end, the i.f. amplifier, the a.g.c. system and a check of a.f. output. It is, however, useful to be able to check the a.f. amplifice on its own and the following method, illustrated in Fig. 2, is used by the author for the purpose.

A taut 10 in . length of piano wire is stretched across the wooden baffle board supporting the loudspeaker (tightening is achieved by passing one end of the wire through a hole drilled in the shank of a No, 6 wood serew which has been run well
-continued on page 758


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| :---: | :---: | :---: |
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| $8^{\prime}$ H.F. 812 | 12,000 gauss | E3 166 |
| $88^{\text {P M.F. } 810}$ | 10,000 gausa | 62170 |
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## A COMMENTARY BY HENRY PRACTICALIY WREILSS <br> <br> No. 4 <br> <br> No. 4 For the For the Present

 Present}THE national dailies are clamorous, just about now, with suggestions of seasonal gifts. The lady columnists slink between laden counters, licking their pencils, filling their notebooks with apt ideas.
In these days we have to shop this early for Christmas, otherwise the stores will only have Easter eggs on show.
Remembering some of the presents we have received from misguided maiden aunts, and malicious colleagues, we thought it could be a good notion to suggest a few suitable ideas for some of the characters who have haunted the radio enthusiast in these pages and elsewhere.
Simple gifts, as for example a second-hand flea-trainer's outfit for the chap who thinks up those diminutive designs which so tax the constructor's evesight and defeat his fumbling fingers.
Or a "Lucky-Dip" parcel of unrelated oddments for the contributor whose constructional article advocates: " 33 zurns of 24s.w.g. enamelled copper on a tin. former, and 100 turns of 42s.w.g. double-silk covered on XYZ former type 54321 ", I mean, have you ever tried to calculate how miany inches (feet. yards?) make 100 turns of


Lady columnists slink between laden counters.

42s.w.g., then ask for that odd length at your local factor's spares counter?

Then there is the chap who thought up the modern. plastic knob, which disintegrates at a touch. This horror-for which a replacement can seldom be obtained-has to be pulled or twisted off before any work can be done on the receiver. Perhaps a blown-out Chinese egg, suitably mounted?

And for the creator of the other kind of knob, with concealed security, a grub-screw beneath a flange. or an angled spring just beyond the reach of one's longest screwdriver, a set of wire puzzles.

A ball of tangled string would not be inappropriate as a gift for the bright bloke who thought up the combination of harness and printed circuit used on some television receivers. Tracing h.t. on these without a circuit diagramand sometimes with one-is like touring Wales with a home-made man.

Don't let us forget. while on the subject of diagrams, two wellearned awards. First. one of those teasing "Present to follow" postcards we used to get at school for the producer of the radio for which a circuit is never-not nohow-obtainable. And a modern. do-it-yourself novel for the technical author whose manual flops about like a stranded fish. with components on one page, tables of values on another, and portions of the circuit satlered about like plums in an alms-house pudding.

Jig-saw puzzles used to be frequent presents when Henry was a lad. One of the interlocking type would do well for the designer of the set which used those banks of moulded componente in which the middle one always seems to go.

Then there is always the tool and equipment market-ue could think of more examples


A ball o, tongled string.
here than the Editor would allow us to cite. But we must not forget to send a tube of burn salve to the genius who first thought up the method of mounting multi-contact switches in a printed-circuit panel. He must have burned his fingers mightily while mocking up that prototype.

Remember those games that used to swell our stocking. the ones that required the victim to get a dozen balls simultaneously on a dozen shallow depressions, annoyingly heneath glass? Suitable, don't you think, for the chap who wants us to hold four pen-light cells at once. or even five U-11 type cells, to make any test on a small transistor receiver that entails removing the back.

And. going even further back in memory. a cats-cradle of string for the inventor of some of the more irrationa! drive-cord designs. A rubber one. if such can be imagined. for the tape recorder brain who loops his belts around hidden pulleys in inaccessible places.

I leave you. gentle Reader. to think up gifte that might suit others of sur tormentors. 1 must away to consult with fellow contributors to cook up something special for the Editor.

## An Experimenter's

GALVANOMETER

## BY C. J. PAULL

T$\rceil$ HIS article describes the construction of a moderately sensitive D'Arsonval-type galvanometer for the amateur experimenter. The complete instrument consists of three separate parts: (a) The galvanometer itself, (b) the lamp and lens assembly and (c) the scale over which the lightspot moves.

## The Galvanometer (a)

This consists of a coil, two suspensions which act as current leads and provide the restoring force, a mirror glued to the bottom of the coil, a U-shaped magnet to provide the magnetic field


Fig. I: This shows, approximately full-size, the construction of the galvanometer itself.
and a soft iron core to concentrate the field in the region of the coil.

The coil was made from 100 turns 36s.w.g. enamelled copper wire wound on a rectangular wooden former about $\frac{1}{4} \mathrm{in}$. narrower than the air gap of the magnet. After winding, the former was removed and a little glue rubbed into the coil to hold the strands of wire together.

The suspensions were made from "silver paper" (actually aluminium foil) cut to $1 / 100 \mathrm{in}$. wide strips, 4 in. long, with the ends widened to about $\frac{1}{8}$ in. to facilitate joining to the copper wire. The necessary fineness of the suspensions was achieved with the help of a very sharp pointed modelling knife, a steel rule to act as a guide and a sheet of aluminium to afford a suitable base for the cutting operation. The suspensions (above and below) were joined to the bared copper leads from the coil by winding them round and round these leads and then binding some fine copper wire over them to make certain of a good contact. The other ends were connected to suitable terminals at the top and bottom of the case by a similar method, the top terminal being rotatable.

A small, carefully chosen piece of a concave shaving mirror was stuck to the bottom of the coil.

The case was made from mahogany-faced ply and had the dimensions 1 in . $x 2 \frac{1}{2} \mathrm{in}$. $x 3 \mathrm{in}$. with a removable glass panel inserted in the front.

## The Lamp and Lens Assembly (b)

The lamp was rated at 6 V 0.5 A and the lens was an ordinary lin. diameter magnifier, adjustable to between 3 in . and 6 in . from the lamp. A fine
-continued on page 794


Fig. 3: Details of the scole.


Fig. 2: The complete set-up of galvanometer, scale and light source. Approximate total cost of the complete instrument, 10s.

# PHOTOCONOLCTITRS 

 BY B. R. GAINES
## The Cadmium Sulphide Photo-conductive Cell in Practice

UNTIL the advent of the photo-transistor. the only light-sensitive devices generally available were the barrier-cell used in photographic exposure meters, the photo-emmisive cell used in sound-film projectors and the selenium photo-conductive cell (often made up from a burnt-out rectifier!).

None of these has the sufficient sensitivity or ease of use for practical general-purpose work, and it was only when photo-transistors became readily available about six years ago that real interest in light operated devices was stimulated:
Even photo-transistors have disadvantages in some applications however. especially where robustness, high-sensitivity, wide-range of illuminations, power-handling. voltage-handling or exact measurement of light intensity have to be catered for. There has, however become available a device which fulfils all these requirements: this is the Cadmium Sulphide Photo-conductive Cell. which operates on the same principle as the old

Fig. I (below): Data on the Ericcson K42 photo-conductive cell.
A: Maximum Ratings
Maximum Polarising Voltage
50 V
Maximum Photocurrent
50 mA
Maximum Power Dissipation
0.4 W

Ambient Temperature Range
$-25^{\circ} \mathrm{C}-60^{\circ} \mathrm{C}$
B: Sensitivity


C: "Rule of Thumb" Sensitivity Guide
Cell Resistance in:

| Bright Sunlight | $\ldots$ | $\ldots$ | $\ldots$ | $10 \Omega$ |
| :--- | :--- | :--- | :--- | :--- |
| Daylight | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| Late dusk $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 1 ks |
| Darkness | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |

Selenium Cell but is in all respects a great advance on these.

The characteristics of one very good example of this type of cell, the Ericcson K42, are shown in Fig. 1. The K42 may be regarded as a resistor whose resistance is determined by the amount of light falling upon its sensitive surface.
It is the enormous range of this resistance from 102 in bright sunlight to more than 10M!? in darkness. from virtually short circuit to virtually open circuit, which makes this cell so useful.

Its colour response also does not have the great peak in the infra-red of photo-transistors and extends over the entire visual range, making the K42 suitable for light measurement.

The sensitive part of the K42 consiste of a layer of cadmium sulphide with traces of copper and chlorine added. This unit is potted in epoxy resin inside a metal can behind a glass window scaled with silicone rubber.


Fig. 2: This graph indicates the $K 42$ 's relative response to different colours.

The systen is extremely robust and moisture resistant, and the writer has certainly found no way of damaging the K42 except by using it with voltages and currents well outside the manufacturer's ratings. The constructional part of this article centres about :he K42 and describes its use in light-operated switches and automatic volume controls.

## Direct Operation of Relays

Because of its high sensitivity and ability to handle large currents the K42 is able to control relays directly without prior amplification: in this applicalion it may be regarded as a variable resitance of $100 \Omega$ or less in light, $1 \mathrm{k} \Omega$ in the dim light of late dusk, 10M1! in darkness.


Fig. 3 (above): Dimensions and general appearance of the K42.

Fig. 4 shows the simplest circuit for direct relay operation in which the K42 is placed in series with

- the relay coil and its power supply. When the photo-conductor is in darkness little current flows because its resistance is high. and the relay is open. When light falls on the cell its resistance decreases and sufficient current flows to close the relay.

Note that there is no need for a protective dinde across the relay coil. since the $\mathbf{K} 42$ in series with the relay coil does not generate large back e.m.f.'s as do some transistor circuits.

In the operation of the circuit of Fig 4, there is : " "electrical hacklash" in that. whilst the relay may close on a certain current (about 6 mA for a $1 \mathrm{k} \Omega$ P.O. relay with one contact). it will not open again until the current falls rather below this (about 4 mA for the relay considered).

This effect is of considerable importance in practical applications which require the relay to operate on currents due to slowly changing illumination.

If there is little backlash the relay tends to " chatter" when the light-level brings the current near its open/close point; backlash by making a very definite difference between open and close currents obviates this defect.

The only restriction on the relay used in Fig. 4
$\therefore$ " is that it should not require more than 50 mA or 50 V to operate. The writer has found that Post Office relays with coil resistances of about $1 \mathrm{k} \Omega$ work satisfactorily on a supply of 12V and has designed parking light switches about these.

Almost any relay may be used however, and the simplest procedure with one of unknown properties is to find out what voltage will just cause it to operate and then to use a supply voltage about one - and a half to two times this, subject to the restriction above.

## Parking Light Switch

The simple circuit of Fig. 4 has - insufficient backlash to guarantee chatter-free operation when the K42 is used to open and close a relay in the slowly changing light of dawn and dusk.

Additional backlash can be created by connecting a shunt resistor, R1 (Fig. 5), in parallel with the relay coil when the relay is open. This takes some of the

Fig. 4 (right): The K42 in series control of a relay.
Fig. 5 (below): Here RI is added
in parallel with the relay to provide additional backlash. Its operation with RI disconnected is described in the text.

current supplied to the relay and thus reduces its sensitivity when open.

If R1 is disconnected once the relay has closed the sensitivity goes back to normal, and hence the difference between "open" and "close" currents has been made greater, i.e. the backlash has increased. In practice the relay is made to switch the shunt resistor in and out by means of its own contacts.

Fig. 6 shows a practical circuit for this type of parking light switch and the method of connecting it into the car wiring. The centre section is the


Fig. 6: A car porking light system using the K42.


Fig. 7 (left): Parallel control of a relay.
Fig. 9 (right): A power supply for 12 V relays.
switch itself which is essentially that of Fig. 4 with the addition of automatic bachlash described above.

The K42 is in series with the relay coil, opening the relay during the night, and therefore the switch contact on the relay must be of the "normalclosed" type. This same contact is used to switch the shunt resistor R1 in parallel with the relay coil when the relay is closed, thus increasing the backlash as described above.

If a relay of different resistance to that shown is used, R1 should be changed to be about five times the relay, resistance. The "over-ride" switch bypasses the relay contacts and converts the parking light to normal manual operation.

The actual details of construction and connection of the parking light switch will vary with the requirements of the individual car. The K 42 must, of course, be placed so as to see the full effect of the ambient light. and the most convenient place to put it is just behind the front window facing outwards; it need not face straight up into the sky.

The relay unit can usually be found a place behind the dash or in the map or glove compartment: for reliability a sealed relay is preferable, and some protection of the contacts should in any case be provided.

The wire to the parking light may be broken into and the automatic switch fitted (Fig. 6) at any point after it has left the main lighting switch. The chassis-earth connection should be securely attached to the metal-work.

A 2 A fuse in the 12 V line is some worth-while protection against blowing the main car fuses when installing the unit!

## Parking Light Switch II

In many towns parking lights are only required after $11 \mathrm{p} . \mathrm{m}$. or when the street-lighting goes off, and the automatic switch has only to switch them off at dawn, there being no advantage in one
which would switch them on long before they were required.

This " single-shot" working has the advantage that relay chatter can be completely eliminated by a switch which switches off the lights automatically, but requires manual re-setting to switch them on. Then the relay opens at dawn and once open stays open.

The previous circuit could be changed to this mode of operation, but there is an alternative way of controlling a relay directly with a $\mathbb{K} 42$ which is sometimes advantageous and the writer will describe this rather than cover the same ground again.

In this mode of operation the K 42 is connected in parallel with the relay coil and therefore shares with it the current supplied by R2 (Fig. 7). In darkness the K42 has a high resistance and all the current flows through the relay.

In light the K42 is low resistance and takes most of the current so that the relay opens. R2 should be greater than a third of the relay resistance and must limit the current through the K42 to less than 40 mA .

This switch is converted to single-shot working described above, by arranging for the relay to cut off its own power supply when it opens so that it cannot close again.

Fig. 8 shows a practical circuit for this type of parking light switch and the method of connecting


Fig. 8: A 'single-shot' parking light' system (II).
it into the car wiring. Only one switch contact on the relay is used as before, but since the relay is now closed in darkness this must be of the " normal-open" type.

This contact not only controls the supply to the parking light but also that to the relay itself, and hence once the relay opens it cuts off its own supply and cannot close again.

When the lights are to be switched on at night the supply to the relay must be mementarily switched on, whence the relay will lock-in until it opens automatically at dawn.

The simplest way to do this is to push in the relay armature, which makes the relay contact and acts as the required starting switch; if some means of locking the armature in is also provided this
-continued on page 774


THE quality of sound produced by lower-priced tape-recorders and small radio receivers is of a high order bearing in mind the restricted space within the cabinet which must of necessity accommodate both the speaker and the rest of the "works" and it is generally appreciated that given a specially designed enclosure the same loudspeaker would perform more efficiently so that for the equivalent amount of electrical power a greater volume of sound over an extended frequency range would result.

In some cases a listener may wish to effect an improvement in his equipment but he will be deterred from embarking upon the project for fear that it will be a complicated task beyond his capabilities or resources or more likely he will doubt whether, as applied to inexpensive equipment, his efforts are likely to be rewarded with success.

If the reader wishes to prove to his own satisfaction the importance of the correct mounting of loudspeakers and has a spare which can be used as an extension unit, it is an easy matter to compare the effect of a rusimentary baffle, fashioned from a large piece of stiff cardhoard with a central hole of appropriate size, added to the otherwise unmounted speaker while this is in operation, to observe the immodiate improvement in reproduction especially in the lower register.

Even though this arrangement is not by any means ideal, the sound now has a more pleasant "quality' compared to the thin 'toppy" effect without the baffle.

There is a risk, of course, that an ill-designed
or poorly constructed complex enclosure may prove disappointing where a well made simple one may give satisfaction, especially if it is desired to have the equipment in portable form for lectures and recitals where the question of transportation weighs heavily.

It is suggested that the reader who desires to find out whether his equipment is capable of producing better results may care to construct a plain baffle for test purposes and if he is satisfied with what he hears he can then convert it into something more elaborate.

## WHY A baffle is NECESSARY

A full discussion of the theory governing this subject is beyond the scope of this brief article but it must be explained that the air vibrations which constitute the sound waves from the loudspeaker are the result of the reciprocating action of the cone.

It is easy to sec that air compressed as the cone moves forward will escape round the unprotected edge of the speaker to reinforce the low pressure region created at the rear so that the two trains of waves, being in anti-phase, tend to cancel out; an effect which is less pronounced as the frequency rises, hence the apparent lack of bass.

By interposing a physical barrier between these two vibrating air masses it is possible to reduce the effect by a factor which depends upon the area of the baffle, which should be as large as possibie, although in practice the dimensions need not exceed about three feet per side for reasonable performance from a small speaker.

It is important, however, to choose a material having sufficient density to prevent the structure yiclding to the effects of the sound waves impinging upon it and thus transmitting the wave motion. It is especially important to avoid the natural frequency of vibration of the baffle falling within the frequency range of the equipment as such reasonance, can cause a very objectionable 'boominess .
Mounting the speaker in a hole in a brick dividing wall between two rooms is an excellent practical solution to the problem hut this and other bizarre ideas, often proposed in Hi-Fi circles, such as the use of a length of drainpipe or a brick corner cabinet are ideas which are seldom received with enthusiasm by other members of the family so that the average listener must be content with conventional materials such as thick plywood or blockboard.

## MAKING A SIMPLE BAFFLE

Fig. 1 shows one way of making an efficient baffle from materials which at first seem unsuited to the task. Hardboard is an attractive alternative to the other popular materials by virtue of its cheapness but it lacks the requisite degree of density, a deficiency which can be overcome by producing a composite structure of cellular form in which the cavities are filled with sand.

The sheet of hardboard selected for the front is first prepared by cutting a circular hole of the required diameter to suit the loudspeaker. Strips of plared wood about 1 in . square are then fixed round the edges and to form a square enclosing
the speaker opening with cross members inserted to sub-divide the intervening space. Liberal use of adhesive, supplemented by tacks, is recommended to ensure sound joints. Fig. 1a shows a detall of the construction

When the adhesive is set, the cavities may be filled with dry sand which is settled by tapping the edge of the sheet. The second piece of hardboard. with a square central hole 10 match the wood frame surrounding the speaker then completes the assembly. It may be prudent to enclose the speaker in a fabric bag as a precaution against stray sand grains entering between the speech coil and the magnet gap.

It is advisable to ensure that the sand is quite dry to prevent deterioration due to dampness which could occur after a lapse of time and when securing the loudspeaker to the inside surface of the front sheet the use of bolts with wing nuts
will render its removal easy for storage and transportation. The face of the baffle may be covered with one of the ornamental woven fabrics. Attach a couple of rubber feet, a carrying handle and a hinged rear support with safeiy chain and the job will be finished.

The principle of sand loading is not. of course, conlined to this simple form of baffle. Almost any enclosure will benclit from the increased density obtained in this way. A plain baffle modified to form a comer cabinet by including a port and a triangular plywood top is shown in Fig. 2.

The writer has successfully used a simple baffle mounted in a disused fireplace so that the chimney acts as the cabinct. In a large hall or on stage a temporary corner can be fashioned from two large plain rectangular sand-loaded panels set at right angles as shown in Fig. 3 .

Figs. I to 4 below


## CONNECTING THE EXTERNAL SPEAKER

Most commercial tape-recorders and some radio receivers provide an outlet for an external loudspeaker and it is important to ensure that the component which you propose to use has a speech coil of the correct impedance.

If in doubt, consult the handbook or the manufacturer's agent and if it should happen that your loudspeaker has a $15 \Omega$ coil and the equipment is designed for $3 \Omega$, or vice-versa, a special transformer, designated type WMT 1. is available from Messrs. Wharfedale to take care of this situation.

In the absence of an external speaker socket it is a simple matter to instal one. Purchase a standard telephone jack socket and plug and locate the former in a conveniently placed hole in the cabinet. disconnect the internal speaker leads from the matching transformer and re-connect them to one side of the socket as shown. Connect the
internal speaker to the remaining contacts on the socket. For details of socket connection see Fig. 4.

The external loudspeaker should now be connected to the plug through a length of fairly thick flex, such as five ampere mains flex, and when the plug is inserted into the socket the internal speaker will be automatically disconnected as the external one becomes operative.

It is important not to use an audio amplifier without a speaker, or some other form of load, as this may be detrimental to the output transformer.

It must be stressed that you cannot make a silk purse from a sow's ear. In the type of equipment considered here, mediocre results are very often due to deficiencies in that part of the circuit which converts the electrical energy into sound and the use of a properly mounted external speaker will often give a very satisfying improvement for a small financial outlay.

## MONITORING A BIG RECEIVER

## —continued from page 748

into the board. The other end is looped around a strong steel pin).

A right-angled piece of aluminium is placed as a bridge under the wire at about one-third of its length from the pin and the wire then tuned to about $800 \mathrm{c} / \mathrm{s}$.

Under the wire an electromagnetic pick-up (made from an Eclipse button magnet wound with 200 turns of $36 \mathrm{~s} . w . g$. enamelled wire) is mounted. The output from the pick-up is passed into a microphone step-up transformer placed clear of the field from the loudspeaker output transformer.

The output from the transformer is passed by an earthed, screened lead to a switch (" tone test ") on the receiver panel. Closing the switch applies the transformed output to the input of the a.f. amplifier and disconnects the diode output.

To test the amplifier the receiver h.t. switch is opened and the "tone test" switch closed. The monitor is set for a.f. output. The a.f. gain control is set to about half-travel and the h.t. switch is then closed.

The noise pulse emanating from the loudspeaker on application of h.t. will cause a wide range of frequency vibrations in the baffle board, also acoustic shock waves, and their combined effect will set the tone string into vibration.

This produces an output from the pick-up which passes to the amplifier, thence, if all is well, to the loudspeaker. thus sustaining the vibration which initiated the string movement. The note from the loudspeaker will build up to a maximum determined by the gain setting and the a.f. output can be visually checked at the monitor.

Knowing the output to be expected from a given a.f. gain setting the output performance of the amplifier (if not its quality!) can be checked.

The above systems still leave something to be desired but have proved quite effective in practice and are far better than nothing. To those readers win use a big set and have no means of monitoring other than an S-meter or a magic eye they may possibly cause some interesting thought on the subject.

## SHORT-WAVE SUPERHET

-continued from page 737
domestic receiver tuned to the BBC Light Programme on $200 \mathrm{kc} / \mathrm{s}$ near the generator. Tune the generator until zero beat is obtained. The $200 \mathrm{kc} / \mathrm{s}$ signal may now be injected into the main receiver. In this way the points between the $1 \mathrm{Mc} / \mathrm{s}$ intervals may be filled in. Note that for the higher harmonics the coupling between the generator and receiver will have to be increased.

The receiver dial is marked with Indian ink, using a fine nib. The author found that a gentle roughening of the dial surface with a moist rag smeared with a trace of scouring powder was necessary to achieve a good writing surface. Care is essential during this operation.

## ALTERNATIVE USES

The author has found other uses for this simple generator. For example, because the oscillator is a two-terminal type coils may be matched exactly by inserting them in the grid circuit of the generator. With one coil in position the generator dial is set an arbitrary point and the signal tuned in on a receiver. The coil is removed and with the generator dial unchanged the other coil inserted. The turns on the coil are then adjusted until the radiated signal is picked up on the set. Similarly, by using known values of inductances the capacities of capacitors may be measured over the range $50-1,000 \mathrm{pF}$.

The unit may also be used, if so desired, as an audio frequency source by modifying the oscillator as follows: Insert the secondary of an old audio frequency transformer between the blank position on the switch and earth. A capacitor of approximately $5,000 \mathrm{pF}$ should be placed in parallel with this secondary winding. Delete C1 and insert a $0.01 \mu \mathrm{~F}$ capacitor in place of C1. Disconnect the a.c. source to the oscillator and connect the oscillator to a d.c. supply of approximately $200-250 \mathrm{~V}$. The heaters, of course. are still fed with 6.3 V a.c. The audio output may be taken from the grid via a $0.01 \mu \mathrm{~F}$ capacitor.

## IIIPROVENEVTS

# to transistor portables <br> by J. Longrise 

SIEVERAL smali improvements or modifications can be made to most home built transistor receivers, and it is useful to make some of these, to fili the need for an external aerial, personal phone, or other features not already provided. It is assumed that the receiver is in good condition, and may have been used for some time.

## External Aerial

Due to directive effects and screening, the internal ferrite rod aerial is unsatisfactory in a vehicle. To overcome this, an outside aerial is often clipped to the vehicle window.

The external aerial is best coupled to the receiver by having a small additional winding on the ferrite rod, as in Fig. 1. This coil can be


Fig. 1: A coupling coil for an external (car) aerial.
purchased, or may be about 30 turns of any thin insulated wire. A screened co-axial lead is generally taken from the vehicle aerial, so a co-axial socket is best on the receiver. The inner pin goes to the aerial, and the outer sleeve to the outer brading of the co-axial cable.
If the external aerial is merely to increase range and sensitivity, the screened lead is not wanted, and is best omitted. A single sucket of ordinary type will then do for the aerial connection. The loop is returned to the receiver earth line (battery positive). A telescopic or wire aerial can then be plugged in.

## Reduction Drive

Many receivers have a knob directly on the tuning capacitor spindle. Miniature tuning capacitors of the type fitted in transistor sets may be obtained with integral reduction drive. This
has a ratio of about 6:1, and makes tuning easier.
With some receivers, a small ball drive can be fitted. as in Fig. 2. For example, this is possible in the Practical Wireless Celeste if the gang capacitor is moved to the rear of the panel.

Such epicyclic drives have a lug, which must be securely anchored. This nay be done by using a long bolt and extra nuts or spacing washers, or fitting a strong bracket. The pointer rotates with the capacitor. The usual ball drive of this type has a ratio of aboust 6:1.

## Typical Circuit

Fig. 3 is the circuit of a typical transistor receiver, which may be of ordinary size, or miniature type. This circuit is given to illustrate connections for other modifications. Mast of the points covered would apply equally to somewhat different circuits.

## Clamp Diode

In Fig. 3, automatic gain control bias is obtained from the diode. and applied to the base of $\operatorname{Tr} 2$, via R10. Much better control of strong transmissions will be obtained if a elanp diode is added. This requires $680 \Omega$ and $2 \cdot 2 \mathrm{k} \Omega$ resistors, a $2 \mu \mathrm{~F}$ or similar capacitor, and a diode such as the OA79.


Fig. 2: Adding a ball drive to the tuning gang.


Fig. 3: A typical transistor superhet circuit used to indicate the various modifications.

The second i.f.t. is disconnected from the negative line, so that the $2 \cdot 2 \mathrm{k} \Omega$ resistor may be added, and the circuit changed to that in Fig. 4. Diode polarity is important. The original a.g.c. circuit is left unchanged.

Bias from the voltage drop in the $2.2 \mathrm{k} \Omega$ resistor results in the diode only conducting when very strong signals are tuned in. This prevents overloading and improves the a.g.c. action at these signal levels.

## Low Noise First I.F. Stage

A transistor receiver may have an almost silent background when a reasonably strong station is tuned in, but may have a severe background hiss on weak transmissions. This is because the gain of $\mathrm{T}_{\mathbb{L}} 2$ in Fig. 3 is maximum with weak signals. With strong signals, $\operatorname{Tr} 2$ base voltage shifts in a positive direction, reducing gain and hiss.

The hiss may be bad if an unlucky combination of R4 and R10 makes Tr2 base voltage rather negative. If this is so. shunting a $33 \mathrm{k}, 47 \mathrm{k}$ or $100 \mathrm{k} \Omega$ resistor across C 5 may reduce the hiss considerably. Alternatively, R10 may be slightly reduced in value; or R4 may be increased in value.

With 10 per cent tolerance resistors, the actual base voltage of Tr2 may vary considerably, between different receivers. Tr2 base voltage must not be too far positive, or gain is reduced badly. If one of the transistors $\operatorname{Tr} 2$ or $\operatorname{Tr} 3$ is relatively noisy it should be in the $\operatorname{Tr} 3$ position.

## Low Noise A.F. Stage

If bad background hiss is present, and does not change in volume when the $5 \mathrm{k} \Omega$ volume control VRI is admated, it is probably generated in the first audio amptifier stage. This is most likely when an additional audio amplifier precedes the driver, as in popular 7-transistor circuits.


Fig. 4: A clamp diode circuit for improved control of strong transmissions.

If hiss arises in Tr4 in Fig. 3, it may be better to change R13 to 47 kg , or to increase R15 to $1 \mathrm{k} \Omega$. Values in Fig. 3 are typica! when Tr 4 is the first audio, amplifier and driver.

If an extra audio stage is wanted. or if an existing stage is already present before the driver and values are suspected. then the circuit in Fig. 5 may be adopted. Values are chosen to allow good amplification at moderate power levels. with low noise.

The amplifier in Fig. 5 can be added to a circuit like that in Fig. 3, by taking the OC71 base lead $X$ to $X$ in Fig. 3. The new coupling capacitor in

Fig. 5 goes to the existing driver base, $\mathrm{Y}, \mathrm{Tr} 4$, in Fig. 3. The existing connection between $X$ and $Y$ in Fig. 3 is disconnected.

The additional audio stage is useful if the volume of some stations needs to be increased, though many receivers give an adequate performance with the arrangement in Fig. 3.

## Battery Economy

An unfortunate combination of resistor values in the output stage, in particular, may reduce battery life, yet result in no improvement in performance. This may happen if R17 and R18 are 10 per cent tolerance resistors, and if R17 proves to be a little low in value, and R18 a little high. The current drawn by Trs and Tr6 may then be much higher than necessary.

If this is so, the simplest cure is to shunt R18 with another resistor. values from about 470! to $2 k \Omega$ being tried. This can be done with the set working. Or R 17 may be increased in value. The receiver must not be switched on with R18 disconnected.

Should reproduction be distorted, especially when the battery is a little discharged, or when the receiver has been left in an unheated room in winter, R17 may be too high in value, and R18 too low. If so, shunt R17 with resistors of about $5 \mathrm{k} \Omega$ to $15 \mathrm{k} \Omega$. or increase R 18 in value. Tr5 and Tr'6 should draw about 2 mA , with no signal.

To obtain maximum gain and output. R19 is sometimes omitted, or is of very low value. This causes high peak currents. It is better that R19


Fig. 5: A low noise first a.f. stage.
should be $4.7 \Omega$ or $5 \cdot 6 \Omega$, which allows good power and sensitivity, with reasonable current drain.

## Mains Powered Eliminator

When a receiver is often used indoors, and fer long periods. it is economical to draw current from the mains. A suitable eliminator circuit is shown in Fig. 6.

An output of about 9 V is obtained from a 18 V secondary with centre tap. The $220 \Omega$ resistor helps to maintain a uniform voltage, with changes in current drawn. The $390 \Omega$ resistor and $0.25 \mu \mathrm{~F}$ capacitor form a transient suppressor to protect the equipment from surges caused by switching on and off domestic apparatus.

Half-wave rectification is also satisfactory, though the capacitor should then be increased to $1000 \mu \mathrm{~F}$. For half-wave circuits, the transformer needs no secondary centre tap, and only one rectifier is required.


Fig. 7: Incorporating a phone jack sacket which mutes the loudspeaker when the plug is inserted.

The unit is best built in an insulated case, with the socket strip taken from an old battery, so that the transistor receiver can be connected easily.

## Phone Jack

Phones, or a personal phone, allow listening without any disturbance to other persons. If a jack is used with contacts which open when the plug is inserted, these contacts can silence the loudspeaker.

A crrcuit for this purpose is shown in Fig. 7, and does very well for most medium impedance phones. Few changes are needed to existing wiring.

With some receivers, a phone iack is simply connected so that phones may be plugged in while the speaker still operates. This is also quite useful, as the rolume needed for the phones is quite small.

Occasionally, a jack for low resistance phones is wired in parallel with R18 in Fig. 3. The phones are then operated from the driver stage, and the reduction in resistance across R18 causes the output transistor base voltage to be more positive than usual, so almost cutting off the cutput transistors Trs and Trb.


## All times are in G.M.T.

## The Broadcast Bands-by John Guttridge

A$S$ most aspects of interest to the new shortwave lisiener have been covered now in this feature, in future much more space will be devoted to schedule changes and observations of various stations. Information from readers will be a great help in making this as comprebensive as possible.

First this month, though, there is an announcement of interest to all shortwave listeners from the International Short Wave Club, which is at present conducting a poll (held every three years) to find the most popular short wave station.

All listeners. whether members of the cluh or not, are invited to take part. To do so all that is necessary is list your five favourite short wave stations in order of popularity, together with a short note explaining the reasons for your No. 1 choice.

Your vote should be sent to ISWC. London, S.E. 16 by December 31st, 1964. Some winning stations have in the past given prizes for the best reasons put forward by listeners in support of their choice. ISWC, by the way, has just celebrated its 35th anniversary-congratulations!

Some good results in the 90 and 60 metre hands have been achieved recently by D. A. Lavender of Gravesend. He reports hearing Radio Santa Fe. Bogota, Colombia in Spanish from 0630-0730 on 4,965: Radio Abidjan, lvory Coast, with news in French at 2225 on 4.940; Radio Rumbos, Venezuela, on 4,970 in Spanish at 2220: and Radio Tananarive. Malagasey Republic. with music and French on 3,232 between 2200-2230. On Sundays, he says, the programme continues until 2300 .

Good reception of the European service of Radio Habana (Apt. Postal 7026. Habana, Cuba) is reported by P. H. Holgate of Blackpool. English is carried on 15,155 from 2010-2140.

Over in Ireland, D. Walsh has been picking up Damascus, Syria, on 15.165 in English from 1600 - 1630 and French from 1630-1700. E. II. Conduit of Wolverhampton, however, reports hearing these transmissions on 15,230 .
D. Walsh also reports that the General Service of Radio Japan. Tokyo, Japan, is getting through between 0800 and 1200 on 15,310 and 1200 and 1400 on 9,740 .

Several other stations are reported by E. H. Conduit. He says that relays of debates of the United Nations Security Council can be heard on 15,190/21.610. The Voice of America. Bound Brook, transmitter is used. Radio Pekin's transmission to Australia in English comes in well at

0830-0930 on 15.060 he says. Finally he has heard Radiodiffusion Television Marocaine in English between 2030-2130 on 1.1.735. In London this programme has also been heard on 15,410.

From Arhroath in Scotland, D. Taylor reports on Radio Vilnius, Vilnius, Lithuania, U.S.S.R., which, he says, has an English transmission between 0000-0030 on a frequency in the 42 metre band.

Extensive frequency changes were made by Radio Australia (P.O. Box 428G, G.P.O. Melbourne, Australia) on October 24th. English transmissions affected are: To Southern Asia $2214-2345$ on 15,2220 and $1430-1730$ on 9,5701 7.220; to East Asia 0859-1000 on 11,810/9.570, 2059-2300 on 17.820/15,240, 2300-0015 on 15,240 ; to Mid Pacific Islands $0630-0915$ on $11,710 / 9.570$ and $1800-2115$ on 9.600 ; to North Pacific Islands $0029-0645$ on 15.240 ; to North America $0100-0345$ on $17.840 / 15,220$; to Africa 0400-0515 on 17.820/15,220.

The British Isles transmission on 11,710/9.570 moved to the new time of 0814-0915. French can now be heard at 2315-0015 on 17.820 and $0515-0615$ on $11,710 / 15,180 / 15,220 / 17,820$. Finally new frequencies for the 2245-2345 Indonesian transmission are $11,760 / 15.330 / 17,870$. Radio Australia's programme for DX'ers may now be heard on Saturdays at 1930 and 2200 , Sundays at $0500,0900,1300$ and 1530 , and Mondays at 0215.

A colourful QSL giving all verification details is issued free of charge by Radio Warsaw, Warsaw, to those who submit correct reception reports. Until April, Warsaw broadcasts in English to the British Isles as follows: 1830-1857, 1930-2000 and $2135-2155$ on 6,135/7,125; 2030-2100 on $5,950 / 7.145$; and $2230-2300$ on $9.540 / 5.950$ and 1.502 medium wave. Listeners' letters are answered on Thursdays during the 2030 and 2230 transmissions. You may also be able to pick up the Australian service which goes out from $0730-$ 0800 and $0830-0900$ on 15.120/11,840/9.675.

On November 1 the Swiss Broadcasting Corporation, Berne, put a new schedule into operation. It is valid until May 1st, 1965. Several quite sweeping changes are made including the switching of the British Isles transmission to the morning. It is now aired from 1200-1300 on 7,110/9.665. Other English transmissions are 0715 - 0845 to Japan and China on $9.670 / 11.865$ / 15,305: 0900-1030 to Australia and South-east Asia on $0900-1030 ; 1315-1445$ to India and

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parts now only $\mathbf{4 2 / 6}$ 「. \& P. Parts Price List and casy build parts now only $32 / 6$. pians $2 \%$.

## TRANSONA SIX

- 8 stages-6 transistors and 2 This is a top performance receiver covering fuil Medium and Long Waves and Tramper Band. High-zrade approx. 3in. speaker makes listeming a Dipasure. Push-pull transformers Man ample power. Forrite rod aerial. Many stations listed in one evering includine Luxemboury loud and cirar. Sire $54 \times 48 \times 141 \mathrm{in}$ (Uses PP 4 battery avallable anywhere).
$\begin{array}{lll}\text { Total cost of all } & 59 / 6 & \text { P. \& P } \\ \text { parts now only } \\ \text { Parts Price List and easy }\end{array}$

MELODY SIX


nerisin amazed $a_{i}$ volume and mionemi has reully conte 3. (s. itu h lon-on-Tecs.

## 8 stages-6 transistori

 and $?$ diodesOur latest compietely portable transisto: ratio covering medium and long waves. lncorpotates pre-tagged elrcust board, 3n. beavy duty speaker. oob grede transistors, volnme control, tuning condenter. Wave change slide swlich sensitive tinn. rerrite
lod aerlat. Fush-pull output. tondejul recemtion ol R.B.C. Home and Liglt. 208 and Mand Contmental stations. Hand=ome dathet-look pocket srille and sumplied with hand and showder thapisPartstrice lisi and Total cost of all $\mathbf{Z 3 . 9 . 6}$. 8 \& P.

## POCKET FIVE

- 7 stages- 5 transistors and 2 diodes Covers hedjum and Long
Wave and Traw ei Band, a harerand Traw/eu Band, a ondy the mosi expensive fadios. On test Home. J.jght, L.uxembourg and many ontmentits sations werg Desimend rourifi and clear. $t$ bef Fetrite Rod Aerlal and
 file tone $2 ? 1 \mathrm{n}$. moving coll speaker butt into attractive biack cane with red speaker grilic. Sizc i' x it a ulln. (USes Parts Price List and easy buld plans 116. Total cost of all

42/6
P. \& P. $3^{\prime}-$

ROAMER SIX NEW!!
NOW WITH PHILLU MICRO-ALLOY R.F. TRAN.IISTORS - 6 WAVEBAND!!

-8 stages-6 transistors and 2 diodes
Listen ta stations half a walleband portable This 6 able on Atedium and Long able mes. frawler band and Yaves shomt Wave. Senslthue territe rod ae:lal and checocie acrial tar short waves. Ton grade transishandsome case w.th gilt
 Carrying sulap $2 \%$ - cxira. * EXTRA BAND FOR EASIER TUNING OF LUX, ETC. Ports Price List and Total cost of all
easy build plans 21 -
parts now only $\mathbf{9 . 6}$ P. \& 8 P.


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## (1) Electric Soldering Irons <br> 11/6



Africa on $9.535 / 11,865 / 17.845 / 17.795$ : 15001630 to Western North America on 15.305; 15001700 to the near and middle East on 9,535/9.665/ 11,865: and 0115--0245 to Eastern North America on $6,105 / 6,080 / 9,535$. S.B.C.s DX programme will as before be transmitted during Saturday's programmes.

An early morning $0600-0630$ broadcast in English to Europe is now aired by the Canadian Broadcasting Corporation on 9,625 . "Short wave listener's club" is now broadcast on Saturdays and
"Listeners' corner" on Surdays during the European transmission from $1215-1313$. This is on $17.820 / 15,320$.

Kol Isracl, Jerusalem, Isrāel, has switched beams for its 2015-2045 English trailsmission. It now uses 9,625 to Europe and 9,009 to South Africa.

Finally a note on a fairly easy South American. Radio Clube de Pernambuco, Brazil, can be heard well on 11,865 after 2100 . There is slight interference from the BBC on 11,860 .

## The Amateur Bands-by David Gibson G3JDG

TYHF Amateur Bands this month have proved quite interesting and DX has shone through here and there, although it has been a bit of a struggle at times.

## 160 m

The first band out of the hat this month is "Top Band" and is proving to be very lively indeed. Some years ago when I was first licensed, " $G$ " stations were the usual thing expected of the $1,800-2,000 \mathrm{kc} / \mathrm{s}$ section.

By way of contrast one recent listening period of 30 minutes only logged GW3SUY (RST569), GW3TJE (569), GI3JEX (579), OH3NY (569), and OK1AHB. Some 15-20"G" stations were in evidence at the time, notable signals from "G"s" 3ARI). 3SPJ, 3NTD, 3RBP and 6BX.

All were received on a dipole cut for 14,100 and just 15 feet high! Anyone with a decent aerial should be having a ball and American stations are rumoured to be roaming around top band. How about a postcard from you SWL's with a better antenna (or sharper ears)?

## 20 m

From trawlers and top hand out into the wild and woolly 20 m . $14,000-14,350$ is really hotting up these days and with the numerous contests which are in favour at the moment the band is really humming.

Newcomers might like to note that the band (as are all bands) is divided into two sectors, the CW sector and the Phone sector, the CW sector occupying the l.f. portion of the band. However there is no shortage of activity at either end of the 20 m band at the moment.

The 1964 Scandinavian Activity Contest was very much in evidence and OH5SM, OHIVR, OH1QY, OH5NQ and OH0NI (Aaland Island) were worked in 14 minutes on a.m. 'phone. After this the novelty rather wore off, hearing the other station coming back "Ur 58082 73-CQ . . CQ . . etc."

Later in the month it was decided to check how popular single-sideband was by logging only stations using this mode of transmission in the 'phone sector of 20 m . One sitting, over a period of $1 \frac{1}{4}$ hours resulted in some thirty stations logged on s.s.b.
"Twenty" at the moment dies out from about 01.00 onwards but from mid-afternoon till midnight it's a virtual hive of activity. Heard in one hour from 2045-2145: W9ECC, W1QCL. W2GWE, W4HCM/P, W0HLT, HB9NY, W9NWQ, W0QUU,

W8NKW, W9JT, VE3COB, "W2KXL, W1HZ, WA2SFP, W0VQ, K2UYG, CN8AX, W4HZR, K81,TT, W4ODL, CT1SQ, W4HZI, W8LXU, W3ZAO/MM (Maritime mobile), PY4AEB, SVOWGG (Crete) and K2YLM, all averaging five and eight except PY4AEB. All these with a dipole just 15 ft high. Anyone with a bean hear anything clse: JA-VK?

Speaking of VK, the VK/ZL contest might have afforded someone their first station from that part of the world, or was it the same as at G3JDGrather quiet? At the time of writing the 'phone event has passed silently on but the c.w. event is scheduled for the coming weetend, needless to say the receiver is being checked and the dial polished in readiness.

## 15 m

In the 15 m band report last month I said that things at this QTH were rather dead. This brought a letter from K. J. Clark in London, N. 15 , reporting W2JY, G3CAZ, HL1JP, WA4YO, K1WPF and HL4OX, using an HE40 receiver acquired the day before, and the antenna a 30 foot vertical.

So there it is. There are stations about on $21 \mathrm{Mc} / \mathrm{s} 80$ perhaps it's a question of what time to listen. K. J. Clark's times for the above list was the period $19 \cdot 30-20.00$.

## 40 m

$7000--7100$ has been almost hopeless at the time of writing. Listening in the evenongs from 1900 onward, European stations have appeared but the QRM from commercials (who have no right to be there anyway) makes it extremely difficult.

On one occasion a 9 M call sign (Malaya) was located and read as 9 M 2 L ? ? (either LD or LO or even LM), but due to terrific QRM from a commercial the station was lost. Remarks made at the time will not be repeated here!

A suggestion which might prove hopefor? is that all licensed amateurs who run tests with the antenna connected, in future should do so on frequencies occupied by these stations. If this procedure were adopted on a world-wide scale it might well prove a success, especially if our friends in W-land joined in, since their licence permits them to run $1,000 \mathrm{~W}$ as opposed to the British amateurs' 150 W .

## 10 m

Activity on the 10 m band is still quite high. Local nets are very much in evidence still, though
-continued on page 786


## Earls Court, August 24-September 5, 1964

## "Practical Wireless" Report

* A summary of new models seen at Earls Court and the trade exhibitions around London, and notes on design trends and features.
* The tables list new models only and do not necessarily represent the complete range of the makers concerned.
$\star$ For details of all the new TV sets, refer to the November issue of Practical Television.

CONTINUED FROM PAGE 640 OF THE NOVEMBER ISSUE

Last month, our Radio Show Report covered radiograms, transistor portables and table radios, leaving record players and tape recorders for comment this month.

## Tape Recorders

This was perhaps the least novel market, makers concentrating more on general improvement than innovations. New models were shown by Dansette, Sound, Defiant, Ferguson, HMV, Ultra and the luggage makers, Wood and Son (Revelation), at Earls Court.

Outside the main show there was more variety from the many low-priced Japanese and German models to the very fine American design by Roberts shown by Argelane.

Those of most interest to enthusiasts were the newer Grundig offerings, including the TK32A at

49 gns. which now includes a switch to cut out the automatic recording level circuit this firm brought in with a flourish originally.

The "automatic" facility has also been added to the two lower priced models, Auto-2 and Auto-4, 25 and 27 gns ., of the Elizabethan range, in a determined effort to capture the "pop" market. Similar circuitry can be incorporated in the new Sound range of five machines on demand at no extra cost, we are informed.

Of the Elizabethan offerings the two attractive newcomers were the stereo models LZ511 and



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$5,00 p \mathrm{~F}$. $1 / 6$. Resistors-Ful Range 10 nhms. 10 Resistors-Full $t$ and $\frac{1}{6} \mathrm{~W} .3 \mathrm{~d} ., \mathrm{W}$, sh. (Midget type modern rating) 1 w, 6d., tW gd. Hi-Stab. $5 \% \frac{1}{2} W$. 1 W, 6d., 2 W . 100 obms-1 meg). Other values 8 d . $1 \% \frac{1}{d}, 1 / 6$, etc., etc.

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HANDBOOK. $2 / 6$. 48 hr . Aligntuent services, 7/6. P. \& P. 2/6.

TRIMMERS. Ceramio (Compression Type)-30pF, $50 \mathrm{pF}, 70 \mathrm{pF}, 9 \mathrm{~d} . ; 100 \mathrm{pF}$ $150 \mathrm{pF} 1 / 3 ; 250 \mathrm{pF}, 1 / 6 ; 600 \mathrm{pF}, 1 / 9$ PHILIP8. Bee Hive Type (conc. sir -2-8pF, 1/-; ENOBS-Modera Continental trpet Brown or I vory with Gold Ring;
$1^{*}$ dia., 9d, each: 13 , 1/- each: Brown or Ivory with Gold cenire $1^{2}$ dia., 10 d . each; $13^{2}$. $1 / 3$ each. LAKGE BELECTIÓNAVALAABLE: METAL RECTIFIERS, STC TypesRM1, $4 / 9 ; 1 \mathrm{RM2}, \mathrm{5/6:} \mathrm{RM3}, \mathrm{7/6;}$
RM4, 16/-; RMs, 21/-; RM4B, $17 / 6$.

TUB-ELECTROLYTICS-CAN 25/25v. 50/12v. 1/9: $8+8 / 450$ v. $4 / 6$ 50/50v. $100 / 125 v .2 /-32+32 / 275 \% .4 / 6$ $1 / 450 \mathrm{v} .4 / 350 \mathrm{v}$. 2/3; $50 / 50 / 350 \mathrm{v}$. $6 / 6$ $16+16 / 450 \mathrm{v} .5 / 6 ; 60 / 250 / 275 \mathrm{v} .12 / 6$
$32+32 / 450 \mathrm{v} .6 / 6 ; 100+200 / 275 \mathrm{v} .12 / 6$

## RECORD PLAYER

 CABINETS 59/6Contemporars otyle rexine corr. a ins. 51 in twotone maroon rexine covered cabinet In two-tone maroon and cream. Bize $15 \xi^{* *} \pi$ baffle board and Vinair iret sories includitig for all modern amplifiers and space available etc. Uncut record player mounting board $14 t^{\circ}$ x $12 t^{\prime \prime}$ gupplied.
2-VALVE 2 WATT AMPLIFIER EZ80 and Twin stage ECL82 with vol. and neg. feedback tone control. A.C. 200/200) with knobs, etc., ready wired to fit ahove cabinet. £2.17.6. P. \& P, 1/6. $7^{\prime \prime} \times 4^{*}$ speakerand trans., 22/- P. \& $P$. 2
COMPLETE R/PLAYER KIT. As ill. inc. BSR UA14 Unit. New Bargain Double wound mains Ttr, no live chassi

BONDACOUST Speaker Cabinat Acoustic Wadding (lin, thick approx.) 12in. wide, any length cut, $1 / 6 \mathrm{ft}$. $4 /-7 \mathrm{~d}$. TINN ED COPPER WIRE, $16-22 \mathrm{~g}$ 2/6 $\ddagger \mathrm{lb}$. ERSIN MULTICORE SOLDER. 6o/40 4 d . per yard. Cartons $2 / 6$ etc

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$4 / 6$, etc.
 3 ohm P.M. Speaker onlt required. Kiecomruended Quality speakere loin

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## $\forall$ alvo line-up ECC85, ECH8I, EF89,

 EABC80, EL84, EM81, EZ80. Three Waveband and Switched Gram positions. Med. 200-550 wi. Lon $1.000-3.000 \mathrm{mo}$. VHF/FM $80-95$ Mc/s, Phllips Continental Tunang Lusert with permeability turing on FM and consbined AM/PM IF tranntormera 400 ail colle. Latest circuitrs including output. sensitivity and reproduction fo very high standard. . Wasm,

 nazed glass dal $11 \frac{x}{} 3$ zin
Vertical pointer. Horizontal station namee Gold on brown Eackground. Alikned and tested ready for use $£ 13.10 .0$ Carr. \& Ins. $7 / 8$
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| $\begin{aligned} & \text { ACE AP631 } \\ & \text { ALBA } 2128 \\ & \text { DANSETTE Imperial } \end{aligned}$ | Player Unit <br> BSR UAIS <br> BSR UAI4 <br> BSR Transcription | RECORD <br> Price <br> $19 \frac{1}{2} \mathrm{gns}$. <br> 16 gns. <br> 30 gns. | AYERS <br> Notes <br> $7 \times 3 \frac{1}{2}$ in. L/S. 2 W o/0. <br> $7 \times 4$ in. L/S. <br> Separate tone controls. Diamond stylus. $9 \frac{1}{2} \times 5 \frac{1}{2}$ in. speaker. |
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| DECCA RP205 DEFIANT CPI | Garrard AT5 Garrard ATS | 32 gins. 38 gn. | $8 W$ push-pull amplifier. Detachable legs. <br> Deram stereo cartridge. $8 \times 5 \mathrm{in}$. speaker. <br> Part of Unit-plan, Consolette. Stereo facilities, less second |
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| FALCON Falcon | Garrard | $19 \mathrm{gns}$. | $7 \times 4$ in. speaker. |
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| LSTER-BRANDES KP03! | Garrard Autostim | $19 \frac{1}{\frac{1}{2}} \mathrm{gns}$. | Transistorised. $7 \times 3 \frac{1}{2} \mathrm{in}$. $L / / 5$. |
| ARPO32 ${ }^{\text {KPIPHONE }}$ | Garrard AT5 | 23i2 grs. | Transistorised. $7 \times 3 \frac{1}{2} \mathrm{in}$. L/S. |
| MUL.'HY A-Major A85iG | BSR UAIS | 24 gns. | Transistorised. Mic. input. |
| HMV $2010{ }^{\text {a-Major A8SIG }}$ | Garrard AT5 p <br> Garrard AT5 | $\begin{aligned} & 34 \mathrm{gns} \\ & 45 \mathrm{gns} \end{aligned}$ | 3 W push-pull. $8 \times 6$ in. L/S and 4 -in. tweeter. Sonntone head. |
| M 5205 |  |  | tweeter. |
| 5206 | BSRUAIS |  | $7{ }^{\text {¢ }} 4{ }^{4}$ in. speaker |
| RDIO Deejay | BSR UAI5 | $14 \mathrm{glis}$. | - |
| Stortime | BSR UAI5 | 17 gns . | Transistorised. |
| Starmaker <br> PYE Achoic | BSR UAI5 BSR UAI5 | $19 \mathrm{gns}$. | Transistorised. |
| Transistor Black Box REVELATION APIS | BSR 4-speed BSR UAIS | 69 gns. <br> 41 gns. <br> 28: g gh | Transistorised. Stereo. 6 loudspeakers. Bitteorfly head. SW each channel. <br> Transistorised version of popular range. <br> Impact cabinet. Stereo adapted. 6 W pep 2mp. $8 \times 5 \mathrm{in} . \mathrm{L} / \mathrm{S}$. |
| RIB | BSR UAI4 |  | separate ton <br> Styled to match RT18 tape recorder. |
| REGENTONE TP431 | Garrard Autoslim | $19 \frac{1}{2} \mathrm{gns}$. | Transistorised. |
| RGD RP231 | BSR UAIS | $23 \frac{1}{2} \mathrm{gns}$. | Transistorised. Separate tone controls. Pilot It. |
| RGD RP232 | Garrard Autoslım | 19, ${ }^{\text {a }}$ 2ns. | Transistorised. |
| STELLA 571A | Philips. 4-sp. | ${ }_{27}{ }^{2} \mathrm{~g}$ gns. | Traisistorised. |
| ULTRA 6004 | BSR UAIS | $15 \frac{1}{2} \mathrm{gns}$. | $2 \frac{1}{2} W$ output. $7 \times 4 \mathrm{in}$. $L / \mathrm{S}$. |

LZ507. The former is an Anglicised version of their very successful American export with 6 W output and two detachable speakers, while the latter is a fully transistorised mains model selling at only 49 gns . with three speeds and two recording level meters.

Fidelity again showed established models and added their nane to the list of those making a debut into stereo radiograms.

## Record Players

Transistorisation, with its attendant advantages of instant operation, cooler running and claimed greater dependability, as well as an obvious weight saving, makes the record player market again newsworthy.

It was pleasing to note one subsidiary feature of this trend-the smaller, cheaper mains transformer could now be fitted on all models requiring the low power consumption of the "solid state" circuit and, consequently, the dangerous a.c./d.c. chassis was much less in evidence.

Common features were the lront-facing speaker of generous proportions, more comprehensive tone control systems, provision of a tape socket (despite the strong copyright law against its use!) and input arrangements that allowed the record player to be employed as a straight-through amplifier, some makers fcaturing this as a speciality by also providing a microphone.

Lighter pick-ups, improved versions of the popular mechanisms and common provision of a stereo cartridge are to be found even in quite modest price brackets.

The new Thorn deck was nuch in evidence, heing incorporated in models by Ferguson, HMV, Marconi. Ultra and the Retra "Five-Star".

Kodak made news with a quadruple-play tape, type P400, made for portable battery tape recorters, on 3 in . spools (or $3 \frac{1}{4} \mathrm{in}$.) at $£ 113 \mathrm{~s}$. 6 d . and $£ 22 \mathrm{~s}$. for 600 ft and 800 ft respectivcly, giving a playing time for an 800 ft spool of 42 min . at $3 \frac{3}{4} \mathrm{in}$. scc .

One or two specialities made an impact ineluding the Pye Achoir. claimed to be the smallest truly stereo una quality performance. Sidemounted banks wi two-plus tweeter speakers bounce the sound from adjacent walls. The deck uses the "butterfly" pick-up now widely employed by this company which tracks at only two grams but has a floating action, enabling the stylus to keep its groove, even on a warped record or under sulden shock.

Several newcomers to this field were noted. Sound, the Tape Recorder (Electronies) people, had a record player on show, as did Perdio, better known for portable radios, Arnolds (Arts) Ltd., Sanders (Electronics) and Robuk.

Among those of particular interest outside Earls Court was a stereo portable, battery-powered record player with hi-fi stereo headphones by S. G. Brown, marketed by Lugton's. With the addition of haftle speakers in matching shoulder bags this three-speed player at 32 gns ., plus 7 gns . for the phones, makes a notable return to domestic entertainment for this firm.

## PART 3-TRANSISTOR VOLTAGE AMPLIFIERS

## Understanding SEMICONDUCTORS <br>  <br> BY LESLIE MOORE

CONTINUED FROM PAGE 666 OF THE NOVEMBER ISSUE

IVHE basic requirement of an amplifier is to make some electrical signal larger. The "voltage swing" or peak to peak voltage of the input signal should be known to enable the design of an amplifier. The frequency range of the input signal is also of great importance.
Input signals to transistor amplifiers are usually applied across the base-emitter terminals. The output is taken from the collector and emitter.

It was seen that the base current necessary to operate a transistor is in the order of microamps and a variation of a few $\mu \mathrm{A}$ base current produces a variation of mA collector current.

Consider the circuit in, Fig. 19-B1 and R in series provide the emitter-base voltage, $B 2$ and $R^{t}$ in series provide the collector-emitter voltage.


Fig. 19: Illustrating the principle of the transistor voltage amplifier.

Upon the application of a small alternating voltage signal across the base and emitter the collector current will also alternate. A rise of the input voltage will result in a decrease of collector current, a fall in input produces a collector current rise.
Assume the input signal voltage variation to be 0.1 V causing a collector current swing of, say 10 mA . A value of $500 \Omega$ for $\mathrm{R}^{1}$ would produce a voltage swing across $\mathrm{R}^{1}$ of $10 \mathrm{~mA} \times 500 \Omega=5 \mathrm{~V}$ by Ohm's law. This is the principle of the voltage amplifier.
There are several disadvantages, however, with the circuit in Fig. 19. and a more practical circuit is shown in Fig. 20. Only one battery is used in the oircuit and the base-emitter bias has been
achieved by the inclusion of two additional resistors and a capacitor.
The values of components may be obtained simply with the aid of the transistor static. characteristic curves and a knowledge of the current flow directions in the circuit. The current directions marked in Fig. 20 are those of hole conduction. $\mathrm{R}_{1}, \mathrm{R}_{2}, \mathrm{R}_{3}$ and C provide the baseemitter bias.


Fig. 20: Illustrating hole conduction in a $p-n-p$ transistor voltage amplifier.

To obtain the static value of collector current a "load line" must be drawn on the output characieristic curves.

The position of the load line depends on two factors:
(1) the value of supply voltage;
(2) the value of $\mathrm{R}^{1}$.

Two points, one on the Vce axis and the other on the Ic axis of the output characteristic graph provide sufficient information to allow the construction of the load line.
When no current flows through the transistor (cut off) no current will flow through $\mathrm{R}^{\prime}$ or through the emitter-resistor $\mathrm{R}_{3}$. therefore the value of Vce is equal to the supply voltage. This point can be plotted on the Vce axis when the collector current is equal to zero.

For maximum collector current flow the transistor will be virtually a short circuit so that the whole supply voltage will be seen across $\mathrm{R}^{2}$.
From Ohm's law, maximum value of current is given by $\frac{V_{s}}{R^{2}}$ amps.


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Fig. 21: Use of the load line for abtaining circuit parameters. The dotted line represents the power limitation curve set by the manufacturer.

A suitable working value of collector-emitter voltage is chosen (VT in Fig. 21), and hence a value of base current and collector current from use of the load line.

The voltage drop across $\mathrm{R}^{1}$ is calculated, again, by Ohm's law:

Voltage drop $=I_{c} \times R^{1}$ volts
$V_{T}$ is known
Therefore the voltage across $\mathrm{R}_{3}$

$$
=V s-\left[\left(1_{c} \times R^{1}\right)+V T\right]
$$

From the appropriate input characteristic curve for the transistor ( $\mathrm{I}_{\mathrm{b}}$ against $\mathrm{V}_{\mathrm{be}}$ ), a static value of $V_{\text {pe }}$ may be obtained.
The voltage drop across $R_{2}$ must then be the voltage drop across $R_{s}$ less $V_{b e}$
i.e. Voltage drop $=\left[\left(\mathrm{R}_{\mathrm{g}} \times\left[\mathrm{I}_{\mathrm{c}}+\mathrm{I}_{\mathrm{b}}\right]\right)-\mathrm{V}_{\mathrm{be}}\right]$.

By choice of a suitable value of $\Lambda_{L}$, a value of $R_{2}$ could then be calculated from:

$$
\left|\left(R_{3} \times\left[I_{c}+I_{b}\right]\right)-V_{b e}\right|
$$

$\mathrm{I}_{\mathrm{L}}$

The voltage across $R_{1}$ is the difference between the supply voltage and the voltage across $\cdot \mathrm{R}_{2}$. A value of $I_{L}$ has been chosen. a value for $I_{b}$ is taken from the load line and hence $\mathrm{R}_{1}$ can also be calculated by Ohm's law.

It is important that the input signal neither saturates nor cuts off the transistor.

Some of the design points of a transistor amplifier have now been dealt with, but frequency range, which has only been brieffy mentioned, can be the most important consideration

The collector and emitter of a transistor themselves act as a capacitor, the value is extremely small but sufficiently large to limit a transistor's working frequency.

The required working frequency range of an amplifier is important as the gain of an amplifier varies with frequency due to a number of factors. These include frequency response of the transistor used. choice of components and type of inter-stage coupling.

An amplifier may consist of more than one transistor stage; Fig. 22 shows the circuit diagram for a typical two stage amplifier using $\mathrm{R}-\mathrm{C}$ coupling.


Fig. 22: A two-stage transistor voltage amplifier.

Capacitor $C$ blocks any d.c. levels on the collector Trl from the base of $\operatorname{Tr} 2$ but allows an alternating signal to be passed on.

Capacitors oppose the flow of alternating currents to a certain amount, the amount of opposition depending on the frequency applied and the value of capacitance of the capacitor. Opposition of this kind is known as capacitive reactance.

Considering the first transistor stage of Fig. 22 we know that its output resistance can be large. Opposition to both a.c. and d.c. is known as impedance. The output impedance will also be large.

The input impedance of a common emitter transistor is small compared with its output impedance.

With reference to Fig. 22, if the first stage amplifies a signal with a factor of 40 (i.e., a gain of 40 ) and the second stage has a gain of 40 . the overall gain of both amplifier stages will be:
$40 \times 40=1600$
The second stage appears as a low impedance to the first, but the first stage has a high output impedance. The total effect is for the internal impedance of the source to "drop" a greater pioportion of the output signal than is desired, the actual output being less than the theoretical value of 40 times the input value. The overall gain of the amplifier would effectively be less due to the " missmatch" of impedances.

A circuit with a considerably higher input impedance than the grounded emitter amplifier and a much lower output impedance could be included between the two amplifier stages to nullify the effect of missmatched impedances. The "emitter follower" is suitable for this purpose.
In Fig. 23, $R_{1}, R_{2}, R_{3}$ and $C$ supply the Vbe bias.

If the base were to go positive with respect to Vbe. the current in the collector becomes smaller or the transistor appears to have a larger resistance. A greater proportion of the supply voltage is dropped across the transistor thus making the emitter go more positive.

Conversely, if the base were to go negative with respect to Vbe, the emitter would go more negative.

Fig. 23: Common-emitter circuit diagram.


The gain of this circuit is slightly less than unity but the output voltage remains more or less constant for whatever load is applied to it providing the current being drawn is allowing the transistor to work within its power limitations.

We have then a method of providing a method of amplifier stage impedance matching.

It is often desirable to have a reasonable power output from an amplifier. Unfortunately the characteristics and limitations of the more inexpensive transistors do not allow a large power dissipation. Power transistors are expensive and require a high static current.

An amplifier known as a "push-pull" amplifier is very of ten used to overcome such difficulties. The circuit diagram is in Fig. 24.


Fig. 24: The push-pull transistor amplifier.

To direct current the windings of the transformers are virtually short circuits. $R_{1}, R_{2}$ and $R_{3}$ aci as biassing resistors for both Tr 1 and Tr 2 .

Across the secondary windings of T 1 the positive and negative half cycles of the signal would alternatively act in opposite directions. Tr1 will amplify one half of the cycle, Tr2 will amplify the second. T2 operates in the opposite mannet to T1 and an amplified output is obtained.

## PHOTOCONDUCTORS

will serve as an over-ride switch, cutting out the photo-cell control and converting from automatic to manual operation.

Alternatively both starting and over-riding may be done electrically by fitting an over-ride switch as shown in the diagram. Switching this on momentarily locks in the relay at night. and leaving it on cuts out the automatic control: in some cars the parking-light switch position already provided may be used in this way.

The same considerations about construction and mounting applied to the previous switch also apply to this.

## Light Operated Switches in General

The circuits so far described have obvious applications not only to parking light switches but also to automatic shop display-lighting switches, simple burglar alarm systems, automatic counters etc. The following notes will help the reader to modify the previous circuitry to his specific requirements.

In counters and alarms speed of operation is essential since the light beam may be broken for only a fraction of a second. The K 42 cells do not change their resistance instantaneously when the illumination changes but have a time constant of about one tenth of a second. Thus the relay used must be sensitive and of the high-speed type.

In burglar alarm systems the alarm once set off by the breaking of a light-beam must continue to sound even when the beam is made again. Thus the single-shot working in which the relay cuts off its own power supply is essential; this also ensures that the alarm sounds if the power supply to the relay fails.

When controlling shop-lighting or any other high-power system it is essential to have heavy duty contacts on the relay. The light-contacts commonly found on P.O. relays rapidly deteriorate when used to switch high voltage and power.

There are cadmium sulphide photo-conductive cells which will operate a.c. relays direct from the mains, but these are larger and more expensive and the K42 will not do so. Some d.c. power supply must always be provided, either batteries or rectified a.c. The latter need not be wellsmoothed. and a simple power supply to drive 12 V relays is shown in Fig. 9.

The reader will notice that so far no provision has been made in the circuitry for adjustment of the sensitivity of the K42 control circuits. This is because optical adjustment by means of masks over the K42 is far easier, less wasteful of power and more reliable than electrical control.

The sensitivity of the K42 is proportional to the sensitive area exposed to light, and by placing masks over the glass window the sensitivity may easily be controlled.
Any opaque material may be used for masking and the writer has found black p.v.c. tape most useful. To make the K42 sensitive to light from one direction only it may be placed at the end of an opaque tube facing in that direction.

Part 2 next month

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#### Abstract

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# BOOKS RE  RWED 

TSTEREOPHONY, by N. V. Franssen. Published by Philips Technical Library and distributed in the U.K. and Eire by the Cleaver Hume Press Led. $86 \mathrm{pp} ., 6 \mathrm{in} . \mathrm{x}$ 9in., 64 illustrations. Price 21 s. HIS book is rather different from most on the subject. It concerns itself mainly with the actual mechanism of hearing and offers many theories on this.

I found the book in no way practical, and rather heavy going, somewhat reminiscent of certain textbooks on psychology.

For the expert or someone who wants another facet of stereophony to examine then this is undoubtedly the book. If however, you are practically minded, or if you like your theory complete with diagrams and circuit values then it is not possible to recommend this volume to you.

The inside front cover assured me that certain principles would be made clear in a very readable and non-technical manner. Yet before I had gone 12 pages I was beseiged by 14 graphs, informed that.
$\Delta t=0 \cdot 24(a+\operatorname{Sin} a)$ and also that $\psi(\Delta L, \Delta t)=$ $\psi(0, \Delta t)+\psi(\Delta L, 0)$
There are only three chapters excluding the introduction and two appendix. To give an idea of the theme, chapter two is headed "The Faculty of Auditory Perspective", and is divided into various headings such as " The theory of intensity ratios ": " The theory of difference in timbre "; "Binatural frequency analysis" etc.

As may be judged by the above, the book is theoretical and somewhat specialised in its outlook. The curious will probably enjoy a browse through such a work, and the knowledgeable might perhaps find interest in the various theories contained therein. To the layman, beginner. and average radio enthusiast however, it is doubtful of there will be much of value offered by this book-D.J.G.

## ㅍ WIRELESS FOR BEGINNERS, by C. L. Bolx. <br> Published by George G. Harrap \& Co. Led. <br> 232 pp., 7 łin. $\times$ Sin., boards. Price 18 s .

ARE you a newcomer to the world of wireless? Do you come into the category of a novice? Would you like to read a book which will enlighten you without boring you?

If the answer is "yes" to these three questions, and your bank balance stands at 18 s . or more, then purchase of the above book is recommended.

Everyone. no matter how clever, must always at some time or another have been a beginner. Intelligent reading of technical journals helps in the education of a particular subject, but the author of a technical magazine must, of necessity, limit his contribution to reasonable dimensions and omit many obvious points. Obvious to him and to more knowledgeable readers, but not to the poor novice. The reading of a good basic book, therefore, is a decided asset. In Wireless for Beginners a great number of the basic facts are presented in an easily digested form.

A criticism of the book would be that one or two statements in it are dogmatically alarming if not actually untrue. This is mentioned an all fairness to any beginner buying a copy after reading this review. One sentence on page 104 states that "Valve triode detectors are now never used at all". This is not strictly true as readers of Practical Wireless will know! Again, page 172 -speaking in terms of $3-30 \mathrm{Mc} / \mathrm{s}$ the author says a station in Edinburgh would probably not produce any signal which could be picked up in London, yet the working of Scottish stations by London amateurs between 3 and $30 \mathrm{Mc} / \mathrm{s}$ is quite common.

One haffling part of the book is a sentence on page 174 which leads us to believe that f.m. is useless unless a limiter is used, and five pages further on assures us that a ratio detector can give good results without a limiter.

Other than these few small points, the book would appear to be a good "buy" from a beginner's point of view. especially to those who prefer "easy" reading.-B.S.A.

EADIO SERVICING MADE EASY, by Leonard C. Lane.
Two volumes. Published by Gernsback Library Inc.

## Two volumes. Published by Gernsback Library Inc. <br> 191 pp . each volume, $8 \frac{1}{2} \mathrm{in} . \times 5 \frac{1}{2} \mathrm{in}$. Price 20 s . each

11IRST impression to be gleaned from a reading of these two volumes is that the " $C$ " in the middle of the author's name stands for "Chatty". In a free and easy manner that must be envied by the British technical writer, accustomed 10 qqueezing quarts of information into his publisher's pint pot. Mr. Lane spreads himself over and around his subject, omitting nothing.

Some indication of his confident approach can he given by a quote: ". .. you'll be able to look anv radio set right in the face and say: See here. No nonsense out of you or else . . !'"

The irony of this is that, provided the reader can stomach the brashness, a real, working knowledge of radio sets, their circuitry and the servicing procedure that can unravel their faults, \& contained in these twelve chapters.

Mr. Lane begins with transistors, the first chapter explaining the semi-conductors and their characteristics, with a venture into basic circuitry. while the second chapter goes into printed circuit boards and transistor testing. Only after sixty pages do we meet the question of servicing techniques. This book is worth buying for this chapter alone, and for the trouble-shooting charts, a feature of several transatlantic books that has been slow to catch on in this country.

Chapters 4 and 5 deal with auto-radios, ending with a few pages on the troubles that can crop up from the mechanical and electrical systems of the car itself. Chapter 6 takes us into Volume 2, and to a.m. receivers, valve-operated, that is. Next, we
meet f.m. sets, then a.m.-f.m. tuners, and so to the " good ". stuff, to use the author's phraseology-the communications receiver.

Chapter 10 goes even further, dealing with marine receivers, while the mobile systems that are coming into more regular use are discussed in the next few pages. The final chapter covers miscellaneous receivers and a few special circuits.

At the end of each chapter a list of questions is given. These are carefully chosen-even provocatively chosen-to test the reader's attention to the foregoing text. These, in conjunction with the trouble-shooting charts, would be of help to the reader who wishes to use a work of this nature as a reference book. The comprehensive index at the end of each volume is also a helpful point. Despite a few insultingly childish illustrations, the drawings and photographs that are generously scattered throughout these pages do much to underline the author's points.
Given a tolerance of the patronising air which assumes the reader knows nothing, and an ability to discount some shocking doggerel and worse naivety, the casual reader might profit from these volumes. Whether he would be able to "jump right in with both feet", and earn a living by servicing radio receivers is another matter entirely. -H.W.H.

THOW TO READ SCHEMATIC DIAGRAMS, by Donald E. Herrington. Published by W. Foulsham \& Co. Ltd. 128 pp., 6 in. $\times$ 9in. Price 18 s. HE art of mastering the languages of different countries is practised by many people and these are usually referred to as linguists. A person referred to as a radio, wireless or electronics enthusiast also has to master a language-that of circuit diagrams.
A good map reader can win or loose a motor rally and so too the electronics hobbyist can make very little headway in the field of radio until he can "read" circuits.

If you are unable to follow circuit diagrams or are floundering then you can be saved! Mr Donald Herrington has thrown you a life-belt labelled "How to read schematic Diagrams".

Each chapter is not content merely to show a component and the symbol for it, but describes its construction, function and use. There are numerous photographs of the different components which will assist in identifying the actual article, together with many symbols of the same component which are likely to be encountered.

One small point is that there is a photograph on page 40, Fig. 4.1., which depicts two coils wound, according to the text, on phenolic coil formers. These are referred to as "air cored coils". To me an air cored coil is one which is self supporting, i.e. the core is air. The text states " as long as this form is not capable of being magnetized, the effect is the same as if no form were employed.
However, there assuredly is a difference, especially on short waves between winding a receiver or v.f.o. coil on cardboard and the same coil wound on ceramic.
The book is completely successful in accomplishing what it sets out to do-teach how to read schematic diagrams, and can be confidently
recommended at the reasonable price asked.L.S.A.

## ELECTRONICS DATA HANDBOOK, by Martin Clifford. <br> Published by Gernsback Library Inc. <br> 158 pp., $8 \frac{1}{2} \mathrm{in} . \times 5 \frac{1}{2} \mathrm{in}$. Price 23 s .

THE formulas which form the basis of this book are many, and all of course, in some way relate to the subject of electronics. Now this might lead the average reader to expect a formidable mass of unintelligible equations with meaning only to an Oxford don. This is not the case however, as most of the formulas are arranged to follow on from one another in logical sequence with explanatory text between each. More than this, the author illustrates how formulas or groups of formulas are used to solve various problems.
For the serious amateur radio enthusiast then, this work of reference will be of use, for even the simplest circuit is subject to the basic laws which can also govern the operation of a computer.
Grouped under appropriate headings, formulas are easy to locate with complete information, lacking only practical examples which would have helped considerably in clarifying the equations.
In his introduction, the author says "A knowledge of elementary algebra and trigonometry and some skill in handling algebraic functions will be of considerable help." This recommendation should not deter the non-mathematical reader however, as there are several important chapters dealing with nothing much more complicated than impedance calculations. But Mr. Clifford is perhaps being optimistic if he expects an elementary knowledge to carry the reader through the higher maths which appear towards the end of the book.

Besides the numerous formulas the book includes a host of tables and useful information which will be found, for once, really useful, its presentation being clear and complete and not the usual jumble appended to many technical publications.

With the warning that this is an American publication (which of course means language difficulties) it must be considered a valuable library addition, containing facts and figures in one volume which would only otherwise be found scattered throughout a host of electronics text-books.-P.R.R.

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## a <br> BAND II Preamplifier

for a boosted f.m. signal

by J. D. Benson



Fig. I: The single-transistor preamplifier circuit.


Fig. 2: The main wiring diagram.

TWE experimenter tho is in search of high-qua-ity reproduction must invar ably turn to the BBC f.m. transmission on Band II. The medium and longwave stations with their very restricted bandwidth leave much to be desired even with: the best of ecuipment. One of the stumbling blocks in the reception of f.m. is the fact that, if good reception is to be enjoyed, it is necessary to seed the receiver from an efficient aerial system. The answer to this problem is obviously an outdoor aeriad, but, this in itself raises a problem, as most chimney stacks are already festooned with TV aerials and any addition greatly increases the risk of collapse during stormy weather, A strong signal is necessary in order to reduce the signal-to-noise ratio so that reception is free from man-made interference and the annoying background which a weak sigal produces. The problem may seem insurmountable, but fortunately it can be overcome by amplifying the signal before it is fed into the receiver.

## Positioning the Aerial

In most houses access to the roof is possible, and it is then quite easy to install an aerial of either professional or homemade construction. In positioning a roof aerial, care should be taken that it is located away from water tanks or any piping that may be there. The preamplifier which is about to be described can be fitted adjacent to the aerial and its power supply fed through the down-lead cable. The amplifier is designed around the AFll4 Mullard transistor, hut any other similar transistor can be used. nrovided it is of first-class aualits. an inferior transistor will add to the background noise and ruin reception.

## Amplifier Construction

In construction, the amplifier is straightforward, provided the design is adhered to, and good quality components used throughout. The chassis is a simple Lshape, and is preferably made of


Fig. 3: Details of the screen.
copper. A screen is fitted which provides rigidity and also serves as a holder for the transistor. The shortest possible connections should be made throughout, especially to the transistor and, here a word of caution, a heat shunt-a pair of longnosed pliers-must be used when making the transistor joints or it may be ruined. It will he noted that both aerial and output coils are tapped. The coils should be wound and made a tight fit on the formers and then cemented in position to prevent any change in inductance by movement or vibration. When thoroughly dry, the enamel can be carefully removed from the wire with a sharppointed knife and the tapping soldered on. In the case of the output coil. a little experimenting is called for to find the best position for the tap. Starting from the collector end of the coil. a point will be found where the amplifier becomes unstable; this can be recognised by a sudden change in current, if a milliammeter is used, or by a rushing noise if connected to the receiver. When either of these conditions obtain, the tap should then be moved back towards the collector end until the circuit is stable. The tapping wire should be attached to a piece of nonconducting material to eliminate unwanted capacities whilst the best position is being found.

## COMPONENTS LIST

Resistors:

| Resistors: RI $1.8 \mathrm{k} \Omega$ | R3 | $68 \mathrm{k} \Omega$ | R4 $1 \mathrm{k} \Omega$ |
| :---: | :---: | :---: | :---: |
| All $\pm 10 \% \frac{1}{4} \mathrm{~W}$ carbon |  |  |  |
| Capacitors: |  |  |  |
| Cl 1000 pF | C5 | 20 pF |  |
| C2 20pF | C6 | 1000 pF |  |
| C3 1000 pF | C7 | 1000pF |  |
| C4 1000 pF | C8 | 1000pF |  |
| All ceramic. |  |  |  |

## Inductors:

Li 5 turns 22 s.w.g. enamelled copper wire, spaced by diameter of wire. Tap at one turn from Cl end.
L2 5 turns 22s.w.g. enamelled copper wire, spaced by diameter of wire. See text for tapping.

## Miscellaneous:

Trl AFll4 transistor.
Two 7 mm coil formers with cores (Alladin). Length of 22s.w.g. enamelled copper wire. Two battery connectors. Copper for chassis and screen. Springy brass for transistor clip. Four coaxial sockets.


Fig. 4: Details of the battery connector.
During the locating of the tap. the dust core should be screwed in until level with the top of the former. Tuning should be carried out from the output coil first and then peaked for maximum by tuning the aerial coil. returning to the output coil and so on. until hest results are obtained. A further refinement. an on/off switch. could be fitted to obviate the removal of aerial and receiver plugs each time the preamplifier is used. The total battery consumption is better than 2 mA .

## Outdoor Installation

If an outdoor aerial is to be used. then the preamplifier will be subjected to large changes in ambient temperature. from which the transistor must be protected in order to preserve the correct working conditions. The amplifier must be connected as close as possible to the aerial connection. A gain of $14-15 \mathrm{~dB}$ can be obtained from an amplifier of this type. The difference in reception with it is well worth the time and patience put into its construction. The battery connection fitting shown in Fig. 4 can be made to fit on top of the particular battery chosen and held in position by elastic bands.

## A MODEL CONTROL TRANSMITTER

-continued from page 746
fully unscrewed, the coil has too many turns A turn or so should then be removed, or turns should be spaced farther a part. Alternatively, if TC1 is screwed down to full capacity, without $27 \mathrm{Mc} / \mathrm{s}$ being reached. more turns are needed on the coil, or turns should be closer to each other.
For good range, a self-supporting vertical aerial about 8 ft .6 in . long. is satisfactory. If the receiver is sensitive. and maximum range not required, a shorter aerial can be fitted. For moderate range, a 3 ft to 5 ft aerial will often suffice. The aerial can be telescopic. or made from interlocking rods, or may be of wire. supported by a thin bamboo, or by an insulator and string to an overhead point.
Tuning is slightly modified by the aerial, so the transmitter must be re-adjusted with the wavemeter. after the aerial is fitted. When testing and tuning, the key or switch wired to the "key", terminals should be closed. or these terminals should be connected together with wire. Though the transmitter can be battery operated. it should not be overlooked that the cathode takes 20 seconds or so to heat up.

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$1.2 \cdot 5 \cdot-50-250$
$101 . v^{21} 12.500$ 3 50,
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 Remote contral suitch on cherophone Siveg trang wore nae wo the wape re-
corder, it also has a buit in ampilies aceser ior telepbone amplilleation. Alany other uses. It somes complete whb thurophotie pergonai exrplece
31L. Tape suare simot Bat
 (Fuly glitiateed).

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P. M. Aperc. blaze track omit in thith approx. on 200ft. tepe. Hatterieal U 亿1 PP3. Complete with crystal ruerophone. pe sous) ear phone, 200ft. taye and reet. spare soont carrytng strap and
batterles. Wonderfut value. At onit
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Moter Ringes: Curtert 0.20 V.D.C.
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 TUBE VOLTMETERFinest deaign rou stable and accurate meastureruent. $1 \%$ toleance on all resistors. Large design fin. 200 a metes tor accurate readings 11 weg Rang irp
 A.C.Y. $0.1 .5-\mathrm{i}-15-60 \cdot 1511-5100-1500 \mathrm{~V}$ Resistance: $10-1-4-4-14-40-14(1)-1400-4000$
30 A .10 mA
teristance $0-5 \mathrm{~K} \Omega-5000 \mathrm{k} \Omega-5 \mathrm{M} \Omega$. $150 \mathrm{DF}-0.12 \mathrm{~L} \mu \mathrm{~F}$. D.B $-20 \Omega+20 \mathrm{~B}$ 2018 ziDB, The simplest and most below its true $\mathrm{E5.15.0}$


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Plin rematisabic wete! How dever tent instruments Fincted itio one wocket alat case which can be taiken wad ued any where.
Renztance Subsimuton $100 \Omega-1 \mathrm{KO}, 10 \mathrm{KO}$
 4. F. Stynat Weneraco Prevelucy Itra , Soub gemerator requenes 400 e/s Output $35 \mathrm{~m} / \mathrm{V}$ aphox D.O. and A.O Volls. 4 ralgee $0-15-50-150-560$ voits at 4000 O.P.V.


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Complete with Teet Erode atad Batten 58.19.6 each.


Die cast, hand shaped body. Speciar offer $15 / \mathrm{B}$ ping P. \& P. 2/6,
MULTI METER BARGAIN. Model TK20A
1000 O.S.V. ou roth A.L. and D.L. A.L. aud D.C. volle wh



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Output 200 mW . Low aud bigh gain Wonderful vakue $31 / 6$ P. \& P. Wonderful vatue $\mathbf{3 1 / 6}$ P. \& $\mathbf{P}$. Compiete with overatiog limatructiona A GENUINE 4 AMP BAT. TERY CHARGER for Only 45/. P \& P. 4/5


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P/ug. puot 50 V . Pug. Cun 50V. Maine Selactor Plugplete with mitins lead charging lead and creronile cills.
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Fulty trainsistorised $\mathrm{Ni}=\mathrm{e}$ a $\times 2 \frac{2}{4} \times 1 \mathrm{in}$. batt. Push to call on uib ot ation. P.P. 3 to taik on master and polume cantion Our Price $55 / 6$ P. \& F

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## TRADE NEWS •TRADE news • trade news TRADE NEWS •TRADE NEWS • TRADE NEWS

## Mains Unit for Transistor Radios and Amplifiers

IROM RCS Products L.t., comes a range of battery eliminators suitable for almost any transistor radio, battery record player, amplifier etc. All these mains units are completely isolated from the mains by a double wound mains transformer giving the highest safety factor.

Also available at 35 s . retail is an eliminator for BBC-2 625-line booster units requiring a 12 V or 18 V d.c. supply. The eliminators are available with either a single or double d.c. output.

The range is as follows: single outnut units, $4.5 \mathrm{~V}, 6 \mathrm{~V}$ and 9 V, at 29 s . 6d. retail and the size, $2 \frac{1}{2} i n . x$ in. $x$ itin.: iwo separate output units, $4.5 \mathrm{~V}+4.5 \mathrm{~V}, 6 \mathrm{~V}+6 \mathrm{~V}, 9 \mathrm{~V}+9 \mathrm{~V}$, all at 42 s .6 d . retail, all 3 in . x 3 in . x 2 in .

The makers claim that these units are the cheapest of their kind, available with double wound mains transformers, currently available on the British market. Messrs RCS Products (Radio) Lid., Il Oliver Road, Walthamstow, London, E.I7.


One of the battery eliminators available from R.C.S Products Ltd.

## Electrician's Tools

WROM the Continent come four new servicing aids. Griptou is a three-pronged trigger-operated gripping tool. It is 285 mm long and the prongs open to 10 mm ; this makes the instrument particularly suitable for placing or retrieving objects in inaccessible places. The handle and trigger are of plastic, and the arm, which is flexible is made of polyamide. The powerful action of the return spring enables this tool to lift objects of up to $4 \frac{1}{2}$ lbs.

Dynatest is a mains circuit tester incorporating a pilot light inside the handle. It is rated for
voltages of $120 / 220$, and insulated to 10.000 V .
Pick-fil is a brass pointed contact tester fo: printed circuit work. insulated to 10.000 V . It can be supplied with a flexible extension lead. insulated for h.t. work to fit all standard testing apparatus. This lead can also be used with the Dynatest.

A rubber-headed mallet-a flexible, well insulated tube with a snall rubber head-can be used by an electrician to locate faults with a gentle tap. Henri Picard \& Frere Lid., 34-35 Furnival Sirees, London, E.C.4.

## Grampian Cardioid Microphone

1)EVELOPED for users to whom oyercoming background noise and acoustic feedoack is a serious problem, the Cardioid Microphone type (GC. 1 is useful for many kinds of p.a. work.

As its name implies, this microphore has a heart-shaped polar response pattern with a front-to-back discrimination of approximately 15 to 20 db over the mid-frequency range. The effective response of the GC. 1 extends from $40 \mathrm{c} / \mathrm{s}$ to $12 \mathrm{kc} / \mathrm{s}$ with a gradually rising tilt towards the higher frequencies.

The non-metallic diaphragm is protected by a perforated steel plate, is non-hygroscopic and is resistant to temperature changes. corrosion and acoustic and mechanical shock.
The new Cardioid microphone developed by Grampian Reproducers Ltd. to overcome background noise and acoustic feedback.

The alloy casing of this unit is fininhed in Old Silver Polyurethane enamel and a Melamie primer and is fitled with a chrome plated bezel ring. The microphone is less than 6in. long and weighs less than 120zs.


Cardioid microphones are available in four impedances from $25 \Omega$ to $50 \mathrm{k} \Omega$ and are supplied complete with swivel holder, connector and detachable 18 ft length of screened lead. Grampian Reproduceps Lid., Humworth Trading Estate, Felham, Middiesex.

## Antex Lightweight Soidering Iron

${ }^{\prime}$ THE lastest addition to the Antex range of soldering irons is model C240N. It is fitted with Ferraclad"-the new type bit which is clamed to last at least five times longer ihan ordinary nickel plated bits. The construction of the iron makes the bit instantly interchangeable, and with a low leakage current all risk of damage to transistors when soldering is virtually eliminated. Antex Lid., Grosvenor House, Croydon, Surrey.


The latest Antex soldering iron, model C240N.

## Regulated Power Supply

FROM K.L.B. comes the P. 300 regulated power supply, with facilities for working on either conventional valve circuitry where it will provide $0-400 \mathrm{~V}$ d.c. at up to 150 mA or $0-50 \mathrm{~V}$ d.c. for operating transistor equipment. Two meters are incorporated which offer comprehensive monitoring of both voltage and current. In addition, the P. 300 provides the usual heater voltages and a low current negative bias supply. The K.L.B. P. 300 is priced at $£ 47$. K.L.B. Electric Limited, Whitehorse Road, Croydon. Surrey.

K.L.B.s P. 300 regulated power supply unit.


The new Sinclair IOW transistor amplifier, available in kit form or ready-assembled.

## 10W Transistor Amplifier

A NNOUNCED by Sinclair Radionics Ltd., is
their 10 W integrated amplifier. This amplifier uses the pulse-width modulation principle. permitting a large reduction in the power dissipation in the output transistors. so that no heat sink is required and small high frequency transistors can be used in place of the conventional l.f. power transistors.

The circuit embodies 11 transistors and has a transformerless output feeding into a $15 \Omega$ speaker.

The overall size of the " $\mathrm{X}-10$ " unit is 6 in . x 3 in $x \frac{3}{4} \mathrm{in}$., and its weight is less than 5 ounces. The price is $£ 519 \mathrm{~s}$. 6 d . in component form, or ${ }^{6} 619 \mathrm{~s}$. 6 d . built and tested.
A mains power pack, providing 12 V is available at a price of $£ 2$ 14s. Technical Suppliers Ltd., (sole distributors) Hudson House, 63 Goldhawk Road, London, W.12.

Baltimore district and has the rig on board complete with a five element beam (honest it's the truth).
Top band addicts please note the M.C.C. run by the Short Wave Magazine takes place this year on the weekend 14 th and 15 th November. There are two four-hour periods from 17.00-21.00, one on each day.
H.F. enthusiasts might like to be reminded of the $21 / 28 \mathrm{Mc} / \mathrm{s}$ telephony contest on December 5th and 6th. Just gives you time to make up that ground-plane referred to earlier?
Incidentally, if you hear a Cyprus station (call sign 5B4), from now on it will either be a pirate or an illegal transmission anyway as all 5B4 licences have been suddenly and mysteriously withdrawn for some strange reason not yet made clear.
I would be very pleased to hear from any reader who listens or works the amateur bands 1.8$30 \mathrm{Mc} / \mathrm{s}$, just address to G3JDG, Amateur Band DX, c/o Practical Wireless, Tower House, Southampton Street, London, W.C. 2.

That just about wraps it up for this month, time to hang up the headphones and go Q.R.T. to B.E.D. . . . well perbaps just a quick listen round on forty, perhaps that $9 \mathrm{M} 2 \ldots$ !

Items of general interest gleaned over the past month include the gen. that there are two DXpeditions afoot: VQ8AMR on Rodriguez island and PY1CK on Trinade 1sland. But if you really want something unique to listen for, search on 2 m for the call-sign K 2 QHZ , he drives a tractor in the

## ON THE SHORT WAVES

-continued from page 765
the only non-G heard so far was a UT5. However this was with a 20 m dipole with the feeders strapped.
A thought for those wishing to try 10 m and haven't much space for elaborate antennas is that a ground-plane is quite a compact aerial for this band and also is omni-directional.

Another point of interest for those learring or wishing to learn morse is a special slow morse transmission ( $3-4$ w.p.m. up) between 28.100 and 28,300 by G3JDG (St Albans) on Sundays at 11.00 (120W to a dipole running NW/SE).

## GENERAL NEWS

## KEEP AN EYE ON THE FUTURE WITH PRACTICAL TELEVISION

The December issue of "Practical Television" speculates on the future of TV Receivers and reviews the situation of Indoor Aerials today.

The December issue of P.TV is on sale 20th November.

Don't Miss These Bargains
Tranaistor ferrite rod aerial with medium und long wave coils with circuit, $7 / 8$, Oscillator Coil and set of 3 I.F. transformers for tramistor sel with circuit, $12 / 6$.
trinuterag $g /$ enser to sult. alresplated with
Ditto but 4ub. inan. 7 mm . $10 /$ - the set; two gang comithiscra to sumt, 8/6. (hequest sub.

Midget 3in. P.M. Loudspeaker 3 ohu 12/6. 80 ohm 13/6.
Midget $208 \mathrm{pF}+176 \mathrm{pF}$ two-gang Tuning coludanser with trimmers for transistor set Price $9 /-$
Push-Pull Transformer. Bub-biniature $\mathrm{s} / \mathrm{C}$. 0005 mfd . Single Tuning Condenser. Solia dielextric din. apindile for trinisistor ar Crystal set. with spibile tapjed in 13A, $2 / 6$.
46 Sets (Heceiver/Transmittel pack set) 46 Sets (Heceiver/Transmitter pack setl. Unumed sets complete excrpt fol crystals. fiward with parte and lasmis rebuidable into other gear. $19 / 6$ each. Fost $3 /$.
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.5 tht 500 v .
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.05 mf 501 v .
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.002 dif $1.000{ }^{5}$
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.02 mf 750 y. $.01 \mathrm{mf} 1 . \mathrm{bu} \mathrm{v} \quad . \quad . \quad . \quad 8 / 6$ doz. Battery Charger Recticer-aelenium 10/-doz $5 \mathrm{amp} .9 / 6$.
Metal Chassis-punched for Mullard 510 Auplitier, romplete with Inner screening Filament Transformer. 6.3 v . I $\frac{1}{\frac{1}{2}}$ ampus., $8 / 6$.
Find Filament Transformer. ©.3 v. If amps., $6 / 6$.
Neon Lamp-Iuidpet wire ented. IJeal mains Neon Lamp-ruidget wre ented. I Jed mains
tegtor, fetc. $2 /-$. Fi, Goft, $1 / 6$. Phillips Trimis. $1 / 6$
Philips Trimmers- $-3.30 / 1 \mathrm{~F}$ 1/- ea., $9 /=$ doz. Tag Panela. Nuea! for constructors experimental circuite, etc. 3 of each of 12 dillerent 6.jors. 5/

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Motal Rectiler. 250 \%. 60 - 80 milliampa inleal for madis get or inst curuent or to replace that expensive valve, $4 / 6$.
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Piano Key Type Switohes. 3 key type $3 /-$ 1 key type $3 / 8,5$ key twpe 4/8, poot and pack 500 M W Amplifiter of number ordered. 600 MW Amplifler. Uses 3 trankistors. 2 of Whach are in Glass B pustipull for lattery econding. Ideal little unit ior baby alarma enord player, intercom. ete. etc, 19/6 peaker 12/6 extra
Electrolytio Condenser-Bargain.
utndature type 50 m.f.d. fiv, raade by T.c.c /8 per tozen (momitumu quantity supplied) Tranaintor get Cases. kinished it twotone With handle and back. Blze $102 \times$ if $x$ is
$15 /-$ emeh phis $2 / 6$ Carriage and Inamance.

## THERMOSTATS

TYpe 'A' 15 amp. for cont rontiog roum beaters, greenhouse. aimas cuphoard. Has apinile for $80^{\circ} \mathrm{F}, 9 / 6$ phas $1 /-$ post. Wultabie box tor wat munatiag, $5 /-, F$ and $P 1 /-$
Type ' $B$ ' 15 amp . This is a 17 it . long rod type tnade by the famous Sunvic Co. spladle adalters the setung so this could be adjuatable over $30^{\circ}$ to $1,000^{\circ} \mathrm{F}$. Butable for controling rurnace, oven, kith. immersion heater or to make tarme-gtat or the aiarm. 8/6 plus 2/6 post and insurance.
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Where postage is not definitely stated add 2/all orders under 43 .

## Good Companion

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## OUR BARGAIN OF THE YEAR

 A complete kit of parts to build transistor 2 wave superhet receiver at only 39/6. Post \& Ins, 3/6
"CORONET" Mk. IV It fulty covers the mediutn wate hand shad that part of the long
waveband io bring in B.B.C. Wavebatad to bring in B. B.O


## THIS MONTH'S SNIP

### 45.10.0 Radio for only $37 / 6$

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components. Sensitivity 10 , components. Sensitivity 16,000 ohms pet volt A.C. and D.C. ranges B.e. voltage up to 1.2 kV in 5 rames. A.C. voltage uf two $1.2 \mathrm{k} V$ is ranges. D.C. chrrent up to 300 ma ranges. Resirtance up to 2 meg. Capacites . 015 to 15 mplit and decibels. Condplete with full instructous iall test prods and battery rem ohms ranme. A reas bargan not Price 69/6. Carriage and hasuratice Price 69/6. Carriage and Lusuratice

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heaters. lieal for tuth-
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## LIGHTOPERATED

## SWITCH

## BY <br> P. LISTER

THIS device can be constructed cheaply and easily. The circuit is of hybrid design, working the transistor in a difierent mannar from usual.

## Employing a Transistor

The prototype model was evolved to make use of an OC71 which had become chipped. the black paint heing partially removed. This transistor is still in use in the original.

Any general-purpose transistor will do, providing it is of glass construction.

The first thing to do is to remove any lightexchading paint. After this has been carefully scraped off, the transistor can be tested for general light-sensitivity by measuring its photo-e.m.f.. This is done by joining the collector and emitter and taking the junction to the negative terminal of a milimeter ( 1 mA f.s.d. is ideal) whislt the base is taken to the positive terminal. If the transistor is now heid near an clectric light bulb (40W) there should be a deflection of 1 mA or so. It will be found that the transistor is slightly more sensitive in some directions than others.

## The Circuit

For its operation, the circuit does not rely on the transistor's property of develnping a photoe.m.f., but on its photo-resistance property. The resistance between the emitter and collector varies with the light falling on the transistor, the greater the light, the lower the resistance.

Originally the idea was to apply the photo-c.m.f. to the grid of a valve. This was not practical however, as the eight of a volt or so would not givea great ennugh anode current change to operate an ordinary relay.

It was thus decided to use the photo-resistance property and to make this varying resistance the cathode resistance, this being used to make the cathode more or less positive. When dark the cathode is far enough positive. that with the grid earthed, this now negative potential is enough

## COMPONENTS LIST

VI EF73, EF72, EF91, EF50, Z77, etc.
TI Mains transformer to suit valve
Trl Almost any general-purpose transistor
RLA $4,000 \Omega$ to $5,000 \Omega$ relay
$\mathrm{Cl} \quad 8 \mu \mathrm{~F}$ electrolytic
Rc $150 \Omega$ see text
MRI Metal rectifier 15 mA
SI Mains on/off switch
almost to cut-off the anode current and so render the relay de-energised. When the resistance of the transistor decreases-with an increase in light--the negative grid voltage decreases until it is more or less equal to the voltage dropped across the included cathode resistor (Rc) can be varied to suit the valve or to vary the sensitivity. In the prototype an EF73 was used for V1 but any moderately high gain valve will do, e.g. EF72, EF91, EF50, 277.


Fig. I: The simple circuit of the device.

## The Device in Operation

The prototype operated from a 40 W lamp held at about 12. By the use of a lens and by experimenting to find the most sensitive spot on the transistor, this distance can be extended to several feet from a less powerful light source such as a torch.

A further refinement can be made by replacing the ordinary transistor with a photo-transistor, such as an OCP71 which has a built-in lens.

The power-pack can be any that will supply the required anode voltage and heater current; smoothing need not be great.

The uses of such a device are many, one of the most obvinus being to operate garage doors from car headlights.


ACTON, BRENTFORD AND CHISWICK RADIO CLUB Hon. Sec.: W. G. Dyer, G3GEH, 188 Gunnersbury Avenue, London, W.3.

Whin members meet at the Club headquarters on 10th November. chey will hear a talk given by G3IGM ontitled "Radio Test Gear".
BATH SPA RADIO CLUB
BATH SPA RAD.: W. Wynes G3TLV 14 Brook Road, East Twerton, Bath, Somerset
W, th the recent move to new headquarters, this Club is now able to welcome local short-wave enthusiasts and visitors to any of its meatings ac 7 Lambridge Mews, Larkhall, Bath. Meetings begin ar 3 pm . and are held every Monday and Thursday.
CHESTER AND DISTRICT AMATEUR RADIO SOCIETY
Hon. Sec.: P. Holland, Field House, 19 Kingsley Road, Gt. Boughton, Chester, Cheshire.

During October, members of this Society heard lectures at each of the three meetings.

The first was on 13th October, when H. Morriss (G3ATZ) gave lecture on "Antennae". This was followed a week later by G3OWY's talk on "Receiver Selectivity" and on 27th October, "Interference Decection" was the subject of the lecture.
"Interference Detection" was the subject of cLu
Hon. Sec.: C. J. Rourke, Gi3iVJ, 63 Kirkliston Park, Belfast 5, Northern Ireland.
This society's meetings are held every Wednesday and Saturday, beginning at $8 \mathrm{p} . \mathrm{m}$. Visitors and new members will always be welcomed at these meetings. At the meeting for 7th Oetober member at "RTTY" by W Kane (GI3GQB). NORTHERN HEIGHTS AMATEUR RADIO SOCIETY Hon. Sec.: A. Robinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.
After discussions and preparations on 14th October, a group from this Sociery manned a station (G3MVH) over the weekend of 17 -18th, during the Scout "Jamboree-on-the-Air".
Later in the month, on the 21 st, members of the Society and visitors to it enjoyed a recorded lecture by the famous American mateur WIBB on "DXing on 160 m .".
28th October was ragchew night and the 31st, a party made a visit to the International Radio Communieations Exhibition in London.
READING AMATEUR RADIO CLUB
Hon. Sec: R. G. Nash, G3EJA, "Peacehaven", 9 Holybrook Road, Reading, Berkshiro.
The October meeting of this Society was held on the 3lst, when the subjects under discussion were TVI and BCI.

## PREPARING FOR THE R.A.E.

See page 744

ANSWERS to Question 1 given in the first part. Refer to Fig. 9, page 631, last month.

1. First find the value of the parallel connected resistances. Let the $4 \Omega$ resistance be R1, and $2 \Omega$ be R2.

$$
R 1 \times R 2
$$

$$
\begin{aligned}
\mathrm{R} & =\frac{\mathrm{R}_{1+\mathrm{R} 2}^{4 \times 2}}{} \\
& =\frac{4+2}{4+2} \\
\mathrm{R} & =1.33 \Omega
\end{aligned}
$$

Total resistance in circuit will then be $1 \cdot 33+6$ $=7.33 \Omega$

$$
\begin{aligned}
\mathrm{E} & =10 \mathrm{~V}, \quad \mathrm{R}=7.33 \Omega . \\
\text { from } I & =\frac{\mathrm{R}}{\mathrm{R}} \\
I & =\frac{10}{7.33}
\end{aligned}
$$

Total current dwawn $=1.36 \mathrm{~A}$


SPEN VALLEY AMATEUR RADIO SOCIETY
Hon. Sec.: N. Pride, 100 Raikes Lane, Birstall, Leeds.
On 15th October, Spen Valley A.R.S. was host to a number of visitors from other radio societies, and then on the 28th, Spen Valley members were the guests of Northern Heights Amateur Radio Socialy.
The lecture given at the meeting for 29 th October was entited
"Radio Astronomy" and was delivered by W. J. Baggeley.
Activities for October ended with a visit by a group of members to the Radio Communications Exhibition.

## UXBRIDGE RADIO SOCIETY

1. Batten, 36 Collingwood Road, Hillingdon Heath, Middlesex.

After the activity of the 17 th and 18 th October when the club participated in "Jamboree-on-the.Air", a surplus sale was held on the 19th.

Current constructional projects include work on a club receiver and conversions on a transceiver to cover top band and 80 m .
WELLINGBOROUGH RADIO CLUB
Hon. Sec.: J. Baker, 34 Essex Road, Rushden, Northamptonshire.
The first meeting of October was the Annual General Metting, when the Club's affairs came under discussion.

The three following meetings were devoted to lectures given on the 15 th, 22 nd and 29 th. The subjects and lectures were, respectively, "Basic Radio Components" by D. Lyne. "The Radio Valve" by P. Butler and "The Transmitter and Receiver" by K. Knibs.

## WESSEX AMATEUR RADIO GROUP

Hon. Sec.i P. Cutler, G3MXF, 43 Langside Avenue, Wallisdown, Poole, Dorset.

The Group's participation in the Scout "Jamboree-on-the-Air" was the operation of a station at a site near Brownsta Castle.
WEST KENT AMATEUR RADIO SOCIETY
Hon. Sec.: H. F. Richards, 17 Reynolds Lane, Tunbridge Wells, Kent.

At the 9th October meeting, members were given a guide to the communications receivers on the market, with off-air demonstrations and performance tests for illustration.
23 rd October was "Audio Night" and two days later, a number of members visited the Decca Navigator Transmitting Station at East Hoathly.
2.
$\mathrm{E}=1.36 \times 6$
Voltage across the $6 \Omega$ resistance will therefore $=$ $8 \cdot 16 \mathrm{~V}$
3.

$$
\begin{aligned}
& I=1.36 A . \quad R=1.33 \Omega \\
& \text { From } W=I^{3} R \\
& W=1.36 \times 1.36 \times 1.33
\end{aligned}
$$

Power dissipated by R 1 and $\mathrm{R} 2=2.47 \mathrm{~W}$
4.

$$
\begin{aligned}
& E=10 V . \quad I=1 \\
& \text { From } W=E I \\
& W=10 \times 1.36
\end{aligned}
$$

$$
I=1 \cdot 36 \mathrm{~A} .
$$

Total power dissipated $=13.6 \mathrm{~W}$
5. First find voltage appearing across R1. Battery voltage $=10$. Voltage across the $6 \Omega$ resistance $=8 \cdot 16$. $\therefore$ voltage across $\mathrm{R} 1=10-8 \cdot 16$

$$
=1.84 \mathrm{~V}
$$

$$
\begin{aligned}
\mathrm{E}=1.84 \mathrm{~V} . & \mathrm{E}=4 \Omega . \\
\text { From } \mathrm{I} & =\frac{\mathrm{R}}{\mathrm{R}} \\
\mathrm{I} & =\frac{1.84}{4}
\end{aligned}
$$

Current flowing through $4 \Omega$ resistance $-0 \cdot 46 \mathrm{~A}$

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(Mono PU plug in head) B.S.R. UA15 (TC8 Mono PÜ) B.S.R. UA15
(TC8S Stereo/LP/78) ..

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## AMERICAN LITERATURE

SIR,-Having rcad (with great pleasure) many technical publications from the U.S.A. I really cannot agree with your correspondent James Goodwin (Octoher issue) that there is anything at all "difficult" in them.

Surely all your readers are aware that what we call a valve they refer to as a tube; our anode is their plate and earth becomes ground on the other side of the Atlantic, together with antema for aerial.

Most of these changes seem to me to he self-explanatory-like their " $A$ ". " B " and " C " voltages for the power supplies l.t., h.t. and g.b. (grid bias).

The only real stumbling-block is in following the circuit diagrams as 1 personally much prefer the European idea of keeping the h.t. line " at the top of the page ". However, the Yanks' method of keeping the power supplies at the bottom has one advantage-it is much easier to "follow" the a.c. signal through the circuit.

Talking of difficult circuit diagrams. how many readers have tried to unravel one in a French magazine-where the valves (or should I say tubes?) are all printed horizontally, probably the result of too much vin rouge?-D. Byrne, G3KPO (Peterborough).

SIR.-Whilst I cannot help hut endorse Mr. James Goodwin's praise of your book reviews in the October issue of Practical Wireless I must disagree with his criticism of American technical literature. I have read several books from the U.S.A. on radio and electronics and have experienced little or no difficulty in following the text. Anyone with a modicum of intelligence and common sense should be able to "interpret" all these terms in a few moments. Many are more descriptive than the corresponding term used in England-vacuum tube for valve, plate for anode. For those who do have any difficulty, some of the British editions of American books have forewords written especially for British readers.

As for the circuit diagranm and symbols, whilst hese look vastly different, on closer inspection the only real difference turns out to be the absence of a reference point in the form of a line repreenting chassis. Thus the whole diagram looks to se "falling apart".

The real difficulty is in obtaining American omponents in Britain at prices comparable with he British ones. Coils and transistors are the vorst in this respect. I have had to abandon

Whilst we are always pleased to assist readern with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercied or surplus equipment. We cannot supply alternative detaile for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OYER THE TELEPHONE. If a postal reply is required a itamped and addressed envelope must be enclosed with the coupon from page iii of the cover.
The Editor does not necessarily agree with the opinions expressed by his correspondents.
several interesting circuits because of the high cost or total unavailability of the suitable components.

No, it is not the theory which causes the trouble hut putting it into practice.-D. C. Brown (Leeds, Yorkshire).

## COILS FOR THE SPECTREUPHON

SIR.-With reference to the above article in the
October, 1964, issue of Practical Wireless, I should like to make the following comments: I found difficulty in obtaining the Denco coils suggested for use in the Euphon section of the unit. Having access to a commercial inductance bridge I wound the coils myself. the following being the details: 90 turns wound in twe layers each of 45 turns on a 1 din. diameter former with 18 s .w.g. enamelled copper wire give the required inductance. I constructed the Euphon section and the results were extremely satisfying. The unit adds more depth to a mono recording and gives the impression that one is in the same room as the recording artist. The balance control proved to be very critical to adjust and requires adjustment on each record. The latter disadvantage is offset, however, by the amazing performance of the unit.-D. Amyes (Hull, East Yorkshire).

## REGENERATIVE RECEIVERS

NIR,-With reference to the " High Compression Front End" P.W., September, 1964) by C. Leslie Thomson. "This small regenerative receiver is a hot little thing, one curious fact about the SB Transistor series and the MATs being that although the latter are, on the whole, considerably better performers, they are inferior to SBs in circuits like Mr. Thomson's.

I have had lots of fun with regenerative receivers and I thought your author might like to hear of someone else who has also devoted quite some tine (wasted, according to some!) to them.

In the 1961 Electronic Experimenters' Handbook there is a similar circuit by Alvin Mason. The transformer used in my circuit was the Ardente 1001.

In the Gernsback Series "Transistor Projects" there is an outstanding circuit by Edwin Bohr. This one uses an SB100, though others in the SB and MAT, series were tried and all performed upell. The advantage of this type of set is that the transformer is eliminated, though it is true that the size of an extra mercury cell is almost as much. Discounting in each circuit the usual tuning arrangements, Bohr's circuit has three resistors and no capacitors, as against Mr. Thomson's tive
resistors, three capacitors and an audio transformer (offset to some degree, it is agreed, by the absence of a second cell).

This little note on regenerative receivers would be very incomplete if mention were not made of what I have, so far, found to be the most extraordinary circuit, particularly in respect of audio quality. This is Wotton's " Amplified d.c. Transistor Receiver", described in P.W., February, 1961. Mr. Wotton's circuit is based on the original by Cleland in P.W., November, 1959, and merits the attention of all those interested in a really high quality receiver. I have built several versions and can honestly say that it is not overdifficult to build a sub-miniature set into a box smaller than the average matchbox. Naturally a mercury cell should be used.

Incidentally, replacing the first semiconductor with a MAT100 will, of course, improve the sensitivity, but there seems to be little point in doing so unless one likes to lie in bed at night and attempt to pull in some distant medium wave stations.

That this circuit is good has been testified by its inclusion in a well-known constructor's manual of transistor circuits. Apart from using different transistors the circuit, as far as I can see, is identical. The performance in so far as sensitivity and noise are concerned is better; but not because of circuit changes, rather component improve-ments.-H. A. L. Wagner (Kuala Lumpur, Malaya).

REQUESTS FOR INFORMATION ARE INSERTED IN THIS COLUMN ON THE UNDERSTANDING THAT READERS USING THE SERVICE UNDERTAKE TO |reply To ALl OfFERS RECEIVED AND TO RETURN ALL DATA NOT REQUIRED. BECAUSE OF THE LARGE NUMBER OF REQUESTS RECEIVED, ILLEGIBLE WRITNUMBER OF REQUESTS RECEI DISQUULIFY LETTERS ING WILL AUTOMATICALLYHE SAME REASON. WE FROM PUBLICATION. FOR THE SAME REASON PAST CANNOT GIVE SPACE TO REESES OPRACTICAL WIRELESS."

SIr-l would be grateful if any reader could sell or loan me . . .
. . . any details of the connections of an "Antinodal" coil covering i2-80m and manufactured by R.I. Limited.-J. M. Cranke, The Nook, 85 Castle Road. Newport, 1.O.W. Cranke, the circuit diagram tor the Marconi receiver CR 150 or CRisol $/ 2-\mathrm{H}$. Humphrics. The Old Vicarage, Gazeley, Newmarket, Suffolk.
... the manual and/or circuit diagram of the R1116A receiver.-A. D. Couchman, 3 Manor Grove, Sittingbourne, Kent.
. practical audio circuits using two 838 valves in push-(pull.-i.. ${ }^{\text {R. }}$. Reynolds, 11 Bridse Street, Stowmarket, Suffolk. portabie the circuit diagram and any other information on the Banastre Road, Southpori, Lancashire.
. the circuit and any other details of the receiver B.34.A. J. Harris, 74 Bodmin Road, Whitleigh, Plymouth. Devon. . . the blueprints for anything betwecn a $4+4$ and $10+10$ atereo transistor preamp. If required 1 will return data by regislered mail and refund M.C.R.U., R.A.A.F. Butterworth, Penang, Malaysia.
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Crecent, , the base connections and or any other information regarding the cathode ray tube type CV960.-Philip Bcet, 17 Firs Avenue, Alfreton, Derbyshire. . . a service sheet or instruction book for Ex-government
radio set No. 62 Mk. 2.-J. E. Pearce, 52 Cranford Lane. Heston, Middiesex.
the circuit of the Marconi HP112 transmitter/receiver, also the circuit of the 38 set.-W. Burke, 6 Belgrave Terrace, Glasgow W.2.
the handbook and circuit for the R107 receiver and also any details of modifications.一R. WILD, 140 Nansen Road, Ward End, Birmingham 8.
the circuit of the Dynaport No. 55 Radio.G. Wison, 62 Russell Road. Tottenham, London, N. 15.19 set Mark 3.-A. Sellwood, 151 Chestnut Drive South, Leigh. Lancashire.
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Dryburgh any information on Receiver Type 73, also Transmitter Type 49.-E. S. Webs, 6 Pond Hill, Halberton, Tiverton Type
Devon.

## CORRESPONDENTS WANTED

$S^{I R},-1$ am 17 years old and interested in all aspects of radio. I would be grateful if any reader about my own age or older would correspond with me. I am studying electronics at home and another home studier would be most suitable because we could help each other.-Gerard Wallace (Ballyvaughan, County Clare, Eire).
$S^{I R},-1$ am interested in radio and electronics and would like to correspond with people who are interested in exchanging radio parts for Indian curios and novelties or anything of equal value from my country. The reason for this request is that radio components are not easily available here or are unduly expensive. I am 18 years old.Chainnit Singh (122/Narmada, Indian Institute of Technology, Madras 3, India).
$S^{I R},-I$ am very keen on tape recording and would like to tapespond with anyone who shares my hobbies of C.W. and folk music, photography, sound effects and TV DX-ing. I have a two-track $3 \frac{3}{3}$ i.p.s. Fidelity Argyll with maximum spool size of $5 \frac{3}{4}$ in. -IAN UDEN ( 7 Ash Road, Strood, Kent).

## AN EXPERIMENTER'S GALVANOMETER -continued from page 752

straight wire was placed immediately in front of and in the middle of the lens.

## The Scale

This was made from a strip of greaseproof paper with graduations on one side. The papes was held in position by a light balsa wood frame
These, (b) and (c), could be moved around unti a sharp image of the lens was obtained on the scale after reflection from the mirror of thi galvanometer.

The suspensions are not ideal as they are rathe easily broken and sometimes do not quite returi to zero after prolonged deflection, but they ar quite satisfactory for many purposes. They are in fact, far better than the somewhat amateuris. method of construction might lead one to expec

The dimensions given are not intended to b exact but are a general guide to the constructior

The sensitivity is approximately $25 \mathrm{~mm} / \mu \mathrm{A}$ a a scale distance of one metre.
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