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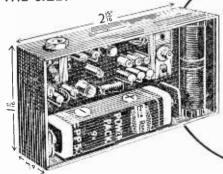


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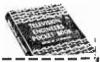
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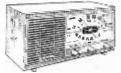
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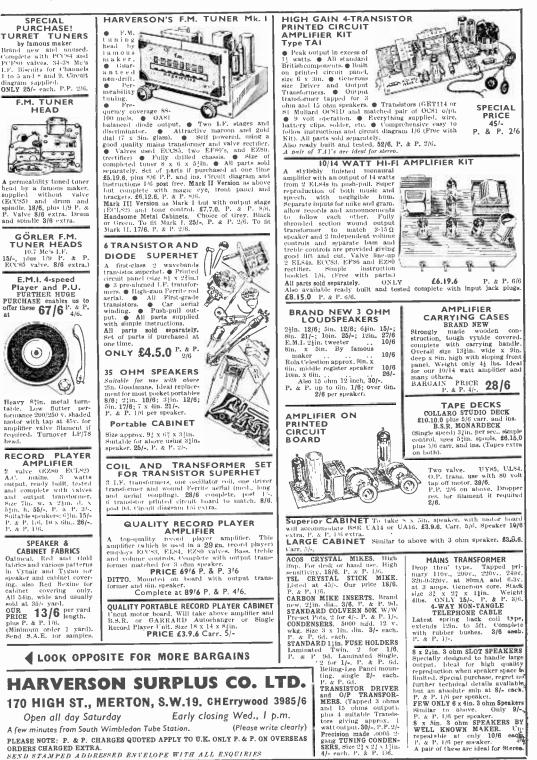
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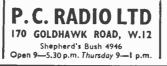
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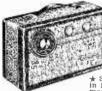


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PRE-AMPLIFIER A professional addition to your H1-F1 Stereo Sys-tem consisting of two basic Units. the Tape Deck and Pre-amplifier, which employs 4 Transis-tors and 4 Valves. The Unit with record and playback i track stereo or 1 track mono at either 71; 1.p.s. or 31; h.p.s. both speeds being tully equalised. Features: Track System: 1 track 2 channel stereo or monaural record and playback. Independent single channel recording on either channel while playback on other channel. Head Type: 1 track 2 channel inline stereo and associated erase heads. Low loss laminated pole pieces. Level indicators: 2 Meters. 1 per channel. Dicital Counter: 3 digit tape position indicator. Automatic Stop: When tape runs out or breaks. Inputs: Microphone ImV (50K, othms Impedance) Gram/Tuner 50mV (high 10ks Kols. SIN Ratio. - 450B or better at 71' tape speed. Separation: 45db or more between stereo channels. Frequency Response: 40 to 15,000 cycles per sec. at 74 1.p.s. 40 to 9,000 cycles per sec. at 34 1.p.s. Single Motor: 4 pole heavy duty induction type. Power Supply: 240v A.C. 50 cycles. Size 61' x 104' x 15'. Tape Size: Up to 7'. Line Up: 4-25H73 Transistors. 2-12AT7. 1-1AU7, 1-12BH7 Valves.

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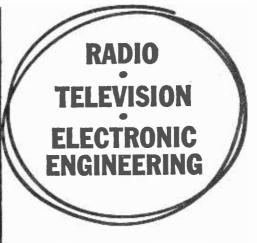
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PRACTICAL WIRELESS



February, 1964



Practical Wireless



Vol. XXXIX No. 684 FEBRUARY, 1964 🗮
Editorial and Advertisement
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NCE every month, it behoves your editor to write the several hundred words which comprise the leader column. It is, of course, an old cynical precept that nobody bothers to read leader articles (except in The Times!) and that if sufficiently emboldened an editor could fill his column with all manner of libellous, scurrilous and defamatory matter and no one would be the wiser.

Anvone who has sat at an editor's desk will be able to refute this most emphatically! This hoary old gag is only a gag and was most likely first thought up by a frustrated assistant editor!

Thus, in framing the month's leading article, an editor is aware that a large percentage of his readers is going to read the results of his literary efforts, be they modest, be they profound. However, there is more truth in the assertion that the leader is the toughest part to write and there can be very few editors who at some time in their career have not sat temporarily baffled, awaiting an idea to bourgeon.

For, especially in a magazine such as PRACTICAL WIRELESS, the subject matter must relate to something with which the average reader can associate himself. That is why, though often tempted, we seldom stray into the realms of trade and broadcasting politics, ethics and practices; these subjects receive sufficient airing via more appropriate mouthpieces.

The aim is to deal with topics of direct interest to readers. To comment. To provide talking points. To stimulate activities. To offer guidance. It is an opportunity for your editor to forge a personal link with readers once a month.

Before becoming a professional journalist, your editor would willingly have volunteered to write a supply of leaders for the contemporary radio magazines on what were (at the time) burning issues or pet theories. And now, hundreds of leaders later, it might be interesting and enlightening to reverse the procedure. In short, we invite you to write a leader!

Here is a glorious opportunity to air your comments on a chosen subject, to address fellow readers. The rules are simple: just write approximately 250-300 words (about half the length of this article) on a suitable theme-anything providing it deals with the hobby of radio constructionand give it a title. Send it to PRACTICAL WIRELESS, marked "Leader Competition". Entries need not be typed, though this is preferable.

Two guineas will be awarded to the entry considered the best by a panel of judges from the staff of PRACTICAL WIRELESS, and one guinea for the runner-up. The judges' decision will be final and we regret that it will not be possible to acknowledge individual entries.

The winning leaders will be published within the pages of the April issue. The closing date is January 31st.

Let's have a good response to this invitation. At least it will prove that you do read the leader page!

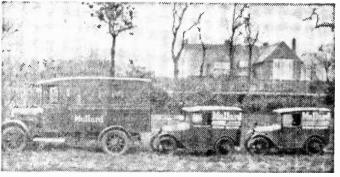
Our next issue dated March will be published on February 7th



25 Years of Valve Manufacturing

DESPITE the transistor, the Blackburn plant of Mullards Limited -25 years old in November last year-still manages to produce approximately 50 million valves a year. This recent anniversary was also marked by the 80th birthday of Mr. S. R. Mullard who founded the first Mullard Radio Valve Company in 1920. During the two decades which followed, the demand for radio valves increased enormously so that new premises were always being sought and larger factories being built to supply this demand, with the eventual establishing of the plant at Blackburn in 1938.

By 1944 the output from this plant, which had a labour force of 200, was 6.5 million valves a year. This had risen to 33 million by 1955 and to 50 million by 1958, when 5.000 were employed in this one factory. Now the Blackburn plant is only one of 18 Mullard factories throughout England, producing a variety of sophisticated components for the electronics industry, bearing only a technical similarity to the early transmitting and receiving valves, with which S. R. Mullard began his manufacturing company 43 years ago.



Even in 1924 the growing imbortance of valves was indicated by the number of Mullard vans such as these, which were then familiar sights on the roads.

RADIO EQUIPMENT FOR TSR-2

THE R.A.F.'s new tactical-strike-reconnaissance and strategic nuclear bomber, the TSR-2, will be fitted with instrument landing system and h.f. communication equipments manufactured by the Marconi Company Limited. The ILS is that of the Marconi Sixty Series equipment. The

The ILS is that of the Marconi Sixty Series equipment. The communication equipment will provide both single and double sideband transmission and reception at high power.

NEWS AT HOME AND ABROAD

Retailers Association Adopts New Symbol

AS a result of a large number of requests from domestic and electrical retailers, the Radio and Television Retailers Association recently formed a separate association for the benefit of these retailers. Known as the Electrical Appliance Association, this new body has recently adopted a symbol which will be displayed in shops so that the consumers may benefit by identifying tirms belonging to the E.A.A.

The new symbol has been designed along the same lines of the already well known R.F.R.A. trade mark.

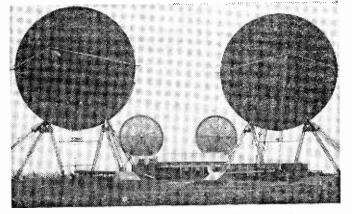


The symbol of the Electrical Appliance Association

NATO COMMUNICATIONS NETWORK COMPLETE

Allied Powers Europe has recently accepted, on behalf of Treaty the North Atlantic Organisation, the final station in NATO's ACE HIGH communi-

THE Supreme Headquarters cations network. This vast system of radio stations stretches from Norway to Turkey; an 8,300 mile link, incorporating 82 stations, located in nine of the NATO countries.



One of the 82 stations of NATO's ACE HIGH network.

NEW TITLE FOR I.E.E. JOURNAL

THE official organ of the I.E.E., in which papers originally presented to meetings of the Institution are published, has for years been known as the Journal of the Institution of Electrical Engineers. Now the Council of the Institution has changed the name 'Electronics and Power", with the previous title remaining as a to sub-title.

sising the scope of the Institution and to dispel the idea that the I.F.E. is mainly concerned with power engineering when, in fact, for several years electronic subjects have been more in evidence in papers and at meetings than power engineering.

Aircraft Equipment Tours West Germany

DEMONSTRATION aircraft belonging to the Marconi Company Limited, recently completed a sales tour of West Germany. Aboard the aircraft was a variety of equipment, manufactured by the company, which was shown to aircraft and constructors operators throughout the Federal Republic during the ten days of the tour.

Included in the demonstration equipment was standard airline Doppler Navigator and the new helicopter Doppler systems.

The Council decided on this change as a means of empha-

R.T. for Desert Patrols

IN its fight against the menace of locusts, the Desert Locust Control Organisation of East Africa keeps a constant surveillance on the breeding grounds and movements of this pest. Much of this work involves patrols over barren and underdeveloped areas, extending sometimes hundreds of miles from centres of communication. To provide their patrols and static stations with a reliable means of communication, the D.L.C.O. recently selected and ordered Marconi h.f., s.s.b. transmitter/ receiver equipment.

This equipment can provide adequate daytime communica-tions over many hundreds of miles, using only a simple dipole aerial and a transmitter power of only 100W.

The design, manufacture and installation of the complete project has been the task of Inter-national Telephone and Telegraph Corporation and its affiliated companies, and included in each of the stations is multiplex equipment made by Standard Telephones and Cables Limited.

The purpose of the ACE HIGH system is to provide a reliable method of communication between the nations of the European-wide command area of NATO, and to accomplish this, both tropospheric forward scatter (over-the-horizon) and line-ofsight types of transmissions are used throughout the network. The stations have all been built on high ground, each with two pairs of 65ft. circular dish-aerials positioned to pick up and retransmit any of the 250 telephone and 180 telegraph circuits which can be accommodated by the system.

STC ACQUIRES HUDSON ELECTRONICS

THE firm of Hudson Electronic Devices Limited, manufacturers of mobile radio communication equipment, was formed and built up by Mr. A. D. Hudson, at one time an apprentice of Standard Telephones and Limited. Now STC Cables Limited has acquired the issued capital of Hudson Electronic Devices, so that it becomes part of STC's radio division.

Mr. Hudson will remain as a director, however, as plans for the firm's expansion go on under new management.

Electronics Symposium in Birmingham

ONE day symposium on A "Electronics in the Auto-mobile Industry", has been arranged by the Electronics Section of the South Midland Centre of the l.E.E. and the West Midland Section of the British I.R.E. The symposium is to be held during April, this year, and will take place in the Electrical Engineering Department of the University of Birmingham.

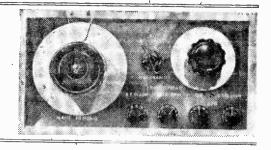
A MODERN COMPACT 3-TRANSISTOR S.W. CONVERTER

FOR 1.7-31.5 Mc/s

BY J. VAITES

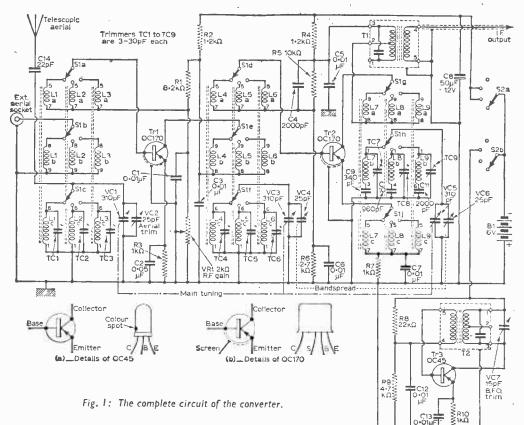
THE converter to be described is a portable, high performance, transistorised front-end unit covering the short wave bands from 1.7Mc/s to 31.5Mc/s. It is designed to feed into any broadcast receiver without any alteration at all to that receiver.

Being of compact size, it is an ideal companion to any standard transistor portable, provided the portable has an external aerial socket. It can, of course, be used also with any



other type of broadcast receiver, whether mains domestic receiver or car radio. This add-on unit thus converts the basic receiver into a double conversion receiver, providing an interesting and useful combination.

The unit provides a cheap introductory step to the short wave bands for the beginner, who will almost certainly have the use of at least one broadcast receiver in the household. At the same time, being electrically bandspread and incorporating facilities for s.s.b. reception, the converter is an ideal piece of equipment for the "ham" station, whether fixed or mobile.



Circuit Description

The circuit (see Fig. 1) is designed around the new Denco transistor coils—based on their welltried range of Miniature Dual Purpose Coils. Ranges 3, 4 and 5 are used, covering respectively 1.67 to 5.3Mc/s, 5 to 15Mc/s, and 10.5 to 31.Mc/s. The coil connections are switched by a 3-way 9-pole Yaxley switch (S1), using three wafers with interposed screens.

The r.f. stage uses an OC170 transistor (Tr1) with blue coils in the aerial stage and yellow coils as coupling to the second stage. An r.f. gain control VR1 varies the base voltage of Tr1. An external fore, tuned to this frequency, corresponding to 187.5m on the medium wave band. In practice, since the medium wave band of many receivers only goes down to just below 200m, the lowest clear wavelength on the band is selected (this may fall anywhere between 190 and 200m) and the output of the converter adjusted to it.

The three-gang tuning capacitor (VC1, 3, 5) is fitted with a calibrated dial incorporating a slow motion tuning device. The bandspread capacitor (VC4, 6) is coupled to the mixer and oscillator sections only; this two-gang capacitor is also fitted with a calibrated dial. The aerial section is trimmed separately by VC2, this being necessary to accommodate different types and lengths of aerial.

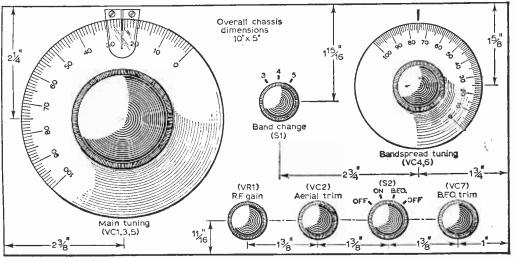


Fig. 2: Drilling details and control layout of the front panel.

aerial can be fed to the primary of the aerial coils, or a built-in telescopic aerial can be used, this being connected permanently to the aerial tuned circuit via a small capacitor.

The second stage is the mixer oscillator and the transistor (Tr2) is also an OC170. The white coils are used here and an output of nominally 16Mc/s is obtained at T1. The broadcast receiver is, there

	TABLE I	
Frequency	and Wavelength Coverage	ð

Range	DIAL SETTING			
-	100	0		
3	i ∙67Mc/s 180m	5·3Mc/s 57m		
4	5.0Mc/s 60m	15Mc/s 20m		
5	10·5Mc/s 28m	31∙5Mc/s 9∙5m		

Beat Frequency Oscillator

The b.f.o. unit uses an OC45 transistor (Tr3), with the appropriate b.f.o. transformer (T2). The swing of the trimming capacitor (VC7) is adequate to permit reception of all s.s.b. transmissions. The b.f.o. may be coupled by means of a 1pF capacitor from pin 2 of T2 to pin 2 of T1, but this should not be necessary, since the b.f.o. coil and the i.f. transformer are physically adjacent.

The b.f.o. is switched on and off by S2, which also serves as the on/off switch for the unit as a whole. A large capacitor, C8, is fitted to smooth out any fluctuations in the power supply, this latter item consisting of four pen-torch batteries in series, giving a 6V supply.

Mechanical Construction

The front panel, of $\frac{1}{16}$ in. aluminium, size 10in. x 5in. is drilled as per Fig. 2, countersinking most of the 6B.A. holes as indicated.

The chassis, of $\frac{1}{8}$ in. bakelite or perspex, size 9in. x $4\frac{3}{8}$ in., is drilled as per Fig. 3.

The exact dimensions for the two transformers (T1 and T2) are not given, only the centres being indicated. This is because the drilling figures are

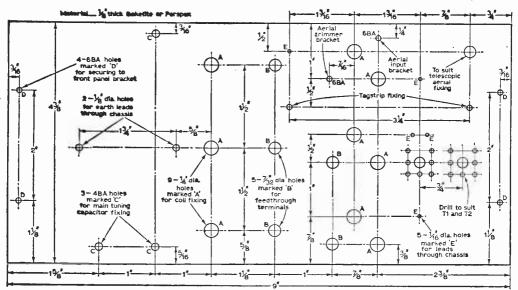


Fig. 3: Chassis dimensions diagram

rather awkward and the constructor would perhaps prefer to consult the information leaflet supplied with the components. All the transformer drillings, except the core adjusting hole, should be heavily countersunk from the underside of the chassis. as the component pins are rather short, being originally designed for use on rather thinner printed circuit boards.

The two supporting brackets are constructed from 20s.w.g. tin sheet as shown in Fig. 4, taking care to make the bends in the two brackets in the reverse mode, so that the whole job is symmetrical when fastened together.

Finally, at this stage, the two small brackets for the aerial input and trimmer can be formed as per Fig. 5.

The Case

The converter may be housed in a metal case, size 10in. wide x 5in. high x $4\frac{3}{4}$ in. deep (internal

dimensions), this giving a slightly recessed front panel. Drillings will be needed for the telescopic aerial, the external aerial and the output lead.

The best method of fixing the converter into its case is by two bolts through the back of the case screwing into two tapped brackets fitted to the back of the chassis. The constructor may have his own ideas on this subject, however, and the above ideas are offered only as a suggestion. It is, however, advisable to use a metal case if at all possible, so as to provide full screening of the converter circuits.

Mounting and Wiring-up

If not purchased complete, switch S1 should be made up with wafer layout as indicated in Fig. 6, and with screens (Fig. 7a) and spacings as indicated (Fig. 7b).

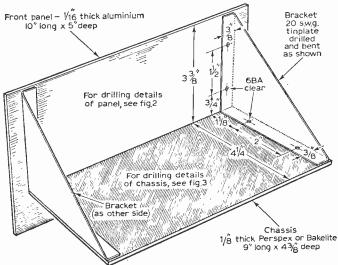


Fig. 4: The assembly of the front panel and chassis.

The first components to be mounted on the chassis are the two transformers T1 and T2, these being held in position by bending the can tags. Next, a 12-way tag-strip is mounted on the underside of the chassis using holes marked G (see Fig. 3). Finally, mount five feed-through terminals into the holes marked E1 to E5 (Fig. 8).

The assembled switch should now be mounted, but before doing so, it is advisable to fit earth tags on to *either* side of the corner holes in the screens and also to solder flying leads on to the 7, 8 and 9 o'clock contacts of the front and middle wafers (these are the pin 5 connections, Fig. 6), since these points may be difficult to get at later.

When the switch is mounted, refer to Fig. 6, and first connect the lower wipers to the appropriate feed-through terminals. Then mount all coils with pins uppermost (see layout diagram, Fig. 9), and complete all switch wiring, with the exception of the leads from the top wipers (tuning capacitor leads), and the aerial wiper on the rear wafer.

Next complete all the coil wiring, by commoning up appropriate pins (e.g. white coils, all pins 8 commoned, all pins 7 commoned, etc.).

Certain of the other components can now be mounted inside the coil compartments. These are: R1 from pin 8 of 1.4 through hole in screen 2 to

- pin 7 of L1. R6 and C6 from pin 7 of L4 to earth tag
- adjacent. R7 and C7 from pin 7 of L7 to earth tag
- adjacent.
- C3 from pin 8 of L4 to earth tag adjacent.
- C1 from pin 7 of L1 to earth tag adjacent.
- C9 from pin 3 of L7 C10 from pin 4 of L8 C11 from pin 6 of L9 Difference from pin 6 of L9 C11 from pin 6 of L9 C11 from pin 6 of L9

Next, certain leads can be taken from the coil pins to points below the chassis and also on the screens (refer to Fig. 8 for tagstrip numbering).

These are:

- Pin 1 of L1 to earth tag adjacent.
- Pin 1 of L4 to earth tag adjacent.

Pin 7 of L2 through hole F1 to tag 6 on tagstrip.

- Pin 7 of L5 through hole F3 to tag 8 on tagstrip.
- Pin 8 of L5 through hole F2 to tag 9 on tagstrip.
- Pin 8 of L8 through hole F4 to pin 2 of T1.

The main tuning capacitor and the bandspread capacitor can now be mounted. The top wipers on each switch wafer are wired to the appropriate tags on the main tuning capacitor and, in the case of the front and middle wafers, to the appropriate tags on the bandspread capacitor as well.

VR1, S2 and VC7 are mounted next, making sure that the spindle of VC7 does not touch the front panel.

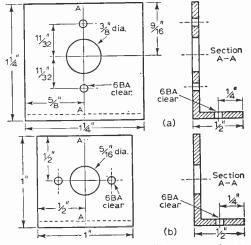


Fig. 5 (a) aerial trimmer bracket; (b) aerial input bracket.

The earth wiring is then fitted, using 20s.w.g. tinned copper wire. The earth tags on the bandspread capacitor are connected to screen 1 adjacent, soldering direct to the screen. The earth tags on screens 1 and 2 are wired together and the wiring continued to all earth tags on the main uning capacitor, making use of holes C to run underneath the capacitor. The earth wiring is continued underneath the chassis to the appropriate tags on VR1, then on to the tagstrip, joining up tags 2, 3 and 12, and finally to the can tags of T1 and L10.

The underchassis components are now wired up as follows:

Pin 3 of T1 to tag 10 on tagstrip.

C4 and R5 across tags 8 and 10 on tagstrip.

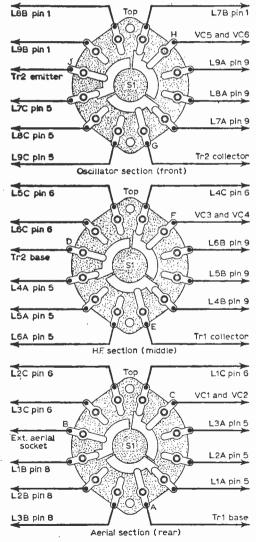


Fig. 61 Wiring of SI. Note1 wafers viewed from rear.

C5 across tags 10 and 12 on tagstrip.

- R4 across tags 7 and 10 on tagstrip.
- R2 across tags 7 and 9 on tagstrip.
- C2 and R3 across tags 1 and 3 on tagstrip.
- C8 across tags 7 and 12 on tagstrip. R10 and C13 across tags 11 and 12 on tagstrip. Wire lead from top of VR1 to tag 6 on tagstrip.
- Wire lead from contacts 2 and 3 on S2a to tag 7 on tagstrip.
- Wire lead from contact 3 on S2b to one contact of VC7 and continue on to pin 1 of T2.
- Wire lead from other contact of VC7 to pin 3 of T2.
- Wire R8 from pin 4 of T2 to pin 1 of T2.
- Wire R9 and C12 from pin 4 of T2 to tag 12 on tagstrip.

The transistors can now be wired in (see Fig. 1 for connections). All wires except the OC170 screens should be sleeved and the full length of lead wire should be retained.

- W.	iring points	are :			
Trl	Collector	-	feedthrough terminal E2.		
	Screen	-	tag 2 tagstrip.		
	Base	-	feedthrough terminal E1.		
	Emitter	-	tag 1 tagstrip.		
Tr2	Collector	-	feedthrough terminal E3.		
	Screen	-	use earth terminal on VR1.		
	Base	-	feedthrough terminal E4.		
	Emitter	-	feedthrough terminal E5.		
Tr3	Collector	-	pin 3 T2.		
	Base	-	pin 5 T2.		
	Emitter	-	tag 11 tagstrip.		
TABLE 2					
Tracking Points					
1	BAN	d end	D TRACKING		

Range	BAND	END	TRACKING POINTS		
	L.F.	H.F.	L.F.	H.F.	
	(Dial 100)	(Dial 0)	(Dial 89)	(Dial 8 <u>1</u>)	
3	1.67Mc/s	5·3Mc/s	1.83Mc/s	4.5Mc/s	
4	5.0Mc/s	15·0Mc/s	5.5Mc/s	13.5Mc/s	
5	10.5Mc/s	31·5Mc/s	11.5Mc/s	28.5Mc/s	

The coaxial aerial socket and the aerial trimmer VC2 are mounted on their brackets and fitted to the chassis with an extension spindle on VC2 coming out through a bush on the front panel.

The body of the coaxial socket is wired to pin 1 of L3 and the centre connection to the appropriate wiper on the rear wafer. The earth connection of VC2 is taken to tag 3 on the tagstrip and the other connection through hole F5 to the top wiper on the rear switch wafer.

The coaxial output lead is soldered across pins 4 and 5 of T1, pin 5 also being connected to tag 12 on the tagstrip. This output lead should preferably be clamped to the chassis to prevent jerking.

The nine concentric trimming capacitors may now be fitted into position. The "live" connection (outer connection) should be soldered either on to the appropriate switch contact or coil pin, whilst the earth connection (centre spindle) should be soldered directly on to the screen. Care must be taken to keep the top of the trimmers below the level of the top of the front panel, otherwise they will foul the case.

Finally, the batteries can be mounted (clamped to chassis underneath the main tuning capacitor) and the linking wires soldered. The positive battery terminal is taken to tag 3 on the tagstrip and the negative terminal to the wipers of S2A and S2B.

Knobs and dials are then fitted and the converter is ready for lining-up.

Telescopic Aerial

It will be noted that no exact details have been given for fitting the telescopic aerial. This is because there is a wide variety of suitable devices on sale, ranging from the truly telescopic (and rather expensive) type, to the cheaper semitelescopic car aerial.

The general idea is that the aerial selected should have a tapped hole in its bottom section A corresponding bolt of some $\frac{1}{2}$ in. length is fed up through hole M (Fig. 3) and tightened down with a nut, leaving enough thread to screw into the aerial. A solder tag is placed under the head of the bolt (i.e. underneath the chassis) and C14 is wired from this tag to the "live" tag of VC2.

A suitable hole is cut in the top of the can and fitted with a rubber grommet, making a good push fit for the aerial, which is screwed in when the converter has been fastened in its case.

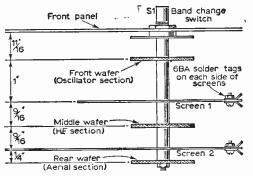


Fig. 7a (above): Showing the build-up of the switch. Fig. 7b (right): Drilling details of SI screens (viewed from rear).

Lining Up

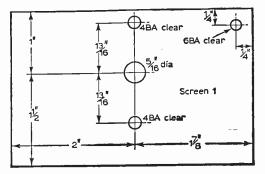
Lining-up should preferably be done with the use of a signal generator although, as will be shown, it is possible to manage without such an instrument.

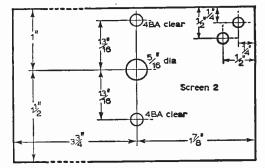
The output lead should be fitted with a terminal appropriate to the input socket of the main receiver and should be kept as short as is practicable.

The main receiver should be tuned to the selected frequency at the bottom end of the medium wave band. In the case of a mains-operated receiver or car radio this can certainly be the very end of the scale, since with the normal aerial removed there will be no pick-up. The case of a transistor portable is rather different, since the internal ferrite aerial cannot be disconnected. However, the lowest clear wavelength should be selected and any residual pick-up can be minimised by suitable orientation of the receiver.

Once this has been done the converter output lead is plugged in and the unit switched on. Range 3 is selected, with the main tuning capacitor fully meshed and the oscillator temporarily stopped by shorting across L7(b). The signal generator is fed into the aerial input socket via a 400 Ω resistor (link generator chassis to converter earth) and adjusted between 1.5 and 1.6Mc/s (modulated) until a note is heard in the speaker. T1 is peaked and is now tuned to the input frequency of the basic receiver.

The generator is now fed in unmodulated and the b.f.o. switched on. With VC7 set in midposition, T2 core is adjusted until a beat note is





Material for both screens _____ 20 sw.g. tinplate

heard and the centre position found where the note disappears.

Standard procedure is now used for the main lining-up. The b.f.o. is switched off, the shorting link on L7 removed, VC4-6 set to minimum capacity, VC2 set at half capacity and the generator used modulated.

Referring to Table 2, each band is lined up in turn, first setting the band-end limits by adjusting the oscillator core with the generator set to the low-frequency end of the band and then adjusting the oscillator trimmer as the top-end frequency is fed in.

When this has been done the generator is set to the lower tracking frequency and the main dial set to a reading of 89. The cores of all coils of the appropriate range are now adjusted for maximum signal. The generator is then set to the higher tracking frequency and the main tuning dial set to a reading of 8¹/₂. The trimmers of all coils are adjusted for maximum signal. This process is repeated until no further adjustment of cores or trimmers is required.

Lining Up Without a Signal Generator

After adjusting the main receiver to the frequency chosen, short out L7(b) coil as before and switch converter on with the b.f.o. also on. Set VC7 to midposition and adjust the core of T2 until a loud rushing noise is heard in the speaker. This denotes that the b.f.o. is oscillating at the selected input frequency and the core of T1 can now be peaked, using this "noise" source.

The b.f.o. is then switched off and the shorting link removed. The band edges cannot be set accurately (although they can be altered at a later date when known stations are identified), so

it is suggested that the oscillator cores and trimmers are set to mid-position. Some measure of liningup can now be achieved by selecting reasonably strong transmissions near the $\$\frac{1}{2}$ and \$9 dial settings and peaking cores of the aerial and h.f. coils at the higher setting and peaking trimmers associated with these coils at the lower setting, repeating 'the process until further adjustment makes no improvement.

Operating the Converter

The converter performance has been found to be very good, when fed into a standard six-

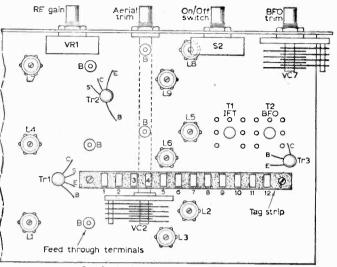


Fig. 8: Underchassis layout diagram.

transistor portable and exceptional when backed by a more sophisticated strip.

The r.f. gain control should be kept well down on the stronger stations to avoid overloading the main receiver. The bandspread tuning gives good results and the aerial trimmer is hardly needed but should be peaked when any change of aerial is made.

When an s.s.b. transmission is received the b.f.o. should be switched on and b.f.o. trimmer adjusted until the speech becomes intelligible. The r.f. gain control should be turned well down when doing this, otherwise distortion may occur.

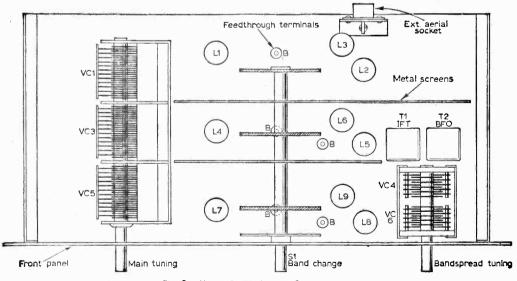


Fig. 91 Above-chassis layout of components.

February, 1964

Further Applications of the practical wireless "Sixteen" Multirange METER

O N the reverse side of the blueprint issued last month, featuring the P.W. "Sixteen" multirange test meter, details were given of typical tests and applications of such an instrument. This month, we follow up with a few more notes on applications to further illustrate the versatility of a basic multirange meter.

Capacitor Testing

The reactance of capacitors can be calculated from voltage and current tests when a suitable a.c. is applied. A circuit such as Fig. 1, making use of a double-wound transformer with tapped secondary for high-voltage capacitors and a lowvoltage secondary for testing electrolytics, can be used for obtaining readings.

First measure the voltage across the capacitor, then place the meter, switched to the 25V a.c. range, across the variable resistor R1 to measure the current taken by the capacitor. If R1 is 500 Ω , full-scale deflection represents 50mA.

In the low-voltage position R2 should be 100Ω , giving a 5V deflection on the 25V a.c. range, which represents 650mA.

To calculate reactance in ohms first consider the 10^6

formula $Xc = \frac{1}{2\pi fC}$, where Xc is the reactance in

ohms, f is in this case 50 cycles (mains supply), and C the capacitance in microfarads. Xc is also equal to E/I, the a.c. voltage across the capacitor divided by the current through it.

Combining the two formulae,

 $Xc = \frac{10^{6}}{2\pi fC} = \frac{E}{1}.$ Transposing, we obtain $C = \frac{10^{6}}{2\pi f} = \frac{I}{E}.$ With an applied frequency of 50c/s the factor $\frac{10^{6}}{2\pi f}$ becomes 3.18 if the conversion is to milli-

amperes, volts and microfarads. Thus $C = K \times I/E$.

The double-wound transformer affords isolation from mains supply, but direct connection to the mains can be used for this test if sufficient care is taken. If R1 (and R2) is made variable, compensation can be made for small differences in circuit capacitance, meter impedance, etc., by checking a good capacitor of known value. It is further advisable to check several, taking an average, to allow for normal tolerances.

The low-voltage winding of the transformer can be used to apply 3 to 7V to electrolytic capacitors of high working voltage, but is not suitable for low working voltage capacitors, which should be tested by bridge methods. In this test the readings will all be at the lower end of the scale.

Inductance Testing

Similar measurements can be taken for inductances of high value, such as transformer windings and loudspeaker fields, but accuracy is not so great

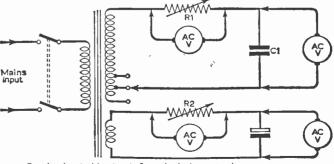


Fig. 1: A suitable circuit for calculating capacitor reactance.

as the current is limited not only by the inductance but also by the self-capacitance and resistance of the windings. In this case the inductance in hearves = $K \times E/l$.

It should be remembered that the inductance of an iron-cored coil or transformer winding decreases when d.c. flows through it, as in the case of a smoothing choke.

Alignment Procedures

The multimeter can be used in various ways to indicate output voltages, current and power for alignment and response checking.

Most obvious method is to measure the a.c. voltage across the secondary winding of an audio output transformer for sound level, as in Fig. 2. The loudspeaker is disconnected and its place taken by a resistor of equivalent impedance. (Note that this resistor must be of sufficient wattage to dissipate the expected power output.) Power output is V^2

equal to - where V is the indicated voltage and R

R the equivalent resistance.

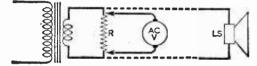


Fig. 2: Output voltage measurements.

Alternative methods include the measurement of detected signal voltage across the detector load, using a low d.c. milliamp or microamp range in series with a suitable resistor. The resistor acts as multiplier to the meter and as an isolating component in conjunction with the decoupling capacitor which should be fitted. (See also Fig. 4.) Another method is the measurement of a.g.c. voltage.

Indication of sensitivity on f.m. receivers is also taken at the detector stage in the manner illustrated in Figs. 3 and 4 on last month's blueprint.

Output measurement on transistorised portable radios presents a different problem as the output is in the region of a few milliwatts. Across a 500 loudspeaker an indication of perhaps half-scale on the 25V a.c. range may be obtained at full output, but where a 3 Ω loudspeaker is used there may only be two or three volts available and readings will be too closely spaced at the lower end of the scale.

A better alternative method is to insert the multimeter in the battery supply lead to the receiver, switched to the 50mA range (250mA range for larger sets). As the current consumption is dependent on output power this gives a suitable indication for alignment purposes and a current of about 10mA would be expected under quiescent conditions, increasing to perhaps 35mA or more when fully loaded with the signal generator input. This gives an easily visible variation over the central portion of the scale.

For vision alignment either a.c. or d.c. conditions can be used, as in Fig. 3. The varying d.c. voltage across the video amplifier anode load resistor can be measured, with the disadvantage that both meter leads are then at high potential and that the signal being measured is unmodulated.

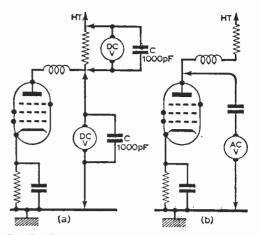


Fig. 31 Output measurements for vision olignment purposes.

With a negative-going video signal the reading is from minimum to maximum. If measured from chassis to anode the readings will commence at the "black-level" anode voltage and dip as resonance is approached during tuning. Adjust for maximum dip.

A modulated input can be measured as in Fig. 3(b). With a capacitor of about 0.25μ F in series with the meter, switched to a.c. volts, the signal gives an indication from zero to maximum.

If signal levels are such that accurate indication cannot be obtained other methods may be used as, for example, inserting the meter, switched to a suitable mA range, in the anode lead of the video amplifier, or applying it, switched to microamps, with a series resistor (as r.f. stopper) across the vision detector load.



Fig. 41 A method of decoupling the meter which may be used with low currents and voltages.

A convenient measuring point is the modulating electrode of the cathode ray tube, where a d.c. varying in sympathy with the signal is to be found.

As a final stricture remember to decouple the meter, as near the point of application as possible, where the self-capacitance and inductance of the leads could cause instability in the circuit being tested. Fig. 4 shows the method employed for television testing, which lends itself to other applications where both current and voltage are low.

Coaxial cable is used to connect the prods or clips to the meter and a decoupling capacitor, 0.001μ F, is fitted directly to the "live" prod and the other end soldered to the braided outer of the coaxial cable. This method is not suitable for high voltage or current measurements where normal, separate leads should be used.

February, 1964

PRACTICAL WIRELESS

975



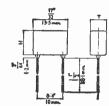
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Can	Dime	T.C.C.	
Cap. μF	н.	Τ.	Type No.
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0.022	<u>₩</u> 9mm	77 5.5mm	PM X2
0.047	₩ 9mm	7/ 5.5mm	PMX3
0.1	₩ 11mm	<u>9</u> ″7·2mm	PMX4





Cap Tolerance

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Test:

Power Factor: ≤ 0.01 at 1,000 cps.

 \pm 85°C. without de- tection against the inrating.

Insulation $\pm 20\%$ Resistance: 10,000 megohms

Terminations: 22 s.w.g. solder coated 400V. D.C. for 2 secs. at parallel wires for side 20°C. mounting.

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GETTING THE BEST FROM AUDIO EQUIPMENT

OW can one get the best out of one's sound reproducing equipment? Ideally, one room in the house should be earmarked as the "nusic room", and equipment should be carefully built therein to give the very best results when sitting in normal listening position, the room treated with curtains and soft furnishings to give acceptable acoustic conditions.

Descriptions of such music rooms have been seen and occasionally one can visit a demonstration room lavishly provided for by some knowledgeable architect. These as often as not just make us realise that hi-fi in that sense is not for us. We have to fit in with more normal budgets, not to mention the aesthetic but less technical aspirations of one's wife and family.

Typically, the average household has two rooms in which listening is concentrated. In the author's case these are the lounge, providing the best surroundings for listening, and the family living room, a utility room in constant use.

Speaker Extensions

February, 1964

The simplest and perhaps the most satisfactory solution from a technical point of view is for both radio and gramophone equipment to be in one of the rooms. Generally speaking the lounge would be chosen because the piece of furniture needed to house this equipment to today's standard must be large, long and low—not a piece for the family room. Besides, though the lounge is less often used, when it is occupied the best possible reproduction is needed there.

Under these circumstances an extension speaker will probably be provided in the family room—the best quality that can be afforded, of course, in order to do justice to the amplifier. At this stage it is not proposed to deal with the provision of a mono speaker output from a stereo record—would anyone really be happy to do this anyway?—and it is assumed that the amplifier provides a mono output.

The connection between amplifier and extension speaker is not just a simple matter of using any old piece of flex or bell wire. Almost invariably the extension speaker will have a low impedance input, the speaker transformer in the main amplifier serving both local and extension speaker. This is advisable because an extension at low impedance is less likely to pick up interference and mains hum than would an extension at the high impedance (primary) side of the speaker transformer.

The low impedance connection has the disadvantage, however, that unless the cable used to connect the extension speaker is carefully chosen, or else the cable run is very short, the impedance of the cable can be comparable to the speaker impedance itself (perhaps only 30) and consequently there will be a loss of audio power in the cable. A cable impedance equal to the speaker impedance will attenuate available speaker power to a half the total available. Also it should be noted that the speaker impedance varies with frequency and therefore if the cable impedance is low it is likely to introduce amplitude distortion.

Modern amplifiers generally have a high degree of negative feedback taken from the secondary of the output transformer and such amplifiers are sensitive to reactive load. It is difficult to design an amplifier which will be stable with an appreciable capacitive load but inevitably an extension lead introduces a capacitive component. Unless care is taken, therefore, an extension speaker might well result in amplifier instability.

The answer to all these problems, attenuation, amplitude distortion and instability, is a low loss cable of low capacitance. Fortunately, electronics workers dealing with the other end of the frequency spectrum—the television engineers have developed just the cable for the job. Television coaxial lead-in cable is ideal for speaker connections.

It is an odd thought that knowledgeable workers will take every precaution at the v.h.f. end of the scale but will fail to appreciate the equivalent precautions necessary when working at audio frequency. In practice, coaxial cable has many useful applications in audio work. It can be unsightly for long extension speaker leads unless care is taken and ideally it should be run under the floorboards. Avoid joining pieces of cable if possible, because, sooner or later, a joint is likely to introduce noise; if a joint must be made use a proper connector.

Switching Circuits

Assuming that the main speaker system (adjacent to the amplifier) when used alone is properly matched to the amplifier, connecting an extension speaker, whether in series or in parallel, will cause a mismatch. The popular types of amplifier using a normal degree of feedback are not very sensitive to changes in load and a reduction in effective load caused by wiring an extension speaker across the main speaker is unlikely to cause trouble,

However, it is desirable that the volume at both speaker positions should be similar. The extension speaker should have an impedance similar to the main speaker or else the available power will not be evenly divided between the two.

BY R. HINDLE

Some kind of built-in switching is highly desirable. It should be possible to mute the speaker at both ends and also the circuit should be so arranged that if both speakers are muted (or the local speaker muted and the remote speaker disconnected) the amplifier is not running without load.

This being so, one might just as well arrange matters so that there is less likelihood of mismatch. An additional advantage is that by wiring in this way there will be no change in power in one speaker when the other is switched on or off. Figure 1(a) gives the wiring. It will be seen that when a speaker is muted, a resistance is brought into use to dissipate the power that would otherwise drive that speaker. The resistance in each case must equal the nominal impedance of the speaker (i.e. a 15 Ω resistor for a 15 Ω speaker etc).

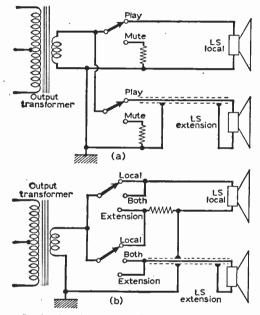


Fig. 1: Switching circuits for extension speakers.

Assuming that the two speakers have similar impedances as recommended above, this circuit results in a permanent division of available audio power into two equal parts, one part fed to each room. In practice a reduction of audio power by a factor 2 is not very noticeable to the ear.

However, if the equipment is being designed or bought with such a distribution system in mind the fact that only half audio power is available at each location should be borne in mind.

It will be seen that two separate switches are provided, one for each speaker. Consequently the switch for the extension speaker could conveniently be moved to the extension speaker cnd of the cable, fitting it on to the speaker cabinet itself for local control. If the switch control is to be entirely at the amplifier end a single three position switch might be preferable, providing main speaker only, extension speaker only or both speakers. This should be wired as in Fig. 1(b). It will be noted that only one resistor is used, brought into circuit when either one speaker is connected. This connection prevents the muting of both speakers or open circuits in case the extension speaker is disconnected.

It will be realised that either of these methods of wiring results in halving the impedance presented to the amplifier and this should be borne in mind if various output impedances are provided for. However, the usual type of amplifier will be quite happy under these circumstances.

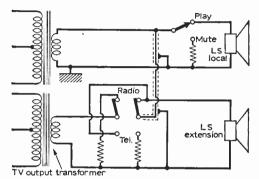


Fig. 2: Utilising a television loudspeaker as an extension speaker.

The extension speaker could, perhaps, be the television speaker if impedances are compatible. In this case care must be taken to see that the television output stage cannot be switched on without a load. A modification of Fig. 1(b) given in Fig. 2 is suggested. The switch disconnects the TV output transformer from the speaker when this is in use as an extension but at the same time inserts a resistive load to prevent the TV output being open circuited.

Two separate resistors are shown but if the load needs of the amplifier and the TV are similar (the latter will probably be of the order of 3Ω) a single one will suffice, the two points of the switch to which the separate resistors are connected being thus connected together and the single resistor being from this connection to the earthy lead.

Volume Control

The amplifier will be adequately provided with volume control but there may be a need for a local control at the extension speaker end. A resistive potentiometer type of control can be fitted as at Fig. 3, but not without introducing new

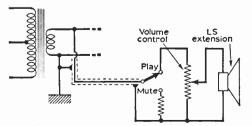


Fig. 3: Volume control for the extension speaker.

problems. When the volume control is set for full volume the potentiometer resistance is in parallel with the speaker and therefore to avoid power loss (and also possible amplitude distortion) the resistance must be appreciably higher than the speaker impedance.

On the other hand, at low volume levels the potentiometer resistance becomes the amplifier extension load and if this is appreciably higher than the speaker impedance the amplifier will be presented with a mismatch! One must compromise. A potentiometer total resistance of not less than four times the speaker nominal impedance is suggested and, in round figures, 50Ω for a 3Ω speaker and

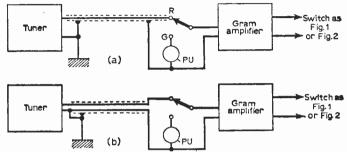


Fig. 4: Inter-wiring between separate tuner and amplifier.

100 Ω for a 15 Ω speaker are sizes likely to be available.

More elaborate circuits can be developed to minimise variation in load but are probably not worth the trouble except as nice little technical problems to solve.

A Personal Problem

The problem actually facing the author, when the line of thought that resulted in this article was generated, was somewhat different to those already dealt with. The habits of the family were such that in the living room the normal form of entertainment called for was television and radio, with only very occasional call for gramophone reproduction, whereas in the lounge the gramophone is most frequently used and only occasionally is radio used.

This being so it seemed wrong to install the radio in the lounge, requiring a visit to that room whenever a change of programme was required in the living room, or alternatively the provision of a complex remote control system.

The problem thus became as follows: radio equipment was to be installed in the living room and gramophone equipment was to be in the lounge. How should these be interconnected so that the occasional facility should be provided in each room to use the equipment fitted in the other, and would such a scheme be an acceptable and cheaper alternative to any duplication of equipment?

Using the Main Amplifier

The first temptation was to provide only a tuner and speaker in the living room and to bring into use for radio the main and comparatively expensive amplifier in the lounge equipment. The tuner output would then be permanently wired by means of a coaxial cable into the lounge equipment where there would be the usual radio-gram switch, and on the output side of the amplifier would be one of the switch versions given in Fig. 1.

This arrangement is given schematically in Fig. 4(a). There would be complications to the radio-gram switching if stereo gramophone reproduction was provided, but that is another story.

Using this arrangement some precautions have to be taken. It is desirable that the tuner audio output should be reasonably high so that the risk of appreciable pick-up of interference is minimised; a cathode follower output would be preferred. The outer screen of the coaxial should be connected to the tuner chassis at one end and the amplifier chassis at the other; it should connect to an earthed

point only at one endpresumably at the tuner end.

A better scheme to avoid hum pick-up would be to use a twin core screened cable in place of the single core of the usual coaxial cable. The outer sheath in this case is connected to a good earth at only one point, the earth return signal lead being carried by one of the cores as in Fig. 4(b).

However this lead from tuner to gramophone is arranged, there

will be the need for an additional and separate coaxial lead back from the gramophone amplifier to the extension speaker.

Self Contained Radio

The main objection to the above scheme is the need to go to the lounge to switch on when radio is needed in the living room. The disadvantage of such action in reverse was not considered to be scrious because the need for radio in the lounge was less frequent.

Of course, the system could be elaborated. It would not be difficult to arrange for mains to be switched on a both equipment positions by operating one switch at either end, using the well-known changeover switch technique found in practically every house to switch on or off a light, say, from the top of bottom of the stairs. The tuner could be switch tuned and the switch could be relayoperated so that remote control of tuning would be practicable.

At this stage one begins to wonder it if would not be better to duplicate the radio equipment at the gramophone end.

Finally, it was decided to provide a separate amplifier for the radio in the living room so that the radio there was self-contained and could be completely operated from that room. Provision was to be made to feed signals between rooms only to allow the radio output to be heard in the lounge and to allow gramophone reproduction to be heard in the living room.

The Method Adopted

The method of connection finally decided npon, is given in Fig. 5. A radio/gramophone switch is wired between output transformer and speaker at each end. If the living room equipment is switched to radio and the lounge equipment is switched to —continued on page 931

TEST GEAR accessories

Part 1

MANY of the cheaper type of test instruments are sold today without any form of accessories such as test leads, dummy aerials for signal generators, diode detector probes for use with oscilloscopes, signal tracers, etc., or cathode follower probes. Often they are not even available as an extra, although they may be absolutely essential for the correct operation of the instrument.

The constructor, too, is often faced with a similar problem after having built an expensive piece of apparatus and then not being able to complete it properly.

TEST LEADS

A large number of the problems associated with test leads are matters of individual requirements and, accordingly, the experimenter must use his own ingenuity.

However, it should be said that there must be available a large number of test leads of all types. Good. well-insulated components and flex (preferably not solid core wire) should be used throughout. Remember that it is definitely a mistake to make leads too long, since they invariably manage to form the most unbelievably complex knots as

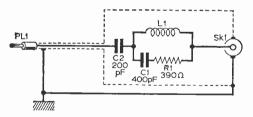


Fig. 1: The circuit of the dummy aerial unit.

COMPONENTS LIST FOR DUMMY AERIAL UNIT RI 390 Ω carbon composition IW 400pF midget ceramic 200pF midget ceramic CI C2 SK1 coaxial socket PL1 coaxial plug Lt 40 turns 28s.w.g. on $\frac{1}{4}$ in. former (see text) Miscellaneous: One 7-way tagstrip. 2 yards coaxial cable. Screening can (Denco (Clacton) Ltd.). Nuts and bolts, etc.

BY C. MACKAY

well as acting as most efficient aerials for picking up mains hum and other forms of interference,

THE DUMMY AERIAL

When the front end of a receiver is being aligned with the aid of a signal generator the impedance of the source must be the same as that of the aerial. To make this so a matching network called a dummy aerial unit is placed between the signal generator and the receiver.

The circuit of such a dummy aerial unit constructed by the author is shown in Fig. 1.

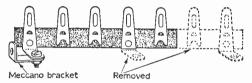


Fig. 2: The dummy aerial tagstrip,

The unit was constructed in a small coilscreening can made by Denco (Clacton) Ltd. It is normally supplied with their Maxi-Q range of coils but is also available separately.

The can is cylindrical, $1\frac{7}{16}$ in, in diameter, $2\frac{3}{16}$ in, high, with a screw-on lid. The size of the can is unimportant and a different type can be used equally well.

CONSTRUCTIONAL DETAILS

It is advisable to construct the coil first. The original was made out of a short length. of insulated spindle extension rod about 14in. long and 4in. in diameter. On it are wound 40 turns of 28s.w.g. wire so as to occupy 1in. of the former. The coil is then made tight and the whole component covered in polystyrene cement or some similar substance.

Now we start in the screening can. A tagstrip on which the components will be mounted is to be bolted vertically to the underside of the lid of the can as follows:

First drill a hole about 4in. in diameter in the centre of the lid, then drill two 6B.A. holes to suit the coaxial socket used.

The tagstrip is a seven-way type, three contacts having "earth" bolt holes. At one end only a two-tag section is sawn off, leaving a five-way tagstrip. The central earth tag has the bolt hole section either bent up double or removed (see Fig. 2). To the third and now only remaining earth bolt hole is attached a right-angled bracket of the Meccano type (may be bought in any good toy shop).

The tagstrip bracket assembly is then bolted under one coaxial socket bolt and wired up as follows (see Fig. 3):

The tags are numbered as in Fig. 3, tag 1 being earthed.

First take a short length of wire and join tag 2 to the central connector of the coaxial socket. Wire R1 between tags 2 and 3, C1 between tags 3 and 5, C2 between tags 4 and 5 and L1 between tags 2 and 5.

CONNECTIONS FOR OPERATING

A hole is now drilled in the main part of the can in the centre of the base to take the connecting cable to the signal generator. This cable, with a coaxial plug attached, is passed through the hole in the can. The inner of the cable is soldered to tag 4 and the outer of the cable to earth (tag 1). The two halves are now carefully screwed together, taking care that no components touch the side of the can.

The unit is now ready for use.

Wiring for Sound

-continued from page 929

gram (the nsual state of affairs) the signals at each end pass to the local speaker without involving the coaxial leads.

However, the radiogram switch at each end has a second bank of connections whose purpose is seen to be to switch in a resistance dummy load into the circuit of the equipment not being called upon to deliver a signal. In the case of the switch positions referred to above these resistive loads are applied at the remote end of each coaxial cable.

Thus the switching is comparable to that in Fig. 1 in that in all permutations of switching a half of the output power of each equipment—radio and gramophone—is fed to each room whether it is used there or not. At each end the signal not in use at any time is dissipated in the resistance at that end.

Thus it follows also that the load is a half of what it would be if the switching had not been introduced. This and the halving of power should be remembered when connecting up the other equipment.

Looking again at Fig. 5 it will be seen that both

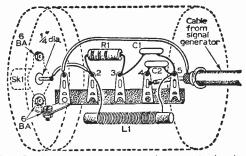


Fig. 31 Wiring and mounting the tagstrip bracket.

WARNING

If the above unit is to be used with "live" chassis equipment the signal generator should be isolated from the mains and the chassis of the generator must not be earthed. Care should also be taken to ensure that the "live" chassis to be tested has the neutral side of the mains connected to the chassis.

Part 2 appears next month

ends can take radio simultaneously, in which case the resistors are in parallel and across the gramophone output. The gramophone equipment need not be switched on, of course. Similarly, both ends can take gramophone.

The final permutation permits each end to take the signal from the remote end, thus feeding the the gramophone output to the living room and radio output to the lounge, in which case the resistors are applied as load to the local ends.

The important point to realise is that all these permutations apply comparable loads at each end (it is assumed and it should be so arranged that the nominal speaker impedances at both ends are the same) and consequently there will be no apparent change in reproduction at either end when the switch is operated at the other.

Little need be said about the methods of construction. The switch can be mounted at each end at a suitable position and the wiring could be supported by the switch. It would be preferable, however, to make up a unit on a little aluminium chassis containing the switch sockets to take the two coaxial terminations and connections for the speaker and output transformer connections.

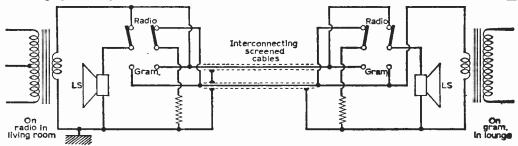


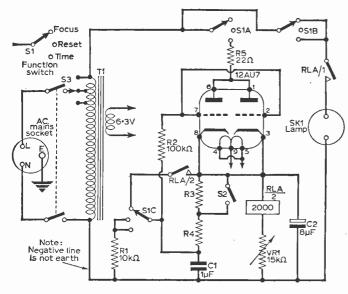
Fig. 5: The radio/gramophone interconnections.

PHOTOGRAPHIC TIMER

This simple design will provide a very functional piece of equipment

HIS simple timer gives time delays from 0.5 second to 60 seconds in two continuously variable ranges, each with a linear scale, and has a reasonable compensation for wide changes in mains supply voltages, so giving, when used as a photographic timer, near constant exposure factor by automatically making the actual switching time a function of the lamp brightness.

Using the specified type relay, normal enlarger bulbs up to 150W rating can be adequately



switched, and although the top limit of 60 seconds may not in all cases be sufficient, the exposure set can be repeated if necessary, or the experimenter may increase the range by the addition of an extra capacitor or resistor. This will be dealt with later in the article.

Few Components Required

The complete circuit diagram is shown in Fig. 1 from which the simplicity is at once apparent. No mains rectifier is required as such as the valve used

By S. A. KNIGHT

provides its own rectification in addition to its function as the timing control, and the only major components apart from this are a heater transformer capable of supplying 6.3V at 0.3A and a Post Office type 3000 relay, which is readily available on the surplus market.

Note that as the a.c. mains supply is applied directly across the valve circuit, the entire wiring of this circuit must be insulated from any exposed metalwork.

Limitations of Simple CR Circuit

Nearly all timing devices depend upon the charge of a capacitor through a resistance, where the time constant of the combination is given by CR seconds. The major disadvantage of such a basic system is the fact that the charge is not linear with time, and when it is used to

Fig. 1: The simple circuit of the timer. The values of R3 and R4 are found by experiment (see text).

trigger off the control valve circuit, the scale used to indicate the time delay in seconds exhibits severe cramping at one end or the other of its rotation. For the charge to be linear, the charging current into the capacitor requires to be constant, and the rise in voltage across the capacitor terminals then increases proportionately with time.

The second failing of the simple C and R charging circuit is the fact that long time-constants call for large values of capacity and resistance, making the assembly hulky. The use of electrolytics is generally precluded from charging circuits where good stability is required, and paper capacitors of large capacity are not only bulky but expensive.

It will be seen from the circuit of Fig. 1 that the charging capacitor C1 is a 1μ F and that the charging resistors R3 and R4 are standard $\frac{1}{4}$ W types of a few megohms.

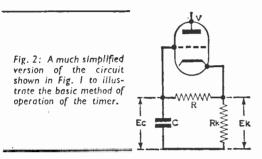


934



Circuit Operation

To understand the operation of the circuit, a simplified diagram is shown in Fig. 2. Here the valve V is effectively a cathode-follower, where, for sharp cut-off valves, the voltage Ek developed across the cathode resistor Rk is nearly equal to the voltage Ec developed across the capacitor C. The small difference existing between grid and cathode, Ek-Ec, depends on the actual valve characteristic, but it has a finite value and capacitor C is consequently charged very slowly from this small potential difference.



The important thing is that this voltage across R is substantially independent of other potentials and so the current through R has a constant value (Ek - Ec)/R. The capacitor is therefore charged at a constant rate and the voltage rises across it linearly with time. This arrangement overcomes the difficulties experienced with the simple C and R circuit which has an exponential charge curve and requires bulky components for a long delay.

The actual operation of the whole circuit of Fig. 1 is rather more involved than the simple explanation given above, hut the basic theory obtains. The valve acts as a rectifier to the a.c. mains supply, developing a d.c. voltage across the variable control VR1 and the relay coil RLA, smoothed by the electrolytic C2. The grid "follows" the cathode potential so that, when the switch S1C moves to the "Time" position and removes the $10k\Omega$ shorting resistor from capacitor C1, this latter begins to charge by virtue of the small grid-cathode potential existing across R3-R4.

As the charge proceeds, the grid moves progressively away from the cathode potential, and after a certain interval. determined by the setting of VR1, sufficient valve current flows to operate the relay. Contacts RLA-1 then open, extinguishing the lamp, while contacts RLA-2 close, shorting out the resistors R3, R4 and clamping the relay fully.

To reset the operation, the switch S1 (which has three poles) is moved to the centre position, discharging C1 through R1, and breaking the anode supply to the valve. The relay then drops out, in readiness for the next charging cycle.

Construction

There is nothing critical about the layout of this circuit, and no details need be given therefore of the actual mechanical arrangements. The timer is easily assembled in a small case and builders will suit themselves on the details of appearance. It must be noticed, however, that the "earth" line is NOT chassis, and that the case, if metal, must be isolated from this negative line, being earthed back through the mains supply third pin. Particular care should be taken to ensure that the case of capacitor C2 is insulated from the chassis, especially if it is of the type where the case and negative terminal are commoned.

The Function Switch

The three-pole, three-way switch S1 is a standard wafer type, not a midget variety however, and if a ceramic wafer can be obtained so much the better. This switch gives three positions as indicated in the diagram, namely FOCUS, RESET and TIME. In the FOCUS position, the lamp is connected directly across the mains, and is used in this position when setting up and focusing of the enlarger is necessary.

In the RESET position, the lamp is extinguished, the charging capacitor shunted by the $10k\Omega$ resistor R1, and the valve anode supply is broken.

When switched to TIME, the lamp will light, and remain lighted for the duration of the charging cycle after which it will extinguish and remain so until the following exposure is prepared. Provided that about one second is allowed to elapse while the switch is at the RESET position, the following timing will be unaffected by the period at which the reset is actually switched.

The Post Office type 3000 relay has a 2000 Ω coil and two pairs of contacts, one pair normally open (RLA-2) and one pair normally closed (RLA-1). The pair RLA-2 should close *just before* the pair RLA-1 open. The lamp contacts RLA-1 should preferably be of the "heavy duty" type, although two "light duty" pairs have been used by the writer for many months without adverse effect,

		COMPON	IENTS L	IST
Resisto	10k Ω R4	see text 22 Ω		n es: 3-pole, 3-way wafer switch (Oak-NSF) S.P.S.T. toggle switch
R3	$\begin{array}{llllllllllllllllllllllllllllllllllll$	ZZ 14	S3 Misce	D.P.S.T. toggle switch Haneous:
VRI	VRI ISk Ω wire-wound potentiometer (Colvern CLR 3001)			P.O. type 3000 relay, 2000Ω coil. Two sets of contacts; one normally open, one normally closed
Capacitors: Cl IµF paper 350V			Heater transformer, Primary 200-250V. Secondary 6.3V 0.3A	
C2	$B\mu F$ electrolytic 450V		. VI	I2AU7 or ECC82

Setting Up

The timing ranges are determined by the values of R4 and R3, the latter being shorted out by switch S2 for the lower range.

With the unit connected to the mains supply and S2 closed, set the control VR1 to a maximum, that is all registrance in circuit. True

is. all resistance in circuit. Try a resistor of value between $2.2M\Omega$ and $3.3M\Omega$ for R4 and on switching to TIME, check for a period of about 10 seconds, using a stop watch or the second hand of a

is adequate overlap between the ranges. The values for R3 and R4 thus found, they should be permanently wired into the circuit, R3 going across the range switch S2. An idea of what the completed panel of the unit should look like, with a calibrated scale, is shown in Fig. 3.

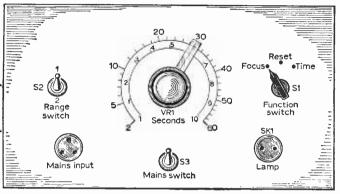


Fig. 3: A suggested layout of controls for the front panel of the instrument.

watch. When a value has been found that will give a maximum of about 10 to 12 seconds, the rest of the scale can be calibrated

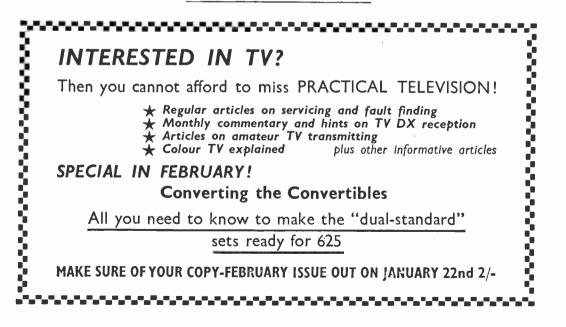
down to a lower limit of about 0.5 second. Note that the extreme lower part of the scale will be indeterminate, the lowest consistent timing being obtained with about one-eighth travel of the control in circuit.

Now connect a further resistor of about 6.8 to $10M\Omega$ in scries with the value for R4 already used, and with the control again at maximum, check the timing to get a value of about 60 seconds. When this has been done, the rest of the scale can be calibrated as before; this time a lower limit of about 3 to 5 seconds will be obtained, so that there

Extending the Range

For longer timings, C1 may be increased to 2μ F or higher, but an electrolytic should not be used here, only paper of 350V working or higher, and of best quality. Similarly R3 and R4 may be increased to give higher ranges.

All resistors may be 4W rating, though higher ratings may be used if readily to hand. The valve should be of a type such as the 12AU7 (ECC82) using a B9A base, or the 6SN7 or equivalent in the octal series. The two triode sections in these valves are strapped across to make a single triode.





MEDIUM WAVE RECEIVER

C3

C4

C5

C6

C7

C8

TCL

100pF mica or cerámic

25µF electrolytic 25V

16µF electrolytic 350V

16µF electrolytic 350V

VCI 500pF air-spaced variable

5-40pF trimmer

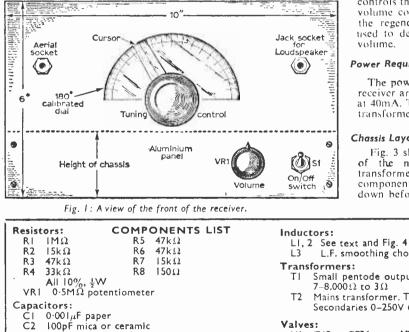
0.01µF paper

0.01µF paper

An inexpensive two-valve circuit

THIS receiver was designed to give enough power to operate a loudspeaker and yet use -few inexpensive and readily available components. It is therefore ideal for beginners to construct.

Fig. 1 shows the front view of the receiver, but the front panel can be omitted if desired. In the prototype it was found that a slow-motion drive was not required as there was good separation between the stations. This set is quite sensitive and



By D. G. HARDING

it will pick up Radio Luxembourg and many other Continental stations as well as local stations.

Circuit Detail

The circuit (Fig. 2) is very simple and uses only two valves. V1 (Z63) is the r.f. amplifier and detector. V2 (6J5) is used as the a.f. output valve.

To increase sensitivity, regeneration has been used. By this system some of the r.f. signal at the anode of VI is inductively coupled back to the grid circuit by L2. The amount of regenera-tion is determined by the position of VR1, which

controls the gain of this stage. No volume control has been used as the regeneration control can be used to decrease or increase the volume.

Power Requirements

The power requirements of this receiver are 6.3V at 1A and 250V at 40mA. This means that a small transformer can be used.

Chassis Layout and Wiring

Fig. 3 shows the chassis layout of the main components. All transformers and other major components should be bolted down before wiring commences.

L.F. smoothing choke 10-15H 60mA T1 Small pentode output transformer: 7-8.000 Ω to 3 Ω Mains transformer. Tapped primary. Secondaries 0-250V 60mA; 6.3V IA

Valves:

VI Z63 or EF36 V2 L63 or 615

- Miscellaneous:
 - MRI Selenium rectifier DRMIB or DSMI (Brimar) \$1
 - S.P.S.T. toggle switch
- Chassis I0in. x 6in. Two octal valveholders. Terminal strip. Jack socket.

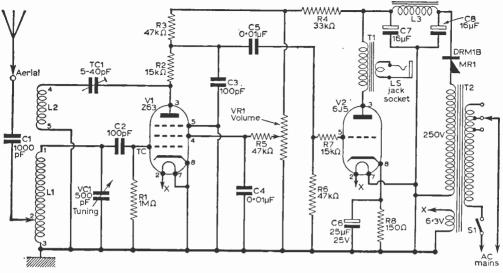


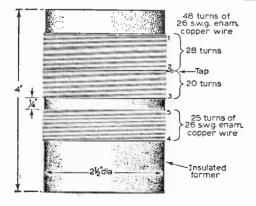
Fig. 2: The simple, two-valve circuit.

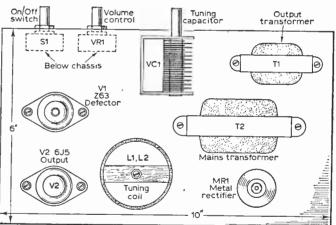
The wiring is straightforward and should present no difficulties but a point worthy of note is that the electrolytic capacitors must be connected the right way round with the red tag connected to h.t.+ and the black tag connected to h.t.-.

Coil Data

The coils used in the prototype were wound on a former $2\frac{1}{2}$ in. in diameter. At the time of construction a $2\frac{1}{2}$ in. custard powder

- Fig. 3 (right): The layout of the major components on the chassis.
- Fig. 4 (below): Winding details of the coils.





carton was used as this was the only former available. L1 is wound at the top of the former and consists of 48 turns of 26s.w.g. tapped at 28 turns from the start. L2 consists of 25 turns of 26s.w.g. enamelled wire spaced 4in, from L1 (see Fig. 4).

Alignment

A good aerial and earth are required to operate this receiver. When both of these have been connected the set may be switched on.

With the regeneration control VRI set about midway, VC1 is now rotated until a station is received. There may be violent oscillations and if this happens VRI must be turned anticlockwise. The trimmer TC1 is now carefully adjusted so that smooth regeneration can be obtained at all positions of VRI: If the set is aligned correctly there should be good volume and little distortion.





SEE that an eminent Q.C. has proposed that statements made to the police by accused persons should be tape recorded, and that this recording should be played back in court and used as evidence, in place of the normal written and signed statement.

While I can appreciate that this suggestion is put forward as being in the interest of the individual concerned in a charge, I admit being a little worried about the implied immunity from interference which one supposes is the chief reasonthat has prompted this recommendation. It has been stated that special recorders without erase or rewind facilities would be employed and that the tape itself would be enclosed in a plug-in cassette; in this not edite way the recorded tape inaccessible and \$0 could not be cut and edited or otherwise tampered with. Nevertheless there would still remain the possibility of complete erasure if the cassette was brought near a strong magnetic field, although such a possibility is not, maybe, a serious objection since the presentation in court of a blank tape would prove highly embarrassing to the police.

As a further guard against electronic tampering it has been suggested that the original recording could embody a coded signal possibly at supersonic frequency, but this would complicate the equipment somewhat.

What is Your Verdict?

Assuming all these technical problems can be solved so that the security of the recording is no longer in doubt, will it be easy to convince the public that this is so? Remember that tape recorders are widely used by all kinds of people nowadays, and the creation of unusual sound effects by tape trickery is now a common pastime for many amateurs. Will this "inside" knowledge of recording techniques and the appreciation of

our Wavelength **By THERMION**

how flexible this method of recording is help to promote confidence in the minds of these members of the public when it appears a question of conviction or acquittal may depend upon a tape replayed in court? It would seem not.

This psychological aspect is, I submit, extremely important. Before such a system is adopted in courts of law it is essential that it be demonstrated to the public at large that it is, beyond all reasonable shadow of doubt, proof against interference.

Mains Connections

The need for rationalisation of colour coding for mains leads has been accepted by many countries, but the implementation of international agreements takes time. In the meanwhile a great variety of electrical appliances have been imported into this country and quite often the mains connections are at variance with our method of coding, i.e. red-live, black-neutral and green-earth.

Dangerous situations can arise particularly in the case of equipment of German origin since in that country it was common practice until recently to use the red lead for earthing purposes.

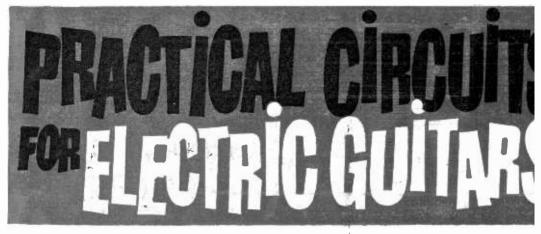
Before putting any imported equipment into service the obvious course is to examine the mains lead connections at the appliance itself, and to change these over if necessary in order to conform with British practice. If this cannot be easily per-formed, a suitable label bearing the identification of the three conductors should be tied to the plug end of the cable; this will be a future reminder, to other users, if not to you.

To Earth, or Not to Earth!

The use of double insulation for portable appliances is becoming increasingly common. For those not familiar with this term, it describes a method of construction where any exposed metal work is completely insulated from the remainder of the assembly-this protective insulation being quite separate from and additional to the functional insulation associated with the current carying parts.

Such appliances require only a two-core cable; no earthing connection being needed. Vacuum cleaners, shavers and clocks are typical examples. The 1963 Amendments to the Regulations for Electrical Equipment of Buildings issued in December last year by the Institution of Electrical Engineers extend further the list of domestic appliances that now may use the double-insulation method of construction.

Familiarity with double-insulated appliances must not, of course, blind us to the vital importance of properly earthing the outer metalwork of all apparatus having only single insulation.



GUITAR AMPLIFIER, PRE-AMPLIFIER AND PICK-UP (

ECTRIC plectrum guitars employ magnetic pick-ups which are usually situated just beneath the steel strings. Acoustic instruments, i.e. those with a normally shaped hollow body, can easily be converted for electric operation by fitting suitable "pick-ups". The more modern version of the plectrum guitar may have a solid body and therefore the sound must be produced entirely by means of a magnetic pick-up and amplifier. These observations apply also to Hawaiian guitars constructed from solid wood.

Magnetic Pick-ups

However, the principle of electrical operation for both plectrum and Hawaiian guitars is the same: the steel strings are made to interrupt a magnetic field, thus creating small electric currents which can be amplified in the same way as those from a gramophone pick-up or a tape recording head. The construction of sensitive magnetic pick-ups is somewhat tedious and it is cheaper in the long run to purchase these ready made. Excellent pick-ups with a high degree of sensitivity can be obtained from most large musical instrument dealers.

Control

As with any device which transforms mechanised vibration to alternating electric currents, subsequent amplification is usually required. The signals produced by such devices can also be modified electrically: this means that various forms of tone control can be applied and other effects introduced before or during amplification.

The position of the pick-up(s) relative to the strings and the bridge, for instance, has considerable effect on the harmonic content of the output, and therefore the overall tone. To make the most of this two, and sometimes three, pick-ups are employed, as shown in Fig. 1. The pick-up nearest the bridge produces a thin, hard tone, the one nearest the fret board a deeper and more mellow effect. In addition to this variable electrical tone control may be applied as well as

REFERENCES I AND 2

Electronic Music and Musique Concrête, by F. C. Judd, A.Inst.E. (Neville Spearman Limited). Radio and Electronic Hobbies, by F. C. Judd, A.Inst.E. (Museum Press). suitable volume control and/or fixed attenuation for "solo to rhythm" playing.

Control Circuits

Electrical circuits may be employed for the modification of an acoustic plectrum guitar or

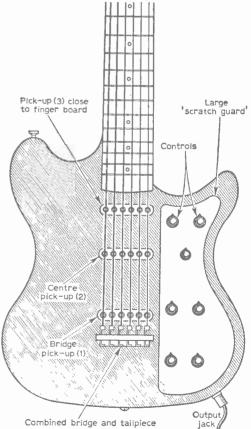


Fig. 1: The layout of controls and pick-ups on a modern guitar.



VTROL CIRCUITS DESCRIBED BY F. C. JUDD

incorporated in home-constructed Hawaiian guitars (Refs. 1 and 2).

The control system of Fig. 2 is for tone and volume control with a single pick-up and the few components can be mounted on the "scratch guard" or an extension of it. A rhythm switch has also been included (S1).

Component details are given in the circuit and so long as screened interconnecting leads are used where indicated there should be no problems with induced hum. As an extra precaution against this the underside of the scratch guard or an extension of it may be lined with thin aluminium or tinplate which must be earthed to the common earth of the output lead. (Note: The output lead to the amplifier must, of course, be screened.)

Control for Three Pick-ups

The circuit of Fig. 3 is for three pick-ups, although this could be modified for two if required. It provides for independent volume and tone control over each pick-up, either of which may be selected by the ganged switch SI, S2 and S3.

and S3. A "rhythm switch" S4 and S5 has also been included. This brings a fixed attenuator into circuit, thereby reducing the output automatically for "rhythm" or chord playing. This control system does, of course, require more space but with careful layout can be built into a large "scratch guard" as in Fig. 1.

Tremolo Control

In *Practical Wireless*, February, 1961, the author described an electronic tremolo unit which could also serve as a guitar preamplifier.

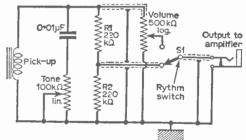
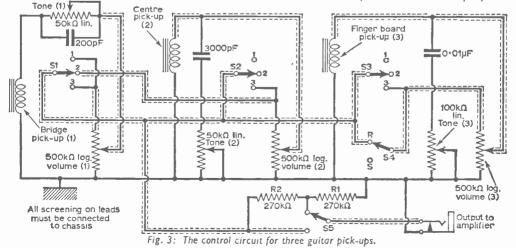


Fig. 2: A tone and volume control circuit. (Note: reducing the value of R2 will reduce the output.)



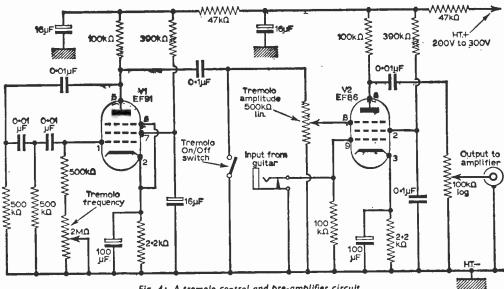


Fig. 41 A tremolo control and pre-amplifier circuit.

One of the greatest problems with electronic tremolo is the familiar "thump" caused by harmonics from the tremolo oscillator, which operates on a fundamental frequency of 6 to 10c/s. The circuit shown in Fig. 4 is a much modified version of the one which appeared in the Practical Wireless article mentioned above. (Those who have already built this unit could modify it quite easily to the new circuit.)

The tremolo oscillator VI employs the familiar phase shift circuit and almost any modern h.f. pentode will operate-viz.: EF91, EF80, etc. The

preamplifier V2 must be an EF86 because the tremolo signal is applied to the suppressor grid (G3).

The tremolo amplitude is controlled by VR2, but remember that beyond a certain point " thump " might be apparent due to excessive level. Tremolo frequency is controlled by VR1 and the output from the preamplifier by VR3. Because of the high gain of V2 the output voltage from the preamplifier is quite considerable. The gain

-continued on page 961

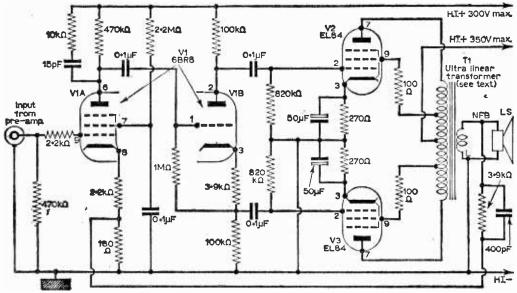


Fig. 5: A power amplifier circuit for electric guitars.

A DOOR INTERCOM

A simple yet versatile piece of equipment

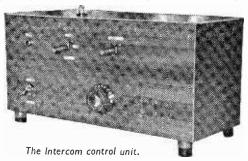
By P. HENDERSON

HIS unit was designed for an upstairs flat to avoid tiring journeys up and down stairs in order to answer the door to callers. It allows for two-way conversations between the living room of the flat and callers at the front door, by way of an amplifier unit and an extension loudspeaker unit, the latter being installed outside the front door. An additional facility is provided, namely that the door can be unlocked from upstairs when required.

The Amplifier Unit

The basic unit is a two-stage high-gain amplifier, using a 6SH7 resistance coupled to a 6V6 in a simple manner as shown in Fig. 1. The switch S1 connects the unit to any number of separate extentions as well as to the front door. In the prototype for example, there is an extension to the garageworkshop. A relay RLA with a high impedance coil that is actuated from the h.t. line of the amplifier through a suitable ballast resistor when the "press-to-talk" switch S3 is closed, controls the changeover from "Listen" to "Talk". This relay is equipped with two sets of changeover contacts.

is equipped with two sets of changeover contacts. Resistors R6 and R7 act as "ballast" for the relays RLA and RLB respectively; their values must be determined by experiment. The connections to and from the relay contacts should be carried out using screened cable to minimise hum pick-up. No feedback is incorporated in the ampli-



fier, and the unit is quite stable after the addition of the 0.002μ F mica capacitor C9 across the primary of T2. The design of the amplifier cabinet is not critical. As very little heat is liberated during the quiescent period, only a fair degree of ventilation is required. The power unit is shown in Fig. 2.

Extension Leads

For the door extension, three-core wire is used, two cores feeding the speaker, and the remaining core, together with one of the speaker leads as

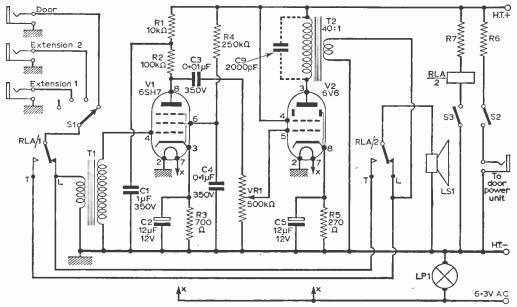


Fig. 1: The two-stage amplifier circuit.

common, supplies the feed from S2 to the relay RLB in the l.t. power unit. See Fig. 3 and Fig. 4. All other extensions require only twin feeds.

Door Loudspeaker

In the author's installation, a surplus Tannoy speaker unit was pressed into service. This speaker is mounted outside the front door in a suitable position in its original case. However the terminals on the outside are ignored as they feed a transformer and a capacitor, both of which are not used in this unit now.

The supply to the speaker is connected directly to the speaker leads, and the speaker itself is

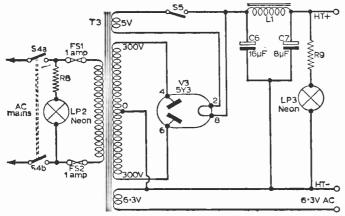


Fig. 2: The power pack circuit.

enveloped in a polythene bag to make it more weatherproof. Although the Tannoy's impedance is actually 7Ω , the mismatch does not appear to cause trouble, as callers are clearly heard even at considerable distances from the speaker.

Method of Operation

In the "Listen" position, the loudspeaker outside the front door acts as a microphone and feeds its signal to the primary of T1 through contacts RLA/1 in the "L" position. The signal is amplified, the gain being controlled by VR1, in the usual manner. The output transformer T2 conveys the audio signal to the amplifier loudspeaker LS1 by way of contacts RLB/2 in the "L" position.

An elliptical loudspeaker is used in the author's main control unit. This loudspeaker is mounted facing upwards, and one speaks down to it, with very satisfactory results.

When one wishes to know who a caller is, the press-to-talk switch S3 is closed, and so relay RLA is energised and the contacts "1" and "2" are set to the "T" position. The loudspeaker LS1 in the amplifier now acts as a microphone, and its output is fed to the primary of T1, and the signal from the amplifier is fed to the door loudspeaker LS2 through the output transformer and S1.

Each morning the mains switch S4 is switched on and the heaters of the 6SH7 and the 6V6 are thus supplied with current. The unit is left in this state ready for use, all day, as consumption is quite small, and the unit is then always ready for immediate use. When the door bell rings, one closes the switch S5, and the current is fed to the heaters of the 5Y3 rectifier. This being a directly heated valve, h.t. is applied to the amplifier after a delay of only five seconds or so. A neon indicator V5 connected to the h.t. line indicates when the h.t. is applied, and one can then speak.

A similar neon (V4) is used to indicate that the mains is switched on to the unit: alternatively, a 6.3V dial lamp can be wired into the heater circuit.

Remotely Controlled Door Lock

Although knowing who is at the door is a great help, it is still often necessary to go downstairs to open the door to allow the caller to enter. This

unit allows a modified Yale type lock unit to be unlocked from upstairs (or any other distant position) as well. A Yale type lock is installed in the usual way. if not already fitted, but the lock case is altered as shown in Fig. 5.

A small hole is cut in the case, and a short length of screwed rod is connected to one of the "legs" of the lock mechanism, and the other end is connected to the solenoid plunger.

The solenoid itself is made from a car indicator arm solenoid. The original windings are removed, and 85z. of 20s.w.g. enamelled copper wire wound on to the original former. Two cardboard or formica "cheeks" will be needed to contain all the new wire within the length of the

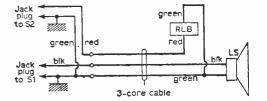


Fig. 3: Interconnecting wiring for the door extension.

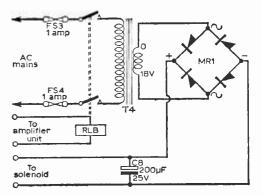
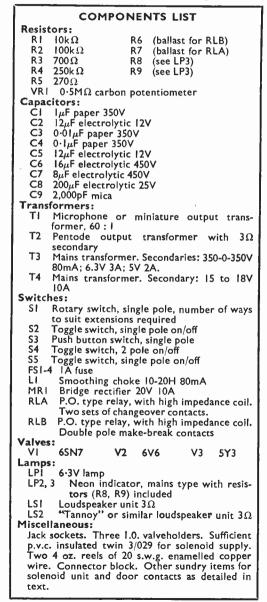


Fig. 4: Wiring between S2 and the l.t. power unit.

former. The ends of the windings are taken to a small connecting block. The remote end of the solenoid is screwed to the inside of the door, using washers to space the solenoid off the door so that the solenoid plunger and lock mechanism is free to move and does not bind.

The solenoid is energised by a l.t. supply unit, as shown in Fig. 4. This unit supplies sufficient d.c. to energise the solenoid, ensuring a certain and small withdrawal of the lock tongue.

The supply from the l.t. unit to the solenoid is carried out in mains type twin 3/029 in order to minimise volt drop due to the heavy current drawn by the solenoid. The lead is carried up the inside



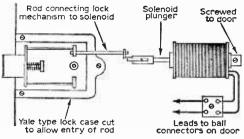


Fig. 5: Modifications to the Yale lock.

edge of the door frame (see Fig. 6(b)) and each core supplies its own brass contact strip, as shown.

The supply is picked up from these two strips by a pair of small spring-loaded balls in brass cases used as ball and socket door catches. These are fitted as near to the outside face of the front door as shown in Fig. 6(a). The holes to accommodate the catches are drilled well into the door frame, so that small holes may be drilled from the inside of the door to meet them.

Wires are soldered to the rear of the ball holders as in Fig. 6(c) and the leads are lead through the communicating holes, and the leads connected to the connecting block to complete the supply circuit.

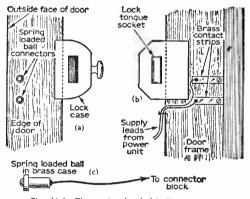
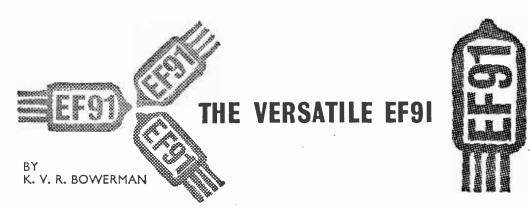


Fig. 6(a): The spring-loaded ball contacts. Fig. 6(b): Fitting the solenoid supply lead. Fig. 6(c): Wiring to the ball contact holders.

It will be appreciated that the supply to the solenoid will cease when the door has been pushed so far open, and the balls lose contact with the brass strips, but this is of no consequence, as by then the tongue of the lock will be well clear of its socket on the door frame.

When S2 on the amplifier is closed h.t. current energises RLB in the l.t. supply unit, switching on the mains supply to the transformer T4. This transformer supplies about 10A and 15-18V to a 10A bridge rectifier. (The 200μ F capacitor is not essential, but does eliminate the a.c. hum from the solenoid.)

The complete l.t. unit is situated as near to the door as possible so as to keep the supply lead short.



NE of the cheapest and most efficient pentode valves obtainable is the EF91. This valve has a large number of "aliases", among them 6AM6, 8D3, 6F12, Z77 and CV138, and it can be obtained for as little as 1s. 9d. from advertisers in this magazine.

Designed as a high-slope r.f. pentode, the EF91 is, in fact, far more versatile than this might suggest. It operates well at any frequency and appears to be quite tolerant about operating conditions, and consequently, lends itself well to every kind of circuit. E.M.I. even used it in early television receivers as a sound output valve. The purpose of this article is to give two

The purpose of this article is to give two examples of simply constructed equipment, quite suitable for beginners, which work extraordinarily well and cost very little to make. If you have a well-stocked "junk box", so much the better.

EF9I Switched Superhet

The first piece of equipment to be described is a switched superhet receiver for a.m. Three stations can be selected and, in the prototype, these were the Light Programme on 247m., the Home Service on 330m., and the Third Programme on 464m. Of course, any three stations in the medium waveband .can be brought in as required. A modification described later enables one long wave station to be substituted for one of the medium wave stations, if necessary.

The Superhet Circuit

Five EF91 valves are used in the receiver shown in Fig. 1(a).

The r.f. signal appears across the ferrite rod winding and is tuned by TC1 alone, or TC1 plus TC2, or TC1 plus TC2, plus TC3, depending on which station is required. The tuned signal is fed to the control grid of V1.

V2, strapped as as a triode, acts as the local oscillator. The oscillator coil L2 is tuned by TC4, or TC4 plus TC5, or TC4 plus TC5 plus TC6, depending on which station is required. The oscillator signal is fed via the very small capacitor C2 to the control grid of V1, this latter valve thus acts as a mixer. This system, unconventional though it may be, nevertheless works extremely well.

A number of complex signals now appear at the anode of V1, including the i.f. The i.f. transformer.

T1, selects the required signal and feeds it to the grid of V3. This valve operates as a straightforward, conventional, i.f. amplifier. The amplified i.f. signal now finds it way via C8 and R7 to the grid of V4.

Strapped as a triode, V4 is wired as a "leaky grid" detector, mainly because this is simple to set up and is very sensitive.

The detected audio signal now appears across the volume control VR1, the slider of which is connected to the control grid of V5. This valve operates as an output pentode and drives the loudspeaker via T3.

The power pack is very simple (Fig. 1b). One secondary on T4 supplies the heater current, and another supplies the half-wave rectifier MR1. Choke L3 and the two electrolytic capacitors, C13 and C14, provide adequate smoothing and regulation.

C9 serves to remove any residual i.f. signal from the audio circuits. R12 and R13 may not be required, but can be fitted if there is a tendency to i.f. instability; their function is to broaden the tuning of the i.f. transformers so that they do not give too "peaky" a response which can lead to oscillation in the very high gain EF91 valves.

Construction

The chassis illustrated (Fig. 2) is considerably larger than necessary but was used merely because it happened to be on hand. Obviously a smaller chassis can be employed, so long as the components fit fairly well without overcrowding.

Layout is not critical, provided grid and anode leads are kept well away from each other and as short as practicable.

First, mark out the chassis and drill as necessary. Next, mount the valveholders (with a solder tag under one bolt on each), then the i.f. transformers, mains transformer, choke (if used), smoothing capacitors, rectifier and output transformer (Figs. 2 and 3).

Now fit the volume control, station selector switch and on/off switch.

The wiring can now be started. Solder the heater wiring first, tucking the "hot" lead well into the corners of the chassis. Next, wire the bias resistors and by-pass capacitors, together with the chassis returns for the heater and any other earth wiring on the valveholders. Don't forget to earth

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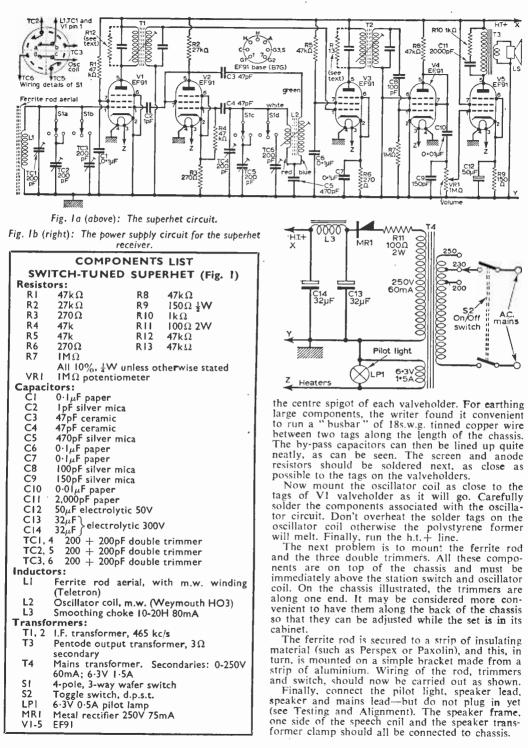
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Testing and Alignment

Before plugging in, test between the positive terminal of C14 and chassis with an ohmmeter set to a high resistance range. The needle should give a kick as the capacitor charges and then sink back to infinity (or at least $2m\Omega$). If the needle swings over to zero and stops there, there is a short on the h.t.+ line and the wiring should be carefully checked to find the fault. If all is well, however, plug in the mains lead and switch on. The pilot light and valveheaters should light up.

pilot light and valveheaters should light up. Set meter to 300V d.c. range and again apply it betwen the positive tag of C14 and chassis. The h.t. line voltage should be between 220 and 250V. This is not critical but if much above 250V, increase the value of R11. If all is well, proceed with the alignment, which is given below in numbered steps:

- 1 Switch on and allow set to warm up. Unscrew all trimmers. Set volume control three-quarters towards full volume. Set S1 to position 1.
- 2 Temporarily attach about a yard of wire to act as a "throw-out" aerial to the "hot" tag of TC1.
- 3 Using a screwdriver of insulating material (a piece of ebonite or Tufnol rod filed to a screwdriver point is ideal), slowly screw in TC4 until the Light Programme is heard faintly.

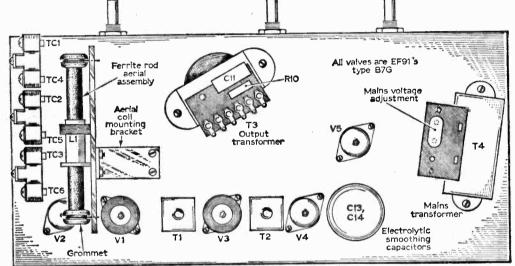


Fig. 2: The layout of components above-chassis.

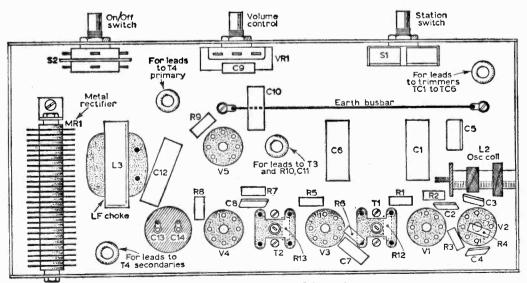


Fig. 3: An underchassis view of the receiver.

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PRACTICAL WIRFLESS

February, 1964



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- 4 If nothing is heard even when TC4 is screwed all the way from "fully out" to "fully in", give TC1 one turn clockwise and repeat 3.
- 5 As soon as the Light Programme is heard, remove the temporary wire aerial and adjust TC4, then TC1 for maximum signal, if necessary swinging the set round to orientate the ferrite rod towards the transmitter.
- 6 Switch S1 to position 2. Slowly screw in trimmer TC5 until the Home Service is heard.
- 7 Adjust TC5 then TC2 for maximum signal.
- 8 Switch S1 to position 3. Slowly screw in trimmer TC6 until the Third Programme is heard.
- 9 Adjust TC6 then TC3 for maximum signal.

Note that the Light Programme on 247 metres is not receivable in some localities. In these areas the long wave (1,500 metres) station must be brought in. This can be done by using a dual wave ferrite rod and an extra oscillator coil. The wiring modifications are shown in Fig. 4. the same principles in setting up apply.

Cabinet

The cabinet will, of course, depend largely on the shape and size of the chassis. The writer converted an old table receiver cabinet in somewhat crude fashion, see picture.

If the set is to do service in the kitchen it is usually possible to find a small space in a cupboard and build the set into that. Or a simply constructed cabinet made from 5-ply, carefully painted or covered with plastic material, often gives a surprisingly professional-like finish.

EF91 Push-pull Gramophone Amplifier

The circuit shown in Fig. 5 uses four EF91 valves and gives good volume and quality from a crystal pick-up. It is, of course, not in the hi-fi class, but it is ideal for "pop" records and gives reproduction well up to the standard of most "pop boxes". A simple top-cut tone control helps to get rid of surface noise on old records.

The Circuit Stage by Stage

The signal from the pick-up is fed through screened cable to the input terminals (these can conveniently be incorporated in a coaxial socket). The signal appears across VR1, which is the volume control. The slider of the volume control is connected directly to the grid of V1 which acts as a voltage amplifier. VR2 and C1 together form a simple tone control.

R2 and C4 provide automatic bias for V1, and R1 is the screen feed resistor. C5 forms the coupling between V1 and V2.

V2. strapped as a triode, is the phase-splitter. The anode load is split between R7 and R6. R6 being in the cathode line, and two equal signals but 180° out of phase appear, one at the "bottom" end of R7. the other at the "top" end of R6. These out-of-phase signals are fed via the coupling capacitors C7 and C8 to the control grids of V3 and V4.

The anodes of V3 and V4 are fed via the centretapped primary of T1, which is a push-pull output transformer.

The power pack shown for the switched superhet is quite suitable for this amplifier.

COMPONENTS LIST				
Additional Parts for L.W. Operation (Fig. 4)				
C5a	47pF silver mica			
TC3a	100pF ceramic			
TC6a	100pF ceramic			
Lla	Ferrite rod aerial, with I.w. and m.w. windings			
L2a S3	Oscillator coil, I.w. (Weymouth HOI) 3-pole, 2-way wafer switch			

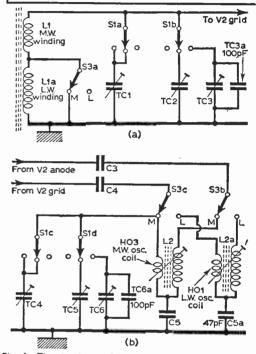


Fig. 4: The circuit modifications necessary to incorporate long waves.

Amplifier Construction

A chassis as small as 8in. x 10in. x 2in. should comfortably accommodate all components. Note that if the mains transformer is mounted on the same chassis as the choke and/or the output transformer, then the cores should be orientated at right angles to one another or separated by a metal screen (or screened by mounting one item under the chassis and another on top).

All earth connections should be made to an earth bus bar of thick copper wire (not less than 18s.w.g.) and this should be connected to chassis at one point only (the coaxial input socket). Heater wiring should be by closely twisted flex tucked well into corners of the chassis. All signal wiring up to the input to V1 must be in screened cable.

Testing

Test the power supply as for the superhet receiver then, after allowing the valves to warm up, turn the volume control up to full volume and

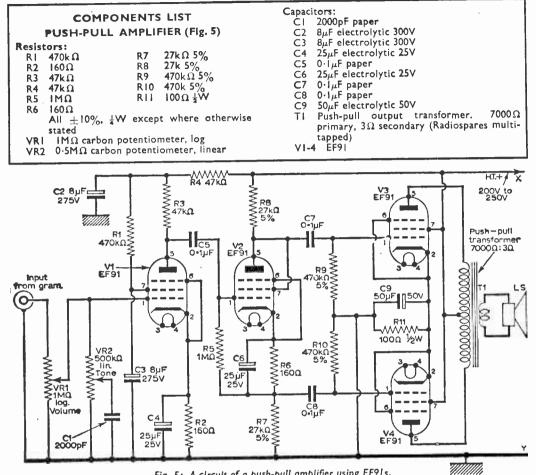


Fig. 5: A circuit of a push-pull amplifier using EF91s.

briefly touch the centre pin of the coaxial socket with a finger. A loud hum should issue from the loudspeaker. If this is reduced nearly to zero as the volume control is operated, and if the character of the hum is altered by the setting of the tone control, then all is well and the pick-up can be connected to the input.

Other Applications

It will be seen from the foregoing what a plendid little valve the EF91 is. One would be

hard put to it to find an application for which it could not be used!

The author has made a morse practice oscillator and a "valve voltmeter" type of alignment aid using these valves.

Other uses could be in photo-electric relay circuits as an amplifier, as a microphone pre-amplifier, or in a pre-amplifying mixer circuit for tape recorders.

The valve has also been used very successfully in v.h.f. f.m. applications described in this magazine.

"PRACTICAL WIRELESS" FILM SHOW THE

The "Practical Wireless" Film Show which is held annually and to which readers of P.W. are invited, is to be held, as before, at Caxton Hall, Westminster. The date and time of the Show, which is arranged in collaboration with Mullard Limited, is the 31st January, 1964, at 7.30 p.m. The programme will appeal to all readers of "Practical Wireless" and of especial interest will be the illustrated

talk on colour, 625-line and u.h.f. television, which will form the first part of the programme. After a break for refreshments, the programme will continue with a film entitled "Ultrasonics"

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Simpler Electronic MUSIC

A Guide for the Creative Tape Enthusiast By Lloyd Brunt

A Tone time or another most of us have felt the desire to be creative and, with an interest in sound, music is often the most satisfying outlet. Our mind perhaps first turns to a musical instrument, but most instruments are expensive and require many years of study for complete mastery.

The only other course, then, seems to be electronic music. Again the big problem is money, and electronic computers, and the other complex circuits connected with this form of composition are not the easiest things to obtain and understand!

Frustrated in this way, the author looked around for something within the reach of anyone with a limited budget a_{Jd} a small amount of talent. The only equipment necessary would be that which the ordinary tape recording amateur would possess, and the method that which even the least experienced person could easily master.

The idea devised is simple, yet can give pleasing results, even at the first attempt. A signal varying in frequency within the audio range is recorded in a continuous stream on to ordinary magnetic recording tape. The tape is then cut into lengths varying from about 1 to 5 in., and the pieces thoroughly mixed. A blank tape is also cut into varying lengths and kept separate from the recorded tape.

The pieces are then joined together on an editing block with, say, two recorded pieces and a blank, five recorded pieces and a blank, the length and the number of recorded insertions being left entirely to the whim of the individual.

On the author's first attempt, when a reasonable length was composed, it was found to give an amusingly jig-like tune, and after some substitution, a pleasant melody was compiled.

A problem that must be solved before any "composing" can begin is from where to obtain the varying signal. A signal generator, covering the whole audio range is the obvious and probably the most convenient answer, but it is not essential. The author found that by recording the tuning-in signal transmitted before the beginning of the day's programme on Network Three, several different frequencies were obtained. But this method limited the notes to the number of tape speeds, and was therefore unsatisfactory.

therefore unsatisfactory. An alternative, using the same transmission was found. The tape recorder is set to "record" but left in the "pause" position. The take spool is then turned by hand at varying speeds. As any speed can be obtained by this method it is found that when the tape is played back at a constant speed many varying notes are obtained, and with care and a little practice any frequency is attainable. The more musically minded may wish to be more precise and not compose "by accident". If a few basic rules of composition are adhered to, and the notes sorted into groups by the length and pitch, a passable piece of music can be easily compiled. It may even be possible to put together existing musical works by careful following of the score, but the author found that even to set out "Ba Ba Black Sheep" took a great deal of time and patience.

It was found that the quickest way to join the tape was by using "jointing tape" and that the weld joint took much too long to dry for this sort of editing. Leader-tape was first used between the notes but was later discarded in preference of blank tape because of the unnatural pause the former gave.

It must also be noted that the tape must remain the same way up unless used on a single track or twin channel tape recorder as inversion will cause the note to appear on the lower track and therefore disappear upon playback. This inversion was found to give a pleasing stereophonic effect on the author's twin channel recorder but it may be guarded against by using a tape with the manufacturer's name printed along its length, the inversion of the name indicating that the note is inverted.

If you are fortunate enough to have two tape recorders, the edited tape should be re-recorded on to a continuous length as a tape that is so edited will not play very smoothly. Two tape recorders may be used to obtain a rhythm by loading one with a continuous loop arrangement while adding the other notes to the other.

This by no means exhausts the possibilities of this type of recording and these notes are only intended as a guide; echo, superimposition, addition of everyday sounds, are just a few of the numerous extensions which will suggest themselves to the operator. A person with imagination and patience could produce some really worth-while results even with the simplest of equipment.

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February, 1964

NEON RELAXATION OSCILLATORS

A PRACTICAL UNIT COVER-

ING AN AUDIO RANGE OF 500-2000 c/s BY M. J. BUNCE

O NE of the simplest types of oscillator available is the neon relaxation oscillator. Operation of this circuit depends upon the charging of a capacitor via a resistor and its subsequent discharge via a neon tube which is caused to "strike" when the voltage across the capacitor reaches a certain value.

The Simplest Circuit

In Fig. 1 we have a neon which will fire at 200V. Across it is a capacitor Cx. The neon and capacitor are connected to 200V d.c. through resistor Rx. On switching the apparatus on, Cx is slowly charged through Rx until the p.d. across the capacitor reaches 200V, whereupon the neon will fire and discharge Cx. Immediately afterwards the capacitor charges up again and the process is repeated.

Component Values

The frequency of the pulses is entirely dependent upon the component values used in the circuit. If, for example, Rx is increased, the charging time of the capacitor would be delayed somewhat, and the frequency would be lower. By using a variable resistor, the frequency may be varied continuously. A word of warning may not be out of place here. If Rx is reduced to a minimum of $5k\Omega$, the neon may arc across and be damaged. It is usual, therefore, when using a variable resistor as Rx, to include a fixed resistor of not less than $5k\Omega$ in series with the variable component.

Type of Waveform

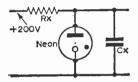
The waveform produced can be seen from Fig. 2. The sloping part of the waveform represents the capacitor charging and the vertical stroke is where the neon fires. For obvious reasons this is called a sawtooth wave. The ideal shape is indicated in Fig. 2(a), but as a capacitor charges exponentially the slope has a distinct curve in it. This can be seen if the oscillator is used in conjunction with an oscilloscope.

Power Requirements

The consumption of such an oscillator is small indeed. 200-250V d.c. at 15-30mA is ample for such a device. Smoothing is a relatively simple matter (Fig. 3). Two 2μ F electrolytic capacitors are all that is required, in conjunction with a resistor of 5-6k Ω or possibly two 4μ F electrolytics with a 4-7k Ω resistor. A full-wave rectification system is not essential and if an isolating transformer is used

Fig. I (right): The simplest circuit for the oscillator.

Fig. 2 (below): The ideal and actual waveforms produced.







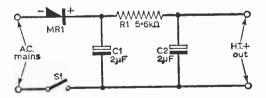
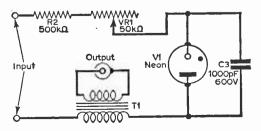


Fig. 3 (above): The h.t. supply circuit.





PRACTICAL WIRELESS

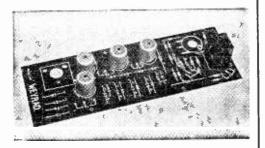


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February, 1964

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9	6	Ł

	COMPONENTS LIST
RI	5·6k Ω 3W
R2	5k Ω 3W
VRI	50k Ω wire-wound potentiometer
CI	2μ F electrolytic 250V
C2	2μ F electrolytic 250V
C3	1000pF ceramic 600V
TI	Interstage transformer 1 : 1
51	Toggle switch s.p.s.t.
MRI	Rectifier 250V 50mA
VI	Neon tube 200V

in series with the negative lead as shown in Fig. 4, no mains transformer is necessary.

Uses of Neon Oscillators

Neon oscillators may he found in old television sets, operating the timebases. Under these circumstances the lower portion of the waveform only is used to avoid distortion due to its exponential nature. In recent models gas-filled or "thyratron" triodes have been used instead. They are ideal as

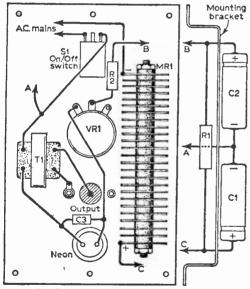


Fig. 5: Constructional details of the unit.

general purpose oscillators for testing radio receivers, amplifiers etc. They are of particular interest to readers possessing oscilloscopes.

A Practical Design

A practical general purpose oscillator which was built for less than £1. using surplus components and spares from the "junk box" will now be described. This oscillator was designed to operate at audio frequency in the range 500-2,000c/s.

The whole unit was made on a panel of 18s.w.g aluminium measuring 6in. x 4in. In the centre of

the panel a hole is drilled for a variable resistor $(50k\Omega)$. Above this a s.p.s.t. toggle switch is mounted, and below the 50k Ω variable, a coaxial socket (used for TV aerial sockets), is mounted. Below the coaxial socket, the neon is placed. This serves also as an indicator as to whether or not the unit is operating. The toggle switch (S1)controls the mains input and the 50k Ω variable (VR1) is a frequency control



Fig. 6: The front panel layout of the unit.

The coaxial socket is for the output and the wiring is shown in Fig. 5. The underside view of front panel and mounting brackets are shown in Fig. 5. To avoid "live" output sockets an interstage transformer with a ratio of 1:1 was used as shown.

The output can be checked by connecting a loudspeaker with output transformer across the coaxial output socket. When using the oscillator into a high impedance input (i.e. mike socket on a tape recorder) always use screened coaxial cable to avoid hum pick-up. It is advisable to include a 60mA fuse in the negative lead in case the neon or the capacitor C1 should break down. Note that C3 must be a 600V working component to avoid leakage losses.

Practical Circuits for Electric Guitars --continued from page 942

control VR3 must therefore be adjusted with discretion if an existing guitar amplifier is being used.

A Guitar Amplifier

Since all the tone controlling can be best effected at the guitar pick-ups, further tone controls are superfluous.

A combination of the control circuits given in this article, the tremolo/preamplifier of Fig. 4 and the power amplifier of Fig. 5, will provide a complete electric guitar amplification system.

The power amplifier employs a Brimar 6BR8 triode-pentode which functions as a first amplifier and phase splitter. The output stage uses two EL84's in ultra-linear push-pull, providing a maximum undistorted output of 10-12W. For guitar work this output can be taken up to peaks of 15W or so without appreciable distortion. The amplifier has negative feedback between the output and the cathode of VIA and it is most important that this is included and, of course, in the correct phase.

The output transformer in the original design was a Radiospares EL84 type which is supplied with wiring instructions for correct phasing of the negative feedback.



ELECTRONICS EXPERIMENTS AND PROJECTS By Len Buckwalter; 128 pages, 52 ins × 82 ins. Price 25s. ELECTRONICS FOR THE BEGINNER By J. A. Stanley; 190 pages, 52 ins × 83 ins, Price 25s. Both published by W. Foulshaw & Co. Ltd.

HESE two interesting American books have now been published in the U.K. and each contains an introductory chapter specially written for the English reader. This is a very sensible idea, since a novice is likely to be mislead or confused by certain Americanisms, while it is also most important to draw attention to the difference in the legal position with regard to the use of transmitting apparatus in this country as opposed to the U.S.A. Thus the English reader is advised not to build the oscillator and simple transmitter described in these books, but to treat these particular articles purely as a theoretical study. However such qualifications hardly diminish the value of these books to beginners on this side of the Atlantic. Both authors have adopted a friendly conversational style, and this helps to create the right atmosphere between teacher and pupil.

With the absolute beginner in mind, it is very difficult to decide which volume should take precedence, for each provides in its own particular way a valuable initiation into the field of Electronics.

Whereas Electronic Experiments and Projects sets out to give an understanding of the elementary principles by means of simple experiments that can be performed on the table at home, Electronics for the Beginner deals with the building of equipment—not so much for finding out how things work, but rather more for the enjoyment the completed equipment will provide. Actually, to be more correct, this latter book should be entibled "Radio and Audio for the Beginner" because the equipment described is limited to radio receivers and audio amplifiers.

Electronic Experiments and Projects conducts the reader through a series of experiments, most being performed using a piece of perforated hardboard as a "breadboard". Only a small number of commonly available parts are needed and as all electrical connections are made by clips the only tool required is a small screwdriver.

The earlier experiments involve the use of simple home-made circuit elements of R, C and L. Simple tests with a crystal diode and a transistor demonstrate the action of these semiconductor devices. Then follow a variety of experiments (or perhaps the term "projects" is here more applicable) which put into operation the basic ideas. These devices range from a simple telephone and a radio receiver to electronic devices for detecting such quantities as light, moisture and heat. The book computer for multiplication and division.

The arrangement of each article follows a standard pattern with sub sections entitled Preparation.

-

Setup, Operation, Conclusion and Parts List. Each experiment is illustrated with a photograph of the complete breadboard set-up, a layout diagram and a circuit diagram.

The essentially practical character of **Electronics** for the Beginner is indicated by the first Chapter; this is devoted to tools and soldering. The second Chapter "Building a Trap for Radio waves" is not as one might suppose concerned with a high Q rejector circuit but deals with the constructon of an aerial system. Next, a simple crystal receiver is fully described so that the reader is very soon equipped for "listening in".

But having wetted his appetite, the beginner is not allowed to proceed too far on the constructional side before being given some essential basic information regarding components and symbols and the art of circuit reading. Then he is better equipped to continue the exploration of the remainder of the book, and as his mood and fancy takes him, may direct his attention to the realms of world-wide radio or to hi-fi and stereo. The instructions for building the various equipments are clearly written, well illustrated and are wellnigh foolproof. For example, the wiring-up is in every case detailed wire by wire.—D.D.R.

TRANSISTOR INVERTERS AND CONVERTERS By Thomas Roddam; published by lliffe Books Ltd. 240 pages, 201 diagrams. Price 42s.

D OUBTS that have existed in this reviewer's mind concerning the desirability or logic of giving a fine distinction to the terms "inverter" and "converter" have not been entirely dispelled by Mr. Roddam in his excellent work dealing with transistor circuits for a.c. to d.c. or d.c. to a.c. conversion.

Why not simply use the term "converter" and qualify it by the adjectival use of "a.c. to d.c." or "d.c. to a.c." as the case may be?

This is not, of course, a criticism that one can level at the author personally, since he is using words already generally established in electronic engineering, but I feel this opportunity of drawing attention to another unfortunate choice of terms must not be neglected.

The opening chapter of **Transistor Inverters** and **Converters** surveys all the present sources of electrical power and suggests that the omnipresence of a.c. is perhaps only transient, since in the future the distribution of power may be performed more effectively by d.c. mains circuits. This prospect, in addition to the existing quite considerable requirements for operating various types of apparatus from low-voltage d.c. supplies. gives a further emphasis to the relevance of this book. Having assured us of the indispensability of these devices the author commences his detailed discussion.

-continued on page 966





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PRACTICAL WIRELESS

Tape Deck

NEW tape deck made by Lorlin Electronic Co. Ltd., has recently become available in two or four track models. The deck employs three motors and can be operated at three different speeds. It can accommodate spools up to 7in. in diameter and when running a tape-controlled brake tensions the tape evenly from beginning to end of the reel.

Two models of the tape deck (type SB.26) are available, costing 31 and 39 guineas. The manufacturers are Lorlin Electronic Co. Ltd., 23 Wardour Street, London, W.1.

A.M./F.M. Radiogram

RAIRD Television Limited have recently introduced a new radiogram, the model 286. The receiver on this model tunes over the whole of the medium waveband and to the Light Programme on

long waves. F.M. transmissions are received from 88 to 100Mc/s.

The gram unit incorporates a fourspeed autochange record deck which provides good quality reproduction through the 8in. round loudspeaker, which is housed in a sound chamber at the righthand side of the cabinet.

The price of the model 286 is 57 guineas and the makers are Baird Television Limited, Seymour Mews House, Wigmore Street, London, W.1.

The Baird Model 286 a.m./f.m. radiogram

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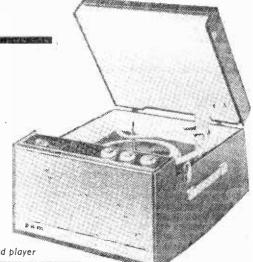
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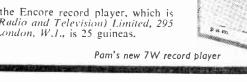
Seven Watt Record Player

THE new Encore record player from Pam has been designed to give better-than-normal reproduction from a portable record reproducer. Its features include a new Monarch BSR-UA.15 four speed autochanger (taking all sizes of records) and a crystal pick-up,

The circuit of the Encore (Model 5206) delivers an output of 7W through a $6\frac{1}{2}$ in. diameter speaker. Three controls atop the attractive cabinet give separate bass, treble and volume control of the output.

The price of the Encore record player, which is made by *Pam (Radio and Television) Limited, 295 Regent Street, London, W.1.*, is 25 guineas.



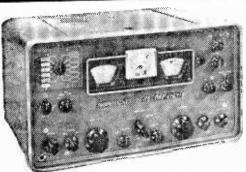


Professional Tape Recorder

THE Nagra IIINP is a Swiss-made portable tape recorder of professional standards and capable of studio quality performance.

The transistorised circuit operates from self-contained batteries or from a mains unit. The tape deck provides for a choice of three speeds, 34in.p.s., 7½in.p.s. and 15in.p.s., and at the highest tape speed the frequency response is 30c/s to 18kc/s.

The Nagra HINP tape recorder is manufactured by Kudelski of Switzerland and the U.K. agents are Livingston Laboratories Limited, 31 Camden Road, London, N.W.1. Its price?—£340.



The latest communications receiver from Hammarlund

BOOKS REVIEWED

-continued from page 962

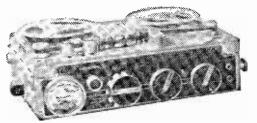
First, the two principal circuit elements, the transistor and the transformer, are in turn closely examined and their characteristics analysed; they are then brought together in subsequent chapters where various forms of single-ended, push-pull, bridge, sine-wave and driven inverter (or converter) cricuits all receive thorough attention.

Without doubt a valuable reference source for design engineers, this book will also be of great interest to many others who seek more than a mere surface knowledge of the subject.—F.E.B.

AUDIO AND ACOUSTICS

By G. A. Briggs, with James Moir; published by Wharfedale Wireless Works Limited, Idle, Bradford, Yorkshire. 168 pages, 8½ in. x 5½ in. Price 10s. 6d. (11s. 6d. post free).

MANY readers have seen, or have on their bookshelves, a book called Sound Reproduction. This, published originally in 1949, was an enlarged version of a booklet Loudspeakers, but covering a larger field. It was, in fact, the forerunner of the now well known series of audio books by G. A. Briggs. The author's unconventional style and his method of presenting facts and data in a most readable form caught the imagination of audiophiles and Sound Reproduction eventually went into three editions.



This is the Nagra IIINP portable tape recorder

General Coverage Receiver

THE latest general coverage receiver to come from the Hammarlund Manufacturing Company, is the type HQ-180AX, an improved version of the HQ-180A. This receiver features 11 fixed frequency crystals in addition to the v.f.o., six of which are plugged in on the face of the instrument, the remainder being reached through a hinged compartment in the cabinet. An unusual feature of the HQ-180AX is the facility for compensating for minor frequency variations of the crystals by means of a ± 3 kc/s vernier tuner control.

Complete technical data of this new communications receiver may be obtained from the U.K. agents for Hammarlund equipment, K. W. Electronics Limited, Vanguard Works, 1 Heath Street, Dartford, Kent.

In 1962, when Sound Reproduction ran out of print, it was decided not to reprint again, or to bring out a revised edition, but (in the words of the author) "to divide and conquer and have two or three modest volumes instead of one huge tome running to several hundred pages."

Audio and Acoustics is the first in this programme of revision and, as the name suggests, concentrates mainly on the problems of acoustics. Although some of the material is taken from Sound Reproduction much of it is completely new and those who found the original book of value will certainly not be wasting their money in purchasing this new publication.

A very informative historical section deals with audio and acoustical developments, ranging from Edison's phonograph of 1877 to modern demonstration rooms and transistorised videotape recorders. This leads into chapters on the Ear. Resonance, Echo and Reverberation and Room Acoustics, all of which provide hard facts and food for thought. Other sections cover Free-field Sound Rooms, Transient Response, Stereo, Concert Halls and Studios and Live/Recorded Tests.

As the author points out, there is a growing interest in the acoustic aspect of sound, and in any audio set-up the real final link in an audio chain is **not** the loudspeaker system but the acoustics of the listening room. Therefore, this aspect requires more attention than that to which it is generally given.—W.N.S.



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122/19A	Dual	30-15000	15 -	32 or 75	20	12,000	160,000	Aluminium	121n.	11in.	6lbs.	£7.19.6
122/14	Single	25-5000	15	82 or 75	22	14,000	186,000	Copper	12in.	llin.	71bs,	9 gns.
122/14A	Dual	80-15000	18	32 or 75	22	14,000	186,000	Aluminium	12in.		71bs.	10 gns.
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152/14	Single	25-3500	15	30 or 75	22	14,000	186,000	Copper	15in.	13#in.	91bs.	14 gns.
152/14A	Dual	30-15000	15	30 or 75	22	14,000	186,000	Aluminium	15in.	13#in.	9lbs.	15 gns.
152/17	Single	25-4000	1.5	30 or 75	25	17,000	226,000	Copper	15in.	131in.	12Hbs.	16 gns.
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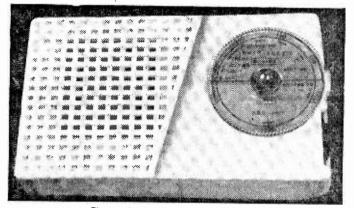
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Long Waves for the M.W.



The receiver as it appeared originally.

THE receiver described in the September, 1962, issue of *Practical Wireless* tunes medium waves only. However, it can quite easily be modified to include long waves if this is required. Two methods will be found satisfactory and either may be adopted.

The simplest arrangement is to add sufficient capacity to give preset tuning of the Light Programme on 1.500m, the original medium wave

ferrite rod winding being used on both bands. Reception on the long wave band is then confined to 1.500m only. The second method is to provide a long wave loading coil and coverage is then about 1,100m to 1.750m, allowing reception of other stations in this band. In both cases the oscillator coil remains unchanged, the necessary extra capacity being switched in.

Preset Tuning

The circuit for this arrangement is shown in Fig. 1. When the switch is in the medium wave position mediam wave reception is obtained as before. With the switch in the long wave position

TC3 and C16 are in parallel with the medium wave aerial winding and the 180pF capacitor is across the oscillator coil. The usual tuning control acts as a fine tuning or manual trimmer.

The receiver is sufficiently sensitive for this arrangement to give adequate volume in very many localities. The set is, of course, intended for reception of the Light Programme only on this band as mentioned.

C16 and TC3 need to total about 1,750pF and



By J. G. Thompson

MODIFYING THIS P.W. TRANSISTOR DESIGN FOR L.W. RECEPTION

this can conveniently be obtained with a 1,600pF fixed disc capacitor and a 300pF or 500pF trimmer. VC1 provides 208pF and this allows further adjustment, since it is not very important where the Light Programme is found on the dial. It should, however, be possible to obtain 1,500m with the gang capacitor roughly half closed, this depending on the exact capacity of the 180pF oscillator capacitor and the coil core. On the long wave

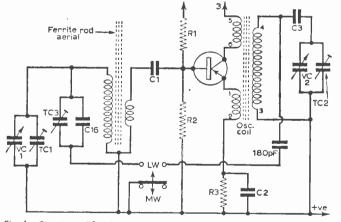
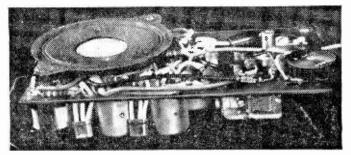


Fig. 1: Circuit modifications to receive the Light Programme on long waves.

band the position of the oscillator coil core has a great effect on frequency. If necessary slight readjustment may be made, followed by realignment on the mediam wave band.

It is feasible to obtain 1,500m at a marked point on the dial by adjusting TC3 and C16 and by including a further trimmer in parallel with the 180pF capacitor. But tuning will still be restricted to the Light Programme only.

If a few small fixed capacitors are to hand values



The chassis of the prototype receiver.

may be selected to bring 1,500m within the swing of the gang capacitor. Capacitors can be tried experimentally by wiring them across VC1 and from pin 4 of the oscillator coil to the positive line.

Long Wave Tuning

This method gives normal tuning and allows reception of one or two other stations in addition to the Light Programme on 1,500m. The circuit is shown in Fig. 2.

The long wave loading coil, with TC3 in parallel, is in series with the existing medium wave coil. The base coupling winding is returned to a tapping on the long wave coil. The long wave coil is shorted out when the switch is in the medium wave position. With the switch in the long wave position the loading coil is in circuit and the 180pF capacitor and TC4 are in parallel with the oscillator coil.

It is important that the tapping is near the "earth" end of the long wave coil and that both medium wave and long wave coil turns are in the same direction when they are in series. The long wave section is slid on the free end of the ferrite rod.

Frequency coverage may be modified by adjusting TC4. TC3 is adjusted for best volume around

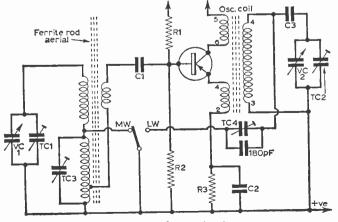


Fig. 2: The circuit for complete l.w. coverage.

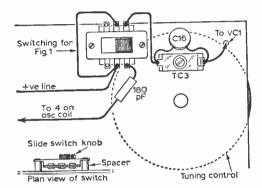
February, 1964

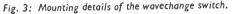
1,200m. The receiver is then tuned to about 1,650m and the long wave winding is moved along the rod for best results.

Switch Mounting

A miniature slide switch can be positioned in the free space left near the oscillator coil, taking care that it clears the tuning control, as in Fig. 3.

The circuit in Fig. 1 requires two poles closed for long wave reception. A two-pole, two-way





switch, as actually shown in Fig. 3, will thus be needed. The outer tags will have to be bent over to clear the case.

For the circuit in Fig. 2 a single pole two-way switch is sufficient. The switch shown in Fig. 3 may, of course, be used, but a single pole two-way switch will require less space as one set of contacts will be omitted. The centre tag goes to the positive or "earth" line, exactly as in Fig. 3. One

outer tag is wired to the junction of medium wave and long wave aerial coils. The remaining outer tag is connected to TC4 and the 180pF capacitor, which are returned to pin 4 of the oscillator coil.

The switch is held by 8B.A. or smaller bolts with countersunk heads, spacers (or extra nuts) being used so that it is just clear of the paxolin panel. Carefully measure the switch position, drill a small pilot hole through the case and enlarge this with a small file to match the switch slot.

After either of the modifications shown, slight retrimming and realignment will be necessary on the medium wave band because of the stray capacity of switch wiring, etc.

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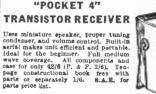
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Mains Voltage Adjuster

HIS simple piece of equipment makes it possible by a turn of a switch to vary the mains supply voltage by up to about 50V above or below normal. It will be especially useful to those who have to service receivers in areas where the supply voltage is not uniform and can also be used to compensate for lost volts during peak load periods.

This device consists essentially of an auto transformer arranged so that both the input and output tappings can be varied at will as shown in Fig. 1 and a meter to indicate the output voltage.

Choice of Transformer

It will be seen at once that although the transformer is an indispensable part of the device, it does very little work, so that quite a large output is obtainable from a component of modest size.

An ordinary mains transformer as used in radio receivers is quite suitable and it does not matter if one or more of the secondaries is defective, so long as there are no shorted turns. The transformer must have a tapped primary and needs, of course, to be chosen with some regard to the out-put required. The following figures refer to the transformer used in the prototype and show how the maximum output current may be calculated.

Secondary ratings:

350-0-350V	120mA	(700	х	0.12)	=84	volt-amps
6.3V 2A						volt-amps
6·3V 4A					=24	volt-amps

Total 120

Assuming a transformer efficiency of 80 per cent, this total may be increased to 150 when referred to the primary and it is deduced that the primary will be capable of 150 volt-amperes at the lowest input tapping of 200V; and that the maximum current which can safely be permitted to 150

flow through it is -=0.75A. 200

This figure however, relates to service in a radio receiver, where the poor form factor of the h.t. secondary current, caused by the presence of the rectifier and reservoir capacitor. contributes appreciably to the heating effect.

A further consideration is that the currents in the two sections of an auto-transformer winding are in exactly opposite phase, so that the current in the section which is common to both input and output circuits is limited to the difference between the input and output currents. Thus the full output current will flow only in that small portion of the

winding which is used to step the voltage up (or down) and its heating effect will be correspondingly small.

BY V. E. HOLLEY

The result of all this is that the figure arrived at by calculation may be increased by about a third, and in fact, the transformer in the prototype unit becomes only faintly warm when a current of 1A is drawn continuously.

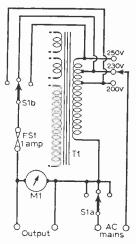


Fig. I: The circuit of the unit

Other Components

The 2-pole, 4-way rotary switch, S1. should be of the "make before break " variety. One pole (a) is used as a mains on/off switch in the input circuit and the other (b) to select the required out-put tappings.

An a.c. voltmeter, reading to 300V, is needed to indicate the output voltage. High accuracy is not necessary and a cheap moving iron meter will be quite satisfactory.

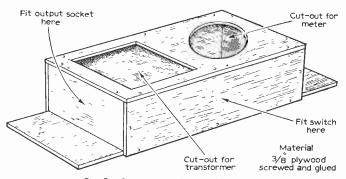


Fig. 2: Construction details of the case.

The cartridge fuse, FS1, in the output circuit should be of the anti-surge type, and its value should be chosen according to the maximum permissible output current.

Construction

The form of construction is unimportant. The prototype was built in a kin, plywood box 9in, x $4\frac{1}{2}$ in. x $2\frac{1}{2}$ in. the bottom being extended at each -continued on page 974

Testing Dry Batteries

By G. A. W. Partridge

D RY cells are used extensively as a portable power supply for valve and transistor radios. The cells which give approximately 1-5V each are made into batteries in order to produce the necessary electrical power.

After a certain length of time the cells cease to produce electricity and therefore have to be discarded and fresh batteries installed.

The usual idea, when a dry battery is under suspicion, is to simply test it with a voltmeter (Fig. 1). This is, however, not always satisfactory.

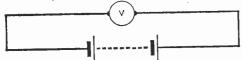


Fig. 1: The straightforward test for dry batteries.

For example, a radio battery was tested in this manner and gave a reading of 9V which was correct, but the radio barely functioned. The answer was that the battery had sufficient power to pass the tiny current necessary to operate the voltmeter but when it was called upon to pass about 25mA for the radio it could not do it.

In other words the e.m.f. (electromotive force) of the battery was still 9V but its p.d. (potential difference) was much less. The answer therefore, is to measure the p.d. and also the e.m.f.

What is the difference?

The e.m.f. can be taken as the battery's opencircuit voltage, and the p.d. is the voltage across the battery when a normal current is being drawn from it. The p.d. varies with this current so the battery should be tested while operating at normal load conditions. The p.d. and e.m.f. readings will

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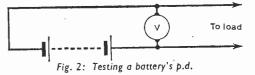
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end so that the assembly could be fastened to the workshop wall. Details are given in Fig 2.

Measurements will, of course, depend on the size of the transformer and meter. Connection to the mains should be by 3-core cable so that the exposed metal of the transformer can be earthed.

Operation

The prototype is operated from a supply which is nominally 240V but is frequently less. The mains voltage adjustment on the transformer is therefore usually set at 230V and voltages of 200, 220 and 240 are then available by operation of the switch.



therefore show up the condition of the battery (Fig. 2).

Another point that is overlooked is that a battery has an internal resistance. Actually the difference between e.m.f. and p.d. is the voltage necessary to overcome this resistance which can be calculated from:

 $r = \frac{E - V}{I}$

r=internal resistance.

E = e.m.f. (open circuit) in volts.

V = p.d. (closed circuit) in volts.

1=current in amperes.

Here is an example taken from an actual test. A torch cell was found to have an e.m.f. of 14V. It was connected through a milliammeter to a small resistance and the current drawn was 240mA. The p.d. was found to be 1.1V. The internal resistance is:

$$r = \frac{E - V}{I} = \frac{1 \cdot 4 - 1 \cdot 1}{240/1000} = \frac{1 \cdot 4 - 1 \cdot 1}{0 \cdot 24} = 1 \cdot 3\Omega.$$

This cell is starting to deteriorate. The e.m.f. is low and the internal resistance rather high. A test on a good cell indicated an e.m.f. of 1.5 and an internal resistance of 0.37Ω .

A battery of cells will have a higher internal resistance if they are connected in series. For example a 6V dry battery will have four 1.5V cells connected in series. If each cell has an internal resistance of 0.4\Omega then the total resistance will be $0.4 \times 4 = 1.6\Omega$.

Large capacity batteries for low voltages and higher currents have their cells connected in parallel. The total internal resistance will then be: 1 1

= \times The number of cells.

R r A battery of ten cells, each with a resistance of 0.4Ω will give a battery internal resistance of:

 $\frac{1}{R} = \frac{1}{0.4} \times 10 = 0.04\Omega.$

In addition to providing supplies to receivers and amplifiers of varying voltage requirement, the unit is extremely useful for supplying a soldering iron. A high voltage can be used for quick heating, after which it can be reduced to normal or, if the iron is not to be used for some time, to sub-normal to keep it "simmering" ready to be brought quickly to working temperature when required.

An indicator lamp, supplied from one of the 6V transformer windings could be fitted, if desired, but is not essential as the voltmeter serves the same purpose.

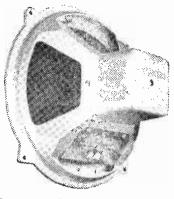
ONE WORD OF WARNING: The unit should not be left unattended for long periods when it is being used to compensate for a reduced supply voltage. because if the supply should return to normal, damage might be done to equipment connected to it.



H.F. 1016 'MAJOR' MODEL

This unit makes use of the high flux density available in the magnet system of the previous H.F.1016 unit. A curved diaphragm is used with a rigid centre section coupled to the voice coil. The rigid coupling and the design of the cone termination give a balanced response over the whole audio range. The unit is specially suitable for use in the smaller type of enclosure having a volume of approximately 13 cubic feet.

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Specification:

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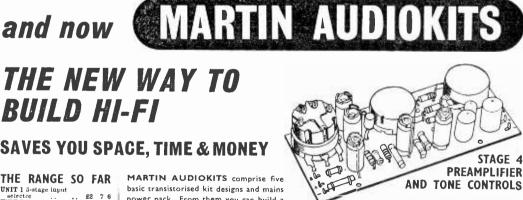
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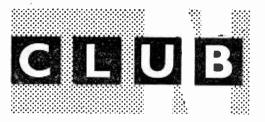
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Hon. Sec.: M.A. Woof, G3SGO/T, "Copperkins", Copperkins Lane, Amersham, Buckinghamshire.

Prospective members are invited to attend any Club meeting, especially those interested in joining the R.A.E. course which is being run at the moment. It should be noted, however, that the club-night has been changed recently to Fridays.

DERBY AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: F. C. Ward, G2CVV, 5 Uplands Avenue, Littleover, Derby.

At the meeting for December 11th, members reviewed the events of 1963 as they appeared in members photographs taken through-out the year. Later in the month on the 15th, members competed for the GYY Trophy and on the 18th the Annual Christmas Party provided an enjoyable evening for all who attended.

The first day of the New Year was marked by a surplus sale.

LICHFIELD AMATEUR RADIO SOCIETY Hon. Sec.: V. Hickman, 143 Main Street, Stonnall, Walsall, Staffordshire.

A full programme of lectures and social activities is helping to increase the membership of this Society. All meetings are held at the Swan Hotel in Lichfield on the first Monday and third Tuesday of each month.

MITCHAM AND DISTRICT RADIO SOCIETY

Hon. Sec.: A. L. Thurley, 50 Bruce Road, Mitcham, Surrey. The meeting for December 6th was devoted to a film show arranged by G3LCH, the Society's Chairman.

The main event of the meeting on December 20th, was a constructional contest.

NORTHERN HEIGHTS AMATEUR RADIO SOCIETY Hon. Sec.: A. Robinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.

The Society's third Annual Dinner was held on December 11th and this proved to be a most enjoyable event. This was followed

a week later by a ragchew meeting. The first meeting of the New Year was held on January 1st, when Mr. H. Makin gave a lecture entitled "The Building of a 10-80 Transmitter."

READING AMATEUR RADIO CLUB Hon. Sec.: R. G. Nash, G3EJA, "Peacehaven", 9 Holybrook Road, Reading, Berkshire.

A session of questions and answers was the main event at the December meeting of this Club, when members met at the Palmer Hall in Reading on the 28th. However the competition for a Club badge design, was judged on the same evening.

SCARBOROUGH AMATEUR RADIO SOCIETY Hon. Sec.: P. B. Briscombe, G8KU, "Roseacre", Irton, Scarborough, Yorkshire. The meeting for December 12th was devoted to a review of the

past year, in photographic slides, and on December 19th members, their families and friends, had an enjoyable time at the Society's Christmas party.

SPEN VALLEY AMATEUR RADIO SOCIETY Hon. Sec.: N. Pride, 100 Raikes Lane, Birstall, Nr. Leeds. Because of the Season's festivities only one meeting was held during December. This was on the 12th and was a film show.

STOURBRIDGE AND DISTRICT AMATEUR RADIO SOCIETY

Hon. Sec.: R. A G. MacIntosh, 50 Field Lane, Oldswinford, Stourbridge, Worcestershire.

On December 20th, members gathered in the Bell Hotel in Stourbridge for the usual Christmas informal get-together.

UXBRIDGE RADIO SOCIETY Hon. Sec.: A. Duell, "Treetops", Bakers Wood, Denham, Buckinghamshire.

ctivities currently under progress in this Society include an R.A.E. class (in preparation for the May examinations) and also a series of lectures on oscilloscopes and communications.



WEST KENT AMATEUR RADIO SOCIETY

R. Trevitt, 28 Dales Avenue, Tunbridge Wells, Kent. On December 13th a group of members went out on a pre-arranged visit, and later in the month on the 20th, the Society's Christmas party was held.

WIRRAL AMATEUR RADIO SOCIETY

Hon, Sec. A. Seed, G3FOO, 31 Withert Avenue, Bebbington, Wirral, Cheshire.

On December 18th, members attended a lecture given by Mr. Roberts, (G3EFX), his subject being valves.

On January 1st the Society held a symposium under the title of "Why Amateur Radio Appeals to me.

TEST GEAR TECHNIQUES

An error in Fig. 9 of this article (page 429 of the September issue) has been pointed out by several readers. The cathode of V1 should have inserted a 300 Ω resistor, and the grid 3 load, shown as 300 Ω . should in fact be $500k\Omega$.

THREE-WATT AMPLIFIER

Two errors appeared in this article which was published in the November issue. In the circuit diagram and components list V2 is given as an EL86. This should be an EL84 as mentioned in the text. Also in the components list, the mains transformer is shown to have a rating of 8mA instead of the correct 80mA.

HELP FOR HOME BUYERS

When you are buying or selling property it is vitally important to know where you stand as far as the law is concerned. Ignorance or carelessness might cost you hundreds of pounds. There's sure to be a big welcome, then, for the new FREE ADVICE LEGAL SERVICE just announced by Newnes Property Advertiser and Holiday Guide. Every week, from now on, this paper will carry questions and answers on such topics as mortgages, insurance, surveying and general legal points. In addition any reader may have his own particular questions answered by a panel of experts simply by filling in a Query Coupon on the Legal Advice Page. Newnes Property Advertiser and Holiday Guide. which contains details of thousands of houses, flats, shops, business and holiday addresses, is on sale every Thursday, price 4d.



DEFINITELY THE LAST WORDS ON "LICENCES"

SIR.—I offer the following in reply to all those who seek "novice licences":

Enough, let's hear no more these weary tales.

These jealous cries of Tired Tims and mental snails. Let their authors, miserable souls. Use up their leisure playing bowls.

e ap then teleare pulying the

A curse on all these armchair critics Seeking complimentary tickets.

Away ye parasites and infant bawlers, Spawn of Weirdies, Lids and Creepy Crawlers.

MAGNETIC PICKUP

SIR.—I do not wish to criticize unduly, but I do think that the pre-amplifier described by Mr. Banthorpe in his very interesting article on a "Magnetic Pickup" in the July 1963 issue, is worthy of attention. The circuit as shown on page 274 will not work unless the transistors are chosen for their current gains (β).

Consider: the base current of Tr1 is $4\cdot 2/330$ mA assuming a Vbe of 0.3V. This equals 0.013mA. In order that this stage should conduct properly and not "bottom", the voltage drop across the collector load ($22k\Omega$) should not be more than 3.5V approximately.

This means that the β of Tr1 should be less than 3.5

- =12-2. If the β is greater than 14, Tr1 0.013×22

will "bottom". From the Mullard data, the average β of an OC71 is 40. Admittedly, at the low values of collector current used that β will be lower than this figure, but it cannot be guaranteed that it will be less than 12.

It can likewise be shown that if the current gain of Tr3 is greater than 9.5 this stage will be permanently "bottomed" which will make it insensitive to all but the positive peak signals—a very effective clipping device. Unfortunately, if the first stage is "bottomed" this will only be sensitive to negative peaks, so as a whole the circuit is rather insensitive.

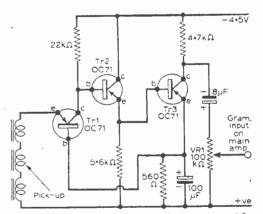
I enclose a somewhat better circuit. This has the advantage that the circuit is d.e. stabilised by negative feedback and is thus unlikely to "run

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERTES OVER THE TELE-PHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iii of the cover.

The Editor does not necessarily agree with the opinions expressed by his correspondents

away". It is also tolerant of β in all stages. It should be noted that the method of biasing a transistor with a single resistor in the base lead, makes the circuit extremely critical since the value of the resistor depends upon β which is a variable parameter. The only advantage is a reduction in the number of components required. However, a method of overall d.c. feedback as shown, can have this advantage with none of the disadvantages of instability.—D. G. WHITEHEAD (Marple, Cheshire).

[The author of this article has read and agreed with Mr. Whitehead's observations and has suggested they should be published for the benefit of any readers who have built or are contemplating building the pre-amplifier.—ED.]



The revised circuit of the Magnetic Pickup pre-amplifier.

IN DEFENCE OF THE HAM

SIR.—After reading the letter from Mr. H. A. L. Wagner (December issue) in his self-appointed role of "picador of the air". like any tortured animal in the ring, I have been goaded into making this reply.

Practically everyone knows, of course, that the average licensed radio amateur, far from being a ham (a detestable misnomer, this) is more likely to be a professional of very high standing, and indeed the electronics and associated industries would look very sick without him.

Reading between the lines of Mr. Wagner's letter, it appears to me to be a strong case of "sour grapes", and your correspondent displays a great

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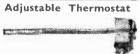


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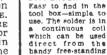
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deal of ignorance. He unmercifully criticizes the licensed amateur and yet praises the pirate operator to the full. The obvious reason why pirates "cut the cackle to a minimum" is the perpetual fear of being traced by the authorities because they are breaking the law.

Mr. Wagner states neither which system of emission nor which bands he operates, and he does not indicate the subject matters heard under discussion, but most of us are quite capable of exchanging technical data if the occasion arises. Conversely, by virtue of our licensing regulations, we are at liberty to discuss much more personal matters at any time-and we do! - REX TOBY (London, W.I.).

EVEREST PRAISE

SIR.-May I say a word of praise for the "Everest" tuner, which was described in the June and July 1962 issues of P.W.? As stated by the author, alignment needed plenty of patience, however once this has been mastered, it certainly does all that was claimed of it. and was well worth the cost of the crystal.-J. SMETHURST (Oldham, Lancashire).

A DIFFERENCE OF OPINION

SIR,-Mr. Hellyer in his article "Test Gear Techniques", published in the November issue of P.W., appears to be confused.

He says: "Mathematically, NdB=10log₁₀(P2/P1), where P1 is the input and P2 the output power."

This is perfectly correct. The bel is a ratio (logarithmic) of powers. This can be also written, $V1^2 \times R2$ of course, as: NdB=log₁₀ and, as the $R1 \times V2^{\circ}$

R1 = R2author states, if then: NdB = $10\log_{10}(V1^2/V2^2)$, or: NdB= $20\log_{10}(V1/V2)$.

This however, is not equivalent to: NdB= $10\log_{10} (V2/V1)$. . . (a) and therefore cannot be termed as a voltage ratio or as a voltage decibel, which (a) would represent. As $V^2/R=P$ however, therefore: $20\log_{10}(V1/V2)$ can be said to be again a ratio of powers. There is only one type of decibel -power. Anyone who speaks of the other types of decibels-voltage. resistance, current-either has no knowledge of what he is speaking, or is being deliberately misleading. - P. J. McGoldRick (London, S.E.9).

SIR-In reply to Mr. Goldrick's letter. This is an example of the academic versus practical controversy more often found in the pages of the "glossy" technical magazines. Mr McGoldrick is as right in his facts as he is rude in his conclusions.

While it is perfectly true that the bel is a logarithm to the base 10 of the ratio of two powers, it is also true that since the power ratio is also the square of the voltage or current ratio for a given load impedance, the power ratio in decibels can be stated as 20 times the logarithm to the base 10 of the voltage or current ratio V1/V2 or 11/12. When

using this convenient measuring tool, we do not always state that the expression dB is a power ratio: this is understood. Engineers who regularly employ the dB as a means of response curve, bandwidth and sensitivity checks are quite familiar with its use. They are concerned with comparative voltages, but are well aware that the use of the dB is a mere convenience, not an absolute measurement. They know quite well that $20\log_{10}(V1/V2)$ is a ratio of power, and do not speak of different *types* of decibel. In doing so, they are not intentionally misleading and could hardly do their work without knowledge of what they were saying.

A closer reading of page 646 of the November P.W. will show that this stricture was indeed put forward. Space prevented a fuller theoretical discussion in an article of this nature. It would have been quite proper to continue to the effect that voltage ratios are more correctly stated in *nepers*. But to bring in logarithms to the base "e" would have done nothing to improve the article, or clarify the subject. However, if a more technical (less misleading?) treatment is needed, the author will be happy to oblige.-H. W. HELLYER (Gilfach, Glamorganshire).

Sir-I would be grateful if any reader could sell or loan me . . .

... the May and June 1957 issues of P.W.

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No. 52--H. C. LOXLEY, 51 Guy Street, Warwick.
... the June 1957 issue of P.W.-D. W. FROST,
6 Queen's Road, Harpurhey, Manchester 9.
... the circuit and data of the a.m. test set, type
74.A.-G. H. PARK, 32 Stonefield Street, Moorside, Cleckheaton Vorkehire

heaton, Yorkshire.

details of the No. 19 set.—J. AULESBROOK, 61 South Road, Beeston, Nottinghamshire.

beeston, Nottinghamshire. ... the instruction book for a G.E.C. four-valve portable receiver, type BC.1255.—M. SELLARS, 9 Oaklea, Sherwood Road, Heath Grove, Buxton, Derbyshire. ... the January 1961 issue of P.W.—A. Crabb, "Jara", Central Avenue, Hullbridge, Essex. ... data for the No. 38 and No. 46 transmitter/ receivers.—23861901 Tpr. HARGRAVES, A. W., Q.M. Troop, 2nd Royal Tank Regiment, Lisemally Camp, Omagh, Co. Tyrone, N. Ireland.

...the September 1960, September and December 1961 issues of *Practical Television*.—R. F. DARBY, 5 The Firs, Bell Bar, Hatfield, Hertfordshire.

... the August, September and October 1961 issues of P.W.-P. A. BLAKEY, Cox Hill, Boxford, Colchester, Essex.

... the September 1956 issue of P.W.--M. A. FORRESTER, SB Bede Avenue, Sherburn Road Estate, Durham. ... details of the valve line-up and internal con-nections to the coil pack plugs of the receiver type M.C.R.I.--L. O. BEALING, Del Monica, 93 Alma Road, Bournemouth, Hampshire.

the September 1957 issue of P.W .- A. GUY,

27 The Drive, Lightcliffe, Halifax, Yorkshire. ...the issues of P.W. dealing with the conversion of the R1155 receiver.—J. REED, 14 Firth Road, Rondebosch,

Cape Town, South Africa. ...the circuit and wiring diagram of the supply unit Mk.III No. 2.—S. M. MARSHALL, 18 Anne Way, Barkingside, llford, Essox.

... the circuit and/or any other data for the R.107 Mk.1/I set. R. S. KING, 46 Maesteg Road, Cwmfelin, Maesteg, Glamorganshire.

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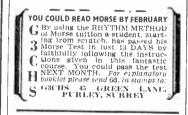
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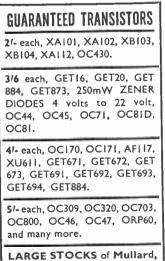
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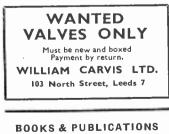
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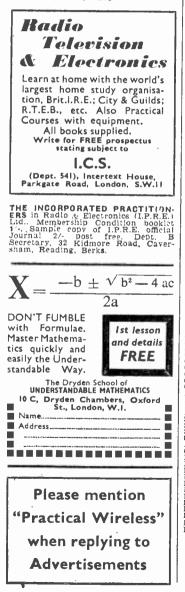
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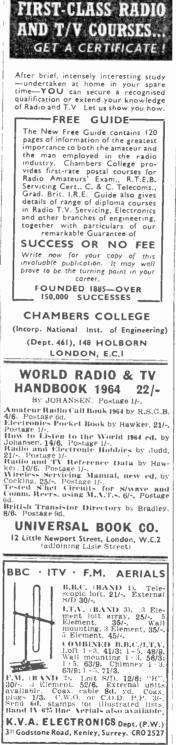
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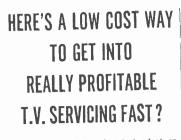
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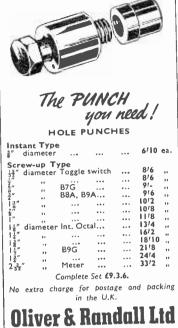
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Practical Wireless

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