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PRACTICAL WIRELESS

December, 1962

Specification:

—15 ohms.

Price: £10.0.0 (inc. tax)



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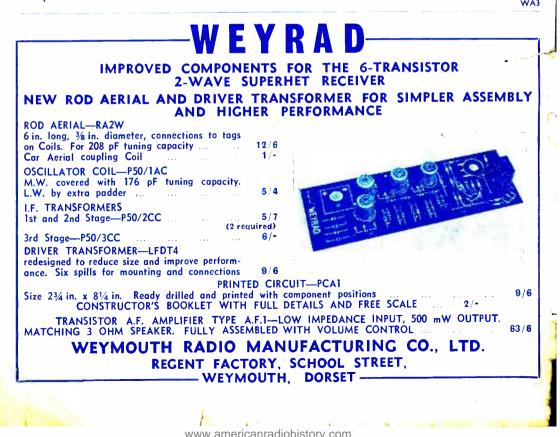
NEW MODEL H.F. 1016 'MAJOR'

This new unit makes use of the high flux density available in the magnet system of the previous H.F.1016 unit. A curved diaphragm is used with a rigid centre section coupled to the voice coil. The rigid coupling and the design of the cone termination give a balanced response over the whole audio range. The unit is specially suitable for use in the smaller type of enclosure having a volume of approximately 1½ cubic feet.

Туре	Flux Density	Price	Туре	Flux Density	Price
8" H.F.816*	16,000 gauss	£6.13.9	T.816	16,000 gauss	£6.6.9
8" H.F.812*	12,000 gauss	£4.1.3	T.I2 tweeter	16,000 gauss	£13.4.6
8" H.F.810	10,000 gauss	£3.0.6	T.10 tweeter	14,000 gauss	£4.8.3
6" H.F.610		£2.10.3 Steel £2.12.3diecast		9,000 gauss	£1.14.0

* Incorporates g universal impedance speech coil.

WHITELEY ELECTRICAL RADIO CO. LTD. MANSFIELD, NOTTS Telephone: MANSFIELD 1762-5 London Office: 109 Kingsway, London, W.C.2



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AC2/PEN ECC85 7/6 21/- ECC88 12/6 AC2/PEN ECC89 12/6 AC2/PEN ECC89 12/6 AC2/PEN ECC89 8/6 AC2/PEN ECC91 3/- DD 21/- ECF82 8/6 AC/TP 3/- ECF82 8/6 AC/TP 3/- ECF82 8/6 AC/TA ECH31 10/- AZ1 10/- ECH32 10/- AZ31 10/- ECH32 10/- AZ31 10/- ECH33 10/- CC131 15/- ECL80 8/6 CC33 15/- ECL80 10/6 CY1 15/- ECL80 10/6 CY1 15/- ECL81 10/6 CY1 15/- ECL81 10/6 CY2 EF40 15/- DCF90 DAF91 6/6 EF37 8/- DF92 7/2 EF40 <th>EY86 77. PCC85 976 EY91 37. PCC88 126 EZ35 67. PCC88 126 EZ41 77. PCF80 97. EZ40 77. PCF80 97. EZ40 77. PCF80 97. EZ80 676 PCF84 1276 EZ81 676 PCF86 1276 EZ81 676 PCF84 1276 EZ81 676 PCF86 1276 EC4 157. PCL85 1076 FC13 157. PEN45 1076 FW4/800 97. PEN440 776 GZ30 1076 PEN450 GZ33 1973 PEN450D HABC86107. PEN450D PEN450D</th> <th>TDD13C TD13C TF141 27/6 TF441 27/6 TF46F 12/6 U12 9/- U12 9/- U12 9/- U12 9/- U24 21/- U25 12/6 U26 10/- U31 9/- U35 17/6 U37 17/6 U37 17/6 U37 17/6 U43 8/6 U37 17/6 U43 10/- U52 4/- U78 4/6 U78 4/6 U191 15/6 U329 12/6 U301 22/6 U329 12/6 U404 10/- U8801 19/9 UA8C80 7/- U6841 8/- U86281 10/- U8628 10/- U8628 10/- U8628 10/- U8628 10/- U8628 10/- U8628 10/- U6828 10/- U6828</th> <th>3Q4 8/- 6K7 1/6 12AT7 5/- 50C5 10/- 3Q5 9/- 6K7G 2/- 12AT7 5/- 50C5 10/- 3S4 7/- 6K7GT 7/6 12AU7 5/- 50C6627/6 3V4 7/6 6K8 9/6 12AU7 5/- 50L6 8/6 5U4 4/- 6K8G 9/6 12AU7 5/- 53KU 12/- 5Y3G 7/9 6K8G 9/6 12BA6 7/6 78 7/- 5Y3GT 8/6 6L1 10/- 12BH7 10/- 80 9/- 5Z4G 9/6 6L6 7/6 12C8 8/6 85 17/6 5Z4GT 9/6 6L7 10/- 12J7GT 8/6 85 17/6 6A7 9/- 6L19 15/- 12/7GT 8/6 85 17/6 6A86 8/6 6134 10/- 12/7GT 16/6</th>	EY86 77. PCC85 976 EY91 37. PCC88 126 EZ35 67. PCC88 126 EZ41 77. PCF80 97. EZ40 77. PCF80 97. EZ40 77. PCF80 97. EZ80 676 PCF84 1276 EZ81 676 PCF86 1276 EZ81 676 PCF84 1276 EZ81 676 PCF86 1276 EC4 157. PCL85 1076 FC13 157. PEN45 1076 FW4/800 97. PEN440 776 GZ30 1076 PEN450 GZ33 1973 PEN450D HABC86107. PEN450D PEN450D	TDD13C TD13C TF141 27/6 TF441 27/6 TF46F 12/6 U12 9/- U12 9/- U12 9/- U12 9/- U24 21/- U25 12/6 U26 10/- U31 9/- U35 17/6 U37 17/6 U37 17/6 U37 17/6 U43 8/6 U37 17/6 U43 10/- U52 4/- U78 4/6 U78 4/6 U191 15/6 U329 12/6 U301 22/6 U329 12/6 U404 10/- U8801 19/9 UA8C80 7/- U6841 8/- U86281 10/- U8628 10/- U8628 10/- U8628 10/- U8628 10/- U8628 10/- U8628 10/- U6828	3Q4 8/- 6K7 1/6 12AT7 5/- 50C5 10/- 3Q5 9/- 6K7G 2/- 12AT7 5/- 50C5 10/- 3S4 7/- 6K7GT 7/6 12AU7 5/- 50C6627/6 3V4 7/6 6K8 9/6 12AU7 5/- 50L6 8/6 5U4 4/- 6K8G 9/6 12AU7 5/- 53KU 12/- 5Y3G 7/9 6K8G 9/6 12BA6 7/6 78 7/- 5Y3GT 8/6 6L1 10/- 12BH7 10/- 80 9/- 5Z4G 9/6 6L6 7/6 12C8 8/6 85 17/6 5Z4GT 9/6 6L7 10/- 12J7GT 8/6 85 17/6 6A7 9/- 6L19 15/- 12/7GT 8/6 85 17/6 6A86 8/6 6134 10/- 12/7GT 16/6
META RMI 5/3 I4RA I-2-8- RM2 7/6 I6RC I-1-14 RM3 7/9 I4RA I-2-8- RM4 I4/- I8RA I-1-14 RM5 19/6 18RA I-2-8- 14A86 17/6 18RD 2-2-8-	6-1 8/6 14A100 -3 19/- (FC31) 16RD 2-2-8- 6-1 6/6 (FC116) 16RE 2-1-8- -1 11/- 18RA 1-1-8-	8/6	TRANSISTOR BARGAINS OC44 61- OC45 71- OC71 51- OC72 61- OC74 61- OC75 61- OC77 61- OC81 61- OC81D 61- OC82 81- OC82D 81- SILICON RECTIFIERS 400 volts 350 mA I51- each
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PRACTICAL WIRELESS

December, 1962

SURBITON PARK RADIO LTD. FOR POST HASTE-POST FREE SERVICE

MARTIN RECORDAKITS

The following recorders, available now in four track, are a proprietary range of machines in kit or assembled form. This enables you to take advantage of mass production techniques and prices, abould you wish to assemble yourself. The components used are the finest available, with B.V.A. valves, and the decks are the latest baving all the improvements B.S.R. and to lato make from time to time, heads, etc. The amplifiers are packed in special cartons with instructions to enable anyone to build. We are confident you will that these recorders very good value, they have been built up to a standard and not down to a price.

HALF TRACK

FET1, complete with valves	\$6.17.6
JASON F.M. TUNERS	
Building Instructions available at 2/6 each kit (refunded if kit	bought)
This machine is listed at 39 gns, by makers and is a very good huy.	
Deposit 23.10.0 and 12 monthly	42,18,9
phone, in a DA Luza two tone grey as hinet assembled for	\$35.0.0
We can offer the above recorder, complete with tape and micro-	22.8.2
Total Kit as above	£29.0.0
	\$5.5.0
Deposit \$1.4.0 and 12 monthly.	19/-
	£11.11.0
makic eye, radio and mic, in nuts RY 1/8 english ter-	
Complete with valves, knobs, plana, screws, etc. EF86, ECC53, EM84, EZ81. OA81 and 2 EL84, 3 watts output.	
control and input usnels, mains and output transformers	
	#=1010
	\$1.0.8
	£2.1.6
	\$25.0.0
The above recorder can be supplied assembled, tested and com- plete with tape and microphone for	
	\$1.16.6
CAST CAST	\$22.0.0
CARH VIG VIG X 410. SDEAKER, ID LWO LODE FRY. CARH	\$4.4.0
Deposit 21.0.0 and 8 monthly	£1.1.0
mounts onto the deck, making a self contained unit CARE	\$8.8.0
Tape Amplifier for B.S.R. deck, printed circuit ready wired, with ECC83, ECL92, EM85 and EZ31. Complete with all	
Deposit ar and a monthly	£1 1 0
B.S.E. TDE Monardeek, latest model 5 in. spoolCASH	£9,9,0

Deposit At 1.0 and 8 menthles	90.11.0
Deposit 21.1.0 and 6 monthly	£1.2.9
	\$7.17.6
	£1.2.6
Deposit \$1.0.0 and 9 monthly	£9.15.0
The second state of the se	£1.1.8
	\$9.12.6
	\$1.1.4
	£12.0.0
Deposit £1.4.0 and 12 monthly	
Power pack kit ready drilled chassis for FMT1, etc.	19/10
The instance is the ready drined changes for FMT1, etc.	\$2.12.6
	ι. · ·
JTV/2, switched F.M. and TV. Sound self powered. All valves.	-
CASH (214.15.0
Deposit #1.9.6 and 19 monthly	81 4 5
	#10 15 O
Deposit \$1.0.0 and 18 monthly.	\$10,19.0
The instruction book is easing the head of the	\$1.6.6
The instruction book is again included but is otherwise 3/6 each.	
All the above units are available ready built and aligned. Price on	request.

GRAMOPHONE EQUIPMENT

	B.S.K. UA 14 TCS/H cartridge	47 15 0
	· Deposit si.u.u and 7 monthly	01 0 0
	Garrard Autoslim, new unit	\$1,\$,3
•	Deposit #1 0 f and 5 conthing to the CABH	#8.14.6
	Deposit \$1.0.6 and 8 monthly	£1.1.9
		#1018 a
	Deposit \$1.0.0 and 12 monthly	0111
	Fullys AUIVID, DOW LEADSCIDLIOD unit (changes on 45 mm) CAGE	879 10 0
	Deposit \$1.7.0 and 12 monthly	#13,10,0
	Depose state and 12 monthly	\$1.2.4

REGENCY

speaker. no conti Regancy, etc.

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TRANSISTORS

Mullard have reduced the price of many Transistors to: OC44 11/-, OC45 10/-, OC70 6/6, OC71 8/6, OC72 8/-, OC76 8/-, OC76 8/-, OC81 8/-. These are their new list prices. Why buy surplus. OC72 in matched pairs only at 16/- pair (No other types.)

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B.S.R. TD2	£11.11.0
	19/-
	£9.9.0
	\$1.1.0
	24.4.0
Complete Kit as above	\$25.0.0
	\$17.17.0
	419.19.0
	£1.0.8
Case with Sin. I Din. ADGAKEP	\$5.5.0
	\$34.0.0
Deposit \$3.5.0 and 12 monthly	\$2.16.6
	8410.0
ECL82, EZ80 and EM85, Radio and Mic. sockets, gives	
an equalised output of 400 m/Volts	
Hall Track	\$8.8.0
Deposit \$1.0.0 and 8 monthly.	\$1.1.0
Quarter Track CASH	
Deposit #1.0.0 and 9 monthly	\$9.9.0
Marriott Tape Heads. 4 track type L/RPS/7 and L/ES/9 Record/	£1.1.0
Playback and Erase with mounting bracket for Studio	
deck.	
Pair Complete (Marriott list price is \$8.14.0)	
Marriott 2 track type R/RP/1 Record/Playback only with bracket	\$4.4.0
for Studio deck. Ideal 3rd head	
Pressure pad (Studio deck only)	\$1.7.6
M.S.S. 2 track type DR1 and DE1 Record/Playback and Erase	8/6
Bets only	
Bets only	\$1.2.6
MAKERS	PROM

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T4B V.H.F. Tuner, self powered
Deposit #2.6.6 and 12 monthly
PART AND CARE AND CARE AND CARE AND LONG CARE AND LONG
Deposit 22.16.6 and 12 monthiy \$2.6.1
AF200 A.M./F.M. Kadio Chassis, bass and treble controls
P.U. inputs, single ended output stage
Deposit \$2,5,0 and 12 monthly
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both channels. Separate tone and volumeCASH #32.15.0
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Deposit 24.7.0 and 12 monthly
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Individual leaflets giving full description and technical details.

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Weymouth Radio 6 Transistor Superhet, using the P50 coils as they advertise in this journal. P50/1AC Osc., coil 5/4, P50/2CC 1st and Pnd 1,F.T. 5/7 each, P5:0/32C Srd 1,F.T. 6/4. RA2W rod aerial 12/6, LPDT4 driver 9/6, PACI printed circuit 9/6, Instruction Book 2/, soft resistors 7/6, Vol. control D.P. 6/, set conciences 20/. J.B. gang 12/6, Beebive trim-mers 1/3 each, W/C switch 3/6, dial and knob 5/6, battery PP11 5/6, Battery piug 1/-, OA81 3/-. Bet of Mullard transistors 53/6. Car aerial comping coil 1/-.

\$5 ohm 7in. x 4in. speaker, Ideal for Weyrad circuit \$1.7.8 Transistor Cabinet for 7in. x 4in. speaker. Ideal for Weyrad circuit,

two tone grey #1 19 A ******

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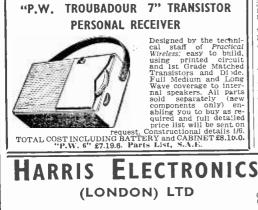
AMPLIFIER TYPE A1413, Ex.R.A.F. For normal A.C. Mains use. 524 Rectifications with 606 output, Input and output jack sockets, gain control, tully fused, 600 ohms output trans-tormer easily changed for 3 ohms type. Standard rack mounting size 19. x 7 × 6°. Used, good condition. ONLY 5906 (carriade etc. 10/6).

POWER UNITS TYPE 234. Primary 200/250 v. 50 cycles. Outputs of 250 v. 100 mA, and 6.3 v. 4 amps. Fitted double smeething For normal rack mounting (or bench use) having gree 'front panel size 19' x 7'. Fitted Input and Output Voltmeter, 79/6, or model less meter 59/6. (Carriage either type 10/6.)

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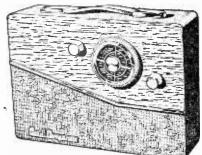
THE FINEST COMBINED PORTABLE and CAR RADIO YET DESIGNED FOR THE HOME CONSTRUCTOR

diodes. Full Medium and Long Wave Long Wa

Ouality speaker.

• Brillian-tly styled 2-tone cab-inet, size 11 x 8 x 3in,

Very fine tuning with calibrated dial.



• Latest printed circuit. • Internal high gain aerial with car aerial socket. Easy to follow construction data (available separately 3/6). All parts sold separately and full tilustrated details will be sent on **FO** £9.19.6. request.

Total Cost With alternative luxury cabinet using 7 x 4in. speaker, **\$10.19.6**. Either type, plus 5/- post and ins. (Battery 3/6 extra.)



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(carr. paid) Brand new set, in superb wainut cabinet (size 19 x 84 x 144)in. high). Covering 80-100 McN. 16-49 M. and 200-500 M. Mains trans. 200-200 v. with 2 tappings. Ferrite rod aerial for A.M. Controls: volume on/off, tone tuning; w/change. Gram and ext. speaker position provided. Vaives 12AT7, 12AH8, 6BJ6, EAB/C90, 6BW6 and metal rectifier. Fully guaran-teed. Today's Value, £20.

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500mW push-pull output. Ferrite rod aeriai. Car acrial aocket and coil. M.W. and L.W. full coverage. Operates on two 4.5v. cells. Printed circuit board 31 x 21in. All holes drilled and component positions marked. Instructions 28 for 16 p. (refunded on purchase of kit). Size 9 x 31 x 7in. 8 x 22in. P.M. high quality speaker. Attractive Vynair covered cabinet two tone. Two batteries 58 fbt he pair (Ever Read) 1263. Mulland transis-tors 0C44, 2 x 0C45. 0C431D, and 2 x 0C431. Top grade Weymonth Radilo coils and transformers. All gament service if required 17/6 (inc. post). Write for list of prices. All parts supplied separately. Built in two hours. post). Wi two hours.

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FILE XIZ CARF. paid Fully built 2-valve amplifier B.S.R. 4-sp. autochanger, case 17 x 15 x 84in. Assembled in 15 mins. Similar cabinet for tape recorder with plain board only \$3, carr. paid. Attractive colours.

or with 3-valve amplifier 15'- extra

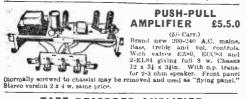
AUTOMATIC RECORD CHANGERS-I.ATEST MODELS. 4 SPEED CRYSTAL CARTRIDGE. All 6/- extra carr. B.S.R. UA14, £7,10.0, Oarrand Slimilne, Mono 25, Sterco, 28,5.0. Motor Board tor UAS, UA20, UA14, Slimilne, 5/- (post 1/6) or 3/8 post paid when purchased with Autochanger. Motor Board for Collaro UG0, 4/- Fost paid.

TELEFUNKEN STEREO AMPLIFIERS. 2 ECL42-2 x 24 watts, 12 x 9 x 2in. piano keys, \$7.0.0, post paid. Complete with power.

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SELF-POWERED VHF TUNER CHASSIS Covering 88-95 Mc/s. Mullard permea-bility Tuner. Dims. $10\frac{1}{3} \times 4\frac{1}{3} \times 50$. Mc/s. BCC95. EF91, EF91 and 2 diodes. Metai Rectlifter. Mains transformer. Fully wired and tested. Only 27.10. (carr. pd.). Some tarnished chassis otherwise O.K., 8710.0. 26.10.0





TAPE RECORDER AMPLIFIER



TAPE RECORDER AMPLIFIER The second s

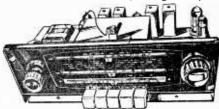
Also available for Collaro Deck. State which.

Transistor Set Battery Eliminator. Converts your 6 transistor receiver to mains operation. Size 1 1 x 1 n fin. With flex lead and battery charging attachment, 18/6.

Staar "Galaxy" or Garrard 9v. battery operated single 45 r.p.m. record player deck, with pick-up arm, and stylus. etc. Unly 501-, P. & P. 4/-.

NEW LOUDSPEAKER BARGAINS. Good Makes. 2-3 ohns 13 x 8 jin, 35/- (4/-); 7 x 4in. 14/6 (2/-); 6] x 4 jin. 12/6 (2/-);
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 9 x 6in. 28/- (2/6); 8in. circ. 18/6 (2/6); 10in. circ. 25/- (3/-). Postal charges bracketed.

BRAND NEW AM/FM (V.H.F.) RADIOGRAM CHASSIS AT £14.0.0 (Carriage Paid)



A.C. ONLY. Chassis size 15 x 61 x 3-16. New manufacture. Dia. 14j x 4in. in 2 colours predominantly gold. Pick-up. Ext. Speaker. Ac., E., and Dipole Socketa. Five push buttons-OFF L.W., M.W., F.M. and Gram. Aligned and tested. O.P. Transformer. Tone Control. 1000-1900 Mi. 200-500 Mi. 38-98 Me/s. Valves E230 rect., ECH31, EF99, EABC30, EL54, ECC35. Speaker and Cablnet to fit chassis (table model). 47/6 (post 4/-), 9 x 6in. ELLIFTICAL SPEAKER, 20/-, to purchasers of this chassis. TERMS: (Chassis) 25 down and 5 monthly payments of 22. Cheap Room Disole for V.H.F., 12/6. Feeder 6d. yd. Circuit diagram 2/6.



6-TRANSISTOR PORTABLE-Fully Built

The "SCALA" for only \$9,17.6, carr. paid. $\delta_3^+ \propto 2 \times \delta_1^{\rm lin}$ high. Choice of colours. Revine. M.W. and L.W. Ferrite aerial. Battery included. Printed circuit. Nicel's styled. A professional job. 31m. speaker. Fully Tunable M.W. and L.W.

THIS SUPERB SET for £10

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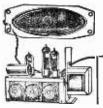
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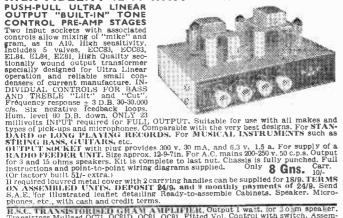
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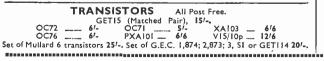


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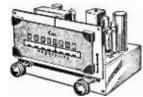
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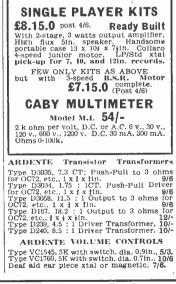
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BALANCED TWIN FEEDER yd. 6d. 80 or 300 ohms. DITTO SCREENED per yd. 1/6. 80 ohms only.	BULGIN PLUGS AND SOCKETS. Non-reversible P74, 2-pin, 4/3; P73, 3-pin, 4/6, etc.
Wirewound Ext. Speaker Control, 10 Ω 3/ WIRE-WOUND POTS, 3 WATT. Pre-set Min.	JACKS. English open circuit, 2/6. Closed clrcuit,
TV Types. All values 10 ohms to 25 K., 3/- ea.	JACKS. English open circuit, 2/8. Closed clrcult, 4/3. Grundig type. 3 pin, 1/3. JACK PLUGS. English, 3/-; Screened, 4/-; Grundig,
WIRE-WOUND 4 WATT Pots. Long spindle.	3 pin, 3/6.
PHILIPS TRIMMERS. 0-10 pF. 3-30 pF. 1/	ALADDIN FORMERS and cores, in., 8d.; in., 10d. 0.3in. FORMERS 5937 or 8 cans TV1 or 2, in. sq. x 2in. or in. sq. x 1in., 2/- with cores.
TRIMMERS, Ceramic. 30, 50, 70 pF. 9d.; 100 pF, 150 pF. 1/3; 250 pF. 1/6; 500 pF, 750 pF, 1/9.	sq. x 2 ¹ / ₂ in. or ² / ₁ in. sq. x 1 ¹ / ₂ in., 2/- with cores. SLOW MOTION DRIVES. 6:1, 2/3.
TV etc. TRIMMER, 1000 pF, with knobs, 2/ RESISTORS, Preferred values, 10 ohms to 10 meg.	SOLON IRON, 25W, 200V or 230V. 24/
i w., 4d.; i w., 4d.; 1 w., 6d.; 1 w., 8d.; 2 w., 1/	ANTEX SUB-MIN IRON 15w. 200 or 240 v., 29/6.
ALANCED TWIN FEEDER y_4 id. 80 or 330 ohms. DITTO SCREENED per yd. 1/6. 80 ohms only. WIRE-WOUND FORS. 8 WATT. Pre-set Min. TV Tpres. All values 10 ohns to 25 K., 3/- es. 30 K. 50 K. 4/a (izhoba S0 K.) to 2 msg. 3/-). WIRE-WOUND 4 WATT Pols. Long spindle. Yalue, 50 ohms to 50 K. 6/68. 00 K. 7(6. YHILIPS TRIMMERS, 0-10 / PF. 3-30 F. 16. FHILIPS TRIMMERS, 0-10 / PF. 3-30 F. 16. FRIMMERS, Persnel, 3/6, 600 / P, 750 PF. 1/9. TV etc. TRIMMERS, 1010 pF, 150 nms to 10 msg. i.w., 4d.; i.w., 6d.; 14 w., 8d.; 14 w., 8d.; 16 nf. 1/3, 150 pF. 1/6, 100 pF. TV etc. TRIMMERS, 100 pF. 7750 pF. 1/9. TV etc. TRIMMERS, 100 pF. 761 pF. 1/9. TV etc. TRIMMERS, 100 pF. 761 pF. 1/9. TV etc. TRIMMERS, 100 pF. 761 pF. 1/9. TV etc. TRIMMERS, 100 pF. 1/9. 1/9. 1/9. 1/9. 1/9.	JASON FM TUNER COIL SET
10 J WIKE-WOUND RESISTORS C 0/_	JASON FM TUNER COIL SET 29/ H.F. coil, aerial coil, oscillator coil, two 1.f. transformers 10.7 Mc/s detector transformer and heater choke.
15 watt 10 0hms-10,000 onms 2/-	detector transformer and heater choke.
12.5K to 50K 10 w 3/-	Circuit and component book using four 6AM6, 2/6. Complete Jason FMT.1
AMERICAN "BRAND FIVE" PLASTIC RECORDING TAPE	Kit. Jason chassis with calibrated dial, components and 4 valves, £6.5.0.
Double Play 7in. reel, 2,400it. 60/- Spare	MAINS DROPPERS, Midget adjustable sliders,
Reels	0.3A, 1,000 ohms, 5/-; 0.2A, 1,200 ohms, 5/-; 0.15A, 1,500 ohms, 5/-; 0.1A, 2,000 ohms, 5/-;
5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	MIKE TRANSFORMER. 50-1, 3/9.
Standard 7in. reel, 1,2001 23/6 4in. 2/- Standard 7in. reel, 1,200ft. 25/- 51in. 2/-	P.V.C. Conn. Wire, single or stranded, 2d. yd. Sleeving, 1 or 2 mm, 2d.; 4mm, 3d.; 6 mm, 5d. yd.
5in. reel, 600ft. 16/- 7in. 2/6	SPEAKER FRET. Gold cloth, 17 x 25in., 5/-: 25 x
"Instant" Bulk Tape Eraser and Read Defluxer, 200/250 v. A.C., 27/6.	35in., 10/-, Tygan, various colours, 52in. wide from 10/- ft.; 26in. wide, from 5/- ft. Samples, S.A.E.
Leaflet with full details, S.A.E.	Expanded Metal, Gold, 12 x 12in., 6/
CRYSTAL SET BOOKLET, 1/-, CRYSTAL DIODE (J.E.C., 2/-, GEX34, 4/-, OA81, 3/-, HIGH RESISTANCE PHONES, 4,000 ohms, 15/- pr. SWITCH CLEANER. Fluid squirt spout, 4/6 tin.	TELEVISION REPLACEMENTS
HIGH RESISTANCE PHONES. 4,000 ohms, 15/- pr.	Line Output Transformers from 45/- each, NEW Stock
	and other timebase components. Most
HIGH GAIN TV PRE-AMPLIFIERS RAND 1 B.B.C.	makes available. S.A.E. with all enquiries
HIGH GAIN IV PRE-AMPLIFIERS BAND I B.B.C. Tunable channeis I to 5. Gain 18dB. ECC84 valve. Kit price 29/6 or 49/6 with power pack. Details 6d. (PCC84 valves if preferred.) BAND III I.T.A.—Same prices. Tunable channels 8 to 13. Gain 17 dB	WEYRAD
with power pack. Details 6d. (PCC84	COILS AND TRANSFORMERS FOR 2-WAVE TRANSISTOR SUPER- HETS WITH PRINTED CHRCUIT
BAND III I.T.ASame prices.	HETS WITH PRINTED CHRCUIT AND FEBRITE ROD AFRIAL
Tunable channels 8 to 13. Gain 17 dB	AND FERRITE ROD AERIAL Long and Medium Wave Aerial—RA2W. On 6in. rod, 208pF tuning. 12/6
1/16in. Paxolin Panels, 10 x 8in., 2/-,	On 6in. rod, 208pF tuning. 12/6 Car Aerial Coil. 1/-
1/16in. Paxolin Panels, 10 x 8in., 2/-, Miniature Contact Cooled Rectifiers, 250V 50mA. 7/6: 250V 60mA, 8/6: 250V 85mA. 9/6: 200 mA. 21/-; 300mA, 27/6. TV etc., Silicon Sub-Min. Rectifier. 125V. 300mA. 6/6: 250V, 300mA, 14/6. Selenium Reet., 300V 85mA. 5/-, Colis Wearlte "P" type. 3/- each. Osmor Midget "Q" type, adj. dust core, from 4/- each. All ranges. List S.A.E. Teletron D.W.R. L. and Med. T.R.F., with reaction. 4/-, Med. wave D.R 3/6. Ferrite Acrials. M 8/9; M. and L., 12/6. Osmor Ferrite Rod Acrials, L. and M. for transistor circuits. 10/- each.	On oth. Tog, 2007 cuning. 1270 Car Aerial Coll. Osc. Coll P50/1AC. 176pF tuning. 5/4 Ist and 2nd 1.F. Trans.—P50/2CC. 470k C. 11/16in. dia. by 1in. 3rd 1.F. Trans.—P50/3CC. 6d. each. Sparsc Cressformer—LFDT4. 6d. each. Wavee hares Silde Switch. 3/8
85mA, 9/6; 200 mA, 21/-; 300mA, 27/6. TV etc., Silicon Sub-Min, Rectifier, 125V.	11/16in. dia. by lin. 5/7 each. 3rd I.F. Trans.—P50/3CC. 8/-
300mA, 6/6; 250V, 300mA, 14/6. Selenium Rect. 300V 85mA, 5/-	Spare Cores 6d. each. Driver Transformer—LEDT4. 9/6
Coils Wearite "P" type, 3/- each.	Wavechange Slide Switch. 3/6 Printed Circuit—PCA1. Size 24 x 84in.
from 4/- each. All ranges. List S.A.E.	Printed Creater PCAL, Size 24 Volt. Ready drilled and printed. 9/6 Volume Control, 5K8DP. 4/6 7 x 4/n, 35 ohm Speaker. 25/- 3łin. round 35 ohm speaker. 19/6 24 Fixed Resistors. 10/6 16 Fixed Condensers. 21/- The Cong. with triburgers 10/6
with reaction, 4/ Med. wave D.R., 3/6.	Volume Control, 5K8DP. 4/6 7 x 4in., 35 ohm Speaker. 25/-
Ferrite Aerials. M., 8/9; M. and L., 12/6. Osmor Ferrite Rod Acrials, L. and M.	3in. round 35 ohm speaker. 19/6 24 Fixed Resistors. 10/6
for transistor circuits, 10/- each. Ferrite Bods, 8 x iin., 3/-; 8 x 5/16in., 3/-;	24 Fixed Resistors. 10/6 16 Fixed Condensers. 21/- Tuning Gang with trimmers. 10/6
H.F. Chokes, 2/6. Osmor QC1, 6/9.	Tuning Cang with trimmers. 10/6 6 Mullard Transistors and diode. 42/8 Constructor's Booklet. 2/-
Repanco DRR2. 4/-, DRX1. 2/6.	Constructor's Booklet. 2/- Circuit and Details S.A.E.
Osmor Ferrite Rod Acrials, L. and M. for transistor circuits, 10/- each. Ferrite Rods, 8 x 11n. 3/-3 x 5/161n. 3/- H.F. Chokes, 24 & Osmor QCI, 6/9. T.R.F. Colls, A/HF. 7/- pair: HAX. 3/-, Repanco DR.2. 4/H. 7/- pair: HAX. 3/-, Repanco DR.2. 4/H. J. 2/8- Radio Sciewed Tects, 51n. 66(Hrver, 5/-, Solder Radiograde, 4d. yd., Hb. 5/-, Black Crackle Paint, Alr drying, 3/- tin.	NEW MULLARD TRANSISTORS
Solder Radiograde. 4d. yd., 4b. 5/ Black Crackle Paint. Air drying, 3/- tin.	OC71 6/-, OC72 7/6, OC81D, 7/6, OC81. 7/6, OC44 8/9, OC45 8/9, OC171 10/6, AF117 9/8
Aluminium Chassis, 18 s.w.g. Plain	 NEW J. COLD ARG. CITA AND CITATA AND CITAT
undrilled, 4 sides, riveted corners,	mfd. 15 volt 2/8 each Transistor Holders
4/6; 9 x 7in., 5/9; 11 x 7in., 6/9; 13 x 9in.,	1/3.
8/6; 14 x 111n., 10/6; 15 x 141n., 12/6; Aluminium Panels, 18 s.w.g., 12 x 121n.	B.B.C. Pocket 2 Transistor. M.W. and L.W. Radio Kit. 22/6. Miniature earpiece, 7/6. Batt. 2/3.
Aluminium Chassis, 18 s.w.g. Plain undrilled. 4 sides, riveted corners, lattice fixing holes, 24th. sides, 7 x 4in. 4/6: 9 x 71n., 5/9; 11 x 71n., 6/9; 13 x 91n., 8/6: 14 x 111n., 10/6; 15 x 141n., 12/6; Aluminium Panels, 18 s.w.g., 12 x 121n. 4/6: 14 x 91n., 4/-; 12 x 81n., 3/-; 10 x 71n., 2/3; 8 x 61n., 2/-	Miniature earpiece, 7/8. Batt. 2/3.



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PRACTICAL WIRELESS

December, 1962



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Practical Wireless

Vol. XXXVIII No. 670 DECEMBER, 1962

= **Editorial and Advertisement** Offices: PRACTICAL WIRELESS George Newnes Ltd., Tower House, Southampton Street, W.C.2. © George Newnes Ltd., 1962 Phone: Temple Bar 4363 Telegrams: Newnes, Rand, London, Registered at the G.P.O. for transmission by Canadian Magazine Post. SUBSCRIPTION RATES including postage for one year Inland - - - - £1.9.0 per annum Abroad - - - - £1.7.6 per annum Canada - - - £1.5.0 per annum Contents Page Editorial 689 Round the World of Wireless 690 The Berkeley Loudspeaker 692 Enclosure ... Transistor Tuner/Receiver ... 696 Central Control Amplifier ... 703 DX on Medium Waves 706 ••• On Your Wavelength ... 708 ... The Auditron ... 711 ••• The Luxembourg Tuner 716 ... An Audio Absorption Watt-718 meter Radio Components and their 720 Functions An Advanced Geiger Head ... 725 733 Trade News A Simple Three Valver 737 ... 742 Midget Mains Portable • • • 750 Letters to the Editor 753 Club News

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The Final Link

HIS month we present the last in the current series of free, П double-sided blueprints and we feel we have produced two designs of widespread appeal and interest.

The first is the Luxembourg Tuner which, as the name implies, has been specifically designed for peak performance on 208m. This tuner incorporates some novel features which will appeal to those wanting to try something a little different, it is easy to build and is strongly recommended to readers who want betterthan-normal reception of Radio Luxembourg.

The reverse side of our blueprint also breaks new ground, so far as PRACTICAL WIRELESS is concerned. It is probably true to say that of the thousands of enthusiasts who take the trouble to build good quality receivers and amplifiers, a good many make do with inferior or indifferent arrangements for the final link in the audio chain.

One can, of course, mount a loudspeaker on a solid baffle or insert it into a box of any convenient shape and size and get reasonable (even superb) results. Much depends, naturally, on the predominating acoustics and the degree of audio discernment in the ears of individual listeners.

But this hit-or-miss approach, while capable of relatively good results can lead to disappointment and, in any case, it seems odd to carefully design the electronics and take the acoustics for granted.

In general, then, a well-designed enclosure is the only real housing for a loudspeaker and the only acceptable device for disseminating high quality audio.

We feel it is appropriate, therefore, to conclude this series of blueprints with The Berkeley-a specially designed bass reflex speaker enclosure which is suitable for use with P.W. or other high quality amplifiers and which will give added pleasure to your record, radio or tape listening.

Our Query Service

NCE again we must remind our readers of the rules of our Free Query Service. The following points should be carefully noted:

- (i) We cannot undertake to answer technical queries over the telephone
- (ii) All queries must be accompanied by the query coupon from the current issue
- (iii) If a postal reply is required a stamped and addressed envelope must be enclosed with the query.

We must also point out that we cannot design circuits to readers' specific requirements. Nevertheless we shall continue to help readers as far as possible but it should be remembered that all information necessary for answering the query should be sent to us.

Our next issue dated January will be published on December 7th.

ROUND THE WORLD

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NEWS AT HOME AND ABROAD

Broadcast Receiving Licences

THE following statement shows the approximate number of Broadcast Receiving Licences in force at the end of August, 1962, in respect of wireless receiving situated within stations the various Postal Regions of England, Wales. Scotland and Northern Ireland. The numbers include Licences issued to blind persons without payment.

Region London Home Counties Midland North Eastern North Western South Western Wales and Border C	Counti	es	т 	otal 636,984 592,973 429,035 453,898 390,268 348,923 198,280
Total England and Scotland	Wales	•••		3,050,361 325,608 109,518 3,485,487

High-power Radars for Ministry of Aviation

ONTRACTS by the Ministry of Aviation have been awarded to Marconi's for the provision and setting to work of three dual installations of 500kW, 50cm radars, type S264A. These will be sited at St. Annes (near Blackpool), Ash (near Sandwich, Kent) and Ventnor (Isle of Wight). These are the first radars ordered by the Ministry for the United Kingdom Airways System.

The dual installations consist of the complete transmitting/ receiving and ancillary equipment in duplicate, feeding a common aerial head on a main/

standby basis. One particular feature of the S264A equipment is that, being crystal controlled. it can be switched into operation from "cold" if necessary. Marconi 50cm radars

are currently in operation at many British airports. Service establishments and airfields.

Conference on the Design and Use of Microwave Valves

THE Electronics Division of the Institution of Electrical Engineers is organising a threeday national conference in September, 1963, on the design and use of microwave valves. This has been timed to fall between international conferences on microwave valves which are held every other year and the pro-gramme will be complementary to these conferences.

The forthcoming conference will review present techniques and developments and will cover fundamental valve design, present performance and the use of valves in systems, including matching system characteristics with achievable valve performance.

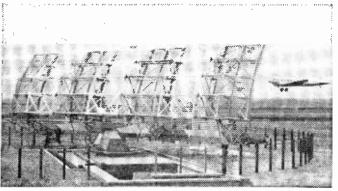
It will be of particular interest to engineers in this country who do not attend international conferences and among the subjects to be covered will be "signal amplification and physical measurement ", "communications and industrial applications and "radar".

New Headquarters Installation for R.A.F. Radio Amateurs

THE new headquarters of the R.A.F. Amateur Radio Society was opened recently at No. 1 Radio School, R.A.F. No. Locking.

The society, which was formed in 1939, includes a large number of professional wireless operators. both R.A.F. and ex-Service, in its membership and most local R.A.F. amateur radio clubs are affiliated.

A grant of £660 from the Nuffield Trust for the Forces has paid for the most expensive of the new installation which is used in conjunction with a beam aerial which can be directed to any part of the globe. A standby transmitter also capable of top band communication has also



A Marconi 50 cm surveillance radar of the type recently ordered by the Ministry of Aviation.

Recording Noise

LONDON is the first city in the world to be systematically surveyed for noise. The information obtained will be useful for town planning generally and especially to architects when making provision for insulation in new buildings of all kinds in the central area.

Information about noise levels at selected sites throughout central London is also being recorded for use in particular town planning problems such as assessing the noise effects of elevated motorways and heliports and for siting hospitals and other buildings where noise may be detrimental to their use.

The London Noise Survey is being conducted by the Building Research Station of the Department of Scientific and Industrial Research and the London County Council. Two vans with equipment which includes TR 52/2 professional tape recorders supplied by EMI Electronics Ltd. are sampling noise levels for 100 seconds once an hour over a 24-hour period at each of 540 points, distributed at 500yd. intervals on a rectangular grid over central London. The work has continued since early in 1961 and more than 350 sites have already been monitored.

Noises are automatically recorded on magnetic tape every hour on the unattended tape recorders. At the end of the 24-hour period the tape is taken to the Building Research Station at Garston for analysis.

New T.I.M. Recording

THE Post Office is to make new recordings for T.I.M., the Speaking Clock.

Speaking Clock. The present Speaking Clock, which has been in use since 1936, is to be replaced early next year. While the timekeeping of the present clock is as good as it was a quarter of a century ago some parts of it are obsolete.

The new clock, which has been designed and built by Post Office engineers at the Research Station at Dollis Hill, London, will, with the new techniques employed, be cheaper to instal, maintain and operate. The quality of the recordings will also be improved.



A member of the LCC staff is seen here switching on an EMI tape recorder in a van at an Albert Embankment site, in London, to record sample noise levels (see "Recording Noise").

The Great German Radio Exhibition

OVER 100 firms to date have registered for the Great German Radio Exhibition to be held at the Berlin Funkturm from August 30 to September 8, 1963. Final figures can only be estimated at the commencement of next year. However, it can already be determined that once again all halls and pavilions of the exhibition area occupied in 1961 will also be in demand for the Radio Exhibition of 1963.

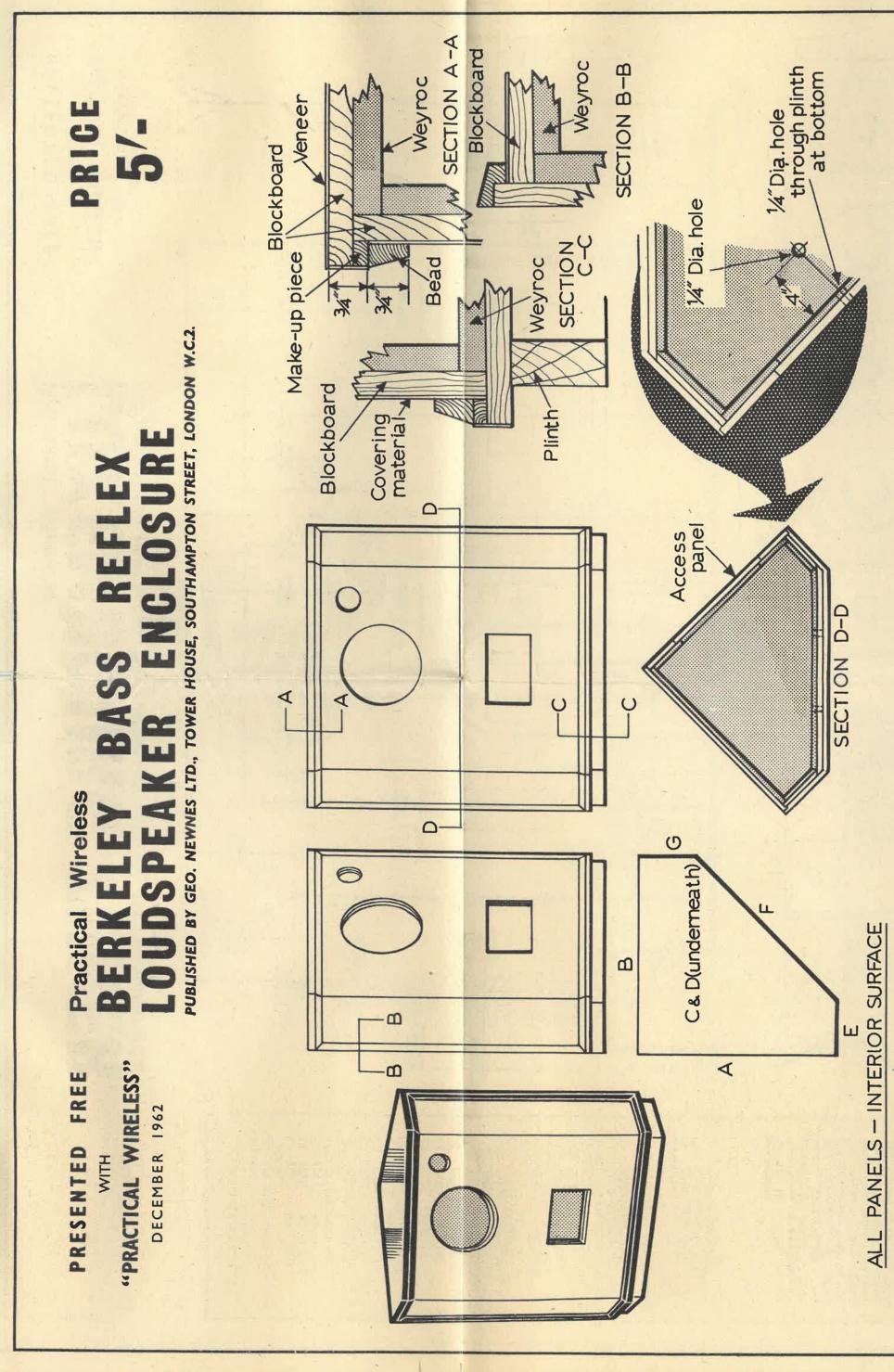
The studios of the broadcasting stations will again participate with demonstrations in the exhibition. Formerly only one hall of the exhibition grounds was required to house the Channel I television programme; however, in the coming year a further hall is planned for the Channel 2 programme.

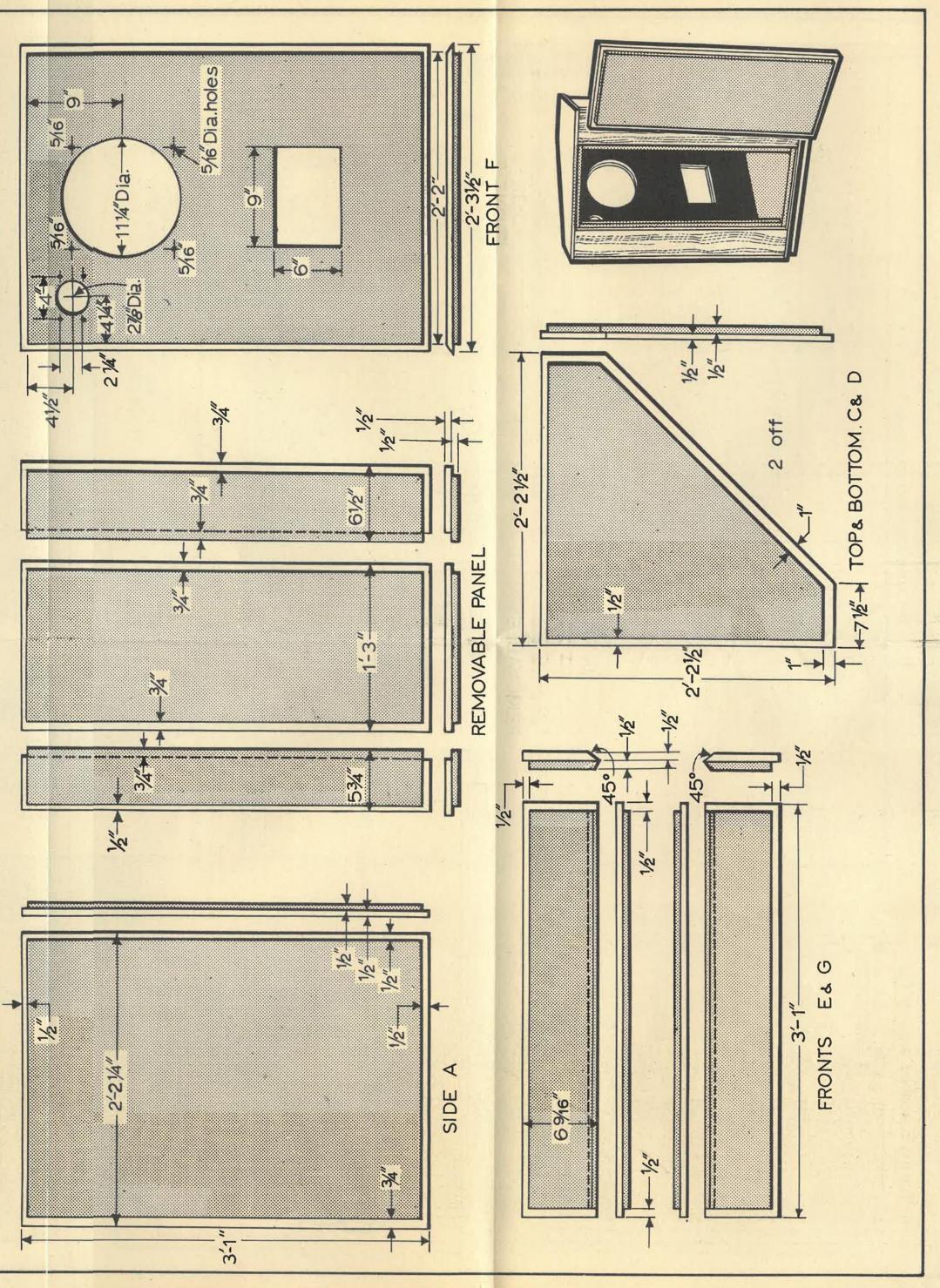
Temporary VHF Station on the Isle of Skye

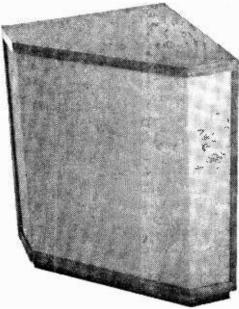
THE BBC's plans for extending and improving reception of

its sound and television broadcasting services in the West of Scotland and the outlying islands provide for several new transmitting stations, including a combined television and VHF sound station for the Isle of Skye. As the completion of this station and of the necessary radio links to connect it with the BBC's Scottish programme networks will take some time a temporary low-power VHF sound relay station has been brought into service at Penifiler to serve the town of Portree. This station is now transmitting the Scottish Home Service on 93.9Mc/s with horizontal polarisation, which means that VHF receiving aerials should be mounted horizontally.

It is hoped to complete the television station for the Isle of Skye and the permanent VHF sound station, which will radiate the Light and Third programmes as well as the Scottish Home Service, early in 1964.







A HIGH QUALITY BASS REFLEX CABINET

By R. Edwards

The BERKELEY Loudspeaker 7. Enclosure

HE bass reflex type of loudspeaker enclosure has been popular for many years on account of its ability to provide good smooth output down to the lowest frequencies normally reproducible by the particular moving coil unit employed.

In this type of enclosure, which is also known as a "vented enclosure" or "phase inverter cabinet", use is made of the sound waves radiated from the rear of the loudspeaker cone, and these waves are allowed to emerge at the front of the cabinet through an aperture or "vent" close to the loudspeaker opening. The interior of the cabinet forms a resonant cavity and its resonant frequency is determined by the volume of air enclosed and the area of the vent. It is usual practice for the enclosure to be tuned to the bass resonant frequency of the loudspeaker unit.

resonant frequency of the loudspeaker unit. Due to the loading provided by the enclosure, the characteristic peak in the loudspeaker speech coil impedance curve at bass resonance resolves into a pair of peaks, one just above the enclosure resonant frequency, and the other just below. The amplitude of both peaks is considerably less than that of the original single bass resonant peak, consequently there is less mismatch with the amplifier at this frequency than there would be normally, and so more power is delivered to the speech coil.

Furthermore, in the region of resonance, greater air loading is offered to the cone resulting in improved efficiency of the system together with a reduction of amplitude distortion.

For sound frequencies equal to and just above the enclosure resonant frequency sound waves radiated from the rear of the cone undergo a 180° phase change and appear at the vent in phase with the radiation from the front of the cone, thus the effective sound output is the combined output of these two sources.

When the sound frequency is lowered below resonance the phase of the air in the vent changes abruptly and tends to oppose that from the front of the cone. The response of the system therefore falls off just below the enclosure resonant frequency. On the other hand, as the frequency is raised above the enclosure resonance the enclosed volume of air becomes increasingly capacitive and the sound waves from the rear of the cone tend to become absorbed within the cavity, until eventually at high frequencies there is practically no output from the vent and the system performs as an infinite baffle.

Design Features

Optimum size for a bass reflex cabinet is governed by the particular loudspeaker to be used, the cone diameter and fundamental resonance being key factors in this respect. The Berkeley bass reflex enclosure is intended for use with a high power amplifier, such as the *Strand Amplifier* (described in the October issue of PRACTICAL WIRE-LESS), and has been designed around a 12in. dia-

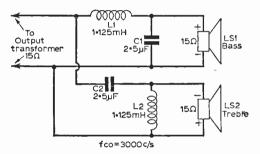


Fig. 1—A half-section, constant-resistance network; parallel connection.

meter moving coil unit having a power handling capacity of 15W. Provision is also made for the fitting of a H.F. tweeter unit.

The loudspeaker specified is WB Model H.F. 1216. This is a full range unit, covering 20c/s to 16,000c/s and has a fundamental resonance of 37c/s. A second choice would be the WB Model H.F. 1214. This is a less expensive unit and has a frequency coverage from 25c/s to 14,000c/s, while the bass resonance is at 39c/s.

A corner style enclosure has been adopted as this allows full advantage to be taken of the walls as reflecting surfaces and these improve the low frequency sound distribution. A triangular cabinet has good acoustical properties and is, of course, likely to prove the most convenient shape for installation in a room.

The dimensions of the *Berkeley* have been chosen to provide a volume of 9 cu. ft. which is about ideal for the type of loudspeakers specified, and it is tuned to just below 40c/s approximately by a plain vent. A smaller cabinet would result in inferior bass response and would also prove more critical in respect of tuning. The effects of standing waves are less serious in a large enclosure and can usually be dispelled by the use of only a small amount of lagging material.

To ensure rigidity and so prevent resonance effects from any of the surfaces, all panels are lin. thick and are built up from equal thicknesses of blockboard and chipboard and glued together. All joints must be glued and must be air tight since any air leakage other than through the two apertures in the front panel will impair the proper functioning of the enclosure as a "bass reflex".

The small aperture to the right of the large loudspeaker opening is for an H.F. tweeter unit, but the fitting of such a unit is quite optional. It is certainly advisable to try the enclosure with only the 12in. unit in position before incurring further expenditure which, subsequently, may not perhaps appear fully justified.

The question of what is correct tonal balance is very much a matter for the individual to decide, and it is possible that due to the efficient bass response there may seem to be some deficiency in the upper register. In such a case the incorporation of a tweeter unit should restore the balance satisfactorily by adding the necessary brilliance to the reproduction.

It is considered prudent to carry out this drilling and to fit the four screws during construction, or at any rate before the covering material is fitted to the front panel, since it would obviously be an inconvenient task to perform once the cabinet has been completely finished.

If a tweeter is not to be installed initially this hole must be covered by means of a piece of $\frac{1}{2}$ in. plywood about 6in. x 4in. This should be drilled to accept the four captive screws, and then clamped tightly against the inside surface of the cabinet with nuts.

The drilling details given on panel F (Blueprint) are for the W.B. Model T.12 Tweeter Unit. Details of this unit and suitable crossover networks are given later.

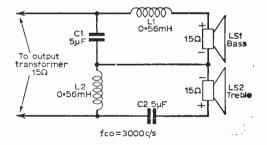


Fig. 2—A half-section, constant-resistance network; series connection.

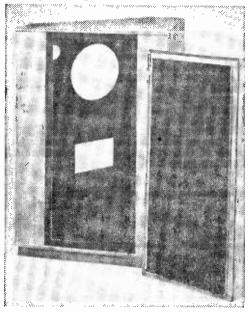
Lagging the Enclosure

Sound waves from the rear of the loudspeaker cone at middle and upper frequencies produce standing waves in the cavity, and these are sometimes of sufficient severity to disturb the smooth response characteristic of the system and so to "colour" the output. It may be necessary to lag the interior with absorbent material in order to eliminate such effects. The amount of lagging needed can be determined only by experiment.

needed can be determined only by experiment. Critical listening tests should be made with the completed (but unlined) enclosure installed in its final location. Such tests must be of fairly lengthy duration and should involve the reproduction of both music and speech, to permit a proper assess ment of the loudspeaker enclosure performance to be made. Dry, unnatural colouration or tendency to boominess or over accentuation of the lower frequencies may be cured by partially lining the inside of the enclosure with felt or fibreglass blanket material $\frac{1}{2}$ in. to 1 in. thick. It is suggested that only two interior surfaces

It is suggested that only two interior surfaces be lined, preferably the underside of the top panel and one of the side panels. An alternative and possibly better scheme is to suspend a curtain of the same material from the top panel so that it hangs diagonally across the interior of the cabinet.

The application of absorbent material must be carried out discriminately, since excessive damping of the enclosure can have an adverse effect on the high frequency response. The inspection panel must always be replaced firmly in position before resuming listening tests.

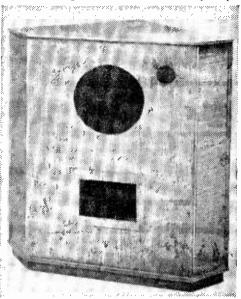


H.F. Tweeter Unit

The H.F. tweeter W.B. Model T.12 is a horn-loaded pressure driven moving coil unit. It has a frequency range of 3,000 to 17,000c/s, an impedance of 15Ω , and a power handling capacity of 15W.

When using the tweeter, a crossover or dividing network is also required in order to restrict the range of frequencies applied to each loudspeaker. The type of crossover network recommended is that known as a half-section constant-resistance network. This particular kind of crossover can take two forms, either "parallel connection" as shown in Fig. 1 or "series connection", Fig. 2. Actually there is very little to choose between these two forms. The series connection is often considered as being somewhat better in performance than the parallel arrangement; however, the latter circuit uses smaller value capacitors and so is cheaper and perhaps easier to make up. A crossover frequency of 3,000c/s should be used, and the appropriate component values are given in the circuit diagrams. That part of the circuit feeding the L.F. unit forms a low-pass filter, and has an attenuation rate of 12dB per octave above the crossover frequency. The H.F. unit is fed from a high-pass filter, this having a similar rate of attenuation below the crossover frequency.

The input impedance of the crossover network is 15Ω and the matching to the amplifier is not altered at all by the addition of the tweeter, although a slight loss in the total output does occur in the region of the crossover frequency.



Above—The enclosure ready for the finishing touches. Left—A view inside the cabinet.

A suitable crossover unit (type CX300—series connection) can be obtained from the manufacturers of the loudspeakers. For those who may wish to construct their own networks details are given below.

Paper, or metallised plastic film type capacitors should be used and these should have a voltage rating of 50-100V. Electrolytic capacitors are not suitable. It will be necessary to use capacitors in parallel in order to obtain the values specified.

The coils can be easily constructed by winding 16s.w.g. enamelled wire on a cardboard or plastic former 1in. diameter and 14in. long. Cheeks about 34in. diameter should be fitted at either end of the former. The 1·125mH coil requires 210 turns (about 16 layers) and the 0·56mH coil 145 turns (11 layers). All turns must be close wound and the layers even. Terminate the completed coil by passing each end of the wire through a pair of holes in the end cheeks then bringing out about 1in. of wire to provide the connection.

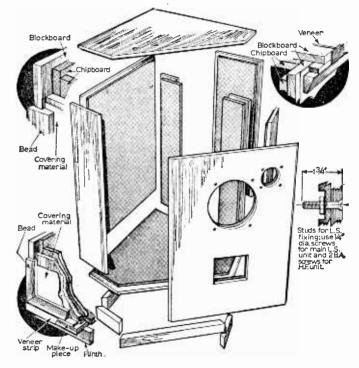
For convenience the filter components should be assembled on a small wooden panel and, after the wiring has been completed, this can be mounted on the floor of the cabinet. In order to avoid inductive coupling it is advisable to arrange the two coils so that there axes are at right angles to one another, and to space them about 3in. apart.

Since there is a 180° phase shift through the crossover network, the two loudspeakers must be connected in what would be normally anti-phase. Correct phasing can be established by reversing the two leads to one loudspeaker speech coil and observing which arrangement gives best sound output.

The Finish

Regarding the finish to the cabinet, use has been made of applied "Vinyl" or "Fablon" to the sides, and wood or plastic veneer to top and edges. This eliminates the necessity of polishing to great extent. The front is covering with approved loudspeaker fabric. It is suggested that the cabinet should be first made up "dry", then dismantled and finally glued up after any needful adjustments have been made.

Start by cutting all the blockboard panels to drawings on the Blueprint,, plane all edges square,



The units undermentioned in this article are manufactured by Whiteley Electrical Radio Company Ltd., Mansfield, Notts., England.

Building the Cabinet

The construction of this corner cabinet is quite simple, complicated joints being eliminated entirely. A little care and attention to planing edges square and true will be well repaid when finally assembling.

Two types of board are used, both of half an inch thickness. The inside is of chipboard (Weyroc) and the outer of blockboard or laminated blockboard. This latter material is a superior board and is well worth the extra expense. Owing to the acoustic requirements regarding cubic volume of the inside of the cabinet it will be found that a 9ft. x 4ft. board of each material will be needed. Stock sized boards are usually 8ft. x 4ft., so enquiries should be made concerning the availability of material of suitable size. and where required at 45°. Gauge a line to mark the boundary of the chipboard all around the inside face of each panel. Care must be taken to get these marks the right distance in from the edges. They vary, due to the overlapping.

Now cut the chipboard panels to fit the markings and screw each pair together with $\frac{3}{4}$ in. **x** No. 8 csk. screws at 1ft. centres. Having proceeded this far all sections should correspond to details on the Blueprint. Assemble the cabinet by screwing through the edges of the blockboard with 1in. **x** No. 6 csk. screws. making any adjustments to the meeting rabbeted edges, etc.

Glueing

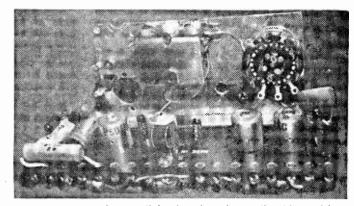
Having checked for squareness and tight joints, dismantle and glue and screw the respective panel sections together. These should be placed one on top of each other on a flat surface and weighted on top. Leave for a day to thoroughly set. This (Continued on page 749)

Fig. 3 (right)—An exploded view of the Berkeley.

transistor

tuner-

receiver



By A. Sydenham

ESPITE many criticisms of transistorised receivers one must acknowledge the high sensitivity of the superhet form—the distinction immediately being drawn between it and the TRF configuration.

A simple TRF receiver employing regeneration might perform well enough in an area of high signal strength but when used under less favourable conditions cause disappointment due to the low reserve of gain and limited tuned circuits.

The superhet holds pride of place for reliability, stability, sensitivity and general performance and no TRF receiver can be made to equal it without becoming equally expensive. Beginners in particular are well advised to realise this for it is easy to become misled.

Criticism of the audio quality emitted by transistor receivers and which is often considered inadequate for home use, is, however, frequently justified and is the price that must be paid for using small loudspeakers in small cabinets driven by Class B output stages from depreciating batteries.

But listening to a radio programme on a mains powered A.M. receiver—where good quality audio is available—is, in many areas, rather unsatisfactory, due to the characteristic whistle caused by neighbouring TV receivers and/or the sundry bangs and pops due to radiated interference.

It is an interesting project therefore to construct a transistor superhet tuner—which can be kept physically small—and feed its output to a good quality amplifier or, alternatively, to the "Gram" sockets of a suitable receiver. In this way much of the radiated interference is avoided for no external aerial is needed and at the same time an adequate reserve of audio gain becomes available.

Details of a suitable tuner are presented here of a model recently constructed. When fed to the input sockets of a 10W mains powered audio amplifier similar to the "5-10" the unit gave an excellent performance equalling that of the 2-valve superhet tuner it displaced, the quality obtained being considered superior to that of the model using

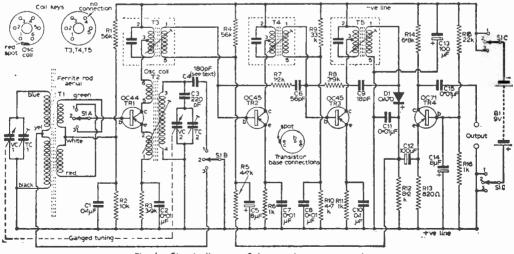


Fig. 1—Circuit diagram of the transistor tuner-receiver.

valves-which also had to have an aerial connected.

The unit has also been tested in connection with the "Gram" sockets of a standard broadcast receiver and it was further proved that the unit could be used as a complete headphone, or personal, receiver if so desired.

The Circuit

This is on conventional lines, reliability being the aim—see Fig. 1. No claims to originality are made; the circuitry is familiar and easily recognised. Practical problems arise, however, in converting a circuit diagram to a working model and a good layout is not always easily obtained. Here the difficulty is resolved.

Both the medium and long wavebands are covered, the switching being arranged so as to minimise the chance of the unit being left switched on accidentally. A standard 3-way, 4-pole rotary switch is employed: SIA and SIB selecting the waveband coverage, and the other two sections performing on/off duties and ensuring that the battery is completely disconnected at position "2". The central switch position is "off"; it is thus impossible to change from one band to the other without going through the "off" position.

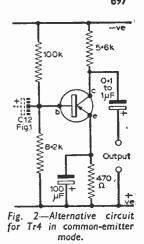
other without going through the "off" position. TR1 (OC44) functions as the frequency changer with TR2 and TR3 (OC45) as intermediate frequency amplifiers. Following the demodulator diode, D1, is an additional transistor, TR4 (OC71) which is used to drive the subsequent amplifier. The average emitter current of TR4 is 400μ A and the whole tuner consumes less than 4mA, thus making battery replacement only a minor problem.

If higher gain is required TR4 may be operated under common emitter conditions but the output impedance will be lowered to approximately $5k\Omega$. The necessary rearrangement of the stage is shown in Fig. 2 and if the unit is to be used as a headphone receiver this is the best method to adopt.

A minor economy can then also be effected by omitting the 5.6k Ω collector resistor together with the output capacitor connecting instead high impedance phones between the negative rail and TR4 collector. It might also become necessary to experiment slightly with the 100k Ω base feed resistor to obtain optimum results.

If the circuit of Fig. 2 is used to feed a valve amplifier it might also become necessary to vary the value of the upper base feed resistor, $100k\Omega$, since the collector resistor is, as specified, a little on the high side. Only a small emitter current is required — about 0.5mA.

Referring again to Fig. 1 it will be noted that all transistors a re stabilised by the familiar potentiometer, e m itter resistor form, and this together with the neutralising circuitry makes the u n it completely stable.



Mechanical Details

The whole tuner is constructed on a standard 18-way tag-board, the tags having been given imaginary numbers to assist correct identification. Although the appropriate figures can be marked on to the board it will usually be sufficient to locate No. 1 and No. 19 and count from there as required.

The oscillator coil and the three I.F. transformers are mounted so that their pins project through the tag side of the board and although a separate hole may be drilled for each pin it is generally simpler to use a single hole—just large enough for all the pins to pass through together for each component. This also makes the cores available from either end of the can. An array of small holes lies along the centre of the tag-board when it is purchased and it is only necessary to enlarge as required.

Panel

The wavechange switch, twin gang tuning capacitor and outlet insulator are mounted on a metal panel affixed to the tag-board in such a way that the tags come at the bottom as may be seen in the appropriate illustration. For dimensions of this panel see Fig. 4. Because it is made of metal the kin. fixing holes must be arranged to coincide with tags 3 and 11 on the board as shown and

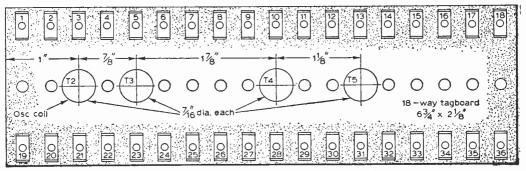


Fig. 3-Drilling details for the component tag board.

prior to bolting it in position $\frac{1}{16}$ in. thick paxolin washers must be placed over the bolts before they are passed through the board to prevent the underside of the "L" from short circuiting all the tag eyelets it hides.

A very simple bracket will also be needed to hold the ferrite aerial (which should be left to one side at this stage) and this will be bolted to tag 28 on the same side as the panel.

Constructional Notes

Actual wiring construction should commence by fixing the canned transformers by letting their fixing lugs pass through small holes drilled for them. Care should be taken to check that the orientation agrees with that shown. These lugs are then pressed out flat and soldered as shown in Fig. 5.

Before proceeding further it is advisable to plug each core hole on the transformers with sleeving or something similar to prevent any blobs of solder accidentally spilling in and locking the cores which are rather fragile.

The remainder of the tag side of the board can then be wired as indicated in Fig. 5. The transistors should be left until last. Check that electrolytic capacitor C12 and diode D1 are connected in the correct sense as shown. The taut layout allows for all component lead-out wires to be snipped off short.

When wiring of the tag side of the board is complete (except for the transistors) the other side can be tackled and all wiring is illustrated in Fig. 6 where the panel is shown pressed out flat for

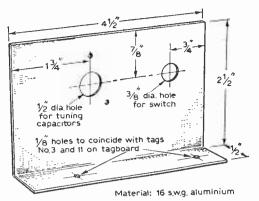


Fig. 4-Drilling details of wavechange switch panel.

clarity. C13 actually lies flush with the top of the board and must be slender enough not to foul the aerial (see illustration).

When the capacitors are in position—observe polarities—the transistor wires may be sleeved and passed through existing small holes on the board. Provided thin sleeving has been used the set of leads on each transistor will fit firmly yet not overtightly. The transistor shells thus remain on the top side of the board whilst their wires pass below and are soldered using the normal techniques.

The aerial may now be fixed in position as shown and wired allowing the connecting leads

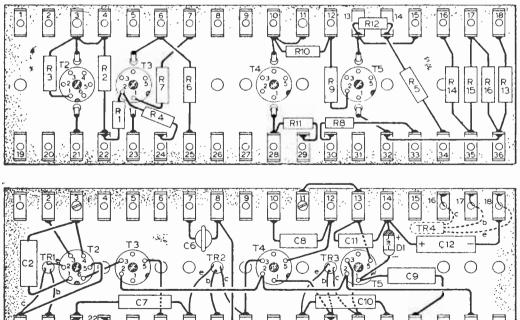


Fig. 5-(a) Details of fixing transformer lugs. (b) Details of tag board wiring.

0

0 25

C1

0 26

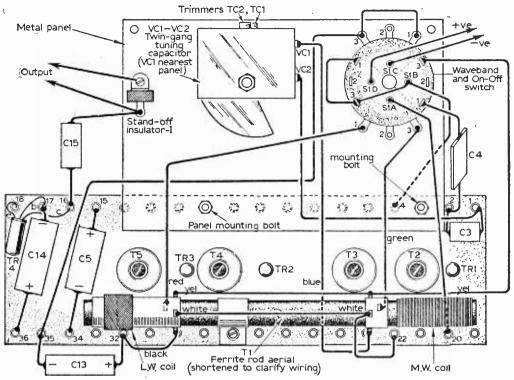


Fig. 6-Wiring diagram for top side of the tag board.

(which should be of stranded conductor) just loose enough to permit free movement of the two coils along the ferrite rod.

The Switch

Each of the four central "pole" tags control three of the "way" tags disposed around the rim of the switch and visual check is initially required to identify them correctly. It is then advisable to press flat alternate "way" sections as shown to obviate incorrect connections being made. If the battery flex leads are left until all the wiring has been checked over chances of damaging the transistors will be minimised.

When satisfied that all is well a black flexible lead approximately 6in. long is soldered to SIC rotor and a similar, but red, lead connected to SID rotor. The switch should then be set to position "2", the central position, and the appropriate stud connectors affixed to the free ends of the flexible leads which may then be twisted together neatly.

Setting Up

A length of suitable cable (coaxial will do if not very long) should be connected to the stand-off insulator "1" (Fig. 6) the far ends being equipped suitably and connected to an amplifier or to the "Gram" sockets of a suitable broadcast receiver which may then be switched on and adjusted to normal three-quarter volume level setting. Alternatively high impedance phones may be used. Control knobs are then fitted to the tuner spindles and a battery connected. The rotary switch should then be turned to position "3" (M.W.) and the vanes of the ganged tuning capacitor fully enmeshed.

The modulated output from a signal generator tuned to 470 kc/s is now applied to the fixed vanes connection of VC1. The cores of T5, T4 and T3 should be adjusted for maximum output in that order, the generator output being kept at a low level.

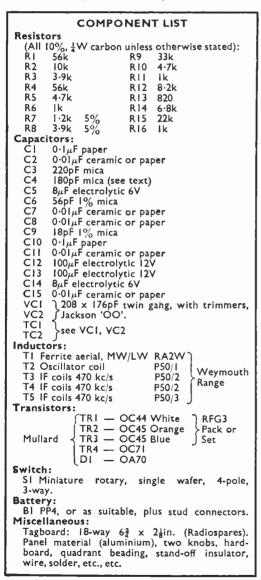
Next the generator is set to 600kc/s and the oscillator coil core adjusted to receive the signal which is then further strengthened by sliding the medium-wave coil along the ferrite rod until best results are obtained.

If the ganged capacitor is now rotated towards the other end of its travel the note should reappear again at 1.200kc/s. before the vanes are fully disengaged, to which frequency the generator may now be set before the aerial and oscillator trimmers TC1 and TC2 respectively, are carefully adjusted for best results.

Should the aerial trimmer need to be set fully home and the signal is still not considered correctly peaked then unscrew the oscillator trimmer slightly until the signal disappears. Now adjust VC1 to slightly fuller capacity when the signal will reappear; it should now be necessary to unscrew the aerial trimmer TC1 slightly to obtain a peaking point. The adjustments should then be made all over again, viz at 600kc/s and 1,200kc/s, until no improvement is possible.

The Long-wave Band

The rotary switch is next turned to position "1" and an attempt made at receiving the Light programme on 200kc/s with the vanes of VC1 approximately one-half enmeshed. It is quite possible that C4 will need padding a little and is located in such a way as to be easily accessible for this purpose. Values as small as 30pF connected in parallel make a good deal of difference. Experiment by temporarily connecting various small value capacitors (50-150pF) across VC2 in



turn at the same time swinging the vanes over full travel.

Another quick method is to connect a 90pF trimmer across VC2 temporarily. Immediately the signal is received the long-wave coil should be slid gently along the ferrite rod to obtain best results in association with VC1, and an assessment made of the precise value of capacitance needed for C4.

Warning

The unit must not be used under any circumstances in connection with a receiver or amplifier of the A.C./D.C. class nor with a so called A.C. receiver that derives its H.T. from the mains direct. It may be used with a transistorised amplifier, however, if required.

Comparable results are not likely to be obtained if alternative components, or transistors of another make, are utilised; the use of any sub-standard items is almost certain to ensure disappointment.

Cabinet

Dimensions of a suitable easily made cabinet constructed are shown in Fig. 7. It is made from hardboard held together with internally glued reinforcement strips, little weight being involved.

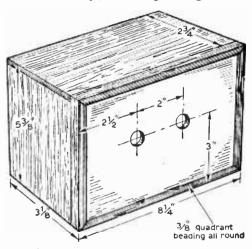


Fig. 7-Dimensions of suggested cabinet.

To avoid defacing the cabinet front the tuner can be locked by creating a sub-panel of hardboard through which four 4B.A. bolts may be passed and countersunk to coincide with holes in the metal tuner panel. This sub-panel can then be glued—with the bolts projecting—to the inside of the cabinet. When dry the tuner is placed in position and the four 4B.A. nuts applied and screwed home.

The actual cabinet front is cut $\frac{1}{2}$ in. smaller than the dimensions given in Fig. 7, a frame of $\frac{1}{8}$ in. quadrant beading being allowed to overlap by $\frac{1}{8}$ in all round to form a rebate for the sides, top, etc.

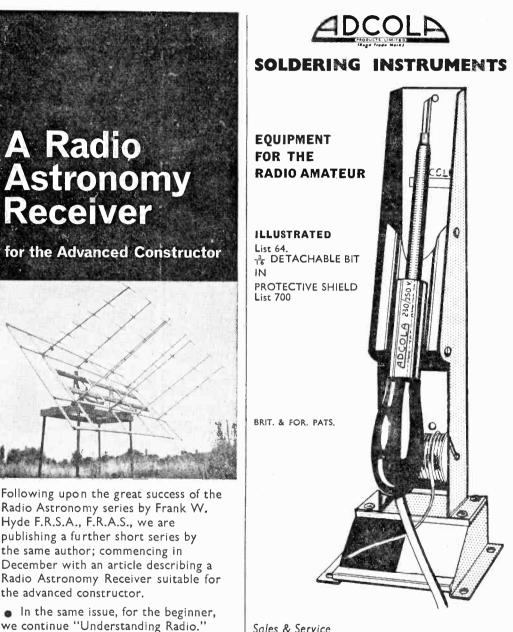
As mentioned earlier the unit can be used as a completely self-contained headphone receiver if required and in this case a phone outlet can be provided on the panel.

December, 1962



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PUBLISHED DECEMBER I, 1962, PRICE TWO SHILLINGS DATA PUBLICATIONS LTD., 57 MAIDA VALE.

LONDON W.9.

Central Control Amplifier

By E. McLoughlin

A MASTER CONTROL UNIT FOR AN AUDIO INSTALLATION

(Continued from page 630 of the November issue)

T must be stressed that voltages from the power supplies *must* be up to the full specified values. *Slight* deficiencies were found to produce immediate *huge* reductions in power in the prototype in both amplifiers, leading to inferior performance. If the H.T. is down by only 50V below specified value there is almost 40% power loss from the EL84. If the L.T. D.C. supply is down by only 1V at the points shown in the circuits, below the specified values, the available output power can be halved!

But do not use voltages in excess of those specified. Excesses (or deficiencies) can be cured to some extent by changing tappings on the mains transformer primaries (but watch the valve heater voltage!) or by altering the values of reservoir or smoothing capacitators or by using suitable droppers. The power unit *must* be trimmed to the specified voltages, using appropriate measures with the particular power supply components obtained. Rule-of-thumb methods using any old lash-up are here particularly likely to lead to such poor results as to make the whole unit rather disappointingly weak.

Inputs

The amplifier input is switched at will to "Laboratory" or "Line" by means of S4 (Fig. 2). In the position "Line" any signal on the line from apparatus at other stations can be fed into the amplifier and listened to in the laboratory/den on the internal loudspeaker in this unit provided that S3 is set to position "receive". In this position S3 breaks the mains feed to the L.T. power-pack on contacts A, breaks the base-drive on contacts B (so that the transistors are not damaged by receiving base-drive without emitter-collector voltage), breaks the connection of T5 to the line on contacts C (so that other signals are not fully or partially shorted, as explained above) and, finally, on contacts D, switches the incoming signals on the line through to R2 and R7 and hence to the amplifier input.

In the position "Laboratory" on S4 the amplifier input is connected to both of two sources within the laboratory simultaneously via the decoupling and impedance-transforming resistance network R3, 4, 5, 6. This network assures that both sources transfer virtually all of their signal voltage into the amplifier, but negligible amounts mutually to each other. Which of the sources actually feeds the amplifier then must be decided simply by switching the desired source on and the others off at their own switches. If both are on they will mix in the amplifier without otherwise interfering with each other.

Now, with S4 in the position "Laboratory", S3 may be at either position. The position "Receive" is then used as a "dummy" if the signal is merely to be listened to on the internal loudspeaker, confining it to the laboratory (e.g., when using the oscilloscope/signal tracer source for internal work in the laboratory—see below and possibly somebody else in the flat or house has other apparatus feeding other signals on to the rest of the line). Such other signals on the line will, of course, not then be actually received until S4 is also switched to "Line".

If the signals from a laboratory source (S4 at position "Laboratory") are now required to be sent on to the whole line—with suppression of any other signals possibly present—then S3 is switched over to "Send". This switches mains on for the L.T. power-pack and connects the transistor amplifier input and output appropriately, also shorting R2 to prevent any possibility of instability.

R2 to prevent any possibility of instability. The combination S3 at "Send" and S4 at "Linc" serves no useful purpose, neither does any damage nor causes instability.

The internal loudspeaker can be switched on or off independently. If S3 is at "Send" and all loudspeakers in the system are of the same type the volume on the internal loudspeaker is a true replica of the volume on any other loudspeaker on the line when the series-resistors used as individual local volume controls on the line loudspeakers are cut out of circuit (maximum volume).

Mains/Distribution/Power Supplies

The unit described in this article contains all its own power supplies, which are built in tier fashion on to one side panel of the cabinet body, details of which will be given later.

Fig. 1 (last month) gives details of the mains distribution wiring. This follows the principles and general scheme sketched in the initial general article. Great care is essential in carrying out this wiring, which should be checked, checked, and rechecked before switching on mains power. Wrong connections or insecure, untidy connections could lead to highly dangerous conditions or to destruction of valuable equipment.

Note carefully the arrangements for the mains isolation transformer. This item is generally too heavy and bulky and has too great a stray magnetic field for inclusion within the cabinet of the present unit. It is thus attached via a four-core mains power cable of suitable length and quality and mounted separately at a suitable safe position in a proper and secure manner. The reasons for requiring this transformer were fully discussed in the introductory article. Take great care not to confuse the connections; errors could lead to dangerous conditions.

Cabinet Construction

This unit is to be considered as a fixed item of electrical installation. As such it will most easily satisfy supply company regulations regarding mains wiring.

If the laboratory/workshop wall is of good dry wood at the location where the unit is to be installed, as was the case for the prototype, then the wall itself may be used directly as the rear of the cabinet, of which sides are formed by wooden slats screwed on internally with angle-iron. The distribution tags and cables can then be screwed directly on to the rear wall, according to the drawings, using appropriate regulation fixtures available in the electrical trade. It is advisable to consult an electrician at the start of the whole for their valves EF86 and EL84. Ample publication has occurred elsewhere, so that only brief comment on essentials is necessary here.

It is essential to mount the two valveholders such that R13 can be mounted as direct and short between the relevant pins as possible (Fig. 3). Furthermore, R10 must have its wire cut off very short and soldered direct on to pin 6 at the valveholder of V1. Failure to observe these conditions will cause treble-performance loss.

High gain is obtained in V1 by means of the unusually large anode load R10. D.C. coupling via the anti-parasitic R13 to V2 grid avoids one source of low-frequency phase-shift and losses. The positive D.C. thereby fed to V2 grid requires the unusually high cathode bias resistor R16 to

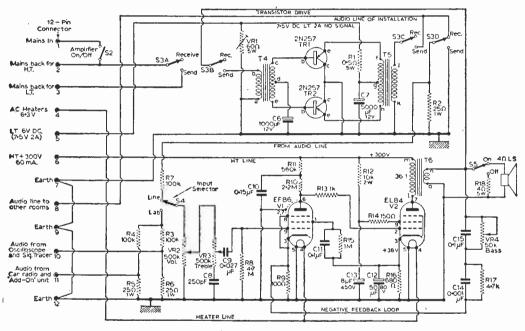


Fig. 2-The circuit of the "lid-unit".

project if one is not conversant with wiring regulations oneself.

The amplifier unit itself is seen, in the drawings and illustrations, to be built in more or less conventional form of construction on to a panel of wood forming the "lid" of the vertical cabinet. A good 12-pin connector, rated at 500V/2A on all pins relative to all other pins, is used to connect the "lid-unit" to the body. This enables rapid removal and replacement for servicing, especially if the take-off hinge and latch type of fixture is adopted.

The Amplifier

This is an excellent "hi-fi" circuit of low expense but fine performance specifically developed by Mullard engineers some time ago compensate. The value of R16 is critical and a close-tolerance resistor is specified. The cathode voltage resulting for V2 is then sufficient for the screen of V1. which is thus D.C.-coupled to V1 cathode. This also represents D.C.-negative-feedback, which stabilises the operating points of the valves—otherwise such a circuit would drift. C11 is also critical. Too low a capacity causes bass loss, whereas too high a capacity causes pure low-frequency phase-shift oscillation at some or all settings of VR4, especially if inadvertently too high a ratio is used for T6. This oscillation may be of such a pure note and frequency that it can be mistaken for severe mains hum.

If the amplifier howls uncontrollably at full power, whatever settings of the controls are undertaken, reverse connections to the output transformer primary, T6, m and 1.

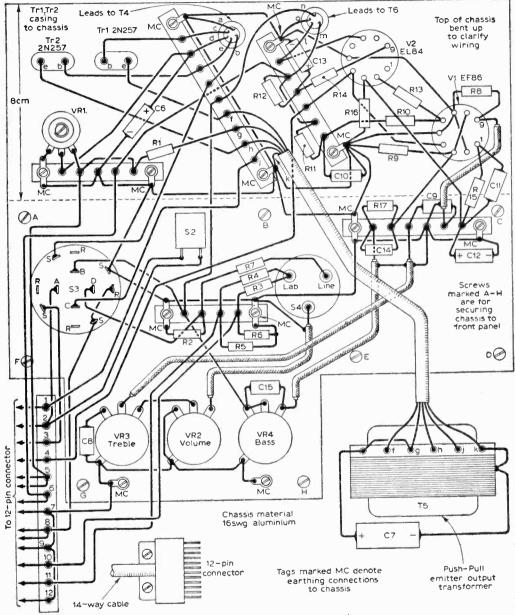


Fig. 3—The "lid-unit" and sub-chassis wiring diagram.

Use low-capacity coaxial cable for the leads shown screened in the wiring diagram, Fig. 3. to avoid treble loss. Note that all screens are bonded together and joined to chassis at only one point. This is highly important as hum is easily introduced if screens are earthed at several points because they can then carry random chassiscurrents, which may be partially A.C. Use suitable sleeving or other measures to prevent the screening from touching the chassis at unwanted points. Note in this connection also the separate earthbusbar for VR2, 3, 4. connected locally to chassis at the earth-feed from the 12-pin plug and not connected to the earth-ring-busbar under the amplifier components.

(To be continued)

December, 1962

DX on MEDIUM WAVES

As a change from shortwaves try for some M.W. broadcast band DX this season. This article tells you how.

By S. A. Money

ANY radio enthusiasts will probably be surprised to learn that DX signals from many parts of the world can be heard on the medium wave broadcast band. In the early 1930's many trans-Atlantic stations were heard on quite simple domestic radio sets. With modern receivers it is possible to achieve quite remarkable results despite the great rise in the level of interference since those early days.

During the past two years the writer and a number of other enthusiasts have listened for DX stations on this band. Many stations from both North and South America were regularly heard and others from the more remote parts of Africa and Asia were also logged.

Optimum conditions for long distance reception on the medium waves occur in the winter during the hours of darkness. In the evening reception of DX signals is extremely difficult due to the high level of interference from the very strong European signals. After midnight most of the European stations have closed down and reception of the weaker DX stations is possible. During the summer a high level of "static" noise makes DX reception more difficult and less frequent.

Sunspot activity is well known to have a considerable influence on short wave reception conditions. In the case of medium waves it has been found that the best conditions for DX reception occur during the years around the sunspot minimum. With the next sunspot minimum due to occur around 1963/64 conditions should be excellent for the next few years.

Receivers and Aerials

Under favourable conditions it should be possible to receive the regularly heard North American stations on any good domestic receiver provided that a good aerial system is used. For serious DX listening a communications

For serious DX listening a communications type receiver with its high sensitivity and selectivity is almost essential. Ex-Service receivers such as the R1155 have proved to be very good in this respect. Long wire aerials seem to be the best for DX reception. They should be mounted as high as possible and should be outdoors for the best results. Indoor aerials mounted in the loft or around the picture rail in an upstairs room can give very good results. In order to erect the necessary length of wire it may be necessary to bend it into the form of a square or rectangle. A wire 60 to 90ft long is suitable.

Ferrite rod aerials are not usually sensitive enough for DX reception. A good earth connection is usually needed with domestic radios and will often improve reception on a communications receiver.

North America

Reception from North America usually occurs for a period of from three to five days at a time every two or three weeks, in mid-winter however, the opening may last for as long as two weeks with the exception of one or two poor nights. On many nights there may be heavy "static" interference from thunderstorms over the Atlantic.

Generally reception is possible from just after midnight until about 5 a.m. when interference from local European stations starts to build up, although some trans-Atlantic stations can be heard as late as 7 a.m.

Programmes from North America are for local entertainment and are in English with the exception of a few French-speaking Canadian stations. Identification of stations is fairly easy since they all give their call-signs regularly, often during the breaks for "commercials".

East Coast, U.S.A.

Those stations located in the eastern coastal region of the U.S.A. are the most frequently heard here in Britain. There are no less than 16 radio stations in New York City and of these 14 were known to have been logged in England last winter.

Four of the stations in New York carry the major network programmes. The A.B.C. network broadcasts over station WABC on a frequency of 770kc/s. Further along the band on 880kc/s is WCBS, owned by the Columbia Broadcasting System. Both of these stations are regularly heard at excellent strength. Station WNBC (660kc/s), operated by the N.B.C. network, is not too well received here since its aerial is directed away from Europe. The fourth regularly heard station is WOR on 710kc/s run by R.K.O. and carrying the Mutual Network programme.

Of the independent stations in New York, WHN (1050kc/s), WINS (1010kc/s) and WNEW (1130kc/s) can be heard with very good signals on almost every opening to the U.S.A. These three stations broadcast popular music and newscasts. The New York equivalent to our Third Programme is provided by WQXR on 1560kc/s. Two stations frequently heard from New York State are WPTR (1540kc/s) at Albany and WKBW (1520kc/s) at Buffalo. Other stations which give good signals from the New England states are WTIC (1080kc/s) Hartford, Conn., WEGP (1390kc/s) Presque Is., Maine, WTOP (1500ks/s) Washington D.C. and WMEX (1510kc/s) at Boston, Mass.

Hill-billy music and songs heard on 1530kc/s will probably be from station WCKY at Cincinnati, Ohio. Pennsylvania state can usually be heard over stations WCAU (1210kc/s) at Philadelphia and KDKA (1020kc/s) at Pittsburgh.

Those stations in the southern states which are near the coast, such as WAVY (1250kc/s) at Portsmouth, Virginia, WBT (1110kc/s) Charlotte, N. Carolina, WCSC (1390kc/s) at Charlston, S. Carolina and WLCY (1380kc/s) at St. Petersburg, Florida, are frequently heard at good strength.

The state of Georgia can sometimes be heard over station WSB in Atlanta which operates on 750kc/s. Some of the other stations which have been logged from time to time are, WHAS at Louisville, Kentucky, on 840kc/s, WSM (650kc/s) at Nashville. Tennessee, and WALA (1410kc/s) at Mobile, Alabama. Most of these stations can be difficult to receive but, with improving band conditions, they should be more frequently logged this coming winter.

Central U.S.A.

What might be considered to be the cream of the DX signals from the United States are those stations located in the central and mid-western states. The nearest and thus most frequently noted stations are WOWO (1190kc/s) Fort Wayne, Ind., WJR (760kc/s) Detroit, Michigan and WCFL (1000kc/s) Chicago, Illinois. Station KXEL at Waterloo, Iowa can sometimes

Station KXEL at Waterloo, Iowa can sometimes be heard through WPTR's signal on 1540kc/s and usually peaks up at around 0300 GMT. Another station which is often noted at about this time is KMOX at St. Louis, Missouri operating on 1120kc/s.

Texan stations which have been frequently logged here in Britain are WFAA at Dallas and WOAI at San Antonio using frequencies of 820kc/s and 1200kc/s respectively. Perhaps the most distant U.S. stations noted recently are WCCO (830kc/s) at Minneapolis, Minnesota and KOMA (1520kc/s) at Oklahoma City, Oklahoma.

Reception of these more distant stations does require quite a bit of patience since they are usually weak signals and are often only audible for five to ten minutes at a time.

Canada

The Canadian Broadcasting Corporation, which runs the main network, is a public body similar to the BBC. Station CBA at Sackville, New Brunswick (1070kc/s) is the most consistent of the CBC stations heard in this country. CBA can usually be heard at excellent strength just before midnight whenever the band is open to North America and is useful as an indicator of band conditions.

Other CBC stations which are often heard in England are CBC Montreal (940kc/s), CBI Sydney. N.S. (1140kc/s) and CBE Windsor, Ontario, on 1550kc/s.

Of the independent stations CJON (930kc/s) at St. John's, Newfoundland is usually an excellent signal from midnight and like CBA can be used to indicate the state of the band. Other Canadian stations which usually give good reception are CHNS (960kc/s) Halifax, N.S., CFNB (550kc/s) Fredericton, N.B. and CFCY (630kc/s) Charlottetown, Prince Edward Island.

Generally Canadian signals are not as frequently heard as those from the U.S.A. but reception will normally occur on the same nights as for the U.S.A.

South America

Most of the South American stations broadcast in either Spanish or Portuguese and can usually be heard on any night when the North American stations are not audible. Brazilian stations are the most frequently heard with programmes in the Portuguese language. Radio Globo on 1180kc/s, R. Tupi on 1280kc/s and R. Jornal on 780kc/s are three stations which are usually excellent signals.

Other countries which are frequently logged are Argentina (*Radio Nacional*, 870kc/s), Venezuela (*R. Ondas del Lago* on 1120kc/s) and Uruguay with stations CX6 (650kc/s) and CX14 (810kc/s).

Programmes in English can be heard from *Radio* Demarara (ZFY 760kc/s) in Georgetown British Guiana, which usually gives fair to good reception in the early morning.

Central American stations have been heard from Mexico, Cuba, Jamaica and Trinidad. Generally reception from this area is limited to a short period when the conditions change from the North American area to South America.

For details of these and other South American stations the reader is referred to the *World Radio Handbook* which lists the frequencies, operating times and addresses of nearly every broadcast station in the world.

Asia and Africa

North African stations can usually be heard during the evenings in the winter months and are often stronger signals than the more local European stations.

South Africa has been heard in the early mornings on frequencies of 1268kc/s and 1286kc/s. Other countries logged from Africa have been Kenya, Somalia, Nigeria and Senegal.

Middle East countries such as Syria, Iraq and Iran are best heard during the period of the feast of Ramadan when they operate all night with programmes in Arabic.

Indian, Pakistani and Chinese stations have been heard just after midnight with programmes in their native languages.

The Voice of America stations at Okinawa and in the Philippines Islands have been heard in the afternoon on 1140kc/s and 1180kc/s. Reports have been received of the reception in Scotland of stations from the Pacific islands such as Guam and Fiji but so far nothing has been heard from that area by listeners in England.

area by listeners in England. The BBC have however, received reports of reception of their Home Service stations in New Zealand so it would seem that reception of Pacific stations in England should be possible if conditions improve as expected.



Electronic Organ Keying

VINCE there are now very many different makes of American electronic organs available in this country, a study of some of the tech**niques** involved is very interesting, and although no all-transistor instruments appear to have arrived there are many interesting features to be seen which have hitherto not been used in any English designs.

One of the sections which has always interested me is that concerned with the keying of the instrument, not only from the electrical, but from the actual mechanical point of view. As most of my readers know, the depression of a key actuates some form of electrical contact; in its simplest form two metallic points being brought into contact, or opened, and in its most complicated form, 10 or more contacts being operated, all being opened or closed, or various combinations of them being operated.

Many organs suffer from defects in this part of the instrument, the contacts being very prone to oxidisation or the action of dust or fluff, and it is interesting to note the various methods of overcoming these defects.

The use of mixed metals for the contacts, or the introduction of some form of wiping or slight scraping action are well known, but the most interesting is, I think, that employed by the Baldwin Company, where a printed circuit resistance element is so arranged that when a key is operated a spring strip is lowered and travels across the resistance element, thereby gradually cutting it out of circuit.

In addition to getting rid of the difficulties of dirt, corrosion, etc., this also gives a gradual attack effect, and results in the note being sounded in a similar manner to a standard pipe instrument, but I still feel that there are better ways of doing the job.

Again, I wonder if any of my readers have spent any time on this aspect and have any ideas of their own they would like to air. Incidentally, the use of the scheme mentioned above does not restrict the instrument to sounding a single note, as the resistance elements can be stacked and practically any number can be operated by a single

Of course, the difficulties of suggesting or designing a keying system are restricted, as keys may be of two types, balanced or rear-hung, and thus the contact mechanism must be in the front of the instrument or at the rear, and may present difficulties in accommodating the mechanism.

A Salvage Tip

I know that many of my readers are interested in hints and tips such as are accumulated by the keen serviceman, and I am always anxious to pass on anything which is really worth while. I was recently shown a tip which, although originally used to salvage a valve, is also applicable to transistors. Here it is.

In the case of the valve it relates to the older type with a top cap, which often becomes loose and eventually pulls away leaving the merest piece of wire projecting from the glass. In the case of the transistor, a wire may break and leave a similar short stub of wire projecting. In both cases, the application of a soldering iron being impracticable.

The hint is to obtain a two or three inch length of suitable replacement wire, and to tin one end and then carefully to add solder to this end, holding it end downwards so that a fairly large "blob" of solder is formed.

Now hold the piece of wire at its opposite end in a pair of pliers and lower the "blob" end until it nearly touches the protruding end of the wire you are repairing. Place the soldering iron on the wire being held, at a point midway between the pliers and the solder and as soon as the solder is seen to begin to run, lower it so that it touches the protruding end, and then quickly remove the soldering iron.

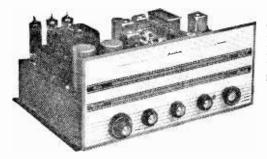
Provided that you can keep everything steady the two ends will unite, and the soldering iron will carry off the extra heat so that no damage will arise. You need a very steady hand, however, and will soon see how much solder to leave at the "blob".







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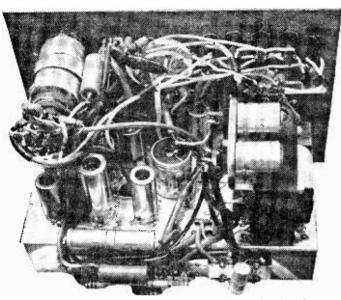
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THE AUDITRON (This instrument was previously known as the MINISCOPE-see footnote)



(Continued from page 599 of the November issue)

MILLER-TRANSITRON oscillator is a special form of multivibrator, in which, loosely speaking, the grid and anode function as one triode and the screen and suppressor as the other triode. The fact that both "triodes" are in one electron-path gives the new characteristics.

The action of one cycle is as follows, starting at the end of a timebase-run. This is reached when the grid voltage has risen to that value for which anode current ceases to show further rise, a condition known as pentode bottoming. (This has

nothing to do with anode current saturation.) All increase of total *cathode* current then resulting from further rise of the grid voltage (on the charging-curve of the capacitor selected on S5b, via VR9, etc.) is therefore suddenly diverted to the screen-grid at this point, which therefore suffers a sudden rise in current, i.e. fall in voltage. This sudden fall in voltage, at the end of the linear anode run-down, shown in the second lines of waveforms in Figs. 6 and 7 (last month), and shaped in V7 to blank out the flyback as already mentioned, is coupled to the suppressor grid via the capacitor selected on S5a, and thus reduces anode current.

But this reduction of anode current causes a rise of anode voltage, which is fed as a further sharp rise to the grid, via the capacitors on S5b, causing

By M. L. Michaelis, M.A.

further cumulative transfer of current from anode to screen. The final result of this very rapid cumulative process is to cut off anode-current completely at the suppressor grid, and send the screen-current to saturation. The screen-current to saturation. anode voltage then returns to H.T. as the capacitor selected on S5b charges via VR10 and grid-current in V6.

Being exponential, however, this process would take, theoretically, infinite time to go to full completion. But in the practical circuit used, it soon reaches the voltage on C18, this being less than H.T., and D5 arrests the process there, the flyback proper being therewith complete.

Conditions then remain stable as long as the negative blocking anode current at the suppressorgrid remains, i.e. as long as the capacitor selected on S5a is still charging through the combination R40, S6, R41. As soon as this charging process has progressed so far that the voltage drop across

R40/R41 has become less than the suppressorgrid-base, a tiny bit of anode current can flow. This causes a few volts drop at the anode, immediately, which are of the order of the normal grid-base of the valve and are fed to the grid via the capacitor selected on S5b.

The result is that all cathode-current is immediately almost cut off, giving a sharp rise of screen voltage, fed as a similar sharp rise to the supressor, so that the valve is now fully "open" again for any further anode current that wants to flow.

But the anode current at first remains at the very low value giving a drop across VR10 no larger than the grid-base, because any further increase would cause a drop across VR10, fed to the grid via the capacitors on S5b, large enough to cut the valve off, i.e. such increase could not take place. At any rate, it can only take place slowly at a rate such that the charge on the capacitors on S5b,

THE "MINISCOPE"

The General Electric Company Ltd. have drawn our attention to the fact that the name "Miniscope" is a registered G.E.C. trade mark. In view of this we have changed the name of our instrument to "The Auditron". We apologise to G.E.C. for the unwitting infringement of their trade mark.

charging through VR9, R35, etc. can follow, thereby avoiding the checking-feedback at the grid.

This gives the relatively slow and very linear rise of anode current, and consequent fall of anode voltage, used for the timebase-sweep of the spot on the CRT. This terminates when the anode current has increased with slowly rising grid voltages up to the point where further rise of grid voltage has no further effect on *anode* current (bottoming), and we are back where we started.

Current is suddenly diverted to the screen, resulting in total cut-off of anode-current at the suppressor, the flyback takes place, is "caught" by D5, waits until anode current cuts on again at the suppressor, the value is almost cut off at the grid suddenly, a new linear timebase-run takes place, and another cycle is then complete, and so on repeatedly.

Speed-Influencing Elements

It is clear that each cycle consists primarily of two portions, as in any multivibrator, associated with independent CR-time constants, which may be influenced independently.

Thus we have *here* firstly the linear timebase run, determined by the time constant given by VR9 and R35 together with the selected capacitor on S5b, and secondly the anode-current cut-off time. determined by the time constant set by R40/ R41/S6 together with the capacitor selected on S5a.

Each time-constant can, in principle, be controlled fully independently from the other, but a *purposeful* ganging is in practice desirable, and has been adopted.

Ganging of Time Controls

S5 constitutes the ganged coarse speed-control for the timebase. This is a three-position switch selecting capacitors of equal values for both timeconstants simultaneously, in steps of 10:1 in capacity, and thus 10:1 in speed-ratio. VR9 is the timebase-run fine-speed control.

It has no effect on the anode current cut-off period including the flyback, but as a continuously —variable range of 20:1 for the timebase—run speed, because R35 has one twentieth the resistance of the full track of VR9. This gives sufficient overlap of all ranges for all purposes.

It is *not* the flyback-time, which determines the time from the end of one timebase-run until the circuit commences the next run, but rather the time for which the capacitors on S5a and R40 (and R41, if in circuit) hold the anode blocked at the suppressor. If the latter is shorter than the true flyback, the new run starts before D5 operates, resulting in decreased amplitude of the sawtooth and higher overall frequency. If the suppressor cut-off time is much longer than the true flyback, the anode simply waits resting at C18-potential until the suppressor is ready again (Figs. 6 and 7 respectively).

These two conditions can be selected by means of S6. In the position "short" for S6, only R40 is in circuit for the "recover" time constant, so chosen as to match the flyback proper, i.e. when the flyback has reached the C18/D5 catching-level, the suppressor is then just ready for the next run too.

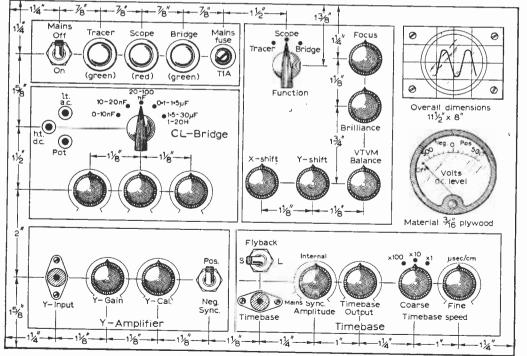


Fig. 8—The layout of the front panel.

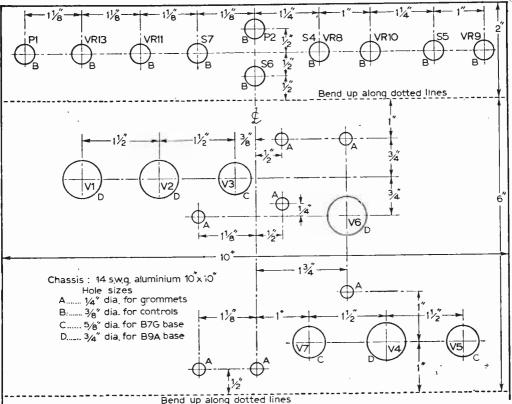


Fig. 9—The main chassis drilling.

In fact, the given value of $47k\Omega$ for R40 is such that the suppressor is ready a little sooner than the flyback would be caught by D5, i.e. D5 never operates in the "short" setting of S6, and the timebase consequently runs at slightly reduced amplitude, with the advantage of the higher overall frequency.

However, constructors can trim R40 as they wish, using a $100 \,\mathrm{k\Omega}$ preset potentiometer here, and adjusting it to the point where further reduction of resistance causes the length of the horizontal trace on the CRT *just* to begin to decrease. This is then the true matched condition, where D5 just starts to operate, i.e. flyback is just complete, when the suppressor gives the anode free for the next run, without any waiting time. Fig. 7 shows this condition. A new run starts *immediately* the flyback from the previous one is over, without any delay.

any delay. Switching S6 to "long" increases the "recovery" time-constant by a factor of about ten, so that now flyback is over long before the suppressor is ready for the next run, giving considerable waiting times seen in Fig. 6. The advantage of this form of operation is apparent when desiring to display very asymmetric signal waveforms, where the portion of interest is only a fraction of a cycle.

It is seen that, in the "long" setting, increasingly towards the faster end of the range of VR9, the actual timebase run (which is all that is displayed, across the *whole* CRT screen) is only a fraction of each cycle of the timebase oscillation, yet it is the latter which is locked to the signal frequency by means of the synchronisation. Consequently a stationary display of a magnified

Consequently a stationary display of a magnified version of the interesting portion of the asymmetric signal is possible, selected by suitable setting of polarity on the synchronisation switch on the signal amplifier. This arrangement gives similar effects to "triggering", though of course not successful in all cases of asymmetric signals, whereas true triggering is always successful.

Triggering

An oscilloscope may be operated, basically, in two modes: "sync" in which the timebase is allowed to oscillate, the sync signal merely forcing the frequency into step with the signal frequency, and "trigger" in which the timebase is never allowed to oscillate, but is "kicked" into singleresponses.

Trigger operation frees one of the need to have the timebase run slowly enough to have at least one cycle of the signal frequency included in the timebase frequency period, which is the basic condition for "sync".

However, triggering is of far less importance for audio work than for TV or pulse work, and so sync facilities only have been provided in the Auditron. The sync facilities incorporated, together with the "long/short" function, will satisfy all normal needs of the radio and audio experimenter.

Synchronisation

The Miller-Transitron timebase is synchronised by setting VR9 such that the overall frequency is somewhat lower than the signal frequency, when left to run uncontrolled. The positive pulses, in step with the signal frequency, amplified and shaped by V4 and V5, then jerk the suppressor to cut-on just that little sooner to bring the two frequencies into step.

The gain of V4 and the arrangements for extracting a sync signal from the signal amplifier are such that good strong sync is possible for all signals having at least 10% of the screen-size vertical amplitude, at all frequencies of operation for which the instrument is intended.

VR8 serves as gain-control for the sync signal, to control the strength of the effect with stronger signals, or to remove all sync if desired. VR8 carries a D.P. switch. S4, which switches over to 50c/s mains sync (for frequency-comparisons against the mains) if turned beyond the point of "no sync". The mains-sync & ig n a l is obtained from the heater-line via R23 and R24.

Calibrations for the Timebase

A special feature of the Auditron is that the conventional calibration of the timebase controls in terms of basic frequency has been abandoned in favour of a "time per centimeter" of CRT-screen display calibration, which is vastly more useful. A frequency-calibration is relatively useless, as the flyback and wait times are indefinite fractions of a timebase cycle, and thus even if exact number of cycles of the signal appear stationary in the display, the interpretation in terms of signal-frequency is very often rather ambiguous, because it is not clear how much is located on the invisible flyback.

The "time-per-centimeter", in conjunction with a centimeter-grid of lines on the perspex window in front of the CRT, represents a form of calibraevery ambiguity. S6 tion. removing has no effect whatsoever on the speed of the timebase run, which is controlled solely by VR9 and S5b. Fully unambiguous calibration of VR9 from 12 to 250micro-seconds per centimeter was thus possible in the prototype, with the three positions of S5 labelled approximately X1, X10, X100. Thus all times from 12 microseconds to 25 milliseconds per centimeter are covered. This enables time measurements to be read off direct, and frequency measurements to be made as follows.

The signal waveform is syncronised stationary, and the length of one cycle read off against the centimeter lines on the perspex window in front of the CRT, which is then multiplied by the timeper-centimeter readings on the timebase-controls. The result is the time for one cycle of the signal waveform, whose reciprocal gives the frequency.

It might be asked why here a once-and-for-all direct calibration of the timebase controls has been adopted, whereas for the signal voltage calibration an independent Zener-standard calibrator was used instead of direct calibration of the Y-gain control. The reason is that in the timebase our time-determining elements are largely the capacitors C22 to C27, and valve-ageing or voltage fluctuations can act only on the single stage V6, resulting in no drifts greater than tolerable for normal workshop standards of accuracy.

The Flyback-Blanking Circuit

In order to black-out the flyback of the spot on the CRT-screen we need to cut-off the CRT at its grid during all times except the linear timebaserun used for the display. This requires an

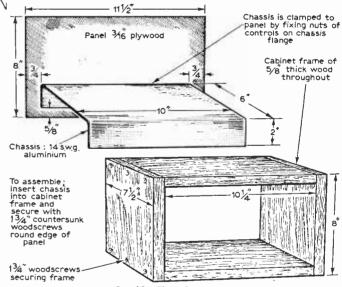


Fig. 10-The cabinet details.

accurately-timed squarewave, whose negative portion coincides with the "flyback and wait" portion of the timebase cycle, and whose positive portion coincides with the linear timebase run.

In order to perform the blanking function properly, this must be as good a squarewave as possible. Furthermore, the D.C. level of this squarewave must be such that the positive part of the wave is coincident with the voltage set on the manual brilliance control, and the negative part goes negative to this level by an amount equal to the amplitude of the wave, the latter needing to be sufficient to cut the CRT off, even for the brightest setting of the manual brilliance control. In other words, the amplitude of the squarewave must be just a little more than the grid-base of the CRT, and 30V was thus found to be satisfactory. The circuitry round V7, with associated diodes

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D6, D7, D4, was devised to meet all these requirements to within sufficient limits of accuracy for all normal amateur purposes.

Shaping of the V6-screen Waveform

Figs. 6 and 7 show that the screen-grid waveform of V6 is already of the required form, very roughly, for the flyback-blanking function. Thus the screen goes negative during the flyback and wait time, because anode-current is then cut-off and heavy current diverted to the screen. During the timebase run, the screen is much more positive, because anode-current is flowing, and thus screen current is low or normal.

Yet the original screen waveform is anything but a good squarewave. At the fastest settings of VR9 the positive-going transition takes about the same time as the timebase run, so that at least half the trace on the CRT would still be dark, and the other half would increase progressivly in brightness, were this waveform used directly to bias the CRT grid.

At the slowest settings of VR9 the screen wave rises fairly soon to a maximum positive, and then gradually falls as the anode and screen draw increasing current during progression of the timebase-run. This wave, if applied to the CRT grid,

would have the undesirable result of giving a trace which starts dark, rises fairly soon to maximum intensity, and then gradually tails off in intensity towards the end.

However, looking at this screengrid waveform of V6, it is apparent that both positive and negative transitions commence with steep portions having at least the desired final amplitude of 30V, and pretty accurately coincident, in time, with the start and end of the timebase run. It is thus the purpose of V7, D6, D7, D4 to cut out this portion of the wave, and reject all else.

The D.C.-level of the screen waveform shifts with the setting of VR9, on account of the symmetry-changes there by involved. It is therefore necessary to clamp the wave to a definite potential prior to introduction of clippers at the desired relative D.C. levels. The combination of C21, D6, R42 performs this function, clamping the wave to -18V (derived from the Y-amplifier bias circuit) as its most negative limit under all circumstances. R31

merely serves the purpose of reducing loading thereby imposed at the screen-grid of V6, which would otherwise react back to distort the timebase action. The function of such a clamp-circuit is identical to a peak-rectifier circuit.

The output waveform at V7 cathode is now clamped at chassis potential and is positive-going from there. All that is needed is to retain the first 30V, and chop off the rest, which is performed by the simple diode-limiter circuit D7, which is returned to the desired potential of plus 30V on R36, C19, D7 and C19 thus short-out all portions of the waveform lying above plus 30V.

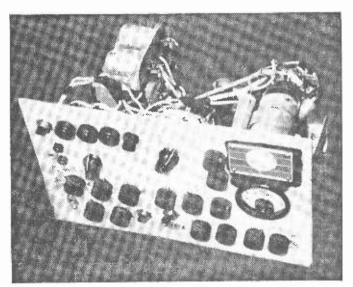
We are now left with the desired waveform for flyback blanking. It is merely necessary, as a final step, to give this the desired D.C. level, i.e., to change over from positive-going-to-chassis to negative-going-to-brilliance-control-setting.

This is performed by another clamp-circuit, whose principles of operation are identical to those of the first. A coupling-capacitor C29 first of all removes all D.C., D4 is a negative peak rectifier, and the series-added D.C. is whatever voltage is present at the slider of VR1, the brilliance-control. R37 and C30 were introduced as an equaliser, to make the action of this clamp circuit slightly frequency-selective, speeding it up at the higher frequencies of operation to compensate for slight delays in rise of the original wave there.

The specified value of C30 should be found satisfactory, but if the trace on the CRT is found not to have a clean sharp start at the highest possible timebase-speed setting, *slightly* larger values should be tried.

Diodes

Although silicon diodes are less critical than germanium diodes, heat shunts should nevertheless be used when soldering these diodes. If diodes are unwittingly damaged during soldering,



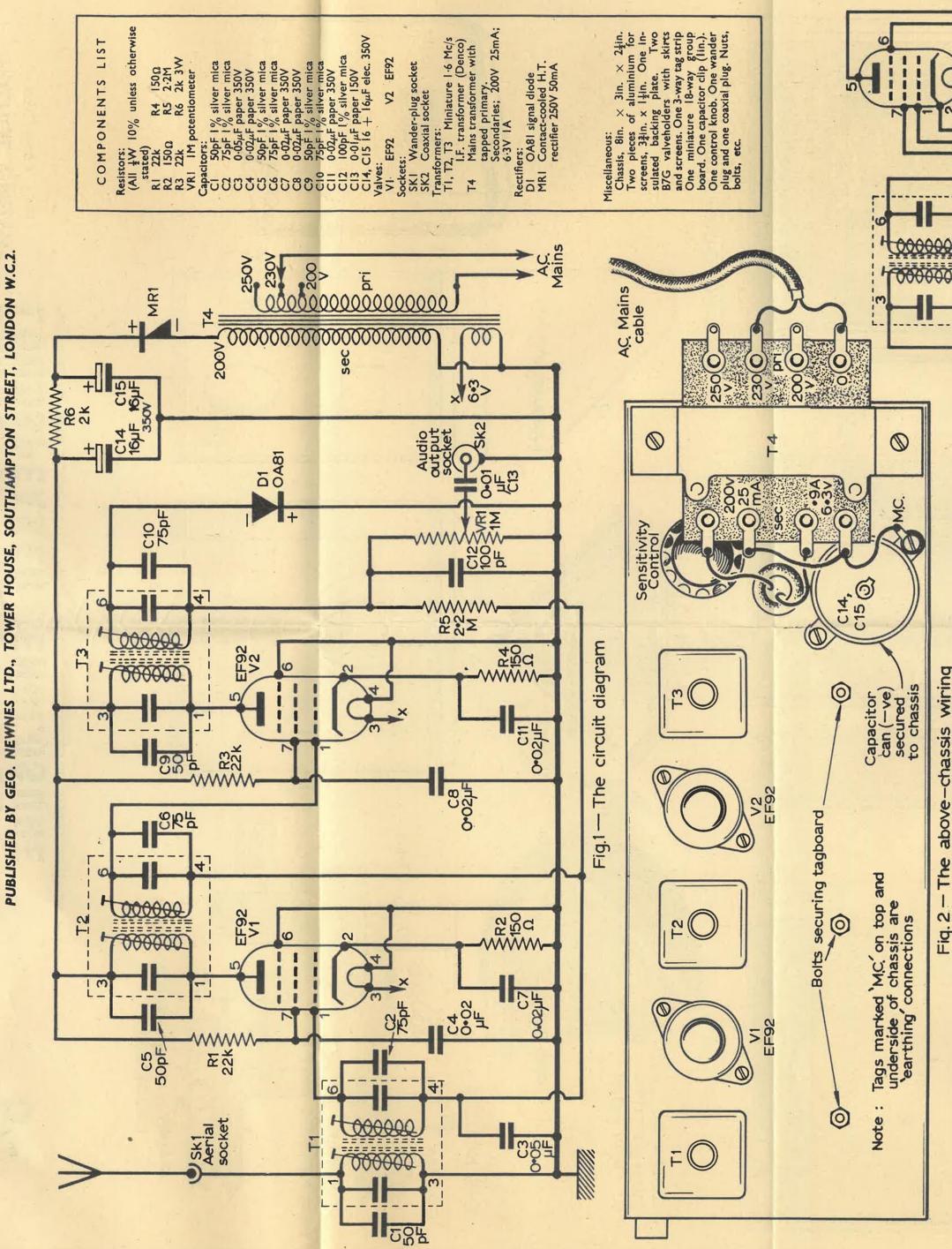
The Miniscope as it appears in an advanced stage of construction.

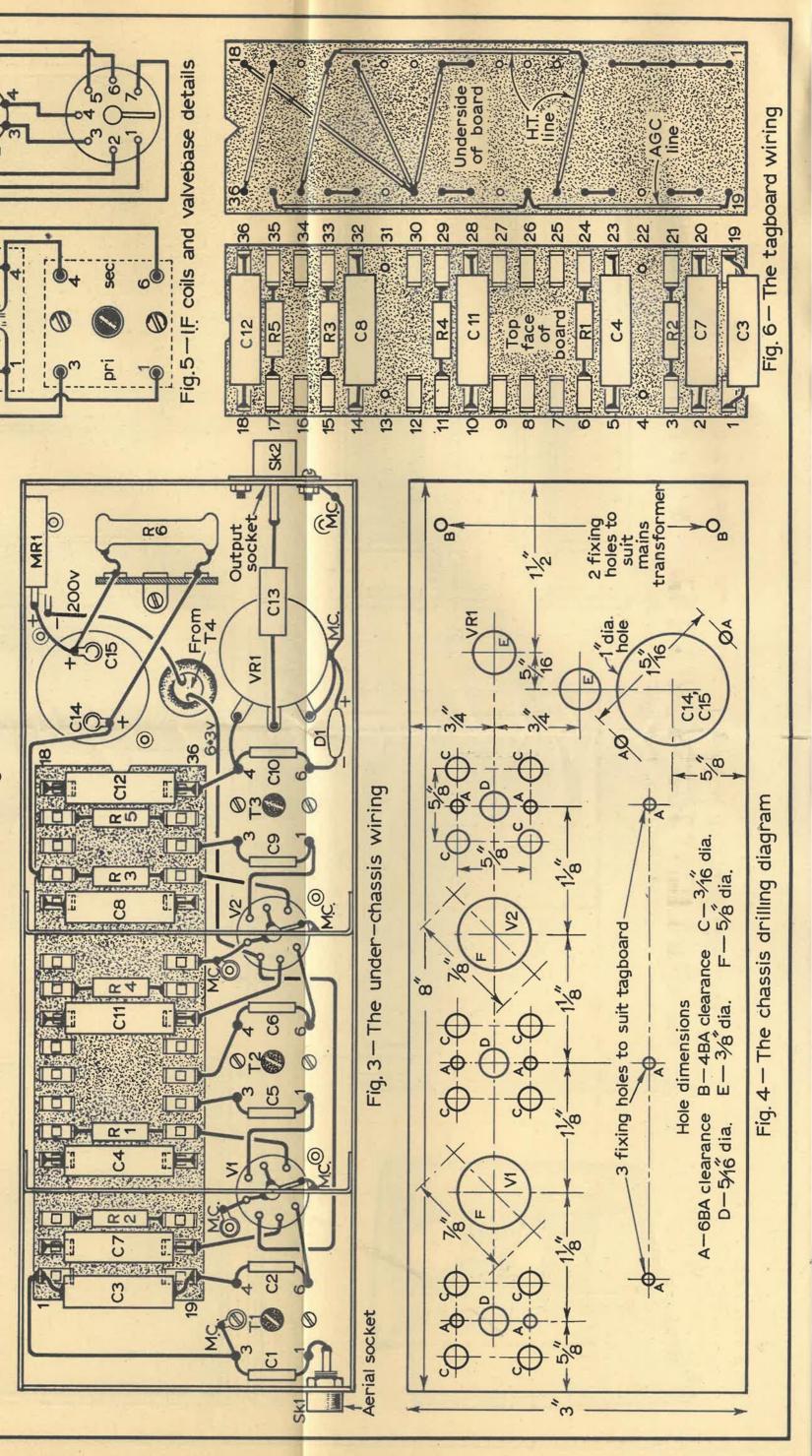
this circuit can give a variety of forms of erratic performance. Take care, also, to wire all diodes with the correct specified polarity. It is *NOT* permissible to use normal germanium diodes of the RF or low-voltage types *anywhere* in the Auditron, as the voltage ratings of such are far too low, and they would suffer immediate destruction. The peak inverse voltages appearing on the diodes in the Auditron amount to some one or two hundred volts in some cases, and thus the single type number specified throughout is a silicon diode of 350V peak inverse voltage rating.

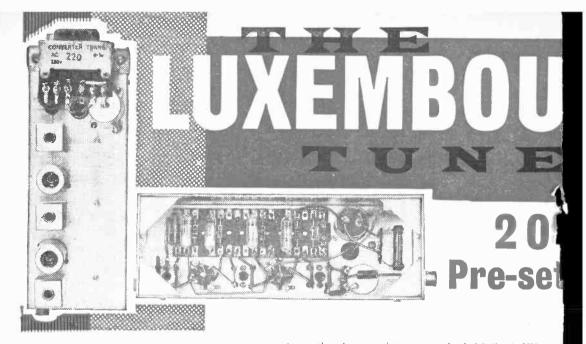
(To be continued)

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WOWADAYS most people have an F.M. tuner to give them high quality interference-free reception from their local BBC stations but there are numerous occasions when the programmes transmitted are not of the more popular light music type and an alternative is required.

Without doubt the most popular station for light entertainment particularly among the younger generation is Radio Luxembourg on 208m.

In order to receive this station it would normally be necessary to have a complete medium wave tuner but this novel design shows how a high gain and selective tuner pre-set to the Luxembourg frequency can quite easily be constructed.

The Design

The original idea for the circuit came from experiments carried out with a 1.6Mc/s I.F. amplifier strip when it was found that by adding a small fixed capacitor to each winding of the I.F. transformers it was quite simple to bring the tuning point down from 1.6Mc/s to 1.439Mc/s which is the exact frequency for Radio Luxembourg.

As miniature 1.6Mc/s I.F. transformers are available from all the component shops they provide a ready made perfectly screened band-pass coil unit adjusted for optimum coupling which can be easily tuned to 208m.

The circuit which is shown in Fig. 1 on the Blueprint is quite simple but has proved to be very sensitive and yet perfectly stable over long periods. It consists of two straightforward R.F. amplifiers followed by a germanium diode which provides detection and negative bias for non-delayed AVC. In practice the use of a miniature group-board to mount all the small components makes it both very easy to construct and at the same time gives the tuner a neat professional appearance.

It will be noticed that no audio amplifying stage has been included as it was found that feeding trom the detector into a standard Mullard 3W amplifier sufficient signal was always available to overload the input and in fact a preset output control was included, which is normally set at about the halfway position. Good reception has been obtained with this tuner in various locations in and around London and also in parts of South East England using only 4ft of wire as an aerial, however in view of the characteristic fading that does occur from time to time on Luxembourg it is considered that the best aerial possible should always be used.

When the first prototype was completed a considerable amount of experiment was carried out with various different input circuits from the aerial including winding small coupling coils on to the first I.F. transformer to give a step-up ratio but the difference in results was so slight that it was not considered worth the additional time and trouble.

As a precaution against the possibility of some instability due to the high gain with two R.F. stages small screens were fitted across the centre of each valveholder but it would appear that these are not absolutely essential and some constructors may prefer to build on a try-it-and-see basis and only fit them afterwards if needed. The position occupied by the screens is shown dotted in the under chassis wiring diagram Fig. 3 but it should be noted that they were removed for the photograph (at the top of this page) in order to provide a clearer view of the wiring and components.

Construction

The chassis used was an aluminium type with reinforced corners and it measured 8in. x 3in, x $2\frac{1}{2}in$. Actually a chassis having a depth of only Iin, would have been sufficient but the deeper one was chosen as it appeared to be a standard ready made component that was stocked by most of the well-known component shops.

There is comparatively little metal work or drilling to be carried out as will be seen from the chassis drilling diagram Fig. 4. To simplify the

3 m Tuner

marking out of the I.F. transformers a small paper template should be used and if desired this can be lightly stuck on to the chassis before drilling.

Having drilled all the holes in the chassis the various components can be fitted into position according to the diagrams Fig. 2 and Fig. 3 but care should be taken to ensure that the valveholders are the correct way round. This also applies to the I.F. transformers and these can be checked quite easily by reference to the small numbers moulded on the base of the formers, 1 and 3 being primary and 4 and 6 the secondary.

Component Group-board

The secret of the clean layout and the easy assembly lies in the 18-way miniature group-board which takes practically all the small components, and by wiring up the various tags on the back first the majority of the work can be done before this item is fitted into the chassis.

The two views of this group-board given provide all the necessary information for carrying out the wiring, but in view of the ease with which it is possible to become confused when constantly turning this component over while working it is strongly advised to positively mark one end with a dab of paint or a small "V" notch as shown. It is recommended that all the wires on the rear of the group-board should either be PVC insulated or covered with 1mm sleeving to avoid the possibility of short circuits.

It is also essential that an insulated backing plate should be fitted between the group-board and the chassis or if preferred it can be mounted just clear of the chassis by two spacing nuts. It will be noted that the two pairs of tags in positions 4 and 13 have been removed and this was done to allow the screens across the valveholders if fitted to be taken close to the chassis.

Power Supply

No mains on/off switch has been included as it was thought that in most cases this unit would

By S. Collins

probably be controlled from the main amplifier, but this is a matter of personal requirements.

The mains side consists of a conventional double wound transformer T4 of the type used in most Band III convertors giving 200V half-wave H.T. and 6.3V for the heaters; this type of transformer also effectively isolates the chassis from mains to ensure complete safety. The H.T. is rectified by means of the usual contact-cooled rectifier MR1 which must be fixed to the chassis so that the smooth side makes good contact all over for cooling.

One side of the H.T. winding on the transformer goes to chassis together with one side of the 6-3V winding. The other side of the H.T. winding then goes to the tag on the rectifier marked – ve while the +ve tag is taken to the 16μ F reservoir capacitor and through to the H.T. positive line.

Having completed the actual construction and wiring and carefully checked each part in turn against the diagrams the unit should be connected to the mains and switched on. If a testmeter is available it is a good idea to check at the various valve pins to make sure that there is H.T. on the screens and anodes (pins 5 and 7), and also a small positive on the cathodes (pin 2).

Setting Up

The output socket SK2 should now be connected to an amplifier input and the controls turned to near maximum to start with. If a signal generator is available then the adjustment is very simple and routine.

First of all set the signal generator to about 1440kc/s and feed the modulated signal into pin 1 of V2, then adjust the cores of T3 for maximum sound from the loudspeaker. Now transfer the generator to pin 1 of V1 and adjust both cores of T2 for maximum signal and then connect the signal generator to the aerial socket and finally adjust T1 cores for the best output.

This will bring the tuner fairly close to the Luxembourg programme and if desired a short aerial can be fitted and the final adjustment carried out on the actual transmission. A better way if (Continued on page 749)

An AUDIO ABSORPTION WATTMETER

By K. BERRY

HIS wattmeter was developed to enable the power output of audio amplifiers to be measured. It is suitable for use with amplifiers having output impedances of 3 or 15Ω , and will measure powers of between 1 and 20 watts. A feature of this design is the fact that the meter has a nearlinear scale as opposed to the more usual "squarelaw" scale associated with instruments of this type.

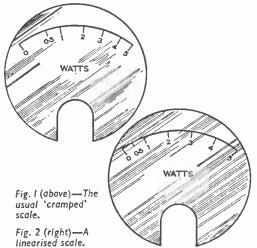
Theory

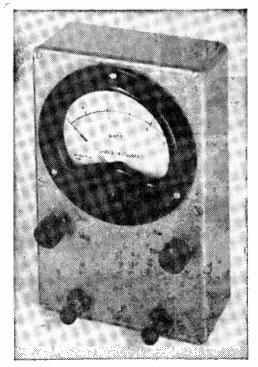
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The power dissipated in a resistor is given by the expression $P = \frac{V^2}{R}$ watts, where R is the value

of the resistor in ohms, and V is the voltage developed across it in volts. Thus if it is desired to measure the output power of an amplifier, a resistor, whose value is the same as the output impedance of the amplifier, should be connected to the output terminals of the amplifier and an A.C. voltmeter connected across it to measure the voltage developed. The power dissipated in the resistor can then be calculated. If, however, the meter was so calibrated, then the power developed could be read off directly thus obviating the need for calculations. This is the basis of the absorption wattmeter.

If the voltmeter used has a linear scale, the power calibration tends to be cramped at the "top" end of the scale as shown in Fig. 1. In this design, the voltage applied to the rectifier bridge which feeds a moving coil meter has been





The finished instrument.

deliberately kept as small as possible. Consequently the diodes are being worked over the nonlinear portion of their characteristics and since this approximates to a "square law" curve this largely cancels the cramping effect normally found at the top end of the scale as can be seen by comparing the scale in Fig. 2 with that in Fig. 1.

Circuit Description

The circuit diagram of the wattmeter is given in Fig. 3. The appropriate load resistor, 3Ω or 15Ω , is chosen by SW1A. The voltage developed across the load resistor is applied to one of four potentiometer networks, the required network being selected when the impedance and power range switches are set. The output from the selected potentiometer network is fed to the bridge rectifier, Mr1-4, and thence to the meter M1. A

Spe	ecification
Impedance	3Ω or 15Ω
Power range	5 watts or 20 watts
Frequency response	\pm 0.5 dB 10 c/s = 100 kc/s

 250Ω rheostat VR5 is connected in series with the meter. This has been included to enable an adjustment to be made to the linearity of the scale since this will vary slightly depending on the exact type of diodes used in the rectifier bridge.

The use of four separate potentiometer net-

-		•
	1	У

			Imped	lance			
3Ω				15Ω			
Voltage	Power	Voltage	Power	Voltage	Power	Voltage	Power
3.87	5	7.75	20	8.66	5	17.32	20
3.46	4	6.93	16	7.75	4	15.5	16
3	3	6	12	6.7	3	13.42	12
2.45	2	4.9	8	5.5	2	10.95	8
1.73	1	3.46	4	, 3.87	1	7.75	4
1.23	0.5	2.45	2	2.74	0.5	5.5	2

Table I

works instead of the more usual series (multiplier) resistors is explained by the necessity to keep the resistance in series with the bridge, low, and comparable. on all ranges. This results in a common calibration for all ranges.

Components and Construction

The choice of components is quite straightforward. The load resistors, R1 and R2, must, of course, have an ample power rating, but the use of 20W resistors is, perhaps, not essential. Provided the meter is not used to absorb a continuous 20W, there is no reason why, say, 10W resistors should not be used. The 3 Ω board is made up of 3.3Ω and 47Ω resistors in parallel (=3.06 Ω). The germanium diodes used in the prototype were Mullard type OA70, these are general purpose point-contact diodes and any similar diodes should prove suitable. The meter is a $3\frac{1}{2}$ in 0-1mA movement with a D.C. resistance of 50 Ω , but any 0-1mA meter should be equally satisfactory for this purpose.

The prototype wattmeter was housed in an "Eddystone" die-cast case of size $7\frac{3}{8} \times 4\frac{5}{8} \times 2$ inches (approximately) with four small rubber feet fitted

.30

Input

SW1A

ο115Ω

≷R2

≧r1

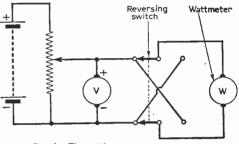


Fig. 4-The calibration arrangement.

to the underside to prevent damage to the paint finish if placed on a rough surface.

Calibration

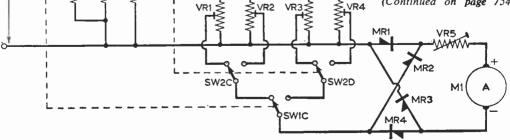
SW1B

SW2B

 ≹R6

When the instrument has been assembled and wired, it is necessary to calibrate it by adjusting the potentionneters RV1-5 inclusive. This, fortunately, is quite a simple matter and requires only the use of an accurate D.C. voltmeter. This meter

is used to measure the voltage applied to the terminals of the wattmeter. Before commencing calibration, the lead to SW1A should be unsoldered so that the load resistors R1 and R2 are disconnected. A variable D.C. voltage is then applied to the wattmeter as shown in Fig. 4. This can be obtained from a battery and poten-(Continued on page 754)



R4

SW2A

R3

Fig. 3-The circuit of the instrument.

Radio Components

(Continued from page 605 of the November issue)

AVING dealt with both TRF and superhet receivers, we now conclude this short series by analysing audio amplifiers in terms of component functions, voltages and currents. Basically, there are two essential types of audio amplifiers which are the concern of the service technician and experimenter, these being the single-ended output stage type and the push-pull arrangement.

Single-stage Amplifier

The simplest of audio amplifiers commercially available is shown in Fig. 6. This is designed for use in a record reproducer (Cossor, Model 559), and uses just a single amplifying stage, V1.

This is a high-slope pentode valve, which receives at its control grid the signal direct from the output of a crystal pick-up. The pick-up used has a relatively high output (hence the omission of an audio driver stage or voltage amplifier), and is a Collaro Studio-T type.

The pick-up signal is applied across the resistive element of a 2M volume control, which gives the correct matching. Instead of the slider of this control going straight to control grid, however, it goes to one side of the track of the tone control, R2, which is valued at 1M. As the other side of the resistive element goes via a capacitor to chassis, we get a tone-control, potential-divider arrangement.

Whatever level of pick-up signal is selected by the volume control. this is applied to R2 and C1 in series. Now, at high A.F., the impedance of C1 is relatively low, compared with its impedance at low A.F. At high audio frequencies, therefore, the capacitor end of R2 can be considered as connected to chassis through a low value resistance. Thus, when the slider of R2 is at the capacitor end of the resistive element, there is very little signal between the control grid of V1 and chassis. There is considerably more low-frequency signal, however, since to such signals C1 "looks" like a high impedance. At this setting of the control, then, we obtain an effective "bass lift".

At the other end of the control's range there is virtually no tone correction at all, because signals at all frequencies are applied direct from the slider of the volume control R1 to the control grid of V1, via the slider of R2. The fact that the high series impedance of R2 and C1 is in parallel with the signal at that setting is of little consequence. However, a progressive "top cut" or "bass lift" occurs as the slider of R2 is turned towards the capacitor end of the resistive element. This is a useful tone control circuit for the simple pick-up amplifier, and

and their Functions

By K. Royal

one for which the experimenter may well find applications.

The rest of V1 is wired in the usual manner. Grid bias for the valve is obtained from the voltage dropped across the cathode resistor R3, and this is of the order of 6V, as measured between cathode (positive) and chassis on a $1.000\Omega/V$ meter. The anode is loaded by the loudspeaker transformer T1, whose turns ratio is selected to match the low impedance loudspeaker to the high anode impedance of the valve. C3 across the primary winding gives further tone correction and damps harmonic resonances which may otherwise be set up in the loudspeaker transformer.

The screen grid of the valve is fed through R4 and heavily decoupled (or smoothed) by C4. It is worth noting that the anode of the valve is fed straight from the output of the rectifier V2 without a smoothing choke or resistor. When this is done on a single-stage circuit the screen grid of the valve must have an almost ripple-free voltage, which is accomplished by the decoupling mentioned above. R4, then, can be considered as the smoothing resistor and C4 the smoothing capacitor. C5, at the cathode of the rectifier, is, of course, the ordinary reservoir capacitor. There is no negative feedback in this simple circuit, for even the cathode of the valve is heavily decoupled by C2.

A fully isolated power supply is employed, T2 being the mains transformer with H.T. and L.T. secondaries. The H.T. winding is centre tapped to facilitate full-wave rectification, while the heaters of the two valves are wired in parallel and energised from the 6.3V L.T. winding.

This kind of amplifier runs at about 260V H.T. (from the rectifier). This gives about 240V on the valve anode and 225V on the screen grid with currents of 41mA and 48mA respectively. The total H.T. current, therefore, is in the order of 46mA as measured in the cathode of V1. The A.C. voltages either side of the centre tap on the H.T. winding of the mains transformer are 235V.

Push-Pull Stereo Circuit

To illustrate the more complex push-pull circuit we show at Fig. 7 the circuit of the Decca SG188 stereo record reproducer. For any stereo system two identical amplifier sections are required which are given as Channels A and B on the circuit.

Each channel has a voltage amplifier tone control stage, followed by two more voltage amplifiers, a phase splitter, two pentodes in pushpull and a pair of parallel-connected rectifiers to provide the necessary current for the two channels. For the following discussion Channel A will be considered, bearing in mind that the rectifiers and power circuits only are common to both channels.

The stereo pick-up gives two outputs, one which is fed to Channel A and the other which is fed to Channel B. The pick-up signal is fed direct to triode V1A via the equalising circuit C50 and R50. This gives a rising response to the higher audio

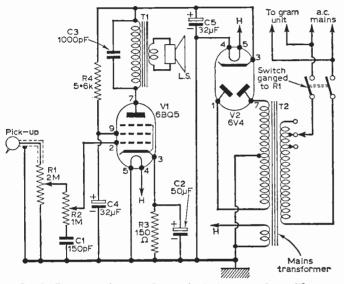


Fig. 6---The circuit diagram of a simple single-stage A.F. amplifier, used in the Cossor, Model 559 Record Reproducer.

signals, since C50 is 100pF (having a high impedance to low A.F.) and R50 is 1M. R52 is simply the grid return for V1A.

The equalised signal is developed across the anode load R51 and fed through C52 to the tone control system. Thus from C52 we have a signal applied to the "treble" circuit (C53, VRI and C54) and also a signal applied to the "bass" circuit (R56, VR2, C55, C56 and R57). Now when VR1 and VR2 are set to the centre of their ranges a signal of frequency characteristics almost equal to that at the output of C52 is fed to the volume control VR3 and there is no tone correction. There is attenuation, though, which is the reason why the circuit features three voltage amplifiers. At high A.F. C54 "looks" almost like a short-circuit, while C53 has a relatively low value of impedance. Thus, with VR1 slider at C53 end of the control, maximum treble is fed to the volume control and this value of treble diminishes as the control is turned in the opposite direction.

The network comprising R56, VR2, R57, C55 and C56 is, in effect, an adjustable low-pass filter.

The signal goes in at the top of R56 and comes out at the slider of VR2. It thus passes only lowfrequency signals to the volume control and the amount of low A.F. relative to high A.F. passed depends upon the setting of VR2.

Two Signals

In that way, then, the volume control receives two signals, one by way of the treble high-pass filter and the other by way of the bass low-pass filter, and as each of these filters are adjustable the required overall frequency response can be accurately established. This type of tone control circuit is also extensively used

circuit is also extensively used in hi-fi amplifiers and control units.

The equalised and tone-controlled signal is developed across the volume control and the required level is tapped off at the slider and fed to the control grid of V2A. This is a fairly conventional A.F. amplifier but has facilities in its cathode circuit for the application of negative feedback. The stage is biased by the voltage dropped across R62 and R64 as series in the cathode circuit. R66 is the anode load from whence the amplified signal is fed to the grid of V3A via the coupling capacitor C60.

R65 is the grid leak for V3A and reflects the voltage dropped across R69 in terms of grid bias at the grid. Current negative feedback is applied to this stage, since R69 does not have a bypass capacitor.

V4A is the phase splitter valve. This is direct coupled to the anode of V3A and the splitter is biased because the voltage at

its cathode is V2 more positive than the voltage at its grid, thereby making the grid V2 negative with respect to its cathode.

Push-Pull Drive

The phase splitter produces two signals, one at the anode, across R71, and the other at the cathode, across R70. As these resistors are accurately balanced the two signals are of equal amplitude, but owing to the phase inversion effect of the valve the signal at the anode swings positive when the signal at the cathode swings negative and vice versa. These signals represent the drive for the push-pull valves and are fed through C64 to the control grid of V3A and through C63 to the control grid of V4B.

The output pair are biased for class A conditions, meaning that there is no flow of grid current, and the signals are re-established as one complete waveform across the centre-tapped primary of the output transformer T1. They are here coupled to the low-impedance secondary winding, which is tapped to suit a range of loudspeaker impedances.

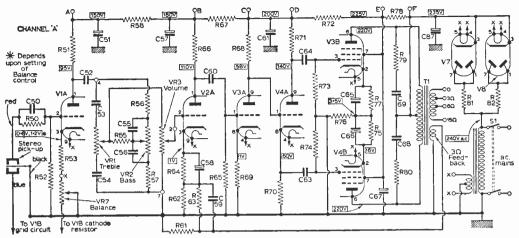


Fig. 7—The functions of all the components employed in this twin-channel, push-pull amplifier (Decca SG188) are given in the text.

Negative Feedback

A further secondary winding on T1 is employed for feeding back a fraction of the output signal to the cathode circuit of V2A as negative feedback. This is done through the frequency-selective network R63 and C59, with R61 as the other arm of a potential divider. In effect the feedback signals are reflected, via the cathode, to the control grid circuit of V2A in counteracting phase to the signals originally applied from V1A. This results in a reduction in total signal applied (hence another reason for the three voltage amplifiers), but its asset, of course, is that it cancels harmonic and other distortions, including hum.

The output valves are biased for class A by R75 and R77 in their cathodes, with the grid return circuit occurring through the balanced grid leaks R73 and R74. R76 is a low-value grid stopper arranged to prevent parasitic oscillations in the output stage. The cathodes of the output valves are decoupled by the electrolytics C65 and C66. This, along with the negative feedback, gives the stage a good damping factor, which is an essential requirement for high-quality reproduction.

Anti-resonant devices comprising R79/C69 and R80/C66 are connected across the primary of the output transformer and the screen grids of the output valves are connected in parallel and fed through R78, with C67 providing decoupling.

Each voltage amplifier stage is individually decoupled on the H.T. line, which is necessary in the interests of low-frequency stability, particularly when two amplifiers are sharing a common power supply. VIA is decoupled by R58/C51, V2A by R67/C57 and V3A by R72/C61.

Power Supply

The power supply used in this model is not isolated from the mains. It will be seen that an auto-transformer is used for feeding the anodes of the rectifiers V7 and V8 and this winding is connected to the mains supply via chassis. There is, however, a separate winding for the parallelconnected valve heaters and is centre tapped to chassis to reduce the pick-up of hum to the smallest possible level.

The valve anodes are connected by limiting resistors, necessary to avoid overloading of the rectifiers on surges, while the cathodes are connected in parallel, with C87 serving as the reservoir capacitor.

Stereo Balance Control

In twin-channel stereo systems a separate control labelled "balance" is often featured. This simply serves to balance the overall gain of the two channels. In Fig. 7 the balance control is VR7 and it is connected in the cathode circuits of the two first voltage amplifiers and, since the slider is connected to chassis, equal gains should occur with the control set to the centre of its range. When the control is adjusted so that the resistance in one cathode circuit is reduced then that valve increases slightly in gain, while its partner decreases slightly in gain and vice versa.

All the voltages to be expected in the various stages are marked on the circuit and, it will be obvious that the circuit of Channel B is identical to that of Channel A.

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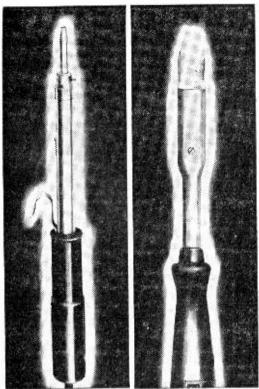
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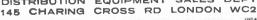
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THIS HEAD IS SPECIALLY DESIGNED FOR USE WITH THE DIGITAL COUNTER DESCRIBED IN THE FEBRUARY 1962 ISSUE, THE COMBINATION BEING SPECIALLY SUITED FOR MAKING MEASURE-MENTS ON RADIOACTIVITY IN LIQUID SAMPLES (SUCH AS RAINWATER).

THE SENSITIVITY OF THE COMBINATION IS SUCH THAT EVEN SMALL LEVELS OF RADIO-ACTIVITY PRESENT FROM NATURAL CAUSES (FAR BELOW CONTAMINATION LEVELS) CAN BE EASILY MEASURED.

IT SHOULD BE POSSIBLE TO BUILD THE UNIT DESCRIBED FOR LITTLE MORE THAN £10.

An Advanced GEIGER HEAD

By E. DEXTER

HE theoretical circuit shown in Fig. 1 is very similar to the simple Geiger Head published with the author's Digital Counter in the February issue. The main difference lies in the choice of a completely different type of Geiger-Tube, the Mullard MX124/01. The actual tube is enclosed in a thinwalled glass envelope coaxially within a sealed-on test-tube for containing the liquid to be tested. Thus the liquid intimately surrounds the Geiger-Tube proper, which accounts for the very high sensitivity.

H.T. Voltages

The MX124/01 has an unusually low operating voltage (400 to 500) compared to other tubes of this type. This is a distinct advantage for amateur circuitry. The arrangement of the H.T. feed in the circuit is somewhat unusual, a conventional 300V positive supply in conjunction with an additional 100V negative supply being used.

There are two good reasons why this arrangement has been adopted. Firstly, +300 and -100are becoming standardised outputs for stabilised power supplies, and are thus also the main outputs of the "Experimenter's Power Pack" published recently in this magazine, which is admirably suited for operation of this unit.

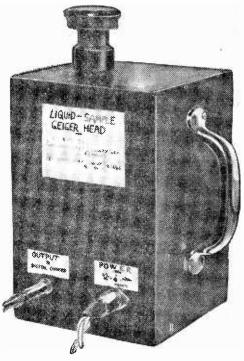
suited for operation of this unit. Secondly, the EC92 cathode-follower headamplifier can be run off the same H.T. supply in this arrangement, as is evident from Fig. 1. The power supply requirements are seen to be identical to those of the Digital Counter, and the two units may be run simultaneously off the "Experimenter's Power Pack".

It is, for reliable and accurately reproducable results, highly desirable to run this equipment off a stabilised power supply, though other ordinary simple power supplies could be tried. It will then probably be necessary to use separate power supplies for this head and for the Digital Counter.

It is absolutely essential that the total voltage applied to the tube never exceeds 450V, as otherwise flashover and possible destruction of the tube can take place. Thus the positive H.T. must not exceed 350V.

Threshold Voltage

Mullard quotation for the Threshold Voltage for the MX124/01 is "maximum 400V". Individual samples vary and the tube in the author's prototype was found to have a threshold at 360V. It is desirable to operate the tube at approx. 50V above threshold which gives 410V for the author's prototype.



The finished instrument.

When the unit is initially put into operation, the output should be connected to an oscilloscope, and the pulses observed as the positive stabilised H.T. is varied on the power pack. As the H.T. voltage is gradually reduced, the pulse amplitude will also decrease, until it vanishes at the threshold voltage.

The voltmeter reading should then be noted, and the H.T. increased by about 40 to 50V. This assures the proper operating point having been set, and it should be checked in the same manner from time to time as the tube ages.

Pulse Amplitude

Fig. 2 is self-explanatory as far as the theoretical details of the generation of the pulses are concerned. The treatment is, of course, simplified, as no account has been taken of chemical effects within the tube also leading to rapid extinction of each discharge.

Nevertheless, the capacity-effects sketched in Fig. 2 generally dominate and are sufficient to give a measure of control over the output pulse amplitude, by means of adjustment of C1. The larger the capacitance of C1 and Cstray, the greater is the charge-per-pulse passing through the tube, i.e. the greater the strain on the tube. It is thus desirable to keep both of these capacitances small.

Naturally, any capacitive loading of the tube increases the violence of the discharge on each pulse, and it may thus seem strange that a circuit is proposed which deliberately introduces such loading.

The advantage gained, however, is the production of a substantial pulse giving secure operation of simple counter circuits aimed to avoid all snags and critical effects in the input stages, and this advantage is considerable for amateur purposes.

Tube Life

The price paid for this advantage is a shortening of tube life, to the region of at least 100 million counts, instead of the almost infinite life achievable in more critical specialised circuits. While such a life would be too short for high counting-rate professional laboratory use, it is still more than ample for the amateur uses intended in this article.

One will be operating at counting rates around 100 per minute for the purposes envisaged, so that even with the minimum life of 100,000,000 counts, at least 15,000 operating hours are certain. Probably much more.

The prototype shows that, after completing more than 2,000 operating hours under these conditions, changes of tube characteristics are at the most a fraction of 1% of those of a brand new tube.

Slow Counting Rates

The adverse effects on dead-time and plateauslope are of little importance at the slow counting rates intended, though probably seriously limiting the suitability of this circuit for work at normal laboratory counting rates of some hundred or more per second. The plateau-constancy over long periods of usage under the conditions specified has proved itself in practice, and the use of stabilised power supplies adequately removes errors of counting due to plateau-slope for the present purposes.

The actual values of C1 and Cstray do not affect the output pulse amplitude as much as the ratio of their values. The total pulse-voltage generated is necessarily equal to the difference between operating point and threshold, which we deliberately set at about 40 to 50V.

This pulse voltage is seen in Fig. 2 to appear across C1 and Cstray in series, the two capacitances thus forming a voltage-divider. Only the portion appearing across Cstray is passed on to the cathode follower V2, and hence to the output. If a reasonably large part of the total pulse voltage is to appear at the output, therefore C1 must at

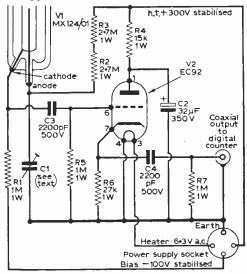


Fig. 1—The circuit of the head.

least be equal to, or somewhat larger than Cstray.

This is the reason for including an actual physical component for C1, part of which is made up by the inherent stray anode capacitances of the tube and wiring, and the rest by a physical component in the form of a pair of twisted insulated wires.

It is desirable to set conditions such that, finally, C1 (total) and Cstray are approximately equal. This condition is realised when the pulse output voltage from the unit is about half of the threshold-excess, i.e., some 20 to 25V peak. The output pulses should be observed on an oscilloscope in comparison with A.C. sinewave voltages of known amplitude, using the same Y-amplifier gain in all cases.

The length of twist of the insulated wires forming C1 is altered, until the output pulses are observed to have 20 to 25V amplitude. It need hardly be said that the operating point must *previously* have been set 40 to 50V above threshold, as described above.

The Cathode Follower

This stage is fully conventional. C3 blocks the negative 100V D.C., allowing only the positive pulses to pass. and be reproduced accurately at the same amplitude and form at the output. R4 (Continued on page 729)

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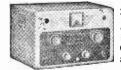
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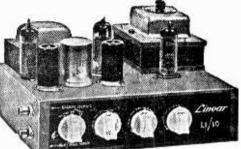
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ELECTRON WORKS. ARMLEY LEEDS



(Continued from page 726)

and C2 give heavy decoupling for the stage. C4 and R7 remove any D.C. component from the output otherwise resulting from the cathode circuit of V2.

The purpose of V2 is *not* voltage amplification as the output voltage of the geiger tube is ample for the digital counter, etc. The purpose is, rather, to reduce the impedance, allowing transmission of the output signal on reasonably long lengths of coaxial cable without loss. This function certainly amounts to a form of power-amplification, however.

Gieger-Tube Screening

The manufacturers specify operation of the tube in a 2in, thick all round lead container, which can weigh anything up to half a hundredweight! Whilst this is certainly essential for efficient industrial use, it is by no means necessary for amateur use, provided the factors concerned are understood and taken into account. At any rate, it is clear why the bare tube alone must be removable in an industrial arrangement, and mercury-cup connectors used: the whole unit with lead casing would be far too heavy and cumbersome to move about!

The advantages of the heavy lead casing are principally twofold, neither of which is essential for the amateur. Firstly, and most important, the tube is thereby screened from ambient levels of X-rays or other radiation from other experiments and equipment operating on the premises nearby, which have nothing to do with, but would scriously interfere with, the experiment running with the tube in question. This danger of interference is not likely to arise under amateur conditions, provided such sources as luminous watches the clocks are kept away from a running experiment.

Secondly, the lead casing would absorb a large portion of the "Cosmic" background radiation coming from outer space, etc. This reduces the "background-count per minute" to be subtracted from a count made with a liquid sample, i.e. it improves the "signal-to-noise ratio", giving better resolution and shorter required counting times for a given desired accuracy.

This may be important for industrial concerns where time is money, but is unimportant for amateur usage. The saving in expense, and convenience in construction, achieved by omitting a lead screen outweighs all other considerations for the amateur.

Important Points

When operating the tube without a lead screen, the following two points must be watched care-fully:---

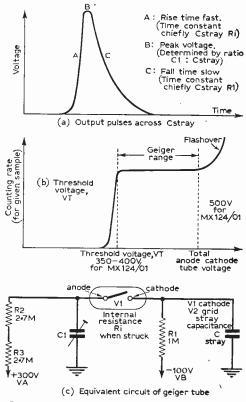
(a) The unit is vulnerable to interference from external radioactive sources of sufficient intensity. Such sources must be removed to a distance of at least three yards, or kept fixed in position during an experiment, their effects being included in the subsequently subtracted "background count" made without the test-liquid in the tube. In particular, do not move the hands about near the unit during a count whilst wearing a wristwatch with luminous figures. (b) The background count will be higher with the tube completely empty than when filled with pure non-active distilled water. This is due to the water acting as a weak screen, absorbing some of the low-energy components of the cosmic radiation.

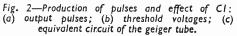
the low-energy components of the cosmic radiation. Thus the "background-count" should always be made with the tube filled with pure distilled water, because the water-content of the subsequently counter test liquid will give the same reduction of cosmic background. Failure to observe this procedure can cause quite serious errors.

In the author's prototype, the background-count was found to be 40.4 per minute with the tube completely empty, but only 38.3 per minute with the tube full of distilled water. The count with a certain sample filled into the tube was 47.2 per minute, representing a correct signal of 8.9 per minute due to the sample.

Had the empty-tube background count been used in error, the sample-signal would apparently have been only 68 counts per minute, an error of well over 20%!

When using a lead screen the weaker cosmicradiation components are absorbed anyway, so that then there will be no difference in background counts for an empty tube or one filled with distilled water.





Photoelectric Effect

Geiger-Tubes of the type here specified are often sensitive to light, giving an appreciable countingrate in response to illumination. This effect was found to be immeasurably small for normal wavelengths of light in the author's prototype. A background-count of 40.4 per minute was obtained with the empty tube, whether completely dark or whether strongly illuminated with a couple of 25W bulbs 5in. away.

The accuracy limits of this experiment were about plus-or-minus one count per minute. Thus error due to normal room illumination, if present at all, is likely to be less than 2%. Nevertheless, it is desirable to keep the tube dark, for safety. The arrangement adopted satisfies this condition, in that most of the tube length is inside the body of the wooden case.

The rest is covered by the black P.V.C.-Tape, to within about 4 in. of the spout, which is covered by a cap, also desirable to reduce evaporation of the sample liquids. Any suitable opaque material of suitable shape and size can be used for the cap, preferably insulating and loosely fitting. *Do not* use a cork of any sort, as this could press down on and break the delicate inner construction of the tube.

Care of the Geiger-Tube

Counting times of more than three hours maximum should seldom if ever be required with the sensitivity achieved by this head. Samples prepared as already discussed in the "Digital Counter" article, and with the further remarks below, normally require counting times of only 30 to 60 minutes for sufficient accuracy. Thus samples need never be left very long in the tube.

Prolonged presence of samples in the tube can cause diffusion through the thin glass of the inner unit, raising the background count permanently. Thus all samples should be poured out im-

Thus all samples should be poured out *immediately* after conclusion of a count, and the tube swilled out thoroughly at least three times with clean or distilled water.

Never use tarry, greasy or sticky liquids which could soil the tube permanently or render cleansing extremely difficult. Although dilute acids do no damage avoid using caustic alkalis and do not insert warm or hot liquids into the tube.

Preparation of Samples

Procedure outlined in the "Digital Counter" article should be observed. Whilst it is still necessary to concentrate rainfall and other water samples, lower concentration factors can be used than with the simple Geiger-Head described in the "Digital Counter" article.

The simple Geiger-Head, furthermore, gives really quick definite signals only with those rainfall samples representing the verge of real contamination. With present levels of radioactivity in rainfall, long careful overnight counts are required for reasonable quantitative measurements but with the unit described in this article, definite strong and reliable signals are very easily and very quickly produced even with rainfall of present levels of activity.

Components List				
VI Mullard Geiger Tube MX124/01 V2 EC92				
Resistors (All resistors IW carbon)				
RI ΙΜΩ R5 ΙΜΩ				
R2 2·7MΩ R6 27kΩ				
R3 2·7ΜΩ R7 ΙΜΩ				
R4 15kΩ				
Capacitors				
CI See text C3 2200 pF, 500V				
C2 32µF, 350V C4 2200pF, 500V electrolytic				
Miscellaneous				
BTG valveholder and screening can				
4-pole panel socket				
Coaxial panel socket				
Tagstrip. Material for cabinet				

Quantitative Data

Serious experimenters, and particularly schools and clubs, will be interested in doing quantitative work with this apparatus, to determine not only relative values of radioactivity in liquid samples but also absolute values in terms of equivalent weight of radium per unit volume of the liquid.

The author has had available standard solutions of uranium and thorium, as well as possessing a high-voltage Geiger-Tube of similar type supplied with extensive calibration charts from the manufacturers. Using this apparatus as comparison standard, the prototype MX124/01 has been carefully calibrated. The results of this work, here given in full, may reasonably be supposed to be applicable to any sample of the MX124/01 tube used under the conditions specified in this article.

The Curle

The unit used for measuring absolute values of the radioactivity of substance is the Curie. A quantity of substance having the same effective activity as one gram of radium is said to have an activity of one Curie. This unit is extremely large, so that convenient practical units are the micro-Curie (μ C) and the pico-Curie (pC) representing a millionth part, and a millionth of a millionth part, of a Curie, respectively.

One millogram or ordinary thorium has an activity of about 100pC. This was found to give, when effectively contained in the (exactly) 8 c.c. of liquid needed to fill the MX124/01. an increase of counting rate of about 10 per minute with the head described in this article.

Similarly, one milligram of ordinary uranium has an activity of about 350pC, and was found to give an increase of counting rate of about 35 per minute when present in the 8 c.c. contents of the MX124/01.

The sensitivity to this type of radioactive substance is thus about one count per minute per 10pc present in the contents. These substances, i.e. heavy elements, emit principally alpha-rays (helium nuclei) and gamma-rays (exceedingly short wavelength wireless waves), the tube responding principally to the latter.

(To be continued)



PRACTICAL WIRELESS

December, 1962



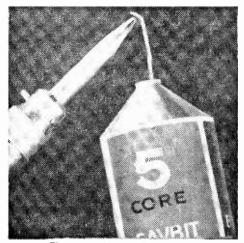


STABILISED POWER UNITS

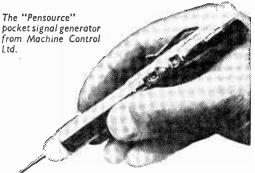
THE latest versions (Mk. III) of the Lexor stabilised power units models LT.12-05 and LT.24-05, are now available.

New features of the Mk. III include a much reduced longitudinal noise factor and an improved overload and short-circuit protection. The two models available have output voltage ranges of $5\cdot5-14V$ or $18\cdot28V$. The output voltage of either instrument is continuously variable and may be adjusted either by a panel knob or a pre-set control. Both instruments will deliver output currents up to 0.5A continuously at all voltage settings.

The units are mounted in steel instruments cabinets 8in, $x \sin x 5\frac{1}{2}in$, finished in grey hammer stove enamel with contrasting blue panels. The price of the new Mk. III units is £25 7s. and they are made by Lexor Electronics Limited. 25-31 Allesley Old Road. Coventry, Warwickshire.



The new Multicore solder dispenser.



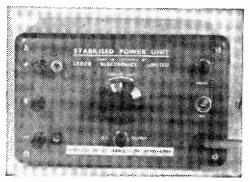
POCKET SIGNAL GENERATOR

FOR engineers, radio and TV servicemen who require a small and convenient form of input for testing or fault finding, Electronic Machine Control Ltd., have produced the "Pensource" range of pocket signal sources.

These instruments are made available in several ranges and give an output of approximately $\frac{1}{2}V$. Basically each "Pensource" is a transistorised

Basically each "Pensource" is a transistorised oscillator built into a robust chromium plated case. The supply to the oscillator is provided by a 1½V penlight cell and under normal conditions of use, should last approximately four to six months. The "Pensource" costs £4 10s. and a leatherette

The "Pensource" costs £4 10s. and a leatherette case is also available at an extra cost of 10s. 6d. The makers are *Electronic Machine Control Ltd.*, *Mayday Road*, *Thornton Heath*, *Surrey*.

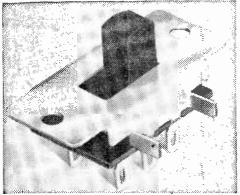


One of the new Lexor stabilised power units.

NEW SOLDER PACK

NEW from Multicore Solders Limited is a solder dispenser especially suitable for use by the amateur constructor. It is, in fact, an extruded aluminium tube, the top being tapered to a delivery hole through which the solder is drawn as required. This arrangement prevents the solder tangling and the flat base of the dispenser allows it to be stood firmly on the work bench, leaving the user complete freedom of both hands whilst working.

The contents of the new pack is a 16ft length of 18s.w.g. Ersin Multicore Savbit alloy and its price is 2s. 6d. complete. The manufacturers are Multicore Solders Ltd., Maylands Avenue, Hemel Hempstead, Hertfordshire.



One of the new switches from Carr Fastener Co. Ltd.

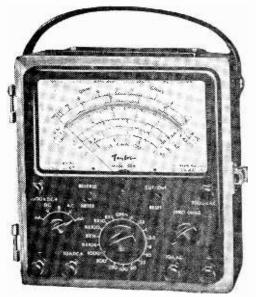
NEW SLIDE SWITCHES

734

JUST incorporated with the range of components produced for the electronics industry by Carr Fastener Co. Ltd., are two new slide switches. These are identical in specification but differ slightly in their mounting facilities. Both switches are of the double-pole, double-throw type, and can be used for radio wavechange, instru-

ment or any relatively low voltage switching application.

Constructionally, the switches differ only in their steel shell, one having vertical fixing lugs and the other having two 0.125in. diameter holes at 1.125in. centres and alternative side-fixing lugs. Carr Fastener Co. Ltd., Stapleford, Nottingham.



This new multimeter is manufactured by Taylor Electrical Instruments Ltd.

MINIATURE SOLDERING IRONS

RECENTLY A.N.T.E.X. Ltd. have added to their range of Precision soldering irons. Amongst the new additions is the model E240, a lightweight instrument operating from 230-240V mains and with a power consumption of 20W.

The novel design of these irons makes them easy to handle and attractive. Interchangeable bits are available to fit this model as well as a wirestripper attachment. The price of the complete iron is 35s. and the makers are A.N.T.E.X. Ltd., Grosvenor House, Croydon, Surrey.

MULTIRANGE METER

THE model 88B multimeter from Taylor Electrical Instruments Ltd., is similar in operation to their popular model 88A, but is somewhat reduced in size. It is available in



The model E.240 soldering iron is made by A.N.T.E.X. Limited.

either a bakelite or wooden case.

The sensitivity of the instrument is $20.000\Omega/V$, and other features include a mirror scale, an overload protection device and a reverse polarity facility.

Among the ranges included in the instrument are, resistance ranges up to $50M\Omega$ and decibel ranges. The instrument will also measure capacitance and inductance but a model 388 adapter is required.

Another accessory which is available is a high voltage probe for measurements up to 25kV.

The two batteries used in the meter are located in a separate compartment. The types used are Ever-Ready U.2 and B.121.

The makers of this new multimeter are Taylor Electrical Instruments Ltd., Montrose Avenue, Slough, Buckinghamshire.

THE TRANSISTOR CLOCK

ONE intriguing result of research in radio engineering—the transistor principle—has now been applied to clock-making. The Kundo (Crown Manufacturing Co. Ltd.) transistor clock, on display at the recent Watch and Jewellery Trade Fair, has an operating mechanism of unusual simplicity. A magnet attachment to its pendulum dips into a coil at each oscillation, producing, by induction, a voltage pulse which, fed into the transistor, triggers the flow of current from the battery to the drive coil. A driving impulse is thus imparted to the pendulum.

Needing no maintenance, this extraordinary timepiece runs continuously for no less a period than three years!

PLAYER

Cabinet Price £3.3,0

Carr. & 1ns. 5/-,

CABINETS

Contemporary style, rexine covered cabinet in two tone maroon and cream. Size 18; x 13; x ht. Sinn. fitted with all accessories including baffie board and anodised

including baffie board and anodised metal fret. Space available lor all modern amplifiers and autochan-gers, etc. Uncut record player mounting board 14 x 13in, supplied. 2-V. M.V.E. 2-W.ATT AMPLIFIER Win stage ECL82 with vol. and neg. feedback Tone control. A.C. 200/ 250 v. with knobs, etc., ready wired to fitabove cabinet. £2.17.6. P. & P. 16

P. & P. 1/6. 6in. Spkr. & Trans., 22/-, P. & P. 2/-. Complete Kit, including UA14 Unit as illustrated, £12.19.6, carr. 7/6.

JACK PLUGS, Standard 24 Igranic Type, 2/6. Screened Ditto, 3/3. Miniature 14', 2/3. Screened Ditto, 2/6. ENAMELLED COPPER WIRE 11b. reels, 14g.-20g, 2/6: 22g-28g, 3/-: 30g-40g, 3/9. Other gauges quoted

Condensers-Silver Mica. All values, 2pF to 1,000pF, 6d. each

Multicore Solder 60/40 3d.

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3 Valves watt, 3 ohm and 15 ohm Out-

and 15 ohm Out-put. A really first-class Amplituer giving Hi-Fi quality at a reasonable cost. Mullard's latest circuit, Valve line up: EF86, EE84, EZ81. Extra HT and LT available tor Tuner Unit addition. This is the ideal companion Amplifier for FM tuner Units. tuner units

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3w. COMPLETE KIT (ncl, Valves, all components, wiring diagram and special quality sectional Output Trans.). ONLY £6,18.6. Carr, 5/-Complete wired and tosted, sgns, Bronze Escutcheon Panel, Prin-ted Vol., Treble, Bass, On-off, supplied with each Kit. Wired OP, socket power and addi-tional smoothing for Tuner Unit, 10/6 extra.

10/6 extra. Recommended Speakers— WB HF1012 95/-. Goodmans AXIOM 110 £5, etc.

SPECIAL BARGAIN OFFER

SPECIAL BARGAIN OFFER A sell-contained Portable Unit Incor-porating latest BSR 4 speed Auto Changer Record Player and famous High Fidelity "Ful-Fi" Xtal Pick Up with Turnover Cartridge, litted with LP and 78 Sapphire Stylli, Internai 2 valve Amplifier of modern design with variable Tone and Volume Controls. This, together with a quality P.M. Speaker ensures a high standard of reproduction. The whole is housed in a robust r.m. Speaker ensures a high standard of reproduction. The whole is housed in a robust wooden Cabinet attractively styled in 2 Tone contemporary leather cloth with contrasting polka dot reliet.

Kit consists of 3 sub assemblies already wired. Grub screw connections between Units only necessary-absolutely no Originally built to be sold at 17 Gns.

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Carr. & Ins. 7/6 Autochanger Unit—BSR Model UA20. Amplifiler—valves UCL82. UY85 and 7 x 4/n. Elliptical Speaker, Cabinet size 17 x 14} x 84in.

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per yard. 11b. 2/6, etc.

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parts: FMTI, 5 gns. 4 valves, 80/-, FMT2, £7, 5 valves, 37/8, JTV MERCURY 10 gns. JTV2 £13,19.6, 4 valves, 39/8 parts NEW JASON FM HAND-BOOK, 2/6, 48 hr. Alignment Service 7/6, P, & P, 2/6.

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TUBULA		CAN TYP	ES
25/25V	1/9	8+8/450V	4/6
50/12V	1/9	8+16/450V	5/-
50/50V	2/-	32+32/2751	4/6
100/25V	2)-	δ0+50/350¥	6/6
8/450V	2/8	60 + 250/	
16/450V	8/6	275V	12/6
16 + 16/45V	5/6	100 + 200/	
32+32/450V	6/6	275 V	12/6
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Est. 1949

December, 1962



Simple -Valver

HIS unpretentious little receiver can be built very cheaply. Considering the extreme simplicity of the circuit, it has a very good performance and with careful manipulation of the controls, the single tuned circuit will enable all the more powerful transmissions to be received clear of interference.

Circuit

The EF91 is a high slope miniature valve which is available ex-equipment very cheaply indeed. Three of them are used in this receiver. The first is arranged as a pentode R.F. amplifier but it will be noticed from Fig. 1 that there is no tuned circuit associated with it. The high slope of the valve, however, goes a long way towards repairing this omission and quite a worthwhile gain is achieved. Because the EF91 does not have variable-mu characteristics it was necessary to achieve some method of gain control other than by variation of bias, and the problem was solved very satisfactorily and simply by feeding the signal from the aerial to the slider of a 1M potentiometer in the grid circuit. The second valve, connected as a triode, is used

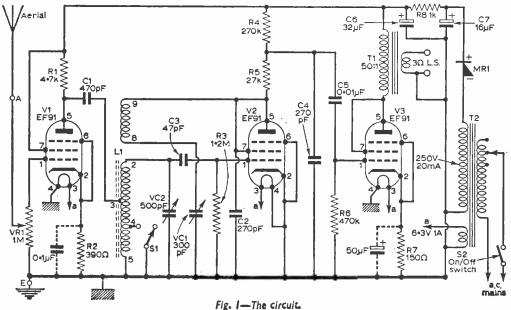
as a conventional leaky grid detector, regeneration

By T. M. Bush

being applied through the variable capacitor VC1 to sharpen the tuning and increase increase the sensitivity. Because the R.F. stage isolates the aerial from the tuned circuit the tuning is not affected by aerial loading and if by chance, as will sometimes happen, too much reaction is applied, the resultant oscillations will not be radiated to the annoyance of the neighbours. Resistor R5 and capacitors C2 and C3 remove the R.F. component from the output and the audio signal is passed via the capacitor C4 to V3, the output valve. This is another EF91, again triode connected. The optimum load could not be discovered but this is not of much importance with the triode connection and an output transformer having a ratio of 50:1 was found very satisfactory for a 3Ω loudspeaker.

Power Supply

A miniature double-wound mains transformer of the instrument type, having an output of 20mA at 250V and 1A at 63V supplies the power in conjunction with a contact-cooled metal rectifier. Smoothing is provided by the resistor R8, and the associated electrolytic capacitors C5 and C6. A



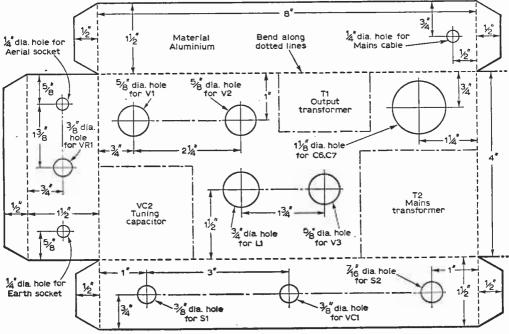


Fig. 2-The drilling dimensions of the chassis.

pilot or dial light, if fitted, should be $6.3V \ 0.04A$, so as not to exceed the rating of the transformer winding. A separate on/off switch was fitted in the prototype but there is no reason why mains switching should not be incorporated with VR1. The power consumption from 240V A.C. mains is less than 20W. connections around V2 and the coil are kept to a reasonable length. Tinned copper wire of 22s.w.g. covered with sleeving is recommended for all the wiring, details of which are given in Fig. 3. The loudspeaker is connected direct to the secondary terminals of the output transformer on top of the chassis. It is good practice to connect one of these

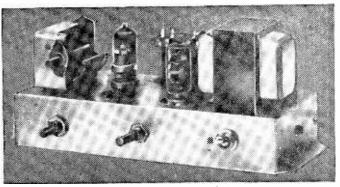
Modifications

It will be noticed that the bias resistors of V1 and V3 are not bypassed. Consequently, if greater gain is required, capacitors may be fitted across them as shown in dotted outline in Fig. 1. A further increase in gain can be obtained by reducing the value of R2 to 150Ω but this will increase the current through the value and is permissible only if the mains transformer can accept the extra load. The total H.T. current in the prototype was exactly 20mA.

Construction

The prototype was constructed on a chassis of 18s.w.g. aluminium sheet measuring 8in. x 4in. x 1½in., details of which are given in Fig. 2. This

gives plenty of room for standard size components with the exception of the reaction capacitor, VC1, where a miniature must be used in order that it may be accommodated within the depth of $1\frac{1}{2}$ in.; alternatively, the chassis could be made deeper. Construction may proceed in any convenient order. The layout and the arrangement of the wiring and components is not at all critical so long as the



The receiver nearing completion.

terminals to chassis and a solder tag should be fitted for the purpose on one of the transformer holding-down bolts.

Components

Resistors may be $\frac{1}{2}W$ or $\frac{1}{4}W$, except R8 which should be 1W. The capacitors have to withstand (Continued on page 741)

PRACTICAL WIRELESS



PRACTICAL WIRELESS

December, 1962



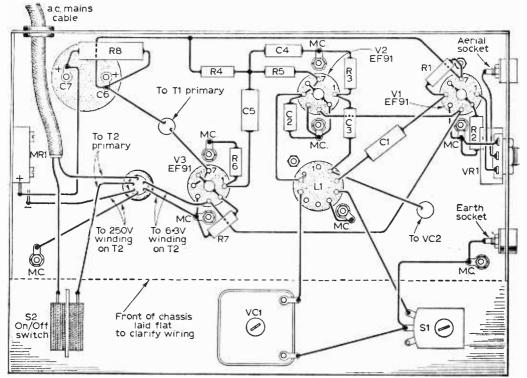
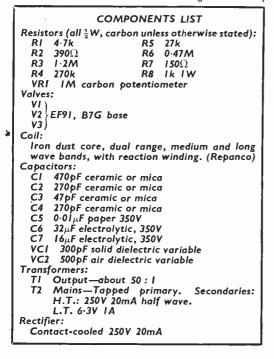


Fig. 3-The complete wiring diagram.



(Continued from page 738)

the full H.T. voltage from the rectifier when first switching on and must therefore be 350V working. Any kind of tuning capacitor, air-spaced or othergang component can be used as in the prototype. The coil L1, may be any iron-dust-cored dual wave type with a reaction winding but it is convenient if it is designed to plug into a B9A or B7G valve base. For tuning, a 3in, diameter engraved knob is fitted direct to the tuning capacitor but there is no reason why a slow motion drive should not be fitted if desired.

Testing and Operation

When the wiring has been completed, a test should be made with a meter between C6 and chassis to see that there are no short-circuits in the H.T. wiring. If all is well, power can be applied and transmissions should then be received. Two or three feet of wire as a throw-out aerial will usually be enough, though in poor reception conditions, some more efficient arrangement may be necessary. An earth is not essential, but will reduce mains-borne interference.

It will probably be found that with VR1 at maximum, some programmes will be receivable at adequate volume with VC1 set at minimum, but will suffer from interference from adjacent stations. In this case, the procedure is to reduce the volume by means of VR1 and bring it back to the desired level by the application of reaction, at the same time adjusting VC2 for the best results.

MIDGET MAINS PORTABLE

By V E HOLLEY

HIS handy little receiver was first built with one R.F. stage followed by a diode detector and in this form it gave good service in the north west London area. When later it was required for use in a less favourable location, a second R.F. stage was added to increase the sensitivity.

R.F. Amplifier

The signal is supplied by a ferrite rod aerial (L1, L2 in Fig. 1) and two R.F. pentodes, EF91, are used to amplify it to a suitable detection level. The full gain of the two stages is not required to the two st

The full gain of the two stages is not required and indeed, could not be used with stability, so the gain is reduced by resistance loading in both anode circuits and by omitting by-pass capacitors from the cathodes. If greater gain is required, one or both of these capacitors may be inserted in the manner of C4, which is shown dotted in Fig. 1. Decoupling is provided in both anode circuits.

The inductance of the rod aerial is adjustable within fairly wide limits and the second tuned circuit, which is ganged to it, may therefore incorporate any dual range iron dust cored coil designed to cover the long and medium-wave bands with a 500pF tuning capacitor.

It will be noted that there is no provision against overloading but as both valves operate with negative current feedback no trouble is likely to be encountered under normal conditions.

Selectivity

The selectivity provided by the two tuned circuits is quite good and with the assistance of the directional properties of the aerial, the BBC programmes and some of the continentals can be received clear of interference in daylight and darkness, in any reasonable reception area. Some further improvement might be obtained by applying reaction to L3 and L4; this was not tried.

Demodulation

The signal at the anode of V2 is rectified by a germanium diode D1 (GEX34). After passing through the R.F. filter C10, R8, C11, audio frequencies appear across the volume control, VR1 together with a \cdot D.C. voltage negative to chassis, which is used for alignment purposes, as will be described.

A.F. and Output Stages

A triode-pentode valve, ECL82, is used here in a conventional arrangement. Grid leak bias for the triode section avoids the need for a bias resistor and capacitor, but the pentode bias resistor must be bypassed in the normal manner in order to avoid negative current feedback which is, of course, undesirable in an output stage. The optimum load of the valve is 5,600 Ω and to match this to a 3 Ω loudspeaker, the output transformer must have a ratio of about 45:1.

If the D.C. resistance of the primary is more than about 200Ω , it is advisable to insert a resistor (R12) in the screen supply so that the voltage at the screen will not exceed that at the anode. The network R14, C15 serves to correct the response at the higher audio frequencies where valve and loudspeaker impedances rise considerably.

Power Supply

The receiver requires an H.T. supply of about 60mA at 210V and a heater supply of something (Continued on page 745)

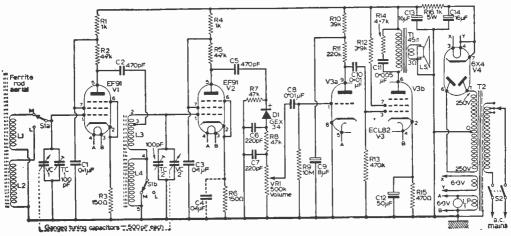


Fig. 1—The circuit.



Build The Sinclair MICRO-AMPLIFIER



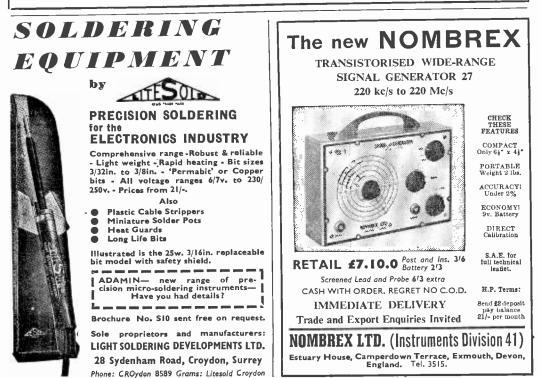
ACTUAL SIZE

- MAT 120 7/9
- MAT 121 8/6

This microscopic amplifier, the smallest of its type in the world, out-performs amplifiers 20 times as large. The main features of the design are listed below:—

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- 2) Power Consumption from 0.4 mA at 1.3 V to 1 mA at 9 V. Any battery may be used.
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- 5) Clear and detailed instructions enable the micro-amplifier to be built in under two hours with ordinary tools.
- 6) Uses brand new microminiature components and micro printed circuit.
- 7) Free applications data supplied with every kit showing how to use the amplifier with high and low impedance pickups and microphones and hi-fi stereo headphones. Circuitry is given for using the amp. in micro-radios and transmitters, and with a micro telephone pick up coil (also available).
- 8) Satisfaction guaranteed. Overall size: $\frac{3}{4}'' \times \frac{3}{8}'' \times \frac{1}{2}''$

28/6 plus 1/6 Postage and packing from: SINCLAIR RADIONICS LTD. 69, Histon Rd. Cambridge TELEPHONE CAMBRIDGE 53965 TRADE ENQUIRES INVITED



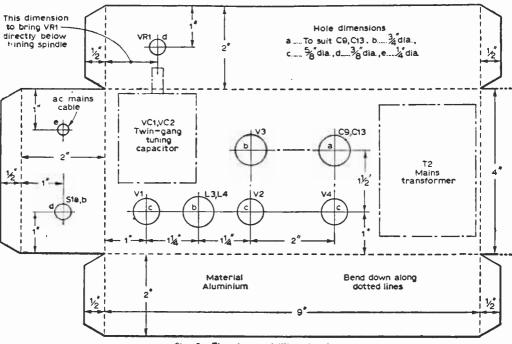


Fig. 2-The chassis drilling details.

(Continued from page 742)

under 2A at 6.3V. The use of a double wound mains transformer to supply this makes the chassis safe to handle at all times and considerably reduces mains-borne interference.

It is convenient to have a separate 6.3V winding to supply the heater of V4 so that there is not a large potential difference between

its heater and cathode, but if only one winding is available, it is quite in order to include V4 heater with the others. If this is done, the winding should be rated at not less than 2.5A and it is most important to omit the connection between pins 4 and 7 of the rectifier. (See Fig. 1.)

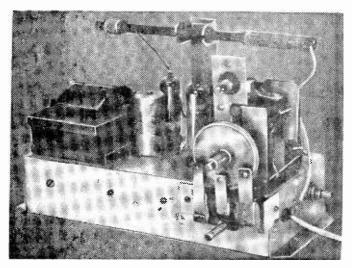
Smoothing is provided by R16 in conjunction with the electrolytic capacitors C17 and C18, while R10 and C13 provide a little extra for the anode of V3a. The value of R16 may need adjustment in some cases to produce the correct H.T. line voltage. The mains switch is incorporated with VR1.

Construction

The receiver is constructed on a chassis of 18s.w.g. aluminium sheet. 9in. x 4in. x 2in., details of which are given in Fig. 2. The layout is not critical. The grid circuit of V1 which includes the aerial, is the point where in-

stability is most easily introduced and care must be taken that it is not capacitively coupled to any of the later wiring. V1 and V2 must be screened. The trimmers TC1 and TC2 are mounted on

The trimmers TC1 and TC2 are mounted on top of the tuning capacitor, and if in this position they can "see" each other, a small screen should be erected between them. The pilot light is also



The complete receiver, less its cabinet

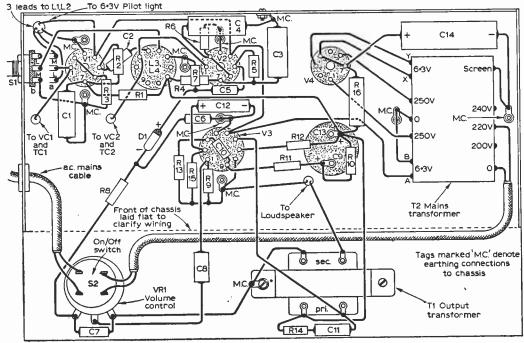


Fig. 3.-The underchassis wiring diagram.

mounted on top of the gang and to achieve a symmetrical appearance in the finished receiver, should be positioned so that its height above the tuning spindle is equal to the distance between that spindle and the spindle of VRI below. (To be continued)

LIST OF COMPONENTS Resistors (20%, $\frac{1}{2}$ W carbon unless otherwise stated): RI Ik Ω R9 IOM Ω R2 4.7kΩ RI0 **39**kΩ 220kΩ **R3 150**Ω RH R4 **R12** 3.9kΩ IkO. 470kΩ R5 **4**·7kΩ R13 **RI4 4·7k**Ω 150Ω R6 **RI5** 470Ω, IW **R7** 47kΩ lkΩ, IW **R**16 **R8** 47kΩ VRI 500k Ω carbon potentiometer with switch (S2) Capacitors: 0.1µF paper 350V 470pF ceramic or mica C2 0.1µF ceramic or mica C3 0.1µF ceramic or mica C4 C5 470pF ceramic or mica 220pF ceramic or mica C6 **C7** 220pF ceramic or mica 0.01µF paper 350V **C**8 8µF electrolytic 350V **C**9 C10 C11 0.01µF paper 350V 5,000pF paper 350V C12 50µF electrolytic 25V 16µF electrolytic 350V C13 16µF electrolytic 350V C14

VCI 500pF twin-gang air variable tuner TCI 100pF trimmer TC2 100pF trimmer Valves: **V**3 ECL82 EF91 ٧L V46X4 V2 EF91 Diode: GEX34 or similar **Pilot lamp:** LPI 6.3V 0.3A Transformers: TI Output 45:1 Tapped Primary. Secondaries: 250-0-250V 60-70mA; 6-3V 2A; T2 Mains 6-3V IA Loudspeaker: LS 3Ω; 7 x 4in. elliptical Switches: 2-pole, 3-way SI D.P.S.T. (see VRI) S2 Coils: LI, L2 Ferrite rod aerial, type FRA.2 L3, L4 Miniature dual range, iron dust cored Miscellaneous: Three B7G valveholders, one B9A valveholder. Screening cans for VI and V2. Material for chassis.





PRACTICAL WIRELESS

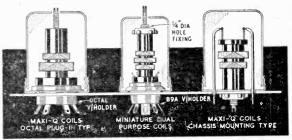
December, 1962

"THOUGH THE WORKING WEEK IS SHORTER WITH WAGES AND MATERIALS EVER MORE COSTLY"

 $\sim Q$ Thanks to you, our Customers who purchase in ever-increasing numbers, we are still able to offer the finest ever coils without increased prices.

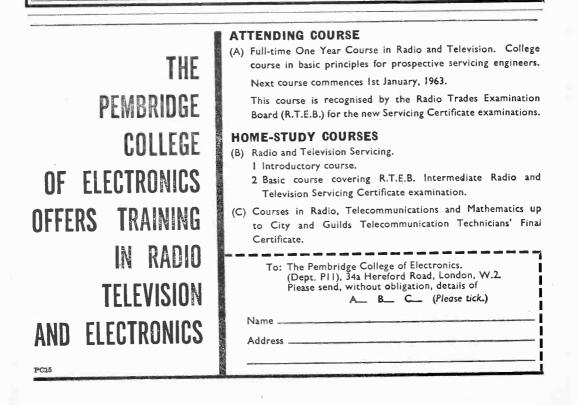
Coverage from 3.8 to 2,000 metres in 7 ranges—Each coil is packed in an aluminium container which may be used as a screening can for the coil itself—Brass threaded, adjustable iron cores—Colour coded moulded polystyrene formers—Chassis/Plug-in Technical Bulletin, DTB.1 1/6—Dual Purpose Technical Bulletin, DTB.4 1/6—Colour Code Identified Coils: BLUE Signal

Technical Bulletin, DTB.4 1/6--Colour Code Identified Coils: BLUE Signal Grid Coil with Aerial Coupling winding -YELLOW Signal Grid Coil with intervalve coupling winding--GREEN Grid Coil with reaction and coupling windings--RED Superhet Oscillator for I.F. of 465 Kc/s--WHITE Superhet Oscillator for 1.6 Mc/s. Prices range from 4/1 to 4/9 each. Five-Colour Glass Scale, Back Plate, Pointer, Pulleys and Cord for use with 315 pF tuning condensers. Coverage (1) 150-400 Kc/s.; (2) 530-1,600 Kc/s.; (3) 1.5-4 Mc/s.; (4) 4-12 Mc/s.; (5) 10-30 Mc/s.; Price 19/-.



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THE BERKELEY

(Continued from page 695)

method is applicable when using "Croid" joinery glue which does enable a slight adjustment to be made before setting. Impact adhesives are extremely powerful, but a great deal of accuracy is then needed when placing the sections together.

Loudspeaker Apertures

Cut out the two loudspeaker apertures in the front panel and drill the holes for the fixing screws. For the main unit, drill four 5/16in. diameter holes equally spaced on a 13in. diameter. The positions of the H.F. tweeter fixing screws are indicated on the Blueprint and a No. 10 drill (2BA clearance) should be used here. All screw holes should be countersunk on the outer surface of the panel, and enlarged on the inner surface to accommodate a box spanner; the locking nut must be flush with the panel surface, or slightly recessed, when the screw is locked in position as indicated in the inset on Fig. 1.

The removable inspection panel on one side has a $\frac{1}{4}$ in. rabbet all round. The top and bottom of the opening to take this panel will need a wood fillet glued and pinned on to make up a deficiency of $\frac{1}{4}$ in. The panel is held in place by a series of $\frac{1}{4}$ in. x No. 8 csk. screws. Provided the edges of the cover fit the opening closely it should be necessary to insert a layer of felt only on the flat of the rabbet.

The base plinth is quite simply made from 1in. x 2in. batten, screwed and glued to the cabinet as shown (see section C/C on Blueprint), the corners being mitred and pinned. A few glue blocks on the inside can be applied.

Glue a thicknessing piece to the insides of the top and bottom front edges to give a $\frac{1}{2}$ in. finish, which is afterwards veneering in conjunction with the top.

Clean up all the cabinet edges and fill in screw holes with plastic filler.

The top and bottom edges can now be veneered with the material selected. The edges should be carried right round the cabinet and form a slight projection to mask the edges of the "Vinyl" or "Fablon" covering on the sides. Should this method be adopted a slight adjustment is required to the inspection cover, which will be half an inch less in length.

Paint the whole of the interior and front, which will be covered by loudspeaker fabric, with flat black undercoating. Unless the front is treated in this way the loudspeaker apertures will be discernible through the fabric.

Fit the loudspeaker screws and secure with nuts as indicated in the inset on Fig. 1. The screws should be countersunk type and 14in. long. Use 4in. diameter screws for the main unit, and 2BA screws for the tweeter.

Make up the beading as shown in section A/Aand B/B on the Blueprint. The vertical lengths are rebated to cover the edges of the side members, but the horizontal length may be left solid.

Now stain and polish, if vencered, the top, edges and beads. The plinth looks well if ebonised.

All that remains now is to cover the sides with "Fablon" or similar material, wrapping this round the front edges, and then to apply the loudspeaker fabric. This material is glued around the edges only, to a depth of 3in. When it is set apply the beads and finish off the wooden surfaces with a final coat of polish.

A suitable loudspeaker covering is the synthetic material sold under the trade name of "Tygan", and is available in many patterns and shades. To obtain a taut surface, the "Tygan" should be shrunk by applying heat for a few seconds. This is most conveniently performed by holding an electric fire in front of the cabinet, about six inches away from the material. Watch carefully for signs of contraction, then immediately remove the fire.

Allow 24 hours for the glue to harden before carrying out this heat treatment.

THE LUXEMBOURG TUNER

(Continued from page 717)

another set is available (a transistor portable is ideal) is to tune the second set exactly to Luxembourg and then to beat the signal generator into it until it is precisely the same.

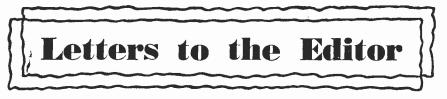
Without altering the signal generator setting go right through the alignment procedure detailed above and the tuner will then be spot on tune to the "Station of the Stars". It is suggested that during the alignment it is advisable to put a shorting link between the junction of C2 and C3 and chassis in order to cut out the AVC, otherwise this can make exact adjustments rather difficult. Do not forget to remove this link afterwards otherwise the AVC will be ineffective.

Alignment without Signal Generator

If you are having to tune up without a generator it will probably take a little longer as there must be a little trial and error adjustment to start with. If a really good aerial is available then this can be connected first to pin 1 of V2 and T3 adjusted until Luxembourg is heard, do not worry if it is not full strength or if other stations are butting in. Now transfer the aerial to pin 1 of V1 and adjust T2 and the station should emerge at full strength and with careful adjustment the unwanted stations can be eliminated.

Whichever method of alignment is used the final adjustment should always be made on the station itself with the tuner connected up to the actual aerial it is intended to use as this can have quite a marked effect on the tuning position of the two cores in T1.

Although the writer did not carry out experiments with other types of valve as more than enough signal was always available it is interesting to note that the EF91 valve which has considerably more gain has exactly the same base and connections and could possibly be substituted if desired although since this is not variable- μ the AVC circuit would not be effective.



HI-FI FANATIC

SIR,—I recently visited a home of an acquaintance of mine who has a fine collection of classical L.P. records and an elaborate hi-fi system, consisting of a separate amplifier, pre-amplifier, record player and loudspeakers. I'm not a great fan of the classics myself, but as he was so enthusiastic in explaining his equipment, I thought it only polite to ask to hear one of his records. This I did and it was obvious that he was delighted. He then told me to choose a record from his collection.

Simple enough, I thought, but it was at this point that I made my big mistake. In my enthusiasm to get the ordeal over with, I had taken both the inner and outer covers of the record off and was turning it over in my hands to choose the side I wanted, before my friend could stop me. The first I knew of my mistake was when my friend grabbed the record from me and started to inspect it closely for any marks or scratches. After a moment or so, it began to dawn on me what I had done. In my innocence I had placed my fingers over the groove!

After many apologies from me and reprimands from my friend, he agreed to go on with the performance. Inside another 20 minutes he had finished making adjustments to the pick-up arm, the tone controls, the loudspeaker positions, cleaning the stylus etc, and then, and only then, could we hear the record.

I have heard about these record fanatics but I never before really believed that anyone could be so concerned about the welfare of something costing only 30s. to £2, and I count myself lucky to be able to listen to my cheap record player without worrying about how much dust is collecting under the stylus. — D. R. DAVENPORT (Doncaster).

ELECTRONIC GAMES

SIR,—You recently asked to hear from readers who have had experience of electronic games. I have designed such a game recently which is played to test a person's ability to recognise aircraft. The unit will be on show at the Schoolboy's Exhibition at Olympia on the Royal Air Force stand.

It consists of 18 transparencies of different aircraft and parts of aircraft which flash on individually for time periods varying from five to twenty seconds (this was achieved by using a modified P.W. circuit). On the control panel there are 18 buttons with 18 captions by the side of them, and a scoreboard registering the number of aircraft the player has recognised correctly.

The operator gets a visual warning to tell him how long he has before the sequence begins.

The master timing circuit operates a uniselector having 25 circuits, out of which 18 are used for the selection of the transparencies. The other seven are used to return the score to zero, to operate a warning as to the time left before the sequence starts and also to tell the player whether he is average, good or excellent at recognising aircraft.

In this unit, I used 59 relays, 58 of which were normal GPO type 3.000 and the other was a highspeed, dual coil type. Twenty-eight of the 58 ordinary relays were needed in order that the score could operate automatically. Eighteen were used for the transparencies, and the others used for a bell and several "anti-fiddle" circuits.—CPL. EDWARDS (R.A.F. Hendon).

RECEPTION ON THE CONTINENT

SIR,—Early next year I am taking my holiday in France and I was wondering what success I could expect of receiving British programmes on my car radio. This year, when I stayed at a hotel in France, I greatly missed hearing the Home and Light programmes, as the hotel's radio was always tuned to Continental stations. I wonder if any of your readers could tell me what the quality of reception would be.—A. A. CHILTON (Cardiff).

R.1481 RECEIVER

SIR,—I have recently been given an old R.1481 receiver and would very much like to receive any details on the power supply and circuit of this set, from any reader who owns one.—C. SHINGSLEY (Burgess Hill, Sussex).

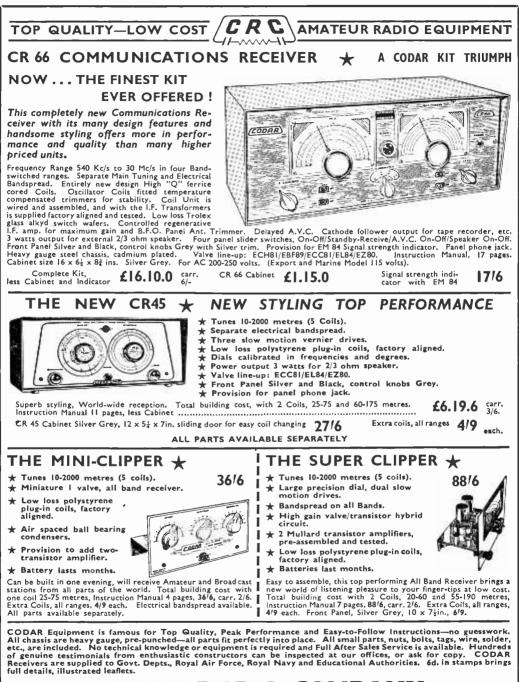
CORRECTIONS

THE TUDOR BATTERY SUPERHET. The 2-gang tuning capacitor VC1, VC2, should be Jackson type 02, not "type L" as stated in the Components List on page 437 of the September issue.

THE STRAND AMPLIFIER. There is a wiring error on the Blueprint enclosed in the October issue. The heater wire of V2 (ECC83) as shown in Figs. 1a and 2 must be amended as follows: Connect together pins 4 and 5. Connect the 6.3V supply to pin 4 (or 5) and to pin 9.

Also note that in Fig. 2 pins 2 and 7 of V1 should be shown connected to the valveholder spigot, as described in the article on page 507. THE TROUBADOUR. Transistor types should read: Trl OC44; Tr2 OC45; Tr3 OC45, and not as given in Fig. 1 and in the Components List of the Blueprint (June 1962 issue).

THE P.W. SIGNAL GENERATOR. The following amendment should be made to the Components List on the Blueprint (October 1962 issue): L4 QHF8, L5 QHF9.



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December, 1962





AMATEUR RADIO SOCIETY OF CHESHAM AND DISTRICT

Hon. Sec.: Capt. C. G. Stephenson, G3CL J/T, 21 Lynton Road, Chesham, Buckinghamshire.

At the moment, many of the society's members are spending their time improving their headquarters. However, morse and practical classes continue to be held each Tuesday, and on Fridays, RAE lectures are given.

CLIFTON AMATEUR RADIO SOCIETY

Hon. Sec.: C. Godsmark, G3IWL, 211 Manwood Road, London, S.E.4.

At the society's recent AGM, W. Martin was elected chairman, C. Godsmark secretary and N. Moore treasurer. On October 5th, G3HWG gave a lecture on "Oscilloscopes" and

also demonstrated some of their uses.

DERBY AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: F. C. Ward, G2CVV, 5 Uplands Avenue, Littleover, Derby.

A surplus sale was held on the first meeting in October and on 10th, "Technical Forum" was the topic for the evening. On October 17th members enjoyed a film show and on November

3rd a number of members visited the R.S.G.B.'s exhibition in London.

DUDLEY AMATEUR RADIO CLUB

Hon. Sec.: D. H. W. Pratt, G3MHS, 23 Kent Street, Upper Gornal, Dudley, Worcestershire.

The Annual General Meeting of this Club was held on October 12th. On 26th of the same month members attended a demonstra-tion and talk by the Wolverhampton Model Radio Control Society.

LOTHIANS RADIO SOCIETY

Hon. Sec.: G. Ritchie, c/o Cormie, 15 Rosslyn Terrace, Edinburgh 6.

'Monkey Glands for the HRO'' was the title of the talk given on October 11th by GM3PQU, who also gave a demonstration of TVI proofing. Visitors from the South Lanark, Fife and Falkirk groups who attended the meeting on October 25th, were entertained with a film show.

Future Events:

November 8th-"Some Aspects of Transistors" by Dr. C. Davidson.

November 22nd-A surplus sale.

MITCHAM AND DISTRICT RADIO SOCIETY

Hon. Sec.: M. Pharaoh, G3LCH, I Madeira Road, Mitcham. A talk on R.F. heating and its uses was given by B. Ayrlwood at the meeting on October 5th and at the following meeting on 19th, VQ4EV presented a film show.

Future Event:

November 16th—"Why be Afraid of Transistors?" by G8TB.

MELTON MOWBRAY AMATEUR RADIO SOCIETY

Hon. Soc.: D. W. Lilet, G3FDF, 23 Melton Road, Asfordby Hill, Melton Mowbray, Leicestershire.

At the meeting on October 18th members listened to a recorded lecture on transmitter design and TVI by N. Shires,

NORTHERN HEIGHTS AMATEUR RADIO SOCIETY

Hon. Sec.: A. Bobinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.

Members operated a station during this year's Scout Jamboree on the Air, under the call-sign G3MVH. On October 23rd, members travelled to Bradford to attend the film show given at St. George's Hall.

For the first meeting in November, G3FQH gave a lecture on single side band.

SHEFFIELD AMATEUR RADIO CLUB

Hon. Sec.: D. R. A. Hill, 16 Tylney Road, Sheffield 2, Yorkshire.

The energy of many members at the moment is being expended on the task of furnishing the club's headquarters. The all-band transmitter and aerials also claim important places in the club's present programme.

In spite of all this work, many members are continuing to attend both the technical and general meetings and the novices classes are carrying on successfully with morse classes held on alternate Wednesdays.

REPORTS OF CURRENT ACTIVITIES

SLADE RADIO SOCIETY

Hon. Sec.: C. N. Smart, 110 Woolmore Road, Erdington, Birmingham 23.

On October 19th, the club secretary gave a comprehensive lecture on a new transistorised D.F. receiver, and on 31st of that month members attended the Annual Dinner.

SPEN VALLEY AMATEUR RADIO SOCIETY

Hon. Sec.: L. A. Metcalfe, IA Moorlands Road, Birkenshaw, Bradford, Yorkshire.

October proved to be a busy month for this society, starting with a talk called "Language of S.S.B." on 4th. A lecture called "Noise Problems" was given on 18th and later in the month members attended a film show.

The first meeting in November was devoted to "Tape Recorders".

STRATFORD-UPON-AVON AND DISTRICT AMATEUR RADIO CLUB

Hon. Sec.: P. Robinson, G3MGJ, 43 Loxley Road, Stratford-upon-Avon, Warwickshire. To meet the May 1963 R.A.E., a series of lectures has been started

dealing with radio theory.

The lectures for the two last meetings have been given by John Hewitt, G3MDU, and his subjects included alternating current and voltage, aljeenating current with inductance, etc.

Future Event: November 9th—Coupled circuits, acceptors and rejector circuits, by M. Webb.

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December, 1962

ABSORPTION WATTMETER

(Continued from page 719)

tiometer, but a reversing switch *must* be included and a reading obtained with the voltage applied to the wattmeter both "forward and reverse". The average of these is the "correct" meter reading. (This procedure takes account of differences in diode forward resistance.)

The voltage developed across 3 and 15Ω resistors for the 5 and 20W ranges have been calculated and are given in Table I. The first step in the calibration process is to set the variable resistor controlling linearity (VR5). Having adjusted VR5 for zero resistance, set the D.C. voltage applied to the wattmeter to 8.66 volts. Switch the wattmeter to measure 5W at 152 and adjust VR3 until the meter reads full scale. Then reduce the D.C. voltage to 7.75 volts and note wattmeter reading, and so on down column 5 of Table 1. When the jinearity control is correctly adjusted, the results obtained should be similar to those given in Table 2. If the readings obtained are lower than these, set RV5 (linearity) to its mid-position and readjust RV3. Repeat the comparison of meter readings and applied voltage.

If the readings are still low then RV5 must be further increased, whilst if the readings are high, RV5 must be reduced in value. This procedure may sound complex but in practice it takes but about 10 minutes.

When the linearity control has been set, the table of applied voltage against meter reading should be put to one side as this is required for absolute calibration of the meter. This may be

Table 2

Voltage	Meter Reading
8·66	I
7·75	0-81
6·7	0-61
5-5	0-40
3-87	0-19
2-74	0-09
0	0

done by drawing a calibration curve or alternatively, the scale can be removed from the meter and re-calibrated by hand. This latter method is preferable, but can result in a very "messy" looking job if great care is not taken.

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Т	а	b	le	- 3

7.5Ω					
Voltage	Power	Voltage	Power		
6.12	5	12.25	20		
5.5	4	10.95	16		
4.74	3	9.5	12		
3.87	2	7.75	8		
2.74	4	5.48	4		
1.94	0.5	3.87	2		

COMPONENTS LIST

R† RIA R2	$ \left. \begin{array}{c} 3\Omega \\ 47\Omega \\ 15\Omega \end{array} \right\} $ See text for power rating $ 1$	g
R3 R4 R5 R6	$ \left. \begin{array}{c} 150\Omega\\ 330\Omega\\ 330\Omega\\ 820\Omega \end{array} \right\} 20\%, \frac{1}{4} W \text{ carbon} $	
VR1-4	100 Ω wire-wound potentiometers	;
VR5	250 Ω wire-wound potentiometer	
MRI-4	OA70 (Mullard)	
MI	Meter, moving coil, 0—1 mA f.s.d	
SWI	Switch 3-pole, 2-way	
SW2	Switch 4-pole, 2-way	

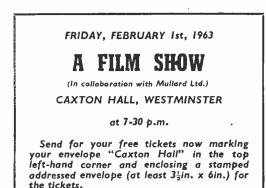
The only job remaining now is to set the remaining range potentiometers as follows:

- 1 Set the meter to measure 5W at 3Ω , apply a voltage of 3.87 volts and adjust RV1 for full scale deflection.
- 2 Sct the meter to measure 20W at 3Ω , apply a voltage of 7.75 volts and adjust RV2 for full scale deflection.
- 3 Set the meter to measure 20W at 15Ω , apply a voltage of 17.32 volts and adjust RV4 for full scale deflection.

The lead to SW1A should now be reconnected and the wattmeter is completed.

Additional Ranges

If additional or alternative ranges are required it is quite simple to add or substitute these. In Table 3 are given voltages appropriate to 5 and 20W ranges for 7.5Ω load.



The films to be shown will include "Fuel for the Future" and "The Electroneers", and as in previous years, the programme has been arranged to appeal to all who are interested in radio.

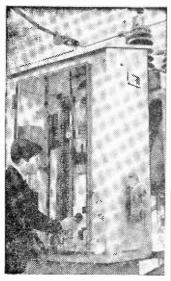
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Q. Where do I go from here?

A. It's impossible to tell you here all about an industry that has to double its output every ten years. But jobs include everything from running a Power Station to bringing power to a new estate. For full details, write (giving age and exams you've passed) to: The Education and Training Officer, The Electricity Council, 155 Winsley Street, London, W.1.

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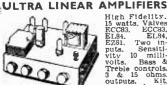
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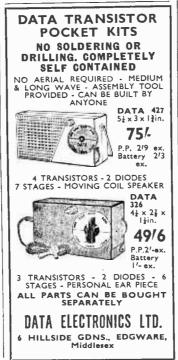
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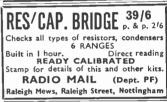


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