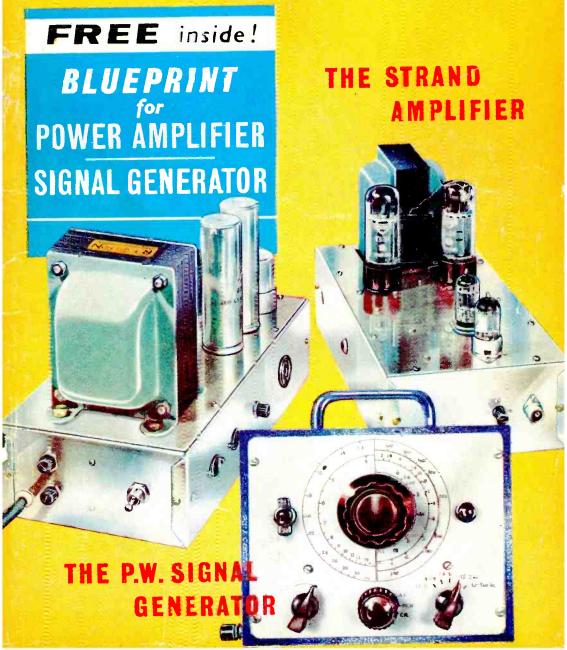
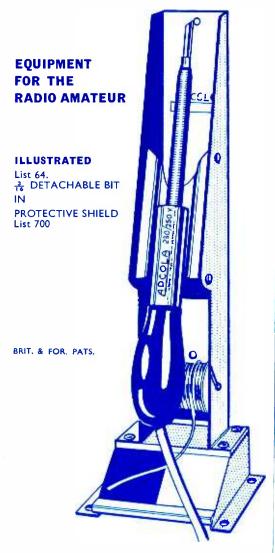
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SUITARLEFOR ALL
BATTERY RECEIComplete kit of parts with diagrams and
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TRANSISTOR RADIO CHARGER/ELIMINATOR UNITS. Ready for use, fifted "Snap On" clips. When connected to 200-250v. A.C. mains will charge 8 v. battery or replace same. PP3 Size 19/9. Larrer size 29/9.

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	SELE	NIUM	RECTIFIERS	
F.W.	BRIDGE		24 v. 2 a	14/9
6/12 v. 1 a.		3/11		00 11 111
6/12 v. 2 a.		6/11	H.T. TYP	
6/12 v. 3 a.		9/9	150 v. 40 mA	3/9
6/12 v. 4 a.		12/3	250 v. 50 mA	3/11
6 12 v. 6 a.		15/3	250 v. 60 m A	4/11
6/12 v. 10 a.		25/9	250 v. 80 mA	5/11
6/12 v 15 a		35/9	250 v. 250 mA	11/9
CONTACT C	COOLED, 28	60 v. 75	mA, F.W. (Bridge),	10/11. 250 v.
50 mA. F.W.	(Bridge) 8/1	 H.W 	. 250 v. 60 mA	5/11

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Components price list and plans, 21-.



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- ★ 250 Milliwatts output stage.
- ★ Can be built for 59/6 P.P. 3/-, or with 3in. speaker 68/-
 - ★ PARTS PRICE LIST, etc. 2/-.

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SPECIAL OFFER!

6 Watt Push-Pull Amplifier

2 ECL82 metal rec., separate bass and treble cont. on aux. panel. Made for one of the largest manufacturers of record players. Used in 30 gn. unit. Size 7 x 4in. panel, 6 x 1½in. 3 ohm output, trans. included.

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TAPE DECKS B.S.R. Monardeck

(Single speed) 3½m. per sec., simple control, uses 5½m. spools, £6.15.0, plus 5/6 carr. and ins. (Tapes extra.)

COLLARO STUDIO DECK £10.10.0, plus 5/6 carr. and ins. (Tapes extra).

10/14 WATT HI-FI AMPLIFIER KIT



stylishly finished monaural ampli-The strict of the strict of th and announcements to follow each other. Fully shrouded ultra output transformer (to match 3-15 speaker) and 2 independent volume controls, and separate bass and treble controls are provided giving good lift and cut. Valve line-up 2 EL84s, ECC83, EF86 Valve line-up 2 EL84s, ECC83, EF86 and EZ80 rectifier. (Simple instruction booklet 1/6, free with kit).

ONLY £6.19.6 P. & P. 616.

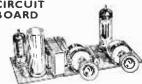
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All 3 ohm impedance.	
2½in.	12/6
5in	12/6
61in.	15/-
12in	27/6
Goodmans 5in. tweeter	10/6
E.M.I. 2†in. tweeter	10/6
Goodmans 8in. x 5in. middle regis-	
ter speaker	10/6
E.M.I. 134in. x 84in. high flux	32/6
Rola Celestion, approx. 9in. x 6in.	
middle register speaker	10/6

P. & P. 1/6 per Speaker.

OC72

AMPLIFIER ON PRINTED CIRCUIT BOARD



Two valve. UY85, UL84 with O.P. trans., use with 80 volt tap off motor. ve. UY85, UCL82, 3 wa.ts O.P. trans. Two valve.

output. O.P. trans., use as above, 49'6. P.P. 2'6 on above. Dropper res. for filaments if required, 2'6.

B.S.R. AUTO UNITS 160 v. Suitable for use with above. (Slightly soiled.) £5.5.0. P. & P. 5/-,

LARGE CABINET

Suitable for above two items. Complete with 3



ohm spaaker. £3.9.6. Carr. 5/-.

Superior Cabinet. Similar to above to take 8 x Sin. speaker, with motor board, will accommodate BSR UA14 or UA16. £3.9.6. Carr. 5/6. Speaker 15/- extra. P. & P. 1/6 extra.

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(Ex equip.), 200-240 v. input. Output 12 v. I amp., tapped I, 8 and 10 v. Ideal for model railways and chargers. 8/6, P.P. 2/-.

Colvern Wire Wound Potentio-meters. 3in. 10 ohm I amp. Suitable for above. 5'-. P. & P. 1'-.

LARGE WODEN MAINS **TRANSFORMER**

220/240 v. input. Output 40 v. at 3 amps. 260 v. clso 90 v. 100 mA. size 44 x 5 x tapped 30 v. clso 90 v. 100 mA. by 260 v. clso 90 v. 100 mA. 250 v. 250 v. 260 v. clso 90 v. 100 mA. 350 v. 260 v. clso 90 v. 100 mA. 350 v. 260 v. 260 v. 270 mA. 350 v. 270 v. 270 mA. 350 v. 270 v. 270 mA. 350 v. 270 P. & P. 5/-.

TRANSISTORS All Post Free.

GET15 (Matched Pair), 151-, OC71 51-2 61- OC76 61- OC34 91-101 616 XA103 616 V15/10p 12/6 OC72 ____ 6/-PXAI0I 6/6 Set of Mullard 6 transistors 25/-. Set of G.E.C. 1,874; 2.873; 3, SI or GET114 20/-.

6 TRANSISTOR AND DIODE SUPERHET

A first class 2 waveband transistor superhet in kit form. Printed circuit panel (size $8\frac{1}{6} \times 2\frac{3}{6}$ in.) pre-aligned. transformers.
High-gain Ferrite rod aerial. 🔴 First-grade G.E.C. transistors. Car aerial winding. Push-pull output. All parts down to the minutest item with simple instructions.

ONLY £4.5.0 P. & P.

35 ohm speaker, 10/6; 3½ in. 35 ohms speaker 16/6; 35 ohm Sin. P.M. 18/6; 7 × 4in. 35 ohms speaker 21/-. P. & P. 1/6 per speaker.



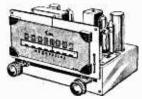
PORTABLE CABINET

Size approx. $9\frac{1}{2} \times 6\frac{3}{4} \times 3\frac{1}{2}$ in. Suitable for above using $3\frac{1}{4}$ in. speaker. 25^{\prime} -. P. & P. 2^{\prime} -.

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3 I.F. transformers, one oscillator coil, one driver transformer and wound Ferrite aerial (med., long and aerial coupling), 28/6 complete, post 1/1. 6 transistor printed circuit, board to match, 8/6, post 9d. Circuit diagram 1/6 extra.

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Frequency coverage 88-100 mc/s. OA81 balanced diode output. @ Two I.F. stages and discrimator. Attractive maroon and gold dial (7 x 3in. glass). Self powered, using a good quality mains transformer and valve rectifier. • Valvas used ECC85, two EF80s, and EZ80 (rectifier). • Fully drilled chassis. Size of completed tuner 8 x 6 x 5\fmathre{\pm}\in. All parts sold separately. £5.19.6, plus 8/6 P.P. and ins. Circuit diagram and illustrations 1'6 P. free.

As above but complete with magic eye, front panel and brackets. £6.12.6. P. & P. 8/6.

As above but with output stage (ECL82) and tone control. £7.7.0. P. & P. 8/6.

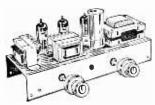
Handsome Metal Cabinets. Choice of Grey, Black or Green. 17/6 extra.

HARVERSON SURPLUS CO. LTD.

RECORD PLAYER AMPLIFIER

- ★ 2 watt output.
- Ready built with valves and 61in. speaker, tone and volume controis. Mounted on panel 13 x 71. 75/-. P. & P. 2/-.

STEREO AMPLIFIER Bargain Offer



- * 4 watts per channel.
- * Full tone and volume controls.
- * Complete with sockets, etc.

89/6 P. & P. 2/6.

QUALITY RECORD PLAYER AMPLIFIER

A top-quality record player amplifier. This amplifier (which is used in a 29gn. record player) employs ECC83, EL84, EZ80 valves. Bass, treble and volume. On/off controls.

PRICE 69/6 P. & P. 3/6.

DITTO. Mounted on board with output transformer and 6½ in. Complete at 89/6 speaker. P. & P. 4/6.

4-SPEED PLAYER UNIT BARGAINS

SINGLE PLAYERS

Garrard TA Mk. 2, £7.15.0. B.S.R. TU/12, £3.15.0. Carr. 3/6 on each.

AUTO CHANGERS

B.S.R. UA14, £6.19.6. Latest B.S.R. UA16. £7.19.6. Latest Garrard "Auto-Slim," £7.15.0. Latest Garrard "Auto-Slim" de luxe, £11.9.6.

Carr. 5/- on each.

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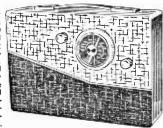
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6 TRANSISTOR AND TWO DIODES RECEIVER

Easy to build, using 6 super transistors and 2 diodes 750 M/W output, full medium and long wave coverage, prin-ted circuit, 5in. ted circuit, speaker, prealigned IFTS & OSC. Very fine tuning, ferrite aerial with car aerial socket, attractive 2-colour cabinet. Simple to follow instructions with circuit. everything complete

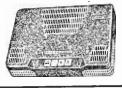


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THIS MONTH'S BARGAIN!

TELEFUNKEN STEREO AMPLIFIER LATEST MODEL S82. 110/250 v. A.C. input. 5 watt undistorted output (10 watts nominal). Size 12 x 9 x 2in. Weight 9 lb. Complete with spec, and instructions.

£6.19.6 Carr. 5/-.



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MIDGET 2 GANG CONDENSERS. Capacity 195 and 100 PF. Polystyrene case with built in trimmers. Size $\frac{1}{4} \times \frac{1}{4} \times \frac{1}{4}$ in. Not used but removed from P/C Boards. 2 for 9/-. Plus 1/- P. & P.

ACOS CRYSTAL MIKES. Hi-imp., 18'6. P. & P. 1'6. 4 MFD MANSBRIDGE PAPER CONDENSERS. Ideal for Crossover Units. 4/6 each. P. & P. 1/-.

TRANSISTOR DRIVER and O/P TRANSFORMERS. (Tapped 3 ohms and 15 ohm o/p), plus 4 suitable Transistors giving approx. I watt o/p. 30/-. P. & P. 2/-.

MAINS TRANSFORMERS

Tapped Primary. ½ wave or Bridge Rectifier. Secondary 250 v. at 75 m/a 6.3 volts at 2 amps. 7/6 each. P. & P. 3/-.

3 PUSH-BUTTON TRANSISTOR SWITCH. D.P.-D.T. Each Switch 5/6 plus I'- P. & P.

FOR PERSONAL CALLERS ONLY.

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From £3.3.0 each.

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permeability tune... head by a maker, sup-valve tuner famous without (ECC85) (ECC85) and drum and spindle, 18/6, plus 1/9 P. & P. Valve 8/6 1/9 P. & P. Val extra. Drum spindle 3/6 extra.

E.M.I. 4-speed Player and P.U.



83in. Heavy 83 in. metal turntable. Low flutter metal 200/250V performance shaded motor with tap at 80V for ampli-fier valve filament if required. Turnover LP/78 head.

> PRICE 7916 Plus 4/6 P. & P.

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E.M.I. 4-speed. battery operated Record Player Unit. Mounted on unit plate. Complete with turnover head and sapphire stylii.

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METAL RECTIFIERS. DRM1B 13/-, DRM2B and DRMSB 15/6. LW7 21/-, LW15 26/-, RM0 7/11. RM1 5/3. RM2 7/6. RM3 7/9. RM3 14/-, RM5 19/6. 14/86 17/6. 14/87 25/-, 14/86 27

Terms of business:—Cash with order or C.O.D. only. Post fid. per item except where stated. Orders over £3 post free. C.O.D. 2/6 extra. All orders cleared same day. C.O.D. orders by telephone for immediate despatch accepted until 3.39 p.m. We are open for personal shoppers 8.30—5.30 p.m. Sats. 3—1 p.m. Complete list of valves, resistors, condensers, transformers etc. 6d. Please enquire for any item not listed with S.A.E.

esigned by MULLARD-presented by STERN'S strictly to specification

MULLARD "5-10" MAIN AMPLIFIER

For use with the MULLARD 2-valve pre-amplifier with which undistorted power output of up to 10 watts is obtained. We supply SPECHFED COMPONENTS AND NEW MULLARD VALVES, including PARMEKO MAINS TRANSFORMER and choice of the latest Ultra-Linear PARMEKO or the PARTRIDGE Output Transformer.

COMPLETE KIT OF PARTS £10.0.0

Alternatively we supply \$11.10.0 INCORPORATING PARTRIDGE OUTPUT ASSEMBLED and TESTED.

MULLARD'S PREAMPLIFIER TONE CONTROL UNIT

Employing two EF86 valves, and designed to operate with the MULLARD WAIN AMPLIFIERS, but also per-fectly suitable for other makes. PRICE COMPLETE \$6.6.0 ASSEMBLED AND TE

RICE COMPLETE \$6.6.0 ASSEMBLED AND TESTED \$8.0.0
IT OF PARTS
Supplied strictly to MULLARD'S SPECIFICATION and incorporating:
Equalisation for the latest R.I.A.A. characteristics.
Input for Crystal Pick-ubs, and variable reductance magnetic types.
Input (a) Direct from High Imb. Tape Head. (b) From a Tape Amplifier or Pre-Amplifier.
Sensitive Microphone Channel. Wide range BASS and TREBLE Controls. KIT OF PARTS

THE MULLARD "510/RC" AMPLIFIER

The popular and very successful complete "5-10" incorporating Control Unit providing up to 10 watts high quality reproduction. Only Specified Components and new MULLARD VALVES are supplied including PARMEKO MAINS TRANSFORMERS and choice of the latest PARMEKO or PARTRIDGE ULTRA-Linear Output Transformers. KIT OF \$211.10.0 OR ASSEMBLED \$13.10.0 PARTS \$11.10.0 OR ASSEMBLED \$13.10.0 ABOVE incorporating PARTRIDGE OUTPUT TRANS. \$1.6.0 extra.

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THE IDEAL AMPLIFIER FOR A SMALL HIGH QUALITY INSTALLATION PROVIDING EXCELLENT REPRODUCTION OF UP to 3 WATTS OUTPUT COMPLETE KIT \$7.10.0 OR ASSEMBLED \$8.19.6 CUMPLETE KIT **£7.10.0** OR ASSEMBLED **£8.19.6** (plus 6% carriage and insurance) H.P. Terms: Deposit £2.0.0 and 5 months at £1.0.0. Complete to MULLARD'S SPECIFICATION including Mullard valves and a PARMEKO OUTPUT TRANSFORMER.

STERN'S INTER-COMM BABY ALARM

A small versatile Unit employing the new MULLARD ECL86 valve and designed to provide two (or three) way conversation up to extreme distances, Operates from A.C. mains 200 to 250 Volts.

PRICES . MANTER UNIT and ONE EXTENSION

KIT OF PARTS £6.17.6 ASSEMBLED AND TESTED £8.8.0 KIT OF PARTS \$0.17.0 ASSEMBLED AND TESTAMONE CONSISTS of a MASTER UNIT, size only 81 x 51 x 61n, and ONE EXTENSION (a second extension may be added to any time). The Master Unit incorporates switching and power supply and with the chassis completely isolated from the mains is operated in absolute safety. Cases covered in quality leatherette.

THE "MONO GRAM" AMPLIFIER

A small Amplifier capable of genuine high quality performance. It incorporates the new Mullard ECL86 Valve, separate BASS and TREBLE CONTROLS and when driven by the standard Crystal Pick Up a power output of 3 watts is achieved without distortion. Up a power output of 3 watts is achieved with PRICE. READY FOR USE £4.19.6

carr. & ins. 5/-The "MONO-GRAM" is ideally suited to incorporate in Portable Record Player and an attractive Portable Case is now under design, this will accommodate the AMPLIFIER with a ROLA 8" x5", pitch 21.00. and has room for one of the modern PLAYER UNITS. Constructors (an Build a Really First-Class Record Player, Complete in all respects, for approx. £14. This will compare with known Record Players currently offered at much higher prices.

A SPECIAL PURCHASE ENABLES US TO OFFER THE "TUDOR" STEREO AMPLIFIER FOR £18.18.0

Deposit \$4.0.0. 12 months £1.9.4.
A self contained Amplifier designed to provide high quality stereophonic and monophonic reproduction. Each channel provides a rated output of 6 watts and for monophonic operation approx. 12 watts is produced. Separate BASS and TREBLE CONTROLS. DESCRIPTIVE LEAFLET IS AVAILABLE.



£1.6.0 extra.

RECORD PLAYERS

Each Unit is available with Stereo Cartridge fitted.

THE NEW GARRARD "AUTO-SLIM" 4-speed Autochanger with Crystal Pick-up.... \$8.10.0

PHILIPS MODEL AGIOIG... A 4-speed Player which can be operated both manually and automatically. Suitable or Mono or Stereo opera- £13.13.0 tion

GARRARD "AUTO-SLIM DE-LUXE" 4-speed Auto changer incor-porates transcription Pick \$12.14.6

top Arm Collaro Cylinor, 4 SPEED SINGLE RECORD PLAY- \$3.15.0 Pick-up. Carriage and Insurance 5/2. Above Pick-up separately for £1.6.6.

The NEW COLLARO
Autochanger unit with
Studio "O" Pick-up....
R.S.R. MODEL CAH,
mixer Autochanger with
Cr. stal Pick-up.... £7.19.6 4-speed

GARRARD MODEL, TA/Mk.II 4speed Player fitted high
\$8.10.0 output Crystal Pick-up... Carriage and Insurance on each above 5/- extrc.

SPECIAL CASH OFFER

together with a good quality GRAM AMP-LIFIER and a matched P.M. SPEAKER ALL lier ONLY 28.7.6 (Plus 76 Carr.) The Amplifier constitution of the co

The Amplifier consists of a 2-stage design incurporating 3 modern B.V.A. valves and has separate BASS and TREBLE CONTROLS.
The Portable Case will also accommodate almost any make of Autochanger and is attractively unished in Mushroom Grey Rexine.
WE ALSO SUPPLY SEPARATELY—

44.2.6
(a) The 2-stage (plus Rectnier) AMPLIFIER \$3.17.6
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with Cathode powered tollower output. Incorporates Two inputs for MICROPHONES One for CRYSTAL PICK UP and a fourth for RADIO or TAPE. £8.8.0 €

Complete Kit of Parts £10.0.0 Assembled and Tested

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TRANSISTOR BATTERY OPERATED INTERCOM

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89/6 P. & P. 4/+.

Including PP3 battery and 25 yards lead with plugs. A completely Portable intercom with 101 uses being ideally suitable for the office or even as a Baby Alarm, since being battery operated, it is completely safe. Two-way calling system and volume on/off switch, the units are housed in attrative plastic cabinets (black/white) with chrome stands, it is extremely economical operating on one 4-volt battery, replacement price being 2/8.

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Stereophonic Sound by Stern's

THE "STP-1" STEREO TAPE PRE-AMPLIFIER

BRENELL MK. V TAPE DECK INCORPORATED IN TRACK MINIFILUX TAPE HRADE.

PUSH PULL OSCILLATOR CHROIF

4-SPOND EQUALISATION
FERROXCUBE OSCILLATOR TRANSFORMER
SENSITIVE METER FOR SIGNAL LEVEL
SEPARATE GAIN CONTROLS IN EACH CHANNEL
MULLARD VALVES INCORPORATED
(A) The BRENELL MK. V ATRACK DEC.

COMBINED PRICE SCHEDULE

(a) The BRENELL Mk. V 1-TRACK DECK with the complete KIT to build the STP-1.

Deposit 212.4.0, 12 months of 24.0.6.
(b) The COLLARO "STUDIO" 1-TRACK DECK with the complete KIT to build the STP-1.

Deposit 27.18.0. 12 months of £2.17.3.

£61.0.0

£39.0.0

(a) The BRENELL Mk. V I-TRACK DECK with the Assembled STP-1 and matched to the Deck. Deposit £13.8.0. 12 months of £4.18.3. (b) The COLLARO "STUDIO" +TRACK DECK with the STP-1 Assembled and matched to the Deck. Deposit £9.0.0. 12 months of £3.6.0.

DESIGNED TO OPERATE WITH

COLLAID "STUDIO" 1A incorporating the latest REUTER TAPE HEADS. A APE DECK

OVERALL SIZE CASE 131 x 3in. FRONT PANEL (choice of Black or White) 14 x 34in.

PRICES . . . INCLUDES SEPARATE POWER SUPPLY UNITS

Kit of Parts £22.0.0 Deposit £4.8.0. 12 months of £1.12.3 Assembled £28.0.0 Deposit £5.1f..0. 12 and Tested £28.1.1.

> £67.0.0 £45.0.0

STEREOPHONIC RECORD PLAYER UNITS ARE AVAILABLE FROM STOCK

MULLARDS "10 PLUS 10"

STEREO AMPLIFIER

A high fidelity design based on the famous Mullard "5-10". Provides up to 10 watts (per channel) Superb reproduction. Frequency response flat to within 3 do from c/s. to 60 Kc/s at 50 Mw. Total Harmonic Distortion at 10 watts 0.1%



Total Harmonic Distortion at 10 watts 0.1%.

(a) ASSEMBLED COMPLETE AMPLIFIER. including CONTROL UNIT (as Illustrated).
Deposit \$4.4.0, 12 months at \$2.10.10.
Deposit \$3.14.0, 12 months at \$2.10.10.
We also supply the assembled MAIN AMPLIFIER only (excludes control unit) for operation with our DUAL CHANNEL PRE-AMPLIFIER, this provides for a more versatile or elaborate installation and would be essential if a low output Magnetic Pick-Up, such as the Deco, is to be used.

(a) THE ASSEMBLED MAIN AMPLIFIER with the ASSEMBLED DUAL CHANNEL PRE-AMPLIFIER.

Deposit \$6.0.0, 12 months at \$2.4.0, \$30.0.0

(b) A complete KIT of PARTS for both Unit....
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Illustrated and Descriptive Brochure available. Please choice S.A.E.

ARMSTRONG RADIOGRAM CHASSIS FULL RANGE IN STOCK. please enclose S.A.E. for leaflets. STEREO 12 Mk. 2 £43.10.0

(ILLUSTRATED)

Deposit £8.14.0, 12 months



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A Hi-Fi mono chassis giving eight watts push-pull output and covering VHF, medium and long bands. Tape recording and play back imputs.

AF238 £22.18.0

AF208 £22.18.0

An AM/FM chassis providing 5 watts output and covering the full VHF and medium wavebands, Tape recording and playback inputs.

TVB L HF TUNER £21.18.0

A self-powered high-fidelity tuner of outstanding design, incorporating features wint h are normally found only in the most expensive tuners. The full VHF band (87-108 M/cs) is covered and a matching output control enables the output to be varied between 0 and 500 mV.

"HI-FI" LOUDSPEAKERS WE HAVE IN STOCK A COMPLETE RANGE BY GOODMANS—WHARFEDALE—W.B. ILLUSTRATED AND PRICE LEAFLETS ON REQUEST.

THE MULLARD "10 + 10" AMPLIFIER (described below) with the "STP-1" PRE-AMPLIFIER and one of the TAPE DECKS provide a complete STEREOPHONIC INSTALLATION. Details are readily available. DUAL CHANNEL PRE-AMPLIFIER

Incorporates two Mullard 2-valve Incorporates two Mullard 2-valve
Pre-amplifiers combined into a
Single unit enabling it to be used
for both STEREOPHONIC or
MONAURAL operation. It is designed primarily to operate with
our range of MULLARD MAIN
AMPLIFIERS but will also operate equally well with any make of Amplifiers requiring an input of 250 myolos.
COMPLETE KIT £12.10.0

AS
OF PARTS



ASSEMBLED **£15.0.0**H.P. £3.0.0 & 12 mths. at £1...0 H.P. £2.10.0 & 12 mths. at 18/4.

STEREO "TWIN THREE" **AMPLIFIER**

STEREO "TWIN IHREE" AMPLIFIER
OFFERED ASSEMBLED and
TESTED for
(Carr. & Ins., 7/6
extra).
Based on a recent design by
MULLARD LTD., the "TWIN
THREE" is ideally suited for use
in PORTABLE RECORD PLAYERS for which purpose we offer
a specially designed Portable
Case. It incorporates MULLARD ECL86 valves, separate BASS
and TREBLE CONTROLS, and produces excellent reproduction
of up to 3 watts per channel. Frequency response is 40 c/s to 30
Kc/s. Sizel sonly lify 3x 5/in.
To construct a STEREO PORTABLE RECORD PLAYER
WE OFFER: The assembled AMPLIFIER with two ROLA 8 x 5/in.
LOUDSPEAKERS and the PORTABLE CASE for
(Carr. & Ins., 10/- extra). Deposit £2.16.0.12 months

CHURALLE RECORD BLAYERS are AVALLABLE

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SUITABLE RECORD PLAYERS are AVAILABLE FROM
An alternative "TWIN THREE" can be supplied for DUAL CHANNEL MONOPHONIC operation producing output of 6 watts.



"The TUDOR" AM/FM TUNING UNIT

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MAIL ORDERS and all POSTAL ENQUIRIES to



A very high quality Amplifier incorporating 3-speed trebla

A very high quanty Ampline incorporating 3-speed trebly equalsation, by the latest FEROXCUBE POT CORE INDUCTOR, FOR COLLAROTR UV OX - B R E N E L L WEARITE Tape Decks. has GILESN Output Transformer. Includes separate

(b)

BUILD A HIGH QUALITY TAPE RECORDER LIKE THIS FOR

CARR, and INS. 10/- extra

FOR THIS WE SUPPLY.....

Deposit 27.0.0 and 12 months at £2.11.4 Complete Kit of Parts to Build : The Latest Collaro "Studio" * Portable Carrying Case (as the HF/TR3 Tape Amplifier. * Rola/Celestion 10 x 61n. p.m. * ACOS Crystal Microphone and Loudspeaker. * Loudspeaker. * Loudspeaker.

ALTERNATIVELY WE SUPPLY THE COMPLETELY ASSEMBLED £39.10.0 and GUARANTEED TAPE RECORDER FOR
H.P. Terms: Deposit £7.18.0 and 12 months of £2.17.11.

HF/TR3MKII TAPE AMPLIFIER (Mullaro Type



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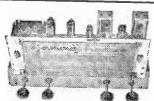
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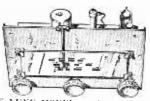
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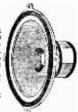
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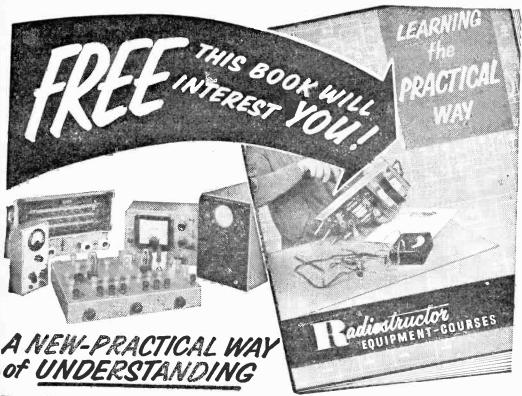
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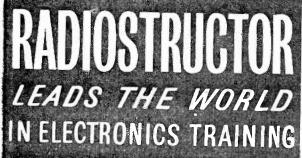
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THE RADIO SHOW

THE Radio Show is over for another year, and although for some of us nothing could have equalled the excitement caused by last year's exhibition, when, for the first time, many manufacturers and the broadcasting companies made colour and 625-line television their prime attractions on their stands, at this year's show it was interesting to note the reactions of these same manufacturers and broadcasting companies to the report of the Pilkington Committee and to the subsequent action taken by the Government on certain points in the report.

The G.P.O.'s exhibit—always one of the most interesting in our opinion-featured a communications satellite like "Telstar"

and a model of the Goonhilly Downs tracking station. As usual, the armed services provided very interesting displays of radio and electronic equipment now in use, and the Metro-

politan Police disclosed some of its methods of fighting crime with radio aids. We were pleased once again to meet many of our readers at

the PRACTICAL WIRELESS stand and we will try to keep in mind the useful suggestions and constructive criticisms which these meetings brought to light.

THIS MONTH'S BLUEPRINTS

Included in this issue of P.W. is the first of our new series of free Blueprints, beginning this month with designs for a signal generator and a power amplifier. The "Strand" amplifier—as the latter is called—consists of an amplifier and a power pack built on separate chassis to facilitate their installation in a suitable cabinet.

The Strand gives a virtually distortion-free output of 20W, making it an ideal addition to a hi-fi enthusiast's range of equip-

The P.W. Signal Generator is a mains-operated, portable, R.F./A.F. instrument which could be used to advantage by a beginner to radio, to form a basis of a set of home-constructed test equipment.

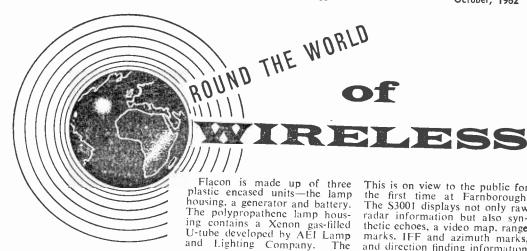
The November and December issues of PRACTICAL WIRELESS will also contain free double-sided Blueprints, making a total of six new designs for the amateur constructor. Four of the six pieces of equipment are capable of being combined into a single hi-fi system, consisting of a radio tuner, a pre-amplifier, a power amplifier and a loudspeaker enclosure. Of course, each piece of equipment may be built and used separately as the constructor wishes.

PRACTICAL TELEVISION DATA CHART

In the October issue of our companion journal Practical Television, we are giving away free, a Data Chart to be used in connection with a new series of articles starting that month and dealing with the principles and practice of television. The Data Chart contains information of interest to all radio and TV enthusiasts, such as; a complete list of television stations throughout the U.K., tables of decibels and power ratios, and comparisons of television standards, colour codes, designs for attenuators, aerial information, etc., etc.

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Our next issue dated November, will be published on October 5th.



NEWS AT HOME AND ABROAD

THE following statement shows the approximate number of Broadcast Receiving Licences in force at the end of June, 1962, in respect of wireless receiving stations situated within various Postal Regions of England, Wales, Scotland and Northern Ireland. The numbers include Licences issued to blind persons without payment.

Region London Postal. Home Counties Midland North Eastern North Western South Western Wales and Border (Counti	es	•••	Total 641,456 593,815 429,453 455,439 387,617 350,165 200,981
Total England and Scotland Northern Ireland	Wales		::-	3,058,926 328,255 108,653
Grand Total	••			3,495,834

New Miniature Rescue Beacon

VALUABLE addition to marine, desert and mountain survival equipment, a miniature distress beacon weighing only 3½lb. and named Flacon, has been introduced by Associated Electrical Industries Ltd. It generates flashes of light so intense that they will attract attention over distances as great as ten miles at night.

Flacon has the advantage over radio survival devices in that it does not demand specialised search equipment. It has been developed primarily as an integral part of equipment for aircraft dinghies and ships' liferafts of the inflatable type.

tube. Radar at Farnborough

generator

Xenon

AT this year's SBAC exhibition (the Farnborough air show) Marconi's Wireless Telegraph Co. Ltd. has on show a wide range of airborne radio equipments and navigational aids, the latter including ground station radar displays.

comprises

torised multivibrator circuits plus transformer and charging

circuit to provide the high

voltage pulse which drives the

battery is a 6V mercury cell type.

transis-

The standard

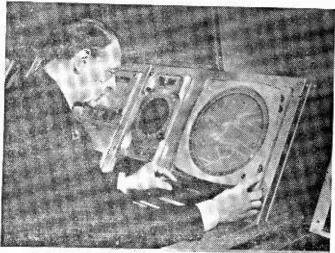
Of particular interest is the new transistorised PPI display type \$3001 made by Marconi's.

This is on view to the public for the first time at Farnborough. The \$3001 displays not only raw radar information but also synthetic echoes, a video map, range marks. IFF and azimuth marks, and direction finding information all on one PPI tube

International Radio Communications Exhibition

THE Radio Society of Great Britain's Exhibition in future will be called the International Radio Communications Exhibition and will be transferred to the Seymour Hall. Seymour Place, Marble Arch, London, W.I. It will be held earlier this year and for a period of four days from Wednesday, 31st October, to Saturday, 3rd November.

Catering accommodation will be larger with increased seating and tables and improved luncheon and tea service. Bar



This illustration shows the new Marconi transistorised PPI display type S3001, on view for the first time at the Farnborough air show.

services will be in separate room and with more accommodation.

A special display of homebuilt equipment will be shown and, as in other years, silver plaques will be presented for the most outstanding home constructed radio equipment and for manufacturer's outstanding equipment contribution to the radio world.

The Armed Services and, it is expected, Government Services, will again show latest developments and offer educational and recruiting services to all visitors.

CENTO Delegation Visits Britain

RECENTLY a party of over 30 senior Naval, Army and Air Force officers from three Central Treaty Organisation Treaty Central countries-Iran, Pakistan and Turkey-visited the Chelmsford works of the Marconi Company as part of a programme arranged for them by the British Govern-

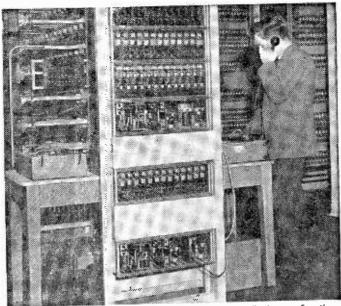
In the morning, after a reception by Mr. R. Telford (general manager) and other senior company officials, the party was taken on a tour of the works. In addition to seeing familiar equipments in process of manufacture, three small exhibitions were mounted for inspection by the included These delegates. of airborne radio, examples closed circuit television, and high-power radar transmitter/ receivers. A demonstration of naval communication transmission systems was also given.

The party also visited the Marconi Development Labora-tories at Writtle, where they saw a mobile high-frequency radio super-higha and station frequency radio link.

Experimental Telephone System in London

A SUBSTANTIAL increase in the number of telephone circuits carried by existing and new cables between telephone exchanges should be possible using a new system of "carrier" telephony which has been on test in London and North Kent.

Equipment has been installed at Faraday Building, London; at Crayford telephone exchange in Kent; and at nine points along this cable route to test the performance of the system designed and built by Standard Tele-



The terminal equipment in Crayford Telephone Exchange for the "local area carrier" telephony trials conducted by Standard Telephones and Cables Limited, by arrangement with the GPO.

phones and Cables Limited. Subject to the success of these

trials the new system could help to provide those extra lines between exchanges needed to cope with the growing use of the telephone. The system is called and is "local area carrier experimental at present. It uses techniques similar to those used for the past 30 years on longdistance cables.

STC are testing two systems over lines in the Faraday-Crayford cable, which passes through the telephone exchanges at Bermondsey, Tideway, Woolwich and Erith. There are nine (amplifiers) spaced repeaters 4,000yd apart, approximately five repeaters being fed with power over the cable from Crayford and four from Faraday Building.

Whereas each pair of wires in voice-frequency junction cable is normally capable of carrying only one telephone circuit, in these tests two pairs are being made to carry 12 circuits. A 13th circuit passes the signalling (dialling) signals for the others.

The system, known as SC-12, transmits the carrier and both sidebands of each channel, thus reducing the complication and

cost of the multiplexing equip-ment. In this respect it differs from long-distance coaxial cable systems which transmit one sideband only, suppressing the other sideband and the carrier frequency.

Equipment for a New Liner

THE new 22,000-ton liner, the s.s. Northern Star, of the Shaw Savill Line, has been supplied with telephones, telegraph equipment, salinometers, X-ray apparatus and some of its Associated wiring cables by Electrical Industries Ltd.

The marine department of El Telecommunications Divi-AEI sion have fitted the Northern Star with one single-point and two ten-point salinometers to monitor the saline content of the boiler feedwater system, a transistorised telephone system to link the bridge to lifeboat and docking stations, and a complete telegraph installation to transmit docking and steering orders.

torsion-AEI electric Two meters have also been fitted by the British Shipbuilding Research Association and will be used to determine the shaft horsepower transmitted by the ship's propeller shaft.

THE SUBJECT OF ONE SIDE OF THIS MONTH'S FREE BLUEPRINT, AN R.F./A.F. TEST INSTRUMENT.

The P.W. SIGNAL **GENERATOR**

By F. G. Rayer.

HIS signal generator has been designed to fit into a cabinet 6in, x 7in, x 3in,, and to use a single double-triode valve, making the circuit quite simple. It covers from 150kc/s to 3Mc/s (2.000 to 10m) in five bands, and can provide a continuous wave or modulated output, as required, over these frequencies. An audio frequency output is also included, for A.F. circuit tests. These features make the signal generator a very useful piece of equipment for aligning, calibrating, testing and trimming all kinds of receiver.

The generator uses A.C. mains for power, and is directly calibrated in frequency. This can be carried out to a standard sufficiently accurate for

all practical purposes.

The Circuit

Fig. 1 on the blueprint shows the circuit, the valve being a 6SL7GT. One triode section acts as an R.F. oscillator, the output being taken from C4 to the potentiometer VR1. For C.W. (continuous wave) output, only this triode operates. Only one coil is included in Fig. 1, the remaining four coils being wired in the same way.

The second triode section acts as an audio oscillator, and an audio signal may be taken from C5. This A.F. output can be used to test all kinds

of audio circuits.

The 3-way function switch permits each kind of working, and when this is in the centre "Mod. C.W. position, the continuous wave is modulated by the A.F. oscillator. The purpose of each kind of output is dealt with later.

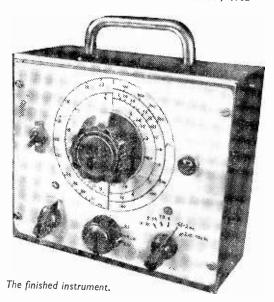
A small power pack provides current for the generator, this being included so that the equip-

ment is completely self contained.

Panel and Cabinet

The panel (6in. x 7in. aluminium), with drilling dimensions, is shown in Fig. 3. Clearance holes are drilled for all the control bushes, or may be stamped out with a punch. Four small holes take self-tapping screws to hold the panel to the cabinet, and two more holes take 6B.A. bolts, to secure the small chassis inside.

A piece of thin, smooth white card is cut slightly smaller than the panel, with holes to match. A similar piece of celluloid, thin Perspex, or other transparent material is also prepared, with holes to agree with those in the panel. Tuning



calibrations and other markings are made on the card, when the generator has been finished. The transparent material is placed over the card to protect it from unwanted marks.

The box or cabinet consists of universal chassis sides (available from Home Radio Ltd., 187 London Road, Mitcham, Surrey), held together with 4B.A. bolts. Two members 7in, x 3in, form the top and bottom of the cabinet, and two 6in. x 3in. pieces are used as sides. A further member 6in. x 3in. acts as a chassis, for the valve-holder, coils and A.F. transformer. A second 6in. x 7in. plate, held with self-tapping screws, forms the back.

The back, top, bottom and one of the sides are left off until construction is otherwise finished.

Power Pack Section

This is built completely on one 6in. x 3in. side, as in Fig. 3. A converter or tuner mains transformer, with an output of 220V at 20mA is adequate, as the actual H.T. consumption is less than 5mA. The valve heater and indicator lamp require 6.3V at 0.6A, and so a 1A secondary serves well. The circuit will work satisfactorily with an H.T. line voltage of 150V or even less, so a 220V H.T. secondary is by no means essential. If the voltage should be higher, it can easily be reduced by increasing the value of R3 or R5, so almost any transformer to hand may be used.

The rectifier is rated at 250V 540mA and is contact-cooled. Rectifiers of other rating may, of course, be used to suit the actual current and transformer voltage. R6 merely keeps the peak

current to a safe limit.

The actual values used for C8 and C9 are of little importance, and may be from $2\mu F$ to $32\mu F$. A small $8\mu F + 8\mu F$ condenser is convenient. Mains leads pass through a grommet in this side of the case, and the switch is fitted to the panel. The fuse holder, with 250mA or other low-rating fuse, is bolted to the chassis.

R.F. and A.F. Section

Coils, valveholders and the A.F. transformer are fitted to the 6in, x 3in, chassis, as in Fig. 2. This chassis, and the power pack, are secured to the panel, and all wiring may then be completed, and the generator can be tested, before adding the other side, or top, bottom and back.

Almost any small A.F. transformer will be satisfactory for the audio oscillator. The primary is wired from C6 to chassis, and the secondary from triode grid (pin 1) to chassis. A check for audio oscillation is made by connecting headphones, or a loudspeaker with output transformer, to the output socket and chassis. If no oscillation is heard with the function switch in the A.F. position, the leads to the primary of the A.F. transformer should be reversed.

A transformer with a centre-tapped winding may be used, the tap being taken to chassis. A small valve receiver output transformer can thus be used, or even a transistor type of output transformer. The unrequired winding (secondary) is then left disconnected. The note will probably be satisfactory, but, if it is too high in pitch, it can be lowered by wiring a capacitor across either the primary or the secondary. The pitch may be raised by wiring a resistor across the secondary.

The audio oscillator section can be tested by itself, R3 and the coils, etc., being omitted. A

For the three H.F. ranges, standard superhet oscillator coils are used. A medium-wave coil is used for L4, and a long-wave coil for L5: M.W. and L.W. oscillator coils cannot be used for L4 and L5, because the actual frequency coverage of an oscillator coil is higher than that of the signal frequency coil with which it is employed. How-ever, M.W. and L.W. coils with reaction windings, or H.F. and R.F. coils, with coupling windings of suitable dimensions, will be suitable. If no oscilla-

difficulty is experienced, the simplest solution is to wire up one coil only, and test the generator. The

other coils may then be added one by one.

nections to the feedback winding on it should be The actual ranges obtained were as follows:

tion is obtained with any particular coil, con-

10-23m or 30-13Mc/s. L1: 21-75m or 14-4Mc/s. L2:

reversed.

L3: 75-170m or 4-1.8Mc/s. L4: 150-550m or 2-0.55Mc/s (2.000-550kc/s)

L5: 600-2.000m or 500-150kc/s.

L1 and L2 are nearest the switch, as in Fig. 2, and wiring to these coils should be short. The range coverage can be adjusted, to obtain suitable overlap, by means of the coil cores, but these must be sealed, or left untouched, after calibration.

The 1,000pF 1,000V condenser in series with the output socket isolates the equipment from any

high voltage circuit to which the prod may be applied.

A check can be made to see that band coverage is suitable, and that the whole unit works correctly, before adding the sides and the back. A transparent cursor about 4in. long, scribed with a line, is cemented to the tuning control knob.

A.F. Output

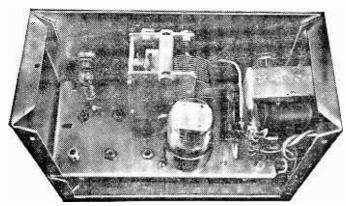
This is obtained with the function switch at A.F. and the signal strength is controlled by the attenuator VR1. To test an amplifier, or the audio section of a receiver, the test prod is applied to various A.F. circuit points in turn. Commence at the loudspeaker or loudspeaker transformer, moving from there

to the output valve anode, then to the output valve grid, then to the grid coupling condenser, and so on, introducing one lead or component at a time. If a fault is present, reproduction will cease, or almost disappear, when the fault is passed. As extra stages of amplification are brought in, the attenuator must be turned back, to keep volume down.

Mains, battery and transistor sets can be rapidly checked in this way, and a faulty stage can often be located in a few moments. A few such tests with a receiver or amplifier in good condition will soon show what to expect.

Mod. C.W. Output

With the function switch in the "Mod. C.W." position, a radio frequency signal is produced, the frequency of the signal depending on the band selected, and position of the tuning control. The



An above-chassis view.

modulated R.F. signal will not be produced if the A.F. circuit is not oscillating.

C4 is a low-value capacitor, made by twisting insulated wires together for about 4in. The capacity required is very small, but not in any way critical.

Band-switch and Colls

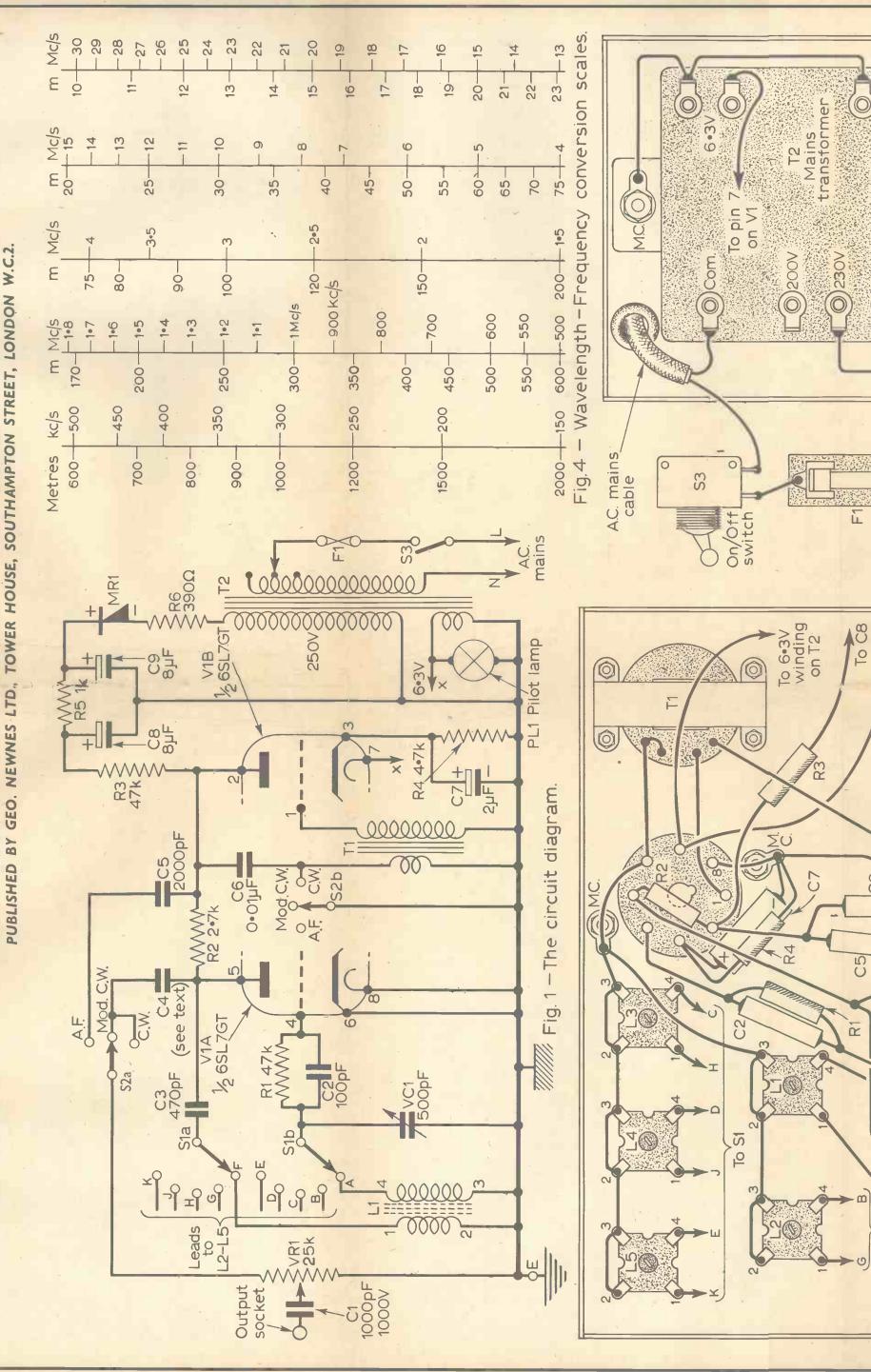
The switch is a 2-pole 6-way component, with one position not used. A lead is taken from the fixed plates of the tuning condenser, to the switch and C2 and R1, as in Fig. 2. This point is switched to A, B, C, D, or E, thereby bringing in the grid, or tuned windings, of the coils. A short lead from L1 (13-30Mc/s) coil, passes to the chassis.

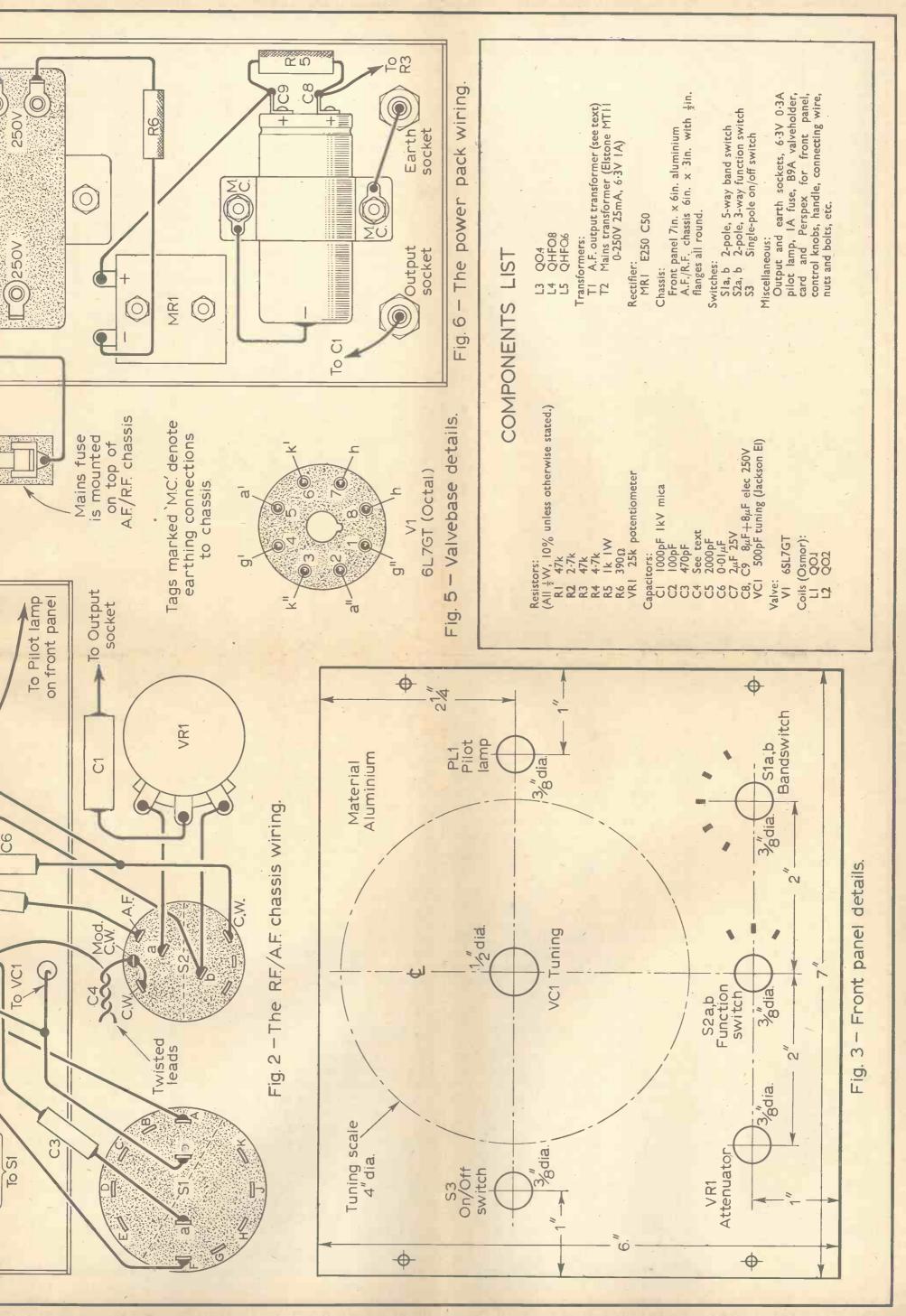
Condenser C3 is switched to F, G, H, I or J, bringing in the coupling windings of the coils. Switching here is very straight forward, but if any

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"PRACTICAL WIRELESS" OCTOBER 1962

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R.F. is modulated by the audio oscillator, so the signal can be heard on any receiver. To check I.F. stages in a receiver, tune the generator to the intermediate frequency of the receiver, and apply the modulated C.W. signal to each circuit point in turn, working backwards from the second detector. Reproduction ceases when the fault is passed, so it is thereby localised to one stage.

To check other circuits, such as R.F. stages, tune the receiver and signal generator to the same frequency, on any required band. To trim circuits, tune the generator to a high frequency on the receiver band. To adjust receiver coil cores, tune the generator to a low frequency on the receiver

band.

Sufficient coupling will often be obtained merely by placing the generator prod or lead near the aerial or other R.F. circuit connection. Coupling between generator and receiver should always be very loose, for final 'imming and alignment.

To calibrate a receiver, the generator will have to be calibrated itself. (This can be done as described later.) It is then only necessary to tune the generator to various frequencies, and tune in the signal on the receiver, and mark its dial. The same method can be used to secure best agreement with a ready marked receiver tuning scale or dial.

· C.W. Output

This is a radio frequency signal, tuned as already described, but not modulated. It will operate a receiver AVC system, or tuning meter or tuning eye, but cannot be heard by ear, with an ordinary receiver.

If a superhet has a beat frequency oscillator, the C.W. signal will be heard as a whistle. This will also be so with a TRF receiver having reaction, if reaction is sufficiently advanced to produce

oscillation.

The C.W. output may be used for trimming, etc., when a magic eye or other tuning indicator is present. It may also be coupled into the second detector of an ordinary superhet, to make C.W. morse audible. The generator is then adjusted to within 1kc/s or so of the intermediate frequency of

the receiver.

If a superhet is not operating, and early tests have made the oscillator suspect, the generator signal may be injected at the frequency changer oscillator or mixed grid. The receiver is tuned to agree with an expected station, and the signal generator is tuned slowly over a band around 470kc/s higher. If results are then obtained, the receiver oscillator is probably faulty (for this test, the generator frequency should be equal to the receiver frequency plus the intermediate frequency of the receiver).

Calibration

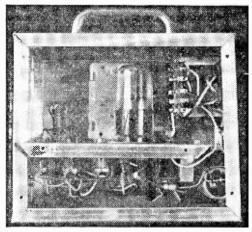
For maximum utility, the generator tuning should be calibrated. Five semicircles are drawn for this, and actual calibration may be achieved in a number of ways. If a communications receiver, or other accurately calibrated receiver is available, the generator may be coupled to this by placing its output lead near a short wire attached to the aerial terminal. The receiver is then tuned to various frequencies, and the generator is adjusted until its signal falls on the receiver frequency, which may

then be marked on the scale. A receiver with a tuning meter is most suitable.

Should a 100kc/s, 500kc/s, 1 Mc/s or other crystal marker be available, a receiver can be tuned to the marker signal, and each multiple (harmonic) and the generator can then be calibrated in 100kc/s or other intervals, with good accuracy.

If a calibrated signal generator can be utilised, its signal can be tuned in on a receiver, and the uncalibrated generator can then be tuned to the same frequency. In this way, calibration marks

can be made on the scales.



The signal generator with the back cover removed

In all cases, it is best to proceed systematically, finishing one range at a time. Fig. 4 shows the relationship between wavelength and frequency, and may be useful. The generator may be marked with frequencies in black, and wavelengths in red. Or wavelengths may be omitted.

Harmonic Calibration

If no ready calibrated receiver or generator is available, it is still possible to calibrate the scales. This will take a little longer, but only need be done once, and can be of good accuracy.

When the generator is tuned to any frequency, its note will be heard on this frequency, and also multiples of the frequency. That is, upon harmonics. For example, harmonics of 200kc/s will be audible to over 4Mc/s, with a sensitive receiver. Similarly, harmonics of 1Mc/s can be heard to nearly 30Mc/s, and harmonics of 2.5Mc/s

can be heard to 30Mc/s.

To use this method, tune in the long-wave Light Programme, which is transmitted on a frequency 200kc/s. Set the generator for C.W. and tune it to zero beat with the received signal, and mark the scale for 200kc/s. The generator is then left at 200kc/s, but is switched to "Mod. C.W." and the receiver is tuned upwards in frequency, until the generator is heard. This will be the second harmonic, or 400kc/s. The receiver is left untouched, and the generator tuned to the receiver frequency, and its scale marked for 400kc/s. The whole process is repeated for 600kc/s, 800kc/s and

(Continued on page 502)

Radio Components

THE COMPONENTS OF A TRF RECEIVER

REASONABLE understanding of the purpose of the many and varied components used in radio and amplifier circuits can go far in helping the experimenter and service technician to reach a speedy and accurate diagnosis of a fault condition. With that in mind, this series of articles sets out to investigate the functions of the components used in three basis pieces of equipment the TRF receiver, the superhet receiver and the A.F. amplifier.

In addition, the symptoms to be expected owing to a fault in any particular component will be considered, as also will the voltages and currents in the various stages, both under normal and fault

conditions.

The TRF Receiver

October, 1962

Although this type of receiver is now extinct so far as radio dealers are concerned, it is still, nevertheless, a popular set with beginners and home constructors. Kits of parts are still available for producing this kind of set, and quite a few are in operation as a second home-made "domestic" receiver. Just before and after the war many American versions were available on the British market, and there is every likelihood that some of

The term "TRF", means "tuned radio-frequency", which indicates that the set is not of the almost universal superhet type, but that it uses an R.F. amplifier to step up the strength of the aerial signals, and that detection occurs direct from the modulated R.F. carrier. With a superhet, of course, the signal frequency is converted to an intermediate-frequency before

In Fig. 1 is given a block diagram of a typical TRF receiver. Some sets are more complicated than others and may employ more than just a single R.F. amplifier stage, but the majority have but a single stage, as shown in the block diagram. The detector invariably uses either a leaky-grid or anode bend circuit, a pentode or tetrode valve being employed for this purpose. This arrangement provides sufficient audio signal at the anode fully to drive a tetrode or pentode output valve. On mains operated versions, the power supply usually consists simply of a valve half-wave rectifier fed direct from the mains supply, with a heater dropper or line-cord resistance to allow the required current to pass through the heaters of the series-connected valves.

Typical Circuit

A circuit typical of a TRF battery receiver is given in Fig. 2. Here V1 is the R.F. amplifier screened grid valve (tetrode). V2 is the leaky-grid

and their **Functions**

By K. Royal

detector and A.F. amplifier valve (pentode) and V3

the output valve (pentode).

The aerial coupling coil is L1, and signals from the aerial are coupled to this through C1, that having a value between 100 and 3.000pF, depending upon the circuit. In some early models, the coupling capacitor was sometimes variable and worked as a form of variable selectivity control—the smaller the capacitance the greater the selectivity. This, of course, resulted from the lighter loading on the aerial tuner-circuits by the smaller capacitance. In the set under discussion, however, Cl is 3,000pF and has no bearing on the selectivity, it being more of an isolating component.

The tuned windings are L2 and L3, with the

inductance of the two in series tuning over the L.W. band and the inductance of L2 only tuning over the M.W. band. Switch S1 is a part of the wavechange switch which when closed short-circuits L3 and gives M.W. operation. The aerial circuits are tuned by VC1, this being one section of a two-gang capacitor and the trimming capa-

citor (TCI) being a part of it.

Thus, VC1 tunes either L2 and L3 in series or just L2 by itself depending upon the position of S1. In this way, tuning over the L.W. and M.W. bands is accomplished, and the selected signal is fed to the control grid of V1, the arrow across the valve symbol indicating that the valve has a variable-mu characteristic. This means that the signal amplification through the stage can be altered fairly evenly by changing the grid bias the smaller the bias the greater the amplification.

Control of Volume

This, then, leads to the arrangement used for control of volume on some TRF receivers. In Fig. 2, VR1 is, in effect, an R.F. gain control. It works in that way because the negative voltage (relative to earth) across R8 and R9 is applied across VR1 and R2 in series and is then tapped off at the slider of VR1 and used as bias for the R.F. valve V1.

It will be seen that continuity exists between the slider of the control and the control grid of V1 through R10, L3 and L2. Thus, by altering the control so the grid bias is altered, and in that way a control of R.F. gain is secured. In addition, however, VR1 serves as a variable loading to the signal across L1. For example, when the slider of VR1 is at the R2 end of the control, L1 is damped by the whole of VR1, via C3. But since VR1 is of fairly high value (50k), the loading is very small and there is virtually no attenuation of the signal. In that position there is also minimum negative bias on the control grid of V1, so both the signal input and the R.F. gain are at a maximum.

input and the R.F. gain are at a maximum. When the slider of the control is moved away from R2, however, the damping across L1 is progressively increased and, further, the bias on V1 is also increased. In these two ways, therefore, a control of volume is effected. C3 is called a signal filter capacitor and has a value of 0.01 µF, R10 serves a like purpose and has a value of around 33k, while C4 is the "bottom end" coupling capacitor for the R.F. tuner circuits and has a value of 0.005 µF. R1 and C2 are rather specialised components of the receiver under discussion, and serve essentially to prevent the tuned circuits from going out of step in the region of 500m.

The tuned signal is redeveloped in amplified form across L4 and L5 in series (L.W.) or across L4 only (M.W.); in the anode circuit of the R.F. amplifier. S2 is ganged to, and serves a similar purpose to S1, being open on L.W. and shorting out L5 on M.W. Current for the anode for the R.F. valve is fed through L4 and L5, and the signal across these inductors is coupled to the detector tuned circuit. L6 and L7 through the coupling capacitor C6, which has a value of 11pF. The combinations L4/L5 and L6/L7 provide bandpass coupling and considerable increase in selectivity. S3, again, is a part of the wavechange switch and shorts out L7 on M.W.

Detector Circuit

The L.W. and M.W. signals across L6 and L7 are tuned by the section VC2 of the two-gang capacitor, and the selected signal is coupled to the control grid of V2 through the 50pF capacitor C11. This capacitor together with the grid leak R4 produces a time-constant which gives the leakygrid detector action. R4 having a value of 4M. A little grid bias is given to V2 by the potential-divider R5 and R6 across the filament circuit, the values being 220k and 77k respectively.

The A.F. of the signal carrier thus occurs at the control grid of V2 and this is developed in amplified form across the anode load resistor R7, a typical value being 33k. There is also a little signal voltage at this anode, and this is fed back to the control grid of V2 via C12 (0·1µF), the differential reaction capacitor C11 and the reaction

winding L8.

The phase of the signal so fed back is such that it adds to the signal already present at the grid and thus gives rise to positive feedback. This is often called "reaction" or "Q-multiplication". The former because when the feedback is sufficiently high oscillation occurs, and the latter because the effective Q or "goodness value" of the detector tuned circuits is enhanced as the feedback is increased. This makes the selectivity of the tuning progressively improve as the feedback is increased, but when a certain point is reached uncontrolled oscillations develop and the detector turns into an oscillator which, of course, is no good for reception. The idea, then, is to adjust the feedback just prior to the point of feedback and this is accomplished by the coupling of the reaction capacitor C11.

This kind of circuit may have several "gimmicks", and those in the circuit under discussion are the differential reaction capacitor, the pre-set capacitor C10 and the switch S4 which brings in resistor R3 (990!2) on L.W. When the reaction capacitor is at minimum, the residual R.F. or signal at the anode of V2 is by-passed to earth or chassis and no feedback occurs. However, as the control is rotated towards maximum, the by-pass effect is decreased and coupling takes place progressively via the other plate. The pre-set capacitor C10 which is shunted across the moving plates and one set of fixed plates ensures, however, that a small amount of "reaction" is applied to the grid of V2 with the manual control at minimum. The fixed capacitor C9 (100pF) balances the other section of the control in a similar manner.

section of the control in a similar manner. Capacitor C7 (0.005µF) is the L.W. and M.W. padder and is also common to the feedback path. Thus. when R3 is switched into circuit by S4, the feedback path is slightly modified, thereby ensuring smooth reaction during reception on the L.W.

band.

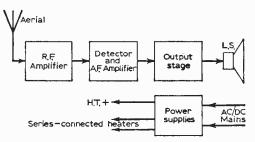


Fig. 1—A block diagram of a typical TRF receiver. Here the R.F. amplifier steps up the weak aerial signals to a level suitable for detection.

To operate a gramophone pick-up on this kind of set it is necessary simply to introduce the pick-up across the detector grid-leak, to turn down the teaction and to detune the set from a station. A separate volume control is necessary, though, for the pick-up, and this usually mounted on the motor board. Care must be taken when connecting a pick-up to a mains TRF set, however, for in this type of circuit the mains is often connected to one side of the receiver chassis and there is always the possibility of severe electric shock and mains hum. The pick-up circuit must be isolated from the mains supply.

The A.F. Stages

C12, apart from coupling residual signal back to the grid for reaction, also serves as the A.F. coupling capacitor, its value $(0\cdot 1\mu F)$ being high enough to permit this without unduly attenuating the lower audio frequencies. The A.F. signal at the anode of V2 is fed to an auto-transformer (or tapped choke) L9, which steps up the signal and increases the impedance to values suitable for the control grid of the output valve V3. In mains receivers and in modern all-dry battery sets, resistor-capacitor coupling is nearly always used instead of a transformer, but with old-style battery models, the extra gain produced by the coupling transformer is often desirable.

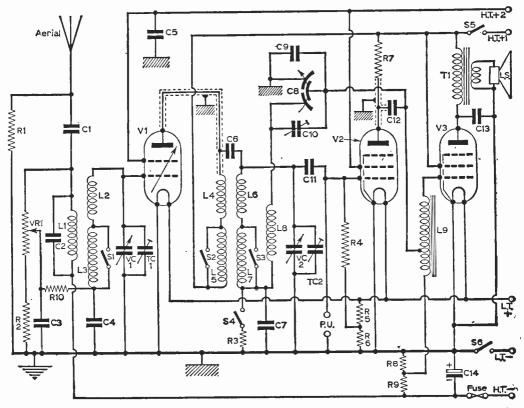


Fig. 2—The circuit diagram of a typical TRF battery receiver with stages conforming to the block diagram of Fig. 1.

Speaker Coupling

The anode of the output valve V3 is loaded by the primary of the loudspeaker transformer T1, while the secondary of the transformer is connected across the speech coil of the loudspeaker. The transformer is to match the loudspeaker impedance (about 3Ω) to the optimum load value of the output valve (several thousands of ohms, depending upon the type of valve). The matching is based on the transformer turns ratio and is equal to $\sqrt{Z1/Z2:1}$ where Z1 is the optimum anode load of the value and Z2 the impedance of the loudspeaker.

The screen grid of V3 is connected direct to H.T.+1 (120V), while the screen grids of V1 and V2 are fed separately from a 90V tapping on the H.T. battery, H.T.+2.

Auto-biasing

Very early battery sets required a 9V grid bias battery, but the set under examination uses an auto-bias system. It works in this way: H.T.— is taken to the chassis or earth line not directly, but through R8 and R9 in series (3500 and 5000 respectively). This means, then, that the full H.T. current of the set flows through these resistors, and thus produces a voltage drop across them, Relative to chassis, therefore, H.T.— is negative and, as well have already seen, this is applied to

the R.F. gain control system (R2 etc. in V1 circuit). Owing to the potential-divider action of R8 and R9, a lesser negative voltage (still relative to chassis) appears at their junctions, and this is applied as grid bias to the control grid V3, via L9. The circuit is completed by a fuse bulb in the H.T.— lead and by the main on/off switch, S5/S6. Decoupling for the auto-bias is provided by C14, which is a $32\mu F$ electrolytic capacitor, and for the screen grids by C5, valued at $0.25\mu F$. C13 is a fixed "tone control" capacitor which, in effect, suppresses certain distortions produced by the output valve.

To conclude this month's article, the voltages and currents to be expected in the three stages are given below.

Voltages and Currents

V1 anode 120V 2mA; screen grid 90V 1mA. V2 anode 100V 2mA; screen grid 90V 1mA. V3 anode 108V 4 to 5mA; screen grid 120V 1mA. Bias across R8 and R9 in series 4 to 5V.

Much, of course, will depend on the condition of the batteries and on the tapping selected for H.T.+2 and so far as the anode of V2 is concerned, on the sensitivity of the voltmeter used for the measurements,

(To be continued)

SERVICING TAPE RECORDERS

RECORDING FROM A.M./F.M. AND A.C./D.C. RECEIVERS

By T. S. Smith

LTHOUGH the method of obtaining a radio signal for recording purposes from across the secondary of the receiver's output transformer probably introduces a smaller distortion content than by placing the microphone in front of the loudspeaker, the overall distortion is still, nevertheless, higher than it need be. This is because the receiver's output stage is designed to supply power at a low impedance, and it is far more difficult to secure a distortion-free signal that way, than a low-level signal at high impedance, which is far more suitable for the input of a tape recorder, as was revealed last month.

Detector Signal

All receivers, valve and transistor types, produce a source of audio-frequency signal which is as free as it can possibly be of distortion. This signal is developed across the load resistor of the detector stage (A.M. or F.M.). This signal is of a relatively low level (in terms of millivolts), and in the receiver itself is fed first to an A.F. amplifier and then to the output stage. It is obvious, of course, that the A.F. and output stages will introduce some distortion to the signal, even if only small, so connecting to a tape recorder before those stages goes a long way to enhance the recorded quality.

A receiver typical of the type used by home recordists is given in Fig 28. This shows the final I.F. amplifier, the A.M. and F.M. detector circuits, the magic-eye tuning indicator, the first A.F. stage, the output stage and the power supply circuits. One rather important point to notice is that the mains transformer has a totally isolated mains primary winding. This means that the chassis of the set may be connected direct to an efficient earth point, and that a tape recorder may be connected direct to the receiver without any danger of electric shock or fear of demands the equipment.

of damaging the equipment.

V3 is the final 1.F. amplifier valve, while V5 serves as both A.M. and F.M. detector and also as tne A.F. amplifier. One diode in the valve (the one connected to pin 6) is used as A.M. detector, and the other two diodes are used in a ratio detector circuit for F.M. The triode section of the multiple valve is the common A.F. amplifier. The amplified A.F. signals from the anode of the triode feed the output valve V6, and the bridge rectifier W1 supplies H.T. voltage for the whole of the set. V4, of course, is the magic-eye tuning indicator.

(Continued from page 418 of the September issue)

It is not proposed to delve into the detailed operation of these stages as such information is available in past issues of this magazine. However, the A.M. detector load resistor is R15 (330k) in series with the "earthy" side of the secondary (L19) of the A.M. I.F. transformer. The A.F. signal from across this load is fed to the A.M./F.M. change-over switch S1a.

Now, in the "F.M." position, C44 (680pF) acts as the load and this, as will be seen, is connected to the other side of the A.M./F.M. change-over switch, via C45. Thus, on the slider contact of the switch (point 5) we have an audio signal which is either A.M.-or F.M.-derived, depending upon the setting of the receiver. These factors are common to all A.M./F.M. receivers and, as with the circuit under discussion, the A.F. is always fed to the top-end of the volume control (R29), in this case, via C51.

For normal operation of the set, the required level of A.F. is taken from the slider of the volume control and fed to the grid of the A.F. triode amplifier. However, for normal driving of the average tape recorder, the A.F. signal across the volume control is of adequate level, and there is absolutely no need to amplify it further in the receiver. Thus, by extracting the signal from across the volume control, the inherent distortion in the receiver's audio stages is eliminated. Furthermore, this component is common to both the A.M. and F.M. audio, so extra switching is not required.

Avoid Shorting the Negative Feedback

In some receivers the bottom end of the volume control is returned direct to chassis, as shown in Fig. 29, but in other sets, as in Fig. 28, the bottomend of the control is loaded with a fixed resistor to facilitate the application of negative feedback.

In the former case, there is no difficulty whatever in obtaining the A.F., for it simply resolves to the connection of a screened cable, with the inner conductor to the top of the control and the braiding to chassis, as revealed in Fig. 29. In the latter case, however, similar connection would almost certainly effect the negative feedback system and result in somewhat confusing symptoms.

Where possible it is always best to retain a direct connection between the braid of the tape recorder signal output cable and the chassis of the receiver. But if that is done in Fig. 28, the input resistance of the recorder would appear across R29 and R30 in series. In certain cases this may

not matter much, but in other cases instability and hum may result, depending upon the exact nature of the receiver's negative feedback loop and the input impedance of the recorder. To be on the safe side, therefore, the braid should be connected to chassis, but the inner conductor of the feed-out cable should be connected to the top of the volume control via an isolating capacitor of $0.1\mu F$ (see Fig. 30).

The A.F. signal across the volume control is upwards to a maximum of about 1V peak, and is adequate for almost all tape recorders. The frequency response at this point is also very good, being limited essentially by the passband of the I.F. circuits and the design of the detector. With A.M./F.M. receivers, de-emphasis usually takes place to some degree between the ratio detector or phase discriminator and the volume control, so that the A.F. across the volume control should be in reasonable frequency balance. However, when a coupling capacitor is used, as in Fig. 30, the value of that can be reduced if necessary to provide a certain amount of bass cut (i.e., top lift) to suit the recording characteristics of the tape recorder.

Isolate D.C.

In some A.M.-only receivers, including transistor sets, the volume control acts as the

whole or part of the detector load. This means that in addition to the A.F. across the resistor, there occurs a direct-voltage which is the rectified I.F. carrier. This voltage is negative with respect to chassis (positive in transistor sets) and increases with increase in signal amplitude. It is thus employed as an AGC bias.

Care must, therefore, be taken to avoid shorting the voltage out or applying it to the input of the tape recorder. This would not harm anything particularly, but it might either introduce distortion due to bias disturbance in the first stage of the tape recorder or, if the radio signal is passed through a volume control in the recorder, noise as the volume control is adjusted.

In all cases where the detector diode is in direct connection with the volume control, as in the transistor circuit in Fig. 31, an isolating capacitor should be connected between the top-end of the control and the inner conductor signal lead-out (Fig. 30).

Even in a transistor set, it is desirable to maintain connection between the braid and the chassis or common battery circuit. This will prevent random earth effects which could produce hum or instability. In transistor sets, the volume control is of a lower value than that in valve receivers, (e.g., 5k in Fig. 31 as compared with 500k in Fig.

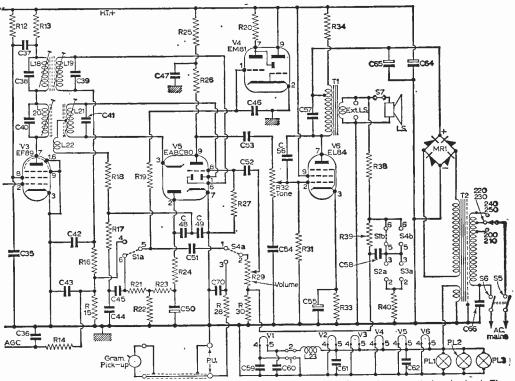


Fig. 28—A typical circuit of an A.M./F.M. receiver from which a "recording" signal can easily be obtained. The audio from both A.M. and F.M. transmissions is developed across the volume control R29, and from here it may be directed to the "radio input" of a tape recorder, as shown in Fig. 30. This set also features a fully isolated mains transformer, which is a requirement for recording purposes.

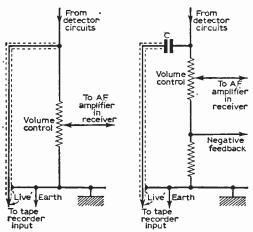


Fig. 29 (left)—When one side of the volume control is connected direct to chassis, and provided there is no direct-voltage due to carrier rectification, across the control, then the audio may be fed direct to the tape recorder as shown.

Fig. 30 (right)—If there is a direct-voltage across the volume control or if a fixed resistor is connected at the "earthy" end to facilitate negative feedback, then the tape recorder signal must be directed through an isolating capacitor C.

28). This does not matter unduly provided the coupling capacitor C (Fig. 30) is no less than 0.1μ F. It may even pay from the bass response point of view to increase the value to 0.25μ F.

At this stage, it should also be remembered large transients are likely to destroy that transients of destroying transistors, and that magnitude can occur due to the connection of mains equipment to a transistor circuit. This can mainly be avoided, however, by ensuring that all the connections are highly efficient and that they are made before switching on the tape recorder and transistor set. A poor connection causes crackles in the loudspeaker or on the tape, and these crackles are really transient surges of current. Further, on no account should a transistor set be coupled direct to A.C./D.C. equipment, but this does not often apply, since almost all tape recorders are for A.C. mains only and feature a fully isolated mains transformer.

Mains Isolation

Tape recordists often require to record from an A.C./D.C. type of receiver. These sets have no mains transformer, and due to that there must exist a connection direct from the mains to the H.T. negative line or chassis. This presents no trouble under normal operating conditions, but if internal connections are made to this kind of receiver, one side of the mains supply is, in effect, brought out to the connecting leads and applied direct to the tape recorder.

Since, for the sake of hum and stability, it is necessary to connect the braid to the chassis of the receiver (Figs. 29 and 30) and to connect the braid at the other end to the "earth" side of the radio input on the tape recorder, the mains supply is connected straight to all the metal work of the recorder. If that happens to be connected to the

(Continued on page 525)

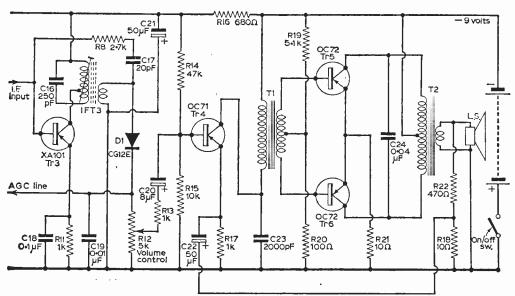


Fig. 31—Although a transistor circuit uses a lower value volume control (R12) than valve circuits, the recorder signal can still be picked up from that point, but a higher value capacitor may be required for isolation. The capacitor is necessary to isolate the D.C from the recorder input circuits (see Fig. 30).

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EBF80		EY86		PY81	6/-			6F33	0/0 .	30L1	7/6
EBF89		EZ40	812	PY82	6/-			GLL	12/-	30 P4	11/3
EBL31		EZ41	6/9	PY83	8/-		12/6	6L18	8/8/,	0P12	8/-
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THE FOLLOWING TWO ARTICLES HAVE BEEN INCLUDED WITH THE INTERESTS OF THE HI-FI ENTHUSIAST KEPT IN MIND

A Small Enclosure for GOOD BASS Reproduction

By W. Groome,

HE demand for small loudspeaker enclosures, intensified by the advance of stereo, has been met to some extent by the development of special loudspeakers, but many enthusiasts would like to use their existing units of conventional design. It was this need that prompted the author to make some interesting experiments described below.

Failure of the usual loudspeaker in a small box is mainly caused by the stiffness of the enclosed air; a springiness which, added to that of the cone suspension, raises the bass resonant frequency by as much as one-third. An open-baffle resonance of 45c/s could become 60c/s in a cabinet having a volume of 2cu. ft. As there is little worthwhile output below this frequency there is serious loss of bass. It is unfortunate because at frequencies above resonance, small enclosures (properly lined) behave very well.

To reduce the stiffness or, to express it properly, to increase the compliance of the box (Cb), would require increased volume, so other factors must be considered. These are, compliance of the cone and suspension (Cs), the mass of cone and suspension (Ms) and the mass of the air load (Ma).

The functions of compliance and mass in acoustic resonance are similar to those of

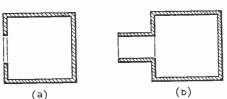


Fig. 1—(a) A simple resonant cavity, (b) with added duct.

capacitance and inductance in tuned circuits, and an increase in either will lower the resonant frequency. Adjustments of Cs or Ms require drastic alterations to the loudspeaker that can be tackled more light-heartedly with a cheap unit than with the quality instrument we are concerned with. Therefore we can experiment only with the mass of the air load.

Horn Loading

The best-known method of air loading is the horn, which compels the cone to activate the large mass of air it encloses and couples it to the outer air over its large mouth area. In contrast the direct radiator cone has nothing to confine the air against it firmly enough to load it and transfer all of its energy.

Any mass of air that is, by some means, confined to the front of the cone becomes part of the resonant system. We can liken the air in a small box cavity, Fig. 1(a), to a stiff spring with a high rate of vibration and the mass of air in the added duct (b) to a weight that will slow the movement of the spring. That is to say, it will lower its resonant frequency. Variation of the length of the duct and the area of its opening provide considerable control over the resonant frequency; it has been claimed that the system can be tuned lower than the bass resonant frequency of the loudspeaker, so increasing the range downwards

The duct also adds acoustic resistance which can be adjusted to damp the resonance, flattening the peak (it seems) to make the system behave like a non-resonant one. Compact practical arrangements of the duct are indicated in Fig. 2, where the drawings show them as they would appear with one side removed. The author has made several enclosures to test the duct idea and has been

surprised at the liberties that can be taken with cavity volume with a loudspeaker of good bass response. Fig. 3 shows one that houses a large 12in. unit and its dimensions, 15in. x 14in. x 10in. plus duct, could hardly be smaller.

Experiments

Experiments, however, cost very little. A reflex cabinet requires about 20sq ft of expensive plywood or blockwood at least 1in, thick and can be a costly failure if panel resonance or loudspeaker

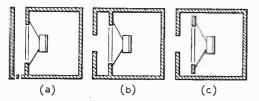


Fig. 2—(a) A practical duct loading with either one or two openings, (b) with front slot, (c) with gap loudspeaker mounting.

mis-match do their worst. Bracing the reflex is almost a feat of engineering but a small box of in. plywood is remarkably rigid. For preliminary tests boxes in any rigid timber can be quickly assembled and then followed, when satisfactory results are obtained, with a first-class job.

Fig. 3 gives constructional details of one of the enclosures. If any adjustments to the dimensions are considered necessary, it is preferable to widen the enclosure to increase the effective length of the duct. Contrary to some long-held opinions, the allowance for the volume of the loudspeaker should be quite small—about 60cu. in. for the magnet and frame only. The cone does not affect the volume because it is transparent to sound, therefore the box is effective

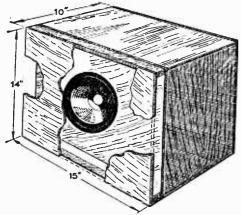


Fig. 3—The construction of an enclosure with vertical slide slots.

as a resonator right up to the loudspeaker opening. Although the box hardly needs any bracing you can add fillets to aid screw assembly. The loudspeaker mounting board and front duct

panel should be screwed, without glue, to allow for removal when necessary.

Dust Opening

Modification of the duct spacing and area of the two vertical openings can be achieved by changing the depth of the top and bottom battens to which the front panel is secured, starting with 2in. gaps and reducing in 4in. steps until the most satisfactory results are obtained. The area of duct opening can be halved simply by standing the box on floor or table with one opening downwards. This has been done in Fig. 3 to off-set the effect of another experiment that will be described later.

Line the box with double layers of 1 in. carpet underfelt, not drawn too tightly. A limp "curtain" of the same material should be arranged across the

cavity behind the loudspeaker.

Distribution of low frequencies is not noticeably affected by the directions in which the slots face, but choice of position can improve the air loading. If the enclosure is placed on the floor in a corner, slots facing the rear and vertical, the air mass partially enclosed by the wall, floor and cabinet side, form a step in the coupling from duct to room. Although the total slot opening area is smaller than that of the cone there is no loss of output (unless it is made ridiculously small) because of the improved transfer of energy by air loading. By experiment it was found that there is a point beyond which further reduction brings no audible improvement; the damping by acoustic resistance can, like electrical damping, be overdone.

The enclosure. shown in Fig. 4, has the slot facing the loudspeaker cone, and has proportions more acceptable than those of Fig. 3. The loudspeaker mounting board is screwed to battens fixed inside and can be brought forward to narrow the gap by interposing spacing strips. Slot area adjustments should be verified by the use of temporary front panels before cutting and fitting permanen. ones. The effect of limited coupling between front and back of the cone can be tried by leaving small gaps at the top and bottom of the loudspeaker mounting board. (They permit some flow of air while resisting sound energy, possibly increasing box compliance and adding some damping.) A simple way of arranging a small air gap is to stand the loudspeaker off the board by means of spacers or washers: another is to drill an array of small holes as is done with larger cabinets using resistance loading.

Appearance

This enclosure can be used in any position, but again the "slot/vertical" corner arrangement is worth trying. Mounted on legs and smartly contemporary, it can be arranged slot-downwards and will gather less dust than in other positions. Beyond this suggestion the author offers no advice on the question of final appearance, for the compactness of these boxes will probably prompt the reader's own adaptations, aided by the helpful fact that in several positions there is no need for a grille.

So long as fidelity is the aim, it may be best not to reduce the volume for a smaller loudspeaker unit. The smaller loudspeaker opening leaves a

longer effective duct for a board of the same size, which will help to off-set the poorer air coupling of a small cone. As 8in. and 10in. loudspeakers require less cabinet depth than 12in. ones, the frontal area can be increased for the same volume to provide another increase in duct length. A cabinet 21in. x 12in. x 8in. should give good results.

The following remarks are for the experimenter who is interested in scaling the size down even more than described. The enclosure shown in Fig. 3 is less than 2,000cu. in., but it gives very fine bass, free of boom or "honking", with the character of the instruments clearly defined with none of the "tuned thud" effect so often heard. Probably because of the resistive loading the system seems tolerant, if not independent, of cavity volume. Removal of the front panel converts the enclosure into a simple box and quickly demonstrates the superiority of the duct loading.

Tests

A test with a cheap radio-set type of 8in. loud-speaker in a ducted enclosure somewhat less than 2.000cu. in. gave surprisingly good bass despite the flabbiness of its thin, soft cone, although it did not, of course, measure up to the massive 12in. unit. In the extreme a small elliptical loudspeaker intended for a portable radio was tried in a roughly-made box measuring 14in. x 10in. x 6in.,

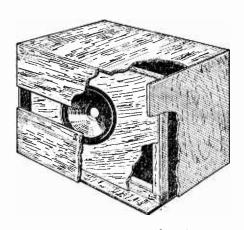


Fig. 4-An enclosure with a front slot.

and the reproduction proved better than the loudspeaker had given in an open-back cabinet. All this tends to show that there is scope for some interesting experiments.

The purpose of the author's tests was to verify claims that the system can maintain and even extend the loudspeaker hass response in a small enclosure without distortion or frequency-doubling, and with good transient response. One of the tests was to try it to the very moderate high frequency range of the 12in, unit without the cross-over network that normally excludes H.F. The enclosure shown in Fig. 3 was modified by cutting an elliptical opening in the front panel to expose

the central area of the cone. The loudspeaker was not a full range model and its response droops above 8.000c/s in any enclosure, and the small enclosure with one slot closed to off-set the area of front opening did not seem to impair its performance.

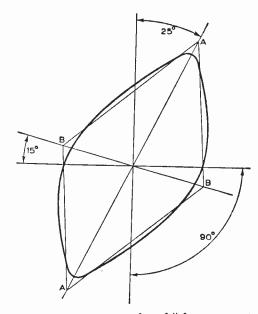


Fig. 5—The duct opening for a full frequency-range loudspeaker.

This may not hold good for a wide-range unit, for American designers have stressed that high-frequency response is dependent on the shape of the opening and described a particular shape claimed to achieve the best results. The author has not tested the idea, but for those who are interested this "lemon" shape is shown in Fig. 5. Draw the axis (AA) 25° from vertical, and the axis (BB) 15° from horizontal and half the length of (AA). Join (ABAB) to form the diamond shown in light line, then round it off to the "lemon" shape shown in heavy line. This opening is intended to replace a single vertical front slot and to have the same area.

As only the front radiation is used there is some loss of volume compared with systems in which the back emission is reversed in phase and used to boost the bass, but it is far less than would be expected from a comparison of size. Against this, however, there seems little, if any, of the bass loss sometimes found with other systems when fed by amplifiers of low output resistance and less boost is needed to capture the lowest notes.

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A Stereo EXPERIMENT

SOME NOTES OF INTEREST TO THE OWNERS OF TAPE RECORDERS WITH 4 TRACK OR STEREO HEADS

By H. Peters

THE author recently fitted a stereo head to a tape recorder, and despite a warning note in the instructions about home-recorded stereophonic tapes, he decided to attempt to produce some form of stereophonic recording using as little extra equipment as possible.

Limitations

True stereo has to be ruled out when recording stereo as only one recording channel (the one in the instrument) is available, and this means that each channel has to be recorded separately and alternately in such a way that the two when played back together will provide some directional effects. The block diagram (Fig. 1) shows the form that the finished arrangement took. For convenience the original recording track which is used for monaural recordings is referred to as track A (head A), and the second track needed for stereo, track B (head B). Track A is used as the right hand channel, track B as the left hand channel.

It is necessary to build a switching unit (Fig. 3) so that the output of the existing recorder can be fed to the A or B track (or both) whilst the output of the other track is taken away outside the recorder to a separate amplifier, which in the author's case was the one in his radio receiver.

This involves building a suitable pre-amplifier to lift the signal level from the B head to a voltage sufficient to feed into the pick-up sockets of a domestic radio. Such an amplifier is shown in Fig. 2.

Switching Unit

This is a standard 2-pole 3-way Yaxley type wafer switch totally enclosed in a metal case. Each wiping contact is connected to the inner of the screened lead to each head, and in the first position these eads are connected to their

eads are connected to their espective amplifiers, the A head to the record/playback amplifier, so that in this position the instrument can be used in its original form.

In the second position no head is taken to the econd channel pre-amplifier; both heads are taken o the record/playback amplifier. Thus a stereo ape may be reproduced as monaural, and it is ilso possible to record on to both tracks at the ame time. This is a useful facility since it repre-

sents "central" noises on the stereo tape, but it must be emphasised that unless special arrangements are made to compensate for the reduction in bias caused by the two head inductances being in parallel, distortion will occur at the higher volume levels.

In the third position the heads are reversed, the second channel amplifier being connected to the A head and the record/playback amplifier to the B head. This enables recording to be carried out in a forward direction on the B track. Any recording made on the B track by turning the tape over and making the recording via the A head will, of course, be heard backwards,

Earthing

The outer braids of all the screened wires are joined together and taken to chassis at the main earth point. There is usually one earth connection only between the tape deck and the amplifier chassis, and this point should be used to avoid an inductive loop creating hum. If the two chassis are joined by random chassis connections at different places, hum may be increased. The metal case around the switch should be taken to chassis, either by bolting it down, or if it is clear of all the metal work, by a wire taken to the aforesaid main earth point.

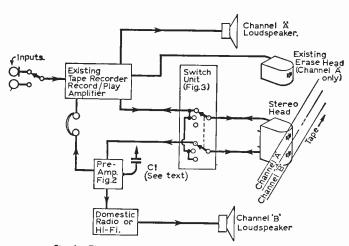


Fig. 1—The arrangement used for the stereo recording.

Pre-amplifier (Fig. 2)

This is a simple two-stage resistance capacity coupled double-triode amplifier. An ECC83 (12AT7) valve is used and this valve takes barely 3mA H.T. and 0·3A L.T., and so can safely be added to the load of the tape recorder power unit. The valve heaters (pins 9 and 4/5) should be left free from the chassis as the heater wiring is

probably taken to chassis elsewhere.. The layout

is not critical.

The purpose of C1 (0·1µF) will be dealt with later. R7 (1M) may be a potentiometer to control the volume of the channel if no other volume control is available, and any tone correction (bass lift) necessary, may be made by suitable resistancecapacity networks between the junction C3/R7 and chassis. No correction or control was fitted into the original pre-amplifier since adequate control was available already in the radio to which it was fitted. A screened lead connects the preamplifier output to the radio and this can be ordinary television (downlead) coaxial cable. The author's radio was not earthed and so no special precautions were necessary, but if both the tape recorder and the radio or amplifier happen to be earthed separately, an inductive loop can be formed giving rise to hum. There are two ways of overcoming this: one is to take the screened lead to chassis at one end only (experiment will decide which end), and the other is to insert a small 1:1 ratio transformer in the screened lead so as to isolate one chassis from the other. An isolating transformer of this type is essential if either equipment has a live chassis.

Accessories

As the basis of the method used for recording directional effects upon the tape relies upon being able to listen to one track whilst recording on the other, three accessories are very useful. One is a pair of headphones adapted for stereo. The high resistance type with 2000Ω impedance per headpiece is the best type to use, and each pair of leads should be separated and extended separately from the junction. The A channel phone is plugged into the "monitor" socket of the tape recorder, and the B channel phone is connected to the output of the pre-amplifier in place of the lead to the radio It is advisable to identify with labels the A and B phones and their associated leads, remembering that it is possible to reverse the channels by means of the switching unit, and at the same time to put the phones on the wrong way round.

The third accessory is C1, a 0.1μ F capacitor This is merely a piece of stiff thin card cut to a shape which will fit around the erase head to prevent the tape from coming into contact with it. It is fitted for two reasons: to avoid erasing the A track whilst recording the B track, and for superimposition so that speech, for example, can be laid on the top of music already recorded. (If the recorder is a 4-track model and has superimposing facilities which cut out the erase head.

there is no need for an erase head guard.) The third accessory is C1, a $0.1\mu\mathrm{F}$ capacitor which is fitted close to the input to the pre-amplifier and which can be plugged into a small socket fitted as near as possible to the grid pin of the first triode: in the author's case this enables one track to be heard whilst recording on the other. It may well be that in other tape recorders, C1 is not necessary, but theory tends to sunport that it is. Its purpose is to by-pass the bias current induced into the adjacent (listening) head from the recording head, which is of sufficiently high an order to overload the first stage of the ECC83

pre-amplifier. The inserting of C1 into the grid circuit naturally muffles the tone of the second channel but there is adequate volume and clarity to enable the output to be understood and for cues to be picked up from it. Without the capacitor absolutely nothing can be heard. (The author has tried various forms of tuned rejector circuit but without any success, due mainly to self oscillation of the circuits when the rejectors were added.)

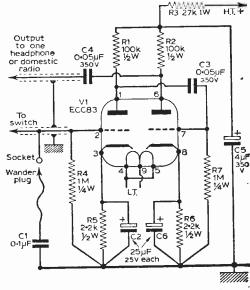


Fig. 2—The circuit of a channel B pre-amplifier.

Making a Simple Recording

To make a simple stereo recording the tap must first be erased on both tracks and then the erase guard should be fitted over the erase head as this is no longer required. Many readers wil realise that these preliminaries are not absolutel essential provided that track not covered by the single erase head has been wiped clean, but it has been found that starting with a clean tape anshielding the erase head reduces the number of mistakes that can be made.

With the erase guard still in position make test recording to check levels, etc. The quicker and most effective way is to record a spell c television advertisements from the ITA channe switching the head selector switch betwee separate advertisements. If this is satisfactory proceed to make the desired recording, workin from a script as in this simple example:

L.H. Channel (B)	R.H. Channel (A)
	Yesterday upon the stair
I met a man	Who wasn't there.
He wasn't there	Again today.
I wish that he would go	Again today. I wish that he would go away.

With the erase guard in position and the selector switch connecting the main record/replay amplifier to track A (as for monaural recording) set the recorder to record from microphone and say "Yesterday upon the stair," then pause, saying to yourself, "I met a man," then say aloud "Who wasn't there"; pause for "He wasn't there," say aloud "Again today, I wish that he would go away."

Stop the recording, wind back to the beginning, connect the headphones so that the tape may be monitored on both channels, reverse the head

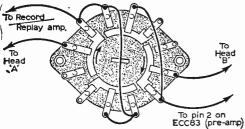


Fig. 3—The wiring details of the switch unit shown in the same position as in Fig. 1.

selector switch (move two positions in one direction) so that the main record/replay amplifier is now connected to track B, plug in capacitor C1 and, with the erase guard still in position, record the left-hand channel speech whilst listening to the right-hand channel thus: Listen for, "Yesterday ipon the stair", and then say "I met a man", wait for "Who wasn't there", say "He wasn't there", isten for "Again today", and then in unison, "I wish that he would go away".

Stop recording, rewind, remove erase guard and 21, switch the head selector switch back to its priginal position and replay. You should now have a stereo type recording sufficiently useful to mable balance and phasing tests to be made.

tereo Sound Cine Films

More ambitious recordings can be attempted nd provided they are scripted beforehand, realistic onversations may be taped in this way. An effecive use of this form of stereo is the production f accompanying sound to cine films. Here, with ne usual mixture of music, effects, and commenary, effective results can be produced, and in view f the increasing popularity of this home enterainment combination a brief description of the echnique used by the author may be of interest readers. Similar methods may be employed to nake demonstration or entertainment tapes in ound only, and these are somewhat easier to prouce since the timing is not so critical. Two things nould be emphasised here; one is that smooth esults can only be obtained by careful planning nd adequate rehearsal, and the other is that misikes can so easily be made due to the compli-ated "set up" and so all switching operations nould be double checked at each stage of record-

lethod of Recording

To make accompanying film sound, the tape tould first be wiped clean on both channels by

recording with the gain control at zero. Then fit the erase head guard and record a "timing scale" on channel B by speaking the time every five or ten seconds into the microphone. Rewind the tape and switch to channel A. Set up the film in the projector so that the beginning of the film and the start of the tape timing scale coincide, and run through the film talking the scenes down on to track A.

This might sound something like: "Opening title, cut to pan shot of bay, M. and J. walking in the background, medium close-up of M. and J. coming towards camera, car passes NOW..."

From these combined monitor tracks the sound script is drawn up. It is essential that the whole tape is scripted in full details on both channels before recording is started, so that the exact sequence of laying on the final sound can be planned. In the "end product" the commentary or dialogue should predominate over the effects and music are to be heard together the effects should be the louder. It follows from this that the music should be laid on first, the effects over the music, and the dialogue on top of the two. Too much sound will tend to be confusing, and it is better to use either effects or music as a background rather than a mixture of the two. Dialogue should be marked on the tape at this stage with marking

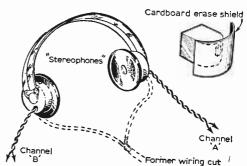


Fig. 4—Two accessories used in the recording process.

tabs or small strips of jointing tape, as the recording of the music and effects will wipe out the monitor tracks with their cue points. Before recordings can be made on track B the tape will have to be turned over and wiped clean of the timing track, and it is better to erase only one portion at a time just prior to recording so that accurate monitoring facilities are retained as long as possible. Except for the erasing of the monitor tracks the erase head shield should be fitted at all times.

Effects

The recording of stereophonic effects is quite entertaining and some realistic noises can be produced. One method is to set the recording head switch to mid-position and record the whole sound effect on both tracks, subsequently working over it and erasing certain noises from one track and other noises from the other.

(Continued on page 508)



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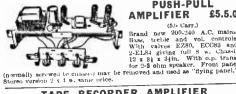
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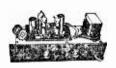




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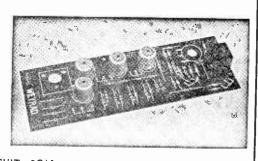
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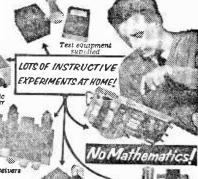
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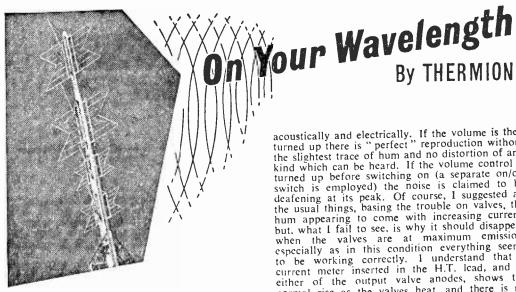
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Power supply circuits

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By THERMION



Those Electronic Games Again

THE response to my recent remark on the above subject has been amazing, and I am afraid that I cannot answer individually all those who have been kind enough to send me letters, articles, and drawings covering almost every aspect of this subject. I have passed many of them on to the editorial section of this paper to see if any of them are suitable for publication and no doubt use will be made of some of the very wide range of material which has been supplied. The only point which surprises me is that this response was not forthcoming when I first wrote about it and it was only after I had pointed out this fact that so much interest appears to have been aroused.

Unusual Faults

When I have mentioned particular faults in past issues I have been surprised at the interest which has been taken and the novel way in which some of my readers have offered solutions to the problems mentioned. I recently heard of another of these peculiar faults which leaves both the amateur concerned, and my humble self, deeply mystified. The apparatus in question is part of a home-built radio-gram which has been in use for many years. The amplifier section has now developed a fault which is baffling and does not appear to answer to all normal tests. It is of the 20W class, with two KT66's in the output stage, and all condensers are of the paper type (no electrolytics) rated at 1,000V, although the H.T. line is only 350V. The fault takes the following form: when the amplifier is switched on there is the usual short period of silence whilst the valves are warming up and then a most terrific hum builds up. This reaches a peak and then slowly fades away to complete silence. This is, of course, with the volume control turned to minimum and in this condition the amplifier is inaudible,

acoustically and electrically. If the volume is then turned up there is "perfect" reproduction without the slightest trace of hum and no distortion of any kind which can be heard. If the volume control is turned up before switching on (a separate on/off switch is employed) the noise is claimed to be deafening at its peak. Of course, I suggested all the usual things, basing the trouble on valves, the hum appearing to come with increasing current, but, what I fail to see, is why it should disappear when the valves are at maximum emission, especially as in this condition everything seems to be working correctly. I understand that a current meter inserted in the H.T. lead, and in either of the output valve anodes, shows the normal rise as the valves heat, and there is no indication of a sudden rise or fall accompanying the cessation of the hum.

Progress?

I had an opportunity of inspecting some of the new season's models which were shown at this year's Radio Show before it opened, and must confess I was not a little surprised at what I consider is a lack of progress in general design. The same old printed circuit seemed to be generally adopted, and there did not appear to be any of the modern component design incorporated in the majority of them. One particular component which has now been on the market for some years, appeared to be conspicuous by its absence, and I have tried to locate its use in many of the receivers which have been produced during the last two or three years, but must confess that I cannot find even one. I suppose the reason is that the printed circuit has taken over, although I feel that there is more scope in the particular item I refer to. This is, of course, the turret valveholder. This enables all the main components associated with a particular valve to be mounted round the actual valve base. The particular component I have in mind also has, at the lower end, a set of valve pins corresponding to the particular socket and this enables the valves to be inserted in the holder and the entire assembly may then be removed or replaced, which greatly facilitates experimental work.

Read the new Practical Mechanics and Science The October issue on sale 28th September

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A HOME-MADE

HI-FI OUTPUT TRANSFORMER

THE USE OF A TERTIARY FEEDBACK WINDING ARRANGEMENT SIMPLIFIES THE CONSTRUCTION OF THIS TRANSFORMER AND REDUCES THE COST.

BY W. GROOME

(Continued from page 400 of the September issue)

N last month's article the author began an explanation of his home-made transformer which included descriptions of some interesting circuits for its use. In Fig. 4, for example, a triode "see-saw" phase-splitter amplifier stage feeds the output pentodes. The tertiary winding, earthed one end, supplies feedback to V1 via R2 and provides a path for the cathode current.

If pentodes were used for splitter stage the sensitivity, held back ratio, would remain the same. ratio, and with it the amplifier sensitivity, can be made variable by shunting the tertiary winding with a 100Ω potentiometer and taking the feedback voltage from the tap, as shown in Fig. 5 (last month). This refinement may be of interest to some experimenters, but the triode circuit will be found suitable for most domestic purposes. The ECL82 valve, comprising an amplifier triode and an output pentode enables a two-stage push-pull amplifier to be built around only two valves—and stereo using only four valves becomes a practical proposition.

Cathode Follower Output

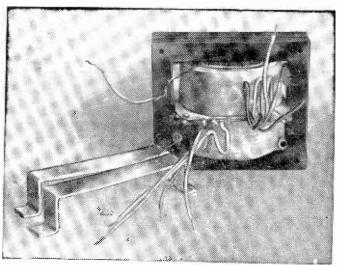
The improvement achieved by the use of feed-back over the output stage (apart from easing the application of overall feedback) is a 'natural sound' that is not likely to show up on instrument tests. It is real enough, however, and the once-popular cathode-follower circuit with its virtually complete cancellation of its own distortion

and immunity from the errors that can arise in a complex loop, gives a realism that is still hard to better. Its limitation to triode efficiency and the arge grid voltage swing needed for full loading have caused it to decline in popularity and designs more suitable for pentodes have become more popular.

These are the "distributed load" circuits, of which the quaintly named ultra-linear version is sest known. As the author's transformer has both secondary sections split into two well-insulated

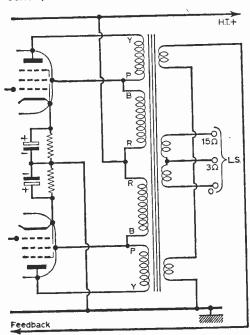
sections with free leads, it can be connected in the ultra-linear mode as shown in Fig. 7. It is true that the tap at 50% is higher than is customary but this closer approach to triode conditions has not been found to be the slightest drawback.

Ultra-linear connections are not the only, or even the first, form of distributed load circuit, for a more elegant circuit was developed in this country several years before the 'ultra-linear' circuit appeared. However, the version shown in (Fig. 7) embodies cathode loading which, as stated



One of the author's prototype experimental output transformers.

in an earlier paragraph, is a highly desirable method of obtaining output stage feedback. Despite the strangeness, on paper, of a load distributed between anode and cathode, the relationship to the ultra-linear arrangement can be appreciated when the screen is considered, this being tapped into the transformer load in both cases. This is obvious in the ultra-linear circuit; in Fig. 7, it is still loaded by the transformer because its current and signal are compelled to flow in the cathode winding.



50:50 Distribution

This form of loading can be tried by connecting the transformer as indicated in Fig. 8. Bear in mind, however, that the output circuit is patented. The transformer and its associated circuits must not be compared with a well-known make of amplifiers to which this form of loading is exclusive. As 50:50 load distribution must be used, the

stage feedoutput back is already nearly enough to give the required reduction in distortion and output impedance and the amount needed in the overall loop is there-fore small. For this reason, a potentiometer is shown across the feedback winding in Fig. 8, which shows the ECL82 circuit modified for this form of loading.

As the grid resistors are returned to earth (via the grid resistor of V2A) the .D.C. resistance of the cathode loads contributes towards the bias voltage of the output

Fig. 7 (right)—Here the load is distributed between the anodes and cathodes.

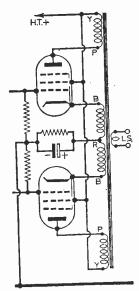
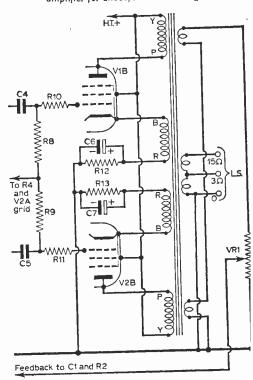


Fig. 6 (left)—Connections for ultra-linear loading.

Fig. 8 (below)—Rearrangement of a two-stage amplifier for anode/cathode loading.



resistance of these portions The valves. the windings should therefore be checked ar reduce bias resistors of the value of this for variation Α correspondingly. of distributed loading has the grid resistors co nected to the cathode ends of the load and adjustment of the bias resistors is needed. It not really suitable for use with a see-saw phas splitter, but can be driven by a "concertina circuit either in the straight form or in the hig gain versions, one of which employs the inp resistance of the phase-splitter to load an amplifi pentode, and another using the pentode in starv tion anode conditions. This phase-splitter c also be used in a positive feedback circuit f high gain but it is preferred to keep the sign 'clean" at every stage rather than have to cle up an accumulation of distortions with the ma feedback loop.

Input Signal

Now that crystal pick-ups have reached his fidelity standard, with outputs so much greathan the magnetic types that were once essent for the discriminating listener, and radio tunalso deliver large signals, there is no longer urgent need for great sensitivity in the domeion amplifier. Indeed, amplifiers requiring as much as 4V input can be fully loaded, for the signals with the discriminant of the signals with the signals with

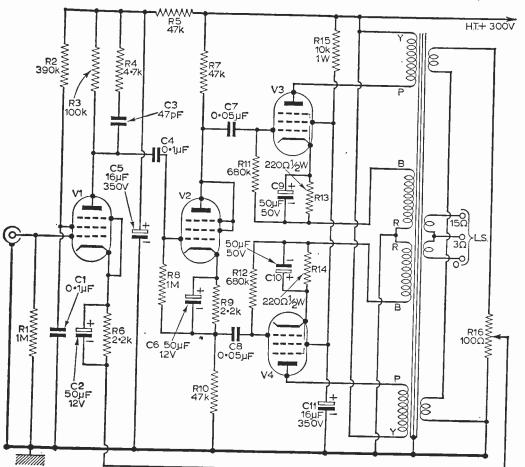


Fig. 9—A three-stage amplifier with another version of anode/cathode loading.

almost always passed through a pre-amplifier ontrol unit first, and a highly sensitive amplifier uld be hopelessly overloaded.

The straignt pentode and concertina circuit own in Fig. 9 will give all the gain likely to be eded. The grid resistors of the output valves e connected to the cathode ends of the cathode

ads. The front end can be altered if it is wished try one of the high-gain versions, without astic alteration of the remainder. The use of o A.C. couplings is not likely to cause instability th tertiary feedback, but direct coupling between I and V2 can be used by the constructor terested in the experiment. V1 and V2 could triodes, i.e., a double triode.

The transformer, of which constructional details Il be given in the next issue, has been used in variety of circuits, not all of which were conered desirable when matters of cost and ease adjustment were taken into account. All, hower, tended to prove the inherent stability of the tiary feedback system.

(To be continued)

P.W. SIGNAL GENERATOR

(Continued from page 482)

so on, at 200kc/s intervals, until the generator

harmonics are too weak to hear.

The fifth harmonic of 200kc/s will be 1,000kc/s, or 1Mc/s, and the generator may be tuned to this. Harmonics of the generator will then be heard at 2Mc/s, 3Mc/s, 4Mc/s and so on, at 1Mc/s intervals, until too weak to be found. It is, of course, necessary to have a receiver with short-wave ranges, for this purpose. By proceeding as described, calibration marks can be obtained at 1Mc/s intervals.

In many parts of the country the National Physical Labaratory signal on 2.5Mc/s can be received. This will furnish a 2.5Mc/s calibration of great accuracy. By proceeding as above, harmonics of this will furnish calibration marks at 5Mc/s, 7.5Mc/s, 10Mc/s and so on, at 2.5Mc/s intervals.

INCREASING

AMMETER

RANGES

By G. A. W. Partridge

OST radio dens have milliammeters or multimeters but not always ammeters. However, a good milliammeter will make a useful ammeter provided a reliable shunt is used. There are times when it is desired to measure the currents of heaters, small motors or such other apparatus which may draw up to one ampere. In some cases it may not be necessary to increase the range to 1A but only to, say, 500mA, which will mean using a shunt of different resistance.

The resistance of a shunt can be calculated

from:-

$$R = Rm$$

Where R is the resistance of the shunt, Rm is the internal resistance of the meter and n is the multiplification factor.

For example, a 0-1mA meter is to be used in a 1A circuit. Its internal resistance is 50Ω . What then will be the resistance of the shunt?

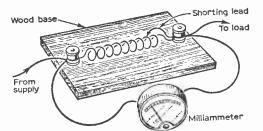


Fig. 1—Connecting a shunt across a milliammeter.

The range of the instrument will be increased 1,000 times, so n will be 1.000.

required here. If the shunt had an error of 0.01 it would make the meter inaccurate by 20%. A shunt of this type would also have to be robust as it has to remain accurate over a long period of

time. There are special types of shunt on the market which are very reliable. However, for reasonable accuracy a shunt can be made up and used for ordinary purposes. Fig. 1 shows a shunt connected to a meter. It is mounted on a hard, dry wooden base between two terminals. Note the copper shorting lead which is for calibration purposes. If resistance wire at one ohm per yard

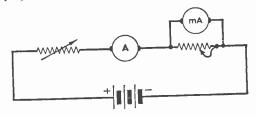
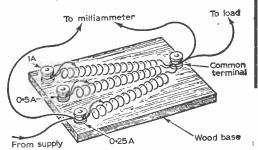


Fig. 2 (above)—The calibration circult.
Fig. 3 (below)—Multi-range shunts.



is chosen an 0.05Ω would require 1.8in. About 2in. should be used and calibrated as shown in Fig. 2. A reliable ammeter is the standard. The rheostat is adjusted until 1A is flowing through the circuit. The shorting lead is soldered on to various points along the shunt until the milliammeter reads full-scale deflection. The leads to the milliammeter that were used when calibrating the shunt must always be used as their resistance is part of the milliammeter circuit.

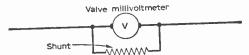


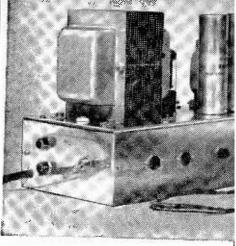
Fig. 4—A valve millivoltmeter as an ammeter.

If various ranges are desired, several shunts can be made up and mounted as shown in Fig. 3.

A.C. milliammeters are not very common bureaders who happen to have such instruments wil have to calibrate their shunts on the frequency that they intend to use. A.C./D.C. instruments will have to have separate shunts for D.C. and A.C. because it is only the internal resistance tha affects the D.C. calibration, but the internal impedance determines the calibration in A.C. work Valve millivoltmeters can also be used a ammeters or milliammeters for A.C. or D.C. work

(Continued on page 522)





OR a close approach to realism in sound reproduction an amplifying system must be capable of handling peak power levels greatly exceeding the average sound level, in order to accommodate transients.

Faithful reproduction of these transients is essential if the character and vitality of the original performance is to be retained. It is generally considered that a power reserve of 15-20W is desirable for a good quality reproduction system, and the full range of audible frequencies should, of course, be amplified with negligible distortion or frequency

discrimination.

The Strand amplifier has been designed to meet such requirements. The circuit contains several well known features including a distributed loading push-pull output stage. This arrangement enables an output of 20W to be obtained for an input of 0.225V, with, 30dB negative feedback applied overall. An output of nearly 30W is obtained before overloading occurs. The frequency response characteristic at the rated output of 20W is flat within ± 0.5 dB from 30c/s to 2kc/s.

A two-unit form of construction has been adopted as this avoids the use of what might be an inconveniently large single chassis, and also has the advantage of providing more flexibility when planning the installation of the equipment. Furthermore, good separation of the power supply components and the amplifier proper is always desirable as this reduces the chance of hum being

induced into the input stage.

Input Stage

A high degree of voltage amplification is obtained in the first stage, with a good signal-tonoise ratio due to the use of a low-noise pentode type EF86. Negative feedback is applied to the cathode of this valve from the secondary of the output transformer, via a high frequency attenuation network, C10, R14 (see Fig. 1a on Blueprint).

It should be noted that high stability cracked carbon type resistors are specified for the anode,

screen and cathode circuits of V1.

The anode of this voltage amplifier is directly coupled to the grid of V2A. The absence of a coupling capacitor reduces phase shift and ensures good stability at low frequencies.

Phase Splitter and Driver

The double triode V2 (ECC83) functions as a phase splitter and a driver stage for the output valves. The two cathodes are connected to chassis via a common resistor R8, and the valve operates as a cathode-coupled phase splitter. This type of phase splitter has a particularly good performance at higher frequencies. The grid of the second triode section, V2B, is earthed by C6, and the operating conditions are determined by the D.C. potential applied via R6.

Output Stage

A pair of EL34 pentodes, V3 and V4, form the push-pull output stage. These valves are operated under distributed load conditions. In this method of operation, also known as "ultra linear", the screen grids of the two output valves are not connected directly to the H.T. supply but are taken to tappings on the primary of the output transformer. These tapping points are arranged so that approximately 20% of the primary winding is between the anode and screen grid circuits in each

Output Transformer

The performance of any amplifier is very largely determined by the characteristics of the output transformer. The output transformer used in this amplifier has a 7.000Ω primary, with a centre tap and screen grid taps at 20%. A high primary inductance of 225H ensures good low frequency performance, while excellent response at the high frequencies is attained through the use of sectionalised primary and secondary windings, which reduce the leakage inductance to about 14mH.

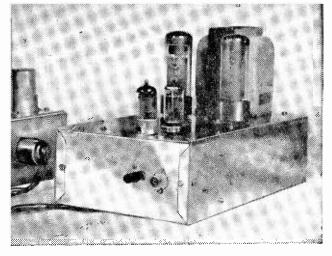
The transformer is capable of delivering the full rated output of 20W over the frequency range 30 to 20kc/s and upwards. The low frequency cut-off point is 5c/s. Resonance occurs at 90kc/s and is thus well beyond the audible range.

Power Supply

H.T. and L.T. supplies are fed into the power amplifier by a four-core cable which is terminated

in an 8-way octal plug PL1.

All power supplies are obtained from the mains transformer T2. H.T. rectification is performed by V5 (GZ34) and filtering by L1, C13 and C14. The



THE CIRCUITS AND WIRING DIAGRAMS FOR THIS AMPLIFIER AND ITS POWER PACK ARE GIVEN ON ONE SIDE OF THIS MONTH'S BLUEPRINT.

By F. E. BENNETT

smoothed D.C. output is approximately 465V. Protection is afforded against overload or short-circuit of the H.T. line by the 250mA fuse, FSI. The H.T. positive line and the common earth return are connected to SK3, pins 4 and 6 respectively; the 6.3V 5A winding on T2 is connected to pins 1, 2 and 7, 8 on this socket.

The H.T. consumption of the main amplifier is about 140mA, and since the 410-0-410V winding is rated at 180mA, a further 40mA may be drawn via the two 5-way sockets SK4 and SK5. Pin 3 of each of these sockets is connected to the main H.T. line via a separate dropping resistor, and a $16\mu F$ smoothing capacitor is connected across each auxiliary H.T. output.

The values of R25 and R26 may of course be varied to meet the requirements of a particular preamplifier, radio tuner or other auxiliary equipment, but the total H.T. current drawn from these outlets must not exceed 40mA.

The second 6.3V winding on T2 is connected to pins 1 and 5 of SK4 and SK5, while the centre tap of this winding is taken to chassis, as is pin 4 on both of these sockets. The maximum current available from this 6.3 V supply is 2A.

Note: a supplementary L.T. supply of up to 1.5A may be drawn from the 6.3V 5A winding since the main amplifier valves consume a total of 3.5A. The modification required would be to disconnect the wiring between pins 1 and 5 of SK4

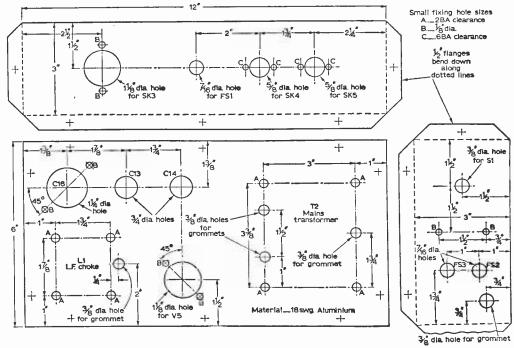


Fig. 4-The drilling details of the power pack.

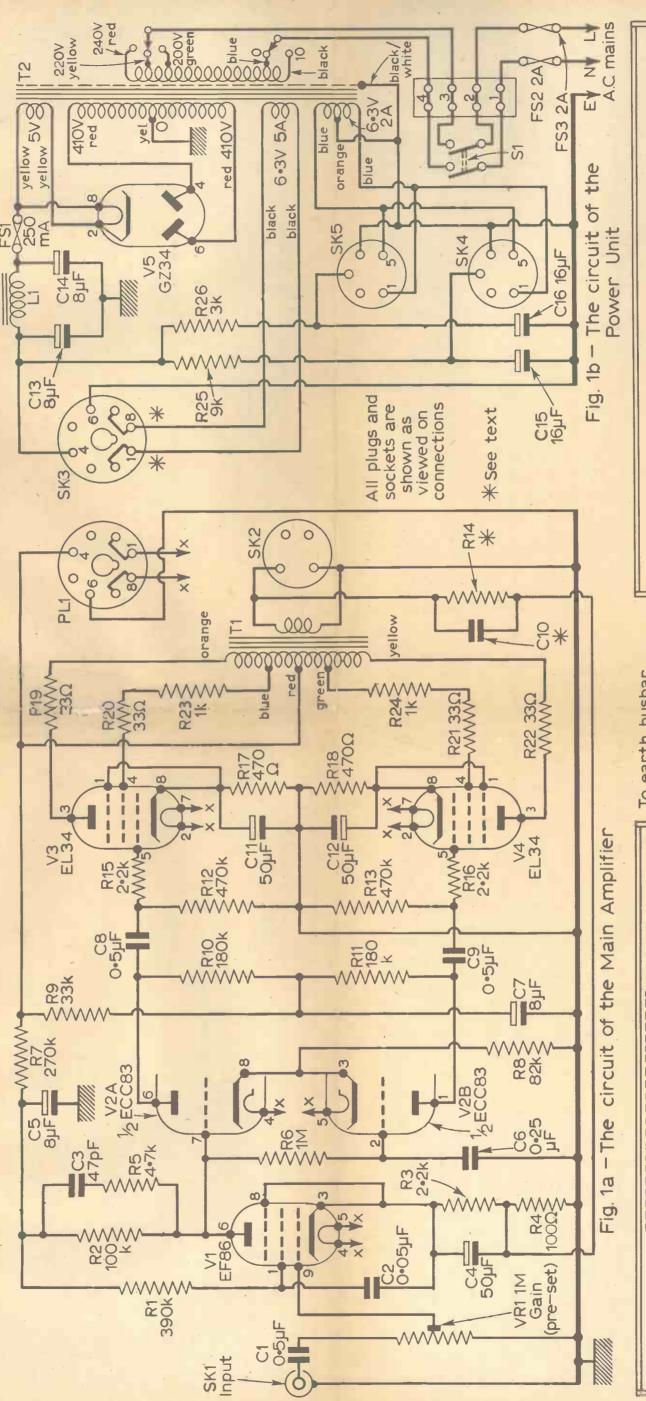
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"PRACTICAL WIRELESS"

OCTOBER 1962

Wireless Practical

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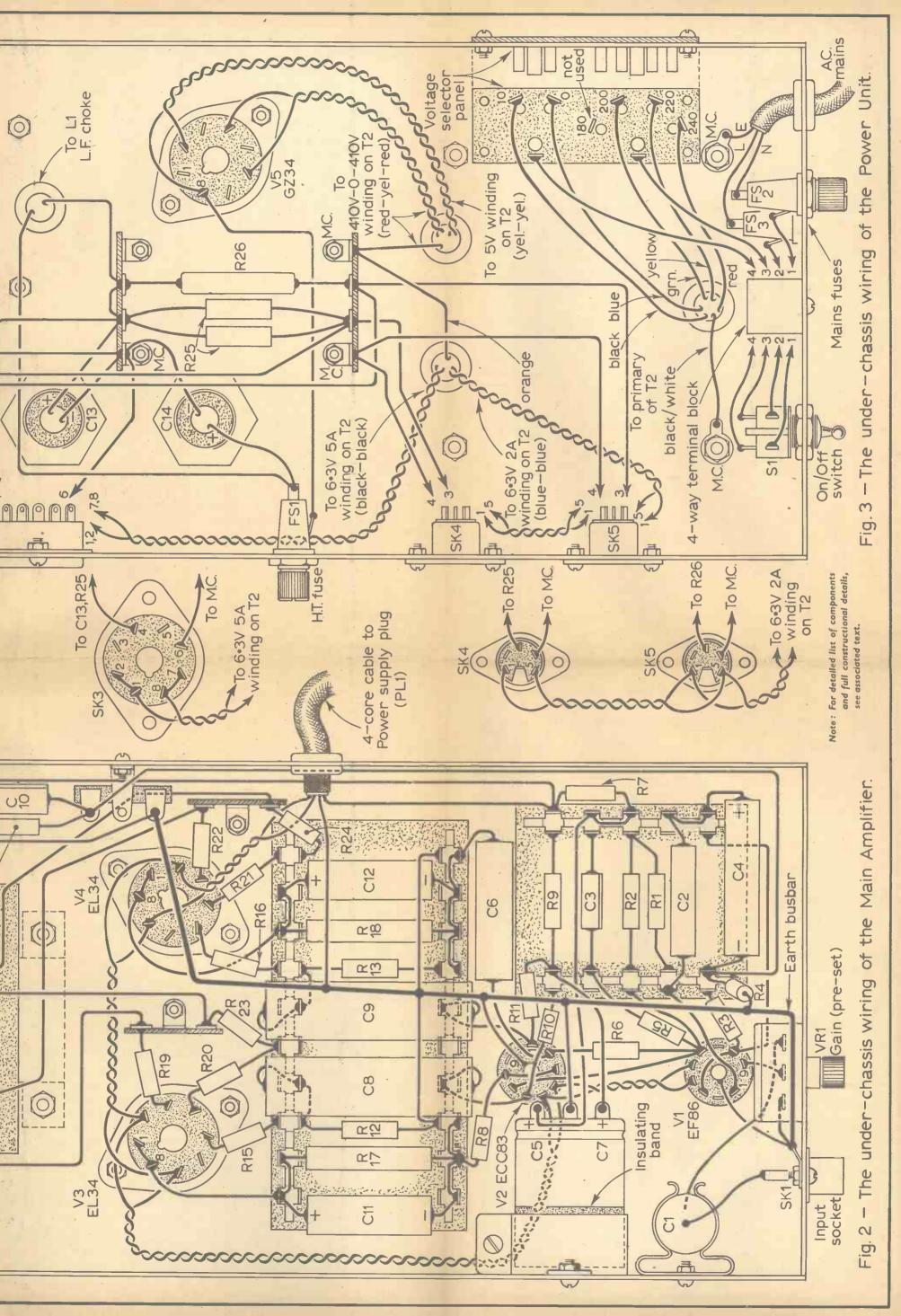
(0) SK2 To earth busbar To C10,R14 SK2 transformer Output が上級 green ne primary 0 Syellow red orange dimensions 12"x 6"x 3" Chassis

0

Tags marked 'M.C.' denote earthing connections to chassis

0

Chassis dimensions 12"x 6"x 3"



and SK5 and then to connect pins 1 and 5 of SK4

to pins 1 and 8 of SK3.

The 4-way terminal block is included in the mains input circuit in order to facilitate the transfer of the mains switch S1 to an associated pre-amplifier if remote control is required.

Construction

The main amplifier and the power supply are built on separate chassis. Both chassis measure 12in. x 6in. x 3in. and can be constructed from 16 or 18s.w.g. sheet aluminium, or may be pur-

Where the installation demands some other arrangement, one chassis may be turned through 90° with respect to the other, provided that the two units are spaced apart.

Assembling the Power Unit

Complete all drilling according to Fig. 4 and remove any burrs. Mount the components, commencing with the smaller items and dealing with the sides before the top of the chassis. The mains transformer and the choke must be securely

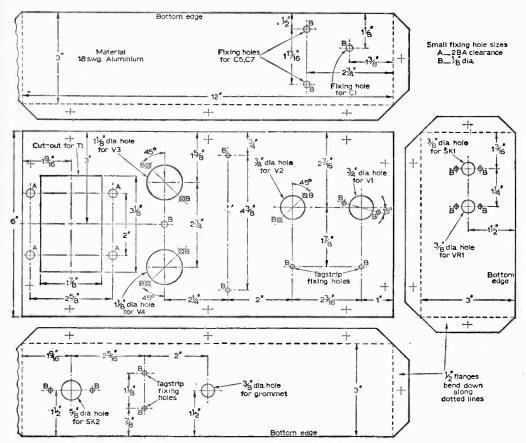


Fig. 5—Drilling dimensions for the amplifier chassis.

chased in prefabricated sections requiring only bolting together.

The arrangement of components and wiring shown in Figs. 2 and 3 (see Blueprint) has proved very satisfactory and should be adhered to as

closely as possible.

The orientation of the mains transformer, smoothing choke and output transformer should be particularly noted. It will be seen that when the two chassis are side by side—thus providing the most compact installation—the core of the output transformer is at right angles to the core of the mains transformer and choke, and hum pick up is reduced to the minimum.

bolted in position, with washers beneath the bolt heads and nuts. Fit rubber grommets to the three holes adjacent to the mains transformer; also to the hole at the side of the choke, and to the hole for the mains cable in the front side panel.

Feed each of the three groups of leads from the mains transformer through the appropriate grommet hole, then proceed to wire up, checking the colour coding of these leads with the circuit diagram (Fig. 1b) and the wiring diagram (Fig. 3) Pay particular attention to the heater leads. Eac' pair should be tightly twisted and then be run close to the chassis, in the angle of the sides and top wherever possible.

Assembling the Power Amplifier

Refer to Fig. 5 for details of the chassis drilling. Proceeding around the sides of the chassis, fix in position the following items: clips for capacitors C5/C7 and C1; input socket SK1 and gain control VR1; and 3-way tag strip and output socket SK2. Mount the valveholders, ensuring that a skirted, low-loss B9A holder is atted in V1 position. Fix the 10-way and 5-way group boards, and the two 3-way tag strips to the underside.

Wire the heater circuit to the valveholders using lightly twisted leads. Run these leads close to the

chassis.

Mount the output transformer and securely bolt n position. The group of eight terminal posts on the underside of T1 must be adjacent to the output socket SK2. Indentify the primary leads and connect these as shown in Fig. 2.

Now proceed to complete the amplifier wiring stage by stage, starting at SK1. Pins 2 and 7 on the valveholder of V1 must be connected to the centre spigot. Avoid overheating the high stability resistors when soldering these components in position. To facilitate the wiring operation, the dual electrolytic capacitor C5/C7 should not be placed in position or connected up until all the other components associated with V1 and V2 have been wired in position. Furthermore, note that the metal can of this capacitor must be isolated from chassis by means of an insulating band fitted around the lower part of the can. Ensure that the bottom of the can is clear of the chassis before tightening up the clamping screw. The earth busbar should be ignored until all the foregoing work has been completed.

The method of ascertaining the appropriate avalues for R14 and C10 is dealt with later.

Earth Busbar

It will be noted that an earth busbar is used for all earthing connections in the amplifier chassis. The busbar is earthed to the chassis at one point only—this being close to the input socket SK1. This arrangement minimises hum picked up from currents circulating in the chassis. The busbar should be made from a length of 14 or 16s.w.g. tinned copper wire. This wire should be stretched out so that it is straight and rigid. Solder a tag to one end of the wire and secure this to one of the screws holding the input socket SK1 in position. Make a sharp bend about 1½in. from this anchored end of the wire, and make another about 7in. further along but in the opposite direction so that the free end may be anchored on

COMPONENTS LIST

```
Resistors (All 10\% \frac{1}{2}W unless otherwise stated)
        390k high stability, cracked carbon
  RI
  R2
        100k high stability, cracked carbon
  R3
        2.2k high stability, cracked carbon
        100\Omega 5% high stability, cracked carbon 4.7k R7 270k R9 33k
  R4
  R5
        4.7k
                       270k
  R6
        IM
                R8
                       82k
        180k Matched to within 5%
  RI0
        180k S
  RH
  RI2
        470k Matched to within 5%
  RI3
  RI4
        see text
                     R15 2-2k
                                     R16 2.2k
        470Ω 5% 3W w.w.
  RI7
        470\Omega 5% 3W w.w.
  RI8
                     R21 33\Omega
                                     R23 Ik
  RI9
        33\Omega
                     R22 33(2)
  R20
                                     R24 lk
        9k 2W (2 x 18k IW in parallel, see text)
  R25
          3k 3W w.w. (see text)
  R26
  VRI
        IM carbon potentiometer (pre-set)
Capacitors
  CI
        O·5µF paper 350V
  C2
        0.05µF paper 350V
  C3
C4
        47pF silvered mica \pm 10\%
        50μF elec 12V
  C5
C6
        8\muF elec 500V (dual section with C7)
        0·25μF paper 350V
  C7
        8μF elec 500V (see C5)
        0·5μF paper 350V
0·5μF paper 350V
  C8
                              Ċ12
                                  50μF elec 50V
  C9
                              CI3
                                   8μF elec 600V
  CIO
                              CI4 8µF elec 600V
        see text
  CII
        50μF elec 50V
        16\mu F \over 16\mu F  dual elec 500V
  C15
  C16
Valves
        EF86
                   V3 EL34
                                   V5 GZ34
  VI
  V2 ECC83
                   V4 EL34
```

```
Choke
        L.F. choke 10H 180mA 200\Omega (Gilson
  LI
        W01341 WES)
Transformers
        Output transformer. Primary 7000\Omega,
  TI
        centre tap, 20% screen grid taps. Secondary 1.7, 3, 7, and 15\Omega (Gilson
        W01932)
        Mains transformer, with tapped primary,
  T2
        200-250V. Secondaries 410-0-410V,
180mA; 5V 3A; 6-3V 5A; 6-3V CT 2A
(Gilson W01566WES)
Fuses (sin. miniature fuse cartridges)
                   FS2 2A
                                   FS3 2A
        250mA
  FSI
Switch
        D.P.S.T. Toggle.
  SI
Sockets
  SKI
        coaxial (Belling Lee L604/S); free plug
        (L734/P/AC)
        4-way, with plug and cover (Cinch)
  SK2
        8-way (octal valveholder)
  SK3
        5-way (T.S.L. B5B); free plug (T.S.L.
  SK4
        A5B)
  SK5
        5-way (T.S.L. B5B); free plug (T.S.L.
        A5B)
Plug
  PLI Octal plug
Miscellaneous
  Three fuseholders (Belling Lee L575). Valve-
  holders: three octal; one ordinary B9A and
  one B9A nylon loaded with screening skirt (for
  VI). One 10-way and one 5-way group boards
  (Bulgin C114 and C109). Three 3-way and
  two 4-way tag strips. One 4-way terminal block (Grelco). Two chassis 6in. x 12in. x 3in.
```

(Home Radio Ltd.). One voltage selector

Capacitor

(Cinch 75/881).

panel

grommets, etc.

the 3-way tag strip which is mounted on the side of the chassis.

The various earth connections can now be made to the busbar. This is best performed by proceeding systematically from the input end of the chassis, and checking with the under-chassis wiring diagram. Tinned copper wire of 18 to 22s.w.g. is suitable for the branch leads.

Output Impedance

The eight terminals on the secondary of the output transformer T1 may be connected in various ways in order to provide output impedances of 1.7Ω , 3Ω , 7Ω or 15Ω . Details of these connections and impedances are given in Fig. 6.

The component values for the H.F. attenuation network. R14, C10, in the negative feedback loop are dependent upon the loud-speaker impedance, and should be selected accordingly from the table below.

Ouput 1	Impedan	ce R14	C10
	3Ω	3.9k	470pF
	7Ω	5.6k	330pF
	15Ω	8-2k	220pF
R 14 mi	ist he a	5% high	stability

resistor.
C10 must be a 5% silvered mica capacitor.

Hum

Negligible hum has been experienced with the heater supply to the amplifier valves unearthed,

as shown in the diagrams. It cannot, of course, be assumed that this will prove to be so in all cases, since minor variations in the layout of components or wiring can upset the hum balancing properties

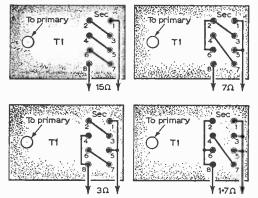
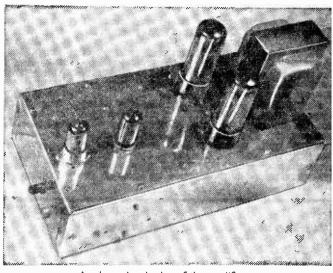


Fig. 6—The transformer connections.

of the circuit. If hum does become troublesome, experiments should be made in earthing (to the busbar) one side of the heater circuit, firstly at V1 valveholder and then at other valveholders in turn. If this does not effect a cure a potentiometer connected across the 6.3V supply in the power unit (wired to pins 1 and 8 of SK3) with its slider connected to chassis may eliminate the hum. A

 100Ω wire-wound potentiometer should be suitable for this purpose.

The amplifier must not be put into operation without a loudspeaker, or a suitable dummy load, connected to the output socket. In the event of a "howl" from the loudspeaker, turn the gain control to minimum and switch off immediately. This "howl" will indicate that the feedback loop is connected in reverse sense—and positive feedback



An above-chassis view of the amplifier.

is in fact being applied. The remedy is to change over the two leads that connect the outer secondary terminals on the ouput transformer to the socket SK2.

A Stereo EXPERIMENT

(Continued from page 496)

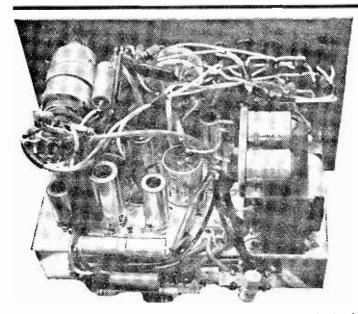
Alternatively a fairly lengthy effects sequence (such as "sea with seagulls") can be laid on one track starting from the beginning, and then on the other track staggered by playing the effect through about 10 or 15 seconds before commencing to record it. The commentary, which goes on last of all will normally need to be inserted "blind", relying on the cue marks affixed with sticky labels whilst the monitor track still exists. These labels should subsequently be peeled of to reduce the chance of the tape catching in the head as they pass through.

Mistakes

Finally, the correcting of mistakes. This car often mean starting all over again, and much patience is needed if it does. Single words or very short sentences can be recorded in place of existing matter without the absence of the few note of background music or effects being noticed. I the sound on one channel drowns the commentar on the other it may be softened by running through the recording lead, with crase guard fitted with the instrument switched to record and the level at zero.

THE

MINISCOPE



(Continued from page 412 of the September issue)

N his description of the circuit, begun last month, the author referred to the advantage of the cathode-follower input stage of the signal amplifier, which is that considerable shunt capacity is tolerable here without high-frequency loss. This has the further advantage that the gain-control does not affect the anode current of the cathode-follower stage, as it appears subsequent to it, and thus the anode current can be passed through a moving-coil meter for simultaneous use of the cathode-follower input stage as valve-voltmeter for D.C. For this purpose the signal input is D.C.-connected, which is fully permissible on account of the large acceptable input level.

The input cathode-follower will accept a drive of 60V peak to peak without distortion under the operating conditions adopted here. All calibrations are made to apply for and include the characteristics of a special probe head with a dividing ratio of about 15:1 (the construction of this probe and discussion of the reasons for its necessity will appear in a later article). The Miniscope should not normally be used without this probe. The actual acceptable input maximum

By M. L. Michaelis

is thus about 900V peak-topeak A.C., D.C. or mixed, which is ample for all normal purposes.

With the linear design range of 60V p.p. for the input cathode-follower, and a cathode resistor of roughly 30k (R53), the anode current swing will be 2mA. The resting anode current should be just a little more than half of this, so that the valve just does not cut off on negative peaks, and consequently a value of about 1.3mA has been chosen. This would require a positive bias of about 30V on the grid, or a corresponding negative bias to which the resistor must cathode returned, in order to set this desired operating point. The former alternative is intolerable,

as the positive grid bias would react back through the signal input into the test circuits and would even be nullified if the signal source had a low impedance. Thus, the cathode resistor R53 has been returned to a stabilised bias supply of about 35V, using two Zener diodes, D10 and D11. Stabilisation is here used to avoid undue slow or fast fluctuations of meter-zero and to avoid injection of timebase signals into the Y-amplifier as part of the same bias supply is used in the timebase circuits.

The meter movement used is a cheap surplus thermocouple R.F. meter, modified for normal moving-coil function (see "Experimenter's Power Pack", in the January 1962 issue). It is shunted to give 4mA f.s.d. and has zero-deflection as normal at the left. R51 and the potentiometer VR12 (meter balance) augment the no-signal standing anode current of the input cathode-follower to exactly 2mA, so that the pointer then stands at mid-scale, where "O" on the new scale is placed. To the left of this centre-zero the new scale is labelled "negative" and to the right "positive" and calibrated such that quarter deflection corresponds to minus 400V and three-quarters deflection to plus 400V. The scale is continued linearly to plus and minus 600V on each side respectively and a dot labelled "off" made at the actual mechanical zero on the left. The resistors in the probe are subsequently trimmed to make this scale hold true. The final

input impedance with probe will be about 2M in parallel with a few pF capacity.

R53 itself is not used as gain control, a separate potentiometer VR13 being fed via a coupling condenser C33 instead. There are two reasons for this. Firstly, if R53 were the gain-control it would be carrying D.C. and any movement of its slider would thus pass spurious transients on to the following high-gain amplifier chain. would cause intense fluttering of the trace on the CRT, causing it to jump temporarily right off the screen with everything but the slowest movements of the knob of this gain control. Secondly, were R53 itself the gain control, consider the conditions which would then prevail at "minimum volume" when the slider would be down at D11. It would then pick up the full ripple voltage from the bias

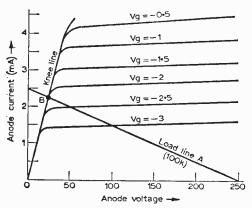


Fig. 2a—The anode-characteristic curves of a typical pentode valve, to explain the phenomenon of "bottoming." Under the conditions shown, the anode current cannot rise above 2.3mA, reached at -2V at the grid, however much the grid voltage rises further in a positive direction. The anode voltage thus "bottoms" at about 20V, represented by point B on the curves, as soon as the grid voltage reaches -2.

line and cause this to be amplified through the amplifier chain. Experiment showed that this ripple is just sufficient to give full-screen deflection on the CRT under these conditions. But, with the actual arrangement used for the gain control, VR13, C33 blocks the D.C., so that there is no flutter upon movement of the knob, and R53 and the low-internal impedance of the cathode follower form a ripple-voltage divider of about 300:1 reduction, which is thus the maximum (negligible) ripple-remnant passed on to the amplifier from the bias line, and it is further reduced, down to zero, as the slider of VR13 is slid down to chassis to reduce gain.

V1 triode (pins 1, 2 and 3) and V2 form a conventional R.C.-coupled three-stage amplifier. The average gain per stage is somewhat under 10 on account of the very small anode loads and the negative feedback given by un-by-passed cathode resistors throughout. Both these measures are necessary to obtain the required extension of level high-frequency response up to over 100kc/s. The small anode loads tolerate correspondingly

high unavoidable stray capacities before the timeconstant rises to the order of a period of a cycle of the highest frequency to be passed (the rough criterion for high-frequency amplification limit), and the cathode-negative feedback gives the usual additional linearisation, stabilisation and greater freedom from ageing and manufacturing tolerances of valves. The first stage of this amplifier chain has the lowest anode load (R50); subsequent stages cannot have such a low load on account of the need for the greater voltage swing at those stages and the final requirements for full deflection of the CRT (about 100V p.p. in the tube used in the prototype).

Note the generous grid-stoppers used at all stages, including the input cathode-follower.

Parasitic Prevention

A chain of high-slope triodes as used here in the signal amplifier is very unlikely to be stable if any arbitrary wiring arrangement is used. In fact, it is virtually impossible to make more than two stages of the ECC81/EC92 type of valve run stable if grid-stoppers are not wired very close to all grids and wiring otherwise kept very short and direct.

It must be remembered that cathode followers count as normal amplifiers for the purpose of parasitic oscillation considerations because the tiny distributed capacitive and inductive strays responsible for these VHF oscillations will make the stage appear as a normal amplifier or oscillator at VHF if all the stray virtual components were drawn in on the circuit and the cathodefollower arrangement at lower frequencies were disregarded.

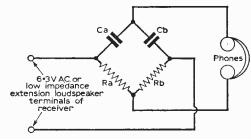


Fig. 2b—A simple method for trimming two condensers, Ca and Cb, to have exactly the same capacity ratio as the resistance ratio of two standard resistors Ra and Rb. Various small condensers are tried in parailel with Ca or Cb, until minimum sound is heard in the headphones.

The common manifestations of severe parasitics in high-slope triode chains can be of a form outwardly so puzzling that some further discussion is not out of place. The common symptom is namely, in a poorly-designed amplifier of this type, strong low-frequency motor-boating. The uninitiated experimenter will not attribute this to VIIF parasitics and will start looking for the " normal ' motor-boating-namely, causes of inadequate H.T. decoupling. He will then find, however, that the inclusion of large decoupling condensers or even feeding the stages from

(Continued on page 513)

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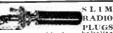
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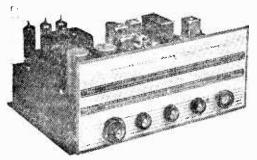
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(Continued from page 510)

entirely separate rectifiers and smoothing will

make virtually no difference.

This form of motor-boating, which may be called "parasitic motor-boating", is a new form of instability which has arrived with the advent of modern high-slope valves. Older valves of the old PM2HL or HL2 class had far too small a mutual conductance to give parasitics of the necessary intensity if at all. Thus motor-boating with such low-slope valves was almost invariably due to insufficient decoupling, increase of which then effected a cure. But, when using modern high-slope miniature valves in multi-stage highgain audio amplifiers, both possible sources of motor-boating must be watched and distinguished, which should not be difficult from the above discussion of the symptoms.

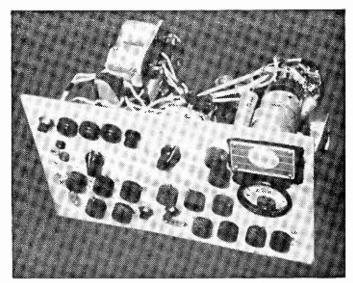
Parasitic motor-boating is positively cured by wiring adequate grid-stoppers very close to all

grid pins. Normal values of 1k are not necessarily sufficient; 10k is more advisable in a multistage amplifier and sometimes 47k or more may be needed. Emphasis is on "really close" to the grid pins, which means cutting off the wire end of the resistor to within a fraction of an inch, bending a hook which is passed through the tag on the valve-holder and pinched with pliers and then soldered. The resistor thus stands as a "tree" projecting immediately from the valveholder. Nothing else whatsoever must be wired direct to the grid-pin concerned. It is often not permissible to run a neat wire from the grid-pin to a nearby tag on a tagstrip and wire the grid-stopper there, not even if the connection is as short as less than an inch. With high-slope frame-grid valves the in→ ductance of this short lead can be sufficient to bring the parasitic resonant frequency to within the range at which the valve can oscillate. "Neatness"

must here, in a sense, be sacrificed for stability! It is necessary to remember that no object, wire, etc., has zero capacity or zero inductance; thus every circuit whatever its appearance on the theoretical circuit, will in practice also have a VHF resonance given by the stray inductance and capacity. Oscillation is then likely if the circuit is associated with a valve or transistor capable of amplification at the stray resonance involved. This oscillation is prevented by means of heavy resistive damping of the tuned circuit involved, by means of interposing a large resistance in series with its virtual "coil", which is our familiar grid-stopper.

As far as the Miniscope Signal Amplifier is concerned, 10k grid-stoppers throughout proved adequate. The arrangement to be adopted has been indicated as well as possible under the conditions of geometric perspective involved. Gridstoppers and cathode resistors are wired close to

the respective pins as indicated above and all made to stand up vertically from the valve-holders. The grid leaks are cut short at their connecting wires and soldered securely between the free ends of the The cathode grid-stoppers and cathode resistors. resistor end is then wired with a direct lead to chassis and actual grid circuit connections made to the grid-stopper end. Other components should be wired in as compact a bundle as possible to these assemblies. The resulting "floating" junc-tion points of components—i.e., free in the air and not on tagstrips everywhere, are necessary. Those constructors thinking that a layout using the slightly longer leads where everything goes to tagstrips has the neater appearance and is thus to be preferred are warned that they undertake such experiments at their own risk; there is a serious risk of instability in such cases under the conditions of the compact chassis here used. The layout here given has been proved stable.



The Miniscope as it appears in an advanced stage of construction.

Earthing

There are basically two methods of earthing (chassis connections) in electronic equipment chassis. The first is the single-anchorage busbar and the second is the multiple-anchorage busbar.

The single-anchorage busbar uses a stout bare tinned copper wire, insulated from chassis except at one point, normally at the power supply, where it is securely connected to chassis. All component ends connected to chassis on the theoretical circuit are connected not direct to chassis but to this busbar as it passes the part of the circuit concerned. The main feature of this type of earthing is that it prevents random circulating currents in the chassis proper. The chassis carries no currents whatsoever, A.C. or D.C., in this arrangement, serving as a pure screen. This arrangement is thus ideal for ultra-high gain amplifiers, preventing hum introduction into the sensitive input stages

which could result from earthing loops embracing chassis currents in random earthing, yet it aggraunwanted couplings between amplifier stages and gives the poorest earthing resistance. This form of earthing is particularly undesirable at high frequencies, as the one-anchorage busbar, which must carry all return currents, here repre-

sents appreciable inductive impedance.

Thus, for everything except extremely high gain low-frequency amplifiers, one is well advised to use some form of multiple-anchorage busbar earthing with its possibilities of better earth contact and lower inductive impedance. The familiar VHF practice of using the chassis itself as busbar and taking all earth leads of each respective stage by as direct a route as possible to a chassis-connection tag on or near the respective valve-holders comes under this class.

offers the minimum possible but inductive coupling necessarily the minimum contact resistance to chassis. When any particular earth lead relies on a single bolt and tag for chassis connection, having no alternative route, one is rather relying on just that bolt not working slightly loose after a long period of use and vibration. Thus, when one is not dealing with too high frequencies and can thus tolerate less strict reduction of inductive coupling, as is the case with the Miniscope, a form of earthing very popular with the author is This gives useful. excellent compromise between coupling, low low contact resistance and the added of availability very handy earthing points almost anvwhere as required on the chassis. This involves including a tinned soldering-tag washer under every (or almost every) valve-holder fixing bolt and tagstrip fixing bolt and other suitable component fixing bolts. Bare tinned copper wire is strung between all these tags so that all tags have electrical connection not only through the chassis but also by at least one path along the bare wire, which is securely soldered at each tag. This gives a chassis connection grid of excellent contact security and reliability. Com-

ponents to be earthed can have a hook bent on the end of their leads pinched on to the earth wiring at any convenient point and soldered secure. This gives excellent rigidity if the anchorage tags are not too far apart and the inductive coupling is merely that of the short lengths of bus wire to the next tag. Earth points belonging to critical components of different stages should located on different sections of bus wire. arrangement is ideal for equipment dealing with frequencies not exceeding 5 to 10Mc/s and as low as one pleases at the other end, which includes the great majority of non-VHF equipment.

The Miniscope uses this earthing arrangement in duplicate. In other words, independent earthing frames are used for the amplifier and the timebase sections. The signal amplifier occupies one half of the underchassis space and the timebase circuit the other half. A brass foil is interposed and connected at two ends to the signal amplifier earthing frame to stop direct radiation of timebase transients into the Y-amplifier. These measures combine to give extremely low injection of unwanted timebase signals into the Y-amplifier, which could cause serious disturbance otherwise when listening to weak signals on the headphones in the "tracer and scope" function. A further measure adopted to reduce such injection is the inclusion of a synchronisation amplifier between the point of extraction of the sync-signal from the signal

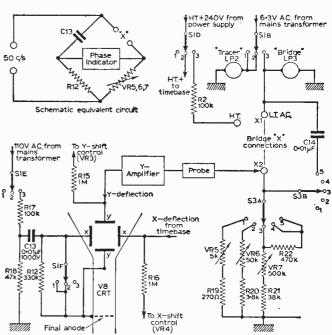


Fig. 3—A phase-shifted sample of the mains frequency is here used as X-deflection, and an unknown capacity of inductance is used in conjunction with calibrated potentiometers to shift phase of the mains frequency applied to the Y-amplifier. The potentiometers are adjusted for balance, indicated by the general ellipse closing to a diagonal line in the case of a capacity measurement, and by a true circle in the case of an inductance measurement.

amplifier and its point of injection into the timebase oscillator.

(To be continued)

CORRECTION

In the components list of the Miniscope given on page 411 of the September issue, the name of the manufacturers of diodes D4 to D11 was shown incorrectly as the Bush Crystal Co. Ltd.; it should, of course, be the BRUSH CRYSTAL CO. LTD.

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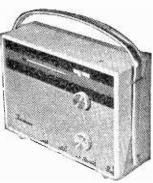
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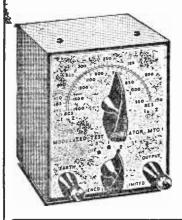
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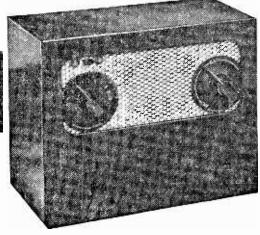
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GRIPA





A FOUR-VALVE
BATTERY SUPERHET
FOR MEDIUM AND LONG
WAVES

By S. Collins

(Continued from page 438 of the September issue)

HEN carrying out the aerial modifications described in last month's article, the reader should refer to Fig. 10.

Great care should be taken in wiring the battery plug as a careless mistake can prove an expensive one since all the valves could be destroyed in a moment if incorrect voltages were applied to them. To be absolutely safe it is a good idea not to insert

the valves at first but to test the filament wiring by plugging in the battery and checking between pins 1 and 7 on the valveholders of V1, 2, and V3, and between pins 1 and chassis on the valveholder of V4 using a voltmeter or a 2.5V bulb. The reading should be 1.5V in each case or if using a bulb it should just light up dully. If the bulb flashes and blows then there is a mistake in the L.T. wiring which must be located and put right before the valves go in.

Alignment

Having carried out this test satisfactorily the valves can be inserted into their correct position and the set switched on. With the volume control turned full on a quick test of the L.F. portion of the set can be made by lightly touching pin 6 of V3 when distinct clicks and possibly a faint hum will be heard. Now turn the tuning control slowly until some signal is heard however faint and then the upper and lower tuning cores in the two I.F. transformers should be carefully adjusted in turn to bring the signal to its loudest, if necessary reducing the setting of the volume control progressively

as it is easier to detect the peak of adjustment at lower volume levels. It is worth while to go over these adjustments several times to ensure that the best setting has been obtained. This alignment is more easily carried out if access to a signal generator is possible but in any case it is not difficult using the normal broadcast stations.

In view of the fact that the tuning dial is marked nominally from 0 to 10 it was considered that exact calibration was not very important and therefore no oscillator trimmers were provided, the

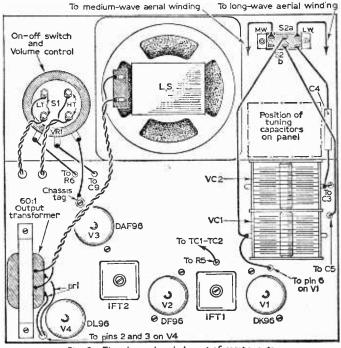


Fig. 8—The above-chassis layout of components.

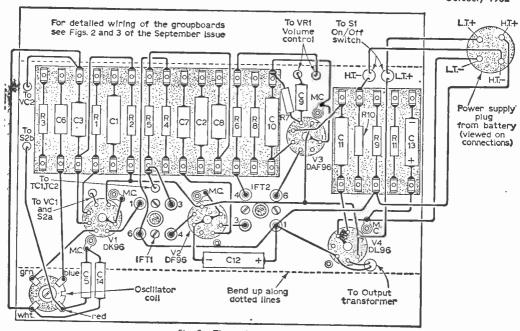
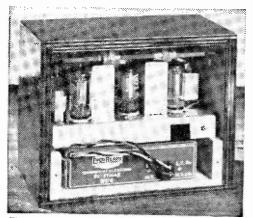


Fig. 9—The underchassis wiring diagram.

only oscillator adjustment is the core of the coil and this was set to give the medium wave Light programme on 2.5 on the dial. The Home service then came in at 4 and Luxembourg was received at excellent strength on 1.

Having completed the I.F. and oscillator adjustments the aerial circuits should be trimmed for optimum performance, and it should be noted that for all the alignment adjustments it is preferable to use a non-metallic trimming tool. Switch to long wave and tune in the Light Programme which should be about 6 on the dial and then adjust for the maximum result by sliding the long wave aerial coil each way along the ferrite rod aerial and at the same time adjusting the long wave aerial trimmer.



The completed receiver assembled in its case.

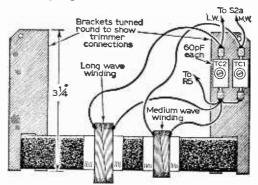
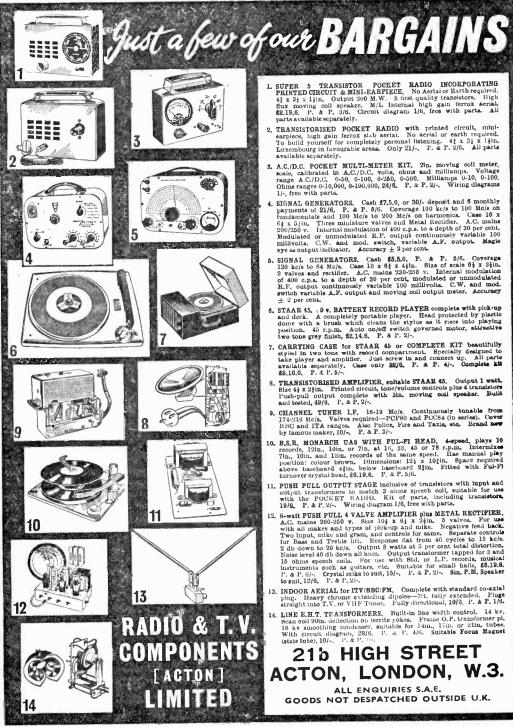


Fig. 10—The ferrite rod aerial and trimmers.

Now switch to medium wave and select a station round about 6 (probably Hilversum) and adjust the medium wave aerial coil by sliding each way on the ferrite rod aerial for optimum signals. Next tune to Luxembourg or another station at about 1 on the dial and adjust the medium wave trimmer condenser for maximum volume. As it will be found that all these adjustments are slightly inter-independent and altering one will affect the others, it is worth while going over them all two or three times until satisfied that the best results are being obtained.

Owing to this set's neat and compact shape the cabinet is quite simply constructed from \$\frac{1}{2}\$ in. plywood with a suitable cut-out in the front for the controls and loudspeaker. Two runners, also of \$\frac{1}{2}\$ in. plywood, are fitted to the inside of the cabinet support the set which is then held firmly in position by a small block glued inside the back.



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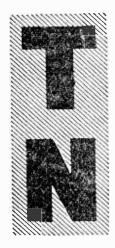
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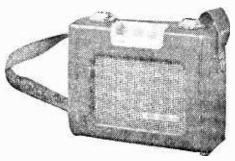
AT this year's Radio Show, Pam (Radio and Television) Ltd. displayed a large selection of their radios, television receivers and record players. Among the last section was the model SP63 portable stereo record player.

This compact instrument measures 14 in. x 20 in. x 84in. and weighs only 31lb. A twin-channel amplifier feeds two sensitive loudspeakers. The four-speed record deck is housed in a two-tone cabinet.

The model SP63 costs 28 guineas and is made by Pam (Radio and Television) Ltd., 295 Regent Street, London, W.1.

LIGHTWEIGHT PORTABLE RADIO

↑ MONG other Ever Ready receivers exhibited at this year's Radio Show was the "Sky Leader". This six-transistor receiver weighs less than 51b. and measures 9½in. x 3½in. x 7½in. It normally uses a built-in aerial but a socket is provided for connection to a standard car aerial. The loudspeaker is a 4in, moving-coil type and the whole receiver is housed in a wooden cabinet.



The "Sky Leader" receiver from The Ever Ready Company Limited.

A printed circuit is used in the construction of this receiver which covers fully the medium and long wavebands. The price of the "Sky Leader", including the battery and purchase tax, is £20 9s, 10d. It is made by The Ever Ready Co. Ltd., Hercules Place, Holloway, London, N.7.

NEW CAR RADIO

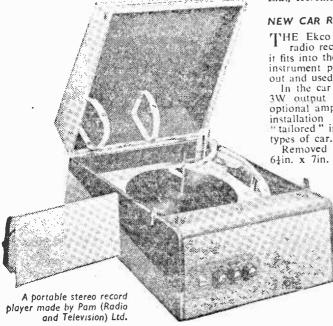
THE Ekco "Twin-Set" is a dual-purpose car radio receiver, its important feature being that it fits into the opening provided for a radio in the instrument panel of most cars or may be taken out and used as an ordinary portable.

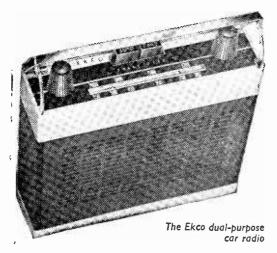
In the car the receiver is a true car radio with 3W output when used in conjunction with an optional amplifier. There is available a range of installation kits and loudspeakers to permit a "tarlored" installation in more than 100 different

Removed from the car the receiver measures 64in. x 7in. x 13in. and is finished in black and

chromium plate. The tuning covers both the medium and long wavebands. In the car a very low current is drawn from the car battery and, out of the car, power is supplied by a 9V dry battery.

The price of the "Twin-Set" (model CP920) is $18\frac{1}{2}$ guineas and the optional 3W amplifier costs 4 guineas, while the receiver housing costs a further 3 guineas. This new set is manufactured by Ekco Radio and Television Ltd. South end-on-Sea, Essex.

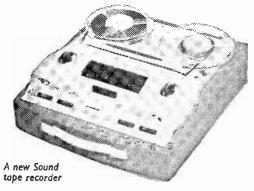




TAPE RECORDERS

THE makers of Sound Tape Recorders have released eight new models to add to their Slimline and Riviera ranges, all of which were on show at the Radio Show.

One of the new recorders in the Slimline range is the Three-Two, which is a three-speed, twintrack model giving up to nine hours recording and playback time. Each recorder is supplied with a



crystal microphone and a spool of tape. The built-in loudspeaker delivers over 3½W output. The price of the Three-Two tape recorder is 40 guineas and the makers are Tape Recorders (Electronics) Ltd., 784-788 High Road, London, N.17.

HEADPHONES AND HEADSETS

A NEW lightweight headphone set (available with or without a boom microphone) has recently been introduced by Amplivox Ltd. under the name of Jetlite. They are available with magnetic, tropicalised or moving-coil earphones. The headphone set alone weighs only 4oz. It is designed for use with tape recorders, dictating machines, television and broadcasting, film monitoring, etc.

The boom microphone headset version weighs 5oz. and may be fitted with magnetic or carbon microphones, high or low impedance headphones and a miniature lapel switch.

The manufacturers of the new Jetlite headsets are Amplivox Ltd., Beresford Avenue, Wembley, Middlesex.



A Jetlite boom microphone headset made by Amplivox Limited.

Increasing Ammeter Ranges

(Continued from page 503)

depending upon their design. The resistance of the instrument can be taken as infinite so that the value of the shunt is arrived at by dividing the voltage by the current. Fig. 4 shows a simple arrangement for measuring up to 1A. The shunt resistance will have to be as low as possible in order to reduce its effect upon the circuit. Its resistance is, say, 0.1Ω .

Therefore if the instrument reads 100 millivolts the current in the circuit will be:—

$$I = \frac{E}{R} = \frac{100/1000}{0.1} = 1A$$

Bigger shunts must be used for smaller currents -0.2Ω is suitable for 500mA circuits, while a 1Ω shunt will give the same reading on 100mA.

The resistance of the shunt can be taken into consideration by measuring the supply voltage. From this the total resistance or impedance can be found (R = E/I).

The current taken by the circuit without the shunt will be:—

$$I = \frac{E}{Rt - Rs}$$

Rt is the total resistance of circuit and Rs is the resistant of the shunt.

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MODEL ITI-2.



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bels: —20 to 722 dR. A fully guaranteed pocket size meter (actual slice: 44 x 34 x 1') knife edge pointer, top quality supplied complete with test prods and full operating ONLY \$5.5.0 POST instructions. ONLY

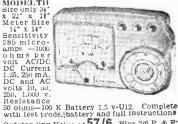
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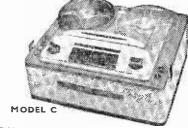
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P.W.10

Letters to the Editor

The Editor does not necessarily agree with the opinions expressed by his correspondents

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELE-PHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iii of the cover.

STRIPED SOUND

SIR.—I have been an avid reader of your magazine for the last 15 months and, although many of the articles are still above my head. the home construction bug has bitten hard. I have imported a number of the kits advertised in Practical Wireless and my most recent attempt—a stereo amplifier-is now working well, albeit a little distortion in the left-hand channel.

I now wish to attempt some experimental work with 8mm, striped sound, using the above amplifier

and the necessary pre-amplification.

Therefore, I am appealing for information from any readers who may already have attempted this sort of thing. I wish to keep the record/playback unit as compact as possible, using the existing film drive sprockets of my projector. If any readers could let me have any such information I would be very grateful and would endeavour to reply to all correspondence.

I am currently busy constructing a stereo preamplifier and am hoping that this will also be of use with these experiments.—A. P. RAATS (6 Elizabeth Road, Bedfordview, Tyl., South Africa).

COPIES OF P.W. WANTED

SIR.—I require urgently certain copies of Practical Wireless duting from 1948 onwards. I will pay the full price for copies in good condition.—B. E. WASHER (15 Bower Road, Harrogate, Yorkshire).

ELECTROMAGNETIC RADIATION

SIR,—With reference to Mr. Craske's letter in the August issue, I fear that he has misconstrued the Quantum theory of electromagnetic radiation (EMR) entirely.

Mr. Craske proposes to emit EMR as a particle, then convert it into a wave at a later stage.

While it is true that the Quantum theory treats EMR as particles, reference to the theory will show equations involving the frequency of the EMR and only waves have frequency. In fact, the "wave" and "particle" conceptions are only analogies used to explain certain observable phenomena of EMR. Actually EMR is neither wave now particle and should not be considered. wave nor particle and should not be considered as such.

It follows, therefore, that a photon cannot be emitted and converted into a wave or vice-versa. It simultaneously exhibits the properties of both

wave and particle!

Also, if a photon were, as Mr. Craske put it. to "explode", its energy would be dissipated among several secondary photons and the frequency would be lowered in a random manner!— K. ROBBINS (Coventry).

CORRESPONDENT WANTED

SIR.—I am 15 years of age and I have been interested in S.W. radio for some time. I would like to correspond with amateurs of my own age or anyone interested in 38 and 18 sets.—S. Amos 53 Meldon Terrace, Newbiggin-by-Sea, Northum-

SERVICING TAPE RECORDERS

(Continued from page 488)

"live" pole of the mains, the whole equipment becomes highly dangerous. There is not only the possibility of fatal electric shock, but a random earth connection made on the recorder could

cause severe damage to the equipment.

Some operators feel that adequate isolation is possible by interposing two capacitors, one in each conductor, at the set-end of the signal lead-out cable. Such isolation is pretty futile for several reasons. One is that an isolating capacitor must not exceed 0.005 µF, since a higher value would pass too much alternating current due to its lower reactance at 50c/s and would thus be almost as unsafe as a direct connection. Another is that such a relatively low value capacitor would attenuate the lower-frequency audio signals too much for good quality recording. A third reason is that the impedance across the isolating capacitors gives rise to a 50c/s voltage, which is extremely difficult to remove from the low-level signal circuits.

There is only one real answer to this problem and that is to connect a 1-to-1 ratio isolating transformer between the mains supply and the A.C./D.C. set. In that way the chassis is at zero potential and can be retained that way by connecting it to a good earth point. The external tape recorder circuit may then be connected as shown in Figs. 29 and 30 without damage. On no account, however, must an earth be connected to an A.C./D.C. receiver without an isolating transformer. It should also be noted that some sets. although for A.C. mains only, may have a mains transformer to supply only the valve heaters, with the H.T. mains circuit still in connection with chassis. Such models should be handled in the same way as A.C./D.C. receivers.

(To be continued)

Club No

REPORTS OF CURRENT ACTIVITIES

BURSLEM AMATEUR RADIO CLUB Hon. Sec.: W. Luscott, 36 Rothsay Avenue, Sneyd Green, Hanley, Stoke-on-Trent, Staffordshire.

At the August meeting, held on 15th at the Queens Hall, Burslem, G3MUX gave a lecture covering all aspects of two metre operation. Future Event:

September 19th—"A home constructed two metre rig" by G3EHM.

CRAY VALLEY RADIO SOCIETY

Hon. Sec.: S. Coursey, G3JJC, 49 Dulverton Road, London, S.F.9.

At the request of the First Swanley Scout Group, a station was put on the air at their recent (ete, and a number of contacts were made on 160m by the members who operated it.

DERBY AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: F. C. Ward, G2CVV, 5 Uplands Avenue, Little-over, Derby.

Over, Derry,

The now well known Derby Mobile Rally was held on 19th August at Rykneld School. On Wednesday, 22nd August, members attended a stereophonic demonstration, and on 5th September a sale of surplus equipment was held.

Future Event:

September 12th—Transistors.

HALIFAX AND DISTRICT AMATEUR RADIO SOCIETY Hon, Sec.: G. Sunter, 24 Booth Fold, Luddenden Foot, Halifax, Yorkshire.

Plaintax, Torkshipe.

On August 7th, members listened to a lecture given by G3EKE on the subject of "amateur television". The other meeting for that month was devoted entirely to a ragchew.

The subject of G2VO's talk, which he gave on September 4th, was "amateur radio through the years".

Future Event:

October 2nd—The annual general meeting.

NORTHERN HEIGHTS AMATEUR RADIO SOCIETY Hon. Sec.: A. Robinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.

On August 29th all interested members attended a discussion on the R.A.E. course to be held during the 1962/63 season. Future Event

September 12th—"Simple fault finding" by G30GV.

WIRRAL AMATEUR RADIO SOCIETY Hon. Sec.: A. Seed, 31 Withert Avenue, Bebington, Wirral, Cheshire.

Owing to the decorating and repairs carried out on the club's new premises, no meetings were held during August. The address of the new H.Q. is, The Scout Headquarters, Park Road West, Claughton, Birkenhead.

On September 6th members attended a lecture on single sideband which was given by G2FOS.

COURSES OF INSTRUCTION

The following classes, organised by the East London R.S.G.B. group, in conjunction with the Essex County Council, are available for all those interested in amateur radio, irrespective of whether they are members of any society or of the general public. There are two R.A.E. courses to be held on Wednesday and Thursday evenings. Also a Morse and codes of practice course held on Mandal Ventilans. Monday evenings.

The venue for the classes is, The Ilford Literary Institute, High School for Girls, Cranbrook Road, Ilford, but those interested should first write to Mr. C. H. L. Edwards, 28 Morgan Crescent, Theydon Bois, Epping, Essex.



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etc. 10/6).

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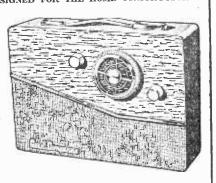
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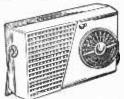
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MODULATION MONITORING

By G3OGR

HE need for checking the depth of modulation with a telephony transmitter makes some method of modulation monitoring very useful. Over-modulation can cause interference, and must always be avoided, while insufficient modulation makes a signal difficult to copy when conditions are bad.

Methods

There are several methods of checking the depth of modulation, and they are very helpful indeed, both for regular working, and when testing or

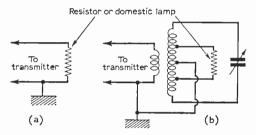


Fig. I—An artificial aerial consisting of a lamp load or resistor.

setting up a new transmitter. It is also useful to be able to listen to the speech quality of the actual radiated signal.

When adjusting or testing the equipment, some over-modulation will probably arise. It is thus essential to use an artificial aerial with the transmitter to avoid unnecessary interference with other transmissions. Two methods of providing an artificial aerial load are shown in Fig. 1. For a small transmitter (such as a top-band rig) it is feasible to use ordinary carbon resistors (Fig. 1a). Two 5W 24Ω resistors in series will provide a 10W 48Ω load or five 2W resistors, or some similar combination, may be to hand. The exact load is generally unimportant, the transmitter matching can be

adjusted to suit.

Large non-inductive resistors for such purposes are obtainable, but are expensive, so for transmitters in the 25W to 150W range, an ordinary domestic lamp (200/250V) is generally adopted. A 15W lamp is also suitable for a low power transmitter. The lamp is chosen to suit the

transmitter power and the wattage is not critical. If the transmitter can be loaded into the relatively high impedance of the lamp (as many transmitters can) then it is only necessary to connect the lamp in place of the aerial or aerial tuner, as in Fig. 1, but if the transmitter will only match a low impedance load, some form of impedance matching circuit is needed. A convenient method is to use a tuner, as in Fig. 1b. This could be the usual aerial tuner, or a tuner wired up for the purpose. The coil is tuned to the operating frequency. The transmitter is coupled with a loop of about two or three turns round the coil, and the lamp is tapped across a portion of the coil, to give

suitable loading. Most transmitters use a π -output circuit; loading into this follows normal practice. That is, the π -output capacitor is set at high capacity, and the power amplifier (P.A.) capacitor is tuned to resonance, as shown by a dip in anode current. The output capacitor is opened a little at a time, the P.A. being kept tuned to resonance, until the anode current reaches the required figure. This process will cause the lamp to light more and more brightly, as R.F. output increases.

Monitoring with an Oscilloscope

An oscilloscope can be used to monitor modulation depth, by taking a small R.F. voltage to the Y (vertical) input. Sufficient R.F. input may be obtained by twisting an insulated lead round one lead to the lamp load, this lead forming capacitor

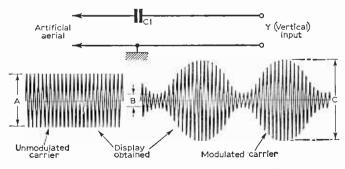


Fig. 2—Monitoring with an oscilloscope, with timebase.

C1 in Fig. 2. The oscilloscope attenuator is adjusted to give a display of suitable height. If the oscilloscope is a simple one with no attenuator, adjust the coupling provided by C1.

A steady tone is preferable for monitoring, as

the irregular display obtained from speech is less easily examined. This tone can be obtained from an oscillator or other convenient source. By locking the timebase to the oscillator by means of the sync control of the oscilloscope, a stable display will be achieved.

The unmodulated R.F. has the amplitude "A" in Fig. 2. As modulation is increased, the waveform of the modulated carrier will grow more pronounced. Downwards modulation produces the

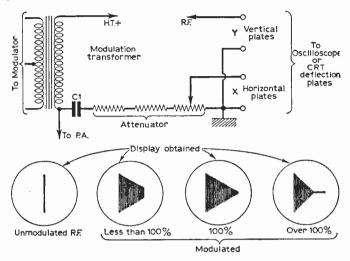


Fig. 3-Using an oscilloscope without timebase.

dips, the amplitude being measured as at "B". The downwards modulation, as a percentage, is:

$$100 \, \left\{ \frac{A - B}{A} \right\}$$

The distances can be measured in millimetres or any other units. Upwards modulation produces the "humps" and the upwards modulation percentage is:

 $100 \left\{ \frac{C-A}{A} \right\}$

If modulation is symmetrical the upwards and downwards modulation percentages will be the same. Downwards modulation must not exceed 100% or interference will be caused.

The same display can be obtained with a received transmission. A station with an oscilloscope can thus monitor the transmission of another station. This can be useful when setting up a modulation meter of the type described later. To obtain the display modulated R.F. can be taken from the last I.F. amplifier in the receiver.

Using a Simple Oscilloscope

Modulation can be monitored with a simple oscilloscope having no timebase. To do this, R.F. is applied to the Y-input, as already described coupling being adjusted to obtain sufficient deflection to draw a vertical trace, as in Fig. 3.

The X-input (horizontal) is taken from the audio

amplifier, via the isolating capacitor C1, which can be of any convenient fairly large value. Two or more resistors are used as an attenuator, as shown. Two 1M fixed resistors, with a 500k potentiometer, will suffice for many transmitters.

When the signal is modulated, a display of the kind shown will be obtained. The attenuator setting merely controls the extent to which the audio shifts the trace horizontally, and is adjusted to obtain a reasonably large display, but one not

exceeding the screen size. As with the previous method, a steady tone is most suitable, as merely speaking into the modulator microphone will give a rapidly fluctuating pattern less easily examined.

Monitor Oscilloscope Circuit

With a small tube, sufficient trace can easily be obtained without amplifiers, so the X- and Y-inputs can be taken directly to the tube plates (via isolating capacitors). A simple circuit of this kind is shown in Fig. 4, and is intended for the DH3-91 tube. This has a 6-3V 550mA heater, which should receive current from a 6-3V transformer winding. For H.T. 500V will easily suffice, and this can most probably be obtained from the transmitter power pack, or from a simple half-wave pack using the full winding of a 250-0-250V transformer. The 560k resistor (R3) may be adjusted to modify the

trace brilliance; a variable control may be fitted, if preferred. If so, a 470k fixed resistor in series with a 500k potentiometer can be used.

As no timebase is available, the display obtained will resemble that in Fig. 3. No X-amplifier is present, so the attenuator will need adjusting to

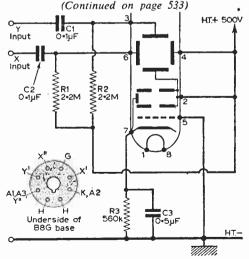


Fig. 4—A circuit for a lin. oscilloscope.

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(Continued from page 530)

obtain sufficient deflection. In the same way, there is no Y-amplifier or adjustable attenuator, so coupling must be so adjustable to the lamp load or aerial, to give a suitable vertical trace.

Such a monitor is easily made as a small, separate unit. A magnifier, preferably with hood, can be fitted over the screen, to enlarge the display, as the tube mentioned is only lin. in diameter. Larger tubes may be employed in a similar manner, but a much higher voltage will generally be needed for them.

Neon Indicator

A 240V or similar neon lamp can be used as a modulation indicator, as shown in Fig. 5. C1 is merely an isolating capacitor, of $0.05\mu F$ or similar value. R1 and VR1 form a voltage dropping network, and VR1 is so adjusted that the neon just strikes when modulation reaches nearly 100%. While transmitting, repeated flashing of the neon is a warning to move farther from the microphone, or reduce the modulator gain control setting. The values of R1 and VR1 will depend on the

The values of R1 and VR1 will depend on the P.A. voltage, but VR1 can be a 500k potentiometer. R1 will then probably be from about 250k to 1M, depending on the transmitter H.T. voltage. If the neon does not light with VR1 set for maximum voltage across it, then R1 must be reduced in value.

If there is no objection to having the neon at H.T. potential, the network and neon may be in parallel with the modulation transformer winding. The neon can be mounted behind the panel, preferably screened from too much extraneous light,

If an oscilloscope is available, the neon indicator can be set up with the oscilloscope monitoring the modulation level. If it is not possible to obtain an oscilloscope for this purpose, the receiver can be employed to listen for the sideband splatter caused by over-modulation. To do this, it will probably be necessary to use a lamp load, and to remove the receiver aerial, to avoid overloading the receiver. This depends on the screening, and transmitter power. Alternatively, a valve, such as an R.F. amplifier, may be removed from its socket, if the signal strength is still too great with the R.F. gain control on the receiver at minimum.

When the transmitter is being modulated, side-band splatter as a result of over-modulation will be heard when the receiver is tuned slowly away from the correct frequency. The sound is heard only at the instants of over-modulation, and will not be audible with a properly modulated signal (such as from a BBC station). Modulation is then adjusted until splatter has just ceased, and VR1 is adjusted so that it is then just igniting, on speech or modulation peaks.

Modulation Level Meter

Modulation reaches 100% when the P.A. anode voltage is swung from zero to twice its unmodulated voltage. For example, if the power amplifier operates with 500V on its anode, the modulator swings this from zero to 1,000V for 100% modulation.

An A.C. voltmeter will thus act as a modulation meter, and a multi-range meter with A.C. ranges can be used, though a separate meter is preferable. A suitable circuit is shown in Fig. 6. C1 is merely

an isolating capacitor, of suitable working voltage. A $0.05\mu\text{F}$ 1,000V component would be suitable for many transmitters. The meter can be a 1mA, 5mA, or similar instrument, with 1mA or 5mA rectifier. R1 is the voltage-dropping resistor.

The meter will give no reading when the transmitter is not being modulated (unless there is hum on the carrier) but will kick upwards when speech is present. If a signal is obtained from an audio oscillator or similar source, the meter will take on a steady reading. It is necessary to adjust R1 to obtain a convenient deflection of the meter pointer,

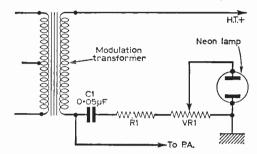


Fig. 5-A neon modulation indicator.

and the meter can then be calibrated for 100% modulation, by one of the methods previously described. This calibration is most accurate if carried out with the usual microphone and by speaking in the usual manner. After calibration, it is only necessary to observe the meter, when checking modulation, to see that its reading is well up, but not over the 100% mark.

Modulator H.T. Current

Class B modulators are used with all but the smallest transmitters, and with these the H.T. current drawn by the output stage depends on the audio power handled. A meter in the H.T. supply to this stage can thus be used as a check on modulation. The reading to which the meter will rise, for nearly 100% modulation, can be found

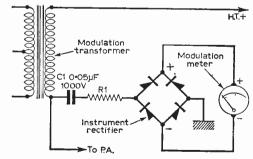


Fig. 6—A speech level meter for monitoring.

by the methods previously described, as well as by obtaining reports from stations contacted.

A disadvantage of this method lies in the fact that the audio input required for full modulation depends on the loading of the P.A. The P.A. should thus always be loaded to the same extent, or nearly so, by means of the usual aerial coupling adjust-

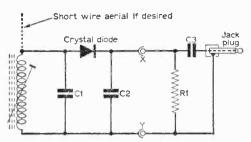


Fig. 7—A diode pick-up for audible monitoring.

ments. It is then only necessary to speak or adjust the modulator gain control, until the meter peaks are around the accustomed figure.

Speech Polarity

If a trace like that in Fig. 2 is observed, while speaking into the modulator microphone, the modulation peaks in both directions will probably not be equal. That is, upwards modulation may exceed downwards modulation, or the reverse. If downwards modulation exceeds 100% (broken carrier) interference is caused. But upwards modulation exceeding 100% need not cause interference. It is therefore preferable that the lack of equality in the modulation should be so arranged that the highest peaks are in the upwards direction, as a greater level of average modulation is then possible, without exceeding 100% modulation in the downwards direction.

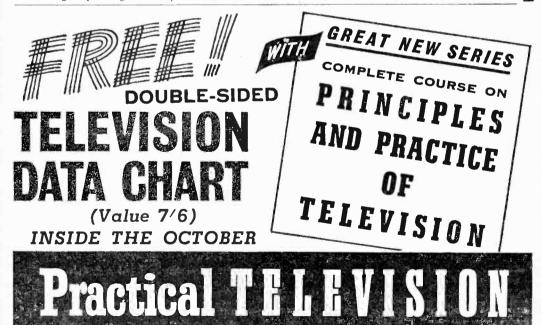
The human voice functions in such a way that many sounds are not of symmetrical waveform. If the strongest peaks give an upwards modulation

trace, these peaks may exceed 100%, while downwards modulation does not exceed 100%. If the peaks result in downwards modulation, the average audio signal has to be reduced, to keep these peaks within the 100% limit. This can be overcome by reversing the connections to any audio transformer winding, in the modulator. Probably the driver secondary or modulator transformer primary connections can most easily be reversed. The best polarity for one microphone is not necessarily most suitable for another microphone. If no oscilloscope is available, the best polarity or phase is that giving most freedom from splatter.

Modulation Quality

A simple pick-up for audible monitoring is shown in Fig. 7. C1 can be any convenient capacitor, fixed or variable, from about 25pF to 500pF, to allow the coil to be tuned to the required amateur band. C2 is 500pF to 5.000pF or so. Phones are connected at the points X and Y for audible monitoring.

If a tape recorder is available, R1 and C3 may be added. About 100k and 0.01 µF will be satisfactory, and a short screened lead is equipped with a plug to suit the recorder input socket. The pick-up tuner is then placed at a suitable distance from the transmitter, aerial, aerial tuner, or lamp load. In this way, a recording of any test or other transmission can be made, and it will be of the same quality as radiated over the air. The recording can be played back afterwards, as a check on speech quality, modulator operation, and so on. If the recorder volume control setting is noted, the test can be repeated without difficulty, when necessary, and no helper is required.



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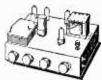
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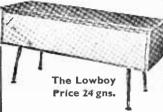
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The Index letters which precede the Blueprint Number indicate the periodical in which the description appeared. Thus PW refers to PRACTICAL WIRELESS; AW to Amateur Wireless and WM to Wireless Magazine.

Send (preferably) a postal order to cover the cost of the Blueprint (stamps over 6d. unacceptable) to

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TELEVISION

Organ

The PW Roadfarer

The PT Band III converter

PRACTICAL WIRELESS, Blueprint Dept., George Newnes, Ltd., Tower House, Southampton Street. London W.C.2.

SPECIAL NOTE

THE following blueprints include some pre-war designs and are kept in circulation for those constructors who wish to make use of old components which they may have in their spares box. The majority of the components for these receivers are no longer stocked by retailers.

This coupon is available until 5th October, 1962, and must accompany all queries in accordance

with the notice on our "Letters to the Editor"

page.

PRACTICAL WIRELESS, OCTOBER, 1962

				Title		umber	Price	
Title		Ni	ımber	Price	A.C. Fury Four		PW20	2/6
CRYSTA Junior Crystal Set Dual-wave Crystal Diode			PW94 PW95	2/- 2/6	Experimenter's Short Wave Midget Short Wave Two Band-Spread Three (Battery) Crystal Receiver		PW30a PW38a PW68 PW71	2/6 2/6 2/6 2/-
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Modern One-valver			PW 96	2/6	Fyrainid One-vaivei		1 44 93	2/0
All-dry Three			PW97	3/6				
Modern Two-valver		• •	PW98	3/6	BBC Special One-valver A One-Valver for America		AW387 AW429	2/6 2/6
SUPEI	RHE	TS			Short-Wave World Beater		AW436	3/6
A.C. Band-pass Three			PW99	4/-				
A.C. Coronet-4			PW100	4/-	Standard Four Valve S.W.		WM383	3/6
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The PW Pocket Superhet				5/-	Standard Four Valve		WM391	3/6
MISCELI	LANI	EOU	JS		Listener's 5-Watt Amplifier		WM392	3/6
The PW 3-speed Autogran	n			8/~				
The PW Monophonic E				8/•	QUERY C	DU	PON	. !

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