## SEPTEMBER 1962 <br> Practical 2' WIRELESS

## The MINISCOPE



## The TUDOR <br> 4 -valve battery portable

# BRAND NEW AM/FM (V.H.F.) RADIOGRAM CHASSIS AT £13.13.0 (Carriage Paid) A.C. ONLY. Chassis size $15 \times 6 \neq 54$ in. high. New manufacture. Dial $141 \times 4$ in. In 2 colours predominantly gold. 

 Pick-up. Ext. Speaker. Ae.. E., and Dipole Sockets. Five push buttons-OFF L.W., M.W., F.M. and Gram. Aligned and tested, O.P. Transformer, Tone Control. $1.000-1.00 \mathrm{M} .: 200-500 \mathrm{M}$; $88-98 \mathrm{Mc} / \mathrm{s}$ Valves EZ80 rect., ECH81, EF89, EABC80, EL84, ECC85.Speaker and Cabinet to fit chassis (table model). $47 / 6$ (post $2 / 6$ ).
$9 \times 6 \mathrm{in}$. ELLIPTICAL SPEAKER, $20 /-$ to purchasers of th1s TEHME:-(Chassic) E5 down and 4 monthly purchasers of this chassis. TERMS:-(Chassis) $\boldsymbol{e f}_{5}$ down and 4 monthly payments of $£ 2$, and 1 of 21.13.0.

Cheap Room Dipole for V.H.F.. 12/6. Feeder 6d. yard.
Circuit diagram 2/6. Circuit diagram 2/6.

## THE "CANTATA" 6-TRANSISTOR AND DIODE PORTABLE

COMPLETE KIT FOIt ONI.I £7.19.6
(post $3 / 6$ )


500 mW push-pull output. Ferrite rod aerial. Car aerial soc4.5 v . cells. Printed circuit board 81 coverage. Operates on two component positions marked. Instructions $2 / 6$ for $16 p$ (refund ded on purchase of kit). Size $9 \times 3$ x $\times 7 \ln$. $8 \times 211 \mathrm{n}$. F. M. high quality speaker. Attractive vinair covered cabinet. Fwo tone. Two batteries 5 / 8 the pair (Ever Air covered cabinet. two tone. OC44, $2 \times 0 \mathrm{OC45}$, OC81D, and 2 x OC81. Top grade Weymouth Radio coils and transformers. Alignment service if required $17 / 6$ (Inc. post). Write for list of prices. All parts supplied separately. Bulit in two hours.

## BUILD YOUR OWN RECORD PLAYER Price $£ 12$ carr. paid <br> Fully built 2 valve amplifier

B.S.R. 4-sp. autochanger. case $17 \times 15 \times 8 / i n$. Assembled in
 only £3. carr. paid. Attractive colours.

$$
\text { or with } 3 \text { valve amplifier } 15 \text { '. extra }
$$

AITOMATIC IRECORD CHINGFIRS-LATEST MODELS. 4SPEED, CRYSTAL CARTRIDGE. All 5/- CXtra carr. B. S. R.
UA14. £\%.10.0. Garrard Slimline. Mono e8. Stereo. £8.5. MA14. £\%.10.0. Garrard Slimline, Mono f8. Stereo, £8.5.0. or $3 / 6$ post paid when purchased with Autochanger. Motor Board for Collaro C60. 4/-, post pald.
THIEFUNKEV STEREO AMPLIFIEIRS. 2 ECL $82-2 \times 21$ watts. $12 \times 3 \times 2 i n$. piano keys, $£ 7$, post pald.


6 TRANSISTOR PORTABIE FULIY HUHLT, The "SCALA" for onls $£ 7.19 .6$, carr. paid. $8 \pm x$ $2 \times 5 \mathrm{in}$. high Cholce of colours. Rexine. M.W. and L.W. Ferrite aerial. P.P. 4 battery $2 / 3$ extra. Printed circuit. Nicely styled. A protessional lob 318 . speaker.

SELF-IOWEITED NII THNER CliAssis. Covering 88-95 Mc/s Mullard permeability 'T'uner, Dims EF91 and 2 diodes. Metal Rectider Mains transformer. Fully wired and tested. Only fz. 10.2 cally wired and tested. Only £7.10.2 (carr. pd.) Room dipole 12/6. Feeder. Bi. vd.
 Front panel (normally screwed to chassis) mas be removed and used as "flying panel." stereo version $2 \times 4 \mathrm{w}$. same price.

## THIS SUPERB SET FOR £10

6 -transistor radio covered in sponge clean Duracour fabric. in latest two tone shades. M.W. and L.W. ferrite rod. provision for car aerial. 2 -colour scale. With PP9 battery giving 300 hours use. Welghs under 4 lbs. With carrying handle. $12 \times 7 \mathrm{inn}$. high $x 4 \mathrm{fin}$. at base tapering to $21 n$ at top.
Brand new. fully guaranteed, £10 Carr, paid. Worth $£ 16$.


PUSH-PULL AMPLIFIER
(5/- Carr.)
Brand new 270-240 A.C. mains Bass, treble and vol. controls With yalves EZ80, ECC83 and
 Chassis $12 \times 3!\times 314$. With o.p.
trans. for $2-3$ oh $A$ speaker. $\$ 5.5 .0$
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## SUPERIOR GRAMOPHONE AMPLIFIER

Vaives UY85, UFBO and UL84. Mains trans. 200-2 10 a.c. Covered baffle 13\& x 7itn. (64n. Speaker) or $11 \times$ x 9 in. $8 \times$ sin. speaker). 3 front controls bass, treble. on-off/vol. F4/- (post 4/-) either type. Hexine cabinet to fit, with carrvins handle, and lid
(detachable) $141 n$. or $12 \times 8 t \times 5 i n$ (detachable) 141 n . or $12 \times 8!\times 5 \mathrm{n}$., $16 /$ extra.

GRAMOPHONE IMPLIFIFIR. With Sin. SPEAKER Baffle
12 x 6 in. ECL82 and Rectifler. Tone and Volume. Onfor switch.
IEST INEAD KIT. Leads, Prods, Terminals, Clips, in case. 10/-, post paid.

TAPE TOP QUTLITY HOXED. $5 \% \mathrm{in}$.-850it. $15 /-; 1.200 \mathrm{ft}$., 17/6; 71n.-1,200 ft., 17/6: 1.800 ft. ., $26 / 6$ (all plus $1 / 6$ post. $2 \%$. ior 2).

## SPECIAL OFFER

Brand new tape recorder, two tone bet ee case, "gold" trimmings. Magic eye. monitor. ext. speakel sockets. With 5intape and mike. Fully guaranteed. Price ustally f19. gns. Very high gain with low noise. Price 818 carr. padd

COLLARO STUDIO TARE TRANSCIRIPHOIR. 3 MOTORS;
3SPEEL. 16 , 3 and 74 I.P.S. Push buttons.


## 3-VALVE AMPLIFIER (Inc. RECT.)

21 watts. ECC83. ECL82 and EZ80. Controls, volume, bass and
treble. On/off switch. Mains and O.P. trans, Size as for Pushtreble. On/off switch. Mains and O.P. trans. Size as for PushPull Amp. Suitable for inicrophone
input and for Guitar,
$95 /=$ P. \&P. 5/Also acts as telephone ampilifier using pick-up coil price 14/-. Chassis $12 \times 3 \ddagger \times 3 \pm \mathrm{tn}$. Fixed front panel. Price includes handhigh quality 3 ohm P.M. speaker 5$\} \times 4$ in ( $20 /$ cab and speaker).

## BATTERY ELIMINATOR

For 4 Low Consumption Valves ( 96 range). 90 v .15 mA and 1.4 v . $125 \mathrm{~mA}, 45 /-(2 / 6$ post). $200-250 \mathrm{v}$. A.C. Also to $250 \mathrm{~mA}, 1.4 \mathrm{v}$. and $90 \mathrm{v} \cdot 1 \mathrm{in}$ A at same price.

## TAPE RECORDER AMPLIFIER

Tybw Tis3. Fully built, high gain. low noise printed circuit. Attractive grey and gold front panel $13 \times 14 \mathrm{in}$. Height 54 Ln . overalt. Front to back 5 h In . Vol. and un/off-tone. Mike. radio. monitor and ext. speaker jacks. Valves ECC83, ECL'32. EZ80. Mains trans. Ready to bolt to B.S.R. Deck. Complete with switch wafer wired. Our Price ONLY \&8.2.6 (6/-Packing and Carr.) Similar model without magic eye, Type T.R.1. $3^{\circ}$
instead of $1 \mathrm{I}^{*}$ £5.15.0. (6/-Carr.)

## CHASSIS BATTERY RADIO

Valves DK96. DF96, DAF96. DL.96. Two Short Wavebands 16 to 49 M and 25 to 75 M . Size $10 \mathrm{x} 44 \times 5 \mathrm{in}$. £4.16.0, carr. pald. MW
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 TEIRMS AVAILABEL ON ITEMS OVER \&5
Send $6 \mathrm{~d} .\left(\begin{array}{c}\text { (stamps will do) for } 20 \text { page illustrated catalogue. All } \\ \text { New Goods. Delivered by }\end{array}\right.$ New Goods. Delivered by return. (C.O.D. 2/-extra.)

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 we are oftering MW 31/74 Tubes at the unrepeatable price of $29 /-$, BW $36 / 24$ ditto. 39/-. I.P. 12/6. The above are guaranteed for 6 tnonths.RECORDERS. "Verdik" 4 Track Collaro 3 Apeed Transeription Deck, superior reproduction, gtremmlined Portable Case. Complete with Mike.
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4-SPEED RECORD PLAYERS. batent Turntable, together with agphire cryatal turnover plek-up sapphire crystal turnover plek-up only 18/-), 23.10 .0 . Carr. 3/4.

PORTABLE RECORD PLAYERS. Takes all sizes Records, all speeds. amplitier, auto-changer, Garrard new "slimline" irum. In two-tone lutely new. 14 gns.

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 Table Models, Famous Makes. AbsoIutely Complete. These seta are un equalled in vane due to buge purchase threct rutn sumree. They are untested. and not guaranteed to be in workingorder. Carr. etco, $15 /=$.

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## TRANSISTOR PORTABLES. dionde lightweight, approx. 11b.,

 slighty larger than pocket bet, but much greater volume, better yuality, complete battery, mazz-ing sensitivity worth es11. Our ing rensitivity wo
nice ondy $\mathbf{~} 7.10 .0$.
F.M. TUNER KITS. Well-known make Gomprising F.M. Tuning Head, guaranteed mone drit. Frequency coverage $8 \times-16 y$ mu/s. OABI balanced diode
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TRANSISTORS.
Red apot $8 / 6$ es. White spot $4 / 6$ ea. Yellow 8 pot $2 / 8$ ea. Cermanium diodes 9 d ea. $8 /-\mathrm{doz}$
TAGSTRIPS. From 3 way to 12 way. TAG STRIPS, From 3 way to 12 way,

> Forther delivery of these excellent anits to hand complete with 6Fs amplifer, 20P3 output, and UU9 rectifler. Easily converted into high gain unit, oomplete with good quality, 8in, apeaker in attraotive worted for buitgrg case easily conFerted for guitars, record players,
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ASSAULT CABLE. 1,000 yds. Covered steel Telephone Wire.
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12 VOLT Blowera, ex-Gov., 19/6.
VOLUME CONTROLS $\$ 5$ to 2 Mes: from $8 / 8$ to $6 / 9$ each.

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Fsmous makes complete with
PCF80, PCC84 Fsives. $38 \mathrm{M} / \mathrm{C}$ L. F.
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NEW SPEAKER CABLNETS, cOvered in attractive Rexiae, Liold Mretsl tront 11/-. Or complet
Speaker, $19 /=$ P.P. $1 / 6$.

UA20 Autochangers. Latent B.S.R. 10 mixed records, Brand New, Unrepeatable, £6.19.0. Also UA14. A Proven Choice $\mathbf{2 7 . 1 9 . 0}$. P.P. 4/-
"GARRARD" Slimline Very lateat Compact Autochanger. Just released. Anazing value, $£ 8.19 .0$. A lso avaliable Gurrard Model 209. e9.17.6. P.P. 4/-

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100 CONDENSERS 10/Miniature Ceramic and suver Micm
Condensers 3 pH to $\delta, 000 \mathrm{pH}$ LIST VALUEOVLUR 生

IVORY/GOLD ENOBS $1^{\prime \prime}$ Diemeter, half price $1 / 2$, 5 for $4 / 8 ; 11^{\circ} 1 / 8$. 5 for $5 / a$

VALVE HOLDERS. B76, 6d es., with Screen 8d, ea. B9A, 8d ol, with Screen Screen
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 Caravan?
Tooperate yourrazor from car battery or surt-
able for many other uses, wo offer Mótor Generator 12 v
input, output. which must have cost at least \&io to make for only 1 cost a 4/6 post and insurance.

The J.B. Tangential Air Conditioner
"A jolly fine set but deserving a better case,"


This is a comment which many constructors have volced and therefore we now offer a De Luxe version of the Pocket Companton. This uses a solid hide case of very pieasant red tering and letPocket Companpocket compan15 guinea has the
The most up-to-date superhet portable of its type it uses a transflter in conjunction with Philco R. $\mathrm{F}_{\text {. }}$ transistors and Mulard output transistors. Complete bullding costs with plastic case s6.15s. or with solld hide case. $27.15 s$.
If you have already built and want to change your case, then return the plastic case with a postal order for send 26/-, plus $1 / 6$ Post and Ins. for the hide case only. AGENTS WANTED TO BUILD OUK COMPANION PORTABLES. SEND S.A.E. FOR FULL DETAILS.

Tancenplacement caused by the new Tangential fan is quite amazing, but What is more amazing is the almost complete absence of nolse.
Stand the J.B. A1r Conditioner on a window ledge near an open window, and you can have alther extraction inana or inpur of clean. new air. depending upon which way you turn
In addition to a fan for moving the alr, the unit also contains a heater and control switch. Wired such that may be used The total bullding cost of this offeconditioner is $\begin{aligned} & \text { at a specially low price dut is }\end{aligned}$ the summer months. this price namely 28.10 .0 , plus 5 - carriage and insurance. The case is very nicely finished in hammered enamel, and when assembled, the unit is indistingulshable from those selling at £12 and more. Don't miss this spechal summer offer.

## Adjustable Thermostat



Sultable for Industrial or domestic purposes, such as controlling furnace oven, immersion heater etc. Can also be used as a flamestat or flre alarm. Made by Sunvic these are approxdmately 17 long and adjustable over a range 0 to 550 F . The contacts are rated at 15 amps., 230 volts, and the adjustment spindle, whtch comes to the top, can be fitted with a flexible drive cor remote control or just a at 93 or 24 each. these are offered at only $10 / 6$ plus $2 / 6$ postage and a surance.

Introducing the J.B. Range of Transistors
Try these, you will be very pleasedJB1. All wave mixer
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## Transistor Components Send S.A.E. for our new price list, just printed

## ROMANTICA 7

Cheaper than you can possible make 1t. We offer a completely made up transistor Pocket Super het. Uses all first made minialeather case is complete with battery. $535-1065$ earphone and vity 300 micro volts/M. sensiti150 mW , ferrite slab aeria output approximately $4 t x$ arial. Size Price £6.19.6. Post and Lns. $3 /$ -


## Cabinet \& Pick-up

Cablnet ior battery record plaver. Size approx. $9 \times 11 \times$ speaker and or $7 x$ 4in. speaker and amplifer. Must have cost two tone. to make. New and perfect Offered whilst stocks last $19 / 6$, plus $4 / 6$ post and insurance.
Cosmocord Pick-up As illustrated with cartrldge and headrest. Ready new and perfect. Suitable 9/6, plus $2 / 6$ post and insurance.

CLOSED CIRCUIT TV
If you feel luke taking a day out we invite you to our studio here at Eastbourne and will domonstrate 405 and 625 systems. as well as under water
and other types of instaliations. We hav: equipment for sale or loan, and will be plad to discuss any proposals which you may have. You will be interested to note that a transistorised camera for working direct into a domestic TV recelver can now be purchased for llttle more than the cost of a good photo camera.

## The 'Good Companion'

## Mk.l| using

## Transfilters

In the 'de-luxe' cabinet as illustrated it cost what a set! build-but what a set!
scan these pages: you will find nothing to compare with its specifilters instead of IF transtormers, has vari able feedback as well as
 rite Aerlal, Slow Moton powerful Medium \& Long Wave set, conservatively rated at 750 mW . Every component used is by a famous maker, such as American Philco MADT R.F. transis-tors-Mullard A.F. transistors-Jackson Brother's tuning condensers-Rola-Celestlon loudspeaker-Dubilier-1.C.C.-Morganite resistors and controls. Also full after sales service avallable.
You will definitely be doing the right thing if you
buy a Good Connanion.

with high grade rexine fitted with rubber feet. The ront is particulariy nice being made Size approximathorizontal gold bar. Size approximately litin, wide, 8 in. dimilar record player or tape deck similar record player or tape deck least es eqch our special cost at $35 /$ - each carriage and insuran price
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## Power Unit

A ugeful source of D.C. for experimenting energising instruments electroplating, reactivating batteries etc. This power unit can be made in a few hours and due to the avallability price. we can sunply the a very low of parts with supply the complete kit of parts with ABC instructions, fits and tnsurance for 9s. 6d. plus 1s. post and insurance.

Building A 'Scope ?


31n. oscilloscope tube. American made type No. 3FP7. 6.3 v. 0.6 amp. heater, electrostatic deflection, brand new and guaranteed with circult diagram of scope, 15/ each, plus $2 / 6$
post and insurance.

## Last of these

## Brayhead

 Turret Tuner Complete with Band 1 and Band 3 coils. New but removed from unused equipvalves $15 /-$ eac valves $15 /-$ each or with valves $25 /-$each. Post $2 / 6$ (Knobs $3 / 0$ extra).


## Fishing Rod from Dinghy

Mast Tubular aluminium not sebarate seethons, extends like telescope from $15 i n s$ to $9 \mathrm{ft} .6 / 6$ each.

## Transfilters

These ceramic devices save alignment problems and improve performance. Use instead of $\mathrm{I} . \mathrm{F}$, transformer. Complete with circuit. $8 / 6$ each

Miniature Microphone American made. DVnamic at 2/6, plus ud. postage.

Blueprint Receiver
The International SW2 All components to make up this receiver as described in the Apri-
issue are avallablc.
Price $39 / 6$. issue are avallabic. Price $39 / 6$.
plus $2 / 6$ postage and insurance. plus $2 / 6$ postage and insurance. Note this price does nheadphone.
A.C./D.C. Multimeter Kit Ranges:D.C. volts $0-500$, , $0-1,000$ A.C. volts $0-5,0-500$ $0-100,0-500,0-1,000$ D. C. milliamps $0-5$. 0-100. $0-500$, Ohms O-50,000 with internal battertes. O-50.01 Wrather Measures A.C.ID.C. Measures A.C.f.C. and ohms. All the essential part
 essential parts including metal case, 24n. moving coll meter, selected resistors, wire for shunts, range selector, switches. callbrated scale and full instructions.
Transistor Set Cabinets


Very modern cream cabinet. size $5 \frac{1}{2} \mathrm{x}$ $3 \times 1$ in. with chrome handle, tuning knob and scale. Price 7/6, plus 1/6 postage and packing

## MULTI-METER BARGAINS!

MODEL 200 H (Illus. on right). 20,000 ohms per volt, 20 ranges comprising A.C. volts, 5 ranges up to 1,000 V D.C. volts, 6 ranges up to $2.5 \mathrm{KV}, \mathrm{C} . \mathrm{C}$. current, 3 ranges up to 26 ohms, rasistan 2 ranges up to 6 meg. capacity 2 ranges up to 0.1 , esistance, 2 ranges up to 6 ma. capacity 2 ranges up olo decibels -20 to +22 . Scale cornerwise to the equivalent of 4 in . movement is a pocket size instrument measuring $4 \frac{1}{2} \times$ instrucrions, price $£ 6.19 .6$, post free.
MODEL EPIOK. Similar in size and appearance to 200 H acept this is 10,000 hms per volt and maximum D.C volts 1,200 instead of 2.5 K , also no capacity range. Price C5.19.6. Post free.


## ALL METERS BRAND NEW AND FULLY GUARANTEED



MODEL TP5S. (Illus. on left). 20,000 ohms per volt, D.C volts, 5 ranges up to 1,000 A.C. volts, 5 ranges up to 1,000 resistance, 2 ranges up to 10 meg., capacity 2 ranges up to 0.1 decibels - 20 to +26 . One switch control really beautifully made precision instrument, size only $3 \frac{1}{2} \times 5 \frac{1}{2} \times 1 \frac{3}{4} i n$., price only $£ 5.19 .6$. Fost tree.
MODEL TPIO. Similar in size and appearance to TPSS, but sensitivity 2,000 ohms per volt, price $£ \mathbf{3} \mathbf{1 9 . 6}$. Post free. MODEL UI. A robust instrument of 1,000 ohms per volt sensitivity A.C./D.C. volts up to 1,000 D.C. current up to 500 , resistance up to 200 K , size $5 \frac{1}{4} \times 3 \frac{1}{2} \times 2 \frac{3}{4}$ ins. complete with test prods, single switch control, large easily read scale, price only $£ 2.19 .6$. Post free.

lifier?
Hero 1 s a buy for Unit Type 20 . ConUnit Type 20. Contains parts dieal for building alarge output amplinel and alreads set out name a tow:name aicw Valves Type KT44. Driver valve Type Ir1H41. Iron cored choke fo up to 200 milli-amps. Dozens of wire wound and carbon resistors, paper and mica condensers.
Terminals and tag panels, etc. etc.
everybody and well Three other items of interest tu ev
worth the price asked for the unit are:- This can act as auto transformer to convert 230 to 110 or 230 to 460 , and also as a flament transiormer 230 to 63 or 230 to 12.6 volts

- Mliniature (ireuit

2. Miniature cireut isreaker. For
gmps A.C. reset by pusing knob. Sicel Case. With heavy gauge ch
cut out and fitted valve holders etc price for complete unit is 19 s . 6il., carriage $5 /-$
Portable Tape Recorder for only

£6.19.6
You'll be really thrilled at its performance. Superior to many seling at $£ 12$ to $£ 15$. Supplied as sub-assemblyes which fro together in about an hour. Three transistor amplifier with centre switch lorward-stop-rewind with microphone input record play-volume contw-tone and with microphone reel of tape and spare reel. Nothing else to bus. Do not miss this bargain! Gmiy f6.19s. 6d., plus l"oal \&

Making An Extension Speaker?
 be cut through middle to make two stereo cabinets. Bargaln at only 9/6,
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Parcel of Electric Switches and Switch Plugs
All bakelite types, suitable for normal housewiring. Parcel comprises, 6 oblong 1 way 5 amp, 4 oblong 2 way 5 anp. two 5 amp 3 pin switch socket. Value easily $25 /-$, yours for $10 \%$, plus 2/6 postage etc.
Parcel of Mica Condensers 50 all very useful valves. Total list price over $£ 5$ and yours for $5 /$-, plus $1 / 6$ post.


Lens system for direct TV Infira-Red Bingenlars
See in the dark for night hunting etc You get 2 complete optical systems (could be used for T.V. camera) and casein cells. Part of the Tabby equipment. Unused, believed in good order, but no guarantee at this silly
orice of $\mathbf{f 2 . 1 \% . 6 \text { . Dlus } 1 0 / \text { - carriage. }}$ orice of $£ 2.17 .6$. dlus $10 /$-carriage.

## ELECTRONIC



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Including PP3 battery and $\therefore 5$ yards lead with plugs A completely Portable Intercom with 101 uses being ideally suitable for the office or even as a Baby Alarm. since being battery operated, ivtem and volume on/off switch, the units are housed in attrao on/of tive plastic cabinets (black/white) with chrome stands, it is extremely economical operating on
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 We also supply the assembled MAIN AMPLIFLER only (exCludes control unit) for operation with our DUAL CHANNEL PREAMPLGFLER, this provides for a more versatile or elaborate instaliation and would be essential if a low output Masmetic Plok(a) THE ASSEMBLED MALN AMPRI

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## Incorporates two Mullard 2 -valve Preampilifers combinard ${ }^{2 \text { nvo }}$

 Single unit enabing it to be used For both sitrazinionic or MoNaURAL operation. It is desisned primarily to operate writh OUR range of MULARD MAAN AMplifiers but will also operate equaily well with hay make of Ampl-fors requirng an input of 250 on

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 OFPERES ASSEDHLED and Besed on a oxtra). Mased on a recent design by THREE" is ideally suited "TWIN in PORTABLE RECORD PLAY. ERS for which purpose we offor a specially designed Portable Case. It Incorporates MULLAAD ECL86 valves, separate $B A$ and TREBLE CONTROLS, and produces excellent reproduction of up to 3 watts per channel. Frequency response is $40 \mathrm{c} / \mathrm{s}$ to 30 Kc/s. Sizeisonly $11+\times 3 \times 5 \mathrm{~m}$.
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The PD8 and 84 comprise two self-contained units to add
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 Incorporating GARRARD TAPE DECK and MOLI;L MF/GきP PIRE-ANIPLIFIER Supplied on ONECHASSIS (as mustrated) READYFOR USE 18 Gns. FOR USE
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50,000 ohms
5,000 ohms
A truly efficient Meter for the amateur or profes sional man, having features found normally in more expensive Meters. Ranges:
D.C. volts $2.5-10-50-250-1 . K$
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 T SPECIAL OFFER we have a limited evantity of HMV Model 544 STEREO AMPLIFIERS

 Size $11!\times 10 \times 41 n$, high.
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A complete Stereo Amplifer incorporatio for Crystal or Ceramic Stereo Pick Ups producing 4 watts peak output per channel from input of $200 \mathrm{~m} / \mathrm{volts}$. Operates wiwa

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$\mathrm{CP} .3 / 370 \mathrm{pF}$ and CP. $3 / 500 \mathrm{pF}$. These 3 waveband Coil Packs are available for use with either 370 pF or 500 pF tuning condensers. The coverages are: Long Wave 800-2,000 metres. Med. Wave 200-250 metres, Short Wave 16-50 metres. Designed for use with "MAXI-Q" glass scale type S2. Retail price of each unit: $32^{\prime}$ - plus $9 / 7$ P.T.- total $41^{\prime \prime} 7$.
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$300-0-300 \mathrm{v} .100 \mathrm{~mA} .6 .3 \mathrm{v} .4 \mathrm{a}, 5 \mathrm{v} .3 \mathrm{a} \quad \because 20 / 9$ $350-0-3 j v \mathrm{v}, 100 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, 5 \mathrm{v}, 3 \mathrm{a} \quad \ldots 26 / 9$
 FULLY SHROUDED UPRIGHT $250-0-250 \mathrm{v} .60 \mathrm{~mA} .6 .3 \mathrm{~V} .2 \mathrm{a}, 0-5-6.3 \mathrm{v} .2 \mathrm{a}$, Midget type $2 \frac{1}{2}-3 \mathrm{Hn}$. $250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \dot{\mathrm{a}}, 0-5-\dot{8}, 17 / 11$ $300-0-300 \mathrm{v}, 100 \mathrm{~mA}, 8.3 \mathrm{v} .4 \mathrm{a}, 5 \mathrm{v}, 3 \mathrm{a} .2 \mathrm{a} 27 / 11$ $300-0-300 \mathrm{v}$. $130 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, \mathrm{C}, \mathrm{T}, 6.3 \mathrm{v}$. 1a, tor Mullard Amplifior $\begin{array}{lll}350-0-350 \mathrm{v}, 100 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, 5 \mathrm{v} .3 \mathrm{a} & 033 / 9 \\ & 50-0-350 \mathrm{v} .150 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, 5 \mathrm{v} .3 \mathrm{a} & 071\end{array}$ $425-0-425 \mathrm{v} .200 \mathrm{~mA} .6 .3 \mathrm{v}$. $4 \mathrm{a}, \mathrm{C} . \mathrm{T} .5 \mathrm{v}$. $3 \mathrm{a}^{\circ} \quad 35 /-$


## Assembled

 6/12v. 4-5 amps. Fitted Ammeter and variable charge rate selactor. Also seleo12 plug for 6 v. or vred charging. Loured sual case with toved blue hammer and ready for $69 / 9$ use with Carr. $5 /-$ mains and output leads. Terms. Deposit $13 / 3$ and 5 monthly payments 13/3. 6/12 v. 38., all acflities as above. mly $59 / 9$, carr. $3 / 9$.FUGLI SHROUDED (eontinued)-$\frac{425-()-425 v . ~}{4 \mathrm{C}} \mathrm{T}$. $500 \mathrm{~mA}, 6.3 \mathrm{v}$. 4 a . C.T.. G.3v.
 OUTPUT ${ }^{250 \mathrm{~mA}, 6.3 v, 4 a \mathrm{C} . \mathrm{T} .5 \mathrm{~V} .3 \mathrm{a} . .69 / 9}$ Midget Battery Peatode $66: 1$ for 3S4, etc.
Smali Pentode, $50000 n$ to $3 a$ 4/6
Smail Pentode $7 / 8,000$ a to $3 a$
Standard Pentode 5,000 to $3 \Omega$
Standard Pentode 7.000 to 30
$10,000 \Omega$ to $3 \Omega$
Push-Pull 8 watts. EL $\ddot{84}$, or $\ddot{6} v 6$ to Push-Pull $10-12$ watts to matich $6 \mathrm{~V} \dot{6}$ or EL 84 to 3-5-8 or 150
ollowi Push-Pull 10-12 or and 15 a speakers: ush-Puil 15-18 watts 6V6 or EL84 $\ldots 18 / 9$ Push-Pull for Mullard 510 KT60 $\because 2$ 2/9 Linear for Mullard 510 Ultra


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6 . or 12 v . 2 amps.
Fitted Ammeter and selector plug for 6 v . or metei Louvrea metal case finhammer blue. Ready for use with mains and output leads.
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BATTERY CHAILGLUR KINS Consisting of Mains Trans former, F.W. Bridge, Metal Rectifier, well ventilated steel Case. Fuses. Fuse-holders. Crommets, panels and circult. 6 v or 12 v ar
As above with Amme...... $24 / 8$ As above, with Ammeters $24 / 8$
$32 / 8$ 6 v . or 12 v .2 amps. 25/9 6 v. or 12 v. 2 amps. inclusive of Ammeter. inclu6 v . or 12 v .4 amps . 49/8 6 v . or 12 v. 4 amps, with Ammeter and varlablo charge rate selector ................. 58/9 CHARGER AMIMETERS, $\begin{array}{llll}0-1.5 & \text { a.. } & 0-3 & \text { a., } 0-4 \\ 0-25 & \text { a., } & 0-7 & \text { a. }\end{array}$

Both above size $24 \times 21 \times 2$ xins.
All with $200-250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$. primarles 6.3 v . 1.5 a. $5 / 9 ; 6.3$ v. 2 a. 7/6; 0-4-6.3 v. 2 a. $7 / 9 ;$ 2 v. 1 a, $7 / 11 ; 6.3$ v. 3 a, $8 / 11 ; 6.3$ v. 6 a 17/6: 12 v. 1.5 a twice, $17 / 6$.
$150 \mathrm{~mA}, 7-10 \mathrm{H} 250 \mathrm{ohms}$.
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All with $200-230-250 \mathrm{v}, 50 \mathrm{c} / \mathrm{s}$ Primaries: $0-9-15$ v. 1 L . $12 / 9 ; 0-9-15$ v. 2 a, 14/9; 0-9-15 $6 \mathrm{a}, 23 / 0: 0-9-15 \mathrm{v} .8$ a, $28 / 9$.
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Practical ifadio Inside Out ${ }^{2} 6$. Yaster colour Code Chart， $1 / 6$ ． Transistor controlied Models．7／6．

C．LR．T．HOOSTER TRANSFORMERS for heater cathode short circuit，C．R． tubes with failing emission．Full instructions supplied
Type A optional $w \%$ and $50 \%$ boost． 2 v or 4 v ．or 6.3 v ．or 10.8 v ．or 13.3 v ． llains inpuî́ PHICE 10／6．
LOUUDSPEAKER P．M． 3 OHM，2\}, 3, 4in., 18/6.万in．Rola，17／6；8in．Plessey，18／6；7in．I 4in．Rola， 18／－； $6 \frac{1}{2}$ in．Kola， $18 / 6 ; 10 \times 6 \mathrm{in}$ ．27／6； 10 in ．Rols $30 /-$ ； 4 in, Tweeter， $25 /-$ ；12in．R．A． $30 /-$ ；
， 2 ．
STENTORLAN HF1012．10in， 3 to $15 \mathrm{ohms}, 10 \mathrm{w}, 85 / \mathrm{r}$


## BAKER SELHURST

## LOUDSPEAKERS

vetails A．A．E．

12 in．Baker 15 w．Btalwart | 3 or 15 ohms， | $45-13,000$ |
| :---: | :---: |
| c．p．s． | ．． | 12in．Baker Stalwart，Fosm Buspension，

13,500 e．p．s．
13,500 e．p．s．$\quad .$. 12in．Stereo，Foam Sus－
pension， 12 wn， $\begin{array}{lrr}\text { pension，} & 12 \text { w．，} & 35-16,000 \\ \text { c．p．s．} & \text { ．，} & £ 6.17 .8\end{array}$ 12in．Baker Ultrs Twelve， 20 c ．p．f．to $25 \mathrm{kc} / \mathrm{g}_{4} 817,10$ 15in．Auditorium， 35 W．，
 TWIN GANG TUNING CONDENSERS．365 pF miniature lin．x $1 \frac{\mathrm{in}, \mathrm{x}}{} 1_{1} \mathrm{in} \mathrm{n}_{4,} 10 /-500 \mathrm{pF}$ standard
Fith trimmers，$\theta /-$ midget， $7 / 6 ;$ with trimmers， $9 /-$ ． 500 pi show motion tuning $9 /-$ SMALL 3 gang 500 pF ，
SINGLE $25 \mathrm{pF}, 50 \mathrm{pF}$ ， $75 \mathrm{pF}, 100 \mathrm{pF}, 160 \mathrm{pF}, 5 / 6$ Solid dielectric $100,300,500 \mathrm{pF}, 3 / 6$ ．
CONDENSERS．New stock 0.001 mid． 7 kV T．e．c．， $5 / 8 ;$ Ditto， $20 \mathrm{kV}, 9 / 6 ; 0.1 \mathrm{mfd}, 7 \mathrm{kV}, 9 / 6$ Tubular 500 V． 0.001 to 0.05 mtd ．，9d． $0.1,1 /=$ ．．2v，1／8． 0.57500 v．，1／8． $0.1 / 350$ v．， $9 \mathrm{~d}, 0.1 / 2,000$ v CERAMIC CONDS 500 ， 0.
CERAMIC CONDS． $000.3 \mathrm{pF}^{\text {to }} 0.01 \mathrm{mfd}$ ， 9 d SILVER MICA COIDEENSERS． $10 \% 5 \mathrm{pF}$ to 500 pF ． Od．i 500 pF to $3,000 \mathrm{pF}^{\text {，}} 1 / \mathrm{m}$ ．Close tolerance－
 to $510 \mathrm{pF}, 1 /-; 1,000 \mathrm{pF}$ to $5,000 \mathrm{pF}, 1 / 9$.
 rrice 15／－．Uses B，F．O．Unit，ZA 30038 ready made with valve IS5．POCKET required full instructions supplied． Battery $8 / 6$ extra 69 V 13 V ．Details S．A．E．

## WAVECHANGE SWITCHES <br> 8 p .4 －way 2 wafer long spindle

$2 \mathrm{p} . \stackrel{2}{ }$－way，or 2 p． 6 －way long spindle or 4 p．$\ddot{2}^{6 / 6}$ way or 4 p．3－way long spindle．
3 p． 4 －way，or 1 p． 1 tw－way long＂pindle＊$\quad$ ． $3 / 6$ Wavechange＂MAKITS＂，Wafers avail－ able； 1 p． 12 way， 2 p． 6 way， 3 p． 4 way， 4 p． 3 way， 6 p． 2 way． 1 watel，switch $8 / 6$ ； 2 wafer switch，12／6； 3 wafer switch．16／－： additional wafers up to $12,3 / 6$ each extra． Togele wwitehes，s．p．，2／－：d．p．，3／6； d．p．t．d．，4／－．Ex．Govt．s．p．d．t．， $1 /=$

## Procision ensineered．Ifin，dia．$x$ in <br> A（O＇S 39－I I）ELUXHOTICK NIKE 35／－

Valvehohlers．Pax．int．oct．4d．EA50， 6d．B12A，CRT，1／3．Engl．and Amer．4， 5 ， 6 and 7 pin， $1 /=$ MOULDED Mazda and int．oct．，61．；B7G，B8A，B8G，B9A．Ed． B7G with can， $1 / 6$ ．B9A with can． $1 / 9$. Ceramic EF50，B7G，B9A．int．oct． $1 /-$ B7G，B9A cans， $1 /$－each．
 A．C．only， $200-250$ v．Valves ECL 86 and EZ80．is watt quality output．Mullard tone circuits，bass boost，treble and Volume controls．Separate engraved Perspex front－panel with de－1uxe finish． Heavy duty output transformer 3 ohm， enamelled chassis size 6 in．$x$ in stovo Rarpain Priceft 100 Circuit supplied

THE ORIGINAL RADIO COMPONENT

Volume Controls $80 \underset{\text { cable }}{\text { anm }}$ COAX Linear or Log Tracks Bemiebly spaced tin. Long spindies Midget $\begin{gathered}\text { Stranded core. } 6 d . y d . \\ 40 \text { yds, } 17 / 660 .\end{gathered}$ ${ }_{5} \mathrm{~K}$ ohma to 2 Meg , $60 \mathrm{Fds}^{2} 2 \mathrm{~J} /$


TELESCOPIC CHROME AERIALS. 13in. extebilng to 43 in ., $8 / 6 \mathrm{ea}$ Coax Adaptor Plug, $1 / 6$ extra. TRIPLEXERS Bands $L$, IT, III COAX PLUG . $1 /=$ LSAD SOCKEXES FANEL SOCKERS $1 / \sim$ OUTL 80 or 300 ohme DITTO SCREENED per yd, $1 / 6$. 80 ohms only. DITTO SCREENED Der Fd, WATT, Pre-set MIn. WIRE-WOUND POTS, 3 WhTT' 25 K ., $3 /-$ ea
 WIRE-WOUND 4 WATT Pots. Lons spindle. Values, 50 ohus to 50 K ., $8 / 6 ; 100 \mathrm{~K} .7 / 6$. PHILIPS TRIMMERS, 0-10 pIr, $3.30 \mathrm{pF}, 1 /$ TRIMMERS, Ceramic. $30,50,70 \mathrm{pr}, 9 \mathrm{~d}_{0} ; 100 \mathrm{pF}$, $150 \mathrm{pF}, 1 / 3 ; 250 \mu \mathrm{~F}, 1 / 6 ; 500 \mathrm{pF}, 750 \mathrm{pF}, 1 / 0$. TI. V, ete. TRIMMER, $1000 \mu \mathrm{~F}$, with knob, $2 /-$
RESISTORS. Preferred valuen. 10 ohms to 10 mego,
 HIGH S'CABILITY. tw. $1 \%, 2 /{ }^{\circ}$. Freferred values. $10 \Omega$ to 10 meg. Ditto $5 \%, 100$ to 22 meg. 80 . 5 watt 10 Watt $\left\{\begin{array}{c}\text { WIRE-WOUND RESISTORS } \\ 10 \text { ohms- } 10,000 \text { ohm }\end{array}\right\} \begin{aligned} & 1 / 3 \\ & 1 / 6\end{aligned}$ 15 watt $\left\{10\right.$ ohme- $10,000 \mathrm{ohms} \int \begin{array}{l}1 / 8 \\ 2 / \mathrm{F}\end{array}$ 12.5 K to 50 KK 10 w

 Double Play 7in. reel, 2,400ft. 60/- Spare 5in, reel, $1,+100 f$ t. $38 / 6$ Plastic Long Play 7in, reel, 1,8001 . $35 /-1$ Reels | $5 z i n . ~ r e e l, ~$ | $1,2 n 0 f t$ | $83 / 6$ | $3 i n$ |
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| sin. reel, goott. | $18 / 6$ | $1 / 6$ |  |
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Standard 7in. reel, 1,200ft. 26/- 54, 2/"Instant" Bulk Tape Eraser and llead Defluxrr, 200/250 v. A.C.. 27/6. Leafet with full detrails. A.A.F.

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GRYTAL DIODE G.E.C., 2/-, GEX34, //-, 0A81. 3/-. HIGH RESISTANCE PHONES. 4,000 ohma, $15 /=\mathrm{pr}$. SWITCH CLEANER. Fluld squirt apout, $4 / 6$ tho.

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Vliniature Contact Cooled Mintature Contaet Cooled. 250 V 50 mA ; $7 / 650 \mathrm{~V}$ $85 \mathrm{~mA}, 8 / 6 ; 200 \mathrm{~mA}, 21 /-; 300 \mathrm{~mA}, 27 / 6$.
TV otc.. Silicon Slls.-Min. Ikectifier. 125 V . $300 \mathrm{~mA}, 6 / 6 ; 250 \mathrm{~V}, 300 \mathrm{~mA}, 14 / 6$.
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Colls Wearlte "P"' type, 31-each.
Osmor Midget "Q" type. adj. dust core. Trom 4/- each. All ranges.
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H.F. Cinokes, 2/6. Osmor (k'1, 6/9.

Repanco Screwdrlver, sin, 6d
Neon Mialns Tester serewdriver, 5/Solder Radiograde, 4d. yd., tib. 5/= Solder Radiograde, Ad. yo., tib. Si=.

Aluminhmm (hassis, 18 s.w.g. Platn lattice fixing holes, 2 in. sides, 7 x 41 n . $4 / 6 ; 5 \times 7 n_{1}, 5 / 9 ; 11 \times 7 \mathrm{n} ., 6 / 9: 13 \times 91 \mathrm{n}$.
 $18 \times 16 \times 31 n .10 / 6$.
Aluminlum Panels, 18 s.w.g.. $12 \times 121 \mathrm{n}$. 4/G; $14 \times 9 \ln ., 4 /-; 12 \times 8 i n ., 3 / ; 10 \times 71 \mathrm{n}$. 2/3; $8 \times 61$ n., $2 /=$

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Wirowound Ext 8poarer Control, 10 ia 8 . 0.3 in FORMERS 5937 or 8 and cans TVi of 2 , $\frac{7}{6}$ in.
 $\mathrm{sy} . \mathrm{X}$ MOT OTION DRIVES. $6: 1,2 / 8$.
SLOW MOTI SOLON IRON, $25 \mathrm{~W}, 200 \mathrm{~V}$ or $230 \mathrm{~V}, 24 / \mathrm{F}$ ANTEX SUB-MIN IRON 15 w. 200 or 240 v , $29 / 6$

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MAINS DROPPERS Midget djustable sllders 0.15 ,, 000 , 1.20 ons, LINE GORD. 0.3 A 60 ohme per foot, 0.2 A 100 ohm LINE CORD. 0.3A 60 ohms per 100t, 0.2 A 100
per foot, 2 was $1 /-$ per foot; 3 -way $1 /-$ per foom per foot, 2way, $1 /$ - per foo:, 3.way $1 / \%$
MIKE TRANSFORMER. $50.1,3 / 9$.
MIKE TRANSFORMER. $50.1,3 / 9$,
P.V.C. Conn. Wire, 8 colours, single or stranded, $8 d$ P.V.C. Conn. Wire, 8 colours, single or atranded, $8 d$, yd . Sleeving, $1.2 \mathrm{mam}, 2 \mathrm{~d} . ; 4 \mathrm{~mm}, 8 \mathrm{~d} . ; 6 \mathrm{~mm}, 5 d . y d$. SPEAKER FRET. Gold cloth, $17 \times 25 \mathrm{in}, 5 / \mathrm{m} ; 25 \times$ $35 \mathrm{in}_{\mathrm{c}}, 10 / \mathrm{F}$ TJgen, varloue colours, 52in. Fide, from 10/- ft.; 26in. wide, from $5 /=\mathrm{ft}$. Samplea, $8 . A$. E. Expanded Metai, Gold, $12 \times 12 i n, 16 / \mathrm{s}$.

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Medium and long wave. Powerful 7 I 4 in. high Flux Bpeaker. T.C.C. Printed Circuit and condensers. Components of tinest quality clearly identited with assembly instructions Osinor Ferrite Aerial Coils. Rexine covered attache case cobinet. Sizu l2in. x Sin. $x$ 4in. Batteriea used B1 26 (L5512) and AD35 (L5040). 10/9 extre. Instructions 90, (free with kit.)

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Wired and tested ready for ure with above Wired and tested ready for ust with above.
All thpphire styll avaliable from $8 / \%$.
1.F. TRANSFORMERS 7/6 patr $465 \mathrm{kc} / \mathrm{s}$ slug tuning miniature can. High $Q$ and good band width. Data hosh sheet supplled.

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COITS AND THANSFORMERS FOR A 2WWAVE THANSISTOR SUPER-
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Long and Modium Wave Aerial-RAZW. On 61n. rod. 7/161n. diameter. 208pF tuning..
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NEW MELILARI TRANSISTORS Audlo OC71 0/- R.F. OC44 8/9 OA70 3/OC72 7/6 OC45 8/9 OA81 3/Suh Ninfature Condensers. 0.1 mid,
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AMATEUR TRANSMITTER. Model DX-40U. Selfcontained. 80-10 m. Power input 75 w. C.W., 60 w . peak, C.C. phone. Output 40 w . to aerial. Provision for V.F.O.
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# Practical Wireless 

Vol. XXXYIII No. 667 SEPTEMBER, 1962

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## COMMERCIAL RADIO

THE possibilities of introducing commercial sound broadcasting in this country have long been evident but until the Pilkington Committee reported, no decision could be given. The Committee reported in June and recommended that a service of local sound broadcasting should be introduced by the BBC and that commercial sound broadcasting (broadcasting financed from advertisement revenue) should not be introduced. The reasons for the Committee's decision were similar to those given for their recommendation that there should be a radical overhaul of the commercial television broadcasting services. They were that, when programmes are financed from revenue derived from the sale of advertisement time, then the planners of the programmes always, consciously or unconsciously, arrange the programmes to attract as much advertisement revenue as possible. The programmes, the Committee stated, must necessarily decline in standards and it therefore considered that local sound broadcasting should be provided by the BBC and financed from licence revenue. It had been argued that a commercial network would be able to provide the public with "what it wanted" rather than "what set of programme controllers thought it wanted". However, the Committee pointed out the fallacies in this argument: public taste would gradually be debased-unless the opportunity is available to listen to or view programmes of a high standard, such programmes can never be appreciated or enjoyed by the majority of the general public. The aim should be to improve public taste gradually yet provide programmes which are of high entertainment value.
In the White Paper published by the Government after the Pilkington report, it was stated that there has been little evidence of any general public demand for local sound broadcasting, and the Government would study public reaction before making a decision. We are inclined to think that the lack of demand for a system of local sound broadcasting is due to the lack of public knowledge of the subject; no doubt demand will increase when the public realises the potentialities of such a service. We should be interested to hear readers' views.

## MORE BLUEPRINTS

With the next issue, dated October, we are beginning another series of free double-sided blueprints. On one side of the blueprint in next month's issue, will be the first of a series of designs for a comprehensive hi-fi system. This part will consist of the main amplifier and power supply sections of the chain. The main amplifier will have a maximum output in excess of 20 W with very low distortion,

On the other side of the October blueprint will be a design for a simple signal generator covering $150 \mathrm{kc} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$, modulated or unmodulated. Provision will also be included for use of the internal audio oscillator for test purposes. Although the signal generator uses a simple circuit, is inexpensive. and is easy to build with the large clear diagrams included on the blueprint, all amateur constructors will find it a valuable addition to their range of test equipment.
|||||||||||||||||||||||||||||||||||||||||||!||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||| Our next issue dated October, will be published on September 7th.


## NEWS AT HOME AND ABROAD

TTHE following statement shows the approximate number of Broadcast Receiving Licences in force at the end of May, 1962, in respect of wireless receiving stations situated within the various Postal Regions of England, Wales, Scotland and Northern Ireland. The numbers include Licences issued to blind persons without payment.


## Sound at Wimbledon

FOR over 30 years the sound amplification and distribution for the Wimbledon Lawn Tennis Championships has been the responsibility of the Public Address Department of Standard Telephones and Cables Limited.
STC equipment feeds all sound, except commentaries. from the Centre Courts Nos. 1, 2 and 3 to the BBC and into the Wimbledon distribution system generally. It feeds a ring of monitoring loudspeakers from which the electric scoreboards are operated; it provides facilities for car-park calling, turnstile control, emergency police controll, and an overriding call sym-
term under the control of Col. A. D. C. Macaulay, the secretary of the All England Lawn Tennis Club.

An elaborate telephone system is also installed by STC to link each umpire with the chief umpire and the referee's room, and also to link the pay boxes and turnstiles.

## Fuel cell battery power for

 GEMINI two-man Spacecraft${ }^{\prime}$ YHE fuel cell, one of the most promising new ways of making electricity, will be put :o operational use for the first time
in the next phase of the United States' manned spaceflight programme.

Under contract to McDonnell Aircraft Corporation, U.S. General Electric will develop a fuel cell battery, the most advanced of its type yet produce, to supply primary power for the two-man Gemini spacecraft.

In the Gemini vehicle, fuel cells will for the first time take the place of conventional battries or mechanical power units as the primary electrical power source in space.


Two STC engineers of the Public Address (Hire) Department, making final adjustments to the amplifier equipment before the start of play at the Wimbledon Lawn Tennis Championships.

The fuel cell system was chosen for Gemini because its weight will be significantly less than that of a combination of conventional batteries and solar cells which could also be used in space flight.

The Gemini fuel cell battery will delıver a peak load of almost two kilowatts of D.C., providing primary power for all equipment aboard the spacecraft, including control, artificial environment, communication and instrumentation apparatus.

In addition to its electrical output, it will have a by-product in the form of pure, potable water, accumulating at the rate of one pint per kilowatt-hour of operation. This water can be used, without treatment, to augment the supply stored aboard the spacecraft for drinking, cooling or other life-supporting purposes.

The system is based on General Electric's ion-exchange membrane fuel cell, which produced electricity through the chemical reaction of oxygen and hydrogen. A fuel cell battery is composed of many of the sand-wich-like cells connected in series to form building blocks that can in turn be connected in series or parallel to meet specific power requirements. Each cell is separated into two sections by the membrane, a sheet of tough plastic.

In operation, hydrogen gas is fed to one side of the membrane and oxygen to the other. Electrons from the hydrogen atoms are picked up by a thin metallic electrode in contact with the membrane surface, while the remaining hydrogen ions pass through the membrane. The electrons flow into an electrical circuit, providing power, and then return to the other side of the membrane, where they re-combine with the ions and join with the oxygen atoms in the formation of water.

## Radio tour of the Guildhall

'「HE Lord Mayor of London, Sir Frederick Hoare, inaugurated the Radio tour of the Guildhall in the City of London, on July 5th this year. The radio tour enables visitors to hear a taped commentary of the 15 th century Hall and its Crypt, its connections with the Corporation of London, the Freedom of the City and the Livery Companies, by means of a hand-held


The Mullard research laboratories at Salfords, Surrey, was visited recently by representatives of the Press. At these up-to-date laboratories, much experimental work is carried out on colour television, transistors, computors, and many other aspects of the electronics industry.
receiver which picks up the transmissions which are radiated at a fixed frequency.

## Radio for Mobil Tanker

r"HE "Mobil Endurance", a tanker built for the Mobil Shipping Co. Ltd., has been fitted with radio equipment by Associated Electrical Industries Ltd.

The "Mobil Endurance", which has now completed her acceptance trials, is the third of five vessels to be built for Mobil at Gothenburg. All five ships will finally be fitted with AEI marine apparatus. The radio installation on the "Mobil Endurance" will include a 600 W W.T./R.T. transmitter, a 28 channel international channel transceiver and an AEI "Escort 601" Chartplan radar.

## Satellite Communication System Ground Station

ALMOST all of the equipment at the British Post Office Satellite Communication Ground Station at Goonhilly Downs, Cornwall, planned for the initial experimental projects Relay and Telstar, is of British design and manufacture.

The predominating feature of the facilities which have been provided is an 85 ft diameter steerable aerial. The aerial is in the form of a paraboloidal dish with
full automatic steerability over the hemisphere above the horizontal plane on the basis of predicted orbital data, and manual control for resetting purposes.

The steering of the aerial in azimuth and elevation is by means of closed-loop servo type motors. The angular positions of the azimuth and elevation shafts are indicated by digital shaftangle encoders.

Not the least important of the equipment at Goonhilly, the design authorities for which are the Space Communications Branch and the Research Branch of the Post Office Engineering Department, is the variety of cables which form the vital interconnections between the aerial and the control building, as well as those on the equipment on the aerial itself. The former cable runs in troughs above ground level.

British Insulated Callender's Cables Limited have supplied no less than 20 miles of cable, comprising all of the coaxial cable ( $31,000 \mathrm{yd}$ ) which runs from the azimuth and elevation position encoders back to the control building-a distance of about a quarter of a mile-and some 5000 yd of the multicore PVC SWA PVC sheathed $250 / 440$ and $660 / 1100 \mathrm{~V}$ control cabling between the aerial and the control building.

# MEDOUM Wave POCKET SUPEPHET 



by J. G. THOMPSON

AN ECONOMICAL<br>PORTABLE RECEIVER

$\leftrightarrow$HE circuit of this receiver is shown in Fig. 1, and has the advantage that the battery drain is quite small. The full superhet circuit provides very good sensitivity, and the single-ended pushpull output stage is particularly economical. Current consumption, at low volume, is only about 8 mA . At average listening volume, this rises to about 12 mA to 14 mA or so. The usual small type of 9 V battery thus has a long working life.

## Coverage

The receiver tunes medium waves only, as this simplfies the first stage, but it is possible to add long waves later, without disturbing other parts of the set.

If possible, it is recommended that an OC44 is. used for Tr1, with OC45's for Tr2 and Tr3, and an OC71 for Tr4. However, other transistors of similar type were found to work satisfactorily in these stages. For the output stage, a maker's matched pair of OC72 transistors ( $2 \times$ OC72) should be fitted. Resistors R18, R19, R20 and R21 should also be of $5 \%$ tolerance, while all others can be of $10 \%$ tolerance. Correct working conditions will then be assured, without any need to experiment, or change resistor values.

## Poxalin Ponel

This should be made first, all important drilling being finished before mounting any parts. The panel is $5 \frac{1}{4} \mathrm{in} . \times 3 \mathrm{in}$. $\times \frac{1}{16}$ in. thick, this giving a little clearance all round in the specified cabinet. Drill three holes so that the panel can be secured in the case by short 6B.A. bolts. (A piece of thin card can be used as a template, piercing holes in it in the correct positions.)


Fig. 1-The circuit diagram.

The gang condenser fits in a fairly large clearance hole. Check that there is space for the battery, with at least $\frac{1}{8}$ in. to spare; then, drill holes for the three short 4B.A. bolts shown in Fig. 3. The pierced card will show exactly where to drill. If the screws project more than the thickness of the condenser plate, washers are needed under their heads.
readily in the case, with battery. Note that the case tapers slightly towards the back; there should be a little clearance all round.

The loudspeaker is now removed until the set is wired. When finally mounted, it is held by two 6B.A. countersunk bolts, inserted from the front. The bolt near the rod mount has two nuts, one locking the loudspeaker, and the other giving

## Volume Control

Mount the volume control as in Fig 2. One switch tag projects up through a hole, and the other tags are bent flat. Check that the set will fit in the case, and that the battery can be accommodated. The volume control slot in the case will need widening slightly, with a small file. It may also be necessary to enlarge the tuning condenser hole.

These parts are then removed, and the holes are drilled for the four screened coils. If the pins are pressed on the thin card template, this will show where to drill. Check that each corl fits easily, then place it on one side. If any holes are not quite correct they can be enlarged with a small round tile.

## Loudspeaker Mounting

The loudspeaker hole is about $\frac{d}{d}$ in. larger all round than the loudspeaker magnet. It can be made with a washer cutter, a fretsaw or other very small saw, or by drilling holes, and clearing up with a half-round file. Temporarily position the loudspeaker, mark the two speaker fixing holes (Fig. 3) and drill them. After drilling holes for the driver transformer,


Fig. 2-The layout and wiring diagram of the rear of the receiver panel.
correct clearance between loudspeaker and panel, a third nut then being tightened behind the panel. The remaining loudspeaker mounting hole (Fig. 3) is obscured by the driver transformer. A short countersunk bolt is therefore inserted from behind, and locked with a 6B.A. terminal head. The transformer can then be permanently mounted. Another 6B.A. bolt may then be inserted from the front of the loudspeaker, and run into the terminal head. washers or nuts providing spacing.

## Construction

All wiring is of 26 s.w.g. tinned copper wire, insulated with 1 mm sleeving. It will be helpful to use red sleeving throughout the positive side of the circuit, and black sleeving throughout the negative line, with yellow or some other colour for all other leads. Sleeving is also placed over all transistor leads, and the wire ends of all resistors and condensers. Sleeving on the transistor leads can be of such a length that the
transistor lead holes can be positioned as in Figs. 2 and 3. A short 4B.A. bolt holds the rod mounting. Clean up all holes, and mount the rod. gang condenser, speaker, driver transformer and screened coils, and check that the whole can fit
tops of the transistors Trl to Tr4 come about level with the tops of the screened coils; Tr5 and Tr6 are bent over as in Fig. 2. Be sure that the transistors are in their correct stages, and that the collector base and emitter leads all emerge as


Fig. 3-The wiring on the front of the panel.
shown by the letters $\mathrm{c}, \mathrm{b}$ and e in Fig. 3.
The various points marked MC form the earth, or positive, side of the circuit, and are all joined. These include the can tags of the oscillator coil and I.F. transformers, and the metal frame of the gang condenser.

## Control Wiring

Fig. 4 shows the tag side of the volume control. the speaker will occupy. Electrolytic condensers are wired with the polarity shown in Fig. 3. Other condensers. and all resistors, may be wired in either way round. The negative end of the diode must go to pin 1 of the third I.F. transformer.

C13 and R16 are wired in parallel. The wire end of R16 passes through a hole, to the MC tag in Fig. 3. The negative lead of C13 goes to the same hole as the emitter of Tr4, to which it is joined.


Another view of the completed set, less its cose.

The negative end of C15 passes into the same hole as the collector of the one OC72, as in Fig. 2 , these leads being joined, and also going to R19, R20 and R2? (Fig. 3).

It is best to leave all the transistor leads reasonably long, but prolonged heating with the soldering iron should be avoided.

The larger fixed condensers are mounted behind the panel. as in Fig. 2; C5, C7, C9 and C11 each have a lead passing directly down through the panel, and all are soldered to the MC or earth line. The top wires of these condensers

are bent over, and pass down through other small holes, as in Fig. 2, so that they can be connected as in Fig. 3.

CI4 and C15 must have insulated sleeves, or be covered with insulated material. They are secured side by side with tape, and rest on the speaker magnet. C14 goes from the positive line to the negative line. C15 is wired from collector to loudspeaker, as in Fig. 2.

In Fig. 1, short pieces of thin coloured flex are soldered to the aerial winding tags, for identification. Both "earth" ends of the windings are joinect, for the orange lead. These leads are then connected up as in Fig. 2. That is, orange to condenser frame, red to T1 and VC1, and black to CI, Fig. 3.

After checking the wiring, solder lengths of thin flex to the $75 \Omega$ loudspeaker. One lead goes to MC in Fig. 3, and the other passes back to the positive end of C15. Fix the loudspeaker as described, making sure that its tags do not bear upon leads or parts already fitted. The loudspeaker itself is of insulated material. The spacing between loudspeaker and panel should be so adjusted that the


The receiver mounted inside its cose.


Fig. 4-The details of the volume control and tuning condensers.

A strip of paxolin or similar material should now be filed so that it will engage with the coil and transformer cores, to be used as an adjusting tool.

If a signal generator is available, set it for $470 \mathrm{kc} / \mathrm{s}$. with modulation, and connect its output to the black lead in Fig. 2, including an isolating condenser in circuit. Put the receiver volume control at maximum. reducing the generator signal, if volume is 100 great. The three transformer cores are then adjusted for best results, which will also be the highest reading on the meter included in the battery circuit. All cores should have quite a sharp tuning peak.

## Alignment on Stations

If no generator is available, tune in the local station, adding an external aerial a few feet long. if required. Then adjust the three transformer cores for best volume. They should be in a reasonable position, not screwed right in, or very far ont.

Aerial and oscillator stage tuning can then be adjusted. TCl and TC2 must be capable of reaching a low capacity. To begin, unscrew both trimmers, carefully separating the plates, if necessary. If a signal generator is available, adjust it to 550 m , close the gang condenser, and rotate the oscillator coil core for best results. Then move the aerial winding on the rod, to obtan maximum volume. The generator is then set to 205 m . the gang condenser is opened, and TC1 and TC2 are adjusted for best results.

If coverage is restricted on the low wavelength end of the band, this probably indicates that TCI and TC2 need opening to a lower capacity. Repeat the trimming and inductance adjustments described a number of times, always adjusting the trimmers at a low wavelength, and the aerial and oscillator coil inductances at a high wavelength. Keep the receiver volume control at maximum, but choose
(Continued on page 417)

# INCREASING voitmeter RANGES 

By G. A. W. Partridge



HERE are several types of high reading voltmeters on the market-the multimeter which caters for current and resistance measurement usually reads up to 1000 V . But not all instruments have such high ranges. There are, however, quite simple ways of increasing the range of a voltmeter either permanently or temporary.

The most well-known method is to use a resistance type of multiplier connected as shown in Fig. 1. In this case a $0-500 \mathrm{~V}$ instrument is able to read from $0-1,000 \mathrm{~V}$, by connecting a suitable resistance known as a multiplier in series with it.

## Multipliers

The following example will show how a multiplier is chosen. The voltmeter reads from say, 0 to 100 V and it is desired to increase its range to 1.000 V . The sensitivity of the voltmeter is 10.0002/V.

The total resistance of the meter and the multiplier must be $1.000 \mathrm{~V} \times 10.000 \Omega 2 / \mathrm{V}$ which is $10,000.000 \Omega$. Now the resistance of the meter alone is $100 \mathrm{~V} \times 10.000 \Omega 2 / \mathrm{V}$ which is $1.000,000 \leq 2$.
$10,000,000-1,000,000=9,000,000 \Omega$; the required resistance of the multiplier.

## Alternative Calculation

Another way of calculating this resistance is first to find the current taken by the meter on its own, at full scale deflection, which is 100 V .

$$
\mathrm{I}=\frac{\mathrm{C}}{\mathrm{P}} ; \quad=\frac{100}{1,000,000}
$$



Fig. 1 (above)-The use of a multiplier to increase the range of $a$ voltmeter.
Fig. 2 (below)-A transformer used as a multiplier.


$$
I=\frac{1}{10,000} \quad A \quad(0 \cdot 1 m A)
$$

At full scale deflection with the multiplier in circuit it must still draw $0 \cdot 1 \mathrm{~mA}$. The voltage across the multiplier will be $1000-100=900$. Its resistance will be:-

$$
\begin{aligned}
& \mathrm{R}=\frac{\mathrm{E}}{\mathrm{I}} ; \quad=900 / \frac{1}{10,000} \\
& \mathrm{R}=9,000,000 \Omega
\end{aligned}
$$

In this case the instrument reading will have to be multiplied by 10 to give the correct voltage. The wattage of the multiplier is also important. It will be given by I.E, which is $1 / 10.000 \times 900=$ 0.09 W . A 0.25 W resistor will be ample here as it will not overheat.


Fig. 3-Converting a milliameter for use as a voltmeter.

If alternating current is to be measured, the calculations must be based on the internal impedance, or ohms-per-volt rating of the instrument as an A.C. meter, not as a D.C. instrument. The multiplier must be non-inductive.

There are special types of instrument resistors on the market which are designed to remain at constant values for many years.


Fig. 4-The voltage divider.

## Transformer Multiplier

For temporary and less accurate A.C. work, a transformer can the used as a multiplier (Fig. 2). In this case it has a ratio of $220 / 110 \mathrm{~V}$. The voltmeter reads from 0 to 100 and the transformer doubles this scale. The ratio error has been over. looked, but a reliable transformer should be chosen in erder. to prevent erroneous readings.

A 0-1 milliameter can also be used as a voltmeter provided a sui:able multiplier is connected in series with it. Fig. 3 shows an instrument of this type arranged to measure up to 500 V . The internal resistance of the meter is $50 \Omega$. Therefore the voltage required for full scale deflection is:
$\mathrm{E}=\mathrm{IR} ;=1 / 1,000 \times 50 ; 0.05 \mathrm{~V}$.
(Continued on page 400)

# High-fidelity Main Amplifier 

## THIS UNIT PROVIDES A GOOD QUALITY IOW OUTPUT

$\mathcal{J}^{2}$HE increasing number of hi-fi enthusiasts who wish to start a hi-fi system from scratch will welcome this article about a hi-fi amplifier capable of providing up to 10 W of good quality reproduction with negligible distortion, and good frequency response.

## Circuit

The main amplifier is usually built separately and can be stored away from the control unit if desired. An obvious choice for the output section in an amplifier of good quality is a push-pull one. The output stage consists of two EL84's in push-pull, under normal or low-loading conditions as required. Distributed loading was considered but due to the lack of peak power handling this arrangement was discarded. The normal loading condition for the output valves results in a distortion figure of about $0.3 \%$ at 10 W over a power response of better than $30-15,000 \mathrm{c} / \mathrm{s}$ within one decibel. This response is more than adequate for even the most critical of listeners, and only very expensive speaker systems can reproduce below

By J. Haskell

$30 \mathrm{c} / \mathrm{s}$ at the rated output. The frequency response is $10 \mathrm{c} / \mathrm{s}$ to $20 \mathrm{kc} / \mathrm{s} \pm 1 \mathrm{~dB}$ or better.

The , valves are cathode-biased under both loading conditions. A balance control is included in the cathode circuit of $V 2$ and $\vee 3$.

## Low-loading

Under this loading, the distortion content at 10 W is approximately $0.1 \%$ over the specifled range, and is therefore more suitable for music and speech reproduction in the home than normal loading. The anode to anode load for EL 84 's, in normal and low-loading conditions is $8.000 \Omega$ and $6,000 \Omega 2$ respectively. The usual "grid stopper" resistors are included in the circuit to prevent any parasitic oscillations from taking place.

## The Phase Inverter

The phase inverter circuit is designed around a high-gain double-triode valve type ECC83, the first section of which acts as a driver and the second section as the phase inverter proper. This type of circuit gives good reproduction and is quite popular, the only disadvantage being that the overall gain is slightly more than unity ( $1 \cdot 8$ ). Since the cathode resistors of the phase inverter are not by-passed, there is heavy negative feedback, giving good transient response and also


Fig. I-The circuit diagram.
helping towards the balance of the output stage.
The output iransformer was a Partridge type P3667. which has an 8 k primary winding tapped at 6 k . The constructor may therefore try both loadings out on the output stage, bearing in mind that resistors R13 and R14 will have to be changed as well (220』 for normal loading and (390』) for low-loading conditions).

## Increased Feed back

The degree of negative feedback is about 20 dB , and increasing it to 30 dB resulted in no instability, giving a good feedback stability margin.

An interesting feature about the driver-section is the resistor R 6 and condenser C 2 in series from the anode of V1A to earth. This is to prevent parasitic oscillations (rarely present in triode valves) and to provide a time constant giving good stability in the lower registers of the frequency range.

Close tolerance resistors should be used for the anode and cathode loads of the phase inverter, as well as in the grid resistors and stoppers of the output valves. The two coupling condensers, C4, C5 should have no leakage since any D.C. on the output valve grids will result in distortion.

## The Power Supply

(Fig. 1). Valve V5, used in the prototype, was a 5 Y3, though an EZ81 may also be used. In this case, the rectifier winding will be 6.3 V at 1A. If additional current is not required for a radio tuner, 10 mA for a pre-amplifier is available. An EZ80 may be used instead of the EZ81, and


Fig. 2-The circuit of the power supply.
a common heater winding can then be used for all the valves. It should be noted that on no account should more than 90 mA be drawn from an EZ80. Two resistors must be included in the anode circult of the rectifier; the values for the EZ81 are 1900 per anode. and for the EZ80 216 ? per anode. Under normal loading conditions the amplifier requires about 80 mA of H.T. current, and 60 mA under lowloading.

Since a smoothing choke was not used, a large smoothing condenser was required to supply the extra voltage on peak drives of the output stage.

## COMPONENTS LIST

| Resistors (all $\frac{1}{2} \mathbf{W}$ unless otherwise stated) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| RI | 22k |  | 2-2k |  |
| R2 | 220k | R5 | 180@ | $\pm 5 \%$ |
| R3 | 100k | R6 | 8.2k |  |
| R7 | 220k (may be increased to IM for H.F. stability) |  |  |  |
| R8 | 47k $\pm 2 \%$ | RII | 4.7k |  |
| $R 9$ | 2.7k | R12 | 4.7k |  |
| R10 | 47k $\pm 2 \%$ |  |  |  |
| R13, | R14 $220 \Omega$ (for normal loading) or $390 \Omega$ (for low loading) |  |  |  |
| R15 | 220k | R18 | 47 $\Omega$ |  |
| R16 | 220k | R19 | 1-2k | IW |
| R17 | $47 \Omega$ |  |  |  |
| VRI | 100 w.w. potentiometer |  |  |  |

## Copacitors

Cl, C9 $50 \mu \mathrm{~F} 450 \mathrm{~V}$ elec.
C2 680 pF
$\left.\begin{array}{ll}\mathrm{C} & 0.05 \mu \mathrm{~F} 600 \mathrm{VI} \\ \text { C4 } & 0.05 \mu \mathrm{~F} \\ \text { C5 }\end{array}\right\}$ low leakage types
C5 $\quad 0.05 \mu \mathrm{~F}$ $50 \mu F$ elec.
C7 $50 \mu \mathrm{~F}$ elec.
C8 $220 \mathrm{pF} \pm 5 \%$ (for $3.75 \Omega$ speaker)
Valves:

| Valves: | ECC83 | V3 |
| :--- | :--- | :--- |
| V1 | EL84 |  |
| V2 | EL84 | $V 4$ |

Mains transformer
Primary: 200-220-240V
Secondaries: $300-0-300 \mathrm{~V}, 60$ or 80 mA (see text)
3.15-0-3.15V, 2A

Winding to suit heater of $\mathrm{V}_{5}$
Output transformer:
Partridge P3667

## Chassis:

12in. $\times 9$ in. $\times 2 \frac{1}{2}$ in. approximately.
Pilot lamp, wire, solder, bolts, sockets, etc.

The possible change in line voltage is only $0.5 \%$. Adequate decoupling of the stage is also assured.

## Feedback

The values of R5 and R20 govern the degree of voltage fed back, and the values used in the prototype were $560 \Omega$ and $180 \Omega$ respectively. giving about 20 dB of feedback. Constructors who wish to increase the feedback may do so by decreacine the value of R20 slightly. Resistors R8 and R10 should be good quality components of $\pm 2 \%$ tolerance. lack of balance here or in the output stage itself will result in unnecessarily high second harmonic distortion, owing io incomplete cancellation of the distorted anti-phase wave forms. A condenser in parallel with the feedback loop resistor promotes a phase shift opposite to tha: of the output transformer at the high frequency resonance of this component, and thus prevenis the feedback from becoming positive at this frequency. If the output transformer is different from the one specified, it niay be necessary slightly to modify the value of this component. The optimum value is best found by trial and error. Best results


Fig. 3-The complete underchassis wiring diagram.
will be obtained if this amplifier is used in conjunction with the pre-amplifier designed by the author (June issue, 1961), as this was used with the poototype. The basic sensitivity is about 600 mV and any high quality pre-amp capable of this output may be used.

## Assembly

The components are first mounted on the group boards as shown in Fig. 3. When resistors R8 and R10, R15 and R18 are being soldered, a heat shunt should be used. Only one wire goes beneath the group boards, this is from C3 to R6 and is shown dotted in Fig. 3. When the group boards are assembled, they may be bolted into place with a spacer located between the board and the chassis, to allow for the wiring underneath.
All earth connections are soldered to the busbar, which may be held insulated from the chassis by means of two tagstrips: this busbar should be earthed to chassis at the input socket only.

An output socket may be included if desired, and should be insulated from chassis if possible.

## Wiring

The heater and power supply should be wired in first. Tightly twisted wires are used for all A.C. circuits, and this wiring should be kept away from signal circuits and positioned as close to the chassis as possible.

## Feedback

For negative feedfack to take place, the amplifier output secondary winding must be correctly phased in relation to the input. If in phase with the input, violent oscillations will take place, which may damage a high-grade speaker suspension; hence, it is best to use a lowgrade speaker to secure the correct phase relation.

## Output Stage Balance

The output stage is next balanced and is a very simple procedure. The balance control VR1 should be slotted with a file for screwdriver adjustment only. Before switching on, check for an H.T. short with the meter. After switching on, if positive feedback occurs, then switch of immediately and reverse fhe anode connections on the output transformer primary. After about thirty seconds the set should have warmed up and a very slight hum only should be present (the hum level is approximately 80 dB below full output).

A D.C. voltmeter is next connected across the anodes of the EL84's and the balance control VR 1 is adjusted until no reading is obtained (ignore random fluctuations). The valves are now balanced from the D.C. aspect, which is usually the same for signal input. If a balance cannot be obtained, the valves should be switched over and the procedure carried out again: if a balance is still not obtained. then the valves should be checked for emission. Usually a balance is easily obtained.
 looked in at the door during the demonstration one would have seen dozens of couples waltzing round the hall in dead silence--yet all in perfect step. The secret was that they were all wearing a form of hearing aid earpiece inserted in the ear, and they carried a small unit which picked up sound from a loop running round the floor of the hall. Fed to this was the output from a record player, and the signal was inductively coupled to their pick-up device. It would seem that there are many very suitable uses for this type of coupling, not oniy inside buildings, but also out of doors. I will leave my readers to think of some of the most intriguing of these.

## Electronic Games

I have now received a large number of letters
CONSIDERABLE publicity has been given ONSIDERABLE publicity has been given to a suggestion made in a letter on the "killing" of interference from transistor portables. A reader suggested that the annoyance from these sets could be removed by using a radiating device -which readers will remember was first suggested on this page a long time ago, and I mentioned the fact that it was not known at the time what the reaction of the Post Office authorities would be on the use of such "jamming apparatus". We subsequently published a quotation from the Wireless Telegraphy Act which pointed out that it was an offence to use any apparatus which could cause interference with other apparatus and that therefore such jamming equipment would be considered to be illegal. The references to the interference device quoted in the opening paragraph of these notes has brought apparently shoals of letters in which such terms as "knighthood" and even "canonisation" have been suggested as suitable rewards for the student whose letter first drew attention to the idea. It is, of course. not an "invention". but merely an application of a known device, which is, in fact, being used illegally if its purpose is to iam another receiver, and most readers will know that even a simple super-regenerative set, if it does not have a buffer input stage, can cause interference over a wide area even under the most correct operating conditions. The estimate of $£ 20$ for constructing one of these "jammers" seems rather excessive.

## Remote Controls

Hard on the heels of my notes about remote controls (August issue) a reader reminds me of a demonstration given many years ago of a magnetic induction form of control which seems to have disappeared with time-although it would
on the above subject and some of these make most interesting reading. The one " like best is that describing a "Bingo machine" built by a reader in Kent, and when I have had time to study a! of these, I will try and see if the Editor can alford the space to publish details of one or more. Some very ingenious ideas seem to have been applied, and so far expense seems to have been saved by utilising standing equipment which can be obtained very cheaply. I felt sure that our readers would overcome difficulties such as "expense" by making do, and this now does seem to be the case.
One reader suggested the simple plan of having ordinary on-off switches, either toggle or simple bell type. by means of which two people could play against each other, and he pointed out that these switches may be obtained with a bias in some cases so that their operation consists merely of pushing them against the bias, which will operate a desired circuit. and then on releasing them they will return to their original setting. This does offer some scope. but in most cases this arrangement could only be used with what I might call "electrical" circuits, rather than electronie. That is to say, battery and lights with switches in circuit could be employed. and by this means the "game" would be reduced to its most simple form. but this is not the type of device 1 had in mind in my first remarks on this subject. I was visualising the arrangement where a form of "electronic brain" was employed. whereby after one player operating a button or switch recorded information in the complete equipment analysed the results of his "move" and automatically made an answer to that move and thus enabled one person to "play" the machine. And. of course. such a machine could be so constructed that it could not lose but would always win or draw.

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# POWER <br> By L. N. Nash <br> Rectifier Circuits 

## common and uncommon

## A SURVEY OF PRINCIPLES OF PRACTICAL IMPORTANCE, AND USES OF SUCH CIRCUITS

(Continued from page 308 of the August issue)
 voltage doubler circuit over the conventional voltage doubler circuit.

Fig. 21 gives an example of a combined H.T:/EHT supply on these principles. A further advantage of this circuit is shown in Fig. 22, where the same circuit but of inverse polarity is added to the same transformer winding, in the same method of circuit development as the previous treatment of the other basic circuits. The result here is an output at four times the voltage output of a simple half-wave circuit, so that this circuit is called the "Cascade Quadrupler". These types of circuit are called "Cascades" on account of their cumulative method of working. Thus the first rectifier and condenser, MR1 and C1, function as a normal simple halfwave circuit, charging up C1 to the peak. On the half cycle of opposite polarity, where MR1 is now


Fig. 21 (above)-Combined H.T./EHT circuit using the cascade voltage doubler principle.

Fig. 22 (right)-The coscode voltoge quadrupler circuit. Transformer secondory 250 V r.m.s.; rectifiers E250C50 selenium. Do not mount on the same metal chassis, as otherwise floshover inside the cosing is likely. Use separate cooling plates of aluminium insulated from each other. (The values given are approximate.)
blocked, polarities are such that the charged C1 and the reversed transformer winding voltage act in series addition as voltage drive for the second rectifier and condenser MR2, C2 also operating in simple half-wave circuit, thus clearly leading to a doubled voltage output. The operation of C3/MR2 and MR4/C4 follows similar lines.

## Progressive Cascading

In principle, the charge voltage on C2 and the transformer voltage can be made to act in series across a further rectifier on the next half cycle, and so on up to any number of cascaded stages. Thus a D.C. output voltage of any desired multiple of the output of a simple half-wave circuit is possible with rectifier cascade-multipliers, without the need for any transformers. But such circuits are of little use to the constructor, because rectifiers and condensers of the large voltage ratings required are not commercially available.

It may be mentioned, however, that the rectifiers may be replaced by spark-gaps of graded separation, trimmed so that breakdown just occurs at the half-cycles corresponding to the maximum voltage, exactly where a normal rectifier would be required to conduct in such a circuit. This is an interesting example of the use of spark gaps in substitution for rectifiers, which has actually been used in historical equipment for high-voltage supply for atomic research. Generators with spark-gap cascades have been built with an output of well over a million volts, using a transformer winding input of some thousands of volts.

This completes the survey of those rectifier circuits considered to be of practical use to the experimenter. Many other interesting types, sucb

as three-phase and polyphase equipment, gridcontrolled rectifiers, etc., are not considered to be of practical importance for the general experimenter.

## Peaking and Smoothing

All rectifier circuits work into an output load through which the D.C. output current flows. In basic principle, this output load consists of a resis-


Fig. 23-Resistive and capacitive elements in porallel representing the output load.
tive element (the actual useful load) and a capacitive element (the "smoothing ") in parallel, as shown in Fig. 23. Fig. 24 shows the more conventional smoothing, where the capacitive element is split at the "hot", end into two, and a choke or resistor inserted. This enhances the characteristic that the A.C. component of the output (hum ripple) goes preferably through the capacitive element to earth, whilst the true D.C. component goes through the resistive element (real load) to earth, which is the familiar purpose of smoothing -namely to remove as much as possible of the remaining A.C. component of the output.

Now, the capacitive element of the circuit of Fig. 23, as long as it is not charged to the final voltage, represents a short-circuit as soon as the


Fig. 24-Conventional smoothing.
transformer winding voltage has reached a part of the half cycle of the conduction-polarity where the voltage has risen above that to which the condenser is at the moment charged and charge current will then flow into the condenser to increase its voltage. It is thus perfectly obvious that this process goes on until the condenser has charged up to the peak voltage of the A.C. wave, which is about 1.5 times the r.m.s value for the mains sine wave. This property of rectifier circuits is known as (capacitive) peaking, and raises the peak inverse voltage rating required for the rectifier, as explained earlier in this article. Even if no physical condenser is present, the circuit stray capacities, even if very small, are inevitably fully sufficient to give full peaking on open-circuit output, so that no reduction in inverse voltage rating of the rectifiers is permissible even if no physical smoothing condensers are used, as in common accumulator charging circuits.

## Load Characteristics

The remarks regarding full peaking made in the previous section apply to open-circuit output, i.e.,
the case when the resistive component of the output load is of infinitely large resistance. As soon as a finite resistive component is connected, i.e. an actual pure D.C. output current is drawn, this will draw charge away from the smoothing condensers.

Thus, in actual practice, the tinal operating output voltage will be somewhat less than the full peak voltage, according to the balance struck between the load current passing out of the condensers and the rectifier current passing into them on the appropriate portions of the A.C. cycle. Zero output D.C. load results in full peaking, as explained above, and as the output D.C. load current increases the voltage will fall below the peak, the decrease being normally linear with rise of current in most circuits, which means that Ohm's Law is obeyed to the extent that a definite corresponding internal impedance may be ascribed to the circuit. This internal impedance lies in the region of about 1 k to 2 k for normal conventional fullwave H.T, rectifier circuits, so that a decrease of 1 V to 2 V may be expected in the output voltage for each rise of about 1 mA of output current drawn. The actual exact figures in a particular case will depend greatly on the smoothing capacity values, rectifiers, resistances of transformer windings. etc. A good power supply should have as small a change of voltage with load current as possible, i.e. as low an internal impedance as possible.


Fig. 25-Measuring peak surge rectifier current.

## Condenser Values

Large values of smoothing capacities reduce the internal impedance, in that they keep the output voltage high at greater load currents, but this is at the expense of large surges of current through the rectifier at the A.C. cycle peaks, which exceed the surge-current rating of the rectifier for smoothing capacities larger than a critical value for a given circuit. Thus the use of too large a smoothing capacity can cause overheating and flashover in the rectifier.

Metal rectifiers, and especially the new silicon rectifiers, can tolerate higher peak currents than normal valve rectifiers. This is a great advantage of these devices, and allows the use of much larger
smoothing capacities, which is very useful in half-wave circuits requiring the extra smoothing effect. It is extremely difficult to determine the maximum tolerable smoothing capacity on theoretical lines if one is about to try out a new rectifier circuit of one's own design, but fortunately it is a simple matter to measure the peak rectifier current in an experimental circuit if one posesses an oscilloscope and an A.C. voltmeter. Fig. 25 shows the arrangement for such a measurement, as typically applied to a conventional full-wave H.T. rectifier circuit. The normal load which the circuit is intended to feed is connected, and the small measuring resistor of about $1 \Omega$ (the resistance ( R ) of which must be known accurately) is connected as shown. It does not disturb the function of the circuit appreciably, serving merely to monitor the rectifier current.

The oscilloscope input is now connected to A, and the trace adjusted to suitable height and the timebase to display a convenient number of cycles. The waveform will not be a sine wave, but will display the regular current surges through the rectifiers. Without altering any settings of the oscilloscope controls, the oscilloscope input is now switched to B, and R2 adjusted until the mains sine wave display has exactly the same peak to peak amplitude as the peak to peak amplitude of the rectifier current display. If V is the reading of the A.C. voltmeter, then the peak rectifier current is given by

$$
\begin{gathered}
\text { I peak }=\frac{V}{R} \times \frac{3 R 2}{R 1+R 2} \text { Amps } \\
\binom{R e s i s t a n c e s ~ i n ~ O h m s ~}{V \text { in Volts r.m.s }}
\end{gathered}
$$

The data list should then be consulted to check whether the measured peak current is within the surge-current rating of the rectifier in use. If not, then the smoothing capacity must be reduced, the load current reduced, a different rectifier type used, or a surge limiting resistor or choke inserted (Fig. 26), or any suitable combination of such measures. If one were very careful in the design of circuits, the initial surge currents through the rectifiers as the condensers charge up from zero upon initially switching on would also be studied.

## Surge Limiters

If the initial surges are found to exceed the rating of the rectifiers, then the same measures as indicated above can be used, though the best measure in this case would be the use of surgelimiter resistors or chokes. There is in principle a choice of three positions for such components, as illustrated in Figs. 26 a, b, c. Fig. 26a is normally used if resistors are used, whereas Fig. 26b is common if a choke is used, whereas Fig. 26c is seldom found.

There is not a great deal to choose between the three arrangements, the particular preferences being largely a matter of convention. Fig. 26b represents the familiar choke-input smoothing circuit, which has the characteristics of a very rapid initial fall of output voltage away from the full peak at low output currents, but thereafter far slower fall of output voltage with output current in the region of the operating value of output current (assuming proper choice of component values). The result is that such a smoothing


Fig. 26-The three positions for surge limiters.
circuit gives a smaller output voltage at a given load than the conventional smoothing circuit of Fig. 24, but the effective internal impedance is lower, i.e the regulation is better.


Fig. 27-This circuit provides decoupling and smoothing in one, and avoids unnecessarily large rectifier surge currents.

## High Ratings

It should be mentioned that the use of television booster diodes as power rectifiers, in addition to advantages already discussed, has the further advantage of high surge-current rating. This is because these diodes are specially designed for pulse-operation in television line-output circuits, and therefore are fitted with excellent high-emission cathodes. Thus the PY81 is rated at a peak surge current of half an amp. so that with a 400 V r.m.s. transformer winding giving a peak voltage of 600 V forward, the surge-limiting resistance would only need to be at the very most about 10002. The
(Continued on page 438)

# A HOME-MADE <br> <br> THE USE OF A TERTIARY FEEDBACK <br> <br> THE USE OF A TERTIARY FEEDBACK WINDING ARRANGEMENT SIMPLIFIES WINDING ARRANGEMENT SIMPLIFIES THE CONSTRUCTION OF THIS TRANS THE CONSTRUCTION OF THIS TRANSFORMER AND REDUCES THE COST. 

FORMER AND REDUCES THE COST.} HI-FI OUTPUT TRANSFORMER

## P

RICES of quality output transformers are still high enough to deter the experimenter who has cconomy in mind, particularly when the cost has to be doubled for stereo. Substitutes bring distinct risks of trouble with published designs, a fact which emphasises the importance of considering transformer and amplifier circuit side by side. Despite this cautionary remark, the transformer to be described will be found to be stable in several circuits and will provide the basis for some interesting, inexpensive experiments.

## Sections

The number of winding sections is small and their arrangement simple enough for home workshop methods and yet the transformer docs not


Fig. la-Voice-coil feedback circuit; b-tertiary feedback circuit.
lend itself to factory production, possibly because it requires a centre-partitioned bobbin and a "stop-and-start" procedure unsuitable for automatic machinery. Therefore, despite its advantages of small size, simplicity, cheapness and highquality performance, it is not likely to appear in the shops.

The achievement of stability in an amplifier having overall feedback generally demands a complex sectionalised winding arrangement in the output transformer. A successful alternative for the small amplifiers which, in stereo pairs, can supply a total of about 10 W output, is to operate

## BY W. GROOME

the output stage safely within class " $A$ " conditions so that small and simple transformers can be used. Another method is to apply heavy negative feedback over the output stage to clean up distortion at its principal source, thereby reducing somewhat the risks of instability with the voice-coil loop.

## Separate Feedback

Winding
A further arrangement is the provision of a tertiary (third) winding to supply a
Fig. 2 (right)-A push-pull output tronsformer with
 tertiary windings ( $T$ ).

Fig. 3 (below)-Each anode winding is confined to one side of the partition and divided into two sections separated by the secondary. The secondary and tertiary are wound across the full width of the former.

AA Tertiary, one layer, full width:
BC Primary, inner section, one side of the partition;
DE Secondary, full width;
FG Primary, outer section, one side of the partition;
H Tertiory, one loyer, full width;
$J K$ As BC;
Tap secondary tap;
LM AsFG.

feedback voltage that suffers none of the distortions to which voice-coil connections are prone. It becomes possible to apply very heavy feedback without the sectionalising normally required. This is the basis of this transformer. To obtain the greatest versatulity, the windings are so arranged and insulated that the leads, which are all brought out instead of being internally connected, provided a choice not only of turns ratio but also of output stage conditions and feedback circuits.

Fig. I shows in the simplest forms (a) the conventional feedback circuit and (b) the tertiary arrangemeni. A very simple tertiary winding would seem to be possible by wrapping the very few necessary turns around the outside of any transformer winding. This can be tried and the transformer may be found to behave reasonably well, but the feedback will be out of balance and some distortion is certain. A virtual replica of the anode signal can be obtained when the tertiary is divided into two single-layer sections in series, one on the inside of the bobbin and the other on the outside. It is also preferable, and easily arranged, to have a balanced primary having the winding for each valve of a push-pull pair kept to its own side of a partitioned bobbin. This not only gives excellent push-pull conditions but balances the D.C. supply and the resistive component of the A.F. load.

## Tertiary Sections

The arrangement adopted has both primary windings divided into two sections, each pair on its own side of the partition with the secondary


Fig. 5-The method of obtaining variations of gain and feedbock by the potentiometer $(P)$ placed across the tertiary windings.
as a single section wound across the full width and tapped for alternative loudspeaker impedances. The tertiary sections comprise only


Fig. 4-The circuit of a two-stage push-pull amplifier.
twelve turns each, spaced across the full width. The arrangement of the sections is shown schematically in Fig. 2, with colour identification that will be used throughout this article and the one which follows. Fig. 3 will give some idea of the actual positions of the sections.

No rigid specification for core dimensions and quality will be given because of the difficulty of obtaining laminations of any particular size and
is good and there seems to be little to gain by dividing the windings into the many sections found in the usual high quality job. Nevertheless, for the very finest quality, a generous stack of good quality laminations should be provided. In a 10 W amplifier very fine bass down to $30 \mathrm{c} / \mathrm{s}$ is possible with a $1 \frac{1}{2} \mathrm{~m}$. stack: a $\frac{3}{4}$ in. stack gives excellent results in a stereo amplifier giving about 6 W per channel.


One of the author's experimental transformers.
grade in the shops. Instead, some guidance will he officred to enable the constructor to use the best he has or can obtain and to adjust the windings to suit. A feature of the transformer is that it is tolerant in this respect, and good results can be achicved with cores rather smaller than might be needed with others. High frcquency response

## Pre-amp

The amplifier should have sufficient gain to overcome the attenuation of heavy feedback. and the necessary amplification must be achieved with the minimum of A.C. coupled stages. Two stages coupled by one R.C. network is safe enough, and the tertiary transformer can be made to work quite well in a thrce-stage amplifier. The phase shift with three stages can be kept well within the stability margin if one is direct-coupled. With more than three stages an amplifier is likely to be unstable with any transformer if all are within the feedback loop. A safe and satisfactory method for small domestic amplifiers is to use a twostage main amplifier and to feed it from a pre-amplifier having its own local fecdback. The object of the nain loop is to clean up the distortion that is generated chiefly in the output stage and there is no point is using voicc-coil or tertiary feedback for earlier stages where simple local loops can be more effective and stable.

In Fig. 4, a triode "see-saw" phase-splitter and amplifier stage feeds the output pentodes. The tertiary winding, earthed one end, supplics feedback to VI via RI and provides a path for the cathode current.
(To be continued)

## INCREASING VOLTMETER RANGES

(Continued from page 388)

The multiplier must take $500-0.05=499 \cdot 95 \mathrm{~V}$. Its resistance will therefore be:-

$$
\mathrm{R}=\frac{\mathrm{E}}{1}=\frac{499 \cdot 95}{1 / 1.000}=499,950 \Omega
$$

Such a multiplier can most conveniently be made by connecting $470,000,22,000,7.000,820$, 100 and $30 \Omega$ resistors in serics. Taps can be arranged for 250.100 and 10 V or other such ranges, calculated in the same way.
The multiplicr in circuit at 500 V is $499.950 \Omega$, at 250 V is 249,9502 , at 100 V is 99,950 ?, and at 10 V is $9.950 \Omega$.

## The Voltage Divider

Valve voltmeters and oscillographs have a difforent multiplier system. Fig. 4 illustrates the arrangement. $R$ is known as a divider. The valve voltmeter is connected to a small portion of $R$ and therefore measures only a fraction of the voltage under test. $R$ is usually made up of several high resistances connected in series giving
a total value of about 20 M . It is essential to have $R$ as high as possible in order to maintain the sensitivity of the valve voltmeter.

In Fig. 4 the total value of $R$ is 20 M . Therefore on $1,000 \mathrm{~V}$ it will pass:-

$$
\mathrm{I}=\frac{1,000}{20,000,000} \quad=1 / 20,000 \mathrm{~A}=0.05 \mathrm{~mA}
$$

The valve voltmeter reads one volt at full scale deflection. Therefore the resistance between $b$ and c will be:-

$$
\mathrm{R}=\frac{1}{1 / 20.000} ; \quad=20,000 \Omega
$$

The resistance between a and $b$ will, of course, he the difficrence between $20,000,000$ and $20.000=$ $19,980,000 \Omega$. Tappings can also be arranged between the various components of $R$ to give, say 500. and 250 V ranges. In Fig. 4 the resistors are as follows: $b$ to $c=20,000 \Omega$, $b$ to 250 V tap $=$ $4,980,000 \leq 2,250$ to 500 V tap $=5,000,000 \Omega$, and 500 to 1000 V tap $=10,000,000 \Omega$.

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# SERVICLING TAPE HECORIDERS 

## PROGRAMME SOURCES AND SIGNALS

By T. S. Smith

1- AST mond we deale wh record and ply equalisation and discovered how a reasonably flat overall frequency response can be obtained by applying controlled treble lift on record and bass boost on replay. This month we shall be considering the various programme sources and signals used by the home recordist.

## Recording from the Radio

The radio is undoubtedly the most used source of programme material exploited by the amateur but, unfortunately. full advantage is not always taken of this medium and consequently the quality of reproduction may be sadly lacking.

The easiest way of getting a radio recording is to site the microphone in front of the loudspeaker and record in the usual manner. Although the results so obtained are acceptable to some, this is a very poor method of recording technically and far better results are possible by the use of other methods. With the loudspeaker/microphone method, three basic distortions are introduced to the recorder, and these are: (i) the inherent distortion in the output stage of the receiver (even the best sets produce some distortion in the output stage): (ii) the distortion and coloration produced by the loudsocaker itself and by its baffle or enclostre; and (iii) the distortion. reverberation and coloration reflection reflected from the room.

The first kind of distortion is present always and cannot be redticed or eliminated: (ii) is, again, always present and depends much on the loudspeaker and enclosure employed by the receiver; (iii) however, can be varied to some extent by playing with the spacing between the loudspeaker and microphone and by cutting out excessive reverberation by covering the channel between the loudspeaker and microphone with a heavy cloth.

The loudspeaker/microphone channel is virtually an electro-acoustic transducer. in which there are, two distortions to contend with: the "electro" distortion and the acoustical distortion, as already described.

## Eliminating the Acoustics

It is rather pointless to use the A.F. signal produced by the set to operate a loudspeaker, and for this loudspeaker to cause the diaphragm of a

## (Continued from page 315 of the August issue)

microphone to vibrate in sympathy, and then to use the signal produced by the microphone for recording (see Fig. 25). By far the best idea is to utilise the A.F. produced by the set as the recording signal (Fig. 26).

This. then. presents several problems; the best way of extracting the A.F., etc. The obvious arrangement is to disconnect the loudspeaker and apply the two loudspeaker wires to the input of the recorder. This. although obvious, is a bad thing to do for several reasons. One is that as soon as the loudspeaker is disconnected from the set, the output stage is operating without a load. This immediately introduges quite a lot of extra distortion, but not only that, it also causes the A.F. voltage to rise to dangerous peaks at the anode of the output valve and across the primary of the output transformer. Before very long either the valve would flash over or the primary of the transformer would short-circuit or break down.


Fig. 25-The simplest way of recording from the rodio is to site the microphone in front of the loudspeaker. This is technically poor, however, since there are various distortions introduced to the programme signal as this diagram shows.

If this method of feeding is to be used, then it is essential for either the loudspeaker to remain connected or a resistive load to be used instead. The resistive load should have a value equal to the impedance of the loudspeaker, which, in most ordinary valve-type receivers, is of the order of 32. With transistor receivers, the impedance may be entirely different and in some cases the loudspeaker speech coil may be centre-tapped, in which case special precautions will have to be taken to prevent damage to the output transistors.

Where possible, it is best to operate without the loudspeaker for, apart from the disturbances created by a watt or so of audio during a recording excrcise, the varying impedance with frequency of the loudspeaker can detract from the quality of the recording and, in certain cases, upset the equalisation. When a resistor is used instead, it should be able to handle the full output power of the set or amplifier hook-up. As $3 \Omega$ resistors are rather difficult to come by, a length of resistance wire (available almost anywhere) wound round the body of a ceramic high-value resistor, and terminated at the lead-out wires, is adequately suitable for this application.

## Voltage and Matching

Next things to consider are the signal voltage required at the input of the recorder to give full modulation without overload, and the impedance matching between the output of the set and the input of the recorder.


Fig. 26-If the A.F. signal is taken from the loudspeaker circuit, the loudspeaker must be left connected or a load resistor equal to the impedance of the speaker, must be connected instead.

## Voltage Considerations

Tape recorders usually have two (or more) inputs, one for microphone and the other for radio. The microphone input is usually more sensitive than the radio input. This is because the voltage at the output of a microphone is much below that available from a radio set. Typical levels for full modulation are: microphone 1 mV and radio $100 / 150 \mathrm{mV}$. Sometimes there is a second radio input suitable for low-level signals direct from the diode detector, but this will be considered later.

The question, then, is what sort of voltage is present at the loudspeaker leads of an average radio set? This depends very much on the impedance of the loudspeaker circuit and the output of the set. The voltage is easily found, however, for any set, by using the simple expression $\mathrm{F}=\sqrt{ }(\mathrm{W} \times \mathrm{R})$, where E is the r.m.s. output voltage W the watts output and $R$ the impedance of the loudspeaker or load resistor in ohms.

A typical set, for example, might be giving, say $3 W$ across $3 \Omega$. Three times three is nine, and the square-root of nine is three. Thus, it follows that, at full output, 3 V r.m.s. exist across the loudspeaker load. This is well above the input signal required on most recorders, so the signal is either turned down at the set (set's volume control) or at the recorder-but this can cause trouble. For
example, say the radio is turned up to nearly full output, using a resistive load instead of a loudspeaker, so that 3 V peak are applied to the recorder. This will mean that the record level control will have to be turned well back to avoid overmodulation as indicated on the modulation depth indicator. Indeed, under such conditions the record level control will only be a fraction on.

Now, although the modulation or record level indicator will be showing that overloading is not apparently taking place, the recording will almost certainly be very poor indeed. The main reason for this is not so much a question of matching, but one of overloading in the first stage. The recording level control is usually connected after the first valve, so the first valve is receiving a full 3 V of A.F.! It cannot handle that, of course, and distortion will occur, the distortion being controlled, in terms of recording level, by the level control after the amplifier.

## The Best Settings

The best way of setting up such a combination is, first to turn on the recording level control almost to maximum. then turn up the radio volume control for maximum record level as indicated. In


Fig. 27-This circuit shows a "loudspeaker on/off" switch, a dummy load R3 and an attenuator RI and R2. The attenuator ensures that the first stage of the recorder is not inadvertently overloaded and also gives a theoretically better match between the set and the recorder.
that way the first stage of the recorder will always work well below the distortion level. but difficulty may be had in obtaining a sufficiently low setting of the receiver's volume control-a slight touch being sufficient to push the recording level indicator well over the limit. Also, if the receiver's loudspeaker is to be used as programme moritor, the low volume control setting will not give sufficient output, bearing in mind that only 0.001 V or so is required to drive fully the recorder and that this corresponds to very little audio power across $3 \Omega$.

## Attenuation

Thus, an attenuator is a good thing to have between the set output and the tape recorder input. This will enable the set to be operated at near normal volume without overloading the first stage
(Continued on page 418)

# Servicing the P.W. PDCKET SUPERIIET <br>  



SERVICING DATA FOR THIS POPULAR PRACTICAL WIRELESS DESIGN

By F. G. Rayer

by a quarter revolution, or less. Speech and music should be of pleasant quality, from low volume right up to ample volume for ordinary listening in an average room.

## Battery Space

The unused tags of Cl and C 2 should be bent in against the condenser. A round body battery such as the Vidormax T.6004, will fit more easily than a square battery. The 1FT2 can safely be positioned a little more to the right, and targer battery clips can then be accommodated. Neither clip must touch the IFT can. To avoid this. a piece of thin card, about 23 in . x lin. may be bent to isolate the battery from the IFT and Cl and C 2.
If a trifle more space is needed the tuning condenser can be moved slightly higher by elongating the holes in the paxolin. This can be carried out with a small round file. The T. 6004 battery should fit without need for this, unless the holes for the securing screws have been drilled a little inaccurately.

## Waveband Coverage

This is about $200-525 \mathrm{~m}$ on M.W. and $1100-1750 \mathrm{~m}$ on L.W. A high minimurn capacity in the trimmer C 3 will prevent 200 m from being reached. If so, the spacing between the trimmer plates needs increasing. This can be done by unscrewing the trimmer and bending up the plates with a knife, taking care not to break the insulation.

Stray minimum capacity should be as low as possible, so leads to C7 and C8, and the switch, should be clear of the condenser frame, or earthed wiring.
Trimming can be on 208 m (Radio Luxembourg) with the audio gain control at maximum, the set being oriented to keep volume low. Failure to tune to a sufficiently low wavelength indicates that the trimmer is screwed down too much, or that stray capacity is too high.
It signals at about 525 m cannot be reached, with the tuning condenser closed. this probably indicates that the oscillator coil core is not screwed into the coil far enough. Even half a turn on this
core will considerably influence band coverage. If C8 is abnormally low in value, this will have the same result.

On the L.W. band, 1500 m (Light Programme) should be found near the middle of the L.W. range. If not, C7 may be too low in value, or the oscillator coil core may not be screwed in far enough. If C7 is too low 10 capacity, wiring a 60 pF trimmer in parallel with it will correct this. Adjust C4 near 1200 m and the position of the L.W. winding on the rod near 1700 m . Poor L.W. reception may be caused by wrong wiring to the L.W. winding tags, switch, or•C7.

Complete failure of the oscillator stage to work, with a set iust constructed, may arise from wrong oscillator coil positioning. There is electrical continuity between pins 1 and 2, between pins 3 and 4, and between pins 5 and 6 . If this is not so, remove the coil, turn it as necessary, and replace it.

## Noisy Reception

Receiver background noise should be very low. If high, a transistor may be responsible. Reputable transistors of named make will have passed a low noise test, but chcap or surplus transistors may be noisy.

Noise from defective soldered joints may be found by examination, by moving suspected leads carefully with an insulated tool, or by checking each stage individually. It takes only a moment to "tin" the leads of resistors, etc., by applying the iron and cored solder. If this is always carried out, no joint should be defective.

## 1.F. Oscillation

Instability in the intermediate frequency amplifier may be heard as a whistle or similar noise. It may arise from wrong values for R7 and R11, or C10 and C13, which should be of $2 \%$ tolerance. Very long leads to Tr 2 and Tr 3 may contribute, and base and emitter wires should not bc close together.

If the frouble ceases on tuning in a strong station, it is very slight. If it ceases only on detuning one or more I.F. transformer, check that wiring is short and direct. Increasing the values of C11, C12 and C14 may help. This is most easily done by adding other condensers in parallel. to a total of $0 \cdot 1 \mu \mathrm{~F}$ or $0.25 \mu \mathrm{~F}$.

## Current Drain

A meter included in one battery lead should read approximately 8 mA , with no programme


Fig. I-The original circuit of the pocket superhet.

If R14 is of abnormally low value, or R15 unusually high in value, noise may increase. Noise from this cause will remain if one end of C17 is temporarily disconnected.

A high background noise which ceases abruptly if one or more of the IFT's is detuned, is caused by I.F. instability, described later. This will usually be accompanied by whistles.

Noise generated outside the set, due to ignition systems, light switches etc., cannot be prevented, but the receiver may be placed as far as possible from the source, or from mains wiring.
tuned in, or with volume very low. Current consumption depends directly on volume, rising to about 15 mA on peaks with average good volume. Maximum volume from a local station can give peaks of 25 mA or higher.

Consumption up to and including $\operatorname{Tr} 4$ should be about 6 mA . If the no-signal drain of the output stage, $\operatorname{Tr} 5$ and $\operatorname{Tr} 6$, is much over $2 \mathrm{~mA}, \mathrm{R} 19$ should be slightly reduced in value to correct this. R18, R19 and R20 should be of 5\% tolerance, and these values are correct only for OC72's.

If consumption of the output pair is very low,
 should be increased slightly in value. Alternative transistors will probably require some change to the value of R18 or R19, to obtain a suitable base voltage. With the OC72's, R20 may be $4 \cdot 7 \Omega$.
The driver and output transformers are for OC71 and OC72's and near equivalents. Resistor values shown permit economical working with full output.

## Low Temperatures

Very low temperatures, such as may arise in winter in a vehicle or unheated room, may shift transistor characteristics, so that output is reduced and distorted. This is common to many such circuits, and is most likely when R18 and R19 chance to be of such a value as to make the output pair base voltage rather positive. The need for a new battery may be suspected. The trouble should cease when the set is run for some time in a heated room. or is otherwise allowed to reach a more normal temperature.
If this effect is unduly troublesome, R19 should be increased slightly in value to suit the actual output pair fitted. R19 should not be unnecessarily high in value as this will increase current consumption.

## Distortion

This is most probably caused by wrong values for R18 or R19, as explained, or for R14, R15 and R17. The first three stages can be most simply checked by wiring phones across R15. Adequate volume with good quality should be obtained.

Transferring the phones to the driver transformer primary should give a very great increase in volume with good quality maintained. If not.
suspect R14, R15 and R17, or Tr4. If quality is good here, but not from the speaker, suspect R18 or R19.

## Resistor Coding

Errors in reading values are most likely with low values, such as $4 \cdot 7 \Omega, 47 \Omega$, and $470 \Omega$. If values are in doubt, they should be checked with a meter.

The $5 \%$ tolerance resistors should have a gold band, and all other resistors should have a silver band to indicate $10 \%$ tolerance. Unmarked resistors ( $20 \%$ ) should not be used.

## Transistors

Leads will be of about the right length if the transistor tops are level with the tops of the I.F. transformers. Alternative transistors will be found to work satisfactorily, if of equivalent or near equivalent type.
If different transistors are incorporated, some changes in component values may be required. With Tr1 (OC44 specified) R2 might require changing, or a low value resistor may need adding between collector and pin 6 . With different transistors for Tr2 and Tr3 (OC45's specified) it could occasionally be necessary to modify neutralising values, or base supply resistors.

## Warning

This article has been published for the benefit of those readers who built the original P.W. design and the servicing information given here may not apply to later versions of the receiver although it may be found of assistance.
 and amplifier circuits.

## Introduction

Many keen experimenters must confine their activities to some odd corner of a room used for other purposes too, or possess only a workshop of very limited size. Experimental work, on the other hand, is considerably hampered if essential apparatus has to be stored away in inaccessible places, requiring considerable preliminary settingup work prior to any working session. This trouble is particularly aggravated if such apparatus is bulky or consists of many separate units. It is thus highly desirable to have the essential measuring and test equipment in as compact and multipurpose a form as possible, so that it may be left permanently set up ready for immediate use, even under conditions of very limited space.

The "Experimenter's Power Pack" (already published in this magazine in the January 1962 to July 1962 issues inclusive) is aimed to meet experimental power-supply needs under the conditions just mentioned. This article describes a very compact test-set, measuring only $11 \frac{1}{2} \mathrm{in}$. x 8 in . $x \quad 7 \frac{1}{2} \mathrm{in}$. deep, which embodies the full functions of (a) oscilloscope (b) signal tracer (c) audio testoscillator (d) frequency-meter (e) valve-voltmeter (for A.C. and D.C.) (f) quantitative waveform analyser, and (g) resistance-Inductance measuring bridge. It uses only seven valves and a miniature cathode-ray tube, and has a built-in moving-coil meter and all power-supplies also built-in.

By M. L. Michaelis
Very considerable experimenting time has been devoted during design to obtaining a really stable and reliable circuit which should function well without any difficulties if the points discussed in the course of this series of articles are carefully observed.

## Equipment for the Experimental Workshop

The following question has often been raised: "What basic equipment does the keen experimenter require if he really wants to be able to observe systematically what exactly is going on in his experimental circuits, rather than rely on more hit-and-miss methods?", The "Experimenter's Power Pack" and the "Miniscope" of the present article are the answer which this magazine offers, in a practical way, to this vital question. In addition to these two items (apart from the obvious need for an adequate set of the usual hand-tools such as soldering-iron. screwdrivers, files, pliers, etc.) the following may also be recommended:
(a) A good multimeter which may be homemade, according to information already published in these pages. or any good commercial model from the wide selection of advertiser's offers.
(b) A small handy grid-dip meter covering those ranges of radio frequencies with which the experimenter intends to work. For generalpurpose use, an instrument with a set of plug-in coils covering the range $100 \mathrm{kc} / \mathrm{s}$ to $100 \mathrm{Mc} / \mathrm{s}$ would be ideal. It is of advantage to see that this instrument is usable as R.F. and I.F. signal generator and absorption-wavemeter too (as most grid-dip meters will already be, or will be after simple modification). Capacities below 1.000 pF and inductances in the milli-henry and micro-henry
ranges can then be measured with this instrument, as well as tuning-ranges of tuned circuits, etc., thus augmenting the functions of the Miniscope.

A useful third item here would be a small wobbulator for use in conjunction with the "Miniscope" for aligning tuned circuits, bandpass filters, etc. Provision is made on the Miniscope for connection of such a wobbulator, in conventional fashion.
A constructor possessing this list of equipment, and having acquired the necessary skill and knowledge in its practical use and possibilities, should be in a position to carry out almost any quantitative or qualitative observation on processes in normal experimental work, giving him a very clear picture of what is going on in his circuits at every stage.

Regarding the Miniscope in particular in this scheme of equipment, the parts-list may appear formidable, with 73 resistors and 43 condensers

## THE

The second position of the function switch, entitled "scope". brings the small cathode-ray tube and the sawtooth-sweep timebase circuit into operation in addition. The signal can now be observed in form of its waveform on the CRT in addition to the continued audibility via the earphones. speaker or external amplifier. Of the three pilot lamps the green one labelled "tracer" is still lit and the red one labelled "scope" is switched on too in this setting. A zener-diode calibrator is included in the signal circuits, enabling the vertical-deflection sensitivity to be set accurately to any desired value between $1 \mathrm{~V} / \mathrm{cm}$ and $125 / \mathrm{cm}$. This enables the A.C. component voltage of any waveform to be read off (A.C. Valve-Voltmeter function), whilst the D.C. component which the waveform may possess in addition is simultaneously indicated, in polarity and magnitude, on the moving-coil meter situated on the panel below the CRT, this representing the D.C. 'valve-voltmeter function.

and a quantity of other material. But, remembering that this instrument combines the functions of about seven instruments which would otherwise have to be built and bought separately, and which are all essential, the price of these components is in fact astoundingly cheap for the benefits reaped.

## General Circuit Plan

The Miniscope consists basically of four circuitportions. The first is the combined H.T./EHT power-supply. The second is the Wide-Band Signal Amplifier ( Y -amplifier), including valvevoltmeter functions in the input stage and a signaltracer output stage. The third is the special timebase circuit, calibrated quantitatively for time and frequency measurements in the range from a few microseconds to about 25 milliseconds. The time-base-wave is available externally at a coaxial socket for feeding a wobbulator, or for general use as audio test signal. The fourth circuit portion comprises the additional elements and switching for a novel phase-bridge for $L$ and $C$ measurements.
A function-switch selects three operating positions. The first is entitled "tracer". In this position only, the Signal Amplifier (and associated valve-voltmeter) is operating. The amplifier signal may be heard on headphones connected to the output provided or on a miniature loudspeaker which is connected there, or else passed into an external separate power amplifier. Of the three pilot lamps only the green one labelled "tracer" is lit.

If the applied signal is pure A.C., then the waveform appears on the CRT, but the meter needle does not move. If the applied signal is pure D.C., then the meter shows it, but the CRT shows only the undisturbed timebase trace. The advantage of this arrangement over the otherwise more conventional signal-amplifier passing the fult D.C. component (D.C. amplifier) and giving D.C indication by a corresponding bodily shift of the trace on the CRT screen is that the relative D.C and A.C. sensitivities may be chosen independenth. to suit the relative D.C. and A.C. contents of the waveform being observed. Thus, for example accurate observation of hum-ripple percentage or a power supply is immediately possible which requires two separate measurements with a conventional D.C. oscilloscope.

Furthermore, the arrangement here adopted allows the essential D.C. measurements yet does not require a full D.C. amplifier, which would normally be tricky to construct under amateur conditions. A straightforward, stable and reliable A.C. amplifier is thus used.

The main signal amplifier has a bandwidth, level to within the usual specifications of $\pm 3 \mathrm{~dB}$, extending from $25 \mathrm{c} / \mathrm{s}$ to $120 \mathrm{kc} / \mathrm{s}$, and will thus give accurate displays of pulsed waveforms even at the highest audio frequencies. A low-pass filter is built in between the CRT-feed stage and the tracer output stage to prevent frequencies higher than $15 \mathrm{kc} / \mathrm{s}$ reaching the earphones $/$ speaker output (as these could otherwise be rectified at the inpur
to a subsequent amplifier, causing grid-current blocking or distortion or creating various forms of instability). Thus, even if applied signals are of a frequency well above the highest audible, they are still displayed on the CRT, yet give no tracer output. The amplifier still shows appreciable (though much reduced) gain at $1 \mathrm{Mc} / \mathrm{s}$ and will just resolve individual cycles of the carrier of medium-wave stations operating around this frequency on the CRT display. These will be seen by connecting a tuned circuit and good aerial to the input or the output of an R.F. signalgenerator if local-station signal strength is not sufficient.

The third position of the function switch brings the L-C bridge into operation. The green pilot lamp "tracer" is now extinguished. the red "scope" lamp is still lit, and the third lamp. a green one labelled "bridge", is now also lit. The signal amplifier is operating, as is the CRT, but the sawtooth-sweep timebase is inoperative, the X -deflection now being by the mains $50 \mathrm{c} / \mathrm{s}$ sine wave. A fixed $R-C$ combination shifts this sine wave so that it is running $45^{\circ}$ out of phase with the local mains. If now a sample of the in-phase mains wave is applied to the Y -amplifier (from the 6.3 V heater line) the oblique-ellipse trace charac-
teristic of two waves of equal frequency but constant phase-shift relative to each other is obtained on the screen.
But the in-phase wave is taken from the heater line, via an unknown condenser to be measured, on to a calibrated potentiometer, taking the Yamplifier input from the potentiometer. This gives a phase-shift of an amount dependent upon the relative sizes of condenser and resistance, and a certain definite combination gives $45^{\circ}$, so that $X$ and $Y$ signals are then in phase again, both being $45^{\circ}$ off the mains. This condition gives a clean diagonal line on the CRT. As the potentiometer is adjusted. therefore, the ellipse will close up to a narrow diagonal line at balance, and open up again beyond, and the potentiometer may be calibrated in capacity values correspondingly. This arrangement gives very clean, unambiguous balance readings. Ranges giving continuous coverage from 1.000 pF to $30 \mu \mathrm{~F}$ are incorporated in the Miniscope. Smaller capacities are better measured with a grid-dip meter and larger ones by a method described later in this article.

Inductances give a phase-shift in the opposite direction to condensers with the arrangement here described and thus augnent the phase difference between $X$ and $Y$ signals. $A$ good reference


Fig. I-The Y-amplifier circuit. The input is direct-coupled, and will tolerate a maximum D.C. component of 25 V (of either polarity), or an A.C. signal of maximum amplitude 50 V peak-to-peak. With the probe to be described at the end of this article, fifteen times these inputs are tolerable, and the calibrations on the D.C. level meter and on the calibrator are made to apply to conditions when using the probe. It is undesirable to use the Miniscope without the probe, unless the extra sensitivity is indispensible. Less waveform distortion of H.F. components of a signal is also obtained when using the probe.

condition is then when the phase difference has been complemented to $90^{\circ}$, giving a vertical or horizontal ellipse instead of an oblique one, which can be adjusted to a true circle by suitable adjustment of the Y-amplifier gain. The potentiometer is thus calibrated for coils for the condition for having a trace in the form of a true circle on the CRT screen. A range of 1 H to 20 H is incorporated for chokes, transiormers, etc. Smaller values arising in R.F. coils, etc., are better measured with a grid-dip meter.

A number of other useful measuring operations are possible in the "bridge" setting of the Miniscope, which will be discussed below in conjunction with the circuit details.

## The Signal Amplifier (Y-amplifier)

Fig. 1 shows the theoretical circuit of this portion of the Miniscope circuitry. It employs three valves, using high-slope triodes throughout. The input stage, VI (pins 6, 7 and 8), is a Class-A cathode-follower with unity voltage gain but impedance step-down. The purpose of this arrangement as input stage is to meet several requirements. Firstly, it accepts very high input amplitudes without overloading, so that the input can be run "fully open"-i.e., without a gain control. The input is at high impedance (as it must be, otherwise the signal source would be loaded and its waveform possibly changed in nature) and any volume control connected there would shunt high frequencies considerably on account of its inevitable self-capacity. The wide bandwidth achieved here would then not have been possible. The cathode-follower input stage,


A view of the sub-chassis with the $Y$-amplifier wiring.
however, transforms the impedance at its output down to a mere onc or two hundred ohms and considerable shunt capacity is tolerable there without high-frequency loss-thus the gain-control appears in this position.
(To be continued)


Fig. 2-The timebase circuit. This embodies an extremely linear sweep generator, with speed continuously variable from $12 \mu \mathrm{sec} / \mathrm{cm}$ to $25 \mathrm{~m} \mathrm{sec} / \mathrm{cm}$ on the CRT screen and also o powerful sync circuit, operating on the $\gamma$-signal on either polarity at will, or on the mains frequency. The sync amplifier acts as Buffer, preventing timajose signals entering the $Y$-circuits, as well as amplifying the sync signals, so that lock is rigid even at tiny $Y$-amplitudes on the CRT screen. Finally, the timebase screen-grid waveform is shaped in a special circuit, giving effective flyback-blanking, avoiding confusion in displays.

# A COMPACT CONVERTER for short waves 

(Continued from page 319 of the August issue)

$\mathcal{J}$HE constructor following the instructions given in last month's issue will have fixed the chassis to the front panel and mounted some of the larger components.

When this stage is reached, wiring can be begun using Figs. 4 and 5 for reference. (Avoid overheating the coil spills when soldering.) The small dimensions of the chassis permit short and mostly self-supporting wiring, which is a desirable feature in short-wave equipment. Note the location of the stand-off insulater used as an anchoring and take-off point for the coaxial outlet lead.

All fixed capacitors should be of very high quality and of modern miniature design, since leaky specimens are likely to cause poor operation. Ceramic valve bases were used in the prototype, but are periaps not entirely essential.

## THIS INSTRUMENT WILL PROVIDE SHORT WAVE LISTENING ON A MEDIUM WAVE RECEIVER

## Testing the Converter

If all wiring is correct $S 1 / S 2 / S 3$ may be adjusted to position " 2 ", valves inscrted and batterics connected at the appropriate points. polarity being carcfully observed. Coaxial cable should then be connected to the aerial and earth sockets of the receiver with which the unit is to be used, after first transferring the aerial lead to the converter.

The receiver should then be switched on and tuned to a silent point on its dial around $1.5 \mathrm{Mc} / \mathrm{s}$ ( 200 m ), the volume control being turned well up. The converter sensitivity control, VR1, should next be set to the H.T. end of its travel and VC3 set at approximately half capacity-with its moving vanes half enmeshed in the stationary ones. The converter can now be switched on and aligned.

If no signal generator is to hand the dial of the converter should be rotated until some hiss or a


Fig. 4 (above)-Chassis loyout of components.
signal is heard when the core of L3 should be manipulated in an attempt to strengthen the signal. The next step lies in trimming and padding the signal and oscillator circuits at the high and low frequency ends of the scale, taking care to allow only the minimum of capacity to be introduced via the trimmers. The oscillator should operate on the high side of the signal frequency, and normally the coil cores will be screwed in reasonably well.

No adjusiments should be made to VC3 until alignment is complete, which might take a little time in the absence of at signal generator. The sensituvity control might need to be turned

(Above)-The front of the unit.
 Fig. 5-The underchassis wiring diagram.
down as certain transmissions are received.

## Faults

The above supposes "first tiple working", which in practice might not result. When the converter is first switched on, silence might well result, and if this occurs, and voltage supplies, etc. are in order. as indicated by a suitable testmeter, the oscillator section of V2 should come under suspicion. All-dry frequency changers quite often are more (Continued on page 417)


An above-chassis view.


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(Right)-The underchassis wiring of the converter.
(Continued from page 414)
temperamental than their mainspowered contemporiaries, but oscillator functioning can be checked by disconnecting R4 from the H.T. line and inserting at this point a meter switched to read $0-10 \mathrm{~mA}$. The current flow should then be noted, and the value should alter when spills 8 and 9 of L2 are momentarily short circuited. Should no change be detected the oscillator is not operating and no


Fig. 6-A circuit modification to increase output.

frequency changing can occur. The remedy lies in checking that part of the circuit very carefully and reducing R 4 to 10 k or increasing the value of C3 to, say, 100 pF .

When the oscillator is working, the above test should be made at several points on the tuning scale, for it is quite possible for it to cease functioning at a particular frequency. Should no signals be heard when oscillator operation is satisfactory, try removing $V_{1}$ and temporarily connecting a lead from pin 6 on its base to pin 6 on V2 base. If signals now result, V1 or the associated circuitry is at fault and should be investigated.

## Modifications

Where the output is considered insufficient. or where the broadcast receiver used with it is of low sensitivity, improved converter efficiency would result from fitting a further valve of the type specified for V1 and using it as an intermediate amplifier. The principle is shown in Fig. 7 where V3 is the added valve. Coil L3 is removed from the frequency changer anode and a miniature $1.6 \mathrm{Mc} / \mathrm{s}$ I.F. transformer fitted instead. The amplified output is taken from L3, which is transferred to V3 anode. Extra care must be taken in a circuit of this kind to ensure adequate rejection of signals in the $1.5 \mathrm{Mc} / \mathrm{s}$ band and a wavetrip tuned to the frequency might become necessary at the aerial input.

## MEDIUM WAVE POCKET SUPERHET

## (Continued from page 387)

weak signals. to keep volume down. Final adjustment should be at frequencies a little from the extreme ends of the bands, once it has been found that band coverage is satisfactory. It may be difficult to keep volume down to a level where the effect of adjustments can be easily heard, when aligning with broadcast stations. If so, rotate the whole receiver, to make use of the directional properties of the rod, to reduce volume. During alignment, volume should not be reduced with the receiver volume control, or an exact setting of trimmers and cores will be difficult to find.

Reproduction should be at adequate volume, and of pleasing quality. Should results sound extremely distorted, it is probable that one secondary of the driver transformer has been wrongly wired, in error. If so, reverse leads to one secondary.

The tuning knob should rotate with a little clcarance. If not, a washer may be needed under
it. The set can be used flat, or standing, with the rod horizontal. Only in rare instances need the receiver be rotated for best signal pick up, as volume should easily be sufficient.
The new version of the P.W. Pocket Superhet case can be used for this receiver; the use of this case will facilitate construction since it is larger than the original.


# Short-wave Listeners' Log 

7OR the best possible listening results, a general idea of the way in which short-wave signals are propagated will prove to be very helpful. Two types of signals are of interest-those furnished by the ground wave, and those from the sky wave.

On the S.W. bands, the ground wave is soon absorbed and lost, so long distance reception is not possible with its aid. Frequencies in the 20 and 15 m bands, or around 14 and $21 \mathrm{Mc} / \mathrm{s}$, are most used for long distance reception, and ground waves from stations in these bands may already have become too weak at 20 or 30 miles range. For this reason, local stations may not be heard, even when remote overseas countries are coming in well.

The sky wave travels upwards at an angle, ind reaches the ionised layers which surround the earth. When conditions are favourable the wave is bent or reflected by these layers, and returns to earth, often at a considerable distance. The distance from the transmitter to the point where the wave again reaches the earth is the "skip distance". There may be short or long skips, according to time of day, frequency, and other factors. The wave may be reflected from the earth, and again be deflected downwards by the ionised layers. reaching earth again at even greater distances from the transmitter. If conditions or frequencies are unsuitable, the wave may pass through the ionised layers, and be lost in space.

## Long Distance Reception

Long distance reception is by waves that have been reflected from the ionised layers, possibly travelling a thousand miles or more at each hop, when skip is long. So best long distance reception will be around those times and frequencies giving long skip conditions.

The 20 m or $14 \mathrm{Mc} / \mathrm{s}$ band is extremely popular for long distance reception, and can give world "wide coverage. The ionised layers are not stable, but are influenced by sunspots, magnetic storms, and solar radiation, so results change hour by hour. Usually, most remote stations (Australia, New Zealand) will be audible early in the morning. Somewhat later in the morning, there may be a period when only relatively near stations (European) can be heard. Range may increase after noon, with Near East, Far East, South African, and other distant stations coming in during early afternoon. These are likely to fade out later in the afternoon, when Far East stations are liable to disappear, and many American stations will begin to come up in strength. With evening, very considerable-distances can still be covered.

A somewhat similar pattern is repeated daily, except that conditions vary day by day, and month by month. due to seasonal and other changes. With the 15 m or $21 \mathrm{Mc} / \mathrm{s}$ band. rather similar results can be expected. hut with even more irregular fluctuation. So this band may be excellent one day, and almost dead the next.

Unless conditions are very bad, listening on these bands will almost certainly furnish some Dx (long distance) stations, and 15 m and 20 m are often termed the "Dx bands". When conditions are good, signal strength from remote countries may be good enough for satisfactory reception with simple 2 -valve and similar receivers.

## SERVICING TAPE RECORDERS

## (Continued from page 404)

of the recorder, whilst leaving a reasonable margin on the recording level control for low level signals.

Fig. 27 shows a very convenient arrangement. where the attenuator comprises R1 and R2. The single-pole, two-position switch allows the set's loudspeaker to be used as programme monitor when required, while in the "loudspeaker off" position, the output stage is automatically loaded by R3. This resistor. of course, should have a value equal to the impedance of the loudspeaker.

Values for R1 a..I R2 are well worth considering. From the impedance aspect. there is not too much to worry about by connecting $3 \Omega$ across a megohm or so of the radio input socket. On the face of it, there would appear to be a bad case of mismatching, but in practice this has remarkably little adverse effect. Overloading is the chief trouble. However. when an attenuator is employed, the impedance can be stepped up to the tape recorder input so that the match is more theoretically exact.

R1 and R2 simply form a potential-divider. That is. all the signal is applied across the two resistors in series and only a fraction of it is tapped off from across R2. Ignoring the loading effect of the recorder input circuits. then in proportion the voltage across R2 is equal to R2 divided by the sum of R1 and R2. For example, take R1 and 100 k and R 2 as 50 k . then R 2 would be 50 divided by 150 . which is one-third. meaning that one third of the full voltage from the set's. output stage would be fed to the recorder.

In practice, the applied signal would be a little below one-third, since R2 would be shunted by the input impedance of the recorder which. in effect, would reduce the value of R 2 in relation to R 1 . but this should not make a lot of difference in the majority of cases. Thus, the attenuator can be made any required value simply by working out suitable combinations of resistors, as explained above. The value of 100 k and 50 k may well be used in practice. and this would mean that the input of the recorder would see a resistance almost equal to 50 k and 100 k in parallel, which is approximately 33 k .

The signal should be conveyed via screened cable, the R2 side of which should beconnected to the braid and earthed. But beware át this point, since the set may have a "live" chassis: that is, connccted to one side of the mains supply to follow the now popular A.C./D.C. technique. This aspect of recording, however, will be discussed in next month's article.
(To be continued)


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[^2] A COMMON FAULT

By E. Dexter



(Continued from page 345 of the August issue)

$\mathcal{T}$HE reader was introduced to three examples of correct and incorrect circuitry associated with volume controls in last month's article (Figs. 3, 4 and 5, pages 342 and 345).

Fig. 4 shows a volume control used in the same arrangement as Fig. 1, which is basically pernissible, but the value is now made very high. If the grid leak of a valve is higher than half to one megohm, quite considerable D.C. voltages may be developed across it due to the electron-current reaching the grid of the valve by virtue of the electrons' energy of ejection from the cathode, even though the actual grid voltage may still be quite negative, and thus, theoretically, electron grid-current not to be expected. Thus no volume control track used directly in the grid leak position of a valve should have a total resistance exceeding about 500 k . If a greater resistance is, for any reason, desired, then another blocking condenser or separate grid leak, as in Fig. 4b, should be used. Otherwise the volume control is likely to become noisy very quickly.

Fig. 5 gives a typical example from transistor circuitry. It is common practice in modern high-gain transistorised amplifiers to insert the volume control not right at the input to the first stage but between the first and second stages, so that signal-to-noise ratio is improved with reduction of volume (this feature is good practice in all high-gain amplifiers, valve or
transistor, yet carries the danger of running the input unprotected from overload at the first stage).

Now a transistor, in contrast to the grid-circuit of a valve, always draws current at its input, with a D.C. component also in addition to the A.C. signal component. Thus the transistorised version of Fig. 1 is fundamentally incorrect in a transistor amplifier. The subsequent transistor will always draw D.C. through a volume control track if all or part of this were used as the direct-coupled input resistance to the stage. Thus, if a volume control is used between two transistor stages, a


Fig. 6 (left)-A circuit often used for the input stage of oudio amplifiers; this is satisfactory provided no D.C. is present with the input signal.

Fig. 7 (right)-Another input circuit for an amplifierany D.C. present in the input is prevented from reaching the valve.
blocking condenser must be used on both sides of it. For a volume control between two valve stages we saw that a blocking condenser on the input side generally suffices, provided that the resistance of the volume control is not too high. Fig. 5b shows the correct arrangement for a volume control between-two transistor stages.

## Input; Terminals for Amplifiers

The arrangement of Fig. 6 is often used for the input to the first stage of an amplifier. This is quite satisfactory as long as pure A.C. signals are applied as inputs. As soon as the signals contain a D.C. component, noisiness is likely. The arrangement of Fig. 7 would prevent the D.C. component shifting the operating point of the input stage, and thus prevent distortion under such circumstances. But, as the discussion in this article should have made clear, it will not remove noisiness in the presence of a D.C. component in the input signal. The arrangement of Fig. 8 will, however, remove this trouble, too. Thus Fig. 8 is considered to be the ideal arrangement for the input to an amplifier if the volume control is to be situated there. This circuit pattern applies equally to valves and transistors.

## Time Constants

Consider Fig. 9. Here we have a transistorised amplifier input circuit, following the scheme of Fig. 8 and with typical component values given. Suppose now we feed this amplifier from a signal source containing a D.C. component and having an internal resistance of 2 M -for the purposes of illustrating the following argument with an intentionally severe example. The input electrolytic C 3 , of $50 \mu \mathrm{~F}$, will now need to charg: up to its final resting potentia! difference through a total resistance of 2 M . This represents a time constant of 100 seconds. Charging will not be complete


Fig. 8-The ideal input circuit for an amplifier if the volume control is to be situoted at the input.
until three to five times this time. Thus it will take about five minutes. All this time D.C. will be flowing in the volume control track. The symptoms are thus that, upon switching on, the volume control will be extremely noisy, becoming gradually less and less so, until after some five minutes it will be quiet. This procedure will repeat itself every time the apparatus is switched on after a rest!


Fig. 9-Transistorised version of Fig. 8-in such o circuit, the large time constonts need to be taken into account (see text).
This point is trivial for valve circuits where capacities of coupling condensers are so small that time-constants are normally smaller than the filament-warming-up times of the valves. But for transistors, where large capacities are common, the point must be watched.

However, an arrangement such as Fig. 9 is undesirable anyway on account of its large signalattenuation (unless this is deliberately wanted). Furthermore, C3 is an electrolytic operating in a low-current, high-impedance circuit-or with a high-impedance-to-capacity ratio. Under such circumstances electrolytics have been known to function as electrolytic rectifiers, giving severe signal distortion. Thus, if a high-impedance source is to feed a low-impedance transistor input circuit. it is desirable to interpose a cathodefollower, an emitter-follower, or a transformer.

## Intermittent Faults in Coupling Condensers

The author has had receivers in for repair where intermittent, or permanent, crackling (of low rumbling pitch) appeared alone or in conjunction with volume control crackling of the usual relatively high pitch. This type of fault is indicative of intermittent or randomly-variable leakage in a coupling condenser. The variability of this fault-i.e., its A.C. component. is shunted by the capacity of the coupling-condenser, removing higher harmonics; hence the low pitch.
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 2 transistor stages, 2 coils $20-60$ and 55-190 metres. Step-by-step pictorial plans, nuts, bolts, wire 88/6. P. \& P. 2'6. Plans only, $2 / 6$. THE CLIPPER. As above but one transistor stage, 79/6. P. \& P2/6. Optional Front Panel, Silver Hammer finish, all holes, $6 / 9$.

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Previously produced exclusively for Export, the de-luxe version of this famous ALL BAND receiver is now also available for the home market. Superb new styling, satin silver front panel, frequency calibrated scales, grey and silver trim knobs, perspex disc cursors. High gain circuit with ECC8 duotriode, EL84 output. EZ80 full wave rectifier. Power output $3 \frac{1}{3}$ watts for $2 / 3$ ohm speaker. 3 Planetary vernier slow motion drives, separate electrical bandspread. Covers $10-2000$ meters ( 5 Coils). World wide reception. For A.C. supply 200-250 volts (Expori version $105-120$ volts). Total building cost all parts, valves, front panel, ready punched chassis, 2 coils, $20-60$ and $55-190$ meters, wire, solder, instruction manual.
 for easy coil changing, Silver grey finish, $27 / 6$.
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## TRANSISTOR PORTABLE

ANEW six-transistor pocket portable receiver has been introduced on to the market recently by Pam (Radio and Television) Ltd. The printed circuit gives a maximum output of 45 mW through a 2 in . loudspaker. This set will tune over the medium wave band and also provides the Light programme on long waves.

The dimensions of the receiver are 4 in . $\mathrm{x} 2 \frac{3}{3} \mathrm{in}$. $x 1$ in, and the grey polystyrene cabinet has a facia of white and gold. A socket is provided in the cabinet for a 102 impedance ear-piece.

The power for the set is supplied by three 1.5 V cells, giving a total of 4.5 V . The price of the set is $10 \frac{1}{2}$ gumeas and an optional carrying case is available at 7s. 6d. extra. Pam Radio and Television Lid., 295 Regent Street, London, W.I.

## POWER DISTRIBUTION UNIT

THIE latest addition to the range of distribution boards made by Lexor Electronics Ltd., is the DDis-board' portable unit.
This mit is available in 2-. 4- and 6-way groups of 5.13 or 15A sockets. The finish can be either in brown or ivory and the suckets may be switched or unswitched.

There is a wide varicty of extension cables and plugs which can increase the usefulness of any particular unit. The "Dis-board" is connected to the mains outlet by a length of heavy-duty flexible cable.
L.st prices range from $£ 39 \mathrm{~s} .6 \mathrm{~d}$. to $£ 519 \mathrm{~s}$. 0 d . and all standard combinations (and the available combinations and types now exceed 300) are available from stock.

The manufacturers are Lexor Electronics Lid., 25 Allesley Old Road, Coventry, Warwickshire.


A 4-way distribution unit from Lexor Electronics Ltd.

## STABILISED POWER SUPPLY

'THIS Heathkit power supply kit -model MSP-1—has been developed by Daystrom Ltd.

The stabilised D.C. output is variable over a range from 200 to 410 V . by a control mounted on the front panel. Separate transformers are used for H.T. and L.T. sup-1 plies and Mains H.T. supplies are indicated by two neon lamps. A 3-position off/stand-by/on switch enables the D.C. outputs o be switched off while leaving the heater supplies connected. The unit also features an unstabilised $6 \cdot 3 \mathrm{~V}$ A.C. centre-tapped output at 4.5A.

Two models are available. one with meters and one without. In the former model, the meters are 3 in. moving coil instruments; a voltmeter reading $0-400 \mathrm{~V}$, and a milliameter reading $0-25 \mathrm{~mA}$.

The unit is of all steel construction and the cabinet is louvred to ensure adequate ventilation. The dimensions of the cabinet are 13 in . $x 8 \frac{1}{2}$ in. $\times 9 \frac{1}{2} \mathrm{in}$. The kit is made by Daystrom Lid., Gloucester.

(Above) The model 127A Tavlor Multimeter.

## TRANSISTOR CLIPS

RECENTLY made available from the Plessey Co. Ltd., are two transistor clips (types A and B), which are intended for 5 or 6 mm nominal diameter transistors.
The type A clip is moulded in virgin polythene which incorporates a high density pigment to eliminate absorption of ultraviolet radiation. This pigment also serves to identify the two sizes of clipblack for 5 mm and brown for 6 mm diameter transistors. The poly-


New Plessey transistor clips.
thene used is completely inert and will not affect protective coatings on either metal or glass cased components. Tests indicate that these clips do not limit transistor heat dissipation and can be used over a range of ambient temperatures from $-55^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

Type $B$ is formed from beryllium copper, hardened by heat treatment. One clip covers both 5 and 6 mm diameter transistor units.

The Plessey Co. Lid., Ilford, Essex.

## IMPROVED MULTIMETER

AN improved version of the Taylor $20,000 \Omega / \mathrm{V}$ pocket size multimeter (model 127A) has been recently announced.

A feature of the new model is the facility for measurement of high D.C. The instrument now has a special "millivolt"" socket and a range of "plug-in" miniature shunts is now available for readings of 1,5 and 10 A D.C. These shunts are designed to locate directly into the millivolt sockets incorporated in the Model 127A, thus forming a compact unit for measurement of high D.C. current.

A new type of ohms adjust control is now fitted which ensures greater stability and an improved type of A.C./D.C. selector switch is also incorporated.

The instrument is made by Taylor Electrical Instruments Limited, Montrose Avenue, Slough. Buckinghamshire.

## COMMUNICATIONS RECEIVER

'HE model CR 66 is a new communications receiver kit from the Codar Radio Company.

The CR 66 covers a frequency range from $540 \mathrm{kc} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$ in four ranges. The separate main tuning is calibrated in frequencies and the bandspread is calibrated in degrees. The circuit includes a regenerative l.F. stage for maximum gain and BFO for C.W. reception.

The size of the cabinet is 16 in . $x 6 \frac{1}{2} \mathrm{in}$. $\times 8 \frac{3}{4} \mathrm{in}$. and the front panel is finished in silver and black. An output socket is provided for tape recorder; etc. and also one for an external speaker.

The total cost of parts, less the cabinet, is $£ 1610 \mathrm{~s}$. and the cabinet costs $£ 115 \mathrm{~s}$.

The kit is made by the Codar Radio Company, Culebrook Road, Southwick, Sussex.

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 \({ }^{8} / 6\); \(100 \mathrm{H} ., 80\) IDA, \(8 / 6: 9 \mathrm{H}, 100 \mathrm{~mA}, 5 / 8\); Potted \(10 \mathrm{H}, 100 \mathrm{~mA}, 7 / 6\); SWITCHES': Waser, es pole, 4 way, 4 bank, \(3 / 8 / 8 ; 30 \mathrm{H}_{\text {, }} 30 \mathrm{muA}\)., \(\% / 6\)

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(Continued from page 294 of the August issue)
By B. Lewisham

9 circuit was followed by details of the construction
of the chassis. Now the constructor may proceed to the next stage, which is wiring.


Fig. 4-The complete wiring diagram.

The chassis of the receiver can be wired up independently of the remainder of the circuit. Wiring is simple but the valveholders are best attended to first. In the layout and wiring diagram (Fig, 4), the valve platform is shown pressed out flat so that the underside connections may be seen clearly. Use of modern miniature capacitors and resistors is desirable in order to prevent undue congestion and the electrolytic decoupling capacitor, C8. should be a miniature type.

\section*{Testing}

The usual tests and checks for faults in the wiring, etc. are made with a testmeter prior to switching on, particular care being taken to ensure that the mains wiring is correct. A three-pin plug should be fitted to the end of the mains lead in the correct sense and a pair of attractive control knobs fitted to the receiver. If all is in order, the receiver may be switched on and an aerial (a few feet of wire will do) connected. It should then be possible to tune in various transmissions by operating VCl and VR1 judiciously, care being


Fig. 5-The method of construction used by the author in making a suitable cabinet for the receiver.


A view of the interior of the completed set.
taken not to let the receiver oscillate. The precise setting of TCl will depend upon the aerial in use, location, etc. but the best position can soon be found by experiment. the smallest capacitance possible probably giving the most satisfactory
results over the band. The value of C7 can also be altered experimentally: for example. if reproduction tends to be shrill. the value may be increased to \(5,000 \mathrm{pF}\) or more as required.

\section*{Housing the Receiver}

All the woodwork dimensions required are shown in Fig. 5. The sides are glued to the inside of the panel and are held securely by metal "L" brackets; wooden reinforcement blocks will also serve just as well. Quadrant ( \(\frac{3}{8} \mathrm{in}\).) is glued to the top of the panel and sides to form a frame mitred at the front corners. Similarly. quadrant is fitted to the inside edges of the loudspeaker aperture.

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PO15


WHILE transistors have unquestionable advantages for portable equipment, there are many constructors who still prefer the positive and assured results that are obtained with a well-tried and conventional valve circuit. By taking advantage of the miniature components that are now available a very compact valve set may be constructed with the sure knowledge that it will work first time and give good performance.

Modern low consumption valves are used in this circuit and these, in conjunction with an inexpensive combined H.T. and L.T. battery, provide quite an economical receiver.

All the parts are standard proprietory lines, easily obtainable from any of the suppliers who advertise in this journal and probably many constructors will find quite a few of the parts already in their own store of spares.

\section*{Circuit}

It will be seen that the circuit (Fig. 1) is a completely conventional 4 -valve superhet covering


\author{
A FOUR-VALVE \\ BATTERY SUPERHET \\ FOR MEDIUM AND LONG WAVES
}
full medium wave and sufficient of the long wave to tune the Light programme, at good strength, anywhere in the country.

The actual lay-out has been very carefully arranged to achieve a neat and compact design and from the group-board wiring diagrams (Figs. 2 and 3 ) it will be seen that practically all the small components can be mounted on to two groupboards which can be completely assembled and wired up before fitting to the chassis.

The original prototype had the chassis and front panel made in one from a single piece of aluminium, but this had several disadvantages atif it will be found much easier to make these as the separate items as shown in Figs. 4 and 5.

\section*{Wiring the Group-boards}

Before assembling any components on to the chassis, it will be best to wire and mount the smaller components on the two group-boards; the exact position of these and the method of wiring up at the back of the boards will be seen quite


Fig. I-The circuit.

Fig. 2-Wiring of the main group-boord.
clearly in Figs. 2 and 3. It is recommended that one end of the board is marked in some way, as it is quite easy to be confused when constantly turning it round for wiring up.

As these group-boards have to be bolted to the main chassis, remember to leave the two relevant components off until the boards have been mounted, to enable the
 screws to pass through the holes. It is also important to note that an insulated back-plate is placed between the back of the board and the chassis.

\section*{Mounting the Major Components}

Having completed and fitted the tag-boards, the next step is the mounting of all the main components to the chassis taking particular note of the orientation of the valveholders. The I.F. Trans-
 formers have similar windings for primary and secondary and it is not important which way round they are fitted. Some constructors may prefer to leave the front panel with its associated controls and

Fig. 3 (left)-Wiring of the auxiliary group board.

(Above)-The receiver assembled in its cose.

parts separate from the main chassis until later in the assembly, and it is suggested that a strip of insulation tape along the inside lower part of this front panel is a useful precaution as the clearance between it and the group-board tags is rather small.

It is advisable to leave the ferrite rod aerial to last as some alterations to it are necessary before fitting, and also it will eliminate the risk of breaking or damaging it during construction.
The two-gang tuning condenser is mounted from the front of the panel using three countersunk 4B.A. screws. (Ensure that these are cut down short enough to prevent them from projecting through and interfering with the movement of the vanes of the condenser.) The loudspeaker can also be mounted in a similar manner,
(Continued on page 437)
Fig. 4-The chassis drilling dimensions.

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The chassis of the receiver viewed from above.
some slight alterations will need to be carried out to the rod aerial before fitting. In the first place it will be found that there are low impedance coupling windings over the top of each of the two coils and these were removed completely. if it is desired to use this set , ith a car radio aerial in a car these windings may be left on and taken in parallel to a suitable socket for the car aerial. In the prototype it will be seen that the medium wave winding is connected to the upper two tags with a miniature 60 pF trimmer soldered into position across it, and the long wave winding is connected to the lower tags and another 60 pF trimmer positioned in parallel.

\section*{COMPONENTS LIST}

Resistors (All \(\frac{1}{2}\) W \(10 \%\) )
\begin{tabular}{clllll} 
Resistors \((A l l\) & \(\frac{1}{2} W\) & \(10 \%\) & & & \\
RI & \(82 k\) & \(R 5\) & \(2 \cdot 2 M\) & \(R 9\) & \(I M\) \\
R2 & \(33 k\) & \(R 6\) & \(100 k\) & \(R I O\) & \(2 \cdot 2 M\) \\
R3 & \(27 k\) & \(R 7\) & \(10 M\) & \(R I I\) & \(390 \Omega\) \\
R4 & \(27 k\) & \(R 8\) & \(2.7 M\) & &
\end{tabular}

VRI 2 M log. with D.P. switch
Capacitors (All miniature components)
\begin{tabular}{|c|c|c|c|}
\hline CI & 0.04 \(\mathrm{F}^{\text {F } 150 \mathrm{~V}}\) & C8 & loopF mica \\
\hline C2 & 0.04 \(\mu\) F 150V & C9 & \(0.01{ }_{\mu} \mathrm{F} 150 \mathrm{~V}\) \\
\hline C3 & 100pF mica & Clo & \(0.04 \mu\) F 150 V \\
\hline C4 & 100pF mica & CII & \(0.04 \mu \mathrm{~F}\) 150V \\
\hline C5 & 500pF mica & Cl2 & \(2 \mu \mathrm{~F} 150 \mathrm{~V}\) elec \\
\hline C6 & 0.01 \({ }_{\mu} \mathrm{F}\) 150V & CI3 & \(25 \mu \mathrm{~F} 15 \mathrm{~V}\) elec \\
\hline C7 & \(0.01 \mu\) F 150 V & C14 & 33pF mic \\
\hline
\end{tabular}

VCI, VC2 \(500 / 500 \mathrm{pF} 2\) gang tuning (Jackson type L)
TCI, TC2 60pF miniature compression trimmers

Valves
VI DK96 V3 DAF96
V2 DF96 V4 DL96
Two Denco IFT.II I.F. transformers (465kc/s)
Miniature output transformer
Oscillator coil (Weymouth radio type H03) Switches

SI D.P. switch on VRI
S2 D.P.D.T. slider switch
\(69 \mathrm{~V}+1.5 \mathrm{~V}\) battery
Miniature 14-way and 5-way group-boards
Medium and long wave aerial (Repanco FS2)
\(2 \frac{1}{2}\) in \(3 \Omega\) loudspeaker
Miscellaneous:
Valveholders; knobs; battery plug; nuts; bolts; etc.
(Continued from page 434) using 4B.A. countersunk screws with nuts on the inside to make it secure. When all the parts have been fitted to the front panel it can be completed by covering with fine mesh expanded metal, or loudspeaker covering material, leaving a small aperture for the miniature wave-change switch. If it is intended to fit dials one can be mounted under the fixing nut for the volume control and the other one for the tuning indicator is best secured by using contact adhesive.

Most of the wiring is quite itraightforward and obvious From a study of the diagrams. In order to simplify the wiring


This underchassis view shows the two group-boards clearly.


Fig. S—The front panel drilling details.

Sufficient length of lead should be left to allow both these coils to be noved along the ferrite rod for tuning to the best position. It should be noted that this aerial coil wire is Litz and it is essential when making soldered joints that every single strand is carefully cleaned and tinned otherwise performance may be
affected. The ends can be carefully cleaned by placing on a firm surface and scraping gently with fine emery cloth, or another method is to heat the wire ends in a small flame and while still hot, plunge them into methylated spirit after which the ends can be wiped clean and then soldered.
(To be continued)

\section*{Power Rectifier Circuits}
(Continued from page 397) resistance of the tranformer winding is often an appreciable fraction of this value, and added to this there is already the internal resistance of the rectifier present. Thus surge limiters of at the most a few hundred ohnms will be needed with a PY81, however large the smoothing capacitors may be made. Under the conditions of Fig. 19 where the smoothing capacitors are only \(5 \mu \mathrm{~F}\) each, no limiting resistor was deemed necessary. It is in fact good practice not to make the smoothing condensers too large in the power supply itself, providing the additional smoothing internally in each consumer circuit connected, in the form of a large series resistor and electrolytic condenser, as shown in Fig. 27. This provides decoupling and smoothing in one, and avoids unnecessarily large rectifier surge currents.

\section*{Values}

Good power supply designs use surprisingly small values for the smoothing capacitors, of ten only a few microfarads, especially for the first capacitor (the "reservoir". condenser) connected directly to the rectifier. If insufficient smoothing'is thereby achieved, then electronic stabilisation is resorted to, which gives far lower internal impedances and far greater smoothing than is achieved by haphazard increases of smoothing capacities, and far lower strain is imposed on the rectifiers. Several such circuit designs have been published in this magazine.

All circuits using large values of smoothing apacitors connected directly to a rectifier are to
be considered basically as compromises in compact or cheap-to-construct apparatus, where it is not deemed desirable to waste 100 much space or attention on the power supply. Such circuits give very reasonable performance life if capacities not exceeding about \(32 \mu \mathrm{~F}\) are connected direct to the output of normal valve rectifiers, and not exceeding about \(64 \mu \mathrm{~F}\) for metal rectifiers, and not exceeding about \(100 \mu \mathrm{~F}\) for silicon power-rectifiers. However, these figures must be treated as mere, very rough guides. The higher the reservoir capacity, the greater the strain on the rectifier, and the more is its useful life likely to be shortened.

\section*{Domestic Equipment}

In domestic radio sets and other equipment subject only to intermittent service with long periods of rest, the matter is far less critical than for laboratory apparatus intended for long-period non-stop experiments. Thus the author is at present conducting experiments with Geiger-counter monitors for atomic radiation, for which a large quantity of electronic equipment is in non-stop operation day and night for weeks on end. If insufficient attention would have been given to proper design of power supplies, for example, frequent breakdowns would have been inevitable, whict. would have caused the loss of valuable measurements, as well as the trouble and expense of such break. downs. Even for television circuits a highel measure of care is required for power-supplies than for simple radio receivers, because highe, voltages and currents are involved, more expensive equipment is in danger in case of breakdown, anc the operating hours of television sets in mos families are longer than those of radio sets!

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The Editor does not necessorily agree with the opinions expressed by his correspondents

\begin{abstract}
Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative details or surplus equipment. We cannot supply alternative details
for receivers described in these pages. WE CANNOT for receivers described in these pages. WE CANNOT
UNDERTAKE TO ANSWER QUERIES OVER THE TELEPHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iii of the cover.
\end{abstract}

\section*{P.C.R. COMMUNICATIONS RECEIVER}
\(S^{I R},-\) I wonder if any of your readers could advise me as to what is the correct I.F. of the P.C.R. communications receiver currently available. Also, 1 would like to know, the make and type of a suitable BFO coil for use with half a 6 SN 7 in this set.
I would also be very grateful if anyone could sell or loan me a copy of the original circuit for the R.F. unit No. 24.-A. Watt ( 67 Glenhurst Avenue, Bexley, Kent).

\section*{american station}

SR,-In answer to a query made by Mr. T. Gerrard in the July issue, regarding an American station he heard on the 32 m band, the station is one of the American Telephone and Telegraph Co. radio telephone services. These stations are not engaged in broadcasting but are used solely for international communication.

A station which may be of interest to Mr. Gcrrard and other readers, is WRUL New York. which broadcasts some excellent programmes and is, in fact, the only commercial S.W. station operating from the U.S.A. The times of transmissions are 15.00-23.00 GMT on week days; \(18.30-23.00 \mathrm{GMT}\) at weekends. The frequencies for Europe are \(15,380 \mathrm{kc} / \mathrm{s}\) ( 19 m band) and \(17,760 \mathrm{kc} / \mathrm{s}\) ( 16 m band). -R . Patrick (Derby).
\(\mathrm{S}^{I R}\),-The transmission identified by T. Gerrard (July issue) as coming from an American station, is in fact a single sideband transmission by a German station.

The message in English is as follows: "This is a test transmission by a single sideband system operated by the Overseas Service of the DeutschePost Francis Main Terminal. Please give identification signal on channel A for receiver adjustment".

The other message is in German. - R. R. Diamond (Stockport, Cheshire).

\section*{medium wave fading}

\(S^{1}\)IR,-I have been having trouble with a 12 -yearold McMichael receiver. It has the habit of fading on medium waves after it has been switched on for about 10 minutes.

The only way I have found to rectify this, is by
disconnecting the aerial lead-in and connecting it to earth! Could any reader explain this or suggest another way of curing the fault? - K. Clough (Bolton).

\section*{THE P.W. TROUBADOUR}

SIR,-I have just completed constructing the P.W. Troubadour, 7 -transistor receiver (June and July issucs) and am amazed at its performance. This pocket set gives better selectivity, sensitivity and none-fade reproduction than some expensive models owned by friends. Although it does work out expensive if the constructor has not any of the components in stock, this receiver must surely be worth double the complete kit price.R. W. Craig (Bexley, Kent).

\section*{TELEVISION BREAK-THROUGH}

SIR,-There have been a number of letters in recent issues about the reception of longdistance stations on crystal receivers and I think there is no doubt that in the majority of cases this reception is not direct from the station concerned, but re-radiated from a neighbouring aerial. I experienced a very similar effect some time ago. when I heard music as a background on my simple set, and on trying to resolve it found it was the BBC television programme. I felt that this could not be direct pick-up on account of the frequency used and my distance from the nearest station, and this was confirmed a little later when the station disappeared instantly-that is, it did not fade out. A few nights later I noted that the station returned, again in a sudden manner rather than a gradual signal strength build up, and I knew the people downstairs had a TV and made a few inquiries, as a result of which we carriec \({ }^{\text {d }}\) out some tests, and the programme did, in fact come from their aerial, which was of the indoot type, and their contrast control had to be full up There was obviously some H.F. instability which resulted in the signal being radiated in thimanner. I hope this will be of interest to others -E. Gowing (Portsmouth).

\section*{CORRESPONDENTS WANTED}

S\(\mathrm{R},-\mathrm{I}\) am 22 years of age, and I am interested in radio servicing as a hobby. 1 would like to correspond with amateur enthusiasts of my age from any country. - D. L. Kiriwandala, P.O. Box 732, Colombo, Ceylon).
SIR,-I am 16 years of age and would like to correspond with amateurs of my age. I have been interested in S.W. for about a year now.Butch Bone, c/o Daw Thein Wa's, Bookland, P.O Box 294, 385 Bogyoke Street, Rangoon, Burma

\section*{REPORTS OF CURRENT ACTIVITIES}

BRADFORD RADIO SOCIETY
Hon. Sec.: M. T. G. Powell, G3NNO, 28 Gledhow Avenue, Roundhay, Leeds 8 .

On June 26 th a number of members visited a firm of engineers. The two meetings for July consisted of an informal evening on loth and a talk by G30GV-"160m SSB"—on 24th.
DERBY AND DISTRICT AMATEUR RADIO SOCIETY
Hon. Sec.: F. C. Ward, G2CVV, 5 Uplands Avenue, Littleover, Derby.

G3ERD/P operated from Harborough Rocks, Brassington on July 7th and 8th for the second R.S.G.B. Two-metre Field Day. L. Ball gave a talk on July IIth and the meeting for 18th was taken up by the fourth direction finding league fixture.

A sale of members' surplus equipment was held on August ist.
Future Events:
August 15th-Direction finding league fixtura, No. 5.
August 22nd-Stereophonic demonstration.
MIDLAND AMATEUR RADIO SOCIETY
Hon. Sec.: A. B. Watt, G2DRG, II Holly Road, Handsworth, Birmingham 20.

On Tuesday, i7th July, members attended a lecture given by H. C. Smith. The title of his lecture was "Tape Recording", and it was given at the Birmingham and Midland Institute.

Future Event: "GGDAF receiver for SSB" by G3LLN.

\section*{MORECAMBE AMATEUR RADIO SOCIETY}

Hon. Sec.: K. J. SIngleton, G3NLM, 8 Westmoor Grova Heytham, Morecambe, Lancashire.

Metings of this society are held on the first Wednesday of each month at the Liberal Club. Balmoral Road, Morecambe, and start at 7.30 p.m. Any new members will be mado welcome.

For the July meeting, a number of members visited the automatic telephone exchange in Lancaster. The meeting for August was devoted to a ragchew.

NORTHERN HEIGHTS AMATEUR RADIO SOCIETY
Hon. Sec.: A. Robinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.
Recent club accivities have included a display of members' equipment which was held on July 4th.

At the meeting on August Ist, the sociery played host to membery of the Manchester Radio Society, who gave a D.F. demonstration. On August 4ch, members operated a demonstration station at the Warley Club and Instituce Charity Gala.

PURLEY AND DISTRICT RADIO CLUB
Hon. Sec.: E. R. Honeywood, G3GKF, 105 Whytecliffe Road, Purley, Surrey.

A portable expedition was held on the evening of July 6th, at Walton Heath. Operation was on Two-metres and Top Band. On July 20th, members heard an R.S.G.B. tape recorded lecture which was illustrated by slides.

Future Event:
August 17 th -Film of National Fiold Day.
RADIO CLUB OF SCOTLAND
Hon. Sec.: A. Barnes, GM3LTB, 7 Southpart Terrace, Glasgow W. 2

This is a new radio club which held its inaugural meeting on June ist this year. Meetings are held every Friday evening, and commence at \(8 \mathrm{p} . \mathrm{m}\). A welcome is extended to anyone who is interested in the hobby of amateur radio. All interests are catered for but suggestions are always welcome for expanding the prom gramme. The first Friday in every month is especially for beginners.

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\] & \(7 / 8\) & 10 FL & 4／6 \\
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\section*{SPECIAL NOTE}

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[^1]:    B. B.C. Pocket Frransistor. M.W and L. W Radio Klt, 22/6.
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[^2]:    

