# FEBRUARY Practical 2/-WIRELESS

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**ELECTRONIC** DIGITAL COUNTER with Geiger-head



16m TO 175m TRANSISTOR S. W. TUNER

MIDGET MAINS SUPERHET



# BRAND NEW AM/FM (V.H.F.) RADIOGRAM CHASSIS AT £14 (Carriage Paid)

A.C. ONLY. Chassis size 15 x 61 x 51 n. high. New manufacture. Dial 141 x 41n. in black and gold. P. L. and Dipole Sockets. Five push bittons—OFF L.W., M.W., F.M. and Gram. Aligned and tested O.P. throssomer. Tone Control. 1,000—1,900 M.: 200-500 M.: 88-98 Mc/s. Value E2/80 rect., ECH81, EF98, EABC80, EL81, ECC85. Speaker and Cabinet to it chassis (table model). 47/6 (post 2/6). 10 x 61 E.L.(PTICAL SPEAKER, 20/-, to purchasers of this chassis. WILLIAMS.—Glassis) 25 down and 5 Monthly Payments of £2, or with Cabinet and Speaker £5.10.0 down and 6 Monthly Payments of £2. Cheap Room Dipole 10/-. Feeder 6d, yard.

# THE "CANTATA" 6-TRANSISTOR DIODE PORTABLE

COMPLETE KIT FOR ONLY

£7.19.6

(post 3/6)

- of kit).

  Size 9 x 31 x 7in. ★ 8 x 2iin, P. M. high quality speaker.

  Attractive Vinair covered cabinet, two tone.

  Two batteries 5/6 the pair.

  High Sensitivity. ★ Good selectivity.

  Mullard transistors 0.6.44. 2 x 0.6.45, 0.681D. and 2 x 0.681.

  Top grade Wey mouth Radio Colis and transformers.

  Alignment service if required 17/6 (inc. post).

  Write for list of prices.

  All parts supplied separately.

  Note the total cost—no extras at all.

  Built in two hours.

BATTERY ELIMINATOR. For 4 Low Consumption Valves (96 range), 90 v. 15mA. and 1.4 v. 125mA, 42/6 (2/6 post). 200-250 v. A.C. Size 5) x 3} x 2m. Also for 250 mA. 1.4 v. and 90 v. 15 mA at

AUTOMATIC RECORD CHANGERS. ALL 4-SPEED WITH TURN-OVER CRYSTAL CARTRIDGE (carr. 5/- extra). Latest UA14, £7.18.0. Collaro C.60 Studio model, plays any records. 7-12in. only \$7.15.0. Motor board for UA8. UA14 or Collaro 3/6 (post 1/6). Both UA14 and C.60 fitted monaural cartridge but wired for stereo.

BEREC BATTERY RADIO IN MAKERS' CARTON. Valves DN96. Dr96. DAF96. DL96. Two Short Wavebands 2.5 to 7 Mc/s and 6.5 to 17 Mc/s. Cabinet 12 x 12 x 6in. ONLY 25 (2/6 p. & p.); MW and SW 25.4.0 (plus 2/6 p. & p.).



SELF-POWERED VHF TUNER CHASSIS. Covering 88-95 Mojs. Mullard permeability Tuner, Dims. 10½ x ½ x 5in. high ECCS5. EP91. EF91 and 2 diodes. Metal Rectifier. Mains transformer. Fully wired and tested. Only £71.40 (carr. pd.). Room dipole 10/-, 300 ohm twin feeder, 6d. yd. Tuner without power pack £6.14.0 (carr. paid).



#### PUSH-PULL AMPLIFIER £4.15.0

(4/- Carr.)

Brand new 200-240 A.C. Bass. treble and vol. controls. With valves EZ80, ECC83 and 2-EL84 giving full 8 w. Chassis 12 x 3 i x 3 in. With o.p. trans. for 2-3 ohm speaker.

Front panel (normally screwed to chassis) may be removed and using as "flying panel". Stereo version 2 x 4 w. same price.



#### COMPLETE V.H.F./A.M. RADIO FOR £12.10.0

Carr. paid)
Brand new set. in superb walnut
cabinet (size 19 x 8 x 144 in. high).
Covering 80-100 Mc/s. 16-49 M., and
200-500 M. Mains trans. 200-210 v.
with 2 tappings. Ferrite rod aerial
for A.M. Controls: volume on/off.
tone, tuning, w/change. Gram and
ext. speaker position provided.
Valves 12ATT, 12AH8, 6BJ6, EABC80
6BW6 and metal rectifier. Fully
guaranteed. Today's Value £20. (carr. paid)

COLLARO STUDIO TAPE TRANSCRIPTOR. 3 MOTORS, 3 SPEED. 14, 33 and 74 1.P.S. Push buttons. £10.17.6 (10/- carr.) incl. spool.

#### SUPERIOR GRAMOPHONE AMPLIFIER 3 valves, 4 watt

13½ x 7½in. (2½in. front to back). 3 front controls, bass, treble, vol./ on-off, 6¼in, circ. or 8 x 5in. speaker; UY85, UF86 and UL84. Mains trans. 200-240ac; "gold" fret front. ONLY 70/- (p.p. 3/6).

GRAMOPHONE
AMPLIFIER
With 5in. SPEAKER
Baffle 12; x 6in. E240 and
EL41. Tone and Volume
On/Off switch. Two
Knobs. Ready to play.
Useful for Stereo. ONLY
57/-, post 3/-.



3-VAI.VE AMPLIFIER (INC. RECT), 21 watts. ECC83, ECL82 and EZ80. Controls, volume bass and treble. On/offswitch. Overall size 10 x 4 x 4in. over valves. Mains and 0.P. trans. and 61 x 4in. Celestion speaker. Suitable for microphone input and for guitar amplifier. A.C. only.



70/- P. & P. 4/-.

#### MAINS OPERATED RADIO CHASSIS AND AMPLIFIER OF FAMOUS MANUFACTURE

Chassis 10 x 5 + x 4 in. front to back. Valves: UBC41. UCH41. UF99, UL84 with metal rectifier. 5 in. speaker. Ferrite rod aerial. Tone, vol. and gram. position. Covers L. and M. waves. Limited quantity at only 26 (5/- carr.) complete with small dial. Unused and in working order.



#### UNREPEATABLE OFFER OF AM-FM CHASSIS AT ONLY £9.9.0 carr. pd.

A Small quantity of Printed Circuit chassis by famous manufacturer. Valves UY85, UCH81, UF89, UABC80, UL84 and UCC85. O.p. trans. for 2-3 ohm speaker. Chassis 14 x 7 x 7in. Front controls concentric, left—Vol. and Tone; right—Wic and Tuning. "Gold" centre knobs provided. 2-dial bulbs. Sockets. AE: E. Ext. sp; P.U. Mains isolating transformer free. Covers Long. Med., VHF (87-101 Mc/s). Unused slightly tarnished, but not dirty; New Mullard Valves; not our manufacture, so no guarantee. Dial in gold and brown, size 13 x 3iin.

Send 6d. (stamps will do) for 20 page illustrated catalogue. All New Goods. Delivered by return. (C.O.D. 2/-extra).

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# GLADSTONE RADIO "SCALA", CAMP ROAD, FARNBOROUGH, HANTS.

(See other advertisement on page 918)

Farnborough 3371

Tel: Mitcham 6201 Open Daily to Callers

All Valves Brand New and Fully Guaranteed

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AC2PEN   ECC91 4/-	EZ35 6/-	PCF80 9/6	UI2	9/-	UY85	7'-	5Z4GT	9/-	6LD20 6P25	10/6		<i>ii</i> . I
21/- ECF80 8/6	EZ40 7/-	PCF82 7'-	UI4	9/-		12/6	6A7			17/6		16
AC2PEN ECF82 8/6	EZ41 7'-	PCF84 16/-	U22	8/-		15/-	6A8G_	8/6				1.
DD 211- ECH3 211-	EZ80 7/-	PCF86 15'-		21/-		17/6		13/6	6Q7	6'6		ó/- I
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AZI 15% ECH35 10%	E1148 2/-	PCL84 10/6	U27	8/-	VR15030	7/-	6AK5	5/-	6SG7	7/-		5/-
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D172	10/-	PL33 15/-	U339	15/-	X78	21/-	6BR7	12/6	7B6	10/-		5/-
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B 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		PL82 8/-	UABC8	0 7/-	Z63	7/6	6BX6	5/-	7C6	8/-		8/-
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SPECIAL OFFER

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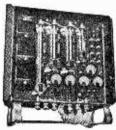
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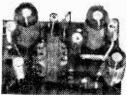








874	PRACTICAL WIRELESS	February, 1962
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Fluorescent Lighting  Complete lighting fittings. Built-in ballast and starters—stove enamelied white and starters—stove enamelied white and starters—to work. Ideal kitchen, workshop—anywhere. Twin 20 approximately 27m. long complete with we 20% tubes, 49/6. Single 40 approximately 4ft. long complete with one 40% tube, 39/6. Inductor 80 approximately 5it. long complete with one 80% tubes, 49/6. Carriage and insurance up to 150 miles 7/6, up to 250 miles 8/6. 21in. Miniature complete with 13 watt tube. Ideal for showase or position where miniature fitting is required. Complete with 40 watt tube, 24.19.6. Complete with 40 watt tube, 24.19.6. Carriage and Ins. 7/6 any type.  Smallest Possible 2-gang  With built in trimmers, polystyrene cased, size only 1 x 1 x 7/16in., price 12/6. Simallest IF and oscillator to match, 21/- P.P. Input and P.P. output transformers, 12/6. Circuit diagram free with any of above.  Transistor Set Cabinets  Very modern cream cabinet, size 5½ x 8 x 14in. with chrome handle, tuning knob and scale. Price 7/6, plus 1/6 possage and packing.  Special quotations for quantities.  Miniature Earphones	TRANSFILTERS	"Dim and Full" Switch
AND STREET, ST	Save alignment problems and improve performance. Use instead of I.F. trans-	Particularly useful for control photoflood lamps which have on short life at full brilliance.
	former. Complete with circuit 8/6 each,	switch has three positions; the position puts two lamps in se
		switch has three positions; the position puts two lamps in se at half brilliance for setting up, second position is off and the tiposition full brilliance for the position full brilliance for the second position full brilliance.
	CHARGING SWITCHBOARDS	position full brilliance for the op- tion shots. Also useful for carried rolling night lights, heaters, e- etc. Price 3/9 each, post 9d. Circulagram included.
	Carlotte Assessment	etc. Price 3/9 each, post 9d. Circ diagram included. Ditto but without the off position.
Complete lighting fittings. Built-in ballast, and starters—stove enom-	ু প্রতিষ্ঠ	d.p.d.c., 10 amp. 2/9.
ballast and starters—stove enam- elled white and ready to work. Ideal kitchen, workshop—anywhere.		Morganite Potentiomete
complete with two 20W tubes, 49/6. Single 40 approximately 4ft, long		Single and 2-gang types available.
complete with one 40W tube, 39/6. Inductor 80 approximately 5it.		standard size with
49/6. Carriage and insurance up to	A 100 A	spindle, all new and boxed. Single types, 1/
2lin. Miniature complete with 13 watt tube. Ideal for showcase or	4.	each, values available: 5K, 10K, 25K,
eiled white and ready to work. Ideal kitchen, workshop-anywhere. Twin 20 approximately 27m. log complete with two 20W tubes, 496. Single 40 approximately 4ft. long complete with one 40W tube, 396. Inductor 80 approximately 5ft. long complete with one 80W tube, 496. Carriage and insurance up to 150 miles 7/8, up to 250 miles 8/6. 2lin. Miniature complete with 13 watt tube, Ideal for showase or position where miniature fitting is required. Complete with latest lin. diameter tube, 49/8 each. Circular, Complete with 40 watt	Type A. 550 w. 18 v.—contains three reverse current	Single types, 1/each, values avail- able: 5K, 10K, 25K, 50K, 100K, 250K, 1 meg., 2 meg. Gang type 3/- aach—values av- ablve: 5K±5K, 100K±100K i meg. i Meg. 2 meg. +2 meg.
Circular. Complete with 40 watt tube. £4.19.6.	relays, one voltmeter rated 25 v. f.s.d., one main ammeter rated 40 amps. f.s.d., one secondary ammeter rated 45 amps. f.s.d., and two secondary meters rated 20 amps. f.s.d., and two secondary meters rated 20 amps. f.s.d. and two 12 comps. f.s.d. one 2 ohm variable resistor, one 11 ohm variable resistor, one 11 ohm variable resistor, one 12 ohm variable resistor ohm var	Meg. 2 meg. ±2 meg.
Carriage and Ins. 7/6 any type.	rated to amps, f.s.d. and two secondary meters rated 20 amps, f.s.d., one 2 ohm variable resistor, one 11 ohm variable resistor one 11 ohm variable re	Component Storage Drawers
Smallest Possible 2-gang		
-	Complete in metal case 2tt. 6in. x 2ft. 8in. approx. Price 22.15.0. carriage and ins. 15.  Type B. 1230 w. 50 v. 0.12 amps—contains one 14 ohm variable resistor and tour 1 ohm variable resistors, one main ammeter rated at 40 amps. 1.s.d., four secondary meters rated at 40 amps. 1.s.d. and one volumeter rated at 50 volts, and two reverse current relays. Complete in metal case—size approximately 2ft. 6 in. x 2ft. 8in. Price 24.15.0. carriage 15/-	
	dary meters rated at 20 amps. f.s.d. and one voltmeter rated at 50 volts, and two reverse current relays	
CONTROL ST	Complete in metal case—size approximately 2ft. 6 in. x 2ft. 8in. Price £4.15.0, carriage 15/ Connecting Leads for these switchboards with Nifam	0,0
With half in the	pross 30/- each.	Stout board construction, the
cased, size only 1 x 1 x 7/16in., price 12/6, Smallest IF and oscillator to	BATTERY CHARGER BARGAIN Components Would Cost More	Supplied complete with simple erection instructions—1/6 each or drawers each 6 x 24 x 64 in., 13/6, post
With built in trimmers, polystyrene cased, size only 1 x 1 x 7/16in., price 12/6. Smallest IF and oscillator to match, 21/ P.P. input and P.P. output transformers, 12/6. Circuit diagram free with any of above.	Car Battery Charger—ready-made high output battery charger in stove enamelled sheet steel louvred case. New, complete and ready to work. Rated at 12 v. 5 amps. and variable rate selector for trickle charging, also a meter to show charging rate. Suitable for 230/250 A.C. mains. Special snip price of 65/-, plus 3/6 poet and ins.	
The state of the s	enamelled sheet steel louvred case. New, complete and ready to work.	Yaxley Switches
Transistor Set Cabinets	rated at 12 v. 5 amps. and variable rate selector for trickle charging, also a meter to show charging rate	1 Pole 3 Way 1 Pole 5 Way 1 Pole 8 Way 1 Pole 12 Way
The second secon	Suitable for 230/250 A.C. mains. Special snip price of 65/-, plus 3/6	2 Pole 2 Way
// <b>(0)</b>	INFRA-RED HEATERS	2 Pole 4 Way 2 Pole 6 Way 2 Pole 12 Way 3 Pole 3 Way
	Make up one of these	4 Pole 4 Way
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For Transistor Circuits or Deaf Aid Very lightweight and easy to wear, cord almost invisible, good quality	SUNVIC SIMPLED CLATH THE AND A	
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msurance i/	The second of the charteness of the I	
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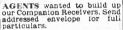
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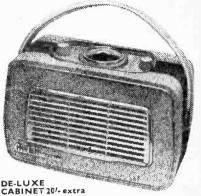
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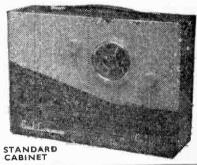
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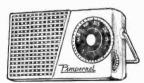
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A70C	17/6	D43	10/6	EL34		KT45	12/- PC/1 12/- (5 F	ren in sit	S11D	9/- U339 10/- U403	14/- X	71M	12/- 6B7	6/- 68K7M	6/- 2014	18/6 85AI	18/6
A70D	17/6	D63		EL35	18/6	KT55	12/- Tern	ninal)	8215 V	M 9/- U402	0 9/- X6	63	5/- 6B7M 6/- 6B8G	5/- 68 YG	F 9/- 25A6G 8/- 25L6		12/-
AC/P		D433 DA41		EL37 EL38		KT66 KT71	12/6		3 3 D 6	7/- UAF	41 11/- Z1	14	6/- 6BAG	7/6 6887	8/- 25 Y 5	10/- 89 10/- 117Z6	GT 12/-
AC/H	L 15/-	DARL	0 8/6	E1.50		KT74	12/6 PL3: 12/6 PM2	3 18/-	8D20 8D61	9/- UB4	10/- Z2 21 18/6 Z3	21	6/- 6 BG60	21/-6T8G	12/- 25 Y 5G	10/-	12/-
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AC/SF		DD-PI	: 10/-	EM4 EN31	12/6	KTW6	3 5/6 PM2	B 7/-	8P4	12/6 UCL	1 14/6 26	36 ]	15/- 8C5G	6/- 6U80	8/- 28D7	6/- 202DI	9/- T
AC/8G	10/6	1	18/6	EZ2		KTZ68		M 9/-	Met)	Pin UM3-	16/- Z9 16/- Z8		12/- 606	6/6 6V6GT	7/= 30FF	7/-	16/6
AC/52		DD13s DD41	16/6	EZ3	9/-	LI2	6/- PM3	9/-	SP4B	12/6/UR3	16/- 28		12/_ 6C8 12/- 6C8G	12/- 6W7G 12/- 6X5	9/- 30LT 6/- 30P4	7/= 202PT 11/-(202ST	
AC/52	18/6	DD101	10/6	FC4	15/-	L21 L42	6/- PM3 6/- PM4		SP6	12/6 UU7	15/- 1A	14E	6/_ 6OH5	8/- 6 X 5 G	6/- 31	12/-	16/6
AC/SX	V17	DD207	10/6	FC13	15/-	L63	6/- PM4		SP13 SP13C	12/6 UUS 12/6 UUS	23/- 1A 1/250 1A	15GT	6/- 6CJ5 12/- 6D1	9/-6X6	6/- 33	12/- 202 VP	B
ACUTE	16/6	DD620 DD402	10/6				6/-	12/-	SP22	12/6	18/6 1C		10/- 6D6	7/- 6Y6 5/6 6Z5	6/- 34E 8/6 35	12/- 18/- 203TH	16/6
AC/TE	118/6		10/6	FW4/5		LP4 LP220	6/- PM5 8/- PM1:	B 9/-	SP41	12/6 UU60	/250 1C	5GT 1	12/-/6D8	6/6 625/122	5 35A5	17/6	16/6
AC/VI	1 15/-	DDL-4	8/6	GT1C	010	TTITOO	10/- PM2	2NL 9/- 2A 10/-	SP130F	12/6 (4 Pir 12/6 UY11			10/- 6D8G 10/- 6F1	6/6	8/6 35 E	17/6 210DG	16/6
AC2H		DDT2	8/8	GTD4E	10/6	ME41	12/- PM2:	2D 10/-	BP132	12/6 U Y 31	15/- TF	5G 1	10/- 6F5G	18/6 7A3 9/- 7A7E	17/6 35ZA 11/- 35Z5	17/6 210LF 8/- 210VP	16/6
		DET19	5/6	GTD4C	22/-	MH4	7/8 PM2	A 10/-	SP141	12/6 V914	12/- 1F	6 1	0/- 6F6G	7/- 7B8	14/- 36	9/-	16/6
AC3	10/6	DH76	5/-	GZ32	10/-	MH41	8/6 PM25	10/-	SP215	12/6 V L86	B 19/8 10	7 1	0/- 6F7	7/- 7C5 9/- 7C6	7/- 39/44 7/- 40	11/- 2158G	16/6
AC4 AC5/P		DH101 DL63		H13	12/6	MH41	PM20	2 10/-	8P220	12/6 VO4	12/6 IL.	A6 1	2/- 6F8G	9/- 7 D3	9/- 40SUA	11/- 220HP	16/6
	10/6	DL72	16/- 12/6	H42	12/6	(0 Pin) MH410	14/6 PM27	0 10/-	SP1320	12/6 VP2	10/- IL	B4 1	0/- 6F11	16/- 71)7	9/- 41	12/- 220PT	16/6
AC5/P	EN-	DL82	12/8	H63	12/6		10/- PM2: 12/- PM2: 12/- PM2: 7/6 PM2: 8/6 PM2: PM2: 14/6 PM2: 15 PM2: 10/6 PP3/:	250 8/-	SB210	12/6 VP4	19/8/11/	C6 1	0/- 6F12 4/- 6F13	3/6 7D8 11/- 7K7	9/-,41E	12/- 220T	16/6
AG8	12/6	DL810 DN41	7/6	H141D	12/6	MHL4M	4 6/- PP4	9/- 10010/-	BT11		18/6 1L1	E3	9/- 6F14		11/- 41M DG	12/- 230PT	16/6 10/6
AGX2	270	DC20		HD24 HP4101	10/6		14/6 PP13	10010/-	SU25	10/6 VP4 10/6 (5 Pin	102	5	9/- 6F15	14/- 707	11/- 41 MHL	12/- 304	10/6
		DC25	10/6		10/6	MKT4	PP35	9/-	SU2150	A VP13	A 12/6 1W	7.1	9/= 6F32 9/= 6G6	10/- 7¥4 5/- 8A1	8/6 41MLF	12/- 354♥	8/6
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APP4E	17/6	DW 4/50	00 0	HP4115	10/8	ML6	7/6 PT-10			10/6 VP23 10/6 VP41	5/6	14	4/6 6H6	3/- 9AI	3/- 41MPG 9/- 41MPT	12/- 402P	
APV4	8/6		16/6		10/6	MPT42	18/- (4 Pir	1) 6/-		10/6 VP10:	5/- IW	4/500	6H6GT 4/6 6GH7	3/- 9D2 6/- 10D1	4/- 41MRC	12/- (7 Pin 12/- 431U	18/6
ARPS8	5/6 2 5/6	EAB1 EB4	9/-	HL13	15/-	MS/PE	N PT23	0	TDD9A	1916 VPT A	10/8 2A3	3 8	8/8 6J5	0/- 101 4	11/6 41MTS	12/- 45111	8/6
A84120	12/6	EB34		HL23	15/-	MS/PE	12/6 (5 Pir N PV30	1) 9/-	TDD13	12/6 VPT4 12/6 VR19	10/6 2A5 9/- 2D4	5 8	8/6 6J5GT	5/- 10.P14	18/- 41M X P	12/- 565	8/6
ATH 43		EBC3	18/6	HL41	18/-	(7 Pin)	12/6 PY31	15/-	TH13C	12/6 V R53	7/6 2D4	4A 8	8/8 6J7 8/8 6J8	7/- 12A6 9/- 12A8	5/- 418TH 8/- 42		8/6
AW2		EBC33 EBC81	5/- 8/-	HL41D	18/-	MS/PE	N-4 PY32 18/6 PZ30	141	THEFT	10/2 V DEE	8/6 2D1	13 8	3/6 6J 5G	7/- 12AH7	7/- 42MPP1	11/- 615-3T EN 774	8/6 8/6
AW3	5/-	EBF11	9/-	HL42D	D .	MS/PE	18/6 PZ30 N B PEN4	VA/5	FH2321	12/6 V R 26	8/6 2D1 8/6 2D1	13A 8	3/6 6J86	12/- 12AM76		17/6 807	7/6
AZI	18/7	EBL21 EC31			10/-		19/0	15/-	FF22	12/6 VR91	8/6 2-P	22	2/- 65.7	8/- 4/- 12BE6	12/- 42MPT 9/- 42/OT	17/6 870	8/6 8/6
AZ2	18/7	EC50		HL46 HL1331	18/-	MSP4 (5 Pin)	19/8 PEN4	VB   17/6	FP23	12/6 V R92	8/6 2 X 2	2 4	1/8 6 K 7 CF	4/- 12C8	9/- 420TD1	884	8/6
AZ11	18/7	EC52	5/8		21/-	MSP4	PEN2	5 15/-	P1340	12/6 VR116 12/6 VR135	8/6 2X2 8/6			10/6 12J5 18/- 12J5GT	4/-	11/- 956	3/-
AZ31 AZ50	12/6	EC53	5/6	HL1320 HVR2	21/-	(7 Pin) MUI	10/6 PEN3	6C 11	FP2020	12/6 V R 136	8/6 31)6	1 5		18/6 12J7	4/6 42SPT 9/- 43	9/6 1701	8/6 8/6
B21	15/-		13/-	HVR2A	7/-	MU14	8/- 8/- PEN4	23/-	PSE4	12/6 VR137 12/6 VR505	8/6 3L3	86 8	8/- 6L7	6/6 12K7	5/- 44	9/6 1×81	8/6
B36 B65		ECC31	5/6	HW/30	18/6		18/6 18/6 PEN4	23/-	rr4	12/6 VR105	8/6 4D1 30 4TH		3/- 6L7G	6/6 12K8 12/- 128A7	7/6 45	10/- 2050	8/6
BR201	10/-	ECC32 ECC33		K23B K30G	8/6	N16	18/6 PEN4	4 23/-	T11	12/6	8/6 4TP	12	/- 6L19	18/6 128C7		10/- 2051 10/- 2101	8/6 8/6
BB1050	-50	ECH3		K30K	8/6		18/6 PEN4 17/6 PEN4	5 18/- 1		12/6 VT25 9/6 VT61	6/- 4TP 6/- 4TS		7-6LD20	14/- 12817	8/- 47E	10/-2151	8/6
PITOOO		ECH34		K40N	8/6	N 108	18/6 PEN 2	20 A U	J17	9/6 VT100	6/- 478		y-6N1 y-6N7	9/- 128G7 7/- 128J7	8/8 47MG	10/- 2220TH	
BU200 Cl	12/6	ECH35			12/8		18/6	22/- U	J19 ;	25/- VT105	8/- 5B/2	25/M	6N7GT	7/- 128K7	7/6 50 A5 5/- 558		18/6 17/6
C1C	12/6	EF5	5/- 1	K80B	12/6	O54 B	18/6 PEN4: 7/- PEN4:	2822/- L	121	8/- VT109 8/- VT119	6/- 6/- 5U46		/-6N7M	7/- 1281.7	9/- 50	11/- 4687	10/6
C5PEN		EF6 EF8	10/- 1	K BC32	10/6	OA4	6/-	22/ L	J23 1	2/6 VT136	6/- 5Y3		/- 6P1 /- 6P25	12/- 128Q7 11/6 128 87	9/- 57 8/- 61	11/- 4687A 11/- 6153H/0	10/6
CloB			16/6 I	KCF30	10/6	OC3 OD3	9/- PENA	4 17/6 L	J31	9/6 VT202	6/- 5Z3	10/	/6/6P26 1	17/6 12887	8/- 61BT		05 12/6
C20C	8/8	EF11	18/6   I	KF35	7/8	OM1	8/- PEND 9/- 1360 (		J33 1	8/6 VT203 8/6 VU39	6/- 5Z4	9	/- 6P28 1	L8/6 12Z3	8/6 618PT	11/- 7193	8/6
C23B C36A	8/6 12/6	EF37A	11/- 1		10/6	OZ4	9/-	22/- L	147	9/- VUIII	6/- 6A3 6/- 6A4		6 6 R Y		2/- 62BT 2/- 63SPT	11/- 7475	8/6
CBL1	21/-		6/6 1 5/- 1		10/6 I		7/- PEND		150	6/6 W21	fi Afi	10/	6 6 R 7 G	9/- 14B6 1	2/- 70LY	9/- 8012 8/-	12/6
CL4	21/-	EF51	5/- F	CT24	10/- (	(4 Pin)	7/- PT4	22/- U		6/6 (# Pin) 8/- W21	9/- 6A60	G 10/	6 68A7	8/- 14H7 1	2/- 70LY 8/6 71A	8/- 9002 8/- Barreter	12/3
CYI	16/6		5/- H		18/- 1	P220	9/- QP21	6/-, U	76	6/- (7 Pin)	12/- 6A80	GT 8/	/- 68C7 /6/68F7	7/=(14N5 L	2/6 75 3/6 76	8/- Barreter	8
	16/6	EK2 EK32	8/6 F		10/- 1	P220A	9/- QP22B	6/- U	81 1	2/- W61	12/- 6AB	5 8/			3/6,77	8/_ 101-GEC 8/-	
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2002	2/01		3/=: F	7 1 20 ]	18/6	722A	7/- QP230	12/6 U	201 1	5/- WT40	15/- 6AC7	7 3/	- 68H7		3/6-79	8/-Philips	14/-
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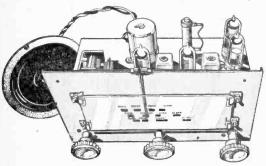
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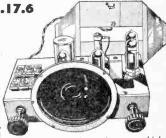
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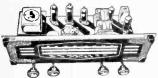
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NOW AVAILABLE A robust cabinet

made from heavy gauge metal which has been specially designed to house the above F.M. Tuner. Beautifully finished in a choice of glossy hammer green, or hammer grey enamel, or black crackle. The front panel (illustrated) has holes for control spindles, and apertures for tuning dial and magic eye. PRICE 25/= P. & P. 1/9. (Front panel only 10/6, P.P. 9d.).

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a low level.

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Modern AC/DC chassis with printed circuit and ferrite rod aerial. Although not completely built, the main components are mounted. L. & M. wave coverage. 4 valves (UBF89, UCL83, UCH81, UY85). Everything supplied except valvas and cabinet. With speaker and simple £3.6.6 plus 3/6 p. & P.

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3 I.F. Transformers, one oscillator coil, one driver transformer, and wound ferrite aerial (Med., Long and aerial coupling) 28/6 complete, post 1/4, 6 transistor printed circuit board to match 8/6, post 9d. Circuit diagram 1/6 extra.

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50 mixed P.F. Condensers and 50 mixed Resistors. An assortment of useful valves. All popular sizes—all new—a must for the serviceman and constructor 10/- P. & P. 1/-

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A first class 2 wave band transistor superhet in kit form.

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AT LAST-A COMPLETE F.M. RECEIVER IN K!T FORM!

Specially designed with the home constructor in mind, this kit enables the construction of a completely self-contained V.H.F., receiver, at fraction of the normal cost of comparable equipment.
This is basically a quality selfpowered F.M. tuner plus 2
separate audio amplifier stages,
and output transformer and spaaker.

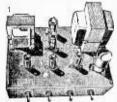
- # F.M. Tuning Head by famous maker.
- ★ Guaranteed Non-drift.
- \* Permeability Tuning.
- ★ frequency coverage 38-100
- ★ OA81 Balanced Diode Output. ★ Two I.F. Stage and Discriminator.
- ★ Self powered using a good quality mains transformer and
- valves used ECC85, two
  EF80's, ECL82 and EZ80 (rectifier).
- # fully drilled chassis.
- # Good quality speaker.
- \* Wall designed output transiormer. \* Attractive maroon and gold
- glass dial. \* Two output stages (using ECL32).
- ★ Everything supplied, down to the last nut and bolt.
- Compact siza.

\* All parts sold separately. OUR PRICE £6.19.6 Plus 416



# HIGH STREET, MERTON, S.W.19

# WATT HI-FI AMPLIFIER



A kit designed to meet the exacting requirements of the audio enthusiast, yet remain within the price range of the average construc-tor. A stylishly finished monaural amplifier with an output of 14 Watts from 2 EL84's in push pull. Super reproduction

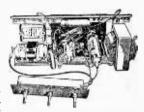
of both music and speech (Frequency response ±3dB c/s-60 Kc/s with negligible hum.) Separate inputs for mike and gram allow records and announcements to follow each other and Technology ments to follow each other and make this amplifier ideal for ments to follow each other and make this amplifier ideal for small halls, youth clubs, etc. Fully shrouded Ultra Linear output transformer (to match 3-150 speaker), and fully shrouded mains transformer (these alone are worth over £3.10.0). 2 independent volume controls, and separate Bass and Treble controls are provided. Treble controls are provided, giving good lift and cut. Valve line up 2 EL84's, ECC83, EF86 and EZ80 rectifier. All parts down tine up 2 ELO3 5, ECC63, FOO and ELO3 FECTIONER. All pair 8 down to the last nut and bolt, including valves, knobs, heavy gauge metal chassis finished in glossy hammer green enamel, mains and output transformers finished to match.

P. & P. 6 66 (simple instruction booklet 1/6, free with kit).

ONLY £6.19.6

## QUALITY RECORD PLAYER AMPLIFIER KIT

A top quality record player amplifier in kit form. This amplifier (which is used in a 29-gn, record player) has a printed circuit and has an internal fully smoothed power supply (input AC/



DC Mains) using a mains dropper and contact cooled rectifier. A flying panel is supplied accommodating BASS, TREBLE AND VOLUME — ON/OFF controls. 2 valves (UL84 and UF89) and linear output transformer give crisp reproduction from all records at 4 watts. Our price for the complete kit of parts (including valves) ONLY plus P. & P. 6/6. Simple instructions I/6. (Free with kit).

#### **TABLE** RADIO SUPER CABINET

A very fortunate purchase allows us to offer this quality table radio cabinet for only 18/6 (this cabinet cost the manufacturers 35/each to make).. The



positions of the controls make it ideal for housing our 6 TRANSISTOR SUPERHET KIT described Beautifully finished in walnut and opposite. Plus 1/6 OUR PRICE tygan. P. & P. ins.

#### SUPER STEREO MK. II

A kit of ready-built units only requiring interconnection. Comprising two midget 3W amplifiers, push button switch, transformer, control unit (bass, treble and vol.), power pack, two speakers, indicator light valves (ECL82, EZ80 range), and comprehensive instructions.





E.M.I. 4-speed Player and P.U.



8åin. turntable. Low flutter performance 209/250V shaded motor with tap at 80V for ampli-fier valve filament if Turnover required. LP/78 head.

PRICE 8916 Plus 4/6 P. & P.

WE HAVE 20,000 IN STOCK—ALL AT BARGAIN PRICES. See our list in December "Practical Wireless", write, phone or call for your requirements Don't miss our bargain OBSOLETE VALVE LIST—turn back to page 878

SPECIAL OFFER ... 6 TRANSISTOR RADIO



transstor 2 wave band superhet chassis. Ideal for portable or table radio. All parts including transistors, ferrite aerial, printed circuit, etc., but EXCLUDING speaker and cabinet.

Few Only.

Simple instructions 1/6 (Free with kit).

SPECIAL OFFER 54-in LOUDSPEAKER SILKS Heavily woven in ivery and gold. Original price 35'- per yard length. OUR SPECIAL PRICE, 13'6 per yard length. TAPE DECKS

B.S.R. Monardeck (single speed) 3\frac{1}{2}\text{in. per sec., simple control, uses 5\frac{1}{2}\text{in. spools. } £7.5.0, plus 5/6 carr. and ins. (tapes extra). COLLARO STUDIO DECK £10, plus 5/6 carriage and ins. (tapes extra)

A 5 valve HI/FI amplifier with switched stereo/monaural operation. Output 3 watts per channel, provision for bass and treble speakers on each. Volume and tone controls fitted both channels. All housed in stylish blue/grey metal case, with gold finished knobs and \$9.19.6 Plus 4/6 OUR PRICE ONLY 5/6 remainings. \$9.19.6 P. & P. 1/-.

HI/FI STEREO
MONAURAL AMPLIFIER
TRANSISTOR SWITCH

В	ranc	new	indi	vidually	_	I PEN65	6/6	UU9	5/6	4AC7	31	· CONTRO	T 411				
						PEN22			5/6 6/-	6AC7	3/- 3/6	6SN7G			6/-	7193	1/9
, c			-	ranteed	4	PEND		UY85	6/6	6AG7	3'6 6'-	6SQ7	61-		6/- 8/-	6475	5/-
	V	AL	V	FS		1360			3/6	6AJ7	4/3	6V6G	5/6	76	5/-	8013A 8020	25/-
						PL81	9/-	VP4I	5/6	6AK5	5/-	6V6GT		77	6/-	9001	61- 416
AC5PE					9/_	PL82	8/-		4/-	6AK7	8/-	6X4	5/-	78	7/-	9001	5/6
AL60	41- 61-		1/6		22/6	PL83	7/9		8/-	6AM6	6/3	6X5GT		80	6/3	9003	6/-
AL6U AP4	4/-		3/9   8/-		6/6	PT15	10/-			6AT6	5/-	6Y6G	8'-	82	8/-	9004	4/-
AR8	5/-				5/ <sub>-</sub> 3 8/-	PT25H		VR 150/3		6AQ5	7'-	6Z.4	8/-	8V3	12/-	9006	4/-
ARDD.					8/-	PVD7	7/6	VT4C	25/-	6BA6	6/-	7B7	7/6	84	3/-	Cathe	-
ARP3	3/-				8/-	PX25	19/-	VU111	6/-	6B8	5/6	7C6	7′-	85A3	15/-	Ray T	
ARP4	3/6		8/-		3/6	PY83	7/3	AX3138	3/3	6B8G	2/6	7C7	6/6	89	6/-	5BPI	35/-
ARPI2	2/9	EC70	10/-	EZ40	71-	PY80	6/9	W3138	7/-	6C4 6C5	3/6	7H7	7/3	210LF	. 3/-	5CP1	42/6
ARP21	3/6		10/-	EZ4I	6/9	PYBI	7/-	Y63	5/-	6C6G	6/- 4/3	7Q7 7V7	71- 51-	210VPT		5FP7	45/-
ARP24	4/6			EZ80	6/6	PY82	8/-	Y66	8/-	6C8G	5/-	7Y4	6/-	7 pin		7BP7	40/-
ARP34	5′6				6/9	QP21	6/-	Z3i	61-	6D6	4/6	7Z4	6/6	250TH 274B	£9 3/-	12DP7	
ARTH2					10/-	QP25	5/3	IA3	3/-	6F6	71-	8D2	2/6	350B	8/-	CV1596	
ATP4	2/9					QS75/2	0 6/9	IA5GT	5/-	6F6G	4/-	9D2	3/-	393A	15/-	(091)	55/-
AUI AU4	5/- 5/-				91-	Q595/I		1C5GT	716	6F8G	6/6	12A6	5/-	705A	17'6	VCR138	
AW3	4/-		8/6		6/-	Q\$108/		ID8GT	6/-	6F12	4/6	12AH7	71-	715B	97/6	VCR139	
AZ3I	8/-					QV04/7		IE7G	7/6	6F17_	7/6	12AT7	5/6	717A	8/6	VCRX2	35/-
BL63	61-			KF35	12/6	QV05-2		IG6GT		6G6G	3/-	12AU6	91.	801	61-	(with so	
BS4A	5/6		8/-	KRN2A		R3 R3/10	8/-	ILD5	3/6	6H6M	2/-	I2AU7	6/-	803	22/6	ing coil)	
BT45	40/-	ECL82	9/-	KT31	8/-	R10	12/6	IR5	6/-	635	3/6	12AX7	7/-	804	55/-	Phot	
BT83	22/6		7/3	KT32	8/-	REL21	12'6 25'-	1S5 1T4	5/9 4/-	6J5G	3/-	12C8	3/-	805	30/-	Tube	
вт9в	25/-	EF36	3/6	KT33C	4/9	RK34	2/6	114   W4	61-	6J6 6J7G	4/3	12E1	22/6	807AME		CMG25	
CV54	5/-	EF37A	8/-	KT44	6/3	RX235	10%	2A3	8/-	6K6GT	6/6	12H6 12J5GT	3/6	807BR	5/-	931A	50/-
CV264	35/-	EF39	4/3	KTW62	7/6	5P2	4/-	2A5	8/-	6K7G	2/3	12/3G1		808	8/- 80/-	Speci	
CY31	7/6	EF50	2/6	KTW63		5PI3C	4/6	2A6	7/-	6K7GT	4/9	12K8M	9/-	813	67'6	Valv	
D41	3/3	EF54	3/3	MH4	3/6	SP41	2/6	2034	2/6	6K8G	5/9	12SA7	7/6	815	40/-	2331	45/-
D77 DA30	4/3 12/6	EF55	6/-	MH4I	5/-	5P61	2/-	2D21	61-	6K8GT	8/3	125C7	4/6	816	30/-	3A/1481	
DAF86	8/-	EF70 EF73	4/- 6/-	ML4	4/-	5TV280		2D4A	4/-	6K8M	8/6	125G7	6/6	826	10/-	723AB	45/-
DAF91	6/-	EF80	5/6	ML6 MS/PEN	6/-	5112150	12/-	2X2	4/-	6L5G	6/-	12SH7	3/-	829A	30/-	725A	30/-
DET5	15/-	EF85	6/10	NT37	0,-	5U2150, T41		3A4	5/-	6L6	9/-	12SJ7_	61-	832	15/-	726A	27/6
DF72	7/6	EF86	9/-	(4033A)	10/-	TH41	7/- 8/-	3B7	5/-	6L6G	6/6	125K7	4/-	832A	35/-	931A	50/-
DF91	3/3	EF89	7/9	NU12	5/-	TP25	15/-	3B24 3E89	8/-	6L34	4/6	12SL7	7/-	843	7/6		200/-
DK96	7/3	EF91	3/6	ОВЗ	7/-	TTII	3/-	(889B)	401	6N7G	5/9	12SN7	8/-	866A	12/6	ACT17	75/-
DF96	8/-	EF92	4/6	OC3	5/-	TZ20	16/-	3Q4	6/-	6N7GT	6/-	12Q7GT		872A	35/-	ACT25	40/-
DL92	6/-	EF95	7/6	OD3	5/-	UIT	5/-	3Q5GT	9/-	6Q/G 6R7	8/-	12SR7 15D2	6/-	930	8/-	CV691 KR3	60/- 45/-
DL94	6/-	EL32	3/9	OZ4	5/-	Üİ	5/-	354	5/-	6SA7	6/-	15D2 15R	5/-	954 956	2/-	L57B	30/-
DL96	8/-	EL33	8/-	PCC84	7/-	U27	8/-	3V4	6/-	65C7G	5/6	20A2	7/6	956 958A	5/-		22/6
DX25	9/-	EL35	8/3	PCC85	8/3	U52	5/-	5T4	9/_	65C7GT		21B6	9/-	1616	3/-	VX7110	
E1232 E1323	5/6 25/-	EL41	8/3	PCF80	7/-	UCH42		5U4G	5/-	6SG7	5/-	30	5/-	1619	5/-	WL417A	
E1436	3/6	EL42 EL84	9/-	PCF82	8/-	ULII	5/-	5V4G	8/-	6SH	5/-	35L6GT		1625	6/-	Curre	
E1524	6/6	EL84   EL85	7/6	PCL82 PCL84	8/6	UL12	5/-	5Y3GT	6/-	6SH7	4/6	35T	30/-	1626	4/6	Product	
EA50	1/6	EL91	7/6	PEN25	91-	UL41	7/-	5Z3	8/6	6SJ7GT	5/9	35Z4GT		1629	4/6	3J/170/E	
EABC80		EM80				UL84	7/6	5Z4G	8/-	6SK7	5/3	37	4/-	4120	4/-	3J/192/E	
AND	4AN'	V OTH	EBSI	PI STOC	31-1	UL85	7/-	6AB7	4/- 1	65L7GT	6/6	38	4/-	6064			37.10
A	belo	w 10/-, I	1. P. &	P 2/6 046	10/-	ICLUDI	NG C	ATHOR	DE RA	AY TUBI	ES AL	ND SPEC	CIAL	VALVES	. All		
				C221 TEC		· Orders	Over L	.3, F. & F. T	ree.	C.O.D. 2	'6 extr	a. Overse	eas Pos	stage extr	ra at co	ost.	
1		L MAN				BRAN	1D N	IEW OR	RIGIN	IAL SPA	ARF	POW	FK S(	UPPLY (	UNIT	• Input	200/
FIELD	TEL	-EPHO	NE 1	TYPE "	"L"	I. PAF	₹TS_F	OR ARE	38 RE	CEIVER	S	250 v. /	A.C., 3	50 cycles.	Outpu	t: 1, H.T.	.280/
Excellen	t gua	aranteed	condi	ition, £5.	-5.0	II.F. II	ransto	rmers.	lst, 2	nd, 3rd,	4th	40m A	Ouma	smoothe	d; Z, M	. 1. 150/20	J0 v.
per pair.	, carri	age paid.				(ior ty	pe U),	, 12/6 eac	:h or	complete	set	4 amo	DC	ive earthe	(0,000	L. 1. 10/4	.5 v.

B.P.5 TRANSRECEIVERS. Specially B.P.5 TRANSRECEIVERS. Specially built for Parachutists during the war. Receiver superhet Transmitter crystal controlled. C.W., and phone. 2-8 Mc/s. 829 valve as output. 60 w. on C.W. 15 w. on microphone together with mains power pack 120/220 v. Two rotary converters to work from 12 v. battery, microphone, key and dipole aerial. Price £15. Carriava 30/s.

Carriage 30/-. RECEIVER TYPE BC342. 110 v. A.C. 1.5-18 Mc/s. £22.10.0, carriage 30/-.

RECEIVER TYPE BC312. As above but 12 volt battery. £22.10.0, carriage 30/-. R109 RECEIVER. Covering 2-8 Mc/s 6 v. D.C. with set of spare valves and carrier,

Brand new in original packing case, 66.18.0, including delivery in U.K. VIBRATOR U.NIT. 12 v./160 v. 35 mA, Exceedingly well filtered and smoothed. Excellent for car radios. Including one 6X5G valve and vibrator 17/6. P. & P. 7/-. MARCONI SIGNAL GENERATOR.
TFI44G. 85 kc/s, 25 Mc/s. Made up to
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SPECIALLY BUILT POWER PACK

for TC5 Receiver. 230 v. A.C. mains, in-cluding 6X5GT valve, £3,10,0. Carr. 5/-TELEPHONE HANDSET, standard G.P.O. type. New 12'-, P. & P. 1/6.

VACUUM CONDENSER. 32,000 v. 50pf. 12/6 P. & P. 3/6.

AR 88's. Completely rebuilt with new PVC wiring. Type "D" £75; Type "L" F£70.

of 6, 60/-.

I.F. Transfs. Crystal Load, 12/6 each.

Plates escutcheons (for D and LF), 15/- each.

Dials (for type D), 10% each. Logging Dial (for D and LF), 10% each. Filter Chokes (for D and LF), 22% each. Output Transformers (for LF), 30% each

Antenna Trimmers (LF and D), 2/6 each. Filter Condenser 3 x 4µF, £2.10.0

Condenser 3 x 4μг, ε2.10.0 Condensers: 3 x .25μF (D and LF), 2/6 each. 3 x .01μF (D and LF), 2/6 each. RF Antenna Inductors (D and LF), 7/6 each.

Mains Transformers (LF), £3 each.
Small Trimming Tool, 71-.
Small Mica Condensers, val values, 1/6 each.

Instruction Manual for AR88D, 61.

19 SET OWNERS. To increase output of your set 6 to 10 times use RF Amplifier No. 2 with built-in rotary converter for 12 v. input. Four 807 valves output. Simple connection with transmitter. Fully tested condition, £9.15.0, including necessary connectors and instructions Carriage and packing 15/-.

P.C. RADIO LTD. 170 GOLDHAWK RD., W.12 Shepherds Bush 4946

40mA (positive earthed); 3, L.T. 18/25 v, 4 mp. D.C. smoothed (negative earthed), 2 relay switching, H.T. & M.T., safety switch fuses on A.C. and all D.C. Two 523 for H.T., one 6X5 for M.T., Selenium rectifier for L.T. Ideal for Ham transmitters. Weight 45 lb. Dimensions 14 x 8½ x 18in. Price £12.10.0 including valves. P. & P. 25/-.
R209 RECEPTION SET. A 10-valve High-Grade Super Horsed-dia 9. Services.

High-Grade Super Heterodyne Receiver with facilities for receiving R/T (A.M. or F.M.) and C.W. Frequency I-20 Mc/s. Hermetically sealed. Built on miniature valves and incorporating its own vibrator valves and incorporating its own vibrator power supply unit driven by a 6 v. battery (2-point connector included). The set provides for reception from rod, openwire or dipole aerial with built-in loud-speaker or phone output. Overall measurements: Length 12in, width 8in, depth 9in. Weight 23 lb. In as new, tested and guaranteed condition £23,10,0,0 including special headphones and supply including special headphones and supply leads. Carriage £1.

SUPPLY UNIT RECTIFIER No. 21.

Fully sealed enabling all sets built for 6 v. (R209, R109, etc.) to work from A.C. mains. Input 90-260 v. A.C. (Taps at 10 v. intervals). Output excellently smoothed up to 10 amps with meter indicating revact output voltage. Measurements: 12 x 9 x 10in. Price £8. Carr. and p. 15/-. FAMOUS T.17 CARBON MICRO-PHONES. £2.5.0. Post & packing 3/6. CARBON INSET MICROPHONE, CARBON INSET MICROPHONE, G.P.O. Type 2/6. P. & P. 1/6.

igned by MULLARD-presented by STERA

#### COMPLETE KIT OF PARTS **MULLARD "5-10" MAIN AMPLIFIER**

For use with the MULLARD 2-valve pre-amplifier with the MULLARD 2-valve pre-amplifier with undistorted power output of up to 10 watts is obtained. We supply SPECIFIED COMPONENTS AND NEW MULLARD VALVES, including PARMEKO MAINS MULLARD VALVES, including PARMEKO MAINS TRANSFORWIER and choice of the latest Ultra-Linear PARMEKO or the PARTRIDGE Output Transformer. COMPLETE KIT OF PARTS \$10.0.0 (PARMEKO Output Trans.). Alternatively we supply ASSEMBLED and TENTED. \$11.10.0 INCORPORATING PARTRIDGE OUTPUT ASSEMBLED and TENTED.

#### **MULLARD'S PREAMPLIFIER** TONE CONTROL UNIT

Employing two EFEB valves, and designed to operate with the MULLARD MAIN AMPLIFIERS, but also perfectly suitable for other makes.

PRICE COMPLETE \$6.6.0 ASSEMBLED AND TESTED \$8.0.0

KITS OF PARTS:

Supplied strictly to MULLARD'S SPECIFICATION and incorporating:

Supplied strictly to MULLARD'S SPECIFICATION and incorporating:

Input for Crystal Pick-ups, and variable reluctance magnetic types,

Input (a) Direct from High Imp. Tape Head, (b) From a Tape Amplifier or Pre-Amplifier.

Sensitive Microphone Channel.

Wide range BASS and THEBLE Controls.

COMPLETE MULLARD "5-10" AMPLIFIER

The popular and very successful complete "5-10" incorporating Control Unit providing up to 10 watts high quality reproduction. Only Specified Components and new MULLARD VALVES are supplied including PARMEKO MAINS TRANSFORMERS and choice of the latest PARMEKO or PARTRIDGE ULTRA-Linear Output Transformers.

KIT OF £11.10.0 OR ASSEMBLED £13.10.0 PARTS £16.0 12 months at 177. Dep. £2.6.0, 12 months at 177. Dep. £2.14.0 12 months at 19/10 ABOVE Incorporating FARTRIDGE OUTPUT TRANS. £1.6.0 extra



COMPLETE MULLARD "3-3"

THE DEAL AMPLIPIER FOR A SMALL HIGH QUALITY INSTALLATION PROVIDING EXCELLENT REPRODUCTION OF THE WATTS OUTPUT COMPLETE RIT \$7.10.0 OR ASSEMBLED \$8.19.6 OF PARTS (OUTPUT) and TESTED CATTON including Mullard valves and a PARMEKO OUTPUT TRANSFORMER.

STERN'S INTER-COMM **BABY ALARM** 

A small versatile Unit employing the new MULLARD ECL& valve and designed to provide two (or three) way conversation up to extreme distances. Operates from A.C., mains 200 to 250 Volts.

PRICES . . . MASTER UNIT and ONE EXTENSION

KIT OF PARTS **\$6.17.6** ASSEMBLED AND TESTED **\$8.0.0** Consists of a MASTER UNIT, size only 8t x 5t x 6in, and ONE EXTENSION (a second extension may be added to any time). The Master Unit incorporates switching and power supply and with the chassis completes located from the mains is operated in absolute salety. Cases covered in quality leatherette.

## ARMSTRONG RAD!OGRAM CHASSIS

FULL RANGE IN STOCK, please enclose S.A.E. for descriptive leaflets

STEREO 12 (MK. 2)

(Illustrated)

£44.15.0 Deposit £9.0.0, 12 months at £3.5.7

The most complete chassis ever produced, combines and FM Tuners, a Stereo Control Unit and two High Fidelity Amplifiers in one compact unit, provide a total of 16 watts for both mono cond stereo. Other leatures include: inputs for tape recording, play back, pick-ups and stereo radio (should this come about); separate wide range bass and treble controls and balance control.

#### STEREO 55 £33.15.0

Deposit £6.15.0, 12 months at £2.9.6 A jumor version of the Stereo 12 Mk. 2 providing ten waits output, five watts from each amplifier and covering the VHF and Medium wavebands.

#### COMBINED ORDER PRICE REDUCTIONS

(a) The KIT OF PARTS to build both the "5-10" Main Amplifier and the 2-valve PRE-AMP CONTROL UNIT H.P. Dep. 23.7.0 and 12 215.15.0 months at 21.2.9... the 2-stage PRE-AMP both ASSEMBLED and TESTED H.P. Dep. 23.16.0 and 12 218.18.0 months at 21.7.8... unit PARTRIDGE O/PUT TRANSFORMER 21.6.0 extra

RECORD PLAYERS

The Latest Models are in stock, many at reduced prices.

many at reduced prices.
Send S.A.E. For Hustrated Leaflet.
THE NEW GARRARD "AUTOSLIM" 4-speed Autochanger \$8,10.0
with Crystal Pick-up ....
COLLARO "JUNIOR" 4 SPEED
SINGLE RECORD PLAYSINGLE RECORD PLAYPick-up Carriage and Insurance 5/Above Pick-up separately for \$1.88

The NEW COLLARO C60 4-speed Autochanger unit with \$7.19.6 Single

The E.M.I. 4-speed Sin Player with crystal Pick-£6.9.6 . . . . . . . . . . . .

MODEL UA14. 4-speed 

GARRARD MODEL TA/MRII 4speed Player fitted high
output Crystal Pick-up.

GARRARD MODEL RC210. Autochanger 4-speeds. High £10.10.0
output. Crystal Pick-up..

Carriage and Insurance on each above 5/- extra.

#### CASH OFFER SPECIAL

£3,17.6

This very attractive PORTABLE AM-PLIFIER CASE together with a good quality GRAM AMPLIFIER and a matched P.M. SPEAKER. ALL for ONLY **\$8.7.6** (Plus 7/6 Carr & Ins.).

The Amplifier consists of a 2-stage design incorporating 3 modern B.V.A. valves and has separate BASS and TREBLE CONTROLS.

The Portable Case will also accommodate almost any make of Autochanger and is attractively finished in Mushroom Grey Rexine. WE ALSO SUPPLY SEPARATELY 44.2. (2) The 2-stage (plus Rectifier) AMPLIFIER 2.174 £4.2.6

(b) The PORTABLE CARRYING CASE

(c) 61in. P.M. SPEAKER 18/9. Carriage and Insurance 4/- extra.

#### MULLARD FOUR CHANNEL MIXER UNIT

Self powered with Cathode follower output. Incorporates Two Imputs for MICROPHONES One for CRYSTAL PICK UP and a lourth for RADIO or TAPE 88.80

Complete Kit of Parts

Complete ALO Parts
Assembled and Tested
\$10.0.0

MODEL 1.L. one microphone Input matched for moving coll or Ribbon Mike. 21.17.0 extra.

JUBILEE MK. 2 £31.15.0

Deposit £6.7.0 12 months at £2.6.7 A Hi-Fi mono chassis giving eight watts push-pull output and covering VHF, medium and long bands. Tape recording and play

Deposit £4.15.0 12 months at £1.14.10 £23.15.0 An AM/FM chassis providing 5 watts output and covering the full VHF and medium wavebands. Tape recording and playback inputs.



There are no better

Recorders on the market-if you can't call and hear them send criptive leaflet. EACH MODEL INCORPORATES
THE MODEL HFITRS
MK.II TAPE AMPLIFIER
(Described below)

Each price quoted pro-vide for the COM-PLETE RECORDER

including CRYSTAL MICROPHONE and

1,200ft. Spool of Tape.

Tane

value-for-money



# tern'.

## For truly "Hi-Fi" Recordings

MODEL CR3/S Incorporates the COLLARO "STUDIO" TWIN TRACK 3-speed Deck, operating at 14-in. 3tin. and 71in. speeds.
H.P. Terms: Deposit £7.18.0 and 12 months at £2.17.11.

£39.10.0

MODEL TR3/MK.VI Incorporates the New TRUVOX Mk. VI TWIN TRACK 2-speed Tape Deck operating at 34in. and 74in. speeds. H.P. Terms; Deposit 28.16.0 & 12 months at £3.4.7.

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MODEL HFG/2R PORTABLE TAPE RECORDER (Orlginal Price £33.0.0) FOR ONLY 22 gns.

TUK UNLY 22 gns.

H.P. Dep. £4.14.0. 12 months at £1.13.9. (Carr. and Ins. 10)-etra).

Incorporates THE LATEST GARRARD "MAGAZINE" TAPE DECK and a High QUALITY ABSENCE OF THE GARRARD TO THE GARRARD TO THE GARRARD TO THE GARRARD TO THE GARRARD TO THE GARRARD TO THE GARRARD TO THE GARRARD TO THE GARRARD TO THE GARRARD THE MAGAZINE and 4In. SPOOL of DOUBLE PLAY TAPE. Comprised Target and 4In. SPOOL of DOUBLE PLAY TAPE. Comprised to the total playing time. Truly "Portable" weighs only 22 lb. Dour 10 mins. playing time. Truly "Portable" weighs only 22 lb. Outstanding leatures are excellent performance and simplicity of operation.

ADD "HI-FI" TAPE RECORDING TO YOUR EXISTING AUDIO INSTALLATION WITH MULLARD TYPE "C"
TAPE PRE-AMPLIFIER—ERASE LIVE"

EXISTING AUDIO INSTALLATION WITH
MULLARD TYPE "C"
TAPE PRE-AMPLIFTER—
ERASE UNIT
For "Hi-F" link to add full tape recording facilities to High Fidelity home installations. Incorporates FEROXCUBE POT CORE PUSH PULL OSCILLATOR and 3-speed treble equalisation by FEROXCUBE POT CORE INDUCTOR FOR WEARITE-COLLARO-TRUVOX OR BHENELL TAPE DECKS. Includes separate power Supply Unit.

arate power Supply Unit.

KIT OF PARTS

£14.0.0 Deposit £2.16.0.

£17.0.0 12 months at £1.0.6

Excluding power unit £11.15.0 and £14.10.0 respectively.

"SPECIAL COMBINED ORDER" PRICES OR ASSEMBLED
Deposit £3.8.0
£17.0.0 12 months at £1.4.11

"SPECIAL COMBINED ORDER" PF
The COLLARO "Studio" Deck with the Model
"C" Preamplifier and POWER SUPPLY UNIT
ASSEMBLED AND TESTED
Deposit £5.180. 12 monthly payments of £2.3.3
As above but the TYPE "C" Unit and POWER
UNIT supplied as COMPLETE KIT OF PARTS
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Deposit £9.4.0 and 12 months at £3.7.6
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OF PARTS
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As above but the Model "C" PREAMPLIFIER
and POWER UNIT supplied as a COMPLETE KIT
OF PARTS
Deposit £9.12.0. 12 monthly payments of £3.3.1 (b) £26,10,0 (c)

£35.0.0 (4)

£31.10.0 (e) £46.0.0

(1) £43.0.0

OF PARTS.

Deposit £3.12.0. 12 monthly payments of £3.3.1

The WEARITE MODEL "" DECK with ASSEMBLED and TESTED Model "C" PREAMPLIFIER AND POWER UNIT incorporating

WEARITE HEAD LIFT TRANSFORMER. Etc.

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(Carriage and Insurance on above is 10/- extra.) £56.0.0

HF/TR3 MK.II TAPE AMPLIFIER

(Mullard Type "A". 'design')
A very high quality Ampilifer incorporating 3-speed treble equalisation, by the latest FEROXCUBE POT CORE INDUCTOR, FOR COLLAROTR UV OX 'S BR E NE L L WEARITF Tape Decks, has GILSEN Output Transformer, Includes separate Power Supply Unit.



THE 'ADD-A-DECK'

THE 'ADD-A-DECK'
Incorporating
GARRARD "MAGAZINE"
TAPE and the MATCHED
MODEL HP/GEP
PRE-AMPLIFIER
Supplied on ONE CHASSIS (as illustrated) READY
18 Gns.
(Carr. & Ins. 10)- extra.)
Price includes Garrard Magazine
and a 4in. Spool Double Play Tape
H.P. Deposit & 3.16.0. and 12 months at £1.7.8.
Provides complete tape recording facilities and
designed to operate through the pick-up sockets of
the standard type of RADIO RECEIVER, or an AMPLIFIER,
from which really first class reproduction is obtained. It consists of a Twin Track Deck connected to the Pre-amplifier and operates at 3/in/sec, speed providing up to 1 hr. 10 mins. playing time.

# BUILD A HIGH FIDELITY



TAPE RECORDER LIKE THIS for £35.0.0

Deposit £7.0.0 12 months at £2.11.4

FOR THIS WE SUPPLY

Complete Kit of Parts to Build the HF TR3 Tape Amplifier. The New Collaro "Studio" Tape Deck, Portable Carrying Case (as illustrated). Rola/Celestion 10 x 6in. p.m.

£42.0.0

£56.0.0

# Rola/Celestion 10 x 6in. p.m.

# ACOS Crystal Microphone and 1.200f. Spool E.M.I. Tape.
Loudspeaker.

Alternatively for those who prefer another make of Tape Deck.
we will supply precisely as above—but in place of the Collaro
"Studio" Deck. We will include:
The Truvox Mk. VI Deck
The Truvox Mk. VI Deck
Complete KIT to build the HFTR3 Amplifier
Logether with the COLLARO "STUDIO" DECK
As above but with the HFTR3 supplied ASBEBLE and TESTED BYTED (d)

£45.10.0

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KIT OF £13.13.0 H.P. Deposit £3.8.0 and OR PARTS £13.13.13.0 H.P. Deposit £3.8.0 and OR

ASSEMBLED £17

# Stereophonic Sound by Stern's

#### THE "STP-1" STEREO TAPE PREAMPLIFIER DESIGNED TO OPERATE WITH

• TROVOX MR.VI TAPE DECK incorporating the latest t-TRACK MINI-FLUX TAPE HEADS.

PUSH PULL OSCILLATOR

4-SPEED EQUALISATION FERROXCUBE OSCILLATOR TRANSFORMER

SENSITIVE METER FOR SIGNAL LEVEL SEPARATE GAIN CONTROLS IN EACH CHANNEL

MULLARD VALVES

• BRENELL ME.V TAPE DECK Incorporating similar 1-TRACK MINIincorporating similar



• COLLARO "STUDIO" TAPE DECK incorporating the latest 1-TRACK incorporating the latest REUTER TAPE HEADS.

OVERALL SIZE CASE 134 x 3in, FRONT PANEL (Choice of Black or White) 14 x 34in.

26.0.0

including separate Power Supply Unit. Deposit £5.4.0, 12 months £1.18.2.

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#### THE "STP-1" PREAMPLIFIER is offered

WITH TAPE DECKS AS FOLLOWS:

TRUVOX Mk.VI 4-TRACK MODEL...
Deposit £9.8.0, 12 months at £3.8.11. £47.0.0

 BRENELL Mk. V 4-TRACK MODEL.....

Deposit £13.0.0, 12 months at £4.15.4. £65.0.0

• COLLARO "STUDIO" 4-TRACK MODEL.......
Deposit £8.12.0, 12 months at £3.3.1.

STEREOPHONIC RECORD PLAYER UNITS MICROPHONES & TWIN LOUDSPEAKERS ARE AVAILABLE FROM STOCK

#### MULLARD'S "10 PLUS 10"

#### STEREO POWER AMPLIFIER

A high fidelity design based on the famous Multard "5-10". Provides up to 10 watts (per channel) Supern reproduction. Frequency response list to within 3 diversity of the first of the fir

£21.0.0

Deposit £6.0.0, 12 months at £2.4.0.

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D) A complete KIT of PARTS for both Units...... Deposit \$5.4.0, 12 months at £1.18.2

!! A BARGAIN!! We are able to offer BRAND NEW and FULLY GUARAN-DEED-TRUVOX MK. VI TAPE DECKS. List Price £18.18.0 £26.5.0 for Deposit £3.16.0 and 12 months at £1.7.8. (Carr. & Ins. 7/t extra) A twin track model operating on 31 and 74in./sec. speeds and incorporating pause Control and Rev. Counter.

Dept. P.W. 109 FLEET ST., LONDON, E.C.4 Telephone FLEET STREET 5812/3

## THE MULLARD "10+10" STEREO AMPLIFIER

(described below) with the "STP-1" PREAMPLIFIER and one of the TAPE DECKS provide a COMPLETE STEREOPHONIC INSTALLATION.

WE OFFER

£67.0.0

£85.0.0

• As above with COLLARO "STUDIO" DECK......
Deposit £12.12.0, 12 months at £4.12.4. £63.0.0

Please enclose S.A.E. with all enquiries.

#### DUAL CHANNEL PREAMPLIFIER

Incorporates two Muliard 2-vsive Preampilitiers combined into a Single unit enabling it to be used for both STEREDI'IIONIC or MONAURAL operation. It is designed primarily to operate with our range of MULLARD MAIN AMPLIFIERS but will also operate equally well with any make of Amplifiers requiring ar input of 250 mivolts. COMPLETERIT £12.10.0

H.P. £2.10.0 & 12 mths. at 1844

H.P. £3.0.0 & 12 mths. at £1.2.0

£14.0.0

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#### STEREO "TWIN THREE" AMPLIFIER with specially designed

PORTABLE CASE

A most compact portable design of the possible of TWIN CHANNEL AMPLIFIER based on the latest design by MULLARD IT also programme to grade Out, but Iransommers, and the new ando Irrode-Fence and the new ando Irrode-Fence and the new ando Irrode-Fence and the new ando Irrode-Fence and the new ando Irrode-Fence and the new ando Irrode-Fence and the new ando Irrode-Fence and the new ando Irrode-Fence and the new ando Irrode-Fence and the new ando Irrode-Fence and the new ando Irrode-Fence and the new and the Irrode-Fence and Contemporary portable Case in two tone colours. The unique leature of the design is the loudspeaker mounting. Two 8 x 56m.

p.m. elliptica: loudspeakers are separately baffed and mounted in the ind, which is detachable, allowing for each speaker to be individually positioned. A very versatic stereo arrangement lested and guaranteed which can be assembled in the minimum of time.

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EBL31		EF80		FW4/5		PY8I		UF89		354 3V4	7/6			6V6GT		12K8M			3/6
EC90		EF85	7/~	, .		PY82		UL4I	9/_			6CH6 6F6G		6X4		12Q7GT			
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1 OC44, 2 OC45, 1 OC81D, 2 OC81. Only 37/6 set.

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RECORDING of Top TAPE Special Offer Special Offer of Top quality recording tape, 3½in. spool 200ft, 5/3, 5in. spool 600ft, 13/9, 5½in. spool 850ft, 18/6, 7in. spool 1200ft, 23/-, Extraplay tape, 3½in. spool spool 1200it, 23'-. Extra-play tape, 3½in. spool 300ft, 7'-, 5in. spool 900ft. 21'-, 5½in. spool 1275ft, 26'6, 7in. spool 1800ft. 37'6. Empty spools, 3½in., Empty spools, 3½in., 5in., 2/-, 7in., 3/-. 1/6.

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#### HIGH RESISTANCE **PHONES**

Resistance 13/6 ohms. pair.

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All brand new	
2½in. square EMI	.18/6
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with O.P.T	.16/6
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## STENTORIAN HF 1012

10in. die-cast unit, incorporating 12,000 gauss magnet. Handling capacity, 10 watts. Frequency response, 30 c.p.s.-14,000 c.p.s. Bass resonance, 35 c.p.s.

Total price, £5.2.6

## MARTIN

Model C for Collaro Studio Deck. Amplifier 8311/V assembled and tested with 5 BVA valves, controls, switches, transformers, knobs and full instructions. £11.11.0.

Smart 2 tone leatherette covered wooden case and 9 x 5in. high quality loud-speaker, type C6659/V. €5.5.0.

Circuit diagram, full instructions, shopping list, etc., 3/6 ea. Collaro Studio Deck

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UAI4 Four speed motor, Magidisc selector enabling 7, 10 and 12in. records to selected automatically crystal cartridge. Attractively styled in cream and grey. Suitable for A.C. mains, 100/125 v. 50 cycles. Unit plate. £6.19.6 \* Garrard Autoslim
The latest 4-speed automatic Record Changer from Garrard-Autoslim, €9.0.0.

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4-speed Turntable Unit complete with Pickup.
An extremely reliable and inexpensive Unit inexpensive Unit suitablefor Record Players and Radiograms; a heavy 86in, dia. Metal Turn-table with low flutter performance, 5-position switch, 4 speeds and off, ivory finish with red with red T/T mat. 89/6.

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D.C. or A.C. Resistance .... Will also measure decibels. Villalso measure decibels of test prods, instruction book and batteries.

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A new version in a re-designed cabinet with carrying strap, complete kit of parts, £7.19.6. Detailed price list available on request.

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A 2-band 6-Transistor Superhet for long and medium waves, 2-colour case,  $10 \times 7\frac{1}{2}$  x  $3\frac{1}{2}$  ins. £10.19.6. Send for comprehensive manual and parts list, 3/6.

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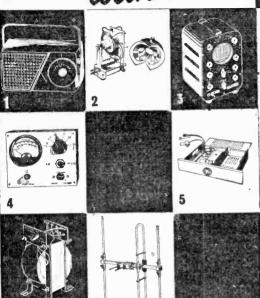
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# BARGAIN



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1. 3-TRANSISTOR POCKET RADIO with MINIATURE SPEAKER, FERRITE ROD, and 2 GERMANIUM DIODES. The only 3 transistor radio available at the price. Build it in 1 voining! Tunable over M/L waves. Complete with easy-to-foliow 27(4), P. 6. P. 2/6, (All parts available separately.)

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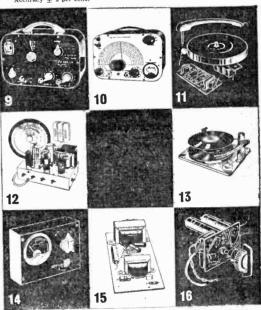
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P. & P. 4/-.

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- BATTERY RECORD PLAYER AND AMPLIFIER. 45 r.p.m. "Star" motor "Acoa" crystal pick-up, 3 transistor push-pull amplifier complete with transistors. Output 500 milliwatts, 49/8. P. & P. 4/-.
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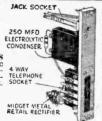
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A complete set of parts for the construction of a stereophonic amplifier giving 5 watts high quality output on
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250-0-250 v. 200 mA. 6.3 v. 4a, 5 v. 3a. 35/9
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250-0-250 v. 200 mA. 6.3 v. 4a, 5 v. 3a. 35/9
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Comprising A12 kit, 2
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FICK-UF ARMS complete with Hi-Fi turnover crystal head. Acos GF54. Limited number brand new, perfect at approx. half price. Cnly 29/11.

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Jason FMTI V.H.F/FM Radio Tuner design. Total cost of parts including valves, Tuning dial, Escutcheon, etc. £6.19.6.

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0,1/1,000 v., 1/9; 0,1/850 v., 98; 0,0/12,000 v.

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			5in.	2/-
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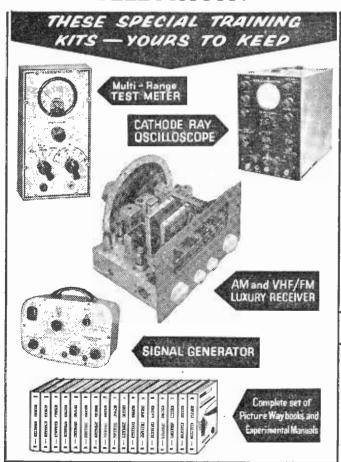
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# Practical Wireless

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# Wired Wireless and Commercial Radio

T seems only a short time ago that the "wired wireless" was as prominent a topic for conversation as 625-line TV is today, and yet little has been heard of it since. Surely the idea deserves much greater attention and, in fact, the time is fast approaching when a practical application of this form of transmission, in its fullest sense, must be found. Sending a radio signal over a wire is, in fact, what is meant by the term "wired wireless", and one very well-known application of this is the employment of voice-operated carrier systems, over coaxial cables, on the trunk telephone systems. By this means hundreds of simultaneous telephone conversations can be carried on a single cable, without interaction.

A really practical development of this form of radio, would be that in which the normal house wiring systems, which after all, are in effect "networked" and serve the majority of homes in the country, could be used to carry not only normal radio programmes, but commercial or sponsored radio, as well as television on various channels. It would not be a very great step to make these systems of such a type that coin-operated selecting devices could be incorporated to provide not only revenue but various forms of 'exclusive' programmes. Both the telephone system and the lighting services in this country are operated on a national basis, and therefore there would be no difficulty about using the existing wiring. The actual development of a technique which would permit the use of all forms of broadcasting, including what we now know as V.H.F., or F.M., together with television, should not present insurmountable difficulties. It would, of course, limit programmes to each country and perhaps render unnecessary such developments as resulted in the superhet receiver. It would also remove many difficulties, not the least of which would be the fringe area, the need for interference suppressors, and last, but by no means least, the mass of unsightly decorations on our roof tops. (The forthcoming television development on Bands IV and V will lead to greater congestion on our roof tops and it appears highly probable that the Pilkington Committee will recommend some form of "wired wireless" or "carrier wireless" for sound only to enable commercial sound programmes to be inaugurated.)

There may be a limit to the number of transmissions which could be dealt with in this manner, and perhaps the inclusion of television may complicate matters, but surely this is one very good ground for development of radio, and the day must come when radio and television programmes will form part of the domestic service supply systems, taking their place with the electric light, water and other essential services.

MATERIA DE LA COMPANIO DE COMPANIO

Our next issue dated March, will be published on February 7th

# Round the World of Wireless

# POTENTIAL AND CURRENT NEWS

#### **Broadcast Receiving Licences**

THE following statement shows the approximate number of Broadcast Receiving Licences in force at the end of October, 1961, in respect of wireless receiving stations situated within the various Postal Regions of England, Wales, Scotland and Northern Ireland. The numbers include Licences issued to blind persons without payment.

Region				Torai
London				679,407
Home Counties				635 399
Midland North Eastern	• •	• •		463,496
	• •	• •	• •	494,695
North Western	• •			427,159
South Western				374,467
Wales and Border (	Counti	es		218,547
			_	
Total England and	Wales	٠.,		3,293,176
Scotland				361,335
Northern Ireland		• •		114,603
			_	
Grand Total		• •		3,769,108

#### Sweden Orders Eighty-two Transmitters

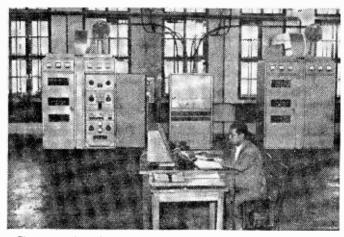
THE Royal Board of Swedish Telecommunications has placed another order for sound and television broadcasting transmitters with Marconi's Wireless Telegraph Company Limited.

The new contract calls for the supply of 21 vision transmitters, 21 sound transmitters, 40 frequency-modulated sound transmitters and a considerable quantity of programme input, paralleling, feeder and ancillary equipment.

The transmitters are intended to augment Sweden's already extensive television and VHF frequency modulated sound broadcasting systems by providing first-class reception in the northern area and in what are at the moment fringe areas throughout the country. Deliveries, at the request of the Royal Board of Swedish Telecommunications, are to be spread over the next four years.

# Transmitter for Satellite Communications Project

A CONTRACT for the supply of a transmitter for use by the GPO in satellite communication experiments, to be carried out next year in co-operation with the Amercan authorities, has been awarded to Standard Telephones and Cables Limited.



These two independent sideband transmitters and aerial exchange were installed in a station outside Ankara, Turkey.

The equipment will be installed in a room built into the 85ft diameter steerable aerial now being erected at a site on Goonhilly Down, in Cornwall. The transmitter will operate in the 2000Mc/s communication band, and will deliver a frequency-modulated output of 10kW.

Additional items to be supplied by the company include power equipment for the transmitter and a water-to-air heat exchanger unit

The present programme calls for the whole transmitter to be installed on the site and fully operational by April, 1962. An active repeater communication satellite to be launched by the U.S.A. authorities will enable tests to be conducted on television transmission and two-way speech communication between Cornwall and the American ground station at Rumford, Maine.

# Communications Transmitters in Turkey

AS part of its programme of technical assistance to member countries of the Central Treaty Oganisation, the British Government have presented radio communications equipment to Turkey. Two independent sideband transmitters, aerial exchange, and matching transformers were among the pieces of equipment presented, and these were made by Marconi's.

The installation is at a transmitting station outside Ankara, Turkey.

#### Royal Navy Order

THE Admiralty has awarded a contract for the supply of a number of 500W medium-frequency/high-frequency independent sideband communication transmitters to Marconi's Wireless Telegraph Company Ltd., together with high-stability master oscillators and remotely controlled aerial matching units.

#### Weather Radar Orders

THE new duplicate version of the Type E190 airborne weather radar, which is a product of Ekco Electronics, has been ordered by Short Brothers and Harland Ltd. for installation in ten of their new Belfast air freighters. This equipment employs a dual transmitter/receiver and indicator system, in keeping with the current practice of duplicating essential services which are the subject of mandatory requirements. Fully "failsafe" conditions are thus provided, either transmitter/receiver operating with either indicator unit

Ekco airborne weather radar is also to be installed in the de Havilland Comet 4 airliner recently ordered by King Saud of Saudi Arabia.

# VHF Sound Broadcasting Station for Northern Ireland

THE BBC's new VHF sound broadcasting station at Londonderry which is on the same site as the BBC's television station at Sherriffs Mountain was brought into service on 23rd October. This is one of the twenty-one new VHF satellite stations so far approved for extending the coverage of the VHF sound service to over 99% of the population of the United Kingdom.

Londonderry radiates the Northern Ireland Home Service on 92.7Mc/s, the Light Programme on 88.3Mc/s, and the Third Programme together with Network Three on 90.55Mc/s. The signals are horizontally polarized, which means that receiving aerials should be horizontal. The programmes are fed by Post Office cable from a special receiving site at Glenderowen where they are received by radio from the BBC's VHF station at Divis.

The new station brings the BBC's VHF sound broadcasting service within reach of some 120,000 additional people in the counties of Londonderry and Tyrone.

#### 4th Jamboree-on-the-Air

FROM 00.01 hours GMT on Saturday, 21st October until 23.59 hours GMT on Sunday, October 22nd radio hams from forty countries all over the world took part in the Boy Scouts' 4th Jamboree-on-the-Air.

In this country alone there were over forty stations operating. One of these was in the recently opened Baden-Powell House in South Kensington.

This year Scout stations were on the air in Australia, Canada and the Philippines. In previous years contact has been made with Scouts in America, Canada, Holland, Sweden, Finland, Germany. Bermuda. France, Norway and New Zealand.

# Changes in Times of International Time Signal

FOR over one hundred years, the Royal Greenwich Observatory has been responsible for providing exact time signals for a wide variety of users both at home and abroad.

In recent years this service has become increasingly important in various fields of scientific research where extreme accuracy is essential. In order to provide the various users with more frequent opportunities for checking the time. on 1st December, the daily transmissions from Rugby were increased from two to four.

This means that the transmissions on the low frequency of 16kc/s until recently radiated at 10 a.m. and 6 p.m. are now superseded by signals at 3 a.m. 9 a.m., 3 p.m. and 9 p.m. There is, however, no change in the form of the signals.

To ensure a world-wide coverage, the 10 a.m. and 6 p.m. broadcasts have also been transmitted on short wave. This service is continuing, but the times have been changed to 9 a.m. and 9 p.m.

The transmissions from Rugby are proving to be indispensable to users all over the world. Such persons as marine surveyors and scientists engaged in tracking artificial satellites will undoubtedly find the new and more frequent transmissions of great value.

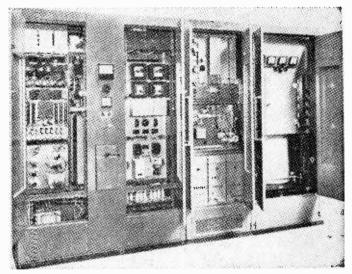
#### Ten High Power Short Wave Transmitters

THE British Broadcasting Corporation has placed an order with Marconi's Wireless Telegraph Company Ltd. for the supply and installation of ten high-power (250kW) short-wave sound broadcasting transmitters of a new type which, when they come into service, should very materially improve overseas listeners' reception.

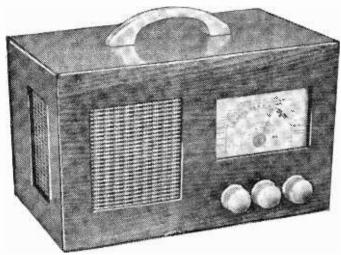
Six of these transmitters will be installed at the "Voice of America" relay station at Woofferton. Two more will go into service at the BBC station at Rampisham and the remaining

two at Daventry.

The transmitters are specially designed to combat the ever increasing amount of interference experienced by overseas listeners on the short waves. This is achieved by employing a method of modulation which cuts through the interference to bring the signal to the listener. Intensive experiments have shown that the use of this trapezoidal modulation, as it is called, gives an intelligibility at the receiving end which could only otherwise be brought about by more than doubling the transmitter powerthat is, in this instance, from 250kW to 550kW. The overall efficiency of the new type of transmitter is approximately double that of the older equipments supplied to Rampisham and Daventry.



A transmitter of the type to be supplied by STC to the GPO for use in satellite communication experiments. On the left is the power control cubicle (double width), with the drive unit in the centre and the klystron power amplifier cubicle on the right. This transmitter aperates in the 2000Mc/s communication band, and will deliver a frequency-modulated output of lokW.



A HIGHLY SENSITIVE DOMESTIC RECEIVER

By V. E. Holley

HIS receiver will perform satisfactorily in most parts of the country. Though small in size, its overall sensitivity is above average and unless reception conditions are very unfavourable it will work quite well on two or three feet of wire as a "throw-out" aerial. The valves, which at first sight may seem an odd assortment, have been selected (as will be explained) for low cost and high performance.

#### **Aerial Circuit**

Referring to Fig. 1, the signal from the aerial is passed first through the 1.F. rejector, L1, C1, which is an iron-cored inductor tuned to the intermediate frequency. It will be found useful in coastal areas where morse transmissions around 500kc/s are apt to find their way into the 1.F. amplifier; in other areas it will probably not be required and can be omitted. The filtered signal passes via the switch S1 to the appropriate aerial coil and thence via S2 to the grid of the first valve.

# midget mains

**Output Stage** 

In order to economise in the bulk, weight and cost of the power supply, a Mazda octal valve SP61, is used in the output stage. This valve can be obtained very cheaply indeed and although intended for R.F. amplification it makes a very satisfactory small power valve. It has a high slope and an output of one watt can be obtained in return for a modest signal at the grid. Grid and cathode resistors are  $1\,\mathrm{M}$  and  $150\Omega$  respectively.

If the greatest gain is required in the output stage the resistor R16 can be by-passed by an electrolytic capacitor of 100 µF and this will increase the sound output. The output transformer in the anode circuit should have a ratio of about 70:1 for a 30 speaker and can be of the type usually described as "small pentode."

#### Negative Feedback

The SP61 is a very efficient amplifier of radio frequencies and it is necessary to arrange that any such frequencies reaching it shall be excluded from the output. Accordingly, frequency selective negative voltage feedback is taken from the anode via the capacitor C21, to the cathode circuit of V3.

#### Second Negative Feedback

If maximum overall gain is not required, a second negative feedback loop, effective at all frequencies, can be formed by connecting a resistor of from 200 to  $1,000\Omega$  between points X and Y in Fig. 1.

#### **Power Supply**

The total H.T. current in the absence of a signat is 35mA at about 220V, while the valve

# SUPERHET

heaters and dial lamp need approximately 0.15A at 6.3V. This is supplied by a miniature mains transformer, the high voltage half-wave secondary of which feeds a metal rectifier, DRM1. A contact cooled rectifier is equally suitable. The rectified current is taken first through a fuse, which is in fact a 6.3V. 0.15A bulb; though not essential, this is a useful safeguard against the consequences of short circuits, catastrophic failure of capacitors, etc. Smoothing is provided by the capacitors C22, C23 and C24, and the resistors R17 and R18. This double stage arrangement gives good smoothing with negligible voltage drop, an important point if as in the prototype, the transformer voltage is only 220. The values of these resistors must be

adjusted according to the output of the transformer-rectifier combination so that the H.T. line voltage in the receiver is  $220\pm10$  in the absence of a signal. Miniature transformers do not usually have tapped primaries so the mains supply voltage must also be taken into account.

#### Components

The tuning scale and the gang condenser must be selected for compatibility if the transmissions are to be received at the points indicated on the scale. The coils may be any standard dust-cored components covering the long and medium wavebands and the trimming and padding capacitors should be of the values recommended by the

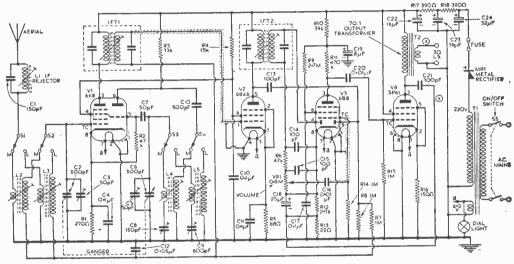


Fig. 1—The circuit of the receiver.

$C19$ $8\mu F$ electrolytic $C20$ $0.01\mu F$ C21 $300pFC22 16\mu F electrolyticC23 16\mu F electrolytic$	
C24 32μF electrolytic  Valves  VI 6K8, octal base V1 6K8, octal base V2 6BA6, B7G base V3 6B8, Octal base V4 SP6I, Mazda octal base  Transformers  Mains—220V, 40mA, ½-wave; 6·3V, 2A  O·IμF Output—Pentode type, 70: I  I.F.—I pair, 465kc s  O·05μF Dial light 6·3V, 0·15A  100pF Fuse 6·3V, 0·15A bulb  100pF Rectifier 250V, 50mA, half-wave, DRMI	

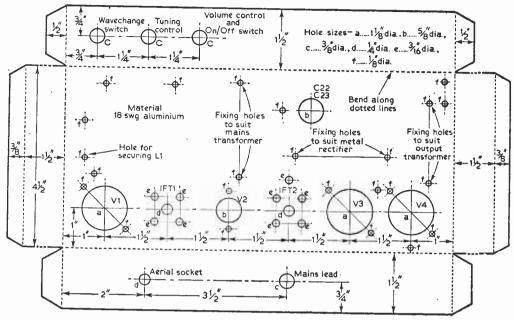
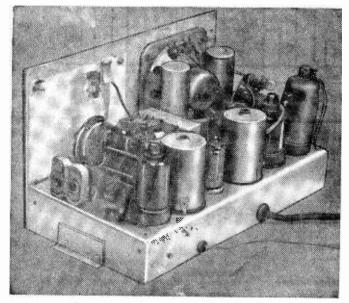


Fig. 2—The drilling details of the aluminium chassis.



The completed receiver without the cabinet.

makers. The values given in Fig. 1 are fairly typical and may be used in the absence of more authoritative information. Most manufacturers feature a suitable 1.F. rejector coil in their range, either with or without the parallel fixed capacitor, C1.

#### **Tuning Drive**

The tuning drive can be made from an old volume control. Remove the body and fit to the rear of the spindle a brass coupler in which a groove has been cut for the drive cord. Holes must, of course, be cut in the chassis for the cord to pass up to the drive drum and down again.

The resistors may be ½W except for R4, R17 and R18, which should be of 1W rating and, because the H.T. comes on through the metal rectifier before the valves are warmed up and ready to receive it, all the capacitors should be 350VW except for C18, for which 25VW working will be adequate.

#### Mains Transformer

The mains transformer must be a miniature type and it is convenient though not essential that the tuning condenser be semiminiature. All other components can be standard. The trimmers C2 and C16 should be fitted to the top of the gang condenser, which also carries a bracket for the dial light.

#### Construction

The receiver is constructed on a chassis of 18s.w.g. aluminium sheet, 9½in. x 4½in. x 1½in. (Fig. 2).

(To be continued)

# 16m T0 175m



# TRANSISTOR S.W. TUNER

A UNIT DESIGNED TO BE USED WITH A SEPARATE AMPLIFIER

By F. Neville Hart

OW that short-wave transistors have become about as cheap as valves and there are coils on the market for frequencies as high as the VHF bands, the simplicity of transistor circuits opens up an attractive field for the experimenter.

The set described here is a portable tuner which can be plugged into any amplifier, such as a tape recorder, or radio provided with 'gram' input terminals. It has a 3ft 6in. telescopic chromium plated aerial fixed in a 3-ply, leather cloth-covered cabinet, which was built to house the set. The construction of this is not described as readers may have their own ideas on carpentry.

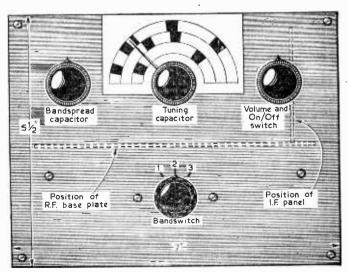


Fig. 1-The front panel layout.

	COMPON	ENTS LIST
Resistors (all ½W)		DI WG4B, OARI OF equivalent
RI I5k R9	8·2k	
R2 2·2k R10		
R3 Ik RII	680Ω	VC2 Three gang bandpass 30 pF (or 2 gang, see text)
R4 2.2k or 3.3k (see text) R12		TCI-8 30pf beehive trimmers
R5 10k R13		Tuning coils (Repanco)
R6 2·2k R14		Range I —
	Ik	Aerial type XTA31 blue mauve spots
R8 68k	110	R.F. type XTF32 blue black spots
Capacitors:		Oscillator type XOT33 blue brown spots
<del>-</del>		Range 2—
		Aerial type XSA34 red yellow spots
	121/14/	R.F. type XSF35 blue yellow spots
$C3 \ 0.01 \mu F$ $C14 \ 0.1 \mu F$ $C4 \ 0.003 \mu F$ $C15 \ 18 p F$	1277	Oscillator type XOS36 blue red spots
C6 0.01 µF · · · C16 0.1 µF	121/14/	Range 3—
	r 50μF 12VW	Aerial type XSA37 blue green spots
C8 8µF 12VW elec. C18 8µF 12	TOURT IZT TO	R.F. type XSF38 blue white shots
C10 0.25 µF 150VW C19 0.25 µF	F ISOVW	(Oscillator uses range 2)
(C5, 9 and 13 are inside the I.F. of	cans)	1.f. transformers—2 XT26 and one XT27(465kc/s)
	.0113)	2 blue spots, 2 green spots
VRI 5k potentiometer TrI, 2 OCI70		A battery blug for 7.5V battery
Tr3 OC45		Extending Aerial; 9-pole 3-way wafer switch,
Tr4 OC45		Zin. in diameter (H L Smith Ltd. 287 Edgware
114 0045		Road, W2)

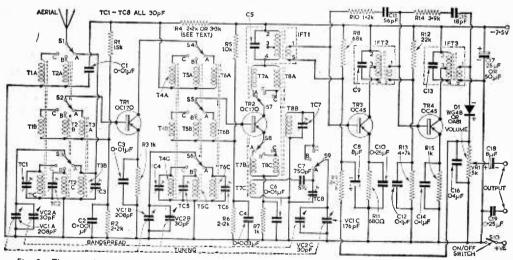


Fig. 2—The complete circuit diagram. Note that if instability occurs in the R.F. Stage, C4 should be reduced in value from  $0.003\mu F$  to  $0.001\mu F$ .

#### Frequency Coverage

The coverage is approximately from 16m to 175m, in three ranges, using a nine-pole three-way switch with three wafers. A number of these are obtainable as "surplus," but switch makers will make them up for about 15s. each.

Any I.F. coils for use with transistors can be employed, but since the short-wave tuning coils are made by Repanco, the use of their I.F. coils is described here. Although an R.F. stage rather complicates adjustment and trimming, it assists the rejection of second channel interference and gives better selectivity and volume.

The set compares favourably with the author's battery superhet with R.F. and two I.F. valves. Volume depends upon the amplifier following, but the output part of a transistor radio using driver and push-pull OC72's gives sufficient volume in the author's caravan, where, indeed, most of the construction was carried out.

#### **Aerial**

Although its own aerial is normally used, pick-up can be improved by using a longer aerial.

(To be continued)

# **Experimenter's**

# THE FINAL DESIGN AND CIRCUIT

(Continued from page 824 of the January issue)

By M. L. Michaelis

HE power unit is extremely versatile, giving outputs of almost all types normally required in experimenter's workshop. Whilst the unit is definitely advanced in nature, and thus not advisable for the the beginner, it is felt that it will meet a long-felt for requirement constructor. who. experienced once he has built it, will find virtually all of his power supply problems solved in one.

The outputs provided are the

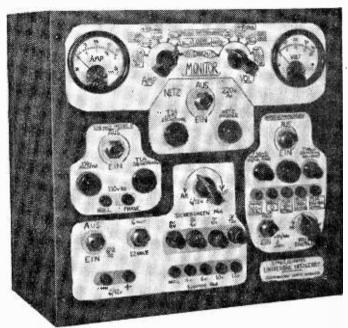
following:-

(a) A stabilised H.T. output, continuously variable from 120V to 350V, at a nominal maximum current of 100mA.

This output can thus be used for virtually any H.T. requirements, from battery-valve circuits requiring 120V H.T. at the one extreme, to mains-valve circuits requiring the higher voltages up to 350. Stabilisation is such that the remaining effective internal impedance is about  $50\Omega$ , so that in most cases several pieces of apparatus can be fed without mutual interference.

(b) An unstabilised H.T. output of about 300V, fully independent and capable of supplying some 50mA. This is intended for operating various pieces of apparatus, such as a valve voltmeter or a test oscillator, etc., at the same time as the experimental circuits being worked on are being fed from the main stabilised H.T. supply.

(c) Two neon-stabilised output voltages, one at plus 90V and the other at minus 100V, relative to earth (chassis). These are capable of being loaded up to about ImA each. Their purpose is for providing facilities for any bias-bleeder chains that may be required in advanced experimental circuits, and to this end they may be used together or independently.



The author's unit

(d) A.C. heater outputs at 4V, 6:3V, 10V and 12:6V. All are rated at 4A maximum continuous loads. By simultaneous loading at various of these voltages, the total current must not exceed 4A:

(e) Low-voltage D.C. output at a maximum of 18V and a maximum of 2A. This output is intended for a variety of uses. It is not stabilised, but it is fully smoothed, and is variable by means of a variable wire-wound resistance. It can be used for the following purposes:—

heating battery valves of 1.4V or 2V type; heating mains valves with D.C. in circuits requiring this;

charging accumulators (anything from a single 2V cell to a 12V car-battery);

feeding transistorised apparatus. On account of this last envisaged use, the positive pole of the supply is earthed, and not the negative pole, as is otherwise more usual. This does not in any way impair the other uses named. (f) An output at 110V A.C. up to about 100W. for feeding any 110V apparatus that may come in for attention. (It is assumed that the power unit is to be built for 230/250V mains, but if readers' local mains have other voltages, then it is merely necessary to purchase transformers with the appropriate primary windings.

A comprehensive system of indicator pilot-

A comprehensive system of indicator pilotlamps, fuses and other protective measures are incorporated, and a definite orderly plan has been devised and followed in the allocation of switchfunctions. These features will all become apparent in the course of the circuit description below.

#### Checking Output

A multi-purpose monitor system is built-in, for metering any of five important voltage outputs and any of five important current outputs. Two moving-coil meters are used, with suitable switching, shunts and multipliers. One meter functions as voltmeter and the other as current meter. Any one voltage and any one current may be displayed at any one time. The meter may be switched on to voltages and currents on load, and this process does not disturb the functioning of the power unit. Thus if all five outputs are simultaneously loaded, the meters may be switched successively to read off all circuits in turn, without disturbing them.

All outputs are fully independent. Thus, for example, the low-volts D.C. output may be connected to charge accumulators, and at any time the other sections of the power supply used for feeding electronic circuits. After checking for correct charging current, the meters may be switched over to monitor the H.T. and other circuits being used. At any time the meters may be switched momentarily back to the accumulators on charge, to check that charging is still correct. This is only one example of possible simultaneous uses of the power supply, so that in actual fact the power supply serves the purpose of several smaller power units. This represents a considerable saving in space and expense, compared to the actual construction of the equivalent range of separate power units.

#### Heat

Attention has been given to the question of adequate heat dissipation. This has been successfully achieved whilst at the same time satisfying the apparently contradictory requirements of maintaining as compact a form as possible. In the author's unit the front panel is approximately one foot square, and the cabinet is 6in. deep. To make the best possible use of the space available, the usual chassis construction has been rejected in

```
COMPONENTS LIST
Resistors (\pm 20\% unless otherwise stated)
RI 22k IOW RI6 IOk 2W \pm 5\%
                                                        Valves
                                10k 2W ±5%
33k 2W ±5%
                                                           VI.
                                                               EL34
   R<sub>2</sub>
        82k 10W
                          R17
                                                           V2
                                                               ECC83
  R3
        820k 2W
                          RI8
                                82k 2W
                                                           V3
                                                               90Cl neon (90V
  R4
        820k 2W
                          R19
                                1.8k 6W
                                                               90Cl neon (90V)
  R5
        6.8k 2W
                          R20
                                5\Omega w.w. \pm 1\%
                                                          V5
                                                               108Cl neon (100-108V)
                                5\Omega w.w. \pm 1\%
  R6
        IM 2W
                          R21
                                                          V6
                                                               90Cl neon (90V)
  R7
        18k 2W
                          R22
                                                               Four E250Cl 30 selenium elements
                                                          DI
        18k 2W
  R8
                          R23
                                                          D2
                                                               Selenium E250C50
                               -100k 2W ±5%
                                                                                                    500
        185\,\Omega\,\pm5\% w.w., 5W
  R9
                          R24
                                                          D3
                                                               Selenium B300C75
                                                                                                    text
                          R25
                                                          D4
                                                               Copper oxide E12C2000
  RIO
        100k IW
                                5k 2W \pm 5\%
                          R26
                                                        Switches
  RII
        100k IW
                          R27
                                Shunt
                                                          SI
  RI2
        220k I W
                                                                 Single pole toggle
                          R28
                                Shunt
                                                          52
                                                                 Double pole toggle
  RI3
        IM IW
                          R29
                                150 Ω I W
                                                                 Double pole toggle
                                                          S3
        82k 2W
  RI4
                          R30
                                150 Ω IW
                                                          S4
  R15
       150k IW
                                                                 2-pole/2-pole on/on toggle
                          R3I
                                Shunt
                                                          S5
                                                                 Single-pole double-throw toggle
 (R20 to R31 are in the meter circuits to be described)
                                                                 Single-pole toggle
                                                          56
Condensers
  C1 }
                                                          RLYI Three-phase A.C. relay 2A, 10-12V coil,
       8 \muF metallised paper, 500/750 VW
                                                                 400V contacts
                                                          MSI \ Meter wafer switches 2-pole, 6-way,
  Alternatively, CI and C2 can be 8µF 500VW
                                                          MS2 | break-before-make
    electrolytics (as on the circuit diagram)
3 8 μF 450VW electrolytic
  C3
                                                       Sundries
  C4
        8 μF 450VW electrolytic
                                                          Two mains transformers as specified in text
  Eight panel-fuses, single hole, insulated
                                                          Three pilot lamps: two red, one green
  C7
        0.02 μF 1000VW high insulation
                                                          Two bulbs 6.2V 0.3A
  C8
        0·1 μF 500VW paper
                                                          One bulb 10V 0-2A
  C9
       8\,\mu\dot{F} metallised paper 350/500 VW
                                                          Fourteen insulated wanderplug-sockets
  CIO
       0·I μF 500VW paper
                                                          Two moving coil meters as specified
 CII 25 µF 350VW electrolytic
                                                         One octal, one noval, four B7G valveholders
                                                            (ceramic)
 CI3
                                                         Four pointer knobs
       > 1000 µF 35VW electrolytic
 CI4
                                                         One yard tagstrip
Variable Resistors
                                                         Bolts, wire, sleeving, etc.
                                  VR3 \begin{cases} lk \ w.w. \\ lin., 5W \end{cases}
 VRI 100k IW lin.
                                                         Sheet aluminium, wood, screws, etc.
 VR2 10 Ω w.w. lin., 25W
                                                         Mains lead (3 core) and 3-pin plug
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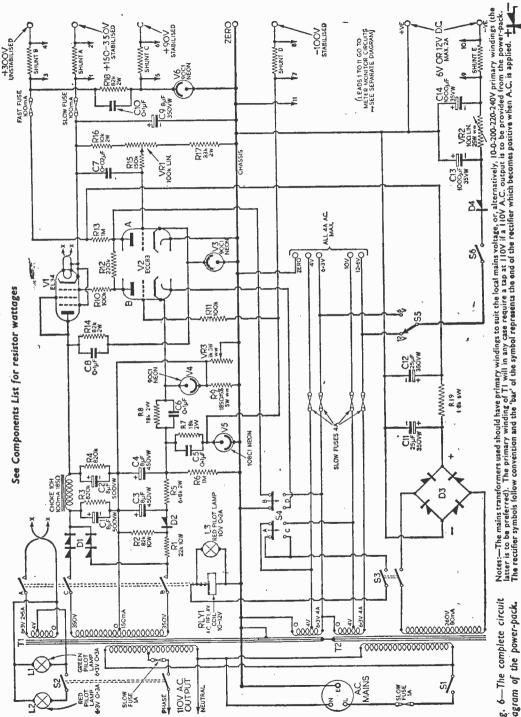
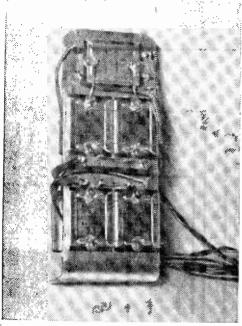


Fig. 6—The complete circuit diagram of the power-pack.

favour of a "spatial-construction". This latter form of construction is more difficult than conventional chassis construction, but has the advantage of complete utilisation of the available cabinet space, thereby reducing the size of a unit by at least a factor of two. However, the layout of the whole circuit is in all respects fully noncritical, so that those constructors who can tolerate a larger final size of unit may use the normal chassis form of construction, with any convenient layout. Adequate insulation is more important than any particular layout.



Front view of the rectifier sub-chassis.

#### Procedure

The "spatial-construction" consists of building the unit in the form of several sub-units. A wooden cabinet is used, with two sides, top, bottom, front panel and back. Any one of these six pieces of wood is independently removable, by means of loosening the appropriate screws. Construction is started on the basepiece of the cabinet, on which all larger components are mounted and wired up (transformers, etc.). In the case of the power unit here described, the next step was to make a small bracket-chassis on which the metal rectifiers and associated circuitry were mounted. This rectifierunit was then also mounted on the basepiece. When all the wiring of the basepiece was complete, all points to be connected to other components not on the basepiece were wired to suitably positioned tagstrips. The next stage was to make the front panel, on which all outlets, switches, fuses, lamps, controls, etc., were mounted and wired up. A sub-unit containing the low-volt D.C. rectifiers and smoothing was also mounted on this. All points to be connected elesewhere were again taken to tagstrips. The third stage was

then to make a small chassis containing all the valves and associated circuitry, and mount this on the right-hand side panel of the cabinet, again taking all points to be connected elsewhere to a suitably positioned tagstrip. The fourth stage was then to mount the few remaining components (in this case the A.C. relay, the smoothing choke and the output condenser) on the left-hand side panel. Nothing is mounted on the top-piece or the back of the future cabinet.

#### Inter-wiring

Four separate sub-units have now resulted, on four pieces of the future cabinet. These are now laid on the workbench in such a position relative to each other that (a) all parts of all of them can be reached comfortably for repairs and altera-tions, and (b) they are nevertheless as close as possible to their proper relative positions in the final asembled cabinet. The units are now interconnected by neat bunches of insulated wires, of the correct lengths, running between the tagstrips of the various units. After completion of this work, the power unit is electrically complete, and may be switched on and tested. If all is found satisfactory, the four sub-units and the top-piece of the cabinet are screwed together with woodscrews, to form the cabinet. All cable-bunches are neatly tucked away in positions where they cannot chafe or otherwise be damaged. After cutting suitable ventilation holes in the back panel, this is screwed on too. It remains to label all items externally on the front panel and to paint the cabinet as desired, and the power unit is then ready for service.

#### Interlocking

The geometrical arrangement of the components on the four sub-units is such that complete spatial interlocking (without, however, touching and shorting of components) is achieved within the cabinet after assembly. The arrangement used by the author satisfies some further points, too:—

(a) All valves are immediately accessible for quick replacement if ever required. Thus the valve chassis is at the rear, reached as soon as the back is removed, without further dismantling.

(b) All components generating much heat, principally the transformers, choke and valve chassis, are mounted at the rear, so that they induce a strong convection current through the generous ventilation holes in the rear panel, and do not heat up the rest of the circuitry unnecessarily.

(c) The build-up otherwise avoids horizontal

(c) The build-up otherwise avoids horizontal layering, and stresses vertical channelling, to give full freedom to convection cooling; the author's prototype has been on non-stop operation for periods of up to one week without the slightest indication of undue heating.

The detailed building plans to be given will bear out these points, but it must be borne in mind that considerable modifications may be necessary according to the actual shapes and sizes of components individual constructors may purchase or have available. For this reason it was stated above that this type of construction is more difficult than a conventional chassis. It is absolutely essential that the constructor should collect all essential components together, and then sit down and very carefully envisage the complete final construction. (To be continued)

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ILLUSTRATIONS



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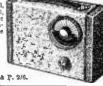
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# TRANSMITTING (TO A CLASS "A" MODULATED MINIATURE VALVE

TRANSMITTER

Amateur Transmitter

HE transmitter described here is a single, compact unit with its own modulator and power supplies, and is constructed on a chassis 7½in. x 111in. x 21in. Send/Receive switching is incorporated, so that it is only necessary to add a receiver to obtain a complete table-top type of

station. There is no need for an aerial changeover relay, or separate control of the receiver. Instead, the one control on the transmitter provides complete change-over from transmit to receive, and this is found very convenient when working.

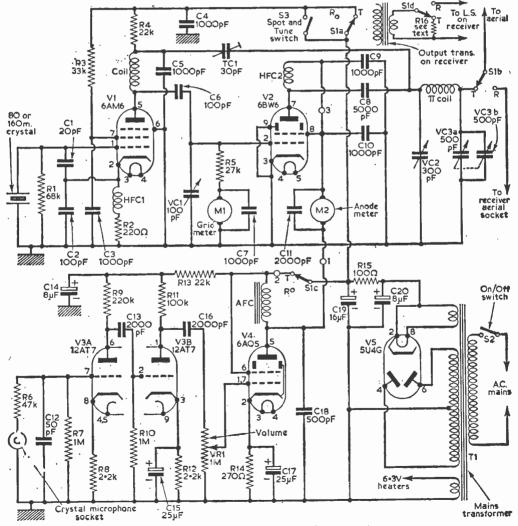


Fig. 1—The complete circuit diagram of the transmitter.

The circuit is shown in Fig. 1. The Spot and Tune switch applies H.T. to the oscillator only. This allows the transmitter frequency to be located exactly with the receiver, so that the latter can be tuned to the same frequency. It also permits tuning up the transmitter for suitable grid current, and shows where the signal will fall, compared with other stations which may be working. If a VFO is used, it allows the transmitter to be netted on another transmitter frequency, ready to answer a call.

#### Switching

The Send/Receive switch applies H.T. to oscillator, modulator and P.A., and connects the aerial to the transmiter. When in the transmit position it disconnects the receiver speaker, to silence this. When the switch is turned to "Receive" the aerial is connected to the receiver, the speaker is in operation, and the transmitter H.T. supply is off.

The 6AM6 oscillator will operate at fundamental frequency, or as a doubler. This permits 2-band working with one crystal. Two crystals will give four operating frequencies in two bands. Grid drive when operating as a doubler is almost the same as when working on the fundamental.

The 6BW6 will run at up to 10W input, which is of course the maximum permitted on the 160m band. It was found generally best to load to an input of about 40mA and this resulted in 9 and

even 9-plus reports, with a correctly coupled dipole. An end-fed aerial, preferably correctly tuned at the transmitter, would give almost similar results.

#### Modulation

A high-gain double triode is used in the modulator, so that a crystal microphone may be employed. With 250V on anode and screen grid, the 6AQ5 has a power output approaching 4.5W and reports or monitoring indicate that good modulation and speech quality can be expected. When a class-A stage is operating normally, the anode never swings completely to zero voltage. This means that over-modulation in a downward direction (which must always be avoided) cannot arise. It will be found that attempts to increase the modulation too far will cause distortion due to overloading of the audio amplifier. This will be apparent on a simple monitor, whereas evermodulation may not. For this reason it was decided not to add a P.A. condenser and resistor dropper, such as may be used with class-A modulators. This change might make over-modulation possible, and was not felt necessary, after testing the circuit as in Fig. 1.

The transmitter requires approximately 100mA at 250V, so a large receiver or amplifier type transformer will suffice. Heaters consume 1.5A at 6.3V. The rectifier was a 5U4G, which needs 5V at 3A, but 5R4, 5V4 and similar rectifiers are

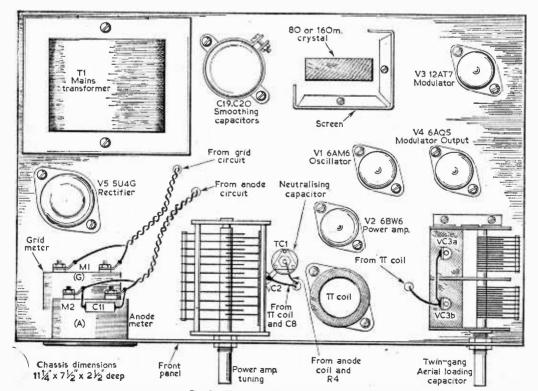


Fig. 2—The above-chassis wiring.

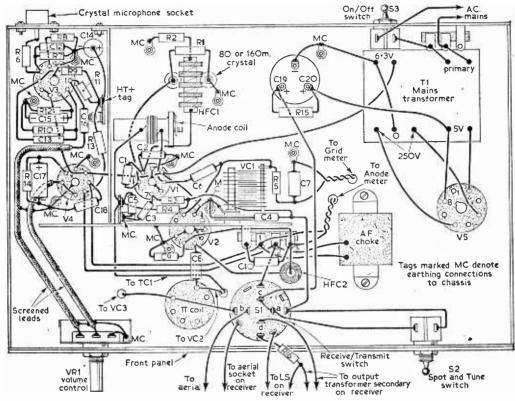


Fig. 3—The underchassis wiring.

equally suitable. No separate mains switch was used because the transmitter and receiver were controlled from a single switch. The transmitter heaters run continuously, in the usual way.

#### Chassis Layout

This is shown in Fig. 2 and is not very critical. The P.A. tuning condenser should best be at least 200pF, or it may be necessary to modify the number of turns on the  $\pi$  coil, when changing from one type of aerial to another. (A surplus condenser was used here.) The 30pF air-spaced neutralising condenser is soldered to the fixed plates tag. The other lead from the 30pF condenser passes through the chassis to the junction of the oscillator anode coil, 22k resistor, and 1000pF condenser.

For aerial loading a 2-gang broadcast type receiver condenser has sections wired in parallel. A short lead passes from the coil to the fixed plates.

A simple screen round the crystal holder was

A simple screen round the crystal noticer was found useful as some of the valves are quite near. It is preferable to use valve screens over the 6AM6 and 12AT7.

It is necessary to meter both grid and anode current, and this can be done with two separate instruments, or with a single meter and 2-way switch, as will be described next month. The neters, or meter and switch, occupy the left of the panel.

#### Underchassis Wiring

Fig. 3 shows all components and wiring. The space is divided into sections for the modulator, oscillator, and output stages. Heater wiring is completed before mounting the screens, which are notched to allow the heater connections to pass. These leads should run close against the chassis.

The modulator is built in the small section near the microphone socket. An insulated tag bolted to one screen serves as a H.T. anchor point. Two screened leads pass round the end of the other screen, to the volume control. Externally, a screened lead should be used for the microphone, to reduce R.F. pick-up and avoid hum. The 47k resistor and 50pF condenser provide some R.F. filtering.

A speaker output transformer was found to be satisfactory for the modulator A.F. choke. A reasonably large transformer, rated to carry about 100mA, is required. A component intended for mains pentodes is suitable.

The second screen passes across the 6BW6 valveholder, which is so positioned as to have grid tags behind the screen, and anode and g3 tags in front. Sufficient is cut from the screen to clear the holder.

(To be continued)

## Improving Broadcast Receivers

By K. Berry

A SMALL INVESTMENT IN A
FEW NEW COMPONENTS
WILL REJUVENATE AN OLD SET

(Continued from page 853 of the January issue)

N all of the additional R.F. circuits described last month, no extra AVC voltage was used, i.e. in all the circuits which were given, the AVC was applied either to the original frequency changer or to the new amplifier. This is in fact completely satisfactory except where the receivers are operated very close to a transmitter—under these circumstances some overloading could occur. This possibility could be eliminated by always applying the AVC voltage to the R.F. stage (see Fig. 6, last month).

It is perhaps worth mentioning that whilst the circuits given in Figs. 3 and 5 were untuned, it is very easy to include a single, fixed-tuned circuit which will have the result of increasing the R.F. gain a! (and close to) the resonant frequency of this tuned circuit whilst retaining the general increase in gain over the whole band. This will thus enable any particular desired frequency to receive extra amplification—e.g. a circuit tuned to 208m would give a considerable increase in gain for reception of Radio

Luxembourg.

If it is desired to fit such a tuned circuit, it should be connected between the grid of the R.F. stage and the 10k grid leak resistor.

#### Components

Components values are given only for those components shown in the circuit which are additional to those already in the receiver. The valve recommended is an EF92.

If the layout of the receiver will allow it, extra gain may be obtained in the circuits given in Figs. 3 and 5 by using an EF91 or EF80. In this case, the screen is taken straight to H.T.+ and the cathode resistor should be reduced to  $150\Omega$ . Since these valves give a very high gain it might be necessary for the H.T. supply to the R.F. stage to be decoupled—a resistor of 2.7k in series with the supply to the anode and screen with a  $0.1\mu$ F capacitor to chassis should suffice.

#### Increased I.F. Gain by Additional I.F. Stage

A typical superhet I.F. stage is shown in Fig. 7. This is shown again in Fig. 8 with the addition of another stage of amplification preceding the original I.F. stage. This additional I.F. stage may be mounted directly on the receiver chassis; alter-

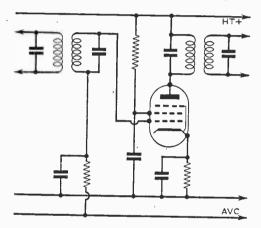


Fig. 7—Circuit of a typical superhet I.F. stage.

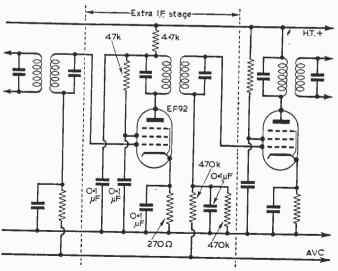


Fig. 8—The circuit of Fig. 6 with the addition of an extra I.F. stage.

natively it may be mounted on a small sub-chassis which is in turn bolted to the main chassis.

This new I.F. stage is controlled by the set's AVC, thus no overloading problems should occur. The normal techniques associated with the R.F. wiring must be employed if instability is to be avoided, i.e. short, direct leads—anode and grid leads kept away from existing "hot" wiring, etc.

#### Components

As previously, component values are given only for those components shown in the circuit which additional component required for this modification, but a considerable improvement is effected.

#### Tone controls

It will normally be found that "tone" controls of the top-cut variety operating on the primary of the output transformer will be virtually inoperative when feedback is applied in this manner (or indeed in any manner). The reason for this is that negative feedback tends to "straighten out" the frequency response of an amplifier whilst the effect

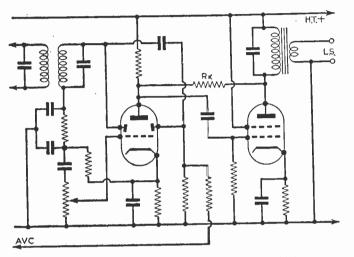


Fig. 9—A typical audio output stage with a resistor Rx added to give negative feedback.

Fig. 10—This circuit shows how

Fig. 10—This circuit shows how the extra feedback resistor forms the upper part of a potential divider (see text).

of the "tone control" is to distort the frequency response so that the net result is that the influence of the tone control will be very much reduced.

# are additional to those already in the receiver. Once again the valve recommended is an EF92. The use of an EF91 or EF80 here should not be attempted as neither of these valves has a vari- $\mu$ characteristic, thus preventing the use of AVC.

Improving the Frequency Response of the Audio Stage

This is a very simple modification, and in the author's opinion, the most worthwhile one. Most commercial domestic receivers have a triode L.F. stage followed by a pentode or beam tetrode output stage: It is not usual to employ negative feedback, and "tone correction" is effected by shunting the primary of the output transformer with a capacitor. This sometimes has a fixed resistor in series with it, or sometimes a potentiometer which serves as a "tone" for top-cut control. The average receiver of this type has a considerable excess of audio gain, and this can be reduced considerably by the use of negative feedback. This will result in reduced distortion and improved frequency response—particularly at the L.F. end.

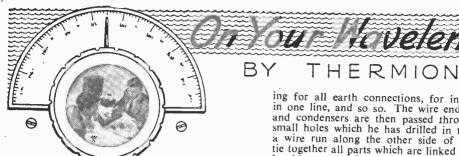
In Fig. 9 is shown the L.F. side of a typical domestic receiver. This receiver has fixed "tone correction" by means of the capacitor across the primary of the output transformer. Shown connected between the anodes of the L.F. and output valves is a resistor, Rx. This is the only

#### **Potentiometer**

The method of operation of the feedback circuit is shown in Fig. 10. It will be seen that the feedback resistor forms the "upper" part of a potentiometer which divides the output of the valve. The "lower" part of the potentiometer is formed by the anode load of the previous valve and the grid leak of the output valve in parallel. The exact value of Rx will depend on how much gain can be "thrown away" and the values of the anode load of the previous valve and the grid leak of the output valve. As a rough guide, the ratio of the potentiometer should be about 10:1, so if for example, the anode load is 100k and the grid leak resistor is 1M, the shunt value of these is 91K; hence the feedback resistor Rx will be about 10 × 91k = 910k. The nearest value to this in 20% resistors would be 1M.

#### Applying Feedback

It must be emphasised that applying feedback in this manner will result in reduced A.F. gain, so if your radio has no gain to spare—do not try this. If there is no gain to spare, it is possible to obtain more by removing the existing double diode triode and fitting a pentode valve in its place. The diodes can be replaced by germanium crystal diodes.



#### Experimental Hardships

T is surprising what a lot of time can be wasted when you are carrying out experiments and are not in a position to have parts properly checked before use. I recently heard of an engineer who was a keen radio experimenter and who owned both R and C bridges with which he used to check all components before using them. The one big thing he lacked, however, was a valve tester. He tells me that he was carrying out some experiments with a new instrument in which were three double triode valves. He wired them up and commenced his tests, only to be met with failure. Altogether, he tells me, he spent nearly three weeks on this circuit, the valves in use having been removed from a piece of equip-ment which was working satisfactorily. To sum-up, after fruitless endeavours, he removed the valves for some fresh wiring, and apparently replaced them in different sockets. The circuit worked! The difficulty had been due to one of the triodes being low emission, and of such a character that it failed to work in one stage only. It was one of the high-mu triodes, and he found later that in the particular stage in which it had originally been plugged, it would not oscillate. It functioned quite well elsewhere and is, in fact, still in use as an audio amplifier, but it will not oscillate in that particular circuit. I suppose a good valve tester would have revealed the fault and prevented so many wasted hours, but I think there is a moral here, and that is, not to rely on a first test, but to either change all the parts or have them tested, especially if it is some new arrangement which has not before been used or tried out.

#### **Printed Circuits**

My comments, some time ago, about the printed circuit have brought many letters and I think it is true to say that opinion is equally divided. I had many interesting suggestions sent to me as to mending or repairing them and it would certainly appear that broken foils are a keen source of trouble. One manufacturer suggested that cracks should not be bridged over, but a new length of wire should be used for the entire run of the broken conductor. One very interesting suggestion was made by a reader to simulate the printed circuit board in ordinary wiring, and I have tried this out and certainly think that it has merits. He takes a sheet of paxolin and drills it to suit the particular layout in which he is interested. First of all he draws out the layout and wiring, arrang-

ing for all earth connections, for instance, to be in one line, and so so. The wire ends of resistors and condensers are then passed through the very small holes which he has drilled in the sheet and a wire run along the other side of the board to tie together all parts which are linked in the circuit. In this way he finally has an insulated board on which the components are on one side, and all connections on the other, and he tells me that testing is facilitated, the final construction is much neater, and the set can be practically prefabricated. I must admit that I tried out the idea and certainly found it had its merits.

#### In the U.S.A.

Do the Americans take their radio more seriously than we do in this country? I am prompted to ask this after seeing an American magazine, sent to me by one of my friends who has left this country. With the magazine he also sent two or three "men only" types, and some domestic (home) magazines. I am greatly struck by the large amount of space which is devoted to radio in these magazines, one having about five pages on the subject of loud-speakers. It is a most exhaustive account of the development of this "beast" in all parts of the world, and gives some details which I had not seen in print before.

The amount of space which is devoted to radio, in all of these magazines, leads me to think that they are much more radio-minded in America, and as a result this must lead to a much greater development in the art. Current market items do not, however, seem to bear this out, and there are not so many items on the American market which cannot be seen here, although they are more advanced in such things as colour television. Of course, with all the channels which are available in every part of their country, I suppose the manin-the-street must be more radio minded, but I would have led to much greater development.

would have led to much greater developments. Considering how lacking in general knowledge the majority of people are here, I think we have done a really good job in both the radio and the television fields, although I still would like to see someone come along with something new in the way of aerials. After all, the unsightly mess on the roofs of houses both here and in the U.S.A. will grow still worse as more channels are opened, and some new "receptor" covering from centimetric to long wavelengths would earn a pretty penny for the inventor and the blessings of every householder.

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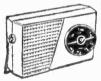


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## All about CATHODE

# FOLLOWER circuits

By E. McLoughlin

## PRINCIPLES AND USES OF THIS TYPE OF CIRCUIT

(Continued from page 808 of the January issue)

HE last example of the use of cathode followers which we discussed in the January issue was in circuits where pulses of high voltage are required, for example, in the synchronisation of timebases.

#### Calculations

all highamplitude uses, it is very simple to decide whether a combinacertain tion of valve, RK and H.T. voltage, is capable of handling an in-tended signal. Let Vn be the peak signal negative amplitude. Then grid leak (Fig. 6, last month) returned to a point at about plus Vn to chassis. It

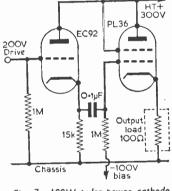


Fig. 7—100W pulse-power cathode follower.

follows that the cathode will also rise to about plus Vn (just a little more). By Ohm's Law, the current flowing in RK is then easily calculated. This represents the "resting "anode current of the valve used. Furthermore, let Vp be the peak positive signal amplitude. The sum of Vp and Vn must not exceed one half of the rated H.T. voltage of the valve used. The H.T. voltage chosen should thus be double the peak-to-peak signal, or more, within the rating of the valve, and the smallest possible value for RK be chosen which neither causes the anode current rating of the valve to be exceeded, nor lies below about 50 times the reciprocal of the mutual conductance. It is desirable to make RK as small as tolerable within these limits, because the voltage fluctuation with further external loading is then as small as possible. Normal operating anode current ratings, and not peak values, should be consuited in the above design procedures.

It should be mentioned that the signal frequency response of a normal cathode follower is virtually linear over the entire video spectrum, including pure D.C., and goes right up to many megacycles.

Cathode Followers as Signal Generator Output Stages

As the output stage of an Audio or R.F. Signal Generator, one often finds a cathode follower. The reason lies in most cases in the use of the property that the output voltage is largely independent of the exact value of the external load resistance connected. This enables an output calibration to be made for the signal generator which can be relied upon to hold, with tolerable

accuracy, for the most varied external loads connected. We are thus mainly concerned with 1:1 voltage-transfer cathode followers here, with their typical high value of RK of about  $10,000\Omega$  to  $20,000\Omega$ , or more.

Power-output cathode followers are normally not in question for signal generators, at any rate for audio and broadcast R.F. signal generators. But, for extreme VHF signal generators, such as are used for the high television channels, as well as for video-waveform test-signal generators, where maintenance of accurate waveform is essential, new factors play a role, which necessitate the use of a power cathode follower in many of these cases. If any disturbance is made in a electrical circuit, then the effects of that disturbance are not felt immediately at all other parts of the circuit, but spread out with the velocity of light or less. In particular, if we have a length of coaxial cable, and switch on a signal at the input end, it is not present at once at the output end, but only after

a time corresponding to a definite speed of travel of the signal down the cable, which is of the approximate order of the velocity of light. Now, this high speed means that, for reasonable lengths of cable, and audio or broadcast radio frequencies, signal transfer down the cable may be considered, for all intents and purposes, instantaneous. But at very high frequencies, such as are met in modern television techniques, the transit time of even a

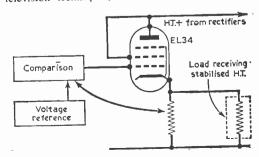


Fig. 8-H.T. voltage stabiliser.

few inches of cable is an appreciable fraction of a cycle. If impedances are not properly matched at all cable/apparatus junctions, a partial reflection giving signals travelling in the opposite direction to that intended occurs as well as loss of power. Reflections from separate ends of a cable will not be in phase, on account of the transit time. Moreover, the phase difference will depend upon the

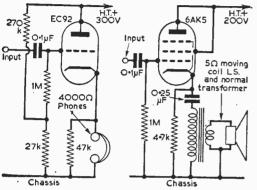


Fig. 9 (left)—Circuit of a "safe" output stage for 'phones using a cathode follower.

Fig. 10a (right)—Simple cathode follower output stage.

frequency of the components of a complex waveform. The net result will be a complete change in the waveform. It is thus essential to match a television waveform signal generator output to the intended load, and thus one finds power cathode followers in many cases in such apparatus.

#### The Pulse Power Cathode Follower

It is indeed possible to obtain very considerable power out of specially designed cathode followers. If we take a valve of high mutual conductance and having a pulse cathode capable of one amp or so peak current (although, of course, the mean current rating is much smaller), such as are found among modern line-output valves in television receiver circuitry, then short pulses of high power can be generated with such a valve connected as a cathode follower. Let us assume a typical mutual conductance of 10 mA/V, giving an output impedance, as cathode follower, of  $100 \Omega$ . Using

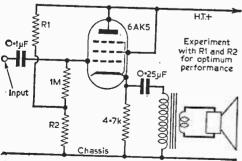


Fig. 10b—Improved cathode follower output stage. RI is 220k, R2 is 100k, and the H.T.+ is 200V.

a drive of 200V to give an output signal of 100V in the matched condition with a  $100\Omega$  cathode load, we just run up to the permissible 1A peak anode current. The output power realised in the external  $100\Omega$  load is then given by  $1A \times 100V$ ; i.e. 100W. Let us assume, typically, that the maximum mean current rating of the valve is 100mA. Then the peak 100W condition may be operated only for one tenth of the total time. For example, one 100W output pulse, lasting a tenth of a second, is permissible once every second. between times the valve would be resting at its set D.C. operating point, and we can now consider where this will have to lie. At the pulse-peak, when IA anode current is flowing, the gridcathode signal will be virtually zero. Thus the grid will be at the same voltage as the cathode, i.e. 100V positive. We are using a 200V positive drive, and thus the D.C. resting point will have to be with the grid at 100V negative to chassis. In other words, the valve is heavily cut off when no signal is present, and thus we see that the pulse power cathode follower is a special case of a Class-C amplifier.

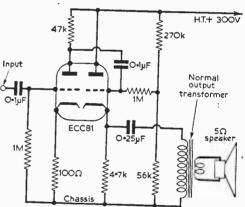


Fig. II—A double triode cathode follower output stage.

#### Cathode Follower Drive

The drive for such a power cathode follower naturally consumes no appreciable power, it is a pure voltage drive. Nevertheless, just in case gridcurrent flows at the pulse-peaks, the drive can be from a smaller cathode follower, this time in 1:1 transfer circuit with the usual high Rκ. Fig. 7 shows a typical complete circuit. The chief use of such a circuit is for firing grid-controlled hydrogen thyratrons in large radar installations, which consume considerable power at the grid. It is also known to the author that such a system has been used to modulate the output stage of a transmitter. The power output cathode follower supplies the entire H.T. power for the P.A., simply by making the P.A. itself take the place of the cathode load. Such modulation circuits, also known as series-modulation, are used in several pulsed radar transmitters.

Finally in this group, it should be pointed out that the usual H.T.-stabiliser circuits using a series-regulator valve (such as in several designs recently published in this magazine) are virtually a special form of D.C. power cathode follower. Redrawing

the circuit of such a stabilised power supply in the form of Fig. 8 immediately brings out this point.

#### Continuous Power (Class A) Cathode Followers

These are the true members of the "power" class of cathode follower, in that they can supply output power, say at audio frequency, in much the same way as a conventional output stage delivering power from the anode circuit.

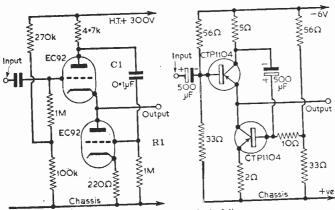


Fig. 12 (left)—A White cathode follower.

Fig. 13 (right)—The transistor equivalent of the White cathode follower (or all resistors increased by the same factor).

It is little known by experimenters that sometimes considerable advantages are to be gained by using an output stage feeding a loudspeaker or headphones in the form of a cathode follower. The first and obvious advantage is that the problem of isolation of the phones from the H.T. voltage is automatically absent (Fig. 9).

The second great advantage is apparent in circuits requiring a small monitor-speaker, but where for reasons of power economy or heat dissipation limits, a conventional output valve is undesirable. In such cases, constructors have often used simple A.F. triodes or R.F. pentodes, frequently with relatively poor results because of the very high anode matching impedances generally required in such circuits, which cannot always be realised with normal loudspeaker transformers. Much improved results are often possible using the same valves as cathode followers, with the normal loudspeaker transformer primary forming RK. In many cases the D.C. resistance of the transformer primary is sufficient to set a proper D.C. operating point of the stage without further attention to the matter. Fig. 10a shows a typical circuit example which the author has had in operation for a long time. A tiny 6AK5 R.F. pentode strapped as triode cathode follower delivers over 50mW into a small moving coil loudspeaker. The circuit is a small addition to an oscilloscope, to monitor the Y-signal audibly. There was not room, nor spare H.T. power, no heat dissipation facility, for operating a conventional audio output stage. But this tiny cathode follower output stage draws only some 5 or 6mA H.T. current.

#### High Impedance Loudspeakers

Those experimenters still possessing large moving-iron loudspeakers of formers days in their junk boxes, having coil impedances of some few hundred ohms, may like to try one direct as cathode load, without transformer, in such a cathode follower output stage. Any small R.F. pentode can be used, strapped as triode. In many cases the constructor will very likely be astonished at the results. Apart from good volume, the

tone is generally much better than with the same speaker used in an anode circuit, as the extremely low internal impedance of the cathode follower damps the unpleasant resonances of this type of loudspeaker to a high degree. It is even worthwhile, just for this last reason, trying a conventional output valve such as the 6V6 or the EL84 as a cathode follower. In such a case, however, it is necessary to pay special attention to the correct D.C. operating point, so that the valve does not run at low or excessive anode current. D.C. resistance of the transformer winding or speaker coil in the cathode circuit must equal the normal cathode bias resistor of the valve used. If it is less than this, then an appropriate series resistor must be used to make up the difference. If it is a little more, that does not matter much, as long as it is not excessive.

Naturally, the voltage drive required by a cathode follower output stage is high, being about 10 to 100V in most cases. Thus, the audio amplifier preceding the stage will have to have higher gain than is otherwise normal. An extra triode stage can often provide this gain. It is often convenient to use one triode of a double triode to give this extra gain, and the other as the cathode follower. In this way, a valve such as the ECC81 can replace a conventional output valve (see Fig. 11), the rest of the audio amplifier being unchanged. In the case of the author's 6AK5 output cathode follower of Fig. 10a the necessary drive was present anyway, as the Y-deflection of the tube in the oscilloscope requires a similar drive, so that sufficient voltage to drive the cathode follower was present at the Y-amplifier output.

#### The White Cathode Follower

Fig. 12 shows a further development of the cathode follower principle, to give even lower internal impedance. It is possible to achieve an impedance of a few ohms with this circuit, so that in principle, a moving coil speaker would match direct without transformer into it. This is true in in practice, too, but the power output is then poor in comparison with the H.T. consumption and size of the valves. This is simply because of the restriction that the valves may not be permitted to run up to the necessary anode current. Thus using a PL36 triode-strapped in each position, only 50mW is possible into a 15Ω moving-coil speaker.

(To be continued)

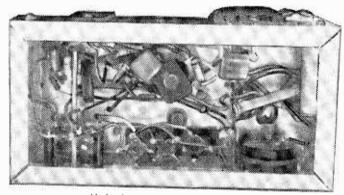


By A. Sydenham

(Continued from page 833 of the January issue)

N the previous article, the circuit was described and it now remains to assemble the complete unit and build a cabinet for it. It may then be tested. A diagram that shows prac-

tically all the chassis drilling is given in Fig. 4, the coil mounting apertures being those required for the coils specified. Should the tuning capacitor contact the coil bases when in position, washers should be fitted to provide clearance. Alternatively, the coils may be fitted to a rectangular piece of paxolin held by spacers. Most of the wiring can be made so short that small items are easily



Underchassis view of the pre-selector.

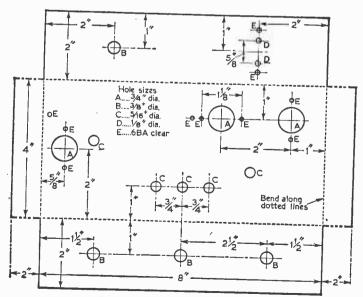


Fig. 4—The chassis drilling diagram.

suspended in the leads and the orientation of the coils and valveholders assists in respect. Electrolytic condensers C9/C10 and C11 are held against the chassis by clips.

#### Assembly

The front panel is secured to the chassis by means of the nuts securing VR1 and S1/S2 and reference to Fig. 5 will show the locations of the various aper-The tuning condenser spindle also projects through the front panel and a coloured warning lens is fitted to the lower central aperture. It will be found when the panel is firmly bolted in position that the assembly slopes backwards slightly and this not only brings the controls to a more con-venient operating height but also improves the general also improves the general appearance. Mitred sections of quadrant glued firmly to the panel edges further assist in this respect.

#### Wiring

Use of a soldering iron with a pencil bit is essential and modern miniature resistors and condensers are needed to avoid congestion of subchassis components. The use of differently coloured sleeving will also assist final checking considerably.

#### The Cabinet

The simple design is shown in the semi-exploded diagram of Fig. 5 and may easily be made from tin. plywood held together with reinforcement strips, pins and glue. Strips of veneer 'obtainable from some model supplies shops) may be glued using Bostik No. 1 adhesive to the edges where joins appear if desired, and the finish may be chosen to suit one's personal taste. The prototype is lacquered in ivory. The slots cut in the sides serve as carrying handles and also provide

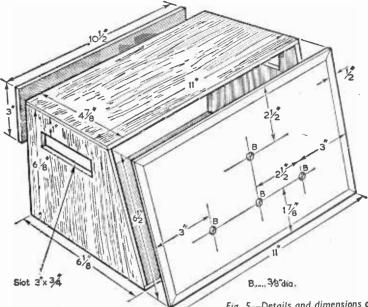
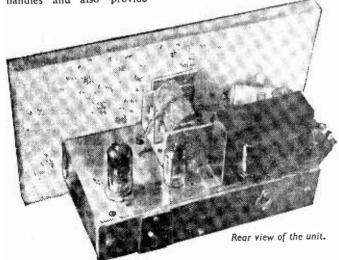


Fig. 5—Details and dimensions of the cabinet for the pre-selector.



ventilation as cool air is convected from the rear. Four small rubber feet may also be fitted.

#### Using the Pre-selector

When the unit has been completed and checked the aerial and earth leads should be removed from the receiver with which it is to be used and plugged instead into the sockets provided for them on the pre-selector.

A length of coaxial cable should then be prepared, aerial and earth plugs being fitted at one end (the braiding being connected to the earth plug) and a coaxial plug at the other. This lead should then be plugged into the appropriate sockets on each piece of apparatus. Control VR1 on the pre-selector should now be set to off" and the wave-change switch turned to position 4. The main receiver should then be switched on and adjusted to receive a transmission in a band also available to the pre-selector. The receiver should now act normally, since the aerial is effectively connected to it direct. The pre-selector may then be switched on and allowed to warm up when its wavechange switch may be rotated to select the appropriate band in use. The received signal should now improve in strength considerably and, as the tuning control of the pre-selector is adjusted, it may be found necessary to back off the sensitivity control, VR1, to avoid overloading. A little practice will soon reveal the best

method of use but it should be remembered that too strong a signal fed to the receiver may bring the AVC circuit into action too strongly. Once the user has familiarised himself with operation of the unit it may be calibrated.

When it is desired to use the main receiver on its own it merely becomes necessary to turn the wavechange switch, SI/S2, to position 4 and rotate VR1 to "off" when the indicator lens will become dark. By then, however, the advantages of R.F. gain will have been made apparent.

(Continued on page 942)

THIS UNIT WAS ORIGINALLY DESIGNED FOR USE WITH A SIMPLE GEIGER HEAD, BUT IT WILL OPERATE SATISFACTORILY FROM ANY SUITABLE INPUT SOURCE

By A. Cole

A DIGITAL

25 O

ITH the reintroduction of frequent atomic bomb tests recently, it is an interesting—and possibly useful—occupation for the electronically minded experimenter, to monitor the degree of radioactivity in the air, rainwater, drinking water, or any other samples of interest. Contrary to common belief, this is neither difficult, nor does it require any unusual or expensive circuit components, except for a suitable small Geiger tube. There are some excellent small tubes on the market now, available in the United Kingdom from Messrs. Mullard. The author uses a tube of type number MX146. These small tubes have the great advantage that they require only about 450 to 500 operating voltage, which is easily obtainable from ordinary mains transformer/rectifier circuits.

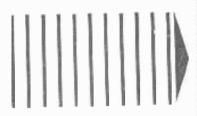
For checking atmospheric radioactivity, etc., a pure counting of the pulses is required, and the present article describes a suitable automatic electronic counter, giving a direct numerical display of the result on a type of digital relay used by the GPO for counting telephone calls and easily obtainable for about 15s to flat many counting telephone.

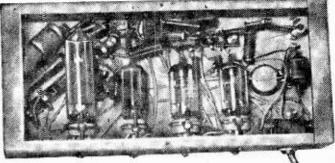
able for about 15s. to £1 at many surplus stores.

The digital counter unit may, of course, also be used for any other appropriate purpose. It will count accurately the number of times a voltage of at least plus 10 is switched on into the input. It does not react when this voltage is switched off again, but counts one more when it is switched on again, and so on. So long as this voltage is 10 at again, and so on. So long as this voltage is 10 at least, and positive, and capable of delivering a current of about ImA, it does not matter exactly how large it is. Thus a morse key and battery in series connected to the input can be used for manual counting of large numbers of small articles, without the need to keep the numbers in one's head with consequent danger of error. With one's head, with consequent danger of error. With a relay wired to contacts on the space bar of a typewriter, the unit can be used to count the number of words in a piece of typescript. But for all such uses, the circuit could probably have been a lot simpler: the main use is in conjunction with a Geiger counter, and for this purpose the circuit features have primarily been developed, as will be seen below. Above all, the unit is designed to be as fast as possible, and free of any grid-current-blocking so that two pulses following very rapidly one after the other are both counted individually. The actual resolution achieved in the author's unit is better than 15 counts per second at the upper limit, which is far greater than the pulse-rate ever obtained with the type of Geiger tube specified with atmospheric radioctivity. In fact, the normal atmospheric count with this tube is about 20 counts per minute, i.e. only about one count every three seconds on the average. But these counts are fully irregular-

GOUNTER

Internal construction of the digital counter unit.





there may suddenly be many close together, and then for a long time absolutely none, yet it is virtually impossible for a whole minute to pass without any counts at all.

## Principle of the Digital Counter Circuits (see Fig. 1)

This is a four-valve triggered pulse-amplifier circuit. V1 is the input amplifier, comprising two stages:—V1A is an earthed-grid input stage, meeting the three requirements (a) freedom of feedback, (b) keeping the same signal polarity (positive), and (c) good gain, so that the stage is over-driven, giving very steep output pulses to V1B, which is a cathodefollower decoupling V2 from V1A as far as feedback is concerned. V1B also returns the signal to

low impedance, and now delivers a good steep pulse of at least 100V amplitude. The tiny value of C3, the coupling condenser to V2, differentiates this pulse, so that only a very brief but very steep spike of about 100V is applied to the grid of V2A.

Valve V2 is a monostable multivibrator, the purpose of which is to provide a good squarewave pulse of current, starting exactly at each 100V "trigger" spike from VI, and lasting about one twentieth of a second, which is the optimum switching-time for the counter relay. V2A is normally cut off, because its grid is on a bleeder chain from the low voltage at the anode of the normally conducting section V2B down to a variable negative bias from VR1. The other section, V2B, is, as just stated, normally conducting

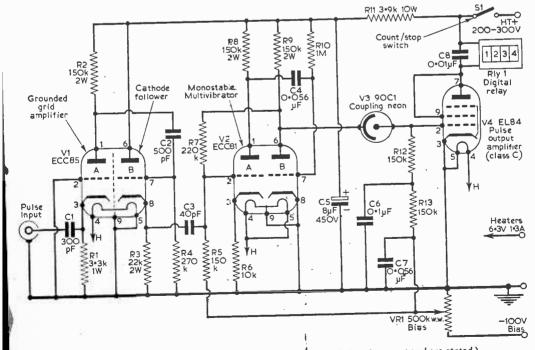


Fig. 1—The circuit of the digital counter. (All resistors are IW rating except where stated.)

heavily because its grid leak is returned to H.T. positive. This condition is perfectly stable for any length of time until the circuit is suitably disturbed. This disturbance is the short positive 100V spike applied to V2A grid. This lifts it to cut-on and above, which causes an equivalent voltage drop at the anode, which is fed via C4 to the grid of V2B, thus tending to cut off V2B. This causes the anode potential of V2B to rise, which is fed as a further rise to V2A grid on the bleeder. The net result is that the formerly cut-off V2A has suddenly been tuned hard on, and the formerly conducting V2B has been cut off.

Maintenance of this new condition depends

upon maintenance of the signal at V2B grid, which remains only as long as C4 is charging via R10. As soon as C4 has charged sufficiently, which takes about one twentieth of a second, V2B cuts on again, and reverses the procedure back to the previous stable state with V2A cut off and V2B conducting, until the next trigger spike arrives. The net result is thus a positive-square-wave pulse of about 100V amplitude and about one twentieth of a second duration at V2B anode.

V4 is a class-C amplifier, i.e. the bias-point is beyond cut-off, applied via R12 and R13 from VR1. In the normal, stable, resting state of V2, with V2B anode at a low voltage because of the heavy conduction of V2B, the voltage difference between V2B anode and V4 grid is not sufficient to strike the neon tube V3; thus V4 is fully disconnected from V2 and resting, cut-off. But during the temporary

change-over position of V2, when V2B is cut off and thus the anode voltage high, the neon V3 is struck, driving V4 grid heavily positive. The surge of anode current in V4 moves the digital relay RLY1 one unit on. As soon as V2 reverts to the stable condition, V2B anode potential falls again and the neon V3 extinguishes. V4 grid returns at once to beyond cut-off, and anode current ceases instantaneously. This sudden stoppage of anode current could cause high inductive voltage peaks across the coil of RLY1, if C8 were not there. Thus it is essential not to omit C8, as otherwise the relay could be damaged by flashover in the coil. On the other hand, do not make

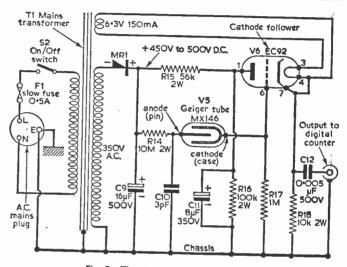


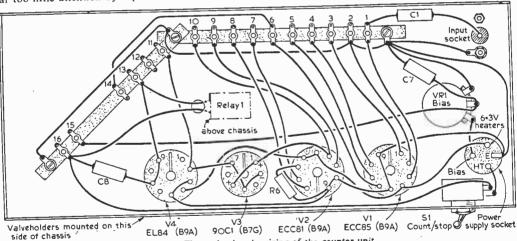
Fig. 2-The circuit of the Geiger head.

#### COMPONENTS LIST Resistors (All ±20% Carbon): Valves: 3.3k IW RIO IM IW VI ECC85 R2 150k 2W RII 3.9k 10W V2 ECC81 R3 22k 2W RI2 150k IW **V3** 90Cl (neon) R4 270k IW RI3 150k IW V4 **EL84** R5 150k IW **RI4** 10M 2W V5 MXI46 Geiger Tube (Mullard) R6 IOK IW **R15** 56k 2W V6 EC92 R7 220k IW **RI6** 100k 2W DI Metal rectifier 350V A.C./25mA D.C. 150k 2W R8 RI7 IM IW Sundries: R9 150k 2W RI8 10k 2W Three B9A valveholders, ceramic VRI 500k Pot. IW (w.w.) Two B7G valveholders, ceramic Two coaxial plugs and connecting lead Condensers: One digital relay, GPO, approximately CI 300pF ceramic 500VW 2000 $\Omega/25$ mA (Service Trading Co., 47-49 High C2 500pF ceramic 500VW Street, Kingston-on-Thames, Surrey.) C3 40pF ceramic 500VW Two toggle switches on/off, single pole $0.056\,\mu \mathrm{F}$ paper, $500\mathrm{VW}$ $8\,\mu \mathrm{F}$ 450VW electrolytic C4 One panel fuse, complete Chassis material, wire, solder, tagstrips, bolts, C5 C<sub>6</sub> 0·I μF paper, 500VW C7 $0.056\,\mu\text{F}$ paper, 500VW $0.01\,\mu\text{F}$ paper, 500VWsleeving, etc. Test tubes, rubber cork. C8 Power supply (preferably stabilised) 200-300V/ 100mA 6:3V 1:3A A.C. (heaters) Bias supply: about (-100)V on above power C9 16 μF 500VW electrolytic CIO See text next month CII 8 μF 350VW electrolytic unit, or otherwise a small 90V H.T. bottery CI2 0.005 μF ceramic 500VW Mains lead and plug

C8 appreciably larger than specified, as this would then destroy the steepness of the current rise at the start of each pulse, possibly leading to erratic counting. It is of interest to discuss why a neon, V3, is used to couple V2 to V4 instead of the usual coupling condenser. The reason is simple. The signal from V2 is of such a high amplitude that V4 is driven from beyond cut-off right up to heavy grid current by it, and such grid current would charge any coupling condenser heavily and very rapidly during the pulse. After termination of the pulse, this would leave V4 at a correspondingly greater negative voltage at the grid than the intended operating point. This would have the result that the circuit would be more or less blocked at V4 for any pulse coming in subsequently before the coupling condenser had discharged, and would also block the circuit at V2A grid, because the excess negative voltage at V4 grid would react via VR1 and R5 to pull down V2A grid too. The neon thus prevents the amplifier blocking when working at counting-rates approaching the limit of resolution. The alternative method of preventing gridcurrent blocking of amplifiers handling large signal amplitudes, namely the insertion of grid-stoppers, is not usable here, because it causes signal loss due to voltage drop across the stoppers, and thus makes the anode current rise in V4 too slow for stable counting.

It should be mentioned in passing, that the use of neons as coupling elements in amplifiers receives far too little attention by experimenters. They have

Returning to the digital counter circuit. A supply of about minus 100V is required on the bias line input (the exact value is not critical, but should be stabilised preferably-if the constructor has no power unit supplying this output in addition to normal H.T. and heaters, then a small 90V H.T. battery will serve the purpose excellently. This battery may be very small, as the current drain is only about a fifth of a milliamp (but do not forget to switch this battery off after use). The actual value of optimum bias taken to V2A and V4 is quite critical, and also dependent on the H.T. voltage used. The circuit operates excellently with any H.T. voltage between 200 and 300, but requires a different bias value with each H.T. voltage. Consequently the potentiometer VR1 has been incorporated, to set the bias to the optimum value. This potentiometer should be used more or less as a reaction control is used on a simple radio. Bias should first of all be increased until counting stops altogether even when the Geiger-head is supplying pulses at the input, and should then be reduced sufficiently to be quite certain of counting all pulses received. It is too difficult to make this adjustment with the mere 20 pulses per minute of the normal atmosphere, and thus it is advisable to place an alarm clock with luminous figures, or a pocket-watch with substantial luminous figures, near the Geiger tube. The radioactive content of any such luminous paint is sufficient to raise the counting rate of only 20 per minute right up to possibly several hundred per minute, which is



a number of advantages over condensers. In a normal class-A audio frequency amplifier, the coupling neons would be permanently struck, and thus represent D.C. coupling and theoretically freedom of all gain variation with frequency. Such an amplifier would amplify D.C., could have many stages, yet use otherwise conventional A.C.-ampligher circuitry with a single common H.T. supply on which all stages run in parallel as usual. And, as seen above, neon-coupling is free from blocking on transients. Of course, the value of cathode resistors, etc. would have to be modified in such an amplifier. But the principle is clear, and might interest more experienced constructors.

sufficient to make bias adjustments conveniently. At the slower counting rates, the bias setting is not in the least critical. If too high, counting stops altogether and if too low, then V4 runs at heavy anode current which will soon destroy it. Between these two points lies at least one third of the travel cf VR1, and slow counting is equally good at any point within this range. But if fast counting is desired, e.g. when checking the radioactivity of luminous paints, or possibly X-rays from poor or defective television cathode-ray tubes, it will be found that if the bias is set too far below the critical value, many counts will be missed.

# Faults in Transistor

ALIGNMENT AND CIRCUITRY

By J. Christy

RANSISTOR superhets usually have two intermediate frequency stages, and faults in these may cause lack of sensitivity, or oscillation and other troubles. The I.F. amplifier should be able to provide a very high gain, and if it does not do this, good reception of distant or weak stations will be impossible.

#### Alignment

Correct alignment of the I.F. transformers is easily achieved. If a signal generator is available, this may be set to the correct intermediate frequency (often 470kc/s) and coupled to the I.F. amplifier at a convenient point. If the circuits are out of tune, a fairly strong input may be needed, or it may be necessary to take the generator output directly to one of the transformers, a small isolating condenser being included in circuit. However, if the alignment is approximately correct, a very small signal will suffice. Merely placing the end of the generator prod or output lead a few inches from the mixer collector circuit should then give enough coupling.

When receivers have the popular type of push-pull output stage, battery current depends directly on the volume of the audio signal. If the generator is delivering a modulated output, a 15mA or similar meter in one battery lead is thus a convenient means of checking for maximum output.

When a good output is being obtained, when the I.F. stages are aligned approximately, the input from the signal generator should be reduced. Accurate adjustment is then easily achieved.

An insulated tool (made from an ebonite rod, for example), is used to adjust the I.F. transformer cores. They are simply screwed in or out, as needed, to obtain best results. Each core should have a fairly sharp tuning point.

If no generator is available, a local station should be tuned in, and the cores adjusted for best results. A weak station should then be found, with the audio volume control at maximum, and final adjustments should be made.

If all cores are in a reasonable position, it should generally be possible to align the aerial and oscil-

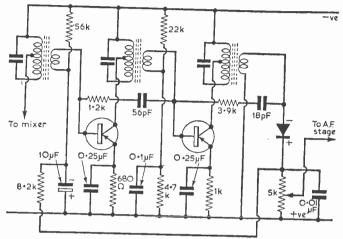


Fig. I—A typical transistorised I.F. amplifier circuit.

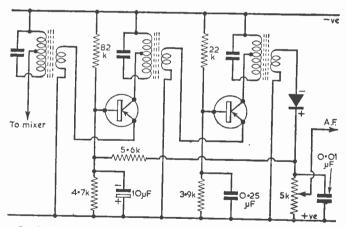


Fig. 2—An I.F. amplifier in which the transistors are used in the common base mode.

lator stages satisfactorily, even if the I.F. does not fall exactly at 470kc/s, or the correct frequency; if the frequency is much in error, correct ganging of aerial and oscillator circuits may be impossible.

When the I.F. transformers are adjusted without the aid of a signal generator, check that no core is fully in, or too far out. If one of the cores is not in the correct position, all of the cores should be readjusted by an approximately similar amount, and the stages are then realigned for best results at the new frequency.

# I.F. Stages

#### Neutralisation

Neutralisation is generally required, to maintain stability. In Fig. 1, the 1.2k resistor with 56pF condenser, and the 3.9k resistor with 18pF con-

denser form the neutralising circuits.

The values required can only be varied by a very small amount, if sufficiently accurate neutralisation is to be achieved. The values also depend on the transistors, and are a function of the transformer ratio. This means that with a given circuit, neutralisation can only be ensured if the transistors, I.F. transformers, and values in the neutralising circuits are as specified.

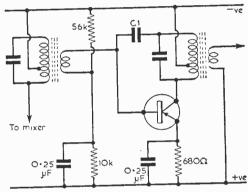


Fig. 3—An alternative neutralisation circuit.

As accurate values are so necessary, components of 2% tolerance may be specified. Individual 5% or wider tolerance components could be suitable, but other samples might be too far from the correct value, so that neutralising is incomplete. The overall feedback is small, and can easily be modified by stray capacity in wiring, especially if leads are long, or base and collector wires are close together.

If the receiver breaks into oscillation when the I.F. transformers are being adjusted for maximum sensitivity, this indicates instability in this section. This oscillation may appear as a continuous whistle or heavy background hiss, or it may only arise when tuning through a weak station. If the instability ceases on tuning in a powerful signal, so that AVC reduces gain, or if it ceases with one or more I.F. transformers only very slightly de-tuned,

its cause is probably not serious.

#### Common Base Circuit

A typical I.F. amplifier of this type is shown in Fig. 2.4 The gain can be expected to be less than with the common emitter type. This circuit is given because it will be found in some receivers. Each base is supplied through a potential divider, and is earthed to intermediate frequencies by the condeners wired from the base to the positive line.

The emitters are connected directly to the trans-

secondaries, these components being designed for this type of circuit.

Decoubling

In Fig. 1, each emitter resistor is by-passed with a 0.25 µF condenser. In midget sets, lower values, such as  $0.1\mu F$  or  $0.04\mu F$ , may be encountered. These lower values usually give an increased possibilty of instability, which may show as oscillation, motor-boating, or whistles on weak signals only. In such cases, it may be worth increasing the by-pass values. This can easily be done by temporarily wiring a larger capacity condenser in parallel with the existing condenser. If this cures the trouble, the larger value may be permanently incorporated.

In Fig. 1, the first I.F. transformer secondary is decoupled by the 10µF condenser. A large value is required here, as audio frequencies will be present in the automatic volume control line from the diode. Such condensers may deteriorate, and need replacing when they no longer offer a low-impedance path for intermediate frequencies. If so, a  $0.1\mu F$  or similar condenser may be shunted in

parallel.

In the second stage, a  $0.1\mu F$  condenser is used, in parallel with the 4.7k resistor. Midget receivers may use 0.04µF here, but 0.1µF or 0.25µF can often be more suitable. If the 1.F. stages are unstable, the capacity can be temporarily increased, to see if results improve, as already mentioned.

#### Modified Neutrallsing and By-passing

In some circuits, neutralisation is obtained by using a small capacity, C1 in Fig. 3, from transformer to base. The value will depend on the transistor, but may be in the region of 5pF. Such small capacities are sometimes obtained by means of twin insulated wires, or a twin-lead wire, reduced in length until the required value is reached.

When the neutralising condenser is in this position in the circuit, its value is not influenced much by the transformer ratio, but will depend on the transistor, and position of the I.F. transformer

primary tap.

In some circuits, by-pass condensers are not taken to the earth line afforded by the battery positive circuit. Instead, the by-pass condensers for any

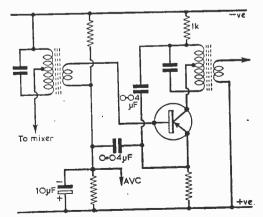


Fig. 4—An example of a circuit in which the by-pass condensers are taken to the emitter of the transistor instead of to the positive line.

stage are taken to the emitter of the transistor, as in Fig. 4. This can be a little confusing, if not expected, but otherwise the circuit is practically the same as that in Fig. 1.

#### Diode Detector

Receivers of this type use a diode, as detector, and to provide AVC. If this diode has a low efficiency, good results will never be achieved. If no means of testing the diode are to hand, and it is suspected, it should be replaced by a new one such as the OA&1 or GEX58,

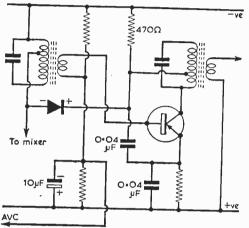


Fig. 5—The typical circuit arrangement for a damping diode.

The diode must be wired in the right way round, as shown. When signal strength increases, an increased positive voltage is developed at the positive end of the diode (Fig. 1). This is transferred to the first I.F. stage, through the 8-2k resistor, and makes the base voltage more positive, reducing amplification. This provides some measure of AVC (Automatic Volume Control) action, but the effect is much less than with most valve receivers. If the set is stable on loud signals, but unstable

If the set is stable on loud signals, but unstable on weak signals, this probably arises from the AVC action, as already explained. That is, the instability is not severe, so that the reduced gain on a strong signal temporarily clears the fault

on a strong signal temporarily clears the fault.

Some receivers employ a damping diode, in addition to the AVC diode. One method of connecting this is shown in Fig. 5. The collector current through the 470\Omega resistor results in the positive end of the damping diode being slightly positive, and the diode has little effect on the mixer I.F. transformer, but, when signal peaks exceed the damping diode potential, the diode conducts, loading the transformer and reducing gain. This gives increased AVC efficiency, and in particular avoids overloading on very strong signals.

#### Reflexed Amplifier

A circuit similar to that in Fig. 6 is used in some receivers. Here, one transistor acts as both I.F. and A.F. amplifier. This gives improved results, from a given number of transistors, but is somewhat less effective than the use of separate transistors.

In this circuit, the first I.F. transformer secondary is by-passed to the emitter (see Fig. 4) by the  $0.01\mu F$  condenser. Instability at intermediate frequencies may arise from this condenser being defective or disconnected. The primary of the second transformer is similarly decoupled to the emitter. The values used  $(0.01\mu F)$  are rather small, but cannot very well be much increased, because they are in parallel with the audio signal, and thus reduce top response.

After detection in the normal way, by the diode, the signal passes from the 5k volume control slider, through the  $6\mu$ F condenser and 3.9k resistor, and the secondary of the I.F. transformer, which has negligible impedance at audio frequency. The transistor then acts as an A.F. amplifier, and the A.F. signal is developed across the 1.2k resistor.

A large emitter by-pass capacity (50µF) is required, as this stage is acting as an amplifier at audio frequencies, as well as intermediate frequencies.

Oscillation at audio frequency is not very likely. The stage can be tested at A.F., if necessary, by temporarily disconnecting the diode, and feeding in an A.F. signal from an outside source.

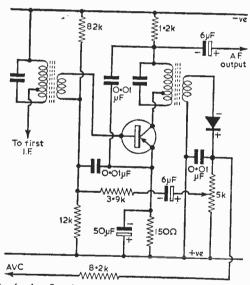


Fig. 6—A reflexed circuit—here, one transistor is used to amplify both I.F. signals and A.F. signals.

After any of the points described have received attention, it should be possible to adjust the I.F. transformer cores for best results.

If it is necessary to connect the generator directly to the receiver, this may be carried out by taking a  $0.01\mu\text{F}$  or similar isolating condenser to the base of the first transistor (the mixer). If the generator signal is taken to a transformer or collector circuit, the core will probably need slight readjustment after the generator lead is removed.

The transistors used in such stages should have a cut-off frequency of 5Mc/s or higher, so reliable transistors, designed for such purposes, should be employed. General lack of sensitivity may arise from poor transistors in these stages.

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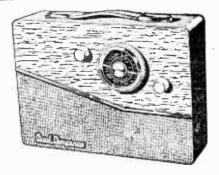
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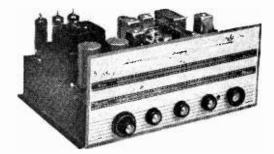
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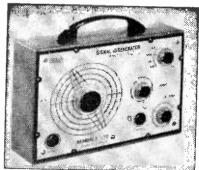
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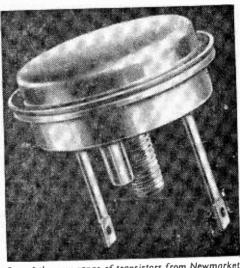
A new push button switch from the Plessey Co. Ltd.

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This switch is made by The Plessey Co. Ltd., Ilford, Essex.

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One of the new range of transistors from Newmarket Transistors Limited.

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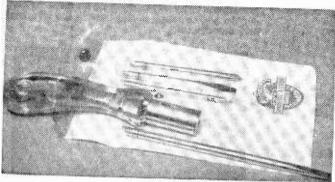
The distinguishing features of the NKT 500 range are the very high current ratings (up to 25A), a guaranteed minimum current gain of 12 at the

maximum rated collector current, high power rating and voltage ratings of 60 and 30. The low saturation voltage results in low-self dissipation when used for switching applications. The drive voltage for peak collector current is low and distortion is minimised by controlled beta fall off.

These transistors are manufactured by Newmarket Transistors Limited, Exning Road, Newmarket. Suffolk.

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The extremely small size of these new devices and their tab-ended configurations, have reduced

their inductance to such an extent, that a typical limiting frequency of oscillation of 900Mc/s is now attainable.

A single version, known as the JK30A, is now in production. It is being followed by a new version incorporating a matched pair of tunnel diodes and forming a single integral unit having three tabs. These units are matched for peak current and capacitance and are intended for applications in the computer field. They may be used in high speed logic and counting circuits or as the thresh-hold amplifier/gate at the input of a pulse amplifier. Standard Telephones and Cables Limited, Connaught House, Aldwych, London, W.C.2.

The complete screwdriver with four blades costs 19s. 6d. from most hardware and tool dealers. Replacement blades can be obtained at 2s. 3d. each. J. Stead and Co. Ltd., Manor Works, Cricket Inn Road, Sheffield 2.

#### MINIATURE SOLDERING TWEEZERS

A NEW type of soldering instrument has recently been developed to meet the need for precision soldering in laboratories and on production lines with micro-miniature circuits modules, diodes, transistors, relays, etc.

Designed, developed and manufactured in the U.K. by Oryx Electrical Laboratories Ltd., the instrument is in the form of a pair of tweezers having separate heating elements to both tips. The elements operate at up to 554°F tip temperature from 6V supply.

Light to handle and requiring only minimum finger pressure, these tweezers provide unobstructed view at all times for close precision soldering. These soldering tweezers are marketed in the U.K. by W. Greenwood Electronics Ltd., 667 Finchley Road, London, N.W.2.

#### 5-DIGIT VOLT/OHM METER

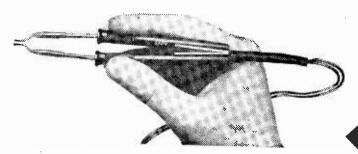
A NEW addition to the Ferranti range of digital instruments is the type D201, 5-digit volt/ohm Meter. This instrument, which makes extensive use of semiconductor, elements, has been designed to measure D.C. voltage and resistance over a wide range to an accuracy of better than 0.03% of reading of ±3 digits, whichever is the greater.

The voltage range is 0.0001 to 1000V D.C. and the resistance range  $000.01\Omega$  to 1299.8k. The ranging is automatic on both inputs, except for the most sensitive range in each instance, which is selected by a "divide by 10" switch. D.C. current can be measured from full scale readings of  $1.9999\mu$ A to 1.9999mA after slight modification to the instrument. The conversion time is normally 250 milliseconds—irrespective of reading—and the input impedance is 4.44M on all ranges, although this can be increased to 10M if required.

Servicing of the instrument has been simplified by using detachable sub-units which are easily maintained, printed circuit cards being used for the transistor circuitry.

The instrument is housed in a cabinet measuring 20in. × 15in. × 14in. and weighs 35lb approximately. A rack mounted version is also available.

The type D201 meter is made by Ferranti Ltd., Ferry Road, Edinborough 5, Scotland.



Oryx soldering tweezers

#### MONTH ONLY! THIS

"SONOTONE" MIN. EARPIECE free with all parts totalling £4.10.0 or over

#### TRANSONA-6

(6 Transistors plus 2 Diodes)

M/L & T. BAND



350 Mw XCI01's push-pull output Transistors, 1Powerful magnet 3in. high grade speaker. Push-pull trans-formers. This is a top performing receiver.

Nearly 30 stations listed in one evening including Luxembourg loud and Luxembourg loud and clear. A pleasure to listen to. FERRITE ROD to. FERRITE ROD AERIAL. All parts sold separately, including pale blue gleaming polystyrene case with duo-diffusion grilles in red. Uses 9 volt battery.

Sockets for car aerial.

Total building cost **£5.19.6** P.P. 3/-. Size 6½ × 4½ × 1½in.

"Agreeably surprised with Trawler Band reception. Luxembourg as loud as local. Your easy build diagram helped a lot. .. my first attempt."—H.S., Penzance, Cornwall (poor reception area).

PARTS PRICE LIST AND EASY BUILD PLANS 1/6

#### **TRANSONA-4**

(4 Transistors, plus 2 Diodes)

Miniature speaker, FERRITE ROD AERIAL. MW/LW and Trawler Band coverage down to 80 metres. On test tuned in nearly 30 stations inc. Luxembourg. Easy-build plans 1/3. Handsome pocket case.



May be built for 52/6 P.P. 3/-.

"Best transistor set I have ever built-dozens of stations."-A.G.H., Deal, Kent.

PARTS PRICE LIST AND EASY BUILD PLANS 1/6

#### **BEGINNERS** PUSH-PULL FIVE

(5 Transistors, plus Diode)



- 21 in. M/C Speaker Ferrite rod aerial
- Tuning condenser Volume/oscillator con-
- Case with speaker grille in red.
- Fully tunable over med/ long waves Simple assembly dia-
- grams 250 Milliwatts output
- stage Can be built for 59/6 P.P. 3/-With 3" speaker

PARTS PRICE LIST, etc. 2/-

68/- post free

#### **BEGINNERS POCKET 5**

(MW/LW and TRAWLER BAND)

(5 Transistors, plus 2 Diodes)



Designed round supersensitive FERRITE ROD AERIAL and 3in. speaker. Attractive case in black with speaker grill in red. On test Home, Light, Radio Lux., and many Continental stations we received.

Total cost of all parts £2.19.6 P.P. 3/-.

EASY BUILD PLANS AND PARTS PRICE LIST 1/6

#### NOW THE SUPER SEVEN 4-WAVEBAND RADIO

(7 Transistors plus 2 Diodes) 3 R.F. STAGES

- Mullard and Surface
  Barrier Transistors
  Coverage of Medium,
  Long Waves, Trawler
  Band and approximately 20-60 metres short wave
- ★ Use as domestic radio, car radio or fit with strap (not supplied) for carry-about.

No aerial required except for use as car radio and for short waves

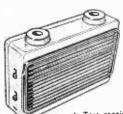


3-inch speaker but will drive a larger speaker Performance comparable to many receivers costing treble 400 milliwatts output stage

May be built for £6.19.6 plus 3/6 post, etc.
PARTS PRICE LIST AND EASY BUILD PLANS 2/-

#### SUPER SIX DESIGN NFW

MED/LONG WAVES, TRAWLER BANK TO APPROX. 40 METRES TRAWLER BAND AND S.W.



- 6 Ist grade Transistors (inc. Mullard and Surface Barrier) plus 2 DIODES. Top grade 3in. L/speaker. 2 R.F. Stages for extra
- hoost. High Q 7in. Ferrite Rod Aerial.
- Easy-build diagrams No aerial or earth required (except as car radio).
  Attractive pale blue case with speaker grilles in red.
- 350 Milliwatts output stage

Sockets for car radio.

\*\* Test receiver tuned in over 30 stations (inc. Luxembourg loud and clear.)

THIS FINE RECEIVER MAY BE BUILT FOR Plus 3/- P.P. #6.9.6

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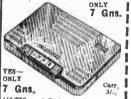
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CIP-6	600ft. 5in.	Standard Play	13/-
LP-9	900ft. 5in.	Long Play	
CMXP-12	1,200ft, 5in.	Double Play	17/6
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LP-12	1,200ft, 51in.	Long Play	16/-
CMXP-18	1,800ft, 5fin.	Double Play	19/6
IP-12	1,200ft. 7in.	Standard Play	37/-
P-18	1,800ft. 7in.	Long Play	21/-
MXP-24	2.400ft, 7in.	Double Play	28/6

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Many other types available including "Scotch," "EMI," "Triton," "Synchrotape," B.A.S.F., etc. Send s.a.e. for our huge money-saving literature on Tayes and Accessories.

BARGAIN OF THE MONTH: Telefunken Stereo Hi-Fi Amplifier



10/250 v. A.C. input. 5 watt undistorted output (10 watts nominal) and 12 s s. 2in., weight 9th. illustrated easies available.

CRYSTAL MICROPHONE MODEL BM. 3

Three-way mike for hand, desk or floor stand use. Response 100-8,000 c/s. Scantitvity —62418. Length 7in. Head dia. 14in. Supplied with neckband. Terrific performancet Outstanding value at ONLY 39/6. P. & P. 2/-

AVO MODEL 7
Latest Ministry release of this well-known test instrument Supplying 50 ranges of current, voticase and resistance tosts. Computer with leads and batteries. Ready for use. Perfect condition. \$11/10/-. Carr. 5/-.

SUPER QUALITY TEST LEAD KIT



Post Paid Comprises | leads and prods, English and Continental type plugs, spade terminals and crocodile crocognic clips. Com-plete in at-tractive case

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TELESCOPIC FLOOR STD. HEAVY 9in. dome chromium base, chromium stand with sorew top.
Extends to approx. 6ft. Suitable for our mikes, etc.; \$2.15.0, Carr. 5/-. POCKET TEST METER MODEL "CASIE H.20"

(4,000 O.P.V.) FOR ALP POST FREE

A pocket size individual circuit tester with bakelite panel and metal cabinet. Complete with test leads batteries and ready to use. Ranges: D.C. Volts: 10-50-250-1,000 v. (2,000 o.p.v.). D.C. Current: 250(LA/10 mA/250 mA. Resistance: 0-10 K ohms/0-1 M ohms (by 3V internal battery). Resistance: 0-10 K ohms/0-1 M ohms (by 3V internal battery).
Decibels: -20 to + 22db (0dB -- 0.775v. 8ize: 4fin, x 3fin, x 1fin.

Also available: MODEL TK.50

1.000 o.p.v. Ranges; D.C. ma; 1-250 mA., D.C. and A.C. Volta: 10-250-500-1,000 v. Ohms: 0-10K nhms 0-100K ohms, \$2,7.6,

AVO VALVE TESTER

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Outstanding offer of this fine test instrument. Supplied in good condition. Equipment is in two parts—valve panel with selector switches—and meter with voltage adjustment controls, etc. 12 valve bases and 3 blanks. Very simple to operate. ONLY \$5.19.6. Carr. 716. (Adaptors to the control of the control

SUPER QUALITY HI-FI DYNAMIC (M/C) MIKE



B7G, B8A and B9A bases. \$10. Carr. 7/6.

SPEAKER BARGAINI
Goodman's Hi-Fi AX 10M 110, 15 ohm Few o. iy at \$4.15.0. Carr. 3/6.
Brand New and Boxed.

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TRADE SUPPLIED Our well-known Traveller is now supplied with printed circuit, 3 top quality transistors, 2 diodes in latest circuitry, £3.17.6.

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The second of our Transistor Radio designs. 4 Mullard tran-sistors in a circuit specially designed around the new AF117 designed around the new AFII/
diffused alloy R.F. transistor.
OC81D-20C81. Push-pull output
on printed circuit. Sensitivity
approx. I m/v per metre. Airspaced tuner. Luxembourg guaranteed at excellent volume (if normally receivable).

Both sets of components have following outstanding features. Both sets of components have following outstanding features. Supplied complete with full Easy-to-follow Instructions. Physical layout and theoretical circuits. 3in. Moving Coil Speaker. Fully tunable on Medium Waves, Ferrite Rod Aerial. Solenoid Wound Coils. Plug in 9 v. Battery. Fully portable. No Aerial or Earth required. All components tested and guaranteed 12 months. Complete sacisfaction or money refunded. All components supplied separately. Instruction Book 1/6 post free. Supplied free with set of components. ALL PARTS and BLUE PLASTIC CASE AS ILLUSTRATED. Post and packing 3/6. Personal earplece with instructions 9/-, Battery extra 2s 6d. P. & P. 3/6.

G.E.C. S1, 3/6; G.E.C. S3, 3/6; SB078, 8/6; Mullard AF117, 12/6; Matchd. Pr. OCB1 and OCB1D 22/6; 6 ins. Ferrite Rod ½ or ¾ ins., 179; Litz Wire 3d. yd. 5K Edgewise V/C with S/W, \$7-; 32 mfd., coil Loudspeaker, 10%, Plus P.P. 2/6.

Complete range of Caby Test Meters, prices 54/-, 97/6, 130/-.
S.A.E. for Descriptive Leaflets.

## Short-wave Listeners' Log

HE choice of a suitable receiver is not always easy, as prices and specifications vary so much. With home-built receivers, improvements and additions can, of course, be made. There are also a number of current communications receivers available, and full details of these can be obtained from the makers. The price is generally quite high.

When a ready-made receiver of high efficiency, at relatively low cost, is required, a second-hand, used, or surplus model is probably the only choice. Brief details of some of the most popular and suitable receivers of this kind are given here.

R1155. About 16½in. × 9in. × 9in. Seven valves, plus two in unused direction-finding circuit, and magic eye tuning indicator. BFO (beat frequency oscillator for C.W. morse) Needs separate power pack and output stage for speaker. Many cover 17-4000m, with gap between 100 and 200m, but other coverages available. Frequency calibrated dial.

R1224A. About 19in. × 14\fin. × 9\fin. Battery 5-valver: R.F./F.C./I.F./DET/output, tuning 30-300m in 3 bands. Charts for numbered dial.

CR100 and B28. About 16in. × 16\frac{1}{2}in. × 12\frac{1}{2}in. Ten to 5,000m in 6 switched ranges. Frequency calibrated and logging scale. Eleven octal valves. Internal power pack. Controls: Tuning, band-change, pass-band (6,000-100c/s) crystal filter, aerial trimmer, H.F. gain, A.F. gain, BFO, function switch, on/off switch, and noise limiter on some models.

CR150. About 16½in. × 17in. × 13½in. Double superhet model. 5-150m in 5 switched bands. Noice limiter, crystal calibrator, S-meter. Small triode output stage. Separate power unit.

AR88D. About 194in. × 194in. × 11in. About 9.5 to 550m in 6 switched hands. Twelve valves, plus rectifier and voltage regulator, full communications facilities. Internal power supply. Companion models with different coverage.

HRO. About 17in. × 11½in. × 8½in. Nine general coverage plug-in coil units over 10 to 6,000m. In some cases special coil units giving bandspread tuning over amateur bands are available. Numbered dial tuning. Ten UX type valves, but octal valves in later models. Separate power pack. BFO, S-meter and full communications facilities. Some models have fewer coils.

Collins T.C.S. About 13in. × 11in. × 11in. For use with companion transmitter, 25 to 200m. Octal valves. May be run from separate rotary generator.

BC312. About 18in.  $\times$  10 $\frac{3}{4}$ in.  $\times$  9 $\frac{1}{4}$ in. Nine valves, covering 17 to 200m. BFO and other facilities. Intended for 12V accumulator supply.

Any of these receivers will provide very good results. The band coverage available may be

important, as some receivers have a more limited short wave coverage than others. Those sets which include normal long and medium wave bands will provide very good long-distance reception, on these bands, in addition to covering S.W. bands. Receivers which require a separate power unit, or are intended for accumulator or battery running, are not suitable when a single, self-contained set, for A.C. mains operation, is required. In all cases a separate, moving-coil permanent magnet speaker is necessary.

Actual models naturally vary somewhat in age, condition, and exact details, but it is nearly always possible to obtain a reasonably complete specifica-

tion in advance.

A brief description of features which will be found in detailed specifications should be helpful. Those generally present are as follows:

#### Pass-band Selector

A control giving variable selectivity, typically from 100 to 6,000c/s, in a high-grade set. The very high degrees of selectivity can only be used for C.W. (morse) reception, as a rule.

#### Function or Operation Switch

A control bringing the AVC in or out, possibly bringing the BFO in, for C.W. reception, and leaving the receiver standing by with heaters on but H.T. off.

#### H.F. or R.F. Gain

Control of the R.F. stage or stages, and possibly the I.F. stages.

#### A.F. Gain

The usual type of audio volume control.

#### **BFO Pitch**

Control adjusting the pitch of the beat frequency oscillator, to give best results through interference when receiving C.W. (morse).

#### Crystal Filter or Phasing Control

This allows adjustment of a crystal filter, giving high selectivity, and allowing an interfering C.W. signal to be rejected or reduced.

#### Aerial Trimmer

A control, frequently panel operated, allowing the first circuit to be trimmed manually, to compensate for stray aerial capacity.

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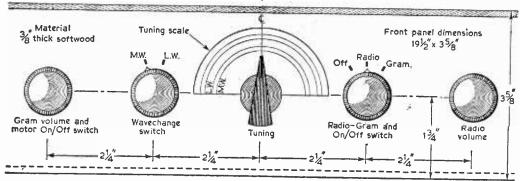


Fig. 24—The layout of the front panel of the radiogram.

#### Wiring the three sections of the

## CITIZEN

## together, to form the complete radio or radiogram

(Continued from page 817 of the January issue)

AST month, the construction of a cabinet for the 'Citizen' was described; it now remains to describe the mounting and inter-wiring neces-

sary when the units are incorporated in the cabinet. The cabinet described last month was designed to provide a modern housing for the 'Citizen' and a battery record player to make a complete battery-operated radiogram. However, for those readers who require only a battery operated radio set, the wiring needed to connect the 'Mini-Amp' to the two units of the 'Citizen' will also be described.

#### Wiring for the radiogram

Before this can be carried out, the 'Citizen' must be tested and aligned as described in the December issue (on pages 718 and 719). It is very important that the units should work correctly before starting to mount them in the cabinet.

The control panel of the radiogram is shown in Fig. 24. From this it can be seen that six control knobs are provided. There are: a 'gram volume and

'gram motor on/off switch (this switch ensures that the 'gram motor cannot be left running when the radio is in use); a wavechange switch; a tuning condenser; a three-position switch for radio/gram change-over and (in the third position) radio off switch, and a radio volume control.

(Continued on page 941)

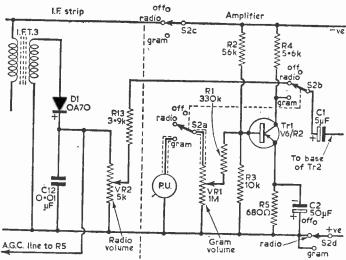


Fig. 25—The theoretical diagram of the connections needed for wiring the units as a radiogram.

#### Easy - to - build kit - sets of

THE "MOHICAN" GENERAL COVERAGE RECEIVER Model GC-1U Fully transistorised, 4 piezo-electric transfilters. Excellent portable or piezo-electric transfilters. Excellent Fixed Station receiver for the amateur and short-wave listener. £38 15 0

SHORT-WAVE TRANSISTOR PORTABLE Model RSW-1 Extending aerial, leather case, four band (2 short-wave, Trawler and Medium). £22.10.0

6-TRANSISTOR PORTABLE Model UXR-1 Pre-aligned i.F. transformers printed circuit, 7 × 4in. high-flux speaker. Real hide case. £14.18.6

DUAL-WAVE TRANSISTOR RADIO UJR-1
This sensitive headphone set is a fine introduction to electronics for any youngster. £2.16.6

HI-FI F.M. TUNER Tuning range 88-108 Mc/s. For your convenience this is available in two units sold separately: Tuning Unit (FMT-4U) with 10.7 Mc/s. I.F. output £3.5.0 (inc. P.T.) I.F. Amplifier (FMA-4U) complete with cabinet and valves £14.16.0

HI-FI 16W STEREO AMPLIFIER Model S-88 20mV. basic sensitivity (4 mV. available, 76 extra.)
Ganged controls. Stereo-Monaural gram. radio and tape recorder input. Push-button selection. Two-tone grey metal cabinet.

6W STEREO AMPLIFIER Model S-33 3 watts per channel, 0.3% distortion at 2.5 w/chn 20dB N.F.B. Inputs for Radio (or Tape) and Gram. Stereo or Monaural, ganged controls. Sensitivity £12.8.6

TRANSCRIPTION RECORD PLAYER, GL-58 Goldring—Lenco four speed unit. G.60 pick-up arm and infinitely variable speed adjustment between 33½ and 80 r.p.m. with fixed speed at 16 r.p.m. Balanced turntable (3½ lb.). Stereo. £20,12.2

HI-FI SPEAKER SYSTEM Model SSU-1 Ducted-port bass reflex cabinet "in the white", speakers. With legs, £11.18.6. £1 £10.17.6

"COTSWOLD" HI-FI SPEAKER SYSTEM KIT Acoustically designed enclosure "in the white" 26 × 23 × 15 in., housing a 12 in. bass speaker with 2 in. speech coil, elliptical middle speaker and pressure unit to cover the full frequency range of 30-20,000 c/s. Complete with speakers, cross-over unit, level control, etc.

COMPLETE MATCHED STEREO OUTFIT includes record player, amplifier and twin speaker systems (pedestal speaker legs optional £44.9.4 £2.2.0 extra).

STEREO CONTROL UNIT USC-1 Luxury model with press-button inputs to suit any pick-up or tuner and most tape-heads Output 1.3 v. R.M.S. per channel. Printed

circuit construction.

MULTIMETER Model MM-1U Measures wide range of voltage, current resistance and dB in over 20 ranges. Sensitivity 20,000 ohms/ volt D.C. and 5,000 ohms/volt A.C. 0-1.5, 1,500 ovolts A.C. and D.C. 0-150µA, 15 A D.C. Resistance 0.2Ω to 20MΩ. 4½in. £11.18,6 Heathbit DAYSTROM

#### highest quality at lowest cost

F.M. TUNER

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5.88



DX-40



UXR-1



OS-L





AG.9U



GC.IU

AMATEUR TRANSMITTER Model DX-100U

Covers all amateur bands from 160-10 metres. 150 watts D.C. input. Self-contained including Power Supply Modulator V.F.O. £81.10.0

AMATEUR TRANSMITTER Model DX-40U From 80-10 m. Power input 75 w. C.W., 60 w. peak C.C. phone. Output 40 w. to aerial. Compact and self-contained. Prov. for V.F.O.

VAR, FREQ. OSCILLATOR VF-1U Calibrated 160-10 m. Fundamentals on 160 & 40 m. Ideal for our DX-40U and similar transmitters. £11.2.0

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AUDIO SIGNAL GENERATOR Model AG-9U 10 c/s to 100 kc/s. switch selected. less than 0.1% 10 v. sine wave output metered in volts and dB's. Distortion £19.19.6

VALVE VOLTMETER Model V-7A Measures volts to 1,500 (D.C. and R.M.S.) and 4,000 pk. to pk. Res. 0.10 to 1,000MΩ. D.C. input imped. 11MΩ. Complete with test prods leads and standardising battery.

Portable 23/4in. SERVICE 'Scope Model OS-1. Compact portable scope ideal for servicing and general work. Y amplifier sensitivity 10 mV/cm; response ± 3 dB 10 c/s-2.5 Mc/s. Time base 15 c/s-150 kc/s. Printed circuit. Case 7\frac{3}{2} \times 4\frac{3}{2} \times 12\frac{1}{2}in. £19.10.0 Wt. only 1011b.

Sin. OSCILLOSCOPE Model O-12U Wideband amplifiers, essential for TV servicing. F.M. alignment, etc. Vertical freq. response 3 c/s. to over 5 Mc/s. without extra switching. T/B covers 10 c/s to 500 kc/s. in 5 ranges.

RES - CAP BRIDGE Model C-3U Measures sistance 100Ω to 5MΩ, capacity 10pF to 1000μF, and power factor. Test voltages 5-450 v. with automatic safety switch.

SINGLE CHANNEL AMPLIFIER, MA-12 10-12 watt Hi-Fi amplifier, low distortion £10.19.6 and wide frequency range.

HI-FI EQUIPMENT CABINETS Range of cabinets available with at least one to suit your particular needs. From small to large, housing Tape Deck, Record Player and full equipment. In the white for finishing to personal taste.

From £11.5.6 to £17.18.6

GRID DIP METER Model GD-1U from 1.8 Mc/s to 250 Mc/s Complete £10.9.6 set of plug-in coils provided. ----- TAPE RECORDING/PLAYBACK

AMPLIFIER Model TA-1 Monaural (TA-IM) £18.2.6. Conversion unit to Stereo £6.10.0. Stereo (TA-IS). \*PACKAGED DEALS\* Equipment including TAPE DECKS, RECORD PLAYERS and DECCA ffss PICK-UPS. Write in to see how these deals save you further

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meter, 50µA f.s.d. Please send me FREE CATALOGUE (Yes/No)\_ Full details of model(s)\_ NAME -ADDRESS \_\_\_\_ PW<sub>2</sub>

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P.C.R. COMMUNICATION RECEIVERS

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8 valves. Frequency coverage on three bands: 850-2,000
metres, 180-550 metres, 8-18 Mc/s. Super slow motion
drives. Act trimmer. AS NEW bullt-in speaker £61.19.6,
carriage 7/6.
F.C.R 3 Communication Receiver. 190-550 metres,
2-7 Mc/s, 7-23 Mc/s. Output for phone or 3 ohms speaker. AS
NEW, 8 sns. carr. 7/6. Both above models are available with
Internal Power Pack to operate on 200/250 v. A.C. at 39/6
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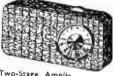
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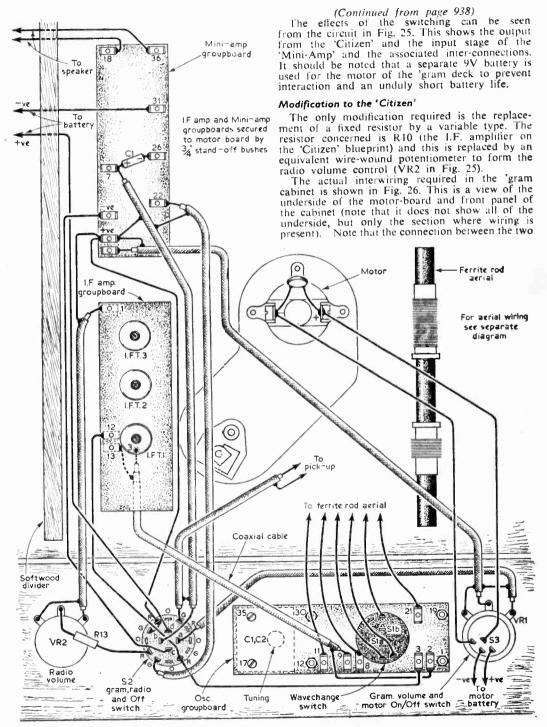


Fig. 26—The radiogram wiring.

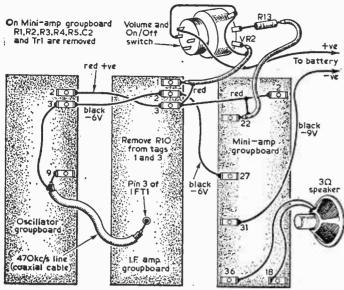


Fig. 27—The interwiring for the tree sections as a radio.

group boards on the 'Citizen' which carries the I.F. signals is made of coaxial cable to reduce the capacity of this link. The wiring of the ferrite rod aerial windings is not shown since it was given earlier (Fig. 17 on page 718 of the December issue). The three tag-boards are mounted by the means of stand-off bushes as stated in Fig. 26. A diagram of the mounting of the oscillator section of the 'Citizen' was given in Fig. 22 in the January issue.

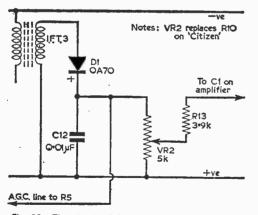


Fig. 28—The circuit of the radio wiring. Note that R4 has been removed.

The inter-wiring can be carried out and then checked most carefully—if, for example, the battery feeding the 'Citizen' and 'Mini-Amp' were wired incorrectly, the transistors would be ruined.

Following this check, the unit can be switched on and tested. Results from the radio may not be

as good as they were before mounting the units in the cabinet and the alignment procedure may be gone through again now that the units are occupying their final positions. The alignment was described in detail in the December issue on pages 719 and 720—it starts at the side-heading 'The Alignment'.

#### The 'Citizen' without the gram unit

The interconnection for using the 'Citizen' with the 'Mini-Amp' to form a superhet radio set are shown in Fig. 27. The three group boards are shown viewed from the tag sides and not from the riveted sides. As in the radiogram, it is necessary to replace R10 on the 'Citizen' with a variable resistor — see Fig. 28. Since the 'Citizen' gives a high-level output, certain components can be removed from the 'Mini-Amp' and these are listed in Fig. 27. (They are R1, R2, R3, R4, R5, C2 and Tr1.)

the 'Mini-Amp' and these are listed in Fig. 27. (They are R1, R2, R3, R4, R5, C2 and Tr1.)

As in the radiogram, the connection between the two group boards on the 'Citizen' which carries the I.F. signals is made of coaxial cable to reduce the capacity which the interconnection places across the I.F. output coil.

When the three units have been mounted in the cabinet (which may be of any form) the alignment should be carried out again.

### SHORT-WAVE SECTION

(Continued from page 923)

#### Conclusion

Although the unit described is an efficient one it is open to improvements. It would not be difficult, for example, to tune the grid circuit of V1 to improve sensitivity and the spare section of C6 could be employed in this connection, aerial coils being mounted in front of V1 for this purpose above chassis.

#### **VI Substitute**

A valve of different type may be used for V1 if desired provided it has variable- $\mu$  characteristics and that attention is paid to the basing which might well be different. A metal rectifier may also be used in place of V3 if preferred and in some cases it might be possible to link the receiver AVC line to the pre-selector.

NOTE—The isolating transformer, T1, should not be omitted or exchanged for a heater transformer, neither should the preselector be used in conjunction with a receiver of the A.C./D.C. class or danger to life might result.

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# CONDENSER

This article is expressly written for a particular type of amateur constructor: the beginner who, though perhaps familiar with condensers and their use in practice, may not yet know what a condenser actually is, how it functions as it does and why.

By S. R. Vella

EFORE explaining what constitutes a condenser, we have to distinguish between a conductor and an insulator. A conductor allows electricity to pass through it, while an insulator does not. For example, copper, silver and most metals are conductors; while air, mica, glass, paxolin are insulators. A conductor allows electricity to pass through it by virtue of its free electrons (the electrons in its atoms' outer shells).

#### The Dielectric

When two conductors are separated by an insulator, we have what is called a capacitor or condenser—a device capable of storing electricity. The insulator separating the two conductors, which might be a vacuum, air, glass etc., is called the dielectric. For the purpose of discussion, let us imagine the two conductors constituting our condenser in the form of two separated metal plates to which are connected suitable lengths of flexible wire so that we can connect them in a circuit as will be explained later on. This arrangement (Fig. 1) constitutes the simplest form of condenser.

It should be noted that the capacity of the condenser (i.e., the ability to store electricity) in Fig. 1 is very small, the condenser being made up simply of two relatively small metal plates with air as the dielectric.

The capacity of a condenser depends on:

(1) the area of the plates.

(2) the distance between the plates.

(3) the material of the dielectric.

The capacity of a condenser increases as the area of the plates is increased and the distance between them is diminished. In practice, the dielectric is

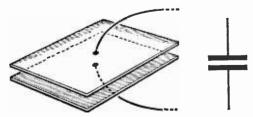


Fig. 1 (left)—The simplest form of condenser, or capacitor.

Fig. 2 (right)—The theoretical circuit symbol for a condenser.

very rarely air. It is usually either mica or paper. Fig. 2 shows the theoretical representation of a condenser.

#### Storage of Electricity

We have stated above that a condenser is a device capable of storing electricity. But how exactly is this effected we ask? Why and where is electricity stored in the condenser?

Let us try to visualise what happens when we connect our condenser to a battery. This is shown in Fig. 3. Free electrons from plate 1 will be attracted to the positive side of the battery, thus leaving plate 1 with a deficiency of electrons i.e. positively charged. The electrons attracted from plate 1 of the capacitor to the positive side of the battery will appear (after flowing through the battery) on the negative side. This surplus of electrons or negative charge will therefore also

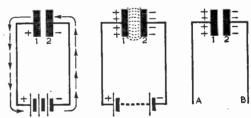


Fig. 3 (left)—When a condenser is connected to a battery, it becomes charged, as shown.

Fig. 4 (centre)—The charged condenser—the electric field between the two plates is represented by the lines from one plate to the other.

Fig. 5 (right)—Even if the battery is removed from the circuit, the condenser remains charged.

appear on plate 2 of the condenser since this is directly connected to the negative side of the battery. We may now say that the condenser is charged; and the situation is represented in Fig. 4. In other words, we may say that what actually happened during the charging process is a flow of electrons from plate 1 to plate 2 as indicated by the arrowed path in Fig. 3. The electrons on plate 2 try to move further on and reach plate 1 but they are impeded by the dielectric which is a non-conductor (insulator). This tendency of the electrons to reach plate 1 from plate 2 across the dielectric exerts a kind of pressure, force or strain on the dielectric. We call this the dielectric strain. When a condenser is charged, an electric field is

set up between the two plates. This electric field is represented in Fig. 4 by a number of hypothetical lines from one plate to the other. These lines are as imaginary and hypothetical as the lines of force representing the magnetic field around a magnet

It is interesting to ask what would happen if the battery were removed from the circuit after the condenser is fully charged. This is shown in Fig. 5. The negative charge on plate 2 can in no way reach plate 1. It is prevented from doing so by the dielectric in one direction and by the fact that the circuit is open (between A and B) in the other. Therefore plate 1 retains its positive charge and plate 2 its negative charge. The resulting accumulated energy from the charging process is stored in the electric field. This potential energy is ready to be released as soon as a conducting path between A and B is provided.

#### The Charging Cycle

Fig. 6 reproduces the charging cycle. Essentially, the circuit is the same as that of Fig. 3. The only additions are a switch and a sufficiently sensitive centre-zero current measuring device. Current flow is here assumed to be identical with flow of electrons. Hence the direction of flow is from the negative to the positive terminal of the battery.

#### A. Capacitor Uncharged

This is the initial stage of the cycle. The switch is open. Thus the battery is not yet connected across the capacitor. The meter cannot indicate any current flow.

#### B. Capacitor charging

The switch is closed with the result that the battery is connected across the capacitor. Current flows until the condenser plates are charged to practically the same potential as the battery. We have discussed the charging process above, and the result is a positive charge on A and a negative charge on B. The centre-zero ammeter shows a flow of current (indicated by arrows). This flow ceases and the pointer returns to the zero position in the centre when the condenser is fully charged. In the present case, the charging (indicated by a sharp to-and-fro kick of the pointer) is instantaneous as, for simplicity's sake, no resistance has been provided for the condenser to charge through.

#### C. Capacitor charged

The switch is opened. The condenser retains its charge (theoretically, at least). Again, the meter cannot indicate any current flow.

#### D. Capacitor discharging

The battery is removed and instead a direct path is provided by a conductor (or a resistance). The switch is closed. The surplus of electrons on plate B rush out to meet the positive charge on plate A until both charges cancel out each other and the condenser is uncharged once again. The ammeter this time deflects to the left thus showing that during discharge the direction of current flow is in the opposite direction to that during the charging of the condenser.

After the condenser is completely discharged, the pointer returns to the zero position; we are back again to where we started (Fig. 6a) and the whole cycle can be repeated over again.

#### A Condenser Blocks D.C. but not A.C.

We have said that a condenser blocks D.C. because of the dielectric which is an insulator. Now keeping this in mind, let us consider Fig. 7. When the switch is thrown to position 1, the lamp lights for a very brief interval and then remains extinguished. This is due to the charging current. The same thing happens again with the switch in position 2. This time it is due to the discharging current. If, however, we could flick the switch from position 1 to position 2 very rapidly, say 50

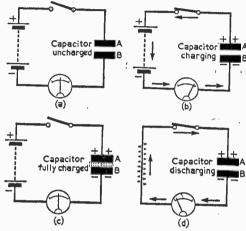


Fig. 6 (a to d)—The condenser charging cycle (see text).

times per second, the lamp would be lit and extinguished at the same frequency; but we would not be able to perceive this and the lamp would appear to be continually lit just as if the condenser were not there at all. Why is this? The reason is that the current is no longer direct but pulsating. Fig. 8a and 8b help us to understand this more

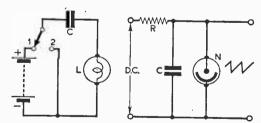


Fig. 7 (left)—A switched circuit which shows the effects of applying A.C. to a condenser.

Fig. 9 (right)—The circuit of a simple neon relaxation oscillator.

easily. In the first case, a 1-pole 4-way rotary switch is provided. The wiper, rotating in a clockwise direction, successively makes contact with the four positions. Notice the crude triangular waveform with a positive peak above and a negative peak below the zero axis.

(Continued on page 949)

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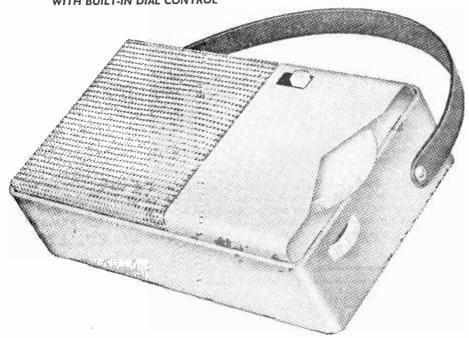


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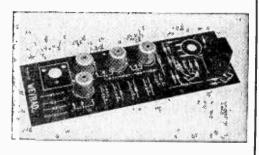
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#### (Continued from page 946)

Fig. 8b provides a smoother rise and fall by the insertion of other batteries supplying intermediate potentials. This waveform is nearer the familiar sine wave. In actual fact, an alternating voltage is produced by a coil rotating in a magnetic field at constant speed, the amount of voltage induced at any instant being proportional to the speed at which the coil cuts the magentic lines of force. One cycle represents one complete revolution. Moreover, the speed of rotation determines the frequency of the alternating voltage.

Another important point with respect to Fig. 8b is that the faster the switch rotates, the brighter the lamp lights; just as if the resistance offered by the condenser is progressively diminished. This brings us to the important

concept of Reactance.

#### Reactance

Although, as explained above, the condenser does not block A.C., it offers a resistance to it, as is shown by the fact that the battery voltage (supplying the lamp) has to be much higher than the actual voltage across the lamp. The reactance of a condenser is the resistance it offers to alternating current at a given frequency. Reactance (XC) is measured in ohms. The formula is:

$$XC = \frac{1}{2\pi fc}$$

Where f=frequency in c/s.
c=capacitance in Farads.
Reactance, therefore, is inversely proportional to the frequency and the capacitance.

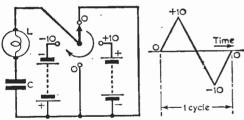


Fig. 8a—Using a rotating switch to give a crude form of A.C.

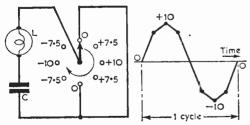


Fig. 8b—If more batteries are added to the circuit of Fig. 8a, a smoother waveform is obtained.

If the capacitance is constant, the higher f is, the lower Xc is. The reactance of a  $2\mu$ F condenser at 50c/s is  $1591\Omega$ . But at 100kc/s, it is  $0.795\Omega$ .

If the frequency is constant, the higher C is, the lower Xc is. The reactance of a  $2\mu$ F condenser at 50c/s is  $1591\Omega$ . But the reactance of a  $10\mu$ F condenser at 50c/s is  $318\Omega$ .

Therefore, reactance is lowered either by increasing the frequency or by increasing the capacitance.

#### The Condenser in Use

The peculiarities of the condenser are put to practical use in all kinds of circuitry, from the simplest crystal set to the most complex of electronic computors. Fig. 9 shows the circuit of a simple relaxation oscillator. The condenser C is charged through R. As soon as the voltage across C is equal to the striking voltage of the neon lamp N, C is discharged through it. The process of charge and discharge is repeated over and over again as long as D.C. continues to be supplied.

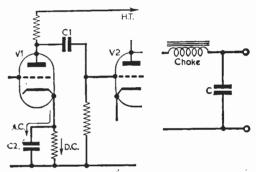


Fig. 10 (left)—Resistance-capacity coupling between valves.

Fig. 11 (right)—An H.T. smoothing circuit.

Two other important and common uses of the condenser are shown in Fig. 10 where we have resistance-capacity coupling between V1 and V2. The coupling condenser C1 prevents the D.C. voltage present at the anode of V1 from reaching the grid of V2 and driving it positive, while at the same time allowing the A.C. signal to reach the grid of V2 for further amplification. The bias condenser C2 bypasses the fluctuating A.C. signal component which prefers to pass through the condenser rather than through the resistance, the capacitance of the former being chosen so that its reactance is much lower than the value of the resistance. The purpose of bypassing the A.C. signal is to maintain a steady D.C. bias voltage at the cathode of the valve.

The condenser C in the choke-input smoothing circuit (Fig. 11) filters out any trace of A.C. ripple which manages to pass through the choke. (The choke offers a high resistance to A.C. while it allows D.C. to pass through it quite easily; its function is opposite that of the condenser).

It has not been possible here to give more than a few basic applications of the condenser in common circuits. The constructor will no doubt be able to find other uses for himself by carefully studying the various circuits which appear in every issue of "Practical Wireless".

# The

# BASS THEORY AND PRACTICAL DESIGN Cabinet B

By J. B. Dance

(Continued from page 850 of the January issue)

AST month, the theoretical aspects of the bass reflex cabinet were given; some details on construction were also given and it was stressed that to achieve good results, care must be taken to ensure that the cabinet is strong and rigid. If the cabinet walls are allowed to flex, then the sound output will be coloured by cabinet resonances.

#### Damping

The cabinet should be at least partially lined with a coating of heavy felt to subdue resonances—about in. in thickness. The felt should not be thick enough, however, to damp sound waves at frequencies below about 200c/s. It is probably wise not to use too much felt at first, as the amount can always be increased later, if desired.

No allowance should be made for the volume of the felt when calculating the cabinet volume. It is the low frequency response which is affected by the cabinet volume and low frequency sound waves

can travel through the felt to the walls.

It is usual to place a piece of expanded aluminium (which is sometimes given a gold coloured finish) over the loudspeaker and vent openings, but care should be taken that this will not produce an irritating rattle when the loudspeaker is producing sound of one particular frequency.

If a piece of cloth is used to cover the grill openings, it is important to use a type of cloth which presents little resistance to the sound waves. Closely interwoven threads should be avoided. Cotton or plastic cloth which is very loosely woven and which has hard threads is ideal.

#### Finish 1"9

It is well worthwhile taking great care over the finish of the cabinet so that one can take a pride in its appearance as well as its acoustical characteristics. A very neat finish can be obtained by staining the wood to the desired colour and then applying a solution of shellac in methylated spirit carefully. The shellac solution should be allowed to dry and several more coats may be applied to give the finished article a high polish.

#### Testing

The ultimate and most important test for any loudspeaker system is undoubtedly that of the human ear and the amount of satisfaction obtained by the owner and his friends. Nevertheless there are some measurements which can be carried out.

It is worthwhile to measure the loudspeaker impedance-frequency characteristic at low frequencies with the unit mounted in its cabinet. The apparatus for measuring this characteristic was given in Fig. 3, last month but an A.C. voltmeter

should be connected across the output terminals of the amplifier. Using low power, values of the voltage and current passing to the loudspeakers at various frequencies between about 25c/s and 200c/s can be found and the impedance at each frequency can be calculated from Ohm's law. The impedance should then be plotted against the frequency as in Fig. 1 (last month).

When the loudspeaker is mounted in a well designed cabinet, the characteristic should no longer look like that of Fig. 1 (last month). The one large peak at the fundamental resonant frequency of the loudspeaker should have completely vanished and two much smaller peaks on either side of the original peak should be found. If the original peak is still present, the cabinet has not been tuned correctly. The characteristic should be replotted with blocks of wood of about 100cu.in. in volume placed inside the cabinet. If it is impossible to remove the peak due to the loudspeaker resonance by raising the frequency in this way, the characteristic should be plotted with the vent reduced in size by a piece of wood. This will lower the frequency at which the cabinet resonates.

If peaks other than the two already mentioned are found in the response curve of frequency between about 80c/s and 150c/s, they are probably caused by standing waves in the loud-speaker cabinet. The area of the walls covered by the damping felt should then be increased until they vanish. It is not possible to remove standing waves completely at very low frequencies, but it is possible to remove them from the loudspeaker

resonance curve.

#### Results

The performance of a correctly designed bass reflex cabinet system at low frequencies is much better than that of the more common and cheaper methods of mounting loudspeakers. Some of the advantages are listed below:—

(1) Improved bass response. The bass range may be improved by several dB over a range of nearly two octaves when compared with the same loudspeaker mounted in a closed cabinet or on a

very large baffle.

(2) The impedance curve will be much flatter and hence the frequency response curve will be much more level in the low frequency region.

(3) The cone will vibrate with a much smaller amplitude when the input is at the resonant frequency of the loudspeaker than it would if the loudspeaker were mounted in an open cabinet. This will result in reduced distortion at the same power output, or alternatively more power will be available for the same degree of distortion.

(Continued on page 961)

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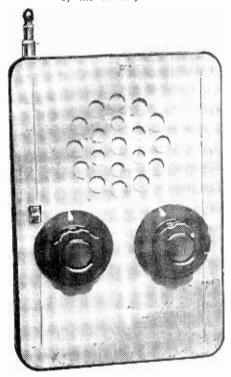
A TRF

POCKET PORTABLE RECEIVER

**WITH** 

FOUR TRANSISTORS

(Continued from page 798 of the January issue)



P W I

AVING carried out the constructional work described last month, the detector stage can then be built up complete, and tested. Counting the tags from the top (in Fig. 4, last month), connections can be checked as follows: 1, Collector. H.F. Choke, lead 5; 2, Base, lead 2; 3 Emitter, 10k (R3), 500pF pre-set condenser (C1), tuning condenser frame and battery positive; 4, H.F. Choke, 5·6k (R1), 0·25µF condenser (C5); 5, 0·1µF condenser (C2), 10k (R3) and 100k (R2) resistors, lead 3 from ferrite slab.

The 500pF pre-set is held in position by soldering one of its tags directly to tag 3. All the transistor leads can be left long, but should be covered with sleeving. The transistor can be added last, the joints being quickly made, and

the iron removed.

Testing

If desired, this part of the receiver can be tested with phones. To do this, connect the phones from the free end of the  $0.25\mu$ F condenser (C5), to the tuning condenser frame, marked M.C. in Fig. 4. Take a lead from the 50k regeneration

control to battery negative.

Smooth regeneration, right up to oscillation point, should be obtained with the 50k control. If oscillation cannot be obtained, screw down the 500pF pre-set slightly. If oscillation is too violent, unscrew this condenser. The correct setting is not very critical, and should allow adequate, yet smooth, regeneration with any battery supply of 4½V to 9V. If a regeneration winding has been added to an existing slab or rod, it might be necessary to adjust the position of this winding, to secure satisfactory results. If no regeneration at all can be obtained, the winding may have been reversed in error.

Reproduction in the phones should be free from distortion, and of reasonable volume. When the receiver is adjusted for maximum sensitivity, tuning is sharp, and both controls should be operated carefully together. The regeneration control should never be merely turned fully clockwise (as if it were a volume control) as this will not give

satisfactory reception.

Audio Amplifler

This is built as a separate unit. A piece of paxolin is shaped as shown in Fig. 4, so as to clear the tuning condenser, regeneration control, and leave space for the battery.

and leave space for the battery.

Small holes are drilled, and the resistors and other parts are placed with their leads through the holes, as shown in Fig. 4. The reverse side

By F. G. Rayer

of the audio panel is shown in Fig. 5.

The colour coding of the driver transformer T1, and output transformer T2 applies to the transformers listed. Other driver and output transformers would be equally satisfactory, and the maker's connecting data should be followed. The leads pass straight down through small holes, and are bent over. A little adhesive under the transformers will hold them to the panel, in conjunction with the leads. Leave the two secondary leads of the output transformer free, for connecting to the speaker.

#### Lead Lengths

All transistor leads can be left quite long, as mentioned, but the soldered joints should still be made quickly. Cover all wires, including the ends of resistors, with sleeving. A few inches of thin flex are used for battery connections, terminating with the appropriate positive and negative clips.

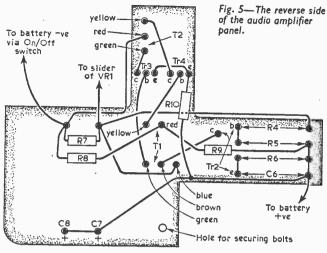
When the audio amplifier panel is finished, it is placed in the position shown in Fig. 4. Two short bolts hold it there, with spare nuts so as to obtain about 4in. space between the audio panel and the

receiver panel.

#### **Connections**

The leads shown in Fig. 5 can then be connected to their correct points: one lead goes to the switch (battery negative); a second lead passes to the 50k regeneration control; transistor Tr2 base, which is joined to the 33k and 10k resistors (R4 and R5), goes to the 0.25µF condenser (C5), and, finally, a lead connects the battery positive side of the circuit to M.C., or the frame of the tuning condenser.

After connecting speaker and battery, the receiver can be tested. Reproduction should be



clear and distinct. No further adjustments should be necessary, if the 500pF pre-set has been adjusted as described. If a meter is included in one battery lead, the resting (quiescent) current (no signal) should be around 5mA. This should rise to about 8mA to 15mA on peaks, with average speech or music, according to volume.

#### Case and Rod

A piece of silk or other thin material about 4in. square is placed over the speaker, and held with adhesive. Fit the threaded bush for the back screw, tightening it securely. The control knobs are removed, together with the nut of the 50k potentiometer, and one screw of the tuning condenser. The receiver is then inserted in the case, and the nut and screw replaced, and tightened. Pointer knobs of reasonable size will be best for tuning.

The aerial rod has a bracket to take two 6B.A. bolts, with 1/2 in. spacers, or spare nuts, between bracket and case, as shown in Fig. 4. A clearance hole is drilled in the case above the top of the rod. An insulated lead passes from the rod to the fixed plates of the tuning condenser. A small terminal on the side of the case would do for an external aerial connection instead.

#### Equivalents

The circuit will work satisfactorily with transistors of similar type, including surplus transistors in proper condition. Tr1 must be an R.F. transistor, or regeneration may not be obtained. Tr2 is an audio amplifier, and other types may need a change in value of R4, R5 or R6. Tr3 and Tr4 are best a matched pair for push-pull output. Some transistors may need

(Continued on page 962)



Rear view of the 'Minuette'.

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# FAULTS IN VHF/F.M. RECEIVERS 4-Transistor Sets

By G. J. King

(Continued from page 826 of the January issue)

EVERAL of the more common faults in the final stages of VHF/F.M. receivers were dealt with last month, but a confusing symptom is the presence of hum and distortion. The treble-diode-triode valve (see Fig. 9, last month) often produces the above symptom, particularly that type of valve which is designed for A.C./D.C. operation, such as the UABC80. One complaint in this respect was that hum and distortion occurred, on F.M. only, a little while after the receiver has been switched on. It was discovered that the fault was fairly consistent and that it could be almost cleared by detuning. Replacing the valve cleared the trouble completely, but a subsequent check on a valve tester failed to reveal the trouble.

This is one of those cases where a faulty valve can only be discovered by substitution. Once the faulty stage has been located, quite a lot of time can often be saved simply by substituting the associated valve before detailed tests are carried

If distortion is present on both A.M. and F.M., attention should be given to the common A.F. stages. A typical cause of such trouble is a leak in the A.F. coupling capacitor (C58 im Fig. 9). This puts a positive voltage on the grid of the output valve and causes it to pass much more anode current than is good for it. The valve thus becomes very hot and the voltage across the cathode bias resistor rises above that given in the service manual.

Similar distortion, particularly at high volume levels, should lead to a check of the A.F. amplifier load resistor, such as R24 in Fig 9. If this goes high in value the distortionless output of the stage is considerably limited.

#### Ralance

Severe distortion on F.M. only, which can be reduced by detuning slightly, is often caused by unbalance in the ratio detector. This may be due to one of the ratio detector diodes going out of balance. Some sets use germanium crystal diodes for the ratio detector instead of the diodes in a multi-electrode valve. These are more prone to unbalance effects; in fact, one of the crystals may go open-circuit completely. This not only causes severe distortion but it also considerably reduces the output on F.M.

The ratio detector can be balanced by applying an amplitude-modulated F.M. I.F. signal (usually at 10.7Mc/s) to the control grid of the last I.F. valve and recording the output either on the speaker or on an output meter connected across

the speaker or across a resistor connected in place of the speaker. The resistor should have a value equal to the impedance of the speaker which it is to replace

to replace.

The signal generator should be accurately adjusted to the F.M. I.F., after which the core in the ratio detector winding of the transformer (e.g., L29 in Fig. 9) should be carefully adjusted for minimum output. The ratio detector is in correct balance when it does not respond to an amplitude-modulated signal. In practice, however, there is usually some residual frequency-modulation of the generator signal so zero output is rarely accomplished.

A series on VHF/F.M. receivers would be incomplete without reference to combined F.M./A.M. models using transistors, and the remainder of this series will be devoted to such sets.

There is no doubt now that transistors are going to take the place of valves in almost all types of electronic equipment of the domestic category. Industry is already using vast quantities in special instruments, control systems, computers and the like, and there has also been an almost complete changeover from valves to transistors in the popular A.M.-only portable sets.

#### Noise and Reliability

The new alloy diffusion technique has made the manufacture of VHF transistors possible. These, which are able to operate up to 200Mc/s, are finding their way into VHF/F.M. receivers and television sets. A fully transistorised television turret is already available.

Apart from the smaller power requirements and resulting improved efficiency, transistors are also proving to be far more reliable than valves. This means that, while, in the past, transistors were employed essentially for miniaturisation, their use in the future will also be for reliability, and for that reason they will be exploited on an increasing scale in equipment which, by reason of its nature, does not particularly require to be made smaller, such as television receivers, radiograms, audio and hi-fi amplifiers, tape recorders and so on.

For the present we will concentrate on the transistorised VHF/F.M. set. In Fig 11 is shown the circuit of the VHF tuner of such a receiver. The two transistors are of the alloy diffused type and the circuit is based on the popular Perdio Portable, Model 95 which uses a total of nine transistors and five crystal diodes and is designed for A.M. and F.M. reception.

#### Common Base Mode

Transistors Tr1 and Tr2 are operated in the common base mode. That is to say the base is earthed to the signal while the input signal is applied to the emitter. The collector is loaded in the usual way with the tuned circuits, across which the output signal is developed.

This arrangement, of course, is analogous to the valve earthed grid circuit, where the grid is earthed so far as the signal is concerned and the input signal is applied to the cathode circuit and the anode loaded with a tuned circuit across which the output signal is developed. For those not fully conversant with transistors, it should be noted that a transistor can be likened to a triode valve in certain respects, with the base being equivalent to the grid, the emitter to the cathode and the collector to the anode.

Transistor Tr1 is the R.F. amplifier for VHF. The aerial signal is coupled through C1 to the wide-band input circuit comprising L1 and C2. The loaded Q of this circuit is quite low, so the circuit responds to the whole of Band II. The base is held at chassis potential (earth) so far as the signal is concerned by C3 (it should be noted that battery negative is, in fact, the chassis or earth line, this being the opposite to the circuitry in most transistor portables).

#### Biasing

The base of Tr1 is biased by the potential divider formed by R1 and R2 across the battery and thermal stability is maintained by the emitter resistor R3. Coil L2, C4 and C5 form the collector tuned load, and the R.F. tuning section of the gang C5 is coupled to the oscillator counterpart in the usual way. The capacitor, C6, connected between the emitter circuit and base provides a degree of feedback.

The amplified signal is fed to the frequency-changer stage, Tr2, through C7. In this particular receiver, it will be seen that the signal can either be applied to a conventional aerial socket from an outside aerial or, in good signal areas, from a simple telescopic rod aerial.

For the sake of completeness and to help newcomers to transistor circuits achieve a better understanding on the basis of comparison, the equivalent valve earthed-grid R.F. amplifier is given in Fig. 12.

#### The Frequency-Changer Stage

Transistor Tr2 performs the dual functions of local oscillator and mixer, and for this reason the stage is often called a "self-oscillating mixer". Again, the input signal is applied to the emitter, but this time across L3. The base is connected to chassis through C8 and is biased by the potential divider R4 and R5. The emitter resistor, R6, provides thermal stability (to prevent thermal runaway) and C9 gives a little feedback. Further feedback is provided by C10.

The oscillator tuned circuit comprises L4, C12 and C13, and is coupled to the collector through C11. C12 is the oscillator section of the tuning gang which is ganged with the R.F. section. Capacitors C4 and C13 respectively are R.F. and oscillator trimmers.

#### 10.7Mc/s Intermediate Frequency

The stage is caused to oscillate at the frequency governed by the tuned load described above by regenerative feedback provided by C14, between emitter and collector.

The collector is also loaded by the tuned circuit L5, which forms the primary of the I.F. output transformer, L6 being the secondary across which the coupled I.F. signal is developed for feeding to the I.F. stages of the receiver. In common with most F.M. receivers, the intermediate-frequency is 10-7Mc/s which, of course, is obtained by the VHF signal heterodyning with the oscillator signal in Tr2.

When the receiver is switched to "F.M.", switch S1 is closed, so that the VHF tuner section is working normally, but when the set is switched to "A.M." S1 is open. This, of course, cuts off col-

(Continued on page 961)

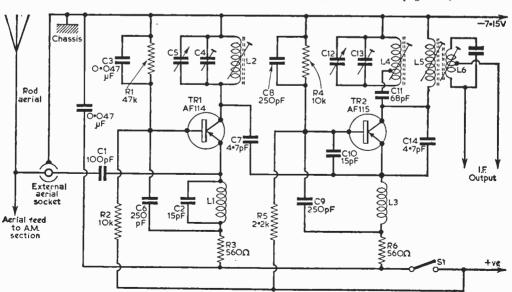


Fig. 11—The VHF section of a combined F.M./A.M. transistorised portable set.

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	Cabinet for above including 9 x 5in. speaker	\$5.5.0 \$29.0.0
l	Hire purchase deposit £6.0.0 and 12 monthly	\$2.2.2
	We can supply the above recorder, complete with tape and Mic.,	
	in a DE LUXE cabinet, assembled for	\$35.0.0
	THIS MACHINE IS LISTED 241.0.0 BY MAKERS AND IS A	VERY
	GOOD BUY.	
	Hire purchase deposit £7.0.0 and 12 monthly	\$2.11.4
ŀ	Tape Pre-amplifier, for recording and playback, as above less	

output stage, with power supplies
Hire purchase deposit £1.14.0 and 6 monthly..... 81 5 9 ### Hire purchase deposit \$1.14.0 and 6 monthly ... \$1.5.8 Microphone for the above recorders, Acos MIC 04, 25/-, 8/C plug 4/8. Synchrotape 5in. \$60tt. 19/6 5in. \$900tt. 19/8 Finest 5jin. \$50tt. 19/6 5in. 1.200tt. 22/8 Hoxed 7in. 1200tt. 22/8 7in. 1800tt. 32/8 Tape Recorder Speaker Cabinet. corner, 20 x 10in. High class finish in two-bone Grev "Vymair" ... \$2.15.0 With 9 x 5in. high flux speaker ... ... 24.0.0 Marriott Tape Heads. I track K/PB & Erase with mounting plate for Collato deck. ... \$4.0 pair

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B.S.R. UA14 TC8/H cartridge	 £7.15.0
Hire purchase deposit £1.11.0 and 6 monthly	 £1.4.0
Collaro C60 Autochanger "O" cartridge	 £8.15.0
Hire purchase deposit \$1.15.0 and 6 monthly	 £1.6.8
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Hire purchase deposit \$1.17.4 and 6 monthly	 £1.7.8
Philips AG1016 New semi-auto piayer	 £14.3.6
Hire purchase deposit \$3,3.6 and 12 monthly	 £1.0.2
MINI AMD	

MINI AMP P/W November issue, Resistors 6/-, V/C 6/-, Condensers 9/-, Transistors V6/R2 9/-, CC1 6/6, CC72 pr. 16/-, T/T3 13/-, T/T2 9/8. PPB 3/6, Tress studs 1/-, Speaker 7 x 4in. 17/6, Group/b 2/9, All the above, if ordered at one time, \$4.15.0. Diagram may be obtained from "Fractical Wireless". 5/-.

CITIZEN P.W. Transistor tuner, December issue, Resistors 5/-, Condensers 11/-, W/C 3/6, OA70 3/-, Group boards 2/9 ea., Transistors 31/-, set, Coll set 22/6, RA2W 12/6, J.B. 12/6 with trimmers.

#### **TRANSISTORS**

MULLARD HAVE REDUCED THE PRICE OF MANY TYPES TO CC44 11/-, OC45 10/-, OC70 6/6, OC71 6/6, OC72 8/-, OC75 8/-, OC76 8/-, OC78 8/-, OC81 8/- ABOVE ARE THEIR NEW LIST PRICES. WHY BUYSURFLUS? MATCHED PAIRS ONLY. Mullard OC72 at 16/- pair.

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OSMOR printed circuit version. Osmor Rod aerial 10/-. I.F.T.s and Osc. Colls, 22/6. Osmor Driver, 11/6. Osmor Output, 10/6. Bet MULLARD transistors, 53/6. OASI Diode. 3/-. J.B. Gang, 11/-. Trimmers, 2/8 pr. Bet Condensers, 15/-. Set Resistors, 6/6. Ardente Vol. Control, 8/-. Ardente W/C, 3/6. Speaker, 19/10. Hardware, 4/8. Printed Circuit, 9/-. Case and Knolt, 7/6. Dial, 6d. Battery Pf4, 2/-. Leaftet giving full illustrated details, 1/9. All the above components if purchased at one time £9.9.0. OSMOR undertake to align this receiver for a charge of 10/-. Modification Kit, 10/-. New contemporary case, 12/6.

#### "WEYRAD"

WEYMOUTH RADIO 6 Transistor Superbet using the P50 coits, as they advertise in this journal. P50/LAC Osc. Coit, 5/4. P50/2CC 1st and 2ad L.F.T.s, 5/7 ea. P50/3CC 3rd 1.F.T., 5/4-, RAZW Rod Aerial, 12/6. LEDTA Driver, 8/6. PCA1 Printed Circuit, 9/b. fustruction Boos, 2/-, Set Resistors, 7/8, Vol. Control D.P., 5/6. Set Condensers, 20/-, J.B. Gang, 11/-, Bechive Trimmers, 1/3 ea. W/C, 3/6. Dial and Kinch, 3/6. Battery PP11, 5/6. OA81, 3/-, Set MULLARD transistors, 53/6. 35 ohm 5in round L/8, 15/-, Car Aerial Coupling Coil, 1/-,

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THE REGISTERED TRADE MARK

OF DENCO (CLACTON) LIMITED IT IS ALSO A GUARANTEE OF WORKMANSHIP TECHNICAL PERFORMANCE

OUR RANGE OF PRO-DUCTS IS SO GREAT THAT WE NOW HAVE TO REQUEST THE AMOUNT OF 1/6 FOR OUR GENERAL CATALOGUE AND TO SAVE YOU POSTAL ORDER POUNDAGE CHARGE WE REQUEST SEND 1/6 IN

COMPONENTS FOR USE WITH THE "PRACTICAL WIRELESS"

#### AMATEUR

PUBL SHED JULY/AUGUST 1961)

COIL TURRET—CT7/B
This turret is the basic portion of the CT7. It comprises cadmium plated steel frame (size 5½" deep x 4½" high x 3½" wide), silver plated contacts, poly-styrene insulation and a rotary turret movement incorporating Aerial, Mixer and Oscillator coils for the three bands 1.5-4 Mc/s, 4-12 Mc/s and 10-30

Coil strips for the long and medium wavebands may be purchased separately for incorporation in PRICE 10/6 each

The turret requires a 315pF tuning capacitor. A suitable 3-gang component with ceramic insulation PRICE 19/-

Air spaced concentric trimmers, 3/30pF.

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SCALE ASSEMBLY—S1

Comprising basic 5 waveband glass scale for use with 315pF tuning condenser, back plate, pulleys, rubber scale mounts, pointer, cord, drum, spring, drive spindle, screws, nuts and spacers.

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BEAT FREQUENCY OSCILLATOR COIL— BFO.2/465/kcs.

A compact coil wound on a bakelite former and enclosed in an aluminium screened can. PRICE 5/-

I.F. TRANSFORMER-IFT.11/465 kc/s (Four required)

A miniature I.F. Transformer for 465 kc/s. Permeability tuned, litz wound coils, enclosed in an aluminium screening can 13" high x 18" square.

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# KITS THAT 'BUILD THEMSELVES



- quality printed-circuit amplifiers, supplied checked and assembled
- Complete with valves, transformers and everything down to wire cut to length.

Produced by the makers of amplifiers for some of today's best known recorders and backed by years of experience in audio design. The specially designed kits offered here set entirely new standards of performance and finish for the home constructor. Amplifier available separately or with case and speaker and deck. EASY TO FOLLOW INSTRUCTIONS. All equipment complete and guaranteed.

From radio dealers, or in cases of difficulty please write direct

FOR HIGH OUALITY TWO & FOUR TRACK TAPE RECORDERS

AMPLIFIER 'C' for Collaro Studio Deck (illustrated above), II gns. Case and Speaker for above. 5 gns. AMPLIFIER 'A' (4-TRACK) for BSR Monardeck. 9 gns. AMPLIFIER 'B' (TWO TRACK) for BSR Monardeck. 8 gns. Two-tone covered wooden case with speaker for above. 4 gns. KIT 'A' with Deck, Case and Speaker. 24 gns. KIT 'B' with Deck, Case and Speaker. 21 gns. KIT 'C' with Case, Speaker and Deck (as illustrated). 284 gns. All amplifiers supplied assembled on printed circuit boards with valves.

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Leaflet free on request. Set of full instructions for any one model 2/6d, post free. (Allowable on purchasing kit).

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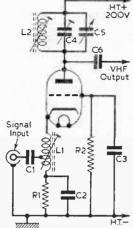


MARTIN ELECTRONICS LIMITED, 155 HIGH ST., BRENTFORD, MIDDX. Leaflet on Martin Recordakits please NAME. # ADDRESS (in Block Letters.)

(Continued from page 958)

Fig. 12—The valve equiva-lent of the R.F. stage in Fig. 11. Here, RI is for bias and R2 is the grid return resistor.

lector current on Tr1 and Tr2, but it will be noted that the bases remain biased since the bottom ends of the potential dividers, R2 and R5, are connected to the battery side of S1. This is done to prevent damage to the transistors, which might otherwise occur owing to a rise in base voltage.



#### Tracing Faults in the VHF Section

The VHF section is often built into a selfcontained screened box, and intermittent troubles on VHF/F.M. due to poor connections, dry joints and so on occur equally in transistor units as they do in valve units. However, owing to the cool operation of transistors, frequency drift is not so troublesome as it is with valve circuits, but printed circuits and inter-connections still give trouble, and should be investigated as described in previous articles should intermittent symptoms on VHF/F.M.

The alignment of a transistorised VHF tuner is sometimes more important than in valve units, for if the 1.F. or oscillator alignment is misplaced by a small amount, the local oscillator may

fail over a section of the tuning range.

Excessive "noise" on F.M. when a station is tuned in should lead to a check of the aerial system for, although the new VHF transistors are endowed with remarkably good noise figures, one is often tempted with a portable to use the smallest aerial possible, and while this is perfectly in order in areas of reasonably high signal where there is little I cal shielding, something better is required in shielded locations.

If the VHF section fails completely, and the set operates normally on A.M., there is every possibility that the VHF tuner is faulty. This can be proved speedily by switching the set to "F.M." and injecting the F.M. I.F. from a signal generator across L6, for example. If the output from the speaker is loud and clear, then the tuner is definitely faulty. If there is no output, attention should be directed to the F.M./A.M. changeover switching.

In most cases of VHF unit failure, apart from dry joints and poor connections, the local oscillator section is to blame. This invariably gives rise to a "hiss" when the set is switched to "F.M." and the volume control turned up full and, in some cases, there may be a sudden restoration of signals

at certain settings of the tuning gang.

#### Readings

Much information on the operation of the transistors can be obtained by measuring the voltage across the emitter resistors (R3 and R6 in Fig. 1). The voltages will be low normally, not much more than one volt, so a low reading voltmeter is essential, and to avoid loading the circuits unduly the voltmeter should also have a fairly high resistance or sensitivity. A  $20,000\Omega/V$  meter with a full-scale deflection on the "low volts" range of 2.5V to 5V is ideal.

Tests are best made with meter positive connected to battery positive. With the negative lead connected to Tr1 emitter a reading of around 0.85V would indicate that the transistor is passing collector current. On the same electrode of Tr2, the reading should be about 1.1V. Zero voltage would indicate either that the transistor is open-circuit or that the negative supply to the collector is missing. This supply should next be checked, if necessary, by connecting the negative of the meter to the collector. The voltage here should be almost equal to the negative line voltage, since the collector loads are of low resistance, though it may not be equal to the battery voltage owing to the voltage dropped across decoupling and filter resistors in the negative circuit from the battery to the VHF tuner. A value of about 7V is typical for VHF collectors.

The base voltage can also be checked by connecting the meter negative to base (positive still connected to battery positive). Base bias for VHF transistors is around 1V though it may be slightly higher on the frequency changer when oscillating

properly. If the voltages deviate substantially from the above examples, the feed components should first be checked for continuity and value, and if normal, the associated transistor will, in most cases, be found responsible.

#### The BASS Reflex Cabinet

(Continued from page 950)

(4) The radiation resistance will be greater at low frequencies, and therefore the power will be more efficiently transferred to the surrounding air. When compared with a similar loudspeaker mounted in a closed cabinet, a power gain of about 3dB might be expected, as half of the power from a loudspeaker in a closed cabinet is wasted by being trapped in the cabinet. In actual practice the gain may be greater than 3dB when a bass reflex cabinet is used owing to the more efficient transfer of energy to the air.

The only possible disadvantage of the use of a bass reflex cabinet is that if the amplifier feeding the loudspeaker contains any hum, this will sound much more prominent than before, but the remedy for this is obvious.

Care should be taken not to obstruct the vent or the front of the loudspeaker; at the loudspeaker resonant frequency the sound is radiated almost entirely from the vent.

The frequency response should extend down to half the loudspeaker resonant frequency or-less; with conventional mounting, the bass output from a loudspeaker is almost negligible below its resonant frequency.

# Club News

AMATEUR RADIO MOBILE SOCIETY Hon. Sec.: G3FPK, 79 Murchison Road, London, E.10.

At this year's Radio Hobbies Exhibition in London, the society had their own stand, manned entirely by A.R.M.S. members. **BRADFORD RADIO SOCIETY** 

Hon. Sec.; M. T. G. Powell, G3NNO, 28 Gledhow Avenue,

Roundhay, Leeds 8.

The society's last spares sale in 1961 was held on November 28th. On December 12th, the development of time measurement was discussed by W. Barton, and amateur receiver construction was the subject of the lecture given by D. M. Pratt at the meeting on January 2nd.

**Future Events:** 

January 30th—Use of simple test gear, by D. G. Enoch.

February 13th-Field-day discussion and informal meeting. DERBY AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: F. C. Ward, G2CVV, 5 Uplands Avenue, Little-

over, Derby.

The society's Open Night on December 13th was also appointed as the management committee meeting. On December 20th, members enjoyed the Annual Christmas Party. As there was no meeting on 27th December, those members who wanted to joined in a 160 metre net instead. Yet another surplus sale was held at the first meeting of the new year, on January 3rd.

Future Events:

January 10th—The year in retrospect—an opportunity for members to see some of the activities of 1961 in photograph form. January 17th—A selection of communication receivers will be shown for members to compare.

GUILDFORD AND DISTRICT RADIO SOCIETY Hon. Sec.: J. R. Barker, G3PDX, 35 Banders Rise, Merrow,

Guildford.

All the entrants for the car treasure hunt, held on October 1st, managed to complete the course. The proposed 2-metre equip-ment for the club net, was the subject of a talk given by Harry Mead at the meeting on October 12th. It was at this meeting that the society decided to enter the MCC top band contest, and so on November 11th, 12th, 18th and 19th, the club took an active part in the contest, using the call sign G3FZC. On October 24th the club visited the Dorking group for a ragchew and films.

Four club members took part in the RSGB top band contest which was held on November 11th and 12th.

DUDLEY AMATEUR RADIO CLUB
Hon. Sec.: S. E. Plumtree, G3OSP, II Wallows Wood, The
Straits, Lower Gornal, Dudley, Worcestershire.
On October 13th, members payed an outside visit to attend a

demonstration of closed circuit television, hi-fi, tape recorders and

audio equipment, and to see a film show.

A committee meeting was held on 20th October and another was held on 3rd November. On November 10th, members enjoyed a film show and on December 8th the Christmas dinner was held.

#### REPORTS OF CURRENT ACTIVITIES

NORTHERN HEIGHTS AMATEUR RADIO SOCIETY Hon. Sec.: A. Roninson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.

Recent activities have included a talk on 2 metres by G8CB and a demonstration of hi-fi and stereo. On December 13th members took part in a ragchew.

Future Events:

January 10th—Informal meeting. January 24th—Tape recorders.

PETERBOROUGH AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: D. Byrne, G3KPO, Jersey House, Eye, Peter-

At the annual general meeting of the society, on the 3rd November, S. Hunting was elected president, C. J. Guscott was elected chairman, and D. Byrne was elected secretary and treasurer.

ROTHERHAM RADIO CLUB

Hon, Sec.: S. J. Scarbrough, 25 Crawshaw Avenue, Sheffield 8.

During November members took part in the MCC top band contest. In December the club's own Annual Competition for contest. the G3KUH shield was held.

The annual general meeting was held on January 3rd.

SALISBURY AND DISTRICT SHORT WAVE CLUB Hon. Sec.: E. J. Spicer, 43 Vale View Road, South Newton, Salisbury, Wiltshire.

Arrangements have been made for the club to show a series of films, fortnightly to members, and the first of these were shown on November 21st. Taped lectures are also a fortnightly attraction. and morse classes are given most weeks.

SILVERTHORN RADIO CLUB

Hon. Sec.: K. Marley, G3EIO, I7 Luctons Avenue, Buckhurst Hill, Essex.

Meetings are held every Friday at 8 p.m. at the South Chingford Community Centre. A club station is operated at constructional meetings on alternate Fridays.

SPEN VALLEY AMATEUR RADIO SOCIETY
Hon. Sec.: N. Pride, 100 Raikes Lane, Birstall, Nr. Leeds.
The society's Brains Trust was held on December 20th and the meeting on January 3rd was taken up by a ragchew.

Future Events:

January 17th—Electronic timing devices, by S. Marsden. January 31st—Safety in the shack.

WANSTEAD AND WOODFORD RADIO SOCIETY
Hon. Sec.: K. Smith, G3JIX, 82 Granville Road, Waltham-

stow, London, E.17.

At every Tuesday evening meeting, G3JIX gives a lecture on the requirements of the G.P.O. Radio Amateur's Examination.

The "constructional project" at the moment is a C-R bridge, and

each member is constructing one from the same basic design.

#### ... P.W. MINUETTE

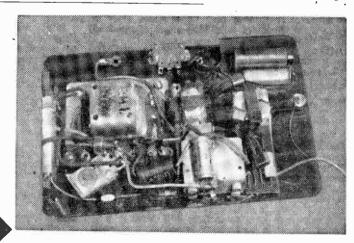
(Continued from page 954)

values other than  $220\Omega$  for R9 and  $5\Omega$  for R10, to obtain full gain and distortion-free reproduction.

#### Miniature H.F. Choke

A miniature H.F. choke can be made by taking a ferrite slug and winding several hundred turns of fine gauge wire upon it. For good results, there is little latitude in values, but condenser values are less important. Typical possible values, with marked values in brackets, are:  $0.1\mu\text{F}$  to  $0.5\mu\text{F}$ (0.1 $\mu\text{F}$ );  $0.25\mu\text{F}$  to  $6\mu\text{F}$  (0.25 $\mu\text{F}$ );  $1\mu F$  to  $6\mu F$  ( $2\mu F$ );  $6\mu F$  to  $50\mu F$  $(30\mu F)$ .

Another view of the set.



#### SPECIAL BARGAIN OFFER! RECORD PLAYER KITS

A UTO CHANGER KII—Comprising three Units, Contemporary styled Cabinet—2 valve, 2 watt amp. and 7 x 4in. quality speaker. Variable tone and Volume Controls with leedback circuit and B.S.R. 4-speed 10 Record Mixer, Auto Changer Unit.

BARGAIN PRICE. £12.10s. only.

Cabinet Size: 17 x 144 x 84 ins. Carr. 7/6.

SINGLE PLAYER KIT—Similar spec. to Autochanger Kit except Player is 4-speed B.S.R. TU.9. Single Record Player Unit. Attractive Contemporary Styled Cabinet. Size: 131 x 13 x 6 ins. with splendid volume and reproduction.

BARGAIN PRICE £8.19.6 only

Carr. 5/-LE UNITS READY WIRED, SIMPLE SCREWDRIVER ASSEMBLY ONLY FULL SATISFACTION—REFUND GUARANTEE
Send for leaflet. Full details—3d. stamp.

ENAMELLED COPPER WIRE—ilb. reels. 14g-20g, 2/6: 22g-28g. 3/-: 30g-40g, 3/9. Other gauges quoted for.

-10 colours (for chassis wiring, etc.)—Single or stranded conductor, per yd., 2d.

METAL RECTIFIERS, STC Types-RM1, 4/9; FM2, 5/6; RM3, 7/6; RM4, 16/-; EM5, 21/-; RM4B, 17/6. SIEMENS TYPES - Contact Cooled; 250V. 50mA, 7/6; 250V. 85mA, 10/-; 250V. 125mA, 15/-; 250V. 300mA, 26/6. CONNECTING WIRE

RECORDING TAPE-SPECIAL BARGAIN OFFER Famous American Columbia (CBS) Premier Quality Tape at NEW REDUCED PRICES. A genuine recommended Quality Tape—TRY IT! Brand new, boxed and fully guaranterd. Fitted with leader and stop folis.

Standard 600ft. 15/-900ft. 17/6 1,200ft. 21/-Long Play 900ft. 18/6 1,200ft. 22/6 1,800ft. 32/8 Double Play 1,200ft. 31/6 1,800ft. 39/6 2,400ft. 47/6 5fin. 7in.

Post and Packing, per reel. 1/-, plus 6d. each for additional reels. SPECIAL OFFER—3in. mfrs. surplus tape, 225ft. 5/6. P. & P. per reel. 6d. Plastic Tape Reels. 3in. 2/6, 5in. 3/-; 5iin. 3/3, 7in. 3/6.

Volume Controls—5K-2 Meg-ohms. 3in. Spindles Morgan-ite Midget Type. 1lin. diam. Guar. 1 year. LOG or LiN ratios less Sw. 3/-. DP. Sw. 4/6. Twin Stereo less Sw. 6/6. DP Sw. 8/-.

COAX 80 OHM CABLE High grade low loss Cellular air spaced Polythene—iin. diameter. Stranded cond. Famous mirs. Now only 6d. per yard. Bargain Prices— Special Lengths— 20 yds. 9/-. P. & P. 1/6. 40 yds. 17/6. P. & P. 2/-. 60 yds. 25/-. P. & P. 3/-. Coax Plugs 1/-. Sockets 1/-. Couplers 1/3. Outlet Boxes 4/6



TAPE RECORDER KIT Special Offer. Latest 5 valve circuit based on Mullard's design Marchael Control of the Contr

Condensers—Silver Mica, All values, 2pF to 1,000pF, 6d. each. Ditto, Ceramics 9d. Tub. 450V T.C.C., etc., (001 md., 0.01 and 0.1/350V, Pd. 0.92-01/500V 1/- 0.25 Elunts 1/6, 0.5 T.C.C. 1/9, etc., etc., Close Tol., S/Micas—10%, 5pF-50ppF 8d. 600-5,000pF 1/- 1%, 2pF-100pF 9d. 100pF-50pF 1/16, The 1% 570pF 5,000pF 1/6, Resistors—Pull Range 10 ohns-10 meg-ohms 20% i and iw 3d., iw 3d. (Midget type modern rading) 1W 6d., 2W 9d. Hs-Stab 10% iw 5d., iw 9d. 1%, iw 1/6 5%, iw 1/

JASON FM TUNER UNITS Designer-approved kits of

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FMTI, 5 gns. 4 valves. 20/-.
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32/6.
NEW JASON FM HANDHOOK, 2/6. 48 hr. Alignment
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Speakers P.M.—3 ohms 2½in. Elac. 17/6. 3½in. Goodmans 18/6. 5in. Roia 17/6. 6in. Elac 18/6. 7 x 4in. Goodmans 18/6. 8in. Roia 20/-. 10in. R. x A. 25/-10 x 6in. Goodmans 25/-. E.M.I. Tweeter 29/6.



#### 7 VALVE AM/FM RADIOGRAM CHASSIS

ECC85 ECH81 EF89 LABC80 Line-up: EL84 EMSI EZ80.

Three Wayechard and Switched Gram position, Med 200-500 m., Long 1,00e-2,000 m., VHF/FM 85-95 Mc/s. Phinps Continental Tusing, insert with permeauility tuning on FM and combined AMFM IF transformers, 460 Kc/s and 10.7 Mc/s. Dust core tuning all colls. Latest circuitry including AVC and Neg. Feedback. Three wat output. Sensitivity and reproduction are of a very high standard. Chassis size 13½ x 5½in. Height 7½in. Edge Illuminated glass dial 11½ x 3½in. Vertical pointer. Horizontal station names. Gold on brown background. A.C. 200/250 v. overstion.



Aligned and tested ready for use £13.10.0 Carr. & ins., 5/-.

Complete with 4 Knobs—walnut or lyory to choice, Indoor FM Aeria), 2/6 satra.
Three ohm P.M. speaker only required. Recommended quality speakers.
Sin. Rola for Else (heavy duty). 30°.

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#### 4-SPEED PLAYER UNITS BARGAINS

Single Players Carr. 3/6 Garrard 4 S.P. 26.19.6 Garrard TA Mk.2 27.19.6 Collaro "Junior" 75/-B.S.R. (TU9) 79/6 E.M.I. Junior 89/6 Carr. 5/-£10.10.0 £7.15.0 £7.15.0 Auto-Changers Control of Garrard RC210 for Collaro "C 60" B.S.R. (UA14) Latest Model Garrard "Auto-glim" €8.12.6 Auto-slim

KNOBS—Modern Continental types: Brown or Ivory with Gold Ring, Inn. dia., 9d. each; 18im. 1/2 each; 18im. 1/3 each; 18im. 1/3 each. LARGE SELECTION available. TYGAN FRET (contemp. pat.) 12 x 12im. 2/4. 12 x 12im. 2/4. 12 x 24im. 4/-, 18 x 24im. 6/- etc.

New VALVES All

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1T4	6/-1	ECC83	8/-	PCC84	9/6
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DAF96	9/-	EL84	8/6	PL82	9/6
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DL96	9/-	EZ81	7/6	PY81	9/6
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#### TRANSISTOR COMPONENTS

GOMPONENTS

Midget 1.F.'s-465 Ko/s,
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Osc. Coil-M/W, 9/16in, dia. 5/3
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Osc. Coil-M/W, 9/16in, dia. 5/3
Osc. Coil-M/W, 9/16in, dia. 5/3
Osc. Coil-M/W, 9/16in, dia. 5/3
Osc. Coil-M/W, 9/16in, dia. 5/3
Osc. Coil-M/W, silver, coil-M/W, older Trans. 3.5:1 6/9
Midget Drive Trans. 3.5:1 6/9
Midget Olyut Trans. P.P. to 3
Osc. Osc. Olyut Trans. P.P. to 3
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Oomid, 2/; 67/12V wkg.
Condensers—0.0mid. ea. 1/9.
Oomid, 1/6.
Oomid, 1/

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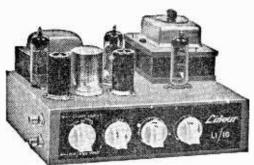
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# Letters to the Editor

The Editor does not necessarily agree with the opinions expressed by his correspondents

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELE-PHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page ii of cover. page iii of cover.

#### CORRESPONDENTS WANTED

SIR,-I am a regular reader of PRACTICAL Wireless. I am very much interested in the radio technology and have started my own shop of radio repairs. I would like to correspond with any radio technician from anywhere. I will answer all the letters received promptly.—B. S. GULSHAN, Falcon Radios, Kota JN, India.

#### **VALVE-TRANSISTOR SHORT-WAVER**

SIR,-I have been gratified that so many people have enquired about the above receiver described in the July issue of PRACTICAL WIRELESS. A large proportion of these are concerned with the winding of the coils. These few notes should remove any difficulties.

L3 consists of 10 spaced turns over 2in., tapped at 5 turns and  $7\frac{1}{2}$  turns. The latter figure unfortunately appeared in the issue as  $2\frac{1}{2}$  turns.

Extensions to any of the coils to cover different wavebands is possible, only at the expense of losing other sections of the frequency spectrum. No experiments have been carried out which concern the fixing of a fourth coil.

The actual positions of the coils on the baseboard or chassis are not important as the three coils each carry their own reaction winding and aerial section.—P. K. CRIPPS (Liverpool).

#### RECORD 'WOW'

SIR,—With reference to the article by L. E. Higgs in the September issue on record player faults. may I suggest that the fault of wow and slurring owing to records being warped can very simply be cured. The seven-inch records seem to be the chief offenders. If eight strips of Sellotape, about ½in. x ¼in. wide, are placed at 45° intervals across the driving serrations, making certain they are clear of the run-off grooves, it will be found that even a badly warped record does not skid. I do this to every record regardless of its condition and have consequently had no trouble.—W. D. HESELTINE (Wallsend-on-Tyne).

#### VINTAGE MODELS

SIR,-I was very interested in the letter in the December issue, by Mr. Mansell, as I too think that some of the old radios in true reproduction were very good indeed. I am sure anyone who has not heard one, tuned in to a good concert, would be very much surprised by the good quality obtained.

I have a very old tuned R.F. set which first had come from Chicago, U.S.A., 1931 to 1932, and was called the Zenith Autovox. This set had five tuned stages of H.F. and double push-pull output stages. These, working into a 15in. energian energy of the set of the se gised loudspeaker, resulted in a very powerful output and the quality of reproduction was amazing.

I have recently had to rebuild the set as the old valves gave out and could not be replaced. The set is still working well and it will pull in any station on a short piece of wire as the aerial, and the tuning is very selective. - D. J. FORWARCH (Watford).

#### L.F. INSTABILITY

SIR,-I should like to report an interesting case of L.F. instability and its cure, in the hope that it may be of interest to others who may come

across a similar unexplained fault.

The circuit was a simple mains amplifier, with a push-pull output stage fed from two audio stages (EF86's; one strapped as a triode and acting as phase splitter for the push-pull output stage). When switched on a very loud hum was experienced and the usual cursory tests failed to disclose the cause. Eventually the two EF86's were removed but the hum still persisted. The phase splitter had just a single resistor to the H.T. line and there was adequate smoothing (60µF). It was eventually found that a large electrolytic from the anode of the phase splitter to earth stopped the hum and finally the cure was a simple resistor (10k) between the anode resistor and the H.T. line, with a  $32\mu F$  condenser to earth. — F. G. Roberts (Torquay).

#### **SOLDERING TRANSISTORS**

SIR,-I should like to pass on a small hint which others may not have seen and which I feel is very important for those who are building the latest types of miniature transistor sets. As most readers now know these components are easily damaged, or even completely ruined, in the act of soldering them into a set. Fitting a heat sink is one very good idea, but I have met cases where the compactness of the set is such that there was no room to fit the shunt unless the leads were left extremely long. In addition whilst the heat shunt may protect the actual component being soldered there is also the risk that nearby parts may be damaged by the radiated heat from a soldering iron. Therefore, when constructing this small type of receiver I have found it a good idea to wind a length of ordinary copper wire, not heavier than 24s.w.g. round the bit and to draw off the remaining two inches, this giving in effect a two inch projection to the bit of thin copper and I find that it carries just sufficient heat to melt the very fine printed circuit solder without risk of damage. I even dispense with heat sinks when using this iron. -F. WALTERS (Hampstead).

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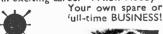
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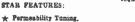
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The Index letters which precede the Blueprint Number indicate the periodical in which the description appeared. Thus PW refers to PRACTICAL WIRELESS; AW to Amateur Wireless and WM to Wireless Magazine.

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TELEVISION

The PT Band III converter

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#### SPECIAL NOTE

THE following blueprints include some pre-war designs and are kept in circulation for those constructors who wish to make use of old components which they may have in their spares box. The majority of the components for these receivers are no longer stocked by retailers.

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PRACTICAL WIRELESS, FEBRUARY, 1962

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