february 1962

Practical 2: WIMPMESS

## ELEHTRONIO DIGITAL GOUNTER with Geiger-head

## ELECTRONIC DIGITAI

 COUN16 m TO 175 m TRANSISTOR S.W.TVNER

## BRAND NEW AM/FM (V.H.F.) RADIOGRAM CHASSIS AT $£ 14$ (Carriage Paid) <br> A.C. ONLY. Chassis size 15 x 6 x x 5 in. high. New manulacture. Dial

 14d $x$ in. in black and goldPick-up. Ext. Speaker. Ae., E., and Dipole Sockets Five purn buttons-OFF L.W. M.W. F.M and Gram. Aligned and tested O.P. 'iranstormer. Tone Control. $1.000-1.900 \mathrm{M}$. $2200-500 \mathrm{M}$. $88-98 \mathrm{Mc} / \mathrm{s}$. Valves E 280 rect., ECH81. EF89. EABC80, EL8: ECC85. Speaker and Cabinet to tit chassis (table model). $47 / 6$ (post 2/6) NEIt us:-(Chassis) 25 down and 5 Monthly Cabinet and speaker $£ 5.10 .0$ down and 6 Monthly Payments of $£ 2$. Cheap Room Dipole $10 \%$ Feeder 6il. yard.
the "cantata" 6-TRANSISTOR AND
dIODE PORTABLE
COMIPLETE KIT FOR ONLY

## Ł7.19.6

(post 3/6)


* 500 mW push-pull output. * Ferrite rod aerial.
* Car aerial socket and coll. * M.W. and L.W. lull coverage.
$\star$ Operates on two 4.5 vells. t Printed circuit board $8 \leqslant \mathrm{x}$ 2 in. * All holes drilled and component positions marked on reverse * Sicle of board
* Borklet of lull instructions 2/6 for 16 p. (refunded on purchase * ofkit).

Size $4 \times 3$. X 7in. $\star 8 \times 2$ in. P.M. highquality speaker.
Two batteries $5 / 6$ covered cabinet. two tone.
High Sensitivits the pair.
Muland transistors * Good selectivity
Top grade Werstors (3cst. $2 \lambda$ OC45. OC81D. and $2 \times 0 C 81$
Alignment service if required $1 \sim 16$ and transionmers.
Wirite ior list of pidees.
All parts suppli prices.
Note the totalied separately

* Note the total cost-no extras at all
* Built in two hours.

13ATIERY IELIMINATOH, For 4 Low Consumption Valves ( 96 Jange). $90 \vee .15 \mathrm{~mA}$. and 1.4 v .125 mA , $42 / 6$ ( $2 / 6 \mathrm{post}$ ). $200-250 \mathrm{v}$. A.C. size $5 i \mathrm{x} 3 \mathrm{x} 2 \mathrm{in}$. Also for 250 mA .1 .4 v . and 90 v .15 mA at
same price.
_ _ -
AUTOMATIC I\&FCOIB CHINGERS. ALI, 4-SPEED WITH UARN-OVER CRYSTAL CARTRIDGE (carr. 5/- extra). Latest ${ }_{7-12 i n}$ on. 10.0 Collaro $C .60$ Studio model, plays any records. (post 1/6). Both UA14 and C 60 for UA8. UAl4 or Collaro 3/6 wired for stereo. UA14 and C. 60 fitted monaural cartridge but

REREC IBATJEIRY IRADIOIN MAKIIRS' CAIRTON. Valves DK96. DF96, DAF96. DL96. Two Short Wavebands 2.5 to $7 \mathrm{Mc} / \mathrm{s}$ and 6.5 to $17 \mathrm{Mc} / \mathrm{s}$. Cabinet $12 \times 7 \mathrm{f} \times 61 \mathrm{n}$. UNLY $25(2 / 6 \mathrm{p} .8 \mathrm{p}$.$) ;$
MW and SW $\mathbf{~} 5.4 .0$ plus $2 / 6 \mathrm{p} .8 \mathrm{p}$ ).


SHLF-FOWEREN VIF TUNFIR CIlAs-is. Covering $88-95 \mathrm{Mc} / \mathrm{s}$. $10 \frac{1}{2} \times 4 \frac{1}{x} 5 i n$. hish ECC85, DF91. EF91 and 2 diodes. Metal Rectifier, Mains transformer. Fully wired and tested. Only er 14.0 (carr wired Room dipole $10 /$. 300 ohm twin feeder, 6d. yd. Tuner without power pack e6.14.0 (carr. paid).


## PUSH-PULL

 AMPLIFIER £4.15.0(4/-Carr.)
Brand new 200-240 A.C. mains Bass. treble and vol. controls W'Ith valves EZ80, ECC83 and 2 ELL 84 giving [ull 8 w. Chassis $12 \times 31 \times 34$ in. With o.p. trans. for $2-3$ ohm speaker.
Front panel (normally, screwed to chassis) may be removed and using as "flying panel". Sterea version $2 \times 4 \mathrm{w}$. same price.


COMPLETE V.H.F./A.M. RADIO FOR £12.10.0
 (carr. paid)
Brand new set, in superb walnut Covering $80-100 \mathrm{Mc} / \mathrm{s}$. 16 -49 in ligh). $200-500 \mathrm{M}$. Mains trans $200-2$ and with 2 tappings. Ferrite rod aerial to' A.M. Controls: volume onfoff tone, tuning. W/change. Gram and ext. speaker position provided Valves 12AT7, 12AH8, 6BJ6. EABCB0 6BW6 and metal rectitier Fully guaranteed. Today's Value £20.
('OLIAAKO NUDIO TAPE TRANSCRIPTOIR 3 MOH'ORS,
 nel. spool.

## SUPERIOR GRAMOPHONE AMPLIFIER 3 valves, 4 watt

$13 \frac{1}{2} 7$ in. ( 2 in. front to back). 3 front controls, bass. treble. vol./ on-ont. 600-240ac: "gold" fiet front : UY8

GiRAMOPIONE
With MMDHNHLR 5 SPEAKER Batfle 12 x 6 in. EZ 40 and EL41. Tone and volume On/Oif switch. Two Knobs. Ready to play. UseluI for Stereo. ONLY $57 /-$ post $3 /$.

3-VAINE AMILIIIER (INC. RECT, $2 \frac{1}{2}$ watts. ECC83, ECL82 and EZ80. Controls, volume bass and treble. Onfoff switch. Overall size $10 \times 4{ }_{x}$ 4itin. over valves. Mains and $O$.P. trans. and $6 \frac{1}{4} \times 4 \frac{1}{4} \mathrm{in}$. Celestion speaker. Suitable for microphone input and for guitar
amplifier. A.C. only.

70/- Р. \& P P 4

## MAINS OPERATED RADIO CHASSIS AND AMPLIFIER OF FAMOUS MANUFACTURE

Chassis $10 \times 54 \times 4 i n$ front to back.
Valves: UBC41, UCH41, UF89, UL84 with metal rectifier. sin. speaker. Ferrite rod aerial. Covers L. and M. waves. Limited quantity at only g6 (5/- carr.) complete with small dial. Unused and in working order.


## UNREPEATABLE OFFER OF AM-FM CHASSIS AT ONLY 89.9 .0 carr. pd.

A small quantity of Printed Circult chassis by famous manuiaeturer. Valves UY85, UCH81, UF89, UABC80, UL84 and UCC85,
O.p. trans. for $2-3$ ohm soeaker. Chassis 14 , 7 fin O.p. trans. For $2-3$ ohm speaker. Chassis $14 \times 7 \times$ Fin. Front "Gontrols concentric, left-Vol. and Tone: right-W/C and Tuning. "Gold" centre knobs provided. 2-dial bulbs. Sockets. AE: E : Ext. sp; P.U. Mains isolating transformer free. Covers Long, Med. VHF ( $87-101$ Mc/s). Unused slightly tarnished, but not tee. New Mullard Valves; not our manufacture, so no guarantee. Dial in gold and brown, size $13 \times 3 \nmid n$.

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(See other advertisement on page 918)
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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Special 24 Hour Express Mail Order Service |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AC2PEN $21 \%$ | ECC91 ECF80 | 4. <br> 816 | EZ35 61. <br> EZ40  <br> EZ41 $7 \%$ <br> 1.  | $\begin{array}{ll} \text { PCF80 } & 916 \\ \text { PCF82 } & 71= \\ \text { PCF84 } & 16 \% \end{array}$ | U12 U14 U22 | $\begin{aligned} & 91 . \\ & 91 . \\ & 81 . \end{aligned}$ | UY85 <br> VMS4B <br> VP4 | $\begin{aligned} & 7 / \\ & 12 / 6 \\ & 15 / 6 \end{aligned}$ | $\begin{aligned} & 5 Z 4 \mathrm{GT} \\ & 6 \mathrm{A7} \\ & 6 \mathrm{ABG} \end{aligned}$ | $\begin{array}{r} 1216 \\ 916 \\ 816 \end{array}$ | $\begin{aligned} & \text { 6LD20 } \\ & \text { 6P25 } \\ & \text { 6P28 } \end{aligned}$ |  | $\begin{aligned} & 12 \mathrm{C8} \\ & 12 \mathrm{JGT} \\ & 2 \mathrm{2JGGT} \end{aligned}$ | $8^{\prime 6}$ <br> 41. <br> $8 / 6$ |
| AC2PEN | ECF82 | 816 | $\begin{array}{ll}\text { EZ41 } & 71 . \\ \text { EZ80 } & 71 .\end{array}$ | $\begin{array}{ll}\text { PCF84 } & 16 \% \\ \text { PCF86 } & 151\end{array}$ | $\cup 22$ $\cup 24$ | $21 \%$ | VP4A | 1716 | 6A8GT | $13 / 6$ | 6 Q 7 | 616 | 12 K 7 GT |  |
| $\begin{array}{cc}\text { DD } & 21 \\ A C T P & 32\end{array}$ |  | 21\% | EZ80 EZ81 | $\begin{array}{cc}\text { PCF86 } & 1516 \\ \text { PCL82 } & 916\end{array}$ | U25 | 1216 | VP4B | 1716 | 6AB8 | 91. | 6Q7GT | 816 | $12 \mathrm{K8G}$ | 0\% |
| ACTP 32 |  | 216 | EZ90 71. | $\begin{array}{ll}\text { PCL83 } & 1216\end{array}$ | U26 | $10 \%$ | VR10530 | $7 \%$ | 6 AJ8 | 916 | 6SA7 | $7 \%$ | 12Q7GT | 616 |
| $\begin{array}{ll}A C V P 1 & 176 \\ A Z 1 & 151\end{array}$ | ECH35 | $10 \%$ | El148 2\%. | PCL84 1016 | U27 | 81. | VR15030 | 71. | 6AK5 | 51. | 6SG7 | $7 \%$ | 125A7 | $8 / 6$ |
| AZ31 10\% | ECH81 | 81. | FC2 211. | PCL85 16:- | U31 | 91. | VU39 | 91. | 6AK8 | 716 | 6SH7 | 61. | 12SK7 | 16 |
| $\begin{array}{ll}\text { B36 } & 10 \%\end{array}$ | ECH83 | 816 | FC2A $21 \%$ | PENA4 1716 | U35 | $17 / 6$ | VU111 | 216 | 6AL5 | 61. | 6SJ7 | 616 | $12 \mathrm{SQ7}$ | 816 |
| CIC 1216 | ECL80 | 91. | FC4 151. | PENB4 1716 | U37 | $17 / 6$ | VU120 | 216 | 6AM5 | $5 \%$ | 6SK7 | 516 | 7 | 81. |
| CBL31 216 | ECL81 | 101. | FCI3 21. | PEN4DD | U43 | 816 | W61 | 111. | 6AM6 | 4\% | 6SL7GT | 816 | 13 | 1216 |
| CCH35 21t. | ECL82 | 916 | FCI3C $21 /$. | 25!- | U45 | 101. | W76 | 5. | 6AN5 | 6 | T | 816 | $13 D 3$ $14 \mathrm{H7}$ | $12 \%$ |
| CL33 18'6 | ECL83 | 121. | FW4/500 9\%- | PEN4VA | U47 | $12^{\prime} 6$ | W77 | 4. | 6 | 616 913 | 6U4G | $10 \%$ | $14 \mathrm{R7}$ | $10 \%$ |
| CYI 15t | EF6 | 211. | FW4/800 9\%- | 1716 | U50 | 716 | W81 | $6 \%$ | 6AQ8 | 61. | 6U5G | 716 | 1457 | $15 \%$ |
| CY31 1519 | EF9 | 211. | GZ30 10/6 | PEN36C 21. | U52 | 716 | W | 816 | 6AU6 | 91. | 6V6 | 416 | 19AQ5 | 81. |
| D77 4! | EF22 | 141. | $\begin{array}{ll}\text { GZ32 } & 10 / 6\end{array}$ | PEN45 10 PEN450 | U78 | 416 | $\times 17$ $\times 18$ | $9 \%$ | 6B8G | 31. | 6V6GT | $8 \%$ | 19B6G | $21 \%$ |
| DAC32 916 | EF36 | 41. | $\begin{array}{ll}G Z 33 & 1913 \\ G 734 & 1316\end{array}$ | PEN45DD | U78 U191 | $4 \%$ $15 \%$ | 18 $\times 41$ | 15\% | 6B8G $6 \mathrm{BA6}$ | $6 \%$ | 6×4 | 416 | 20D1 | $10 \%$ |
| DAF91 716 | EF37 | 81. 81. | $\begin{array}{ll}\text { GZ34 } & 13 / 6 \\ \text { GZ37 } & 1913\end{array}$ | PEN46 ${ }^{22 / 6}$ | U251 | $12 / 6$ | $\times 61$ $\times 61$ | $12^{\prime 6}$ | 6BE6 | 61. | $6 \times 5$ | 416 | 20F2 | 1716 |
| DAF96 819 | EF37A | 8\% | GZ37 1913 $\mathrm{HABC80101}$. | PEN46 PEN453D | U281 | $18 \%$ | $\times 61 \mathrm{M}$ | 2216 | 6BG6G | $17 / 6$ | $6 \times 5 \mathrm{GT}$ | 51. | 20LI | 1716 |
| $\begin{array}{ll}\text { DCC90 } & 1416 \\ \text { DF33 } & 101 .\end{array}$ | EF39 | 4\% | HABC80101. HL41DD 816 | PEN453D $27 / 8$ | U282 | 1916 | +65 | 1216 | 6BH6 | 81. | $6 \times 6$ | 151. | 20P\| | 25\% |
| $\begin{array}{ll}\text { DF33 } & 10 \\ \text { DF91 }\end{array}$ | EF40 | $15 \%$ $8 \%$ | HL410D 816 <br> $H L 92$ <br> 16 | NDD 4020 | U301 | 2216 | $\times 76$ | 1216 | 6BJ6 | 61 | 630 L 2 | 10\% | 20P3 | 25. |
| DF92 7\% | EF42 | $10 \%$ | HLI33DD | 25\%. | U329 | 1216 | $\times 76 \mathrm{M}$ | 1216 | 6BQ7A | $12 / 6$ | 785 | $12 / 6$ | 20 P 4 | 22I. |
| DF96 816 | EF50A | 4. | $10 \%$ | PL33 15\% | U339 | $15 \%$ | $\times 78$ | 211. | 6BR7 | 1216 | $7 \mathrm{B6}$ | $10 \%$ | $20 \mathrm{P5}$ | 25\% |
| DF97 916 | EF50E | 316 | HN309 20\% | PL36 151. | $\cup 403$ | 10\%. | $\times 79$ | 211 | 6BS7 | $12 / 6$ | 787 | 816 | 2186 | 21\% |
| DH63 6\% | EF80 | $5 \%$ | IW4/350 10\% | PL38 211. | U404 | 101. | Y61 | 101. | 6BW6 | 71. | 788 | - | 25 | $8 \%$ |
| DH77 7\% | EF85 | 51. | IW4/500 10\% | PL81 12'. | U801 | 291. | Y66 | 916 | $6 \mathrm{BW7}$ | 5. | 7C5 |  |  | - |
| DK32 11'6 | EF86 | 1016 | KT33C 81. | PL82 8', | UABC80 | 0 71. | Z63 | $7 / 6$ | $6 \mathrm{~B} \times 6$ |  |  |  |  |  |
| DK91, 81. | EF'89 | $9 \%$ | KT36 17'6 | PL83 1016 | UAF42 | 816 | Z66 | $10 \%$ | 6 C 4 |  |  |  |  | $8 \%$ |
| DK92 816 | EF91 | $4 i$ | $\begin{array}{ll}\text { KT55 } & 1716\end{array}$ | PL84 91- | UB41 | 716 | 7 |  |  |  |  |  | 25 | 81. |
| DK96 816 | EF92 | $4^{\prime}-$ | KT61 916 | PL820 181. | UBC41 |  |  |  |  |  | 706 | 151. | 27SU | $17 / 6$ |
| OL33 816 | EF95 | 76 | KT66 15\% | PM24M 1316 | UBC81 | 816 | 2 Z 17 | 816 | 6 CD 6 | 126 | 708 | 151. | 30 Cl | 916 |
| DL35 10/6 | EF97 | 1276 | KT76 10\% | $\begin{array}{ll}\text { PX4 } & 15 \% \\ P \times 25 & 25 \%\end{array}$ | UBF89 | 716 | O24 | $5 \%$ | 6CH6 | 101. | 7H7 | 716 | 30 F 5 | 101. |
| DL92 716 | EF98 | 101. | $\begin{array}{ll}\text { KT81 } & 15 \% \\ \text { KT88 } & 21 \%\end{array}$ | $\begin{array}{ll}\text { PX25 } & 25 \% \\ \text { PY } 31 & 15 \%\end{array}$ | UBF89 | 716 211. | OR4 \| 47 | 1116 | 6CH6 6 D 2 | 10. | $7 \mathrm{K7}$ | 816 | 30 FLI | 1016 |
| DL93 7\% | EFI83 | 18\% | $\begin{array}{lr}\text { KT88 } & \text { 21\% } \\ \text { L63 } & 5 \%\end{array}$ | $\begin{array}{ll}\text { PY31 } & 15 \% \\ \text { PY } 32 & 1216\end{array}$ | UCL21 | 210'6 | 1 Al | 116 816 | 6 6 6 | 516 | $7 \mathrm{P7}$ | 10\% | 30 LI | 916 |
| DL94 8\% | EF184 | $14 \%$ 816 | $\begin{array}{ll}\text { L63 } & 5 \% \\ \text { LN52 } & 9 \% \\ \text { \% }\end{array}$ | $\begin{array}{lr}\text { PY } 32 & 1276 \\ \text { PY80 } & 716\end{array}$ | UCC85 | 716 | 1 C 2 | 91. | 6E5 | 101. | 7R7 | $12 \%$ | 30 LI 15 | 1116 |
| DL96 816 | EK32 | 816 | LN152 ${ }^{\text {LN309 }}$ 1216 | PY80  <br> PY81 716 <br> 1681  | UCFE0 | 1316 | 1 C 3 | 916 | 6 FI | 1016 | 7S7 | 101. | 30 P 4 | $21 \%$ |
| EA50 2\% | EL2 | 211 | LN309 126 | PY81  <br> PY82 716 <br> 16  | UCFEO | 1316 | $1 C 5$ | 1076 | 6F6 | 619 | $7{ }^{7} 4$ | 716 | 30 PI 12 | $10 \%$ |
| EABC80 61- | El-3 | $21 \%$ | $\begin{array}{ll}\text { LZ319 } & 126 \\ \text { MKT4 } & 1716\end{array}$ | $\begin{array}{ll}\text { PY82 } & 7 / 6 \\ \text { PY83 } & 8 / 6\end{array}$ | UCH42 | 216 | ID5 | 816 | 6FII | 10\% | 803 | 41. | 30 Pl 16 | 91. |
| EAC9] 41\% | Ei6 | $21 \%$ | $\begin{array}{lll}\text { MKT4 } & 1716 \\ \text { MS4B } & 1716\end{array}$ | $\begin{array}{lr}\text { PY83 } & 8 / 6 \\ \text { PZ30 } & 1816\end{array}$ | UCH81 | 81. | ID6 | $10 \%$ | 6 FI 2 | 41. | 9 BW 6 | $12^{\prime} 6$ | 30 PL I | 151. |
| EAF42 916 | EL32 | 416 | MS4B MYSPEN | P230 05910 10\% | UCL82 | $10 \%$ | 1 H5 | 916 | 6 FI 3 | $10 \%$ | 10 Cl | 1216 | 30 PL 13 | $12 / 6$ |
| EB34 216 | EL33 | 10\% | MVSPEN ${ }_{1716}$ | QS9510 | UCL83. | 1316 | IL4 | 51. | 6 FI 4 | $10 \%$ | 10C2 | $17 / 6$ | 35L6GT | $8 / 6$ |
| EB41 716 | E.34 | 15\% | MVSPENB 1716 | QSI5015  <br> R2 $10 \%$ <br> $10 \%$  | UF41 | 1316 716 | ILN5 | 416 | 6 FI 5 | 1216 | 10 Fl | 151. | 35 W 4 | 716 |
| EB91 4io | EL35 | 1716 | MVSPENB | R3 10\% | UF42 | 716 | IN5 | 916 | 6F19 | $12 / 6$ | JOF3 | 151. | $35 \geq 3$ | 1016 |
| ESC3 21/a | EL37 | 1716 | MUl4 91. | $\begin{array}{ll}R 3 & 816\end{array}$ | UF80 | 71. | IR5 | 716 | 6F23 | 1016 | 10F9 | $12^{\prime} 6$ | 35Z4 | 716 |
| $\begin{array}{ll}\text { EBC33 } \\ \text { EBC41 } & 46 \\ 916\end{array}$ | EL38 | 21. | MU14 $\begin{array}{lr}\text { MX40 } & \text { I5\% }\end{array}$ | $\begin{array}{ll}R 12 & 1716\end{array}$ | UF85 | 716 | IS4 | $8{ }^{6}$ | 6 F33 | 516 | 10LD\|1 | 151. | $35 \geq 5$ | 816 |
| 81 10\% | EL42 | 101. | N18 8\% | R19 191- | UF86 | 12'6 | IS5 | 716 | 6 H 6 | 21. | 10LD12 | $10 \%$ | 40SUA | 15\% |
| 816 | E181 | 1216 | N37 141. | R20 191. | UF89 | 616 | IT4 | 41. | 615 | 416 | IOP13 | 151. | 415 H | 211 |
| EBF83 876 | E.84 | 619 | N78 1716 | S130 716 | UL41 | $8 / 6$ | $1{ }^{\text {1 }}$ | 519 | 6J5GT | 416 | 10P14 | 191. | 42 | $12 / 6$ |
| EBF89 816 | E85 | 101. | N108 181. | SP41 316 | UL44 | 211. | 2 P | 2419 | $6 J 6$ | 316 | $10 \mathrm{P1} 8$ | 15\%. | $50 \mathrm{C5}$ | 1016 |
| EBL21 22\% | E. 90 | $8 / 6$ | N308 20\% | SP61 316 | UL46 | 1416 | 3A4 | 51. | $6 J 7$ | 51. | 11 D5 | $23 / 6$ | 50L6 | 816 |
| EBL31 2116 | E.91 | 41. | N339 15' | SU2150 25\% | UL84 | 76 | 3 A 5 | 106 | $6 J 7 \mathrm{GT}$ | 716 | $2 A 6$ | 6 | 50 CD 6 |  |
| ECC34 15\% | EL95 | 1076 | N369 1016 | SU2150A | UL85 | 716 | $3 \mathrm{Q4}$ | $8 \cdot$ | 6 K | 2)- | 12 A |  |  | 6 |
| ECC35 8\% | EM80 | 816 | OD3 5\% | 251. | UM80 | $10 \%$ | 3 C 4 | 9. | 6K7GT |  | 12AT6 |  |  | 81. |
| ECC40 21\% | EM81 | 816 | OZ4 516 | T41 15\% | URIC | $15 \%$ | 3 V 4 | - | 6 K 8 GT | 916 | 1 | 816 | 78 | 716 |
| ECC81 519 | EM84 | 916 | P2 10\% | TDD4 1216 | UU6 | 191. | $3 V 4$ $5 \cup 4$ | 8 | 6 K 8 GT 6 K 25 | 181 | $12 A \times 7$ | 716 | 80 | 91. |
| ECC82 816 | EM85 | 101. | PABC80 131- | TDD13C | UU8 | 21. | 504 | 46 | 6 | 131. | 12AU6 | 1716 | 85 AZ | $12^{\prime 6}$ |
| ECC83 716 | EY51 | 816 | PCC84 91. | 176 | UU9 | 116 | 5 5 4 | 816 | 616 | 716 | 12 BA 6 | 716 | 185BT | 301 |
| ECC84 816 | EY81 | 816 | PCC85 916 | TH41 2410 | UYIN | 126 1516 | $5 Y 3$ $5 Y 3 G T$ | 816 816 | 6L6 6 | $10 \%$ | 12BE6 | 716 | 305 | 916 |
| ECC85 8\% | EY83 | 151. | PCC88 151. | TY86F $12 \%$ | UY21 | 1516 716 | 5Y3GI 584 | 816 916 | 6 L 19 | 1716 | 12 BH 7 | $10^{\prime}$. | 807 BR | $5 \%$ |
| ECC88 17'6 | E.Y86 | 816 | PCC89 916 | UlO 9\%. | UY41 | 716 | 524 | 96 | 6 619 | 176 |  |  |  |  |

## METAL RECTIFIERS

| RMI | 513 | HRRA | 1-2-8-2 | 1716 (FC31) | 14497 | 25\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RM2 | 716 | 16R | 1-1.16-1 | 816 | 14 Al 100 | 27\%. |
| RM3 | 7/9 | [4RA | 1-2-8-3 | 191- (FC31) | 16RD 2-2-8-1 | 12'- |
| RM4 | 14'. | I8RA | $1 \cdot 1 \cdot 16-1$ | 616 ( $\mathrm{FCl\mid 6)}$ | 16RE 2-1-8-1 | $8 / 6$ |
| RM5 | 1916 | 18RA | 2-8-1 | 111. | I8RA 1-1-8-1 | 416 |
| 14A86 | 1716 | \#8RD | 2-2-8-1 | 15'-(FCl24) |  |  |

TERMS OF BUSINESS C.W.O. or C.O.D. 219 PACKING CHARGE ON ALL C.O.D. ORDERS. POSTAGE 6d. PER VALVE

## SPECIAL OFFER

EABC80 6'-, EAC91 41., EB91 41-, EBF89 816, ECC81 519, ECC85 81-, ECC91 41., ECH81 8/2, EBC33 4/6, EF39 4/1, EF50 3/6, EF80 5/-, EF85 5/., EF91 4/ヶ, DF91 4/-, EL84 6/9, PCC89 916, PL84 91., UABC80 71/, UBF89 716, UF41 7/6, UL41 816. UF89 616, UL84 7\%, UY85 7/-, W81 6\%, OZ4 5\%, $5 \cup 4$ 4 $\%$, 6AQ5 616, 6BA6 6\%, 6BE6 6\%, 6D2 41., $6 K 72^{\prime} \cdot, 6 K 1581 \cdot, 6 L 6716,6 \mathrm{Q} 7616,6 \mathrm{SL} 7616$,
 12AH89I-, I2BA6 716, 12BE6 716, ' $12 K 751 \%$, $12 Q 7616$.


Complete lighting fttings. Built-in ballast and starters-stove enamelled white and ready to work. Ideal kitchen, workshop-anywhere. Twin 20 approximately 27in. long complete With two 20W tubes, $49 / 6$. Single 40 approximately 4 ft . long omplete with one 40 W tube, $39 / 6$. Inductor so approximately 51 t . 49/6. Carriage and insurance up to 150 miles $7 / \theta^{4}$ up to 250 miles to 21in. Miniature complete with 13 watt tube. Ideal for show with 13 position where miniature fitting is required. Complete with latest fin. diameter tuble. $49 / 6$ eaoh. latest Cireular. Complete with 40 tube. 84.19.8.

Carriage and Ins. 7/6 any type.
Smallest Possible 2-gang


With built in trimmers, polystyrene cased. Size only $1 \times 1$ x'7/16in., price 12/6, Smallest IF and osclllator to match, 21/-. P.P. input and P.P. out put transformerg, 12/6. Ciroult diagram free with any of above.

## Transistor Set Cabinets



Very modern cream cabinet, size $5 \frac{x}{x}$ $8 \times 1+1 n$. With chrome handle, tuning knob and scale. Price 7/6, plus $1 / 6$ postage and packing.
Spectal quotations for quantities.
Miniature Earphones


For Transtator Circuits or Deaf Ata Very lightweight and easy to wear, cord almost invisible, good quality production of music and voice, oomplete with miniature plug and socket, for red spot and similar pedance OK Crystal and Mand similar transistors. Crystal and Magnetic, $9 / \%$. Post and
Insurance $1 /$-.

## SPECIAL TV SNIP!

BRAYHEAD TURRET TUNER With valves $39 / 6$
Both plos $2 / 6$ postage and insurance

## TRANSFILTERS

Save alignment problems and improve performance. Use instead of I.F. transformer. Complete with circuit $8 / 6$ each.

## CHARGING SWITCHBOARDS



Type A. 550 w .18 V .-contains three reverse current relays, one voltmeter rated 25 v. f.s.d.. one main ammeter rated 40 amps. I.s.d., one secondary ammeter 20 gmps . tis.d. one 2 anm tar secondary meters rated variable resistor and two 1.2 ohm variabie one 11 ohm Complete in metal cose 1.2 in $x$ resistors. Price et 15 metal case $21.61 n$. $x 2 t$. 81n. approx Type B. 1260 w .50 v. 0.12 arops-con
variable resistor and tour 1 ohm varins one 14 ohm one main ammeter rated at 40 amps is. dary meters rated at 20 amps. fis,d, and one voltmeter rated at 50 volts. and two reverse current relays. Complete in metal case-size approximately $2 f t$. 61 n . x 2 2t. Bin. Price g4.15.0. carriage 15\%-.
Connectiog Leads for these switchboards with Nifem plugs 30/-each.

## BATTERY CHARGER BARGAIN

## Components Would Cost More

 Car Battery Charger-ready-made high output battery charger in stove New. complete steel louvred case. rate selector for trickle charging also a meter to show charging rat. Suitable for $230 / 250$ A.C. mains. Special snip price of $65 /=$ plus $3 / 6$ post and ins.

## INFRA-RED HEATERS

Make up one of these
atest type heaters
deal for bathroom,
They are simple to mak
They are simple to make
rom our easy to follow
nstructions-uses silica enclosed elements designed for the correct for 750 watt for 750 watt element and instructions 15/6, plus $2 / 6$
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## LIMITED QUANTITY ONLY!

Waterproof heater wire. 16 yds. length. 70 watts. Self regulating temperature control. 10\%. Post Free.

## THIS MONTH'S SNIP!

## "ASUNVIC SIMMERSTAT" HEATER

 REGULATOR, suitable to control elements or heaters up to 2,500 watts on A.C. The unit Which is a ceramic body with bakelite case comprises a thermostat. adjustable for various temperature settings and in addition there used as an coll so that the thermostat can be used as an intermittent make or break (simmerstat arrangement, thus giving complete control SPECIAL SNIP PRICE of this unit is 12/6, plus $1 / 6$ postage and insurance. 230 volts. CLAD ELEMENT, 1,500 watts. for volts. 2ft. long. $17 / 6$ each. Post 2/6. Ideal for oonvector heater, which could be controlled by the above.
## "Dim and Full" Switch

Particularly useful for controlling photoflood lamps whioh have only a short life at tull brllhaace. 'This switch has three positions: the frrst position puts two lamps in series at half brilliance for setting up, the posind position 18 off and the third position full brillance for the operation shots. Also useful for controlling night lights, heaters etc. th. Price 3/9 each, post 9d. Circutt dias ram included.
Ditto but without the of position, 1.e.
d.p.d.t., 10 amp . $2 / 9$.
Morganite Potentiometers
 $50 \mathrm{~K}, 100 \mathrm{~K}, 250 \mathrm{~K}, 1 \mathrm{meg} .2 \mathrm{meg}$. Gang type 3/* oach-values availMeg 2 mer, $100 \mathrm{~K} \pm 100 \mathrm{~m} \mid \mathrm{meg}$.

## Component Storage Drawers



Btout board construction these drawers are ideal for smal parks. Supplied complete with simple erection instructions-1/6 each or 12
drawers each $6 \times 24 \times 641 \mathrm{a} ., 13 / 6$, post $2 /-$

## Yaxley Switches

| 1 Pole 3 Way | 6 |
| :---: | :---: |
| 1 Pole 5 Way |  |
| 1 Pole 8 Way | 6 |
| 1 Pole 12 Way |  |
| 2 Pole 2 Way | 28 |
| 2 Pole 4 Way |  |
| 2 Pole 6 Way | 218 |
| 2 Pole 12 Way |  |
| 3 Pole 3 Way |  |
| 3 Pole 6 Way | 16 |
| 4 Pole 4 Way | , |
| 6 Position Sho | rting **-.....-*.. 2)- |
| 6 Pole 3 Way | 218 |
| 6 Pole 3 Wry | 36 |
| 8 Pole 2 Way | ${ }^{0}-$ |
| 9 Pole 3 Way | 6 |
| 12 Pole 2 Way | ......****........** ${ }^{\text {y }}$ - |

## All parts for the "P.W. CITIZEN"

available

Price ed one parcel or separttely. please send for lish.
750mW TRANSISTOR AMPLIFIER


4 trangistors including two in push-pull-input for orybtal or magnetic miorophone for pick-up-feed baok
loops-sensitivity $5 \mathrm{~m} / \mathrm{v}-\mathrm{output} 1$ watt peak into 36 ohm speaker Speakers svaikable. Prioe $5 थ / 6$. Postage and Insurance 2/6.

# A NEW LOOK FOR The "GOOD COMPANION" 

## CAR RADIO \& PORTABLE

One of the finest of its kind available. The design is the combined efforts o our technicians and of those of several of the leading manufacturers in the country, and the resulting set has a performance as good as, if not superior to, those selling at $£ 20$ and more-It has the eight transistor set performance. Features include American Phitco R.F. transistors and Mullard A.F. transistorsQ.P.P. output giving 750 mW -full coverage on Medium and Long-very fine tuning arrangement-excellent reception of difficult stations like 208-variable feed-back control-full tonal qualities-really superior looking cabinet size $11 \times 8 \times 3 \mathrm{in}$. approximately-car aerial attachment-several months' operation from battery costing only 316.
Circuit employs six transistors and two diodes, it incorporates all latest refinements, and oscillater. I.F. Transformers are pre-aligned so no instruments are necessary. Anyone who can solder competently can make this set. The instructions are fully comprehensive with plenty of illustrations. Service is avaifable in the unlikely event of your getting into difficulties. All components fully guar. Price of all components Post and Insurance 5iand Standard Cabinet

Battery $3 / 6$ extra.
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MK. : uses latest ceramic transflters in place of the normal I. F. transproblers. This saves alimproves periormance. Price 10/-extra.

AGENTS wanced to build up our Companion Recelvers. Send addressed onvelope for fuli particulars.

## The "POCKET COMPANION" is now ready!

This is without doubt the most modern and best pocket set avallable. It uses the very latest I.F transflters. Philco R.F. transistors, alrspaced tuning condenser in Superhed circuit cover . Data iree with parts or separately cost £6.15.0. Battery $2 /$. Post and Ins. 2/6, Data iree with parts or sebarately $2 / 6$.


## MOST AMAZING BARGAIN! All components for the IMPROVED PIMPERNEL 5 Transistor Radio

that works really well!

## ONLY <br> 6916

Postage and Insurance 216 Battery 21-


This remarkable little recelver uses 5 transistors and 2 diodes. 3in. Moving Coll Speaker, Tuning Condenser, Volume Control with On/Of switch, latest type circuitr giving excellent station separation and ample voiume at PP4 battery. All components facluded for Medium Wave operation in Demonstrations at all branches Circuit diagram FREE with parts or $2 /$ - separately. OPTIONAL EXTRAS
All components and switch tor Long Waves

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## Proved without

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translstors reflexed to equal 4
stages. Permanent germanilum diode
and high gain AF output stage, fittud with
miniature speaker, proper thaing condenser, volume
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$50 \times 50 \mathrm{mfd}$., 350 v . 71- $100 \times 400 \mathrm{mfd}$., $275 \mathrm{v} .12 / 6200 \mathrm{mfd}, 275 \mathrm{v}$.
3i. $100 \times 200 \mathrm{mfd}, 275 \mathrm{v} .9 / 6 \left\lvert\, \begin{array}{ll}16 \mathrm{mid} ., & 450 \mathrm{v} . \\ 32 \mathrm{mid} & 450\end{array}\right.$
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## MODERN VALVES

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# 2 BAND SUPERHET CHASSIS <br> with Speaker <br> ONLY £4.19.6 <br> Plus 616 Post \& Packing. 



A quality 4 value $A C / D C$ superhet chassis made by a world famous manufacturer, Long and Medium wave coverage, Fitted with a cord and drum reduction tuning drive and attractive illuminated glass dial (size 6 . $\times 2 \frac{1}{2} \mathrm{in}$.) Conerols: Volume on/off, tuning and wave change. The receiver is self-powered, employing a mains dropper and a valve rectifier. Chassis dimensions $6 \frac{1}{3} \times 9 \times 5$ in high. Supplied complete with a good quality 5 -inch loudspeaker, valves (UCH42, JAF42, UL41, UY41), AC/DC mains input lead, ivory knobs, etc.
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A chassis of distinction, by a famous maker. Covering Long, Med. and Short Waves, plus gram position. this chassis (size $15 \frac{1}{2} \times 7 \times 6 \frac{1}{2}$ in. high) incorporates the latest circuitry, using fully delayed A.V.C and negatise feedback. Controls: Tone, Vol. On/Off, W/Change (L.M.S, and Gram). Tuning. Tapped input 200-250 v. A.C. only. An attractive brown and gold illuminated dial with matrhing knobs, make this one of the most handsome, in addition to being one of the best performing chassis yet offered. Complete ertorm (ECH81 EF89 EBC81 El84 EZ81), knobs, output transiormer, leads, etc. OUR PRICE ONLY \&9.19.6

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## MIDGET 2 GANG CONDENSERS

Polystrene cased, with built-in trimmers. Size I $\times 1 \times \frac{y}{16}$ ins. Not used, but removed from printed circuit boards.

## UNBEATABLE <br> VALUE 2 for $9 /=$

HARVERSONS' F.M. TUNER


At last a quality F.M. Tuner Kit at a price you can afford. Just look at thase fine features which are usually associated with equipment at twice the price.
NOW available

## 4 STATION PRESET CHASSIS with Speaker

 ume on/off and Programme (Long Wave), Third Programme to Light Service and Light Programme (Medium Wave), but may of course be adiusted to alternative selections if required. A frame aerial with throw-out extension is supplied, making this receiver ideal as a general purpose transportable set for the home. A fully smoothed power supply is provided from AC/DC mains input by a mains dropper and a valve rectifier. The good tonal qualities are assisted by the provision of a quality 5 in . speaker, which is readymounted on the chassis (this is easily detachable if alternative positioning is required), Valve line up, UCH42, UAF42, UL41, UY41. This chassis (size $9 \times 6 \frac{1}{2} \times 5 \frac{1}{2} \mathrm{in}$. high) is supplied complete with valves, knobs, mains lead, acrial, etc. It is beautifully made by a famous maker, and is a first-class buy at the rock bottom price of only £4.17.6, plus $6^{\prime} 6$ post and packing. made from heavy gauge metal which has been specially de- signed to house the above F.M. Tuner. Beautifully finished in a choice of glossy hammer green, or hammer grey enamel, or black cracklc. The front panel (illustrated) has holes for control spindles, and apertures for tuning dial and magic eye. PRICE $25 /=$ P. \& P. 1'9. (Front panel only 1016, P.P. 9d.).

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Probably one of the most outstanding soldering instruments yet produced, this iron has a derachable handle which can be placed over the bit and barrel, enabling it to be carried in complete safery even when hot. The provision of an extremely stable 30w element makes this ideal for transistor and all similar lightweight applications. Brand new in P.V.C. bag, with lead and plug. ONLY 18\%, plus 1/3 P. \& P.

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A deaf aid type earpiece of top grade quality. Gives an exceptionally crisp reproduction of both speech and music. Brand new and fully guaranteed. Two types available. CR-5 high impedance crysta MR-4 low impedance magnetic. $7 / 6$ Plus II. crystal,
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P. \& P.
F.M. TUNER HEAD


A permeability tuned tuner head by a famous maker, supplied without valve (ECC85) 1816 plus 119 P. \& P. Valve 816 extra.

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## Introducing HARVERSON'S

 rom dellighted purchesers of our BUPER STEREO KIT" We have produped a "MONAURAE AMPLIFIER" on simil. 5 lines.

- A UCL 52 vaive provides a triode ampltiying stage, ard a pentode outbut staye ( 3 watts). Enabling cood amplitication and sparking reproduvtion to be combined with physich com, )achness (amolitier size, $7 \times 3$ ! $x$ stin. hishl.
$\star$ Modern arcuitry design, soon quallt: O.P. transformer (to matoh 3 al keep hum and distortion to a low tevel.
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* The amplifier nas a buititin tuily quallity maing rieansformer a (A.C. mains only) and metal recritter.
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| OC36 | - | *.. | *** | 101 | GET15 (matched pr.) |  |  | $16^{16}$ |
| - 0 C44 | *** | *** | *** | 910 | GETI02... | $\cdots$ | ** | 716 |
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## TRANSISTOR SPEAKER

Western Electric $3 \Omega$ or $80 \Omega$ spaaker. Size $2 \frac{1}{2} \times$ Hin. deep. 12'6 p.p. $1^{\prime}$-.
SUPERHET CHASSIS-less Valves \& Cabinet Modern AC/DC chassis with printed sircuit and ferrite rod atrial. Although not completely built, the main components are mounted. L. \& M. wave coverage, 4 valves 1 UBf89, UCL83, UCHBI, UYB5). Evarything supplied exeep? valvas and cabinet. With speaker and simple $\{3,6,6$ plus 316 instructions.

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3 I.F. Transformers, one oscillator coil, one driver transformer, and wound ferrite aerial (Med., Long and aerial coupling) $28 / 6$ complete, post $1 /=.6$ transistor printed circuit board to match 816, post 9d. Cirsuit diagram $1^{1 / 6}$ extra.

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50 mixed P.F. Condensers and 50 mixad Resistors. An assortmont of useful valves. All popular sizes-all new-a must for the serviceman and constructor $10 / m$
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THE HARVERSON 6 TRANSISTOR \& DIODE SUPERHET KIT
A first class 2 wave band transistor superhet in kit torm.
$\star$ Printed circuit panel (size $8 \frac{1}{8} \times$ $2 \frac{3}{4}$ ins.)

* 3 Pre-aligned I.F. Transformers.
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All parts down to the minutest item with simple instructıons. ONLY


Plus $2 / 6$ P. \& P.

Cabinet to Suit (if available) 151. extra.


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AT LAST—A COMPLETE F.M RECEIVER IN K!T FORM
Specially designed with the home constructor in mind, this kit enables the construction of a sompletely self-contained V.H.F. receiver, at fraction ol the normal cost of comparabie equipment. This is basieally a quality sellpowered F.M. tuner plus 2 separate audio amplifier stages, and output transformer and spaker.

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* Two I.F. Stage and Discriminator.
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$\star$ Valves used ECC85, two EF80's, ECL82 and EZ80 (ractifier).
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## AMPLIFIER KIT

A kit designed to meet the exacting requirements of the audio enthusiast, yet remain within the price range of the average constructor. A stylishly finished monaural amplifier with an output of 14 Watts from 2 EL84's in push pull. Super reproduction of both music and speech (Frequency response $\pm 3 \mathrm{~dB} \mathrm{c} / \mathrm{s}-60 \mathrm{Kc} / \mathrm{s}$ with negligible hum.) Separate inputs for mike and gram allow records and announcements to follow each other and make this amplifier ideal for small halls, youth clubs, etc. Fully shrouded Ulera Linear output transformer (to match $3-15 \Omega$ speaker), and fully shrouded mains transformer (these alone are worth over (3.10.0). 2 independent volume controls, and separate Bass and Trebie controls are provided, giving good lift and cut. Valve line up 2 EL84's, ECC83, EF86 and EZ80 rectifier. All parts down to the last nut and bolt, including valves, knobs, heavy gauge metal chassis finished in glossy hammer green enamel, mains and output transformers finished to match. P. \& P. $6 / 6$ (simple instruction booklet $1 / 6$, free with kit).
only $£ 6.19 .6$

## QUALITY RECORD PLAYER AMPLIFIER KIT

A top quality record player amplifier in kit form. This amplifier (which is used in a 29 -gn. record player) has a printed circuit and has an internal fully smoothed power
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A very fortunate purchase allows us to offer this quality table radio cabinet for only 1816 (this cabinet cost the manufacturers 35/-
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OUR PRICE
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A kit of ready-built units only requiring interconnection. Comprising two midget $3 W$ amplifiers, push button switch, transformer, control unit (bass, treble and vol.), power pack, two speakers, indicator light valves (ECL82, EZ80 range), and comprehensive instructions.

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\text { 23. } 8.6 \begin{aligned}
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E.M.1. 4-speed Player and P.U.


Heavy 8 zin. metal turntable. Low flutter performance $200 / 250 \mathrm{~V}$ shaded motor with tap at 80 V for amplifier valve filament if fier valve filament
required. Turnover required.
LP/78 head.

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$600 \mathrm{ft}, \quad 13 / 9,5 \frac{1}{4} \mathrm{in}$. $\begin{array}{lll}\text { spool } 850 \mathrm{ft}, & 18 / 6, & 7 \mathrm{in} \text {. } \\ \text { spool } 1200 \mathrm{ft}, & 31 . & \text { Extra- }\end{array}$ spool 1200ft, 231 I-. Extraplay tape, $3 \frac{1}{2} \mathrm{in}$. spool $300 \mathrm{ft}, 71-$, 5 in . spool 900 ft . 211-, $5 \frac{1}{2} \mathrm{in}$. spool 1275 ft , $26^{\prime \prime}$, 7 in . spool 1800 ft , 3716. Empty spools, $3 \frac{1}{4}$ in., $1 / 6,5 \mathrm{in} ., 21$, 7 in., $3 \%$.

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[^1]February, 1962

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| 574 G | $8 / 6$ | 6F6M | 71 | 6 BH 7 | 418 | 12Af | 5／－ | － 2586 | 12／－ | C10 | $7 / 6$ | EbCRi | \％／8 | F．F86 | $9 /-$ | KT68 | $8 / 8$ | PY80 | $7 /=$ | U PG41 | 7／9 | X 76 M | 12／6 |
| $5 / 490$ | 11／－ | 6 F 8 G | $8 / 8$ | 68， $\mathrm{IV}^{7}$ | 4／6 | 12AH7 | 6／9 | 27：4 | 25／＊ | CBL31 | 21／－ | ERF80 | $7 / 8$ | E F＇99 | $6 / 9$ | KT6 | 14／3 | PY81 | 6）－ | UBC81 1 | 101－ | X78 | $14 / 6$ |
| $6 / 30 \mathrm{~L} 2$ | 9／－ | 6 F 12 | 316 | dsK7 | 5／8 | 12A H8 | $9 / 9$ | 3041 | 716 | CC＇H35 | 14／－ | EBF89 | $8 / 6$ | EF91 | 81－ | KT76 | $8 / 6$ | PY82 | 6／8 | UBF89 | $7 / 9$ | $\times 79$ | $16 / 8$ |
| 6A6 | 718 | $6 \mathrm{Fl13}$ | $6 / 9$ | 6817GT | 81－ | 12AT6 | $7 / 6$ | 30 F 5 | $8 / 9$ | CL33 | $11 / 9$ | EBL21 | 12／6 | EF92 | 4／6 | KTW61 | $5 / 9$ | PY83 | $7 / 6$ | UBL21 1 | 14／6 | X 81 M | $8 /=$ |
| 6A7 | 10／＝ | 6Fl4 | 916 | 68N7GT | 418 | 12AT3 | $5 / 8$ | 30 FLl | $9 / 8$ | CY31 | 716 | EBL31 | 21／－ | CF95 | 6／8 | KTW63 | 519 | PR330 | $9 / 6$ | UCust 1 | $14 / 6$ | Y63 | 6／3 |
| BABG | 9／6 |  | $9 / 6$ | $6897$ | 81 | 19AU7 | 6／－ | 30 LL | $7 /$ | D63 | 1／6 | EC52 | 3／8 | EK32 | $71-$ | KTZ88 | $5 / 6$ | R 18 | 11／－ | vCC85 | $7 / 8$ | 288 | 6／－ |
| 6ABGT | 18／－ | $6^{6818}$ | 816 | 6SSy | 4／8 | 12AK7 | 6／9 | 30 P 41 | 12／6 | D77 | 816 | EC90 | 3／6 | ELa3 | $8 / 9$ | L88 | $5 / 6$ | 819 | 11／－ | UCF80 1 | 16 | 206 | $6 / 8$ |
| 6AB8 | 7／－ | 6F38 | $6 / 6$ | 6 U 40 T | 10／6 | 12B46 | 81／ | 30210 | 81 | D152 | $5 / 8$ | EC91 | ． $4 / 6$ | EL38 | 8／－1 | LN158 | 71 | 8D6 | 8／6 | UCH21 1 | 18／6 | 277 | 81－ |

13 Channel TV＇s－Absolutely Complete
These sets are mequalled in value．They are untested and are not gusranteed to be working．
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## LOUDSPEAKERS

Top Makes manufacture ireah，2tin．13／－；万in．18／－；
 21／－； $3 \times 18,29 /=$ ，

## PM SPEAKERS

${ }_{\text {Bin }}^{3}$ ohms，top makes periormatice guaranteed，
 1,000 YDS．ASSAULT CABLE P．V．C．comered uteel，Ideal lelephone lines，garden lay． $9 /-$ drim．Postage $4 /-$

Valves all guaranteed 3 months PL81 SOLLED，AMAZING $4 / 6$ EY51 $\underset{\text { ENDS }}{\text { SHORT }} 4 / 6$ U25 $\underset{\text { ENDS }}{\text { SHORT }} 8 /=$ COMPLETE RECORD PLAYERS B．S．R．DA14，4－Syuead Autochanger ．．${ }_{88} 190$ B．S．R．DARO，Autochanger

$$
\begin{aligned}
& \text { Autochanger } \\
& \text { P. \& P Po above 4/-" }
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 with the following CARTRIDGES：ACO 3 a．P． 35．3．29／B：SONOTONE， $17 /-:$ STELG and REUTER 151－；POWRE PONT， $17 \%$ All Al the sbove cota－ plete with＂ $\mathrm{BTARR-GALAXY}$＂Tone Arm，3／－extra．
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single Bifole． 3 Eiement，Wall roountiug． $32 / 6$
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＂TRICQLOUR＇NIashiight，with Focus． Red，Greed and White light，7dju．tong．
Battet ter $1 / 2$ esch．P．P． 4 d.

AERLAL OSCLLLATOR COILS，LONG
AND MEDIUM WAVE
pr．4／6
Square Pluss and Sockets，Fused， 13 amp．
6／6
SILICONE DIODES
$12 \pi \nabla .50 n$ M．A． 2 thi geriea make sinperior replace－ weut tor R．M．t and K．M．⿳亠二口，etc．8／－each．

## RECTIFIERS

For Chargers，seleninno full wave， 12 rolt， 8 84 amps，

 15RA1－1－L61－1／9；1SRD2－2－8－1，14／－；14RA1－2－8－2 177－；14FAL－2－4－3．20／－．

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7／029， 15 amp .2 core，power cable，1／－yd．； 3 core， 1／6 yd．i $\$$ amp．P／C Twin Flex，4d．yd， $100 * g d$ drom．30／－，pilus postage

## P．V．C．WIRE SPECIAL BARGAIN

 100 yds． 30 milt special price $7 / 6.200$ yds， 30 mull． 12／6．P．P．2／．CO－AX standard sod low lose， 25 yds， $12 / 4$, Pluys $1 / 3$ ．Wall outiet boxes $8 / 6$ ．

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Full VHF Band (87-108 Mc/s and Medium Band. $187-570 \mathrm{M}) \star 7$ Valves $\star 5$ Watts Output Wide range Bass and Treble Controls $\star$ wide range Bass and Treble Controis $\star$ 2 Compensated Pick-up Inputs $\star$ Frequency Response $30-22,000$ c.p. $9 . ~ \pm 2 \mathrm{db} \star$ Tape Record and Playback Facilities $\star$ Continental Reception of Good Programme Value $\star$ For 3 . 7 and 15 ohm speakers.
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DK98, DF96, DAF96, DL96, 8/6 each or 27/6 eet. 1 R §, 1T4, 185, 384 or 3V4. $19 / 8$ $8 \mathrm{~K} 8,6 \mathrm{~K} 7,6 \mathrm{O}, 6 \mathrm{6} 6,5 \mathrm{~h} 4$ or 6 X 5 . CCH81, EF89, EBC41,
12K8, 12K7, 12Q7, 35 LG .3524 . $35 /=$

| ELECTIROLYTICS |  |  |  | FANOUS MAKES |  |  |
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| T |  | TUBULA |  |  | TYP |  |
| 1/350V | 2/- | 50/350V |  | $16 / 4$ |  | \% |
| $2 / 350 \mathrm{~V}$ | $2 / 3$ | $100 / 25 \mathrm{~V}$ |  | $32 / 350 \mathrm{~V}$ |  | 41. |
| $4 / 450 \mathrm{~V}$ | 8/3 | 250/25V |  | $100 / 270 \mathrm{~V}$ |  | 5/6 |
| $8 / 450 \mathrm{~V}$ | 2/3 | $500 / 12 \mathrm{~V}$ | 3/- | $2,000 / 6 \mathrm{~V}$ |  | 4/- |
| 81500 V | 2/9 | $8+8 / 450 \mathrm{~V}$ |  | 8,000/6V |  | 5/0. |
| 16/450V | 3/- | $8+8 / 500 \mathrm{~V}$ |  | $32+32 / 8$ | 50V |  |
| 16/500 ${ }^{\text {P }}$ | 4/- | $8+161450 \mathrm{~V}$ |  | $32+32 / 4$ | 50 V | 8/- |
| 82/450 ${ }^{\text {P }}$ | $3 / 0$ | $8+16 / 500 \mathrm{~V}$ |  | $32+32$ |  |  |
| 25/25v | 1/8 | $16+16 / 450 \mathrm{~V}$ |  | $50+50$ |  |  |
| $50 / 25 \mathrm{~V}$ | 21-1 | $16+18 / 500 \mathrm{~V}$ | 8/-6 | $64+120$ | 350 V | 11/6 |
|  |  | 32/35 |  | $100+200$ | 1275 |  |

TUBULAR TUBULAR CAN TYPES
$\begin{array}{llll}1 / 350 \mathrm{~V} & 2 /-50 / 350 \mathrm{~V} & 5 / 616 / 45 \mathrm{~V} \\ 2 / 350 \mathrm{~V} & 2 / 3 & 100 / 25 \mathrm{~V} & 3 /-32 / 350 \mathrm{~V}\end{array}$

| $4 / 450 \mathrm{~V}$ | $2 / 3$ | $250 / 25 \mathrm{~V}$ | $3 /-100 / 270 \mathrm{~V}$ |
| :--- | :--- | :--- | :--- |
| $8 / 450 \mathrm{~V}$ | $2 / 8$ | $500 / 12 \mathrm{~V}$ | $3 /-2000 / 6 \mathrm{~V}$ |

$8 / 500 \mathrm{~V} \quad 2 / 98+8 / 450 \mathrm{Y} \quad 3 / 65.000 / 6 \mathrm{~V}$ $16 / 450 \mathrm{~V} \quad 8 /-8+8 / 500 \mathrm{~V} \quad 5 /-32+32 / 350 \mathrm{~V}$ $\begin{array}{llllll}10 / 000 \vee & 4 /- & 8+16 / 480 \vee & 8 / 9 & 32+32 / 450 \mathrm{~V} & 6 /- \\ 82 / 450 \mathrm{~V} & 3 / 0 & 8+16 / 500 \mathrm{~V} & 5 / 6 & 32+32+32 / 350 \mathrm{~V} 7 /-\end{array}$ $\begin{array}{lllll}25 / 25 V & 1 / 9,16+16 / 450 \nabla & 4 / 3 & 50+50 / 350 V & 7 /- \\ 50 / 25 \nabla & 2 /-16+16 / 500 \nabla & 6 /-64+120 / 350 \nabla & 11 / 6\end{array}$ $50 / 60 \% \quad 2 / 832+32 / 350 \mathrm{~V} \quad 4 / 6100+200 / 2757 \quad 12 / 6$

## C.R.T. BOOSTER TRANSFORMERS

For Cathode Ray Tubes having heater cathode short circuit and for C.R Tubes with falling emission. Full instructions supplied.
Type A. Optional $25 \%$ and $50 \%$ Boost. 2 V or 4 V or 6.3 V or 10.8 V or 13.3 V . Mains input. TYPE A2 High quality, low capacity. $10 / 15 \mathrm{pF}$. Optional boost $25 \%, 50 \%$. $75 \%$ Mains input.
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## COMPLETE RADIO

## £4.19.6 post free



4 Mullard valves, Sin. speakers, frame aerial. 4 pre-set stations. 1 long, 3 med. wave. Superhet Circuit.
Size $9 \times 6 \times 5 \frac{1}{4} \mathrm{in}$. high. Tested ready for use. $200 / 250$ v. A.C.-D.C. Mains.

MAINS TRANSFORMERS $200 / 250$ V. A.c. STANDARD tapped 4 ₹. 4 a. Rectitter 6.3 v. 1 a 5 v. Ma or 4 v. 2 a. 22/6 ditto, $350-0-350$ Minamo 200 v. $20 \mathrm{~mA}, 0.3$ v. 1 an .. 2016 MIDGET, 240 v. $45 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{~s} . \quad \because \quad 15 / 6$ SMALL, $22000 \cdot 020,50 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a}$.. $17 / 6$ STD., $250 \cdot 0-\frac{20}{2} 0,6 \overline{0} \mathrm{~mA}, 6.3 \mathrm{v} .3 .5 \mathrm{a} \quad \because \quad 17 / 6$

 Ditto, rec. 6.3 . ${ }^{2} 3$ smp. GENERAL PORPOBE LOW VOLTAGE, 2 $3,4,5,6,8,9,10,12,15,18,24,30 \mathrm{\nabla}$. $22 / 6$ AUTO TRANSFORMERS. 150 \%. .. 22/6 $0,120,200,230,230$ ₹., 500 w. $\quad \because \quad 82 / 6$
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 4 AMP CAR BATTERY CHARGER with amp meter Leads, Fuse Case, etc., for 6 v. or 12 v., $^{69 / 6}$.

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PYE STEREOPHONIC PLAYER Complete with Giarrard TA MKI Stereo unit and selt contained quality deep $x 8{ }^{-}$hifer, size 14 Wide $x$. deep x oth hafin brand new in maker' antee. OUR PRICE E12.10. Carrias and Insurance, $10 /$. 2 , Sultable for use with any two of ohm loudspeakers.

LOUDSPEAEER PM. \& 0EM. $2 \mathrm{H}, \mathrm{8}$, $4 \mathrm{~m} .19 / \mathrm{L}$ sin . Hols, 17/8; 8in. Pleasey, 19/8. 7in. x 4in. Rola

 8ita. 45/\%.
STENTORIAF HEIO1R 10Hn. 8-16 olmma, 10 w.. 96/-

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Details B, A. R.
121n. Baker 15 w . Stalwart 8 or 15 ohms, $45-13,000$ c.p.n. ... .. 90/uspension, 15 ohme, 40 13,500 c.p.e. 12ln 8tereo, $12 w_{n}$ 35. $16,000 \mathrm{c}, \mathrm{pas}$
12 in . Baker DItra Twelve,
20 c.p.s. to $25 \mathrm{ke} / \mathrm{s}$. 317.10
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TWIN GANG TUNIG COMDRMERES 305 pH
 with trimmers, $9 /=:$ midget, $7 / 8$; with triminern, $0 /$ SMALL 3 gang $500 \mathrm{pF}, 17 / 4$.
SIHGLE $26 \mathrm{pF}, 50 \mathrm{pF}, 75 \mathrm{pF}, 100 \mathrm{pF}, 180 \mathrm{pF}, 5 / 6$. sohd dielectric $100,300,600 \mathrm{pF}, 8 / \mathrm{E}_{4}$ i
CONDENSRR8. NeF stock. 0.001 mfd. $7 \mathrm{k} \nabla$
 Tubular 500 7. 0.001 to 0.05 mid., gde, $0.1,1 /=$ $0.25,1 / 8 ; 0.5 / 500 v_{c}, 1 / 9 ; 0.1 / 850 \mathrm{~F} ., \%$; $0.01 / 2,000$ v

CERAMIC CONDS. 500 च. 0.3 pF to 0.01 mid., od SILVER MICA COMDENGERS, $10 \%$ p DP to 500 PF $1 /-: 600 \mathrm{pF}$ to $8,000 \mathrm{PR}, 1 / \%$ Close tolerance $( \pm 1 \mathrm{pF}) 1.5 \mathrm{pF}$ to $47 \mathrm{pF}, 1 / 8$. Ditto
to $815 \mathrm{pF}, 1 / 9 ; 1,000 \mathrm{pF}$ to $5,000 \mathrm{pF}, 2 /$.
$465 \mathrm{ke} / \mathrm{s}$ SIGNAL GENEIRATOR Total cost $15 /{ }^{2}$ U Uses B.F.O. Unit SIZEL $24 x 41 \times 11 n$, Slight modiflcations required, full instructions supplied. Battery $7 / 6$ extra $69 \mathrm{~V}+14 \mathrm{~V}$. Detalls S.A.E.

Wavechange Switches 2 p. 2-way 3 p. 2 -way, short spindie, ef6; 8 p. 4 way 2 waier, long spindie, 6/6; 2 p. 6-way,
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## CRYSTAL MIKE INSERT <br> Pret Acos 8/6 <br> size only lin. dia. x tin.


Valveholderg. Pax. int. oct. 4d. PA50, 6d. B12A. CRT, 1/3. Eng. and Amer. 4 5,6. and 7 pin, i/a. MOULDED Mazds and int. oct., 6d.: B7G. B8A, B8G. B9A, 9d. B7G with can, 1/B, B9A with can, $1 / 9$. Coramic EF50, B'G. B9A, int oct. $1 \%$ $7 B G$, B9A cans. $I$ - each.

THE ORIGINAL RADIO COMPONENT

 $\begin{array}{lll}\text { COAX PLUG } \\ \text { PANEL SOCKETS } & 1 /- & \text { LEAD SOCKET.: } \\ \text { OUTLET BOXES } & \text { 4/- }\end{array}$ BALANCED TWIN PEEDER yd. $6 d .80$ or 300 ohme. DITTO SCREENED per yd. 1/8. 80 ohtise Onis. WIRE-WOUND POTS. 3 WATT. Pre-get Mid. TV Type. Al values 10 ohms to 25 K. . $31-\mathrm{ea}$.
 Values. 50 onme to $50 \mathrm{~K} .$. b/6: 100 K ., 7/6. PRILPS TRIMMERS. 30 DF $1 /$ -
TRIMMERS, Ceramio. 30, $30.70 \mathrm{pF} ., 9 \mathrm{~d} . ; 100 \mathrm{pF}$. 150 pF., $1 / 3 ; 250 \mathrm{pF} ., 1 / 8 ; 600 \mathrm{pF.}$,750 vF ., $1 / \theta^{\prime}$. RESISTORS. Proferred vainel. 10 ohma to 10 meg.,
 HIGH STABILITY. \& w., $1 \%, 2 /$. Preterred vainen. $10 \Omega$ to 10 mes. Ditto $5 \%$, $100 \Omega$ to 5 mek., 9 d . 10 watt ${ }^{5}$ wath WIRE-WOUND RESISTORS $\} 1 / 8$
 18.5 K to 50 K 10 w

| AMERICAN "BRAND FIVE" PLASTIC RECORDING TAPE |  |  |  |
| :---: | :---: | :---: | :---: |
| Double Play <br> Long Play | ort |  | Spare <br> Plastic Reels |
|  | Bia. reel, 1,2unit |  |  |
|  | 719. reel, 1,800rt |  |  |
|  | 5 tia. reel, $1,200 \mathrm{ft}$ |  | 3in. $1 / 6$ |
|  | Sinu reel, 9000f | 18/6 |  |
| 8tandard | 7in. reel, 1,200tr |  | $\begin{aligned} & 3 \operatorname{lin} .8 / 2 \\ & 7 \mathrm{in} .2 / 6 \end{aligned}$ |
|  | Sis. reel. 600 ft . |  |  |
| "IDstant' Bulk Tape Eraser and Head Defluxer, 200/250 V. A.C., 27/6. Leaflet. S.A.E. |  |  |  |
|  |  |  |  |  |

Radio Screwdriver;in. 6d,
Neon Mains Tester Serewdriver, 5/Solker Radiograde, 4d. yd., t1b. 5/-. Black Crackle I'alnt. Air drying, 3/- tin.

> HIGH GAIN TV PRE-AMPLIFIERS
> BAND 1 B,B,C.
> Tunable channels 1 to 5 . Gain 18db. ECCB4 valve. Kit price 29/6 or $48 / 6$ with power pack. Details 6d. (PCC84 valves if preferred.)
> $\begin{gathered}\text { BAND III I. T.A.-Same prices. } \\ \text { Tunable channels } 8 \text { to } 13 \text {. Gain } 17 \mathrm{~dB}\end{gathered}$

Paxolin Panels, $10 \times 81 \mathrm{n} ., 1 / 6$
Minlature Contact Cooled Rectifiers. $85 \mathrm{~mA}, 9 / \mathrm{B}: 200 \mathrm{~mA}, 81 /-: 300 \mathrm{~mA}$. $2 \% / 6$.
Selenium Rect. 300 Y 85 mA . $7 / 6$.
Colls. Wearite "P" type. 3/- each.
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ANS CARINET. OGMOR DE: SIGNED KIT, E8.15.0.

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Vol. XXXYII No. 660 FEBRUARY, 1962.


## Wired Wireless and Commercial Radio

IT seems only a short time ago that the "wired wireless" was as prominent a topic for conversation as $625-$ line TV is teday, and yet little has been heard of it since. Surely the idea deserves much greater attention and, in fact, the time is fast approaching when a practical application of this form of transmission, in its fullest sense, must be found. Sending a radio signal over a wire is, in fact, what is meant by the term "wired wireless", and one very well-known application of this is the employment of voice-operated carrier systems, over coaxial cables, on the trunk telephone systems. By this means hundreds of simultaneous telephone conversations can be carried on a single cable, without interaction.

A really practical development of this form of radio, would be that in which the normal house wiring systems, which after all, are in effect "networked" and serve the majority of homes in the country, could be used to carry not only normal radio programmes, but commercial or sponsored radio, as well as television on various channels. It would not be a very great step to make these systems of such a type that coin-operated selecting devices could be incorporated to provide not only revenue but various forms of 'exclusive' programmes. Both the telephone system and the lighting services in this country are operated on a national basis, and therefore there would be no difficulty about using the existing wiring. The actual development of a technique which would permit the use of all forms of broadcasting, including what we now know as V.H.F., or F.M., together with television, should not present insurmountable difficulties. It would, of course, limit programmes to each country and perhaps render unnecessary such developments as resulted in the superhet receiver. It would also remove many difficulties, not the least of which would be the fringe area, the need for interference suppressors, and last, but by no means least, the mass of unsightly decorations on our roof tops. (The forthcoming television development on Bands IV and V will lead to greater congestion on our roof tops and it appears highly probable that the Pilkington Committee will recommend some form of "wired wireless" or "carrier wireless" for sound only to enable commercial sound programmes to be inaugurated.)

There may be a limit to the number of transmissions which could be dealt with in this manner, and perhaps the inclusion of television may complicate matters, but surely this is one very good ground for development of radio, and the day must come when radio and television programmes will form part of the domestic service supply systems, taking their place with the electric light, water and other essential services.
 Our next issue dated March, will be published on February 7th

## Ronnel the Worlal of Wireless

## POTENTIALAND

 CURRENT NEWS
## Broadcast Receiving Licences

THE following statement shows the approximate number of Broadcast Receiving Licences in force at the end of October, 1961, in respect of wireless receiving stations situated within the various Postal Regions of England, Wales, Scotland and Northern Ireland. The numbers include Licences issued to blind persons without payment.


## Sweden Orders Eighty-two Transmitters

THE Royal Board of Swedish Telecommunications has placed another order for sound and television broadcasting transmitters with Marconi's Wireless Telegraph Company Limited.

The new contract calls for the supply of 21 vision transmitters, 21 sound transmitters, 40 fre-quency-modulated sound transmitters and a considerable quantity of programme input, paralleling, feeder and ancillary equipment.

The transmitters are intended to augment Sweden's already extensive television and VHF frequency modulated sound broadcasting systems by providing first-class reception in the northern area and in what are at the moment fringe areas throughout the country. Deliveries, at the request of the Royal Board of Swedish Telecommunications, are to be spread over the next four years.

## Transmitter for Satellite Communications Project

A CONTRACT for the supply of a transmitter for use by the GPO in satellite communication experiments, to be carried out next year in co-operation with the Amercan authorities, has been awarded to Standard Telephonez and Cables Limited.


These two independent sideband transmitters and aerial exchange were
installed in a station outside Ankara. Turkey. installed in a station outside Ankara, Turkey.

The equipment will be installed in a room built into the 85 ft diameter steerable aerial now being erected at a site on Goonhilly Down, in Cornwall. The transmitter will operate in the $2000 \mathrm{Mc} / \mathrm{s}$ communication band, and will deliver a frequencymodulated output of 10 kW .

Additional items to be supplied by the company include power equipment for the transmitter and a water-to-air heat exchanger unit.
The present programme calls for the whole transmitter to be installed on the site and fully operational by April, 1962. An active repeater communication satellite to be launched by the U.S.A. authorities will enable tests to be conducted on television transmission and two-way speech communication between Cornwall and the American ground station at Rumford, Maine.

## Communications Transmitters in Turkey

$\mathbf{A}^{S}$ part of its programme of technical assistance to member countries of the Central Treaty Oganisation, the British Government have presented radio communications equipment to Turkey. Two independent sideband transmitters. aerial exchange, and matching transformers were among the pieces of equipment presented, and these were made by Marconi's.

The installation is at a transmitting station outside Ankara, Turkey.

## Royal Navy Order

THE Admiralty has awarded a contract for the supply of a number of 500 W medium-fre-quency/high-frequency independent sideband communication transmitters to Marconi's Wireless Telegraph Company Ltd., together with high-stability master oscillators and remotely controlled aerial matching units.

## Weather Radar Orders

'【HE new duplicate version of the Type E190 airborne weather radar, which is a product of Ekco Electronics, has been ordered by Short Brothers and Harland Lid. for installation in ten of their new Belfast air freighters. This equipment employs a dual transmitter/ receiver and indicator system, in keeping with the current practice of duplicating essential services which are the subject of mandatory requirements. Fully "failsafe" conditions are thus provided. either transmitter/receiver operating with either indicator unit.

Ekco airborne weather radar is also to be installed in the de Havilland Comet 4 airliner recently ordered by King Saud of Saudi Arabia.

## VHF Sound Broadcasting Station

 for Northern IrelandTHE BBC's new VHF sound broadcasting station at Londonderry which is on the same site as the BBC's television station at Sherriffs Mountain was brought into service on 23rd October. This is one of the twenty-one new VHF satellite stations so far approved for extending the coverage of the VHF sound service to over $99 \%$ of the population of the United Kingdom.

Londondery radiates the Northern Ireland Home Service on $92.7 \mathrm{Mc} / \mathrm{s}$, the Light Programme on $88.3 \mathrm{Mc} / \mathrm{s}$, and the Third Programme together with Network Three on $90.55 \mathrm{Mc} / \mathrm{s}$. The signals are horizontally. polarized, which means that receiving aerials should be horizontal. The programmes are fed by Post Office cable from a special receiving site at Glenderowen where they are received by radio from the BBC's VHF station at Divis.

The new station brings the BBC's VHF sound broadcasting service within reach of some 120,000 additional people in the counties of Londonderry and Tyrone.

## 4th Jamboree-on-the-Air

FROM 00.01 hours GMT on Saturday, 21st October until 23.59 hours GMT on Sunday, October 22nd radio hams from forty countries all over the world took part in the Boy Scouts' 4th Jamboree-on-the-Air.
In this country alone there were over forty stations operating. One of these was in the recently opened Baden-Powell House in South Kensington.

This year Scout stations were on the air in Australia, Canada and the Philippines. In previous years contact has been made with Scouts in America, Canada, Holland, Sweden. Finland, Germany. Bermuda. France, Norway and New Zealand.

## Changes in Times of International Time Signal

FOR over one hundred years, the Royal Greenwich Observatory has been responsible for providing exact time signals for a wide variety of users both at home and abroad.

In recent years this service has become increasingly important in various fields of scientific research where extreme accuracy 'is essential.

In order to provide the various users with more frequent opportunities for checking the time. on 1st December, the daily transmissions from Rugby were increased from two to four.

This means that the transmissions on the low frequency of $16 \mathrm{kc} / \mathrm{s}$ until recently radiated at $10 \mathrm{a} . \mathrm{m}$. and 6 p.m. are now superseded by signals at 3 a.m.. 9 a.m., 3 p.m. and 9 p.m. There is, however, $n o$ change in the form of the signals.

To ensure a world-wide coverage. the $10 \mathrm{a} . \mathrm{m}$. and $6 \mathrm{p} . \mathrm{m}$. broadcasts have also been transmitted on short wave. This service is continuing, but the times have been changed to 9 a.m. and 9 p.m.
The transmissions from Rugby are proving to be indispensable to users all over the world. Such persons as marine surveyors and scientists engaged in tracking artificial satellites will undoubtedly find the new and more frequent transmissions of great value.

## Ten High Power Short Wave Transmitters

THE British Broadcasting Corpozation has placed an order with Marconi's Wireless Telegraph Company Ltd. for the
supply and installation of ten high-power ( 250 kW ) short-wave sound broadcasting transmitters of a new type which, when they come into service, should very materially improve overseas listeners' reception.
Six of these transmitters will be installed at the "Voice of America" relay station at Woofferton. Two more will go into service at the BBC station at Rampisham and the remaining two at Daventry.
The transmitters are specially designed to combat the ever increasing amount of interference experienced by overseas listeners on the short waves. This is achieved by employing a method of modulation which cuts through the interference to bring the signal to the listener. Intensive experiments have shown that the use of this trapezoidal modulation, as it is called, gives an intelligibility at the receiving end which could only otherwise be brought about by more than doubling the transmitter powerthat is, in this instance, from 250 kW to 550 kW . The overall efficiency of the new type of transmitter is approximately double that of the older equipments supplied to Rampisham and Daventry.


A transmitter of the type to be supplied by STC to the GPO for use in sotellite communication experiments. On the left is the power control cubicle (double width), with the drive unit in the centre and the klystron power amplifier cubicle on the right. This transmitter operates in the $2000 \mathrm{Mc} / \mathrm{s}$ communication band, and will deliver a frequency-modulated output of 10 kW .


# A HIGHLY SENSITIVE DOMESTIC RECEIVER 

By V. E. Holley

$J_{\text {HIS }}$receiver will perform satisfactorily in most parts of the country. Though small in size, its overall sensitivity is above average and unless reception conditions are very unfavourable it will work quite well on two or three feet of wire as a "throw-out" aerial. The valves, which at first sight may seem an odd assortment, have been selected (as will be explained) for low cost and high performance.

## Aerial Circuit

Referring to Fig. 1, the signal from the aerial is passed first through the 1.F. rejector, L1, C1, which is an iron-cored inductor tuned to the intermediate frequency. It will be found useful in coastal areas where morse transmissions around $500 \mathrm{kc} / \mathrm{s}$ are apt to find their way into the I.F. amplifier; in other areas it will probably not be required and can be omitted. The filtered signal passes via the switch S1 to the appropriate aerial coil and thence via $\mathbf{S} 2$ to the grid of the first valve.

> midget mains

## Output Stage

In order to economise in the bulk, weight and cost of the power supply, a Mazda octal valve SP61, is used in the output stage. This valve can be obtained very cheaply indeed and although intended for R.F. amplification it makes a very satisfactory small power valve. It has a high slope and an output of one watt can be obtained in return for a modest signal at the grid. Grid and cathode resistors are 1 M and $150 \Omega$ respectively.

If the greatest gain is required in the output stage the resistor R16 can be by-passed by an electrolytic capacitor of $100 \mu \mathrm{~F}$ and this will increase the sound output. The output transformer in the anode circuit should have a ratio of about $70: 1$ for a $3 \Omega$ speaker and can be of the type usually described as "small pentode."

## Negative Feedback

The SP61 is a very efficient amplifier of radio frequencies and it is necessary to arrange that any such frequencies reaching it shall be excluded from the output. Accordingly, frequency selective negative voltage feedback is taken from the anode via the capacitor C 21 , to the cathode circuit of V3.

## Second Negative Feedback

If maximum overall gain is not required, a second negative feedback loop, effective at all frequencies, can be formed by connecting a resistor of from 200 to $1,000 \Omega$ between points $X$ and Y in Fig. 1.

## Power Supply

The total H.T. current in the absence of a signal is 35 mA at about 220 V , while the valve signai is 35 mA at about 220V, while the valve
heaters and dial lamp need approximately 0.15 A at 6.3 V . This is supplied by a miniature mains transformer, the high voltage half-wave secondary of which feeds a metal rectifier, DRM1. A contact cooled rectifier is equally suitable. The rectified current is taken first through a fuse, which is in fact a 63 V .0 .15 A bulb; though not essential. this is a useful safeguzrd against the consequences of short circuits, catastrophic failure of capacitors, etc. Smoothing is provided by the capacitors C22, C23 and C24, and the resistors R17 and R18. This double stage arrangement gives good smoothing with negligible voltage drop, an important point if as in the prototype, the transformer voltage is only 220 . The values of these resistors must be
adjusted according to the output of the trans former-rectifier combination so that the H.T. line voltage in the receiver is $220 \pm 10$ in the absence of a signal. Miniature transformers do not usually have tapped primaries so the mains supply voltage must also be taken into account.

## Components

The tuning scale and the gang condenser must be selected for compatibility if the transmissions are to be received at the points indicated on the scale. The coils may be any standard dust-cored components covering the long and medium wavebands and the trimming and padding capacitors should be of the values recommended by the


Fig. 1-The circuit of the receiver.



Fig. 2-The drilling details of the aluminium chassis.


The completed receiver without the cabinet.
makers. The values given in Fig. 1 are fairly typical and may be used in the absence of more authoritative information. Most manufacturers feature a suitable I.F. rejector coil in their range, either with or without the parallel fixed capacitor, C1.

## Tuning Drive

The tuning drive can be made from an old volume control. Remove the body and fit to the rear of the spindle a brass coupler in which a groove has been cut for the drive cord. Holes must, of course, be cut in the chassis for the cord to pass up to the drive drum and down again.
The resistors may be $\frac{1}{2} \mathrm{~W}$ except for R4, R17 and R18, which should be of 1 W rating and, because the H.T. comes on through the metal rectufier before the valves are warmed up and ready to receive it, all the capacitors should be 350 VW except for C 18 , for which 25 VW working will be adequate.

## Mains Transformer

The mains transformer must be a miniature type and it is convenient though not essential that the tuning condenser be semiminiature. All other components can be standard. The trimmers C2 and C16 should be fitted to the top of the gang condenser, which also carries a bracket for the dial light.

## Construction

The receiver is constructed on a chassis of 18 s.w.g. aluminium sheet, $9 \frac{1}{2}$ in. $x \quad 4 \frac{1}{2}$ in. $x \quad 1 \frac{1}{2}$ in. (Fig. 2).
(To be continued)

## 16m TO

175m

## TRANSISTOR S.W. TUNER

## A UNIT DESIGNED TO BE USED WITH A SEPARATE AMPLIFIER

## By

## F. Neville Hart

nOW that short-wave tran* sistors have become about as cheap as valves and there are coils on the market for frequencies as high as the VHF bands, the simplicity of transistor circuits opens up an attractive field for the experimenter.

The set described here is a portable tuner which can be plugged into any amplifier, such as a tape recorder, or radio provided with 'gram' input terminals. It has a 3 ft 6in. telescopic chromium plated aerial fixed in a 3-ply, leather cloth-covered cabinet, which was built to house the set. The construction of this is not described as readers may have their own ideas on carpentry.


Fig. 1-The front panel layout.


Fig. 2-The complete circuit diagram. Note that if instability occurs in the R.F. Stage, C4 should be reduced in value from $0.003 \mu F$ to $0.001 \mu F$.

## Frequency Coverage

The coverage is approximately from 16 m to 175 m , in three ranges, using a nine-pole threeway switch with three wafers. A number of these are obtainable as "surplus," but switch makers will make them up for about 15 s . each.

Any I.F. coils for use with transistors can be employed, but since the short-wave tuning coils are made by Repanco, the use of their I.F. coils is described here. Although an R.F. stage rather complicates adjustment and trimming, it assists the rejection of second channel interference and gives better selectivity and volume.

The set compares favourably with the author's battery superhet with R.F. and two I.F. valves. Volume depends upon the amplifier following, but the output part of a transistor radio using driver and push-pull OC72's gives sufficient volume in the author's caravan, where, indeed, most of the construction was carried out.

## Aerial

Although its own aerial is normally used, pick-up can be improved by using a longer aerial.
(To be continued)

## Experimenter's



# THE FINAL DESIGN AND CIRCUIT 

(Continued from page 824 of the January issue)

By M. L. Michaelis

ЭHE power unit is extremely versatile, giving outputs of almost all types normally required in the experimenter's workshop. Whilst the unit is definitely advanced in nature, and thus not advisable for the the beginner. it is felt that it will meet a long-felt requirement for the more experienced constructor. who, once he has built it, will find virtually all of his power supply problems solved in one.
The outputs provided are the following:-
(a) A stabilised H.T. output, continuously variable from 120 V to 350 V , at a nominal maximum current of 100 mA .
This nutput can thus be used for virtually any H.T. requirements, from batteryvalve circuits requiring 120 V H.T. at the one extreme, to mains-valve circuits requiring the higher voltages up to 350 . Stabilisation is such that the remaining effective internal impedance is about 500. so that in most cases several pieces of apparatus can be fed without mutual interference.
(b) An unstabilised H.T. output of about 300 V , fully independent and capable of supptying some 50 ma . This is intended for operating various pieces of apparatus. such as a valve voltmeter or a test oscillator, etc., at the same time as the experimental circuits being worked on are being fed from the main stabilised H.T. supply.
(c) Two neon-stabilised output voltoges, one at plus 90 V and the other at minus 100 V , relative to earth (chassis). These are capable of being loaded up to about 1 mA each. Their purpose is for providing facilities for any bias-bleeder chains that may be required in advanced experimental circuits. and to this end they may be used together or independently.


## The outhor's unit

(d) A.C. heater outputs at $4 \mathrm{~V}, 6.3 \mathrm{~V}, 10 \mathrm{~V}$ and 12.6 V . All are rated at 4 A marimum continuous loads. By simultaneous loading at various of these voltages, the total current must not exceed 4A:
(e) Low-voltage D.C. output at a maximum of 18 V and a maximum of 2 A . This output is intended for a variety of uses. It is not stabilised. but it is fully smoothed. and is variable by means of a variable wire-wound resistance. It can be used for the following purposes:-
heating battery valves of 1.4 V or 2 V type;
heating mains valves with D.C. in circuits requiring this;
charging accumulators (anything from a single 2 V cell to a 12 V car-battery);
feeding transistorised apparatus. On account of this last envisaged use, the positive pole of the supply is earthed. and not the negative pole, as is otherwise more usual. This does not in any way impair the other uses named.
(f) An output at 110 V A.C. up to about 100 W . for feeding any $110 \%$ apparatus that may come in for attention. (It is assumed that the power unit is to be built for $230 / 250 \mathrm{~V}$ mains. but if readers' local mains have other voltages, then it is merely necessary to purchase transformers with the appropriate primary windings.

A comprehensive system of indicator pilotlamps, fuses and other protective measures are incorporated, and a definite orderly plan has been devised and followed in the allocation of switchfunctions. These features will all become apparent in the course of the circuit description below.

## Checking Output

A multi-purpose monitor system is built-in, for metering any of five important voltage outputs and any of five important current outputs. Two moving-coil meters are used, with suitable switching, shunts and multipliers. One meter functions as voltmeter and the other as current meter. Any one voltage and any one current may be displayed at any one time. The meter may be switched on to voltages and currents on load, and this process does not disturb the functioning of the power unit. Thus if all five outputs are simultaneously loaded, the meters may be switched successively to read off all circuits in turn, without disturbing them.

All outputs are fully independent. Thus, for example. the low-volts D.C. output may be connected to charge accumulators, and at any time the other sections of the power supply used for feeding electronic circuits. After checking for correct charging current, the meters may be switched over to monitor the H.T. and other circuits being used. At any time the meters may be switched momentarily back to the accumulators on charge, to check that charging is still correct. This is only one example of possible simultaneous uses of the power supply, so that in actual fact the power supply serves the purpose of several smaller power units. This represents a considerable saving in space and expense, compared to the actual construction of the equivalent range of separate power units.

## Heat

Attention has been given to the question of adequate heat dissipation. This has been successfully achieved whilst at the same time satisfying the apparently contradictory requirements of maintaining, as compact a form as possible. In the author's unit the front panel is approximately one foot square, and the cabinet is 6 in . deep. To make the best possible use of the space available, the usual chassis construction has been rejected in


favour of a "spatial-construction"., This latter form of construction is more difficult than conventional chassis construction, but has the advantage of complete utilisation of the available cabinet space, thereby reducing the size of a unit by at least a factor of two. However, the layout of the whole circuit is in all respects fully noncritical, so that those constructors who can tolerate a larger final size of unit may use the normal chassis form of construction, with any convenient layout. Adequate insulation is more important than any particular layout.


Front view of the rectifier sub-chassis.

## Procedure

The "spatial-construction" consists of building the unit in the form of several sub-units. A wooden cabinet is used. with two sides, top, bottom, front panel and back. Any one of these six pieces of wood is independently removable, by means of loosening the appropriate screws. Construction is started on the basepiece of the cabinet, on which all larger components are mounted and wired up (transformers, etc.). In the case of the power unit here described, the next step was to make a small bracket-chassis on which the metal rectifiers and associated circuitry were mounted. This rectifierunit was then also mounted on the basepiece. When all the wiring of the basepiece was complete, all points to be connected to other components not on the basepiece were wired to suitably positioned tagstrips. The next stage was to make the front panel, on which all outlets. switches, fuses. lamps. controls. etc., were mounted and wired up. A sub-unit containing the low-volt D.C. rectifiers and smoothing was also mounted on this. All points to be connected elesewhere were again taken to tagstrips. The third stage was
then to make a small chassis containing all the valves and associated circuitry, and mount this on the right-hand side panel of the cabinet, again taking all points to be connected elsewhere to a suitably positioned tagstrip. The fourth stage was then to mount the few remaining components (in this case the A.C. relay, the smoothing choke and the output condenser) on the left-hand side panel. Nothing is mounted on the top-piece or the back of the future cabinet.

## Inter-wiring

Four separate sub-units have now resulted, on four pieces of the future cabinet. These are now laid on the workbench in such a position relative to each other that (a) all parts of all of them can be reached comfortably for repairs and alterations, and (b) they are nevertheless as close as possible to their proper relative positions in the final asembled cabinet. The units are now interconnected by neat bunches of insulated wires, of the correct lengths, running between the tagstrips of the various units. After completion of this work, the power unit is electrically complete, and may be switched on and tested. If all is found satisfactory, the four sub-units and the top-piece of the cabinet are screwed together with woodscrews, to form the cabinet. All cable-bunches are neatly tucked away in positions where they cannot chafe or otherwise be damaged. After cutting suitable ventilation holes in the back panel, this is screwed on too. It remains to label all items externally on the front panel and to paint the cabinet as desired, and the power unit is then ready for service.

## Interlocking

The geometrical arrangement of the components on the four sub-units is such that complete spatial interlocking (without, however, touching and shorting of components) is achieved within the cabinet after assembly. The arrangement used by the author satisfies some further points, too:-
(a) All valves are immediately accessible for quick replacement if ever required. Thus the valve chassis is at the rear, reached as soon as the back is removed, without further dismantling.
(b) All components generating much heat, principally the transformers, choke and valve chassis, are mounted at the rear, so that they induce a strong convection current through the generous ventilation holes in the rear panel, and do not heat up the rest of the circuitry unnecessarily.
(c) The build-up otherwise avoids horizontal layering, and stresses vertical channelling, to give full freedom to convection cooling; the author's prototype has been on non-stop operation for periods of up to one week without the slightest indication of undue heating.

The detailed building plans to be given will bear out these points, but it must be borne in mind that considerable modifications may be necessary according to the actual shapes and sizes of components individual constructors may purchase or have available. For this reason it was stated above that this type of construction is more difficult than a conventional chassis. It is absolutely essential that the constructor should collect all essential components together, and then sit down and very carefully envisage the complete final construction.
(To be continued)

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[^3]
# Thand Mithug Topice 

## A CLASS "A" MODULATED MINIATURE VALVE TRANSMITTER.

$\checkmark$

HE transmitter described here is a single, compact unit with its own modulator and power supplies, and is constructed on a chassis $7 \frac{1}{i n}$. $x$ $11 \frac{1}{\mathrm{in}}$. $x 2 \frac{1}{2}$ in. Send/Receive switching is incorporated, so that it is only necessary to add a receiver to obtain a complete table-top type of
station. There is no need for an aerial changeover relay, or separate control of the receiver. Instead, the one control on the transmitter provides complete change-over from transmit to receive, and this is found very convenient when working.


Fig. 1-The complete circuit diagram of the transmitter.

The circuit is shown in Fig. 1. The Spot and Tune switch applies H.T. to the oscillator only. This allows the transmitter frequency to be located exactly with the receiver, so that the latter can be tuned to the same frequency. It also permits tuning up the transmitter for suitable grid current, and shows where the signal will fall. compared with other stations which may be working. If a VFO is used, it allows the transmitter to be netted on another transmitter frequency, ready to answer a call.

## Switching

The Send/Receive switch applies H.T. to oscillator, modulator and P.A., and connects the aerial to the transmitter. When in the transmit position it disconnects the receiver speaker, to silence this. When the switch is turned to "Receive" the aerial is connected to the receiver, the speaker is in operation, and the transmitter H.T. supply is off.

The 6AM6 oscillator will operate at fundamental frequency, or as a doubler. This permits 2-band working with one crystal. Two crystals will give four operating frequencies in two bands. Grid drive when operating as a doubler is almost the same as when working on the fundamental.
The 6BW6 will run at up to 10 W input, which is of course the maximum permitted on the 160 m band. It was found generally best to load to an input of about 40 mA and this resulted in 9 and
even 9 -plus reports, with a correctly coupled dipole. Ain end-fed aerial, preferably correctly tuned at the transmitter, would give almost similar results.

## Modulation

A high-gain double triode is used in the modulator, so that a crystal microphone may be employed. With 250 V on anode and screen grid, the 6AQ5 has a power output approaching 4.5 W and reports or monitoring indicate that good modulation and speech quality can be expected. When a class-A stage is operating normally, the anode never swings completely to zero voltage. This means that over-modulation in a downward direction (which must always be avoided) cannot arise. It will be found that attempts to increase the modulation too far will cause distortion due to overloading of the audio amplifier. This will be apparent on a simple monitor, whereas vvermodulation may not. For this reason it was decided not to add a P.A. condenser and resistor dropper, such as may be used with class-A modulators. This change might make over-modulation possible. and was not felt necessary, after testing the circuit as in Fig. 1.
The transmitter requires approximately 100 mA at 250 V , so a large receiver or amplifier type transformer will suffice. Heaters consume 1.5 A at 6.3 V . The rectifier was a 5 U 4 G , which needs 5 V at 3 A , but $5 \mathrm{R} 4,5 \mathrm{~V} 4$ and similar rectifiers are


Fig. 2-The above-chassis wiring.


Fig. 3-The underchassis wiring.
equally suitable. No separate mains switch was used because the transmitter and receiver were controlled from a single switch. The transmitter heaters rua continuously, in the usual way.

## Chassis Layout

This is shown in Fig. 2 and is not very critical. The P.A. tuning condenser should best be at least 200 pF , or it may be necessary to modify the number of turns on the $\pi$ coil, when changing from one type of aerial to another. (A surplus condenser was used here.) The 30 pF air-spaced neutralising condenser is soldered to the fixed plates tag. The other lead from the 30 pF condenser passes through the chassis to the junction of the oscillator anode coil, 22 k resistor, and 1000 pF condenser.

For aerial loading a 2 -gang broadcast type receiver condenser has sections wired in parallel. A short lead passes from the coil to the fixed plates.

A simple screen round the crystal holder was found useful as some of the valves are quite near. It is preferable to use valve screens over the 6AM6 and 12 AT7.

It is necessary to meter both grid and anode current, and this can be done with two scparate instruments, or with a single meter and 2 -way switch, as will be described next month. The meters, or meter and switch, occupy the left of the panel.

## Underchassis Wiring

Fig. 3 shows all components and wiring. The space is divided into sections for the modulator, oscillator. and output stages. Heater wiring is completed before mounting the screens, which are notched to allow the heater connections to pass. These leads should run close against the chassis.

The modulator is built in the small section near the microphone socket. An insulated tag bolted to one screen serves as a H.T. anchor point. Two screened leads pass round the end of the other screen, to the volume control. Externally, a screened lead should be used for the microphone, to reduce R.F. pick-up and avoid hum. The 47 k resistor and 50 pF condenser provide some R.F. filtering.

A speaker output transformer was found to be satisfactory for the modulator A.F. choke. A reasonably large transformer, rated to carry about 100 mA , is required. A component intended for mains pentodes is suitable.

The second screen passes across the 6BW6 valveholder, which is so positioned as to have grid tags behind the screen. and anode and g3 tags in front. Sufficient is cut from the screen to clear the holder.
(To be continued)

# Improving Broadcast Receivers 

By K. Berry

## A SMALL INVESTMENT IN A • FEW NEW COMPONENTS WILL REJUVENATE AN OLD SET

(Continued from page 853 of the January issue)

9N all of the additional R.F. circuits described last month, no extra AVC voltage was used, i.e. in all the circuits which were given, the AVC was applied either to the original frequency changer or to the new amplifier. This is in fact completely satisfactory except where the receivers are operated very close to a transmitter-under these circunistances some overloading could occur. This possibility could be eliminated by always applying the AVC voltage to the R.F. stage (see Fig. 6, last month).

It is perhaps worth mentioning that whilst the circuits given in Figs. 3 and 5 were untuned, it is very easy to include a single, fixed-tuned circuit which will have the result of increasing the R.F. gain a! (and close to) the resonant frequency of this tuned circuit whilst retaining the general increase in gain over the whole band. This will thus enable any particular desired frequency to receive extra amplification-e.g. a circuit tuned to 208 m would give a considerable increase in gain for reception of Radio Luxembourg.

If it is desired to fit such a tuned circuit, it should be connected between the grid of the R.F. stage and the 10 k grid leak resistor.

## Components

Components values are given only for those components shown in the circuit which are additional to those already in the receiver. The valve recommended is an EF92.

If the layout of the receiver will allow it, extra gain may be obtained in the circuits given in Figs. 3 and 5 by using an EF91 or EF80. In this case, the screen is taken straight to H.T. + and the cathode resistor should be reduced to $150 \Omega$. Since these valves give a very high gain it might be necessary for the H.T. supply to the R.F. stage to be decoupled-a resistor of 2.7 k in series with the supply to the anode and screen, with a $0.1 \mu \mathrm{~F}$ capacitor to chassis should suffice.

## Incretased I.F. Gain by Additional I.F. Stage

A typical superhet I.F. stage is shown in Fig. 7. This is shown again in Fig. 8 with the addition of another stage of amplification preceding the original I.F. stage. This additional I.F. stage may be mounted directly on the receiver chassis; alter-


Fig. 7-Circuit of a typical superhet I.F. stage.


Fig. 8-The circuit of Fig. 6 with the addition of an extra I.F. stage.
natively it may be mounted on a small sub-chassis which is in turn bolted to the main chassis.

This new I.F. stage is controlled by the set's AVC, thus no overloading problems should occur. The normal techniques associated with the R.F. wiring must be employed if instability is to be avoided, i.e. short, direct leads-anode and grid leads kept away from existing "hot" wiring, etc.

## Components

As previously, component values are given only for those components shown in the circuit which
additional component required for this modification, but a considerable improvement is effected.

## Tone controls

It will normally be found that "tone" controls of the top-cut variety operating on the primary of the output transformer will be virtually inoperative when feedback is applied in this manner (or indeed in any manner). The reason for this is that negative feedback tends to "straighten out" the frequency response of an amplifier whilst the effect


Fig. 9-A typical audio output stage with a resistor Rx added to give negative feedback.


Fig. 10—This circuit shows how the extra feedback resistor forms the upper part of a potential divider (see text),
of the "tone control" is to distort the frequency response so that the net result is that the influence of the tone control will be very much reduced.
are additional to those already in the receiver. Once again the valve recommended is an EF92. The use of an EF91 or EF80 here should not be attempted as neither of these valves fasa a vari- $\mu$ characteristic, thus preventing the use of AVC.

## Improving the Frequency Response of the Audio Stage

This is a very simple modification, and in the author's opinion, the most worthwhile one. Most commercial domestic receivers have a triode L.F. stage followed by a pentode or beam tetrode output stage: It is not usual to employ negative feedback, and "tone correction" is effected by shunting the primary of the output transformer with a capacitor. This sometimes has a fixed resistor in series with it, or somerimes a potentiometer which serves as a "tone" (or top-cut) control. The average receiver of this type has a considerable excess of audio gain, and this can be reduced considerably by the use of negative feedback. This will result in reduced distortion and improved frequency response-particularly at the L.F. end.

In Fig. 9 is shown the L.F. side of a typical domestic receiver. This receiver has fixed "tone correction" by means of the capæcitor across the primary of the output transformer. Shown connected between the anodes of the L.F. and output valves is a resistor, Rx. This is the only

## Potentiometer

The method of operation of the feedback circuit is shown in Fig. 10. It will be seen, that the feedback resistor forms the "upper" part of a potentiometer which divides the output of the valve. The "lower". part of the potentiometer is formed by the anode load of the previous valve and the grid leak of the outpit valve in parallel. The exact value of $R x$ will depend on how much gain can be "thrown away" and the values of the anode load of the previous valve and the grid leak of the output valve. As a rough guide, the ratio of the potentiometer should be about $10: 1$, so if for example, the anode load is 100 k and the grid leak resistor is 1 M , the shunt value of these is 91 K : hence the feedback resistor Rx will be about $10 \times 91 \mathrm{k}=910 \mathrm{k}$. The nearest value to this in $20 \%$ resistors would be 1 M .

## Applying Feedback

It must be emphasised that applying feedback in this manner will result in reduced A.F. gain, so if your radio has no gain to spare-do not try this. If there is no gain to spare, it is possible to obtain more by removing the existing double diode triode and fitting a pentode valve in its place. The diodes can be replaced by germanium crystal diodes.


## Experimental Hardships

IT is surprising what a lot of time can be wasted when you are carrying out expcriments and are not in a position to have parts properly checked before use. I recently heard of an engineer who was a keen radio experimenter and who owned both $R$ and $C$ bridges with which he used to check all components before using them. The one big thing he lacked, however, was a valve tester. He tells me that he was carrying out some experiments with a new instrument in which were three double triode valves. He wired them up and commenced his tests, only to be met with failure. Altogether, he tells me, he spent nearly three weeks on this circuit, the valves in use having been removed from a piece of equipment which was working satisfactorily. To sum-up, after fruitless endeavours, he removed the valves for some fresh wiring, and apparently replaced them in different sockets. The circuit worked ! The difficulty had been due to one of the triodes being low emission, and of such a character that it failed to work in one stage only. It was one of the high-mu triodes, and he found later that in the particular stage in which it had originally been plugged, it would not oscillate. It functioned quite well elsewhere and is, in fact, still in use as an audio amplifier, but it will not oscillate in that particular circuit. I suppose a good valve tester would have revealed the fault and prevented so many wasted hours, but I think there is a moral here, and that is, not to rely on a first test, but to either change all the parts or have them tested, especially if it is some new arrangement which has not before been used or tried out.

## Printed Clreuits

My comments, some time ago, about the printed circuit have brought many letters and 1 think it is true to say that opinion is equally divided. I had many interesting suggestions sent to me as to mending or repairing them and it would certainly appear that broken foils are a keen source of trouble. One manufacturer suggested that cracks should not be bridged over, but a new length of wire should be used for the entire run of the broken conductor. One very interesting suggestion was made by a reader to simulate the printed circuit board in ordinary wiring, and I have tried this out and certainly think that it has merits. He takes a sheet of paxolin and drills it to suit the particular layout in which he is interested. First of all he draws out the layout and wiring, arrang-
ing for all earth connections, for instance, to be in one line, and so so. The wire ends of resistors and condensers are then passed through the very small holes which he has drilled in the sheet and a wire run along the other side of the board to tie together all parts which are linked in the circuit. In this way he finally has an insulated board on which the components are on one side, and all connections on the other, and he tells me that testing is facilitated, the final construction is much neater, and the set can be practically prefabricated. I must admit that $I$ tried out the idea and cer!ainly found it had its merits.

## In the U.S.A.

Do the Americans take their radio more seriously than we do in this country? I am prompted to ask this after seeing an American magazine, sent to me by one of my friends who has left this country. With the "magazine he also sent two or three : men only" types, and some domestic (home) magazines. I am greatly struck by the large amount of space which is devoted to radio in these magazines, one having about five pages on the subject of loud-speakers. It is a most exhaustive account of the development of this "beast" in all parts of the world, and gives some details which I had not seen in print before.
The amount of space which is devoted to radio, in all of these magazines, leads me to think that they are much more radio-minded in America, and as a result this must lead to a much greater development in the art. Current market items do not, however, seem to bear this out, and there are not so many items on the American market which cannot be seen here, although they are more advanced in such things as colour television. Of course, with all the channels which are available in every part of their country, 1 suppose the man-in-the-street must be more radio minded, but I would have thought this increased public interest would have led to much greater developments.
Considering how lacking in general knowledge the majority of people are here, I think we have done a really good job in both the radio and the television fields, although I still would like to see someone come along with something new in the way of aerials. After all, the unsightly mess on the roofs of houses both here and in the U.S.A. will grow still worse as more channels are opened, and some new "receptor" covering from centimetric to long wavelengths would earn a pretty penny for the inventor and the blessings of every householder.

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# All about CATHODE 

# FOLLOWER circuits 

By E. McLoughlin

## PRINCIPLES AND USES OF THIS TYPE OF CIRCUIT

(Continued from page 808 of the Jantary issue)

7HE last example of the use of cathode followers which we discussed in the January issue was in circuits where pulses of high voltage are required, for example, in the synchronisation of timebases.

## Calculations

In all highamplitude uses, it is very simple to decide whether a certain combination of valve. Rk and H.T. voltage. is capable of handling an intended signal. Let Vn be the peak negative signal amplitude. Then the grid leak (Fig. 6, last month) is returned to a point at about plus V n to chassis. It follows that the cathode will also rise to about plus Vn (just a littlc more). By Ohm's Law, the current flowing in RK is then easily calculated. This represents the "resting " anode current of the valve, and must not exceed the rated value for the valve used. Furthermore, let $V p$ be the peak positive signal amplitude. The sum of Vp and Vn must not exceed one half of the rated H.T. voltage of the valve used. The H.T. voltage chosen should thus be double the peak-to-peak signal. or more, within the rating of the valve, and the smallest possible value for RK be chosen which neither causes the anode current rating of the valve to be exceeded. nor lies below about 50 times the reciprocal of the mutual conductance. It is desirable to make RK as small as tolerable within these limits, because the voltage fluctuation with further external loading is then as small as possible. Normal operating anode current ratings, and tot peak values. should be consuited in the above design procedures.

It should be mentioned that the signal frequency response of a normal cathode follower is virtually linear over the entire vider spectrum. including pure D.C., and goes right up to many megacycles.

## Cathode Followers as Signal Generator Output Stages

As the output stage of an Audio or R.F. Signal Generator, one often finds a cathode follower. The reason lies in most cases in the use of the property that the output voltage is largely independent of the exact value of the external load resistance connected. This enables an output calibration to be made for the signal generator which can be relied upon to hold, with tolerable accuracy, for the most varied external loads connected. We are thus mainly concerned with 1:1 voltage-transfer cathode followers here, with their typical high value of RK of about $10,000 \Omega$ to 20.000 , or more.

Power-output cathode followers are normally not in question for signal generators, at any rate for audio and broadcast R.F. signal generators. But, for extreme VHF signal generators, such as are used for the high television channels. as well as for video-waveform test-signal generators, where maintenance of accurate waveform is essential, new factors play a role, which necessitate the use of a power cathode follower in many of these cases. If any disturbance is made in a electrical circuit, then the effects of that disturbance are not felt immediately at all other parts of the circuit, but spread out with the velocity of light or less. In particular, if we have a length of coaxial cable, and switch on a signal at the input end, it is not present at once at the output end, but only after a time corresponding to a definite speed of travel of the signal down the cable. which is of the approximate order of the velocity of light. Now, this high speed means that, for reasonable lengths of cable, and audio or broadcast radio frequencies, signal transfer down the cable may be considered, for all intents and purposes, instamtaneous. But at very high frequencies, such as are met in modern television techniques, the transit time of even a


Fig. 8-H.T. voltage stabiliser.
few inches of cable is an appreciable fraction of a cycle. If impedances are not properly matched at all cable/apparatus junctions, a partial reflection giving signals travelling in the opposite direction to that intended occurs as well as loss of power. Reflections from separate ends of a cable will not be in phase, on account of the transit time. Moreover, the phase difference will depend upon the


Fig. 9 (left)-Circuit of a "safe" output stage for 'phones using a cathode follower.
Fig. 100 (right)-Simple cathode follower output stage.
frequency of the components of a complex waveform. The net result will be a complete change in the waveform. It is thus essential to match a television waveform signal generator output to the intended load, and thus one finds power cathode followers in many cases in such apparatus.

## The Pulse Power Cathode Follower

It is indeed possible to obtain very considerable power out of specially designed cathode followers. If we take a valve of high mutual conductance and having a pulse cathode capable of one amp or so peak current (although, of course, the mean current rating is much smaller), such as are found among modern line-output valves in television receiver circuitry, then short pulses of high power can be generated with such a valve connected as a cathode follower. Let us assume a typical mutual conductance of $10 \mathrm{~mA} / \mathrm{V}$, giving an output impedance, as cathode follower, of $100 \Omega$. Using


Fig. 10 b -Improved cathode follower output stage. RI is 220 k, R2 is 100 k , and the H.T.+ is 200 V .
a drive of 200 V to give an output signal of 100 V in the matched condition with a $100 \Omega$ cathode load, we just run up to the permissible 1 A peak anode current. The output power realised in the external $100 \Omega$ load is then given by $1 \mathrm{~A} \times 100 \mathrm{~V}$; i.e. 100 W . Let us assume, typically, that the maximum mean current rating of the valve is 100 mA . Then the peak 100 W condition may be operated only for one tenth of the total time. For example, one 100 W output pulse, lasting a tenth of a second, is permissible once every second. In between times the valve would be resting at its set D.C. operating point, and we can now consider where this will have to lie. At the pulse-peak, when IA anode current is flowing, the gridcathode signal will be virtually zero. Thus the grid will be at the same voltage as the cathode, i.e. 100 V positive. We are using a 200 V positive drive, and thus the D.C: resting point will have to be with the grid at 100 V negative to chassis. In other words, the valve is heavily cut off when no signal is present, and thus we see that the pulse power cathode follower is a special case of a Class-C amplifier.


Fig. II-A double triode cathode follower output stage.

## Cathode Follower Drive

The drive for such a power cathode follower naturally consumes no appreciable power, it is a pure voltage drive. Nevertheless, just in case gridcurrent fows at the pulse-peaks, the drive can be from a smaller cathode follower, this time in 1:1 transfer circuit with the usual high Rk. Fig. 7 shows a typical complete circuit. The chief use of such a circuit is for firing grid-controlled hydrogen thyratrons in large radar installations, Which consume considerable power at the grid. It is also known to the author that such a system has been used to modulate the output stage of a transmitter. The power output cathode follower supplies the entire H.T. power for the P.A., simply by making the P.A. itself take the place of the cathode load. Such modulation circuits, also known as series-modulation, are used in several pulsed radar transmitters.

Finally in this group, it should be pointed out that the usual H.T.-stabiliser circuits using a seriesregulator valve (such as in several designs recently published in this magazine) are virtually a special form of D.C. power cathode follower. Redrawing
the circuit of such a stabilised power supply in the form of Fig. 8 immediately brings out this point.

## Continuous Power (Class A) Cathode Followers

These are the true members of the "power" class of cathode follower, in that they can supply output power, say at audio frequency, in much the same way as a conventional output stage delivering power from the anode circuit.

## High Impedance Loudspeakers

Those experimenters still possessing large moving-iron loudspeakers of formers days in their junk boxes, having coil impedances of some few hundred ohms, may like to try one direct as cathode load, without transformer, in such a cathode follower output stage. Any small R.F. pentode can be used, strapped as triode. In many cases the constructor will very likely be astonished at the results. Apart from good volume, the tone is generally much better than with the same speaker used in an anode circuit, as the extremely low internal impedance of the cathode follower damps the unpleasant resonances of this type of loudspeaker to a high degree. It is even worthwhile. just for this last reason, trying a conventional output valve such as the 6 V 6 or the EL.84 as a cathode follower. In such a case, however, it is necessary to pay special attention to the correct D.C. operating point, so that the valve does not run at low or excessive anode current. The D.C. resistance of the transformer winding or speaker coil in the cathode circuit must equal the normal cathode bias resistor of the valve used. If it is less than this, then an appropriate series resistor
Fig. 12 (left)-A White cathade follower.
Fig. 13 (right)-The transistor equivalent of the White cathode follower (or all resistors increased by the same factor).

It is little known by experimenters that sometimes considerable advantages are to be gained by using an output stage feeding a loudspeaker or headphones in the form of a cathode follower. The first and obvious advantage is that the problem of isolation of the phones from the H.T. voltage is automatically absent (Fig. 9).
The second great advantage is apparent in circuits requiring a small monitor-speaker, but where for reasons of power economy or heat dissipation limits, a conventional outpot valve is undesirable. In such cases. constructors have often used simple. A.F. triodes or R.F. pentodes. frequently with relatively poor results because of the very high anode matching impedances generally required in such circuits, which cannot always be realised with normal loudspeaker transformers. Much improved results are often possible using the same valves as cathode followers, with the normal loudspeaker transformer primary forming Rk: In many cases the D.C. resistance of the transformer primary is sufficient to set a proper D.C. operating point of the stage wishout further attention to the matter. Fig. 10a shows a typical circuit example which the author has had in operation for a long time. A tiny 6AK5 R.F. pentode strapped as triode cathode follower delivers over 50 mW into a small moving coil loudspeaker. The circuit is a small addition to an oscilloscope, to monitor the Y-signal audibly. There was not room. nor spare H.T. power. no- heat dissipation facility. for operating a conventional audio output stage. But this tiny cathode follower sutput stage draws only some 5 or 6 mA H.T. current.

Naturally, the voltage drive required by a cathode follower output stage is high, being about 10 to 100 V in most cases. Thus, the audio amplifier preceding the stage will have to have higher gain than is otherwise normal. An extra triode stage can often provide this gain. It is often convenient to use one triode of a double triode to give this extra gain, and the other as the cathode forlower. In this way, a valve such as the ECC81 can replace a conventional output valve (see Fig. 11). the rest of the audio amplifier being unchanged. In the case of the author's 6AK5 output cathode follower of Fig. 10a the necessary drive was present anyway, as the Y-deflection of the tube in the oscilloscope requires a similar drive, so that sufficient voltage to drive the cathode follower was present at the Y -amplifier output.

## The White Cathode Follower

Fig. 12 shows a further development of the cathode follower principle, to give even lower internal impedance. It is possible to achieve an impedance of a few ohms with this circuit. so that in principle, a moving coil speaker would match direct without transformer into it. This is true in in practice, too, but the power output is then poor in comparison with the H.T. consumption and size of the valves. This is simply because of the restriction that the valves may not be permitted to run un to the necessary anode current. Thus using a PL 36 triode-strapped in each position. only 50 mW is possible into a $15 \Omega$ moving-coil speaker.
(To be continued)
(Continued from page 833 of the January issue)

# A PRACTICAL <br> PRE-SELECTOR 

By A. Sydenham

$\ell$N the previous article, the circuit was described and it now remains to assemble the conplete unit and build a cabinet for it. It may then be tested.

A diagram that shows practicall:: all the chassis drilling is given in Fig. 4, the coil mounting apertures being those required for the coils specified. Should the tuning capacitor contact the coil bases when in position, washers should be fitted to provide clearance. Alternatively, the coils may be fitted to a rectangular piece of paxolin held by spacers. Most of the wiring can be made so short that small items are easily


Underchassis view of the pre-selector.


Fig. 4-The chassis drilling diagrom.
suspended in the leads and the orientation of the coils and valveholders assists in this respect. Electrolytic condensers C9/C10 and C11 are held against the chassis by clips.

## Assembly

The front panel is secured to the chassis by means of the nuts securing VR1 and S1/S2 and reference to Fig. 5 will show the locations of the various apertures. The tuning condenser spindle also projects through the front panel and a coloured warning lens is fitted to the lower central aperture. It will be found when the panel is firmly bolted in position that the assembly slopes backwards slightly and this not only brings the controls to a more convenient operating height but also improves the general appearance. Mitred sections of quadrant glued firmly to the panel edges further assist in this respect.

## Wiring

Use of a soldering iron with a pencil bit is essential and modern miniature resistors and condensers are needed to avoid congestion of subchassis components. The use of differently coloured sleeving will also assist final checking considerably.

## The Cabinet

The simple design is shown in the semi-exploded diagram of Fig. 5 and may easily be made from tin. plywood held together with reinforcement strips, pins and glue. Strips of veneer 'obtainable from some model supplies shops) may be glued using Bostik No. 1 adhesive to the edges where joins appear if desired, and the finish may be chosen to suit one's personal taste. The prototype is lacquered in ivory. The slots cut in the sides serve as carrying


should then be plugged into the appropriate sockets on each piece of apparatus. Control VR1 on the pre-selector should now be set to "off" and the wave-change switch turned to position 4. The main receiver should then be switched on and adjusted to receive a transmission in a band also available to the pre-selector. The receiver should now act normally, since the aerial is effectively connected to it direct. The pre-selector may then be switched on and allowed to warm up when its wavechange switch may be rotated to select the appropriate band in use. The received signal should now improve in strength considerably and, as the tuning control of the pre-selector is adjusted, it may be found necessary to back off the sensitivity control, VR1, to avoid overloading. A little
ventilation as cool air is convected from the rear. Four small rubber feet may also be fitted.

## Using the Pre-selector

When the unit has been completed and checked the aerial and earth leads should be removed from the receiver with which it is to be used and plugged instead into the sockets provided for them on the pre-selector.

A length of coaxial cable should then be prepared, aerial and earth plugs being fitted at one end (the braiding being connected to the earth plug) and a coaxial plug at the other. This lead
practice will soon reveal the best method of use but it should be remembered that too strong a signal fed to the receiver may bring the AVC circuit into action too strongly. Once the user has familiarised himself with operation of the unit it may be calibrated.

When it is desired to use the main receivel on its own it mercly becomes necessary to turr the wavechange switch, S1/S2, to position 4 anc rotate VR1. to "off" when the indicator lens wil become dark. By then, however, the advantage: - of R.F. gain will have been made apparent.

THIS UNIT WAS ORIGINALLY DESIGNED FOR USE WITH A SIMPLE GEIGER HEAD, BUT IT WILL OPERATE SATISFACTORILY FROM ANY SUITABLE INPUT SOURCE

By A. Cole









February, 1962
internal construction of the digital counter unit.


there may suddenly be many close together and then for a long time absolutely none, yet it is virtually impossible for a whole minute to pass without any counts at all.

## Principle of the Digital Counter Circuits (see Fig. 1)

This is a four-valve triggered pulse-amplifier circuit. $\mathrm{V}_{1}$ is the input amplifier, comprising two stages:-V1A is an earthed-grid input stage, meeting the three requirements (a) freedom of feedback, (b) keeping the same signal polarity (positive), and (c) good gain, so that the stage is over-driven, giving very steep output pulses to VIB, which is a cathodefollower decoupling V2 from V1A as far as feedback is concerned. VIB also returns the signal to
lów impedance, and now delivers a good steep pulse of at least 100 V amplitude. The tiny value of C 3 , the coupling condenser to V 2 , differentiates this pulse, so that only a very brief but very steep spike of about 100 V is applied to the grid of V2A.
Valve V2 is a monostable multivibrator, the purpose of which is to provide a good squarewave pulse of "current, starting exactly at each 100 V "trigger" spikc from Vi, and lasting about one twentieth of a second, which is the optimum switching-time for the counter relay. V2A is normally cut off, because its grid is on a bleeder chain from the low voltage at the anode of the normally conducting section V2B down to a variable negative bias from VR1. The other section, V2B, is, as just stated, normally conducting


Fig. 1-The circuit of the digital counter. (All resistors are IW rating except where stated.)
heavily because its grid leak is returned to H.T. positive. This condition is perfectly stable for any length of time until the circuit is suitably disturbed. This disturbance is the short positive 100 V spike applied to V2A grid. This lifts it to cut-on and above, which causes an equivalent voltage drop at the anode, which is fed via C 4 to the grid of V 2 B , thus tending to cut off V2B. This causes the anode potential of V2B to rise, which is fed as a further rise to V2A grid on the bleeder. The net result is that the formerly cut-off V2A has suddenly been tuned hard on, and the formerly conducting V2B has been cut off.

Maintenance of this new condition depends upon maintenance of the signal at V2B grid, which remains only as long as C 4 is charging via R10. As soon as C4 has charged sufficiently, which takes about one twentieth of a second, V2B cuts on again, and reverses the procedure back to the previous stable state with V2A cut off and V2B conducting, until the next trigger spike arrives. The net result is thus a positive-square-wave pulse of about 100 V amplitude and about one twentieth of a second duration at V2B anode.

V4 is a class-C amplifier, i.e. the bias-point is beyond cut-off, applied via R12 and R13 from VR1. In the normal, stable, resting state of V2, with V2B anode at a low voltage because of the heavy conduction of $V 2 B$, the voltage difference between V2B anode and V4 grid is not sufficient to strike the neon tube V3; thus V4 is fully disconnected from V2 and resting, cut-off. But during the temporary
change-over position of V 2 , when V 2 B is cut off and thus the anode voltage high, the neon V3 is struck, driving V4 grid heavily positive. The surge of anode current in V4 moves the digital relay RLY1 one unit on. As soon as V2 reverts to the stable condition, V2B anode potential falls again and the neon V3 extinguishes. V4 grid returns at once to beyond cut-off, and anode current ceases instantaneously. This sudden stoppage of anode current could cause high inductive voltage peaks across the coil of RLY1, if C8 were not there. Thus it is essential not to omit C8, as otherwise the relay could be damaged by flashover in the coil. On the other hand, do not make


Fig. 2-The circuit of the Geiger head.

## COMPONENTS LIST

| Reslstors (All $\pm 20 \%$ Carbon): |  |  |  |
| :---: | :---: | :---: | :---: |
| RI | 3.3k IW | RIO | IM IW |
| R2 | 150k 2W | RII | 3.9 k 10 W |
| R3 | 22k 2 W | RI2 | 150k IW |
| R4 | 270k IW | RI3 | 150k IW |
| R5 | 150k IW | R/4 | 10M 2W |
| R6 | 10k IW | R15 | 56k 2W |
| R7 | 220k IW | R16 | 100k 2W |
| R8 | 150k 2W | R17 | IM IW |
| R9 | 150k 2W | R18 | 10k 2 W |
| VRI | 500k Pot. | .w.) | 10k 2 |

## Valves:

V1 ECC85
V2 ECC81
V3 90Cl (neon)
V4 EL84
V5 MX146 Geiger Tube (Mullard)
V6 EC92
DI Metal rectifier 350V A.C./25mA D.C.
Sundries:
Three B9A valveholders, ceramic
Two B7G valveholders, ceramic
Two coaxial plugs and connecting lead
One digital relay, GPO, approximately 2000 Q/25mA (Service Trading Co., 47-49 High Street, Kingston-on-Thames, Surrey.)
Two toggle switches on/off, single pole
One panel fuse, complete
Chassis material, wire, solder, tagstrips, bolts, sleeving, etc.
Test tubes, rubber cork.
Power supply (preferably stablised) 200.300V/ 100mA 6.3V I.3A A.C. (heaters)
Bias supply: about ( -100 )V on above power unit, or otherwise a small goV H.T. bottery Mains lead and plug

C8 appreciably larger than specified, as this would then destroy the stecpness of the current rise at the start of each pulse, possibly leading to erratic counting. It is of interest to discuss why a neon, V3, is used to couple V2 to V4 instead of the usual coupling condenser. The reason is simple. The signal from V2 is of such a high amplitude that V4 is driven from beyond cut-off right up to heavy grid current by it, and such grid current would charge any coupling condenser heavily and very rapidly during the pulse. After termination of the pulse, this would leave V4 at a correspondingly greater negative voltage at the grid than the intended operating point. This would have the result that the circuit would be more or less blocked at V4 for any pulse coming in subsequently before the coupling condenser had discharged, and would also block the circuit at V2A grid, because the excess negative voltage at V 4 grid would react via VRI and R5 to pull down V2A grid too. The neon thus prevents the amplifier blocking when working at counting-rates approaching the limit of resolution. The alternative method of preventing gridcurrent blocking of amplifiers handing large signal amplitudes, namely the insertion of gridstoppers, is not usable here, because it causes signal loss due to voltage drop across the stoppers, and thus makes the anode current rise in V4 too slow for stable counting.
It should be mentioned in passing, that the use of neons as coupling elements in amplifiers receives far too little attention by experimenters. They have

Retarning to the digital counter circuit. A supply of about minus 100 V is required on the bias line input (the exact value is not critical, but should be stabilised preferably-if the constructor has no power unit supplying this output in addition to normal H.T. and heaters, then a small 90 V H.T. battery will serve the purpose excellently. This battery may be very small, as the current drain is only about a fifth of a milliamp (but do not forget to switch this battery off after use). The actual value of optimum bias taken to V2A and V4 is quite critical, and also dependent on the H.T. voltage used. The circuit operates excellently with any H.T. voltage between 200 and 300 , but requires a different bias value with each H.T. voltage. Consequently the potentiometer VR1 has been incorporated, to set the bias to the optimum value. This potentiometer should be used more or less as a reaction control is used on a simple radio. Bias should first of all be increased until counting stops altogether even when the Geiger-head is supplying pulses at the input, and should then be reduced sufficiently to be quite certain of counting all pulses received. It is too difficult to make this adjustment with the mere 20 pulses per minute of the normal atmosphere, and thus it is advisable to place an alarm clock with luminous figures, or a pocket-watch with substantial luminous figures, ncar the Geiger tube. The radioactive content of any such luminous paint is sufficient to raise the counting rate of only 20 per minute right up to possibly several hundred per minute, which is


Fig. 3a-The underchassis wiring of the counter unit.
a number of advantages over condensers. In a normal class-A audio frequency amplifier, the coupling neons would be permanently struck, and thus represent D.C. coupling and theoretically freedom of all gain variation with frequency. Such an amplifier would amplify. D.C., could have many stages, yet use otherwise conventional A.C.-amplifier circuitry with a single common H.T. supply on which all stages run in parallel as usual. And, as seen above, neon-coupling is free from blocking on transients. Of course, the value of cathode resistors, etc. would have to be modified in such an amplifier. But the principle is clear, and might interest more experienced constructors.
sufficient to make bias adjustments conveniently. At the slower counting rates, the bias setting is not in the least critical. If too high, counting stops altogether and if too low, then V4 runs at heavy anode current which will soon destroy it. Between these two points lies at least one third of the travel cf VR1, and slow counting is equally good at any point within this range. But if fast counting is desircd, e.g. when checking the radioactivity of luminous paints, or possibly X-rays from poor or defective television cathode-ray tubes, it will be found that if the bias is set too far below the critical value, many counts will be missed.
(To be continued)

# Faults in Transistor 

7RANSISTOR superhets usually have two intermediate frequency stages, and faults in these may cause lack of sensitivity, or oscillation and other troubles. The I.F. amplifier should be able to provide a very high gain, and if it does not do this, good reception of distant or weak stations will be impossible.

## Alignment

Correct alignment of the I.F. transformers is easily achieved. If a signal generator is available, this may be set to the correct intermediate frequency (often $470 \mathrm{kc} / \mathrm{s}$ ) and coupled to the I.F. amplifier at a convenient point. If the circuits are out of tune, a fairly strong input may be needed, or it may be necessary to take the generator output directly to one of the transformers, a small isolating condenser being included in circuit. However, if the alignment is approximately correct, a very small signal will suffice. Merely placing the end of the generator prod or output lead a few inches from the mixer collector circuit should then give enough coupling.

When receivers have the popular type of push-pull output stage, battery current depends directly on the volume of the audio signal. If the generator is delivering a modulated output. a 15 mA or similar meter in one battery lead is thus a convenient means of checking for maximum output.

When a good output is being obtained, when the I.F. stages are aligned approximately, the input from the signal generator should be reduced. Accurate adjustment is then easily achieved.

An insulated tool (made from an ebonite rod, for example), is used to adjust the I.F. transformer cores. They are simply screwed in or out, as needed, to obtain best results. Each core should have a fairly sharp tuning point.

If no generator is available, a local station should be tuned in, and the cores adjusted for best results. A weak station should then be found, with the audio volume control at maximum, and final adjustments should be made.

If all cores are in a reasonable position, it should generally be possible to align the aerial and oscil-


Fig. I-A typical transistorised I.F. amplifier circuit.


Fig. 2-An I.F. amplifier in which the transistors are used in the common base mode.
lator stages satisfactorily, even if the I.F. does not fall exactly at $470 \mathrm{kc} / \mathrm{s}$, or the correct frequency; if the frequency is much in error, correct ganging of aerial and oscillator circuits may be impossible.

When the I.F. transformers are adjusted without the aid of a signal generator, check that no core is fully in, or too far out. If one of the cores is not in the correct position. all of the cores should be readjusted by an approximately similar amount, and the stages are then realigned for best results at the new frequency.

February, 1962
PRACTICAL WIRELESS

# I.F. Stages 

## Neutralisation

Neutralisation is generally required, to maintain stability. In Fig. 1, the $1 \cdot 2 \mathrm{k}$ resistor with 56 pF condenser, and the 3.9 k resistor with 18 pF condenser form the neutralising circuits.
The values required can only be varied by a very small amount. if sufficiently accurate neutralisation is to be achieved. The values also depend on the transistors, and are a function of the transformer ratio. This means that with a given circuit, neutralisation can only be ensured if the transistors, I.F. transformers, and values in the neurralising circuits are as specified.


Fig. 3-An alternative neutralisotion circuit.
As accurate values are so necessary, components of $2 \%$ tolerance may be specified. Indiwidual $5 \%$ or wider tolerance components could be suitable, but other samples might be too far from the correct value. so that neutralising is incomplete. The overall feedback is small, and can easily be modified by stray capacity in wiring. especially if leads are long, or base and collector wires are close together.

If the receiver breaks into oscillation when the I.F. transformers are being adjusted for maximum sensitivity, this indicates instability in this section. This oscillation may appear as a continuous whistle or heavy background hiss, or it may only arise when tuning through a weak station. If the instability ceases on tuning in a powerful signal, so that AVC reduces gain, or if it ceases with one or more I.F. transformers only very slightly de-tuned, its cause is probably not serious.

## Common Base Circuit

A typical I.F: amplifier of this type is shown in Fig. 2.2 The gain can be expected to be less than with the common emitter type. This circuit is given because it will be found in some receivers. Each base is supplied through a potential divider, and is earthed to intermediate frequencies by the condeners wired from the base to the positive line.

The emitters are connected directly to the transformer secondaries, these components being designed for this type of circuit.

## Decoupling

In Fig. 1, each emitter resistor is by-passed with a $0.25 \mu \mathrm{~F}$ condenser. In midget sets, lower values, such as $0.1 \mu \mathrm{~F}$ or $0.04 \mu \mathrm{~F}$, may be encountered. These lower values usually give an increased possibilty of instability, which may show as oscillation, motor-boating, or whistles on weak signals only. In such cases, it may be worth increasing the by-pass values. This can easily be done by temporarily wiring a larger capacity condenser in parallel with the existing condenser. If this cures the trouble, the larger value may be permanently incorporated.

In Fig. 1, the first I.F. transformer secondary is decoupled by the $10 \mu \mathrm{~F}$ condenser. A large value is required here, as audio frequencies will be present in the automatic volume control line from the diode. Such condensers may deteriorate, and need replacing when they no longer offer a lowimpedance path for intermediate frequencies. If so, a $0.1 \mu \mathrm{~F}$ or similar condenser may be shunted in parallel.

In the second stage, a $0.1 \mu \mathrm{~F}$ condenser is used, in parallel with the 4.7 k resistor. Midget receivers may use $0.04 \mu \mathrm{~F}$ here, but $0.1 \mu \mathrm{~F}$ or $0.25 \mu \mathrm{~F}$ can often be more suitable. If the l.F. stages are unstable. the capacity can be temporarily increased, to see if results improve, as already mentioned.

## Modified Neutrallsing and By-passing

In some circuits, neutralisation is obtained by using a small capacity, Cl in Fig. 3, from transformer to base. The value will depend on the transistor, but may be in the region of 5 pF . Such small capacities are sometimes obtained by means of twin insulated wires, or a twin-lead wire, reduced in length until the required value is reached.

When the neutralising condenser is in this position in the circuit, its value is not influenced much by the transformer ratio, but will depend on the transistor, and position of the I.F. transformer primary tap.

In some circuits, by-pass condensers are not taken to the earth line afforded by the battery positive circuit. Instead, the by-pass condensers for any


Fig. 4-An example of a circuit in which the by-pass condensers are taken to the emitter of the transistor insteod of to the positive line.
stage are taken to the emitter of the transistor, as in Fig. 4. This can be a little confusing, if not expected, but otherwise the circuit is practically the same as that in Fig. 1.

## Diode Detector

Receivers of this type use a diode, as detector, and to provide AVC. If this diode has a low efficiency, good results will never be achieved. If no means of testing the diode are to hand, and it is suspected, it should be replaced by a new one such as the OA81 or GEX58.


Fig. 5-The typical circuit arrangement for a damping diode.
The diode must be wired in the right way round, as shown. When signal strength increases, an increased positive voltage is developed at the positive end of the diode (Fig. 1). This is transferred to the first I.F. stage, through the 8.2 k resistor, and makes the base voltage more positive, reducing amplification. This provides some measure of AVC (Automatic Volume Control) action, but the effect is much less than with most valve receivers.
If the set is stable on loud signals, but unstable on weak signals, this probably arises from the AVC action, as already explained. That is, the instability is not severe, so that the reduced gain on a strong signal temporarily clears the fault.
Some receivers employ a damping diode, in addition to the AVC diode. One method of connecting this is shown in Fig. 5. The collector current through the $470 \Omega$ resistor results in the positive end of the damping diode being slightly positive, and the diode has little effect on the mixer I.F. transformer, but, when signal peaks exceed the damping diode potential, the diode conducts. loading the transformer and reducing gain. This gives increased AVC efficiency, and in particular avoids overloading on very strong signals.

## Reflexed Amplifier

A circuit similar to that in Fig. 6 is used in some receivers. Here, one transistor acts as both I.F. and A.F. amplifier. This gives improved results, from a given number of transistors, but is somewhat less effective than the use of separate
transistors.

In this circuit, the first I.F. transformer secondary is by-passed to the emitter (see Fig. 4) by the $0.01 \mu \mathrm{~F}$ condenser. Instability at intermediate frequencies may arise from this condenser being defective or disconnected. The primary of the second transformer is similarly decoupled to the emitter. The values used $(0.01 \mu \mathrm{~F})$ are rather small, but cannot very well be much increased, because they are in parallel with the audio signal, and thus reduce top response.
After detection in the normal way, by the diode, the signal passes from the 5 k volume, control slider, through the $6 \mu \mathrm{~F}$ condenser and 3.9 k resistor, and the secondary of the I.F. transformer, which has negligible impedance at audio frequency. The transistor then acts as an A.F. amplifier, and the A.F. signal is developed across the $1 \cdot 2 \mathrm{k}$ resistor.

A large emitter by-pass capacity $(50 \mu \mathrm{~F})$ is required, as this stage is acting as an amplifier at audio frequencies, as well as intermediate frequencies.

Oscillation at audio frequency is not very likely. The stage can be tested at A.F., if necessary. by temporarily disconnecting the diode, and feeding in an A.F. signal from an outside source.


Fig. 6-A reflexed circuit-here, one transistor is used to amplify both I.F. signals and A.F. signals.

After any of the points described have received attention, it should be possible to adjust the I.F. transformer cores for best results.
If it is necessary to connect the generator directly to the receiver, this may be carried out by taking a $0.01 \mu \mathrm{~F}$ or similar isolating condenser to the base of the first transistor (the mixer). If the generator signal is taken to a transformer or collector circuit, the core will probably need slight readjustment after the generator lead is removed.

The transistors used in such stages should have a cut-off frequency of $5 \mathrm{Mc} / \mathrm{s}$ or higher, so reliable transistors. designed for such purposes, should be employed. General lack of sensitivity may arise from poor transistors in these stages.

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THE operating frequency of tunnel diodes has been raised by a technique of miniature ceramic encapsulation developed by Standard
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A single version, known as the JK30A, is now in production. It is being followed by a new version incorporating a matched pair of tunnel diodes and forming a single integral unit having three tabs. These units are matched for peak current and capacitance and are intended for applications in the computer field. They may be used in high speed logic and counting circuits or as the thresh-hold amplifier/gate at the input of a puise amplifier. Standard Telephones and Cables Limited, Connaught House, Aldwych, London, W.C.2.

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# Short-wave Listeners' Log 

$\mathcal{J}$HE choice of a suitable receiver is not always easy, as prices and specifications vary so much. With home-built receivers, improvements and additions can, of course, be made. There are also a number of current communications receivers available. and full details of these can be cobtained from the makers. The price is generally quite high.

When a ready-made receiver of high efficiency, at relatively low cost, is required, a second-hand, used, or surplus model is probably the only choice. Brief details of some of the most popular and suitable receivers of this kind are given here.

R1155. About $16 \frac{1}{2} \mathrm{in}$. $\times 9 \mathrm{in} . \times 9 \mathrm{in}$. Seven valves, plus two in unused direction-finding circuit, and magic eye tuning indicator. BFO (beat frequency oscillator for C.W. morse) Needs separate power pack and output stage for speaker. Many cover $17-4000 \mathrm{~m}$, with gap between 100 and 200 m , but other coverages available. Frequency calibrated dial.

R1224A. About $19 \mathrm{in} . \times 14 \frac{1}{2}$. $\times 9 \frac{1}{2} \mathrm{in}$. Battery 5-valver: R.F./F.C./I.F./DET/output, tuning $30-300 \mathrm{~m}$ in 3 bands. Charts for numbered dial.

CR100 and B28. About 16 in . $\times 16 \frac{1}{2}$ in. $\times$ $12 \frac{1}{6}$ in. Ten to $5,000 \mathrm{~m}$ in 6 switched ranges. Frequency calibrated and logging suale. Eleven octal valves. Internal power pack. Controls: Tuning, band-change, pass-band ( $6,000-100 \mathrm{c} / \mathrm{s}$ ) crystal filter, aerial trimmer, H.F. gain, A.F. gain, BFO, function switch, on/off switch, and noise limiter on some models.

CR150. About $16 \frac{1}{2} \mathrm{in} . \times 17 \mathrm{in} . \times 13 \frac{1}{2} \mathrm{in}$. Double superhet model. $5-150 \mathrm{~m}$ in 5 switched bands. Noice limiter, crystal calibrator, S-meter. Small triode output stage. Separate power unit.

AR88D. About $19 \frac{1}{4}$ in. $\times 19 \frac{1}{2}$ in. $\times 11 \mathrm{in}$. About $9 \cdot 5$ to 550 m in 6 switched hands. Twelve valves, plus rectifier and voltage regulator, ful! communications facilities. Internal power supply. Companion models with different coverage.

HRO. About $17 \mathrm{in} . \times 11 \frac{1}{2} \mathrm{in} . \times 8 \frac{1}{2}$ in. Nine general coverage plug-in coil units over 10 to $6,000 \mathrm{~m}$. In some cases special coil units giving bandspread tuning over amateur bands are available. Numbered dial tuning. Ten UX type valves, but octal valves in later models. Separate power pack. BFO, S-meter and full communications facilities. Some models have fewer coils.

Collins T.C.S. About 13in. $\times 11 \mathrm{in} . \times 11 \mathrm{in}$. For use with companion transmitter, 25 to 200 m . Octal valves. May be run from separate rotary generator.

BC312. About $18 \mathrm{in} . \times 10 \frac{3}{3} \mathrm{in}$. $\times 9 \frac{1}{4} \mathrm{in}$. Nine valves, covering 17 to 200 m . BFO and other facilities. Intended for 12 V accumulator supply.

Any of these receivers will provide very good results. The band coverage available may be
important, as some receivers have a more limited short wave coverage than others. Those sets which include normal long and medium wave bands will provide very good long-distance reception, on these bands, in addition to covering S.W. bands. Receivers which require a separate power unit, or are intended for accumulator or battery running, are not suitable when a single, self-contained set, for A.C. mains operation, is required. In all cases a separate, moving-coil permanent magnet speaker is necessary.

Actual models naturally vary somewhat in age, condition, and exact details, but it is nearly always possible to obtain a reasonably complete specification in advance.
A brief description of features which will be found in detailed specifications should be helpful. Those generally present are as follows:

## Pass-band Selector

A control giving variable selectivity, typically from 100 to $6,000 \mathrm{c} / \mathrm{s}$, in a high-grade set. The very high degrees of selectivity can only be used for C.W. (morse) reception, as a rule.

## Function or Operation Switch

A control bringing the AVC in or out, possibly bringing the BFO in, for C.W. reception, and leaving the receiver standing by with heaters on but H.T. off.

## H.F. or R.F. Gain

Control of the R.F. stage or stages, and possibly the I.F. stages.

## A.F. Gain

The usual type of audio volume control.

## BFO Pitch

Control adjusting the pitch of the beat frequency oscillator, to give best results through interference when receiving C.W. (morse).

## Crystal Filter or Phasing Control

This allows adjustment of a crystal filter, giving high selectivity, and allowing an interfering C.W. signal to be rejected or reduced.

## Aerial Trimmer

A control, frequently panel operated, allowing the first circuit to be trinumed manually, to compensate for stray aerial capacity.


Fig. 24-The layout of the front ponel of the radiogram.

## Wiring the three sections of the

## citizen

## together, to form the complete radio or radiogram

(Continued from page 817 of the January issue)

$\cdots$AST month, the construction of a cabinet for the 'Citizen' was described; it now remains to describe the mounting and inter-wiring necessary when the units are incorporated in the cabinet. The cabinet described last month was designed to provide a modern housing for the 'Citizen' and a battery record player to make a complete battery-operated radiogram. However, for those readers who require only a battery operated radio set, the wiring needed to connect the "MiniAmp' to the two units of the 'Citizen' will also be described.

## Wiring for the radiogram

Before this can be carried out, the 'Citizen' must be tested and aligned as described in the December issue (on pages 718 and 719). It is very important that the units should work correctly before starting to mount them in the cabinet.
The control panel of the radiogram is shown in Fig. 24. From this it can be seen that six control knobs are provided. There are: a 'gram volume and
"gram motor on/off switch (this switch ensures that the 'gram motor cannot be left running when the radio is in use); a wavechange switch; a tuning condenser; a three-position switch for radio/gram change-over and (in the third position) radio off switch, and a radio volume control.
(Continued on page 941)


Fig. 25-The theoretical diagram of the connections needed for wiring the units as a radiogram.

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(Contimued from page 938)


Fig. 26 -The radiogram wiring.


Fig. 27-The interwiring for the tree sections as a radio.
as good as they were before mounting the units in the cabinet and the alignment procedure may be gone through again now that the units are occupying their final positions. The alignment was described in detail in the December issue on pages 719 and 720 -it starts at the side-heading 'The Alignment'.

## The 'Citizen' without the gram unit

The interconnection for using the 'Citizen' with the 'MiniAmp' to form a superhet radio set are shown in Fig. 27. The three group boards are shown viewed from the tag sides and not from the riveted sides. As in the radiogram, it is necessary to replace R10 on the 'Citizen' with a variable resistor - see Fig. 28. Since the 'Citizen' gives a high-level output, certain components can be removed from the 'Mini-Amp' and these are listed in Fig. 27. (They are R1, $\mathrm{R} 2, \mathrm{R} 3, \mathrm{R} 4, \mathrm{R} 5, \mathrm{C} 2$ and Tr 1 .) As in the radiogram, the connection between the two group boards on the "Citizen" which carries the I.F. signals is made of coaxial cable to reduce the capacity which the interconnection places across the I.F. output coil. When the three units have been mounted in the cabinet (which may be of any form) the alignment should be carried out again.

## SHORT-WAVE SECTION <br> (Continued from page 923)

## Conclusion

Although the unit described is an efficient one it is open to improvements. It would not be difficult, for example, to tune the grid circuit of V1 to improve sensitivity and the spare section of C6 could be employed in this connection, aerial coils being mounted in front of V1 for this purpose above chassis.

## VI Substitute

A valve of different type may be used for VI if desired provided it has variable- $\mu$ characteristics and that attention is paid to the basing which might well be different. A metal rectifier may also be used in place of V3 if preferred and in some cases it might be possible to link the receiver AVC line to the pre-selector.
NOT'E—The isolating transformer, T1, should not be omitted or exchanged for a heater transformer, neither should the preselector be used in conjunction with a receiver of the A.C./D.C. class or danger to life might result.


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# The <br> CONDENSER 

This article is expressly written for a particular type of amateur constructor: the beginner who, though perhaps familiar with condensers and their use in practice, may not yet know what a condenser

By
S. R. Vella actually is, how it functions as it does and why.

$\mathcal{B}$
EFORE explaining what constitutes a sondenser, we have to distinguish between a conductor and an insulator. A conductor allows electricity to pass through it, while an insulator does not. For example, copper, silver and most metals are conductors; while air, mica, glass, paxolin are insulators. A conductor allows electricity to pass through it by virtue of its free electrons (the electrons in its atoms' outer shells).

## The Dlelectric

When two conductors are separated by an insulator, we have what is called a capacitor or condenser-a device capable of storing electricity. The insulator separating the two conductors, which might be a vacuum, air, glass ete., is called the dielectric. For the purpose of discussion, let us imagine the two conductors constituting our condenser in the form of two separated metal plates to which are connected suitable lengths of flexible wire so that we can connect them in a circuit as will be explained later on. This arrangement (Fig. 1) constitutes the simplest form of condenser.

It should be noted that the capacity of the condenser (i.e.. the ability to store electricity) in Fig. 1 is very small, the condenser being made up simply of two relatively small metal plates with air as the dielectric.

The capacity of a condenser depends on:
(1) the area of the plates.
(2) the distance between the plates.
(3) the material of the dielectric.

The capacity of a condenser increases as the area of the plates is increased and the distance between them is diminished. In practice, the dielectric is


Fig. I (left)-The simplest form of condenser, or capacitor.
Fig. 2 (right)-The theoretical circuit symbol for a condenser.
very rarely air. It is usually either mica or paper. Fig. 2 shows the theoretical representation of a condenser.

## Storage of Electricity

We have stated above that a condenser is a device capable of storing electricity. But how exactly is this effected we ask? Why and where is electricity stored in the condenser?

Let us try to visualise what happens when we connect our condenser to a battery. This is shown in Fig. 3. Free electrons from plate 1 will be attracted to the positive side of the battery, thus leaving plate 1 with a deficiency of electrons i.e. positively charged. The electrons attracted from plate 1 of the capacitor to the positive side of the battery will appear (after flowing through the battery) on the negative side. This surplus of electrons or negative charge will therefore also


Fig. 3 (left)-When a condenser is connected to a battery, it becomes charged, as shown.
Fig. 4 (centre)-The charged condenser-the electric
field between the two plates is represented by the lines from one plate to the other.
Fig. 5 (right)-Even if the battery is removed from the circuit, the condenser remains charged.
appear on plate 2 of the condenser since this is directly connected to the negative side of the battery. We may now say that the condenser is charged; and the situation is represented in Fig. 4. In otiner words, we may say that what actually happened during the charging process is a flow of electrons from plate 1 to plate 2 as indicated by the arrowed path in Fig. 3. The electrons on plate 2 try to move further on and reach plate 1 but they are impeded by the dielectric which is a nonconductor (insulator). This tendency of the electrons to reach plate 1 from plate 2 across the dielectric exerts a kind of pressure, force or strain on the dielectric. We call this the dielectric strain. When a condenser is charged, an electric field is
set up between the two plates. This electric field is represented in Fig. 4 by a number of hypothetical lines from one plate to the other. These lines are as imaginary and hypothetical as the lines of force representing the magnetic field around a magnet.

It is interesting to ask what would happen if the battery were removed from the circuit after the condenser is fully charged. This is shown in Fig. 5. The negative charge on plate 2 can in no way reach plate 1. It is prevented from doing so by the dielectric in one direction and by the fact that the circuit is open (between A and B) in the other. Therefore plate 1 retains its positive charge and plate 2 its negative charge. The resulting accumulated energy from the charging process is stored in the electric field. This potential energy is ready to be released as soon as a conducting path between A and B is provided.

## The Charging Cycre

Fig. 6 reproduces the charging cycle. Essentially, the circuit is the same as that of Fig. 3. The only additions are a switch and a sufficiently sensitive centre-zero current measuring device. Current flow is here assumed to be identical with flow of electrons. Hence the direction of flow is from the negative to the positive terminal of the battery.

## A. Capacitor Uncharged

This is the initial stage of the cycle. The switch is open. Thus the battery is not yet connected across the capacitor. The meter cannot indicate any current flow.

## B. Capacitor charging

The switch is closed with the result that the battery is connected across the capacitor. Current flows until the condenser plates are charged to practically the same potential as the battery. We have discussed the charging process above, and the result is a positive charge on A and a negative charge on B . The centre-zero ammeter shows a flow of current (indicated by arrows). This flow ceases and the pointer returns to the zero position in the centre when the condenser is fully charged. In the present case, the charging (indicated by a sharp to-and-fro kick of the pointer) is instantaneous as. for simplicity's sake, no resistance has been provided for the condenser to charge through.

## C. Capacitor charged

The switch is opened. The condenser retains its charge (theoretically, at least). Again, the meter cannot indicate any current flow.

## D. Capacitor discharging

The battery is removed and instead a direct path is provided by a conductor (or a resistance). The switch is closed. The surplus of electrons on plate B rush out to meet the positive charge on plate A until both charges cancel out each other and the condenser is uncharged orice again. The ammeter this time deflects to the left thus showing that during discharge the direction of current flow is in the opposite direction to that during the charging of the condenser.
After the condenser is completely discharged, the pointer returns to the zero position; we are back again to where we started (Fig. 6a) and the whole cycle can be repeated over again.

## A Condenser Blocks D.C. but not A.C.

We have said that a condenser blocks D.C. because of the dielectric which is an insulator. Now keeping this in mind, let us consider Fig. 7. When the switch is thrown to position 1, the lamp lights for a very brief interval and then remains extinguished. This is due to the charging current. The same thing happens again with the switch in position 2. This time it is due to the discharging current. If. however, we could flick the switch from position 1 to position 2 very rapidly, say 50


Fig. 6 (a to d)-The condenser charging cycle (see text).
times per second, the lamp would be lit and extinguished at the same frequency; but we would not be able to perceive this and the lamp would appear to be continually lit just as if the condenser were not there at all. Why is this?. The reason is that the current is no longer direct but pulsating. Fig. 8a and 8 b help us to understand this more


Fig. 7 (left)-A switched circuit which shows the effects of applying A.C. to a condenser.
Fig. 9 (right)-The circuit of a simple neon relaxation oscillator.
easily. In the first case, a 1 -pole 4 -way rotary switch is provided. The wiper, rotating in a clockwise direction, successively makes contact with the four positions. Notice the crude triangular waveform with a positive peak above and a negative peak below the zero axis.
(Continued on page 949)

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(Comtinued from page 946)
Fig. 8b provides a smoother rise and fall by the insertion of other batteries supplying intermediate potentials. This waveform is nearer the familiar sine wave. In actual fact, an alternating voltage is produced by a coil rotating in a magnetic field at constant speed, the amount of voltage induced at any instant being proportional to the speed at which the coil cuts the magentic lines of force. One cycle represents one complete revolution. Moreover, the speed of rotation determines the frequency of the alternating voltage.

Another important point with respect to Fig. 8b is that the faster the switch rotates. the brighter the lamp lights; just as if the resistance offered by the condenser is progressively diminished. This brings us to the important concept of Reactance.

## Reactance

Although, as explained above, the condenser does not block A.C., it offers a resistance to it, as is shown by the fact that the battery voltage (supplying the lamp) has to be much higher than the actual voltage across the lamp. The reactance of a condenser is the resistance it offers to alternating current at a given frequency. Reactance (Xc) is measured in ohms. The formula is:

$$
\mathbf{X c}=\frac{1}{2 \pi f \mathrm{c}}
$$

Where $f=$ frequency in $c / s$.
$c=$ capacitance in Farads.
Reactance, therefore, is inversely proportional to the frequency and the capacitance.


Fig. 8a-Using a rotating switch to give a crude form of A.C.


Fig. 8 b -If more batteries are added to the circuit of Fig. 8a, a smoother waveform is obtained.

If the capacitance is constant, the higher $f$ is, the lower $X \mathrm{C}$ is. The reactance of a $2 \mu \mathrm{~F}$ condenser at $50 \mathrm{c} / \mathrm{s}$ is $1591 \Omega$. But at $100 \mathrm{kc} / \mathrm{s}$, it is $0.795 \Omega$.

If the frequency is constant, the higher $C$ is, the lower $X C$ is. The reactance of a $2 \mu \mathrm{~F}$ condenser at $50 \mathrm{c} / \mathrm{s}$ is $1591 \Omega$. But the reactance of a $10 \mu \mathrm{~F}$ condenser at $50 \mathrm{c} / \mathrm{s}$ is $318 \Omega$.

Therefore, reactance is lowered either by increasing the frequency or by increasing the capacitance.

## The Condenser in Use

The peculiarities of the condenser are put to practical use in all kinds of circuitry, from the simplest crystal set to the most complex of electronic computors. Fig. 9 shows the circuit of a simple relaxation oscillator. The condenser. $C$ is charged through $R$. As soon as the voltage across $C$ is equal to the striking voltage of the neon lamp $N, C$ is discharged through it. The process of charge and discharge is repeated over and over again as long as D.C. continues to be supplied.


Fig. 10 (left)-Resistance-capacity coupling between valves.
Fig. II (right)—An. H.T. smoothing circuit.
Two other important and common uses of the condenser are shown in Fig. 10 where we have resistance-capacity coupling between V1 and V2. The coupling condenser Cl prevents the D.C. voltage present at the anode of V1 from reaching the grid of V2 and driving it positive, while at the same time allowing the A.C. signal to reach the grid of $V 2$ for further amplification. The bias condenser C2 bypasses the fluctuating A.C. signal component which prefers to pass through the condenser rather than through the resistance, the capacitance of the former being chosen so that its reactance is much lower than the value of the resistance. The purpose of bypassing the A.C. signal is to maintain a steady D.C. bias voltage at the cathode of the valve.

The condenser $C$ in the choke-input smoothing circuit (Fig. 11) filters out any trace of A.C. ripple which manages to pass through the choke. (The choke offers a high resistance to A.C. While it allows D.C. to pass through it quite easily; its function is opposite that of the condenser).

It has not been possible here to give more than a few basic applications of the condenser in common circuits. The constructor will no doubt be able to find other uses for himself by carefully studying the various circuits which appear in every issue of "Practical Wireless".

## THEORY AND PRACTICAL DESIGN

bass AST month, the theoretical aspects of the bass reflex cabinet were given; some details on construction were also given and it was stressed that to achieve good results, care must be taken to ensure that the cabinet is strong and rigid. If the cabinet walls are allowed to flex, then the sound output will be coloured by cabinet resonances.

## Damping

The cabinet should be at least partially lined with a coating of heavy felt to subdue resonances -about $\frac{1}{2}$ in. in thickness. The felt should not be thick enough, however, to damp sound waves at frequericies below about $200 \mathrm{c} / \mathrm{s}$. It is probably wise not to use too much felt at first, as the amount can always be increased later, if desired.
No allowance should be made for the volume of the felt when calculating the cabinet volume. It is the low frequency response which is affected by the cabinet volume and low frequency sound waves can travel through the felt to the walls.

It is usual to place a piece of expanded aluminium (which is sometimes given a gold coloured finish) over the loudspeaker and vent openings, but care should be taken that this will not produce an irritating rattle when the loudspeaker is producing sound of one particular frequency.

If a piece of cloth is used to cover the grill openings, it is important to use a type of cloth which presents little resistance to the sound waves. Closely interwoven threads should be avoided. Cotton or' plastic cloth which is very loosely woven and which has hard threads is ideal.

## Finish ${ }^{0 \times 9}$

It is well worthwhile taking great care over the finish of the cabinet so that one can take a pride in its appearance as well as its acoustical characteristics. A very neat finish can be obtained by staining the wood to the desired colour and then applying a solution of shellac in methylated spirit carefully. The shellac solution should be allowed to dry and several more coats may be applied to give the finished article a high polish.

## Testing

The ultimate and mosi important test for any loudspeaker system is undoubtedly that of the human ear and the amount of satisfaction obtained by the owner and his friends. Nevertheless there are some measurements which can be carried out.
It is worthwhile to measure the loudspeaker impedance-frequency characteristic at low frequencies with the unit mounted in its cabinet. The apparatus for measuring this characteristic was given in Fig. 3, last month but an A.C. voltmeter
should be connected across the output terminals of the amplifier. Using low power, values of the voltage and current passing to the loudspeakers at various frequencies between about $25 \mathrm{c} / \mathrm{s}$ and $200 \mathrm{c} / \mathrm{s}$ can be found and the impedance at each frequency can be calculated from Ohm's law. The impedance should then be plotted against the frequency as in Fig. 1 (last month).

When the loudspeaker is mounted in a well designed cabinet, the characteristic should no longer look like that of Fig. 1 (last month). The one large peak at the fundamental resonant frequency of the loudspeaker should have completely vanished and two much smaller peaks on either side of the original peak should be found. If the original peak is still present, the cabinet has not been tuned correctly. The characteristic should be replotted with blocks of wood of about 100 cu in. in volume placed inside the cabinet. If it is impossible to remove the peak due to the loudspeaker resonance by raising the frequency in this way. the characteristic should be plotted with the vent reduced in size by a piece of rod. This will lower the frequency at which the cabinet resonates.
If peaks other than the two already mentioned are found in the response curve of frequency between about $80 \mathrm{c} / \mathrm{s}$ and $150 \mathrm{c} / \mathrm{s}$, they are probably caused by standing waves in the loudspeaker cabinet. The area of the walls covered by the damping felt should then be increased until they vanish. It is not possible to remove standing waves completely at very low frequencies, but it is possible to remove them from the loudspeaker resonance cutve.

## Results

The performance of a correctly designed bass reflex cabinet system at low frequencies is much better than that of the more common and cheaper methods of mounting loudspeakers. Some of the advantages are listed below:-
(1) Improved bass response. The bass range may be improved by several dB over a range of nearly two octaves when compared with the same loudspeaker mounted in a closed cabinet or on a very large baffle.
(2) The impedance curve will be much flatter and hence the frequency response curve will be much more level in the low frequency region.
(3) The cone will vibrate with a much smaller amplitude when the input is at the resonant frequency of the loudspeaker than it would if the loudspeaker were mounted in an open cabinet. This will result in reduced distortion at the same power output, or alternatively more power will be available for the same degree of distortion.
(Continued on page 961)

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(Continued from page 798 of the January issue)


HAVING carried out the constructional work described last month, the detector stage can then be built up complete, and tested. Counting the lags from the top (in Fig. 4, last month), connections can be checked as follows: 1, Collector. H.F. Choke, lead 5; 2, Base, lead 2; 3 Emitter, 10 k ( R 3 ), 500 pF pre-set condenser ( Cl ), tuning condenser frame and battery positive; 4, H.F. Choke, 5.6 k (R1). $0.25 \mu \mathrm{~F}$ condenser (CS); $5,0.1 \mu \mathrm{~F}$ condenser (C2). 10k (R3) and 100k (R2) resistors, lead 3 from ferrite slab.

The 500 pF pre-set is held in position by soldering one of its tags directly to tag 3. All the transistor leas's can be left long, but should be covered with sleeving. The transistor can be added last, the joints being quickly made, and the iron removed.

## Testing

If desired, this part of the receiver can be tested with phones. To do this, connect the phones from the free end of the $0.25 \mu \mathrm{~F}$ condenser (C5), to the tuning condenser frame, marked M.C. in Fig. 4. Take a lead from the 50 k regeneration control to battery negative.
Smooth regeneration, right up to oscillation point, should be obtained with the 50 k control. If oscillation cannot be obtained. screw down the 500 pF pre-set slightly. If oscillation is too violent, unscrew this condenser. The correct setting is not very critical, and should allow adequate, yet smooth, regeneration with any battery supply of $4 \frac{1}{2} \mathrm{~V}$ to 9 V . If a regeneration winding has been added to an existing slab or rod, it might be necessary to adj,ust the position of this winding, to secure satisfactory results. If no regeneration at all can be obtained, the winding may have been reversed in error.

Reproduction in the phones should be free from distortion, and of reasonable volume. When the receiver is adiusted for maximum sensitivity, tuning is sharp, and both controls should be operated carefully together. The regeneration control should never be merely turned fully clockwise (as if it were a volume control) as this will not give satisfactory reception.

## Audio Amplifler

This is built as a separate unit. A piece of paxolin is shaped as shown in Fig. 4, so as to clear the tuning condenser, regeneration control, and leave space for the battery.

Small holes are drilled. and the resistors and other parts are placed with their leads through the holes, as shown in Fig. 4. The reverse side


By F. G. Rayer
of the audio panel is shown in Fig. 5.
The colour coding of the driver transformer Tl , and output transformer T2 applies to the transformers listed. Other driver and output transformers would be equally satisfactory and the maker's connecting data should be followed. The leads pass straight down through small holes, and are bent over. A little adhesive under the tran'sformers will hold them to the panel, in conjunction with the leads. Leave the two secondary leads of the output transformer free, for connecting to the speaker.

## Lead Lengths

All transistor leads can be left quite long, as mentioned, but the soldered joints should still be made quickly. Cover all wires. including the ends of resistors. with sleeving. A few inches of thin flex are used for battery connections, terminating with the appro-
 priate positive and negative clips.

When the audio amplifier panel is finished, it is placed in the position shown in Fig. 4. Two short bolts hold it there, with spare nuts so as to obtain about $\frac{1}{4} \mathrm{in}$. space between the audio panel and the receiver panel.

## Connections

The leads shown in Fig. 5 can then be connected to their correct points: one lead goes to the switch (battery negative); a second lead passes to the 50 k regeneration control; transistor $\operatorname{Tr} 2$ base, which is joined to the 33 k and 10 k resistors ( R 4 and R 5 ), goes to the $0.25 \mu \mathrm{~F}$ condenser ( C 5 ), and, finally, a lead connects the battery positive side of the circuit to M.C., or the frame of the tuning condenser.
After connecting speaker and battery, the receiver can be tested. Reproduction should be
clear and distinct. No further adjustments should be necessary, if the 500 pF pre-set has been adjusted as described. If a meter is included in one battery lead, the resting (quiescent) current (no signal) should be around 5 mA . This should rise to about 8 mA to 15 mA on peaks, with average speech or music, according to volume.

## Case and Rod

A piece of silk or other thin material about 4in. square is placed over the speaker, and held with adhesive. Fit the threaded bush for the back screw, tightening it securely. The control knobs are removed, together with the nut of the 50 k potentiometer, and one screw of the tuning condenser. The receiver is then inserted in the case, and the nut and screw replaced, and tightened. Pointer knobs of reasonable size will be best for tuning.
The aerial rod has a bracket to take two 6B.A. bolts, with $\frac{1}{2}$ in. spacers, or spare nuts, between bracket and case, as shown in Fig. 4. A clearance hole is drilled in the case above the top of the rod. An insulated lead passes from the rod to the fixed plates of the tuning condenser. A small terminal on the side of the case would do for an external aerial connection instead.

## Equivalents

The circuit will work satisfactorily with transistors of similar type, including surplus taansistors in proper condition. Tri must be an R.F. transistor, or regeneration may not be obtained. Tr2 is an audio amplifier, and other types may need a change in value of $R 4$, R5 or R6. Tr 3 and Tr4 are best a matched pair for push-pull output. Some transistors may need
(Continued on page 962)

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# FAULTS IN VHF/F.M. RECEIVERS <br> <br> 4-Transistor Sets 

 <br> <br> 4-Transistor Sets}

By G. J. King
(Continued from page 826 of the Jantuary issue)

EVERAL of the more common faults in the final stages of VHF/F.M. receivers were dealt with last month, but a confusing sympiom is the presence of hum and distortion. The treble-diode-triode valve (see Fig. 9, last month) often produces the above symptom, particularly that type of valve which is designed for A.C./D.C. operation, such as the UABC80. One complaint in this respect was that hum and fistortion occurred, on F.M. only, a little while after the receiver has been switched on. It was discovered that the fault was fairly consistent and that it could be almost cleared by detuning. Replacing the valve cleared the trouble completely, but a subsequent check on a valve tester failed to reveal the trouble.

This is one of those cases where a faulty valve can only be discovered by substitution. Dnce the faulty stage has been located, quite a lot of time can often be saved simply by substitating the associated valve before detailed tests are carried out.

If distortion is present on both A.M. and F.M., attention should be given to the common A.F. stages. A typical cause of such trouble is a leak in the A.F. coupling capacitor (C58 in Fig. 9). This puts a positive voltage on the grid of the output valve and causes it to pass much more anode current than is good for it. The valve thus becomes very hot and the voltage across the cathode bias resistor rises above that given in the service manual.

Similar distortion, particularly at high volume levels, should lead to a check of the A.F. amplifier load resistor, such as R24 in Fig 9. If this goes high in value the distortionless output of the stage is considerably limited.

## Balance

Severe distortion on F.M. only, which can be reduced by detuning slightly, is often caused by unbalance in the ratio detector. This may be due to one of the ratio detector diodes going out of balance. Some sets use germanium crystal diodes for the ratio detector instead of the diodes in a multi-electrode valve. These are more prone to unbalance effects; in fact, one of the crystals may go open-circuit completely. This not only causes severe distortion but it also considerably reduces the output on F.M.

The ratio detector can be balanced by applying an amplitude-modulated F.M. I.F. signal (usually at $10.7 \mathrm{Mc} / \mathrm{s}$ ) to the control grid of the last I.F. valve and recording the output either on the speaker or on an output meter connected across
the speaker or across a resistor connected in place of the speaker. The resistor should have a value equal to the impedance of the speaker which it is to replace.

The signal generator should be accurately adjusted to the F.M. I.F., after which the core in the ratio detector winding of the transformer (e.g., L29 in Fig. 9) should be carefully adjusted for minimum output. The ratio detector is in correct balance when it does not respond to an amplitude-modulated signal. In practice, however, there is usually some residual frequencymodulation of the generator signal so zero output is rarely accomplished.

A series on VHF/F.M. receivers would be incomplete without reference to combined F.M./A.M. models using transistors, and the remainder of this series will be devoted to such sets.

There is no doubt now that transistors are going to take the place of valves in almost all types of electronic equipment of the domestic category. Industry is already using vast quantities in special instruments, control systems, computers and the like, and there has also been an almost complete changeover from valves to transistors in the popular A.M.-only portable sets.

## Noise and Reliablity

The new alloy diffusion technique has made the manufacture of VHF transistors possible. These, which are able to operate up to $200 \mathrm{Mc} / \mathrm{s}$, are finding their way into VHF/F.M. receivers and tele'vision sets. A fully transistorised television turret is already available.

Apart from the smaller power requirements and resulting improved efficiency, transistors are also proving to be far more reliable than valves. This means that, while, in the past, transistors were employed essentially for miniaturisation, their use in the future will also be for reliability, and for that reason they will be exploited on an increasing scale in equipnent which, by reason of its nature, does not particularly require to be made smaller, such as television receivers, radiograms, audio and hi-fi amplifiers, tape recorders and so on.

For the present we will concentrate on the transistorised VHF/F.M. set. In Fig 11 is shown the circuit of the VHF tuner of such a receiver. The two transistors are of the alloy diffused type and the circuit is based on the popular Perdio Portable, Model 95 which uses a total of nine transistors and five crystal diodes and is designed for A.M. and F.M. reception.

## Common Base Mode

Transistors Tr 1 and Tr 2 are operated in the common base mode. That is to say the base is earthed to the signal while the input signal is applied to the emitter. The collector is loaded in the usual way with the tuned circuits, across which the output signal is developed.

This arrangement, of course, is analogous to the valve earthed grid circuit, where the grid is earthed so far as the signal is concerned and the input signal is applied to the cathode circuit and the anode loaded with a tuned circuit across which the output signal is developed. For those not fully conversant with transistors, it should be noted that a transistor can be likened to a triode valve in certain respects, with the base being equivalent to the grid, the emitter to the cathode and the collector to the anode.

Transistor Tr1 is the R.F. amplifier for VHF. The aerial signal is coupled through C1 to the wide-band input circuit comprising L1 and C2. The loaded $Q$ of this circuit is quite low, so the circuit responds to the whole of Band 11. The base is held at chassis potential (earth) so far as the signal is concerned by C3 (it should be noted that battery negative is, in fact, the chassis or earth line, this being the opposite to the circuitry in most transistor portables).

## Biasing

The base of $\operatorname{Tr} 1$ is biased by the potential divider formed by R1 and R2 across the battery and thermal stability is maintained by the emitter resistor R 3 . Coil $\mathrm{L} 2, \mathrm{C} 4$ and C 5 form the collector tuned load, and the R.F. tuning section of the gang C5 is coupled to the oscillator counterpart in the usual way. The capacitor, C6, connected between the emitter circuit and base provides a degree of feedback.

The amplified signal is fed to the frequencychanger stage, Tr2, through C7. In this particular receiver, it will be seen that the signal can either be applied to a conventional aerial socket from an outside aerial or, in good signal areas, from a simple telescopic rod aerial.

For the sake of completeness and to help newcomers to transistor circuits achieve a better under-
standing on the basis of comparison, the equivalent valve earthed-grid R.F. amplifier is given in Fig. 12.

## The Frequency-Changer Stage

Transistor Tr 2 performs the dual functions of local oscillator and mixer, and for this reason the stage is often called a "self-oscillating mixer". Again, the input signal is applied to the emitter, but this time across L3. The base is connected to chassis through C8 and is biased by the potential divider R4 and R5. The emitter resistor, R6, provides thermal stability (to prevent thermal runaway) and C9 gives a little feed'sack. Further feedback is provided by C10.

The oscillator tuned circuit comprises L4, C12 and C13, and is coupled to the collector through C11. C12 is the oscillator section of the tuning gang which is ganged with the R.F. section. Capacitors C4 and C13 respectively are R.F. and oscillator trimmers.

## $10.7 \mathrm{Mc} / \mathrm{s}$ Intermediate Frequency

The stage is caused to oscillate at the frequency governed by the tuned load described above by egenerative feedback provided by C14, between emitter and collector.

The collector is also loaded by the tuned circuit L5, which forms the primary of the 1.F. output transformer, L6 being the secondary across which the coupled I.F. signal is developed for feeding to the I.F. stages of the receiver. In common with most F.M. receivers, the intermediate-frequency is $10.7 \mathrm{Mc} / \mathrm{s}$ which, of course, is obtained by the VHF signal heterodyning with the oscillator signal in Tr2.

When the receiver is switched to "F.M.", switch S1 is closed, so that the VHF tuner section is working normally, but when the set is switched to "A.M." S1 is open. This, of course, cuts off col-
(Continued on page 961)


Fig, II - The VHF section of a combined F.M./A.M. transistorised portable set.

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for shelf or cabinet mounting, and has the space for power supplies if required. supplied complete with four EF80 valves
 FHT8 With power. Complete kl ................... Hire purchase deposit 21.19 .0 and 6 monthly ............... 1s the iringe version and should be used when farther than
70 miles irom the transenitter. Bupplied complete with 6 70 miles irom the transmitter. Bupplied complete with 6 valves
Hure purchase deposit 21.18 .6 and 6 monthily
FMT8 With power. Complete kit
Hire purchase deposit $\$ 2.8 .0$ and 8 monthly
The instruction bruk is Included in all kits, but otherwise 2/8.

## JASON SWITCHED TUNERS

The JTV/2 and Mercury 2 are both of the pre-set station type with the addition of BBC and ITA sound. They une the lateat 'Fireball' turret and the A.F.C. ensures freedom irom drift. The Mercury 2 is for csbinet mounting with external power, the JTV/2 has the same taning heart, with power supplies mounted in a case, and can be used for shelf or cabinet JTV/2 Complete with valves and book. ......................... 814.15 .0 Meroury 2 complete with valves and book ...................... 210.16 .0 Hire purchase deposit 22.8 .0 and 8 monthiy .............. 21.4 .0 Power pack kit for Mercury 2 ready drilled chanis .... 82.12 .6 Instraction brok for swithed tuners 4/- each.
REQUIRED CHANNELS MUST BE SPECIFIED FOR SWITCHED TUNERS A more detailed list can be sent apon request.
all dason tuners are on demonstration, and always mi STOCR.

## READY BUILT TUNER

F.M. Tuner Aligned and assembled, using Philips tuning head with ECCS5, EF85, EHS5, EZ81 and EMR1, with \% diodes. UNREPEATAYLE BARGNN.
.CABH

## JASON ARGUS

Tranaistor 2 wave band A.M. Tuner in attractive wroden care. ........................................ KIt 87.10 .0


## MIARTIN IEECORDAKITS

We are able to offer for the Grat time, a prourietary range of Recorders in kit or asgembled form. Thia enables you to talke advantage of masa production techniques and prices, hould you wigh to asembie sourself. The components ased are the thest available, with By a vaives, and the decks are the lateat having all the fmprovementa B.e.R. and CoNsro make from time to tine, heads, etc.: The alluplitiers are packed in special cartons with instruction. which enable anyoue to buld. We are confient you will fod these Reenrders very good value, they have been buit up to a standard and not down to a price.
B.8.R. TD3 Monardeck, fatest model 5if. mpools...........CASH 89.9 .0 Hire purchase deposit 5119.0 and 6 monthly
Tape Amplifer tor B.s.R. deck, printed circuit ready wired, with ECUB3, ECL8:2, EM85 and ER/B1. Complete with all phugs oukets, panety, knobs, etc. The whole amplitler mumbts on
to the deck, makiny a self-contanned unit... CASH PRICE Hire purchase deposit $£ 1.14 .0$ and 6 monthly
48.8.

Cabinet for above inctuding $7 \times 4 \mathrm{~m}$. speaker
Toid kit as above, Hire purchase deposit $\$ 4.10 .0$ and 12 monthiy
.CABH
The above recorder can be bupulied complete with Mio tape assembled and tested for. . . . . . . . . ©ABH PRICE Hire purchase deposit $\$ 5.0 .0$ and 12 monthly Collaro Studio Deck. Very latest model 3 specde

Tape Amplifer for studio Deck. with ready wired printed circuit, control and input panelia, mains and oistout transe, complete with knoles, plans, , Acrewa, etc., EE'8h, ECC83, EMA4 EZBSI. OABl and 2 E Lst, 3 watts out put. Magic eye, Radio and Mic, ioputs. EX L/s socket. Tone control. Can be user a\& an sıuplifier.......................... MPLETE CASH 811.11 .0 Hire purchane de posit 82.7 .0 and 8 monthio

## GRAMOPHONE EQUIPMENT

B.8.R. UA14 TU\&iH vartridge $1 \cdots \ldots . .$.
$\mathbf{2 7 . 1 5 . 0}$
81.4 .0
e8.15.0
Collaro C60 Autochanger " 0 " cartridge .i. '.....ibly
Garrard "Autoshin" $67 / 2$ cartridge
Hire purchase deposit $\$ 1.17 .4$ and 6 monthly
Philips AG1016 New semi-a uto player
89.3 .4
917.8
14.3 .6

Hire purchase deposit 83.3 .6 and 12 monthly
21.0 .2

M|NA AMP H/W November lssue, Resistors 6/-, V/C 6/-, Condensers 9/. Transietors V6/R2 9/a, OC71 6/6, OC7! pr. 16/m, T/T3 13/-. T/T2 9/8. PP9 3/6. Press studs $1 /$. Speaker $7 \times 414$. 17/6, Group/b 2/9. All the above, If ordered at one time, \$4.16.0. Diagrau may ve obtaned from 'Practical Wirelese" $5 / \%$
CITIZEN P.W. Transistor tuner, December isane, Resistore 5/Condensers 11/=, W/C 3/6, 0A703/-, Group bourds 2/9 eac, Transistors 31/m set, Coil set $42 / 6$, RA: $W$ 12/6, J.B. $12 / 6$ with trimwers.

## TRANSISTORS

MULLARD HAVE REDUCED THE PRICE OF HANY TYPES TO OC44 11/-, OC45 10/-. OC70 6/6, OC71 6/6, UC72 8/-, Oथ.75 8/-, OL76 8/m, OC78 8/-. OCR1 8/-. ABOVE ARE THEIR NEW L18T PRICES. WHY BUYSURPLOSP MATCHED PAIRS ONLY. Mullard UC7\% at $16 /$ pair

Cabinet for above lnclading $9 \times 51$. speaker . . . . . . . . . . . . . . . . . . . 8 8.5.0 Total kit as above. . . . . . . . . . . . . . . . . . . . . . . . . . CABH E E89.0.0
Hıre purchase deposit $\$ 6,0,0$ and 12 monthly ............. 82.8 .8
We can supply the above recorder, complete with tape and Mic. 88.0 .0
THIS MAUHINE IS LIBTED EA1.0.0 BY MAKERS AND IS A VEBY BUY.
BUY
Hire purchase deposit $£ 7.0 .0$ and 12 monthly $\qquad$ 82.11. 4

Tape Preamplifier, for recording and playback, as above less output stage, with power supplics
88.8 .0

Hire purchase deposit, $£ 1.14 .0$ and 6 monthly...................
Wicrophone for the above recorlers, Acos M1C 40, 25/-. 8/C plug $4 / 6$.
Synchrotspe Sin. 600 ft . $15 /-\quad$ Sin. 900 ft . $19 / 6$
Finest $\bar{j} / \mathrm{in}$. 850ft. $19 / 6 \quad 5 \geqslant \mathrm{in}$ 1200ft. 22/6
Hoxed 7in. 1200 it . 22/6 7in. 1800ft. 32/6
Tape Reoorder Speaker Cabinet, corner, $20 \times 10 \mathrm{ib}$. High class fialsh

With $9 \times$ sin. high Hux speaker ................................
Marriott Tspe Heads. + track K/PB \& Erase writh mounting plate
for Collaro deck. ................................................. 4.4.

## TRANSISTOR SUPERHET KITS

## "PRACTICAL WIRELESS" POCKET SUPERHET

OsmOR printed circuit version. Osmor Rod aeral 10/-. I.F.T.s and Osc. Colls, 24/6. Gsmor Driver, 11/6. Osmor Output, 10/6. Bet MULLARD

 Condensers, 15/-. Set Kesintors, 6/6. Ardente Vol. Control, 8/-. Ardente
W/C, 3/6. Bpeaker, 19/10. Hardware, 4/B. Prinled Circuit. 8/-. Cabe and
 Knot, 7/6. Dial, 6d. Battery PP4, 2/: l, eatiet givibg full thetrated-detaile,
 New contemporary case, 12/6.

## "WEYRAD"

WEYMOUTH RADIO 6 Transistor suvesthe using the P50 coils, as they advertise to this journal. P50/LAC Ose: Con, $5 / 4$. P50/2CC 1st and 2nd L.F.I.s. $5 / 7$ ea, P50/3CC 3rd 1.F. F., 6/: KA2W Hod Aerial, 12/6. LFDT Driver, 8/6. PCA1 Printed Circuit, 8/6, 1 ustruction Book, 2/-. Bet Resistors, 7/6. Voi. Control D.P., 5/5. Set Condensers, 20/-. J.B. Gang, 11/- Beehiv Trimmers, $1 / 3$ ea. W/C, $8 / 6$. Dial aud K not, 3/6. Battery PP11, 5/6. OA81 3/e. det MULLARD transistors, 53/6. 35 ohm 5in. round L/8, 15/-. Car Aerial Coupling Coil, 1/-.

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OUR RANGE OF PRO. DUCTS IS SO GREAT THAT WE NOW HAVE TO REQUEST THE AMOUNT OF I'6 FOR OUR GENERAL CATALOGUE AND TO SAVE YOU POSTAL ORDER POUNDAGE CHARGE WE REQUEST SEND $1 / 6 \mathrm{lN}$ STAMPS.

## COMPONENTS FOR USE WITH THE "PRACTICAL WIRELESS"

 an amateur communichtions receiverPUSL SHED JULY/AUGUST 1961)

COIL TURRET-CT7/B
This turret is the basic portion of the CT7. It comprises cadmium plated steel frame (size $5 t^{*}$ deep x $4 \frac{1}{*}^{\prime \prime}$ high $x 3 \frac{1^{\prime \prime}}{}$ wide), silver plated contacts, polystyrene insulation and a rotary turret movement incorporating Aerial, Mixer and Oscillator coils for the three bands $1.5-4 \mathrm{Mc} / \mathrm{s}, 4-12 \mathrm{Mc} / \mathrm{s}$ and $10-30$ $\mathrm{Mc} / \mathrm{s}$.

PRICE 75/-
Coil strips for the long and medium wavebands may be purchased separately for incorporation in the turret.

PRICE $10^{\prime \prime} 6$ each
The turret requires a 315 pF tuning capacitor. A suitable 3-gang component with ceramic insulation is available.

PRICE 19/-
Air spaced concentric trimmers, $3 / 30 \mathrm{pF}$.
PRICE $3 / 6$ each

SCALE ASSEMBLY-S1
Comprising basic 5 waveband glass scale for use with 315 pF tuning condenser, back plate, pulleys, rubber scale mounts, pointer, cord, drum, spring, drive spindle, screws, nuts and spacers.

PRICE 19/ـ
BEAT FREQUENCY OSCILLATOR COILBFO. $2 / 465 / \mathrm{kcs}$.
A compact coil wound on a bakelite former and enclosed in an aluminium screened can. PRICE 5/-
I.F. TRANSFORMER-IFT, $11 / 465 \mathrm{kc} / \mathrm{s}$ (Four required)
A miniature I.F. Transformer for $465 \mathrm{kc} / \mathrm{s}$. Permeability tuned, litz wound coils, enclosed in an


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HI-FI quality printed-circuit amplifiers, supplied checked and assembled
Complete with valves, transformers and everything down to wire cut to length.
Produced by the makers of amplifiers for some of today's best known recorders and backed by years of experience in audio design. The specially designed kits offered here set entirely new standards of performance and finish for the home constructor. Amplifier available separately or with case and speaker and deck. EASY TO FOLLOW INSTRUCTIONS. All equipment complete and guaranteed.
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## TWO \& FOUR TRACK TAPE RECORDERS

AMPLIFIER 'C' for Collaro Studio Deek (illustrated above). II gns.
Case and Speaker for above
5 gns.
AMPLIFIER 'A' (4-TRACK) for BSR Monardeck. 9 gns.
AMPLIFIER 'B' (TWO TRACK) for BSR Monardeck. 8 gns.
Two-tone covered wooden case with speaker for above. 4 gns.
KIT 'A' with Deck, Case and Speaker. 24 gns.
KIT 'B' with Deck, Case and Speaker. 21 gns.
KIT ' $C$ ' with Case, Speaker and Deek (as illustrated). $28 \frac{1}{\mathbf{1}} \mathbf{8 n s .}$
All amplifiers supplied assembled on printed circuit boards with valves.

## MARTIN <br> PECORDAKITS

Leaflet free on request.
Set of full instructions for any one model 2 '6d. post free. (Allowable on purchasing kit).
COUPON BRINGS DETAILS


## (Continued from page 958)

Fig. 12-The valve equivalent of the R.F. stage in Fig. II. Here, RI is for bias and R2 is the grid return resistor.
lector current on Tr 1 and Tr 2 , but it will be noted that the bases remain biased since the bottom ends of the potential dividers, R2 and R5, are connected to the battery side of S 1 . This is done to prevent damage to the transistors, which might otherwise occur owing to a rise in base voltage.

## Tracing Faults in the VHF Section



The VHF section is often built into a selfcontained screened box, and intermittent troubles on VHF/F.M. due to poor connections. dry joints and so on occur equally in transistor units as they do in valve units. However, owing to the cool operation of transistors, frequency drift i: not so troublesome as it is with valve circuits, but printed circuits and inter-connections still give trouble, and should be investigated as described in previous articles should intermittent symptoms on VHF/F.M. develop.

The alignment of a transistorised VHF tuner is sometimes more important than in valvz units, for if the l.F. or oscillator alignment is misplaced by a small amount, the local oscillator may fail over a section of the tuning range.

## Aerial

Excessive "noise" on F.M. when a station is tuned in should lead to a check of the aerial system for, although the new VHF transistors are endowed with remarkably good noise figures, one is often tempted with a portable to use the smallest aerial possible, and while this is perfectly in order in areas of reasonably high signal where there is little l`cal shielding, something better is required in shielded locations.

If the VHF section fails completely, and the set operates normally on A.M., there is every possibility that the VHF tuner is faulty. This can be
proved speedily by switching the set to "F.M." and injecting the F.M. I.F. from a signal generator across L6, for example. If the output from the speaker is loud and clear, then the tuner is definitely faulty. If there is no output, attention should be directed to the F.M./A.M. changeover switching.
In most cases of VHF unit failure, apart from dry joints and poor connections, the local oscillator section is to blame. This invariably gives rise to a "hiss" when the set is switched to "F.M." and the volume control turned up full and, in some cases, there may be a sudden restoration of signals at certain settings of the tuning gang.

## Readings

Much information on the operation of the transistors can be obtained by measuring the voltage across the emitter resistors (R3 and R6 in Fig. 1). The voltages will be low normally, not much more than one volt, so a low reading voltmeter is essential, and to avoid loading the circuits unduly the voltmeter should also have a fairly high resistance or sensitivity. A $20,000 \Omega / \mathrm{V}$ neter with a full-scale deflection on the "low volts" range of 2.5 V to 5 V is ideal.

Tests are best made with meter positive connected to battery positive. With the negative lead connected to TrI emitter a reading of around 0.85 V would indicate that the transistor is passing collector current. On the same electrode of Tr 2 , the reading should be about 1.1 V . Zero voltage would indicate either that the transistor is open-circuit or that the negative supply to the collector is missing. This supply should next be checked, if necessary, by connecting the negative of the meter to the collector. The voltage here should be almost equal to the negative line voltage, since the collector loads are of low resistance, though it may not be equal to the battery voltage owing to the voltage dropped across decoupling and filter resistors in the negative circuit from the battery to the VHF tuner. A value of about 7 V is typical for VHF collectors.

The base voltage can also be checked by connecting the meter negative to base (positive still connected to battery positive). Base bias for VHF transistors is around 1V though it may be slightly higher on the frequency changer when oscillating properly.

If the voltages deviate substantially from the above examples, the feed components should first bc checked for continuity and value, and if normal, the associated transistor will, in most cases, be found responsible.

## The HBASS Reflex Cabinet

(Continued from page 950)
(4) The radiation resistance will be greater at low frequencies, and therefore the power will be more efficiently transferred to the surrounding air. When compared with a similar loudspeaker mounted in a closed cabinet, a power ga:a of about 3 dB might be expected. as half of the power from a loudspeaker in a closed cabinet is wasted by being trapped in the cabinet. In actual practice the gain may be greater.than 3 dB when a bass refex cabinet is used owing to the more efficient transfer of energy to the air.

The only possible disadvantage of the use of a bass refiex cabinet is that if the amplifier feeding the loudspeaker contains any hum, this will sound much more prominent than before, but the remedy for this is obvious.

Care should be taken not to obstruct the vent or the front of the loudspeaker; at the loudspeaker resonant frequency the sound is radiated almost entirely from the vent.

The frequency response should extend down to half the loudspeaker resonant frequency or-less; with conventional mounting, the bass output from a loudspeaker is almost negligible below its resonant frequency.

雨 雨 雨 事 Club News


## REPORTS OF CURRENT ACTIVITIES

AMATEUR RADIO MOBILE SOCIETY
Hon．Sec．：G3FPK， 79 Murchison Road，London，E． 10.
At this year＇s Radio Hobbies Exhibition in London，the society had their own stand，manned entirely by A．R．M．S．members． BRADFORD RADIO SOCIETY
Hon．Sec．；M．T．G．Powell，G3NNO， 28 Gledhow Avenue， Roundhay，Leeds 8.

The society＇s last spares sale in 1961 was held on November 28th． On December 12th，the development of time measurement was discussed by W．Barton，and amateur receiver construction was the subject of the lecture given by D．M．Pratt at the meeting on January 2nd．

Future Events：
January 30th－Use of simple test gear，by D．G．Enoch．
February 13th－Field－day discussion and informal meeting．
DERBY AND DISTRICT AMATEUR RADIO SOCIETY
Hon．Sec．：F．C．Ward，G2CVV， 5 Uplands Avenue，Little－ over，Derby．

The society＇s Open Night on December 13th was also appointed as the management committee meeting．On December 20th members enjoyed the Annual Christmas Party．As there was no meeting on 27th December，those members who wanted to joined in a 160 metre net instead．Yet another surplus sale was held at the first meeting of the new year，on January 3 rd ．

Future Events：
January loth－The year in retrospect－an opportunity for nembers to see some of the activities of 1961 in photograph form． January 17 th－A selection of communication receivers will be shown for members to compare．
GUILDFORD AND DISTRICT RADIO SOCIETY
Hon．Sec．：J．R．Barker，G3PDX， 35 Banders Rise，Merrow， Guildford．
All the entrants for the car treasure hunt，held on October ist， managed to complete the course．The proposed 2 －metre equip－ ment for the club net，was the subject of a talk given by Harry Mead at the meeting on October 12th．It was at this meeting that the society decided to enter the MCC top band contest，and so on November 11 th， 12 th， 18 th and 19 th，the club took an active part in the contest，using the call sign G3FZC．On October 24th the club visited the Dorking group for a ragchew and films．
Four club members took part in the RSGB top band contest which was held on November 11 th and 12th．
DUDLEY AMATEUR RADIO CLUB
Hon．Sec．：S．E．Plumtree，G3OSP，II Wallows Wood，The Straits，Lower Gornal，Dudley，Worcestershire．

On October 13th，members payed an outside visit to attend a demonstration of closed circuit television，hi－fi，tape recorders and audio equipment，and to see a film show．
－A committee meeting was held on 20th October and another was held on 3rd November．On November 10th，members enjoyed a，film show and on December 8th the Christmas dinner was held．

NORTHERN HEIGHTS AMATEUR RADIO SOCIETY Hon．Sec．：A．Roninson，G3MDW，Candy Cabin，Ogden， Halifax，Yorkshire．

Recent activities have included a talk on 2 metres by G8CB and a demonstration of hi－fi and stereo．On December 13 th members took part in a ragchew．

Future Events：
January 10th－Informal meeting．
January 24th－Tape recorders．
PETERBOROUGH AND DISTRICT AMATEUR RADIO SOCIETY
Hon．Sec．：D．Byrna，G3KPO，Jersey House，Eye，Peter－ borough．

At the annual general meeting of the society，on the 3rd Novem－ ber，$S$ ．Hunting was elected president，C．J．Guscott was elected chairman，and D．Byrne was elected secretary and treasurer．

## ROTHERHAM RADIO CLUB

Hon．Sec．：S．J．Scarbrough， 25 Crawshaw Avenue，Sheffield 8.
During November members took part in the MCC top band contest．In December the club＇s own Annual Competition for the G3KUH shield was held．

The annual general meeting was held on January 3 rd．

## SALISBURY AND DISTRICT SHORT WAYE CLUB

Hon．Sec．：E．J．Spicer， 43 Vale View Road，South Newton， Salisbury，Wiltshire．
Arrangements have been made for the club to show a series of films，fortnightly to members，and the first of these were shown on November 21st．Taped lectures are also a fortnightly attraction， and morse classes are given most weeks．
SILVERTHORN RADIO CLUB
Hon．Sec．：K．Marley，G3EIO， 17 Luctons Avenue，Buckhurst Hill，Essex．

Meetings are held every Friday at 8 p．m．at the South Chingiord Community Centre．A club station is operated at constructional meetings on alternate Fridays．
SPEN VALLEEY AMATEUR RADIO SOCIETY
Hon．Sec．：N．Pride， 100 Raikes Lane，Birstall，Nr．Leeds． The society＇s Brains Trust was held on December 20th and the meeting on January 3rd was taken up by a ragehew．

Future Events：
January 17th－Electronic timing devices，by S．Marsden． January 31 st－Safety in the shack．
WANSTEAD AND WOODFORD RADIO SOCIETY
Hon．Sec．：K．Smith，G3JIX， 82 Granville Road，Waltham－ stow，London，E．17．

At every Tuesday evening meeting，G3JlX gives a lecture on the requirements of the G．P．O．Radio Amateur＇s Examination．

The＂constructional project＂at the moment is a C－R bridge，and each member is constructing one from the same basic design．

## P．W．MINUETTE

（Continued from page 954）
values other than $220 \Omega$ for R9 and $5 \Omega$ for R10，to obtain full gain and distortion－free reproduction．

## Miniature H．F．Choke

A miniature H．F．choke can be made by taking a ferrite slug and winding several hundred turns of fine gauge wire upon it．For good results，there is little latitude in resistor values，but condenser values are less important．Typical possible values，with marked values in brackets，are： $0.1 \mu \mathrm{~F}$ to $0.5 \mu \mathrm{~F}$ $(0.1 \mu \mathrm{~F}) ; 0.25 \mu \mathrm{~F}$ to $6 \mu \mathrm{~F}(0.25 \mu \mathrm{~F})$ ； $1 \mu \mathrm{~F}$ to $6 \mu \mathrm{~F}(2 \mu \mathrm{~F}) ; 6 \mu \mathrm{~F}$ to $50 \mu \mathrm{~F}$ （ $30 \mu \mathrm{~F}$ ）．


## SPECIAL BARGAIN OFFER! RECORD PLAYER KITS

AUTOCIIANGEIE Kil-Comprising three Units, Contemporary styled Cabinet2 valve, 2 watt amp. and 7 x $41 n$. quality speaker. Variable tone and Volume Controls with ieedback circuit and B.S.R. $4-$
speed 10 Record Mixer, Auto Changer Untt. speed 10 Record Mixer, AUto $1212.10 \mathrm{~S}_{\mathrm{i}}$ only.
Cabinet Size: $17 \times 141 \times 8+1 n s$. Carr. $7 / 6$.
©INGLE PLAYER KIT-Similar spec. to Autochanger Kit except Player is 4-speed B.S.R. T.U.9. Single Record Player Unit. Attractive Contemporary Styled Cabinet,
Size: $134 \times 13 \times 6 \mathrm{~ns}$. With splendid volume and reproduction.
BARGAIN PRICE 88.19 .6 only
ALL UNITS READY WIRED. SIMPLE SCREWDRIVER ASSEMBLY ONLY FULL SATISFACTION-
Send for teaflet. Full details-3d. stamp.

7 VALVE AM/FM RADIOGRAM CHASSIS Valve Lime-up: ECC85 ECH81 EF89 "EABC80 EL84 EM81 EZ80.
Three Wapeband and 8witehed Gram position. Med 200.500 ma , Lonk $1,004-j_{0}, 000 \mathrm{~m} .$. VHFiFM $85-95 \mathrm{Mc} / \mathrm{s}$. Philips Continental Tuthins inftit with permeablity tupug on FM and combuned AM/FY IF transformers, 460 Kcis and 10.7 Mcha Dust core luning ail mik, Latest vircuitry inciuding AVC aud Neg. Feed back. Three watt output. very high Btiandard. Chassis size 13 z $\quad 6$ rin. Heignt fin. Edge Illuminateu, gisas dial station nat
operation.


Aligned and eested ready for use f 13.10 .0 Corr. \& ins., 5/..
Complete with 4 Knobs-walnut or ivory to chotce. Indoor FM Aeris), 2/6 extra.
Three ohm P, M. speakez onty required. Becommended quality speakers. 10in. Bola tHeavy Dutv). 30'-

8in. Hota or Elac (hempy duty) $25 /-$, pn en p. $2 / \%$.

## BARGAINS 4-SPEED PLAYER UNITS <br> Carr. 5

Single Players Cart. 3/6 Garrard 4 S.P. $\mathrm{E}^{2} 6.19 .6$ Garrard TA Mk. 2 \& 7.19 .6 Collaro "Junior" 75/0 $\begin{array}{ll}\text { B.S.R. (TU9) } & 79 / 6 \\ \text { E.M.I. Juntor } & 89 / 6\end{array}$

Auto-Changers
$\begin{array}{ll}\text { Guro-Changers } & \text { Carr. 5/- } \\ \text { Garrard R210 } & \mathbf{\$ 1 0 . 1 0 . 0}\end{array}$
Collaro "C 60"
B.S.R. (UA14)

IAtest Model Garrard
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ENAMELLED COPPER VIRE-Ilb. reels. $148-20 \mathrm{~g}$, $2 / 6$ : $22 \mathrm{~g}-28 \mathrm{x}$. $3 / \mathrm{B} \quad 30 \mathrm{~g}-40 \mathrm{~g} . \quad 3 / 9$. Other gauges quoted ior.

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METAL KECTIFIERS, STC TVJC KM3, 7/6; RM4. 16/-; EM5, 21/RM4B. $17 / 6$.

SIEMENS TYPES - Contact Cooled; 250 V . $50 \mathrm{~mA}, 7 / 6 ; 250 \mathrm{~V}$. $85 \mathrm{~mA}, 10 / \mathrm{F} .250 \mathrm{~V} .12 \mathrm{ma}$. $15 / \mathrm{F}$ $250 \mathrm{~V}, 300 \mathrm{~mA}, 26 / 8$.

Famo Famous American Columbia (CBS) Premier Quality Tape at NEW RED LCED PRICES. A genuine recommendes Quality with leader and stop folls.

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| :---: | :---: | :---: | :---: |
| $5 i n$. | $600 f$ t. 15J- | 900ft. 18/6 | 1,200ft. 31/6 |
| 5 in. | gooft. 17/6 | 1,2001t. $22 / 6$ | 1,8001ts 38/6 |
| 7 in. | 1.200ft. 21/- | 1,8001t. $\quad 32 / 6$ | 2.400ft. $47 / 6$ |

Post and Packing, per reel. $1 /-$, plus $6 d$. each for additienal reels. SPECLAL OFFER-31n. mfrs. surplus tape, 225ft. 5/G P. \& P. per reel. 6d, Plastic Tape Reels, 3in. 2/6, 5in. 3/; $5 \operatorname{tin} .3 / 3,7 i n .3 / 6$.

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> DASON FAS TUNHR UNI'TS parts:
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> $\begin{gathered}\text { FWre, eq. } 5 \text { valves. } 37 / 6 . \\ \text { JTV MERCURY } 10 \text { gns. }\end{gathered}$
> $\begin{gathered}\text { JTV MERCURY } 10 \text { gns. } \\ \text { JTVZ } \\ \text { £13. } 19.6 .\end{gathered}$ $\begin{aligned} & \text { JVV2 £13.19.6. } \\ & 32 / 6 .\end{aligned}$ NEW NEW JASON FM HANDBook, 2/6. 48 hr Alignment Service 7/6. P. \& F. $2 / 6$.

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 $\underset{\text { Bow }}{\text { Noxed }}$ VALVES Gaztanteod

 \begin{tabular}{ll|ll|ll}
$1 T 4$ \& $8 /-$ \& ECC83 \& $8 /-$ \& PCC84 \& $9 / 6$ <br>
$1 R 5$ \& $7 / 6$ \& ECL82 \& $9 / 6$ \& PCF80 \& $9 / 6$

 

$1 R 5$ \& $7 / 6$ \& ECL82 \& $9 / 6$ \& PCF80 \& $9 / 6$ <br>
185 \& $7 / 6$ \& ECL80 \& $10 / 6$ \& PCL83 \& $12 / 6$

 

3S4 \& $7 / 6$ \& EF80 \& $8 / 6$ \& PCL84 \& $12 / 8$ <br>
$3 V 4$ \& $7 / 6$ \& EFS6 \& $12 / 6$ \& PLo1 \& $12 / 6$

 

DAF96 \& 日/- \& EL84 \& $8 / 6$ \& PL82 \& $9 / 6$ <br>
DY9 \& $9 /-$ \& EY51 \& $9 / 6$ \& PL63 \& $10 / 8$

 

DK96 \& 9/- \& EY86 \& $10 /-$ \& PY82 <br>
DL96 \& 9/- \& EZ81 \& $7 / 6$ <br>
PY81 \& $9 / 6$ <br>
ECC81 \& 8/- \& GZ32 \& $12 / 6$ \& PY82 <br>
I/B

 

ECC81 \& $8 /-$ GCi32 $^{2}$ \& $12 / 6$ \& PY82 \& $7 / B$ <br>
ECC82 \& $8 /-$ \& EM81 \& $9 / 6$ \& $\mathrm{U} \geqslant 5$ \& $12 / 6$
\end{tabular}

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## Midget 1.F.'s-465 Ko/s

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Elect. Condensers-M1dget Type 1 mid-50mfd. ea. $1 / 9$. $100 \mathrm{mfd}, 2 /-; 6 \mathrm{~V} / 12 \mathrm{~V}$ wkg. Condensers- 01 mfd , .03 mfd . Yd.: $.05 \mathrm{mfd} .1 \mathrm{mid} .1 /-; .25 \mathrm{mfd}$, 1/3: . midi $1 / 6$.
Vol. Controls-Midget Type with edge Control Knob
$47 \mathrm{~K}, 1 \mathrm{M} / \mathrm{ohm}$, ea. $2 / 6$.
Speakers P.M.-2tin. E.M.I. 3 ohms 17/8. $7 \times 4 i n$. Plessey 35 ohe
Ear Plug Phones-Min. Continental type, 3ft. lead, jack plug and socket. Hish Imp. 8/\%.
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Brand New-BVA 1st Grade Brand New-BVA 1st Grade $\begin{array}{lccc}\text { OC44 } & 10 / 6 & 873 & 9 / 6 \\ \text { OC45 } & 9 / 6 & \text { GET114 } & 6 / 6 \\ \text { OC } 81 & 7 / 6 & \text { OC72 } & \text { 1/6 }\end{array}$

| OC45 | $9 / 6$ | GET114 | $6 / 6$ |
| :--- | :--- | :--- | :--- |
| OC81 | $7 / 6$ | OC72 | $7 / 6$ |
| $2 / O C 81$ | $15 / 6$ | OC70 | $5 / 6$ |



| XA101 | 9/6 | 0 O 78 | $7 /$ |
| :---: | :---: | :---: | :---: |
| X ${ }^{103}$ | \%/6 | GEX34 |  |
| $\times \mathrm{C} 01$ | $8 / 6$ | OA70 | 2 |
| 874 | $8 / 6$ | OA81 |  |
| SB30 | foce | GEX |  | SB305 Surface

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$36 \times 12 \mathrm{n}$.
$13 / 6$. etc.. etc.
 SLEEVING-Various Colours $1 \mathrm{~mm}, 2 \mathrm{~mm}, 2 \mathrm{~d}, \mathrm{yd} .: 3 \mathrm{~mm}, 4 \mathrm{~mm}$. 3d. yd.. $6 \mathrm{~mm}, 5 \mathrm{~d}$. yd.

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4 pole 2 way, 4 pole 3 way, $3 / 6$ each,
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MAXIMUM POWER
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in excess of 14 watts
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peaker and practically any make of deck Negative feedback equalisation adiustment by multi-position switch for $1 \frac{1}{6}, 3 \frac{3}{4}$ and $7 \frac{1}{2}$ in. per second. Retaif price 12 gns.
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| . 354 | 6/- |
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| 6BJ6 | 5/9 |
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| 6BW6 | 71 |
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| 6 F 1 | 10 F |
| 6 F 6 G | \%/8 |
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| 737 | $9 \%$ | DF33 | 9/- |
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The Editor does not necessarily agree with the opinions expressed by his'correspondents


#### Abstract

Whilst we are always pleased to asslst readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELEPHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupron from page iil of cover.


## CORRESPONDENTS WANTED

SSIR,-I am a regular reader of Practical Wireless. I am very much interested in the radio technology and have started my own shop of radio repairs. I would like to correspond with any radio technician from anywhere. I will answer all the letters received prompily.-B. S. Gulshan, Falcon Radios, Kota JN, India.

## VALVE-TRANSISTOR SHORT-WAVER

SIR,-I have been gratified that so many people have enquired about the above receiver described in the July issue of Practical Wireless. A large proportion of these are concerned with the winding of the coils. These few notes should remove any difficulties.
L3 consists of 10 spaced turns over 2 in., tapped at 5 turns and $7 \frac{1}{2}$ turns. The latter figure untortunately appeared in the issue as $2 \frac{1}{2}$ turns.

Extensions to any of the coils to cover different wavebands is possible, only at the expense of losing other sections of the frequency spectrum. No experiments have been carried out which concern the fixing of a fourth coil.
The actual positions of the coils on the baseboard or chassis are not important as the three coils each carry their own reaction winding and aerial section.-P. K. Cripps (Liverpool).

## RECORD 'WOW'

SR,-With reference to the article by L. E. Higgs in the September issue on record player faults. may I suggest that the fault of wow and slurring owing to records being warped can very simply be cured. The seven-inch records seem to be the chief offenders. If eight strips of Sellotape, about $\frac{1}{2}$ in. $x \frac{1}{2}$. wide, are placed at $45^{\circ}$ intervals across the driving serrations, making certain they are clear of the run-oft grooves, it will be found that even a badly warped record does not skid. I do this to every record regardless of its condition and have consequently had no trouble.-W. D. Heseltine (Wallsend-on-Tyne).

## Vintage models

SIR,-I was very interested in the letter in the December issue, by Mr. Mansell, as I too think that some of the old radios in true teproduction were very good indeed. I am sure anyone who has not heard one, tuned in to a good concert, would be very much surprised by the good quality obtained.

I have a very old tuned R.F. set which first had come from Chicago, U.S.A., 1931 to 1932, and was called the Zenith Autovox. This set had five tuned stages of H.F. and double push-pull output stages. These, working into a 15 in . energised loudspeaker, resulted in a very powerful output and the quality of reproduction was amazing.

I have recently had to rebuild the set as the old valves gave out and could not be replaced. The set is still working wel! and it will pull in any station on' a short piece of wire as the aerial, and the tuning is very selective.-D. J. Forwarch (Watford).

## L.F. INSTABILITY

$S^{I R}$,-I should like to report an interesting case of L.F. instability and its cure, in the hope that it may be of interest to others who may come across a similar unexplained fault.

The circuit was a simple mains amplifier, with a push-pull output stage fed from two audio stages (EF86's; one strapped as a triode and acting as phase splitter for the push-pull output stage). When switched on a very loud hum was experienced and the usual cursory tests failed to disclose the cause. Eventually the two EF86's were removed but the hum still persisted. The phase splitter had just a single resistor to the H.T. line and there was adequate smoothing ( $60 \mu \mathrm{~F}$ ). It was eventually found that a large electrolytic from the anode of the phase splitter to earth stopped the hum and finally the cure was a simple resistor ( 10 k ) between the anode resistor and the H.T. line, with a $32 \mu \mathrm{~F}$ condenser to earth. - F. G. Roberts (Torquay).

## SOLDERING TRANSISTORS

$\mathrm{S}^{1 R}$,-I should like to pass on a small hint which others may not have seen and which I feel is very important for those who are building the latest types of miniature transistor sets. As most readers now know these components are easily damaged, or even completely ruined, in the act of soldering them into a set. Fitting a heat sink is one very good idea, but 1 have met cases where the compactness of the set is such that there was no room to fit the shunt unless the leads were left extremely long. In addition whilst the heat shunt may protect the actual component being soldered there is also the risk that nearby parts may be damaged by the radiated heat from a soldering iron. Therefore, when constructing this small type of receiver I have found it a good idea to wind a length of ordinary copper wire, not heavier than 24 s.w.g. round the bit and to draw off the remaining two inches. this giving in effect a two inch projection to the bit of thin copper and I find that it carries just sufficient heat to melt the wery fine printed circuit solder without risk of damage. I even dispense with heat sinks when using this iron. -F. Walters (Hampstead).

MISCELLANEOUS

## ELECTRONIC MUSIC?

Then how about making yourself an electric organ? Constructional data available-full circuits, drawings and notes. It has 5 octaves, 2 manuals and pedals with 24 stops-uses 41 valves. With its Yariable a
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## RECEIVERS \& COMPONENTS

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The Index letters which precede the Blueprint Number indicate the periodical in which the description appeared. Thus PW refers to PRACTICAL WIRELESS; AW to Amateur Wireless and WM to Wireless Magazine.
Send (preferably) a postal order to cover the cost of the Blueprint (stamps over 6d. unacceptable) to

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## SPECIAL NOTE

THE following blueprints include some pre-war designs and are kept in circulation for those constructors who wish to make use of old components which they may have in their spares box. The majority of the components for these receivers are no longer stocked by retailers.

| Title | Number | Price |
| :---: | :---: | :---: |
| A.C. Fury Four | PW20 | 2/6 |
| Experimenter's Short Wave | PW30a | 2/6 |
| Midget Short Wave Two ... | PW38a | 2/6 |
| Band-Spread Three (Battery) | PW68 | 2/6 |
| Crystal Receiver | PW71 | 2/- |
| Signet Two (Battery) | PW76 | 2/6 |
| Simple S.W. One-valver | PW88 | 2/6 |
| Pyramid One-valver | PW93 | 2/6 |
| BBC Special One-valver | AW387 | 2/6 |
| A One-Valver for America | AW429 | 2/6 |
| Short-Wave World Beater. | AW436 | 3/6 |
| Standard Four Valve S.W. | WM383 | 3/6 |
| Enthusiast's Power Amplifier | WM387 | 3/6 |
| Standard Four Valve | WM391 | 3/6 |
| Listener's 5-Watt Amplifier | WM392 | 3/6 |

Listener's 5-Watt Amplifier
WM392
3/6

The PW 3-speed Autogram
8/-
The PW Monophonic Electronic Organ

8/-
(No constructional details are available with this blueprint)
The PW Roadfarer
5/-
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TELEVISION
The PT Band III converter
1/6

Title Number Price
CRYSTAL SETS
Junior Crystal Set .. .. .. PW94 2/-
Dual-wave Crystal Diode .. .. PW'95
2/6

## STRAIGHT SETS <br> Battery Operated

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PW100
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The PW Pocket Superhet

## MISCELLANEOUS

[^9]

Size $4 \frac{3}{3} \times 1 \times 1 \mathrm{in}$.

| All |
| :---: |
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| 7916 P.P. 116 |
| Evervething |
| Supplied | instrucrions follow inscructions with pietorial layout

free on request. Reception of Radio Luxembourg guaran-
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Size $8 \frac{1}{2} \times 6 \frac{1}{2} \times 3 \frac{1}{2}$ in.

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6 BUILDING PLANS \& PRICES FREE ONREQUEST 6


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95 Mullard Transistors and diode.
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A new printed circuit design fully tunable on borh wavebands. Guaranteed reception of Continental and local stations including Luxembourg. any where with full station separation. Fitted Car Aerial \& Earpiece Sockets

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59/6
P.P. 116


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3/4 WATT 4 TRANSISTOR AMPLIFIER

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1 watt peak output.
$\pm 3 \mathrm{db} 70 \mathrm{c} / \mathrm{s}$
to $12 \mathrm{ke} / \mathrm{s}$.
Output to 3 ohmspeaker.
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6 TRANSISTOR MEDIUM AND LONG WAVE SUPERHET



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