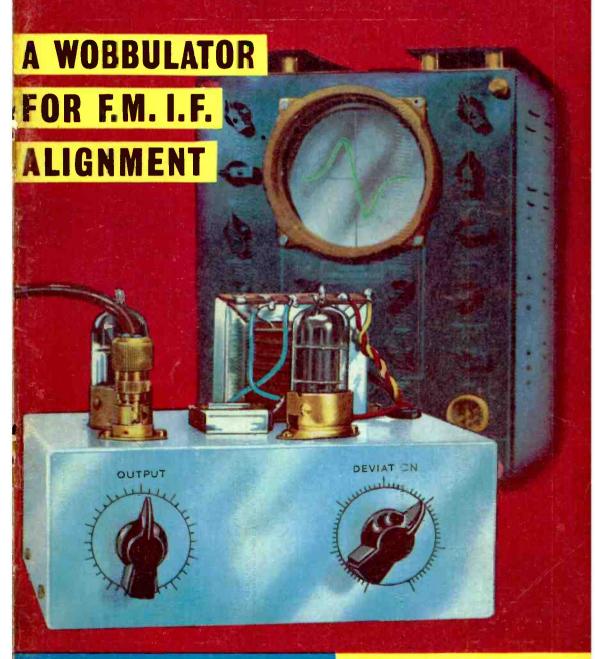
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Hi-impedance-2,000 ohms-general use headset. Black and Ivory plastic cased electro-mag units with netic uni adjustable band for comfort-able fit. Individual listening for all types of applica-Istening for all types of applica-tions. Individually packed, with flexible cord att-

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3Q5	10/6	6L18	12/6	12K7G1		80	10/-	DH719	7/6	EL32	5/-	KT55	22/6	PZ30	18/6	UF80	9/-
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6AQ5	8/3	65N7G1	5/6		24/4	AC6	21/-	EBL31	21/6	EZ35	71-	MS4B	17/6	U16	10/-	W142	91-
6AQ8	9/3	6U4GT		20D1	12/6	ACTP	32/-	EC90	9/6	EZ40	7/6	MSP4	17/6	U18/20	10/-	W719	7/6
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6C6	616	7Q7	11/6	30F5	11/6	B152	8/6	ECF82	12/6	H30	5/6	N729	8/-	U142	8/-	Z719	7/9
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All prices quoted provide for the COMPLETE RECORDER including CRYSTAL MICROPHONE and 1,200 ft. Spool of Tape.

Each Model incorporates the highly successful HF/TR3 Amplifier (described below) thus ensuring truly "Hi-Fi" record and playback facilities.

There are no better value-for money Tape Recorders on the market—if you can't call and hear them send S.A.E. for fully

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The COLLARO, "STUDIO" TAPE DECK and our
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KIT OF £14.0.0 H.P. £3.8.0 Deposit and £17.0. 12 months £1.4.11 (Excluding power unit £11.1.15.0 and £14.10.0 respectively). £17.0.0

COMPLETE KIT to build the HF/TR3 Amplifier together with the COLLARO "STUDIO" DECK. As above but with HF/TR3 supplied ASSEMBLED and TESTED the New York of the New TRUVOX MK, VI TAPE DECK. As above but HF/TR3 supplied ASSEMBLED and TESTED The Deposit 28.0.0, and 12 months 22.3.3 (240.0.0 H.P. Deposit 28.0.0, and 12 months 22.18.3 (240.0.0 H.P. Deposit 28.0.0, and 12 months 22.18.3 (240.0.0 H.P. Deposit 28.0.0, and 12 months 24.18.3 (240.0.0 TESTED The New York of the New Yor

TESTED H.P. Deposit £9.2.0, and 12 months £3.5.9.

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Carriage and insurance on each above is 10/-extra.

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designed to operate through the pick-up sockets of
the standard type of RADIO RECEIVER, or an AMPLIFIER,
from which really first class reproduction is obtained. It consists of a Twin Track Deck connected to the Pre-amplifier and operates at 3fin /sec.. speed providing up to 1 hr. 10 mins. playing time.

COMPLETE KIT OF PARTS

MULLARD "5-10" MAIN AMPLIFIER

FOR use with the MULLARD 2-valve pre-amplifier with which undistorted power output of up to 10 watts is obtained. We supply SPECTPLED COMPONENTS AND NEW MILLARD VALVES, including PARMEKO MAINS TRANSPORMER and choice of the jatest Ultra-Linear PARMEKO or the PARTRIDGE OUTPUT Transformer. COMPLETE KIT OF PARTS. \$10.0.0

Alternatively we supply ana.

\$11.10.0 INCORPORATING PARTRIDGE OUTPUT ASSEMBLED and TESTED, \$11.10.0 TRANSFORMER, \$1.6.0 EXTRA.

MULLARD'S PRE-AMPLIFIER

TONE CONTROL UNIT

Employing two EF86 valves, and designed to operate with the MULLARD MAIN AMPLIFIERS, but also per-tectly suitable for other makes. PRICE COMPLETE £6.6.0

RICE COMPLETE \$6.6.0 ASSEMBLED AND TESTED

TOF PARTS
Supplied strictly to MULLARD'S SPECIFICATION and incorporating:
Fqualisation for the latest R.L.A. characteristics.
Input for Crystal Pick-ups, and variable reluctance magnetic types.
Input (a) Direct from High Imp. Tape Head. (b) From a Tape Amplifier or Pre-amplifier.
Sensitive Microphone Channel. • Wide range BASS and TREBLE Controls.

COMPLETE MULLARD "5-10" AMPLIFIER

The popular and very successing complete "5-10" incorporating Control Unit providing up to 10 watts high quality reproduction. Only Specified Components and new MI LLARD VALSES are supplied including FARMEKO MAINS TRANSPORMERS and choice of the latest PARMEKO or PARTRIDGE ULTRA-Linear Output Transformers.

KIT OF S11.10.0 OR ASSEMBLED \$13.10.0 PARTS \$11.10.0 AND TESTED and TESTED TESTED TESTED AND THE STATE OF THE

COMPLETE MULLARD "3-3"

THE BEAL AMPLIFIER FOR A SMALL HIGH QUALITY INSTALLATION PROVIDING EXCELLENT REPRODUCTIONS OF TOO SWATTS OUTPUT COMPLETE KIT \$7.10.0 OR ASSEMBLED \$8.19.6 (plus 6/6 carriage and insurance) H.P. Terms: Deposit \$2.0.0 and 8 Months at \$1.0.0. Complete to MULLARD'S SPECIFICATION including Mullard valves and a PARMEKO OUTPUT TRANSFORMER.

SPECIAL CASH OFFER!!

This very attractive PORTABLE AM-PLIFIER CASE together with a good quality GRAM AMPLIFIER and a matched P.M. SPEAKER. ALL for ONLY 28.7.6 (Plus 7/6°Carr. & Ins.)

The Amplifier consists of a 2-stage design incorporating 3 modern B.V.A. valves and has separate BASS and TREBLE CONTROLS.

The Portable Case will also accommodate almost any make of Autochanger and is attractively infished in Mushroom Grey Rexine. WE ALSO SUPPLY SEPARATELY—(a) The 2-stage (plus Rectlier) AMPLIFIER \$4.2.6

(b) The PORTABLE CARRYING CASE £3.17.6

(c) 6iin. P.M. SPEAKER 18/9 Carriage and Insurance 4/- extra

RECORD PLAYERS THE LATEST MODELS ARE IN STOCK,
SEND S.A.E. FOR ILLUSTRATED LEAFLET
E.S.R. MONARCH UAS 4-speed mixer Autochanger
with Crysta Pick-up.
The NEW COLLARO MODEL RP594 4-speed Single
Record Player, Studio Cartridge.
The NEW COLLARO C69 4-speed Autochanger unit
with Studio "O" Pick-up.
The E.M. I. 4-speed Single Record Player with crystal
Pick-up.

26.9.6 £6.19.6 £9.18.9 £7.19.6 The E.M. I. 4-speed Single Record and UA14. Each a 4-speed mixer autochanger with Crystal Pick-up.
Bosh available incorporatins the B.S.R. STEREO \$1
Pick-up, plays L.P. and 78 Records.
GARRARD MODEL TA/Mkil 4-speed Player fitted high output Crystal Pick-up.
GARRARD MODEL RU/289. Autochanger 4-speeds. High output Crystal Pick-up.
Carriage and insurance on each above, 5/-extra. £6.9.6 £7.19.6 £10.10.0 £8.10.0 £8.19.6

109 FLEET ST., LONDON, Telephone: FLEET STREET

PRICE REDUCTIONS

PRICE REDUCTIONS

(a) The KIT OF PARTS to build both the "5-10" Main Amplifier and the 2-valve PRE-AMP CUN- £15.15.0

(b) The "5-10" and the 2-stage PRE-AMP LOT AND AMPLIFIER AND LOT AMPLIFIER AMPLIFIER CON- £21.10.0

(c) The KIT OF PARTS to build the DUAL-CHANNEL "3-3" AMPLIFIER and the DUAL-CHANNEL "3-3" AMPLIFIER AMPLIFIER AMPLIFIER CON- £21.10.0

(d) The DUAL-CHANNEL "3-3" AMPLIFIER AMPLIFIER AMPLIFIER CON- £21.10.0

(d) The DUAL-CHANNEL "3-3" AMPLIFIER AMPLIFIER AMPLIFIER CONTROL UNIT CON- £21.10.0

(d) The DUAL-CHANNEL "3-3" AMPLIFIER CONTROL UNIT CON- £21.10.0

(d) The CHANNEL "5-10" AMPLIFIER CONTROL UNIT CON- £25.00" MAIN CHANNEL and the DUAL-CHANNEL PRE- £21.10.0

(d) ONE "5-10" AMPLIFIER AND THE CONTROL UNIT CONT

H.P. Terms: Deposit £5, 12 months of £25.0.0
H.P. Terms: Deposit £5, 12 months of £1.16.8.
(g) KiT OF PARTS to build Two "5-10" MAIN AMPLIFIERS (Incorporating Parmeko Output Transformers) and the DUAL-CHANNEL PRE-AMPLIFIER CONTROL £31.0.0
UNIT
(h) TWO "5-10" AMPLIFIERS and the DUAL-CHANNEL PRE-AMPLIFIER CONTROL UNIT BOTH ASSEMBLED & TESTED £36.0.0
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STEREO PRE-AMPLIFIER

This model Incorporates two Mullard 2-valve Pre-Amplifiers combined



Terms: Deposit \$2.0.0

MULLARD'S SPECIFI
into a Single
unit enabling it to be used for both STEREO
PHONIC or MONAURAL operation. It
is designed primarily to operate with our range of MULLARD
MAIN AMPLIFIERS but will also operate equally well with any
make of Amplifiers requiring an input of 250 myolts.

COMPLETE KIT \$12.10.0 ASSEMBLED
ST. OF PARTS
H.P. £3 Dep. and 12 mths. at £1.2.0 MAIN

MULLARD FOUR CHANNEL MIXER UNIT

Self powered with Cachode lollower output. Incorporates Two inputs for MICROPHONES One for CRYSTAL PICK UP and a lourth for RADIO or TAPE.

0.8.83 Complete Kit of Parts Assembled and Tested £10.0.0



Assembled and rested 10.000 Assembled and rested 10.000 MoDEL I.L. one microphone input matched for moving coil or Ribbon Mike. £1.17.0 extra.

STEREO PRE-ANNOUNCEMENT

To meet the increasing demand for stereophonic sound equipment our Design Engineers are producing. STERFO TAPE PREAMPLIFIER for operation with the latest MINIFLUX and COLLARO

for operation with the latest MINIFLUX and COLLARO
thrack tape heads.
The Unit incorporates the latest circuitry, the design
being based on the very popular MULLARD TYPE "C"
Unit. and employs a sensitive meter for accurately setting
the record level. High-grade Tape Decks incorporating
the MINIFLUX Heads will be available and in keeping
with our normal practice will be offered with the Preamplifler. Full details and the assembled Preamplifler
will be available in September.

STERN'S INTER-COMM or BABY ALARM

STERN'S INTER-COMM OF BABY ALARM A small versatile unit employing the new MULLARD ECL88 valve and designed to provide two (or three) way conversation up to extreme distances. Operates from A.C. Mains 200 to 250 Volts and as in all our designs only new high grade and guaranteed. components are incorporated.

PRICES ... MAYFER UNIT and ONE EXTENSION KIT OF PARTS \$6.17.6 ASSEMBLED AND TESTED \$8.0.0 The equipment consists of a MASTER UNIT, size only 8½ x5½ x6ia. and ONE EXTENSION (a second extension may be added at any time). The Master Unit incorporates switching and power supply and with the chassis completely isolated from the mains in operated in absolute salety. Attractively presented in Cases covered in quality leatherette.

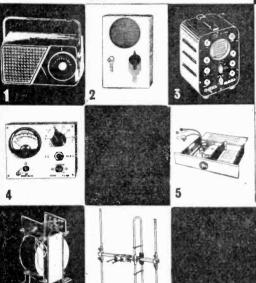
BENTLEY ACOUSTIC CORPORATION LTD.

38 CHALCOT ROAD, CHALK FARM, LONDON, N.W.I.

Telephone: PRIMROSE 9090

XPRE	SS	POSTAL TELEG	SER RAM	VICE	. A	LL OF	RDER	S DES	PATO	HED	SAMI	E DAY	AS CEP	RECE TED U	IVED.		EPHO	NE A	NE
			7/- 10 7/3 10	F9	11/6	35Z4G 35Z5G	T 9'-	DH76 DH77	51- 71-	EF41	15/-	HN309 HVR2	20/-	PL84 PL820	12/8 18/8	UAF42	916 X	(H(1.5)) 616
Z4			4/6 10	LDII I		43		DK32	12/-	EF42	10/6	HVR2A	8/6	PM84 PX4	17'7	UB41 UBC41		(SG(1.! ′63	5) 6/6
45 A7GT	12/-			P13	19/3	50C5 50CD60	10/-	DK91 DK92	6/6	EF50(#		KF35 KL35	8/6	PY31	16/7	UBC81		263	7/
:5	12/6	6F23 I	0/6 12	A6	5/.		36/6	DK96	8/6	EF54	5/-	KLL32		PY32	12/6	UBF80	91- Z	.66	17/
				AC6 AD6	15/3	50L6GT 53KU		DL33 DL66	17/6	EF73 EF80	10/6	KT2 KT33C	10%	PY80 PY81	7/6 8/6	UBF89 UBL21		77	61
SGT				AE6		77	81-	DL68	15/-	EF85	61-		29/10	PY82	71-	UCC84	14/7	.,,,	·
ŧ.	3/6	6G6 (AH7	8/-	78	616	DL72	15/-	EF86	10/6	KT41	23/3	PY83	8/6	UCC85		ransist	
OS NS				AH8	12/6	80	9/-	DL92 DL94	71-	EF89	91.	KT44 KT61	12/6	PY88 PZ30	13/3	UCF80 UCH21		nd dioc	71 71
SGT	10/6	616	5/6 12	AT7	61-	85A2	16/-	DL96	8/6	EF92	4/6	KT63	7/-	OP21	7/-	UCH42	9/6 C	CG4E	71
5				AU6	6/6	90AG 90AV	6716	DM70 E80F	30/-	EF97 EF98	13/3	KT66 KT88	15/-	QP25 QS150	14/6	UCL82		G6E G7E	71
				AV6	12/8	90CI	16/-	E83F	30/-	EF183	18/7	KTW61	616		10/6	UCL83	19/3 C	GIOE	7
5			6/- 12 0/6 12	AX7 BA6	7/6	90CG	37/6 13/6	EA50	9/6	EF184 EK32	12/6	KTW62 KTW63		R12 R18	9/-	UF41	9% G	6, 8	, 5,
21			6/6 12	BE6	91-	150B2	18/-	EA76 EABC	30 9/-	EL32	5/-	KTZ4I	8/-	RI9	19/11	UF80	10/6 C	DA70	3
				BH7	21/3	161	10/6	EAC91			12/6	KTZ63	7/6	RG1/2	40A	UF85 UF86		DA73 DA79	3
2				EI J5GT	30/-	185BT 304	33/2	EAF42 EB34	216	EL34 EL38	26/6	L63 MHL4	716	RK34	541-	UF89		0A81	3
5	10/6	6L6M	9/6 12	J7GT	916	305	10/6	EB4I	8/6	EL4I	91-	MHLD6		5130	22/6	UL41		DA86	4
6			7/6 12 3/- 12	K5 K7GT	17/11	807 956	7/6	EB91 EBC3	23/3	EL42 EL81	10/6	ML4 MS4B	23/3	SP4(7) SP41	14/6	UL44 UL46		DA91 DA95	3
4				K8GT		1821	16/7	EBC33	5/-	EL83	19/11	MU12/1	4 8/-	SP42	12/6	UL84	8/6 C	DA210	ĬĬ
5G T	9/6	6LD20 15		Q7G1	T 5/-	4033L	12/6	EBC41	8/6	EL84	13/11	N37 N78	23/3	SP61 SU25	3/6	UM4 UM34		DA211	20
	716		/11 12	SA7	8/6	5763 7193	12/6	EBC81	9/-	EL85 EL86	17/3	N108	23/3	T4I	91-	UM80	15/3 C	OC16	48
GY	17/6	6P28 2	6/6 12	SG7	71-	7475		EBFB3	13/11	EL91	5/-	N308	20/7	TDD4	12/6	URIC UU6	18/7 C	DC23	25
IG *	101-			SH7	8/6	9002 AC/PE	5/6	EBF89	29/6	EL95 EL820	18/7	N339 P61	3/6	TH233		UU7		C28	25
3.	6/6	6R7G	0/- 12	SK7	61-	5-pin	23/3	EBL21	23/3	EL822	19/-	PABC80	0	TP22	15/-	UU8	26/6 C	DC35	25
4G	9/11			SQ7	8/6	7-pin AC2PE	15/-	EBL31	23/3	EM34 EM71	23/3	PCC84	13/11	TP25	15/-	UU9 UYIN		DC44 DC45	10
	10/6	6SG7GT		Y4	10/6	DD	12/6	EC54	61-	EM80	91-	PCC85	916	TY86F	13/3	UY21	16/7 C	C65	22
8	91-	6SH7GT	8/- 14		27/10	AC6PE		EC70	12/6	EM81	10/6	PCC88	18/-	U12/14	4 8/6	UY41 UY85		DC66	25
C7 G5	514			AQ5	10/6	AC/TP ATP4	33/2	ECC32	13/3	EM84 EM85	17/3	PCF80	8/-	U18/20		VMP4G		DC71	6
Ğ7	7/6	6SL7GT	6/6 20	DI	15/3	AZI	18/7	ECC33	8/6	EN31	53/-	PCF82	10/6	U19	361-	VMS4B	15/- C	DC72	. 8
K5	8/-		5/6 20 9/- 20)F2	26/6	AZ31 AZ41	13/11	ECC35		EY51 EY83	16/7	PCF84 PCF86	16/7	U22 U24	29/10	VP2 VP4		DC73	16
M6	416		8/- 20		26/6	B36	15/-	ECC40	23/3	EY84	14/-	PCL82	10/-	U25	17/11	VP2B	14/6 C	C77	15
Q5	7/6			P3	23/3	BL63	7/6	ECC81		EY86 EZ35	91-	PCL83	10/6	U26	9/6	VP4B VP13C		OC78	8
16 U6	10/-)P4)P5	26/6	cic	12/6	ECC8		EZ40	71-	PCL85	16/7	U33	26/6	VP23		C170	13
V6	12/8	6V6G	71- 25	A6G	10/6	CBLI	26/6	ECC84	91-	EZ4I	7/-	PCL86	16/7	U35	26/6	VP41		OC171	14
8 A6	5/- 7/4		8/- 25	YSG	10/-	CBL31		ECC85	8/6	EZ80	71-	PENA4 PENB4		U37	26/6	VR105 VR150		OC200	
E6	61-	6X5GT	61. 25	74G	916	CK 506	6/6	ECC91	5/6	FC4	15/-	PEN4D	D	U45	9/-	VT61A	5/- C	OCP71	29
G6G	23/3	6/30L2 I	0/- 25 2/6 25	Z5	916	CV63	19/3	ECF80	10/6	FW 4/8		PEN25	26/6	U50	6/6	VT501 W76		112	40
6	61-	786 2	1/3 27	'SU	19/11	CYI	18/7	ECF86	19/11	GU50	27/6	PEN40	OD	U54	19/11	WIBW	6/- T	13	50
	15/-		8/6 28 8/ ₂ 30		71-	CY3I	11/-	ECH3	26/6	GZ30	10/-	PEN44	25/-	U76	5/-	W 107		PI P2	40
R7	12/6	7C5 7C6	8/- 30)CI	6/-	DI DIS	10/6	ECH3		GZ32 GZ33	19/11	PEN 45	19/6	U107	16/7	X24M		SI	10
W6	8/6	7H7	8/- 30	FLI	40/-	D77	41-	ECH4	91-	GZ34	14/-	PEN46	7/6	U191	16/7	X41 X61(C)		TS2 TS3	12
W7	5/-		2/6 30 9/6 30)L (11/6	DAC32 DAF91	6/-	ECH8		GZ37 H63	19/11	PEN 383		U201	14/-	X61(C)		S4	24
Š	616	777	8/6 30)P4	12/-	DAF96	8/6	ECL80	91-	HABC	80		33/2	U281	19/11	X65		/30/10	
9				P12	716	DD41 DET25	13/11	ECL82		HL2	13/6	PEN/DI	33/2	U282	22/7	X66 X76M		KAIOI KAIOZ	20
10	91-	8D3	4/6 30	PLI	10/6	DF33	10/6	ECL86	16/7	HL23	15/3	PL33	19/3	U329	14/-	X78	23/3 ×	KA103	- 19
D6G	36/6	9BW6 1	5/3 30	PL13		DF66	15/-	EF9 EF22	23/3	HL230	D 7/6	PL36 PL38	12/- 26/6	U339 U403	16'7	X79 X109	23/3 X	KA104 KB102	18
H6 6	616	,	4/- 35 3/- 35	A5 L6GT	21/3	DF94	8/6	EF36	4/-	HL410	19/3	PL38	10/6	U404	8/6	XD(1.5		KB102	i i
5	12/6	10C2 2	6/6 35	W4	716	DF97	9:-	EF37A	8/-	HL420	OD	PL82	7/6	U801	29/10	XFGI	18/- >		10
	26'6	DS BRAN	2/- 35	Z3	10/6	DH63	6/6	EF39	5/6	VEDC!	C11A	PL83	9/-	U4020	16/7	XFY12	7'0 7	KC101	NO
LG	50	DS BRAN	DINE	SELL	. SEC	ONDE	INAL	600	DDS C	OR MA	NUF	ACTU	RERS	REJE	CTS.				
1		CONTRO				13/ 1 -						ull List w	ith rai				ISRA 1	1-1-14	1 4
with	n Lo	Switch, 4/6	e and	DE	RMIB RM2B		M-1 M-2	5/3 7/6	14A86 14A97	17/6	14B1		11/6	(FC	31)		(FCI	16)	
		.50 K	100 K	DR	RM3B	15/6 R	M-3	7/9	14A10	0 271-	14RA	1-2-8-2	17/6	16RD	2-2-8-	1 12/-	ISRA I	1-2-8-1	
	- N	I meg. 2		LLV			M-4 M-5	19/6	14A12	4 28/-	I GRC	1-1-16-1	8/6	IBRA	2-1-8-1	4/6	IBRD 2		15
K :	me		ET S	LIC	ON F	RECTIF	IERS.	OUT	PUT	120 V	OLTS	AT A	MP.	TWO	IN SI				LT
K :	mg.	T. MIDG	E 1 31		AT I			MINUE	W ILL		VESI	JI UK.	10.0	-wen					
mg. 1	o U T	T. MIDG		A	ELE	CTRO	LYTIC		IDEN	SERS			ended	tubular	r	8 x 8	mfd., 45	50 v.	3
mg. 1 UST (o U T	T. MIDG		A 50 x 2	ELE 250 mf	CTRO	LYTIC	100	NDEN rfd., 27		41-	8-mfd.	450	٧.	1/9	16 x 1	6 mfd.,	450 v.	. 4
Sta x8x x32	andar 8 mfd.	rd Can d., 500 v. 4 , 450 v. 5	1/- 6	60 x 2 100x4	ELE 250 mí 00 mís	CTRO d., 275 v d., 275 v	LYTIC 1. 9/6 1. 12/6	200 m	ıfd., 27	5 v.	41-	8-mfd.	450 , 450	v. v.	1/9 2/9 3/9	16 x 1 32 x 3	mfd., 45 6 mfd., 2 mfd., 6 mfd.,	450 v. 350 v.	. 4
Str × 8 x x 32 x 120	andar 8 mfd. 0 mfd.	T. MIDG	/- 6 /9 6 /3	60 x 2 100x40 100 m	ELE 250 mi 00 mid id., 27	CTROI d., 275 v d., 275 v	. 9/6 . 12/6 . 3/-	200 m	16d., 27	5 v. 1., 275 v	O.D.	8-mid. 16 mid 32 mid	450 1., 450 1., 450	v. v. v. all List	1/9 2/9 3/9	16 x 1 32 x 3 8 x 1	6 mfd., 2 mfd., 6 mfd., of Bu	450 v. 350 v. 450 v.	3

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TRANSISTOR POCKET RADIO with MINIATURE SPEAKER, FERRITE

1. 3-TRANSISTOR POCKET RADIO with MINIATURE SPEAKER, FERRITE ROD, and 2 GERMANIUM DIODES. The only 3 transistor radio available at the price. Build it in I evening! Tunable over M/L waves. Complete with easy-to-follow instructions and all components (less batteries obtainable any-to-follow instructions and all components (less batteries obtainable any-to-follow instructions and all components (less batteries obtainable any-to-follow instructions and all components (less batteries obtainable any-to-follow) instructions and all components (less batteries obtainable any-to-follow) instructions and instruction and instruc

with kit:
CHANNEL TINER. Will tune to all Band I and Band III stations. Complete with P.C.C.84 and P.C.F.80 valves (in series) I.F. 16-19 or 33-38. Can be modified as an aerial converter (instructions supplied). 32/6, plus 3/6 P. & P. HEATER TRANSFORMERS. to suit above. 200-200 v., 6/-, plus 1/6 P. & P. MAINS TRANSFORMERS. All with tapped primaries, 200-250 volts, 0-160 180. 200 v., 60 m.A. 63. v. 2 anpp. 10/6. 300-2-350 v., 70 m.A. 63. v. 1 amp. 6.3 v. 2 amp. 10/6. 250-250 v. 70 m.A. 6.3 v. 2 amp. 10/6. P. & P. 3/-280-2804 v. 70 m.A. 63. v. 2 amp. 10/6. P. & P. 3/-280-2804 v. 70 m.A. 63. v. 2 amp. 10/6. P. & P. 3/-280-2804 v. 70 m.A. 63. v. 2 amp. 10/6. P. & P. 3/-280-2804 v. 70 m.A. 63. v. 1.0 f. p. & p. 3/-280-2804 v. 70 m.A. 63. v. 1.0 f. p. & p. 3/-280-280 v. 70 m.A. 63. v. 1.0 f. p. & p. 3/-280-280 v. 1.0 f. p. 3/-280-280 v. 1

7. WOLSEY 3-ELEMENT FOLDED DIPOLE. 1.T.V. Aerial less mounting bracket for external use, complete with 12 yds. of coarial cable, 15/r. P. & P. 3/6.
9. SIGNAL GENERATORS. Cash 26.19.6 or 25/- deposit and 6 monthly payments of 21/6. P. & P. 5/r. Coverage 100 kc/s to 100 Mc/s on fundamentals and 100 Mc/s to 200 Mc/s on barmonics. Case 10 x 6/g x 5/m. Three miniature valves and Mctal Rectifier. A.C. mains 200/260 v. Internal modulation of 400 c.p.s. to a depth of 30 per cent; Modulated cummodulated R.F. output continuously variable 100 millivolts. C.W. and mod switch, variable A.F. output. Magic eye as output indicator. Accuracy ± 2 per cent.

10. SIGNAL GENERATORS. Cash \$4,19.6 or 25/- deposit and 4 monthly payments of \$21/6, P. & P. 5/-. Coverage 120 ke/s to 84 Mc/s. Case 10 x 0½ x 4½lin. Size of scale 6½ x 3½in. 2 valves and rectlifier. A.C. mains 230-250 v. Internal modulation of 400 c.p.s. to a depth of 30 per cent, modulated or numodulated R.F. output continuously variable 100 millivolts. C.W. and mod. switch variable A.F. output and moving coil output meter. Accuracy. A 20 sec. and c. 20 sec. and Accuracy ± 2 per cent.

BATTERY RECORD PLAYER AND AMPLIFIER. 45 r.p.m. "Star" motor "Acos" crystal pick-up. 3 transistor push-pull amplifier complete with transistors. Output 500 milli wasts, 49/6. P. & P. 5/6.

12. 8-watt PUSH-PULL 5 VALVE AMPLIFIER. A.C. mains 200-260 v. Size 10½ v. 6½ v. 2½ln. 5 valves. For use with all makes and type of pick-up and milke. Negative feed back. Two inputs, mike and grain, and controls for same. Separate controls for Bass and Treble lift. Response flat from 40 vycles to 15 kc/s. ½ db; 4 db down to 20 kc/s. Output 8 watts 45 per cent total distortion. Noise level 40 db down all hum. Output transformer tapped for 3 and 15 olims speech coils. For use with 81d or f..P. records, musical instruments such as guitars, etc. Suitable for small halls, £3.19.6, P. & P. 6/6. Crystal mike to suit 15/-, P. & P. 1/6. Sin. P.M. Speaker to suit 12/6, P. & P. 1/6.

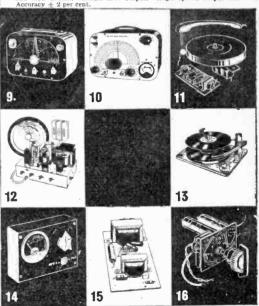
13. B.S.R. MONARCH UAS WITH FUL-FI HEAD. 4-speed, plays 10 records, 12in., 10in., or 7in. at 16, 33, 49 or 78 r.p.m. Intermixes 7in., 10in. and 12in. records of the same speed. Has manual play position: colour, brown. Dimensions: 12\frac{1}{2} \times 10\frac{1}{2} \times \text{Plus}. Space required above baseboard 4\frac{1}{2} \times \text{Plus}. Pittled with \text{Pul-Fit turnover crystal head. £6.19.6, P. & P. 6/-With Stereo Head £7.19.6, P. & P. 6/-

14. TRANSISTOR TESTER. For both P.N.P. and N.P.N. transistors incorporating moving coli meter. In metal case, size 4½ x 3½ x 1½n. Scale marked in gain and leakage. 19/6, P. & P. 2/6.

15. PUSH-PULL OUTPUT STAGE inclusive of transistors with input and output transformers to match 3 ohms speech coil, suitable for use with the POCKET RADIO. Kit of parts, including transistors. 19/8, P. & P. 1/6. Wiring diagram 1/6, free with kit.

PORTABLE AMPLIFIER. On printed circuit for A.C. Mains 200/250 v. Size 4 x 3in. with tone and volume control. Valves: ECLS2 and EZSO. 3946, P. & P. 2/0.

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REALISM AT INCREDIBLY LOW CONT, CAN BE ASSEMBLED IN HALF AN HOUR The Recorder incorporates the Latest Collaro Studio Tape Transcriptor. The Linear LT45X High Quality Tape Amplifier listed \$12.120 High Flux P.M. Speaker listed \$20.- empt Jape Spool, a Reei of Best quality Tape listed \$20.6 and a Handsome Portable carrying Cabinet with latest attractive two-tone polyedrome finish, size 18 x 13 x 91n. high, listed \$4.10.0 and circuit. Total cost if purchased individually approximately \$40. Performance equal to units in the £30.£80 class. S.A.E for leaflet.

HIGH FIDELITY 12-14 WATT AMPLIFIER TYPE A11

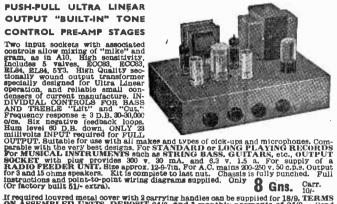
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If required louvred metal cover with 2 carrying handles can be supplied for 18/9, TERMS ON ASSEMBLED UNITS. DEPOSIT 24/9, and 3 monthly payments of 24/9. Send 8.A.E. for illustrated leaflet detailing Ready-to-assemble Cabinets, Speakers. Microphones, etc., with cash and credit terms.

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A complete set of parts for the construction of a stereophonic amplifier giving 5 watts high quality output on each channel (total 10 watts). Sensitivity is 50 millivolts, suitable for all crystal stereo heads, Ganged Bass and Treble Controls give equal variation of "lift" and "cur". Provision is made for use as straight (monaural) 10 watt amplifier. Valve line-up ECCSS, ECC, and the straight of the control of the control



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H.P. TERMS. Deposit 25.7.6 and 12 monthly payments of 2 gns. Cash price it settled in 3 months.

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ASSEMBLED
OF 12 v. 4 amps.

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OF 12 v. 4 amps.

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OF 12 v. 0r 12 v. 2 amps.

Settled Ammeter and

ASSEMBLED
OF 12 v. 0r 12 v. 2 amps.

Settled Ammeter and

ASSEMBLED
OF 12 v. 0r 12 v. 2 amps.

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for Mullard 510 Amplifier 29/9
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	5/6
Push-Puli 10-12 watts 6V6 to 30 or	0,0
150	9/0
Push-Pull 19-12 watts to match 6V6	310
50 3-5-8 or 15 Ω 1	010
Durch Durch Pit Control of the Contr	
Push-Pull EL84 to 3 or 150 1	8/8
Push-Pull 15-18: watts, 6L6, KT66 2	2/9
Push-Pull for Mullard 510 Ultra	
	9/9
Push-Pull 20 watts, sectionally	0,0
wound 6L6. KT66 etc., to 3 to 15Ω 4	010
WOULD OLD, KI 00 600, 600 to 1015 , . 4	010
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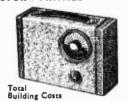
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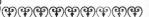
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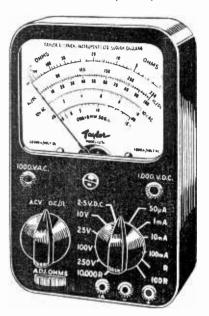
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A kit of ready-built units only requiring interconnection. Comprising two midget 3W amplifiers, push-button switch, transformer, control unit (bass, treble and former, control unit (bass, treble and vol.), power pack, one speaker (second speaker 14'6 extra), indicator light, valves (ECL82, EZ80 range), and comprehensive instructions. 5916 plus 6'6.

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AZ31 10/- DAF96 8/- DF96 8/- HL23DD 8/6 DK96 8/- HL23D 8/- HL23D 8/- DK96 8			•					
AZ31 10/- DAF96 8/- DAF96 8/- DK96 8/- DK96 8/- HL42DD 8/6 DS96 8/- HL42DD 10/- EABC80 9/- EAF42 9/6 EBG13 5/- EB91 4/6 KT336 6/- EB91 4/6 KT61 10/- EBBC3 5/- KTW61 6/6 EBC33 6/9 MX40 12/6 ITA 5/6 EBR03 9/9 PCC84 12/- EBR80 9/9 PCC85 8/6 BBC31 6/6 EBC33 6/9 PCC85 8/6 BBC41 8/9 DC4 4/6 BBC41 8/9 DC4 4/6 BBC41 8/9 DC4 4/6 BBC41 8/9 DC4 4/6 BBC31 6/6 EBC33 6/9 PCC85 8/6 BBC33 6/9 PCC85 8/6 BBC41 8/9 DC4 4/6 BBC41 8/9 BC682 9/9 BC683 9/9 BC683 9/9 BC7 8/6 BC683 9/9 BC7 8/6 BC683 9/9 BC7 8/6 BC7 10/6		10/-1						
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Practical Wireless

VOL. XXXVII No. 655 SEPTEMBER, 1961

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BLUEPRINTS FREE MORE

NCLUDED with each copy of our next issue, will be a blueprint for our new receiver-the P.W. Tutor. As its name implies, it is designed essentially for the beginner, although it will also be found instructive for those who have not built a radio set for some time. The great success of our previous series for the beginner—The Beginner's Constructional Course and others—shows that there is a real need for this type of apparatus. Young people are continually leaving school and entering the radio field, and wish to add to any knowledge they may have gained at school, with practical work, which at the same time, will introduce them to new aspects of construction.

It is natural that the beginner will need to start from the very simplest point which means the crystal receiver, but the transistor must also be employed as this is becoming more and more to be accepted in place of the valve. Printed circuits are, of course, very widely used to-day, but it was felt that it would be rather too involved to try and use these in a receiver of the progressive kind, so the technique of utilising standard tag-boards has been adopted, and the receiver is built on these. The constructor goes from stage to stage, gradually adding parts and so advancing the design of each set.

NOVEMBER AND DECEMBER BLUEPRINTS

In the November and December issues, further free blueprints will enable more additions to be made to the preceding receivers. Included in the second and third blueprints will be a transistor battery superhet tuner together with its amplifier, which will also be suitable for a battery operated record player.

The blueprints will be such that the stages of construction are complete in themselves and each reader will be able to choose a design to suit his pocket and requirements.

INCREASED PRICE

The steadily increasing costs of production, paper, and other materials have made it necessary to increase the price of this magazine from the October issue-or to reduce it in size. We know that the latter procedure would not meet with approval and that most readers would rather pay an increased price than buy a smaller edition of PRACTICAL WIRELESS.

We shall, of course, keep up the same high standard of articles and endeavour to make each issue appeal to the widest possible circle of readers-catering both for the absolute beginner, as in the blueprint mentioned in the above paragraphs, as well as the advanced constructor and amateur transmitter. Blueprints in later issues will be designed for more experienced readers and we shall continue to provide the maximum service not only to individuals, but also to clubs and societies. From the October issue, therefore, the price of PRACTICAL WIRELESS will be increased to 2/-.

The October issue of PRACTICAL WIRELESS is published on September 7th-order your copy now and be sure of obtaining the first of the free blueprints.

TADAK LASTALIK KAPATAN KARANCAN PANGKAN PANGKAS PANGKAS PANGKAN PA

Our next issue, dated October, will be published on September 7th.

Round the World of Wireless

POTENTIAL AND CURRENT NEWS

Broadcast Receiving Licences

THE following statement shows the approximate number of Broadcast Receiving Licences in force at the end of May, 1961, in respect of wireless receiving stations situated within the various Postal Regions of England, Wales, Scotland and Northern Ireland. The numbers include Licences issued to blind persons without payment.

Region London Postal Home Counties Midland North Eastern North Western South Western Wales and Border (Countil	es	Total	
Total England and Scotland Northern Ireland	Wales	::	3.372,460 376,605 117,560	
Grand Total	••		3,866,625	

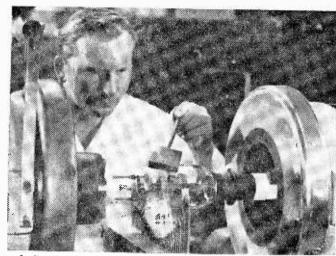
Tape Recorder Company Interests Change Hands

A WHOLLY-OWNED subsidiary of Multicore Solders Limited, Multimusic Limited, announces that it has disposed of all its interests in Reflectograph Tape Recorders to Pamphonic Reproducers Limited, a Pye Group Company. Pamphonic are now responsible for all service of Reflectograph recorders. Enquiries from the public concerning Reflectograph recorders should now be directed to Pamphonic Reproducers Limited at 17 Stratton Street, London, W.1.

Expansion at Valve and Capacitor Factory

A FURTHER expansion programme for the production and marketing of new and present types of valves and capacitors has recently been started by Standard Telephones and Cables Limited.

Manufacture of both these product lines is at the modern S.T.C. factory in Paignton, Devon. In the Valve Division plant, the principal products are valves for use in telecommunication systems, such as microwave radio links and transoccanic telephone cables.



Sealing the glass envelope of a water-cooled power triode, at the S.T.C. factory at Paignton, Devon.

Expansion is envisaged in the production and application of many types of valve.

many types of valve.

Capacitors, like valves, have been key products of S.T.C. for many years and were formerly made mainly at North Woolwich, London, with a satellite plant at Treforest in Wales. The success of the Valve Division operations led to the building of a second factory for the manufacture of capacitors.

Multi-channel Radio Telephone System for British Railways

As part of the British Railways modernisation programme, its north-eastern region is to be equipped with a high-frequency nulti-channel radio telephone system between York and Newcastle, via Darlington—a distance of 78 miles. This will be the first such installation to be used by British Railways.

The radio equipment is to be supplied and installed by Marconi's Wireless Telegraph Co. Ltd., and the carrier equipment by Automatic Telephone and Electric Co. Ltd. The system is designed for a maximum capacity of 300 telephone channels, but initially 180 will be in operation. It will handle the telephone traffic between the regional centres, with full facilities for through subscriber trunk dialling.

The installation is duplicated to operate on a main-standby basis, with automatic changeover in the event of failure. In this connection, particular features of the equipment are the relatively low number of valves used and the simplicity of the R.F. transmission circuits, which employ one microwave klystron per unit equipment, both factors which greatly reduce the probability of equipment failure. The telephone channelling equipment is of the latest design, using transistors throughout and printed wiring cards for mounting all components.

Radio and Television Exhibition

THE Radio and Television Exhibition of France will be held this year from September 14th to 26th in Paris—Porte de Versailles. It will be situated in the Parc des Expositions—Halls 101 to 110. This exhibition is undertaken by the Radiodiffusion Télévision Française and by the Fédération Nationale des Industries Electroniques.

The exhibition, which covers all fields of radio and television, is open to all foreign visitors but is for French exhibitors only. The utilization of the "Palais des Sports" enables the organizers to receive the largest audience in conditions of comfort. A studio

with 1,000 seats for broadcasting lyrical and dramatic programmes, and high fidelity demonstrations will be included in the exhibition.

Minicabs Radiotelephone System

WITH the opening of the London minicab scheme, Pye Telecommunications put into operation, for Welbeck Motors, a radiotelephone system which operates 200 radiotaxis initially, expanding to 800 by the end of the year.

The system with six-channel radiotelephone equipment is installed under the dashboard of each car and gives communication over a radius of 20 to 25 miles of Piccadilly Circus. A special control room has a conveyor-belt message system designed to handle calls at the rate of one every two seconds.

V.H.F. Unit for Lifeboat

THE President of the Dieppe Lifeboat Committee has been presented with a Pye International marine radiotelephone by the French National Railway.

This is the first French national lifeboat to be equipped with V.H.F. radio. It will work into the Dieppe railway radio station and the local public correspondence scheme. The lifeboat will thus be able to communicate with cross-channel steamers, with local fishing boats, which have the requisite equipment, and with the Boulogne Sur Mer Radio Station.

Mobile Microwave System

THE United States Government has recently placed a contract with Marconi's Wireless Telegraph Co. Ltd., for the supply of a mobile microwave telephone and telegraph communication system to link many of the United States Air Force bases in the U.K. Marconi's and the Automatic Telephone and Electric Co. Ltd., who are also involved in the contract, are currently fulfilling this three-and-a-half million dollar agreement.

The Marconi radio equipment and the Automatic Telephone and Electric telephone carrier equipment is housed in semi-trailer air-conditioned vehicles. Inside these large vehicles the transmitter, receiver and supervisory equipment are each contained in racks arranged for easy accessibility by the operators.

Naval Plotting System

MOST of the Western nations were represented at a recent demonstration of a new naval automatic plotting system—developed by E.M.I. Electronics Ltd.—given on board H.M.S. Rhyl, one of Britain's latest antisubmarine frigates. The system constitutes a big advance in plotting the positions of other craft in the vicinity, and is of particular use when hunting fast submarines. It is also of great value for coastal navigation.

In ships fitted with this system, the former method of manual plotting and the reporting of bearings and ranges over an intercom network has been replaced by E.M.I.'s electronic equipment, which produces much quicker and more accurate results.

Radio Paging System

PHILLIP W. HOLLAND, M.P. for Acton Constituency, visited the Ultra Electronics factory at Western Avenue, Acton, recently to inspect their radio paging system.

He became interested in this equipment when he saw it at the Crime Prevention Exhibition organised recently at Acton Town Hall, by the local police authorities.

Mr. Holland has a question tabled to the Secretary of State regarding the use of such equip-

ment by the policeman on the beat.

Moscow Exhibition

THE Council of the Scientific Instrument Manufacturers' Association of Great Britain states that its 19 members who took part in the combined stand at the recent British Industries Fair in Moscow are very well pleased with the results.

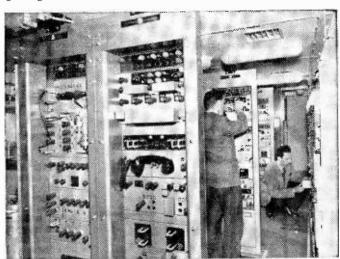
Firm contracts have been signed for 75 per cent. of their exhibits. Preliminary contracts for a considerable additional quantity of equipment to be exported immediately or in the near future have also been placed.

Cable Across The Thames

A £100,000 contract from the South Eastern Electricity Board to reinforce the electricity distribution system between substations at West Weybridge in Surrey, and Laleham in Middlesex, has been awarded to Associated Electrical Industries Limited.

The project will involve laying four miles of 33kV oil-filled cable and associated pilot cables. They will be taken across the River Thames in buried pipes. Two canal crossings are also involved.

The work will be carried out by AEI Construction (Cables and Lines) Division and will begin in July. The cable will be of AEI manufacture, from AEI Cable Division's Gravesend factory.



The interior of one of the vehicles which Marconi are supplying to the U.S. Air Force. The rack on the extreme left houses the transmitter, the middle rack the receiver, and the right-hand rack contains the supervisory equipment.

20c/s TO 200kc/s ON FUNDA-MENTALS WITH LOW DIS-TORTION AND STABLE OUT-PUT LEVEL

HERE are four problems involved in the design of a variable low frequency signal generator: stability, waveform, frequency range, and output level characteristics. Of the three main audio oscillator circuits, the beatfrequency oscillator is suitable for general purpose applications. especially where a wide frequency range is required with a single tuning control. It has, however, several serious drawbacks, includ-ing lack of stability, bad waveform at low frequencies, and R.F. in the output. These disadvantages may all be overcome by careful design, but the resulting instrument is very large and very expensive.

The conventional L-C oscillator

is ideal for single frequency operation but requires an impos-

sibly large tuning capacitor to produce the lowest ranges of a variable oscillator. In addition to this, it is difficult to obtain a frequency coverage greater than 3: 1 in each band, which means that 7 ranges are necessary to cover the audio spectrum of 20-20,000c/s.

The R-C oscillator, however, easily achieves a coverage of 10: 1, reducing the number of ranges to three. It has the further advantage that the basic circuit satisfies the four design problems set out above. The R-C circuit has therefore been chosen for this design.

The R-C circuit

The basic circuit is shown in Fig. 1. It consists of an amplifier back-coupled through a Wein bridge. The bridge is made up of the resistors

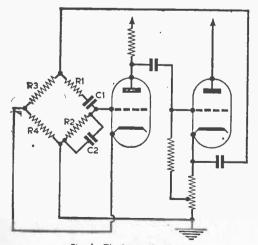
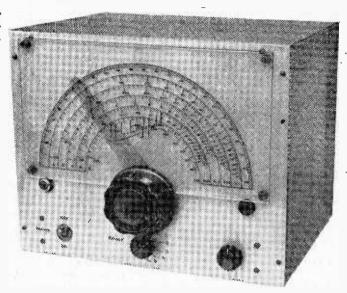


Fig. 1. The basic circuit.



WIDE-RANGE **AUDIO** OSCILLATOR

By R. C. Englefield

R1-R4 and the capacitors C1-C2, with the input and output of the amplifier connected to the diagonal points. By this means, both positive and negative feedback are applied to the amplifier. The circuit oscillates at the balance frequency of the bridge. The negative feedback, through RIC1 and R2C2 determines the frequency, given by

$$f = \frac{1}{2\pi \sqrt{(C1. C2. R1. R2.)}}$$

The positive feedback, through R3 and R4, stabilises the level of the oscillation.

Since the input and output impedances of the amplifier are not directly connected across the arms of the frequency discriminating network, the amplifier characteristics have no effect on the oscillator frequency.

In order to stabilise the amplitude of the oscillation with change of frequency, the attenuation of the negative feedback network must be kept constant, that is, the ratios R1/R2 and C1/C2 must be constant. The frequency of the oscillation may be adjusted by alteration of either pair of these components, and in this design, continuous frequency variation is achieved by varying the capacitances, different ranges being selected by

variation of the resistances. A much higher degree

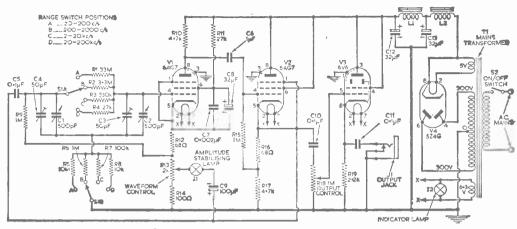


Fig. 2.—The complete practical circuit diagram.

of amplitude stability can be obtained by substituting a metal filament lamp for the resistor R3. Thus when the amplitude of the oscillation falls, the positive feedback current decreases, so reducing the resistance of the lamp—this in turn increases the positive feedback and compensates for the original drop in amplitude.

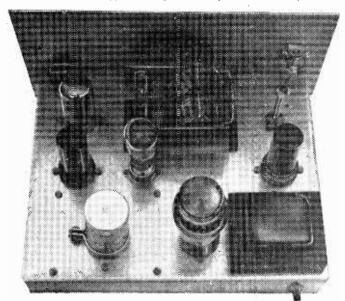
The practical circuit

A complete bridge-stabilised circuit is shown in Fig. 2. The first two stages are based on the circuit of Fig. 1, with the addition of the 15W 240V lamp, 11, and range switching. The tuning capacitor is a standard two-gang capacitor with trimmers, and the resistors R1-R8 are low temperature-coefficient types, though ordinary resis-

tors should prove satisfactory in use. The range resistors are best mounted on a ceramic switch.

The output of the oscillator is fed to the grid of a cathode follower, and the output from the unit is taken from a shorting-type microphone jack. If the oscillator is required to work into load impedances lower than 20k, it will be necessary to substitute a 25 µF capacitor in place of C11, if excessive loss of voltage is to be avoided at very low frequencies.

The power section is a conventional full-wave circuit, and generous smoothing arrangements are used, with the result that the hum level of the output is less than 0-2per cent of the maximum output voltage. Screened wire should be used for the wiring of the heaters and panel lamp.



Rear view of the oscillator.

Construction

Construction is simple straightforward. The tuning capacitor is insulated from the chassis with a sheet of Paxolin, and carries the pointer; slow motion tuning is employed, a simple frictional drive being easy to make and perfectly satisfactory. The range switch is mounted beneath the tuning control, and selects the following ranges: 20 to 200c/s (A) 200 to 2000c/s (B) 2 to 20ke/s (C) 20 to 200ke/s (D), The range can be extended up to IMc/s if necessary by using a 2.2k resistor and a 6800 resistor, mounted on a lifth pole of the range switch. A continuously variable output control, the output socket, the main switch, and the indicator lamp complete the panel items.

The scale is made from Perspex sheet, mounted in front of the pointer; the calibrations are drawn in Indian ink on the back of the Perspex this type of scale being very durable, and has the advantage that errors can be corrected without trace by removing the ink with

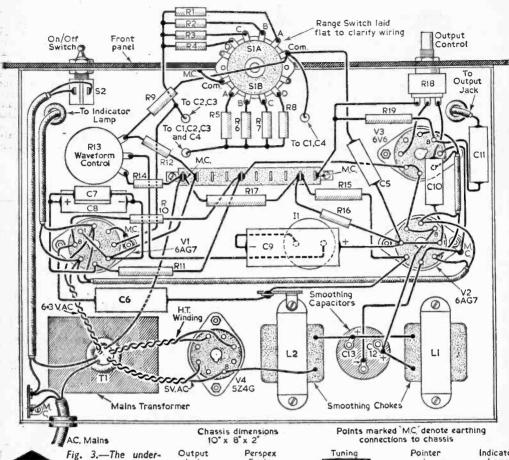


diagram.

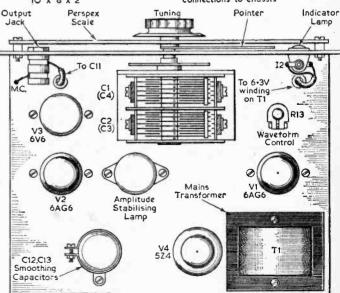
the finger-nail. The whole unit is contained in a case made from perforated zinc.

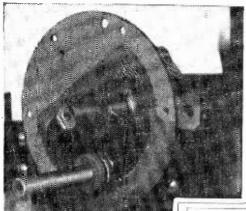
chassis wiring

Calibration

An oscilloscope is essential for the accurate calibration of the instrument. Two preliminary adjustments are necessary: first, feed the output of the oscillator into the 'scope, and adjust R13 until a good sine-wave is obtained—this circuit gives an exceptionally low distortion, less than 0.5per cent at all frequencies. Second, set the trimmers C3 and C4 to maximum capacity, and find the 200c/s point in range A, using the 50c/s mains supply as standard; then adjust the trimmers a

Fig. 4.—The above-chassis layout.





By connecting the 'scope to display Lissajoua figures, using 50e/s mains as standard, ranges A and B can now be calibrated; points should be logged every 5e/s in range A, and every 50e/s in range B. To calibrate range C, set the internal timebase of the 'scope to 500e/s, again using the mains as standard, and log points every 50e/s throughout the range—it is recommended that the sweep frequency be checked directly after each calibration is taken. Lissajous figures may again be used to calibrate range D if a 100kc/s quartz crystal standard or other ultra-stable oscillator is available, but if not, points can be accurately obtained by beating the harmonics of the oscil-

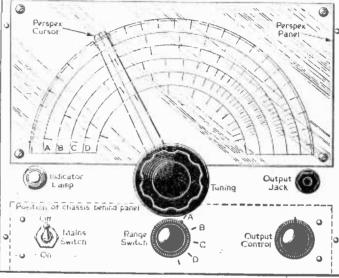
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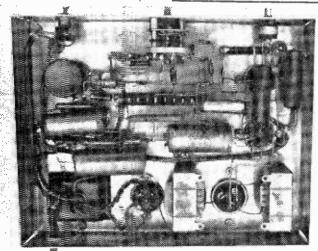
The tuning drive mechanism.

little af a time, keeping their capacities about equal, until the 200c/s point is just at the end of the range. This sets the high end of all four ranges.

Before commencing the calibration proper, remove the Perspex dial and construct a logging scale on the surface nearest to the pointer: this scale should have as large a radius as the length of the pointer will simplify the division of the circumference into 180 parts, but if this is not available, then a scale of divisions (say 256) may be constructed by continuous bisection of a 300°—this is best drawn out on paper first, and then transferred to the Perspex.

Fig. 5.—The front panel.





lator against the carrier waves of broadcasting stations, especially in the Long-wave band.

The scale may now be removed, and the dial calibrated directly in terms of frequency: further points may be obtained if necessary by graphical means; if any marks are nisplaced, they can easily be corrected as explained.

The overall performance of this instrument is more than adequate for ordinary testing: the output is inherently stable in frequency and level, and the hum level and distortion are especially low. These advantages more than offset the slight disadvantage that range-switching is necessary to cover the andio spectrum.

An underchassis view.

ANY amateurs have made up an R.F. generator and then found that the greatest difficulty, often insuperable, has been accurate calibration.

Details will be given of methods of calibration using broadcast stations as standards, but it is so simple to build a standard crystal oscillator that it is proposed to deal with the construction of a simple unit as part of this instrument.

The author housed the crystal check unit in the same case as the other chassis, but it could be kept separate and only plugged in or connected when required. Valves from the variable audio oscillator could be "borrowed" for this, but it is better to have two kept for use in the unit alone.

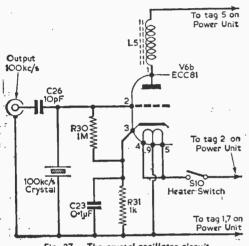


Fig. 27.—The crystal oscillator circuit.

BUILDING CHASSIS No. 4— THE CRYSTAL CHECK OSCILLATOR

(Continued from page 306 of the August issue)

By E. V. King

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.1%

THE P.W. SIGNAL GENERATOR

How it works

Valves V6a and V7a (Fig. 28) function as another oscillator, a multi-vibrator (working at 10kc/s), but the frequency is very unstable and therefore a synchronising signal is fed from the crystal controlled oscillator.

The actual frequency of 10kc/s is set by using the pre-set variable resistance VR5 which corrects for slight variations in component values. Switch S11 is used to control this 10kc/s oscillator—when S11 is "open", the oscillator is switched off. The resistor R37a, which is wired across the switch, is to ensure that some H.T. current is always

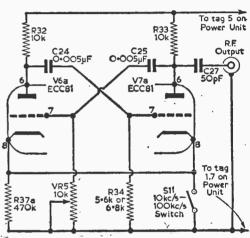


Fig. 28.—The circuit of the multivibrator.

passing through the valves V6a and V6b—if the valves were operated for long periods without H.T., the cathodes would become "poisoned" and the circuit would no longer operate.

Switch S10 is used to switch on or off the complete crystal check oscillator—Chassis 4. When S10 is on, the 100kc/s oscillator will function.

The signals obtained are fed to V7b, a harmonicproducing amplifier (Fig. 30); the diode helps in this respect, too. If S11 is on, 10kc/s signals and harmonics are thus fed to the

and harmonics are thus fed to the output socket. When S11 is off, the 100kc/s signal from V6b goes through C26, C25 and C27 and is thus amplified in the same way. The 100kc/s signal will thus be fed through to V7b in addition to the 10kc/s signal from the multivibrator (V6a and V7c).

Mounting the Components

There is plenty of room in the chassis and the layout is in no way critical. Fig. 29 shows the wiring for the 100kc/s crystal oscillator.

Rotary toggle switches are used so that the fact that Chassis 4 is a check unit is apparent from the front, all other switches being of the lever toggle type. Likewise the output socket is at the back so that it cannot be used in error for the R.F. or audio socket.

Make sure the tag strip does not short to earth and that the valveholders are correctly positioned as in Fig. 29.

Inductance L5

This has an inductance (measured) of 11.5mH,

but is not critical.

A length of ferrite rod (see the Components List and Fig. 29) is covered with a layer of Sellotape and then 400 turns of 32s.w.g. enamelled copper wire are wound on approximately to the dimensions of Fig. 29 where distances "a" are ½in. and "b" are ½in. Wind-

510 To tag 5 Points marked MC To rag 2 Output HUATOR denote earthing connections 'nη Oli socket Switch 100kc/s to chassis Power Unit-Power Unit ECC81 C26 Health His Ceramic 5/6 dia Insulator 00 Rod Sit 10kc/s 100kg/s 100kc/s :Crystal Insulating washer To tag 1,7 on Power Unit

Fig. 29.—The underchassis wiring of the crystal oscillator.

ings are pile-wound and must all be in the same direction. Balsa cement may be used to keep the windings in place. Check that the windings do not short to earth when mounted.

The rod may be mounted in any convenient manner. The author preferred to insulate it from the chassis at the ends, but it worked quite satisfactorily uninsulated.

Wiring the Crystal Oscillator (V6b)

The circuit is shown in Fig. 27 and the layout and wiring in Fig. 29. Proceed as follows: take pin 1 and the centre spigot of each valve to earth. Join pins 4 and 5 of each valve and wire them via S10 to a tag (2) of the tag strip which is on top of the chassis. This tag strip is fixed in a similar position to the strips on the other three chassis—see Fig. 23 last month for example. Connect the unit to the power pack tags 1 (or 2) and 7. Plug in the valves and observe that all heaters light correctly.

Now take one end of the coil to pin 1 of V6 and the other end to a tag (5) of the tag strip.

Note that tag 5 of the power unit is also used for the audio oscillator, but this does not matter as the two units will not be used at the same time.

Take one side of the crystal to earth and the other side to pin 2 of V6. Join pin 2 to pin 3 via R30 and connect C26 from pin 2 to the output socket (temporarily only). From pin 3 take R31 to earth and C23 also to earth. Note there are now three wires on pin 3,

Testing the Crystal Oscillator

Connect it to the power unit. Put a milliammeter in the H.T. lead to tag 5. The current taken will be about 2mA if the unit is oscillating and 8mA if it is not oscillating.

While the unit is connected, withdraw the crystal and the H.I. current should alter from the approximate value of 2mA to about 8mA. If

difficulty is experienced and wiring is correct, try another valve or suspect the wrong inductance for L5—try putting small condensers across it, starting with 100pF. If the crystal recommended is used there will be no trouble.

Now put the oscillator near the long wave crystal transistor or another receiver (page 27, May issue). A high pitched whistle or hiss (which may be hum-modulated) should be heard, it should also be possible to tune it slightly. If necessary, join the output terminal to the receiver's aerial terminal through a small condenser (say, 50pf).

If a good mains receiver is available for long waves put the crystal oscillator near to it, with 6in of wire connected to the output socket. On thining the long waves, a whistle, hiss,

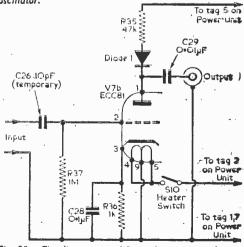


Fig. 30.—The distorter amplifier or harmonic producer.

or hum, should be heard at the 200kc/s mark (Light Programme) and also at 300kc/s and 400kc/s. If the receiver will tune to 100kc/s, a stronger signal will be heard there. If the output is connected via a condenser to the aerial terminal, strong signals will be heard as the receiver is tuned through the 100kc/s, 200kc/s, 300kc/s and 400kc/s points.

The 100kc/s point is the fundamental. It is now proposed to increase the number of strong harmonics so that the receiver may pick them up even on 25Mc/s. As it is now, the crystal oscillator will check receiver calibrations on the Long Wave band and part of the Medium Wave

The Harmonic-producing Amplifier

The circuit is shown in Fig. 30 and the layout

and wiring in Fig. 31.

Proceed as follows: remove C26 from the output socket and solder it to pin 2 of the other valve (V7), and then wire pin 2 to earth via R37. From pin 3 of this valve take R36 and C28 to earth. To pin 1 connect the diode (do not shorten the leads too much or allow them to become hot), and wire the other end of the diode through R35 to tag 5 on the tag strip (for H.T. from the power unit). Note that the red (+) end of the diode is connected to pin 1 of V7b and the black (-) end to R35. From pin 1 take C29 to the output socket. From the H.T. end of R35, wire R32 to pin 6 of V6.

Testing the Amplifier

Connect 'phones to the output socket. Remove V6 from its holder, plug in, switch on, etc., and touch pin 2 of V7. A humming should be heard in the 'phones. Replace V6 and repeat the previously described tests with receivers. Calibration points will be found every 100kc/s up to at least

COMPONENTS LIST FOR CRYSTAL CHECK UNIT

Baking Tin (as for the other chassis) Resistors:

R30 IM 1W R35 47k 1W R36 Ik 1W R31 Ik W R37 IM W R32 and R33 10k 1W R34 5.6k or 6.8k 1W R37a 470k 1W Condensers:

C23 0-1 µF 200 VW

C24 and C25 0.005 µF (5000 pF) Mica (No other value is suitable—parallel wiring of say 1000pF and 4000pF condensers will give the required value)

10pF, mica or ceramic 50pF, mica or ceramic $0.1\,\mu\text{F}$ 200VW C27

C28

C29 0·01 μF 350VW

Valve V6 and V7 Mullard ECC81

Switch SII Rotary toggle type Switch SIO Rotary toggle type

Diode Any germanium or silicon diode

(surplus)
Inductance L5 About loz of 32s.w.g. enamelled copper wire and a 15 in. diameter ferrite rod $5\frac{1}{4}$ or $5\frac{1}{2}$ in. long is required

Quartz Crystal Any 100kc/s crystal will suit, the prototype uses a rather large surplus type available from Henry's Radio. A holder is available also

Output Socket Normal co-axial type 4 or 4-way tag strip—two tags being earthed

by fixing Variable Resistor VR5 10k, any type will suit. A surplus locking ring is useful to prevent this control from moving once it is set

Nuts, bolts, grommets, etc.

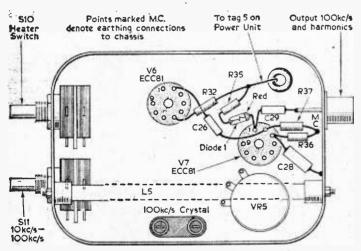


Fig. 31.—The wiring of the harmonic-producing amplifier.

25Mc/s (i.e., even on the 16m band which is considered adequate for this instrument). Note that most ordinary receivers are only approximately aligned to the scale on the short-wave bands.

Building the I0kc/s Multivibrator

The valve heaters for this part of the circuit are already wired and tested. The circuit can be seen in Fig. 28 and the wiring, which has to be added to that already carried out (Figs. 29 and 31), can be seen in Fig. 32.

Unsolder C26 from its temporary connection on pin 2 of V7. Join pins 8 of both valves together. Connect pin 8 of V6 to one side of S11 and the other side of S11 to earth. Take pin 8 of V6 temporarily direct to earth. Take pin 7 of V6 to one outer tag of VR5 and also through C25 (which must be of the correct value) to pin 6 of V7. Take pin 7 of V7 to earth via R34 (this must also be of the correct value). It will probably be easiest to earth pin 7

of V7 to the centre spigot or to pin 9. Join pin 7 of V7 also to pin 6 of V6 via C24 (again, this must be of the correct value). From pin 6 of V6, join R32 (positioned upright) to a similar

resistor R33 (also upright) and the junction of these two (R32 and R33) is joined to R35 where it leads off to tag 5 (H.T.). The wire joining the three resistors is left "in the air". The other end of R33 is connected to pin 6 of V7.

Testing the Multivibrator

Connect up to the power pack with a milliammeter in the H.I. lead to tag 5. The current should be about 10 to 12mA with both the amplifier and crystal oscillator working.

Connect to the aerial socket of a receiver via a small condenser (10pf) (and via C27) to pin 6 of V7. Loud and numerous "swishes" will be heard in many places on any waveband, the number of swishes being controlled partly by VR5 which must not be turned to the

must not be turned to the completely "off" (i.e., shorting) position.

Synchronising the Multivibrator

Condenser C26 has already been connected to pin 2 of V6 and is now not connected at the other end; solder this end to pin 7 of V6. The 100kc/s signal will now synchronise the multivibrator.

Connect up as before to a receiver set to long waves. Notice exactly where the 100kc/s points were (they will be the loudest "whistles" or "swishes") and verify that "swishes", previously non-existent, are now heard in between the 100kc/s points. Verify that the number can be altered by means of VR5.

Setting the Multivibrator on 10kc/s

Connect the unconnected end of C27 to pin 2 of V7. Disconnect the earth lead from pin 8 of V6. The circuit is now as shown in Fig. 28.

It is vital that VR5 control is correctly setguess-work is not good enough. Place the unit near to a selective receiver, and connect it to the aerial socket via a low value condenser (only if it proves necessary). Disconnect the normal aerial. Switch to Long waves and tune in the Light Programme.. Switch S10 on and S11 off. Note very carefully (a piece of gummed paper on the dial will help) the crystal calibrator point at 200kc/s and tune in the next one at 300kc/s and mark it accurately. Now switch on S11 so that the multi-vibrator functions. Count very carefully the "swishes" between the two points already marked. There should be nine (i.e. eleven counting the two main points). If the number is not correct, move VR5 slowly until you hear it lock to another frequency (in the receiver, or, if your hearing is good, from the vibrating valve electrodes in the vibrator). Repeat this until you are sure. Near the actual 100kc/s points, the hiss or whistle may be so loud that it spreads over some of the dial and masks what might be another "swish" or "whistle".

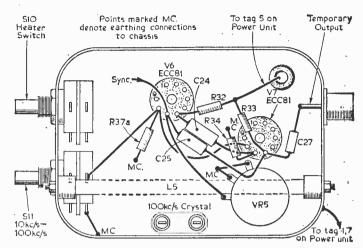


Fig. 32.—The wiring of the multivibrator.

The remedy is to move the generator farther away from the receiver so that the "swishes" are not so loud.

Finally, when VR5 has been correctly set, there should be nine smaller "swishes" between the two larger "swishes". If the receiver used is not sufficiently selective, then only seven smaller "swishes" may be heard. The two which are nearest the two larger "swishes" may be hidden by them. However, it should be obvious that two are being hidden because the spacing between the seven smaller "swishes" will be regular, while the spacing between the final smaller "swishes" and the two larger "swishes' will be noticeably greater: it will be obvious that there is space for the two "swishes" which are masked.

When VR5 is correctly set it is sealed; sealing wax is suitable,

Checking Receiver Dials

The receiver dial may now be checked; approximately, using the 100kc/s points (these are, however, exactly accurate), and then in detail with the 10kc/s points throughout the whole range of most ordinary receivers. The beginner should experiment in this direction to gain experience.

(To be continued)

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Those Portables

OME time ago I mentioned the annoyance which was being caused by the transistor type of portable and suggested that perhaps legislation would have to be introduced to limit the use of this latest weapon. Since then, I was very relieved to see that a number of authorities have taken steps to preserve the rights of the majority of us who prefer quiet and peace. At Lord's cricket ground the use of the portable has been banned, as well as on the sun-deck of the pier at Southend. At least one other seaside re-sort has a bye-law preventing the playing of radio in the streets after a certain hour and one visitor who was walking along with his radio

playing was fined.

These little sets are wonderful, if properly used, but now one sees them, in my view, being abused. On an underground train recently, one gentleman was tinkering with one and when he got out at my local station (which was above ground) he slipped it in a small cloth shopping bag, still playing, and his taste in music was inflicted on all the passengers, and presumably also on the pedestrians in every street through which he passed. The recent spate of cricket and tennis relays has brought un-told misery to many and I do feel very strongly about these receivers, and think that the type with a plug-in earpiece deserves wider use, as then others do not have to listen. It is surely a very selfish attitude to use these loudspeaker portables in such a way that others can hear them, and I feel sure that their continued use to the annoyance of others will cause so many complaints that eventually they will be banned from public places, or at least a limit will be put on the volume of sound which may be used. This, of course, brings in the problem of our old friend the decibel. When a standard such as this is adopted, some measuring device must be employed and users of road breaking apparatus and others who may fall foul of the law may plead that the volume was not excessive whilst those who object contradict this, so without a reliable yardstick, legal actions will not be possible. Perhaps the Noise Abatement people will produce some instrument which may be legalised as a measurer of noise, and receive police sanction, so that those who wish to complain will be able to do so with every chance of being upheld in their complaint.

Speed Detectors

The talk of noise measurers, brings to mind the speeding car detector, and it seems that our lives are being rather filled with modern scientific apparatus to the exclusion of our own senses and abilities. The modern calculating machine, the instant photo copier and similar devices are now commonplace, and whilst there is little doubt that they do improve efficiency by speeding up the result, the human endeavour is ousted and I won-der whether this is all to the good. We shall not need the clever mathematician in future years, as the calculator will take his place, and the efficient typist will be pushed out by the electrical type-writer, complete with automatic gadgets, whilst the skilled photographer who is now called upon to make accurate copies of documents, etc., will be replaced by the "copier".

Amateur Satisfaction

My postbag contains letters on a multitude of subjects, but it is surprising how many deal with the radio of earlier days. As one who saw radio commence its entry into the world, I do agree with a correspondent who wonders whether the modern amateur gets as much satisfaction from modern equipment. He sends me a neat pile of leaflets which he found amongst some gear at home and sends them for my inspection. He

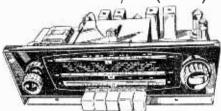
"From my point of view, the list of the Northampton Plating Co. was of particular interest, as I remember that it was one of those sources of components at a price low enough for me to afford, being a schoolboy at that time. Their S.L.F. variable condensers at 3s 11d were well made and smooth in use, one of them was surviving until some ten years ago when it was passed on to some local Scouts with other items for further use. It was still quite free of wear or shake. Incidentally S.L.F. type single con-densers do not seem to be very easily obtainable nowadays, which is a plty in view of the number of circuits appearing for small receivers and alignment oscillators in amateur publications. Most condensers offered at "popular" prices seem to be either S.L.C. or law types, and twin

gang at that.
"The dull emitter valves advertised by the Plating Co. were also quite good for their time, although the two I purchased had a greater tendency to microphony than the Mullard and Cos-

sor products.
"Still, one sometimes wonders whether the present day schoolboy, with a range of components available at relatively low price, gets quite the same gratification as my generation did at receiving Schenectady on a crystal and cats-whisker."

Yes, I wonder whether the same degree of satisfaction is experienced, especially by those who received tuition in radio at school and therefore regard it not so much as a mystery but as an accepted thing—like the essential services to be found in the home?

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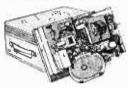
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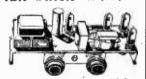
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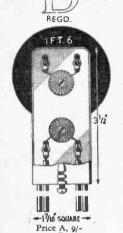
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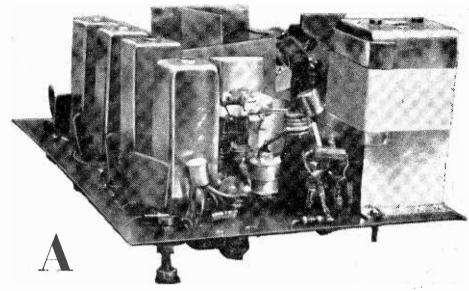
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Transistorised VIIF Superhet

AN ALL TRANSISTOR PORTABLE RECEIVER

Designed by D. R. Bowman

HE design of the receiver described here is admittedly a by-product in the development of a fully-transistorised television receiver. Before the latter can be presented, a number of serious problems remain to be solved; but the radio-frequency and intermediate-frequency stages proved vety amenable to normal transistor design procedure, and it was therefore decided to make the few necessary modifications to offer a fully transistorised VHF receiver. Work with this will afford valuable experience to the constructor, as it did to the writer.

It was realised from the outset that the production of a receiver of the too-usual miniature type would result in the also too-usual "tinny" reception, and this would do far less than justice both to the excellent and interference-free VHF transmissions and to the present-day high quality transistors. Provision has therefore been made for class AB audio output up to IW, and for reasonable reproduction of bass trequencies, a minimum

size of cabinet had to be specified. The receiver is certainly quite portable, as it weighs only a few pounds, but is not in the vest-pocket class.

Sensitivity is of the same order as the usual kind of domestic F.M. mains-operated receiver. An aerial signal of $5\mu V$ gives a power output of 50mW with the prototype receiver. The normal spread of transistor parameters may cause this to vary appreciably—perhaps from 3 to $20\mu V$ —but this will be found quite adequate in practice. Signals of 200mV can be handled, but where such a strong signal is obtainable, a very sketchy aerial can be used, and doubtless will be used, by many constructors. An outside aerial, 20ft high, consisting of a plain dipole, will ensure reception at distances of 100 miles or more from the transmitter.

In the prototype receiver, printed-circuit construction has been employed. The circuit will be found readily adaptable however for those who wish to use a normal chassis, but the use of copperciad laminate is recommended for its ease of working and its good electrical properties—no difficulty will be experienced in the etching process.

Fig. I shows the circuit diagram. This, it will be seen, denotes a "line-up" of nine transistors; an R.I. amplifying stage, self-oscillating frequency-changer, three I.F. stages, ratio detector, audio preamplifier, driver and push-pull output stages.

The R.F. Stage

The R.F. stage consists of a Mullard OC171, operating in the grounded-base configuration. The real part of the emitter input impedance under the conditions of the circuit, is about 1200. The aerial is therefore connected direct to the emitter through the usual coaxial cable of nominal impedance 80Ω This provides a very reasonable match. If, how ever, a length of wire is used for portable operation, best results are obtained by plugging a 42in. length into the centre connection of the coaxial input socket. It will be remembered that a single 33in, length will present an impedance of about 400 to the emitter, and the extra length is required for a better match.

The input is of course not aperiodic, as might be supposed: the input tuned circuit is in fact the aerial. As long as its Q is about 12 or less, the sensitivity drop at the edges of the VHF band will be less than 6dB. The aerial should therefore ideally consist of a dipole using copper or aluminium tubing of 1 in. diameter. However, the writer uses a picture-rail aerial consisting of two 33in. lengths of 14s.w.g. copper wire, with good reception of the "local" station

(56 miles away).

The R.F. OC171 operates at a collector current of about 1.4mA. A higher current gives negligible increase of gain and a noticeable rise in noise-level. A capacitor connected between emitter and base, of value 20pF, may require some comment. The purpose of this is to bring the collector feed-back current more into phase with the aerial current, and results in a measure of positive feedback, increasing R.F. gain by 3 to 4dB. It may be pos-

The collector circuit is tuned partly by a fixed capacitance of negative temperature coefficient and partly by a variable capacitor in series with another capacitor of negative temperature coefficient. The collector transformer is so designed that the secondary winding matches the input impedance of the frequency-changer transistor.

The Frequency-Changer

The frequency-changer, another OC171, is also operated in the grounded-base configuration, current from the R.F. stage being introduced by including the secondary of the inter-stage transformer in the emitter circuit. As this is a self-oscillating frequency-changer, and feedback from the collector is arranged by capacitive coupling, it is necessary to include a resistor of about 100Ω in the emitter circuit also. This causes some reduction in the signal injected, but the effect is small. The oscillating circuit is tuned partly by a pre-set capacitor, and partly by a variable capacitor ganged with the R.F. inter-stage tuning capacitor. Both are in series with a fixed capactor of negative temperature coefficient which also does duty as the fixed capacitor of the I.F. transformer in the collector circuit.

The use of negative temperature coefficient capacitors in the R.F. and F.C. circuits is not—as with valve operated equipment—to correct for warming-up drift. In the transistor receiver their function is to correct for changes in ambient temperature, and conditions are much less critical. If the user does not object to re-tuning as the room temperature changes, silver-mica capacitors can be

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used instead.

Fig. 1a.—The input and I.F. stages of the circuit.

sible to increase this capacitor to a value of 25pF, but in the prototype receiver such an increase caused the R.F. stage to oscillate when the collector circuit was tuned to 95Mc/s or higher frequency. By the same token, with certain transistors, it may be necessary to reduce its value to 15pF or even 10pF.

The Intermediate-Frequency Amplifier

It was realised that many constructors would be unwilling to undertake the construction of a receiver in which the setting-up and alignment would require a valve voltmeter or oscilloscope. In this circuit, adjustable coupling has been avoided wherever possible, and the I.F. transformers have been arranged for fixed capacitive coupling between primary and secondary, with non-critical spacing between windings. The only variable coupling is in the collector circuit of the last I.F. stage, where a simple drill enables the precise conditions to be reached, using a meter, or "nearenough" conditions by ear.

Mullard transistors, type OC170, are employed in the I.F. stages. Two pairs of coupled circuits are used between the first and second I.F. stages and between the second and third. Coupling is "critical", and the dynamic impedance of primary and secondary have been calculated to give the bandwidth needed. For exact bandwidth the transformers should be tuned by 160pF capacitors; but 180 pF capacitors are here specified because the inevitable slight inaccuracies in practical alignment, result in a very slightly "stagger-tuned" amplifier,

The last I.F. stage, which drives the ratio detector, requires tighter coupling than critical, and coupling of approximately 1.5 critical is used. The intermediate frequency is 10.7Mc/s nominally, though the constructor may prefer to vary this a little one way or the other to avoid a powerful local short-wave transmitter.

which still has the correct bandwidth.

The Ratio Detector

The use of a ratio detector was decided upon because of its simplicity and its ability to deal with small signals effectively. Because of this latter consideration, AGC has not been provided and its absence has not been acutely felt. The

Neutralisation

As the transistor may be regarded for some purposes as a triode with the grid operated in the positive region, it will be understood that at the intermediate frequency concerned, 10.7Mc/s. neutralisation of the collector-base feedback will be needed. By suitable design of the I.F. transformers, fixed non-critical capacitive neutralisation can be achieved. In fact, this circuit possesses very slight over-neutralisation, and with certain transistors the 5pF neutralising capacitors may need reduction to 3.3pF if I.F. instability is experienced. If desired, the addition of small resistors (about 47 Ω) in series with the neutralising capacitors will improve stability and gain. This process, known as unilateralisation, enables wanted and unwanted feedback to cancel each other out exactly in magnitude and phase. However, this is a refinement found not to be necessary in practice,although the purist may prefer to include it in his receiver.

The Audio Amplifier

No claim is made that the audio amplifier is original. In fact it is almost identical with the Mullard 1W amplifier, described in "Reference Manual of Transistor Circuits" (first edition, 1960). There seemed to be no point in gilding the lily. However, with the transformers specified, crossover distortion at low signal levels was more noticeable than might be desired, and a slight increase in output quiescent current has been arranged to overcome this.

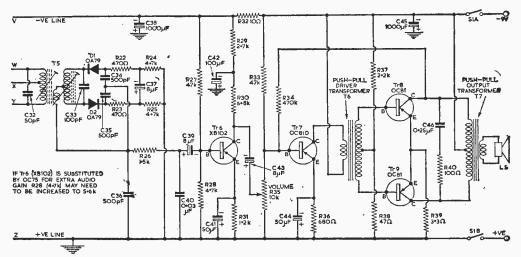


Fig. 1b.—The detector and audio stages of the circuit.

ratio detector is of conventional design. Diodes supplied in a matched pair (OA79) avoid the need for adjustable resistances in series. Amplitude limiting is improved by the stabilisation of only about 90per cent of the developed voltage, and this is arrived at by the inclusion of small fixed resistors in series with the diodes. The normal de-emphasis (in this case, 45µsec) is provided.

Very thorough decoupling has been found essential in the audio section of the receiver. This is hardly surprising, since approximately 70dB audio gain is obtained. Layout however is not critical. The inevitable increase in battery resistance during discharge causes no instability, and as much as 300Ω has been put in series with the battery without causing trouble.

(To be continued)

A Pre-wired Valveholder Extension

A SPACE SAVING MODIFICATION

By D. J. Gill

READER'S letter in the February issue, on the subject "Extension of Valveholders," tempts me to submit this simple and effective solution, which I adopted some years ago.

This simple method not only climinates the cumbersome tagboard, thus enabling the amateur to reduce the overall size of the unit under construction, or take advantage of the space saved to accommodate better his other components, but it has the added advantage of allowing each valveholder and its associated components to be wired and checked as a separate sub-unit before the valveholders are mounted on the chassis, as will be seen. Added to this is the advantage of being able to wire all valveholders while they are on a clear bench with every component readily accessible, as opposed to having to probe into

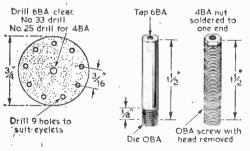


Fig. 1. (left)—The dimensions of the Paxolin disc.

Fig. 2. (right)—Two suitable extension pillars.

hidden corners with a soldering iron, sometimes at the expense of wiring, or other components, only to finish up with a doubtful connection.

Reference to the diagrams will show that the only tools required are a couple of taps and dies, but even these are not absolutely necessary. Fig. 1 shows the type of disc used by the writer, but the shape is optional, and end cheeks from discarded coil formers, or any other thin Paxolin or Bakelite will serve equally well. The dimensions for Fig. 1 can also be left to the reader, though those shown have been found to be more than adequate to accommodate all the components associated with any valve. When the size and shape has been decided, they can be drilled in batches of about six at a time as shown.

The extension pillar, Fig. 2, can be made from brass, dural, or one of the many thin rods or tubing easily obtained. For those whose kit does not include taps or dies, this pillar can be made equally well from a OBA. Hin, long screw, in the case of a nine pin valveholder. For a seven pin valveholder, the procedure is the same but the screw is 2BA.

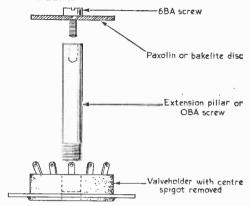


Fig. 3.—The simple construction of the extension.

The head of the screw is removed and a 68.A, or 48.A, not soldered on one end of the screw. The thread is then hled off about a \(\frac{1}{2}\)in. at the other end. This will leave the screw a tight pushfit into the centre of the valveholder.

Fig. 3 shows the unit ready for assembly, and needs no explanation further than to say that the

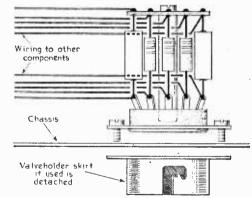


Fig. 4.—The valveholder extension in use.

top disc can be left off until all the components have been soldered to the valveholder pins.

When all components have been soldered to the valveholders, the free ends are slipped through the eyelets and the outgoing leads with them, the disc having been screwed in position. The reason for putting the outgoing wires in at this stage is that it is easier to put two or three wires if necessary through an eyelet before soldering, although there is nothing against making small loops in the component wires after they have been passed through the eyelets, and taking the wiring from these.

Record-player and Radiogram Faults

CAUSES AND CURES OF NOISE DISTORTION, WRONG SPEED, ETC.

By E. Higgs

ADIOGRAMS can suffer from a number of troubles in addition to the usual radio receiver faults with symptoms peculiar to themselves. These defects are generally either pick-up faults or turntable faults.

Pick-up Faults---Hum

Hum is more pronounced on radiograms, when present because of the larger speakers fitted and the extra attention given to the audio circuit by the designer to increase bass response. The larger baffle area for the speaker also accentuates this. Never attempt to clear hum troubles on a gram chassis without the accompanying speaker connected and fitted in its cabinet. If this is not possible, then make sure that the bench speaker used is well baffled, because a low-level hum which is tolerable on a small speaker turns out to be overpowering when the chassis is fitted back in its cabinet.

Hum that occurs when the gram is switched to records, and is unaffected by the volume control, is residual and is introduced in the circuit after the volume control. Deteriorating smoothing capacitors and partial heater to cathode leaks in following audio valves are the most likely reasons.

Variation in hum level when the pick-up or motor board are handled denotes incorrect earthing. Check the earth connections under the board but do not add extra earths to chassis in the case of A.C./D.C. grams or the motor board might become live to mains. Some A.C./D.C. grams give less hum with the mains plug a certain way round in the supply socket (taking the chassis to neutral).

Pick-up Faults (Fig. 1)

Distortion on gram only, can be caused by the stylus or by the pick-up crystal itself. The stylus can be checked on rotating cartridges by reversing to the other stylus; if this gives undistorted results (on the correct speed record), then the other stylus is proved defective. In any case, it pays to replace worn styli before evidence of wear is audible. See that the stylus is properly located on the crystal transmission pad. Too often, through mishandling and heavy set-down on auto-changers, the stylus becomes dislodged and is found jammed between the cartridge side and pad (see Fig. 1). Debris picked up as dust should be cleaned periodically from the stylus.

Cracked Crystals

Good reproduction on radio but weak distorted

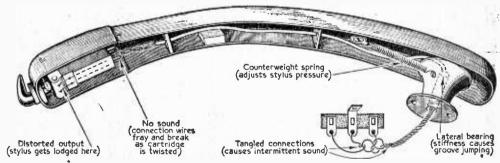


Fig. 1.—Typical faults which may develop in the pick-up arm.

Hum which reduces with the volume control setting on "gram" only nearly always originates from the pick-up. This can be checked by unplugging the pick-up leads from the chassis when the hum drops to a tolerable level. Check that the pick-up leads are not reversed—the screen should be earthed or connected to the chassis—this is a common trouble as many grams are not provided with polarised sockets and the plugs can be fitted the wrong way round by a novice without affecting the sound but causing hum.

sound from records is often due to a cracked crystal. This can be checked by unplugging the pick-up plugs from the chassis and fitting a crystal microphone or a substitute crystal pick-up from a portable record player. Good results from any of these shows the original crystal to be at fault. Crystal cartridges are fragile and can be fractured by careless handling—it is not generally known however that they are prone to failure with high temperature and portable mains radiograms with upper vents discharging heat into the space under

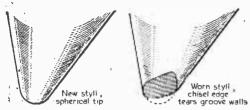
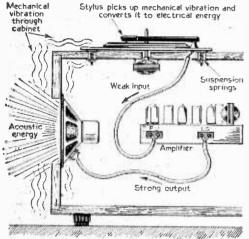


Fig. 2 (above).—The styli may become worn if the balance of the arm is maladjusted.

Fig. 3 (below).—Howling is caused by mechanical vibration being picked up and circulated by the acoustic feedback loop.



the lid "cook" pick-ups if the gram is operated for an hour or two with the lid down.

One of the commonest troubles with turnover pick-up cartridges is the breaking off of the fine wire leads at the terminals on the cartridge due to the constant flexing with rotation. Do not solder direct to the terminals but remove the clips first and solder to them otherwise the heat may damage the crystal. This trouble is sometimes intermittent if the broken lead makes and breaks with vibration.

Instifficient pick-up weight can also cause cutting out of the sound owing to the stylus tip being held clear of the bottom of the groove. An adjustable lowering stop at the base of the pick-up can allow the stylus to drop lower, or if the arm is almost weightless, the counter balance spring also situated under the, arm at the base can be slackened off one hole. Too much weight however causes excessive wear of records and styli (see Fig. 2).

Microphony

Howling which commences when the volume is increased above a certain minimum (similar to amplifier acoustic feedback in a hall) is due to the cabinet conducting vibrations from the loud-speaker to the turntable and record where they are picked up by the stylus, amplified, and sent round the feedback loop again (see Fig. 3). This is usually a fault with home constructed equipment where the motor hoard is unsprung or hadly fitted. A rigid cabinet with haffle bracing reduces mechanical vibration and raises volume at which the threshold of howl is reached. On manufacturers equipment this trouble is more often due to tight, unslackened, turntable transit screws.

Turntable Speed

The usual fault causing wow, slurring, and slowing of the record is not the turntable at all but the record slipping and skidding on its label with the one in contact with it (Fig. 4). This loss of friction can cause a warbling noticed on sustained high notes or severe slowing and at times stopping of the top record while the underside pile continue to rotate normally. The upper record when examined will be found to be saucer-shaped or to possess a small eruption on the label lifting the upper record clear of the main friction plane. A greasy or polished rim on the jockey wheel can cause the same effects but this time the turntable will be found to be turning slowly (Fig. 5). Check the pressure spring pulling the jockey wheel on to the pulley for reduced tension.

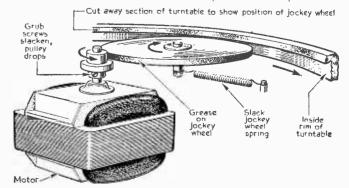
Permanent steady slow speed is most usually caused by engagement of the wrong pulley. The pulley bush can slip down the motor spindle if the grub screws loosen accidentally and with little flywheel momentum, wow or flutter may be present to iron it out.

Warped, saucer shaped record slipping on label

Turntable and lower records revolve at correct speed — warped record revolves slower

Fig. 4 (above).—Slow speed, slurring and wow, is usually caused by a warped record.

Fig. 5 (below).—Some of the causes of permanent slow speed.





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6AM6	3/6	10C2	17/6	DK32	11/6	EF86	9/9	PČL82	- Ř/-	UCH81	8/-
6AQ3 6AT6	6/-	10P13	14/6	DK91	5/6	EF89	7/-	PCL83	11/6	UCL82	10/9
6AT6	6/9	12AT6	7/-	DK92	7/6	EF91	3/6	PLC84	7/6	UCLAS	13/3
6BA6	6/-	12AT7	5/-	DK96	7/6	EF92	4/3	PCG85	13/6	UF41	8/9
6BE6	5/9	12AU7	6/3	DL33	9/-	EF183	14/-	PENA4	11/-	UF42	5/6
6BH6	5/9	12AX7	7/-	D1.35	9/6	EL33	10/-	PEN36C	8/-	UF85	8/6
6BJ6	5/9	12K7GT	5/3	DL92	6/-	EL41	8/6	PLis	11/6	UF89	2/0
6BW6	8/-	12K8GT	11/6	DL94	7/-	EL42	9/-	PLSI	9/6	UL41	7/-
6CD6G	26/9	12Q7GT	4/9	DL96	7/6	EL84	7/-	PL32	7/-	UL34	8/*
6F1	12/6	12Z3	7/6	EABC80	7/-	EM34	6/9	PL83	7/6		7/6
6F6G	6/6	1457	18/6	EAF42	8/6	EM80	8/6	PL84		URIC	8/-
6F13 ·	11/-	20F2	17/6	EB91	3/9	EM81	8/6	PY32	10/-	UU6	13/6
6F14	16/6	201.1	17/6	EBC33	5/-	EM84		PY80	11/-	UY21 ·	13/6
6K7G	2/6	25A6G	8/-	EBC41	8/-	EY51	7/6		7/6	UY41	6/6
6K7GT	5/-	25L6GT	7/9	EBF80	8/-	EY84		PY81	6/9	UY85	6/6
6K8G	6/3	25Z4G	7/6	EBF89	8/9	EY86	10/-	PY32	6/6	VP4B	9/6
6K8GT	9/3	25Z6GT	9/6	EBL21		EZ40	7/9	PY83	7/9	VP41	5/-
6T.18	10/3	30L15	11/-	ECC40	13/6		6/9	PZ30	17/-	W76	5/3
6LD20	10/3	30P12	15/-		15/-	EZ41	7/-	T41	9/6	W77	4/6
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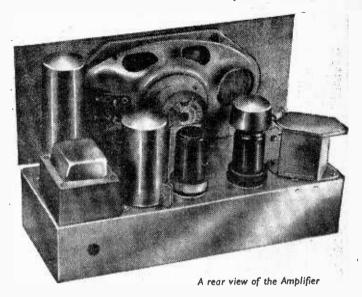
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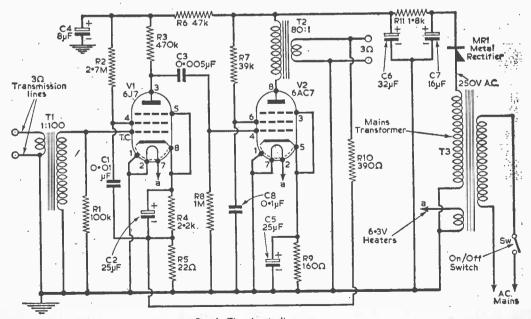
An Intercom Amplifier

By V. E. Holley

THIS AMPLIFIER WILL GIVE RELIABLE SERVICE AS A GENERAL COMMUNICATIONS UNIT.

HIS amplifier is designed for the reproduction of speech and it will give long and reliable service as an intercom, baby alarm, etc. Power consumption and heat generation are both very low and it is therefore especially suitable for continuous duty over long periods. The prototype has been in service for more than 3000 hours without valve replacement or deterioration in performance.





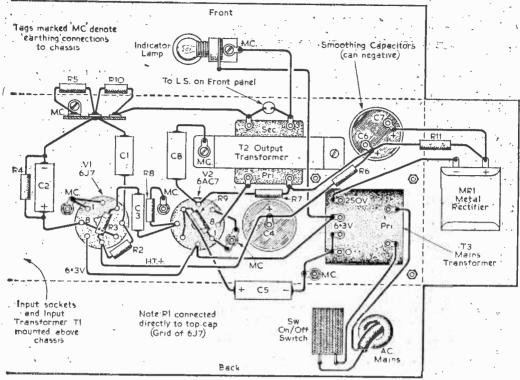


Fig. 2.—Details of the underchassis wiring.

Output Stage

This stage uses a high gain pentode, 6AC7, in the circuit given in Fig. 1. Though not properly an output valve, the 6AC7 performs that function very well, with an output approaching one watt for a signal of about 2V peak on the grid. The output transformer in the anode circuit should have a ratio of 80 or 90:1 for a 3 Ω loudspeaker. Both cathode and screen resistors are bypassed for maximum gain.

Voltage Amplifier

The signal required by the output stage is derived from the anode circuit of V1, a resistance

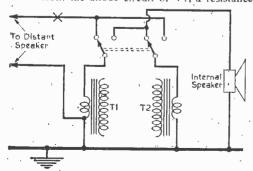


Fig. 3.—The "talk-listen" switch circuit.

coupled A.F., pentode (617). The coupling capacitor, C3 is given a value of 0.005μ F to introduce some attenuation of the lower audio frequencies which is desirable for clean crisp speech. With anode and screen loads of 470k and 2.7M respectively, and a cathode bias resistor of 2.2k the gain of the stage is 180 and the upper frequency limit is around 5000c/s. In the grid circuit is a microphone transformer, T1, having a step-up ratio of 1:100. so that the external lines can be at low impedance and therefore less susceptible to hum pick-up. The screen of V1 is decoupled to the junction of R4 and R5. This avoids degeneration and loss of gain which R5 would introduce if the decoupling were to chassis.

Negative Feedback

The overall gain of the two stages is more than is required and is reduced by negative feedback taken from the output transformer secondary to the junction of R4 and R5 in the cathode circuit of V1. The feedback, and, therefore, the gain, can be adjusted as necessary by varying the value of R10 in the range 220 to 1000Ω and if the gain cannot be reduced to the desired working level, a further reduction can be effected by removing C5

With equipment of this sort it is found that if the gain is fixed-and constant, the user rapidly becomes accustomed to it so that the results are always consistent; it might be compared in this respect with a telephone. No external gain control is therefore provided.

Power Supply

The H.T. required is 14mA at 250-300V and the total heater current including the indicator lamp, is is a little less than 1A. A miniature mains transformer of the instrument of television convertor type is used, together with a half-wave, contactcooled, rectifier. The power consumption from 240V mains is less than 15W.

The resistor RH, and the capacitors C6 and C7. provide the main smoothing, supplemented by R6 and C4 for the supply to V1. It must be mentioned that the elimination of hum requires rather special attention. A background hum which would pass unnoticed in a domestic radio receiver can be prominent and objectionable in apparatus where the sound output is normally zero, especially in quiet surroundings. In this amplifier, adequate smoothing and negative feedback give a silent background.

Construction

Fig. 4 gives a plan of the chassis on which the prototype was built. It is not essential to adhere to this, but, whatever layout is adopted, it must be arranged that there is a distance of not less than about 6in, between the mains and input transformers and that the magnetic axes of the nains and output transformers are at right angles. The output transformer also, must not be less than about 4in, from the input transformer and the latter should not be bolted to the chassis until after it has been wired up and orientated to the position of minimum hum pick-up—this position is usually quite critical. A wiring diagram is

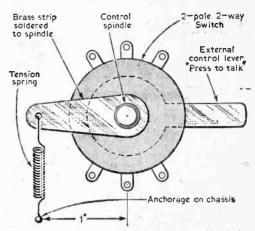


Fig. 5.—The construction of the "talk-listen" switch.

ner in two places and the speaker is supported at the rear by a light aluminium bracket.

Components

All the capacitors except C2 and C5 should be 350VW as they have to withstand the full H.T. voltage from the rectifier while the valve cathodes are warming up. The resistors can all be W except R11, which should be 1W. R9, which has a non-standard value of 160Ω is easily found by

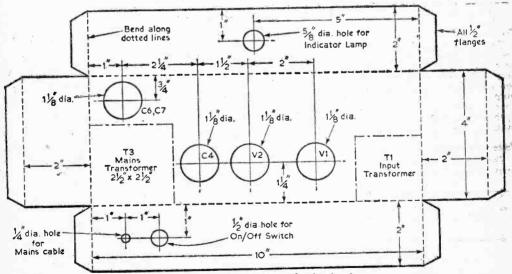


Fig. 4.—The drilling dimensions for the chassis.

given in Fig. 2. It is convenient to omit the connection between the output transformer and R10 until the test stage is reached.

The speaker in the prototype is a 7in. x 4in. elliptical unit mounted on a piece of hardboard 10in. x 6½in. in which a suitable aperture has been cut. The board is bolted to the chassis runmeasurement from a batch of 150Ω components of usual tolerance. V1 may be a 6J7, 6K7, 6SJ7, 6SK7, or any direct equivalent, without alteration of component values and with very little difference in performance, though the use of a valve with a top grid cap and a metal body is recommended. (Continued on page 414)

Ferrite Rod Aerial Concersion By C. Fletcher

CONVERTING A TRF SET TO A RECEIVER USING A FERRITE AERIAL AND ONE STAGE OF TUNING

HIS article describes a method of converting a simple TRF receiver using a tuned R.F. stage with air-cored coils, to a receiver with a ferrite rod

aerial and only one stage of tuning.

The conversion was carried out on a miniature three valve mains receiver during the course of a complete overhaul, the valve line-up being three Z77's used as the R.F. stage, the A.F. amplifier and the output valves (plus a crystal diode detector). The main advantage of the conversion was the elimination of the inconvenience of having to

ventional and the valve drew an anode current of about 9mA. The values of inductance against the secondaries of the coils refer to the medium-wave sections of the windings only.

Choice of New Circuit

On looking at Fig. 1 it might be thought that the simplest thing to do would be to wind a coil on a ferrite rod, with inductances the same as for the air-cored secondaries, and wire it in the grid circuit; leaving the rest of the circuit unaltered. However, such a solution is neither necessary nor practical. It is not necessary

since with two similar cascaded tuned circuits, as are present in Fig. 1, the effective O of the combination is approximately double that of the O of one circuit considered separately: hence with a Q of 60 for each circuit the overall Q is about 120. With a ferrite rod aerial it is quite easy to construct a coil with a medium wave Q of several hundreds - in fact the acrial constructed by the writer had a measured Q of 300 at 1.5 Mc/s. Hence, it is

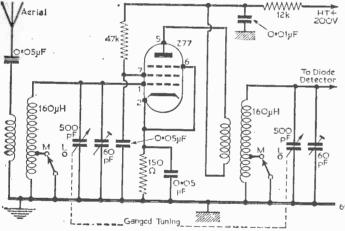
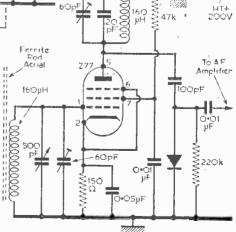


Fig. 1.—The R.F. stage of the receiver.

provide even a short length of aerial wire when the set was transported from room to room. A further, although not so obvious, advantage was the elimination of the anode tuning of the R.F. stage. This meant a very simple alignment procedure. This second advantage was gained because of the extremely high unloaded "Q" of the Ferrite rod aerial.

The circuit of the R.F. stage of the receiver was as shown in Fig. 1. The circuit was quite con-

Fig. 2.—The circuit of Fig. 1 with the alterations necessary for the use of a ferrite aerial; the resistor previously used for anode decoupling is now employed as the anode load.



unnecessary to increase the effective Q of the R.F. stage by employing anode tuning.

It is not practical to tune the anode of the R.F. stage since, with most double-tuned TRF receivers, the anode and grid coils are not separately screened, but merely screened from one another by being placed one above and one below the chassis. With a high Q grid coil it is extremely difficult, without special precautions in layout and screening, to ensure that positive, uncontrolled, feedback does not take place. Since this was a conversion, the layout had been already fixed and the slight increase in selectivity which would be obtained did not justify extensive modifications to the existing layout.

The circuit so far described is an R.F. stage with grid tuning only. A further simplification made in the writer's set was to restrict the tuning to medium-waves only. This was decided since the set was mainly intended for domestic listening and the only station normally required on long waves was the BBC Light Programme. Since this is easily obtainable, in the writer's location, on medium waves, the inclusion of long waves was not considered justified. In order to use all the control positions of the set, the hole previously used by the wave-change switch was used for the "on-off" switch and a volume control without a switch was employed.

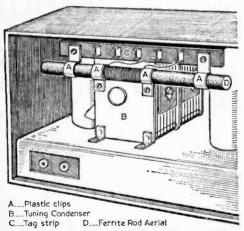


Fig. 3.—A suitable method of mounting the aerial.

A difficulty which arises on medium waves (without a tuned anode circuit), particularly at the high frequency end of the band, is due to the stray capacities appearing across the anode load of the R.F. stage. The effect of such capacities is to shunt the anode load and so reduce the gain of the stage. This is unfortunate, particularly if it is required to receive Radio Luxembourg since this station is fairly elusive anyway. However, the difficulty can be easily overcome by employing the anode coil (previously tuned by the variable condenser) in series with a resistive anode load, and peaking this coil on about 1.5 Mc/s by means of its trimmer. Hence, instead of the gain falling at the H.F. end of the band, it can be made to rise and then fall away sharply. No difficulty was experienced with unwanted feedback since the

fixed anode tuned circuit is quite isolated from the variable grid tuned circuit, and no long grid and anode leads need to be adjacent. With a coil inductance of 160 µH, to tune to 1.5 Mc/s, the preset tuning condenser must have a value of at least 60 pF; this assumes a stray capacity of 10 pF. In order to be sure of satisfying this condition a fixed condenser of 20 pF was added in parallel with the 60 pF trimmer already available. The circuit arrived at from the above considerations is shown at Fig. 2. It can be seen that the resistor previously used for anode decoupling is now employed as the anode load.

The aerial coil was wound on a piece of £in. x 6½in. ferrite rod, 52 turns being required for an inductance of 160µH. In order to achieve the high Q necessary the coil was wound with Litz wire. A suggested method of mounting the aerial is

indicated by Fig. 3.

Since the coil was wound with Litz wire, care had to be taken to be certain that each strand of wire was soldered on to the tags. An extremely satisfactory way of cleaning the ends of the Litz wire is given as follows. A small tin lid is filled with "meths" and the "meths" is ignited: the end of the Litz wire is first placed in the blue flame. The wire is held here for a few seconds allowing the cotton to burn off, and the copper to become red hot. The wire is then plunged into the "meths" and then immediately withdrawn over the side of the tin lid. If the method has been carried out correctly, each strand of the Litz wire will be perfectly clean and show the characteristic pink colour of unoxidised copper. As soon as the wire has been withdrawn from the "meths" it should be tinned. The receiver should first be tuned to a station

The receiver should first be tuned to a station at the L.F. end of the dial, and the aerial trimmer and tuning condenser adjusted until the station coincides with its marked position on the dial. The set is then tuned to the required H.F. station at which the anode tuned circuit is to be peaked (e.g. Radio Luxembourg) and the anode trimmer adjusted for maximum volume.

Record-player and Radiogram Faults

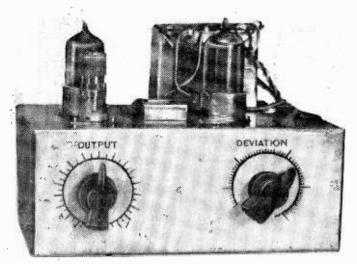
(Continued from page 400)

Generally quiet passages or sustained notes show up this effect which is heard as a flutter or gnawing sound. It may be due to a fault in the rotor causing uneven pull, or to a flat on the drive pulley.

Groove Jumping

Microgroove records in good condition that exhibit this trouble at any random place across the record point to excessive lateral stiffness of the pick-up arm. See that the pick-up screened wire is flexing freely without resistance and that the central bearing holding the arm is lightly lubricated.

Groove jumping that takes place always near the end of the record is often caused by the trip mechanism becoming stift. When examining this small, lightly riveted pawl, under the turntable do not oil it. Clean it and exercise it with a few twists with the fingers to clear any chemical corrosion that can increase friction but to oil it will only attract the dirt and dust and cause the same trouble later.



A WOB

for

ECEIVERS for the BBC's F.M. service have always presented difficulties of alignment for the amateur. The usual methods employ an A.M. signal generator and a sensitive voltmeter. In such a method, the generator is connected between the chassis and the input of the receiver's LF, amplifier, and the meter between the chassis and the grid of the limiter valve. The cores of the LF, transformers are adjusted for maximum readings on the meter. The meter is then moved to the discriminator stage and the alignment completed.

Of course, the characteristic of an I.F. amplifier may be plotted on graph paper by using an accurately calibrated signal generator in conjunction with a meter. Unmodulated signals are ted into the I.F. amplifier at various frequencies, and the out-

put voltages are noted for each. A curve may then be drawn showing output voltage against frequency; a similar procedure may be adopted with the discriminator. However, should the curves have the wrong shape, then when steps have been taken to correct them, another set of curves must be drawn. This alignment procedure is obviously not one to be recommended for the amaleur.

What is needed is a visual display of the various characteristics without the necessity of drawing graphs. The instrument for this display is the oscilloscope—as in the graphs which may be drawn, the x-axis is used to represent frequency and the y-axis to represent the output voltages. In

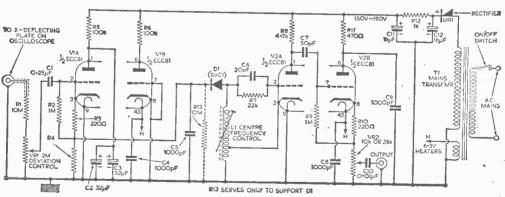


Fig. 1.—The circuit of the wobbulator. Note: the value of the resistor R4 is 6.8k.

Whilst this procedure is satisfactory for approximate alignment, it is not always good enough, as I.F. amplifiers in F.M. receivers need to have a certain bandwidth if the signal from the transmitter is to retain its high fidelity. The discriminator especially needs to be aligned accurately so that its characteristic is linear if distortion is not to be heard in the output of the receiver.

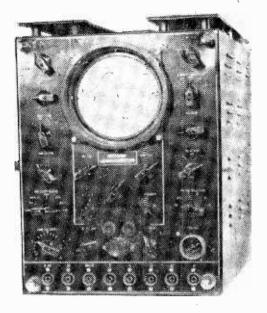
use, a frequency-modulated signal is applied to the LF, amplifier and the output of the amplifier is fed to the Y-plates of the oscilloscope to deflect the spot vertically. Horizontal deflection of the spot is obtained in the usual way by using the internal timebase of the oscilloscope. If the frequency modulation of the input signal is synchronised with the timebase of the oscilloscope, then a trace will

BULATOR

.M. I.F. Alignment

VISUAL DISPLAY OF, I.F. AMPLIFIER AND DISCRIMINATOR CHARACTERISTICS

By R. E. F. Street



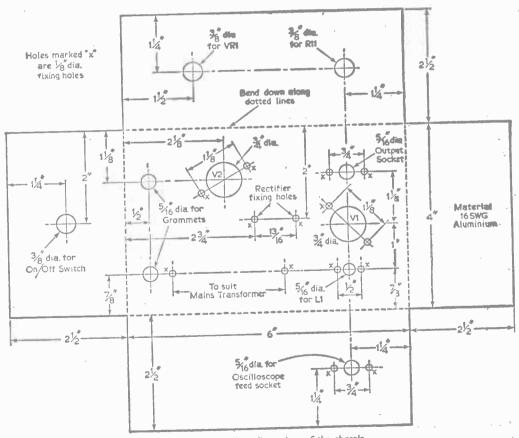


Fig. 2.—The drilling dimensions of the chassis.

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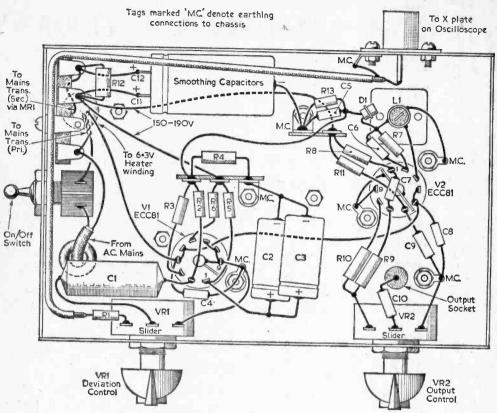
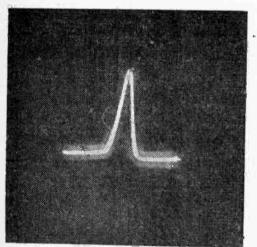


Fig. 3.—The underchassis wiring and component layout.

be formed on the face of the tube which represents the amplifier characteristic.



I.F. response of an F.M. receiver at limiter grid.

The Principle of Operation

In this instrument, a signal is generated at a frequency of 10.7Mc/s—the optimum F.M. I.F. and this signal is frequency-modulated by a signal derived from the timebase of the oscilloscope. Early methods of obtaining frequency-modulation employed variation of the inductance of the oscillator producing the 10.7Mc/s signal, or the use of a reactance valve circuit, which acted as a voltage-dependent capacitor across the tuned circuit of the oscillator. However, the circuit used in this unit employs a silicon-junction diode as a voltagedependent capacitor. When such a diode is biased in its reverse direction, a "depletion" layer is formed which acts as a dielectric of a capacitor formed by the two halves of the diode. The width of this layer, and thus the capacity of the junction, may be varied by altering the reverse bias across the diode. This is the principle of operation of the unit described.

It might be thought that the use of the 50c/s mains voltage as a modulating source would make for a simple instrument, but using such a high sweep frequency would give a misleading set of curves—the tuned circuits would not have time to respond to the rapidly changing frequency of the input signal.

(Continued on page 430)

ADDING COMMUNICATIONS

FEATURES

(Continued from page 342 of the August issue)

By F. G. Rayer

OOD results can be obtained with the older type of valve, such as those with octal bases, and many highly valued communications receivers have such valves. But when a receiver is being modified, or stages are to be added, it may be worth while using modern miniature valves, which will save space, and in some cases may give improved results.

Value of Modifications

If octal valves are to hand, or already fitted, it will not be worth while to replace these by miniature valves, in some stages. This particularly applies to audio amplifiers. Even in earlier stages, an anticipated improvement from substituting an old type valve by one with higher gain may scarcely be realised. This is because gain will almost always be reduced to some extent by the AVC circuit, so that the extra gain of the newer valve is not used.

It is in the early stage or stages in particular (e.g., R.F. amplifiers, and mixer or frequency changer) that modern valves with a lower noise level can best be used. Even here, it must be remembered that the noise level referred to is that

CHOICE OF VALVES AND STAGES

such as the 6K7 (or equivalents CV1941, CV1943, FF39, OM6, W63 etc.) in R.F. and I.F. stages. That such receivers are still in regular use indicates that these valves can give good results. With them will often be found the 6K8, 6Q7, 6H6, 6V6, and similar octal valves.

Receivers of later design tend to use more modern valves, such as the 6SG7, 6BA6, UAF42, 6BJ6, etc., in R.F. and l.F. stages. Frequency changers, converters, mixers and oscillators are also of more modern type, such as 6U8, UCH42, 6AJ8, 6AH6, 6C4, etc.

In later stages, miniature valves are also generally used, but some of these are equivalents of octal types, and are only fitted to save space and give uniformity. For example, a 6BW6 may be used instead of a 6V6, and except for being a miniature, is identical, for audio purposes.

To obtain best results with the modern valve types, some resistor values may require changing. The circuits given here, and in other articles in this series, may be used with either octal or miniature valves. When adapting and improving a receiver, it should be remembered that a double valve can often be introduced, to perform more than one function. For example, a twin triode may act as A.F. amplifier and BFO. Or such a valve could be used for a 100kc/s crystal marker, and audio or other purposes.

HT4 Aerial 6B.16 5OpF To Frequency Changer 100k 5Op₽ 5OpF 0.05µF 0.05µF C2 0.05yF 0.05 OHµF 🚎 1008 μF 251 HT-AVC. 100k

Fig. 13.—This circuit shows a 6BJ6 R.F. stage.

generated inside the set, and not that picked up by the aerial from external sources, which will often predominate.

The valve types favoured in commercially built communications receivers are a good guide to those which may be used when adapting or building a receiver. Many reputable communications receivers of older type, still in use, employ valves

R.F. Stage

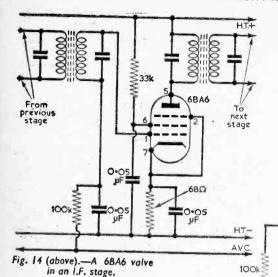
Suitable valves for a 6BJ6 are shown in Fig. 1. C1 and C2 are sections of the usual gang tuning condenser. This valve is economical, and can give very good results. A 6K7 may be used if the bias resistor is changed to about 2200. The high slope 6BA6 is also employed in this stage in high quality receivers, and should have a 33k screen grid resistor, and 680 bias resistor. Its heater current is twice that of the 6BJ6, but its gain is higher.

The usual popular type of superhet has no R.F. gain control, and one should certainly be introduced when improving the receiver. One method of doing this is shown in Fig. 13, where the 25k potentiometer is panel mounted, and acts as R.F. gain control. The most suitable value depends to some extent on the value and H.T. voltage, and may be from about

5k to 50k. If the value is too small volume will be too great, even at minimum setting. But a very large value will give abrupt control of volume. A value of about 20k can thus often be fitted. The fixed resistor from cathode to H.T. positive (100k in Fig. 13) helps to give more uniform control.

If a receiver of fairly simple type is in view, quite good results are possible on the lower

H.T.+



more than one valve it is useful to fit an I.F. gain control, which can be arranged in a similar manner to that in Fig. 13.

A crystal filter may be incorporated in an I.F. stage, and this will be dealt with later. A simple way of securing additional selectivity is to use two I.F. transformers in the coupling between I.F. stages. The secondary of the first transformer is connected to the primary of the second transformer through a very small capacity.

Frequency-Changer or Mixer

Many popular sets have a triode-hexode frequency changer, such as an octal 6K8, or miniature 12AH8. Older communcations receivers often have a valve such as the 6K8 operating as mixer only, with a separate oscillator valve. These methods can work well in general coverage receivers.

TOLE

Transformer

Fig. 15 (right).—An E6F82 mixer-oscillator stage.

frequency amateur and S.W. bands, without the use of an R.F. stage. It is usual, however, to have at least one R.F. stage, as this reduces second channel interference, and improves sensitivity and signal-to-noise ratio.

L.F. Stages

When an ordinary type of superhet is being improved, it is usually fairly easy to add an I.F. stage. This will give considerable increase in selectivity and sensitivity. Such a stage is particularly easy to add in a receiver originally having only one I.F. stage. If the receiver already has two intermediate frequency stages, much more care is necessary to avoid instability. Complete screening, and decoupling of AVC and H.T. feed circuits, will be required.

A typical I.F. stage is shown in Fig. 14, using a high slope valve. Valves such as the 6K7 may be used, with a 220Ω bias resistor, and 47k screen grid resistor. The additional I.F. transformer must, of course, be for the same frequency as those already fitted.

If the I.F. amplifier has

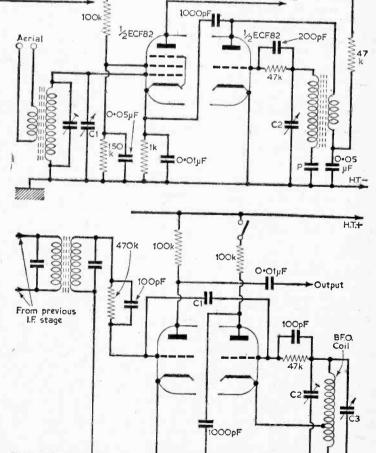


Fig. 16.—A double triode used in a detector and BFO circuit.

HT4

AVA

6BW6

etc.

A mixer-oscillator stage using an ECF82 is shown in Fig. 15. A similar circuit may be used with a separate oscillator valve, and a 6C5. 6C4, 6AM6, or similar valve may then be used as oscillator.

Fig: 15 also shows connections for a dipole aerial-the coil primary is not earthed, but twin sockets or terminals are provided, for the twin feeder. Such an aerial will usually give better results, especially in reducing untunable background noise from external sources.

Good results can be achieved by using the ECF82 as the first stage, and this has the merit of simplicity. In a larger or more ambitious receiver, a 6BA6 R.F. stage, followed by the ECF82 stage, will allow of a very good performance.

C1 and C2 are sections of the usual gang condenser. The padder condenser P should be of the correct value for the band in use. Several wavebands will normally be provided, as already explained.

Combined Valves

When high sensitivity is required from a superhet with few stages, a grid detector may be used, instead of the more usual diode. Such a detector may be easily overloaded, but can give a very good output with weak signals.

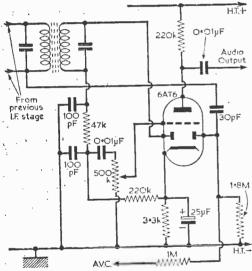


Fig. 17.-An AVC, detection and audio amplification circuit using a 6AT6.

A detector of this kind is shown in Fig. 16. Here, a double-triode has been used, and the second triode section is employed as BFO. The coupling condenser CI is of very small capacity, such as can be made from twisting together insulated connecting wire for a short distance. Octal valves such as the 6SL7 or 6SN7 may be usefully employed. Full details of BFO oscillators have been given. The BFO circuit is tunable 1kc/s or so either side the intermediate frequency, C3 being used for adjustment. It renders CW morse audible, and is switched off for voice reception. Miniature

Fig. 18. - This output stage could use any of a number of valves; 6V6, B6W6, 6AQ5, etc,

valves, such as the 12AT7, are equally suitable.

If a BFO is not wanted, or is already a twin available, triode may be used as grid detector and A.F. Alternaamplifier. tively, one triode section can furnish a 100kc/s marker signal, as previously plained in an earlier article. Some receivers employ a twin triode for BFO and audio amplifier.

2200 470k 50µF HT Fig. 17 shows suitvalues for a 6AT6, employed for detection. A.F. amplification, and automatic volume control. If a miniature valve is not wanted, a 6Q7 octal type may he used instead. An AVC in/out switch may be wired from the AVC line to chassis, to permit manual control in R.F. and I.F. stages, and prevent the

0.005

μĒ

Frem

Anode

is generally worth while. When phone reception is in view, the output of the triode will often be adequate. Alternatively, a second small triode can be used. Or a 6H6 or other double-diode may be fitted, for detection and AVC and a double-triode to provide two stages, of A.F. amplification.

automatic volume control circuit trying to follow morse. A double-diode-triode stage of this kind

is very popular indeed. The H.T. positive feed

may be decoupled by means of a 33k resistor and 8µF or similar condenser. This will slightly reduce hum, if H.T. smoothing is a little inadequate, and

Output and Rectifier

Very many communications receivers, including modern sets of high quality, employ a single hearn tetrode or similar valve, such as the 6BW6 or 6AQ5. These are miniatures, and similar, except that the 6AQ5 is intended for up to 250V only. and has a miniature 7-pin base, compared with the 9-pin of the 6BW6. If octal valves are preferred, a 6V6 may be employed, with no change in values or performance. Suitable values for any of these valves are shown in Fig. 18. Other valves may, of course, be used instead. If so, the hias resistor should be chosen to suit.

The existing power supply circuit of the receiver can probably remain unchanged, especially if transformer and rectifier are of fairly generous rating. If the H.T. rating of the transformer is rather small, it may be necessary to replace the output valve by a more economical type, for example, a 6BW6 might be replaced by a 6AM5, and this would save roughly 30mA of H.T. current, which would be available for extra I.F. or other stages.

The 6AM5 requires a 6800 bias resistor.

Club New

REPORTS OF CURRENT ACTIVITIES

BRADFORD RADIO SOCIETY Hon. Sec.: M. T. Powell, G3NNO, 28 Gledhow Avenue, Roundhay, Leeds 8.

Leeds 8.

At the Annual General Meeting it was decided to change the name of the society from "Bradford Amateur Radio Society" to "Bradford Radio Society". On May 23rd members visited the Granada TV studios in Manchester, and on June 6th they visited the Leeds and Bradford Airport. G3LZW gave a talk on "Audio Amplifier Design and Construction" on July 25th.

All meetings commence at 7.30 p.m. Slow Morse classes, if previously arranged, are held before meetings.

Future Event:
September 12th—The first meeting of the new session.

DERBY AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: F. C. Ward, G2CVV. 5 Uplands Avenue, Littleover,

The Society's Golden Jubilee Year celebrations are continuing, and on July 2nd the second Two Metre Field Day was held. A Surplus Sale was held on July 5th and on the 12th a Direction Finding Practice Run.

Future Events:
August 5th.—"Fifty Years of Radio"—an exhibition at the Derby Art Gallery—will be held for three weeks until August 26th.
August 13th—A Mobile Rally at Rykneld School.

LICHFIELD AMATEUR RADIO SOCIETY Hon. Sec.: T. L. Painter, G3NEO, Lyndhurst, 98 Gaia Lane, Lichfield.

The Society meets on the first Monday and third Tuesday of every month, at the King's Head, Lichfield.

AND DISTRICT AMATEUR RADIO CLUB Hon. Sec.: H. J. Hughes, 4 Pen-y-morfa, New Dock, Llanelly.
Lectures for the RAE were continued each Thursday up to
the end of May. A highly successful "Ladies' Night" was held on May 18th.

During Technical Training Week, commencing May 30th, a club transmitter, under the call sign GW3LL U/A, was set up at the Drill Hall, Lianelly.

LUTON AND DISTRICT RADIO SOCIETY Hon. Sec.: D. Bavister, 70 Crawley Green Road, Luton, Bedford-

The Society is organising a Mobile Rally for August 20th at Stockwood Park, Luton.

Meetings are still held at Surrey Street School every Monday night at 8 p.m.

MITCHAM AND DISTRICT RADIO SOCIETY
Hon. Sec.: M. Pharaoh, G3LCH, 1 Madeira Road. Mitcham.
Recent meetings included one where various members brought along a piece of equipment and gave a short descriptive talk about it. On Friday, June 30th, there was a discussion on Club affairs and outside activities.
On July 22nd members operated an exhibition station at the Mitcham Horticultural Show. The Society operated a similar station at the Show last year.

NORTHERN HEIGHTS AMATEUR RADIO SOCIETY Hon. Sec.: A. Robinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.

On July 26th the Society held an informal meeting. Future Event:

August 9th-A discussion on the Scout-Jamboree-On-The-Air,

NORTHERN MOBILE RADIO RALLY Hon. Sec.: J. Charlesworth, G3IJC, 23 Craven Lane, Gomersal,

Leeds.
The Rally was held in fine weather and attracted approximately 900 visitors of which 80 were mobiles, which with 160 non-mobiles, made a total of 240 cars. The majority operated on 160m, although a few 2m and All-band operators were present.

PADDINGTON AND DISTRICT AMATEUR RADIO SOCIETY

SOCIETY
Hon. Sec.: N. A. Lambert, G3LVK, Beauchamp Lodge Settlement,
2 Warwick Crescest, London, W.2.
The Society continues to meet on Wednesday evenings at 7.30,
Recent activities have included a sale of surplus equipment and
talks by Mr. Alban (G3JEA), and Mr. Legge (G3KNL). Mr.
Kippin, G8PL, brought along a large number of pre-war QSL
cards and certificates to show the members.
On Jene 24th the Society was active on G3PAD and also had
an exhibition of home-made coutoment.

an exhibition of home-made equipment.

SHEFFIELD AMATEUR RADIO CLUB
Hon. Sec.: D. R. A. Hill, 16 Tylney Road, Sheffield 2.
The two technical lectures will be held during October and December at the Dog and Partridge Hotel, Trippett Lane, Sheffield 1. They are to be held on the second Wednesday of each month.

The October lecture will be on High Power Transmitters and will be given by Dr. Kaiser Department of Physics, Sheffield University; and the December lecture will be given by Mr. Lyon, and is entitled "New Receiver".

SOUTH YORKSHIRE AMATEUR RADIO SOCIETY Hon. Sec.: E. Brailsford, G3PAF, 15 Ayrsome Walk, Cantley 4,

Doncaster.

The Society continues to increase its membership, and is now on the air as G30WK. Members recently saw two Mullard films

An Intercom Amplifier

(Continued from page 405)

Pin 1 on each valve base should be earthed to chassis.

Testing

When construction is complete and the wiring has been checked against the diagram, test with a meter between C7 and chassis that there are no shorts in the H.T. circuits. If all is well, apply power and check that the proper voltages appear at the valve electrodes. R10 can then be connected to the output transformer and if this causes oscillation, the connections to either the primary or secondary of the output transformer should be reversed to make the feedback negative. Orientate T1 to the position of minimum hum and bolt it to the chassis; hum should then be inaudible 6in. from the speaker when the primary of the input transformer is short circuited.

Operation

The external lines should be unshielded and if an earth connection is used, and it is not essential, it should be to the amplifier chassis only. In this way, interference which may be present is picked up on both transmission lines equally and is cancelled out in the primary of T1. Ordinary lighting flex is very satisfactory for distances up to about 50ft but for longer runs, a cable of lower D.C. resistance is desirable. The signal source may be a moving coil microphone but a small moving coil speaker is equally satisfactory and much cheaper.

Talk-back Facilities

For intercom service, talk-back facilities will be required and may be arranged quite simply with the circuit of Fig. 3. The switch should be a double-pole change-over component preferably of the key type, but, if this is not obtainable, an ordinary rotary switch can be modified by removal of the locating device and the addition of a spring-loaded arm as shown in Fig. 5, so that it will automatically return to the "Listen" position after use. Communication to any number of distant points can of course be established by including a multi-way switch in the transmission line at point X in Fig. 3.

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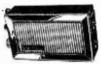
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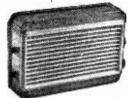
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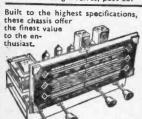
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SIGNAL GENERATOR OUTPUTS

(Continued from page 315 of the August issue)

By R. Brown

HE output impedance of a signal generator can, he changed, quite easily, with the aid of external impedances.

Supposing the required output impedance is greater than the actual signal generator

impodance, the signal generator output impedance can be increased to the new value by connecting a resistance RB in series with the output lead. RB must have a value such that RB + RA'is equal to the required output impedance. Under these

OUTPUT CONNECTIONS	REQUIRED OUTPUT IMPEDANCE RO OF ZO	VALUE OF EXTRA RESISTOR RB	New Source EMF	VOLTAGE DEVELOPED ACROSS LOAD R
E RO = RA + RB	.Resistive Ro>Ra	Ro-RA	E	$\frac{R}{RA+RB+R}$, E
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Resistive Ro <ra< td=""><td>Ro.Ra Ra-Ro</td><td>RP .E</td><td>R.RB R.RB+RA.RB+R.RA</td></ra<>	Ro.Ra Ra-Ro	RP .E	R.RB R.RB+RA.RB+R.RA
E $Ro = RA + RB$ $Zo = \sqrt{(RA + RB)^2 + X^2}$	Resistive and reactive (Ro+iX)	Ro-RA	E	$\frac{R}{\sqrt{\left\{(RA+RB+R)^2+X^2\right\}}}$
$RA = \frac{RA \cdot PB}{RA + RB} $ $ZO = \sqrt{\left(\frac{PA \cdot RB}{RA + RB}\right)^2 + X^2}$	Resistive and reactive (Ro+/X)	Ro.Ra Ra-Ro	RB E	$ \frac{R}{\sqrt{\left\{\left(R + \frac{RA, RB}{RA + RB}\right)^3 + X^4\right\}}} $
E	Resistive Ro=RA	_	E	RA+R.E

The connecting cable X-X should have a characteristic impedance equal to RA. Y-Y should have a characteristic impedance equal to RO. (or ZO).

Fig. 4.—Altering the signal generator output impedance. For convenience X may be connected at load end of Y-Y, which should then have a characteristic impedance equal to Ro.

conditions the source EMF will have the same value, E. as before but the voltage developed across a load, R, will now equal:

RA + RB + R (1)

A reduction in the signal generator output impedance can be achieved by connecting a suitable value resistor, RB, directly across the signal generator output. The value of RB is chosen so that the parallel combination of R, and RA,

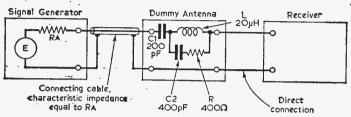


Fig. 5.—Connecting a signal generator to a broadcast band receiver.

R = RBRA/(RB + RA) is equal to the desired output impedance. The source EMF is now given by:

$$E = \frac{R_B}{R_B + R_A} \cdot E \tag{2}$$

The voltage developed across a load, R, will be given by:

$$e = \frac{RB.R}{RB + R} \times \left(\frac{RB + R}{RB.R} + R\right) \times E$$

$$e = \frac{R.RB}{R.RB + RA.RB + R.RA} \cdot E$$
(3)
$$E = \frac{RRB}{RAB} \cdot E$$

$$Characteristic Impedance Volume Volum$$

fig. 6.—The effect of connecting cable. Here the cable has a characteristic impedance equal to RA, and its far end is open circuited (see text).

If the required output impedance is to be reactive and resistive then a suitable reactive component may be connected in series with the out-put. These results are summarised in the chart Fig. 4. The connections marked X-X and Y-Y are usually coaxial cables, and the correct value for their characteristic impedance will be discussed later.

Connecting the Signal Generator to Low Frequency Receivers

- As has already been mentioned, low frequency receivers usually operate from non-resonant aerials; aerials which present an impedance which has a resistive and a reactive component. This type of aerial can be effectively simulated by connecting the signal generator to the receiver via a network which has an impedance equivalent to the aerial impedance. A standard network, called a dummy aerial, is shown in Fig. 5. This, with the output impedance of the signal generator, effectively simulates a broadcast band aerial.

The Connecting Cable

The signal generator is usually connected to the receiver with a length of coaxial cable. This cable does not need to be terminated in a resist-

ance equal to its characteristic impedance. It must, however, have a characteristic impedance equal to the signal generator output impedance.

That this is so can perhaps best be seen with the aid of Fig. 6. This shows a signal generator, to the output of which is connected a length '1' of coaxial cable. The far end of this cable is open circuited. It has a characteristic im-

pedance equal to RA. Now, it can be shown, that if such a cable is "loss-less", then the voltage Vi developed across the input end will be given by:

Vi = E coss1where B is the phase constant $(2\pi l\lambda)$ of the cable. It can also be shown that the voltage Vo at the end of such an open-circuited line is given by:

$$\begin{array}{rcl} Vo &=& Vi/cosB1\\ &=& EcosBI/cosBI\\ Therefore, Vo &=& E \end{array} \tag{6}$$

In other words the source EMF is still E volts even though the cable is unterminated.

If we now look back along the cable from the far end we see a line of characteristic impedance Zo terminated in a resistance RA. But RA=Zo. So we are looking at a cable which is correctly terminated. The impedance we see looking back from the far end of the cable is therefore RA.

Thus provided the cable does have the correct characteristic impedance, the receiver, or other

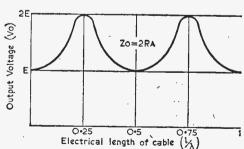


Fig. 7.—The cable output voltage for an open circuited cable which has a characteristic impedance equal to 2RA.

equipment, to which the signal generator is connected will still see a generator of E volts in series with a resistance RA.

(Continued on page 422)

OVER

ILLUSTRATIONS

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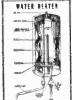
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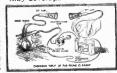
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APE recorders do not normally have built-in radio receivers. When one wishes to record a radio programme, it is, therefore, necessary to feed a signal from a receiver into the input of the tape recorder through a length of cable which may have to be fairly long. It is preferable to use coaxial cable.

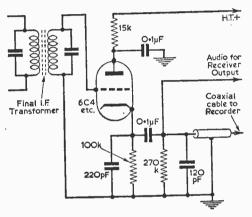


Fig. 1.—The cathode follower detector.

Final I.F. Transformer AGC AGC Volume H.T.+ Receiver Output Valve Valve V2 V2 Volume

FROM THE RADIO

Signal Supply Point

It is common practice to take the signal from the external speaker terminals of the radio receiver or (if no such terminals are fitted) the signal may be taken from the output side of the speaker transformer. Although a low impedance output is conveniently obtained by this method, it necessarily means that any distortion in the receiver output valve or in the speaker transformer will be present in the recording. Most radio receiver distortion usually occurs in the output stage unless the receiver is an expensive one.

On the other hand, it is not wise to connect a length of coaxial cable to the detector output or to the anode of an audio amplifier which is in the radio receiver (via a D.C. blocking condenser), because the capacity of the cable will severely affect the high frequency response.

Cathode Follower Detector

If a radio receiver is being constructed so that it can be used to feed a tape recorder, a cathode follower detector may conveniently be used. This circuit, which is shown in Fig. 1, has a low output impedance and can be used to feed a tape recorder through a long length of coaxial cable without high audio frequency attentuation. The circuit

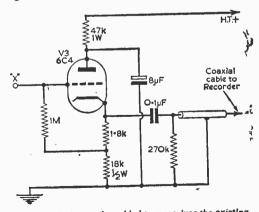


Fig. 2.—The circuit on the right is a cathode follower audio stage which may be added to a receiver the existing circuit of which is shown in the left-hand diagram. Point "X" should be connected to one of the points "A", or "C".

has the additional advantages that it does not appreciably load the previous tuned circuit and maximum selectivity and gain are therefore obtained. The distortion given by the cathode follower detector is very low. Almost any small triode or triode connected pentode, e.g. the 6C4 triode, can be used as the detector valve in the Fig. 1 circuit.

Cathode Follower Stage

If it is required to feed a tape recorder from an existing receiver, the substitution of a cathode follower detector for the common diode detector would involve re-alignment of the receiver. This can be avoided by the use of an additional cathode follower audio stage in the receiver.

Assuming a diode detector is used in the usual double diode triode circuit shown in Fig. 2, the audio output may be taken from one of the points marked A, B and C in the circuit and fed into the point marked X. The component values shown in the left-hand circuit of Fig., 2 are typical, but will vary slightly from receiver to receiver.

If the point X is connected to the point A, considerably more amplification will be obtained than if it is connected to the point B or point C. The receiver volume control will affect the tape recorder input if the connection is made to point A or B, but it is probably more convenient to connect point X to point C so that the receiver volume control does not affect the recording level.

Double Triode Circuit

Those readers wishing to use the double triode FCC82 (or the 6SN7 or 12AU7) may find the Fig. 3 circuit convenient. The first triode is an ordinary amplifying stage which is directly coupled to the grid of the second stage. The positive voltage applied to this grid (about 100) is counteracted by a slightly greater positive voltage on the cathode owing to the flow of the anode current through the large cathode resistor. The difference

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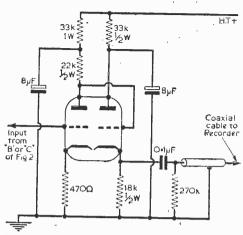


Fig. 3.—A double triode as amplifier and cathode follower.

between these voltages provides the bias for the second triode. The input can be taken from points B or C of Fig. 2. The audio voltage at point A is too large for connection to the input of the Fig. 3 circuit.

With the circuits shown, the signal can be fed into a very long length of coaxial cable, and hence to the recorder, without the high frequency response being noticeably affected. The circuits must be placed in the radio receiver and not in the tape recorder. When the circuit of Fig. 2 or Fig. 3 is used, the lead from the audio take-off point (A, B or C) to the additional valve circuit should not be more than about three inches long -shorter if possible. Care should be taken to ensure that there is only one earth connection between the receiver and recorder; this is the outer connection of the coaxial cable.

SIGNAL GENERATOR OUTPUTS

(Continued from page 418)

There will, of course, be standing waves on the cable (except when the load equals RA), but provided the cable introduces negligible losses, this will not cause any error. The cable will not normally introduce losses, for the signal generator will be close to the equipment under test, and the cable will be very short.

Incorrect Cable Impedance

The incorrect reading of the signal generator attenuator, and an incorrect connection to the equipment under test can certainly result in errors in measurements. The cause of these errors is often difficult to find. A graph is shown in Fig. 7 giving the variations in the cable output voltage with length, when the cable has a characteristic impedance equal to 2RA. The output impedance seen by the equipment under test will also be wrong with this condition, and it does not need much imagination to picture the completely incorrect and probably baffling results which could be achieved. Provided reasonable care is taken, however, one can usually be sure what output voltage the signal generator is giving, and what its output impedance is,

Wharfedale



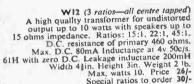
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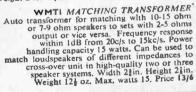


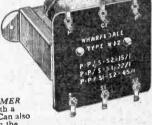
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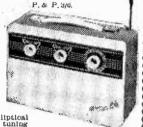


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6AG7	2/9	7B7	7/9	9003	4/-	EF22	2/-	PCL94		ÜBC41	
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6 A T 6	8/-	7 Y 4		CBT31	21/-	EF89 EF91	6/9	PLSS	10/6		
gAU6		10C1	11/-	CCH35	14/-	EF91			16/6		7/6 8/6
6BSG		10C2	13/6	CL33	11/9	EF92	4/8	PLSI		JCL82	
BRAH		10F1	5/9	CY31	9/9	EL22	12/6	P1.89	BIOLI	JCL83	11/0
6BE6	5/9	10LD11		D63	1/6	EL32		PL83		F41 .	
BO6G		10P13	9/-	DA90	2/6	EL33		L54	9/		8/6
6BW6		10P14	9/-	DAC32	9/9	EL35	7/	P ¥31	7/9 L	(Dec	
BW7		12AH7		DAF91	4/9	EL37	11/6	P¥32.	10/- (7/6 8/9
8C4		12AH8	9/9	DAF96	7/8	EL38	12/6	PVKO	7/- 1	TDAR	14/6
6C6		12AT6		DF33	9/9	EL41		P¥81	6/- 1	IDed	7/-
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BIF1	4/9	12K7OT		DHSI	9/-	EM80	8/8	R14	11/- T	II WO	
FEG		12K8GT		DK32	11/3	EM81	8/9 1	141	7/6 0		9/6 12/6
3F12	3/-		11/-	DK91	5/6	EM84	9/8 1	rDD4	7/6 U		8/4
3F13		12Q7GT		DK92	7/6	EM85	10/6 t	114	8/- 0		11/-
F14	9/6	128K7		DK96		ENS1	16/- 1		8/-10	V41	6/-
3F15		128K7G	T .	DL33		EY51		722	6/9 U		6/6
H6	2/-			DL35		Small	8/- T		15/- V		a/a
3J5G		128N7G'		DL91	8/- 1	EY86	8/- 1		12/6	11100/	6/6
J5GT	8/9			D£92		E240	8/8 i			R150/	0/10
J7G	5/-	13D3		DL93	4/8	EZ41	7/-11		7/9	~~ 2 2 0 /	
J7GT		1487	8/85	DF44	6/9	EZ80	6/- 1		14/- 3	68	8/9 9/6
Kour		19BU6G	- 1	DTAR	7/3 1	EZ81	6/6		11/- 🕏		11/-
K7G	2/8		15/-	EA50	94.	TIU	7/- 1		28/- X	76M	11/-
K7GT		20D1	8/8	EABC80	7/6 (11/- 1		6/9 3	78	14/6
K8G		20F2	8/6	EAF42	8/8 (¥Z32	8/9 1	158	4/9 3	79	16/6
KSUT	9/9 :	SOT1 :	16/- 1		1/8 1	LABC80	9/8 L	170	6/6 1	03	6/8
K25	7/6 :	(0P)	9/9	EB41	7/-IE	IBC90	7/8 L		8/- 2		9/6
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ECHNICAL 350/352 FRATTON ROAD, PORTSMOUTH

Converting the TRF Transistor Four to L.W. Tuning

A SIMPLE MODIFICATION TO THIS P.W. SET TO ALLOW RECEPTION ON THE LONG WAVE BAND.

HE four transistor TRF receiver featured in the June 1960 issue of PRACTICAL WIRELESS was described as simple to construct and therefore particularly suitable to the newcomer to transisitor circuits. For simplicity, medium waveband tuning only was included, and this arrangement is entirely satisfactory for readers living equidistant from the transmitters covering the Light and the Home programmes on the medium waveband. However, in areas where it is the usual practice to receive the Light programme on the long waveband, medium waveband tuning only restricts the usefulness of the receiver, and details are given here of how best to modify the original design, in order to accommodate both wavebands. The modification necessitates introducing a four-pole, two-way, switch into the circuit, which may be the circular type (14in. in diameter) and also an additional L.W. R.F. transformer.

40pF

40pF

M

AF

Output

turns

10

turns

150 turns

(tags 3 and 5 not used)

Fig. 1.—The arrangement of the second tuned circuit.
The L.W. Coil used is a Teletron HLX.

The Construction of the Aerial Coils

There are three methods of constructing the aerial coils: winding the coils for both wavebands on the same ferrite rod; winding the medium-wave coil on the ferrite rod and winding a separate frame aerial to cover the long-wave tuning; or winding the long-wave coil on the ferrite rod and winding a separate frame aerial to cover medium-wave tuning. If either of the last two methods is used, the choice between them is determined by the weakest signal strength in a particular area—a frame aerial has greater sensitivity to weaker signal strengths.

By D. SAULL

In the first method, where both coils are wound on the same ferrite rod, the medium-wave coil forms parts of the winding of the long-wave coil. When the wave-change switch is turned to the medium-wave position, the long-wave section of the coil is left floating. This section of the coil has an inductance of about 2.2mH and requires only a 10pF parallel capacitance to resonate at 1.2Mc/s, which is the wavelength of the Light programme on the medium waveband. Should this section of the coil, when not in circuit, so resonate -being tightly coupled through the ferrite rodi to the medium-wave tuning section of the coil-it will result in heavily loading the medium-wave coil and will render the 1.2Mc/s tuning section inoperative. The self capacity of the wave-change switch will be about 3pF, and the single-layer wound aerial coil will also possess a little self capacity—hence the stray capacity of the wiring in the circuit must be kept to an absolute minimum if trouble is, to be avoided. This may be achieved by keeping the connecting lead from the top end of the long-wave coil to the switch as short as possible. To achieve

this, the wave-change switch should be mounted directly beneath the ferrite rod—the switch control spindle may then extend to the rear of the receiver cabinet.

The Method of Winding the M.W. and L.W. Coils on the same Ferrite Rod

The dual-wave coil consists of 150 turns of 34s.w.g. double silk covered wire, close wound in a single layer on the former that should be a sliding fit on the two ferrite rods; the coil is tapped as shown in Fig. 2. The former is made by winding a strip of thick paper, two inches wide, three times round the ferrite rods, adhesive having first been applied to the surfaces in contact. A piece' of similar paper wrapped round the ferrite rods beforehand

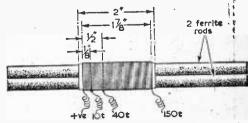


Fig. 2.—The winding details of the dual-wave coil.

will ensure a little clearance, so that the finished former is free to slide on the ferrite rod when the under piece is removed.

The gauge of wire is not critical, and it is not important that double silk covered wire is usedenamelled covered wire would function electrically. However, the best conditions prevail if the given specifications are adhered to-and the guide to the physical measurements, in Fig. 2, may then be followed.

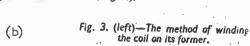
rods adjusted to give the best results. This position will most likely be in the centre.

Winding the M.W. and L.W. Coils Separately—One or a Ferrite Rod—the Other as a Frame Aerial

If the L.W. coil is to be wound as a frame aerial, the existing M.W. winding on the ferrite rods need not be disturbed. If the L.W. coil is to be on the ferrite rod, then wind the coil as in the first method, omitting the 10-turn tap.

The frame aerial may be wound on the inside of the back cover of the receiver cabinet; the size

should be about 7in. x 10in The coil is wound round four blocks, lin. square, cut: from hardboard and cemented to the inside of the back cover of the receiver; four larger blocks. fin square, also cut from hardboard, are cemented on top of the former blocks, to prevent the wire from sliding off (Fig. 4).



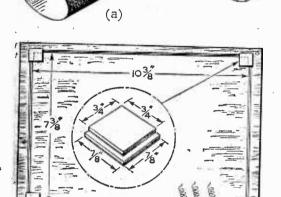


Fig. 4.—This shows the way in which the frame aerial

is wound on to the inside of the back of the receiver. The taps on the coil are formed by making a loop in the wire and twisting together the pair thus formed: then carry on winding.

A convenient method to wind the coil is to cut

a narrow piece of Sellotape to a size about in x in to form an anchoring tab. Then wrap the extreme end of the tape round the wire and attach the wire to the former (Fig. 3a) by means of the remaining length of adhesive tape. Successive turns of the winding will hold the tape firmly in position. Likewise, slip a piece of tape, the same size as before, underneath the wire (adhesive side uppermost) about 15 turns from the completion of the winding (Fig. 3b). When the final turn has been wound on, pull the extruding length of tape upwards and back over the top of the winding. A coating of varnish over the entire winding will hold it secure, but first remove the former from the ferrite rods, otherwise it may stick to the rods. The ferrite rod aerial may then be connected, and the position of the coil on the

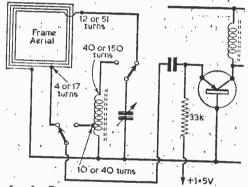


Fig. 5.—This shows the method of connecting the frame aerial in circuit.

For medium-wave tuning, the frame aerial.con sists of 12 turns of 34s.w.g., d.s.c., wire tapped at 4 turns; for long-wave tuning, 51 turns of the same type wire is tapped at 17 turns, connected as in Fig. 5.

The Second Tuned Circuit

The arrangement of the second tuned circuit remains identical for the three methods; and is shown in Fig. 1.

The L.W. coil used is a Teletron HLX. Ascertain that connecting wires in the first and second tuned circuits of the receiver are not in

close proximity, which would result in instability. The method of aligning the receiver is the same as that described in the June 1960 issue, but in the first instance make sure that the 40pF reaction capacitor is fully out and then slowly turn in to increase the positive feed-back until the best results are obtained once the required signal is heard.

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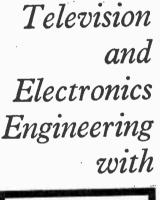
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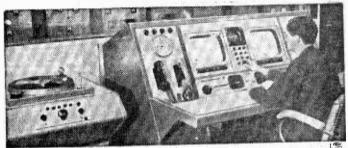


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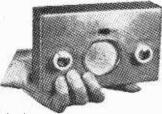
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Letters to the Editor

The Editor does not necessarily agree with the opinions expressed by his correspondents

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commerical or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELE-PHONE. If a postal reply is required a stamped and addressed envilope must be enclosed with the coupon from page ill of the cover.

TRANSMITTER LICENCES

SIR,—Surely we have not started that stupid business about low-power transmitter licences again? Mr. Dick's letter in the July issue seems to point to this. To own a "ham" transmitter licence is a privilege, not a right, and it seems only fair that one should earn this privilege by taking the G.P.O. examination. As for saying that only a simple test, if any, would be required, is ridiculous; the present test does not seem all that difficult.

Regarding his wish to abolish the morse test for inputs of under one watt, I should have thought that morse was the only way to achieve a reasonable range with this type of equipment. Moreover, if this test were abolished, there would be dozens of irresponsible people using ex-government transceivers, which, among other things, are by no means TVI-proof.—M. J. REDMAN

(Brighton).

SIR,—I have read with interest the great deal of correspondence which you have published

recently on the subject of novice licences. It has been my ambition for the last three years to obtain an amateur transmitting licence, and at last I have taken the Radio Amateurs Examination, and am now striving to attain the morse sending speed necessary for the G.P.O. test. If, and when, I finally obtain my licence, I shall feel justified in using the frequency bands allocated to amateurs. I have been asked by many people studying science subjects what justification amateurs have in using parts of the precious frequency spectrum for their own pleasure. I then proceed to tell them that at least the amateur has a knowledge of morse, which might be valuable in an emergency.

If novice licences or special concessions to "phone-only" operators were permitted in this country, the people who have to defend the amateur's cause would have no argument for the

continued existence of amateur bands.

It takes three years as an SWL to become really familiar with amateur procedure, and anyone who cannot accumulate enough knowledge in that time to pass the RAE cannot be really interested in amateur radio.—D. A. PARK (Bagshot).

ITY SOUND

SIR.—The reception of TV sound on a radio receiver, as described by B. Quest (July issue) can sometimes be caused by the sound channel of a local TV station interacting with part of the lower vision side-band to form an intermediate frequency; similar to the I.F. generated in a frequency changer.

Reception of such a signal can only be on a sensitive TRF receiver; not with a superhet. This effect disappears below 1Mc/s—750kc/s, this being the separation between the furthest sound and vision signals, and it should disappear altogether when the vision carrier is not modulated. — C.

BARNES (Cheshire).

VINTAGE MODELS

SIR,—I was not surprised to read in the July issue of P.W. a letter from Mr. A. V. Newman expressing his pleasure on hearing a friend's 1934 radio.

The pleasant tone of these vintage sets is a phenomenon not met in these days of "high

fidelity "

I would not care to open any discussion on the merits or demerits of high fidelity in these columns—it would rage on indefinitely—but the pleasure derived from listening to music on the old faithfuls is almost entirely due to the absence of the more irritating top frequencies and the presence of a measure of "woofiness" from the larger cabinets with their uncontrolled resonances.—W. J. HUNTINGFORD (Guildford).

CORRESPONDENTS WANTED

SIR,—I am 15 years old and I am very interested in radio and TV construction and theory. I would therefore like to correspond with any other readers of the same age.—H. JOHNSTONE (2 Fox Hill, Distington, Cumberland).

DISHEARTENED SWL

SIR,—Being one of the "younger SWL's set", and after reading in several books that local hams are always ready to help SWLs, I decided to visit a nearby operator.

The books could not have been more wrong! He considered that SWLs were maniacs, forgetting

that he was once one himself.

I can only hope that not all amateur radio enthusiasts hold similar opinions.—E. L. W. (Cheshire).

THREE FREE BLUEPRINTS

WITH the October, November and December issues we are presenting free blueprints intended to teach the beginner the fundamentals of practical radio construction and also to enable him to build useful receivers for his own use. The final design will be a transistorised superhet tuner unit with an amplifier which may also be used with a battery-operated record player.

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A Wobbulator for F.M. I.F. Alignment

(Continued from page 410)

The circuit of the instrument is shown in Fig. 1. A signal derived from the X-detecting plates of the oscilloscope is fed to VIA which is arranged in a cathode-follower circuit. The silicon-junction diode is connected from the cathode load of this valve to the tuned circuit of the oscillator, which is set to give a centre (unmodulated) frequency of 10.7Mc/s. The voltage across the cathode resistor (R4) also provides the reverse bias necessary for

the diode. The decoupling condensers C2 and C3 are given large values to ensure that the timebase waveform suffers negligible distortion in passing through VIA.

Although the second half of V1 is not used in the circuit, it is given a feed from the H.T. so that a current passes through it all the time that the unit is switched on; this avoids "cathode poisoning" or loss of emission in V1B.

The 10.7Mc/s oscillator is provided by V2A and the circuit values are so arranged that the frequency of operation is 10.7Mc/s when there is no input to V1A. This centre frequency is set by altering the setting of a dust core in the former of coil L1.

(To be continued)

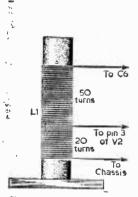


Fig. 4.—Details of the cail windings (on \$\frac{1}{2}\$ in, farmer with dust care).

Resist	ors:		•	. 97717	CHEIA	ia Fia	i		
RI R2	10M 1M 220Ω	R4 R5 R6	6-8k 100k 100k	R7 R8 R9	22k 4-7k 1 M		220 Ω 476 Ω Ik		10M 2M 10k or 25k
Ċ1 C2	citors: 0·25 μF 32 μF 32 μF	150 V V	/ — Daly	W3	, 13-10 13-10	C7 C8 C9	50pF (1000pl	Ceram F Cera	nic amic

COMPONENTS LICT

C2 32 µF 350VW—Daly W3 13-10
C3 32 µF 350VW—Daly W3 13-10
C4 1000pF Ceramic
C5 1000pF Ceramic
C6 20pF Ceramic
C6 20pF Ceramic
Valves: VIA and VIB ECC81

C7 SOpF Ceramic
C9 1000pF Ceramic
C1 000pF Ceramic
C10 001 µF Paper 250VW
C11, C12 16, 16 µF 350VW—Daly W2/39/10
V2A and V2B ECC81

Diode: DI SVCI GEC Semiconductor Division, School Street, Hazel Grove, Stockport, Cheshire

Chassis: $6in \times 4in \times 2\frac{1}{2}in$., approximately

Coil: This is wound on a $\frac{1}{4}$ in. internally threaded coil former and details are given in Fig. 4. A dust core is required.

Sundries: Two B9A valveholders, tag strips, mains switch, wire, etc.

Transformer: Mains primary, 180V to 250V H.T. secondary, 6.3V IA winding for heaters. (A "converter" transformer is very suitable.)

Rectifier: Miniature contact-cooled type-200-250Y, 40mA

Note that the value of R12 may require to be altered to ensure that the H.T. line voltage does not exceed 190.

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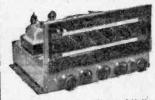
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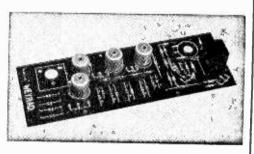
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350-0-350v. 100 m.a. 6.3v. 2a. 5v. 3a. 27/6
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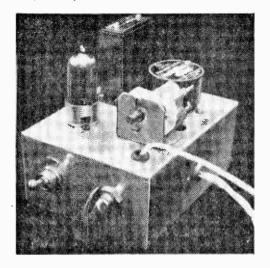
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A crystal frequency marker

By J. Longwood

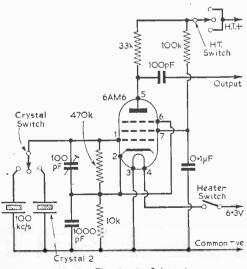


Fig. 1.—The circuit of the unit.

RYSTAL frequency markers are intended to give frequency check points over a wide range, so that receivers or signal generators may be accurately calibrated. The marker described here has a useful coverage of 100kc/s (3,000m) up to about 15Mc/s (20m) or more, the maximum frequency depending on the sensitivity of the receiver.

The Circuit

The circuit is shown in Fig. 1, and any high slope, R.F. type pentode may be used instead of the 6AM6. With some valves pin connections will of course be different, while octal valves will require an octal holder instead of the miniature Two crystals are provided for, but it is perfectly in order to use a single crystal only, as will be explained. The current required by the valve may usually be drawn from the receiver. The marker may be permanently connected—the heater switch being opened when it is not required. In addition to the heater switch, the 3-way rotary switch, which allows either crystal to be selected, has a central "off" position which interrupts the H.T. circuit. This allows the marker to be turned off and on again without waiting for the heater to reach working temperature. It also allows the marker signal to be interrupted at any time, so that it can be easily distinguished from other carriers which may be heard on crowded S.W. bands.

Operating Details

Constructors who have not used a crystal marker will probably find details of the method of operation useful. When the 100kc/s crystal is in circuit, the output from the marker is at 100kc/s and nultiples of 100kc/s. As example, its signal will be heard at 200kc/s (1500m), 300kc/s (1000m) and so on. In terms of wavelength, the marker signals are widely spaced on long waves, but much closer together on medium waves, and closer still on short waves. As 100kc/s is the same as 0·1Mc/s, the signal will be heard at 0·1Mc/s intervals troughout M.W. and S.W. bands. For example, on the M.W. band of about 600kc/s to 1500kc/s, the marker signal will be present at 600, 700, 800, 900 and 1000kc/s, and 1·1Mc/s (1,100kc/s), etc., up to 1·5Mc/s (1,500kc/s). The same result is obtained on S.W. bands. Harmonics become weaker, and this sets the upper limit at which the marker signal can be heard. With a highly sensitive receiver, harmonics may be heard up to 30Mc/s (10m).

Receiver Calibration

For receiver calibration, the appropriate marker harmonics are tuned in, and the receiver scale is drawn up to agree, or the dial readings are noted down. For example, marker signals at 3.5, 3.6, 3.7 and 3.8Mc/s will accurately set the limits of the "80m" amateur band. Medium wave tuning scales, or commercial S.W. bands, can be calibrated in the same way.

In the unit shown, crystal 2 was a 1750kc/s crystal. When in circuit, this gives marker signals at 3.5 Mc/s, 7 Mc/s, etc., in addition to the fundamental (1750kc/s), for easy identification of

amateur bands, with any receiver. Almost any crystal which may be to hand can be used for a somewhat similar purpose. It is also quite usual to have a 1Mc/s crystal, to give tuning points at 1Mc/s intervals, the 100kc/s crystal then being used to fill in the 0·1Mc/s tuning points between those obtained with the 1Mc/s crystal.

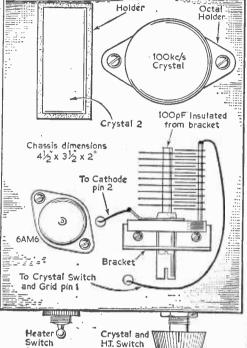


Fig. 2 (above).—Above chassis view of the marker.

It is perfectly in order to omit the second crystal and change-over switch. This will not in any way influence the accuracy of calibration at 100kc/s intervals, but will mean that the 100kc/s marker signals will have to be counted off fairly carefully; or known stations or bands will have to be tuned in, to identify the particular harmonic.

Unit Construction

Dimensions and layout are of little importance, but a small chassis about $3\frac{1}{2}$ in. x $4\frac{1}{2}$ in. x 2in. deep will be convenient. Fig. 2 shows a suitable layout. The 100pF variable

shows a suitable layout. The 100pF variable condenser, which is used for exact frequency setting of the 100kc/s crystal, must be insulated from the chassis. This can be done by having a clearance hole in the bracket, and using insulating washers. Some surplus condensers have mounting bushes isolated from the moving plates—if this is the case, insulating washers are

unnecessary. The spindle is slotted to receive a screwdriver blade.

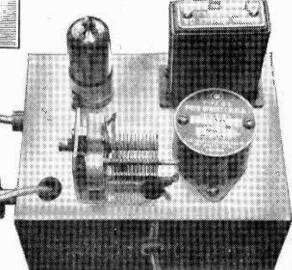
Fig. 3 shows underchassis wiring, the 3-way switch actually being mounted on the chassis runner. An octal holder is shown, for an octal based 100kc/s crystal, but the holder should of course suit the crystal to be used. The second holder was for surplus \{\frac{1}{2}\text{in. spacing crystals.}\}

A small tagboard provides anchorage for power supply leads, and some of the components. Power requirements are 6.3V, 0.3A for heater, and approximately 5mA at 200V to 300V for H.T. Wiring should be reasonably short and direct, and well insulated.

If the second crystal is not to be used, wire the 100kc/s crystal holder directly to the 100pF condenser fixed plates, and tag 1 of the B7G valveholder. A second toggle switch in the H.T. circuit will then allow the marker to be switched off, with heater running.

If a separate power pack is required, this can use a small converter or eliminator transformer, and metal rectifier. Two $8\mu F$ or similar smoothing condensers will be adequate, and the usual smoothing choke may be omitted, a 2k resistor being employed instead. In addition to about 250V for H.T., the transformer must have a 6.3V heater secondary.

When drawing power from the receiver, any convenient means of connecting the leads may be employed. It may be feasible to mount a socket on the receiver chassis, and to fit the marker leads with a plug to suit.



The Prototype Marker Unit

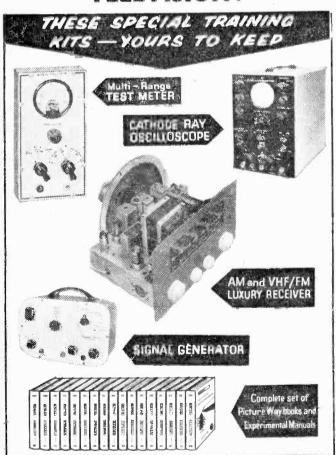
Frequency Adjustment

Crystal No. 2 is used for quick location of bands, with an entirely uncalibrated receiver, as described, and no attempt is made to adjust its frequency, as the 100kc/s crystal is used for actual, exact calibration. With the 100kc/s crystal, the 100pF pre-set condenser permits a very small shift in (Continued on page 437)

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(Continued from page 434)

frequency. The exact setting of this condenser can be found by beating the marker against the BBC 200kc/s (1500m) Light Programme, or against the National Physical Laboratory signal radiated on 2.5Mc/s. By this means, an extremely high degree of accuracy indeed can be reached.

If a new 100kc/s crystal is purchased and used with the parallel capacity setting specified by the maker, the standard of accuracy will be high enough for all practical purposes. But it is quite easy to check against one of the standards mentioned, so this is in any case worth while.

To set the 100kc/s crystal against the BBC 200kc/s transmitter (the frequency of which is maintained to

high standards) it is necessary to arrange that the Light Programme signal and marker signal are of roughly the same strength. This can be done by removing the receiver aerial, or using a short piece of wire for aerial, and also by modifying the coupling between marker output lead and receiver aerial lead. An exact balance between signal strengths is in no way necessary, but adjustment will be difficult if one signal almost completely swamps the other.

With the receiver tuned to the Light Programme, and the marker working, a very low-pitched audio tone. or flutter, may be

heard. This is the difference between crystal harmonic and BBC frequencies, and the 100pF trimmer is adjusted with an insulated blade so that the tone or flutter falls in frequency, and ceases.

If the receiver has a tuning eye or tuning meter, this will show fluctuations in signal strength when the marker tuning is almost exactly correct (say within 1c/s). If there is no eye or meter, a rise or fall in background noise or volume will be apparent. A higher standard of accuracy would be quite pointless for all normal purposes.

Receiver Calibration

The method of using harmonics has been described. Through the L.W. and M.W. bands, the marker signals will be very strong, and only loose coupling between marker output lead and receiver aerial input will be necessary.

For higher frequencies, the marker signal will be weaker, and tighter coupling will be required. It will be necessary to bring the marker output lead near the receiver aerial lead, or to twist it

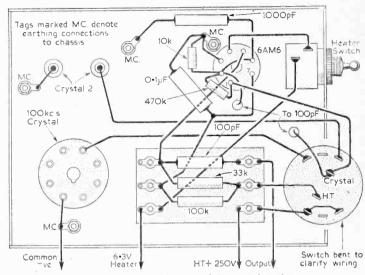
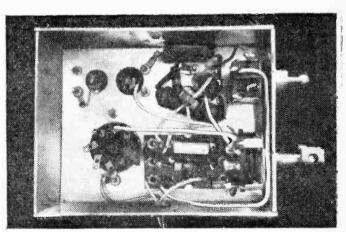


Fig. 3.—The wiring diagram of the crystal marker.

round a short insulated wire inserted in the receiver aerial socket. The receiver aerial may then be temporarily detached.

Tuning Indication

If the receiver has a tuning eye or meler, this will show fluctuations when the marker signal is tuned in. The marker signal is unmodulated. That is, it consists of a radio frequency carrier only, with no audible tone. With TRF receivers, the signals can be located by advancing reaction until the detector is just oscillating. The marker harmonics



An under-chassis view of the unit.

can then be tuned in at 100kc/s intervals, in the same way as broadcasting stations. A receiver with BFO (beat frequency oscillator) will make the harmonics audible in a similar manner.



rade

receiver which weighs only 6lb 13oz. The price of the "Courier" is 25 guineas and it is made by Pam Radio and Television Ltd., 295 Regent Street, London, W.1.

TRANSISTOR RADIO FOR STANDBY NAVIGATION

A PORTABLE transistor receiver, called the "Navigator" is now being marketed in this country by the Zenith Radio Corporation. This set, as well as receiving normal broadcasting stations, is suitable for standby navigation purposes by private pilots and yachtsmen, as it covers weather stations and L.F. directional beacons

poses by private pilots and yachtsmen, as it covers weather stations and L.F. directional beacons.

The "Navigator", which covers the 550-1600kc/s and 150-400kc/s bands, is an 8 transistor set with 500mW output. It weighs only 5lb.

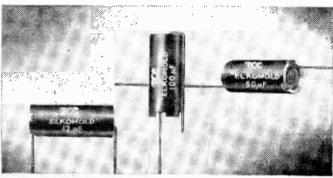
The "Navigator" is fitted with an accurate and easily read azimuth scale for taking cross-bearings and has precision vernier tuning on the main control. The price of this receiver in this country is £69 6s. 11d. The agents for the Zenith Radio

NEW PORTABLE RECEIVER

FOUR wavebands are covered by the "Courier" receiver, which is made by Pam Radio and Television Ltd. It employs eight transistors and printed circuit chassis. Apart from the internal ferrite aerial for long and medium wavebands, a telescopic rod aerial is included.

Provision is made for connecting this set to a car aerial for use in a car.

700mW output is achieved from this



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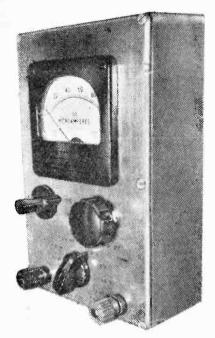
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A Sensitive Multimeter

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(Continued from page 296 of the August issue)

By R. Murray-Shelley

HE figures, given in Table 1 (

HE figures, given in Table 1 (page 296 of the August issue) should only be used as a guide, the exact lengths being found by a process of trial and error, using another meter of known accuracy in the circuits of Fig. 2. The additional components required for the construction of the shunts are, a 3V dry battery, a 1k potentiometer (pre-set, linear), a 2·2k resistor and a 50Ω resistor. The minciple of this method of construction is to vary the length of wire in the shunt until the readings of the two meters are the same for a given current (e.g. for the 10mA range, the multimeter reads full scale when the check meter reads 10mA).

Somewhat lower accuracy can be tolerated for the 1A range, and thus the shunt should be adjusted so that while the check meter reads 100mA, the reading of the multimeter is 10, assuming that the meter is calibrated from 0 to 100, i.e. 0.1 of the full scale deflection. The reason for this is that a normal dry cell battery cannot supply 1A for even a short period and thus calibra-

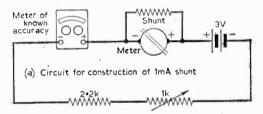
tion must be achieved using a Jower current.

When the correct lengths of wire have been obtained, they should be wound either on a small choke former or a 2 or 3W resistor of at least 5.000Ω resistance. The purpose of this is merely to act as a carrier for the wire. Resistance wire is occasionally difficult to obtain, and in the prototype, wire removed from a 50Ω 5W resistor was used very satisfactorily. Insulated copper wire (40s.w.g.) was used for the 100mA shunt, and 28s.w.g. for the 1A shunt. The formula for calculating shunt values is:

 $R = \frac{Im \times Rm}{I - Im}$

where I is the maximum current which the meter is to measure in amps, and Im and Rm are as in the August issue.

The shunt for the 1mA range has a value of over 100Ω . This is most easily made by using a 100Ω close tolerance high-stability resistor in series with a wire-wound resistor made as described above.



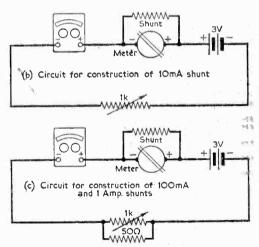


Fig. 2.—These circuits illustrate the use of a meter of known accuracy to calibrate the multimeter under construction.

Tolerance

The resistors used for the multipliers should be high-stability components of 1per cent or 2per cent tolerance. The exact calculated values are not always obtainable, since only preferred values are usually stocked. In the component list, therefore, when a resistor is not a preferred value, a pair of preferred resistances has been suggested, which when connected in series or parallel, depending on

the resistance in question, will give the required value of the multiplier.

Resistance

This instrument has provision for measuring resistances to 1M in two ranges. The circuit used is quite conventional, and although it is by no means the most accurate method which may be employed, nevertheless, it is adequate for general purposes.

The principle of this method depends on measuring the current flowing in a circuit, the potential across which is known, and thus obtaining the resistance of the circuit from Chm's Law. If the unknown resistance is a part of that circuit, then, assuming the resistance of the rest of the circuit is known, the unknown resistance may be found by subtraction. The basic circuit measuring to 1M is shown in Fig. 3.

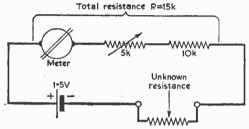


Fig. 3.—The basic ohms circuit, measuring up to IM.

Calibration

In use the meter terminals are first shorted together, and the variable resistor is adjusted until the meter reads full scale. The unknown resistance is then connected across the meter terminals, when the reading of the meter will drop. The new reading is noted and the resistance is calculated using formula:

$$Rx = \frac{R(1-D)}{D}$$

where D is the fraction of the full scale current, and R is the resistance of the rest of the circuit (in this case 15k). This method of calculating the resistance can be rather tedious, and the most accurate alternative method is to draw a graph between resistance and meter readings for various resistances. (Two graphs will be required, one for each range.) Another method of achieving the same result is to add a resistance scale to the meter itself, though this is not so accurate, since the current does not vary directly as the unknown resistance.

It is a good idea to wire the resistance ranges before wiring the voltage ranges, since, then, the precision resistors which are to be used for the multipliers can be used to calibrate these ranges.

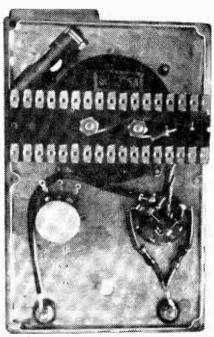
The resistance R14 is used as a range multiplier to achieve a resistance range of up to 10k. The

$$R14 = \frac{R}{(N-1)}$$

value of this resistance is given by the formula: $R14 = \frac{R}{(N-1)}$ where R, as before, is the resistance of the meter circuit, and N is the ratio of the resistance ranges. In this case:

$$N = \frac{1M}{10k} = 100.$$

For meters not having the specified characteristics, the value of R is given by (battery E.M.F. \div Im) where the battery E.M.F. is the voltage of the cell used—in this case a 1.5V renlight cell, or a larger U10 cell is recommended. Im is the meter full-scale deflection as before (in amps).



A view of the meter components, before the wiring is completed.

The resistance ranges are also useful for testing continuity, at the same time giving some idea of the resistance of the circuit under test.

Construction

The prototype instrument was housed in a metal box, size $7\frac{1}{2}$ in. x $4\frac{1}{2}$ in. x 2in. deep. This box was of very stout construction, being diecast, and made of zinc alloy. Ranges of meter boxes are available, and the exact size used will depend entirely upon the size of the basic meter movement. There is no real objection to the use of a steel box since the meter used is of the moving coil type, and is not easily affected by external magnetic fields as a moving iron meter might be.

The layout is in no way critical. In the original instrument the multipliers and shunts were carried on a group board attached to the rear of the meter movement.

Connection should be made with stout (16 to 20s.w.g.) tinned copper wire, insulated where necessary with insulating sleeving. The rectifier elements can be wired directly to the range switch and to the A.C./D.C. switch. The range switch has three wafers, each being 1-pole, 12-way, giving a composite 3-pole, 12-way switch. If this is difficult to obtain, a 3-pole, 11-way switch could be used

(Continued on page 445)



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(Continued from page 442)

in its place, though one, or possibly two ranges would now have to be omitted (e.g. 1.000 volts A.C. and D.C., or the 1A range of the 10k range). The purpose of the third wafer of the range switch, S2c, is to avoid any possibility of damaging the meter movement on the higher current ranges. This might well happen if the positive terminal of the instrument were to be connected directly to the pole of the wafer, S2b, and a faulty contact were to develop on S2b. The result would then be that the shunt would be removed from the circuit, and the full current in the circuit under test would be applied to the meter movement, in most cases causing it to burn out.

It is important when wiring the range switch to note carefully which position of the switch cor-

responds to which range.

All connections to the multimeter are made using only two terminals, and these terminals should be of the type which are totally insulated from the panel. The cell is conveniently held with a Terry clip. Connections to the cell may be soldered, since its life is many months.

Resistor Ratings

The resistors used for the multipliers need only be of ½W rating, since they will only be called upon to carry a very small current. In the case of an instrument using a 1mA meter, however, the resistors should be rated at 1W, at least for the 300V and 1,000V ranges.

The power dissipated by a resistor is given by the formula: Power (watts)=(Ir)² x R,

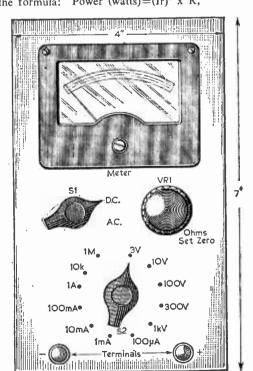
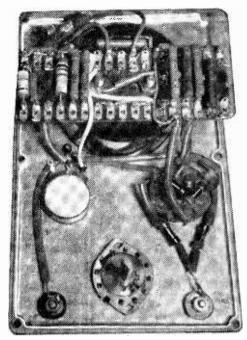


Fig. 4.—The layout of controls on the front panel.



The underchassis view with the wiring complete.

where Ir is the current in the resistor in amps, and R is its resistance.

The current in the resistor will be the same as that in the meter, and thus the maximum current which a multiplier will be called upon to carry is equal to the full scale deflection of the meter. Using this relationship the ratings of the resistors required for any meter movement can be calculated.

Soldering

It is particularly important when constructing equipment of this kind that all soldered joints should be of low resistance, and not of the "dry," type. Cored solder should always be used, and the iron should be clean, and sufficiently hot that the solder flows easily. The components to be soldered should be cleaned carefully, particularly the switches, if these are of the "surplus" type. In this case, the switch contacts themselves should be cleaned, first by scraping them, and then by using a proprietary switch cleaner, preferably one which contains switch lubricant.

Taking Readings

When using the completed instrument, always start with a high range, working down to the lower current and voltage ranges. This avoids any possibility of damaging the meter movement. The instrument should be disconnected from the apparatus when changing ranges. The test leads can be about 3ft long, and they should terminate in a pair of test prods, if possible of the retractable type.

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