

HI-FI HEADPHONES

softrubber ear moulds give correct spacing for optimum acoustle load. Each unit has a built-in miniature Hi-fl transformer to ensure the finest music and voice reproduction. Supplied free is a small transformer unit which steps impedance up to 4000 ohms. Only 15/- P. & P. 2/6.

COMMAND TRANSMITTERS Complete with all valves, crystal etc. 3-4 Mc/s. 45/-. 4-5.3 Mc/s. 45/-. 5.3-7 Mc/s, 45/-. P. & P. 3/6 each.

COMMAND RECEIVERS 6-9.1 Mc/s. 60/-. P. & P. 3/6 ea.

PORTABLE TRANS/ RECEIVER No. 18. A self-contained Trans/Receiver for Telephone and C.W. Range approx. 10 miles. Freq.: 6-9 Mc/s. (50-33.3 metres). Vaive line-up: 3 ARP-12. 2 AR-8. 1 ATP4. Com-plete with aertal. H.T. and L.T. meter and all accessories. Weight 20 lbs. Size 8 x 10 x 17in. Only 80/-. Carr. 10/-.

AERIAL VARIOMETERS

enable

Precision

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MICROPHONES, BRAND NEW. Throat magnetic, 4/8; Throat carbon 3/8; No. 8 carbon with switch 6/8; No. 7 moving coil 7/8, Tannoy power mikes only 5/4. Crystal mike 22/8.

CRYSTAL MIKE INSERTS lin. dia. 70-6000 c/s response. Brand new, ONLY 6/8. P. & P. 6d. 2 for 12/-.

These magnificent

instruments will

receive maximum signal strength on all S.W. receivers.

12/6. P. & P. 2/6.

you to

cali-

control.

These miniature Hi-Fi phones use high use high quality permanent

magnetic speakers with regu-latedvoice coil The

softrubber

PORTABLE RADIOPHONES MODEL

Brand New British Army Portable Transmitter Receivers.

Designed for reliable voice intercommunication operating up to 10 miles depending upon obstructions and elevation. The combined Transmitter Receiver covers the whole frequency range between 74-9 Mc/s, and is fully tunable on both Transmitter and Receiver. Simple and a delight to operate as all controls are mounted on the front panel of the set and clearly marked. Operates from standard dry batteries 3 v. L.T. and 120 v. H.T. Incorporates 5 valves: R.F. Amplifier. I.F. Amplifier. Second Detector, Output and Power Amplifier.

All sets are supplied complete with all accessories comprising dynamic sound powered headdhones, electro magnet supersensitive microphone, 4ft. aerial, junction box, battery connection details and full circuit diagram.

full circuit diagram.



NEW! TRANSISTOR RADIO With Miniature Speaker. Simple instructions enable Simple instructions enable anyone to build this miniature radio. Gives reception over the entire broadcast band. Each kit is suppiled with all latest miniature parts including. ** two transistors ** ferrite rod ** speaker ** coloured plastic case ** step by step fillustrated instructions. Size 4 x 3 x fin. ONLY 27/6 **P. P. 1/6. Battery 1/- ex.



15 valve superhet covering 95-150 Mc/s which includes police, aircraft and amateur bands, Complete with slow motion tuning tuning meter, circuit diagram, etc. Here is your opportunity to explore the Ville bands on a reality sensitive receiver offered at a fraction of original cost.

ONLY 26.5.0 Carr. 15/-.







OSCILLOSCOPE MODEL 74

This basic scope represents one of the finest buys we have ever made! Contains Brilliance. Focus. Gain and 2 speed time base controls. Separate X plate terminals. Signal Generator modulated at 2 frequen-cies over 150-255 Mc/s. Complete with 12 valves. VCR 1394 tube. Internal A.C. power pack, and complete circuit and technical details.

ONLY 97/6 Carr. 12/6



A really sensitive dynamic earphone of exceptionally fine quality. Provides clear reproduction of music as well as speech. Fully Guaranteed and complete with transparent ear insert. 3 feet cord, sub-miniature plug and socket.

CR-5 High imp. B/- Each MR-4 Low imp. B/- Post 1/-



SIGNAL GENERATOR
Model SW0-300 150 kc/s-300
Mc/s. Frequency Range: 150
kc/s-150 Mc/s on fundamentals
66 bands). 150 Mc/s-300 Mc/s or
harmonics. Calibration Accuracy
within ± 1 per cent. Modulation;
Internal and external. Attenuaation: To -40db. Output: Facilities for high and low. Power
Supply: Internal 230 v. A.C. Size:
7 x 10 x 5 in. Complete with test
leads and instruction manual.
ONLY £14.19.6. Carriage 5/6.



Fully Guaranteed.

PRICES:

60/- EACH (P. & P. 4/-), TWO FOR £6.0.0 (Post Free). Batteries 20/- per set.

MINIATURE MODEL MOTOR



A really high-speed precision motor with 101 uses: Model con-trol. fan. saw. buffer. etc. Oper-ates from stan-dard battery (3-6 volts), Complete withfullinstruc

tions at only 5/each. Post 1/-. 2 for 10/-. post free.

R.F. UNITS. R.F. 25, 40-50 Mc/s, switched tuning, 8/6, R.F. 27, 65-85 Mc/s, variable tuning, 29/6. Circuits supplied. P. & P. 3/6 on each.

POCKET VOLT TEST METER Two D.C. ranges: 0-250 v. and 0-25 v. Complete with test prods. and leather case. Very limited quantity. Only 12/6. P. & P. 1/6.



R.C.A. COMMUNICATION
RECEIVER AR-88 LF. Range:
73-550 kc/s and 1.48-30.5 Mo/s.
Undoubtedly the finest communication receiver ever produced for service and laboratory
use. Now Relda's exclusive purchase enables you to obtain this
Rolls-Royce of communication
receivers at the lowest price ever
offered. Fully guaranteed. ONLY
237.10.0, carr. 50/-

ACCUMULA-TORS. 2 volts 18 A.H. (unspillable). TORS, 2 volts 18
A.H. (unspillable). Ideal for 6 and 12
volts supply, etc.
Brand new. Original cartons. Size 4in x
7in. x 2in. 5/6 each.
P. & P. 1/6. 3 for 15/P. & P. 3/6, 6 for 27/6.
P. & P. 5/-



WIRELESS SET No. 19 MK. 11 Incorporates TX/RX covering 2-8 Mc/s (37-5-150 metres), and intercom. amplifier. Complete with 15 valves, 500 microamp check and tuning meter, circuit and instruction book. ONLY 65/s. Carr. 10/s.

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T.C.S. RECEIVER. 1.5 to 12 Mols. 7-valve superhet, built like a dream. Panel controls: R.F. Gain. A.F. Gain. C.W. Pitch. band-switch. mod.-C.W. switch. power switch. ground and aerial posts. M.O. or crystal frequency switch. speaker lack, card holder to log 30 stations, hand vernier tuning knob turning a large etched calibrated plate behind hair lined window. anti-backlash gears used. 90% complete, store soiled. offered at ONLY \$5.10.0. Carr. 10/-.

Exciting New Product Exclusive to RELDA

TELEPHONE PICK-UP COILS

MODEL FC-8 Induction Pick-up coil enabling conversations to be picked up without tapping of wires or special telephone circuits. No electrical connections: Simply place telephone on the pick-up platform and connect lead to the input of any medium gain amplifier or direct to any tape, disc, or wire recorder. The coil is electrostatically shielded to minimise hum pick-up. Brand new complete with 5it. shielded catle. FC-8 only. 16i-plus 1/6 p. & p. MODEL FC-8 Induction Pick-up

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Tel: Mitcham 6201 Open Daily to Callers

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All Valves Brand New and Fully Guaranteed

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Special 24 Hour Express Mail Order Service

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OZ4	5/9	6CH6	12/-	10C2 27/10	32 13/6	CCH35 21/	ECL83 12/6	H23DD	PCL83 12/6	U281 20/-
1A5	61-	56EGT	10/-	10F1 26/2	35A5 15/-	CL4 12/6		10/6	PENA4 17/6	U282 22/-
1A7	14/6	6FI	15/6	10F3 17/6	35L6GT 10'6	CL33 18/6	EF22 17/6	HL41 12/6	PENB4 17/6	U301 22/6
ID5	141-	6F6	619	10F9 12/6	35W4 8/-	CY1 15/9	EF36 7/6	HL4IDD	PEN4DD	U329 17/6
		6F7	15/-	I0LD3 12/6	35Z3 10/-	CY31 15/9		13/6	22/6	U339 19/-
1D6	10/-	6F12	419	IOLDII 15/-	35Z4 7/6	D41 12/6		HL42DD	PL33 18/6	U403 11/6
1H5	10/6	6F13	17/6	10P13 21/-	35Z5 9/6	D42 12/6		13/6	PL38 23/9	U404 10/-
IL4	61-	6F14	17/6	10PI4 20/-	40SUA 15/-	D63 3/6		HY90 8/-	PL81 14/9	U801 29/-
ILNS	416	6F15	14/9	11D3 17/6	415TH 23/6	D77 5/6		IW4/350 10/-	PL82 8/-	U4020 15/6
1N5	10/6	6F17	12/-	11D5 17'6	42 15/-	DI52 6/	AF42 10/6	IW4/500 10/-	PL83 10/6	UABC80 8/-
IRS	9/-	6F33	5/6	12A6 6/6	43 15/-	DAC32 10/6		KBC32 9/6	PL820 21/-	UAF42 9/6
154	8/6	6H6	2/6	12AH8 10/-	50C5 15/-	DAF91 7/6	L130(L) 3'0	KF35 8/6	PM2A 12/6	UB41 9/-
155	91_	615GT	4/6	12AT6 91-	50CD6G	DF33 10/6	F130(V) 41-	KL32 10/6	PM2HL 14/-	UBC41 9/6
IT4	41_	616	7/6	12AT7 8/-	21/-	DF91 4/	E F 60 0'-	KLL32 11/6	PM22A 13/6	UBF80 9/6
1U5	10/-	6J7GT	9/6	12AU7 9/-	50L6GT 9/-	DF92 7/		KL35 9/6	PM24M 21/6	UBF89 8/6
2D21	8/6	6K7G	3/-	12AX7 9/6	61BT 17/6	DF96 916	E100 11/-	KT2 7/6	PM202 16/-	UCC85 10/-
2X2	5/-	6K7GT	10/6	12BA6 9/-	61SPT 17/6	DF97 9/6	EF07 10/-	KT32 10/-	PY31 16/6	UCH42 9/-
3AS	12/6	6K8GT	12/6	12BE6 916	62BT 17/6	DH63 10/	EF91 4/9	KT33C 10/-	PY32 15/6	UCH81 9/-
3D6	14/6	6K 25	19/6	12EJ 17'6	75 12/6	DH76 716	EF92 5/-	KT36 28/6	PY80 8/-	UCL82 12/6
3Q4	8/-	6LI	15/6	12J7GT 9/6	77 12'6	DH77 8/3	EF93 7/6	KT41 22/6	PY81 7/6	UCL83 13/6
3Q5	10/6	6L6	7/6	12K7GT 8/6	78 12/6	DH107 13/6	EF95 15/-	KT44 13/6	PY82 8/-	UF41 9/-
354	8/-	6L18	12/6	12K8GT12/6	80 10/-	DH719 7'6	EL31 12/6	KTS5 22/6	PY83 8/6	UF42 11/6
3V4	9/-	6L19	21/-	12Q7GT 8/6	85A2 12/6	DK91 9/	EL32 5/-	KT61 18/6	PZ30 18/6	UF80 9/-
5R4GY	9/-	6L34	10/-	12SA7 8/-	15OB2 12'6	DK92 9/6	EL33 12/6	KT63 8/6	QP25 14/6	UF85 9/-
5U4G	4/6	6/30L2	10/-	125C7 8/-	150B3 15/-	DK96 10/	EL35 12/6	KT66 17/6	QP230 17/6	UF89 8/-
5V4	8/-	6LD3	916	125G7 8/6	185BT 32/-	DL33 9/.	EL37 18/6	KT71 9/-	QP21 12/6	UL41 8/-
5Y3GT	8/6	6LD20	15/6	12SH7 4/-	303 7/6	DL35 12/6	EL38 23/9	KT74 12/6	RIO 21/-	UL44 24/6
5Z3	10/-	6N7GT	7/6	125J7 4/-	304 7/6	DL92 8/6	EL41 10/6	KT76 12/6	R19 19/6	UL46 21/-
5Z4G	10/-	6MI	10/6	12SK7 8/~	305 7/6	DL94 9/.	EL42. 10/-	KT101 25/-	SD6 8/6	UL84 9/6
6A7	18/6	6M2	10/6	125Q7 11/6	328 7/6	DL96 9/6	EL81 14/9	KTW62 7/6	SP4 14/6	UU6 20/11
6A8	10/-	6PI	17/6	125N7 17/6	329 7/6	EA50 2/-	EL84 7'-	KTW63 7/6	SP41 3/6	UU7 15/-
6AB8	91-	6P25	19/6	12Z3 15'-	807 7/6	EABC80 7/6	EL85 10/6	KTZ41 8/-	SP42 12/6	UU8 26/-
6AJ8	9/6	6P28	261-	13D3 12/6	955 4'-	EAC91 7/6	EL90 8/6	KTZ63 10/-	SP61 3/6	UY21 15/6
6AKS	8/-	6Q7GT		14H7 12/6	5763 17/6	EAF42 10%	EL9! 5/-	L63 4/9	T41 22/6	UY41 7/6
6AK8	7/6	6SA7GT		14R7 12/6	9002 7/6	EB41 7/6	EM80 10/-	LN309 15/-	TDD4 17/6	UY85 7'6
6ALS	61-	6SG7	7/6	1457 21/-	9003 7/6	EB91 5/.		LZ319 12/6	TDD13C	VP2B 17/6
6AM5	5/-	6SH7	6/6	15A2 17/6	AC4/PEN	EBC33 4/-	EY84 10/6	MH4 8/6	17/6	VP4B 17/6
6AM6	4/-	65J7	5/6	15D2 23/9	25%	EBC41 916		MHD4 17/6	TH41 23/9	W17 8/6
6AN5	7/6	65K7	7/6	19AQ5 10/6	ACS/PEN	EBF80 9/6	EY86 9/6 EY91 9/-	MHL 10/-	TP22 17/6	W76 7/-
	8/3	6SL7GT		19BG6G	22/6	EBF89 9/-		MKT4 (5/7)	TP25 17/6	W77 5/-
6AQ8 6AT6	9/3 8/3	6SN7GT 6U4GT		24/4	AC6 21/-	EBL21 22/-	EZ35 7/- EZ40 7/6	17/6	U14 15/9	W81 6/-
6AU6	10/.	6U5	7/6	20D1 12/6 20D2 23/-	ACTP 32/-	EBL31 21/6	EZ41 7/6	MS4B 17/6	U16 10/-	W142 9/-
6B7	10/-	6U7	7/6	20F2 26/6	ACHL 12/6 AC/PEN	EC90 9/6	EZ80 7/6	MSP4 17/6	U18/20 10/-	W719 7/6
6B8	4/-	6V6G	5/-	20L1 26/6	17/6	ECC31 101	EZ81 7/6	MU14 9/- MX40 17/6	U22 10/- U24 29/6	W727 7/6
6BA6	7/6	6V6GT	8/-	20P1 26'-	ACTHI 34'9	ECC32 10'-	EZ90 7/6	N18 8/-	U24 29/6 U25 14/-	X18 11/6 X61M 21/-
6BE6	7/6	6X4	5/-	20P3 23/-	ACVPI 17/6	ECC33 5/-	FC2 21/-	N19 8/-	U26 12/6	X65 23/9
6BG6G	21/-	6X5GT	51-	20P5 22/6	ACVP2 17/6	ECC34 15/-	FC13 17/6	N37 18/6	U31 9/6	X66 21/-
6BJ6	7/6	7B7	8/-	25L6GT 9'6	AC2/PEN	ECC35 8/-	FC13C 21/-	N78 17/6	U33 21/-	X78 21/-
6BR7	15/-	7C5	8/-	25Y5 10/-	21/-	ECC40 21/-	FW4,500	N108 18/	U35 21/-	X79 21/-
6BW6	8/6	7C6	8/-	25Z4 9'6	AC2	ECC81 8/-	10/-	N142 9/6	U37 25/-	Y61 10/6
6BW7	6/6	7D5	15/-	25Z5 9/6	PENDD21/-	ECC82 916	FW4,800	N147 18/6	U45 21/-	Y63 9/-
6BX6	61-	7D6	15/-	25Z6 10/6	AZ1 15/6	ECC83 916	10/-	N150 10/-	U47 21/-	Z21 12/6
6BY7	7/6	7D8	15/-	27SU 17'6	AZ31 10/6	ECC84 9/6	GZ30 10/6	N153 11/6	U50 8/6	Z63 7/6
6C4	616	7H7	8/-	30 13/6	B36 21/-	ECC85 9/6	GZ32 11/6	N309 11/6	U52 7/-	Z66 19/6
6C5GT	8/_	7K7	10/6	30C1 12/6	B65 8/6	ECC91 5/6	GZ34 13/6	N329 10/-	U76 7/6	Z77 4/9
6C6	6/6	7Q7	11/6	30FS 11/6	B152 8/6	ECF80 12/6	H30 5/6	N727 7/6	U78 7/-	Z152 8/6
6C9	12/6	7R7	12/-	30FL1 10/6	B309 9/6	ECF82 12'6	H63 9/6	N729 8/-	U142 8/-	Z719 7/6
6C10	12/6	757	10/6	30L1 11/6	B329 9/6	ECH21 22/-	HBC90 916	P2 10/-	U145 15/-	ZD152 9/6
6CD6G		7Y4	7/6	30P4 22/-	B339 9/6	ECH42 10/-	HL92 6/6	PCC84 9/6	U147 7/-	
6D1	8/-	8D3	4/-	30P12 11/6	B719 916	ECH81 9/-	HL133DD	PCF80 10/6	U153 9/6	
6D2	5/-	9BW6	14/9	30P16 10/-	CBLI 17/6	ECH83 12/6	10/-	PCF82 9/6	U191 20/-	ngin.
6D3	15/-	1001	18/-	30PL1 15/-	CBL31 21/-	ECL80 9/-	HL23 12/6	PCL82 11/6	U251 17/6	

METAL RECTIFIERS

RMI	61-	18RA 1-1-8-1 4/6	16RE 2-1-8-1	8/6
RM2	8/_	18RA 1-1-16-1 6/6	18RA 1-2-8-1	11/-
RM3	91-	16RC 1-1-16-1 88/6	14A86	17/-
RM4	16/6	14RA 1-2-8-2 18/-	14A97	23/6
RM5	22/-	14RA 1-2-8-2 21/-	14A100	24/-

TERMS OF BUSINESS C.W.O. or C.O.D. 2/9 PACKING CHARGE ON ALL C.O.D. ORDERS. POSTAGE 3d. PER VALVE

SPECIAL OFFER

1T4 41-, 6K8 81-, 6K7G 31-, 6V6G 51-, EBC33 41-, EF39 41-, EF80 61-, EF91 419, 6X5G 51-, 5U4G 416.

OBSOLETE VALVES A SPECIALITY.
QUOTATIONS GIVEN ON ANY TYPE
NOT LISTED.

DEPT. P.W.I.

HARVERSON SURPLUS CO. LTD

MONAURAL AMPLIFIER



This amplifier as illustrated, made by a leading manufacturer. Mullard valves— ECC83, EL84 x EL84, EZ80. Bass Treble and Volume on remote panel. Elegant Knobs. OUR PRICE one month only £4,16.6 plus P. & P. 3/6.

STEREOPHONIC AMPLIFIER

Complete with 2 Loudspeakers

Plus 4/6 P. & P.

£5.10.0

This is a compact amplifier embodying the latest features and giving a high standard of reproduction, with ample volume. Supplied complete with valves (ECL82, ECL82, EZ80), panel, knobs, etc. and two specially selected 312 matched loudspeakers. We only have a few, and we will never be able to repeat this offer at such a low price. Don't risk disappointment. Order now.

HARVERSON SUPERHET 4 KIT

A medium and longwave superhet, incorporating two I.F. stages modern B9

valves (UCH81, UBF89, UCL83, U785), built-in ferrite rod aerial. All you need supplied from theoretical wiring diagram to last nut and bolt (main components ready mounted), including an attractive contemporary styled cream plastic cabinet with gold trimmings. Size III x # 2 x 6lin.

PRICE £6.12.6

Post 3/6

RECTIFIERS TRANSISTOR BARGAINS MULLARD FIRST GRADE -FOR BATTERY

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\$ 5'- 8'- 10'-	OC71	1 1

SPECIAL OFFER

DON'T MISS THIS MULLARD O.C.76 10/6 MATCHED PAIR £1.0.0

Post and packing 6d.

SLOW MOTION TUNERS

500-500 Twin gang condensers with geared slow motion drive. 3/6 ea. 36/- per doz. P. & P. 6d.

WIRE WOUND POTS 12 Wire wound Colvern Pots -all different values 10/6 P. & P. 9d.

TRANSISTOR RECORD PLAYER CASE

A few only—Transistor record player cases in light grey cloth—complete with motor board. Size: 12 x 8 x 6in.

18/6 each. P. & P. 1/9.

THIS MONTH'S BARGAIN! SUPERHET CHASSIS

CHARGERS

. . . .

12 v. f amp. ... 12 v. 2 amp. 12 v. 3 amp.

12 v. 4 amp.

12 v. 5 amp.

P. & P. 6d.

Complete and ready for your cabinet, 4 valve superhet chassis, complete with valves, ferrite aerial, dial and knobs. Valve line-up—UCH81, UBF89, UCL83, UY85. Long and Medium wave coverage.

PRICE £4.19.6 P. & P. 3/6.

COSSOR C.R.T. SNIP

108K 10-inch. New and boxed, 15/-, plus 6/- P. & P. 75K 10-inch. New and boxed. 151-, plus 61- P. & P.

ION TRAP MAGNETS

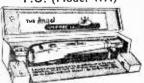
To suit the above, 2/9 each. P. & P. 3d.

SPEAKER FRET

Super quality heavily woven fret, 54 inches wide. Usual price 50/per yard. P. & P. I/per yard. P. OUR PRICE 12/6 per yard.

GRAM & TAPE EQUIPMENT BARGAINS

THE WORLD FAMOUS E.M.I. ANGEL TRANSCRIPTION P.U. (Model 17A)



A Pick-up for the connoisseur originally priced at £17.10.0. The last remaining few offered at £4.10.0 Plus P. & P. 5/-.

PICK-UP CARTRIDGE BADGAING

DAMOAIIIO		
STUDIO P		17/6
ACOS HIGH G		17/6
E.U. POWER POINT		12/6
RONETTE	•••	18/6
G C 7	•••	16/6
		10.0
P. & P. I/		

RECORD CHANGERS

	= GAKKA	KD-	
RC 98 Mk. 4H.	4-speed	autochanger	£16.10.0
RC 120/D Mk.2	**	11	£9. 0. 0
RC 120 Mk.4D		.,	£9. 0. 0
RC 120 Mk.4H			£9. 0. 0
RC 121 Mk.I	**	11	£11.0. 6
RC 121 Mk.4H			£11.0. 6
RC 121/40 Mk.2		"	£11.0. 6
	=COLLA	RO-	
RC 54	4-speed at	itochanger	£6.19. 6
RC 594		**	£7.19. 6
Conquest	.,	**	€6.12. 6
Challenger			£7,19, 6
	——B.S.R		

Monarch UA8 4-speed autochanger £6,19. 6 TUB 4-speed single player less pick up £2.10. 0
NOTE: Any of the above with Stereo Cartridge and
Fittings, 16'- extra. Carriage and ins. on each
of above 5/- extra.

TAPE DECKS-

LATEST B.S.R. MONARDECK (single speed) Boxed Plus 6/- carr. and ins. (tapes extra).

CYLDON 12 CHANNEL TURRET TUNERS

New purchase offered at still lower price. I.F. 33-38 Mc/s. Complete with PCC84 and PCF80 valves and 8 sets of Coils for 5 Band I Channels and 8, 9, 10 Band III. New and unused. Value over £7. 37/6 OUR PRICE, post paid 32/6

MIDGET I.F. TRANS & COILS

A Pair of midget 465 kc/s J.F. transformers, plus LW and MW coils. OUR PRICE 10/- per set. P. & P.

Set of I.F. transformers for transistor superhet. 12/6. P. & P. 1/9.

CONDENSER/RESISTOR PARCEL

50 mixed P.F. Condensers and 50 mixed Resistors. An assortment of useful values. All popular sizes—all new—a must for the serviceman and constructor. ONLY 10/-P. & P. 1/-.

83 HIGH STREET, MERTON, S.W.19

CHErrywood 3985/6/7

HARVERSONS SUPER STEREO KIT

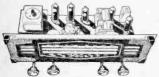
The product of a renowned maker, this stereo amplifier is composed of "ready-built" units, only requiring Interconnection. This system has the advantage of being adaptable to fit any cabinet. Each unit is made from first-grade components, and valves used (ECL82, EZ80 range) are genuine Mullard. The comprehensive instructions supplied make the simple interconnection of units easy even for the novice.

THE KIT COMPRISES ...

TWO MIDGET AMPLIFIERS each of 3W output, good reproduction from both your stereo or monaural records. Both amplifiers complete with well-designed O.P. transformers providing perfect matching 3-7(2 speakers, and have remote bass, troble and volume controls. Size $5^{\circ} \times 2_{2}^{1/\circ} \times 3^{\circ}$ high (each amplifier).

CONTROL UNIT, is a flying panel with three 2-gang pots, enabling the bass, treble and volume controls of each amplifier to be conveniently positioned. Supplied with attractive cream and gold knobs.

A.M. RADIOGRAM CHASSIS



A chassis of distinction, by a famous maker. Covering Long, Med. & Short Waves, plus gram position, this chassis (Size 15½ x 7 x 6½ in. high) incorporates the latest circuitry, using fully delayed A.V.C., and negative feedback. Controls: Tone, Vol. On/Off, W/Change (L.M.S. & Gram). Tuning. Tapped input 200-250 v. A.C. only. An attractive brown and gold illuminated dial with matching knobs, make this one of the most handsome, in addition to being one of the best performing chassis yet offered. Complete with valves (ECHB1, EFB9, EBCB1, ELB4, EZB1), knobs, output transformer, leads, etc. OUR PRICE ONLY

GUARANTEED VALVES * NEW and BOXED

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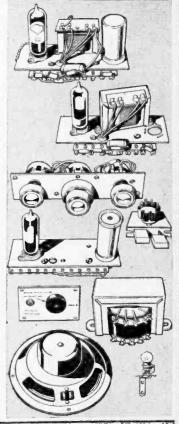
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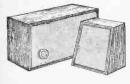
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OSC 87pF, size I x I x
Jin., 17/6 each.
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3 and Oscillator coil, size of each $\frac{7}{16}$ in. $\times \frac{7}{16}$ in. $\times \frac{1}{2}$ in. high, per set 21/4. Driver Transformer type TR 190/EIP: ratio 2 +1, size § x ½ x ½in., 6/3

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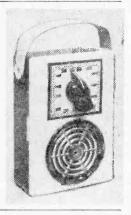
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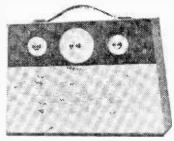
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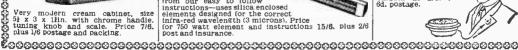


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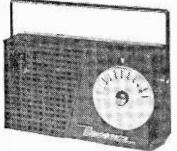
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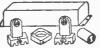
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AU4 5/	ECC84	7/-	KT2 4/-	OS75/20		· ·	7/-	6F6	7/-	7Z4	6/6	715B	97/6	43,
AW3 4/	ECC85	7/9	KT31 8/-	Q595/10		W31	7/-	6F5G	5/6	8D2	2/6	717A	8/6	Photo
AZ 8/		41-	KT32 8/-	QS 108/4		Y63	5/-	6F6G	41-	9D2	3/-	723A/B	45/-	Tubes
BL 63 6/		8/-	KT33C 6/3	Q3100/-	6/9	Y66	8/-	6F8G	6/6	IOY	8/6	801	6/-	
BT45 40/		7/3	KT44 6/3	Q\$150/		Z31	61-	6F12	4/6	12A6	5/_	803	22/6	GL16 12/0
BT9B 40%		5/-	KT63 6/-	Q3130/	6/9	IA3	3/-	6F32	6/-	I2AH7	7/-	805	30/-	931A 50/
CY31 11/6		3/6	KT66 11/-	R3	8/-	IASGT	5/-	6G6G	3/-	12AT7	5/6	807 A ME		
DI 3/		8/-	KT241 9/-	RIO	12/6	IC5GT	7/6	6H6GT	1/9	12AU7	6/-	00,,,,,,	7/-	Special
D41 3/3		4/3	KTW62 7/6		25/-	ID8GT	61-	6H6M	2/-	12AX7	7/-	807BR	5/-	Valves
D42 4/		2/6	KTW63 6/6	REL21 RL37	3/6	IE7GT	7/6	6HA7	4/3	12CB	3/-	808	8/-	2J31 457
D77 4/3		3/3	L30 4/-			ILD5	3/6	615	3/6	IZEI	22/6	813	67/6	3A/1481 45/
DA30 12/6		6/-	MH4 3/6	RK34	2/6	iR5	61.	615 G	3/-	12H6	2/-	815	40/-	3J/170/E 63
DAF86 8/		4/-	MHL4 3/9	5P2	4/-	155	5/9	616	4/3	12J5GT	3/6	816	30/-	3J/192/E
		5/6	ML4 4/-	5P4B	7/6	IT4	41.	617	7/6	12K8GT		827A	35/-	£37.10
		6/10	ML6 6/-	SP13C	4/6	2A3	8/-	6K6GT	6/6	12SA7	7/6	829A	30/-	723AB 45/
			MPT42 5/3	5P21O	41-	2A5	8/-	6K7G	2/3	12SC7	4/6	832	15/-	723AG 50/
DET5 15/		9/-	M5/PEN 6/-	SP41	2/6	2A6	7/-			125G7	6/6	843	7/6	
DET19 2/6		7/9	N34 8/-	SP61	2/-	2034	2/6	6K7GT	4/9 5/9	125H7	3/-	861	15/-	726A 27 /0 ACT2 5 40 /
DET20 2/6		3/6		STV280		2D4A	4/-	6K8GT	8/3	12517	6/-			
DF70 9/		4/6		31 4 2 80	12/-	2D4A 2X2	41-		8/6	125J/	4/-	866A 930	12/6	
DF72 7/6		7/6	NT37	6112150				6K8M					8/-	KR3 45/
DF91 3/		3/9	(4033A) 10/-	SU2150	A 4/7	3A4	5/-	6LSG	6/-	12SL7	7/-	954	2/-	VX7110 15/
DF96 8/		8/-				3B24	3/-	6L6	9/-	125N7	8/-	956	2/-	WL417A 151
AND MAI	HTO YE	ERS I	N STOCK, I	NCLUD	ING (CATHO	DE R	AY TUB	ES A	ND SPEC	CIAL	VALVES	S. All	U.K. Order
below	10/-, P. &	P. I/-	; over 10/-, 1	6; Order	s ove	r £2, P. &	P. fi	ree. C.O.	D. 2/-	extra. O	verse	as Postag	e extr	a at cost.
				_								_		

Marconi CR-100 Communication Receiver. 60 kc/s to 30 Mc/s, in very good condition, £25. Carriage 30/-.

T.C.S. Receivers. Made by Collins of U.S.A. In fully guaranteed working condition. 1.5-12 mcs. Line up: 12SA7 (1), 12SQ7 (1), 12A6 (2), 12SK7 (3). Power requirements 12 v. L.T., 225 v. H.T. £11.10.0. Carriage 12/6.

Eff.10.0. Carriage 12/0.

Specially Built Power Pack for the above. 230 v. A.C. mains, including 6X5GT valve, £3.10.0. Carriage 5/-.

Transmitter/Receiver No. 22. 2 mc.

Transmitter/Receiver No. 22. 2 mc. to 8 mc. Built almost exactly as No. 19 set but much more economical in battery consumption. Complete in fully working condition with power pack for 12 v., Headgear and Microphone assembly and Key, £9.19.6. Carriage 15/-. Brand new original spare parts

for AR88 Receivers.

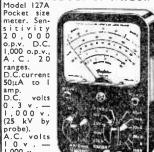
Please write your requirements.
Low Resistance Headphones, brand
new. Balanced Armature DLR, 7/6.

new. Balanced Armature DLR, 7'6. P. & P. 1'-Telephone Handset. Standard G.P.O. type, new. £1. P. & P. 1/6.

type, new. 61, P. & P. 1/6.
S.C.R. 522 Receivers (BC624) 100-156
Mc/s, including all valves, 25'-, P. & P. 5/-,
H.T. Chokes made by Bendix Radio
(U.S.A.), 3 Henrys 0.600A D.C. 25 ohms
D.C. resistance (8,000 v. R.M.S. 60 cycle
test, £1,12.6, P. & P. 6/-, Ditto 10 Henrys
250 A D.C. 90 ohms resistance 1,500 v.
R.M.S. 60 cycle test, 16/6, P. & P. 3/6.
Throat Microphones T 30 (U.S.A.),
3/6, P. & P. 1/6.
Carhon, Inset Microphone, G.P.O.

Carbon Inset Microphone, G.P.O. Type 2/6. P. & P. I/-.

NEW PRODUCT OF TAYLOR



ranges. D.C.current 50μA to amp.
D.C. volts
0.3 v.—
1,000 v.
(25 kV by probe). A.C. volts 1,000 v. 3 resistance

ranges from 0-20 megoh megohms (self contained). 40μA 3½in. arc. Accuracy D.C. 3% A.C. 4%, ohms 5%. Dimensions 5¾in. x 3¾in. x 1¾in. weight 14 ozs. Price £10 complete with instruction manual, test plots and clips. Leather case £1.12.0 extra.

Output Transformer in screening can give 9 different ratios 10:1 up to 120:1 for battery receivers or any high resistance pentodes used as output valves, 6/6. P. & P. 1/6.

P. C. RADIO LTD. GOLDHAWK RD., W.12 170 Shepherds Bush 4946

Variometer's for W/S No. 19. Fully tested and working, 12/6. P. & P. 2/6. Filament Transformers. Primary 0.190-210-230-250 v. 50 C. 5ec. 1 2.5 v. C.T. at 10 amps., 2 2.5 v. C.T. at 10 amps., 3,000 v. insulation. Price £219.0. P. & P. 5/-. Primary 0.190-210-230-250 v., 50 C. Sec. 1 10 v. C.T. at 4.5 amps., 4,000 v. insulation £1.16.0. P. & P. 5/-. Primary 230 v. 50/60 c. 67 v. amp. Sec. 1 6.3 v. 1-6 amps.; 2 63 v. C.T. 3 amps.; 3 6.3 v. C.T. 3 amps.; 4 6.3 v. C.T. 3 amps. €1.12.0. P. & P. 5/-.

Ferranti Transformer. Oil cooled, 20/19.5 K.V.A., 3 phase, 50 cycles. Primary 360/380/400/420/440 v. Secondary 2,700/2,900/3,100/3,300/3,500 v., 2.1 amp. Voltage regulation by simple switches on primary and secondary. Weight 1.150 lbs. Price £125.0.0. Carriage at cost.

Primary 500 Transformers. ohms imp. Sec. to match two 805 in push-pull. £1.7.6. P. & P. 5/-.

Vibrator Unit. 12 v./160 v. 35 mA-Exceedingly well filtered and smoothed.

excellent for car radios. New, including 6X5G valve and vibrator, 17/6. P. & P. 5/-. Moving Coil Round Hand Microphone No. 13. 2½in. dia. with press switch, 12/6. P. & P. 1/-.

Complete Set of Strong Aerial Rods (American). Screw-in type MP49, 50, 51, 52, 53, total length 15ft. 10in., top diameter 0.615in., bottom diameter 0.185in., together with matched aerial base. MP37 with ceramic insulator, ideal for car or roof insulator, £2.10.0, post free.

PERSPEX FRONTS

(As on 110; TVs). Heavy, ideal windscreens, etc., traction of cost, 17in. 9/6, 21in., 15/-,

SYSTOFLEX

1-3 mm. assorted colours. Twenty-four 1 yd. lengths, 3/6.

1,000 YDS, ASSAULT CABLE

P.V.C. covered steel, ideal telephone lines, garden-ing. 9/- drum,

MORSE KEYS

V.G. finish, 2/6. Buzzers, 2/6.

INSULATING TAPE

Good quality, half price, 6 rolls, 2/6.

CERAMIC CONDENSERS

Top quality, rock-bottom prices, 3, 6, 8, 8, 2, 9, 10, 12, 13, 16, 18, 20, 22, 26, 30, 33, 35, 47, 50, 70, 82, 100, 110, 120, 130, 150, 180, 200, 500, 350, 450, 470, 500, 300, 700, 755, 800, 1000, 1000, 1000, 2000, 3000, 4000, 5000, 600, 600.

TUBULAR CONDENSERS

Top makes. 350/500 vm. 0.001, 0.002, 0.005, 0.01, 0.02, 0.03, 8d.; 0.05, 0.1, 0.2, 0.25, 0.5, 10d.

ELECTROLYTIC CONDENSERS

4 mfd 300 vw, 1/8; 5 mfd 50 vw, 1/3; 8 mfd 275 vw, 1/3; 8 mfd 450 vw, 1/9; 8-8 mfd 450 vw, 2/8; 25 mfd 50 vw, 2/8; 25 mfd 25 vw, 1/2; 13 mfd 350 vw, 1/2; 32 mfd 350 vw, 1/2; 32 mfd 350 vw, 1/2; 35 mfd 350 v

FERRITE RODS

6 z jin. approx., 2/9 ea.; 6 x jin., 2/9 ea.

BATTERIES

All-Dry, ex-government, 60 plus, 1.5 v., 2/6 ea.; 6 for 12/6; 1 doz. 22/6.

INSTRUMENT KNOBS

White, beautifully finished. fin., 1/-; lin., 1/3; 1jin., 1/6.

RADIO AERIALS Top quality, insuiated, 25ft., 1/- ec., 10/6 doz.

SWITCHES

YAXLEY type. 4 pole, 3 way, 3/3; 3 pole, 4 way, 3/3; 2 pole, 6 way, 3/3; 2 pole, 2 way, 3/3; Toggle, small, 1/9; 5-10 amp rating, 2/3; Spring loaded

COILS

Techtrad Midget Superhet coll sets, aerial and oscillator, long and medium wave, Polystyrene formers, complete circuit, 8/6.

1000 ohm, 10 watt RESISTORS Ideal Smoothing Droppers, 1/3 ea.; 13/ doz.

CARBON RESISTORS

1/4 watt. 3d. ea.: 1 watt and above, 4d. ca.; Close tolerance resistors, 6d. Unless stated on order, mear values will be supplied.

MAINS DRIVEN BELLS 200-250 A.C., incorporates step down transformer.

CHARGING EQUIPMENT

TRANSFORMERS. Primary 0.210/240, 12 v batteries. 1 amp size, 9/9, plus 1/- post. 2 amp size, 14/8, 1/6 post; 4 amp size. 19/-, 1/9 post; 6 amp size, 9/5/. 2/. post. 25/-, 2/- post.

VALVE HOLDERS

International Octal. Old English, 7 pin, B3G (EA50), 3d. ea., 2/9 doz.
Moulded Mazda Octal. 3d. ea., 2/9 doz.
International Octal. B7G, B8A. 6d. ea., 5/- doz.
B7G with skirt, BA with skirt, BA d. ea., 7/- doz.
Breening Caus, B7G and B9A, 6d. ea., 6/- doz.
Poet 1/- doz.

FOCUS MAGNETS

Wide angle with focus control. Single Magnet type, 9/8; Double Magnet type, 12/6. Post 1/-.

DEFLECTION COILS

Standard, wide angle, low impedance, 19/-, post 1/-.

PICK-UP CARTRIDGES

ACOS 22/6 POWER POINT 18/6 AND REUTER 15/-. SONOTONE 17/6

Amazing Value!

STEREO OUTFITS

Consisting or two 3 valve (10f'3, 10P14, UU9) 3-watt mains amplifiers each complete with Sin. loudspeaker in neat bakelite cases with independent controls, together with UAS Independent controls, together with UAS Stereo changer and screened leads. Unrepeatable. £11.10.0

PORTABLE RECORD PLAYERS

COLLARO 4-speed autochanger, 2½ watt high gain amplifier. Super two-tone case. 13 gns. Or case only 59/-. 2½-watt Amplifier complete on baffle with Speaker, \$3,10,0.

TAPE DECKS

B.S.R. "MONARDECK". Latest type, 81 i.p.s., takes 5½10. spools. Slunple controls. 59,15.0 LATEST COLLARO STODIO TAPE TRANSCRIPTOR. Three motors, three speed, 1½, 33, 84 i.p.s. takes 7in. spools, super quality failsh, push button controls. 214,10.0,

CO-AXIAL CABLE

Semi-Air-Spaced low loss, 1-19 yds., 7d. per yd., P. & P. 1/3, 20-30 yds., 6d. per yd., P. & P. 1/9, 50 YD. DRUMS, 24/-.

CONNECTING WIRE

25 ft. P.V.C. insul., excellent (Scolls, diff. colours, 4/8) (Gork AKIT: Consisting of Tuning Heart, assembled, with lat I.F. Transformers. Second FM. AM and Discriminator Transformers, complete kit. Comprehensive instruction booklet supplied. Booklet only 2/-; Kit. with ECQES valve, £3.13.6; Kit, less ECCES valve.

SOLDERING IRONS

50 watts, 45° pencil bit, 16/9.

SPARES FOR OLDER-TYPE SETS

Frame Output Transformers. Blocking Oscillators. Line Output Transformers. Scan Coils, Focus Coils, etc., cta. (Send S.A.E. for Enquiries).

SUPER STEREO KIT

Two Midget Amplifiers ww. Control Unit, Separate Power Pack. Voltage selection Panci. 5in. Loudspeaker. Double Push Button Switch. Indicator Light. The Kit 59/8, P. P. 3/8.

JASON TUNER KIT

FMT1 . £6.15.0. Less Power Pack. FMT3 .. £9.15.0. Less Power Pack.

UNIVERSAL VOLT OHM MULTIMETER

Reads A.C. D.C. Volts to 1000. 5 Ranges at 1000 ohms per volt. D.C. current 3 Ranges to 500 millhamps. Resistance Reading to 200K in 2 Ranges. Complete with Prods. 52/6. P.P. 1/6.

BATTERY CHARGERS

6 v. and 12 v. 4.5 amps, 49/8; 6 v. and 12 v. 3 amps, 75/-; 6 v. and 12 v. 5 amps, 99/-. P.P. 3/-.

POTENTIOMETERS

100 ohm jin. sp. 200 ohm w.w. jin. sp. 250 ohm w.w. jin. sp. 500 ohm w.w. lin. sp. 500 ohm preset lk jin. sp. lk small jin. sp. 1k preset lk preset lk w.w. lin. sp. 2k d/p switch 2k w.w. preset 2k small preset

2k lin. sp. 5k w.w. lin. sp. 5k w.w. preset ok w.w. preset 10k in. sp. w.w. 10k in. sp. 10k preset 20k in. sp. 20k lin. sp. 20k w.w. preset

250k preset 500k preset in. ohm preset m. ohm lin. sp. 1.5 m. ohm 2 m. ohm preset
5 m. ohm only
25 m. ohm w.w. preset 22k w.w. preset 25k 1 lin. sp. 25k preset 25k preset 25k jin. sp. 25k lin. sp. 25k preset small 50k lin. presets 50k lin. sp. 60k preset 100k lin. sp. 100k lis.

200k pres

CABY MULTI-METERS

Inclusive of Test prods, Batteries, Instrn. Book. MODEL A-10. 2k ohms/v. 10 ranges of voits, current, resistance. \$2.15.0, post 276. MODEL B-20. 10k ohms/v. on 0.5v. and 2.5v. 4k ohms/v. on (10v. to 1000v.) 19 ranges. 4k ohms/v. on £6.10.0, post 2/6

NEW METERS

0-500 Micro amp m.c.	2in.				19/-
0-1 ma m.c. 2in.			.,		19/-
0-30 ma m.c. 2 in.		• •			15/~
0-500 ms m.c. 2jin.		• •	• •		15/-
0-4 amp hot wire 2 in	ke			• •	10/-
0-20 amp m.c. 2in.			0.7		9/-

RECORDING TAPES

5in. 600ft., 18/-; 5in. 900ft, 18/6; 5\{in. 1200ft, 23/6; 7in. 1800ft., 35/-.

"MYLAR DUPONT" TAPES

5in. 1200ft., 37/6; 7in. 1800ft., 44/-: 7in. 2400ft, 60/-. All post 1/-.

CAR RADIO AERIALS

Telescopic. Heavily chromed, complete with mounting equipment. 22/6.

CAR RADIO KITS

Transistorised, M/L waves. No vibrator. 12 volt small. Can be built for £12.19.0.

BBC/ITA AERIALS

3 Element combined, 31/6. Post 2/6.

LINE OUTPUT TRANSFORMERS

Most types available. State make of receiver.

TRANSFORMER FILAMENT

230v. Primary: 6.3v.-1.5 a., 6/8; 210v.-240v. Primary: 6.3v.-2.75a., 8/*. Post 6d.

J.B. DIAL ASSEMBLY

Type SL16, a General Purpose Blide Rule Drive for FM/VHF units, Short Wave Converters, etc. Printed in three colours on aluminium with a 0-100 scale. Provision is made for individual calibrations. Travel of pointer ### \$\frac{1}{2}\text{in}\$, scale plate 7 x 4\frac{1}{2}\text{in}\$, scale aperture 5\frac{1}{2}\text{x 1\frac{1}{2}}\text{in}\$. Normally 11/8.

MIDGET MAINS

230v. Primary. 220v.-30 m.a. and 6.3v. 1ja. Standard, 9/-. As above, Drop through mounting, semi-shrouded, 10/6; Fully shrouded, 11/-.

TOOLS

TWIST DRILLS. Set of 9 in plastic case, 1/1e-lin.,

SCREWDRIVERS. Reversible blade, Phillips No. 1 and 2. Clear plastic handle. 2/9.

RADIO PLIERS. Gun finish. 5 jin., 3/11; 6 jin., 4/6.

MINIATURE DYNAMIC SPEAKERS

A must for all build-it-yourself hams. As supplied with all current transistor kits. Can also be adapted for homes phones or inter-com. 2in. diameter resistance 70 ohms. 448. Post 64

CRT HTR ISOLATION TRANSFORMERS

New improved types, low capacity, small size and tag terminated, Prim. AC 200/250v. Secondaries Nil, +25%, +50% BOOST for 2v., 4v., 6.3v., 12v. or 13v. Tubes. 12/8 each.

POSTAGE MUST BE ADDED UNLESS OTHERWISE STATED

12 MONTHS BRAND NEW

TYPES

MW31/74 £4-15

MW36/24

£5-15

MW43/64

£6-15

FURTHER HUGE PURCHASES DIRECT FROM SOURCE

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TABLE MODELS, FAMOUS MAKERS. Complete with al valves and tubes. Unequalled in value. They are untested and not guaranteed to be in working order.

AMAZINGLY POPULAR-IDEAL SECOND SETS

- £3.19. (P. & P.)

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12" 5 CHANNEL TV'S 45/- $\binom{p_1 & p_2}{12/6}$ 14" 5 CHANNEL TV'S 85/- (P. & P.)

STAAR GALAXY SPARES

Huge quantity (Autochangers). S.A.E. enquiries. Record Players Carriage 4/-

GARRARD 4-speed 4/546 ... GARRARD RC120D Mk. II £5 19 0 .. £9 17 6 .. £7 19 0 B.S.R. (UA14) Autochanger B.S.R. (UA14) Autochanger EMI 4-speed stereo B.S.R. (UA8) Autochangers £6 15

4-SPD. RECORD PLAYERS Latest B.S.R. TU9 Turntable, together with 3 lightweight Staar Galaxy dual sapphire crystal turnover pick-up head Truly

amazing value £3.10.0 Carr. GALAXY PICKUPS, as above, only 19/6.

External ITV Converters with power pack

Very compact. Gain and Listed at £7.7. OUR PRICE 39/-Hammered finish. Very Trimming controls.

DIODES General purpose, tanous make, 8d.

8/- doz. GEX44 type, 3/8. **TRANSISTORS**

DIRECT FROM OUR FACTORY

Due to the increasing demand for our wide range of CRTs and our efficient handling methods we offer unheatable value.

REGUNNED TUBES have new Guns Getters, Aquadac Coating Bases, etc.

TOP QUALITY GUARANTEED
6 MONTHS 12 MONTHS
ance 12/6 REVACUUMED REGUNNED Carriage and Insurance 12/6 GRIFIAGE 280 MW22-7. MW22-14, MW22-14C, MW22-17. MW22-18
12KPA, 121K, C12B, CRM121, CRM121A, CRM121B, CRM12B, CRM121B, MW31/14C. MW31/16, MW31/18, MW31/14C. £1-10 £3 £2 £4 141K. 7201A C14FM. CRM141, CRM142, CRM143 MW38-24, MW36-44 17A5P4. 171K. AW36/21, C17FM, CRM171, CRM172. MW43-64, MW43-69 £2-10 £4-10 ли ч за-оз. л. w 43-ч9 7401A. A W45-80. C14BM, C17BM, CRM151. CRM152A. CRM182b. CRM153. CRM173. M W 43-80. M W 41-1 A W 53-80, CRM212. M W 58-20, M W 53-80 £3 £5-5 £4 £6-10

PLEASE NOTE: Many other types not listed available. S.A.E. enquiries. SPECIAL OFFERS

UA8 Stereo Changers

B.S.R. tamous Monarch autochangers, with quality stereo cartridge.

Truly anazing value. fitted £6.19.0

MAINS AMPLIFIERS

3 valve (10P3, 10P14, UU9), 3 watt, 8in. speaker, in two tone cases with controls, Ideal for record players, P.A. work, etc. 49/-Loutispeakers

TOP MAKES—MANUFACTURER FRESH
2½m., 18/-; 3½m., 18/-; 3½m., 18/-; 5½m., 18/-;
4½m., 18/-; 8½m., 18/-; 9½m., 18/-; 25/6;
7 x 4½m. elliptical, 18/-; 9 x 6½m. elliptical, 22/6;
10 x 6½m. elliptical, 23/6; 8m. 84ertorian 15 ohms
HF810, 70/-; 10½m. Stenfordan 3-7-5-15 ohms
HF810, 70/-; 10½m. Stenfordan 3-7-5-15 ohms
HF1012, 90/9; 12½m. Closed Field, 27/6,
STOP PRESS, 8 x 13½m. Speakers, 22/6.

PM SPEAKERS Surplus 3 ohm

Tested, to, top makes, performance guaranteed.

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RECTIFIERS

For Chargers, scientum, full wave, 12 volt, 3-4 sups, 9/6; (Carr. 1/-); 250 v. 80 mA. 5/-, kM1, 9/6; KM2, 9/-; RM2, 9/-; RM3, 15/6, RM5, 21/-; 14486, 17/-; 14487, 23/-; 144100, 25/-; 16RC1-14-1. 7/6; 18RD2-2-8-1, 14/-; 14RA1-2-8-2 17/-: 14RA1-2-8-3, 20/-.

6/6 RESISTORS 100 10/-100 CONDENSERS

Miniature Ceranic and Silver Mica Condensers.
3 pF to 5.500 pF. List VALUE OVER 65.
VALUES ALL GUARANTEED 3 MONTHS
PL81 SOILED 4/6 EY51 SHORT 4/6

TV PROJECTION UNITS

Complete Standard Philips optical units with Mullard MW6-2 projection tube 100 40 4 Mullard MW6-2 projection tube (untested) at a fraction of cost.

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38 Megs at 29/-, 16 Megs at 39/-. Complete with Valves PCC84, PCF80. Famous make.

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VALVES 10% DISCOUNT SPECIAL TO PUR OFFER

NEW LOW PRICES GUARANTEED 3 MONTHS

FREE TRANSIT INSURANCE. All valves are new or of fully guaranteed ex-Government or ex-equip-ment origin. Satisfaction or Money back Guaran-tee on goods if returned unused within 14 days.

10% DISCOUNT TO PURCHASERS of any 81% VALVES marked in black type (15% in dozen). Post: I valve, 6d., 2-11, 1/-. 4/9 N 108 8/6 N 152 9/3 P41 9/8 P61 18/- T41 7/6 UF41 10/6 TH30C 12/6 UF42 4/6 U14 8/- UF80 2/3 U18 8/6 UF85 OZ4 5/6 6AM6 1A5GT 5/- 6AQ5 1A7GT 11/9 6AT6 1C5GT 9/9 6AU6 3/6 6J7G 6/- 6J7GT 7/- 6J8 7/9 6K6GT 8/9, 12E1 8/6 DAF91 7/6 DAF96 6/9 EL91 5/9 EM34 074 5/6 6X2 7/9 6X4 8/6 6X5G 12/6,35Z5GT 5/3 ECC35 7/9 ECC81 9/9 ECC82 1/- ECC83 7/8 ECC84 5/6 12J5GT 3/6 42 5/6 12K7GT 5/6 13 6/- 12K9GT11/6 50C5 6/9 8/- 1 P80 8/6 1 F85 9/-DF33 6/6 8/6 6X5GT 5/9 7A7 2/8 7B5 5/- 7B6 EM81 9/6 DF91 71-9/-12K8 12/6 50L6GT 9/3 DF96 12Q7GT 5/6 53KU 10/6 DH63 12SG7 6/- 54KU 8/9 DH76 12SJ7 5/6 616PT 11/-1D5 1D6 EMSA 9/9 PABC8011/~ PCC84 7/6 1122 6/9 1186 19/6 3/9 ECCS5 7/6 15/-EM85 12/6 8/3 7/8 13/6 UL41 1H5GT PCC95 9/6 128G7 7/3 128J7 5/6 ECF80 7/- ECF82 9/3 U25 U26 8/8 **EN31** 18/-EY51 PCC88 19/-8MALL 8/9 PCC89 18/9 EY86 8/- PCF89 7/6 11.4 7/- ECF82 11/9 ECH21 9/9 EV51 11/-12/6 7/3 UL46 8/9 UL84 1'31 1LD5 5/6 75 8/6 77 9/6 78 DK22 9/9 198 K 7 9/6 81. 12SN7GT 8/6 12Y4 9/6 1LN5DK91 8/6 ECH42 7/9 ECH51 EX36 8/-7/6 U35 IN5GT 1R5 DK92 PCF92 PCL82 9/9 6BJn 6/- 6BR7 8/6 6BW6 5/3 6BW7 4/- 6BW6 4/6 6C4 5/6 6C4 8/6 UM80 UU6 DK36 DL38 E740 8/6 U43 14/9 80 7/6 1487 8/8 8/8 EZ40 7/6 EZ41 19AQ5 7/6 80 19BG6G15/- 90AV 20D1 9/6 117Z6 8/9 ECL80 PCL83 11/6 PCL54 9/9 8/-9/6 9/6 1150 6/- 007 185 DL35 9/8 ECL83 EZS0 EZS1 9/9 052 4/6 1:118 25% 6/3 PEN25 7/- PEN45 8/9 PEN46 111.52 14/6 5/6 6L19 5/6 6L19 6LD2 20D1 20F2 20L1 20P1 5/6 UY1N 5/6 UY21 11/-10/6 1176 9/6 155BT 13/6 723A 11/6 807A D1.91 EF22 EF36 GT IC 16/-6/- EF36 7/- EF39 7/9 EF40 9/6 TY41 5/8 U191 3A4 DL92 3/3 GZ32 12/6 6/8 PL38 PL36 PL38 6139 724 4/3 9/-7/6 5/-G 2.37 10/6 U281 U282 9/6 U Y 85 6/9 8/6 20P3 1/- 20P4 12/6 S07E 13/6 HL41DD9/6 15/-12/6 VR105/30 8/9 C 6G 18/6 6LD12 6LD20 6N7 8D3 10C1 7/6 3Q5GT 7d. EF41. 7/6 EF42 8/6 7/8 EA₃0 14/6 (1309 11/- 20P4 9/- 20P5 6/9 25A6G 10/8 25L6G 24/- 808 16/- 954 8/- 955 15/-2/-3/9 EABCS0 7/6 EAC91 4/9 EAF42 8/6 HVR2 7/8 7/-6/- He 7/- D1 9/6 D: 5/- D 9/8 D 384 9/8 H6 9/3 KL35 KT32 KT33C 10C14 11329 12/6 4/9 EF50-BR 2/-8/6 EF50-USA VR150/30 10F1 10F9 PL82 7/6 U339 7/6 U403 11/-25A6G 5/6 W61M 11/-W76 5/6 6P1 14/-5R4G 3/9 3/8 6P2 12/6 6P29 4/9 6Q7G PL83 PL84 6/9 956 6/6 2/9 11/-9/9 U404 6/6 9/9 U801 26/-16/-UABC80 8/9 2/8 CAR12 9/-1,6 7/- EF54 3/9 EF80 5TI4G **EB34** 918 25L6GT 25Y5G KT86 KT44 KT45 10L14 9/- 5763 9/- 9001 9/-9/6 10/- EB41 PM 80 PX 25 5 V 4 G 12/B 5Y3G 5Y3GT 10LD3 41-W77 4/9 6/6 BF1 EB91 EBC3 4/9 4/-2/9 5/3 10LD12 8/9 25Z4G 7/3 9002 8/- 0003 9/- ATP 8/6 607GT W 81 9/2 9/- EF95 5/- EF96 PY31 PY32 F6M 7/- UH41 8/- X61 6/6 UBC41 8/3 X63 6/8 UBC81 10/- S66 6/9 UBF59 8/6 X66 8/- UBL21 14/6 X78 12/- UCC84 14/8 X78 6/8 KT61 KT63 CAF42 9/-8/-9/6 25Z5 9/6 25Z6 10/3 9/-6/6 X61M X63 5 Y 4 G 687G 7/6 12/6 7/-3/6 6/9 6SA7 10P14 PY81 9/6 11/-8/6 HF13 **EF89** 81-10P18 278 U 16/-16/- AZ31 7/6 B36 9/- EBCS1 8/6 EBFS0 KT65 12/6 68G7 68H7 68J5 574G 4/9 4/6 2/9 EF91 8/6 EF92 3/8 4/9 30C1 574GT 11/-12A6 5/3 4/9 EBF59 8/6 5/0 CBL31 21/-7/9 CCH35 17/6 EBL21 14/-2/6 CL33 18/-8/- D63 1/6 EC52 3/6 7/9 D75 KT76 KT81 9/6 PY82 PY83 P/6 6514 12AH7 6/8 30F5 7/- 865 9/6 CBL31 14/-6A7 10/- 6F15 6A8G 8/6 6F16 6A8GT 18/6 6F33 9/6 8/6 7/9 KTW61 4/6 KTW63 9/- KTZ63 8/6 L63 11/6 LN152 5/6 PZ30 4/9 R18 5/6 R19 2/9 SD6 5/3 12AH8 30FL1 68 8 7 EK 32 12/-12/6 UCC84 14/6 12/6 UCC85 8/-12/6 UCF80 17/-8/6 8/6 6817GT 8/- 6817GT 8/- 6817GT 4/3 6887 12AT6 12AT7 7/9 30F1 5/9 30P4 E1.32 16/6 6/-| 12AT7 | 4/3 | 6887 | 5/3 | 12AT7 | 4/3 | 6887 | 5/1 | 12AX7 | 2/9 | 5114GT | 10/6 | 12BA6 | 4/9 | 615G | 6/3 | 12BE6 | 4/4 | 646G | 5/6 | 12BH7 | 7/9 | 646T | 6/6 | 12BH7 12/6 3/9 EL33 6ABS 18/- EC52 1/6 EC90 3/9 EC91 8/3 6G6 4/3 6H8 Y63 6/3 3/6 EL35 4/8 EL37 9/6 EL38 4/- EL41 6/6 30112 8/-8/6 11/6 8/-263 5/3 8/9 UCH21 14/6 2/6 UCH42 7/9 7/6 SP8 7/6 SP41 8/- SP61 7/-7/9 D77 10/6 D152 64(15 9/6 4/3 6J5 Z66 30PL1 6/6 ECC31 12/6 ECC32 2,6 ECC33 LZ319 MU14 8/ J5G 6/9 3GT 12/6 UCH81 8/6 Z77 6AG7 8/6 12BE6 8/9 351.6GT 9/- DA30 12BH7 10/6 25W4 6/9 DA90 12C8 8/6 35Z4GT 5/6 DAC32 8/6 2/6 11/- SU25 15/- UCLS1 11/3 Z152 15/- SU2150A4/6 UCLS3 18/8 Z719 5/8 4/9 EL42 9/- EL44 9/6 N37 7/- N78 BALS 5/2 9/9 ECC34

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RECORDERS. THEY ARE COMPARABLE TO THE MUCH HIGHER-PRICED MODELS

MODEL CR3/S Incorporates the new COLLARO"STUDIO" TWINTRACK 3-speed Deck LP. Terms: Deposit £7.18.0 and 12 months of £39.10.0 £2.17.11.

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All prices quoted provide for the COMPLETE RECORDER including CRYSTAL MICROPHONE and 1,200 ft. Spool of Tape.

Each Model incorporates the highly successful HF/TR3 Amplifier (described opposite) thus ensuring truly "Hi-Fi" record and playback facilities.

There are no better value-for-money Tape Recorders on the market—if you can't call and hear them, send S.A.E. for fully descriptive leaflets.

TAPE AMPLIFIERS and PRE-AMPLIFIERS PRESENTED FROM MULLARD

MODEL HF/TR3 TAPE AMPLIFIER
(Mullard Type "A" design)
A very hith quality Amplifer
incorporating "speed the lee
equalisation, using the late
FEROXCUBE FOT
INDUCTOR FOR COLLAROTRUVOX-BERNELL-WEARITE or MOTEK Tape Decks,
has GILSEN Output Transformer. Includes separate former. Includes Power Supply Unit. KIT OF separate £12,15,0

£12.15.0 OR ASSEMBLED H.P. Deposit £3.6.0 and 12 months at £1.4.2. £16,10.0 MULLARD TYPE "C" TAPE PRE-AMPLIFIER— ERASE UNIT

The "H-f" link to add full tape recording facilities to High Fidelity home installations. Incorporates FEROXCUBE POT CORE INDUCTOR FOR WEARITE-COLLARO-TRUVOX-BRENELL or MOTEK TAPE DECKS. Includes separate power Supply Unit. OR ASSEMBLES INCLUDED TO SEPARTS \$14.0.0 H.P. \$28.8.0 Deposit and PARTS \$14.0.0 H.P. \$20.8.0 Deposit and P

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together with the COLLARO "STUDIO" DECK
As above but with HF/TR3 supplied ASSEMBLED
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FOR THE HOME CONSTRUCTOR SPECIAL 'COMBINED ORDER' PRICES

The COLLARO "STUDIO" TAPE DECK and our Mullard Type "C" PRE-AMPLIFIER and POWER Unit Assembled and Tested.

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The TRUVOX Mk. VI DECK and the assembled Type "C" Pre-amplifier and Power Unit. H.P. Deposit 28-06, and 12 months 22-18-8. H.P. Deposit 28-06, and 12 months 22-18-8. As above but Type "C" as complete KIT OF (d) (a)

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Type "C" PRE-AMPLIFIER and POWER UNIT
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(Carriage and Insurance on above quotes 10/- extra.)

EACH OF THE ABOVE CAN BE SUPPLIED IN A PORTABLE CASE THUS FORMING A COMPLETE PORTABLE PRE-AMPLIFIER. FULL DETAILS ON REQUEST.

LARGE PURCHASE OF BRAND NEW AND FULLY GUARANTEED TRUVOX and GARRARD TAPE EQUIPMENT ENABLES THESE OUTSTANDING PRICE REDUCTIONS

£35.0.0

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The "MODEL HF/G2R" PORTABLE TAPE RECORDER (Original Price £33.0.0)

FOR ONLY 22 gns.

H.P. Dep. \$4.14.0. 12 months
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Incorporates THE LATEST
TAPE DECK MAGAZ HIGH
QUALITY AMPLIFER which
is entirely based on the very
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DESIGN and specifically developed
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Operates a Twin Track Recorder operating at 3 flin/sec, sneed and
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The "MODEL TK/MkIV" PORTABLE TAPE RECORDER

PORTABLE TAPE RECORDER
(Original Price £49.10.0)
FOR £36.10.0 Price includes a 7-ONLY £36.10.0 Spool of EMI Lapel
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Macorporates the Truvox MkIV
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Typ and peaker and the Truvox
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rectly operate their MkIV Tape
Deck, As a result we are able to present
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A Twin Track Two Speed model operating at 31 and 71 in/sec,
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(Prevents accidental erasure). Ext. Speaker output, tone and
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COMPLETE KIT OF PARTS-

MULLARD "5-10" MAIN AMPLIFIER

For use with the MULLARD 2-valve pre-amplifier with which undistorted power output of up to 10 waits is obtained. We supply SPECIFIED COMPONEATS AND NEW MULLARD VALVES, including PARMICO MAINS TRANSFORMER and choice of the latest Ultra-Linear PARMERO or the PARTHERO or the PARTHERO 6 the PARTHERO E OUTput Transformer. PRICE COMPLETE KIT (PARMERO Output \$10.00 £10.0.0

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£11,10,0

ABOVE INCORPORATING PARTRIDGE OUTPUT TRANSFORMER, £1.6.0 EXTRA

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Employing two EF86 valves, and designed to operate with the MULLARD MAIN AMPLIFIERS, but also perfectly suitable for other makes.

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PRICE COMPLETE \$6.6.0 ASSEMBLED AND TESTED \$8.0.0

Supplied Strictly to MULLARD'S SPECIFICATION and incorporating:

Equalisation for the latest R.I.A.A. characteristics.

Input for Crystal Pick-uos, and variable rejuctance magnetic types.

Input (a) Direct from High Imp. Tape Head. (b) From a Tape Amplifier or Pre-amplifier Sensitive Microphone Channel. • Wide range BASS and TREBLE Controls.

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The popular and very successful complete "5-10" incorporating Control Unit providing up to 10 walls high quality reproduction. Only Specified Components and now MULLARID AALYS are supplied including PARMEKO MAINS TRANSFURDERS and choice of the latest PARMEKO OF PARTRIBGE Specified Components
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THE "ADD-A-DECK"

Incorporating
GARRARD "MAGAZINE"
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Supplied on ONE CHASSIS (as illustrated) READY FOR USE

FOR USE (Carr. & Ins. 101- extra). Price includes Garrard Magazine and a 4in. Spool Double Play Fupe Price includes Garrard. Magazine and a 4m. Spool Daubie Play Turbe. He Deposit \$23.60. and 12 months of \$2.7.8. Frovides Complete tape recording facilities and designed to a facilities and designed to a facilities and proceeding to the state of the sta

Pick-up. THE NEW B.S.R. Model UAI2 in Stock. A4 "SPEED"

MIXER AUTOCHANGER.
UAI2 also available incorporating the STEREO Pick-up, plays L.P. and 78 Records.
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This model incorporates two Mullard 2-valve Pro-Amplifiers



Amplifiers
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ULLARD'S SPECIFIInto a Single
Unit e naling it to be used for both STEREOPHOVIC or MONAURAL operation. It
is designed primarily to operate with our
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200 m/volts. E KIT £12.10.0 ASSEMBLED AND TESTED THE BOOK AND TESTED THE BOOK AND TESTED THE BOOK ASSEMBLED THE BOOK COMPLETE KIT £12.10.0 £15.0.0

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powered with Cathode " Self tell powered with validite phower output. Incorporates two inputs for MICROPHONES one for CRYSTAL PICK UP and fourth for RADIO or TAPE

£8.8.0 % Complete Kit of Parts



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MODEL I.I., one microphone Input matched for moving coil or Ribbon Mike. £1.17.0 extra.

FM TUNING UNIT Mk.11 "Fidelity"

An attractively presented Unit incorporating MULLARD PER-MEABILITY TUNING HEART and corresponding Mullard valve line up. FOR THE £10.10.0 ASSEMBLED £14.5.0

A SPECIAL CASH OFFER!!

This very attractive PORTABLE AM-PLIFIER CASE together with a good quality GRAM AMPLIFIER and a matched P.M. SPEAKER. For ONLY £8.7.6 (Plus 7/6 Carr. & Ins.)

The amplificr consists of a 2-stage design incorporating 3 modern B.V.A. adves und has separate BASS and TREBUE CONTROLS.
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£4.2.6 £3.17.6 (c) 6in. P.M. SPEAKER 18/9 Carriage and Insurance 4/- orter



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AMATEUR TRANSMITTER Model DX-100U Covers all amateur bands from 160-10 metres. Self-contained including Power Supply 579-10-0 Modulator and V.F.O.

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VAR. FREQ. OSCILLATOR VF-1U From 160-10 m. Ideal for our DX-40U and similar transmitters. Price less valves £8.19.6. £10.12.0 £10 12 0

R.F. SIGNAL GENERATOR, Model RF-1U Up to 100 Mc/s fundamental and 200 Mc/s. on harmonics and up to 100mV. output on all £11.11.0 bands.

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Portable 23/4 in. SERVICE 'Scope Model OS-1 Portable 234 in. SERVICE Scope Model Con-Compact portable scope ideal for servicing and general work. Y amplifier sensitivity 10 mV/cm; response ±3 dB 10 c/s-2.5 Mc/s. Time base 15 c/s-150 kc/s. Printed circuit. Case 73 x 43 x 12 in. long. £18.19.6

5 in. OSCILLOSCOPE Model 0-12U Has wide-band amplifiers, essential for TV servicing. F.M. allgnment, etc. Vertical freq. response 3 c/s. to over 5 Mc/s. without extra switching. T/B covers 10 c/s to 500 kc/s. in 5 ranges. £34.15.0 covers 10 c/s to 500 kc/s. in 5 ranges.

RES.-CAP. BRIDGE Model C-3U RE3.-CAF. BRIDGE MIDGE CSUMMASSURES capacity 10pF to $1,000\mu F$ 100Ω to 5 M Ω and power factor 5-450 v. test voltages. With safety switch. resistance

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Practical Windows

YOL. XXXVI No. 649 MARCH, 1961

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ANOTHER FREE BLUEPRINT

N the next issue of Practical Wireless, the first of a new series will appear on constructing the "P.W. Roadfarer". This is an A.M./F.M. Receiver which is transistorised throughout. Its advance design allows it to be operated either from its own internal batteries or direct from the domestic mains supply. Printed circuits have been used and the construction of the receiver should therefore possess few difficulties even for the inexperienced constructor. The set is constructed in four main sections: the A.M. tuner; the F.M. tuner; the audio amplifier and the main power supply unit. The complete receiver is housed in an attractive plastic cabinet of small size which contains a ferrite rod aerial for A.M. reception and also a telescopic aerial for F M.

Each copy of the April issue will contain a free blueprint of the "Roadfarer"—normal price 5s. 0d.—which will give the complete circuit diagram and components list and other information necessary to build the set. Be sure to order your copy NOW.

The P.W. Signal Generator

THIS issue contains the first article of a new series on the progressive construction of a wide range Signal Generator which will provide all the facilities required by the amateur radio enthusiast and will stand comparison with many of the designs for the amateur which are now on the market. The series is written by E. V. King—the author of two popular, constructional series which have previously appeared in this magazine. Whilst the performance of the Signal Generator is excellent, great care has been taken in the design to minimise the cost of construction and together with the progressive constructional system used, enables the cost of the unit to be spread over as long a time as the constructor desires. The Generator is constructed in four chassis and if required one or two chassis may be omitted if the constructor has no use for the facilities which they would provide.

Talking Books for the Blind

TALKING books for the blind have been used for some years but now a new library of tape recordings is being accumulated to replace the long-playing gramophone record A revolutionary type of play-back machine will be used which possesses a number of basic advantages over the present disc reproducer, the result of almost twenty-five years' research and development by the R.N.I.B. and St. Dunstan's. Amplifier, loudspeaker and drive mechanism are housed in one compact case, controls have been reduced to one On Off-Volume switch and one Start/Stop lever.

The truly unique feature of the machine, however, is the tape cassette. Little larger in size than an average letterpress novel, this can contain up to twenty hours recorded speech. This has been achieved by the use of half-inch tape and recording on it not two tracks, as on domestic machines, but no fewer than eighteen tracks, which reduces the number of times a tape must be changed and so simplifies matters for the user.

STISCO DI CONTROLO DI CONT

Our next issue, dated April, will be published on March 7th

Round the World of Wireless

POTENTIAL AND CURRENT NEWS

Broadcast Receiving Licences

THE following statement shows the approximate number of Broadcast Receiving Licences in force at end of November, 1960, in respect of wireless receiving stations situated within the various Postal Regions of England, Wales, Scotland and Northern Ireland. The numbers include Licences issued to blind persons without payment.

Region				Tota
London Postal				733,512
Home Counties				688,009
Midland				504.025
North Eastern			2.	555,770
North Western				475.975
South Western				411.298
Wales and Border	Countie	25		245,498
Makel Besterd on			-	
Total England and	1 WAIGS			3,614,085
Northern Ireland	• •			409,088
Mortnern Treiand	• • •	• •		124,137
Grand Total			-	4.147.310

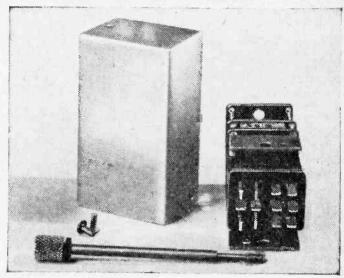
Factory Extensions

FACTORY extensions at Luaton Road, Dunstable, scheduled for occupation in March. 1961, are announced by Erg Industrial Corporation Ltd. The increased floor space will make it possible to increase the output of the wire wound Resistor division. Additionally, new and modern equipment for the now established Erg Transformer division will occupy a large proportion of the new extension, with an enlarged airconditioned, constant-temperature laboratory. Test facilities covering full service requirements will be in operation to ensure the highest degree of reliability.

Erg Industrial, already serving the Electronic Industry with "Custom-built" special products. intimate that strong emphasis is being given to an immediate expansion of this service, for which highly qualified design engineers have been engaged and are solely devoted to this "Custom-built" division.

Dopplers and Automatic Direction Finders

AFTER an exhaustive evaluation, the Ministry of Aviation has selected the Marconi Doppler Navigation Type AD2300B and the Automatic Direction Finder Type AD712 for use in their new



Transistorised plug-in logic units form the basis of the electronic signal interlocking developed by Mullard Equipment Ltd. for British Railways (see page 967).

Argosy C. Mark 1 aircraft for R.A.F. Transport Command.

The doppler order is worth £552.000 and the automatic direction finder order £100.000. Ancillary equipment and spares are included in both contracts.

The AD2300B comprises the basic AD2300 sensor, the 5452 computer and the 5453 display unit. The computer processes ground speed and drift angle from the doppler sensor, together with heading information from the aircraft compass system, and presents to the pilot the aircraft's displacement from selected track and distance to go to the turning point. It also feeds steering information into the flight system and/or autopilot to enable the selected track to be maintained.

The AD712 automatic direction finder is a crystal-controlled ADF embodying a true and positive decade tuning system and a fixed loop aerial system. Frequency selection is by switch: no tuning whatever is required. This equipment is in wide use by many airlines.

Battery Firm Changes

TO achieve closer liaison between their technical, production and sales departments, Chloride Batteries Ltd. transferred the major portion of their sales headquarters from London to the head office and the principal manufacturing centre of the company at Exide Works, Clifton Junction, near Manchester, on January 2, 1961.

Mr A. C. Stewart, the present sales manager, who is approaching retirement age, will not be moving north. He will be succeeded by Mr. M. A. Griffith-Jones on completion of the move, but his services will be retained by the company in the capacity of consultant until he retires.

Export TV for Design Index

THE latest Ekco export television models — the 17in. models T737 and T738—have been accepted by the Council of Industrial Design for "Design Index". The "Design Index" already includes nearly sixty Ekco products and is Britain's record of well-designed goods from which exhibits are chosen for display in the Design Centre.

Tape Recorders for BBC

THE BRC is purchasing two three-track portable and one twin-track console Philips magnetic tape recorders for use in engineering research work.

Negotiations for the order were carried out for Philips by Mr. Terence Perkins, the company's tape recorder section manager.

Silicon npn Diffused Junction Power Transistors

THE Semiconductor department of A.E.I. Radio and Electronic Components division entered the silicon power transistor field with the introduction of three Ediswan Mazda uppn diffused junction type devices. Types XC703, XC713 and XC723 are intended for a wide variety of industrial applications in equipment operating at temperatures ranging from -65°C to +175°C. They are particularly useful in power-switching circuits, oscillator regulator and pulse amplifier circuits, and as Class A and Class B pushpull audio and servo amplifiers:

They are characterised by an extremely low saturation resistance, high current and power dissipation ratings, high Beta at high current, and excellent high temperature performance up to +175°C. At 100°C they offer a range of dissipation of from 2 to 30W. They are available in standard JEDEC cans.

Direct View 3-D Picture Process

FULL-COLOUR 3-D pictures that can be "blown up" to 40in, x 30in, are now being produced for viewing without coloured spectacles or a stereoscope by a new process sponsored by Deep Vision Ltd.

This process is based on the familiar grid system in which each of the viewer's eyes sees the picture through a different set of "windows" — hundreds of extremely narrow vertical slits between invisibly fine opaque lines.

But apart from their size, the Deep Vision pictures can also be brought forward from their frames or set back in perspective—or both. And as in the case of the equally familiar lenticular system (in which vertical corrugations break up the picture into two eye-fields), they can also be made to "change".

Two more advantages are that any number of identical prints can be made in fast colours, and that as 2-D colour pictures can be made simultaneously, magazine advertising, for example, can be precisely matched in 3-D for illuminated display.

The process involves the use of specially-designed camera which, although bulky and heavy, has no single awkward component, and so can be dismantled and reassembled in a matter of minutes for location work.

A shot takes about five seconds to complete, but considerable subjective movement can be tolerated without the picture being spoiled.

Talk-back System for New Tamar Bridge

RIGGERS working high up, on and between the 250ft towers of the new Tamar Bridge - now being built by Cleveland Bridge and Engineering Co. to provide a new road link between Devon and Cornwall—keep in touch with the main control station at one end of the bridge through equipment supplied by Radio Components and Special Products Department, A.E.I. Radio and Electronic Components Division.

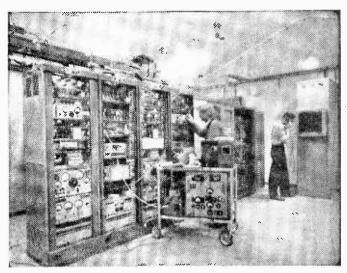
The twin towers of the bridge are 1,100ft apart and the distance between the top of each and two ground stations is 500ft so that communication was required over a total distance of about 2,000ft. To provide this

a transistorised loudspeaking intercommunication system has been supplied. A ten-line master unit, of a type specially developed by A.E.l. to work over a post office line and therefore eminently suitable for this application, is installed in the constructor's main office at one end of the bridge.

British Railways to use Electronic Signal Interlocking

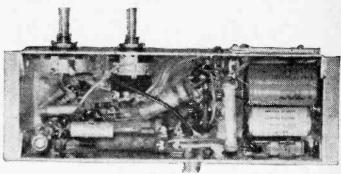
part of the railway's modernisation programme, the British Transport Commission has awarded a contract to Mullard Equipment Ltd. for the development of an electronic signal interlocking plant. equipment will be the first plant using electronic interlocking to be used on British Railways and will replace the mechanical interlocking on the lever frame at Henley-on-Thames Western Region signal box. It will be installed during the early summer of 1961.

Recently the company was able to demonstrate to British Rail-ways' signal engineers a working model of a double junction, completely controlled by the new electronic system. The technique has the substantial advantage that it employs solid state electronic eircuitry throughout.



Final testing in progress at the New Plymouth terminal station of the New Zealand microwave telephone network (installed by STC). The four equipment cubicles on the left are the transmitter and receiver equipments for the "working" and "standby" radio channels. The supervisory VHF radio equipment is in the background.

A MIDGET PUSH-PULL AMPLIFIER



The component layout of this amplifier.

By V. E. Holley

HIS amplifier was built originally for a portable record player. Though modest in size, weight and cost, it has an output of four watts and a very acceptable standard of reproduction.

The Circuit

Fig. 1 shows the circuit; it is largely conventional. The valve, V1, is a resistance coupled pentode voltage amplifier having in its grid circuit

THIS 4W AMPLIFIER IS ESPECIALLY SUITABLE FOR PORTABLE RECORD PLAYERS

the volume control, VR1, and a simple top-cut tone control, C1 and VR2. Matters are so arranged that in the minimum cut position, the tone control has practically no effect on the response, but there is sufficient range to enable the surface noise from the older 78rev/min shellac records to be reduced to inoffensive proportions. R3 is the bias resistor which is by-passed in the normal way by C3; R4, inserted between the

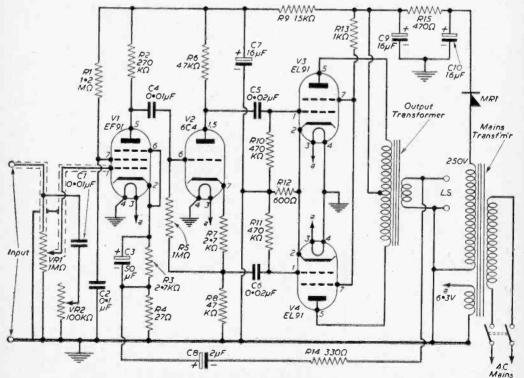


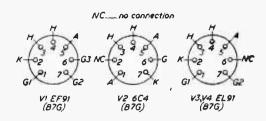
Fig. 1a .- The circuit diagram.

lower end of these components and chassis, provides a point for the injection of negative voltage feedback derived from the output transformer secondary.

Inverter

The amplified signal from V1 is passed to V2, a triode, 6C4, arranged as a phase inverter with

Fig. 1b (right).—The valve-base connections.



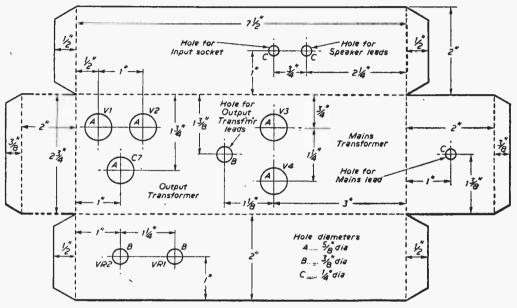


Fig. 2.—Constructional details for the chassis.

equal anode and cathode loads of 47k. Two signals, 180deg out of phase, are thereby produced for the push-pull output stage. A cathode bias resistor of 2.7k and a grid leak of 1M, returned to the junction of the bias and cathode load resistors, complete the stage. Heavy negative current feedback ensures excellent linearity though it limits the gain of the stage to 0.9 on each side, or 1.8 times overall. No de-coupling is necessary between V1 and V2.

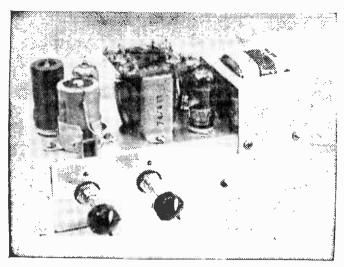
Output Stage

Two miniature output pentodes. EL91, are employed in this stage with 250V on anodes and screens. They should be reasonably well matched but exact matching is not necessary as the common bias resistor tends to equalise them. The optimum load, anode-to-anode, is 24K, so that for adequate low frequency response, an output transformer with unusually high primary inductance is required. Such transformers are not readily available but the difficulty can be overcome by using one of lower inductance and making good the low frequency attenuation by negative feedback. Several small push-pull transformers are available commercially with a primary inductance of 40H

or so and affording ratios of around 80 or 90 to 1 for operating a 3Ω speaker. As the D.C. resistance of the speaker is rather high, there is some loss of volts, at the valve anodes and the resistor R13 is included in the supply to the screens so that the voltage here will not rise above that at the anodes.

Negative Feedback

Heavy negative feedback is taken from the output transformer secondary via R14 and C8, to the cathode circuit of V1. The inclusion of C8 reduces the feedback at the lower frequencies and so allows the gain of the amplifier to rise in the region in which attenuation is introduced by the output transformer. The values of C8 and R14 will need adjustment according to the characteristics of the output transformer. It is suggested that the amplifier be completed with R14 equal to 330Ω and C8 omitted, and that the best combination should then be selected after a listening test under service conditions. The optimum value for R14 will lie between 200 and 600Ω and for C8 between 2 and $8\mu F$. The circuit is very well behaved and none of these combinations will cause instability.



The complete amplifier.

Power Supply

The mains transformer should be of the miniature" type and should have a half wave secondary winding capable of supplying 35mA and a 6.3V, IA heater winding. A contact cooled rectifier is adequate, and mains smoothing is provided by C9 and C10 in conjunction with R15. The smoothing is not lavish, but push-pull plus negative feedback reduces the hum to a very low level. Some additional smoothing is necessary for the supply to V1 and V2 and is provided by R9 and C7.

Construction

The prototype was built on a chassis of 18s.w.g. aluminium sheet measuring $7\frac{1}{2}$ in. x $2\frac{3}{4}$ in. x 2in., a plan of which is given in Fig. 2. There is nothing critical about the lay-out except that to prevent inter-action between them, the mains and output transformers must be mounted so that their magnetic axes are at right angles. There is a little difficulty here if both are of clamp construction but it can be overcome by mounting the mains transformer on its side in the "drop-through" position and securing it with a strap of 18s.w.g. aluminium across the top, the normal mounting lugs being bent inwards out of the way. This method was adopted in the prototype as will be seen from the illustration. A detailed wiring diagram for the amplifier is given in Fig. 3.

Components

No special components are necessary but it is an advantage if the resistors and capacitors are on the small side. The resistors can be \(\frac{1}{4}W \) except R9 and R12 (\frac{1}{2}W) and R15 (1W). R6 and R8 must be a matched pair as also must be R10 and R11. If matching facilities are not available, close tolerance components must be used (5 per cent or better). All the capacitors should be 350VW D.C. except C3 and C8 for which 25VW will be adequate.

Testing

When construction is complete and before switching on, a check should be made with a meter between C10 and the chassis to see that there are no shorts in the H.T. wiring. If all is well the power can be connected and measurements taken of the voltages on the output valve anodes and screens. It should be between 240 and 250V, measured between these electrodes and the cathodes, and some adjustment may be necessary to the value of R15 to make it so, depending on the output from the mains transformer. Likewise, it may be necessary to adjust the value of R13 according to the voltage drop in the output transformer primary. If there is instability, the connections to either the primary or secondary of the output transformer should be reversed so that the feedback becomes negative. All that now remains is to decide by trial and error on the most

suitable values for R14 and C8. It should perhaps be mentioned that if the amplifier is operated without feedback, the reproduction will be very

COMPONENTS LIST

COMPONENTS LIST				
Resistors (¼W unless otherwise stated): R1—1·2M R2—0·27M R3—2·7k R4—27Ω R5—1M R6—47k R7—2·7k R8—47k R9—15k (¼W) R10—0·47M R11—0·47M R11—0·47M R12—600Ω (¼W) R13—1k R14—330Ω R15—470Ω (1W)	Capacitors (350VW D.C. unless otherwise stated): $C1-0.01\mu\mathrm{F}$ $C2-0.1\mu\mathrm{F}$ $C3-50\mu\mathrm{F}$ 25VW electrolytic $C4-0.01\mu\mathrm{F}$ $C5-0.02\mu\mathrm{F}$ $C6-0.02\mu\mathrm{F}$ $C7-16\mu\mathrm{F}$ electrolytic $C8-2\mu\mathrm{F}$ 25VW electrolytic $C9-16\mu\mathrm{F}$ electrolytic $C9-16\mu\mathrm{F}$ electrolytic $C9-16\mu\mathrm{F}$ electrolytic $C10-16\mu\mathrm{F}$ electrolytic			
Potentiometers: VR1—1M log. VR2—100k log. Valves: V1—EF91, B7G base and screen V2—6C4, B7G base. V3 EL91, B7G base Mains transformer: Miniature, 250V half wave, 35-40mA, 6·3V, 1A Output transformer: Push-pull, high inductance primary (see text). Ratio 90 to 1 for 3Ω speaker or 40 to 1 for 15Ω				

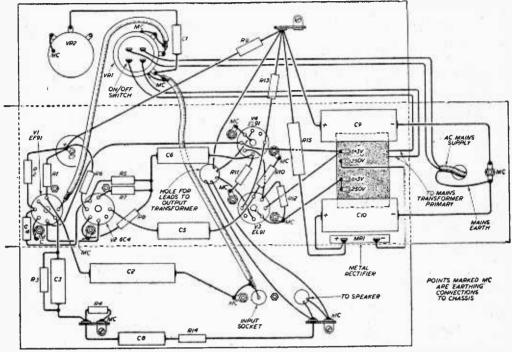
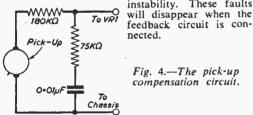


Fig. 3.—The component wiring details.

high pitched and, because the de-coupling is not generous, there may be a slight tendency to instability. These faults



Operation

If the amplifier is to be used with a pick-up, it will be necessary to provide some compensation for recording loss. While this could easily be incorporated in the chassis, it will usually be more convenient to fit it at the pick-up so that it is eliminated when the amplifier is used for other purposes. The output of the popular type of crystal pick-up rises in the low frequency region and it will generally be satisfactory to add external compensation at the rate of 3dB per octave below about 250c/s. This may be done with the circuit of Fig. 4.

Heartbeat Timer

An electronic heartbeat timer with no external wiring can be sewn into a patient's chest or near his heart because it has self-contained batteries. The circuitry is in a plastic envelope about 2\frac{1}{2}in. in diameter, \frac{1}{2}in. thick.

The timer supplies a stimulating pulse at regular intervals to keep the heart beating regularly, where otherwise it might beat dangerously out of time, slow down or stop entirely.

This heart timer will run for five years, and has been tested on dogs for periods up to 100 days. Dr. Wm. Chardack, of the Veteran's Administration, and electronic consultant Wilson Greatbatch of Buffalo, N.Y., U.S.A., developed the device. Meanwhile, it was resported that RCA in

Meanwhile, it was resported that RCA in America developed a heart timer using a generator strapped around the patient's chest which induces power into a device sewn inside the chest cavity.

High Power Klystron Installations

One of the 50cm commercial radar installations using the English Electric Valve Company's K347, 600kW klystron is well on the way to completion at Kastrup. Copenhagen's new international airport, which is expected to be operational some time this month. The K347 is the first high power klystron to be designed specifically for use in commercial radar and in this installation two klystrons are used with a Marconi S264A radar comprising two transmitter/receivers feeding an aerial system on a main/standby basis.

The K347 is an external cavity tuned klystron operating in the 585 to 610Mc/s frequency range and repeated tuning operations can be made, to meet changing operational requirements, without stressing or damaging the tube.

Crystal Controlled C.W. TRANSMITTERS

By G3OGR

(Continued from page 877 of the February issue)

HEN using a doubler, make sure that the crystals chosen are of such a frequency that operation is always in the permitted bands. Provided this is remembered, a doubler will make available other frequencies, with a limited number of crystals. It is also in order to use a further doubler. This is often done to permit three band working from one crystal, for example.

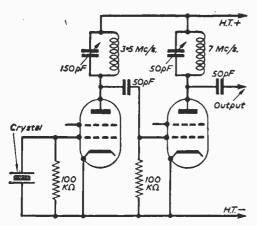


Fig. 6.—Oscillator and multiplier stages.

Power Supplies

The circuits shown have great latitude in power supply requirements. Almost any power pack available may be used. This item can thus be arranged to suit the output wanted. Even a small receiver type supply will allow 10W or more input to a single valve transmitter.

A typical separate power pack is shown in Fig. 7. The mains transformer, choke, and rectifier should be chosen to suit the output voltage and current desired. For inputs of up to 50W or so, a 400/0/400V H.T. secondary rated at 150mA, with a 5R4GY rectifier, will be satisfactory. The choke current rating should at least equal the current drawn. The working voltage of the smoothing condensers should be rather higher

than the actual H.T. voltage.

A fuse is an added safeguard against short circuits or similar defects. A 100mA or 150mA fuse will do for small power packs, with 250mA for larger supplies.

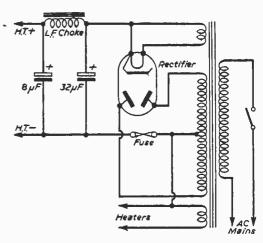


Fig. 7.—Power supply circuit for the transmitters.

If the power pack can be disconnected, or its circuit is interrupted by keying, a 100k 5W bleeder resistor should be connected across the H.T. supply, to discharge the condensers. In some circuits the screen grid resistors will act as a bleeder.

It is usually necessary to insert a switch, so that the valve heaters may be run without H.T. being applied. When initially testing a circuit, it is advisable to apply reduced H.T. voltage, until resonance has been found. A dropping resistor may be used for this purpose.

Key Clicks

Crystal oscillators usually key well, but if key clicks are produced, the cathode or key by-pass condenser may be changed in capacity. Using a rather large capacity will tend to cause "tails" to the characters, but this depends on the current drawn by the valve.

If a condenser alone is insufficient, a choke may be added in series with the key. Another condenser may then be joined directly across the key

contacts

Many operators have favourite methods of keying. The key may interrupt the cathode circuit, or may be in the H.T. negative circuit. An alternative is to use a separate transformer to obtain H.T. only, and key this in the primary. The rise and decay time can then be adjusted by modifying the smoothing condenser capacity. When keying mains and other high voltage circuits a relay is preferable, for maximum safety.

1

A BAND II Pre-Amp

A USEFUL ADDITION TO RECEIVERS FAR FROM THE TRANSMITTER

(Continued from page 874 of the February issue)

HEN construction of the preamplifier is finished, all wiring should be checked carefully. The unit may now be switched on and if possible the H.T. and L.T. should be measured without the valve in position. If all is in order the unit should be switched off, the valve inserted and the unit switched on again. As a check, the H.T. and L.T. voltages may again be measured. Plug the downlead into the input socket and connect the output to the receiver aerial socket.

The dust cores in L2 and L4 should be altered in position for best results and finally the positions of the two coupling coils L1 and L3; movement of these coils may necessitate altering the position of the slugs again. If the slugs are loose in the coil formers they should be removed and a piece of

thin elastic inserted down the threads of the former and the slug screwed in again. When the best positions for the slugs and coupling coils have been found, the coupling coils may be lightly cemented in position. (A tool for adjusting the position of the cores can be made from a plastic knitting needle.)

Alternative Coupling

If the incoming signal is very weak, it may be

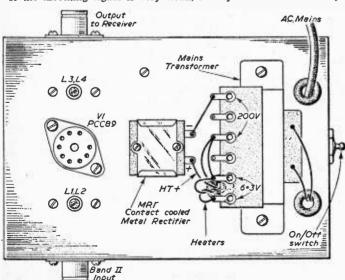
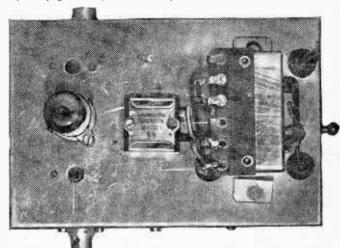


Fig. 4.—The above-chassis layout of the unit.



found that the signal from the pre-amp is less than that from the aerial direct. Whilst this may be due to L2 and L4 resonating at the wrong frequency, it is more likely that the coupling between the aerial and L2 and the receiver and L4 is not optimum. Various alternative methods of coupling may be tried instead of using the coil L1, the wire from the aerial input socket may be tapped directly on to L2 and the optimum position be determined by trial. The effect of including a small capacitor—2-10pF—may

also be tried.

Matters are easier as far as L4 is concerned. The effect of omitting L3 and employing a small capacitor between the anode of V16 and the inner conductor of the output coaxial cable is certainly worth trying. The value of this capacitor may be again 2-10pF. If good results are obtained with the initial arrangement the number of turns on L1 and L3 may be altered in an endeavour to secure better results.

Final Adjustments

The condenser C1, which is part of the neutralising network is set for optimum results. The turns of the inductance L5 may be opened out or closed up to secure best results. Accurate alignment of the circuit is best carried out by using a sensitive meter to monitor the voltage of the limiter grid of the

receiver. A resistor of about 10 to 47k should be included at the receiver end of the meter lead. (Note that the positive lead of the meter must be connected to the chassis of the receiver and the negative lead—through the stopper resistance just mentioned—to the grid of the limiter valve.)

If it is desired to avoid the losses which may be

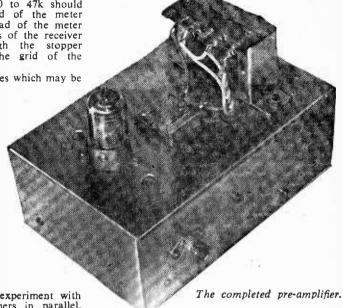
associated with change of cable at the input socket this socket may be omitted and the aerial downlead wired directly to L1a.

Instability

Owing to the high gain of the pre-amplifier it is possible and, if construction is not particularly well carried out, likely, that instability in the pre-amplifier will be experienced. In curing this instability the positions of the output and input leads relative to each other are critical and re-arrangement will often effect a cure. The decoupling capacitors can likewise have a great effect upon the performance—particularly C6 and C7. In the event of

instability, it is worth while to experiment with these condensers by putting others in parallel, perhaps connected to different earth points, until

the instability is cured.



Housing

The finished unit may be housed in a wooden box which can be fitted or placed on top of the radio receiver.

Although a great deal of heat is not generated in the unit, adequate ventilation should be assured to avoid frequency drift. During the testing, the unit can be operated direct from the mains supply but finally when it is fitted permanently to the receiver the mains supply should be taken direct from the set (after its mains switch) and then the pre-amplifier cannot be left switched on inadvertently.

Bandwidth

The damping of the input tuned circuit is such that the coil resonates over the whole of Band II and no tuning is necessary. However, it may be found that the tuning of the anode coil is sufficiently sharp to render impossible a flat response over the complete band. In this event, a damping resistor may be connected across the coil L4 in parallel with the condenser C8. It may have a value of, say, 1k to 4.7k, depending on the damping required to obtain best results. This resistor may result in some loss of signal, and if reception is such that no signal can be "wasted." then it may prove necessary to employ variable tuning in either the input or the output circuit.

Conclusion

It is worth while emphasising again that where signal strength is low a pre-amplifier such as this must be "tailored" to suit the conditions of the location concerned. To obtain maximum transfer of energy from aerial to first grid and from second anode to receiver will necessitate, in most instances, some experiment, but it will then be certain that the best use is being made of the available signal.

COMPONENTS LIST

 Resistors:
 Capacitors:

 R1—82k.
 C1—2 to 10pF, bee

 R2—82 Ω .
 hive type (or similar).

 R3—100k 10per cent.
 C2—2pF.

 R4—180 Ω .
 C3, C4, C5, C6, C7,

R5-100k 10per cent. 1000pF, min. ceramic. Valve: PCC89. C8-3pF ceramic.

Power Unit Components:

Resistors, R6, 1k or to suit H.T. voltage. Capacitors, C9 and C10, 8 to 32/F, 350VW. Rectifier, miniature contact-cooled type for 200V r.m.s. input and rated at about 30mA. Transformer—type used for converters, with tapped primary and 7V secondary. Chassis: see diagram (Fig. 4.)

Solder, wire, wooden case, etc.

COIL WINDING DETAILS

No. of turns L1 (over L2)

L2 7 L3/4 (over L7) 2 L4

Coils are wound on in small polystyrene coil formers with purple coded dust cores. No spacing is used between turns—the coils are closewound.

L5 consists of about 15 turns of 22-26s.w.g. enamelled or DCC copper wire wound to \frac{1}{2}in. inside diameter.

Valve Bias Explained

BASIC THEORY FOR THE BEGINNER

A CIRCUIT for a triode valve is shown in Fig. 1 and is representative of many audio-frequency amplifiers. At this stage let us consider the circuit purely from the D.C. point of view in relation to the resistive elements connected to the various electrodes.

The valve heater is energised either from a low voltage winding on the mains transformer or, as we will recall from the last two articles, direct from the mains through a voltage dropping resistor in series with the heaters of the remaining valves. With battery valves, of course, the heaters

are powered from the L.T. battery.

It will not be out of place here to discuss in broad outline the action of a triode valve. The heater of the valve (see Fig. 2) is placed inside a white powder such as thorium oxide. When the heater is switched on, it heats the cathode causing it to glow. The white powder as a result of the heating emits "electrons" which are tiny particles of electricity. These particles are charged negatively. Now negative charges are repelled by negative

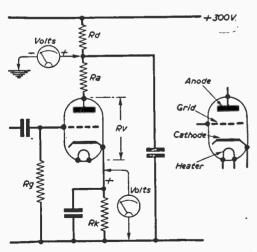


Fig. 1 (left).—A simple basic circuit for a triode valve.

Fig. 2 (right).—The conventional circuit symbol for a triode valve.

charges and attracted by positive charges. Therefore, if the anode (made up of a metal plate) is charged positively with respect to the cathode, then the electrons emitted from the cathode are attracted to the anode and travel to it. This flow of electrons constitutes a current of electricity through the valve.

The grid of the valve consists of a mesh of fine wire through which the electrons from the cathode have to pass on their way to the anode. If this grid is charged negatively with respect to the cathode, then some of the electrons travelling to the anode will be repelled and the current through the valve will be decreased. It can be seen that the current through the valve depends on the potential of the grid with respect to the cathode—the current increases as the grid becomes more positive (or less negative) relative to the cathode and decreases as it becomes less positive (or more negative).

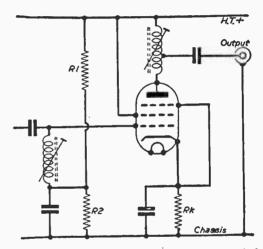


Fig. 3.—A valve bias system using both a cathode resistor and a grid potential divider.

The name "valve" is derived from the way in which the grid is used to control the flow of current, just as mechanical valves are used to control the flow of water in pipelines.

If, in Fig. 1 we assume that the grid potential is constant the conditions in the circuit are steady and the valve can be represented by a resistor of, say, Rv ohms (as indicated in Fig. 1). Thus we may consider that there are five resistors in circuit, Rd, Ra, Rv, Rk and Rg. Thus current flows through the valve of a value determined by (Rd+Ra+Rv+Rk), neglecting Rg.

Resistor Calculation

In Fig. 1 it is supposed that the H.T. line is 300V positive with respect to the chassis (H.T. negative). The circuit constants may be arranged so that with 200V at the junction of Rd and Ra, with respect to chassis, the current through the valve and resistive elements is 10mA (0.01A).

In this case, the value of Rd can easily be computed by using Ohm's law, this is, Rd=(300-200)/

(0.01). This follows because Rd is called upon to drop 100V, this being the difference between the H.T. line voltage and the required voltage at the junction of Rd and Ra. This works out to 10,000 ohms (10k). Thus, a voltmeter connected to the junction as shown in Fig. 1 would read 200V, provided Rd is 10k and the meter does not load the circuit in any way. In practice, of course, the meter acts as a load across the resistive elements and the reading as indicated is below that computed as governed by the extent of the loading.

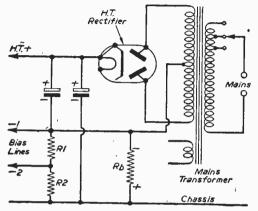


Fig. 4.—A circuit using a common bias resistor to obtain bias for all valves—the bias lines are connected to the grids of the valves through decoupling networks, and the cathodes are connected direct to chassis.

The 10mA of current is also flowing in Ra and Rk. The value given to Ra is usually decided by the operational factors of the circuit, as distinct from the D.C. or static aspect, and the same applies in some degree to Rk in the cathode circuit.

The value of Rg is usually very high, often in the region of 1M, but as current does not normally flow in this resistor, there is no potential difference across it and the grid is at chassis potential. (Use Ohm's Law: $V=Rg\times 1$, I=O, and therefore V=O.) This fact is essential to the understanding of the following explanation and one which often causes confusion or bewilderment in the mind of the beginner but is easy to grasp when the principle is understood. There is no current through Rg; therefore there is no P.D. across it.

Let us suppose that Rk is 1,000 ohms, and that the circuit is set up as previously mentioned with 10mA flowing. The volts drop across Rk is then equal to $(0.01 \times 1,000)$ which works out to 10V. Or another way of looking at it is to multiply the current in mA by the resistance in $k\Omega$, which in this case is (1×10) , 10 volts.

The polarity of the voltage across Rk is such that the cathode is 10V positive with respect to the chassis or H.T. negative line, as shown on the circuit. The grid of the valve is connected to the H.T. negative line or chassis through Rg. This means that the cathode grid is 10V positive with respect to the chassis and grid or stating it another way, the grid is 10V negative with respect to the

cathode, always provided 10 mA of current is flowing in the 1k cathode resistor.

The best way of measuring the bias voltage is by connecting a voltmeter across Rk. There will be the least error in the reading by adopting this method because the resistance of the voltmeter on the 10V range is almost certain to be far greater than the value of Rk. If it is attempted to measure the grid bias by connecting a voltmeter between the grid and cathode, then current will flow through Rg by way of the meter and the reading will be considerably less than the actual voltage.

If ever we require to discover the value of Rk for any grid bias voltage then all we do is divide the value of grid bias required by the cathode current of the valve. This, of course, is simply R=E/I, and where R is in ohms, I must be in amperes, but where R is in $k\Omega$, then I must be in mA.

Where a pentode, tetrode of any other multielectrode valve is in use, then the current through Rk is equal to the total H.T. current of the valve (i.e. anode current+screen grid current, etc).

Other curious methods are sometimes adopted to secure a bias voltage. Fig. 3, for example, shows such a method, Here is an R.F. amplifier which uses cathode bias, having Rk in the cathode circuit, but in addition has a positive potential on the control grid. Rk provides some fixed bias, but since the control grid is also connected to the junction of the potential divided R1, R2 some of the bias given by Rk is counteracted.

However, this arrangement provides a degree of compensation, and the circuit is stabilised to some degree in the event of a reduction in emission of the valve—when the white powder on the cathode begins to emit fewer electrons than before, resulting in an increase of the apparent resistance of the valve.

A Common Bias Resistor

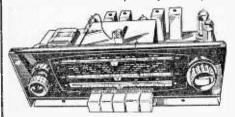
Isome receivers use a common bias resistor and have all the valve cathodes returned to chassis. The idea is shown in Fig. 4. Here Rb is the common bias resistor and is connected between the centre tap on the secondary of the mains transformer and chassis. It will be realised that the total current of the receiver flows through Rb, and a P.D., depending upon its value, is developed across it.

If the total current of the receiver is 100mA (0·1A) and Rb is 100Ω , then 10V is developed across it (i.e., $E \doteq 0.1 \times 100$). The voltage across Rb is negative at the secondary tap with respect to chassis, so it can be used ideally as a negative bias. In some cases the potential is applied direct to the grid of a valve after passing through a suitable filter circuit, while more often it is applied across a potential divider, such as that made up of R1, R2 in Fig. 4. In this way two bias lines can be drawn off and suitably filtered individually.

Since the bias is usually applied to a high resistance circuit relating to the valve, R1 and R2 can be of fairly high value, considerably higher, in fact, than the value of Rb. This means that they have little shunting effect on Rb, which can be computed as given above.

The full bias voltage (10V in the case cited) is present on bias line 1, and the bias voltage on line 2 is governed solely by the ratio of R1, R2, as fully detailed in a previous article in this series.

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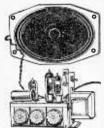
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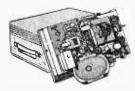
B-90—10K ohms/v. on 0.5 v. and 2.5 v.; 4K ohms/v. on 10, 50, 250, 500 and 1000 v., A.C. and D.C. Resistance, 2K, 200K, 2 M and 20M ohms, D.C. current, 100 microA. 2.5 mA, 25 mA, 250 mA. Size: 51 x 31 x 21n. Weight, 24 oz.



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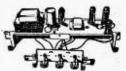
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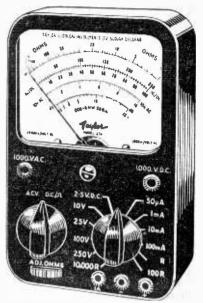
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QUARTZ CRYSTAL ETCHING

RAISING THE FREQUENCY OF A QUARTZ CRYSTAL

By J. B. Dance

HE resonant frequency of a quartz crystal can be increased somewhat by reducing the thickness of the crystal. It is not easy to alter the frequency of crystals which have gold or silver foil electrodes deposited on them (especially if the crystal is vacuum sealed), as these electrodes are usually "spluttered" on to the quartz using special apparatus. It would be difficult for the amateur to redeposit the electrodes on to the etched crystal or to connect wires to the foils. Such crystals are used mainly for frequencies below about 500kc/s. Above this frequency, rectangular quartz plates are common; the electrodes may consist of two metal plates held in position by a spring. The frequency of such crystals can be increased fairly easily by the method to be described.

Technique

There are two main methods by which the frequency of a quartz crystal can be raised, namely by grinding (lapping) or by etching. It is preferable to maintain the surface of the crystal flat to within 1/100,000 of an inch and therefore grinding creates some problems. If the crystal is not maintained perfectly flat, its activity diminishes; that is, when it is used in an oscillator circuit, the amplitude of oscillation becomes smaller and the crystal may even refuse to oscillate at all.

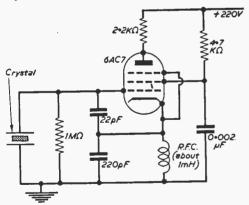


Fig. 1.—An oscillator circuit, using a crystal.

After a crystal has been ground, there is a certain optimum amount of etching which will lead to maximum activity. Ideally the amount of etching is such that the frequency is increased by etching by about the same number of kc/s as the square of the crystal frequency in Mc/s. Whilst this amount is not very critical, it is to be expected that a good commercially manufactured crystal will lose some of its activity during etching. This can usually be tolerated, however, in order

to obtain a crystal of the desired frequency; otherwise preliminary grinding will be required.

Etching Materials

Quartz is chemically very similar to glass and therefore very few liquids will etch it away. Hydrofluoric acid has been used for etching, but the average person is most strongly advised to avoid the use of such an extremely dangerous liquid. A solution of ammonium bifluoride, whilst much safer, is nevertheless quite dangerous. It can be ordered from most chemists at about 7s. 6d. for 1lb. A solution containing about 1 or 2 parts of the solid in 5 parts of water should be made in a plastic container. It is quite satisfactory to place the liquid inside a sheet of polythene which is put in the mouth of a wide-necked bottle or on a "tin-lid." It is wise to use the ammonium bifluoride solution out of doors and to keep a bucket of water nearby in case the liquid should be splashed on the hand. Only a very small quantity of the etching solution is required.

A pair of tweezers for handling the crystal is essential. They should be plastic tipped so that the etching solution does not come into contact with the metal. It was found convenient to coat the points of the tweezers with a solution of polystyrene in an organic solvent, allowing it to dry before use.

Frequency Measurement

The crystal frequency should be measured as accurately as possible by means of a wave-meter or even an accurately calibrated receiver. The crystal has to be incorporated in a suitable oscillator circuit (such as that shown in Fig. 1) for frequency tests. The anode current is a measure of the crystal activity, being small with a crystal of high activity. The value of the anode current should also be found when the crystal has been removed from the circuit, as this is the value which indicates that no oscillation is taking place. The valve used was a 6AC7, but any sharp cut-off, high gm pentode such as the EF91, EF80, Z77, 6AM6, EF42 or EF54 would also have been suitable. No direct form of coupling was used between the oscillator circuit and the wave-meter, stray coupling being quite adequate.

The crystal should be removed from its holder

The crystal should be removed from its holder by lifting it by the edges with tweezers, care being taken not to touch it with the fingers. If it is dirty or if it is accidentally touched with the fingers, it should be cleaned with chromic acid or with an organic solvent, as it is essential that the etching solution should come into contact with the whole of the crystal faces.

Etching Rate

The rate of etching depends on the temperature, the strength of the etching solution, the crystal frequency and the type of crystal cut. A maximum

(Continued on page 1010)

Checking Transistor Circuits

FINDING FAULTS WITHOUT INSTRUMENTS

By F. G. Roger

Checking Transistor Receivers Without Instruments

F a transistor receiver fails to work or to give normal results, stage by stage checking will probably be the quickest way of locating the fault. The tests described here are particularly intended for constructors who have no instruments, or perhaps only a simple meter for reading voltages, etc.

A typical transistor circuit, with check points, is shown in Fig. 1. Most of the tests described can be applied to any transistor receiver, though the number of stages, and exact circuit details, will vary.

Newly-Bullt Sets

When the receiver has been constructed, but fails to work correctly, wiring should be carefully checked against the wiring plans or circuit. Any wrong connection, omitted lead, or short circuit can prevent the receiver working. Particular care should be taken to see that switch tags, or coil and transformer pins, are not shorted due to fragments of solder or projecting ends of wire. At the same time check that all joints are securely soldered.

If no fault is discovered, and components are new, the alignment of aerial, oscillator coil, and intermediate frequency stages may be so badly at fault that no signals can be received. If so, this can be corrected as described later. In a superhet such as that in Fig. 1, wrong alignment can make the set quite dead, though no actual wiring or component fault is present.

Transistor connections, and the pin identification of all coils and transformers, should be checked. If no fault is found, stage by stage checks can be made as will be described.

checks can be made as will be described.

When examining wiring, assure that resistor values are correct. Colour coding is usual, and a mistake can be made in reading the values. A slight change in value from that specified will not usually have a severe effect, but a large error (such as in reading the number of noughts) may prevent the set working or cause very poor reception.

Resistance Checks

If a meter with "Ohms" scale is available, suspected resistors may be disconnected at one end, and measured. If a simple milliammeter is to hand, resistors can be checked with a 3V dry battery. From Ohm's Law, current will equal 3 divided by the resistor value in ohms. The result is changed to mA by multiplying by 1,000. For example, a 1k or 1,000 Ω resistor in series with the meter and 3V battery will pass 0.003A, or 3mA. If no meter at all is available, suspected resistors should be checked again, to discover if any error was made in reading the values.

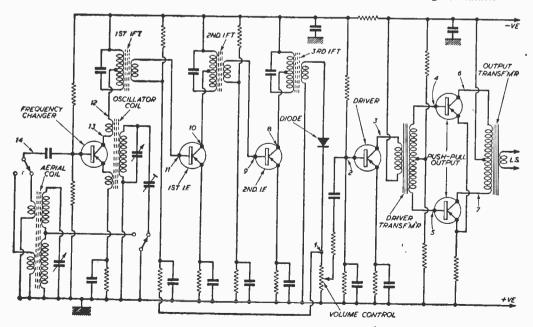


Fig. 1.—A typical transistor circuit with test points.

If these tests do not reveal any fault, stage by stage checks can be made. These checks apply both to a newly constructed receiver which has never worked correctly, and to an existing receiver which has failed.

Stage By Stage Checks

The purpose of these is to discover which stage in the receiver is at fault. Investigations are then localised to the few condensers, resistors, connections, and other items in the defective stage.

If headphones are available, they can be used to trace the audio signal. A 0.1 µF similar condenser should be included in one phone lead. Referring to Fig 1, the phones may be connected from (1) to chassis or earth line. If reception is good, the first three stages are working. Transfer one phone lead from (1) to (2). If reception ceases, the volume control or resistor and condenser between (1) and (2) are suspect. Remove the lead to (3). Signals should be considerably louder If not, the driver transistor or associated connections and parts are defective. Try the lead on (4) and (5). If there is no signal at either point that half of the driver transformer, or connections to it, should be

tested. If the signal is still available at (4) and (5), check at (6) and (7). A further amplified signal should be heard. If not suspect the associated

transistor.

Similar tests can easily be carried out with a TRF type receiver. When the point at which the fault is present is passed, reception will cease. Unsuspected faults can often be quickly located by this method.

For checking all stages, a source of audio and intermediate frequency signals will be extremely useful. Such signals may, of course, be obtained from a generator. But assuming that such an instrument is not available, an ordinary radio receiver may be pressed into service.

Fig. 2 shows stages in a typical battery portable or similar receiver. If a station is tuned in, an audio output will be available at point (1). Point (2) also gives an audio signal, at greater power. The usual volume control allows the signal

strength to be adjusted.

Many receivers have a 465kc/s I.F., so a modulated signal at about this frequency may be taken from points (3) or (4). A short piece of flex can be used as a test lead. For audio outputs, use points (1) or (2), and include a condenser of about $0.01\,\mu\text{F}$ in series with the lead. For 465kc/s outputs, use points (3) or (4), and wire a 100pF or similar condenser in series with the test lead.

Mains receivers may also be used, with appropriate care, and reliable isolating condensers in the test lead. With a TRF receiver, no intermediate frequency signal will be available.

Method of Testing

The valve receiver is tuned to a station and switched on. For 1.F. outputs, the valve receiver speaker can be muted by turning the volume control to zero. When using audio outputs, the

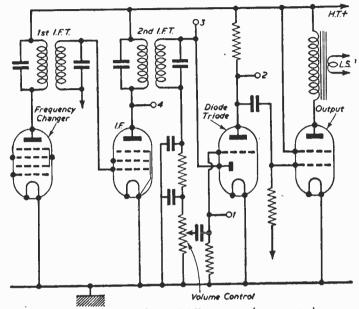


Fig. 2.—Obtaining audio and I.F. outputs from a receiver.

speaker in the valve receiver must be muted. This can be achieved by connecting an equivalent resistance in its place.

To check the transistor receiver speaker and output transformer, if necessary, apply the audio signal at (6) or (7). With the A.F. signal injected at (4) or (5) volume should be increased. If the lead is removed to (3) and reception ceases, the driver transformer, or connections to it, are defective.

Taking the lead to (2) should give increased volume. If not, the driver stage is faulty. With the lead taken to point (1) output should be adjustable by means of the volume control. If not, this component, or wiring to its tags, must be checked.

When working backwards from the output stage in this way, reception will cease when the point of the defect is passed. Also look for additional volume, as each additional stage is brought in, and reduce signal strength with the valve set volume control, to avoid overloading.

These tests will localise any defect in the audio stages of the receiver. Once this section has been cleared, or the defect found, attention can be given to the I.F. stages.

Checking I.F. Amplifiers

An intermediate frequency output is now obtained from the valve receiver, as described. The test lead is taken to point (8). If results are good, the third I.F.T. and diode are working. If signals were obtained with audio injected at (1), but not

with the I.F. signal injected at (8) suspect the third I.F.T., or diode, or associated connections.

It results are obtained, transfer the lead to (9). Amplified signals should be heard. If not, suspect the second I.F. transistor, and associated resistors and wiring. If a signal is obtained, and valve receiver and transistor receiver both have a similar intermediate frequency, it should be possible to adjust the core of the third I.F.T. for maximum results.

The lead is then connected to point (10). If reception ceases, the second I.F.T., or connections



Various types and makes of transistor differ in appearance and three of the common types are shown above to facilitate identification.

to it, must be checked. When the lead is taken to (11), volume should increase. If not, suspect the first I.F. transistor, or associated components,

AVC Action

As more stages are brought into use, it will be necessary to avoid overloading the transistor receiver. A very small series condenser should be used in the test lead. This can be arranged by twisting two insulated wires together for an inch or so, and reducing the length twisted together if signals are too strong. When testing the I.F. stages, keep the transistor receiver audio volume control at maximum, and reduce volume if necessary by keeping down the strength of the signal injected.

With the lead connected at (11), or merely placed near this wire, the second and third I.F.T.s can be aligned. The lead may be transferred to (12). If reception ceases, suspect the first I.F.T. or connections to it. If results are obtained with the lead at (12) but not at (13) then the oscillator coil collector winding it defective, or the coil wrongly wired.

If the two receivers have the same intermediate frequency, and one of the transistor set, I.F.T.s cannot be adjusted for best results, connections to this transformer should be checked. The injected signal must be kept at a very low level, as explained, or the automatic volume control circuit of the receiver will make adjustment difficult.

If an intermediate frequency amplifier is suspected, it may be temporarily eliminated, with its transformer, by connecting point (11) to point (9), in the case of the first I.F. stage. Or the first I.F.T. can be eliminated by connecting point (10) to point (12), and so on. Any unused transistor should be unsoldered. One I.F. stage transitor should be unsoldered. sistor can be compared with the other by using only one I.F. stage in this way, and trying the transistors in this stage in turn.

When the defective stage has been located, check wiring and resistor values carefully. If all components are in order, and connections are correct, the associated transistor must be suspected.

F.C. Stage

When good results are obtained with a weak signal injected at (13), but the receiver will not operate, the F.C. stage is probably defective. If the defect shows up on one waveband only, this would have immediately made the associated coil windings, switching, and wiring suspect. These items should in any case be checked, when a fault

has been localised to the F.C. stage.

To eliminate the aerial circuit, lead (14) can be disconnected from the switch, and taken to an exterior tuned circuit. This can be any coil and variable condenser tunable to the medium or long wave band. The coil is returned to the earth line, or base feed network. If good reception is then possible, the aerial circuit is probably faulty.

Alternatively, an aerial may be connected to point (14). If reception is possible, the aerial circuit may be faulty, or trimming badly in error. But if neither of these tests allow any signal to be received, after the checks previously described, then the F.C. transistor is probably not oscillating. Oscillator coil connections should then be checked.

When reception is good with an aerial, but ceases when this is disconnected, lack of alignment alone may be responsible. If so, adjustment of the oscillator coil core, or aerial coils, or trimming, will remove the trouble. Remember to adjust cores at a high wavelength on each band, and trimmers at a low wavelength. Alignment is correct when no further improvement in volume is possible. As reception is improved by early adjustments, select weak stations for subsequent adjustments, to prevent the AVC action already mentioned.

Other Tests

If a new battery is not being employed, it should be checked with a meter. The correct polarity is absolutely essential. Switch, and positive and negative circuit continuity, can be checked by working along point by point from the battery.

A meter and small battery can also be used to check continuity of aerial, oscillator coil, I.F. transformer, and other windings. Disconnect one end of suspected windings first.

In most cases only a few of the tests described will be required. For example, if A.F. is applied as explained, working back from the speaker, a defect in the A.F. amplifier may be at once located. Similarly, if the A.F. amplifier is cleared. applying an I.F. signal to points (8) through to (13) will quickly show where the fault is.

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A STEREO AMPLIFIER

8W WITH SINGLE-ENDED OUTPUT CIRCUITS

By R. Hindle

(Continued from page 902 of the February issue)

HE main circuit is fully conventional. R4 C1 and R12, C4 serve to decouple the first audio stages. The gain controls (VR1, VR2) are placed between the two audio stages where the signal is of the order of IV. It will be seen that the H.T. switch connects the centre-tap of the 300-0-300V winding to earth via the indicator lamp L1 which, when the switch is in the "on" position, carries the H.T. current of the whole amplifier, or more correctly the charging current to the capacitor C8 which is of pulse form. Normal current lights this lamp quite adequately, the initial surge on switching on being evidenced by the brightness of the bulb. Excessive current will burn out this lamp, however, so that it acts as a fuse. The transformer specified has two 6.3V centre-tapped windings in addition to the winding for the rectifier heater and these are used one for each amplifier line. It is not essential to feed these from separate windings if a transformer with only one such winding is available. The "mains on" indicator lamp may be across one half of one of these windings, this being found to give quite adequate light with the lamps used. Centre taps go to earth, of course, and both sides of the heaters of the valves are floating.

The gain of this amplifier even without a preamplifier is likely to be adequate for the popular type of stereo cartridge of the crystal or ceramic type and the constructor may like to try it out coupled directly into this amplifier pending the production of the pre-amplifier. In this case it should be borne in mind that the crystal pick-up has to be correctly loaded in order to produce the correct frequency characteristic. The appropriate resistance is quoted by the makers and this value should be substituted for R1 and R9.

Construction

The amplifier is constructed on an aluminium chassis 12in. x 6in. x 3in. The drilling diagram was given in Fig. 3, which shows the sides of the chassis as if they were opened up. The layout shown is as on

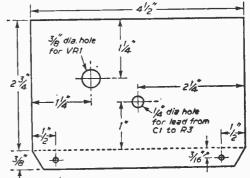


Fig. 4.—The drilling details for the screen to support the volume control.

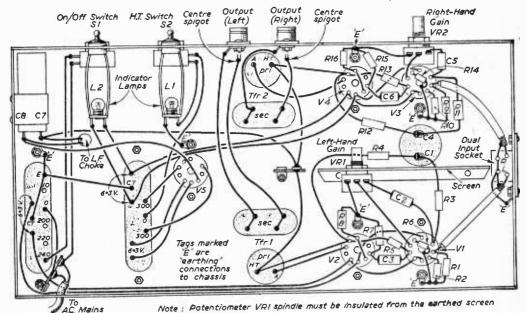
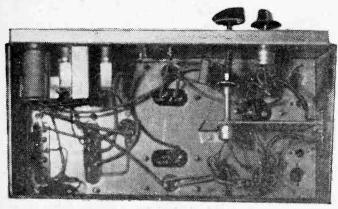


Fig. 5.—The under chassis wiring diagram.



The amplifier with all the wiring completed.

the outside of the chassis. The actual components to be used should be measured of course before drilling in case they are found to vary somewhat from the sizes shown. No mounting holes are drawn for valve holders and electrolytic condenser clip. The best way is to drill the hole as shown, drop in the component, turn it until the pins are in the relative positions shown on the wiring diagram (Fig. 5) remembering that this is the underneath of the chassis, and then mark the positions for the fixing bolts.

The mains and output transformers are of the shrouded type with soldering pins projecting underneath. Slots have to be cut in the chassis to allow passage for these, the method being to drill holes at each end of the slot position, then cutting away the metal between the holes. The positions for the possible additional valves are shown but not the holes themselves. The position of the screen is shown in Fig. 3, and the dimensions of the actual screen are in Fig. 4, from which the positions of the fixing screws on the main chassis can be taken.

Wiring

When the components are mounted, wiring should begin by feeding the heater supply with twin plastic flex, running this close to the chassis. A soldering tag under one of the securing bolts of each valve holder is used for all earths for the circuit associated with that valve. The only exception is the earth for the input socket which goes to a tag on one of the bolts holding this socket. All resistors are self-supporting on the valve-holders and are put as close as possible to the holder. The input lead from the socket to the valve is a short piece of coaxial cable of which the screen is earthed at the input socket end only.

If two signal lamps are to be fitted it will be found that the light from one bulb will shine through the window of the other, so obscuring the meaning of the lights, unless an aluminium shield is shaped and fitted between the lamps (or, of course, the enclosed type of signal lamp could be used).

Note that the output transformers can be used for either 15Ω or 3Ω speakers according to the connections made to the secondaries. The wiring diagram shows the two secondary windings of each transformer connected in parallel for 3Ω working. If 15Ω work-

ing is required the windings are connected in series.

The spindle of the volume control fitted to the screen is extended to the front of the chassis using a flexible coupler and a piece of bakelite rod. Bear this in mind when wiring so that there is room for the coupler, Knobs were fitted to the volume controls on the prototype, though these are really unnecessary; instead slots could be cut in the spindles for screwdriver adjustment.

This amplifier could supply 6.3V heater supply and up to 15mA of H.T. to a preamplifier if required. If this is needed it is suggested that an output socket be fitted at the mains transformer end of

the chassis to allow easy connection.

Surrey's Most Modern Factory

The second stage in the erection of the new factory at Chessington for the Solartron Laboratory Instruments, Ltd. the electronic instrument manufacturing company of the Solartron Electronic Group, Earphorough, Hants, is now under work

Group, Farnborough, Hants., is now under way.

The administrative block of 25.000 sq.ft, which presently houses the instrument sales and the international division of Solartron, was occupied early in 1960. Also in this block are the instruments servicing and works training sections, together with some production facilities.

The second section of 50,000 sq.ft being built will be completed in October, 1961, and the third stage—a further expansion of 50,000 sq.ft, for which the Chessington site has available space—will be completed in three years' time. The final factory will be one of the most modern in Britain for the manufacture of electronic instruments and will employ more than 1,000 people.

The training centre, which is now incorporated in the new buildings, is claimed to be the most advanced for workers in electronics. A special study has been made of training methods, and the result is that operators are working confidently at full production at their benches after an initial training period of six weeks. The training continues from time to time in intensified courses for two years for the creation of an expert operator. In fact, training is integrated with production somewhat as is a University "sandwich" course.

The Solartron Electronic Group is a member of the Firth Cleveland Group of Companies, under the chairmanship of Mr. Charles Hayward, and currently Solartron's sales of electronic test instruments alone exceed £2,000,000 per annum, and it is planned to double this amount over the next five years.

The Solartron Group Director responsible for the Chessington factory is Mr. E. R. Ponsford, Managing Director of Solartron Laboratory Instruments, founded 13 years ago as the first Company of the Group. The decision is yours. To be a success in your chosen career; to qualify for the highest paid job . . . to control a profitable business of your own. ICs home-study courses put your plans on a practical basis; teach you theory and practice; give you the knowledge and experience to take you, at your own pace, to the

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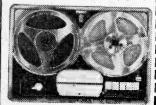
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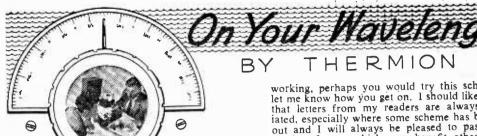
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Aerial Design

NE important feature arising out of correspondence from some of my readers was regarding the choice of aerial suitable for short-wave section. In the old days one was content to erect a large horizontal aerial system, usually running the full length of a garden, with a large mast at each end and the lead to the set was taken from one end or from the centre. This type of aerial (an inverted 'L' or a 'T') was a good all-round arrangement, and many newcomers are inclined to copy this arrangement and in spite of the all-important feature of height and insulation, and the use of the multi-stranded wire, only obtain very indifferent results. I am asked why this is. The main reason is that nowadays the majority of high-powered short-wave stations use a very high metallic mast which itself is the radiator or aerial. Under these conditions, therefore the signal is vertically polarised. As most readers know, it is desirable that the receiving aerial and the transmitting aerial should be in the same plane—compare the television aerial or the VHF aerial, for instance. The types of aerial used earlier and for instance. The types of aerial used earlier and referred to above, are horizontal types and must naturally, therefore, be productive of inferior results. I have found that a very good aerial for all-round short-wave reception (that is, for a receiver which may be used on a large number of bands and not tied down specifically to one amateur band) consists of a vertical wire. The arrangement which I have tried out and have indeed recommended to a number of amateurs, is to fit a length of stout battening to the soffit carrying the gutter and to the end of the batten attach an insulator. One end of a length of wire should be attached to the insulator which should be at least 3ft from the walls of the house. The lower end of the wire should be anchored to a similar arrangement of batten and insulator fixed to the lower part of the house so that the wire is about 15ft long. The lead to the receiver is taken from the lower end. In the majority of cases this arrangement will be found productive of very good all-round results except in some cases, where the house acts as a screen. Except on the very short wavelengths, this should not have a very marked effect, and the only ill-effects which have been noted were in the case of very heavy rain-storms when the wall immediately behind the aerial became soaked, and signals did then drop off. If you have not tried such an arrangement, and are experiencing indifferent results in your short-wave

working, perhaps you would try this scheme and let me know how you get on. I should like to stress that letters from my readers are always appreciated, especially where some scheme has been tried out and I will always be pleased to pass on the results of tests which may benefit other readers.

Rain Effects

Whilst on the subject of aerials I should like to mention a peculiar effect which was reported to me by an acquaintance. He was listening to the short-waves one evening and suddenly a ticking noise started on the band on which he was listening and he thought that it was an amateur starting up his transmitter, or a new beacon which he had not previously heard. He found, however, that the noise extended over the entire hand and was not tunable. For a time he put it down to some form of electrical interference, but as it continued he began to wonder whether something was wrong with his equipment and so started to take particular notice. The ticking had an almost clockwork regularity, and was of very constant strength. Suddenly the regularity fell off and longer intervals occurred between the individual "clicks", and after a very short time they ceased. He was left wondering what had been the cause of the trouble and then continued his "searching". After a few minutes the noise started again with the constant regularity, and fortunately at that moment the wind apparently changed and he heard rain beating against his window. This gave him an idea and he looked out at his aerial and from the insulator nearest his house he saw a constant steady drip of rain. The water was running down the aerial, over the insulator to its lowest point, and then dripping from there. There was obviously some electrostatic effect taking place, and when he pushed up a length of wood to take away the drips the noise ceased, as it did when it stopped raining. The insulator, incidentally was one of the ex-government Pyrex long components and was not fractured-but it was coated with a very heavy deposit of soot. He gave it a good scrub with warm water and a detergent and at the next heavy shower it gave no trouble at all. Perhaps, therefore, if your aerial equipment has been up for some long time it might be worth while lowering it and giving it a clean up; a heavy sooty deposit could cause signal losses.

Heat Sinks

To obtain maximum efficiency from heat sinks used for power transistors, paint them dull black. Black is a much better radiator of heat, so that a small black heat sink may be much better than a larger shiny one. The principle can also be used for ordinary transistors. If a transistor is going to be near something warm, paint it with a shiny aluminium paint. If you are worried about the transistor itself heating, paint it dull black so it can easily radiate its excess heat.

A Versatile TAPE RECORDER

COMMENCING THE WIRING

By D. L. Woolley

OR the deck used by the author, the front panel should be made 11 in. wide. If the record-level indicator is to be built into the recorder, the front panel should be drilled as shown in Fig 5 but

if not the panel should be drilled as in Fig. 4.

For the record-level indicator (whether built into the recorder or not) a small moving-coil milliammeter is required. Any value of full-scale deflection up to a maximum of 5mA can be used. An old thermo-couple R.F. meter with the thermo-couple removed should be ideal as the scale readings are unimportant—a linear scale is not required, any calibration will do. The diameter of the meter-case should be about 2in. although up to 2½in. can be fitted on the panel. A hole to suit the meter should be cut in the panel including the three or four fixing holes required. If

the depth of the meter-case is greater than 11 in. the meter will not fit flush with the front of the panel as it will touch the second and third valves. This small difficulty can be overcome by using small stand-off washers to keep the front of

the meter about in. from the panel.

Drilling

When drilling the front panel it is advisable to make sure that the lower holes coincide, as near as possible, with the similar ones on the front wall of

(Continued from page 899 of the February issue)

The Function Switch

As stated before, the function switch is very important. A good quality well insulated 3-pole, 3-way, 2-bank switch is required. It must be of standard size and not a miniature. This is important as the stray capacitance between tags on a miniature switch is high and such strays must be kept low in order to avoid instability and unwanted feedback.

First of all, the switch is dismantled, except for the ball-bearing mechanism, and all parts cleaned,

especially the two wafers. These two wafers will, for convenience, be named Bank I and Bank 2. A small piece of Mumetal, radiometal or similar high-permeability metal is now needed for a screen between the two banks. Ordinary tin-plate would do the job. but not as efficiently as the Mumetal. An old cathode ray tube screen would be a suitable source of high-permeability alloy. The size of the screen is 34in. long by 24in. wide and it should be cut and drilled as shown in Fig. 6 although the measurements are nominal and depend on the size of the switch.

Holes P and Q should be drilled to suit the two fixing bolts of the switch. Two small grommet-holes are needed as

shown. The switch is now built up as illustrated in Fig. 7. More details are given in Fig. 11. After bolting the switch together,

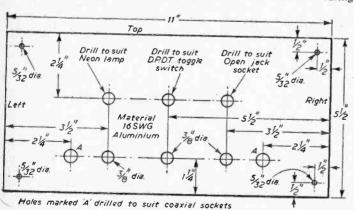
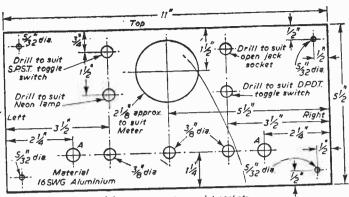


Fig. 4.—Drilling details of the front panel,

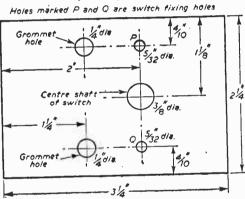
the chassis. The panel and chassis should now be cleaned with a cloth to remove all small metal particles and dust, before being put to one side.



Holes marked A drilled to suit coaxial sockets

Fig. 5 (above).—Alternative front panel drilling details when a record-level meter is to be included.

Fig. 6 (below).—Dimensions of the Mumetal screen for the function switch.



The connection it can be partially wired. from SA3 to SC3 (Fig. 2, page 898 last month) goes through the lower grommet-hole in the screen, whilst the two earthed sections on Bank 1 and Bank 2 are connected via the upper grommet-hole, It should be noted that the two banks are back-toback and that the tags of Bank 2 face the balllocating mechanism. In all cases SA, SB and SC, SD indicate the moving contact and the numbers 1, 2 and 3 the fixed contact being touched by the wiper. Although the switch, when described, seems a little complicated, its function and building are easy to see once one actually handles the switch and can inspect the various contacts.

Wiring the Amplifier

The most difficult part has now been completed and the actual wiring of the amplifier can be commenced. Two tag-boards are needed, one 16-way, and one 5-way. Both should have two contacts per tag and about 14in, between the inner tags. The larger tag-board is wired first: a complete wiring diagram is given in Fig. 10. It is best to wire in all connecting links before any actual components. Short leads of tinned-copper wire should be fixed to the lower, outer contacts, as shown, for connections to the valve-bases. About 2½in, is a con-venient length to make these leads. The tag-board has been designed in such a way that no leads need cross, and each can take a direct route to the valvebase in question. As a general rule, all resistors should be fitted first, between the inner bv followed contacts capacitors between the outer contacts. Any leads likely to short or touch other tags. should be covered with thin sleeving.

Amplifier Components

A word is now needed about the components used in the

Ordinary carbon resistors are apt to amplifier. be noisy in operation. If such resistors are used in a high-gain stage, any small fluctuation in the current through them is amplified background a high produces quite noise level. Thus for resistors R1, R2, R3 and R4, good quality cracked-carbon, high-stability components should be used. This type of resistor need not be very expensive-in the prototype amplifier, all W resistors were 10per cent tolerance high stability components.

C2 and C9 provide decoupling in the amplifier in conjunction with R16 and R5. These two capacitors are wire-ended tubular electrolytics, as are C1, C12, C19 and C22. Good-quality paper tubular capacitors must be used for C3, C10 and C14 as any leak in C3 and C10 will upset the biasing of valves 2 and 3, whilst a leak in C14 would pass a direct-current through the record/ playback head and magnetise it. The equaliser circuit can now be built on to a small 5-way tagboard. The equaliser described uses a network of resistors and capacitors, but no inductors, as is more usual. In the recorder it was desired to use the fastest speed of 71 in. per second for recording concerts and the speed of 32in, per second for ordinary work. Although a speed of 12in, per second is available on the tape-deck, it was decided to use this speed for private work only,

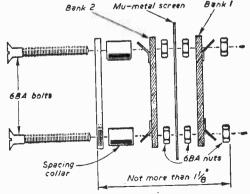


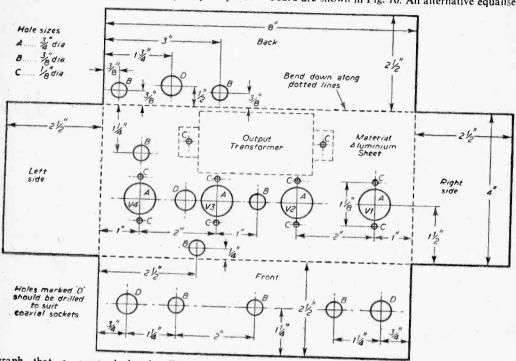
Fig. 7.—The assembly of the switch, including the Mumetal screen.

which did not require good quality at high volume. Recordings made at 17 in. per second are good, but only if played back quietly. High volume tends to make the noise-level in very quiet passages too much of a distraction.

Treble Boost

It will be seen from the frequency response

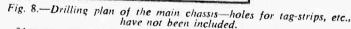
speeds although it must be stated that it is a compromise, providing theoretically correct equalisation at 6in. per second. R11 controls the amount of bass equalisation, and provides perfectly correct results at both speeds. being fully variable. Fig. 9 shows the approximate record/playback characteristics. The layout of the equaliser circuit and its tagboard are shown in Fig. 10. An alternative equaliser

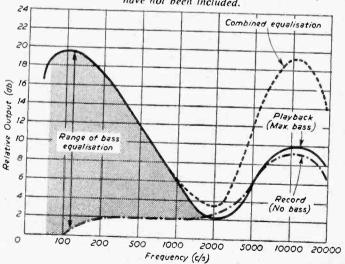


graph that a great deal of treble boost is required above 1,500c/s. In many recorders, it is the practice to apply treble equalisation during recording and bass equalisation during playback, but for this recorder, treble boost is applied both during record and playback, whilst bass correction can be made on record or playback, or both. However, the magnetic tape is easily overloaded if too much bass equalisation is made recording and only enough bass should be used to counteract any lack of it in the recording signal.

The circuit used for both 7½in, and 3¼in, per second was shown in Fig. 2 (page 898, Feb. issue). This circuit gives ample treble equalisation at both

Fig. 9 (right).—Equalisation curves.





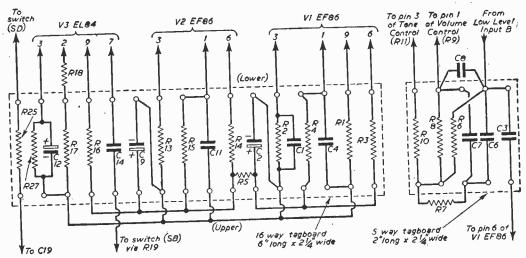


Fig. 10.—The main and equaliser circuit tag-boards.

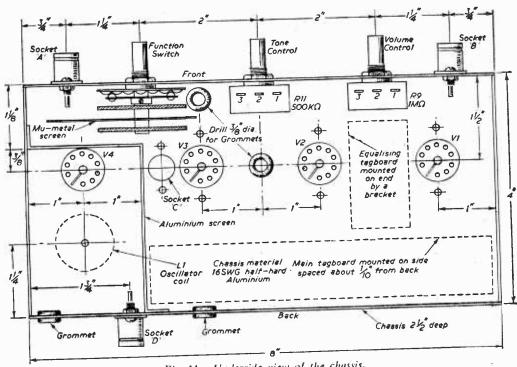


Fig. 11.—Underside view of the chassis.

circuit is shown in Fig. 12 with components from Fig. 2 to give the best equalisation at the three speeds. Either of the alternative equalisers can be built on to a 4 or 5-way tag-board. For C6a trial and error would probably give the best results, using a 300pF variable trimmer. For either type of equaliser, the tag-board should be mounted on to the chassis using a small bracket, and details are given in Fig. 13. The amplifier proper can now be built. Grommets and valve holders are put in

(Continued on 1021)

THE P.W. SIGNAL MAKING THE POWER GENERATOR SUPPLY LINIT

ANY constructors find they need a signal generator, but few eventually possess such a unit—their cost is generally too great. Although most enthusiasts cannot afford to buy a signal generator, they would nevertheless like to build one but are hampered by lack of plans. This new series has been especially prepared for the home constructor and will describe in detail the construction of a widerange signal generator.

By E. V. King

by soldering as shown in Fig. 3. Make sure that tags 2 to 6 inclusive do not short to earth.

Grommets should be fitted in the holes A, B, and C. The switch SI is fitted with the slot in the threaded portion uppermost, the switch is then "on" when pressed down. Leave plenty of thread showing outside the chassis and tighten the nut. For the

position of S1 see Fig. 3. The warning light is fitted from the inside using two nuts and bolts.

Component Positions—Inside the Chassis

Fig. 3 shows the position of the transformer. It is bolted tightly to the tin plate and should have a small strip of mild steel fitted on top of the chassis. This strip is shown shaded in Fig. 2 and the general method of mounting in Fig. 6. If this is not incorporated the unit will work well, but will give rather more hum than necessary.

A small tag strip with two isolated

Fig. 1 (left)—The circuit of the power

WWW. Resistor rating RS SKO Swatt unless otherwise R4 5KQ 6X5 R3 SKO $3K\Omega$ AC C1 and C2 16-100uF 350VW Warning CJ.C4,C5 and C6 8 or 16µF 350VW lamp Green

The chassis used for all the units are the same, basically a baking tin 6in. x 4in. x 2½in. high, and are easily obtainable. The bottom of the tin, after drilling the necessary holes for valve base, condenser and grommets, is soldered in position. The seam down one side of the tin is also soldered on both sides to give additional strength. There is no reason why readers should not make their own chassis or use aluminium instead of tin plate. If aluminium is used every earth connection to the chassis must be made via a solder tag and tight nut and bolt.

Component Positions—Outside the Chassis

Reference to Fig. 2 will show where to drill for V1 and C1/C2. The hole for V1 is 11 in in diameter, and can be made with an ordinary carpenter's bit, chassis cutter, tank cutter or using small tin snips. The condenser hole will probably have to be a little larger. The valveholder may be holted or soldered in position and the condenser clip bolted up tightly. Verify that the valveholder is an International Octal, as damage to the valve pins will be caused if the wrong one is used. Fit the valveholder so that the central "keyway" is in the position shown in Fig. 2.

The tag strip is attached to the rear of the unit

tags is soldered to the side of the chassis near the primary side of the transformer. (Fig. 3.)

Alternative Component Positions

If an upright-mounting transformer is used, it will have to be fitted on the top of the chassis. The component positions remain the same with the exception of the following points.

The condensers C3 to C6, which are wired in, will

be inside and not outside the chassis. The transformer itself will be outside in the position shown in Fig. 8, and grommet holes will be required at E, D, and F. Another 6-tag strip (with 4 tags isolated) is required and is soldered in place inside the chassis about in. from the top, as in Fig. 9. Make sure that no tags are earthed other than those at the extreme ends (i.e. 1 and 7 in Fig. 9).

All other components are fitted during the wiring process.

Wiring the Unit

It will pay the beginner dividends in both time and patience if he develops the habit from the start of checking, double checking and testing at every

stage of his work. This will be explained in detail.

Refer to Figs 1. 2 and 3 as you proceed. Take
the mains lead through the grommeted hole
"C" and tie a knot in it. Connect the and tie a knot in it. Connect the

black wire to one unearthed tag of the small tag strip. Also solder one primary lead from the transformer to the same tag. Check that 'all soldered joints are well made, strong, and with no sharp edges. Now solder the red mains lead to any tag on St. Solder the other primary lead to the unused tag of St If a three-core cable is being used, solder the green lead to the chassis. The chassis may be separately earthed if desired, but it must be earthed in some manner.

Testing the Transformer Primary

Make sure that the leads on the secondary side of the transformer are not touching anything. Plug in and switch on. A hum should be heard. If no hum is heard check the power supply, mains lead, S1 and the primary wiring.

If a loud hum is heard check that the transformer is correctly Fig. mounted with the steel strip above, and that the secondary wires are not shorting.

Wiring the Heater Circuit

Scrape and tin the thick 6-3V on the secondary side of the transformer; solder one to the chassis (use a large very hot iron for this joint) and connect the other to one side of the warning lamp holder. Connect the other tag of the holder to earth (always use a very hot iron for chassis connections). Screw in a low wattage, 6V lamp. Plug into the mains and switch on. Ensure that the lamp lights. If it does not and the transformer appears to be operating correctly check the lamp,



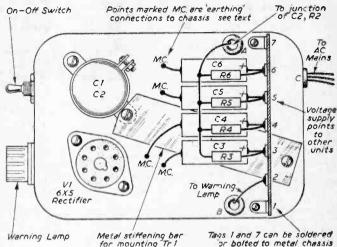


Fig. 2.—The above chassis view of the unit.

Refer to the valveholder and looking under it make sure you have the tags numbered correctly, sometimes this is not always easy. Be quite sure about this. Solder a wire from chassis to pins 1 and 2. Also solder a wire from pin 7 to the uncarthed tag of the lampholder. Plug in the 6X5 valve and check that when connected to the mains and switched on, the heater is alight. If it is not, check the valve pin numbers and the valve itself. Take an insulated wire from the uncarthed tag of the lampholder through the grommet at B and on tag 2 above the chassis (see Fig. 2). This is the main external heater connection.

Take the lamp out of the holder and hold it between tag 2 (Fig. 2) and earth (chassis). Switch on. The lamp should light. If not the last wire added has been wrongly connected or tag 2 is shorting to earth. Put the lamp back in the correct

holder and test again.

Warning

When carrying out this procedure of building and testing, never be tempted to work with the unit plugged in. In any case, when working in a garage or other location with a concrete floor it is wise to have a thick rubber mat on the ground,

Wiring the H.T. Circuit

Temporarily connect the two red secondary leads of the transformer to a small wattage (15 or 25W) main lamp or mains neon lamp. Switch on and check that the secondary H.T. is all right. If this lamp does not light, but the one in the holder does, check that the lamp itself is not to blame, that the holder is correctly wired and fitted and that the wires are not shorting.

Disconnect the mains lamp, and connect one secondary wire to the chassis. Connect the other to pins 3 and 5 of the valveholder. If a voltmeter is available connect it on the 250V range (D.C.) to the chassis (negative) and nin 8 of the valveholder (nositive). "Switch on, and the meter should read about 100 to 150V D.C. The needle may quiver a little as the supply is unsmoothed. If no reading is obtained the valve is suspect.

Connect pin 8 through a resistor (R1) to one positive tag of the large electrolytic smoother C1/C2. You will need to examine this carefully as they vary somewhat in their coding. One tag is the negative pole, usually either black or colourless. Two other tags are the C1 and C2 positive tags and are usually, but not always, yellow and red. Sometimes the positive tags are red and colourless, so care is needed. Details are printed on the side of the can. if the instructions tell you that one positive connection is for the maximum ripple, that is the one to use for the connection to R1. Connect the negative tag to the chassis.

Testing the Initial H.T. Supply

Connect the voltmeter on the same range as before, but with the positive lead on to the

junction of R1 and C1. Switch on, and the D.C. voltage should be about 250 with no vibration of the needle. If not, verify that R1 is a good component and of the correct value, and that C1 is correctly connected.

Wiring the Smoothing and Decoupling Circuits

Connect R2 so that it stands in air supported on the tags of the electrolytic condenser C1/C2. Connect the voltmeter as before, but with the positive lead to the junction just made between R2 and C2. Switch on and the voltage should be about 250. Switch off. Leave for 30 seconds. Short, with an insulated screwdriver, R2 and earth (chassis) when a spark should jump, showing that the condenser C1/C2 is working properly and holding a charge. Henceforth, whenever you are working on the unit after switching it off always discharge the condensers twice at 15-second intervals before recommencing work.

Connect an insulated wire to the junction of R2 and C2, lead it through the grommet "A" and bare the end for 2\(\frac{1}{2}\)in. to allow connection to resistors R3 to R6.

With reference to Fig. 2, cut the leads to R3, 4, 5 and 6 so as to leave about £in. lengths on each. Solder them as shown between tags 3, 4, 5 and 6 and the bared lead. Bend them more or less upright. Switch on the supply and connect each tag (3, 4, 5 and 6) to the voltmeter positive in turn. The voltage reading will depend on the voltmeter used. Expect a drop of the following voltages from the reading previously taken at the junction of R2 and C2:

Voltage Drop:

 $200\Omega/V$ meter ... $500\Omega/V$ meter ... $1000\Omega/V$ meter ... $5000\Omega/V$ meter ... Above $5000\Omega/V$... Neg

Above $5000\Omega/V$... Negligible If one tag gives a different voltage from the others then the associated resistor may have been wrongly chosen. If any tag gives zero reading

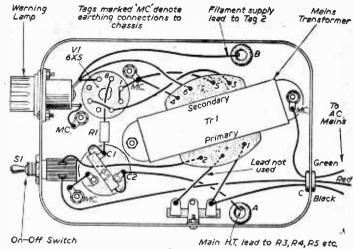


Fig. 3.—Underchassis wiring and layout.

it is earthing to chassis or the resistor is completely open circuit. Check by substitution.

Now solder in the four decoupling capacitors (C3 to C6). These need not all be the same type, but the constructor must again make sure of the polarity of the connections. Solder them as shown in Fig. 2, between the tags and the chassis. Negative ends going to chassis always.

Now check the voltage at each tag again and although they may vary somewhat (10V or so) from one to another, all should give over 200V. Switch off and quickly short each in turn to chassis with an insulated screwdriver. Each should give a good sharp spark and "crackle". Remember to discharge twice at junction R2/C2 as previously explained.

Specification of the Power Unit

The unit will operate from 200 to 240V A.C. mains and gives four outputs, almost independent of each other, at about 220V (low current). A 6.3 A.C. filament supply is also available. The unit may be used for other purposes than that in mind, and readers may take H.T. at 250V at up to 50mA from the junction of R2/C2 for driving applifiers, tuners, etc. Being small, the unit is very useful in the radio laboratory. In this unit the various outputs will be used as follows:

Tags 1 and 7, earth (chassis), this is H.T.— and one side of L.T.

Tag 3, R.F. oscillator and cathode follower; Tag 4, L.F. 400c/s oscillator for modulation; Tag 5, L.F. variable Wien bridge oscillator (A.F.) and crystal calibration unit;

Tag 6. amplifier for variable A.F. oscillator;

Tag 2, heater lead to all units.

Using Upright and Larger Transformers

The type of transformer used is not critical so long as the ratings are those specified in the components list. The placing and mounting of the transformer will depend on its construction but

(Continued on page 998)

-STYLUS WEAR TIMER-

AN EFFICIENT MEANS OF KEEPING A RECORD OF STYLI PLAYING TIME

ECORD manufacturers point out that styli may be worn and in need of replacement long before this is made apparent by increased surface noise; with consequent damage to valuable records. The recommended life of a diamond tip is about 2.000 hours, and that of a sapphire about 40 hours. There are probably some methodical enthusiasts who keep a careful note of playing times. but I suspect that most of us quickly lose the habit. By using the simple little instrument described below, it is possible to know at any time, exactly how long a particular stylus has been in use.

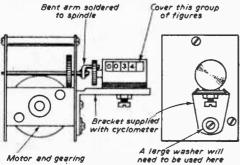


Fig. 1.—The method of coupling the motor to the cyclometer,

Components Required

The parts required are, a small "shaded-pole" synchronous motor fitted with reduction gearing giving hours instead of miles, a cyclometer or small counter, a piece of 18 in. sheet brass—2½ in. x ½ in.—and a few 4B.A. nuts and bolts. The motor complete with suitable garing can be obtained at moderate cost from suppliers advertising surplus equipment. (Note, an ordinary electric clock will not do, because it is not self-starting.) Whilst it is possible to get the counter from a similar source, if one buys a new cyclometer, this will be supplied complete with an adjustable bracket, and thus make it unnecessary to construct one from brass sheet.

Transmitting the Drive

The method of transmitting the drive from the final spindle to the counter will depend on the type of spindle fitted to the latter instrument. A true cyclometer is fitted with a "star" wheel, and this type can be driven by a bent arm fixed to the gear spindle and engaging in one of the teeth of the "star" wheel. The author's cyclometer has a spindle which is slotted at one end; consequently it was only necessary to file two flats on the end of the gearing spindle, which, when engaged with the slot, formed a positive drive.

By F. Churchill

Many of these small motors with gear-train have a spring-loaded clutch on the final spindle, to facilitate altering the hards when used as a clock. It is essential that this clutch is made inoperable, so that the drive is direct. If this is not done, there will be a tendency for the drive to slip whenever the load increases, e.g. when the figures change from 99 to 100, etc.

It is advantageous to fit a length of thin twinflex to the existing motor leads so that the unit can be placed in any convenient position; taking care to keep well away from pick-up leads and the pre-amp, to avoid inducing hum. These leads are connected to the terminal block on the gramophone motor, so that the counter only operates when the gramophone motor is actually switched on.

As fractions of an hour are not required, it will avoid confusion if the extreme right-hand set of figures are obscured with a piece of opaque Sellotape, or by some other method.

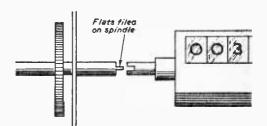


Fig. 2.—An alternative method of coupling the motor to the cyclometer.

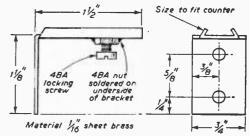


Fig. 3.—Dimensions of a suitable mounting bracket.

CORRECTION

In an advertisement for Stern Radio Ltd., which appeared in the February issue of PRACTICAL WIRELESS, the price given for "A Complete Kit of Parts for Stereo Pre-amplifiers" should have read £12 10s. 0d. and not £21 10s. 0d. as printed.

A valve voltmeter

THIS INSTRUMENT GIVES READINGS FROM I TO 1000V.

By J. B. Dance

F an ordinary voltmeter is connected across two points in a circuit, it takes a certain amount of current from the circuit. The voltage across the two points will normally decrease when a current is being taken owing to the internal resistance of the circuit, and therefore the true voltage between the points when the voltmeter has been removed is not known. This error is often negligible, (e.g. when measuring power supply voltages) but it always exists and may be very large in high-resistance circuits. The error can be minimised by using a voltmeter which has a high internal resistance in comparison with the internal resistance of the circuit being measured.

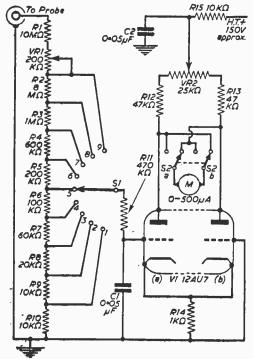


Fig. 1.—This circuit may be used over nine voltage ranges.

Moving Iron Voltmeters

Moving iron voltmeters invariably have a low internal resistance. An expensive moving coil 0-50 microammeter has an internal resistance of $20,000\,\Omega/V$ at full scale deflection when it is used as a voltmeter; even this is not high enough for some purposes, but all cheap meters have an internal resistance much lower than this.

The four main types of simple apparatus which can be used to measure voltages without taking any appreciable current are:—

- 1. neon bulb circuits,
- 2. electrostatic voltmeters,
- potentiometer circuits.
- 4. valve voltmeters (including methods using cathode ray tubes).

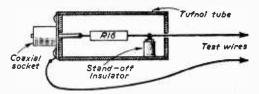


Fig. 2.—The test-probe for D.C. instruments.

Methods 1 and 2 cannot be used to measure voltages of values less than about 100V. Method 3, when used in skilled hands, is excellent, especially for low voltages, but method 4 is probably the most convenient method when quick direct readings over

a large variety of ranges is required.

The circuit of a simple valve voltmeter is shown in Fig. 1. This has nine D.C. ranges shown in Table 1 (page 998), with full scale deflections varying from 1V to 1,000V. It can also be used to measure audio and radio frequency voltages below 50V. The D.C. input resistance is greater than 20M and is constant from range to range. On the one voltage range, at full scale deflection, the current taken by the instrument is about 50/1000 of a microamp (20M/V) whilst on the 1000V range the current taken is 50µA at full scale deflection (20k/V).

D.C. Probe

The probe shown in Fig. 2 is used for D.C. measurements. It is connected to the main instrument by coaxial cable. The body of the probe consists of a "Tuffnol" tube with end pieces which are glued on to the tube after the resistor (R16) and the stand-off insulator have been fitted inside the probe. The wire end of the resistor is used as one contact, the other contact being made by means of a wire connected to the outside of the coaxial cable. Coaxial connection to the main instrument is used in order to prevent hum voltage pick-up in the high resistance circuits.

Components

All of the resistors, R2 to R10 should, if possible, be high-stability components and it is desirable that they should have a tolerance of ± 1 per cent. If great accuracy is not required, however, ± 5 per cent resistors could be used. R1 and the D.C. probe resistor, R16, should be high-stability components, but their tolerance is not important. If high-stability resistors are not available, it should be possible to obtain reasonably accurate readings by using the ordinary carbon type. The unusual resistor values can be made by using two or more resistors in series or parallel combinations.

A ceramic wafer switch was used for S1, so that the unwanted leakage current would be kept to a minimum.

Cl should be selected for high leakage resistance. A good quality component should have a leakage

resistance of over 2,000M.

The valve used may be a 12AU7 (B9A base) o a 6SN7 (octal), but almost any small double triode would be satisfactory providing that the constructor is willing to adjust the resistor values to suit the valve chosen

The double-pole double-throw switch S2(a) and S2(b), in the valve anode circuits, is provided so that the meter deflection can be arranged to be in a forward direction, no matter whether the voltage applied to the grid of V1(a) is positive or negative. If a centre reading microammeter had been available the switch S2 would not have been required. The meter was calibrated from 0 to $500\mu A$ and it was therefore easy to read the voltages being measured directly in volts for all of the ranges shown in Table 1.

Principle of Operation

The voltage from the probe is fed into the potential divider resistors R1 to R10. The total resistance of the potential divider (including the resistor in the probe, R16) is constant whatever the position of S1. The range is selected so that the switch S1 taps off a voltage from the potential divider which the valve circuit is capable of measuring (a fraction of a volt). R11 and C1 filter out any alternating voltages before the input reaches the grid of the valve. VR2 is adjusted before use so that the meter reading is zero when no input is being applied.

when no input is being applied.

Let us suppose that a small positive voltage is applied to the grid of V1(a). The anode current of this valve will then increase, making the anode voltage more negative with respect to the chassis. At the same time both cathodes become more positive owing to the increased current through the common cathode resistor, R14, and V1(a). This is equivalent to a negative bias on the grid of V1(b) and the current through this valve therefore decreases and its anode voltage increases. A current will therefore flow from the anode of V1(a). If a negative voltage is applied, the

current will flow in the reverse direction.

D.C. Calibration

The instrument should be used to measure any accurately known voltage which ought to give a full scale deflection on any particular range, e.g. 100V. The value of R1 should then be adjusted until a value is found which gives almost exactly a full scale deflection on the correct range. The value of this resistor will generally be of the order of 10M. Various high-stability resistors should be tried for R1, until a value which is very nearly correct is found. The final adjustment is then made by VR1. The value of this potentiometer should be kept reasonably small in order to preserve stability.

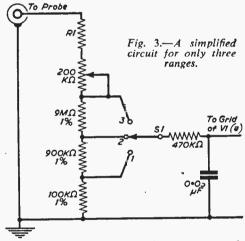
When one range has been calibrated, all of the others should be correct providing that the tolerance of the resistors R2 to R10 is within the limits of

accuracy required.

Simplified Version

The number of high-stability resistors required can be reduced by constructing an instrument having fewer ranges. The ranges can be selected to meet the

COMPONENTS LIST R1-10M (see text), high stability. R2—8M ½W high stability. R3—1M ½W high stability. R3—101 ½W high stability.
R4—600k, ½W high stability.
R5—200k ½W high stability.
R6—100k ½W high stability. R8—20k ½W high stability. R9—10k ½W high stability. R10—10k ½W high stability. R11—470k ½W. R12-47k 1W. R13-47k 1W. R14-1k 4W. R15-10k ½W. R16-2 to 4M high stability. R2-R10 are 1per cent tolerance; R11-R16 20per cent tolerance. VR1-200k preset potentiometer. VR2-25k (or 50k) potentiometer. C1, C2-0.05µF, 500VW. M-0-500 microammeter. S1-Single-pole 9-way ceramic single wafer switch. S2-Double-pole double-throw toggle switch. Via and Vib-12AU7 or similar (see text).



requirements of the constructor, but an example of a simplified instrument is given in Fig. 3. In this circuit the ranges provided are 0 to 100V (switch position 1), 0 to 10V (position 2) and 0 to IV (position 3).

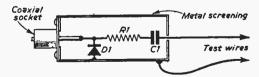


Fig. 4.—An A.C. test-probe.

A.C. Probes

A separate probe must be used for all A.C. measurements and it is desirable that different probes should

be used for audio and radio frequency measurements. The circuit of an A.C. probe is shown in Fig. 4. Cl removes all D.C. from the input and the series resistor R1 prevents the diode and the capacitance of the coaxial cable from loading the circuit under test to any appreciable extent. The diode D1 shunts all negative-going pulses to the screening, whilst positive pulses are fed down the coaxial cable to the main instrument. The valve grid receives a steady positive voltage which is measured.

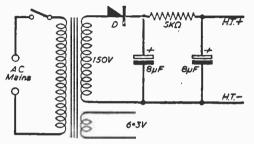


Fig. 5.—A suitable power supply unit. " מ" should be 150V, 5mA, or more.

In the case of the audio probe, the value of C1 may be 0.05μF or 0.1μF, but a 500pF, ceramic condenser is much more suitable for the radio frequency probe. If one wished to make high audio and low radio frequency measurements only, it would be possible to do this with one probe by using the compromise value of about 0.002 µF for C1 in Fig. 4.

The use of the resistor RI, shown in Fig. 4, not only enables the range to be accurately adjusted, but also prevents the circuit under test from being appreciably loaded by the capacitance of the coaxial cable. The average constructor will not wish to make actual measurements of radio frequencies in volts, but will only require to compare voltages (e.g. when aligning a receiver). It will therefore probably be unnecessary to calibrate the R.F. probe against a standard instrument. The audio probe can be calibrated by using suitable 50c/s voltages from transformers and a standard A.C. meter. R1 of Fig. 4 may be adjusted so that the instrument reads either peak A.C. voltages or root mean square voltages, as desired.

An OA81 is a suitable diode for both R.F. and audio probes, but care should be taken that no attempt is made to measure an A.C. voltage which has a peak value greater than about 50V. The

	TAB	LE I	
VOLTAGE	RANGES SHOWN	OF THE	CIRCUIT
l s	witch		
Po	sition	Range (V	'}
	1	0-1000	,
	2	0-500	
1	3	0-250	
l	4	0-100	
	Ś	0-50	
l	4	0-25	
l	7	0-10	
	8	0-5	
	0		
	y	0-1	

maximum frequency at which the R.F. probe can be operated satisfactorily is not known, but it should be quite satisfactory for comparative measurements to over 10Mc/s. The minimum frequency of accurate operation of the audio probe is well below the lowest audible frequency.

Power Supply

The instrument requires 6.3V at 0.3A for the valve heater and approximately 3mA at about 150V as H.T. This can usually be obtained most conveniently from a receiver power supply using a suitable series dropping resistor. If the receiver H.T. voltage is 250V, a 33k, ½W resistor should be used in the H.T. lead. Alternatively the power supply shown in Fig. 5 could be used.

Construction

The controls on the front panel are S1, S2, and VR2. The meter itself is also fixed there. Resistors R2 to R10 should be mounted around the switch wafer, S1. The potentiometer VR1 should be mounted on a piece of ebonite or perspex in order to minimise leakage. The insulating material used can be mounted on a hole cut in the chassis.

The P.W. Signal Generator

(Continued from page 994)

little difficulty should be encountered if the transformer maker's connection details are followed carefully in conjunction with the circuit diagram.

COMPONENTS LIST FOR POWER SUPPLY UNIT.

R3-4·7k 1W. R4-4·7k 1W. Resistors: R1-2200 JW.

R2-3k or 3.3k 3W. R6-4.7k 1W. Condensers:

CI-350VW, any value between 16 and 100µF. Electrolytic.

C2-As for C1. (These are both obtained in one can.)

C3. 4. 5 and 6—Each 350VW 8 or 16µF. Electrolytic.

Chassis: 6in. x 4in. 21in. high of tin plate or aluminium. (Prototypes use baking tins. The removable bottoms are soldered in place and form the top.)

Switch: S1 Arcolectric T600.

Transformers: Tr1. Input to suit mains (or 200/220/240V tapped). Secondary 0-250V or 0-300V at about 60mA and 6-6.3V at about 2A.

Note: Transformers with a centre tap, i.e. 250-0-250V secondary can be used, but one 250V lead must be cut short or taped and must on no account be used. This type was not used in the prototypes.

Valve: V1, 6X5. International Octal Valve

base.

One or two tag strips, 5 tags not earthed, two earthed.

Warning Lamp: Arcolectric SL82/1/3 from dealers or Messrs. Arcolectric (Switches) Ltd., Central Avenue, West Molesey, Surrey.

Bulb: Any small wattage 6.3V M.E.S. type.

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CP.3/G. As above but with Gram. position, suitable for use with 500 pF tuning condenser: 39'- plus 13'-

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A Capacity Tester for Small Values

THE UNKNOWN CONDENSER IS USED TO ALTER THE TUNING OF AN R.F. OSCILLATOR

By B. J. Roome

OME types of small capacitors are not marked with their capacitance value at all, whilst the values marked on other types—especially the markings on the small waxed mica types—often become obliterated with age. In addition the meaning of the colour coding of some old types of capacitor is not always clear and the colours may not be decisive. If such capacitors are to be used in any apparatus, it is first necessary to ascertain their value. Even if the value is clearly marked, a quick check is worthwhile if the component is not new and will also disclose any open circuited or short circuited component. It is

much wiser to test a doubtful component before use than to spend a very long time finding out why a

completed piece of apparatus will not function.

Principles of Circuit

Fig. 1 shows a circuit which can be used for measuring the value of small condensers. V1(a) is an oscillator, working at a fixed frequency of a few megacycles. The exact frequency is unimportant providing that it is constant. The tuned circuit L/C2 determines the frequency of oscillation. The output of the oscillator is fed, via C7, into V1(b) which is a cathode follower buffer stage. This stage prevents pulling of the oscillator frequency by the test circuit. L4 couples the output from V1(b) into the test circuit

which absorbs maximum power from L3 when the tuned circuit formed by L4, L5, C8, C9 and any capacitors under test (Cx or Cy for future reference), resonates at exactly the same frequency as the frequency of oscillation of VI(a).

The voltage appearing across the test circuit is detected by the germanium diode D1 and the resulting D.C. current deflects the 0-500 microammeter M1. C10 by-passes the R.F. so that it does not pass through the meter, whilst VR1 enables the current passing through the meter to be adjusted to a suitable value.

The 12AU7 is perhaps the most convenient miniature valve, but the octal based 6SN7 is quite suitable. Alternatively two separate 6C4's or 6J5's could be used. Almost any small triodes or triode connected pentodes are perfectly satisfactory. The part of the circuit on the right-hand side of the screen in Fig. 1 is placed on or near the front panel with the valve behind it.

Preliminary Adjustments

A 0-500 microammeter should be inserted between the lower end of R2 and the chassis at the point marked with a cross in Fig. 1. If no reading is obtained at first, reverse the connections of L2. The reading of the microammeter is a measure of the amplitude of oscillation of V1(a). The number of turns on L2 and the spacing of L2 from L1 should be adjusted until the ammeter in the R2 circuit reads about $100\mu\text{A}$. The amount of feedback in the oscillator circuit is controlled by the number of turns on L2 and by its proximity to L1. Generally L2 will consist of about seven turns spaced $\frac{1}{4}$ to $\frac{1}{2}$ in. from L1. After adjustment, L2 should be fixed in position with polystyrene cement. R1 drops the H.T. voltage to

about 100V and also decouples the anode circuit of V1(a).

C8 and C9 should then be adjusted (with no connection across the Cx or Cy terminals) until a reading is obtained on the meter M1. The trimmer C5 should be adjusted for maximum reading on M1 and it should then be set in position with a suitable cement. No further adjustment of the circuit should be required for some years.

Calibration

A fairly large type of tuning dial (calibrated from 0 to 180°) is fitted on the front panel and connected to C9. It has a vernier attachment for accurate reading to 0·1°, but this is not essential. It is advisable to arrange for the dial reading to be zero when the vanes are fully meshed.

A number of 1 or 2per cent

A number of 1 or 2per cent tolerance capacitors should be used for calibration of the instrument, but 5per cent capacitors will suffice for

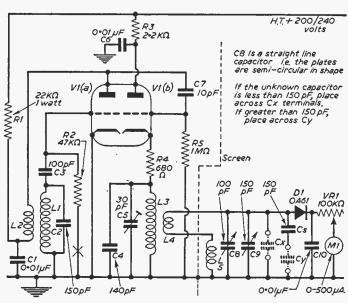


Fig. 1.—The circuit diagram.

approximate work, those used for calibrating the Cx position should all have values between

0 and 150pF.

C9 should be set so that the dial reading is zero when the vanes are fully meshed. C8 is then adjusted for resonance as shown by a maximum reading of M1. If the meter goes off the scale, the resistance of VR1 should be increased, but when C8 has been set, VR1 should be adjusted so that the meter does not read less than half scale (for accuracy). Place one of the calibrating condensers across the terminals marked Cx in Fig. 1; the meter reading falls as the circuit is now off resonance. Alter the value of C9 until resonance is again found, care being taken that C8 is not touched. The reduction in the value of C9 is then equal to the added calibrating capacitance, Cx. Note the reading of the dial connected to C9. Repeat this for other values of calibrating condensers.

A graph of Cx against the dial readings should then be plotted as accurate as possible. The graph should be almost exactly a straight line if C9 has semicircular plates. The graph should be kept for use with

the instrument.

Operation

Values of capacitors from 0 to 150pF can be measured in the following manner. Adjust C8 to resonance with the dial reading of C9 at zero. Connect the unknown, Cx across the terminals and, leaving C8 unaltered, find the C9 dial reading at the new resonance. Using this dial reading and the graph, the unknown capacitance value can be found. The result should be accurate to $\pm 1 \mathrm{pF}$ or better.

Larger Values

The maximum value of the measuring condenser, C9, is 150pF, and therefore capacitance values greater than this cannot be measured by connecting the unknown directly across the Cx terminals. If however, the unknown condenser is placed across the terminals marked Cy in Fig. 1, it will be placed in series with a 150pF capacitor. The series combination will have a value of less than 150pF—in fact it will be between 75pF and 150pF—and the value of this combination can therefore be measured as before.

Thus it is possible to calculate the value of the unknown Cy, from the following equation

Cy=Cr.Cs/Cr-Cs where Cr is the capacitance of Cy and Cs in series, it is well worthwhile calibrating the instrument for values of Cy greater than 150pF. This should be done by placing various known calibrating capacitors across the Cy terminals and plotting the values of Cy against the dial readings as before. In this case, however, the graph will not be a straight line. The graph can then be used to obtain values of unknown capacitors directly from the dial readings.

Whilst there is no definite maximum limit to the value of capacitance which can be measured, the accuracy of the measurement will fall as the value of the unknown increases above 150pF. The practical upper limit is in the region of 2,000 to 10,000pF, depending on the accuracy required and on the accuracy with which the dial can be read.

Final Check

The accuracy of the instrument and of the graph can be quickly checked by determining the capacity of two condensers separately and then determining their capacity in parallel. The latter value should be equal to the sum of the two separate capacities.

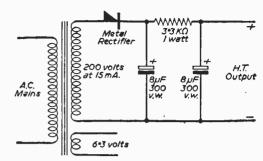


Fig. 2.—A suitable power supply circuit for the tester.

Power Supplies

The instrument requires a 6.3V heater supply at about 0.3A and an H.T. supply of 200 to 240V at about 12mA. This can usually be obtained from a receiver power pack, but if it should be desired to make a separate supply for the unit, the circuit shown in Fig. 2 is quite adequate. The metal rectifier should have a rating of not less than 300V at 15mA.

Alternatively it would be possible to use a small battery double triode (e.g. type DCC90 or 3A5) and make the unit entirely portable. The H.T. voltage could be obtained from a 90V H.T. battery, in which case R1 should be reduced to 2k. The batteries should have a very long life—almost as great as their

shelf life.

COIL DATA L1—25 turns. L2—7 turns on chassis side of L1. L3—25 turns.

L4-6 turns on chassis side of L3.

L5—15 turns.

All coils close-wound on formers, 0-4In. in diameter, using 32 to 36s.w.g. single silk-covered wire. The wires of all coils to be cemented in position with polystyrene solution.

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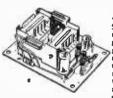
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A D.C. TEST METER

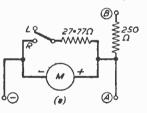
A SIMPLE INSTRUMENT FOR MEASURING VOLTAGE, CURRENT AND RESISTANCE WITH EXTERNAL SHUNTS

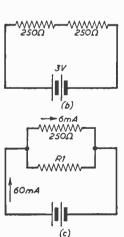
By B. E. Wilkinson

HIS meter is not intended to be the ultimate in test meters, but rather more as a beginner's instrument or as a second one for quick checks. It has the advantages that it is very easy to make, is inexpensive and the number of ranges available is almost unlimited. This is because the series resistors or shunts used to provide the voltage or current ranges are not installed internally in the meter, and switched in as required by a range selector switch, but are made up as jacks, and are plugged in externally. It is thus possible to provide additional ranges when required. To enable those interested to select their own choice of ranges and provide the correct shunts, etc., the calculations will be given for the general case, and a set of recommended ranges.

An Ex-Government Meter

The meter, which is intended to measure D.C. current, voltage and resistance to about 5k, is constructed from a robust ex-government meter, which is intended for checking cells, and measuring resistances approximately. The only indication of type is "Instrument Testing No. 1", which appears at the top, in front of the three terminals and toggle switch. These meters are currently available. The meter is enclosed in a thick, black plastic case, the movement itself being pro-



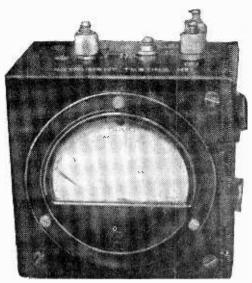


itself being protected by a circle of thick glass and a metal plate screwed over the front. The scale is graduated in volts to 1.5 or 3.0, milliamps to 60, and ohms to infinity, 5k being the highest indicated value.

The Meter Movement

Before deciding upon the ranges required, it is necessary to know something of the meter movement. On the face for instance it states that it has a resistance of 250Ω .

Fig. 1 (left):
(a) The circuit of the instrument.
(b) Equivalent circuit for the low voltage range.
(c) Equivalent circuit on the 60mA range.



The completed meter.

This is essential to calculations, but is not sufficient, for the current required for full scale deflections of the meter needle must be known. However, it will be found that a circuit diagram of the instrument as it stands is provided on the top, and is reproduced in Fig. 1a. Now, from the back of the instrument, where operating instructions are given, it is seen that with the toggle switch to (L) voltages to 3V can be measured across (—) and (B). Since voltages are being measured it is clear that the 250Ω resistor must be in series with the meter and the 27.77Ω shunt resistor must not be connected. Position (L) must therefore be with the switch open. For this voltage range then, the circuit will be similar to Fig. 1b, where the second 250Ω resistor represents the meter movement. The total resistance of the circuit is $250+250=500\Omega$ and the applied voltage for full scale deflection is 3, so that by Ohm's law the current flowing will be

 $a = \frac{E}{R} = \frac{3}{500} = 6mA$

This then is the current required fully to deflect the meter needle, and is a basic value in the calculations. This value may be checked by considering the current-measuring range of the instrument. It will be seen that with the switch in position (R) 60mA will cause a full scale deflection between (—) and (A). This is clearly with the shunt connected but without the series 250Ω . The equivalent circuit is shown in Fig. 1c. Here 60mA are being measured, but since only 6mA may pass through the meter, 60-6=54mA must pass through the shunt. The potential difference across the meter will be E=I. $R=6\times250=1500\text{mV}$. This must be the same as the P.D. across R (since they are in parallel), so that the value of R, will be, by

Ohm's law, $R = \frac{E}{I} = \frac{1500}{54} = 27.77\Omega$, which is in fact the value of the shunt used. We are now in a position to discuss the required current and voltage ranges and the shunts and resistors necessary to provide them.

Fig. 2 (right):
(a, b and c) How the shunts are calculated.

Current Ranges

As far as current is concerned, the meter scale is graduated in milliamps to 60. The ranges considered acceptable for this sort of meter are 6, 60 and 600mA. By using multiples of 6, confusion over readings is avoided. Now, since the meter itself has a 6mA movement, the first range is achieved without a In Fig. 2a the meter is in parallel with a shunt-which is to be calculated for any cur-rent flowing (i). Since the meter must only pass 6mA, the shunt must pass (i-6)mA. The potential difference is The again 1500mV, and by Ohm's Law R1 will be $R1 = E = 1500\Omega$

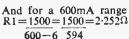
(where I is in milliamps). By substituting for I in this relation it is possible to provide R1 for any

Fig. 3 (right)—Circuit of the instrument when used as an ohmmeter.

desired current range (providing of course it is not less than the sensitivity of the meter movement itself). Thus for a 60mA range

$$R1 = 1500 = 27.7\Omega$$

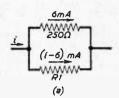
Fig. 4 (right).—Complete circuit arrangement.

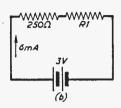


Voltage Ranges

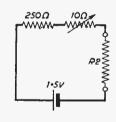
Two voltage ranges are provided on the meter scale, 1.5 and 3. It is suggested that multiples of 3 be con-

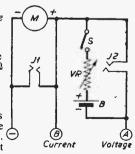
multiples of 3 be considered, i.e.: 3V, 30V and 300V, though the reader is not bound to follow these ranges. To calculate the series resistors required, Fig. 2b must be consulted,





Range	Shunt	Resistor
6mA	None	
60mA	27•77Ω	
600mA	2•525Ω	
3V		250Ω
30V		475ΩΩ
300V		49750V
	(c)	





where the meter is shown in series with a resistor R1 and a voltage to be measured (V). The total circuit resistance (neglecting the source) is (250+R1), and since for full scale deflection, the current flowing must be 6mA the potential difference (V), must be given by

$$V = 6(250 + R1)$$

To obtain R1

$$1000V = 1500 + 6R1$$

$$R1 = \underline{1000V - 1500}$$

$$R1 = \underline{100 (10V - 15)}$$

(The 1000 factor is necessary to convert milliamps into amps.)

For 3V range, the relation becomes:

$$R1 = \frac{100 (30 - 15)}{6} = \frac{100 (15)}{6} = 250\Omega$$

For a 30V range, $R1 = 100 (300 - 15) = 100 (285) = 4750\Omega$

and for a 300V range,

$$R1 = \frac{100 (3000 - 15)}{6} = \frac{100 (2985)}{6} = 49750\Omega$$

For convenience the required values are tabulated in Fig. 2c.

Fig. 2c.

No multimeter should be without a continuity test and ohm range (in fact it is frequently felt that this range is the most useful of all) and since the face is provided with a scale in ohms the opportunity can hardly be missed.

The ohmmeter, which, as will be seen later is built into the instrument, consists of a series circuit—meter, battery, and two resistors, one for adjustment and the other being measured.

Now, on the back of the instrument, instructions will be seen, a note stating that to use the ohmmeter, a cell reading 1.5V should be connected in series with the resistor under test and the (—) and (A) terminals. No adjuster is provided, because the cell is known to be 1.5V before the measurement is made, and the scale is calibrated for use with this cell and a meter resistance of 250Ω.

Therefore the meter is used as it is for measuring resistance by merely providing a 1.5V dry battery. Since at first this may provide a little more than 1.5V, it is well to use a small variable resistance (10Ω) in the circuit to provide a zeroing adjustment. In Fig. 3, the ohmmeter circuit is shown, if the cell is giving exactly 1.5V, then R1 will be adjusted to zero resistance. Suppose that for a resistance R2 (as yet unknown), a current flow of, say, 5mA. The total circuit resistance is (250+R2). Thus we may write:

$$\begin{array}{ccc} E = I \times R & 1.5 = 5 & \underline{(250 + R2)} \\ & 1500 = 1250 + 5R2 \\ & 5R2 = 250 \\ & R2 = 50\Omega \end{array}$$

It will be seen from the meter scale that a current of 5mA (50 indicated because of the internal shunt), corresponds to a resistance of 50Ω . Since the ranges of the proposed multimeter have been discussed, and the values of resistors required have been established, the actual circuit may now be considered.

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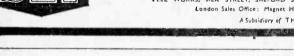
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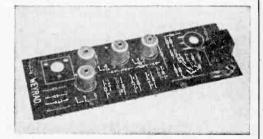




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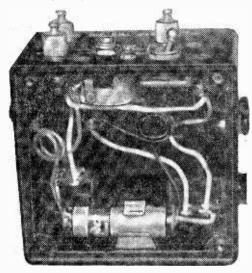
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The Meter Circuit

The circuit is shown in Fig. 4. Here it will be seen that while there is no range selection switch, two jack sockets J1 and J2 are provided. J1 accepts shunts across the meter movement, so that current is measured between terminals (—) and (B). J2 accepts resistors for the voltage ranges, the terminals used being (—) and (A). When neither J1 or J2 is being used, the switch may be closed, and resistance measured between (—) and (A). The variable resistor shown is 1042 and is for zeroing.

Constructional Details

It is now necessary to modify the instrument, and rewire it using the circuit shown in Fig. 4. The unit is held together by eight 4B.A. screws, four at the front, and four holding the back plate in position. If all of these screws are removed the wiring inside may be disconnected and removed, and the meter movement pressed out, forward. Three spring clips, attached to the meter flange by three 6B.A. screws should be removed and discarded. A thick piece of glass under the front plate and two soft-rubber rings are no longer required and should also be discarded.



A rear view of the complete instrument.

The two resistors wound on a plastic former must be removed, but should be set aside as the resistance wire with which they are wound is required. Measurement of the centre hole in the brass plate which was screwed to the front of the unit shows it to be 2.5in. in diameter. The meter itself is 2.7in. in diameter, and since it is intended to fit the meter to the plate, the hole must be enlarged by 0.1 in. all the way round. This can be done quite quickly with a sharp halfround file. When the meter will fit easily through the hole, it should be lined up so that a line drawn through the centre of the scale and the needle adjustment screw is parallel with two opposite sides of the plate. Clearance holes (6B.A.) may now be drilled through the plate to mate with the corresponding holes in the meter flange. The meter may then be bolted to the plate and the plate fitted back on the case.

Looking into the back of the unit, it will be seen that this modification has moved the meter forward, and thus provided sufficient space for further components. The two jack sockets J1 and J2 may now be fitted. They are fitted, one each side of the case, by means of $\frac{1}{8}$ in. holes drilled as shown in Fig. 5b which also shows the meter mounted to the front plate.

The 1012 variable resistor for adjustment of the ohnmeter range, is fitted through a \(\frac{1}{2} \) in. hole drilled in the top of the case, at the intersection of two lines drawn between the centres of the (—) and (B) terminals and the switch and the (A) terminal. The shank of this resistor should be cut down to about \(\frac{1}{2} \) in. and a saw cut made across the diameter to accommodate a screwdriver. The ohnmeter range needs a 1-5V cell to operate the meter, and this takes the form of a single pen cell held to the bottom of the inside of the case by means of a small Terry clip. This can be seen in the photograph of the back of the instrument.

Additional Wiring

Wiring should be carried out with single-strand plastic covered wire similar to that removed from the meter initially. Fig. 5a shows the wiring system. A length of wire is connected between the (-) terminal, and the negative point of the meter. Then a wire is jointed to the positive side of the meter and one side of the toggle switch. The other side of the toggle switch is taken to one side of the 10Ω resistor. The two meter terminals are now connected to the two tags of JI, and the outermost tag of JI is taken to the corresponding tag of J2. Terminal (B), is now taken to the positive side of the meter while terminal (A) is taken to the inner tag of J2 and the negative side of the 1.5V cell. Finally the centre tag of the resistor is taken to the positive side of the cell. In wiring, unless leads are taken to terminals, they should be soldered. The instrument is now virtually complete and the ohm range can be tested. Set the toggle switch to R and connect a piece of wire from (-) to (A). The meter should indicate zero resistance. If it tries to indicate less than zero; i.e. beyond full scale deflection, it can be set to zero by means of the 10Ω resistor. If it indicates a finite resistance, the cell is down and should be replaced. Tests can now be made using resistors up to about 5k. The rear plate of the instrument may now be screwed in position. However, it will be observed that engraved on the back are instructions which are no longer relevant, so that the back plate may be put on reversed, the four holes being countersunk slightly to receive the 4B.A. screws.

The Jacks and Test Prods

To complete the instrument, it is necessary only to provide the shunts and resistors in jacks, and the test prods. Referring to the table of Fig. 2c, we see that for the recommended ranges we require five resistors. For the current ranges the resistors are low, and are made-up from resistance wire. The resistor removed from the meter initially consists of a $27 \cdot 7\Omega$ and a 250Ω resistor. If the $27 \cdot 77\Omega$ resistor is carefully unwound avoiding kinks, as this piece of wire is required, and measured, it will be found to be almost exactly 8ft long. Thus:

exactly 8ft long. Thus: $27.77\Omega = 8$ ft or 96in. $\therefore 1\Omega = 96/27.77$ in. $\therefore 2.525\Omega = 96 \times 2.525 = 8.726$ in. 27.77

Thus a piece of resistance, wire 8.726in. long, taken from the 250Ω winding, will provide a shunt for the 600mA current range. When using this wire, the cotton covering should be removed at each end, and the wire tinned for solderingin. It should be remembered that the actual resistance between the two tags joined by a length of resistance wire does not include that wrapped around the tags, or tinned. Thus the length of wire cut should be slightly longer than that actually required. The jacks to which the resistances are connected are of the standard Post Office type. The resistances are connected across the two connections in the handle of the jack, and the handle replaced. No trouble should be experienced with the series resistors, but the shunts, being made of wire need some support. They may be wound upon a small Tufnol former, with small lengths of tinnned copper wire at either end to provide lead-out tags. The range provided by each jack

should be typed on a small label or piece of paper and stuck to the appropriate jack by means of Sellotape. Pieces of paper with "Current" and "Voltage", should be similarly fixed to J1 and J2 respectively, on the meter case, so that confusion does not arise.

Test prods are an essential part of every test meter, and should be made from flexible, stranded insulated wire. The ends connecting to the meter should be soldered to short lengths (lin. or so) of brass wire, the joint being neatly taped. The brass wire will then fit easily in the angled slots cut in the terminals. At

Fig. 5a (left).—Rear wiring details. Fig. 5b (right).—Side view of the completed test-meter.

the other ends of the leads either brass prods or crocodile clips may be fixed. The brass prods should be sleeved almost to the end, so that one does not hold the bare metal when making measurements.

The instrument should require no calibration, but it is advisable to check it either against a test meter known to be correct, or resistors and cells known also to be correct. To check, for instance, the 3V range it is necessary only to use 1.5 and 3V cells, while the 30V range may be checked with grid bias batteries, car batteries, etc. Any adjustments necessary may be effected by varying slightly the values of resistance in the appropriate jacks.

QUARTZ CRYSTAL ETCHING

(Continued from page 979)

rate of about 1kc/s per minute of immersion has been found with crystals of a frequency of about 8Mc/s, but a longer etching time per kilocycle frequency rise would probably be required for crystals of lower frequencies.

The crystal should be completely immersed in the etching solution for a comparatively short time—perhaps ten minutes—or' less if a small frequency change is desired. The crystal should be removed from the etching solution with the coated tweezers, washed in two successive jars of water (not hard water) and finally dried in a current of warm (not hot) air. Alternatively, the final wash can be made with pure alcohol which is then allowed to evaporate.

The crystal is then remounted in its holder. If it is a type which is held at the corners only by the metal electrodes, care must be taken that the electrodes are replaced so that the projecting corners face the quartz crystal. The frequency of the etched crystal should be determined as accurately as possible. The rate of etching can be determined from the frequency change and an estimate can be made of the time for which the

crystal should be left in the same solution in order to achieve the desired increase of frequency.

The crystal should be etched for not more than three-quarters of the calculated time and the frequency checked again. It should now be possible to calculate fairly accurately the etching time required to increase the frequency to the desired value. If the final frequency must be extremely close to the desired value, it is advisable to etch for somewhat less than the calculated time and to check the frequency several times before completing the process. With care the error in the final frequency will not be appreciably greater than that of the measuring device used—certainly less than 1kc/s.

As etching proceeds, the anode current of the oscillator (Fig. 1) will probably increase somewhat with each frequency check owing to a reduction in the activity of the crystal. The anode current should be noted at each frequency check; an increase of more than a few milliamperes may indicate that the crystal is useless. Do not forget, however, that a change in the oscillator H.T. voltage may cause a change in the anode current.

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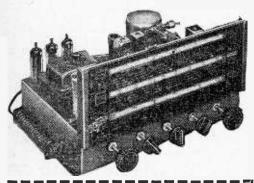
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Trade News

NEW PRODUCTS AND DEVELOPMENTS

A PRECISION MOULDED MAGNETIC TAPE CASSETTE

MUSIC of just the right kind for hotel lounges, ships' lounges, restaurants, fashion houses, etc. or even factories, is provided by the "Reditune" service. Music from a library of over 7.000 titles is provided on magnetic tape which is rented with a playback machine and the required number of speakers giving the effect of a portable orchestra with a repertoire exactly suited to the requirements of the user.

Reditune Ltd. is a member of the Rediffusion

group of companies.

So that the programme can be changed as needed without any skill on the part of the user, tapes are supplied in ingeniously-designed cassettes which are simply inserted into the machine as easily

as posting a letter.

The cassettes are injection moulded by Ekco Plastics Ltd. in polystyrene, each cassette comprising four separate mouldings—the body, the spool base, the spool top and the lid. All except the latter are in high-impact polystyrene, the lid being moulded in transparent polystyrene. The body incorporates two precision-ground brass inserts, a spindle on which the spool turns and a further small spindle to locate an interlocking brake lever. The spool spindle is internally threaded to take the single screw which attaches the lid to the body. The successful operation of the cassette demands freedom from distortion and a high finish with complete absence of flash. A feature which calls for rigidly controlled moulding technique is the need for moulding the spool centre hole to a tolerance of 0.002in The endless magnetic tape unwinds and rewinds on the spool simultaneously and this involves considerable movement between tape and spool. To facilitate this movement, the base of the spool has 12 radially positioned graphite rods cemented to it, the tape actually resting on these rods during playing. The spool top is moulded separately and subsequently cemented in position. (Ekco Plastics Ltd., Press Section, Southend- on-Sea, Essex.)

PERSONAL TRANSISTOR RADIOS

TWO personal transistor radios are now being marketed by Magnavox. Specially-designed printed circuits ter really sensitive long-distance reception, plus hermetically sealed long-life transistors, are included in these new models, retailing at very reasonable prices.

retailing at very reasonable prices.

The "Companion" eight transistor radio features a germanium crystal rectifier and a 2½in. PM dynamic high fidelity speaker. (Price, 13 gns., including purchase tax.) The "Pocketmate" is a six-transistor version with fine reproduction and performance. (Price, 11 gns., including purchase

tax.)

Both are finished in coloured high impact plastic cases and have leather cases with carrying strap plus private listening earphones. An easel clip allows the Magnavox transistor sets to stand firm on any flat surface. (Magnovox, 129 Mount Street, London, W1.)

WIRE RECORDER

AN improved and longer playing version of the well-known Minifon P55 pocket-size wire recorder has been introduced by the Office Equipment Division of E.M.I. Sales and Service Ltd. Known as the Minifon P55L, it now provides a recording/playing back time of five hours. Letters, notes, and memoranda totalling more than 30,000 words can thus be recorded. It is therefore a very convenient instrument for long overseas tours by directors and senior executives, also for busy people—architects, surveyors, civil engineers and plant managers—whose work takes them out and about.

The P55L is the same compact size (4in. by 6½in. by 1½in.) as the Minifon Attache tape dictation machine, and it slips easily into an overcoat pocket. The recording medium is very fine (0.002in. gauge) steel wire wound on two small



A new pocket transistor radio.

plastic spools. The fineness of the wire, even compared with 1 in. wide tape, gives the exceptionally long recording time.

The frequency response is 150-3.500 c/s, the input impedance 2M. and the output impedance 40k. The low-tension battery is a 1.4V standard single cell, with a working life of up to 20 hours. The high-tension battery is of 30V, with a working life of up to 200 hours. Both batteries are, of course, contained in the compact case. (E.M.I. Sales and Service Ltd., Blyth Road, Hayes, Middlesex.)

Club News

REPORTS OF CURRENT ACTIVITIES

CLIFTON AMATEUR RADIO SOCIETY Hon. Sec: C. H. Bullivant, G3D1C, 25 St. Fillans Road, London S.E.6.

Recent meetings have included talks on "DX operating" and "G.P.O. equipment" and a constructional contest which produced 16 entries. On February 24th P. Deacon, G3BCM, will speak on International Radio Regulations.

MITCHAM AND DISTRICT RADIO SOCIETY

Hon. Sec.: M. Pharaoh, G3LCH, 1 Madeira Road, Mitcham. The G5UX Key Award was presented to G2BLa who won the 1959/60 contest for this trophy with a score of over 200 points. On January 13th a talk was given on Lifeboat Radio Equipment. The RSGB affiliated Societies Contest was held on February 5th and 6th. The Annual General Meeting will take place on Friday, 24th February.

Future Events: April 7th—A talk by G2ZU.

PETERBOROUGH AND DISTRICT RADIO SOCIETY

Hon. Sec.: D. Byrne, G3KPO, Jersey House, Eye, Peterborough. At their mid-winter rally held in Peterborough Technical College, members had a working demonstration of new transmitters and receivers by Mr. J. Herries, of Glasgow, who spoke on ssb techniques. Talk-in mobile stations were G3ARS/A on two metres and G3KPO/A on Top Band.

Future Events:
March 3rd—"Aerials". April 7th—Film show. May 5th—"Oscilloscopes".

REIGATE AMATEUR TRANSMITTING SOCIETY

Hon, Sec.: F. D. Thom, G3NKT, 12 Willow Road, Redhill, Surrey. The highlight of the December meeting was a demonstration by BRS 20809 of an ex-R.A.F. morse recorder (made in 1918) which coped quite efficiently with a modern electronic bug-key. The closing date for the constructional contest was January 31st and the entries will be judged at the Annual Dinner on February 11th. This will be held at Laker's Hotel, Redhill 7 for 7-30 p.m. The tickets can be obtained from any committee member price 15/6d. It is hoped that the chief guest will be Les Knight G5LK who was formerly Secretary of the East Surrey Radio Club for many years.

SLADE RADIO SOCIETY

Hon. Sec.: C. N. Smart, 110 Woolmore Road, Erdington, Birmingham 23:

mingham 23.

The Club Station (G3JBN) at the Church House, High Street, Erdington, Birmingham 23, is available for the use of members for constructional purposes. Thursday evening meetings will include informal discussions, operation of the Club transmitter, and instructional Morse classes. A licensed operator of G3JBN will always be in attendance on Thursday evenings. Slow Morse transmissions are radiated on the air each Monday evening from station G3AYJ on 1.9Mc/s from 8 p.m. to 8.30 p.m.

Future Events:

Future Events: February 10th—A special meeting to consider alterations to rules and a discussion on D/F contests and equipment for the 1961 season.

February 24th-Sale of surplus equipment.

SUTTON COLDFIELD RADIO SOCIETY

Hon. Sec.: L. E. R. Hall, 24 Calthorpe Road, Walsall, Staffordshire.

The G3GLQ Trophy was again won by Pat Darrag for a 2m transmitter. On January 12th George Collins, among others, gave a talk on the "Applications for Cheap Valves". A discussion on a standardised design for construction as a group project entitled "Build your own Communication Receivers" was the restriction on languary 26th subject of the meeting on January 26th.

Future Events: February 9th—"Methods of Receiving CW". A discussion of and about CW with demonstration of keys oscillator, B.F.O's etc

February 23rd-"Crystal Grinding and Etching" by John Symes.

March 9th—Club Station Night.

March 23rd—"Tape Recorders". A talk by Len some commercial and industrial uses of tape recorders. A talk by Len Hall about

PLYMOUTH RADIO CLUB

Hon. Sec.: R. Hooper, 2 Chestnut Road, Peverell, Plymouth. Club meetings are held on Tuesday evenings at 7,30 p.m. at Virginia House Settlement, St. Andrews Cross.

Future Events: February 14th—Junk Sale.

April 18th—Judging for the Ernie Hillya May 2nd—Judging for the G5ZT Trophy. -Judging for the Ernie Hillyard Trophy.

WANSTEAD AND WOODFORD RADIO SOCIETY

Hon, Sec.: J. Seaman, 67 Beattyville Gardens, Ilford, Essex, The junior section of the club now meets on Tuesday evenings and not Wednesdays. The senior section meets on Wednesdays. The senior section meets on Wednesdays. The club shack is now being reorganised with better facilities for constructional work.

WEST KENT AMATEUR RADIO SOCIETY

Hon. Sec.: H. F. Richards, 17 Reynolds Lane, Tunbridge Wells. Meetings are held, unless otherwise stated, at Kent County Council Adult Centre, Culveden House, Culverden Park Road, Tunbridge Wells, Kent. Meetings commence at 7.30 p.m. and end at 10 p.m.

A meeting to plan club stand for Tunbridge Wells Hobbies Exhibition was held on January 13th, and a talk on Hi-Fi Techniques was given by R. Trevitt on the 27th.

Future Events:

February 10th—Film Show.
February 23rd—Visit to Crawley Radio Society to hear a lecture on the History of Radio by the Curator of the Science

Museum G5CS.

March 10th—Informal meeting,
March 24th—Planning Meeting for National Field Day.

APPOINTMENTS

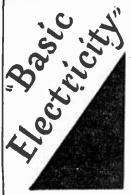
Belling and Lee Ltd. announce the appointment of B. M. Lee as manager of their industrial group, reporting to the company's general manager, and to the board of executive directors. This is a further step in the divisionalisation of the company into separate industrial, and domestic groups, in a programme of controlled expansion which began with the reorganisation of the sales department earlier in the year. He will be responsible for co-ordinating the production, publicity and sales of the industrial group.

Mr. Lee, who is the son of E. M. Lee, B.Sc., M.I.E.E., director and General Manager, and one of the original founders, has spent a number of years in different departments of the Company, and in other companies in the industry, in training for his new post. His appointment will relieve the directors of a considerable amount of detailed work, allowing them more time for matters of general management and planning for the future.

L. A. Norman, assistant sales manager of Stella Radio and Television Co. Ltd. since May 1960, is appointed sales manager as from January 1st, 1961.

During the thirty-two years that Mr. Norman has spent in the radio industry he has become a well-known figure. He joined Philips in their radio sales office in 1928, and after serving in the R.A.F. from 1941 until 1946, re-joined the company in charge of the Century House showroom.

Shortly afterwards he represented Philips radio and television in S.E. and S.W. London and the West End.



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Autochanger RC210
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OZ4 IR5 IS5 IT4 2X2 3Q5 3S4 3V4 5U4 5Y3G	61- 61- 51- 216 91- 716 716 61- 61-	6BA6 6BE6 6C4 6D6 6F6G 6G6 6H6 6J5 6J6	71- 51- 61- 71- 316 516 516	65N7GT 6U5G 6V6G 6X5G 12AT7 12AU7 12AX7 12K7GT	61- 616 716 51- 61- 61- 616 616	DF96 DK96 DL96 EABC80 EB91 EBC41 EBF80 ECC84 ECH42 ECH42	8/- 8/- 8/-	EL41 EL84 EM81 EY51 EY86 EZ40 EZ80 E1148 HABC8	91- 816 916 716 71- 71- 71-	PCL82 PY80 PY81 PY82 PY83 QP25 R3 SP61 UF41 UL41	81- 716 816 71- 91- 71- 716 316 816	FERRODYNAMICS "BRAND FIVE" Sin. 600ft. 16/- Sln. 900ft. 18/6 Spin. 1,200ft. 23/6 Tin. 1,200ft. 25/- Tin. 1,800ft. 35/- Tin. 1,800ft. 35/- Tin. 1,800ft. 35/- Tin. 2,400ft. 60/- Illustrated loaflet 5.A.E. Spare Reels, plastic, all sizes. 3/- "Instant" Bulk Tape Eraser and Head De- fluxer, 200/250 v. A.C., 27/6. Leaflet, S.A.E.
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6/12 V. 4 a 12/3	250 v. 80 m.a 5/11
6/12 V. 6 a 15/3	250 v. 250 m.a 11/9
6/12 v. 10 a 25/9	CONTACTCOOLED
6/12 v. 15 a 35/9	250 v. 80 m.a. H.W.
24 V. 2 a 14/9	6/11, 250 v. 75 m.a.
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line. Fitted Mullard valves, Duar inputs
for 'mike' and gram, etc. Bass and
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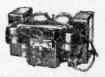
MICRO-AMMETERS, 3in. diam. 0-50 micro-amps, 33/9, 3in. diam. 0-500 micro-amps, 39/9.

RELAYS. Carpenters' Type. Polarised 2 times 9.500 turns at 1.885 ohms, 13/9. Miniature Moving Coil Differential Type. Single pole 2-way, or centre stable. Two coils each 350 ohms, Minimum operating current 140 micro-amps, nominal 400 micro-amps maximum 8 milli-amps. Two way contact current 100 mA at 50 v. A.C. or D.C. Size 1½ x½ x iin. approx.. 13/9. Miniature Type G.E.C. 670 Sealed, wire ends. 4 c/overs. platinum M1095, 12/9. SPECIAL OFFER MENT SELENIUM RECTIFIERS, 12v. 15 amp, with large square cooling fins. 19/9 each.

EX. GOVT. SMOOTHING CHOKES. 200 mA., 3-5 H., 50 ohms, Parmeko 8/9: 100 mA., 5 H., 100 ohms, 3/11: 150 mA., 10 H., 50 ohms 9/9: 30 mA., 20 H., 500 ohms 5/9: 120 mA., 12 H., 100 ohms 8/9: 50 mA., 50 H., 1,000 ohms 6/9: 100 mA., 10 H., 100 ohms 6/9: 60 mA., 5-10 H., 250 ohms 2/11.

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THE Senior H.R.O. was designed and produced originally in 1935 to provide reliable communication even under adverse conditions and soon established a reputation of reliability. Based on a fundamentally sound design and built to precision standards, this high performance receiver was not cheap to produce, ranking among the more expensive representatives of its class.

Superhet Models

The Senior H.R.O. is no longer manufactured having been superseded by more up-to-date double superheterodyne models of very advanced design.

The author however has had in daily use a Senior H.R.O. for some time in conjunction with a variety of aerials. This particular model has been available for some time.

Models Available

The models available on the surplus market are the H.R.O., H.R.O.-M and H.R.O.-MX, all of which apart from slight modifications are fundamentally alike. The valves used in all instances are of the UX based types.

Valve Line Up

The valve line up is as follows: the first and second R.F. amplifiers are 6D6 valves, the first and second I.F. amplifiers are 6D6 valves and the mixer valve is a 6C6. There is a separate local oscillator 6C6 valve. The detector AVC diode and first audio amplifier is a 6Q7. The beat frequency oscillator is a 6C6 valve and the power output valve is a 42.

Tuning Range

These receivers cover a very wide band of frequencies by means of a separate four-coil unit. The total range being from 10m to 6000m, nine coil units being provided. These are of the general coverage type which are not fitted with the extra band spread facilities common to the pre-war standard models.

Standard Model Bandspread

In the standard models, bandspread was accomplished by the transfer of set screws from one set of contact plates to another. By this means small padding condensers were introduced in series with the tuning condenser to reduce the tuning range, and a parallel trimmer to adjust the range to the desired part of the tuning dial.

This system enabled the user to cover the amateur bands with the more limited spread of the general coverage setting with one coil and with extra bandspread covering 400 divisions of the 500 division tuning dial. The overlap between the two coils being arranged with this idea in view.

That the surplus models are supplied only with nine general coverage coils is not the disadvantage it may appear, as the normal dial spread is sufficient to meet the requirements of the average listener, as later details relative to the main tuning arrangements will show.

Later Models

In addition to the earlier models mentioned, all of which use glass valves, later models in which the international types are used are also available. The valve line up being 6K7M, 6K7M, 6J7M, 6J7M, 6K7M, 6K7M, 6SQ7M, 6J7M, and 6V6GT/G, and the models are the H.R.O. 5T and 5R. The former being the table model and the latter the rack model.

All were manufactured during the war and are fitted with a 0-1 milliammeter instead of a calibrated S meter. According to the National Company, 0.5 designates S9 and 1mA is 40dB over S9.

Tuning Ranges

Type

The full coverage of the H.R.O. is as follows:

L.F. Bands

4Mc/s band.

I - 50	 	 100kc/s	band.	
H - 100		 200kc/s	band.	
G - 180		430kc/s	band.	
F - 480		 960kc/s	band.	
E - 900		 2050kc/s		
Coil Set				
Type		H.F. B	ands	
JA-14-0	 	 30.0Mc/s	band.	
		 14-4Mc/s	band.	
16 3.5		7-3 Mc/s		

This coverage is a most extensive one and reference to the chart mounted on each coil unit enables the operator to quickly check frequency. The calibration of each coil unit being very accurate indeed.

A Useful Suggestion

One of the bugbears met by most users of mains driven short wave receivers is frequency drift after switching on. As the coil units in the H.R.O. are below the chassis and well insulated from the heat generated in the well ventilated steel cabinet frequency

drift after a twenty minutes warm-up period is negligible.

Technical Features

One of the highlights of this receiver is the four gang tuning condenser, reduction gear box and tuning The condensers being of the straight line frequency type of 225pF capacity.

Instead of a common rotor shaft each condenser is completely insulated from the others. This principle of construction has considerable bearing on

the stability of the receiver.

Ceramic trimmers are used in all coil units and maintain their setting, resulting in a very superior L/C ratio with constant gain through the various

tuning ranges.

The tuning dial with its 20-1 ratio gear drive which includes a precision hobbed worm is spring loaded. The direct reading dial is divided into fifty divisions with apertures ten divisions apart. Ten turns of the dial are necessary to cover the full travel of the condenser rotors. This totals 500 divisions providing an effective scale length of twelve feet and allows readings to one part in five hundred, The calibration is nearly linear.

Controls

Fig. 1 shows a detailed sketch of the H.R.O., H.R.O.-M, and H.R.O.-MX type receivers.

Panel Controls

There are five controls mounted on the front panel and five switches, in addition to the tuning dial.

The R.F. gain control varies the gain of the second R.F. stage and the two I.F. amplifiers. This control is also used to zero the S meter in conjunction with an internal pre-

set potentiometer.

An A.F. gain control is also fitted. The inclusion of these two controls enables the operator, by the combination of adjustment, to obtain a most satisfactory signal to noise ratio on both strong and relatively weak signals.

Selectivity Switch

At the top-right-hand side of the panel is the selectivity switch which tunes the secondary of the first L.F. transformer and is used in conjunction with the crystal filter. When the crystal filter is not in use the selectivity control is used as an I.F. trimmer and set to a point which provides maximum volume and sensitivity.

This control in operation is a very effective one; so much so that in many instances the crystal filter is not required.

Phasing Control

Below the selectivity control is the phasing control with an integral crystal filter switch.

The crystal phasing control dial plate is graduated from 0—10. When set at zero the crystal filter is out. When at settings between 1 and 10 the crystal filter is in, and the phasing control is used to balance the crystal bridge.

Using the phasing control in conjunction with the selectivity control enables the receiver selectivity to be varied according to requirements, and interfering signals suppressed. Band width variation is from 2.5kc/s to 200c/s in the sharp position.

As the official handbook supplied with the Senior H.R.O. receivers at present available provides full details as to setting up and operating the receiver controls including the crystal filter, the author does not propose to offer further comment on the subject.

Fig. 1, shows the beat oscillator control which also has an integral on/off switch. The dial plate is also graduated from 0-10. This control clockwise switches H.T. voltage to the anode and screen of the beat oscillator valve and between 0 and 10 provides a frequency variation over a range of 10kc/s.

While the beat oscillator tunes to the I.F. frequency, when set at approximately 9, the pitch of the note can be varied as desired.

With the facilities which enable the C.W. listener to vary the pitch of the C.W. note, the beat oscillator is an asset to the amateur phone and S.W. broadcast listener in the location of the DX stations carrier

Immediately above the beat frequency oscillator control is the AVC switch. This is switched to the left for AVC in and to the right for AVC out. The AVC being switched out for C.W. reception, with the beat oscillator switched in and pitch control set initially to nine on the dial plate, later to be adjusted to a pleasing note.

10 revolutions of dial = 500 divisions

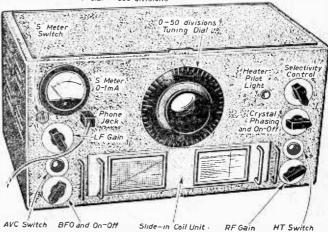


Fig. 1.—The controls of the Senior H.R.O.

L.F. Gain Control

Above the AVC switch is the L.F. gain control which also has the dial plate graduated from 0-10. Above this and slightly to the left is the S meter switch and to the right the headphones jack.

The S Meter

The S meter should always be switched out when receiving strong S.W. broadcast signals.

As previously mentioned the S meter is not as

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fitted to pre-war commercial models and including dB above \$9, but is a 0—1 milliammeter graduated as follows: 0, 0.2, 0.4, 0.6, 0.8, 1.0. This form of S meter is not easy to read at a glance and the operator should graph the scale with one graph from 0 to \$9 and another from \$9\$ to 10dB over \$9\$. Alternatively the two can be combined in one graph.

Apart from its usefulness as a check on variations in signal intensity, an S meter is an adjunct which can be very useful in comparing the signal gain of one aerial and another be they of the same or different

types.

This applies especially to fixed relay controlled

doublets and rotary beams.

The H.R.O. S meter circuitry is in the form of a three element bridge all of which are fixed. Adjustment of the R.F. gain control brings the controlled valves to a predetermined value of A.C. resistance and the S meter needle to zero amplification will thus conform to the S meter scale.

Modification

In some instances competent amateurs have modified the H.R.O. by fitting the more modern octal valves or alternatively miniatures. The UX types fitted are, however, in plentiful supply and as it stands the H.R.O. receiver is an excellent performer more especially if used with an efficient aerial.

The sensitivity available far exceeds that which can be used in industrial locations. The judicious use of the R.F. and L.F. volume controls assuring a satisfactory signal to noise ratio on both strong and

weak signals.

Noise Limiters

Most of the modern communication receivers are fitted with some form of noise limiter, but the H.R.O. models outlined in this article are not.

But while such modifying devices which have been designed are effective where there is strong electrical interference with signals of average strength, what effect the addition of a noise limiter will have on sensitivity and weak signals is worth considering. This being so, a tried and proved design of noise limiter is advised which should have provision for switching out.

Aerials

Provision is made in the H.R.O. for the use of single wire fed and twin wire fed aerials. If doublets are used the jumper lead from the E terminal to chassis is removed from the earth terminal end, and the twin feeders inserted in the aerial and earth terminals. This also applies to the noise reducing type doublets and vertical rod systems which are used in conjunction with matching transformers.

Owing to its wide frequency coverage, high sensitivity and selectivity the Senior H.R.O. will meet the requirements of both the amateur bands

and short wave broadcast listener.

Power Supplies

Unlike many other communication receivers the H.R.O. has no built in power supply. Type D power units which include a built in 6in. speaker are of British manufacture and are readily available. Also the original National 697 unit which does not include a speaker.

In addition are the 697AB for 105 to 120V, A.C.,

and the 6V vibrator, 686S.

For those who wish to use a separate loudspeaker the output is 3W at a nominal impedance of 7k, the headphone jack being for high impedance headphones.

A Versatile Tape Recorder

(Continued from page 991)

place and before anything else is added, the valve heaters are wired with twisted, P.V.C. covered copper wire. After being put in place the wire should be pushed flat on to the chassis. The leads from V4 out of the chassis should be wired

with flexible, plastic covered wire.

If the neon bulb to be used has its own lead it should be mounted now to save difficulty later when wiring is commenced. The switch, volume and tone controls, coaxial sockets and front panel are now added. A screened lead (with screen earthed to the earthed sections on the switch) should be taken along the angle of the chassis from SA to pin 9 of VI. SAI and SA2 are connected to socket A and SC is connected to socket C. (Care should be taken not to overheat the centre pin of sockets A, B, C and D as the insulation may melt.)

The oscillator coil L1 and C19 are now fixed in place; L1 being attached by its plastic fixing bolt so that the three contacts of the coil are in a convenient position for wiring. Wire the oscillator section completely, except for the earthed ends of K21 and R22 which will be connected later to

the earth-bar.

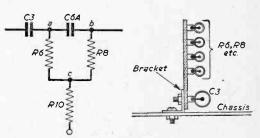


Fig. 12 (left).—An alternative equaliser circuit.

Fig. 13 (right).—The tag-board for the equaliser.

The Oscillator Screen

Bolt the oscillator screen in place, taking care not to short-out any wires. The next step is to fix the large tag-board to the back wall of the chassis by two 6BA bolts, using nuts as spacers. Using sleeving if necessary, wire the tag-board to valve holders 1, 2 and 3. The equaliser tag-board is now mounted as shown in the diagrams and wired in.

(To be continued)

Letters to the Editor

The Editor does not necessarily agree with the opinions expressed by his correspondents

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELE-PHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iii of cover.

PUSH-PULL AMPLIFIER

SIR.-Referring to the query of J Haskell (January issue), the value of resistors for EL84 valves is about 270Ω, 5per cent tolerance, 3 to 5W, and the cathode by-pass capacitors $25\mu F$, 12V.W. A suggestion I would like to make is that only one fixed resistor be used, the other being balanced. This ensures that the valves are balanced. If an ammeter is connected in series with the fixed resistor and by-pass capacitor, and the cathode of the valve, note the reading on the meter. Next connect the meter in series with the cathode of the other valve and the variable resistor and the by-pass capacitor, now adjust the variable resistor until the reading on the meter is the same as that for the first valve. The valves are now balanced. If the fixed resistor is 270Ω the variable resistor value should be about 500Ω.-R. Davies (Nottingham).

HIGH FIDELITY

SIR.—I find it most annoying that the phrase "High Fidelity" is so mis-used.

Now I see small gramophones (with atrocious reproduction, scratch, etc.) described as High Fidelity reproducers; but I had always been taught that high fidelity apparatus was large, with several speakers and far more than portable.

Now, recently I have seen a cardboard disc with a plastic outside for the grooves (which, incidentally had far worse scratch than the average 78 r.p.m., record, for it was a 45 r.p.m., record) with "Hi Fi" Disc in letters one half of an inch high on it.

Would that people would only use "High Fidelity" in its proper sense.—P. H. (Langport, Somerset).

ONE VALVER

SIR,—With reference to Mr. D. Illingworth's letter in the January issue, the internal resistance of his H.T. battery may cause a misleading voltmeter reading.

If his set continues to work while the voltmeter is connected, he can use with advantage a two cell battery for H.T. — C. H. WHITE (Ilfracombe, Devon).

CRYSTAL SET RECEPTION

SIR,—with reference to Mr. A. Radmore's letter (P.W. January), I should like to inform him that the coil I used in my crystal set was a home wound, medium-wave type and consisted of 90 turns of 22s.w.g. copper wire, on a 2in. wooden former. The detector was a germanium diode.

He may also be interested to learn that French, German and other Continental stations have been received at good strength. — D. J. CONNOLLY (Edinburgh).

MODULATION

SIR,—With reference to J. R. Miller's letter (January issue), the snag in his proposed method of modulation lies in the low plate efficiency of the final amplifier, the maximum efficiency obtainable being about 35 per cent. This is because the peak instantaneous power in a 100 per cent modulated signal is four times the carrier power. Under carrier conditions (i.e. with no modulation), the final amplifier will be producing one quarter of its maximum power output. The plate current, and therefore the power input, will be about half the maximum. The plate efficiency will therefore be only half the efficiency at maximum power, i.e. about 35 per cent. In practice the efficiency may be considerably less, since the amplifier must be operated in class AB or B.

In answer to Mr. Miller's second question, to give an output of 150W an input of 200W to 250W will be required (depending on the valve(s), used), 100W to 125W of audio will be needed for modulation. If, however, Mr. Miller means 150W input, which would give an R.F. output of 100W to 120W, 75W of audio are required. In order to allow for losses, the theoretical power output of the modulator valves should be about 20 per cent greater than the figures given above.

At 750V on the plate, a pair of 807's in class AB2 will deliver 120W into a 6950Ω load (plate to plate). At 600V, the output is 80W into 6400Ω , and may be increased to about 90W by reducing the load impedance. — D. PRICE (Cape Town, South Africa).

SIR.—Referring to Mr. J. R. Miller's letter in the January issue, I would like to explain why amplitude modulation is only carried out in the final R.R. amplifier. (Apart from the possibility of F.M. being caused by coupling or poor power supply regulation, etc.)

In most transmitters the doubling, amplifying and final stages are usually run in class "C" because of the high efficiency possible using this mode of operation (70 to 80 per cent). If modulation of intermediate stages is attempted, the

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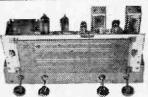
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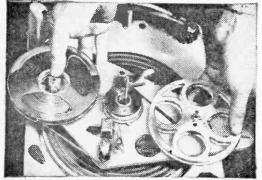
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modulated R.F. waveform would be extremely distorted since the output of a class C amplifier is

not directly proportional to its input.

Modulation of an early stage, followed by amplification is possible however if the succeeding stages are operated in linear class B, but the efficiency of such a stage for a modulated R.F. input is only around 35per cent, i.e. to give the same output in the final amplifier as a corresponding class C stage, the power drawn from the supply would have to be doubled (assumed to be within the valve's ratings).

To modulate 150W of R.F. the power output from the modulator valves should be around 85 to 90W to compensate for modulation transformer losses, and this can easily be supplied by 807's in AB2 with 650V on the anodes.—M. D. POLLARD

(Chertsey).

RADIO MOSCOW

SIR,—I read with interest both Mr. P. J. Kennett and Mr. E. Haines's letters (January 1961) concerning Radio Moscow. Mr. Haines in his letter states that the Moscow transmitters are the most powerful in the world, this is not so. In the 49m band Moscow broadcasts on about 20 wavelengths on three of these wavelengths, to be precise 49.67, 49.59 and 49.42m, the power output is 100KW. In the other short wavebands, Moscow commands many wavelengths, e.g. in the 25m band Moscow broadcasts on 23 wavelengths, and the most powerful output on one of these wavelengths is 100KW on 25.17m in fact.

Many of the American stations are twice as powerful, e.g. radio stations KRCA, at Dixon, and

WLWO at Cincinnati.

In the longwave band, on 1734m, Moscow's output is 500KW, 100KW more than our own Light programme, on 1,500m. Even this phenomenal output cannot be compared with the V.O.A. transmitters, at San Fernando, in the Phillipines, and at Okinawa in the Ryukyu chain. These stations broadcast on 263m, and 254m respectively, and both their power outputs are 1,000KW! This is twice as powerful as the known most powerful Russian transmitter.—T. Roeves (Alcester).

SIR,—With reference to the letter of E. Haines (January 1961), I should like to state that the transmitters employed by Radio Moscow are not the most powerful in the world. The Voice of America fills this position with three transmitters each having an output of one million watts located at Munich (173kc/s), Okinawa (1180kc/s) and Manila (1140kc/s). It is possible that Radio Moscow's short-wave transmitters are more powerful than those of the Voice of America whose most powerful have an output of 200KW. However, the Voice of America is currently building a new shortwave station in North Carolina which will house six 500KW shortwave transmitters which will be in operation by the end of 1962.

Reader P. J. Kennett (January 1961), has already stated the correct facts which need not be duplicated here concerning the relay of Radio Moscow by other stations. However, it is of interest to note the following facts about the Voice

of America relay stations:-

There are nine relay stations (excluding those in the U.S.A.) of which eight are land-based. The ninth is situated off the island of Rhodes in the Mediterranean and takes the form of the United States Coast Guard vessel "Courier". The others are situated in Germany, Great Britain, Greece, Ceylon, Ryukyu Islands and Philippine Islands.

Those Voice of America stations which announce a call sign are located in the U.S.A. — stations WBOU, WDSI, WLWO and WGEO in New Jersey, New York and Ohio and KNBH and

KCBR in California.

The only links which the Voice of America studios in Washington have with the relay bases overseas are via the transmitting stations in the U.S.A. Should trans-Atlantic or trans-Pacific communications be impossible due to prevailing atmospheric conditions the relay bases are obliged to broadcast recorded programmes from tapes.—B. J. Ayres (Chessington, Surrey).

TRANSISTOR HOLDERS

SIR,—May I add a few comments to some of the letters and opinions expressed in the current issue of Practical Wireless.

E. M. Krell asks why nobody has produced a transistor holder to avoid soldering. If he cares to look through the advertisements in this or most of the other publications of a similar nature he

will see them offered time and again.

F. Keating asks how to play a tape backwards. To do this he should turn his tape over as if he was going to play back the other track and then twist it so that the glossy back of the tape is running against the playback head instead of the dull-coated side.—J. G. WATT (Yorkshire).

MODULATION

SIR,—Referring to Mr Miller's letter in the January issue of PRACHICAL WIRELESS, I would like to say that modulation of an oscillator is very undesirable. It is due to F.M. that always occurs when amplitude modulation is applied directly to the frequency-controlling stage (the oscillator).

In America, at least, amplitude modulation of an oscillator is permitted only on frequencies above 144Mc/s.—V. Th. KJARTANSSON (Reykjavik,

Iceland).

CRYSTALS

S1R,—In February PRACTICAL WIRELESS there is a letter from T. L. Mence who requires some Hertzite crystal. I was connected with the wireless trade from 1928 to 1938 and I have a small supply of Hertzite that we used to put into glass tubes for sales purposes.

If T. L. Mence or any other readers would like a piece (so far as my small stock allows) and cares to contact me I will let them have some if they would send a stamped addressed envelope. I have also been an amateur radio fan on and off since about 1922 and took the first PRACTICAL WIRELESS. So far back, anyway, that I can remember an issue that gave instructions for running a radio from

gas.

I was very interested a month or so ago when Thermion looked back. I also remember the glass tube with practically all of a 3 valve set enclosed made by a German firm at about 1932.—

B. Andrew (37 Grimsbury Drive, Banbury, Oxfordshire).

PLAYING A TAPE BACKWARDS

SIR,—With reference to the letter "Playing a record backwards," February edition, I have two solutions. Either record on a twin track taperecorder then remove the spools, placing them on a four track tape-recorder, one of these tracks will play the recording backwards; or record as normal and then place the left spool on the right and right on left, pick up right spool and turn over (the twist in the tape take comes before the recording head) and play.—M. BRICKWOOD (London, E7).

SIR,—I was interested to read, in the February issue, how Mr. Keating played a gramophone record "backwards," and perhaps I can help him in his efforts to play a tape recording in this manner.

He must first make a normal recording near the end of a reel of tape. The tapes are then "changed over" so that what was once the "feeder" spool becomes the "take-up" spool. The other spool (which now "feeds"), is forced to move clockwise instead of anticlockwise as it would normally do.

Although this means that the tape can now be played "backwards", it also means that the tape is being played with the insensitive side towards the head and consequently a slight lessening of volume is also noted.—J. B. DE BOER (Huddersfield).

SIR,—I would like to let Mr. Keating know how to play a tape recording in reverse. The only disadvantages are that the output of sound is reduced, and that the higher treble frequencies are lost.

Having placed full reel of tape on the feed spindle as normal, turn it over and replace on spindle. Take the leader tape and join it to the take-up spool in the normal manner. The tape can now be played in reverse, but do not attempt to rewind as the tape will unreel from the spool.

Incidentally, if the reversed tape spools are interchanged to give the same pattern of feed and take-up, then the recorded sound will be heard as normal

l hope this will enlighten all interested parties.

—D. HARTLAND (Bournemouth).

SHORT-WAVE LISTENERS' LOG-5

HORT-WAVE listeners who are learning Morse, but cannot attend a group or class, may obtain good practice in reading by listening on the amateur bands. Many recently licensed amateurs commence working on the 80m band, and listening on frequencies around 3.5Mc/s to 3.6Mc/s will usually provide some Morse signals of only moderate speed. It is not, of course, possible to read Morse at once, even after the code has been memorised, but all practice at reading "off the air." will help to increase speed. Normally, listening and reading should not be for more than 10 or 15 minutes at a time, for a beginning. Amateur activity also varies greatly from time to time, so lack of suitable signals does not mean it is not worth trying the band again.

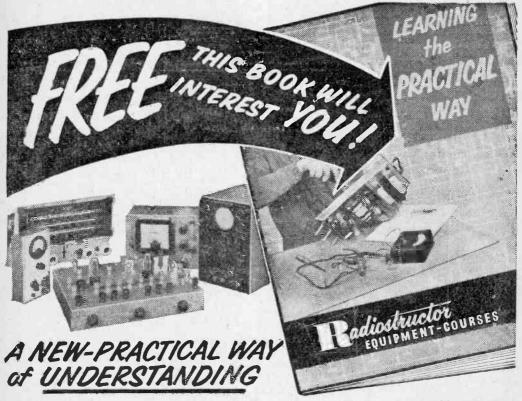
In addition to usual activity, broadcasts of particular interest are occasionally heard on the amateur bands. Shipping, or ship to shore, communications may be heard around 1850kc/s in the 160m band. Around 3-6Mc/s in the 80m band will often give good reception of special bulletins of particular interest to amateurs, commencing at 10 a.m. on Sundays. On the higher frequency bands it is usually possible to hear and identify transmissions from a number of distant countries, in addition to regulars such as the U.S.A. It is best to try each band at various times, as conditions change from hour to hour.

The listener who has no special short-wave set will find the 31m and 41m bands particularly satisfactory after dark. Strong signals from Prague, Rome, and other fairly near stations can be expected, with English programmes beginning at 18.00 G.M.T. Voice of America transmissions will often furnish 9-plus signals. For more distant reception, it is worth trying approximately 7-1Mc/s, as Radio Peking can easily be an R9 signal during the early evening, and gives a programme in English at 21.00 G.M.T.

It is interesting to hear the news in Special English, radiated each weekday except Saturday by the Voice of America at 19.00 and 20.00 G.M.T. Frequencies and wavelengths used include: 21.5Mc/s, 13.95m; 15.2Mc/s, 19.73m; 11.76Mc/s, 25.5m; 9.635Mc/s, 31.41m; 9.62Mc/s, 31.19m, 9.52Mc/s, 31.51m; and 6.185Mc/s, or 48.5m, Broadcasts in the international language Esperanto may also be heard, some of the transmissions being as follows: Rio de Janeiro, 30.78m and 25.48m, 09.00 to 09.30 G.M.T. Sundays; Sofia, 41.35m, 39.11m and 30.93m, 19.00 to 19.25 G.M.T. Sundays; Juiz de Fora, 60.91m, 00.45 to 01.00 G.M.T. Mondays; Bern, 48.66m and 31.46m, 17.35 to 17.40 G.M.T. Mondays: Rome, 50.34m, 41.24m and 30.9m, 17.55 to 18.10 G.M.T. Tuesdays.

Listeners who are badly troubled by untunable interference, or lack of good signal strength, may find that a simple dipole solves these problems. With a single-wire aerial, feeding the receiver from one end, static is carried to the set with the signal. But with a dipole, static is in phase in both halves of the aerial, and thus largely cancels out on reaching the twin feeder. The desired signals, on the other hand, are out of phase in the two halves of the aerial, and are thus carried to the receiver. In addition, a dipole does not have the broad-band reception characteristics of a single, end-coupled aerial wire, and this also reduces general interference very considerably.

A dipole can be made from 7/22 or similar aerial wire. Its total length is 0.95 of a half-wave—or about 66ft for the 40m band. This total length is cut in half, and an insulator is inserted. From this insulator a twin-lead or coaxial cable is taken to the receiver. One conductor of this feeder thus goes to each 33ft portion of the aerial. The whole is supported in the usual way with insulators at each end of the two 33ft horizontal top wires, the feeder descending from the centre to the receiver. Very good results will also be obtained on 20m and 10m bands.



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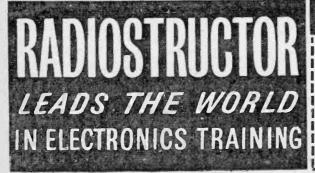
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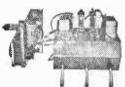
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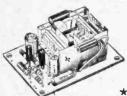
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