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 OZ4 ．$10 Z 4$
IA3
$1 A 5$
IA7GT
IC5

｜A7GT| $31-6 F 11$ | 1713 | 10 Cl | 131.30 PLI 3 | 1216 |
| :--- | :--- | :--- | :--- | :--- |
| 1016 | DF97 |  |  |  |A7GT 2＇$=6$ F12 $\quad 416$ 10C2 $\quad 2616$ 35A5 $21 / 3$ DH63

ID6 IG6

IH5GT $10166 F 17$ \begin{tabular}{ll|l}
ILDS \& $5 \%$ \& $6 F 23$ <br>
ILNS \& $5 \%$ \& $6 F 33$

 

IN5GT 1016 \& $6 G 6$ <br>
IRS \& 616 \& 6HSGT
\end{tabular} IRS

IS4
IS5
$1 \cup 5$
2 P
$1 \cup 5$
2 P
$2 \times 2$
$3 A 4$
3 A 4

| $3 B 7$ | $10^{\prime} 6$ | $6 K 8 G$ |
| :--- | :--- | :--- | :--- |
| $3 K 25$ |  |  |

$\begin{array}{lllllll} & 51 & 6 \mathrm{LI} & 2313 & 12 \mathrm{AX7} & 7 / 6 & 185 \mathrm{BT} \\ 3 \mathrm{Q} & 716 & 33!2 & \mathrm{EABC} & 60\end{array}$

| $3 Q 5 G T$ | $9 / 6$ | $6 L 6 M$ |
| :--- | :--- | :--- |
| $3 S 4$ | $7 /$. | $6 L 7 G T$ |

71 6L7GT $\quad 76$ 12BH7| 5R4GY 1716 | 6 L 19 | 2313 | 12 EI | 301.807 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1215 GT | 416 | 956 |  |  |

$5 \vee 4 G \quad 101-6 L D 20$


| $6 A 8 G$ | $9 \prime$ | $6 Q 7 G$ | 616 | $12 S A 7$ |
| :--- | :--- | :--- | :--- | :--- |
| $6 A 8 G$ | $9 /$ | $11 /$ | $12 S C 7$ |  |


| $6 A B 8$ | $9 \prime-6 R 7 G$ | $10^{\prime}-$ |
| :--- | :--- | :--- |
| $6 A C 7$ | $4 \prime-6 S A 7 G T$ | $8 / 6$ |
| $6 S H 7$ | $12 S H 7$ |  |

$\begin{array}{llllllll}\text { 6AG5 } & 5 / 6 & 6 S C 7 & 7 / 6 & 12 S J 7 & 8 / 6 & \text { AC6PEN } 7 / 6 & E C S 2\end{array}$
6AL5 4 －6SH7GT 8＇－ $12 \mathrm{SQ7} \quad 1$


6AV6 1218 6SQ7GT 9＇－ $19 \mathrm{AQS} 10^{\prime} 6 \mathrm{BL} 63$
6AV6 1218 6SQ7GT 9＇－ $19 \mathrm{AQS} 10^{\prime} 6 \mathrm{BL} 63$

6BA6 716 6U4GT 101．CI 126 ECC35 8| $6 B E 6$ | $6 \%$ | $6 U 5 G$ | $7 / 6$ | 20 F 2 |
| :--- | ---: | :--- | :--- | :--- |

$\begin{array}{lrl}68 G 6 G & 23 & 6 U 7 G \\ 68 H 6 & 81 . & 6 V 6 G\end{array}$ | 1 |
| :--- |
| 1 |

6816 6\％6V6GTG ..... 81．20P36BQ7A $15{ }^{\prime} .6 \times 4$$\begin{array}{ll}68 R 7 & 15 \% \\ 6856 & 6 \times 5\end{array}$$6 B 57 \quad 25^{\prime}-6 / 30 \mathrm{~L} 2 \quad 10^{\prime} .25 \mathrm{~A} 6 \mathrm{C}$| $6 B W 6$ | $8 / 6$ | $7 A 7$ | $12 \prime 6$ | 25 L6GGT |
| :--- | :---: | :--- | :--- | :--- |
| $6 B W 7$ | $6 \prime$ | $7 B 6$ | $21 / 3$ | $25 Y 5 G$ |

| $6 B W 7$ | $6 \%$ | 7 A 6 | $12 \prime 6$ | 25 L 6 GT | $10 \%$ |
| :--- | ---: | :--- | :--- | :--- | :--- |
| 6 CW | $21 / 3$ | $25 Y 5 \mathrm{G}$ | $10 \%$ | DI |  |
| $68 \times 6$ | $6 \%$ | 7 B 7 | 816 | 2574 G | $9 \prime 6$ |

$\begin{array}{llll}6 C 4 & 5 \prime & 7 C 5 & 8 \prime \\ 6 C 5 G & 6 \prime 6 & 7 C 6 & 85 Z 5 \\ 6 \mathrm{C} & 8 \prime & 25 Z 6 G\end{array}$ 016 27SU 101－D77 ..... 
AC 32
$8 / 6$ EZ 41
$3 / 3$ EZ 90
23.
$6, ~ E Z 90$
$E Z 81$
61

7| $6 / 6$ | $F C 2 A$ |
| :--- | :--- |
| $7 / 6$ | FC $_{4}$ |816 EF39 516 HVRLA${ }^{816}$ EF3991．EF40 151．KF35 816 PL820 1817 U4020 1617 XFGI $181-$616 EF41 1010 KF35 816 PM2B 1218 UABC80 91．XFY12 916

5．KT33C $10 \%$ PX4

5．KT33C $10 \%$ PX4 \begin{tabular}{l|l|l|l|}
5：－ \& KT33C \& 101 \& PX <br>
KT36 \& 29110 \& PX 25


216 \& KT41 \& 29110 \& PX25 <br>
KT4 \& $12 \prime 6$ \& PY31
\end{tabular}

10
59 16 UBC 811
14 Y63

| 1.7 | 263 | 716 |
| ---: | ---: | ---: |
|  | 1716 |  | 1617 UBF89 $916 \quad$ Z66 ..... 41613111EF5412＇－EF73| 61 | $K T 41$ | $12 \prime 6$ | PY31 |
| :--- | :--- | :--- | :--- |
| 6 KT44 | 126 | PY 32 |  || 616 | EF85 |
| :--- | :--- | :--- |
| $9 /-$ | EF8 |
| $8 / 6$ | EF89 |916 FF991


| 016 | KT63 | $7 \prime$ | PY 31 |
| :--- | ---: | ---: | ---: |
| $91_{-}$ | KT66 | 151. | PY 92 |

46 KT88
816 UCFBO15＇－EF97
16 PZ30
16 PZ30
$13 / 3$
1313 KTW662
KTW63
$115^{14}$

$115^{14}$ | 1817 | KTW W 23 | 616 | QP25 |
| :--- | :--- | :--- | :--- |
| 1817 | QS150／15 |  |  |
| 1817 | $K T Z 3$ | 716 |  || $77^{\circ}$ | EFI83 |
| ---: | ---: |
| 716 | EF184 |

$$
\begin{array}{r|r|}
1877 & \text { KT } \\
816 \\
\text { L6 }
\end{array}
$$

716 EL 32
21．EL 34$91 \mathrm{EL} \mathrm{EL}^{2}$
416 EL 415．－MHR12
R13
${ }^{9 \prime}-\mathrm{EL} 42$
B／6 EL 83
2616
17

$\square$| 917 |
| :--- |
| 1 |

16 Transistors| $7 \prime$ | UCH31 | 916 |
| :--- | :--- | :--- |
| 416 | $U C L 32$ | 116 |
|  | $\cup C L 83$ | 1913 |

ござ$\begin{array}{ll}016 \\ 81 . & 27 \mathrm{SU} \\ 19111 & \text { UAC32 } 10 \% \\ 10 \% & \text { ECH42 } \\ \text { ECH81 }\end{array}$

8| 9.6 |
| :--- |
| 18 FCl 3 |10

16 CG
がッ が
216
91.
9

5 Cl 10 91．7R7$\begin{array}{rl}81.28 D 7 \\ 12.630 \mathrm{Cl} & 1 / \text { ．DAF91 } 6 \% \text { ECH81 } \\ \text { ECH33 }\end{array}$| 6CD6G | 91. |
| :--- | :--- |
| 3616 | $7 R 7$ |
| 57 |  |

| 606 | 616 | $7 Y 4$ | 716 | 30 L 1 |
| :--- | :--- | :--- | :--- | :--- |
| 602 | 316 | 3015 |  |  |

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METAL RECTIFIERS
「ull
513
716
719
144.
1918
$14 B 130$ 148261 $\begin{array}{ll}14 \mathrm{BI} 130 & 35 \prime \\ 14 \mathrm{~B} 261 & 116 \\ 14 R A & 1-2-8-2\end{array} 17 \prime 6$ （FCIOI）
$4 R A 1-2$
（FC31） （FC31）
 16RE 2－1－81 12！－ $\begin{array}{ll}18 R A & 1-1-8-1 \\ \text { I } & 4 / 6\end{array}$

BRA－1－1－16．1 816
18RA 1－2－8－1 $11 /$ I8RD 2－2－8－1 $15^{\prime}$.

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$\begin{array}{ll}16 \times 8 \times 6 \text { mid，} 450 \mathrm{v} . & 4 / 9 \\ 32 \times 32 \mathrm{mid} .450 \mathrm{v}\end{array}$ | $64 \times 120 \mathrm{mid} ., 350 \mathrm{v}$ | $5 / 3$ | $100 \times 400 \mathrm{mld} ., 275 \mathrm{v}$. | 1218 | $100 \times 200 \mathrm{mid} .275 \mathrm{v}$ | 916 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
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For UNLY £8.7.6 (1'lus 7/6 Carr. \& Ins.)
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YOL. XXXYI, No. 648, FEERUARY, 1961


## COMMERCIAL BROADCASTING

EVER since commercial radio transmissions were first directed at this country from stations on the Continent, there have been periodic comments in the press and elsewhere on the possibility of introducing sponsored radio broadcasting in the United Kingdom. In our editorial in the October issue, we mentioned an announcement by the Government of the setting up of an inquiry into the future of sound and television broadcasting in this country; this announcement has renewed speculation as to whether commercial radio will soon make its appearance. Those who favour its introduction seem, for the most part, to visualise the eventual establishment of one station for every 50,000 people, perhaps with the use of medium waves by day, and Band II by night. The stations.would derive their revenue from advertisements, in much the same way as commercial television.
Upon consideration, this clamour for commercial radio seems to be based on a desire for novelty alone. It appears to us that there is insufficient material and talent for the success of local broadcasting to be ensured. In other countries, even where there is no national network, small local stations have generally had to reduce their standards until programmes have eventually degenerated into an output of almost continuous music, with breaks only for advertisements and news summaries.
It may be argued that because the major commercial transmitter on the Continent with programmes directed at the British Isles is a highly successful concern, then similar sources of entertainment operating in this country would also be a success. This is not necessarily a valid argument: if the number of commercial stations is increased, the popularity of the broadcasts may well deteriorate.

The introduction of sponsored local broadcasts could have serious effects on other advertising media-the press for example. Many small firms would be forced to purchase time on the radio programmes and would have no spare funds to continue their advertising in the local evening newspaper.

We are of the opinion that commercial radio would not improve, but detract, from present programme standards. It is generally admitted that to attract and retain a large listening audience, programme quality must be degraded-commercial television is often cited as evidence of this. The BBC at present provides a balanced service which caters for most tastes-even for minorities. By the nature of its source of revenue, a sponsored network cannot transmit programmes which attract small audiences. Only if the revenue of the stations were derived from the small audience concerned could suitable programmes be transmitted and the method for deriving such an income might well cause difficulties.

If there is an increasing demand for some form of local transmission system, and such a system is ruled to be impracticable, the way out of the impasse would seem to be to increase the regional activities of the BBC. Naturally, some modification of the present regional divisions would be necessary, but some form of local broadcasting could be achieved without the attendant disadvantages and possible dangers of a sponsored system.
 Our next issue, dated March, will be publistied on February 7th

## Hound the Worlal of Wireless

## POTENTIAL AND CURRENT NEWS

## Broadcast Receiving Licences

THE following statement shows the approximate number of Broadcast Recciving Licences in force at the end of October. 1960. in respect of wireless receiving stations situated within the various Postal Regions of England. Wales. Scotland and Northern Ireland. The numbers include Licences issued to blind persons without payment.


## Manuals for Technical Colleges

A N issue of service manuals covering Philips" current radio and television range is to be made to all of the main technical colleges throughout Britain.

Until now. while manuals and other technical information have normally been supplied to technical colleges on request, there has been no " matter of course" issue.

Philips' offer was made direct to the Ministry of Education. and colleges receiving the manuals are being asked to treat the information being made available as confidential and to use it only for academic purposes.

## Conference on Microwave Measurement Techniques

THE Electronics and Communications section of the Institution of Electrical Engineers is organizing a conference to discuss recent advances in microwave measurement techniques to be held in the Institution building. Savoy Place. London W.C.2., from the 6th to the 8th September. 1961. The topics to be discussed will include: The measurement of microwave power, frequency. $Q$ factor. impedance, admittance, reflection coefficient and noise.


The 45 ft radio telescone which was used during investigations by the Roval Radar Establishment at Malvern into the roughness of the Moon's surface. Future investigations may possibly include Venus, Mars and Jupiter. An English Electric Valve Co. Ltd. M543 21 12 WW Magnetron is used in this equipment.

The organizing committee will welcome the submission of papers for consideration for inclusion in the proceedings of the conference. and invite intending authors to submit. as soon as possible. and preferably not later than 15th February. 1961. abstracts of not more than 250 words for preliminary consideration.

It is proposed to associate with the conference an exhibition of microwave measurement techniques.

## Traffic Radars

'I'HE portable electronic device which measures the speed of passing vehicles made by Marconi's has been ordered for the police forces of fifteen counties in Great Britain. The equipment is now being evaluated by police authorities abroad and Australia. Canada. South Africa and Singapore. are amongst the first countries to try this new apparatus.

In the past two years Marconi's have demonstrated the portable electronic traffic analyser to nolice authoritics and local government departments in Portugal, Italy, Irance, Austria,

Belgium, Holland and Switzerland.

The first company in Britain to develop a traffic radar device. Marconi's have received in the last twelve months orders for the apparatus totalling about $£ 14,500$.

## Appointment

THE BBC announces the appointment of Mr. J. D. MacEwan. B.Sc.. A.M.I.E.E.. A.M.Brit.I.R.E.. as Engineer-inCharge. Television. Birmingham. in succession to Mr H . G. Whiting. A.M.I.E.E.. who recently became Regional Engineer, Midland Region.

Mr. MacEwan joined the Operations and Maintenance Denartment of the BBC in 1947 and after service in Glasgow and Edinburgh he became a member in 1953 of the staff of the BBC's Television Outside Broadcast unit covering Scotland and northeast England. During the following year he was transferred to the television staff in Glasgow.

In 1956 Mr. MacEwan was appointed Senior Lecturer (Technical Onerations) at the Corporation"s Enginecring Training Department. Wood Norton. Worcestershire, which post he
has held until taking up his new duties in Birmingham on 14th November, 1960.

## New Zealand's First Broadband Microwave Telephone System

NEW ZEALAND'S capital, Wellington, and the country's largest city, Auckland, are now linked by a 262 -mile microwave multi-circuit telephone system supplied by Standard Telephones and Cables Limited, London.

The system may be used. with certain additions, to carry television programmes at a later date, using the existing buildings and equipment.

At present the link has one two-way radio channel capable of carrying 600 simultaneous telephone calls. There is also an identical "standby" radio channel to which the telephone traffic is switehed automatically in the event of severc fading or excessive noise on the "working" channel.

The radio terminals for the new $4.000 \mathrm{Mc} / \mathrm{s}$ radio link are at Hamilton and Palmerston North: these are linked by cables to Auckland and Wcllington respectively. There is also a spur connection between Urenui. on the main link, and New Plymouth, on the west coast.

Between Hamilton and Palmerston North eight repeater stations amplify the broadhand block of 600 telephone channels. The incidence of carthquake shocks and high winds called for special care in the construction of the masts at these stations. This lype of communication system uses a transmitter power of only 5 W , concentrated into a very narrow heam. Consequently, the alignment of the acrials must remain correct in all circumstances to maintain the quality of the link.

The automatic supervisory equipment for the microwave link uses a VHF radio system also supplied by STC. This supervisory channel enables faults at repeaters to be reported and identified at the terminal control stations: it also allows the control stations to interrogate each repeater for checking its operational condition.

## Sound Reinforcement System

I'HE contract for an installation at the Aldwych Theatre, London, and covering the provision of a comprehensive sound
reinforcement system, a dressing call system, programme monitoring system, bar interval signals and staff location has been given to RCA Great Britain Lid.

The object of the sound reinforcement system is to produce sound effects and some incidental music, and not to amplify actors' voices from the stage. The system provides for inputs from remotely controlled tape decks, onc disc player and three microphone channels. These six inputs are fed into a patch panel which incorporates input volume controls and switching to enable the six inputs to be pre-selected into four outgoing channcls in any combination.

The main/call programme system has some 30 points, and each is so arranged that the programme volume can be altered to zero, but no control over paging calls is possible. The programme is picked up by a single microphone on the circle front, and paging is done from the prompt cormer. and the circuit. heing normally "dead". is actuated by a push-button oll the microphone. Since programme monitoring is continuous. the action of paging automatically reduees the programme level to a pre-set point.

The bar interval signals also use the paging circuit, and by depressing an additional button the backstage paging is cul off and 10 front-of-house speakers
are introduced, conditions reverting to normal when the button is released. The staff location system also uses the paging circuit, and is done from the stage door, but the prompt corner microphone has, of course, overriding facilities.

## VHF Sound Broadcasting Station

'I'HE BBC has placed contracts with British Insulated Callender's Construction Co. Ltd. for the supply and erection of the $500 f \mathrm{ft}$ mast in carry the derials, and with F. R. Hipperson and Son Ltd.. for the construction of the huilding for the new Oxford television and VHF sound broadcasting station to be built near Beckley, some four miles north-east of the city.

This is one of several lownower stations which the BBC is building in extend and improve the coverage of its television and VHF sound servcies.

The Oxford station will improve television reception for ahout a quarter of a million peuple in the area including Bicester. Thame, Ahingdon and Witney. It will alan extend the VHF sound service to more than a quarter of a nullion people, including those in Swindon, and will give improved reception for a further quarter of a million people. It is expected that the station will he completed in ahout 15 months' time.


An operator actmating the controls of the reading console of the Solartron ER A (Electronic Frading A (utomaton), The tally roll on the right-hand side has been read by the machine.


Of course, the use of high gain, low noise valves must be accompanied by the use of the optimum aerials for the particular site: a signal must be present at the input of the receiver before it can be amplified. The best acrial for a particular location is not always the most complicated array: much depends on local conditions, particularly upon the incidence of reflections which give rise to in-phase and out-of-phase effects. Thus. in fringe areas, it is extremely important to test out various aerial arrays, or at least, move the available one around until a comparatively strong signal is found. The use of a low loss downlead is also a necessity which is seldom appreciated; the normal

## a BANI II Pre=Amp

7HE coverage of the BBC's F.M. may now "e said to range from "satisfactory" to "excellent" in most parts of the country. However, in certain areas. perhaps because of local conditions, reception is difficult or almost impossible using conventional techniques.

Initially, if signals are weak. it would seem only necessary to use a sufficient degree of amplification. However. upon further consideration. it is realised that the limit to amplification is set by the signal-to-noise ratio; "noise" in this context refers to any unwanted signals which are picked up with the radio signals and amplified with then. These noise signals may proceed through the ether or be caused by the random movement of electrons in the first valve of the receiver. The current flow from the cathode of this valve to the anode and any other electrodes is not steady hecause it is composed of negative charges (electrons) and the quantity of electrons is not constant. The effect is a change in anode current and this gives rise to spurious signals in the output. The noise voltages are only of appreciable magnitude in the first stage where they can become comparable with the signal voltages. It can therefore be seen that one of the limiting factors in the amplification is the choice of a low-noise valve for the first stage in the receiver.

## Cascode Circuit

The standard input circuit which is employed is the "cascode" and this consists of two triode valves in series. The first triode operates as a neutralised. grounded cathode amplifier and the second as a grounded grid amplificr. Triodes are used to reduce the number of active electrodes and thereby reduce noise and, as the sanie H.T. current flows through both of them. noise is still further reduced. In this pre-amplifier the cascode valve used is the PCC89, a comparatively recent introduction.

## A USEFUL ADDITION TO RECEIVERS FAR FROM THE TRANSMITTER

downlead can give rise to sufficient losses to reduce the signal reaching the set to negligible proportions. A low loss downlead, while more expensive. is essential.

## General Design

When designing this pre-amplifier various circuits and valve types were reviewed but as previously stated a cascode circuit was chosen with a frame grid valve for low noise and high gatin. One of the prohlems which arose in the design of this pre-amplifier is worthy of note: whilst it is possible to design a circuit and unit which will give some improvement in most locations it is virtually impossible to make a design to give optimum restilts with every receiver and aerial system. Naturally. the input circuit of the pre-amp tends to be the most critical as regards losses and care should be taken to avoid unnecessary losses.

## Circuit Analysis

The circuit employed is conventional. The input is designed for 75 ! coaxial cable but cables of other impedance or ballanced cables could, no doubt he employed with suitable alterations to the input circuit.

Coils L2 and I. 4 are the input and output tuned coils and L1 and L.3 are their associated aerial and output coupling coils respectively. Bias for the first triode is provided by $R 2$ in the cathode circuit and this triode is neutralised by the two capacitors C1 and C2. These two capacitors form two arms of a hridge circuit. the other two arms being the inter-electrode capacitances of V1. Capacitor C2 is made variable so that the bridge circuit can be balanced to give lowest noise. From the anode of $V 1$ the signal passes to the cathode of $V 2$ via
the inductance I. 5 which is adjusted for best results. As previously mentioned the grid of V2 is earthed but only so far as R.F. is concemed and this decoupling is achieved hy capacitor (6. Resistors R5 and R3 form a potential divider across the H.T. supply to the valve for biasing purposes. It must be emphasised here that the capacitor C6 must be wired with short leads, otherwise the combination of capacity and inductance may give a resonance resulting in ineffective decoupling.

## H.T. Voltage

The H.T. used is not critical and can have a voltage of about 140-180; for highest gain the voltage should be in the region of 180 . As might be expected, the decoupling capacitors used in the circuit and their wiring have a large bearing upon the results obtained. The associated leads must be made


Fig. 1.-Underchassis component layout.

as short as possible and it is best if the "earthy" leads of these capacitors are taken to a common point as indicated on the circuit diagram. This common point can be the metal spignt of the valveholder. The spigot is then wired to chassis by the shortest rolite, probably to a soldering tag underncath a!bolt used to secure the valveholder.

## Constructional Details

The construction of this preamplifier is not unduly critical but the layout given in the diagrams has been proved to give good results and should be used, lhe chassis is a box type about loin. $x$ 6in. $x 2$ in. hut these dimensions are not critical and will depend to some extent on the parts employed and on the chassis available.

## Coils

The coils are wound on small polystyrene formers with purple coded dust cores. No spacing is employed between turns and the ends of the winding are fixed to the formers with cellulose cement. The coupling windings are wound on a suitable former slightly larger in diameter than the tuned windings so that they

Fig. 2 (loft). - The simple circuit employed in this preamplifier.
may be slipped over them before the tuned windings are soldered into circuit.

When final adjustments are made, and the optimum positions of the coupling coils have been found, they may be cemented lightly in position. Coils L2 and L4 may be wound with 18-22s.w.g. bare copper or tinned copper wire. Alternatively, the wire used may be 22-26s.W.g. copper, enamelled or DCC.

Inductance L5 is wound with 22-26s.w.g. copper wire, enamelled or DCC, and on a $\frac{1}{3} \mathrm{in}$. diameter former. It is wired between piris 9 and 1 on the valveholder.
obtain a transformer with a suitable heater winding rating it should be remembered that many converter transformers rated at 6.3 V at 1 or 2 A give about 7 V when the total load is only 0.3 A -the winding resistance is comparatively high. The H.T. smoothing is by R6. C8 and C9. The value of R6 is not critical and may be adjusted when tests are made to give the optimum H.T. voltage. The values of C 8 and C 9 are also not critical but should be at least $8 \mu \mathrm{~F}$. As the H.T. consumption is low, a small metal rectifier can conveniently be used and a contact-cooled type is ideal. The rectifier should be rated at about 30 mA .


Fig. 3.-The drilling dimensions for the aluminium chassis (the details of the corner brackets are shown in the top left of the diagram).

## Power Supply

The H.T. circuits of the power supply employ half-wave rectification for convenience. The transformer used is of the type commonly sold for use in the construction of television converters. A tapped primary is not essential provided the correct rating is obtained for the local mains voltage. The H.T. secondary winding should be rated at about $150-200 \mathrm{~V}$ r.m.s. at 30 mA . The heater winding should give 7.2 V at 0.3 A if the valve heater is to be run correctly. However if it is difficult to

## Valve Connections

The input triode of the PCC89 has two cathode leads. Pin 7 should be wired, at the valveholder, to pin 8. This reduces the effect of the inductance of the cathode lead of the input triode and-results in improved performance. It should be noted that the triode connected to pins $9,6,8$ and 7 should be used for the input and the one connected to pins 3,2 and 1 for the output as the valve was designed for this arrangement.
(To be continued)
 C.W. TRANSMITTERS

$\overbrace{H}$By G3OGR HOUGH a variable frequency oscillator is often used to control the operating frequency of a transmitter, crystal control has the advantage of simplicity. The main disadvantage of crystal control lies in the fact that the transmitter is confined to one or more fixed frequencies. according to the type of circuit. and number of crystals. To some extent this limitation can be overcome by calling for contacts, instead of replying to calls from other transmiters. When answering a call from another station. it is usual to net the V.F.O. on that station's carrier. and reply on his frequency. With crystal control it is unlikely that a crystal will fall on the correct frequency. Therefore a call can be made, and an answering station can net on the crystal frequency. With this method of working, many satisfactory contact can readily be made.

## One-Valve Transmitter

A circuit suitable for a one-valve transmitter is shown in Fig. 1. This will operate successfully with almost any valve. For a fairly good output. a power valve such as a 6 V 6 . 6L6. 6F6. 6BW6 or any similar type will be satisfactory. A 6L6 may easily be run at up to 15 W input. which is a very useful level. If more output is required. a single 6146 can be run with an input of 50 W or more. With a given valve. the maximum input will depend largely on the power supply. It is, of course, necessary to avoid over-running the valve, but on the other hand good outputs can be obtained with an H.T. voltage much lower than the maximum for the value.

Such a transmitter is extremely easy to start working, and can be run from even a receiver type power pack, if necessary. It is thus excellent as a standby. or as a simple unit with which to begin working while a more elaborate transmitter is being constructed. It is unlikely that more than 50 W input will be required. even for long distance working, and the 6146 R.F. power valve mentioned can then be run from an H.T. line of about 400 V . with 10 k for R1. and 47 k for R2. With other valves. RI and R2 may be modified to obtain a suitable screen grid voltage. Or

Fig: 2 (right).-Crystal and output tank switching.
a 50 k or similar resistor, with a movable clip, can be used. The screen grid is then fed from the clip. which is adjusted to obtain a suitable voltage. When using a relatively low H.T. voltage the screen grid can be run directly from the H.T. line.

Fig. 1.-Crystal controlled one-valve transmitter.


For the $3.5 \mathrm{Mc} / \mathrm{s}$ band, the $\pi$-tank can have about 36 turns of 18 s.w.g. or similar wire. on a ribbed former about $1 \frac{1}{1} \mathrm{in}$. in diameter. For the $7 \mathrm{Mc} / \mathrm{s}$ band. 16 turns will suffice. For other than small power. the 200 pF condenser should be a transpitting type. The 1000 pF condenser does not need to have widely spaced plates, and may conveniently be obtained by wiring the two sections of a 500 pF
or similar 3-gang receiver tuning condenser in parallel.

For working on one band, a fixed coil can be used. For two or more bands, plug in coils may be provided, and changed while changing crystals. For working the various crystals in one band, the same tank coil is retained. The 200 pF condenser is adjusted to obtain a current dip on the meter. If this dip indicates less input than required. the 1000 pF condenser is adjusted to a lower value to increase loading, and the 200 pF setting modified as necessary to restore the current dip, which will then be higher.

## Crystal and Tank Switching

Though crystals can quite easily be changed in a holder. it is an added convenience to fit a switch, as shown in Fig. 2. Immediate operation upon any of the crystal frequencies is then possible, with only slight re-adjustment of the tank tuning condenser. A H.F. choke may also be included. as indicated, and can give a slight increase in efficiency.


Fig. 3.-A regenerative oscillator.
For two-band working, a tapped coil may be fitted. This can have 36 turns as described. tapped at-16-turns. The whole coil will then provide $3.5 \mathrm{Mc} / \mathrm{s}$ band working. with $7 \mathrm{Mc} / \mathrm{s}$ band working when the switch is closed to short out the unrequired turns.

If a 2-way switch is used. as in Fig. 2, this can bring a fixed condenser Cl into circuit. for $3 \cdot 5 \mathrm{Mc} / \mathrm{s}$ band working. This is an advantage when the aerial loading condenser ( 1000 pF in Fig. 1) is of insufficient capacity for the aerial. In these circumstances. Cl can be a high grade mica condenser of 100 pF to 500 pF , as required. The crystals may, of course. be for two bands, according to what is available.

## Regenerative Oscillator

The radio frequency output from the stage may be increased by providing some regeneration. One method of doing this is shown in Fig. 3. The 300 pF condenser may be modified in value. if necessary, to obtain a suitable effect. Actual results depend
to some extent on crystal activity. Fig. 3 also shows values for a 6L6. which may be run to 12 to 15 W input, if desired.

Another method of obtaining regeneration is to increase the 300 pF condenser to about 500 pF . and connect a 20 pF or similar trimmer from grid to cathode. Regeneration can then be adjusted by means of the trimmer.

A $\pi$-tank, as in Fig. 1, may be used in Fig. 3. With the tank in Fig. 3, loading is adjusted by modifying the loop coupling. To feed a single wire aerial, the loop can be taken to an aerial tuner. For band changing, 4-pin plug-in coils may be used. each with its own loop. Windings may be as described. with two turns for the $7 \mathrm{Mc} / \mathrm{s}$ loop. and 4 turns for the $3.5 \mathrm{Mc} / \mathrm{s}$ loop, tightly coupled to the H.T. end of the coils.

Regeneration is also useful when the stage will be used to drive a doubler. to give 2-band working from one crystal. With any of the one-valve transmitter circuits. doubling is possible. However, R.F. output will fall off, and an aerial tuner should be added to reduce possible radiation of the fundamental. Regeneration is also desirable, with an active crystal, and adequate H.T. voltage.

## A Push-pull Circuit

Similar valves may be employed in push-pull, to obtain increased output, and one circuit for this is shown in Fig. 4. This can give a powerful output. the actual maximum depending on the valves and H.T. voltage. The valves should be similar, but it is not necessary that 6L6's be used.

The screen grid supply may be obtained from a resistor with clip, as described, if preferred. For 250 V receiver type power supply, the resistors may be omitted, as mentioned.

When adjusting any of the circuits, a $200 / 250 \mathrm{~V}$ household lamp may be used as an R.F. indicator. for the smaller powers, a 25 W lamp is suitable. If a 6146 is employed, a 60 W lamp will be satisfactory. With $\pi$-tanks, connect the lamp from the output socket to chassis. With tank circuits like those in Figs 3 and 4, best loading will be obtained by connecting the lamp across some turns of the aerial tuner.

## An "Automatic" Two-Band Circuit

In Fig. 5. the oscillator drives two output valves. The grids of these are operated in push-pull, but the anodes are in parallel. This provides a good output at twice the crystal frequency. When working in this way no neutralisation is needed, because of the frequency multiplication, and the high band coil Ll is in use.

For operation on the crystal frequency. the anode circuit is switched to L2. At the same time one output valve heater is switched off. The remaining valve then operates as a straight through amplifier. while the inter-electrode capacity of the unused valve provides neutralisation, due to the centretapped grid coil.
This circuit is particularly useful for the $1.8 \mathrm{Mc} / \mathrm{s}$ and $3.5 \mathrm{Mc} / \mathrm{s}$ bands. Here, regulations limit the input to 10 W on the $1.8 \mathrm{Mc} / \mathrm{s}$ band, so that the H.T. voltage or aerial loading can be adjusted until this figure is approached. When doubling into the $3.5 \mathrm{Mc} / \mathrm{s}$ band the input will then be about 20 W . as both valves will be in use. This provides extra useful power, as the 10 W limit does not apply to this band.

For operation in this way, the oscillator coil can have about 70 turns of 24 s.w.g. or similar wire, on a $1 \frac{3}{4} \mathrm{in}$. or near diameter former. The coil is centre tapped. To maintain circuit balance, a split stator or butterfly type condenser is preferable for tuning this coil, but is not essential.

The screen grid resistors are selected as already explained. Three fL6 valves will be satisfactory, but other valves are equally suitable. The screen grid resistors may be omitted for moderate voltages.
then be ensured that the normal grid drive is present, before switching in the output stage. With this method of operation, there will be no need to provide a separate bias supply for the output stage. It is in order to obtain safety bias for the output stage by using a cathode resistor. With a $6146,2 \mathrm{~mA}$ to $2 \cdot 5 \mathrm{~mA}$ grid current with a 27 k grid resistor will be satisfactory. The output stage may otherwise be as shown for Fig. 1
(To be continued)


Fig. 5.-A circuit for two-band operation with one crystal.

## Multiplier Stages

A simple method of obtaining frequency multiplication by the use of an extra stage. The anode circuit of the first stage is tunable to the crystal frequency, and the second stage is tuned to twice this frequency. The output then drives the grid of the valve or valves forming the output stage.

Normal screen grid voltages are provided. Bias for the second stage is obtained by grid rectification, so the circuit should not be left switched on without the first tuned circuit correctly adjusted. If preferred. a cathode resistor may be added to provide safety bias for the doubler. For efficient doubling. fairly high bias is required. Even with cathode bias, additional bias will be developed across the 100 k grid resistor.

The output stage should have a grid current meter, so that grid current may be read before applying the anode and screen grid voltage. It should


Fig. 4.-A push-pull 20 W transmitter.

# CDMBINED RADID ANI TABLE LAMP 

USING A 40W LIGHT BULB INSTEAD OF A MAINS DROPPER<br>By M. J. Dunn

(Continued from page 805 of the January issue)


LTHOUGH general wiring details were given last month. it must be borne in mind that the final form of the set may be altered to suit individual requirements. Most of the connections between and around the valve sockets and tag-strips can be made by soldering the components straight in from point to point. All grid and anode leads in the R.F. and detector stages should be kept very short and the coils mounted so as to achieve this. A few points will be mentioned later on with regard to the possibility of encountering R.F. instability, but at this stage careful attention to the "hot" leads and stray capacities in the circuits associated with the two coils will pay dividends later. Nearly all the information required can be derived from the circuit diagram of Fig. 4, but Fig. 1 showed a suggested form of layout which is in fact that adopted with success in the author's model. Figs. 2 and 3 gave all the switch connections.
two sections of which ("A" and "B") act as a normal wave change switch for the coils in positions 2 (L.W.) and 3 (M.W.). In position 1, Section C short circuits the heater chain so that the lamp is connected directly across the mains and section D disconnects the mains from the rectifier, so that in this position the apparatus works solely as a source of illumination. R2 (470k) is included connected across the H.T. supply to act as a bleeder and it discharges the smoothing capacitors when the set is switched off, or switched to "lamp only" position. The mains are switched on and off by SW1 ganged to the volume control and it is a wise policy to leave SW2 in position 1 when the set is not in use so that the lamp takes the initial surge when switching on. However, no ill effects have been noticed from switching on and off with the heaters in circuit and in practice the surge is so instantaneous that the brunt is almost entirely borne by, the lamp which reaches incandescence so rapidly compared with the many seconds required for the heaters to warm up. The author strongly recommends the use of a three-pin mains plug-not necessarily for earthing the set, but to ensure that the polarity is such that the neutral lead goes to chassis. If the set is earthed through a three-pin plug, the inclusion of the two capacitors Cll and Cl2 is good for avoiding mains-borne


Fig. 4.-The circuit diagram.

## The Power-Pack

After passing through the double-pole on/ot switch, one limb of the mains goes direct to the chassis and the other to one of the lamp connections, the second of which returns to chassis via the valve heater chain. The "hot" mains lead also goes to the negative end of the H.T. rectifier via section "D" of SW2, the function of which can now be explained. This is a four-pole, three-way selector switch,
irterference and modulation hum; however, the earth often gives excellent results as an aerial, in which case the arrangement in Fig. 6 can be adopted and the earth lead can terminate in a standard wander-plug to be placed in the aerial socket. All the usual precautions should be taken, of course, to see that in the finished article no part of the chassis, or anything connected with it, can be touched by the operator.

## Final Setting-up, Aligning and Testing

After wiring up, the circuit should be thoroughly checked over and this is best done stage by stage Particular attention should be paid to the mains, heater and power supplies. It is a wise procedure first to switch on with the H.T disconnected and to check the voltages across the heaters, both individually and as a whole, unless this has been done as a separate operation during construction Using a high resistance voltmeter, V1 and V2 should read 12.6 V across each of their heaters and V3 should read $6.3 \mathrm{~V} \pm$ the 7 per cent allowed. If the heaters are found to be working within their tolerance limits the H.T. can be reconnected and the set lined up. To do this the standard procedure for lining up T.R.F. receivers is adopted. Insert the aerial and tune the dial to within a few degrees of the lower end to receive any readily available station. Adjust the trimmers for maximum reception. Then swing the tuning capacitors to the top end of the dial and on hearing a station, adjust the cores for maximum reception. Repeat this process at the lower and upper ends of the dial until a good compromise is oblained. Due to the excellent selectivity of this set, the trimmer of the first stage will probably require adjustment for different lengths of aerial so that initial setting should be done on the actual aerial to be used or one of similar characteristics. The above procedure applies, of


The completed receiver prior to fixing in its cabinet.


Fig. 5.-The underchassis component layout and wiring diagram.

## Instability

The cathode follower detector imposes no load on its associated tuned circuit (L4) with the result that with a good coil a very high $\mathbf{Q}$ is obtainable with excellent selectivity and gain. Because of this.


Fig 6.-This shows the mains connections for a 3-pin plug; in the lower diagram the earth pin is connected to the aerial socket.

|  | COMPONENTS LIST |
| :---: | :---: |
| R1 | $3 k, 5 W$ <br> all other resistors are $\frac{1}{2} \mathrm{~W}$. |
| R2 | 47k |
| R3 | $100 \Omega$, see text |
| R4 | 15k |
| R5 | 47k |
| R6 | 10k |
| R7 | 27k $\}^{\text {see text }}$ |
| R8 | 3.3k |
| R9 | 270k |
| R10 | 2.2M |
| R11 | $560 \Omega \text { (6G6). }$ $390 \Omega(12 \mathrm{~A} 6) .$ |
|  | 1 k (12J5). |
| RV | 0.5M with D.P. switch. |
| C1 | $100 \mathrm{pF}(500 \mathrm{~V})$. |
| C2, 3, 4 | $0 \cdot 1 \mu \mathrm{~F}$. |
| C5 | 100pF. |
| C6, 7 | $8 \mu \mathrm{~F}$, see text. |
| C8, 9 | $0.01 \mu \mathrm{~F}$. |
| C10 a-b | 32-32 $\mu \mathrm{F}$. |
| C11,12 | $0 \cdot 1 \mu \mathrm{~F}$ ( 500 V ). |
| Twin-gang | g tuning capacitors: 500 pF . with trimmers: 30 pF . |
| Slow mo | tion drive, pointer and dial. |
| V1 | 12SK7 (or 12K7, 12SJ7, 12.J7). |
| $\checkmark 2$ | 12 SL 7. |
| V3 | 6G6 (or 12A6, 12J5). |
| 3 Interna | tional Octal valve sockets. |
| Pair of | matched T.R.F. dual range coils (Repanco). |
| Miniature | O.P. Transformer. Loudspeaker. |
| Metal Re | ectifier: $\mathbf{2 5 0 V}, \mathbf{5 0 m A}$. |
| SW2 | 4-pole, 3 -way rotary switch. |
| Electric li | light bulb-40W, 240 V rating (see text). |
|  | (Holder, lampshade and support). |

however, the circuit is rather prone to R.F. instability and this will arise if the anode to grid capacity of V is above a certain safety margin. There is, of course, an inherent capacity between these two electrodes in the valve itself, but apart from this extra will arise from the external wiring and possible coupling between the grid and anode coils. Although the latter are separated by being above and below chassis, one critical item is the leads from the coils to the wavechange switch, which although at chassis potential on M.W. are part of the tuned circuit on L.W. and unavoidably near each other. They should, therefore. be kept as far apart as possible throughout their course, and should be kept short and non-parallel. If the set howls on L.W. but not on M.W. this wiring should be suspect. Oscillation may occur over certain parts of the tuning range if the set is not properly lined up, so this matter should be attended to before condemning and making radical alterations to the wiring. If intractable oscillation is found to be present, apply the minimum necessary of "negative reaction". The specified pair of coils has an otherwise unused reaction winding on L3--4. One end should be connected to chassis and the other to the grid of V1 via the smallest possible capacity, making sure that the feedback is out-of-phase. Over-doing this will impair the high Q otherwise obtainable in the circuit and the procedure should be avoided if possible.

## Transistorised, Stabilised D.C. Supply

THE type PP. 2 is a heavy duty power supply designed for the engineer developing transistorised equipment, and provides a stabilised D.C. voltage over the range $0-50 \mathrm{~V}$ at currents up to a maximum of 10 A . The output voltage and current are monitored and the instrument is fully protected against overload conditions by an electronic circuit similar to that used on previous models. Four terminal output connections are provided to enable the connecting lead resistance to be effectively eliminated. The instrument is designed for bench use. or, alternatively, can be placed on a special trolley to enable the model to be conveyed around a laboratory more easily. This unit was designed by Advance Components Lid., Roebuck Road, Hainault, llford, Essex.

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[^1]
# CEIRAMIC SPEAKETL CAHINETS 

IN sound reproduction, the mounting of the speaker is of the utmost importance. Of the various methods that have been tried, none has the compactness and simplicity of a tuned reflex cabinet.

## A reflex Cabinet

A reflex cabinet consists of an enclosure of between $1-27 \mathrm{cu} . \mathrm{ft}$. the larger the better. There is a small vent hole in the cabinet that makes it resonate at a low note. The smaller the hole the lower the note. A speaker is mounted in one wall or on the top of the cabinet. facing outwards. While the speaker projects the higher notes into the room, the cabinet builds up the bass notes which come out of the vent hole. The principles involved are that as the note from the speaker descends towards the resonant note of the cabinet the cabinet resonates louder, but at the same time the enclosed air reacts against the cone of the speaker. damping down the cone movement. These two factors give an even bass response.


Fig. 1.-Plan and sectional views of the enclosure.
Making these cabinets out of wood and packing them with sand is a skilled job, for not only must they be solid and heavy. but no part of them must vibrate. Any vibration of a speaker cabinet

## INEXPENSIVE, HIGH QUALITY ENCLOSUKES

By F. B. Burge

destroys the purity of the tone and absorbs the energy of the speaker.

Expensive reflex cabinets 1 ft square and 3 ft high, fitted with full range 8 in . speakers are becoming very popular as they are neat and well fitted to stereophonic reproduction.
The ideal cabinet would be one made of concrete, but these, of course, are not produced.


Fig. 2.-Plan views of the loudspeaker board, the acoustic resistor board and the base of the enclosure.

Fortunately the same effect can be obtained by using standard cheap objects made for other purposes.

## Suitable Materials

Concrete sewer pipes. flue linings, chimney pots and drain pipes may be used and are cheap and can be made very presentable when painted. Speakers mounted in these give astonishing results even from ordinary wireless sets, tape recorders and record players. Chimney-pots tend to give slightly better results than the others as their tapered shape improves the tone.

The choice of design of the cabinet is entirely the constructor's as large ornamental chimney-pots give as good results as plain sewer pipes, etc. The recommended dimensions of the cabinet are 3 ft (tall) $x 12 \mathrm{in}$. (diameter). For this size a speaker of not more than 8 in . is suitable.

## An Acoustic Resistance

An acoustic resistance must now be fitted onethird of the way up the pipe. The resistor consists of a piece of $\frac{1}{2} \mathrm{in}$. plywood cut to fit into the pipe. This board has parallel saw cuts in it, $1 \frac{1}{2} \mathrm{in}$. apart starting and finishing 2 in . from the edge so that
(Cominued on page 886)

## 80-Melre Merial Coupler

A COMPREHENSIVE MATCHING CIRCUIT<br>By G3OGR

ALTHOUGH coil details for the aerial coupler described here are for the $3.5 \mathrm{Mc} / \mathrm{s}$ to $3.8 \mathrm{Mc} / \mathrm{s}$ band, the coupler can be used on other bands merely by changing the number of turns on the coil. The coupler is intended as a matching device between transmitter and aerial, or ats a coupler allowing a dipole to be fed from a $\%$ output network. It also provides a means of feeding a single wire aerial from a coupling link, and allows loading up of the transmitter with endi-fed aerials which would not load sufficiently with a $\pi$ output.

## Former Winding

The circuit is shown in Fig. 1. For the 80 m band a standard ribbed former approximately $2 \frac{1}{2} \mathrm{in}$. in diameter and 5 im . long will be satisfactory. The winding can consist of
 26 turns of 18 or 20s.w.g. wire. occupying about $3 \frac{1}{2}$ in. winding length. With formers of other diameters, it is only necessary to change the number of turns until resonance can be ohtained.

Fig. 1 (lefn). - The circuit for the conpler.

For coupling, three turns of adequately insulated wire. placed centrally round the coil as shown in Fig. 2. will usually he sufficient. This loop may be noodified as described later. if necessary.

A radio-frequency type meter is included as shown in Fig. I. so that aerial current may he read. This is a useful addition. as it inmediately shows if the transmitter is providing its accustomed output. It also indicates how aerial current is modified by tuning. coupling adjustment. etc. Provided the aerial itself is not changed. the meter will give an increased reading, as the transmitter and coupling are adjusted for optimum performance.

For most moderately powered transmitters. an $0-350 \mathrm{~mA}$ or $0-500 \mathrm{~mA}$ R.F. meter will be satisfactory, when the aerial is end-fed. For powers in excess of 40 W or so, a meter with a higher full

scale reading can be employed, or the meter may be shonted with a piece of connecting wire.

When feeding a dipole, the meter is in one feeder only. As feeder currents will roughly balance, two meters are not essential. Since a dipole will normally be fed at a low impedance point. the current will be larger. However. the meter can easily he shunted, as mentioned, if necessary.


Fig. 2.-The wiring diagram of the unit.

## Coupler Construction

Fت̈g. 2 shous a suitable layout. An insulated baseboard ahour yin. x Gin. With a panel about gin. $x$ Sin. will be convenient. Sirips Yin. long rase the base. to give elearance for the terminals.

The meter may be a flush or projecting type. either being equally satisfactory. The tuning condencer may be about 100pF to 200 pF . For low powers. a receiver type condenser will do. But for larger power. wider spacing will be necesary. New and suplas eondensers are available from many suppliers.

If the coil is wound as directed. leads from it may be permanently connected to the condenser. But if the coil in of different size a theck thould first be made that resonance can be obtained throughout the band.

A short, insulated spindle is best used with the control knob,


Fis. 3. This shous the methed of coupling to a $\quad$ output. as the condenser spindle will be alive with R.F. when a centre tap is employed on the coil winding.

## Feeding from $\pi$ Output

A co-axial socket is watally provided with -- ontpult circuits, and a thort piece of en-axial cable is then convenient hetween the tramimitter and tunes.


## Link Coupling

When link coupling is used, a loop is connected as shown in Fig. 4. This loop should be similar to

that in the tuner. That is, it can have the same number of turns, if of similar diameter. If smaller in diameter, an additional turn or so can be added. With a singleended P.A. tank, the loop is situated as near as possible to the H.T. end of the coil. With pushpull output, the loop should be placed at the centre of the coil.
The feeder can be of twin flex. or any suitable twin lead tape. One side of the loon circuit is earthed, as this reduces

Fig. 5 (left)-The connections for end-fed and dipole aerials.
harmonic radiation, in addition to the normal barmonic suppression furnished by the aerial tuner.
With link coupling, tune the aerial circuit to resonance, and adjust the loop until the P.A. draws its normal loaded anode current. Moving the aerial tapping on the tuner coil will also modify loading,
so a suitable degree of coupling can be found without much difficulty.

## End-fed and Dipole Aerials

When using an end-fed aerial better results are normally achieved if the centre of the coil is earthed, as in Fig. 5. With a co-axial input. this circuit may be completed through the sheath to the transmitter (Fig. 3.)
End-fed aerials will usually present an impedance of several hundred or thousand ohms, when approaching a half-wave in length. For this method of operation, the acrial curfent will not be very large for a given wattage. Reasonable results are obtainable with no carth. in these circumstances, and this is sometimes a convenient system.

When the end-fed aerial is near a quarter wave, it will be current-fed, as its impedance is lower. For a given wattage. the aerial current will then he very much larger. A really good earth is desirable, for maximum efficiency in these circumstances.

The usual dipole will be current-fed at the centre for the band for which it is cut when used with an untuned feeder. The feeder may be any twin conductor. Good results are obtainable without an earth, in these circumstances.

With a harmonically operated aerial, or aerial with a tuned feeder. current and voltage will be present at the tuner, in varying proportions, according to the acrial and feeder length.

In all cases. any of these aerials may be matehed by tuning to resonance, then adjusting $\pi$ or link coupling until the P.A. draws its maximum anode current on resonance.
If it should be found that the transmitter cannot be loaded with the tuner loop described. more turns should be added to the loop. When first adjusting the tuner, the aerial feed points should be modified a turn at a time. When suitable positions are found. connections should be soldered. After adjusting the tuner at the centre of the band (e.g. $3650 \mathrm{kc} / \mathrm{s}$. for the 80 m band) no other modifications will be necessary.

## CERAMIC SIPEAEEER CMBINETS

(Continued from page 883)
the board is not made too weak. This limits the amount of air that can move in the pipe. When fixing the hoard it is easier to manage if a serew is inserted as a handle. 11 can then be wedged into position with another serew placed between the board and the pipe. The edges then can be made air-tight with plaster of Paris or similar compound.

The speaker (which must match the amplifiers) should have its face protected from dust by a covering of thin material, and then be bolted firmly on to a board. This board ( $\frac{1}{2}$ in. plywood) should have been shaped to fit on to the top of the pipe and can be firmly fixed with more plaster of Paris, etc. The speaker is now in the pipe facing upwards.
A base is now made for the pipe to stand on with a slit about 4 in . $x 1 \frac{1}{1} \mathrm{in}$. (for a 3 ft by 12 in . pipe) left open for the vent. If the bars that hold the base together fit the pipe exactly they will
keep it centrally positioned on its base. A larger cabinet would have a proportionately larger vent hole.
(A reffector may be placed above the speaker to throw the higher notes into the room and gives improved results.)

When all is assembled it can be finished as the reader chooses.
Large ornamental chimney-pots look the best. 3 ft tall. 12 in . flue linings are the neatest. But sewer pipes and drain pipes can be made to look quite neat. 1 recommend a 12 in . pipe with a speaker not larger than 8in. Chimney-pots have the additional advantage of being tapered, which seems to improve their tone. The general rule is the bigger the better. A 9in. pipe seems to be the minimum size for good results. Large spcakers find difficulty in moving fast enough for the high notes.

## A STEIRED ANPLIFEER

7
8W WITH SINGLE-ENDED OUTPUT CIRCUITS O put this amplifier into use it is necessary
only to operate an H.T. switch and there is no delay awaiting the heaters. This switching could be dispensed with, depending on how the constructor wished to use the unit. Some kind of feeder unit will be required and this also could be quite simple. but this will generally carry all the operable controls. being litted near the turntable. If the assembly is to be built into a cabinet for domestic use the main
indicate that H.T. is switched on. These work with the switches, of course, but they could be provided even in the absence of the switches. The H.T. indicator. in fact. also acts as an H.T. fuse as will be seen when the circuit is reviewed.

## Circuit

The circuit is shown in Fig. 1 and no doubt the exceptional simplicity will be noted. This is because ol the absence of the usual cathode bypass capacitor.


Fig. 1.-The circuit of the amplifier.
amplitier is then likely to be tucked away in an inaccessible position and there is no point in butting any controls on it. On the other hand if the amplifier is to be used on the bench the switches are an adoantage. Tiwo dial lights are provided also, one to indicate that the mains are switched on and the other to

There is a very good case for avoiling reactive components wherever posible because inevitably the introduce a frequency discriminating element. and hence distortion, into the design. If they are made big enough their effect is not noticeable, hut this necessitates electrolytic capacitors and these lose
their capacitance with age so that distortion not present when new, might later find its way into the equipment. On the other hand omission of the cathode bypass capacitor causes negative feedback because any signal appearing across the cathode resistor is effectively in the input circuit. All depends on whether the effective gain reduction can be tolerated. In this design it was found that the loss could be accepted and so the capacitors were avoided. Certainly this was an advantage from the point of view of cost, because good electrolytics are not cheap, but there is another advantage arising from the omission of the capacitors. Constructors will know that there is some difficulty in finding room for all the components which normally have to be fitted close to the valve holder, and the comparatively bulky electrolytics are often the most difficult to fit, separate tagboards can be used, but these have the effect of lengthening the connections and in some positions this is undesirable. By eliminating the bypass capacitors such steps are unnecessary and construction is thereby simplified.

It is not a difficult matter to assess the order of loss of gain as a result of this simplification. Each half of the 12AU7 gives a gain of 12 times. This applies over a wide range of working conditions; a triode does not have the wide variation of gain with working conditions that is shown by an audio pentode such as the 6BR7. This gain takes place as between the input measured between grid and cathode and output in the load resistor which is measured between anode and cathode. In order to clarify the situation the appropriate part of Fig. 1 is modified in Fig. 2, the component numbers being those from Fig. 1. for the first half of $V 1$, with the numbers of the
equivalent components for the second half of V1 in brackets. The signal voltage in (Vin) produces an output signal current, i.e. it causes variations in the anode curremt of the valve. This anode current flows internally from cathode to anode and externally via $\mathrm{R} 3, \mathrm{C} 1$ and R 2 back to the cathode. Cl is chosen to have a negligible reactance to audio frequencies and so can be looked upon as a short circuit to audio
 signals: effectively therefore the anode signal currents can be considered as flowing through R3 and R2 in series. By Ohm's Law the signal voltage produced by that current will be generated across these two resistors in proportion to the size of those resistors. In the present case the anode load is 100 k and the cathode resistor is 3 k . Thus 3 per cent of

Fig. 2 (left)--The
feedback circuit.
the output signal is Iost in the cathode resistor and this is insignificant. The gain of the stage being 12 times, however, the cathode signal voltage will be $3 \times 12$, i.e. 36 per cent, or roughly a third of the input signal ( $V$ in) and this opposes the signal from the previous stage (Va).
(Continued on page 902)


Fig. 3.-The drilling details for the chassis.

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验ALL, 2270-0.220, $50 \mathrm{~mA}, 6.3$ ₹. 8.5 a. $17 / 6$
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 0.3 amp, 1000 ohme, $4 / \mathrm{a}$. 0.2 amp . 1000 ohms, $4 / 8$.
 Live Cord. 0.3 amp, 20 obran par 1 , 0.2 anp., LOMD per fig 2 -way, P. Bia. Plospey, 19/6. 6in. x 4in. Rola, 18/.. 6inin. Rola: 18/8, 8 I 6 in., $21 /-.10 \times 6 \mathrm{in} ., 27 / 6.10 \mathrm{in}$. Rols, $80 /-$.
 stemrtominithiole 10 in . 3 to 15 ohm 10 w., $85 /$. 13iz. Raker 15 wati 3 ohms or 15 ohms. $90 \%$. 12in. BAKER POAM SUBPENEIOH. 15 ohms, 26 . GRTGTAL DIODE, G.EC. $2 / 6$ GEX34, $1 / \%$ GIGH RESIBTANGEG PRONES. 4,000 ohme, is/- Pr. MEE TRALFF; $50.1,3 / 9 \mathrm{ea}$. ; 100:1, Potted, $10 / 6$ ©WTTOH CLEANER Huid squirt ppaut. $4 / 8$ tin. TWIA GANG TUNING CONDENGERE S6S PF. miaiature lin. I 1 tin. I $18 \mathrm{in} ., 10 /-0.00058$ tandard mith trimmers, $9 /$; iess triminers, $8 /-;$ midiget, 7/4, gingle $50 \mathrm{pF}, 2 / 8 ; 80 \mathrm{pP}$, 100 PF ,
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| $3 V 4$ | $7 / 6$ | 68J7 | 6/6 | EvC84 | 9/8 | ${ }^{\text {PCC84 }}$ | $9 / 6$ |
| 8 St | $7 / 9$ | 6SN7 | 6/6 | LCF80 | 9/8 | PCFEO | $9 / 6$ |
| BY3 | 76 | BV6G | 6/6 | ECH42 | 10/8 | PULS 2 | $11 / 8$ |
| 62.4 | $9 / 8$ | 6X4 | $7 / 6$ | HClsiz | $10 / 6$ | PENHE | 6/6 |
| 6AM6 | 5 S- | 6X5 | $8 / 6$ | EN39 | 5/6 | PLiz2 | 1018 |
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| 6 6rba | $7 / 8$ | $1 * 47$ | 6/6 | E1as2 | $5 /-$ | UCH42 | 9/6 |
| $6{ }^{6} 6$ | $8 / 6$ | $3 \$ 1.0$ | $9 / 8$ | ELI 1 | $9 / 6$ | UF31 | $9 / 6$ |
| 6.3 |  | 1324 | 71 | EL84 | $8 / 8$ | UL41 | $9 / 6$ |
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| 3Q5 | 91. | 6G: | 51. | 12AT7 | 61. | EBC41 |
| 354 | 716 | 6Hs | 316 | $12 A \cup 7$ | 61. | EBF80 |
| 3V4 | 716 | 615 | $5 / 6$ | $12 \mathrm{~A} \times 7$ | 61. | ECC84 |
| $5 \cup 4$ | $6 \%$ | 616 | 516 | 12K7GT | 816 | ECH42 |
| $5 Y 3 \mathrm{G}$ | 61. | 617G | $6 / 6$ | 12Q7GT | 616 | FCL80 |
| 5Z4G | 916 | 6K6GT | $5 \%$. | 25 YG5 | 816 | ECL8 ${ }^{2}$ |
| $6 \mathrm{AC7}$ | 316 | $6 K 7 \mathrm{G}$ | 51. | 35L6 | 516 | F-39 |
| 6AG5 | 5/. | $6 K 7 M$ | 116 | 3524 | 516 | CF41 |
| 6AL5 | 4. | 6K8G | if. | 80. | 51. | FFSC |
| 6AM | 41. | 6N7M | 51. | 954 | 116 | 二F91 |
| 6AT6 | 116 | 6Q7G | 716 | 956 | $\because 16$ | =F9, |
| 6B8G | 51. | 6SA7M | 51. | DAF9, | ' | E:32 |


| Matched Pairs 1/= extra |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 81. | EL41 | $9 \prime$. | PCL8 | 81. |
| 81. | EL84 | 316 | PY80 | 716 |
| 8! | EM8! | 916 | PY8I | $3 / 6$ |
| 81. | EYS! | 116 | PY82 | 1. |
| 41. | EYBt | 71. | PY8: | $7{ }^{\prime}$ |
| 81. | EZ40 | $7{ }^{\prime \prime}$ | QP2. | 7 - |
| $10^{\prime}$ | 5Z80 | 71. | R: | 16 |
| $3{ }^{1}$ | E1148 | 1. | SP61 | $3 / 6$ |
| 19. | HABC80 |  | UF41 | 316 |
| $10 \%$ |  | 12'. | UL41 | $: 16$ |
| $10 \%$ | HVR2A | $6 \%$. | UY41 | $7 \prime$. |
| 516 | KI33C | 10. | U22 | 31. |
| 7. | MU | 76 | VP2 ${ }^{\text {2 }}$ | 516 |
| 14. | -61 | $1 / 6$ | U7. | 216 |
| '. | ${ }^{3} \mathrm{CC8:}$ | 1. | VRIO5 30 |  |
| ', | PCF8 | 716 |  | 91. |



## 25 FOAMCOURT WAY, FERRING, WORTHING, SUSSEX



I was recently loaned a pocket set of doubtful make and asked what 1 thought of it. I had not previously trouhled about this type of apparatus, but was agrecably surprised by the quality and tone of reproduction in London. I had to make a journey and thought it would be a good idea to take the set with me. I am glad I did so. as I found that the performance of the set varied considerably from area
S.W. Receivers

IRECENTLY wrote about short-wave reception and in the course of my notes I mentioned that many years ago a set which I was using had proved better than a commercial (American) S.W. set, and that details of this set had been published in these pages. I have received dozens of letters since those notes appeared, asking if a copy of the issue or issues describing the set could be obtained, and in many of these letters readers suggested, if the information was no longer obtainable, that I might be in a position to recommend a modern set which would be ideal for short-wave listening. The details of the set in question are completcly out of print (it was in a pre-war issue), and in any case it could not now be built as it incorporated certain components and parts which are no longer on the market. The circuit incorporated the superhet principle, with an " $S$ " meter, and the main novelty was in the tuning circuits, where band-spreading was employed, but the band-setter consisted of the ganged main tuning condensers, and the small band-spreaders were ganged and taken to the main slow-motion tuning control fitted with a 300deg tuning dial which formed the main control. Therefore, if you are seeking a new set, look for some similar type of tuning system if this arrangement interests you and above all try and select one with an "S" meter. Although this means little from a point of view of reporting signal strengths (there is no basic measurement, remember, and it is purely an arbitrary reference) it does give the user of the receiver a direct reading which may be used for comparisons.

## The "Best" Set

As for my recommending a set, this is a little difficult as personal preferences play such a large part in the choice of a set, not only from the point of view of operation, but also from the appearance. Some amateurs like to see a set full of dials and controls, even if half of them are more ornamental than useful, whilst others prefer an open breadboard type of construction which gives resultsnever mind the looks. 1 have tried many exgovernment pieces of apparatus, but remember that these have in the main been designed to do a specific iob, and as such price has not been spared. But whether they will fulfil a general purpose situation such as is needed in the amateur's den is another matter. The receiver which 1 kept longest in my active transmitting days was an AR88, and I had no fault to find with it. It had an "S" meter and stood up well to the work it had to do at an active amateur station, but I know it does not suit everybody.
to area. In fact at one place I could hear nothing at all on it, and it must be remembered that the small aerial which is fitted is very dependent upon signal strength in the area. 1 am sure that much of the disappointment which is expressed by readers in this type of apparatus is due to its use in unsuitable areas, or perhaps by the use of an unsuitable set in a bad area. If you happen to be one of those who perhaps have been disappointed, try a better type of set. Perhaps you tried a two transistor loudspeaker set and did not get much joy out of it, whereas a four transistor set might completely change your mind on this type of receiver.

## Annoyance

Whilst on the subject of these little sets I would like to mention that a note appeared in a local paper recently deploring the introduction of them, as they annoy other people. The writer said he had visited a beach on the south coast and could not enjoy his stay as several portables were "blaring out" in the neighbourhood. After all, many people do go out into the country or to the seaside to get away from the noises of civilisation, and it can be very annoying to hear the radio following you-especially as in many cases the users of these sets seem to prefer modern jazz. I venture to think that if these little sets do become very popular and this type of outdoor use grows, the Noise Abatement Society will try and do something about it. 1 believe that in the London parks the L.C.C. have a by-law preventing the use of radios at a volume which can cause annoyance to members of the public.

## Radio Speeds X-ray Servicing

All X-ray service engineers of Philips Electrical Lid. working in the Home Counties now have their cars fitted with two-way radio. And after only two months working the scheme has already shown reductions in engineers' time and costs and an all-round increase of efficiency.

The control room is at the company's X-ray service H.Q., Balham. Signals are put out on $70 \mathrm{Mc} / \mathrm{s}$, the transmitting mast being situated at nearby Crystal Palace.
The longest distance over which a conversation has so far been held was between London and Winchester.
Engineers on the system call Balham whenever they have completed a job. They can then be sent to other calls which have since come in, or they can be recalled to base.

# Amplified D.C. Transistor Receiver 

THIS RECEIVER MAY BE USED WITH EITHER AN AMPLIFIER OR AN EARPIECE

/ By E. J. Wotton
AVING spent considerable time trying to produce a small radio receiver which could compete with the commercial sets now on the market, the following effort justifies the time and small outlay entailed. The complete arrangement consists of:-1 A receiver. 2 An earpiece. 3 An amplifier. The approximate cost is £6 10s. Od., although most amateurs will find many of the components in their spares box. The receiver can be used with the deaf-aid earpiece as a pocket personal receiver using a small ferrite rod aerial. If on the other hand one wishes to share the radio with others, the earpiece is simply unplugged, complete with flex, and the amplifier plugged in and switched on. The mere act of removing the small homemade plug from the receiver switches it off. The amp:ifier can also be used as an intercom. using the earpiece as a microphone, and also as a gram amplifier. When used this way it would be necessary for a volume control to be introduced.

## Receiver

It will be noticed that the circuit is the now well-


The completed receiver and its amplifier.
a Sellotape covering tapped at 23 turns. Transistor holders are used throughout. A U12 battery is also accommodated in the case, and, as only 2 mA are consumed, it will be found to last many weeks.


The receiver circuit (the tapped coil is wound on a ferrite rod and constitutes the aerial).
known 4-transistor type. first published in the May issue of Practical Wireless. The only modification which seemed necessary was the aerial winding. this being some 2 in . of $\frac{3}{8}$ in. ferrite rod with 47 turns of $33 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. enamelled copper wire wound on

## Method of Assembly

The first procedure is to cut a stiff piece of cardboard about $2 \frac{1}{8} \mathrm{in}$. x 3 din . Then cover the ferrite rod with one or two layers of Sellotape and, starting about $\frac{1}{2}$ in. from one end, wind on 23 turns of approx. 33s.w.g. enamelled copper wire and twist a 3 in . long loop, then continue with another 24 turns leaving a 3 in . end. Cover with a layer of Sellotape. Clean and tin the ends and tap ready to solder in position. Carefully lay out the components on the cardboard making sure that there is enough room for the socket contacts (see Fig. 1). and battery. Mark the position of the transistor holders, battery, and sockets and pierce the cardboard each side of the transistor holders and secure them with thread. Make battery contacts from springy brass (see Fig. 2), and $c:$ p into the cardcoard allowing the battery to be a spring fit. The compression condensers can be temporarily secured by their nuts. The socket
contacts are also made with springy brass and secured at a later stage. Proceed with the wiring.

## Socket Contacts

The centre contact also acts as the switch, so be careful that the two pieces of brass do not come into contact with each other. This method of fixing the contacts to the card chassis is very satisfactory, it was found better if the brass was laid flat on to the card and ears marked before bending


Fig. 1.-General layout of receiver.


Fig. 2.-Receiver battery clips.


Fig. 3a.-Details of the construction of the socket contacts.
at right angles. The small slots were formed by using a small screwdriver. The indents in the one side of the plugs were cut out with a $\ddagger$ in. chisel, being careful not to cut right through the plastic.


Solder end of flex into folded clip


Fig. 3b.-Method of mounting the brass clips on the plastic.

It can be seen that it is not important to prevent the two halves of $\mathbf{X}$ and $\mathbf{Z}$ from touching. A small strip of plastic was bolted over the set of three contacts (Fig. 3). At this stage it is best to mount the whole assembly on the top of the case. Cut a piece of plastic, size $3 \frac{1}{2} \mathrm{in} . \times 2 \frac{2}{8} \mathrm{in}$.

Carefully mark the position of the compression condensers making sure the chassis is $\frac{1}{2} \mathrm{in}$. smaller


Fig. 4.-Removing the back nuts.
on all sides. drill two $\ddagger$ in. holes for this. remove back nuts and bolt the chassis to the top with them (see Fig. 4). Now the plastic strip can be bolted right through the chassis and the top with two 8B.A. countersunk bolts (Fig. 3).

## The Cabinet

The tuning knobs are quite easy to make and fix. Cut two pieces of 6B.A. threaded brass rod lin. long and solder a nut on one end. Remove the adjusting screw supplied with the condensers and screw in the prepared spindles which should stand out about fin. when screwed in tight. Obtain two plastic container covers about 1 in . in diameter.


Fig. 5 (above right).-The layout for the amplifier.
 amplifier.


Fig. 7.-The amplifier circuit.

Mark two circles on stiff cardboard to fit tightly into the knobs and drill a hole in the centre to pass over the 6B.A. spindle. Secure in position with a nut and washer each side. Press the knobs over and secure with some adhesive. Turn the knobs clockwise until the trimmers are fully open, and leave to set (see Fig. 4). The case is then made by cutting the four sides from plastic or any material preferred by the reader. Three notches are cut in one side to correspond with the sockets, and four sides are glued to the top. When quite dry, a cover is cut to fit securely with four pieces of Sellotape, and carefully the corners are filed smooth. Remove the back and fit the battery and transistors and check that the polarity is correct. Replace the back and plug in the earpiece lead. It


The lay-out of components in the completed receiver.

the expense of

Fig. 7.-Dimensions for the amplifier and receiver cases.
should be quite easy to sbtain a strong signal when C 4 is at the point of oscillation.

## Amplifier

Cut a piece of plastic size $3 \frac{1}{2} \mathrm{in}$. $\times 4 \frac{1}{2} \mathrm{in}$. Position the components on the back of this and mark the fixing holes. Drill these to take about size 6B.A. bolts. Cut a hole either square or round to correspond with the loudspeaker position (Fig. 5), it was found that a rectangular hole was quite adequate.

Before fixing the loudspeaker in position a piece of fine linen was glued over the apperture. Now that the loudspeaker and transformers are in position. carefully lay out the other components. Next proceed with the wiring from the loudspeaker end, working back to the input transformer. leaving enough space to slip the transistors into their holders. The batteries should be allowed plenty of space. When the wiring is complete, the sides can be fitted together. With the small switch it is as well to solder the connections to this before gluing into position on the sides. The best way to accommodate the batterics is to make a small cardboard frame with the contacts fixed in the usual manner (Fig. 6). In all cases when making the small brass contacts it is wise to leave a large nib which can be soldered to the wiring. The
imput flex is soldered into position, knotted and passed out through a small hole in the side, after which the bome-made plug can be attached. (Sce Fig, 4).

With the coil wound as before it is not possible to receive the Third Programme. If a 100 pF is wired in parallel with. C3 this station can be tuned in, but at losing Radio Luxembourg.

## Miniature I.F. Transformers

A new range of miniature pass-band intermediate frequency transformers has been introduced by the Wireless Telephone Co. Lid., one of the Plessey Group of companies. These are intended for portable transistorised receivers with intermodiate frequencies within the range of 450 $480 \mathrm{kc} / \mathrm{s}$. The chief feature of the new. transformers is the parallel mounting of the coils which gives stable coupling and compact assembly. The ferrite cup cores are potted in an epoxy resin to give good mechanical rigidity with resistance to vibration. The can size has been reduced to $1 \frac{1}{2} \mathrm{in}$. $x$ fin. $x \frac{1}{1}$ in.

Double tuned transformers are used in the first two stages, and a single tuned unit in the third stagc. and I.F. alignment is carried out by adjustable dust cores. These are mounted in a novel way: in place of the normal threaded core a plain corc is bonded to a polystyrene serew working in a threaded hole in the coil former. This provides a robust adjusting screw for operation by conventional metal-bladed screwdrivers, and this design allows the cores to be wax sealed after final trimming.

The transformer for the third stage has the diode R.F. by-pass capacitor mounted inside the shielding can. Wireless Telephone Co. Led. Hallangate Works, Crookes Road. Sheffield 10.


Aoove.-An above-chassis view of the amplifier.

## Below.-The lower side of the tapedeck.



The underchassis view of the amplifier and its panel.

## A Versatile TAPE REC

$\mathcal{T}$HIS tape-recorder uses a Motek K. 9 tape-deck in conjunction with a home-built amplitier and cabinet. For convenience, the recorder can be divided into two sections. The tape transport mechanism and associated motors, together with the record/playback and erase heads, form one section; whilst the amplifier. power-supply, cabinet and loudspeaker form the other.

## The Tape-Deck

From the start. it was decided to use a commercially huilt tape-deck, as previous efforts to build a satioliactory deck had not been successitul. One of the main difficulties in constructing a tape-deck is to achieve a very steady tape transport mechanism together with a fast and efficient rewind. Although reasonably fitir results were obtained, these were not of a high standard. The tape-deck finally chosen is easily built into a home-made cabinet. small in size although taking 7in. reels, and has simple, push-button controls. The liyout of the mechanical parts of the deck is such that there is ample room for placing an amplifier, power-supply and loudape:aker underneath it. without any necd to miniaturise or place components in positions likely to get overheated.

## Positioning the Power Supply

Preliminary measurements on the deck gave an idea as to what room was available for the various pieces of equipment and also the best layout. One of the difliculties in magnetic recording is the susceptibility of the various parts of the apparatus to interact with each other and produce undesirable hum and noise. The power-supply is the chef offender. especially if placed close to the record/playback head. The hest place for the power nack is as far away as possible from the head. yet in a space that will allow an uncramped layout and a small amount of movement. for even altering the position of the mains-transformer by $\frac{1 i n}{}$. can greatly reduce hum.

## Choice of the Loudspeaker

In order to ohtain good results frum the loudipeaker. it shoubd he as large as possible and well mounted in the cabinct. The masimum size of Ioudspeaker that could be used without making the cathinet too bulky was found to be $8 \frac{1}{2}$ in. $x 5 \frac{1}{2}$ in. An

## JRDER

## A HOME-MADE <br> AMPLIFIER AND <br> CABINET WITH <br> A COMMERCIAL <br> TAPE-DECK


alternative was considered in the form of two smaller loudspeakers, but on comparing the results obtained from the two arrangements, the larger loudspeaker sounded more realistic, especially for music. Finally, a highflux permanent-magnet loudspeaker was chosen.

## The Amplifier

With a general idea as to the room available, the amplifier was considered next. It had already been decided as to what was expected of the amplificr and it was necessary to design one which would fit into the allotted space and yet would function as required.

For a recorder of this type, the amplifier has to serve both as a record and play-back amplifier; each function being determined by suitable switch-


Fig. 1,-The graph of the relative output (dB) to frequency.
ing. In addition, there are several aspects of such an amplifier which are very important. It must have sufficient gain to amplify signals from the microplane, or other source, to provide an adequate
signal to energise the recording head in the record position, and a similar amount of gain to drive the loudspeaker from the small playback signal. As the average output from a combined record/ playback head is only about 3 mV , the gain has to be very high. In carrying out these functions, the hum and noise level should be kept as low as possible. or the signal to noise ratio will be greatly reduced. Another difficulty to be faced is that of providing the correct compensations for the nonlinear recordiplayback process.

The graph (Fig. 1) shows the probable constantcurrent recording frequency response and the required playback compensation. At low fre-quencies-between $S=2 / \mathrm{s}$ and $1,500 \mathrm{c} / \mathrm{s}$ a compensation network, giving 6 dB per octave boost. is required, but above about $1.500 \mathrm{c} / \mathrm{s}$ another network is needed giving more than 6 dB . A number of ways of doing this are described later, including the one chosen for this recorder.

In order to provide a high frequency signal for both erasing and biasing, an occillator is needed, working at a frequency of ahout $60 \mathrm{ke} / \mathrm{s}$, hut it is only required during the record process.

With these thoughts in mind, the circuit diagram (Figs. 2 and 3) was the one finally chosen, In all. only five valves arc used. one being a full-wave rectifier, and of the other four. only three are used during , play back.

## Record'Playback Switch

With amplifiers of this type. great catre is needed when designing the switch that will convert the amplifier from the record to the playback position. In this case, the number of switched circuits has been kept down to a minimum without sacrificing
any efficiency. There are only four sections of the switch, each being three-way. The second, or central, position of the switch is used to convert the amplifier into a general purpose one, so that it can be used without the tape-deck. Another important feature of the switch mechanism is that
via C14 and R19 to SB1 where they are switched on to the high-impedance record head. The oscillator valve V4, is also switched on by SDI and bias signals are applied via C17 and SC1 to the record head, whilst an crase signal is fed via C18 to the high-impedance erase head.


Fig. 2.-The circuit of the amplifier, excluding the bias oscillator and power supply.
on switching from record to amplifier, the bias voltage on the record head is made to die away slowly as C19 discharges. This prevents the record head from becoming magnetised by abruptly switching off the bias. A magnetised head will introduce a great deal of additional noise on playback.

## Amplifier Theory

For recording, the grid of V1 is connected via SAl to the high-gain input socket $A$. V1 acts as a high-gain voltage amplifier with screen grid and bias voltages supplied by R4 (decoupled by C4) and R2 (decoupled by C1) respectively. After amplification the signals are passed via C3 to a frequency-compensating network; which will be described in. detail later, and on to the volume control R9. From here the signals are further amplified by $V 2$ facting in exactly the same way as VI) and passed on to the output valve via C 10 and R18. After further amplification in V3 the signals can be heard via the output transformer and loudspeaker for through headphones if it is desired to mute the loudspeaker when recording "live" from a microphone).
From the anode of $V 3$ the signals are also passed


Fig. 3a.-The bias oscillator circuit.

If a high input source is available (e.g. a radiotuner or gramophone). this can be connected to the low-gain socket (B) and socket A shorted out with a shorting plug, or fed from a microphone with a built-in volume control. In this way, two signals can be mixed together at the volume control and then recorded.

## Record-Level Indicator

One feature during recording is the record-level indicator. This is built as a separate unit in a small box and not into the recorder as is the general practice. If the source of sound is varying in intensity considerably, constant watch on the record-level indicator is required.
The recorder was used mainly with a small mixer unit. which controlled the signal being fed into the input socket ( $B$ ). the volume control R9 being at maximum. With the indicator close at hand (being fed from the output transformer with the loudspeaker switched off). the recorder could be placed over 20 ft or more away. The indicator can easily be built into the recorder if so required.

In the amplifier position, both input sockets $A$ and B are used as before. but R19 is now earthed via SB2 and the bias oscillator switched off. The amplifier can now be used on its own for a good quality reproducer of radio or gramophone signals, at a maximum output of 5 W . In all three positions of the switch, negative feedback is applied from the secondary of the output transformer to the cathode of V2. This greatly improves the quality of reproduction of the amplifier.

In the playback position, the grid of V 1 is connected via SA3 and SC3 to the record/playt. ck head: R19 remains earthed via SB3. Socket B can now be used to supply a larger amplifier with signals from the tape in order to obtain the very best reproduction, although the playback amplifier will be ample for normal purposes. especially if an extension loudspeaker in a large cabinet is used. If required, socket $B$ can be used to mix another signal with that from the tape (e.g. background music for a play can be tried out this way without spoiling the tape).


Fig. 3b. -The circuit of the record level indicator.

## The Amplifier and Power Supply

The amplifier itself is built on to an aluminium chassis measuring 8 in . $x 4 \mathrm{in}$. $\times 2 \frac{1}{2} \mathrm{in}$. deep. Except for the hias oscillator and equaliser circuits, all small components are built onto one 16 -way tag board. The equaliser circuit is itself built on to a smaller 5 -way tag board which is mounted in such a way that it can be removed casily and an alternative equaliser circuit tried. A smaller aluminium chassis, 7in. $x 3 \frac{1}{2}$ in, $x$ lin. deep holds all the power


Fig. 3c.-The power supply circuit.
supply components and has $\frac{1}{2}$ in. external flanges on the $3 \frac{1}{2} \mathrm{in}$. sides in order to mount the powerpack on to the wall of the cabinet.

## The Front Ponel

An aluminium front panel is used with the amplifier chassis, the size of the panel can be altered slightly to suit requirements. It must, however, be $5 \frac{1}{2}$ in. high, although the length can be from 9 in. to over 11 in. depending on the width of the recorder cabinet used.

First of all. the amplifier chassis is required. This can be home-made to the dimensions given in Fig. 4a. or a commercial chassis may be used: The four valve-holder holes should be cut first. A valve holder ( $\mathrm{BOA}^{\prime}$ ) should be placed in each hole in turn and two marks made indicating positions for holes to be drilled for fixing bolts. These holes should be $\frac{1}{4}$ in. in diameter. The other holes can now be drilled, care being taken to make sure that the socket, grommet or other component fits the hole made for it. Do not mount any components yet. A piece of $16 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. aluminium is cut to size and drilled to form the screen that isolates the oscillator section. The three bends should be made carefully-a good idea is to score the metal heavily with a sharp tool on the inside of the bend. A sharp bend will then result. The screen can now he fitted into the chassis temporarily and tested for size and shape. its fixing holes being made to align with others drilled in the chassis. Now, remove the screen and put it carefully to one side.
It should have already been decided as to the make of tape-deck and size of cabinet to be used. In most cases. an external width of about 12 in . is needed. (The length does not affect the size of the front panel used.)

## (To be continued)

## A Tremolo Unit for an Electric Guitar

## THIS PIECE OF EQUIPMENT MAY BE USED SEPARATELY OR IN AN AMPLIFIER

7

HE well-known Tremolo constitutes variations of either frequency, has recently beconre guitarists using the modern electric instrument and its associated amplifier.

## Amplitude Variation

One of the problems with the amplitude variation method is that of preventing the harmonics of the low-frequency tremolo oscillation from being amplified, thus producing an objectionable thumping sound, especially when the amplifier chain is


Fig. 1.-The circuit of the tremolo and pre-amp unit.
operated at full gain. The problem may be partly solved by injecting the tremolo oscillation at the final stages of the amplifier: for example. into the amplifier valve directly preceding the actual output stage. This is quite practicable if the main amplifier can be specially constructed with an incorporated slow-rate oscillator. However, for those who have an existing amplifier and do not wish to modify it, the only solution is to build an entirely separate but combined tremolo and pre-

The output from the tremolo unit is taken from a 500 k potentiometer, VR3, which provides full control over the output voltage so as not to overload the main amplifier first stage. The original design was contained in a case 11 in . $x$ sin. $x 4 \frac{1}{2}$ in. which included the power supply transformer and components. Layout of the unit is not critical, and providing the usual rules for audio equipment are observed no trouble with hum or instability should be experienced.

February, 1961



Fig. 3.-The control panel

## Circuit Description

Two inputs are provided which may be used for guitar or microphone. The one marked "Microphone" requires only a low voltage input and may be found useful for guitars with low sensitivity pick-ups. The input marked "Guitar" is adjusted to comply with pick-ups of average sensitivity. Negative feedback prevents full gain from V1 whose cathode is taken via a potentiometer VR2 (tremolo amplitude) to the cathode of the phąse shift oscillator V2. Note the very high capacity decoupling capacitors on V2 cathode. The use of a smaller value will result in harmonic thump from the main amplific. Variation of the tremolo rate between 4.5 and $10 \mathrm{c} / \mathrm{s}$ is provided by VR1 and the tremolo may be switched off by S 1 .

## Adjustment of Tremolo Rate

The output from the tremolo unit is taken to the guitar input of the main amplifier which may be operated with nearly maximum gain, thus allowing the gain control on the tremolo unit to be used for normal gain control purposes. In this way overloading of the main amplifier input may be prevented. unless the guitarist wants a squarewave output-which incidentally is an effect sometimes deliberately introduced for single string solos.
To produce the best and most pleasing tremolo, adjust the amplitude control until a slight waver
on a struck note is just noticeable, the most effective ra1s being about $6 \mathrm{c} / \mathrm{s}$. Too much amplitude and too fast a rate of oscillation will spoil the effect and is likely to ${ }^{\dagger}$ introduce a certain amount of harmonic thump.

## Constructional Details

The original design was produced for commercial application and a prototype was constructed in a mild steel (18s.w.g.) case, 11 in . x 5 in . x $4 \frac{1}{2} \mathrm{in}$. Fig. 2 gives chassis and panel dimensions and shows the layout adopted with regard to the positions of the valves and the tagboard on which all


Fig. 4(a).-This unit can be mounted on an existing guitar amplifier.
the small components were mounted. The chassis is folded at an angle of 45 deg to accommodate the valves with in the case. There is ample space for the small mains transformer on the back of the panel within the area marked. Controls may be arranged side by side on the front panel above the chassis. and if small single-hole fixing microphone jacks are used they may be accommodated on the section of panel below the chassis (see Fig. 3). The tagboards (miniature 12 way) are mounted on the under side of the chassis, thus permitting short


Fig. 4(b).-An amplifier with a tremolo unit fitted in the back.
leads to the valveholders. The order of components on the tagboard is not critical as there is no likelihood of instability or cross-talk; simply plan the layout for convenience of wiring and if an allmetal box is in use no leads need be screened. The output co-axial socket may be mounted at the rear
of the case or on the front panel; whichever is more convenient.

## Alternative Arrangement

Some may find it more practical to mount the unit in the guitar amplifier case. An alternative version was in fact assembled on a fairly long but narrow panel that could be mounted on the back cover at the top. Fig. 4 shows how this may be done and if this arrangement is used the chassis need be only 2 in . or so wide but long enough to comfortably accommodate the two valves and the tagboard. Power may, of course, be obtained from the main amplifier H.T. and heater supplies as the unit consumes only a few milli-amps of H.T. current and 0.6 A for the heaters.

## COMPONENTS LIST.

V1 EF86.
C2, C3, C5, C9, C10,
V2 EF80.
Microphone Jacks.
Resistors all $\mathbf{1 W}$. C11, C12 Electroly. tic Capacitors.

## Remaining of capa-

 citors are tubular.S1 On/Off type toggle switch.
M1 Metal Rectifier - Westinghouse type 16.R.C.-1-16-1.

T1 Mains transformer $220-250 \mathrm{~V}$ pri. 250 V single sec: H.T. $6 \cdot 3 \mathrm{~V} 1 \mathrm{~A}$.
VR3 and VR1 Standard size potentiometers. VR2 Wire wound.
Standard type co-axial Output socket. Valve Holders B9A Noval.

## A Steres Amplifier

## (Continued from page 888)

The previous stage must provide a signal Va equal to Vin plus the signal voltage across $R 2$.

Va must therefore be $4 / 3$ of Vin, which is the same as saying that the stage gain is reduced to $\frac{3}{3}$ of what it was without feedback. The stage gain thus becomes 9 , and for the two stages the overall gain is $9 \times 9=81$ times. An input of 150 mV , will produce 12 V of audio for the output valve which will thus be fully loaded. It follows from the above argument that the higher the anode load the less the loss through feedback, but the higher the cathode resistor the greater the feedback; unfortunately the higher the anode load the higher the cathode resistor has to be for a given bias voltage, and consequently the benefits of a larger anode load can be taken only in stages working at a low signal level in which a low bias voltage can be accepted.

In the present design the cathode bypass capacitor has been omitted in the output stage also. The effect on gain is noticeable but not serious whereas the feedback does clean up reproduction to any degree. If the constructor found the need for just a little extra gain he could try the effect of fitting a $25 \mu \mathrm{~F}$ electrolytic across R8 and R16.
(To be continued)

## COMPONENTS LIST

Resistors:
$\left.\begin{array}{ll}\text { R1, } 9 & 1 \mathrm{M} \\ \text { R2, } 6,10,14 & 3 \cdot 3 \mathrm{k} \\ \text { R4, } 12 & 10 \mathrm{k} \\ \text { R7, } 15 & 220 \mathrm{k}\end{array}\right\} \frac{1}{2} \mathrm{~W}$
R7, 15 220k
R3, 5, 11, 13 100k high stability $\frac{1}{2} W$
R8, $16240 \Omega$ wire wound 5W
Condensers:
C1, $4 \quad 32+32 \mu \mathrm{~F} \quad 350 \mathrm{~V}$ electrolytic
C7, $8 \quad 16+16 \mu \mathrm{~F} 350 \mathrm{~V}$ electrolytic
C2, $5 \quad 0.01 \mu \mathrm{~F} 400 \mathrm{~V}$
C3, $60 \cdot 1 \mu \mathrm{~F} 350 \mathrm{~V}$
VR1, 2 1M
Valves:
V1, 312 AU 7
V2, 4 6BW6
V5 EZ81
Other Parts:
S1, 2 Single pole toggle switch.
L1, 2 Indicator lamps in holder.
TFR1, 2 Output transformer (Parmeko P2641).
TFR3 Mains transformer $\mathbf{3 0 0 - 0 - 3 0 0 V} 120 \mathrm{~mA}$ (Parmeko P2644).
$2 \times 6.3 \mathrm{VCT}, 6.3 \mathrm{~V}$
Choke 10 H 120 mA (Parmeko 549).
Output sockets.
Input socket-4 pin miniature.
Valve holders- 5 off type B9A.

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| 185 | $6 / 3$ | 6BX6 | $6 / 8$ |  | 9／－ | $7{ }^{7}$ | 719 | 20L1 | 13／6 | ${ }_{723}$ | $29 /-$ | DL．94 | $7 /$ | EF40 | 13／6 | HL41D D8／6 | PL81 | $9 \cdot 9$ | U301 | 14／－ | UY41 | $6 / 6$ |
| 1T4 | 4／－1 | HC4 | $61 /$ | rill 19 | $12 / 6$ | 7 Y 4 | 71 | 20 Pl | 11／6 | 723 $\times 07 A$ | 58／－ | DL96 | $7 / 9$ | EF41 | 8／6 | HVR2 76 | PL89 | 7／6 | U309 | 12／6 | Y85 |  |
| 21021 | 4／6 | かC5 | $5 / 6$ | HLD 3 | 8／6 | 7\％ | $7 / 6$ | 20P3 | $12 / 6$ | 807A | $3 / 9$ | EA50 | 9d． | EF42 | $7 / 6$ | KL33 $\quad 7 / 9$ | P183 | $7 / 6$ | U32\％ | $12 / 6$ |  | 8 |
| 1A | 5／6 | 8С | 4／8 | ¢LD12 | $7 / 6$ | 3 | $3 / 6$ | 20 P 4 | 17\％ | 808 | $15 / \mathrm{F}$ | EABC80 | $7 / 6$ | EF50－B |  | KT32 8／8 | PL\＆4 | 11／－ |  | 11／－ | V810 |  |
| 316 | 4／6 | ${ }^{\circ} \mathrm{Ca}$ | P／e | RLDI2 | 16 | 10 Cl | 11／－ | 20 P 5 | 18／－ | 8 | ［5／－ | EAC91 | 4／9 | EF50－ | A | KT33C 616 | PM80 | 819 | U339 | 11／4 |  | 71 － |
| 4Q4 | $7 / 3$ | 6CD6G | 18／6 |  |  | 10 C 2 | 13／6 | 25 A 6 G | 8！－ |  | 8 | EAF42 | 8／8 |  | 2／8 | KT36 8f－ | PX25 | 18／－ | U403 |  | V |  |
| 1Q5GT | $8 / 9$ | ${ }_{5}^{5 \mathrm{CH}} 6$ | $3 / 9$ | 6 Pl | 14／－ | 10C14 | 818 | 25L6G | 6／9 | 95 F | $3 / 9$ | E334 | 1／6 | EF54 | 3／3 | KT44 $\quad$ 9／6 | PY81 | $8 / 3$ |  |  | － | 5／6 |
| 384 | 6f－ | 6D1 | 9d． | 6P25 | $91-$ | 10 Fl $10 \mathrm{F9}$ | 6／8 $10 / 3$ | 25 LiGGT | 91－ | 5763 | 10 f | EB41 | $7 /$ | EF80 | $5 / 3$ | KT45 8／6 | PY32 | 10／6 | U801 | 29／＊ |  |  |
| 3 V 4 | $7 /=$ | 6D2 | $3 / 9$ | 6P28 | 12／6 | $10 \mathrm{F9}$ | 10／3 | $25 Y 59$ | 9／－ | 9001 | 4\％－ | EB91 | $8 / 9$ | EFP5 | $7 /$. | KT61 8／－ | PY80 | $7 /$ | UAB | $8 / 8$ | W61M | 11． |
| 5R4G | $9 / 6$ | 6D3 | $12 / 6$ | 687G | $8 / 9$ | 10L14 | $81 /$ | $25 \mathrm{Z4G}$ | $7 / 3$ | 9002 | 4／8 | EBC3 | $8 /-$ | EF86 | 10／3 | K＇T63 8／6 | PY81 | 8／8 | UAF42 | 9／－ | W76 | $5 / 6$ |
| ${ }_{3} \mathrm{H} 4 \mathrm{G}$ | $5 /-$ | 506 | 4／8 | 6Q7GT | $0 / 3$ | LD3 | $8 / 8$ | $25 \mathrm{Z5}$ | 8／－ | 0003 | 4／－ | EBC38 | $5 /-$ | EF89 | 8／－ | KT66 12／6 | FY82 | 6／8 | UB41 | $81 /$ | W77 | ／8 |
| ${ }_{5} \mathrm{~V} 4 \mathrm{G}$ | $8 / 8$ | 6 F 1 | \＄／9 | firg | $7 / 6$ | $1{ }^{10 L D 12}$ | 819 $8 / 6$ | 576 | 9／－ | ATP | 2／9 | FBC4 | $8 / 6$ | EF91 | 3／6 | KT76 8／6 | PY83 | 81－ | UBC41 | 8／3 | W81 | 5／9 |
| 5 Y 3 G | 81－ | 6F6G | 6／3 | ARTG GSA？ | $7 / 6$ $5 / 9$ | 10P18 | $8 / 6$ $8 / 6$ | 2780 | 16／－ | A 731 | 4／1－ | EBC81 | $7 / 8$ | EP82 | 4／8 | KT8］14\％ | PZ30 | 12／－ | UBC81 | 10／－ | X61M | 18／6 |
| 5Y3GT | 6／b | ＋iF6M | $7 / 18$ | 6SG7 | 4／9 | 10P18 | $8 / 6$ | 30 Cl | 718 | B36 | $8 / 6$ | EBFA9 | $8 / 6$ | EF95 | 6／9 | KTW61 5／6 | R14 | $12 / 8$ | UBF89 | $8 / 6$ | X63 |  |
| 3 Y 49 | 11／－ | 6 F 12 | $8 / 8$ $6 / 9$ | 6SH7 | 4／6 | 12A | $5 / 8$ | 30F5 | 71 | B65 | 419 | EBF89 | $8 / 6$ | EK32 | 719 | KГW83 4／9 | $R 19$ | 12／6 | UBL21 | 14／8 | X <br> $\times 85$ | 11／－ |
| 374 | $11 /-$ | 6F13 4 F 14 | $6 / 9$ <br> $8 / 6$ <br> 18 | 6SJ5 | $5 \%$ | 12A 1247 | 6／9 | 30 FL 1 | $9 / 6$ | CBLS1 | 21／－ | EBL21 | 14／－ | EL32 | $4 / 6$ | $\begin{array}{ll}\text { KTZ } 63 & 5 / 6\end{array}$ | 8 SPG | 810 | UCCS 4 | 14／6 | X 45 | 11／－ |
| ${ }^{\mathbf{5} 74 \mathrm{4}}$ | 8／6 | ¢FP14 | 9／6 | A8K7 | $5 / 3$ | l2aH7 l2aH8 | 819 | 30 FL | 779 | CCH35 | 716 | EBL31 | 21／－ | EL33 | 19／－ | L63 2／9 | SP6 | $8 / 8$ | UCCA | 8／－ | \％ 66 | 11／． |
| 574GT | 11／－ | RFIS | $9 / 6$ | R8K7 68L7T | 5／3 | l2ats | 779 | 30 Pa | 12／6 | CL3＊ | 18／－ | EC52 | $3 / 9$ | ELis5 | 8／6 | LN152 7\％ | SP41 | $2 / 6$ | UCF80 | 16／－ | 876M | 9／6 |
| SA7 6A8G | 10／－ | $6 \mathrm{SF}^{3} 6$ $6 \mathrm{~F}^{3} 3$ | $8 / 6$ $8 / 9$ | 68L77T 58N7GT | 4／9 | 12AT7 | 5／9 | $30 \mathrm{P}^{1} 12$ | 8／－ | CY31 | $9 / 9$ | EC90 | 3／6 | EL37 | $11 / 6$ | L7，319 716 | SP61 | $2 / 8$ | UCH21 | 14／6 | K8 | $11 / 6$ |
| ¢AXGT | $13 / 6$ | 6（2） | 8／－ | ¢SQ7 | 6／3 | 12AU7 | $6 / 8$ | 30P14 | 719 | D63 | $1 / 6$ $3 / 9$ | EC81 | 4／6 | EL88 | $12 / 6$ | $\begin{array}{lr}\text { MU14 } & 8 /- \\ \text { N37 } & 11 /-\end{array}$ | 9U21 | A4／6 | UCH42 | $7 / 9$ | $\mathbf{X 7 8}$ | 20／6 |
| EAB8 | 8／3 | 6H6 | 21－ | 68S7 | $5 /-$ | 12AX7 | 7 \％ | 30 PL 1 | 0／6 | D77 | $3 / 9$ $6 / 6$ |  |  | E 1 | $9 / 6$ | N78 15 <br> 1  | T41 | 7／6 | UCH881 | 8／6 | Y 63 | 0／8 |
| 6AC7 | 4／8 | 6.55 | $4 / 8$ | 6U4at | 20／6 | 12 BAA | $8 / 8$ | 35 LGG | 9／－ | D152 | 12／6 |  | $4 / 9$ | EL94 | $7 /$ | N108 18j－ | TH30 | $12 / 6$ | UCL81 | 1178 | 288 | $5 / 8$ |
| riAc5 | 4／3 | $6 J 50$ | 219 | 6U5G | $6 / 8$ | 12BEf | 818 | 35 W4 | 6／9 | Da30 | 12／6 | ECCB4 | $8 / \%$ | EL91 | $4 / 9$ | N152 10／6 | U14 | 8／－ | UCL83 | $13 / 8$ |  | $9 / 6$ |
| BAG7 | 81－ | 6.55 GT | $3 / 8$ | 6Vfict | $5 / 8$ | 128H7 | 1016 | 3574 GT | 516 | DA90 | $8 / 8$ | FCC35 | $8 / 9$ | EM34 |  | P41 4／6 | U1 | 8／8 | UF41 | 8／6 | 77 | 16 |
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# An Efficient Mains Filter 

## ELIMINATING MAINS-BORNE INTERFERENCE

By M. D. Roberts

$\mathcal{J}$HIS filter was designed for use with mains radio receivers in areas where mains interference is troublesome. It consists simply of two chokes and four condensers, but the very nature of the construction makes it into an efficient filter network


Fig. 1 (above).-The simple circuit.
Fig. 2 (below).-Details of the coil cheeks fitted on the bakelite tube.


## Mains Input

The mains to the receiver is fed through LI and L2. These two coils being wound on the same core to help limitation of interference in the filter. The addition of the four condensers make up a very efficient filter.

## Construction

The first stage is to obtain a piece of $\frac{r^{3}}{5}$ in. diameter Bakelite tube, 5 in. long, and four Bakelite discs 1 fin in diameter with a hole in the centre of each so that they iust fit on to the tube. Fig. 2 shows these in position, but before they are glued down two of the discs must be modified
slightly. From Fig. 2 it will be seen that there are some connecting lugs on two of the Bakelite discs. These lugs are at $90^{\circ}$ to each other (Fig. 3). They consist of 8B.A. nuts and bolts with SB.A. solder tags, and they must be as close to the edge as possible, as otherwise they get in the way of the coils when they are wound.

When two of the discs have been modified, assemble them as shown in Fig. 2 and cement them into place with some hard-setting glue.

Fig. 3 (right).--The hakelite formers and the lugs set at $90^{\circ}$ to one another.


Marerial.... $\frac{1}{16}{ }^{\text {nthick }}$ bakplite 4 required

## Coil Winding

When the glue has set, pile-wind 140 turns of 18s.w.g., tinned copper wire for L1 and L2. Wind hoth coils in a clockwise direction. and about four layers of winding will be needed for each coil. Connect the ends of each coil to tags $A$ and $C$ on its respective disc. Next join the $B$ lug on both dises together with a short piece of lead. Wire the earth of the mains input lead on to one of the $B$ tags. and the live and neutral mains lead on one end of each choke. Take the mains output from the other end of each choke via a piece of mains lead.


Fig. 4.-The unit complete without its case.


The unit should appear as it does in Fig. 4 at this stage. being completely wired except for the condensers. Take two condensers each to B1. Wire one side of the remaining two condensers to lug B. One of the condensers that has been wired to B must be wired on to A . and the other on Bl must be wired to C.
Fig. 5 (left).-Drilling details of the case ends.

# High Impedance Voltage Indicator 

# A USEFUL AID FOR ALIGNING VHF/F.M. RECEIVERS 

$\mathcal{T}$

By J. Willmott with alignment of the com dificult problem. that of major difference between, say, the normal A.M. superhet receiver and a VHF/F.M. unit. the former can be aligned to a reasonable degree of at. traty without the use of instruments, provided that care and patience are taken over the procedure. When it comes to the alignment of F.M. tuner, a much higher degree of aceuracy is required il satislactory results are to be obtained, and the use of instruments is essential. Many of the firms retailing kits offer an alignment service for a very modest lee, and doubtless to many constructors this represents the easiest and most satisfactory solution, but for the radio enthusiast who neither wants to resort to these means nor to buy equipment such as wobbulators and oscilloscopes, necessary for any such operation, all is not lost, provided he is in possession of an ordinary A.M. signal generator, capable of covering the $10.7 \mathrm{Mc} / \mathrm{s}$ I.F. of standard F.M. receivers, and a sensitive output indicator of some sort. either a voltmeter set to the 10 V range and having a sensitivity of not less than 10.000 s/V. or at valve voltmeter. Moving-coil meters of this sensitivity are expensive and somewhat delicate, and most constfuctors have to make do with a 1 sensitive, multi-range meter seneral testing needs. and so e "Valve" voltmeter comes 1 gind. which is an ideal instrument for the purpose in hand, as it draws virtually no current from the circuit to which it is connected.

## Valve Voltmeters

There have been a number of designs for valve voltmeters featured in Praciical Wirfless from time to time but these were of fairly elaborate deagn. having provision for measuring a large ratnge of volugen with great accuracy. All that is required in the present instance is sume indication of the presente and amplitude of voltages in the 0 to 10 V range, the exact voltage represented by any particular meter deflection is of no importance. In other words all that is needed is an indication of rise or fall in voltage present at the selected high impedance test point. With these factors in mind, a simple indicator to which the normal multimeter can be connected to provide the comparative readings wats designed, and has proved highly satislactory. The indicator can be used with any meter possessing a basic movement of $2 \cdot 5 \mathrm{~mA}$, or better still, 1 mA . The cost of construction is extremely low, even if every component had to be
purchased, but the majority of parts will be found in most "spares boxes". The prototype was constructed to operate from the standby bench power supply ol 6.3 V (heaters) and 250 V (H.T.), but as it is obviously preferable to have a more self-contained instrument, a lurther design was developed, incorporating a lully isolated halt-wave power supply unit, using a smail mains transformer of the type designed for TV pre-amplifiers ete. The imperance of the completed instrument is in the region ol 10 M . and will be found to give a useful deffection of the meter movement when connected to the AVC line of an F .M. tuner for ordinary A. M. superlet receiver), or across the ratio detector network.

It is well known that the current passed in the anode circuit of a triode valve is dependent upon the applied H.T. voltage at the anode, and the negative "bias" voltage applied to the control grid. and that if the anode volts remain constant whilst the grid bias wolage is varied. the anode current will vary. a reduction in bias causing an increase in anode current. If it is arranged to monitor the anode currem passed
$4 \mathrm{~K} \Omega$ 10 watt wirewound


Fig. 1.--The theoretical circuit of the woltage indicator. ( RI. R2 wht R3 are 3-4 M.)
by the valve with a meter in the anode cirenit. any change in whtage existing at the control grid will be reflected in the meter reading. The impedance of the gride ercuit can be made so high ( 10 M in the present case) that practically no disturbance is made to the voltage distribution of any circuit to which the test probes are connected. It is usual to arrange that under static conditions, i.e. when no external voltage is present at the test probes, the valve is so biased that anode current is exactly cut off, and the meter reads "zero". As soon as a positive voltage is applied, this will oppose (and therefore decrease) the standing negative bials. allow current to flow, and the meter to be deflected accordingly.

In practice, it is lomed desirable to have both the anode voltage and grid bias voltage variable within

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- Plastic Cable Stripperi
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lllustrated is the 25 w .316 in . replaceable bit model with mafety shield.

[^2]
limits. so that the exact point of "cul off" can be readity aet up. Reterring to 1 ig. 1. the theoreticat diagram. it will be wen that the preset potentiometere VRI and VR2 provich the necessary adjustments. 11 is comvenicnt to til acontrol knoh to VRI. as this will require "reseting" io eron the meter aceurately from time to time, as a simple instrment of thas lype invariably show signs of the mal dift when in we.

## Construction Details

( onvtraction of the imprument is extremely vimple, and aphat from the need to keep the connections between the iunction of $K I . K 2$ and $R 3$. and the valve control grid. as short as possible. the layout is in no way critical. A chassis of standad size. 7in. x 4 in . $\times 2 \frac{1}{8} \mathrm{in}$, is used, and drilling dimensions are given in detail in Fig. 2. Fig. 4 should make the fayout of components perfectly clear. The mains supply leads enter through the sin. grommetted hole in the rear chassis runner, and are anchored to the two insulated tags of a 3 -way tagstrip mounted nearby. No on/otf switch was provided in the original. although there is no reason why one should not ne provicled. and mounted at any convenient point on the rear or side chassis runners. The test leads.


Fig. 3a-Comections to the Octal valve-holder.


Fig. 3b.-The wiring of the balance potentiometers.
comprising red and black plastic-covered flexible wires (not twisted together. as this would introduce

## COMIPONENTS LIST

Resistors:
R1-3.9.1 $\frac{1}{2} \mathbf{W}$.
R2-3.9M ${ }_{2}^{2} \mathbf{W}$.
R3-3.9 M1 W.
R4-2.2N $\frac{1}{2} W$.

R5-1k $\frac{1}{2} W$.
R6-27k $2 W^{\prime}$.
R7-4 to 5 k 5 or 10 W W.W.

C2-0.001 $\mu \mathrm{F}$.

Chassis 7in. $x$ tin. $\times 2 \frac{1}{2}$ in.
A small mains transformer, 6.3 V and 220 V 40 mA .
A metal rectitier, $250 \mathrm{~V}, 10 \mathrm{~mA}$ or more.
$32 \mu \mathrm{~F}+32 \ldots \mathrm{~F}, 275 \mathrm{~V} . \mathrm{W}$, electrolytic (C1A and CIB).
Fixing clip for above.
One I.o. Valveholder.
6.15 Valve.

Two insulated terminals.
One small knob (for VRi).
Mains lead and plug.
Red and black flexible test leads.
Two crocodile clips.
Four rubber grommets.
Nuts, bolts, solder tags, connecting wire, sleeving. etc.
"Multimeter" with basic movement 2.5 mA or better.
VR1-5k W.W. potentiometer.
VR2-25k W.W. potentiometer.
unwanted capacity), enter through the holes " $B$ " in the rear runner, the black lead going to any convenient earth point and the red lead to pin 4 of the octal valveholder, which in the case of the 6.15 valve

range available, and the potentiometers VR1 and VR2 adjusted to bring the pointer to rest exactly at zero, VRI should first be set with maximum resistance in circuit, and VR2 adjusted to obtain as near zero reading as possible. VRI then being used as the "fine" control. Now connect a low voltage D.C. source to the test prods, e.g. a single, or double cell torch hattery, when the meter should immediately show a considerable deflection.

## Alignment procedure

It is not proposed to relate in detail the procedure to be adopted int the alignment of F.M. receivers; if a proprietary kit has been purchased, full instructions will be given with the kit.

Fig. 4.-Plan view of the chassis.
is a "spare" pin used for anchoring purposes. Two well-insulated terminals are mounted in the holes, tin. diameter, on the rear runner, and it is to these that the external meter is connected. The power supply requirements are 6.3 V at 0.3 A , and about 200 V at about 5 to 10 mA . So that any type of metal rectifier capable of withstanding an input voltage of 250 V will be suitable.

## Wiring the Instrument

Wiring is perfectly straightlorward, and if the theoretical diagram is used in conjunction with Figs. 3 and 4 no difliculty should be experienced. It is recommended that the power supply components be wired into position first, followed by the heater and H.T. supply to the valveholder. The two potentiometers must be of the wirewound type, as they have to carry D.C.

The two test leads are terminated in crocolile clips, to facilitate easy connection to the external circuit under test. When connecting the "live" kead to a tuned circuit, such as the windings of an I.F. transformer, it is advisable to incorporate a 100 k resistor at the point of connection to minimise the disturbance to the tuned circuit. It should also be remembered that when measuring the AVC voltage present at the limiter valve of an F.M. receiver, or on the AVC diode of an A.M. superlet, it is a negative voltage that is being measured, and in order to prevent the indicator meter movement from trying to record a reverse voltage, care should be taken to reverse the polarity of the meter connections to the terminals at the rear of the instrument.

## Testing the Completed Unit

To test the completed instrument, when wiring has been finished and checked for any possible errors, connect a multimeter across the terminals, set to a fairly high current range (say 100 mA ), in order to avoid any danger of the pointer swinging hard over and causing damage. After two or three minutes warming-up period, the meter may be gradually switched (or plugged) down to the lowest curreat

## AN EFFICIENT MAINS FILTER

(Continued from page 905)
Also one condenser wired on to B must go to Al , and the other to C1. This completes the wiring of the filter. and its wiring should be carefully checked against the circuit diagram (Fig. 1).

To complete the unit all that is needed is a case.

## The Case

Obtain two Bakelite discs lin. $x$ 1 $\frac{1}{8}$ in. diameter and drill a ${ }^{5} \mathrm{i}$ in. diameter hole in the centre of each. Also drill a $\frac{1}{4}$ in. diameter hole in both discs and fix one on each end of the mains filter. Feed the mains leads through the $\frac{1}{4}$ in. holes. A piece of Bakelite tube with a $1 \frac{7}{8} \mathrm{in}$. internal diameter. $5 \frac{1}{8}$ in. long is fixed over the whole filter assembly and glued into place. The ${ }_{16}^{5} \mathrm{in}$. diameter tube should be packed with 5 in . length of iron wire to form a core before the unit is linally glued.

## Installation

This completes the unit and makes it ready for imstallation in the mains circuit of a radio receiver. This is simply a matter of fixing a plug on the input end of the filter to fit the mains socket, and feeding the other end into the receiver.


Fig. 6.-The case of the filter unit.

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measurements of $9 \times 7 \times 5$ ins. In addition two high im. pedance input sockets are provided for microphone and gram., etc. With selector switch and vol. control, five B.V.A. vaives are employed ECC83, ECC83, EL84, EL84, EZ81, H.T. and L.T. power supply point is included for a radio tuner.
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# Radio Construction for the Beginner 

No. 5-COMPLETING THE REGENERATIVE RECEIVER

By D. B. Kidd

T"IHE two small tool-clips used to secure the small piece of ferrite rod in the last receiver described may be used to hold the long rod in this receiwer. Both clips are placed on the rod on the side farthese from L2. One clip is slid towards the middle until it almost touches the fixed coil L1, the other remains near the end of the rod. The two clips are thus much less than half the rod-length apart.
Now the three "extra" parts mentioned can be fitted. The fin, brass spindle is fitted into the small knob and secured, the spindle passed through a $\frac{1}{4} \mathrm{in}$. hole in the panel (near the bottom on the right) and the bush tightened on to the spindle so that the friction between the bush and the panel makes it fairlv difficult to turn the knob. If desired, a cardboard or rubber washer may be introduced to increase the friction. The position of the hole in the panel is chosen so that when the two tool-clips are screwed down and the ferrite rod is
in position, the unsupported end of the rod passes just underneath the spindle with about $\frac{1}{\pi}$ in. clearance. The ferrite rod assembly is as close as possible to the panel without quite touching the bush.

A mark must now be made on the spindle just over the centre line of the rod and a very small diameter hole drilled through the spindle at this point. This will mean removing the bush and reassembling the arrangement when completed. The constructor will need to file a slight "flat" at the point marked before drilling, otherwise the drill point will slip. The spindle should be held in a vice while drilling.

## The Regeneration Control

The end of a length of strong thread is passed
through the hole in the spindle and secured by knotting. The movable coil is slid along the rod until it touches L1 then the thread is laid over it and bound on to L 2 with Sellotape or other means. The thread is extended iust beyond L1 then cut and tied to the end of a piece of rubber hand. The far end of the rubber band is anchored to a nail, woodscrew lughook. or any other convenient pillar on the extreme left of the board and exactly in line with the centre line of the rod.
The elastic cord need not be very strong: it is only required to overcome the friction between the sleeve and the ferrite rod. A single strand will probably be enough.

When the regeneration knob is turned it will now
The complete transistor recemer
wind the sleeve to the end of the rod. This is its normal position when tuning in stations. Regeneration is obtained to the desired extent by turning the knob in the opposite direction when the elastic cord will cause L2 to approach L1. Although the arrangement is simple, and indeed almost crude, better and finer regeneration control is obtained by it than by more orthodox methods on expensive receivers. Figs. 3 and 4 gave the details. Note that the knob should be turned on so that the thread winds unde' the spindle.

The two leads of L2 should lastly be made spiral in form by releasing them from points " $N$ " and " $C$ "" wrapping them tightly round a knitting needle then replacing. This keeps them tidy in spite of thr movements of L2.

Two experiments may be tried with the completed receiver. Firstly, the aerial and earth may be disconnected and reception attempted with the ferrite rod alone. This will require the regeneration control to be advanced much more, but under good conditions and especially after dark it is worth trying. The receiver will now be found to be very "directional", the whole apparatus needing to be turned for the best results from a given station.

## Adding a Loudspeaker

If reception is very loud with an aerial and earth, the constructor may care to try connecting the two leads of a loudspeaker across the output terminals in place of the headphones. If faint reception is heard, then it is worth risking the expense of an output transformer which will greatly increase the volume of sound obtainable.

This should be bought as "suitable for transistor circuits" (valve-type transformers are almost useless for this job), and it should have a ratio of between $15: 1$ and $30: 1$. The two primary leads of the transformer go to the headphone terminals; its two secondary leads go to the loudspeaker terminals. The reader need not worry if the primary and secondary leads are not marked. Connecting the transformer each way in turn will soon settle the question, one way increasing the volume, the other greatly
diminishing it. The largest diameter loudspeaker obtainable should be used; it will give the greatest volume and the best tone.
The receiver just described should give pleasing results if built and handled correctly. Regenerative receivers require a little skill to operate but this soon comes with practice, both controls being used in conjunction. When the station required is correctly tuned, it is usual to advance regeneration until oscillation just commences, then to reduce it slightly until normal undistorted reception is obtained with a slight final adjustment of the tuning.

The queer noises which the receiver produces whilst being tuned are quite normal to this type of sel. They can, however, cause annoyance to other listeners if too long an aerial is employed. A modest aerial of a few yards only is therefore suggested for this receiver where other receivers are known to be fairly close.

This marks the end of the series to introduce beginners to the art and science of radio construction, completely without the use of solder.

There is, however, no substitute in the long run for the technique of soldering, and it is to be hoped that having gained some experience and confidence while constructing the three receivers in this series, the constructor will make an effort to learn the technique, and so move on to more ambitious projects.

# Short-wave Listeners' Log-4 ANY USA transmitters beam English trans- <br> stations they tune in are situated. Many amateurs 

Mmissions towards Europe, and these programmes can generally be received well in this country. Numerous frequencies are employed, so if propagation conditions make one band unsatisfactory, other bands will often give good reception. As many of the frequencies fall within the coverage of ordinary all-wave receivers, a special short wave set is not necessary.
Some of the "Voice of America" transmissions which may be tuned in, with times, frequencies, and wavelengths, are listed below. These are generally half-hour programmes, consisting of news followed by announced features. (Greenwich Mean Time is used throughout.)


18:00 (GMT): Generally similar to 17:00 (GMT).
Later in the day the lower frequencies, such as those in the 31 and 49 m bands, will often be well received, while the higher frequencies, in the 13, 19 and 25 m bands will generally give better reception earlier. News in "Special English" may be heard at 19:00 and 20:00 (GMT). This employs a limited vocabulary. "Radio Amateur's Notebook" may be heard at about $21: 15$ (GMT).

The 19,25 , and 31 m bands, at least, will generally be within the tuning coverage of any all-wave receiver. Very good results can often be obtained on these bands.

Listeners who are just becoming interested in Amateur band reception may wish to know where the
all over the world use English, and they have to announce their call signs frequently, when carrying out a contact. As a result, it is usually easy to log quite a number of countries in a short time. Lists of calls may be obtained, but some of the most generally heard calls, with the countries they indicate, are as follows:
DJ, DL and DM, Germany; El, Ireland; F, France; G, England; GI, Northern Ireland; GM, Scotland; GW, Wales; 11,IT1, Italy; OZ, Denmark; VE, VO, Canada; K, W, USA.
Others, less frequently heard, include: $\mathrm{CN} 8, \mathrm{CN} 9$, Morocco; DU, Philippines; GC, Channel Islands; HB, Switzerland; HP, Panama; LA, Norway; OH, Finland; VK, Australia; ZS1 to ZS9, Africa.
When logging such stations, individual call numbers and letters follow the prefix showing the country. For example, G2XYZ, G3ABC, and G3XYZ, etc., would all be in England. Very many stations also give their locality during the course of the transmission and this is a further aid to logging new countries.
As most S.W. listeners will know, reception conditions on the various frequencies vary in approximately a 24 -hour cycle, according to whether the transmission path between station and receiver is in daylight or darkness. For this reason it is wise to check over two or three bands when beginning a period of DX listening. Some frequencies which may have been giving good reception from one part of the world will cease to be usable for that direction, as darkness falls. But at the same time other frequencies will come into use, giving reception from other stations. When conditions are suitable for the band employed, transmissions may be heard over exceedingly great distances, even with the simplest type of receiver.

## WhartedaleTRAMSFORMERS <br>  <br> OP3 (3 ratios) <br> Small output transfor* mer for battery and port able sets or mains sets up to 3 watts output. Ratios 30, 60 and 90 to 1. Max. D.C. 30 mA . Inductance at $4 \mathrm{v} 50 \mathrm{c} / \mathrm{s} .26 \mathrm{H}$ with zero D.C. 3.8 H with 30 mA D.C. Width 2 lin . by height 14 in . Weight 6 oz. Max. watts 3 . <br> TYPE P (4 ratios) <br> The ideal replacement transformer for sets up to 5 watts output. Ratios $30,45,60$ and 90 to 1 ( 90.1 centre tapped) Max. D.C. 50 mA . $\ln$ ductance at $4 \mathrm{v} 50 \mathrm{c} / \mathrm{s}$. 28 H with zero D.C. 6.5 H with 30 mA D.C. 4.0 H with 50 mA D.C. Price $7 / 6$ <br>  Width 2 in. Height $2 i n$. Weight $12 \frac{1}{2}$ oz. Max. watts 5 . Price 9 .



GP8 (8 ratios) General purpose output transformer with two centre-tapped primary windings and two secondaries. Matches practically all output conditions to speakers of 1 to 15 ohms impedance. Suitable for use up to 5 watts autput. Ratios 12,18.24,30,36, 48, 60 and 72 to 1 (ratios 36, 48 and 72 to 1 are centretapped). Max. D,C. 50 mA . Inductance at $10 \mathrm{v} 50 \mathrm{c} / \mathrm{s}$ (each primary winding 22.5 H with zero D.C. 5.0 Hith 30 mA D.C. Width 2 I in. Height 2 in. Weight 12 g oz . Max. watts 5. Price $12 / 6$

W12 (3 ratios-all centre tapped) A high quality transformer for undistorted output up to 10 watts with speakers up to 15 ohms impedance. Ratios: 15:1, 22:1, 45:1.
D.C. resistance of primary 460 ohms .

Max. D.C. 80 mA . Inductance at $4 \mathrm{v} 50 \mathrm{c} / \mathrm{s}$. 61 H with zero D.C. Leakage inductance 200 mH Width 4 g in. Height 3 in . Weight 2 ib . Max. watts 10 . Price 26\% Special ratios to order 30\%-


SMI STEREO MIXER TRANSFORMER Enables stereo systerns to be operated with a single bass unit and two treble speakers. Can also be used to add a centre speaker to "fill in the middle" where existing speakers are too widely spaced. Existing full range speakers can also be converted to stereo using the SM1 and an additional treble unit. Size $4 \times 2$ th in Weight 2 lb . Input 15 watts Max. Price 30/-

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Auto ransformer for matching with $10-16$ ohm or $7-9$ ohm speakers 10 sets with $2-5$ ohnls output or vice versa. Frequency response within 1 dB from $20 \mathrm{c} / \mathrm{s}$ to $15 \mathrm{kc} / \mathrm{s}$. Power handling capacity 15 watts. Can be used to match loudspeakers of different impedances to cross over unit in high-quality two or three speaker systems. Width $2 \frac{4}{4} \mathrm{in}$. Height 27 in .
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FOR ADDRESSES SEE THE OTHER A DVERTISEMENT FOR GLADSTONE RADIO ON PAGE 88I.

# A Simple R-C Bridge 

THIS INSTRUMENT MEASURES COMPONENTS FROM IOS TO IOM, AND FROM IOpF TO $10 \mu$ F.

By A. Guy

ЭHIS unit is simple both in construction and operation, self-contained battery operated, uses only two resistance and two capacitance ranges giving wide coverage, reasonably accurate in use, and can readily be made portable if desired. No special components are required and, with the exception of the bridge standards, the instrument is constructed from parts found in most spares boxes, a choice of valve or transistor oscillator being described.

## The Valve Oscillotor

- The oscillator shown in Fig. 1 follows conventional circuitry and utilizes a $3 S 4$ valve only because this was to hand; a 1S4 or 1 T 4 would use less current and result in longer battery life. Providing that the oscillator is switched off when not in use (a warning light being included for this purpose), the battery will give nearly a year of satisfactory service with normal usage. $\mathrm{A} 67 \frac{1}{2} / 1 \frac{1}{2} \mathrm{~V}$ battery is required to operate the unit.


## The Transistor Oscillator

If a portable bridge is desired, a transistor oscillator provides the answer, and Fig. 2 shows that very


Fig. 1.-This shows a valve oscillator circuit. The valveholder used is a B7G type and " $T$ " is a $3: 1$ interstage transformer.
rew components are required. The transistor can be either one of the surplus "red spot" variety, or a OC71 or similar. The transformer is not critical and almost any interstage transformer will suffice, that used by the writer being a $3: 1$ type salvaged from an old battery amplifier. If midget construction is required a suitable transistor transformer should be obtained.


Fig. 2 (Above).-A transistor oscillator for portable use " $T$ " is a 3:1 interstage transformer.

Fig. 3 (Below).-The two test terminals are marked " $X$ " in this circuit diagram of the bridge. (Cl is $0 \cdot 1 \mu F$ and $C 20.001 \mu F$.)


## The Bridge

Fig. 3 shows the extreme simplicity of the network, the only critical components being R1, R2, C1, and C2. The resistors are 1 per cent tolerance and the capacitors good quality paper types, all checked for accuracy against a bridge by an obliging dealer. The bridge balance potentiometer should not exceed about 50 k , and in the prototype a 20 k was used. It must however be of the linear wire-wound pattern as large as possible. The power factor potentiomete
is also a linear wire-wound type of $500 \Omega$. A 47 k resistor feeds the bridge and is inserted to limit the load on the oscillator and prevent variations in trequency and amplitude.
The "null point" is detected on the original by a single earpiece which, when not in use, is hung on the side of the case by a small hook. This has one disadvantage in that it must be held when using the bridge, but normal headphones may be used if desired, this being entirely a matter of preference by the constructor. High resistance phones must however be used, and if not available, a suitable matching transtormer will be necessary to feed low resistance types; a small loud speaker transformer will serve the purpose adequately.

Tיe switch numbering shown in Fig. 3 indicates the oridge ranges as follows:

Range $1-10 \Omega$ to 100 k .
Range 2-1, to 10 M .
Rang: $5-10 \mathrm{pF}$ to $0 \cdot 1 \mu \mathrm{~F}$.
Rang $4-1000 \mathrm{pF}$ to $10 \mu \mathrm{~F}$.
If desired, and to avoid marking-out two separate scales, a chart to convert pF to $\mu \mathrm{F}$ can be affixed to the side of the case. A number of additional ranges could easily be added if required, but this was considered unnecessary, the ranges obtained having proved satisfactory for general checking purposes.
Switching is very simple and the changeover from resistance to capacitance ranges is effected in one movement.

## Constructron

The instrument can be censtructed in any convenient form and the original was housed in a discarded multi-range meter case measuring 8in. $x$ $4 \frac{1}{2}$ in. $x 2$ in. All components were mounted on the back of the panel and the battery fixed inside of the case. A circular piece of white card was used for the scale which, when calibrated was covered with thin perspex. The pointer was made from a small piece of thicker perspex having a narrow line scribed down its centre by a razor blade, and "blacked in" with pencil. This was screwed to the back of a large tuning knob. Panel lettering was done with a small artist's brush, but the finish of the instrument is left to the constructor.

## Callbration

Calibration is simply a matter of balancing the bridge against a number of resistors and capacitors of known value, using series and parallel arrangements, a little thought showing that about ten components only are needed. If desired the scale can be marked in preferred values, with red or other coloured bands to indicate the limits for each value. The power factor control is calibrated quite simply as shown in Fig. 4, $0-250 \Omega$ indicating a high power factor, and $250-500 \Omega$ a low power factor.

## Use

To check the value of any resistor or capacitor, connect the component under test to the terminals marked " $X$ ", switch to the appropriate range and turn the dial to the null point, when the value can be directly read. If difficulty is experienced in finding the nult point, the power factor control should be rotated clockwise, a reading over the half-way mark indicating a low power factor. When testing resistors and capacitors it is important that they be disconnected at one end from their associated wiring,
otherwise incorrect readings will be obtained. When a component measures out in the overlapping areas of any scale, it is worth taking a reading on both ranges, as the centre portions of each range are more accurate than the extremities.


Fig. 4.-The completed bridge.
No originality is claimed for the design which follows standard circuitry, and providing leads are kept as short as possible, the layout is not in the least critical, any convenient cabinet being suitable. The original instrument using the valve oscillator has been in use for a period of approximately tour years and has been invaluable in the workshop.

## British Standard for Fixed Wire-wound Resistors (B.S.21II: Part I: 1960.)

The latest in a series dealing with components intended primarily for use in telecommunication and allied electronic equipment, this British Standard is divided into two parts, the first (now available) specifying requirements and tests, and the second (to be published later) comprising a list of standard sizes and ratings, for fixed wirewound resistors.

The specification applies to insulated and noninsulated fixed resistors consisting of a winding of resistance wire on a heat-resisting former. and having a dissipation of 70 degC not exceeding 200 W and a rated resistance value not greater than 200 k . Precision wire-wound resistors are excluded from the standard.

Part 1 of the standard requires reference to B.S.2011, "Basic climatic and durability tests for components for radio and allied electronic equipment." The object of the tests is to establish. as far as is possible. in laboratory conditions: the components suitability for use over stated ranges of temperature and humidity. their ability to withstand specified conditions of mechaniçal shock. expected in transit or under operational conditions, and their ability to withstand normal assembly. processes, such as soldering.


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lone waves. Extremely aimple to build Circuit diagram and tull lostructions. 1/6 (free with parcel).


## Expanding Meter Ranges

USING<br>ZENER DIODES WITH VOLTMETERS

$\ell$

By J. B. Dance

T is often necessary to measure a voltage fairly accurately over a limited range of values. Suppose, for example, that it is required 10 measure a voltage which varies between 100 and 120. The normal method would be to use a voltmeter with a full scale deflection of 120 V or more but the part of the meter scale from 0 to 100 V would then be wasted. In order to ohtain the greatest possible accuracy, a meter which reads from 100 to 120 V is required such that this range of voltage occupics the whole of the meter scale.

## Alternative Methods

It would be possible to use a 100 V battery in opposition to the voltage being measured so that the remaining voltage could be measured on a 0 to 20 V meter. Such a method employing a large battery is not convenient and variations in battery voltage would render it very inaccurate. Special meters have been designed for limited ranges. but these would normally have to be specially ordered and would consequently be very expensive.


Fig. 1.-The current-voltage curve of a zener diode.

The zener diode provides an excellent means of removing the unwanted 100 V so that a 0 to 20 voltmeter can be used to give a zero reading at 100 V and a full scale deflection at 120 V . The voltage-current curve of the zener diode is shown in Fig. 1. but when such a diode is employed for expanding meter ranges its properties that produce the reverse of the curve are used.

As the reverse voltage abross a zener dinde increases, the current remains at zero until quite suddenly, at the breakdown voltage, the current rises and the voltage remains constant.

## Range of Diodes

The circuit used is as shown in Fig. 2. The meter and the resistor form a normal voltmeter, but the zener diode has a constant voltage across it irrespective of the current passing through it providing that the voltage is above the breakdown value. Zener diodes with a wide range of breakdown voltages are available and can therefore be used in circuits for the measurement of a few to many hundreds of volts. Several zener diodes can be connected in series, if desired, so as to obtain a higher breakdown voltage. On many types of diodes this is not usually quoted to an accuracy greater than about $\pm 5$ per cent, therefore it is necessary to calibrate the circuit shown in Fig. 2 against a standard voltmeter. Nevertheless it is not necessary to do this if only the changes in voltage, and not the actual voltage must be known accurately.


Fig. 2.-The simple circuit employing a zener diode.

Zener diodes have a maximum current rating which if exceeded causes a large amount of power to be dissipated in the diode which may subsequently be destroyed. This fact must be taken into account when the circuit values are being chosen. The meter used normally has a full scale deffection of between about $100 \mu \mathrm{~A}$ and a few milliamps, but the optimum value depends on the voltage to be measured and the type of zener diode used. If several diodes are used in series, the maximum power dissipation becomes greater, but the largest permissible current is the same as that for a single diode.

The small size and long life of a zener diode make it a very convenient device for fitting inside the case of a meter.

FRIDAY, JANUARY J3th, 1961 A FILM SHOW
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CAXTON HALL, WESTMINSTER at 7-30 p.m.


#### Abstract

A few tickets still remain and may be obtained from our offices. Mark your envelope "Caxton Hall" in the top left-hand corner and enclose a stamped addressed envelope (at least $3 \frac{1}{2} \mathrm{in} . x$ bin.) for the tickets.


The films to be shown are "Conquest of the Atom", "The Invisible Force" and "Particles Count':

#  <br> Club News 

# REPORTS OF CURRENT ACTIVITIES 

CHESTER AND DISTRICT RADIO SOCIETY
Hon. Sec.: A. Bagley, G3JJS, Oak Lea, Long Lane, Saughall, near Chester.
Future Events
January 10th-Annual General Meeting.
January 17th-GW3HEU will give an account of his tour of Germany illustrated by transparencies.
January $241 \mathrm{~h}-$ "My Tx" by G3OPT and G3MGK.
January 31 st-".IThe Uscilloscope" by GW3HEU.
February 14 th-Mr. C. Riche will give a talk on electric motors'
February 21st-Discussion on National Field Day.
February 28th-G3FWV will explain and exhibit a K.W. Vanguard.
All meetings will be held at the Y.M.C.A., The Old Bishop's Palace, Chester, at 8 p.m.

## CHILTERN AMATEUR RADIO CLUB

Hon. Sec.: C. Simpson, 2 Mead Street, High Wycombe, Bucks. The November meeting was a talk given by G2iNZ and the December.meeting, which was held on the 29 th, was entitled "This or That". All interested in any aspect of radio are invited to join.

## CLIFTON AMATEUR RADIO SOCIETY

Hon. Sec.: C. H. Bullivant, G3DIC, 25 St. Fillas Road, London, S.E.6.

Meetings are held on Fridays and Wednesdays at $8 \mathrm{p} . \mathrm{m}$. and on Sundays at 11.30 a.m. Morse Practice is held on Wednesdays.
On November Ilth G30AW iniroduced a quiz on various radio subjects. On December 2nd the club chairman, G3FVG, conducted a Junk Sale and on December 16 th the annual constructional contest was held.

HALIFAX AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: A. Robinson, G3MDW, Candy Cabin. Ogden, Halifax. Future Events:
January I7Lh-Pea and Pie Supper at the Sportsman Inn, Ogden, at 7.30 p.m.

February 7th-Lecture on Transistors by Mr. E. C. Bell, lecturet at the Bradford Technical College.

February 2 Ist-Ragchew Night.
March 7th-National Field Day arrangements,
Meetings are held on the first and third Tuesday of each month at the Sportsman Inn, Ogden.
LIVERPOOL AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: H. James, G3MCN, 448 East Prescot Road, Knotty Ash, Liverpoól 14.

The December meetings included a Film Show on the 6th, a talk by G.3FBH on "Quartz Crystals" on the 13th, and a B.Y.O.B. (Bring Your Own Beer) night on the 20th.

## MEDWAY AMATEUR RADIO SOCIETY

Hon. Sec.: S. W. Nutton, 42 Richmond Road, Gillingham, Kent.
The new headquarters is at Riverside Buildings, Gun Wharf, Chatham, Kent, and meetings are held on alternate Mondays at $7.30 \mathrm{p} . \mathrm{m}$. The club will soon be back on the air with their old call G2FJA. Equipment installations are nearly ready at the club's new headquarters and a grand opening night in the near future is arousing great interest. The new headquarters provide plenty of room for aerial construction.

## NORTHAMPTON SHORT WAVE RADIO CLUB

Hon. Sec.: S. F. Berridge. G3ITW, 20 Ethel Street, Northampton.
Meetings are held at Allen's Pram Works, 8 Duke Street, Northampton. On December 1st twenty members and guests visited the BBC transmitting station at Daventry and tollowing a most interesting tour of inspection under the guidarice ol Mr. D. Pasfield, G5NH. the party was entertained by the BBC (Daventry) Amateur Radio Club, G5XX. Visits to other places of interest are being planned. Working demonstrations of esfuipment have included V.H.F./U.H.F. receivers, a receiver and its associated panoramic adaptor, teleprinter equipment and frequency meter. These demonstrations have been given by Mike Perry, G2ANS. The Club is operational under its call-sign *3GWB on two metres and "Top Band", and work is on hand to fill in the gaps between those two extremes. All senior officers are now licensed amateurs, the former "odd man out", treasurer Stan Haddon, having just received his licence, G3UOJ.

## PLYMOUTH RADIO CLUB

Hon. Sec.: R. Hooper, 2 Chestnut Road, Peverell, Plymoith.
Meetings are held at 7.30 p.m. On Tuesdays at Virginia House Settlement, St. Andrew's Cross. The club may be heard on 80 m and 160 m under the call-sign G3JYB/A.

## READING AMATEUR RADIO CLUB

Hon. Sec.: P. Nash, G3EJA, "Peacehaven'", 9 Holybrook Road, Reading.

Recent meetings have been fairly well attended despite other attractions, and have included "Mobile Operations on Two Metres" by G2AHL and a taped lecture "Two Metres" by G2JU. The December meeting was held at Palmers Hall, West Street, Reading, on December 31st, at 7.30 p.m. and was devoted to the Short Wive Listeners and their queries.
All subscriptions are now due, and the treasurer will be glad to receive them.

Future Event:
January 28th-Election of officers for the coming year followed by a talk on "Low Power Equipment for $2 m$ " by G3ASH and G2BRQ.
ROYAL NAVAL AMATEUR RADIO SOCIETY
Hon. Sec.: H. Matthews, G3JFF, H.M.S. Mercury, Leydene, Petersfield, Hants.
Ahter just over three months since the Inaugural Meeting of the Socisty the membership totals 66 corporate inembers, 6 associate members and 3 junior members.

Membersilip of the socisty is open 10 all serving, or past menbers of the Royal Navy, Royal Matrines, Women's Royal Naval Service, Reserves or Commonwedth Navies. Associate membership is open to civilians who are, or have been, connected with the above services in any way.
The Headquarters Amateur Radio Stations, G3BZU, is regularly on the air on 40 m and the DX hands, and will welcome calls from "Naval Types". The Society has applied for affliation to the Radio Society of Great Britain.

## WEST KENT AMATEUR RADIO SOCIETY

Hon. Sec.: M. R. Richards.
Meetings are held at the Kent Education Committee's Adult Centre, Culverden House in Culverden Park Road, Tunbridge Wells. Meetings commence at 7.45 p.m.

Recent events have included "Getting Going on 2m", Part III; "Transmitters", by G2UJ; "Single Side Band", a 'talk and demonstration by B. Williams. An audio night was held on December 9th and the Christmas party on December 21st.

A morse tape is run from 7.15 to 7.45 p.m. before each meeting for the benefit of members learning the code.

## COURSES OF INSTRUCTION

RISLEY EVENING INSTITUTE
Rowland Hill School, Lordship Lane, Totenham, N.I7. Head of Institute: R. Fiuch, A.F.T. com. Tottenham 2419.

A course entitled "Amateur Radio" is being held at the above institute on Monday evenings from $7.30 \mathrm{p} . \mathrm{m}$. to $9.30 \mathrm{p} . \mathrm{m}$. The Spring term commences on January 9th, 1961. The course is mainly intended to serve as an introduction to Amateur Radio and is not a course for the Radio Amateurs' Examination, atthough if enough interest is shown this later course will be started.

The main emphasis will be on the practical side and it is hoped to have an amateur radio station operating by the end of the spring term. The course is mainly intended for 14-17 age group, but naturally all will be welcomed. Inquiries should be made to J. D. Harris, G3LWM, 2 Lambion Avenue, Watham Cross, Herts.
STREATHAM AND TOOTING EVENING INSTITUTE
H. N. Caley, 6 Farnan Road, Streatham. S.W.16.

Streatham and Tooting Evening Institute announce that Radio and TV classes for beginners will recommence on January 9th, 1961. There is room for a few more enrolments at each of the classes which take place on Mondays, Wednesdays and Fridays at Dunraven, Penwortham and Hillcroft schools respectively. The terms are the same as for other L.C.C. evening classes,

[^3]
## (2)

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## CENERAL COVERAGE RECEIVER

T
THE GC-1U is a portable or fixed station receiver for both the ham and the short-wave listener. It has been designed for good performance and some of its features are a ten transistor circuit, printed circuit board, internal dry battery power supply, telescopic whip antenna, tuning meter and a large slide-rule dial giving a total scale length of approximately 70 in .

To overcome the problems of alignment etc., the R.F. "front-end" of the receiver is supplied as a pre-assembled, wired and aligned unit.

Continuous frequency coverage is provided from $550 \mathrm{kc} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$ in five bands thus enabling world-wide teception. Electrical bandspread on five additional bands covers the amateur frequencies from 80 to 20 m each, the band having a scale length of approximately 8 in . The latest printed circuit techniques are employed and the use of a printed circuit board assists greatly in successful kit assembly and ensures circuit stability and consistent performance.

A 7in. $x 4 i n$. loudspeaker is mounted on a side panel within the cabinet and is automatically disconnected when the phone plug is inserted in the socket.

The GC-1U is housed within a strong steel cabinet finished in stove-enamelled green and it is powered by a 12 V dry battery mounted internally. For static and mobile use a socket is provided for the connection of external power supplies. It is available from Daystrom (Heathkit) Ltd., Gloucester, England.

## NEW PRODUCTS AND DEVELOPMENTS

noise and ensures highly satisfactory performance under adverse acoustic conditions.

For a given feedback level the microphone can he placed at 75 per cent greater distance from the performer than is possible with conventional models.

Of dual-impedance, the "Unidyne III" can be connected direct to a $50-250 \leq 2$ line or high impedance input. It is supplied complete with 18 ft of high quality shielded cable and plug and with an adjustable swivel adaptor which permits instant withdrawal for hand use.

Also available is the Model 544 Series, comprising the "Unidyne III" mounted on a flexible support for fitting to control desks and consoles.

The Model 545 " Unidyne III " Microphone, cost $£ 29$ 15s. J. W. Maunder. 22 Orchard Strcet, London W,I.

## STYLUS PRESSURE GAUGE

A STYLUS pressure gauge is being produced by Garrard Co. Ltd.
The gauge ensures optimum reproduction of all types of gramophone records by providing an accurate means of co-ceting the pressure of the stylus on the record. It accommodates all current pick-up arms and heads, and a swivelling balance lever ensures sensitivity. The gauge is freely adjustable and easy to operate. The Garrard Engineering and Manufacturing Co. Ltd., Swindon, Wilts.

## MOVING COIL MICROPHONE

J.W. MAUNDER, U.K. agent for Shure Brothers Incorporated, announces the release of Model 545 "Unidyne III", a small cardioid dynamic microphone.

A slinder moving-coil microphone only $1 \frac{1}{1}$ in. diameter x 6in. long, the "Unidyne III" provides wide-range reproduction of music and speech whilst the uni-directional characteristic largely overcomes problems of feedback and unwanted

## HIGH TORQUE BATTERY MOTOR

DESIGNED primarily for professiona: tape recorders, this new EMI battery motor (part no. 98170 D ) is also suitable for television camera remote control, and for medical and other scientific uses. This high-grade precision motor is built for long life and exceptional speed regulation over a wide range of load and voltage. A multi-pole armature gives low electrical interference, long brush life and high efficiency and a ball race bearing is incorporated for handling heavy duty side loads. The Gramophone Co. Lid. (Components Division), Hayes, Middlesex.

## MONAURAL RECORD PLAYER

THIS new monaural record player is made by Magnavox and is selling at $19 \frac{1}{2} \mathrm{gns}$. (including purchase tax). The M. 602 "Manhattan" record player incorporates features normally found in instruments selling in a higher price range.

Owing to advanced amplification technique, the "Manhattan" gives freedom from distortion at high volume. This is due to the first-class per-
formance of the 7in. $x$ tin. elliptical wide range unit. The Magnavox standard auto-changer operates at $16 \frac{2}{3}, 33 t .45$ and 78 r.p.m.

There is a crystal turnover cartridge with a 1 mil sapphire stylus for L.P. discs and a 3 mil sapphire stylus for $78{ }^{\prime} \mathrm{s}$. The cabinet features clean-cut contemporary styling. Magnavox, 129 Mount Sireet, London W.I.

## A.M. VHF TRANSISTOR TABLE RADIO

A
NEW 8-transistor A.M./VHF table radio, by Ekco (model BT359), makes everyday family listening independent of the mains supply without involving any undue extra rumning cost.

It is a full-size tahle model measuring $11 \frac{1}{6}$ in. high by $17 \frac{1}{4} \mathrm{im}$. Wide by $6 \frac{1}{\mathrm{in}} \mathrm{in}$. deep and a Class $B$ push-pull output stage delivers up to 1 W into a high-flux ( 10,000 line ) 8in. by Sin. ellipticat speaker. In addition 10 the usual ferrite rod acrial for medium waves. a double folding-rod dipole is provided for VHF reception.

This receiver can provide a standard of performance at least comparable with that of a typical better-class mains receiver while the ahsence of all external connections means that the receiver can be used wherever it is most convenient - without reference to the availability of a mains socket.

An attractive feature of this receiver is the clearly marked runing scale which also carries the two concentric pairs of control knobs and extends to the full width of the cabinet. Controls include luning, wavechange, volume on/off and tone. Waveranges are 185 to 570 m and 85 to $100 \mathrm{Mc} / \mathrm{s}$.

In appearance, the receiver is of modern design, the cabinet is veneered in sapele mahogany and trimmed with silver-colour metal styling bars and a woven plastic speaker grille.

The price of the receiver is 27 gns. ( $£ 21$ 9s. 3d. plus tax £6 17 s .9 d ) and the recommended battery costs $11 /$.

Technically, the receiver makes few concessions to tradition. There are four printed wiring panels, one for the R.F. tuner, one containing the audio frequency circuits, another containing the F.M. intermediate frequency and demodulator circuits and the fourth containing the A.M. frequency-changer, intermediate frequency and demodulator circuits. Between the two latter panels, a slide switch carries three transistors which are switched from one
 panel to the other by the wavechange switch. All three transistors serve as I.F. amplifiers when switched into the F.M. panel, only two of them serving as amplifiers when switched to the A.M. panel, the third then forming
an oscillator/miser. With ample space inside the cabinet. all the printed panels are easily accessible for servicing if required. $E$. K, Cole Lid., Southend-on-Sea, Essex.

## TORCH ATTACHMENT

THE "Chinton Prodlite" can be fitted to any wo-cell electric torch in place of the standard miniature screw bulb.

The diameter of the stalk is only $\frac{1}{6} \mathrm{in}$., or with an insulating sleeve. $\frac{5}{3}$ in. and it contains a specially made ultra-miniature bulb incorporating a lens which difects an intense beam of light wherever required. As the bulb is sheathed within the hollow stalk. it is protected from damage and has a long working life.

For such purposes as inspecting the interior of radio apparatus. the practical value of this device is obvious. It can be obtained with a longer. or a specially shaped stalk. or with a Hexible lead and switch. Incidentally, a 12 V model for motorists and garage service will also be available. The price is $15 / 6$. The Prodlite has been introduced hy the Clinton Laboratory, 43 Broomhall Place. Sheffield 10 .

The "Clinton Prodlite" torch accessory enables areas normally inaccessible to light to be illuminated.


# MAXI-Q TRANSISTORIZED F.M. RATIO DISCRIMINATOR \& I.F. TRANSFORMERS FOR THE HOME CONSTRUCTOR 

## I.F. TRANSFORMER, IFT. 15

A $10.7 \mathrm{Mc} / \mathrm{s}$ double-tuned transformer with tapped secondary and primary windings. Wound on polystyrene former complete with srondust tuning cores and sub-miniature polystyrene foil capacitors. Completely enclosed in an aluminium screening can measuring $7 / 8 \mathrm{in}$. high by $17 / 32 \mathrm{in}$. square with two fixing clips. Termination is made to base mounted silver plated pins which are ideal for either printed circuit board or normal metai chassis mounting.
Bandwidth of single transformer at -6 dbs is approx. $250 \mathrm{kc} / \mathrm{s}$. Unloaded ' Q ' of winding 70.

Price 10/6

## RATIO DISCRIMINATOR TRANSFORMER, RDT. 2



ACTUAL SIZE

A sub-miniature $10.7 \mathrm{Mc} / \mathrm{s}$ transformer for use in ratio discriminator type circuits. Secondary winding is of bifilar construction. Dimensions as IFT. 15.
Peak Separation approximately 220 ke/s.
Connection diagram supplied with each coil.

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## IREADEMS RAMID

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SIA. 4587



The Editor does not necessarily agree with the opinions expressed by his correspondents


#### Abstract

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNAOT UNDERTAKETO ANSWER QUERIES OVERTHE TELEPHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iit of cover.


## LOUDSPEAKER DESIGN

$\mathrm{S}^{1}$IR.- Recent letters have given details of loudspeaker design and problems, but I have not so far seen any mention of some experiments which were carricd out some time ago and according to the reports which I read, foretold great steps in development in the reproduction of sound. I believe that a flame was modulated in some way and that this gave reproduced sound of a very high quality. I have heard nothing further of this. Similarly, the flat plate type of reproducer was hailed as a wonderful new departure in loudspeakers. but also has faded away without any models incorporating it coming on the market. Can anyone tell me if there has been anything new in loudspeaker design in the period since the war? Apart from the fabric cone of certain models it seems to me that the modern loudspeaker is no different from those in use before the war.-F. R. Endell (Bristol).

## WIDE-BAND S.W. TWO

SirR.--I recently finished the set described in the June issue but was very disappointed as it would not work. After some trouble 1 discovered a fault in the wiring in your Fig. 4 and when this was remedied the set responded well. I have had immense pleasure from this little set. and although it was built primarily to give to a young friend. 1 am keeping this for my own use and building another. I was terribly thrilled on the first night's listening by the large number of entertaining stations which could be picked up. and I think that I shall now have to build myself a really good aerial as the scope of this set seems endless-R. T. Burton (Wembley).
[In Fig. 4 on page 128 of the June 1960 issue. the 270 k screen resistor of VI should be connected to H.T.+, as in the circuit diagram.-Ed.]

## TRANSISTOR HOLDERS

SIR,-I have followed your articles and my main interest nowadays is in the transistor. I find. however, that after I have used a transistor three or four times it seems to have worn out. This prompted me to make some enquiries and I finally found that I had in fact more or less ruined the transistors by soldering them into the sets. I would have thought that after the time which these com-
ponents have been on the market. some attempt would have been made to produce a transistor to plug in. just the same as the valve, and it looks to me as though the transistor manufacturer is cashing in on the fact that you have to solder them and therefore you will ruin them and have to buy another. Could not you publish an article on how to fit pins to the base (with a minimum risk of damage) and how to make sockets to take them. I am sure this would be welcomed by all. and could be done without making them any larger.-E. M. Krfle (Reading).

## PLAYING A RECORD BACKWARDS

SIR.-During Christmas I saw a stunt carried out by a radio enthusiast which has me guessing. First of all he showed us how to play a gramophone record backwards. hy putting it on a pencil and letting its edge rest against the edge of the turntable. Whilst we appreciated the "stunt" (it was quite good as a sort of party game to try and guess the artiste. and was really funny to listen to) he then astounded us by playing a tape recording hackwards. I know a little about tape recording, but cannot see how he managed this, as it would not be sufficient just to turn the tape over. What has to be clone so fatr as 1 can see it is to turn the tape " inside out backwards."-just turning it over will not give the same effect. Perhaps some ingenious reader has ideas on this and could let us have the "know-how".-F. Keating (S.W.5).

## tAG BOARDS

SIR.-The modern set is a masterpicce of "juggling ". the many components having to he placed in awkward positions. and. the wiring made intricate. unless some special procedure is adopted. 1 some time ago took to using tag boards to simplify construction. making a drawing and mounting all the components required on the tag hoards. which result in only the connecting wires from the edges of the boards to the valveholders having to be made to complete the set. I believe it is now possible to obtain valveholders in which à step further in this direction has been made in the U.S.A. and an extension of the valveholder base is made so that all the items associated with the valve may be mounted actually on the holder. Thus all the wiring to the valveholder may be made before it is mounted on the chassis, and this would surely greatly simplify construction. as well as making it much casier to ensure that there were no bad connections to a component which is very inaccessible when the same is completed. Does anyone know of this type of valveholder and whether it is available in this country? - H . Neville (Bournemouth).

## MODULATION

SIR.-Witl reference to Mr J. R. Millers letter printed in the January issue, concerning modulation at low power in the VFO modulation in the oscillator stages is certainly practicable and was popular with amateurs in the early days of high-cost power values when any economy not incurring too many disadvantages was given serious consideration.

The main falt with this method is that in modulating the oscillator on grid. screen or anode, a current change must occul and a corresponding voltage variation. Thus in turn reduces stability. frequency modulation occurring with consequent reduction of quality.

Now that cheap valves for power amplifier and modulator output stages are available e.g., the ubiquitous 807 type mentioned, it is surely worth the extra outlay to obtain the stability necessary for modern amateur operation on crowded bands such as 40 m .

In reply to Mr. Miller's other query, it is possible to run 120 W unnodulated R.F. from two 807's in parallel.

In the same issue Mr. E. Haines relers to Radio Luxembourg as having "hardly enough power to bridge the ether"! It would seem to me that the 350 kW output radiates efficiently enough for have beard the station with consistency whilst residing in Orkney. This was at a distance of roughly 800 miles and still $S^{9}+$. R. A. White (Sevenoaks, Kent)

## PUSH-PULL AMPLIFIER

SIR,-In reply to Mr. Haskell's request January issue) for the value of separate cathode resistors for two EL84 s in push-pull, I can inform him that the value will depend upon the loading of the output stages.

For normal loading. the value will be 270 for each resistor, and for low loading it will be $437 \Omega$ (i.e., $390 \Omega+47 \Omega$ ). The latter mode of operation will give a reduced distortion level, approvimating the conditions of fived bias. although the former arrangement also works admirably.-R.J. Burg (East Ham, E.16).

## SHORT WAVE LISTENING

SIR - With reference to Mr. F. N. H.'s letter that appeared in your December 1960 issuc. I would also like to remark on such interesting reception. For, on the afternoon and early evening of November 27th I received on the 10 and 15 m amateur bands large numbers of U.S. and Canadian amateurs as well as stations in Central America. Hawaii and Alaska. The receiver used was a 7 valve superher and an R.F. 24 pre-selector-1. K. Gukney (Chalfom St. Peicr, Bucks.)

## INTERFERENCE

$S^{1 R}$,-Reading the December 1960 issue of Practical Wireless, section "Letters to the Editor"."I came across a sub-heading "Interference".

The explanation for this type of interference is commonly known as the Luvemburg effect. This phenomenon has been the object of much investigation. and an explanation of it was first given by
two Australian physicists. Batey and Martyn. They showed how a powerful low frequency station could affect the ionosphere in such a way that any other waves deflected from the aflected region would acquire a modulation from the unwanted power station.

The only cure for this unfortunate mixing of Hansmissions would appear to be a reduction of a proportion of the skyline.

Under the action of a powerful electric field, such as a powerful transmitting sation, the motion of the elections does not follow a linear law. It is possible to make ase of this non-linear characteristic in the way which one does when employing grid modulation by a process resembling the later. The waves of the distant station passing through the alea of the powerful electric field have a modulation from the later impressed on them. E. S. Jacobson ZS6ATQ (Bratpan, South Africa).

## CRYSTALS

SIR.-What has happened to the old-fashioned crystals which we uscd in carlier days as a detector? The various circuits which I have tried lately have not proved very thrilling, in spite of the exchange of silicon diodes and transistors, and 1 wanted to try a diode arrangement with a piece of the old Galena or Hertzite, but when I asked at the shop the dealer said he had never heard of them. Why not? I leel convinced that they are more sensitive than the modern conponents when once a suitable sensitive point has been found. and perhaps one of your readers hnows a source of supply-T. L. Mence (N.W.)

## A.C.D.C. EQUIPMENT

$\mathrm{S}^{\prime}$IR,-I hnow there has been a long controversy about the merits and demerits of apparatus wired to what has become known as the A.C./D.C. lechnique. but there is one point which I do not think I have seen touched upon. What ahout hum? In a properly wired A.C. set. the heater wiring will be continuous on both pins. with the wires lwisted tightly and run close to the chassis, thus ensuring that ally A.C. field surrounding those wires will be so small as to be negligible. thereby avoiding the ejection of A.C. (hum) into other wires. In it set where the heaters are all wired in series. there is usually one single wire running all round the chassis, radiating. in my opinion, quite a considerable A.C. Field which is bound to make its presence felt at one point or another. The purists may argue that the tranformer gives a larger field, but it is possible to obtain totally shrouded transtormers. and I am convinced many of the troubles of the set wired "A.C.D.C." are dite to the A.C. bearing wires. - H. Frinks (Belmont).

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