

## SERVICING-PROJECTS•VIDEO-DEVELOPMENTS



Servicing the Panasonic NV777/788 Fault Finding in EW Modulators Simple Satellite Sound Adaptor DX-TVoCD Player Fault Reports Servicing TDA4600 Chopper PSUs TV Fault Finding•VCR Clinic



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November
1991

Vol. 42, No. 1<br>Issue 493

## On sale October 16th

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## QUERIES

We regret that we cannot answer technical queries over the telephone nor supply service sheets. We will endeavour to assist readers who have queries relating to articles published in Television, but we cannot offer advice on modifications to published designs nor comment on alternative ways of using them.

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OUR NEXT ISSUE DATED DECEMBER WILL
BE PUBLISHED ON NOVEMBER 13




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$\begin{array}{ll}\text { Hyper VHF: } & 300-470 \mathrm{MHz} \\ \text { VHF }: & 470-862 \mathrm{MHz}\end{array}$
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## SUBSCRIPTION <br> ENQUIRIES

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## COVER PHOTO

This month's cover photograph shows a Panasonic NV777 VCR with the covers removed. See servicing article on page $2 x$.

## What did you tape last night?

Despite the lact that the VCR has been a standard item of domestic equipment for many years now little was known about owners use of their machines for time-shifting until recently, when BARB (the Broadeasters' Audience Research Board) started to check on playback viewing. Since the ability to time-shift programmes is one of the basic advantages provided by the VCR, it's surprising to tind how little use is made of it. BARB's research reveals that there is now measurable taping with four out of five networked programmes. while only one per eent of UK viewers appear to make use of the time-shift facility. In the four weeks to September lst only eleven programmes had playback audiences that execeded ano.(x)( ) They included three movies and tive episodes of Coronation Street. Tinne-shifting added about two per cent to the various networks viewers, which works out at about half an hour a week per viewer. The terrestrial channels and satellite TV attract what time-shifting there is evenly. tilms and soaps being the main items that are time-shitied. The public is certainly being rather unenterprising in its use of the VCR. Is this possibly to do with the problems that so many people have in setting their timers? Or is it that so many people simply switch on and watch what comes? Whatever the answer is, it appears that VCRs are used atmost entirely for viewing bought/hired tapes. This being so it's strange that playbackonly machines never caught on. Perhaps the price differential was not enough to make such machines an attractive proposition. This unimaginative use of video could be bad news for the prospects of CD-I and CD-TV as mass-market products.

## At the Funkausstellung

The main interest at the 1991 Berlin Consumer Electronics Show was HD-TV and these 16:9 aspect-ratio sets. HD-TV will not be with us for some years, as the authorities and broadasters continue to argue about what standard to adopt. But those expensive $16: 9$ sets are due to start appearing in the shops any day now - though in very small quantities at first. It seems that the public showed little interest in 16.9 TV at the Funkausstellung. Is this so surprising? To this observer at least, the $16: 9$ sereen looks not so much a larger one as a screen with the top and hottom chopped off. A small, shall we say slim-tine, screen inf fact. If this is the public's perception of wide-screen TV, it's future must be in some doubt. Japanese manufacturers seem to be taking to the $16: 9$ format however - a number of working $16: 9$ cameorders were on show

At a special press presentation Thomson showed a prototype HD-MAC decoder the size of a standard VCR. The company is developing a set of eleven chips to reduce the size of the decoder. It will use SGS-Thomson (1.8 micron technology and should be available to setmakers by late 1993, at a price of around $£ 1$ ( $\mathcal{M}$ ()). By 1997 a futher chip set using $(1) .5$ micron technology should be available, enabling a decoder to be fitted into a $16: 9$ receiver nearly.

## Faraday

Last month saw, on September 22nd, the two hundredth anniversary of the birth of Michael Faraday who. amongst many other things, discovered the principle of the electric generator and motor. His father was a blacksmith who died when Faraday was thirteen. He was thus forced to leave school and seek work, taking up an apprenticeship with a bookbinder. The crucial break came when, at 22, he was hired by Sir Humphry Davy, director of the Royal Institution of Great Britain and famed as the inventor of the miner's lamp. At this time Faraday was self-taught and without any qualifications: he was within a few years to become Britain's foremost analytical chemist however. An early discovery was stainless steel - the rustless razor. In 1820, at the age of 29, he read of the discovery that a wire carrying an electric current would deflect the needle of a compass. His subseguent work in this field led him, in 1831, to lay down the laws of electromagnetic induction. Three vears later he discovered the laws of electrolysis, which led to the electroplating industry. Ten years after that he linked magnetism and light, showing that a magnetic field could rotate the plane of polarisation of a light heam - the Faraday effect. These and other innovative work were great achievements: just how do you achieve sueh suecesses with so few elues? It seems that it was through a long process of patient research - observation and experimentation. That he managed it all with negligible mathematic knowledge might perhaps give those of us who always falter when it comes to maths just a little reassurance.

## Equivalents

Following an appeal to readers earlier this year we were able to publish a number of VCR and TV equivalents lists. While they covered a lot of ground there's much additional information of this sort that would be helpful to readers. Comprehensive equivalents lists for TV sets/chassis and video equipment have been published by Mauritron Technieal Services, 8 Cherry Tree Road, Chinnor. Oxfordshire OX9 4OY and Technical Information Services, 76 Church Street. Larkhall. Lanarkshire ML9 IHE

## The BBC Debate

The Home Secretary Kenneth Baker intends to produce next year a discussion paper setting out various possible options for the future of the BBC, whose Royal Charter runs out in 1996. The declared aim is to consult with the public and to look into all aspects of the services provided by the BBC, its finances and how it should operate. In an address to the Royal Television Society Mr. Baker commented that "there is clearly a role for public service broadaisting, but that role will have to be defined more explicitly". Since the role of the BBC is perfectly clear, one can't help suspecting that what he really meams is that it should be curtailed. There are danger signals ahead.

## The Video Bench

Steve Beeching, T.Eng.

We find that communications with dealers are poor at the best of times. Some of them could do with a kick up the backside for assuming that engineers are psychic. Telepathetic, yes possibly, but not psychic.

## A Couple of Nicam VCRs

The fault report with a JVC HRD860 Nicam/hi-fi sound VCR that came in the other day read "audio E-E fault". Neither Darron nor I could find an audio fault, so we contacted the dealer. His engineer explained that it was a peculiar audio fault that sounded a bit like an echo and was somewhat "ambient" - like talking with one's head in a bucket.

No fault was found until some time later when we were wandering through the audio selector switches. The hifi/normal/mix button selects hi-fi left and right or normal or both. What's more on this model it functions with E-E monitoring as well as during playback. Demodulated Nicam audio and normal f.m. are mixed, the "ambient effect" being due to the time difference between the two channels.

Another HRD860 came in with a definite Nicam fault. The audio was very distorted, with a lot of background hiss. It sounded like an off-tune m.w. radio receiver.

No fault with the data or clock signals could be seen and all the crystal frequencies were correct. The DA converter


Fig. 1: Expander chip waveforms, JVC Model HRD860.


Fig. 2: Simplified circuit to show the cause of the problem with a JVC Model HRD500.
chip was replaced, but this made no difference. As I had to get the machine back to the dealer, a new panel was fitted and aligned.

When a bit of time was available later that month a more detailed investigation led me to the expander chip. Its inputs and outputs were checked with the scope locked to the $L / R$ switching signal. Fig. I shows the input, the $L / R$ switching and the correct and incorrect output waveforms. The data signal starts at the right-hand side of its "window" and moves to the left with increasing volume. On average the audio leaves the data about half way through. The output from the faulty expander filled the window however. As a result the DA converter was overloaded. It was the expander chip that was faulty of course.

## HRD500 Power Fault

A peculiar problem with a JVC HRD500 had Darron perplexed for some time. Replacement of the timer/display PCB had been requested. The symptoms were a dim display with R5, a fusible $220 \Omega$ resistor in the -30 V power supply, going open-circuit. Damage was also sustained by the 10 V zener diode D 16 in the timer and tuning memory circuit and the -30 V supply regulator transistor QI. The dealer and Darron had replaced these items.

The problem and the failures suggested a severe overload on the -30 V supply. Since D16 is linked to the display the latter could have been at fault. After fitting three or four more fusible $220 \Omega$ resistors, a couple of zener diodes, a new memory chip and a replacement display we were getting nowhere.

On one occasion the machine ran all right for a whole day - until we reassembled the power unit in the VCR, when the display dimmed and another 2202 resistor went open-circuit. Ah, I hadn't mentioned that the fault was intermittent, had I? It's so common these days that I forget.

We made a small drawing of the power supply circuit, see Fig. 2, in order to try to make sense of the situation. It was soon obvious that for D16 to be involved the loading had to be in the fluorescent display, but this had been replaced. A d.c. resistance check then showed that the a.c. supply for the filament, normally a high-resistance path, measured $40 \Omega 2$ to chassis when the power unit was moved. The cause of the trouble was a faulty mains transformer, a new one providing a complete cure.

Had the dealer managed to obtain a complete (and expensive) timer/display PCB from JVC it wouldn't have helped!

## A Two-speed Model

A dual-speed JVC VCR came in because there were noise bars insteal of thin lines in the cue and review modes. The dealer's engineers had replaced a chip in the f.m. preamplifier section but this hadn't helped.

We quickly traced the cause of the problem to a nonoperational LP video head which produced noise instead of an f.m. carrier. It would have been casy to assume that the output from the head was f.m., except that the envelope didn't vary when the tracking was altered by judicious application of a finger to the head drum.

The heads had been changed previously because of a hifi audio fault. Unfortunately we had to fit another new drum to prove that the heads weren't defective. The cause of the elusive fault was in the lower drum: a new assembly and alignment put matters right. I didn't delve into what exactly had failed however.

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## A Look at Chopper Power Supplies

J. LeJeune

In my youth it was my lot to have to design chopper power supplies for use with cable TV systems. Ah well, everyone has some cross to bear! The basic idea of the switch-mode power supply, to give the arrangement its correct name, is a good one. In a "conventional" multi-voltage power supply, especially where some current demands are over 250 mA , a lot of power is lost and consequently heat is generated where voltages are dropped using large power resistors. A series regulator is also wasteful in terms of dissipation.

Switch-mode power supplies of recent design have all been of the shunt type, with a transformer used to provide from individual windings the raits required in the equipment. Each winding can be optimised for the load it has to supply, and atl the windings are interlocked by tight coupling to the core of the transformer. This arrangement provides regulation of all the supplies derived from the transformer in one go, and can also be used to provide mains isolation.

## Cable Network Supplies

With a cable TV network the repeater amplifiers are powered via the signal-carrying coaxial cable. A static regulator at each amplifier is inefficient, and the number of repeaters that can be powered from any one point is seriously reduced when static regulators are used. Say the repeaters require a 20 V supply. A 65 V d.c. supply can be sent with the signal via the cable and quite a large voltage drop can be tolerated before the regulation with repeaters at the extremities of the system suffers. Use of a simple passive regulator will throw away 45 V at say 200 mA , resulting in a loss of 9 W . In addition to this disadvantage it's not a good idea to use d.c. with cable networks because electrolysis at connectors results in high corrosion rates. So 65 V a.c. is used with on-board rectification. This gives us $65 \times 1.4=91 V$ d.c. to play with. Conventional 50 Hz transformers with an input voltage selector at the primary and low-voltage secondaries can of course be used with such a system. But switch-mode power supplies with their high efficiency are more advantageous. Fewer injection points are needed, with a cost saving, and no input voltage selection is necessary. There's also a weight saving, which is important with equipment that has to be mounted on walls or up poles. This weight saving is brought about by the use of ferrite-cored transformers, which can be employed with the h.f. operation of a switch-mode power supply - the transformers are also smaller.

## Basic Series Chopper Circuit

Early switch-mode power supply designs used in TV chassis such as the Thorn $3000 / 3500$ were of the series type, supplying a single stabilised output. If other, lower, voltages were required they hatd to be "dropped" from the stabilised line (see Fig. 1). This defeated the primary usefulness of the system, so the series-type chopper power supply soon ceased to be used where more than one stabilised rail was needed.

We'll briefly outline the operation of the arrangement shown in Fig. 1. Chopper transistor Trl is switched on and off by a variable mark-space ratio squarewave drive
waveform. When the load increases, the output voltage will tend to fall. This is sensed by the comparator, which adjusts the chopper drive. Trl is thus switched on for a longer period during its on/off cycle, increasing the supply to the load. Inductor LI acts as the energy reservoir for the system. When Tr l is switched off, the voltage at its emitter swings negatively and the efficiency diode DI conducts. This clamps the feed end of L1 at chassis potential and the stored energy supplies the load.

## Shunt Circuit with TDA4600

In a TV set several rails with widely different voltage and power requirements have to be provided. These can be supplied by a shunt-mode chopper circuit. As an example we'll consider the very common arrangement based on the TDA460) control chip: Fig. 2 shows the circuit as used in the Mark III version of the Ferguson TX9 chassis.

The mains input is fed to a standard bridge rectifier (D62-5) which produces some 350 ) V across its reservoir capacitor C140. This supply feeds the primary winding of the chopper transformer Tl . The earthy end of this winding is connected to chassis via the chopper transistor Tr62. Drive for the base of $\operatorname{Tr} 62$ is provided by the TDA 4600 chip IC57. As Tr62 is switehed on and off, so the d.c. supplied to the primary of the transformer is chopped. This chopped d.c. looks like a.c. to the transformer, and a simple transformation from the primary to the secondary windings provides, after rectification, the stabilised output rails. One might be tempted to accept this simplistic view as being all there is to switch-mode power supply operation. If only it was that simple!

The cycle of events is rather more complicated. When Tr62 is switched on, current flows in the primary winding of T1. Because Tr62's load is inductive, the current flowing in the primary winding will rise relatively slowly. not instantaneously as it would if the load was resistive. The reason for this is that the transformer's core will be magnetised as current flows in the primary winding. Because the flux is changing (increasing), an opposing current is set up. The net result is the production of a current ramp waveform. As the current increases, so does the flux in the core. If this was to continue unchecked the core would eventually saturate. Before this happens Tr62 is switched off, interrupting the current flow. With nothing to maintain it, the flux now collapses quickly, producing a reverse current flow in the windings coupled to the core. As a result $\mathrm{D} 67, \mathrm{D} 69, \mathrm{D} 70$ and D 71 conduct, charging their respective reservoir capacitors. $\operatorname{Tr} 62$ is subsequently


Fig. 1: Basic series chopper arrangement, which provides a single stabilised output.


Fig. 2: The shunt chopper circuit with TDA4600 control chip used in the Ferguson TX9 Mk. III chassis.
switched on again by the chip and the cycle is repeated. IC57 controls the on/off switching cycle by sensing the transformer's output and the a.c. conditions within it.

At switch-on there's no supply from D67 at the chip's supply pin 9. To get things going D 66 charges C 150 from the mains supply via R163. Because of R163, the voltage across C150 rises slowly. When the voltage at pin 9 of the chip rises to 7.5 V . short pulses are delivered to the base of Trg2 so that it conducts briefly once each cycle. The object of this exercise is to provide a supply for D67, which conducts to increase the voltage across C150. When this voltage reaches 12.5 V D66 is reverse biased, IC57 has its normal operating voltage and the chopper supply is fully operational. In other words a soft-start action has been provided.

Regulation depends on the voltage at 3 of IC57. An internal voltage regulator produces a reference voltage of $4 \cdot 2 \mathrm{~V}$ at pin 1 , which is linked to pin 3 via R168 and R169. The winding between pins 3 and 4 of the transformer provides feedback for regulation purposes. D(9) rectifies the output from the feedback winding, developing across C144 a negative voltage that's proportional to the power supply outputs. This voltage is fed to pin 3 of the chip via RV171 and R170, backing off the positive voltage from pin 1. The resultant voltage, about $2 \cdot 1 \mathrm{~V}$, is sensed by the logic in the chip and is used to adjust the conduction time of Tr62. As an example, if the output from Tl is excessive D69 will provide a greater negative potential across C144 and the internal logic will shorten the on time of $\operatorname{Tr} 62$ accordingly.

Pin 2 of the chip receives an a.c. input from the same reference winding, via R172/3. This pin feeds a zerocrossing detector which senses the point at which the feedhack waveform passes through zero. The significance of this relates to the fact that D70/71 conduct when $\operatorname{Tr} 62$
switches off, transferring the energy stored in Tl to the load. As the flux in T1 collapses, the feedback waveform passes through zero. This is the point at which Trfi2 must be switched on again. The zero-crossing detector tells the control logic in the chip to do this.

The supply's frequency of operation is not locked to the line frequency. In normal service it free runs at between $18-23 \mathrm{kHz}$.

Whilst $\operatorname{Tr} 62$ is conductive pin 4 of IC57 is open-circuit. C138 then charges from the 350 V rail via R165. When Tr 62 is cut off by the drive at pin 7, pin 4 is earthed and C138 is discharged. Thus there's a sawtooth waveform at pin 4. This serves two purposes. Since $\operatorname{Tr} 62$ is a power device it has a low current gain in the region of 20-30. As Tre2's collector current increases, its gain falls and a greater base drive is required to hold it saturated. This is achieved by using the rising ramp voltage at pin 4 , after amplification, to provide a rising current drive ramp at pin 8 . In addition, protection in the event of an overload on one of Tl 's secondaries is achieved by sensing the amplitude of the ramp waveform at pin 4: should its peak-to-peak amplitude reach 4 V the control logic reduces the width of the drive pulse at pin 8 . A short-circuit across the 115 V line will reduce the base drive on/off time further.

## Fault Finding

Thus the time-constant of C138 and R165 determines the maximum current passed by the chopper transistor. Should the value of either of these components alter. Tr 62 could be subjected to a current overload. This sort of trouble can occur when an unsuitable type of resistor is used in the R165 position: it should be a metal-glaze resistor with a working voltage of 500 V . In many designs two resistors in series are used in this position. R166 at
pin 8 sets Tr62's maximum base drive current. Problems have been experienced with this small wirewound component - check it should $\operatorname{Tr} 62$ fail for no apparent reason.

Failure of $\operatorname{Tr} 62$ is usuatly catastiophic, as a result of punch-through between its collector and base. Thus 350 V appears at pins 7 and 8 of the chip which dies. C1.37 generally suffers and R164 and D104 will also be damaged.

When repairing a power supply that's been damaged in this way it's as well to check that the base drive from the chip is o.k. before replacing Tr62 and applying the mains supply. Use a 4.5 V battery to simulate the action of the transformer's reference winding - connect its positive terminal to chassis and its negative terminat to the anode of D 69 . Then use a bench power supply to provide 12 V at pin 9 of the chip. A short train of pulses should be seen at pin 8 as the chip tries to get $\operatorname{Tr} 62$ going. The putses will not be present for long as there's no zero-crossing information at pin 2 - the chip thinks the start-up has been aborted, which of course it has.

Though IC57 provides comprehensive protection this is insufficient to prevent destruction of Tr 62 when components in its collector circuit are defective. The snubber capacitor C136 is included to delay Tr62's collector voltage rise time at switch off, thus reducing the dissipation in Tr62. Should the value of Cl 36 change or Tl have shorted
turns $\operatorname{Tr} 62$ will be rapidly destroyed, with the previously mentioned trail of destruction amongst its base circuit components. C 136 and Tl are best checked by substitution. It can be expensive in terms of silicon to track down failure here.

## Hum Cancellation

Hum reduction is a feature of most switch-mode power supplies. With the circuit shown in Fig. 2, any ripple on the 350 V line will be reflected in the d.c. feedback to pin 3 . Thus the mark-space ratio of the chopper transistor's base drive waveform will be modulated to compensate. Connecting pin 5 to chassis gives remote control standby operation.

## Safety

A final wort about safety. Since the d.e. supplied to a chopper circuit is usually derived from a bridge rectitier connected directly across the mains input, it follows that circuitry on the primary side of the chopper transformer is at peak mains potential. Thus care should be exercised when fault-finding and carrying out repairs. An isolation transformer helps, but there are still some hefty voltages present at considerable power.

## A Neptune 171

John C. Priest

One of these 12 in . monochrome portables, of East European origin, came in recently with the complaint that it went off after a quarter of an hour. When we put it on the bench and switched it on we immediately got a picture and sound. Half an hour later it showed no sign of going off, so we put it on one side to play to itself while more urgent (and profitable) matters were dealt with. It ran quite happily without fault for three days. I was considering the possibility of a faulty mains socket when the picture and sound went, leaving a slightly noisy raster.

## Test Procedure

By the time the back had been removed the fault had of course cleared. So after spending a short while checking for dry-joints in the area of the tuner and its 30 V supply the set was once more put to one side. Some time later I noticed that the screen had blacked out. Turning up the volume showed that the sound was still present, so attention was turned to the line output and driver stages. The main semiconductor devices here were first checked and found to be o.k. Then the line output transformer was checked for continuity of the windings and dry-joints. Everything was in order.

Voltage checks showed that the 10.9 V I.t. supply was not present at the collector of the line output transistor though it was present at the anode of the efficiency diode D40G. This diode had measured o.k. both in circuit and out, but a replacement brought the set back to life. The original had rather smeary markings which were difficult to make out, possibly DYP-071 350R. Anyway, a BY223 fitted the heatsink and print and as this device stands up to the demands of the Philips Gll chassis we felt that it should be all right in a small mono portable TV set.

While tracing the cause of ne fault we had established
that the TBA950 sync/line generator chip U251 was producing a line-frequency squarewave output at pin 2. When the raster was restored however there was a distinct lack of line sync. We found that the sync waveform from the labelled pin of the i.f. module was not present at the TBA950 end of the series resistor. All the chips in this set have sockets, so the quickest check was simply to plug in a new TBA950. Fortunately this cleared the fault. The original trouble about which the customer had complained, the loss of signals, turned out to be due to a lazy BF970 oscillator transistor in the tuner.

## Background Information

This is a solidly built little portable. Its robust PCB is held in a metal frame that slides horizontally into the black, wedge-shaped cabinet. The simple 1.t. bridge rectifier plus series regulator power supply is fed from a substantial mains transformer that's mounted in the middle of the PCB and supported by two screws through the bottom of the cabinet. The u.h.f. tuner and i.f. module are mounted to the right of the chassis, the line output transformer is to the left, the six-position channel selector switch unit is along the front left-hand edge of the chassis while the tuning potentiometers are in the centre, behind a small flap. The contrast, brightness and volume/on-off rotary controls are to the right. Component layout is uncluttered and the circuitry uncomplicated, so repair of these sets should present no problems.

The set that came in was less than a year old. A few years ago a couple of imported sets with a similar chassis but with a mechanical u.h.f. tuner and the controls mounted at the top of the white cabinet came in. They were of Czechoslovakian manufacture, but this latest set gave no che as to its origin other than a couple of production labels inside with Cyrillic seript - all the other markings were in English.

You will probably meet a number of similar sets sold, under various names, by mail-order companies, minimarkets and discount shops.

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## Teletopics

## VIDEOPHONES

Could the videophone, enabling catlers to see each other, become one of the next mass-selling consumer electronic products? Quite possibly, since Amstrad aims to start selling videophones by September 1992. The price will be all important of course - at this stage Amstrad is unwilling to suggest a firm figure but something in the $£ 250$ to $£ 500$ range seems likely. Development is being undertaken by Amstrad in conjunction with GEC Marconi, who will be responsible for the data-compression system used. The units will have an in-built camera and a flip-up, $3 \times 4 \mathrm{in}$. colour display. They will work via an ordinary telephone socket, providing "extremely acceptable" picture quality.

BT has estimated that by 1995 the European videophone market will be worth $£ 1.7 b n$ a year. It has developed prototype videophones for use with integrated services digital networks (ISDNs) - BT charges $£ 401$ ) to instal an ISDN socket and an annual rental of $£ 360$. This should ensure a higher quality picture than with an ordinary telephone line. The units have a $9 \times 4 \mathrm{in}$. display with a 4 in . built-in camera above. Price could be anything from $£ 2$, ()() to $£ 5,000$, but is expected to fall dramatically as the service develops. Possible features include a switch to give selfviewing and another to remove viewing access.

Various other phone/video products have been developed by BT. One is a PCB for slotting into a personal computer. This, with an associated, separate camera, would result in much improved picture quality using the computer's monitor. Another is videophone multipoint, which would enable a number of videophones linked via a $64 \mathrm{kbit} / \mathrm{sec}$ line to be used simultaneously for group discussions etc. So that the speaker is in view, the cameras are voice-operated.

The Cable Television Association reports that cable TV companies throughout the UK are connecting in the region of two thousand telephone lines a month and that the figure is accelerating. The number of telephone lines linked via cable TV networks now stands at over 11,500. A report by CIT Research suggests that by the year 2000 $700,0(0)$ households and 100,000 businesses in the UK will take their telephone lines via cable TV networks, representing ten per cent of the telecommunications market with revenues of some $£ 1.35$ bn a year.

## CHANNEL 5

ITC engineers have been investigating the possible Channel 5 coverage and the implications of the new channel for domestic video equipment. It's expected that subject to international clearance six additional transmitting sites will be used, bringing the total to 31 . Coverage would be increased to 73 per cent of the population and many localities would be able to have local programming. Under the terms of the 1990 Broadcasting Act, the Channel 5 operator will be responsible for retuning equipment affected by the Chamel 5 transmissions. It's expected that some 2.4 m VCRs will have to be retuned.

## TRADE NEWS

Annual UK production of TV sets by Japanese manufacturers is expected to reach 4 m this year and rise to 6.8 m in 1995 . VCR production is expected to rise from
1.7 m this year to 2.9 m in 1995 . Last year the UK had a TV receiver trade surplus of $£ 271 \mathrm{~m}$.

Thomson Consumer Electronics has received an order for $30,0(0)$ BBC Select decoders. Production of Thomson's cheaper VCRs is to be moved from Berlin to Singapore (see Singapore Briefing, page 882 last month). TCE plans to open a new plant fer the production of up-market VCRs in Germany later next year. As with the Berlin plant, which will now produce exclusively for JVC, the new plant will be a joint venture with JVC.

Philips has signed pretiminary DCC technology licensing agreements with Sanyo, Sharp, Yamaha and Tandy.

Wizard Distributors, Empress Street Works, Empress Street, Manchester M169EN (telephone 061872 5438) has been appointed official distributor of spares for Loewe Opta products to trade customers throughout the UK. A similar agreement has been reached with Sakura Ltd. for the supply of satellite receiver components. Wizard has also added computer spares to the range of parts available for Schneider equipment.

NEBS has introduced a new two-part form to simplify service and repair paperwork. It acts as an invoice and customer receipt and enables a record of work done/required and parts supplied etc. to be kept clearly. There are also service call cards. These well laid out forms could be very helpful for smaller firms. For details contact NEBS Business Stationary, Sovereign Way, Chester West Park, Chester CHI 4QU (telephone (0244390)222).

## VIDEO STILL CAMERA SYSTEMS

Fuji has developed, mainly for professional use, a still video camera system that records $2140(1,0(1)$-pixel images on an 8Mbit memory card, using data-compression technology. The card can be plugged into a computer workstation where the images can be manipulated. Fuji admits that the resolution is not up to conventional photographic quality but points out that it is adequate for many commercial applications, such as desk-top publishing, and has the advantage of image processing flexibility. The data-compression chips were developed jointly by Fuji and Toshiba. Images can also be printed, displayed on a TV sereen or transmitted over an ISD network. The camera is due to be launched next year in the Japanese and North American markets at an equivalent price of around $£ 2.875$. Fuji intends to pursue a five-ten year programme of further development.

Canon is to set up a High Street print service for users of its Ion dise still video cameras. It hopes that at least a hundred outlets in the UK will be able to provide the service by the end of next year. The cameras have not sold well to date - some 3,500 have been bought in the UK. They store up to fifty images on a 2 in . disc. Image quality is similar to that of a Polaroid print.

## SATELLITE TV

BSkyB, which is still losing around $£ 1.6 \mathrm{~m}$ a week, has added a sixth channel to its services. The Comedy Channel is scrambled and is available to subscribers to one or both of the BSkyB film channels. According to the Financial Times satellite monitor there were some 62,000 dish installations during August. BSkyB claims that its services are now available to over 2.4 m households in the UK, with a total of some 1.64 m individual dish installations.

Amstrad has added a PAL/D2-MAC receiver to its range. Model SRD 000 has a suggested price of $£ 499$ with a 60 cm dish. The company showed a combined TV/satellite receiver/decoder and various VCR/satellite receiver combinations at the Berlin Consumer Electronics Show.

Amstrad has now sold nearly two million dish installations and claims 86 per cent of the UK market and 50 per cent of the European market.
Fujitsu has developed a chipset that reduces the number of i.c.s required to process the Japanese MUSE HD-TV signals from some 100 to 31 . Using a number of processors to manipulate individual frames simultaneously reduces the number of memory chips required. Fujitsu claims that the chipset enables the price of MUSE receivers to be reduced by about $\mathfrak{£ 6 , 5 0 0}$. Toshiba/Motorola and Sanyo/LSI Logic are amongst other groups working on the development of MUSE chipsets.

## CD-I LATEST

Philips has confirmed that its Compact Disc Interactive system is to be launched in the USA this autumn. The player, Model CDI901, will have a list price of $\$ 1,000$ but will probably sell for around $\$ 800$. It's expected to be available in some 1,000 outlets and will be supported by interactive kiosks and trained in-store demonstrators. There will be a catalogue of over 50 CD-I titles at the launch. GoldStar is developing a low-cost CD-I player that's expected to be available next year at around $\$ 50()$.

Philips and Kodak have now finalised their Photo CD standard and will begin marketing Photo CD players next summer.

## LASER DISC NEWS

According to the European Laser Dise Association sales of Laser Disc players in France and Germany should have reached the 75,000 mark by the end of the year. The dise catalogue in both languages now has some 400 titles - a further 150 titles are due for release shortly.

## HD-TV CONFERENCE

The HDTV 92 conference and exhibition are to be held at the Business Design Centre, Islington Green, London N1 on December 9-10th 1991. HDTV 92 is concerned with "the business of high definition and new television systems", primarily from the software/studio/programme maker point of view. The attendance charge for the two days is $£ 499.38$ inclusive of VAT. Contact Meckler Ltd., 247/9 Vauxhall Bridge Road, London SW1V $1 H Q$ (telephone 0719319985 ) for further details.

## TV NEWS

Philips has announced its first $16: 9$ aspect ratio, 100 Hz field rate TV set in the UK. Model 8906 has a price tag of $£ 3,500$ which includes the Philips Home Cinema audio system. Amongst the set's features are a movie-expand system to enlarge $4: 3$ pictures to $16: 9$, an 86 cm tube, a colourtransient improvement circuit, a Nicam decoder, detachable speakers, PIP, Fastext and two scart, three S video and a phono audio socket. In addition Philips is to introduce three $4: 3$ aspect ratio TV sets with $1(6) \mathrm{Hz}$ field scanning and Nicam sound in the 59,66 and 79 cm screen sizes.

Nokia introduced a novel remote control handset called the TV mouse at the Berlin Consumer Electronics Show. It relies on the action of a small internal ball bearing that moves as the unit is tilted to the left, right, upwards or downwards or is held straight. As the bearing moves, light from IR diodes is blocked. This triggers, in conjunction with simplified button operation, the required commands. The unit also controls Nokia`s VCRs. It will be avaitable in the UK with a new range of stereo TV sets at the end of the year.

Two new ranges of c.r.t.s have been announced by Philips. The Cineline range has the $16: 9$ aspect ratio and will be produced in 36,32 and 28 in . screen sizes. The tubes are designed for 1,250 -line scanning and have the new Philips DAF ( dynamic astigmatism and focusing) gun for correct focusing over the entire screen area. They have Invar masks and Philips' own black matrix system. Philips' enhanced black matrix system and Invar masks are also a feature of the $4: 3$ aspect ratio Black Line $S$ range. Its new Polygon overlapping electron gun system gives a sharp. clean spot.

## ASTRA 1B

Problems with Astra IB have been traced by the satellite manufacturer's engineers to misfunctioning chips in the onboard attitude control system. The craft is now being controlled from Astra's Betzdorf Satellite Operations Centre.

## VIDEO NEWS

A large number of camcorders have been launched this autumn. One interesting technical development is digital signal processing. In the Sony CCD-TR105 for example the output from the CCD image sensor is fed to a gain controlled amplifier and then to an AD converter, after which matrixing, white balance, aperture and gamma correction, are carried out in digital form under the control of a microcomputer. DA conversion then gives analogue huminance and chrominance outputs to feed to the record section of the camcorder. Sony claims that this digital signal processing makes possible the camcorder's compact, lightweight design and high-quality performance. Other features are hi-fi stereo sound; six times variable-speed power-zoom and a full-range autofocus system with macro facility; manual override controls for focusing and shutterspeed adjustment up to $1 / 4,000$ of a second; backlight compensation; a one-page digital superimposer (titles can be stored and displayed in a choice of eight colours, with scrolling and background reverse); insert edit and edit search, with an external connection for a Sony edit controller; high-quality playback capability of $\mathrm{Hi}-8$ recorded tapes; and a black fader for smoother seene changes. All this in a 630 g camcorder for $£ 800$ including case and accessories.
Hitachi's two new lightweight Video 8 camcorders, Models VM-E23 and VM-E25, also employ a digital signal processor (DSP). The claim is that by integrating most of the image processing into a single DSP chip space is saved, reliability is improved and picture quality is enhanced. Auto white balance and auto iris are also digitally controlled. The VM-E23 has a $\times 64$ digital zoom, a $\times 8$ optical zoom, five fast shutter speeds and a program autoexposure system. It weighs 830 g and has a price tag of £ 800 ). The VM-E25 has a twist-and-shoot mechanism and hi-fi stereo sound. It weighs 760 g and has a suggested price of $£ 9(0)$.

Sony's CCD-TR705 is a palmeorder that features Hi-8 technology. It has a $440,00(0)$-pixel image sensor and hi-fi stereo sound. The shutter speed can be adjusted down to $1 / 10,000$ of a second. Sensitivity is two hux and extensive user controls are provided. A newly-designed tape stabiliser mechanism to reduce jitter uses a special tungsten tape guide between the supply reel and the drum. Associated with this the drum geometry has been changed, with a lower drum window incorporated to improve tape-to-head contact and output. There are full edit facilities and a credit-card sized IR handset to control playback.
recording and zoom - a hold switch prevents accidental operation. The camcorder weighs 80 og and has a suggested price of $£ 1,000$.

Panasonic's NV-S5 is a lightweight ( 680 g without battery and tape) VHS-C cameorder with a digital image stabiliser and various digital effects including still picture, strobe and mirror - this gives kaleidoscopic picture effects. Suggested price is $£ 900$.

Canon's two Slimline Video-8 camcorders. Models UC10 and UC20. use the new lightweight MC-5LT chassis (weight 165 g ). The UC10 has a $320,(000)$-pixel and the U20 a 470,000 -pixel $1 / 3 \mathrm{in}$. image sensor. At 580 g the UCl0 costs $£ 800$ while the 710 g U20 with hi-fi stereo sound has a. suggested price of $£ 950$ ).

Mitsubishi's two VHS-C palmcorders, Models CXI and CX4, both weigh less than 600 g and feature six-event settings for specialised shooting situations. The CX1 is priced at $£ 700$. The CX4, which has a twin gyro image stabiliser that senses movement along the horizontal and vertical axes, hals a suggested price of $£ 850$.

Nikon's NV3100 Video-8 camcorder weighs just 590 g and is priced at $£ 800$. Features include a $\times 6$ zoom, LP operation and remote control. The VN7OOO adds Hi-8 picture quality. It weighs 790 g and has a suggested price of fl, 000 ).

Akai has launched two lightweight VHS-C camcorders that feature its Intelligent HQ picture enhancement system. Both models weigh 750g. Model PVS-C20 has a price tag of $£ 650$ and Model PVS-C4() a suggested price of £750.

Philip's new camcorders include the VHS-C Model VKR6870 and the S-VHS-C Model VKR90I0 which has hi-fi stereo sound and LP operation. Both are priced at £800.

Two new S-VHS-C camcorders, Models NV-S7 and NV-S9, have been announced by Matsushita in Japan. They have a digital image stabiliser plus digital zoom, strobe and snapshot recording, still mix and wipe, hi-fi stereo sound and a new 360 .(M) 0 -pixel $1 / 3 \mathrm{sin}$. image sensor. No details of a European launch have been released.

## CD Player Casebook

Reports from Mike Leach, Alfred Damp, Michael W. Bliss and P.J. Roberts

## Kenwood DP710

This machine came in a few months ago because it wouldn't read the discs. Since the turntable spun too fast the diagnosis was a faulty laser unit. A new unit was ordered, but a complete deck assembly with a different type of laser unit - it appeared to be a Sony KSS150A was supplied because the original type is no longer available. Fitting it cured the problem, and the machine was returned to the customer.

It came back recently, again because it wouldn't read the dises. This time the turntable wouldn't spin at all. A quick inspection once more led me to the laser. With no dise in the machine there was very little focus coil movement. As the focus drive waveforms were o.k. I suspected the new laser. But with the machine turned upside down and a dise in the tray the player worked normally! It seemed that the coil found it easier to focus on the dise in the upside-down position. The trouble is that it carried on working correctly when the machine was turned upright again. I've now got to convince Kenwood that the laser unit is faulty.

In cases like this it's sometimes possible to lubricate very slightly the pivot around which the focus coil moves up and down. But it's not possible with this type of laser as the coil has no pivot as such - it moves up and down by what appears to be thin rubber attached to the coil. Presumably in this case the rubber was too springy. thus slowing the focus coil action with the result that there was no focus.
M.L.

## JVC CAE21LBK

This JVC midi system had been a problem - a big problem. It came to me after two new laser units (type Optima 4), an 80 -pin YM3805 signal processor chip and various other bits had been fitted elsewhere. The complaint was that it wouldn't read dises, which it certainly wouldn't. The dise rotated extremely fast while the sled assembly sped to the outer edge of the dise then returned. That was it. I pressed the open/close button and the dise almost flew out of the tray.

My first thoughts related to the signal path. Maybe there was no r.f. signal? I connected the scope to the r.f. test
point and saw that the eye pattern started to appear then disappeared as the turntable sped faster. I assumed that the r.f. section was o.k., though I could have been wrong. The laser power was $o . k$, and the bit of r.f. waveform that was present was of the correct amplitude.

Servicing these players is no joke. As with most modernday players/midis. the leads aren't long enough for the board to be taken out for servicing. All in all it was a bit of a struggle. Anyway, scope checks around the tracking servo (I knew that the machine was focusing all right) lead me in the right direction. Adjusting the tracking gain and offset controls made no difference at all to the tracking waveform. At the emitters of Q801/2 the tracking drive was low. Checks were then carried out around the YM3805 signal processor. Everything seemed to be in order apart from the voltage at pin 21, the TRHD signal. This pin should have been at 4.9 V but was low at 1.5 V .

The TRHD output from the YM3805 chip helps to generate the tracking error signall. It's fed to the base of Q80 13 in the tracking servo via a $10 \mathrm{k} \Omega$ resistor. The voltage at the base of this transistor should have been $-1 \cdot 1 \mathrm{~V}$, but was 1.5 V , thus upsetting the tracking servo. R $\$ 27$ ( $100 \mathrm{k} \Omega$ ) links Q803's base to the -12 V rail. It was found to be open-circuit under load! When removed and checked it read $98 \mathrm{k} \Omega$, which seemed to be near enough, but when checked in situ it gave an open-circuit reading. Fitting a replacement restored normal operation.
M.L.

## Hinari DK100

The symptoms with this player were the same as those with a DK200 reported by V.W. Cox in the September Casebook, i.e. at switch on the arm slammed against the outer stop. In this case RI22 (1S2) was open-circuit.
M.W.B.

## Sony CDP-M20

Only noise came from the audio outputs. Checks showed that the EFM was correct and that the signals arriving at the DA converter chip IC10 were apparently correct. So

ICl0 was replaced. As this made no difference we had to assume that the data fed to IClO was incorrect. Checks were then made around the digital signal processor and 16 Kbit RAM chips. Replacing the RAM restored normal operation.
A.D.

## Philips CD104/304

These machines use double-sided PCBs with holes that are copper plated to link the two sides. This through-hole plating can go open-circuit, causing all sorts of problems. The most common is that the machine won't read the TOC or play. I've found that the best thing to do is to push through a length of 22 SWG TCW whilst heating the solder that's visible on the ground plane side of the linking hole, then cut and solder both ends.

Other problems I've had with these players have been as follows: thickened lubricant on the dise clamp and turntable spindle; worn turntable height adjustment serew
(carbon screw); dry-joints on the voltage regulators; a build-up of debris under the turntable motor's rotor; and dry-joints on the servo and decoder PCBs.

Other faults have been caused by power supply problems. Hum on sound (both channels) occurred when the -18 V supply was high while sound distortion (both channels) oceured when this supply went low. The 12 V supply going high resulted in skipping during the first part of any track. Thus a quick check on the power supply outputs can save you a lot of time that might otherwise be spent chasing wild geese.

On one occasion a fault was caused by very fine breaks in some of the PCB tracks leading to the microcomputer chip.

We've found that the laser units used in these models seldom fail. So if a player that refuses to work comes in, don't straight away condemn the laser unit.

These are very good quality, well-built players: it's well worth spending money on keeping them going.
P.J.R.

## Satellite TV Notes

S. Pearson

Some satellite TV channels, for example the French TV5 channel via Eutelsat II-F1 at $13^{\circ} \mathrm{E}$, have a mono sound carrier at 6.6 MHz or thereabouts. This is something that the Amstrad SRDHOO satelite TV receiver can't handle. Using a short-wave receiver I discovered that such audio subcarriers are present at the receiver's baseband video output socket. Thus a simple sound i.f. adaptor can be made to add to the receiver for reception of these "nonstandard" sound channels.

A suitable sound i.f. adaptor can be provided very simply by using the sound panel from a scrap GEC C2110 series chassis - other sound i.f. pancls could no doubt be used in a similar manner. Fig. 1 shows the connections required to the GEC C2110 panel and the power supply circuit used in the prototype. The satellite receiver's video output signal is loosely coupled to the sound panel's input via a 12 pF capacitor. Coils L198 and L199 on the panel can be tuned to the required frequency by ear. Pl99 (panel PC 471 ) sets the audio output level.

On the prototype unit I removed the audio amplifier chip IC181 and took the demodulated audio output via C192 ( $0 \cdot 1 \mu \mathrm{~F}$ ) to a VCR's audio input socket. Alternatively you could leave IC181 on the panel and connect an external speaker to it. I found one puzzling problem with the former approach - perhaps someone could throw some light on it.

If the Amstrad SRD400's baseband video output is


Fig. 1: Use of the sound panel from the GEC C2110 series chassis as an i.f. adaptor to obtain extra sound channels with a satellite TV receiver.
connected to a VCR the picture flickers like mad when viewed via the machine's r.f. modulator, though recordings made in this way are fine - I've tried this with three different VCRs. The adaptor is being used with a Goodmans/Dacwoo VCR which has switched sockets for the baseband inputs instead of the more usual switch on the front panel. I solved the problem by feeding the satellite receiver's r.f. output to the VCR's aerial input socket with the sound adaptor connected to the audio input socket. It works with this particular VCR as the video and audio inputs are independently switched.

## Two-satellite Dish Alignment

To simplify dish alignment to either Eutelsat or Astra I cut two small nicks in the dish's bracket, near the large securing not, using a hacksaw. This enables the disth to be realigned simply by lining up the saw cuts by eye. Obviously the elevation angle also has to be changed slightly, but this can be done using the bracket's elevation scale. These notes apply to the standard 60 cm dish.

## General Points

Finally I'd like to raise some general points on the subject of satellite TV.
(1) There seem to be two types of $F$ connector available, with different centre hole diameters - a small hole for RG59 coaxial cable or a large hole for low-loss coaxial cable. I feel that to avoid a mismatch where the cable enters the connector it's important to use one with the correct diameter hole. The inner dielectric of the cable should be a close fit through the hole and lie flush where exposed at the front of the connector. It's not unknown for installers to use the wrong type of F connector for the cable being used.
(2) A rubber boot that covers the F connector completely is now available from RS components.
(3) If you find it difficult to drive cable clips into a problem wall without destroying no end of clips, or mashing the cable, try drilling 5 mm holes in the wall, plugging them with short lengths of 6 mm wooden dowel, then driving the clips into the plugged holes. Clips can in this way be fixed to high spots on old stone walls. This avoids the cable being forced into the recessed mortar joints, with sharp kinks being made in it.

# TV Fault Finding 

## Grundig T55-340 (CUC3400 Chassis)

Several of these sets have come to us dead and tripping. So far the causes have been: the set-h.t. control R 637 intermittently or permanently open-circuit; D666 (BYV16) short-circuit; D664 (BA159) short-circuit; or IC686 (78M05) short-circuit.
P.B.

## Philips GR1-AX Chassis

There was no picture or sound, but the remote-command received LED flashed when the handset was tried. A quick check showed that the 95 V output from the chopper power supply was low at 10 V . I next made a few resistance checks on the power supply outputs and found that a reading of $60 \Omega 2$ was obtained across the +9 ( 10 V ) supply. The culprit was the sound chip, but although disconnecting the chip removed the short the symptoms remained the same.

A quick read through the circuit description was called for. In order to start the power supply requires 15 V across D6613, which is a BYX79C15 zener diode. There was only 10 V because D6613 was leaky. A new zener diode and sound chip restored normal operation.
P.B.

## Grundig CUC44XX/46XX

Models with teletext have a dealer facility that puts the station identification on all the time - it's normally on for only a few seconds at channel change. The procedure isn't given in the instruction book, but customers seem to find it by accident. To remove the permanent station display identification, switch to TV then to reveal with the remote control handset. To bring it back on, repeat the process.
P. $\mathbb{B}$.

## Philips CTX Chassis

This set suffered from line tearing. It was much worse in the VCR position. The dealer had already changed the TDA2577 chip and the VCR switching components T7374, D6374, etc. As the tearing varied with the picture content I homed in on the sync separator section. C2378 ( $1 \mu \mathrm{~F})$ had dried up.
$\mathbb{P} . \mathbb{B}$.

## B and 07702

The complaint was of intermittent loss of colour. It would tend to disappear more regularly with a high-brightness scene and a fairly high setting of the contrast control. When the fault was present, very weak, tlickering inversephased chroma could be seen on the screen. The reason for this link was a very slight reduction in height with increased beam current: this resulted in a change in the width of the field flyback pulses that are taken from the deflection PCB via the field blanking circuit $70 \mathrm{TR} 11 / 10$ etc. to pin 28 of the TDA3300 colour decoder chip 70IC1. If the height control was adjusted in one direction the colour would come and go. The cause of the fault was the chip itself - it should work correctly with a wide range of pulse widths.
I. $\mathbb{B}$.

## Salora 15L37

This set had a very dark picture. The colour level appeared to be normal but the luminance was low. We traced the luminance signal to pin 36 of the TDA3301B decoder chip

Reports from Philip Blundell, AMIEIE, lan Bowden, Steve Cannon, Alan Smith, Michael Dranfield, Ed Rowland, Paul Hardy and Stephen Leatherbarrow

IF(0), where it's clamped and level-shifted before emerging at pin 34. The signal level at pin 34 was very low. A check on the components connected to this pin led us to the $22(1) \Omega$ preset PF01 which was open-circuit. Replacing this preset restored the amplitude of the luminance signal. I.B.

## Sony KVM2511 (AE1 Chassis)

On occasions this set wouldn't come out of standby. The exact symptoms were as follows. On selecting standby the red LED lit but when a programme was selected to power the set the LED went out but the set didn't come on. Now these sets have a standby set-h.t. preset which in some cases was apparently misadjusted during production. We checked the h.t. when the set was up and running and found that it was correct at 135 V . But when standby was selected the h.t. rose to 143 V . When we attempted to power the set again the protection circuits sensed the increased h.t. voltage and shut the set down. After turning the set off completely at the on/off switch and waiting a couple of seconds the set could be switched on again and worked normally. We then set the standby set-h.t. control for 135 V in the standby mode, after which everything was o.k. We've had to do this with several sets since then. S.C.

## Philips K40 Chassis

This set came to us with a note to say that it destroyed line output transistors. Sure enough the BU508A was shortcircuit collector-to-emitter, so a replacement was fitted and the set was switched on. As the picture and sound came up we put it on soak test. Whilst I was working on something else I heard the squeal of an overloaded power supply. Yes, it was the K40 and the line output transistor had failed again. We were going to have to maintain close observance whilst it was running on test to see whether there were any clues before the transistor failed again. We also decided to fit the higher rated BU508V, which would probably handle the fault condition better and give us a bit more time to watch for any clues.

With the set running on test we watched it like a hawk. After a short while the picture shifted to the left and the width reduced drastically. I dived for the on/off switch and managed to save the new transistor, but where was the fault? We replaced C 2161 and C 2163 in the line output transistor's collector circuit - they've given us trouble before - but this time they weren't guilty. We did discover however that the fault could be instigated by knocking the set or tapping the chassis. Dry-joint time, but none could be found in the line output stage. What about the line driver stage? This is on the bottom power supply panel, and when this was removed an obvious cracked and dryjoint was found on the line driver transformer. Resoldering it cured the problem. We have had this problem with quite a few sets from various manufacturers, but the usual symptom is intermittent loss of the picture. S.C.

## Ferguson 41P3 (IKC2 Chassis)

When this three-month old set was switched on the standby light lit but the power supply was tripping. A check on the 107 V h.t. rail at test point BP50 showed that is was at $50 \mathrm{~V}-75 \mathrm{~V}$ between trips. On the assumption that
the cause of the trouble was heavy loading in the line output stage a check was made around the line output transformer and associated components. This revealed that the BA157 180V rectifier DL11 was short-circuit. In addition the associated series surge limiting safety resistor RL11 was open-circuit. This of course removed the shortcircuit diode from the load; funny, I thought, the set trips when no current is drawn from the 180 V rail! Anyway after replacing these two components the set still tripped out because I'd forgotten to reconnect the scan coil plug - it had been removed to get at RL1l.

## Binatone Colortron 01/9014

A very common fault with these 14 in . colour portables is failure of the line output transformer - it usually burns out in a big way! Be sure to get the right one when ordering a replacement. Two types were fitted. They can be identified by the numbers, CF82 or CF65A. The two are interchangeable but give different focus voltages depending on the type of tube fitted. If you fit the wrong one the result will be a blurred picture.
M.Dr.

## Logik/Ferguson TX90 Chassis

The complaint was of a snowy picture. Tuner I thought, but on going through the channels I found that some were still tuned in. Perhaps children had pressed the tuning buttons? I retuned channels $1-4$, but when these were reselected they had disappeared. Further checks showed that channels 1-8 couldn't be stored in memory, though channels $9-16$ would store o.k. Tuning and memory are handled by the M293BI chip IC902 on the left-hand subpanel. As the 25 V memory supply voltage was correct a new chip was fitted. This cured the problem.
M.Dr.

## Fidelity AVS2000

The fault report read "stuck on channel 8". This was true," but there was no audio either. The middle fuse (1A) of the three attached to the side of the record deck had blown. This fuses the bridge rectifier on the audio panel. Lifting R379, the feed to the 12 V regulator, proved that the fault was due to the bridge or the audio output chips. The bridge was innocent, but both IC4 and IC5 were short-circuit. Two new TDA 1908As and a new fuse restored normal operation. Stuck on ch. 8 was of course due to there being no 12 V supply to the M104B1 chip.
A.S.

## Philips CF1 Chassis

The problem with this 14 in . colour portable was field collapse, accompanied by sound from a foreign radio station. This indicated that there was an i.f. fault as well. A look at the circuit diagram showed that the field timebase and i.f. sections of the receiver are both supplied from the same source. Tracing back revealed that R3583 (19) was open-circuit.
E.R.

## Salora J Chassis

This set was dead with the h.t. filter resistor RB713 opencircuit and the two Ipsalo transistors $\mathrm{TB} 700 / 1$ short-circuit. These items were replaced and after resoldering several suspect joints, including one that, at CB712, looked as if it could possibly have been responsible, I switched the set on. The on/off switch had to be pressed several times before the set would come on, then after about half an hour the two transistors failed again. At this point I rather
belatedly decided to consult Nick Beer's article on the J chassis (December 1989). As a result CB712, CB726, RB703 and RB705 in the Ipsalo transistors' base drive circuits were replaced. RB705 was difficult to locate as it was designated CB705 on the PCB! Two new transistors and a filter resistor then had the set working normally. E.R.

## Ferguson TX9 Chassis

Intermittent loss of colour was the fault with this set. I dived in and changed the TDA3560 colour decoder chip, the delay line and the crystal, but this didn't cure the fault. Scope checks around the chip with colour bars present proved inconclusive. Oscillator adjustment in accordance with the instructions in the manual didn't produce the desired effects: the colour didn't lock very well and was very weak. I eventually found that the delay line balance control RV67 didn't do what it's supposed to do. On removal it was found to be open-circuit. Replacing it provided a cure.
P.H.

## Philips K30 Chassis

A colleague had spent some time on this set, trying to cure permanent tripping. He`d proved that there was an a.c. load on the power supply by disconnecting the drive to the line output transistor. In this condition the power supply would drive a 100 W bulb. The line output transformer's secondary windings had been disconnected one at a time, and the line output transistor and transformer had been replaced. After such a thorough investigation there was very little left to check. Disconnecting the scan coils made no difference. Changing the flyback tuning capacitor C1567 ( $8 \cdot 2 \mathrm{nF}, 1.5 \mathrm{kV}$ ) got the set working - it was opencircuit. The original line output transformer was refitted, but it had met its Waterloo.
P.H.

## Philips KT4 Chassis

This set was dead. Having got the power supply out I carried out some cold checks. T7182 (BC547) in the standby circuit was open-circuit.
P.H.

## Ferguson TX10 Chassis

We've had this fault several times recently. You find that the picture is blanked except for the final inch or so at the right-hand side, where the picture content is correct. A check on the RGB h.t. line, which is normally at 205 V , will produce a low reading of typically 55 V . A scope check will show excessive line-rate ripple on this supply. The cause is the relevant reservoir capacitor, which is $\mathrm{C} 726(22 \mu \mathrm{~F})$.

[^0]
## Hitachi CPT1471 Mk 1

The complaint was of tripping and going dead, ${ }^{*}$ accompanied by ticking or arcing noises. This was caused by the usual power supply probtems. A kit is available, including the STR6020 power supply chip, the field chip feed/supply transistor etc. After fitting these items the set gave us new symptoms. Although the power supply was now working well the field sean was accompanied by text lines and the flyback blanking was very poor. The field generator and driver stages, also the line oscillator and blanking circuits, are all within the LA7801 chip. Replacing this restored normal operation. It presumably died during the power supply's failure.
S.L.

# Letters 

## TIME WASTERS

While reading through some back issues I came across a correspondence on repair charges. It seems to me that we've been our own worst enemy in this respect. My particular concern is with time wasters. We've all had them, and there will always be people (you can't call them customers) who want something for nothing. Many TV/video repair advertisements offer a 24 -hour service, free estimates, free call-out etc. No wonder that time wasters think nothing of calling out two or three different firms for quotations. They assume that we've nothing to lose. After all, repairing TV sets and VCRs cen't be that difficult, otherwise why would so much free service be on offer? Can we blame the time wasters for thinking in this way?

But TV and video servicing to a high standard involves dedication, a lot of head-scratching, and technical knowhow that has to be constantly up-dated. Just stop and think about your job. Is it really as the public seems to see it? Of course not. So let's get with it and start respecting ourselves and valuing our craft as it deserves.

My business was also guilty of offering too much free service. Yes, the phone never stopped, but detailed analysis of all calls over a six months' period showed that there was a very high percentage of time wasters. They represented a substantial loss in terms of wasted time, effort and money. Each and every time waster stops productive, profit-making work and often prevents calls on likely paying jobs because you're over-booked.

No matter how busy or slack we are our policy now is to make a fixed charge to cover time, petrol ete, when called out for fault assessment and a repair estimate. If our estimate is accepted however we don't make the call-out charge. These conditions are made clear on the phone before a call is booked in. We`ve found that this policy enables us to avoid time wasters as far as possible. Our overheads have been substantially reduced - yet the phone is as busy as before.
We're in business to make a living. Yes, job satisfaction is important, but it should be considered as a bonus, not a reason for running a business. If in doubt, ask your bank manager!

If you think that by carrying on with a free this, free that policy you are on to a winner, be prepared for the public to regard TV/video servicing as a low-grade job.

So let's get with it. There's plenty of work out there. Stop throwing your hard-earned knowledge away and don't worry about the cowboys. They never live long - let them have the time wasters.
John Edwards,
Bromley, Kent.

## WORKSHOP MANAGEMENT PROGRAM

It's not very often in this day and age that one is able to applaud good service, but the service we have had from a software firm is second to none. It relates to a complete workshop management program. We purchased the original one in February, and although it was good we felt that with a few additions/modifications it could be even better. The firm not only accepted our suggestions but added a few new ideas of their own and sent these to us. The result is a program of outstanding quality at a
price that's well within the means of any good workshop.
Just a little about what the program does. After booking in an item the program takes the repair through all its stages and finally keeps a record in the archive file until you decide either to dump it for good or to file it outside the system on a monthly dise. It can search its record by jol) number, make of unit or customer's name. Repair details stored include parts ordered/received/fitted, the engineer concerned, when the unit was collected/delivered and miscellaneous information such as "scratched cabinet" or "loose back cover", things it might be useful to be able to refer back to at a later date. The program can automatically send out up to ten standard letters that incorporate the job no., title, name and address - this is very useful for getting overdue items collected. It lists repairs still to be looked at as well as parts to order and to be fitted. A menu-driven system contols the data to dise to back-up and archives. The old records can be taken out and put on to separate dises so that the records for say only the last three months are current, giving more efficient back-up. A complete job card, label, customer receipt and invoice are provided. Without doubt the program is a great asset to a repair department.

I have no connection with the authors of the program other than as a customer and have nothing to gain from singing its praises, but I do feel that the service I have been given deserves wider acknowledgement. The firm concerned is TBR Software, 369 Chepstow Road, Newport, Gwent (telephone 0633282556 ). I came to hear of it through the pages of Television.
Geoff Fardon, Station Television,
Llanelli, Dyfed.

## THANKS

I'd like to thank the many readers who wrote in following my reminiscences in "Fifty Years in Radio and TV". Without their letters we would not have known for example about the true origin of the two-pin plug, the spot where Blumlein fell or the true meaning of H2S (though I still like mine better!). I'm sure everyone understands that they were only the personal recollections of someone as fallible as the next man, and who like most people never had the time to keep a diary. As well as sparking off memories in us old-timers, I hope they entertained the younger generation of readers who perhaps have never changed a valve, ridden behind a steam locomotive or endured the "Crazy Gang" live!

It was a change to write hindsight. In the past foresight was needed. It took two months at least to get a piece from the pen to the newsagent's shelf, and at times inspired guesswork was required when definite information on latest developments was hard to obtain. Fortunately we were right most of the time!' 's good to see that today's contributors are as forward booking and our readers as hawk-eyed as ever!
Harold Peters,
Lowestoft, Suffolk.

## BEOVISION CORNER

In the September issue Paul Glazebrook asked for information on removing teletext lines with the $B$ and $O$ $340 \%$ ) series 323 X chassis. There's an official modification for this, to add the extra field flyback blanking circuit shown in Fig. 1. Take the input from the collector of 2TR8. at the bottom centre of board PCB3. Mount the added components at the top right-hand side of the board. The


Fig. 1: Extra flyback blanking circuit for the B and O 3400 series $323 X$ chassis to remove teletext lines.
blanking pulse is injected in the control-grid circuit of the 12 HG 7 luminance output pentode.
Can anyone supply part of the convergence drawer for a B and O $50(0)$ type 3905 colour set? It's the larger part with the speaker grille finish, part no. 3131095 . Alternatively I would take a complete drawer. It's required to complete restoration of the set. I'd gratefully pay for parts and postage
C. R. Taylor, 8 Echo Barn Hill,

Kendal, Cumbria LA95NA

## OCR SCANNER TIP

A Panasonic Model FX-RS505 OCR scanner just out of guarantee got worse and worse and finally read nothing it's a device to read printed text and pictures into a computer. I couldn't see anything obviously wrong when I opened it up for a visual check and to look for any adjustments. So there loomed the prospect of an expensive repair and a long wait. I then noticed that the mirror which slopes upwards was covered with an almost imperceptibly fine film of dust. Carefully cleaning it provided a complete cure.

There was nothing in the manual about cleaning this mirror. The mind boggles at the likely cost of sending the scanner to the repair agents via the shop just to clean this item.
John de Rivaz. B.Sc. (Eng.), AMIEE,
Porthtowan, Cornwall.

## SAGA OF A G11

Here's a little story for those of you who think, like me, that they can do Glls blindfolded. The phone rang and a worried voice said "I've got a bit of a problem with my television". When I called on the customer I found that I'd misplaced my 4 BA nut spinner, so I had to use my neon serewdriver on the three back bolts. I should have taken that as an omen.

With the back off I swung open the power panel and was confronted with a red $470 \mu \mathrm{~F}$ h.t. reservoir capacitor. Sharp intake of breath. "Who did the last repair then?" "It's gone wrong only once in the past - my son-in-law who works for BT fixed it by soldering a dry-joint. This time I took the back off because the set was whistling and soldered that bit (pins 15 and 16 on the dynamic correction panel). After that it went bang."

I told him that it would have to go back to the workshop, and explained about the damage that can occur when the $470 \mu \mathrm{~F}$ eapacitor is a red one - the BU208A and TDA26010 ruined and a star-shaped hole in the tube neck. Seeing the look of horror on his face, I softened the blow by checking the BU208A. As it was all right I told him that the capacitor, having lasted all these years, was unlikely to be faulty but would nevertheless have to be changed to prevent damage during my three-months guarantee period.

Back at the workshop I found that Id run out of Gll capacitors - we don't keep much of the old stuff now. I could get one next day from NEC however. It arrived on time but when I removed the red one I found that the two VDRs (015 and 017) had burnt out against the can. Both mains fuses had blown, two of the bridge diodes had gone short-circuit, both thyristors were leaky and two resistors (R19 and R53) had burnt up. Due to a crack in the board there was no h.t. adjustment.

After replacing these items I wound up the mains imput slowly using a variac. This showed that there was field collapse. A new TDA2600 gave me a raster with pincushion distortion - the BD238 EW modulator driver transistor had succumbed. Having done all this I was stuck with a noisy push-button channel selector unit. At my age I should know better than to say "this won"t take long"!
John Hopkins,
Felixstowe, Suffolk.

## HELP WANTED

I've been repairing TV sets and VCRs as a hobby for about five years and would like to start a servicing carcer. The trouble is that being nineteen and self-taught, with only limited qualifications, it's difficult to find an employer who is interested. If anyone would be prepared to take me on as a trainee technician would they please write to the address below.
Robert Ingleby, 8 Gilbert Mead,
Havling Island, Hants POll ORE.

Can anyone supply a service manual or circuit diagram for a Commodore 1901 colour monitor? It may be of Samsung manufacture. Also does anyone have information or connection details for the MA 1043LR clock module made by NS Electronics (National Semiconductors)?
John Walker, Eng. Tech., 14 Leamside,
Leam Lane Estate, Gateshead NEIO SNT. (19) 4690157.

Can anyone supply an AN239 chip for the Panasonic TC275G colour receiver?
Roy Goodall, 15 Bainbridge Road,
Bolsover, Derbyshire S44 OUD.
0246827.365.

Has anyone in the Lancashire/Yorkshire area an Hitachi 17FHP22 tube or a set with a good one in it'? I'm in the process of restoring an old CSP(80).
H. Keighley, 117 Bradford Rood, Riddlesden, Keighley. Yorks BD20 5JH. 0535003012 .

Can anyone supply a circuit diagram/manual for the Alba CTV10, also a working push-button channel selector unit? Inving Finch, Engineering Faculty, Luton College of Higher Education, Park Scuare, Luton LUI 3JU.
058234111 e ext. 249 or 0582.576693 (home).

Can anyone suggest how to get an Amstrad PC CM colour monitor to work with an Atari 520 STFM?
Steven Postgate, 10 Newman Close.
Wittering, Peterborough PE8 $6 E F$.

# Servicing the Panasonic NV777/788 


#### Abstract

Amongst the various VCRs that have been marketed by Panasonic in the UK these two are a bit special. They are very similar, though by no means identical, top-of-therange models dating from 1983-4. The NV777 was the first to appear: its features include front loading, an eight-event timer, infra-red remote control, reverse play and variablespeed slow motion. The later NV788 has the additional benefit of two-speed operation. While the LP quality is not as good as that with the NV730, a later machine that was on the market simultaneously for a short while, it's certainly better than that with the NV688, Panasonic's first consumer dual-speed model in the UK.

The mechanisms are a cross between the NV366 and the NV7200 series, with slight modifications. Anyone familiar with these mechanisms will soon find themselves at home with the NV777 and NV788.


## Points to note

The NV788 has index searching, which means that there's an extra head at the front centre of the direct-drive unit. It inserts itself in the cassette cutout at this point when a cassette is loaded and is known as the MR head. The annoying thing is that the lead to the head, which is plugged at only the system control PCB end, is fed to the top of the mechanism through the large loading belt. Thus belt replacement involves undoing the PCB and all the lead retainers, then unplugging the lead, passing it through the old belt and threading it through the new one before this is fitted.

The still/slow performance is good. The still lock controls are accessible without removing covers. There's a small rubber strip on the right-hand side of the machine (viewed from the front): when this is removed the controls can be adjusted through the exposed hole.

At this stage of their life these machines, particularly the NV788s, will have begun to get a bit noisy. The reel motors tend to tick and buzz and the mains transformer can also buzz loudly when old. The power supply circuits are straightforward and, in our experience, have been very reliable.

## Dismantling

The top cover is held on by four screws, one at each corner. With this removed you can take out the screening can by slackening the red screws and sliding it off. The heads can then be cleaned.

The front of the machine is clipped as well as being held by screws across the top. To remove the front you first have to take off the metal bottom plate, which is held by brass-coloured screws. Doing this allows the clips across the bottom of the front to be undone.

After removing these three items the cassette carriage can be taken out. Undo the four red securing bolts, one at each top corner, taking care of the earthing leads that will now be free. The small PCB mounted in the right-hand corner, over the mechanism. will also have to be removed - it's secured by three red screws. Lay it on the adjacent PCBs, with foam or something similar between for safe operation. If you want to remove the carriage completely. for example to replace mechanical parts, undo the multipin
connector at the rear right-hand side. To run the mechanism with no tape or carriage, leave this plug connected, lift the carriage out and tip it upside down on to a piece of foam placed over the adjacent timer/presetter PCB. If you now insert a cassette into the carriage, bottom side up of course, the machine will run as the photosensors are on the side of the carriage and the emitter is in the machine. Note that in the rewind mode the machine will cut out if the take-up reel is not spun by hand, as this is where the reel-rotation sensor is situated.

One uncommon feature of these machines is that when the cassette carriage is removed you see a metal plate that's mounted over the reel drive and brake mechanisms beneath, with only the two reel turntables protruding. To replace the idler brake band etc. this plate has to be removed. It's secured by two circlips, one large and one small one. The latter is usually damaged when it's removed, so it is useful to stock some spares. If you use the Panasonic VUD kit you'll find that all relevant circlips are included. Use of small circlip pliers helps to avoid damage. Remember to refit this plate before refitting the carriage.

## Mechanical Servicing

Mechanical servicing follows the procedures for the NV333/366/7000/7200. We'll deal here with replacement of the parts included in the Panasonic 1,000-hour maintenance kit, which was reviewed by Ian Bowden in the October 1988 issue, and some other commonly required replacements. The kit is type VUD 4090 KIT .

## Video Head Replacement

To replace the video heads, part no. VEHO20) for the NV788 and VEH0177 for the NV777, remove the single bolt that secures the discharge angle on top of the drum, then the two bolts that hold the upper and lower drum together. The drum connections are via flying leads from the lower drum to a PCB on the upper drum. There are quite a lot of leads in the NV788: although the colours are marked to show where the leads go, it's wise to draw a diagram before you start - the letters, $K$ for black etc., are not all obvious. Take care when soldering the leads, which vary in length, as they are easy to damage and there are no spares - a new DD unit will be the unfortunate consequence of broken leads, unless you dare trying to take the unit apart and run in a new lead!

The heads are quite expensive and do fail. Very good rebuilds are available from MCES Ltd, 15 Lostock Road, Davyhulme, Manchester M31 ISU. Unfortunately however there's a tendency for the drum to become burred, which means that it's not suitable for rebuilding. This is caused by excessive back tension or poor tapes. These factors also cause excessive audio/control head wear, which has been a problem with some of these machines. The back tension should be checked and, if necessary, reset whenever one of these machines comes into the workshop.

## Back Tension

The back-tension specification is the usual 25-30g, measured with a Tentelometer half way through a three-
hour tape. For good noise suppression and quality in the trick modes the back tension should be set near the top of the specified range, i.e. typically at $28-30 \mathrm{~g}$. Don't fall into the trap of setting it higher than this in order to get better results. Doing this is quite unnecessary: the trick is to adjust the back-tension post landing position carefully then compensate by adjusting the soft-brake band. This will give you correct back tension and trick-mode operation.

## The Audio/control Head

Audio/control head wear is comparatively common, especially with the NV788, and as just mentioned is made much worse if the back tension is excessive. The deck needs to be fairly clear for head replacement. Though it's not essential to remove the cassette carriage, life is made a lot easier if you do - and anyway you'll probably be replacing the idler etc. at the same time. The head has the usual three-screw mount. The centre screw is threaded into the base of the head assembly and so needn't be removed until the head is taken out. The rearmost screw (left-hand side viewed from the front) is the counterspring holder: it's best to remove this one last. The foremost, right-hand side screw is threaded into the mechanism and thus hats to be removed - it's best to do this before the counterspring one.

After removing it the tilt screw can be fitted to the new head. First note the approximate protrusion into the head so that the new head will be roughly aligned when fitted. Then fit the new head, ensuring that the indentation at the front fits over the pip, about which it pivots. on the mechanism. Fit the azimuth screw, roughly in place, then fit the counterspring screw to the correct tension, i.e. don't over compress the spring. Finally align the head using a standards tape. Align the tilt carefully in order to prevent tape-path crinkling - watch the tape travel around the adjacent guides and posts.

## Idler Replacement

Idler replacement is a bit more involved and tricky than one would like. Remove the top and bottom covers, then the front and the cassette carriage. The metal plate has to come out next. Remove the retaining cirelip at the top of the take-up spool, after which the spool can be pulled off take care not to lose any washers underneath it. Next remove the reel motor underneath in its plastic frame. This is done by taking out the three brass bolts/screws that hold it. At this point take a careful look at the idler from underneath: note the position of the spring at the rear of its arm. Use a screwdriver blade to move the nylon lever to


Fig. 1: Replacing the idler. (a) Underside of the mechanism (simplified) showing the nylon arm and spring positions when fitting the idler. Machine is on its left-hand side. (b) A simplified view of the upper side of the mechanism, with the take-up reel table and the idler removed.

## next month in



## - SERVICING THE FINLUX 1000 CHASSIS

The sets in the Finlux 1000 series have been on the go for a good number of years now. Apart from a couple of points they have proved to be very reliable. This means that any problems that do occur can be difficult to handle due to engineers' lack of familiarity with the chassis. Fortunately the circuitry is straightforward, so that servicing is reasonably simple. Steve Cannon provides general guidance plus a faults list. Armed with this, you should have no difficulties when a 1000 chassis comes along.

- SATELLITE TV RECEIVER PROJECT

Charles Murray, I.Eng., AMIED, GOMIA, has so far designed two satellite TV receivers. It's a good way of coming to grips with the requirements of satellite TV reception! Next month he describes his Mk 2 receiver. The tunerfi.f. block is bought in of course - it's an Astec unit. The rest of the receiver uses just a few i.c.s. Construction is on two PCBs. As the receiver is intended for use in exploring and monitoring satellite TV it doesn't offer hi-fi stereo or video outputs for a VCR etc.

- FIVE DECADES OF STEREO TV!

The BBC launched its Nicam 728 TV plus stereo sound service on August 31st this year. However the Corporation has been experimenting with stereo sound transmission since the Fifties! Keith Hamer and Garry Smith fill in the history and provide a technical specification for the Nicam 728 system.

## SERVICING THE FISHER FVH-P520

This popular VHS machine dates from 1982-3. Features include freeze frame and wired remote control. John Coombes provides a run-down on fault-finding procedures.

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the front of the machine, carefully unhook the spring then, from above, move the idler towards the space vacated by the take-up spool along its slot. The idler's tail can now come through the expanded slot and the idler will come out.

Fit the replacement in the reverse order, ensuring that you place the spring correctly on the idler's tail. See Fig. 1.

## Capstan Motor

The capstan motor is a direct-drive unit. Note that the part number is given incorrectly as VEM0165 in the mechanism photograph in the manual for the NV777. The correct part no. is VEMO164. The capstan motor is quite pricey but rarely fails. Capstan servo problems can be caused by dryjoints or breaks on the small PCB for the FG circuit at the base of the capstan motor.

## Mode Switches

The mode switches are very reliable and align in the standard manner, notch to notch in the eject mode.

## Belt Replacement

Apart from the previously mentioned problem with the large loading belt in the NV788, belt replacement is straightforward. The kick-pulley belt (part no. VDV(0138) simply fits over pulleys at either end and should be removed first and fitted last. To replace the large loading belt (part no. VDV0135) you have to remove the DD unit connector at the drum end (untike the NV7000/7200/7800 where you have to ferret around the loom, tracing it back

## FAULTS LIST

The following is a list of the main troubles we've had with these machines.
(1) Low sound level or poor h.f. response. The audio/control head in these machines tends to wear out. Part nos. are VBR006l for the NV777. VBR0067 for the NV78s. The fault is particularly noticeable with the NV788 in the L.P mode, since the head-to-tape speed is slower. After replacing the head, check the back tension and audio bias.
(2) Poor or noisy rewind/fast forward. This is usually due to a faulty idler (VXP046.3) or reel motor (KFN56FB8A).
(3) Tape remaining counter reads four hours with certain three-hour tapes. You can't correct this fault - it's a design quirk!
(4) Squeaks in play. The squeak stops when pause is selected. This is usually due to a noisy pinch roller. Replace it and clean the tape path. Also lubricate the reel shafts with a very small amount of thin oil.
(5) As (4) but continues in pause. Suspect a noisy discharge angle (VXA1584).
(6) Goes into play then immediately returns to stop. Large loading belt (VDV0135) faulty. It's worth replacing all three belts at the same time.
(7) Noisy picture during or following trick-mode operation. Check the head switching relay(s) by substitution.
to the PCB end) and the small plastic belt cover which is secured by a single bolt. This belt has to be taken off the intermediate loading pulley before the small loading belt (VDV0122) can be replaced. Therefore the best policy is to remove all three belts and fit them in the following order: small loading, large loading and kick pulley.

## Pinch Roller

To replace the pinch-roller arm (roller only part no. VXP0518), first remove the cassette carriage, then the cassette blinder release bracket. The arm is held by a single circlip about the centre pivot. Take care not to over-stretch and damage the spring.

## Impedance Roller

A single nut secures the impedance roller in the usuat manner. Take care to ensure smooth travel of the tape over it when it's aligned. Also take care not to lose the roller's inner sleeve when removing the old one. The replacement will usually be plastic, unlike the original metallic version.

## Brake Band

The brake band clips into the back-tension lever at one end and is bolted through its slot at the other end. See the previous notes about adjustment. For correct back tension the right-hand edge of the washer under the head of the bolt usually needs to just cover the inner edge of the righthand side of the slot in the band - anyway this is a good starting position for adjustment.
(8) Loses timer and clock information during a power interruption. Replace the back-up battery (VSBOO(4). When this is fully charged it should give a reading of approximately 4.25 V , falling to 4.07 V after 48 hours' discharge. An eight-hour charge should allow a 48 -hour discharge. When fully charged the battery will last for 72 hours on average. The battery, usually consisting of three NiCd cells, is on the timer PCB.
(9) Doesn't accept a cassette/other loading problems. Replace broken or dirty cassette up and down switches on the side of the cassette carriage.
(10) Machine is affected by mains-borne noise, e.g. when a fluorescent light is switched on or off. The unit then for example enters the stop mode. If this hasn't been done during production, add a $1 \mu \mathrm{~F}, 50 \mathrm{~V}$ electrolytic capacitor between pin 9 of IC7505 (positive lead) and chassis (negative lead), on the print side of the board. The component is C7552, part no. ECEA1HSO10.
(11) Remote control unit doesn't work. The remote control units are straightforward and all the usual advice applies, i.e. check batteries, LEDs etc. as necessary. The only stock fault is failure due to the legs of the ceramic resonator (CSB420) fracturing, usually as a result of the unit being dropped once too often.
(12) Various Y/C faults, e.g. unlocked colour. As these machines have aged, dry-joints have become quite common on the Y/C board (the lower PCB, beside the bottom of the mechanism). Try resoldering suspect chassis connections, the flying leads and the large hybrid chips on this board. Also check relay contacts.

# What a Life! 

## Donald Bullock

"My wife accidentally upset a little fairy last night Mr. Bollard" said the hesitant young man at the door. "Can you have a look at it?"

I followed him out to his car. As he stopped I touched his elbow. "Look, it might just be me" I said, "I feel a bit odd today. Every day come to that. I don't quite..."

## A Saisho CT141X

He took a Saisho CT141X colour portable from the boot and handed it to me. "It went in there" he said, pointing to a slot near the tube neck

I eyed him closely. "The fairy went in there because your wife upset him, or maybe her?" I asked. "And you want me to coax her out. Is that it?"
"I'm talking about washing-up liquid" he said. "My wife upset some into the set. We'd like you to see what you can do."
"I don't feel too optimistic" I said "but I'll have a go. I hope it's kind to my hands." Laughing at my little joke, I took the set back to the workshop.

The liquid must have gone in some while before since the chassis looked quite dry and some of the jumpers were corroded. The STR50103 power chip was soapy, so I took it out, cleaned it and compared its resistance readings with a new one. Shedding a tear I fitted the new one. Before doing so I cleaned this part of the panel and got to work with the hairdryer. Then I checked the bridge rectifier diodes and found that one of them was short-circuit. In went a new BY127. The $5 \cdot 6 \Omega, 5 \mathrm{~W}$ surge limiter next door had laid down its life in sympathy, so this was also replaced.

## The Switch On

Feeling uncertain if not actually afraid, I crouched back and switched the set on. It came to life but there was no field scan. The obvious thing to do was to replace the UPC1378H field output chip IC402. This restored the raster but there was a sizzling from the tube base panel, followed by a whisp of smoke. It was damp. I discarded the tube's socket, cleaned up the panel, fitted another socket and tried again. This time there was a picture of sorts, but with no sync and flaring, distorted colour. The huge 48legged UPC1420CA chip IC401 contains the colour decoder and the sync and timebase generator stages. After cleaning this area of the panel I fitted a replacement. This restored the sync but did nothing for the colour.

So it was now a question of checking through the chroma circuit. My Mastercare manual is a rather poor photocopied affair with no waveforms. Nevertheless I found that the waveform at pin 5 of IC401 looked decidedly dodgy. This pin feeds the 2SA733 chroma delay line driver transistor Q602. A check showed that the latter had a collector-base leak, but the colour was still far from right when it had been replaced. Further time-consuming checks revealed corrosion across C609's leadout wires. It's a $2 \cdot 2 \mu \mathrm{~F}, 50 \mathrm{~V}$ electrolytic that decouples pin 4 of the chip. Cleaning the board and fitting a new capacitor restored the
colour, and in fact the picture was now of excellent quality. However the time I'd spent on the set was out of all proportion to any charge I could make. I replaced the back and put the set on soak test (ha ha!).

An hour later there was field collapse. After withdrawing the chassis and switching the set on again the raster was back. I searched for a dry-joint around the new field output chip. The joints looked satisfactory, but I did some resoldering here and there. All now seemed to be well, so I returned the set to the soak test bench and got on with the next job.

## Dead Ferguson FV31R

This was a Ferguson FV3IR VCR that was dead - its mains fuse had come to a violent end. The cause was failure of the BA159 start-up supply rectifier DP11. When I replaced it the machine sprang to life. It's a flimsy model with panels that have those nasty little resistors tacked all over the print side. A never-soldered one was dancing about loose inside the case. A free bonus, I supposed. The screws that secure the top panel to its frame are minute, almost watch screwdriver jobs. So are the top cover fixing screws. An unattractive recorder to work on, though the results are excellent: after recording and playing back bits of live television I had, on one occasion, to press the pause button to check that I was in fact watching a recording and not a live transmission.

## A Call from Greeneyes

As I finished the FV31R Greencyes gave me a call on the intercom.
"First, can I give your old brown suit to the jumble"? Secondly I've just phoned Davey Ruggles about some little glass tables. Thirdly he's got a TV that needs repair. He's coming round."
"No, o.k. and blast" I replied.
I gave the Saisho another glance. Field collapse, so I opened it up and started off once more. When the little service switch was wiggled sideways the field scan was restored. I pirated a similar switch from another set, fitted it. and got a solid raster. I was growing tired of the Saisho, the fairy and the hesitant young man. In fact I was getting hungry and had a slight headache. The serewdriver boxed up the set with minimal help from me and I put it back on soak test.

## Davey Ruggles' TX10

Then Davey Ruggles' van pulled into the drive, its tyres down to the canvas. He pulled a Ferguson set from amongst the mats on board and we put it on the bench. I opened it up to see the TX10 chassis, with the focus control cracking up as they do. There was a set under the bench just like Davey's. I'd had to tell its owner that the tube had gone, so he'd left the body with me for spares. In no time I'd fitted its focus control in Davey's set. Having set up the picture I took the set back to the van. Couldn't really charge for that.

As Davey left I saw that the Saisho's raster had once more collapsed. No amount of violence towards the cabinet would get it back up, so I told the set what I thought of it and took it apart again. When I switched the set on the raster was all right. Twenty minutes later it collapsed. It took me quite a time to establish that the set did this consistently when boxed up but behaved perfectly when it was out of its cabinet. I put it aside as Mrs. Ruff
came in with her Akai VSll2EK VCR.
"Sometimes it just wouldn't start up, Mr. Billhook" she said. "At other times it worked perfectly for weeks. Then old Pukey had a go and now it won't work at all."
"Who's old Pukey'?" I asked.
"The lodger of course" she said. "If he's messed it up he's out."

As I put the machine on the bench I heard something rattling inside. When I took the bottom off I found that the drive mechanism had been got at. The securing plate, with its microswitch, had been taken off and among the bits adrift were two large white channelled cogs, a pair of smaller ones, a couple of shaped metal pieces and a couple of plastic mouldings. I also found a few circlips and a pair of coiled springs about an inch long.

I studied the manual and followed the well-illustrated procedure for reassembling it all. At the end I'd the two springs left over and the mechanism jammed as the machine began to initiate. After puzzling for an hour over where the two springs should go I telephoned Akai. I was told that they should be curled around inside the channels in the underside of the two smatler gear-loading cogs. Having done this I set up the timing and found that the machine worked well - sometimes. At other times it seized half way through loading. I was back with the original fault.

Akai knew about this when I contacted them again. The fault arises as the machines age. The large plastic cogs get tired and misshapen and then sometimes prevent operation. They are surprisingly cheap from Akai. Fitting replacements completed the job.

When Mrs. Ruff returned I told her that the time her machine had taken to be put right would have to be reflected in the charge, which would be enough to buy several bottles of Spanish whisky. At this her eyes narrowed. She paid up and, clutching the machine, made for the door. "Start packing Pukey" she muttered.

I turned to the dreaded Saisho and took a more careful look at the circuit. The field drive comes from the large UPC1420CA chip l'd replaced at the start of the saga. Pins $21-24$ are associated with the vertical deflection. So I resoldered these four legs, boxed the set up and put it on test again.

## End of the Saisho Saga

It was still working merrily next day when the young man returned, this time with his wife. I showed them the picture, which was excellent, and told them that the charge would be $£ 45$.
"Lotta money" she said. "We won't bother. Crubbs Foodstore has new colour sets for ninety five quid. Put it as it was". And off they went.

1 limped back to the house and found that Greeneves was on the phone. She turned to me as I went in.
"There's someone on the phone who's upset a cup of coffee into their portable TV" she said. "Smoke came out of the back before it went bang. They don't want to spend much on it. Want to know if you'll see whether it's worth doing."

I pulled a face and patted the air in front of me. "I'm not quite myself at the moment. When l've simmered down l'll tell you why I want to become a traffic warden."

Greeneyes mentioned Davey. "What did you charge him?" she asked.
"Nothing" I said, "he's an old friend and needs all he"s got for some new tyres on his van. It's his living." Then I noticed that we were sitting around a large new mat. On top of the original.
"From Davey" said Greencyes.
"But you didn't need a mat" I said, "you wanted a couple of glass tables."
"I saw his tyres too - oh, and I gave him that old brown suit you didn't want."

## Video Output Circuits

The main factors that limit the h.f. response of a video output stage used to be quoted as collector load resistance and total output shunt capacitance, though the response could always be boosted by including precise-value peaking coils. Nowadays you are more likely to find reference to the time taken to charge or discharge the total output capacitance, or the time taken by the tube's input capacitance to do the same.

## HF Response

This different way of putting things highlights three aspects of circuit action. First, that despite a tube being a voltage-controlled device the drive source impedance must be low enough to enable the input capacitance to charge and discharge very rapidly in response to h.f. changes in the waveform. Secondly that the charge and discharge times may not be the same, which is true unless steps are taken to equalise them. Thus the h.f. response may be asymmetrical. Thirdly that the value of the output stage's load resistor is not the sole factor in establishing the top h.f. response. In other words the output waveform rise and fall times may be dissimilar, something that can be especially unwanted with data displays ete.

Fig. I illustrates this effect. It shows a basic video output transistor which is assumed to be biased to the mid-point of its characteristic. Thus the leading edge of a negative-going step input waveform will reduce the collector current and increase the collector voltage because of the reduced voltage across the load resistor. This cannot occur instantancously however because there is always some stray collector-chassis capacitance present. As a result, the shape of the amplified and inverted output waveform is rounded instead of being a step - the new potential reached at the collector following the negative-going step input depends on the time taken by the shunt capacitance to charge. When the input step waveform is positive-going the shunt capacitance is discharged via the transistor instead of being charged via the load resistor. Once more the output waveform is curved instead of being a step, but this time the curve is of much shorter duration because the transistor's impedance is much less than that of the load resistor.

Thus the rise time of the output waveform is determined by the time-constant of the load resistor and the shunt capacitance while the fall time is determined by the transistor`s impedance (plus the emitter resistance) and the shunt capacitance. Clearly if the pulse duration is less than


Fig. 1: Basic class A video output stage circuit, showing the effect of the load shunt capacitance with a squarewave input. When the transistor is switched off, the shunt capacitance has to charge via the load resistor, producing the lengthy output rise time a. When the transistor is switched on, the shunt capacitance is discharged via the much lower resistance of the transistor and its emitter resistor. Thus the output waveform fall time $b$ is much less than the rise time a.


Fig. 2 (left): Basic complementary-symmetry video output stage circuit.

Fig. 3 (right): Class A video output transistor stage with an emitter-follower transistor added to reduce the output waveform's rise time with a squarewave input.
either time-constant the shunt capacitance will begin to charge/discharge before the previous charge/discharge has been completed. If the pulse repetition frequency is high, the output waveform will be a poor reflection of the input waveform.

## Circuit Techniques

Various output stage circuits have been devised to reduce and equalise the shunt capacitance charge/discharge times, also to provide other advantages such as reduced transistor dissipation and improved tolerance to power supply variations.

The usual approach is to use a pair of output transistors connected across the supply, with the top one charging the output capacitance while the lower one discharges it. NPN transistors may be used in both positions or a complementary pair of pnp/npn transistors can be used. Fig. 2 shows an example of the latter arrangement. The lower transistor Tr 2 has d.e. input coupling while the input signal is a.c. coupled to the base of the upper transistor $\operatorname{Tr} 1$ by C1.

## Complementary-symmetry Circuit

Tr 2 's collector load is provided by $\mathrm{R} 4 / \mathrm{Trl}$ with R 6 in parallel. R4 and R5 also limit the power dissipation of the transistors and provide protection against tube flashovers.

The values of the emitter resistor decoupling capacitors C2 and C3 are selected to provide compensation, i.e. by being relatively small in value negative feedback is introduced by the emitter resistors at the lower and medium frequencies, reducing the gain at these frequencies to improve the overall linearity. The ratio of R8 to R7 determines the overall negative feedback and thus the stage gain, and also improves the stage's tolerance to h.t. variations. The base of Tr 1 is forward biased by $\mathrm{R} 1 / 2$. C 1 couples mainly the higher frequencies and transients to the base of $\operatorname{Trl}$. Though both transistors operate mainly as class A amplifiers, with high-amplitude h.f. signals the operation veers towards class B. Overall power dissipation with this circuit is much better than with a single-transistor stage.

## Two NPN-transistor Circuit

Use of a pair of npn transistors in a circuit such as that shown in Fig. 3 is a rather more common arrangement. Here Tr 2 is a conventional class A amplifier but the value of its load resistor R 1 is much higher than with a singletransistor circuit. This is made possible through the use of Trl as an emitter-follower to discharge the output capacitance when the signal at the collector of $\mathrm{Tr}_{2}$ is positive-going. R2 is included simply to reduce the dissipation in TrI. With a positive-going input at the base of $\operatorname{Tr} 2$ the output capacitance is rapidly discharged via D 1 . Tr2 and D2.

## Emitter-follower Output

A third way of improving and equalising the h.f. response is to take the entire output from an emitterfollower stage. Though an emitter-follower has less than unity gain its low output impedance means that the current gain is high, while removal of the output capacitance from the load resistor of the previous voltage-amplifier stage means that a much higher load resistor value can be used here. This more than compensates for the voltage loss introduced by the emitter-follower and markedly improves the h.f. performance.

## Causes of Shunt Capacitance

Various factors contribute to the output capacitance seen by a video output stage. These include each drive lead in a ribbon type connector. Lead capacitance to chassis can be taken as being about 10 pF , while that between adjacent leads is about 6 pF . Thus a very significant improvement in the capacitive loading is obtained by mounting the output transistors on the e.r.t.s base panel. Cross-lead capacitance has in practice far less effect than this figure suggests however. since if two adjacent leads carry identical signals the capacitance is nullified. With RGB amplifiers the output voltage difference between any two stages ranges from zero to about thirty per cent of the peak-to-peak value on many seenes. Thus the effective capacitance between adjacent leads is no more than about a third of the nominal value.

## Input Capacitance

Because the input capacitance of a common-emitter transistor amplifier is high - it's largely determined by the transistor's collector-base feedback capacitance, and varies with gain - a low-impedance drive is required. This is quite a complex matter and is fortunately taken care of by i.c. designers in modern TV sets.

# Choosing a Digital Multimeter 

Last month we took a brief look at digital multimeter operation, types of DMM and basic characteristics. Time to consider the various features offered by DMMs so that an informed choice can be made.

Most hand-held DMMs use a liquid crystal display (LCD) for the readout, with seven-segment numbers. Some early models had LCD panels that became dim and hard to read after a year or so as the display changed from black to a dirty, unreadable grey. In time some segments failed to light at all. The LCD technology used with today's DMMs has improved however and fading is no longer a problem with good-quality meters. But before purchasing a DMM with an LCD panel it's important to check that the digits are jet black: you can then be reasonably sure that it will stay like this for many years. An advantage with an LCD panel is that lots of function annunicators can be included in the readout.

Bench DMMs may use an LCD display panel, LEDs or a vacuum fluorescent display.

## How Many Digits?

How many digits do you need? This is the question most often asked by the first-time DMM buyer. A 3.5 digit display means that the meter has a maximum reading, or count, of 1999. Until quite recently this was the accepted standard for TV/video/microcomputer repair work. It's fine for outside servicing.

Greater accuracy and resolution are preferable on the bench, where the long-suffering TV/video/microcomputer engineer has to struggle with the latest state-of-the-art equipment. A DMM with at least a $32 / 3$ (maximum reading $30(0)$ ) or a $33 / 4$ ( $320(0)-4999$ counts) display is better.

The reason for this is simple. Suppose you are measuring 1.856 V with a 3.5 -digit DMM on its 2 V range. The reading you'll get is 1.856 V . But if you wished to measure 2.051 V you would have to switch up to the 20 V range, where the reading you'd get would be 2.05 V , which is not such an accurate result. With a 3200 count DMM however the 2 V range becomes 3.2 V and $2 \cdot 051 \mathrm{~V}$ reads out as that.

A 4.5 digit meter has a maximum readout of 19999 , ten times the resolution with a 3.5 digit meter. Personally I feel that for normal TV/video/microcomputer work a $33 / 4$-digit meter has at the present time sufficient accuracy.

Resolution is the smallest increment of change that a DMM can indicate on a particular range. For example the smallest change in value a $3 \cdot 5$-digit meter can read on its 2 V range (a.c. or d.c.) is $0 \cdot(001 \mathrm{~V}$. With a 4.5 -digit meter the resolution is ten times greater, i.e. 0.0$) 01 \mathrm{~V}$. On the $2 \mathrm{k} \Omega$ range a $3 \cdot 5$-digit meter has a resolution of $0 \cdot 001 \mathrm{k} \Omega$, i.e. $1 \Omega$.

Sensitivity is the smallest voltage change that a DMM can indicate on its lowest range. For example a $3 \cdot 5$-digit DMM whose lowest range is 200 mV has a maximum sensitivity of 0.1 mV or $1000 \mu \mathrm{~V}$. With a $4 \cdot 5$-digit meter on the same range the sensitivity is 0.01 mV or $10 \mu \mathrm{~V}$.

## Accuracy

It's no good having a DMM with lots of digits if you can't rely on its accuracy. Looking at a 1.9998 V readout is of no
help if the actual voltage is 2.0004 V . DMM accuracy is quoted as an error percentage ( $\pm \mathrm{X}$ per cent). This is where construction quality and stability are important. But as with any piece of electronic gear, calibration accuracy tends to drift with age.

Since the d.c. voltage supplies in modern TV sets and video equipment must be set to a high standard of accuracy, for TV/video/microcomputer servicing you need a well-designed, robust instrument with an accuracy of at least $\pm 0.5$ per cent. Unless critical circuit voltages are spoton, equipment won't work properly - if at all.

DMMs are rated to measure accurately at a specified room temperature - around $23^{\circ} \mathrm{C}$. Most however will work accurately over a fairly wide temperature range.

A high-performance, quality instrument is generally guaranteed to retain its specified accuracy for at least a year. After that it's necessary for the maker or a specialist firm to recalibrate the DMM. You'll notice that most manufacturers of low-cost DMMs don't specify long-term accuracy.

Some DMMs do however retain their accuracy. Twelve years ago I bought an inexpensive DMM from Tandy. This instrument has lived a hard and busy life. Despite this it has retained its specified $\pm 0.8$ per cent accuracy.

## Ranges

D.C. voltage ranges of 200 mV to 1 kV with a.c. voltage ranges of 200 mV to 750 V are essential for TV/video/microcomputer servicing. Ability to measure a.c. and d.c. up to a maximum of at least 10 A is also a requirement.
E.H.T. up to 40 kV can be measured with an e.h.t. probe plugged into the DMM. I prefer to use a separate, specialised e.h.t. probe with its own built-in meter however. These are available from Heathkit, B \& K Precision Test Instruments and Beckman Industrial. When high voltages are measured with an e.h.t. probe plugged into a DMM, damage can be done to both the DMM and the engineer should the earth lead become disconnected from chassis. So be warned. E.H.T. is the one thing that can wreck an otherwise apparently indestructable DMM.

It's useful to have a bar graph (analogue) scale. With this the TV/video engineer has the best of both worlds analogue and digital displays on the same multimeter. The bar graph display can be used for nulling and peaking measurements - then, if desired, a final accurate measurement can be made with the digital readout. Before buying your DMM, check that its bar graph has a fast update - a 20 per second rate is good. A slow update bar graph is useless for many measurements. Updating is handled by a microcomputer within the DMM. It may also enable the DMM to change ranges (not functions) without the need for manual switching. Decide for yourself whether or not you need a bar graph display.

## RMS Measurements

For some applications a DMM that measures true r.m.s. is desirable. It's more expensive to manufacture however, so the price rises accordingly. The r.m.s. (root mean
square) value of a sinewave is obtained by multiplying the peak current by 0.707 - see Fig. 1(a). The average value of a sinewave is 0.637 times the peak value. The majority of DMMs respond to the average value but are scaled to give the r.m.s. value readings. Such instruments are known as average-sensing or average-responding DMMs. They respond to a much narrower band of frequencies, typically $40-500 \mathrm{~Hz}$, than a true r.m.s. meter. When an a.c. waveform is more complicated - see Fig. I(b) - or consists of several different harmonics - Fig. 1(c) - it becomes more difficult to measure.

Crest factor is the ratio of peak signal value to r.m.s. value, and defines the limits within which a true r.m.s. meter will measure accurately. A true r.m.s. DMM responds to higher frequencies than an average-sensing instrument, perhaps to 20 kHz .

Plenty of complex a.c. waveforms are present in TV/video equipment. If your servicing is all done in the workshop an oscilloscope can be used to give an easy reading of the value of such waveforms. But it's often convenient to be able to measure r.m.s. values directly with a DMM. If you decide that true r.m.s. measurement is a must, bear in mind that this will add quite a bit to the price.

## Features

A DMM that's able to measure frequency enables you to check line drive and other signal frequencies in TV receivers quickly. You'll also be able to check the various critical frequencies in VCRs, camcorders and CD players.

If you decide that frequency measurement is a feature you require, be sure to obtain a DMM with an upper limit of at least 20 kHz , preferably higher - some DMMs measure up to 10 or 20 MHz .

When used with a special probe some DMMs provide temperature measurement. You can thus check transistor and component temperatures without burning your fingers. If the meter you select doesn't have temperature ranges you can buy an adaptor/probe that turns it into a temperature meter.

Data hold freezes the reading displayed when a button is depressed. Reading hold is a similar feature. Peak hold


Fig. 1: The average, r.m.s. and peak-to-peak values of a sinewave signal are shown at (a) and apply with both voltage and current measurements. Most DMMs respond to the average value but are calibrated for r.m.s. values. Nonsymmetrical waveforms, for example (b), or those that consist of several harmonics, e.g. (c), are more difficult to measure.

## METER SUPPLIERS

Avo/Megger: Megger Instruments Ltd., Archcliffe Road, Dover, Kent CT179EN. Tel. 0304202620.
Beckman Industrial: Beckman Industrial Ltd., Astec Building, High Street, Wollaston, Stourbridge, West Midlands DY8 4PG. Tel. 0384442394.
BK Precision: Canadian Instruments and Electronics Ltd., The Bass Building, Widdowson Close, Blenheim Industrial Estate, Bulwell, Nottingham NG6 8WB. Tel. 0602770 075.

Cirkit: Cirkit Distribution Ltd., Park Lane, Broxbourne, Herts EN107NQ. Tel. 0992444111.
Fluke/Philips: Philips Test and Measurement, Colonial Way, Watford WD2 4TT. Tel. 0923240511.
ITT: RS Components Ltd., PO Box 99, Corby, Northants NN17 9RS. Tel. 0536201234.
Metex: East Cornwall Components, 119 High Street, Wem, Shropshire SY4 5TT. Tel. 093932689.
Micronta: InterTan UK Ltd., Tandy Centre, Leamore Lane, Walsall WS2 7PS. Tel. 09227100000.
Solex/Soar: Analogue Numeric Devices Ltd., 25 Swannington Road, Cottage Lane Industrial Estate, Broughton Astley, Leicestershire LE9 6PD. Tel. 0455283 486.
retains the highest value obtained during a measurement that involves varying voltage or current levels.

A min-max function enables you to hook the DMM to the equipment under test and attend to other matters while the meter automatically stores the highest, lowest and true average (mean) of all its readings. This function is available with the Fluke Model 83, the B \& K Model 2912 and the Beckman Industrial Model DM97. It's handy when dealing with intermittent faults.

Many DMMs contain a piezoelectric buzzer that gives audible continuity checks. There's a cheerful beep when the resistance being checked is less than about 100$) \Omega$. This is a great help when PCB tracks are being checked for breaks and lead destinations are being traced, since you don't have to look at the DMM
Nearly all DMMs feature auto-polarity, which means that if you reverse the leads on a d.c. voltage or current range the meter indicates the value with a minus sign prefix.

Some DMMs now have inductance ranges. The Solex SM666 for example measures inductance values between 20 mH and 20 H .
A notable development is the Tandy Voice Meter which was reviewed in the February 1991 issue. This $32 / 3$-digit instrument not only displays the measured value but also announces it in a clear voice.

## Guarantee

Check the guarantee period before making your purchase. DMMs are reliable, but failure outside a short guarantee period would be disastrous. DMM guarantees range from ninety days to three years, with parts and labour warranty.

## Safety

Virtually all modern DMMs have protection against damage by accidental overloading. Since most DMMs are housed in a moulded plastic case an electric shock from the meter itself is unlikely, but make sure that the test input
sockets are recessed so that you won't place a finger on an unused socket and get a nasty shock. The test prods should have a finger protecting guard at the business end and a moulded plug. often angled, at the socket end.

If the internal high-energy fuse in a DMM blows as a result of an accidental overtoad, be sure that the replacement is of the correct type and rating. If it isn't and the meter is again overloaded it could be damaged, with possibly internal arcing, fire, an explosion and an electrical shock hazard for the user.

## The Choice

For the TV/video/microcomputer service engineer who works mostly at the bench a good-quality, hand-hedd DMM with plenty of functions and ranges and at least a $32 / 3$ - or $33 / 4$-digit display is a suitable choice. Such a DMM is relatively expensive, but the money is not wasted: it should be a profitable fong-term investment.

## Table 1: Digital multimeter specifications.

All meters have an LC display, a continuity test, overload protection and battery operation unless otherwise indicated. Prices exclude VAT.

## Avo

M2004: Hand-held meter with $33 / 4$-digit display. Autoranging; bar graph; diode test; d.c. accuracy 0.7 per cent; one current range (10A). £108.

M2005: As M2004 plus 3mA-10A a.c./d.c. ranges and range hold. 0.5 per cent d.c. accuracy. $£ 116.50$.

M2006: As M2004 plus data hold and $300 \mu \mathrm{~A}-10 \mathrm{~A}$ a.c./d.c. ranges. 0.25 per cent d.c. accuracy. $£ 156$.

M2007: As M2004 plus peak hold. $0 \cdot 1$ per cent d.c. accuracy. £212.50.

M2008: As M2007 plus true r.m.s. reading. $£ 247.50$.
M2036: Bench meter with $43 / 4$-digit display. Autoranging; $300 \mu \mathrm{~A}-15 \mathrm{~A}$ a.c./d.c. ranges; bar graph; diode test; data, peak and range hold; true r.m.s. reading; 0.05 per cent d.c. accuracy. £355.

M2037: As M2036 plus decibel measurements. $£ 378$.
M2042: As M2037 less autoranging and data, range and peak hold but with $300 \Omega-300 \mathrm{M} \Omega$ resistance ranges and $3 \mathrm{~mA}-20 \mathrm{~A}$ a.c./d.c. ranges. $£ 525$.

M801: Hand-held meter with 3-5-digit display. Diode test; d.c. accuracy 0.5 per cent. $£ 64$.

M806: Hand-held meter with 3 -5-digit display. Autoranging; bar graph; $200 \mathrm{mV}-600 \mathrm{~V}$ a.c. ranges; diode test; data and range hold; temperature measurement; d.c. accuracy 0.5 per cent. $£ 89$.

TD20: Probe meter with 3 -5-digit display. Autoranging; 2V500 V a.c. ranges; data hold; d.c. accuracy 0.5 per cent. £61-60.

## Beckman Industrial

HD153: Hand-held meter with 3.5-digit display. Autoranging; diode test; audible read-out tone; logic test; range hold; d.c. accuracy 0.25 per cent. $£ 129.95$.

For the outside engineer a wide variety of reasonablypriced $3 \cdot 5$-digit meters are available. It's best to get one that has the widest possible range of functions. Examples are the Beckman Industrial DM27XL, the Cirkit TMI75 and the B \& K 388 HD .

Table I is included to provide a guide to DMMs suitable for TV/video/microcomputer servicing. It lists only a relatively small number of the excellent DMMs that are now available - if every DMM was included the table would take up many pages of this issue. Before buying a DMM, get a copy of the manufacturer's product brochure.

In conclusion I hope that this article has given you a reasonable understanding of the basies of DMM operation and the factors to consider when making a choice.

Thanks are due to Megger Instruments, Sue Round of Beckman Industrial, B \& K Precision Test Instruments, Philips Test and Measurement, Louise of InterTan UK and Solex International for supplying technical information, catalogues and photographs.

4410B: Hand-held meter with 4.5 -digit display; diode test; true r.m.s. reading; d.c. accuracy 0.07 per cent. $£ 245$.

360B: Bench model with 3 -5-digit display. Diode test; 20』 range measures $0.01 \Omega$; true r.m.s. reading; d.c. accuracy 0.1 per cent; temperature measurement. $£ 286$.

850: Hand-held meter with 4.5-digit display. Diode test; frequency measurement; data hold; true r.m.s. reading; d.c. accuracy 0.05 per cent. $£ 185$.

DM27XL: Hand-held meter with 3 -5-digit display. Capacitance measurement; diode test; logic test; frequency measurement; transistor test; full annunicator set; d.c. accuracy 0.5 per cent. $£ 79$.

DM71: Probe meter with 3.5-digit display. Autoranging; diode test; data and touch hold; no current ranges. $£ 42$.

DM78: Pocket-size meter with 3-5-digit display. Autoranging; diode test; no current ranges; d.c. accuracy $0 \cdot 7-2$ per cent. $£ 24.50$.

DM97: Hand-held meter with $33 / 4$-digit ( 4000 count) display. Autoranging; bar graph; capacitance measurement; diode test; logic test; frequency measurement; data and peak hold; min-max; full annunicator set; d.c. accuracy 0.3 per cent. £95.

## B\&K Precision

2911: Hand-held meter with $33 / 4$-digit (3999 count) display. Autoranging; bar graph; diode test; temperature measurement with optional probe; d.c. accuracy 0.5 per cent. $£ 59$.

2912: As 2911 plus capacitance and frequency measurement; peak and data hold; min-max. D.C. accuracy 0.3 per cent. $£ 89$.

377: Compact test bench with $3 \cdot 5$-digit display. Diode, transistor and logic tests; capacitance and frequency measurement; temperature measurement with optional probe; d.c. accuracy 0.5 per cent. $£ 57$.

388HD: As 377 plus current measurement to 20A. Slightly larger case. £73.

2802B: Probe meter with 3 -5-digit display. Autoranging; diode test; data hold; no current ranges; d.c. accuracy 0.7 per cent. $£ 34$.

2860: Ruggedised hand-held meter with 3.5 -digit, 0.8 in. display. Diode test; 500 V a.c./d.c.; d.c. accuracy 0.5 per cent. £57.

2833: Bench model with 4 -5-digit display. Mains powering via adaptor. Diode test; frequency measurement; peak and data hold; decibel measurements; d.c. accuracy 0.05 per cent; no continuity test. £212.

2704: Hand-held meter with $3 \cdot 5$-digit display. Diode and transistor tests; capacitance measurement $1 \mathrm{pF}-20 \mu \mathrm{~F}$; resistance measurement $200 \Omega-2,000 \mathrm{M} \Omega$; temperature measurement with optional probe; d.c. accuracy 0.5 per cent. $£ 54$.

2703: As 2704 less transistor test and capacitance measurement. D.C. accuracy 0.8 per cent. $£ 34$.

2907: Hand-held meter with 3.5 -digit display. Logic test; capacitance measurement; peak hold; true r.m.s. reading; d.c. accuracy 0.1 per cent. $£ 139$.

2906: As 2907 less peak hold, capacitance measurement and true r.m.s. reading but with transistor test and temperature added. D.C. accuracy 0.25 per cent. $£ 90$.

2905: As 2906 less logic test and temperature measurement. D.C. accuracy 0.5 per cent. $£ 74$.

2940: Hand-held meter with 4.5-digit display. Diode test; data hold; frequency measurement; d.c. accuracy 0.05 per cent. £141.

2945: As 2940 plus true r.m.s. reading and temperature measurement. $£ 221$.

## Cirkit

TM115: Hand-held meter with 3.5-digit display. Diode and transistor tests; d.c. accuracy 0.5 per cent. $£ 28.91$.

TM135: Hand-held meter with 3-5-digit display. Diode and transistor tests; capacitance and temperature measurement; d.c. accuracy 0.5 per cent. $£ 39.96$.

TM175: Hand-held with 3 -5-digit display. Logic, diode and transistor tests; capacitance and frequency measurement; d.c. accuracy 0.5 per cent. $£ 49.99$.

TM5315B: Hand-held meter with 3.5 -digit display. Diode test; d.c. accuracy 0.8 per cent. $£ 17.38$.

TM5365: Hand-held meter with 3-5-digit display. Diode, transistor and logic tests; capacitance and frequency measurement; d.c. accuracy 0.5 per cent. $£ 32.96$.

TM5375: Hand-held meter with 3.5-digit display. Diode test; frequency measurement; d.c. accuracy 0.5 per cent. $£ 31.96$.

## Fluke (Philips)

45: Bench meter with 5-digit fluorescent readout. Dual display; diode test; data and touch hold; min-max; decibel measurements; frequency measurement; true r.m.s. reading; RS232 interface; d.c. accuracy 0.02 per cent. Mains powered with optional rechargeable battery. Temperature measurement with probe. $£ 499$.

73: Hand-held meter with $33 / 4$-digit display. Autoranging; bar graph; d.c. accuracy 0.7 per cent. £85.

75: As 73 plus range hold, diode beeper and autoranged mA ranges; d.c. accuracy 0.5 per cent. $£ 112$.

77: As 75 plus touch hold. D.C. accuracy 0.3 per cent. $£ 125$.
83: Hand-held meter with $33 / 4$-digit display. Autoranging; bar graph; diode test; data, range and touch hold; capacitance and frequency measurement; min-max; conductance measurement to $100,000 \mathrm{M} \Omega$; temperature measurement with probe; d.c. accuracy 0.3 per cent. $£ 179$.

85: As 83 but d.c. accuracy 0.1 per cent. $£ 199$.
87: As 85 but 4 -5-digit display plus true r.m.s. reading, special analogue pointer and peak min-max. £269.

## ITT

MX547: Bench model with $33 / 4$-digit ( 4000 count) display. Mains powered. Autoranging; data and peak hold; full annunicator set; true r.m.s. reading; temperature measurement; d.c. accuracy 0.1 per cent. $\mathbf{f} 269$.

MX570: Hybrid analogue (moving-coil) and digital meter with $33 / 4$-digit ( 4000 count) display. Autoranging; diode test; data, range and peak hold; full annunicator set; d.c. accuracy 0.5 per cent digital, 2 per cent analogue. $£ 165$.

## Metex

M818B: Hand-held meter with $33 / 4$-digit display. Autoranging; bar graph; diode test; data hold; frequency measurement; true r.m.s. reading; d.c. accuracy 0.5 per cent. £65-50.

M3630B: Hand-held meter with 3-5-digit display. Bar graph; capacitance measurement; diode and transistor tests; d.c. accuracy 0.3 per cent. $£ 64.50$.

M4650B: Hand-held meter with 4.5-digit display. Bar graph; capacitance measurement; data hold; diode and transistor tests; frequency measurement $0-200 \mathrm{kHz}$; d.c. accuracy 0.5 per cent. $£ 88 \cdot 50$.

## Micronta (Tandy)

22-164 Voice Meter: Hand-held meter with $32 / 3$-digit display. Autoranging; diode test; full annunicator set; d.c. accuracy 0.8 per cent. £79.95 inc. VAT.

22-165: Probe meter with 3 -5-digit display. Autoranging; data hold; full annunicator set; no current ranges. $£ 24.95$ inc. VAT.

22-194: Hand-held meter with $3 \cdot 5$-digit display. Diode and transistor tests; capacitance measurement; d.c. accuracy 0.8 per cent. $£ 59.95$ inc. VAT.

## Soar

ME530: Hand-held meter with 3.5-digit display. Autoranging; diode test; full annunicator set; d.c. accuracy 0.35 and 0.5 per cent. $£ 51$.

ME4040: Hand-held meter with $33 / 4$-digit display. Autoranging; bar graph; diode test; data hold; full annunicator set; frequency m.easurement; d.c. accuracy 0.3 per cent. Mains powering via ADP adaptor. £109.

## Solex

SM666: Hand-held meter with 3.5 -digit display. Diode and transistor tests; inductance and capacitance measurement; full annunicator set; d.c. accuracy 0.5 per cent. $£ 79$.

The above list is only a selection from various ranges to indicate the variety of DMMs available.

# VCR Clinic 

## Philips VR6185 (later 5V version)

How's this for a saga! The machine came in from another dealer with the complaint that it was dead. There was no clock, no signals were present and there was no deck activity. But the power supply was working. A check showed that the Wickman fuse on the family board was open-circuit, but replacing it didn't change any of the symptoms. Checks were carried out around the P8051A-H1-2-D2 syscon chip. Its supplies were present, the reset worked and the clock oscillator was o.k., but it gave no output. So a replacement was ordered. With this fitted the deck initialised but there was gibberish on the display and none of the keys worked. A new TMP47C87()N chip cured that. We'd no playback colour however. As the paint seals on the H-PLL control had been broken it was reset as per the manual. Finally all was well! I kept the machine for a few days on test however, just to be on the safe side. P.B.

## Grundig VS310

The symptoms here were that Fl flashed on the display and the machine wouldn't take in a cassette. A check can be made on the cassette-in switches at connection 3 of plug L12. The voltage here should be 5 V until the switches close, when it should drop to zero. But the voltage never rose above IV. A new M722ABI chip was required. P.B.

## Philips VR2334

I've had this fault on three of these machines now. The deck doesn't initialise and there's no clock display. With the first one that came along I temporarily fitted a new A630 panel. This proved that the fault was here. Scope checks showed that pin 38 (bus data in/out) of the 8050 chip was being held down. The chip had an internal leak.
P.B.

## NEC N831

When the covers of this NEC machine were removed I found a JVC HRD120 (Ferguson 3V35). Lucky that. The problem was no record or playback colour. A quick run round with the frequency counter showed that all the oscillators were running at the correct frequency. So why was the colour-killer operating? The colour/monochrome switching line was at mono because the colour/mono/test switch was leaky!
P.B.

## Philips VR6548

This model is a Sharp clone. Until this one came in the only problem I've had with these VCRs has been with the cassette tray - the symptom is intermittent failure to accept a cassette. Fitting the modified tray switch kit, part number 482221432583 , usually puts matters right. This particular machine also seemed to stall the loading motor at odd times. The cause was a faulty mode control switch. part no. 482227612482.
P.B.

## Sanyo VTC5150

Fast forward and rewind were o.k., but when play was selected the tape would lace up then, after a few seconds,

## Reports from Philip Blundell, AMIEIE, Ed Rowland, John Edwards, Mick Dutton, Graham Richards, S. Da Costa, E.M. Beddow, Roger Burchett and Nick Beer

unlace. The fact that the loading motor continued to run after the tape was fully laced drew attention to the afterload switch. It closed but the contacts were oxidised. A squirt of Electrolube cleared the trouble.
E.R.

## Mitsubishi HS307

We don't know whether this trade has a patron saint. If so he wasn't in a very benign mood when this machine came along. The complaint was that it sometimes failed to record the sound. We removed the plugs on the audio/control head and hard-wired the leads to the panel. This cured the problem and we though that was it. Two days later however the customer rang to say that although the sound was now being recorded it became distorted after an hour. The machine would then stop playing. A check showed that after an hour the capstan speed became erratic. The capstan motor would then stop altogether, after which the machine would work only in the rewind mode. Freezing the MN6168MBB chip IC4Al got the capstan motor running again and a replacement chip restored normal operation. Luckily we obtained one from a scrap machine, as the customer made it plain that he wouldn't pay for attending to a fault that wasn't present when the machine came in initially. Now how do you argue with that? E.R.

## Matsui VX800

The symptoms were slow rewind and fast forward, also tape chewing in the play mode. We initially suspected the clutch/idler assembly, but while running through the mechanical operations without a tape in we noticed that in the play mode the reel motor didn't rotate. A check showed that there was only $0 \cdot 5 \mathrm{~V}$ across its terminals. The culprit turned out be the 2SD1246 transistor Q2022 which was short-circuit base-to-emitter. It forms a low-resistance chassis return for the motor, which instead was relying on a couple of low-value resistors that are in paraltel with the transistor.
J.E.

## Mitsubishi HS-B20

Playback and the tape functions were o.k. but there was no E-E picture or sound. Channel selection was shown on the display and the tuning indicator searched normally for a station to lock to, but as none was found the search continued in vain, the monitor's sereen remaining blank. A check on the voltages around IC101 in the i.f./a.g.c. can showed that pin 2 was at a much lower voltage than its normal 5V. So the a.g.e. wasn't working and the signal was cut off. The cause was the $0 \cdot 1 \mu \mathrm{~F}, 35 \mathrm{~V}$ tantalum capacitor C105 which was leaky.
J.E.

## Matsui VX880

This machine would accept a cassette then almost immediately eject it, after which it would switch off. We noticed that during the attempt to load the tape the cassette-in symbol flickered on then, as the tape was ejected, off. The after-load leaf switch mounted on the carriage was o.k. We then made a careful study of the action of the mechanism during the cassette loading
operation. This showed that the leaf switch is activated by a lever driven by the side-mounted rotary cam, which is in turn driven directly by the loading motor. The lever pressed the leaf switch home all right but immediately returned back a small way so that the switch went opencircuit again. During the loading process the motor spun normally, but as soon as the cassette reached the bottom the motor reversed by about three revolutions. A meter connected across its terminals showed no reverse voltage when this occurred, thank goodness. A new loading motor cured the problem.
J.E.

## Saisho VR3600/Orion VCR-MD3

This machine cut out after a short while, i.e. it returned to standby, and wouldn't accept a cassette. I noticed that there was no sign of any jog from the loading mechanism, and when I tried to advance it by hand it was as solid as a rock. When the gearing on the tape transport was stripped down I saw that the master cam gear had disintegrated. After fitting a replacement and rebuilding the mechanism the machine ran smoothly.
G.R.

## Panasonic NV370

The E-E picture was half white and half black, i.e. there was hum on vision. $\mathrm{C} 1102(2,200 \mu \mathrm{~F})$ in the power supply was open-circuit. The playback picture was only slightly affected.
G.R.

## Hitachi VT410

The complaint was of vertical black and white bars instead of a picture during the first fifteen minutes of playback. On test we found that a tap on the panel would clear the fault. The signal appeared to be getting lost within IC202, but a replacement made no difference. We then found that connecting a scope probe to pin 14 of IC203 would remove the black and white bars, leaving snow on the screen. It seemed that the f.m. demodulator wasn't operating correctly and that as a result the dropout compensator was working overtime, causing instability in the form of the bars. Replacing IC201 cured the fault but it was impossible to prove which part of the chip was defective.
M.D.

## Philips VR6467

When a tape was being played there was no sound or vision, just a blank screen. This was due to absence of the 10 V supply at the head amplifier panel. Transistor 7607 ( BC 328 ) was open-circuit.
M.D.

## Panasonic NV370

The picture was o.k. with some tapes but with others there was rolling and a small white bar was visible at the bottom of the screen. Playback of the machine's own recordings was o.k. except for the white bar. After a lot of deck realignment we established that the fault was being caused by the drum assembly. The rotor base at the bottom had shifted slightly out of position, so that the pole switching was incorrect. Slight adjustment by loosening the hex nut in the base and realigning it put matters right.

All was now o.k. except for cue. When this was selected the machine ran in the cue mode but when the button was released it still ran in the cue mode though the cue sign disappeared from the display. The AN3822 capstan chip was faulty, pin 17 being virtually open-circuit when a check
was made between here and chassis.
A common problem with these machines is a dew indication. Touching the dew sensor on the deck with the tip of a hot soldering iron for about $20-30$ seconds usually provides a lasting cure. If the dew indication is erratic however the sensor is at fault.
S.DaC.

## Amstrad VCR4600 Mk II

The report over the telephone was "not rewinding". In due course I took the top off and saw a spotless mechanism would that they all were! The machine worked perfectly when it had warmed up. It was left overnight then sometimes failed to respond to any deck command, including eject, though the display changed to show the appropriate symbol.

On this machine the mode switch is operated via a bell crank and levers. Cleaning and greasing cleared the fault. A linkage like this is asking for trouble as there are too many points of friction and potential wear.

A few months later the mode switch itself started to play up, giving no rewind or fast forward.
R.B.

## Grundig VS310

Warble on sound was the complaint with this machine, which had already been somewhere else for repair. When we tested it the sound was indeed poor. We were told that the capstan belt and motor had been replaced. After checking that the power supply voltages and ripple levels were o.k. we removed the chassis screws and hinged it out so that we could watch the flywheel and belt running. There was a noticeable vibration with the belt, which looked new but didn't seem to be as tight as one would expect. When a new, original Grundig belt was fitted everything was all right. The old belt had a lot more stretch than the new one and was obviously not a proper Grundig spare. The usual fault with these belts is that they split and break, maybe due to the hard rubber of which they are made.
E.M.B.

## Mitsubishi HS-B30

This machine had been playing around for some time. A couple of calls had been made but nothing amiss had been found. Eventually we saw what was happening. The drum motor would slow to the point where line lock was lost on the TV set. When the wires that connect the drum motor to the servo panel were moved normality was restored. We removed the drum motor and found that the connector plug hadn't been pushed home fully. Refitting it restored normal operation.
E.M.B.

## Panasonic NV-M10

This camcorder was accused of not focusing. Indeed on test the image from the camera head was very strange. The centre could be focused fairly well manually, but it was as if a special-effects filter was fitted - the edge of the image was severely defocused. In addition the unit made no attempt to auto-focus. The cause of the auto-focus fault was that the lens focus ring moved much too freely: the bracket that holds the auto-focus motor and its gearing to the side of thelens was bent, so the gear wasn't contacting the focus ring. The bracket is made of very thin aluminium. A faulty lens was the cause of the focus fault. Putting two and two together I came to the conclusion that the unit had been dropped.
N.B.

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# Long-distance Television 

Roger Bunney

There was a steady decline in Sporadic E propagation during August, with infrequent openings, particularly towards the end of the month. The 7th was perhaps the most active day, with signals from North America in evidence. During mid-August the Perseids meteor shower caused considered press comment. It had its moments for Meteor Scatter enthusiasts, with signals reaching as high as Band III. The MS displays were evident in the night sky: I witnessed a particularly brilliant burn-up, with the meterorite streaking across the sky as a white slash of light. Tropospheric propagation, helped by true summer weather conditions and stable high-pressure systems, gave a lift to both reception and flagging spirits! The collated SpE log for the UK is as follows:

5/8/91 RAI (Italy) ch.IA; JRT/HTV (Yugoslavia) ch. E3.
6/8/91 RAI IA; TVE (Spain) E2, 3; + PTT (Switzerland) E2. 3; NRK (Norway) E2; DR (Denmark) E3.
7/8/91 TVE E2, 3, 4; TVE-2 E2; RAI IA, B, C; C+ (Canal Plus) L2, 3, 4; + PTT E2, 3; DR (Denmark) E3; JRT E4; MTV (Hungary) R2; CST (Czechoslovakia) R1. 2; SVT (Sweden) E2, 3, 4; NRK E2, 3, 4: TSS (USSR) R1, 2, 3; RUV (Iceland) E3, 4: ARD (West Germany) E2; RTP (Portugal) E3. In addition Band III SpE was noted and Simon Hamer received unidentified North American signals on chs. A2 and 3 .
8/8/91 TVE E3; RAIIA, B.
9/8/91 TVEE3; RAIIA; NRKE2.
10/8/91 SVTE2, 3; TSS R1, 2; NRK E2, 3; DR E3; TVE E3
11/8/91 RAIIA, B; JRTE3,4; MTV R1, 2; C+ L2,3; TSS RI, 2; DR E3; NRK E2, 3; TVP (Poland) R1, 2.
12/8/91 CST R1; DRE3; NRKE3.
13/8/91 RAIIA, B; C+ L2, 3; TVE E2, 3; ARD E2, 3; ARD E3; TVP R1, 2; TSS R1-7 (the Band III signals logged by Simon Hamer); JRT E3, 4: EPT (Greece) E3; RTSH (Albania) IC; MTV R1-4.
14/8/91 + PTT E2; TVE E2; SVT E2.
15/8/91 TVE E2,3.4.
16/8/91 TVE E2; RAIIA. B; JRT E3; SVT E3.
17/8/91 + PTT E2. 3; ARD E2; TVE E2; JRT E3; RAIIA. B; TSS R1; DR E3; TVR (Rumania) R2.
18/8/91 TVE E2, 3; C+ L2; ARD E2, 3, 4; ORF (Austria) E2a; RAI IA; JRT E3; NRK E2, 3, 4; SVT E2, 3,4; TSS R1; CSTR1; RUVE4.
20/8/91 ARD E2; TVE E3; RAIIA.

22/8/91 CST R1; JRT E3; TSS R1, 2; RAI IA; TVE E2. 3; C+L2.
23/8/91 CSTR1, 2; JRT E3; TVE E3.
24/8/91 RAI IB; + PTT E2, 3, 4; C+ L2; ORF E2a, 4; ARD E2, 3, 4; NRK E2; CST R1, 2; SVT E2; RUV E4; TVP R1; TVR R2.
25/8/91 TVE E2,3.
26/8/91 TVE E2; RAIIA.
29/8/91 RAIIA; TVE E3.

August 8th was the most active day for MS reception, while auroral activity was present on the 8th, 9th, 12th and 13th. On the latter date reflection occurred at up to Band III. Tropospheric propagation gradually improved from the middle of August, when there was a stationary highpressure system with hot days and clear nights. From the 14th there was tropospheric reception from West Germany, the Benelux countries and France on most days. The most dramatic reception occurred during late August/early September, when extensive loggings were made of German, Danish and Scandinavian stations in Band III and at u.h.f. In the south west reception was mainly from Spain and Ireland.

David Glenday spent a caravan holiday in a pineforested valley in Scotland during August. Despite 1,(0))ft hills all round he managed to receive Band III signals from Norway. So don't give up, wherever you happen to find yourself! Mark Baldwin in Northampton received TVE-I ch. E11 Montanchez (45kW) and a weak signal from Zamora ch. E37 (160kW) via tropospheric ducting on the 10th - an excellent catch so far north. Of relevance to F2 reception, Robert Copeman writes that the identifications RTQ-() and WIN Queensland are now being used by DDQ-().

My thanks to the following for sending in reception logs and reports: David Glenday, Arbroath; Peter Schubert, Rainham; Roger Fussell, Torpoint; Simon Hamer, Powys; Cyril Willis, King's Lynn; Mark Bladwin, Northampton; Brian Renforth, Newcastle; and Brian Williams. Penarth.

## News Reports

Poland: Apparently a $2,120 \mathrm{ft}$ high radio/TV tower near Lodz, 72 miles west of Warsaw, collapsed during renovation work. The tubular structure with 85 sections weighed 420 tons.
UK: Star TV, which is aimed at an "all-black" audience. has been given a ten year licence by the ITC and should be available, primarily via cable networks, from next April. LWT is to provide facilities and training.
Denmark: The government has given Kanal Danmark the go-ahead to form a third network. The Copenhagen-based private station will work with five other existing


Left: A weak Iranian (IRIB) test pattern received by lan Waller via Intelsat VA F11 at $63^{\circ} \mathrm{E}$. This was a low on the horizon signal. Centre: Thailand TV received by Anthony Mann in Perth, Western Australia, showing smudgy multi-path propagation. Right: An unidentified ch. E2+ test pattern received via F2 propagation by Ryn Muntjewerff in Holland. Any ideas?
commercial stations to offer both national and regional advertising.
Japan: NHK at present provides a one-hour daily HD-TV service, known as Hi-Vision. A full-time HD-TV service is to be started when the BS-3b satellite comes into operation. Programmes will be supplied by NHK and commercial broadcasters.
Latvia/USSR: Some four and a half million people in Riga, Tbilisi and Moscow can now receive via satellite three scrambled West European channels. The decoder required is made by Jerrold and costs about $£ 1$ a month to rent. The systems hope to be profitable by 1993.
Italy: Tele Piu's three-channel pay-TV service, which started in carly July, has proved to be a great success. The eneryption system, which involves a complete management service for invoicing. repairs etc., has been provided by the Dutch company Irdeto.
India: The FUBK test pattern is now being used in India: Delhi ch. E4 carries the identification " $\mathrm{CH}(44$ DELHI".

## Miscellany

The Jersey Post Office has issued a commemorative stamp set featuring satellite services. There are two 20 p and two 26p stamps. The 20p ones feature oceanography and Earth resolution, the $26 p$ stamps meteorology (Meteosat) and telecommunications (Olympus). Issued on March 19th, the attractive "Europa 91" set is still available from the Jersey Post Office, Dept 304. Postal Headquarters, St. Helier, Jersey JE1 1AB, Channel Islands. The price is $£ 1.47$ including postage - add a further 50 ) p for air-mail postage overseas. Cheques should be made payable to The Treasurer of the States.
In his Technical Topics column in the RSGB journal Radio Communication Pat Hawker mentions a new type of lamp bulb developed by Philips. The QL Lamp will also be marketed by GE-Thorn and Sylvania. Its significance from the radio angle is that it works by r.f. induction. Discussions on the operating frequency have suggested $2 \cdot 65 \mathrm{MHz}$, though consideration of 6.13 and 27 MHz have been suggested in the USA and $13 \cdot 56 \mathrm{MHz}$ has already been used. One can only speculate on the harmonic problems that could arise with 27 MHz bulbs $-2 \times 27 \mathrm{MHz}$ $=54 \mathrm{MHz}$, Band I centre! I shudder at the thought of the house mains wiring acting as a giant radiating acrial.

Interference has always been a prime concern of DXers. In recent times the increasing use of baby alarms, walkietalkies and other low-power devices operating in the 49-8249.98 MHz band has led to the loss of ch. R1. In theory the output from such devices should not exceed 10 mW , but in my experience the output levels from some units provide a coverage with a radius of up to a mile. Radio amateurs have noticed that some devices operate outside the allocated band - the Tomy Walkabout baby alarm for example was measured at 51.035 MHz .

In a recent issue of Six News Chris Gore, G3WOS, mentions extremely high-level hash experienced, especially on wet and windy days, at 50 MHz . Using a portable radio he traced the cause to an electric pole that supplied a water pumping station. No, not a cracked insulator: a mains wire insulation had broken down and was arcing to an insulator wire tie. Chris also tells of intermittent high-level 50 MHz radiation that was traced to a house one and a half miles away. The interference disappeared when the doorbell was pressed, a light was switched on or the phone was answered. Its cause was a burglar alarm mains on/off switch. The current pulse produced by pressing the doorbell etc. stopped the burglar alarm switch arcing oddly enough at 50 MHz .

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We're always interested to hear from others about their radio/ $\Gamma \mathrm{V}$ interference problems.

## Satellite TV

Olympus is now back in position at $19^{\circ} \mathrm{W}$ and has resumed normal operation. It left orbit on May 29th. following error commands from the Fucino uplink station. This was a dramatic rescue by British Aerospace.

Following its launch on August 14th, the Intelsat VI F5 craft at $36^{\circ} \mathrm{W}$ has been under test. It has 38 C band and ten Ku band tramsponders.

Super Channel is transmitting a daily one-hour US news service provided by the Consumer News and Business Channel (CNBC). also a breakfast time news package from the same source prepared for the European market. CNBC hopes to rival CNN in providing news services to Europe.

The music channel MTV plans an expansion to three channels by the end of 1993 , using video compression to provide the three channels via a single transponder

## Book Review

The fourth edition of Ku-Band Satellite TV, Theory. Installation and Repair, by Frank Baylin and Brent Gale. has been published by Baylin Publications. Boulder. Colorado, USA. The emphasis is definitely on the practical side, with a mass of photographs and drawings - even going into detail on installing a large dish in deep snow! This edition has additional contributions by that wellknown hacker John McCormac. It has been considerably expanded and is pretty well up to date.

The first parts of the book cover the basics and general theory of satellite launching. downlinks, path loss and
orbits. It then deals in considerable depth with the hardware - dishes, feedhorns, polarisers. LNBs, cables, actuator drive systems, receivers, demodulation and scrambling/decoding. There's a very long and in-depth treatment of system installation, both large and small: footings, alignment of polar and horizon mounts, distribution systems and interference are all covered. I was particularly interested in a discussion of the polyrod lens feed system and a section on retrofitting Ku-band hardware in a C-band feed, something I've experimented with and achieved some success. At the end of the book there are several appendices, notes on test equipment, lots
of footprints, a glossary of terms, a list of useful addresses and technical data.

The book has 3,432 pages in an $8.5 \times 11 \mathrm{in}$. format and weighs 21 lb . Considering the amount of information it contains, the book represents extremely good value at $£ 23$ including UK mainland postage (add a further ten per cent for air mail in Europe and twenty per cent for air mail elsewhere around the world). I can honestly recommend it. Orders should be sent to J. Vincent Technical Books, 24 Riverside Gardens, Purley, Reading, Berks RG8 8BX. Telephone or fax 0734414468 . If ordering from outside the UK, ensure that any draft is drawn on a London bank.

# Ferguson/Thorn Rental TV Models/chassis 

Alexander Allan

Following the video equivalents listing in the August issue, mainly relating to Ferguson/JVC/Thom rental VCRs, readers may find the Ferguson/Thorn rental TV chassis/model listing in Table I helpful. The three-figure numbers have a prefix number that indicates the rental chain. These are 5 for DER, 8 for Radio Rentals and 7 for Multibroadeast Focus and TVVC. Thus the 5170) is a DER set using the TX9 chassis and is more or less identical to the 8170 and 7170 . The TX100 range was not customised for the rental market and thus retains the Ferguson or Ulta model numbers. Two trial models fitted with the TX100 chassis, the S7971 and S7981, were extensively tried out by the rental companies in selected regions. This list includes modets from 1979 to October 1980.

It would be interesting to have similar listings for other brands. I recently had a Solavox CTV set in and had trouble finding an equivatent ITT remote control handset,
and I'm totally confused by the number of VCRs that use say Starp or Sanyo mechanisms.

Although I have only recently joined the league of selfemployed, I have to endorse Steve Beeching's views on the trade (Letters, March). Try obtaining information on say an Ericsson personal computer (an on-going problem of mine) and you begin to see the way in which the technology is going and the approach to providing information and spares. On the subject of computers, many publications suggest that it's not worthwhile trying to repair a faulty power supply as the unit is cheap and easy to replace. At say $£ 50$ plus VAT I suppose a replacement is cheaper than the cost of undertaking diagnosis and repair. But where do you get them from? I was told by one supplier that PSUs are not available to the public for safety reasons. They are a lot safer than the floating chassis used in today's CTV sets!

Table 1: Thorn rental models/chassis

| Model | Chassis | 311 | TX10 | 22D1 | TX100 | 3760 | TX9 | 6013 | TX10 | 37100 | TX9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 101 | 9900 | 757 | 9000 | 22D2 | TX100 | 3763 | 9600 | 6019 | TX10 | 37101 | TX9 |
| 102 | 9900 | 773 | 9000 | 22D3 | TX100 | 3764 | 9600 | 6021 | TX9 | 37103 | TX9 |
| 111 | 9900 | 776 | 9600 | 22G1 | TX100 | 3765 | TX10 | 6023 | TX9 | 37140 | TX90 |
| 112 | 9900 | 778 | 9000 | 22G2 | TX100 | 3787 | TX10 | 6031 | TX9 | 37141 | TX90 |
| 132 | 9600 | 782 | 9600 | 22G3 | TX100 | 3768 | TX9 | 6053 | TX9 | 37340 | TX10 |
| 133 | 9600 | 784 | 9600 | 2251 | TX100 | 3769 | TX9 | 6070 | TX9 | 37341 | TX10 |
| 134 | 9600 | 785 | 9600 | 2261 | TX100 | 3780 | TX9 | 6071 | TX9 | 37350 | TX9 |
| 142 | 9600 | 14C1 | TX90 | 2323 | TX100 | 3781 | TX9 | 6076 | TX9 | 37351 | TX9 |
| 143 | 9600 | 14C2 | TX90 | 2343 | TX100 | 3785 | TX10 | 6083 | TX10 | 37360 | TX9 |
| 144 | 9600 | 16A1 | TX90 | 2353 | TX100 | 3788 | TX10 | 6093 | TX9 | 37361 | TX9 |
| 170 | TX9 | 16A2 | TX90 | 2422 | TX100 | 3789 | 9600 | 6103 | TX10 | 37370 | TX10 |
| 171 | TX9 | 16A3 | TX9 | 2423 | TX100 | 3790 | TX9 | 6116 | TX9 | 37600 | TX9 |
| 190 | TX9 | 1764 | 9600 | 2433 | TX100 | 3791 | TX10 | 6121 | TX9 | 37650 | TX10 |
| 202 | 9000 | 1765 | 9600 | 2452 | TX100 | 3792 | TX9 | 6144 | TX10 | 37850 | TX10 |
| 203 | 9600 | 1785 | TX10 | 2453 | TX100 | 3793 | 9600 | 6170 | TX90 | 37953 | TX10 |
| 204 | 9600 | 1791 | 9600 | 2463 | TX100 | 3795 | TX10 | 6171 | TX90 | 37963 | TX10 |
| 213 | 9600 | 1796 | 9600 | 26D1 | TX100 | 3796 | TX10 | 6175 | TX90 | C28* | 9000 |
| 221 | 9000 | 1798 | 9600 | 26D2 | TX100 | 51A2 | TX100 | 6213 | TX9 | C30E* | 9000 |
| 232 | TX10 | 1799 | 9600 | 26D3 | TX100 | 51A3 | TX100 | 66B2 | TX100 | C43* | 9600 |
| 233 | TX10 | 20A1 | TX100 | 3722 | 9000 | 51A4 | TX100 | 66B3 | TX100 | 1 C 26 | 9600 |
| 242 | 9600 | 20A2 | TX100 | 3734 | 9600 | 51A5 | TX100 | 6603 | TX10 | 1C31 | 9600 |
| 243 | 9600 | 20C3 | TX100 | 3736 | 9600 | 59B2 | TX100 | 8154 | 9600 | 3C40E | 9900 |
| 244 | 9600 | 20E1 | TX90 | 3737 | 9600 | 59B3 | TX100 | 37041 | TX9 | 3C47E | 9600 |
| 262 | TX9 | 20E2 | TX90 | 3740 | 9000 | 59B4 | TX100 | 37060 | TX10 | MC01 | TX90 |
| 271 | TX9 | 20G1 | TX100 | 3742 | 9000 | 59B5 | TX100 | 37063 | TX10 | MC05 | TX90 |
| 272 | TX9 | 20G2 | TX100 | 3743 | 9600 | 59H5 | T×100 | 37081 | TX9 | S7971 | TX100 |
| 273 | TX9 | 20G3 | TX100 | 3747 | 9600 | 5164 | 9600 | 37090 | TX9 | S7981 | TX100 |
| 282 | TX10 | 2281 | TX100 | 3755 | TX9 | 6003 | TX10 | 37093 | TX9 |  |  |
| 283 | TX10 | $22 \mathrm{B2}$ | TX100 | 3757 | 9900 | 6004 | TX10 |  |  |  |  |
| 289 | TX10 | 22B5 | TX10 | 3758 | 9900 | 6012 | TX10 |  | With pr | 5,7or 8. |  |

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# East-West Modulator Circuits 

Joe Cieszynski

For the last fifteen years or so east-west correction in colour TV receivers has generally been carried out using some form of diode modulator. In the following article we'll examine the operation of this type of circuit, list the common faults encountered and outline fault diagnosis routines.

In the design of deflection coils there has always been a degree of trade-off between spot quality and deflection geometry. Since spot quality camnot be improved by external means, correction for pincushion distortion has been a traditional requirement in TV sets. It was simple to achieve the necessary correction in a monochrome set by using permanent magnets. This can't be done in a colour set because the magnets would interfere with the colour purity. In the first generation of colour sets a transductor was used to provide pincushion correction, modulating the line scan at field frequency and the field scan at line frequency.

The introduction of in-line gun colour tubes, along with precision made scan coil assemblies, removed the need for north-south correction and virtually eliminated the need for convergence correction. The price however was an increased amount of east-west (EW) distortion. By the time that the 30AX tube had been introduced scan coil construction had advanced to the stage where selfconvergence was possible, but the EW distortion had increased to about eight per cent. These new coils on the other hand had the desirable effect of providing optimum spot quality over the entire screen area in addition to selfconvergence and NS correction. Further advances in tube/yoke design have meant that external EW correction is required only with $110^{\circ}$ tubes.

## Scan Current Modulation

It's appropriate indeed to use the term modutator to describe the circuit employed for EW correction in modern sets, since the circuit amplitude modulates the 15.625 Hz line scan waveform with a parabolic 50 Hz waveform - Fig. 1 gives an impression of this. Fig. 2 illustrates the need for this modulation: it shows a pincushion distorted raster of


Fig. 1: Line scan current amplitude modulated by a fieldfrequency parabola.


Fig. 2: Correct width raster with east-west (pincushion) distortion.
correct width in relation to the c.r.t.'s screen. From this diagram you can see that the requirement is to reduce the line scan current during the earlier and later parts of each field scan.

The modulator is driven by a circuit that incorporates components to shape the sample waveform obtained from the field output stage. It includes EW adjustment controls and a width control. Modulation itself occurs in the line output stage, where critically tuned $L C$ circuits are switched by the modulator's power diodes. The idea is to vary the impedance of the line scan current path, but to do this only during the line scan period, not during the flyback. If the line flyback current were to be modulated, the line output stage tuning would be modulated with adverse effects on the e.h.t. (unless this is generated elsewhere).

Several versions of the diode modulator and driver have been used over the years, though the basic elements of the circuit have remained the same. Well look at the three basic versions of the modulator in the order in which they appeared in TV sets.

## Low-voltage Diode Modulator

A basic "low-voltage" two-diode modulator circuit is shown in Fig. 3. The two coils L1 and L2 on the line output transformer and the external coils L3 and L4 form a balanced bridge. It's because of this that $L 4$ is known as the EW bridge coil. In a monochrome receiver the bottom end of L3 would be connected directly to chassis and the scan current would flow via L3, C2, L5 and L1. The inclusion of L 4 , with the varying potential across C 4 , has the effect of varying the impedance of the scan current path and hence the scan current itself.

The current that flows in a coil depends, amongst other things, on the voltage across the coil. In this case the voltage across L3 is the sum of the h.t. voltage and the voltage across C 4 . The latter has two components, a d.e. voltage A and a 50 Hz parabola B , as shown in the diagram. Varying the d.c. voltage across C 4 affects the overall line scan current and thus the width. So this d.c. voltage is the width control voltage. If it's increased the voltage across L3 and the width are reduced. As the voltage across C4 falls that across L3 is increased and so is the overall picture width.

It's casy to see how modulation takes place. At the start and end of each field scan the parabola is at its maximum amplitude, so the voltage across L3 is at minimum. The reverse is the case at the centre of the screen. Altering the peak amplitude of the parabola affects the degree of scan current modulation.

So far so good. One might at this point be forgiven for wondering why the diodes are necessary. Why not simply stick with altering the impedance of the scan current path as described? The fact is however that we don't want to modulate the e.h.t. and any other supplies derived from the line output transformer. So the action of the line flyback must be isolated from the modulator. This is where the diodes come in.

Detailed, in-depth analysis of the operation of this circuit can become quite an involved business. Basically however the action of the diodes is to steer the scan current


Fig. 3: Basic low-voltage, two-diode EW modulator circuit.


Fig. 4: Basic high-voltage, two-diode EW modulator circuit.
through either L4 or L2, depending on the width setting, and the flyback current through Cl and a combination of C 3 and C5, again depending on the width. Cl and C 3 have critical values, because their reactances relate to those of L1, L3 and L4. Suffice it to say that the steering action of the diodes not only ensures correct amplitude modulation of the line scan current but also prevents modulation of the flyback by ensuring that the reactance and tuning of the line output transformer remain constant. In a monochrome set C 1 forms a resonant circuit with L 1 and L 3 to tune the line flyback. The EW modulation parabola can't be switched off during flyback, but the resonance conditions can be adjusted by the action of the diodes to maintain the tuning.

The l.t. voltage that's developed across C5 is more than just a by-product of the circuit action. C5 is responsible for balancing the bridge. The voltage across it is produced by the rectifying action of D1 and D2. Without a load, this voltage could build up to the point where the diodes would be permanently reverse biased: the circuit would then cease to work. A load resistor could be connected across C5 to provide a discharge path, but a more efficient approach is to use the voltage across C5 as a supply rail. In our example it's shown as being used to supply the audio output stage. This is simply because to maintain circuit operation the discharge current needs to be of the order of 1 A .

The circuit shown in Fig. 3 is called a low-voltage diode modulator because the diodes operate at the scan voltages and are thus relatively low-voltage devices. An advantage
of this circuit is that the damping effect of C 5 removes any ringing, leaving a clear raster. In addition the tuning characteristics of the circuit are such that it lends itself to being driven by a switch-mode power supply operating at line frequency.

## High-voltage Diode Modulator

Fig. 4 shows the basic "high voltage" two-diode modulator circuit. The term high-voltage relates to the fact that D1 acts as an efficiency diode across the line output transistor Trl. Thus its voltage rating must be much higher than that of D2 and both diodes in Fig. 3.
The circuits shown in Fig. 3 and Fig. 4 are basically very similar: to aid comparison, where components perform the same task they have been given the same reference numbers. The drive applied across C 4 is the same as that in the low-voltage circuit, and to all intents and purposes the circuit operation is the same.

The best way to analyse the high-voltage circuit is to look at each difference and examine why it has been made. The first thing to note is that C3 is no longer in parallel with D1 but is connected to a centre tap in the line output transformer's primary winding. This compensates for the transformer's stray capacitance, which would otherwise unbalance the bridge, causing modulation of the e.h.t. Tapping L1 replaces L2 (Fig. 3): each half of the primary winding forms one arm of the bridge. From the a.c. point of view, C3 is still effectively across D1.
Another improvement to the raster shape introduced with this circuit relates to the S-correction and the linearity control. The passive correction components C2 and L5 are fully effective only at the centre of the field scan. Because of the c.r.t. geometry, there's still slight distortion at the top and bottom of the screen. Adding C6 and tapping L5 provides modulated S-correction and linearity, giving the required correction. C6 and the lower section of L5 come into effect only at the start and the end of the field scan.

The bridge coil in Fig. 3 is replaced in Fig. 4 with the bridge transformer L4A/B. This change is necessary only when the line output stage is driven by a line-frequency switch-mode power supply. In this case the conduction of Trl cannot be easily controlled - the chopper transistor's conduction period takes priority. Because of this the switching of D2 may be delayed, giving rise to raster distortion. The bridge transformer L4 corrects for this. I should point out that this change would be necessary in the low-voltage circuit if it was driven from the power supply also that circuit designers in general prefer to use a separate, conventional line drive circuit rather than taking the drive from the chopper circuit (the trend has been to use higher-frequency chopper circuits, which are of course more efficient).

Loading coil L6 is necessary to maintain the critical tuning of the balanced bridge circuit.

The main advantage of the high-voltage circuit over the low-voltage version is that there's no need for a high current drain (from C5). This means that the circuit is more efficient. Unfortunately the omission of C5 means that the circuit is prone to ringing, so the setmaker may have to add damping resistors.

## Three-diode Circuit

Fig. 5 shows the basic three-diode high-voltage circuit, which combines the advantages of the two previous circuits, i.e. because of the action of C5/D1/D2 it's not prone to ringing, it provides modulated S-correction and


Fig. 5: Basic high-voltage, three-diode EW modulator.


Fig. 6: Simple EW modulator circuit that can be used when the e.h.t. is not generated in the line output stage. C7 is a filter capacitor.


Fig. 7: Typical EW modulator control/driver circuit. C7 corresponds with C4 in Figs. 3-5.
linearity, and can if required be driven by a switch-mode power supply without the need for a complex bridge transformer (the three-diode arrangement overcomes the switching problems.) The main problem with the circuit shown in Fig. 3 was the large discharge current required from C5: the discharge rate is much less with the threediode modulator.

## Simple Modulator

In some chassis, such as the Ferguson TX10, the e.h.t. is generated in the switch-mode power supply. When this is done the line output stage simply provides scan drive. The provision of EW modulation is a much simpler matter since we no longer need to worry about the e.h.t. being modulated. Fig. 6 shows how EW modulation can be applied. The usual S-correction (C2), linearity coil and flyback tuning ( Cl ) components are included. Scan current
amplitude depends on the modulator transistor's collector voltage. Increasing the d.c. voltage at the base of Tr 2 reduces its collector voltage. Thus Trl conducts more heavily and the width is increased. Superimposing a field parabola on the d.c. at the base of Tr 2 modulates the scan (and flyback) current.

## Driver Circuit

Fig. 7 shows a simple EW modulator control/driver circuit. Trl with the $C R$ networks in its base circuit acts as a Miller integrator to convert the incoming field-frequency sawtooth waveform into a parabola suitable for EW correction. A field-frequency sawtooth waveform can be obtained from a low-value resistor connected in series with the field scan coils, on the earthy side. RVI affects the phase shift introduced by C3/RVI, thus applying tilt to the parabola. The effect of this on the raster is to provide greater correction at one end of the field scan than at the other, compensating for c.r.t./yoke tolerances. RV1 is usually called the EW phase control. The amplitude of the parabola is determined by the EW amplitude control RV2.

Drive for the modulator is provided by the low-power amplifier Tr 2 (not necessarily a Darlington transistor). The bias applied to this transistor by RV3 sets the width. Thus the output at Tr 2 's emitter is a parabola that sits on a d.c. potential. With the circuit shown in Fig. 6, where the driver is directly comnected to the line output transistor. the output parabola would have to be inverted.

## Common Fault Conditions

Perhaps the most common problem in EW modulator circuits is dry-joints. The transformers and coils used are of relatively large size. This, combined with the fact that the components run quite warm, often results in the joints cracking after three-four years. As soon as the smallest fracture occurs, the high voltages at the terminals produce arcing. At the very least this will result in a burnt PCB.

Once that arcing has done its work the modulator will normally cease to function. The result will be a narrow raster with pincushion distortion. Repairing damage of this sort is usually not difficult, but it's advisable to resolder all joints in the power area of the modulator - you generally uncover a number of potential dry-joints in the process.

When a burn-up has occurred at an inductor terminal it's advisable to inspect the component visually as in some instances the heat and back-e.m.f.s in the open-circuit winding can damage it. In most cases a damaged coil will be discoloured. When this is noticed the component should be replaced even though the raster can be set up correctly. Since the diode modulator is a critically tuned circuit, if a winding has gone partially short-circuit due to overheating the tuning will inevitably alter. Even though the circuit may appear to function, unwanted transients can occur. resulting in intermittent destruction of the driver transistor or modulator diodes.

In many cases the viewer continues to watch his set when a dry-joint has devetoped, even though the width has reduced and the picture is distorted. He may even ignore the smoke signals coming from the rear of the set! As one customer explained to me a few years ago, "well the smoke stopped after a few minutes, so we were able to watch the rest of the programme". In such an event it will be necessary to test the diodes and the driver transistor for shorts and leakage. In addition, examine the inductors and carry out a visual inspection of the carbon resistors, looking for black or non-existent ones.

Another common problem is failure of the driver transistor. The symptom will be either an excessively wide raster or a narrow one, depending on whether the transistor has gone short- or open-circuit respectively. In either case the raster will have pincushion distortion.

In most cases the transistor goes short-circuit between its collector and emitter. Unless the transistor is a peculiar Darlington type, there are usually several equivalents that can be used. In many cases the driver is a pnp transistor, something that should be borne in mind when faced with an unknown transistor and no service information

## Faulty Modulator Diodes

When a modulator diode goes short-circuit the symptoms will vary, depending on the type of modulator (low- or high-voltage) and which particular diode has failed. In general one of two things will happen: the power supply will go into the trip condition or the width will be at one of its two extremes.

If you have a set that's tripping or blowing fuses, check the modulator diodes not only for shorts but also for highresistance reverse leakage. Also beware of the diode that breaks down only under load. Such a component may give perfectly good readings when checked with a test meter but will fail in operation, causing a power supply overload. If you decide to fit a substitute type diode, ensure that its ratings are high enough. Other characteristics may be important. Just because a certain type of diode is used in one chassis it doesn't follow that it will function for long in a different chassis - remember that there are low- and high-voltage modulators. As an example, the BYX7I was widely used in older receivers but its rating is such that it
cannot replace something like a BY223, which looks identical, or the much smaller but higher rated BY228.

## Defective Capacitors

The capacitors used in diode modulator circuits seldom give problems. If a capacitor does fail it's essential to use the correct type and value otherwise the critical tuning will be lost and the bridge will be unbalanced. Fitting the correct type often means ordering it from the manufacturer or his official distributor, as the capacitors can have obscure values and very high voltage ratings. Don't fit a near equivalent. I've come across a number of receivers in which this has been done: the result is regular failure of the driver transistor and in a few cases this continual failure leads to the associated inductor melting.

Should you encounter a receiver in which the driver transistor fails regularly for no apparent reason, and you've replaced the usual culprits such as the inductors and diodes, it's reasonable to suspect that the value of a capacitor has changed. Also be on the lookout for changed value resistors, though these are usually conspicuous as a result of their changed colour.

## Fault Diagnosis

Where there's raster distortion but the width is at neither extreme, the cause of the fault may be in either the modulator itself or the driver circuit. As a general rule if the raster is affected when the pincushion and width controls are adjusted the cause of the fault is likely to be in the modulator. Faults in the wave-shaping section of the control circuit are rare as it's a low-power signal circuit.


Where the width is at one extreme and you're uncertain as to whether the cause of the fault lies in the driver or the modulator a simple test usually works.

If the width is excessive and the driver transistor is not short-circuit, remove the transistor and switch the set on. If the width comes in it means that the driver transistor is being turned on excessively by a fault in the drive circuit. If on the other hand the width remains at maximum, the cause of the fault is in the modulator and is more than likely to be a defective diode.

If the width is at minimum and the driver transistor is not open-circuit, switch off and place a shorting link across the transistor's collector and emitter. Switch on and observe the raster. If the width increases, the fault lies in the driver circuit. If it remains at minimum the fault is in the modulator.


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Each month we provide an interesting case of TV/video servicing to exercise your ingenuity. These are not trick questions but are based on actual practical faults.

Real Technician was not in a particularly good mood this nippy autumn morning. He'd used his holiday entitlement, the workload was building up steadily and Service Manager was becoming more testy and irritable by the day. TV and video faults seemed to be getting more complex and obscure, and the customers more demanding. Nor had the descriptions of faults, written at the counter, become any better. This one just said "running away"! RT looked at it closely. It stood quite still on the awaitingrepair rack. Resisting the urge to write "tested, didn't move, returned as received" in the work-done space he carried it off to his bench with a jaundiced air.

It was a Toshiba VCR, Model V81B. RT loaded his Walt Disney test tape without enthusiasm. Rabbits and wizards, chipmunks and wise owls rushed to and fro across the screen, screeching at each other in even more squeaky tones than they generally do in cartoons, their images broken up by mistracking bars. The tape spools were turning much faster than usual, as if the machine was in the forward-search mode. It wasn't though, because the sound wasn't muted. RT pressed the rewind key to put the machine into reverse search. The result was a still picture, broken by a mistracking bar, with the tape now stationary. Anticipating auto shut-down, RT pressed the stop key and went to find the service manual.

When a tape is running too fast the likelihood, it seemed to RT, is that the capstan is turning too quickly, a perfectly reasonable assumption on the face of it. So RT turned to
the servo block diagram in the manual and studied it carefully. He discovered that the output from the capstan FG generator passes through an amplifier in IC502 before entering the main servo chip IC501. Knowing that lack of an FG feedback signal usually has the effect of increasing the motor speed, he started by examining the FG waveform. It was correct at the output from the preamplifier and at the input (pin 5) of IC501. Waveform 13, the capstan speed control signal from pin 15 of IC501, also looked like that shown in the block diagram.

RT had to turn to the circuit diagram to obtain information on the d.c. conditions in the servo. Here he discovered that the voltage applied to the motor, at the emitter of Q534, should be 6.79 V . RT's little meter, hooked to this point, gave a reading of 6.85 V . Could a capstan motor fail in such a way that it ran at twice the correct speed, or more, when the applied voltage was approximately right? It seemed unlikely, especially as this is no fancy direct-drive electronic motor - it's a cylindrically shaped brush type. Even if the motor wasn't running too fast because of an internal reason, why wasn't the servo reducing the supply voltage and current? RT was at a loss. Could it be that the control track pulses were not being read from the tape to control the motor? No, the motor drive voltage was normal. Could it be that... his eye reverted to the monitor screen, where two squirrels were chasing an owl - at normal speed! No noise bars, normal sound track pitch. The wretched machine had put itself right. RT measured the capstan motor voltage again: it was 6.82 V , very little different from before, when the tape was whizzing through. What could have caused the original symptom then? See next month for the answer and another item in the test case series.

## ANSWER TO TEST CASE 346 - page 898 last month -

It's a fact that chroma faults in VCRs are rare: the colour processing circuits run cool and lead a quiet life. Last month's story related to a Sony VHS machine with noisy, grainy colour in playback, though the luminance playback was fine.

If for any reason the playback chroma signal level is low the result is not colour desaturation: the a.g.c. system ensures that the colour burst amplitude, and with it the amplitude of the chroma signal itself, is held at the correct level over a wide variation in off-tape signal strength. High chrominance noise level usually indicates low signal level at the input to the colour processor chip. So the place to be with the oscilloscope probe is at the 627 kHz low-pass filter which separates the luminance f.m. and the colour-under signals, at the output from the playback preamplifiers. Failure here would most likely be due to the filter itself, which of course is not used in the record mode.

The playback envelope signal from the heads was fine. A clear, sharp signal could be traced through the low-pass filter (L80)2). At the input (pin 5) to the processor chip IC80] however the signal was weak and noisy. The coupling capacitor C808 was virtually open-circuit. A replacement saved the day.

[^1]Lick

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\end{tabular} \& \({ }_{\text {STKB260I }}\) \& ¢ 12.95 \& idarozo \& \(¢_{¢ 1.50}\) \& 2SA1106 \& \(\underline{2} .75\) \& HITACHI V17／17／19 \(\quad \$ 32.00\) \\
\hline \({ }^{\text {ANS512 }}\) AN515 \& \({ }_{52}{ }_{5}^{2} 295\) \& BA6219 \& ¢2．20 \& HA13001
HA13007 \& ¢1．50 \& LA4505 \& £2．80 \& STK465 \& \({ }_{69} 9.95\) \& \& \& tdazo30 \& £1．50 \& \({ }^{2}\) SA1186 \& ¢3．95 \& HITACHI VT35／39 \(\quad\) ¢34．00 \\
\hline AN5521 \& \(\underline{2.20}\) \& BA6238A \& ¢1．95 \& HA13119 \& £2．50 \& LA4508 \& 22.50 \& STK1050\｜ \& ¢7．25 \& \& \& tDA2510 \& ¢3．95 \& 2SA 1264 \& ¢1．95 \& JVC FERGUSON PV 31332G \\
\hline AN5610N \& \({ }^{4} 9.50\) \& BA6239A \& £2．20 \& HA\3118 \& ¢2．75 \& LA4510 \& \(\underline{18.75}\) \& STK1060 \& \(\underline{27.95}\) \& STR371 \& 55.20 \& TDA2600 \& ¢5．00 \& \({ }_{2}\) SAA 4159 \& ¢2．95 \& JVC FERGUSON PV 31332L \\
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\hline AN6136 \& \(\underline{\$ 1.95}\) \& \& \& La1140 \& £2．20 \& LA7808 \& £2．75 \& S1K2240 \& \({ }^{\text {c．}} 50\) \& STR1096 \& \({ }_{54} 5.95\) \& TDA4501 \& ¢4．50 \& \(2 \mathrm{SC1} 1913\) \& ¢1．20 \& PANASONIC VEH 0177．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．\(£ 21.50\) \\
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