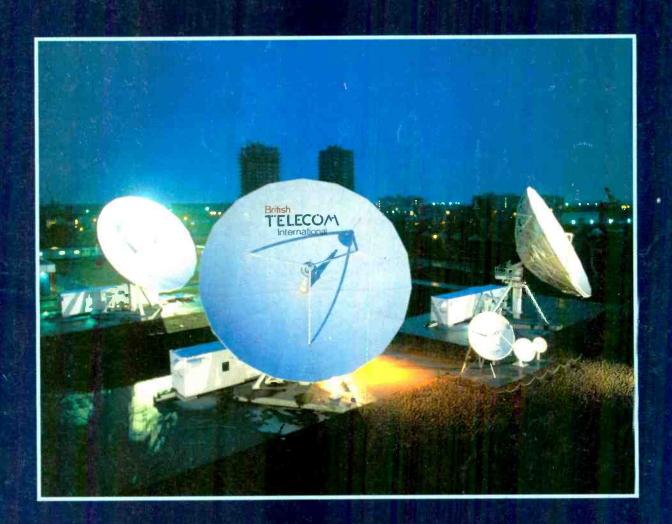
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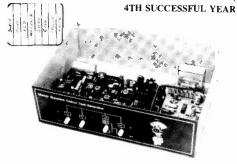




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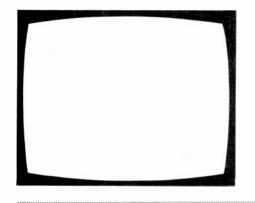
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TELEVISION

July 1985

Vol. 35, No. 9 Issue 417

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Requests for advice on dealing with servicing problems should be directed to our Queries Service. For details see our regular feature "Service Bureau". Send to the address given above (see "correspondence").

this month

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484 Letters

489 Big Foot

Les Lawry-Johns

Someone seems to be getting error prone. He might even end up in court.

490 Teletopics

News, comment and developments.

492 11GHz Low-noise Amplifier

Hugh Cocks

Building and testing a low-noise amplifier for satellite TV reception in the 11GHz band. The unit provides a gain of 25dB or better with a noise figure of around 3dB.

496 VCRs and the Mains Supply

Derek Snelling

VCRs are prone to a number of faults due to defective mains supplies. Symptoms and remedies.

497 Approaches to TV Servicing

S. Simon

One can work through test procedures that will eventually reveal the causes of most faults. Or one can assess the symptoms carefully and take short cuts based on experience. The latter course can save a great deal of time. Advice with examples based on common chassis.

499 Next Month in Television

500 The Lid off Microcomputers, part 3

Mike Phelan

This time a look at the basic system – CPU, memories, etc. – used in the Amstrad CPC464 microcomputer.

502 TV Fault Finding

Reports on TV faults and servicing from J. K. Potts, David Rainey, Mick Dutton, Philip Blundell, Eng. Tech., Stephen Howe and Malcolm Burrell.

506 VCR Clinic

Reports on videc faults from B. Ross, Steve Beeching, T. Eng., Derek Snelling, John Coombes and Philip Blundell, Eng. Tech.

508 Long-distance Television

Roger Bunney

Reports on DX conditions and reception, news from abroad and notes on DX equipment.

511 Making PCBs

Malcolm Burrell

A simple approach based on experience gained from producing boards for prototype equipment.

512 More on the Philips G8 Chassis

Dennis Apple, B.Sc.

Notes on servicing and fault finding. These sets can still give years of reliable operation if carefully serviced and adjusted.

514 Sonys and Suchlike

Nick Lyons

What have we done to deserve some of the odder problems that come our way? Sonys, a Contek portable and a troublesome monitor.

516 BBC Micro Test Pattern Program

Patrick Kniveton, B.Sc.Eng.

A program that provides most of the patterns normally produced by a TV pattern generator including a composite test card with circle.

518 Service Bureau

519 Test Case 271

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4022B 70 4053B 72 4163B 72 4531B 4023B 21 4060B 96 4502B 72 4532B 4024B 50 4066B 43 4505B 1.88 4536B 4025B 21 4068B 22 4510B 76 4538B	72 4597B 1.84 18 William 1.00 4598B 2.40 QUIL 14 will 1.04 16 will 16 will 16 will 18 William 1.04 16 will 18 William 18	vay 37 4.3Mhz IL to QUIL 8.8Mhz vay 32 9.94Mhz vay 36 10.692Mhz	1.30 100K 1.30 GEC TCE 6.00 PHILIPS (6.00 DECCA, R	S8 W ANK 55 S	MILE	DISC CERAMIC CAPS 8kV (12kV) 39pF, 200pF, 150pF, 220pF,	40p
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PHILIPS 320 8.70 THURN 1800/3500 PHILIPS GB 8.75 PHILIPS GB 8.75 PHILIPS GB 7.75 THORN 8000/8800 PHILIPS GB 13.50 DECCA 1730/1830 PYE 697 (Printed) 14.50 DECCA 30 DECCA 30	5.28 PHILIPS 7.15 PHILIPS 8.70 PHILIPS 4.48 PHILIPS	100 (800/250V) 1700 (200/200/400/350V) S GB (600/300V) S G9 (600/300V) S G11 (470/250V) 11/7 (200/300/350V)	5.32 10 2.53 22 2.44 16V 3	10 10 1 20 15 2 70 20 4 13 11 10	17 19 10 23 20 37	POLYESTER CAPS 250V 0.01mF 0.1mF 0.22mF 400V 0.01mF	12p
PYE 713/731 10.00 DECCA 80	6.60 PYE 731 7.50 RBM A8 7.600 RBM A8 7.40 RBM 21 6.50 RB1 T20	1 (600/300V) 823 (2500/2500/30V) 823 (600/300V) 146 (300/300/350V)	2.55 100 1.83 330 3.12 25V 1 3.91 2.20	10 53 220 0 11 <i>100V</i> 1 2 13 2 17 #5 4	00 85 10 1.10 10 13 12 15 17 20	0.1mF 0.22mF TANTALUM CAPACITORS 6.3V 47mF	42
DECCA 2230 8.58 GEC 2110 Pre Jan GEC 2110 Pre Jan GEC 2110 Prost Jan GEC 2110 Prost Jan GEC 2100 Prost Jan GEC 2040 9.50 PHILIPS GB Short PHILIPS GB Long PHILIPS GB	777 7.00 ITT CVCI 7.00 ITT CVC Focus Lead 6.75 GEC 211 Focus 550 6.75 GEC 204	C5/9 (200/200/75/25) C 20 (220/400V) 10 (600/250V) 40 (1000/2000/35V) 40 (300/300/150/100/50)	3.28 10 2.20 22 2.14 47 1.31 100 4.51 220	10 15 10 20 29 22 70 30 450 10 55 4. 10 51 1	00 36 20 70 1 33 .7 30		90 22 28 1.03
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Mains 10.00 THORN 1591 8.68 ITT KB CVC5/9 ITT KB CVC20/25/7 THORN TX10 15.00 THORN 1615 9.75 PHILIPS KT3 9.70	7.32 6.90 30 (Mullard) 6.65 6.80 8.65 THORN 1 THORN 1 THORN 1 THORN 1	3500 (1000/63V) 3500 (1000/70V) 8000/8500 (2500/2500/63V) 8000/8500 (700/250V) 8000/8500 (400/350V) 9000 (400/400V)	95 95 Volts D.C. 3.72 250V0.91ml 2.55 400V0.22ml 2.82 600V0.1mF 3.61 1000V0.01ml	CAPS F 1.15 1250V 0.1mF F 29 1500V 0.0047m 38 0.022mF 24 0.033mF	30 62	10mF CONVERGENCE POTS 3W/5R-6R8-10R-15R-20R 50R-100R-200R-500R	57
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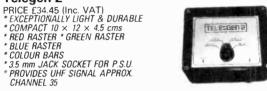
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2.5W Plastic 20W Stud	7.5-75V	64p each £1.35 each		UPC1367C	4.68	2 amp 12 way 0.19	9 Thorn 3000/3500 6R + 1R + 100R Fused 0.93
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400mW ~ 5 e	each value	- 11 values -		UPC2002V	2.78	10 amp 12 way 0.40 15 amp 12 way 0.46	7W - 0.47R to 22K - Available in preferred values 0.25
ually marked	and packe	ed – 55 Zener I £3.00 pe	Diodes er pack.	CA723 CA741	0.35 0.35	32 amp 12 way 0.90	1 11W = 180 to 22K = Available in preferred values 0.20
VALVES		TRANSISTO	ORS + D	IODES			
Type DY802	Price (£) 0.88	Type Pr	rice (£) 0.30		e (£) 0.10		Type Price (E) Type
DY86/87	0.86	AC128			0.10		BD244A 0.65 BF258 0.30 BT101/300 1.15 BYX36/150 0.22 TIC106A 0.70 2AC1449 0.63 BD375 0.32 BF259 0.32 BT101/500 1.25 BYX36/600 0.28 TIP30A 0.46 2SC1507 0.63
ECC81	0.95	AC128K	0.34	BC113	0.14	BC307 0.10	BD410 0.76 BF262 0.30 BT102/300 1.35 BYX48/300 0.72 TIP31C 0.54 2SC1678 1.06
ECC82	0.65	AC132	0.55	BC114	0.12	BC308A 0.10	BD434 0.68 BF263 0.30 BT102/500 1.65 BYX49/300 0.47 TIP32 0.40 2SC1758 0.68

Type	Price (E)		rice (E)	Type	Price (£)		ice (L)	Type	Price (E)	Type	Price (E)	Type	Price (£)	Type	Price (E)	Type	Price (£)	Туре	Price (£)
DY802	0.88	AC127	0.30	BC108	0.10	BC302	0.32	BD244A	0.65	BF258	0.30	BT101/300	1.15	BYX36/150	0.22	TIC106A	0.70	2AC1449	0.63
DY86/87	0.75	AC128	0.30	A,B or C	0.12	BC303	0.32	BD375	0.32	BF259	0.32	BT101/500	1.25	BYX36/600	0.28	TIP30A	0.46	2SC1507	0.63
ECC81	0.95	AC128K	0.34	BC113	0.14	BC307	0.10	BD410	0.76	BF262	0.30	BT102/300	1.35	BYX48/300	0.72	TIP31C	0.54	2SC1678	1.06
ECC82	0.65	AC132	0.55	BC114	0.12	BC308A	0.10	BD434	0.68	BF263	0.30	BT102/500	1.65	BYX49/300	0.47	TIP32	0.40	2SC1758	0.68
ECC83	1.10	AC141	0.26	BC115	0.12	BC323	0.99	BD436	0.68	BF270	0.30	BT106	1.50	BYX55/350	0.29	TIP32C	0.60	2SC1909	1.20
ECC84	0.65	AC141K	0.40	BC116	0.15	BC327	0.14	BD437	0.76	BF271	0.26	BT108	1.30	BYX55/600	0.33	TIP33A	0.63	2SC1923	0.30
ECC85	0.90	AC142	0.26	BC117	0.22	BC328	0.14	BD438	0.75	BF273	0.18	BT109	1.18	BYX71/600	1.18	TIP34A	0.72	2SC1945	2.88
ECC88				BC118	0.17	BC337	0.12	BD439	0.68	BF274	0.32	BT116	1.25	BYZ12	0.42	TIP41C	0.46	2SC1953	0.74
	0.95	AC142K	0.48	BC119	0.30	BC338	0.12	BD507	0.48	BF323	0.92	BT119	3.62	C106D	0.80	TIP42A	0.52	2SC1957	0.76
ECF80	0.95	AC151	0.45	BC125	0.12	BC350	0.14	BD508	0.53	BF336	0.26	BT120	3.60	E1222	0.40	TIP47	0.60	2SC1969	2.88
ECH81	0.75	AC152	0.45	BC140	0.28	BC440	0.30	BD509	0.54	BF337	0.26	BT121	3.02	E5024	0.30	TIP110	0.88	2SC2028	0.73
ECH84	0.75	AC176	0.28	BC141	0.42	BC441	0.32	BD510	0.48	BF338	0.26	BT138/600	1.30	GET872	0.48	TIP2955	0.60	2SC2029	2.10
ECL82	0.75	AC176K	0.46	BC142	0.30	BC461	0.32	BD517	0.56	BF355	0.42	BT151/560		ITT44	0.04	TIP3055	0.60	2SC2078	1.05
ECL86	0.98	AC187	0.42	BC143	0.30	BC547	0.12	BD520	0.66	BF363	0.82	BT151/300		ITT2002	0.11	TIS43	0.32	2SC2091	0.73
EF80	0.65	AC187K	0.48	BC147	0.08	BC548	0.12	BD699	1.25	BF367	0.24	BTY79/400		ME0402	0.20	TIS88	0.40	2SC2098	2.90
EF86	1.60	AC188	0.44	A or B	0.10	BC549	0.12	BD707	0.88	BF371	0.27	BU100A	2.30	ME0404/2	0.24	TIS90	0.25	2SC2122A	3.20
EF183	0.75	AC188K	0.50	BC148	0.08	BC550	0.18	BDX18	2.35	BF422	0.38	BU104	2.00	MEU21	0.60	TIS91	0.28	2SC2166	1.20
EF184	0.75	ACY40	0.88	A or B	0.10	BC550C	0.18	BDX32	2.10	BF450	0.38	BU105	1.20	MJ400	1.25	ZTX108	0.12	2SC2314	0.80
EH90		AD142	1.10	BC149	0.09	BC557	0.12	BF115	0.32	BF457	0.33	BU105/02	1.56	MJ2955	0.90	ZTX109	0.12	2SC2335	1.50
	0.94	AD143	1.10	BC157	0.10	BC558	0.12	BF117	0.54	BF458	0.36	BU108	1.80	MJ3000	1.98	ZTX212	0.28	2SC2371	0.90
EL34	3.25	AD149	0.96	BC158	0.10	BCX34	0.27	BF119	0.82	BF459	0.44	BU124	1.75	MJE240	0.60	IN4001	0.05	2SC2749	2.70
EL84	0.69	AD161	0.42	BC159	0.10	BCY70	0.15	BF120	0.38	BFR39	0.22	BU126	1.25	MJE340	0.54	IN4003	0.05	2SC2752	0.60
EL509	7.85	AD162	0.42	BC160	0.30	BCY71	0.17	BF123	0.40	BFR40	0.22	BU133	1.80	MJE370	0.88	IN4004	0.06	2SD234	0.64
EM87	2.55	AD161/AD16		BC161	0.30	BCY72	0.18	BF125	0.42	BFR41	0.22	BU204	1.35	MJE520	0.48	IN4006	0.07	2SD348	3.30
EY86/87	0.67	AF106	0.48	BC168B	0.12	BCZ10	1.68	BF127	0.38	BFR51	0.30	BU205	1.30	MJE2955	0.99	IN4007	0.07	2SD986	0.62
EY500A	1.65	AF114	2.10	BC169C	0.10	BCZ11	1.45	BF152	0.16	BFR61	0.32	BU206	1.70	MJE3055	0.70	IN4148	0.05	2SJ50	5.20
PCC84	0.50	AF115	2.10	BC170	0.14	BD124P	0.80	BF154	0.23	BFR62	0.28	BU208	1.55	MPSLO1	0.28	IN5400	0.12	2SK134	3.80
PCC85	1.36	AF116	2.10	BC170B	0.12	BD130Y	0.68	BF157	0.40	BFR88	0.34	BU208A	1.63	MRF475	2.50	IN5402	0.15	2SK135	4.60
PCC89	0.74	AF117	2.10	BC171	0.10	BD131	0.34	BF158	0.22	BFR90	1.72	BU208/02	2.05	MRF479	5.20	IN5405	0.16	3N126	1.90
PCC189	0.85	AF118	0.85	BC171	0.10	BD132	0.34	BF159	0.24	BFT41	0.38	BU326S	1.75	MRP477	10.00	IN5406	0.18	3N211	2.52
PCF80	0.75	AF121	0.62	A or B	0.08	BD131/BD132		BF160	0.23	BFT43	0 38	BU407	1.65	OA47	0.10	1N5408	0.20	3SK45	0.76
PCF86	1.25	AF124	0.48	BC172	0.08	BD135	0.32	BF167	0.30	BFW10	0.79	BU407D	1.80	OA90	0.08	1S920	80.0	3SK88	0.66
PCF200	1.95	AF125	0.48	A or B	0.12	BD136	0.36	BF173	0.25	BFW44	0.76	BUX80	3.70	OA91	0.09	2N697	0.55	3SK135	5.20
PCF801	1.45	AF126	0.48	BC177	0.20	BD137	0.36	BF177	0.42	BFX29	0.28	BUY20	1.75	OA95	0.18	2N706A	0.33		
PCF802	1.00	AF127	0.48	BC178A	0.22	BD138	0.38	BF178	0.30	BFX30	0.30	BUY69A	2.60	QA200	0.06	2N2904	0.28	I.C. SOC	KETS
PCF806	1.20	AF139	0.68	BC182	0.09	BD139	0.38	BF179	0.32	BFX80	3.56	BUY69B	1.98	OA202	0.15	2N 2906	0.24	Dil to Dil	
PCL82	0.90	AF178	0.68	A,B or C	0.09	BD140	0.38	BF180	0.35	BFX84	0.24	BY101	0.48	OC25	2.10	2N2926G	0.10	8 pin 0.0	8 0 70/10
PCL83	2.50	AF239	0.68	BC182L	0.09	BD144	1.60	BF181	0.35	BFX85	0.26	BY118	1.10	OC26	1.70	2N3053	0.40	14 pin 0.1	0.095/10
PCL84	1.30	AF279S	0.75	A,B or C	0.09	BD145	1.82	BF182	0.32	BFX86	0.26	BY122	0.68	OC28	1.50	2N3054	0.56	16 pin 0.1	
PCL86	1.15	AL100	2.50	BC183	0.09	BD150A	0.51	BF183	0.32	BFX87	0.26	BY126	0.12	OC29	2.47	2N3055	0.45	22 pin 0.2	
PCL805/8		AL102	5.90	A,B or C	0.10	BD159	0.65	BF184	0.32	BFX89	0.65	BY127	0.10	OC35	1.75	2N3702	0.10	28 pin 0.3	0 2 75/10
PD500	3.75	AL113	2.20	BC183L	0.08	BD160	1.65	BF185	0.32	BFY50	0.21	BY133	0.16	OC36	1.75	2N3704	0.10	40 pin 0.3	
PFL200	1.35	ASY80	1.75	A,B or C	0.12	BD165	0.45	BF194	0.08	BFY51	0.21	BY135	0.25	OC42	0.72	2N3708	0.10	-0 pin 0.3	3.10/10
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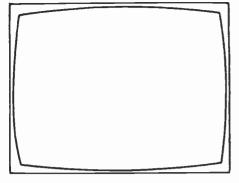
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TELEWISIOM

Reflections at Show Time

This year's radio and TV trade shows were not noteworthy for displays of innovatory consumer electronics products. But then what should we expect? You can hardly have major advances on an annual basis. For the present it's stand still time, though business appears to have been good. What lies ahead? Well, there must obviously be satellite TV receiving equipment to sell once DBS services have started, but for the present the satellite TV equipment field is very much a specialised one, with small batch production.

One impression left behind is of the overwhelming dominance nowadays of the Japanese in the consumer electronics field. Japanese manufacturers certainly had a good year in 1984 - it's been company reporting time. As mentioned last month, Matsushita had a record year. Since then Hitachi have reported profits up 37 per cent, Mitsubishi Electric profits up 52·3 per cent, Sharp profits up 21·5 per cent and Toshiba profits up 38 per cent, all on substantially increased turnover. These profit/turnover increases are for the parent companies however and cover a wider field than just consumer electronic products. In this connection it's perhaps more relevant that JVC, which is predominantly a producer of consumer electronic products, managed a profit increase of only four per cent on turnover up by 18 per cent. Stiff price competition in the VCR field was one of

the main factors blamed for this relatively poor result.

Japanese manufacturers have had a good run for their money. It looks as if they will do well again in 1985. This time the extraordinary thing is a sudden explosion in consumer demand in China, where over seven and a half million TV sets (a market size similar to that of Japan itself) are expected to be sold this year. The market is on Japan's doorstep, but it could well be an unpredictable one - demand has also been high recently for the whole range of domestic electrical products, from refrigerators and washing machines to pocket calculators. China is at present running a trade deficit and it's unlikely that the authorities will allow the situation to deteriorate to any marked extent. Furthermore the increased demand has been fuelled by an explosion of credit, which is unusual to say the least in a communist country. The central bank has expressed concern. There is of course a way around the trade deficit problem – another traditional Japanese ploy. This is to start up plants in the Chinese home market. Several joint venture projects have already been announced, by Philips as well as by Japanese manufacturers. It's a way of ensuring continued presence in a particular market, but one wonders how successful the ploy is financially. Japanese TV and VCR plants in the UK presumably exist primarily to guarantee a presence in the large EEC market, but they don't seem to have been wildly successful on a trading profit basis.

Internationally however fate has smiled upon the Japanese electrical manufacturers. When the European market reached saturation a couple of years ago there was a sudden increase in US demand. Now that the US market has turned flat the Chinese are clamouring for Japanese products. For how long can such a run of luck last? No sales chart has ever shown indefinite rising growth, and at some stage a halt to the rise is bound to occur. The developing world could certainly take a lot more production, but could it pay for this? One thing the Japanese expect is payment (you don't see Japanese banks lending billions upon billions to shaky S. American regimes - they leave that sort of thing to US and UK banks!). There is also the prospet of increased competition from Korea, which expects to export some two million VCRs over the next twelve months. We shall be seeing some of these in the UK, and they will sell at highly competitive prices. But Japanese electronics firms have managed to maintain their position despite competition from a number of lower cost producers in the far east. It will be interesting to see how the situation develops. After all Korea put the Japanese shipbuilding industry out of business many years ago now. But shipbuilding and steel manufacture are at the low-technology end of modern manufacturing. With consumer electronics the situation is rather different: the Japanese now dominate the technology, while the sheer size of their investment in modern plant would be hard to match. For the time being the Japanese lead in the field of TV and VCRs, but these are now mature markets in every sense. Product sales levels have reached saturation point in most markets, while technical development seems to have reached the end of its present phase. Money wouldn't have been poured into the FS tube if flat-screen displays were likely to be competitive, in terms of performance and price, in the foreseeable future, while digital TV doesn't for the present seem to offer much by way of improved performance. The field memory will give trick performance of the sort we're used to with VCRs, but will consumers want such features? One field that does offer scope for development and increased business is satellite TV of course

In this connection the government's decision to relax the regulations on satellite TV reception in the UK is a curious one. Unnecessary restrictions should certainly be removed, but an odd situation could develop. Just suppose that a reasonable market develops for equipment to receive the medium-power satellites at present in operation providing signals intended primarily for cable networks. Mightn't this make it more difficult to get true DBS broadcasting, started, something that's proving difficult enough as it is? The decision looks to be a bit of a gamble, maybe just to get something, somehow, moving.

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OBSCURE BRANDS

Many thanks to several readers who have provided information on Sovereign TV. We will be reporting next month. We have also received letters asking about Sonatel TV but have been unable to trace any source of spares, data etc. Can anyone provide information on this brand?

A DIFFICULT MONTH

Our apologies for any shortcomings this month. We've been involved in an office move (the address remains the same) which hasn't helped exactly. More seriously Dave Davies, who does our technical drawings, is in hospital. We are sure all readers will join in wishing him a speedy recovery.

FRONT COVER

This month's cover photograph shows a night scene at The London Teleport, British Telecom International's satelliteearth station in the Docklands. The Teleport transmits TV channels to cable networks in the UK and continental Europe. Our thanks to BTI for permission to reproduce the photograph.

Letters

IBA's TELETEXT EXPERIMENTS

Eugene Trundle's words of wisdom on "Dealing with Teletext Interference" (May issue) were useful and timely. As a result of the IBA tests he mentioned, the use of up to seven lines per field for teletext has now been authorized for all ITV regions. We had hoped to extend this to perhaps ten lines per field, but the tests in selected ITV regions showed that significant numbers of receivers that experience top-of-the-picture interference when a higher number of lines is employed are still in regular use. These are mostly older models and the number of lines will be limited to seven until most of these sets have either been modified or discarded.

On a point of history I'd like to make a correction. It was the IBA that made the first experimental transmissions of teletext-type signals from the Crystal Palace transmitter, during April 1973 – including "live" computer editing. The very first transmission was made during our "Engineering Announcements" on April 3rd, 1973. It was announced by Peter Ashforth as follows: "Just before we go this week, some of you may be interested to hear that for the past ten minutes or so during the bulletin we've been transmitting a special type of signal which carries information in data form: the information is transmitted during the blanking interval of the television and so, of course, can't be seen on a normal receiver." A filmed report of that early IBA teletext system, by Peter Fairley, then science correspondent of ITN, was broadcast during May 1973.

The IBA later willingly co-operated with the BBC, BREMA and the Home Office in establishing in 1974 the unified UK standard for teletext now used in some twenty countries across the world. Transmissions to this standard were first made by both the IBA and the BBC during the September 1974 International Broadcasting Convention. During our 1973 tests we identified the problems of data buzz and top-of-the-picture interference and the 1974 teletext specification took care to minimise the problem, which is inherently a question of receiver design.

The IBA "Engineering Announcements" referred to above still continue on the Channel 4/S4C network on Tuesdays at 9·15 a.m. and 12·15 p.m. IBA engineering information is also available at all times on Oracle page 590 (C4/S4C), with a list of Channel 4 transmitter conversions on page 390 (ITV).

Pat Hawker,

IBA Engineering Information Service.

SCOTCHTAPE CASSETTES

With reference to Mr. Henniker's letter in your May issue, the Lifetime Guarantee that 3M pledges with its market-leading Scotch videocassettes is supported by prompt, responsive action whenever a VCR owner or a retailer brings a faulty tape to our attention. It's a necessary part of the Guarantee that tapes presumed to be faulty are returned to us. To make returns painless – and free – for our customers all Scotch cassettes are sold with a Freepost label addressed to our Gorseinon, Swansea videotape factory. We check returned tapes to identify the problem – which in seven cases out of ten is due to machine damage or mishandling. We work closely with hardware manufacturers and retailers' service depart-

ments to ensure fault elimination and constant product improvement. What we cannot do is to replace tapes without seeing them.

Before writing to you Mr. Henniker was contacted by our Glasgow sales office, by our Bracknell head office, and was visited personally by our area representative – all in an attempt by 3M to give him satisfaction for his allegedly faulty L250 tape. On all occasions he has refused to return the tape to us.

Perhaps I can use your columns to appeal again to Mr. Henniker to send us the cassette? It will be replaced immediately with a new tape, and we would welcome the opportunity for our engineers to investigate the alleged fault.

D. J. Skinner, Field Service Manager, Video Technical Centre, 3M United Kingdom PLC.

PYE HYBRID CTV MODIFICATION

I was recently asked by a friend to repair an ageing Pye hybrid colour set (691-697 chassis). The main fault was quickly dealt with. On viewing the picture however there appeared to be a lack of d.c. restoration, which I found annoying. The set had at some stage been fitted with a LEDCo CDA panel, so I looked up the circuit diagram given in the June 1979 issue of *Television*. This revealed a design problem with the link to the brightness control and since I wanted to do a good job for my friend (and I might occasionally have to watch the set myself) I decided to seek a solution. Although these sets are old many of them must still be in use so other readers may be interested in the solution I found. It's not perfect since the beam limiter action isn't as effective as it was.

Fig. 1(a) shows the initial arrangement with the luminance signal coupled by C39 to the first transistor (VT701) on the LEDCo panel. It will be seen that the base of VT701 is forward biased by R701/2. The voltage at the slider of the brightness control will be negative however (or possibly slightly positive – D39A will prevent the voltage at the top end of the control being much above zero). Hence the d.c. restorer diode D39 will always be heavily reversed biased and no d.c. restoration can take place. In the original valve circuit the luminance output pentode's control grid would have been biased negatively from the brightness control via R201 and D39 would have prevented any part of the video signal going below the voltage on C201, set by the brightness control. D.C. restoration of the signal was thus achieved.

The solution adopted was to remove R701 and R702 from the LEDCo panel and alter the brightness control

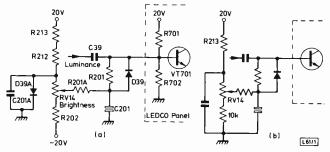


Fig. 1: Brightness control/d.c. restorer circuit used in the Pye 691-697 series chassis, (a) before modification, (b) after modification. Modification was required due to the use of a LEDCo solid-state CDA panel. Note that the collector of the beam limiter transistor VT35 is connected to the junction of resistors R212/R213, so the modification affects the limiting action.

circuit to provide a positive voltage on C201 so that the circuit could bias the base of VT701 directly, as it did the PL802's control grid in the original valve circuit. The modification is quite simple – see Fig. 1(b): D39A and R202 are removed, R212 is replaced with a link and an extra $10k\Omega$ resistor is added between the bottom end of the brightness control and chassis.

The results were quite rewarding: dark pictures are really dark and bright pictures bright, with no black crushing. The only slight drawback is inadequate beam limiting: if the brightness or contrast is set too high there's severe loss of focus. This is no problem however with sensible settings of the controls. Time prevented further investigation into this problem – and I'm not sure that the tube wasn't partly responsible anyway. All in all a worthwhile exercise which should help keep these sets alive even longer.

Anthony Marlow, M.A., Sale, Cheshire.

BBC MICROCOMPUTER PROGRAM

Some alterations are required to the BBC microcomputer program in the June issue (page 446). First, the bit in brackets at the end of line 50 should be (10, "."). The difference is in the spacing – the string is too long with the additional spaces you had at each side of the stop. Secondly, in lines 70 and 80 6% should in each case read c%.

Adding an extra line at the beginning of the program as follows:

5 *TV0,1

stops the interlace jitter.

Changing the last line to:

180 IF GET=9

MODE7:PRINTTAB(13,12)"GOODBYE":

END ELSE UNTIL 0

causes GOODBYE to be printed when exiting the program.

Roger Goodman,

Wandsworth, London SW18.

POINTS ON VCRs

In the May VCR Clinic Steve Beeching said that the Hitachi VT8700 was the first VCR he'd come across that would work without a cassette lamp. This gives the impression that the machine will work in the event of cassette lamp failure, which is not the case. As with all the VCRs in the Hitachi 8000 series, lamp failure is detected by the control microcomputer i.c.'s dew sense input (IC901, pin 33). Failure results in the stop condition with the stop light flashing. The relevant bit of circuit (for the VT8700) is shown in Fig. 2. Under normal operating conditions the lamp is alight and the cathode of zener diode ZD651 is held at a low voltage. If the cassette lamp fails there's no current flow via R653 and ZD651's cathode is at 15V. Being a 9V zener diode it conducts and, via D651, provides a high to IC901's dew sensor input. In Steve's case the lamp was o.k. but the feed resistor was open-circuit, so the safety circuit didn't operate. A weakness in the design perhaps, but it's the first case of this resistor going open-circuit I've heard of and I've had only two faulty cassette lamps.

On the subject of liquids spilt into VCRs, a colleague recently had a Panasonic NV2000 which a pet had used as

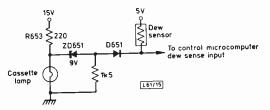


Fig. 2: Cassette lamp/dew sensor circuit used in the Hitachi VCR Model VT8700.

a toilet. It took three weeks to clean and locate the faults, was back with the customer for two weeks then had to come back for further repairs (it's still not fixed). The problem is that as fast as one fault is cured another appears, and they are all obscure faults that wouldn't happen under normal circumstances. I reckon we average one machine a month with spillage of some sort. With chargeable jobs, if the household insurance won't cover the repairs it can be uneconomical to try even without replacement panels – which some manufacturers won't provide anyway.

Finally, I must make a few comments concerning the letters about the present state of the TV trade and its future. I consider training in all industries to be the employer's responsibility, and that this is one of the country's biggest failings in the present economic climate. As to the future, while the service side is no longer expanding the increasing number of VCRs and microcomputers requiring attention are beginning to take up the slack caused by the increased reliability of TV sets. I agree that it's going to be difficult to get into the trade, but for those already in it the future should be reasonably secure, at least for another five to ten years – provided you keep up with the trends.

Derek Snelling, Brownhills, Staffs.

TELETEXT BLANKING CIRCUIT

While chasing an intermittent fault in a Beovision 2600 I thought I'd try out the blanking circuit shown in Fig. 3(a) on page 372 of the May issue. I was suspicious about the connection shown to the field output transformer, feeling that the phasing was incorrect. Sure enough it is! If you connect up as shown the bottom half of the picture is blanked out with teletext flashing merrily in the upper half. The $0.1\mu F$ capacitor has to go to the same point on the transformer as the blanking circuit feed, i.e. the top of the winding shown in Fig. 3(a) not the bottom. Wired like this is works fine.

Keith Cummins, Southampton, Hants.

PORTABLE CRT TESTER

With reference to Tony Thompson's comment about a portable CRT tester (May 1985) the converter circuit shown in Fig. 3 will produce a 240V a.c. output from a

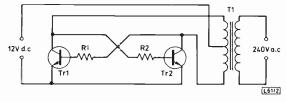


Fig. 3: Converter circuit for 12V d.c. to 240V a.c. Tr1, 2 type 2N3055; R1, 2 100Ω , 10W w.w.; transformer T1 is rated at 20VA and has 12-0-12V and 240V mains windings.

12V rechargeable dryfit lead-acid battery. It can be used with James Dilworth's CRT tester/booster which was described in the August 1981 issue of *Television*.

N. E. Hawkins,

Milton Keynes, Bucks.

THAT G11 MULTIFAILURE

With reference to Ivan C. Tucker's article on G11 problems, I'm sure that a lot of us have by now had first-hand experience of the $red~470\mu F$ capacitor causing damage to the tube, the TDA2600 and the BU208A. Unfortunately the blue capacitors are not 100 per cent reliable either: I had to replace one two weeks ago because it destroyed BU208As.

So what happens if the same thing occurs again six months after replacing these parts? The customer complains to you! You return the tube with its unmistakable little star in the neck to the supplier, who won't replace it because he knows it was caused by the capacitor! The supplier of the capacitor *might* replace that but not the chip etc. Has anyone out there got a sensible answer before one of us gets really stung?

J. Hopkins, The TV Workshop,

Wisbech, Cambs.

SLIPPED SHADOWMASK

Here's an unusual "horror story" concerning a Bush set fitted with the Z718 chassis. On switching on one evening the picture showed severe colour errors, e.g. the snooker table was brilliant purple. A replacement decoder panel made no difference, so maybe it was a degaussing fault or a slipped shadowmask? The degaussing circuit turned out to be o.k., and putting the set on its side in the hope that the mask might return to its correct position brought no change.

We checked to see which guns were firing at which phosphors. Result, red was firing at green, green at blue and blue at red. So let's reconnect the video outputs appropriately. This gave true colours but shameful convergence. At this point we had a bit of luck, which we needed. Whilst examining the convergence strip at the top of the chassis we accidently removed the convergence waveforms by disconnecting the plug from the line output board. With no waveforms to displace the beams we found we had an almost correctly converged picture. This was optimised by adjustment of the red and blue static convergence magnets, giving correct colour across four fifths of the screen with aberrations on the left-hand side. Viewing from ten feet gives a very reasonable picture which has remained stable for some three years. P. R. Atkins,

Southall, Middx.

SPECTRUM TEST PATTERN PROGRAM

As a result of correspondence following my Spectrum test card program (May) I've discovered that not all editions of the Spectrum manual contain a colour bar program. Also when the colour bar program is included it has the bars at two brightness levels and they don't fill the bottom lines of the screen. They also have numbers printed on them to indicate the keys relating to the colours. This feature may be required to set up the Spectrum with a TV set or monitor, but for TV test purposes full-brightness bars filling the entire screen area are required.

Unfortunately there's no way in which the bars can

extend all the way to the border, but it's possible to use the bottom two lines by using the PRINT #1 command.

The original program can be modified as follows. Load the program, then enter the following lines:

472 IF i\$="b" THEN BRIGHT 1: CLS: FOR n=0 to 21: FOR c=1 to 8: PRINT PAPER c(c);

";; NEXT c: NEXT n: PRINT #1; AT 0,0;; FOR n=0 to 2: FOR c=1 TO 8: PRINT #1; BRIGHT 1; PAPER c(c); ";; NEXT c: NEXT n: LET i\$=""

474 IF i\$="c" THEN BRIGHT 0: CLS: RUN 572 IF i\$="b" OR i\$="c" THEN GO TO 472

In addition, change line 100 to:

100 POKE 23658,0: LET nn=0: BORDER 1: PAPER 0: INK 7: CLS

Adding the POKE in this line ensures that the shift is in lower case. Note that there are four spaces between the first two sets of quotes. After testing, resave the whole thing on your cassette or microdrive.

When the program is run the card now appears as usual. If you press "b" you get bars, if you press "c" you get the test pattern. Pressing ENTER stops the program. Pressing any other key turns the music on or off.

If you wish to enter the bars as a stand-alone program, enter just line 472 without the IF... THEN and leave out (c), i.e. use PAPER c instead of PAPER c(c). Then enter line 474 as follows:

474 IF INKEY\$=""THEN GOTO 474

Do not leave this line out. The colours won't appear in the same order as the full program. Pressing any key ends the program.

All cassettes sent out from the address in the original article after May 10th contain the additions.

John de Rivaz, B.Sc. (Eng.),

Truro, Cornwall.

MORE ON PLUGTOPS

I've not seen all the correspondence mentioned in the letter headed "plugtop hints" in the March issue. It seems that readers have been concerned about burning of the neutral pin in 13A plugs. My working life mainly involved trouble-shooting for a large manufacturer of switchgear, control gear and accessories, and in my experience burning of the neutral pin is almost always due to the pin having receded into the plug moulding. In most plugs the neutral pin retention is different from that of the live pin. The neutral pin is usually held in position by the cap moulding pressing against its square head, there being a recess in the cap to accommodate the head of the pinching screw.

When a poorly designed plug or one made of inferior material is pushed into a good quality socket with good socket pressure, either the neutral pin cap retaining corners crumble (thermosetting material) or the neutral pin pushes into the cap (soft PVC or some other thermoplastic materials). The metal head in cheap plugs is often smaller than in good ones so that there's less area of plastic to withstand the force. If the cap is of soft PVC the heat from a well loaded fuse softens the whole cap and the pin recedes even more readily.

Once the pin has receded, contact in the socket is reduced and burning of the pin end occurs.

L.E. Bevan,

Moseley, Birmingham.

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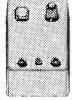
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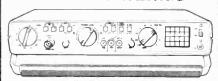
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Big Foot

Les Lawry-Johns

I thought I was the only one here who put his foot in it at least once a day – often more frequently. Now there are two of us. That puppy Zeb has grown rapidly and is now rather large. He'll get bigger – if he lives that long. Honey Bunch tried to bash in his brains (?) the other day after he'd ripped her prize plants out of the ground and then pulled them to pieces. I tried to act as peacemaker and ten minutes later was ready to kill him myself. He'd chased the cat through the shop and she'd leapt up on to a shelf and knocked off a record player just as the owner called to collect it.

Now that the weather is warmer I get a brief respite because he stays outside on a long lead for at least five minutes during which I can get just a little work done. To be fair though that's all we seem to be getting lately – just a little work, not really enough to pay the bills. Charge more they all shout. No. Not when there's not much work coming in. The time to charge more is when there are plenty of jobs and you can afford to lose a few.

What am I rabbiting on about? Sorry, it's the dog you see, he's having an effect on my nerves. When customers try to talk to me I stare past them with my face twitching and they think I'm going funny. Of course I'm not . . . I'm not . . . I'm not . . . I'm not . . .

The CTV14R

Like the chap who brought in the Fidelity CTV14R. "It didn't cost much to buy so I don't want to spend much on having it repaired. Not more than say fifteen pounds."

So I took it in, hoping for a nice dry-joint. What a hope. The fuses were intact and there was a high voltage at the collector of the BUX84 chopper transistor. There was the same voltage, instead of 120V, at its emitter. It was short-circuit. So I stuck another one in. Switched on and there was a funny tripping noise as the h.t. started to rise and then collapsed. I was afraid that the line output transformer was at fault but didn't want to think about it. I checked the line output transistor carefully and then the diodes fed from secondary windings. One (D34) was short-circuit. Glory be. Now normally I would have checked around to see what had killed it, but I had to put my big foot in it. I put another diode in and of course the result was the same tripping. The reservoir electrolytic has shorted I thought, but although a short was found to be present it wasn't the capacitor's fault. When I isolated pins 2 and 5 of the TDA1170 field timebase i.c. the tripping stopped and a nice bright white line appeared across the screen to show that the set was happy to work without the chip to upset things.

So I looked for a TDA1170. I looked where they should be and then where they shouldn't. Perhaps I couldn't see properly? I looked at my glasses. They were smudged. I wiped the lenses and one broke away from the frame as the screw snapped off. Not my new glasses, my old ones – as you'll recall I can't wear my new ones as I can't see close up with them. I even have to take my old ones off to see really close. I knew I didn't have any screws small

enough so I had to stick a piece of wire through the metal frame and solder both sides as I'd done when the lens at the other side broke away long ago. That's why I got the new ones I can't wear. I still couldn't find any TDA1170s however.

"What's wrong" asked Honey Bunch, who was playing ball with the dog.

"I can't find any TDA1170s love, even though I've cleaned and mended my glasses."

"Perhaps you've used them all."

"If I'd used them they'd be on the order sheet."

So I looked at the order sheet and they were on it. Then back it came in a blinding glimpse of the obvious. The Normende. That's where they went, together with the 630mA fuses. So I whipped a TDA2600 off the shelf and dashed down to swap it with Don and Ray.

"Ah Les" they greeted me. "Glad to see you. You don't happen to have a spare TDA26(0) up at your shop do you? We're right out what with all these G11's gobbling them up." So I produced the TDA2600 from my pocket and they were astounded. I modestly looked at the ceiling and then at the teapot.

"What do you want in exchange for it?" asked Don.

"Nothing really, but I'll take a TDA1170 if you like."

So after joining them over a cup of tea (they don't have whisky down there) I nipped off carrying my precious chip which completed the Fidelity repair when fitted. The heatsink is a pest to get off but nowhere near as difficult as the one on the Normende. Perhaps it's my Weller soldering gun that's getting old (tighten up the nuts you fool).

Mack and Millie

These very nice people are old friends of mine and live not too far away in a select area where not very much happens except when their grandchildren visit and all hell breaks loose. Mack had phoned to say that their 26in. G11 had broken down. Their house was on the right as I drove up so I pulled over and ran the nearside wheels on to the path outside their gate and switched off the lights. Now Millie is a local magistrate, and when I went in she was going on about thoughtless motorists parking on the pavements all over the town. After exchanging the usual pleasantries I got on with the set and found a funny fault in the power supply. To save time I nipped out to the car to get my spare panel and was back in a flash.

"My God that was quick" commented Millie.

"Well I've parked on the pavement just outside" I

"YOU'VE DONE WHAT?"

"See you in court Millie."

The Estimate

A chap had left an ITT CVC20 and a message to the affect that £25 was his limit. After quite some time it transpired that the tripler was faulty and that the line output transformer was overheating with the tripler disconnected. After replacing the BU208 and fitting all new parts (I was curious) a blank raster with just a shadow of a picture was resolved. The sound seemed to be o.k. but the contrast control had no effect. Tests cast doubt upon the TBA560 but replacing this merely produced an overbright raster with no signal (vision) at all. At this point I removed all the new stuff and carefully replaced all the faulty items. I should suffer. He was most upset when given an estimate.

Teletopics

IT'S NOW LEGAL

The government has altered the rules on satellite TV reception. Until now it has been necessary to apply to the Department of Trade and Industry for a licence, which was granted only to cable TV operators and organisations carrying out research. Individuals can now apply for a licence under the Wireless and Telegraphy Act - local planning permission to erect a dish aerial of any size is also likely to be necessary. Licences will also be available for linking TV signal distribution systems, for example in hotels and blocks of flats, to a master satellite TV receiver. Restrictions will be imposed to protect the interests of cable TV networks - a licence for SMATV (satellite master aerial TV) operation will not be provided in areas where a wideband cable franchise has been awarded or where a franchise has been advertised or is pending. The move has been welcomed by cable concerns and the TV industry, the hope being that business opportunities will be openned up, leading to increased UK production of satellite TV receiving equipment. Thorn EMI, Telefusion and Visionhire are amongst the companies that have already announced plans to supply satellite TV receiving installations.

SHOWTIME

As we go to press the annual London hotel radio and TV trade shows are in full swing. The main theme on the TV side is a far wider range of models fitted with FS tubes and greater emphasis on cabinet styling – the FS type tube seems to favour "monitor-look" cabinets. Mullard have announced the FSQ tube which is supposed to be even flatter and squarer and should be available in Philips and Pye sets later this year. Doric were showing large-screen (20-26in.) sets fitted with the new Rediffusion Mk.6 chassis. The new Network 14in. colour portable, Model NWC1430, is of interest in that full remote control can be added to an initially manually controlled version.

SATELLITE TV NEWS

Fresh hopes for the start of a UK DBS service have come with the announcement from Unisat of sharply reduced quotes for the provision of a satellite system. Unisat have offered the DBS consortium ten options for different degrees of satellite system management and operation. Meanwhile tentative agreement has been reached on what should be shown on the three DBS channels: the first channel would be used for recently released films and for TV series prior to their being shown on the existing networks, the second would concentrate on live sports coverage and a 24-hour news service while the third would feature popular entertainment such as TV games and soap operas.

GEC McMichael have developed an elliptical dish aerial which is claimed to offer much improved performance compared to the conventional circular designs. The dish is already being used in the Newshawk 14GHz portable satellite news gathering system. It features an offset feedhorn, maximum side-lobe rejection, reduced wind resistance and excellent portability.

Agreement has been reached between Ireland, Spain and Portugal to share a DBS satellite – the three countries were allocated the same orbital position at 31°W under the 1977 Geneva ITU agreement.

AUTOMATED TV PLANTS

Most TV receiver assembly lines have been highly automated for many years now, with the use of automatic component insertion in the PCBs. This is fine for the smaller components but larger, more awkward components have always presented problems. The difficulty is being overcome by adding robots to the assembly lines. The use of computer-controlled robots by Toshiba has for example increased the proportion of components that can be auto-inserted to 95 per cent. Use of computer control has additional advantages in that board revisions can be put into effect simply by keying the required information into the computer. Once a board design has been changed it can take as little as half an hour for the computer to revise the operation of the line robots.

Thorn EMI Ferguson have set up an advanced manufacturing development centre at their Enfield factory to investigate the application of the latest automation technology to the assembly of TV sets and VCRs. Amongst its facilities is a pilot assembly line using IBM robotics systems to insert a range of odd-form electronic components. The centre undertakes feasibility studies based on experimental data from working models. IBM's robotics systems employed at the centre are programmed using the IBM Advanced Manufacturing Language (AML), a highlevel language designed for manufacturing engineers and manufacturing application programmers. Its key features are manipulator control, sensing, intelligence (the ability to modify system behaviour in accordance with preprogrammed ways) and data processing. These are being harnessed to investigate flexible assembly techniques.

SINGAPORE'S TELEVIEW SYSTEM

A consortium of UK firms lead by GEC has been awarded the contract to develop Singapore's Teleview system. This is an advanced system that combines features of teletext and viewdata: it's also a high-capacity system, enabling the service to carry high-definition pictures, graphics and Chinese language characters in picture form. Marconi are to supply an initial 1,100 terminals to Telecoms of Singapore - 800 with hand-held keypads for residential use and 300 keyboard versions for business use. The contract also includes editing terminals, some with full typewriter style keyboards: each terminal will double as a 256K RAM personal computer. Teleview uses both telephone links and off-air data transmission: users send out requests via the telephone link and receive signals offair on their terminals. The service will also operate in both directions via the telephone links in the event of TV signal interruption. The Singapore Telecommunications Authority hopes to have a million subscribers to the service by 1990.

SERVICE BRIEF - THORN TX90

Cases of failure of the line output transistor TR112 in the Thorn TX90 chassis have been traced to leakage in transistor TR109 (BC307B) in the overvoltage trip circuit. This leakage results in reduced line drive. To overcome

the problem R246 (47k Ω) has been added between the base and emitter of TR110: it's recommended that this resistor is added in all cases of failure of TR112.

VCR NEWS

1984 was certainly the year of the VCR in the USA: sales increased by over 86 per cent, from just over four million to well over seven and a half million. The markets are now awaiting VCR exports from Korea – up till now these have been prohibited under the terms of the licence agreements with Japanese manufacturers. Models from Samsung are expected to be available in the UK this autumn – two models were on display at the Samsung trade show. The basic model is expected to sell for around £370.

VCRs using an improved Betamax specification are to be introduced in the USA. The new system – Super Beta – features increased luminance bandwidth plus new video noise reduction and pre-emphasis circuitry. According to Sony the result is a picture resolution of 300 lines and a signal-to-noise ratio of around 45dB.

The launch of Kodak 8mm video equipment in the UK has been postponed until next year "at the very earliest".

The Ferguson Videosafe is an anti-theft device that sells for around £24. It's in the form of a VHS cassette that can be slotted in the machine and locked in place. If an attempt is made to move the machine or eject the device a 98dB alarm signal is produced until switched off using the right key. It's also available as the Videolok.

NEW TV SCREEN FILTER

A new range of easy-to-fit filters for use with TV sets and VDUs has been announced by Wireless and Electronics Ltd., 5 Lansdowne Way, London SW8 1HL (01-735 7910). The filter covers the whole screen and is available in sizes from 9in. to 26in. Each one is individually boxed and comes with neat brackets and clips to make fitting a simple matter. The filters are made of a hard plastic material and result in reduced flicker and the removal of most of the ultra-violet light radiation from the tube.

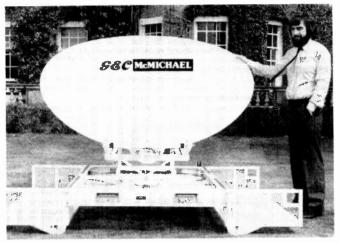
VIDEO CERTIFICATION

Certification of prerecorded videocassettes under the Video Recordings Act is to be carried out by the British Board of Film Censors which is to be renamed the British Board of Film Classification. Certification relates to films – music programmes are exempt unless they include depiction of sex and violence to "a significant extent". There are 58,000 titles on the Department of Trade and Industry's register: certification of these will be carried out over a three year period from the implementation of the act – new releases will require immediate certification. Lists of certified films will be available from the Home Office at about £20 a set.

CABLE NEWS

Work has started on the installation of the Clyde CableVision and Croydon Cable Television systems. The Clyde system is of the switched-star type, qualifying for a 23-year licence. A key component is a new switch jointly developed by GEC and Delta Kabel for the UK market. British Cable Services have started work on the Guildford service. This will use the advanced System 8 network.

Just one application has been made for each of the five



GEC McMichael's Newshawk satellite news gathering system features their new elliptical dish aerial.

recently advertised second group of cable TV franchises – London Docklands, W. Surrey/E. Hampshire, Wandsworth, Bolton, and Cheltenham/Gloucester. The Cable Authority has announced that it is not disappointed with the lack of competition for these franchises and that each application will be given the fullest scrutiny.

A monthly publication in full colour, the *Cable TV Guide*, started with the May issue. It covers the five main channels (The Movie Channel, Screen Sport, Sky Channel, Music Box and The Children's Channel) seen by 90 per cent of UK Cable viewers and is being sent free to some 500,000 cable TV subscribers and potential subscribers. It will also be available through newsagents at 35p a copy

Qualified optimism on cable TV is expressed in a new report from Communications and Information Technology Research. 8.5 per cent of households in W. Europe are now connected to a cable network and the percentage is expected to double over the next ten years. Holland, Belgium and Switzerland have the highest percentage of households connected to cable systems. CIT believes that 6.5 per cent of UK homes will be linked to a cable network by 1989.

The Joint Industries Committee for Cable Audience Research (JICCAR) has carried out the first audience research survey of UK cable TV users. It gives cable TV a somewhat down-market image, though the incidence of VCR and microcomputer ownership amongst cable users is well above average. The specific cable channels account for 19 per cent of viewing in households connected to a cable network.

ODDS 'N' ENDS

A 13A moulded plug-and-lead set is now available to equipment manufacturers from Mullard. It's been introduced in the interests of improving the safe use of both industrial and domestic electrical equipment. The advanced design of the CW3102 plug-and-lead set incorporates the usual safety features plus extras including sleeved line and neutral pins, a built in fail-safe system and very high mechanical strength.

Non-electrical soldering is what you get with the Oryx Portasol soldering iron which is available from STC Electronic Services, Edinburgh Way, Harlow, Essex CM20 2DE. The iron uses a built-in butane gas supply that provides a power equivalent to 60W with a variable bit temperature up to 400°C. A single gas refill gives up to

one hour's continuous use.

11GHz Low-noise Amplifier

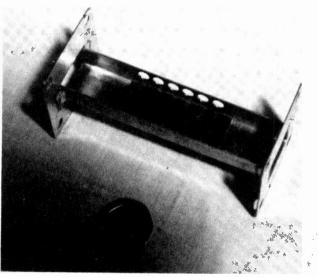
Hugh Cocks

The 11GHz low-noise amplifier to be described is intended as a companion to the low-noise downconverter featured in the February issue. The use of waveguide at the input and output means that different LNA and downconverter combinations can be tried. Construction of the unit is reasonably straightforward if one is experienced in r.f. techniques. Those who have built LNAs for use at 4GHz will find the unit similar but more compact. A matching regulated power supply built around a d.c.-d.c. converter i.c. is used: alternatively the power unit described in the 4GHz LNA article (September 1983) can be adopted, though it's much larger physically.

The LNA's housing is similar to that of the downconverter module. Fairly elaborate screening is required between each of the gallium arsenide f.e.t.s to prevent instability which could occur since the width of the housing is sufficient to support waveguide propagation. Constructional details of the metalwork will be provided, though ready made metalwork and p.c.b.s are available. Before going farther a word of warning. If you're unsure about your abilities with this type of construction it's advisable to leave well alone – the GaAs f.e.t.s alone cost over £100 and are quite easily destroyed if care is not exercised.

Circuit Description

The design of the LNA is based on an application note from California Eastern Laboratories covering an 11·7-12·2GHz (US satellite band) LNA which employed two transistors. The circuit has been rescaled for 10·95-11·7GHz and an extra transistor has been added to increase the gain. The overall gain should be at least 25dB with a noise figure of around 3dB. The first two GaAs f.e.t.s are NEC type NE71083, the final one being an NE70083. Other devices, such as the Mitsubishi series, will work but since the board is not optimised for these



Photograph of the LNA case, with the input and output flanges and the LNA board fitted and the side holes for the power supply feeds drilled.

odd tuning effects will occur due to mismatches. The circuit is shown in Fig. 1; the PCB track layout is shown in Fig. 2.

The incoming signal is transferred by a pickup wedge (see later) to a 50Ω section of printed track. A 10pF chip capacitor then couples the signal to a section of track that acts as a 36Ω , quarter-wave transformer which is followed by two 23 Ω open-circuit stubs. This network matches the 50Ω input impedance to the optimum source impedance of 26Ω . The coupling between the first and second stages is less complex because the source and load impedances are similar: a 50Ω , 0.538 wavelength transmission line is used. The second stage's output matching network is series resonated with a 50Ω , 0.04-wave line and a 21Ω , quarter-wave stub which is then coupled into the third stage via a 50Ω transmission line section and a 50Ω , quarter-wave stub (in practice this must be shortened, see later). The output from the third stage uses the same series resonant network as the second stage. This is coupled by a 10pF chip capacitor to a 50Ω section of track which feeds the output wedge, i.e. microstrip to waveguide launcher.

The bias and drain supplies for each stage are brought in via printed chokes, with 1,000 pF decoupling chip capacitors. The arrangement is identical to that used in the 4GHz LNA. The 10pF coupling chip capacitors are special types with a high Q at 11-12 GHz. Mount them with the body's dot indication on the side rather than parallel with the board. This is due to the unwanted resonance effects that can occur with capacitors used at this frequency – the 4GHz type of 10 pF capacitors shouldn't be used.

Mechanical Details

The f.e.t. source leads go through the board. Due to the slight inductance still present a screen is placed across each transistor, with silver epoxy adhesive used to bond the screen to the source lead protruding above the board. These screens also prevent 11GHz signals being propagated down the housing.

The PCB is Teflon based, has a dielectric constant of around 2·2, and is 0·01in. thick! Both 3M Cu-Clad 217 and Rogers Duroid 5880 have been used with good results. Working with a PCB as thin as this takes a little getting used to: the main point to remember is that with too much heat the track will start to peel away, also that the board is easily marked by sharp objects.

The case is similar to that of the downconverter modulator. Make the main body of about 0.9mm thick tinplate. With the prototype units the two sides and the bottom were bent from a single piece (see photo), flanges being soldered to each end. It's convenient to make the flange size identical to that of the downconverter module.

The unit's lid is sectional and may be made from thinner gauge timplate if required. The input and output sections of the lid have the pickup wedges (see Fig. 3) attached to them. The upper, rear sections of the wedges go through slots in the lid, to which they are soldered: the wedges must not be soldered on the inside of the case.

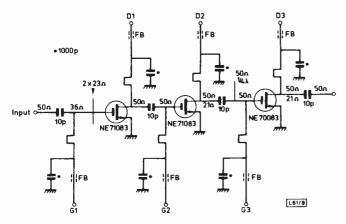


Fig. 1: Circuit diagram of the low-noise LNA.

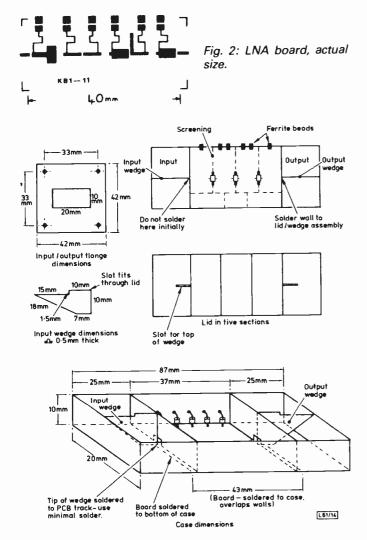


Fig. 3: Details of the case and screening.

Once the panel has been mounted in the case the wedge/cover assemblies are put in place and the "tips" of the wedges are soldered to the input and output striplines. Tuning screws can be inserted in the input and output waveguide sections in the same place as the downconverter input tuning screw. Wedge thickness does not appear to be too critical. The Mitsubishi downconverter module uses very thick metal: the prototype LNAs used about 0.5mm thick tinplate. Some experimentation here may prove beneficial.

Attach the PCB to the bottom of the case in a similar manner to that used in the downconverter: drill a small number of holes in the bottom of the case, tin the bottom

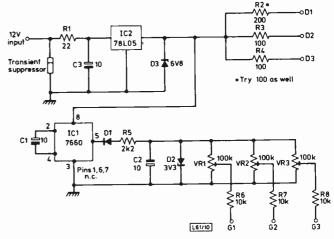


Fig. 4: Power supply circuit. Veroboard can be used.

of the PCB, then put solder through the holes carefully. It's a good idea to hold the board in place with a block of metal to act as a heatsink and prevent it warping in the heat. Make larger holes where the transistor source leads go through the board so that they can go right through to the outside of the case.

Six holes must be drilled in the side of the case to allow the bias and drain supply connections to be made. Because of the extremely small size of the circuitry normal feedthrough capacitors cannot be used – they are much too large. With the prototype units a ferrite bead was used on the inside, covering each lead going to its pad, and a ferrite bead was used in each hole. Sufficient decoupling is provided with the chip capacitors on the board. Solder the decoupling capacitor earthing pads to the side of the case.

After the amplifier has been built screening must be placed over the PCB. An internal wall runs along the length of the PCB over the dead area of the board to prevent any waveguide propagation. The three screens covering the f.e.t.s are then attached to this wall and to the unit's outer wall. By the time the ferrite beads are in place there's not too much room to attach the screening to the outer wall. Silver epoxy adhesive can be used here if it's difficult to use a soldering iron. A cutout for each transistor must be made in the screening: it must be a tight fit and silver epoxy must then be used to cover the remaining sections of source lead and connect to the screen (do this with extreme care, see later).

The lid covering the PCB must be cut into three sections. Odd effects can occur when these are put in place and this must be checked during construction.

The Power Supply

The power supply is relatively straightforward (see Fig. 4). The incoming 12V supply is fed via R1 to a 78L05 5V regulator i.c. which has a 6.8V zener diode connected across its output to provide protection in the event of regulator failure. Resistors R2-4 provide the drain supplies for the f.e.t.s. A simple d.c.-d.c. converter chip, type 7660 (RS stock no. 304-598), is used to generate the negative gate bias required by the f.e.t.s. The output from pin 5 of the i.c. is rectified by D1 and smoothed by R5/C2, with the 3.3V zener diode D2 providing regulation. VR1-3 set the gate bias voltages, the sliders being linked to the gates via R6-8. Miniature presets (RS 185-937) were used to fit the small board. By mounting the feed resistors vertically the board is small enough to fit on the bottom of

the LNA housing.

I recommend fitting a transient suppressor across the 12V input to prevent possible spikes killing the transistors. Provision for this is not made on the board but the suppressor can be soldered to the top of the input resistor (R1) and to the ground plane on the component side of the board. The type used is RS stock no. 283-261 which cuts in at 16V. Its response time to a transient is of the order of a picosecond – so far no transistors have blown in mysterious circumstances! The band end goes to the positive side of the supply.

As previously mentioned the 4GHz LNA power supply

could be used but is much larger.

Test the unit thoroughly before connecting it to the f.e.t.s. On some boards D2 tends to load down IC1 a little. If this occurs, disconnect D2 – the negative supply obtained from the chip is fairly stable and only a small percentage of the available supply is required. By increasing R5 to say $22k\Omega$ the potential dividing action with the presets will drop the voltage sufficiently.

Construction

Start soldering the components on the board after soldering the board to the case. Solder all six decoupling capacitors in place first then check for possible shorts across them – this can happen, and once a transistor is in place it's all too easy to blame it. Next fit the 10pF coupling capacitors. Follow the previously mentioned instruction about mounting them the correct way and use a very fine soldering iron bit and as little solder as possible, consistent with a good joint.

At this point it's advisable to connect the power supply and check that the voltages are reaching the stripline. The board can be fitted to the bottom of the case using either copper wire legs or double-sided tape: ensure that the print side of the board cannot be short-circuited to the case if pushed hard. Use thin, insulated wires through the ferrite beads. It's easiest to glue each bead on to the board and into the holes after taking the wire through.

Next comes transistor fitting – always a worrying time! Ensure that the thick source leads fit through the board: the best way to do this is to use a small, flat screwdriver blade to punch the board gently. The gate and drain leads must be cut as short as possible to connect with the stripline that buts right up to them: no appreciable length of lead should be on the stripline. The lead with the diagonal slash in it is always the gate lead, the one at 180° to it being the drain (the two source leads are much wider). NEC have moved the position of the red dot from being adjacent to the drain to adjacent to the gate lead recently so this is not an accurate guide. Once the leads have been cut it's all too easy to mount the device the wrong way round, so make a note of which way round the dot is to the gate/drain leads.

Solder the source leads initially using only a small amount of solder underneath, consistent with good earthing, in case the transistor (heaven forbid!) should need to be removed if it has died. Lay the gate and drain leads – what there is of them, no more than 0·1in. – flat on the stripline and solder quickly, using a minimum amount of solder. Normal soldering precautions should be taken with the GaAs f.e.t.s – earth the iron's bit to the case and make sure that you're not at a potential to the whole assembly. Never use a soldering gun if you wish the transistors to work afterwards!

When all three transistors have been connected, and

before the screening is inserted, check each one *individually* with its connections made to the power supply. Set the gate bias at around 0·5·1V negative (avoid using a meter at the gate connections) and monitor the drain current by checking the voltage at the drain feed resistor. The voltage should vary between 5V with high negative bias at the gate to less than 1V with minimum bias. Optimum bias is with around 2·5·3V at the drain. If all three transistors are connected to the power supply without screening and without the input/output terminations in place bad instability will occur. This will show as erratic drain current variations.

If all's well, solder the source leads properly on the bottom. If you find that the drain voltage won't move from around 0.5V there's either a short-circuit in the feed to the gate or the transistor has died. If the drain voltage is stuck at 5V it's not reaching the stripline. If there's a problem here cut the feed choke on the board to isolate the transistor as it could well be that the decoupling capacitor has shorted out or has a sliver of solder underneath it.

The screening must next be fitted. Fig. 3 shows the approximate positions of the screens. The sub-wall is attached to the main wall by two stand-off pieces of tinplate. The end of this sub-wall should be soldered to the output wedge/lid assembly in due course but avoid soldering to the input wedge/lid assembly initially – sometimes the signal is better with it disconnected (check on a live signal later).

It's a good idea to smear the silver epoxy between the transistor and the screen as each transistor screen is fitted. Start with the centre screen and work outwards. Smear the adhesive just where the source leads protrude from the body. Be very careful not to smear any between the gate or drain leads and earth or the transistor won't work, being effectively shorted out by the glue. Silver epoxy has a consistency that's slightly different from normal epoxy—it's similar to hard butter. Small granules can come adrift, so make sure that it's firm. It also takes a long time to dry, but this doesn't affect the electrical performance materially.

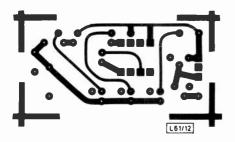
Once this has been done, solder the input and output wedge lids to the case (on the outside only) and carefully solder the rear tip of each wedge to the panel, using only a small amount of solder. Leave any tuning screws at the input/output screwed fully out and check that all three transistors behave correctly as the d.c. bias is varied. Leave each transistor with about 3V at its drain. If all's well here we can proceed with the testing.

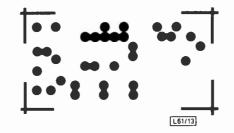
Testing

First of all cut down the stub between the second and third transistor to about half its original length – this is easier to do before the screening is in place. Access to it will be needed when the LNA is being tuned however.

Bolt the LNA (initially less any image filter) to the downconverter module and switch on the downconverter but not the LNA. When the LNA is switched on a vast increase in noise should be seen on the screen – the noise will vary depending on the settings of the bias presets.

If you find a mass of carriers/patterning on the screen as you tune across the band there's instability. See if it disappears when the output lid is placed over the third transistor. If it does, solder the lid in place, preferably leaving the cut down stub exposed for adjustment. If this doesn't cure the instability, try soldering the internal wall





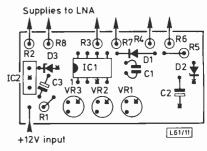


Fig. 5: PSU board track pattern.

Fig. 6: PSU board groundplane side.

Denotes solder connection to component side of board.

Fig. 7 (right): Power supply component layout.

to the front cover – these two actions should stop any instability. It's also worthwhile checking that the source leads are well earthed as poor earthing here will produce instability. Instability is in general much easier to cure than with a 4GHz LNA, though it can look more violent on the screen.

Connect the LNA to the feedhorn and keep a fairly high i.f. (700-800MHz). Use of a subreflector feed system helps a lot when testing and peaking the unit as all the electronics will be at the rear of the dish. When the dish is aligned with the satellite the signals should appear a lot stronger and u.h.f. breakthrough from local transmissions should be minimal. Without an image filter, signals at the top end of the band may seem noisier than those at the low end. This effect is caused by image frequency noise. With an i.f. of 700MHz the image of a signal at 11-6GHz is around 10-2GHz: the amplifier's gain at 10-2GHz will still be quite high and the noise produced will be superimposed on the wanted 11-6GHz signal. With the same i.f. and an 11GHz signal the image at 9-6GHz will be at a point where the LNA's response is much lower.

Peak the tuning screws and voltage presets for optimum pictures. If the signals are too strong for subjective evaluation of the picture quality move the dish slightly off the satellite. Screwing the downconverter tuning screw inwards from fully open will produce a notch where the wanted signal is lost. Just beyond this point the image frequency will be notched out, giving an improvement to a specific signal. The exact notch point will vary from signal to signal. If a signal meter is being used the signal strength will appear to fall due to the loss of image frequency noise drive to the meter.

If no microwave test gear is available alignment of the LNA is virtually impossible without a wideband image filter. Arrangements have been made to supply a filter in waveguide form to fit between the LNA and the downconverter. It has an insertion loss of 0.5dB and an attenuation of some 30dB at 10GHz. Because of the tight tolerances of the tuning elements in the waveguide it's not practical to give constructional details. Assuming that a filter has been obtained, final alignment of the LNA can begin.

Final Alignment

Check the effect of placing the remaining two covers over the first two stages of the LNA. The signals may increase slightly with the middle cover in place but with the input cover on they may decrease. If this is a problem it's probably best to glue a stout piece of plastic in place of the first metal cover.

Note the effect on the third stage of varying the length of the 50Ω stub. A useful tuning tool consists of a flat piece of wire on the end of a holder – note that due to the

dielectric effect of the plastic this can peak the LNA as well! Some performance compromise may be needed between the top and bottom end of the band. A small piece of wire soldered to the rear end of the input wedge can increase the signal level.

In general the input stripline won't need adjustment. The optimum settings of the bias presents may vary a little across the band. This is fairly normal and is caused by slight variation of the transistor S parameters with different currents – this alters the stripline tuning. If you get a violent effect the transistors aren't matched to the board: this should not occur if the specified types are being used.

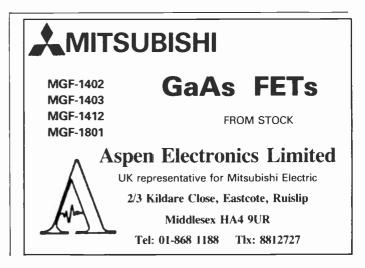
It should be possible to achieve good signals from ECS-1 in the UK using a 1.5m dish and this LNA. The noise figure is around 3dB or a little better.

Once the system is working well, find a box to house the electronics. It may be best to use a "dead" section of waveguide at the input so that the LNA is a little away from the elements: cover the front with plastic to prevent ingress of moisture. Take great care to prevent this: microwave signals hate any form of corrosion!

Sources and Acknowledgements

Aspen Electronics Ltd. of 2 Kildare Close, Eastcote, Ruislip, Middlesex (01-868 1188) are the UK agents for the Dielectric Laboratories Inc. (DLI) 10pF chip capacitors type DI 2A 100K 50 LD. The 1,000pF decoupling capacitors are not too critical. Hugh Cocks TV Services of Cripps Corner, Robertsbridge, Sussex TN32 5RY (058-083 317) can supply the 10pF capacitors, ready etched LNA boards, metal housings and waveguide bandpass filters.

The NEC GaAs f.e.t.s can be obtained from Castle



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Microwave Ltd., Brookfield Drive, Aintree, Liverpool L9 7AN (051-523 4011). Printed circuit board material is available from Walmore Electronics, 11-15 Betterton Street, Drury Lane, London WC2 (01-836 1228) – the board must have a dielectric constant of 2·2 and be 0·01in. thick. The silver loaded epoxy adhesive is RS type 555-

673.

Finally my thanks to everyone who helped with this project: Dave Lewis for the PCB drawings and prototype case design, the two Johns for the image filter, and Mike Stone who had great fun playing with the prototypes and put much work into getting the project off the ground.

VCRs and the Mains Supply

Derek Snelling

The mains supply, or to be more accurate various forms of interference associated with it, can be responsible for many problems with VCRs. The most obvious problem is random fuse blowing: the mains fuse or fuses blow for no apparent reason, a replacement restoring normal operation. Less obvious are the effects on the various microcomputer i.c.s in a VCR caused by transients appearing on the supply lines.

Clock/Timer Problems

Clock/timer circuits are particularly susceptible, with faults such as all the days displayed, a.m./p.m. appearing on a 24-hour clock, the clock losing time dramatically, a meaningless display such as 64-83 hours, or inability to set various timer functions. The problem is often that an internal switch in an i.c. gets tripped into the wrong state: for example, some microcomputer i.c.s have automatic 50/60Hz switching which can get tripped into the 60Hz condition with the result that the clock loses time. The cure in such cases is to unplug the machine from the mains supply, count to ten, then reconnect it. This resets the microcomputer and clears the problem. In some cases a longer disconnection time is required to discharge the backup battery.

Control Circuit Troubles

Microcomputer troubles we've had apart from the clock/timer circuit have been confined to the Mitsubishi HS700 and HS304. With the former the usual symptom is that the cassette can't be ejected or that the lid won't stay closed. Luckily this machine has a reset button near the clock setting controls. Pushing the button with the point of a biro resets the micros and clears the fault. With the HS304 the symptoms are difficulty with closing the cassette lid, the motor running without a cassette in, very slow response to the controls or no response at all. With this machine you need to unplug from the mains, as for clock faults.

Fuse Blowing

Many years of experience have shown that with the exception of some Toshiba V31 and V33 VCRs, for which a modification was introduced, intermittent fuse blowing is generally caused by a faulty mains socket. On a couple of occasions the problem was due to a faulty wall socket; in a few more cases it was caused by a worn multiplug; in over ninety per cent of such cases however the cause has been a worn or faulty two-three way adaptor – the sort of thing where you can put plugs in at the top, front and sides. These adaptors are often worn to the point where a plug will fall out under its own weight. I even had a case

where the live pin stayed in place when the adaptor was pulled from the wall socket.

It's fair to say that when a VCR has a wall socket to itself and the socket is in good condition random mains fuse failure is very rare. One other possible source of trouble however is when the machine is unplugged each night. Not all VCRs have a mains on-off switch (the Mitsubishi HS306 for example), so unplugging and plugging in can result in sparking at the socket and a blown mains fuse.

In view of this, why do some VCRs suffer from random mains fuse failure more than others? The difference lies in the design of the mains filter and the choice of fuse size. For example, the Ferguson 3V29/30 have a 1·25A fuse and an $0\cdot022\mu F$ mains filter capacitor while the Toshiba V31 was originally fitted with a 315mA fuse and an $0\cdot1\mu F$ filter capacitor. The Ferguson machines don't suffer from fuse blowing while the Toshiba V31 does. Obviously the smaller the fuse value the more likely it is to fail under surge conditions: fuse sizes have been reduced to the limit in recent times in order to get BEAB approval. Also, the higher the mains filter capacitor value the lower the impedance presented by the capacitor at any specific frequency.

To overcome the problem of random mains fuse failure two courses can be adopted: increase the fuse rating and/or decrease the value of the filter capacitor. Care is required when increasing the value of the mains fuse otherwise safety problems will arise. Toshiba have officially increased the rating of the fuse used in the V31/33 to 630mA. Decreasing the value of the mains filter capacitor is less risky but reducing it to too low a value could allow too many mains-borne spikes to enter the machine and do damage. Toshiba recommend reducing the value of the mains filter capacitor in the V31/33 to 0.0047µF.

In Conclusion

To sum up, mains or mains related troubles can cause microcomputer confusion and fuse blowing. Can they cause one-off faults? The two established mains related faults have been confirmed by their relatively frequent occurrence. Apart from these I've had one instance where the capstan i.c. in a Mitsubishi HS306 failed and I'm ninety per cent sure that the cause was a faulty wall socket – I recall that when I did TVs repeated line output transistor failure in the Philips G11 chassis was often caused by faulty mains plug wiring. It would be interesting to hear from readers of any faults they can squarely attribute to a spiky mains supply.

Finally I'd like to emphasize that when I mention a spiky mains supply or mains interference the cause in the vast majority of cases lies within the household rather than coming via the mains distribution network.

Approaches to TV Servicing

S. Simon

We all have our own ways of tackling faulty equipment and tend to get rather set in our ways if we are not usually in the company of others engaged in the same profession. My own approach is to weigh up the symptoms reported and try to make a direct attack on the likely source of the trouble, basing this attack on my previous experience of the model concerned.

With a "no raster, sound o.k." condition for example the approach depends wholly upon the model. If the voltage supply for the sound circuits is obtained from the line output stage, as in most sets manufactured in recent years, it's likely that the line output stage is working and that e.h.t. is present. My first action therefore would be to check the tube base voltages to ensure that the cathode voltages are not too high and that the first anode voltages are high enough, i.e. about 150V at the cathodes and 400V at the first anodes. The next move depends on what these readings reveal.

It's quite common for example to find the first anode voltages missing in a receiver such as one of the GEC C2110 series though the line timebase is clearly in order (e.h.t. o.k. and sound present). My first move in this case would be to check the first anode supply presented to the convergence panel. I would expect to find it present and it usually is. The common failing is the resistor on this panel between PL30-4 and the first anode presets – R506, $560k\Omega$. In later production this resistor is not on the convergence board – instead it's on the small panel over the line output transformer where it's designated R616. The two nearby $1M\Omega$ resistors R607/8 are also highly suspect in this chassis and are often found burnt up.

Thoroughness

I had an occasion recently to visit a local workshop and was present when one of these sets was put on the bench for servicing. The symptoms were as described above and I was interested in the young man's approach. First he stripped the supply plug and rewired it, checking the fuse etc. He then checked the condition of the 3·15A mains fuse in the set itself – at the top left – and its holder. Next he checked for shorts across the h.t. line and across the thyristor mains rectifier. Satisfied that all was well, he plugged the set in and listened for the e.h.t. to rustle up. He proceeded to check the h.t. voltage against that given in the manual, then most of the voltages on the video panel. Finally he turned to the tube base and found that the first anode supply was missing.

He saw my look and turned his nose up. "We were taught to be thorough in order to avoid comebacks" said he. I crept away and vowed that I too would be more thorough in future. But old habits die hard and I still tend to jump in at the deep end and leave the plugs etc. unchecked.

The Ferguson 9600 Chassis

Shortly after this a Ferguson set fitted with the 9600 chassis required attention. The no raster condition this time seemed to be the result of high cathode voltages at the tube base. We chased this condition back to the

signals panel where we found the 24V supply absent. So we moved over to the power supply panel where we expected to find fuse F511 open-circuit (34V feed to the 24V regulator on the scan panel). There was no voltage at either side of F511 and we then found that the relevant rectifier diode W518 (SKE2G2/02) was non-conductive in either direction. If we'd been more thorough and checked the supplies first we would have saved ourselves some time. Next time we'll check at the diagnostic sockets fitted as the makers suggest.

Pye 725 Chassis

The Pye 725 chassis is the one with the vertical panels. It's given us some headaches in the past. In this case the mains supply was present at the anode of the mains rectifier thyristor but there was nothing at the h.t. fuse and the associated resistors (surge, smoothing and antibreathing). Not wishing to fall for the old one we carefully checked the continuity of these wirewound resistors (if the surge limiter section goes open-circuit there's no h.t. at either end and nothing starts up). As all was well we returned to the power unit. The two $82k\Omega$ charging resistors R898/9 in the trigger pulse generator circuit are suspect and one of them was found to be open-circuit. In went another and we confidently switched on, expecting to hear the rush of sound and e.h.t. Silence.

We spent a lot of time checking this panel before we returned to the centre h.t. fuse. We were then surprised to find just over 100V present. Resetting the h.t. presets brought the voltage up to normal and the set then behaved impeccably. How were we to know that eager little fingers had adjusted the presets wrongly?

Incidentally if the centre h.t. fuse is found to be open-circuit, waste no time – look into the top of the screened line output section and note the position of the capacitor right at the top (C561, first anode supply reservoir). Note its leadout wires to the print and check for a direct short. Failure to do this can lead you on a merry dance – a replacement tripler can be the first of many unnecessary acts as disconnecting this may leave the fuse intact. We all know this one by now of course, but it's an example of how methodical testing according to the book can lead one astray. Incidentally C561 is $0.1\mu F$, rated at 1.25kV.

Rank T20/T22 Chassis

Mention of the Rank T20/T22 chassis will bring groans from those who are fully conversant with these sets. This isn't for you: it's for the majority who are not so fortunate. It's essential with these models to have a clear idea of how the system works. The power supply module is situated beneath the tube. It's a fairly complex self-oscillating chopper circuit designed to deliver a 200V h.t. supply to the right side line output panel. In most cases it does this, the fault or faults being elsewhere.

If the 200V supply is absent, remove the plug from the upper right side, thus isolating the power supply for fault tracing. There are two fuses. The front left side one is the mains fuse. Failure of this should direct attention to the bridge rectifier diodes 7D14-17: it's common to find two

of them shorted, not one. BY127s are suitable for replacement purposes – they have a higher voltage rating than the BY126s originally fitted. If the diodes are not at fault, check the degaussing circuit posistor 7TH1 and the mains filter capacitor 7C19. Remove them for a positive check, though their appearance will often leave no doubt as to which one is at fault. If there is doubt, remove the posistor and shake it: if it rattles, fit a new one (there's science for you). In all probability however the mains fuse will be intact and the fuse that will have failed will be the one at the rear of the panel – the 1-6A HRC (high rupture capacity) d.c. fuse which is connected in the negative side of the supply. If it's open-circuit, carry out a general check on the BU326 chopper transistor and the associated diodes and thyristors.

HT Present

It's far more common to find that the 200V supply is present at the line output panel although the tube's heaters (fed from a winding on the line output transformer) show no signs of life. If the 27Ω wirewound antibreathing resistor 5R11 is hot or the 800mA fuse 5FS1 (if fitted) has failed, the voltage at the body of the BU208A line output transistor, which is on the metal panel, will be low, suggesting that the transistor has gone short-circuit collector-to-emitter. Check for this. But don't replace it and reconnect the supply until further checks have been carried out. Possible causes of the death of the transistor could be failure of the 9-1nF tuning capacitor 5C14, which goes open-circuit, a shorted tripler (disconnect from the line output transformer) or a poor earth connection at pin 2 of 4Z2 on the centre, swing-down timebase panel. This is the long plug on the right side: if in doubt about the earth connection solder a long lead from pin 2 to the earthing on the line output panel.

BU208A Intact

It's more common to find that the full 200V is present at the body of the BU208A. In this event it's logical to check that the supply is also present at the collector of the driver transistor 5VT3. Under normal conditions the voltage here should be 125V: it's common to find the full 200V present, thus showing that the driver is inactive. In this event it's essential to appreciate the nature of the kick-start circuit used in these sets. The line oscillator is provided with an initial kick by 4C19 (10μ F) on the right centre swing-down panel. With the set switched on this capacitor has 200V on one plate at all times: at the moment of switch on it charges via 4R49 and zener diode 4D14 on its negative side, the kick being applied via 4D13 to pin 3 of the TBA950 so that this i.c. gets going for long enough to enable the rest of the line timebase to come into operation - if it's in a condition to do so. The 12V regulator circuit should then start up and take over the supply to the TBA950 and the other low-voltage circuits. Shunting 4C19 with a wirewound resistor of some $5-10k\Omega$ will maintain the supply to the TBA950 so that the trouble can be sorted out.

Short Cuts

That's the logical way to start fault tracing. In practice the writer employs a short cut once he's established that the 200V supply is present at the body of the BU208A. Release the top screws and unhinge the chassis outwards –

with the set switched off. With the meter switched to the low ohms range, check the EW modulator diodes 5D7 and 5D6 at the front end of the print. 5D7 should read about 20Ω both ways due to the circuit. 5D6 should readabout 20Ω one way and 200Ω the other. One of the diodes could well be open-circuit or perhaps short-circuit. If these are o.k move farther to the rear and check 5R8 which is in series with the BU208A's base. It should read 1Ω . It will often be found to read higher and when removed be found to be open-circuit. If 5R8 is in order, move over to the left side of the swing-down panel to check the value of 4R16 in the 12V regulator circuit. It should read 910Ω. If it's open-circuit the 12V regulator won't provide an output and the set will fail to get going after the initial kick start. These few quick checks will save a great deal of time.

Philips G11 Chassis

We've discussed the Pye/Philips G11 chassis in the past. There are now large numbers on the second-hand market however, so it will do no harm to outline the habits of this chassis briefly.

Most of these sets have two 3.15A anti-surge fuses mounted on the lower rear panel (some sets have only one fuse here). This is a convenient starting point in the event of a dead set. Are these fuses intact and is there 240V between them? If they have obviously blown one would assume that the fault is on the lower right power panel, and this would be so if the h.t. fuse F4037 on the upper left of the power panel is 1A as it's supposed to be. All too often however a higher rated fuse is found in this position so that if the fault is on the upper line timebase panel the excess current flows via the mains fuses which accordingly fail. So check this point first. If the h.t. fuse is rated at 1A, concentrate on the power supply panel: in particular, check the four diodes in the bridge rectifier circuit. Two of the diodes also form a bridge with the two thyristors which are far less often at fault. This "double bridge" arrangement means that the two diodes that form part of both bridges work harder than the other two: these will most often be found to be short-circuit, thus explaining the blown fuses.

If the fuses are intact and there's about 120V a.c. at the anode of each thyristor but no voltage at the h.t. fuse it's likely that trigger pulses are not being applied to the gates of the thyristors. There can be many reasons for this but a weak point is transistors T4085/6 in the excess beam current protection circuit. Since these two transistors are d.c. coupled and one is an npn device while the other is a pnp device it's impossible to check them by means of incircuit ohmmeter readings: the pins from which a reading is required must be isolated. T4085 is the BC148 npn device and T4086 the BC158 pnp device.

A prime cause of trouble in these sets is poor connections – where the original soldered connections have become dry or burnt away, possibly due to arcing. Examine the panels very closely for signs of minor volcanic eruptions. Don't omit to look into the partially concealed corners of the panels.

HT but No Results

If there's h.t. at the 1A fuse but otherwise no results continue the search in the upper line timebase panel: this is a hotbed for dry-joints and close inspection really does pay dividends. The h.t. from the power panel does not go

direct to the line output stage. It's routed via the dynamic convergence correction panel (top centre) – through pins 3D7, 15A15, 15A16 and back to 3D6. This ensures that the h.t. is removed from the line output stage when the scan coils are disconnected. Check these contacts carefully if h.t. is not reaching 3D6 and pin 12 of the line output transformer. Check also the plug and socket connections that go off to the BU208A – these are at the top of the panel.

Remove this white plug in order to check the BU208A properly. The only readings to be obtained are from the base to the emitter and from the base to the collector (body). Switch to a high range to ensure that there's no

reverse leakage.

If the h.t. supply is reaching the BU208A, check the supply to the driver transistor T3102 (BF355). There should be 127V at its collector. The supply comes via R3106 (820Ω) which often goes open-circuit.

HT Fuse Blown

If the 1A h.t. fuse has blown, check whether the BU208A (remove the plug to do this) or the BY223 EW modulator diode D3133 has gone short-circuit. The BY223 is the flat, black diode with the heatsink clip on it. There should be a low reading in one direction only. If it has gone short-circuit, the condition of the EW driver transistor T2150 (BD238) – upper left on heatsink – should also be checked. A shorted BY223 often signals the demise of the BD238. Failure to check this may result in the raster sides being curved in, i.e. no EW correction.

Access

To gain access to the components, fuses etc. check whether the original transit screws are still fitted, one at either side. Remove them and swing open the top clip. Lift the frame slightly and swing it open. The separate panels can be removed if necessary once the edge connectors have been pulled off (carefully, noting their positions and the holes for the locating pins). There are clips on the same side as the plugs: these allow the panel to be eased off the locating pegs and out of the slots at the outer edges.

We mentioned fuses. There's a row of them on the line timebase panel. Of these, the one most likely to fail is FS3143 (800mA) in the 37V supply to the field timebase.

Field Timebase

The TDA2600 field timebase chip is located on the left side upper panel. It's concealed beneath a Vee-shaped heatsink which is secured in position by two soldered tags above and below the staggered pins of the i.c. holder. Check the soldering to these pins in the event of erratic height variation, particularly the upper right pin 16 (output) – this is the most likely one to be found dry-jointed. If the holder is found to be discoloured at pin 16 when the heatsink is removed it must be replaced.

Apart from this pin, the holder can be responsible for erratic height, linearity etc., as can the TDA2600 itself. The chip has an appetite for fuses: the associated components can also be responsible for fuse blowing – amongst other things. The two $1,000\mu F$ scan coupling capacitors C2099/C2100 are particularly likely to short and blow the fuse. As they are shunted by a 470Ω resistor they should be isolated for checking.

next month in

TELEVISION

• THE BEOVISION 20AX CHASSIS

Eugene Trundle provides a run-down on common faults and guidance on circuit operation and setting up in the sections of the chassis unique to this design — mainly the remote control system, the power supply (a full-wave thyristor circuit) and the auto grey-scale correction system. These sets are not too difficult or expensive to sort out once their habits and operating principles are understood.

VCR RECONDITIONING

Steve Beeching decided to buy a batch of ex-rental VCRs (Sony and JVC/Ferguson) to do up during slack moments. A report on the sorts of troubles you can expect to encounter in second-hand machines.

THE STRANGEST SET EVER

Our vintage TV series has looked at some odd sets in the past but the oodest so far must be the Murphy V134C/V136C. The line timebase used a pair of parallel-connected beam tetrodes in a self-oscillating arrangement while the field timebase employed the scan coils as a feedback transformer. The joys of TV in 1948!

INITIAL VCR CHECKS

Is it safe to insert a tape in a faulty machine that's just come into the workshop? A few moments spent checking the tape deck and operating the machine without a tape can save a lot of time and expense. William Lockitt outlines a simple test procedure.

COMMODORE 64 PROGRAM

This test pattern program provides a crosshatch then overlays colour bars on the upper part of the screen and a grey-scale wedge at the bottom. There's also switchable scund – a harmonious three-voice chord!

APPROACHES TO TV SERVICING

S. Simon describes fault-finding problems with the ITT CVC20 chassis.

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The Lid off Microcomputers

Part 3 Mike Phelan

In the first two parts of this series we took a fairly general look at the subject of home microcomputers. This time we'll take a closer look at a particular machine, the Amstrad CPC464. Its features include a 64K RAM, fairly powerful BASIC and a built-in cassette deck for saving/loading programs. Saving is recording on tape something that's in the computer's memory – usually a program, but it can also be other data, e.g. the screen part of the memory or a data file. Loading is playing back from the tape into the computer. The CPC464 comes with a monitor – either colour (RGB drive) or green screen monochrome (green instead of black and white to make viewing for long periods easier on the eyes).

To reduce the tangle of wires, the 5V supply for the computer/tape deck is obtained from the monitor. Thus there's a mains lead to the monitor and only two leads from the monitor to the computer – for RGB/sync and 5V. A modulator unit which contains a 5V supply and a PAL encoder is available to enable the computer to be used with a TV set that doesn't have RGB inputs (or 5V out!).

The layout inside the CPC464 is quite neat: apart from the cassette electronics, everything is on one large PCB. The keyboard is of the rubber membrane type, giving a nice feel and offering a degree of protection for the PCB against the various comestibles and liquids which descend in showers from the owners and their friends/relatives. Phelan's Law states that the amount of feeding electronic equipment receives is in proportion to the square of its intrinsic value.

A simple block diagram for the CPC464 is shown in Fig. 1. The CPU/microprocessor chip is a Z80A. The 16-bit address and 8-bit data buses are shown along the top. A simple reset generator consisting of an RC charging circuit and a couple of gates is used. The inverted reset line goes to the Z80A, the CRT controller i.c. and the

ULA i.c. (uncommitted logic array – a collection of gates etc. used for various purposes): the reset line goes to the PIO (parallel input/output) chip. The 64K RAM consists of eight i.c.s – one for each bit of the data word. At this point it's useful to take a look at the CPC464's memory map – see Fig. 2.

This shows the ROM divided into two blocks of 16K. The addresses used are also used by the RAM. So how does the CPU know whether an address refers to ROM or RAM? This brings us to the first function of the ULA, which starts life as just that - an assortment of gates and other logic units with no interconnections. The i.c. can be used for a variety of purposes therefore since the connections can be tailored to suit the job in hand. As far as home micros go the ULA is simply an assortment of bits of circuitry that don't fit in anywhere else - in early computers a dozen or so i.c.s would have been required to do the same work. One of the ULA's jobs is to produce control signals for the ROM and RAM. If the CPU is writing to a memory it must obviously be the RAM, but if it's reading information either the ROM or RAM could be the source of the required data. If the address is between #4000 and #BFFF it can't be the ROM. ULA produced control signals sort the matter out otherwise.

ROM Functions

When the computer is switched on the "bottom" section of ROM is started, clearing the memory etc. This then transfers control to the "top" BASIC interpreter section which awaits an input from the keyboard.

RAM Functions

Part of the RAM is used as working space by the operating system. The character set is also loaded into the

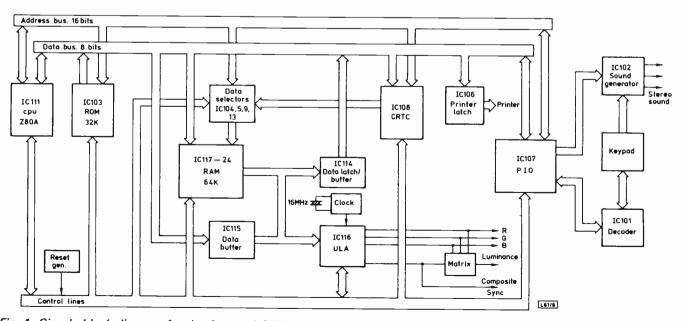


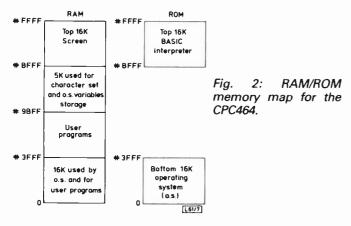
Fig. 1: Simple block diagram for the Amstrad CPC464.

RAM by the operating system. This is done so that we can redefine characters without in any way affecting the permanent character set. The screen memory is the "top" 16K section of the RAM and is arranged as follows. Each line of the screen consists of 80 bytes or 640 bits. This gives us 200 lines for 16K. Since each character consists of an 8×8 matrix it occupies eight lines, giving us 25 lines of characters. The top 80 bytes is the top line across the screen, the next 80 the ninth line and so on – this means that the top lines of all character rows are stored in a block, then the second lines, etc. Or, to put it another way, there's a 2K jump between adjacent lines.

The CPC464 has three screen modes. Mode one gives forty characters per line and four colours, mode zero twenty characters and sixteen colours, mode 2 eighty characters and two colours. The information stored in the screen section of the RAM is arranged to have what are called parallel attributes: this means that each byte contains information on what colour is to be displayed. Those who have had much to do with teletext will have met the alternative system where each screen memory byte contains either a character (ASCII) code or a control code that sets the foreground or background colour, graphics, double height etc. for the rest of the line. Some home micros use this system, which has the advantage of using less memory for the screen -25×40 takes up 1K, not 16K. On the debit side, a control code (attribute) takes up one character square which can be occupied by nothing else - so you cannot, for example, have two adjacent letters of different colour. The parallel attribute system used in the CPC464 uses a lot more memory space but is much more flexible since each individual pixel colour can be determined by the user.

Each character consists of 8×8 pixels irrespective of mode. Since there are always 80 bytes or 640 bits per line of the screen the number of bits per pixel varies with the mode. In mode two there are 80 characters per line, so each character is one byte and each pixel is one bit which can be only zero or one – therefore only two colours can be used, one for foreground and one for background. In mode one the characters are wider, so each pixel is two bits giving four possible values or four colours. In mode zero with only twenty characters per line each pixel consists of four bits so we can have values from 0 to 15, giving sixteen colours. Table 1 summarises this.

From the software point of view there is no reason why a complete screen cannot be put in the portion of RAM from #4000 to #7FFF (it will be invisible of course) and then instantly (or nearly so) transferred to the top 16K. The effect from the user's point of view is that the whole display changes within a fraction of a second. This idea is made use of extensively in games software, where a



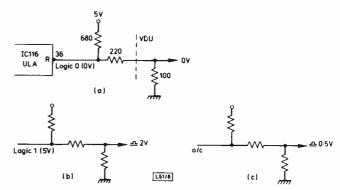


Fig. 3: Tri-state switching. (a) Logic zero output from the ULA provides 0V at the VDU; (b) logic one (5V) provides about 2V at the VDU; (c) the open-circuit state provides about 0·5V at the VDU.

complete screen can be loaded without being visible: a machine code program is then used to shift it to the visible screen section of the RAM.

Uses of the ULA

The ULA is driven by a 16MHz crystal clock. It divides this by four to provide a clock signal for the CPU. The clock signal also goes to the CRT controller IC108 whose job is to select the correct addresses in the RAM to provide screen information to the ULA, also to generate sync and blanking signals. The RAM is shared between the CRTC and CPU by means of the data selectors IC104, 5, 9 and 13 which switch the address bus between the CRTC and the CPU with a time ratio of 3:1 respectively. These i.c.s are controlled by signals from the ULA.

Next on the list of jobs for the ULA is the provision of a composite sync signal from the separate sync outputs provided by the CRTC. The ULA also contains a "palette latch" which is fed with information from the data bus to decide which colours to use – the CRTC decides which parts of the screen are to be of a particular colour. The software determines this. A total of 27 colours can be used, the number in use at any one time being restricted by the mode in use.

The palette latch output consists of a five bit code which is decoded within the ULA to give R, G and B outputs. How can we get 27 colours with only three bits? If each bit can be only zero or one we would have eight possible combinations. The answer lies in tri-state logic, in which each output can be one, zero or open-circuit. If you look at Fig. 3 you'll see how this works: each input to the colour monitor can be at one of three possible levels, i.e. there are $3^3 = 27$ possible combinations. Matrixing is used to produce a luminance signal to which the sync signal is added.

The ULA also stores the mode information until it's changed. It also generates the switching signals for RAM section selection: these are synchronised with the 4MHz clock. Each CPU instruction can take up to four clock cycles to complete. On the fourth, the CPU is halted by a

Table 1: CPC464 display modes

Mode	0	1	2
Bits per line	640	640	640
Characters per line	20	40	80
Colours available	16	4	2
Bits per pixel	4	2	1
Bytes per character	4	2	1

signal from the ULA: the CRTC is then connected to the RAM for one clock cycle.

Buffers

In an earlier instalment we mentioned that in computer parlance a buffer is a temporary storage area for small amounts of data. Computers also need to use the other sort of buffer with which we are more familiar – a stage to provide impedance conversion or isolation between its input and output. The various buses – data, address etc. – are connected to several parts of the circuit. It would not do for this to be done directly, otherwise if one bit went high or low the corresponding connections everywhere else would follow suit. To prevent this, tri-state buffers are used at the inputs and outputs: if a device is not in immediate use its ports are switched to the open-circuit state.

We also have buffer i.c.s that store one byte of information and read it out later. IC114 and IC115 are examples. The printer latch IC106 is another. Since a printer operates at a much slower speed than a computer

we must stop the computer after each byte has entered the latch. This is done by a "busy" signal from the printer. The CPU is restarted when each byte has been printed (one byte = one character). Larger computers have print buffers of typically 64K capacity: the computer ends up quite a long way in front!

VCR Microcomputer ICs

All this should have given you a better understanding of the operation of microcomputer i.c.s in video and TV equipment. The popular $\mu PD552$ and $\mu PD553$ used in JVC products are CPUs with their own ROM – the suffix number tells us which one. The ROM contains a complete program to operate the machine – and spends most of its time waiting for the user to press a key! These are 4-bit micros. The other main type is that used by Sharp and Toshiba, with a few parallel inputs for safety functions (these can be regarded as several levels of interrupt) and a serial input bus for key scans etc.

Next month we'll look at the PIO, sound and cassette electronics in the CPC464.

TV Fault Finding

GEC C2110 Series - Touch Tuning

Erratic channel changing and difficulty with changing stations are common problems with these sets. The usual solution is to change the neons then if necessary to change the high-value resistors. On one occasion this approach had little effect so we decided to strip down the touch tuner head assembly. When the aluminium escutcheon was removed we found that the centre carbon insert which connects the escutcheon to the rear panel via a spring had seized up and was not making contact due to an accumulation of dirt. We removed the insert and connected the escutcheon directly to the rear panel with 20 s.w.g. wire bent and trapped between the escutcheon and the front panel. This remedy has worked reliably on several of these sets.

J.K.P.

Thorn 9800 Chassis

The fault was excessive width plus e.h.t. flashover after ten-fifteen minutes. A quick check revealed that the h.t. was high at about 210V instead of 181V. Further checks suggested that the fault lay in the ramp generator circuit. R724 $(120k\Omega)$ in the ramp generator transistor's base bias circuit turned out to be high in value. It's mounted on the little auxiliary panel on the power supply board. D.R.

ITT CVC1200 Chassis

I've been having a few problems with the power supply in this chassis. Here's an example of how to learn the hard way. The set was dead since a short-circuit BU508A chopper transistor had blown the mains fuse. In went a new BU508A, fuse and protective zener diode D702. Switch on: bang! – another BU508A short-circuit. Another BU508A was fitted, the other seven transistors in the power supply were replaced, a dummy load was connected instead of the line output stage and the set was powered from a variac set to 90V. The bulb (dummy load) lit but an arcing noise could be heard coming from

Reports from J. K. Potts, Mick Dutton, Philip Blundel, Eng. Tech., David Rainey, Malcolm Burrell and Stephen Howe

the set and a burning smell drifted across the workshop. A puff of smoke could be seen coming from the filter capacitor C701 which was arcing internally. So now the drill is to fit a new BU508A, D702 and C701, connect the dummy load and variac, then switch on with your left hand touching wood . . . P.B.

Philips CTX-E Chassis with VST

The report by P. Walsh in the May issue made interesting reading – it showed that I wasn't the only one having problems with these sets. When the mains bridge rectifier or the 4.7Ω surge limiting resistor fails the TDA2541 i.f. i.c. sometimes goes short-circuit, open-circuiting its supply resistor and a coil in the earth line – L9157, which is not shown on the circuit diagram. With this coil open-circuit the supplies to the tuner and VST module go haywire, causing them dire distress. The VST microcomputer i.c. often dies, but when you've replaced it you could well find you've still got problems. Such as:

No green tuning line - check D5852.

Will not stop tuning when a station is found. If the tuning speed slows down when a station is found, suspect the LM339 or an incorrect a.f.c. signal from the main panel. If the tuning speed doesn't slow down, check that the mute/transmission ident signal at pin 2 of VST module plug V11 goes to 0V on station. If it does, the microcomputer isn't reading the signal. Suspect transistor T7856 and diodes D6840, D6841. The mute signal is generated in the line oscillator i.c. P.B.

Sharp C1491/Rediffusion Mk V

One of these colour portables came in with the complaint that the picture went off when the set warmed up. Sure enough when we tried it the set worked o.k. for about twenty seconds then the raster disappeared and a loud ticking noise came from the power supply. When the back was removed it was clear from the way in which all the semiconductor devices in the power supply had been changed for European types that an unknown engineer had had a long and meaningful relationship with this part of the set. Now the switch-mode power supply and the line output stage work together in this set, and if the line timebase doesn't start up that ticking noise is what you get. A scope check showed that the line oscillator stopped when the fault occurred, so attention was turned to the protection circuit which acts to shut the oscillator down. Sure enough pin 9 of the i.c. in which the line oscillator lives (an IX0065CE) went high just before the oscillator stopped. The protection circuit monitors the beam current, the amplitude of the flyback pulses and the conditions in the field output stage. It transpired that zener diode ZD602 in the beam current sensing circuit was short-circuit.

Grundig 2210

Last August I mentioned a tuning fault on the Grundig 2210 (not 2222 – sorry). I've since learnt that the tuning system is very prone to board cracking. The solution is to replace the board containing the carbon tracks. It's quite easy. Unsolder the lugs and slide the old one out. Move the contact wipers to one end, raise them with a strip of paper, then slip in the new board. Don't forget to remove the strip of paper.

M.B.

Rank T20 Chassis

This set was described as dead though a loud whistle came from the power supply. The h.t. was about 50V instead of 200V so I dived for the line output transistor which turned out to be faultless. Only then did I notice the tell-tale burn mark around plug 5Z1. Replacing this together with its socket provided a cure. The moral is, and always has been – make a quick visual inspection first.

M.B.

Binatone 01/9860

This set came in with the description "smoking". R512 which supplies the line driver stage was a little discoloured but not open-circuit. The line output transistor TR503 was short-circuit. Replacing this failed to produce any appreciable e.h.t. and I was beginning to have expensive thoughts. I then found that the boost reservoir capacitor C512 ($220\mu F$, 16V) was hot. It turned out to be leaky, a replacement restoring normal operation. I think this could become a common problem and since it upsets the operation of the line output stage it's always worth a check. Incidentally the line output transistor is type 2SC508 or 2SC2233: a BU508 (expensive) or a BD535 can be used.

Grundig 5012

We got caught out nicely the other day with this set. It had two problems. First there was no blue tilt or parabola control. Simple this – C725 $(0.22\mu\text{F})$ had gone opencircuit. I've come across this one on several occasions. The second problem was excessive width. The width control worked, but at minimum the picture was still several inches too wide. We spent a lot of time checking the width control circuit – as everything seemed to be running cool we thought we were looking for a control circuit fault. Eventually we turned our attention to the scan circuit. The scan-correction capacitor was an $0.68\mu\text{F}$

metal type. We thought this couldn't possibly be faulty. Wrong: a replacement cured the problem. M.D.

Thorn 9800 Chassis

This set had no blue. There was no blue first anode voltage due to the $100k\Omega$ series resistor R612 being open-circuit. A replacement got very warm however and we found that the associated spark gap was leaky. M.D.

Philips TX Chassis

A quickie: the fault was no sync, due to $R370~(820k\Omega)$ which provides the sync separator transistor TS370 with base bias having gone open-circuit.

M.D.

Philips KT3 Chassis

The complaint with a Philips colour portable fitted with this chassis was no picture when warm. We ran the set up and found that after a few minutes the screen went blank. Turning up the brightness control produced a very faint picture. We checked the voltages around the decoder panel, which was of the older two-chip type, and found that with the contrast control at maximum the voltage at pin 16 of the TDA2560Q chrominance/luminance amplifier i.c. was only 0-7V instead of something like 4V. C3205 $(0.022\mu F)$ which decouples this pin turned out to be leaky.

Rediffusion Mk III and Mk V

Now that Rediffusion has been taken over by Granada we're finding that calls to service Rediffusion sets are beginning to come in. One of the first sets to come our way was fitted with a Sharp chassis (Rediffusion Mk. V chassis). The problem was field collapse. As we didn't have a circuit we wasted a lot of time trying to work out what did what.

Eventually we found that R513 $(1.2k\Omega)$ was open-circuit: come to think of it this was the subject of a Test Case item not so long since.

Another set was fitted with the Mk. III chassis. This one was dead. The fuse had blown and as we could find no obvious shorts we fitted a replacement and switched on. The set started to come on then tripped. We removed the power supply panel and found a dry-joint on the regulating thyristor 6THY2, but resoldering this failed to stop the tripping. Now regulation with this type of circuit is a sort of line output stage damping action, and for this purpose 6THY2 has to be fired – if it isn't fired excessive voltages build up and the trip operates. 6THY2 wasn't receiving trigger pulses because 6R17 (68Ω) was opencircuit.

A couple of weeks later we had another of these sets tripping. This time the trouble was due to a faulty tripler.

M.D.

Thorn TX10 Chassis

The set would start up at switch on but after a few seconds it would shut down again. The set didn't go through the normal shut down/start up sequence: it simply remained dead after its first shut down. The fault was traced to the BC547 regulator transistor TR801 which provides the 12V supply for the chopper control i.c. It had gone short-circuit. In addition the associated 12V reference zener diode D802 was leaky.

E	CONO	MIC DE	VICES,	PO BO	X 228	TELF	ORD TE	2 80P	
15/80H 15/85R 16029 16181 16182	2.48 2SA884 2.48 2SA940 1.24 2SA940-2 1.04 2SA951 1.04 2SA966	2.15 2SC620 1.81 2SC643A 2.14 2SC668 1.26 2SC673 0.54 2SC681	1.46 AC138 1.54 AC141 0.67 AC151 1.23 AC153 4.40 AC176	0.09 BA318 0.29 BA328 (IC) 0.28 BA333 (IC) 0.34 BA401 (IC)	4.77 BC464 1.37 BC465 0.64 BC477	0.64 BD538 0.64 BD544B 0.64 BD580 0.32 BD590	0.67 BF479 0.83 BF480 1.17 BF491 1.17 BF495	0.61 BU111Y 0.60 BU124 0.49 BU125 0.64 BU126	4.16 1.38 2.48 0.90
16334 16335 16446 16600	0.51 2SB325 0.80 2SB375 0.98 2SB400 1.38 2SB407	3.87 2SC684 3.87 2SC685 0.40 2SC685A 3.24 2SC693	1.65 AC179 0.00 AC183 2.89 AC187 0.63 AC187K	0.30 BA5102A (IC) 0.28 BA511 (IC) 0.72 BA521 (IC) 0.39 BA526 (IC) 0.43 BA532 (IC)	5.97 BC478 2.18 BC479 2.02 BC532 7.98 BC546	0.32 BD598 0.41 BD677 0.28 BD680 0.17 BD681	1.25 BF506 0.53 BF509 0.76 BF523 1.48 BF594	0.43 BU134S 0.41 BU204 0.20 BU205 0.27 BU206	4.57 1.58 1.08 1.27
16799 16801 16802 16803	2.62 2SB411 0.54 2SB449B 1.14 2SR511 5.30 2SB54	3.30 2SC710 6.60 2SC711A 1.63 2SC717 1.39 2SC734	0.69 AC188K 0.50 AC194K 1.14 AC76003N 1.43 AD140	0.43 BA536 (IC) 0.65 BA6209 (IC) 2.72 BA6304A (IC) 1.06 BA843 (IC)	1.83 BC547 3.44 BC548 4.71 BC549 2.92 BC550 3.96 BC566	0.10 BD695 0.09 BD696 0.10 BD697 0.40 BD698	2.30 BF595 2.47 BF596 3.60 BF597 1.85 BF617	0.27 BU207 0.18 BU208 0.27 BU208/02 1.05 BU208A	1.65 1.12 1.97 1.12
16905 17052 17074 17088	0.86 2SB546 5.61 2SB56 6.60 2SB618A 4.80 2SB631	3.64 2SC735 2.23 2SC782 1.83 2SC783 3.25 2SC806	1.16 AD145 2.47 AD149 3.98 AD162 11.29 AD262	1.60 BAV18 0.90 BAV19 0.45 BAV20 1.05 BAV21	3.96 BC556 0.21 BC557 0.11 BC558 0.11 BC559 0.34 BC560C	0.16 BD699 0.10 BD700 0.10 BD701 0.10 BD702 0.10 BD709	3.49 BF618 3.70 BF694 3.48 BF757 3.70 BF758	1.05 BU208D 0.22 BU209 0.58 BU226 0.65 BU312	1.43 1.93 2.39 2.38
17089 17127 17376 17523	5.35 2SB643 5.51 2SB669 1.58 2SB681 1.32 2SB695	0.40 2SC814 3.67 2SC828 3.96 2SC867A 1.98 2SC876	1.39 AF114 0.28 AF115 3.04 AF117 0.96 AF118	2.47 BAX12 1.24 BAX13 0.75 BAX16 1.20 BB119	0.11 BC635 0.11 BC636 0.11 BC637 0.17 BC638	0.10 BD709 0.20 BD710 0.20 BD807 0.24 BD809 0.20 BD810	1.12 BF759 0.80 BF760 0.34 BF762 0.75 BF870 0.69 BF871	0.34 BU326 0.65 BU326S 0.34 BU406 0.30 BU407	2.00 2.20 1.35 0.82
17524 1N4001 1N4002 1N4003 1N4004	1.32 2SB75 0.06 2SB819 0.06 2SB861 0.06 2SC1050	1.04 2SC926A 0.87 2SC930 0.85 2SC935 4.03 2SC937	1.42 AF127 0.54 AF139 4.13 AF178 3.58 AF179	0.50 BC107 0.53 BC107A 1.45 BC107B 0.55 BC108B	0.13 BC639 0.11 BC640 0.11 BC879 0.15 BC880	0.20 BD879 0.24 BD880 0.31 BD895 0.31 BD899	0.71 BF900 0.79 BF907 2.18 BF959 2.48 BF960	1.81 BU407D 0.83 BU412 2.79 BU426 0.42 BU426A 1.90 BU500	1.29 4.80 1.90 1.67 1.78
1N4004 1N4005 1N4006 1N4007 1N4148	0.04 2SC1061 0.08 2SC1096 0.08 2SC1104 0.07 2SC1106 0.04 2SC1114	1.26 2SC940 1.16 2SC9400 2.60 2SC982 4.54 2SD1051 6.75 2SD1128	4.68 AF180 4.68 AF181 0.70 AF182 0.75 AF186	0.55 BC109B 0.53 BC113 0.55 BC116A 0.53 BC126	0.15 BCX32 0.14 BCX33 0.25 BCX34 0.20 BCX37	0.42 BD901 0.27 BD902 0.40 BDV64B 0.67 BDV65B	0.70 BF970 0.61 BFR39 1.26 BFR52 1.26 BFR62	0.61 BU508A 0.44 BU526 0.50 BU608D 0.50 BU705	1.89 2.02 1.57 3.81
1N4448 1N5401 1N5402 1N5403	0.05 2SC1124 0.14 2SC1128 0.15 2SC1129 0.16 2SC1131	6.75 2SD1128 1.26 2SD1138 0.00 2SD1265 0.34 2SD1453 0.50 2SD198	2.25 AF239 0.86 AF279 0.76 AL100 0.75 AL103 3.87 AL113	0.53 BC132 0.88 BC135 4.03 BC137 2.68 BC138 1.36 BC139	0.14 BCY70 0.14 BCY71 0.18 BCY72 0.34 BD115	0.30 BDX32 0.21 BDX53 0.20 BDX53A 0.36 BDX53B	1.75 BFR79 0.88 BFR81 4.05 BFR86 3.35 BFR89	0.29 BU800 0.50 BU806 1.08 BU806D 0.43 BU807	1,57 1,79 1,49 1,40
1N5404 1N5408 1N914 1S1555	0.15 2SC1151A 0.87 2SC1152 0.04 2SC1157 0.20 2SC1162	4.72 2SD234 4.68 2SD235 4.54 2SD257 1.05 2SD288	0.47 AN155 0.60 AN206 2.94 AN208 0.00 AN210	1.36 BC139 1.89 BC141 2.58 BC142 3.55 BC147 2.28 BC147A	0.28 BD116 0.31 BD124 0.34 BD124P+KIT 0.11 BD131 0.12 BD132	0.70 BDX54B 1.31 BDX62A 0.69 BDX63A 0.42 BDX64A 0.42 BDX65A	2.61 BFT41 1.96 BFT42 1.96 BFT43 2.61 BFT84	0.30 BU826A 0.43 BUV46 0.43 BUV84 0.40 BUVV81A	3.94 1.53 1.24 3.06
1S44 1S5012A 1S921 1S689	0.09 2SC1172 TR 0.81 2SC1172Y 0.10 2SC1195 2.06 2SC1213	2.22 2SD291 2.20 2SD292 3.02 2SD313 0.89 2SD315	2.94 AN214 2.59 AN2140 2.59 AN231 2.94 AN234	2.26 BC148 1.86 BC148B 14.43 BC148C 5.09 BC149	0.13 BD133 0.13 BD135 0.11 BD136 0.11 BD137	0.42 BDX65A 0.53 BDX76 0.36 BDY20 0.36 BDY62/01 0.36 BDY81	2.61 BFW10 0.59 BFX29 1.21 BFX30 4.62 BFX84 1.18 BFX85	0.60 BUW84 0.34 BUX84 0.65 BUY69A 0.37 BY126	1.39 1.00 2.04 0.13
1S751 2N1302 2N1303 2N2148	2.06 2SC1226 0.27 2SC1306 0.38 2SC1307 TR 6.27 2SC1316	1.46 2SD325D 1.98 2SD348 1.98 2SD350 4.10 2SD350A	0.91 AN236 16.13 AN238 5.20 AN239 2.29 AN240P	3.33 BC149B 5.48 BC153 4.35 BC154 1.72 BC157	0.13 BD 138 0.14 BD 139 0.14 BD 140 0.14 BD 144	0.46 BF115 0.34 BF117 0.37 BF118 1.43 BF121	0.40 BFX87 0.40 BFX88 0.67 BFX89 0.25 BFY50	0.39 BY127 0.55 BY133 0.34 BY176 0.44 BY179 0.27 BY182	0.13 0.11 1.52 1.42
2N2218 2N2219A 2N2222 2N2646 2N2904	0.42 2SC1317 0.40 2SC1364 0.38 2SC1383 0.80 2SC1391 0.36 2SC1398	0.87 2SD353 TRA 0.49 2SD389 1.20 2SD401 2.45 2SD551	6.12 AN241 2.41 AN245 3.55 AN247P 2.42 AN252	1.71 BC158 4.49 BC159 3.95 BC161 2.57 BC167	0.10 BD150 0.16 BD157 0.28 BD159 0.36 BD160	1.19 BF123 0.67 BF127 0.53 BF137 1.60 BF152	0.13 BFY52 0.13 BFY90 0.13 BLY49 0.31 BR100	0.27 BY184 0.27 BY184 0.61 BY187 2.20 BY189 0.22 BY198	1.05 0.47 0.77 1.76 1.62
2N2905 2N2906 2N2906 2N2926 GRN 2N2926 RED	0.36 2SC1398 0.43 2SC1410 0.38 2SC1413 0.15 2SC1413A 0.19 2SC1475	0.84 2SD588A 2.39 2SD600 3.55 2SD621 5.26 2SD636 0.37 2SD657	1.99 AN253 3.25 AN262 12.67 AN272 0.25 AN281 2.80 AN295	2.97 BC168 1.98 BC170 7.92 BC171 5.45 BC172	0.36 BD163 0.16 BD165 0.11 BD166 0.10 BD168	0.71 BF153 0.62 BF154 0.42 BF157 0.73 BF158	0.58 BR101 0.26 BR103 0.33 BR303 0.18 BR88B	0.70 BY201/2 0.66 BY203/20 1.26 BY206 0.64 BY207	1.50 0.20 0.17 0.22
2N3053 2N3054 2N3055 2N3055H	0.27 2SC1514 0.99 2SC1573Q 0.61 2SC1578 0.85 2SC1617	1.37 2SD669 1.25 2SD679 8.74 2SD731 3.89 2SD787E	3.67 AN301 3.35 AN302 2.11 AN303 0.58 AN305	5.52 BC172B 5.55 BC173 3.99 BC174B 4.39 BC177 8.88 BC178	0.27 BD175 0.17 BD177 0.27 BD179 0.20 BD181 0.26 BD182	0.43 BF159 0.43 BF160 0.49 BF167 0.99 BF173 0.99 BF177	0.18 BRC-M-300 0.31 BRC116 0.38 BRC1330 0.34 BRC300	0.97 BY208 0.67 BY210-400 1.76 BY210-600 2.01 BY210-800	0.46 0.18 0.27 0.34
2N3442 2N3702 2N3703 2N3704	1.16 2SC1670 0.14 2SC1678 0.14 2SC1810 0.14 2SC1815	3.13 2SD811 1.98 2SD823 1.70 2SD837 0.66 2SD856	5.54 AN313 1.98 AN315 1.07 AN316 6.61 AN318	3.41 BC179 2.46 BC182 5.53 BC182 6.20 BC182B	0.26 BD183 0.11 BD184 0.09 BD187 0.26 BD189	0.99 BF177 0.99 BF178 1.21 BF179 0.53 BF180 0.39 BF181	0.55 BRC4443 0.40 BRC4444 0.36 BRC5296 0.36 BRC6109 0.32 BRC82	1.02 BY223 1.02 BY224-400 0.77 BY225-100 0.83 BY226 1.08 BY227	0.85 0.99 1.13 0.25
2N3705 2N3706 2N3707 2N3711	0.14 2SC1829 0.14 2SC1875 0.16 2SC1881K 0.11 2SC1891	2.22 2SD869 4.77 2SD889 2.98 2SD894 3.69 2SD898B N	7.17 AN320 0.21 AN331 0.30 AN337 7.45 AN340P	5.47 BC182L 4.59 BC182LB 5.32 BC183 1.17 BC183L	0.10 BD190 0.14 BD201 0.10 BD202 0.11 BD203	0.65 BF182 0.67 BF183 0.60 BF184 0.60 BF185	0.34 BRC83 0.39 BRC84 0.43 BRX44 0.39 BRX49	1.08 BY227 2.19 BY228 2.08 BY229-800 0.60 BY255 0.53 BY295-600	0.49 0.60 0.00 1.07 0.81
2N3771 2N3772 2N3773 2N3819 2N3823	2.04 2SC1893 1.71 2SC1929 2.29 2SC1938 0.40 2SC1941 1.17 2SC1942	3.02 2SK105H 2.25 2SK152 7.50 2SK34 1.65 2SK41 5.70 2SK79	2.15 AN355 2.46 AN362 0.76 AN5111 1.07 AN5132	5.98 BC183LB 1.75 BC184 2.92 BC184L 4.39 BC184LB	0.26 BD204 0.13 BD207 0.14 BD208 0.26 BD222 0.27 BD225	0.40 BF194 1.22 BF195 1.23 BF196 0.49 BF197	0.14 BRY39 0.14 BRY55 0.17 BRY56 0.16 BSR59	0.69 BY298 0.67 BY299 0.50 BY409 1.29 BY448	0.20 0.60 1.49 0.67
2N3904 2N3908 2N4101 2N4240	0.62 2SC1945 0.62 2SC1953 1.33 2SC1957 3.30 2SC1959	4.53 40408 1.93 40594 0.95 40595 0.31 40636	2.98 AN5250 0.50 AN5435 1.53 AN5602 1.53 AN5610 1.43 AN5612	2.89 BC186 3.08 BC187 0.00 BC204 7.43 BC207 3.51 BC212	0.27 BD225 0.20 BD228 0.16 BD229 0.14 BD231 0.11 BD232	0.49 BF198 0.63 BF199 1.05 BF200 0.50 BF216	0.17 B\$\$38 0.17 B\$TB0140G 0.37 B\$TB01409 0.36 B\$TB0140E	0.59 BY476A 4.34 BYV95C 2.73 BYW56 4.81 BYX10	0.84 0.46 0.34 0.29
2N4444 2N4914 2N5064 2N5293	0.90 2SC1962 0.72 2SC1969 0.71 2SC2009 0.50 2SC2027	1.93 40871 2.92 40872 0.34 74LS00 1.42 74LS02	1.53 AN5613 1.53 AN5602 0.40 AN5703 0.40 AN6310	3.41 BC212B 4.25 BC212L 1.42 BC212LB 5.15 BC213	0.11 BD232 0.26 BD234 0.10 BD237 0.26 BD238 0.10 BD240	0.50 BF218 0.42 BF222 0.47 BF237 0.45 BF240 0.37 BF241	0.36 BSTC0146 0.55 BSTC0233 0.66 BSTC0246 0.17 BSTC1233 0.17 BSTC3146	2.48 BYX55-350 6.12 BYX55-600 6.99 BYX71-600 4.34 BYX84	0.53 0.15 1.25 0.83
2N5294 2N5296 2N5297 2N5298	0.50 2SC2028 0.49 2SC2029 0.50 2SC2057 0.61 2SC2073	2.11 74LS04 2.33 74LS08 1.18 74LS10 1.54 74LS123	0.40 AN6320N 0.70 AN6340 0.40 AN6342 1.05 AN6344	4.28 BC213L 6.46 BC213LB 1.61 BC214 5.87 BC214L	0.10 BD241 0.15 BD242 0.10 BD243 0.14 BD243A	0.39 BF244 0.50 BF245A 0.50 BF255 0.37 BF256	0.47 BSTC20143 0.37 BSTC20643 0.20 BSTD1043 0.28 BSV57B	0.79 BYX93-C24 3.07 BYX93-C7V5 3.37 BYX94 2.85 BYY56 3.31 BZV15-C12	1.75 1.35 0.14 1.20 0.58
2N5490 2N5496 2N6107 2N6109 2N6122	1.49 2SC2078 0.50 2SC2091 0.59 2SC2122A 1.58 2SC2141 1.76 2SC2166	2.39 74LS13 1.30 74LS132 5.12 74LS138 1.86 74LS157 1.98 74LS161AN	0.53 AN6363 0.80 AN6531 0.94 AN6551 0.87 AN6552	11.22 BC214LB 1.95 BC225 0.68 BC237 0.58 BC238	0.26 BD244 0.40 BD244A 0.10 BD245C 0.10 BD246C	0.51 BF256LC 0.85 BF257 0.82 BF258 0.86 BF259	0.42 BSW68 0.34 BSX19 0.33 BSX20 0.34 BSX21	0.60 BZV15-C12R 0.34 BZV15-C24 0.34 BZV15-C24R 0.87 BZV15-C30R	1.28 0.80 1.09 0.80
2N6130 2N6133 2N6178 2N6180	0.72 2SC2216 1.25 2SC2233 0.73 2SC2271 0.73 2SC2278	0.69 74LS196 2.20 74LS20 3.64 74LS244 1.14 74LS245	2.72 AN6610 1.38 AN7114E 0.41 AN7115 1.82 AN7145 2.81 AN7146	4.40 BC238A 5.94 BC239B 2.52 BC252 2.80 BC258 9.90 BC261A	0.13 BD253 0.25 BD278A 0.10 BD317 0.25 BD318 0.22 BD375	1.05 BF262 0.70 BF263 2.35 BF264 2.59 BF271	0.57 BSY52 0.57 BSY79 0.37 BT100A 0.34 BT106	0.50 BZY93C30 0.51 C10188 1.61 C106D 1.18 C1129	1.86 16.52 0.30 0.58
2N6292 2N696 2N698 2N707	0.62 2SC2314 0.43 2SC2320 0.43 2SC2335-KIT 0.43 2SC2526	0.87 74LS26 0.21 74LS30 10.41 74LS367 1.87 74LS373	0.53 AN7150 0.32 AN7151 1.16 AN7156 1.79 AN7158	2.45 BC262 2.26 BC287 2.26 BC294 6.75 BC300	0.22 BD377 0.50 BD379 0.50 BD380 0.45 BD410	0.42 BF273 0.26 BF274 0.76 BF324 0.76 BF336 0.49 BF337	0.20 BT108 0.20 BT109 0.23 BT112 0.30 BT113 0.36 BT116	1.45 CA1310E 1.45 CA1352 2.48 CA3044 2.48 CA3046 1.20 CA3060	2.70 2.05 3.50 2.06
2SA1011 2SA1027R 2SA1076 2SA1095 2SA1103	1.65 2SC2551 0.45 2SC2570 1.96 2SC2570A 2.31 2SC2578 6.55 2SC264A	1.26 74LS47 2.39 74LS73 1.05 74LS74 6.75 74LS75 4.82 74LS86	1.16 AN7218 0.43 AP58076 0.43 AS560S 0.58 AU113	1.64 BC301 4.68 BC302 1.56 BC303 2.97 BC307	0.45 BD412 0.53 BD418 1.04 BD433 0.18 BD434	6.27 BF338 0.76 BF355 0.41 BF362 0.43 BF363	0.40 BT119 0.44 BT120 0.60 BT121 0.60 BT122	1.20 CA3060 1.76 CA3065 2.17 CA3089 2.48 CA3089E 2.48 CA3090	1.65 1.29 0.83 1.43 1.38
2SA329 2SA351 2SA489 2SA490	0.40 2SC2671 1.17 2SC2785 1.17 2SC372 1.67 2SC373	4.82 74LS86 1.99 74LS90 0.75 74LS92 1.40 74LS93 1.16 74LS95B	0.54 AY105K 0.83 AY106 0.83 BA130 0.41 BA1310 (IC) 0.94 BA1320	2.08 BC307A 1.09 BC308 0.14 BC308A 1.98 BC309 1.38 BC317A	0.14 BD435 0.18 BD436 0.11 BD437 0.17 BD438 0.13 BD441	0.49 BF371 0.60 BF391 0.41 BF393 0.49 BF417	0.50 BT123 0.25 BT125 0.59 BT126 0.84 BT128	1.98 CA3094 2.48 CA3131EM 2.48 CAH7023N 2.48 CAH76023N	2.20 3.12 2.67 6.60
2SA493 2SA564 2SA614 2SA628	1.05 2SC383 0.44 2SC388 4.88 2SC394V 1.14 2SC403C	1.33 7805 TO-220 0.50 7805 TO-3 0.81 7806 780B	0.63 BA1330 (IC) 1.16 BA145 0.73 BA157 2.39 BA159	2.75 BC327 0.19 BC328 0.22 BC337 0.12 BC338	0.15 BD442 0.11 BD507 0.08 BD510 0.12 BD517	1.42 BF418 0.66 BF422 0.60 BF423 0.75 BF435 0.00 BF450	1.87 BT128P 0.29 TBA970 0.29 BT151-800R 0.54 BT151 500R 0.35 BTT6018	3.07 CBF16848N-07 3.06 CD4001 1.15 CD4002 1.38 CD4008 2.42 CD4011	1.56 0.38 0.27 1.06
2SA637 2SA673 2SA683 2SA684 2SA699	1.46 2SC41 1.27 2SC458 1.61 2SC495 1.33 2SC508 1.75 2SC515A	2.19 7812 TO-3 0.34 7812 TO-220 0.92 7815 3.70 7818	0.64 BA182 1.16 BA222 (IC) 0.64 BA284/2 0.70 BA301 (IC)	0.19 BC360 1.66 BC368 0.17 BC440 0.87 BC441	0.34 BD518 0.24 BD519 1.09 BD529 0.44 BD530	1.50 BF451 1.50 BF457 1.32 BF458 1.10 BF459	0.29 BTT6218 0.41 BTT8024 0.39 BTT8124 0.52 BTT8224	2.42 CD4011 2.42 CD4013 4.43 CD4016 4.89 CD4017 2.97 CD4020	0.29 0.47 0.45 0.82 1.23
2SA748 2SA817 2SA818 2SA835	1.08 2SC536 0.48 2SC537 1.82 2SC558 2.50 2SC605L	1.85 7824 0.05 AC107 0.54 AC117 3.69 AC123K 1.161 AC128	0.64 BA302 (IC) 0.73 BA311 (IC) 0.43 BA312 (IC) 0.43 BA313 (IC) 0.28 BA317	1.24 BC454 1.32 BC455 0.97 BC460 0.76 BC461 0.04 BC462	0.36 BD533 0.36 BD534 0.42 BD535 0.47 BD536 0.30 BD537	0.67 BF460 0.53 BF469 0.77 BF470 0.61 BF471	0.99 BU105 0.31 BU106 0.55 BU108 0.31 BU109S	1.50 CD4021 2.48 CD4023 1.50 CD4025 2.25 CD4028	0.39 0.28 0.64 0.84
IF YOU DO	ON'T SEE IT LISTE	D ASK FOR QUOT	TE. GIVE MAKE MO	DEL LOCATION.	REMEMBER TO A	0.74 BF472 DD 0.60p POST	8. HANDLING. ADI	5.69 CD4047 D 15% VAT TO TO	1.06 OTAL

	CONO	MIC DE	VICES	DO PO	V 229	TEL SO	PD TE	2 80P	
CD4049 CD4050	0.58 HM9015 0.55 HT4207	3.24 M58478P 17.16 MA06	6.75 OA90 1.07 OA91	0.08 SAF1039 0.09 SAS5010	3.35 SN76131 8.39 SN76226DN	1.92 T6059 1.98 T8001V	1,16 TBA120AS 1,20 TBA120S 0,95 TBA120SB	1.24 TDA1104 1.05 TDA1151 1.05 TDA1170	6.55 1.17 2.37
CD4052 CD4053 CD4069	0.75 ITT2003 0.80 K174YP 0.24 KA2101	0.22 MA1457 3.25 MA8001 2.65 MB3705	2.72 0A95 0.82 0C28 1.79 0C29	0.09 SAS560 2.52 SAS560S 2.15 SAS560T	1.85 SN76227N 1.65 SN76228N 3.14 SN76231	0.75 T9003V 3.27 T9005V 2.55 T9007V	2.38 TBA120T 0.00 TBA120U	0.95 TDA1170S 2.50 TDA1180 2.03 TDA1190	2.04 2.90 2.11
CD4081 CD4093 CD4511	0.29 KC581C 0.72 KC582C 1.10 KC583C	6.32 MB3712 3.97 MB3713 5.54 MB3730	1.85 0C35 1.69 0C36 3.49 0C44	1.06 SAS570 1.28 SAS570S 0.35 SAS570T	1.78 SN76242 2.61 SN76243 2.75 SN76222	5.23 T9008V 5.23 T9010V 2.77 T9011V	1.29 TBA1440 0.96 TBA1440G 1.27 TBA240A	7.20 TDA1190Z 3.99 TDA1200A	2.48 1.43 1.95
CD4516 CP5521 CX034	1.17 KIVI5B 17.83 L129V 11.83 L200CV	0.25 MC1303P 1.69 MC1307P	6.22 OC45 2.16 OC72 1.92 OC75	0.18 SAS580 0.44 SAS5800 0.44 SAS590	2.85 SN76350 2.89 SN76350 2.85 SN76356	2.17 T9013V 3.08 T9014V 2.90 T9016	7.96 TBA395 1.68 TBA3950 1.02 TBA396	1.10 TDA1220 1.10 TDA1230 0.80 TDA1235	3.23 3.88
CX095D CX104 CX108	3.14 LA1111AP 9.64 LA1201 8.16 LA1210	0.88 MC1310P 1.02 MC1327P 1.38 MC1330P	1.30 ON188 1.33 ON236 1.69 OT112	1.07 SAS5900 1.06 SAS660 1.08 SAS6600	2.56 SN76510N 2.97 SN76530P 1.33 SN76532N	1.05 T9019W 1.57 T9034V 0.91 T9035V	1.98 TBA400 1.38 TBA440C 1.39 TBA440P	2.39 TDA1236 5.75 TDA1270 2.45 TDA1327A	4.30 3.74 1.50
CX109 CX121 CX130	7.86 LA1320 11.83 LA1352 5.55 LA1357N	2.87 MC1349P 1.54 MC1350P 6.49 MC1351P	0.81 OT121 1.21 PD144 1.33 PT2014	1.32 SAS660S 2.24 SAS6610 3.04 SAS670	1.33 SN76533N 1.33 SN76540N 3.96 SN76544	1.65 T9038V 1.98 T9051 2.89 T9053V	9.42 TBA480 3.71 TBA4800 1.40 TBA500P	1.57 TDA1327B 1.30 TDA1330 6.58 TDA1365	1.82 1.76 6.99 1.05
CX131 CX134 CX136	11.83 LA1363 11.04 LA1364 11.49 LA1365J	6.21 MC1352P 3.02 MC1357P 3.44 MC1358P	1.12 PT5006 2.15 PT6042 1.30 PT6045	2.48 SAS6700 1.79 SAS670S 6.12 SAS6710	1.33 SN76545 1.33 SN76546 1.33 SN76549	4.87 T9054V 1.65 T9057V 2.59 T9063V	1.19 TBA510 0.70 TBA520 3.24 TBA5200 2.02 TBA530	1.37 TDA1412 1.84 TDA1420 1.68 TDA1470 1.30 TDA1512	1.52 2.90 2.89
CX137 CX139 CX157	11.83 LA1378 11.83 LA1385 4.84 LA1387	6.52 MC14001 1.87 MC14011 7.60 MC14013	2.40 R1038 0.26 R1039 0.41 R2008B	2.19 SAS6800 2.19 SAS6810 1.33 SBA750	2.53 SN76550 1.43 SN76551 1.61 SN76570 2.09 SN76620	0.37 T9064 1.49 TA16420 3.08 TA16421 1.21 TA5814	5.98 TBA530Q 5.98 TBA540 1.49 TBA540Q	1.30 TDA1670 1.15 TDA1770 1.15 TDA1905	4.48 2.90 1.76
CX158 CX170 CX177	4.10 LA3155 7.62 LA3300 6.75 LA3301	1.25 MC14016CP 1.54 MC14025 1.28 MC14049UBC	0.84 R2009 0.60 R2001B 0.58 R2029	1.96 SC9488P 1.33 SC9503 1.33 SC9511P	1.65 SN7660N 2.09 SN76611 1.33 SN76620	0.00 TA6002 2.59 TA7020P 2.59 TA7027	4.20 TBA550 4.80 TBA550Q 4.80 TBA560C	5.25 TDA1908 5.25 TDA1940 1.40 TDA1950	3.20 1.95 4.81
CX187 CX20004 CX506	5.26 LA3350 6.74 LA3361 9.33 LA4030P	1.43 MC1438R 1.23 MC14493P 4.20 MC14497	1.05 R2030 2.82 R2257 14.99 R2265	1.33 SCR957 2.38 SDA2112/2 1.49 SG264A 1.18 SG608	10.28 SN76622 5.26 SN76623 5.26 SN76630	1.65 TA7050 0.69 TA7051 2.55 TA7060AP	1.74 TBA560CQ 1.74 TBA570 0.71 TBA570A	1.60 TDA2002 1.60 TDA2003 1.71 TDA2004	0.90 1.20 2.25
CX507 CX758 D1693	7.62 LA4031P 7.62 LA4032P 2.59 LA4050P	3.20 MC14510BAL 1.92 MC14511BCP 1.57 MC1455	4.43 R2305 1.10 R2306 0.28 R2322 3.47 R2323	1.18 SG608 1.36 SG613 0.59 SG629 0.76 SG6533	8.75 SN76640 8.27 SN76650N 10.31 SN76651	4.24 TA7061AP 2.05 TA7069 1.49 TA7070P	1.27 TBA625A 3.13 TBA625B 1.68 TBA625C	2.17 TDA2005 2.17 TDA2006 2.17 TDA2010	5.08 1.55 1.85
DEC2 E1222 E5024	2.20 LA4051P 0.40 LA4100 0.28 LA4101	1.79 MC14556BCP 1.25 MC1712 1.30 MC7724CP	3.47 R2323 3.88 R2348 3.49 R2354A 2.18 R2354B	2.01 SI-1020H 2.01 SI-1125HD 2.01 SI1125H	10.89 SN76660N 13.86 SN76665N 13.86 SN76666N	2.48 TA7071 1.49 TA7072P 1.41 TA7073AP	3.69 TBA641A12 2.57 TBA641B11 5.86 TBA641BX1	4.13 TDA2020 3.03 TDA2030 1.79 TDA2140	2.77 1.99 1.59
E5386 E5529 E8021	0.25 LA4102 0.25 LA4112 1.29 LA4125	2.81 MC7818C 4.83 MC7824CP 2.13 MC78M12 3.38 MC78M24	4.68 R2441 0.83 R2443 0.94 R2461	1.36 SI-1130H 0.88 SKE1/02 1.50 SKE2F 1/04	6.93 SN76705N 1.20 SN76707N 1.39 SN76708	1.34 TA7073P 4.39 TA7074P 4.86 TA7076P	5.86 TBA651 1.98 TBA673 7.50 TBA7000	1.76 TDA2150 2.45 TDA2151 2.00 TDA2160	6.20 1.93 4.01
E9003 E9005 ESM310BP	0.46 LA4138 IC 0.50 LA4140 4.15 LA4192 4.60 LA4220	3.38 MC78M24 0.88 MCR101 3.65 MCR106/5 1.62 MCR220/7	0.67 R2477 1.57 R2501 2.28 R2540	1.02 SKE2G 2/04 1.28 SKE2G 3/04 1.98 SKE4F 1/02	0.95 SN76709 1.05 SN76730 1.39 SN76810N	5.12 TA7089M 4.66 TA7089P 0.60 TA7092P	1.56 TBA720 1.50 TBA730 6.84 TBA7500	2.50 TDA2161 2.14 TDA2190 2.90 TDA2510	1.85 2.47
ESM432C ESM532C ESM632C ESM732C	4.60 LA4420 4.60 LA4420 4.60 LA4422	2.25 ME0402 1.72 ME0404 1.72 ME0404/2	0.17 R2540X 0.26 R2615 0.47 RC4195NB	3.30 SKE4F 1/06 0.67 SKE4F 2/06 2.16 SKE4F 2/08	0.73 SN76920N 0.85 SN94041 0.86 SN94042	2.90 TA7102P 5.54 TA7108P 4.35 TA7109	5.88 TBA760 1.61 TBA780 3.71 TBA800	1.71 TDA2520 1.65 TDA2521 1.08 TDA2522	2.37 3.30 1.50
ML232B ETTR6016 FND500	2.92 LA4430 3.33 LA4440 5.78 LA4460	1.47 ME0411 4.95 ME0412 2.32 ME4102	0.28 RCA16029 0.24 RCA16083 0.50 RCA16334	2.01 SKE4F 2/10 5.30 SKE4G 2/02 1.02 SKE5F 3/10	1.24 SP5422 0.96 SP8385 1.60 SPS5384	1.83 TA7120P 0.55 TA7122B/P 1.95 TA7124P	0.64 TBA810AS 0.92 TBA810S 2.34 TBA810T	1.00 TDA2523 1.61 TDA2524 1.50 TDA2525	3.03 4.50 3.90
FT3055 GC374 GF758	1.16 LA4461 1.33 LA5112N 0.84 LA7020	2.95 ME545B 2.65 ME6002 7.33 ME6102	10.02 RCA16335 0.26 RCA16600 0.28 RCA16799	1.36 SKS1/10 1.38 SL1310 2.38 SL1327E	2.15 ST1702L 3.14 STA401 1.33 STA441C	0.99 TA7130P 6,76 TA7136AP 2.75 TA7137P	1.27 TBA820M 1.27 TBA890 0.98 TBA900	0.74 TDA2530 1.85 TDA2532 2.48 TDA2533	2.70 2.50 2.30
GF759 GF761 GH3F	1.13 LA7025 1.20 LA7027 1.82 LA7800	8.05 ME8001 9.35 MED411 2.34 MJ2501	0.29 RCA16801 0.75 RCA16802 3.30 RCA17028	0.95 SL1430 1.08 SL1430T 2.48 SL1432	1.39 STK0029 2.31 STK0039 2.25 STK0050	5.54 TA7141AP 5.35 TA7146P 7.67 TA7148P	3.87 TBA920 4.23 TBA9200 1.67 TBA940	1.85 TDA2540 2.31 TDA2541 1.87 TDA2545Q	2.15 2.48 5.94
HA11211 HA11215 HA11223W	2.53 LA7801 5.06 LB1274 0.00 LC4011B	4.15 MJ2955 2.49 MJ3000 1.24 MJ3001	0.99 RCA17074 2.37 RCA17376 1.43 RCA17523	6.60 SL414 1.58 SL432A 0.83 SL437	3.69 STK0059 3.44 STK0080 7.43 STK011	7.13 TA7149P 9.16 TA7152P 3.96 TA7161P	3.26 TBA950 1.52 TBA970 6.23 TBA9700	1.55 TDA2560 1.79 TDA2571A 3.28 TDA2571AQ	2.17 3.10 3.60
HA11225 HA11226 HA11229	4.29 LC7800 8.71 LD3120 2.88 LM1011N IC	7.89 MJ3028 1.13 MJ481 3.46 MJ802	2.65 RCA2060 1.53 RCA60857 5.45 RGP10	2.00 SL439 4.95 SL471 0.50 SL480	2.48 STK013 3.28 STK014 3.14 STK015	7.75 TA7162P 8.84 TA7169 7.75 TA7171P	2.59 TBA990 9.54 TBA231 2.79 TC4001	1.82 TDA2575A 2.57 TDA2576A 1.42 TDA2577	0.50 3.96 2.95
HA11235 HA1124 HA11244	2.48 LM1017N IC 5.25 LM1101 2.82 LM1111	3.41 MJE2955 3.94 MJE3055 4.29 MJE340	1.89 RT402 1.65 RT905A 0.49 S0280	1.58 SL490 2.38 SL901B 2.14 SL917B	2.37 STK016 8.32 STK022 11.96 STK025	6.91 TA7172P 5.25 TA7176P 8.27 TA7193AP	1.41 TC4053BP 2.48 TC4069 6.67 TC9002BP	4.34 TDA2581 1.52 TDA2590 10.38 TDA2591 1.79 TDA2591Q	2.69 2.50 2.50 0.83
HA1125 HA11251 HA1138	4.29 LM1303P/N 4.47 LM1310P/N 5.03 LM2808 IC	1.65 MJE520 1.38 ML231 5.94 ML232B	0.49 S0281 0.99 S1299 2.15 S15H	2.14 SL918A 4.74 SN16848 1.27 SN16861AN0	6.32 STK031 11.07 STK054 4.95 STK070	12.37 TA7193P 7.13 TA7201P 22.31 TA7202P 7.67 TA7203P	4.95 TCA150 2.71 TCA160B 2.47 TCA270Q 2.18 TCA270S	1.79 TDA2593 1.71 TDA2594 2.15 TDA2600	2.47 3.08 5.00
HA11414 HA1144 HA1156	5.65 LM2877 7.52 LM3065N 1.16 LM317CKC	4.93 ML237B 0.85 ML238 1.38 ML741CS	2.51 S175 5.77 S2062D 0.59 S2800	31.48 SN16861N-07 2.07 SN16862AN 5.78 SN16880N	2.72 STK077 2.98 STK073 3.63 STK082	8.52 TA7204P 11.86 TA7205	2.18 TCA270S 2.16 TCA270SQ 1.38 TCA290A	1.65 TDA2610 2.39 TDA2611A 2.16 TDA2611AQ	2.79 1.25 2.81
HA11580 HA1160 HA1166	9.00 LM324N 3.80 LM339N 2.22 LM3407	0.50 ML923 0.80 ML926 1.42 MM5314N	3.28 S28000 3.58 S2802 4.02 S2818	5.54 SN 16965 3.47 SN 16966N 4.05 SN 29715N 5.24 SN 29716N	8.95 STK086 6.04 STK2101 6.04 STK2110 3.66 STK2230	6.32 TA7208P 7.33 TA7210P 7.70 TA7214P	2.15 TCA440 3.58 TCA4500A 3.63 TCA530	1.62 TDA2612Q 2.15 TOA2620 2.16 TDA2631	4.68 1.96 2.73
HA1166X HA1167 HA11711	5.36 LM340T5 5.36 LM340K 18.33 LM340T	0.83 MM5316N 11.85 MM5318N 0.00 MM5369N	3.96 S3702S 3.11 S3703F 2.01 S3707 4 6.20 S40W	5.21 SN29716N 5.21 SN29717N 4.32 SN29722 10.63 SN29723AN	7.19 STK2240 11.95 STK4019 7.65 STK415	0.00 TA7215P 4.50 TA7217AP 7.70 TA7222	2.58 TCA640 1.37 TCA650 1.95 TCA660B	10.26 TDA2640 2.04 TDA2643 3.30 TDA2651	2.59 12.12 2.95
HA11713 HA11714 HA11715 HA11724	8.13 LM340T12 7.76 LM340T5 7.76 LM342N 22.25 LM342P 12V	0.83 MM5387AA/f 0.83 MM5841N 0.62 MN1405 1.62 MN6016A	6.49 S551 9.52 S552 20.56 S6080B	4.54 SN29744N 4.54 SN29764AN 7.57 SN29767	2.29 STK433 1.38 STK435 4.98 STK436	4.95 TA7226 5.94 TA7227P 7.21 TA7229P	10.25 TCA730 2.81 TCA740 4.45 TCA750	3.81 TDA2652 2.48 TDA2653 1.93 TDA2654	6.95 6.18 4.73
HA11725 HA11738 HA1192	18.26 LM342P 15V 22.25 LM342P 5V 0.00 LM348N		1.49 S6087AR 1.49 SAA1006 1.57 SAA1020	4.90 SN29770BN 1.59 SN29770AN 4.76 SN29771BN	4.24 STK437 2.25 STK439 4.93 STK441	7.80 TA7232P 8.31 TA7240AP 11.28 TA7310P	6.60 TCA800 6.75 TCA8000 2.15 TCA830M	5.95 TDA2660 5.95 TDA2661 2.25 TDA2670A	2.47 2.47 1.94
HA1196 HA1203 HA1306	7.43 LM380N 1.72 LM384N01 2.26 LM567CN	2.80 MPC1355C 3.25 MPC596 1.43 MPF256C	1.98 SAA1021 2.13 SAA1024 0.60 SAA1025	4.76 SN29772BN 2.81 SN29773 4.40 SN29791	4.64 STK443 2.51 STK459 1.67 STK460	10.29 TA7312P 8.27 TA7313AP 10.75 TA7314 IC	2.45 TCA830S 1.50 TCA890 5.94 TCA900	2.38 TDA2670 4.95 TDA2680 2.04 TDA2690A	2.48 3.20 2.65
HA1322 HA1339 HA1342	2.18 LM6402A093 2.33 LM6402A123 2.23 LM748	10.15 MPS6570	0.48 SAA1050 0.65 SAA1051 0.27 SAA1061	4.16 SN29798N 5.83 SN29799N 3.61 SN29845	5.56 STK461 8.88 STK463 2.36 STK465	9.60 TA7323P 11.50 TA7324P 10.31 TA7325P	5.78 TCA910 0.96 TCA940 0.98 TCA940E	1.65 TDA2780AQ 1.80 TDA2790Q 2.93 TDA2791	5.14 6.52 2.50
HA1350 HA1365 HA1366WF	3.27 LM8360 4.02 LM8361	3.22 MPSA92 3.57 MPSU05 2.81 MPSU10	0.45 SAA1075 0.86 SAA1082 1.56 SAA1121	4.86 SN29861 8.85 SN29862 4.43 SN72709	2.29 STK466 2.29 STK501 0.44 STK502	11.77 TA7607AP 6.32 TA7609 5.74 TA7611AP	13.90 TCE330 3.17 TCE527 4.05 TCE82	3.89 TDA2795 1.86 TDA2800 1.08 TDA2910 1.08 TDA3000T	2.78 12.98 13.25 2.55
HA1367 HA1368 HA1368R	4.32 M1025 1.90 M1124 1.98 M1130	5.17 MPSU55 2.80 MPSU56 5.35 MPSU60	0.99 SAA1124 0.60 SAA1130 1.33 SAA1174	2.45 SN7400N 4.13 SN7401N 7.77 SN7402N	0.34 STK5314 0.27 STR1096 0.65 STR441	9.48 TA7622 4.50 TA7628P 10.73 TA7640AP	7.50 TCE83 9.38 TCE84 1.19 TCEP1000 2.81 TD190	1.08 TDA3000T 1.08 TDA3030A 10.25 TDA3190 0.95 TDA3300B	11.49 2.68 6.47
HA1370 HA1374A HA1377	3.71 M191 8.80 M193 3.96 M21C	6.32 MR510 18.55 MR812 0.83 MR818	0.67 SAA1250 0.21 SAA1251 0.27 SAA3027P I	3.90 SN7404N 4.90 SN7408N 9.37 SN7410N	0.24 STR451 0.27 STR453 0.27 STR454 1.60 STR6020	4.95 TA7676P 8.16 TA7726P 7.50 TAA300 8.31 TAA310A	2.81 TD190 10.25 TD3F700H 2.97 TD3F800H 1.16 TD3F900H	6,60 TDA3500 4,86 TDA3501 4,16 TDA3506	4.25 12.09 13.01
HA1389 HA1389R HA1392	2.39 M23C 2.05 M51102L 3.90 M5115P	0.83 MR914 6.35 MSM4069 5.24 MSM5816RS		4.02 SN74121 5.39 SN74122 4.50 SN7413N 5.78 SN74151AN	1.60 STR6020 1.05 T6007\/ 0.37 T6016 1.51 T6017	9.95 TAA320A 0.40 TAA350A 0.72 TAA435	1.27 TD3F900R36 0.80 TDA1001B 1.82 TDA1002	4.16 TDA3510 2.31 TDA3520 1.98 TDA3521	6.55 9.71 13.39
HA1394 HA1397 HA1398	8.00 M51231P 3.76 M5124P 3.98 M5134-9341	3.04 MSSD7002 4.82 MVS240 4.13 MVS460 11.97 MVS460-02	0.72 SAA5020 0.51 SAA5030 0.34 SAA5040A 0.61 SAA5050	8.25 SN74151AN 16.23 SN74190 7.74 SN7420N	1.27 T6018V 2.00 T6021 0.34 T6022V	0.72 TAA550 0.40 TAA570 3.92 TAA611B12	0.37 TDA1003A 1.74 TDA1005A 1.30 TDA1006A	1.79 TDA3541 2.22 TDA3560 1.69 TDA3561	3.80 5.00 6.50
HA1406 HA1452 HA17723 HBF4030A	2.07 M51394P 1.63 M5139AP 5.94 M5142P F 2.48 M5143P	7.43 NE545B 5.49 NE545B 7.33 NE5534N	3.94 SAA661B 4.18 SAA700 1.63 SAB1009B	1.96 SN7430 3.30 SN7440N 4.99 SN7473	0.49 T6026 0.27 T6027 0.62 T6028V	0.98 TAA621AX1 0.81 TAA630 0.39 TAA661B	2.48 TDA1010 2.95 TDA1011 1.00 TDA1028	1.33 TDA3561A 2.08 TDA3562A 2.45 TDA3571Q	5.77 4.50 2.48
HD4480 HD44801A HD44801A	17.16 M5144P	3.77 NE555 2.55 NE556 3.10 NE5560N	0.38 SAB1046P 0.83 SAB3011 3.48 SAB3012	4.03 SN7474N 7.34 SN7490AN 5.88 SN75110	0.44 T6029V 0.93 T6032V 0.75 T6033V	4.86 TAA691 0.98 TAA700 0.60 TAA840	8.58 TDA1029 2.59 TDA1034B 2.50 TDA1035T	4.89 TDA3571A 2.42 TDA3576 2.55 TDA3590	6.24 7.09 6.79
HEF4001 HEF4011 HEF4528 HM6231	0.00 M51516L 0.00 M51517L 9.81 M5152L	3.95 NE565N 3.71 NE645BN 2.88 NE646N	1.33 SAB3013 3.35 SAB3021 2.98 SAB3022B	5.61 SN76001AN0 7.90 SN76003 13.58 SN76003N	1.65 T6035\ 0.00 T6036 2.50 T6037	0.73 TAA930 0.67 TAA970 2.11 TAD100	4.87 TDA1037 2.83 TDA1037D 2.52 TDA1041	2.95 TDA3651A 5.55 TDA3950 2.16 TDA4040	2.96 3.40 6.12
HM6232 HM6251 HM7103	8.89 M51522 5.70 M5191P 2.46 M5192	5.39 NE650N 4.94 NE654BN 2.20 NP1106	4.34 SAB3023B 4.18 SAB3024 4.80 SAB3209	12.30 SN76013HDG 6.36 SN76013N 5.23 SN76013ND	8.88 T6041V 3.99 T6044V 2.48 T6045	0.73 TAD110 0.95 TAG232-600 1.20 TAG626-600	2.52 TDA1044 0.73 TDA1047 1.06 TDA1054M	2.31 TDA4050A 4.10 TDA4180P 1.21 TDA4260	3.47 1.92 1.54
HM9032 HM9102 HM9104	3.22 M5194AP 3.22 M53273P 3.24 M53274P	5.74 OA200 1.02 OA202 1.33 OA47	0.11 SAB3210 0.11 SAB4209 0.14 SAF1031	3.23 SN76023N 14.03 SN76033N 2.53 SN76115AN	2.59 T6049 2.68 T6052V 1.61 T6058	1.45 TBA11701 0.87 TBA120 0.59 TBA120A	6.25 TDA1059B 1.05 TDA1060 1.05 TDA1082	0.80 TDA4280 2.59 TDA4290 3.06 TDA440 All goods should be di	7.20 4.47 4.90
	STERED OFFIC			XTON LANE, 1	TELFORD			All goods should be di within 4 working d	ays

TELEVISION JULY 1985

VCR Clinic

Sharp VC381

This machine would play back in colour but wouldn't record in colour. Everything was checked - a.f.c., 4.35572MHz carrier, there was even a down-converted output to the record drive stages. The level of the 625kHz signal seemed to be low however, though there were no levels shown in the service manual to confirm this. So the i.c. was changed - to no avail. At this point Andy made coffee and was asked to prohibit all disturbances whilst intense concentration took place. The conclusion reached was that the 5.06MHz output from filter FL503 was very low. Although a large difference does occur between the input and output from this filter, in this case the output was very, very low. The filter was suspected with some trepidation, since filters don't usually fail - unless it's in a Sharp VC381 that is! So beware: it's now a known stock fault. Just as a point of interest, the down-converted colour signal level at pin 1 of the colour i.c. should be 500mV p-p on colour bars. The carrier signal at pin 28 should also be around 500mV.

Mitsubishi HS300

The fault on this machine could be termed a video nasty. It was a classic symptom to put the blood pressure up a few points. The machine would run for a couple of seconds then stop – a system control fault. On closer inspection we noticed that the playback picture broke up into noise bars just before the machine stopped. This indicated that the r.f. switching pulse (flip-flop to you) was breaking up, which was confirmed when the trusty scope was connected to TP4C. The signal from the drum pick-up coil was correct at IC401 (AN6340) and no other problems were evident, so the i.c. was diagnosed as faulty and was replaced. Well, er, anyway the fault remained.

The monostable signals from within the i.c., at pins 21 and 22, were checked and found to remain stable even as the flip-flop pulses disintegrated. Rather disconcerting, since everything that followed was within the i.c. which we'd just changed. I then noticed that the pulse level at pin 22 was not as high as that at pin 21 - it was only about a third of the amplitude. Both monostables within the i.c., PG1 and PG2, are identical, with the same timeconstants, but there's an extra "switching control" external to the PCB linked to pin 22. This control is mounted at the back of the machine and is labelled "still adjustment". We found that a screened cable to a plug marked ED had been badly positioned at some time and was forced tight against the potentiometer tag, cutting the PVC coating and forming a resistive path chassis. This reduced the voltage to the potentiometer. While the timeconstant remained the same, the pulse level was reduced and this affected the triggering of the following internal bistable flip-flop. Phew!

Sony SLC7

The 400mA fuse (F004) had blown. Another blew whilst I tried to check the operate and standby switches. With a six inch nail across the fuseholder I was able to ascertain that the machine didn't switch off – it was on all the time. First impressions were that the clock display was reading

Reports from Steve Beeching, T. Eng., Derek Snelling, B. Ross, John Coombes and Philip Blundell, Eng. Tech.

"E:E" and that all the red LEDs on the programme timer were lit. The power supplies were o.k. and something smelt hot: it was transistor Q3 on the timer panel – I got a blister on my finger! The programmable timer IC1 didn't have any switching pulses at pins 22-27, though the clock pulses at pin 1 were present and correct. A new i.c. (MB8841-180) and Q3 restored normal operation. The reason for the machine failing to switch off was that pin 11 of IC1 remained high, holding the power supply on via D1. It seems that most of the i.c.'s output pins were set high, hence the demise of Q3.

Sony SLC5

Eject and rewind were o.k. but there was no playback or fast forward. Move straight to the forward sensor i.c. (IC8) on the systems control panel. Output pin 8 was high with the result that the system control microcomputer i.c. thought the tape end sensor had operated. I think IC8 (BX342) also has a tendency to play up intermittently.

S.B

Grundig VS200

This is a fine machine but we have had a couple of problems. One had a faulty r.f. amplifier. As this is fixed to the tuner/i.f. panel it must be removed before being returned to Grundig – it's not necessary to replace the lot. A second VS200 produced spots on playback, similar to static discharge: there was also some noticeable sideways shift to the picture, as though the drum speed was changing. The cause was found to be grease on the motor wiper contacts, inside. If you have to remove the bottom fixing plate, mark it with respect to the outer casing of the motor - the reason for this is that rotating the plate with respect to the motor body (stator) will cause more interference. The plate is rotated during assembly for minimum electrical noise: either reassemble it where it was or carry out the "tuning" adjustment as specified in the manual.

Watch this Space!

We've just purchased some duff Sony SLC5s and SLC7s from one of the bulk suppliers in Birmingham. Most of them seem to have been abandoned due to system control faults. Watch this space!

The New Mitsubishis

A few words on the new Mitsubishi models. The HS307 is a two-speed version of the HS306, with infra-red remote control. No skew correction etc. is incorporated in the long-play mode so visual search in this mode is poor. On the other hand narrower heads have been used than in the HS330, giving a better long-play picture. One possible problem is that there's no indication as to whether L.P. or S.P. has been selected.

The HS400 is a single-speed hi-fi machine. The standard sound is in mono and the pause is of the "instant stop" type with a noise bar where it happens to stop.

There are facilities for TV/external stereo/simulcast recording and the machine can be used as an audio only hi-fi recorder. The record levels can be set manually or automatically, two bar-type meters giving indication of the levels. There's audio dropout compensation for head switching.

D.S.

Mitsubishi HS304

A fault we've had several times recently with these machines is dry-joints on IC2A0 (M51450P). This can give rise to various symptoms – intermittent picture on record, intermittent colour on record, intermittent speed variation and intermittent plackback luminance. Care must be taken when resoldering this i.c. as many machines have a soft varnish sprayed over the solder side of the panel in this area: the varnish must first be scraped off thoroughly to make correct soldering possible. In fact it seems to be the machines with this varnish that suffer from dry-joints.

A weakness that's shown up on this model is the remote control socket. It's mounted directly on the corner of the presetter board and we've had four cases so far where the customer has pushed too hard when inserting the remote control plug with the result that the corner has broken off the panel. This can cause loss of signals as the return path for the tuning potentiometers passes near the socket. If the customer wishes to continue using the remote control system the panel should be replaced, since any repair is likely to fail after a couple of insertions of the remote plug. Fortunately the panel is quite cheap. D.S.

Ferguson 3V32

Dead VCRs are usually easy, aren't they? Don't be fooled, not all of them are! This one looked dead at first glance, until you noticed that the off light was illuminated. A quick check on the supply lines showed that nothing was wrong except that the switched 12V line was missing because the relay wasn't energising when the on switch was operated. Attention was turned to the tuner/timer board as this drives the relay. The clock oscillators were running and the reset/interrupt lines were normal. A study of the manual was called for. One of the tables shows the functions of all the microcomputer pins in detail. Using this we scoped each pin in turn. Pin 36 of the i.c. (IC206) is shown as being the power off/a.c. detector and was low when it should have been high. D207 rectifies an a.c. input from the tuner/timer subpanel and was found to be P.B. open-circuit.

Grundig 2 × 4 Super

The machine was playing back when unthreading was selected by remote control. It unthreaded and ejected the cassette but thereafter refused to load a cassette. Switching on subsequently started the head and reel motors, the machine appearing to be in the "stop" (still frame) mode. Fifteen seconds later the tape fault logic put a stop to things – confirmed by the keyboard (system control) module lines WS1/2/3 all reading high. The threading ring switch contacts and cassette compartment switches were checked, including the one hidden inside the cassette retaining lip. All were in order, as was the operation of the reel brake solenoid and the c/o switch.

We turned the threading motor manually to load and thread a cassette, switched on and found that the machine unthreaded correctly. Attention was then directed to the keyboard module, particularly to the power supplies. During fault chasing the symptoms changed to playback LED lit, no motor action, with lines WS1/2/3 all low, meaning "tape" (stop mode). The relay remained deenergised.

At switch on a 150μ sec reset pulse is sent to the microcomputer i.c. This is followed by an initiation cycle. If the power supplies to the keyboard module are low or slow to build up this time window may be missed. The back-up batteries and accumulator module were removed and tag A and AC1-5 on the power board linked. No improvement. Meter and scope checks on the reset line revealed a blip at switch on, implying that the reset pulse was present. The 15V rail was correct and the 5V line read 4.8V (it comes via a transistor until the relay energises). Further checks were made on the keyboard module. The clock signals were present and no obvious faults could be found. The previously mentioned switches were meter checked from strobe lines 5 and 6 to input lines AF1/2/3, proving that the connections via the motor connection board were sound - this is an area where poor connections can give trouble.

We diagnosed a faulty microcomputer i.c., but as the cost of this is half the cost of an exchange module and much of the board logic is interrelated an exchange unit was fitted. This produced play, record and the wind functions but cassette eject produced nothing followed by no other control functions. Controlled anxiety (deep depression) followed. We wound the threading motor manually to unload the cassette and return the slide rack to the end stop. Thereafter cassettes would load and unload and all functions worked. We can only assume that during fault finding the relative positions of the sliding rack and ring drive gear on the threading mechanics became displaced. One question remains: did the remote control unit that operates the strobe and input lines to the microcomputer i.c. cause the damage?

B.R.

Mitsubishi HS320

For poor or no fast forward check the pinion cog which can slide down the shaft, removing the drive to the take-up reel. If you order the pinion cog for the HS330 you'll find that it has two grub-screw fitting, giving more secure positioning on the shaft. This fault can also break the tape in the playback or rewind modes and has been known to chew the tape in playback.

J.C.

Hitachi VIP201P Disc Player

In the event of no stylus arm movement first ensure that the cartridge cover is locked in. If this is all right and the disc loads correctly but there's no arm movement check the arm motor. In one case we found the motor seized up: a drop of oil released the shaft to prove the point, a new arm motor restoring correct operation.

J.C.

Panasonic NV333

The fault was no field lock in playback. The sync signal amplitude turned out to be only 1V p-p instead of 2V due to IC3003 (AN6327) in the luminance channel being defective.

J.C.

Mitsubishi HS303

In the event of intermittent hum on sound, check the audio head switching relay K3F0 by replacement. J.C.

Long-distance Television

Roger Bunney

April saw a dramatic improvement in long-distance signal propagation, particularly towards the end of the month with improved Sporadic E conditions. There has also been productive auroral activity. A small event on April 9-10th gave Band I reception from Scandinavia in the northern UK. Over April 19-21st there was a much larger auroral event. A sudden, high-level disturbance on the sun produced storm conditions which were particularly intense on the 20th, giving auroral 144MHz amateur band propagation from Leningrad to the UK. During this period Band I was full of characteristically "hummy" vision signals from Scandinavian and E. European sources. The auroral conditions continued through to the early hours of the 21st, a smaller auroral opening occurring during the afternoon. Following this major event, ionospheric conditions remained very unsettled up to the end of April.

Tropospheric conditions also improved marginally over the month. During the evening of the 19th Benelux and W. German signals were received in the south and east of the UK in Band III and at u.h.f. A more intense tropospheric opening late on the 22nd produced more sustained Benelux, French and W. German signals over much of the UK, as far as the Midlands. As I write this on May 6th it looks as if a further tropospheric opening is about to occur. Several enthusiasts have reported an increased number of Band III Canal Plus stations during the slightest of tropospheric lifts. Caen ch. F9 has proved to be an easy catch here in the Southampton area. Lille ch. F5 can be received throughout much of the UK and along the N.E. coast – as it could be when the old 819-line system E transmissions were in use.

SpE provided the main excitement towards the end of the month, with four consecutive days of openings, most being of long duration with intense signal strengths. This is undoubtedly a sign of better things to come. Unfortunately some of the openings occurred during weekday working hours and will thus have been missed by many. The SpE log is as follows:

9/4/85 SRG (+PTT - Switzerland) ch. E2; ARD (W. Germany) E2; TSS (USSR) R1; CST (Czechoslovakia) R1.

15/4/85 ORF (Austria) E2a; CST R1.

29/4/85 TSS R1, 2; CST R1; ORF E2a; JRT (Yugoslavia) E3; RAI (Italy) IA, B; SRG/+PTT E2; TVE (Spain) E2.

1/5/85 TSS R1 (very strong during the early morning); ORF E2a, 4;MTV (Hungary) R1; RAI IA; TVP (Poland) R1; TSS R1, 2.

2/5/85 ORF E2a; JRT E3, 4; unidentified ch. R1 and 2 signals.

3/5/85 EPT (Greece) E3; JRT E3, 4; RAI IA, B; TVP R1, 2; TVR (Rumania) R2.

An opening during the morning lasted up to 1200. Ray Davies (Norwich) received EPT during much of the morning period.

My thanks to Iain Menzies (Aberdeen), D. Patuzzo and Roger Pates (both in Nottingham), Dave Shirley (Hastings), Reg Roper (Torpoint), Cyril Willis (nr. Cambridge) and Ryn Muntjewerff (Holland) for their reception reports which supplement my own log.

Roger Pates mentions a mystery transmitter radiating Anglia TV in colour on ch. E10. It was noted towards the end of April – a query to the IBA failed to produce any information. Roger checked his immediate neighbourhood for a faulty, i.e. radiating, receiver then set out on a trip to try to establish the source of the signals, which are weak in the Nottingham area. He thinks they come from the Lincoln area.

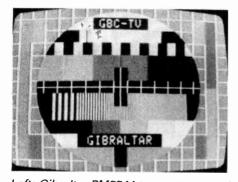
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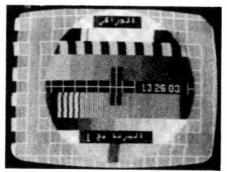
Fred Pilkington (Newmarket) lives for part of the year near Torremolinos in Southern Spain. In addition to TVE, signals can be picked up there from Morocco and Gibraltar. He reports that GBC presents problems, with only 250W e.r.p. at 70 miles – Fred is now using a ZL special Yagi to receive GBC, which has moved from ch. E12 to ch. E11 to avoid interference from RTM (Morocco).

News Items

France: Advertisements on Canal Plus during unscrambled transmission times started in early May: the service now claims to have over 300,000 subscribers. The TV5 French language satellite channel is to increase programming to four and a half hours this autumn: a further extension to eight hours is planned. A reciprocal agreement for the exchange of programmes has been reached by TV5 and Canada.

Greenland: The 50·045MHz amateur radio beacon OX3VHF at Denmarks-Haven has closed down. Plans are to start up from another location in late July/early August.







Left: Gibraltar PM5544 test pattern received by Fred Pilkington at his flat near Torremolinos, S. Spain. Centre: Moroccan test pattern received by Fred Pilkington in S. Spain. Right: EBU News exchange at 4GHz, received by Frank Lumen in Denver, Colorado via a Satcom downlink.



Lattice aerial mast for the 900MHz cellular phone network, at Rhownams near Southampton. The mast carries several vertically polarised colinear arrays with corner reflectors.

New Zealand: Advertisements are to be allowed on the TV1 and TV2 networks for a similar amount of time daily - but not on Sundays, Christmas Day or Good Friday. Pakistan: A second network is under construction. Programmes will be mainly educational. Three studio centres are being established, at Lahore, Karachi and Islamabad,

feeding a network of eighteen transmitters via an extensive microwave link system.

USA: Ted Turner's CNN cable news service is to be made available to European cable networks this autumn, linked via an Intelsat satellite.

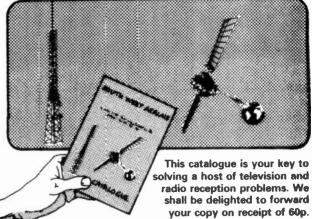
High Spec Ch. E2/R1 Amplifiers

The end of UK TV broadcasting in Band I has left the band relatively wide open for DX reception, though cordless phones are causing headaches for some enthusiasts. Multiple-hop SpE sometimes brings in ch. E2 signals from the Ghana/Nigeria region. In the past such signals have often been marred by distant BBC-TV signals on ch. B2. Along the south coast it would be worthwhile monitoring ch. E2 for the weak, scattered SpE signals that are commonly seen in central and southern France but are less frequently noted in the UK.

There's great interest at present in the 50-52MHz amateur radio allocation, use of which is currently on an experimental basis and restricted to non-TV hours. This interest has resulted in the appearance of high-specification 50MHz aerial amplifier kits on the market. It occurred to me that this type of preamplifier could be retuned to cover ch. E2, providing high gain, very low noise and good selectivity (i.e. no overloading from local CB operators, something that can happen with wideband preamplifiers). Apart from the specialised Mutek Model BBBA500u 20-500MHz aerial amplifier with its 1.5dB noise figure, most commercial amplifiers tend to have a noise figure of around 4dB at best.

The Cirkit Holdings PLC (Park Lane, Broxbourne, Herts EN10 7NQ) kit type 40-08006 is available at £7.25 plus 60 postage, excluding VAT, for use on the six metre amateur band. I bought the kit with a view to using it to cover the ch. E2/R1 section of the band, though there's enough gain to pass ch. E3/R2 signals (ch. E4 signals suffer attenuation). Maximum gain of some 20dB is available over a bandwidth of around 3MHz, the gain





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falling rapidly on each side: the noise figure is 1.5-2dB. Construction is very simple apart from the need to wind a wideband toroidal transformer. The kit comes complete with a metal case, BNC sockets, PCB and all components. A dual-gate m.o.s.f.e.t., type 3SK45, is used: fitting a 3SK88/BF960 provides increased gain with a slightly reduced noise figure. The preamplifier was originally a REW project by Graham Leighton. Using the tuning capacitors and Toko coils provided I found that the input circuit wouldn't peak to give maximum gain on ch. E2 further shunt capacitors were needed. With 4-7pF added across C1 and 3.9pF across C3 the bandpass coils L1 and L2 could be peaked as required. As a specialised amplifier for ch. E2/R1 DX use this project can be highly recommended.

For the more adventurous the narrow-band 50MHz

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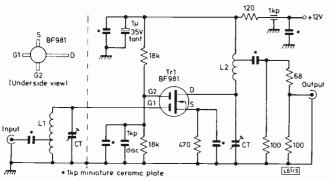


Fig. 1: G4IJE's 50MHz narrow-band preamplifier. L1 consists of 9 turns, 22g, tapped 2½ turns from the chassis end; L2 has 10 turns, 22g, tapped 1½ turns from the 12V end.

preamplifier (see Fig. 1) designed by Paul Turner (G4IJE) is worth serious consideration. Once again a dual-gate transistor is used, this time the higher performance BF981 which provides higher gain and lower noise than the device used in the Cirkit project. The input and drain load circuits are both tuned by miniature variable trimmers (5-65pF, RS type 125-660) and can be peaked above and below the 50MHz band. This circuit is for the more experienced r.f. operator, since care must be taken over the screening, decoupling and close observation of v.h.f. constructional techniques (i.e. minimal lead lengths etc.) if stability is to be achieved. Our thanks to Paul and the Six Metre Group for permission to reproduce the circuit which originally appeared in their bulletin *Six News*.

We'd be interested to hear from DXers of the results they achieve with narrow-band Band I amplifiers and if possible any observations on comparisons with the use of wideband amplifiers.

PAL/SECAM Converter Module

News of a converter module which can be fitted to a normal PAL-only colour receiver to enable it to display PAL or SECAM signals has come from our Dutch DX-TV friends. It's made in W. Germany by Dahner Elektrik and is available from S.A.P. of Wiesbaden-Bierstadt as Module KS478/SM1. It's suitable for use with most PAL only sets and will switch automatically on reception of an E. European SECAM signal, i.e. from GDR or another OIRT source. There are just eight wired connections and the module requires 85mA (typical) at between 12-30V d.c.

We understand that 6-5MHz system D sound adaptors are also available. The S.A.P. company will indicate connection points for specific receivers and the cost, at early April 1985, was DM 142 plus 14 per cent VAT. Ryn Muntjewerff tells us that he has been using one of these modules and that good SECAM is resolved.

For French system L SECAM reception, a VTK1

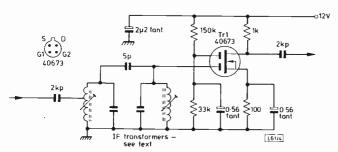


Fig. 2: Mike Gaskin's selective i.f. preamplifier circuit.

module can be used in conjunction with an SMI to give vision and sound on a standard PAL receiver. It appears however that certain teething troubles have been experienced as a result of which marketing of the package has been delayed. We will pass on any further news received from our Benelux/German friends.

Simple Selective IF Preamplifier

Mike Gaskin (Caterham) has sent in the simple but effective i.f. preamplifier circuit shown in Fig. 2. It provides good selectivity using a 40673 dual-gate m.o.s.f.e.t. in a simple, non-critical circuit. The double-tuned, lightly coupled input transformers give (depending on whether peaked or stagger tuned) a variable bandpass characteristic. It's suitable for cascading, each stage providing a gain of some 12-15dB.

Mike used i.f. transformers taken from old transistor i.f. strips. He feels that they may give less than optimum matching to the 40673 transistor and suggests that experimentation could give improved results. Cirkit have a range of Toko 35MHz i.f. transformers that could be used in the circuit. Although Mike's prototype has the input tapped in at the hot end of the first coil there's no reason why the input shouldn't be experimentally coupled to the top of this coil.

Commercial Corner

East Cornwall Components (119 High Street, Wem, Shropshire SY4 5TT, telephone 0930-32689) tell us that they can supply 22in. remote-control v.h.f.-u.h.f. Decca/Tatung TV sets in single-standard format (e.g. system B/G with 5·5MHz sound) for either PAL or SECAM colour (the latter with a slight delay) at £295 inclusive of VAT, carriage paid in the UK. Apart from the French system L, sets for any system in use throughout the world can be supplied – apparently the service is used by people returning from the UK to countries where the prices of TV sets are vastly in excess of UK prices. Send enquiries to Mr. M. Cox at the above address.

The Worthing and District Video Repeater Group has available for ATV enthusiasts considering 23cm/1·3GHz operation a kit of parts to make a three full-wave colinear plus reflector aerial system with a gain of 10dBd over a dipole and a horizontal beamwidth of 60° (-3dB points). The array covers the whole 23/24cm band and has been found to give excellent results into France as far as Paris. The kit of parts costs £10·95, with instructions, and can be obtained from Mr. R. Stephens, Toftwood, Mill Lane, High Salvington, Worthing, W. Sussex – the price includes post and packing. The group has no other products available at present.

Satellite News

We understand that Sky Channel is to drop scrambling – this should be of interest to exiled UK residents along the south coast of Spain/Portugal.

The 4GHz Spacenet-2 satellite at 69°W has been received in Yorkshire (elevation 5°) with the CNN cable news feed.

The Intelsat organisation has given permission for their TV programme feeds to be downlinked via several US satellites, including Satcom 1, 3, 5, Comstar D4, Spacenet-1 and Galaxy-1. Frank Lumen in the USA checked and found that various European news feeds, including ITN, TG1 (Italy) and certain EBU services, were available via transponder 11 on Satcom F1.

Making PCBs

Malcolm Burrell

It often happens that you want to build something or even replace a damaged subassembly in a piece of equipment but the cost of a new board is exorbitant or one simply isn't available. The disadvantage of using Veroboard is that you can easily make mistakes while the amount of cutting and wiring can be time consuming. Varying the component layout can also sometimes cause problems. The solution is to make your own board.

Unless you are likely to be involved with a large number of projects the investment required for photographic board production is not worthwhile. It also remains a time consuming process. Recently I wanted to make a small number of boards. I couldn't afford much time or money but devised a compromise method that worked well.

Layout Design

The first step was to design the layout. I'd a working prototype built on Vero V-Q board and it was quite easy to sketch in the components on the paper template supplied. The previously wired sections were then linked as tracks and gradually a layout was developed. One thing to remember is that the print pattern is the reverse of the component layout. Dealing with this is quite easy really: draw your design on paper then soak it in varnish so that you can see the layout on the reverse side. This can be photocopied so that you have a record of the original design however much you mutilate the original drawing.

Making the Holes

Starting with the original drawing, it's easiest first to mark out the component mounting holes. Tape the drawing to the top of the board and use a 1mm drill to make the holes. The miniature drills advertised by firms such as Maplin are a useful investment. It's possible to use the average household DIY type of drill but these are clumsy and you'll all too easily break the small bits. If you intend to make two or three boards to the same circuit they can be stuck together with tape and drilled in one go. It's best to drill the mounting holes in the corners first, then temporarily fix the boards together using say 6BA screws.

Print Pattern

This will leave you with a plain board full of holes but with no print pattern. The holes will act as a guide: you can join them up by sketching in the print design with a felt-tipped pen. For a really neat job you can buy dryprint transfers – these are especially useful for i.c. pads.

Using this method of drilling the holes first you must make sure that all burrs have been removed. Then clean the board with alcohol to leave a clean surface for the transfers. A pen and ruler can give quite a good pattern without transfers however.

One way to make neat i.c. pads is to link all the holes

with a paint marker pen When the paint is completely dry, score lines between the holes with a knife so that the bright copper shows through.

Having laid out the tracks I like to make each one as thick as possible without adjacent tracks touching. The paint marker pen is useful for this purpose since it gives thick, even lines that are less likely to be eroded by the etching acid. There are two other reasons for keeping the tracks thick – unless you're concerned with v.h.f. circuits. First, some circuits take a considerable current: there's nothing worse than to spend a lot of time making a neat board only to see the tracks melt like fuses when the power is switched on. Secondly, the acid can be reused several times: since its strength decreases as more copper is dissolved it's best to etch away only as much copper as necessary, leaving the rest behind to strengthen the board and ensure satisfactory connections.

Etching

Check the board before etching it. For the etching bath a good disposable plastic tray such as an old polythene sandwich box can be used, preferably with some plastic tongs. If you wish, attach a piece of thread to one corner of the board so that it can be moved without direct contact.

Take everything into the garden shed away from everyone – and wear old clothes! Pour enough acid into the tray to cover the board. Etching is a tedious business: agitate the acid every minute or so or it will take a very long time indeed. Etching should be complete after twenty to thirty minutes. Carefully remove the board from the etchant and plunge it into cold water. Cover the acid and rinse the board thoroughly under a tap – remember that all traces of acid must be removed from the holes.

Hints and Tips

If you wish to store the acid, either pour it into the original bottle using a funnel or use a secure glass bottle labelled "acid". I understand that it's dangerous and undesirable to dispose of acid into the sewerage system. If no neutralising agent is supplied the best course is to dig a hole in the garden and pour the used acid into this.

Painted markings on boards can be quite easily removed with alcohol. A touch with emery cloth will leave a bright copper surface for soldering. Once the components have been mounted and soldered it's a good idea to brush the print with varnish to help protect it from corrosion.

The print patterns are often given with projects in the magazine. If they are to scale it's better to photocopy them rather than to cut the magazine, using the photocopy as a template for drilling. It's all rather like painting by numbers, but you have the option to vary the layout or increase the size of the circuit to suit yourself.

Mounting the board in its case is easy if you use 6BA threaded spacers. Screw these into the case first, then use ½in. 6BA screws to secure the board. Alternatively plastic stand-offs can be used. These need slightly larger fixing holes, typically 0.2in. – I find a 3/16in. drill useful for these.

Prototype Working

A final hint. For prototype working, off-cuts of printed circuits can be etched without drilling and the components mounted on the print side.

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More on the Philips G8 Chassis

Dennis Apple, B.Sc.

Tony Thompson's article in the May issue contained much valuable information on the Philips G8 chassis. The following notes may also be of interest to readers – they are based on experience gained servicing a large number of these sets.

Connector and Panel Faults

Before switching on, check the various plugs and sockets on all panels. A small needle can be used to close up slightly all tired spring holders within these connectors. Don't forget the tube base. Also ensure that the various fuses are all securely fitted in their holders. Finally the flying leads, especially those on the line scan panel, should be checked for tightness. A quick spray of cleaning fluid such as WD40 on all connectors prior to reassembly helps prevent further problems. It's surprising how many baffling, intermittent faults disappear after this treatment!

You may also find hairline cracks around each panel where the edge connectors are located, no doubt caused by someone's over-zealous attempt in the past to tighten the two retaining screws without first ensuring that the edge connector is correctly mated. The timebase panel is the one most likely to be affected by this problem. You will almost certainly find that the print under the contrast and field hold controls has suffered stress due to careless back cover fitting in the past: insert the knobs through the holes in the cover before locating the cover in its retaining groove.

Setting up the HT

The correct h.t. voltage at TP67 (either of the h.t. fuses) should be 205V under normal working conditions. The official setting up procedure is as follows:

- (1) Turn the set h.t. control R1370 to approximately mid-position.
- (2) Turn the overvoltage preset R1396 fully anticlockwise to disable the overvoltage protection circuit.
- (3) Turn R1370 until the reading at TP67 is 225V.
- (4) Turn R1396 clockwise until this reading falls to 220V. On a working set the picture will then flutter, showing that the overvoltage protection circuit is operating.
- (5) Turn R1370 to obtain 205V at TP67.

If you cannot carry out this procedure the power supply is faulty. The most common faults are picture flutter, inability to obtain the correct voltage, and intermittent fuse blowing.

Picture Flutter

The causes of picture flutter are usually as follows:

- (1) Defective BR100 trigger diac (D1377) in the power supply. In an emergency this device can be reversed. Testing is difficult since the device measures virtually infinite resistance both ways substitution is the best way of proving the guilt or innocence of this component.
- (2) Defective power supply thyristor (SCR1379). A standard fault on the G8. It should be replaced whenever the power supply is suspect. The thyristor can appear to be all

innocent when checked with a tester but play silly games when in circuit. For example, in one case of picture flutter the thyristor was found to be light sensitive: its anodecathode resistance fell to a few thousand ohms when a bright inspection light was shone on to it! Gentle heat had the same effect.

- (3) H.T. smoothing capacitor C5536 (600μ F) on the line scan panel defective.
- (4) Very low field sync pulse amplitude due to a defective TBA550Q i.c. on the signals panel.
- (5) H.T. reservoir capacitor $\dot{C}1385$ (600 μ F) on the power supply panel defective: this capacitor tends to leak horrible-looking gunge as it slowly loses capacitance.

Incorrect HT

Causes of inability to obtain correct h.t. voltage (205V) are usually:

- (1) Thyristor becoming leaky as the set warms up.
- (2) Assuming that no other faulty component is found, you'll probably find that one or both of the two high-stability resistors R1368 ($470k\Omega$) and R1369 ($8.2k\Omega$) has changed value. Such changes are usually small and difficult to detect using a normal test meter substitution is by far the quickest way of testing these components. Temporarily dabbing a $1M\Omega$ resistor across these suspects will show which if either has changed value. Be careful not to blow the set up by careless testing in this area: as you probably know, the line output transformer in this chassis has suicidal tendencies.

Fuse Blowing

The mains fuse is rated at 3·15A and is of the anti-surge type. It's useful to distinguish between violent fuse blowing (blackened, charred debris) and peaceful demise. In either case check the thyristor first by substitution.

Violent fuse blowing is often caused by:

- (1) The insulation between the "mains dropper" R1367/R1381 and the chassis mounted fixing lugs becoming defective.
- (2) A defective mains switch, especially when of the earlier open variety.
- (3) A short-circuit mains filter capacitor C1366, 0.33μ F. In the event of non-violent fuse blowing simple replacement may restore normal operation. If not, suspect the h.t. reservoir capacitor C1385 and the line output transformer the latter may blow fuse FS5557 (800mA) on the line scan panel.

Timebase Panel

The most common fault on the timebase panel is failure of the transductor, which can suddenly go up in a cloud of smoke. A quick check is to disconnect plug H, which will take the line section of the transductor out of circuit, but leaving the plug out permanently will impair the picture geometry. This can normally be observed only on a crosshatch pattern. Its importance depends on the screen size and the cost of repair.

Inability to set up the line hold can be caused by the 18V zener diode D4531.

Poor field lock and picture jumping between scenes can be caused by the TBA550Q i.c. on the signals panel.

Field collapse sometimes occurs when R4533 (if fitted) springs open. Resoldering often provides a permanent cure. Later boards were modified to prevent this.

C4452 in the field charging circuit can leak to give bottom foldover when cold.

Note that although the field scan coupling capacitor C4479 is shown with the correct polarity on circuit and wiring diagrams on some panels the connections are incorrectly printed. If the capacitor is fitted the wrong way round the whole picture floats gently upwards, no amount of field shift control adjustment restoring correct conditions. This occurs because as C4479 becomes more leaky more unwanted d.c. flows through the field scan coils.

Lack of height can be caused by the bootstrap capacitor C4469 (220 μ F) falling in value.

Line Scan Panel

The line scan panel, on which the driver and output stages are mounted, causes the majority of faults in the G8 chassis. The dreaded line output transformer lives here. Anyone attempting to service G8 chassis should have a stock of replacement transformers to hand if only to prove the innocence of this component should a weird symptom present itself. The cost of replacement transformers is fortunately not high and they are easy to obtain – perusal of advertisements in the magazine will soon confirm this.

For the uninitiated, the line output transformer can cause the following symptoms: (1) failure of fuse FS5557 (800mA), often intermittently; (2) reduced width with overheated windings; (3) intermittent crackles and picture fluctuations; (4) smoking from the overwinding.

If both line output transistors go short-circuit FS5557 blows. It's more common for one transistor to go short-circuit however, leaving the other to plod on. In this event the symptoms are a slightly oversize picture with low brightness and contrast, the picture size changing with alteration of the brightness control setting. In general the picture looks drab and lacks sparkle, giving the impression that the tube is about to meet its maker. Low h.t. voltage will also produce this state of affairs of course, so the prudent engineer will always start by checking the voltage at the two fuses on the power supply panel.

A quick, reliable check on the output transistors is to measure the voltages at the two heatsinks. Under normal conditions one voltage should be about half the other, i.e. 190V and 90V. If both collectors are at about 190V one transistor is probably short-circuit. The originals were BU105s: a pair of BU208s make ideal replacements.

There's a trap here for the unwary however. After replacing both transistors with known good ones the original fault symptoms may persist, with both heatsinks still at about 190V. In this case the fault is nearly always due to the balancing coil L5003, which is at the extreme top of the panel. In fact this may be all that was originally wrong. You'll almost certainly find that the core is stuck,

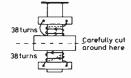


Fig. 1: Details of the line output transistor balancing coil L5003, which is at the extreme top of the line scan panel.

and any attempt to force it will result in the little metal cap breaking off. A replacement coil can be purchased, but a quick way of dealing with it is as follows:

(1) Unscrew the four mounting screws then unsolder the whole coil from the upper board (take care not to leave little solder bridges across the print).

(2) Very carefully cut around the centre of the coil former with a junior hacksaw until you just hear the blade contact the stuck ferrite core (see Fig. 1).

(3) Unscrew one half of the assembly from the other, gently – they are not connected electrically.

(4) Gently unscrew the protruding ferrite core from one half of the assembly, using hand pressure only.

(5) The threads of the former can now be cleaned and the core reinserted with a trace of silicone grease on its threads. The whole assembly can then be resoldered to the board. Use a small amount of Araldite to hold the cut halves of the coil together.

After refitting the coil, turn the core while observing a stationary test pattern. At the correct core position the picture will be of minimum width and the e.h.t. will be at its correct, maximum value. The voltages at the two transistor heatsinks should then be at approximately 190V and 90V. Note that zero voltage at the heatsink of the "lower" transistor T5532 can also be caused by misadjustment of L5003.

The whole surgical operation on the coil takes about five minutes and is easily carried out using the simplest of tools.

Always make the output transistor heatsink voltage test when dealing with this chassis – it saves so much heartache!

Failure of F5557 has been traced to D5567 (OA91) going short-circuit (very early version of the panel with original type of beam limiter circuit). Failure of F5560 (1.25A – late version of the panel) has been traced to the 25V rectifier diode D5539 (BY210-400).

It pays to check the various diodes on the line scan panel before condemning the output transformer.

Sound Faults

A crackling sound with the volume control turned to zero has been traced to noisy BD131 audio output transistors, also a noisy TAA570 intercarrier sound i.c. This i.c., used in the earlier versions of the chassis, has also been responsible for a range of symptoms including no sound and severe buzz. If the associated quadrature coil L2601 is misadjusted the result will be low sound with buzz.

Crackling on one channel only (or when using a VCR) can usually be removed by very careful adjustment of the extreme left-hand core in vision selectivity can U2800, i.e. L2807. Distorted sound can occur when one of the BD131 audio output transistors goes open-circuit. Usually however the print to one of these transistors becomes detached, giving the same symptom even though the voltages may not appear to be too far from their correct values.

Convergence Panels

The earlier, sturdy vertically mounted front convergence panel was very reliable. This cannot always be said of the later, rear chassis-mounted panel used in the 550 series. Convergence drift is caused by the heat-sensitive AC128 transistors and the electrolytics on this panel. The

electrolytics dry up in the heat produced by the convergence potentiometers, especially the infamous R1934 ($10\Omega-R/G$ parabola) which often causes the whole board to burn up. A replacement panel may well cost more than the set is worth. Guard against R1934 overheating by removing the printed card and placing a heatsink around R1934. Noisy potentiometers on this panel can easily be cleaned with a spray of silicone oil. This should be done before attempting convergence.

Chroma Panel

Faults on the chroma panel are usually due to defective i.c.s. Sometimes a dry-joint develops on the luminance delay line (or the print underneath it), causing a double side-by-side image. This symptom is very often intermittent and can make one feel schizophrenic until one realises the cause. Loss of one primary colour is usually caused by a dud output transistor, a broken track or a dry-joint, e.g. on one of the output transistor emitter resistors. The $39 k\Omega$ TBA530 load resistors R7326/R7346/R7363 change value to give incorrect colours.

In General

I agree with Tony Thompson's remarks regarding trade disposal sets. A sharp eye is indeed required when examining sets prior to purchase. One supplier swore on a stack of bibles that all his sets were complete but denied all responsibility when I later found that two panels were missing from one set.

A very good indication of what's wrong with a set is often given by the state of its interior. A line scan panel

hastily put back in position so that it almost falls out of the set usually means line output transformer trouble. The tube base left disconnected suggests bad news about the tube. A thick layer of dust over everything usually means that the set has simply died and the owner decided to exchange it for a new one. In such cases the fault is often a trivial one and the set can be got going as good as new – bearing in mind that the tube may not be in its prime.

The biggest problem is usually with the state of the cabinet. Very often an otherwise excellent looking set bears horrible scratches on its highly polished surface. Attempts to mask such defects usually fail because the wood becomes discoloured. The only complete solution when dealing with cabinet defects is to scrape the wood along the grain, in the same direction, using a very sharp wide chisel, until the whole surface is restored to its original pristine condition. Two coats of semi-matt clear varnish will then bring the appearance back to new. The discoloured wood veneer surrounding the tube can also be given this treatment - be careful not to crack it as it's very brittle. Use a barely wet fine brush and silver paint to restore the worn tracery around some models. With patience the cabinet can be made to look like new, but only you can decide whether the time spent on this is worthwhile for the return it brings.

It's essential to soak test a G8 before delivering it to the customer. Some faults, such as convergence drift or varying field height, may make their appearance only the morning after delivery, the set having worked faultlessly the previous day. Generally speaking the G8 is an excellent chassis with readily available spares: provided it has been conscientiously serviced and adjusted, a set will give many years of trouble-free viewing.

Sonys and Suchlike

Nick Lyons

Oriental chassis can sometimes be a little mysterious to an old "Empire" brain. Few are more mysterious than Sonys. Although generally very reliable and providing good pictures, there are some models I find it hard to forgive. I do forgive the modified NTSC decoders used in the early colour sets, honest. Also the otherwise superb KV1340 which just looked as if it had two dozen boards, half of which were no bigger than a large box of matches, linked together with a wiring loom like a telephone exchange. There's one sin so vile however that I cannot find forgiveness within me: the gate-controlled switch. Why Sony found it necessary to use these when everyone else managed without I don't know. Anyway, enter on cue a KV1810 with a terminal tube, the bottom of the picture a third of the way up the screen and atrocious linearity. Ever wishing to avoid this set with its GCSs, I suggested to the owner that any fault worse than a loose mains plug wasn't worth bothering about with the tube in such a shocking state. This was not his view however, so without further ado battle commenced. At least the bloody GCSs hadn't gone I thought. More on that later.

The KV1810, Part 1

A linearity control tweak just made matters worse, i.e. the bottom started to fold over. Never trusting linearity networks my first and entirely useless move was to check the two $2.2\mu F$ electrolytics that are connected in series

with the linearity control. Let's move to the other end of the field timebase I thought and see what the output stage is doing. Well, what it was doing wasn't quite right. The Avo proved that the output transistors were o.k. but the scope revealed drive problems. Always suspicious of electrolytics, especially non-polarised ones, I pulled out the bootstrap capacitor C520 (10 μ F, 16V) and also the similar but polarised coupler C522. Both were useless: having replaced them (C520 with a non-electrolytic type – it was huge, but as half the circuit was on the back of the board anyway . . .) things looked better but not completely right. It was not until C529 (10 μ F, 16V) in the height circuit and C533 (1 μ F, 160V) in the field amplifier circuit had also been replaced that the correct range of height and linearity could be achieved.

This left the set displaying a remarkably linear picture on a very weak tube – not only dim and largely green, but it was of the "by the time it's bright enough to see you can't focus it any longer" variety. Focus adjustment on these sets is another pain, being a solder tag effort – this really isn't good enough on a colour set. It did however improve the performance – to pretty bad!

Attention was next turned to the grey scale – magenta blacks, pink dark greys and lime green white. Not very promising. Much twiddling proved that this was about the best of which the tube was capable – at this heater voltage. Now naughty though this is, I thought that the only recourse with this tube was to bump up the heater

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voltage. The mains transformer in these sets (it was a Mark I version) supplies only the c.r.t. heaters and the primary is tapped at 200, 220 and 240V. I thought it would be a good idea to put a crocodile clip on the transformer tap flyhead so that I could quickly change taps with the set running to see whether any worthwhile improvement was achieved. Well it did seem a good idea at the time, but I'd reckoned without the GCSs. As soon as I moved the flylead from the 240V tap and dabbed it on the 220V tap – bump, hum and the set was dead. The back-e.m.f. from the transformer had put enough of a pulse on the mains to kill off the GCSs. By now I was beginning to think that the whole thing was a bad idea: both GCSs had gone dead short - heaven alone knows how well these sets fare in households with poorly suppressed vacuum cleaners and the like.

After replacing the GCSs and putting the tube on the 200V tap a barely passable image could be discerned in a dimly lit room, but at least it was in focus. Time to get it back to the customer in haste. It was to return however, almost as hastily. But first for something completely different.

Monitor Trouble

Professional video monitors are a strange breed and never like to do anything by halves. Here's a case in point. At switch on the e.h.t. rustled up: all should have been well but there was no raster. In this sutuation, with e.h.t. present but absolutely no screen illumination, it's always been a habit of mine to glance at the tube's heater before doing anything else – of course it's always been lit and the trouble has been elsewhere. Always that is except this time. No light at all. Out with the Avo which recorded around 1V across the heater pins. So the heater wasn't open-circuit, but something was amiss. The circuit diagram showed that there's a heater winding on the mains transformer, but this isn't connected directly to the heater. Nothing as crude as that. A bridge rectifier, reservoir capacitor, series resistor and an 8V regulator chip were all present. As with all hi-tech equipment it was the hi-tech bit, i.e. the chip, that had failed.

Slow Slog

It seems to me that I have to slog through even the simplest of faults. I must have been the last person on Earth to attribute almost any fault on a Rank T20 chassis to 4R16. I always attribute faults on these sets first to the start-up circuit then to the line output transistor's series base feed resistor. It seems however that there are those who are slower than I: a colleague was amazed at my revelation that the field cramping on his ageing relative's set (Thorn 1400 chassis) was due to the diode dropper in the heater line going short-circuit. It's successful diagnosis like this that keeps me going. Going where?

The Damaged Portable

Well, on my way to do a little training the chap at the sports centre counter waylaid me to recount a tale of woe. Apparently his dog had had a little sport with the family's Contek portable, bowling it over in the process. Although the case had suffered minimal damage, the same couldn't alas be said of the PCB. Quite extensive damage had occurred in the general area of the heaviest component, the line output transformer. Fortunately the cracks were

for the most part visible and the board could be patched up. In cases like this I always find switch-on to be a bit dicey. This was no exception. A fearful display of arcing from the line output transformer occurred, though the rest of the set seemed quite happy. Close examination showed that the transformer's case was cracked, with particularly bad damage around the moulding where the e.h.t. lead leaves. A new transformer would have cured the fault but one wasn't to hand and the expense had to be considered.

Repairing the LOPT

Strips of tape were used to make a pouch over the cracks in the casing, the tape forming the outer wall of the pouch which stood about an eighth of an inch away from the casing. A proprietary epoxy resin was then mixed and poured into the pouch. A piece of plastic pipe about 3/4in. in diameter and about as long was used to repair the damaged e.h.t. moulding. The pipe was slit open so that it could be got over the e.h.t. lead without having to remove the cavity connector, then positioned on top of the transformer around the lead moulding. Preparations were completed by taping the bottom of the pipe to the transformer and taping up the slit. Epoxy was poured in and left for half a day to set, after which the tape was removed, revealing a neat-looking job. But would it stand the best part of 30kV across it? I switched on with trepidation. The set sprang to life and all was well. Some weeks later it still is. So for a couple of feet of tape, a bit of tube, about a quarter of a pack of epoxy and not a lot more time than it would have taken to fit a new transformer if I'd had one the set was back in service. I wouldn't expect this to work with all transformers or in every case but with transformers of this type of construction (similar to TX10 types) a reasonable success rate looks likely.

The KV1330

Set dead said the report, and so it was. This particular Sony KV1330 had run faultlessly from new (must have been the best part of ten years). The input fuse had popped with some force. On replacing it and measuring the mains input with an Avo a dead short was recorded. Clearly the mains filter capacitor had died and there it was, obvious on the input panel. I removed it, a brown toffee-looking thing, and fitted a purpose-designed mains filter capacitor. Sony had been generous, drilling several sets of spare holes in the panel to accommodate various lead spacings. Incidentally I'd recommend fitting purposedesigned mains filter capacitors for both safety and reliability – if you do use a standard type, use one rated at 1kV d.c. or 400V a.c. at least. Having said all this, as you'll probably have guessed by now the fuse blew at switch on. Why? Well there are actually two such capacitors in this set, the other one residing on the power regulator panel. It was actually this one that had died. C601 by name.

Return of the KV1810

Which brings us back to the KV1810 which had by now reappeared with more field trouble. We'd replaced most of the electrolytics last time. What was left? Well the scan coupling capacitor C517 (22 μ F, 160V) for a start. When it was removed a ring of goo was left on the panel. It had indeed gone to its maker.

TELEVISION JULY 1985 515

BBC Micro Test Pattern Program

550 ENDPROC

570 CLS

560 DEFPROCvert

580 FORX=91TO1279 STEP 91

Patrick Kniveton, B.Sc.Eng.

The following program was designed to provide most of the patterns normally produced by a TV pattern generator plus one or two extras. All operations are called from the function keys - a small identifying strip can be used to label each key. Operation of one of the keys calls up the appropriate procedure: these are all initially listed on the Menu screen which can be recalled at any time by pressing f8. The program is written in BASIC and is therefore slow in parts - readers will no doubt be able to suggest improvements.

The patterns available are: crosshatch; colour bars; dots; vertical lines; horizontal lines; circle (for linearity setting); red, green, blue, magenta, cyan, yellow, white and black rasters; a composite test card. The program can be saved on tape or disc.

```
20 REM TV SERVICING AID
 40 REM BBC MICRO B
 60 REM (C) P.E. KNIVETON 1985
100 *KEY0 MODE0:M PROCxhatch:M
110 *KEY1 MODE2:M PROCcbars:M
120 *KEY2 MODE2:M PROCdots:M
130 *KEY3 MODE0:M PROCvert:M
140 *KEY4 MODE0:M PROChoriz:M
150 *KEY5 MODE0:M PROCcircle:M
160 *KEY6 MODE5:M PROCraster:M
170 *KEY7 MODE2:M PROCcard:M
180 *KEY8 MODE7:M PROCmenu:M
190 PROCmenu
200 END
210 DEFPROCxhatch
220 CLS
230 FORY=0TO1023 STEP 64
240 MOVE0,Y
250 DRAW1279,Y
260 NEXTY
270 FORX=91TO1188 STEP 91
280 MOVEX.0
290 DRAWX,960
300 MOVE(X+2),0
310 DRAW(X+2),960
320 NEXT X
330 ENDPROC
340 DEFPROCebars
350 CLS
360 MOVE0,1000
370 PLOT85,0,0
380 FORbar=1T08
390 IF INT(bar/2)=bar/2 THEN colour=(8-bar)/2 ELSE
    colour=(8-bar)+INT(bar/2)
400 GCOL0, colour
410 PLOT85,(bar*160),1023
420 PLOT85,(bar*160),0
430 NEXTbar
440 VDU23,1,0;0;0;0;
450 ENDPROC
460 DEFPROCdots
480 FORX=91TO1188 STEP 91
490 FORY=0TO1023 STEP 64
500 MOVE X,Y
510 DRAW,Y+1
```

```
590 MOVEX,0
600 DRAWX,959
610 MOVE(X+2),0
620 DRAW(X+2),959
630 NEXTX
640 VDU23,1,0;0;0;0;
650 ENDPROC
660 DEFPROChoriz
670 CLS
680 FORY=0TO1023 STEP 64
690 MOVE0.Y
700 DRAW1279,Y
710 NEXTY
720 VDU23,1,0;0;0;0;
730 ENDPROC
740 DEFPROCcircle
750 CLS
760 VDU29,640;512;
770 MOVE350.0
780 FORC=0TO2.1*PI STEP 0.05
790 PLOT5,350*COSC,350*SINC
800 PLOT5,352*COSC,352*SINC
810 NEXTC
820 VDU23,1,0;0;0;0;
830 ENDPROC
840 DEFPROCraster
850 CLS
860 IF GET$="K"THEN VDU19,0,0,0,0,0
870 IF GET$="R"THEN VDU19,0,1,0,0,0
880 IF GET$="G"THEN VDU19,0,2,0,0,0
890 IF GET$="Y"THEN VDU19,0,3,0,0,0
900 IF GET$="B"THEN VDU19,0,4,0,0,0
910 IF GET$="M"THEN VDU19,0,5,0,0,0
920 IF GET$="C"THEN VDU19,0,6,0,0,0
930 IF GET$="W"THEN VDU19,0,7,0,0,0
940 IF GET$="E"THEN GOTO960
950 GOTO860
960 VDU19,0,0,0,0,0
970 ENDPROC
980 DEFPROCmenu
990 CLS
1000 PRINT TAB(9,2); CHR$(141); CHR$(130); "TV
     SERVICING AID"
1010 PRINT TAB(9,3);CHR$(141);CHR$(130);"TV
     SERVICING AID
1020 PRINT CHR$(129); CHR$(157); CHR$(135); "f0";
     CHR$(156);CHR$(135);"Crosshatch"
1030 PRINT
1040 PRINT CHR$(129);CHR$(157);CHR$(135);"f1";
     CHR$(156);CHR$(135);"Colour bars"
1050 PRINT
1060 PRINT CHR$(129); CHR$(157); CHR$(135); "f2";
     CHR$(156);CHR$(135);"Dot pattern"
1070 PRINT
1080 PRINT CHR$(129); CHR$(157); CHR$(135); "f3";
     CHR$(156);CHR$(135);"Vertical lines"
1090 PRINT
1100 PRINT CHR$(129); CHR$(157); CHR$(135); "f4";
     CHR$(156); CHR$(135); "Horizontal lines"
1110 PRINT
1120 PRINT CHR$(129); CHR$(157); CHR$(135); "f5";
     CHR$(156);CHR$(135);"Circle"
```

520 NEXTY

530 NEXTX

540 VDU23,1,0;0;0;0;

1130 PRINT **1470 NEXTD** 1480 MOVE320.0 1140 PRINT CHR\$(129); CHR\$(157); CHR\$(135); "f6"; CHR\$(156); CHR\$(135); "Raster" 1490 GCOL0,7 1500 FORC=0TO2.1*PI STEP 0,02 1150 PRINT TAB(9); "(Press R for Red, G for Green," 1160 PRINT TAB(10); "B for Blue, C for Cyan," 1170 PRINT TAB(10); "M for Magenta, Y for Yellow," 1510 PLOT5,320*COSC,320*SINC **1520 NEXTC** 1180 PRINT TAB(10); "E to ESCAPE raster routine)" 1530 MOVE0.0 **1190 PRINT** 1540 MOVE309.75 1550 FORF=0.24TO3.0 STEP 0.1 1200 PRINT CHR\$(129); CHR\$(157); CHR\$(135); "f7"; CHR\$(156):CHR\$(135):"Test card" 1560 PLOT85,309*COSF,309*SINF **1210 PRINT** 1570 PLOT85,0,0 1220 PRINT CHR\$(129); CHR\$(157); CHR\$(135); "f8"; **1580 NEXTE** CHR\$(156);CHR\$(129);"RETURN TO THIS MENU" 1590 MOVE-100,0 1600 MOVE-100,-201 1230 VDU23,1,0;0;0;0; 1240 ENDPROC 1610 PLOT85,100,0 1250 DEFPROCcard 1620 PLOT85,100,-201 1630 GCOL0.0 1260 CLS 1270 FORY=0TO1023 STEP 64 1640 MOVE-100,0 1650 MOVE-100,201 1280 MOVE0,Y 1660 PLOT85,100,0 1290 DRAW1279.Y **1300 NEXTY** 1670 PLOT85,100,201 1310 FORX=91TO1188 STEP 91 1680 GCOL0.7 1320 MOVEX,0 1690 MOVE-60,0 1700 DRAW-60,303 1330 DRAWX,960 1710 MOVE-300,-75 **1340 NEXTX** 1720 MOVE-300,75 1350 COLOUR 132 1360 PRINT TAB(8,28);" 1730 L=-225 1370 PRINT TAB(8,29);"TSA1" 1740 FORJ=1TO8 1750 IF INT(J/2)=J/2 THEN B=(8-J)/2 ELSE 1380 PRINT TAB(8,30);" ":COLOUR 128 B=(8-J)+INT(J/2)1390 PRINT TAB(0,0) 1400 VDU29,640;512; 1760 GCOL0,B 1410 GCOL0,0 1770 PLOT85, L, -75 1420 MOVE0,0 1780 PLOT85,L,75 1790 L=L+75 1430 MOVE0,1 **1800 NEXTJ** 1440 FORD=0TO2.1*PI STEP 0.1 1810 VDU23,1,0;0;0;0; 1450 PLOT4,0,0 1460 PLOT85,315*COSD,315*SIND 1820 ENDPROC

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BEOVISION 4000 CHASSIS

The problem is fluctuating h.t. It will steady if the voltage is reduced to below 150V by using the h.t. preset.

A common cause of this problem is failure of one of the two $56k\Omega$ resistors 6R29 and 6R30 in the thyristor's trigger pulse generator circuit. They tend to go high in value. If necessary go on to check 6C20 ($47\mu F$), 6R27 (1Ω) and the setting of the current limiter trip preset 6R33. We've also known leakage in the 39V zener diode 6D19 in the excess current sensing circuit to cause this fault.

WAX-SEALED CORES

I've been trying to convert a foreign Hitachi portable (Model 1A-51) for use in the UK. 6MHz coils have been fitted but there's still a buzz present. Hitachi have suggested tuning T401 and T402 for best sound but the cores are fixed with hard wax.

We've found that the most effective way to deal with waxed-up cores is to invert the chassis and gently heat the relevant can, using a hairdryer, until the wax runs out. The cores should then be movable after applying a couple of drops from a commercial ear-drop preparation. Tune carefully for minimum buzz on a vision with teletext or similar transmission with lots of hard white captions.

BUSH BC6004

The trouble with this Saba manufactured 14in. colour portable is that the chopper/line output transistor (Wessel circuit) lasts for only a few weeks. We've replaced the damping components C841/R841 and have made thorough checks but have been unable to find anything amiss. To start with the transistor would last for about three months: now it's down to a few weeks.

On past experience we'd suggest replacing D687 (SKE4F1/10) which is in series with the line scan circuit, the efficiency diode D688 (BY223) and the flyback tuning capacitor C688 (0·0013 μ F), also R941 (100k Ω , 1·5W) which biases the base of the driver transistor. In addition, check thoroughly for dry-joints and similar "physical" faults.

DECCA 10 SERIES CHASSIS

The colour control has to be turned by at least threequarters of its travel before there's any colour. The colours are otherwise all right, but surely the control shouldn't operate like this?

This effect is not uncommon on some Decca 10 series sets. There may however be some lack of chroma gain. If there's any sign of Hanover bars, check the setting and condition of the controls in the chroma delay line

matrixing circuit – VR267 and L206. If the matrixing is all right, check the following components in the order given: the second chroma amplifier transistor's emitter decoupling capacitor C230 (5μ F), the a.c.c. reservoir capacitor C222 (5μ F) and the chroma delay line driver transistor's emitter resistor R268 (82Ω).

SONY C5

The trouble with this machine is failure to record sound off-air. There's sound with playback of prerecorded tapes. I understand that this is not uncommon.

On every occasion when we've encountered this fault the cause has been the TBA120U intercarrier sound i.c. If replacing it fails to restore the sound an oscilloscope will be necessary to check and trace the signal.

RANK T20 CHASSIS

There's ringing on the left-hand side of the screen, similar to the effect that occurs when a line linearity coil's damping resistor goes open-circuit. Adjusting the fifth harmonic tuning coil has reduced the vertical bands considerably but they are still noticeable.

We assume that you've checked the line linearity coil's damping resistor 5R12 (680Ω). If not, check this, the EW correction coupling capacitor 5C15 ($1\mu F$) and if necessary 5C16 ($0.068\mu F$) in the first anode supply network. For reliability, it's important that the fifth harmonic tuning coil 5L3 is correctly adjusted as per the manual. If replacing the above mentioned components fails to clear the fault and 5L3 cannot be set up correctly it's likely that the line output transformer is defective.

THORN 1690 CHASSIS

The original problem with this set was caused by a faulty line output transformer. When this was replaced the picture was found to be greatly expanded in the middle. The height control will correct the top and bottom of the picture but the linearity control has very little effect. I've checked the electrolytics and transistors in the field amplifier/driver/output stages.

The field waveform is generated across C104 (0.047 μ F). Check this item and the associated charging resistor R128 (330k Ω). The next suspects are the 390 Ω resistors R133/4 which bias the emitters of the driver transistors. They can and do change value. This is also true of R132 (27k Ω), the amplifier transistor's load resistor.

SONY SLC7 VCR

After fitting a Sony chopper power supply replacement kit and a new control i.c. the machine came to life for five seconds then went dead again. On investigation the chopper transistors, the surge limiter resistor and the mains fuse had failed. With a replacement fuse the readings on the control i.c., powered via the start-up supply, were found to be correct – apart from the pins linked to the chopper supply output of course. Any suggestions before a second replacement kit is fitted?

The operation of the control i.c. can be checked by disconnecting D204 (soft-start control circuit) and applying an external source of 12V to C203. A 3V sawtooth should then be seen at pin 5 of the i.c. (TP1) and a 20V pp squarewave at pins 8 and 11. If these waveforms are o.k., the rectifier diodes D201/2 and the $4.7\mu F$ electrolytics C110/1 are in order, and no excessive loading is present on the 12V line, suspect short-circuit turns in the chopper transformer T102 – it can happen.

DECCA 30 SERIES CHASSIS

The problem is intermittent horizontal bands across the screen. They are about half an inch wide and comprise six scanning lines, the first two lines being quite dark while the rest are progressively less intense.

This sort of thing can be caused by discharges inside the focus spark gap. Try replacing it – also check the earthing connections between the tube's outer coating and the base panel, thence to chassis.



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Each month we provide an interesting case of television servicing to exercise your ingenuity. These are not trick questions but are based on actual practical faults.

It's generally acknowledged that Bang and Olufsen TV sets have always had the edge over the competition in terms of picture and sound quality. Their reliability has not always been of the best however, and early solid-state chassis from this stable are no strangers in our workshop. No matter what the source, many of the faults that arise in these sets result in a "pumping" action in the power supply as a result of one or other of the protection circuits coming into operation. This month's story is about one such Beopump . . .

The set was a Beovision 6002 (type 3522-3532) with a beautiful rosewood cabinet – and a complete lack of raster and sound. A gentle pumping sound at a rate of about once per second came from within it. Some quick preliminary checks showed that no obvious short-circuits were present in the line output stage while the h.t. line, which should record 148V at 6TP2, was pulsing to about 100V on each pump cycle. A scope check at 5R18 (18 Ω) which is in series with the 148V h.t. line produced a waveform with an amplitude of about 16V, about twice what's normal, indicating that excessive current was flowing in the line output stage.

It didn't take long to unload the various power supplies derived from the line output transformer: 6D9, which produces a 37V supply for the field timebase and the EW modulator drive circuit, was found to be heavily burdened – its removal brought the set to life, albeit with no field scan. We decided to check the field timebase module, 8003200, where a dead short to chassis was found at the supply input point – P19-5. A few more minutes investigation showed that the TDA1270 field timebase chip 7IC1 was the culprit – pin 2 was solidly shorted to the heatsink tabs

After fitting a new chip we confidently replaced the module and switched the set on. No pumping – but no field scan either! In the next twenty minutes we had the

module in and out several times while we checked the output transistors, their joints, the module socket connections and so on. Then we got sensible and reasoned that if there was no field scan activity the white line on the screen would fade within seconds of switching on – which it didn't - due to lack of gating pulses in the auto greyscale shift circuit. Sure enough a scope check at the i.e.'s output pin 4 produced a 50Hz waveform which was also found to be present at the emitters of the output transistors 7TR2/3. The waveform wasn't the usual "spikedsawtooth" however: it was virtually a squarewave with a peak-to-peak amplitude of almost 40V. At this point experienced TV trouble-shooters will be leaping up and down with the correct answer. Are you amongst them? If so, what's the accompanying symptom that sometimes gives a further clue to the cause of the trouble? For the answer to both these questions, see next month . . .

ANSWER TO TEST CASE 270 – page 456 last month –

In our last "tableau" we were huddled around a Philips colour set fitted with the G8 chassis. Its problem was an intermittent red raster that occurred only spasmodically and only when the set had thoroughly warmed up. Various substitution checks had been made in the field and the set was now on the workshop bench for investigation.

The simple and effective way to deal with this situation is to interchange the video drive between the suspect channel (red in this case) and a known good one. So the red and green leads to the tube base were swapped over and the resulting strange colours were suppressed by turning the saturation control to zero. When the fault next occurred the monochrome picture became suffused with red, and since the red gun was now being driven by the green channel this implied that the tube was faulty.

So it turned out to be, though exactly what was happening within the tube was not clear. Any interelectrode short involving the red control grid would have elevated all three grids to a high potential and turned on all three guns. We suspect that the red grid connection to pin 3 was going open-circuit intermittently, though this is very uncommon with the type of Mullard tube used.

No, the customer didn't have a new tube fitted – and we didn't get a bean for all our efforts!

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TELEVISION JULY 1985

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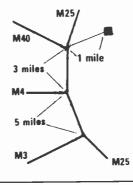
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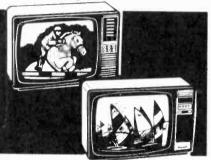
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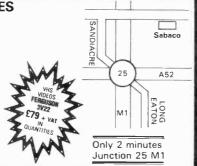
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put-panel	05	U 3845 MR 508	P Freeze	sets	5p £1.20
20AX Line lin coil 50p BU 20	08 80p	MR 501 10 MR 502 10	P Contact Cleaner	Clauman and Ansi C	£1.20 £1.20
trans 20AX ITT CVC20 etc mains BU 20	ND 90m	BCW 71R 30 BYF 1202 10	P Push Button Mains P Lorlin Full Remote Pelay Su		76-
ITT 2,800 mains BU 3:	26 £1 07 60n	BYF 1204 10 BYF 3126 40 BYF 3214 40	Mains timer. 13 amp — up t	o 2 hours: easy to use tion 50mm × 20M	t, plugs into socket £3.00
2110 GEC Power BU 50	26V 60p	BYF 3214 40 BYX 10 6 BYX 36/600 35	Screen locking agent, large ca	in 2014	70p £1.50 £5.00
Panel £8.00 Line o/p frame panels GEC 20AX £10.00 GEC 20 AX BU & BU &	08A £1.20 26 75p 07 £1	BYX 38/300 25 BYX49/600R 75	Red E.H.T. LAED and And 10 × G11 Cap 470/250	•	£1.00 £15.00
Transductor £1.00 BUW	24 50p 84 30 p	BYX 55/350 10 BYX 55/600 (Bead) 10	Weller solder iron 15 watt/25 2 way baby alarm/intercom w	ith long leads	£5.00
Z904 18" Line Panel £10 TIC I	06a 30p	BYX 71/350 20 BYX 71/600 50 BYX 72/300 20	12V Nicad pack, 'AA"		£2.50
Z905B Decoder £10 TIC I Z736 Tuner I.F. £10 TIC I	16n/Y 1003 35p 26N 40n	BYX 72/300 20 BYX 36/600 50 BYV 95B 10	Hitachi TP 007 Battery pack	7.2v/L6A	£6.00 £7
A805 Conv. 7/8 £2 TIC 1: T136A Scan Drive £10 TIC 2: Z780 Line O/P £10 TIC 2: Z968 £10 TIC 2: Z582 L.F. Panel £5 TIC 2:	06m 30p 25S 40p	BVY 95C 12 BYZ 106 10	70ML Silicone Sealer (clear)	GI3 UCC35/ IEC SR	£i
Z968 £10 TIC 2 Z582 l.F. Panel £5 TIC 2	26E 40p 26m 30p 36m 30p	BPW 41 15 BYW 56 2A/1000v G11 8	De-solder pump + 2 nozzels Plastic box for i.e.s 6"×3"×1/2"	,	£12.00 £5.20 50p
Rank Power Panel TICV		BZU 15/24 54 BZY 93c75 50 BZV 15/18 30	Flat Red LED		40p 12p
TA 4127 £1 TIP 30) 35p	BZV 15/18 30 BZV 15/30 30 BZW 70c6v2 10	Clearweld glue pack		£7 30p
HD 3884 2A23 £3 TIP 30 TA 4184 £1 TIP 30)B 40p C 45p	BZX 79.3v 10		F.C	£Î 75p
TA 2125 £1 TIP 31 TA 4138 £1 TIP 33 TIP 33	25p	Bush thyristor RCA 76122 £ Transformer 24(v/2(v-500)Ma 75	1Kg reel of solder		£3.00 £8.00
TA 4196 £1 TIP 33 TA 4174 £1 TIP 34	A 50n	Chassis type Transformer 240v/12 Volts 500m/a 75	/5R/25 Watt 18R/11 Watt	25n 100	stic Boxes 4¾ × 4 × 1 × ¾ 50p) Fuses £2.00 1 W/W Res. £1.50
TA 4139 £1 TIP 34 TA 4198 £1 TIP 34 TA 4167 £1 TIP 35	B 60p C 70n	CVC 20 tube base £ Tube Base Rank & G11 £1.2	MW/LW 13"×3½"	. £3 BF	199 × 20 Turn 100k pots Rank #2
BA 546 £1 TIP 35	C 700	6v-9v-13v tape motor 75 Swiss made 250rpm/240V	SONY 1400KV Chroma Pane SONY 1400KV Tuner unit	. — Tho	orn 9 volt power supply regulated £3.00 470 20 for £2
BA 328 TA 4176 TA 4145 E1 TIP 36 TIP 41	5 50p C 70p	motor very small 75	SONY 1400KV Touch button 12 Volt Mains Trans 500M/A	unit £3.50 6 M	Slider Knobs 70p Mixed UHF Aerial Isolating Sockets, ne with long leads. Fit ITT, GEC.
TA 4191 £1 TIP 41 HA 11710 £1 TIP 42	D 70p VBRC 6109 30p	Infra red led LD57CA 15	18V or 12 Volt Mains Trans :	500M/A 75p	lips, Pye £1.00
TA 4188 TA 4197 TA 4183 £1 TIP 48 TIP 49 TA 4183 £1 TIP 57	40p 30p	Mono scan coil £. G 8 transductor £1.2	Issue 3 with all IC's	£10.00 TO	Mixed Packs 66 12 Power Trans RCA 16182 NPN
TA 4197 £1 TIP 10 TA 4183 £1 TIP 10	0 30p 12 30p	AT 4041/41 transductor £ VHF 3 Fransistor rotary tuner DX-TV £	BY204/4	25 for £1.00 Kits	
TA 4195 £1 TIP 11 TA 4175 £1 TIP 11 TA 4177 £1 TIP 12	5 50p 7 50p	15K-20 turn pots 201 Thorn panel 6×100 pot +	W005 bridge KT3 touch button black	20 6 62 -77	Mixed AC series Transistor £4.50 Panel mount rocker switch 250V/
TA 4192 £1 TIP 12 TA 4146 £1 TIP 13	5 35p 0 30p	changeover switch (Irish) 501 Battery converter TA 75 for	K30 full remote Dawer Ass w	6 for £1 25 [ith 3 10A	Panel Mount Bulbs & Neons £1.50
The Service Engineers Guide to Teletex £1.50 Teletex Colour TP 14	1 25p 6 30p	colour TV. 12/24v Thorn 3787 £0 Thorn 3500 2A cut out 500	K30 VHF. UHF Dawer Ass	£7.00 25 £6.00 201/	LED red/yellow/green £1.50 C Holders £1.20
Teletex Colour Training Manual £3 Mains Trans TIP 14 TIP 64 TIP 29	0 50p 0 50p 55 35n	Stereo GEC amp 20 watt + pre	BU126	20 9	Large LED Red £1.00 Small LED Red £1.00
C. Core 24(by 4v+4v T 6032 Jylly 2 AMP 12v T 6036	30p 40p	amp with 4 pots + mains power unit with circuit	BU105 2SC2122A	0 for £6.00	C20 Turn 100K Pots £1.00 Transistor £2.50 Convergence Pots 80n
lamp £2 T 6040 Mullard split diode AT2076/80 £6 T 6049	40p 40p 40n	SPECIAL OFFER Decca-TTT etc.	BD136	0 for £1.25	Convergence Pots 80p Thermistors 50p Slider Pots £1.00
4 Types Fedility front T 6052	40p 40p	FEO4/1/250AC/4 Mains filters	OA90 4	0 for £1.40 10 for £1.00 10 for £4.00	Presets 50p VDR + thermistors, degaussing, HT,
pats £2 T 9005 Amstrad TV chassis ZTX	07 40 p	(grey type) × 4 80p	KT3 multicaps 50 Ceramic Condensers	0 for £7.50 etc.	glass reed switch £1.00
Complete damaged print £5 + £5 post ZTX	08c 10p 09k 5p	BRIDGES SKB 2/08 L5A 30g	Mixed Mounting Kit for Powe Transistors	r 50p 40 1	press to make switch 70p Pots £1.50 ube Bases £1,00
BB 105A×12 £1 ZTX 3 BB 105B×12 £1 ZTX 3	08c 10p 09k 5p 113 5p 41 10p 42 10p	KBL 005 30p KBL 02 30p	300 Condensers 300 Resistors 150 Electrolytics	£1.50 £1.50 Ban	00 Diodes, Condensers, Resistors on dolier £2.00
BB 105G×12 £1 ZTX 3 BB 121a 100 ZTX 4	KN4 IIIn	KBP 04 30p W02 15p	15 Bulbs Antistatio Diseleth	£2.00 Luc	ky Dip 600 gram £1.00 gle Bag 5Kg £5.00
47 10p each ZTX 5 A 823A chassis MJ 225 Scan drive £5 MJE 30	.5 60m	W004 15p W005 20p AT 2076/35 £7	100 Diodes	£1.50 20m	ım Fuse Holders
IF £3 MJE 23 Scan control panel £3 SP 838	209 10p 5 50p	AT 2076/55 GEC split diode transformer £10	SENIDZ C.	IN4	ssis Mount 20 for £1 001/6 100 mixed £2.50 T Diodes, small 20 for £1
NEW A31/510 tubes SAB 33 sAB 43	205 £1.00 209 £1.00	AT 2048/11 LOPTI Mullard £2.50	SENUZ COM TO ORDER SEE BAG		
				20 1	Mixed Switches £1

SENDZ COMPONENTS TO ORDER SEE BACK PAGE

	SE	E BACK PAGE	4
Thorn Spares New 9000 Decoder	£8.50	XK 3123 THORN 50p	┨;
9000 Frame panel	83.	Hitachi 2A/1500V metal case wire end FARST/REC 20p	
9000 Cyclops panel 8000/8500 timebase panel	£1.50 £8	20.AX	٦,
8800 convergence panel	£6	GEC Degausing Panel 809 with PT37 £1.00	
8500 convergence ganel 4000 Power supply	£3	Line Transformers	Ⅎ∶
1600 Mains lead, switch	£1 50	Hitachi Split Diode and GEC 1981 to	
3500 6 push button + cable form T605 IvNPN T066 30v/6A	10p	1984 £13 2 J/Pots 3,500 1 off each type £3.00	
9000 Sound output panel 3500 Focus unit	£1.50	G8 Symmetry Coil £2.00	13
3500 Mains Trans	£4	G8 Trans. Philips £7.00 G11 Split Diode £12.00	
3500 cut outs 10: 3500 IF panel	for £4 £2	CVC820 Split Diode ITT £10.00 Thorn B/W AD5308F + Stik +	1
3500 Frame panei	£3 £3	Lead £1.50	'
3500 Line panel 3500 A1 Diode	20p	1690 Thorn EHT over-wind with diode lead & anode cap £2.50	1
Export 3500 IF par el IC board with set cf SN74LS	£2 £1	GEC 2040 £3.00	r
4000 Tube base	£4	GEC 2110 £7.00 Mullard AT 2036 £1.50	
3500 A1 pots Beam limiter pane	50p £1.50	Pye 169 Line Trans 23.00	1
3500 Fower panel with Y969	£1	Pye mono £3.00 Rank mono T704A £3.50	
3 Way regulated adaptor 240V 6 7.5/9V/300mA	£3.50	Split Diode Trans £7.00 GEC 20 AX Rank Z522 £3	
Rank/Toshiba prel unit	£9.50	Rank L.O.P.T. Z970 £3	
0354 2 banks of 3 PB urit. Pye 731	£2	CVC 5-8-9 £3.00 CVC20 ITT £3.50	
4 Push button unit preh 6 Push button VH / UHF for	£1.00		
v/cap. GEC-Decca type 7 Push button for CVC5 ITT	£7.00	CVC30 ITT	
7 Push button for CVC5 ITT KT3 12 Push butten unit	£8.00 £2.00	CVC800 Line Trans £6.00 CVC40 Slip/Diode £12.00	
KT3 (Export) 12 F.B.u	£2		
6 Push button Uni. Thorn 6 Push button Uni. fits GEC	£1.00	GEC Portable G1OT2041 £3.00 GEC Portable G1OT2046	
& Decca etc.	£6.00 £3	EHT Split Diode Leads ITT £1.00	1
Hearing aid unit 6 Push button unit PYE 713 7 Button Unit GET with Lamps	£7.00	GEC Portable G10T2041 £3.00 GEC Portable G10T2046 £3.00 EHT Split Diode Leads ITT £1.00 Ex panel "14" Fidelity portable £5 3500 L.O.P.T. & HT Trans each £2 LOPT Pank 7763	
7 Button Unit GET with Lamps	£7	EOTT Kank 2705	
Mains Droppers		Triplers	٦
G8 2R2+68R G8 47R 15 watt	£1.25 75p	ITT CVC 5-8-9 £3.50 Rank T25LE Tripler £2.00 Rank 11TCP A823 £3.50	
Pve 731 3+56+27R	50n	TU 25 30K Rank £3.00	
Pye 3R5/15R/45R Thorn 50/17/1K5	50p £1.00	8500 Triplers £6.50	
120/20/20/48/117 270/10/6 for Thorn 4000	£1.00 50p	G0 Philips £4.00	
18/320/70/39	£1.10	GEC 2110 £4.00 3500 Thorn £3.00	١
Thorn 50-40R-1K5	50p	9000 Thorn £5	1
Ae Socket & Lead GEC, ITT, Philips, Pye 7×3 ³ /4Thorn	25p	9500 Thorn £4.50 2040 GEC £3.50	1
7×3-74 Thorn Rank Toshiba Tube Bases	£1 30p	GEC TVM25 Tripler £2.00	1
		Universal Tripler £5.00 TVK 76/9 £3.00	
Speakers Pair 25 watt 4Ω speaker & twee	ter in	G8 £4.00	
cabinet	£15.00	CVC 825 ITT CVC 20/25/30/32 £3.50 Decca 80 100 £4.50	
6×4 G11 25 ohm	£12.00 £1.00	Grundig TVK 52 £2.50 11TBQ Pye 731 £3.00	
5½×2½ 3 ohm 5×3 80 ohm	£1.00 70p	11THY £4.00	1
5×3 50 ohm	50p	D22 for Pye 18" colour portable £4.00 LP 1193/63 £4.00	
5×3 35 ohm 6×4 15 ohm	70p £1.00	BG 100/41 £3.25	1
7×3 70 ohm	£1.00	KT3 BG200/43 £3.50 T/text ultrasonic rec'r panel £14.00	
8×5 8 ohm 15 watt 8×5 8 ohm	£2 £1	Video cassette lamps on lead.	
5×3 8 ohm 7×3 16 ohm	70p £1.00	20 for £5.00 200 for £25.00	1
5" dia 16 ohm	£1.00	GEC 8 touch unit assy complete with all I.C.'s + pots £4.00	1
5" dia 8 ohm 6½" dia 4 ohm	£1.50 £1.50	G11 E.W. Transformer 50p	1
6½" dia 4 ohm 6½" dia 3 ohm 2¾" dia 8 ohm	£1.50	G11 F.W. coils £1.00 G11 Transient Suppressors 245V 10	
I 3″dia 8 ohm	75p 75p	for £1.00 G11 Scan Coils £5.00	1
4½" sq. 15 ohm KT3 speaker K30 3" dia 15 ohm	75p 75p	G11 100K tuner pots 12 for £1	
	60p	KT3 IF panel £6.00 KT3 line OSC transformer £1	
1690 5×3 12 ohm K45 Philip 15 ohm	£1 75p	KT3/K30 infra-red receiver	
K30 15 watt	£1	head £1 K30 drawer unit with IC's	
KT3-K30		(home) £10 K30 drawer unit with IC's	
OF-550 E.W. OF-513 correction	10p 10p	(export) £10	
OF-557	50p		
Diodes		KT3 line driver transformer 50p	r
BY 127	10p	by switch £1	-
BY 133 BY 134 BY 164	10p 10p	NPN PNP 80V 6 Amp TO66 O.P.	
BY 164 BY 176	50p 25p	Trans pair 25n	1
BY 179	4400	Lunday with ic SAS S60T/S70T 67 00	
BY 184 BY 187	25p 10p	Control panel 5 sliders + mains lead £1.50	. }
BY 187 BY 190 BY 196	40р 30р	C11 9 touch button unit replaces old 6	
BY 198	10p	Tube base + base unit for 820 Euro	ı
BY 204/4 BY 206	8p 8p	chassis £4.00	
BY 208/800	8p	Portable £3.00	١.
BY 208/800 BY 210/400 BY 210/800	5p 10p	CVC 20/25/30/35/40 decoder panel	-
BY 223 BY 224/600: 4.8A/600v bridge	60p 50p	(untested) £5	١.
BY 226	15p	40k Transducer 50n	.
BY 227 BY 229/400 BY 237 BY 254	15p 30p	PHILIPS NESIIN £1.20	
BY 237 BY 254	5p 10p	20 GEC Black Spark Gaps £1.00	١.
BY 255	300	KT3 Front Panel Control	
BY 298 BY 299	10p	Assy. £2.50	
D 1 400	8p	WOLDSON DECODED	\exists
BY 527 BY 407a	20p 10p	LC. SAA 5051 K30	
BY 602	10c	I.C. SAA 5042	
F 247 XK 3102	10p 50p	I.C. SAA 5020 etc. £8.00	╝
International Rectifier EHT Di	iodes G	770/HV34 6KV 3 for 8p	
6A/600V Stud Diodes 6A/1000V Stud Diodes	20p 20p	05 t 472 DMD C/D	
	201	-	_

T	5 Volt Mains Transformer 2 Amp		.50p ≨2.50	Mains Isolation Transformer (R.S. 5 Type) in case	00V/A £25.00
1	30V Power Supply 500M/A 4×2 ¹ / ₄ Pye 731 Power Panel 6 Diode Universal Triplers		£13 £3.25	Rank Secam Decoder Panel UHF & T115A	
l	6 Diode Universal Triplers NEW PYE 725 line O/P panel with L.O.P.T Thorn Mains Isolator unit for 70-80W. Ex-sp	. & Tripler	£10.00	NEW	
4	NEW GEC 20AX Power Supply Switch Mc Complete new GEC portable chassis M120	xde	£12.00	GRUNDIG SPARE PANEL Set No. SC4127; SC4337; SC6217; S	C6237
┪	u can/I OPTI		£10 £1.50	GRUNDIG MODULE TYPE Tuner IF, AF TRX LOP, TP pream Tuning board, Colour RGB, LED E	plafier
\dashv	Field + Jungle panel for GEC 3133/3135 GEC 2110 line panel with transformer GEC 2110 tuner unit + IF Panel Pye/Chelsea Line op panel		£7.00 £12.00	Deflection Board From £3 to £8	Soard
	Pye 713 if panel and tunel		£32.00 £7.00 £30.00	Multi-Caps	
٦	Pye/Chelsea Timebase panel with LOPTI		£10,00 £5,00	350V 300M + 300M 400V 400M 350V 400M	£1.00 60p
	Pye 731 Frame Panel Pye 731 Convergence Panel Pye 731 Chroma		£5.00 £10.00	Thorn 3500 175/100/100/350v	60p £1.00
	Pye 731 IF panel + tuner Pye 607/205 Line panel with transformer		£10.00 £10.00	KT3/200/25/25/385v 300+300+150+100+50MFD	£1.00
	Pye CDA/205 panel GEC portable chassis + LOPTI 2114 New		£6.00 £4.00	350V 47/220/350v	£2 60p
	Thorn 1613/1713 chassis G9 Line Panel		9.75 £12.00	150/150/100/100/100/320v 2500/2500/63v	£2.00 50p
	G9 Power Panel		₹7.00	150/200/200/300v 400/400/200v	70p £1.70 £1.50
	NEW MULLARD TELETEX Decoder Panel (VM6230) £15.00	250/64 3300/70	10p 50p	300/100/100/16/275v 100/200/325v 150/150/100/375v	40p £1.50
1	Panel 6101 £15.00 Panel 6330 £15.00	1.1/100 1.100 × 10	5p 30p	300/300/100/32/32/300v 1500/2000/30v	2.00 50p
l	G8 Tuner Unit + Panel £6.00 G8 Convergence Panel	22/100 4.7M/100	10p 5p	Jelly pot Thorn 00D4/013 150/150/100/100/320v	£3 £2.00
1	(late type) £12.00 G8 Power Supply £6.00	470/100 2000/100 4700/100	20p 70p 75p	100/350 + 300/200/100/16/275v 225+25/380 GEC	£2.00 70p
	G8 6 Sloping PBU £8.00	47/160 47/160 300 300/300V	10p 80p	200/100/100/350v 500/500/25v	£1.50 50p
	G8 Chroma £6.00	800/160 .1/250 Pulse	50p 5p	150/150/100/300v 200/150/150/300v	75p 1.00
	G11 IF Detector £3.00 G11 Selector gain module £3 Complete CVC 825 Chassis (both	2,2 250v 3n3/250 A.C.	10p 10p	ITT Panels CVC 40/2 Chassis, new £30, comple	te with
	panels) £40.00 AEC V/Cap Resistor Unit UHF with IC	.33/250V .39/250V	20p 15p 25p	intrfase panel CVC 820 Line O/P Panel	
	SAS660 SAS670 £3.00 Z714 RANK IF Panels 6MHz 1 l.C.	4n7/250 tested 5KV .91/250 .91/400	25p 35p 30p	CVC20 Mains Panel FTT 8 & 6 Push Button Unit CVC40/2 New Chroma Panel	£3.00 £1.00 £10.00
	SL437F £3.00 Z909B RANK IF Panels	72/250 47/250	15p 10p	CMA 10 CMA 1)	£2.00 £2.00
1	Export 5.5MHz 2 I.C.'s TBA1205B TCA2705Q £2.50	100/250 G11 470/250V	20p £1.75	CMA 30 CMA 40	£2.00 £1.50
	Z743 RANK IF Panel Export 5.5MHz 3 I.C.'s	GEC600/250 700/250	60p £1	CMC 10/2 CMC 16	£5.00 £4.00
	TBA750+SC9504P+ SC9503P £1.50	300+300 MFD 350v 800/250 32/300	£1.00 40p 20p	CMC 38 CMC 45 CMC 47	£8.00 £1.50 £1.00
	Pye G11 Front panel with transducer, pots, tuner pots, 6 pb switch+lead £5.00	4/350 8/350	20ք 5ք 8ք	CMC 52 CMC 57	£15 £6.00
	Pye 6 button switch portable £1.00 GEC V/cap VHF/UHF tuner and IF+	4.7M/350v 33/350	10p 20p	CMC 58	£8.00 £8.00
	sound O/P PC 706B3 (Export) £12.00 GEC Line O/P PC 659B3 £6.00	220/350 300/350	30p 40p	CMC 59 CMC 67 CMC 67/2	£3.75 £4.00
	2110 GEC Power Panel £8.00 GEC Power Supply (Export) £10.00	400/350 10/375	50p 10p	CMC 68 CMD 12	£4.00 £10
	G11 dynamic correction panel £6 CVC 20 Front panel with sliders +	22/375 220/385	15p 75p	CMD 32 CMD 33	£5.00 £5.00 £5.00
	mains input panel £4 CVC 40 PUSH BUTTON ASSY with	330/385 CVC 820HT 9.1/400 KT3 E/W .39/400	60p 15p 20p	CMD 40 CMD 41 CMD 800	£5.00 £10.00
	sliders: complete with lamp assy + pots £14	56K/400v 4700pf/400	20p 10p	CMF 25 CMF 26	£2.00 £2.00
	CVC9 slider pots panel 50p CVC 5 Mains on/off + 5 pots £2	.22/400 8/400	10p 15p	CMF 40 CMH 10	£2.00 £1.50
	Universal Focus. Fits Pye, Thorn and Decca Units.	33/400 400/400	20p 40p	CMH 31 CMK 12 (untested)	£1.00 £4.00
	Large Type 75p Decca Small 75p	394K/400V 220/450 .47/500	20p 40p 25p	CMK 30 (untested) CMN 20 CMN 21	£4.00 £1.50 £1.50
	KT3 Focus Unit 75p K30 Focus Pot 75p	9.1/600 .047/600	15p 15p	CMN 40 CMN 45	£1.00 25p
	TX10 Focus Units £6.00 CVC 32 Focus Unit 75p	0.047/1000 0.01/1000	10p 10p	CMP 10 CMP 11	£2.00 £4.00
	Fedility Focus Unit 14R-14S 30p 3500 Thorn Focus Unit £1.00	0.1/1000 .47/1000v	10p 65p	CMP 40 CMS II	£2.00 £2.00
	ITT Small for use with Split Diode 50p	.47/250V A C. .001K/1250	10p 10p	CMS 40 CMU 12	£2.00 £10.00
	TV11 50p Remo TV12SP 50p	0.0047/1500: .005/1500 .0105/1500	10p 10p 10p		£8.00 £7.00 £7.00
	TV13 50p TV14 50p	1n8/1500 2n0/1500	15p 15p 10p	CMU 43 CMZ 30 GMA 90	£5.00 £5.00
	TV18 60p TV20 £1.00	2n2/1500 .01/1600	15p 15p	GMC 120 GMR 64	£2.50 £5.00
,	TV45 50p Thorn 14/1500 rec stick 5p	G11.8200/2KV 0.1/2KV	15p 20p	TMN 2 VCA 20	£2.00 £10
	G7000 Philips Video Games Packs 11 types £8.00 each	1 10n/2KV 3n9/2KV	15p 15p	VCA 21 VMC 26 VMC 34	£10.00 £3.00 £5.00
	G11 drawer ASS 3 pots Mains switch and lead £2.00	0.0015/2KV 5n2/2KV 6n2/2KV	10p 10p 15p	VMC 44 + 45	£5.00 £4.00 £5.00
	Line O/P panel GEC 2217/2218/2213/ 2214/2226/2227/2228 £10	2n0/2KV 2n2/2KV	15p 15p	Hand Sets	
,	CLOCK DISPLAY	7500pf/2KV 4n7/2KV	10p 15p	G11 Ultrasonic Teletex Handser 8 C.H. Ultrasonic GEC Full Remo C2219H	£24.00 re C2014H1/ £15.00
•	4 SEG ACDM45 £1.00 4000 thick film £2.00	8n2/2KV 0.0082/2500	15p 15p	Many Deadlesses of for CIL Library	
)	DISPLAYS 4()4() Clock £1.00	150/3500 1800/4KV 4.7nf/5KV	10p 5p 10p	Thorn 4000 insert with 7 buttons	£5.00 £14.00
	7seg Red LED	170/8KV 180/8KV	10p 10p	G11 Infra-red full teletext	£14.00 £24.00
ī	2 digit LED ÷1.8 with panel + MCI4511 £1.00	210/8KV 1000/10KV	10p 10p	Dynatron-Full remote CTV 62, 63	£10.00 . 64 £19.00 £18
ó	4700/63 £1.50	.47/100V	80p	Hitachi infra red handset Philips full remote KT3, 16C928/20 7228/7324; K12 26C 797/1ST 66K 1	C934;
;	CVC 20-25-30 Mains Switches Infra Red and Ultrasonic G11 Teletext De	eooder Panel	75p £30	G11. Full remote top button assy. G11. Full remote repair service (e:	£12.00 schange
)	RANK & ITT Mains Remote On-Off Swit RANK & ITT Mains Remote Switch 2865	(720R)	£1.50 £1.50	unit) Philips infra red full remote 9 char	£12.00 mel for 60
)	RANK & ITT Remote Switch 2800 ohm G11 Mains Switch		£1.50	CP2605 Philips infra red full remote 12 cha	£6.00 annel for 60
,	4 amp Mains Switch GEC Mains Switch 4 amp		25p 30p	Philips Key Pad set K13/K30	£12.00 £3.00 £15.00
,	THORN Rotary Mains Switch		£1.00 50p 75p	KT3/K30 Full remote	£15.00 £15.00 £4.00
	G8 Mains Switch Thyristor 600/4 amp C106/2 G11 Preh Red LED P/Button for C.H. Cl	hange	24p 20p	Hitachi 8 button unit with resistor year mod.	
)	RANK TOSHIBA Transductors TPC-201 Mains Switch ITT Long Type Print	.1	50p 75p	GEC infra-red 2236-2026 GEC push pad hand set huttor bk	£4.00 hs 10p each
-	Mains Switch Philip Long Type TAG Mains Switch GEC Long Type TAG		75p 75p	RC4001-RC5150-RC5176-RC5171	assis. No RC5177.
5	Thorn 12 or 24 volt battery convertor for Tape Heads R/Play/Back Mono/Stereo	Extranie colour 1/V	£6.00 £1.00		£13.00 CR £12.00
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Tuner Units V/Cap Rank UHF Z77617/Unit \$6 V/Cap Rank VHF Z77317/Unit \$5 NEW G8 Tuner V/Cap \$5.50 ELC 2000 on Panel \$2.50 GEC 6 Push Button Unit \$6 ETT 6 Push Button Unit \$6	SENDZ C 63 Bishops Shoeburyness, E	steignton, ESSEX SS3 8AF	SAB4209 £2.0 TBO0124 £1.0 SAA5000A £1.3 SAA5012A £5.0 SAA5020 £3.3 SAA5030 £5.0	0 SN76110N 0 SN76115AN 0 SN76131 0 SN76141N 0 SN76226	£1.50 £1 50p 50p £1.00 £1.00	MJE661 MJE3055 MJE2801 MJE2955 MJE13005 Sanikron Diode	25p £1.00 30p 50p 30p 30p
DECYA 6 Push Button Unit 66	All items subject No Accounts : N Postal Order/Che Add 15% VAT, th Add Postage	t to availability. lo Credit Cards eque with order nen £1 Postage for overseas	SAA5040A £4.6 SAA5050 £3.5 SAF1032p £2.6 SAF1039 £2.6 SAS560 £2.6 SA5660 £1.6	0 SN76228N 0 SN76270 0 SN76532N 0 SN76544N 0 SN76546 0 SN76550	£1.00 £1.00 50p £2.00 £1.00 30p	Philips Cartri GP422 (4CH) GP412 GP412/11 GP406	£6.00 £6.00 £6.00 £6.00
FIT 6 Push Button Unit	SAME DAY All items subject No Accounts : No Accounts	SERVICE to availability. to Credit Cards eque with order nen £1 Postage for overseas £212 London Rd., 0702-332992 orders accepted on official billing charge. BIT1822 BIT1823 BIT1824 BIT1824 BIT18124 BIT18124 BIT18124 BIT18124 BIT18224 BIT18224 BIT18224 BIT18018 BIT8100 CA270AE CA270CE CA920AE CA270CE CA920AE CA3100 CA3110 CA3110 CA3110 CA3118 CA3118 CA3118 CA3118 CA3118 CA3118 CA3118 CA3118 CA3118 CA3119 CA3118 CA3119 CA3118 CA3119 CA3118 CA3119 CA3118	SAA5030 £5.5 SAA5040 £3.4 SAA5040 £3.4 SAA5040 £3.4 SAA5040 £3.4 SAA5050 £3.5 SAF1033p £2.5 SAF1032p £2.5 SAF1032p £2.5 SAF1032p £2.5 SAF1033p £2.6 SAS560 £2.6 SAS560 £1.6 SAS570 £1.6 SAS570 £1.6 SAS580 £1.5 SAS580 £1.6 SA	\$N76226 \$N76227N \$N76228N \$N76228N \$N76228N \$N76228N \$N76228N \$N76228N \$N76228N \$N76221N \$N76221N \$N76221N \$N76221N \$N76221N \$N76221N \$N76221N \$N76221N \$N76221N \$N76521N \$N76532N \$N76532N \$N76532N \$N76532N \$N76520 \$N76620 \$N76620 \$N76620A \$N76720 \$N76620A \$N76620A \$N76620A \$N76620A \$N76620A \$N76620A \$N76620A \$N76720 \$N76	1.00	Philips Cartri GP422 (4CH) GP412 GP412/11 GP406 Transistor: A1222 A1223 AC106 AC121 AC124 AC124 AC128 AC137 AC151 AC131 AC131 AC138 AC152 AC153K AC142K AC142K AC176 AC176K AC178K AC188 AC189 AC191 AD143 AD149	30p
2SB407 Sanyo BC308 BC308 BC309 BC319 BC327 BC328 BC337 BC328 BC337 BC328 BC337 BC328 BC338 BC328 BC338 BC338 BC388 BC388	10p BF871 30p 10p BFR39 15p 10p BFR52 7p	Thyristors BT151/890R 8 1D318901 51 8T106 Plastic 51 8T106 Plastic 51 8T119 51 8T119 51 8T220 51 8RC4443 7 G11 Thyristor 6 6 Cecca 80:100 6	CVC 9 power supply board £1 CVC 20/2 mains panel £2 Oppose CVC 20 to 45 chassis: Oppose Pots 10 k with Switch:	8 867238	£1.00 £3.00 n Case 20p	BF448 BF450 BF458 BF459 BF468 BF469 BF470 BF480 BF594 BF597	10p 30p 15p 15p 30p 30p 30p 30p 20p 50p 10p
100 BC3495 SC1030	10p BFR.79 15p 10p BFR.81 15p 10p BFR.81 15p 10p BFR.87 10p 10p BF.84 10p 10p BF.84 10p 10p BRC.366 20p 30p BRC.3064 50p 30p 30p 30p 30p	2N4444	pots 4 / k with Switch : pots 4 / k with Switch : Mullard Surface Wave Filter RW 153P Colour TV Filter Mullard Surface Wave Filter RW 154 Colour TV Filter GI1 Line Scan	DIL - DIL	I.C. Hold	Post DIL – QIL 16 Pin × 10 18 Pin × 10 28 Pin × 4 8 Pin × 10	£1.00 £1.00 £1.00 50p ach 10p