

PRACTICAL

APRIL 1983





Part One

Plus...

PROJECTS:

PHASER - CAR WIPER



CONTROLLER - MICROBUS

NENS & FEATURES -

SPACEWATCH - BAZAAR -

MICROFILE - SEMICONDUCTOR

UPDATE : INDUSTRY NOTEBOOK

Get moving with these new developments in UK Robotics

- advanced electrohydraulic designs for education, industry and now available to the home constructor.

Hebot II is a jurile-type robot which takes programming out of the two dimensional world of the VDU into the real three dimensional world Given a DC supply of 9 15V it can perform a bewildering number of moves under computer control — lockwards backwards left and right — with each wheel independently controlled It has blinking eyes, bleeps with a choice of two lones and has a solenoid operated pen to chart its progress. Touch sensors coupled to its shell return data about its environment to the computer for if to calcula evasive or exploratory action. Hebot II connects directly to an I. O port or alternatively with the universal interface board to the expansion bus of a ZX81 or other computer.

Robotic experience is becoming as essential a subject as computing MICROGRASP provides the lowest cost means of acquiring that experience but despite its ultra low price the robot has considerable versatility. There are 5 axes each using a servo motor and there is feedback from each of the arm movements. Control is by any computer with an expansion bus - the ZX81 being particularly suitable. Servoing is achieved with hardware on the interface board to keep programming simple and the robot is operated under BASIC commands with no computer specific software required. The interface board is memory mapped using only 64 bytes at any of 1024 switch selectable locations
MICROGRASP robot foll with power supply

Universal computer interface board kill 7x81 peripheral RAM Pack splitter board

£85 00

HEBOT KIT LOS.SS INTERFACE BOARD KIT £10.00

€48.50 €2.50



printing, call to machine code routines, hexadecimal support and userfriendly textual error trapping messages.

CON 10-7

If computers interest you then the Cortex will expand your understanding infinitely more than off the shelf machines. Use it in business, education, research or just play with the incredible graphics capability. At Powertran we are using these machines in conventional roles, in product control and R & D. We shall coordinate the Cortex user group and distribute software for the TMS 9995 CPU. Complete 16 bit 64K computer kit £295.00 + VAT Complete 16 bit 64K computer ready built £395.00 + VAT



colours on 36 prioritised planes of user definable characters. Software FORTH coming includes this trendy language along with NOS C/PM.

Hardware components available separately with details in Nov. Dec. and Jan issues of ETI. Software features include: Real time clock, full renumber command, buffered I/O to free machine whilst

Top of the range is the Genesis P102 which has dual speed control, continuous servo operation and double acting cylinders for increased torque on the wrist and arm rotation joints. The microprocessor based control system has additional memory, position interrogation via the RS232C inter face increasing the versatility of computer control and inputs are provided for machine tool interfacing.

6 axis system READY BUILT €1950.00 Powertran CORTEX 16 bit 64K computer Kit £295.00 READY BUILT



Genesis \$101 Base: 19.5" x 11" x 7.5" Lifting capacity: 1500gm Weight: 29Kg

4 axis model in kit form 5 axis model in kit form £425 £475

Genesis P101 Base: 19.5" > 1.1" × 7.5" Lifting capacity: 2000gm Arm lengths between axles: 14.0" Weight: 34Kg

6 axis model in kit form £675

Complete Systems as shown in Photograph on right

Genesis S101 4 axis system in kit form £681.50 5 axis system in kit form £737.50 5 axis system Ready Built £1450

All prices exclusive of VAT

With prices starting below £1,000 the Genesis range of general purpose robots With prices starting below £1 000 the Genesis range of general purpose robots provide a first rate introduction to robotics for both education and industry Each has a self-contained hydraulic power source which enables loads of several pounds to be smoothly handled. The system operated from a single phase 240 or 120V AC supply or a 12V DC supply. The machine can be supplied with up to 6 axes each of which is fully independent but capable of simultaneous operation. Position control is achieved by means of a closed-loop feedback system based around a dedicated microprocessor. Movement sequences can be exhaust stored and replaced the sequences can be entered stored and replayed by use of a hand held controller alternatively the systems can also be interfaced to an external computer via a standard RS 232C



GENESIS S101 AND GENESIS P101 WITH PROCESSOR BOXES AND HAND-HELD CONTROLLERS

WORLD **LEADERS** IN **ELECTRONIC** KIT DESIGN AND SUPPLY

(CYBERNETIC DIVISION) PORTWAY INDUSTRIAL ESTATE ANDOVER HANTS SP10 3WN Phone Enquiries (0264) 64455

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OUR MAY ISSUE WILL BE ON SALE FRIDAY, APRIL 8th, 1983

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| 2N918 | 35 | 2SA671 | 2N930 | 20 | 2SA715 | 2SA715 | 2N13014/5 | 24 | 2SC495/6 | 2N13014/5 | 24 | 2SC495/6 | 2N13014/6 | 25 | 2SC1096 | 2N13014/6 | 295 | 2SC1172 | 2N13014 | 25 | 2SC1172 | 2N12194/20A | 2SC1172 | 2SC1172 | 2SC1172 | 2SC1172 | 2N12194/20A | 2SC1172 | 2SC BFX85/86 BFX85/86 BFX86/88 BFX86/88 BFX86/88 BFX96/BFX96 BFY86 BFY86 BFY86 BFY86 BFY86 BFY87 BFX97 BFX 250 60 70 250 85 30 125 125 100 150 85 190 140 85 200 90 140 85 200 85 TIP31C TIP32A TIP33C TIP33A TIP33C TIP34A TIP35C TIP35A TIP35C TIP36C TIP41A TIP41B TIP42A TIP42B TIP42B TIP120 TIP121 TRANSISTORS. BC307B BC3008B BC327/8 BC337/8 BC441 BC461 BC461 BC516/7 BC516/7 BC556/7 BC558/9 BCY70/2 BD131/2 BD131/2 BD133/8 BD133/7 Tel. Watford (0923) 40588. Telex: 8956095 WAELEC ALL DEVICES BRAND NEW, FULL SPEC, AND FULLY GUARANTEED. ORDERS DESPATCHED BY RETURN OF POST, TERMS OF BUSINESS: CASH/CHEQUE/P.O.s OR BANKERS DRAFT WITH ORDER GOVERNMENT AND EDUCATIONAL INSTITUTIONS OFFICIAL ORDERS ACCEPTED (ACCESS ORDERS BY TEL. PHONE: 0923-50234). TRADE AND EXPORTINGUIRY WELCOME. P & P ADD 50p TO ALL CASH ORDERS. OVERSEAS POSTAGE AT COST. PEDET ORDERS TO VAT. U.K. Gustomers please add 18% VAT to total cost incl., p&p, We stock VAT (housands more items. It pays to visit us. We are situated behind Watford Football Ground. VAT Open Monday to Saturday, 9.00 am to 6.00 pm. Ample FREE Car parking. POLYESTER CAPACITORS: (Axial Lead) 400Y: InF, InS; 202, 303, 407, 688 11p; 100, 150, 180, 220 12p; 33n, 47n, 680, 16p; 100, 150, 20p; 220 a) 30p; 330 42p; 470 n52p; 680h 60p; 1µx 68p; 2µx 4y 85p. 1000Y: Inf 17p; 10nf 30p; 15n 40p; 120 a) 48p; 31n 42p; 47n 10n 50p. POLYESTER RADIAL LEAD CAPACITORS: 250Y; 10n, 20n, 15n, 22n, 27n 6p; 33n, 47n, 68n, 100 n7p; 150n, 220n 10p; 330n, 470n 13p; 680 19p; 1µx 23p; 1µx 64p; 2µx 48p; 47 8p; 63Y: 0.47, 1.0, 1.5, 2.2, 3.3, 8p; 4.7 9p; 101 10p; 15, 2, 12 12p; 31 35p; 47 18p; 63 16p; (10) 19p; 220 36p; 100 70p; 220 09p; 25V; 50p; 3300 76p; 4700 78p; 101 10p; 15, 221 2a, 3b; 33n, 12p; 330, 470, 32p; 1000 48p; 2200 90p; 25V; 50p; 3300 76p; 4700 78p; 101 10p; 15, 221 2a, 3b; 33n, 12p; 330, 470, 32p; 1000 48p; 2200 90p; 25V; 50p; 3300 76p; 4700 78p; 101 10p; 15, 22 12p; 120 33p; 33n, 470, 32p; 1000 48p; 220 90p; 25V; 50p; 3300 76p; 4700 78p; 101 10p; 150 10 TIP121 TIP141 TIP142 TIP147 TIP295S TIP3055 TIS43 TIS44 TIS88A TIS90 TIS91/93 BD138/9 BD 144 BD 245 BD 245 BD 278 BD 278 BD 278 BD 278 BD 245 BF 167 BF 178 BF 178 BF 178 BF 198 BF 244 BF 256 BF 198 BF 256 BF 198 BF 257 BF 187 BC117/8 BC140/42 BC147/8 92p; 16V: 2·3. — 36p; 4700 79p. VK.1010 VN.1016M VN.46AF VN.66AF VN.86AF VN.86AF VN.89AF ZTX.107/8 ZTX.107/8 ZTX.122 ZTX.303 ZTX.310 Z POTENTIOMETERS: Carbon Track. 0.25W Log & Linear Values. 500w, I.K. & 2K (LIN ONLY) Single 3 5Kw-2Hw single gang D/P switch 3 5Kw-2Hw usingle gang tereo. TAG-END TYPE: 64V: 4700 245p; 3300 198p; 2200 139p; 50V: 3300 154p; 2200 110p; 40V: 4700 160p; 25V: 4700 98p; 10.000 320p; 15.000 345p. BC149 BC149/4 BC157/8 BC157/8 BC157/8 BC167A BC166 BC177/2 BC177/8 BC177/8 BC177/8 BC177/8 BC182/3 BC182/3 BC182/3 BC182/3 BC182/3 BC182/3 BC182/3 BC212/3 BC212/3 BC212/4 BC214 SKW-2FW dual gang stereo SLIDER POTENTIOMETERS 0 25W log and linear values 60mm track SKW-500KW Single gang 10KW-500KW Dual gang 30p; 33, 4, 100 55p. SILVER MICA (pf) 2, 3-3, 4-7, 6-8, 8-2, 10, 16, 18, 22, 27, 39, 47, 50, 56, 68, 75, 82, 85, 100, 120, 150, 180 15p each 220, 250, 270, 330, 360, 390, SIEMENS mulitlayer miniature 2. 3-3, 47, 6-8, 82, 10, 16, 18, 22, 27, 39, 47, 50, 56, 68, 75, 25, 50, 120, 150, 180 15p each 220, 250, 270, 330, 360, 390, 470, 600, 800 & 820pF 21p each 1000, 1200, 1800 30p each 1000, 1200, 1800 4700 60p each 2100, 4700 6 PRESET POTENTIOMETERS 0 1W 50w-2-2M Mini Vert. & Honz. 0 25W 100w-3-3Mw Honz. larger 0 25W 250w-4 7Mw Vert. 7p 10p 10p 0 25W 250w-4 7Mw Vert. RESISTORS Hi-stab, Miniature, 5%, C. RANGE Val. 0 25W 2w2-4 M7 E12 1 W 2w2-1 M E12 2 W Metal Film 10w-1 M 1% Metal Film 51w-1 M 1-99 2p 2p 6p 6p 8p 100+ 1p 4p 4p 6p CERAMIC Capacitors: 50V Range 1pF to 6800pF 4p; 10nF, 15n. 10pF to 1nF 8p 1n5 to 12nF 10p RESISTORS S.I.L. Package: 7. Commoned. 1001, 6801). IK, 2K2, 4K7, 10K, 47K, 10K 24p. 8. Commoned(f) pmis) 1501, 1801, 2701, 33012. IK, 2K2, 4K7, 10K, 22K, 47K, 10K 26p. BC237/8 5AB3210 SAB3210 SAB3271 SAB4209 SG3402 SL490 SG3402 SL490 SNF6033N SNF6033N SNF6033N SNF6033N SNF6033N SNF6033N SNF6237N SNF6477 SNF6488 SNF6460 SF8659 TA7120 TA7120 TA7204 TA7205 TA7222 TAA661A TA7400 TAA900 ZN423E ZN424E ZN425E-8 ZN426E-8 ZN427E-8 ZN427E-8 ZN429E-8 ZN459 ZN1034E ZN1040E ZNA234E Z80CTC Z80ACTC Z80B Z80DART Z80ADART Z80ADMA Z80DMA Z80P10 Z80AP10 Z80AS10 | 44400 | 44400 | 44400 | 44400 | 44400 | 44400 | 44400 | 44400 | 44400 | 44400 | 44400 | 44400 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 44000 | 4400 250 TTL 74 260 TTL 74 260 TAUD 11 550 TAUD 12 675 TAUD 12 675 TAUD 12 675 TAUD 13 260 TAUD 14 277 TAUD 15 677 TAU | S191 | S192 | S192 | S194 | S194 | S195 | S196 | 36 4014 31 4017 31 4016 317 4016 317 4016 317 4016 318 4018 455 4020 455 4020 555 4020 555 4020 555 4021 556 4021 557 4021 557 4021 558 4021 559 40 999 350 350 350 675 28 60 35 75 185 35 35 130 LINEAR IC's 8214 8214 8226 8226 8226 8226 8226 8226 8226 8226 8227 8235 8235 8235 8253 8253 8253 8253 8253 8253 8253 8253 8253 8253 8253 8253 8253 8253 8253 8253 8253 8254 8253 8254 8254 8254 8254 8254 8254 8254 8254 8254 8257 8264 8277 8279 8270 325 485 595 295 350 350 350 350 420 480 120 279 195 195 195 197 275 395 159 70 275 330 130 130 345 300 590 410 210 570 200 665 850 74147 74142 74143 74143 74143 74143 74143 74143 74143 74153 555 CMOS 700 COMPUTER IC's 74S Seri 1702 1802CP 2112-2 2114L-300n 2147-3 2532-3 2532-3 2564 2708 2716-5V 2732 2764 3242 4027 350 650 250 90 95 425 300 68 225 225 350 575 590 190 85 80 325 425 BXI TBA651 TBA8005 TBA8105 TBA8105 TBA8105 TBA8106 TBA8200 TBA9200 TBA9300 TBA9301 TBA9201 TBA9301 TBA9201 TBA9301 TDA1031 TDA103 FUI/71 | FUI ICL7611 ICL7660 ICL8038CC ICL8211 ICM7204 ICM7205 ICM7207 290 540 000 400 365 325 620 1150 400 800 620 950 000 7.493 000 7.494 400 7.495 335 7.495 620 7.4100 150 7.4104 800 7.4105 800 7.4105 7.4110 7.4111 7.4112 95 7.4118 90 7.4119 1125 7.4121 97 7.4121 860 7.4125 861 7.4125 861 7.4125 861 7.4126 861 7.4126 865 7.4136 865 7.4136 865 7.4136 865 7.4136 865 7.4136 865 7.4136 865 7.4136 865 7.4136 865 7.4136 865 7.4136 865 7.4136 865 7.4136 865 7.4136 865 7.4136 865 7.4136 95 99 99 99 105 105 790 790 480 280 770 770 850 420 250 350 £18 80 80 85 225 125 350 225 225 225 225 225 8080A 8085A 8088 81LS95 81LS96 81LS97 81LS98 8118-10 8123 8155 8156 8202 8205 8212 8214 CMC LS165 LS166 LS170 LS173 LS174 LS175 LS181 LS183 LS190 74C 74C244 C245 C373 C374 C922 C923 C923 195 195 240 245 420 500 400

SPEAKERS	OPTO ELECTRONICS 05	IQUID	VOLTAGE RE	GULATOR		DIL	TS	311	ULT	IMUM	
8Ω, 0 3W, 2"; 2-25", 2-5", 3" 80p 0 3W, 2-5" 40Ω; 64Ω or	TIL209 Red 3mm 10 DISP TIL211 Green 3mm 14 33 dis	STAL LAYS it 495	1A T0220 Plasti +ve 5V 7805	c Casing — ve 40p 7905	45p	SOCKE	Low Wire profile wrap		FORD'S most SION SYSTEM.		
80(1) 80p DIODES BRIDGE	TIL212 Yellow 14 4 digr TIL220 - 2" Red 12 6 digr 0-2" Yel, Grn, Amber 14	530	12V 7812 15V 7815	40 p 7912 40 p 7915	45p 45p	8 pin 14 pin 16 pin	8p 25p 10p 35p 10p 42p	ATO	M, DRAGON, JE, SPECTRUM	PET, RESEA	RCH MA-
AA119 15 RECTIFIERS AA129 20 (plastic case)	Rectangular LEDs with BPX2 two part clip. R. G. 8. Y. 29. BPW	21 295	1 24V 7824	40p 7918 40p tic Casing >	45p	18 pin 20 pin	16p 52p 20p 60p	EO C	GENIE, ZX81, e	cc. As publis	
BA100 15 IA/50V 18 BA100 15 IA/100V 20	Rectangl. Stackable BPX6 LEDS 8 1L74	45	5V 78L05 6V 78L62	30p 79L05 30p	60p	22 pin 24 pin 28 pin	22p 65p 25p 70p	Startin	ng from Nov., I'		
BAX13 20 IA/400V 25 BY100 24 IA/600V 34 BY126 12 2A/50V 30	Triangular LEDs R&G 18 ILD74 0.2" Flashing LED Red 56 ILQ74 0.2" Bi colour LEDs TIL 11	185	12V 78L12	30p 79L12 30p 79L15	60p 60p	40 pin	30p 99p			for details.	
BY127 12 2A/200V 40 CRO33 250 2A/400V 46	Red/Green 65 OCP: Green/Yellow 80 ORP1	2 78	LM300H I	70 LM305H 60 LM309K	140 135	I6 way 24 way	\$OCKET 475p 575p	IDC C	ONNECTORS (Sp PCB Male	Female Fen	nale
OA9 40 2A/600V 65 OA47 12 6A/100V 83 OA70 12 6A/400V 95	0 2" Tri colour LEDs	77 45	1040378H0		320 99	28 way 40 way	850p 975p	2 rows	with latch s Strt. Angl Pins Pins		d-Edge wector
OA79 15 6A/600V 125 OA81 20 10A/200V 215	LD271 Infra Red (emit) 46 TIL32 Infra Red (emit) 52 OPT	0	78HI2 I2V/SA 5 78HG+5 to	80 LM323K LM337T 99 LM723	500 175	DIL (Header	PLUGS s) older IDC	10 way	y 90p 99p 130p 150p	85p 120 110p 195	р
OA85 15 10A/600V 298 OA90 8 25A/200V 240 OA91 8 25A/600V 395	SFH205 (detector)	tive	79HG -2.25V to	TBA625B	35 75	14	38p 95p 42p 100p	20 way 26 way 34 way	175p 200p	150p 320	D .
OA95 8 BY 164 56 OA200 8 VM18 50		d similar	SWITCHES SLIDE 250V	TOGGLE	2A 250V	24 40	95p 218p	40 way 50 way	220p 250p	190p 420	D
IN914 4 ZENERS IN916 5 Range: 2V7 to	7 Segment Displays	M.BOXES	IA DPDT C/OFF		33 44 off 54		r CABLE er foot)q erey Color	EURO		MALE MAI	
1N4001/2 5 39V 100mW 1N4003 6 8p eachq	TIL322 5 C.th 115 4×25 DL704 3 C.Cth 99 4×25	×21" 103	A DP on/on/on PUSH BUTTON	SURMIN		10	5p 28p 5p 40p			CKETS PLU rt. Angle Stri	
IN4006/7 7 33V 13W	FND357 or 500 120 5×4× 3" Green C.A. 140 5×2	2 105 x 1 90	Spring loaded Latching or Momentary 6A	SPST on of	ver 60	20 3	0p 50p 0p 65p	DIN 41	1612 2×32 way 27 1612 2-3×32 way 29	Sp 320p 220 Sp 340p 240	p 285p p 300p
IN5401 IS	# 1-3" Red or Green > 150 5 x 22 Bargraph 10 seg. Red 225 5 x 4 x	13" 99	SPDT c/over	99 SPDT c/off SPDT Base 45 DPDT 6 12	d 105	40 7	0р 85р 0р 90р 00р 135р	DIN 41	1612 3×32 way 36	0p 385p 240	p 395p
1544 9 BA102 30	SERBIC CHI ORIDE 6X4X	2" 120 3" (50	MINIATURE Non Locking	DPDT 6 to DPDT C/O DPDT on/	on/on 185	-	ONNECTOR	S:	TRANSFORMERS 3-0-3V, 6-0-6V 100H	nA; 9-0-9V 75m/	
6A/100V 40 BB106 40	7x5x Crystals IIb 8x6x 195p + 50p p&p 10x4	3" 210	Push to make 1	Sp 3 pole c/or		Pins w	9 IS 25 ay way way	37 way	12-0-12V 75mA: 15- 6VA: 2x6V5A: 2x 2x15V25A		98p 3A: 220p
6A/800V 65 Z5J 195	DALO ETCH RESIST 12×5	×3" 275 ×3" 260	ROCKER: 5A. 250 ROCKER: 10A 25		28p 38p	MALE Solder E Angle ES		240p 355	12VA: 2x4V5-1-3A; 2x15V4A	25	2V~5A; PSp (35p p&p)
Noise Diode Z5] 195 3A/100V 48 3A/400V 56	Pen plus spare tip 90p 12×8	x3" 295	ROCKER: With n 10A. 250V, DPST	eon lights red w	hen on. 85p	Strait 17	¹⁰ p 160p 226p	310p	24VA: 6V-1-5A 6V- 12V-1A 12V-1A; 15- 20V6A	8A 15-8A: 20V	-6A 10p (60p p&p)
SCR's 3A/800V 85 Thyristors 8A/100V 60	COPPER CLAD BOARDS Fibre Single Double- Glass sided sided	5RBP 95"×85"	ROCKER: (White ROTARY: Make y Switch, Shafting Ass	our own Multiw	27	Solder	105p 160p 200p 165p 215p 290p	338p 440p	50VA: 2×6V-4A 2×15V-1-5A; 2×20	: 2×9V-2-5A;)V-1-2A; 2×25V	2×12V-2A;
0-8A-100V 32 8A/400V 69 5A/300V 38 8A/800V 115 5A/400V 40 12A/100V 78	6"×6" 90p 110p 6"×12" 150p 195p	95p	dates up to 6 wafer Break before make	s. Wafers, Silver o	90p ontacts.	COVERS			0-8A 465p (60p p8p 100VA: 2×12V-4/ 2×30V-1-5A; 2×40V	A: 2×15V-3A:	2×20V-2 5A.
5A/600V 48 12A/400V 82 8A/300V 60 12A/800V 135	VEROBOARDS 0 I" Clad Plain 'VQ' Board	180	I pole/12 way; 2 pi 4 way; 4 pole/3 wa Mains DPST 5witch	y: 6 pole/2 way	65p 45p	IDC 25 v	vay Plg. 38 5p, Slui 4		JUMPER LEADS		20p (60p p&p)
12A/100V 78 16A/400V 105 12A/400V 95 16A/800V 220	2 × 3 85p — 'DIP' Board 2 × 5" 100p — Vero Scrip	374 144	Screen & Spacers ROTARY: (Adjus	table Stop Ty	6p		EDGE CONNEC	-156"	DIL Plug (Headers) Single Ended Lead, 2	4" long	
BT106 150 25A/400V 185 25A/800V 295	3 x 3 100p — \$100 Board 3 x 5 115p 87p 3 x 17 390p 298p PROTO-1	DECs	1 pole/2 to 12 way. 2 to 4 way, 4 pole/	2 to 3 way	45p	SHL	2x 10 way 2x 15 way 2x 18 way 180b	135p 140p 145p	Length 14pm 24' 145p Double Ended Leads	16pin 24 pin 165p 240p	40 pin 325p
C106D 38 250 1000 480 TIC44 24 304 4004 535	4½x 18" 495p 275 Veroblock Plct. of 100 pins 55p S-Dec Spot Face Cutter 150p Eurobreadt	405 350	POTARY: Mains 2 DIL SWITCHES: 6 way 80p; 8 way	(SPST) 4 way 6	Sec:	Sockets 0.1"	2×22 way 199p 2×23 way 170p	200p 1 90 p	6" 185p 12" 198p	205p 300p 215p 315p	465p 490p
TIC45 29 T2800D 120	Pin Insertion Tool 185p Bimboard Superstrip	695	6 way 80p; 8 way I (SPDT) 4 way I 90p THUMBWHEEL Decade Switch Moo	Mini front mour	rding 220p	20 way 65p 32 way	2 x 25 way 225p 2 x 26 way 210b 2 x 30 way 245p	220p	36" 230p	235p 345p 250p 375p	540p 595p
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DIAC 5T2 25 500 370p	Wire Wrapping Stakes 100	mbs 6p ea 250p	PROXIMITY Swi	ch with magnet	125p		2×75 way 550p			370p 480p	525p
COMPUTE			WE-ROM for		32.768KI	Hz 100	AMPHE	- 1	DC Solder		TEC UHF ULATORS
	resolution graphics 10" Tractor		Acorn ATOM		100KHz 200KHz 455KHz	235 268 370	24 way IEE 36 way Centro	Mik	475p 450p 525p 485p	6MHz 8MHz	325p Wideband
feed, parallel interface standar SEIKOSHA GP 250X Prin		ROM. Plugs	ophisticated Acorn straight into floating et. Gives many uniqu	point Atom's	IMHz I-008M I-28MHz	275 275 392					450p
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BIPOLAR MODULES

Module Number	Output Fower Watts rms	Loed Impedance	T.H.D. Typ at 1KHz	I.M.D. 60Hz/ 7KHz 4:1	Supply Voltage Typ	Size mm	WT	Price inc.
117 [0]	14)	4-8	9,015%	<0.006%	1.18	76 × 68 × 40	240	£8.40
11/26/1	- 10	4.8	13,015%	<11,006%	1 25	76 × 68 × 40	240	19.55
11/49/25()	30 + 30	4.8	U,015%	<0.006%	£ 25	120 x 78 x 40	420	118.69
H - 124	60	- 4	0,01%	<0.006%	1.26	120 x 78 x 40	410	£20,75
HCC17H	60	H	0.01%	<0.006%	1 35	120 × 78 × 40	411)	€20.75
HY 244	120	4	11,111%	<0.006%	£ 35	120 x 78 x 50	520	€25.47
FF < 24B	1.20	- 8	0,01%	<0.006%	£ 50	120 x 78 x 50	520	1.25,47
HY Byl	180	-4	0,01%	<0.006%	1.45	120 x 78 x 100	1030	£38.41
H F 85B	180	R	0.01%	< 0.006%	± 60	120 x 78 + 100	1030	138.41

Protection: Full load line, Slew Rate: $15\nu/\mu$ s. Risetime: 5us. S/N ratio: 100db, Frequency response $\{-3d8\}$ 15Nz-50KHz, Toput sensitivity: 500mV rms, Input Impedance: 100K Ω . Damping factor: 100Mz >400.

Module Module Number		ntser		
1176	Misno pre amp	Mic/Mag, Cartridge/Tuner/Tupe/ Aux + Vol/Bass/Treble	10mA	£7.60
HVIII	Stereo pre amp	Mic/Mag, Cartridge/Tuner/Tape/ Aux → Voi/Bass/Treble/Balance	20mA	£14,32
HY 7.3	Ciurtar pre amp	Telio Guitar (Bass Lead) and Mic + separate Volume Bass Treble + Mix	20mA	£15.36
HY7H	Stereo pre amp	As HY66 less tane controls	20mA	£14.20

Most pre-amp modules can be driven by the PSU driving the main power amp. A separate PSU 30 is available purely for pre amp modules it required for £5-47 (inc. VAT). Pre-amp and mixing modules in 18 different variations. Prease send for details.

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Model Number	For Use With	Price Inc. VAT
PSU 52X	2 x HY124	£17,07
PSU 53X	2 n MOS128	117.86
PSU 54X	1 x HY248	£17.86
PSU 55X	1 x MOS248	£19.52
PSU 71X	2 s HY244	£21.75

MOSFET MODULES

Module Number	Output Power Watts rms	Load Impedance		RTION I.M.D. 60Hz/ 7KHz 4:1	Supply Voltage Typ	Size mm	WT gms	Price inc. VAT
MOS 128		4-8	<0.005%	<0.006%	1 45	120 - 78 - 40	120	1.30.4.5
MOS 248	120	4.8	<0.005%	<0.006%	1 55	120 x 78 x 80	H50	1.39,86
MOS 364	180	4	<0.005%	< 0.006%	1 55	120 × 78 × 100	1025	1.45.54

Protection: Able to cope with complex loads without the need for very special protection circuitry fluxes will suffice).

Siew rate: 200/µs. Rise time: 3µs. SNr satio: 100db
Fracumory response (= 3dB): 15½ = 100KHz, input sensitivity: 500mV rms. Input impedance: 100K.D. Damping factor: 100Hz > 400.

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UC1 PRE AMP UNIT: Incorporates the HY78 to provide a "no frills", low distortion, (<0.01%), stereo control unit, providing inputs for magnetic cartridge, tuner, and tape/monitor facilities. This unit provides the heart of the hi fi system and can be used in conjunction with any of the UP Unicase series of power amps. For ultimate hum rejection the UC1 draws its power from the power amp unit.

POWER AMPS: The UP series feature a clean line front panel incorporating on/off switch and concealed indicator. They are designed to compliment the style of the UC1 pre-amp. Performance for each unit which includes the appropriate power supply, is as specified on the facing page.

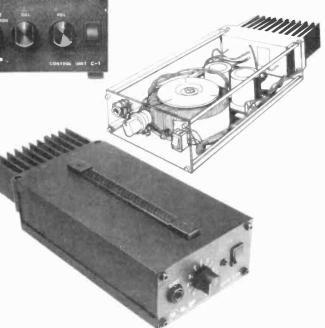
Power Slaves

Our power slaves, which have numerous uses i.e. instrument, discotheque, sound reinforcement, feature in addition to the hi fi series, front panel input jack, level control, and a carrying handle. Providing the smallest, lowest cost, slave on the market in this format.

UNICASES

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UP2X	60W/4Ω	Bipolar	Mono	HiFi	€54.95
UP3X	60W/8Ω	Bipolar	Mona	HiF:	£54.95
UP4X	120W/4Ω	B polar	Mono	HiFi	£74.95
UP5X	120W/8Ω	Bipolar	Mono	HiFi	€74.95
UP6X	60W/4−8Ω	MOS	Mono	HIF:	£64.95
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Power SI	aves				
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US3X	60W/4-8Ω	MOS	Power	Slave	£69,96
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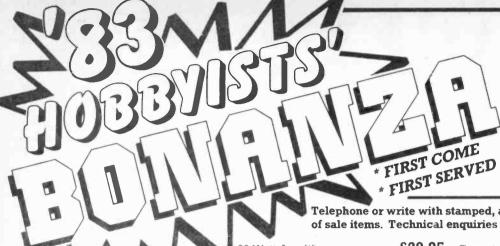
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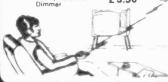
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enabling the temperature of an en-closure to be maintained to within 0.5°C. Max, load 3KW MK5 MAINS TIMER Based on the ZN1034E Timer IC this kit will switch a mains load on (or off)

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THERMOMETER KIT

This new designais based on the ICL7126 (a lower power version of the ICL7106 chip) and a 31/2 digit fliquid crystal display. This kit will form the basis of a digital multimeter lonly a few additional resistors and switches are required—details supplied), or a sensitive digital thermometer (-50°C to -150°C) reading to 0.1°C. The basic kit has a sensitivity of 200mV for a full scale reading, automatic polarity indication and an ultra low power requirement—giving a 2 year typical battery life from a standard 9V PP3 when used 8 hours a day. 7 days a week.

Price £15.50

DISCO LIGHTING KITS

£14.60 DL 2100 K

andirectional channel sequence variable by means of a pre-set p switched only at mains zero cro switched only at mains zero to reduce radio interference

Optional opto input DLA1 Only £8.00
Allowing audio ("beat") light

DL3000K

60p

zero voltage switching, automatic level con trol and built in mic. No connections to speaker or amp required. No knobs to adjust simply connect to amps. (1Kw channel)

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MICROCOMPUTER uses FORTH which executes about 10 times faster and

in stock requires less program memory than a comparable program using basic. Features 8K ROM, 3K RAM, built in speaker, 40 key keyboard and a 32 x 24 line-flicker free display on TV.

Comes supplied complete with leads, mains adaptor, a comprehensive easy-to-follow manual on Forth programming + FREE cassette containing 5 sample programs.

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The XK103 is a general purpose infra-red transmitter/receiver with one momentary (normally open) relay contact and two latched transistor output. Designed primarily for controlling motorised garage doors and two auxillary outputs for drive/garage lights at a range of up to 40 ft. The unit also has numerous applications in the home for switching lights, IV, closing curtains, etc. Ideal for aged or disabled persons.

The Kit comprises a mains powered receiver, a four button transmitter, complete with pre-

The Kit comprises a mains powered receiver, a four bution transmitter, complete with pre-drilled box, requiring a 9V battery and one opto-isolated solid state switch kit for interfacing the receiver to mains appliances. As with all our kits, full instructions are supplied.

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16 ranges including DC voltage (200 mv-1000v) and AC voltage, DC current (200 mA-10A) and resistance (0-2 M) + NPN & PNP transistor gain and diode check. Input impedance 10M. Size 155 × 88 × 31mm. Requires PP3 9V battery. £29.00

REMOTE CONTROL KITS

MK6 SIMPLE INFRA RED TRANSMITER

Pulsed infra red source complete with hand-held plastic box. Requires a 9V battery.

MK7 INFRA RED RECEIVER

Single changel cancer received.

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el, range approx. 20ft. Walns powered with a triac output to switch loads up to 500W
9.00 (RC500K – Special Price for MK6 and MK7 together £12,50

at 2309 ac. £300 (RC500K ~Special Price for MK6 and MK7 together £1 MKE CODED (NFRA RED TRANSMITTER Basad on the SL490, the kit incluces all components to make a coded transmitter and requires a 9V (PP3) battery and keyboard. 8 x 2 x 1.3.cms

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For use with MK8 and MK18 to generate 16 different codes for decoding by the ML928 or ML926
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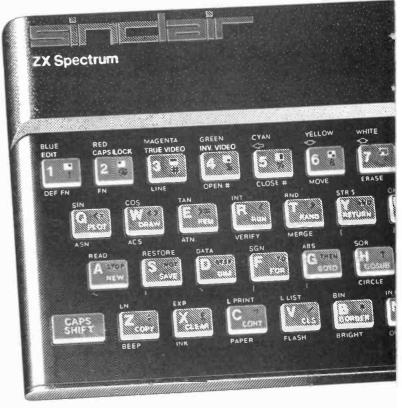
You have access to a range of 8 colours for foreground, background and border, together with a sound generator and high-resolution graphics.

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Yet the price of the Spectrum 16K is an amazing £125! Even the popular 48K version costs only £175!

You may decide to begin with the 16K version. If so, you can still return it later for an upgrade. The cost? Around £60.



Ready to use today, easy to expand tomorrow

Your ZX Spectrum comes with a mains adaptor and all the necessary leads to connect to most cassette recorders and TVs (colour or black and white).

Employing Sinclair BASIC (now used in over 500,000 computers worldwide) the ZX Spectrum comes complete with two manuals which together represent a detailed course in BASIC programming. Whether you're a beginner or a competent programmer, you'll find them both of immense help. Depending on your computer experience, you'll quickly be moving into the colourful world of ZX Spectrum professional-level computing.

There's no need to stop there. The ZX Printer – available now – is fully compatible with the ZX Spectrum. And later this year there will be Microdrives for massive amounts of extra on-line storage, plus an RS232 / network interface board.



Key features of the Sinclair ZX Spectrum

- Full colour 8 colours each for foreground, background and border, plus flashing and brightness-intensity control.
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something for everyone. And they all make full use of the Spectrum's colour, sound, and graphics capabilities. You'll receive a detailed catalogue with your Spectrum.

ZX Expansion Module

This module incorporates the three functions of Microdrive controller, local area network, and RS232 interface. Connect it to your Spectrum and you can control up to eight Microdrives, communicate with other computers, and drive a wide range of printers.

The potential is enormous, and the module will be available in the early part of 1983 for around £30.

sinclair

Sinclair Research Ltd, Stanhope Road, Camberley, Surrey GU15 3PS. Tel: Camberley (0276) 685311.

The ZX Printer – available now

Designed exclusively for use with the Sinclair ZX range of computers, the printer offers ZX Spectrum owners the full ASCII character set—including lower-case characters and high-resolution graphics.

A special feature is COPY which prints out exactly what is on the whole TV screen without the need for further instructions. Printing speed is 50 characters per second, with 32 characters per line and 9 lines per vertical inch.

The ZX Printer connects to the rear of your ZX Spectrum. A roll of paper (65ft long and 4in wide) is supplied, along with full instructions, Further supplies of paper are available in packs of five rolls.



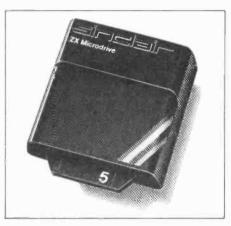
The ZX Microdrive – coming soon

The new Microdrives, designed especially for the ZX Spectrum, are set to change the face of personal computing by providing mass on-line storage.

Each Microdrive can hold up to 100K bytes using a single interchangeable storage medium.

The transfer rate is 16K bytes per second, with an average access time of 3.5 seconds. And you'll be able to connect up to 8 Microdrives to your Spectrum via the ZX Expansion Module.

A remarkable breakthrough at a remarkable price. The Microdrives will be available in the early part of 1983 for around £50.



How to order your ZX Spectrum

BY PHONE-Access, Barclaycard or Trustcard holders can call 01-200 0200 for personal attention 24 hours a day, every day. BY FREEPOST-use the no-stamp needed coupon below. You can pay by cheque, postal order, Access.

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EITHER WAY-please allow up to 28 days for delivery. And there's a 14-day money-back option, of course. We want you to be satisfied beyond doubt-and we have no doubt that you will be.

Qty	Item	Code	Item Price £	Total £
	Sinclair ZX Spectrum - 16K RAM version	100	125.00	
	Sinclair ZX Spectrum - 48K RAM version	101	175.00	
	Sinclair ZX Printer	27	59.95	
	Printer paper (pack of 5 rolls)	16	11.95	
	Postage and packing: orders under £100	28	2.95	
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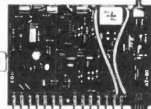
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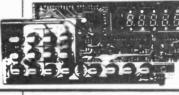


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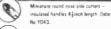
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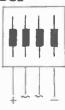
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ONLY £31.00 plus £2.75 p&p.

· NOISE REDUCTION SYSTEM. · AUTO • NOISE REDUCTION SYSTEM. • AUTO STOP. • TAPE COUNTER. • SWITCHABLE E.O. • INDEPENDENT LEVEL CONTROLS. • TWIN V.U. METER. • WOW & FLUTTER 0.1%. • RECORD/PLAYBACK I.C. WITH ELECTRONIC SWITCHING. • FULLY VARIABLE RECORDING BIAS FOR ACCURATE MATCHING OF ALL TYPES

Kit includes tape transport mechanism ready punched and back Printed quality circuit board and all electronic parts, i.e. semiconductors, resistors, capacitors, hardware, top cover, printed scale and mains transformer.

You only supply solder & hook-up wire. Featured in April P.E. reprint 50p. Free with kit.



Amplifier for your personal stereo cassette player - as featured in January issue of Everyday Electronics. Turn your personal stereo into a mains powered home unit. Parts:

Stereo power amp PCB with all components, £3.50 + 75p p&p. Power supply unit £1.95 + £1.50

Pair of eliptical speakers



6.1.50 the pair +£1 p&p. Input & output sockets and plugs,£1.50. Recommended case (for the power supply and amp only),£2.95+80p p&p. P&P inclusive price of £1.75 for any two or more

125W HIGH POWER AMP MODULES

The power amp kit is a module for high power applications - disco units, guitar amplifiers, public address systems and even high power domestic systems. The unit is protected against short circuiting of the load and is safe in an open circuit condition. A large safety margin exists by use of generously rated components, result, a high powered rugged unit. The PC board is back printed, etched and ready to delife news of construction and the ready to drill for ease of construction and the aluminium chassis is preformed and ready to use. Supplied with all parts, circuit diagrams and instructions.

ACCESSORIES: Suitable mains power supply kit with transformer: £8.50 + £2.00 p&p, Suitable LS coupling electrolytic. £1 + 25p p&p,



SPECIFICATIONS:
Max. output power (RMS): 125 W. Operating voltage (DC): 50 - 80 max. Loads: 4 - 16 ohm. Frequency response measured @ 100 watts 25Hz - 20KHz, Sensitivity for 100w: 400mV @ 47K, Typical T.H.D. @ 50 watts, 4 ohms: 0.1%. Dimensions: 205x90 and 190x36mm

£10.50 +£1,15 p&p

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SPEAKER BARGAINS BSR RECORD DECK

Manual single play record deck with auto return and cueing lever. Fitted with stereo ceramic cart-ridge 2 speeds with 45rpm spindle adaptor ideally suited for home or disco £12.95 + £1.75 p&p.

13"x 11" app.

SPECIAL OFFER! Replacement Stereo cassette tape heads — £1.80 each. Mono: £1.50 each, Erase: £0.70 each. Add 50p p&p to order.

218 HIGH STREET, ACTON, W3 6NG.

Note: Goods despatched to U.K. postal addresses only. All items subject to availability. Prices correct at 30/10/82 and subject to change without notice. Please allow 7 working days from receipt of order for despatch. RTVC Limited reserve the right to up-date their products without notice. All enquiries send S.A.E. Telephone or mail orders by ACCESS welcome

2 WAY 10 WATT SPEAKER KIT

8" bass/mid range and 3%" tweeter. Complete with screws, wire, crossover components and cabinet. All wood pre cut – no cutting required. Finish - chipboard covered wood simulate, size 14%"x 8%"x 4", PAIR for ONLY £12.50 plus £1.75 p&p.



ALL CALLERS TO: 323 EDGWARE ROAD, LONDON W2, Telephone: 01-723 8432.



Gatewaytoa Commission in the Technical Corps of the rmy.

Since 1953 Welbeck, Britain's first Sixth Form College, has played a crucial role in providing Officers for the Technical Corps of the Army and now produces a large proportion of the Army's technical graduates.

It is not a military unit but a boarding school with very high academic standards offering 'A' level courses in science and technology, with some Arts subjects; great emphasis is placed on games, leadership training and preparation for Sandhurst through the Combined Cadet Force to which every boy must belong.

To an intelligent, energetic and fit young man with the ambition and genuine motivation to be an Army Officer Welbeck offers a first class prospect with an opportunity, at a later stage, for a degree course in engineering or related science at the Army's expense.

The maintenance contributions are reasonable. Entry is highly competitive and applicants should be expecting to obtain good passes at GCE 'O' level (or equivalent) in Mathematics, Physics, English and at least two other subjects preferably including Chemistry.

Normal entry is in the September or January following 'O' levels and the closing date for the next available entry in January 1984 is 1st May 1983. The age limits on entry are from 16 to $17\frac{1}{2}$ years.

Further details about the College and the prospectus may be obtained from the Headmaster, Dept. G 17, Welbeck College, Worksop, Notts S80 3LN.





VOLUME 19 No. 4 APRIL 1983

NO FOOLING

ALL readers please note that this is our April issue. We have had some interesting correspondence in past years following publication of our April issue and one or two "not quite true" pieces. If you see what we mean? There are two such pieces in this issue. They are both obvious once you have read them properly, if not before! However, it appears that we may have to consider not publishing any further items of an April 1 nature, since it is becoming more and more difficult to discriminate between fact and fiction.

There are two true news stories in this months' News & Market Place that could be "not quite true". The ones we are referring to are 'Shades of 1984' and 'Walk Around 3D.' Both are true but, in their own way, both are significant steps forward and therefore one could be excused for doubting them. While some of our editorial team were busily at work writing nonsense (something they do particularly well!) it occurred to those slaving over the truth that since some items of the latter commodity are rather wav-out, their work could be undermined by the first group! The moral is believe everything we say unless its code name is April 1, we tell you its rubbish or we have made a mistake! (Please don't ring up

for Llivs Electronics phone number).

THE REAL THING

Having spoken about "news" it is worth looking at where things may go in the next year or so. Obviously the computer will eventually have a considerable impact on the hobby electronics area. By this we do not mean that computing will take over from soldering and testing-it may for some, but that is a change of hobby. What we are getting at is the computer automation of i.c. design, which will change what is generally available.

The cost of a custom i.c. is rapidly falling due mainly to automated design and the ability to manufacture combination circuits with analogue and digital circuitry on one chip. Charles E. Sporck, President of National Semiconductor Corp., recently said in a Electronic Design International article "Now thanks to design automation, we can provide a half dozen circuits with the investment it once took to produce just one. All this will give us the freedom to look at more dedicated circuit applications"

This could affect our hobby in two ways: First, it could mean more complex and sophisticated equipment could be easily constructed from one chip plus some controls, readouts,

transducers etc.

Second, it could mean a demise in our hobby if such chips are not available on the open market. This is bound to happen to some extent—as it does now-but we do not believe we will have to give up and go away in the foreseeable future! Perhaps PE will have to arrange for supply of special chips to our designs in years to come, who knows?

Of course with things changing as fast as they are we could become Practical Bioelectronics at some stage in the not too distant future. Last month we announced in News & Market Place that Mississippi University were close to the birth of a molecular diode using a molecule that can exist in two states. This obviously means that implant electronics, not far from that this months' described in Semiconductor Update, is nearing reality. As we said, we may not be able to publish any more April 1 pieces!

P.S. Don't forget from next month PE will be even better value with more editorial pages in every issue page 6/6 of Micro-file for details of contents.

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We regret that lengthy technical enguiries cannot be answered over the telephone

Queries and letters concerning advertisements to: Practical Electronics Advertisements, King's Reach Tower, King's Reach, Stamford Street, SE1 9LS Telex: 915748 MAGDIV-G

Letters and Queries

We are unable to offer any advice on the use or purchase of commercial equipment or the incorporation or modification of designs published in PE. All letters requiring a reply should be accompanied by a stamped, self addressed envelope, or addressed envelope and international reply coupons, and each letter should relate to one published project only.

Components and p.c.b.s are usually available from advertisers; where we anticipate difficulties a source will be suggested.

Back Numbers

Copies of most of our recent issues are available from: Post Sales Department (Practical Electronics), IPC Magazines Ltd., Lavington House, 25 Lavington Street, London SE1 OPF, at £1 each including Inland/Overseas p&p. Please state month and year of issue required.

Binders

Binders for PE are available from the same address as back numbers at £4.60 each to UK or overseas addresses, including postage and packing, and VAT where appropriate. Orders should state the year and volume required.

Subscriptions

Copies of PE are available by post, inland or overseas, for £13.00 per 12 issues, from: Practical Electronics, Subscription Department, Oakfield House, Perrymount Road, Haywards Heath, West Sussex RH16 3DH. Cheques and postal orders should be made payable to IPC Magazines Limited.

Items mentioned are available through normal retail outlets, unless otherwise specified. Prices correct at time of going to press.

... MEUSS &

Shades of 1984

The video age works both ways. Be warned! The Pacman and Invader watching society is in turn being watched. Not just by those television cameras which oversee the busy commuterways, but by less obvious ones. Tomorrow's world will bring the thinking camera into commonplace existence. Today's world has seen to it.

The Home Office's Research and Development Branch has, after five years work, succeeded in bringing to fruition a remote vehicle number plate reading camera. This TV camera is undergoing operational trials, now, in London. The Home office requests that its whereabouts is not revealed.

Because the tireless policeman does not exist, it is impossible to note the registration number of every passing vehicle to see if it has been stolen; but now, this portentious camera system surely heralds the demise of organised car theft. Terrorists too, may find themselves inexplicably netted. From its secret vantage point, the number plate reader checks out each passing number via a landline to the Police National Computer.

In fact, the camera itself is conventional, save sensitivity in the infra-red region for night viewing. Its focus setting is guaranteed by using a sensor buried in the road,

which triggers the "snap shot". Presumably it's because rear number plates tend to stay cleaner than front ones that the camera views receding traffic. The clever bit is that the signal from the camera is somehow electronically processed to extract the registration number, and sound the alarm if something is amiss. It is our guess that some sort of block scan takes place to seek out recognisable alphanumeric characters, and then convert them to their ASCII (or other) codes for transmission.

According to Crime Prevention News, overall accuracy on the experimental system is about 50 per cent in all conditions, rising to 70 per cent with new cars. Quick visual, and other checks are said to keep false alarms to a minimum. Computer errors in the electricity bill are irritating enough, so let's hope so.

Despite a projected production cost of £60,000 a number of police forces are keenly interested in the trials.

INNOVATIONWORKSHOP

Ever had an idea for an electronic device, but lacked the funds to try it out? Ever wondered how many other seeds of ingenuity remain ungerminated elsewhere? Residents of the North East need not allow their potential contributions to science remain on ice. Newcastle's Microelectronics Applications Research Institute (MARI) is prepared to help them thaw out their frozen dreams at its Microelectronics Innovation Workshop. Based at MARI's own premises, the workshop is a bid to attract local inventors and entrepreneurs with new applications for microelectronics, and, hopefully, to spark off fresh companies. The scheme is funded by Tyne and Wear County Council and the DoE under the Urban Programme.

Individuals using the workshop receive supervision and assistance during the early stages of their development work. They are able to experiment and test their ideas using equipment and facilities which would otherwise be beyond their means; and they may also attract customers and backers.

The workshop was opened in December last year, and many projects are already growing within it which include an assembly system for technical dentistry, and a reading aid for the blind

The Innovation Workshop appears to be a very good idea, and it would not be a bad thing if they were to spring up elsewhere.

MICROCONTROLLER VIDEO

SAT Electronics have developed a video RAM card for use with the PE Microcontroller which is the first of a series of expansion boards.

The video card is a full memory mapped display interface for use with a VDU or TV. The memory of the interface is accessed in exactly the same way as the existing RAM within the Microcontroller and as such, can be used as extra memory if required, on full battery back-up.

The size of the memory is 2K and it is arranged as a 32x16 on screen matrix. There are 128 characters available and these are ideally suited to control or text handling operations because of the inclusion of a graphics set. In addition, these characters are available in a flashing mode.

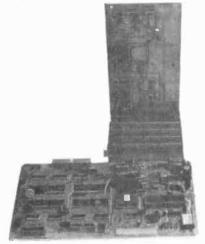
The card itself has a 43 way edge connector and can either be plugged directly onto the expansion socket or fitted via a Mother card assembly.

Complete documentation is provided together with the card, expansion socket and all the necessary wires and components.

The price of the video RAM card is £49-68 including VAT and p&p.

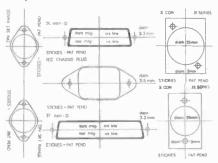
In addition to the video RAM card other

cards which will be available soon include a Mother board assembly, multi-channel AtoD and DtoA convertors, real time, day, date card, counter timer, full ASC11 keyboard controller, RAM cards (various sizes) and a sound generator card. For further details contact SAT Electronics 235 Cross Street, Sale, Cheshire (061 905 1040).



MARKING BLUES

For those of us who have trouble marking out front panels and cutting out same without damage, there is now an easier and far less hazardous alternative. Namely—'Sticky Templates'. These self-adhesive clear film templates are simply stuck onto the panel in the required position. Each one has horizontal and vertical centre lines which makes lining up multi-connector arrays easy. When the area is worked the film also protects the panel. From Futronics Technology (UK) Ltd., 15 North Avenue, London, W13 8AP (01-991 0070).



MARKEZ PLACE

The Amazing Mr. CUBOT

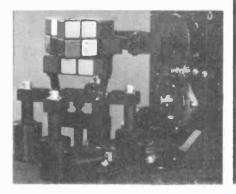
Some say that Rubik's Cube is now passe, but not Cubot. Cubot is a portable robot weighing about 70 pounds, that can solve Rubik's Cube and, like a ventriloquist's dummy, retire to a standard size suitcase. Cubot may not be humanoid, but it can nevertheless clasp a randomised Cube in its gripper, view it knowlingly, and then proceed to unscramble it.

Enginners of the Battelle Memorial Institute designed and built Cubot as a fun, off hours effort. Battelle spokesman, Dr. Michael Lind said that this robot is intended to demonstrate the Institute's unique capabilities in the integration of differing technologies. Cubot combines electro-optics, microprocessing, and mechanics, and was created by a volunteer force of twenty scientists and engineers of the Pacific Northwest Laboratories, Engineering Physics department.

Cubot has an eye that is sensitive to the Cube's six colours, and which is used to recognise patterns as it surveys the Cube's six faces. Information is absorbed by the robot's first microcomputer. Here, an algorithm generates the series of instructions for a second microcomputer which controls the minipulator. With a clunk and a whirr Cubot can unscramble the Cube in less than four minutes. Not as fast as some human beings, true, but Cubot's designers are confident that they can hone their prodigy's performance down to two minutes.

Rubik's Cube has a staggering number of combinations $(4\cdot3\times10^{19})$. To put its ability to beguile firmly into perspective, it has been calculated that if a person had started generating legitimate combinations at a rate of one a second, upon the creation of the universe, by today only one per cent of all possible combinations would be completed.

Cubot is not the first robot to solve this intricate puzzle, but as far as is known, it is the first robot to physically unscramble the cube without human intervention.



ZX SPECTRUM ADD-ONS

Two new 'add on' accessories for the ZX Spectrum are the DCP Interspec and the DCP Speech pack. These products are direct descendants of the successful ZX81 peripherals produced by DCP Microdevelopments (David C. Palmer). Interspec provides many electrical interfaces including an 8 channel A to D converter for joysticks or temperature sensing, 4 relay outputs for high current control, 4 switch inputs buffered for direct connection to contacts and an 8 bit I/O port for the users own digital design applications. Featured on the rear of the unit is the DCP BUS; an expansion system using a 15 way connector directly controlling up to 4 more accessories, this is expandable to 255 more devices with the addition of a few discrete components. Second is the Speech Pack: this is the Spectrum version of its ZX81 namesake, it features a built in speaker, expandable vocabulary, volume control and ZX connector for other accessories. This pack is controlled by simple OUT commands followed by the number of the selected word. Interspec costs £39-95 and the Speech Pack £49-95 inc VAT and p&p. Available from, DCP Microdevelopments Ltd, 2 Station Close, Lingwood, Norwich NR13 4AX. (0603) 7124821.





Silicon News Corner

Bulletins covering new semiconductor devices arrive at PE almost daily, and it is possible only to describe them briefly. Details of how to obtain further information are included, however.

Motorola: A T0220 packaged 15A thyristor, one of a series designed for high speed invertors and switching. The MCR2150/A has a maximum turn-off time guaranteed at 4µs!

A TMOS SCR, the MCR 1000 offers the input impedance of a power MOSFET with the latching action of a thyristor. It is rated at 600V, 15A, with turn on and off times of 200ns and 6µs respectively. Ask for engineering bulletin EB103 from Motorola Semiconductor products Dvn., York House, Empire Way, Wembley, Middlesex.

National Semiconductor: The DP8409-2 multimode DRAM Controller/Driver is a one-chip approach to dynamic memory design. It is capable of driving up to 88 DRAMs!

National's new Nitride Plus passivation technique goes into their LP165/LP365 series simultaneously programmable quad comparator. This highly flexible device dissipates only 10µW/comparator, and its outputs are compatible with DTL, TTL, CMOS and MOS. National Semiconductor, 301 Harpur Centre, Horne Lane, Bedford.

Burr-Brown: Low noise, instrumentation grade op. amps, OPA27 and OPA37 with gains of 1.8kV/mV (125dB), and c.m.r. ratio of 126dB. Power consumption is 3mA. They

differ only in frequency compensation. Burr-Brown, Cassiobury House, Station Rd., Watford, Herts.

RCA: A 741 pin compatible op. amp, the CA3420 series combines PMOS and bipolar technology to tolerate supplies down to 2V, and common mode input voltages down to 0.45V below negative rail. RCA, Lincoln Way, Windmill Rd., Sunbury-on-Thames, Middlesex.

Altek: A 2K byte CMOS RAM of ultra low power data retention. The M5M5118P will standby at 10µA with the supply reduced from 5V to 3V. Access time is less than 200ns.

A new d.i.l. active delay line, the Lexor 84300 series is TTL compatible. Delay is from 25 to 500ns, with tapped outputs, and fan-out is 10 TTL loads per tap. Altek Microcomputers, 22 Market Place, Wokingham, Berks. Intersil: A low power A/D converter featuring 3½ digits, auto-zero, auto-polarity, differential input, single differential reference, and direct drive to l.c.d. or l.e.d. The big step forward in the ICL 7136 is overrange recovery, faster conversion speed (3 per sec.), yet with only 100µA power consumption (2000 hr. battery life). Input noise can be reduced below predecessors by use of a larger auto-zero capacitor without side effects. This is a pinfor-pin upgrade from the ICL 7216 without circuit changes. Intersil Datel (UK) Ltd., Belgrave House, Basing View, Basingstoke,

... MEUSS &

SHARP'S PC-1251

The PC-1251 from Sharp Electronics is a wallet size computer featuring extended BASIC, 24K bytes of ROM and 4.2K bytes of RAM including 3.7K bytes of user area.

Frequently used commands, statements or mathematical functions can be user defined using any of the 18 reservable keys.

Battery backup protects the contents of the memory in the RAM when the power is off. With this feature, you can turn off the unit in the middle of a program, or load several programs and, without the need for rewriting or reloading, have full use of them later.

The display is a 24-digit 5x7 dot matrix the brightness of which can be varied. Other features include auto power-off to prevent battery drain and a 10 digit calculation feature.

Also available for use with the PC-1251 is the CE-125 which is an integrated printer and microcassette recorder. The PC-1251 has been designed to fit into the CE-125.

The 24-digit thermal printer can type at approximately 0.8 lines/second.

A wide range of software is also available

for use with the PC-1251 including the already proven software of the PC-1211.

The complete system including the printer/cassette module has overall dimensions of 205×149×23mm and weighs just 1·2lbs. The price of the PC-1251 is £79·95 and the CE-125 is priced at £99·95 (prices include VAT and p&p). With each unit Microl will be giving away a free £10·00 software voucher.

Microl, Dept PE, 38 Burleigh St. Cambridge (0223 312453).



Walk Around 3-D

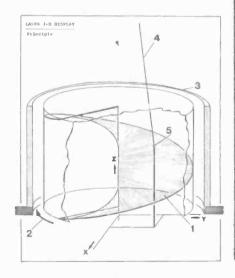
The prospect of a three-dimensional chess game shimmering at the centre of a computerised 3-D display has more appeal than imminence. Yet developments are taking place, and these utilise contraptions ranging from contorting mirrors to whirling corkscrews. Surprisingly, holography is not a front runner in the race for the '3DU'. Whilst the technical problems associated with the production of three-dimensional graphics may not be as simple as X Y Z, a recent development has made possible a true volumetric image within a glass cylinder.

The system uses an upright helix revolving at 30 times a second, acting as a target for a computer controlled, low power helium neon laser. By modulating and deflecting the beam under microelectronic control, it is possible to generate flecks and lines of light on the rotor. Rapid rotation of the helix target makes it virtually invisible, thus creating the illusion of light lines in space. The shape of the rotor is such that sooner or later, any point within the display volume will have a solid surface passing through it, upon which the laser beam may be struck. The computer takes care of the crucial timing.

The experimental system, developed by an IBM scientist and a team at Heidelburg University in West Germany, is only capable of delineating framework outlines. Because of its 360 deg. viewing angle, a feature which in itself has illuded engineers

until now, it is not practical to suppress out of view contours. This is because the observer's viewpoint is not always known, and means that solids can be represented, but not viewed as opaque. A full colour, real time, interactive display is claimed to be feasible, which can be as compact as five centimetres, or as large as five metres in diameter.

Among the suggested applications is an air traffic control display set above a map of the area.



Briefly...

Two new miniature loudspeakers now available from Mullard, are claimed to be the thinnest ever offered. Both are only 5mm in depth, the smallest (type ADO1980) has a 34mm (diameter) cone whilst the slightly larger (type ADO1985) has a 38mm cone.

Even though only button-sized, the loudspeakers can handle 0.3W r.m.s. and have a 400 to 3000Hz frequency range. Each is offered with impedances of 8Ω , 15Ω or 25Ω .

Construction is rugged, both mechanically and environmentally. The frame is a tough plastic pressing. The cone is also plastic. A high permeability samarium cobalt magnet enables high efficiency to be achieved within an ultra-slim format.

Digital television signals to the recently approved CCIR Standard have for the first time been successfully transmitted by optical fibre link between two television studio centres. The experimental transmission, which took place in December 1982, used equipment developed and built by BBC Research Department at Kingswood Warren.

The optical fibre cable contains eight graded-index multimode fibres, and was installed by British Telecom in the existing ducts between the BBC studios at Lime Grove and Television Centre, a path length of about 800 metres. The signals were carried on a single fibre, the basic bit rate of 216 Mbit/s being increased to 270 MBit/s by channel coding. A direct modulated 820 nm laser transmitter was used, the power launched into the fibre being $600\mu W.$

As the television signal was carried in separate component form, pictures of original RGB quality were obtained at the receiving terminal. This avoidance of intermediate PAL coding will allow remote down-stream processing, e.g. colour separation overlay and special effects, to be done with a precision which has hitherto only been achieved at the source itself.

Mitsubishi Electric Corporation Plan to manufacture VTRs in it's UK Factory for sales in the European market.

The initial production of **5**,000 units per month will be made at the Haddington Works of Mitsubishi UK which currently produces colour TVs.

The company envisages a full scale production of 10,000 units per month with parts for the VTRs being supplied from Japan at first but it is hoped that as many parts as possible will be supplied from the EC market.

MARIGE BLACE

ORIC 1

Late in January Oric Products International officially launched the Oric 1 microcomputer from their HQ at Coworth House, Ascot. This mansion set in landscaped woodland seems an unlikely nest from which to fledge such a futuristic bird. Oric 1 presently available with a 16K or 48K memory is their answer to Sinclairs apparent monopoly of the home and small business users market, and at £99.95 and £169 respectively they are very competitive. Although Oric 1 has been available for some months now on a mail order basis the company



plan to phase out this method in favour of the high street retailer. Indeed orders already received have outstripped their predicted sales figures five times over, first year sales are now expected to reach a guarter of a million units. An important feature of this 57 key machine is its ergonomic similarity to the typewriter keyboard, offering such luxuries as tactile feedback and auto repeat keys. The two inch loudspeaker has an impressive range covering six octaves, and can be programmed to synthesise various musical instruments. Other technical details include-28×40 character high resolution graphics and Teletext/Viewdata compatability. With an extended BASIC this machine uses the 6502A microprocessor chip, and comes with a comprehensive manual and a FORTH

AND FINALLY...

Until recently, a family of biproducts of the petrochemical industry, called Tetraprils were quite useless. Now, thanks to the research work of Botch Laboratories of Drudgely, the lowest density member of this family of synthetic proteins has a future in the electronics and electrical industry. Scientists at Botch have discovered that extruded fibres of Tetrapril 1 display a phenomenon called electrostriction. The electrostrictive effect is the physical distortion of a material whilst conducting electricity, and is usually only a fraction of a per cent variation in overall volume. Yet, while looking and feeling much the same as a piece of common elastic band, a Tetrapril fibre will contract by up to 250 per cent when conducting small currents.

Conversion from electrical power dissipation to mechanical force is 85 per cent efficient, so that a lightweight electromechanical actuator can be constructed which develops amazing leverage from one watt of power consumption. It is only necessary to anchor a fibre to the mechanism chassis at one end, attach its other end to a lever, and pass current through it, and you have an actuator. The fibre can either work against a spring, or in antiphase against another fibre. To prove the point, Botch has built a radio controlled aircraft using Tetrapril fibres throughout, as its servo's.

How did Botch discover such a peculiar characteristic in a material which for years has been thought of, literally as rubbish? Research Director, Tom Foolery said that the name of the biproduct itself provides the clue!!!

Goundania

Please check dates before setting out, as we cannot guarantee the accuracy of the information presented below. Note: some exhibitions may be trade only. If you are organising any electrical/electronics, radio or scientific event, big or small, we shall be glad to include it here. Address details to Mike Abbott.

Brighton Electronics March. T

BEX Leeds Mar. 16-17. Dragonara Hotel, K

INSPEX Mar. 21-25. National Exhibition Cntr. Birmingham International. 7.1

Sensors & Systems Mar. 22-24. The Forum, Wythenshawe. T

Compec Wales Mar. 22-24. Cardiff University. Z1

ETM (Electronic Test/Measurement) Mar. 22-24. The Forum. Wythenshawe, Manchester. T

Laboratory Manchester Mar. 23-24. New Century Hall, Corporation

American Holography Mar.-June inc. Light Fantastic Gallery. Covent Garden, London. A8

London Computer Fair April 14-16. Central Hall, Westminster. B5 All Electronics Show April 19-21. Barbican Cntr., London. E

Fibre Optics April 19-21. Porter Tun Rooms, The Brewery (!), Chiswell St., London EC1. E

International Materials Handling April 19-26. Earls Court. 1 International Packaging Exhibition April 25-29. NEC B/ham. I

HEVAC (Heating, Ventilation & Air Cond.) Apr. 26-28. Barbican. 1 Scottish Personal Computer World Show April 16-18. MacRobert

Pavilion, Ingliston, Edinburgh M

Midland Computer Fair April 28-30. Bingley Hall, B/ham. Z1

Biotech May 4-6. Wembley. O

Micro City May 10-12, Bristol Exhibition Complex. F3

The Business Computer Show May 10-12. Wembley. O

Cable (Conf. & Ex.) May 10-12. Wembley Conf. Centr., London. O

Defence Components Expo May 10-12. Metropole, Brighton. I

Welsh Amateur Radio, TV & Electronics Rally May 22. Barry Memorial Hall, S. Glam. C

Computers In The City (conf. & ex.) May 24-26. Barbican. O

Business Telecom May 24-26. Barbican. O

International Word Processing May 24-27. Wembley Conf. Cntr. Z East Suffolk Wireless Revival May 29. Ipswich Civil Service

Sportsground. V1 Russian Holography June-Sept. Inc. Light Fantastic Gallery. A8 Semlab June. Olympia. I

IBM Productivity (conf. & small ex.) June 14-16. Tara Hotel, London.

The Computer Fair June 16-19. Earls Court Z1

Compec North June 21-23. Belle Vue, Manchester. Z1

Transducer/Tempcon June 28-30. Wembley Conf. Cntr. T

Leeds Electronics Show July 5-7. University. E

A8 Holographic Exhibitions & 01-826 6423

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BATTERY TESTER

N recent years the dry battery has become much less used due to the ready availability of mains derived supplies, and, more recently the increased price competitiveness of Nickel Cadmium rechargeable cells. Even so much portable equipment still relies on batteries which bring with them the need for replacement at regular intervals, and more importantly the problem of when to do this. In theory it is very easy to test a battery by measuring its output voltage but this can be very misleading since a battery can often give an almost new voltage reading if no current is drawn from it as happens with a standard voltmeter. Some form of dummy load is obviously required and by the time that this and the meter have been organised it is often simpler to ignore the problem until the batteries go totally flat, probably leaking as they do so.

This article describes a fairly simple and cheap battery tester which loads the battery to 15 milliamps and indicates the output voltage state on three light emitting diodes. The circuit was designed for use with standard 1.5 volts/cell batteries and accordingly will test for the following voltages: 1.5, 3, 4.5, 6, 9 and 12. There is no reason why other voltages cannot be chosen, and the unit may be converted to test NiCads by simply altering a few resistors. The tester has no on/off switch and switches itself on when a voltage greater than 700 millivolts is applied to the test terminals. The current drain when not in use is well below a microamp and so will not discharge the PP3 battery specified any faster than the normal storage charge loss. Obviously this implies that an absolutely flat battery will not switch the tester on and this may be taken as a very positive indication of the state of the battery under test.

The circuit can be split into three very distinct sections which are the power switch, the dummy load and the voltage detector/display. Each section will be considered separately. Fig. 1 shows the complete circuit diagram.

POWER SWITCH

The purpose of the power switch is to turn off the supply to the main circuit when the unit is not testing a battery. As soon as a battery with a terminal voltage greater than 700



Chris LARE

millivolts is applied to the probe TR1 switches on and thus TR2 also switches hard on allowing the battery current to flow into the rest of the circuit. C1 and C2 provides the main supply decoupling. When TR1 turns off R2 and R3 pull the emitter and base of TR2 very close together so that TR2 is firmly held in a non conducting case with very minute current flow into the main circuit. The measured consumption was considerably less than a microamp. Diode D1 was included to help prevent possible damage if the test battery is connected back to front because although the base-emitter junction of the transistor TR1 will work in this way damage might occur if a 6 volt or larger battery is wrongly connected.

A self test button was included which simply connects the internal battery supply to the test probe input. The voltage selector should be set to 9 volts for any useful conclusions to be drawn from this.

DUMMY LOAD

This type of test equipment usually uses a bank of high wattage resistors to act as the dummy load with the resistor values chosen such that the desired current is drawn for each applied voltage. The main disadvantages of this method are that the resistors are quite bulky and furthermore, should the source voltage fall the current drawn will also fall. In order to avoid these problems a constant current sinking circuit was employed, which will draw 15 milliamps from the source irrespective of the source voltage and so no load switching is required.

A purpose designed integrated circuit, the LM334Z, was used to drive the dummy load sink circuit. In its natural form the LM334Z can only pass a maximum of 10 milliamps and so an external pass transistor (TR3) was used to increase the current handling to the desired 15 milliamps. The LM334Z works by sensing the voltage across R5 which it attempts to maintain at 67.7 millivolts (at 25°C). As the voltage rises across R5 the LM334Z passes less current and thus the base current into TR3 falls, reducing the overall current flow and hence the voltage across R5. In the same way as the voltage across R5 falls so the current flow through TR3 is increased. Since this configuration is essentially a very high gain feedback system C4 and R4 were included to prevent oscillation starting by slightly damping the feedback control. If a full 12 volt battery is tested, TR3 will dissipate 180 milliwatts and so a small heatsink is recommended.

The LM334Z is heat sensitive and as the temperature increases so does any given current flow in exact proportion. The exact figure for this rise is 0.33% per °C and implies that if the temperature rises by 10% the load circuit will draw about 0.5 milliamps more but this is of no real consequence in this application.

THE VOLTAGE DETECTOR/DISPLAY

It was decided that a three state output of 'good', 'poor' and 'flat' would be sufficient. Three l.e.d.s were used, two driven directly from the outputs of a voltage comparator, the other from a couple of transistors to make it light when neither of

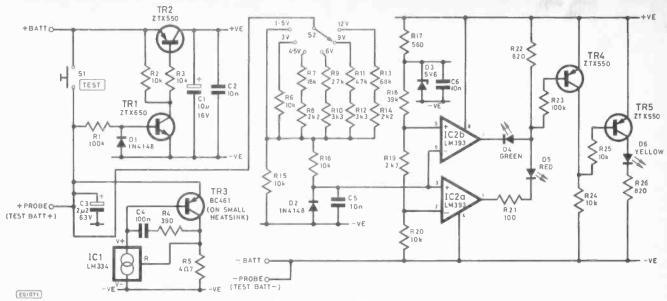


Fig. 1. Circuit of Tester

the other two are on. The basic circuit uses a dual low power open collector comparator in the form of an LM393 which is a cut down version of the well known LM339.

In the design of a circuit such as this where various input voltages are to be compared against a known reference value the reference may be varied and compared with a fixed, reference. The latter approach offers far less problems and was adopted here, where two fixed reference voltages of 1.37 and 1.1 volts were chosen to correspond to a 1.5 volt cell somewhat discharged and totally useless. These voltages were derived from a 5.6 volt Zener diode chosen as being the most stable value available. R17 allows some 6 milliamps to flow through the Zener, the voltage thus generated being decoupled by C6. R18, 19 and 20 form a simple divider chain to produce the required voltages which are fed directly to the two comparators. The probe voltage is passed to S2 which selects the required potential divider to drop the desired test voltage down to 1.5 volts. These dividers are not perfectly accurate but are quite good enough for this application. This method has the advantage that the tolerance allowed on each type of battery increases as the battery voltage increases which is ideal. Table 1 shows the intended threshold levels for each battery. Obviously the 1.5 volt test input is a simple direct connection. The voltage from the common point of the divider is fed to the comparators via R16, which together with D2 gives protection against wrongly connected batteries. C5 simply decreases the impedance seen by the comparators and helps prevent oscillation at the threshold points.

Consider the case where the battery is fully charged up to its rated voltage which is set on the selector switch. The voltage at pin 6 of the comparator will be 1.5 volts which is higher than the 1.37 reference and so the output of that comparator will be driven low which will turn on the green l.e.d. Similarly if the battery under test is nearly flat the voltage on pin 3 of the comparator will be lower than the reference on pin 2 and since the inputs to the comparators are swapped this condition will drive the comparator output low light the red l.e.d. The extra series resistor R21 simply evens up the brightness of the red l.e.d. in comparison with the other two. Both the green and red l.e.d. use the same current limit resistor R22.

When the battery is in the state termed 'poor' the voltage

applied to the comparators will be between 1.1 and 1.37 volts and so neither the green or the red l.e.d. will light and so no voltage will be dropped across R22. This means that TR4 will turn off so that its collector voltage will fall by virtue of R24 with the effect that TR5 switches on lighting the yellow l.e.d. It can thus be seen that one of the l.e.d.s will be on the whole time the tester is switched on.

As stated before the prototype was powered from a PP3. When the unit is in use the current drain of 16 milliamps is larger than that recommended for the PP3 but the actual on time should be so small as to not make this a cause for concern.

CONSTRUCTION

The prototype was housed in a plastic box $120 \times 40 \times 65 \, \text{mm}$. The test probe connections were brought out to two 4mm terminals allowing standard meter prods to be used since the wide variety of available batteries renders the mechanical design of a universal test clip very difficult. The rotary switch was mounted directly onto the printed circuit board and was used to hold the board into the box. It is therefore suggested that the circuit board design shown is used rather than Veroboard (Fig. 5).

Assemble the circuit board first but do not fit the BC461 (TR3) at this stage. When fitting the switch cut off the normal connection loops on the terminals and offer the switch up to the p.c.b. Solder in only two of the pins and check that it is mounted level with the board before soldering the rest of the pins. Solder in the l.e.d.s so that they stand some 11mm away from the board. It is as well to test the board fully before final assembly.

Mark the lid of the box as shown (Fig. 2). The easiest way of marking the voltages on is to mark the centre of the switch and then lightly draw a 27mm diameter circle around

Table 1: Ca	lculate	ed thre	shold	levels	(Volts	3)	
Battery Voltage	1-5	3.0	4.5	6.0	9.0	12	
Flat Threshold	1×1	2.2	3.32	4.44	6.62	8.8	
Poor Threshold	1.37	2.74	4.14	5.5	8.25	10.96	

In actual practice these values will not be attained due to resistor tolerances. Obviously 1% resistors may be used but but this was not considered essential.

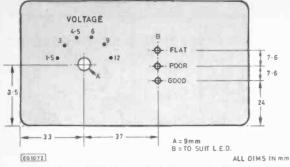


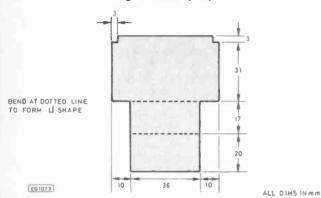
Fig. 2. Details of panel drilling and legending

this point in pencil. Draw arcs on the circle with a pair of compasses set to 6.5mm to correspond to each switch position and mark each intersection with the compass point. Rub out the pencil lines, drill and mark up the lid with Letraset.

Mark up a battery clip out of light gauge aluminium as detailed in Fig. 3, bending it on the dotted lines to form a U.

Adjust the stop position of the rotary switch to the sixth position and assemble the board onto the box lid. A large washer will probably be required to space the shaft slightly. Fit the sockets into the box, together with the test switch and wire to the board. Briefly test the unit again before fitting the lid onto the box.

Fig. 3. Battery clip



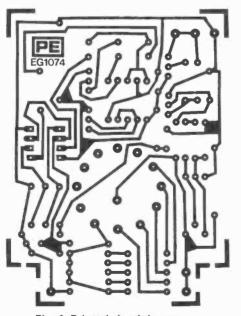
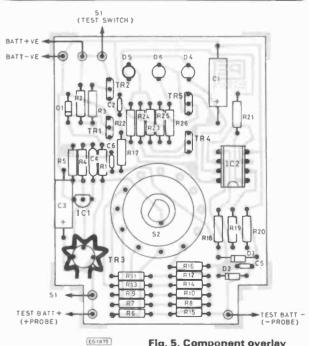
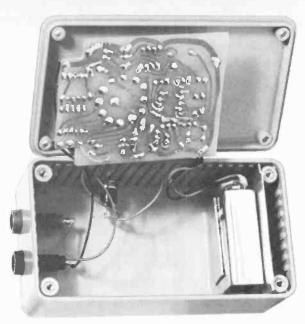


Fig. 4. Printed circuit layout

Compo	nents
Resistors	
R1, 23	100k
R2, 3, 6, 15, 16, 20, 24, 25	10k
R4	390
R5	4R7
R7	18k
R8, 14	2k2
R9	27k
R10, 12	3k3
R11	47k
R13	68k
R17	560
R18	39k
R19	2k7
R21	100
R22, 26	820
All ½ watt 5%	
7 11 4 11 21 2 2	
Capacitors	
C1	10μ 16 volt elect. (or 25 volt)
C2, 5, 6	0.01µ ceramic disc
C3	2μ2 63 volt elect.
C4	0-1μ Mullard C280
Semiconductor	
	10/4140
D1, 2	1N4148 5-6 volt 400mW Zener
D3 D4	Green I.e.d.
	Red I.e.d.
D5 D6	Yellow I.e.d.
TR1	ZTX650
	ZTX550
TR2, 4, 5 TR3	BC461
IC1	LM334Z
IC2	LM393
102	2.1.000
Miscellaneous	
Plastic box 120 x 40 x 6	55, press to make switch,
12 pole single way switch (L	
heatsink clip, PP3 battery, b	
4mm sockets, terminal pins,	



for battery clip, suitable knob, test prods.



Internal layout

TESTING

Apply a 9 volt supply to the board via a battery and measure the current consumption which should be close to zero. Remove the ammeter and press the self test switch. The circuit supply should rise quickly to 9 volts and one of the l.e.d.s should light. If it does not appear to work measure the current consumption which should be less than 20

milliamps with the test switch pressed; a greater current than this will indicate the presence of a short circuit. Wire a 220 ohm pot between battery positive and negative with the wiper connected to the probe input. The voltage selector switch should be set to 1.5 volts. Monitor the wiper voltage which should be initially zero. Slowly increase this voltage and check that the red l.e.d. comes on at 700 millivolts, changes to yellow at 1.1 volts and finally changes to the green l.e.d. at 1.37 volts and above. If this test does not work as intended the voltage reference chain is the most likely source of trouble. Set the switch to 3 volts and slowly increase the voltage again checking the changeover points are close to those in the table.

Now solder in the BC461, having first fitted on the heatsink. Connect an ammeter across the test switch and check that the current flow is around 15 milliamps indicating the correct operation of the dummy load. Finally set the voltage selector to 9 volts and press the test switch whereupon the green l.e.d. should light.

IN USE

It is important to remember that this unit is set up for 1.5 volt cells, and when used on other types of battery, particularly NiCads, erroneous results will be noticed. For NiCad batteries the tester may be modified by slightly altering the resistors in the divider chain, making the 'poor' range much narrower and reducing the base voltage used to 1.2 volts instead of 1.5 volts. Obviously other battery voltages can be tested by simply working out the resistor values in the potential divider e.g. a 15 volt battery would require dividing by 10 to 1.5 volts and so a 100 kilohm divider resistor should be used.

BAZAAR

ATARI games system, plus eleven cartridges, including: adventure, invaders, soccer, chess. Worth over £300, only £180. Mr. M. Ward, 9 St. Andrews Ave., Crewe, Cheshire CW2 6JJ.

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PROGRAMMING Introductory course wanted for free weekend. Details to R. Peace, 24 Mowbray Road, Northallerton.

HEATH kit GR78 receiver, £40. Heath kit scope 10–102, £50. Pye Cambridge R/T, £25. Carr. extra. Edwards, 2 Beach Rd., Burton Bradstock, Bridport, Dorset DT6 RRF. Tel: 0308 897625.

BBC Microcomputer Model 'B'. £100+ worth of software and two books. Cost new £525. Accept £325. Mr. M. Clark, Jardinet, Oakland Park, Falmouth, Cornwall.

TANDY Quick Printer 2, recently overhauled by Tandy, + 3 rolls of paper, £75, including postage. Ian Benton, The Pharmacy, Bardney, Lincoln LN3 5SS. Phone: Bardney (0526) 398208.

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UK101 Enhanced 8K cased plus software. 1/2MHz. 300, 600, 4000, Baud. Tape handler, ROM. £150 o.n.o. D. Lund, 25 Hillcrest Ave., Longridge, Nr. Preston, Lancs. Tel: (077 478) 4517.

BINATONE 5-star 40 channel mobile 27MHz CB transceiver. 4 watts. New. Japan made. £50-00. K. Y. Chang, 041 332 7695, after 7 p.m. K. Y. Chang, 70 1-up Ashley St., Glasgow G3 6HW.

FOR Compukit—RAM/EPROM board + 4K RAM, £30; toolkit, £5; BASIC 5, £10; Motherboard, £5. Mr. N. Odell, 31 Humphrey Rd., Greenhill, Sheffield S8 7SE. Tel: (0742) 745027. PRINTER and keyboard on pedestal (Terminet) 80 col U/L case 30 CPS RS232. Ex. condition, £100. Tel: (evenings) 0744 88 3918.

ZX Spectrum 16K, £75, new. L.C.D. Multimeter, £28; clearing out equipment and projects, s.a.e. No callers. D. Martin, 6 Downland Gardens, Tatenham Comer. Ensom. Surrey.

TELEQUIPMENT Oscilloscope type D43
B/Beam, has anyone any workshop or service information, circuit etc. for sale? John Mitchell, 8
Rutland St., Gorton, Manchester M18 8QH. Tel:
061-231 6522

ADVANCE type H1 a.f. signal generator 15Hz-50kHz Sine/square perfect £35 o.n.o. Newnes Radio/TV service manuals 1949–1961 £20 o.n.o. E. G. Jones, 16 Riverway, Nailsea, Avon BS19 1HZ. Tel: 0272 853747.

ACORN Atom 12K RAM 12K ROM all leads p.s.u. and manual included hardly used £140. Dave Houghton, 2 Western Villas, Church Road, Kennington, Ashford, Kent TN24 90G. Tel: 0233

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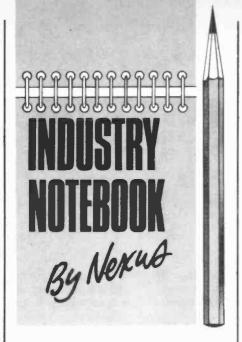


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Inscrutable

China has nearly one quarter of the world's population and is the largest single market as yet untapped by Western technology. The inscrutable oriental of legend is becoming less so but only very gradually, almost reluctantly. The door to large scale international trade is only slowly opening but with it could come a much better appreciation of what China is about.

Apart from the enormous population, other statistics on China are monumental. Her total borderline if we include the coastline extends to 22,000 miles of which her border with the Soviet Union accounts for 4,300 miles. China's main preoccupation in recent years has been fear of Soviet intentions, reciprocated by the Soviets. Earlier friendly relations evaporated in 1966 when Chairman Mao instigated the Cultural Revolution to maintain the purity of the communist ideal which not only rejected the ideology of capitalism but also Soviet communism which, in Mao's view, had become 'revisionist'.

The distrust between the two communist giants resulted in another staggering statistic, the largest standing army in the world with 4-75 million under arms. The land force consists of 169 divisions in 35 armies. Eleven armoured divisions have 10,000 tanks. At sea there are 32 destroyers and frigates, 102 submarines and about 1,000 smaller naval craft. The air arm has 5,000 combat aircraft. And China's nuclear arsenal now includes 5,000 mile range ICBMs with 3-megaton warheads.

The trouble is that, formidable as the Chinese strength appears to be on paper, most of the equipment is as much as 20 years out of date having depended on Soviet technology initially and, later on, copies made in China. Similarly, industrial production suffered during the period of ideological re-education. The present leadership group appears intent on modernisation in the armed forces and in industry,

even though it involves the capitalist countries.

The Chinese trade delegation visiting Britain and Europe in 1980 in search of modern arms were fascinated by developments like the Harrier aircraft but were horrified at the cost. But they could perhaps afford some of the sophisticated electronics to transform existing weapons platforms into efficient defence equipment.

The first fruits of turning to Britain (at least so far reported) are the re-fitting of two Luda class destroyers, themselves derived from the Soviet Kotlin class. They are being re-equipped with Sea Dart missiles, radar, fire control systems and new operations rooms under a £100 million contract. As China has nine of this class of destroyer there should be the possibility of follow-on orders.

Last January, Industry Minister Patrick Jenkin was in Peking attempting to sell British nuclear technology which could result in power station orders worth several hundred million. On a smaller scale Solartron's trade with China in measuring and analysis equipment topped £1 million last year.

There remains the riddle of Hong Kong and the New Territories which are due to be returned to China by treaty in 1997. The prospect of an earlier date caused consternation in Hong Kong last year but confidence was restored by rumours that while Hong Kong would certainly return to China it would have a special status. Indeed it should when tiny Hong Kong exports more goods than the whole of China and would therefore seem invaluable if orthy as a profitable interface with the outside world.

The Chinese trade door may be inching open but also in the queue outside are the other European nations, the United States and Japan, all competing. Lurking in the background is the possibility of the inscrutable Chinese mending fences with the Soviet Union in which case the West may have been wasting its time.

Looking West

As well as looking East, British maufacturers are also looking West, particularly to the United States. Plessey, following a £34 million purchase of Stromberg-Carlson last year, started the New Year with joint ventures with Scientific Atlanta on cable-TV and Rockwell International on military radio. These new associations give Plessey a foot-hold in the US market for telephone exchanges, a technology foot-hold in the UK for cable-TV and a US marketing foothold in the USA for selling the US Army the single channel radio access equipment used in the Ptarmigan radio system developed for the British army.

Racal is also taking on board US technology for future Pay-TV and Cellular Radio projects besides having flourishing wholly-owned subsidiaries in the United States. I note with some amusement that when 10 members of the Italian Parliament recently visited the United States on a trade mission to examine the best electronic manufacturing facilities, high on the list was Racal-Milgo, wholly British owned.

This company, incidentally, rated top in price/performance ratio, top in technology and in the first three on service organisation and trade literature by the 1982 Brand Preference Survey. Overall it won the honour of being 'the one most preferred to do business with'.

Another Racal company in the US is Racal-Dana Instruments. They have just invested in a new 100,000 sq.ft headquarters in East Irvine Industrial Park, near Los Angeles.

Some companies are looking the other way. Philips, for example, is reported to be one of the firms tendering to set up a colour-TV factory in the Soviet Union. They are in competition with Japanese companies. It seems strange that the Russians are so patchy in performace. After all these years they still appear to be incapable of performing routine mass-production tasks like making motor cars without assistance from outside. And what happened to the Hungarian and Polish electronic industries? Surely they could provide the goods?

Inmos

The months and years slip away as do the millions in Inmos, the British semiconductor outfit. Taxpayer investment is already approaching £100 million if, indeed, the figure hasn't already been exceeded. And the 4,000 jobs promised will probably never be achieved. I have always been sceptical on politically motivated investment. If a product is worthwhile then private capital will automatically be attracted to it. I still wish Inmos well but I wish they could have done a lot better. The grant of a further £15 million may yet save the company but it now looks to be an awful long time before the total investment gets repaid.

Telecoms

In contrast we have the recently privatised Cable & Wireless. Lucky those who bought in at the offered price of 168p in October 1981. Those who held on have doubled their money with further growth in prospect. Booming profits have not only benefited shareholders. Swan Hunter Shipbuilders and their workforce on the Tyne have won an £18 million order for a new C & W cable ship. It will provide work for 800 men over a period of 18 months.

And how about British Telecom itself! Best ever profits leading to a freeze in prices for a further few months. Of course we can argue that the call charges were too high in the first place. Never mind! The prospect of competing in a real instead of captive market has done the trick. BT is really trying harder and will, I believe do better.

Fly Smiths

Next time you fly in a Boeing remember you are also flying Smiths Industries. Their electronic auto-throttle system is on all 727s and 737s together with a host of other flight deck instruments. The Smiths auto throttle (100 more sets have just been ordered) saves fuel on all regimes of flight from take-off to landing.

Part 1 SOUND SYNTHESIS BOARD

DIGIT TALKER

THE transmission of speech stimulated the start of the electronics industry. It has, however, taken over 100 years to develop a machine which will economically reproduce the complexity of the human voice.

Until recently, all sound reproduction has been based on electro-mechanical systems centred around plastic discs or magnetic tape. Such systems are generally bulky, delicate and expensive, and can only be used in a limited number of environments. There are, however, a large number of applications, especially in instrumentation, where an operator is not able to look at an instrument panel but needs to know immediately the results of his action, and in what way to correct them. Such applications are found in Motoronics, Avionics and Mechatronics. In effect, the requirement is for a speak-out unit, as opposed to a read-out unit, and it was to this end that the Warwick Design Group produced their Voice Synthesis Board.

Many ways of reproducing speech digitally have been suggested. The simplest of these is to convert the analogue speech signal to a linear digital form. As the maximum bandwidth of speech is around 4kHz, a minimum sample rate of 8kHz is needed. If a 12 bit analogue to digital converter is used this technique would take up memory at a rate of 96,000 bits per second.

A. Wiggin

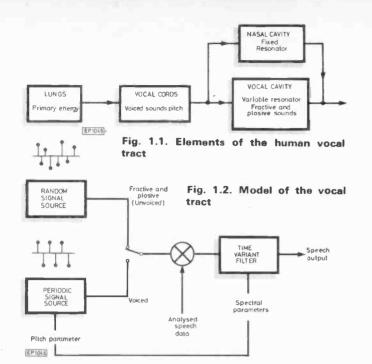
A method for reducing this astonishing amount of memory is to sample the analogue signal at 8kHz but, instead of measuring the absolute value at each step, simply record whether or not the signal is increasing or decreasing. This can be done with just one bit, thus reducing the memory required to 8000 bits per second, without significantly reducing the quality of the speech output.

A more radical approach to the problem is to use a microprocessor to act in the same way as a human voice. This means that the action of each part of the vocal tract has to be analysed and turned into an algorithm which can be programmed into the microprocessor. Such an algorithm is shown in Fig. 1.1. It consists of the lungs which provide the basic energy, the vocal cords, the mouth and the nasal cavities. Sound generated by the vocal cords is modulated by the mouth, the movements of the jaws, the tongue and the lips. The whole combination can be considered as a time variant filter, whereby the nasal cavity acts as a fixed frequency resonator. Another useful feature of the human voice is that the muscles cannot react faster than 20 to 25 milliseconds. Hence speech can be split up into 20 millisecond envelopes. This characteristic can be used to great advantage when trying to condense the amount of memory.

Sounds are produced by the vocal system in three ways. Voiced sounds are generated by tensing the vocal cords which forces them to vibrate as air is expelled from the lungs. An example of a voiced sound is 'ee' in the word 'speech'. Secondly, fricative sounds are generated by air from the lungs rushing past a constriction such as the teeth or lips. The sound 's' at the beginning of the word 'speech' is a fricative. Finally, plosive sounds are generated by a total obstruction of the mouth cavity by either the tongue or the lips. Air pressure is built up and then suddenly released. The word 'pop' begins and ends with a plosive.

COMPUTER ALGORITHM

These elements of a human voice can be built into a computer by using this algorithm. Fig. 1.2 shows a system which comprises a random signal source and a periodic signal source. The former is used to generate the fricative and plosive sounds and the latter the voiced sounds. Either one of these can be selected to drive the time variant filter which simulates the action of the lips, the tongue and the jaw movements. The algorithm assumes that there is complete independence between the source and the filter and that only one of the sources is being used at any given time. In all, 13 parameters are needed to drive the algorithm, but due to the reaction time of the muscles, they only need to be updated 50 times a second. Hence, if a 10-bit analogue-to-



digital converter is used, only 6000 bits are needed to synthesise one second of speech.

Further economies can be achieved by quantitising some of the algorithm parameters such as pitch and amplitude into a set number of values. The periods of silence which occur between syllables need not be recorded, only their duration. In many cases, syllables and phrases repeat and therefore they can be referred to by the computer time and time again. By using all these techniques it is possible to reduce the data needed for the successful synthesis of speech to as low as 1,100 bits per second.

Linear Predictive Coding (LPC), as it is known, is the most efficient means of synthesising the human voice using digital techniques. A maximum of 49 bits are needed to update the 13 parameters of the algorithm every 20 milliseconds. They can be split up as follows:

Energy (amplitude)	4 bits
2) Repeat	1 bit
3) Pitch (frequency)	5 bits
4) The ten reflection coefficients	
K1 and K2	5 bits
K3-K7	4 bits
K8-K10	3 bits

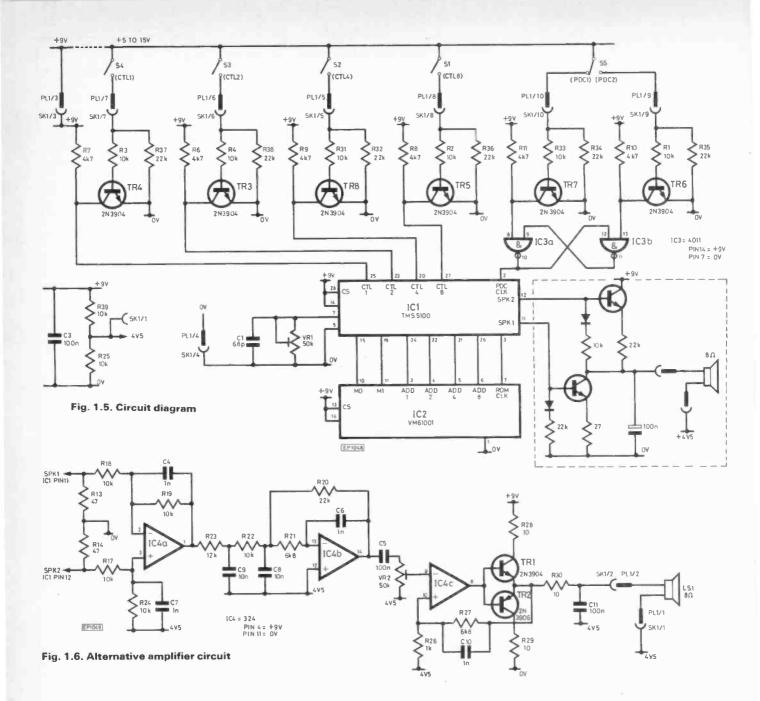
Fig. 1.3 shows how the word "HELP" is synthesised using the LPC algorithm.

	E 0000	R	Р	K1	К2	К3	K4	К5	K6	К7	К8	К9	K10	FRAME TYPE SILENCE
	0100	0		10011	01110	1001	0111							UV
	0111	1	00000											UV-REPEAT
	1101	0	10010	10000	10100	1000	0110	0111	1000	1010	100	101	010	V
	1101	1	10011											V-REPEAT
	1110	1	10011											V-REPEAT
1121	1101	0	10100			1010	1010	1001	0111	1000	100	101	101	V
HEL	1101	0	10100			1000	1100	1101	1000	0100	100	011	101	V
	1101	0		10001	01010	0110	1001	1111	1011	0101	010	000	110	V
	1011	1	11010											V-REPEAT
	1010	0	10010	01101	00111	1000	1100	1111	0111	0010	001	010	110	V
	1001	1	10001											V-REPEAT
	1001	1	01110											V-REPEAT
	1000	1	01101											V-REPEAT
	0010	0	01110	00101	00101	1 1 0 1	1001	1110	0101	0111	001	011	011	V
	0000													SILENCE
	0000													SILENCE
	, 0000													SILENCE
	0111	0	00000			1011	1000							UV
_	0111	0	00000	10001	01011	1011	0110							UV
Р	0101	1	00000											UV-REPEAT
	0011	0		10011		1010	0110							UV
	0010	0	00000	10010	00101	1011	0101							UV
	0000													SILENCE
	1111													STOP CODE
	V-VOICE													
	UV-UNV	OICE	D		F:	40				5.11				
					Fig.	1.3. L.I	C. for	the wor	dHEL	Ρ				

INSTRUCTION NAME			P11 2	TOGGLES OF PDC		
Reset	0	Ū	0	0	1	
Load address	0	0	1	0	2	
Read & branch	1	1	0	0	1	
Test talk	_ 1	1	1	0	3	
Read bit	1	0	0	0	1	
Speak	1	0	1	0	1	
Output	0	1	0	0	3	

Fig. 1.4. Instruction set for the TMS5100

As there are a considerable number of applications for machines with a voice, several companies have developed microprocessor systems to run nothing but the LPC algorithm. Amongst these companies is Texas Instruments, which has developed a dedicated microprocessor, based on their TMS 1100 device. The TMS 5100 Voice Synthesis Processor generates human speech by digitally processing data stored in a non-volatile 128K bit ROM. It has its own Digital-to-Analogue converter and audio push-pull amplifier. The amount of external programming needed to drive the processor has been reduced to a minimum. The seven instructions shown in Fig. 1.4 are loaded into the device on 4 control lines and 1 clock line.



CIRCUIT DESCRIPTION

The circuit shown in Fig. 1.5 can either be driven by a microcomputer or by manual switches. If the latter is used, care must be taken to debounce the PDC switch. Processor timing is provided by a RC network connected to pin 7 of the TMS 5100. When adjusted it will produce a frequency of 640kHz. This is divided down to give the CPU clock of 320kHz and the ROM clock of 160kHz. Three power rails are needed to run the system. The processor uses a 0 to 9 volt rail, whereas an intermediate voltage of 4.5 volts is needed for the audio output stage. The TMS 5100 loads an address to the VM 61001 by means of the M1 control output and the ADD bus. As the PDC is brought high during the address portion of a load address sequence, the TMS 5100 brings M1 high and gates the CTL bus to the ADD bus. When the PDC is brought low, M1 goes low and the TMS 5100 stores the nibble in its address register. Data is transferred from the ROM to the TMS 5100 in a serial form over the ADD 8 line. Toggling MO instructs the ROM to transfer the next bit. As the PDC is brought high during the Read instruction, the TMS 5100 toggles MO and accepts the new bit into its four bit buffer over the ADD 8 line. The first MO after a load address sequence changes the direction of the bi-directional ADD 8 line from transmit to receive.

The audio stage of the TMS 5100 shown in Fig. 1.5 has been optimised for high production runs. An alternative circuit is shown in Fig. 1.6. This circuit significantly improves the quality of the output and consists of a differential amplifier and integrator followed by a low pass filter. The gain of the circuit is controlled by VR2, which in turn drives a non-inverting amplifier and push-pull output stage.

PROGRAMMING

There are two ways in which the system can be operated. Direct Addressing: The start address of the speech data held in the ROM (Fig. 1.7) is toggled into the TMS 5100 via the

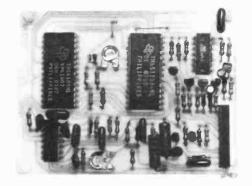
LPC VOCABULARY DATA IN VM61001 (MALE SPEAKER NO. 6)

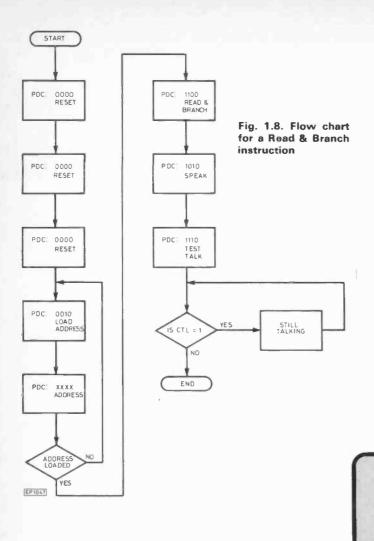
WORD												
Decoration Color												
NNE												-
TWO												
THREE				1			1					
FUIR ODOIG O.255 KILO O.070							1					
FIVE												
SIX ODDE O.360 MIKE O.74 I.DBF LINE ODDA 2133 GET OL140 3145				KILO	0070	100C	TIMER	0006	205B	GAGE	013C	30 FC
SEVEN 0010 0.390 NOVEMBER 0075 1001 MACHINE 000C 2180 C0	1		0313	LIMA	0072	1063	VALVE	8000	20A1	GATE	013E	316A
EIGHT 0012				MIKE	0074	108F	LINE	OODA	2133	GET	0140	31A5
NINE					0076	1001	MACHINE	0000	21B0	GO	0142	31E0
TEN	EIGHT	0012	03F3	OSCAR	0078	1138	UP	000E	2236	GREEN	0144	3233
LEVEN				PAPA	007A	1190	00WN	00E0	226A	HIGH	0146	3270
TWELVE					007C	1105	OFF	00E2	22C4	HOLD	0148	32CC
THIR-		0018	049E	ROMEO	007E	1216	ON	00E4	2308	INCH	014A	333D
FIF.	TWELVE	001A	0504	SIERRA	0800	126D	IS	00 E 6	2362	INSPECTOR	014C	3375
TEEN	THIR-	001C	0556	TANGO	0082	12C4	NUMBER	00E8	239E	INTRUDER	014E	3 3 DF
TWENTY	FIF:	00 1 E	057E	UNIFORM	0084	131B	TIME	ODEA	240E	LEFT	0150	3440
HUNDRED	-TEEN	0020	05A8	VICTOR	0086	1377	CONTROL	OOEC	2458	LOW	0152	3460
THOUSAND OD26	TWENTY	0022	05D4	WHI S KEY	0088	13C3	ALERT	OOEE	24BC	MANUAL	0154	34C1
A	HUNORED	0024	0619	X-RAY	A800	13FB	OUT	00F0	2523	MEASURE	0156	3534
B	THOUSAND	0026	0692	YANKEE	0080	1453	AUTOMATIC	00F2	255E	MILL	0158	3596
C	Α	0028	070F	ZULU	008E	14A2	ELECTRICIAN	00F4	25C0	MOTOR	015A	3500
D	В	002A	074D	AND	0090	14E6	ADJUST	00F6	2632	MOVE	015C	3635
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I			0783	WATTS	009A	1686	BREAK	0100	2792	PASS	0166	37D5
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Fig. 1.7. Vocabulary for the VSB

control lines. As 18 bits are needed to address one location in a memory of this size, and there are only 4 control lines, then 5 nibbles of 4 bits are used. Each nibble is preceded by a load instruction. After all 5 nibbles have been loaded a 'Read Bit' instruction is toggled into the processor. This instruction reverses the bi-directional memory bus and when a 'Speak' instruction is toggled in, data is transferred from the ROM to the TMS 5100. This data is then processed and fed to the audio output via the 10 bit digital to analogue converter.

Indirect Addressing: The second method is to use an indirect 'Read and Branch' instruction. Fig. 1.8 shows the flow chart for this instruction. At the bottom of the ROM there is a look-up table which holds all the start addresses of all the words held in the memory. If the 'Read and Branch' instruction is used the address of the look-up table which holds the





some typical speech scenarios

burglar alarms

RED ALERT. INTRUDER AREA ONE.

video games

RANGE: TWO THOUSAND FEET.
DIRECTION: THIRTY-NINE DEGREES
EAST.
ALPHA BRAVO TO (use TWO) WHISKEY
FOXTROT.

FOXTROT.
POSITION SAFE.
MOVE FAST.

personnel security

STOP. DOOR IS AUTOMATIC.
INSERT PASS.
PRESS ENTER BUTTON ON RIGHT.
WAIT TEN SECONDS. CHECK NOT
COMPLETE.
CAUTION.
FAIL. PASS NUMBER IS NOT O K.
CALL MANUAL INSPECTOR.
CANCEL PASS. ABORT CYCLE.

safety

GET SERVICE UNIT.

DANGER: TEN THOUSAND VOLTS.

LINE VALVE PRESSURE HIGH.

GET ELECTRICIAN.

REPEAT TEST ON TIMER SWITCH.

COMPONENTS ...

Resistors

R1-4, R17, R18, R19, R22, R24, R31, R33 10k (11 off) R6, R7, R8, R9, R10, R11 47 (6 off) R13, R14 47 (2 off) R23 12k R20, R32, R34, R35, R36, R37, R38 22k (7 off) R21, R27 6k8 (2 off)

R26 1k R28, R29, R30 $10\frac{1}{2}$ W (3 off) All resistors $\frac{1}{4}$ W 5% unless otherwise stated

Potentiometers

VR1, VR2 50k (2 off)

Capacitors

C5, C3, C11 100n (3 off) C1 68p C4, C7, C6, C10 1n (4 off) C9, C8 10n (2 off)

Integrated Circuits

IC1 TMS 5100 IC2 VM 61001 IC3 4011 IC4 324

Transistors

TR1, TR3–TR8 2N3904 (7 off) TR2 2N3906

Miscellaneous

8 ohm loudspeaker

10-way printed circuit connector

Constructor's Note

The TMS 5100 is available from the **Warwick Design Group** at £14, the VM61001 at £16, the printed circuit board £5. A full kit of components is available for £37 from the Warwick Design Group, 12 St. George's Road, Leamington Spa CV31 3AY.

starting address of the required word is first toggled into the TMS 5100 via the CTL lines. A 'Read and Branch' instruction is then executed, and on receiving a 'Speak' instruction, the audio output is activated.

CONCLUSIONS

The voice synthesis board described above can be used as a basic building block in many different applications. It

can be interfaced directly to a microcomputer or used to enhance an existing instrument such as a digital voltmeter, frequency meter, digital clock, or CB radio read out.

NEXT MONTH: A method for interfacing the voice synthesis board with a 3 digit, 7 segment display will be described.

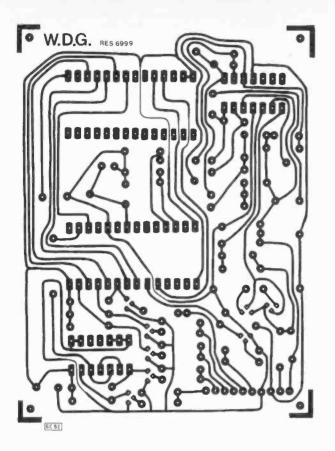
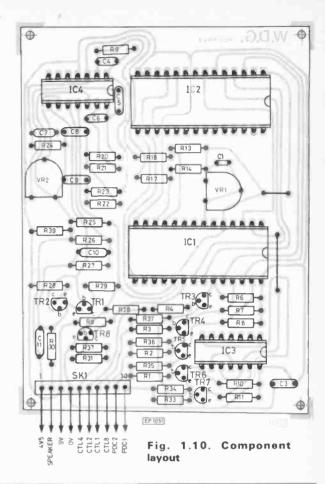


Fig. 1.9. Printed circuit board



BAZAAR

WANTED Buy or borrow, handbook manual for Ferrograph series Four, also require bulk tape eraser. Robert Du Pontet, 55 Staplegrove Road, Taunton. Tel: (0823) 72909.

WANTED Circuit or manual for miniature oscilloscope type CT52. Buy or borrow. W. D. Goodwin, 1 Long Meadow, Natland, Kendal, Cumbria LA9 7 OZ.

ACORN Atom fully expanded TV monitor, cassette recorder, p.s.u., tool kit, ROM, 36 software tapes inclusive, £220-00. Mr. R. W. Hearn, 10 Speedwell Close, Pakefield, Lowestoft, Suffolk NR33 7DU. Tel: Lowestoft 66026.

MAPLIN matines organ for sale, complete and working. £370. Tel: 01-578 5448 (Greenford). D. J. Comber, 66 Chinnor Cres., Greenford, Middx. UB6 9NX.

UK101 32 x 48 12K BASIC 16K RAM Motherhood, EPROMS + Programmer sound & MHz 3/600B software, £280 o.n.o. N. Brooks, 103 Drake Rd., Harrow, Middlesex HA2 9DZ. Tel: 01-868 9524.

WANTED, to buy or borrow, handbook for telequipment oscilloscope type D56. G. V. B. Russell, North Yeo, Instow, Bideford, Devon EX39 4JJ. Tel: (0271) 860570.

ZX81 32K with "Fuller" keyboard, p.s.u. and case. 3-D maze game. Three books, Sinclair manual, £100. M. Bond, 2 The Grange, Eastbourne Road, South Godstone, Surrey RH9 8JQ. Tel: 034-285 3168.

CASIO FX702-P pocket computer with printer, cassette interface and 5 rolls of paper. £115 o.n.o. S. J. Riddle, 51 Marshalswick Lane, St. Albans, Herts. AL1 4UT. Tel: (0727) 53946.

WANTED Cosser type 23D cathode ray tube. A. F. E. Riley, 1 Boulton Sq., West 8romwich, Staffs.

LOGIC cards: 6 FND800 displays and CD4511, £3-00. PSU +5/-12 with power-on reset, £6-00, p.p. extra. Norman Simons, 187 Ladbroke Gr., London W10. Tel: 01-969 6150.

MARSHALL 100 watt amp transistorised, lead good condition. £100 o.n.o. Mr. A. C. Clews, 5 Hedgerow Dr., Kingswinford, West Midlands DY6 7SA. Tel: 271404 (0384).

PHILIPS 1700 V.C.R. with tapes, faulty head, £80. Buyer collects, Cash please. J. Gray, 9 New Road, Hextable, Swanley, Kent BR8 7LS. Tel: Swanley 64486.

WANTED circuit diagram of ZX80. Will pay photostating, postage etc. Robert Forsyth, 45 Cyclamen Road, Swanley, Kent BR8 8HH. Tel: Swanley 64394 after 6pm.

UK101 8K, Cegmon, new Basics, 1,3,4,16/32 x48 screen, cased, PE extension boards (No i.c.'s) £80 o.n.o. Somerton 72663 evenings.

6 VOLUMES Radio TV servicing 1968 to 1974 mint condition £14.50 carriage extra, weight 18lbs. D. Clark, 2 Eriskay Avenue, Hamilton, Strathclyde, Scotland. Tel: Hamilton 421757.

UK101 plus 610bd. 32K RAM 2 x Mini Disk drives, SEK 65D 3-3 DOS, Link 65 Cegmon b/w monitor £450 o.n.o. Stuart Higgins, 138 Lower Farnham Road, Aldershot, Hants. Tel: Ald 28796.

UK101 8K-32L cased Cegmon resident Basics 1,2,3,4,5, T/KIT II, Codekit + cassettes Assembler, Forth, Exmon, games £200. p/exch? Tel: 0252 546739, Farnborough, Hants.

WANTED Reasonably priced synthesised short-wave receiver, also spool type VRT. Write first: 16 Rosalind House, Stanway St., London N1 RR

2 x 5 Octave keyboard 2 x 5 Octave PC/B key swirch assemblies, 2 x foot controls S/L reverb unit, unused, £80. F. L. Mebhurst, 168 Maesglas Cres., Newport, Gwent NPT 3DA.

TWO ±15V power supplies complete, uncased, £10 ea. Four RC4195 ±15V regulators, £3 ea. Paul Blackburn, 33 St. Annes Rd., New Marske, Redcar, Cleveland. Tel: Redcar 485127.

MCNO DX TV for sale, pro. conversion, isolated chassis, all bands, video/audio in/out, £25 o.n.o. Mr. A. Bouskill, 129 Lyminster Rd., Sheffield, S. Yorks S6 1HY. Tel: 0742 311191.

WANTED Good quality Gould oscilloscope, double beam, 10MHz min. or similar. Must have good triggering. Anthony Collins, 34 Lock Assynt, East Kilbride, Glasgow G7H 20W.

SOLDERING iron, Weller TCP 24V/48W (needs transformer to use), plus bench stand, Unused present, £15 including postage. Tel: Oxford (0865) 779855.

WANTED circuit diagram of ZX80. Will pay photostating, postage etc. Robert Forsyth, 45 Cyclamen Road, Swanley, Kent. BR8 8HH. Tel: Swanley 64394 after 6pm.

UK101 8K, Cegmon, new Basics, 1,3,4,16/32 x 48 screen, cased, PE extension boærds (No i.c.'s) £80 o.n.o. Somerton 72663.

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C Patents Review

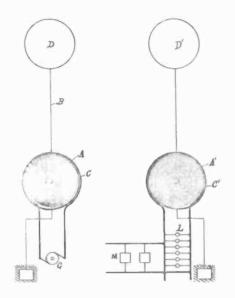
Copies of Patents can be obtained from: the Patents Office Sales, St. Mary Cray, Orpington, Kent. Price £1.60 each.

BACK TO TESLA

Something *old* for a change. There's been a lot of interest recently in the life and work of Nikola Tesla, largely due to the publication of a new biography. Tesla's American patent, number 645576 of March 1900, is well worth a read, even today. You can read it on micro film at the Science Reference Library, attached to the British Patent Office, in Chancery Lane, or you can buy a photo copy made from micro film for around £1.

Tesla's patent, entitled 'System of transmission of electrical energy' was filed in 1897. At first sight it may look like a reinvention of Marconi's first ideas for radio. But Tesla wasn't talking about the transmission of low-powered message signals, he was proposing the transmission of electric power in bulk over long distances, without wires. 'I contemplate employing my invention on an industrial scale', he wrote 'for lighting distant cities or districts from places where power is obtainable'. Was he a hundred years ahead of his time, or a fool?

In the drawing the transmitter is a transformer with a primary C and a secondary A. The secondary is wound from thin wire and connected to a steel cable B suspended high in the air by baloon D. In-



Mikola Tesla

termittent power is input from source G, for instance a capacitor.

The receiver is of similar construction. with lamps L as the load. Tesla built a small scale model and claimed that he could transmit power from one unit to the other in a vacuum environment with a potential of around 4 million volts. 'It was easy under these conditions', he wrote in the patent, to transmit with fair economy considerable amounts of energy. He claimed that by cranking the voltage up to about 50 million volts, with a secondary 50 miles in length, and suspended aerials 35,000 feet above sea level, it would be possible to transmit 'many thousands of horse power --- many hundreds and even thousands of miles'. The system, he said, could also be used to transmit messages. Another idea was to manufacture materials like nitric acid and fertilisers, from gases occurring naturally in the upper atmosphere.

Tesla was at pains in the patent not to claim the apparatus, just the method of transmitting electrical energy through the upper air strata. Reports, perhaps not as crazy as they at first sound, suggest that the Russians may have recently been putting Tesla's patent theories to the test using modern technology.

SPEAKER IMPROVEMENTS

Celestion, the Ipswich loudspeaker manufacturers, have received considerable critical acclaim for their SL6 unit. The company have been cagey about giving technical details on fine points of construction, but their patent applications are now being published.

European patent application 0065882 covers the HF tweeter dome which is an important factor in the sound of the SL6. Conventionally radiating domes have been made out of impregnated cloth, plastics or metals like aluminium or titanium. The snag has been poor heat dissipation. When the speaker is playing loud music, especially pop with synthesizers in the orchestration, there is a considerable amount of high frequency energy to be reproduced. The drive coil heats up and may burn out. Cooling fluids have been used as a heat sink. Now Celestion have killed two birds with one stone by making the dome radiator serve as its own heat sink.

The patent lists a wide range of possibilities, but essentially the dome is for-

med from one or two layers of a metal which is a good heat conductor. Although silver and gold are usable, they are too expensive, so copper is chosen in practice. The dome is less than 1mm thick, and formed by metal deposition, for instance in a vacuum or by RF sputtering. If acoustic damping is needed, the dome can be formed from two layers of metal separated by

a filler layer of plastics or rubber. It can also be protected by a very thin coating of non-metallic material.

Celestion has also filed a European patent application, number 0065883, on a different way of securing a ring radiator to its clamps, so that the unit doesn't fall apart when driven at high power. Fig. 1 shows the conventional way of securing a diaphragm 10 between ring clamps 12. The drive coil 16 is wound on tubular former 14 and secured to the apex of the diaphragm at butt joint 18, by glue. Because the area of adhesive contact is so small, the joint is liable to fail under load.

To overcome this Celestion makes the diaphragm in two halves, one half also serving as the former for the drive coil. Fig. 2 shows one half of the diaphragm 22 with an angled tongue 22C at the end. The other half of the diaphragm 24 has a large flange 24C which serves as the former for coil 28. The two halves of the diaphragm are glued together at the tongue 22C, so there is a much larger area of adhesive contact and less likelihood of failure under load.

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	280ACPU 3.45	2716 350ns	5516 250ns 9.38	Device Price 32	2716 3 rail 1.00 2732 1.40
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Michael Tooley B.A. David Whitfield M.A. M.Sc.

WINDSCREEN wipers have featured on modern motor vehicles since their earliest days. At first, drivers considered themselves lucky to have even a single electrically-driven wiper blade, usually running at a fixed speed, and requiring manual parking when no longer required. With the passage of time, improvements in the form of twin-bladed wipers, switched speeds, self parking and intermittent wash/wipe facilities have been introduced. Although considered by some to have detracted from the 'character' of the earlier cars, these changes have undoubtedly been of significant benefit to the motorist at large. Typically now even the basic models feature two-speed self-parking twin front wipers, usually with intermittent wash/wipe facilities, as standard equipment.

The advent of the popular hatchback style has seen the introduction of tailgate wash/wipe on many cars. The normal arrangement is to provide a single-bladed, slower-running wiper running at a fixed speed with self-parking, and in many respects this is often adequate. There are situations, however, in typically English periods of wet weather when the rain, although continuous, is not really heavy enough for the rate of wipe provided. This can lead to the driver continuously switching the wiper on and off, which is both distracting and tiresome. The alternative is a wiper which tends to 'drag' across the rear screen surface, resulting in a screen which is more smeared than wiped; the noise in itself is often as distracting as the reduced visibility is hazardous.

The unit to be described will provide a variable speed control for a rear screen wiper to help overcome some of the problems described above. It uses a small number of low cost components, and can be fitted with the minimum of rearrangement to the existing vehicle wiring. When installed, the unit can be used to select any rate of wipe between once every minute and the maximum of the rate fitted as standard. The existing wiper controls are retained, allowing drivers unused to the additional facilities to drive as normal.

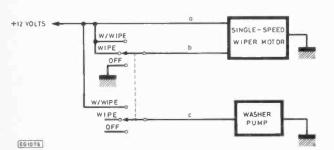
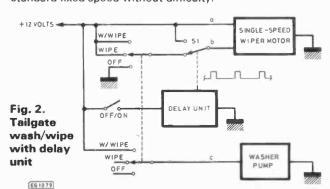


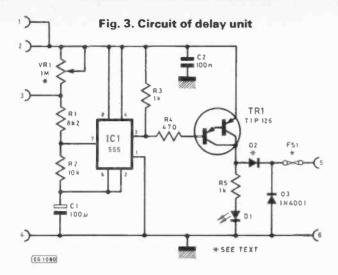
Fig. 1. Conventional tailgate wash/wipe circuit

CONSIDERATIONS

A typical tailgate wash/wipe circuit is shown in Fig. 1 with the controls set in the 'wipe' position. The +12V lead labelled 'a' is permanently connected to the wiper motor, and provides power for self parking when the driver moves the control from 'wipe' to 'off'. The motor housing itself contains another switch which disconnects the winding from lead 'a' when it reaches the parked position. Lead 'b' is connected to ground in the 'off' position to help prevent the motor overshooting the parking position (thereby starting another wipe cycle) by collapsing the motor field when 'a' becomes disconnected. In the 'wipe' position, 'b' ensures that the motor continues turning through the parking position, thereby producing continuous operation of the wipers. Internally within the motor, 'a' and 'b' are both connected via a diode and a rotating switch arrangement to one end of the motor winding, while the other end is permanently grounded.

One consideration in producing a wiper delay unit is that, although intended to be used when the normal wiper control is set to 'off', it should not interfere with the wiper if used when the control is set to 'wipe'. The basic principles of the unit to be described are shown in Fig. 2. The delay unit, when switched on, produces a continuous stream of pulses to drive switch S1. The duration of each pulse is chosen to be long enough to 'kick' the wiper out of its parked position, but not so long as to exceed one complete wipe cycle (which on a small hatchback is typically just under two seconds). Varying the interval between these pulses then gives the method of varying the rate of wiping. The unit described allows variation from one wipe every minute, up to the maximum rate supplied of approximately 30 to 40 wipes per minute. As can be seen from the schematic in Fig. 2, if both the delay unit and the normal wiper controls are both switched 'on', the wiper will operate continuously at the standard fixed speed without difficulty.





CIRCUIT

The wiper delay unit is designed around a general purpose circuit board which may be readily adapted for use with a wide variety of wiper configurations. The circuit diagram for this basic module is shown in Fig. 3. The basic timing element is the ubiquitous 555 monolithic timer, IC1, which is used here in a conventional astable configuration. The output low period from pin 3 of IC1 is set by R2 and C1, according to the equation $T_L = 0.7$ R2 C1, while the output high period for fixed values of R2 and C1 is set by R1 and VR1, according to $T_H = 0.7$ (R1 + VR1 + R2) C1; both equations give times in milliseconds for resistances in kilohms and capacitances in microfarads. The component values shown in Fig. 3 will produce a fixed low output period of 0.7 seconds, while the output high period will vary from approximately 1.3 seconds (minimum VR1), up to around 70 seconds (maximum VR1). This produces a useful range of pulse-to-pulse intervals, but without the need for any unusual component values.

The series switching device is a Darlington power transistor, TR1, which is operated in common emitter mode. The load is connected in its collector with a fuse, FS1, included for protection, and an l.e.d. gives an indication of the output state. In this configuration, the load is switched on when the output of IC1 is low. With the transistor specified mounted on a suitable heatsink, loads of up to 5 amps may be controlled. This would allow the older type of wiper without selfparking facilities to be controlled directly; simply adjust the value of R2 to give an output low period which is equal to the time taken for the wiper to complete one wipe cycle. In simple applications the load is connected between terminals 5 and 6 of the delay unit, and FS1 and D2 are chosen to have ratings appropriate to the load concerned. There is, however, no simple, cheap and robust method of using semiconductor switching when the load is a self parking wiper, and so the load on TR1 will be the relay coil for the switch S1 which is shown in Fig. 2. In this case, the ratings of D2 and FS1 may be significantly reduced; 1 amp will allow a useful number of relays all to be connected to the same output without overload.

The general purpose circuit described above may be used for a wide range of applications simply by changing the timing components to give the required on/off periods. Alternative values may be calculated from the equations given.

CONSTRUCTION

The basic delay unit described above and shown in Fig. 3 is built on a small single-sided p.c.b., the foil layout of which

COMPONENTS

Resistors

R1 8.2k R2 10k R3, R5 1k (2 off) R4 470

VR1 1M variable potentiometer with switch

Capacitors

C1 100μ 16V elect. C2 100n ceramic

Semiconductors

IC1 555
TR1 TIP126
D1 0-2 in l.e.d.
D2 See text
D3 1N4001

Miscellaneous

Terminal pins (6 off)
12 volt changeover relay (see text)
Printed circuit board
Tap-in connectors (4 or 5 off — see text)
P.c.b. fuse holders (2 off) plus fuse (see text)
Insulating hardware for TR1 (optional)
Socket for IC1 (optional)

is shown adjacent. The corresponding component layout (on the top side of the p.c.b.) is shown adjacent. For low power loads such as relay coils, and other loads up to approximately 1 amp, the use of a heatsink for TR1 is not essential, but will render the unit more robust. Above 1 amp, the use of a heatsink is recommended; one rated at around 10°C/W is suitable and will fit on the p.c.b. shown. The metal tab of the TIP126 is connected to the collector and hence in some applications it may be desirable to insulate the tab from the heatsink using a standard mounting kit.

Care should be taken to ensure the correct orientation of the polarised components but otherwise no special handling procedures are required. The use of a d.i.l. socket for IC1 is optional, and connections to the p.c.b. are made using terminal pins which are a push-fit and then soldered to the copper track. The component layout for the unit is in no way critical, and constructors may prefer to use a small piece of Veroboard in place of the p.c.b. shown.

The track layout for the p.c.b. allows either a preset resistor or a fixed resistor to be fitted in the place shown for VR1. This allows the provision of a single preset wiper speed in applications where this will suffice, or where there is insufficient space to mount a variable control on the dashboard. In the majority of applications, however, it is expected that neither a fixed resistor nor a preset will be mounted on the p.c.b., and instead a potentiometer will be wired between pins 2 and 3 and mounted on the dashboard; the unit on/off switch is most conveniently combined with VR1. In situations where the delay unit will be mounted away from easy access, it may be useful to fit a 5 amp fuse in the p.c.b. holder, and then use a standard in-line automotive fuseholder with a more appropriate fuse to protect against overloads and faults. In general, FS1 (or the in-line fuse) and D2 should be chosen to have a rating approximately twice that of the continuous rated load current. In relay-driving situations, a 1 amp fuse and 1N4001 diode or similar are suitable components.

TESTING

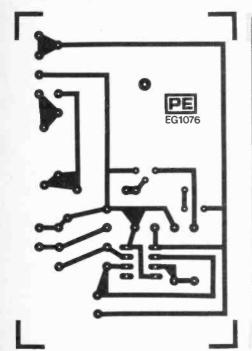
When the p.c.b. assembly is complete, it should be carefully checked for dry joints and solder bridges between adjacent tracks. The board may then be mounted in a small plastic or diecast box if required, prior to some pre-installation tests. A 12 volt supply, preferably with an electronic over-current trip or at least with a 1 amp line supply fuse, should be connected between pins 1 and 4. A short wire link should temporarily be fitted between pins 2 and 3. Turning on the supply should cause the l.e.d. to begin to flash every 2 seconds, with a mark:space ratio of approximately 1:2. The supply current should vary between approximately 5mA (l.e.d. off) and 50mA (l.e.d. on). As a final check, the voltage between pins 5 and 6 should fluctuate between just below the supply voltage and 0 volts, following the indication of the l.e.d. on/off, respectively. Removal of the shorting link between pins 2 and 3, and substitution with a resistor should cause the l.e.d. to remain extinguished for a period which is progressively longer as the resistance is increased.

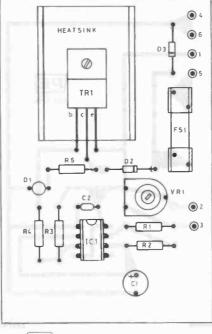
INSTALLATION

The installation of the delay unit, relay and switch/optional speed control follows the wiring diagram shown in Fig. 5. If only a fixed speed is to be used in conjunction with a p.c.b. mounted component for VR1, then the two wires marked with asterisks in the drawing are simply omitted. The first step is to identify the two wires from the normal wiper controls which are marked 'a' and 'b'. This is best done with the aid of the wiring diagram for the car, but may easily be done with the wiring to the dashboard switch exposed. In case of doubt, wire 'a' will carry +12 volts whenever the ignition circuit is switched on, whereas wire 'b' will carry +12 volts only when the ignition is on and the wiper controls are on.

When leads 'a' and 'b' have been identified, switch off the ignition and use four tap-in connectors (coded 1 to 4 in the diagram) to complete the circuit. It will be necessary to cut wire 'b' as shown between connectors 2 and 3, and in many cases a fifth connector may be used to connect p.c.b. pin 4 to ground via one of the leads on the normal wiper switch.

Fig.4. Foil pattern for p.c.b. and board layout (right)





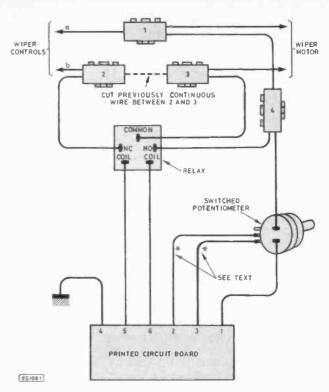


Fig. 5. Details of unit installation

The relay shown may be mounted either in the same box as the p.c.b. or secured anywhere convenient. This relay may be almost any changeover relay fitted with a 12 volt coil; car accessory shops usually stock these for headlight changeover and similar purposes.

CHECK OUT

When installation is complete, ensure that the delay unit is switched off, and turn the ignition back on. Check that the

normal tailgate wiper control still functions correctly. If the wiper runs continuously regardless of the control setting, it is likely that the connections to the relay switch contacts have been confused, and these should be checked. When all is satisfactory, the normal wiper control should be returned to 'off', and the delay unit switched on. Turning VR1 fully clockwise should produce a wiping speed very close to the normal speed. If the control appears to work the other way round, simply move the lead from p.c.b. pin 3 to the unused pin of VR1.

The final check should be to set the unit to the slowest wipe rate (VR1 fully anti-clockwise), and then turn on the normal wiper control. The result should be to restore the normal wipe rate.

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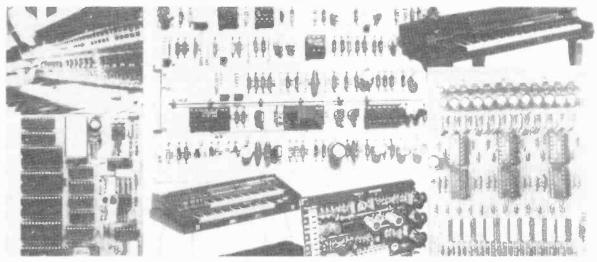
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THE popular phasing musical effect is produced using a filter which has one or more notches of deep attenuation that are automatically swept up and down over the audio frequency range. The two normal methods of obtaining this effect are to use either a delay-line or phase shift networks to generate an output which is out-of-phase with the input at certain frequencies, and then by simply mixing the input and output signals the required notches of high attenuation are produced by a simple cancelling process.

This phaser unit uses a simple alternative which is made possible by the advent of practical switched capacitor filters, and the unit is built around the two filters of this type in the MF10CN device. Each half of the MF10CN actually has two filter sections plus some additional circuitry so that two state-variable filters are produced using a single MF10CN, and depending on the mode of operation selected these each provide notch, bandpass, and lowpass outputs, or highpass, bandpass, and lowpass outputs.

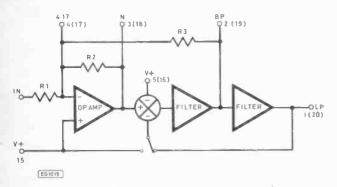


Fig. 1. Block diagram showing one section of the MF10CN

Fig. 1 shows in block diagram form one section of the MF10CN, and this also shows the mode of operation employed in this project. The MF10CN has a 20 pin d.i.l. plastic package, and the diagram shows the pin numbering for one-half plus the equivalent pin numbers for the other half, in brackets. Pin 15 is common to both halves of the device. R1 and R2 are used to set the closed loop voltage gain and input impedance of the input operational amplifier at suitable figures, and R3 introduces negative feedback from the bandpass output which produces the required notch response at the output of the operational amplifier. The Q of the filter is determined by the value given to R3.

BLOCK DIAGRAM

Fig. 2 shows the block diagram for the entire unit. As its name implies, a switched capacitor filter consists of electronic switches which connect the input signal to (and disconnect it from) the filter capacitors, and the switching rate

is determined by a clock signal. This type of filter is very useful since the operating frequency of the filter is directly related to the clock frequency, and for the MF10CN the operating frequency can be either one-hundredth or one-fiftieth of the clock frequency. By making the clock frequency adjustable, the operating frequency of the filter can be controlled, and by using a voltage controlled oscillator (V.C.O.) to provide the clock signal the operating frequency of the filter can be automatically swept up and down using a low frequency oscillator to provide the control signal.

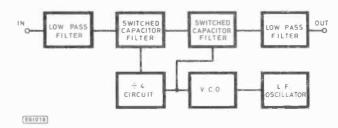


Fig. 2. Block diagram of entire unit

In this design the two filters of the MF10CN are connected in series and are obviously used as notch filters. A simple lowpass filter is used at the input to eliminate any r.f. signals which might otherwise be fed into the input due to stray pick-up, and which could heterodynes with the clock signal or its harmonics. The clock signal only breaks through to the output at a low level (about 10mV r.m.s.) and is not likely to cause any problems, but another low pass filter is used at the output to further attenuate the clock signal.

The clock signal is generated by a simple V.C.O. Which is controlled by a low frequency oscillator having a roughly triangular output waveform. Obviously the two filters must provide notches at different frequencies, and the two simple ways of achieving this are to either use separate clock oscillators with a common sweep oscillator or to feed the output of the V.C.O. to a divider circuit to produce a second, lower frequency clock signal. In practice, the second method seems to be the cheaper and more satisfactory solution, and is the one adopted in the final circuit. A divide by four circuit puts the two notches a couple of octaves apart, and in practice this spacing seems to be about optimum.

THE CIRCUIT

The circuit of the filters is shown in Fig 3, and Fig 4 shows the circuit diagram of the sweep oscillator, V.C.O., and divider stages of the unit.

C2 gives d.c. blocking at the input and R3 plus C3 form a simple r.f. filter. R4 and R5 set the input impedance and voltage gain of the first notch filter at 33k and unity respec-

tively, and R6 gives the filter a fairly low Q value. Making R6 higher in value gives a higher Q value, but the notch produced then tends to be so narrow that the phasing effect becomes barely noticeable with most signal sources. A lower value for R6 gives reduced Q and broader notches which give a more extreme effect, and if desired constuctors can experiment with the value of this resistor in order to obtain the effect that they consider to be most suitable. The output of the first notch filter is direct coupled to the input of the second filter, and this second stage is identical to the first. R10 and C4 form the output lowpass filter and C5 gives d.c. blocking at the output. S1 enables the circuit to be bypassed when the phasing effect is not required.

The MF10CN has a number of terminals which must be connected to the appropriate voltages in order to obtain correct operation of the filters. Pins 13 and 14 are negative supply terminals for the digital and analogue circuits of the device respectively, and pins 8 and 7 are the equivalent positive supply terminals. These two sets of supply terminals can be decoupled separately, or simply wired together as in this case. Pin 6 controls the switch in each half of the device (see Fig. 3), and in the filter mode used here it must be taken to the positive supply voltage. Pin 9 is the level shift input, and for single supply operation this is connected to the

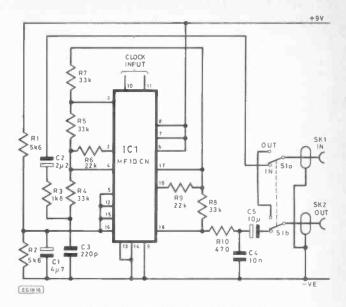


Fig. 3. Circuit diagram of the filters

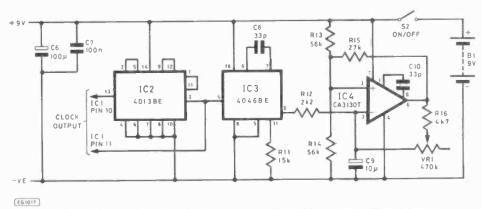


Fig. 4. Circuit diagram of the sweep oscillator, V.C.O, and divider stages

negative supply rail. The device is then compatible with TTL and CMOS clock signals.

A number of pins are biased to half the supply potential, including pin 15 which connects to the non-inverting inputs of the operational amplifiers in the device. Pins 5 and 16 are unused inputs of the MF10CN and must be biased to half the supply voltage in order to give proper operation of the circuit. Pin 12 is the 50/100 clock input and is tied to half the supply potential to give a filter operating frequency which is one-hundredth of the clock frequency (as in this circuit), or high to give an operating frequency which is onefiftieth of the clock frequency. Having the clock at one hundred times the filter frequency is advantageous in this application since it enables the lower frequency notch to be swept down to around 200 Hz without the clock coming down into the audio frequency range and producing audible breakthrough. A minimum notch frequency of only about 400 Hz is possible with the clock at fifty times the filter's operating frequency.

CLOCK AND SWEEP OSCS.

The sweep oscillator uses IC4 in a well-known configuration, and R16 is given a comparatively low value so that the circuit has a high enough voltage swing across C9 to give an adequate sweep range from the V.C.O. The non-linear triangular waveform across C9 is at a very high impedance, but loading on this by the input of the CMOS V.C.O. is negligible.

The V.C.O. uses the 4046BE CMOS device which is actually a low power phase locked loop, but this makes an excellent V.C.O. if the phase comparators are just ignored. The only two discrete components required are C8 and R11 which set the operating frequency range of the oscillator.

The divide-by-four circuit is a CMOS 4013BE dual D type flip-flop which has each section connected as a straightforward divide-by-two circuit, and they are connected in series to give divide-by-four operation.



Phaser Unit

The MF10CN is designed for use with either dual 5 volt supplies or a single 10 volt supply, but it will operate satisfactorily down to a supply voltage of \pm 4 volts or 8 volts, and can therefore be used with a 9 volt battery supply. The average current consumption of the circuit is approximately 8mA.

COMPONENTS Resistors R1.R2 R3 1 48 R4,R5,R7,R8 33k (4 off) R6.R9 22k (2 off) R10 470 **R11** 15k **R12** 2k2 R13.R14 56k (2 off) **R15** 27k R16 4k7 All resistors 1W 5% carbon **Potentiometer** VR1 470k logarithmic carbon Capacitors C1 4µ7 63V axial elect C22μ2 63V axial elect C3 220p ceramic C4 10n nolvester C5 10μ 25V radial elect C₆ 100µ 10V axial elect **C7** 100n polyester C8.C10 33p ceramic plate 2% (2 off) C9 10µ 16V tantalum Semiconductors IC1 MF10CN (Rapid Electronics) IC2 4013BE IC3 4046RF IC4 **CA3130T or CA3130E** Miscellaneous SK 1/S2 Standard 6.35mm jack with d.p.d.t. contacts SK2 Standard 6-35mm lack socket S1 d.p.d.t. heavy duty push button 9 volt PP3 battery and connector 150x80x50mm diecast aluminium box (M.E.S. type DCM5005 or similar). Printed circuit board. Control knob. Veropins, i.c. sockets, wire, etc.

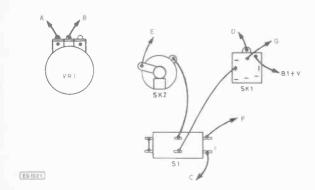
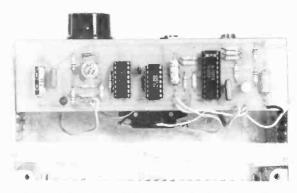


Fig. 5. Wiring diagram.

CONSTRUCTION

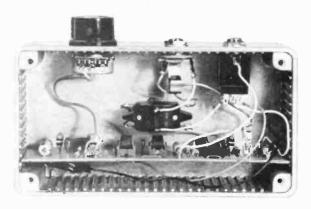
S1 is a heavy-duty push-button switch which is fitted centrally on the top panel of the case so that it can be operated by foot. It is necessary to use a strong case since it will have to withstand a fair amount of pressure each time S1 is operated, and a diecast aluminium box measuring 150 by 80 by 50mm is ideal. The two sockets and VR1 are mounted on one of the 150 by 50mm sides of the case.



P.C.B. withdrawn from unit showing component assembly

Fig 5 shows the wiring of the potentiometer, sockets and foot switch; the corresponding designations being shown in Fig 7 with the component layout. Fig 6 shows the p.c.b. design. There is ample space within the unit to house the PP3 battery which should be securely positioned. All four integrated circuits are CMOS types and the usual MOS handling precautions should be observed when dealing with these. SK1 has d.p.d.t. contacts, but these are only used here as a single set of make contacts which automatically switch the unit on when a jack plug is inserted into SK1. However, on/off switch S2 can be a separate switch if preferred. VR1 controls the phasing speed, and this is a logarithmic potentiometer used in reverse (i.e. clockwise rotation gives a decrease in phasing rate). This control covers a wide frequency range of about 0.1 Hz to 10 Hz, and this method gives easier control of the phasing speed than that obtained using a linear potentiometer, especially at the high frequency end of the range. Note that IC3 has the opposite orientation to the other three integrated circuits, and that this device could easily be damaged if the unit is switched on with it connected the wrong way round.

If the specified case is used the printed circuit board will



Final assembly showing P.C.B. in position

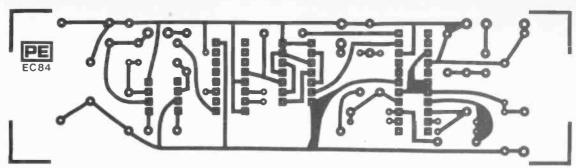


Fig. 6. P.c.b. design

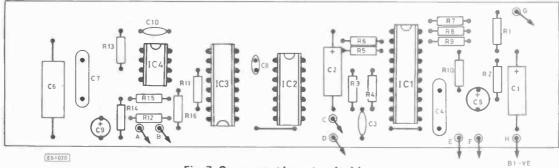


Fig. 7. Component layout and wiring

slot into place in the guide rails at the rear of the case. There is ample space for mounting holes to be drilled in the board if a different case is used.

Provided the unit is used with an input level of a few hun-

dred millivolts r.m.s. or more it will provide a good signal to noise ratio of 60dB or better. The maximum input level the unit can handle without clipping and producing severe distortion is more than adequate at about 2 volts r.m.s.

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THE EXTRA-TERRESTRIAL PROBLEM

In this issue of Spacewatch we will deal with the question of extra-terrestrial intelligence. It must be made clear that this does not mean that it is proposed to deal with UFO sightings, or the value of reports which come into various centres at a rate in excess of one hundred a week. To avoid confusion it is necessary to clarify the origins of the phrases 'Flying Saucer' and 'Unidentified Flying Object'. The term 'Flying Saucers' probably originated from a 'recorded' sighting early in the last century in southern United States, when a farmer described an object as, "It looked like a cup saucer". After that reports were frequent which led to speculation on "Flying Saucers". Because so many of such reports were the result of faulty observation or imagination, it was decided to rename all sightings and call them-"Unidentified Flying Objects." By that time many more frequent reports were coming in and unfortunately the new name made the situation worse because instead of making the claims for seeing flying saucers, the reports were of UFO's, which became synonymous with "Flying Saucers" throughout the media. The meeting which made this brave attempt to regularise matters in 1947 led to an enormous increase in

It is often mistakenly stated that, if a large number of people "see" something and describe it similarly then it means that such an event must be true and accepted. This is still the case, even now, when there is so much evidence of the extreme lack of reliability in these observations. How then to deal with the subject of the possibility of extra-terrestrial intelligence. The first step is to decide the place from which the experiment is to be carried out. This must, if dictated by the Einstein view of the cosmos, be from the Solar System. At the present state of knowledge in matters of communication the electromagnetic spectrum determines the limits. Such an attempt began in 1974 from the 1,000ft. diameter radio telescope at Arecibo, Puerto Rico. The signals were directed to a globular cluster of about a million suns, known to astronomers as Messier 13. It will take about 24 thousand years for the coded signal to reach that vicinity and the time at least, for a return signal to be received back on Earth will also be 24 thousand years. This serves to emphasise the limitations of the system of communication. Within the solar system itself there are time delays in communications that are necessary, even for the short distance to the moon, and from the Voyager spacecraft still longer delays, increasing as time goes by.

The original project for the search was known as Ozmar and was organised by Frank Drake, then at Greenbank, West Virginia. It operated between 1959 and 1960-a coded signal was sent out in the direction of Epsilon Eridani and Tau Ceti and this was continued for only a few weeks. Of course there was not much success and the co-operation was lukewarm. In any case a few weeks was not likely to afford much data since, ideally at least 100 thousand or so stars would need to be studied. Later the construction of a 600 foot dish was begun and this project failed but a number of other attempts were made and because there was little enthusiasm, not many people had much interest in the matter. There is a project in Canada, and the Russians have a station which has now been turned into a full scale search with the RATAN-600 telescope. Half the observing time is spent on extraterrestrial work with this telescope. Now that a much wider view of the matter is taken, and with the development of improved receiving techniques together with spaceborne telescopes, much more can be done. In spite of all this it is difficult, under present thinking, to lay down a definite programme which could offer positive proof within a lifetime.

Another project which has been partly carried out for reaching deep into space, is an American venture. This when completed will consist of a "Mills Cross" so named after the originator B. Y. Mills from Australia. This is in the form of a number of lines of parabolic dishes set up in the form of a cross, each arm being 12.5 miles in extent. This will behave as though it is in fact a 25 mile diameter dish.

It would be even better if one telescope was on the Moon and the other on Earth, and better still if there was one also on Mars. However all this makes certain suppositions which might be set out as;

—The manner of thinking must be the same as the Earth's inhabitants

-They must be at the same stage of development as the Earth is. In the case of the Messier 13 cluster this would mean that the inhabitants of a planet would have existed 24 thousand years before our time unless they have at the time of the arrival of the signal from Earth, a system of communication which could cover all future developments and still conform to the present theories used on Earth. This is an unknown. That being the case then any project has to make certain assumptions. In the projects so far suggested or attempted it has been assumed that any other beings would be humanoid like ourselves and have the same physiology. This had to be, though there were those who suggested that no matter what the form, the physics of the universe must be readable in terms of mathematics. This latter assumption is not justified on the present state of knowledge. There is not enough space in one issue to deal with this at length but suffice to say for the moment that any alternative view has to depart from mathematical concepts based on the work of Einstein. This is a matter which still exercised the great man's mind until his death.

So far although the Universe as a whole has

been mentioned as a source for the possible signals from extra-terrestrials, it is perhaps wise to look at the problem from the point of view of the Solar system and our own Galaxy. Consider then that in our Galaxy which has spiral arms and rotates. The extent of Galaxy is about 100,000 light years in diameter and at its thickest part is about 20,000 light years. The Solar system is situated at a point some 32,000 light years from the galactic centre. Since the Solar system rotates with the galaxy it takes something around 225 million light years for the Solar system to complete this journey. The total number of stars is enormous and they are in various states of birth, growth and death. Among the many millions of stars suppose there are one million which with a developed technology would use the electromagnetic spectrum as a means of communication. Let the distribution be random and the average distance between them be of the order of 300 light years. With communication techniques available to the denizens of the Earth the shortest time for a signal to be sent and an answer received is 600 years. If it is assumed that during the period that attempts have been made to transmit coded signals, deliberately made that is, somewhere the signal is received and returned. In order that that signal may be received the same technique must remain in operation on Earth as that used for the original transmission. This raises many serious problems.

It will be necessary to install a receiver which will continuously operate from some specially built station timed to come into operation in 600 years time from transmission of the original signal. The technology will need to be the same as that of the original transmission. This requires that the site shall not, for that period be disturbed by effects no matter what the cause, terrestrial, extra-terrestrial or internal earth changes. The power supplies must be able to have survived and in working order no matter what may have happened in the vicinity of the site. Records and operational instructions must be known and available. This would be extremely costly and subject to the frailties of the inhabitants of the Earth. So many sources of change are not only from the natural development but from political and religious cults. Indeed it is long enough beyond a single span of a lifetime even with the inevitable increase of that life span to double the norm in the foreseeable future. This is the real point; it is unlikely that funds to execute and maintain such a project would be forthcoming. Is there another solution?

One that springs to mind is the possibility of a beacon in the form of a long time scale satellite with a life to be determined. Since the present techniques available make this an ordinary matter it leaves the problem at the point of the technology of the receiving unit. Power is continuously available with back-up. The question left is continuous operation, this also is within forseeable control. The ground station however remains or at least an apparatus is preserved to be brought into use unless of course the population is moved to a permanent abode on a space station which encloses the Earth.

Frank W. Hyde

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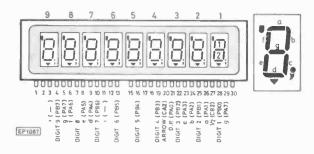
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PE MICROCONTROLLER: DATA SHEET 3

DISPLAY MODULE

THE display module in the Microcontroller is a multiplexed 9-digit Futaba gas discharge unit, type 9-LT-03. In the original application two such units, each mounted on separate p.c.b.s, were connected in parallel to each controller board. On the display p.c.b. digit number 8, the apostrophe and comma are supplied unconnected. In the Microcontroller pins 7 and 22 have been connected together to form the display field separator characters, and hence digits 3 and 8 will always have the same indication.

In order to illuminate any particular display segment it is necessary to set the appropriate digit select line (PBØ to PB7 on IC12) to a logic '1', and then set the corresponding segment select line (PAØ to PA7 on IC12) to a logic '1'. Any number of segments/digits may be selected at a particular instant, but all selected segments in all selected digits will be illuminated simultaneously, so the display driver in DISBUG scans each digit in turn. In addition, the period for which a digit is selected must be chosen to avoid visible flicker, but not be so fast as to render the overall display unreadable. The DISBUG monitor routines which provide these facilities will now be described.



DISPLAY SCAN ROUTINE

The Microcontroller's display is scanned by a subroutine called DISPLAY. This routine includes a delay
to cause each digit to be illuminated for approximately
2 milliseconds, before moving on to the next digit.
DISPLAY assumes that the display PIA has been
correctly set up by the DISBUG initialisation routine
(which is executed automatically at power-up), and it
uses a maximum of six bytes of stack space. The scan
routine is called by 'JSR DISPLAY', which is coded as
BD F8 14. There are no entry or exit parameters
passed in the CPU registers, and all registers except
SP are corrupted by the routine.

The display is actually scanned once each time DIS-PLAY is called, with digits 1 to 7, and 9 illuminated in turn. The character displayed at each digit position is determined by reading the DISBUG RAM locations 03F8 to 03FF; the locations are used to drive the display PIA as shown in Table 1. Each bit position corresponds to one of the segments 'a' to 'g' or the decimal point, and so a wide range of characters may be displayed, e.g. a code of EC would display 'H', and a code of E8 would display 'h'. The display table locations may be written to directly (e.g. CLR to location 03FA will blank digits 3/8), or the routines describe below

may be used to insert display codes for numeric values into the display table.

In order to produce a stable display, user programs should ensure that DISPLAY is called regularly within the infinite loop of the control program, otherwise the display will flicker or be erratic. The way in which DISBUG uses this routine is shown in Part 3 of the Microcontroller series.

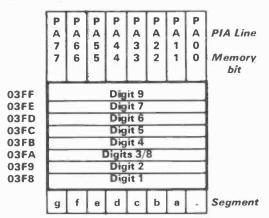


Table 1. DISBUG display table format

CONVERSION ROUTINES

The information provided above is sufficient to allow any character which can be represented by the available segments to be displayed. The process is simply a matter of inserting the appropriate code into the display table, and then calling DISPLAY. A very common requirement is to display a numerical value which may be held in a register or memory/PIA location. This task may be greatly simplified by the use of two routines provided within DISBUG.

The first routine is DIGIT and is called via 'JSR DIGIT', which is coded as BD F8 DO. The routine converts the number in the least significant four bits of rA into the appropriate display code, and then inserts this code into the display table at the address contained in the index register. Thus, for example, if DIGIT is called with rA = 4B, and In = 03F8, then the routine will insert the value 'F8' (the display code for 'B') in location 03F8 (the display table entry for digit 1). DIGIT uses one byte of stack space, and preserves all register values except the index register, whose contents are incremented by one.

The second routine is TWODIG and is called via 'JSR TWODIG', which is coded as BD F8 F7. This routine converts the number in rA into two display codes, and inserts the code representing the LS 4 bits of rA in the location indicated by the entry value of In, and then inserts the code for the MS 4 bits of rA in the next location. In the example above, a call to TWODIG rather than DIGIT would result in a code of 'F8' in location 03F8 and a code of 'CC' (for '4') in 03F9. TWODIG uses three bytes of stack space, and preserves all register values except the index register, whose contents are incremented by two.

M. Tooley BA and D. Whitfield MA MSc.

FOR applications such as the voltage control of oscillators, attenuators etc, the digital to analogue converter will be able to directly drive an externally connected load. The minimum recommended value of load resistance is, however, 1kohm for the normal output (V_{out}) and 100ohm for the complementary output (V_{out}). Note that, since the complementary output exhibits a lower output impedance than the normal output, in some applications its use is to be preferred. In such cases it will, of course, be necessary to use the 1's complement of the data word. This can be quite easily obtained using the appropriate op. code within the machine language program.

When the digital to analogue converter is used to drive very low impedance loads (such as d.c. motors) an additional power amplifier stage will be required. A typical circuit for an "add-on" power amplifier module is shown in Fig.1. This uses a single monolithic integrated circuit which is, incidentally, capable of providing a power of up to 21W in a nominal 4ohm load when operating from plus and minus

+15V

C1

100,u

D1

1N4001

INPUT

1k

2

1N4001

R3

100,u

C3

0UTPUT

R3

-15V

Fig. 1. Circuit diagram of the power amplifier module

into the REAL WORLD part 3

Michael Tooley B.A.
David Whitfield M.A. M.Sc.

18V supply rails. In this particular application, the device is configured for unity gain (non-inverting) and the recommended maximum value of output current is 1A. The TDA2030 features internal short circuit protection, thermal shut-down, and safe operating area protection. The output current is internally limited to 3.5A, however, it is recommended that some form of current limiting (at around 1.5A, or less) be included in both the positive and negative supply rails. A power supply capable of meeting the requirements of both



Fig. 2. P.c.b. layout for the power amplifier module

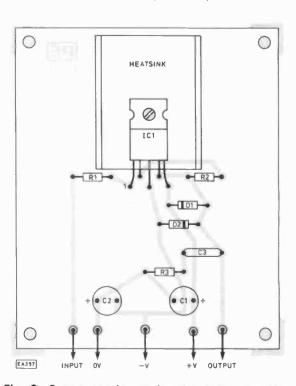


Fig. 3. Component layout for the power amplifier module

COMPONENTS ...

POWER AMPLIFIER MODULE

Resistors

R1, R2 1

1k (2 off)

Capacitors

C1, C2 C3 100μ 16V p.c. electrolytic (2 off)

100n polyester

Semiconductors

D1, D2

1N4001 (2 off)

TDA2030

Miscellaneous

PCB terminal pins (5 required) heatsink

Constructor's Note

Components and PCB are available from Howard Associates, 59 Oatlands Avenue, Weybridge, Surrey KT13 9SU (s.a.e. for details).

STEP	SWITCH SETTINGS	DESIRED OUTPUT VOLTAGE (V _{out})	ADJUSTMENT
1	S1-S8 open S9 open	ov	VR1
2	S1-S8 closed S9 open	V _{FS} V _{LSB}	VR3 (and VR2 if necessary)
3	S1 closed S2-S8 open S9 open	½V _{FS}	none should be necessary
4	S1 closed S2-S8 open S9 open	Check that V _{out} = $-\frac{1}{2}V_{FS}$	none should be necessary
5	S1 closed S2–S8 open S9 open then	½V _{FS}	none should be necessary
6	closed S1-S8 open or closed S9 closed	½V _{FS}	none should be necessary

TABLE 3 Adjustments and tests required for unipolar operation

STEP	SWITCH SETTINGS	DESIRED OUTPUT VOLTAGE (V _{out})	ADJUSTMENT
1	S1 closed S2-S8 open	ov	VR1
2	S9 open S1-S8 open	+V _{FS}	VR2
3	S9 open S1-S8 open S9 open	+V _{FS} -V _{LSB}	VR3
4	S1 closed S2-S8 open	ov	none should be necessary
5	\$9 open \$1 and \$2 closed	½V _{FS}	none should be necessary
6	S3–S8 open S9 open S1 open S2 closed S3–S8 open	$-\frac{1}{2}V_{FS}$	none should be necessary
7	S9 open S1 and S2 closed S3–S8 open	Check that V _{out} = $\frac{1}{2}V_{FS}$	none should be necessary
8	S9 open S1 and S2 closed S3-S8 open	½V _{FS}	none should be necessary
9	S9 open then closed S1-S8 open then closed S9 closed	½V _{FS} (i.e. no change)	none should be necessary

TABLE 4 Adjustments and tests required for bipolar operation

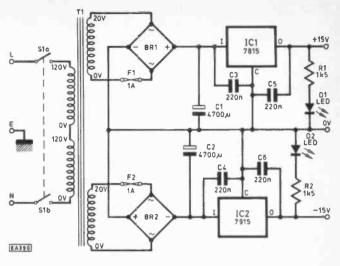


Fig. 4. Typical power supply circuit for use with the D to A converter and associated power amplifier modules

the digital to analogue converter together with one, or more, power amplifier modules is shown in Fig. 4.

The p.c.b. layout for the power amplifier module is shown in Fig. 2 together with the corresponding component overlay which is given in Fig. 3. Assembly is extremely straightforward and, since no adjustment is required, detailed constructional and testing information is unnecessary.

USING THE D TO A CONVERTER

The digital to analogue converter, together with any associated power amplifier modules, can be used in a variety of particular configurations depending upon the requirements and constraints of the particular system. Fig. 5 shows

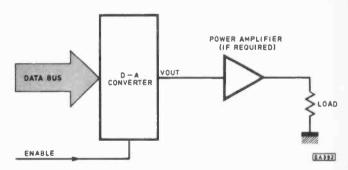


Fig. 5. Conventional single ended output configuration

a conventional 'single ended' arrangement. A bridge arrangement using two power amplifiers, driven from the complementary outputs of the digital to analogue converter, is shown in Fig. 6. This configuration effectively doubles the output voltage swing developed across the load. Fig. 7 shows how several power amplifier modules can be connected to a single digital to analogue converter. Note that, to reduce the loading on the converter where more than one power amplifier is employed, the values of R1 and R2 within the power amplifier module should be correspondingly increased. A value of 10kohm for both R1 and R2 will be adequate for the parallel connection of up to ten power amplifier modules. If desired, loads may be driven in a complementary fashion, as shown in Fig. 8. Finally, several digital to analogue converters may be operated simultaneously from the same data bus. This arrangement makes use of the

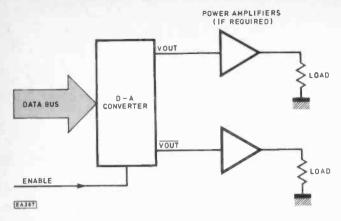


Fig. 6. Bridge output arrangement which doubles the effective voltage swing across the load

latching facility of the ZN428, the ENABLE inputs being driven from the address bus such that each digital to analogue converter can be individually addressed (Fig. 9).

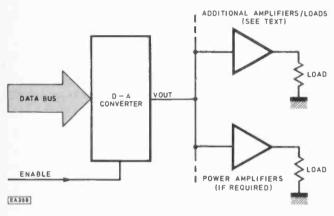


Fig. 7. Method of driving several output loads using a single D to A converter

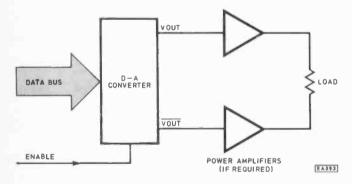


Fig. 8. Complementary driving of loads

ANALOGUE TO DIGITAL CONVERSION

The purpose of an analogue to digital converter is that of generating a digital code which approximates to the actual input voltage level at the instant of sampling. One commonly used method of analogue to digital conversion involves the use of a clock and counter in conjunction with a digital to analogue converter. The clock and counter generate a binary sequence such that the output of the digital to analogue converter is sequenced from zero to full scale. The output voltage from the counter is compared with the input signal voltage using a comparator and the count is stopped when

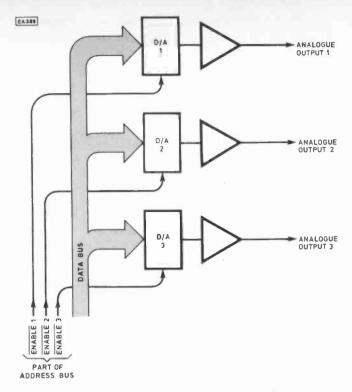


Fig. 9. Technique for driving multiple D to A converters

the digital to analogue converter output is just greater than the signal input voltage. The state of the digital lines thus provides a digital code which is an approximation of the analogue input. The disadvantage of this technique is primarily attributable to the relatively low speed of conversion. In a worst possible case it would be necessary for the counter to produce a full sequence before arriving at the full scale input value. In an 8-bit converter, for example, this worst case condition would necessitate 255 clock cycles. With a 1MHz clock this yields a maximum conversion time of a quarter of a millisecond!

A much better method of analogue to digital conversion involves the use of a technique known as successive approximation. This involves a series of comparisons between the analogue input signal and the output of a digital to analogue converter in which each bit is set in turn, commencing with the most significant bit, MSB. A decision, based upon whether the analogue input is greater or less than the output of the digital to analogue converter, is then made as to whether or not the bit should be retained. The output thus becomes successively closer to the input value; hence the name! The maximum conversion time for such a converter is generally (n + 1) clock cycles, where n is the number of bits employed. An 8-bit successive approximation analogue to digital converter would, for example, require a maximum of 9 clock cycles for conversion; more than twenty times faster than a counter type arrangement! Simplified block diagrams showing the two methods of conversion are given in Figs. 10 and 11.

THE ZN427 A TO D CONVERTER

The ZN427 is a versatile monolithic 8-bit successive approximation analogue to digital converter which incorporates tristate output buffers to permit direct connection to a microprocessor data bus. The device offers a guaranteed maximum conversion time of 15µs (clock frequency = 600kHz) and, like its digital to analogue counterpart the

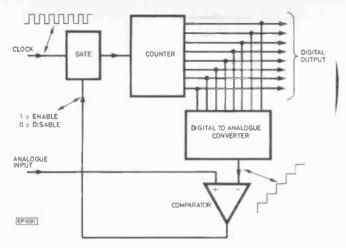


Fig. 10. Simplified block schematic of a counter type A to D converter

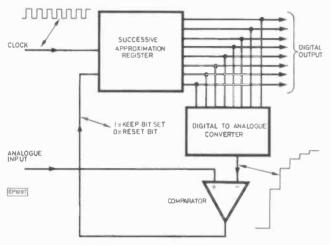


Fig. 11. Simplified block schematic of a successive approximation type A to D converter

ZN428, it also incorporates an accurate voltage reference. The data outputs are fully TTL compatible and the i.c. requires supplies of +5V and -3 to -30V. This latter voltage rail is merely required to establish a constant 'tail' current within the internal voltage comparator.

The internal architecture of the ZN427 is shown in Fig. 12. The principal internal elements of the ZN427 are; a high speed comparator, a successive approximation register, a switch array, an R-2R resistor network, an output buffer array, and a 2.5V precision voltage reference. When a lowto-enable start conversion (SC) pulse arrives, the most significant bit is set to a 1 and all the other bits are set to 0 regardless of their previous state. The analogue output from the R-2R ladder network will then be exactly half the reference input, VREF. The input voltage, VIN, is then compared with this value and a decision made on the next falling clock edge. The MSB will be set to 0 if 0.5V_{REF} > V_{IN} or kept at 1 if 0.5V_{REF} ≤ V_{IN}. The second most significant bit is also set to 1 on the same falling edge and, on the subsequent falling clock edge, a similar decision is made concerning the second most significant bit. The process continues until all eight bits have been examined such that, on the ninth consecutive falling clock edge after receipt of the start conversion (SC) pulse, an end of conversion (EC) signal is generated which indicates that the digital output from the converter is a valid representation of V_{IN}. The digital output data remains latched until the next SC pulse arrives. An output enable (EN) is provided so that data may be read from

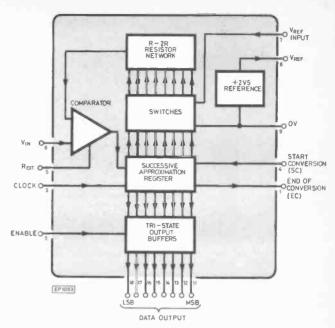


Fig. 12. Internal architecture of the ZN427 successive approximation A to D converter

the converter into the system data bus by means of the tristate output buffer array. A typical timing diagram for the digital word 01010110 is shown in Fig. 13.

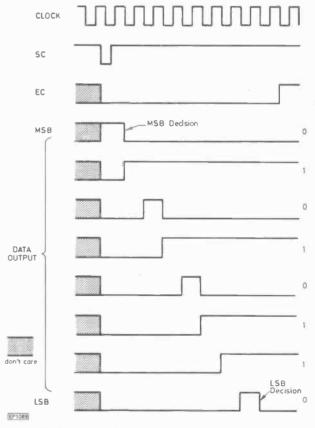


Fig. 13. Timing diagram for the ZN427 A to D converter

The decision as to whether the output of the D to A section is greater, or less than, $V_{\rm IN}$ is made by means of a high speed comparator, the simplified equivalent circuit of which is shown in Fig. 14. This is essentially a differential 'long-

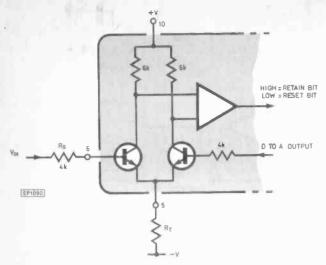


Fig. 14. Simplified equivalent circuit of the high speed comparator section of the ZN427 A to D converter

tailed' pair which is designed to operate with a total emitter ('tail') current of $65\mu A.$ The 'tail' current must be derived from an external negative voltage rail in the range -3 to -30 V and the constant current characteristic may be produced simply by inserting an appropriately high value of series resistor. Various values of negative supply voltage and required series resistance are shown in Table 1.

NEGATIVE SUPPLY	TAIL RESISTANCE
VOLTAGE	(R ₊)
(-V)	
_3V	47k
-5	82k
-10	150k
-12	180k
-15	220k
-20	330k
-25	390k
-30	470k

Table 1 Recommended values of tail resistance and negative supply voltage

The outline circuit diagram of a practical analogue to digital converter is shown in Fig. 15. Whilst it is possible to use a separate low frequency clock within the analogue to digital converter, it is usually expedient to make use of the system clock of the host microcontroller or microcomputer. Such a clock is, nowadays, unlikely to operate at a frequency of much less than 1MHz and therefore it will be necessary to

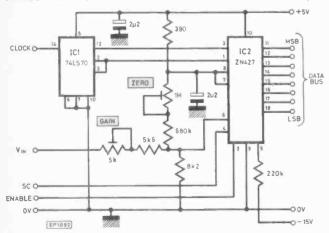
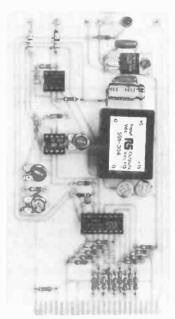


Fig. 15. Outline circuit diagram of a practical A to D converter

incorporate one, or more, stages of frequency division between the system clock and the clock input of the ZN427. In the case of the PE Microcontroller, which has a system clock at 894.75kHz, a single divide-by-two stage is all that is required. In the arrangement of Fig. 15 this frequency division is accomplished by means of a positive edge triggered J-K bistable, IC1. Other division ratios may be easily calculated from the relationship; $N = f_{sd}/f_c$ where f_{sc} is the system clock frequency and fo is the ZN427 clock frequency (maximum 600kHz). The +5V and -15V rails may be derived from the power supply circuit of the Digital to Analogue Converter board described in Part 2 of the series (PE March 1983). To avoid duplication, full constructional details have not been given and readers are therefore recommended to refer to the previous part of this series and to Part 7 of the series on 'Interfacing Compukit' (PE July 1981).

USING THE A TO D CONVERTER

Provided that appropriate signal conditioning can be applied, the analogue to digital converter is suitable for use with virtually any type of analogue transducer. The normal full-scale input voltage for the circuit of Fig. 15 is +10V however larger or smaller input voltages may be catered for by means of appropriate modification of the input potential divider. Where the transducer produces a very low level of



The A to D converter

output, additional amplification may be necessary and this may be provided by means of one or more operational amplifiers. In general, the full-scale input voltage is given by; $V_{FS}=G\times V_{\rm IN}$ where G is the attenuation of the input network. The resolution of the converter is $V_{FS}/256$. Without any input attenuation (G=1) the value of V_{FS} will be the same as V_{REF} and, since the internal reference is $2\cdot 56V$, the resolution will be 10mV/bit. The R-2R ladder network exhibits an impedance of 4kohm thus, to provide an accurate match (minimising offset problems within the comparator), the input attenuator/amplifier should ideally exhibit an output impedance of approximately 4kohm.

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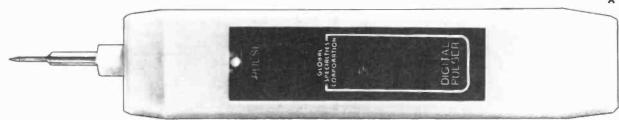
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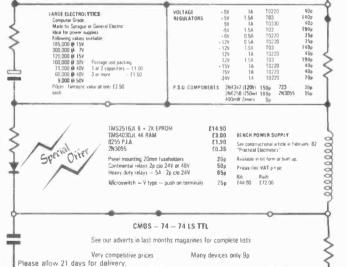
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SEMICONDUCTOR UPDATE R.W.Coles

FEATURING EB2 BB1 LH3 HC16 TFT 3000

SWANSONG

This, dear readers, is the very last "Semiconductor Update" column to appear in Practical Electronics, following an unbroken run since 1975. (Semiconductor Circuits will replace it next month—Ed.)

While pondering on a suitable content for this exodus edition, I at first considered a nostalgic look back at some of the more exotic devices that have appeared here over the years. But nostalgia is hardly the stuff of which this column is made, and so I took a bold step forward instead, by persuading two of the most avant-garde research groups in the country to lift the veil on the electronic future as they see it—with astounding results!

Any doubts you may have harboured concerning the viability of British industry in the 1990s and beyond are about to be dispelled, so step with me now into the brave, new, electronic world which awaits us all . . .

IN-BODY ENTERTAINMENT

Down in Poole, Dorset, of all places, I tracked down Frank N. Stone, boyish head of the new bio-electronic empire. Sceletronic Calcipart. Most of the work down there is still secret, but Frank was kind enough to show me around their BIO-CHIP diffusion facility which is producing a wide range of semiconductor dice for direct implantation in living tissue.

Although electronic implants have been produced before, as heart pace-makers for example, the work at Sceletronic is very different because the integrated circuits are not packaged but are placed directly into a suitable body cavity with the necessary neural connections being achieved with the aid of laser bonding.

Devices of all sorts can be implanted in this way to correct natural deficiences or to provide an enhancement of natural abilities, but the project which sparked my imagination the most was described by Frank as "In-Body Entertainment".

Sceletronic are working feverishly on a set of four CMOS BIO-CHIPS which together will make the "Walk-man" concept of personal entertainment about as obsolete as a stone axe. Integrated onto four thumbnail sized silicon dies will be a complete entertainment system which does not require the lucky recipient to wear headphones or to have a wristwatch TV screen, because the whole thing will be totally internal!

One of the devices, a video processor and display coded EB2, is slipped behind each eyeball to provide back-projection

video facilities capable of displaying both off-air and recorded programs. A second chip, the BB1, acts as an exchangeable storage device of 100 gigabyte capacity which is used to hold a user selectable mix of stimulating audio visual entertainment. This chip has to be more easily accessible and so will be fitted into the trendy owner's navel, or any other orifice of their choice.

Adding yet another dimension to this scintillating ensemble is the LH3 audio processor which is capable of delivering a quadrophonic neural stimulus equivalent to 110 dB's acoustic. In addition to this direct neural audio, which works best at high frequencies, there will also be an optional "cranial woofer" which provides direct internal audio stimulation. Users opting for this extra facility will have to wear the black anodised ear extenders for cooling purposes savs Frank.

To complete the set there will be the HC16 microprocessor based controller chip which will transmit tone, volume, and hue adjustment via existing neural pathways. Inputs will be received directly from analogue-to-digital chemo-receptors integrated onto the surface of the chip. Various other control options will be available, including a panic suppression mode triggered by adrenalin levels which causes all external auditory and visual reception to be suspended in favour of a restful program of soft music and seascapes.

Installation may pose problems, but a survey by Sceletronic revealed that most existing 17 year old hi-fi salesmen can be retrained in the simple technique of laser surgery in a matter of hours.

While I was in the Sceletronic lab I was introduced to Igor who had already been fitted up with a breadboard version. Igor's scars were healing nicely, and apart from a tendency to go cross eyed occasionally, there seemed to be no serious side affects. Unfortunately I was unable to question Igor in depth because he had just been fitted with a new BB1 containing material of Danish origin which appeared to be causing some technical difficulties.

This new technology will revolutionise the lives of all joggers, roller skaters and lecture goers!

SEE YOU LATER PROPAGATOR

A couple of years ago I revealed to you the amazing progress being made by Lliys Electronics over in South Wales. I know that if any firm could provide a stimulating

glimpse into the future it had to be them, so off I went with my notebook and recorder.

The last time I was there Lliys were into hyper-power transistor technology, but things have moved on since then, and I found the research department, headed by the Polish émigré Zarcy Pudsti, hard at work on a revolutionary new microprocessor device.

Apparently Llivs have made a breakthrough in speeding up the operation of digital logic circuits and have got their latest device running at an amazing 2 giga hertz clock rate. Propagation delays in the gates have been cut down to just a few pico-seconds with the aid of a new and secret doping material developed and patented by Llivs.

While I was there they started to test the latest version of this incredible device, the TFT 3000, and the results were impressive to say the least. Apparently one of the chemists had added too much of the dopant to the silicon melt, and during the tests it became apparent that the gate delays had become negative, i.e. pulses were leaving the output of gates before an input signal was received!

While Zarcy and I pondered about the implications of this new effect, we saw the 64 pin leadless chip carrier containing the TFT 3000 begin to metamorphose. Within ten minutes we were left with ten 40 pin dual in line packages, within half an hour these were replaced by one hundred 16 pin d.i.p.s, then four hundred circuit boards containing large numbers of transistors. Just in time, Jim the lab assistant shouted a warning and we escaped with only minor scorch marks and bruises as the whole of Lliys labs was transferred into a glowing mass of EF86 valves.

After the EF86s, the Babbage style analytical engines and the Chinese abacus wielders were tame by comparison, and Zarcy and I retired to the nearby computer room to carry out an analysis of what could be expected next. Zarcy calculated that the TFT 3000 would reappear in about 3 weeks following a reversal of entropy at the genesis of the known universe, and perhaps he is right.

Personally, I hoofed it, after a quick 999 call to the local fire brigade, but everyone at Lliys seemed to think it was a great success. They still plan to market the TFT 3000 after some readjustment of the dopant levels, but if you are interested you had better place your order early, before stocks disappear.

(Readers requiring more information on these items should note the cover date of this issue—Ed)

Ultimum Computer Interface Part

WILLIAM EDWARDS

WATFORD ELECTRONICS

WE CONTINUE our series of cards for the ULTIMUM motherboard with a peripheral card capable of producing speech. It uses a low cost, custom integrated circuit which provides most of the functions needed to produce an almost unlimited vocabulary using the phoneme method of speech production.

SYNTHESISING SPEECH

There are many different techniques available for generating speech using a computer. Ultimately, they all require some method of regenerating the basic elements of speech by modelling the human vocal tract. The heavy handed approach is to sample analogue speech waveforms and convert them to a digital form which may be subsequently regenerated through an analogue-to-digital converter. The number of samples is necessarily high (about 5,000 samples. sec⁻¹) and this means that a large amount of

EXTERNAL ROM CONTROL

ALU

COEFFICIENT REGISTERS

VOCAL TRACT MODEL

2k x 8 BIT ROM

ADDRESS REGISTER

START ADDRESS LATCH

EP 1094

Fig. 6.1. Block diagram of Speech unit

memory is required; a few words would exhaust the memory of most home computers.

There are two, more practical solutions. Firstly, some form of data compression can be used in conjunction with digital circuitry to restore the original signal. This circuitry usually takes the form of a complex digital filter. National Semiconductor, and Texas Instruments have both evolved methods of encoding phrases in such a compressed form, the best known being a system called Linear Predictive Coding. This is the technique employed in the commercial, speaking toys and teaching aids. The drawback is that the encoding process requires complicated equipment and lies beyond the scope of amateurs, so that one is limited to pre-defined vocabularies supplied in ROM form. Against this, the quality of speech is guite good (albeit with a heavy American drawl in nearly all cases). The second method relies on the fact that speech can be broken into a limited number of basic components. There are several such subdivisions, the smallest of which is called the allophone, or more commonly (but incorrectly) the phoneme. Early phoneme generators used analogue circuitry to reconstruct an electronic equivalent of the vocal cords and the rest of the vocal tract, using operational amplifiers as oscillators, filters and noise generators. Digital versions of these analogue predecessors make full integration much simpler, because the discrete components are largely eliminated.

THE SP-0256 SPEECH CHIP

Over the last year or so several new all digital speech chips have been introduced. The SP-0256 (General Instruments) has been chosen for this design because it combines low cost with simplicity. Allophones are encrypted in a 2k x 8 ROM. On selecting an allophone by supplying a count and a strobe pulse, the appropriate area of ROM is accessed and the data is passed to the vocal tract model which then regenerates an allophone. The 2k x 8 ROM stores code for all the allophones as well as periods of silence which are very important in the reconstruction of realistic speech. There are no words or phrases. These have to be put together by the host computer as a string of allophones. This is not difficult, and imposes only a light load on the computer. It is quite possible to produce a reasonable vocabulary without resorting to machine code. The store required for each word is only a handful of bytes.

THE BOARD

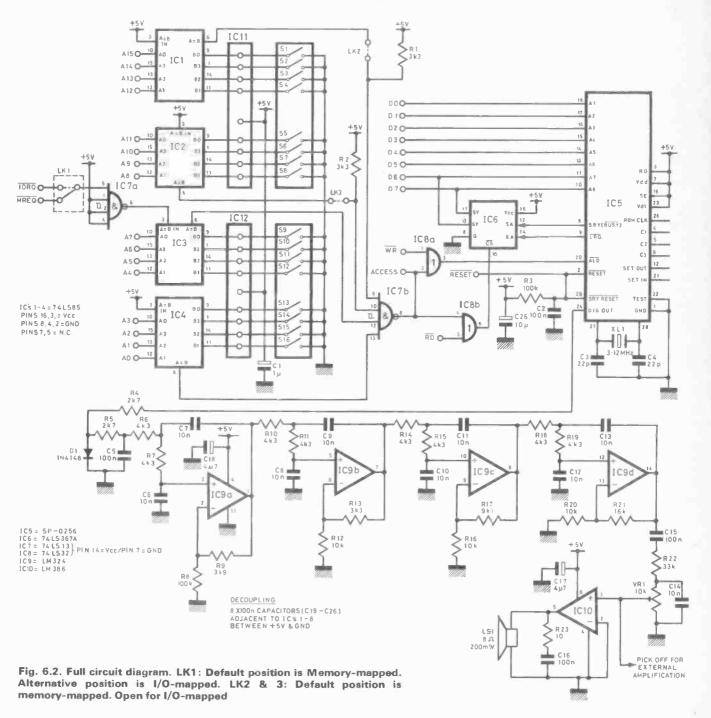
Fig. 6.1 is a block diagram of the Speech system. There are three basic elements, the speech generator, amplification

and the interface to the ULTIMUM motherboard. Fig. 6.2 gives the complete circuit diagram.

The speech board occupies only one memory location (the location to which the allophone code is to be sent (see later). The decoding uses four four-bit magnitude comparators (ICs 1-4) which compare all 16 address lines against a value set on the links 0–15. The magnitude comparators are gated with the Read and Write signals from the motherboard to provide a valid access signal to the speech chip. When the selected location is written to, the byte written is sent to the speech chip. When the same location is read, the two status bits (BUSY and LOAD REQUEST) are put onto the bus (D7 and D6 respectively). Reading these bits allows the programmer to establish

whether the speech chip is ready to accept another command or still busy issuing the last allophone. As speech is comparatively slow by computer standards, it is quite acceptable to poll these status lines periodically, rather than resort to the more complicated interrupt lines, although this is also possible, as all that is needed is to connect the load request line from the speech chip to the interrupt request line on the edge connector.

The speech chip provides a pulse width modulated signal which has to be converted to an analogue waveform suitable for amplification. This can be done with a simple diode/CR network, but we have chosen the more complete four stage filter (IC9), which imparts a much better 'shape' to the audio signal.



Finally, an amplifier (IC10) is included to drive a small speaker. Alternatively, a 'pick-off' point is available for external amplification, or for mixing with the Sound Card (see next month's article).

ASSEMBLING THE BOARD

Refer to the overlay (Fig. 6.3) for details of component placement. This board has many discrete components (mainly used in the filter).

We suggest that these are inserted *after* you have placed the i.c sockets. The crystal (XTAL1) which provides the timing for the speech chip, should be inserted with care. Avoid bending the leads at the base, as strain can fracture the internal connections. The SP-0256 is the most expensive component on the board, so before inserting it, check for shorts by powering the board up, and check that 5 volts appears on pins 7 and 23 of IC5 (the SP-0256 socket).

The d.i.l. switches (0-15) should be set up as follows:

- 1) Find an unused location in memory.
- 2) Write down the binary value of that location (eg. 0113 hex is 000000100010011 in binary.
- 3) Set the switches according to this binary pattern ie. if bit 0 (the least significant bit) is 0 then close switch (shown in the overlay, Fig. 6.3, and on the board itself).
- 4) Repeat 3 for each switch.

TESTING THE BOARD

The board should be tested with the other cards removed from the ULTIMUM just in case there is a short circuit. Do not insert the board with the power on. The SP-0256 is automatically reset as power is applied. Run the BASIC program listed in Table 6.1, noting that you must set the PEEK and POKE location (LOC1 in the listing) to that set up on the speech board. If nothing happens, check the switches are correct and that the speaker is connected.

MAKING SPEECH

Table 6.1 lists all the allophones and the code which has to be fed to the SP-0256. The basic sequence required to feed allophone codes is as follows:

1) When load request is low, issue of any of the listed allophone codes by writing to the location set up on the decoding switches is possible

- 10 LET LOC1=(speech location)
- **20 RESTORE**
- 30 READ D
- 40 IF D=>64 THEN 80
- 50 IF (PEEK(LOC1) AND 128)<>0 THEN 50; ready to load?
- 60 POKE LOCI,D
- 70 GOTO 30
- 80 GOTO 20; repeat indefinitely
 - 56,1,23,3,17,4,48,15,11,4,13,31,4,29,29,39,19,4
- 100 DATA 40,50,4,40,6,35,4,55,55,12,12,41,55,4,55,55, 7,39,15,11,4
- 110 DATA 20,2,17,4,56,6,12,4,13,7,11,64
- 120 END

Table 6.1. BASIC test program for Speech board

2) While the allophone is being "spoken" the busy line will go low to indicate that the word is being issued. As can be seen, this allows for very simple programming.

There is no one-to-one correspondence between allophones and the written word, so we have to convert each word into its component parts before we can pursuade the speech chip to reproduce it. Of course, the best way of doing this is to write a "speech assembler" program which will break down the word and prepare the code for you, and we have no doubt that some readers will try this, as this kind of program has lots of applications, including speaking documents. The starting point must be to manually assemble your code by breaking up each word, and select the appropriate allophones yourself. To make this a little easier, Table 6.3 includes sample words which illustrate the type of sound associated with each allophone. Once the allophone list has been prepared, all that is required is to send single bytes to the SP-0256 in sequence. We have written a simple BASIC program to send a test phrase:

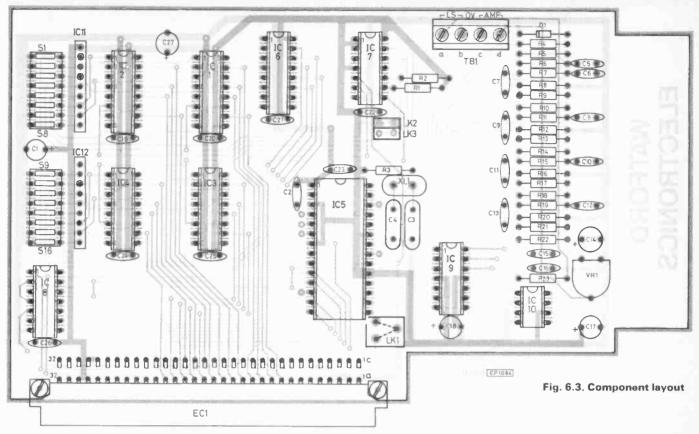
A bird in the hand is worth two in the bush.

Table 6.2. For sample program use these data

- 80 STOP ; preserve sanity
- 90 DATA 20,2,63,52,0,21,2,12,11,2,18,19,2,27,26,11, 0,21,3
- 100 DATA 12,43,2,46,52,29,2,13,31,2,12,11,2
- 110 DATA 18,19,2,63,30,37,64

Hex	Dec.			Hex	Dec.						
00	0	Delay	10ms	16	22	uwl	to	2B	43	ZZ	zoo
01	1	Delay	30ms	17	23	ao	aught	2C	44	ng	anchor
02	2	Delay	50ms	18	24	aa	hot	2D	45	11	lake
03	3	Delay	100ms	19	25	yy2	yolk	2E	46	ww	wool
04	4	Delay	200ms	1A	26	ae	hat	2F	47	xr	repair
05	5	oy	boy	1B	27	hh 1	he	30	48	wh	when
06	6	i	sky	1C	28	bb1	rib	31	49	yy1	yes
07	7	eh	end	1D	29	th	thin	32	50	ch	church
08	8	kk3	comb	1E	30	uh	book	33	51	erl	letter
09	9	pp	pal	1 F	31	uw2	food	34	52	er2	bird
0A	10	jh	dodge	20	32	aw	out	35	53	ow	sew
0B	11	nn l	thin	21	33	dd2	do	36	54	dh2	they
0C	12	ih	sit	22	34	gg3	wig	37	55	SS	vest
OD	13	tt2	two	23	35	vv	vest	38	56	nn2	no
0E	14	rrl	rural	24	36	gg1	guest	39	57	hh2	hoe
0F	15	ax	succeed	25	37	sh	ship	3A	58	or	store
10	16	mm	milk	26	38	zh	azure	3B	59	ar	alarm
11	17	tt1	part	27	39	rr2	brain	3C	60	yr	clear
12	18	dh1	they	28	40	ff	food	3D	61	gg2	got
13	19	iy	see	29	41	kk2	sky	3E	62	el	saddle
14	20	ey	beige	2A	42	·kk1	can't	3F	63	bb2	busines
15	21	ddl	could								

Table 6.3. SPO256 AL2 allophones



The program is given in Table 6.2b. The PEEK and POKE locations will depend on where the speech board is located in memory, and need to be adjusted accordingly.

NEXT MONTH: The Sound board.

COMPONENTS .

Resistors

R1, R2, R13 3k3 (3 off) R3, R8 100k (2 off) R4. R5 2k7 (2 off) R6, R7, R1, R11, R14, R15, R18, R19 4k3 (8 off) 3k9 R9 R12, R16, R20 10k (3 off) 9k1 **R17 R21** 16k R22 33k **R23** 10 All resistors 1W 5%

Potentiometers

VR1 10k Min. Vert. preset

Capacitors
C1 1μ/16V elect.
C2, C5, C15, C16,

 $\begin{array}{cccc} C19-27 & 100n \ cer. \ (12 \ off) \\ C3, C4 & 20p \ cer. \ (2 \ off) \\ C6-14 & 10n \ cer. \ (9 \ off) \\ C14, C17 & 4\mu7/16V \ elect. \ (2 \ off) \\ C28 & 10\mu/10V \ tant. \\ \end{array}$

Semiconductors

IC1-4 74LS85 (4 off)
IC5 SP0256AL2
IC6 74LS367A
IC7 74LS13
IC8 74LS32
IC9 LM324
IC10 LM386
IC11, IC12 4k7 x 8 d.i.l. resistor

Miscellaneous

8 pin d.i.l. socket
14 pin d.i.l. socket (3 off)
16 pin d.i.l. socket (7 off)
28 pin d.i.l. socket
8-way SPST d.i.l. switch (2 off)
3.12MHz crystal XL1
Speaker 8 ohm, 2 in. LS1
2 x 32 way rt. angled Euro plug (DIN41612 A+C)
P.c.b. terminal block
1 metre twin standard cable
WEO8 SPK p.c.b.

Constructor's Note

All kits for the Ultimum system are available from Watford Electronics (see advertisers' Index). Send SAE for price lists of boards now available.

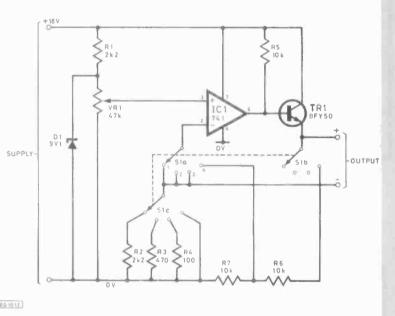
Ingenuity Unlimited

A selection of readers' original circuit ideas. Why not submit *your* idea? Any idea published will be awarded payment according to its merits.

Each idea submitted must be accompanied by a declaration to the effect that it has been tried and tested, is the original work of the undersigned, and that it has not been offered or accepted for publication elsewhere. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought.

Articles submitted for publication should conform to the usual practices of this journal, e.g. with regard to abbreviations and circuit symbols. Diagrams should be on separate sheets, not in the text.

CONSTANT CURRENT VOLTAGE SOURCE



OR any purpose needing a constantcurrent supply, such as charging Ni-Cad cells, this unit provides a remarkably stable current—even shorting the output causes no detectable change in current. The circuit shows switching of three ranges by means of a three pole four way switch, and the fourth position changes the circuit to an equally stable constant voltage supply, a desirable addition to the versatility of the unit only needing two more resistors.

Operation is as follows—the Zener diode provides a reference voltage, part of which is tapped off by VR1 to the non-inverting terminal of the op amp. The output current from the emitter of the transistor is returned to 0V via the resistors R2-4, and the consequent positive voltage at the top end of these is fed to the inverting terminal. The potential of the op

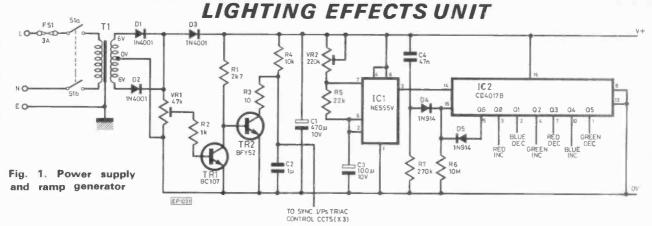
amp output provides the bias for the base of the transistor; if the output current tends to increase, the potential changes, thus reducing the current supplied to the output, so that a stable state is set up. The actual amount of current is governed by the proportion of the Zener voltage supplied to the i.c., so VR I forms a panel control which can be calibrated.

The characteristics of the circuit overall are not quite linear, so a separate dial calibration is needed for each of the resistors R2-4. Their values can be found experimentally for any required current range. The quickest way is to put a meter across the output, and substitute a wire wound variable for the resistor. Rotating VR1 will give the range limits for any given value of the variable, which can be measured, and a suitable fixed resistor chosen.

The ranges of the prototype are given for the values in the drawing, but the current can if necessary be increased to any desired amount, provided only that the transistor used can take it if properly heat-sinked. For currents over about 250 ma, obviously a power transistor is required, but up to that figure a BFY50 on a good heat sink should cope.

The fourth switch position for constant output voltage connects the output return directly to 0V, and puts a resistance across the output. Half of the voltage appearing across this is applied to the i.c., and controls the transistor as before. Positions 1, 2 and 3 of S1 provide the constant current ranges of 1-4 ma, 5-20 ma and 20-85 ma. Position 4 has the constant voltage range of 4-18V.

S. A. R. Guest, Grampound, Truro.



ANY circuits exist to provide exciting effects using coloured lighting, examples such as Sound-to-Light units and Chasers springing immediately to mind; but few exist that may be deployed successfully in a household environment for extended periods of time providing an interesting but slower and more relaxing type of display. Presented here is such a unit which may be used protractedly without excessive fatigue. It may also be of interest to many readers since it contains a voltage controlled dimmer which operates without resort to the more usual and unpredictable arrangement using a light dependant resistor.

The circuit aims to provide the following effect. At switch-on, all three bulbs illuminate. After a time, a regular cycle is set up during which the red bulb slowly increases in brightness until it reaches a maximum when the green bulb begins to light. After this too has reached its maximum level, the red bulb dims. When fully extinguished, the blue bulb begins to switch on whereupon the green bulb is extinguished, to be followed by the lighting of the red bulb and dimming of the blue bulb. The cycle then repeats.

The result of all this is that the colour of the light emitted by the unit cycles approximately every 25 seconds through the entire colour spectrum, beginning at red and changing through yellow-green-blue-magenta and then back to red.

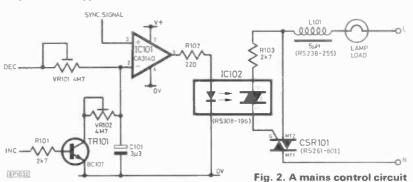
The circuit may be broken down into three sections, these being the ramp generator and power supply, voltage controlled dimmers and logic elements. The ramp generator generates slowly rising and sharply falling waveforms which are synchronised with the mains so that the falling edge of the ramp occurs at mains zerocrossing (see Fig. 1). It operates as follows: unsmoothed d.c. from the transformer is fed via potential divider VR1 and resistor R2 to the base of TR1, so that when the mains voltage is not close to zero, TR1 is switched on. This removes the base current from TR2, cutting it off and preventing it from discharging the capacitor C2. The voltage across C2 therefore represents the type of ramp previously described, and although the rising edge is in fact exponential rather than linear, the approximation is satisfactory in this case

This ramp is sent to the 'sync' input of the mains control circuits and is compared with the voltage across the capacitors (C101 to C301) by the CA3140 comparators, the output of which drive the triac opto-isolators. The higher the voltage across the tantalum capacitors, the more time must elapse before the sync voltage exceeds this voltage, so that the optoisolator's l.e.d. is energised, and the later in the cycle the main triac is fired. Proportional control of the power delivered to the load is therefore obtained, the power beging inversely proportional to the voltage across the capacitor. Three mains control units were constructed, one each for the red, green and blue lamps.

The rest of the circuit consists of the logic required slowly to charge and discharge C101 to C301 in the appropriate manner. A one-of-ten output decade counter (IC2) is connected to an oscillator. If the 555 used is not of the recently available CMOS type (often numbered 7555) then it is strongly recommended that a 22µF/10V electrolytic decoupling capacitor be connected directly across the supply pins of the NE555, otherwise the rest of the circuit may suffer from transients introduced on the supply lines when the chip changes its output state. The period of the oscillator is variable between about a second and approximately 15 seconds or more. During setting up, care should be taken never to set VR2 to its minimum value. The 4017 is connected so that it cycles between only six of the ten outputs (Q0-Q5), since when Q6 goes high, the device is immediately reset. A reset pulse is also applied at switch on via

C4 and R7 to ensure that normal operation commences as soon as possible. Should problems arise during setting up, it should be remembered that the output increasing the light level is the one connected to the transistor discharging C101. Diodes D101, D102 and D103 through to D301, D302 and D303 are necessary to stop the associated capacitor discharging as soon as the corresponding output on the 4017 goes low.

Setting up is accomplished as follows. The presets determining the increase and decrease time (VR101-VR302) should be turned down to their minimum setting. The bulbs should now switch almost instantly between being on and off, rather than fading. VR1 should be adjusted so that the bulbs are as bright as possible while the unlit bulbs remain fully extinguished. VR2 may then be set up to give the required oscillator period (remembering that the full cycle will take six times longer), observing the previously stated precaution. The fade timing presets must now be set up. Wait until the appropriate part of the cycle, then select an 'increase time' preset (i.e. one that discharges C101, C201 or C301) and increase its value. After several cycles have past, the preset should be adjusted so that the bulb just lights fully in the time that the increase input is high. This procedure should then be repeated for all the increase potentiometers. Similarly, the 'decrease' pots should be adjusted so that the associated bulb just extinguishes during the time that the 4017 output is true. This setting up procedure is lengthy and time consuming, but time spent here pays dividends in enhancing the effect.



The bulbs used may be any type of 240V mains bulbs although special care should be exercised in the choice of the blue lamp, since many spotlamp bulbs labelled 'blue' produce a blue/green shade. If spotlamps are employed, then use ones that cast a fairly diffuse pool of light rather than producing three separate spots which would spoil the effect. The prototype currently in operation uses 100W coloured reflector bulbs similar to, but slightly larger than, those used in sound-to-light units, etc. There is of course no reason why larger loads should not be driven providing that the following points are taken into consideration:

1. Make sure that the mains choke is rated for the maximum r.m.s. bulb

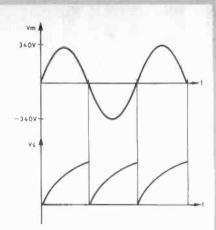
Fig. 3. Showing the relationship between the mains voltage V_m and the sync signal V_n

current plus a suitable safety margin (say 10%).

2. The triac should be rated at about 6 to 8 times the bulb r.m.s. current to allow for the switch-on surges in cold filaments.

It is also probably a good idea to add a fuse on the live side of the bulbs in addition to the single 3A link to protect in the event of any short circuits. All the components are fairly easy to obtain with the exception of the triac opto-isolator which may be obtained from Maplin Electronic Supplies.

N. J. Bailey, Yatton, Bristol.



VERSATILE CONTROLLER

THE uses of this controller have turned out to be virtually legion-originally developed as a precision temperature control for a colour developer water bath to within 0.25°C, it can be used to control beer fermentation, greenhouse and propagator temperature, to turn lights on or off at dusk or when the sun shines, to turn on or off a water pump at some predetermined level, to provide a rain or frost warning-and so on. The only change to suit any particular purpose is in the sensor arrangements, and since these can be included in a DIN plug housing, the unit input is deliberately made universal by means of a DIN socket.

The basic circuit is quite simple, using an input resistance bridge composed of the chain R1-4 and VR1 for two arms, and the sensor socket between both A-B and B-C for the other two. Pin 2 of the i.c. can have the voltage on it altered by rotating VR1, thus setting the operating point, and the line to pin 3 carries a voltage varying with the momentary condition of the sensor. When pins 2 and 3 are at the same voltage, there is ideally no output on pin 6. If pin 3 is positive to pin 2 by even the slighest amount, pin 6 goes into positive saturation-and vice versa. If pin 6 is positive, TR1 turns on and closes the relay. Since the inputs are in bridge formation, the actual value of the supply voltage makes no difference to the operation.

Two features in the diagram may need explanation. The resistor chain R1-4 is broken into sections at three switched sockets, so that VR1 can be plugged in at three different voltage points, giving three overlapping ranges and a much more open scale than if a single potentiometer of say 47k were used across the supply instead. The other odd looking feature is the wiring of the indicator l.e.ds. Obviously the easiest way is to use a set of changeover contacts on the relay, but in the prototype the miniature relay used had only one set of contacts, of mains size, so another method had to be devised. The red l.e.d. for "off" D1 is lit by current sunk by pin 6 when negative, but to avoid damage to the i.c. make R5 as high as will permit an indication. The green l.e.d. D2 is lit by current passing through the relay coil when on. Before connecting D2 choose R8 to allow the relay to just close, and then choose R7 to provide a parallel path which will light D2 and allow the relay to close.

Various sensors may be used; for temperature control a Siemens K164 bead thermistor with a nominal resistance of 22k is ideal. If used in air, all it needs for protection is two or three coats of oil based paint (not cellulose) on it and the wires and joints-probe insulation is vital, and must not be open to moisture. Response will be almost instantaneous. Rx, the balancing resistor, should be about the same resistance as the sensor, whatever kind is used, at the normal state, so 22k is used for the thermistor mentioned. It is mounted inside the DIN plug housing. The sensor lead should be carefully screened to avoid interference, and the screen returned to

For use in water (or beer!) etc., mount the bead in a little piece of the very thin brass ¼in tubing available at model shops, one end closed by a bit of sheet soldered on; fill the closed end for about ¼in with heat sink grease, wrap the bead assembly in a bit of polythene sheet (it must be perfectly insulated from the brass) and push it down into the grease. Seal the cable exit securely with wax or pitch, topped with polyurethane glue to make all tight. If the fluid being monitored will corrode brass or

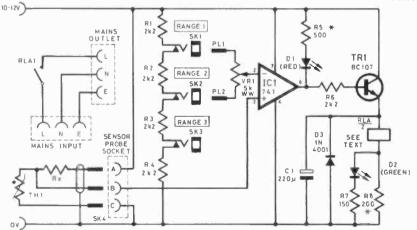
be contaminated by it, a little glass tube will have to be used, which will slow the response but not impair the accuracy.

For light sensing purposes, a CdS l.d.r. is used, with the same proviso about Rx.

For water level detection, a pair of wires about an inch apart and carefully insulated from one another are set to dip into it at the required level. For rain or moisture, a little bit of copper track board is used face up, the tracks connected alternately to the leads. One drop of water bridging them is sufficient to activate the controller. Note that in these cases, the sensor is normally open circuit, so that a high resistance, typically 220k, must be connected both from A to B and from B to C, so as to preserve the d.c. balance of the bridge. To operate with these leakage sensors, the position of VR1 with the probe dry should be such that the relay just does not close. First class insulation is more than ever necessary in these cases.

The rule in working out any operation is always the same—a reduction in the resistance between B and C will turn the controller off, and conversely a reduction of resistance between A and B will turn it on, and if the reverse of this is needed (as for instance if a rise in temperature is to turn something on) change over the A and C leads at the plug, together with Rx.

S. A. R. Guest, Grampound, Truro



I.F. FILTER/AMPLIFIER

for peranger-R.F. MILLINGTON



ONE of the major problems encountered with the PE Ranger CB transceiver (Sept-Dec 1981) was adjacent channel interference. The circuit described here attempts to overcome this problem by increasing the IF selectivity at comparatively low cost.

The CFM2455D IF filter supplied with the Ranger kit is excellent compared to its cost (around 75p), but as its response curve shows its rejection of adjacent channel transmissions is not good. The Ranger board was studied to see how a better filter could be fitted. Consideration was given to the cost of such a modification and it was decided to mount a piggy-back board in a similar manner to the transmitters' output filter board. The circuit uses a small piece of 'Veroboard' which has the same hole spacings as FL100. (0·1").

To overcome the cost of a highly selective ceramic ladder or crystal filters, the circuit in Fig. 1 uses an idea from a model radio control receiver* which cascades the filter

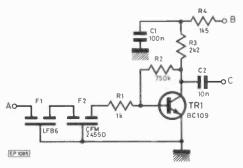


Fig. 1. Circuit diagram of the I.F. Filter/Amp

FL100 with a low cost ceramic ladder filter type CFU455H or LFB6. This arrangement gives an IF curve which has very steep sides, as compared to the sloping sides of the curve given by FL100 only. The extra insertion loss proved to be too much though, reducing the Ranger to a 'locals only' receiver. Selectivity, the object of the exercise, was much improved.

The following IF amp was then evolved to return the gain of the now reduced IF signal to its original level. 6-2V is available at the centre pin of the FL100 position (marked B) and –Ve return is made by soldering the unused tracks of the 'Veroboard' to the can of L106/L107, which also gives the board mechanical stability.

R1 is the CFM2455D output impedance matching resistor. The output impedance of this filter is stated as being 2kohm, but as the input impedance of TR1 is about 1kohm, R1 was made 1kohm.

A BC109, although classed as an audio transistor was used for TR1 and this seemed to work well. R4 and C1 provide decoupling for the supply and the output is taken from the collector of TR1 via C2, which then feeds straight to pin 5 of IC100. (Marked C). The input is from L107, marked A.

R2 is given as 750kohm. Preferred values for the E12 range are 680k and 820k, and either should do if the stated value is not available. There is room for experimentation here, but remember that too much gain will overload the limiting amp in IC100, thereby clipping the wanted signal and causing distortion.

It has been recommended that the oscillator voltage stabiliser diode D100 be reduced to 2.7V to reduce the amount of RF produced. With this filter/amp it was found that the oscillator was now too weak, so the original 5.6V Zener was used. The 100ohm across L105 and the 47kohm from pin 1, IC100 to ground were left in circuit.

CONSTRUCTION

Carefully remove FL100 from the Ranger circuit board, being sure not to overheat the leads or the track on the board, which will lift and tear away. Once removed, use FL100 in position F2 on the filter/amp board.

The components should be laid out on the Veroboard as shown in Fig 2. Don't forget to cut the track in the appropriate places.

Mount all the components before soldering. The three leads for A, B, and C can be made from cut off component leads, and are best left long until the board is soldered to the can of L106/L107.

When the filter/amp board is completed, carefully insert the three leads, A, B, and C (Fig. 1) into the holes left by FL100, and marked A, B, and C in Fig. 2. Note where the link at H9 touches the top of the L106/L107 can, then put the board aside and tin that position on the can, using a fair amount of solder. It is then an easy matter to solder the H9

COMPONENTS ...

Resistors

R1 1k

R2 750k

B3 2k2

R4 1k5

All resistors 1/4 5% carbon film

Capacitors

C1 100nF disc ceramic

C2 10nF disc ceramic

Transistor

BC 109

Filters

F1 CFU455H or LFB6

F2 CFM2455D

Miscellaneous

Veroboard.

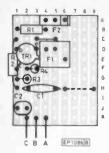


Fig. 2. Veroboard layout for the I.F. Filter/Amp

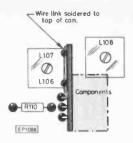


Fig. 3. Mounting details for the I.F. Filter/Amp

link to the can. (Note that this link is soldered to the track side of the board, bridging the unused tracks. Solder leads A,B, and C to their respective pads on the Ranger circuit board.

Do not try to fit the filter/amp board flush with the Ranger board as the amplified signal from the limiting amp in IC100 can be picked up by C2 and fed back in, causing instability. With a gap of about $\frac{1}{4}$ " no feedback problems were experienced on the prototype.

SETTING UP

The core position of L106/L107 may need to be slightly retuned to match the new filter, as with L102/L103. Coil cores should not have to be altered more than $\frac{1}{4}$ of a turn, and with a correctly tuned receiver it is worth while making a mark on the can for that setting before any retuning is done. It is also worthwhile to study the receiver alignment procedure as given in the original article.

CONCLUSION

For an outlay of somewhere around £2.50p the filter makes a worthwhile improvement, putting all but the very close adjacent channel transmissions way down in the white noise, and it would seem that the majority of complaints of 'bleeding over' is more than likely due to poor IF filtering.

Other more expensive filters could also be used using the same mounting principle of a piggy-back board into the holes left by FL100, and in most cases would have the same insertion loss as FL100, so an additional amplifier would not be needed, but this combination of filters seems to be a very effective and low cost alternative.

ACKNOWLEDGEMENTS

*Radio Control Models and Electronics. May 1979. FM Digital Radio Control system by Terry Platt.

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MICRO PROMPT_

The hardware and software exchange point for PE computer projects

Table 1. Software

1F8C	58	CLI		This is the startup routine which	simply enables
1F8D	60	RTS		interrupts	
1F8E	8DFA1F		\$1FFA	Save Accumulator	
1F91	8EFB1F		\$1FFB	Save X register	
1F94	68	PLA	Ψ11 I B	Pull Processor Status Word off	stack
1F95	8DFC1F		\$1FFC	Save PSW	stack
1F98	68	PLA	TIFFC		
	8DFD1F		CIEED	Pull PC low byte off stack	
1F99			\$1FFD	Save it	
1F9C	68	PLA	CIEEE	Pull PC high byte off stack	
1F9D	8DFE1F			Save it	
1FA0	A200		#\$0 0	Clear screen pointer	
1FA2	A928		#\$28	Load Left Bracket character	
lFA4	9D30D0		\$D030,X	Draw on screen	
1FA7	E8	INX		Increment screen pointer	
IFA8	ADFEIF			Get PC high byte	
1FAB	20DC1F	JSR	\$1FDC	Draw on screen	
IFAE	ADFDIF	LDA	\$1FFD	Get PC low byte	
1FB1	20DC1F	JSR	\$1FDC	Draw on screen	
1FB4	A929	LDA	# \$29	Load Right Bracket character	
1FB6	9D30D0	STA	\$D030,X	Draw on screen	
IFB9	ADFEIF	LDA	\$1FFE	Push PC high byte back onto sta	ack
1FBC	48	PHA		-	
IFBD	ADFD1F	LDA	\$1FFD	Push PC low byte back onto sta	ck
1FC0	48	PHA			
1FC1	ADFCIF		\$1FFC	Push PSW back onto stack	
IFC4	48	PHA			
1FC5	98	TYA		Save Y register on stack—it will	he used hy
1FC6	48	PHA		delay count	De asea by
1FC7	AEFFIF		SIFFE	Load delay count into X register	
1FCA	ACFF1F			and Y register	
1FCD	88	DEY	DILL'I	Decrement Y	
IFCE	D0FD	BNE	CIECD		
			\$1FCD	If not zero loop back	
1FD0	CA	DEX	ALECD.	Decrement X	
1FD1	D0FA	BNE	\$1FCD	If not zero branch back	or
1FD3	68	PLA		End of delay—pull Y reg data o	II stack
1FD4	A8	TAY	A.EED	Restore Y register	
1FD5	AEFBIF			Restore X register	
1FD8	ADFAIF		\$1FFA	Restore Accumulator	
1FDB	40	RTI		Return i.e. execute next instructi	on
1FDC	48	PHA		Save the byte on stack	
1FDD	4A	LSR	A	Move the top 4 bits	
1FDE	4A	LSR	A	into the lower 4	
1FDF	4A	LSR	A		
1FE0	4A	LSR	A		
IFEI	20E91F	JSR	\$1FE9	Convert lower 4 bits to Ascii &	output
1FE4	68	PLA		Get next 4 bits	
1FE5	20E91F	JSR	\$1FE9	Convert to Ascii & output	
1FE8	60	RTS		Return	
1FE9	290F		#\$0F	Mask off top 4 bits	
1FEB	18	CLC		Prepare for addition	
1FEC	D8	CLD			
1FED	6930	ADC	⊭ \$30	Add Ascii "zero"	
IFEF	C93A	CMP	#\$3A	If result more than 9 correct to	
1FF1	3002	BMI	\$1FF5	Ascii for A-F	
1FF3	6906	ADC	# \$06		
1FF5	9D30D0	STA	D030,X	Display on screen	
1FF8	E8	INX		Increment pointer to screen	
1FF9	60	RTS		Return	
1FFA				Save accumulator	
IFFB				Save X register	
1FFC				Save Processor Status Word	
IFFD				Save PC low byte	
IFFE				Save PC high byte	Fig. 1. Circui
IEEE				Delay count	ha diaconno

Delay count

MACHINE CODE TRACE

Machine code in RAM can be traced by setting a sequence of breakpoints using the 6502 BRK instruction. If the software is in ROM, however, software interrupts are not possible and another means has to be found. Some processors have a "T-bit" in the status word which when set causes an interrupt after every instruction. This is ideal, but unfortunately not available on the 6502. The nearest solution to the problem is to supply the hardware interrupt input (IRQ) of the processor with a logic level shortly after the start of every instruction. This will cause a branch to an interrupt service routine where the current PC can be displayed on the VDU, allowing the operation of the Monitor and BASIC ROMs to be viewed.

The required signal is most closely provided by the SYNC output from the 6502 chip itself. This output indicates when the processor is carrying out an "instruction fetch" and as such becomes active shortly after an instruction has started. In practice, the SYNC signal must be inverted before feeding it to the IRQ input. This can be done using the circuit in Fig. 1 incorporating one of the spare inverters on the board.

The interrupt pushes the PC high byte, PC low byte and Processor Status Word onto the stack and disables interrupts. The routine given here pulls those bytes off the stack and displays the PC on the top RH line of the screen. This constantly updates and is "transparent" to the operation of BASIC or machine code.

After giving a memory size of 8075 bytes, the routine should be keyed-in using the machine-code monitor and then linked to the IRQ vector by POKE 549,76:POKE 550,142:POKE 551,31.

Once in memory, it can be SAVED to tape using the routine given in the UK101 manual. The trace speed can be changed by POKEs to 8191 ($I = fast\ 127 = mid\ 0 = slow$).

Interrupts are then enabled by including POKE 11,140: POKE 12,31: X = USR(X) to call the startup routine at \$1F8C. Startup should be done from within a program and not in immediate mode, as this is not guaranteed to be successful. The toggle switch in the circuit diagram can be used to turn off the trace at any convenient time.

Two points about the routine—firstly the readout is bracketed to distinguish it from normal screen contents, and secondly it has been placed on the top screen line so that Line-Feeds do not destroy the screen.

Using this facility it is quite interesting to watch the amount of computing required by the various BASIC operations.

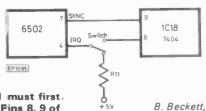


Fig. 1. Circuit diagram. R11 must first be disconnected from IRQ. Fins 8, 9 of IC18 are currently unused.

в. вескетт, Blackpool.

1F8E is the interrupt service routine.

TRANSFORMER DESIGNER

This program was sent in by *Peter Whittaker* of Kliprivier, South Africa. When running, it will take the user through a series of steps leading to the design of a low power transformer. The program takes care of all the calculations.

```
REM PETE WHITTAKER
3 REM DECEMBER 1981
    REM AL MONITORS
6 REM ADVERT
    GOSUB128
8 IFX1=1000RY1=100THENGOTO17
9 ReADXI.YI
11 DATA53547,150,53548,150,53549,150,53550,150,53551,150
12 DATA53580,156,53583,153,53612,156,53615,153,53644,156,53647,153
13 DATA53675,151,53676,151,53677,151,53678,151,53679,151
14 DATA53708,156,53770,156,53772,156,53804,156
15 DATA53805,69,53806,84,53807,69,100,100
16 GOTO8
17 PRINT"
                     TRANSFORMER DESIGNER."
18 FORX=OTO700STEP.1:NEXT
19 CLEAR: GOSUB128
20 PRINT"TRANSFORMER DESIGNER": PRINT"will design all power
21 PRINT"and audio transformers":PRINT including stepup units":PRINT
22 PRINT"Full prompting allows":PRINT"multiple tap options":PRINT
23 PRINT"The user may call on":PRINT"program assumptions to"
24 PRINT"permit safe design on":PRINT"used cores":PRINT
25 PRINT" HIT ESC KEY"
26 IFPEEK (57100) = 222THEN28
27 GOTO26
28 GOSUB128
29 PRINT"*PRIMARY*": PRINT
30 PRINT"One to three primary":PRINT"taps at any voltages
31 PRINT"of your choice may be":PRINT"selected":PRINT
32 INPUT"HOW MANY TAPS ";T1:PRINT
33 IFT1<lort1>3THENPRINT"(1 to 3 PLEASE)":PRINT:GOTO32
34 FORA-ITOTI:ONAGOTO35, 36, 37
35 INPUT"TAP 1 VOLTAGE ";V1:GOTO38
36 INPUT"TAP 2 VOLTAGE ";V2:GOTO38
37 INPUT"TAP 3 VOLTAGE ";V3:GOTO38
38 NEXTA: PRINT
39 PRINT"Frequency range may be":PRINT"between 20hz to 20khz"
40 PRINT" For wide range audio":PRINT"the mid frequency must"
41 PRINT"be input":PRINT
42 IMPUT"DESIGN FREQUENCY";F1:PRINT
43 IFF1<200RF>20000THENPRINT"OUT OF RANGE":GOTO42
44 PRINT"DO YOU WISH TO":INPUT"CORRECT INPUT";B$
44 PRINT"DO YOU WISH TO HIPUT"CORRECT INPUT"; B$
45 IFLEFT(S)R,1)="Y"THEN32
46 GOSUB128 :PRINT"*SECONDARIES*":PRINT"
47 PRINT"Two secondaries may be":PRINT"selected."
48 PRINT"Secondary one allows a":PRINT"choice of one to three"
49 PRINT"taps to ensure design":PRINT"of center or multitap"
50 PRINT"devices":PRINT
55 PRINT The second winding is":PRINT"single ended"
52 PRINT"The second winding is":PRINT"exceed 30 amps ':PRINT
53 PRINT"Windings may be series":PRINT"connected":PRINT
54 PRINT"*SECONDARY 1*":INPUT"HOW MANY TAPS";T2
55 1FT2<10RT2>3THENPRINT"(1 to 3 PLEASE)":PRINT:GOTO54
56 GOSUB128 :PRINT"*SECONDARY 1*":PRINT
 57 FORB=1TOT2:ONBGOTO58 ,59
58 INPUT"VOLTS TAP 1";V4:GOTO61
59 INPUT"VOLTS TAP 2";V5:GOTO61
60 INPUT"VOLTS TAP 3";V6:GOTO61
61 NEXTB: PRINT
```

```
62 PRINT"INPUT CURRENT ": INPUT"IN AMPS SEC.1"; I1: PRINT
63 PRINT"DO YOU WANT A SECOND": INPUT"SECONDARY WINDING"; CS:PRINT 64 IFLEFTS(CS,1) <> "Y"THEN 67
65 INPUT"VOLTAGE SEC.2"; V7:PRINT
66 PRINT"INPUT CURRENT": INPUT"IN AMPS SEC.2"; I2:PRINT
67 PRINT"DO YOU WISH TO": INPUT"CORRECT INPUT";D$
68 IFLEFT$(D$,1)="Y"THEN54 :PRINT
69 GOSUB128 :PRINT"*CORE*":PRINT
70 PRINT"Required core area is":PRINT"dictated by the total"
70 PRINT Required core area is "PRINT" dictated by the total
71 PRINT"Volt/ampere rating of":PRINT"the transformer":PRINT
72 PRINT"In turn it affects the":PRINT"number of turns/volt":PRINT
73 PRINT"the crossectional area":PRINT"is that of the core"
74 PRINT"center leg": PRINT"ie the area of the coil"
75 PRINT"hole opening":PRINT
76 PRINT "Magnetic properties of":PRINT"the core must be input"
77 PRINT"in lines/cm sq.If not": PRINT"known input 0": PRINT
78 INPUT"LINES/cm sq";L
79 IFL=OTHENLETL=10000
80 V8=V4:IFV5>V4THENLETV8=V5
81 IFV6>V4THENLETV8=V6
82 VA=(V8*I1)+(V7*I2)
83 D=(6.5416*SQR(VA))/(5.58*.92):X$=STR$(D)
84 GOSUB128 :PRINT"TOTAL VA
85 PRINT"MINIMUM CORE"
86 PRINT"AREA REQUIRED"; LEFT$(X$,6); "cm sq": PRINT
87 PRINT"WHAT SIZE CORE":PRINT"DO YOU WANT TO
88 INPUT"USE cm sq please";E:PRINT
89 IFE<(.94*D)THENPRINT"TOO SMALL":GOTO87
90 REM T/VOLT
91 F=100000000/(4.44*F1*L*E)
92 XS=STRS(F)
93 GOSUB128 :PRINT"*PRIMARY*":PRINT
94 PRINT"TURNS PER VOLT"; LEFT$(X$,6):PRINT
95 PRINT"NOTE:- all turns are":PRINT"given as total turns" 96 PRINT"from common":PRINT
97 FORX=1TOTI:ONXGOTO98 ,99 ,100
98 PRINTINT(F*V1); "TURNS TO":PRINTV1;" VOLT TAP":PRINT:GOTO101
99 PRINTINT(F*V2); "TURNS TO":PRINTV2;" VOLT TAP":PRINT:GOTO101
100 PRINTINT(F*V3); "TURNS TO":PRINTV3;" VOLT TAP":PRINT:GOTO101
101 NEXT
102 X$=STR$(VA/V1)
103 PRINT"PRIMARY AMPS"; LEFT$(X$,5):PRINT
104 G=SQR((VA/V1)*1.08/(1.55*.7854)):X$=STR$(G)
105 PRINT"WIRE DIAMETER IS:"PRINTLEFTS(XS,6);"mm":PRINT 106 PRINT" HIT ESC KEY":PRINT" TO CONTINUE"
107 IF PEEK (57100)=222THEN109
108 GOTO107
109 GOSUB128
110 PRINT"*SECONDARY 1*": PRINT
111 FORC=1TOT2:ONCGOTO112,113,114
112 PRINTINT(F*V4); "TURNS TO":PRINTV4;" VOLT TAP":PRINT:GOTO115
113 PRINTINT(F*V5); "TURNS TO":PRINTV5;" VOLT TAP":PRINT:GOTO115
114 PRINTINT(F*V6); "TURNS TO":PRINTV6;" VOLT TAP":PRINT:GOTO115
115 NEXTC
116 H=SQR(I1*1.06/(1.55*.7854)):X$=STR$(H)
117 PRINT"WIRE DIAMETER IS":PRINTLEFT$(X$,6);" mm":PRINT
118 IFV7=0 THEN123
119 PRINT"*SECONDARY 2*":PRINT
120 PRINT"TOTAL TURNS FOR": PRINT"SECONDARY 2"; INT(F*V7): PRINT
121 I=SQR(I2*1.06/(1.55*.7854)):X$=STR$(I)
122 PRINT"WIRE DIAMETER IS":PRINTLEFT$(X$,6);" mm":PRINT 123 INPUT"RERUN PROGRAM"; E$:PRINT
124 IFLEFT$(E$,1)="Y"THEN19
·125 PRINT"BYE THEN"
128 FORX=OTO28: PRINT: NEXT: RETURN
```

2716 PROGRAMMER

The circuit of the 2716 (5V) EPROM Programmer makes a simple stand-alone unit which is economical to build. It does not need a microprocessor for its working. In order to input an 8-bit (one byte) data, it employs the popular keyboard circuit published in P.E. Sept. '78. That circuit has become popular, because it directly gives a one byte data-word with two key pressings. Normal keyboard encoder i.c.s (such as the latest 74C922) can give only a 4-bit word, and one needs a micro to rotate the bits left four times to assemble an 8-bit word into the Accumulator of the microprocessor. As a proof of its popularity, it appeared, though somewhat modified, again in P.E. April '80, page 62. So, many P.E. readers will have the keyboard already constructed.

This keyboard, together with a few TTL i.c.s and some i.e.d.s can make a useful

EPROM Programmer. The complete circuit is given in Fig. 1. There is a 10 pole 2 way slide switch connecting the keyboard output to the EPROM data lines. (This switch could be a cassette recorder spare part.) While reading the EPROM (after programming), the switch is kept in the open position and then \overline{CS} pin goes low. The eight data l.e.d.s use two 7400 gates to drive them. In the program mode, the switch is closed, thus connecting to the keyboard outputs, and then \overline{CS} goes high, as required for programming. The address lines are grouped into AO–A7 and A8–A10.

The A8 to A10 are selected high or low using three 2 way slide switches, which are wired to +5V and ground, so that one can choose a 0 or 1 for these address bits. These bits select the page on the EPROM to be programmed or read. The lines A0-A7 are fed from the outputs of the two

7493 4-bit counter i.c.s, which count the address. Incrementing the address is by the toggle switch 'Addr. Incr.' which gives one pulse at a time, so that one location after another of EPROM can be successively programmed. The 11 address lines are indicated by the 11 l.e.d.s at all times. The programming pulse of 50ms is given by the pulser switch which initiates the 74121 monostable to give the 50ms pulse to the PGM pin 18 of the 2716. The 25V supply needed for programming is also selected by a separate 25V-to-5V changeover switch. This separate switch is safer than incorporating it within the 10 way slide switch.

Programming is done by sequencing the address by the Addr. Incr. switch after initially resetting the Address lines to 00 by the push to open switch 'Zero Addr.'. Data is entered on the keyboard and after checking up by looking at the l.e.d.s, the pulser

switch is pressed once and released. That byte would be programmed into the EPROM. The procedure can be repeated for the next address location and so on.

For reading/verifying, the slide switch is opened from the keyboard side and the address is selected by the 'Addr. Inc.' pulser so that the data l.e.d.s indicate the data already in the 2716 at that address.

EXMON DISASSEMBLER

The UK101 Extended Monitor contains an excellent disassembler, but it will only list a given number of lines at one time, depending on the contents of location \$099D. It would be more convenient when a printed listing is desired, to be able to specify the start and end addresses of the program. This may be achieved by using the short program given here, which occupies locations \$07DF to \$07FF.

There are two spare letters available within Exmon, namely J and U. One of these may be used to call the routine, and the relevant locations (i.e. for J:\$0974, 5) should be loaded with #\$DF and #\$07. It is then simply a matter of typing J (start), (end +1) to use.

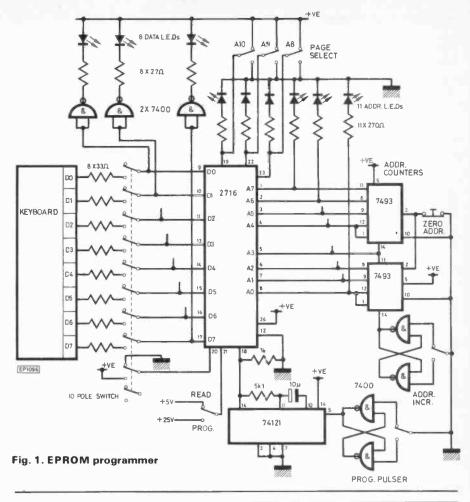
L. J. Dolman, Norwich.

PROGRAM LISTING

07DF	20110B	JSR	\$0B11
07E2	85D5	STA	\$D 5
07E4	A5DB	LDA	\$DB
07E6	85D6	STA	\$D6
07E8	20260B	JSR	\$0B26
07EB	A901	LDA	#\$01
07ED	85D8	STA	\$ D8
07EF	A900	LDA	#\$00
07F1	209E09	JSR	\$099E
07F4	38	SEC	
07F5	A5D5	LDA	\$ D5
07F7	E5DE	SBC	\$DE
07F9	A5D6	LDA	\$D6
07 F B	E5DF	SBC	\$DF
07FD	90F0	BCC	\$07EF
07FF	60	RTS	
:			
PUT	#\$DF	IN	\$0974
PUT	#\$07	IN	\$0975
	ENTER JX		Ϋ́

BASIC TIDY-UP

Sir—After getting to grips with a UK101 computer I discovered two very annoying features about it. The first was the "Out Of Memory" error on the first immediate instruction after a warm start (caused by a stack error) and the second was the fact that the OK message was output to cassette when saving BASIC programs, thus causing a "Syntax" error on LOADing.



I include a short BASIC program to load some machine code which will cure both these faults. An added bonus is that the OK message can be changed to anything one wants; I have made it output READY instead but anyone with machine code experience will be able to change this. The machine code resides at 0222 up to 0245 inclusive. The BASIC can be destroyed after the program is run. After a cold start the two vectors have to be reset for the new routine so one must type in the two lines of POKE (lines 10, 20) in immediate mode.

N. J. Young, Bristol.

CEGMON ERROR MESSAGES

Sir—Since there does not seem to be much information about the UK101/Superboard in the mainline journals I would like to see Micro Prompt monthly.

Although the latest microcomputers have high resolution graphics, many of them do not have an auto-repeat keyboard, a hardware monitor and standard chips, like the UK101.

Here is a quick tip on how to obtain standard error messages with Cegmon.

50000 For X=576 TO 580: READ A:
POKE X,A: NEXT: POKE
538,64: POKE 539,2
50010 DATA 41,127,76,155,255

M. P. Winter, South Glamorgan.

PLEASE

Micro Prompt has been devised to provide an exchange point for ideas which apply to any P.E. computer project—it does not have to be related to the UK1011 Any project which is either computerised (uses a microprocessor), or which is intended to be a computer peripheral, may be discussed here. Submitted material may be hints, suggestions, hardware modifications or software, although software should not be lengthy.

It should be emphasised that material presented in Micro Prompt has not necessarily been proved by us. Neither can compatibility with all generations of the computer equipment to which it relates be guaranteed.

NOTE

¹⁰ POKE 1,34 : FOKE 2,2

²⁰ FOKE 4,38 : POKE 5,2

³⁰ FOR T=546 TO 581

⁴⁰ READ A : FOKE T.A

⁵⁰ NEXT

⁶⁰ DATA 162, 252, 154, 76, 116, 162, 169, 13, 32, 105, 255

⁷⁰ DATA 169, 10, 32, 105, 255, 162, 8, 189, 61, 2, 32, 45

⁸⁰ DATA 191, 202, 208, 247, 96, 10, 13, 46, 89, 68, 65, 69, 82

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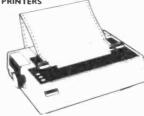
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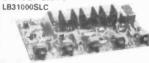
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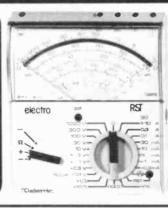


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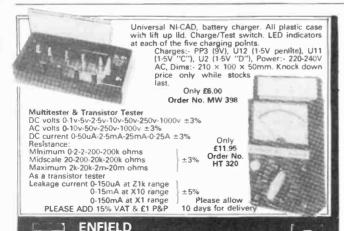


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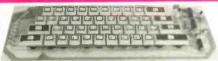
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