## PRACTICAL

# FEBRUARY T9EO OES 



## 

 OCTOBER 1979

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The Compukit UK101 has
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exira. 40 line expansion interface socket on board for attachment ol extender card containing 24K RAM and disk controller. (Ohio Scientific compatible).
. 6502 machine code accessible through powerful
2 K machine code monitor on board.
High quality thru plated P.C.B. with all I.C.'s mounted on sockets
- Professional 52 Key keyboard in 3 colours - soff. ware polled meaning that all debouncing and key decoding done in soltware
COMMANDS
CONT LIST NEW NULL RUN
STATEMENTS DEF DIM END FOR
CLEAR DATA $\begin{array}{lllll}\text { CLEAR DATA DEF } & \text { DIM } & \text { END FOR } \\ \text { GOTO GOSUB IF GOTO IF. THEN INPUT LET }\end{array}$ NEXT ON GOTO ON GOSUB POKE PRINT REAC REM RESTORE RETURN STOP
EXPRESSIONS
OPERATORS
\& NOT.AND.OR $>\lll \ll=$ RANGE $10^{-32}$ to $10^{+32}$
VARIABLES
A.B.C $\quad Z$ and $\pm$ wo leller variables

The above can all be subscripled when used in an array Siring variabies use above names plus $\$$.e g AS

-8K Microsoft Basic means conversion 10 and from Pet, Apple and Sorcerer easy. Many compatible programs already in print. SPECIAL CHARACTERS
(4) Erases line being typed. then provides carriage return, line feed.

Erases lasi character typed.
CR Carriage Return - must be at the end of each line.

Separates statements on a line
CONTROL/C Execution or printing of a list is interrupted at the end of a line.
"BREAK IN LINE $X X X X$ "" Is printed, in dlcating line number of next statement to be executed or printed.
CONTROL/O No outputs occur until return made to cummand mode If an Input state ment is encountered. either another CONTROLIO is typed, or an error occurs.
? Equivalent to PRINT

Simple Soldering due to clear and consise instructions compiled by Dr. A.A. Berk, BSc.PhD

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Absolutely no extras.

Available ready assembled and tested, ready to go for
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FUNCTIONS
ABS (X)
ATN(X)
$\begin{array}{ll}\text { LOG }(X) & \text { PEEK }(1) \\ \text { SPC }(1) & \text { SQR }(X)\end{array}$
FRE $(X) \quad \operatorname{INT}(X)$
$\operatorname{SGN}(X) \quad \operatorname{SIN}(X)$
SGN(X)
USA(I)
$\operatorname{SIN}(X)$
STRING FUNCTIONS
ASC(X\$) CHR\$S(1) AIGHT \$(X\$.I)
LEN(X\$) MID\$(X\$.J.J)
LEN(X\$)
VAL(X\$)

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|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| TAG-END TYPE: 450V: 100uF 180m; 70V: 4700 1650; 64V: 2500 980; 3300 1300: 50V: 2200 99p; 3300 105p; 40V: 15,000 399p; 4700 120p; 4000 92p; 3300 93p; 2500 85p; 2200 85p; $2000+2000$ 120p; 30V: 4700 90p; 25v: $6400105 p ; 4700$ 85p; 3300 80D; 220060 D . |  |  |  |  |  |  |
| TANTALUM BEAO CAPACITORS $2.2 \mu \mathrm{~F}, 3.3,4.7,6.8 .25 \mathrm{~V}: 1.5,10,20 \mathrm{~V}$ : $1.5 \mu, 16 \mathrm{~V}$ : $10 \mu \mathrm{~F}$ 13p each. <br> 16 V : $15 \mu, 2225 \mathrm{p}$; 47, 100, 22040 p . <br> 10v: $15 \mu, 22,3320 \mathrm{p} ; 10035 \mathrm{p}$; 8 V : <br> $47 \mathrm{~N}, 68,100$ 30p; $3 \mathrm{~V}: 100$ 20p. |  |  | POTENTIOMETERS (A8 or EGEN) Carton Track, 0.25W Log 80.5 W Linear values. <br> $500 \Omega 1 \mathrm{~K} \& 2 \mathrm{~K}$ (LIN ONLY) Single $5 K \cap-2 M Q$ single gang $5 K \Omega-2 M Q$ single gang $D / P$ switch $5 \mathrm{~K} \Omega-2 \mathrm{MQ}$ single gang D/P $5 \mathrm{~K} \Omega-2 \mathrm{M} \Omega$ dual gang stereo $5 K \Omega-2 M \Omega$ dual gang stereo |  |  |  |
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|  |  |  | PRESET POTENTIOMETERS <br>  |  |  |  |
| 10 pF to 1 nF . 6p. 1.5 nF to 47 nF 10p. |  |  |  |  |  |  |
| 3.3 .4 .7 6.8. 8.2. 10 . 47, 18, 68, 75, 32, 85: 100, 120, 150, 180. $200,220,9900$,250,270 250.360,390$490,470,6008$ 820 pF 16 peach . 1000.2000 pF 20 p. | TRIMMERS miniature <br> 2.5pF:3-10pF; <br> $3-30 \mathrm{DF}, 3-50 \mathrm{OF}$ $5-25 \mathrm{pF}, 65 \mathrm{p}$ 22 p <br> 5-25pF; 65pF 88pF 30p |  |  | AESISTORS-Erie make $5 \%$ carbon Miniature HIgh Stabibity. Low Noise |  |  |
|  |  |  |  | $1 \mathrm{~W}{ }^{20}$ | E12 ${ }^{\text {Ep }}$ |  |
|  |  |  |  |  |  |  |
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| 810 AY-1-0212 A80 589 | LM 380 | 375 80 | SN76023N 140 SN76023ND 130 | $\begin{array}{ll}74500 & 60 \\ 74504 & 73\end{array}$ | ITEX |  |
| AY-1-1313A 660 | LM381N | 145 | SN76033N 175 | 745132350 | 7400 | 11 |
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Set or clear break point Restore from break Load from tape
Store on tape
Go (recalls last address used)
Reset
Monitor features
System program
Set of sub-routines for use in programming Powerful de-bugging facility displays all internal registers Tape load and store routines

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Modulates the attack, decay and filter characteristics of a signa from most audio sources, producing 8 different switchable effects that can be further modified by manual controls.

Basic parts with foot swirches KIT 42-
Basic parts with panel switches KIT 42-2
PCB \& layout chart PCB 42A 1.67

## ELEKTOR DIGITAL REVERB UNIT

A very advanced unit using sophisticated i.c. techniques instead of mechanical spring lines. The basic delay range of 24 to 90 ms can be extended up to 450 mS using the extenslon unit. Further delays can be obtained using more extensions.
$\begin{array}{llr}\text { Main unit basic component kit } & \text { KiT 78-1 } & \mathbf{8 4 9 . 9 9} \\ \text { Main unit PCB (as published) } & \text { PCB 9913 } & \mathbf{E 3 . 6 9}\end{array}$ $\begin{array}{lll}\text { Main unit PCB (as published) } & \text { PC8 9913 } & \text { £3.89 } \\ \text { Extension unit basic component kit } & \text { KIT 78-2 } & \mathbf{8 4 7 . 6 9}\end{array}$ Extension unit PCB (as published) PCB 788 E1.16

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## ELEKTOR ANALOGUE

## REVERB UNIT

Using i.c.s instead of spring-lines the main unit has a maxłum delay of Up to 100 mS , and the additional set extends this up to 200 ms . May be used in either mono or stereo mode.
$\begin{array}{lll}\text { Main unit basic component sés } & \text { KIT 83-1 } & \text { £29.49 }\end{array}$ Additional Delay basic components KIT 83-2 £20.07 PCB (as publ.) to hold both kits PCB 997

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## P.E. GUITAR MULTIPROCESSOR

An extremely versatile sound processing unit capable of producing, for example, flanging vibrato, reverb, fuzz and tremolo producing, for ex fascinating sounds May be used with most etec tronic instruments. Set of basic component kits KIT 85-3 £43.75 Set of PCBs \& layour charts KIT 85-4 $£ 10.62$ Set of text photocoples $\mathbf{~} 1.52$

## P.E. PHASER

An automatically controlled 6-stage phasing unit with integra oscillator

Set of basic components, incl.
PCB \& chart
KIT 88-1 E10.14 Text photocopy

## ELEKTOR PMASING8.

## VIBRATO UNIT

Includes manual and automatic control over the rate of phasing \& vibrato, and has been slightly modified to also include a 2 -input
mixer stage.
Set of basic components
$\begin{array}{ll}\text { KIT 70-1 } & \text { C19.11 } \\ \text { PCB 70A }\end{array}$ Text photocopy

PCB 70A

## P.E. PHASING UNIT

A simple but effective manually controlled phasing unit Set of basic components inct
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## PHASING CONTROL UNIT

For use with Phasing Kit 25 to automatically control rate of phasing.
PCB \& chart
KIT 36-1
f5.21

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P.E.SWITCMEDTONE

TREBLE BOOST
Provides switched selection of 4 preset tonal responses. Set of basic components.
PCB \& chart KIT 89-1 83.82

## P.E. TREBLE BOOST UNIT

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Set of basic components, KIT 53-1
PCB ${ }^{\text {chart }}$ Khal

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PCB (as published)
KTT 82-1 $\quad$ E16.61

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Sophlsticated versatile fuzz unit including variable controls affecting the fuzz quality whilst retaining the attack and decay and atso providing filtering. Can be used with other electronic in-
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KIT 56.1 $87 . \mathrm{E}^{2}$
PCB \& layout chart
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Set of basic components.
PCB \& chart
KIT 91-1 $£ 5.01$

## TREMOLO UNIT

A slightly modified version of the simple P.E. unit.
Set of basic components.
PC8 \& chart KIT 54-1 E3.23

## GUITARFREQUENCY DOUBLER

A slightiy modified and extended version of the P.E. unit.
Set of basic components.
PCB \& chart
KIT 74-1 $\quad$ 4.97

## P.E. GUITAR SUSTAIN

Maintains the natural attack whilst extending note duration
Basic components, foot switches,
PCB \& chant
Basic components, panel switches,
Basic compon
KIT 75-1 £5.64
PCB \& chart
KIT 75-2 $£ 4.08$

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Can be controlled manually or by integral automatic control. Set of basic components,
PCB \& chart
KTT 51-1 53.99

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Extracted from the P.E. Minisonic.
Set of basic components. PCB \& chant

KIT 60-1

## WIND \& RAIN EFFECTS UNIT

A slightly modified version of the original P.E. unit. Set of basic components,
PCB \& chart
KIT 28-1
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P.E. ENVELOPE SHAPER

## WITHOUT VCA

Provides full manual control over attack. decay, sustain and release functions, and is for use with an existing VCA.

Set of basic components,
PCB \& chart
KIT 44-1 $\quad$ E5.24
P.E.ENVELOPE SHAPER

WITH VCA
Has an integral Voltage Controllad Amplifier, and has full manual control over the A, D,S,R functions

Set of basic components,
PCB \& chant
KIT 50-1
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## P.E. GENERATOR

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PCB \& layout chart
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SYNTHESISER-INTERFACE
Allows external inputs such as guitars. microphones etc., to be processed by synthesiser circuits.

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PCB \& chart

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Power Supply components. PCB \& chart
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| SJ21 | Large 71/" Mains Neon Tester' scre | 0.85 |
| SJ22 | Small pocket size 'Mains Neon Tester' | 0.55 |
| SJ23 | Siemens 220v AC Relay OPOT contacts 10 amp rating - housed in plastic case |  |
| SJ24 | Black PVC tape (i) $15 \mathrm{~mm} \times 25 \mathrm{~m}-$ strong tape for electrical \& household use 0.35 per roll 1.60 |  |
| S. 25 | 100 Silicon NPN uransistors all perfect \& coded mixed types with data \& equivalent sheet | 2.50 |
| S. 26 | 100 Silicon PNP transistors all perfect \& coded mixed types and cases data and equivalent |  |
| S. 27 | 50 Assorted pieces of SCR's diodes \& rectifiers incl. stud types all perfect - no rejects fully coded - data incl. |  |
| SJ28 | 20 TTL 74 series gates - assorted 7401 - 746 |  |
| S.J33 | PC Board - mixed bundle PCB fibregiass $/$ paper single \& double sided - super valuel | 0.75 |
| SJ34 | 200 sq . ins. (approx) copper clad paper board | 0.8 |
| SJ35 | 100 sq. ins. (approx) copper clad fibre glass | 0.80 |
| SJ49 | 8 dual gang carbon pots log \& lin mixed value |  |
| SJ50 | 20 assorted slider, knobs - chroma/black | 1.0 |
| SJ61 | 1 Switchbank 5 way incl. silver knobs | 0.5 |
| SJ52 | 1 pak of vero board approx 50 sq , ins mixed | 1.00 |
| SU53 | 1 Mammoth I.C. Pack: approx. 200pcs assorted fall-out integrated circuits including logic 74 series, linear-audio and O.T.L many coded devices but some unmarked - you to identify |  |
| SJ54 | 20 slider pots mixed values \& sizes | 1.00 |
| SJ56 | 6100 K lin 40 mm slider pots | 0.50 |
| S. 157 | 6100 Klog 40 mm slider pots | 0.50 |
| SJ58 | 61 Klin 40 mm slider pots | 0.50 |
| S.559 | 65 K lin 40 mm slider pots | 0.50 |
| SJ60 | $45 \mathrm{~K} \log 60 \mathrm{~mm}$ single | 0.50 |
| SJ6 1 | 4 100K $\log 60 \mathrm{~mm}$ single | 0.50 |
| SJ62 | 515 mm chrome knobs standard push fit | 0.50 |
| SJ63 | 1 Instrument knob - black winged $\mathbf{1} 29 \times 20$ m with pointer $f^{\prime \prime}$ standard screw fit | n) |
| S. 64 | 1 Instrument knob - blackusilver aluminium top (17 $\times 15 \mathrm{~mm})$ f" standard screw fit | 0.12 |
| MET | ASE DUAL S LIDER POTS: $\mathbf{4 5 m m}$ travel |  |
| SJ65 | 10K log |  |
| SJ66 | 100K lin 0.2 |  |
| S.J67 | Chrome slider knobs to fit o. |  |
| SJ6B | ZTX300 type transistor NPN pre-formed for P/C Board cotour coded blue - all perfect | 1.00 |
| SJ69 | 30 2TX500 type transistor PNP pre-formed for P/C Board colour coded white - all perfect | 1.00 |
| SJ70 | 25 BC 107 NPN TO106 case perfect transistors code C1359 | 1.00 |
| S. 711 | 25 BC1 77 PNP TO106 casu perfect transistors code C1395 |  |
| SJ72 | 42 N3055 silicon power NPN transistors TO3 | $\infty$ |
| SJ73 | 6 TO64 SCRs 5 Amp a ssorted $50 \mathrm{v}-400 \mathrm{v}$ all coded |  |
| SJ74 | B way ribbon cable - colour coded individually insulated solid tinned copper conduction |  |
|  |  |  |
| S. 75 | FM coax cable - plain copper conduction cel polythene insulated and plain copper braided PVC sheath - impedance 75 ohms 0.10 | llular d |
| S. 78 | 1 Board containing $2 \times 5$ pin DIN sockets 180 0 2-2 pin OIN loudspeaker sockets | 0.30 |
| SJ77 | A 5 pin DIN $180^{\circ}$ chassis/normal socket incl. OPOT switch | 0.20 |
| SJB3 | 5 Germ. OCP71 type photo transistors | 1.00 |
| SJ84 | $10 \mathrm{B0131}$ NPN transistors low Hfe rejects | 0.50 |
| S.85 | 6 PNP Darlington Power Transistors T0-126 | 0.50 |
| SJ86 | 5 PNP TO-3 germ. power transisiors at VLTS10-20VCB | 0.50 |
| SJ87 | 20 Asst. heat sinks T01/5/18/92 | 0.50 |
| SJBB | 2 Post Office relays | 0.50 |
| SJ189 | 20 Mixed values 400 mW zener diodes 3-10v | 1.00 |
| SJ90 | 20 Mixed values 400 mW zener diodes $11-33 \mathrm{v}$ | 1.00 |
| SJ91 | 10 Mixed values 1 W zener diodes 3-10v | 0.50 |
| S.922 | 10 Mixed values iW zener diodes 11-33v | 0.50 |
| SJ95 | B Slilicon Bridge Rectifers up to 4Amp |  |
|  | $200 v+$ Data | 1.50 |
| SJ96 | 1 Battery holder to take $6 \times$ HP7's | c0.10 |
| 16168 | 5 assorted ferrite rods | 0.50 |
| 16169 | 2 tuning gangs MW/LW | 0.50 |
| 16170 | 50 meters asst. colours single strand wire | 0.50 |
| 16171 | 10 Reed switches | 0.50 |
| 16172 | 3 Micro switches | 0.50 |
| 16173 | 16 assorted pots | 0.50 |
| 16177 | 1 pack assorted hardware | 0.50 |
| 16178 | 5 Main slider switches assorted | 0.50 |
| 16179 | 1 pack assorted tag strips | 0.50 |
| 16180 | 15 a ssorted control knobs | 0.50 |

[^1]
## BREADBOARD

AT THE time of writing the Breadboard exhibition is pulling in the crowds in London and the editorial staff of PE are at full stretch manning the stand, visiting exhibitors and producing this issue-we hope it doesn't show! Breadboard looks like becoming the premier event for the electronics hobbyist. In only its second year it has attracted large crowds, is very well presented and has an excellent atmosphere-even though it is sometimes difficult to talk to people over the raucous noise being generated by various synthesisers, organs, discos etc. (organisers please note!).

An exhibition such as this gives us a chance to meet casual and dedicated readers. We take the opportunity to discuss various projects and enquire into your views on PE. Thankfully most are full of praise and often some new project ideas get thrown up for our consideration. Some, of course, are not so happy-unfortunately we have failed to please them. It would appear that in these cases we are not giving enough space to their particular subject or, more commonly, we are giving
too much space to another facet of our hobby in which they are not interested.

The problem is, having talked to a number of readers, often with widely varying views, just what do we do with all the information. It is all too easy to twist it around so that it fits in with our own views, or to balance out two divergent attitudes and take the middle path; which may in fact please neither party.

For instance, two comments which came up were (a) we carry too many microprocessor oriented articles and (b) we give too much space to music and audio projects. Now we could please both parties by cutting back on these subjects, but wait, we know these are very popular areas by the number of kits and components sold2000 Compukits (at $£ 250$ each) at the last count and excellent quantities of mixers, guitar sound multiprocessors etc. So we would probably offend many readers by cutting.back on either subject. We do try to keep the balance right, to be aware of new trends and to provide the right information at the right time but it's not easy to please everyone.

## PROJECTS

One thing that fascinates us is that virtually all the comments are concerned with projects. Although we try to publish about five projects, or parts thereof, each month these normally make up less than half of our total number of editorial pagespresumably everyone is over the moon with the rest of the contents?

Another interesting angle is uncovered when one enquires as to how many projects most readers construct during a year-the average is probably about one project per reader per year. So why are some readers so much in favour of reading about their pet subject but so much against learning, or even just reading, about ideas and circuitry from another discipline? Any comments?

Finally, our thanks to all those who visited our stand at Breadboard. To those who live too far away or who just could not come along-it's a great event-if you get the chance we would be pleased to see you next time.

We hope to publish a review of the exhibition next month; our apologies to those who have seen it all first hand.

Mike Kenward

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## Technical Queries

We are unable to offer_any advice on the use or purchase of commercial equipment or the incorporation or modification of designs published in Practical Electronics.

All letters requiring a reply should be accompanied by a stamped, self addressed envelope and each letter should relate to one published project only.

Components are usually available from advertisers; where we anticipate supply difficulties a source will be suggested.

## Back Numbers

Copies of most of our recent issues are available from: Post Sales Department (Practical Electronics), IPC Magazines Ltd., Lavington House, 25 Lavington Street, London SE1 OPF, at 75 p each including In land/Overseas $p$ \& $p$.

## Binders

Binders for PE are available from the same address as back numbers at $£ 3.75$ each to UK or overseas addresses, including
postage and packing, and VAT where appropriate. Orders should state the year and volume required.

## Subscriptions

Copies of PE are available by post, inland or overseas, for $£ 10.60$ per 12 issues, from: Practical Electronics, Subscription Department, Oakfield House, Perrymount Road, Haywards Heath, West Sussex RH 16 3DH. Cheques and postal orders should be made payable to IPC Magazines Limited.


## AUDIO VISUAL

Two new $A V$ machines have just been launched on the market. The 340 model is a cassette recorder with four identical audio channels, each with full metering facilities and Dolby Noise Reduction. Each channel has two inputs, microphone and line, a fixed level

line output, and a controlled output which can give in excess of +8 dBm .

Independent record selectionvis provided for each pair of tracks to facilitate stereo recording (tracks 1 and 2) or all four tracks simultaneously. If required, tracks 1 and 2 can be recorded first then tracks 3 and 4 added whilst replaying tracks 1 and 2. Alternatively, tracks 1 and 2 can be recorded after tracks 3 and 4.

The 330 model has two audio channels with a separate sync track for audio visual applications.

The two audio channels have full metering facilities and Dolby Noise Reduction and each audio channel has the same specification as the 340 . They sync channel also provides full metering facilities and selection for the use of normal and special tapes.

When the 330 is used with external sync pulse coding/decoding equipment, the sync channel has a single line input and a line output. It also has an internal sync pulse generator triggered by a button on the front panel to provide a recorded pulse for direct connection to a projector.

For further details including price and delivery contact: Neal-Ferrograph, Simonside Works, South Shields, Tyne \& Wear NE34 9NX.

## FLUKE DMM

Microprocessor techniques have allowed Fluke to incorporate some very useful features in their latest low cost $4 \frac{1}{2}$ digit 8050A DMM. This highly accurate bench/portable model with 39 measurement ranges and nine functions also provides unique dB computing and offset modes in addition to a high performance true r.m.s. capability.

In the dB mode, the 8050A DMM allows the user to call up any of 16 reference impedance levels from 8 to 1.200 ohms and to display the readings directly in dBs.

Additionally, a reference/offset mode allows any input signals to be stored either as a reference value for relative dB readings or as an offset against any reading. In offset mode, the user can zero-out any lead resistances for really high resolution impedance measurements or set up a reference offset and display
only the variance from that reading.
These absolute and relative dB modes with offset greatly simplify measurements in audio, amplifiers and telecommunications circuits as .well as in production testing where only the variance from the stored value may be required. The offset facility is available on all functions such as a.c./d.c. volts or amps, resistance or conductance.

The high resolution $4 \frac{1}{2}$ digit l.c.d. display is matched by a basis d.c. accuracy of 0.03 per cent specified over a full year. A.c. or d.c. measurements can be made down to $10 \mu \mathrm{~V}$, 10 nA or 10 milliohms.

In addition to its volts, ohms and amps ranges, the 8050 A also has two conductance ranges for high impedance measurements to


100,000 Megohins, as well as low power ranges for in-circuit measuring.

A wide range of accessories such as high voltage probes, current transformers, shunts, temperature and r.f. probes, remote hold probe, battery pack, and safety leads make the 8050 A a complete measurement system for the bench or field.

The 8050 A is priced at $£ 199$ ex. VAT and carriage.

Fluke International Corporation, Colonial Way, Watford, Herts WD2 4TT.

## BOOTS VIDEO

All Boots audio departments are now selling the Ferguson VHS Videostar recorder (Model 3 V 00 ) which has a maximum recording time of 3 hours.

The 3V00 has a remote hand-held "pause unit" which can be used to edit unwanted material during recording or playback. Boots

will also carry a wide range of blank video tapes not only for the Videostar and other VHS recorders but also for machines using VCR and Beta format tapes.

Also available is a full colour catalogue of 45 pre-recorded programmes and feature films.

The price of the $3 V 00$ is $£ 595.00$ with blank cassettes from $£ 6.95$ to $£ 16.95$ and prerecorded films from $£ 17.50$.

## ELECTRONIC NOTEBOOK

Like the first model introduced last year, the Toshiba LC-1038MN calculator offers alpha-numeric facilities which has now been expanded to a full ten digit alphabetic and/or numeric entry and display, plus sign. There is an independent 30 -register memory bank, each register able to retain data consisting of 10 -alphabetic characters and 10 -numerals. The addition of a 26 -location world-time display, plus clock/calendar and alarm. There is instant retrieval of the world-time display; the calendar indicates month, date and day of

week; and the alarm can be set up to one year in advance and to prompt an alpha display.

The calculator is ideal for the storage of information in constant use, but which is subject to frequent change such as currency exchange rates; share buying and selling prices; bank and audit card balances; train and plane departure and arrival times; stock levels; metric conversion factors; travellers cheque numbers.

The LC-1038MN operates on batteries lasting around 9,000 hours; is sized $70 \times 10 \times$ 137 mm and weighs $80 \mathrm{~g}(2.80 \mathrm{z})$. It is priced around $£ 75$, plus VAT.

## SAFETY TESTER

Clare Instruments Limited have developed a portable safety test unit for checking double insulated and earthed electrical equipment.


The V152, will flash test double insulated appliances at 4 kV . Another noteworthy feature, is the high current used for earth bond testing ( 25 A at 8 V ). Too many testers, at present available, offer only a simple continuity check for this important test.

The unit operates from a mains supply and the appliance under test is plugged into the 13 amp socket on the front panel of the tester. When the test button is pressed, neon lamps indicate that the series of tests is completed, with green lights for passes and red lights for failures.

The tester which is housed in a hardwood case is priced at $£ 144.50 \mathrm{ex}$. VAT and p\&ep.

Clare Instruments Limited, Clare Works, Woods Way, Goring-by-Sea, Worthing.

## NEGATIVE ION GENERATORS

Most of the air around us is electrically neutral with only a few of the air molecules gaining or losing electrons and therefore acquiring a positive or negative charge.

The effect of these charged molecules, which are called air ions, on individual health has been researched over many years and it has become clear that it is the balance of negative and positive ions rather than high ion concentration which is important.

Research has also shown that sufferers from asthma, hay fever and bronchitis can benefit from having the air they breathe charged with negative ions. There is also considerable evidence that ion depletion, such as

occurs in offices or crowded rooms, produces discomfort, drowsiness, fatigue and loss of mental and physical efficiency.

The concentration of negative ions in the air can be increased using a negative ion generator. Two such generators have just been introduced by J. P. Bell Ltd., the Kobelair Model 20 is a desk unit suitable for individual usage whereas the Model 40 is suitable for rooms up to 40 cubic metres ( 1500 cubic feet) with a maximum effectiveness over a range of 0.5 to 2.5 metres ( 2 to 8 feet).

The model 20 is priced at $£ 57.50$ and the Model 40 at $£ 98.50$ excluding VAT and $p \& p$.
J. P. Bell (Machinery) Ltd., Jubilee works, London Road, Woolmer Green, Knebworth, Herts.

## SUPERDECK FOR MPUs

The V\&T Superdeck is a high speed cassette unit which will, under CPU control, find any file stored on a C60 cassette (one megabit of unformatted memory on each side) in under one minute using fast forward and fast reverse speeds (up to 50 i.p.s.).

Other features of the Superdeck include: 5000 baud CUTS format as standard (which can be switched to other lower speeds, error detection and correction (it will also write protected areas of tape containing hard errors), it will write into the first empty file, on tape or into any file number or name specified (unless that particular file is write protected in which case an error message is generated).

At the present time only a Z80 operating system is available.

The unit which connects to any 8 bit I/O port and UART includes a 240 V supply unit.

The price of the Superdeck is $£ 110$ plus VAT and p\&p. V\&T Electronics, 82 Chester Road, London N19.

## WIRE BIN

The WB-16 wire bin has been designed for both storage and wiring table use, keeping assorted wires separated in their correct size groups and preventing wasteful tangling.


The sixteen wire storage tubes have adjustable depth stops to take wire lengths from 25 mm and 350 mm . The price of the WB- 16 is £33.81 excluding VAT and p\&p.

OK Machine \& Tool (UK) Ltd, Dulton Lane, Eastleigh, Hants. SO5 4AA

## PANEL MOUNTED CASES

A new range of panel mounted cases which are ideal for housing projects such as clocks, meters, counters etc., have just been introduced by Perancea Ltd.

The black ABS cases are supplied with two front panels, one is an anti-reflective filter for displays and the other is anodised aluminium for mounting controls. Other features include

p.c.b. guides and slots, matt black clip-on bezels and optional mounting clamps for wood or metal panels.

There are four sizes of cases available, $96 \times$ 48 mm and $72 \times 36 \mathrm{~mm}$ front panels in two lengths 120 mm and 75 mm .

These cases could also make excellent housings for our Car Instrument Devices if the l.e.d. mountings were altered.

Distributors for the cases include Watford Electronics, Home Radio and Bi-Pak all of whom advertise in the magazine.

## EPI

The 1978 edition of the Electronic Projects Index is now available. This index covers all the constructional projects published in sixteen magazines including PE, radio, television, hi-fi and computing. The projects are arranged under thirty six headings arranged alphabetically from aerials to Zener testers.
Other information given with each article includes a component guide and method of construction used, i.e: p.c.b., Veroboard etc.

The index is priced at $£ 1 \cdot 30$ including p\&p, and is available from M.L. Scaife, Central Library, Northumberland Square, North Shields, Tyne \& Wear, NE30 IQU.

## ELECTRONICS 79

The Electronics 79 Show was held this year at Olympia and many of the leading UK component manufacturers and distributors were exhibiting there together with equipment, instrumentation and packaging companies.

## VIEWDATA

The latest Viewdata adaptor from Labgear, the 7050 Viewdapta, was on display. This is a compact unit for receiving Viewdata which can be used with an existing TV set without modification to the receiver.


The 7050 consists of a desk top keyboard and a wall mounted Viewdata Processing Unit which are connected together via a multiway cable. A built in loudspeaker gives an audible indication of engaged, dialling and other tones obtained.

## TRIACS AND THYRISTORS

Motorola were showing their range of 15 to 40A triacs which they have now fitted into a TO-3 base type package with push-on terminals.

These 200 to 800 V triacs are primarily designed for full-wave control to a.c. loads and are electrically isolated from the mounting base with a high isolation voltage of 2500 V . Applications include appliance controls, power supplies, solid-state relays, heating and motor controls.


Motorola were also displaying their 8 A MCR 72 thyristor which needs just $30 \mu \mathrm{~A}$ to trigger on and can easily be directly coupled with an MPU or other driver i.c. for power control applications.

## CIRCUIT TESTER

Among the many instruments on display Vero Systems had their "Soundout" touch sensitive cable continuity tester on display which uses the body as a conductor leaving both hands free of probes.

The unit which is battery operated (9V) has a dual input impedance ( $15 \mathrm{M} \Omega$ and $2.5 \mathrm{k} \Omega$ ) and is available in two versions with the MK Il model having the additional feature of an earphone for noisy environments or where more than one unit is in use.


Both units have a volume control and are supplied with an interchangeable crocodile lead. A wrist strap and probe lead are available as accessories. The price of the MK I is $£ 20.00$ and the MK II is $£ 24.00$.

## ZIP SOCKETS

With the high cost of LS1 circuits many constructors are now using zero insertion pressure sockets to prevent pin damage to components whilst they are being inserted.

The BFI range of ZIP sockets included several new types never exhibited before. The socket range is one of the most compichensive currently available and may be used for almost any device, including multi-pin integrated circuits axial lead components, power transistors and non-standard hybrid circuits.


Of particular interest is a new range of sockets for use with LSI devices in test equipment or development "breadboards". The sockets will accept 28 ( $0.4^{\prime \prime}$ pitch), 42 and 64 pin devices with no insertion pressure, thus eliminating the lead damage and distortion which can occur when leads are forced into spring contact sockets.

Each socket has a lever at one end which is connected to an internal cam. The device is simply dropped into the socket and the lever flicked up to positively clamp the leads inside the socket. This protects the leads from
damage and ensures a good electrical connection. When the lever is released the device may be removed without force.

## PLASMAPANELS

Included in the Thompson-CSF display was their TH 7604 plasma-panel module which is intended for low-capacity alphanumeric-display applications.

This module which includes all the necessary panel-drive electronics has a power consumption of less than 30 W . Being a.c. driven, the panel itself features inherent storage which means that the high-intensity display is also free of flicker,


The module's overall dimensions are $295 \times$ $125 \times 57 \mathrm{~mm}$. Its useful panel area ( $219 \times$ 52 mm ) permits displaying up to 6 lines of 40 characters ( 5 by 7), with the possibility of adding underlining or a mobile cursor.

## BREADBOARD KIT

The latest kit from the CSC is the protoboard PB-203AK. This kit, featured in a special pre-release offer in PE (Nov. 79), contains all the components needed to make a solderless breadboard unit with three regulated d.c. power supplies.
The kit comes complete with all the elec-

tronic components, case and breadboard modules, as well as nuts, bolts, connecting wire and solder. The assembly instructions have been written without any assumptions about the constructor's past experience.

The finished Proto-Board incorporates three large breadboards plus four long busbars and one shorter one, giving a constructional area sufficient for 24 integrated circuits in 14 pin packages. In addition, terminal posts allow connection to earth and to the $+5 \mathrm{~V}, 1 \mathrm{~A}$ and $\pm 15 \mathrm{~V}, 0.5 \mathrm{~A}$ power supplies. The power supplies are independent and fully regulated, and the $\pm 15 \mathrm{~V}$ supplies can be internally adjusted over the range $7-18 \mathrm{~V}$. The three power-supply rails allow the board to be used with most types of circuitry, including TTL and CMOS logic.

The PB-203AK is supplied with an earthed metal case measuring $248 \times 168 \times 83 \mathrm{~mm}$, and is still available for a short period at a special offer price of $£ 55.00$ excluding VAT and $p$ \& $p$.

## 

ALTHOUGH compact cassettes have certain advantages over other forms of recording medium, they have the major disadvantage of a comparatively poor signal-to-noise ratio unless they are used in conjunction with some form of noise reduction system. Many pre-recorded cassettes are encoded using the Dolby system and are capable of excellent results, but there are still numerous pre-recorded cassettes currently available that are non-Dolby as are many cassettes purchased some time ago.
The dynamic noise limiter (DNL) which forms the subject of this article was designed for use with a high quality cassette deck to enable an improved signal-to-noise ratio to be obtained when playing non-Dolby cassettes. Of course, the unit can also be employed with a cassette deck which


Fig. 1. Block diagram
does not incorporate any form of noise reduction circuitry when playing any cassette. It can also be used in addition to some other form of noise reduction system to further increase the dynamic range. This can effect a very worthwhile improvement when the original recording is fairly old, and a significant amount of tape hiss has been recorded onto the cassette. It is even possible to use the unit to improve noisy f.m. radio reception, or any other programme source that is affected by low level high frequency noise.

## DNL PRINCIPLE

Tape noise consists mainly of high frequencies, or to be more accurate, it is this high frequency content that tends to be most noticeable and objectionable. Turning back the treble control while playing a cassette will show this quite clearly by apparently greatly reducing the noise. It is by reducing the upper frequency response during playback that a DNL effects a reduction in tape noise, but it only applies the full amount of treble cut at low signal levels. It is then that the noise is most noticeable.

At high signal levels the treble cut is removed to some degree, and at very high signal levels it is totally eliminated. The increased tape noise will not be audible as it will be masked by the main signal.

In this way a DNL provides a very significant reduction in background noise, but there is a minimum loss of treble response.

Fig. 2. Complete circuit diagram of the DNL

The DNL described in this article operates in the manner shown in the block diagram of Fig. 1. The input signal is split into two parts which are then mixed in a simple passive mixer circuit. One part of the signal is simply inverted before being fed to the mixer, and the other part is fed to the mixer via a high pass filter and a voltage controlled attenuator. The high pass filter rolls off signals below about 4 kHz .

The two signals at the mixer are out of phase and therefore tend to cancel one another out. However, as only high frequencies are present at one input, it is only these high frequencies that are attenuated to a significant extent. Under quiescent conditions the VCA is adjusted to balance the two inputs and so optimise the high frequency cut. The output of the mixer is coupled to a low gain amplifier which compensates for circuit losses and provides the unit with almost exactly unity voltage gain.

Some of the output from the high pass filter is used to generate a control voltage for the VCA. An active rectifier and smoothing network are used to provide this voltage. Under low signal conditions only a very small voltage will be generated, and this will not greatly affect the circuit. Higher signal conditions will produce a large enough voltage to significantly attenuate the signal through the VCA. The higher the signal level, the great the attenuation.

If the output from the VCA is reduced, the high frequency cancelling, effect on the signal from the inverter will also be reduced, and so the higher the input signal level, the less the amount of treble cut that the circuit applies. Thus the desired circuit action is provided.

The reason the active rectifier stage is fed from the high pass filter rather than the main input is that high frequency signals mask the tape noise far better than low or middle frequencies do. The unit is therefore designed to respond more readily to high frequency input signals.

## CIRCUIT DESCRIPTION

The circuit diagram for one channel of the DNL is shown in Fig. 2. TR 1 is used as a conventional high pass filter of the type often encountered in rumble filters, but the component values have been modified to provide a much higher cut off frequency of course. TR1 is connected in the emitter follower mode and so the filter has approximately unity voltage gain at pass frequencies.

The VCA is formed by R9 and TR2, the latter being a JUGFET which is used here as a voltage controlled resistance. TR3 is used as the inverting amplifier and this is a common emitter stage. As the emitter resistor (R13) is not bypassed and is equal in value to the collector load resistor (R11), this stage has almost unity voltage gain. R12 and R14 form a simple passive mixer circuit and TR4 is used as the output amplifier. TR4 only needs a voltage gain of a little

## COMPONENTS ...

| Resistors |  |
| :---: | :---: |
| *R1 | 1 k 5 |
| *R2 | 27k |
| *R3 | 33k |
| *R4 | 4 k 7 |
| *R5 | 33k |
| *R6 | 220 |
| -R7 | 68k |
| *R8 | 10k |
| *R9 | 5k6 |
| *R10 | 1 M 5 |
| -R11 | 2k2 |
| *R12 | 33k |
| *R13 | 2k2 |
| -R14 | 22k |
| -R15 | 4 k 7 |
| *R16 | $1 \mathrm{M8}$ |
| -R17 | 2k2 |
| All resistors $\frac{1}{4}$ W 5\% (10\% over 1M) |  |
| Potentiometers |  |
| *VR1 | 47k hor preset |
| *VR2 | 1 M hor preset |


| Capacitors |  |
| :---: | :---: |
| "C1 | $15 n$ |
| - C 2 | 10 n |
| -C3 | $100 n$ |
| - C 4 | $100 n$ |
| -C5 | 100n |
| *C6 | $100 n$ |
| -C7 | 100n |
| - C8 | 100 n |
| * C9 | $10 \mu 16 \mathrm{~V}$ elect |
| ${ }^{\text {C }}$ C10 | 150 n |
| C11 | $680 \mu 25 \mathrm{~V}$ elect |
| C12 | $100 \mu 16 \mathrm{~V}$ elect |
| C13 | 100 n |

All capacitors C280 type except where otherwise stated
Semiconductors

| "IC1 | CA3140T |
| :--- | :--- |
| IC2 | 78L12 |
| TR1 | BC109C |
| TR2 | BF244B |
| TR3 | BC109C |
| TR4 | BC109C |
| "D1 | 1N4148 |
| D2 | 1N4001 |
| D3 | 1N4001 |

## Switches

S1 Rocker switch d.p.s.t.
S2 Rocker switch d.p.d.t.
Transformer
T1 Mains primary, 12-0-12V 50 mA secondary. miniature type with flying leads (M.E.S.)

Miscellaneous
BEC case type GB1a or similar
Four phono sockets
Miniature panel neon
p.c.b.
*Indicates that two devices are required for stereo operation


Fig. 3. Frequency response (low level inputs)
more than two in order to make good the losses in the circuit, and so again an unbypassed emitter resistor is used to introduce negative feedback and set the voltage gain of the stage at the required level.

IC1 is used as a form of active rectifier, and its voltage gain is controlled by feedback potentiometer VR1. This enables the input signal level required in order to remove the treble cut to be varied over a considerable range so that the unit is suitable for use with any normal cassette deck.

VR2 enables the bias on TR2 gate to be adjusted and this control is set to slightly reverse bias TR2 so that there is only a small amount of attenuation through the VCA under quiescent conditions, and the two inputs to the mixer are precisely balanced. Only positive going output signals are produced from the active rectifier in the presence of a suitable input, and these have the effect of raising the voltage at the lower end of VR2 and removing the reverse bias from TR2. This increases the attenuation through the VCA and removes the treble cut.

C5 integrates the output pulses from the rectifier in order to prevent significant distortion, but the attack and decay times are both short so that the circuit quickly responds to changes in dynamic level. As is normal for this type of device, the circuit has hysteresis. This simply means that the attack time is faster than the decay time, which helps the unit to act as fast as possible without generating significant distortion.

The hysteresis is produced by D1 and R8. C5 is charged through the relatively low impedance of R8, but it cannot discharge through the same path since D1 prevents this. Instead it must discharge into the relatively high impedance of R7. This is the only reason for including D1 in the circuit since the CA3140 used in the IC1 position is only operated from a single supply rail, and will provide a rectifier action without D1.

With a high level input the frequency response of the unit is virtually flat over the audio spectrum, but on low level in-



50271
Fig. 4 a \& b. Switching alternatives
puts the frequency response of Fig. 3 is obtained on the prototype. The attenuation rate is about 12 dB per octave from 3.5 kHz to 8 kHz . There is a slight peak in the response at approximately 3 kHz and the roll off rate above 8 kHz is only very gradual, but neither of these points are of any real consequence in practice.

## P.S.U. AND SWITCHING

The filter is powered from a simple stabilised mains p.s.u. This is quite straight forward and consists of a push pull rectifier and smoothing network feeding a monolithic regulator i.c. A well smoothed and regulated output is provided, and the regulator i.c. has output current limiting and thermal overload protection circuitry.

In most cases it will be desirable to have some means of switching the unit out of circuit so that the cassette deck can be used normally. Some amplifiers and receivers have built in switching in the form of a tape monitor facility, or something of this nature, which could be used to accomplish this. An alternative is to use the simple in/out switching arrangement used on the prototype and shown in the circuit of Fig. 4a. This leaves the filter input permanently connected to the cassette deck output, but this does not seem to affect performance even if the cassette deck is used while the filter is switched off.

If preferred, the system shown in Fig. 4b can be used. Here the filter is switched completely out of circuit when the


Internal view
switch is in the "out" position, but a four pole switch is required. It would be possible to gang the on/off and in/out switches, but if this is done care must be taken to ensure that mains hum is not picked up in the in/out switch wiring. Also, care must be taken to ensure that the mains wiring cannot accidentally come into contact with the input or output wiring!

## CONSTRUCTION

The prototype unit was housed in a BEC cabinet but any case of mainly metal construction and having similar dimensions $(230 \times 150 \times 50 \mathrm{~mm})$ should also be suitable. The filters and power supply are constructed on two separate p.c.b.s and these are shown in Figs. 5 to 8 respectively. The negative supply rail connection between the two panels is carried via the mounting bolts and the metal case. The earth connections between the filter p.c.b. and the input and output sockets is obtained in the same manner. The filter and p.s.u. boards should be mounted as far apart as possible.

## ADJUSTMENT AND USE

In use the filter is either connected between the cassette deck output and the "tape" input of the amplifier, or it is


Fig. 5. P.c.b. design for the main board
Fig. 6. Component layout



Fig. 7. P.c.b. design for the p.s.u.


Fig. 8. Component layout
connected into the tape monitor or some similar facility. In either case both the input and output leads should be proper screened types.

Initially VR2 is adjusted in an almost fully clockwise direction and a blank cassette is played through the system to provide a source of tape noise. If VR2 is now adjusted in an anti-clockwise direction a point should be reached where there is a slight but noticeable null in the noise, with further adjustment causing a rise in the pitch and intensity of the
noise. The correct setting for VR2 is at this null point and both channels are adjusted in this way.
The best setting for VR 1 can be found by trial and error. The further it is adjusted in a clockwise direction, the lower the input signal level at which the treble cut starts to be lifted. It should therefore be adjusted as far in a clockwise direction as possible without the lifting of the treble cut becoming audible on low level signals.

#  

The hardware and software exchange point for PE computer projects

If you have ever built a computer, or computer peripheral using plans from the pages of PE, then it is likely that you would have appreciated some "follow up" data on such matters as interfacing and software. Keep an eve on this new column then, if you have constructed Champ, the UK101 or a peripheral device such as our printer or VDU; for it is from this column that we hope hints and snippets of information. short programs, applications and discoveries will spring forth eternal with your help of course!

Sir-Having recently built the Compukit 101 computer, 1 must say that $/$ am
delighted with it, although it has its limitations lone small annoying one being the lack of PRINT USING).

I find that I am learning BASIC by using the computer (hit and miss), and am following your article on learning BASIC.

However, as far as my programming is concerned, one or two things have so far eluded me, and I hope that you or your staff can help.
(a) What are the POKE commands to switch to printer, and to VDU, when writing programs in BASIC.
(b) Having written and loaded a program which has variables giving running totals, how can I load and save these updated programs? II have a feeling that machine code, POKE, or something of the like is involved but what?) (I have already worked
out that to run these programs, RUN sets the variables to 0 , and I have to use GOTO 1 to run them without clearing the variables. The books on BASIC I have do not mention these things, which for a real beginner are a nightmare).

## lain Corrance

Glasgow

Ideally, to carry data over, and update it at will, a cassette file should be generated so that the operating program is recorded on one tape and a data file on another. Alas, the 101 does not have cassette file firmware, but we have been told it can be done using machine code routines which of course can be accessed from BASIC via USR(I). An alternative, if somewhat clumsy, is to list as DATA statements those variables you wish to maintain, before re-recording the program.

We shall endeavour to answer all questions in due course. Next month we will be publishing a game for the 101 called "Torpedo Run", and give details of an independent UK 101 users club.


## Shake-out

Whatever people may say of the electronics industry they can never accuse it of being dull. Change is always around. It is difficult enough to keep track of the technology, even harder to keep up with business fortunes, changing markets and who owns what, and how performance and expectations will be affected by the dynamic economic climate both at home and abroad.

How the tight monetary policy, stiffened even further by the mid-November increase in interest rates, will affect the electronics industry in the UK is still anyone's guess. So is the long-term effect of the abolition of foreign currency exchange after 40 years of restriction. And what happens in the USA affects the whole of the Western world. The dollar is unhealthy, and the USA is in another energy crisis as well as being unsettled by the run-up to the Presidential election.

Pity the poor managers and market analyists struggling with their five year business plans, so beloved and promoted by the business schools! There are so many variables in the equation in these turbulent days that it is practically impossible to formulate a coherent long term policy.

Confusion and an uncertain future, however, has not deterred people from having a go at seizing what they see as good business opportunities. Expect Racal to make further acquisitions soon. Action in this respect may also be anticipated from GEC and Thorn. Expect, too, to see more foreign investment in the UK during 1980 , not excluding the Japanese. There is some timidity among overseas investors on labour relations problems in the UK but fortunately the record in the electronics industry is almost miraculously good. Apropos the Japanese, Toshiba alone already has manufacturing plants in seven countries outside Japan. This trend will continue.

## God and Virtue

How do the Japanese do it? Have they some secret formula denied to the rest of the industrial world? There have been many attempts at analysis.

In two recent commentaries one suggests that the secret is that to a Japanese company and its employees the customer is regarded as God. Actually, not an attitude to be despised although strange for a country whose religious beliefs are principally in Buddhism which has no God and Shinto in which the object of veneration in the shrine may be anything from a stone to a household utensil in which resides the spirit.

The other preaches a virtuous circle of good industrial relations allowing management to get on full time with managing and innovation, coupled with lifetime jobs generating confidence in accepting new technology by employees instead of, as in the UK, resisting it.

In all the years of Industry Notebook I never imagined I should use such a heading as that abovel Nonetheless, such abstract concepts are very real to the Japanese character with their singing of company songs before taking to their work benches, and their dedication to a cause as exemplified by the terrifying suicide attacks by Kamikaze pilots in World War 2.

## Sting Ray

Marconi Space and Defence Systems have won their biggest ever contract in the Sting Ray project. More than $\mathbf{f} 200$ million in the first instance and probably worth $£ 800$ million over its lifetime of 20 years. Among the other heady statistics, 50,000 man years of work spread over a dozen cities (if you include the subcontractors) make good reading.

Sting Ray is a lightweight homing torpedo with an advanced on-board computer, a multi-mode, multi-beam sonar which detects and tracks the target while resisting false echoes and enemy countermeasures, and a quiet yet high speed propulsion system. Deliveries to the Royal Navy should start in the early 1980s and there are expectations of it being adopted by other NATO navies.

## Energy

The energy crisis persists but it is now almost a way of life, the previously unthinkable $£ 1$ per gallon being now a matter of history. The Americans have a conservation policy well reflected in energy-saving campaigns in manufacuring plants strongly re-inforced by publicity in house journals. But are they taking it seriously? I had my doubts when I read in one house journal from an electronics company that temperature in the offices and factory was being maintained at a steady $78^{\circ} \mathrm{F}$. Surely a misprint, but then I read that the company dress code had been relaxed to permit jackets off and ties loosened. Slowly the penny dropped. This was the Texas summer, not the UK winter. Their problem is cooling as well as heating. As much as 20
per cent is being saved by some companies by simple expedients and even further gains by the addition of MPU-controlled fine tuning of air conditioning.

## Paradox

The EMI Scanner, according to the medical profession, was the greatest advance in medical diagnostics since the Röntgen's discovery of X-rays in 1895. Its creator, Godfrey N. Hounsfield, had engineering ambitions when he was a five year old tot, yet he was a late developer who didn't complete his formal engineering education until he was 30 . But his most useful period of training, on his own admission, was self-tuition between the ages of 13 and 19-an encouragement to every hobbyistl

Few people could ever have recelved so many awards and honours for a single invention, culminating in a Nobel Prize and even more recently the 1979 Aachen and Munich Prize for Technology and Applied National Sciences. And he deserved every one of them as well as the gratitude of the sick.

What a fantastic success story for the man and, initially, for the product which up to the mid 70 s was a jack-pot profit maker for EMI. Then came the big cut backs in procurement in the USA, then the biggest market, and an increasing flood of competitive equipment. As the honours poured in for Godfrey Hounsfield the debts poured in for EMI.

Bad organisation, bad management, bad luck? It is difficult to analyse, no single factor being responsible. Hounsfield's great technological achievement still stands, whatever the fortunes of his employer. All the same, one imagines he must be looking over the past five years with very mixed feelings.

A similar story, perhaps less dramatic is the scanning electron microscope, a worldbeater for Cambridge Instruments, a company now in the protective embrace of the National Enterprise Board but still losing millions on a good product. And older readers may remember the British company Perdio who bravely produced the first transistor portable radio in the world before going broke.

## Does it pay?

Does it pay to be first in the field? There is much to be said for the "me-too" philosophy which, put crudely, means letting someone else bear the major development costs and carry the burden of breaking open the market, then moving in at the right moment saying "me-too". I recall Motorola, in its early and middle period in semiconductors, regarding Fairchild as the innovator, Tl as the market developer and themselves as the "me-too" company with special skills in manufacturing coming in later with fast delivery and keen prices.

On the bid front Decca looks even more vulnerable. Thorn, at the time of writing, was still battling for EMI and GEC for Avery, their bid having been upped to a $£ 98$ million package.

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DEATH OF A SATELLITE
One of the most remarkable satellites launched in recent years is the United Kingdom, ARIEL V. It has enjoyed 5 years of great activity. When it was originally launched it was not expected that its operable life would be much more than a year because the propane fuel thrusters would run out of gas. This would deprive the control centre of means to "point" the satellite at suitable targets. The amount of data accumulated for the estimated period alone would have been a major contribution. In fact the satellite has been operational far beyond expectations. This has been due to the expertise developed by the team at the control centre, the Appleton Laboratory near Slough at Ditton Park.

Among other things this team developed a technique which enabled them to economise the gas use thereby adding years to the useful operation. This in itself was a magnificent contribution. Even when the gas was finally exhausted, use was made of the Earth's magnetic field to maintain some control. In all this the team have been very modest. This official statement of the record of this mission is extremely restrained:
"The success of Ariel V is twofold: Outstanding scientific observations have been made by Ariel V and have established the UK group at the forefront of X-ray Astronomy.
"The technical expertise and knowhow in the fields of satellite and data management which have been built up in the Control Centre at the Appleton Laboratory are second to none and invaluable for subsequent projects, and could be an important factor in the UK involvement in future international space programmes."
Ariel $V$ was launched on the 15 th of October 1974 to make observations of cosmic X -ray sources. With 5 years of observations completed it is clearly the most successful UK satellite to date, both operationally and scien-
tifically. The spacecraft, designed and constructed for SRC by Marconi Space and Defence Systems, contains six scientific experiments provided by the Mullard Space Science Laboratory, of University College London, The University of Leicester, Imperial College, London and the Goddard Space Flight Centre of the US.

## TECHNICAL ACHIEVEMENTS

The establishment of the Ariel V Control Centre at Slough in 1974 was the beginning of a major initiative in the area of satellite control and space data support as a complement to the established space project management. It is being further improved for support of the Infra-Red Astronomical Satellite (IRAS).

The staff responsible for the design of the Ariel V covered the following expertise. Electronics, real time software, data communications, celestial mechanics, operational research and large scale data processing. The electronics were needed for the building of the special computer interfaces and data display equipment; the real time software knowledge was needed for the satellite control and data reception; data communications skill was required for the setting up of links between Control Centre real time computers, the Laboratory mainframe computer, back-up computers and computers at four University sites. The celestial mechanics knowledge was required for the design of orbit prediction programmes, attitude computation and observation programmes; O.R. techniques were used to optimise the gas control, finally data base on a large scale was needed for preprocessing of the satellite data.

The Control Centre had two objectives:

1. To control the spacecraft and its experiments and, by monitoring the critical satellite sub-systems, keep the satellite in a safe and healthy state.
2. To interact rapidly with the astronomers.

## FLEXIBILITY

Both these objects were achieved successfully. The second objective was however the most successful for it had a major impact on the programme. The key was the observing programme which was so flexible that astronomers were able to interact with the Control Centre and alter plans within an hour or so. The system operates as follows. The prime Ground Station for Ariel V is the NASA Ground station at Quito in South America. The satellite passes over Quito every 90 minutes. During a satellite pass commands are sent to the satellite and data received from it on-line in the Control Centre. As soon as the raw telemetry data are received they are checked and re-formatted. Orbit and Attitude computations are carried out and data tapes created for each experimenter. These preprocessed data are then transmitted by Post Office lines to Birmingham, Imperial College, Leicester and the Mullard Space Science Laboratory. Data will be received within 45 minutes of the satellite passing over Quito. Thus it is feasible for the experimeter to examine his on-line data and request a change in the observing programme in time for the next pass. This important feature was a basic requirement for the Control Centre because of
the nature of the experiments. Frequently one of the two scanning experiments would detect an X-ray source which was new. The versatility of the control would enable the satellite to be manouevred so that the four pointing experiments could examine this source in detail. The value of this facility is very great for the reason that many sources are transient and in a few hours could fall in brilliance below detectable level.

## MAGNETIC MANOEUVRES

In the early days the attitude of the satellite was controlled by the propane gas jets at the base of the satellite. The gas was expected to last a year, in the event it was prolonged by nearly three years by the ingenuity of the control team. The gas finally ran out in June 1977. Since then attitude has been controlled by using a magnetic dipole cancellation system. This was of course not installed for that purpose but to prevent magnetic drift. In a sense it could be said that it was used in reverse. Since the satellite has an equatorial orbit it passes through the field lines of the earth's magnetic field. By passing a small current round the loop the earth's field was used to control the attitude of the satellite. The torques made available thus, were able to achieve manoeuvre rates of $10 \%$ day in right ascension and $0.5 \%$ day in declination.

The death of Ariel V is expected between the middle of January and February 1980.

## THE EXPERIMENTS

Project Scientist: Professor A. P. Willmore, Department of Space Science, University of Birmingham.
A. University College London's Mullard Space Science Laboratory, Holmbury St. Mary, Dorking.
Measurement of X-ray source positions and sky survey in the energy range 0.3 to 30 keV . This pointing experiment uses a rotation modulation collimator with proportional counters and channel electron multipliers as X-ray detectors, together with a collimated photomultiplier for optical star detection. Principal Investigator: Professor R. L. F. Boyd.
B. Physics Dept., University of Leicester, University Road, Leicester LE1 7RH.
Sky survey in the energy range 1.5 to 20 keV . This scanning experiment, which views from the side of the spacecraft, uses large proportional counters. Principal Investigator: Professor K. A. Pounds.

## C. UCL Mullard Space Science Laboratory.

 Study of the spectra of individual sources in the 2 to 30 keV range. This is a pointing experiment using a proportional counter. Principal Investigator: Professor R. L. F. Boyd.D. Physics Dept., University of Leicester. Measurement of the polarisation of X-rays from 1.5 to 8 keV . This pointing experiment will determine polarisation or line emission by means of a Bragg crystal spectrometer using moveable plane crystals. Principal Investigator: Professor K. A. Pounds.
F. Physics Dept., Imperial College, London SW7.
The study of sources of high energy X-rays up to 2.0 MeV . This pointing experiment uses an active collimator, a caesium iodide scintillator and photomultiplier detectors. It is designed to investigate the energy spectra and time variations of known sources and to measure the spectrum of the diffused cosmic X-ray background. Principal Investigator: Professor H. Elliot.

## G. Goddard Space Flight Centre, Greenbelt,

 Maryland, USA.An all-sky monitor in the energy range 3 to 6 keV . This survey experiment uses two pinhole sensors to detect transient effects in the X -ray sky enabling the other experiments to make the earliest possible measurements on these important phenomena. Principal Investigator: Dr. S. S. Holt.

## ARIEL 6

Ariel 6 which followed Ariel 5 has also a lifetime of about one year. It has not so far achieved full design operation because the control system has been subject to interference from both Russian and American radar systems. The effects are varied but one
troublesome one is that the satelite switching is corrupted. However valuable data is still being acquired.

## THE MAGNETIC FIELD SATELLITE (MAGSAT)

MAGSAT is for the purpose of studying the movements of the Earth's crust and the location of mineral deposits. It is a polar orbiting satellite, and is designed to measure the Earth's near surface magnetic fields and indirectly crustal features related to earthquakes. During the life-span of this satellite which is 120 days it will measure the strength and trace the direction of both the global magnetic field and surface magnetic fields. The surface magnetic fields are caused by the electric currents effect of magnetic storms and by certain elements in the Earth's crust. For example one large magnetic surface anomaly is due to an iron deposit in Africa. This was detected by a satellite magnetometer. After making this survey it will be possible to make available maps of the Earth's surface showing the location of magnetic irregularities and a global magnetic field model.

Having completed the surface irregularities it will be possible to gain a better understanding of the evolution of the crust of the Earth and the various geological processes
which have led to the formation of ore and petroleum deposits. This satellite possibility has only recently been understood when satellites, carrying magnetometers for the measurement of the global fields, mainly due to the Earth's core and working in low orbits showed anomalies which were localised.

It has been known for many years that some rock formations are better conductors of electricity than others and that these played a part in indicating where mineral and petroleum deposits could be found. What was a surprise was that satellite location was possible. The data produced by six satellites carrying magnetometers has led to this special satellite experiment. It is hoped also to shed more light on the reversing of the Earth's magnetic field over cycles of time. It is known now that the field suddenly collapses and slowly rises but in the opposite mode where north becomes south. The building up may take a longer time perhaps a thousand years. There are many consequences of such a happening. It could be responsible for sudden destruction of species of animals or other life.

The clues to drift of continents may help to anticipate earthquake events when the magnetic and gravitational anomalies are better understood. This project will involve most countries in the world over the next two years.

## Houndidun

Organisers: Please send details of exhibitions, club open days and other events to Mike Abbott at least six weeks in advance. Inclusion will be subject to space etc.

BEX Feb. 20-2 1. Pavilion Bournemouth. K
IEA/Electrex Feb. 25-29. National Exhibition Centre, Birmingham. I
Viewdata March 26-28. Wembley Conference Centre, London. O Computer-Aided Design (conference \& exhibition) March 31-April 2. Metropole, Brighton. Details: CAD 80/0483-3126I
Seminex April 14-18. Dept. Physics, Imperial College, London. HI
Communications 80 April 14-18. National Exhibition Centre. I
Electronic Test \& Measuring Information April 22-24. Wythenshaw Forum, Manchester. T
International Conference On The Electronic Office April 22-25. London Penta Hotel. Organised principally by the Institute of Electronics \& Radio Engineers. 99 Gower St., London WCIE 6AZ
North Midlands Mobile Rally April 27. Drayton Manor Park, Tamworth, Staffs. Details: Norman Gutteridge, 68 Max Rd., Quinton, Birmingham.
All-Electronics Show April 29-May 1. Grosvenor House, London. E The Mersey Micro Show April 30-May 2. Adelphi Hotel, Liverpool. 0 Compec Europe May 6-8. Centre International Rogier, Brussels. L
Great British Electronics Bazaar June 20-22. Alexandra Palace. E Intel Fair June 24. Wembley Conference Centre, London. U.
Tempcon July 1-3. Wembley Conference Centre. Exhibition devoted to temperature control \& measurement. T
Transducer July 1-3. Wembley Conference Centre. T Microsoftware (symposium) July 7-10. University of Sussex. S 1
The 1980 Microcomputer Show July 10-12. Royal Lancaster Hotel, London. 0
Avionics (symposium) Sept. University of Surrey. S I
Harrogate International Festival of Sound Aug. 16-19 (18 \& 19 trade).
The Exhibition Centre + hotels. X

E Evan Steadman, 34-36 High st., Saffron Walden, Essex. 0799 22612
HI Seminex Ltd., 79 High st., Tunbridge Wells, Kent. TNI IXZ. 0892 39664/5
I Industrial Trade Fairs, Radcliffe Ho., Blenheim Court, Solihull, W. Midlands B91 2BG. 021-705 6707
K Douglas Temple Studios, 1046 Old Christchurch Rd., Bournemouth, Dorset BHI ILR. 02020533
L Iliffe Promotion, Dorset Ho., Stamford St., London SE1 9LU. $\zeta$ 01-261 8437/8
O Online Conferences. Cleveland Rd., Uxbridge, Middx. UB8 2DD.万 089539262
T Trident International Exhibition, Abbey Mead Ho., 23a Plymouth Rd., Tavistock. Devon PLI9 8A U. $\int 08224671$
U Brian Crank Associates, 58 London Rd., Southborough, Kent. 0892-31812 38414
X Exhibition \& Conference Services, Claremont Ho., Victoria Ave., Harrogate. Yorks. ( 0423-62677
SI Society of Electronic \& Radio Technicians, 57-61 Newington Causeway, London SE1 6BL. Ø 01-403 235 I


## SEASIDE COMPUTER CLUB

ACOMPUTER club in the Bournemouth area has successfully taken off, the first meeting of which was held at the Poole Arts Centre on October 28th last year.

The response was very good and the club looked all set to form a committee. A second meeting was organised for November 30th at Kinson Community centre, where it was expected that a representative from Tandy would demonstrate some equipment.

Details from Robin Pink, 10 Harbour View Road, Poole, Dorset.

## MODELCIRCUIT

If you are interested in the radio control of model 'planes, ships, cars or robots, then you will be very pleased with the Ferranti ZN419CE device because it could save you money on servos. For the uninitiated, servos are used in radio control models to position control surfaces and other mechanisms. Their great advantage over the now rather outdated "on-off" escapement actuator is that they provide a proportional control action which is not jerky.
The R/C modeller controls his creation by adjusting a joystick potentiomenter which causes the transmitter to send out a pulse width modulated signal where the width of pulses is proportional to the deflection of the control. If more than one control function is required, then the associated pulse width signals are time multiplexed and sent to the model in a repeating sequence.

At the receiver the separate channel signals are recovered by demultiplexing, and it is the function of the servo to respond to the changing width of individual channel pulses by producing at its output an angular change proportional to the joystick deflection at the transmitter. The servo output is linked to control surfaces or engine controls, with the result that the model responds in a smooth, proportional manner to every new control setting selected by the modeller.
The, clever bit, as if you hadn't guessed, is turning those variable width pulse signals into a proportional mechanical movement, and that is where the Ferranti ZN419CE comes in. The motive power for the servo is usually provided by a small d.c. motor linked via gearing to the output shaft or lever, and to a variable potentiometer which rotates in synchronism with the servo output. The pot is there to provide information on the present servo output setting, and the pulse signal is there to tell the servo system what new setting is required. Inside the ZN419CE there is a monostable which has to be connected to the servo-pot so that the monostable pulse width is proportional to the pot position. A pulse comparator in the chip compares the monostable pulse width with the received pulse width for the channel, and the result is an error pulse which is stretched and used to turn on one of a pair of external p.n.p. drive transistors which control the motor current.

The motor turns to drive the servo pot (and of course the servo output shaft) until the monostable pulse width is equal to the
received pulse width, whereupon the motor stops.

A great deal of "electrickery" is necessary to produce a practical servo decoder and driver, but fortunately you can get most of it in the 14 pin package of the ZN419CE.

Complete servo modules are already available for R/C modellers of course, but by using the ZN419CE in a home-built servo it should be possible to save money. It would also be possible to use this device in "special" servos, just what you need, perhaps, for that towering microprocessor based robot you've been working on in the garage!

## CMOS SINGLE CHIPPER

Intel were one of the first in the field with a true single-chip microprocessor CPU, RAM and ROM all in a single 40 pin package. Their original 8048 and 8748 devices have now been joined by a whole family of similar devices such as the 8021 , $8022,8035,8039,8041$ and 8741 featuring various combinations of memory and inpuz/output lines.

Most of these devices are of little interest to hobbyists because they utilise maskprogrammed ROM to hold their programs, but those with a " 7 " as their second digit are useful, even for one-off projects, because they employ program memory of the erasable and reprogrammable (EPROM) variety.
The 8748 for example, although intended as a prototyping aid for the pin compatible 8048, can be very useful where the small size of a single chip system is desirable. It contains within its 40 pin package a digital processor system complete with 1 K of EPROM, 64 bytes of RAM a programmable counter/timer and no less than 27 lines of I/O.

Hats off to Intel then for a useful workhorse, but it is not the 8748 I want to tell you about because it isn't really new. The 87C48, however, is very new and it comes from Intersil, the CMOS wizards of Cupertino, California. It seems that Intersil have an agreement to second source the highly successful Intel device, but although identical to the 8748 in most respects, the 87 C48 adds that magic ingredient, CMOS technology, to make a good thing even better. It runs from a 5 volt supply, just like the NMOS 8048 but the Intersil device consumes a maximum of 50 miW against well over 300 mW for the Intel part at the same 6 Mhz clock frequency.

Rumour has it that the 87C48 will actually cost less than the 8748 when it starts to appear on stockists shelves early in 1980, a fact which could make it very attractive for battery powered hobby projects. One problem though, the 87C48 uses a different EPROM technology to that of its Intel cousin and cannot therefore be programmed by using a standard 2716 programmer and a pin-out adapter. Putting together a special programmer circuit may prove to be well worth the effort, however!

## HALF A LOAF

Talking of EPROMs, you may already know about the current world shortage of devices such as the 2716, an effect which has apparently been caused by the popularity of 5 volt EPROM technology in general, combined with a long delay before the appearance of alternative sources to challenge Intel.

Some second sources have appeared however, notably Texas Instruments, closely followed by a collection of Japanese manufacturers, but now Motorola have made a surprise entry into the fray by introducing not just another second source for the 2716, but a brand new device with four times the capacity, the MCM68764. This monster $8 \mathrm{~K} \times 8$ EPROM has leapfrogged the biggest Intel device, the $4 \mathrm{~K} x$ 82732 , and will surely carve out a useful niche for its canny manufacturer-you could get a fair sized BASIC interpreter into a single MCM687641
Making a device with no less than 65,536 separate bits to go wrong is quite a challenge but Motorola obviously hope to achieve useful yields. Those devices that do get rejected may not be wasted however, because Motorola have also announced the MCM68732 which is, surprise surprise, half of an MCM 68764!
They don't saw an MCM 68764 down the middle, they just use a reject device where one complete half of the memory is still fully serviceable. The new ' 32 comes in two versions, -1 or -0 , where the suffix indicates whether the most significant address bit (pin 21) should be tied permanently high or low. This technique is becoming more widespread as memories grow in size, and Intel themselves already sell "partial" versions of some of their memory parts, particularly 16 K dynamic RAMs.
Half a loaf is better than none seems to be a fitting motto for tomorrow's memary makers
 temperature of soldering irons. The unit can also be used for other appliances like a colour developer bath etc., where a very accurate temperature within the range of $\pm 0.5^{\circ} \mathrm{C}$ is required to be maintained, by a single adjustment.

In the ordinary solid state heat control systems, power to the element is usually delivered through a triac. At the preset temperature level the triac is switched off. Power to the element is switched on with the differential drop of the controller which is in the order of $\pm 2^{\circ}$ to $\pm 5^{\circ} \mathrm{C}$. Such 'on-off' control produces large overshoots and undershoots and therefore the heat regulation is coarse.

For more accurate control, power is delivered to the element continuously. Only the duty cycle of the power is varied to achieve the maintaining level. The variation of duty cycle or the pulse width, controls the temperature. Such a method is termed as proportional heat control system as it draws the energy in proportion to the requirement. The temperature control characteristics of the above two systems are shown in Fig. 1.

## SCHEMATIC

A block schematic of the proportional heat control unit is shown in Fig. 2. A1 is an integrator, which integrates any error signal developed due to the difference in sensor diode drop and set reference. The resulting integrated voltage change on biasing resistance R regulates the charging current to capacitor $C$ of the square wave generator $A 2$. The charging and discharging of $C$ determines the output pulse width of A2. The regulated pulse width in turn controls the duty cycle of the firing of the triac correcting the sensor temperature and returning the sensor voltage to that of reference. As the sensor temperature is gradually corrected, the pulse width of $A 2$ also changes due to decreasing error. At equilibrium, the pulse width stays at the maintaining level, when the error signal is zero. Maintainance of the constant temperature is possible only due to the holding feature of integrater A1. When the integrator input error signal is at zero level, the integrator output holds at existing level, this in turn holds the controller output pulse width. The resultant input and control curves are shown in Fig. 3.


Fig. 1. Control characteristics of (a) on/off controller (b) proportional controller

## CIRCUITT

The circuit diagram of the system is shown in Fig. 4. General purpose 741 operational amplifiers are used for the integrator as well as multivibrator.

The split supply to the system is $\pm 5.6$ volt derived from a centre tapped transformer T1 and regulated by Zener diodes D3 and D4. Capacitors C1 to C4 serve for storage and to supply ripple free current.

Two 6 volt batteries can also be used. Silicon diode (D5's) negative temperature coefficient characteristics has been used for the sensor. For this purpose the author used a diode type 1N914, however silicon n.p.n. transistors like BC107 etc., with the base and collector tied, can also be used with the same accuracy.

Current to the sensor diode is limited within 1 to 5 mA by resistance R3.



Fig. 2. Block diagram
The sensors output is fed to the inverting input at pin 2 of integrator IC 1 , through a resistor R8. The reference signal is generated by a 2.2 volt Zener diode D6 and this reference potential is divided by the chain VR1, VR2, R6, and R5. While VR1 is the calibration preset, VR2 is the control potentiometer.

The potential at the wiper of VR2 is fed to the noninverting input at pin 3 of integrator IC1 through a resistor R7. C5 is the integrating capacitor. Its value in combination. with R8 defines the rate of charge.

Integrator output at pin 6 is fed to C6 of the multivibrator formed around IC2, through resistor R9. The potential here regulates the charging current of C6 and therefore the output pulse width at pin 6 of the multivibrator IC2.

The frequency of the multivibrator is defined by the value of R 12 , which is about 70 Hz with the values used. The ratio of R11 to R10 defines the maximum mark-to-space ratio, that is the maximum conduction period for the triac during one cycle of the multivibrator.

The pulse width controlled output at pin 6 of IC2 swings between the positive and negative supply lines and rectified by diode D7 to give positive pulses for triac firing. These are fed to the gate of the triac through current limiting resistor R13. The triac remains on during the entire positive gate pulse period providing a supply to the soldering iron.

## ASSEMBLY

The p.c.b. of the control unit is shown in Fig. 5 and the component placement in Fig. 6. Fix the components in place with due care for polarities. The assembled p.c.b., supply transformer, triac and the three pin socket outlet should be mounted in a suitable metal box.

Mount the triac on a heatsink, well insulated from the


Fig. 3. Control graphs
metal cover. Fix the control pot VR1 on the front of the cover, with a knob graduated evenly to read $200^{\circ}$ to $300^{\circ} \mathrm{C}$ for its full variation.

Clamp the sensor diode onto the metal body of the soldering iron, near the insulated handle grip, well away from the tip. This is because silicon diodes operation is limited to $150^{\circ} \mathrm{C}$. Further, for a $100^{\circ} \mathrm{C}$ variation of tip temperature from $300^{\circ}$ to $200^{\circ} \mathrm{C}$, a variation of $10^{\circ} \mathrm{C}$ from $145^{\circ}$ to $135^{\circ} \mathrm{C}$ is present at the location indicated, making it the best place for monitoring the tip temperature. Connect the sensor leads with the control unit by means of a screened shielded cable, caring for the proper polarity of the diode.

## CALIBRATION

Before energising the unit, check once again that all connections are made properly. Now switch on the supply to the unit, without a soldering iron at the socket outlet and measure across Zener diodes D3, D4 and D6 that the voltages are $+5 \cdot 6,-5 \cdot 6$ and $+2 \cdot 2$ volts with respect to common point. Also check the functioning of free-running multivibrator by a multimeter set to the range 10 volts d.c.


Fig. 4. Circuit diagram


## COMPONENTS

| Resistors |  |
| :--- | :--- |
| R1, R2 | 5601 W |
| R3 | 3 k 9 |
| R4 | 1 k |
| R5 | $2 \mathrm{k} 2 \%$ |
| R6 | $512 \%$ |
| R7, R8 | 220 k |
| R9, R11 | 10 M |
| R10 | 1 M |
| R12 | 2 M 2 |
| R13 | 150 |
|  |  |

Capacitors

| C1, C2 | $250 \mu$ elect |
| :--- | :--- |
| C3, C4 | $1,000 \mu$ elect |
| C5 | 100 n polyester |
| C6 | $1 \mu$ polyester |

Semiconductors

| D1, D2, D7 | 1N4001 |
| :--- | :--- |
| D3, D4 | BZX85-5.6 1.3W Zener |
| D6 | BZY88-5.6 400mW Zener |
| IC1-1C2 | 741 |
| D5 | 1N914 |
| CSR1 | C206D 400V/3A triac |

Potentiometers

| VR1 | 10 k |
| :--- | :--- |
| VR2 | 100 linear |

Transformer
T1 230V pri.-9-0-9V. 400 mA sec

Miscellaneous
S1
Double pole mains on/off, FS 1-2A fuse, LP1-mains neon

Fig. 5. P.c.b. layout of controller
Fig. 6. Component layout and external wiring
between pin 6 of 1C2 and neutral, oscillations should be observed.

Now, energise the soldering iron from a normal supply source, not through the unit, and let it heat for about thirty minutes, to get the iron's temperature and in turn the sensor's output stabilised. Keep pot VR1 set to maximum resistance and turn the control potentiometer anticlockwise, i.e. at $200^{\circ} \mathrm{C}$ mark. Connect a multimeter set to the 10 volt d.c. range between pin 6 of IC1 and common point.
The voltage indicated will be zero. Now slowly reduce the resistance of VR1 until' the meter needle remains at about 5 V . Slow needle movement is due to integrator action.
Now turn VR2 to its other extreme $\left(300^{\circ} \mathrm{C}\right)$, and the meter needle will swing back to zero value.

With careful setting of VR1, arrange that the transition of the meter deflection from 0 to 5 volt commences at exactly mid position of the control pot VR2, i.e. at $250^{\circ} \mathrm{C}$ mark. You
will be able to achieve this state in two to three steps. Now plug in the soldering iron at the socket outlet of the control unit and temperature control is yours.



## CRR-RA <br> IO...

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## PRACTICAL <br> 

OUR MARCH ISSUE WILL BE ON SALE FRIDAY 8 FEBRUARY 1980

CUSTOM designed integration may be every designers dream, but it is the financial planners nightmare, for with every i.c. needing its own individual mask the cost is enormous and must be borne by the buyer. Therefore, custom designed integration is usually confined to applications involving large volume production, and is impractical for smaller low cost projects.

Universal logic elements endeavour to maintain the advantage of custom circuits while reducing some of their disadvantage. They are produced as standard devices designed to fit user application with little modification required, this consisting of custom design for the metallisation mask used on a standard logic array. Such universal logic elements appear in the ROM, PLA (programmable logic array) and ULA (uncommitted logic array) and it is this which will be looked at.

## allatrachetmanen

As the name implies, the ULA consists of a single chip containing an array of uncommitted gates or cells in which the silicon wafers are processed up to the stage just before the final metallisation and then stored. Each cell is separate and all that is required is a mask for an interconnection pattern, this being designed for the users specific circuit requirements. As the individual component in each cell can be readily interconnected, a combination of linear and digital circuits can be produced.

The success of the ULA is due to Ferranti who developed the CDI (collector diffusion isolation) process. A feature of CDI which gives it its facility is that the bulk semiconductor material used within the i.c. can be used for supply and ground return currents. This process greatly assists the manufacture of ULAs as all power rails are removed from the top interconnection plane, enabling the interconnection pattern to be devoted to purely programming the cells.

A schematic diagram of the CDI process is shown in Fig. 1.

The low resistivity of the collector isolation diffusion allows supply connections to be made without metal, and earth connections can be made direct as the epitaxial $p$ layer is on a $\rho$ type substrate.


Fig. 1. The CDI process


Fig. 2. Basic uncommitted cell


Fig. 3. Gate cell


| $A$ | $B$ | $C$ | $\mathbf{Q}$ |
| :--- | :--- | :--- | :--- |
| 0 | 0 | 0 | $=1$ |
| 1 | 0 | 0 | $=0$ |
| 0 | 1 | 0 | $=0$ |
| 1 | 1 | 0 | $=0$ |
| 0 | 0 | 1 | $=0$ |
| 1 | 0 | 1 | $=0$ |
| 0 | 1 | 1 | $=0$ |
| 1 | 1 | 1 | $=0$ |

Fig. 4. Logic symbol and truth table


Fig. 5. Collector ORing to increase fan-in


Fig. 6(a). Input interfacing (b) Output interfacing
The basic uncommitted cell (Fig. 2) consists of three transistors and four resistors, thus providing the usual RTL logic. Though each individual component can be connected as required, the most common cell connection to be found in the array is shown in Fig. 3. This is called the basic gate cell. It is a positive NOR gate, giving great versatility as a basic building block. Fig. 4 shows the truth for this gate. How these gates can be used as complete circuit functions will be shown later.

## INCREASING FAN IN

An example of inter-cell connecting can be seen when designing for a higher fan-in, as in Fig. 5, where components from two cells are used to increase the fan-in to five. This technique termed 'collector ORing' can be used to increase the fan-in up to a maximum of ten. The remaining transistor and two resistors can be used in some later stage.

Owing to the cell being uncommitted, interfacing can be achieved directly for most types of logic and circuitry. In Fig. 6 we see how interfacing is done by using components from one cell. As the maximum input current for the interface gate is in the order of $40 \mu \mathrm{~A}$, it allows several gates to be driven
from any of the typical logic families. For example TTL will drive up to ten ULA interface gates, CMOS, ten also. DTL up to six, etc. Output interfacing is capable of driving much lower numbers though, such as $\Pi L-t h r e e ~ g a t e s . ~ T h i s ~ c a n ~$ be increased by paralleling the interface gates, thus three ULA gates will drive nine TTL gates.

ULA is also capable of driving directly l.e.d.s, and discrete transistors, etc, and in such a mode of operation a total of 10 mA drive current is available.

## APPLICATIONS

The basic uncommitted cell can be connected to provide a large variety of linear and digital circuits. A few of the many ways in which the basic ULA can be used as building blocks are shown in Figs. 7 to 10.


Fig. 7. Operational amplifier, using 13 components from three cells


Fig. 8. Basic oscillator, using ten components from two cells and external timing R/C network


Fig. 9. Analogue voltage comparator using 17 components from four cells


Fig. 10. D type flip-flop using all components from $\mathbf{6}$ cells
An example of how an entire array may be committed to perform a set function is shown in Fig. 11. An automatic control for an item of photographic equipment, containing all the necessary logic in one 28 pin i.c. package. It utilises approx. 140 of the cells, and replaces an equivalent 20 packages of MSI.


Fig. 11. A photographic control system using ULA
To summarise then-ULA, because of low cost and quick availability is ideal for smaller projects, and as an evaluation vehicle. It saves space and assembly costs. Both reliability and performance are greatly improved; basically everything that custom designed integration offers, but cheaper and faster.


TELECOMMUNICATIONS SYSTEMS FOR TECHNICIANS 1
by Walker \& Danielson
Published by Newnes-Butterworths
$\mathbf{1 0 3}$ pages. Price $£ 2.95$

Primarily intended for TEC (Technician Education Council) level students taking courses in electronics. telecommunications and marine radio, this volume should prove popular to a wide readership as it covers a wide range of subjects at elementary level; information transmission, radio, radar, radio navigation. telephony. telegraphy, routing and data communication.

The text is well illustrated by over 180 diagrams and where applicable, BS symbols are maintained throughout.

To check recall simple revision exercises-terminate each chapter.

## SEMICONDUCTOR TECHNOLOGY

Edited by G. W. A. Dummer<br>Published by Pergamon Press<br>$\mathbf{2 0 3}$ pages. Price $\mathbf{f 2 0}$

THis is a collection of papers read at the Seminex technical seminars held at Imperial College, London. during the period 10-14 April, 1978. Topics cover a variety of developments in semiconductor technology.

# TELEVISION PRINCIPLES AND PRACTICE 

by Zarach \& Morris<br>Published by Macmillan Press

$\mathbf{2 9 4}$ pages. Price $£ 12.50$ hardback, $£ 5.95$ paperback

ANOTHER volume that caters for the various television options within the TEC framework as well as City and Guilds courses.
Throughout, circuits relate to modern TV receivers which include transistor, i.c.s., thyristors, etc.

The first three chapters cover the science of colours and the formation of monochrome and colour signals. Then follows a review in block form of the receiver which forms the basis of circuit analyses for future chapters.

Throughout the book emphasis is placed on the practical aspects of TV servicing and as such should prove invaluable to anyone professionally involved whether experienced or just beginning a career. This applies equally to the enthusiastic amateur.

## AUDIO SYSTEM DESIGN FOR SCHOOLS AND COLLEGES <br> by R. H. Welch, B.Sc. <br> Published by NCST Trent Polytechnic 195 pages. Price $£ 2.75$

| N contrast to many books on this subject which set out the relative merits of design bricks in the audio chain tailored to a specification with the inevitable juxtaposing of commercially available systems, this book introduces the basic ideas necessary for the enquiring reader to design and build his own.

Aimed primarily at sixth formers and college students it forms an excellent practical guide and reference for the construction of turntable, pick-up arm, amplifier and loudspeaker cabinets etc., in project work allied to formal Engineering courses.

Albeit motivated academically it is pitched at a level which should prove enlightening to anyone brave enough to go it alone on a di.y. system. Take heart, lasers and digital encoding aren't mentioned.

# Including V.A.T. Postage \& Packing 



This beautiful orange and black finish plastic case is available for Superboard II, Compukit UK 101 or, with an uncut keyboard panel, for mounting many other hobby computers. It is supplied with a mounting wedge to give a suitable keyboard angle and fixing screws for Superboard or Compukit. The case is strong enough to support a small portable TV or video monitor and has ventilation slots and a cable access panel at the back. It does not carry the "PE Compukit" badge shown in the photograph.
The dimensions of the case (with Superboard keyboard cut out) a e shown below-case material is approximately 2 mm thick with 4 mm radius comers. We recommend that the power regulator fitted to Compukit boards is mounted on a heatsink and fixed to the outside back of the case.
The front cover illustration shows part of our own office system employing this case. PE has been able to arrange this special price so don't miss out as the offer closes Friday 29th February 1980.




## BATTERY ALTERNATIVE

The Secretary of State for Industry has patented (British patent No 1552436 which dates from 1976 and is thus issued under the old laws), an interesting idea for storing large quantities of electrical energy by chemical means other than a vast and expensive battery of electrolytic cells. The inventor, Albert Montgomery, suggests that the system could be used either to even out the peak and low load demands on an electric power station or to drive a vehicle.

The invention relies on a reversible exothermic chemical reaction, that is to say a reaction which produces heat from the mixture of two materials which are aubsequently recovered and regenerated by electrolysis. This process is, under some conditions, more efficient at the bulk storage of energy than a conventional battery.

Fig. 1 shows the flow diagram for the cycle of the combination of the two materials

FlG. 1.

to produce a heat output from exothermic chemical reaction and a resultant electrolytic separation of the reaction product resulting from this. Recombination to produce the original materials for recycling is effected by the electrical energy input.

Fig. 2 shows the basic "circuit". Two stainless steel vessels, 1, 2 contain sodium and sulphur respectively. These raw materials are fed through valves to reaction vessel 5 which is of heat and corrosionresistant material. Copper conduit 6 for a fluid to be heated (for instance water or gas) is coiled round the vessel 5 .
The sodium and sulphur react together to form sodium polysulphide with the release of considerable quantities of heat energy. This energy is taken up by the fluid in the coil 5 and led off to a load.
The load is a heating stage for an electric turbine or vapour engine for a vehicle, such as a Stirling cycle heat engine
The spent polysulphide is fed to recovery cell 10 which has a blind-end tube of solid beta-alumina electrolyte. This tube defines a cathode. 9 inside an anode 12. A 3 volt d.c. supply is fed through the electrodes to the polysulphide, and sodium ions are conducted through solid electrolyte 11 to the anode while the sulphur remains in the cathode 9.

Regenerated sodium and sulphur are then recycled to the containers 1 and 2 . Thus the patented energy storage system has a capacity limited only by the size of the storage containers.
Supplies of polysulphide can be converted to sulphur and sodium throughout the entire period when there is excess power available, for instance during low-load night conditions on the national grid, and supplies of sodium and sulphur recombined to provide heat and generate power during the

entire period when there is a heavy load on the grid. In this way large quantities of electrical energy can be stored at far more economical price than with conventional batteries and without recourse to exotic alternative energy storage techniques, such as pumping water up a hill, lifting weights up a slope or compressing gas into vast reinforced cylinders or underground caves.

The fact that the British government has patented the invention suggests that its practical use is under serious consideration. The idea could perhaps also be applicable to domestic central heating. The chemicals would be separated on night storage rates and combined during the day to produce hot water for central heating.

## PE/LEKTROKIT PRIZES

The following prizes were awarded as a result of the PE/Lektrokit competition run in our September 1979 issue.

1 st Prize a Lektrokit Powerace 102, a jumper wire kit and 16 pin Test Clip goes to Mr. D. J. Speakman of Braintree for his dual timebase submission.

Runners up prizes have been awarded to Mr. T. Johansson of Sweden for a l.e.d. logarithmic level meter; Mr. I. M. Crann of Brecon for a novel tone generator for electronic organs and to Mr. T. Davies of Swansea for a combined voltmeter/logic scope.

Due to the very limited number of entries, first, third, fourth and seventh prizes only have been awarded.

## pollits dilishlir

## ULTRASONIC CLEANER (January 1980)

The value of C2 should be 150 pF and not $15 \mu$. ULTRASONIC BURGLAR ALARM IDecember 1979)

The 18 V battery voltage should be wired through the keyswitch instead of the neutral lead.
DIGITAL TEMPERATURE CONTROLLER (October 1979)
The wiper and top end of VR 1 should go to +9 V and not to IC 1/14 (p.c.b. is correct).


ASCII CODE
Every Alphanumeric character to be transmitted differs in bit pattern, and even the number of bits varies. It is possible to identify the whole of the ASCII character set using only seven bits, plus the start and stop bits. Fig. 2 shows this set of characters with their respective logic levels.

A code can be obtained for every Alphanumeric character, and many other characters to be found on certain keyboards.

THE MODEM
The acoustic modem is able to deal directly with the waveform shown in Fig. 1, because it is in serial form. A typical period for one bit is ten milliseconds, thus allowing one character to be transmitted in approximately 100 milliseconds. The bit period may be varied depending upon whether electromechanical or all electronic data transmission/receiving equipment is being used.

Having applied data to the Modem we now wish to transmit same over many miles to a fellow computer user, and it is a question of sending and receiving this digital information over long distances without tampering with post office equipment. The answer is, of course, the acoustically coupled telephone modem. By inserting the handset of a domestic telephone into this device, data may be transmitted and received at will, albeit somewhat slowly.

The principle of operation employs frequency modulation techniques involving the phase locked loop principle. A full explanation of how the complete system works is given in conjunction with the circuit diagrams of Figs. 5, 6 and 7.

Constructional dimensions are given for both the standard telephone handset and the trimphone version. Of course, two such acoustic modems will be required to set up a data link, but it is assumed that each enthusiast would construbt just one modem.

THE FREQUENCY SHIFT KEYED TRANSMITTER
The voltage controlled oscillator section of the phase locked loop (IC2) is utilised for the 1000 Hz tone. The capacitor C1 and resistors VR2, VR3 are responsible for setting this initial frequency. This 1000 Hz tone would be present for the logic level " 0 " on the input of the transmitter. This situation is so when TR1 is turned off. If now a logic level " 1 " is applied to the data input, IC1, using double negation, follows the input voltage level and therefore turns on TR 1, effectively connecting R3, VR2 in Parallel with R4, and VR3. The new resistance value produced by this resistor combination produces a new VCO frequency of 1200 Hz which is the frequency representing logic level " 1 ". Pin 4 on IC2 (4046) contains the frequency shifting signal that is applied as base current to TR2 via R6. TR2 drives the miniature loudspeaker producing the two audible tones which represents the corresponding logic levels of input data. When the modem is in the "Send" mode the 1000 Hz tone can clearly be heard from within the modem.

## SETTING UP THE FSK TRANSMITTER

(a) Switch the Modem to SEND.
(b) Apply a short circuit to the data input.
(c) Connect a frequency meter to TP.
(d) Adjust VR3 until 1000 Hz is shown on frequency meter.
(e) Now remove the short circuit from the input and apply +5 V with respect to the common connection.
(f) Adjust VR2 until the new frequency becomes 1200 Hz l.e. 200 Hz change between " 0 " and " 1 ".
(g) An audible indication will verify that all is well as these two frequencies are trimmed.
When this has been carried out it is worth applying a low frequency square wave to the data input of the transmitter to ensure that the frequency shift operation follows the logic levels being applied. A circuit suitable to carry out this test is shown in Fig. 4.

## THE RECEIVER SECTION

Let us assume we are receiving the transmitted signal from a distant modem. The modem at our end picks up from the telephone handset the faint signals and applies them to an audio amplifier (IC3). A gain of approximately 100 was found to be sufficient to provide a working signal for the phase locked loop (IC4). C2 couples the FSK (FrequencyShift Keying) signal to pin 2 of IC4. Diodes D5, D6, across R16 serve to provide some degree of limiting, as well as protection to IC4's input. Limiting by D5, D6 prevents amplitude modulation interference. The timing components VR1, C3, determine the frequency that the phase locked loop will free run at. This frequency should be adjusted to be 1100 Hz , i.e. between the two FSK frequencies to be received. When a logic " $O$ " is received $(1000 \mathrm{~Hz})$ at pin 2 of IC4, the phase locked loop will lock onto this causing the voltage controlled oscillator of the PLL to suddenly shift from 1100 Hz to 1000 Hz . As this happens, the output signal from the phase comparator (pin 7 of IC4) becomes negative with respect to the reference potential at pin 6 of IC4. This potential difference will force the d.c. comparator IC5 to swing negative and this output signal will be caught at approximately -0.5 V by $D 7$ when the logic " 0 " is received. If now we receive a logic " 1 " signal $(1200 \mathrm{~Hz})$ at pin 2 of IC4, the PLL will lock with its VCO frequency at 1200 Hz , resulting in the phase comparator output becoming greater than the d.c. reference on pin 6 of IC4. Thus the voltage comparator IC5


$$
\begin{array}{|l|l|l|l|l|l|l|l|l|l|l|l|}
\mathrm{B} & \mathrm{D} & \mathrm{O} & \mathrm{D} & \mathrm{O} & \mathrm{O} & \mathrm{D} \mid \mathrm{O} & \mathrm{P} & \mathrm{~F} & \mathrm{~F}|---| & \mathrm{B}
\end{array}
$$

* = ONE BIT TIME $\quad F=$ STOP BITS
$B=$ START BIT $\quad P=$ PARITY CHECKING BIT
D = DATA BITS
66200

Fig. 1. ASCII code format, in this case representing the character " $M$ "

| b7 $\rightarrow$ b 5 | 000 | 001 | 010 | 011 | 100 | 101 | 110 | 111 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{b}_{4} \rightarrow$ b 1 |  |  |  |  |  |  |  |  |
| 0000 | NUL | DLE | SP | 0 | (a) | P |  | $p$ |
| 0001 | SOH | DC1 | ! | 1 | A | a | a | q |
| 0010 | STX | DC2 | " | 2 | B | R | b | r |
| 0011 | ETX | DC3 | \# | 3 | C | S | c | s |
| 0100 | EOT | DC4 | \$ | 4 | D | T | d | $t$ |
| 0101 | ENO | NAK | \% | 5 | E | U | e | $u$ |
| 0110 | ACK | SYN | 8 | 6 | F | v | f | $v$ |
| 0111 | BEL | ETB | , | 7 | G | W | 9 | w |
| 1000 | BS | CAN | 1 | 8 | H | X | h | x |
| 1001 | HT | EM | ) | 9 | 1 | Y | i | y |
| 1010 | LF | SUB | * | : | J | z | , | 2 |
| 1011 | VT | ESC | + | ; | K | [ | k |  |
| 1100 | FF | FS | , | $<$ | L | 1 | , |  |
| 1101 | CR | GS | - | $=$ | M | ] | m | \} |
| 1110 | So | RS | period | $>$ | N | $\wedge$ | n |  |
| 1111 | SI | us |  | ? | 0 | - | - | DELete |

Fig. 2. The ASCII code, showing the binary equivalents of each character
responds with an output voltage positive going. It will in fact saturate in the positive direction at about 4.4 volts, providing an adequate, logic level to become our Data output. C5 is chosen for determining the lock range of PLL, while R19, C6, R20, C7, R21, C9 form a filter network preventing the possibility of the VCO frequency, or harmonics, upsetting the output comparator.

Fig. 3. Block schematic of the Modem link-up. The system is half-duplex. Serial pulse repetition rates should be no higher than the VCO Tx frequency. Input levels are TTL. Applications might include micro' link-ups at 110 Baud, VDU communication using a 20 mA loop, facsimile transfer etc. Trials with the Modem included a link-up with a teletype from Bebington (Merseyside) to Luton



Fig. 5. FSK transmitter of Acoustic Modem


Fig. 6. FSK receiver section


Fig. 7. PSU. $\pm 5 \mathrm{~V}$ at 100 mA

## COMPONENTS . . .

| Resistors |  |
| :---: | :--- |
| R1 | $18 k$ |
| R2 | $5 k 6$ |
| R3 | $47 k$ |
| R4 | $27 k$ |
| R5 | $1 M$ |

R6, R8-R10,R19-R21 10k (7 off)
R7 82
R11,R12 270 (2 off)
R13 100k
R14,R16,R17 1 k (3 off)
R15 100k nom. (subject to trimming)
R18, R22 2 k 2 (2 off)
All resistors $5 \% \frac{1}{4} \mathrm{~W}$ unless otherwise stated

## Capacitors

C1, C3
47n WIMA FKC-3 temp. stable or equiv. (2 off)
$\begin{array}{ll}\text { C2 } & 100 \mathrm{n} \\ \mathrm{C} 4, \mathrm{C} & 1000 \text { p (2 off) }\end{array}$
C5
$220 n$
C6-C8 $\quad 22 \mathrm{n}$ (3 off)
C10. C11 $\quad 1000 \mu / 25 \mathrm{~V}$ (2 off)
C12.C13 470n (2 off)
Ratings and types not critical unless specified

## Potentiometers

VR1, VR2, VR3
10k preset (3 off)
VR4
4 k 7 preset

Transistors and Diodes

| TR1, TR2, TR4 | BCi09 (3 off) |
| :--- | :--- |
| TR3, TR5 | BC147 (2 off) |
| D1, D2 | 1N916 (2 off) |
| D3 | l.e.d. (red) |
| D4 | I.e.d. (green) |
| D5, D6 | OA202 (2 off) |
| D7 | $4 \mathrm{V7}$ Zener (BZY 88) |
| D8-D11, D12-D15 | 1A 50V rectifier bridge (2 |
|  |  |
| Integrated Circuits |  |
| IC1 | CD4011 |
| IC2 | 4046 |
| IC3, IC5 | 741 |
| IC4 | 565 |
| IC6, IC7 | 5 V 1 A regulator (plastic) |

## Miscellaneous

Crystal microphone insert
Miniature loudspeaker $8 \Omega 100 \mathrm{~mW}$
Transformer 0-12V: 0-12V:3VA
1/O d.i.n. socket ( 3 -pin)
Double-pole, double-throw switch (send/receive)
Veroboard $137 \times 64 \mathrm{~mm}(5 \times 2.5$ ins.)
1.c. board type: PCB421 available from West Hyde Developments Ltd.

## CONSTRUCTOR'S NOTE

A complete set of components for the Acoustically Coupled Telephone Modem is available from Watford Electronics (see advertisers' index).

## MODEM OWNERS' REGISTER

Having got you to build the modem, your computer will be on the look-out for other machines to talk to, and so it is our endeavour to compile a list of all PE Modem owners who wish to "ASCIImunicate". We hope response will be sufficient to provide a useful list on request, so send us your details (listed below) and a S.A.E.

Suggested details: Name, address, telephone number, system, micro' used, peripherals and reason for incorporating the modem (in brief please).


## PO REGULATIONS

We believe the specification of the PE Acoustic Modem conforms to the Post Office regulations governing the use of devices acoustically coupled via the Public Switched Telephone Network. However, it should be noted that under the Post Office Act 1969 accoustically coupled devices should not be used with Post Office maintained plant without the prior consent of the Post Office.

Applications for the evaluation of private equipment ffor which a charge in excess of $£ 50$ will be payablel may be made to the Post Office once the supplier is satisfied that the equipment meets the requirements given in Technical Guide No. 32, available from: Post Office Telecommunications Headquarters, Service Department Sv 1.1.3.3, Tenter House, 45 Moorfields, London EC2Y 9TH.



## ACOUSTIC MODEM



E6260
Fig. 12. Transmitter Test Point waveforms. When no input is applied and the Modem is switched to Transmit, the 1 Ms square wave will appear continuously at Test Point 2

## RECEIVER CHECK

(a) Look at signal on TP3 to ensure it is at least 250 mV peak to peak when receiving from distant modem.
(b) If not, the gain of IC3 may have to be raised by increasing R 15 (100k).
(c) With no signal being received, adjust VR1 until the frequency meter placed on TP4 reads 1100 Hz .
(d) With Data being received observe TP5 and refer to receiver waveforms information.

## DATA INDICATOR AND OUTPUT OPTIONS

Signals from both the transmitter and receiver are fed to I.e.d.s D3 and D4. This allows us to monitor the data both when we are sending and also receiving. It should be made clear that the modem will not be doing both at once, being half-duplex.

TR3 switches on when the output of gate (IC1) goes high (Transmit Mode) or when Pin 6 of IC5 goes positive (Receive Mode). This will result in (D3) turning on and indicating a logic " 1 " level being present. As TR3 is turned on, R12 is virtually connected to ground, thus turning off TR5. The transistors TR3 and TR5 form a "see-saw" stage. When one is off the other is on, so that when no base current flows in TR3 it is a sure sign that a logic " 0 " is being received or transmitted, thus TR5 will be turned on and the "0" l.e.d. will be illuminated.

TP5 would normally be the receiver output point. It might be that a $180^{\circ}$ signal is required to drive the device coupled to the modem. If this is so, connect the output of the modem to the open collector of TR4, i.e. TR4 will be turned on when " $O$ " is being received. This is suitable for coupling to a teletypewriter.


Fig. 13. Receiver waveforms. Example shown is the ASCII character " M ". The l.f. pulses, i.e. logic 0 , are a burst of 1 ms puises for the duration of the bit. The h.f. burst (logic 1) contains bit blocks 0.83 ms wide. For Teletype operation the output bit duration is about 10 ms


In the concluding article next month we shall give stripboard layout diagrams for the three boards, plus a considerable amount of applications information and device data showing how the modem can be improved and/or adapted to suit particular link-up requirements


## by K. Lenton-Smith

ANEW instrument was presented at the recent Trade Fair-the Sharma HX80. The manufacturers, Keith Hitchcock, have been mentioned previously in this column in connection with their Doppler-effect speaker systems. Early last year I heard the prototype in action and had an opportunity to examine its very compact circuitry. Played through a rotary speaker, it was a Hammond tone-wheel organ recreated.

At first sight, the HX80 is a fairly conventional portable organ, drawbar controlled with 49 notes on the upper and 37 notes on the lower manual. The 18 -note pedal clavier has either $8^{\prime}$ or $10^{\prime}$ pitch available. Generation is by digital pulse trains and, by splitting the waveform into segments at differing voltage levels, versatile tone synthesis is achieved. The sine waves produced by this means are mixed (Fourier synthesis) in the normal way.
The group of nine drawbars on the upper manual has been arranged so that $5-1 / 3^{\prime}$ is replaced by $1-1 / 7$ '-which is a very odd frequency in relation to the chromatic compass but is possible because of the tone generator used. It is seven times the fundamental frequency and if the latter is taken as $\mathrm{A} 440 \mathrm{~Hz}, 3080 \mathrm{~Hz}$ falls between F and G! Use of the seventh harmonic is not new (one of the overtones in a square wave in fact) but this unusual mutation drawbar provides extra tone colouring.

Other drawbars control $8^{\prime}$ and $4^{\prime}$ string tone, variable sustain, attack, decay and ambience (a form of reverberation). A single switch alters the compass of the manuals down one octave so that $32^{\prime}$ to $2^{\prime}$ pitches are substituted. The lower manual has no mutations but separate sustain covers the $16^{\prime} 8^{\prime} 4^{\prime} 2^{\prime}$ and $1^{\prime}$ pitches. Presets, three vibrato controls and a transposer also feature. Priced at under $£ 700$ including VAT, the HX80 will interest those looking for a comprehensive but fully portable instrument (though a tone cabinet is required). Basically this is a 'straight' organ without too many gimmicks and is made in the UK.

## PIANOCORDER

The Pianola is a rarity these days and, like the fairground organ, uses punched paper rolls. The Kemble Piano Co. has the UK marketing rights for the first electronic version-the Pianocorder. Using cassette tape, digital pulses are recorded as a pianist plays the original. On playback, pulses from the tape are decoded and applied to solenoids on playing key or expression pedal. For teaching purposes, this could be
a most useful aid as, unlike hearing a magnetic tape recording of the conventional type, the Pianocorder's keys are seen to move-and the playback speed can be varied at the teacher's will.

As this article goes to press, the Pianocorder is being demonstrated at the Chappell Music Centre, New Bond Street, London W1.

## NO GO

An interest in electronic music can have its problems as friends may ask for your help in sorting out a small problem caused by transportation or rough usage. Of course, the cause is always obscure, inspection lighting inadequate and time is of essence! If the reader is inadvertently involved, a few guidelines may help:

Modern instruments, and organs in particular, have circuitry that is far more complex than a decade ago. A service manual (or at least block diagram) is essential as CMOS devices are often the order of the day-and it is wise to know what you are dealing with. Instruments in the home are often on nylon carpeting so circuit boards should not be treated with abandon. Although protection diodes are normally employed, the board should be considered as an extension to the i.c. Some special purpose devices are difficult to find so if in doubt earth yourself and obviously use a low leakage iron, also earthed.

If the instrument has been moved without its back panel in place, printed circuit boards can easily get damaged. Equally, forcing it into position over misaligned guides can split the board. If a crack is diagnosed, remove p.c.b. sockets with great care as solid conductors are often used. Run a little cyanoacrylate adhesive into the crack and clamp the board flat for the few minutes it takes to set. After removing the clamp, broken tracks can be patched: clean the copper strip locally with a small, sharp blade (a scalpel is ideal) and solder small bridges of tinned copper across the breaks.

Commercial instruments are designed for easy replacement of sub-assemblies and thus contain many connectors and a wiring harness similar to those used in the car industry. Slide-on tags for multiple connection to a common point are often used and are also reminiscent of BL products. They may be perfectly good for cars, but can cause noise and breakthrough in organs if used for signal earth purposes. Vibration from internal speakers or in transportation can cause them to get noisy or to simply
disconnect themselves: remedies being either to tighten to the maximum or risk the wrath of the professiona! serviceman by chopping off the tags and making a really sound job by soldering!

## TESTING

Digital meters can be very useful at times but, due to the time taken to sample, are not satisfactory for reading moving voltages/currents, e.g. percussion circuits. Although this also applies to analogue meters to some degree, the reaction of a pointer gives a much better idea of the circuit's action. Incidentally, I would suggest that any prospective purchaser takes a good look at a detailed specification of the digital meter in mind as advertisements often omit essential points. Despite claims of high accuracy, current readings are often subject to voltage burdens which, in some models, will cause errors of 25 per cent or so. My own digital meter, which is widely advertised, often refuses to auto-zero itself (and it's no flukel). At least these meters normally have very high input impedance, but analogue meters should be capable of 20kSN.
A box containing an i.c. amplifier, speaker and battery is a useful tool for tracing audio paths. My version has a switched jack socket so that the battery is connected when the test lead jack is inserted: I don't need to remember to switch off before putting it back on the shelf. The connecting cable has a longer earth wire, terminated by a croc clip, so that the probe (inner of the screened lead) can be taken from end to end of an instrument without having to find a new signal earth point repeatedly.
An oscilloscope is perhaps something of a luxury for fault-finding and more useful at the design stage. Assuming that there is no intention of checking the waveform supplied to a top octave synthesiser, which will be in the MHz range and a simple square wave, the timebase range needs to be modest only. Vibrato will call for about 7 Hz as the slowest trace, though unless there is good persistence, flicker makes the display's usefulness questionable. About 15 kHz will be just about the maximum required for the $X$ plate, but a simple 'scope will show whether the waveform is what it is supposed to be and if tone filters are having the required effect. Be careful where the 'scope is connected into the instrument, that the input coupling capacitor is above suspicion and if it should be earthed for that particular application. If in doubt with expensive CMOS devices, test elsewherel
I have not mentioned a CR bridge as most meters can cope with resistor measurement fairly well. Some can also handle capacitors but if not, a single 4001 package and a few discrete components can be assembled into a direct reading capacitor adaptor. Where valve circuitry is concerned-and plenty still exist and work well-it pays to check values of discrete components. Resistors can change their values alarmingly when age and high voltages come into play, so don't always believe the colour of the multiplier band: 10k resistors can easily become 100k in the course of time.


THERE are many types of thermostat in use around the home and in industry. The majority make use of the bimetal strip or bar and for general use there is nothing wrong with them. However, where a wide range, close tolerance, or economical use of energy is required an electronic thermostat is far superior.

The advantage of the circuit to be described here is that the temperature of a body can be held, if necessary, to within $0.1^{\circ} \mathrm{C}$ (ideal for photographic and similar uses) and the economic value is that it does not overheat the body wasting energy in the process. (Fig. 1).

The circuit is designed to give bursts of full power, of sufficient duration to overcome heat losses, and maintain a constant temperature.

The circuit is built around the SGS-ATES L121 i.c. This device incorporates a zero voltage detector, amplifier, comparator, internal power supplies with reference voltages, output stage for triggering triacs or thyristors, and will work from any single phase $50-60 \mathrm{~Hz}$ supply.

## CIFUuIT DESCRIPTIOF

The block diagram of the L121 is shown in Fig. 2. The supply to the i.c. is via Rs which limits the supply current to approximately 30 mA . The mains frequency signal is clipped to $\pm 12 \mathrm{~V}$ at the clipping and rectification stage. Pins 8 and 10 are the i.c.s dual internal supply smoothing. This smoothed supply is regulated by the voltage regulating stage, and used to supply the other internal functions, and also produce a 1.5 volt reference at pin 4 , and a positive supply output at pin 6 .
The zero cross detector determines when the supply on pin 9 crosses zero volts relative to pins 12 and 13 , and whether it is positive, or negative going. Signals from this detector are fed to the ramp generator, control logic and output logic stages. The ramp generator produces a linear rising voltage, the rate of which is determined by C1 (pin 1) and R1 (pin 16). This is referred to as the time base. The voltage of this ramp is from less than 1 V to approximately 6 V , and is fed directly to the comparator.

The amplifier is a high gain d.c. operational amplifier, which is used to amplify the sensor output voltages to a suitable level for the comparator.

The comparator compares the relative levels of the amplifier output ( pin 2 ) with the time base signal (pin 1) and will enable the chopper and control logic when the ramp voltage exceeds that of the amplifier output, as shown in Fig. 3. This has the effect of turning the heater on and off at a rate set by the time base.

The output logic stage determines the gate pulse polarity


50260
Fig. 1. Comparison between an electrical and a mechanical thermostat

$E 6255$
and also synchronises it with the zero voltage of the mains (zero cross detector signal), and this reduces radio frequency interference (R.F.I.) produced by the triac to a very low level.

The control logic is such that it triggers the chopper stage when the voltage from the ramp exceeds the voltage at pin 2 , and for a time dependent on C2, which means that the triac switches at a mains voltage of approximately $\pm 10 \mathrm{~V}$.

To eliminate this transistor TR2 can be included, as in Fig. 4. TR2 inverts the control logic output and feeds it directly to

[6258]
Fig. 3. Waveforms and phase relationships
the chopper. This has the effect of triggering the triac while the mains voltage is between zero and $\pm 10 \mathrm{~V}$, which will reduce R.F.I. to an absolute minimum.

Fig. 4 shows the circuit diagram of the Electrostat with a range of $20^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}$, and a variable time base of 1 second to 1 minute. The minimum time base of the system is set by R1 and C1, with TR1 increasing the value of C1 by a factor dependent on the gain of the transistor as the resistance of VR1 is increased.

Diodes D2 and D3 are extra clipping diodes so that under fault conditions, no high voltages can appear on pin 9. of the L121. The sensor of the system is a thermistor connected to the inverting input of the amplifier as shown in Fig. 5. The 1.5 volt reference from pin 4 is compared with the potential difference across the thermistor, the difference amplified, and fed to the comparator as described earlier. If the amplifier gain is high i.e. 50 or more, any small change in


50256 Fig. 4. Circuit diagram of the Electrostat ('see text) NEUTRAL


Fig. 5. Block diagram of the amplifier, comparator and ramp generator
thermistor potential will result in a large change in output from the amplifier, which will be acted upon by the other circuit functions, to return the sensor voltage near to the reference level. This situation is ideal for photographic work where a temperature can be controlled to within $0.1^{\circ} \mathrm{C}$ or better, depending upon the location of the sensor, and the thermal resistance of the object being heated.

The exact value of time base and temperature setting components depends upon every particular application. Table 1 lists some possible uses and suggested values.

| Application | Temp. Range Centigrade | Time Base and C1 Value | Amplifier Gain R4 \& VR3 Value |
| :---: | :---: | :---: | :---: |
| Photographic | 20-40 | 15-5s | 50-100 |
| Heater |  | $10 \mu-47 \mu$ | $500 \mathrm{k}-1 \mathrm{M}$ |
| Fermentation | 15-30 | $1 \mathrm{~s}-30 \mathrm{~s}$ | 20-50 |
| Heater |  | $10 \mu-330 \mu$ | 200k-500k |
| Fish Tank | 20-30 | 30s-120s | 20-50 |
| Heater |  | $330 \mu-1200 \mu$ | 200k-500k |
| Room | 15-25 | 60s-180s | 20-50 |
| Heater |  | $600 \mu-1800 \mu$ | 200k-500k |
| Immersion | 40-80 | 15s-120s | 20-70 |
| Heater |  | $150 \mu-1200 \mu$ | 200k-700k |
| TABLE 1 |  |  |  |

## TIME BASE SELECTION

The time base is set by R1 and C1. This time must be shorter than the time it takes for the heat to travel through the medium to the thermistor (thermal time constant). Transistor TR1 is used to increase the effective value of C1 to several hundreds of times its true value when long time bases are required, and where a large capacitor would be impractical. Typical time bases range from 1 second to several minutes.

The manufacturers of the i.c. recommend that R1 be set at 100 k and C 1 selected to give the required time using the formula:

$$
\mathrm{C} 1=\frac{1 \cdot 2 \mathrm{~TB}}{\mathrm{R} 1}
$$

where; VR1 $=0 \Omega$

$$
R 1=100 k
$$

C1 in Farads
TB in seconds (1 second minimum)
When the time base needs to be 1 minute or more, T 1 is used to magnify C1:

C1 (effective) $=$ C1 (true value) $\times$ TR1 hfe
where TR 1 is a BC 184L
hfe $=250$ to 900
and VR1 value is greater than 1 M or omitted.

## THERMISTOR AND TEMPERATURE SETTING RESISTOR SELECTION

A thermistor similar to the types GM 473 or VA 3410 is recommended as their operating range is $-60^{\circ} \mathrm{C}$ to $+200^{\circ} \mathrm{C}$, and their resistance is fairly large at mid-range (approximately 47 k at $25^{\circ} \mathrm{C}$ ). The range of resistances at various temperatures is given in Table 2. Referring to Fig. 5, it can be shown that:

$$
\begin{equation*}
R(\max )=5.33 R t(\text { max temp }) \tag{1}
\end{equation*}
$$

and Rp paralleled with Ra

$$
\begin{equation*}
R p / / R a=(5.33 \times R t(\min t e m p))-R(\max ) \tag{2}
\end{equation*}
$$

If $R p$ parallel with. $R a$ is a preferred value $\pm 20$ per cent, use the preferred value. If not use the next biggest preferred value and calculate Ra:

$$
\begin{equation*}
R a=\frac{(R p v / / R a) \times R p v}{R p v-(R p v / / R a)} \tag{3}
\end{equation*}
$$

Select the range of temperature required and substitute in the equations the relevant values of thermistor resistances from Table 2.

Temperature (Centigrade) Approx Resistance (Ohms)

| -60 | 10 M |
| ---: | :---: |
| -30 | 1 M |
| 0 | 159 k 7 |
| 10 | 100 k |
| 20 | $59 k$ |
| 25 | 47 k |
| 30 | 37 k 7 |
| 40 | 24 k 8 |
| 50 | 16 k 7 |
| 60 | $11 \mathrm{k5}$ |
| 70 | $8 k 1$ |
| 80 | $5 k 9$ |
| 90 |  |
| 100 |  |
| 150 |  |
|  |  |
|  |  |
|  |  |
|  |  |

TABLE 2
Example

## Photographic Heater

Preferred range $20^{\circ} \mathrm{C}$ to $40^{\circ} \mathrm{C}$
$R(\max )=5.33 \times R t(\max )$

$$
=5.33 \times 24.8 k
$$

$$
=132 \cdot 2 \mathrm{k}
$$

Nearest preferred value $120 k$
$R \mathrm{R} / / \mathrm{Ra}=(5.33 \times \mathrm{Rt}($ min $)-\mathrm{R}($ max $)$
$=(5.33 \times 59 \mathrm{k})-120 \mathrm{k}$
$=194.5 \mathrm{k}$
Nearest preferred value $220 k$
$R a=\frac{(R p v / / R a) \times R p v}{R p v-(R p v / / R a)}$
$R a=\frac{194.5 k \times 250 k}{250 k-194.5 k}$
=876k

## Nearest proferred value 1 MS

## Amplifer Gain

The amplifier gain is set by the ratio of R2, VR2, and R3:

$$
\begin{equation*}
\text { Gain }=\frac{R 2+V R 2}{R 3} \tag{4}
\end{equation*}
$$

## CONSTRUCTION AND TESTING

The p.c.b. design and component layout for the Electrostat are shown in Figs. 6 and 7. Triac CSR 1 should be of an adequate rating and mounted on a heatsink using a suitable insulating kit.

Care must be taken when assembling the triac on to the heatsink, and ensure the neutral is connected to the MT1 terminal. For 110 V supplies R5 must be reduced to 3.3 k 4 W . Fuse FS1 is 50 mA , and the load should be fused at a suitable value.


Fig. 6. P.c.b. design


Fig. 7. Component layout

## COMPONENTS

```
Resistors
    R1,R2 100k (2 off)
    R3 10k
    *R4
    R5 6k8 7W (3k3 4W for 110V)
    R6 33k
    R7 220k
    *Ra
```

All resistors $\frac{1}{4} \mathrm{~W} 10 \%$ except otherwise stated.

## Potentiometers

VR1, VR2 1 M Lin. (2 off)
*VR3
Capacitors
*C1

| C2 | $10 n$ |
| :--- | :--- |
| C3 | 220 n |
| C4, C5 | $220 \mu 16 \mathrm{~V}(2$ off $)$ elect. |

## Semiconductors

| D1 | 1N4148 |
| :--- | :--- |
| D2, D3 | BZX61 15 V (2 off) |
| TR1, TR2 | BC184L (2 off) |
| CSR1 | 2N5574 (or any 400V triac with a suitable |
|  | current rating for the load) |
| TH1 | VA3410 |
| IC1 | L121 (Quarndon Electronics, Slack Lane, |
|  | Derby.) |

Miscellaneous
LP1, LP2 Mini mains neon (2 off)
FS1 50 mA fuse
P.c.b.

Connector block
Heatsink to suit triac
Suitable case
JK 13.5 mm jack socket
*See text

[E0262]
Fig. 8. Terminal block wiring
The wiring for the terminal block is shown in Fig. 8. The thermistor can be built into a probe as suggested in Fig. 9 and is connected to the circuit via JK1.

Having checked the circuit for correct placing of components, carefully examine around the i.c. for solder splashes and joined tracks. When all is satisfactory, connect the load and the supply, and switch on. If the thermistor is "cold". relative to the temperature setting, the "off" neon indicator LP2 will light immediately. If the "on" neon LP1 lights adjust VR3 to minimum, and check the "off" neon lights.

If neither neon lights, turn off and check all connections. Also check pin 8 for +12 V , and pin 10 for -12 V , with respect to pins 12 and 13. Next check pin 1 for ramp voltage. If satisfactory check pin 2 for voltage swing by adjusting VR3. If an oscilloscope is available, check pins 11 and 15 for control pulses, and pin 7 for output pulses.


Fig. 9. Probe construction
The setting of the sensitivity resistor VR2 will depend on the thermistor location within the medium and the time base. For maximum sensitivity, a time base much shorter than the thermal time constant of the body is preferable.

The sensitivity is best set by trial and error, or if a storage oscilloscope is available, monitor pin 2 for several minutes and adjust VR2 until a still flat trace is obtained.


If the sensitivity is set too high, the system will be under damped and the temperature could vary by a large amount around the required value. Similar results will be seen if the sensitivity is set far too low.

If in use R.F.I. is present, try adding TR2, R6 and R7. as shown in Fig. 4, and omit capacitor C2.

Having checked that the unit works, it can now be built into a unit to suit your own application. If a metal case or front panel is used ensure it is earthed. Remember, for safety DO NOT connect the earth to the neutral.

Where calibration of VR3 is required, it should be against a digital thermometer, or a laboratory standard mercury thermometer, located in the same area of the body as the units sensor.


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# MTCFO-EUS <br> <br> Compiled by DJD. 

 <br> <br> Compiled by DJD.}


#### Abstract

Appearing every two months, Micro-Bus will present ideas, applications, and programs for the most popular microprocessors; ones that you are unlikely to find in the manufacturers' data books. The most original ideas will probably come from readers working on their own microcomputer systems, and payment will be made for any contribution featured here. This is also the place to air your views, in general, on this new technology, so let's be hearing from you!


## MICRO MAGICIAN

THE following unusual program turns the computer into a magician, enabling it to find a card chosen secretly by a spectator. Two versions of the program are given; one in BASIC, and one in machine code for the 6502.

The presentation of the trick is as follows: only the thirteen cards of one suit are used for the trick. The cards are fanned out face down, and the spectator removes one and remembers its value. The remaining pile of cards is cut once, and the spectator replaces the selected card wherever he likes. The pile is then divided into two, and the two halves are shuffled together. Finally the cards are fanned out face-up on the table, and the order of the cards is typed into the computer. After a brief pause the computer announces which was the chosen card.

Although the trick is based on a simple principle, it leads people to believe that the computer's powers extend to mind-reading, and this belief is strengthened by occasional failures of the computer to guess the card correctly.

By way of illustration, try locating the chosen card in the sequence shown in Fig. 1. The cards were originally in order, ace up to king from left to right, and the sequence shown is the result of following the procedure described above.

## HOW THE PROGRAMS WORK

The programs work by comparing the new order of the cards with their previous order; for each card a number is calculated which represents how far the processes of shuffling and cutting have moved that card away from its previous neighbours. The higher this score, the more out of sequence is the card concerned. After calculating this score for each of the 13 cards, the card with the highest score is taken to be the one that was chosen, and in most cases this will be correct. However, in some cases the computer cannot be certain about which card was chosen; for example, if the card is returned to its original position then any card could have been chosen. Also, less obviously, if the card is re-inserted one place to one side of its original position it is impossible to tell whether it, or its neighbour, was the chosen card since the same sequence of
cards would result in each case. The reason for cutting the pack before the card is replaced is to encourage the spectator to replace the card in a different position.


Fig. 1. Find the chosen card in this sequence, which results from a presentation of the trick described in the text

When the programs are first executed they assume that the cards were originally in numerical order, ace up to king. If the cards are not initially in order the program will probably get the first attempt wrong, but in some ways it is more impressive to do the trick without arranging the cards first, and attribute the initial failure to "warming up"! On subsequent operations of the program the initial order is replaced by the new order of the cards, as typed in; the order of the cards should not be disturbed when the trick is repeated.

## CARD TRICK PROGRAMS

The two versions of the card-trick program work in comparable ways. The cards are represented internally by the numbers 1 to 13 . The programs are divided into three sections. First, the new sequence of cards is read in. Secondly, each of the cards in the previous sequence is searched for in the new sequence, and its position there is subtracted from the positions of each of the cards that were its neighbours in the previous sequence. The sequence is considered to be circular, so if the difference between two positions turns out negative then 13 is added to it. The card's distance from one neighbour, plus its distance from the other neighbour, is saved as that card's score. Finally, the card with the maximum score is found and displayed as the chosen card.

The critical part of the trick is that the cards should only be shuffled once, and the shuffle should be of the sort that divides the packet of cards into two halves and merges the two halves back into one pile (e.g. a riffe shuffle). The cards can be cut at any time, and as many times as wished, but each time the packet of cards should only be cut into two piles.

## BASIC VERSION

The BASIC version of the card trick, Fig. 2 , closely follows the above description. The subroutine at 500 looks up the card T in the array containing the previous sequence of cards, A , and returns in X the position of T in that array. The program uses only integer arithmetic, and so can work with integer-only BASIC interpreters.

0010 REM *** CARD TRICK ***
0020 DIM A(13), B(13),S(13)
0030 FOR $J=1$ TO 13: A(J)=J: NEXT $J$
0040 PRINT "ENTER YOUR CARDS"
0050 FOR $\mathrm{J}=1$ TO 13: $\mathrm{S}(\mathrm{J})=0$
0060 INPUT B(J): NEXT J
0070 T=A (13): GOSUB 500
0080 FOR $J=1$ TO 13: $\mathrm{L}=\mathrm{X}: \mathrm{R}=\mathrm{T}$
$0090 \mathrm{~T}=\mathrm{A}(\mathrm{J}):$ GOSUB 500
$0100 \mathrm{Q}=\mathrm{X}-\mathrm{L}: \mathrm{IF} \mathrm{Q}<\mathrm{O}$ THEN $\mathrm{Q}=\mathrm{Q}+13$
$0110 \mathrm{~S}(\mathrm{~T})=\mathrm{S}(\mathrm{T})+\mathrm{Q}: \quad \mathrm{S}(\mathrm{R})=\mathbf{S}(\mathrm{R})+\mathrm{Q}$
0120 NEXT J
$0130 \mathrm{M}=\mathrm{O}$
0140 FOR $J=1$ TO 13: A $(J)=B(J)$
0150 IF $\mathrm{S}(\mathrm{J})<\mathrm{M}$ GOTO 170
$0160 \mathrm{Z=J}: M=S(J)$
0170 NEXT J
O18O PRINT "YOU PICKED THE ": Z
0190 GOTO 40
0500 FOR K=1 TO 13
0510 IF $T=B(K)$ THEN $X=K$
0520 NEXT K: RETURN
Fig. 2. BASIC version of the card trick enables the computer to find a chosen card

## 6502 VERSION

The program for the 6502, Fig. 3, was developed on an Acorn system and uses two routines in the Acorn monitor, so if the program is used with another 6502 system these will have to be modified. Subroutine DISPLAY is a display and keyboard-scanning routine which displays the segment patterns from locations $0010-0017$, and waits for a keypress (although it can be made to give a single sweep of the display without waiting). It returns with the hex value of the key pressed in the A-register, the X-register is preserved, and the Y -register is zeroed. Subroutine HEXTD generates the segment pattern for the hex number in the lower four bits of the Aregister, and stores this in display location Y .

When the program is executed at 0200 the display will go blank. The sequence of cards should then be entered using the hex keys, with ace $=1$, ten $=\mathrm{A}$, jack $=\mathrm{B}$, queen $=\mathrm{C}$, and king $=\mathrm{D}$. When the last card is entered the micro will display its guess at the chosen card. The program is then ready to repeat the trick.


Fig. 4. Programmable frequency generator; the frequency is determined by the number at the output port

For simplicity, 14 bytes are allocated for each of the arrays, the zeroth byte not being used. Subroutine SCAN performs the same function as the subroutine in the BASIC verion.

## MODIFICATIONS

The programs can also guess two, or more, chosen cards, though with less reliability; for example, to find two chosen cards the programs should be modified to display the cards with the two highest scores. The programs can also be modified to work with any number of cards, and as the number of cards is increased the likelihood of the computer getting the card wrong diminishes. Thirteen cards is a happy medium; it is not too time-consuming to type in the order, while at the same time the computer's powers are indisputable!

## FREQUENCY GENERATOR

The following circuit enables a micro to act as a programmable frequency generator. It uses a low-cost digital-to-analogue converter to drive a voltage-controlled oscillator, and to illustrate its operation a program is given which will play monophonic melodies. The circuit and program wére submitted by Mr.P.V. Bayley of Newcastle, and what follows js based on his description:
"The circuit, Fig. 4, was designed for use with an 8080 microprocessor, but is suitable for any 8 -bit micro. It can generate frequencies covering an overall range of at least three octaves, and incorporates a variable pitch control.

## CIRCUIT DESCRIPTION

"Data from an 8 -bit output port is fed to the inputs of the ZN 425 E 8-bit digital-to-


Fig. 3. Card trick program for the $\mathbf{6 5 0 2}$ micro

|  |  | 1 | MUSIC | PROGR |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0000 |  | 1 |  |  |  |
|  |  | dusic | LXIB | 0100月 | ; SET AdDress Prr |
| 0003 | 110008 | LOOP | LXID | 0800日 | ;TEMPO FACTOR |
| 0006 | OA |  | LDAX | B |  |
| 0007 | D300 |  | out | 0 | ;OUTPUT TO PORT |
| 0009 | C600 |  | ADI | 0 | ; TEST $^{\text {acc. }}$ |
| 000B | Cal800 |  | Jz | STOP |  |
| OOOE | AF |  | XRA | A | ; CLEAR ACC. |
| OOOF | 1B | delay | DCX | D |  |
| 0010 | BA |  | CMP | D |  |
| 0011 | C20F00 |  | JN2 | delay |  |
| 0014 | 03 |  | INX | B | ; POINT TO NEXT |
| 0015 | C30300 |  | JMP | LO |  |
| 0018 | 76 | STOP | HLT |  |  |

Fig. 5. Program for the 8080 micro which, with the circuit of Fig. 4, plays tunes stored in memory


Fig. 7. (7a above, 7b right) Routines for the 8080 which implement two-byte jump instructions
$C 8, C 8, C 4, C 4, C 2, C 2, B C, B C, 08, B C, 08, B C, 08, B C, C 2, C 2,08, C 2,08, C 2,08$. $\mathrm{CB}, \mathrm{CB}, \mathrm{C4}, \mathrm{C4}, \mathrm{C2}, \mathrm{C2}, \mathrm{C4}, \mathrm{C4}, \mathrm{BF}, \mathrm{BF}, 08, \mathrm{BF}, 08, \mathrm{BF}, 08, \mathrm{BF}, \mathrm{C} 4, \mathrm{C4}, \mathrm{CC}, \mathrm{CC}$.
$C 8, C 8, C 4, C 4, C 2, C 2, B C, 8 C, 08, B C, 08, B C, 08, B C, C 2, C 2,08, C 2,08, C 2,08$.
$C 8, C 8, C 4, C 4, C 2, C 2, C 4, C 4, B F, B F, 08, B F, 08, B F, 08, B F, 08, B F$.
$C 8, C 8, C 4, C 4, C 2, C 2, B C, B C, 08, B C, 08, B C, 08, B C, B C, B C, 08,08$.
C8, C8, D4 , $04,08, D 4,08, D 4,08,04,08,04, D 1,08, D 4, E 0, E 0, D A, D A, D 4,04$.
D1, $\mathrm{D1}, 08, \mathrm{D1}, 08, \mathrm{D1}, 08, \mathrm{D1}, 08, \mathrm{D1}, 0 \mathrm{D}, \mathrm{DA}, \mathrm{D4}, \mathrm{D4}, \mathrm{D1}, \mathrm{D1}$.
D4, 04, 08, $04,08,04,08, C C, C C, 08, C C, 08, C C, 08, C 8, C 8,08, C 8,08, C 8,08, C 2, C 2$.
O8, C2, C2, C3, C3, $\mathrm{BE}, \mathrm{BE}, 08, \mathrm{BE}, 08, \mathrm{BE}, \mathrm{C}, \mathrm{C}, \mathrm{C4}, \mathrm{C4}, \mathrm{C2}, \mathrm{C} 2, \mathrm{BC}, \mathrm{BC}, 08, \mathrm{BC}, 08$.
$B C, B C, B C, 08,08$.

Fig. 6. Data for a simple tune to illustrate how the frequency generator can be controlled by a micro

analogue converter. The output feeds the noninverting input of a $741 \mathrm{op}-\mathrm{amp}$ used as a buffer amplifier, and this should be calibrated as follows: first VR1 is used to give an output of OV at pin 6 when OOH is output to the port; then VR2 is used to adjust for an output of 3.6 V when FFH is output to the port.
"A second 741 amplifier drives a voltagecontrolled oscillator; this is the oscillator section of a 565 phase-locked loop. VR3 is used as an overall pitch control and can be adjusted to provide a maximum frequency of over 6 kHz . At a mid-range setting the circuit will cover the range 200 Hz to 2400 Hz with good linearity. Note that the 565 operates from $\pm$ 10 V supplies, derived from $\pm 15 \mathrm{~V}$ with two zener diodes.

## MUSIC PROGRAM

"The circuit was used with the program shown in Fig. 5, which produces simple tunes. The values required to produce a musical scale are first determined, and then the tune is written as a sequence of these values, stored in memory starting at 0100 H . Different note durations can be obtained by repeating the
same note code, and blank intervals are obtained by any low-value code, such as 08 H . A zero byte denotes the end of the tune.
"The program was run on a Limrose Electronics MPT8080 microtutor, and to enter data for the tune it is necessary to change the first instruction of the program to C 3 H (jump), and then single-step the first three bytes. After entering the data for the tune make sure that the next location contains OOH , and then change the first instruction back to 01 H .
"The data in Fig. 6 are for a lively tune which should be fairly well known."

## TWO-BYTE JUMP FOR 8080

Jumps in the 8080, whether conditional or unconditional, are all three bytes long: one byte for the op-code, and a two-byte destination address. The following programs, submitted by M. R. Reynolds of Surrey, show how to implement two-byte jump instructions which can be used to save memory in a small system. The second byte of the instruction gives the low-order byte of the destination address.
"The program of Fig. 7a uses just four
bytes of memory to implement a two-byte unconditional jump instruction. It makes use of one of the eight restart instructions, which are one-byte subroutine calls to fixed addresses. They have the format ' 11 AAA 111 ' (binary) and cause the return address, the address after the restart instruction, to be pushed onto the stack, and control passed to the subroutine starting at 'OOAAAOOO' (binary). The program in Fig. 7a uses the F7 instruction which jumps to a subroutine at 0030 H , and the routine simply substitutes the byte following the F7 instruction for the low-order byte of the return address. The return instruction then causes a transfer to that address. Note that this is not a relative jump, although one could be implemented with a longer subroutine.
"A conditional jump can be implemented as shown in Fig. 7b. The extra increment and decrement are needed to skip the address byte if the condition is not met. This example uses the FF instruction, which causes a jump to 0038 H . The condition in the conditional return instruction is the inverse of the condition required for the overall jump; for example, RNZ would be required for a "jump if zero' instruction."


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## GIRL OF THE YEAR

The 1979 Girl Technician Engineer of the Year is Mrs Ann CoxHorton, age 26, an electrical contracts engineer from Chertsey, Surrey. At a recent ceremony in London she was presented with the prize of $£ 250$ and an inscribed rose bowl by Sir Montague Finniston, FRS, Chairman of the Committee of Inquiry into the Engineering Profession.
Sponsored by The Caroline Hasiett Memorial Trust and the IEETE, this award aims to focus attention on electrical and electronic engineering as a worthwhile professional career for women.

Ann Cox-Horton is employed by T Clarke \& Co Limited, a London firm of electrical contractors. She is responsible for contracts valued at up to $£ 1 \frac{1}{2}$ million, including the work of up to 50 people.
The runner-up, Mrs Barbara Needham, 27, a senior research engineer from Harlow, Essex, received a special award of $£ 150$.

Barbara Needham works for Standard Telecommunication Laboratories Limited in Harlow, Essex.

Experimenter's design for equipping the standard oscilloscope with a charge storage facility so that pulses can be examined at leisure.

WITH the recent advent of microprocessor systems and the availability of cheap digital electronics, more home constructors are using these to replace conventional analogue circuitry. In the design, development and de-bugging of these circuits the need often arises to display a low frequency pulse train, or trains, on an oscilloscope for visual analysis. This is quite difficult on a normal oscilloscope because of the nature of the time base scan, especially if the pulses are narrow. Also charge storage and memory scopes tend to be prohibitively expensive for the amateur.

It was decided therefore to produce a unit which would display pulses of TTL level $(+5 \mathrm{~V})$ on a normal oscilloscope with no modifications to the oscilloscope. This would include the facility for storing a train of pulses and freezing them on the screen for closer scrutiny. To extend its usefulness further it was designed to display four separate inputs on the oscilloscope as four separate traces.

## BLOCK DIAGRAM

Fig. 1 shows a block diagram of the complete unit. The four input signals are fed into a quad tri-state buffer the output of which is multiplexed by a four-way data selector. This is clocked by clock 1 via a divide by four counter and the resulting waveform is available from an output stage in a single wire format.

Outputs from the tri-state buffer are also routed to the memory storage section. This consists of a $256 \times 4$ RAM which is controlled by a fast clock (clock 2) and an eight bit binary counter. Another clock (clock 3) operating at a slow rate steps another eight bit counter. The outputs of the counters are fed to a sixteen bit comparator which produces controlling pulses for the output trigger and the read/write phase of the RAM.

## CIRCUIT DESCRIPTION

The input channels (Fig. 2) are fed into a quad tri-state buffer IC1. This is controlled by a signal from the comparator circuitry which enables information to appear at the output


## SPECIFICATION

4 TLL compatible channels
3 ranges of sweep time (1) 0-1s
(2) $0-10 \mathrm{~s}$
(3) $0-100 \mathrm{~s}$

Manual trigger mode or continuous memory cycling Trigger output for oscilloscope with I.e.d. indicator Mains power supply
Frequency response using all channels
(1) Store mode- $0-250 \mathrm{~Hz}$
(2) Free run mode- $0-10 \mathrm{MHz}$
of the buffers with a high level. With no enable present the output of the buffers are high impedance and do not interfere with the read phase of the RAM. These outputs are then multiplexed by IC2, a four way data selector. This is controlled by a two stage counter (IC3) and a clock (IC4) which is formed from a Schmitt trigger and runs at approximately 500 kHz .


Fig. 1 Block diagram
Fig. 2 Complete circuit

$\curvearrowleft$


 (


TR 1 and its associated components form a simple three bit digital to analogue converter. The three inputs to this R2, R3 and R4 are connected to the signal output of IC2 and its two data selector input lines. Information on these last two lines effectively shifts the level of the output from TR1, and gives four distinct traces on the oscilloscope screen. TR1 also provides a buffered, low impedance output and is biased in the emitter follower mode by D2 which has its anode connected to chassis potential (as do the ground connections of the TTL i.c.s) and the cathode to power supply zero volts. This effectively produces a negative bias on the emitter of TR1 and eliminates the need for a negative supply rail.

## STORAGE

The storage section of the unit consists of a $256 \times 4$ RAM IC13, and this is also connected to the outputs of the tristate buffers. The address lines on the RAM are controlled by an eight bit counter IC14 and IC15. These are clocked by a counter running at 256 kHz .

These address lines are also fed into a sixteen bit comparator (IC9 and IC10).

The other eight inputs of the comparator are provided by the outputs of another eight bit counter (IC7 and IC8) which is clocked by a calibrated oscillator. This is the sweep oscillator*which provides the scanning times.

Thus the signals from the two eight bit counters are compared and IC11 produces a pulse only when the outputs from these are coincidental. This pulse is then used to produce a write instruction to the RAM which then stores input data.

The frequency of the slow clock (clock 3) is set to values of $256 \mathrm{~Hz}, 25 \cdot 6 \mathrm{~Hz}$ to give variation in storage rate. Once the waveform has been stored, at an appropriate scanning rate, the output scanning rate can be increased to expand out the trace to see more detail. Triggering in the unit is provided by IC5 and IC6. This is available in three modes:

1. Single shot
2. External or internal trigger
3. Continuous run

In the first mode the monostable IC12 gives a pulse from push button switch S 6 from a manual trigger when desired. In the external or internal trigger mode triggering is achieved from an external pulse or from input channel 1. An l.e.d. is used to indicate correct triggering.

S4 selects the continuous triggering mode which causes the unit to cycle information into the memory continuously. The output trigger pulse is available through S3 via SK6 and is of TTL level.

## POWER SUPPLY

This is a conventional transformer derived mains power supply with a full wave diode bridge rectifier.

Zener dioder D1 provides the reference voltage and TR1 supplies the necessary current, which is approximately 300 mA , and should have a heatsink attached.

## CONSTRUCTION

The prototype was built on two pieces of Veroboard, which were stacked horizontally, one containing the memory and address dividers and the other the oscillators, trigger circuit and power supply. However, the layout of these is not critical and everything could be accommodated on one board.

A case was made for the unit out of aluminium but proprietary cases can be used.

The prototype was made compatible in appearance with

## COMPONENTS

## Resistors

| R1 | 1 k 2 |
| :--- | :--- |
| R2 | 1 k |
| R3 | 2 k |
| R4 | 4 k 7 |
| R5 | 1 k |
| R6 | 470 |
| R7 | 270 |
| R8 | 33 k |
| R9 | 470 |
| R10 | 1 k |
| R11 | 1 k |
| R12 | 1 k |
| R13 | 1 k |
| R14 | 1 k |
| R15 | 910 k |
| R16 | 220 |

0.5W 5\% carbon

Capacitors

| C1 | $4 n 7$ | mylar |
| :--- | :--- | :--- |
| C2 | $4 n 7$ | mylar |
| C3 | $1 n$ | mylar |
| C4 | $330 n$. | carbonate |
| C5 | $470 \mu$ | 10 V elect |
| C6 | $1000 \mu$ | 10 V elect |
| C7 | $100 n$ | mylar |
| C8 | $100 n$ | mylar |

Integrated Circuits

| IC1 | 74126 | IC9 | 7486 |
| :--- | :--- | :--- | :--- |
| IC2 | 74153 | IC10 | 7486 |
| IC3 | 7474 | IC11 | 7430 |
| IC4 | 7413 | IC12 | 74121 |
| IC5 | 7400 | IC13 | 2112 |
| IC6 | 7474 | IC14 | 7493 |
| IC7 | 7493 | IC15 | 7493 |
| IC8 | 7493 | IC16 | 556 |

## Transistors

| TR1 | BC108 |
| :--- | :--- |
| TR2 | 2 N3053 |


| Diodes |  |
| :--- | :--- |
| D1 | BZY88-6.2400 mW Zener |
| D2-D6 | 1N4001 (5 off) |


| Potentiometers |  |
| :--- | :--- |
| VR1 |  |
| VR2-VR4 | 20k |
| V | 100 k (3 off) |

## Switches

| S1 | Mains on/off double pole |
| :--- | :--- |
| S2 | Two pole four way |
| S3 | Single pole change-over |
| S4 | Single pole on-off |
| S5-S6 | Press to make |



Fig. 3 Component layout for prototype boards. Since the unit is primarily a piece of experimenters test gear which will readily translate for stripboard assembly no cutting or intenviring details are given just a guide for component placement
the author's oscilloscope with the front panel containing input sockets and selection switches. The back panel houses the output and trigger sockets and mains input lead switch and fuse.

## SETTING UP AND CALIBRATION

For accurate calibration a digital frequency meter should be used, however, a signal generator can be used for frequency comparison.

The following adjustments should be made:

|  |  |  | Measurement |
| :--- | :--- | :--- | :--- |
| Adjust | S2 range | Measure <br> Pins |  |
| VR1 | - | 256 kHz | IC16/5 |
| VR2 | 1 s | 256 Hz | IC16/9 |
| VR3 | 10 s | 25.6 Hz | IC16/9 |
| VR4 | 100 s | 2.56 Hz | IC16/9 |
|  |  | $(390 \mathrm{~ms})$ |  |

## USING THE UNIT

The unit should be connected to the Y input of one of the oscilloscope's channels (or channel) and the external trigger of the oscilloscope connected to the trigger output of the unit. The $Y$ gain of the oscilloscope should be set to approximately 0.5 volts per centimetre and the timebase to 100 milliseconds per centimetre.

Four traces should appear on the screen with random information on each one. This can be cleared by pressing the sweep trigger button leaving four straight lines.

Connect a low frequency pulse generator ( 1 Hz approximately) to the input (channel 1) and switch the unit to the 10 second sweep range. A trace of 1 Hz pulses will slowly be produced on the top trace from left to right and halt when the scan reaches the right-hand margin of the screen.
The input can now be removed and the waveform will remain until the power is removed to the unit.

The unit can also be used in continuous mode where the memory will constantly refresh at the end of each scan. Also the trace can be returned to the time origin by use of the sweep trigger button.

## LIMITATIONS

When using the unit care should be taken not to exceed higher frequencies than the maximum stated.

It is useful to note that the trace is actually broken up into 256 sections and at for example 1 second sweep rate the minimum pulse duration that can be recorded is 4 ms in 5 . If a too high frequency is fed in, depending on its harmonic relationship with the number of bits a lower frequency is produced on the screen, therefore it is useful to know the approximate value of the frequency of the waveform to be measured.

Since the unit writes in all four channels simultaneously one waveform cannot be served while 3 new ones are recorded.

## MODIFICATIONS

Although designed for TTL level signals, by using a simple CMOS buffer on the input the usefulness is extended by increasing the input impedance and the level of input. Longer sweep times can be produced by using more ranges with extra capacitance on clock 3. As the sweep time is 256 times longer"than the time interval of the 556, sweep periods of up to 100,000 seconds are feasible.


A selection of readers: original circuit ideas it should be emphasised that these designs have not been proven by us They will at any rate stimulate further thought.

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## TAPE/SLIDE SYNC

SHOWN are circuits for a Tape/Slide Synchroniser. First of all the commentary is recorded onto the tape in the normal way and whenever it is necessary for the slide projector to advance one slide, S 1 is pressed which records a burst of ultrasonic sound onto the tape. When the recorder is played back (connected to the projector via the 'tuned amplifier' Fig. 2) the relay closes and advances the slide projector one slide every time an ultrasonic sound is detected.

The oscillator should be tuned to the right frequency simply by connecting the output to the input of the tuned amplifier, and adjusting VRI until RLAI closes. The circuit only amplifies frequencies of about 48.2 kHz .

The output of the 741 is amplified by TR1 and 2 which switches on the relay. The circuit works well despite the fact that the recorders response is very low at 48.2 kHz . A small mono recorder works better than an expensive stereo tape deck because the latter usually have bias oscillators running at about $60-90 \mathrm{kHz}$ which might beat with the synchronisers' output.
R.N. Johnson.

Coulsdon Surrey


## VOLTAGE SENSITIVE RELAY

The circuit diagram as shown right is an electronic relay with two wires on the input side and three wires at the output. The input leads are connected to the voltage to be sensed. Its range is from 10 V a.c./d.c. to 20 V a.c./d.c. The relay is a 6 volt/ 30 ohm coil type with changeover contacts rated for $5 \mathrm{~A} / 230 \mathrm{~V}$ a.c.

The heart of the control system is a general purpose operational amplifier type 741. The control voltage is rectified by diode D1 and filtered and stored by capacitor Cl . The non-inverting inpul (pin 3 ) is fed with a Zener regulated fixed potential of 3.9 volts, whereas the inverting input (pin 2 ) is variable and can be set by a preset potentiometer VRI to any desired voltage. It is only by adjustment of this pot that a control point is achieved.
The output of the 741 changes state with input potential difference of as low as I millivolt. The positive going output at pin 6 biases a switching transistor through a diode and 10 kilohm resistor. The transistor in turn energises a relay whose normally open and normally closed contacts could be used in a number of applications. The differential at which the relay is desired to be operated is provided by positive feedback to non-inverting input. by a 10 k preset pot VR2 in parallel with C2.
Any desired hysteresis can be set by VR2. An electrolytic is used at the base of switching transistor TRI to avoid chattering of the relay on a.c. operation.


## Automatic Temperature controller

This application is shown below. Here a slight modification in the control circuit of the VSR is needed. R1 is removed and a thermistor with long leads substituted. The thermistor is placed near the heating source. Its resistance will change with heat resulting in control initiation. The preset potentiometer VRI now can be set for the desired temperature. The n.c. contacts of the relay can be used for opening the heater circuit when desired temperature has reached. In this case the input supply' to the VSR is obtained by a low voltage transformer and regulated by a Zener.

## Twilight switch

Alternative connections to the VSR (shown in outline) provide a light switch. Here RI is replaced by an l.d.r. The resistance of this increases with a decrease in ambient light and thus initiates the
switching operation. The n.o. (normally open) contacts are connected in series with the load and supply. Thus the lamp load lights up on falt of ambient light at preset value.
M. S. Dhingra. Chittaranjan.

India.


WHEN a precise voltage source is required for a particular application, it is common practice to modify the output voltage of a voltage regulator by "jackingup" the common. i.e. raising its potential above ground. This useful method has its disadvantages. In the event of a shortcircuit the common would become reversed biased and the regulator would loose its protection. thus resulting in its destruction.

In the circuit shown the germanium diode DI prevents the common becoming more than 0.2 volt reverse biased under short circuit conditions and thereby protecting the regulator from damage.

The addition of C2 is to ensure stability. Diodes D2 and D3 (as an example) raise the output voltage by about 1.3 volts.
J.A. Barrow

Rugby
Warwickshire

## 'JACKED UP'

REGULATOR


## WA VEFORM CON VERTOR FOR MINISONIC



THIS circuit will convert an input of sawtooth shape into a triangle shape and then convert the triangle waveform into a synthesised sine waveform. IC1 amplifies the input signal to a level of 15 V peak to peak. The value of R1 should be chosen according to the input level. RI should in fact be chosen as ( $100 \times$ peak-to-peak input voltage) kilohms. For Minisonics 1 and 2, R1 should be 39 kilohms. and 100 kilohms respectively. IC2 is a differential amplifier which inverts the positive going half cycle with respect to the negative going half cycle. With a certain amount of smoothing from C 4 this produces an output of about 7.2 V peak-to-peak which is triangular in shape. VR1 should be adjusted to give a triangle output of IV peak-to-peak for Minisonic 2. Of course the level can be any value up to 7.2 V depending on what suits the constructor's application.

The triangle output is then fed into IC3 which is another differential amplifier and identical to IC2's circuitry. This produces an output of about 3.5 V peak-to-peak which is triangular in shape and twice the frequency of the input triangle waveform. This double frequency triangle wave controls the amount of attentuation in the voltage controlled attentuator built around TRI and IC4.

As the input triangle wave approaches either its positive or negative peaks the gain of the output stage gradually decreases by the action of the double frequency wave at the gate of the f.e.t. TR 1 . This has the effect of rounding off the peaks. The shape produced is a very good approximation of a sine wave.

Setting up is quite simple. First the wiper of VR2 must be taken to its 0 V end. VR3 is now adjusted to give an output level of around 500 mV r.m.s. VR2 can
now be adjusted until the best approximation of a sine wave is produced. An os cilloscope would be useful here but I have found that the adjustment can be made fairly accurately by ear. With the output connected to an audio amplifier VR2 should be adjusted until the sound contains fewest harmonics. Finally VR3 should be readjusted to give an output of about 350 mV r.m.s. (IV peak-to-peak).

The circuit can be used as a triangle to sine convertor quite simply by leaving out IC2 and its associated circuitry.
P.G. Ludgate High Wycombe Bucks.

## car cassette POWER SUPPLY



THIS unit enables a 6 V cassette player or recorder to be powered from the 12 V car battery. while drawing only 100 mA in excess of the cassette player's consumption. Short-circuiting the output of the unit does not damage the circuitry, and only 2A flows, whereas the unit can provide 6 V at up to 800 mA .

RI limits the short-circuit current to about 2 A . and reduces the power dissipation of the series regulator transistor TRI, which acts as an emitter follower with the base voltage provided by R2/DI. (Note that DI must be rated at IW or greater.)

The complete unit fits easily into the smallest size of diecast case. which can also act as a heatsink for TR 1 .
N. Riddiford

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## RHYTHM CODE GENERATOR

The circuit shown was used to generate the 4 bit BCD rhythm select code required by the rhythm generator i.c. M252. It could also be used in any application that requires the generation of a 4 bit BCD word, for example, a hexadecimal keyboard.
If a pushbutton is pressed, the two SN74148 priority encoders code the 16 inputs to a 4 bit BCD word. This word is latched into the SN74175 quad latch by the combined GS outputs (pins 14) of the priority encoders. Capacitor C1 is used to show the edge of the latching signal so that latching takes place when the input data is valid.
The outputs of the quad latch can be decoded back to 16 bits by a SN74154 and the outputs used to drive l.e.d.s to give a visual indication of the button pressed, or as in this example the rhythm selected.
E.J. Weremiuk, Brantham,

Essex.


## AUTOMATIC CAR AERIAL CONTROL

IN February 1977, a circuit was published in "Ingenuity Unlimited" for the automatic control of an electric car aerial. The circuit described here is an alternative approach to the problem. The prototype has been in trouble-free use for over four years. It may be operated by the radio on/off switch so that the aerial is only raised when needed, or, if preferred, by the ignition switch. No additional switch is
necessary. The device may be left permanently connected to the car battery, since the leakage current when the radio is switched off is very low.
The main control circuit may be used either by connecting terminal $\mathbf{B}$ to the radio on/off switch (or the ignition switch) and shorting C and D , or by shorting A and B and connecting C to an additional control circuit. The main circuit contains

two relays, each with two changeover contacts. When the radio is turned on (or the ignition if preferred) RLA switches on, the motor starts to wind up the aerial, C1 charges up and, after a delay (adjusted by the preset VR2), RLB switches on and stops the motor. When RLA switches off, the aerial starts to wind down, Cl discharges and, after a delay (adjusted independently by VR2), RLB 2 switches off and again stops the motor. VRI and VR2 are adjusted so that the aerial winds completely up and down, the motor making about two revolutions against the slipping clutch for good measure.

If RLB has two changeover contacts, the spare set may be used to mute the radio whilst the aerial is winding up, to prevent crackling from the loudspeaker, e.g. by shorting the volume control. If the radio has a tape recorder socket through which the audio signal passes by means of a shorting plug, that can be used to make the connections to the muting contacts without disturbing the radio internally. A stereo radio would, of course, need a more complex system, or extra contacts in the relay.
D. A. Petty,

Aylesbury, Bucks.

THERE are many published circuits which enable two lamps to be controlled along two wires giving provision for either lamp or both lamps to be illuminated at any one time.

The circuit described below enables three lamps to be controlled along two wires enabling any one lamp to be illuminated at any one time. It was originally designed for a busy office to convey the instructions of 'Engaged', 'Wait' and 'Enter'.
The circuit is powered by 12 volts a.c. which is derived from the mains. The three lamps are controlled by $\mathbf{S} 1$ which gives the four possible operations. In position 1 no lamps are on, since no power is being applied to the wires a and b. In position 2, the alternating current from the transformer is half wave rectified by D1, making wire a positive with respect to b . TR1 and hs associated components respond to this and so LP1 is illuminated. TR1 is prevented from conducting when S1 is in the a.c. position (position 4) by D4, R1, and D8. These ensure that Cl is charged by the negative half cycles so that TR1 will be made non-conducting.

In position 3 the alternating current is again half wave rectified, but this time wire $a$ is negative with respect to wire $b$. The circuitry for LP2 is the same as that for LP1 except that it is connected the other way round to the wires $a$ and $b$.

In position 4 of SI, an alternating voltage is applied to a and b . The circuitry for LP3 works in the following way; with S1 in position 2 (wire a positive) TR3 is conducting so keeping TR4 nonconducting. In position 3 (wire a negative), D7 is reversed biased so that LP3 is again

not illuminated. With an alternating voltage, the negative half cycles reduce the voltage across C3 to a sufficiently low level that TR3 is non-conducting. TR4 becomes conducting so allowing LP3 to light.

The 200 uF electrolytic capacitors in
each lamp circuit offers a small amount of smoothing to the half rectified a.c., producing approximately 10 volts d.c. across each lamp when alight.
J. P. Kemp, Kings Norton, Birmingham.

## SCOPE CALIBRATOR



THIS simple circuit can be used to check oscilloscope Y-amplifier Volts/ Cm calibration accuracy, and to set the frequency compensation trimmer R4 on a high input impedance oscilloscope probe.
IC la and IC1b form a simple multivibrator type circuit, and IC1c acts as a pulse shaper. (The unused gate, IC Id, is connected so as to minimise battery current consumption.) The output is an excellent square-wave having fast rise and fall times with flat top and bottom base lines. Frequency is about 1 kHz .

The output feeds the simple ladder attenuator (two per cent resistors should be used if high attenuation accuracy is required). VR1 should be set to give 2.0 V at point X with respect to 0 V .

D1 provides a stabilised 5V for the IC so that the ladder network receives a constant level square wave. Battery current drain is about 25 mA .
A. Andrews, Brighton.

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