CTRON

PRACTICAL

FEBRUARY 1980

CHATLE

<u>5</u>5p

# PLUS... SPECIAL COMPUKIT/SUPERBOARD IL CASE OFFER

single

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INPUTS

SWEEP TIME



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reset

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#### EUROPES FASTEST SELLING ONE BOARD COMPUTER -SAMPLE TAPE JUST CHECK THE SPEC'S. AS SEEN IN WITH EXTENDED P.E. AUGUST, SEPTEMBER MACHINE CODE MONITOR PUKIT UK101 AND DISSASSEMBLER **OCTOBER 1979** INCLUDED FREE COST SUPERBOARD IN KIT FOR

The Compukit UK101 has

everything a one board 'superboard' should have Uses ultra-powerful 6502 microprocessor.

Uses ultra-powerful 502 microprocessor.
 50Hz Frame refresh for steady clear picture (U.S.A. products with 60Hz frame refresh always results in jittery displays)
 48 chars by 16 lines — 1K memory mapped video system providing high speed access to screen display

system providing high speed access to screen display enabling animated games and graphs \* Extensive 256 character set which includes full upper and lower case alphanumerics. Greek symbols for mathematical constants and numerous graphic characters enabling you to form atmost any shape you desire anywhere on the screen

Video output and UHF Highgrade modulator (8Mz Bandwidth) which connects direct to the aerial socket of your T V. Channel 36 UHF.
 Fully stabilised 5V power supply including trans-

Standard KANSAS city tape interface providing

standard domestic tape or cassette recorder. 4 K user RAM expandable to 8K on board £49 extra

extra. • 40 line expansion interface socket on board for attachment of extender card containing 24K RAM and disk controller. (Ohio Scientific compatible). • 6502 machine code accessible through powerful

2K machine code monitor on board. \* High quality thru plated P.C.B. with all I.C.'s mounted on sockets

Professional 52 Key keyboard in 3 colours — soft-ware polled meaning that all debouncing and key decoding done in software

000			DC
1.1.1.1	VI IV	IAN	105

COMM	ANUS				
CONT	LIST	NEW	NULL	RUN	
STATE	MENTS				
CLEAR	DATA	DEF	DIM	END	FOR
GOTO	GOSUB	IF GOTO	IF .THEN	INPUT	LET
NEXT	ON GOTO	ON. GOSUB	POKE	PRINT	REAC
REM	RESTORE	RETURN	STOP		
EXPRES	SSIONS				

#### OPERATORS

1.1 NOT.AND.OR. > < <> > = <= RANGE 10 - 32 to 10 + 32

#### VARIABLES

A.B.C. Z and two letter variables The above can all be subscripted when used in an array String variables use above names plus \$.e g A\$



\*8K Microsoft Basic means conversion to and from Pet, Apple and Sorcerer easy. Many compatible programs already in print SPECIAL CHARACTERS

© Erases line being typed, then provides carriage return, line feed. Erases last character typed. CR. Carriage Return — must be at the end of

each line.

each line. Separates statements on a line. CONTROL/C Execution or printing of a list is interrupted at the end of a line. "BREAK IN LINE XXXX" Is printed, in-cleating line number of next statement to be worked or printed.

CONTROL/O is typed, or an error occurs. ? Equivalent to PRINT

Simple Soldering due to clear and consise instructions compiled by Dr. A.A. Berk, BSc.PhD

NO EXTRAS NEEDED JUST HIT 'RETURN' AND GO.

Build, understand, and program your own computer for only a small outlay

KIT ONLY £219 + VAT including RF Modulator & Power supply Absolutely no extras.

Available ready assembled and tested, ready to go for £

Z	69	+	VAT
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FUNCTIONS ABS(X) LOG(X) SPC(I)	ATN(X) PEEK(I) SOR(X)	COS(X) POS(I) TAB(I)	EXP(X) RND(X) TAN(X)
FR <mark>E(X)</mark> IN SGN(X) SIT USR(I)	F(X) N(X)		
STRING FUN ASC(X\$) RIGHT\$(X\$.Į)	CHR\$S(I)	FRE(X\$) STR\$(X)	LEFT\$(XS.I)
LEN(X\$) MII VAL(X\$)	(L.I:8X)8C		

#### LOUR ADD SOON -ON CARD AVAIL

Enables you to choose your foreground the background colour anywhere on the screen. Flash any character on the screen at will. Full documentation and parts in kit form



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33/35, CARDIFF ROAD, WATFORD, HERTS, ENGLAND MAIL ORDER, CALLERS WELCOME. Tel. Watford 40588/9	AC128 20 BC461 AC141 24 BC477 AC142 24 BC516 AC187 24 BC517	36 BFY71 20 25 BFY81 90 48 BSX20 18 48 BSX29 45	TIP41B 73 2N2219A 22 TIP42A 64 2N2220A 26 TIP42B 82 2N2221A 23 TIP42B 70 2N2222A 20	CX17W 395 CCN15W 410 X25W 395
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Football Ground. Naerest Underground/Br. Rail Station: Watford High Street. Open Monday to Saturday 9 a.m6 p.m. Ample Free Car Parking space available.	AF114 50 BD131 AF115 50 BD132 AF116 50 BD133 AF117 70 BD133	45 MJE3055 70 45 MPF102 66 43 MPF103 36 38 MPF104 36	ZTX107 12 2N3504 55 ZTX108 12 2N3663 26 ZTX109 14 2N3702 11 ZTX212 28 2N3703 11	22 pin 25p. 70p 24 pin 36p 78p 28 pin 39p 85p 36 pin 105p
<b>400</b> ¥: InF, In5, 2n2, 3n3, 4n7, 6n8, 10n, 15n, 9p; 18n <b>10</b> p; 22n, 33n <b>11</b> p; 47n, 68n 14p; 100n <b>17p</b> ; 150n, 220n 24p; 330n, 470n 41p; 650n 48p; 1μF 64p; 2μ2 <b>82p</b> . 160¥; 10n5, 12n, 39n, 100n, 150n, 220n 11p; 330n, 470n <b>19</b> p; 650n, 1μF <b>22p</b> ; 2-2μF	AF118 70 BD136 AF139 35 BD137 AF178 70 BD138 BC107 10 BD139	36 MPF105 36 36 MPF106 40 50 MPSA05 25 40 MPSA06 25	ZTX300 13 2N3704 11 ZTX301 15 2N3705 11 ZTX302 20 2N3706 11 ZTX303 25 2N3707 11	SPECIAL
1000V: 10n, 15n 20p; 22n 22p; 47n 26p; 100n 38p; 470n 53p; 1/F 175p.	BC108 10 BD140 BC108B 12 BD144 BC108B 12 BD145 BC108C 12 BD205	36 MPSA12 42 198 MPSA55 25 198 MPSA56 25 110 MPSU02 58	ZTX304 24 2N3708 11 ZTX314 24 2N3709 11 ZTX320 30 2N3710 16 ZTX326 40 2N3711 12	741 17 555 20 2114 435
10n, 15n, 22n, 22n 5p; 33n, 47n, 58n, 100n 7p; 190n 10p; 220n, 400Hz 380p pr. 30n 13p; 470n 17p; 680n 19p; 1/2 22p; 1/2 36p; 2/2 34e, 400Hz 380p pr. ELECTROLYTIC CAPACITORS: Axial lead type (Values are in µF). 500V; 10/40p; 47, 680p; 250V; 100(55p; 53V, 0.472, 1.0, 1.5, 2, -2, -5, 5, 3, 4, 2, 6, 3, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4,	BC109B 12 BD378 BC109C 12 BD434 BC109C 12 BD517 BC140 35 BD695	65 MPSU05 50 42 MPSU06 56 65 MPSU52 65 4 65 MPSU55 55	ZTX501 15 2N3771 233 ZTX501 15 2N3772 195 ZTX502 19 2N3773 288	2708 675 TMS2716 1750
10, 15, 22 86; 32, 47, 50 126; 53, 100, 276; 909; 50, 100, 220 259; 370 346; 1000 506; 409; 22, 336; 85; 100 126; 2200, 3300 85; 4700 986; 559; 10, 33 76; 30, 470 326; 1000 506; 259; 10, 22, 47 56; 80, 100, 160 86; 220, 250 136; 470, 640 256; 1000 276; 1500 306; 2200 456; 3300 652; 4700 746; 169; 10, 40, 47, 68 76; 356	BC142 30 BD696/ BC143 30 BDY56 BC147 8 BF115 BC1478 10 BF167 BC1478 8	4 65 MPSU56 60 156 OC23 170 34 OC26 170 30 OC28 150	ZTX504 25 2N3819 22 ZTX531 25 2N3820 45 ZTX550 25 2N3823 95 ZTX550 25 2N3866 90	Access
100, 125 8p; 220, 330 14p; 470 16p; 1000, 1500 20p; 2200 34p; 640 TAG-END TYPE: 450V: 100#F 180s: 70V: 4700 165s: 64V: 2500 98s; 3300 130s; 50V: 2200 99p; 3300 105p; 40V: 15,000 399p; 4700 120p; 4000 92p; 3300 93p; 2500 85s: 2200 85s: 2000 4 2000 120s: 30V 4700 98s: 5400 105s: 4700 85s: 200	BC148B 10 BF178 BC148C 10 BF178 BC149C 10 BF179 BC149 8 BF180 BC149C 10 BF194	24 0C35 130 25 0C36 130 30 0C41 48 35 0C42 48 12 0C43 55	40251 97 2N3903 20 40251 97 2N3904 18 40311 60 2N3905 18 40313 125 2N3906 17 40315 55 2N4037 52	CMOS
806:22:0 600. TANTALUM BEAO CAPACITORS 35V: 0.1µF, 0.22, 0.33, 0.47, 0.68, 1.0, 2.2µF, 33, 47, 68, 25V: 1.5, 10, 20V: Carbon Track, 0.25W Log & 0.5W	8C153 27 BF195 BC154 27 BF196 BC157 10 BF197 BC158 11 BF198	12 0C44 31 12 0C45 28 14 0C70 28 18 0C71 28	40316 85 2N4058 17 40317 52 2N4061 17 40319 71 2N4062 17 40320 56 2N4069 45	(CONT.) 4081 20 4082 21
1.5µ, 16V; 10µ f 3g each. 16V; 15µ, 22 5p; 47, 100, 220 40p, 16V; 15µ, 22, 33 20p; 100 35p; 6V; 47, 68, 100 30n 3V; 100 20n 35p; 6V; 5K0-2MD single gang 0/P switch 65p	BC159 11 BF199 BC160 42 BF200 BC167A 11 BF244 BC168C 12 BF244	18 0C72 45 32 0C74 55 29 0C76 36 4 28 0C81 50	40362 48 2N4427 75 40406 65 2N4829 65 40407 52 2N4922 55 40408 70 2N5135 42	4085 74 4086 73 4089 150 4093 78
WYLAR FILM CAPACITORS         5KU-CMUI dual gang stereo         78p           100V-0.001 0.002, 0.005, 0.01p/F         5         SLIDER POTENTIOMETERS         0.25W log and linear values 60mm track           0.115, 0.02, 0.03, 0.04, 0.05, 0.056/F         7         D         2.25W log and linear values 60mm track	- BC169C 14 BF244I BC170 18 BF256 BC171 11 BF257 BC172 11 8F258	3 30 0C82 50 50 0C83 48 30 0C84 44 30 0C140 110	40411         295         2N5136         42           40412         65         2N5138         20           40467         95         2N5172         25           40594         90         2N5179         60	4094 190 4095 105 4096 105 4097 372
CERAMIC CAPACITORS 50V Range: 0.59F to 10.6 15.05 2.70 330F 47.65 50 15.05 2.70 330F 47.65 50 15.05 2.70 330F 47.65 50 15.05 2.70 330F 47.65 50 15.05 2.70 530F 47.65 50 15.05 2.05 51 15.05 51	BC177 18 BF274 BC178 16 BF336 BC179 18 BF594 BC179 18 BF594	30 0C170 85 18 0C171 75 35 0C200 85 40 TIP29 43	40595         98         2N5180         80           40603         65         2N5191         70           40594         90         2N5305         40           40595         98         2N5457         32           40595         98         2N5457         32	4098 110 4099 145 4160 109 4161 109 4161 109
POLYSTYRENE CAPACITORS:         0.1W 50Q-2-2M Mini, Vert. & Horiz.         7p           10pF to 1nF, 6p.         1.5nF to 47nF 10p.         0.25W 100Q-3.3MQ Horiz.         1arger 10p           0.25W 250Q-4-7MQ Vert.         10pF 100 Mini Vert.         10pF 100 Mini Vert.         10pF 100 Mini Vert.	BC182 9 BF910 8C183 9 BFR39 BC184 9 BFR40 BC182L 11 BFR41	95 TIP298 56 25 TIP29C 60 25 TIP30 47 28 TIP30 56	40636         125         2N5459         32           40673         68         2N5459         32           40673         68         2N5455         35           2N697         25         2N5642         750           2N698         44         2N5737         45	4163 109 4174 110 4175 99 4194 108
SILVER MICA (pf)         TRIMMERS mInisture         RESISTORS-Erie make 5% carbon           3.3, 4.7, 6.8, 8.2, 10, 2:5pt; 3-10pf;         12, 18, 22, 27, 33, 39, 3-30pf; 3-50pf         22p           47, 50, 68, 75, 82, 85, 5-25pt;         55pt; 56pt;         55pt;         23p, 44, 1-9, 20, 20, 10, 20, 10, 10, 10, 10, 10, 10, 10, 10, 10, 1	BC183L 10 BFR79 BC184L 11 BFR80 BC187 28 BFR81 BC212 10 BFR98	28 TIP308 64 28 TIP30C 65 28 TIP31A 52 105 TIP31A 52	2N699 54 2N6027 40 2N706A 18 2N6109 50 2N708 19 3N128 112 2N914 32 3N140 112	4408 720 4409 720 4410 720 4411 958
100, 120, 150, 180, 20, 20, 20, 20, 20, 20, 20, 20, 20, 2	BC212L 11 BFX29 BC213 10 BFX84 BC213L 12 BFX85 BC214 10 BFX86	28 TIP32A 58 26 TIP32C 75 28 TIP33A 85 28 TIP33A 85	2N916 27 2N918 40 Matched 2N1131 22 Pair	4412V 1380 4415F 795 4415V 795 4419 280
820pF 16p each. 100-500pF 33p 150-500 V 51 min Each of a solution of each typ 400-1250pF 58p not mixed values 100-500 pF 58p not mixed values	BC214L 13 BFX87 BC307B 20 BFX88 BC308B 20 BFY50	28 TIP34A 85 28 TIP34C 110 20 TIP35A 185	2N1303 50 <b>25p</b> 2N1304 50 2N1305 28 extra	4422 545 4433 995 4435 825
LINEAR LCM/2030 32 NE5869 120 COMPUTER Sh/24/5 IC's 1236 360 NE566 160 IC'S Sh/24/5 N42562 102-2 225 Sh/24/5/0 NE570 375 L102-2 225 Sh/24/5/0	63 7473 32 7416 118 7474 25 7416 895 7475 38 7416 120 7476 36 7416	4 105 74LS 5 105 LS00 11 6 140 LS01 11 7 200 LS02 12	L\$132 95 L\$290 128 401 L\$136 55 L\$293 128 401 L\$138 85 L\$295 185 401 L\$139 85 L\$295 185 401	5 82 4440 1275 6 45 4450 295 7 82 4451 295 887 4452
700 4 pin 38 LM308T 110 RC4138D 120 2112-2N 280 SN75451 710 67 LM311H 120 SAD1024 1350 2114 22N 280 SN75452 723 14 pin 39 LM318H 205 SG3402 295 214 439 SN75452 741 8 pin 37 LM324A 68 SN76003N 170 2708 672 TMS6011	70 7480 48 7417 70 7481 86 7417 225 7482 69 7417 355 7483 72 7417	0 185 LS03 12 2 625 LS04 12 3 120 LS05 23 4 87 LS08 22	LS145 108 LS299 468 401 LS147 170 LS300 175 402 LS148 173 LS302 175 402 LS151 96 LS323 468 402	9 48 4490F 695 0 99 4490V 525 1 95 4501 19 2 85 4502 120
747C 14 pin 748 LM339 70 SN76013N 140 2700 6 16K 1025 748C 8 pin 36 LM348 90 SN76013N 140 16 16K 1025 753 8 pin 150 LM349 125 SN76018 148 4007 750 810 pin 150 LM349 125 SN76018 148 1502 750	7484 95 7417 7485 75 7417 7486 31 7417 7486 31 7417 7489 140 7417	5 87 LS09 22 6 75 LS10 20 7 78 LS11 22 8 153 LS12 23	LS153 76 LS324 240 402 LS155 96 LS325 290 402 LS156 96 LS326 294 402 LS157 76 LS327 286 402	3         22         4503         69           4         66         4535         75           5         19         4506         51           26         180         4507         55
AY-1-10212         580         LM380         80         SN76023ND         130         74204         73         (TEXAS)           AY-1-1313         660         LM381N         145         SN76033N1         175         74512         350         7400         11           AY-1-1320         315         LM381N         248         SN76115N         215         745138         250         7400         11           AY-1-5200         190         LM382         128         SN761131         110         745138         250         7400         11           AY-1-5000         190         LM382         128         SN761131         110         745138         250         7402         11	7490 30 7418 7491 75 7418 7492 38 7418 7493 32 7418	0 85 LS13 38 1 165 LS14 75 2 88 LS15 30 4 135 LS20 20	LS158 96 LS327 286 402 LS160 128 LS346 185 402 LS161 98 LS347 206 402 LS162 138 LS347 206 402	7 45 4508 298 8 81 4510 99 9 99 4511 150 0 58 4512 98
AY-1-5051 145 LM386 99 SN76227N 115 745188 210 7403 12 AY-1-6721/6195 LM387 150 SN76650 90 745194 168 7404 12 AY-3-1015 560 LM387 150 SN76660 90 745194 750 7405 18 AY-3-1270 840 LM389 93 SP8629 450 745194 750 7406 28	7494 78 7418 7495 65 7418 7496 57 7419 7497 189 7419	130         LS21         22           8         275         LS22         22           0         95         LS26         48           1         95         LS27         28	LS163 102 LS352 228 403 LS164 114 LS353 228 403 LS165 75 LS365 65 403 LS166 226 LS366 65 403	1         205         4513         206           12         100         4514         265           13         145         4515         299           34         116         4516         120
AY-3-8500 390 LW733 125 TAA621AX1250 742247 195 7407 38 AY-5-1013 450 LW1458 50 TAA661A 155 742562 895 7408 17 AY-5-1224A 260 LW3900 60 TAA960 320 742587 325 7409 17 AY-5-1230 450 LW3909N 70 TAP100 159 742470 325 7410 11	74100 119 7419 74104 62 7419 74105 62 7419 74107 29 7419 74107 29 7419	2 58 LS28 48 3 98 LS30 22 4 98 LS32 27 5 98 LS33 39	LS168 155 LS367 65 403 LS169 150 LS368 66 403 LS170 288 LS373 180 403 LS173 105 LS375 160 403	15     111     4517     382       16     335     4518     102       17     100     4519     55       38     108     4520     108
AY-5-1315 560 LM3911 125 TBA1205 70 745472 1150 7411 20 AY-5-1317A630 LM3914 258 TBA540 220 745475 825 7412 17 AY-5-3500 510 LM13600 125 TBA5500 320 81LS95 125 7413 30 AY-5-3507A415 M252AA 750 TBA9900 270 81LS95 125 7414 45	74109 54 7419 74110 54 7419 74111 68 7419 74112 125 7419	7 80 LS37 39 8 150 LS38 39 9 150 LS40 28 9 150 LS42 98	LS174 106 LS374 165 403 LS175 110 LS377 212 404 LS181 398 LS378 184 404 LS183 298 LS379 215 404	19         320         4521         228           10         105         4522         149           11         80         4526         149           12         76         4527         152
AY-5-4007D 638 M253AA 795 TBA641-A12/ 811597 137 7416 30 AY-5-8100 735 MC1204 250 BX1 or BX11250 AY-5-2376 980 7417 30 CA3011 100 MC1301 79 TBA651 180 CP1610 920 7420 16 CA3014 137 MC1303 88 TBA800 90 Mc1488 85 7421 29	74116 198 7424 74118 83 7424 74119 149 7424 74120 115 7424	6 204 LS47 63 7 204 LS48 120 7 204 LS49 120 8 240 LS51 24	LS189 348 LS384 86 404 LS190 140 LS385 155 404 LS191 140 LS386 86 404 LS192 132 LS390 230 404	3         94         4528         99           14         95         4529         145           15         145         4530         85           16         128         4531         135
CA3018 68 MC1304P 260 TBA810S 95 MC1489 30 7422 17 CA3020 170 MC1310P 150 TBA820 70 MC14411 958 7423 27 CA3023 170 MC1312P0 195 TBA9200 260 MC14412 1080 7425 27 CA3028A 80 MC1495 350 TCA965 120 MK4072747325 7426 36	74121 25 7424 74122 46 7425 74123 48 7426 74125 38 7427	9         204         LS54         28           1         125         LS55         30           5         63         LS63         150.           3         320         LS73         46	LS193 130 LS393 230 404 LS194 166 LS395 218 404 LS195 136 LS396 215 404 LS196 100 LS398 276 404	17     87     4532     115       18     58     4534     575       19     48     4536     365       50     48     4538     142
CA3035 240 MC1496L 92 TDA1004 290 MK4027-2 470 7427 27 CA3036 110 MC1596 225 TDA1008 310 MK4027-3 445 7428 35 CA3043 190 MC1710 79 TDA1022 575 MK4027-3 455 7430 17 CA3045 140 MC302 150 TDA1024 105 MK4016.4 1057 7432 25	74126 57 7427 74128 74 7427 74132 73 7429 74136 65 7510	8 120 LS74 41 9 119 LS75 48 8 185 LS76 40 8 350 LS78 40	LS197 140 LS399 230 400 LS202 345 LS445 150 400 LS221 96 LS447 144 400 LS240 236 LS490 180 400	1     72     4539     105       52     73     4541     135       53     72     4543     155       54     110     4549     375
CA3046 210 MC3340P 120 TDA2020 320 MK4118-42099 7433 40 CA3048 350 MC3360P 120 TL061C 76 R0-3-2513 650 7437 30 CA3075 175 MC3401 52 TL062CP 125 745288 210 7438 33 CA3080 70 MC3403 135 TL071 76 TM54027 325 7440 15	74141 56 7515 74142 209 7549 74143 314 7549 74144 314	1 92 LS83 115 2 92 LS85 118 2 92 LS86 43 LS90 38	LS241 231 LS668 182 400 LS242 232 LS669 182 400 LS243 232 LS670 248 400 LS244 155 LS6731050 400	16         128         4550         398           36         135         4554         150           57         1950         4556         72           59         480         4557         451
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CA3130         90         IMM57160         620         TL082CP         96         Z80 CPU2.5         990         7445         94           CA3140         70         MSM5526         320         TL083CP         105         Z80 CPU2.5         990         7445         94           ICL7106         795         NE518         210         TL083CP         105         Z80 4M         1099         7446         94           ICL7107         975         NE543K         210         UAA170         198         Z80 P10         660         7447         57           VLCL7107         975         NE543K         210         UAA170         198         Z80 CFU2.5         7448         56	74151 64 74153 64 74154 96 74155 53 74L	LS96 116 LS107 44 LS109 55 LS112 55	LS251 134 4000 14 400 LS253 142 4001 14 400 LS257 110 4002 15 400 LS258 110 4006 87 400	36         4562         533           37         380         4566         155           38         22         4568         268           39         20         4569         280
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WATFORD E	ECTRONICS	6.9TO ELECTRONICS LEDS Plus. Clip TIL209 Red 125" 13 TIL211 Gra 125" 19	VOLTAGE REGULATORS	OHIO SUPERBOA Yes, we are now selling th £188.00: Due to the rece	RD II Only £188.00 ex stock is single board microcomputer at only of devaluation of US Dollar against f
(Continued from o	oposite side)	TiL212 Yellow         22           TiL32 Infra Red         58           TIL32 Infra Red         58	12V 7812 145p 7912 220p 15V 7815 145p —	Sterling, we have been ab	le to purchase Superboards at lower
DIODES         BRIDG           AA119         15         RECTI           AA129         25         [plastic           AA129         25         IA/500           AA129         25         IA/500           AA129         25         IA/500           BA100         10         IA/400           BA100         10         IA/400           BY126         12         2A/100           BY127         12         2A/200           CR033         157         2A/400           OA47         12         4A/200           OA70         12         4A/400           OA79         12         4A/800           OA81         15         4A/800	E SPEAKERS B0.0.3W 224"74 202.5:3"74 2202.5:3"74 22602.5"74 22602.5"74 22602.5"74 22602.5"74 229805W 24602.5"74 29805W 24603.5"74 25035 25055 25055 25055 25055 25055 25055	1122002         110           0.2" Yellow, green         18           Andber         18           Rectangular LEDS.         Red, Green and Yellow 36           0CP71         120           0RP12         63           2N5777         45-           0PT0 isolators         11/12           11/17         110           7 Segment Displays         15           TiL312 & 313.3"         105           TiL322 - 5" C.h         115           TiL322 - 5" C.ch         115	16v         7618         143pp	customers. Buy now to Thatcher & Co. decide to d Superboard II is supplied T.V. spec. Requires +5V a RF Converter to be up an can also supply the RF Co or ready-built). 8k Microsoft BASIC IN RC dable to 8k. Full 53 Key user programmability and a Continuous demonstration .Specially designed case for CRYSTALS 6-5536MHz	avoid disappointment should Mrs. evalue the pound. fully assembled and tested to British t 3A and a Video Monitor or TV with d running. (Data sheet supplied. We nverter and Power Supply in kit form DM. 4k Static RAM on BOARD expan- Keyboard with Upper/Lower Case & I ot more. See it for yourself. on at our retail shop. Superboard available at £25.00. Power Supply Kit (55/34)
OA85         12         6A/100'           OA90         6         6A/200'           OA91         6         6A/200'           OA95         8         VM18 D           OA200         9         ZEN           IN916         7         A000' V           IN916         6         A00' V           IN916         6         A00' V           IN400/2         5         Rng: 2V           IN400/2         6         1 3W           IN4004/5         6         A102           3A/100V         18         B8104           8A/102         18         B8105           3A/400V         20         7	73 4 x 4 x 2 73 78 5 x 4 x 2 73 85 6 x 4 x 2 73 85 6 x 4 x 2 73 10 56 7 x 5 x 2 x 130 56 7 x 5 x 2 x 130 10 x 4 x 3 7198 73 9 12 x 8 x 3 7265 3 3 3 V VEROBOARD 15 0 15 0	DL704 3 C.Clin 99 DL707 3 C.Cand 99 DL707 3 C.Cand 99 DL747 6" An 180 FND357 120 MAN3640 165 XAN351 3" Green 180 Liquid Crystal Display 31 digit 875p; 4 digit 975p Pitch 0.15 0.1 0.15 opper clad) (plain) 39p 31p 24p 50p - 31p 50p - 41p 67p 50p 43p p 180p 141p 120 p - 183p	CINITIAL         State         State	100kHz 385p 7-880MHz 455kHz 385p 9-375MHz 1008HZ 323p 100Hz 1-008MHz 323p 107Hz 1-832MHz 365p 12MHz 1-832MHz 365p 12MHz 1-832MHz 365p 18MHz 3-2768MHz 323p 18-432M 4-032MHz 323p 27-648MHz 4-032MHz 323p 27-648MHz 4-03619M 135p 48MHz 5-0MHz 355p 100MHz 8hythm Generator, Diamatic Mod Send SAE for list.	323p         incl. RF Modulator         £21.50           323p         Readybuilt and tested         £28.50           323p         UHF Modulator         £20p           323p         UHF Modulator         250p           323p         Wide Bandwidth Modulator         250p           392p         Special for Computers         470p           900p         Power         Supplan         £14.95           33p         ±12V = 0.25A         £14.95           362p         ±15V = 0.2A         £14.95           362p         ±15V = 0.2A         £14.95           350p         KEYPADS, 4 × 4 matrix, Reed         323p           300p         Full ASCH Keyboard         £45.50           322p         witch assembly         350p           ern, etc.         10° MONITOR, suitable for alphanumerics or analogue signals.           220V mains or 12V DC. Compatier System.         Value for money           Value for money         £85.00
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**Specification** 

Set or clear break point Restore from break Load from tape Store on tape Go (recalls last address used) Reset Monitor features System program Set of sub-routines for use in programming Powerful de-bugging facility displays all internal registers Tape load and store routines

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Practical Electronics February 1980

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R's & tur	ning pots - see list for options		
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Additional Delay basic components	KIT 83-2	£20.07
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# Apple I plus Nascom 2

Microprocessor 280A 8 bit CPU. This will run at 4 MHz but is selectable between 1/2/4/ MHz.

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- Memory
- On-board, addressable memory 2K Monitor Nas-sys 1
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PIO

There is also a totally uncommitted PIO (MK3881) giving 16, programmable, I/O

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Naccom 2 in hit	Nett	V.A.T.	Total
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Graphics ROM	15.00	2.25	17.25

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devices. Complete manual with sample software

Applications Light displays Industrial process control Model Railway Control. Pre programmed music generation Robots, Central Heating Systems Stepping Motors

	Nett	V.A.T.	Total
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Kit	49.95	7.49	57.44
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CASE (includes				
P.S.U.)	78.00	11.70	89.70	
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Console: CPU: 9900 family, 16 bit microprocessor, plus 256 byte scratchpad RAM.

Memory

## Sharp

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A complete personal computer system for the microcomputer user at an additional A complete personal computer system for the microcomputer user, at an economic price The Sharp comes complete with all necessary perpherals, sample software and excellent documentation — giving the user a personal system of unmatched liexibility and ease of use. At the heart of the machine is the 2-80 CPU — widely accepted as the most powerful 8-bit CPU on the market A 4K byte system monitor controls system operation. From 4 to 48K of RAM can be resident on board; enough room for the most demanding applications.

applications

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Nett V.A.T. Total

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Console

Modules

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Түре АС107	Price*	Type BC441	Price £0.25	Type TIP30A	Price £0.30
AC126 AC127	£0.14 £0.16	BC460 BC461	£0.28 £0.28	TIP30B TIP30C	£0.32 £0.34
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C1C4	with pointer #" standard screw fit	0.15
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5364	1 Instrument knob – black/silver aluminium top (17 × 15mm) <sup>1</sup> / <sub>2</sub> " standard screw fit	0.12
METAL	1 Instrument knob – black/silver aluminium top (17 × 15mm) ‡" standard screw fit CASE DUAL SLIDER POTS: 46mm travel	0.12
METAL ( SJ65	1 Instrument knob – black/silver aluminium top (17 × 15mm) ‡" standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 0.21	0.12
METAL ( SJ65 SJ66 SJ67	1 Instrument knob – blackjsilver aluminium top (17 x 15mm) ∦ standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 0.2t 100K lin 0.22 Chrome slider knobs to fit 0.11	0.12 each each
METAL ( SJ65 SJ66 SJ67 SJ68	1 Instrument knob – blackjeliver aluminium top (17 x 15mm) <sup>1</sup> / <sup>9</sup> standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 00K lin 0,22 Chrome slider knobs to fit 0,10 30 ZTX300 type transistor NPN pré-formed for	0.12 Seach Seach Seach
METAL I SJ65 SJ66 SJ67 SJ68	1 Instrument knob – blackjeilver aluminium top (17 × 15mm) ∳* standard screw fit CASE DUAL SLIDER POTS: 46mm travel 100K log 0.2t 100K lin 0.2t Chrome slider knobs to fit 0.1t 30 ZTX300 type transistor NPN pre-formed for P/C Board solour coded blue – all perfect 20 ZTX500 uses tensister PNB me formed for	0.12 Seach Seach Seach Seach
METAL ( SJ65 SJ66 SJ67 SJ68 SJ69	1 Instrument knob – blackjeilver aluminium top (17 × 15mm) ≟* standard screw fit CASE DUAL SLIDER POTS: 45mm travel 100K kin 0.22 Chrome slider knobs to fit 0.10 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect	0.12 seach seach seach 1.00
METAL ( SJ65 SJ65 SJ67 SJ68 SJ69 SJ69 SJ70	1 Instrument knob – blackjeliver aluminium top (17 × 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 Chrome slider knobs to fit 0.31 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded white – all perfect 25 BC107 NPN T0106 case perfect transistors	0.12 seach seach 1.00 1.00
METAL ( SJ65 SJ66 SJ66 SJ67 SJ68 SJ69 SJ69 SJ70	Instrument knob – blackjeliver aluminium top (17 x 15mm) ½* standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 00K lin 0.22 00K lin 0.23 02 TX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded white – all perfect 25 B C107 NPN T0106 case perfect transistors code C1359 25 B PLT DNB T0106 case perfect transistors	0.12 5 each 5 each 1.00 1.00 1.00
METAL ( SJ65 SJ66 SJ67 SJ68 SJ69 SJ70 SJ71	1 Instrument knob – blackjeliver aluminium top (17 x 15mm) ½* standard screw fit 10K log 0.2t 10K log 0.2t 20K lin 0.2t 20K lin 0.2t 20 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded white – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC177 PNP T0106 case perfect transistors code C1395	0.12 each each each 1.00 1.00 1.00 1.00
METAL ( SJ66 SJ66 SJ67 SJ68 SJ69 SJ70 SJ71 SJ72	1 Instrument knob – blackjeliver aluminium top (17 × 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 Chrome slider knobs to fit 0.11 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1355 25 BC177 PNP T0166 case perfect transistors code C1395	0.12 5 each 5 each 1.00 1.00 1.00 1.00 1.00
METAL ( SJ66 SJ66 SJ69 SJ69 SJ70 SJ71 SJ72 SJ73	1 Instrument knob – blackjeliver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 Chrome slider knobs to fit 0.10 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1395 25 BC177 PNP T0106 case perfect transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded	0.12 5 each 5 each 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 1.00
METAL ( SJ66 SJ67 SJ68 SJ69 SJ70 SJ70 SJ71 SJ72 SJ73 SJ74	Instrument knob – blackjeliver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit (CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 00K lin 0.22 00K lin 0.22 00 ZTX300 type transistor NPN prei-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded white – all perfect 25 BC107 NPN T0106 case perfect transistors code C1395 25 BC177 PNP T0106 case perfect transistors code C1395 4 2N3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded B way ribbon cable – colour coded individually	0.12 5 each 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 PVC
METAL ( SJ66 SJ66 SJ67 SJ68 SJ69 SJ70 SJ70 SJ71 SJ72 SJ73 SJ74	1 Instrument knob – blackjeilver aluminium top (17 x 15mm) <sup>1</sup> / <sup>9</sup> standard screw fit CASE DUAL SLIDER POTS: 46mm travel 10K log 0.22 Chrome slider knobs to fit 0.10 30 ZTX300 type transistor NPN prei-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded white – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC177 PNP T0106 case perfect transistors code C1395 4 ZN3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded B way ribbon cable – colour coded individually insulated solid tinned copper conduction	0.12 5 each 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 PVC
METAL ( SJ66 SJ67 SJ68 SJ69 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75	1 Instrument knob – blackjeliver aluminium top (17 × 15mm) <sup>4</sup> / <sup>9</sup> standard screw fit (CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 Chrome slider knobs to fit 0.11 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 B C107 NPN T0106 case perfect transistors code C1359 25 B C177 PNP T0106 case perfect transistors code C1395 2 N3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded B way ribbon cable – colour coded individually insulated solid tinned copper conduction 0.20 FM coax cable – plain copper conduction	0.12 5 each 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 PVC
METAL ( SJ66 SJ67 SJ68 SJ69 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75	Instrument knob – blackjeliver aluminium top (17 × 15mm) <sup>4</sup> / <sup>5</sup> standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 10K log 0.22 Chrome slider knobs to fit 0.27 X300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1395 2 N3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded B way ribbon cable – colour coded individually insulated solid tinned copper conduction color PM coax cable – plain copper conduction color plain copper conduction P/M coax cable – plain copper traiter P/M coax cable – plain copper conduction cellor P/M coax cable – colour code cellor pla	0.12 5 each 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 PVC
METAL ( SJ65 SJ65 SJ67 SJ68 SJ69 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ76	Instrument knob – blackjølver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 100K lin 0.27 Chrome slider knobs to fit 0.10 30 ZTX300 type transistor NPN prei-formed for P/C Board colour coded blue – all perfect 30 ZTX300 type transistor PNP prei-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP prei-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1395 2 BC177 PNP T0106 case perfect transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded way ribbon cable – colour coded individually insulated solid tinned copper conduction 0.20 FM coax cable – plain copper conduction cel polythme insulated and plain copper braidee PVC sheath – impedance 75 ohms 0.10 Board containing 2 x 5 bin D10 Sockets 180	0.12 seach seach seach seach 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
METAL ( SJ65 SJ65 SJ65 SJ69 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ76	Instrument knob – blackjalver aluminium top (17 × 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit IOK log     Ozt 10K log     Ozt Chrome silder knobs to fit     Ozt Chrome silder knobs to fit     Ozt Ozt X300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN TO106 case perfect transistors societ C1355 25 BC177 PNP T0106 case perfect transistors Societ C1355 4 2N3055 silicon power NPN transistors T03 6 T064 SCR3 Amp assorted 50v – 400v all codrat 8 way ribbon cable – colour coded individually insulated solid tinned copper conduction Cax cable – plain copper conduction PVC Beath – impedance 75 ohms     0,10 10 Board containing 2 x 5 pin DIN sockets 18C 0 2-2 pin DNN sockets     10 Codes 18C	0.12 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 1.00 PVC meter lular 5 0.30
METAL ( SJ66 SJ66 SJ67 SJ69 SJ70 SJ71 SJ72 SJ74 SJ75 SJ76 SJ76 SJ77	Instrument knob – blackjeliver aluminium top (17 × 15mm) <sup>4</sup> / <sup>2</sup> standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 10K log 0.27 Chrome slider knobs to fit 0.27 Chrome slider knobs to fit 0.27 CB and colour coded blue – all perfect 20 ZTK300 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC107 NPN T0106 case perfect transistors code C1395 2 N3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded B way ribbon cable – colour coded individually insulated solid timed copper conduction 0.20 FM coas cable – plain copper braidec PVC sheath – impedance 75 bin DIN sockets 180 0.20 - 10 NI N040peaker socket A 5 pin DIN 180° chassix/normal socket incl. PDOT	0.12 5 each 5 each 5 each 1.00
METAL ( SJ66 SJ66 SJ67 SJ68 SJ69 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ75 SJ75 SJ76 SJ77 SJ83	Instrument knob – blackjeliver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit IOK log 0.22 IOK log 0.22 IOK lin 0.22 Chrome slider knobs to fit 0.10 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC177 PNP T0106 case perfect transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded B way ribbon cable – colour coded individually insulated solid tinned copper conduction insulated solid tinned copper conduction cell polythane insulated and plain copper braidec PVC sheath – impedance 75 ohms 0.10 Board containing 2 x 5 pin D1N sockets 1 BC 0 2-2 pin OIN loudspeaker socket A 5 pin D1N 180° chassis/normal socket incl. OPOT switch 6 Germ. 0CP71 type photo transistors	0.12 5 each 5 each 5 each 1.00 0.00 1.00 0.00 1.00 0.00 1.00 0.00
METAL ( SJ66 SJ66 SJ67 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ76 SJ77 SJ75	Instrument knob – blackjälver aluminium top (17 × 15mm) <sup>4</sup> / <sup>9</sup> standard screw fit IOK log 0.22 100K log 0.22 Chrome slider knobs to fit 0.11 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC177 PNP T0106 case perfect transistors code C1359 4 ZN3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded 8 way ribbon cable – colour codec individually insulated solid tinned copper conduction COC PM coas cable – plain copper conduction PVC sheath – impedance 75 ohms 0.10 10 Board containing 2 x 5 pin DIN sockets 18C 0 2.2 z pin OIN lood casesistors A 5 pin OIN 180° chassis/normal socket inct. OPOT switch 5 Germ. OCP71 type photo transistors 10 BD131 NPN transistors MHe rejects 10 BD151 NPN transistors     10 BD151 NPN tra	0.12 5 each 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.30 0.30 0.20 1.00 0.50
METAL ( SJ66 SJ66 SJ67 SJ68 SJ69 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ76 SJ76 SJ77 SJ75 SJ76 SJ77 SJ83 SJ84 SJ85 SJ85	1 Instrument knob – blackjeliver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit 10K log 0.22 100K lin 0.22 Chrome slider knobs to fit 0.11 30 ZTX300 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1355 28 BC177 PNP T0106 case perfect transistors code C1395 2 N3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded B way ribbon cable – colour coded individually insulated solid tinned copper conduction 0.20 FM coax cable – plain copper conduction board containing 2 x 5 pin DIN sockets 18C 0.2.2 pin OIN loadpeaker sockets A 5 pin DIN 180° chassis/normal socket incl. 0POT switch 5 Germ. OCP71 type photo transistors T0-126 6 PNP Darlington Power transistors T0-126	0.12 5 each 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.20 0.50
METAL ( SJ65 SJ66 SJ67 SJ68 SJ69 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ75 SJ76 SJ75 SJ76 SJ77 SJ83 SJ84 SJ85 SJ86 SJ85 SJ86	1 Instrument knob – blackjälver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit (CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 Chrome slider knobs to fit 0.11 30 ZTX300 type transistor NPN pre-formed for P/C Board solour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board solour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC177 PNP T0106 case perfect transistors code C1395 2 N3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded 8 way ribbon cable – colour coded individually insulated solid tinned copper conduction 0.20 FM coas cable – plain copper conduction board containing 2 x 5 pin DIN sockets 180 0 2-2 pin OIN loudspeaker socket A 5 pin DIN 180° chassis/normal socket incl. 0POT switch 5 Germ. 0CP71 type photo transistors 10 BD131 NPN transistors at vLTS10-20VCB	0.12 each each each each each 1.00 0.00 0.50
METAL ( SJ86 SJ86 SJ67 SJ68 SJ67 SJ70 SJ77 SJ73 SJ74 SJ75 SJ75 SJ76 SJ75 SJ76 SJ77 SJ75 SJ76 SJ77 SJ75 SJ76 SJ77 SJ84 SJ86 SJ86 SJ86 SJ87	Instrument knob – blackjälver aluminium top (17 x 15mm) <sup>4</sup> / <sup>9</sup> standard screw fit CASE DUAL SLIDER POTS: 46mm travel 10K log 0.22 10K log 0.22 Chrome slider knobs to fit 0.10 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC107 NPN T0106 case perfect transistors code C1395 4 2N3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded B way ribbon cable – colour coded individually insulated solid tinned copper conduction plotythene insulated and plain copper braidee PVC sheath – impedance 75 ohms 0.10 Board containing 2 x 5 pin DIN sockets 1BC 0 2-2 pin OIN loudspeaker socket 4 5 pin DIN 180° chassistors 10 BD131 NPN transistors tow H6 rejects 6 PNP T0-3 germ, power transistors T0-126 5 PNP T0-3 germ, power transistors at VLS10-20VCB 20 asst. heat isinks T01/5/18/92	0.12 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.00 0.00 0.20 0.50 0.50
METAL ( SJ86 SJ86 SJ69 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ76 SJ76 SJ76 SJ76 SJ76 SJ77 SJ83 SJ84 SJ85 SJ87 SJ88 SJ87 SJ88	1 Instrument knob – blackjälver aluminium top (17 × 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit (CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 Chrome silder knobs to fit 0.11 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code 0.1355 26 BC177 PN P0106 case perfect transistors code 0.1355 26 BC177 PN P0106 case perfect transistors code 0.1355 4 2N3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded 8 way ribbon cable – colour coded individually insulated solid tinned copper conduction PVC deat containing 2 x 5 pin DIN sockets 180 0.2.0 FM coax cable – plain copper braide PVC sheath – impedance 75 ohms 0.100 1 Board containing 2 x 5 pin DIN sockets 180 0.2.2 pin OIN 180° chassis/normal socket incl. OPOT switch 5 Germ. OCP71 type photo transistors 10 BD131 NPN transistors 101/16/92 2 Asst. heat sinks T01/5/18/92 2 Post Office relays 20 Mixet dualues 400mW resea diode 2.10.	0.12 0.12 0.12 0.12 0.100 1.00 1.00 1.00 1.00 1.00 1.00 0.00 0.00 0.50 0.50 0.50 0.50
METAL ( SJ65 SJ66 SJ67 SJ67 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ76 SJ75 SJ76 SJ77 SJ75 SJ76 SJ77 SJ83 SJ85 SJ70 SJ71 SJ72 SJ73 SJ75 SJ85	1 Instrument knob – blackjeliver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit (CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 Chrome slider knobs to fit 0.11 30 ZTX300 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC107 PNP T0106 case perfect transistors code C1395 2 N3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded B way ribbon cable – colour coded individually insulated solid tinned copper conduction 0.20 FM coax cable – plain copper conduction body these the impedance 75 ohms 0.100 10 Board containing 2 x 5 pin DIN sockets 180 0.2.2 pin OIN 1080 peaker socket A 5 pin DIN 180° chassis/normal socket incl. 0 POT switch 5 Germ. OCP71 type photo transistors 10 BD131 NPN transistors 10v He rejects 5 PNP T0-3 germ, power transistors at vLTS10-20VCB 20 Asst. heat slinks T01/5/18/92 2 Post Office relays 20 Mixed values 400mW zener diodes 11-30v	0.12 5 each 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 1.00 5 0.30 0.50 0.50 0.50 0.50 0.50 0.50
METAL ( SJ65 SJ66 SJ67 SJ68 SJ67 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ75 SJ76 SJ75 SJ76 SJ77 SJ75 SJ76 SJ77 SJ83 SJ84 SJ85 SJ86 SJ87 SJ85 SJ86 SJ87 SJ87 SJ87 SJ7	1 Instrument knob – blackjeliver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit (CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 Chrome slider knobs to fit 0.11 30 ZTX300 type transistor NPN pre-formed for P/C Board solour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board solour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC177 PNP T0106 case perfect transistors code C1395 4 2N3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded 8 way ribbon cable – colour coded individually insulated solid tinned copper conduction code code cable – plain copper conduction by theme insulated and plain copper braides PVC sheath – impedance 75 ohms 0.100 1 Board containing 2 x 5 pin DIN sockets 180 0 2-2 pin OIN loudspeaker socket 6 Spin DIN 180° chassis/ormal socket incl. OPOT switch 6 Germ. 0CP71 type photo transistors 10 BD131 NPN transistors low He rejects 5 PNP T0-3 germ. power transistors at vLTS10-20VCB 20 Asst. heat sinks T01/5/18/32 2 Post Office relays 20 Mixed values 400mW zener diodes 3-10v 20 Mixed values 400mW zener diodes 3-10v 20 Mixed values 400mW zener diodes 3-10v	0.12 5 sech 5 sech 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.00 0.50 0.50 0.50 0.50 0.50
METAL ( SJ86 SJ86 SJ68 SJ67 SJ68 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ75 SJ76 SJ75 SJ76 SJ75 SJ76 SJ77 SJ83 SJ84 SJ86 SJ87 SJ88 SJ87 SJ88 SJ87 SJ88 SJ87 SJ89 SJ90 SJ70 SJ70 SJ71 SJ72 SJ72 SJ75 SJ76 SJ76 SJ77 SJ76 SJ77 SJ77 SJ76 SJ77 SJ76 SJ77 SJ77 SJ76 SJ77 SJ76 SJ77 SJ76 SJ77 SJ76 SJ77 SJ80 SJ87 SJ80 SJ87 SJ80 SJ90 SJ90 SJ90 SJ90 SJ90 SJ90 SJ90 SJ90 SJ80	1 Instrument knob – blackjälver aluminium top (17 × 15mn) <sup>1</sup> / <sup>2</sup> standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 100K lin 0.23 Chrome silder knobs to fit 0.11 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC177 PNP T0106 case perfect transistors code C1359 2 BC177 PNP T0106 case perfect transistors To C C C C C C C C C C C C C C C C C C C	0.12 5 each 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.00 0.50 0.50 0.50 0.50 0.50
METAL ( SJ86 SJ86 SJ69 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ76 SJ76 SJ76 SJ76 SJ77 SJ83 SJ84 SJ85 SJ86 SJ89 SJ89 SJ89 SJ89 SJ89 SJ89 SJ81 SJ85 SJ86 SJ89 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ76 SJ76 SJ76 SJ77 SJ76 SJ77 SJ77 SJ77 SJ77 SJ77 SJ78 SJ77 SJ78 SJ79 SJ79 SJ79 SJ79 SJ79 SJ79 SJ79 SJ79 SJ79 SJ79 SJ79 SJ79 SJ79 SJ79 SJ79 SJ79 SJ89 SJ99	1 Instrument knob – blackjsilver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit 10K log 0.22 100K lin 0.22 Chrome silder knobs to fit 0.11 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded white – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded white – all perfect 25 BC107 NPN T0106 case perfect transistors code C1355 28 BC177 PNP T0106 case perfect transistors code C1355 2 X305 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded B way ribbon cable – colour coded individually insulated solid tinned copper conduction P/C Goax cable – plain copper conduction P/C soax cable – plain copper transistors 0.20 FM coax cable – plain copper transistors 10 B D131 NPN transistors MB rejects 6 PND Darlington Power transistors 10 B D131 NPN transistors at vLTS10-20VCB 20 Aast, heat sinks T01/5/18/92 2 Post Office relays 20 Mixed values 400mW zener diodes 3-10v 20 Mixed values 1W zener diodes 11-33v B Silicon Bridge Rectifiers up to 4Amp 200v + Data	0.12 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 1.00 5.00 0.50 0.
METAL ( SJ66 SJ66 SJ67 SJ68 SJ67 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ76 SJ76 SJ76 SJ77 SJ83 SJ85 SJ86 SJ85 SJ85 SJ87 SJ88 SJ87 SJ88 SJ87 SJ88 SJ87 SJ87 SJ87 SJ87 SJ87 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ87 SJ87 SJ86 SJ87 SJ97 SJ77 SJ7	1 Instrument knob – blackjälver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit (CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 Chrome slider knobs to fit 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC107 NPN T0106 case perfect transistors code C1395 2 N3055 allicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded 8 way ribbon cable – colour coded individually insulated solid tinned copper conduction 0.20 FM coax cable – plain copper conduction boy the status of the	0.12 5 each 5 each 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.50
METAL ( SJ86 SJ86 SJ86 SJ67 SJ68 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ75 SJ76 SJ75 SJ76 SJ75 SJ85 SJ85 SJ85 SJ86 SJ87 SJ88 SJ87 SJ88 SJ87 SJ88 SJ87 SJ86 SJ87 SJ86 SJ87 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ75 SJ76 SJ76 SJ76 SJ76 SJ77 SJ75 SJ76 SJ77 SJ76 SJ77 SJ76 SJ77 SJ76 SJ77 SJ77 SJ76 SJ77 SJ76 SJ77 SJ76 SJ77 SJ76 SJ77 SJ76 SJ77 SJ76 SJ77 SJ76 SJ87 SJ87 SJ87 SJ87 SJ87 SJ86 SJ87 SJ87 SJ87 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ86 SJ87 SJ86 SJ86 SJ87 SJ86 SJ86 SJ87 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ87 SJ86 SJ86 SJ87 SJ86 SJ86 SJ87 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ86 SJ90 SJ96	Instrument knob – blackjälver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 10K log 0.22 Chrome slider knobs to fit 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC177 PNP T0106 case perfect transistors code C1395 4 2N3055 allicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded 8 way ribbon cable – colour coded individually insulated solid tinned copper conduction red polythene insulated and plain copper braider PVC sheath – impedance 75 ohms 0.10 10 Board containing 2 x 5 pin D1N sockets 18C 0 2-2 pin OIN loudspeaker socket 4 S pin D1N 180° chassis/ormal socket incl. OPOT switch 6 Germ. 0CP71 type photo transistors 10 BD131 NPN transistors low He rejects 5 PNP T0-3 germ. power transistors 10 - 125 5 PNP T0-3 germ. power transistors 2 - 125 5 PNP T0-3 germ. power transistors 2 - 20 20 Asst. heat sinks T01/5/18/92 2 Post Office relays 20 Mixed values 400mW zener diodes 3-10v 10 Mixed values 1W zener	0.12 5 sech 5 sech 1.00 1.00 1.00 1.00 1.00 1.00 0.00 PVC PVC 0.30 0.50
METAL ( SJ86 SJ86 SJ68 SJ67 SJ68 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ76 SJ76 SJ76 SJ77 SJ83 SJ84 SJ85 SJ84 SJ85 SJ84 SJ85 SJ84 SJ85 SJ84 SJ85 SJ84 SJ85 SJ87 SJ85 SJ87 SJ83 SJ90 SJ92 SJ90 SJ92 SJ95 SJ96 SJ96 SJ66 SJ67 SJ76 SJ77 SJ83 SJ84 SJ85 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ87 SJ76 SJ76 SJ76 SJ76 SJ76 SJ76 SJ76 SJ76 SJ76 SJ76 SJ76 SJ76 SJ76 SJ76 SJ76 SJ76 SJ87 SJ86 SJ87 SJ86 SJ87 SJ86 SJ86 SJ87 SJ86 SJ86 SJ86 SJ87 SJ86 SJ86 SJ86 SJ86 SJ87 SJ86 S SJ86 SJ86 SJ86 S SJ86 S SJ86 SJ86 S SJ86 S SJ86 SJ86	1 Instrument knob – blackjälver aluminium top (17 x 15mm) <sup>12</sup> standard screw fit 10K log 0.22 100K lin 0.23 Chrome silder knobs to fit 0.11 30 ZTX300 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor NPN pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1355 20 BC177 PNP to power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded 8 way ribbon cable – colour coded individually insulated solid tinned copper conduction PVC sheath – impedance 75 ohms 0.100 1 Board containing 2 x 5 pin D1N sockets 180 0 2.2 pin O1N 180° chassis/normal socket incl. OPOT switch 5 Germ. OCP71 type photo transistors 10 BD131 NPN transistors 101/5/18/92 2 Post Office relays 20 Mixed values 400mW zener diodes 3-10v 20 Mixed values 400mW zener diodes 3-10v 20 Mixed values 100 zener diodes 3-10v 10 Mixed values 100 zener diodes 11-33v 8 Bilicon Bridge Rectifiers up to 4Amp 200v + Data 1 Battery holder to take 6 x HP7's 5 assorted ferrite rods 2 tuning gangs MW/LW 50 meter asst. colours single strand wire	0.12 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 5 0.50
METAL ( SJ65 SJ66 SJ66 SJ67 SJ70 SJ71 SJ72 SJ73 SJ74 SJ75 SJ76 SJ76 SJ76 SJ77 SJ75 SJ76 SJ77 SJ83 SJ85 SJ85 SJ88 SJ89 SJ85 SJ89 SJ89 SJ95 S	1 Instrument knob – blackjsilver aluminium top (17 x 15mm) <sup>1</sup> / <sup>2</sup> standard screw fit (CASE DUAL SLIDER POTS: 45mm travel 10K log 0.22 Chrome slider knobs to fit 0.30 ZTX300 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 30 ZTX500 type transistor PNP pre-formed for P/C Board colour coded blue – all perfect 25 BC107 NPN T0106 case perfect transistors code C1359 25 BC107 NPN T0106 case perfect transistors code C1395 2 N3055 silicon power NPN transistors T03 6 T064 SCRs 5Amp assorted 50v – 400v all coded B way ribbon cable – colour coded individually insulated solid timed copper conduction 0.20 FM coax cable – plain copper torduction body these the impedance 75 ohms 0.100 1 Board containing 2 x 5 pin DIN sockets 180 0 2.2 pin OIN 1040 peaker socket A 5 pin DIN 180° chassis/normal socket incl. 0 POT switch 5 GPM Darlington Power Transistors at vLTS10-20VCB 20 Asst. heat sinks T01/5/18/92 20 Mixed values 400mW zener diodes 11-33v B Silicon Bridge Rectifiers up to 4Amp 200V - Data 1 Battery holder to take 6 x HP7's 5 assorted ferrite rods 2 tuning gang MW/LW 50 meters asst. colours single strand wire 1 denter asst. colours single strand wire 1 denter asst.	0.12 5 each 5 each 5 each 5 each 5 each 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 5 0 0.55 0.5
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#### BREADBOARD

A<sup>T</sup> THE time of writing the Bread-board exhibition is pulling in the crowds in London and the editorial staff of PE are at full stretch manning the stand, visiting exhibitors and producing this issue-we hope it doesn't show! Breadboard looks like becoming the premier event for the electronics hobbvist. In only its second year it has attracted large crowds, is very well presented and has an excellent atmosphere-even though it is sometimes difficult to talk to people over the raucous noise being generated by various synthesisers, organs, discos etc. (organisers please note!).

An exhibition such as this gives us a chance to meet casual and dedicated readers. We take the opportunity to discuss various projects and enquire into your views on PE. Thankfully most are full of praise and often some new project ideas get thrown up for our consideration. Some, of course, are not so happy-unfortunately we have failed to please them. It would appear that in these cases we are not giving enough space to their particular subject or, more commonly, we are giving too much space to another facet of our hobby in which they are not interested.

The problem is, having talked to a number of readers, often with widely varying views, just what do we do with all the information. It is all too easy to twist it around so that it fits in with our own views, or to balance out two divergent attitudes and take the middle path; which may in fact please neither party.

For instance, two comments which came up were (a) we carry too many microprocessor oriented articles and (b) we give too much space to music and audio projects. Now we could please both parties by cutting back on these subjects, but wait, we know these are very popular areas by the number of kits and components sold-2000 Compukits (at £250 each) at the last count and excellent quantities of mixers, guitar sound multiprocessors etc. So we would probably offend many readers by cutting back on either subject. We do try to keep the balance right, to be aware of new trends and to provide the right information at the right time but it's not easy to please everyone.

#### PROJECTS

One thing that fascinates us is that virtually all the comments are concerned with projects. Although we try to publish about five projects, or parts thereof, each month these normally make up less than half of our total number of editorial pagespresumably everyone is over the moon with the rest of the contents?

Another interesting angle is uncovered when one enquires as to how many projects most readers construct during a year-the average is probably about one project per reader per year. So why are some readers so much in favour of reading about their pet subject but so much against learning, or even just reading, about ideas and circuitry from another discipline? Any comments?

Finally, our thanks to all those who visited our stand at Breadboard. To those who live too far away or who just could not come along-it's a great event-if you get the chance we would be pleased to see you next time.

We hope to publish a review of the exhibition next month; our apologies to those who have seen it all first hand.

Mike Kenward

#### EDITOR

#### Mike Kenward

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#### **Technical Queries**

We are unable to offer any advice on the use or purchase of commercial equipment or the incorporation or modification of designs published in Practical Electronics.

All letters requiring a reply should be accompanied by a stamped, self addressed envelope and each letter should relate to one published project only.

Components are usually available from advertisers; where we anticipate supply difficulties a source will be suggested.

#### **Back Numbers**

Copies of most of our recent issues are available from: Post Sales Department (Practical Electronics), IPC Magazines Ltd., Lavington House, 25 Lavington Street, London SE1 OPF, at 75p each including Inland/Overseas p&p.

#### Rinders

Binders for PE are available from the same address as back numbers at £3.75 each to UK or overseas addresses, including postage and packing, and VAT where appropriate. Orders should state the year and volume required.

#### Subscriptions

Copies of PE are available by post, inland or overseas, for £10.60 per 12 issues, from: Practical Electronics, Subscription Department, Oakfield House, Perrymount Road, Haywards Heath, West Sussex RH16 3DH. Cheques and postal orders should be made payable to IPC Magazines Limited.

# Market Place

Items mentioned are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned. All quoted prices are those at the time of going to press.

#### by David Shortland

#### **AUDIO VISUAL**

Two new AV machines have just been launched on the market. The 340 model is a cassette recorder with four identical audio channels, each with full metering facilities and Dolby Noise Reduction. Each channel has two inputs, microphone and line, a fixed level



line output, and a controlled output which can give in excess of +8dBm.

Independent record selection is provided for each pair of tracks to facilitate stereo recording (tracks 1 and 2) or all four tracks simultaneously. If required, tracks 1 and 2 can be recorded first then tracks 3 and 4 added whilst replaying tracks 1 and 2. Alternatively, tracks 1 and 2 can be recorded after tracks 3 and 4. The 330 model has two audio channels with a separate sync track for audio visual applications.

The two audio channels have full metering facilities and Dolby Noise Reduction and each audio channel has the same specification as the 340. They sync channel also provides full metering facilities and selection for the use of normal and special tapes.

When the 330 is used with external sync pulse coding/decoding equipment, the sync channel has a single line input and a line output. It also has an internal sync pulse generator triggered by a button on the front panel to provide a recorded pulse for direct connection to a projector.

For further details including price and delivery contact: Neal-Ferrograph, Simonside Works, South Shleids, Tyne & Wear NE34 9NX.

#### FLUKE DMM

Microprocessor techniques have allowed Fluke to incorporate some very useful features in their latest low cost  $4\frac{1}{2}$  digit 8050A DMM. This highly accurate bench/portable model with 39 measurement ranges and nine functions also provides unique dB computing and offset modes in addition to a high performance true r.m.s. capability.

In the dB mode, the 8050A DMM allows the user to call up any of 16 reference impedance levels from 8 to 1,200 ohms and to display the readings directly in dBs.

Additionally, a reference/offset mode allows any input signals to be stored either as a reference value for relative dB readings or as an offset against any reading. In offset mode, the user can zero-out any lead resistances for really high resolution impedance measurements or set up a reference offset and display only the variance from that reading.

These absolute and relative dB modes with offset greatly simplify measurements in audio, amplifiers and telecommunications circuits as well as in production testing where only the variance from the stored value may be required. The offset facility is available on all functions such as a.c./d.c. volts or amps, resistance or conductance.

The high resolution  $4\frac{1}{2}$  digit l.c.d. display is matched by a basis d.c. accuracy of 0.03 per cent specified over a full year. A.c. or d.c. measurements can be made down to  $10\mu$ V, 10 nA or 10 milliohms.

In addition to its volts, ohms and amps ranges, the 8050A also has two conductance ranges for high impedance measurements to



100,000 Megohms, as well as low power ranges for in-circuit measuring.

A wide range of accessories such as high voltage probes, current transformers, shunts, temperature and r.f. probes, remote hold probe, battery pack, and safety leads make the 8050A a complete measurement system for the bench or field.

The 8050A is priced at £199 ex. VAT and carriage.

Fluke International Corporation, Colonial Way, Watford, Herts WD2 4TT.

#### **BOOTS VIDEO**

All Boots audio departments are now selling the Ferguson VHS Videostar recorder (Model 3V00) which has a maximum recording time of 3 hours.

The 3V00 has a remote hand-held "pause unit" which can be used to edit unwanted material during recording or playback. Boots



will also carry a wide range of blank video tapes not only for the Videostar and other VHS recorders but also for machines using VCR and Beta format tapes.

Also available is a full colour catalogue of 45 pre-recorded programmes and feature films.

The price of the 3V00 is £595.00 with blank cassettes from £6.95 to £16.95 and prerecorded films from £17.50.

#### **ELECTRONIC NOTEBOOK**

Like the first model introduced last year, the Toshiba LC-1038MN calculator offers alpha-numeric facilities which has now been expanded to a full ten digit alphabetic and/or numeric entry and display, plus sign. There is an independent 30-register memory bank, each register able to retain data consisting of 10-alphabetic characters and 10-numerals. The addition of a 26-location world-time display, plus clock/calendar and alarm. There is instant retrieval of the world-time display; the calendar indicates month, date and day of



week; and the alarm can be set up to one year in advance and to prompt an alpha display.

The calculator is ideal for the storage of information in constant use, but which is subject to frequent change such as currency exchange rates; share buying and selling prices; bank and audit card balances; train and plane departure and arrival times; stock levels; metric conversion factors; travellers cheque numbers.

The LC-1038MN operates on batteries lasting around 9,000 hours; is sized  $70 \times 10 \times 137$ mm and weighs 80g (2.80z). It is priced around £75, plus VAT.

#### **SAFETY TESTER**

Clare Instruments Limited have developed a portable safety test unit for checking double insulated and earthed electrical equipment.



The V152, will flash test double insulated appliances at 4kV. Another noteworthy feature, is the high current used for earth bond testing (25A at 8V). Too many testers, at present available, offer only a simple continuity check for this important test. The unit operates from a mains supply and the appliance under test is plugged into the 13 amp socket on the front panel of the tester. When the test button is pressed, neon lamps indicate that the series of tests is completed, with green lights for passes and red lights for failures.

The tester which is housed in a hardwood case is priced at £144.50 ex. VAT and p&p.

Clare Instruments Limited, Clare Works, Woods Way, Goring-by-Sea, Worthing.

#### **NEGATIVE ION GENERATORS**

Most of the air around us is electrically neutral with only a few of the air molecules gaining or losing electrons and therefore acquiring a positive or negative charge.

The effect of these charged molecules, which are called air ions, on individual health has been researched over many years and it has become clear that it is the balance of negative and positive ions rather than high ion concentration which is important.

Research has also shown that sufferers from asthma, hay fever and bronchitis can benefit from having the air they breathe charged with negative ions. There is also considerable evidence that ion depletion, such as



occurs in offices or crowded rooms, produces discomfort, drowsiness, fatigue and loss of mental and physical efficiency.

The concentration of negative ions in the air can be increased using a negative ion generator. Two such generators have just been introduced by J. P. Bell Ltd., the Kobelair Model 20 is a desk unit suitable for individual usage whereas the Model 40 is suitable for rooms up to 40 cubic metres (1500 cubic feet) with a maximum effectiveness over a range of 0.5 to 2.5 metres (2 to 8 feet).

The model 20 is priced at £57.50 and the Model 40 at £98.50 excluding VAT and p&p.

J. P. Bell (Machinery) Ltd., Jubilee works, London Road, Woolmer Green, Knebworth, Herts.

#### **SUPERDECK FOR MPUs**

The V&T Superdeck is a high speed cassette unit which will, under CPU control, find any file stored on a C60 cassette (one megabit of unformatted memory on each side) in under one minute using fast forward and fast reverse speeds (up to 50 i.p.s.).

Other features of the Superdeck include: 5000 baud CUTS format as standard (which can be switched to other lower speeds, error detection and correction (it will also write protected areas of tape containing hard errors), it will write into the first empty file, on tape or into any file number or name specified (unless that particular file is write protected in which case an error message is generated).

At the present time only a Z80 operating system is available.

The unit which connects to any 8bit I/O port and UART includes a 240V supply unit.

The price of the Superdeck is £110 plus VAT and p&p. V&T Electronics, 82 Chester Road, London N19.

#### WIRE BIN

The WB-16 wire bin has been designed for both storage and wiring table use, keeping assorted wires separated in their correct size groups and preventing wasteful tangling.



The sixteen wire storage tubes have adjustable depth stops to take wire lengths from 25mm and 350mm. The price of the WB-16 is £33.81 excluding VAT and p&p.

OK Machine & Tool (UK) Ltd, Dulton Lane, Eastleigh, Hants. SO5 4AA

#### PANEL MOUNTED CASES

A new range of panel mounted cases which are ideal for housing projects such as clocks, meters, counters etc., have just been introduced by Perancea Ltd.

The black ABS cases are supplied with two front panels, one is an anti-reflective filter for displays and the other is anodised aluminium for mounting controls. Other features include



p.c.b. guides and slots, matt black clip-on bezels and optional mounting clamps for wood or metal panels.

There are four sizes of cases available,  $96 \times 48$  mm and  $72 \times 36$  mm front panels in two lengths 120 mm and 75 mm.

These cases could also make excellent housings for our *Car Instrument Devices* if the l.e.d. mountings were altered.

Distributors for the cases include Watford Electronics, Home Radio and Bi-Pak all of whom advertise in the magazine.

#### EPI

The 1978 edition of the Electronic Projects Index is now available. This index covers all the constructional projects published in sixteen magazines including PE, radio, television, hi-fi and computing. The projects are arranged under thirty six headings arranged alphabetically from aerials to Zener testers.

Other information given with each article includes a component guide and method of construction used, i.e. p.c.b., Veroboard etc.

The index is priced at £1.30 including p&p, and is available from M.L. Scaife, Central Library, Northumberland Square, North Shields, Tyne & Wear, NE30 1QU.



#### **ELECTRONICS 79**

The Electronics 79 Show was held this year at Olympia and many of the leading UK component manufacturers and distributors were exhibiting there together with equipment, instrumentation and packaging companies.

#### VIEWDATA

The latest Viewdata adaptor from Labgear, the 7050 Viewdapta, was on display. This is a compact unit for receiving Viewdata which can be used with an existing TV set without modification to the receiver.



The 7050 consists of a desk top keyboard and a wall mounted Viewdata Processing Unit which are connected together via a multiway cable. A built in loudspeaker gives an audible indication of engaged, dialling and other tones obtained.

#### **TRIACS AND THYRISTORS**

Motorola were showing their range of 15 to 40A triacs which they have now fitted into a TO-3 base type package with push-on terminals.

These 200 to 800V triacs are primarily designed for full-wave control to a.c. loads and are electrically isolated from the mounting base with a high isolation voltage of 2500V. Applications include appliance controls, power supplies, solid-state relays, heating and motor controls.



Motorola were also displaying their 8A MCR 72 thyristor which needs just  $30\mu A$  to trigger on and can easily be directly coupled with an MPU or other driver i.c. for power control applications.

#### **CIRCUIT TESTER**

Among the many instruments on display Vero Systems had their "Soundout" touch sensitive cable continuity tester on display which uses the body as a conductor leaving both hands free of probes.

The unit which is battery operated (9V) has a dual input impedance  $(15M\Omega \text{ and } 2.5k\Omega)$ and is available in two versions with the MK II model having the additional feature of an earphone for noisy environments or where more than one unit is in use.



Both units have a volume control and are supplied with an interchangeable crocodile lead. A wrist strap and probe lead are available as accessories. The price of the MK I is £20.00 and the MK II is £24.00.

#### **ZIP SOCKETS**

With the high cost of LS1 circuits many constructors are now using zero insertion pressure sockets to prevent pin damage to components whilst they are being inserted.

The BFI range of ZIP sockets included several new types never exhibited before. The socket range is one of the most comprehensive currently available and may be used for almost any device, including multi-pin integrated circuits axial lead components, power transistors and non-standard hybrid circuits.



Of particular interest is a new range of sockets for use with LSI devices in test equipment or development "breadboards". The sockets will accept 28 ( $0.4^{"}$  pitch), 42 and 64 pin devices with no insertion pressure, thus eliminating the lead damage and distortion which can occur when leads are forced into spring contact sockets.

Each socket has a lever at one end which is connected to an internal cam. The device is simply dropped into the socket and the lever flicked up to positively clamp the leads inside the socket. This protects the leads from damage and ensures a good electrical connection. When the lever is released the device may be removed without force.

#### **PLASMA PANELS**

Included in the Thompson-CSF display was their TH 7604 plasma-panel module which is intended for low-capacity alphanumeric-display applications.

This module which includes all the necessary panel-drive electronics has a power consumption of less than 30W. Being a.c. driven, the panel itself features inherent storage which means that the high-intensity display is also free of flicker,



The module's overall dimensions are  $295 \times 125 \times 57$  mm. Its useful panel area (219 x 52mm) permits displaying up to 6 lines of 40 characters (5 by 7), with the possibility of adding underlining or a mobile cursor.

#### BREADBOARD KIT

The latest kit from the CSC is the protoboard PB-203AK. This kit, featured in a special pre-release offer in PE (Nov. 79), contains all the components needed to make a solderless breadboard unit with three regulated d.c. power supplies.

The kit comes complete with all the elec-



tronic components, case and breadboard modules, as well as nuts, bolts, connecting wire and solder. The assembly instructions have been written without any assumptions about the constructor's past experience.

The finished Proto-Board incorporates three large breadboards plus four long busbars and one shorter one, giving a constructional area sufficient for 24 integrated circuits in 14pin packages. In addition, terminal posts allow connection to earth and to the +5V, 1A and  $\pm 15V$ , 0.5A power supplies. The power supplies are independent and fully regulated, and the  $\pm 15V$  supplies can be internally adjusted over the range 7–18V. The three power-supply rails allow the board to be used with most types of circuitry, including TTL and CMOS logic.

The PB-203AK is supplied with an earthed metal case measuring  $248 \times 168 \times 83$ mm, and is still available for a short period at a special offer price of £55.00 excluding VAT and p&p.

# Penfold

LTHOUGH compact cassettes have certain advantages A over other forms of recording medium, they have the major disadvantage of a comparatively poor signal-to-noise ratio unless they are used in conjunction with some form of noise reduction system. Many pre-recorded cassettes are encoded using the Dolby system and are capable of excellent results, but there are still numerous pre-recorded cassettes currently available that are non-Dolby as are many cassettes purchased some time ago.

The dynamic noise limiter (DNL) which forms the subject of this article was designed for use with a high quality cassette deck to enable an improved signal-to-noise ratio to be obtained when playing non-Dolby cassettes. Of course, the unit can also be employed with a cassette deck which



does not incorporate any form of noise reduction circuitry when playing any cassette. It can also be used in addition to some other form of noise reduction system to further increase the dynamic range. This can effect a very worthwhile improvement when the original recording is fairly old, and a significant amount of tape hiss has been recorded onto the cassette. It is even possible to use the unit to improve noisy f.m. radio reception, or any other programme source that is affected by low level high frequency noise.

#### **DNL PRINCIPLE**

Tape noise consists mainly of high frequencies, or to be more accurate, it is this high frequency content that tends to be most noticeable and objectionable. Turning back the treble control while playing a cassette will show this guite clearly by apparently greatly reducing the noise. It is by reducing the upper frequency response during playback that a DNL effects a reduction in tape noise, but it only applies the full amount of treble cut at low signal levels. It is then that the noise is most noticeable.

At high signal levels the treble cut is removed to some degree, and at very high signal levels it is totally eliminated. The increased tape noise will not be audible as it will be masked by the main signal.

In this way a DNL provides a very significant reduction in background noise, but there is a minimum loss of treble response.

100n

TR3 BC109C

R13

2 k 2

100n

TR4 BC 109C

R10

R15

TR2

VR2

R9 5k6

R10 1N4148

C5

VR1

C 10

OUTPUT

The DNL described in this article operates in the manner shown in the block diagram of Fig. 1. The input signal is split into two parts which are then mixed in a simple passive mixer circuit. One part of the signal is simply inverted before being fed to the mixer, and the other part is fed to the mixer via a high pass filter and a voltage controlled attenuator. The high pass filter rolls off signals below about 4kHz.

The two signals at the mixer are out of phase and therefore tend to cancel one another out. However, as only high frequencies are present at one input, it is only these high frequencies that are attenuated to a significant extent. Under quiescent conditions the VCA is adjusted to balance the two inputs and so optimise the high frequency cut. The output of the mixer is coupled to a low gain amplifier which compensates for circuit losses and provides the unit with almost exactly unity voltage gain.

Some of the output from the high pass filter is used to generate a control voltage for the VCA. An active rectifier and smoothing network are used to provide this voltage. Under low signal conditions only a very small voltage will be generated, and this will not greatly affect the circuit. Higher signal conditions will produce a large enough voltage to significantly attenuate the signal through the VCA. The higher the signal level, the great the attenuation.

If the output from the VCA is reduced, the high frequency cancelling effect on the signal from the inverter will also be reduced, and so the higher the input signal level, the less the amount of treble cut that the circuit applies. Thus the desired circuit action is provided.

The reason the active rectifier stage is fed from the high pass filter rather than the main input is that high frequency signals mask the tape noise far better than low or middle frequencies do. The unit is therefore designed to respond more readily to high frequency input signals.

#### **CIRCUIT DESCRIPTION**

The circuit diagram for one channel of the DNL is shown in Fig. 2. TR1 is used as a conventional high pass filter of the type often encountered in rumble filters, but the component values have been modified to provide a much higher cut off frequency of course. TR1 is connected in the emitter follower mode and so the filter has approximately unity voltage gain at pass frequencies.

The VCA is formed by R9 and TR2, the latter being a JUGFET which is used here as a voltage controlled resistance. TR3 is used as the inverting amplifier and this is a common emitter stage. As the emitter resistor (R13) is not bypassed and is equal in value to the collector load resistor (R11), this stage has almost unity voltage gain. R12 and R14 form a simple passive mixer circuit and TR4 is used as the output amplifier. TR4 only needs a voltage gain of a little



#### COMPONENTS ....

lesistors	
*B1	1k5
*R2	27k
*R3	33k
*R4	4k7
*R5	33k
*R6	220
*R7	68k
*R8	10k
*R9	5k6
*R10	1M5
*R11	2k2
*R12	33k
*R13	2k2
*R14	2 <b>2</b> k
*R15	4k7
*R16	1M8
*R17	2k2
Allegainte	TO 114/ EQ/ 1100/ auge 1

Il resistors 4W 5% (10% over 1M)

#### **Potentiometers**

VR1	47k hor preset	
VR2	1M hor preset	

#### Capacitors

*C1	15n
*C2	10n
*C3	100n
*C4	100n
*C5	100n
*C6	100n
*C7	100n
*C8	100n
*C9	10µ 16V elect
*C10	150n
C11	680µ 25V elect
C12	100µ 16V elect
C13	100n

All capacitors C280 type except where otherwise stated

#### Semiconductors

+IC1	CA3140T
IC2	78L12
*TR1	BC109C
*TR2	BF2448
*TR3	BC109C
*TR4	BC109C
*D1	1N4148
D2	1N4001
D3	1N4001

#### Switches

T1

51	Roc	ker	switch	d.p.	s.t
	-				

Rocker switch d.p.d.t.

#### Transformer

Mains primary, 12-0-12V 50mA secondary, miniature type with flying leads (M.E.S.)

#### **Miscellaneous**

BEC case type GB1a or similar Four phono sockets Miniature panel neon n.c.b.

Indicates that two devices are required for stereo operation



Fig. 3. Frequency response (low level inputs)

more than two in order to make good the losses in the circuit, and so again an unbypassed emitter resistor is used to introduce negative feedback and set the voltage gain of the stage at the required level.

IC1 is used as a form of active rectifier, and its voltage gain is controlled by feedback potentiometer VR1. This enables the input signal level required in order to remove the treble cut to be varied over a considerable range so that the unit is suitable for use with any normal cassette deck.

VR2 enables the bias on TR2 gate to be adjusted and this control is set to slightly reverse bias TR2 so that there is only a small amount of attenuation through the VCA under quiescent conditions, and the two inputs to the mixer are precisely balanced. Only positive going output signals are produced from the active rectifier in the presence of a suitable input, and these have the effect of raising the voltage at the lower end of VR2 and removing the reverse bias from TR2. This increases the attenuation through the VCA and removes the treble cut.

C5 integrates the output pulses from the rectifier in order to prevent significant distortion, but the attack and decay times are both short so that the circuit quickly responds to changes in dynamic level. As is normal for this type of device, the circuit has hysteresis. This simply means that the attack time is faster than the decay time, which helps the unit to act as fast as possible without generating significant distortion.

The hysteresis is produced by D1 and R8. C5 is charged through the relatively low impedance of R8, but it cannot discharge through the same path since D1 prevents this. Instead it must discharge into the relatively high impedance of R7. This is the only reason for including D1 in the circuit since the CA3140 used in the IC1 position is only operated from a single supply rail, and will provide a rectifier action without D1.

With a high level input the frequency response of the unit is virtually flat over the audio spectrum, but on low level in-



**Fig. 4 a & b. Switching alternatives** 

puts the frequency response of Fig. 3 is obtained on the prototype. The attenuation rate is about 12dB per octave from 3.5kHz to 8kHz. There is a slight peak in the response at approximately 3kHz and the roll off rate above 8kHz is only very gradual, but neither of these points are of any real consequence in practice.

#### P.S.U. AND SWITCHING

The filter is powered from a simple stabilised mains p.s.u. This is quite straight forward and consists of a push pull rectifier and smoothing network feeding a monolithic regulator i.c. A well smoothed and regulated output is provided, and the regulator i.c. has output current limiting and thermal overload protection circuitry.

In most cases it will be desirable to have some means of switching the unit out of circuit so that the cassette deck can be used normally. Some amplifiers and receivers have built in switching in the form of a tape monitor facility, or something of this nature, which could be used to accomplish this. An alternative is to use the simple in/out switching arrangement used on the prototype and shown in the circuit of Fig. 4a. This leaves the filter input permanently connected to the cassette deck output, but this does not seem to affect performance even if the cassette deck is used while the filter is switched off.

If preferred, the system shown in Fig. 4b can be used. Here the filter is switched completely out of circuit when the



#### Internal view

switch is in the "out" position, but a four pole switch is required. It would be possible to gang the on/off and in/out switches, but if this is done care must be taken to ensure that mains hum is not picked up in the in/out switch wiring. Also, care must be taken to ensure that the mains wiring cannot accidentally come into contact with the input or output wiring!

#### CONSTRUCTION

The prototype unit was housed in a BEC cabinet but any case of mainly metal construction and having similar dimensions (230  $\times$  150  $\times$  50mm) should also be suitable. The filters and power supply are constructed on two separate p.c.b.s and these are shown in Figs. 5 to 8 respectively. The negative supply rail connection between the two panels is carried via the mounting bolts and the metal case. The earth connections between the filter p.c.b. and the input and output sockets is obtained in the same manner. The filter and p.s.u. boards should be mounted as far apart as possible.

#### **ADJUSTMENT AND USE**

In use the filter is either connected between the cassette deck output and the "tape" input of the amplifier, or it is



Fig. 5. P.c.b. design for the main board

Fig. 6. Component layout



EG 277



EG275

connected into the tape monitor or some similar facility. In either case both the input and output leads should be proper screened types.

Initially VR2 is adjusted in an almost fully clockwise direction and a blank cassette is played through the system to provide a source of tape noise. If VR2 is now adjusted in an anti-clockwise direction a point should be reached where there is a slight but noticeable null in the noise, with further adjustment causing a rise in the pitch and intensity of the

noise. The correct setting for VR2 is at this null point and both channels are adjusted in this way.

The best setting for VR1 can be found by trial and error. The further it is adjusted in a clockwise direction, the lower the input signal level at which the treble cut starts to be lifted. It should therefore be adjusted as far in a clockwise direction as possible without the lifting of the treble cut becoming audible on low level signals.



The hardware and software exchange point for PE computer projects

delighted with it, although it has its limitations (one small annoying one being the lack of PRINT USING).

I find that I am learning BASIC by using the computer (hit and miss), and am following your article on learning BASIC.

However, as far as my programming is concerned, one or two things have so far eluded me, and I hope that you or your staff can help.

(a) What are the POKE commands to switch to printer, and to VDU, when writing programs in BASIC.

(b) Having written and loaded a program which has variables giving running totals, how can I load and save these updated programs? (I have a feeling that machine code, POKE, or something of the like is involved but what?) (I have already worked out that to run these programs, RUN sets the variables to 0, and I have to use GOTO to run them without clearing the variables. The books on BASIC I have do not mention these things, which for a real beginner are a nightmare).

> Iain Corrance Glasgow

Ideally, to carry data over, and update it at will, a cassette file should be generated so that the operating program is recorded on one tape and a data file on another. Alas, the 101 does not have cassette file firmware, but we have been told it can be done using machine code routines which of course can be accessed from BASIC via USR(I). An alternative, if somewhat clumsy, is to list as DATA statements those variables you wish to maintain, before re-recording the program.

We shall endeavour to answer all questions in due course. Next month we will be publishing a game for the 101 called "Torpedo Run", and give details of an independent UK101 users club.

Sir—Having recently built the Compukit 101 computer, I must say that I am

If you have ever built a computer, or

computer peripheral using plans from

the pages of PE, then it is likely that

you would have appreciated some

"follow up" data on such matters as in-

terfacing and software. Keep an eve on

this new column then, if you have con-

structed Champ, the UK101 or a

peripheral device such as our printer or

VDU; for it is from this column that we

hope hints and snippets of information,

short programs, applications and dis-

coveries will spring forth eternal

... with your help of course!



#### Shake-out

Whatever people may say of the electronics industry they can never accuse it of being dull. Change is always around. It is difficult enough to keep track of the technology, even harder to keep up with business fortunes, changing markets and who owns what, and how performance and expectations will be affected by the dynamic economic climate both at home and abroad.

How the tight monetary policy, stiffened even further by the mid-November increase in interest rates, will affect the electronics industry in the UK is still anyone's guess. So is the long-term effect of the abolition of foreign currency exchange after 40 years of restriction. And what happens in the USA affects the whole of the Western world. The dollar is unhealthy, and the USA is in another energy crisis as well as being unsettled by the run-up to the Presidential election.

Pity the poor managers and market analyists struggling with their five year business plans, so beloved and promoted by the business schools! There are so many variables in the equation in these turbulent days that it is practically impossible to formulate a coherent long term policy.

Confusion and an uncertain future, however, has not deterred people from having a go at seizing what they see as good business opportunities. Expect Racal to make further acquisitions soon. Action in this respect may also be anticipated from GEC and Thorn. Expect, too, to see more foreign investment in the UK during 1980. not excluding the Japanese. There is some timidity among overseas investors on labour relations problems in the UK but fortunately the record in the electronics industry is almost miraculously good. Apropos the Japanese, Toshiba alone already has manufacturing plants in seven countries outside Japan. This trend will continue.

#### **God and Virtue**

How do the Japanese do it? Have they some secret formula denied to the rest of the industrial world? There have been many attempts at analysis.

In two recent commentaries one suggests that the secret is that to a Japanese company and its employees the customer is regarded as God. Actually, not an attitude to be despised although strange for a country whose religious beliefs are principally in Buddhism which has no God and Shinto in which the object of veneration in the shrine may be anything from a stone to a household utensil in which resides the spirit.

The other preaches a virtuous circle of good industrial relations allowing management to get on full time with managing and innovation, coupled with lifetime jobs generating confidence in accepting new technology by employees instead of, as in the UK, resisting it.

In all the years of *Industry Notebook* I never imagined I should use such a heading as that above! Nonetheless, such abstract concepts are very real to the Japanese character with their singing of company songs before taking to their work benches, and their dedication to a cause as exemplified by the terrifying suicide attacks by Kamikaze pilots in World War 2.

#### Sting Ray

Marconi Space and Defence Systems have won their biggest ever contract in the Sting Ray project. More than £200 million in the first instance and probably worth £800 million over its lifetime of 20 years. Among the other heady statistics, 50,000 man years of work spread over a dozen cities (if you include the subcontractors) make good reading.

Sting Ray is a lightweight homing torpedo with an advanced on-board computer, a multi-mode, multi-beam sonar which detects and tracks the target while resisting false echoes and enemy countermeasures, and a quiet yet high speed propulsion system. Deliveries to the Royal Navy should start in the early 1980s and there are expectations of it being adopted by other NATO navies.

#### Energy

The energy crisis persists but it is now almost a way of life, the previously unthinkable £1 per gallon being now a matter of history. The Americans have a conservation policy well reflected in energy-saving campaigns in manufacuring plants strongly re-inforced by publicity in house journals. But are they taking it seriously? I had my doubts when I read in one house journal from an electronics company that temperature in the offices and factory was being maintained at a steady 78°F. Surely a misprint, but then I read that the company dress code had been relaxed to permit jackets off and ties loosened. Slowly the penny dropped. This was the Texas summer, not the UK winter. Their problem is cooling as well as heating. As much as 20

per cent is being saved by some companies by simple expedients and even further gains by the addition of MPU-controlled fine tuning of air conditioning.

#### Paradox

The EMI Scanner, according to the medical profession, was the greatest advance in medical diagnostics since the Röntgen's discovery of X-rays in 1895. Its creator, Godfrey N. Hounsfield, had engineering ambitions when he was a five year old tot, yet he was a late developer who didn't complete his formal engineering education until he was 30. But his most useful period of training, on his own admission, was self-tuition between the ages of 13 and 19—an encouragement to every hobbyist!

Few people could ever have received so many awards and honours for a single invention, culminating in a Nobel Prize and even more recently the 1979 Aachen and Munich Prize for Technology and Applied National Sciences. And he deserved every one of them as well as the gratitude of the sick.

What a fantastic success story for the man and, initially, for the product which up to the mid 70s was a jack-pot profit maker for EMI. Then came the big cut backs in procurement in the USA, then the biggest market, and an increasing flood of competitive equipment. As the honours poured in for Godfrey Hounsfield the debts poured in for EMI.

Bad organisation, bad management, bad luck? It is difficult to analyse, no single factor being responsible. Hounsfield's great technological achievement still stands, whatever the fortunes of his employer. All the same, one imagines he must be looking over the past five years with very mixed feelings.

A similar story, perhaps less dramatic is the scanning electron microscope, a worldbeater for Cambridge Instruments, a company now in the protective embrace of the National Enterprise Board but still losing millions on a good product. And older readers may remember the Britlsh company Perdio who bravely produced the first transistor portable radio in the world before going broke.

#### Does it pay?

Does it pay to be first in the field? There is much to be said for the "me-too" philosophy which, put crudely, means letting someone else bear the major development costs and carry the burden of breaking open the market, then moving in at the right moment saying "me-too". I recall Motorola, in its early and middle period in semiconductors, regarding Fairchild as the innovator, TI as the market developer and themselves as the "me-too" company with special skills in manufacturing coming in later with fast delivery and keen prices.

On the bid front Decca looks even more vulnerable. Thorn, at the time of writing, was still battling for EMI and GEC for Avery, their bid having been upped to a £98 million package.

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#### **DEATH OF A SATELLITE**

One of the most remarkable satellites launched in recent years is the United Kingdom, ARIEL V. It has enjoyed 5 years of great activity. When it was originally launched it was not expected that its operable life would be much more than a year because the propane fuel thrusters would run out of gas. This would deprive the control centre of means to "point" the satellite at suitable targets. The amount of data accumulated for the estimated period alone would have been a major contribution. In fact the satellite has been operational far beyond expectations. This has been due to the expertise developed by the team at the control centre, the Appleton Laboratory near Slough at Ditton Park.

Among other things this team developed a technique which enabled them to economise the gas use thereby adding years to the useful operation. This in itself was a magnificent contribution. Even when the gas was finally exhausted, use was made of the Earth's magnetic field to maintain some control. In all this the team have been very modest. This official statement of the record of this mission is extremely restrained:

"The success of Ariel V is twofold: Outstanding scientific observations have been made by Ariel V and have established the UK group at the forefront of X-ray Astronomy.

"The technical expertise and knowhow in the fields of satellite and data management which have been built up in the Control Centre at the Appleton Laboratory are second to none and invaluable for subsequent projects, and could be an important factor in the UK involvement in future international space programmes."

Ariel V was launched on the 15th of October 1974 to make observations of cosmic X-ray sources. With 5 years of observations completed it is clearly the most successful UK satellite to date, both operationally and scientifically. The spacecraft, designed and constructed for SRC by Marconi Space and Defence Systems, contains six scientific experiments provided by the Mullard Space Science Laboratory, of University College London, The University of Leicester, Imperial College, London and the Goddard Space Flight Centre of the US.

#### **TECHNICAL ACHIEVEMENTS**

The establishment of the Ariel V Control Centre at Slough in 1974 was the beginning of a major initiative in the area of satellite control and space data support as a complement to the established space project management. It is being further improved for support of the Infra-Red Astronomical Satellite (IRAS).

The staff responsible for the design of the Ariel V covered the following expertise. Electronics, real time software, data communications, celestial mechanics, operational research and large scale data processing. The electronics were needed for the building of the special computer interfaces and data display equipment; the real time software knowledge was needed for the satellite control and data reception; data communications skill was required for the setting up of links between Control Centre real time computers, the Laboratory mainframe computer, back-up computers and computers at four University sites. The celestial mechanics knowledge was required for the design of orbit prediction programmes, attitude computation and observation programmes; O.R. techniques were used to optimise the gas control, finally data base on a large scale was needed for preprocessing of the satellite data.

The Control Centre had two objectives:

1. To control the spacecraft and its experiments and, by monitoring the critical satellite sub-systems, keep the satellite in a safe and healthy state.

2. To interact rapidly with the astronomers.

#### FLEXIBILITY

Both these objects were achieved successfully. The second objective was however the most successful for it had a major impact on the programme. The key was the observing programme which was so flexible that astronomers were able to interact with the Control Centre and alter plans within an hour or so. The system operates as follows. The prime Ground Station for Ariel V is the NASA Ground station at Quito in South America. The satellite passes over Quito every 90 minutes. During a satellite pass commands are sent to the satellite and data received from it on-line in the Control Centre. As soon as the raw telemetry data are received they are checked and re-formatted. Orbit and Attitude computations are carried out and data tapes created for each experimenter. These preprocessed data are then transmitted by Post Office lines to Birmingham, Imperial College, Leicester and the Mullard Space Science Laboratory. Data will be received within 45 minutes of the satellite passing over Quito. Thus it is feasible for the experimeter to examine his on-line data and request a change in the observing programme in time for the next pass. This important feature was a basic requirement for the Control Centre because of

the nature of the experiments. Frequently one of the two scanning experiments would detect an X-ray source which was new. The versatility of the control would enable the satellite to be manouevred so that the four pointing experiments could examine this source in detail. The value of this facility is very great for the reason that many sources are transient and in a few hours could fall in brilliance below detectable level.

#### **MAGNETIC MANOEUVRES**

In the early days the attitude of the satellite was controlled by the propane gas jets at the base of the satellite. The gas was expected to last a year, in the event it was prolonged by nearly three years by the ingenuity of the control team. The gas finally ran out in June 1977. Since then attitude has been controlled by using a magnetic dipole cancellation system. This was of course not installed for that purpose but to prevent magnetic drift. In a sense it could be said that it was used in reverse. Since the satellite has an equatorial orbit it passes through the field lines of the earth's magnetic field. By passing a small current round the loop the earth's field was used to control the attitude of the satellite. The torques made available thus, were able to achieve manoeuvre rates of 10°/day in right ascension and 0.5°/day in declination.

The death of Ariel V is expected between the middle of January and February 1980.

#### THE EXPERIMENTS

Project Scientist: Professor A. P. Willmore, Department of Space Science, University of Birmingham.

A. University College London's Mullard Space Science Laboratory, Holmbury St. Mary, Dorking.

Measurement of X-ray source positions and sky survey in the energy range 0.3 to 30keV. This pointing experiment uses a rotation modulation collimator with proportional counters and channel electron multipliers as X-ray detectors, together with a collimated photomultiplier for optical star detection. **Principal Investigator:** Professor R. L. F. Boyd.

B. Physics Dept., University of Leicester, University Road, Leicester LE1 7RH. Sky survey in the energy range 1.5 to 20keV. This scanning experiment, which views from the side of the spacecraft, uses large proportional counters. Principal Investigator: Professor K. A. Pounds.

C. UCL Mullard Space Science Laboratory. Study of the spectra of individual sources in the 2 to 30keV range. This is a pointing experiment using a proportional counter. Principal Investigator: Professor R. L. F. Boyd.

D. Physics Dept., University of Leicester. Measurement of the polarisation of X-rays from 1.5 to 8keV. This pointing experiment will determine polarisation or line emission by means of a Bragg crystal spectrometer using moveable plane crystals. Principal Investigator: Professor K. A. Pounds.

## F. Physics Dept., Imperial College, London SW7.

The study of sources of high energy X-rays up to 2.0MeV. This pointing experiment uses an active collimator, a caesium iodide scintillator and photomultiplier detectors. It is designed to investigate the energy spectra and time variations of known sources and to measure the spectrum of the diffused cosmic X-ray background. **Principal Investigator:** Professor H. Elliot.

## G. Goddard Space Flight Centre, Greenbelt, Maryland, USA.

An all-sky monitor in the energy range 3 to 6keV. This survey experiment uses two pinhole sensors to detect transient effects in the X-ray sky enabling the other experiments to make the earliest possible measurements on these important phenomena. **Principal In**vestigator: Dr. S. S. Holt.

#### ARIEL 6

Ariel 6 which followed Ariel 5 has also a lifetime of about one year. It has not so far achieved full design operation because the control system has been subject to interference from both Russian and American radar systems. The effects are varied but one



#### THE MAGNETIC FIELD SATELLITE (MAGSAT)

MAGSAT is for the purpose of studying the movements of the Earth's crust and the location of mineral deposits. It is a polar orbiting satellite, and is designed to measure the Earth's near surface magnetic fields and indirectly crustal features related to earthquakes. During the life-span of this satellite which is 120 days it will measure the strength and trace the direction of both the global magnetic field and surface magnetic fields. The surface magnetic fields are caused by the electric currents effect of magnetic storms and by certain elements in the Earth's crust. For example one large magnetic surface anomaly is due to an iron deposit in Africa. This was detected by a satellite magnetometer. After making this survey it will be possible to make available maps of the Earth's surface showing the location of magnetic irregularities and a global magnetic field model.

Having completed the surface irregularities it will be possible to gain a better understanding of the evolution of the crust of the Earth and the various geological processes which have led to the formation of ore and petroleum deposits. This satellite possibility has only recently been understood when satellites, carrying magnetometers for the measurement of the global fields, mainly due to the Earth's core and working in low orbits showed anomalies which were localised.

It has been known for many years that some rock formations are better conductors of electricity than others and that these played a part in indicating where mineral and petroleum deposits could be found. What was a surprise was that satellite location was possible. The data produced by six satellites carrying magnetometers has led to this special satellite experiment. It is hoped also to shed more light on the reversing of the Earth's magnetic field over cycles of time. It is known now that the field suddenly collapses and slowly rises but in the opposite mode where north becomes south. The building up may take a longer time perhaps a thousand years. There are many consequences of such a happening. It could be responsible for sudden destruction of species of animals or other life.

The clues to drift of continents may help to anticipate earthquake events when the magnetic and gravitational anomalies are better understood. This project will involve most countries in the world over the next two years.



Organisers: Please send details of exhibitions, club open days and other events to Mike Abbott at least six weeks in advance. Inclusion will be subject to space etc.

#### BEX Feb. 20-21. Pavilion Bournemouth. K

IEA/Electrex Feb. 25-29. National Exhibition Centre, Birmingham. I Viewdata March 26-28. Wembley Conference Centre, London. O Computer-Alded Design (conference & exhibition) March 31-April 2.

Metropole, Brighton. Details: CAD 80/0483-31261

Seminex April 14-18. Dept. Physics, Imperial College, London. HI Communications 80 April 14-18. National Exhibition Centre. I Electronic Test & Measuring Information April 22-24. Wythenshaw Forum, Manchester. T

International Conference On The Electronic Office April 22-25. London Penta Hotel. Organised principally by the Institute of Electronics & Radio Engineers. 99 Gower St., London WC1E 6AZ

North Midlands Mobile Rally April 27. Drayton Manor Park, Tamworth, Staffs. Details: Norman Gutteridge, 68 Max Rd., Quinton, Birmingham.

All-Electronics Show April 29-May 1. Grosvenor House, London. E The Mersey Micro Show April 30-May 2. Adelphi Hotel, Liverpool. O Compec Europe May 6-8. Centre International Rogier, Brussels. L Great British Electronics Bazaar June 20-22. Alexandra Palace. E Intel Fair June 24. Wembley Conference Centre, London. U.

Tempcon July 1-3. Wembley Conference Centre. Exhibition devoted to temperature control & measurement. T

Transducer July 1-3. Wembley Conference Centre. T

Microsoftware (symposium) July 7-10. University of Sussex. S1 The 1980 Microcomputer Show July 10-12. Royal Lancaster Hotel, London. O

Avionics (symposium) Sept. University of Surrey. SI

Harrogate International Festival of Sound Aug. 16-19 (18 & 19 trade). The Exhibition Centre + hotels. X

- E Evan Steadman, 34-36 High st., Saffron Walden, Essex. © 0799 22612
- HI Seminex Ltd., 79 High st., Tunbridge Wells, Kent. TNI 1XZ. 6 0892 39664/5
- I Industrial Trade Fairs, Radcliffe Ho., Blenheim Court, Solihull, W. Midlands B91 2BG. & 021-705 6707
- K Douglas Temple Studios, 1046 Old Christchurch Rd., Bournemouth, Dorset BH1 1LR. & 020 20533
- L Iliffe Promotion, Dorset Ho., Stamford St., London SE1 9LU. & 01-261 8437/8
- Online Conferences, Cleveland Rd., Uxbridge, Middx. UB8 2DD.

   <sup>0</sup> 0895 39262
- T Trident International Exhibition, Abbey Mead Ho., 23a Plymouth Rd., Tavistock. Devon PL19 8AU. & 0822 4671
- U Brian Crank Associates, 58 London Rd., Southborough, Kent. & 0892-31812 38414
- X Exhibition & Conference Services, Claremont Ho., Victoria Ave., Harrogate, Yorks. & 0423-62677
- SI Society of Electronic & Radio Technicians, 57-61 Newington Causeway, London SE1 6BL. & 01-403 2351



#### SEASIDE COMPUTER CLUB

A COMPUTER club in the Bournemouth area has successfully taken off, the first meeting of which was held at the Poole Arts Centre on October 28th last year.

The response was very good and the club looked all set to form a committee. A second meeting was organised for November 30th at Kinson Community centre, where it was expected that a representative from Tandy would demonstrate some equipment.

Details from Robin Pink, 10 Harbour View Road, Poole, Dorset.

# Semiconductor UPDATE FLATURING ZN419CE 87C48 MCM68732 R.W. Coles

#### **MODEL CIRCUIT**

If you are interested in the radio control of model 'planes, ships, cars or robots, then you will be very pleased with the Ferranti ZN419CE device because it could save you money on servos. For the uninitiated, servos are used in radio control models to position control surfaces and other mechanisms. Their great advantage over the now rather outdated "on-off" escapement actuator is that they provide a proportional control action which is not ierky.

The R/C modeller controls his creation by adjusting a joystick potentiomenter which causes the transmitter to send out a pulse width modulated signal where the width of pulses is proportional to the deflection of the control. If more than one control function is required, then the associated pulse width signals are time multiplexed and sent to the model in a repeating sequence.

At the receiver the separate channel signals are recovered by demultiplexing, and it is the function of the servo to respond to the changing width of individual channel pulses by producing at its output an angular change proportional to the joystick deflection at the transmitter. The servo output is linked to control surfaces or engine controls, with the result that the model responds in a smooth, proportional manner to every new control setting selected by the modeller.

The clever bit, as if you hadn't guessed, is turning those variable width pulse signals into a proportional mechanical movement, and that is where the Ferranti ZN419CE comes in. The motive power for the servo is usually provided by a small d.c. motor linked via gearing to the output shaft or lever, and to a variable potentiometer which rotates in synchronism with the servo output. The pot is there to provide information on the present servo output setting, and the pulse signal is there to tell the servo system what new setting is required. Inside the ZN419CE there is a monostable which has to be connected to the servo-pot so that the monostable pulse width is proportional to the pot position. A pulse comparator in the chip compares the monostable pulse width with the received pulse width for the channel, and the result is an error pulse which is stretched and used to turn on one of a pair of external p.n.p. drive transistors which control the motor current.

The motor turns to drive the servo pot (and of course the servo output shaft) until the monostable pulse width is equal to the received pulse width, whereupon the motor stops.

A great deal of "electrickery" is necessary to produce a practical servo decoder and driver, but fortunately you can get most of it in the 14 pin package of the ZN419CE.

Complete servo modules are already available for R/C modellers of course, but by using the ZN419CE in a home-built servo it should be possible to save money. It would also be possible to use this device in "special" servos, just what you need, perhaps, for that towering microprocessor based robot you've been working on in the garage!

#### **CMOS SINGLE CHIPPER**

Intel were one of the first in the field with a true single-chip microprocessor CPU, RAM and ROM all in a single 40 pin package. Their original 8048 and 8748 devices have now been joined by a whole family of similar devices such as the 8021, 8022, 8035, 8039, 8041 and 8741 featuring various combinations of memory and input/output lines.

Most of these devices are of little interest to hobbyists because they utilise maskprogrammed ROM to hold their programs, but those with a "7" as their second digit are useful, even for one-off projects, because they employ program memory of the erasable and reprogrammable (EPROM) variety.

The 8748 for example, although intended as a prototyping aid for the pin compatible 8048, can be very useful where the small size of a single chip system is desirable. It contains within its 40 pin package a digital processor system complete with 1K of EPROM, 64 bytes of RAM a programmable counter/timer and no less than 27 lines of I/O.

Hats off to Intel then for a useful workhorse, but it is not the 8748 I want to tell you about because it isn't really new. The 87C48, however, is very new and it comes from Intersil, the CMOS wizards of Cupertino, California. It seems that Intersil have an agreement to second source the highly successful Intel device, but although identical to the 8748 in most respects, the 87C48 adds that magic ingredient, CMOS technology, to make a good thing even better. It runs from a 5 volt supply, just like the NMOS 8048 but the Intersil device consumes a maximum of 50mW against well over 300 mW for the Intel part at the same 6Mhz clock frequency.

Rumour has it that the 87C48 will actually cost less than the 8748 when it starts to appear on stockists shelves early in 1980, a fact which could make it very attractive for battery powered hobby projects. One problem though, the 87C48 uses a different EPROM technology to that of its Intel cousin and cannot therefore be programmed by using a standard 2716 programmer and a pin-out adapter. Putting together a special programmer circuit may prove to be well worth the effort, however!

#### HALF A LOAF

Talking of EPROMs, you may already know about the current world shortage of devices such as the 2716, an effect which has apparently been caused by the popularity of 5 volt EPROM technology in general, combined with a long delay before the appearance of alternative sources to challenge Intel.

Some second sources have appeared however, notably Texas Instruments, closely followed by a collection of Japanese manufacturers, but now Motorola have made a surprise entry into the fray by introducing not just another second source for the 2716, but a brand new device with four times the capacity, the MCM68764. This monster 8K x 8 EPROM has leapfrogged the biggest Intel device, the 4K x 8 2732, and will surely carve out a useful niche for its canny manufacturer—you could get a fair sized BASIC interpreter into a single MCM687641

Making a device with no less than 65,536 separate bits to go wrong is quite a challenge but Motorola obviously hope to achieve useful yields. Those devices that do get rejected may not be wasted however, because Motorola have also announced the MCM68732 which is, surprise surprise, half of an MCM 68764!

They don't saw an MCM 68764 down the middle, they just use a reject device where one complete half of the memory is still fully serviceable. The new '32 comes in two versions, -1 or -0, where the suffix indicates whether the most significant address bit (pin 21) should be tied permanently high or low. This technique is becoming more widespread as memories grow in size, and Intel themselves already sell "partial" versions of some of their memory parts, particularly 16K dynamic RAMs.

Half a loaf is better than none seems to be a fitting motto for tomorrow's memory makersl

IN the workshop probably the least cared for tool is the soldering iron, excessive temperature of which can ruin present day CMOS devices and f.e.t.s. This article describes a highly sensitive and responsive unit for controlling the tip temperature of soldering irons. The unit can also be used for other appliances like a colour developer bath etc., where a very accurate temperature within the range of  $\pm 0.5$ °C is required to be maintained, by a single adjustment.

In the ordinary solid state heat control systems, power to the element is usually delivered through a triac. At the preset temperature level the triac is switched off. Power to the element is switched on with the differential drop of the controller which is in the order of  $\pm 2^{\circ}$  to  $\pm 5^{\circ}$ C. Such 'on-off' control produces large overshoots and undershoots and therefore the heat regulation is coarse.

For more accurate control, power is delivered to the element continuously. Only the duty cycle of the power is varied to achieve the maintaining level. The variation of duty cycle or the pulse width, controls the temperature. Such a method is termed as proportional heat control system as it draws the energy in proportion to the requirement. The temperature control characteristics of the above two systems are shown in Fig. 1.

#### SCHEMATIC

A block schematic of the proportional heat control unit is shown in Fig. 2. A1 is an integrator, which integrates any error signal developed due to the difference in sensor diode drop and set reference. The resulting integrated voltage change on biasing resistance R regulates the charging current to capacitor C of the square wave generator A2. The charging and discharging of C determines the output pulse width of A2. The regulated pulse width in turn controls the duty cycle of the firing of the triac correcting the sensor temperature and returning the sensor voltage to that of reference. As the sensor temperature is gradually corrected, the pulse width of A2 also changes due to decreasing error. At equilibrium, the pulse width stays at the maintaining level, when the error signal is zero. Maintainance of the constant temperature is possible only due to the holding feature of integrater A1. When the integrator input error signal is at zero level, the integrator output holds at existing level, this in turn holds the controller output pulse width. The resultant input and control curves are shown in Fig. 3.



M.S. DHINGRA

SALDERING IRAN



#### CIRCUIT

The circuit diagram of the system is shown in Fig. 4. General purpose 741 operational amplifiers are used for the integrator as well as multivibrator.

The split supply to the system is  $\pm 5.6$  volt derived from a centre tapped transformer T1 and regulated by Zener diodes D3 and D4. Capacitors C1 to C4 serve for storage and to supply ripple free current.

Two 6 volt batteries can also be used. Silicon diode (D5's) negative temperature coefficient characteristics has been used for the sensor. For this purpose the author used a diode type 1N914, however silicon *n.p.n.* transistors like BC107 etc., with the base and collector tied, can also be used with the same accuracy.

Current to the sensor diode is limited within 1 to 5 mA by resistance R3.





Fig. 2. Block diagram

The sensors output is fed to the inverting input at pin 2 of integrator IC1, through a resistor R8. The reference signal is generated by a  $2 \cdot 2$  volt Zener diode D6 and this reference potential is divided by the chain VR1, VR2, R6, and R5. While VR1 is the calibration preset, VR2 is the control potentiometer.

The potential at the wiper of VR2 is fed to the noninverting input at pin 3 of integrator IC1 through a resistor R7. C5 is the integrating capacitor. Its value in combination with R8 defines the rate of charge.

Integrator output at pin 6 is fed to C6 of the multivibrator formed around IC2, through resistor R9. The potential here regulates the charging current of C6 and therefore the output pulse width at pin 6 of the multivibrator IC2.

The frequency of the multivibrator is defined by the value of R12, which is about 70Hz with the values used. The ratio of R11 to R10 defines the maximum mark-to-space ratio, that is the maximum conduction period for the triac during one cycle of the multivibrator.

The pulse width controlled output at pin 6 of IC2 swings between the positive and negative supply lines and rectified by diode D7 to give positive pulses for triac firing. These are fed to the gate of the triac through current limiting resistor R13. The triac remains on during the entire positive gate pulse period providing a supply to the soldering iron.

#### ASSEMBLY

1

The p.c.b. of the control unit is shown in Fig. 5 and the component placement in Fig. 6. Fix the components in place with due care for polarities. The assembled p.c.b., supply transformer, triac and the three pin socket outlet should be mounted in a suitable metal box.

Mount the triac on a heatsink, well insulated from the



rig. o. control graphs

metal cover. Fix the control pot VR1 on the front of the cover, with a knob graduated evenly to read 200° to 300°C for its full variation.

Clamp the sensor diode onto the metal body of the soldering iron, near the insulated handle grip, well away from the tip. This is because silicon diodes operation is limited to 150°C. Further, for a 100°C variation of tip temperature from 300° to 200°C, a variation of 10°C from 145° to 135°C is present at the location indicated, making it the best place for monitoring the tip temperature. Connect the sensor leads with the control unit by means of a screened shielded cable, caring for the proper polarity of the diode.

#### CALIBRATION

Before energising the unit, check once again that all connections are made properly. Now switch on the supply to the unit, without a soldering iron at the socket outlet and measure across Zener diodes D3, D4 and D6 that the voltages are +5.6, -5.6 and +2.2 volts with respect to common point. Also check the functioning of free-running multivibrator by a multimeter set to the range 10 volts d.c.



Fig. 4. Circuit diagram





COMPONENTS		
Resistors R1, R2 R3 R4 R5 R6 R7, R8 R9, R11 R10 R12 R13	560 1W 3k9 1k 2k 2% 51 2% 220k 10M 1M 2M2 150	
<b>Capacitors</b> C1, C2 C3, C4 C5 C6	250μ elect 1,000μ elect 100n polyester 1μ polyester	
Semiconductor D1, D2, D7 D3, D4 D6 IC1–IC2 D5 CSR1	8 1N4001 BZX85-5-6 1 - 3W Zener BZY88-5-6 400mW Zener 741 1N914 C206D 400V/3A triac	
Potentiometers VR1 VR2	10k 100 linear	
Transformer T1	230V pri.—9–0–9∨, 400mA sec	
S1	Double pole mains on/off, FS1-2A fuse, LP1-mains neon	

Fig. 5. P.c.b. layout of controller

Fig. 6. Component layout and external wiring

between pin<sup>,</sup> 6 of 1C2 and neutral, oscillations should be observed.

Now, energise the soldering iron from a normal supply source, not through the unit, and let it heat for about thirty minutes, to get the iron's temperature and in turn the sensor's output stabilised. Keep pot VR1 set to maximum resistance and turn the control potentiometer anticlockwise, i.e. at 200°C mark. Connect a multimeter set to the 10 volt d.c. range between pin 6 of IC1 and common point.

The voltage indicated will be zero. Now slowly reduce the resistance of VR1 until the meter needle remains at about 5V. Slow needle movement is due to integrator action.

Now turn VR2 to its other extreme (300°C), and the meter needle will swing back to zero value.

With careful setting of VR1, arrange that the transition of the meter deflection from 0 to 5 volt commences at exactly mid position of the control pot VR2, i.e. at 250°C mark. You will be able to achieve this state in two to three steps. Now plug in the soldering iron at the socket outlet of the control unit and temperature control is yours.



# NEXT

# CAR-RADIO...

A five push button long and medium waveband car radio for under £11. This design employs an excellent tuner head with a ceramic i.f. module and 6W i.c. output stage to give exceptional performance for price. Our article will give full constructional details.

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# ELECTRONICS

OUR MARCH ISSUE WILL BE ON SALE FRIDAY 8 FEBRUARY 1980

CUSTOM designed integration may be every designers dream, but it is the financial planners nightmare, for with every i.c. needing its own individual mask the cost is enormous and must be borne by the buyer. Therefore, custom designed integration is usually confined to applications involving large volume production, and is impractical for smaller low cost projects.

Universal logic elements endeavour to maintain the advantage of custom circuits while reducing some of their disadvantage. They are produced as standard devices designed to fit user application with little modification required, this consisting of custom design for the metallisation mask used on a standard logic array. Such universal logic elements appear in the ROM, PLA (programmable logic array) and ULA (uncommitted logic array) and it is this which will be looked at.

#### THE MLA GESCALGED

As the name implies, the ULA consists of a single chip containing an array of uncommitted gates or cells in which the silicon wafers are processed up to the stage just before the final metallisation and then stored. Each cell is separate and all that is required is a mask for an interconnection pattern, this being designed for the users specific circuit requirements. As the individual component in each cell can be readily interconnected, a combination of linear and digital circuits can be produced.

The success of the ULA is due to Ferranti who developed the CDI (collector diffusion isolation) process. A feature of CDI which gives it its facility is that the bulk semiconductor material used within the i.c. can be used for supply and ground return currents. This process greatly assists the manufacture of ULAs as all power rails are removed from the top interconnection plane, enabling the interconnection pattern to be devoted to purely programming the cells.

#### CHEMATIC

A schematic diagram of the CDI process is shown in Fig. 1.

The low resistivity of the collector isolation diffusion allows supply connections to be made without metal, and earth connections can be made direct as the epitaxial p layer is on a p type substrate.



Fig. 2. Basic uncommitted cell

# E.FRY B.Sc.

Committed logic Arra




Fig. 6(a). Input interfacing (b) Output interfacing

The basic uncommitted cell (Fig. 2) consists of three transistors and four resistors, thus providing the usual RTL logic. Though each individual component can be connected as required, the most common cell connection to be found in the array is shown in Fig. 3. This is called the basic gate cell. It is a positive NOR gate, giving great versatility as a basic building block. Fig. 4 shows the truth for this gate. How these gates can be used as complete circuit functions will be shown later.

### **INCREASING FAN IN**

An example of inter-cell connecting can be seen when designing for a higher fan-in, as in Fig. 5, where components from two cells are used to increase the fan-in to five. This technique termed 'collector ORing' can be used to increase the fan-in up to a maximum of ten. The remaining transistor and two resistors can be used in some later stage.

Owing to the cell being uncommitted, interfacing can be achieved directly for most types of logic and circuitry. In Fig. 6 we see how interfacing is done by using components from one cell. As the maximum input current for the interface gate is in the order of 40µA, it allows several gates to be driven from any of the typical logic families. For example TTL will drive up to ten ULA interface gates, CMOS, ten also. DTL up to six, etc. Output interfacing is capable of driving much lower numbers though, such as TTL—three gates. This can be increased by paralleling the interface gates, thus three ULA gates will drive nine TTL gates.

ULA is also capable of driving directly I.e.d.s, and discrete transistors, etc, and in such a mode of operation a total of 10mA drive current is available.

# APPLICATIONS

The basic uncommitted cell can be connected to provide a large variety of linear and digital circuits. A few of the many ways in which the basic ULA can be used as building blocks are shown in Figs. 7 to 10.



Fig. 7. Operational amplifier, using 13 components from three cells



Fig. 8. Basic oscillator, using ten components from two cells and external timing R/C network



Fig. 9. Analogue voltage comparator using 17 components from four cells



Fig. 10. D type flip-flop using all components from 6 cells

An example of how an entire array may be committed to perform a set function is shown in Fig. 11. An automatic control for an item of photographic equipment, containing all the necessary logic in one 28 pin i.c. package. It utilises approx. 140 of the cells, and replaces an equivalent 20 packages of MSI.



Fig. 11. A photographic control system using ULA

To summarise then—ULA, because of low cost and quick availability is ideal for smaller projects, and as an evaluation vehicle. It saves space and assembly costs. Both reliability and performance are greatly improved; basically everything that custom designed integration offers, but cheaper and faster.



# TELECOMMUNICATIONS SYSTEMS FOR TECHNICIANS 1 by Walker & Danielson Published by Newnes-Butterworths 103 pages. Price £2.95

**PRIMARILY** intended for TEC (Technician Education Council) level students taking courses in electronics. telecommunications and marine radio, this volume should prove popular to a wide readership as it covers a wide range of subjects at elementary level; information transmission, radio, radar, radio navigation. telephony. telegraphy, routing and data communication.

The text is well illustrated by over 180 diagrams and where applicable, BS symbols are maintained throughout.

To check recall simple revision exercises terminate each chapter.

# SEMICONDUCTOR TECHNOLOGY Edited by G. W. A. Dummer Published by Pergamon Press 203 pages. Price £20

T HIS is a collection of papers read at the Seminex technical seminars held at Imperial College, London, during the period 10-14 April, 1978. Topics cover a variety of developments in semiconductor technology.

# TELEVISION PRINCIPLES AND PRACTICE by Zarach & Morris Published by Macmillan Press 294 pages. Price £12.50 hardback, £5.95 paperback

A NOTHER volume that caters for the various television options within the TEC framework as well as City and Guilds courses.

Throughout, circuits relate to modern TV receivers which include transistor, i.c.s., thyristors, etc.

The first three chapters cover the science of colours and the formation of monochrome and colour signals. Then follows a review in block form of the receiver which forms the basis of circuit analyses for future chapters.

Throughout the book emphasis is placed on the practical aspects of TV servicing and as such should prove invaluable to anyone professionally involved whether experienced or just beginning a career. This applies equally to the enthusiastic amateur.

# AUDIO SYSTEM DESIGN FOR SCHOOLS AND COLLEGES

by R. H. Welch, B.Sc. Published by NCST Trent Polytechnic 195 pages. Price £2·75

N contrast to many books on this subject which set out the relative merits of design bricks in the audio chain tailored to a specification with the inevitable juxtaposing of commercially available systems, this book introduces the basic ideas necessary for the enquiring reader to design and build his own.

Aimed primarily at sixth formers and college students it forms an excellent practical guide and reference for the construction of turntable, pick-up arm, amplifier and loudspeaker cabinets etc., in project work allied to formal Engineering courses.

Albeit motivated academically it is pitched at a level which should, prove enlightening to anyone brave enough to go it alone on a d.i.y. system. Take heart, lasers and digital encoding aren't mentioned.

# PUTER Including V.A.T. Postage & Packing

This beautiful orange and black finish plastic case is available for Superboard II, Compukit UK101 or, with an uncut keyboard panel, for mounting many other hobby computers. It is supplied with a mounting wedge to give a suitable keyboard angle and fixing screws for Superboard or Compukit. The case is strong enough to support a small portable TV or video monitor and has ventilation slots and a cable access panel at the back. It does not carry the "PE Compukit" badge shown in the photograph.

The dimensions of the case (with Superboard keyboard cut out) a e shown below-case material is approximately 2mm thick with 4mm radius corners. We recommend that the power regulator fitted to Compukit boards is mounted on a heatsink and fixed to the outside back of the case.

The front cover illustration shows part of our own office system employing this case. PE has been able to arrange this special price so don't miss out as the offer closes Friday 29th February 1980.



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# **BATTERY ALTERNATIVE**

The Secretary of State for Industry has patented (British patent No 1 552 436 which dates from 1976 and is thus issued under the old laws), an interesting idea for storing large quantities of electrical energy by chemical means other than a vast and expensive battery of electrolytic cells. The inventor, Albert Montgomery, suggests that the system could be used either to even out the peak and low load demands on an electric power station or to drive a vehicle.

The invention relies on a reversible exothermic chemical reaction, that is to say a reaction which produces heat from the mixture of two materials which are aubsequently recovered and regenerated by electrolysis. This process is, under some conditions, more efficient at the bulk storage of energy than a conventional battery.

Fig. 1 shows the flow diagram for the cycle of the combination of the two materials



# PATENTS REVIEW...

to produce a heat output from exothermic chemical reaction and a resultant electrolytic separation of the reaction product resulting from this. Recombination to produce the original materials for recycling is effected by the electrical energy input.

Fig. 2 shows the basic "circuit". Two stainless steel vessels, 1, 2 contain sodium and sulphur respectively. These raw materials are fed through valves to reaction vessel 5 which is of heat and corrosionresistant material. Copper conduit 6 for a fluid to be heated (for instance water or gas) is coiled round the vessel 5.

The sodium and sulphur react together to form sodium polysulphide with the release of considerable quantities of heat energy. This energy is taken up by the fluid in the coil 5 and led off to a load.

The load is a heating stage for an electric turbine or vapour engine for a vehicle, such as a Stirling cycle heat engine.

The spent polysulphide is fed to recovery cell 10 which has a blind-end tube of solid beta-alumina electrolyte. This tube defines a cathode. 9 inside an anode 12. A 3 volt d.c. supply is fed through the electrodes to the polysulphide, and sodium ions are conducted through solid electrolyte 11 to the anode while the sulphur remains in the cathode 9.

Regenerated sodium and sulphur are then recycled to the containers 1 and 2. Thus the patented energy storage system has a capacity limited only by the size of the storage containers.

Supplies of polysulphide can be converted to sulphur and sodium throughout the entire period when there is excess power available, for instance during low-load night conditions on the national grid, and supplies of sodium and sulphur recombined to provide heat and generate power during the



entire period when there is a heavy load on the grid. In this way large quantities of electrical energy can be stored at far more economical price than with conventional batteries and without recourse to exotic alternative energy storage techniques, such as pumping water up a hill, lifting weights up a slope or compressing gas into vast reinforced cylinders or underground caves.

The fact that the British government has patented the invention suggests that its practical use is under serious consideration. The idea could perhaps also be applicable to domestic central heating. The chemicals would be separated on night storage rates and combined during the day to produce hot water for central heating.

**PE/LEKTROKIT PRIZES** 

The following prizes were awarded as a result of the PE/Lektrokit competition run in our September 1979 issue.

**1st Prize** a Lektrokit Powerace 102, a jumper wire kit and 16 pin Test Clip goes to *Mr. D. J. Speakman* of Braintree for his dual timebase submission.

Runners up prizes have been awarded to *Mr. T. Johansson* of Sweden for a l.e.d. logarithmic level meter; *Mr. I. M. Crann* of Brecon for a novel tone generator for electronic organs and to *Mr. T. Davies* of Swansea for a combined voltmeter/logic scope.

Due to the very limited number of entries, first, third, fourth and seventh prizes only have been awarded.

# POINTS ARISING

# ULTRASONIC CLEANER (January 1980) The value of C2 should be 150pF and not 15μ. ULTRASONIC BURGLAR ALARM (December 1979)

The 18V battery voltage should be wired through the keyswitch instead of the neutral lead.

DIGITAL TEMPERATURE CONTROLLER (October 1979)

The wiper and top end of VR1 should go to +9V and not to IC1/14 (p.c.b. is correct).

# Kenneth Amor

THIS article outlines the methods used to send and receive digital information, and shows in detail an inexpensive method of accomplishing this using conventional telephone facilities. The Acoustic Modem allows data and software exchange almost instantly, over any distance.

Data to be transmitted over varying distances has been standardised in its format, known as the American Standard Code for Information Interchange, and is abbreviated to ASCII. The ASCII Code format is shown in Fig. 1.

# **ASCII CODE**

Every Alphanumeric character to be transmitted differs in bit pattern, and even the number of bits varies. It is possible to identify the whole of the ASCII character set using only seven bits, plus the start and stop bits. Fig. 2 shows this set of characters with their respective logic levels.

A code can be obtained for every Alphanumeric character, and many other characters to be found on certain keyboards.

### THE MODEM

The acoustic modem is able to deal directly with the waveform shown in Fig. 1, because it is in serial form. A typical period for one bit is ten milliseconds, thus allowing one character to be transmitted in approximately 100 milliseconds. The bit period may be varied depending upon whether electromechanical or all electronic data transmission/receiving equipment is being used.

Having applied data to the Modem we now wish to transmit same over many miles to a fellow computer user, and it is a question of sending and receiving this digital information over long distances without tampering with post office equipment. The answer is, of course, the acoustically coupled telephone modem. By inserting the handset of a domestic telephone into this device, data may be transmitted and received at will, albeit somewhat slowly.

The principle of operation employs frequency modulation techniques involving the phase locked loop principle. A full explanation of how the complete system works is given in conjunction with the circuit diagrams of Figs. 5, 6 and 7.

Constructional dimensions are given for both the standard telephone handset and the trimphone version. Of course, two such acoustic modems will be required to set up a data link, but it is assumed that each enthusiast would construct just one modem.

COMPUNE

# THE FREQUENCY SHIFT KEYED TRANSMITTER

The voltage controlled oscillator section of the phase locked loop (IC2) is utilised for the 1000Hz tone. The capacitor C1 and resistors VR2, VR3 are responsible for setting this initial frequency. This 1000Hz tone would be present for the logic level "O" on the input of the transmitter. This situation is so when TR1 is turned off. If now a logic level "1" is applied to the data input, IC1, using double negation, follows the input voltage level and therefore turns on TR1, effectively connecting R3, VR2 in Parallel with R4, and VR3. The new resistance value produced by this resistor combination produces a new VCO frequency of 1200Hz which is the frequency representing logic level "1". Pin 4 on IC2 (4046) contains the frequency shifting signal that is applied as base current to TR2 via R6. TR2 drives the miniature loudspeaker producing the two audible tones which represents the corresponding logic levels of input data. When the modem is in the "Send" mode the 1000Hz tone can clearly be heard from within the modem.

# SETTING UP THE FSK TRANSMITTER

- (a) Switch the Modem to SEND.
- (b) Apply a short circuit to the data input.
- (c) Connect a frequency meter to TP.
- (d) Adjust VR3 until 1000Hz is shown on frequency meter.
- (e) Now remove the short circuit from the input and apply +5V with respect to the common connection.
- (f) Adjust VR2 until the new frequency becomes 1200Hz i.e. 200Hz *change* between "0" and "1".
- (g) An audible indication will verify that all is well as these two frequencies are trimmed.

When this has been carried out it is worth applying a low frequency square wave to the data input of the transmitter to ensure that the frequency shift operation follows the logic levels being applied. A circuit suitable to carry out this test is shown in Fig. 4.

# THE RECEIVER SECTION

Let us assume we are receiving the transmitted signal from a distant modem. The modem at our end picks up from the telephone handset the faint signals and applies them to an audio amplifier (IC3). A gain of approximately 100 was found to be sufficient to provide a working signal for the phase locked loop (IC4). C2 couples the FSK (Frequency-Shift Keying) signal to pin 2 of IC4. Diodes D5, D6, across R16 serve to provide some degree of limiting, as well as protection to IC4's input. Limiting by D5, D6 prevents amplitude modulation interference. The timing components VR1, C3, determine the frequency that the phase locked loop will free run at. This frequency should be adjusted to be 1100Hz, i.e. between the two FSK frequencies to be received. When a logic "O" is received (1000Hz) at pin 2 of IC4, the phase locked loop will lock onto this causing the voltage controlled oscillator of the PLL to suddenly shift from 1100Hz to 1000Hz. As this happens, the output signal from the phase comparator (pin 7 of IC4) becomes negative with respect to the reference potential at pin 6 of IC4. This potential difference will force the d.c. comparator IC5 to swing negative and this output signal will be caught at approximately -0.5V by D7 when the logic "0" is received. If now we receive a logic "1" signal (1200Hz) at pin 2 of IC4, the PLL will lock with its VCO frequency at 1200Hz, resulting in the phase comparator output becoming greater than the d.c. reference on pin 6 of IC4. Thus the voltage comparator IC5

\* \* \* \* \* \* \* \* \* \* \* \* LOGIC 1 BIT BIT BIT 811 BIT BIT BIT BIT 6 0 LOGIC O 0 0 0 0 D 0 \* = ONE BIT TIME E = STOP BITS P = PARITY CHECKING BIT - START BIT R EG266 = DATA BITS



b7-→b5	000	001	010	011	100	101	110	111
b7→b5 b4→b1 0000 0011 0100 0101 0101 0110 0101 1000 1001 1010	000 NUL SOH STX ETX EOT ENQ ACK BEL BS HT LF	DLE DC1 DC2 DC3 DC4 NAK SYN ETB CAN EM SUB	010 SP ! " # \$ % & *	011 0 1 2 3 4 5 6 7 7 8 9 9	100 @ A B C D E F G H I J	101 P Q R S T U V W X Y Z	a b c d e f g h i i	111 p q r s t u v v v v x y z
1011 1100 1101 1110 1111	VT FF CR SO SI	ESC FS GS RS US	+ - period	· < # > ~	K L M N O	[ \ ] ~	k I m n o	{  }  ∼ DELete

Fig. 2. The ASCII code, showing the binary equivalents of each character

responds with an output voltage positive going. It will in fact saturate in the positive direction at about 4.4 volts, providing an adequate logic level to become our Data output. C5 is chosen for determining the lock range of PLL, while R19, C6, R20, C7, R21, C9 form a filter network preventing the possibility of the VC0 frequency, or harmonics, upsetting the output comparator.

Fig. 3. Block schematic of the Modem link-up. The system is half-duplex. Serial pulse repetition rates should be no higher than the VCO Tx frequency. Input levels are TTL. Applications might include micro' link-ups at 110 Baud, VDU communication using a 20mA loop, facsimile transfer etc. Trials with the Modem included a link-up with a teletype from Bebington (Merseyside) to Luton





# COMPONENTS ....

# Resistors

R1	18k
R2	5k6
R3	47k
R4	27k
R5	1M
R6, R8-R10, R19-R21	10k (7 off)
R7	82
R11, R12	270 (2 off)
R13	100k
R14, R16, R17	1k (3 off)
R15	100k nom. (subject to trimming)
R18, R22	2k2 (2 off)
All resistors 5% 1W unle	ess otherwise stated

### Capacitors

C1, C3	47n WIMA FKC-3 temp. stable
	or equiv. (2 off)
C2 .	100n
C4, C9	1000p (2 off)
C5	220n
C6-C8	22n (3 off)
C10, C11	1000µ/25∨ (2 off)
C12, C13	470n (2 off)
Ratings and types no	ot critical unless specified

### Potentiometers

TR3, TR5

D1, D2

D5, D6

D3

D4

D7

VR1, VR2, VR3 VR4

10k preset (3 off) 4k7 preset

# **Transistors and Diodes**

BC109 (3 off) **TR1, TR2, TR4** BC147 (2 off) 1N916 (2 off) I.e.d. (red) I.e.d. (green) OA202 (2 off) 4V7 Zener (BZY 88) 1A 50V rectifier bridge (2 off) D8-D11, D12-D15

### **Integrated Circuits**

IC1	CD4011
IC2	4046
1C3, 1C5	741
IC4	565
1C6, 1C7	5V 1A regulator (plastic

# **Miscellaneous**

Crystal microphone insert Miniature loudspeaker 80 100mW Transformer 0-12V: 0-12V: 3VA I/O d.i.n. socket (3-pin) Double-pole, double-throw switch (send/receive) Veroboard 137 x 64mm (5 x 2.5ins.) I.c. board type: PCB421 available from West Hyde **Developments Ltd.** 

# **CONSTRUCTOR'S NOTE**

A complete set of components for the Acoustically Coupled Telephone Modem is available from Watford Electronics (see advertisers' index).

# MODEM OWNERS' REGISTER

Having got you to build the modem, your computer will be on the look-out for other machines to talk to, and so it is our endeavour to compile a list of all PE Modem owners who wish to "ASCIImunicate". We hope response will be sufficient to provide a useful list on request, so send us your details (listed below) and a S.A.E.

Suggested details: Name, address, telephone number, system, micro' used, peripherals and reason for incorporating the modem (in brief please).



# **PO REGULATIONS**

We believe the specification of the PE Acoustic Modem conforms to the Post Office regulations governing the use of devices acoustically coupled via the Public Switched Telephone Network. However, it should be noted that under the Post Office Act 1969 accoustically coupled devices should not be used with Post Office maintained plant without the prior consent of the Post Office.

Applications for the evaluation of private equipment (for which a charge in excess of £50 will be payable) may be made to the Post Office once the supplier is satisfied that the equipment meets the requirements given in Technical Guide No. 32, available from: Post Office Telecommunications Headquarters, Service Department Sv 1.1.3.3, Tenter House, 45 Moorfields, London EC2Y **9TH**.





# **ACOUSTIC MODEM**



EG 268

Fig. 12. Transmitter Test Point waveforms. When no input is applied and the Modem is switched to Transmit, the 1Ms square wave will appear continuously at Test Point 2

# **RECEIVER CHECK**

- (a) Look at signal on TP3 to ensure it is at least 250mV peak to peak when receiving from distant modem.
- (b) If not, the gain of IC3 may have to be raised by increasing R15 (100k).
- (c) With no signal being received, adjust VR1 until the frequency meter placed on TP4 reads 1100Hz.
- (d) With Data being received observe TP5 and refer to receiver waveforms information.

# DATA INDICATOR AND OUTPUT OPTIONS

Signals from both the transmitter and receiver are fed to I.e.d.s D3 and D4. This allows us to monitor the data both when we are sending and also receiving. It should be made clear that the modem will not be doing both at once, being *half*-duplex.

TR3 switches on when the output of gate (IC1) goes high (Transmit Mode) or when Pin 6 of IC5 goes positive (Receive Mode). This will result in (D3) turning on and indicating a logic "1" level being present. As TR3 is turned on, R12 is virtually connected to ground, thus turning off TR5. The transistors TR3 and TR5 form a "see-saw" stage. When one is off the other is on, so that when no base current flows in TR3 it is a sure sign that a logic "0" is being received or transmitted, thus TR5 will be turned on and the "0" l.e.d. will be illuminated.

TP5 would normally be the receiver output point. It might be that a 180° signal is required to drive the device coupled to the modem. If this is so, connect the output of the modem to the open collector of TR4. i.e. TR4 will be turned on when "0" is being received. This is suitable for coupling to a teletypewriter.



Fig. 13. Receiver waveforms. Example shown is the ASCII character "M". The I.f. pulses, i.e. logic 0, are a burst of 1ms pulses for the duration of the bit. The h.f. burst (logic 1) contains bit blocks 0.83ms wide. For Teletype operation the output bit duration is about 10ms



NEXT MONTH



In the concluding article next month we shall give stripboard layout diagrams for the three boards, plus a considerable amount of applications information and device data showing how the modem can be improved and/or adapted to suit particular link-up requirements by K. Lenton - Smith

Strictly

A NEW instrument was presented at the recent Trade Fair—the Sharma HX80. The manufacturers, Keith Hitchcock, have been mentioned previously in this column in connection with their Doppler-effect speaker systems. Early last year I heard the prototype in action and had an opportunity to examine its very compact circuitry. Played through a rotary speaker, it was a Hammond tone-wheel organ recreated.

At first sight, the HX80 is a fairly conventional portable organ, drawbar controlled with 49 notes on the upper and 37 notes on the lower manual. The 18-note pedal clavier has either 8' or 10' pitch available. Generation is by digital pulse trains and, by splitting the waveform into segments at differing voltage levels, versatile tone synthesis is achieved. The sine waves produced by this means are mixed (Fourier synthesis) in the normal way.

The group of nine drawbars on the upper manual has been arranged so that 5-1/3' is replaced by 1-1/7'—which is a very odd frequency in relation to the chromatic compass but is possible because of the tone generator used. It is seven times the fundamental frequency and if the latter is taken as A 440Hz, 3080Hz falls between F and G! Use of the seventh harmonic is not new (one of the overtones in a square wave in fact) but this unusual mutation drawbar provides extra tone colouring.

Other drawbars control 8' and 4' string tone, variable sustain, attack, decay and ambience (a form of reverberation). A single switch alters the compass of the manuals down one octave so that 32' to 2' pitches are substituted. The lower manual has no mutations but separate sustain covers the 16' 8' 4' 2' and 1' pitches. Presets, three vibrato controls and a transposer also feature. Priced at under £700 including VAT, the HX80 will interest those looking for a comprehensive but fully portable instrument (though a tone cabinet is required). Basically this is a 'straight' organ without too many gimmicks and is made in the UK.

# PIANOCORDER

The Pianola is a rarity these days and, like the fairground organ, uses punched paper rolls. The Kemble Piano Co. has the UK marketing rights for the first electronic version—the Pianocorder. Using cassette tape, digital pulses are recorded as a pianist plays the original. On playback, pulses from the tape are decoded and applied to solenoids on playing key or expression pedal. For teaching purposes, this could be a most useful aid as, unlike hearing a magnetic tape recording of the conventional type, the Pianocorder's keys are seen to move—and the playback speed can be varied at the teacher's will.

As this article goes to press, the Pianocorder is being demonstrated at the Chappell Music Centre, New Bond Street, London W1.

# NO GO

An interest in electronic music can have its problems as friends may ask for your help in sorting out a small problem caused by transportation or rough usage. Of course, the cause is always obscure, inspection lighting inadequate and time is of essence! If the reader is inadvertently involved, a few guidelines may help:

Modern instruments, and organs in particular, have circuitry that is far more complex than a decade ago. A service manual (or at least block diagram) is essential as CMOS devices are often the order of the day—and it is wise to know what you are dealing with. Instruments in the home are often on nylon carpeting so circuit boards should not be treated with abandon. Although protection diodes are normally employed, the board should be considered as an extension to the i.c. Some special purpose devices are difficult to find so if in doubt earth yourself and obviously use a low leakage iron, also earthed.

If the instrument has been moved without its back panel in place, printed circuit boards can easily get damaged. Equally, forcing It into position over misaligned guides can split the board. If a crack is diagnosed, remove p.c.b. sockets with great care as solid conductors are often used. Run a little cyanoacrylate adhesive into the crack and clamp the board flat for the few minutes it takes to set. After removing the clamp, broken tracks can be patched: clean the copper strip locally with a small, sharp blade (a scalpel is ideal) and solder small bridges of tinned copper across the breaks.

Commercial instruments are designed for easy replacement of sub-assemblies and thus contain many connectors and a wiring harness similar to those used in the car industry. Slide-on tags for multiple connection to a common point are often used and are also reminiscent of BL products. They may be perfectly good for cars, but can cause noise and breakthrough in organs if used for signal earth purposes. Vibration from internal speakers or in transportation can cause them to get noisy or to simply disconnect themselves: remedies being either to tighten to the maximum or risk the wrath of the professional serviceman by chopping off the tags and making a really sound job by soldering!

# TESTING

Digital meters can be very useful at times but, due to the time taken to sample, are not satisfactory for reading moving voltages/currents, e.g. percussion circuits. Although this also applies to analogue meters to some degree, the reaction of a pointer gives a much better idea of the circuit's action. Incidentally, I would suggest that any prospective purchaser takes a good look at a detailed specification of the digital meter in mind as advertisements often omit essential points. Despite claims of high accuracy, current readings are often subject to voltage burdens which, in some models, will cause errors of 25 per cent or so. My own digital meter, which is widely advertised, often refuses to auto-zero itself (and it's no fluke!). At least these meters normally have very high input impedance, but analogue meters should be capable of 20kΩ/V.

A box containing an i.c. amplifier, speaker and battery is a useful tool for tracing audio paths. My version has a switched jack socket so that the battery is connected when the test lead jack is inserted: I don't need to remember to switch off before putting it back on the shelf. The connecting cable has a longer earth wire, terminated by a croc clip, so that the probe (inner of the screened lead) can be taken from end to end of an instrument without having to find a new signal earth point repeatedly.

An oscilloscope is perhaps something of a luxury for fault-finding and more useful at the design stage. Assuming that there is no intention of checking the waveform supplied to a top octave synthesiser, which will be in the MHz range and a simple square wave, the timebase range needs to be modest only. Vibrato will call for about 7Hz as the slowest trace, though unless there is good persistence, flicker makes the display's usefulness questionable. About 15kHz will be just about the maximum required for the X plate, but a simple 'scope will show whether the waveform is what it is supposed to be and if tone filters are having the required effect. Be careful where the scope is connected into the instrument, that the input coupling capacitor is above suspicion and if it should be earthed for that particular application. If in doubt with expensive CMOS devices, test elsewhere!

I have not mentioned a CR bridge as most meters can cope with resistor measurement fairly well. Some can also handle capacitors but if not, a single 4001 package and a few discrete components can be assembled into a direct reading capacitor adaptor. Where valve circuitry is concerned—and plenty still exist and work well—it pays to check values of discrete components. Resistors can change their values alarmingly when age and high voltages come into play, so don't always believe the colour of the multiplier band: 10k resistors can easily become 100k in the course of time.



THERE are many types of thermostat in use around the home and in industry. The majority make use of the bimetal strip or bar and for general use there is nothing wrong with them. However, where a wide range, close tolerance, or economical use of energy is required an electronic thermostat is far superior.

The advantage of the circuit to be described here is that the temperature of a body can be held, if necessary, to within 0.1°C (ideal for photographic and similar uses) and the economic value is that it does not overheat the body wasting energy in the process. (Fig. 1).

The circuit is designed to give bursts of full power, of sufficient duration to overcome heat losses, and maintain a constant temperature.

The circuit is built around the SGS-ATES L121 i.c. This device incorporates a zero voltage detector, amplifier, comparator, internal power supplies with reference voltages, output stage for triggering triacs or thyristors, and will work from any single phase 50-60Hz supply.

### CINEUIT DESCRIPTIO

The block diagram of the L121 is shown in Fig. 2. The supply to the i.c. is via Rs which limits the supply current to approximately 30mA. The mains frequency signal is clipped to  $\pm$ 12V at the clipping and rectification stage. Pins 8 and 10 are the i.c.s dual internal supply smoothing. This smoothed supply is regulated by the voltage regulating stage, and used to supply the other internal functions, and also produce a 1.5 volt reference at pin 4, and a positive supply output at pin 6.

The zero cross detector determines when the supply on pin 9 crosses zero volts relative to pins 12 and 13, and whether it is positive, or negative going. Signals from this detector are fed to the ramp generator, control logic and output logic stages. The ramp generator produces a linear rising voltage, the rate of which is determined by C1 (pin 1) and R1 (pin 16). This is referred to as the time base. The voltage of this ramp is from less than 1V to approximately 6V, and is fed directly to the comparator.

The amplifier is a high gain d.c. operational amplifier, which is used to amplify the sensor output voltages to a suitable level for the comparator.

The comparator compares the relative levels of the amplifier output (pin 2) with the time base signal (pin 1) and will enable the chopper and control logic when the ramp voltage exceeds that of the amplifier output, as shown in Fig. 3. This has the effect of turning the heater on and off at a rate set by the time base.

The output logic stage determines the gate pulse polarity



E0280 Fig. 1. Comparison between an electrical and a mechanical thermostat



EG 2 5 5

Fig. 2. Block diagram of the L121

and also synchronises it with the zero voltage of the mains (zero cross detector signal), and this reduces radio frequency interference (R.F.I.) produced by the triac to a very low level.

The control logic is such that it triggers the chopper stage when the voltage from the ramp exceeds the voltage at pin 2, and for a time dependent on C2, which means that the triac switches at a mains voltage of approximately  $\pm 10V$ .

To eliminate this transistor TR2 can be included, as in Fig. 4. TR2 inverts the control logic output and feeds it directly to



Fig. 3. Waveforms and phase relationships

the chopper. This has the effect of triggering the triac while the mains voltage is between zero and  $\pm 10V$ , which will reduce R.F.I. to an absolute minimum.

Fig. 4 shows the circuit diagram of the Electrostat with a range of 20°C to 80°C, and a variable time base of 1 second to 1 minute. The minimum time base of the system is set by R1 and C1, with TR1 increasing the value of C1 by a factor dependent on the gain of the transistor as the resistance of VR1 is increased.

Diodes D2 and D3 are extra clipping diodes so that under fault conditions, no high voltages can appear on pin 9 of the L121. The sensor of the system is a thermistor connected to the inverting input of the amplifier as shown in Fig. 5. The 1.5 volt reference from pin 4 is compared with the potential difference across the thermistor, the difference amplified, and fed to the comparator as described earlier. If the amplifier gain is high i.e. 50 or more, any small change in



(\*see text) Fig. 4. Circuit diagram of the Electrostat (\*see text)



Fig. 5. Block diagram of the amplifier, comparator and ramp generator

thermistor potential will result in a large change in output from the amplifier, which will be acted upon by the other circuit functions, to return the sensor voltage near to the reference level. This situation is ideal for photographic work where a temperature can be controlled to within 0.1°C or better, depending upon the location of the sensor, and the thermal resistance of the object being heated.

The exact value of time base and temperature setting components depends upon every particular application. Table 1 lists some possible uses and suggested values.

Application	Temp. Range	Time Base	Amplifier Gain
	Centigrade	and	R4 & VR3
		C1 Value	Value
Photographic	20-40	1s-5s	50-100
Heater		10μ-47μ	500k-1M
Fermentation	15-30	1s-30s	20-50
Heater		10μ-330μ	200k-500k
Fish Tank	20-30	30s-120s	20-50
Heater		330µ-1200µ	200k-500k
Room	15-25	60s-180s	20-50
Heater		600µ-1800µ	200k-500k
Immersion	40-80	15s-120s	20-70
Heater		150μ-1200μ	200k-700k
TABLE 1			

# TIME BASE SELECTION

The time base is set by R1 and C1. This time must be shorter than the time it takes for the heat to travel through the medium to the thermistor (thermal time constant). Transistor TR1 is used to increase the effective value of C1 to several hundreds of times its true value when long time bases are required, and where a large capacitor would be impractical. Typical time bases range from 1 second to several minutes.

The manufacturers of the i.c. recommend that R1 be set at 100k and C1 selected to give the required time using the formula:

$$C1 = \frac{1 \cdot 2 \text{ TB}}{R1}$$

where;  $VR1=0\Omega$ 

R1=100k

C1 in Farads

TB in seconds (1 second minimum)

When the time base needs to be 1 minute or more, T1 is used to magnify C1:

C1 (effective)=C1 (true value) X TR1 hfe where TR1 is a BC 184L

hfe = 250 to 900

and VR1 value is greater than 1M or omitted.

# THERMISTOR AND TEMPERATURE SETTING RESISTOR SELECTION

A thermistor similar to the types GM 473 or VA 3410 is recommended as their operating range is  $-60^{\circ}$ C to +200°C, and their resistance is fairly large at mid-range (approximately 47k at 25°C). The range of resistances **a**t various temperatures is given in Table 2. Referring to Fig. 5, it can be shown that:

R(max)=5·33Rt (max temp) (1) and Rp paralleled with Ra

 $Rp//Ra = (5.33 \times Rt (min temp)) - R (max)$  (2) If Rp parallel with Ra is a preferred value  $\pm 20$  per cent, use the preferred value. If not use the next biggest preferred value and calculate Ra:

$$Ra = \frac{(Rpv//Ra) \times Rpv}{Rpv - (Rpv//Ra)}$$
(3)

Select the range of temperature required and substitute in the equations the relevant values of thermistor resistances from Table 2.

Temperature (Centigrade)	Approx Resistance (Ohms)	
60	10M	
30	1 M	
0	159k7	
10	100k	
20	59k	
25	47k	
30	37k7	
40	24k8	
50	16k7	
60	11k5	
70	8k1	
80	5k9	
90	4k3	
100	3k2	
150	1k0	
TABLE 2		

Example

# Photographic Heater

Preferred range 20°C to 40°C

 $R(max) = 5.33 \times Rt(max)$ 

=5.33 x 24.8k

=132.2k

Nearest preferred value 120k

=194.5k

Nearest preferred value 220k

```
Ra = \frac{(Rpv//Ra) \times Rpv}{Rpv - (Rpv//Ra)}
```

194.5k x 250k

Ra=250k-194.5k

```
=876k
```

# Nearest preferred value 1MS

**Amplifer Gain** 

The amplifier gain is set by the ratio of R2, VR2, and R3: Gain=R2 +  $\forall$ R2

$$\frac{+ \sqrt{R2}}{R3}$$
(4)

# CONSTRUCTION AND TESTING

The p.c.b. design and component layout for the Electrostat are shown in Figs. 6 and 7. Triac CSR1 should be of an adequate rating and mounted on a heatsink using a suitable insulating kit.

Care must be taken when assembling the triac on to the heatsink, and ensure the neutral is connected to the MT1 terminal. For 110V supplies R5 must be reduced to 3.3k 4W. Fuse FS1 is 50mA, and the load should be fused at a suitable value.



Fig. 7. Component layout

# COMPONENTS ....

### Resistors

R1, R2	100k (2 off)
R3	10k
*R4	
R5	6k8 7W (3k3 4W for 110V)
R6	33k
87	220k
*Ba	

All resistors 1/W 10% except otherwise stated.

### **Potentiometers**

**VR1, VR2** 1M Lin. (2 off) \*VR3

### Capacitors

*C1	
C2	10n
C3	220n
C4, C5	220µ 16V (2 off) elect.

### **S**emiconductors

D1	1N4148
D2, D3	BZX61 15V (2 off)
TR1, TR2	BC184L (2 off)
CSR1	2N5574 (or any 400V triac with a suitable
	current rating for the load)
TH1	VA3410
IC1	L121 (Quarndon Electronics, Slack Lane, Derby.)

# Miscellaneous

LP1, LP2	Mini mains neon (2 off)
FS1	50mA fuse
P.c.b.	
Connector	block
Heatsink to	o suit triac
Suitable ca	ise
JK1 3.5m	m jack socket
*See text	



Fig. 8. Terminal block wiring

The wiring for the terminal block is shown in Fig. 8. The thermistor can be built into a probe as suggested in Fig. 9 and is connected to the circuit via JK1.

Having checked the circuit for correct placing of components, carefully examine around the i.c. for solder splashes and joined tracks. When all is satisfactory, connect the load and the supply, and switch on. If the thermistor is "cold", relative to the temperature setting, the "off" neon indicator LP2 will light immediately. If the "on" neon LP1 lights adjust VR3 to minimum, and check the "off" neon lights.

If neither neon lights, turn off and check all connections. Also check pin 8 for +12V, and pin 10 for -12V, with respect to pins 12 and 13. Next check pin 1 for ramp voltage. If satisfactory check pin 2 for voltage swing by adjusting VR3. If an oscilloscope is available, check pins 11 and 15 for control pulses, and pin 7 for output pulses.

BRASS SCREW SCREWED INTO TUBE



The setting of the sensitivity resistor VR2 will depend on the thermistor location within the medium and the time base. For maximum sensitivity, a time base much shorter than the thermal time constant of the body is preferable.

The sensitivity is best set by trial and error, or if a storage oscilloscope is available, monitor pin 2 for several minutes and adjust VR2 until a still flat trace is obtained.



If the sensitivity is set too high, the system will be under damped and the temperature could vary by a large amount around the required value. Similar results will be seen if the sensitivity is set far too low.

If in use R.F.I. is present, try adding TR2, R6 and R7. as shown in Fig. 4, and omit capacitor C2.

Having checked that the unit works, it can now be built into a unit to suit your own application. If a metal case or front panel is used ensure it is earthed. Remember, for safety DO NOT connect the earth to the neutral.

Where calibration of VR3 is required, it should be against a digital thermometer, or a laboratory standard mercury thermometer, located in the same area of the body as the units sensor.



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CHOS	4020	50p	4050	25p	LINEAR
Cinoc	4022	13p	4060	30p	
4001 13p	4024	40p	4068	13p	A SELECTION
4002 13p 4007 13p	4026 4027	90p 28p	4070	13p 13p	709 35p 741 16p
4009 30p 4011 13p	4028 4029	45p 50p	4072 4081	13p 13p	747 45p
4012 13p 4013 28p	4040 4041	55p 55p	4093 4510	36p 60p	7106 850p
4015 50p 4016 28p	4042 4043	55p 50p	4511 4518	60p 65p	CA3046 55p
4017 47p 4018 55p	4046	90p 25p	4520	60p 60p	CA3130 90p
FULL DET	AILS IN	CA	TALOG	UEI	TRANSIST
TTL	7473	20p	74141	55p	10002 12
7400 10p	7475	25p	74145	90p	AC128 16p
7401 10p 7402 10p	7485	20p 55p	74150	55p 40p	AD161 38p
7404 12p 7406 22p	7489 1	35p	74154	40p	BC107 8p
7408 12p 7410 10p	7492	30p	74164	55p	BC108 8p BC108C 10p
7413 22p 7414 39p	7494	45p	74170	55p	BC109 80 BC109C 10p
7420 12p 7427 20p	7496	45p	74177	50p	BC148 7p
7430 12p 7432 18p	74121	25p 35p	74191	50p	BC177 14p BC178 14p
7442 38p 7447 45p	74123	38p 35p	74193	50p	BC179 14p BC182 10p
7448 50p 7454 12p	74126	35p 45p	74197 74199	50p 90p	BC182L 10p BC184 10p
OPTO	1				BC212 10p BC212 10p
			a se a ba	1004	BC214 10p
Red Til	25in. 0.2	.220	each 9p	7.5p	BC477 19p
Green TIL Yellow TIL	211 TIL	.221	13p 13p	12p 12p	BC548 10p
Clips 3p	3р				BCY70 14p BCY71 14p
DL704 0.3	in CC		130p 1	20p	CAPACITO
FND500 0.5	in CC	_	100p	80p	TANTALUM
SKTS	/		3-	1	0.1, 0.15, 0.22
				1	4.7, 6.8, 10uF
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Low profile by Texas Boin & Bo 14pin 10p 16pin 11p 3 lead T018 c Soldercon pin PCBS Size in. 2.5 x 1 2.5 x 3.75 2.5 x 5 3.75 x 5 3.75 x 5 3.75 x 5 3.75 x 5 3.75 x 5 3.75 x 5 5.75 x 5	18pin 20pin 22pin or T05 soc sis: 100:55 VEROBO 0.1in, 0.1in, 0.1 45p 4 564p 6 205p 18 40p 4 ibre glass 4 205p 18 40p 4 ibre glass 4 205p 18 40p 4 ibre glass 4 205p 18 40p 4 ibre glass 6 205p 18 40p 4 ibre glass 6 205p 18 40p 4 ibre glass 6 205p 18 0.5w 67 LM RESI billty, love each 10, sw from 10, SW 67 LM RESI	14p 16p 16p 16p 16p 17p 17p 17p 17p 17p 17p 17p 17p 17p 17	24pin 28pin 40pin 00p each 000:370 Vero Cutter Pin instool 1 r board. Peach. 145p per High stal noise 5% W. Any t 100 0.25W E RS e rated a to 330k + 100	18p 22p 32p 32p P ertion OSp Single pack. resist- oblity, , mix: 00+ 30 g of Meg- 5,70, t %W t %W	22 @ 16V, 47 @ MYLAR FIL 0.001, 0.01, 0.1 0.068, 0.1 POLYESTEF Mullard C280 s 0.01, 0.015, 0.1 0.15, 0.22 0.33, 0.47 0.68 1.00 File type 50V 220F to 10000 0.0470 File type 50V 220F to 10000 0.0470 File type 50V 220F to 10000 0.0470 File type 50V 220 1000 CONNECT JACK PLUGS A UN PLUGS A Stereo DIN PLUGS A
Low profile by Texas 8pin 8p 14pin 10p 16pin 11p 3 lead T018 d Soldercon pin PCBS Size in. 2.5 x 1 2.5 x 1 2.5 x 3.75 2.5 x 5 3.75 x 17 3.75 x 5 3.75 x 7 3.75 x 7 3.75 x 7 3.75 x 5 3.75 x 7 5.10 pens. Five mixed size 20 Dato pens. Five size 20 Dato	18pin 20pin 22pin or T05 soc is: 100:50 VEROBO 0.1in. 0.1 14p 45p 4 205p 18 40p 4 205p 18 40p 4 205p 18 40p 4 10 205p 18 40 205p 18 40p 4 10 205p 18 40 205p 18 40p 4 10 205p 18 40 205p 18 40 205p 18 40 205p 18 40 205p 18 40 205p 18 40p 4 10 205p 18 40 205p 19 40 205p 19 40 205p 10 205p	14p 16p 16p 16p 17p 16p 5in. 5p 4p 4p 5p 0p copped 5p 0p copped 5p 0p 100 0.9p 1.2p 2cks co 50. 100 0.9p 1.2p 2cks co 105 1.2p 100 1.2p 100 100 100 100 100 100 100 100 100 10	24pin 28pin 40pin 00p each 000:370 Vero Cutter Pin inst tool 1 er board. 24pin	18p 22p 32p 9 * 80p. sertion 08p Single pack. resist- bility, mix: 00+ 8p g of Meg- 5.70. t XW in 00+ 2p	22 @ 16V, 47 @ MYLAR FIL 0.001, 0.01, 0.0 0.068, 0.1 POLYESTEF Mullard C280 s 0.01, 0.015, 0.2 0.33, 0.47 0.68 1.00 F CERAMIC Plate type 50V 220 F to 1000 0.047 U RADIAL LE 63V 0.47 1 100 25V 10 2 1000 25V 10 2 1000 CONNECT JACK PLUGS A 2.5mm 3.5mm Standard Stereo DIN PLUGS A 2pln 3pin 180° 5pin 180°
Low profile by Texas Spin & Sp 14pin 10p 16pin 11p 3 lead T018 d Soldercon pin PCBS Size in. 2.5 x 1 2.5 x 1 2.5 x 3.75 3.75 x 5 3.75 x 5 3.75 x 5 3.75 x 17 Single sided pins per 100 Top quality 4 sided, Size 20 Dato pens. Five mixed si PCBSS E12 series. 4 0.25W Special devel 10 of each v ohm (650 rev METAL FI Very high sta 1%, Available E24 series. A 0.25W PLEASE FOR YOU	18pin 20pin 22pin or T05 soc is: 100:50 VER 080 0.1in. 0.1 14p 45p 4 564p 6 64p 6 205p 18 40p 4 205p 18 40p 4 15re glass 6 33 x 95mm 75p each. herts of A 0RS .7 ohms t each 15p 1.5p opment pp alue from 51c ny mlx: each 4p 4p	14p 16p 17p 16p 17p 5p. 4p 5p. 5p. 4p 5p. 60p 16p. 17p 5p. 4p. 5p. 4p. 5p. 60p 1fac. 100v 11ac. 100v 1	24pin 28pin 40pin 00p each 000:370 Vero Cutter Pin ing tool 1 Probard. 24pin 20pin 2	18p 22p 32p 32p β P · · · · · · · · · · · · · · · · · ·	22 @ 169, 476 MYLAR FIL 0.001, 0.01, 0.1 0.068, 0.1 POLYESTEF Mullard C280 s 0.01, 0.015, 0.2 0.33, 0.47 0.68 1.00F CERAMIC Piate type 50V 220F to 1000p 0.0470F RADIAL LE 63V 0.47 1 100 25V 10 2 100 25V 10 2 100 20 CONNECT JACK PLUGS A 2.5mm Standard Stereo DIN PLUGS A 2pin 3pin 5pin 180° 5pin 240° 1mm PLUGS A
Low profile by Texas Spin 8p 14pin 10p 16pin 11p 3 lead T018 c Soldercon pir PCBS Size in. 2.5 x 1 2.5 x 2 3.75 x 5 3.75 x 1.7 Single sided pinst of pens. Five mixed sl 0.25W 0.5W Special devel 10 of each v ohm (650 ref METAL F1 Very high sta 1%, Available E4 series, A 0.25W PLEASE FOR YOU FREECO	18pin 20pin 22pin or T05 soc is: 100:50 VER 080 0.1in. 0.1 14p 45p 4 564p 6 64p 6 205p 18 40p 4 15p 205p 18 40p 4 15p 205p 18 40p 4 100 4 100 50 00 50 00 50 1	14p 16p 17p 16p 17p 5m 5p 4p 5p 60p 100- 0.9p 1.2p 5cks c 100- 3.5p 100- 3.5p	24pin 28pin 40pin 00 each 000:370 Vero Cutter Pin ins tool 1 r board. 0 each. 145p per tool 1 tool 1	18p 22p 32p 22p 32p 2 P 80p. single s	22 @ 16V, 47 @ MYLAR FIL 0.001, 0.01, 0.1 0.068, 0.1 POLYESTEF Mullard C280 s 0.01, 0.015, 0.0 0.15, 0.2 0.33, 0.47 0.68 1.00 f CERAMIC Plate type 50V 220 F to 1000 0.047 u RADIAL LE 63V 0.47 1 100 25V 10 2 100 25V 10 2 100 CONNECT JACK PLUGS J UNS 2.5mm Standard Stereo DIN PLUGS A 2011 80° 50 in 180° 50 in 180°
Low profile by Texas 8pin 8p 14pin 10p 16pin 11p 3 lead T018 c Soldercon pir PCBS Size in. 2.5 x 1 2.5 x 1 2.5 x 3.75 3.75 x 5 3.75 x 5 3.	18pin 20pin 22pin or T05 soc ss: 100:55 VEROBO 0.1in. 0.1 14p 45p 4 564p 6 64p	14p 16p 17p 16p 17p 16p 17p 5p ket. 1 5p 4p 4p 4p 5p 0p copped 5p 100- 0100 1000 0.9p 1.2p 100- 1	24pin 28pin 40pin 00 each 000:370 Vero Cutter Pin ins tool 1 er board. b each. 145p per 145p per 145p per 145p per 145p per 100,0100,00000000	18p 22p 32p p 80p. sertion 08p Single single spack. resist- bility, mix: 00+ 30 g of g Meg- 5,70, t XW in 00+ 20 20 20 20 20 20 20 20 20 20 20 20 20	22 @ 16V, 476 MYLAR FIL 0.001, 0.01, 0.0 0.068, 0.1 POLYESTEF Mullard C280 s 0.01, 0.015, 0.0 0.15, 0.2 0.33, 0.47 0.68 1.00F CERAMIC Plate type 50V 226F to 10000 0.0470F RADIAL LE 63V' 0.47 1 100 25V 10 2 100 CONNECT 1000 CONNECT JACK PLUGS A UNS 2.5mm 3.5mm Standard Stereo DIN PLUGS A Suitable for low Plugs: 6p each 4mm PLUGS A
Low profile by Texas 8pin 8p 14pin 10p 16pin 11p 3 lead T018 c Soldercon pir PCBS Size in. 2.5 x 1 2.5 x 1 2.5 x 3.75 2.5 x 5 3.75 x 5 3.7	18pin 20pin 22pin or T05 soc 15: 100:55 VEROBO 0.1in. 0.1 14p 45p 4 205p 18 205p 18 20	14p 14p 16p 17p 16p 17p 5p 4p 4p 4p 5p 00 00 00 00 100 0.9p 12p 100 0.9p 12p 100 0.9p 12p 100 0.9p 12p 100 100 0.9p 12p 100 100 100 100 100 100 100 100 100 10	24pin 28pin 40pin 000:370 Vero Cutter Pin ins tool 1 r board. beach. 145p per High stal noise 5% M. Any f 10 0.25W E BRS erated a to 330k 10 3.3	18p 22p 32p p 80p. sertion 08p Single single pack. resist- bility, mix: 00+ 5,70, t XW in 00+ 2p	22 @ 16V, 476 MYLAR FIL 0.001, 0.01, 0.0 0.068, 0.1 POLYESTEF Mullard C280 s 0.01, 0.015, 0.0 0.15, 0.2 0.33, 0.47 0.68 1.00F CERAMIC Plate type 50V 220F to 1000 0.047uF RADIAL LE 63V' 0.47 100 25V 10 25V 10 25V 10 25V 10 20 1000 CONNECT JACK PLUGS A UNS 2.5mm 3.5mm Standard Stereo DIN PLUGS A Suitable for Ion Plugs: 6p each 4mm PLUGS A Available in Dila and yellow. P
Low profile by Texas 8pin 8p 14pin 10p 16pin 11p 3 lead T018 c Soldercon pin PCBS Size in. 2.5 x 1 2.5 x 3.75 2.5 x 5 3.75 x 17 Single sided Display the second of each v ohm (650 res) FOR YOU FOR	18pin 20pin 22pin pr T05 soc ss: 100:55 VEROBO 0.1in. 0.1 14p 45p 4 205p 18 205p 18 20	14p 14p 16p 17p ket. 1 5p 4p 5p 00p coppeo. 60p 16p. 60p 16p. 60p 16p. 75p 00p 00p 00p 10p 00p 10p 00. 90p 10p 100 100 100 100 100 100 100 100 1	24pin 28pin 40pin 000:370 Vero Cutter Pin instool 1 r board. be each. 145p per High stal noise 5% M. Any r 10 0.25W E PRS e rated a to 330k 10 3.7 STEVER	18p 22p 32p p e 80p. section 08p Single single pack. resist- colliny, mix: 000+ 20 g of t XW in 000+ 20 20 p	22 @ 16V, 476 MYLAR FIL 0.001, 0.01, 0.1 0.068, 0.1 POLYESTEF Mullard C280 s 0.01, 0.015, 0.0 0.15, 0.2 0.33, 0.47 0.68 1.00F CERAMIC Plate type 50V 220F to 10000 0.0470F RADIAL LE 63V 0.47 1 100 25V 10 22 100 CONNECT JACK PLUGS A UN Standard Stereo DIN PLUGS A Suitable for Ion PLUGS A Available in blu and yellow. P

LINC	MIL	LF356	80p	NE531	98p
THIS		LM308	60p	NE556	60p
A SELEC	TION	LM318N	75p	NE567 RC4136	100p
709	35p	LM339	45p	SN7647	7 230p
741	16p	LM378	230p	TBA800	) 70p
748	300	LM380	75p	TDA102	2 620p
7106	850p	LM3900	50p	TL081	45p 1250
CA3046	55p	LM3911	100p	ZN414	80p
CA3080	70p	MC1458 MM57160	32p	ZN425	E 390p
CASISO	500	1010137100	, 220p	2111034	2001
TOAN	SIST	ORS		ZTX50	0 16p
Inni		BCY72	140	2N697 2N3053	12p 18p
AC127	17p	BD131	35p	2N3054	50p
AC128	16p 18p	BD132 BD139	35p	2N3055 2N3442	2 135p
AD161	38p	BD140	35p	2N370	2 8p
AD162 BC107	38p 8p	BFY50 BFY51	15p	2N3703 2N3704	8 8p 1 8p
BC108	- 8p	BFY52	15p	2N370	5 9p
BC108C	10p 8p	MJ2955 MPSA06	98p 20p	2N370	5 9p 7 9p
BC109C	10p	MPSA56	20p	2N370	8 8p
BC147 BC148	7p 7p	TIP29C TIP30C	60p 70p	2N3819 2N3820	3 15p 3 44p
BC177	14p	TIP31C	65p	2N390	4 8p
BC178 BC179	14p	TIP32C	80p 65p	2N390	5 8p
BC182	10p	TIP3055	55p	2N405	B 12p
BC184	10p	ZTX107	14p	2N545 2N545	9 32p
BC184L	10p	ZTX300	16p	2N577	7 50p
BC212L	10p			_	
BC214	10p		DIOD	DES	
BC477	19p	1N914	Зр	1N4006	6p
BC478	19p	1N4001 1N4002	4p 4p	1N5401 BZY88	13p ser, 8p
BCY70	14p	ITT Fulls	pec. p	roduct.	
BCY71	14p	1N4148	- £1.4	10/100.	
0104	CITC	BS .	-		_
CAPA	UIL				
TANTA					
	ALUM	BEAD			each
0.1, 0.15	5, 0.22	BEAD 0.33, 0.47	, 0.68,		each
0.1, 0.15	5, 0.22, F @ 39	BEAD 0.33, 0.47	, 0.68,		each 8p
0.1, 0.15 1 & 2.20 4.7, 6.8, 22 @ 16	5, 0.22, F @ 39 10uF V, 47 @	BEAD 0.33, 0.47 5V @ 25V @ 6V, 100 @	, 0.68, 		each 8p 13p 16p
0.1, 0.15 1 & 2.20 4.7, 6.8, 22 @ 16 MYLAI	6, 0.22 F @ 39 10uF V, 47 @ R FIL	BEAD 0.33, 0.47 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	, 0.68,	· · · ·	each 8p 13p 16p
0.1, 0.15 1 & 2.20 4.7, 6.8, 22 @ 16 MYLAI 0.001, 0	ALUM 5, 0.22, F @ 39 10uF V, 47 @ R FIL .01, 0.0	BEAD 0.33, 0.47 25 0 25 0 6 0, 100 0 0 22, 0.033	, 0.68, 3∨ 0.047	· · · ·	each 8p 13p 16p 3p
0.1, 0.15 1 & 2.20 4.7, 6.8, 22 @ 16 MYLAI 0.001, 0 0.068, 0	6, 0.22, F @ 39 10uF V, 47 @ R FIL .01, 0.0	BEAD 0.33, 0.47 0 25V 0 6V, 100 0 M 022, 0.033	, 0.68, 3∨ 0.047	· · · ·	each 8p 13p 16p 3p 4p
0.1, 0.15 1 & 2.2u 4.7, 6.8, 22 @ 16 MYLAI 0.001, 0 0.068, 0 POLYE Mullard	ALUM 5, 0.22, 10uF V, 47 @ R FIL .01, 0.0 .1 STER C280 s	BEAD .0.33, 0.47 5V .0.25V .0.00 @ M 0222, 0.033 eries	, 0.68, 		each 8p 13p 16p 3p 4p
0.1, 0.15 1 & 2.2u 4.7, 6.8, 22 @ 16 MYLAI 0.001, 0 0.068, 0 POLYE Mullard 0.01, 0.0	ALUM 5, 0.22, 16 @ 39 10uF V, 47 @ R FIL .01, 0.1 .1 STER C280 s 015, 0.1 22	BEAD 0.33, 0.47 5V 25V 6V, 100 @ M 022, 0.033, eries 022, 0.033,	, 0.68, 	, <b>0.068</b> , <b>0</b>	each 8p 13p 16p 3p 4p
0.1, 0.15 1 & 2.2u 4.7, 6.8, 22 @ 16 MYLAI 0.001, 0 0.068, 0 POLYE Mullard 0.01, 0.0 0.15, 0.2 0.33, 0.4	ALUM 5, 0.22, F @ 39 10uF V, 47 @ R FIL .01, 0.1 .1 STEF C280 s 015, 0.1 22 47	BEAD 0.33, 0.47 5V 9 25V 9 6V, 100 @ M 022, 0.033 eries 022, 0.033,	, 0.68, № 3 ∨ 0.047 0.047	, 0.068, C	each 8p 13p 16p 3p 4p 0.1. 5p 7p 10p
0.1, 0.15 1 & 2.20 4.7, 6.8, 22 @ 16 MYLAI 0.001, 0 0.068, 0 POLYE Mullard 0.01, 0.0 0.15, 0.2 0.33, 0.4 0.68 1.005	ALUM 5, 0.22, F @ 35 10uF V, 47 @ <b>R FIL</b> .01, 0.1 .1 <b>STEF</b> C280 s 015, 0.1 22 17	BEAD 0.33, 0.47 50 © 25V © 6V, 100 @ M 022, 0.033, eries 022, 0.033,	, 0.68, ⇒ 3∨ 0.047 0.047	, 0.068, C	each 8p 13p 16p 3p 4p 0.1. 5p 7p 10p 14p
0.1, 0.15 1 & 2.2u 4.7, 6.8, 22 @ 16 MYLAI 0.001, 0 0.068, 0 POLYAE MUIARD 0.01, 0.0 0.15, 0.2 0.33, 0.4 0.68 1.0uF	ALUM 5, 0.22, 10uF 0, 47 (0 <b>R FIL</b> .01, 0.1, .1 <b>STEF</b> C280 s 015, 0.1 22 47	BEAD 0.33, 0.47 50 60 60 60 60 60 60 60 60 60 6	, 0.68, 	, 0.068, C	each 8p 13p 16p 3p 4p 0.1. 5p 7p 10p 14p 17p
0.1, 0.15 1 & 2.2u 4.7, 6.8, 22 @ 16' MYLAI 0.001, 0.0 0.068, 0 POLYE Mulard 0.01, 0.2 0.15, 0.2 0.33, 0.4 0.68 1.0uF CERAN Piate typ	ALUM 5, 0.22, 104 104 047 047 05 01, 0.1 1 1 1 1 1 1 1 1 1 1 1 1 1	BEAD 0.33, 0.47 5V 25V 25V 0022, 0.033 eries 022, 0.033, 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	, 0.68,	, 0.068, 0	each 8p 13p 16p 3p 4p 0.1. 5p 7p 10p 14p 17p
0.1, 0.15 1 & 2.2u 4.7, 6.8, 22 @ 16' MYLAI 0.001, 0 0.068, 0 POLYE Mullard 0.01, 0.2 0.33, 0.4 0.68 1.0uF. CERAN Plate typ 22pF to 0.0127	ALUM 5, 0.22 F @ 39 10uF V, 47 @ R FIL .01, 0.1 .1 STEF C280 s 015, 0.1 22 47 MIC De 50V 1000p	BEAD 0.33, 0.47 5V © 25V © 6V, 100 @ M 0222, 0.033, eries 0222, 0.033, criss 0222, 0.033, criss 022, 0.033,	, 0.68,	, 0.068, 0	each 8p 13p 16p 3p 4p 0.1. 5p 7p 10p 14p 17p
0.1, 0.15 1 & 2.2w 4.7, 6.8, 22 @ 16 MYLAI 0.001, 0 0.068, 0 POLYE Mulard 0.01, 0.0 0.33, 0.4 0.33, 0.4 CERAM Plate typ 22pF to 0.047uF BADIA	ALUM 5, 0.22 F @ 39 10uF V, 47 @ R FIL .01, 0.1 .1 STEF C280 s 015, 0.1 22 47 MIC De 50V 1000p	BEAD 0.33, 0.47 5V ∞ 25V 0 6V, 100 € M 022, 0.033, eries 022, 0.033, c Available F and E6 st	, 0.68, 3.3V 0.047 0.047 0.047       	, 0.068, 0	each 8p 13p 16p 3p 4p 0.1. 5p 7p 14p 14p 17p pF to 2p
0.1, 0.15 1 & 2.2w 4.7, 6.8, 22 @ 16 MYLAI 0.001, 0 0.068, 0 POLYE Mullard 0.01, 0.0 0.33, 0.4 0.33, 0.4 CERAM Plate typ 22pF to 0.0470F RADIA 63V 0	AL LEE	BEAD 0.33, 0.47 5∨ © 25∨ © 6∨, 100 € M 022, 0.033, eries 022, 0.033, eries 022, 0.033, constants constant	, 0.68, 3.3. 0.047 0.047 0.047       	, 0.068, 0 series fro om 1500 - YTIC 10	each 8p 13p 16p 3p 4p 0.1. 5p 7p 10p 14p 17p 17p 5p 5p
0.1, 0.15 1 & 2.2w 4.7, 6.8, 22 @ 16 MYLAI 0.001, 0 0.068, 0 POLYE Mullard 0.01, 0.0 0.015, 0.2 0.33, 0.4 0.68 . 1.0wF CERAN Plate typ 22pF to 0.047wF RADIA 63V 0 0	AL UM 5, 0.22, F @ 32 10uF V, 47 @ R FIL .01, 0.1, .1 STEF C280 s 22 MIC De 50V 1000p	BEAD 0.33, 0.47 5V @ 25V @ 6V, 100 € M 022, 0.033, eries 022, 0.033, eries 022, 0.033, A H Eries C AD ELEC 0 2,2 22	, 0.68, → 3∨ 0.047 0.047  0.047   0.047       	, 0.068, 0 series fro om 1500 -YTIC 10 47	each 8p 13p 16p 3p 4p 2.1. 5p 7p 10p 14p 17p 17p 5p 7p 7p
0.1, 0.15 1 & 2.2w 4.7, 6.8, 22 @ 16 MYLAI 0.001, 0 0.068, 0 POLYE Mullard 0.01, 0.0 0.01, 0.0 0.015, 0.2 0.33, 0.4 0.68 1.0wF CERAN Plate typ 22PF to 0.047wF RADIA 63V 0 1	5, 0.22, 10, 5, 0.22, 10, 5, 0, 22, 10, 5, 0, 20, 10, 5, 0, 10, 5, 0, 10, 5, 0, 10, 10, 10, 10, 10, 10, 10, 10, 10,	BEAD 0.33, 0.47 5V @ 25V @ 6V, 100 € M 022, 0.033, eries 022, 0.033, Available F and E6s AD ELEC .0 .22 	, 0.68, 3 3 V 0.047	, 0.068, 0 series fro om 1500 -YTIC 10 47	each 8p 13p 16p 3p 4p 0.1. 5p 7p 10p 14p 17p 17p 5p 7p 13p 200
0.1, 0.15 1 & 2.2u 4.7, 6.8, 22 @ 16' MYLAI 0.001, 0.0 0.068, 0 POLYE Mullard 0.01, 0.0 0.33, 0.4 0.33, 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	5, 0.22, 10, 5, 0.22, 10, 5, 0.22, 10, 5, 0, 22, 10, 10, 0, 1, 10, 10, 10, 10, 10, 10,	BEAD 0.33, 0.47 <sup>SV</sup> <sup>©</sup> 25V <sup>©</sup> 6V, 100 € M 022, 0.033, eries 022, 0.033, eries 0, 0.033,	, 0.68, 3 3 V 0.047 0.047 0.047 0.047 1.17	, 0.068, 0 series fro om 1500 -YTIC 10 47	each 8p 13p 16p 3p 4p 0.1. 5p 7p 10p 14p 14p 17p 5p 7p 13p 20p 5p
0.1, 0.15 1 & 2.2u 4.7, 6.8, 22 @ 16' MYLAI 0.001, 0.0 0.068, 0 POLYE Mullard 0.01, 0.0 0.15, 0.2 0.33, 0.4 0.33, 0.4 0.33, 0.4 0.33, 0.4 0.33, 0.4 0.33, 0.4 0.33, 0.4 0.33, 0.4 1.00F CERAM Plate typ 22pF to 0.047uF RADIA 63V 0 1 25V 1 1	5, 0.22, 10, 5, 0.22, 10, 5, 0.22, 10, 5, 0.22, 10, 0, 1, 0,	BEAD 0.33, 0.47 5V © 25V © 0.47	, 0.68, 3 3V 0.047 0	, 0.068, C series fro om 1500 -YTIC 10 47	each 8p 13p 16p 3p 4p 0.1. 5p 7p 10p 14p 14p 14p 17p 5p 7p 13p 20p 8p 9p
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# STEVENSON **Electronic Components**

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A range of special offer items valid		TI					
during January. All orders placed							
for these items must be received							
during January.							
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Pack of 30 x 1N4001	. 120p	100p					
Pack of 4 x FND500	. 400p	350p					
Pack of 15 x 2N3702	. 1200	100p					
Pack of 15 x BC107	. 120p	100p					
Special pack of outs + holts containing							
over 600 4BA + 6BA nuts holts and							
washers	3300	250n					
		Loop					
Pack of 4 red + 4 black crocodile clips	64p	50p					
Mines as steel (seeks new 100 (mined)							
wixer control knobs, per 100 (mixed)	14000	1200-					
	1400p	1300p					

# MULTIMETERS

A really smart looking multimeter with an impressive specification for such a small size. The very clean scale in white and green on a black background makes this meter very easy to read. The D.C. Impedance of this meter is 4K ohms per volt which is exceptionally good compared with the vast majority of multimeters of a similar size. £5.95 each.



SPECIFICATION DC Volts AC Volts DC Current Resistance

### 5V 25V 250V 500V (4K ohms/V) 10V 50V 500V 1000V (2K ohms/V) 250uA 250mA 0 - 600K (7K ohms centre)

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MICRO-EUS

# Compiled by DJD.

Appearing every two months, Micro-Bus will present ideas, applications, and programs for the most popular microprocessors; ones that you are unlikely to find in the manufacturers' data books. The most original ideas will probably come from readers working on their own microcomputer systems, and payment will be made for any contribution featured here. This is also the place to air your views, in general, on this new technology, so let's be hearing from you!

# MICRO MAGICIAN

The following unusual program turns the computer into a magician, enabling it to find a card chosen secretly by a spectator. Two versions of the program are given; one in BASIC, and one in machine code for the 6502.

The presentation of the trick is as follows: only the thirteen cards of one suit are used for the trick. The cards are fanned out face down, and the spectator removes one and remembers its value. The remaining pile of cards is cut once, and the spectator replaces the selected card wherever he likes. The pile is then divided into two, and the two halves are shuffled together. Finally the cards are fanned out face-up on the table, and the order of the cards is typed into the computer. After a brief pause the computer announces which was the chosen card.

Although the trick is based on a simple principle, it leads people to believe that the computer's powers extend to mind-reading, and this belief is strengthened by occasional failures of the computer to guess the card correctly.

By way of illustration, try locating the chosen card in the sequence shown in Fig. 1. The cards were originally in order, ace up to king from left to right, and the sequence shown is the result of following the procedure described above.

# HOW THE PROGRAMS WORK

The programs work by comparing the new order of the cards with their previous order; for each card a number is calculated which represents how far the processes of shuffling and cutting have moved that card away from its previous neighbours. The higher this score, the more out of sequence is the card concerned. After calculating this score for each of the 13 cards, the card with the highest score is taken to be the one that was chosen, and in most cases this will be correct. However, in some cases the computer cannot be certain about which card was chosen; for example, if the card is returned to its original position then any card could have been chosen. Also, less obviously, if the card is re-inserted one place to one side of its original position it is impossible to tell whether it, or its neighbour, was the chosen card since the same sequence of

cards would result in each case. The reason for cutting the pack before the card is replaced is to encourage the spectator to replace the card in a different position.



Fig. 1. Find the chosen card in this sequence, which results from a presentation of the trick described in the text

When the programs are first executed they assume that the cards were originally in numerical order, ace up to king. If the cards are not initially in order the program will probably get the first attempt wrong, but in some ways it is more impressive to do the trick without arranging the cards first, and attribute the initial failure to "warming up"! On subsequent operations of the program the initial order is replaced by the new order of the cards, as typed in; the order of the cards should not be disturbed when the trick is repeated.

# CARD TRICK PROGRAMS

The two versions of the card-trick program work in comparable ways. The cards are represented internally by the numbers 1 to 13. The programs are divided into three sections. First, the new sequence of cards is read in. Secondly, each of the cards in the previous sequence is searched for in the new sequence, and its position there is subtracted from the positions of each of the cards that were its neighbours in the previous sequence. The sequence is considered to be circular, so if the difference between two positions turns out negative then 13 is added to it. The card's distance from one neighbour, plus its distance from the other neighbour, is saved as that card's score. Finally, the card with the maximum score is found and displayed as the chosen card.

The critical part of the trick is that the cards should only be shuffled once, and the shuffle should be of the sort that divides the packet of cards into two halves and merges the two halves back into one pile (e.g. a riffle shuffle). The cards can be cut at any time, and as many times as wished, but each time the packet of cards should only be cut into two piles.

# **BASIC VERSION**

The BASIC version of the card trick, Fig. 2, closely follows the above description. The subroutine at 500 looks up the card T in the array containing the previous sequence of cards, A, and returns in X the position of T in that array. The program uses only integer arithmetic, and so can work with integer-only' BASIC interpreters.



# Fig. 2. BASIC version of the card trick enables the computer to find a chosen card

# 6502 VERSION

The program for the 6502, Fig. 3, was developed on an Acorn system and uses two routines in the Acorn monitor, so if the program is used with another 6502 system these will have to be modified. Subroutine DISPLAY is a display and keyboard-scanning routine which displays the segment patterns from locations 0010-0017, and waits for a keypress (although it can be made to give a single sweep of the display without waiting). It returns with the hex value of the key pressed in the A-register, the X-register is preserved, and the Y-register is zeroed. Subroutine HEXTD generates the segment pattern for the hex number in the lower four bits of the Aregister, and stores this in display location Y.

When the program is executed at 0200 the display will go blank. The sequence of cards should then be entered using the hex keys, with ace = 1, ten = A, jack = B, queen = C, and king = D. When the last card is entered the micro will display its guess at the chosen card. The program is then ready to repeat the trick.



Fig. 4. Programmable frequency generator; the frequency is determined by the number at the output port

For simplicity, 14 bytes are allocated for each of the arrays, the zeroth byte not being used. Subroutine SCAN performs the same function as the subroutine in the BASIC verion.

# MODIFICATIONS

The programs can also guess two, or more, chosen cards, though with less reliability; for example, to find two chosen cards the programs should be modified to display the cards with the two highest scores. The programs can also be modified to work with any number of cards, and as the number of cards is increased the likelihood of the computer getting the card wrong diminishes. Thirteen cards is a happy medium; it is not too time-consuming to type in the order, while at the same time the computer's powers are indisputable!

# FREQUENCY GENERATOR

The following circuit enables a micro to act as a programmable frequency generator. It uses a low-cost digital-to-analogue converter to drive a voltage-controlled oscillator, and to illustrate its operation a program is given which will play monophonic melodies. The circuit and program were submitted by Mr. P. V.**Bayley** of Newcastle, and what follows js based on his description:

"The circuit, Fig. 4, was designed for use with an 8080 microprocessor, but is suitable for any 8-bit micro. It can generate frequencies covering an overall range of at least three octaves, and incorporates a variable pitch control.

# CIRCUIT DESCRIPTION

"Data from an 8-bit output port is fed to the inputs of the ZN425E 8-bit digital-to-

	CARD TRICK	0233 E5 4B	SBC POSN	
8	***	0235 BO 02	BCS OK	
DİSP	=\$0010 ACORN DISPLAY BUFFER	0237 69 OD	ADC E13 MAKE IN RANGE 0-1	2
DISPL	I = SFEOC DISPLAY ROUTINE	0239 48 OK	РНА	
HEXTD	=\$FE7A HEX DIGIT TO BUFFER	023A 18	CLC	
		023B A6 4A	LDX LAST	
0000	.=\$0020 FREE ZERO PAGE	023D 75 3C	ADC SUM.X	
0020 OLD	.=.+14 PREVIOUS SEQUENCE	023F 95 3C	STA SIM Y ADD TO SUM	
OO2E NEW	.=.+14 NEW SEQUENCE	0241 86 20	LDX OLD Y	
003C SUM	.=.+14 VALUES CALCULATED	0243 86 48	STY LACT PEDEAT FOR OTHER	
004A LAST	.=.+1	0245 68	DIA MADI REFEAT FOR UTHER	
OOAB POSN	= +1	0245 75 20	ADG CUM N	
0046 NAY		0240 75 30	ADC SUM, X	
0040		0246 95 30	STA SUM,X	
0040	STARL OF PROGRAM	024A 88	DEY	
OZOO DO BEGIN	CLD	OZ4B DO D7	BNE LOOP DO FOR ALL 13 CAR	DS.
0201 AU 00	LDY EO	024D A2 0D	LDY 513 LOOF FOR MAY	
0203 A2 0D	LDX E13 ASSUME CARDS ARE	024F A9 00	LDA SO	
0205 8A SET	TXA IN ORDER.	0251 B4 25 FTMD	IDV NEU V CONTRACTOR AND	
0206 95 20	STA OLD, X	0251 B4 26 FIND	LDY NEW, X TRANSFER NEW ORDE	R
0208 94 OF	STY DISP-1,X CLEAR DISPLAY	0253 94 20	STY OLD, X TO OLD.	
020A CA	DEX	0255 D5 3C	CMP SUM,X	
0208 DO F8	BNE SET	0257 10 04	BPL NOTGT	
020D E8 CET	TNY STAPT AT 1	0259 86 4C	STX MAX GREATEST SO FAR	
020F 20 0C FF	TCD DICDLY	025B B5 3C	LDA SUM, X UPDATE WITH VALUE	
0211 05 25	CON NEW Y CER CADD	025D CA NOTGT	DEX	
0211 93 26	STA NEW, A GET CARD	O25E DO F1	BNE FIND DO FOR ALL 13 CAR	DC
0213 94 30	STY SUM,X CLEAR SUM	0260 A5 4C	LDA MAY BEET CADD	03.
0215 84 12	STY DISP+2 CLEAR RESULT	0262 AO 02	LDV 52 DICDINK TH	
0217 20 7A FE	JSR HEXTD KEY TO DISP+O	0264 20 74 FF	TCP UEVED DISPLATIN	
O21A EO OD	CPX E13 ALL DONE?	0267 40 00 02	JAR HEATD POSITION 2.	
O21C DO EF	BNE GET	0207 40 00 02	JMP GET REPEAT WITH NEW OI	RDER
021E A5 21	LDA OLD+1 FIRST CARD			
0220 85 4A	STA LAST	; SUBR	OUTINE SCAN	
0222 AO OD	LDY E13	026A AZ OD SCAN	LDX E13	
0224 B9 20 00 LOOP	LDA OLD Y DO NEXT CARD	026C D5 2E SCAN1	CMP NEW, X LOOK FOR A	
0227 20 64 02	TCD CCAN	026E FO 03	BEQ RETN IN ARRAY NEW	
0723 86 49	CTY DOCH CAUE DOCTOTON	0270 CA	DEX	
02224 00 48	SIA FUSIN SAVE FUSITION	0271 DO F9	BNE SCAN1	
022C A5 4A	LDA LAST	0273 60	RTS DOSTRION TO Y	
022E 20 6A 02	JSR SCAN		POSITION IS X	
0231 8A	TXA	· · · ·	END	
0232 38	SEC		. 5145	
	Fig. 3. Card trick progr	ram for the 6502 micro		

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		3	MUSIC	PROGRAM	
0000 0003 0006 0007 0009	010001 110008 0A D300 C600	MUSIC LOOP	LXIB LXID LDAX OUT ADI	0100H 0800H B 0 0	;SET ADDRESS PT ;TEMPO FACTOR ;OUTPUT TO PORT ;TEST ACC.
000B 000E 000F 0010	CA1800 AF 1B BA	DELAY	JZ XRA DCX CMP	STOP A D D	;CLEAR ACC.
0011 0014 0015 0018	C20F00 03 C30300 76	STOP	JNZ INX JMP HLT	DELAY B LOOP	;POINT TO NEXT

Fig. 5. Program for the 8080 micro which, with the circuit of Fig. 4, plays tunes stored in memory

C8, C8, C4, C4, C2, C2, BC, BC, 08, BC, 08, BC, 08, BC, C2, C2, 08, C2

BC,BC,BC,08,08.

# Fig. 6. Data for a simple tune to illustrate how the frequency generator can be controlled by a micro

; 0030 E3 RST6 0031 6E	TWO BYTE JUMP XTHL MOV L,M	TOP OF STACK TO HL		; ;	TWO BYTE CONDI	ITIONAL JUMP
0032 E3 0033 C9 Fig. 7. (7a above, 7b implement two-byte	xtHL RET right) Routines	RESTORE HL, STACK ;JUMP TO DESTINATION	0038 E3 0039 23 003A E3 003B D8 003C E3 003D 2B 003E 6E 003F E3 • 0040 C9	RST7	XTHL INX H XTHL RC XTHL DCX H MOV L,M XTHL RET	;TOP OF STACK TO HL ;SKIP ADDRESS BYTE ;RESTORE HL ;RETURN IF NOT MET ;GET ADDRESS BACK ;GET JUMP ADDRESS ;L = DESTINATION ;RESTORE HL, STACK ;JUMP TO DESTINATION

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analogue converter. The output feeds the noninverting input of a 741 op-amp used as a buffer amplifier, and this should be calibrated **as** follows: first VR1 is used to give an output of OV at pin 6 when OOH is output to the port; then VR2 is used to adjust for an output of 3.6V when FFH is output to the port.

"A second 741 amplifier drives a voltagecontrolled oscillator; this is the oscillator section of a 565 phase-locked loop. VR3 is used as an overall pitch control and can be adjusted to provide a maximum frequency of over 6kHz. At a mid-range setting the circuit will cover the range 200Hz to 2400Hz with good linearity. Note that the 565 operates from  $\pm$ 10V supplies, derived from  $\pm$  15V with two zener diodes.

# MUSIC PROGRAM

"The circuit was used with the program shown in Fig. 5, which produces simple tunes. The values required to produce a musical scale are first determined, and then the tune is written as a sequence of these values, stored in memory starting at 0100H. Different note durations can be obtained by repeating the same note code, and blank intervals are obtained by any low-value code, such as 08H. A zero byte denotes the end of the tune.

"The program was run on a Limrose Electronics MPT8080 microtutor, and to enter data for the tune it is necessary to change the first instruction of the program to C3H (jump), and then single-step the first three bytes. After entering the data for the tune make sure that the next location contains OOH, and then change the first instruction back to 01H.

"The data in Fig. 6 are for a lively tune which should be fairly well known."

## TWO-BYTE JUMP FOR 8080

Jumps in the 8080, whether conditional or unconditional, are all three bytes long: one byte for the op-code, and a two-byte destination address. The following programs, submitted by *M. R. Reynolds* of Surrey, show how to implement two-byte jump instructions which can be used to save memory in a small system. The second byte of the instruction gives the low-order byte of the destination address.

"The program of Fig. 7a uses just four

bytes of memory to implement a two-byte unconditional jump instruction. It makes use of one of the eight restart instructions, which are one-byte subroutine calls to fixed addresses. They have the format '11AAA111' (binary) and cause the return address, the address after the restart instruction, to be pushed onto the stack, and control passed to the subroutine starting at 'OOAAAOOO' (binary). The program in Fig. 7a uses the F7 instruction which jumps to a subroutine at 0030H, and the routine simply substitutes the byte following the F7 instruction for the low-order byte of the return address. The return instruction then causes a transfer to that address. Note that this is not a relative jump, although one could be implemented with a longer subroutine.

"A conditional jump can be implemented as shown in Fig. 7b. The extra increment and decrement are needed to skip the address byte if the condition is not met. This example uses the FF instruction, which causes a jump to 0038H. The condition in the conditional return instruction is the inverse of the condition required for the overall jump; for example, RNZ would be required for a 'jump if zero' instruction."



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# **GIRL OF THE YEAR**

THE 1979 Girl Technician Engineer of the Year is Mrs Ann Cox-Horton, age 26, an electrical contracts engineer from Chertsey, Surrey. At a recent ceremony in London she was presented with the prize of £250 and an inscribed rose bowl by Sir Montague Finniston, FRS, Chairman of the Committee of Inquiry into the Engineering Profession.

Sponsored by The Caroline Haslett Memorial Trust and the IEETE, this award aims to focus attention on electrical and electronic engineering as a worthwhile professional career for women.

Ann Cox-Horton is employed by T Clarke & Co Limited, a London firm of electrical contractors. She is responsible for contracts valued at up to  $\pounds l_{\frac{1}{2}}$  million, including the work of up to 50 people.

The runner-up, Mrs Barbara Needham, 27, a senior research engineer from Harlow, Essex, received a special award of £150.

Barbara Needham works for Standard Telecommunication Laboratories Limited in Harlow, Essex.



Experimenter's design for equipping the standard oscilloscope with a charge storage facility so that pulses can be examined at leisure.

Whith the recent advent of microprocessor systems and the availability of cheap digital electronics, more home constructors are using these to replace conventional analogue circuitry. In the design, development and de-bugging of these circuits the need often arises to display a low frequency pulse train, or trains, on an oscilloscope for visual analysis. This is quite difficult on a normal oscilloscope because of the nature of the time base scan, especially if the pulses are narrow. Also charge storage and memory scopes tend to be prohibitively expensive for the amateur.

It was decided therefore to produce a unit which would display pulses of TTL level (+5V) on a normal oscilloscope with no modifications to the oscilloscope. This would include the facility for storing a train of pulses and freezing them on the screen for closer scrutiny. To extend its usefulness further it was designed to display four separate inputs on the oscilloscope as four separate traces.

### **BLOCK DIAGRAM**

Fig. 1 shows a block diagram of the complete unit. The four input signals are fed into a quad tri-state buffer the output of which is multiplexed by a four-way data selector. This is clocked by clock 1 via a divide by four counter and the resulting waveform is available from an output stage in a single wire format.

Outputs from the tri-state buffer are also routed to the memory storage section. This consists of a  $256 \times 4$  RAM which is controlled by a fast clock (clock 2) and an eight bit binary counter. Another clock (clock 3) operating at a slow rate steps another eight bit counter. The outputs of the counters are fed to a sixteen bit comparator which produces controlling pulses for the output trigger and the read/write phase of the RAM.

### **CIRCUIT DESCRIPTION**

The input channels (Fig. 2) are fed into a quad tri-state buffer IC1. This is controlled by a signal from the comparator circuitry which enables information to appear at the output



# SPECIFICATION

C.R. Harding

4 TTL compatible channels 3 ranges of sweep time (1) 0–1s (2) 0–10s (3) 0–100s

Manual trigger mode or continuous memory cycling Trigger output for oscilloscope with I.e.d. indicator Mains power supply

Frequency response using all channels

(1) Store mode—0–250Hz(2) Free run mode—0–10MHz

of the buffers with a high level. With no enable present the output of the buffers are high impedance and do not interfere with the read phase of the RAM. These outputs are then multiplexed by IC2, a four way data selector. This is controlled by a two stage counter (IC3) and a clock (IC4) which is formed from a Schmitt trigger and runs at approximately 500kHz.



Fig. 1 Block diagram



Fig. 2 Complete circuit

TR1 and its associated components form a simple three bit digital to analogue converter. The three inputs to this R2, R3 and R4 are connected to the signal output of IC2 and its two data selector input lines. Information on these last two lines effectively shifts the level of the output from TR1, and gives four distinct traces on the oscilloscope screen. TR1 also provides a buffered, low impedance output and is biased in the emitter follower mode by D2 which has its anode connected to chassis potential (as do the ground connections of the TTL i.c.s) and the cathode to power supply zero volts. This effectively produces a negative bias on the emitter of TR1 and eliminates the need for a negative supply rail.

# STORAGE

The storage section of the unit consists of a 256 x 4 RAM IC13, and this is also connected to the outputs of the tristate buffers. The address lines on the RAM are controlled by an eight bit counter IC14 and IC15. These are clocked by a counter running at 256 kHz.

These address lines are also fed into a sixteen bit comparator (IC9 and IC10).

The other eight inputs of the comparator are provided by the outputs of another eight bit counter (IC7 and IC8) which is clocked by a calibrated oscillator. This is the sweep oscillator which provides the scanning times.

Thus the signals from the two eight bit counters are compared and IC11 produces a pulse only when the outputs from these are coincidental. This pulse is then used to produce a write instruction to the RAM which then stores input data.

The frequency of the slow clock (clock 3) is set to values of 256Hz, 25-6Hz to give variation in storage rate. Once the waveform has been stored, at an appropriate scanning rate, the output scanning rate can be increased to expand out the trace to see more detail. Triggering in the unit is provided by IC5 and IC6. This is available in three modes:

- 1. Single shot
- 2. External or internal trigger
- 3. Continuous run

In the first mode the monostable IC12 gives a pulse from push button switch S6 from a manual trigger when desired. In the external or internal trigger mode triggering is achieved from an external pulse or from input channel 1. An I.e.d. is used to indicate correct triggering.

S4 selects the continuous triggering mode which causes the unit to cycle information into the memory continuously. The output trigger pulse is available through S3 via SK6 and is of TTL level.

# **POWER SUPPLY**

This is a conventional transformer derived mains power supply with a full wave diode bridge rectifier.

Zener dioder D1 provides the reference voltage and TR1 supplies the necessary current, which is approximately 300mA, and should have a heatsink attached.

## CONSTRUCTION

The prototype was built on two pieces of Veroboard, which were stacked horizontally, one containing the memory and address dividers and the other the oscillators, trigger circuit and power supply. However, the layout of these is not critical and everything could be accommodated on one board.

A case was made for the unit out of aluminium but proprietary cases can be used.

The prototype was made compatible in appearance with

# COMPONENTS

### Resistors

1k2
1k
2k
4k7
1k
470
270
33k
470
1k
1 k
1k
1k
1k
910k
220
5% carbon

Capacitors		
C1	4n7	mylar
C2	4n7	mylar
C3	1n	mylar
C4	330n	carbonate
C5	470µ	10V elect
C6	1000µ	10V elect
C7	100n	mylar
C8	100n	mylar

# **Integrated Circuits**

IC1	74126	1C9	7486
1C2	74153	IC10	7486
1C3	7474	IC11	7430
iC4	7413	IC12	74121
1C5	7400	IC13	2112
1C6	7474	IC14	7493
IC7	7493	IC15	7493
IC8	7493	IC16	556

Transistors

TR1	
TR2	

BC108 2N3053

### **Diodes** D1 D2-D6

R7198 -	- 0	.2400	m
1N4001	(5	off)	

Potentiometer	rs
ŴR1	
100 101	

**S1** 

**S**2

**S**3

**S**4

# 20k 100k (3 off)

### Switches Mains on/off double pole Two pole four way Single pole change-over Single pole on-off S5-S6 Press to make

V Zener



Fig. 3 Component layout for prototype boards. Since the unit is primarily a piece of experimenters test gear which will readily translate for stripboard assembly no cutting or interwiring details are given just a guide for component placement the author's oscilloscope with the front panel containing input sockets and selection switches. The back panel houses the output and trigger sockets and mains input lead switch and fuse.

# SETTING UP AND CALIBRATION

For accurate calibration a digital frequency meter should be used, however, a signal generator can be used for frequency comparison.

The following adjustments should be made:

Adjust	S2 range	Measure	Measurement pins
VR1		256 kHz	IC16/5
VR2	1s =	256Hz	IC16/9
VR3	10s	25-6Hz	IC16/9
VR4	100s	2.56Hz (390ms)	IC16/9

# **USING THE UNIT**

The unit should be connected to the Y input of one of the oscilloscope's channels (or channel) and the external trigger of the oscilloscope connected to the trigger output of the unit. The Y gain of the oscilloscope should be set to approximately 0.5 volts per centimetre and the timebase to 100 milliseconds per centimetre.

Four traces should appear on the screen with random information on each one. This can be cleared by pressing the sweep trigger button leaving four straight lines.

Connect a low frequency pulse generator (1Hz approximately) to the input (channel 1) and switch the unit to the 10 second sweep range. A trace of 1Hz pulses will slowly be produced on the top trace from left to right and halt when the scan reaches the right-hand margin of the screen.

The input can now be removed and the waveform will remain until the power is removed to the unit.

The unit can also be used in continuous mode where the memory will constantly refresh at the end of each scan. Also the trace can be returned to the time origin by use of the sweep trigger button.

### LIMITATIONS

When using the unit care should be taken not to exceed higher frequencies than the maximum stated.

It is useful to note that the trace is actually broken up into 256 sections and at for example 1 second sweep rate the minimum pulse duration that can be recorded is 4ms in 5. If a too high frequency is fed in, depending on its harmonic relationship with the number of bits a lower frequency is produced on the screen, therefore it is useful to know the approximate value of the frequency of the waveform to be measured.

Since the unit writes in all four channels simultaneously one waveform cannot be served while 3 new ones are recorded.

# MODIFICATIONS

Although designed for TTL level signals, by using a simple CMOS buffer on the input the usefulness is extended by increasing the input impedance and the level of input. Longer sweep times can be produced by using more ranges with extra capacitance on clock 3. As the sweep time is 256 times longer than the time interval of the 556, sweep periods of up to 100,000 seconds are feasible.

A selection of read original circuit ideas should be emphasi that these designs have not been proven by us. They will at any rate stimulate further thought.

Why not submit your idea? Any idea published will be awarded payment according to its merits. Articles submitted for

Articles submitted for publication should conform to the usual practices of this journal, e.g. with regard to abbreviations and circuit symbols. Diagrams should be on separate sheets, not inserted in the text.

Each idea submitted must be accompanied by a declaration to the effect that it is the original work of the undersigned, and that it has not been accepted for publication elsewhere.

# TAPE/SLIDE SYNC

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SHOWN are circuits for a Tape/Slide Synchroniser. First of all the commentary is recorded onto the tape in the normal way and whenever it is necessary for the slide projector to advance one slide, SI is pressed which records a burst of ultrasonic sound onto the tape. When the recorder is played back (connected to the projector via the 'tuned amplifier' Fig. 2) the relay closes and advances the slide projector one slide every time an ultrasonic sound is detected.

M

The oscillator should be tuned to the right frequency simply by connecting the output to the input of the tuned amplifier, and adjusting VR1 until RLA1 closes. The circuit only amplifies frequencies of about 48.2 kHz.

The output of the 741 is amplified by TR1 and 2 which switches on the relay. The circuit works well despite the fact that the recorders response is very low at 48.2kHz. A small mono recorder works better than an expensive stereo tape deck because the latter usually have bias oscillators running at about 60-90kHz which might beat with the synchronisers' output.

> R.N. Johnson. Coulsdon Surrey





# VOLTAGE SENSITIVE RELAY

The circuit diagram as shown right is an electronic relay with two wires on the input side and three wires at the output. The input leads are connected to the voltage to be sensed. Its range is from 10V a.c./d.c. to 20V a.c./d.c. The relay is a 6 volt/30 ohm coil type with changeover contacts rated for 5A/230V a.c.

The heart of the control system is a general purpose operational amplifier type 741. The control voltage is rectified by diode D1 and filtered and stored by capacitor C1. The non-inverting input (pin 3) is fed with a Zener regulated fixed potential of 3.9 volts, whereas the inverting input (pin 2) is variable and can be set by a preset potentiometer VR1 to any desired voltage. It is only by adjustment of this pot that a control point is achieved.

The output of the 741 changes state with input potential difference of as low as 1 millivolt. The positive going output at pin 6 biases a switching transistor through a diode and 10 kilohm resistor. The transistor in turn energises a relay whose normally open and normally closed contacts could be used in a number of applications. The differential at which the relay is desired to be operated is provided by positive feedback to non-inverting input, by a 10k preset pot VR2 in parallel with C2.

Any desired hysteresis can be set by VR2. An electrolytic is used at the base of switching transistor TR1 to avoid chattering of the relay on a.c. operation.



### Automatic Temperature controller

This application is shown below. Here a slight modification in the control circuit of the VSR is needed. R1 is removed and a thermistor with long leads substituted. The thermistor is placed near the heating source. Its resistance will change with heat resulting in control initiation. The preset potentiometer VR1 now can be set for the desired temperature. The n.c. contacts of the relay can be used for opening the heater circuit when desired temperature has reached. In this case the input supply zevec to the VSR is obtained by a low voltage transformer and regulated by a Zener. *Twilight switch* 

Alternative connections to the VSR (shown in outline) provide a light switch. Here R1 is replaced by an l.d.r. The resistance of this increases with a decrease in ambient light and thus initiates the switching operation. The n.o. (normally open) contacts are connected in series with the load and supply. Thus the lamp load lights up on fall of ambient light at preset value.



WHEN a precise voltage source is required for a particular application, it is common practice to modify the output voltage of a voltage regulator by "jackingup" the common. i.e. raising its potential above ground. This useful method has its disadvantages. In the event of a shortcircuit the common would become reversed biased and the regulator would loose its protection, thus resulting in its destruction.

In the circuit shown the germanium diode D1 prevents the common becoming more than 0.2 volt reverse biased under short circuit conditions and thereby protecting the regulator from damage.

The addition of C2 is to ensure stability. Diodes D2 and D3 (as an example) raise the output voltage by about 1.3 volts.

J.A. Barrow Rugby Warwickshire

# 'JACKED UP' REGULATOR



WAVEFORM CONVERTOR FOR MINISONIC



"HIS circuit will convert an input of sawtooth shape into a triangle shape and then convert the triangle waveform into a synthesised sine waveform. IC1 amplifies the input signal to a level of 15 V peak to peak. The value of R1 should be chosen according to the input level. R1 should in fact be chosen as (100 x peakto-peak input voltage) kilohms. For Minisonics 1 and 2, R1 should be 39 kilohms, and 100 kilohms respectively. IC2 is a differential amplifier which inverts the positive going half cycle with respect to the negative going half cycle. With a certain amount of smoothing from C4 this produces an output of about 7.2 V peakto-peak which is triangular in shape. VR1 should be adjusted to give a triangle output of 1V peak-to-peak for Minisonic 2. Of course the level can be any value up to 7.2 V depending on what suits the constructor's application.

The triangle output is then fed into IC3 which is another differential amplifier and identical to IC2's circuitry. This produces an output of about 3.5 V peak-to-peak which is triangular in shape and twice the frequency of the input triangle waveform. This double frequency triangle wave controls the amount of attentuation in the voltage controlled attentuator built around TR1 and IC4.

As the input triangle wave approaches either its positive or negative peaks the gain of the output stage gradually decreases by the action of the double frequency wave at the gate of the f.e.t. TR1. This has the effect of rounding off the peaks. The shape produced is a very good approximation of a sine wave.

Setting up is quite simple. First the wiper of VR2 must be taken to its 0V end. VR3 is now adjusted to give an output level of around 500 mV r.m.s. VR2 can

now be adjusted until the best approximation of a sine wave is produced. An oscilloscope would be useful here but I have found that the adjustment can be made fairly accurately by ear. With the output connected to an audio amplifier VR2 should be adjusted until the sound contains fewest harmonics. Finally VR3 should be readjusted to give an output of about 350 mV r.m.s. (1V peak-to-peak).

The circuit can be used as a triangle to sine convertor quite simply by leaving out IC2 and its associated circuitry.

P.G. Ludgate High Wycombe, Bucks.

# CAR CASSETTE POWER SUPPLY



This unit enables a 6V cassette player or recorder to be powered from the 12V car battery, while drawing only 100mA in excess of the cassette player's consumption. Short-circuiting the output of the unit does not damage the circuitry, and only 2A flows, whereas the unit can provide 6V at up to 800mA.

R1 limits the short-circuit current to about 2A, and reduces the power dissipation of the series regulator transistor TR1, which acts as an emitter follower with the base voltage provided by R2/D1. (Note that D1 must be rated at 1W or greater.)

The complete unit fits easily into the smallest size of diecast case, which can also act as a heatsink for TR1.

N. Riddiford North Shields Tyne & Wear.









# **RHYTHM CODE GENERATOR**

The circuit shown was used to generate the 4 bit BCD rhythm select code required by the rhythm generator i.e. M252. It could also be used in any application that requires the generation of a 4 bit BCD word, for example, a hexadecimal keyboard.

If a pushbutton is pressed, the two SN74148 priority encoders code the 16 inputs to a 4 bit BCD word. This word is latched into the SN74175 quad latch by the combined GS outputs (pins 14) of the priority encoders. Capacitor C1 is used to show the edge of the latching signal so that latching takes place when the input data is valid.

The outputs of the quad latch can be decoded back to 16 bits by a SN74154 and the outputs used to drive l.e.d.s to give a visual indication of the button pressed, or as in this example the rhythm selected. E.J. Weremiuk, Branthere

Brantham, Essex.



# AUTOMATIC CAR AERIAL CONTROL

N February 1977, a circuit was published in "Ingenuity Unlimited" for the automatic control of an electric car aerial. The circuit described here is an alternative approach to the problem. The prototype has been in trouble-free use for over four years. It may be operated by the radio on/off switch so that the aerial is only raised when needed, or, if preferred, by the ignition switch. No additional switch is necessary. The device may be left permanently connected to the car battery, since the leakage current when the radio is switched off is very low.

The main control circuit may be used either by connecting terminal **B** to the radio on/off switch (or the ignition switch) and shorting C and D, or by shorting A and B and connecting C to an additional control circuit. The main circuit contains



two relays, each with two changeover contacts. When the radio is turned on (or the ignition if preferred) RLA switches on, the motor starts to wind up the aerial, C1 charges up and, after a delay (adjusted by the preset VR2), RLB switches on and stops the motor. When RLA switches off, the aerial starts to wind down, C1 discharges and, after a delay (adjusted independently by VR2), RLB 2 switches off and again stops the motor. VR1 and VR2 are adjusted so that the aerial winds completely up and down, the motor making about two revolutions against the slipping clutch for good measure.

If RLB has two changeover contacts, the spare set may be used to mute the radio whilst the aerial is winding up, to prevent crackling from the loudspeaker, e.g. by shorting the volume control. If the radio has a tape recorder socket through which the audio signal passes by means of a shorting plug, that can be used to make the connections to the muting contacts without disturbing the radio internally. A stereo radio would, of course, need a more complex system, or extra contacts in the relay.

D. A. Petty, Aylesbury, Bucks. THERE are many published circuits which enable two lamps to be controlled along two wires giving provision for either lamp or both lamps to be illuminated at any one time.

The circuit described below enables three lamps to be controlled along two wires enabling any one lamp to be illuminated at any one time. It was originally designed for a busy office to convey the instructions of 'Engaged', 'Wait' and 'Enter'.

The circuit is powered by 12 volts a.c. which is derived from the mains. The three lamps are controlled by S1 which gives the four possible operations. In position 1 no lamps are on, since no power is being applied to the wires a and b. In position 2, the alternating current from the transformer is half wave rectified by D1, making wire a positive with respect to b. TR1 and its associated components respond to this and so LP1 is illuminated. TR1 is prevented from conducting when S1 is in the a.c. position (position 4) by D4, R1, and D8. These ensure that C1 is charged by the negative half cycles so that TR1 will be made non-conducting.

In position 3 the alternating current is again half wave rectified, but this time wire a is negative with respect to wire b. The circuitry for LP2 is the same as that for LP1 except that it is connected the other way round to the wires a and b.

In position 4 of S1, an alternating voltage is applied to a and b. The circuitry for LP3 works in the following way; with S1 in position 2 (wire a positive) TR3 is conducting so keeping TR4 nonconducting. In position 3 (wire a negative), D7 is reversed biased so that LP3 is again



not illuminated. With an alternating voltage, the negative half cycles reduce the voltage across C3 to a sufficiently low level that TR3 is non-conducting. TR4 becomes conducting so allowing LP3 to light.

each lamp circuit offers a small amount of smoothing to the half rectified a.c., producing approximately 10 volts d.c. across each lamp when alight.

> J. P. Kemp, Kings Norton, Birmingham.

The 200uF electrolytic capacitors in



SCOPE CALIBRATOR

This simple circuit can be used to check oscilloscope Y-amplifier Volts/Cm calibration accuracy, and to set the frequency compensation trimmer R4 on a high input impedance oscilloscope probe.

IC la and IC lb form a simple multivibrator type circuit, and IC lc acts as a pulse shaper. (The unused gate, IC ld, is connected so as to minimise battery current consumption.) The output is an excellent square-wave having fast rise and fall times with flat top and bottom base lines. Frequency is about lkHz. The output feeds the simple ladder attenuator (two per cent resistors should be used if high attenuation accuracy is required). VR1 should be set to give 2.0Vat point X with respect to 0V.

D1 provides a stabilised 5V for the IC so that the ladder network receives a constant level square wave. Battery current drain is about 25mA.

> A. Andrews, Brighton.





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HY30	$\begin{array}{c} \textbf{15 W} \\ \textbf{into 8 } \Omega \end{array}$	0.02%	80dB	-20 -0- +20	105×50×25	155	<b>£6.34</b> + 95p
HY50	30 W into 8 Ω	0.02%	90dB	-25 -0 +25	105x50x25	155	<b>£7.24</b> + £1.09
HY120	60 W into 8 Ω	0.01%	100dB	-35 -0- +35	114x50x85	575	<b>£15.20</b> + £2.28
HY200	120 W into 8 Ω	0.01%	100dB	-45 -0- +45	114×50×85	575	<b>£18.44</b> + £2.77
HY400	$\frac{240}{100} \text{W}$	0.01%	100dB	-45 -0- +45	114×100×85	1.15Kg	£27.68 + £4.15

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ACY17	0.98	BD182	1.36	0A200	0.10	2G306	1.27	7433	0.41
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AFZ11	3.16	BF179	0.29	0036	1.73	2N1308	0.63	7476	0.46
AFZ12	3.16	BF180	0.35	0C41	0.92	2N1309	0.63	7480	0.63
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SAVVOZ	0.00	8F330	0.35	00122	1.73	2N2905	0.29	74111	0.81
BAX16	0.10	8F338	0.36	OC123	2.02	2N2906	0.24	74116	2.02
BC107	0.14	BFS21	2.56	00139	3.16	2N2907	0.24	74118	1.73
80109	0.15	BFS61	0.23	00141	3.74	2N2925	0.25	74120	0.95
8C113	0.14	8FS98	0.23	00170	1.15	2N2926	0.16	74121	0.46
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BC116	0.17	BFX84	0.25	OC201	2.02	2N3055	0.81	74125	0.63
BC117	0.20	8FX85	0.26	0C202	2.02	2N3440	0.69	74126	0.63
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BC126	0.23	BFY50	0.30	0C205	2.88		4 70	74136	0.63
BC135	0.16	BFY51	0.30	0C206	2.02	2N3614	0.13	74141	2.65
BC130	0.17	8FY64	0.30	OCP71	1.44	2N3703	0.15	74143	2.88
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BC148 BC149	0.10	BSX19	0.23	R2009	2.59	2N3706	0.15	74145	2.30
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BC184	0.13	Jeries		T1P3055	0.64	2N3905	0.15	74176	1.26
BC212	0.15	CRS1/40	0.69	T1543	0.52	2N3906	0.15	74178	1.44
8C213	0.17	CRS3/40	1.04	25140	0.29	2N4058	0.12	74179	1-32
BC237	0.10	GEX66	1.73	ZS178	0.62	2N4060	0.14	74190	1.73
BC238	0.14	GEX541	4.60	ZS271	0.65	2N4061	0.14	74191	1.55
BC301 BC303	0.38	GJSM	0.86	ZTX107	0.13	2N4002	0.17	74192	1.55
BC307	0.12	GL7M	0.86	ZTX108	0.12	2N4126	0.17	74194	1.44
BC308	0.12	GM0378A	2.02	ZTX 109	0.14	2N4286	0.23	74195	1.38
BC32B	0.21	MJE340	0.92	ZTX301	0.15	2N4289	0.28	74197	1.26
BC337	0.21	MJE370	1.35	ZTX302	0.17	2N5457	0.40	74198	2.59
80338	1.15	MJE371	0.60	77X304	0.22	2N5459	0-40	74199 76013N	2.02
8CY31	1.15	MJE521	0.63	ZTX311	0.14				
BCY32	1.15	MJE2955	1.44	ZTX314	0.23	INTEGR	ATCH		
BCY34	1.04	MPF102	0.35	ZTX501	0.15	CIRCUI	TS		
BCY39	3.45	MPF103	0.35	ZTX502	0.18	7400	0.18	Plugs in s	ocket
BCY40	1.15	MPF104	0.35	ZTX503	0.20	7401	0.18	- low prot	nile
8CY43	0.29	MPSA06	0.28	ZTX531	0.23	7403	0.18	14 pin Di	L 0.1
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7ENER	SISCEPTION VILC	LINCAD	4029	760	7493	350	BC212/3 120 7	TX301 180
DIDDER	CAD (BEN)	CIRCINTO .	4020	601	7494	67.0	00214 12-7	77202 700
UIUUES	CAP (ZDV)	CINCUITS	4030 (	oup	7434	97 P	DUZIA IZPIZ	14302 2001
(400 mW)	luF to 50uF 6p	709 40p	4035 10	07pį	1495	400	BU2618 14p 4	IA3U3 2401
2 71/	68uF. 100uF 8p	710-14 330	4041	750	7496	56p	BC461 40a Z	TX304 Z7p
2.7V to 33V	150uE 9r	741.8 220	4042	580	74100	90o	BCA77/8 27m Z	TX311 190
Re.	220.5 10	343.14 40	4042	00-1	74105	130	00470 27-77	TY341 720
op	22007 100	747-14 40p	4043 0	000	74103	ac a	064/8 2/4 2	
VERD	4/Uur 1.Jp	748-8 44p	4044 8	04p	74107	Zop	BL54 //8 14p 4	1400 100
VENO	1000uF 22p	CA3018 70e	4047 8	87p	74109	44p	BC549 14p 2	(IXbUI 16p)
BOARDS		CA3028A 85n	4048 5	550	74110	40p	BC557/8 15g Z	TX502 Z1p
(0.1" Cooper)		CA3046 70e	4049	150	74121	260	80559 158 7	TX503 170
a Fil Sura	AAAAAAA	CA2054 70µ	4050	15-1	74122	40.0	0CV10 18- 7	TY604 280
Z-5"X5" 52p	MAINS	CA3034 70p	4030	3.2b	74122	4 up	DUT/U TOP 2	11004 200 J
3-75"×5"	THANSFORMERS	LA3U8U /5p	4000	190	74123	40b	BL1/1/2 180 4	CM030 33h
67-	9-0~9V	CA3130 90p	4069 1	18p	/4125	37p	8D115 58p 2	2N69/ 25p
0ZP	100mA 140p	CA3140 45p	4070/1 1	80	74126	37p	8D131 to 2	2N698 35p
	15-0-15	LF351N 65m	4072/3 1	80	74132	480	B0140 42p 2	2N706 14p
RESISTORS	200mA 160m	15366N 850	4081/2 1	8.	74141	60n	BE180 30n 2	N914 20n
(1W F12)	cooming 180h	1442014N 12-	4510 1	221	74145	660	DEIDA/E 7Eg 7	N018 350
10 1		LMJUTAN JZP	4510 8	r sp	74150	30,	DF104/5 250 2	111121 20-
10 onms 1 -5p		LM308N 60p	4511 5	99b	74150	rop.	BF194/5 12p 2	ZNIISI ZUP
to 10 Mohms	BRIDGE	LM318N 200p	4516 9	5p	74151	460	BF196/7 12p 2	der Zneim
	DECTIFICAC	LM324N 74n	4518 7	72p	74153	43p	BF244B 35p 2	2N1303 40p
DOFOFTO	NECHIPIENS	1M339N 60m	4520 0	140	74154	90p	BF259 40n 2	N2222A 250
PRESEIS	TA/50V 22p	1M249N 80p	4528 0	10.	74155/6	460	8F830 32n 2	N2369 170
(0 -15 Watt)	1A/400V 34p	LINI3401 900	4950 3	246	74157	430	01030 320 2	1412484 300
100 ohme	2A/50V 400	LM3//N 1/5p			74100/1	64-	Drn/9 320 2	
TUU UIIRIS	24/40 fiv 550	TW3RON 30b			74100/1	040	BFX29 250 2	112040 05p
to 2 Mohms Bp	The react make	LM381N 140p	771		14162/3	04p	BFX84 Z5p 2	INZOU4 ZJp
		LM382N 130p	116		74164/5	78p	BFX87/8 25p 2	2NZ905 Z3p
		LM1310N150n	7400 1	1 3 p	74166	85p	BFY50 22p 2	2N2906 Z0p
POTENII-	VOLTAGE	LM3900N 55n	7401/2 1	13ø	74173	770	BEY51/2 228 2	2N2907 200
OMETERS	REGULATORS	IM3000N 70a	7403/4 1	13p	74174	750	BRY19 60n 2	N29266 11n
(114/ contract	7805 700	MC140C0 PE-	7405 1	130	74175	60.	PU1209 210- 2	N 2053 200
(#w caroon)	7012/15 700	MCI430r 63p	7406/7 2	740	74170	CAL	DU200 2100 2	A13055 E0-
4.7 Kohm to	7012/13 700	NE031 140p	7408/9 1	1 16	74170	0-4p	W15222 110b 5	113034 aup
2.2 Mahm	/818/24 /Up	NE555 25p	7410 1		14111	65p	MJE34U /Up 2	(N3055 500
Z.Z. WOMM	7905 90p	NE556 60p	7419	30	74180	57p	MJE2955 110p] 2	2N3442 140p
Log and Linear	7912/15 90p	NE566 140p	7411	op	74181	99p	MJE3055 850 2	2N3702 to [
280	7918/24 90p	TBA641A 200n	7412 1	15p	74182	570	MPF102/3 40p 2	2N3711 11p
		TRA6418 200m	7413 2	27p	74190	750	MPF104/5 400 2	N3772 1500
		T0A000 760	7414 3	31 p	74191	700	MP\$106 50e 2	N3773 750n
CERAMIC	APTA/DISPLAY	TDA0000 / 50	7416/7 2	250	7/102	660	M06406 36- 3	M2910 27
040	0PD12 50-	TDAOTUS TTUP	7420 1	140	74102	64-	MOCATE 20012	N3030 40-
LAP	MAN 22 800	ZN414 100p	7421/2 1	17.	74193	040 J	MP5A58 200 2	10020 400
(50V)	MAN/Z TTUP	ZN1034 200p	7427 2	0.1	74195	9/p	MPS006 61p 2	2N3823 /Up
2205 10 A705	MAN /4 110p		7427 2	cup	74197 1	00p	0C35 92p 2	2N3866 90p
ZZpr to 47m	-125" & -2"		1420 2	(ob	74199 1	120p ]	T1P298 48p 2	2N3903 10p
2p	LEOs:		7430 1	4p			TIP308 48n 2	N3904 10p
	Red 10n		7432 2	20a			TIP11/2 40a 2	N3905 10a
0.011	Green 140	CMOS	7433 2	240	TRANSIST	TIRS	TID TRO	N3906 100
POLY-	Valleya Sa	4000 180	7437/8 2	Onl	AC126/7	230	IIF33L BUD 2	AU4027 45-
STYRENE	TRUDAA 144b	4001/2 190	7440 1	2	AC1 20	220	TIP34A 9Up	2144037 450
CAD		4000 30	7441	Su .	AG128	ZSP	TIP358 240p 2	2N4058 140
UNF	330010	4000 /Up	7441 3	ab	AL170	ZJP	TIP36B 280p 2	2N4U59 14p
(E12 50V)	DIODES	4007 18p	7442 5	pip	AC187/8	23p	TIP41A 60n 2	2N4060 140
10nEta 1nE	0A4/ 8p	4008 84p	7443/4 8	30p'	A0149	70p	TIP3055 550 7	2N5457 400
ropt to the	0A91 8p	4009 34g	7445 7	15p	A0161/2	400	2TV107 120 2	DUEAED ADD
50	IN4148 40	4010 420	7446 6	35n	AF124	450	2774400 100 2	DNC4E0 90
	IN916 5n	4011/2 1Re	7447 5	661	AC120	40-	ZIX109 130 2	2115459 350
	IN4002 40	4013 40-	7448 6	201	AF330	470	ZIX300	Mauzz the
POLYESTER	INAODE E.	4014 400	7440 0	ZPI	AFZ19	47p	DDICEC VAT	INCLUCING
CAP	IN4005 Op	4014 850	/450/1 1	3p	BC107	10p	PRICES VAL	INCLUSIVE
	IN 5400 13p	4015 70p	1453/4 1	13p	BC108/9	10p	A00 20- 50	100.00
Inr to U-JuF	1N54D4 16p	4016 40p	7460 1	3p	BC147/8	10p	HUU SUP FL	unrar.
50	Aug. 10	4017 570	7470 2	80	8C149	100		and the second second
15 22		4018 68n	7472 2	210	80157/8	120	DELTA	TECU
.13.22	DIL SOCKETS	4019 45-	7473 3	Rol	00160	120	DELIA	
·33uF 6p	Ania 11a	4020 90-	7474 9	op	00103	1 ZP		
4711E .6811E	14 oin 120	4020 90p	1414 2	44P	BL16/	140	CO MAYLO	
	10 -in 13p	4021 85p	14/5 3	54p	801690	13p	OZ NAYLO	R KUAU
10p	10 pin 14 p	4022 82p	7476 3	10p	8C173	8p		
1uF 12n	18 pin 18 p	4023 180	7480 3	32pl	BC177/B	180	TONOON N	120 OHN
2.2.5 20.	22 pin 22p	4024 580	7486 2	250	BC179	200		
2. ZUP ZUP	24 pin 240	4025 180	7490 3	16.	BC182/2	120		CD ONLY
3-3ul 26	28 nin 28n	4027 35-	7491 6	550	DC1D4	120		CH UNTI
4.7uF 300	40 pin 40-	4020 350	7431 5	102	06184	1ZP		4
- Jun 300	-0 pm 40p	4028 6Up	149Z 4	+Up	BC209	130	SAE for com	plete list.

FL	AD/	AR	TRA	NS	FORM	<b>IE</b>	RS	
				ARY	0-240V	50H	z	
SEN	SEND FOR OUR TRANSFORMER CATALOGUE PRICE 40p							
Type Vol	Itage Current	£ p/p	Туре	Voltage	Current	£	p/p	
06FE06 08FE06 12FE06 20FE06 50FE06 60FE06	5+6 0.5A EACH 5+6 0.6A EACH 5+6 1.6A EACH 5+6 1.6A EACH 5+6 3A EACH 6+6 4A EACH	1.82 60p 2.19 60p 2.43 72p 3.06 84p 3.74 84p 4.58 102p	60FE24 80FE24 50FE28 60FE28 80FE28	24+24 24+24 28+28 28+28 28+28 28+28	1-2A EACH 1-5A EACH 0-75A EACH 1-1A EACH 1-4A EACH	4.58 5.66 3.74 4.58 5.66	102p 120p 84p 102p 120p	
06FE09 08FE09 12FE09 20FE09 50FE09	0 3A EACH 9+9 0 5A EACH 9+9 0 75A EACH 9+9 1A EACH 9+9 2 5A EACH	1.82 60p 2.19 60p 2.43 72p 3.06 84p 3.74 84p	20FE30 50FE30 60FE30 80FE30	30+30 30+30 30+30 30+30 MULTI	0-35A EACH 0-75A EACH 1A EACH 1-2A EACH TAP RANGE	3.06 3.74 4.58 5.66	84p 84p 102p 120p	
60FE09 9	9+9 3A EACH	4-58 102p	VOLTAG	ES AVAIL	ABLE 3. 4, 5,	6, 8, 9,	10,	
06FE12 12 08FE12 12 12FE12 12 20FE12 12 50FE12 12 60FE12 12	2+12 0.25A EACH 2+12 0.3A EACH 2+12 0.5A EACH 2+12 0.8A EACH 2+12 1.8A EACH 2+12 2.5A EACH	1 82 60p 2 19 60p 2 43 72p 3 06 84p 3 74 84p 4 58 102p	30FE30 60FE36 80FE36		1A 2A 3A AP SECOND	4.00 4.80 5.88	84p 102p 120p	
80FE12 12 06FE15 11 08FE15 11 12FE15 11 20FE15 11 50FE15 11	2+12         3A EACH           5+15         0-2A EACH           5+15         0-25A EACH           5+15         0-4A EACH           5+15         0-6A EACH           5+15         1-5A EACH           5+15         0-6A EACH           5+15         0-6A EACH	1.82 60p 2.19 60p 2.43 72p 3.06 84p 3.74 84p	06FE30 08FE40 12FE50 20FE80 50FE80 60FE100	6-0-6 9-0-9 12-0-12 20-0-20 20-0-20 28-0-28	1-80A 1A 1A 1A 2A 2-2A	1.80 2.16 2.40 3.00 3.70 4.50	80p 60p 72p 84p 84p 102p	
80FE15 11 06FE20 20 12FE20 20 20FE20 20 50FE20 20 60FE20 20 80FE20 20	5+15 3A EACH 0+20 0-15A EACH 0+20 0-25A EACH 0+20 0-5A EACH 0+20 1-2A EACH 0+20 1-2A EACH 0+20 2A EACH	5.66 120p 2.43 72p 3.06 84p 3.74 84p 4.58 102p 5.66 120p	80FE70 90FE50 90FE80 100FE26 100FE28 100FE30 100FE36	24-0-24 15-0-15 30-0-30 26-0-26 28-0-28 30-0-30 36-0-36	3A 6A 3A 3-5A 3-5A 3-5A 3A 3A	5.66 5.80 5.80 6.05 6.05 6.05 6.05 6.05	120p 120p 120p 138p 138p 138p 138p	
CHAF 48FE12 0- 66FE12 0- 70FE12 0- 90FE12 0- 12FE24 24	IGER TRANSFOR           -6-12         4A           -6-12         5A           -6-12         6A           -6-12         8A           -4-24         0-2A EACH	MERS 4-58   102p 5-30   102p 5-66   120p 6-75   138p 2-43   72p	150FE15 150FE26 150FE30 150FE36 150FE42 250FE42 250FE30 250FE42	15-0-15 26-0-26 30-0-30 36-0-36 42-0-42 28-0-28 30-0-30 42-0-42	7A 5A 4A 3A 3A 7A 5-5A	7.47 7.47 7.47 7.47 7.47 8.60 8.60 8.60 8.60	150p 150p 150p 150p 150p 150p 175p 175p	
FLADAR P.O. BOX WESTCLI ESSEX. O	ELECTRIC 19 IFF-ON-SEA 1702-613314	TRADE	ENQUIRIES	PAYN C.W.C Posta All Pr	AENT TERM D. Cheques, Il Orders ices include	IS: e 15%	V.A.T.	



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