### PRACTICAL ELECTRONICS NOVEMBER 1979 55p

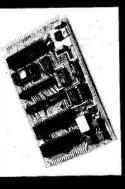




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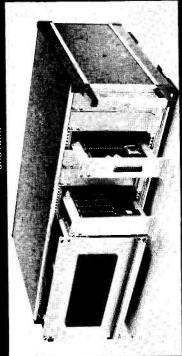


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# VOLUME 15 NO. 11 NOVEMBER 1979

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#### OUR DECEMBER ISSUE WILL BE ON SALE FRIDAY, 9 NOVEMBER 1979

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400V: 1nF, 1n5, 2n2, 3n3, 4n7, 6n8, 10n, 15n, 9p; 18n 10p; 22n, 33n 11p; 47n, 68n 14p; 100n 17p; 150n, 220n 24p; 330n, 470n 41p; 680n 45p; 1 <i>jr</i> 64p; 220 82p, 180V: 10nF, 12n, 39n, 100n, 150n, 220n 11p; 330n, 470n 19p; 680n, 1 <i>µ</i> ; 22p; 2: 2µF 32p; 4: 7µF 36p.	F139 35 BD137 36 WPF106 40 ZTX304 24 2N3708 11 F178 70 BD138 50 MPSA06 25 ZTX314 24 2N3709 11 C107 10 BD139 40 MPSA06 25 ZTX320 30 2N3710 16 SPECIA C107 12 BD140 36 MPSA12 42 ZTX326 40 2N3711 12	2 NL
10669¥; 10n, 15n 20p; 22n 22p; 47n 26p; 100n 38p; 470n 53p; 1μF 175p. POLYESTER RADIAL LEAD CAPACITORS: 2509; 10n 15n 22n 27n 5n; 33n 47n 68n 100n 27n; 15n 10m; 220n 10n 15n 22n 27n 5n; 33n 47n 68n 100n 27n; 15n 10m; 220n TRANSDUCERS	C1088 10 BD144 1981 MPSA55 25 ZX341 20 ZN3822 130 OFFER C1088 12 BD145 1981 MPSA56 25 ZX500 15 ZN3771 233 741 C108C 12 BD205 110 MPSU02 58 ZX501 15 ZN3772 195 555 C109 10 BD727 85 MPSU05 50 ZX502 19 ZN3772 288	17 20
100n, 15n, 22n, 27n 5p; 33n, 47n, 68n, 100n 7p; 150n 10p; 220n, TRANSDUCERS 330n 13p; 470n 17p; 680n 19p; 1y 22p; 1y5 30p; 2y2 34p. ELECTROLYTIC CAPACITORS: Axial lead type (Values are in µF). 500V; 10 40p; 47, 68p; 250V; 100 655; 63V; 0.47, 1.0, 1.5, 2.2, 2, 5, 3, 3, 4, 7, 6, 8, 10, 15, 22 8p; 32, 47, 50, 12p; 63, 100, 27p; 50V: 50, 100, 220 28p; 470 32p;	C109B 12 BD434 42 MPSU06 56 ZTX503 15 ZN3819 22 2708 6 C109C 12 BD517 65 MPSU52 65 ZTX504 25 ZN3820 45 C140 35 BD695A 65 MPSU55 55 ZTX531 25 ZN3823 95	49
100 500; 404; 22; 33µ <sup>2</sup> 89; 100 120; 2200; 3300 850; 4700 320; 350; 100 370; 330, 470 320; 1000 500; 250; 100 120; 2200; 3300 850; 4700 390; 350; 100 300; 370; 330, 470 320; 1000 500; 250; 10, 22, 47 60; 80, 100, 160 80; 220, 250 340; 470, 68 70; 250; 1000 270; 1500 300; 2200 450; 3300 620; 4700 740; 16V: 10, 40, 47, 68 70; 100, 125 80; 220, 330 140; 470 160; 1000, 1500 200; 2200 340; 10V: 100 60; 640	C143 30 BDY56 156 0C23 170 40250 85 2N3903 20 C147 8 BF115 34 0C26 170 40251 97 2N3904 18 C147B 10 BF167 30 0C28 150 40311 60 2N3905 18	
100, 125 8p; 220, 330 14p; 470 16p; 1000, 1500 20p; 2200 34p; 10V: 100 8p; 640 12p; 1000 14p. TAG-END TYPE: 450V: 100µF 180p: 70V: 4700 165p: 64V: 2500 98p; 3300 130p; 50V: 2200 99p; 3300 105p; 40V: 15.000 399p; 4700 120p; 4000 92p; 3300 93p; 2500	C148 8 BF177 24 0C35 130 40313 125 2N3906 17 C148B 10 BF178 25 0C36 130 40315 55 12N4037 52 C148C 10 BF179 30 0C41 48 40316 85 12N4058 17	
85p; 2200 85p; 2000 · 2000 · 2000 <b>120p; 30V</b> : 4700 90p; 25V: 6400 105p; 4700 85p; 3300 80p; 2200 60p.	C149C 10 BF194 12 0C43 55 40319 71 2N4062 17 CMUDS C153 27 BF195 12 0C44 31 40320 56 2N4069 45 (CONT.) C154 27 BF196 12 0C45 28 40362 48 2N4427 75 (CONT.)	
2-2µF, 3-3, 4-7, 6-8, 25V: 1-5, 10, 20V: 1-5µ, 16V: 10P 13p each. Carbon Track, 0-25W Log & 0-5W Linear values. Carbon Track, 0-25W Log & 0-5W Linear values. 2-2µF, 3-2, 4-7, 6-8, 25V: 1-5, 10, 20V: 1-5µ, 1-6V: 10P 13p each. 2-2µF, 3-2, 4-7, 6-8, 25V: 1-5, 10, 20V: 1-5µ, 1-6V: 10P 13p each. 2-2µF, 3-2, 4-7, 6-8, 25V: 1-5, 10, 20V: 1-5µ, 1-6V: 10P 13p each. 2-2µF, 3-2, 4-7, 6-8, 25V: 1-5, 10, 20V: 1-5µ, 1-6V: 10P 13p each. 2-2µF, 3-2, 4-7, 6-8, 25V: 1-5, 10, 20V: 1-5µ, 1-6V: 10P 13p each. 2-2µF, 3-2, 4-7, 6-8, 25V: 1-5, 10, 20V: 1-5µ, 1-6V: 10P 13p each. 2-2µF, 3-2, 4-7, 6-8, 25V: 1-5, 10, 20V: 1-5µ, 1-6V: 10P 13p each. 2-2µF, 3-2, 4-7, 6-8, 25V: 1-5, 10, 20V: 1-5µ, 1-6V: 10P 13p each. 2-2µF, 3-2µF,	C158 11 BF198 18 0C71 28 40407 52 214922 55 4034 1 C159 11 BF199 18 0C72 45 40408 70 215135 42 4095 1 C160 42 BF200 32 0C74 55 40411 295 [215135 42 4095 1	78 90 05 05
16V:         15µ, 22         25p; 47, 100, 220         40p, 100         5001, 11k at 2K (LIN ONLT) single 27p         27p           10V:         15µ, 22, 33         20p; 100         35p; 6V:         5KΩ-2MΩ single gang         27p           47µ, 68         100 30p; 30V: 100 20p.         5KΩ-2MΩ single gang         5KΩ-2MΩ single gang         65p           MYLAR FILM CAPACITORS         5KΩ-2MΩ dual gang stereo         78p	C169C 12 BF244A 28 0C81 50 40467 95 12N5172 25 4098 1 C169C 14 BF244B 30 0C82 50 40594 90 2N5179 60 4099 1 C170 18 BF256 50 0C83 48 40595 98 2N5180 80 4160 1	72 10 45 09
100V:         0.002,0.005,0.01μF         6p         SLIDER POTENTIOMETERS           0.015,0.02,0.03,0.04,0.05,0.056μF         7p         0.25W log and linear values 60mm track         5K0,500K0 Single gang         70p           0.1μF,0.2         10p.         50V:0.47μF         12p         5K0,500K0 Single gang         70p           0.10,0.02,0.03,0.02         10p.         50V:0.47μF         12p         10K0,500K0 Duel gang         80p	C171 11 BF257 30 OC84 44 40.603 65 2N5191 70 4161 11 C172 11 BF258 30 OC140 110 40594 90 2N5305 40 4162 11 C173 12 BF259 30 OC170 85 40595 98 2N5457 32 4163 11	09 09 09
CERAMIC CAPACITORS 50V         10KQ 500KQ Dual gang         80p           Range: 0.5pF to 10nF         4p         500KQ Dual gang         80p           15nF, 22nF, 33nF, 47nF 5p         100nF 6p         PRESET POTENTIOMETERS         25p           0.1W 500-2.2M Mini, Vert. & Horiz.         7p	C178 16 67336 35 00200 85 40636 125 2N5459 32 4175 1 C179 18 8594 40 17929 43 40673 68 2N5485 35 4194 1 C181 20 8594 38 17929 43 2N697 25 2N5642 750 4408 7	10 99 08 20
POLYSTYRENE CAPACITORS:         0.25W 100Ω-3.3MΩ Horiz,         larger         10p           10pF to 1nf, 6p.         1.5nF to 47nF 10p.         0.25W 250Q-4.7MΩ Vert.         10p	C183 9 BFR39 25 TIP29C 60 2N699 54 2N6027 40 4410 7 C184 9 BFR40 25 TIP30 47 2N706A 18 2N6109 50 4411 9 C182L 11 BFR41 28 TIP30A 50 2N708 19 3N128 112 4412V13	20 20 58 80
SILVER MICA (pF)         TRIMMERS miniature         RESISTORS-Erie make 5% carbon           3.3, 4.7, 6.8, 8.2, 10,         2.5pF; 3-10pF;         2p           12, 18, 22, 27, 33, 39,         3-30pF; 3-50pF         2p           47, 50, 68, 75, 82, 85;         5-25pF; 65pF 88pF 30p         2sW 202-4 M7	C212 10 BFR98 105 TIP31C 65 2N1131 22	
100, 120, 150, 180, 200, 220, 4, 17, 12, 25, 10, 200, 220, 270, 300, 330, 2, 40, 51, 0, 80, 51, 300, 230, 240, 51, 0, 80, 51, 300, 230, 240, 51, 0, 80, 51, 300, 230, 240, 51, 0, 80, 51, 300, 230, 240, 51, 0, 80, 51, 300, 240, 51, 100, 100, 100, 100, 100, 100, 100	C212L 11 BFX29 28 TIP32A 58 2N1132 22 Pair 4433 9 C213 10 BFX84 26 TIP32C 75 2N1303 50 4435 8 C213L 12 BFX85 28 TIP32A 85 2N1304 50 25 4435 8	95 25 75
360, 330, 470, 600 & 35, 200, F 330, 1%0 5W 510-1M E24 8p 6p 820pF 16p each 25-200, F 350, 1%0 5W 510-1M E24 8p 6p 100-500pF 45p 100 - price applies to Resistors of each type 1250pF 55p not mixed values.	IC214L 13 BFX87 28 TIP34A 85 2N1307 50 Extra 4451 2 IC307B 20 BFX88 28 TIP34C 110 2N1308 46 4452 IC308B 20 BFY50 20 TIP35A 185 2N1570 50 50 50 50 50 50 50 50 50 50 50 50 50	95 95 05
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702         75         LW308T         110         RC4136D         120         2102-2         225         SN754526         81           709C 8 pin         35         LM311H         120         SAD1024         1350         2111         195         SN75450         11           709 14 pin         38         LM318H         205         SA5560         195         2112-2N         250         SN75451           710         67         LW324A         68         SA5570         195         2114         50         SN75452	7481 86 74167 200 1302 12 15145 108 1539 86 4019 48 453 7482 69 74170 185 1502 12 15145 108 1539 468 4019 48 4535 7483 72 74172 625 1503 12 15147 170 15309 175 4020 92 4506	69 75 51
223         14 pin         36         LM339         70         SG3402         295         2708         775         SW75454         27           741         8 pin         18         LM348         90         SW76003N         170         27L08         995         TM56011         3           7475         SW76013N         140         2716         3400         TTL 74	7485 75 74174 87 LS08 22 LS153 76 LS323 468 4022 85 4508 7486 31 74175 87 LS09 22 LS153 76 LS323 468 4023 22 4510	99 150
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AY-1-6721/6 195 LM1458 50 SN/64// 225 745188 210 /400 26 AY-3-1015 560 LM3900 60 SN76660 90 745189 158 7407 38 AY-3-8500 390 LM390N 70 SP8629 450 745184 750 7408 17	74100 119 74190 95 LS26 48 LS166 226 LS365 65 4033 145 4520	108 228
	74105         62         74192         98         L527         28         L5169         155         L5369         69         4035         111         4522           74107         29         74133         98         L528         48         L5169         150         L5367         66         4035         111         4522           74107         29         74133         98         L5302         22         L5170         288         L5368         66         4036         335         4526           74109         54         74194         98         L5322         27         L5173         106         L5373         180         4037         100         4527           74110         54         74195         98         L5337         39         L5174         106         L5375         160         4038         108         4529           74111         54         74195         92         L5337         39         L5175         106         L5375         160         4038         108         4529           74111         54         74195         92         L537         39         L5175         106         L5374         4039         320 </td <td>149 152 99</td>	149 152 99
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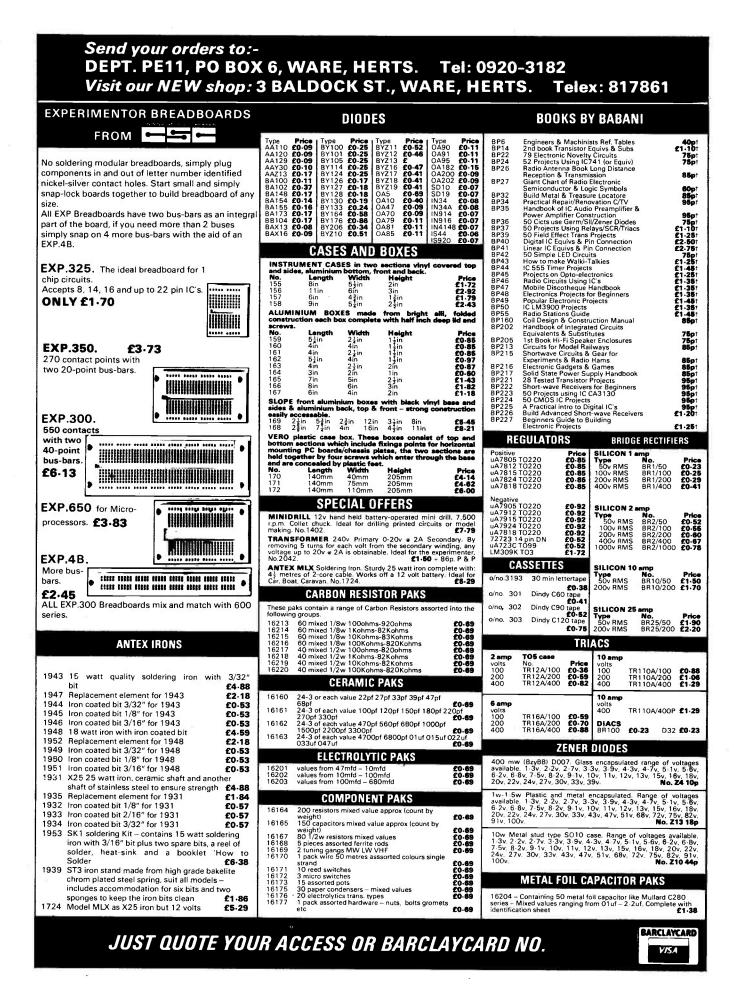
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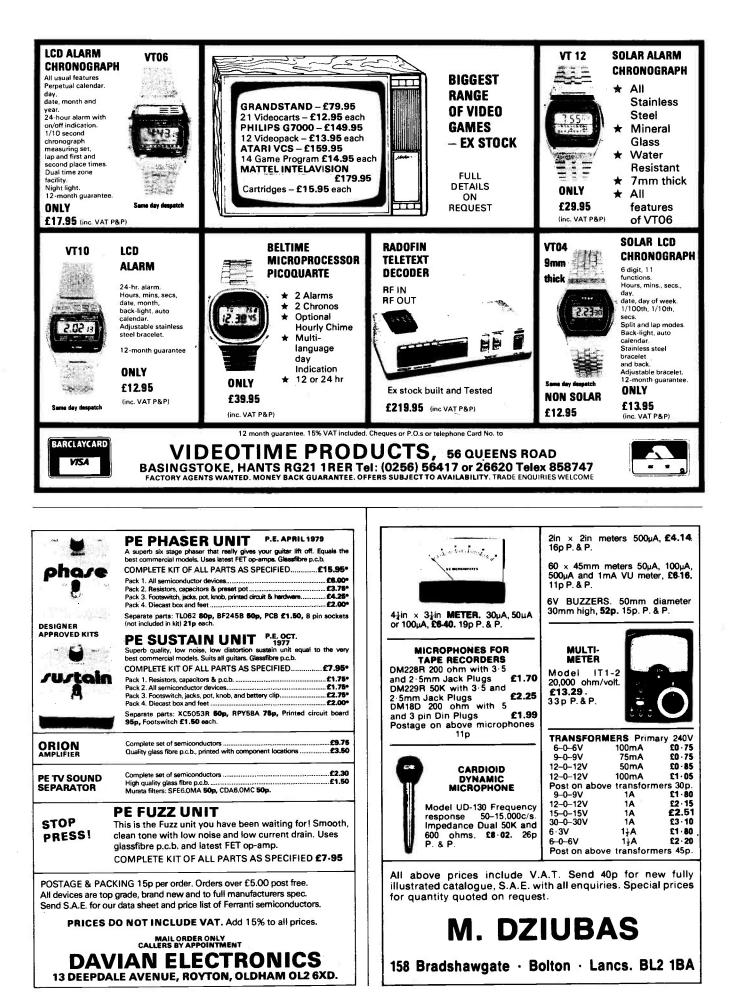
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## BI-PAK SEMICONDUCTORS,

		THYRISTORS SILICON		- OPTOELECTRONICS
TRANSISTORS	S	1 amp TO 5 Case RECTIFIER Volts No: Price 200mA	s	LED'S (diffused)
AC126         F0.21         BC148         F0.08         BC549         F0.12           AC127         F0.21         BC149         F0.08         BC550         F0.16           AC127         F0.18         BC157         F0.12         BC556         F0.16           AC128         F0.30         BC159         F0.12         BC557         F0.15           AC132         F0.23         BC157         F0.12         BC558         F0.16           AC134         F0.23         BC167         F0.14         BC159         F0.12         BC558           AC134         F0.23         BC168         F0.14         BD115         F0.58           AC141         F0.25         BC168         F0.16         BD116         F0.92           AC141         F0.33         BC170         F0.10         BD131         F0.40           AC174         F0.23         BC171         F0.18         BD135         F0.40           AC176K         F0.29         BC177         F0.18         BD135         F0.40           AC178         F0.23         BC178         F0.18         BD135         F0.40           AC178         F0.23         BC178         F0.18         BD135	Type         Price         Type         Price           BU105/02         C22,42         ZTX108         E0.11           BU105/02         C22,42         ZTX109         E0.11           BU205         E1.61         ZTX500         • 60.13           BU205         E1.61         ZTX500         • 60.14           BU205         E1.61         ZTX500         • 60.14           BU208/02         E2.58         2N1613         ± 60.23           MJE2955         £1.64         ZN1890         £ 00.51           MJE3055         £0.69         2N1893         £ 0.35           MF102         £0.32         2N2147         £ 0.86           MPF104         £0.42         2N2147         £ 0.86           MPF104         £ 0.42         2N2147         £ 0.81           MPSA05         £ 0.22         2N2192         £ 0.44           MPSA05         £ 0.22         2N2192         £ 0.44           MPSA05         £ 0.22         2N2192         £ 0.44           MPSA05         £ 0.22         2N217         £ 0.25           C22         £ 1.73         2N2218         £ 0.25           C223         £ 1.73         2N2218         £ 0.23 <td>100 TH/1A/100         £0.29         Issg20 50V           100 TH/1A/100         £0.32         Issg21 100V           200 TH/1A/100         £0.36         Issg22 320V           600 TH/1A/400         £0.36         Issg22 320V           600 TH/1A/400         £0.43         Issg22 320V           800 TH/1A/400         £0.43         Issg22 320V           800 TH/1A/400         £0.43         Issg22 320V           800 TH/1A/800         £0.56         1 Amp           1M4001 50V         IM4001 50V         IM4002 500V           3 amp         T0 66 Case         IM4004 500V           100 TH/3A/100         £0.32         IM4004 500V           200 TH/3A/200         £0.37         IM4005 50V           800 TH/3A/400         £0.48         1.5 Amp           800 TH/3A/400         £0.48         1.5 Amp           800 TH/3A/400         £0.74         Is5021 00V           900 TH/3A/400         £0.74         Is5021 20V           500 TH/3A/500         £0.74         Is5021 600V           900 TH/3A/50         £0.44         Is5021 900V           900 TH/3A/50         £0.44         Is5021 900V</td> <td>£0.07 £0.08 £0.09 £0.10 £0.11 £0.05 £0.05 £0.05 £0.05 £0.09 £0.09 £0.09 £0.11</td> <td>O/no. Type         Price           1501         Size         125mm RED         £0.11           1502         Size         125mm GREEN         £0.21           1503         Size         125mm GREEN         £0.21           1504         Size         2mm GREEN         £0.21           1505         Size         2mm GREEN         £0.21           1506         Size         2mm GREEN         £0.21           1506         Size         2mm GREEN         £0.21           1509         Size         2mm CHEAR         £0.12           SUPER 'Hi-Brite' Type         £0.11         £0.12         \$22           1521         Size         3mm (-125) RED         £0.11           1522         Size         3mm (-125) RED         £0.11           1524         Size         5mm (-2) Rebot masistor         £0.63           1520         OCP1 Photo transistor         £0.63         1508/ 125 pack of 5 -125 clips         £0.17           1508/ 12 pack of 5 -2 clips         £0.20         £0.20         \$0.20</td>	100 TH/1A/100         £0.29         Issg20 50V           100 TH/1A/100         £0.32         Issg21 100V           200 TH/1A/100         £0.36         Issg22 320V           600 TH/1A/400         £0.36         Issg22 320V           600 TH/1A/400         £0.43         Issg22 320V           800 TH/1A/400         £0.43         Issg22 320V           800 TH/1A/400         £0.43         Issg22 320V           800 TH/1A/800         £0.56         1 Amp           1M4001 50V         IM4001 50V         IM4002 500V           3 amp         T0 66 Case         IM4004 500V           100 TH/3A/100         £0.32         IM4004 500V           200 TH/3A/200         £0.37         IM4005 50V           800 TH/3A/400         £0.48         1.5 Amp           800 TH/3A/400         £0.48         1.5 Amp           800 TH/3A/400         £0.74         Is5021 00V           900 TH/3A/400         £0.74         Is5021 20V           500 TH/3A/500         £0.74         Is5021 600V           900 TH/3A/50         £0.44         Is5021 900V           900 TH/3A/50         £0.44         Is5021 900V	£0.07 £0.08 £0.09 £0.10 £0.11 £0.05 £0.05 £0.05 £0.05 £0.09 £0.09 £0.09 £0.11	O/no. Type         Price           1501         Size         125mm RED         £0.11           1502         Size         125mm GREEN         £0.21           1503         Size         125mm GREEN         £0.21           1504         Size         2mm GREEN         £0.21           1505         Size         2mm GREEN         £0.21           1506         Size         2mm GREEN         £0.21           1506         Size         2mm GREEN         £0.21           1509         Size         2mm CHEAR         £0.12           SUPER 'Hi-Brite' Type         £0.11         £0.12         \$22           1521         Size         3mm (-125) RED         £0.11           1522         Size         3mm (-125) RED         £0.11           1524         Size         5mm (-2) Rebot masistor         £0.63           1520         OCP1 Photo transistor         £0.63         1508/ 125 pack of 5 -125 clips         £0.17           1508/ 12 pack of 5 -2 clips         £0.20         £0.20         \$0.20
AC188 <b>f0.21</b> BC1831 <b>f0.10</b> BD175 <b>f0.69</b> AC188 <b>k f0.32</b> BC184 <b>f0.10</b> BD175 <b>f0.69</b> AD140 <b>f0.69</b> BC207 <b>f0.13</b> BD177 <b>f0.78</b> AD142 <b>f0.98</b> BC208 <b>f0.13</b> BD178 <b>f0.78</b> AD143 <b>f0.86</b> BC209 <b>f0.14</b> BD179 <b>f0.86</b> AD149 <b>f0.69</b> BC212 <b>f0.10</b> BD204 <b>f0.92</b> AD161 <b>f0.40</b> BC2121 <b>f0.10</b> BD204 <b>f0.92</b> AD161 <b>f0.40</b> BC2131 <b>f0.10</b> BD204 <b>f0.92</b> AD161 <b>f0.40</b> BC2131 <b>f0.10</b> BD457 <b>f0.43</b> AD124 <b>f0.35</b> BC214 <b>f0.10</b> BF457 <b>f0.43</b> Af124 <b>f0.35</b> BC2214 <b>f0.10</b> BF458 <b>f0.43</b> Af125 <b>f0.35</b> BC227 <b>f0.18</b> BF594 <b>f0.35</b> AF127 <b>f0.37</b> BC231 <b>f0.10</b> BF459 <b>f0.32</b> AF139 <b>f0.40</b> BC2151 <b>f0.11</b> BF459 <b>f0.32</b> AF139 <b>f0.40</b> BC2511 <b>f0.11</b> BF459 <b>f0.32</b> AF136 <b>f0.48</b> BC301 <b>f0.32</b> BFR39 <b>f0.28</b> AF136 <b>f0.48</b> BC301 <b>f0.32</b> BFR79 <b>f0.32</b> AF136 <b>f0.47</b> BC302 <b>f0.33</b> BFR96 <b>f0.32</b>	OC26         £1.15         2N2904         £0.23           OC28         £0.92         2N2905         £0.20           OC35         £1.03         2N2905         £0.20           OC36         £1.03         2N2905         £0.20           OC36         £1.03         2N2906         £0.21           OC70         £0.27         2N2906         £0.18           OC70         £0.37         2N2907         £0.23           TIC44         £0.33         2N2907         £0.23           TIC44         £0.33         2N2907         £0.24           TIP29A         £0.46         2N29267         £0.03           TIP29B         £0.46         2N29267         £0.09           TIP29B         £0.46         2N39268         £0.09           TIP30A         £0.46         2N39268         £0.09           TIP30B         £0.48         2N3053         £0.18           TIP30A         £0.50         2N3053         £0.18           TIP30A         £0.50         2N3053         £0.18           TIP30A         £0.50         2N3053         £0.46           TIP30A         £0.48         2N3055         £0.46           T	100         THY5A/100         £0.51         IS031         1200V           200         THY5A/200         £0.57         3 Amp         3 Amp           400         THY5A/400         £0.65         IN5400         50.05         3 Amp           600         THY5A/400         £0.67         IN5400         50.07         IN5400         20.07           800         THY5A/400         £0.79         IN5404         200V         IN5404         400V           7 amp         TO 48         Case         IN5406         600V         IN5406         600V           7 onthy         THY7A/500         £0.55         10 Amp         IN5407         1000 100V           500         THY7A/200         £0.65         1510/50 50V         1510/100 100V         400 THY7A/400         £0.71         1510/400 400V         800 THY7A/400         £0.71         1510/600 400V         800 THY7A/800         £1.05         1510/600 400V         1510/600 600V         1510/600 600V	£0.28 £0.16 £0.17 £0.19 £0.24 £0.28 £0.34 £0.21 £0.24 £0.24 £0.24 £0.24 £0.24 £0.24 £0.24 £0.24 £0.24 £0.58	DISPLAYS DL703 7 segment D.P. left (-30" height) common RED anode single digit O(N0: 1523 £0.80 DL707 7 segment D.P. left (03" height) common RED anode single digit O(N0: 1510 £0.92 DL527 7 segment D.P. left (-50" height) RED common anode Two-digit reflector O(N0: 1521 £2.53 DL747 7 segment D.P. left (-50" height RED common anode Single-digit light pipe O(N0: 1511 £1.72
AL103 £1.36 BC304 £0.44 BFX30 £0.36 AU104 £1.61 BC327 £0.18 BFX84 £0.25 AU110 £1.61 BC328 £0.17 BFX85 £0.28 AU113 £1.61 BC337 £0.17 BFX85 £0.28 BC107A £0.09 BC338 £0.17 BFX87 £0.25 BC107B £0.10 BC440 £0.35 BFX87 £0.25 BC107C £0.12 BC441 £0.35 BFX50 £0.18 BC108B £0.11 BC461 £0.44 BFY51 £0.18 BC108B £0.11 BC461 £0.44 BFY52 £0.18 BC108C £0.12 BC477 £0.23 BIP19 £0.44 BC109B £0.10 BC478 £0.23 BIP19 £0.44 BC109B £0.10 BC478 £0.23 BIP19 £0.44 BC109B £0.10 BC478 £0.23 BIP19 £0.44	Tip31C         E0:50         2N3615         E1.21           Tip32A         E0.462         2N3616         E1.21           Tip32B         E0.462         2N3646         E0.10           Tip32C         E0.50         2N3702         E0.09           Tip32C         E0.50         2N3702         E0.09           Tip32C         E0.50         2N3702         E0.09           Tip41A         E0.50         2N3704         E0.08           Tip41C         E0.52         2N3705         E0.09           Tip42A         E0.50         2N3706         E0.09           Tip42A         E0.52         2N3706         E0.09           Tip42A         E0.52         2N3707         E0.08           Tip42B         E0.52         2N3708         E0.08           Tip43D         E0.25         2N3708         E0.08           Tip43D         E0.22         2N3709         E0.08           Tip43D         E0.22         2N3709         E0.08           Tip43D         E0.22         2N3710         E0.08           Tip43D         E0.22         2N3819         E0.21           ZTA107         E0.11         2N3820         E0.40	10 amp         T0 48 Case         1510/1000 1000           Volts No:         Price         IS10/1200 120           50 THY10A/50         £0.58         30 Amp           100 THY10A/100         £0.65         IS30/150 50V           100 THY10A/200         £0.65         IS30/200 200V           400 THY10A/200         £0.80         IS30/200 200V           400 THY10A/400         £0.80         IS30/400 400V           600 THY10A/600         £1.40         IS30/800 800V           800 THY10A/600         £1.40         IS30/800 800V           16 amp         T0 48 Case         IS30/1000 100           16 amp         T0 48 Case         IS30/100 100           90 THY16A/50         £0.62         IS70/200 200V           Volts No:         Price 60 Amp           90 THY16A/50         £0.62         IS70/200 200V           100 THY16A/200         £0.71         IS70/200 200V           400 THY16A/300         £0.88         IS70/400 400V           600 THY16A/300         £1.83         IS70/600 600V           600 THY16A/300         £1.33         IS70/600 800V           600 THY16A/300         £1.98         IS70/600 800V	2V £0.79 £0.64 £0.79 £1.06 £1.43 £2.02 £2.65 2V £3.31 £0.86 £1.38 £0.96 £1.38 £2.01 £2.58 £2.87	OPTO-ISOLATORS Isolation Breakdown - Voltage 1500 - continuous fwd current 100mA. CIL74 Single-channel 6 pin DIP standard type - optically coupled pair with infra-red LED emitter and NPN silicon photo transistor O/NO: 1497 £0.57 CILD74 Multi-channel 8 pin DIP two isolated channels O/NO: 1498 £1.15 CIL074 Multi-channel 16 pin DIP four isolated channels O/NO: 1498 £1.53 2nd GRADE LED PAK A pack of 10 standard sizes and colours which fail to perform to their very rigid specification, but which are ideal for amateurs who do not require the full spect. O/NO: 1507 £1.04
7400         £0.10         7427         £0.27         7472         £0.23         74105           7401         £0.12         7428         £0.29         7473         £0.28         74107           7402         £0.12         7430         £0.12         7430         £0.28         74104	£0.43 74163 £0.71 £0.27 74164 £0.78 £0.41 74165 £0.78	AUDIO MODULES		SOCKETS
7403 <b>60.12</b> 7432 <b>60.25</b> 7475 <b>60.33</b> 74111           7404 <b>60.12</b> 7433 <b>60.34</b> 7476 <b>60.28</b> 74118           7405 <b>60.12</b> 7433 <b>60.34</b> 7476 <b>60.28</b> 74118           7406 <b>60.25</b> 7438 <b>60.34 7481 60.97</b> 74121           7407 <b>60.25</b> 7448 <b>60.37</b> 7422 <b>7481 60.37</b> 74122           7408 <b>60.14</b> 7441 <b>60.37</b> 7483 <b>60.66</b> 74123           7409 <b>60.14</b> 7441 <b>60.37</b> 7483 <b>60.66</b> 74123           7409 <b>60.14</b> 7441 <b>60.86</b> 7483 <b>60.67</b> 74132           7410 <b>60.12</b> 7443 <b>60.86</b> 7485 <b>60.78</b> 74141           7411 <b>60.12</b> 7443 <b>60.87</b> 7498 <b>61.98</b> 74150           7411 <b>60.17</b> 7445 <b>60.47</b> 7498 <b>7415</b> 74151 <t< td=""><td>C0.66         74.166         C0.89           C0.92         74.174         C0.74           C1.35         74.175         C0.74           C0.27         74.176         C0.66         Arr           C0.42         74.177         C0.66         Al.2           C0.55         74.180         C1.72         AL.2           C0.63         74.180         C0.66         Al.3           C0.63         74.184         C0.80         C0.63           C0.63         74.184         C0.80         C0.78           C0.55         74.191         C0.78         AL.6           C0.55         74.192         C0.69         AL.2           C0.57         74.193         C0.69         AL.2           C0.57         74.194         C0.71         AL.1           C0.57         74.194         C0.69         AL.2           C0.56         74.194         C0.71         AL.1           C0.57         74.194         C0.69         AL2           C0.56         74.194         C1.20         Pre           C0.57         74.196         C1.20         Pre           C0.56         74.197         C1.20         Pre</td><td>Aplifiers 20 5 watt amplifier module 30A 7-10 watt amplifier module 30 15-25 watt amplifier module 30 35 watt amplifier module 30 35 watt amplifier module 30 125 watt amplifier module 30 325 watt amplifier module</td><td>£3.73 £4.35 £5.39 £8.44 £13.74 £19.24 £8.94</td><td>1671         6 pin DIL         £0.09           1671         4 pin DIL         £0.12           1720         16 pin DIL         £0.12           1721         16 pin DIL         £0.12           1722         20 pin DIL         £0.22           1612         24 pin DIL         £0.22           1612         24 pin DIL         £0.22           1615         28 pin DIL         £0.26           1723         40 pin DIL         £0.31           1615         703 transistor         £0.13           1616         T03 transistor         £0.13           1726         14 pin DIL Wire wrap gold plated Cambion         £0.25           G.P. SWITCHING TRANSISTORS         £0.25</td></t<>	C0.66         74.166         C0.89           C0.92         74.174         C0.74           C1.35         74.175         C0.74           C0.27         74.176         C0.66         Arr           C0.42         74.177         C0.66         Al.2           C0.55         74.180         C1.72         AL.2           C0.63         74.180         C0.66         Al.3           C0.63         74.184         C0.80         C0.63           C0.63         74.184         C0.80         C0.78           C0.55         74.191         C0.78         AL.6           C0.55         74.192         C0.69         AL.2           C0.57         74.193         C0.69         AL.2           C0.57         74.194         C0.71         AL.1           C0.57         74.194         C0.69         AL.2           C0.56         74.194         C0.71         AL.1           C0.57         74.194         C0.69         AL2           C0.56         74.194         C1.20         Pre           C0.57         74.196         C1.20         Pre           C0.56         74.197         C1.20         Pre	Aplifiers 20 5 watt amplifier module 30A 7-10 watt amplifier module 30 15-25 watt amplifier module 30 35 watt amplifier module 30 35 watt amplifier module 30 125 watt amplifier module 30 325 watt amplifier module	£3.73 £4.35 £5.39 £8.44 £13.74 £19.24 £8.94	1671         6 pin DIL         £0.09           1671         4 pin DIL         £0.12           1720         16 pin DIL         £0.12           1721         16 pin DIL         £0.12           1722         20 pin DIL         £0.22           1612         24 pin DIL         £0.22           1612         24 pin DIL         £0.22           1615         28 pin DIL         £0.26           1723         40 pin DIL         £0.31           1615         703 transistor         £0.13           1616         T03 transistor         £0.13           1726         14 pin DIL Wire wrap gold plated Cambion         £0.25           G.P. SWITCHING TRANSISTORS         £0.25
CMOS ICs	PA	module	£18.45	TO18 sim to 2N706/8 BSY27/2B/95A ALL usuable devices no open & shorts.
CD4001 <b>E0.17</b> CD4016 <b>E0.48</b> CD4027 <b>E0.57</b> CD404 CD4002 <b>E0.18</b> CD4017 <b>E0.86</b> CD4028 <b>E0.78</b> CD404 CD4006 <b>E1.05</b> CD4018 <b>E0.97</b> CD4029 <b>E0.97</b> CD4044 CD4007 <b>E0.19</b> CD4019 <b>E0.48</b> CD4030 <b>E0.55</b> CD4044 CD4009 <b>E0.51</b> CD4020 <b>E1.03</b> CD4031 <b>E2.30</b> CD4045 CD4009 <b>E0.51</b> CD4021 <b>E0.94</b> CD4035 <b>E1.15</b> CD4056 CD4010 <b>E0.55</b> CD4022 <b>E0.94</b> CD4037 <b>E1.09</b> CD405 CD4011 <b>E0.17</b> CD4023 <b>E0.17</b> CD4040 <b>E1.01</b> CD4055 CD4011 <b>E0.18</b> CD4024 <b>E0.74</b> CD4041 <b>E1.01</b> CD4055	Price         Type         Price           13 £1.01         Cbd707 £0.19         14           14 £0.34         Cbd707 £0.19         Poil           15 £1.61         Cbd72 £0.19         Poil           16 £1.48         Cbd72 £0.19         Poil           16 £1.49         Cbd72 £0.19         Poil           16 £1.49         Cbd72 £0.19         Poil           17 £1.00         Cbd82 £0.20         15           19 £0.48         Cbd510 £1.13         SPI           19 £0.48         Cbd510 £1.16         SPI           5 £1.15         Cbd518 £1.15         SPI           16 £1.45         Cbd518 £1.15         SPI           16 £1.55         Cbd20 £1.15         SPI           9 £0.19         Cbd318 £1.25         SPI	Wer Supplies       12     Power supply (24 volts DC)       M80     Stabilised power supply (33V)       M120/45     Stabilised power supply (45V)	£19.07 £1.72 £5.06 £6.67	ALSO available in PNP sim. to 2029/96CY70. 20 for 57p - 50 for £1.15 - 100 for £2.07 - 500 for £9.20 - 1,000 for £16.10 - when ordering state NPN/PNP. SILLCON DIODES G.P. 300mW 40PIV (min) sub min FULLY TESTED ideal for Organ builders. 30 for 57p - 100 for £1.72 - 500 for £5.75 - 1,000 for £10.35.
Type         Price         Type         Type <thtype< th=""> <thtype< th=""> <thtype< td="" td<=""><td>Price         Type         Price         SPI           C         £0.46         SN76115         £2.18         SG           C         £0.36         SN76600         £0.86         SG           C         £0.36         SL414A         £2.24         SG           C         £0.36         SL414A         £2.30         SG           C         £0.52         TAA5218         £2.30         MI           C         £0.52         TAA5214         £2.30         MI           C         £0.27         TAA6361         £1.72         GU           C         £0.23         TBA540         £2.41         £2.41           C         £0.27         TAA6361         £1.49         £2.47           C         £0.23         TBA540         £2.41         £2.41           C         £0.43         EBA5105         £2.41         £3.43</td><td>equaliser scellaneous A30 Stereo magnetic cartridge pre-amp 50 Stereo tuner</td><td>£6.67 £6.67 £4.37 £4.42 £26.72</td><td>METAL FOIL CAPACITOR PAK Containing 50 metal foil capacitor – like Mullard C280 series – mixed values rang- ing for 01uf-2:2uf. Complete with iden- tification sheet 0/N0: 16204 £1.38. JUMBO PAK SEMICONDUCTOR</td></thtype<></thtype<></thtype<>	Price         Type         Price         SPI           C         £0.46         SN76115         £2.18         SG           C         £0.36         SN76600         £0.86         SG           C         £0.36         SL414A         £2.24         SG           C         £0.36         SL414A         £2.30         SG           C         £0.52         TAA5218         £2.30         MI           C         £0.52         TAA5214         £2.30         MI           C         £0.27         TAA6361         £1.72         GU           C         £0.23         TBA540         £2.41         £2.41           C         £0.27         TAA6361         £1.49         £2.47           C         £0.23         TBA540         £2.41         £2.41           C         £0.43         EBA5105         £2.41         £3.43	equaliser scellaneous A30 Stereo magnetic cartridge pre-amp 50 Stereo tuner	£6.67 £6.67 £4.37 £4.42 £26.72	METAL FOIL CAPACITOR PAK Containing 50 metal foil capacitor – like Mullard C280 series – mixed values rang- ing for 01uf-2:2uf. Complete with iden- tification sheet 0/N0: 16204 £1.38. JUMBO PAK SEMICONDUCTOR
CA3052         C1384         LW380         C037         NE667         C1385         77747           CA3054         F126         LW381         £1.66         LW4702C         £0.52         LW4748           CA3075         £1.72         LW3800         £0.66         VA702C         £0.52         VA748           CA3075         £1.72         LW3800         £0.66         VA702C         £0.52         VA748           CA3081         £1.72         MC1303L         £0.97         LV4703         £0.28         77407           CA3081         £1.72         MC1303L         £0.97         LV4703         £0.28         77477           CA3083         £2.30         MC1304         £7.18         LW4703         £0.28         N7607           CA3090         £4.14         MC1310         £1.09         7209         £0.28         N7617           CA3123         £2.18         MC1312         £2.18         709P         £0.28         N7617	3 £0.40 TBA820 £0.80 3 £0.40 TBA9200 £2.87 £0.40 TCA270S £2.30 BP D13N £2.01 TBA800 £0.92 GE	124Siren alarm module 5 watts100MKII10 channel mono graphic	£22.66 £4.02 £23.00	16222 - Transistors Germ and Silicon Rectifiers-Diodes-Triacs-Thyristors-ICs and Zeners ALL NEW & CODED. Approx. 100 pieces offering the amateur a fantastic bargain PAK and an enormous saving £2.58.

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We've been making precision instruments since 1935 and our sales are worldwide. We welcome competition, because it lets us show how good we are. So when we make a 3½ digit hand-held multimeter like the 3020, we make it better than anyone else.

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SPECIFICATIONS					
PARAMETER	BECKMAN 3020	FLUKE 8020A			
DC Voltage					
Ranges	5,200mV-1500V	5,200mV-1000V			
Accuracy	$\pm$ (0.1% rdg +1 digit)	$\pm$ (0.25% rdg+1 digit)			
AC Voltage					
Ranges	5,200mV-1000V	5,200mV-750V			
Accuracy					
45Hz—2kHz	$\pm$ (0.6% rdg+3 digits)	$\pm$ (0.75% rdg + 2 digits) to $\pm$ (1.5% rdg + 3 digits)			
DC Current					
Ranges	6,200µA-10A	4,2mA-2A			
Accuracy	$\pm$ (0.35% rdg + 1 digit) (except 10A)	$\pm$ (0.75% rdg +1 digit)			
AC Current	-				
Ranges	6,200µA-10A	4,2mA-2A			
Accuracy					
45Hz–2kHz	$\pm$ (0.9% rdg + 3 digits) (except 10A)	$\pm$ (1.5% rdg + 3 digits) to $\pm$ (2.0% rdg + 2 digits) (up to 1kHz)			
Resistance		_			
Ranges	6,200Ω –20MΩ	6,200Ω 20MΩ			
Accuracy	$\pm$ (0.2% rdg +1 digit)	$\pm$ (0.2% rdg + 1 digit) to $\pm$ (2.0% rdg + 1 digit)			
Battery Life	2000 hrs	$10 \pm (2.0\% \text{ rdg} \pm 1 \text{ digit})$ 200 hrs			
Fast Continuity Check	Yes	No			

Specifications obtained from published data.



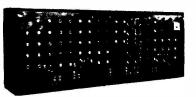
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BECKMAN

2M 200K 20K

3050

KITS FOR SYNTHESISERS, SOUND EFFECTS



#### **P.E. 128-NOTE PROGRAMMABLE SEQUENCER**

Enables a voltage controlled synthesiser to automatically play pre-programmed tunes of up to 32 pitches and 128 notes long. Programs are keyboard initiated and note length and rhythmic

pattern are externally variable.		
Set of basic component kits	KIT 76-5	£28.92
Set of PCBs & layout charts	KIT 76-6	£5.66
Set of text photocopies		£1.36

#### **P.E. 16-NOTE PROGRAMMABLE SEQUENCER**

Sequences of up to 16 notes may be programmed by the use of external panel controls and fed into most voltage controlled syn-

mesisers.		
Set of basic component kits	KIT 86-3	£22.90
Set of PCBs	KIT B6-4	£5.09
Set text photocopies		£1.84

#### **P.E. STRING ENSEMBLE**

A multivoiced string instrument synthesiser		
Set of basic component kits	KIT 77-6	£68.70
Set of PCBs & layout charts	KIT 77-7	£24.19

#### P.E. JOANNA PLUS ORGAN VOICING

A modified version of the P.E. 5-octave plano that retains all the original facilities and also includes switchable organ voicing cir-

Ceruy.		
Set of basic component kits	KIT 71-5	£89.87
Set of PCBs & layout charts	KIT 71-6	£29.51
"Sound Design" booklet		£1.00
	4	

#### **ELEKTOR ELECTRONIC PIANO**

A touch-sensitive multiple-voicing plano using the latest integrated circuit techniques for the keying and envelope shaping, and virtually eliminating "bee-hive" noise hitherto inherent in convince alternation line.

previous electronic planos.		
5-octave set of basic components	KIT 80-6	£100.64
5-octave set of PCBs (as published)	KIT 80-7	£26.02
Additional 3-octave extension		
basic parts	KIT 80-5	£40.98
Additional 3-octave set of PCBs		
(as published)	KIT 80-8	£9.45
Set of text photocopies		£1.81

#### **P.E. MINISONIC MK2 SYNTHESISER**

portable mains operated miniature sound synthesiser with keyboard circuits. Although having slightly fewer facilities than the large Formant and P.E. synthesisers the functions offered by

this design give it great scope and versatilit	γ.	
Set of basic component kits (excl. KBD		
R's & tuning pots – see list for options		
available	KIT 38-23	£67.05
Set of PCBs (incl. layout charts)	KIT 38-24	£9.87
"Sound Design" booklet		£1.00

#### P.E. SYNTHESISER

The well acclaimed and highly versatile large scale mains operated synthesiser. Other circuits in our lists may be used with it to good advantage. Main Unit basic component kits Main Unit set of PCBs & layout charts KIT 23-27 £86.99 KIT 23-28 £14.52

Keyboard Unit basic component kits Keyboard Unit set of PCBs & layout	KIT 23-29	£52.07
charts Main Unit set of text photocopies Keyboard Unit set of text photocopies	KIT 23-30	€8.42 £5.91 £2.30

#### **ELEKTOR FORMANT SYNTHESISER**

A very sophisticated synthesiser for t	the advanced constructor
who puts performance before price.	
Set of basic component kits	KIT 66-12 £193.68
Set of PCBs (as published)	KIT 66-13 £53.92
Set of text photocopies	£7.83

**10% DISCOUNT VOUCHER** 

(PE 70) TERMS: Goods in current adverts & lists over £50 goods value (excl P&P & VAT). Correctly costed, C.W.O., U.K. orders only. This voucher must accompany order. Valid unt<sup>1</sup> end of month on cover of P.E.

COMPONENTS SETS include all necessary resistors. capacitors, semiconductors, potentiometers and transformers. Hardware such as cases, sockets, knobs, keyboards, etc. are not included but most of these may be bought separately. Fuller details of kits, PCBs and parts are shown in our lists.

LAYOUT DIAGRAMS are supplied free with all PCBs unless "as published".

**P.E. GUITAR EFFECTS PEDAL** 

Modulates the attack, decay and filter characteristics of a signal from most audio sources, producing 8 different switchable effects that can be further modified by manual controls.

#### KIT 42-1 Basic parts with foot switches £8.45 KIT 42-2 25.55 £1.57 Basic parts with panel switches PCB 43A PCB & layout chart Text photocopy 280

#### **ELEKTOR DIGITAL REVERB UNIT**

A very advanced unit using sophisticated i.c. techniques instead of mechanical spring lines. The basic delay range of 24 to 90mS can be extended up to 450mS using the extension unit. Further delays can be obtained using more extensions.

uerays can be obtained using more extens	ions.	
Main unit basic component kit	KIT 78-1	£49.99
Main unit PCB (as published)	PCB 9913	£3.69
Extension unit basic component kit	KIT 78-2	£47.69
Extension unit PCB (as published)	PCB 788	£1.16
Text photocopy		
ELEKTOR ANALOGUE		

#### **REVERB UNIT**

Using i.c.s instead of spring-lines the main unit has a maxium delay of up to 100mS, and the additional set extends this up to 200mS. May be used in either mono or stereo mode.

	310100 1110000.	
Main unit basic component set	KIT 83-1	£29.49
Additional Delay basic components	KIT 83-2	£20.07
PCB (as publ.) to hold both kits	PCB 9973	£4.31
Text photocopy		

#### P.E. GUITAR MULTIPROCESSOR

An extremely versatile sound processing unit capable of producing, for example, flanging, vibrato, reverb, fuzz and tremolo as well as other fascinating sounds. May be used with most electronic instruments.

Set of basic component kits Set of PCBs & layout charts Set of text photocopies	KIT 85-3 KIT 85-4	£43.75 £10.62 £2.52
P.E. PHASER		

ELEKTOR PHASING	&	
Set of basic components, incl., . PCB & chart Text photocopy	KIT 88-1	£10.14 68p
oscillator.		
An automatically controlled o-stag	e phasing unit with	integral

#### **VIBRATO UNIT**

Includes manual and automatic control over the rate of phasing & vibrato, and has been slightly modified to also include a 2-input mixer stage.

Set of basic components PCB & layout chart Text photocopy	KIT 70-1 PCB 70A	£19.11 £2.56 87p
P F PHASING UNIT		

#### '.E. PHASING UNIT

A simple but effective manually controlled phasing unit. Set of basic components incl., PCB & chart KIT 25-1 £3.52 Text photocopy

#### **PHASING CONTROL UNIT**

For use with Phasing Kit 25 to automatically control rate of phasing. Set of basic components incl., 

PCB & chart Text photocopy	KIT 36-1	£5.21 10p
P.E. SWITCHED TONE TREBLE BOOST		

Provides switched selection of 4 pre	set tonal responses.	
Set of basic components,		
PCB & chart	KIT 89-1	£3.82
Text photocopy		780

#### **P.E. TREBLE BOOST UNIT**

A simple treble boost unit with manual control of depth. Set of basic components, PCB & chart KIT 53-1 £2.76

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ADD 15% VAT (or current rate if changed), Must be added to full total of goods, discount, post & handling, on all U.K. orders. Does not apply to Exoorts.

280

EXPORT ORDERS ARE WELCOME but to avoid delay we advise you to see our list for postage rates. All payments must be cash-with-order, in Sterling by Inter-national Money Order or through an English Bank. To obtain list – Europe send 20p. other countries send 50p.

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SUPPLIERS ORDER OF PRINTED CIRCUIT BOARDS, KITS AND COMPONENTS TO Α WORLD-WIDE MARKET

#### **ELEKTOR RESONANCE FILTER**

ELERIOR RESUMANC	EFILIER	
Allows a synthesiser to produce a me	ore realistic sim	ulation of
natural musical instruments. Set of basic components PCB (as published) Text photocopy	KIT 82-1 PCB 9951	£16.61 £3.29
P.E. GUITAR OVERDRI Sophisticated versatile fuzz unit inn affecting the fuzz quality whilst retain and also providing filtering. Can be use struments.	cluding variable ing the attack a	nd decay,
Set of basic components PCB & layout chart Text photocopy	KIT 56-1 PCB 56A	£7.57 £1.78 68p
P.E. FUZZ UNIT		
A simple fuzz unit. Slightly modified from Set of basic components, PCB & chart	m the original. KIT 55-1	£2.25
	KII 55-1	22.20
TREMOLO UNIT		
A slightly modified version of the simple Set of basic components, PCB & chart	P.E. unit. KIT 54-1	£3.23
GUITAR FREQUENCY		-
A slightly modified and extended version Set of basic components.	n of the P.E. unit	•
PCB & chart Text photocopy	KIT 74-1	£4.97 39p
P.E. GUITAR SUSTAIN		
Maintains the natural attack whilst exte	nding note durat	ion.
Basic components, foot switches, PCB & chart Basic components, panel switches.	KIT 75-1	£5.64
PCB & chart Text photocopy	KIT 75-2	£4.08 38p
P.E. WAH-WAH UNIT		
Can be controlled manually or by integr	al automatic con	trol.
Set of basic components, PCB & chart	KIT 51-1	£3.99
P.E. AUTO-WAH UNIT		
Automatically Wah or Swell sounds wit	h each note play	ed.
Basic components, foot switches, PCB & chart	KIT 58-1	£8.43
Basic components, panel switches, PCB & chart Text photocopy	KIT 5B-2	£5.31 58p
ELEKTOR WAVEFORN		
Converts a saw-tooth waveform into si tooth, regular triangle, or square-wave ratio.		
Basic components, PCB & chart, but excl. sw's.	KIT 67-1	£9.24
P.E. VOLTAGE CONTR FILTER	OLLED	
Extracted from P.E. Minisonic project. Set of basic components,		
PCB & chart	KIT 65-1	£7.88
P.E. RING MODULATO	R	
Extracted from P.E. Minisonic project. Set of basic components,		
PCB & chart	KIT 59-1	£6.05
ELEKTOR RING MODU	LATOR	
Compatible with the Formant & most o		
Set of basic components PCB (as published) Text photocopy	KIT 87-1 PCB 79040	£4.66 £1.74 38p

### AND OTHER PROJECTS

PHOTOGRAPHS in this advertisement show two four units containing some of the P.E. projects built from our kits and PCBs. The cases were built by ourselves and are not for sale, though a small selection of other cases is available.

LIST—Send stamped addressed envelope with all U.K. requests for free list giving fuller details of PCBs, kits and other components.

OVERSEAS enquiries for list Europe-send 20p: other countries—send 50p.



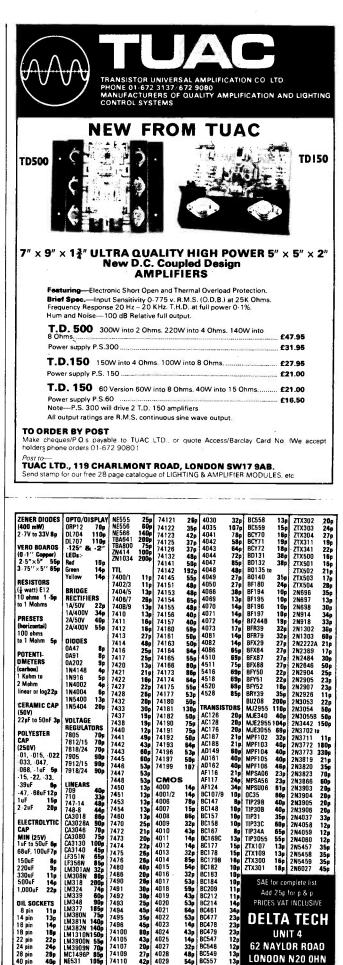
28 pin

40 pin

PHONOSONICS

#### **KIMBER-ALLEN KEYBOARDS AND CONTACTS**

KIMBER-ALLEN KEYBOARDS as				anufacturers
claim that these are the finest mould keys are plastic, spring-loaded, fitted v	ed plastic keyb	oards availa	able All octaves are	C to C, the
3 Octave (37 notes) 4 Octave (49 notes)				£25.50 £32.25
5 Octave (61 notes)				£39.75
CONTACT ASSEMBLIES (gold-cia	d wire) - 1 requ	ired for eac	h KBD note:	
Type GJ – SPCO <b>251p</b> ea. Type GA N/O <b>281p</b> ea. Type GC – 3 pr N/O <b>37</b> <b>581p</b> ea. Type 4PS – 3 pr N/O plus SF	p ea. Type G	E – 4 pr N/C	open <b>∡ep</b> ea. Type GH C <b>461p</b> ea. Type GH	e GB – 2 pr I– 5 pr N/O
P.E. NOISE GENERATO	R		INTEGR	ATED
Extracted from the P.E. Minisonic. Set of basic components,			CIRCL	JITS
PCB & chart	KIT 60-1	£4.00	301	48p
WIND & RAIN EFFECTS	SUNIT		318	220p
A slightly modified version of the original	P.E. unit.		320-15 323	195p 562p
Set of basic components, PCB & chart	- KIT 28-1	£4.68	324	87p
Text photocopy		28p	341-15 356	87p 101p
P.E. ENVELOPE SHAPE	R		709 723	48p 51p
WITHOUT VCA			726	1005p
Provides full manual control over atta release functions, and is for use with an e		stain and	741 748	24p 57p
Set of basic components,			4001 4007	15 <u>1</u> p 17 <u>1</u> p
PCB & chart Text photocopy	KIT 44-1	£5.24 49p	4011	17 <del>]</del> p
P.E. ENVELOPE SHAPE	R	-•	4013 4016	34p 33p
WITH VCA	n		4017 4024	54p
Has an integral Voltage Controlled Ampl	ifier, and has fu	II manual	4046	461p 96p
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PCB & chart	KIT 50-1	£7.34	4069	18p
Text photocopy		58p	4081 4136	1 <del>6}</del> р 126р
P.E. GENERATOR			AM2833 AY-1-0212	396p 617p
An ADSR envelope shaper without VCA Repeat-triggering enabling a synthesise	and additional to be progra	providing mmed for	AY-1-1320	636p
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PCB & layout chart	PCB 63A	£2.00	CA3080 CA3084	63p 209p
Text photocopy		58p	FX209	729p
P.E. EXTERNAL-INPUT SYNTHESISER-INTER			M252 MC3340	680p 150p
Allows external inputs such as guitars,			MCM6810 RC4195	670p 117p
processed by synthesiser circuits.	microphones e	tc, to be	SAD1024	1762p
Set of basic components, PCB & chart	KIT 81-1	£3,23	SG3402 TDA1022	262p 582p
P.E. TUNING FORK			TL074 XR2207	120p
Produces 84 switch-selected frequency	-accurate tone	s with an	ZN425	420p 375p
LED monitor clearly displaying beat-note	adjustments.		7400 7402	20p 20p
Set of basic components, PCB & chart	KIT 46-1	£16.42	7404	18p
Power Supply components, PCB & chart	KIT 46-2	£6.90	7420	31p 15p
Text photocopy		97p	7447 7472	72p 22 <del>1</del> p
P.E. TUNING INDICATO	R		7473	37 <del>1</del> p
A simple 4-octave frequency comparitor	for use with syr	thesisers	7489	31±p 241p
and other instruments where the full ve required.	saunty of KIT	40 IS NOT	7490 7493	42p 49 <del>1</del> p
Set of basic components, PCB & chart, but excl. sw.	KIT 69-1	£8.19	74121	53p
Text photocopy	NI 03-1	58p	74123 7805	55 <del>1</del> p 145p
P.E. DYNAMIC RANGE	LIMITER		7808 7812	145p 145p
Preset to automatically control sound out			7815	145p
Set of basic components, PCB & chart	KIT 62-1	£5.03	7818	145p
P.E. CONSTANT DISPLA				
FREQUENCY COUNTER		1		
A 5-digit counter for 1Hz to 55KHz w	vith 1Hz samp	ling rate.		ARCLAYCARD
Readout does not count visibly or flicker of Set of basic components	lue to blanking. KIT 79-1	£26.45	Buy it with Access	MSA
PCB (as published) Text photocopy	PCB 79A	£3.33		
. sat protocopy		78p		



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**DELTA TECH** 

UNIT 4

**62 NAYLOR ROAD** 

LONGON N20 OHN

23p 23p 23p 12p 12p

4027

4029

42

74109 27p 4028

74110

48p 54p

BC549

BC557

BD1 kit (partially assembled)

Dimensions 15%in x 14%in. x 5%in

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### Connoisseur now offer their famous BD1 Kit in a package deal.

The package consists of the BD1 Kit, SAU2 pick-up arm, plinth with anti-vibration feet, acrylic cover complete with hinges and friction lid stays, a pick-up mounting board, and all necessary screws, washers, etc. The plinth, cover and pick-up mounting board are all pre-drilled and ready for assembly.

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IO 4105-Single Beam 5MHz Oscilloscope

Name

1888

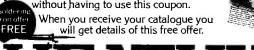
IM 2215

IM 5217 - Portable Multimeter

To: Heath (Gloucester) Limited, Dept. (PE 11), Bristol Road, Gloucester, GL2 6EE. Please send a copy of the Heathkit catalogue. I enclose 20p in stamps.

Address \_\_\_\_

N.B. If you are already on the Heathkit mailing list you will automatically receive a copy of the latest Heathkit catalogue without having to use this coupon.



REATRICT



#### **OPPORTUNITIES ABOUND**

WE ARE all, nowadays, electronics conscious. Yes, even the layman, while not conversant with the technicalities involved, has a general appreciation of the vital part played by this young but exuberant branch of electrical engineering in the complex world of today . . . and this is but the beginning.

"As we step over the threshold into a new exciting technological age, our dependence upon electronics is all too apparent: terrestrial developments centre around automation, with electronics providing the brain and guiding hand for power-operated machinery; extraterrestrial exploration relies utterly upon electronics for remote control, communications and telemetering services.

"These grand scale developments have an impact on the entire field of electronics, for in their wake come new components, new circuits, new methods and, of course, new applications."

Some might query the terms "young" and "the beginning" when applied to electronics and these are the only clues to the fact that those words were the opening paragraphs of the PE editorial in Volume 1 No. 2-back in December 1964! Whilst looking back to see how far we have come over the past 15 years what is most apparent is that we are still part of a relatively young and most certainly exuberant industry.

#### **NO BOUNDS**

The introduction of the transistor-just making a significant impact on the hobbyist market back in '64-has led us into an electronics world which knows no bounds and. while progressing at breakneck speed five years ago is now going twice as fast.

That editorial continued in the following way:

Without a doubt the amateur enthusiast will be eager to reap his share of these benefits of technological progress, as he has been indeed in the past. For it is true that amateurs have been conducting experiments and building electronic equipment since the earliest days of radio communication; even before the thermionic valve drove the crystal diode into (temporary) oblivion, and long before the very term 'electronics' entered into general use.

"But, in more recent times, the technical revolution triggered off by the invention of the crystal triode or transistor some 16 years ago has quite dramatically transformed the situation to the advantage of the home constructor."

The crystal triode! We wonder how many readers using microprocessors know how a triode works.

#### **30 YEARS ON**

Only about 30 years from the discovery of transistor action we are able to put about 100,000 semiconductor devices in the area originally required for one.

If that first 16 years progress "dramatically transformed the situation to the advantage of the home constructor" just think what the last 15 years have done. Far from putting us "out of business", as some intimated when i.c.s. became readily available, the hobby has grown in both numbers and complexity and now forms a significant market for the component industry.

We fully expect the next 15 years to be even more rewarding.

Mike Kenward

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#### **Technical Queries**

We are unable to offer any advice on the use or purchase of commercial equipment or the incorporation or modification of designs published in Practical Electronics.

All letters requiring a reply should be accompanied by a stamped, self addressed envelope and each letter should relate to one published project only.

Components are usually available from advertisers; where we anticipate supply difficulties a source will be suggested.

#### **Back Numbers**

Copies of most of our recent issues are available from: Post Sales Department (Practical Electronics), IPC Magazines Ltd., Lavington House, 25 Lavington Street, London SE1 OPF, at 75p each including Inland/Overseas p&p.

#### **Binders**

Binders for PE are available from the same address as back numbers at £3.75 each to UK or overseas addresses, including postage and packing, and VAT where appropriate. Orders should state the year and volume required.

#### Subscriptions

Copies of PE are available by post, inland or overseas, for £10.60 per 12 issues, from: Practical Electronics, Subscription Department, Oakfield House, Perrymount Road, Haywards Heath, West Sussex RH16 3DH. Cheques and postal orders should be made payable to IPC Magazines Limited.

# SOLID STATE CAR INSTRUMENTS No.2 REV. COUNTER

#### Michael Tooley B.A. David Whitfield B.A. M.Sc.

The second article in a series of car instrument constructionals using the LM3914 (discussed last month), and which produce an l.e.d. bar display

MEASURING the rate at which the engine turns over is something which on first thoughts might not appear to be of much practical interest to the average motorist. In fact it is a very useful facility in both engine tuning and everyday driving situations.

In order to obtain optimum performance, it is necessary to drive at an engine speed which produces the maximum torque for that particular engine (the torque produced by an engine tends to decrease at high and low revs). The average saloon car performs best at approximately 2,000–3,000 r.p.m. and driving at this rate will produce optimum fuel consumption and acceleration for that particular gear. Indeed, one of the reasons for the increasing popularity of the 5speed gearbox is that it allows driving nearer to this optimum rev's while at higher road speeds.

Another point of interest is that the forces exerted on the engine unit vary with the square of the engine rev's, i.e. doubling the r.p.m. increases the forces on, say, the rocker gear by a factor of 4. Hence, it is important that the maximum r.p.m. rating for a particular engine is not exceeded, irrespective of road speed.

In engine tuning, it is often necessary that certain measurements (e.g. ignition timing advance) are carried out at known engine speeds. Also the "tickover" speed should be adjusted so that the engine does not waste fuel while idling, yet moves off smoothly when required.

#### **MEASUREMENT OF RPM**

Measuring the engine r.p.m. would seem to require some type of transducer which is connected to the engine crankshaft. A little thought, however. soon shows that there is usually one already fitted; the *distributor!* The distributor shaft in a 4-stroke engine rotates at exactly half of the engine speed, and is responsible for the opening and closing of the contact breaker points. The contact breaker causes a pulsed signal to be produced across the primary (LT) winding of the ignition coil. The number of pulses produced per minute will be:

#### $\frac{1}{2}$ x r.p.m. x number of cylinders

All that is now required is a circuit to count these pulses and turn the result into an analogue signal which is suitable for driving the display module input, i.e. 0 to +5 volts for the required full scale.

Pulse counting by digital methods is one obvious way of determining contact breaker rate. This approach, however, requires a minimum of three to four i.c.s and also involves a stage of digital-to-analogue conversion, see Fig. 1a for details. A simple charge pump alternative (Fig. 1b) has the advantage of simplicity, but suffers the disadvantages of additional sensitivity to both pulse width and amplitude. These problems may be overcome by the incorporation of a monostable prior to the charge pump (Fig. 1c). With a monostable pulse width which is less than the periodic time of the input pulse train, the output of this new arrangement will now only depend on the input pulse frequency. The response time and full-scale values may then be set by a suitable choice of R and C, and of the monostable pulse width. A derivative of this approach is used in the integrated frequency-to-voltage converter produced by National Semiconductor and used in the r.p.m. counter to be described below.

#### FREQUENCY-TO-VOLTAGE CONVERTER

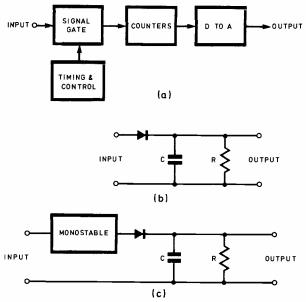
National Semiconductor's LM2917 is a linear monolithic i.c. which contains a frequency-to-voltage converter, together with a high gain op amp/comparator designed to operate a relay, lamp or other external load, up to 50mA. The tachometer section uses a charge pump technique and offers frequency doubling for low ripple, input protection, and an output which falls to ground level for a zero frequency input.

One of the main aims in the design of the LM2917 was ease of use. A single RC network provides the frequency doubling (see Fig. 2), and the output is simply related to the input frequency by the following formula:

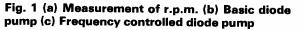
#### Vout = Fin x Vref x Ra x Ca

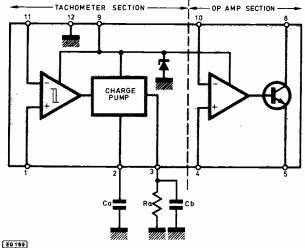
The integral voltage regulator sets the value of Vref and ensures accurate, stable conversion performance.

The input stage is a differential amplifier driving a positive feedback flip-flop circuit. This arrangement allows the user to define the input switching level, while retaining the hysteresis around that level to ensure good noise rejection. Following the input stage there is a charge pump where the input frequency is converted to a d.c. voltage. This operation requires a timing capacitor (Ca), an output load resistor (Ra), and an integrating filter capacitor (Cb). The capacitor Cb determines the trade-off between output ripple voltage and response time of the circuit.



EG190





#### TACHOMETER

The circuit diagram for the complete tachometer is shown in Fig. 3. The input is taken from across the ignition coil and applied to the input of the frequency-to-voltage converter, IC1, via the filter formed by R1, R2 and C1. The input switching level is set by R4 and D1, and consequently the input level must exceed approximately 0.6V before the signal will be recognised.

The output voltage varies depending on the input frequency and on the values of the frequency doubling capacitor. C2, and the composite load resistor, R3 and VR1. The values of these components are chosen such that the output of the circuit is 5.0V when the maximum r.p.m. is reached. This arrangement ensures that the circuit is compatible with the standard display module. Values are given in Table 1 for various maximum r.p.m. ranges and differing numbers of engine cylinders. VR1 may be omitted if desired and the load provided by a single fixed resistor R3.

The response time of the circuit is set by C3; increasing the value of C3 will increase the response time, and vice versa. The dropper resistor for the internal Zener regulator, R5, is chosen to minimise the reference voltage variation over a supply range of 9 to 16V. The remainder of the circuit is the standard display module.

#### **CONSTRUCTIONAL NOTES**

The overall construction of the tachometer closely follows the pattern of the battery condition indicator described last month. Once again only two examples of possible implementations are discussed in detail. A printed circuit design is shown in Fig. 4, and a component and connection diagram is shown in Fig. 5. A corresponding stripboard layout is shown in Fig. 6.

The display mode which appears most appropriate for a tachometer is the bar graph, and these are the connections shown in Figs. 5 and 6. Constructors may wish to colour code the individual l.e.d.s to suit their own taste and engine specifications, e.g. green for the first 8 l.e.d.s, orange for the 9th, and red for the last one. In cases where the l.e.d.s are to be mounted in a circular arc (possibly concentric with the speedometer), it may be desirable to increase the display to 20 or even 30 l.e.d.s by use of additional LM3914 devices. These techniques will be discussed in a later article.

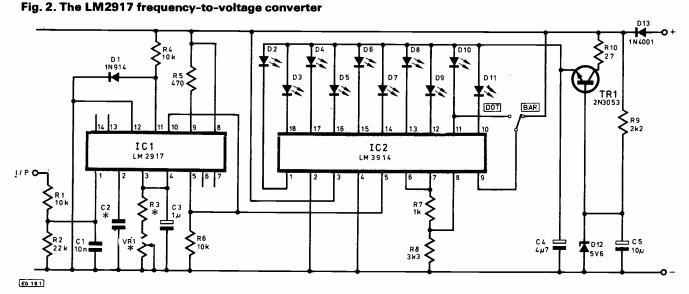


Fig. 3. Full circuit diagram of the Rev. Counter.

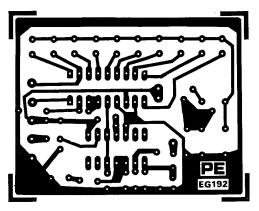
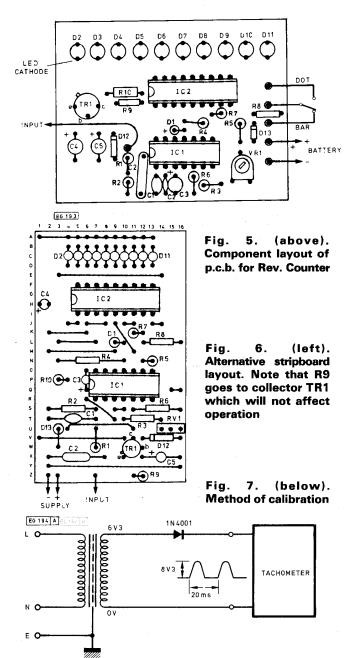


Fig. 4. Printed circuit layout (actual size)



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In most applications the component values given in Table 1 should be enough to ensure adequate calibration of the tachometer. VR1 may be replaced by either a link or a suitable fixed resistor to make up the required total load resistance. However, in situations where a high degree of accuracy is required, some form of calibration procedure is necessary. The first step in such cases is to work out the pulse frequency which corresponds to the maximum indicated r.p.m. This may be found from the following equation for max pulse frequency:

maximum indicated r.p.m. × No. of cylinders	Hz
120	112

Table 1. Vi (R3 + VR1), a			osite	load	resi	stance
<ul> <li>Maximum Ind</li> </ul>	licated C	2 = 10	nF	C2	= 22n	F
RPM	4 cyl	6 cyl	8 cyl	4 cyl	6 cyl	8 cyl
1000	1984	1323	992	902	601	451
2000	992	661	496	451	301	226
3000	661	441	331	301	200	150
4000	496	331	248	226	150	113
5000	397	265	198	180	120	90
6000	331	220	165	150	100	75
7000	283	189	142	129	86	64
8000	248	165	124	113	75	56

#### COMPONENTS . . .

#### Resistors

R1, R4, R6	• ·	10k (3 off)
R2		22k
R3		see text
R5		470
R7		1k
R8		3k3
R9		2k2
R10		27 ½W

All resistors 1W 5% except where stated

#### Potentiometers

VR1 See text for value. Hor. preset for p.c.b., vert. preset for stripboard

#### Capacitors

C1	ceram	

- C2 see text
- C3 1µ elect
- C4 4µ7 elect
- C5 10µ elect

#### **Transistors and Diodes**

1N914 I.e.d.s to suit physical requirement BZY88C5V6 400mW Zener 1N4001 2N3053
2N3053

#### **Integrated Circuits**

IC1 LM2917 IC2 LM3914

#### Miscellaneous

Printed circuit board (or 0-1 inch stripboard:  $70 \times 45$ mm) Suitable moulded case

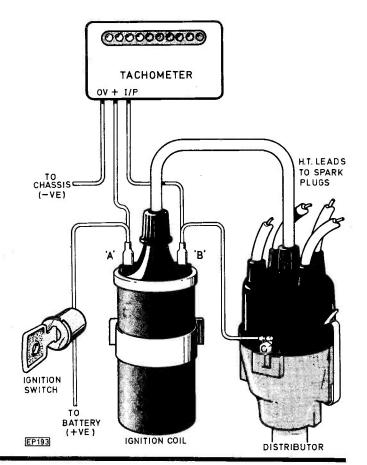
This, for example, gives 200Hz for a 4-cylinder engine at 6,000 r.p.m. A direct method of calibration is then to use a pulse generator to apply a 200Hz square wave (greater than three volts amplitude) to the input, and then adjust VR1 to give  $5 \cdot 0V$  across R6. Should a pulse generator be unavailable, a suitable mains (filament-type) transformer may be used to generate a 50Hz signal, and VR1 is then adjusted to give an appropriate proportion of  $5 \cdot 0V$  across R6, e.g.  $1 \cdot 25V$  (i.e. fifty 200ths of  $5 \cdot 0V$ ) in the case of a 6,000 r.p.m. 4-cylinder tachometer. See Fig. 7 for details.

#### INSTALLATION AND USE

Connecting the tachometer to the engine ignition system is a very simple operation. Fig. 8 shows how the supply (A) and measurement input (B) leads are connected across the ignition coil; the OV connection being made to any convenient point on the vehicle chassis. In cases where the instrument is to be used as a piece of test equipment, switched values of load resistance may be provided for different ranges/numbers of cylinders, and connections brought out on flying leads with crocodile clips.

The tachometer has been successfully tried on a variety of British and foreign vehicles. Constructors should, however, be aware that for vehicles already fitted with a *current* pulse type of tachometer (e.g. *Smiths type RVC*), the readings obtained may tend to be rather misleading.

NEXT MONTH: Battery Current Indicator, Temperature Gauge, Dwell Indicator. All three car instruments form a special supplement with details on extending the displays and on providing extra warnings of high level readings



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ems mentioned are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned. All quoted prices are those at the time of going to press.

by Alan Turpin

#### **FULL FRONTAL**

These BIMDICATORS were designed to satisfy applications requiring indicators with a restricted viewing angle, long operating life, and good aesthetic qualities.

Both devices utilise red, green or amber l.e.d.s which are set back from the front of the indicator and have low current, low voltage characteristics, fast switching times, and are fully i.c. compatible.



The BIM 33 l.e.d. (left) has a nickel plated brass body and is panel mounted in a 6mm dia. hole. The BIM 34 l.e.d. has a chromium plated brass body and is panel mounted in an 8mm dia. hole.

Prices inc. VAT and p&p, for either size are: Red—71p, Green or Yellow—81p.

BOSS Industrial Mouldings Ltd., Higgs Ind. Est., 2 Herne Hill Road, London SE24 0AU (01-737 2383).

#### **FIRST CLASS CATALOGUE**

The Toolrange catalogue is excellently designed and printed. Over a hundred pages, most of them in colour, show a comprehensive range of tools which the serious constructor would be interested in knowing about. No need to send an SAE.

Toolrange supply tools and production aids for the electrical and electronic industries and their address is **Toolrange Ltd.**, Upton Road, Reading, Berks., RG3 4JA (0734 22245).

#### CSC

A new 32 page catalogue from Continental Specialties Corporation features the company's ranges of breadboarding equipment, logic testing devices, and test instrumentation. Products featured include a wide range of solderless breadboards and breadboard assemblies, test clips, instrument cases, pulse and function generators, frequency counters and accessories, logic probes, logic monitors, the CSC digital pulser, test kits and probe kits.

The catalogue is available from Continental Specialties Corporation, Shire Hill Industrial Estate, Saffron Walden, Essex CB11 3AQ



#### **AEROSOLS FOR ELECTRONICS**

Switch cleaning aerosols by Servisol are now available from Toolrange. Other aerosols in the range are anti-static cleaners, water proofing sprays, insulating varnish sprays and chemical circuit freezers. Prices average out at 70p per can.

Toolrange Ltd., Upton Road, Reading, Berks., RG3 4JA (0734 22245).

#### **MICRO-KIT CONSTRUCTION**

If you would like a microprocessor system but are daunted by the assembly then Logsign may be of interest.

Logsign will obtain and build a kit: construct a kit supplied by a customer; even undertake to finish a kit which has proved problematical.

Charges start at around 10 per cent of system value for the most popular kits such as Nascom, Compukit, Newbear 77/68 etc., rising to around 25 per cent for large systems like Horizon.

Logsign Microcomputer Engineers, P.O. Box 33, Truro, Cornwall, TR3 6BZ. (0872 76205).

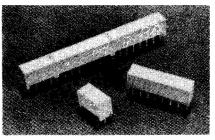
#### LIGHT BARS

and

David

Shortland

For those of you who are intending to construct the "car devices" currently being published by us, this new range of modular l.e.d.s should be of interest.

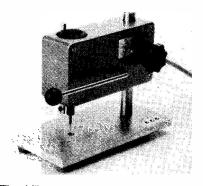


The HLMP 2300, 2400 and 2500 series of 9 to 19mm rectangular devices can be multiplexed and are X-Y stackable. Composed of two or four in-line l.e.d.s with the light from each l.e.d. optically scattered to form an evenly illuminated light emitting surface, these devices may be strobed at high peak currents or driven from d.c. supplies. Available in red, yellow and green the HLMP 2300, 2400, and 2500 are priced from 97p exc. VAT and p&p.

For further information contact Hewlett Packard Ltd., Kings Street Lane, Winnersh, Wokingham, Berkshire RG115AR.

#### **HIGH SPEED DRILL**

A new high speed drilling machine which is ideal for use in p.c.b. prototype workshops had just been announced by Linton Laboratories. The Junior Drillmaster which is mains operated has a motor speed of 14000 r.p.m. with a drill capacity of 206mm dia.



The drill, which is supplied with a guard and four separate collets (0.5 to 3.2mm), is priced at £65 inc. p&p, plus VAT.

Linton Laboratories Limited, 4 Bartlow Road, Linton, Cambridge, CB1 6LY.



#### JVC STEREO RECEIVER

The photograph shows JVC's R-S7, an AM/FM receiver which delivers 50W per channel r.m.s. with both channels driven into 8 ohms, from 20Hz to 20kHz. The THD is no more than 0.03 per cent and a phono equaliser ensures a signal to noise ratio of 90dB.

The R-S7 has a protection circuit which prevents power on/off noise from reaching the speakers, disconnects the speakers electronically if an abnormal d.c. voltage appears at the terminals and protects the power transistors from short circuits, low speaker impedances, etc. Retail price is around £203 (inc. VAT).

#### AM/FM/CB RECEIVER

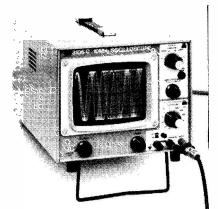
A Hong Kong manufactured receiver labelled Bristal has been under appraisal at the office recently. It is said to comply, as of date of manufacture, with FCC rules and regulations part 15 subpart C.

As well as receiving legal transmissions from the British Broadcasting Corporation it is rumoured that if you switch the Bristal to CB you might hear French, Spanish and Italian CBers as clear as next door, probably a combination of skip and spaghetti burners.

The set measures  $185 \times 90 \times 50$ mm, has a telescopic aerial one metre long, and has been seen for sale at £18.95 plus VAT.

#### **10MHz Scope**

The 3106C oscilloscope is a general purpose single trace instrument which has been designed for college labs, service shop repair and production line testing.



The instrument features a 5in flat c.r.t., d.c. to 10MHz bandwidth, vertical amplifier with a sensitivity of 10mV to 50V/cm in 12 calibrated steps,  $0.5\mu s$  to 0.01 sec/cm sweep range and a times five magnifier. The price of the 3106C is £159.95 including VAT, carriage is £2.50.

Kramer & Co., 9 October Place, Holders Hill Road, London NW4 1EJ (01-203 2473).

#### **3rd HAND**

The 3rd Hand is a rather aptly named p.c.b. holder which can be clamped on the edge of a bench, table or worktop. The p.c.b. is held in position by an open ended clamp which allows any size of board to be held. When in

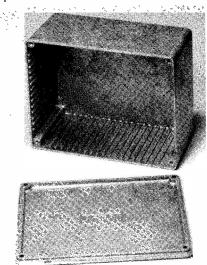


position the board can be flipped over to allow access for soldering and clipping.

The cost is £8.95 including VAT and p&p. Para Sales, 1 Hook Road, Kingsclere, Newbury, Berks. RG15 8PD.

#### P.C.B.s ACCEPTED

This diecast aluminium box incorporates slots on all four sides for quick housing and removal of 1.8mm thick p.c.b.s. Dimensions of the box are  $121 \times 95 \times 61$ mm. Grey hammertone is a shortly to be introduced optional finish.



BOSS Industrial Mouldings make a range of this type of box called BIMBOXES. This size is  $\pounds 3.45$  inc. p&p and VAT.

BOSS Industrial Mouldings Ltd., Higgs Ind. Est., 2 Herne Hill Road, London SE24 0AU (01-737 2383).

#### **CRYSTALS MADE TO ORDER**

Golledge Electronics stock a very good range of crystals for microprocessors, markers, clocks, marine VHF, radio control, etc. They can supply crystals made to order, normal delivery six weeks.

Golledge are also designers of a range of "building block" modules which require only simple external connections and can be made to work well by anyone with little or no experience of radio construction.

Leaflets on the crystals and the modules are available from Golledge Electronics, G3EDW, Merriott, Somerset TA 16 5NS (0460 73718).



This is Ingersoll's latest clock radio waker upper. It has a 12 hour l.e.d. display and will wake you with the three band radio or a nine minute repeating buzzer. For the listener who falls off to sleep it has a 60 minute shut off timer. It is mains operated, has a power failure indicator, and is finished in either teak or satin silver. The price is £30.65 inc. VAT.



**B**ABYCOM is a two unit monitoring system for the nursery. It consists of a control unit with a microphone, which should be placed near the cot and an alarm unit which can be placed anywhere else in the house. The two units are joined together via a 3 core flex.

The alarm is triggered by sound, the microphone picks up the baby's cries and the control unit of the system which contains a 5-bit shift register records the noise as a "1". After 10 secs the contents of each register (A, B, C, D and E) are shifted along (A to B, B to C etc.) with any new noises being entered into register A whilst the information in register E is erased.

For the alarm to sound the baby must trigger it twice (two registers at 1) within a 50 sec. period. When triggered the alarm will sound for one period and then stop unless the baby makes any further noises in which case it will continue to sound until the baby settles down and one or less of the registers is at "1". When the alarm sounds you can listen in to the baby by pressing the switch S3 on the alarm unit.

#### CONTROLUNIT

The circuit diagram of the power supply and the control unit is shown in Fig. 1. The circuit is powered via transformer T1, rectifier diodes D1 and D2, smoothing capacitors C1 and C2 and a regulator circuit formed by TR1, R1 and Zener diode D3.

Any noise picked up by the microphone via JK1 is amplified by IC1 and then fed to the detector circuit of which TR2 and TR3 form a high gain amplifier. If the output of IC1 is above a certain level (when a loud enough sound is detected) the collector of TR3 is switched "high". The output level of IC1 at which this will occur is determined by the setting of VR1, the sensitivity control.

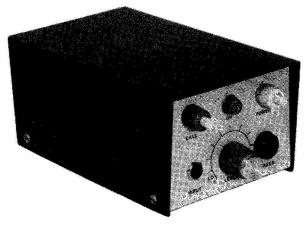
The two timers of IC2 are connected as two astable multivibrators. One timer runs at approximately 1Hz, with 2:1 mark-space ratio and the other runs at approximately 0.1Hz, its output waveform being "high" with very short clocking "lows" every 10 secs. The frequencies are nominal and the clocks can be set accurately enough by suitable choice of timing capacitors and resistors; there is no need for variable preset timing resistors. The logic circuit comprises the 7496 5-bit shift register and the 7425 dual 4-input NOR gate with a strobe input. The output from the detector circuit (collector TR3) is fed to the preset input of register

A (IC3 pin 2). The common preset input (pin 8) is held high by Vcc so that the output of register A (pin 15) goes "high" immediately register A receives a "high" input. Preset inputs of the other registers (pins 3, 4, 6 and 7) are grounded, so that these registers have a "low" output at switch-on.

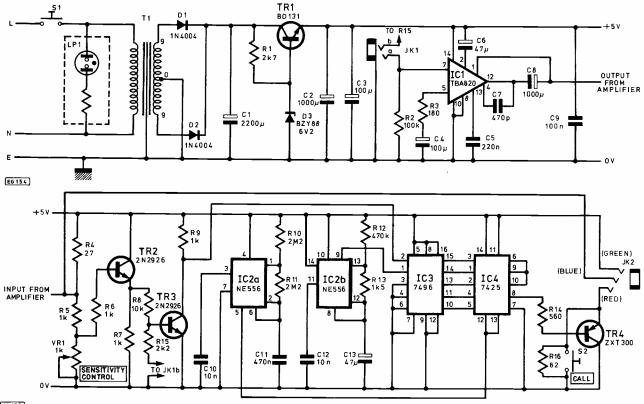
If any noise is detected during a 10 sec. period the output of register A goes "high" and remains high until the end of that period. Then the clock pulse steps the data through the registers.

The NOR function of IC4 operates only if the strobe input (pin 3) is "high". If the input is "low" the gate output is "low" whatever the state of its four inputs. The first NOR gate receives its strobe input from register A and its four inputs from registers B to E. If register A is low (no noise during the 10 sec. period), the gate output is low, irrespective of the other registers. But if register A goes "high" what happens next depends on the state of the other registers. If these are all "low" (no noise during previous four periods), the output remains "low" (no alarm). If any one or more of these are "high", the gate output goes "high", switching on TR4. At the end of the period TR4 is switched off as the output of register A goes low, unless of course baby makes further noises.

The second NOR gate of IC4 has its strobe input (pin 11) permanently wired to Vcc and is wired to function as an



The control unit



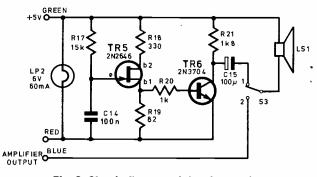
EG 155

Fig. 1. Circuit diagram of the power supply and the control unit

ordinary 2-input NOR gate. This receives inputs from the first NOR gate ("high" = alarm) and from the 1Hz clock. In the "no alarm" state the output of this gate is continuously "low". In the alarm condition, the output of this gate is the inverse of the clock output. The output is used to turn TR4 on and off regularly.

#### **ALARM UNIT**

The alarm unit (Fig. 2) incorporates an oscillator and amplifier to produce the audio alarm tone. The frequency at which the oscillator operates can be varied by changing the value of C14. As TR4 is turned on the red lead of the alarm unit is connected to OV switching on lamp LP2, the oscillator and therefore the alarm. Switching TR4 on and off via the second NOR gate of IC4 causes the lamp to flash and the alarm to bleep.



**Fig. 2. Circuit diagram of the alarm unit** 

#### **FAIL SAFE**

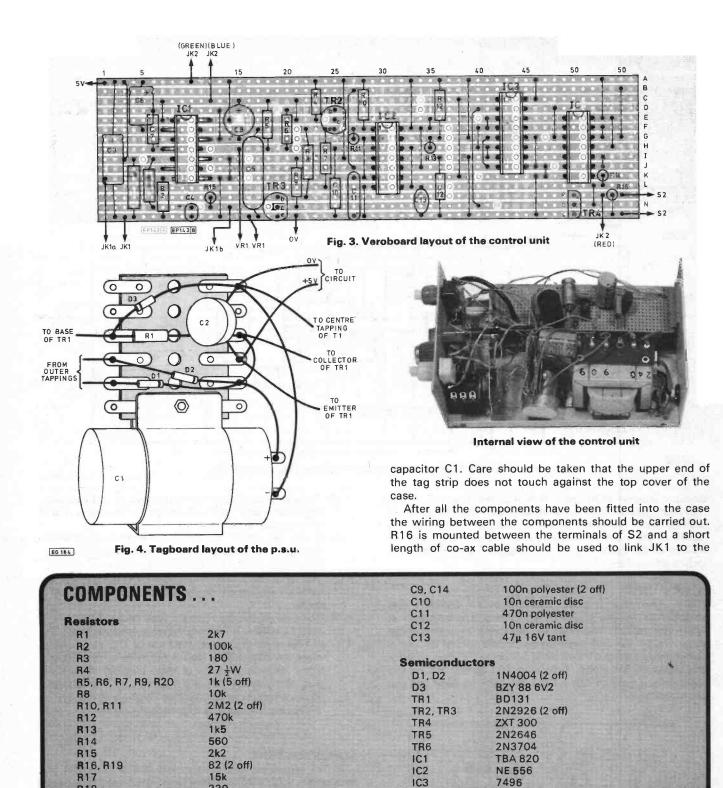
The unit incorporates a number of features to ensure that "no alarm" really does mean "no noise" and is not the result of a failure in the system.

- There is no volume on the alarm unit, so this cannot be turned down and then forgotten. Similarly, the lamp cannot be switched off.
- 2) In the "no alarm" condition a small current flows through R16, bypassing TR4. This current is insufficient to activate the AF oscillator but does cause LP2 to glow. If the unit is operating correctly the lamp should be either flashing brightly or glowing dimly.
- 3) One side of the microphone jack socket (JK1b) is used as switch 1 which is wired in series with R15 to TR3 so as to connect the base of TR3 to ground when the microphone jack is not in its socket. Thus if the microphone has not been plugged in, or its plug partly pulled out of the socket, TR3 is turned off, its collector potential goes "high" and a "high" will appear at register A triggering the alarm.

#### CONSTRUCTION

In the prototype, the control unit of the Babycom was housed in a  $175 \times 95 \times 70$ mm case. The front panel should be drilled and the panel components mounted into position. The Veroboard layout shown in Fig. 3 should be soldered next and then carefully checked to ensure there are no solder bridges or incomplete track breaks to short out the board. After the board has been checked it can be fitted as close to the back and one side of the case as possible using 6BA screws and spacers. Note that only one Veroboard is needed instead of the two used in the prototype

Transformer T1, the smoothing capacitor C1 and the "L" shaped heat-sink for TR1 should be fitted alongside the Veroboard with the transformer at the back of the case. The rest of the power supply circuit should then be mounted on a piece of tagboard (Fig. 4) and fitted to the clip holding



1C4

**T1 S1** 

**S**2

**S**3

LP1

LP2

LS1

JK1

JK2

MIC1

**Miscellaneous** 

7425

S.p.s.t. biased

Min jack socket

Stereo jack socket

240V neon

Push button, push to make

6V 60mA MES filament lamp

High impedance crystal microphone

Miniature speaker 8Ω

9-0-9V secondary 100mA mains transformer

Push button, push to make push to break

**R18** 

R21

VR1

C1

**C**5

**C6** 

**C7** 

Capacitors

C2, C8

C3, C4, C15

Potentiometers

1k linear

330

1k8

2200µ 16V elect.

220n polyester

47µ 10V elect.

470p ceramic

1000µ 10V elect. (2 off)

100µ 10V elect. (3 off)

All resistors 1 W 5% unless otherwise stated

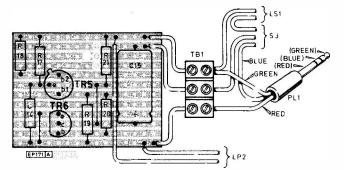


Fig. 5. Veroboard layout of the alarm unit

amplifier on the Veroboard layout.

The prototype alarm unit of the Babycom was housed in a  $130 \times 100 \times 50$ mm case. The Veroboard layout of the alarm circuit is shown in Fig. 5. After the board has been



#### INTELLIGENCE PRINTS BACKWARDS

**SOMETHING** of a price breakthrough is the Trendcom 100 Intelligent Printer from Personal Computers Ltd. A high performance serial printer capable of 40 char's/sec, the Trendcom 100 has a 96 character set and is controlled by its own internal microprocessor.

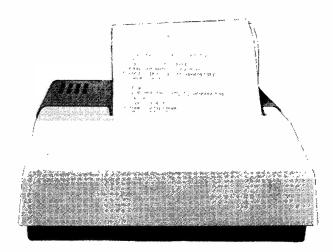
To speed things up, each line of characters is stored ready to be printed, and when summoned, may be printed from left-to-right or right-to-left, so that in effect the print head is quietly zig-zagging its way down the paper (known as bidirectional look-ahead printing).

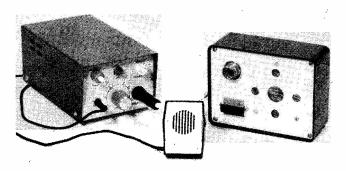
Print-out is aesthetically pleasing (10 char's/inch) based on a  $5 \times 7$  dot matrix onto low cost thermal paper. High reliability is inherent with only two d.c. stepping motors to control the print head and paper roller, and everything is powered from its own mains supply.

Interfacing to most microcomputers should be easy with TTL compatible inputs, and interface cards are available for PET, Apple II, TRS80 and RS232 ports. Signals available from Trendcom 100 are STROBE and BUSY. A Test input activates a self test message.

You may have seen printers with this kind of specification before, but here is the difference: Trendcom  $100 costs \pounds 241$ .

Personal Computers Ltd., 194-200 Bishopsgate, London, EC2M 4NR.





#### The complete Babycom system

soldered and checked it should be fitted into the case with the loudspeaker, indicator lamp and switch S3 fitted into the front panel. The alarm unit is joined to the control unit via 3 core cable and PL1.

#### **ONE-CHIP COLOUR TV SYSTEM**

MOTOROLA Semiconductors announce a European designed, multistandard TV colour system, the TDA 3300, Chroma III, one-chip colour system.

This third generation system accepts a colour TV signal in the form of composite video and gives an output ready for application to the c.r.t. cathode, via a simple output stage.

Included on-chip are a number of features which, Motorola believes, will make the TDA 3300 one of the most sophisticated integrated TV systems yet available. Key features of the system are:

User Controls—The device includes a full range of user controls, saturation, contrast and brilliance, which have been designed with a high input impedance, in the order of  $1M\Omega$ , and an operating range of 0 to 5V. This makes them compatible with Motorola and other Remote Control systems via a simple RC network.

Beam Limiting—An on-chip beam limiter automatically adjusts the output drive to prevent blooming of the picture detail highlights.

Reference Generation—For simplicity the system uses the easily obtainable 4.43MHz crystal for the reference frequency generation. Further, the 90° phase shift is accomplished on-chip by an unique self correcting circuit which will keep phase errors down to a minimum.

Automatic Black Level Setup—By sampling the c.r.t. cathode current the system is able to adjust dynamically the tube black level throughout its life, thus eliminating three complex adjustments during the set manufacture.

Full Multi-standard Capability is available as PAL and NTSC, the latter being aimed at the video recorder user. However, this is extended to SECAM with the soon to be announced TDA 3030 SECAM decoder.

On-Screen-Display—In order to take full advantage of the range of facilities available to the current and coming generation of TV sets, Teletext, games, camera, etc., the TDA 3300 includes on-chip, RGB on-screen-display inputs and the associated fast blanking inputs.

In spite of all these facilities the TDA 3300 requires a single 12V power supply and has low current drain of 50mA.

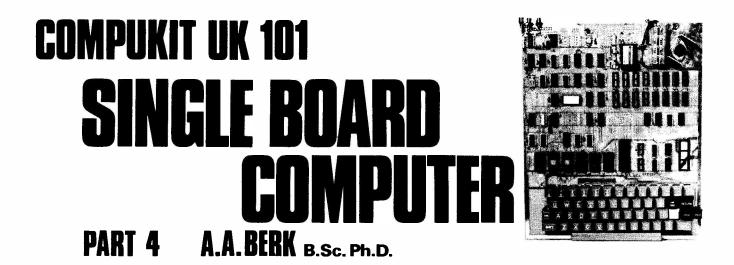
### **POINTS ARISING**

#### AUTORANGING MULTIMETER . (April-May 1979)

The diodes D2 and D3 (BAV 47) may be replaced by BAV 45s which are available from Acc Mailtronix Ltd. Tootal Street, Wakefield, West Yorkshire.

CONSTANT DISPLAY FREQUENCY METER (August 1978)

A link should be made between the centre pin of IC17 and C4-ve.



#### **CONCLUSION OF SERIES**

A<sup>S</sup> INDICATED in the previous articles, the Compukit is hardware expandable in many ways. Expansions to the machine are in the process of being produced and include a Colour Graphics Board, and a large memory board which will bring the machine nearer to its maximum addressing ability in RAM and EPROM/ROM. By the time this article appears, these boards should be available.

Software expansions include a sophisticated Machine Code Monitor, disassembler and assembler which is included with the machine. Many programs, including games, already exist and it is hoped that others will become available in the near future from those software houses which have shown interest in the machine.

The hobbyist who wishes to expand the hardware of the machine himself may be interested in two useful and important methods of doing so. These are described below. Firstly, it is essential to bear in mind a picture of the machine's memory map:

When expanding the system or adding I/O ports, certain addresses are used for specific functions and must not be overlapped. It is also important to allow for future expansions by keeping clear of memory space which may eventually house extra RAM. In general, later expansion boards will add memory consecutively with the 8K of on-board RAM, so that the BASIC interpreter will find it during the usual memory test when C is pressed after Reset.

To decide on suitable addresses, the Address Map shown in Table 4.1 should be consulted. The addresses given are in hexadecimal notation and, as can be seen, BASIC workspace can be as large as 40,191 bytes (0300 to 9FFF) before overlapping with the BASIC ROMs. There is plenty of space

Table 4.1. Memory map.				
Address	Function			
0130	NMI vector			
01C0	IRQ vector			
0000-02FF	Scratchpad RAM for operating system			
0300	Start of BASIC workspace			
1FFF	End of on-board RAM (8K)			
A000–BFFF	BASIC interpreter			
D000-D3FF	Video RAM			
DF00	Polled keyboard			
F000, F001	ACIA serial port			
F800-FFFF	MONITOR ROM			

from C000 to CFFF (4096 bytes), and from D400 up to F7FF, apart from the keyboard and ACIA. It is in this last portion that parallel or serial I/O ports can be neatly added with less danger of interfering with later additions.

In order to expand the Compukit, therefore, a certain amount of address decoding is necessary to locate any peripherals at the right place in the machine's memory. There are two main ways in which this may be achieved. The top 1K of the 8K of RAM (ICs 38 and 52) may be left unused and its address decoded output (RS7) supplied to the expansion as an ENABLE signal. A more general method is to add an expansion board to the system containing its own address decoding. Both of these are described.

#### **PARALLEL I/O PORTS**

Suppose we wish to add 16 I/O ports to the machine in the most straightforward manner possible for some control purpose. A 6820 or 6821 (with greater drive) is most suitable for the job. This chip is the famous PIA or Peripheral Interface Adapter containing a number of I/O drivers and latches as well as several control lines.

A couple of d.i.l. plugs will allow the circuit in Fig. 4.1 to be connected to the Compukit with minimum effort to control almost anything. The circuit shown includes some lights and switches—just imagine the l.e.d.s to be relays and the switches to be sensors of some kind.

To use Fig. 4.1 and appreciate the circuit's full potential, the data sheet for the device must be obtained and studied. This is a very useful chip and each of its sixteen I/O lines (PBO-PB7 and PAO-PA7) may act as either input or output. There are four external control lines for various purposes (CB1, CB2, CA1, CA2), and interrupts, via IRQ, may be generated by external devices. In order to use the chip, which looks life four memory locations (here decoded as 1C00, 1, 2, 3) internal registers must be set to a pattern of bits which informs the device of those lines which are to be inputs, and which are outputs. Data to be written to outputs is sent to the appropriate location within the PIA which subsequently clocks it through to the output latches. Similarly, incoming information is stored in a register and may be retrieved by reading the correct memory location in the PIA at the program's convenience. The Interrupt structure may be used to force the MPU to "look" at the PIA when an external device sends its information through.

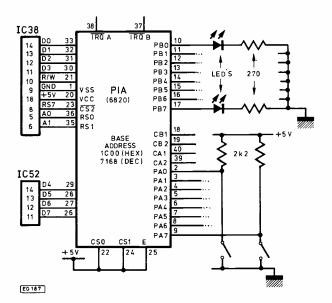


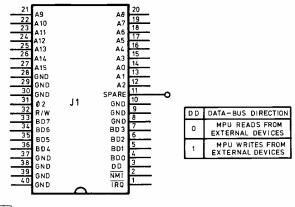
Fig. 4.1. Switches and lamps interface

An interesting feature of such a device is that the time taken to change an input line to an output is similar to the instruction speed of the MPU system driving it. This allows the possibility of swopping between input and output very fast to make any given line (or lines) appear to the operator as if it is performing both functions simultaneously. Handshaking between microcomputers can be arranged in this way, and parallel processing by a set of machines may be envisaged.

The interface in Fig. 4.1 may, of course, be adapted to run many other devices including UARTs, USARTs or just tristate buffers and TTL latches. In fact, by using the lower ten address lines from IC38 and IC52, any 1K (or less) memory mapped device may be attached to the Compukit. So far, the author has successfully driven the PE VDU and the coming EPROM Programmer. The advantages of using BASIC to control these devices are enormous. Tasks which appear most daunting when a machine code microcomputer is used, become almost trivial in the high level language.

Several extra terminals may be added to the basic machine in this way, adding considerably to the system's viability in small business applications.

However, the above expansion method, though quick and easy to implement, does tie up 1K of on-board RAM for each expansion used, and as such may be regarded as



EG 186

Fig. 4.2. Expansion connector

wasteful in the long run. This should lead the user to attach his peripherals to the machine via the 40-pin d.i.l. socket J1. The specifications for this socket are given in Fig. 4.2. All bus lines are brought out to the socket, and they allow external memory mapped devices to communicate with the MPU directly. The BD lines are buffered data lines, with direction controlled by the DD signal which selects Read or Write through ICs 6 and 7 as shown in Fig. 4.2.

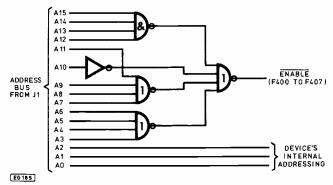
All sixteen address lines are present, as is R/W, IRQ, NMI and  $\emptyset 2$ . For correct memory timing this last signal should be fed to an *active high* enable line from all external devices. There is also one spare line not connected to anything, but brought out to a pad next to the socket. The rest of the pins are Ground connections.

To use this socket, each external device must generate its own address decoding, the details of which depend upon the amount of memory each expansion takes up. Any such device should occupy a unique address position and hence each address line must be involved in its "fetching".

For devices taking up 8 bytes of memory, for instance, Fig. 4.3 gives a straightforward method of decoding. Here, the 8 bytes are arranged to lie at F400 to F407.

This particular circuit is, of course, purely a functional *suggestion* to highlight the fact that NAND gates decode 1's and NOR gates decode O's, and that all address lines play some part in decoding the base address of F400.

Thus, small memory requirements are easily catered for using the simplest logic devices. It is usually a good idea to use CMOS or LS i.c.s to reduce bus loading.



#### Fig. 4.3. Address decoder for 8 bytes

For large memory requirements, the n to 2<sup>n</sup> line decoders such as 74LS138,9 and 74154 are extremely useful. A 24K memory board, for instance, will need its own internal pageselect logic to enable different banks of memory i.c.s, just as the Compukit itself does, via some of the above decoders.

For general hardware control purposes, the Compukit may be operated in either BASIC or machine code. The latter can be considerably faster as it deals fundamentally with *electrical* steps. From BASIC, an I/O port can be controlled by the WAIT statement or using PEEK and POKE. This has the advantage of extreme ease of programming. Imagine controlling a home-security system. The program could continually PEEK a number of I/O ports (PIA perhaps) connected to remote sensors. When a change occurs, an IF statement would decide whether to act, and a few subroutines would decide which action to take. Some other sensors could be PEEKed nearby and, in a short time, an alarm could be sounded or a stream of appropriate invective produced via a speech synthesis unit!

Extremely complex programs with feedback and analysis could be constructed using the powerful BASIC involved, which, though not as fast as machine code, would act many orders faster than any human activity involved.

The speed problem becomes important, for example, in controlling high speed machines or processes. Then, a hybrid program using the USR function could swop back and forth between BASIC and machine code for *instant* response to requirements.

As the IRQ and NMI interrupts are fully available to the user, an even more sophisticated system is possible whereby the external process takes control of the computer, when needed, via an interrupt.

The potential is exciting and to some extent already being exploited. Anyone interested could do worse than construct an "I.e.d. and Switch" I/O expansion as in Fig. 4.1 and learn to use it! The next step would be to add a D/A or A/D converter and learn to control and receive analogue data in real time.

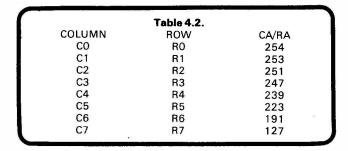
#### **SPECIAL KEYBOARD FUNCTIONS**

Referring to the keyboard matrix circuit diagram and hardware description, it has already been stated that the keyboard is polled in software for key closures except during program execution (unless waiting for an INPUT).

There are two important routines associated with the polling sequence. One determines which key has been pressed, and the other is a routine for detecting CONTROL C. The latter is not in general disabled during program execution, and may be used to BREAK a program for examining variables, etc. The routine involved may, however, be disabled or enabled by the user via the following statements:

#### POKE 530,1 disables POKE 530,0 enables

The first of these may be placed before a part of the program whose execution it is important not to be able to interrupt. If the second statement is placed at the end of the protected region, then CONTROL C will never intrude on that region if pressed.



The keyboard matrix may be used in special applications during the execution of a program, by treating it as an ordinary read/write memory location (57088 decimal or DF00 hexadecimal). To do this, it is often important to disable the CONTROL C routine to prevent it from interfering.

An example of the keyboard's use for special functions could be to allow the keys to be reprogrammed to return graphics characters. A program would be written to allow, say, all the "block" characters to be called from a section of the keyboard when SHIFT LOCK is up.

To perform any special programming of the keyboard, the following statements are used:

#### POKE 57088, RA IF PEEK(57088) = CA THEN (statement)

RA is the *address* of the row being tested for key-closures according to Table 4.2. This POKE statement may be thought of as "setting" the appropriate row to the "on" condition. CA, column address, is the value which location 57088 takes on when a key in the row RA is pressed. Thus if 57088 is POKEd to have value 254, and 57088 is then read (via PEEK) and found to have value 254 then the program knows that SHIFT LOCK is down (see the keyboard matrix diagram).

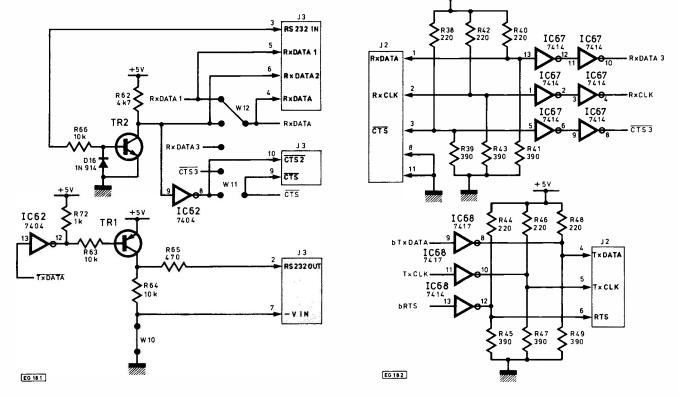


Fig. 4.4. (left) Asynchronous I/O and RS232. (right) Serial data buffers

The following program changes the keys 1 to 7 to graphic characters when SHIFT LOCK is up. When down, the words SHIFT LOCK roll up the screen until SHIFT LOCK is pressed. Then the keys 1 to 7 are active and each gives a different character until 7 is pressed when the program terminates.

#### 10 POKE 530,1 20 POKE 57088,254 30 IF PEEK(57088) = 254 THEN PRINT ''SHIFT-LOCK DOWN'': GOTO 20 40 POKE 57088,127 50 IF PEEK(57088) = 255 THEN 40 60 PRINT CHR\$( PEEK(57088) ); 70 IF PEEK(57088) = 253 THEN END 80 GOTO 10

The program, though rather simple, is meant to illustrate how information can be gathered from the keyboard and used to control execution. Note that in line 50 the keyboard location is assumed to have value 255 unless a key is pressed, as R1–R8 pull up the inputs to IC4 and IC5 and force them to "see" 1's until an active key is pressed.

The applications of the above are manifold, not least in the execution of games or simulation exercises; two areas which in many ways are very similar!

In order to use this keyboard polling easily, it is a good idea to label the keyboard matrix diagram, published in Part 1, with the CA and RA addresses corresponding to the columns and rows. For instance, CO and RO should be labelled 254, C1 and R1 253, etc.

This concludes the description of the Compukit UK 101. By the time this article appears, many readers will have had the opportunity of operating the basic machine. The applications are enormous and stretch across the full gamut of endeavour. It is hoped that through the pages of *Practical Electronics*, future developments can be described as they occur and thus keep readers up to date with a machine considered to be ahead of its time.

It only remains for us to wish you all good luck with the project.  $\bigstar$ 

CO	MPUK	IT CIRCUIT DIAGRAMS
Fig. No. 2		Block diagram
3		Keyboard matrix and interface
4		Power supply
2	-1	Component layout
2	-2	VDU interface
2	.3	Cassette interface
2	.4	The uP and expansion socket
2	.5	Clocks
3	-1	BASIC ROMs
3	.2	Monitor ROM
3	-4	8K RAM
3	.5	Address decoding
4	-2	J1 pin-outs
4	-4	Serial interface

#### MORE!

Next month we will publish Part 1 of an EPROM programmer designed to plug into Compukit—it will also function with other computers. We also expect to be able to publish another exciting computer peripheral in the near future—we do not believe this has previously been published as a hobby design—more details in future issues.



**Satellite Communications** (conference)—Oct. 30, 31, London Press Centre. Will "tele conferencing" replace business travel? Who will finance this expanding technology, and how should outer space be shared between the nations? Details Online Conferences Ltd. *C* Uxbridge (0895) 39262.

Personal Computer World Show-Nov. 1-3, West Centre Hotel, London.

**Compec**—Nov. 6–8. Grand Hall, Olympia, London. Details: Iliffe Promotions Ltd. & 01-261 8437/8.

Professional Viewdata Exhibition '79—Nov. 7 & 8. West Centre Hotel, London.

Technical Innovation In The Service Of The Elderly and Disabled—Markets And Needs (symposium)—Nov. 19–21. Berlin. Details: H. S. Wolff, Clinical Research Centre, Watford Road, Harrow, Middlesex.

Integrated Telecommunications For The 80s—Nov. 20, 21. Carlton Tower, London. Details: Online.

Electronics 79---Nov. 20-23. Olympia, London. & 021 705 6707.

Video Rights 79 (conference)—Nov. 26, 27. Cafe Royal, London. Details: Nord Media & 01-629 9381.

**Breadboard 79**—Dec 4–8. Royal Horticultural Halls, Westminster. Details: Trident International Exhibitions. & 0822 4671.

**IBM Hardware Selection**—Dec. 5, 6. Skyline Hotel, London Airport. Details: Online.

IEA/Electrex—Feb. 25–29, 1980. National Exhibition Centre, Birmingham. Details: Industrial and Trade Fairs Ltd. & 021-705 6707.

Viewdata '80—March 26–28. Wembley Conference Centre, London. Conference and exhibition. Details: Online Conferences Ltd. & Uxbridge (0895) 39262.

Computer-Aided Design (conference and exhibition)—March 31-April 2, 1980. Metropole, Brighton. Details: Organisers, CAD 80. & 0483 31261.

**Communications '80**—April 14–18. National Exhibition Centre, Birmingham. Details: **ITF** Exhibitions. *C* 021-705 6707.

Electronic Test and Measuring Instrumentation—April 22–24, 1980. Wythenshaw Forum, Manchester. Details: Trident.

International Conference On The Electronic Office—April 22–25, 1980. London Penta Hotel. Organised principally by the Institute of Electronic and Radio Engineers. 99 Gower St., London WC1E 6AZ.

All-Electronics Show (1980)—April 29-May 1, Grosvenor House, London. & 0799-22612.

**The Mersey Micro Show**—April 30, May 1, 2, 1980. Adelphi Hotel, Liverpool. Exhibition and seminars, with the co-operation of Liverpool University. Details: Online.

The 1980 Microcomputer Show—July 10–12. Royal Lancaster Hotel, London. Details: Online.

IBC 80—Sept. 20–24. Metropole Centre, Brighton. Details: Secretariat, IEE, Savoy Place, London WC2R 0BL.



Based at our editorial offices in Poole the position carries a salary of £5,771 plus luncheon vouchers and at least 4 weeks paid holiday.

Written applications with full c.v. to Mike Kenward The Editor, Practical Electronics, Westover House, West Quay Road, Poole, Dorset.

NTRODUCTION of the slide dissolve unit has been a most exciting development for the enthusiast in colour slide photography. Two projectors are used with the slides stored alternately in each and smooth dissolves from one picture to the next are made by dimming one bulb whilst brightening the other. Not only does this technique stop that annoying sudden darkness between slides but it also gives a new freedom to the photographer to produce creative sequences of images which suit the changing moods of an accompanying soundtrack. Photographic clubs all over the world have established specialist groups for audio-visual work and some outstanding work has been shown at exhibitions and competitions.

But not all work has to be at this level; even the most ordinary collection of holiday snapshots will benefit from the professional touch given by pictures which automatically dissolve from one to the next in synchronism with a recording of music or commentary. Equipment to operate two projectors and to record the control and soundtrack signals on tape is available commercially but a basic unit will cost over £150 and advanced systems can cost far more.

This series of articles describes a dissolve control unit which is easy to build and adjust yet costs in the region of £40 to make putting it well within the reach of many amateur photographers. Cross-fading between the two projectors is controlled by a knob which allows the user to fade at any speed to suit the mood of the occasion. To change the slide a single button is pressed which automatically changes the slide in the dark projector-very useful in the heat of the moment when it is all too easy to press the wrong button and upset the whole sequence. Two additional buttons provide "twinkle" (rapid switching between two projectors) and automatic superimposition of two images-features not always found on commercial machines. Operation of the controls produces an audio signal which can be recorded on one track of any domestic cassette or reel-to-reel tape recorder and subsequently replayed to reproduce exactly the sequence of fades and changes that were originally recorded.

The control is designed to handle two remote-control projectors having 24V 150W lamps although it is easily modified to handle 250 watt lamps. Each projector needs a simple modification to interrupt the wires carrying current to the bulb and to bring them out at a socket for connection to the control box. Additional connections to each projector operate the slide change mechanism and provide the power to drive the electronics so that no separate connection to the mains is needed.

# DIAMATIC Programmable Audio Visual Unit

J.R.W. AMES

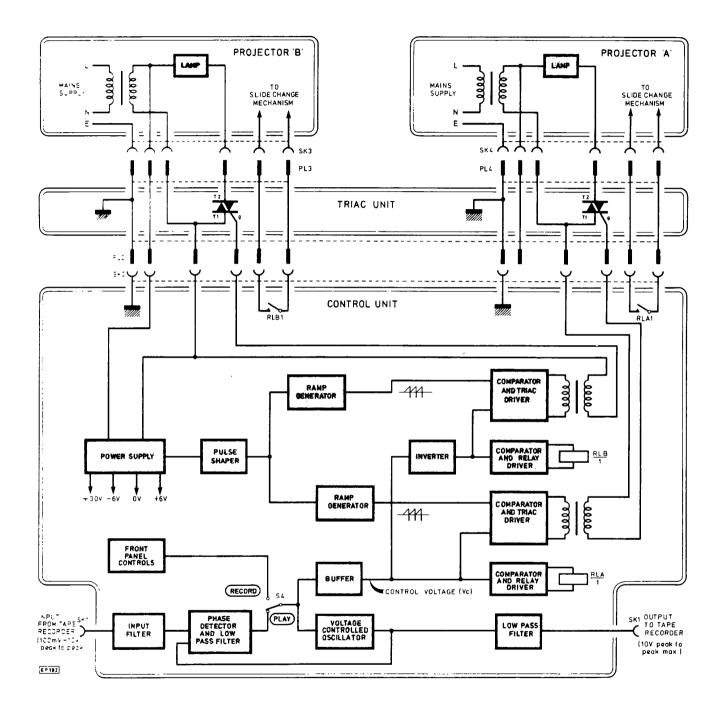


Fig. 1. Block diagram

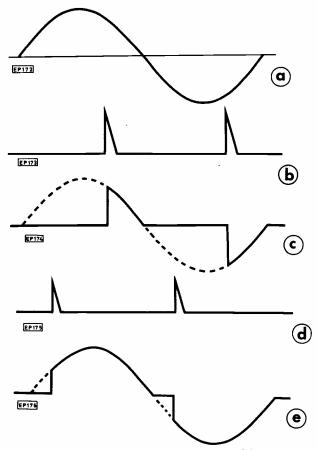


Fig. 2. (a) Mains input (b) late trigger pulses (c) small voltage across load (d) early trigger pulses (e) large voltage across load

#### **BRIGHTNESS CONTROL**

A triac is used to control the brightness of each projector lamp. When the device is connected in series with a circuit it behaves like a switch which is turned on by the brief application of a pulse to its trigger contact. Provided that the current through the triac stays above a certain sustaining level it will remain conducting, but it will turn off as soon as the current falls below this critical level. These features make the triac a useful device for regulating the power applied to a load which is driven from an alternating current supply.

The block diagram of the unit (Fig. 1) shows that a triac is connected in series with the lamp circuit of each projector and Fig. 2 shows how the circuit works. In (c) the triac is turned on late in every half cycle and turns off automatically as the alternating current reverses in direction producing a small average voltage across the lamp. More light is produced in (e) where the triac conducts for the larger part of each half cycle causing almost the full rated current to flow in the lamp. Trigger pulses are applied to each triac via a pulse transformer which isolates the driving electronics from the alternating voltage applied to the load.

In order to exercise precise control over the current flowing in the lamp we need to be able to vary the position of the trigger pulses within each mains half-cycle smoothly and accurately.

#### SAWTOOTH

As the block diagram shows a 100Hz sawtooth signal derived from the full-wave rectified mains frequency is compared in a high gain comparator circuit with a d.c.

control voltage, producing the results shown in Fig. 3. Increasing the control voltage (b) causes the comparator positive-going transition (c) to occur later and later in the mains half-cycle. This transition is differentiated to form the triac trigger pulse so the triac conducts for a shorter period and the average current in the load therefore decreases. Finally the control voltage exceeds the peak of the sawtooth, no trigger pulses are produced, and the light remains off.

As the control voltage is reduced (d) the trigger pulse occurs earlier in each half-cycle so increasing the lamp brightness. Notice the negative-going pulses that are added to the sawtooth at the end of each period. If these pulses are not added to the sawtooth no trigger pulses are produced when the control voltage falls below the lowest point of the waveform and the lamp abruptly changes from full-on to off. With the pulses added the control voltage can fall well below the base of the sawtooth while still producing a narrow trigger pulse at the beginning of each half-cycle to keep the lamp on.

The control voltage is connected directly to one comparator (projector A) and to the second via an inverter (projector B). As the input voltage to comparator A rises the input to comparator B falls and vice-versa producing a smooth cross-fade (dissolve) between the two projectors.

#### **SLIDE CHANGE**

The slide in a projector is only changed when its lamp is dark. At this time the control voltage for that projector is very close to the peak of the sawtooth and slide change is

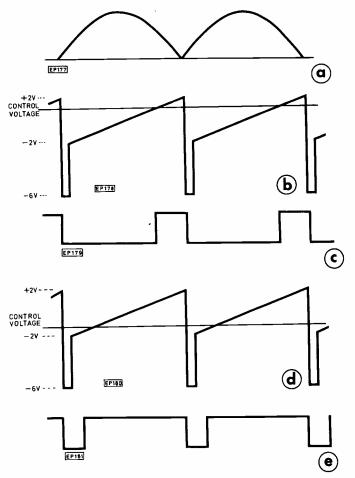


Fig. 3. Comparator waveforms (a) full wave rectified signal (b) sawtooth (c) comparator output (dim) (d) sawtooth (e) comparator output (bright)

initiated by momentarily increasing the voltage to cross a further threshold just above the peak level. This momentary increase is detected by the comparator and relay driver (see the block diagram) and the relay operates, closing a pair of contacts which are connected to the projector slide change solenoid in parallel with the normal remote control contacts.

As the control voltage for the dark projector rises to cross the slide change threshold the control voltage for the bright projector falls below the lowest point of its sawtooth comparison signal. If it were not for the negative-going pulses added to the sawtooth (Fig. 3) the bright projector would turn off momentarily each time a slide is changed.

Fig. 4 summarises the relationship between the control voltage levels and the actions of the two projectors.

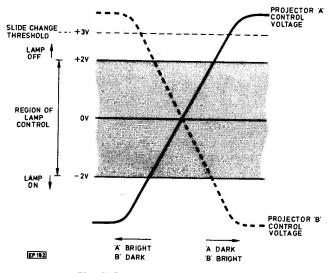


Fig. 4. Control voltage relationship

#### **RECORD AND REPLAY**

When recording a sequence of dissolves, switch S4 (Fig. 1) is placed in the "record" position placing the projectors under manual control. The voltage derived from the front panel controls is also used to vary the frequency of a voltage controlled oscillator (VCO) whose output varies in the band 1kHz to 3kHz as the projectors are cross-faded and makes a jump to either 500Hz or 4kHz when the slide in the dark projector is changed. This varying frequency is sent to the tape recorder after filtering to remove unwanted higher harmonics from the square wave signal.

On replay S4 is moved to the "play" position to form a phase-locked loop whose input signal is derived, after buffering, from the tape recorder. The output of the phase detector and low pass filter now copies the control voltage that was derived from the front panel controls during recording and the original sequence of events is reproduced exactly.

A special signal loss detector in the input buffer stage ensures that the projectors behave predictably when the replay signal is lost during tape editing. Both projectors illuminate at half brightness until the signal returns when the sequence continues from where it was interrupted.

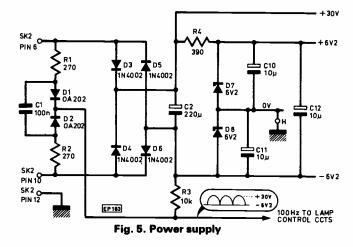
#### **CONNECTIONS TO THE PROJECTORS**

The electrical connections to the projectors are shown in Fig. 1. A triac is connected in series with the bulb circuit and trigger pulses are applied to the gate via a pulse transformer which isolates the projector circuits from the remainder of the electronics. Currents of up to 7A will flow in the lamp circuit so the connections to the triac must be



made with stout wire and the triac itself must be in firm contact with a good heatsink—more about this in the construction information.

Both sides of the low voltage secondary winding of the mains transformer are brought out from the projector to provide power for the unit so that a separate mains connection to the unit is avoided. The slide change button of each projector remote control is duplicated by a relay contact in the unit which closes momentarily to set the slide change mechanism in motion.

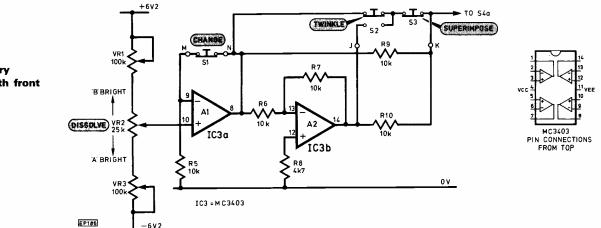


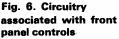
# **POWER SUPPLY**

D3–D6 together with C2 (Fig. 5) form a conventional fullwave bridge rectifier which is fed from the mains transformer of one of the projectors and provides a smoothed output of about 36V. The rectifier output is connected via a dropper resistor to the pair of Zener diodes to generate stabilised supplies of  $\pm 6.2V$  and a OV rail which power the electronics. The unstabilised output is available to operate the three relays in the unit. A separate unsmoothed full-wave rectified supply to drive the triac trigger control circuits is provided by D1, 2 and R3. R1, 2 and C1 form a low pass filter which prevents transients caused by the switching of the projector triac from disturbing the control circuits.

# **FRONT PANEL CONTROLS**

In Fig. 6 a resistive divider chain derives the voltage to control the brightness of the projector lamps during a cross-fade. VR2, the fader potentiometer, produces a control voltage which varies between limits of approximately  $\pm 2V$ , set by presets VR1, 3 when making the initial adjustments. Careful selection of VR2 is important. The component specified was chosen because it behaves in a linear fashion immediately the spindle moves away from either end stop.





Many potentiometers that were tested (both carbon track and wire-wound) showed little or no change in resistance during the first  $20^{\circ}$ - $30^{\circ}$  of rotation giving an unpleasant feel to the control as no change in lamp brightness occurred over this range.

Amplifier A1 serves a dual purpose. S1 is normally closed making A1 a non-inverting high impedance buffer but when S1 is opened it becomes a comparator with threshold at OV and its output then jumps to the supply rail towards which it is already offset. When VR2 is at either end of its range one of the projectors is dark and operation of S1 causes the control voltage to cross the slide-change threshold (set at about +3V) for this projector. In this way the dark slide is automatically selected for change and only one change button is needed.

A1 is one of four operational amplifiers with internal compensation that are housed in a single package—the MC3403. The amplifiers in this package have sufficient slewing rate to give full output for signals of up to 4kHz and they are used in this unit wherever an amplifier or comparator is needed. In all eleven amplifiers are used so three MC3403 packages are required. Because of the relatively low accuracy required of the d.c. amplifiers in this circuit it has not been necessary to use more expensive amplifiers with very high input impedance and low offset currents.

From A1 the output is normally connected via S2 to the lamp control and recording circuit at the record/replay switch. When S2 is operated, however, an inverted version of the control voltage (derived by A2, R6, 7, 8) is produced, inverting the states of the projectors to produce a "twinkle" effect. Operation of S2 allows rapid alternation between two slides and can be used to produce an animation effect.

S3, the superimpose button, breaks the output from S2 allowing R9, 10 to sum the control voltage (from A1) and its inverse (from A2). The opposing voltages add to give OV making both of the projectors light up equally and superimposing their images on the screen. R9, 10 also make sure that the control voltage waits respectably at OV during changeover if S2 is of the break-before-make variety.

# INTERFACE TO RECORDER

With S4 in the "record" position (Fig. 7) the control voltage derived from Fig. 6 is connected to the buffer, A5, and then to an inverter formed by A6, R22–24. The resulting pair of voltages, one of which is the inverse of the other, is used to control the two projectors, A and B.

While making a recording the control voltage is also connected to the input of a voltage controlled oscillator (VCO) which is part of IC1, an integrated phase-locked-loop circuit type MC14046. As the voltage changes the frequency

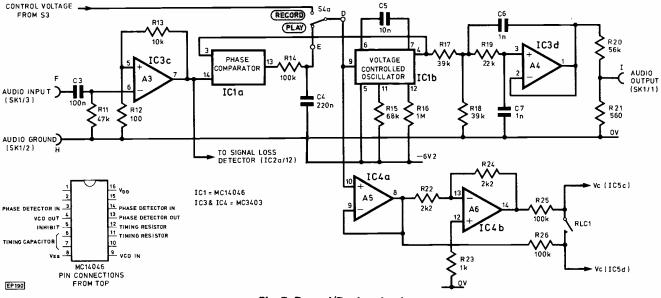


Fig. 7. Record/Replay circuits

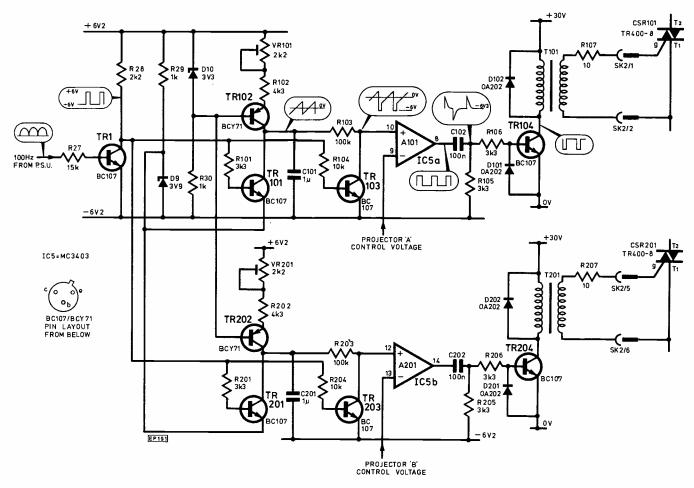


Fig. 8. Lamp control circuits

of the oscillator varies between 500Hz and 4kHz. This varying frequency is filtered by a second order low pass Sallen and Key filter (A4, R17-19, C6, 7) whose break point is set at 4kHz to remove undesirable higher harmonics from the square wave output of the VCO. The filtered tone, whose amplitude is approximately 10V peak-to-peak, is attenuated by R20, 21 before being connected to the input of the tape recorder. The values given for the attenuator resistors result in an output signal of 100mV peak-to-peak but the constructor can choose any suitable value by varying the resistor ratio.

On replay the output from the tape recorder is buffered and amplified by A3. This ampifier has hysteresis (determined by R12, 13) of  $\pm$ 50mV to ensure that no residual noise at the input is recognised as a false signal when the input is removed. If a very large input signal is available the hysteresis can be increased to give added protection by increasing R12. Reducing the hysteresis is not recommended and the input sensitivity of the unit is therefore determined by this figure. Input impedance of the amplifier is 47k fixed by R11.

The buffered tone is fed to one input of the phase comparator (also part of IC1), the other input of which has the VCO output signal applied to it.

With S4 in the "play" position a phase locked loop is formed using R14/C4 as the low pass filter with the result that the VCO locks exactly to the frequency of the input tone. The VCO, however, is the one that was initially used to make the recording so when its frequency corresponds with that of the incoming tone the voltage at its input is exactly equal to the control voltage that was originally applied. The recovered voltage is connected to A5 and used to control the projectors as described above.

If the received signal is lost, or if the unit is switched to "play" before the tape recorder is started, the output of the phase comparator will drop to -6V. A control voltage of this value will turn one projector full on and the other off as well as changing its slide. To avoid this problem a loss of signal detector (described later) monitors the output of A3 and operates RLC if the signal is lost during replay. Contact RLC1 adds together the opposing voltages generated by A5, 6 producing an output to both projector brightness controllers of about OV which turns both projectors half on—a useful feature when initially aligning their images on the screen.

#### LAMP CONTROL CIRCUITS

Apart from common bias components this part of the circuit (Fig. 8) is split into two identical parts, one for each projector. To avoid repetition only the components for one half will be mentioned which are numbered 101 upwards. Components for the other half are numbered 201 upwards with the same second and third digits.

The unsmoothed rectified mains voltage from the power supply circuit is used to saturate TR1, allowing it to turn off only during the short periods when the signal is close to -6.2V. As a result narrow positive-going spikes occur at the collector coincident with the zero-crossings of the a.c. mains waveform.

# COMPONENTS ....

R1       270       C1       Inclusion interfaces in the regressible i	Resistors	Semiconductors			Capaci	Capacitors		
P2         P20         IC2         MC14528 Dual re-triggerable         C2         220µ 63V Electr           R3         10k         monostable         C3         0-1µ 250V Poly           R4         390 5W         IC3         MC3403 Quad op-amp         C4         0-22µ 250V Poly           R6         10k         IC4         MC3403 Quad op-amp         C6         1n 160V Polysty           R7         10k         TR1         BC107         C8         0-1µ 250V Polysty           R8         4k7         TR2         BC107         C9         10µ 25V Tantalu           R10         10k         TR102,202         BCY71         C10         10µ 25V Tantalu           R12         100         TR104,204         BC107         C12         10µ 25V Tantalu           R12         100         TR104,204         BC107         C12         10µ 25V Tantalu           R13         10k         TR105,205         BC107         C10,201         1µ 100V Polyca           R14         100k         D1         0A202         C102,202         0-1µ 250V Polyt           R14         100k         D1         0A202         Single pole push to bra         Single pole push to bra           R13         10k	R1	270	IC1	MC14046	Phase locked loop	C1		0-1µ 250V Polyester
R3         10k         monostable         C3         0.1 µ 250V Polys           R4         390 5W         IC3         MC3403 Quad op-amp         C4         0.2 21 250V Polys           R5         10k         IC4         MC3403 Quad op-amp         C5         10n 250V Polys           R6         10k         IC5         MC3403 Quad op-amp         C6         1n 160 V Polyst           R6         10k         TR1         BC107         C7         1n 160V Polyst           R8         4k7         TR2         BC107         C8         0.1 µ 250V Polyst           R10         10k         TR101, 201         BC107         C10         10g 25V Tantabl           R12         100         TR104, 204         BC107         C11         10g 25V Tantabl           R12         100         TR104, 204         BC107         C101, 201         1 µ 100V Polyca           R14         100k         D1         0.4202         C102, 202         0.1 µ 250V Tantabl           R14         100k         D1         0.4202         S1         Single pole push to bre           R14         100k         D1         0.4202         S2         Single pole push to bre           R14         100k         D1					A CONTRACTOR OF	C2		220µ 63∨ Electrolytic
B4         390 5W         IC3         MC3403 Quad op-amp         C4         0.22 µ 250V Polys           R5         10k         IC4         MC3403 Quad op-amp         C5         10 h 250V Polys           R6         10k         IC5         MC3403 Quad op-amp         C6         1 n 160 V Polys           R7         10k         TR1         BC107         C8         0.1 µ 250V Polys           R8         4k7         TR2         BC107         C9         10 µ 25V Tantalu           R10         10k         TR102, 202         BCY71         C10         10 µ 25V Tantalu           R12         100         TR105, 205         BC107         C12         10 µ 25V Tantalu           R13         10k         TR105, 205         BC107         C10, 201         1 µ 100V Polyca           R14         100k         D1         0A202         C102, 202         0.1 µ 250V Polyd           R15         68k         D2         0A202         Single pole push to breat         Single pole push to breat         Single pole push to breat           R17         39k         D4         1M4002         Single pole push to breat         Single pole push to breat         Single pole push to breat           R21         560         D102, 202 <td></td> <td></td> <td>in the second seco</td> <td></td> <td></td> <td>C3</td> <td>1 ( H</td> <td>0.1µ 250V Polyester</td>			in the second seco			C3	1 ( H	0.1µ 250V Polyester
F5         10k         IC4         MC3403 Quad op-amp         C5         10n 250V Polyst           R6         10k         IC5         MC3403 Quad op-amp         C6         In 160V Polyst           R7         10k         TR1         BC107         C7         In 160V Polyst           R8         4k7         TR2         BC107         C8         0.1µ 250V Polyst           R8         4k7         TR2         BC107         C10         10µ 25V Tantalu           R10         10k         TR102, 202         BCY71         C10         10µ 25V Tantalu           R11         47k         TR05, 203         BC107         C11         10µ 25V Tantalu           R12         100         TR105, 205         BC107         C10, 201         10µ 10V Polyca           R13         10k         TR105, 205         BC107         C102, 202         0.1µ 250V Polyd           R14         100k         D1         0A202         Switches         Single pole push to bre.         Single pole push to bre.           R14         100k         D10         0A202         S3         Single pole push to bre.         Single pole push to bre.           R14         100k         D10         0A202         S3         Single			103			C4		0.22µ 250V Polyester
R6         10k         IC5         MC3403 Quad op-amp         C6         1 n 160 V Polysty           R7         10k         TR1         BC107         C7         1 n 160 V Polysty           R8         4k7         TR2         BC107         C8         0.1 µ 250V Polysty           R9         10k         TR102, 202         BCY71         C10         0.2 SV Tantalu           R11         47k         TR103, 203         BC107         C11         10 µ 25V Tantalu           R12         100         TR104, 204         BC107         C12         10 µ 25V Tantalu           R12         100         TR105, 205         BC107         C10, 201         1 µ 100V Polyca           R13         10k         TR105, 205         BC107         C10, 202         0.1 µ 250V Polyca           R14         100k         D1         0.4202         C102, 202         0.1 µ 250V Polyca           R15         68k         D2         0.4202         S1         Single pole push to brea           R19         22k         D6         1104002         S2         Single pole push to brea           R21         560         D102, 202         0.4202         S3         Single pole push to brea           R21	and the second se	the second s				C5		10n 250V Polystyrene
R7       10k       TR1       BC107       C7       In 160V Polystyl         R8       4k7       TR2       BC107       C6       0-1µ 250V Polystyl         R9       10k       TR101, 201       BC107       C9       10µ 25V Tantalu         R10       10k       TR102, 202       BCY71       C10       10µ 25V Tantalu         R11       47k       TR302, 303       BC107       C11       10µ 25V Tantalu         R12       100       TR104, 204       BC107       C12       10µ 25V Tantalu         R13       10k       TR105, 205       BC107       C12       10µ 25V Tantalu         R14       100k       D1       0A202       C102, 202       0-1µ 250V Polyst         R14       100k       D1       0A202       C102, 202       0-1µ 250V Polyst         R14       100k       D3       1N4002       Switches         R18       39k       D4       1N4002       Stingle pole push to breact         R11       560       D102, 202       0A202       S3       Single pole push to breact         R21       560       D102, 203       0A202       S4       2 pole changeover toge         R23       10k       D7       6-2V						C6		1n 160 V Polystyrene
R8         4k7         TR2         BC107         CB         0.1µ 250V Polyk           R9         10k         TR101,201         BC107         C9         10µ 25V Tantalu           R10         10k         TR103,203         BC107         C10         10µ 25V Tantalu           R11         47k         TR103,203         BC107         C11         10µ 25V Tantalu           R11         47k         TR104,204         BC107         C12         10µ 25V Tantalu           R13         10k         TR104,204         BC107         C10,202         0.1µ 250V Polyk           R14         100k         D1         0A202         C102,202         0.1µ 250V Polyk           R15         68k         D2         0A202         C102,202         0.1µ 250V Polyk           R15         68k         D10         A04002         S1         Single pole push to breating in to					E CARE LA SALE	C7		1n 160V Polystyrene
No.         TB 101, 201         BC 107         CB         10 µ 25V Tantalu           R10         10k         TR 102, 202         BCY71         C10         10µ 25V Tantalu           R11         47k         TR 103, 203         BC 107         C11         10µ 25V Tantalu           R12         100         TR 104, 204         BC 107         C12         10µ 25V Tantalu           R13         10k         TR 105, 205         BC 107         C12, 201         1µ 100V Polyca           R14         100k         D1         0A202         C102, 202         0.1µ 250V Polyd           R15         68k         D2         0A202         C102, 202         0.1µ 250V Polyd           R16         1M         D3         1N4002         Switches         Single pole push to breating         22           R17         39k         D6         1N4002         S1         Single pole push to breating         22         Single pole push to breating         23         Single pole push to breating         24         2 pole changeover togg         23         Single pole push to breating         24         2 pole changeover togg           R22         2 k2         D103, 203         0A202         S3         Single pole push to breating         24         2 pole c					the Free Real Provent	C8		0.1µ 250V Polyester
R10         10k         TR 102, 202         BCY71         C10         10µ 25V Tantalu           R11         47k         TR 103, 203         BC 107         C11         10µ 25V Tantalu           R12         100         TR 104, 204         BC 107         C12         10µ 25V Tantalu           R13         10k         TR 104, 204         BC 107         C101, 201         Iµ 100V Polyca           R14         100k         D1         0A202         C102, 202         0-1µ 250V Polyc           R16         1M         D3         1N4002         Switches           R17         38k         D4         1N4002         S1         Single pole push to breat           R19         22k         D6         1N4002         S2         Single pole push to breat           R20         56k         D101, 201         0A202         S3         Single pole push to breat           R21         560         D102, 202         0A202         S4         2 pole changeover togg           R23         1k         D7         6-2V 1-3W BZX85 series         S4         2 pole changeover togg           R24         2k2         D8         6-2V 1-3W BZX85 series         Stude         Pluga and Sockets           R28					ACCEPTION TO A RES	C9		10µ 25V Tantalum
R11       47k       TR103,203       BC107       C11       10µ 25V Tantabu         R12       100       TR104,204       BC107       C12       10µ 25V Tantabu         R13       10k       TR105,205       BC107       C101,201       1µ 100V Polycal         R14       100k       D1       0A202       C102,202       0-1µ 25V Polycal         R14       100k       D1       0A202       Switches         R15       68k       D2       0A202       Switches         R16       1M       D3       1N4002       Switches         R17       39k       D4       1N4002       Suingle pole push to breat         R18       39k       D4       1N4002       Stingle pole push to breat         R19       22k       D6       1N4002       Stingle pole push to breat         R20       56k       D101,201       0A202       S3       Single pole push to breat         R21       560       D102,202       0A202       S4       2 pole changeover togg         R23       1k       D7       6-2V 1.3W BZX85 series       R24       2 pole changeover togg         R24       2k2       CSR101,201       TR1 400-8 (R/S 261-601)       Pluga and Sockets </td <td></td> <td></td> <td></td> <td></td> <td></td> <td>C10</td> <td></td> <td>10µ 25V Tantalum</td>						C10		10µ 25V Tantalum
Init         The total 204         BC 107         C12         10µ 25V Tantalo           R13         10k         TR105,205         BC 107         C101,201         1µ 100V Polycal           R14         100k         D1         0A202         C102,202         0-1µ 250V Polyd           R15         68k         D2         0A202         Switches         Switches           R17         39k         D4         1N4002         Switches         Switches           R18         39k         D4         1N4002         Single pole push to breact to	and the second se					C11		10µ 25V Tantalum
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R14       100k       D1       0A202       C102, 202       0.4 µ 250V Polyt         R15       68k       D2       0A202       Switches         R16       1 M       D3       114002       Switches         R17       39k       D4       114002       Switches         R18       39k       D5       114002       Single pole push to breat         R19       22k       D6       114002       Single pole push to breat         R20       56k       D101, 201       0A202       S3       Single pole push to breat         R21       560       D102, 202       0A202       S4       2 pole changeover togg         R23       1k       D7       6-2V 1-3W BZX85 series       Single pole push to breat         R24       2k2       D8       6-2V 1-3W BZX85 series       Single pole push to breat         R25       100k       D9       3-9V 400mW BZY88 series       Single pole make 24V 740         R28       2k2       CSR101, 201       TR1 400-8 (R/S 261-801)       Flugs and Sockets         R33       150k       R1A       Single pole make 24V 740       Plugs and Sockets         R33       150k       R1A       Single pole make 24V 740       Pl.3       15 way D			All and the second s	And the second sec		C101	,201	1µ 100V Polycarbona
R15         68k         D2         OA202           R16         1M         D3         1N4002         Switches           R17         39k         D4         1N4002         Single pole push to breact the pole pole pole pole pole pole pole pol						C102	2,202	0.1 µ 250V Polyester
R16         1M         D3         1N4002         Switches           R17         39k         D4         1N4002         S1         Single pole push to bready the push to bready the pole pole push to bready the pole pole push to bready the								
R17         39k         D4         1N4002         Switches           R18         39k         D5         1N4002         S1         Single pole push to bread           R19         22k         D6         1N4002         S2         Single pole push to bread           R20         56k         D101, 201         0A202         S2         Single pole push to bread           R21         560         D102, 202         0A202         S4         2 pole changeover togg           R23         1k         D7         6-2V 1-3W BZX85 series         Single pole push to bread         2 pole changeover togg           R24         2k2         D8         6-2V 1-3W BZX85 series         2 pole changeover togg           R25         100k         D9         3-9V 400mW BZY88 series         2 pole changeover togg           R26         100k         D10         3-3V 400mW BZY88 series         2 pole changeover togg           R27         15k         D11         0A202         CSR101, 201         TR14 00-8 (R/S 261-801)           R29         1k         For 250W lamp use 2N5574 (R/S 261-558)—stud         PL4         5 pin D           R31         3k3         R32         10k         Relays         PL3         15 way E           R34<						1999	S ALE	
R18         39k         D5         1N4002         S1         Single pole push to brea           R19         22k         D6         1N4002         S2         Single pole push to brea           R20         56k         D101, 201         0A202         S2         Single pole push to brea           R21         560         D102, 202         0A202         S3         Single pole push to brea           R22         2k2         D103, 203         0A202         S4         2 pole changeover togg           R23         1k         D7         6-2V 1 -3W BZX85 series         S4         2 pole changeover togg           R24         2k2         D8         6-2V 1 - 3W BZX85 series         S4         2 pole changeover togg           R25         100k         D9         3-9V 400mW BZY88 series         S4         2 pole changeover togg           R26         100k         D10         3-3V 400mW BZY88 series         S4         S4           R28         2k2         CSR101, 201         TR1 400-8 (R/S 261-801)         S4         S4           R30         1k         mounting         R33         150k         S1         S4         S4           R34         100k         RLA         Single pole make 24V 740			the second se			Switc	hes	
119       22k       D6       1 N4002       S1       Single pole push to bready to be push to bready to be push to bready to be push to be public to be		and the second second second						
R10       56k       D101, 201       OA202       S2       Single pole push to that         R21       560       D102, 202       OA202       S3       Single pole push to brait         R22       2k2       D103, 203       OA202       S4       2 pole changeover togg         R23       1k       D7       6-2V 1-3W BZX85 series       S4       2 pole changeover togg         R24       2k2       D8       6-2V 1-3W BZX85 series       S4       2 pole changeover togg         R25       100k       D9       3-9V 400mW BZY88 series       S7       S7       S7         R26       100k       D10       3-3V 400mW BZY88 series       S7       S6       S7       S6       S7			strange and the second state and a second state			S1		
R21         560         D102, 202         OA202         S3         Single pole push to bre:           R22         2k2         D103, 203         OA202         S4         2 pole changeover togg           R23         1k         D7         6-2V 1-3W BZX85 series         S4         2 pole changeover togg           R24         2k2         D8         6-2V 1-3W BZX85 series         S         S           R25         100k         D9         3-9V 400mW BZY88 series         S         S           R26         100k         D10         3-3V 400mW BZY88 series         S         S           R26         100k         D11         OA202         S         S         S           R27         15k         D11         OA202         S         S         S           R28         2k2         CSR101,201         TR1 400-8 (R/S 261-801)         S         S           R33         150k         R         Relays         S         Single pole make 24V 740         Plugs and Sockets           R34         100k         RLB         Single pole make 24V 740         PL2         15 way C           R37         100k         R         RLB         Single pole make 30V 3k         PL3         15 way						S2		
R12       2k2       D103, 203       OA202       S4       2 pole changeover togg         R23       1k       D7       6-2V 1.3W BZX85 series       6-2V 1.3W BZX85 series         R24       2k2       D8       6-2V 1.3W BZX85 series       6-2V 1.3W BZX85 series         R25       100k       D9       3.9V 400mW BZY88 series       6-2V 1.3W BZX85 series         R26       100k       D10       3.3V 400mW BZY88 series       6-2V 1.3W BZX85 series         R26       100k       D11       OA202       6-2V 1.3W BZX85 series         R27       15k       D11       OA202       6-2V 1.3W BZY88 series         R27       15k       D11       OA202         R28       2k2       CSR101,201       TR1 400-8 (R/S 261-801)         R30       1k       mounting         R31       3k3         R32       10k       Relays         R33       150k       RLA       Single pole make 24V 740         R36       100k       RLC       Single pole make 30V 3k       PL1       5 pin D         PL3       15 way E       PL3       15 way E       9 PL3       15 way E         R101, 201       3k3       VR1       100k       Cermet skeleton preset		the second		Contraction of the second s		S3	Sing	le pole push to break
R12         Int         D7         6-2V 1-3W BZX85 series           R24         2k2         D8         6-2V 1-3W BZX85 series           R25         100k         D9         3-9V 400mW BZY88 series           R26         100k         D10         3-3V 400mW BZY88 series           R27         15k         D11         OA202           R28         2k2         CSR101,201         TR1 400-8 (R/S 261-801)           R29         1k         For 250W lamp use 2N5574 (R/S 261-558)—stud           R30         1k         mounting           R31         3k3           R32         10k         Relays           R33         150k           R34         100k         RLB           Single pole make 24V 740         Plugs and Sockets           R35         100k         RLB           R36         100k         RLC           R37         100k         PL3           R38         10k         PL3           R101,201         3k3           R102,202         4k3           R104,204         10k           R105,205         3k3           R105,205         3k3           VR3         100k         C	and the second					S4	2 pol	le changeover toggle
R24       2k2       D8       6.2V 1.3W BZX85 series         R25       100k       D9       3.9V 400mW BZY88 series         R26       100k       D10       3.3V 400mW BZY88 series         R27       15k       D11       OA202         R28       2k2       CSR101,201       TR1 400-8 (R/S 261-801)         R29       1k       For 250W lamp use 2N5574 (R/S 261-558)—stud         R30       1k       mounting         R31       3k3         R32       10k         R34       100k         R35       100k         R36       100k         R37       100k         R38       10k         R39       10k         R38       10k         R101, 201       3k3         R102, 202       4k3         R104, 204       10k         VR1       100k       Cermet skeleton preset         SK1       5 pin D         R104, 204       10k       VR1         R105, 206       3k3       VR101, 201       2k2         Cermet skeleton preset       SK4       15 way E         SK4       15 way E       Shorting links				Contraction of the second second	N R7X85 series			
R25       100k       D9       3.9V 400mW BZY88 series         R26       100k       D10       3.3V 400mW BZY88 series         R27       15k       D11       DA202         R28       2k2       CSR101,201       TR1400-8 (R/S 261-801)         R29       1k       For 250W lamp use 2N5574 (R/S 261-558)—stud         R30       1k       mounting         R31       3k3         R32       10k         R34       100k         R35       100k         R36       100k         R37       100k         R38       10k         R39       10k         R38       10k         R101, 201       3k3         R102, 202       4k3         R104, 204       10k         VR1       100k       Cermet skeleton preset         SK1       5 pin D         R104, 204       10k       VR3         R105, 205       3k3       VR101, 201       2k2         R106, 206       3k3       VR101, 201       2k2         Cermet skeleton preset       SK4       15 way E         Sk44       15 way E       Sk44       15 way E         R10								
R26       100k       D10       3.3V 400mW BZY88 series         R27       15k       D11       OA202         R28       2k2       CSR101,201       TR1 400-8 (R/S 261-801)         R29       1k       For 250W lamp use 2N5574 (R/S 261-558)—stud         R30       1k       mounting         R31       3k3         R32       10k       Relays         R33       150k       RLA       Single pole make 24V 740       Plugs and Sockets         R33       150k       RLA       Single pole make 24V 740       Plugs and Sockets         R36       100k       RLB       Single pole make 24V 740       Plugs and Sockets         R37       100k       RLC       Single pole make 30V 3k       PL1       5 pin D         R38       10k       Potentiometers       PL3       15 way D         R101, 201       3k3       VR1       100k       Cermet skeleton preset       SK1       5 pin D         R104, 204       10k       VR2       25k       Linear wirewound       SK2       15 way D         R106, 206       3k3       VR3       100k       Cermet skeleton preset       SK4       15 way D         R107, 207       10       VR3       100k <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
R27       15k       D11       DA202         R28       2k2       CSR101, 201       TR1 400-8 (R/S 261-801)         R29       1k       For 250W lamp use 2N5574 (R/S 261-558)—stud         R30       1k       mounting         R31       3k3         R32       10k         R34       100k         R35       100k         R36       100k         R37       100k         R38       10k         R101, 201       3k3         R102, 202       4k3         R104, 204       10k         VR1       100k       Cermet skeleton preset         R104, 204       10k         VR2       25k       Linear wirewound         R105, 205       3k3       VR101, 201       2k2         R106, 206       3k3       VR101, 201       2k2         VR101, 201       2k2       Cermet skeleton preset       SK4         SK4       15 way E         Covers for PL2, 3, 4       Shorting links				the second se				
R28       2k2       CSR101, 201       TR1 400-8 (R/S 261-801)         R29       1k       For 250W lamp use 2N5574 (R/S 261-558)—stud         R30       1k       mounting         R31       3k3         R32       10k         R34       100k         R35       100k         R36       100k         R37       100k         R38       10k         R101, 201       3k3         R102, 202       4k3         R104, 204       10k         VR1       100k         R105, 205       3k3         R105, 206       3k3         R106, 206       3k3         R107, 207       10		Contraction of the second s			INV DETOO SCHES			
R29         1k         For 250VV lamp use 2N5574 (R/S 261–558)—stud           R30         1k         mounting           R31         3k3         Relays           R33         150k         Relays           R33         150k         RLA         Single pole make 24V 740         Plugs and Sockets           R34         100k         RLB         Single pole make 24V 740         Plugs and Sockets           R35         100k         RLC         Single pole make 30V 3k         PL1         5 pin D           R36         100k         RLC         Single pole make 30V 3k         PL2         15 way D           R37         100k         R101, 201         3k3         PL4         15 way D           R102, 202         4k3         VR1         100k         Cermet skeleton preset         SK1         5 pin D           R102, 202         4k3         VR1         100k         Cermet skeleton preset         SK1         5 pin D           R102, 202         4k3         VR3         100k         Cermet skeleton preset         SK4         15 way D           R104, 204         10k         VR3         100k         Cermet skeleton preset         SK4         15 way D           R105, 205         3k3					8 (B/S 261_801)			A DECEMBER OF STREET
R301kmountingR313k3R3210kR33150kR34100kRLAR35100kRLBSingle pole make 24V 740R36100kR37100kR3810kR101, 2013k3R102, 2024k3R104, 20410kVR1100kCermet skeleton presetSK1SK15 pin DSK15 pin DPL415 way DR104, 20410kVR3100kCermet skeleton presetSK3SK3VR3100kSK3Covers for PL2, 3, 4R106, 2063k3R107, 20710		and the second se				Bute_(8		
R313k3R3210kRelaysR33150kR34100kRLAR35100kRLBSingle pole make 24V 740Plugs and SocketsR36100kR37100kR3810kR101, 2013k3R102, 2024k3R103, 203100kR104, 20410kR105, 2053k3R105, 2053k3R106, 2063k3R107, 20710				mp use an	0074 (170 201 000	or area		
R3210kRelaysR33150kRLASingle pole make 24V 740Plugs and SocketsR34100kRLBSingle pole make 24V 740PL15 pin DR35100kRLCSingle pole make 30V 3kPL15 pin DR36100kRLCSingle pole make 30V 3kPL215 way DR37100kPotentiometersPL315 way DR101, 2013k3PotentiometersPL415 way DR102, 2024k3VR1100kCermet skeleton presetSK15 pin DR103, 203100kVR1100kCermet skeleton presetSK215 way DR104, 20410kVR225kLinear wirewoundSK315 way DR105, 2053k3VR3100kCermet skeleton presetSK415 way DR106, 2063k3VR101, 2012k2Cermet skeleton presetSK415 way DCovers for PL2, 3, 4Shorting linksShorting linksShorting linksShorting links			mounting					
R33150kRLASingle pole make 24V 740Plugs and SocketsR34100kRLBSingle pole make 24V 740Plugs and SocketsR35100kRLCSingle pole make 30V 3kPL15 pin DR36100kRLCSingle pole make 30V 3kPL215 way DR37100kPotentiometersPL315 way DR101, 2013k3VR1100kCermet skeleton presetSK1R102, 2024k3VR1100kCermet skeleton presetSK2R103, 203100kVR225kLinear wirewoundSK2R104, 20410kVR3100kCermet skeleton presetSK3R105, 2053k3VR101, 2012k2Cermet skeleton presetSK4R106, 2063k3VR101, 2012k2Cermet skeleton presetSK4R107, 2071010Sk2Cermet skeleton presetSk4			Dalasia					
R34100kRLASingle pole make 24V 740Plugs and SocketsR35100kRLBSingle pole make 24V 740PL15 pin DR36100kRLCSingle pole make 30V 3kPL215 way DR37100kPotentiometersPL315 way DR101, 2013k3VR1100kCermet skeleton presetSK1R102, 2024k3VR1100kCermet skeleton presetSK2R104, 20410kVR225kLinear wirewoundSK2R105, 2053k3VR3100kCermet skeleton presetSK4R106, 2063k3VR101, 2012k2Cermet skeleton presetSK4R107, 20710500500Shorting links			nelays					
R35         100k         RLB         Single pole make 24V 740           R36         100k         RLC         Single pole make 30V 3k         PL1         5 pin D           R37         100k         RLC         Single pole make 30V 3k         PL2         15 way D           R38         10k         Potentiometers         PL3         15 way D           R101, 201         3k3         VR1         100k         Cermet skeleton preset         SK1         5 pin D           R104, 204         10k         VR2         25k         Linear wirewound         SK2         15 way D           R105, 205         3k3         VR3         100k         Cermet skeleton preset         SK4         15 way D           R106, 206         3k3         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way D           R107, 207         10         500         Shorting links         Shorting links         Shorting links	A REAL PROPERTY AND A REAL		DIA	Single pel	e make 24V 740			
R36         100k         RLC         Single pole make 30V 3k         PL1         5 pin D           R37         100k         PL2         15 way D         PL2         15 way D           R38         10k         Potentiometers         PL3         15 way D         PL4         15 way D           R102, 202         4k3         VR1         100k         Cermet skeleton preset         SK1         5 pin D           R103, 203         100k         VR1         100k         Cermet skeleton preset         SK2         15 way D           R104, 204         10k         VR2         25k         Linear wirewound         SK2         15 way D           R105, 205         3k3         VR3         100k         Cermet skeleton preset         SK4         15 way D           R106, 206         3k3         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way D           R107, 207         10         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way D						Plu	gs an	d Sockets
R37       100k       PL1       5 pin D         R38       10k       PL2       15 way E         R101, 201       3k3       Potentiometers       PL3       15 way E         R102, 202       4k3       VR1       100k       Cermet skeleton preset       SK1       5 pin D         R103, 203       100k       VR1       100k       Cermet skeleton preset       SK1       5 pin D         R104, 204       10k       VR2       25k       Linear wirewound       SK2       15 way E         R105, 205       3k3       VR3       100k       Cermet skeleton preset       SK4       15 way E         R106, 206       3k3       VR101, 201       2k2       Cermet skeleton preset       SK4       15 way E         Covers for PL2, 3, 4       Shorting links       Shorting links       Shorting links	and the second second second second							
R38         10k         Potentiometers         PL3         15 way E           R101, 201         3k3         Potentiometers         PL3         15 way E           R102, 202         4k3         VR1         100k         Cermet skeleton preset         SK1         5 pin D           R104, 204         10k         VR2         25k         Linear wirewound         SK2         15 way E           R105, 205         3k3         VR3         100k         Cermet skeleton preset         SK3         15 way E           R106, 206         3k3         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way E           R107, 207         10         VR101, 201         2k2         Cermet skeleton preset         Shorting links			ALC	Single poi	e make SUV SK			5 pin DIN
R101, 201         3k3         Potentiometers         PL4         15 way E           R102, 202         4k3         VR1         100k         Cermet skeleton preset         SK 1         5 pin D           R103, 203         100k         VR1         100k         Cermet skeleton preset         SK 1         5 pin D           R104, 204         10k         VR2         25k         Linear wirewound         SK2         15 way E           R105, 205         3k3         VR3         100k         Cermet skeleton preset         SK4         15 way E           R106, 206         3k3         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way E           R107, 207         10         VR101, 201         2k2         Cermet skeleton preset         Shorting links							and the second second	15 way D-type
R101, 201       383       PL4       15 way I         R102, 202       4k3       VR1       100k       Cermet skeleton preset       SK1       5 pin D         R103, 203       100k       VR2       25k       Linear wirewound       SK2       15 way I         R104, 204       10k       VR3       100k       Cermet skeleton preset       SK3       15 way I         R105, 205       3k3       VR3       100k       Cermet skeleton preset       SK4       15 way I         R106, 206       3k3       VR101, 201       2k2       Cermet skeleton preset       SK4       15 way I         R107, 207       10       Stope       Shorting links       Shorting links	the second s		Potentiometer	rs			and the second second	15 way D-type
R103, 203         100k         VR1         100k         Cermet skeleton preset         SK1         5 pm b           R104, 204         10k         VR2         25k         Linear wirewound         SK2         15 way E           R105, 205         3k3         VR3         100k         Cermet skeleton preset         SK3         15 way E           R106, 206         3k3         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way E           R107, 207         10         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way E			- USE REAL OF SHIP	123 27				15 way D-type
R103, 203         100k         VR2         25k         Linear wirewound         SK2         15 way I           R104, 204         10k         VR3         100k         Cermet skeleton preset         SK3         15 way I           R105, 205         3k3         VR3         100k         Cermet skeleton preset         SK3         15 way I           R106, 206         3k3         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way I           R107, 207         10         VR101, 201         2k2         Cermet skeleton preset         Shorting links			VB1	100k (	ermet skeleton preset			5 pin DIN
R104, 204         T0k         VR3         100k         Cermet skeleton preset         SK3         15 way I           R105, 205         3k3         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way I           R106, 206         3k3         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way I           R107, 207         10         Shorting links         Shorting links         Shorting links					The second	S	K2	15 way D-type
R105, 205         3k3         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way I           R106, 206         3k3         VR101, 201         2k2         Cermet skeleton preset         SK4         15 way I           R107, 207         10         Shorting links         SK4         Shorting links					and the second se	S	КЗ	15 way D-type
R106, 200         3k3         Covers for PL2, 3, 4           R107, 207         10         Shorting links					the second s	S		15 way D-type
DIOL DOD IN THE DIOL DI			VIII01, 201	LAC	annot anoteten preset	C	overs f	for PL2, 3, 4
						SI	horting	g links
R108, 208 10k (2 off 15 way D-type) Besistors all ±W except where stated.	R108, 208	10k				(2	off 15	5 way D-type)

Resistors all  $\frac{1}{4}W$  except where stated.

			115	

T101, 201	Transformer assembly
Core	FX2238 (Mullard) 2 off per assembly
Bobbin	DT2281 (Mullard) 1 off per assembly
Ring	DT2356 (Mullard) 1 off per assembly
Clip	DT2357 (Mullard) 4 off per assembly
Board	DT2359 (Mullard) 1 off per assembly
28 swg ena	amelled copper wire
36 swg en	amelled copper wire

# Miscellaneous

Control box	220mm × 1 (R.S. 509		100m	m
Triac housing	Aluminium x 121mr	die <mark>c</mark> ast n x 55mn		171mm
Rubber feet I.c. socket 16 pin I.c. socket 14 pin Control knob	8 off 2 off 3 off			
15 way screened c 1mm Veropins 13A mains cable (3				

TR1 and all the other transistors in this unit are type BC107 or its complement, the BCY71. Constructors should beware of substituting near equivalents without first checking the maximum collector to emitter voltage that the device will tolerate. In several places in the circuit the transistors have collector voltages of 30V or more which is sufficient to damage BC108/9 devices and their equivalents.

TR102 together with R102, VR101 and the common bias supply formed by R30/D10 forms a constant current source which charges C101 causing the voltage across it to rise linearly with time. At each mains zero-crossing C101 is discharged by TR101 to  $-2 \cdot 2V$  determined by the common bias network R29/D9. The peak voltage which the ramp across C101 reaches before the discharge is determined by the charging current and can be varied between +1.5V and +2.5V by VR101. This adjustment, made during initial setting up, determines the value of control voltage which just extinguishes the projector lamp.

The ramp voltage is fed via R103 to the comparator A101. At the comparator input TR103 clamps the ramp signal to -6.3V during each mains zerô-crossing to produce the waveform with negative-going spikes as shown in the figure.

To the other input of the comparator is applied the projector control voltage derived from the manual controls or from the tape recorded signal. When the ramp voltage rises above the control voltage the output of the comparator makes an abrupt positive-going transition of about 10V which is differentiated by C102/R105 and applied to the base of TR104. D101 prevents breakdown of the baseemitter junction of TR104 during the negative-going edge of the comparator output which occurs at the mains zerocrossing when C101 is discharged. TR104 collector produces narrow 30V pulses at the trigger instants which are coupled via the 10:1 step-down transformer T101 to the gate of the triac. R107 limits the triac gate current and prevents damage to TR104 in the event of a short circuit. D102 suppresses overshoot caused by the primary inductance of T101 when the triac is disconnected from the secondary circuit which might otherwise break down the driver transistor.

The emitter of TR104 is returned to OV rather than to -6.2V for a particular purpose. Differentiation of the comparator output produces a steep rising edge followed by an exponential decay to -6.2V as sketched on the circuit

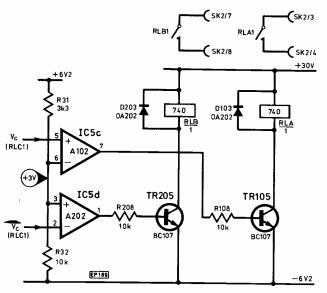


Fig. 9. Slide change relay drivers

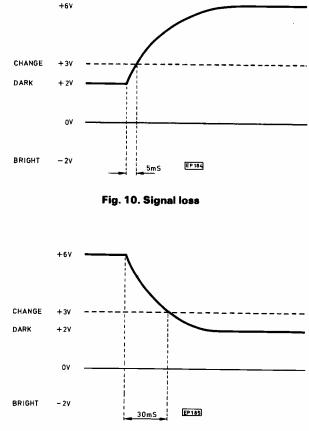


Fig. 11. Signal regained

diagram. If the emitter were returned to -6.2V the point at which the transistor turned off (about 0.6V above the emitter voltage) would be on the shallow part of the exponential decay producing an ill-defined switching point and output pulse width. Furthermore, the slowly changing voltage may result in the slow turn-off of TR104 which may begin to dissipate excessive power whilst in the linear region of operation. Returning the emitter to OV ensures that both turn-on and turn-off occur at rapidly changing points on the differentiated waveform.

# **SLIDE CHANGE RELAY DRIVERS**

The projector control voltage is compared with a common threshold of +3V (generated by R31, 32) in A102 as shown in Fig. 9. When the slide change button is depressed the control voltage of the dark projector jumps from approx +2V to cross the +3V threshold, turning on TR105 as a result. Relay RLA then operates completing the slide change circuit to the projector. D103 prevents damage to TR105 caused by overshoot across RLA when the transistor turns off.

# SIGNAL LOSS DETECTOR

If the signal from the tape recorder is lost during replay (when making an edit, for example) the output of the phase detector falls to  $-6\cdot 2V$  at a rate determined by the low pass filter R14/C4. Fig. 10 shows what happens to the control voltage of projector B (after inversion by A6) assuming that it is dark (the worst case) when the input signal is lost. We see that the projector lamp goes out and about 5ms after the signal is lost the voltage crosses and stays across the slide change threshold. This will cause some projectors to change once, others will change repeatedly, while some will even change backwards—all undesirable effects!

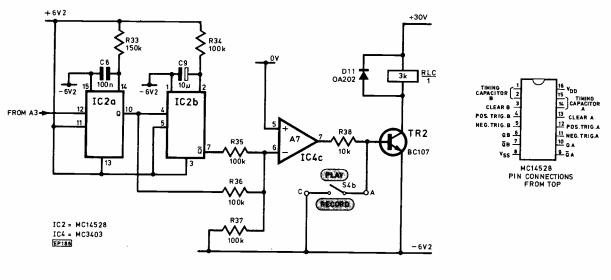
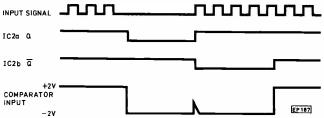


Fig. 12 (above). Signal loss detector circuit. Fig. 13 (right). Showing operational waveforms of signal loss detector



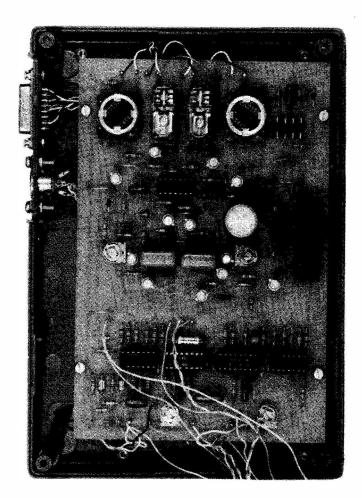


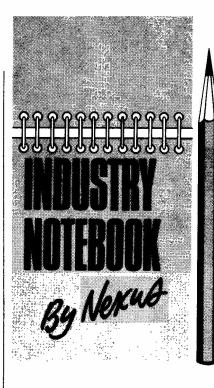
Fig. 11 shows what happens when the input signal returns—it takes about 30ms for the control voltage to stop changing the slide and to return to its correct level.

To prevent this effect it is necessary to clamp the control voltage to a value within the lamp control range before the output of the phase detector crosses the change threshold and to release the control voltage only after the phase detector output comes within this range again. This is done by means of a fast-operate slow-release signal loss detector formed by two CMOS monostables IC2a, b (Fig. 12) which is connected to the output of the signal buffer A3. CMOS devices will work over a wide range of supply voltages enabling IC1 and IC2 to be operated from the  $\pm 6.2V$  rails so that a separate power supply is not needed. Fig. 13 shows the waveforms that result from the operation of the circuit.

Shortly after the signal is lost (the time being determined by R33/C8) the Q output of the retriggerable monostable IC2a falls making the inverting input of comparator A7 fall below the OV threshold. The comparator output rises, operating RLC via TR2, and contact RLC1 in the tape recorder interface circuit closes turning both projectors on at half power. S4b prevents RLC from clamping the control voltage when making a recording as no signal is then present at the input terminal.

On recovery of the signal the Q output of IC2a rises immediately triggering IC2b whose  $\overline{Q}$  output falls, keeping the comparator input below OV for a period determined by R34/C9. In this way the attack and decay characteristics of the signal loss detector can be individually adjusted to prevent mis-operation of the slide change relay of projector B during tape edits or before the show begins when the tape recorder is not running.

# NEXT MONTH: Construction and setting up



# A Matter of Degree

There now seems to be general acceptance that both our primary and secondary educational systems have failed in respect of generating large numbers of employable people, whatever other qualities they may possess. Especially so in mathematics, physics and even English. My own contacts in industry are constantly telling me how hard it is to find good keen youngsters who can do simple arithmetic or write a sensible paragraph.

To a lesser extent but still serious is the university graduate who needs further training before being able to do any useful work in industry.

Now GEC-Marconi and Bath University have got together with a new  $4\frac{1}{2}$  year degree course for electrical and electronic engineers. British educational standards. savaged over the years by trendy educationists, have been thrown overboard. Instead the new standard is proudly announced as equivalent to the French Grandes Ecoles and the German Technische Hoch Schulen which, judging by results in those countries, is far more effective. I can testify, again from experience, that French and German graduates from their respective educational systems are just as 'rounded' and 'human' and 'socially responsible' as our own product. Frequently more so, as well as being better qualified and selfdisciplined.

The new Bath course, which also enjoys a support grant from the Engineering Industries Training Board, is to be a sandwich course with a difference. The difference is that individual students will be sponsored by individual GEC-Marconi companies to which they will return periodically for their industrial training sections of the course, eventually joining that company.

Emphasis is to be on real-life engineering, especially the systems approach to problem solving and design. Students will not only learn engineering fundamentals but will get thrown in at the deep end in case studies, seminars and role-playing, reminiscent of Harvard Business School management training.

I can only spot one fault in the scheme. It doesn't start until September 1980. Anyway, this gives plenty of time for prospective Masters of Engineering to apply to the School of Electrical Engineering, Bath University.

# End of Term

Company annual reports can be compulsive reading. Often for what they leave out or the neat way that difficulties are glossed over. They are obliged to give the facts and figures of performance but beyond the balance sheet there is plenty of scope for originality in keeping the existing shareholders contented and attracting new ones. They are sometimes like end-of-term reports and none more so than that of Teradyne Inc, the Boston-based ATE manufacturer.

Their latest 'theme' company report features seventeen of their top salesmen round the world. Punchy profiles of their backgrounds, their wives, hobbies and business philosophy. And, of course, how well they are doing for Teradyne and its shareholders.

After allowing for the publicity gloss, all are clearly dedicated to their company and to personal achievement. And all are constantly on the move. Champion traveller is Tim Chan, based in Taiwan and looking after his own country, Korea, Hong Kong, Singapore, Malaysia, Thailand and Indonesia. He needs two dozen visas in his passport to get around his vast territory. Stan Fuller, based in Phoenix, pilots his own Cessna 210. Rene Verhaegen covers Benelux in his Audi, clocking up 65,000km a year. And so one could go on.

This is a highly-motivated team with good products, high-priced, and sold worldwide. And the company is growing fast, now turning over \$100 million a year. Since founded it has never had a strike and has no collective bargaining contracts with its 2,000 workforce. Vice-President, sales, who heads up the global marketing is, for the record, not a high-powered tough American entrepreneur but a tough, high-powered Briton, Dennis P. O'Connell.

# Racal Breakthrough

Racal Communications Inc in the USA and Racal (Canada) Ltd were established many years ago in the hope of breaking through the 'Buy American' act which operated so unfairly against non-Americanowned companies in military procurement. Patience has now been rewarded but only with exceptional products which won the day in fierce competition. The US Air Force is initially buying \$11 million worth of a new Racal receiver, the RA 6790/GM, and the Canadian Armed Forces the RA 6778C to the tune of \$5.5 million Canadian.

The significance of the US Air Force contract is that it is the start of a replacement programme for the ageing R-390 communications receiver of which there are an estimated 40,000-plus in service round the world. The RA 6790 is a joint Racal UK/US development. With a different front panel it made its European debut at the Racalex 79 exhibition in London as the RA 1792. It features a new frequency synthesiser based on a special LSI chip designed by Racal Microelectronics Ltd and has a 100-frequency built-in memory for instant tuning to pre-selected channels.

# **Black Chips**

Oil-rich Nigeria might be the first black African country to produce microcircuits. According to reports, the University of Ife has been purchasing production equipment and Nigeria could be in the business by the early or mid-1980s.

# Naval Missile

British Aerospace Dynamics Group has received a £300 million shot-in-the-arm to develop a new sea-skimming anti-ship airlaunched guided weapon. Provisionally known as the P3T, the weapon is of the fire-and-forget type, pre-programmed by fire control computer just before launch with the on-board homing head and computer finding the target and moving in for the kill. It appears to be a further development of the Anglo-French Martel currently in service with the Royal Air Force. The only electronic subcontractor so far named is Marconi Space and Defence Systems for the active radar target seeker and homing head.

BA Dynamic Group is also looking at inhouse costs. At Stevenage a computeraided draughting and design system has been installed which is said to multiply draughtsman productivity by a factor of four. Of the 12,000 drawings a year currently produced, some 2,500 are expected to be handled by the automated system, leading to greater accuracy and consistent standards and cutting out much of the tedium of repetitive manual work. But apart from the benefits, BA Dynamics say, like others, that there is a shortage of suitably qualified design staff.

# Micro-min Laser

The latest in sophisticated micro-min is the world's smallest hand-held laser rangefinder, a little larger than a packet of 20 cigarettes and weighing, including battery, 1·2lb. An infantryman can easily carry it in his pocket and then has instant personal ranging up to 4,000 metres with an accuracy of  $\pm 3$  metres. The pulse output is a third of a megawatt and the manufacturer, International Laser Supplies Inc., expect the cost to be as 'little' as \$2,500 each in 1,000-off quantities.

# **Talking Calculator**

And the latest in calculators is Sharp's desk-top development that repeats calculations with a synthesised voice as you key them in or demand the answer. This feature seems of doubtful value—but then I haven't seen the full specification. Anyway, it appears that you can choose your own language, English, French, Spanish, German or Japanese.

# Learn Basic THIS MAY ...and enjoy it!

T HIS article is directed towards those electronics enthusiasts who have sufficient hardware experience but possess little or no knowledge of programming. According to a recent survey conducted by The Amateur Computer Club, 70 per cent of computer faithfuls are in this category and they will find that few books suit their particular needs. Having your own computer, or at least access to one, means that you can learn at the keyboard and at your own speed. The choice of BASIC as the language is inevitable. It is the most readily available for the home computerist, which is due in turn to the fact that it is easy to learn, to understand and to apply. It is also surprisingly versatile.

# INPUT AND OUTPUT

From here on it will be assumed that you are sitting comfortably at the keyboard, ready to 'converse' with the computer. We will ignore, at least to start with, the usual formal classifications of 'assignments', 'declarations' etc. and jump straight in at the deep end with the first essential in any communication system, INPUT and OUTPUT. This is done with statements which may be used directly, as if we were 'commanding' the computer. At this stage we will regard all such statements as 'instructions' and refer to them in this way. On entering BASIC, the computer will respond with the usual prompt,  $\# \blacksquare$ flashing etc. which indicates that you are in command and may proceed with your first (or next) entry.

In order to embark on a new program however, we must erase all traces of previous entries and initialise all variables. This is done by typing NEW at the terminal. Remember to do this every time a fresh program is started. There is one other entry which must be made each time an instruction is completed. This is the typing of the CR (carriage return) key, which indicates to the computer the end of that particular instruction set. Remember then, to press the RETURN key at the end of each instruction statement: and now we are ready to start. Type,

NEW (+ RETURN key)

and on the next line, type the following

PRINT 
$$25 - (19 - 7) * 2 + 50$$

# (+ RETURN)

The printer will respond with the result of this calculation, which is 51. This illustrates two features:

- 1. The instruction 'PRINT' means, in effect, "Evaluate this expression and PRINT the result".
- 2. The calculation follows the usual arithmetical sequence: brackets; powers; multiplication and division; addition and subtraction: and where two operations are in the same

category, the calculation is effected from left to right. This is more clearly shown in the next example. Try it.

PRINT 25 - 2 \* 3 + (6/2) 
$$\uparrow$$
 2 (+ RETURN)

The order here would be,

(1.) 6/2 (=3) (/ signifies DIVIDE)

(2.)  $3 \uparrow 2$  (=9) ( $\uparrow$  signifies TO THE POWER)

(3.) 2\*3 (=6) (\* signifies MULTIPLY)

This leaves 25 - 6 + 9 to be evaluated, so the last two steps would be,

- 4. 25 6 (=19)
- 5. 19 + 9 (=28)

which will have been printed on the next line. This, of course, is no more than any calculator can do, but it's a start. To move one step beyond the calculator stage, try this:

PRINT "A, B; C: D." (+ RETURN) (note the quotes, "")

# SPACING

You will have found that whatever appeared between the quotes, including spaces, was reproduced exactly as entered. Combining these features, we have simple control over our output. For example, try the following:

PRINT "THE SUM OF 5 AND 4 = "; 5 + 4 (+ RETURN) which produces,

# THE SUM OF 5 AND 4 = 9

Note the semicolon after the second quotes. This controls the spacing before the result of 5 + 4 is printed. Try the same line again using a comma instead of a semicolon. This time a space of about 7 characters will be left before the 9 is printed. The line is automatically divided into printing zones of 14 positions (this may vary slightly in different versions of BASIC) and the comma is used to effect this separation. Next, try

# PRINT "LENGTH", "BREADTH", "AREA"

which will print these headings, suitably spaced out at 14 unit intervals, ready for the print-out of a table of dimensions as follows:

LENGTH BREADTH AREA

Now experiment with various combinations of text, expressions and spacing, using both the semicolon and the comma.

Since each PRINT instruction produces a carriage return and line feed at the end of the statement, a PRINT used alone in a program will have the effect of skipping a line. You will have noticed by now that spaces are ignored by BASIC (except when they appear between quotes).

The computer sees no difference between

If memory space is short, quite a bit can be saved by omitting all spaces, but it will not do your sanity any good when you have to search for errors!

To summarise so far with an example,

which will produce,

$$LENGTH = 5 BREADTH = 7 AREA = 35$$

Note that in the print statement a space is left after each equals sign (=), before the quotes are closed, so that the values 5, 7 and 35 are suitably spaced away from the equality sign.

# **TAB FUNCTION**

There is one more convenient output control available in BASIC, the TAB function. This gives precise positioning for any part of a print-out, which you will now discover if you type the instructions,

# PRINT TAB(10);"BASIC IS BEAUTIFUL"

You will find that the first word is started in the tenth printing position. Note that the value 10 must be in parenthesis and that this in turn must be followed by a semicolon before opening the quotes. The value in brackets may be any expression, with or without variables, so the printing position can be made dependant on an earlier program routine and in the final evaluation, incorporated in the PRINT statement: all of which helps to make graph plotting much simpler.

Finally try,

PRINT TAB(5);"RESISTANCE = "; 25; TAB(25); "VOLTAGE = "; 5; TAB(40);"CURRENT = "; 5/25

This gives,

RESISTANCE = 25 VOLTAGE = 5 CURRENT = 0.2

... which shows that the TAB function may be used more than once in any one PRINT statement, so we have effective control over our print-out. (If the printer encounters a TAB value *less* than its present position, it will continue *from* its present position ... it can hardly go backwards!)

# **PROGRAM CONSTRUCTION**

Having learned to control print-out we can now move on to program construction. The first noticeable difference is that when a program is entered, there will be no response from the computer at the end of each line, as happened previously when in the command mode. Each line should be numbered to indicate that a program is being entered, and this also determines the logical order in which the steps will be executed. The numbered steps or statements may however be *entered* in any order, since the computer will, under BASIC control, execute them in the correct numerical (i.e. logical) order.

Line numbers are in multiples of five or ten. By leaving gaps between, additional lines can be sandwiched in; and the need to add, delete or in other ways alter a program after apparent completion is the rule rather than the exception.

The first example for you to try follows:

NEW

40 LET D = A-B (subtract B from A and place the result in store D)

50 PRINT "A + B = ";C, "A − B = ";D 60 END

The full program has now been entered and resides in memory, waiting for an instruction to start operating. The command in BASIC for this is RUN, so now type,

RUN (+ RETURN) .... and the immediate response will be,

$$\mathbf{A} + \mathbf{B} = 17 \qquad \mathbf{A} - \mathbf{B} = -7$$

The explanations on each line are hardly necessary, which is the beauty of BASIC; it is almost self-explanatory! Note that in some versions, the word LET is optional when in program mode, so line 30, for example, would be acceptable as,

30 C = A + B

#### VARIABLES

This program also demonstrates the use of letters as variables. In fact any letter from A to Z may be used, either alone or with a digit (0 to 9) as a suffix. For example A, A0, A1, A2, B2, Z2 are all acceptable as variables in the same program.

You will no doubt have realised that the above program can be simplified, since the PRINT instruction will deal with more than one calculation in the same line. Enter the following, NEW

10 LET A = 520 LET B = 1230 PRINT "A + B = "; A + B, "A - B = "; A - B 40 END

which will produce exactly the same output as before.

There is one more output control. Enter the following: NEW

- 10 PRINT "ALL THIS TEXT ";
- 20 PRINT "WILL APPEAR ";
- **30 PRINT "ON THE SAME LINE"**
- 40 END

As stated, the entire print-out will be on the one line, due to the effect of the semicolon at the end of lines 10 and 20, which is to suppress the carriage return and line feed normally following a PRINT statement. Notice the space left before the quotes were closed in lines 10 and 20, which prevents a 'cramming' of the words from the end of one line to the beginning of the next. One more similar example:

> 10 LET S = 1+2+3+4+5 20 PRINT "MEAN OF THE FIRST FIVE "; 30 PRINT "NATURAL NUMBERS = "; S/5 40 END RUN

This will give,

MEAN OF THE FIRST FIVE NATURAL NUMBERS = 3

This completes the list of all output instructions and practice should provide proficiency; and now with this repertoire, plus the skeleton of a program to work on, we can proceed to INPUT.

#### INPUT

Up to now, all data has been written into the program, but where the same program is used for different sets of values, it may be necessary to enter the data separately each time the program asks for a new set.

This can be done using the statement 'INPUT', which causes the program to stop and wait for the appropriate entries at the keyboard, each value separated from the next by a comma. When the program stops because of an INPUT instruction, a 'question mark (?)' will be printed to indicate to the user that data is requested. Here is a simple example to start with: NEW

10	INPUT A, B, C
20	PRINT A*A; B*B; C*C
30	END
RU	JN .

After line 10, the program stops, prints a question mark '?' and expects three values (separated by a comma) to be entered. When this is done (and followed in the usual way by RETURN), the three values are placed in stores A, B and C *in that order* and the rest of the program is implemented. In this way, by again entering RUN, a new set of data can be typed in and this can be continued as long as there is data available for evaluation.

Note that the order of entry of data must correspond to the order in which it has to be applied to the variables. If in the above example, we had entered 5, 7, 24 after the question mark '?', the print-out would have been,

# 25 49 576

Now try this complete program, using your own values for L, B and H.  $\!\!\!\!$ 

```
NEW
```

```
10 INPUT L,B,H
```

- 20 PRINT
- 30 PRINT "LENGTH", "BREADTH", "HEIGHT", "VOLUME"
- 40 PRINT
- 50 PRINT L, B, H, L+B+H
- 60 END RUN

The effect of this will firstly be a question mark '?', after which your values for L, B and H must be entered, followed by RETURN as usual. On receiving this input from the keyboard (remember the comma between), the next output will be, (using 5, 4, 3 for the data),

LENGTH	BREADTH	HEIGHT	VOLUME
5	4	3	60

The double spacing is effected by the PRINT statement in line 40 and the horizontal spacing is obtained by the use of commas in lines 30 and 50.

# GOTO

One disadvantage of the above program is that if we again type RUN in order to repeat for another set of data, the print-out will still include the headings LENGTH, BREADTH etc. To avoid this and to allow tabulation of further data under the original headings, it is necessary to introduce a new instruction, GOTO, which directs the program to a specific statement number from where it will continue execution in the usual numerical (logical) sequence. To effect these improvements there is no need to reenter the whole program. Any line may be deleted by typing the line number followed by RETURN; and a line may be altered by retyping the whole line (including the line number) correctly, when the new line will replace the old one. Just make the following additional entries:

20	GOTO	50
60	GOTO	10
70	END	

Now type RUN, when the question mark will appear as usual, but after receiving the next set of values the program will jump to line 50, missing the 'print headings' line and so continue to print out these values and result, tabulated as before. At line 60 the instruction is now 'GOTO 10', so the program returns to the start and requests the next set of data. While all this may satisfy our present requirements, it firstly introduces an undesirable element and secondly presents a problem. The unwanted part of the output, you will already have noticed, is the question mark followed by the data, which intrudes on the continuous tabulation of the print-out. A remedy for the latter will be explained later.

# LOOP PROBLEMS

Since the program returns to line 10 at the end of each routine, the END statement is never reached and we are 'stuck in a loop', a well known nightmare in programming. Although it does not interfere with the execution of this particular program, it will certainly cause you trouble sooner or later and this is as good a time to deal with it as any. To escape from such a dilema, the 'panic button' is used. This may vary in different versions of BASIC, sometimes a single key labelled 'ESC' (escape), or the combination of two keys, one a control key and the other a suitable character such as 'X' (exit), 'O' (out), 'C' (cancel) etc. For our purpose we will call it the ESC key, but refer to your own version to find the appropriate replacement. It may be necessary to press the ESC key repeatedly, depending on what sequence of operations the computer is engaged in, before you succeed in interupting the loop. The ESC key can also be used to halt the execution of a program at any time, if you want to return to the 'command' status, where the keyboard is again in control. Now try a variety of tabulation programs such as,

- 1 Volume of a cylinder (V), given the radius (R) and height (H). (V = 3.1416 \* R \* R \* H)
- 2 Tax (T) payable, given rate of tax (R%), gross income (I) and total allowances (A). (T = (I-A) \* R/100)
- 3 Value of resistance (R), given three resistances (R1, R2, R3) in parallel. (R = 1/(1/R1 + 1/R2 + 1/R3))



The listing for program one and its execution is shown above. If your machine has  $\pi$  in memory, only the actual symbol need be included. As the sign for raise to the power is  $\Lambda$ , statement 70 can be reduced to  $\pi \circ \mathbb{R} \Lambda 2 \circ \mathbb{H}$ .

# **READ AND DATA**

The input of data using the INPUT instruction (which is the only method available on minimum versions of BASIC) has obvious limitations, as you have already discovered. A second method which can be used requires two statements, READ and DATA, which must be programmed as a pair. The READ statement inputs data sequentially and finds its data in the corresponding order following the DATA statement. Type out the following,

> 5 READ A, B, C, D 10 DATA 2,3,4,5 15 PRINT (A+B)\*(C+D) 20 STOP

. . . which produces the output, 45

Several things to note here:

- 1. The values 2, 3, 4 and 5 will be read into stores A, B, C and D *in that order*. Care must be taken therefore, that the values following DATA are entered in the correct sequence to correspond to that of the variables.
- 2. The DATA statement (or statements) may appear anywhere in the program, provided that if there is more than one, they are still kept in the proper order.
- 3. The above example could have been written as,

10 DATA 2,3 16 DATA 4,5

... with exactly the same result, since the READ statement will search for the required data sequentially, wherever it appears in the program.

4. Instead of the usual END as the last entry, STOP has been substituted which, though also halting execution, transfers control to the keyboard to allow investigation of that part of the program before the next part is implemented. Provided that no changes are made to the program at this point, typing CONT will direct the computer to continue from where it received the STOP instruction.

Now enter the following:

- 5 READ A, B, C, D, E, F
- 10 DATA 6,8,9,21,3,13 . . . (or any six integers you care to use)
- 15 LET T = A+B+C+D+E+F
- 20 PRINT "MEAN = "; T/6
- 25 STOP

which will print,

MEAN = 10... then the program will stop and wait for further commands. By retyping line 10 with a fresh set of values, followed by GOTO 5 (no line number, since this is a command after a STOP), the program will return to the start and operate on the new data.

# FOR . . . NEXT LOOP

Attempt to find the mean of several hundred numbers by this method and there will obviously be trouble! Fortunately, the problem is easily solved by the use of a FOR . . . NEXT loop. Enter this program and see what happens.

5 FOR I = 1 TO 6 10 READ N 15 PRINT N\*N; 20 NEXT I 25 DATA 1,2,3,4,5,6 30 STOP The print-out will be, 1 4 9 16 25 36

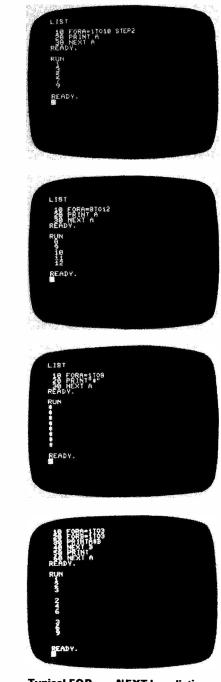
The FOR . . . NEXT loop operates in this way: the variable I (any letter may be used) takes on successive values from 1 to 6 and for each one, that part of the program which lies between

lines 5 and 20 is executed. As each new value of I is reached, a test is made to see if it has exceeded the 'TO' value (6 in this case), when the loop terminates and the rest of the program is completed. In effect, then, 'NEXT I' means, "Repeat this routine for the next value of I".

ł

m

By changing line 5 to have a larger terminating value for I, and by entering the appropriate amount of data, a large number



Typical FOR . . . NEXT loop listings

of values can be accommodated. Try this method now on the earlier program to find the mean of six numbers, but this time make it sixteen—or sixty.

Then try this program, which shows how part of the loop can depend on the value of I itself, and how the incremental step need not be unity. (The latter requires the addition of 'STEP N', where N may be any value, positive or negative, integer or decimal). Can you visualise what the print-out will look like?

5 FOR I = 1 TO 9 10 PRINT TAB(4\*I); I; 15 NEXT I 20 PRINT 25 FOR H = 18 TO 2 STEP -2 30 PRINT TAB(2\*H); H/2 35 NEXT H 40 STOP

It is sometimes helpful, when writing out your program, to offset that part which lies within the FOR . . . NEXT loop; on large programs this serves as a check on the start and finish of each loop. Some versions of BASIC will automatically produce such a print-out. This has been done in the last program at lines 10 and 30.

Before continuing with further examples of the FOR ... NEXT loop, it will be helpful to introduce a few more controls and to be more specific about the use of numbers.

Except in the minimum versions of BASIC, where only integers are acceptable, any real number may be entered, to at least eight significant figures, the range varying for different versions, but usually from  $\pm 10^{-99}$  to  $\pm (10^{100} - 1)$ . Numbers may be entered normally as integers or decimals, or in exponent form; (for example, 176, 49.75, or 314159E-5, the latter representing  $314159 \pm 10^{-5}$ . The E stands for exponent).

You will no doubt have typed a few errors by now and will have found retyping the whole line exasperating. This can be avoided by the use of two devices, the BACKSPACE control and the DELETE. The former will cancel the last character to be entered and the latter will erase the whole line. Refer to the manual for your particular version, since these controls vary, the most likely ones for a BACKSPACE being a CONTROL C (for CANCEL), or a CONTROL  $\leq$ —.

# **REM AND LIST**

Finally, two facilities which will prove invaluable when 'debugging' a program, the REM (remark) statement and the LIST command.

The REM statement allows comments or explanations to be attached at intervals throughout a long program, without interfering with its operation. Anything following REM on the same line will be ignored by the program but will be printed out in any listing. This brings us to the use of LIST which, as a command, will cause the whole program, as then held in memory, to be printed in correct order; which allows an examination and check of the present state of the program. Further, by typing, for example, 'LIST 35', only line 35 will be listed; and by entering 'LIST 20, 70', all lines from 20 to 70 inclusive will be printed.

Combining some of these new facilities and using the FOR . . . NEXT loop, type out this program exactly as shown.

- 5 REM TO FIND THE MEAN OF ANY NUMBER OF VALUES
- 10 PRINT "HOW MANN  $\leftarrow$  Y NUMBERS ARE THERE?
- 15 INPUT N
- 20 FOR I = 1 TO N
- 25 READ X
- 30 LET T = T + X
- 35 NEXTI
- 8 LET T = O
- 40 **PRINT** "TOTAL = "; T
- 45 **PRINT** "MEAN = "; T/N
- 50 STOP
- 40 (+ RETURN)
- 38 DATA 7, 12, 5.8, 2.9E2, 99.4E-1, ... (select your own data) LIST

In line 10, an error was typed, so the backspace (CANCEL) character, control  $\langle - \rangle$ , was entered following the extra 'N', which corrected the word 'MANY'. (Check that your version uses  $\langle - \rangle$ ; it may be different). After line 35 was entered it was realised that the totalling store, T, would have to be set to zero for the first and each subsequent set of values. Line 8 was then typed in to accomplish this. It was also decided at this point that a print-out of the actual total was not required, so line 40 was erased by entering 40 followed by RETURN. It was now discovered, as sometimes happens, that the data itself had been forgotten and this was then entered as line 38. Because of these changes, a listing was requested by typing LIST (and RETURN), when the following output was obtained.

- 5 REM TO FIND THE MEAN OF ANY NUMBER OF VALUES
- 8 LET T = O
- 10 PRINT "HOW MANY NUMBERS ARE THERE ?"
- 15 INPUT N
- 20 FOR I = 1 TO N
- 25 READ X
- 30 LET'T = T+X
- 35 NEXTI
- 38 DATA 7,12,5·8,2·9E2,99·4E-1,...
- 45 **PRINT "MEAN = "; T/N**
- 50 STOP

If the program is now run, the value of the mean will be printed; and if a re-run is required for a new set of values, enter line 38 again with the new data, then type

GOTO 8... which will return control to the program at line 8, repeating the whole process.

This example also demonstrates how the terminating value, N, in the FOR . . . TO statement (line 20) can itself be a variable and therefore alterable for each new set of data.

#### IF...THEN

Most versions of BASIC offer a number of functions such as ABS(X), INT(X), RND(X) and SQR(X), which will find the absolute value of X, the largest integer not greater than X, a random number derived from X and the square root of X respectively. The latter will almost certainly be obtained from a simple sub-routine which uses a process of iteration to obtain the square root; and this will form an ideal example with which to introduce the IF . . . THEN statement. This is the decision-making facility in BASIC, where an expression of relativity appears between IF and THEN.

For example,

IF A > B THEN 50... will cause the program to branch to line 50 if the relation A > B is true. Otherwise it will continue to the next line in the sequence. Here is the program, expanded slightly, in order to make its operation easier to follow.

5 REM SQUARE ROOT 10 LET E1 = 2 15 PRINT "ENTER NUMBER" 20 INPUT N 25 LET Q = N/E1 30 LET E2 = (Q+E1)/2 35 IF ABS(E1--E2) < 0.0001 THEN 50 40 LET E1 = E2 45 GOTO 25 50 PRINT "SQUARE ROOT = "; E2 55 STOP

In line 10, the first estimate, E1, is given any reasonable value, in this case, 2. Line 25 divides the number, N, by E1 and puts the quotient, Q, in store Q. Since the root of N will lie between Q and E1, the average of these two values is calculated in line 30 and placed in store E2. Line 35 tests to see if the absolute difference between this new improved estimate and the previous



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one is significant (you may choose your own degree of accuracy here): if not, the last calculated estimate, E2, is printed. If the absolute difference is still too great, E1 takes on the value of E2 (line 40) and a return is made to line 25 to repeat the loop. A calculation of this type, which may have to be undertaken frequently in a longer program, can be tucked away in a corner as a sub-routine, to be called into use when required. This is effected in BASIC by the statements GOSUB and (to get back to the main program at the exit point), RETURN. An example of this occurs in the following program, which finds the roots of a quadratic equation,  $Ax^2 + Bx + C = O$ , given the values of the co-efficients, A, B and C.

5 PRINT "ENTER CO-EFFICIENTS" 10 INPUT A,B,C 15 LET D = B\*B-4\*A\*C20 IF D < O THEN 80 25 GOSUB 50 30 LET X1 = (R-B)/2/A35 LET X2 = -(R+B)/2/A40 PRINT "ROOTS ARE "; X1; X2 45 GOTO 85 50 LET E = 255 LET R = (D/E+E)/260 IF ABS(R-E) < 0.0001 THEN 75 65 LET E = R70 GOTO 55 **75 RETURN** 80 PRINT "NO REAL ROOTS" 85 STOP

Line 20 tests to see if D is negative and if so, causes a branch to line 80, which declares that there is no real solution and the program stops. If D is not negative, it proceeds to line 25 which in turn directs operations to the sub-routine at line 50. Having obtained the square root of D (held in store R) to the required accuracy, line 75 returns the sequence to line 30, where we left the main program. Finally, line 45 directs operations past the sub-routine to the STOP statement. If required, a 'GOTO 10' command will return everything to the start for the next equation.

#### ON . . . GOSUB, ON . . . GOTO

To complete this topic, there are two more useful statements which are used in conjunction with GOSUB and GOTO; they are ON ... GOSUB and ON ... GOTO. Try to assess the effect of the following program before typing RUN.

PRINT "TYPE 1, 2 OR 3"
 INPUT X
 ON X GOTO 25, 35, 45,
 PRINT "YOU ENTERED 1"
 GOTO 50
 PRINT "YOU ENTERED 2"
 GOTO 50
 PRINT "YOU ENTERED 3"
 END
 RUN

You will have discovered that line 20 effects a branch to either lines 25, 35 or 45, depending on the value of X, which may be any value or expression, greater than zero. For X = 1 the program is directed to line 25, X = 2 sends it to line 35 and X = 3 to line 45. If X < 1 or  $X \ge 4$ , an error message will be printed and if X is not an integer, it will first be truncated to an integer value. The statement ON . . . GOTO could be replaced by ON . . . GOSUB with a similar effect, the branch going to some sub-routine within the program.

#### DIM

A set of numbers arranged in a row or column, or an array of numbers held in matrix or table form can be manipulated very easily using the DIM statement in BASIC. This defines the dimension of an array, when named in the program, using any letter of the alphabet. For example, DIM Y(100) allocates memory space sufficient to deal with 100 values and reserves it for the array named Y. For a two-dimension matrix, the statement becomes DIM Z(A,B), where A and B define the number of elements in the row and column respectively of matrix Z. A table of values consisting of 20 rows and 15 columns would therefore be entered as DIM T(20,15). There is a limit set to the size of A and B, which will vary from one version to another, but usually at least 255 elements are allowed. Although an array having less than ten elements (or ten by ten in two dimensions) need not be defined by the DIM statement, it is advisable, in order to save memory space, to do this anyway. It is usually necessary to use a FOR ... NEXT loop to read into or print from an array, the following program illustrating this for a one dimension set.

5 REM PRIME NUMBERS LESS THAN 1000 10 DIM A(1000) 15 FOR H = 2 TO 1000 20 IF A(H) < O THEN 50 25 PRINT H; 30 IF H > SQR(1000) THEN 50 35 FOR I = H to 1000 STEP H 40 LET A(I) = -1 45 NEXT I 50 NEXT H 55 END

Line 10 reserves space for the one-dimension array named A. This will usually set all elements to zero, but in some versions it may be necessary to do this in the program first, for example:

60 FOR K = 1 TO 1000 70 LET A(K) = 0 80 NEXT K

# **NESTED LOOPS**

Above is the first program which has used nested loops (a loop within a loop) and this will also be required when dealing with a two-dimension array. At line 15, the outer loop is started for the first value of H, which is then printed, line 25. The second, inner loop starts at line 35 and is repeated for all defined values of I by the statement in line 45. Line 50 now returns the program to the start of the outer loop for the next round. Note that all the circuits of loop I are undertaken before the next round of loop H begins. For a two-dimension array, a similar arrangement is necessary. To illustrate, the following program reads in the 20 elements of a 5 by 4 table, replacing all odd values by zero, then printing the revised table.

5	DIM T(5,4)
10	FOR $I = 1$ TO 5
15	FOR $H = 1 \text{ TO } 4$
	READ T(I,H)
25	IF $T(I,H)/2 = INT(T(I,H)/2)$ THEN 35
30	$\text{LET } \mathbf{T}(\mathbf{I},\mathbf{H}) = 0$
35	NEXT H
40	NEXT I
45	DATA
	3,14,12,5,20,18,7,14,19,30,25,25,16,4,7,11,21,30,24,6
50	REM PRINT REVISED TABLE
55	FOR $J = 1$ TO 5
60	FOR $K = 1 \text{ TO } 4$
65	PRINT T(J,K)
70	NEVTV

75 PRINT 80 NEXT J 85 END

The print-out from this will be,

0	14	12	0
20	18	0	14
0	30	0	0
16	4	0	Ō
0	30	24	6

A few points to note from this last program:

1. Since the outer loop is from 1 to 5, the values will be read in as 5 rows, the inner loop expecting 4 elements for each row. The data therefore, must be entered similarly in order, row by row. While the table may, if preferred, be read

# E24 PARASCAN

To assist understanding of how BASIC commands work *together*, the following program is explained step by step.

Should you have need of an odd value resistance, E24 Parascan will compare every possible combination of twin parallel resistors, and display those which meet your require-

- 20 DATA 1, 1.1, 1.2, 1.3, 1.5, 1.6, 1.8, 2, 2.2, 2.4, 2.7, 3
- 30 DATA 3.3, 3.6, 3.9, 4.3, 4.7, 5.1, 5.6, 6.2, 6.8, 7.5, 8.2, 9.1
- 40 DIM R(24) : FOR A = 1 TO 24 : READ R(A) : NEXT A
- 100 X=1:Y=1:INPUT"RESISTANCE ";R
- 105 IF R>4550000 THEN PRINT"OUT OF RANGE ": GOTO 100
- 110 INPUT"% TOLERANCE ";T
- 120 L=R-(T/100)\*R : U=R+(T/100)\*R
- 130 PRINT"FROM ";L;" TO ";U;" OHMS" : PRINT
- **200** FOR Z = 1 TO 7
- 230 FOR M = 1 TO 24 : IF R(M)\*X<R THEN 275
- **233** FOR W = 1 TO 7
- 235 FOR N = M TO 24 : IF R(N)+Y<R THEN 270
- 240 P=R(M)\*X\*R(N)\*Y/((R(M)\*X)+(R(N)\*Y))
- 250 IF P<L OR P>U THEN 270
- 255 T1=((100\*P/R)-100)\*1000 : T1 = INT(T1)/1000
- 256 R1=R(M)\*X : K\$="": K1\$=""
- 257 IF X>100 THEN R1=R1/1000 : K\$="K"
- 258 IF X>100000 THEN R1=R1/1000 : K\$="M"
- 262 R2=R(N)\*Y : IF Y>100 THEN R2=R2/1000 : K1\$="K"
- 263 IF Y>100000 THEN R2=R2/1000 : K1\$="M"
- 265 PRINT R1; K\$; TAB(6)"||"; R2; K1\$; TAB(14);"="; P; TAB(28);T1; "%"
- 270 NEXT N : Y=Y\*10 : NEXT W : Y=1
- 275 NEXT M : X=X\*10
- 280 NEXT Z

Without graphic embellishments this program is fairly portable (will work on most machines) but the UK101 requires that READ statements *precede* DATA statements. The E24 resistors are assumed to be zero tolerance. in columns, it cannot be printed this way and of course it is necessary to have the same arrangement for both the READ and PRINT statements.

- 2. If an odd number is divided by two the result cannot be an integer, so line 25 uses the INT(X) function to test each element for even status. Note also the use of 'nested' brackets in this line.
- 3. If line 35 is now changed to ... 35 PRINT T(I,H), ..., line 36 becomes ... 36 NEXT H ... and a PRINT inserted at ... 38 PRINT ..., lines 50 to 80 will not be required, as the print-out will be processed while the loops are being cycled.

This by no means exhausts all the commands, functions and statements available in BASIC, but with further practice and experience it should be easy to learn the others from a BASIC manual.

ments.

The computer asks for the resistance you require (assumed to be in Ohms), and then asks for the acceptable tolerance (just enter figure).

SDATA statements containing the fundamental decade of the E24 range

A variable R is chosen, subscripted (n), to identify the above DATA. To cope, n must be from 1 to 24, so R(n) is DIMensioned thus.

A FOR-NEXT loop is used to READ in the data, where A plays the part of  $\boldsymbol{n}$ 

Variables to be used later are preset. Then the machine is programmed to ask for the required resistance, and designates it R. The computer will not confuse this with R(n)

The highest resistors this program will compare are:  $9M1 \parallel 9M1$ , so that nothing greater than  $4M55\Omega$  can be found. Only when the IF condition is true will the PRINT and GOTO statements be executed

Requests % tolerance required, designated T

Algorithm calculates upper and lower (U and L) limits allowable

These limits are printed for user reference. The null PRINT statement creates a line space on the screen

Specifies instructions 230 to 275 to be executed 7 times (the number of E24 multiples to be considered for one arm of the parallel pair), eg. 4.7, 47, 470, 4k7, 47k, 470k, and 4M7

Specifies instructions 230 to 270 to be executed 24 times (the number of E24 values to be considered for one arm of the parallel pair)

The IF statement will successively bypass to NEXT M until the sampled resistor is at least as high as the requested one. This avoidance of unnecessary processing considerably speeds up the action

Specifies instructions 235 to 270 to be executed 7 times (same as line 200, but for other arm)

Specifies instructions 235 to 270 to be executed up to 24 times (same as line 230, but for other arm). N is sampled from M to 24 to avoid repeat sampling of that which occurred in the M loop. eg.  $4k7 \parallel 8k2$  and  $8k2 \parallel 4k7$  is avoided

Each time this main algorithm is executed, P becomes the parallel value of the resistors being tested. The "product-over-sum" equation is used on resistors R(M) and R(N), with X and Y as their respective multipliers

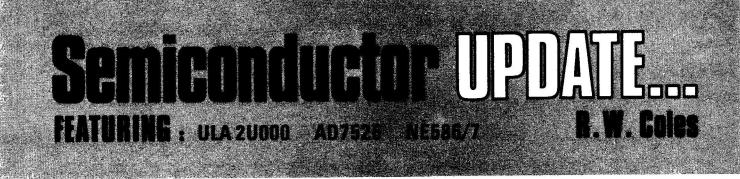
Checks that P falls within U and L, IF not, THEN jumps to next value

T1 becomes the percentage error of P to requested R. The first statement deliberately over-calculates T1 by a factor of 1000, so that the INT statement can round-down to a manageable 3 decimal places, by dividing by 1000

Converts R(M) and R(N) to R1 and R2 ready for PRINT statement. The purpose of this block of instructions is to convert print-out to  $\Omega$ ,  $k\Omega$ , and  $M\Omega$ , to save screen space

The output PRINT instruction (bypassed by out-of-range parallel R combinations). R1 and R2 are the resistor values; K\$ and K1\$ state the units. Quotes contain the parallel symbol "" and "%" symbol

These specify that the NEXT value of N, or M, should be tried. Although two NEXTs may share the same line, NEXT W, for example, will not be selected until all the Ns from M to 24 have been tried (see, line 235). In this example, the multiplier Y will be raised to the power of ten in the process



# THE EVERYTHING CHIP

My first offering this month is not something that hobbyists can easily rush out and buy, but I do feel that it will interest most PE readers for two reasons: (a) It is British to the core, and (b) It is a novel device with almost unlimited potential which is sure to crop up in "hobby sockets" before long.

The device in question is the Ferranti **ULA 2U000,** where the ULA part stands for Uncommitted Logic Array. There isn't anything new about the ULA concept itself, Ferranti have been selling versions based on their unique Collector Diffusion Isolation (CDI) technology for several years, but their latest offering really does look a winner in a truly internationl sense. But first, a word about the ULA philosophy.

In these days of Large Scale Integration (LSI), anyone can get a complex logic system integrated as a single chip providing they are prepared to order at least 10,000 to make it cost effective! Anyone who can't afford those sort of quantities has to make do with random logic chosen from the TTL or CMOS families for example, or perhaps a microprocessor with its attendant memory and peripheral chips. Those are the main options, and for many applications none of them fit very well. It is in these "awkward" applications where the great British ULA compromise can come to the rescue.

The ULA is an LSI chip which consists of an array of standard logic gates without interconnections. The uncommitted semiconductor chips are mass produced with all the economics of scale which that brings, and then stockpiled (unpackaged) as a standard product. When Joe Bloggs & Co. want a washing machine controller chip, or John Smith & Co. need a controller for an electronic camera, they draw up a logic diagram with all the necessary gates, counters, flip-flops and drivers shown, and Ferranti produce a final metallisation mask which interconnects the gates on a ULA to do the job. The fact that only the final mask is "special" means that design time is short and the resulting devices are much cheaper than a discrete logic, or microprocessor, approach.

The 2U000 seems to be the ultimate device in a logical progression of ULAs from Ferranti, and in this case it can do *more* than the custom MOS LSI competition because it has linear circuitry on chip as well as the normal ULA logic gates. With the 2U000 it is possible to build complete systems with gates, flip-flops, counters, Schmitt triggers, l.e.d. drivers, comparators, oscillators, and amplifiers, all on one chip

with any number of package pins from 14 to 40! The new chip can be battery powered too, sipping only about one milliamp from a one volt supply despite the 256 logic cells (each of which can be connected as two two-input gates) *and* the forty linear or interface cells which are arranged around the chip periphery.

You still can't get your hands on goodies like this in one-off or even ten-off quantities of course, but you don't have to order ten thousand either! If there is any justice in this world, this chip should be a real winner for Ferranti and for Britain.

#### **DIGI-POT**

If you need an accurately set potentiometer with good resolution for an instrumentation application say, the old way to do it is to use a bulky, wire wound, helical pot with a turns counting dial. It would be expensive, the pot would wear out eventually, and reading the dial wouldn't be too easy, but it would work, and with luck you might get 1:1000 usable resolution. Soon you'll be able to do it the digital way—thanks to Analog Devices and their Multiplying Digital to Analogue Converters (MDACs).

Now I suppose everyone knows roughly what a DAC is (parallel binary in-proportional analogue signal out at the other end) but I for one always expected to see a precision d.c. reference supply used with every DAC, and that's where the M comes in, to prove me wrong. A multiplying DAC can be used with any signal on its "reference" pin-even an a.c. waveform which swings above and below ground. So, instead of binary in and analogue out with the scaling set by a precision d.c. reference, we get a.c. signal in and a.c. signal out with the output related to the input by a scaling factor determined by the binary input. In effect the a.c. input is multiplied by the binary input, with the largest multiplier being unity.

Now, I have been talking about an a.c. signal input, just to show the change in emphasis in MDAC applications, but actually it can be any sort of signal, a.c., d.c. or precision reference. A classic application for an MDAC might be the control of gain or "level" in an audio channel by means of a computer or microprocessor, but there are many other occasions when an analogue signal has to be kept under precise, digital control.

So much for MDACs but how about Analog Devices and digital pots? Analog devices have a whole family of MDACs available already, but newly added is the

AD7525 which has the distinction of having b.c.d. (binary coded decimal) rather than straight binary inputs. B.c.d. is of course great for interfacing with people as every calculator knows, because it is easy to convert to and from decimal (or denary for the purists!). Team up the AD7525 with a 31 digit thumbwheel switch, which can be set from 0000 to 1999 and you have got yourself the simplest, most reliable, precision potentiometer money can buy. You can use it anywhere you need a precision pot-power supply O/P voltage setting, amplifier gain setting, time delay setting and so on. It will work for a.c. and d.c. signals and you can put it right in the signal path with only the non-critical b.c.d. connections brought to the front panel.

#### **IMPROVED DECODER**

When the 7447 seven segment decoder joined the TTL family it was one of the most complex devices then available, and all those goodies like leading zero suppression and intensity modulation capability made it and its attendant filament or l.e.d. displays very attractive compared with the traditional high voltage "Nixie" tubes previously used for number indication. Time marches on however, and the 7447 has now got competition. Most of the competition up to now has had a limited area of application, but a pair of new devices from Signetics/Mullard look ready to oust the 7447 from its industry-standard position.

The devices, coded NE586 and NE587 do all that the 7447 does, including leading zero suppression and intensity modulation, but in addition they both feature an input latch and constant current output drivers which remove the usual need for a collection of current limiting resistors. The input latches make interfacing with microprocessors and other systems, like counters, where data is available only in a dynamic form, very easy. The NE586 has a fixed O/P drive current of 25mA per segment which is suitable for a range of seven segment l.e.d. digits. The NE587 has an extra pin which allows single resistor programming of the output current up to a 50mA maximum, making display multiplexing easier and the choice of l.e.d. digit even wider.

Ferranti Ltd., Gem Mill, Chadderton, Oldham, Lancs. OL9 8NP.

Analog Devices Ltd., Central Avenue, East Molesey, Surrey KT8 0SN.

Signetics/Mullard Ltd., Mullard House, Torrington Place, London WC1E7HD.



**zaona ante**na si sa ante a si A selection of readers' Star Star original circuit ideas. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought. States and Why not submit your idea? Any idea published will be awarded payment according to its merits. 

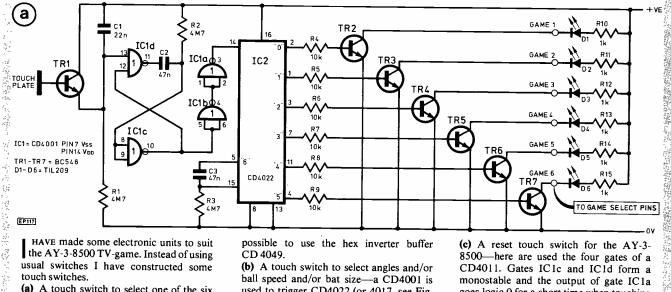
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must be accompanied by a declaration to the effect that it is the original work of the undersigned, and that it has not been accepted for publication elsewhere.

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# TOUCH SWITCHES FOR GAMES CHIP



HAVE made some electronic units to suit the AY-3-8500 TV-game. Instead of using usual switches I have constructed some touch switches.

(a) A touch switch to select one of the six games-this was built around the CD4022 which is made to count from '0' to '5' via R3 and C3. At count '6' pin 5 goes high and thus resets the counter to '0'. Pin 15 is usually held logic 0 by R3.

IC1a and IC1d of the CD4001 form a monostable which is triggered by TR1 by placing a finger on its base. The output of the monostable is fed to IC1b and then to IC1a to give a good pulse to the input of CD4022, pin 14. The outputs will randomly go high

making TR2-TR7 conduct, and by connecting the game selector pins of the AY-3-8500, a touch at the base of TR1 will change game. You may also connect six l.e.d.s and six resistors to the collectors and the positive supply line. Instead of using TR2-TR7 it may be

and and an a color and an and a state and a straight a solution and an an an and an and an and a state of a stat

possible to use the hex inverter buffer CD 4049

(b) A touch switch to select angles and/or ball speed and/or bat size-a CD4001 is used to trigger CD4022 (or 4017, see Fig. 5) in the same way as before. The outputs of CD4022 are connected via twelve diodes to the bases of TR2-TR4 and the collectors are randomly high/low, which is seen from the l.e.d.s. There are eight different stages, which will be seen from the table below.

	<b>4022</b> o/p	Angles TR2	Bat size TR3	Ball speed TR4
2	0	1	1	1
1	1	1	1	0
3	2	1	0	1
7	3	0	1	1
11	4	1	0	0
4	5	0	1	0
5	6	0	0	0
10	7	0	0	0
	Whi	To Pin 5 ich are pins		Pin 7 500

(c) A reset touch switch for the AY-3-8500-here are used the four gates of a CD4011. Gates IC1c and IC1d form a monostable and the output of gate IC1a goes logic 0 for a short time when touching the base of TR1.

(d) Automatic/manual serve of the TVgame-gates IC1b and IC1c form a monostable and the output goes logic 0 for a short time, by touching the base of TR1, this is the manual serve. Gates IC1a and IC1d form a bistable. The output of gate IC1a is logic 1 always after a touch at TR1 but change to logic 0 by touching the base of TR2 and thus remains logic 0-and this is necessary for the auto-serve.

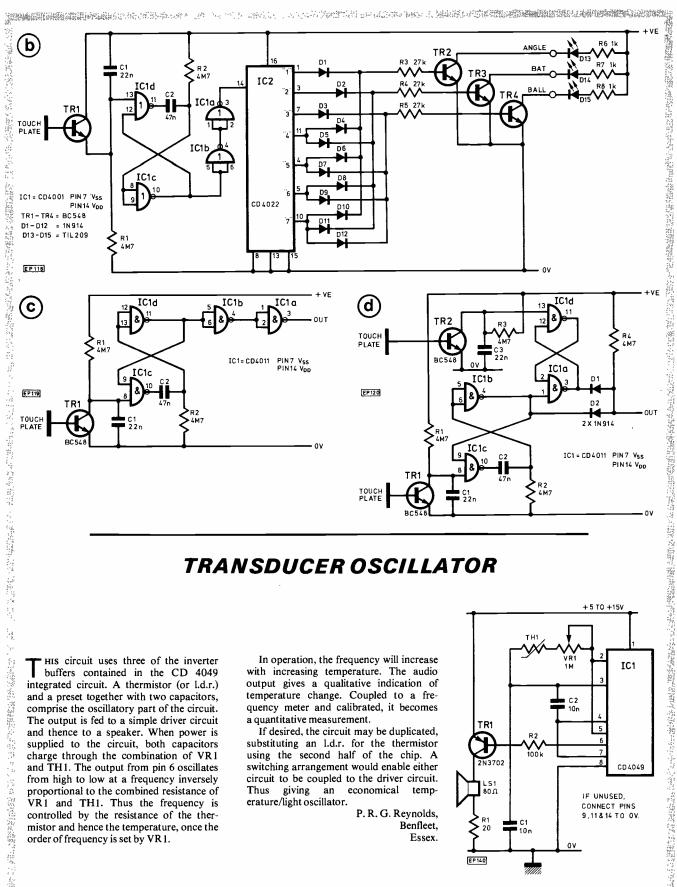
Olav Foldoy, Tananger, Norway. Ŵ

200

3,

19.67.6

100



# TRANSDUCER OSCILLATOR

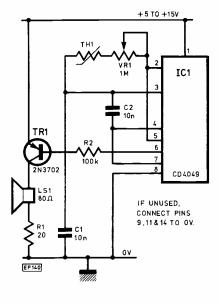
HIS circuit uses three of the inverter buffers contained in the CD 4049 integrated circuit. A thermistor (or l.d.r.) and a preset together with two capacitors, comprise the oscillatory part of the circuit. The output is fed to a simple driver circuit and thence to a speaker. When power is supplied to the circuit, both capacitors charge through the combination of VR1 and TH1. The output from pin 6 oscillates from high to low at a frequency inversely proportional to the combined resistance of VR1 and TH1. Thus the frequency is controlled by the resistance of the thermistor and hence the temperature, once the order of frequency is set by VR1.

2.4.65

In operation, the frequency will increase with increasing temperature. The audio output gives a qualitative indication of temperature change. Coupled to a frequency meter and calibrated, it becomes a quantitative measurement.

If desired, the circuit may be duplicated, substituting an l.d.r. for the thermistor using the second half of the chip. A switching arrangement would enable either circuit to be coupled to the driver circuit. Thus giving an economical temperature/light oscillator.

P. R. G. Reynolds, Benfleet, Essex.



# SOUND-TO-LIGHT SEQUENCER

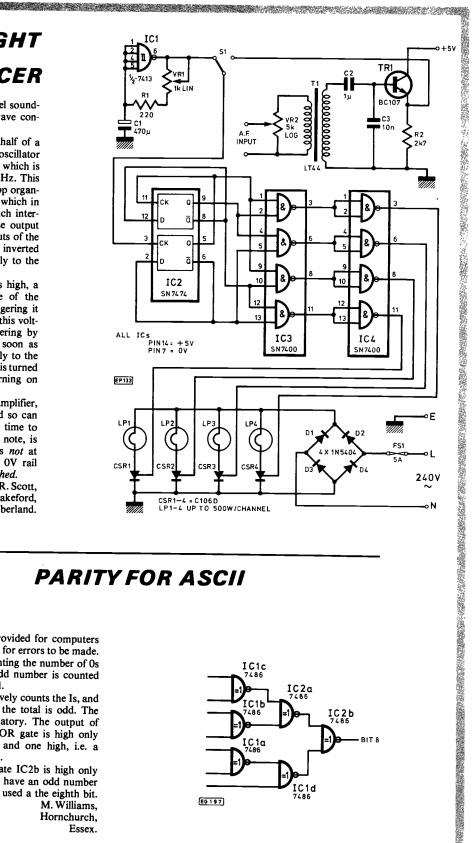
\*HE circuit shows a four channel soundlight sequencer utilising full wave control.

Clock pulses are drived from half of a 7413. This is connected as an oscillator with a fast edge and a frequency which is variable between about 0.5 to 20Hz. This clocks one half of the 7474 flip-flop organised as a divide by four counter which in turn is coupled to a decoder which interprets these four states and whose output sequences a low state at the outputs of the NAND gates. These outputs are inverted by IC4 and then are taken directly to the gates of the thyristors.

When any output of IC4 goes high, a logic 5V is applied to the gate of the corresponding thyristor, thus triggering it into conduction. When, however, this voltage is removed, as it is on triggering by the following clock pulse, so as soon as the full wave rectified mains supply to the thyristor falls to zero, the thyristor is turned off and so the cycle repeats, turning on each thyristor in turn.

The input of the low frequency amplifier, is connected across a speaker and so can be used to sequence the lights in time to the beat of music. One point to note, is that, as the ground connection is not at earth potential, but at 240V, the OV rail on the logic supply must not be earthed.

> R. Scott. Stakeford, Northumberland.



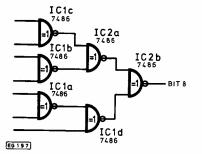
# **PARITY FOR ASCII**

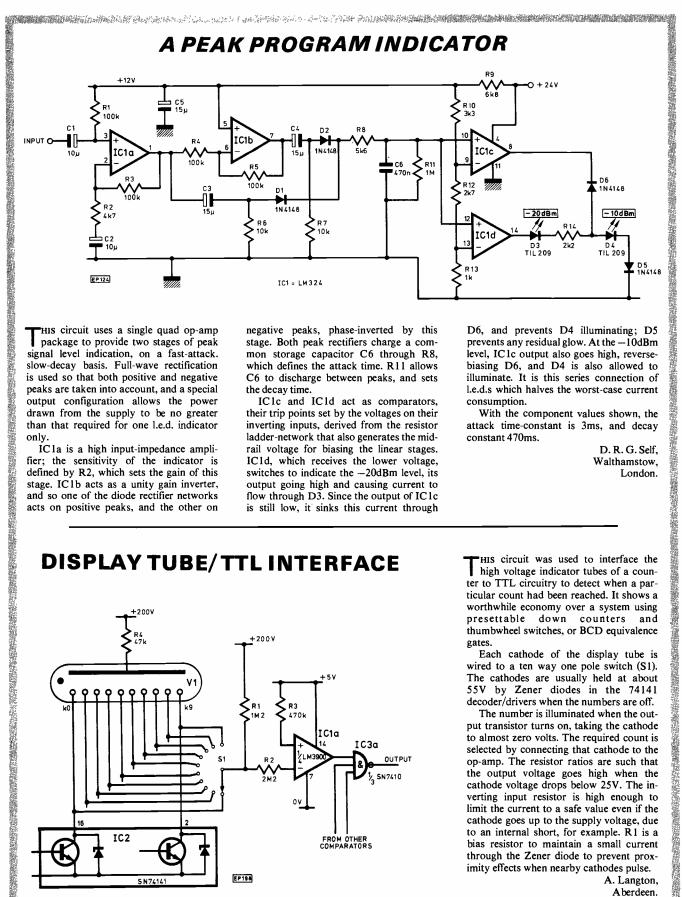
DARITY bits are provided for computers to enable a check for errors to be made. This is done by counting the number of 0s and 1s, and if an odd number is counted an error has occurred.

This circuit effectively counts the Is, and adds a parity bit if the total is odd. The circuit is self-explanatory. The output of each EXCLUSIVE-OR gate is high only if one input is low and one high, i.e. a check for odd or even.

This means the gate IC2b is high only if the first seven bits have an odd number of 1s. This output is used a the eighth bit. M. Williams,

Hornchurch. Essex.





HIS circuit uses a single quad op-amp package to provide two stages of peak signal level indication, on a fast-attack. slow-decay basis. Full-wave rectification is used so that both positive and negative peaks are taken into account, and a special output configuration allows the power drawn from the supply to be no greater than that required for one l.e.d. indicator only.

IC1a is a high input-impedance amplifier; the sensitivity of the indicator is defined by R2, which sets the gain of this stage. IC1b acts as a unity gain inverter, and so one of the diode rectifier networks acts on positive peaks, and the other on negative peaks, phase-inverted by this stage. Both peak rectifiers charge a common storage capacitor C6 through R8, which defines the attack time. R11 allows C6 to discharge between peaks, and sets the decay time.

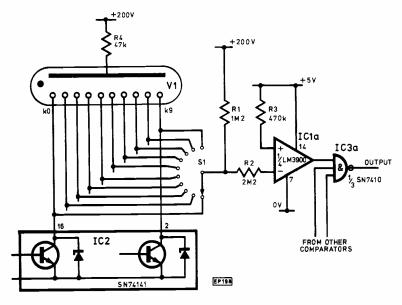
IC1c and IC1d act as comparators, their trip points set by the voltages on their inverting inputs, derived from the resistor ladder-network that also generates the midrail voltage for biasing the linear stages. IC1d, which receives the lower voltage, switches to indicate the -20dBm level, its output going high and causing current to flow through D3. Since the output of IC1c is still low, it sinks this current through

D6, and prevents D4 illuminating; D5 prevents any residual glow. At the -10dBm level, IC1c output also goes high, reversebiasing D6, and D4 is also allowed to illuminate. It is this series connection of l.e.d.s which halves the worst-case current consumption.

With the component values shown, the attack time-constant is 3ms, and decay constant 470ms.

> D. R. G. Self, Walthamstow, London.

# **DISPLAY TUBE/ TTL INTERFACE**



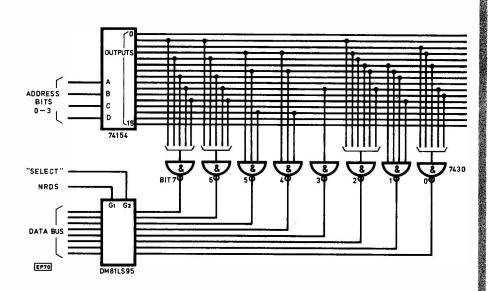
HIS circuit was used to interface the high voltage indicator tubes of a counter to TTL circuitry to detect when a particular count had been reached. It shows a worthwhile economy over a system using presettable down counters and thumbwheel switches, or BCD equivalence gates.

Each cathode of the display tube is wired to a ten way one pole switch (S1). The cathodes are usually held at about 55V by Zener diodes in the 74141 decoder/drivers when the numbers are off.

The number is illuminated when the output transistor turns on, taking the cathode to almost zero volts. The required count is selected by connecting that cathode to the op-amp. The resistor ratios are such that the output voltage goes high when the cathode voltage drops below 25V. The inverting input resistor is high enough to limit the current to a safe value even if the cathode goes up to the supply voltage, due to an internal short, for example. R1 is a bias resistor to maintain a small current through the Zener diode to prevent proximity effects when nearby cathodes pulse.

A. Langton, Aberdeen.

# SIMPLE TTL READ ONLY MEMORY



**O**NE of the problems facing the amateur user of microprocessors is that of loading programs into memory for testing. One can purchase a manufacturer-supplied ROM, which then restricts one to the manufacturer's methods of programming, or one can program one's own ROM, which is expensive. This approach presents an alternative method using a TTL ROM which is both flexible and economical for small programs. The program is designed for a system based around National's SC/MP, but the principle is applicable to any microprocessor system.

The "bootstrap" program is as follows: Location Instruction Rit

Location	manucuon	DIL
		Configuration
0	None	0000 0000
1/2	LDI 1	1100 0100
		0000 0001
3	XPAH P1	0011 0101
4/5	LDI 7	1100 0100
		0000 0111
6	XPAH P2	0011 0110
7/8	LD 0(P2)	1100 0010
		0000 0000
9/10	ST @1(P1)	1100 1101
		0000 0001
11/12	LD 0(P2)	1100 0010
		0000 0000
13	XPAL PO	0011 0000

In this system the RAM memory is mapped from location 100 (hex) to 1FF (hex), and location 700 (hex) is an "input" register whose contents can be set externally by switches, using the SC/MP "hold" facility.

The first four instructions load pointer registers P1 and P2 with, respectively, the addresses of the start of RAM and of the "input" register. At location 7 the contents of the "input" register are loaded into the accumulator. This represents the first data byte to be stored in RAM. At location 9, this is stored and the contents of pointer register P1 incremented. At location 11 a further data byte is input. This should be set as follows:

00(hex) = more data to be loaded

FF(hex) = execute the program justinput

This input byte is then exchanged with PO, the program counter, thus effecting a jump to either location 001 to load further information into RAM, or to location 100, the start of RAM, to execute the program just loaded.

The circuit to implement this program is shown. A 74154 decodes the low order four bits of the address to sixteen word lines. On those words where a 1 bit is required in a given location, the word line

is wired to the input of an appropriate NAND gate. The outputs of the eight NAND gates are taken to the inputs of a DM81LS95 tri-state buffer. This is gated by the SC/MP Read Data Strobe, NRDS, and a "select" input which corresponds to the "chip select" of a conventional ROM or RAM. Fortuitously, bits 4 and 5 and bits 6 and 7 of this program are identical and can thus share the same NAND gates, although this economy will cause a considerable loss of flexibility should it be necessary to alter the program. This is a simple matter of rewiring the NAND inputs.

Thus a small ROM can be constructed using standard TTL for around five pounds. For large ROMs the method is uneconomic, but for programs similar to the above it is cost-effective.

> J. E. Geary, Sunningwell, Oxon.

#### EUROPES FASTEST SELLING ONE BOARD COMPUTER -SAMPLE TAPE JUST CHECK THE SPEC'S. AS SEEN IN WITH EXTENDED MACHINE CODE MONITOR P.E. AUGUST, SEPTEMBER pukit ukioi AND DISSASSEMBLER **OCTOBER 1979** INCLUDED FREE COST SUPERBOARD IN KIT FO The Compukit UK101 has everything a one board 'superboard' should have. • Uses ultra-powerful 6502 microprocessor. • 50Hz Frame refresh for steady clear picture (U.S.A. products with 60Hz frame refresh always results in jittery displays) • 48 chars by 16 lines — 1K memory mapped video system providing high speed access to screen display enabling animated games and graphs. • Extensive 256 character set which includes full upper and lower case alphanumerics. Greek symbols for mathematical constants and numerous graphic characters enabling you to form almost any shape you desire anywhere on the screen. • Video output and UHF Hichdrade modulator (8Mz everything a one board 'superboard' should have. Simple Soldering due to clear and consise instructions compiled by Dr. A.A. Berk, BSc.PhD NO EXTRAS NEEDED JUST HIT 'RETURN' AND GO. desire anywhere on the screen. Video output and UHF Highgrade modulator (8Mz Bandwidth) which connects direct to the aerial socket of your T.V. Channel 36 UHF. Fully stabilised 5V power supply including trans-tormer on board. Standard KANSAS city tape interface providing high reliability program storage — use on any standard domestic tape or cassette recorder. 4K user RAM expandable to 8K on board £49 extra. Build, understand, and program your own computer for only a small outlay. KIT ONLY £219 + VAT \* 4K user RAM expandable to on un used and extra extra. \* 40 line expansion interface socket on board for attachment of extender card containing 24K RAM and disk controller. (Ohio Scientific compatible). \* 6502 machine code accessible through powerful 2K machine code monitor on board. \* High quality thru plated P.C.B. with all I.C.'s mounted on sockets. \* Professional 52 Key keyboard in 3 colours — software polled meaning that all debouncing and key decoding done in software. including RF Modulator & Power supply. 22 Absolutely no extras. Available ready assembled and \*8K Microsoft Basic means conversion to and from Pet, Apple and Sorcerer easy. Many compatible programs already in print. SPECIAL CHARACTERS tested, ready to go for £269 + VAT © Erases line being typed, then provides carriage return, line feed. Erases last character typed. CR Carriage Return – must be at the end of each line. COMMANDS NULL FUNCTIONS NEW RUN CONT LIST NEW NULL HUN STATEMENTS CLEAR DATA DEF DIM END FOR GOTO GOSUB IF...GOTO IF...THEN INPUT LET NEXT ON...GOTO ON...GOSUB POKE REM RESTORE RETURN STOP CONT LIST ATN(X) PEEK(I) SQR(X) COS(X) POS(I) TAB(I) ABS(X) LOG(X) SPC(I) EXP(X) RND(X TAN(X) each line. Separates statements on a line. CONTROL/C Execution or printing of a list is interrupted at the end of a line. "BREAK IN LINE XXXX" is printed, in-dicating line number of next statement to be executed or printed. CONTROL/O No outputs occur until return made to command mode. If an Input state-ment is encountered, either another CONTROL/O is typed, or an error occurs. ? Equivalent to PRINT EBE(X) INT(X) SIN(X) SGN(X EXPRESSIONS USR(I) OPERATORS STRING FUNCTIONS ASC(X\$) RIGHT\$(X\$.I) LEFT\$(XS.I) CHR\$S(I) FRE(X\$) STR\$(X) VARIABLES A.B.C. ....Z and two letter variables The above can all be subscripted when used in an array String variables use above names plus \$.e.g.A\$ LEN(X\$) MID\$(X\$.1.J) VAL(X\$)

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Any documentation that you have for the program (source listing 2)

a) not necessary) 3) This coupon signed by you accepting the rules and conditions of the competition.

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Entries, including documentation, must be printed by computer or typed double spaced, with your name on every page.
 Send or bring your entries to the address shown below.
 Entries must be received by midnight on 29/2/80, any received

after this time are void.

Winners will be notified by post before 31/3/80.

4) You warrant by your signature that all programs and documentation material included is entirely your own creation, and that no rights to it have been given or sold to any other party, and you agree to allow COMPUKIT LTD. to use, publish, distribute, modify, and edit it as it sees fit.

All entries become the property of COMPUKIT LTD. No entries will an entries become the property of Composite LD. No entries will be returned nor any questions answered regarding individual entries.
 Judging will be by a selected panel chosen by, and including representatives of COMPUKIT LTD. Judges may assign programs to any of the categories as they see fit. Decision of the judges is final.
 Employees of COMPUKIT LTD, its dealers, distributors, advertising agencies and media are not eligible to enter.

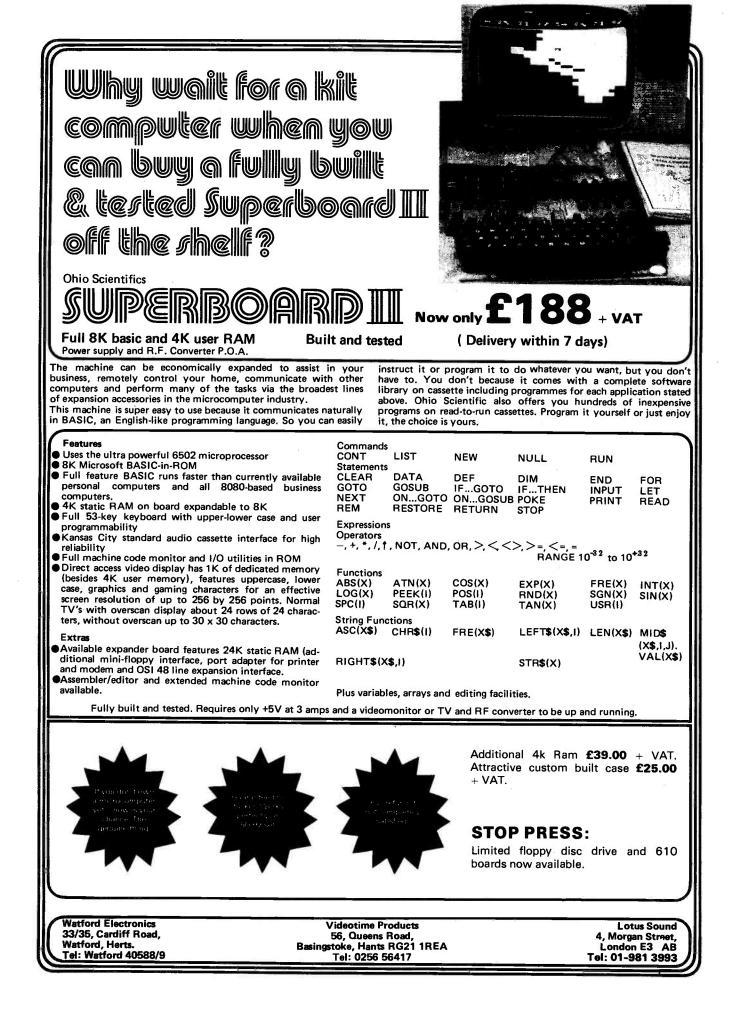
Name.

Address\_

I agree to abide by the above mentioned rules

Signature







# **RECORD FOR RUSSIA**

This is the eleventh month of the year and it is fitting that what must be one of the most exciting years in space history should be recorded as such. On the threshold of the Shuttle era, where the techniques of the hardware have been undertaken by the United States with co-operation from space agencies round the world, the other side of the interface, mankind, has been developed by the Soviet Union. They turned their attention to the study of the biological problems of survival in space.

The longest stay in space and weightless conditions was concluded in August by Soviet cosmonauts Vladimir Lyakhov and Valeri Ryumin. They had been 175 days in space proving that this is also the province of mankind. The record of this year alone is unique for there were many misgivings, some are still vociferously apparent, yet once again the direct approach to a solution has proved the point.

#### **MAN-MACHINE INTERFACE**

In some quarters a great play is made about the so-called difficulties on return to gravity. It is right that these matters should be thoroughly investigated. They have been, and it is clear that provided the exercises prescribed by the medical experts are followed no harm results. Of course in these early stages it is necessary for biological measurements to take place as soon as cosmonauts return. Therefore the maximum information must come from allowing the cosmonauts to land in the 'heavy end'. The speed of their recovery is quite amazing when it is remembered that after several weeks in bed some considerable difficulties are experienced by ordinary people on Earth when they try to walk. Other biological problems have had much special attention in those countries interested. In the United States all the data is available. The Soviet Union has been able to supply the men required. So the

space frontiers are making the new world and it is gratifying that all the nations are cooperating in these activities.

The special attention that Russia has given to the testing of facilites and the direct effect of the man-machine interface has resulted in a major contribution to the space age. The other cosmonauts who showed progressive extensions of time in space have all contributed. The immediately past record holders were preceded by two other Russians, Vladimir Kovalenko and Alexander Ivanchenkov. They too carried out tasks with the ferries as well as the special activities with the Kristall furnace and the Splav (alloy) electrical smelting installation.

## CRYSTALS

Salyut-6 space station saw the active investigation of crystals synthesized from elements of the third and fifth groups of the periodic table such as gallium arsenide and indium antimonide.

Of special interest was the production of crystals of cadmium and mercury tellurides. This particular crystal is the basis of a thermovisor. This is an infra-red device which can yield valuable information on the internal condition of the human body. It is indispensible for certain medical specialists.

Experiments in melting extremely pure optical glass were very successful. Zero gravity is essential for the production of high quality crystals. The natural vacuum of space will no doubt enable crystals of the second generation to exceed the present 100,000 elements per square centimetre. Indeed it is already being forecast that by the late 1980's a million elements will be possible. This again will reduce the size of equipment.

# **CIRCUMTERRESTRIAL SPACE**

There is no doubt that the feeling is growing that space exploration is associated with the application to the use of circumterrestrial space. It is to this end that the Soviet Union has spent so much time with the Salyut-6. The weight of this station is 19 tons. Its length is 15 metres. With two docked cargo ships it grows to 30 metres and 32 tons. The building up of stations by the simple process of joining up successive units, each a vehicle in its own right, seems to the Russians to be an efficient and safe way of dealing with the tasks of the future.

During the two years that the space station has been in orbit much work has been done. One interesting point that emerged from the working conditions in weightlessness was that as time went on the cosmonauts increased their efficiency in performing their allotted tasks. After the return of the last two cosmonauts the station continues orbiting automatically. During the period of its activity seven freight transport ships have made the journey to and from the Salyut-6.

Lyakhov and Ryumin began their record breaking trip in a Soyuz-32 spaceship on February 25 this year. On the 26 of February they commenced work aboard the Salyut-6. Materials and equipment were brought up by Progress-5, Progress-6 and Progress-7 ships. In addition the unmanned Soyuz-34 brought materials and equipment to the station. On June 13th the Soyuz-32 which brought the crew to the station returned with records and the two cosmonauts Kovalenko and Ivanchenkov.

#### **TELESCOPES**

The freight ship Progress-7 had brought up the radio telescope KRT-10. This was assembled in the intermediate chamber of the space station. Progress-7 was undocked and moved away. It was planned to use the Progress-7 as an observation point so that flight control could observe and control the telescope. The telescope was then moved out into position and the 10 metre parabola opened out. As it happened the unit did not quite get clear and the last task of Lyakhov and Ryumin before returning to earth was to execute a space walk to correct the fault.

The telescope was used in conjunction with the new 70 metre parabola at the long range radio communication centre in the Crimea. The distance between the two telescopes, one on Earth and the other in orbit, forming an interferometer. The base line was varied by the movement of the space station unit so that it was possible for this to range from 400km apart to 10,000km during the synchronous radio sessions. The effective aperture was the equivalent of a telescope the size of the Earth itself.

This opens up the possibilities for very large telescopes in space. A 10 metre parabola on Earth would weigh several tons but the space situated units would be a small fraction of this. It is therefore being planned by Russia to set up telescopes of up to 200 metres in diameter. A series of these will first be assembled in low earth orbit by a small team and then taken to a solar orbit. The total size of each unit would be from one to ten kilometres across. It would be possible in one combination to have one unit in near Earth orbit and the other at say Saturn. This would be a distance of about 1,500km.

This would have tremendous resolving power and might well be the means of detecting as yet unknown sources of energy and even perhaps discovering whether there were any planets round stars which might have civilisations. Also it would make it possible to set up a three dimensional picture of the universe directly.

#### **THREE FOR ONE**

Comsat are seeking to reduce the number of antennae in use for satellite communications. The new proposal called the torus antenna will enable three satellites to be in use with one antenna station. Normally there has to be a separate antenna for each satellite, each a parabola focussed at a particular point. In the new proposal, provided the satellites are grouped to a band not more than 30 degrees apart from each other it takes the form of a line focus. The reflector appears almost flat but is in fact shaped. It looks very much like three parallel linear parabolic channels. Within the 30 degree requirements three satellites can be interrogated with one station. The economics are sound for the station costs only 1.1 million dollars against 0.8 million dollars each for the single version.



# Fair adjudication for quiz contests

THIS article describes a monitor set which can be used by a referee or quizmaster to adjudicate fairly the result of a contest between individuals or teams and as such should prove popular in clubs or fund raising activities such as charity functions

Each team is provided with a button or buttons to press when an answer to a question is to be submitted. The first to reply actuates a lamp and buzzer simultaneously alerting the referee to the station answering and disabling all other contestants' units.

A competition state of readiness is resumed by the referee pressing his button, after adjudication, when all units revert to their stand-by state in readiness for the next question or throwing open the question to the other contestants in the event of a wrong answer.

This system was designed for three competitors or teams; however, there is no reason why it cannot be extended to as many contestants as required.

# CIRCUIT

In the off state the anodes of the three thyristors are at a positive potential biasing off D3 to D8. When one of the contestants' buttons is pressed it turns on the respective thyristor dropping its anode voltage to around zero volts; this in turn forward biases the other thyristors. The question master then notes which buzzer is sounding and cancels it by pressing his button removing the voltage from the circuit thus reducing the current through the thyristor below its holding level turning it off.

The type of thyristor used is not critical and any type should function perfectly as any variation in gate current is adjusted by the three presets to suit the manufacturer's data.

To adjust these presets connect an ammeter across the press switch contacts and adjust the wipers to get the right gate current (200mA on the thyristor specified). Do not adjust for gate voltage as this can be very misleading.

If triggering should become a problem use OA47s as these have a lower forward voltage drop although they are more expensive.

The circuit around TR1 forms a simple voltage regulator with the base held at the Zener voltage thus holding the collector of TR1 at the Zener voltage less the forward voltage drop of the transistor junction, approximately 700mV.

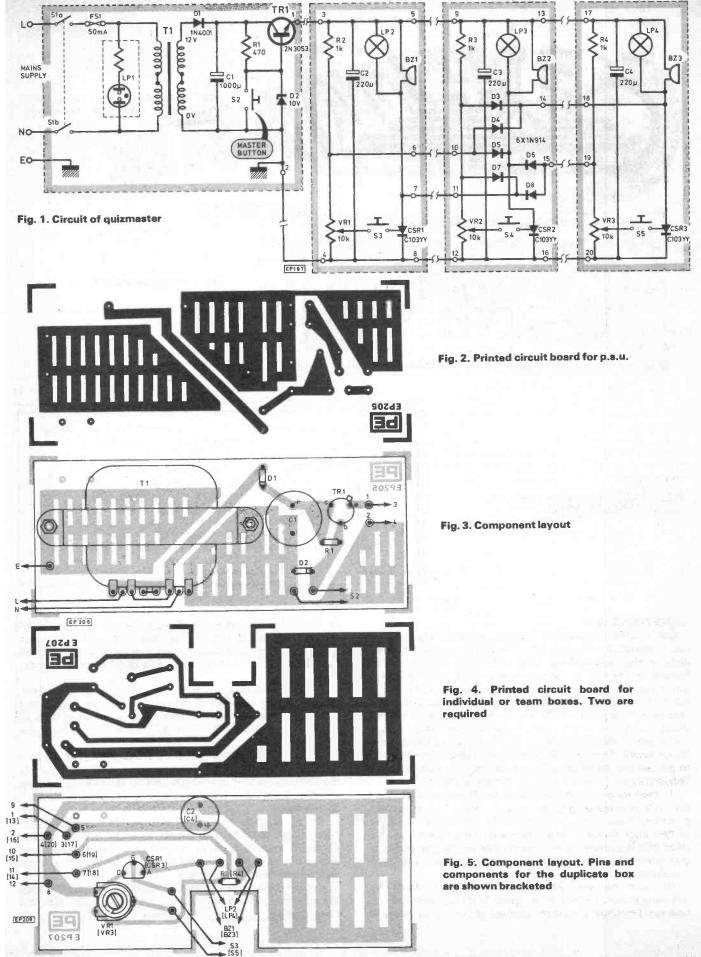
The quiz-master's button shorts out the Zener diode, grounding the base of TR1, effectively removing all the voltage from the output. The Zener voltage is not critical and may be any voltage between 7-15V although the lights will be brighter and buzzers will be louder if the Zener voltage is towards the upper limit.

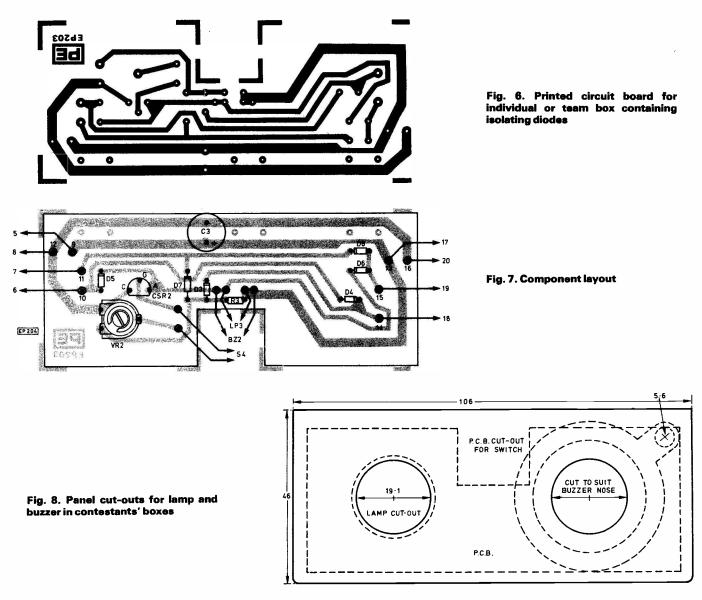
The regulator circuit may be discarded if a press to open push switch is available or even a toggle switch, but if this is done the output to the thyristors will not be stabilised and will rise to something like 22V causing the bulbs to have a shortened life and making it necessary to have higher working voltage capacitors.

Also the lamps may be dispensed with but if this is done the thyristors will not latch as the buzzers take an intermittent current, so some other load will have to be provided to keep the holding current above the threshold level.

Diodes D3 to D8 are needed to stop interaction between the thyristors. It will be noticed that these are all mounted in the centre enclosure instead of their respective boxes. Wiring up in this way enables the use of four core cable, otherwise six core cable would be necessary (Fig. 1).

COMPON	ENTS
Betletere	
Resistors	170
R1 R2-R4	470 1k (3 off)
All W carbor	
Capacitors	
C1 C2-C4	1,000µ elect 25V 220µ elect 16V (3 off)
62-64	220µ elect 10v (3 00)
Potentiomete	and the second
VR1-VR3	10k (3 off)
Semiconduct	Ors
D1	1N4001
D2	BZY88 10V 400mW
D3-D8 CSR1-CSR3	1N914 (6 off) C103YY (6 off) (R.S. 261–873) (3 off)
TR1	2N3053
uzzers	
BZ1-BZ3	12V single tone (R.S. 248-808) (3 off)
Viscellaneou	
the second s	off toggle, S2-S5 push button switches, 4
boxes Astros	Grey (AST578)-West Hyde, 40 feet four
core cable. T	ransformer-6-0-6V 0.5A mains (R.S.
196–296), La Mains neon, F	mpholder—22mm dia. Bulbs—12V 2-2W,
wanto neon, n	





#### EG 203

# CONSTRUCTION

Construction is perfectly straight forward. The printed circuit boards are fitted upright in the slots moulded into the ends of the boxes. These slots are tapered down to the bottom of the box by approximately 1mm each side and seeing as the printed circuit board is also used for strain relief on the cable, some care is needed in fitting them to ensure that they are a fairly firm fit. Four core cable passes through the hole in the side of the box and then through two holes in the printed circuit board, supplying strain relief of the soldered joints. DIN plugs and sockets could be used to join up the separate units but as the cost was of prime importance on the prototypes, these were not used.

If when fitting the buzzers the hole through which they protrude is made a tight fit, the only other means needed to support them is double sided sticky tape top and bottom of the large diameter end, this being held fast by the lid when this is screwed down. Failing this a nylon nut and bolt and spacer must be used to bolt the buzzer to the printed circuit board.

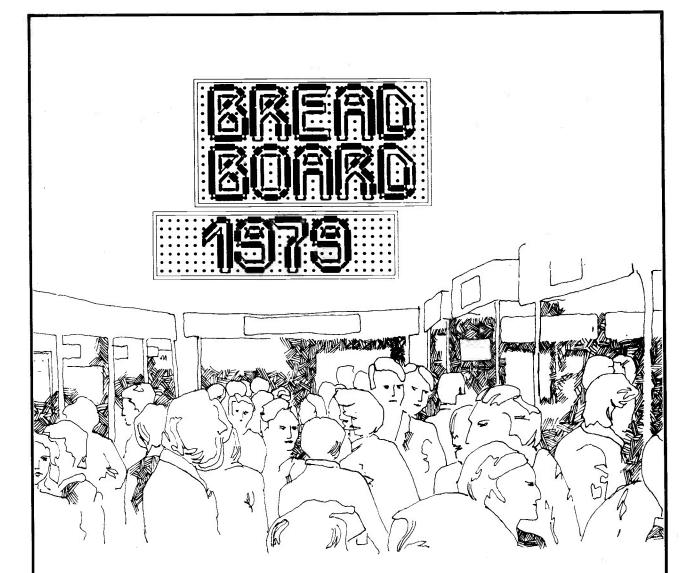
To make the holes for the panel light and buzzer the following procedure may be adopted. Mark the centre of the hole to be made with a punch, then using a pair of compasses or dividers mark the outer diameter of the hole, then drill out the centre as big as you can, filing out the plastic carefully to the outer diameter mark using, if possible, a half round file to finish off with, as this gives a much rounder hole.

A word here about marks and scratches on the boxes. These may be cleaned off (if they are not too deep) using the type of cleaner that is advertised as cleaning without scratching, such as Jiff, but many other brands of the same type may be used.

The wires joining the boxes were brought out of the side and front of the boxes and are thus kept out of the way of the contestants and quizmaster so that their hands can rest comfortably on the tables while they are waiting to push their buttons.

The West Hyde boxes specified can be purchased with plastic or metal lids. The plastic type are needed for this application or the buzzers will not fit in the boxes. These enclosures are used because they have a smooth bottom with no moulding marks visible.

Rubber stick-on feet were also used on the boxes to stop the scratching of the polished table tops; they also hide the fixing screws.  $\bigstar$ 



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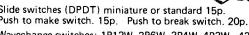
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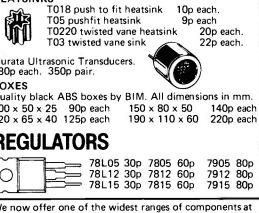


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W ITH the development of simple chemistry processes for colour film printing, more and more amateurs are trying their hand at producing their own colour prints in the home darkroom.

Once you get into colour processing you quickly realise that the good old days where the enlarger button was held down for a count of ten are gone, due to the higher timing accuracy required.

This project describes a simple enlarger timer, the accuracy of which is not affected by fluctuations in the mains voltage, and which fulfils the need for simple operation, as of course the unit is used in total darkness. No indicators or displays have been incorporated as even the red light from such displays is not "safe" for use with colour photography.

#### RANGE

The range of the unit is from 1 to 99 seconds in one second steps but if required the timer can be modified to give a second range of 0.1 to 9.9 seconds in 0.1 second steps.

# **CIRCUIT DESCRIPTION**

The circuit diagram of the Darkroom Timer is shown in Fig. 1. The power supply uses a standard 7805 regulator

to provide +5V. It also provides a 9V a.c. line which is divided by R1 and R2 and clipped by the Zener diode D2 to provide an approximately square 50Hz input to IC2 (pin 1).

IC2 and IC3 are connected in cascade to divide the 50Hz input by 50 to produce a 1Hz standard timing pulse.

This 1Hz pulse is now fed to the input of the b.c.d. counters IC4 and IC5 which will count up the pulses from 0 to 9.

As the counters are cascaded the total count available is 99. The b.c.d. outputs from these counters are fed to the 4 to 10 line decoders IC6 and IC7. The outputs of these decoders will remain normally high and an output will go low when the particular code for that output is presented to the i.c.

Thus by using S3 and S4 any number from 0 to 99 can be selected by feeding one of the outputs from the decoders IC6 and IC7 to a NOR gate IC8a, i.e. if the number 56 is selected S3 will look at the 6 output of IC6 and S4 will look at the 5 output of IC7, thus at the number 56 the output from S3 and S4 will be low causing the output of the NOR gate to go high.

The timing sequence is started by closing S2 which resets the counters IC4 and IC5 to zero and also sets the latch formed by the two NOR gates IC8b and IC8c. Once the

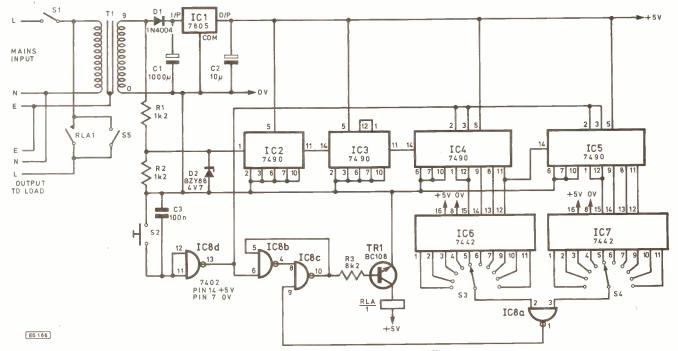
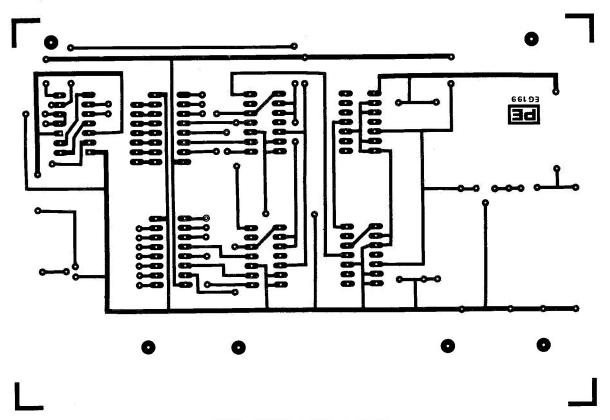


Fig. 1. Circuit diagram of the Darkroom Timer







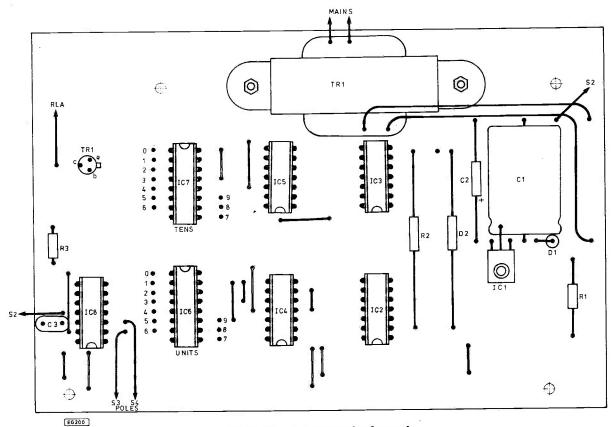
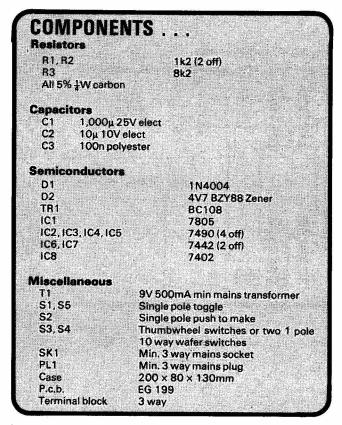
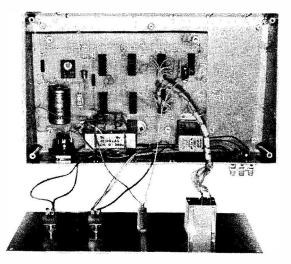


Fig. 3. Component overlay for p.c.b.



latch has been set the output turns on TR1 which operates the relay RLA switching on the enlarger lamp.

When the set count is reached the output of IC8a will go high, resetting the latch and switching off the enlarger lamp.



Internal view of the Darkroom Timer

# CONSTRUCTION

The prototype was constructed on a printed circuit board the design of which is shown in Fig. 2 with the component layout shown in Fig. 3. After the p.c.b. has been soldered and checked the board should be mounted into the case and the switches and sockets fitted.

Thumbwheel switches were used for the time selector as they give a quick and easy method of selecting the exposure period and provide an indication of the set time. Alternatively, standard rotary wafer switches could be used to reduce the cost of the unit. The relay used had a 6V 700 ohm coil but any relay with a coil voltage of about 4 to 6 volts and a coil resistance of over 200 ohms may be used, provided that the contacts are rated for the load.

# CASE

The unit was housed in a plastic case with an aluminium front panel measuring about  $200 \times 80 \times 130$ mm with all the controls mounted on the front panel and a mains input socket and a three way terminal block for the timer output mounted on the back of the case.

# USE

To use the timer once it has been connected up, all that is necessary is to set up the desired time for exposure on the thumbwheel switch and press the "expose" button. The enlarger will then switch on and after the time set has elapsed, switch off.

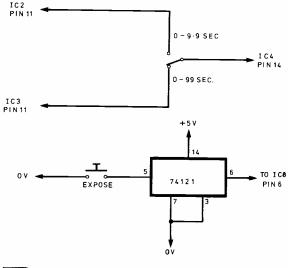
Resetting is not necessary as the timer is reset when the "expose" button is pressed.

If it is desired to switch on the timer for focusing purposes a "focus" switch (S5) has been provided which by-passes the timer causing the enlarger lamp to stay on indefinitely.

#### **ADDING A RANGE**

A second range of 0.1 to 9.9 seconds in 0.1 second steps could be added by making the modifications shown in Fig. 4.

First, a single pole switch (changeover) is added to facilitate range switching. This switch will select either the output of IC2 (pin 11) or the output of IC3 (pin 11) and switch it to the input of IC4 (pin 14), thus feeding the counter with either 1Hz or 10Hz timing pulses.



EG 20 1

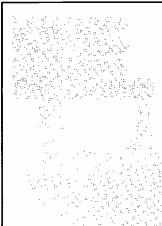
Fig. 4. Modification for adding a second range

Next, a monostable has to be added in the start circuit to give a narrow pulse when the "expose" switch is closed.

The reason for this is that when the "expose" switch is operated the latch sets immediately, switching on the enlarger lamp, but the counters do not start to count until the button has been released. Thus if the start switch is held down for 0.3 sec, there would be a timing error of 0.3 sec.

It is of course necessary to break the existing connections between pin 11 on IC3 and pin 14 on IC4.

A suitable monostable circuit is shown using a 74121 integrated circuit.





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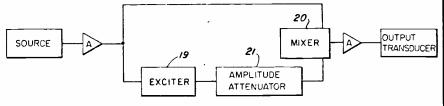
Price 95p each

# THE APHEX SOUND

British patent application 10848/77 in the name of Curt Knoppel was filed in the UK in 1977 under the old patent laws and will thus remain secret until accepted, granted and published by the British Patent Office. This will probably not be for a year or so.

The corresponding USA patent 4 150 253 was, however, recently published in the joint names of Curt Knoppel and Inter Technology Exchange Ltd., both of Los Angeles. This patent will be very interesting to anyone who has puzzled over the circuitry which is contained in the Aphex System as used by pop groups to make instrumental sounds, and the human voice, stand out and seem louder without any actual change in amplitude level.

"The formula by which the Aphex device selectively processes the audio signal has been arrived at after considerable research into the mechanisms of the ear", proclaim the Aphex ads. But so far there has been



little hard fact available on how Aphex actually works. The US patent includes block schematics and circuit diagrams with component values, for both valve and transistor designs.

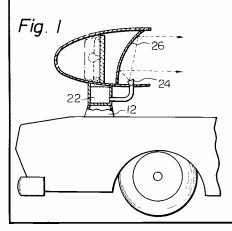
The block diagram shows the source signal amplified and split into two channels. The split signal passes unaffected through one channel to a mixer 20 and in the other channel is fed to an exciter 19 and attenuator 21. The output signal is thus a controllable combination of excited and unexcited signal.

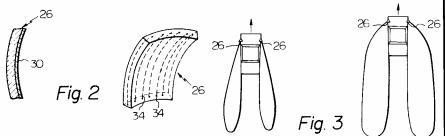
Despite the advertisement claim quoted above, the patent wording admits that "it cannot be said with absolute certainty which specific elements in the exciter circuit 19 perform which function". But empirical tests and the comparison of input and output waveforms have shown that the exciter functions as a high pass filter, and generates low order, odd and even, phase shifted and amplitude dependent harmonics of the frequencies passed. A linear frequency dependent phase shift of about 360° is produced over the audio bandwidth with the point of zero phase shift at around 2kHz. In many respects therefore, the Aphex circuit is controllably producing exactly those audio effects which circuit designers normally strive to eradicate.

(Although the British Patent Office does not publish copies of US patent specifications, the foreign branch of the Patents Library attached to the Chancery Lane Patent Office holds a copy of all US specifications and will sell a photocopy at reasonable cost.)

# **REAR-VIEW RADAR**

Recent UK patent application 2 004 418 (filed under the new laws) discloses ideas from the Nissan Motor Company of Japan for equipping motor cars with radar sensors to warn the driver of an impending collision. The aim is to offer sensing of danger from either behind or the side or both, for instance when a car is changing lane on a motorway.





The optimum position for providing rear and side radar lookout is that already occupied by the rear-view wing mirrors, so Nissan propose that the mirrors should be combined with micro-wave reflectors operating in the range 10GHz to 80GHz.

As shown in Fig. 1 a conventional microwave transmitter unit 22, including an oscillator such as a Gunn diode and modulator, is installed in the wing mirror post 12 and a wave guide connected to a feeder horn 24. This horn sits at the focal point of parabolic reflector 26. The reflector 26 is positioned in front of an ordinary wing mirror but the mirror is visible to the motorist because the parabolic reflector is lighttransmissive. Fig. 2 shows constructions for a light transmissive micro-wave reflector 26. One side of a curved plate of glass can be coated with a thin (few microns thick) film 30 of metal or of transparent and conductive oxide such as tin oxide. Coating is by vacuum evaporation. Alternatively a matrix of fine metal wires 34 are embedded in a curved plate of transparent glass or plastics.

Fig. 3 shows how the resultant radar lobes cover both the rear and side of the car for lane changing. Presumably Nissan intend incorporating an alarm system which will sound or light up if the driver attempts to change lanes when another vehicle is inside the radar lobes.



# selection from our postbag

Readers requiring a reply to any letter must include a stamped addressed envelope. Opinions expressed in Readout are not necessarily endorsed by the publishers of Practical Electronics.

# G3FYO

Sir-I would like to take this opportunity of writing to you to give you details of the recently reformed "Pontefract & District Radio Society".

The club was re-formed in May and the Home Office have re-issued the callsign G3FYQ. The meetings are held fortnightly at Knottingley Town Hall starting at 7.30 pm.

The programme of future meetings is :-Oct. 18th. Slow Scan Television by G41BN/G4FBA.

Nov. 1st. Film Night.

Nov. 15th. Oscar Satellite Operating by Jack Ward, G4JJ.

Nov. 29th. David Tong, of Datong Electronics on the Up/Down Convertor.

Dec. 13th. Social Evening-venue to be announced.

Further details can be obtained from address

below or telephone Pontefract 71071. All new members will be most welcome.

Phil N. Butterfield, G4AAQ, R.S.G.B. Area Representative. Club Chairman, 43, Lynwood Crescent, Pontefract WF8 3QT, West Yorkshire.

# **VLF** Signals

Sir-I was very interested to read the article 'VLF Signals and the Magnetosphere' by C. R. Francis in your September, 1979 edition. I have been interested in this particular part of the electromagnetic spectrum for some time now, as a project with my sixth formers and we have amassed quite a lot of practical experience, much of the time using simple

receiving equipment.

We would be very pleased if, through your columns, we could ask for other schools or individuals interested in VLF work and especially in Whistlers, to write to me at the address below, preferably enclosing a stamped addressed envelope. We could then share our knowledge, and even better, make simultaneous recordings of VLF phenomena. There is considerable scientific value in such co-operative work. Such co-operators need not have any prior experience.

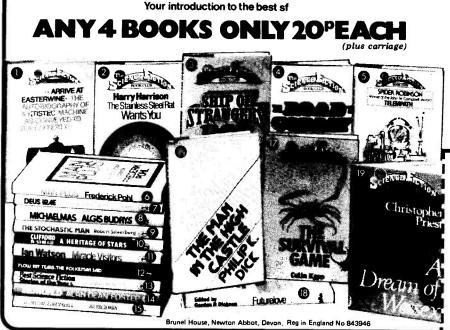
You may be interested to know that we at Mayfield are supported in our work by the Royal Society, who have special arrangements for giving financial grants to schools doing research, and such help would be considered very favourably for any schools willing to join our investigations.

> H. James, Head of Physics, Mayfield School, Mayfield Road, North End, Portsmouth, PO2 0RH.

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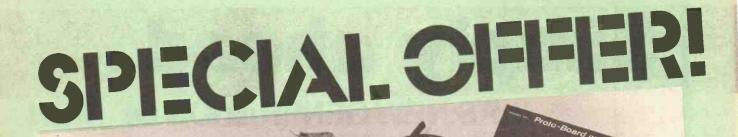
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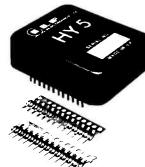
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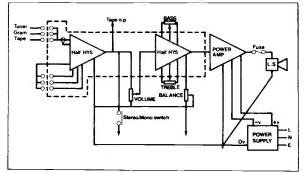
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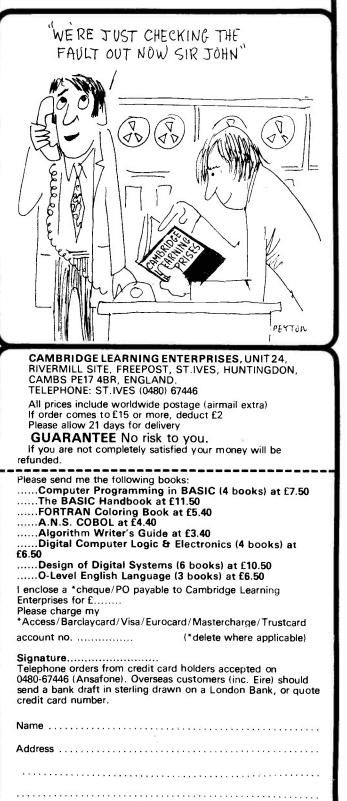
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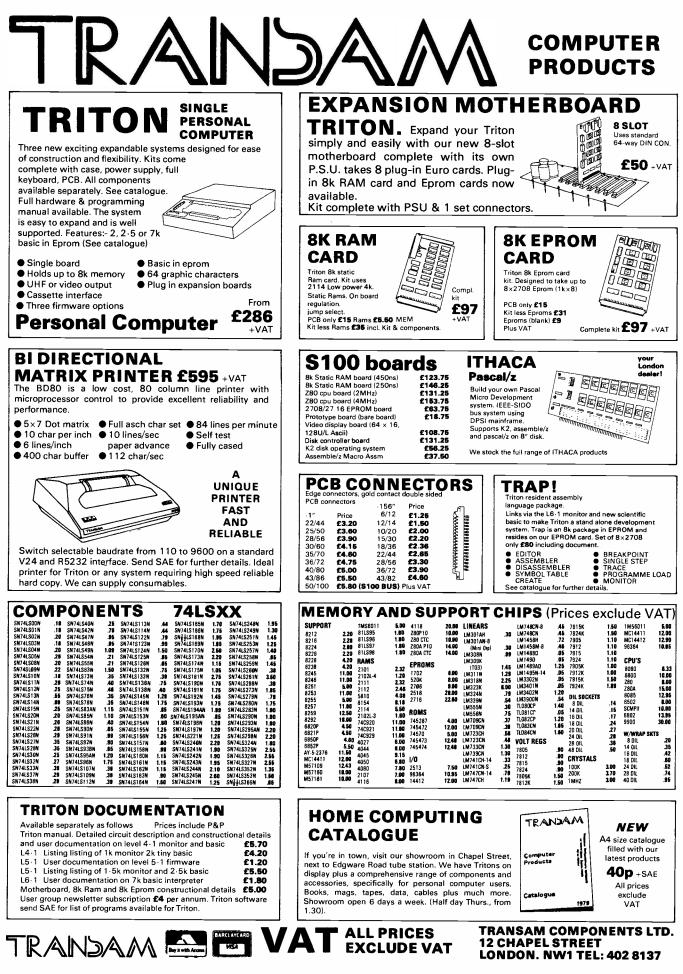
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X02 : X03 - ACTIVE CROSSOVERS

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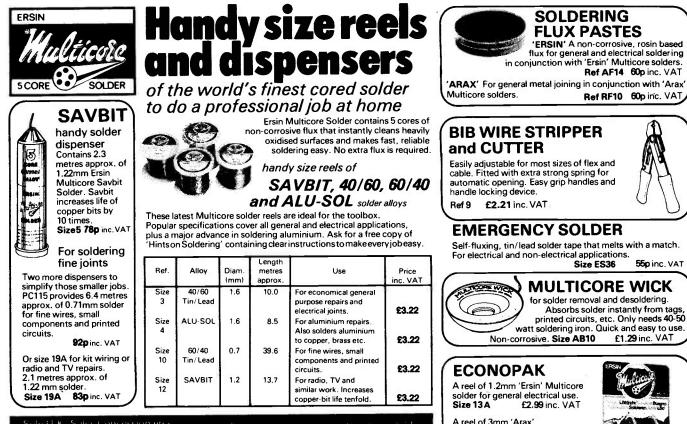
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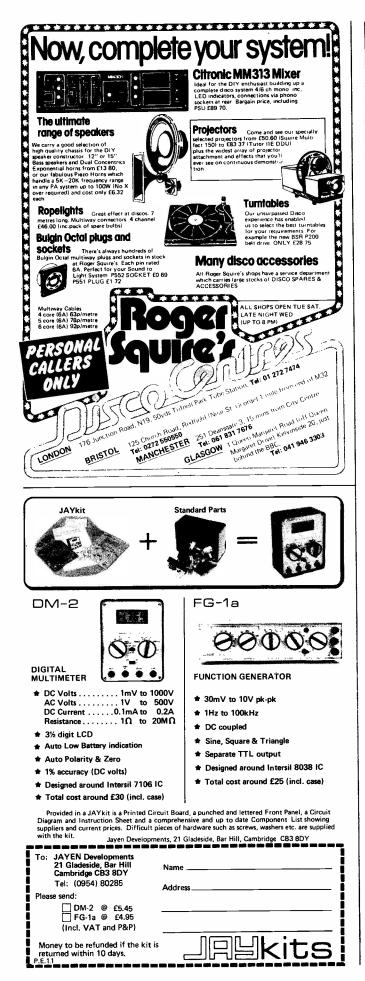
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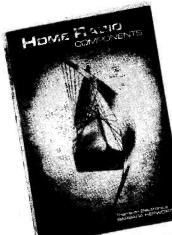
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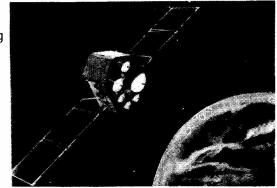
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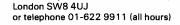
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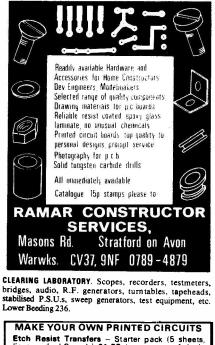
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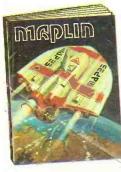
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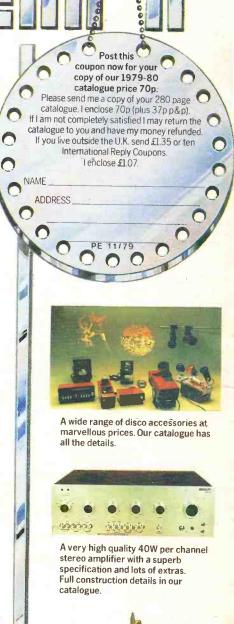
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