PRACTICAL

# ELECTRONICS

AUGUST 1978

45p

# DIGITAL THERMOMETER

DIGITAL THERMOMETER

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MICROPROCESSOR KIT REVIEW



# PRACTICAL

# **ELECTRONICS**

VOLUME 14 No. 12 AUGUST 1978

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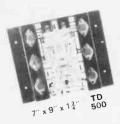
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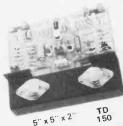
Featuring
Ejectronic Short Open & Thermal Overload Protection.

Brief Spec Input Sensitivity 0.775.v. R.M.S. (O.D.B.) at 25 K Ohms Frequency Response 20 Hz-20 KHz

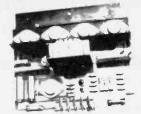
Hum & Noise - 100 dB Relative full output

T.H.D. at full powr 0.1% T.D. 500 300W into 2 Ohms 220W into 4 Ohms Size 7" x 9" x 13" 140W into 8 Ohms Power supply P.S. 300 T.D. 150 150W into 4 Ohms £45.00 £28 50 £26.25 5" x 5" x 2" 100W into 8 Ohms Power supply P.S. 150 T.D. 150. 60 Version 60W into 8 Ohms 5" x 5" x 2" 40W into 15 Ohms. Power supplies P.S. 60 £17.75 £15.25

Note P.S. 300 will drive 2 T.D. 150 amplifiers All output ratings are R.M.S. continuous sine wave output



# **AMPLIFIER MODULES**



SPEC. INPUT SENSITIVITY 60 mV for full output Frequency response 20 Hz-20 KHz HUM & NOISE - 70 d8

TL60 5 = 5 × 3in

60 watt R M S continuous sine wave output
 2 R C.A. 110 watt 15 amp transistors

TL100 5 × 5 × 3 in

 100 watt R.M.S. continuous sine wave output
 2 R.C.A. 150 watt 15 amp transistors £20.75

TP125 7 × 61/2 × 3in

125 wait R.M.S. continuous sine wave output
4 R C A 150 wait 15 amp output transistors

£25.75

£18.25

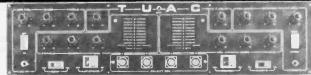
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6p; 220, 250 13p, 470, 640, 25p; 1000, 27p; 1500 30p: 2200 41p; 3300 52p; 4700 54p; 140, 40, 47, 68 7p; 100, 125 8p; 330, 470 16p; 1000, 1500 20p; 2200 34p; 10V: 4, 106 6p; 640 10p; 1000 14p.
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31p				24p	22p	SPDT c/over DPDT 6 Tag	60p 65p 85p
peaker	PLUGS	SOCKETS	In Line				
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(TV)	14p	14p	14p	SP chang ROCKE	eover centre off (black) on/off 1	0A 250V	30p 23p
eq urs	9p 12p	5p single 8p double 10p 3-way	15p	ROTARY	en on: 3A 240V ': (ADJUSTABLE	STOP) 1 pole/2-	52p 12 41p
4mm	10p	12p	-	ROTARY	: Mains 250V A	, 4 Amp	45p
2mm 1mm 3mm	10p 8p 9p	10p 8p 9p	=	8 pin 101	p: 14 pin 12p: 1	6 pin <b>13p</b> : 18 pi	n <b>20p;</b> n <b>55p</b> .
	31p  Deaker udio  TVI  urs ed  4mm 1mm	31p 18p PLUGS Deaker urs 13p TTVI 14p urs ed 12p 4mm 10p 2mm 10p 1mm 8p	31 p   18p   15	31p 18p 15p  PLUGS SOCKETS In Line peaker 13p 8p 20p  TVI 14p 14p 14p  TVI 14p 15p single 8p double 8d 12p 10p 3-way 10p 10p 12p 10p 10p 10p 10p 10p 10p 10p 10p 10p 10	31p   18p   15p   24p	31p 18p 15p 24p 22p  PLUGS SOCKETS In Line  20p SWITCHES ★ Miniature  13p 8p 20p Push to Make 15p ROCKER (white) 10A 25f  SP changeover centre off ROCKER (black) or/off 1  12p 15p single 8p double 15p ROCKER: (black) or/off 1  12p 10p 3-way way 2p/2-6W 3p/2-4W 4p ROTARY: (ADJUSTABLE 4p ROTARY: (ADJUSTABLE 4p ROTARY: (ADJUSTABLE 4p ROTARY: Mains 250 Ap ROTARY: (Dough 25p Ap ROTARY: Mains 250 Ap ROTARY: Mains 250 Ap ROTARY: (Dough 25p Ap ROTARY: Mains 250 Ap ROTARY: M	31p   18p   15p   24p   22p   SPDT clover OPD 1 6 Tag

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32 55 31 20 28 19 25 30	4513 4514 4515 4516 4516 4517 LINEA 702 709C 1 741C* 747C 748C 747C 748C 747C 748C 747C 748C 747C 748C 747C 748C 747C 748C 747C 748C 749C 749C 749C 749C 749C 749C 749C 749
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	210 29 60 325 410 410 185 180 157 450

	AC
SWITCHES* TOGGLE 2A 250V SPST 28p DPDT 38p 4 pole on/off 54p SUB-MIN TOGGLE SP changeover 59p SPST on/off 54p DPDT 6 tags 70p DPDT Centre off 79p DPDT Biased 115p SLIDE 2500V:	AC AC AC AC AC AC AC AC AC AC
1A DPDT 14p	AC
1A DP c/over 15p 2A DPDT 13p	AC AC
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SPST on/off SPDT c/over DPDT 6 Tag 85p	AC AC AC
lon-Locking	AD
Push to Break 25p	AD

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AD149
AD161#
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AF115#
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AF124#
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AF1

BC1078★ BC1088★ BC1088★ BC1098★ BC1099★ BC109B★ BC109C★ BC113 BC113 BC115 BC116 BC117 BC118

BC118 BC134 BC135 BC135 BC135 BC142 BC142 BC143 BC143 BC153 BC154 BC158 BC159 BC167 BC166 BC167 BC168 BC167 BC168 BC168

2N3707 10
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2N3711 16
2N3711 16
2N3715 250
2N372 188
2N3819 22
2N3820 32
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AC107 AC125	0 - 30	BD131	0.51	QA5	0.75	1N4005	0 - 13	7410	0 - 20
AC126	0 - 25	BD132 *BD135	0-54	OA7 OA10	0 · 55 0 · 55	1N4006 1N4007	0 - 15	7412 7413	0 - 26
AC127 AC128	0 - 25	*BD136	0.36	OA47	0.14	1N4009	0 - 15	7416	0 - 40
AC141	0.20	*BD137	0 - 37	QA70	0 - 30	1N4148	0 - 07	7417	0 - 40
AC141K AC142	0.35	*BD138	0 -40	OA79	0 - 30	1N5400	0-14	7420	0 - 20
AC142	0.20	*BD139	0 - 43	OA81	0.30	1N5401	0 - 16	7422	0 · 25 0 · 35
AC142K	0.30	*BD140 BD144	2.00	OA85 OA90	0.30	1S44 1S920	0.08	7423 7425	0.35
AC176 AC187	0 - 25	BD181	1 - 38	OA91	0.08	15921	80 - 0	7427	0 - 35
AC188	0 - 25	BD182	1-48	OA95	0.08	2G301	1.00	7428	0 · 50
ACY17 ACY18 ACY19	0 - 65	BD237	0.80	OA200	0.10	2G302	1-00	7430	0 - 20
ACY18	0.65	BD238 BDX10	0-85	OA202 OA210	0 · 11 0 · 75	2G306 2N404	0.60	7432 7433	0.37
ACY19	0.65	BDX32	2.25	OA211	0.75	2N696	0 - 25	7437	0-42
ACY20	0.65	BDY20	1-42	OAZ200	0.65	2N697	0 - 16	7438	0 - 37
ACY21 ACY39	1.25	BDY60	0.75	OAZ201	0 - 65	2N698	0 - 30	7440	0 - 22
AD149	0.70	BF115 BF152	0 - 39	OAZ206	0.65	2N705	0.80	7441AN	0.92
AD161	0.75	BF152 BF153	0 25	OAZ207 OC16	0 · 65 1 · 25	2N706 2N708	0-12	7442 7447AN	0 · 78 1 · 20
AD162	0.75	BF154	0.25	0016	2-00	2N930	0 - 26	7450	0.20
AF106 AF114	0 - 45	BF159	0.35	OC20	2 - 50	2N1131	0 - 26	7451	0 - 20
AF115	0 - 25	BF:60	0 - 30	OC23	2.75	2N1132	0 - 26	7453	0 - 20
AF116	0 - 25	BF167	0 - 39	QC24	3 - 50	2N1302	0 · 37	7454	0 · 20
AF117	0 - 25	BF173 BF177	0 - 39	OC25	0.90	2N1303	0 - 37	7460 7470	0 · 20 0 · 35
AF139	0 · 40 1 · 50	BF178	0.45	OC26 OC28	2.00	2N1304 2N1305	0.45	7472	0 - 36
AF186 AF239	0 - 45	BF179	0.48	OC29	2.00	2N1306	0 - 50	7473	0.36
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AFZ12	2 - 75	BF181	0 - 45	OC35 OC36	1 - 50	2N1308	0 60	7475	0 - 59
ASY26	0 - 45	BF182 BF183	0.45	OC41 OC42	0 · 50 0 · 50	2N1309 2N1613	0 - 60	7476 7480	0.60
ASY27 ASZ15	0 · 50 1 · 25	BF184	0.39	OC43	1.50	2N1671	1.50	7482	0-85
ASZ16	1 - 25	BF184 BF185	0 - 37	00044	0 - 50	2N1893	0 - 33	7483	1.00
ASZ17	1 - 25	*BF194	0 · 12	OC45 OC71 OC72	0 - 50	2N2147	1 - 40	7484	1.00
ASZ20	0.75	*BF195	0.11	OC71	0 - 45	2N2148	1 · 65	7486	0 · 40 0 · 52
ASZ21	1 · 50 1 · 70	*BF196 *BF197	0-14		1.00	2N2218 2N2219	0.42	7490 7491AN	0.85
AU113 AUY10	1.70	BF200	0 - 32	OC74 OC75 OC76	0.75	2N2220	0.35	7492	0.60
BA145	0 - 15	*BF224	0 - 20	OC75	0 - 60	2N2221	0 - 22	7493	0.70
BA148	0 - 15	*BF244	0 - 35	OC76	0 - 50	2N2222	0 · 25	7494	0.80
BA154	0 - 10	BF257	0 - 37	OC77 OC81	1 - 20 0 - 75	2N2223	2·75 0·17	7495 7496	0.80
BA155	0-12	BF258 BF259	0-45	OC81Z	1.00	2N2368 2N2369A	0-21	7497	3 - 67
BA156 BAW62	0-13	*BF336	0 - 50	OC82	0 - 75	2N2484	0 - 21	74100	1 - 75
BAX13	0.07	*BF337	0.53	OC82 OC83	0 - 55	2N2646	0 - 50	74107	0 - 45
BAX16	0.07	*BF338	0 - 55	OC84	0.60	2N2904	0 - 35	74109	0.86
BC107	0 - 12	BFS21 BFS28	1 - 38	OC122 OC123	1 - 50	2N2905 2N2906	0.35	74110 74111	0 · 57 0 · 86
BC108	0 · 12 0 · 13	*BFS61	0 - 25	OC139	2 25	2N2907	0.21	74116	1 89
BC109 *BC113	0.15	*BFS98	0 - 25	OC140	1-95	*2N2924	0.15	74118	0.95
*BC114	0 - 18	BFW10	0.90	OC141	2 - 25	*2N2925	0-17	74119	2 - 00
*BC115 *BC116	0 - 19	BFW11	0.90	OC170	0.75 0.75	*2N2926	0.13	74120	1-10
*BC116	0 · 19	BFX84 BFX85	0-38	OC171	1-00	2N3053 2N3054	0 - 25	74121 74122	0 - 45
*BC117	0 - 22	BFX87	0 35	OC200 OC201 OC202	1.50	2N3055	0.65	74123	1.00
*BC118	0-18	BFX88	0 - 32	OC202	t-50	2N3440	0.60	74125	0.80
*BC125 *BC126	0 - 25	BFY50	0 - 26	OC203	1.75	2N3441	0.80	74126	0.80
*BC135	0 - 15	BFY51	0 - 26	00004	1 25	2N3442	1.20	74128	0.80
*BC136 *BC137	0 - 19	BFY52 BFY64	0 · 26	OC205 OC206 OC207 OCP71	1 - 75	2N3525 2N3614	1 - 20	74132 74136	0-80
*BC137	0 · 16 0 · 10		1 . 32	00200	1-25	*2N3702	0 - 15	74141	0 - 85
*BC147	0 - 10	BSX19	0 - 34	OCP71	1 - 25	*2N3703	0 - 15	74142	3 - 00
*BC148 *BC149	0 - 13	BSX20	0 - 34	ORP12	0.83	*2N3704	0 - 15	74143	3.00
*BC157	0.12	BSX21	0 · 32 1 · 25	•R2008B	2 - 25	*2N3705	0 - 15	74144	3-00 1-00
*BC158 *BC159	0.11	BT106 BTY79/400R		*R2009 *R2010B	2 - 25	*2N3706 *2N3707	0 · 14 0 · 18	74145 74147	2-45
*BC159	0 · 13		2 - 25	T1C44	0.36	*2N3708	0-14	74148	2.00
*BC167 *BC170 *BC171	0 - 16	*BU206	2 - 25	T1C226D	1 - 30	*2N3709	0.15	74150	1 - 75
*BC171	0 - 14		2 - 50	T1L209	0 - 25	*2N3710	0 - 14		0.90
*BC172 *BC173	0.13		0-45	*T1P29A *T1P30A	0 - 50	*2N3711 2N3771	0·15 1·60		2·00 0·90
*BC173	0 - 15		0.15	T1P31A	0.62	2N3772	1.70	74156	0.90
BC177 BC178	0 - 19	BZX61	0.20	T1P32A	0.75	2N3773	2 - 65	74157	0 - 90
BC179	0 - 20	Series		T1P33A	1.00	*2N3819	0 - 36	74159	2 - 50
*BC182	0 - 11	BZY88	0.13	T1P34A T1P41A	1 - 20	*2N3820 *2N3823	0 - 46		2 · 60 5 · 00
*BC183	0-11	Series CRS1/05	0 - 45	T1P41A	0-70	2N3823 2N3866	1-00		1.75
*BC184 *BC212	0 - 14		0.60	T1P2955	1-00	*2N3904	0 - 21		1 - 57
*BC213	0 - 14	CRS3/05	0-45	T1P3055	0 - 50	*2N3905	0 22	74175	1.00
*BC214	0 - 17	CRS3:40	0.75	*T1S43	0.35		0.22		1.10
*BC237 *BC238	0 - 17	CRS3.60	0 · 90 1 · 50	*ZS140	0 · 25 0 · 12	*2N4058 *2N4059	0 - 20		1 · 65 1 · 65
	0 - 12	GEX66 GEX541	1 - 75	*ZS170 *ZS178	0 - 12		0 - 20		1.65
BC301 BC303	0 - 60	GJ3M	0 - 75	*ZS271	0.22	*2N4061	0 - 17	74190	1 - 48
*BC307	0 - 20		0.75	*ZS278	0 - 56	*2N4062	0 - 18	74191	1 - 48
*BC308	0 - 18	-1404004	1 · 50 0 · 40	*ZTX107	0 - 11	*2N4124	0 17		1 - 25
*BC327	0 . 22		0 - 58	217100	0 · 10 0 · 12		0 - 17	74193 74194	1 - 25
*BC328	0 - 18		0.65	*ZTX109	0 - 12	*2N4288	0.25	74194	1-10
*BC337 *BC338	0 - 11	MJE371	0 - 81	*ZTX301	0-13	*2N4289	0 - 25	74196	1 - 20
BCY30	1 - 04	MJE520	0 - 65	*ZTX302	0 - 17	*2N5457	0 - 35	74197	1.00
BCY31	1 - 01	MJE521	0 · 75	*ZTX303	0 17	*2N5458 *2N5459	0 - 35		2 - 25
BCY32 BCY33	1.0		0.75	*7TX311	0 19		0 - 31		2 - 25
BCY33	0.9	*MPF102	0 - 30	*ZTX314	0 - 20		. , ,		
BCY34 BCY39	3.0	*MPF103	0 - 30	*ZTX500	0 - 13	1/1			
BCY40	1 - 2	5 MPF104	0 - 30		0 - 14			—low prof	
BCY42	0 - 3	SOLADE ADE	0 - 25	*ZTX502 *ZTX503	0 - 16	CIRCUITS	0 - 20		0 - 15
BCY43 BCY58	0 - 3	******	0 - 25		0 - 20		0 - 20	14 pin DIL	0 - 15
BCY58 BCY70	0 - 2			*ZTX531	0 - 20		0.20	16 pin DIL	0 - 17
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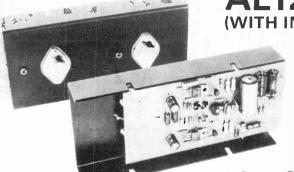
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1000mfd/30V - 30p axial

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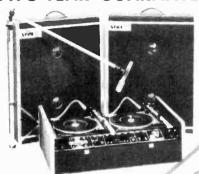


illustration shows GXL Centaur System

These systems feature full mixing for two decks tape & mic with monitoring acilities - override and are supplied complete with sound to light sequencer, display, speaker leads etc.

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	.40

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100	99999999999	MONO ON STEREO	Sept.
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I	Available complete and ready to plug in or as ag	Mone module £22.5	
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	supplied.	Kit of knobs/sockets orc £5.5	_
d		COMPLETE MIXERS (with case	e)
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1	Twin Deck - Mic & Tape Inputs - Wide range boss	Stereo 189 £57.5	0
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(As fitted to our package PA system)

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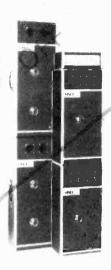
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Type 1 in OBA 1 in OBA 1 in 2BA 1 in 2BA 1 in 4BA	No. 839 840 842 843 844	Price £1 20 £0 75 £0 65 £0 45 £0 52 £0 44	Type lin 4BA lin 6BA lin 6BA lin 6BA	No. 846 847 848 849 850	Price £0.32 £0.25 £0.40 £0.21 £0.25
BA NUTS - 50.	packs of	cadmium p	lated full nu	its in mul	tiples of
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# **SWITCHES**

Description DPDT miniature slide DPDT standard slide Toggle switch SPST	<b>No</b> . 1973 1974		Price £0-11* £0-14*
13 amp 250V a.c. Toggle switch DPDT	1975		£0.33*
1 amp 250V a.c. Rotary on-off mains switch Push switch — Push to make Push switch — Push to break	1976 1977 1978 1979		£0.42° £0.50° £0.13° £0.18°
ROCKER SWITCH A range of rocker switches SPST — moulded in high insulation. Material available in a choice of colours ideal for small apparatus.	Colour RED BLACK WHITE BLUE YELLOW LUMINOUS	No. 1980 1981 1982 1983 1984 1985	Price £0:30° £0:30° £0:30° £0:30°
Description Miniature SPST toggle, 2 amp	No.		Price
250V a.c.	195B		£0 50°
Miniature SPST toggle, 2 amp 250V a.c.	1959		£0.55*
Miniature DPDT toggle, 2 amp 250V a.c.	1960		£0.70*
Miniature DPDT toggle, centre off, 2 amp 250V a.c.	1961		£0.85*
Push button SPST, 2 amp 250V a.c.	1962		£0.78*
Push button SPST, 2 amp 250V a.c.	1963		£0.83°
Push button DPDT, 2 amp 250V a.c.	1964		£0.98•

Description

MIDGET WAFER SWITCHES
Single-bank wafer type – suitable for switching at 250V a.c.
100mA or 150V d.c. in non-reactiver loads make-before-break
contacts. These switches have a spindle 0-25in dia. and 30° indexing.

Descript 1 pole 2 pole 3 pole 4 pole	tion 12 way 6 way 4 way 3 way	Order No. 1965 1966 1967 1968	Price £0.48° £0.48° £0.48°

MICRO SWITCHES	Order No:	Price
Plastic button gives simple 1 pole change		
Patient 10 amp 250V a.c.	1970	£0 25

# **FUSE HOLDERS** AND FUSES

Order No. Price

1 in x in 1 in car in Panel mor	imm chassis mount chassis mount in the type unting 20mm unting 1 ½ in			506 507 508 509 510	£0	0.12° 0.15° 0.20 0.30
QUICKE	LOW 20mm					
Type 150mA 250mA 550mA 800mA	No. 611 6p 612 5p 613 5p 614 7p	1A 6 1-5A 6 2A 6	No. 515 <b>5p</b> 516 <b>6p</b> 517 <b>5p</b> 518 <b>6p</b>	Type 3A 4A 5A	No. 619 620 621	5p 6p 5p
ANTI-SU	JRGE 20mm					
Type 100mA 250mA 500mA	No. 622 623 624	Type 1A 2A 1.6A All 7p	No. 625 626 627 each	7yr 2:5 3:1 5A	5A 15A	No. 628 629 630
QUICK	LOW 1 in					
Type 250mA	No. 631	Type 500mA All 7p	No. 632 each	Тур 80	oe OmA	No. 634
Type 1A 2A	No. 635 637	Type 2.5A 3A	No. 63B 639	Tyj 5A		No. 642
		All 6p	each			

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ALUMII construi and scre	ction each be	S. Made frox complete	om bright al with half inch	deep lid
No.	Length	Width	Height	Price
159	5 lin	2 ½ in	1 ½ in	62p
160	4in	4in	1 <del>∑</del> in	62p
161	4in	2½in	1 ½ in	62p
162	5½in	4in	1 ½ in	70p
163	4in	2 in	2 in	64p
164	3in	2in	1 in	44p
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C26 4 pieces 8"	x 31	(approx.) Single-sided fibreglass	80p
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No. 2021 2022 2023			Price 90p° 90p° 95p°
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Multi-tapp	RD MAINS Primary ned secondary main	s transformer:	s available in ½

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# High quality audio modules for Stereo and mono

**S450** 

STEREO FM TUNER Fitted with phase lock-loop £22 · 30

+ 40p p&p + 121% VAT



7 + 7w R.M.S.

25w

FREQUENCY RANGE	88~108 Mhz	
SENSITIVITY	3.0 µV	
BANDWIDTH	250 kHz	
SPURIOUS REJECTION	50 dB	
SELECTIVITY ± 400 kHz	55 dB	
AUDIO OUTPUT (22 5 kHz devi	viation) 100 mV	
STEREO SEPARATION	30 dB	
SUPPLY REQUIREMENTS	20 to 30V (90mA max)	
AERIAL IMPEDANCE	75 ohms	
DIMENSIONS	240mm × 110mm × 32mm	

The 450 Tuner provides instant programme selection at the touch of a button ensuring accurate tuning of 4 pre-selected stations, any of which may be altered as often as you choose, simply by changing the settings of the pre-set controls. Features include FET input stage. Vari-Cap diode tuning. Switched AFC LED Styreo Indicator.

Stereo 30 COMPLETE CHASSIS £18 ·95 + 40 p&p + 12% VAT

OUTPUT POWER	7 Watts RMS
LOAD IMPEDANCE	8 ohms
TOTAL HARMONIC DISTORTION	Less than .5% (Typically .3%)
FREQUENCY RESPONSE	50 Hz to 20 kHz ± 3dBs
TONE CONTROL RANGE	± 12 dBs at 100Hz and 10kHz
SENSITIVITY	190 mV for full output
INPUT IMPEDANCE	1 M ohms
TRANSFORMER REQUIREMENTS	22 V.A.C. rated at 1A
DIMENSIONS (Less controls and panel)	200mm × 130mm × 33mm

25 Watts RMS

20 Hz to 30 kHz × 2 dBs 280 mV for full output

103mm × 64mm × 15mm

125 Watts RMS continuous

25 Hz 20 kHz measured at 100 Watts

4-16 ohms

450 mV

Less than .25%

75 mV for full output 74mm × 63mm × 28mm

20 Hz to 20 kHz × 1 dB

Within ± 1 dB from 20 Hz to 20 kHz

± 15 dBs at 75 Hz + 10-20 dBs at 15 kHz

Less than -1% (Typically -07%)
100 mV/100 K ohms | For an
100 mV/100 K ohms | output
3-5 mV/50 K ohms | 250 mV

Better than 65 dBs (All inputs)

Better than 26 dBs (All inputs)

300 × 90 × 33mm (less controls)

100 K ohms

8~16 nhms

The Stereo 30 comprises a complete stereo pre-amplifier, power amplifiers and power supply. This, with only the addition of a transformer or overwind will produce a high quality audio unit suitable for use with a wide range of inputs i.e. high quality ceramic pick-up, stereo tuner, stereo tape deck etc. Simple to install, capable of producing really first class results, this unit is supplied with full instructions, black front panel, knobs, main switch, fuse and fuse holder and universal mounting brackets.

SHPPLY LOAD IMPEDANCE

OUTPUT POWER

FREQUENCY RESPONSE

MAX. HEAT SINK TEMPERATURE 90°C

# AL60

AUDIO AMPLIFIER MODULE 25 Watts RMS

£4.55 + 25p p&p

+ 121% VAT

This high quality audio amplifier module is for use in audio equipment and stereo amplifiers and provides output powers up to 25 RMS with distortion levels below 0:1%.

# AL80

AUDIO AMPLIFIER MODULE £7·15 + 25p p&p + 8% VAT



35 Watts RMS
40-60 V
8-16 ohms
Less than 1% (Typically 06%
20 Hz to 30 kHz × 2 dBs
280 mV for full output
90°C
103mm × 64mm × 15mm

TOTAL HARMONIC DISTORTION Less than 1% (Typically 06%)

The AL80 is similar in design to the AL60 above and is of the same high quality but provides output powers up to 35W with distortion levels below  $0 \cdot 1\%$ .

LOADS

OUTPUT POWER

OPERATING VOLTAGE

FREQUENCY RESPONSE

INPUT IMPEDANCE

LOAD IMPEDANCE INPUT IMPEDANCE

SENSITIVITY

FREQUENCY RESPONSE

FREQUENCY RESPONSE

BASS CONTROL RANGE

TREBLE CONTROL RANGE SIGNAL/NOISE RATIO

TOTAL HARMONIC DISTORTION
SENSITIVITY 1. TAPE
INPUTS 2. RADIO TUNER
3. MAGNETIC P.U.

SENSITIVITY FOR 100 WATTS

MAXIMUM SUPPLY VOLTAGE

TOTAL HARMONIC DISTORTION

POWER OUTPUT for 2% THO

TOTAL HARMONIC DISTORTION 50 WATTS into 4 ohms 50 WATTS into 8 ohms

# **AL250**

POWER AMPLIFIER



	S	-
 de		

£17 ·25 + 40p p&p + 8% VAT

This unit, designated AL250, is a power amplifier providing an output of up to 125W RMS, into a 4 ohm load.

# AL30A

AUDIO AMPLIFIER MODULES



£3 75 + 25p p&p + 12}% VAT These low cost 5 and 10 watt modules offer the utmost in reliability and performance,

SPM80



STABILISED POWER SUPPLY £4.25 + 25p p&p + 121% VAT



125W R.M.S.

ing compact in size.
inal
5 amps
арргох.
63mm × 30mm

Designed to power two AL60s at 15 Watts per channel simultaneously. Circuit Techniques include full short circuit protection.

FOUALISATION

INPUT OVERLOAD

# PA100



£15 · 80

DIMENSIONS A top quality stereo pre-amplifier and tone control unit, the PA100 provides a comprehensive solution to the front end requirements of stereo amplifiers or audio units. The six push button selector switch gives a choice of inputs together with two filters for high and low frequencies.

# MPA30

MAGNETIC CARTRIDGE PRE-AMPLIFIER

Enjoy the quality of a magnetic cartridge with your existing ceramic equipment using + 12½ % VA the MPA 30 which is a high quality preamplifier enabling magnetic cartridges to be used where facilities exist for the use of ceramic cartridges only.

3:5 mV for 100 mV output

SEMSITIVITY	3.2 WA JOL JOO WA ORIBRI
EQUALISATION	Within ± 1 dB from 20 Hz to 20 kHz
INPUT IMPEDANCE	50 K ohms
SUPPLY	18 to 30 V-re earth
DIMENSIONS	110 × 50 × 25mm (inc DIN socket)

# PA12 STEREO PRE-AMPLIFIER



£7·10

£2.95

The PA12 Stereo Pre-Amplifier chassis is designed and recommended for use with the AL 20/30 Audio Amplifier Modules, the PS12 power supply and the T538 Transformer. Features include on/off volume, Balance, Bass and Treble controls. Complete with tape output.

ith tape output.
20 Hz-20 kHz (-3dB)
± 12 dB at 60 Hz
± 14 dB at 10 kHz
1 Meg. ohm
300 mV
-60 dB
65 dB
± 20 dB
25 K ohms
152mm × 84mm × 25mm

# **PS12 POWER SUPPLY**

Designed for use with the AL30A S.450 and MPA30 in conjunction with transformer T538. INPUT VOLTAGE OUTPUT VOLTAGE OUTPUT CURRENT SIZE £1 ·30 + 25p p&p + 121% VAT 60mm × 43mm × 26mm

# **GE 100 NINE CHANNEL** MONO-GRAPHIC EQUALIZER

The GE100 has nine 1 octave adjustments using integrated circuit active filters. Boost and Cut limits are ± 12dB. Max. Voltage handling 2 V RMS, T.H.D., 0.05%, input impedence 100K. Output impedence less than 10 K. Frequency response 20 Hz - 20 kHz (3dB). The nine gain controls are centred at 50, 100, 200, 400, 800, 1,600, 3,200, 6,400 and 12,800 Hz. The suggested gain controls are 10 K LIN sliders (not suggested gain controls are 10 K LIN sl

\$630 POWER SUPPLY BOARD for GE100 15-0-15 VOLT £5-50 + 121 VAT + 25p p&p

# SIREN ALARM MODULE

American Police screamer powered from any 12 volt supply into 4 or 8 ohm speaker. Ideal for car burglar alarm, freezer breakdown and other security purposes. Order No. S15. No. BP124. Only £3·50 + 1% VAT + 25p p&p

# MA60 HI-FI AMPLIFIER KIT

Build you own top quality amplifier, save yourself pounds. The MA60 kit comprises the following Bl-kits modules,  $2 \times AL60$  amps,  $1 \times PA100$  pre-amp,  $1 \times SPM80$  stab. power supply,  $1 \times BMT80$  transf. giving 17 watts RMS per channel STEREO. All modules coyered by the Bl-PAK satisfaction or money back guarantee. Details of the above modules are in this ad. Price £32·90 + 12;% VAT + 62p p&p.

# TC60 KIT

A beautifully designed genuine TEAK WOOD veneered cabinet to put the professional touches to your home built amplifier. Full set of parts incl. Front & Back Panels, Knobs, Chassis, Fuses, Sockets, Noen, etc. Ideal for the MA60. Size: 425mm × 290mm ×

95mm. Price £19·95 + 12½% VAT + 86p p&p

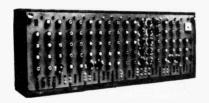
# **TRANSFORMERS**

T538 For use with S.450 AL30A MPA30
Order No. 2036
Price: £3·20 + 55p p&p + 12½% VAT
T2050 For use with Stereo 30
Order No. 2050
Price: £3·25 + 55p p&p + 12½% VAT
BMT80 For use with AL60 SPM80
Order No. 2034
Price: £5·40 + 86p p&p + 12½% VAT
BMT250 For use with AL250 Price: £6:35 + £1:10 p&p + 121% VAT



DEPT. PE8, P.O Box 6, Ware, Herts

# KITS FOR SYNTHESISERS, SOUND EFFECTS



COMPONENTS SETS include all necessary resistors. capacitors, semiconductors, potentiometers and transformers. Hardware such as cases, sockets, knobs, keyboards, etc. are not included but most of these may be bought separately. Fuller details of kits, PCBs and parts are shown in our lists.

CIRCUIT AND LAYOUT DIAGRAMS are supplied free with all PCBs unless "as published".

PHOTOCOPIES of all P.E. texts for most of the kits are available—prices in our lists.

# PHONOSONICS

PRINTED CIRCUIT BOARDS, KITS AND TO WORLD-WIDE COMPONENTS Α MARKET

P.E. MINISONIC Mk. 2 SYNTHESISER
A portable mains-operated Miniature Sound Synthesiser, with keyboard circuits. Although having slightly fewer facilities than the large PE Synthesiser the functions offered by this design give it great scope and versatility Consists of 2 log VCOs. VCF. 2 envelope shapers. 2 voltage controlled amps keyboard hold and control circuits. He oscillator and detector, ring modulator, noise generator, mixer power supply. mixer, power supply.

Set of basic component kits Set of printed circuit boards

P.E. SYNTHESISER (P.E. Feb. 73 to Feb. 74)
The well acclaimed and highly versatile large-scale mains-operated Sound Synthesiser complete with keyboard circuits. Other circuits in our lists may be used with the Synthesiser to good advantage.

The Main Synthesiser: PSU, 2 linear VCOs, 2 ramp generators, 2 input amps, sample hold, noise generator, reverb amp, ring modulator, peak level circuit, envelope shaper, voltage controlled amp.

Set of basic component kits

£83-03
Set of printed circuit boards
£13-20

The Synthesiser Keyboard Circuits (can be used without the Main Synthesiser to make an independent musical instruments: 2 logarithmic VCOs, divider, 2 hold circuits, 2 modulation amps,

mixer, 2 envelope shapers and PSU.
Set of basic component kits
Set of printed circuit boards

£48-18

GUITAR EFFECTS PEDAL (P E July 75)
Modulates the attack decay and filter characteristics of an audio signal not only from a guitar but from any audio source, producing 8 different switchable effects that can be further modified by manual controls. Possibly the most interesting of all the low-priced sound effects units in our range. Circuit does not duplicate effects from the Guitar Overdrive Unit.

Component set with special foot operated switches Alternative component set with panel switches Printed circuit board

SOUND BENDER (P E May 74)

A multi-purpose sound controller, the functions of which include envelope shaper, tremolo, voice-operated fader, automatic fader and frequency-doubler.

Component set for above functions (excl SWs)

Printed circuit board

E1-81

Printed circuit board £1.81
Optional extra—additional Audio Modulator, the use of which, in conjunction with the above component set, can produce jungle-drum rhythms
Component set (incl. PCB) £2.88

PHASING UNIT (P E Sept 73)
A simple but effective manually controlled unit for introducing the phasing sound into live or recorded

Component set (Incl. PCB)

PHASING CONTROL UNIT (P E Oct 74)

For use with the above Phasing Unit to automatically control the rate of phasing

Component set (incl. PCB)

£448

SOPHISTICATED PHASING AND VIBRATO UNIT

A slightly modified version of the circuit published in Elektor. December 1976, and includes manual and automatic control over the rate of phasing and vibrato.

£17.69

WAH-WAH UNIT (P.E. Apr. 76)
The Wah-Wah effect produced by this unit can be controlled manually or by the integral automatic controller Component set (incl. PCB)

£3-55

AUTOWAH UNIT (P.E. Mar. 77)

Automatically produces Wah-pedal and Swell-pedal sounds each time a new note is played Component set. PCB. special foot switches £7.27 Component set and PCB, with panel switches £4.83

P.E. JOANNA PLUS ORGAN VOICING

The basic five octave electronic piano (P.E. May/Sept 75 and Sound Design) has switchable alternative voicings for Honky-Tonk, ordinary piano, and Harpsichord or a mixture of any of these three, together with facilities including fast and slow tremolo, loud and soft pedal switching, and sustain pedal switching. The modification retains all the circuitry associated with the piano but in addition provides an organ-voice envelope facility with 5 switchable pitches, variable attack and sustain, phasing and

orato.

Set of components (excl switches) for PSU, Frequency generator, Pitch and Note Divider, Envelope Shapers, Voicings, and Control circuitries. (Order as KIT 71-5) Set of PCBs (Order as PCB SET 71-6) £109.75

SYNTHESISER TUNING INDICATOR (P.E. July 77)
A simple 4-oclave frequency comparator for use with synthesisers and other instruments where the full versatility of the P.E. Tuning Fork is not required.

Component and PCB (but excl sw.)

GUITAR FREQUENCY DOUBLER (P.E. Aug. 77)

A modified and extended version of the circuit published Component set and PCB

### GUITAR SUSTAIN (P.E. Oct 77)

Maintains the natural attack whilst extending note duration.

Component set, PCB and foot switches £4-90

Component set, PCB and panel switches £3-48 £4-90

WIND AND RAIN UNIT

A manually controlled unit for producing the above-named

Component set (incl PCB)

GUITAR OVERDRIVE UNIT (P.E. Aug. 76)
Sophisticated, versatile Fuzz unit, including variable and switchable controls affecting the fuzz quality whilst retaining the attack and decay, and also providing filtering. Does not duplicate the effects from the Guitar Effects Pedal and can be used with it and with other electronic instruments. Component set using dual slider pot. Component set using dual rotary pot. £6.80
Printed circuit board. £1.62

mple Fuzz unit based upon P.E. "Sound Design" circuit.
Component set (incl. PCB) £2-05

TREMOLO UNIT
Based upon P E Sound Design circuit
Component set (Incl. PCB) £3-64

TREBLE BOOST UNIT (P.E. Apr. 76)
Gives a much shriller quality to audio signals fed through it. The depth of boost is manually adjustable Component set (incl. PCB)

£2.40

P.E. TUNING FORK (P E Nov 75)

Produces 84 switch-selected frequency-accurate tones. A LED monitor clearly displays all beat note adjustments, Ideal for tuning acoustic or electronic musical instruments.

Main component set (incl. PCB) £15-59

Power supply set (incl. PCB)

SEE OTHER PAGE FOR KEYBOARDS, AND OUR LISTS FOR OTHER COMPONENTS AND **ACCESSORIES STOCKED** 

P.E. SYNCHRONOME (P.E. Mar. 76)
An accented-beat electronic metronome, providing duple, triple and quadruple times with full control over the beat rate. Can also be used as a simple drum-beat rhythm generator includes power supply.

Component set (incl. loudspeaker)

£11.62

Printed circuit board

TAPE NOISE LIMITER

Very effective circuit for reducing the hiss found in most tape recordings. All kits include PCBs
Standard tolerance set of components
Superior tolerance set of components
£2.96 Regulated power supply (will drive 2 sets) £4-69

ENVELOPE SHAPER WITHOUT VCA (P.E. Oct. 75)

Provides full manual control over attack, decay, sustain and release functions, and is for use with an existing voltage controlled amplifier

Component set (incl. PCB)

ENVELOPE SHAPER WITH VCA (P.E. Apr. 76)
This unit has its own voltage controlled amplifier and has full manual control over attack, decay, sustain and release

Component set (incl. PCB)

TRANSIENT GENERATOR (P.E. Apr. 77)
An envelope shaper, without VCA, having the usual attack, decay, sustain and release functions, and in addition it also provides a Repeat Effect enabling a synthesiser to be programmed to imitate such instruments as a mandolin or

Component set Printed circuit board

WAVEFORM CONVERTER

Slightly modified from a circuit published in "Elektor". Converts a saw-tooth waveform into four different waveforms: sine-wave, mark-space saw-tooth, regular triangle form, and squarewave with an externally variable mark-space ratio.

Component set (incl. PCB but excl. sw/s) £8:19

VOLTAGE CONTROLLED FILTER (P.E. Dec. 74)
Part of the P E Minisonic now released as an independent kit for use with other synthesisers
Component set (incl. PCB) (Order as Kit 65-1)
£8-22

RING MODULATOR (P.E. Jan 75)

Part of the P.E. Minisonic now released as an independent kit for use with other synthesisers.

Component set (incl. PCB) (Order as Kit 59-1) £5-50

NOISE GENERATOR (P.E. Jan. 75)
Part of the P.E. Minisonic now released as an independent kit for use with other synthesisers.
Component set (incl. PCB.) (Order as Kit 60-1) £3-35

SOPHISTICATED POWER SUPPLIES

A wide range of highly stabilised low noise power supply kits is available—details in our lists.

MICROPHONE PRE-AMP (P.E. Apr. 77) Component set (incl. PCB)

VOICE OPERATED FADER (P.E. Dec. 73)

or automatically reducing music volume during talk-over —particularly useful for Disco work or for ome-movie shows

Component set (incl. PCB) £3-97 £3-97

DYNAMIC RANGE LIMITER (P.E. Apr. 77)
Automatically controls sound output to within a preset

Component set (Incl. PCB)

FUST ANU HANULING

U.K. orders—under £15 add 25p plus VAT, over £15 add 50p plus VAT. Keyboards £2-00 plus VAT.

Optional Insurance for compensation against loss or damage in post, add extra 50p for cover up to £50, £1-00 for £100 cover.

£2:-00 for £200 cover.

Eire, C.I., B.F.P.O., and other countries are subject to Export postage rates.

Add 121% (or current rate if changed) to full total of goods, post and handling. (Does not apply to export orders).

EXPORT ORDERS are welcome, though we advise that a current copy of our list should be obtained before ordering as it also shows Export postage rates. All payments must be cash-with-order, in Sterling and preferably by International Money Order or through an English Bank. To obtain list send 50p.

PHONOSONICS · DEPT. PE68 · 22 HIGH STREET · SIDCUP · KENT DA14 6EH MAIL ORDER AND C.W.O. ONLY

# AND OTHER PROJECTS

PHOTOGRAPHS in this advertisemen o of our units containing some of projects built from our kits and PCBs. The cases were built by ourselves and are not for sale, though a small selection of other cases is available.

LIST—Send stamped addressed envelope with all U.K. requests for free list giving fuller details of PCBs, kits and other components

OVERSEAS enquiries for list Europe send 20p; other countries—send 50p.



TRANSISTORS

BC184 ... BC187 ... BC204 ... BC209 C BC213 ... BC214 ... BC262 ... BC415 ... BC478 ... BD131 ... BD132 ... BF244A BF245A BSY95A MDB001 OC71 ... OC72 .... RPY5BA

TIS43.... ZTX108. ZTX301. ZTX384. ZTX501. 2N2219

26p 26p 14p 14p 15p 14p 12p

22p 22p 66p 60p 12p 12p 35p 64p 39p

# KIMBER-ALLEN **KEYBOARDS AND CONTACTS**

Kimber-Allen Keyboards as required for many published circuits. The manufacturers claim that these are the finest moulded plastic keyboards available. All octaves are C to C, the keys are plastic, spring-loaded, fitted with actuators, and mounted on a robust aluminium frame.

3 Octave (37 notes)

£25-50

4 Octave (49 notes) £32-25

Contact Assemblies (gold-clad wire) for use with the above keyboards (1 required for each

Type GJ: Single-pole change-over	each 24p
Type GB: 2 pairs of contacts, each pair normally open	each 27p
Type GC: 3 pairs of contacts, each pair normally open	each 36p
Type GE: 4 pairs of contacts, each pair normally open	each 45p
Type GH: 5 pairs of contacts, each pair normally open	each 57p
Type 4PS: 3 pairs of contacts plus single-pole changeover	each 53p

Printed Circuit Boards for use with GJ, GB and 4PS contacts (thus eliminating much interwiring) are available. Details in our lists

## RHYTHM GENERATOR

15-Rhythm Tempo, Timing and Logic control	unit (excl. sw's
but incl. PCB)	£12.90
10-Instrument Effects circuits	£13-56
PCB for Effects circuits	£4-25
Power Supply incl. PCB	£12.00

### 128-NOTE TUNE-PROGRAMMABLE SEQUENCER

## (P.E. Nov/Dec 77)

Enables a voltage controlled synthesiser to automatically play pre-programmed tunes of up to 32 pitches and 128 notes long. Programs are keyboard initiated and note length and rhythmic pattern are externally variable. (Please use order codes quoted in

Main Circuit (Nov) excl. sw's (KIT 76-1)	£20-60
Power Supply (KIT 76-3)	£6.05
Trigger Inverter and Alt. Output (KIT 76-2)	£1-35
LED Counter (KIT 76-4)	£2-45
PCB (as published) for KITS 76-1 & 3 (PCB 76A)	£2-61
PCB for KITS 76-2 & 4 (PCB 76B)	£2.54

# P.E. STRING ENSEMBLE (PE Mar-July 78)

the new keyboard string-instrument synthesiser.	
8asic component sets:	
Power Supply (KIT 77-1)	£9.22
Tone Generator (KIT 77-2)	£14.93
Diode Gates (KIT 77-3)	£19.78
Chorus Generator (KIT 77-4)	£19.06
Voicing System (KIT 77-5)	£9.38
Printed Circuit Boards:	
Double-sided PCB for Power Supply, Tone Generato	r & Diode
Gates with most of the Matrix wiring as printed tra	acking
(PCB 77L/R)	£18.40
PCB for Chorus Generator (PCB 77C)	£2.65
PCB for Voicing System (PCB 77D)	£2.62
Fuller details of kits & PCBs are in our lists.	

# FORMANT SYNTHESISER (Elektor 1977/78)

Very sophisticated music synthesiser for the advanced constructor who puts performance before price. Details in our lists.

# DISCOSTROBE (P.E. Nov. 76)

4-channel light-show controller giving a choice of sequential random, or full strobe mode of operation. Basic component set

Printed circuit board £3-45

# 8IOLOGICAL AMPLIFIER (P.E. Jan./Feb. 73)

Multi-function circuits that, with the use of other external equipment, can serve as lie-detector, alphaphone, cardiophone

Pre-Amp Module Components set (incl. PC8) Resic Output Circuits—combined component set with PCBs, for alphaphone, cardiophone, frequency meter and visual feed-back lampdriver circuits. £6-59 Audio Amplifier Module Type PC7

# 10% DISCOUNT VOUCHER (PE68)

TERMS: Correctly costed, C.W.O., U.K. orders over £50 goods value. Valid until end of month on cover of P.E. This voucher must accompany order.

PRICES ARE CORRECT AT TIME OF PRESS. E. A O. E. DELIVERY SUBJECT TO AVAILABILITY

**PHONOSONICS** 

| INTEGRATED CIRCUITS | 301 8-pin DIL | 48p | 318 8-pin DIL | 230p | 320-15 | 324 14-pin DIL | 48p | 321 14-pin DIL | 48p | 321 14-pin DIL | 48p | 723 1705 | 105p | 723 14-pin DIL | 63p | 723 14-pin DIL | 63p | 724 18-pin DIL | 63p | 748 8-pin DIL | 18p | 780 170 220 | 205p | 20

INTEGRATED CIRCUITS

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### KONTAKT 60

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Contains a light lubricant to avoid possible corrosion of contact paths and obviates further oxydisation and 'creep' currents.

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	7400	.13	7447	.08	4001	.17	4047	.95
١	7401	.13	7451	.16	4002	.17	4049	.48
ĺ	7402	.16	7470	.30	4011	.19	4050	.53
ŀ	7403	.16	7472	.28	4013	.45	4070	.53
١	7404	.19	7473	.30	4014	.85	4502	.95
ļ	7406	.36	7474	.30	4015	.85	4508	2.09
١	7407	.36	7475	.40	4016	.52	4510	1.51
١	7408	.19	7476	.35	4017	.85	4511	1.75
ĺ	7410	.14	7486	.35	4018	.85	4514	2.98
l	7413	.36	7493	.35	4023	.19	4516	1.09
l	7414	.74	7496	.82	4027	.52	4518	1.02
l	7416	.36	74107	.32	4028	.97	4528	1.02
l	7420	.16	74141	.70	4042	.85	4536	5.00
l	7442	.68			4046	1.40		
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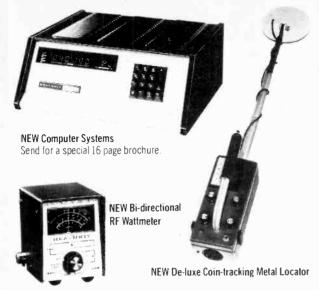
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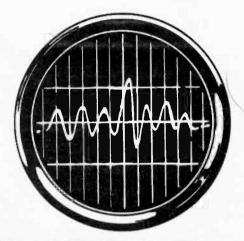
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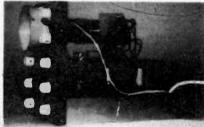
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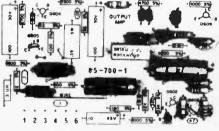


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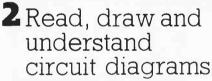
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# **FAST MOVING?**

RECENT news of the development of further advanced passenger trains capable of 150 m.p.h. has triggered interest from overseas governments. The Japanese are known to have a particular interest in the systems used to tilt the trains by up to nine degrees on curves; this is an electro-hydraulic system, the design of which interests the Japanese Government. Let us hope that we can sell these systems, or at least the technology, to them rather than once again allow others to capitalise on our inventiveness.

# INFORMATION

We have also noted one or two other improvements—the installation of "travel computers" at main line stations being one of particular interest.

A simple unit that quickly provides all train times and other general information at the push of a few buttons is a great boon to many travellers. The unfortunate part is that one must be at the station to use the computer. With the now inadequate telephone information system, one can spend a whole day trying to obtain

train times, etc. as anyone who has tried recently in the London area will know.

With the widespread use of Viewdata still a good few years away, it is a problem which would appear to require an interim solution—perhaps the installation of a Viewdata terminal at all stations would assist!

# **ROBOTS**

These are just two minor areas where we are seeing the immediate application of "the new electronics" and it is being widely reported that the advance of technology will change the whole face of industry and society. With approximately 70,000 industrial "robots" already in use in Japan is it any wonder that they are able to produce many items cheaper than Western countries. Although we in Britain are employing robots in increasing numbers, we are generally rather behind other industrial countries in this area, for a variety of reasons.

The knowledge that a revolution is about to commence is said to be partly behind the NEB plan to set up a microelectronics company in partnership with a group of engineers. This controversial scheme has rocked the

established companies in this country—few of which have made the necessary capital investment to enable them to compete with i.c. manufacturers in America and Japan.

The business of chip production was recently referred to as "silicon printing" by Dr. Ed. Sack of General Instrument Microelectronics, one of the few companies producing chips in Britain. It is sad to note that GIM was set up by a group of British engineers with American backing about 10 years ago to design and sell chips for the communications industry. However, many of its products are now selling well abroad but not in Britain because the technology employed is in advance of the British systems.

GIM see the next boom as being in games—particularly hand held ones—and toys. They have developed a remote control system for toy cars which employs two m.p.u.'s. GIM are also active in programmable TV games and have joined forces with EMI who will be selling software in cassette form. Perhaps their recent Queen's Award for export achievement will be augmented by a rapidly expanding home market!

Mike Kenward

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made payable to IPC Magazines Limited.

# Letters

Queries regarding articles published in PE should be addressed to the Editor, at the Editorial Offices, and a stamped, addressed envelope enclosed. We cannot undertake to answer questions regarding other items, nor to answer technical queries over the telephone.

THIS touch switch can be used to directly replace an ordinary household light switch without the need for either additional wiring or fixing. The unit is capable of handling a mains load of up to 300 Watts and if the quadrac CSR1 (a diac and triac combined) is mounted on a suitable heatsink this figure can be increased to 750 Watts.

## CIRCUIT DESCRIPTION

The complete circuit diagram of the Touch Switch is shown in Fig. 1. Gates "a" and "b" of IC1 are connected as a bistable multivibrator with gates "c" and "d" used as a buffer stage.

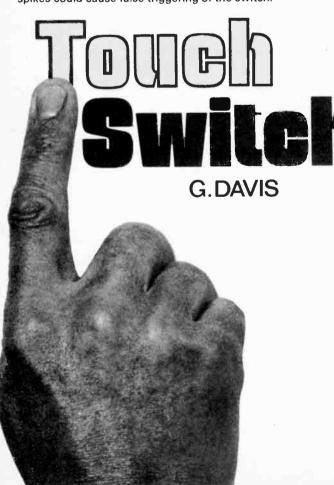
When the switch is off the output from the buffer stage (pins 10 and 11) is high and the transistor TR1 is on. Because TR1 is connected across the diode bridge D1 to D4, when it is on the capacitor C4 is prevented from charging. As the quadrac is switched on by a rising voltage across C4, when the transistor TR1 is on the quadrac and consequently the lamp are both off.

If when the lamp is off a finger is placed against the "ON" plate this capacitively grounds the plate due to the high input impedance of the stage and a voltage is developed across R1 and R2. This voltage takes the input of gate "b" high which results in the output of the bistable being switched from the low to the high state. This high state output from the bistable is inverted by the buffer stage to a low state and TR1 is turned off.

With the transistor off, capacitor C4 is no longer prevented from charging via R7 and the voltage across the capacitor increases. When this charging voltage reaches approximately 33V the quadrac switches the lamp on.

When the switch is off the "ON" touch plate is illuminated to enable the switch to be easily located in the dark.

The capacitors C1 and C2 filter any voltage spikes that may occur from motor starting surges elsewhere in the house, such as when a fridge or freezer is turning on. These spikes could cause false triggering of the switch.



# CONSTRUCTION

The p.c.b. design for the Touch Switch is shown in Fig. 2 with Fig. 3 showing the layout of the components. Note that where R1 is joined to R2 and R3 is joined to R4 the components are not soldered to the board.

As the plain side of the printed circuit board is used as the frontplate for the switch (with all the components being mounted on the copper track at the rear of the board) only four drilled holes are necessary in the p.c.b.; two for fixing the switch to the wall and one in the middle of each touch plate.

After the holes have been drilled the p.c.b. can be sprayed the desired colour and then dry cellotape should be placed on the front panel over the two touch plate holes. If the board is then turned over clear epoxy resin can be used to fill the "ON" plate hole while the "OFF" plate hole should be filled with black epoxy resin. When both resins have set the cellotape can be removed.

The components should then be soldered onto the board keeping the leads as short as possible.

# **TESTING AND MODIFICATIONS**

The "lamp" wire from the touch switch should be connected via the lamp to the neutral lead. If the power is turned on and a finger placed over each touchplate in turn the light should go on and off. Care should be taken to ensure the live and lamp wires are connected correctly otherwise the switch will not operate satisfactorily.

If the switch is to be used to drive a fluorescent light the circuit should be modified as shown in Figs. 4 and 5.

By incorporating the CR Network shown in Fig. 6 the light will remain on for a preset time period determined by the value of the CR network, i.e. if  $C=22\mu F$  and  $R=10M\Omega$  the delay is  $22\mu F\times 10M\Omega=2$  mins.

# COMPONENTS . . .

# Resistors

R1, R3 10MΩ (2 off) R2, R4 4.7MΩ (2 off) R5, R7 100kΩ  $\frac{1}{2}$ W (2 off)

R6 100k $\Omega$ R8 220k $\Omega$ 

All 5% 1W carbon unless otherwise stated

# Capacitors

C1 150pF 50V Ceramic C2 47pF 50V Ceramic C3 22μF 16V Tantalum C4 10nF 100V Polyester

# Semiconductors

D1-D4 1N4148 (4 off) D5 6·2V 400mW Zener

D6 1N4004 TR1 ZTX304 IC1 CD4001

CSR1 400V 6-5A Quadrac

# Miscellaneous

Miniature wire ended neon RS type 586-015

# CONSTRUCTOR'S NOTE

All the components including the p.c.b. can be obtained from G.J.D. Electronics, 105 Harper Fold Road, Radcliffe, Manchester.

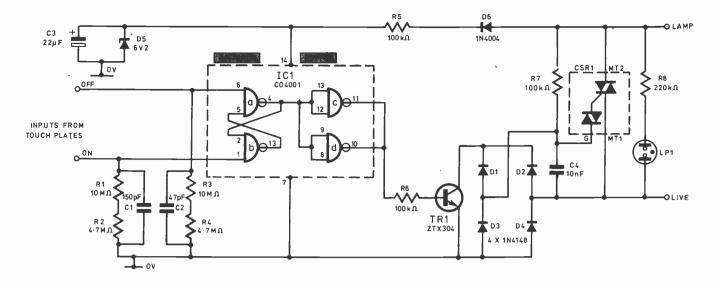


Fig. 1. Complete circuit diagram of the Touch Switch

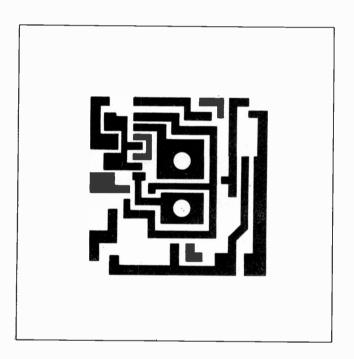


Fig. 2. Printed circuit board design

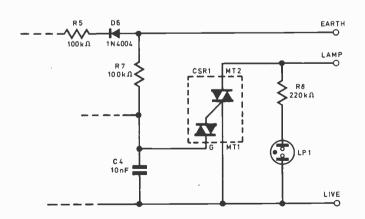


Fig. 4. Modification necessary for switching a fluorescent light

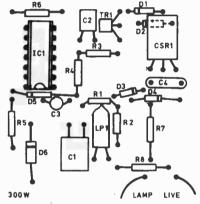


Fig. 3. Component layout for p.c.b.

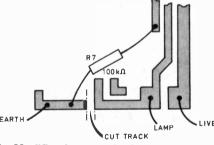


Fig. 5. Modification required to p.c.b. design for switching a fluorescent light

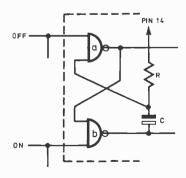


Fig. 6. Modification for obtaining a preset "ON" time period



four motorcycle games
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# PETU GAME CENTRE

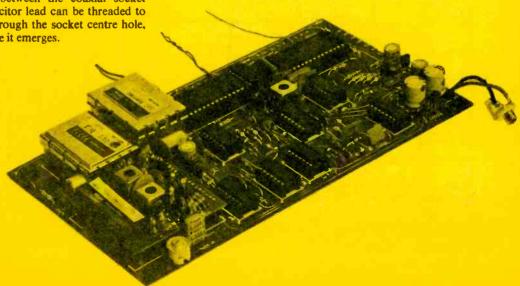
## CONSTRUCTION

Mount all the switches and the potentiometer on the front panel and wire them up as shown in Fig. 2.1, using ribbon cable but leaving the p.c.b. end of the ribbon unconnected.

Insert the i.c.s lastly when assembling the p.c.b., removing them from the conductive foam packing only at the moment necessary. The games chips themselves (IC1 and IC2) should be inserted last of all. Some earthed tin foil laid out on the worktop surface will help to reduce the possibility of damage due to static electricity. It would be advisable to mount the modules early on so that the remaining component space is more apparent. On the UM1263 (sound modulator) it is necessary to remove the lid and solder a 100pF capacitor (C5) between the coaxial socket centre-pin and the p.c.b. The capacitor lead can be threaded to the inside of the modulator box through the socket centre hole, and then soldered at the point where it emerges.

board powered from external power pack

minimal setting-up procedure



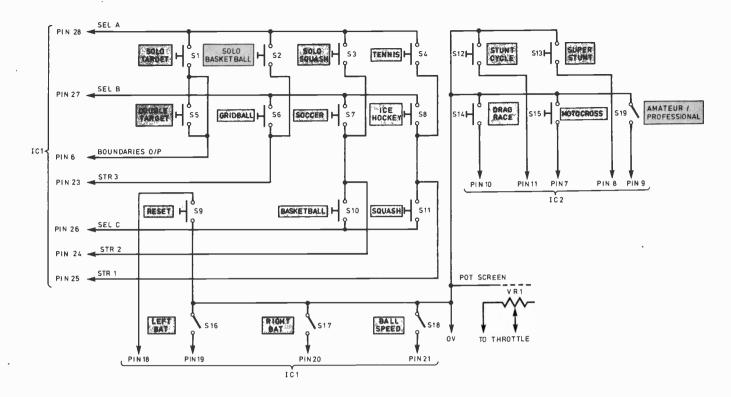
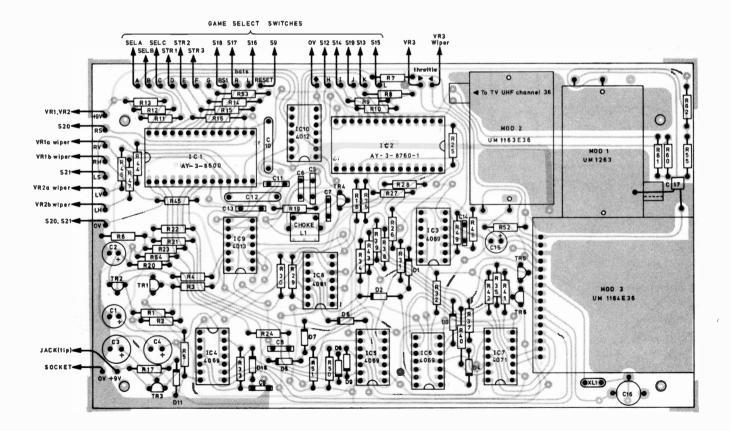


Fig. 2.1. Switch panel wiring diagram. This matrix wiring system was referred to in Part 1, Fig. 1 (wrongly as Fig. 10)

Fig. 2.2. Component board layout. Note that CI7 couples the Sound Modulator output socket to the p.c.b.



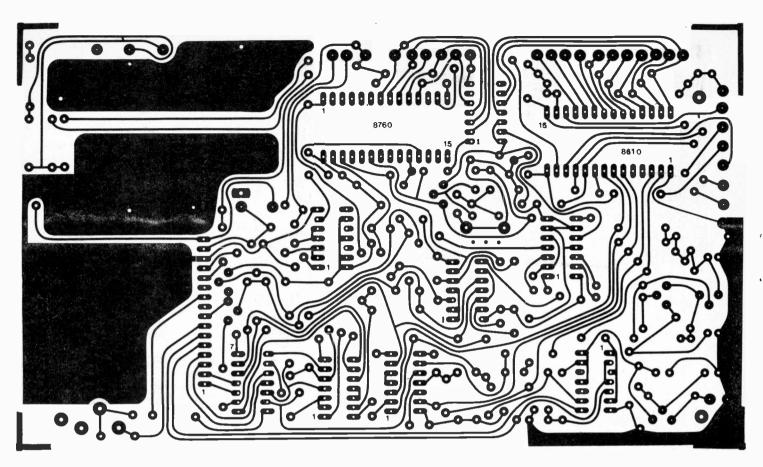
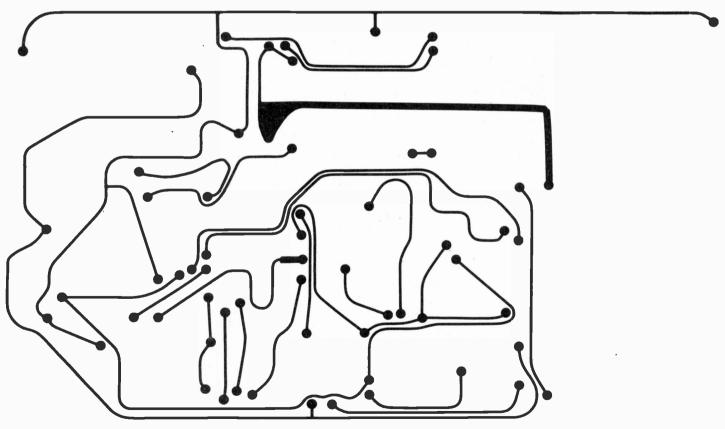
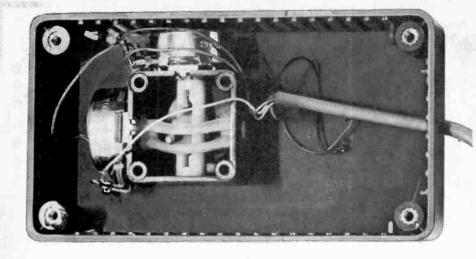


Fig. 2.3. Printed circuit layout (actual size)

Fig. 2.4. Component side p.c.b. (actual size)





The hand-held units (shown here with lid removed), contain dual-axis potentiometers for movement of the bat both up and down, and left and right across the television



The serve buttons supplied by Teleplay are mounted on the outside surface of the box, with only the connection tags passing through the lid

In part one, capacitors C10 and C12 were marked in the components list as  $0.8\mu F$ . This should read  $0.18\mu F$ .

**CORRECTIONS TO PART ONE** 

TR1–TR3 are BC337 transistors, and the tunable choke should be  $40\mu H$  R17 is  $100\Omega and$  not 1 K  $\Omega$ 

It is also necessary to add the following resistors to the components list:

8.2ΚΩ
5.6ΚΩ
2.2ΚΩ
222ΚΩ
6.8ΚΩ
100Ω
100pF silvered mica

The main box should be cut for cable entry holes, and for the miniature jack socket (d.c. supply input). The hand-held units require a square hole of  $15 \times 15$ mm to accommodate the dual axis controls, in addition to further drillings for the push buttons and cable entry.

Screened 5-way cable is necessary to connect the hand-held units to the main box, and the wiring of these can be seen in the main circuit diagram.

Once all the switches and potentiometers are mounted and wired up, the p.c.b. can be fixed into the main box using self-tap screws, and then wired to the various controls. Low loss coaxial lead should be used for the aerial input signal to the television set, the other end of which is connected to the UM1163E36 vision modulator coaxial output socket.

The system is now ready to check out, but first look over the p.c.b. and wiring for possible dry joints, and ensure that all diodes and electrolytic capacitors are connected in the right polarity.

# **SETTING-UP**

All modules supplied by Teleplay should be pre-tuned, but it may be necessary to adjust the oscillator frequency using L1, to lock the picture onto the screen. This should be done with the unit powered up and the television tuned to Channel 36. Fine tuning of the PAL colour encoder crystal is achieved by trimming XL1 (4·4336MHz).

The unit is powered by a mains adaptor unit which plugs straight into a 13A socket, and jacks into the Game Centre via a low tension lead (jack tip + Ve).



# DIGITAL THERMOMETER

M. PLANT

N order to provide a BCD to seven segment display of an analogue quantity, analogue-to-digital circuitry is required. Formerly this meant the use of a large number of discrete and integrated circuit devices which posed problems for the constructor of electronic instruments making use of these digital techniques. The availability of the Siliconix LD130 CMOS i.c. now enables the analogue to digital conversion to be performed with the one device plus a handful of additional components. Sophisticated instrumentation functions can now be obtained with a few components: the LD130 lends itself to the measurement of temperature, voltage, current, resistance, sound intensity, rotational speed, for example, indeed any physical quantity which lends itself to conversion into a voltage change which can then be processed digitally.

In this article the construction of a digital thermometer is described which has the following specifications:

Range -99.9°C to +99.9°C

**Transducer** pn junction diode **Display** 3 digit 7 segment

3 digit 7 seginen

Resolution 0.1°C

Over-and-under range flashing display indication

Minus sign illuminated l.e.d.

Power supply  $6V(4 \times 1.5V - HP7)$ 

Initially the circuit was assembled on Veroboard and gave satisfactory results but a printed circuit board assembly produced improved performance.

# THE LD130

Details of the internal operation of the LD130 will not be described here but are covered in the relevant Siliconix application note. As Fig.1 shows the LD130 is an 18 pin dual-in-line package which features the low power

consumption of all CMOS devices: 25 mW at  $\pm 5 \text{V}$  power supply. The lower limit of the supply voltages is  $\pm 4.3 \text{V}$  and the upper limit is  $\pm 8 \text{V}$  (60 mW consumption). The twin supply voltages must be matched to within 1.5 V for correct operation of the device.

Internal counting is achieved through an oscillator which becomes functional when a single capacitor C4 is connected between pin 14 and ground. This capacitor and C1 together determine the sampling rate of the circuit. In use the i.c. samples the analogue voltage and displays its value in digital form at a sampling rate of  $f_{os}/6144$ .

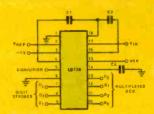


Fig. 1. Pin identity for the LD130



Fig. 2. Graph of frequency related to capacitor choice

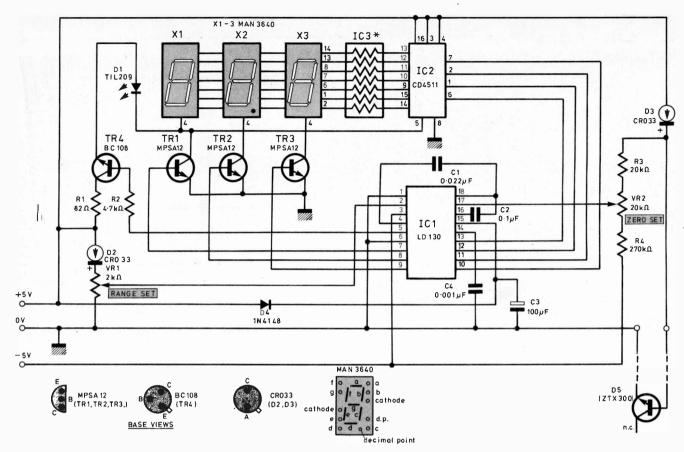


Fig. 3. Thermometer circuit

The oscillator frequency as a functon of C4 is shown in Fig. 2 for various values of the positive supply voltage V1. Thus at V1 = 5V and C4 =  $0.001\mu\text{F}$ ,  $f_{osc}$  is about 30kHz. Therefore the sampling rate is about 5Hz.

The value of the integrator capacitor C1 must be chosen according to the equation C1 =  $(10^3/f_{osc})\mu F$  approximately, that is, C1 should be of the order of  $0.02\mu F$ . The value of the auto zero capacitor should be  $0.1\mu F$ .

The sign and under-and-over range signal appears at pin 5. The analogue input is applied to pin 17 and a reference voltage ( $V_{ref}$ ) is required at pin 2. The multiplexed outputs from pins 10 to 13 and the digit scanning signals from pins 7, 8 and 9 are connected as shown in Fig. 3.

# **CIRCUIT ACTION**

The complete digital thermometer circuit omitting the power supply circuitry is shown in Fig. 3. The reference voltage  $V_{\rm ref}$  for the LD130 is provided by the current regulator diode D2 in series with the potentiometer VR1, the wiper of which is connected to pin 2. This particular current regulator has a zero temperature coefficient and therefore VR1 is able to provide a stable voltage— $V_{\rm ref}$ .

The digits of the seven segment display are scanned by the LD130 pins 7, 8 and 9 via the *npn* Darlington current buffer transistors TR1, TR2 and TR3.

High gain Darlingtons were used ( $\beta = 50,000$ ) although the constructor may use discrete pairs of *npn* transistors to obtain the same function. The l.e.d. D1, indicating the negative sign of the temperature, is driven by transistor TR4.

The digit segments of the common cathode displays X1-3 are driven from IC2 through the current limiting resistors of IC3. For increased brightness these resistors may be reduced to 100 ohms and, of course, individual 0.25W resistors may be used.

# **TRANSDUCER**

Provided the forward current is much greater than the reverse saturation current, the voltage across a pn junction diode biased with a constant current varies by about  $-2\cdot2m\text{V/°C}$  and thus provides a linear temperature-to-voltage transducer—D5. A proportion of the temperature dependent voltage across this sensor is selected by R3, VR2, and R4 voltage divider, one end of which is connected to the negative supply voltage in order that VR2 may be able to set the zero of the temperature scale.

For correct and stable operation of the thermometer, the LD130 must be provided with a short term stable positive supply voltage. As you will see from Fig. 2, any variation in the supply voltage produces a marked change in the oscillator frequency  $f_{\rm osc}$  which in turn leads to jitter of the display reading. This variation in positive supply voltage as seen by the LD130 is liable to be caused by the variable and high currents drawn by the display. These currents can vary from 4mA, when a digit is blanked, to about 100mA assuming say 12mA per segment for a display of 8.

These currents, flowing through the battery impedance and the copper tracks on the circuit board, cause the voltage seen at pin 15 of the LD130 to vary. Some a.c. decoupling at this pin is therefore provided by means of the diode D4 and the capacitor C3.

Note that this provides a positive supply voltage for the LD130 of 0.6V less than the battery e.m.f. The second circuit design feature which ensures display stability is the return of the analogue ground pin 1 of the LD130 direct to the ground connection of the power supply, i.e. the battery negative.

Rather than use a separate battery to supply the negative voltage with respect to analogue ground required by the LD130, an inverter is used to provide a -5V supply relative

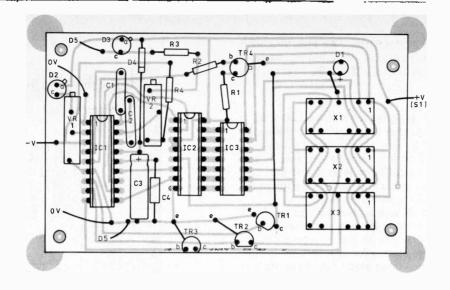


Fig. 4. Main board component layout

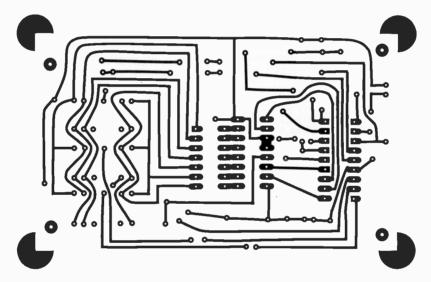


Fig. 5. Etching detail of main board

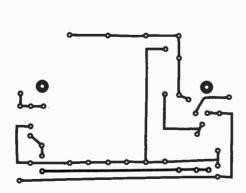


Fig. 6. Inverter p.c. detail

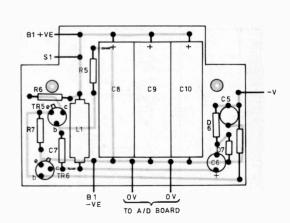


Fig. 7. Component layout

to the zero volts terminal of the battery. An inverter circuit suitable for this is shown in Fig. 8, the output voltage of which is D8's Zener voltage minus TR8's 0-6V be drop, that is 5-6V.

# **ASSEMBLY**

The circuit boards were designed to fit into a 120  $\times$  65  $\times$  40mm box. Four 1.5V calculator batteries power the circuit and display and these just fit across the width of the base of the box. A four pack HP7 type battery holder was broken apart to obtain the terminals. These were fitted into two pieces of SRBP glued into place along the inside edge of the box. This provided a tight fit for the batteries.

The main board is stood off with screws and spaces. Track layout and component assembly for this are given in Figs. 4/5. The base of the box also carries the inverter p.c.b. the track layout and component overlay for this is shown in Figs. 6/7. This board also contains three electrolytic capacitors to soak up any voltage variation on the wires to the LD130 caused by large display current variations as explained above.

A twin power supply leaves the inverter board for the A/D p.c.b.; the negative lead going to pin 3 of the LD130, and 0V to the analogue ground connection pin 1 with the battery positive to pin 15 of the LD130 via diode D4.

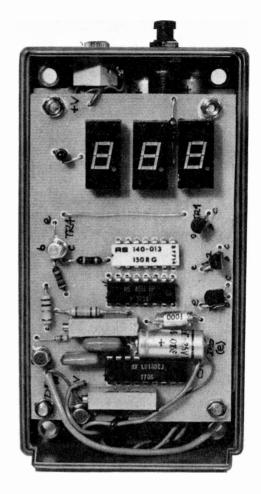
It is recommended that a d.i.l. holder be used for the i.c.s so that thay may be reused unless the constructor has the facilities for desoldering i.c.s in the event of failure. IC1 and IC2 are CMOS devices and need the usual care when handling them, in particular do not solder components in place when power is supplied to the board and do not insert or remove these i.c.s when power is supplied.

# SENSOR

The pn junction temperature sensor is the base-emitter junction of any general purpose silicon bipolar transistor. Both the BC107 series metal can TO18 style and the ZTX300E line types were found suitable.

Using the ZTX300, the collector lead was cut off close to the encapsulation leaving only the base and emitter leads. Single core screened cable, core to base and screen to emitter was soldered to these transistor leads. One connection must be sleeved to avoid shorting.

Quick setting Araldite mixture was smeared over the sleeved and bared connections and the screened cable then threaded through a piece of nylon tubing or similar until the transistor sits tight against one end of the tube. The excess



Araldite was then wiped off so that when the remaining was set it formed a water tight seal against the effects of moisture when the probe is in use.

The other end of the screened cable is terminated in a 2.5mm plug so that it can be plugged into a socket in the box at the side of the push switch. However to save expense the plug and socket can be dispensed with and the lead taken directly to the circuit board.

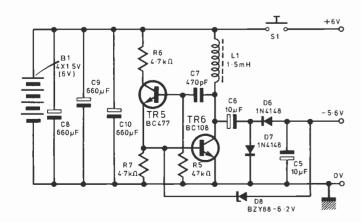


Fig. 8. Inverter circuit



The sensor

# COMPONENTS . . .

# Resistors

R1	82Ω
R2	4.7kΩ
R3	20kΩ
R4	270kΩ
R5	47kΩ (2 off)
R6-R7	4.7kΩ
AH 114/ ca	rhon

# Capacitors

apaoitoro	
C1	0.022µF polyester
C2	0·1μF polyester
C3	100μF elect. 25V
C4	0.001µF polystyrene
C5-C6	10μF elect. 25V (2 off)
C7	470pf
C8-C10	660µF elect. (3 off)

# **Potentiometers**

VR1	2kΩ cermet 20 turn variable
VR2	20kΩ cermet 20 turn variable

# Inductor

1		1	.5m	ш

## Semiconductors

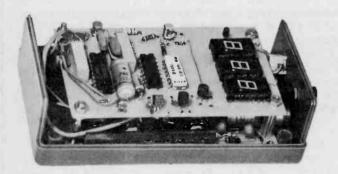
· OIIIIOOIII aa o	10.0
TR1-TR3	MPSA12 Darlingtons (3 off)
TR4	BC109
TR5	BC477
TR6	BC108
D1	TIL209
D2-D3	CRO33 current regulator diode (Siliconix)
D4	1N4148
D5	Sensor diode; ZTX300 (base/emitter only)
D6-D7	1N4148 (2 off)
D8	BZY88 6·2V
X1-X3	MAN3640 (Monsanto) (3 off)
IC1	LD130 (Siliconix)
IC2	CD4511
IC3	7 x 150Ω thick film resistor array
	(Stock No. 140-013—R.S.)

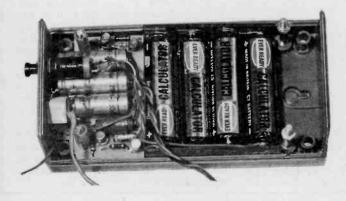
# Miscellaneous

S1-on/o	off swit	ch, 94	4 x 57mr	m (main board)	
42 x 57r	nm (in	ve <b>rt</b> er	board), B	1-6V (4 x 1.5)	V)
2.5mm	plug	and	socket,	polystyrene	case
65 x 20	x 40r	nm.			

# **EXTRACTING THE DIGIT**

Constructors should note that if resolution is not required to the nominal accuracy of 0.1°C, X3 in Fig. 3 can be omitted and the associated driver transistor TR3. Resolution is then to 1°C giving a steadier display which is more restful on the eye and slightly easier on the pocket!





# CALIBRATION

When the boards have been assembled in the box, and all connections checked, the push switch may be pressed whereupon the display will do one of the following:

- (a) Does not light: Check the operation of the switch and all circuit connections.
- (b) Lights and all digits flash on and off rapidly. Adjust VR1 (Range) so that the voltage at pin 2 of the LD130, relative to ground, to 0-35V. This may bring the reading to a steady value, excepting rapid updating of the third digit. If not, adjust VR1 until the display is steady. Place the sensor body in some water at a steady temperature of say 25°C making sure base/emitter leads are not short ciruit. Adjust VR1 until the display reads this value.

Note that due to the operation of the LD130 the display will not stabilise at a precise tenth of a degree reading but will range by as much as  $0.3\,^{\circ}\text{C}$  around the true reading. With experience it will be possible to estimate the temperature to the nearest tenth. Heat some water in another container to say  $75\,^{\circ}\text{C}$  and place the sensor in it applying the same precautions as before and adjust the range potentiometer until the display reads  $75\,^{\circ}\text{C}$ . Return the probe to  $25\,^{\circ}\text{C}$  and readjust VR1 until the display reads this value. Repeat the procedure until the correct temperatures are displayed.

Finally check that the l.e.d. indicating negative temperature lights up when the sensor is in the fridge.

# COMPONENTS

All components are readily available except for the i.c.s and current regulators. Both the LD130 and the CRO33s can be obtained from **Semiconductor Specialists (UK) Ltd.,** Premier House, Fairfield Road, Yiewsley, West Drayton, Middlesex. The Darlington pair MPSA12 digit driver transistors can be obtained from **Technomatic Ltd.**, 54 Sandhurst Road, London NW9.



FRANK W. HYDE

# **OUT OF THE ECLIPTIC**

All spacecraft till now have operated close to the plane of the ecliptic, the plane in which the planets of the Solar System revolve around the Sun. In order to study the higher latitudes of the heliosphere, that is, the environment around the Sun, it is necessary to leave the thin disc of this environment occupied by the planets.

Most of the planets have orbits quite close to the plane of the ecliptic. These are at different angles ranging from approximately 7° for Mercury to 0° for the earth. The exception is Pluto which has an inclination of just over 17°. Thus with this one planet as an exception, the planets are contained in the narrow space at right angles to the place of the ecliptic of 14°.

Since the Sun is in an oblate spheroid, it follows that much of what can be directly viewed is subject to angular distortion, when the observing point is confined to a narrow angle. It is of paramount importance, in an attempt to understand the astrophysics of our own star, that a spacecraft is put in an orbit at right angles, or nearly so, to the ecliptic plane.

To this end the European Space Agency's first deep space mission will be set up, for a launch in 1983, of two spacecraft simultaneously. The launch will be a joint operation with NASA. Designated Out of Ecliptic (OOE) by the European Space Agency and Solar/Polar by NASA, these two spacecraft weighing some 300kg each will be directed toward Jupiter. It is necessary to use the "sling shot" technique to achieve the orbits required. As the two craft near Jupiter, the trajectories will diverge.

One spacecraft will go round Jupiter from north to south and the other from south to north and then toward the Sun, one toward the southern hemisphere and the other to the northern hemisphere. They will be in the vast unknown volume of space round the Sun.

Under certain conditions, the Sun, in addition to the solar wind, emits particles of

very high energy. Streams of such particles are capable of producing "blast" waves in the solar plasma. Lethal gamma-ray bursts could be produced in this manner. It will be possible, it is hoped, to measure the amount of protection that the solar wind provides in inhibiting the intrusion of particles and radiation from galactic sources. From the data acquired by the vehicles it will be possible to discover the precise values for the loss of mass and energy of the Sun. The changes in the acceleration of the Solar Wind can be recorded and related to the other scientific measurements.

The effects of Novae and super Novae are already known in relation to the environment. Recently Hoyle and Wickramsinghe have written on the subject of debris and cometary matter bringing hostile organisms into the Earth's environment. The protection afforded by the high activity of the Sun is a direct effect. An examination of the effects on both Man and the environment can be correlated with the weather and health. This alone would justify the mission of the two spacecraft.

A total of eight experiments will be put aboard each of the spacecraft. One of these is an entirely British package. Dr. Peter Hedgecock of Imperial College is the principal investigator of the project involving a sensitive magnetometer. It is designed to measure the interplanetary magnetic field drawn out from the Sun by the plasma flow. The measurements will be used to provide a map of the Sun's magnetic field in the heliosphere. This will also help to show how lethal radiation is deflected from Earth by the solar magnetic field.

# THE SHIVERS OF THE SUN

In April this year there was a European Conference on Solar Physics at Toulouse. It is remarkable that these conferences suddenly serve as a reminder that, matters obvious, are frequently shrouded in mystery.

The mystery is usually provided by the assessment of the mechanism involved. Yet by the very nature of the body, many photographs and films of the surface show violent and continual activity. Perhaps this is an elaborate way of saying that seeing is not necessarily believing. So it is implied that corroboration is a necessity.

In the matter of the "Shivering Sun" it seems obvious that the internal activities at the temperatures of the elements involved, would lead to a disturbed state. To the three groups of astronomers, who independently came to similar conclusions in this matter some time ago, there must at least have been some considerable satisfaction that their position was unscathed.

It must be said that one of the observers only, saw physical and direct changes. It is certain that more will be heard of this. To be more serious, the phase measurements made by Hill at various frequencies do at least give some clue as to the "ringing" of the Sun.

# **URANUS**

Another star occulation by the rings of Uranus has disclosed that there are in fact, 8 ring systems around this remarkable planet. This observation also disclosed that one of the rings varies in width. At the point where the

ring is nearest to the planet it is narrower than at the point farthest from Uranus. This ring also appears to precess. These observations were made with the 2.5 metre du Pont telescope at Campas Observatory in Chile by Eric Persson of Hale Observatories. The rings are very tenuous for until a star is occulted by them it is not possible to see them with any certainty.

## LANDSAT 3

The first pictures from Landsat 3 show considerable improvement over those of the first two Landsats. The type of imaging on Landsat 3 is different from that on the previous vehicles. The Return Beam Vidicon (RBV) system has now been accepted as a useful tool for the purpose required. Disappointment with Intelstats 1 and 2 was partly due to the system used and also to a degraded camera system. Landsat 3 was launched in March this year and has vindicated the Intelstat project. The RBV system does have a higher order of resolution that the MSS (Multispectral Scanning) system previously used.

The pictures from Intelstat 3 show that objects of 50 metres in length can be resolved and areas of 0.25 hectare. This higher resolution is also accomplished by two cameras instead of four. The two cameras image two adjacent areas of 99 kilometres square. The spectral band width is  $0.5-0.75\mu m$ . Further improvements in coslution were obtained by doubling the focal length of the lens systems on the cameras. Such items as roads, railways and areas like lakes and reservoirs are clearly seen and provide useful information for both Earth resources scientists and resources surveyors.

There seem to be one flaw in the whole matter and that is the objections from the armed services. They seem to fear that too much information is being revealed by way of maps and other means, which may reach unauthorised persons. It is a sad reflection on the integrity of technology when equipment is deliberately degraded in the interest of the services. It seems quite illogical, since what one nation can do another can do also, especially in the matter of observation where the altitudes involved are around 900 kilometres.

# **HALLEY'S COMET**

In previous SPACEWATCH reports Halley's comet has been the object of assessment for a special mission. After the fiscal set-back which seemed likely to kill it years ago there are now second thoughts. NASA has now accepted that it would be a valuable mission. Because of the heavy commitments to EXOSAT and the Large Space Telescope, there may be some hard bargaining.

The new mission is for a two in one project designed to widen the scope of the experiments. A flight past Halley's Comet would be followed by a swing by the Earth and a show flyby of another comet Tempel-2, in 1988. This project would be the first to use solar-electric propulsion, to attain the high velocity which can match the speed of the comets. It is thought that there is a likelihood of the mission now getting under way.

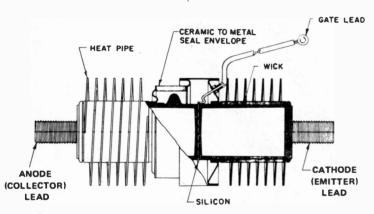
# **News Briefs**

# HEAT IN THE PIPELINE

ONE could only guess what it would be called, but it had to come, and RCA brought it onto the electronics scene. It's called the "transcalent" device, and it's a new class of power semiconductor which uses heat pipes to cool off hot junctions.

These lightweight devices feature integral heat pipes bonded directly to large silicon wafers capable of handling currents of hundreds of amperes. The first devices available include rectifiers, thyristors and transistors.

The integral heat pipes in these devices minimise thermal resistance and increase radiator fin efficiency, thereby permitting RCA to produce semiconductors significantly smaller and lighter than conventional semiconductor/heatsink assemblies of similar power ratings. Typical size reduction is by a factor of four, and weight reduction by a factor of seven.



Transcalent thyristor construction

Other advantages of RCA's heat-pipe/integral-fin construction technique include improved resistance against overloads and high-current surges, and the opportunity either to reduce the silicon-junction temperature for enhanced reliability, or to operate at full ratings at high ambient temperatures.

Installation is also simplified by the elimination of separate heatsinks. The first RCA transcalent devices available are the P95000EB Series of 250A, 500W rectifiers with blocking voltages up to 1,200V, the P95400EB Series of 400A, 500W thyristors with blocking voltages up to 1,200V, and the P95200EE4 100A, 500W n.p.n transistor.

The rectifiers and thyristors use compact radiator structures resulting in a weight of only 340g, and a volume of less than 230 cubic centimetres. The transistor uses a different radiator structure with a dissipation capability of 500W, yet the device weighs less than 1kg and occupies a volume of less than 1,100 cubic centimetres.

Any of these devices can be supplied with radiator structures to accommodate either air or liquid cooling. Thermal resistances are of the order of 0.1 to 0.2°C/W, and operating ambient temperatures at full ratings range up to 50°C.

The transcalent device is appropriate for a wide range of commercial and military applications involving fixed, mobile or aerospace equipment. Typical uses are in welders, electro-chemical platers, power conversion and distributing systems, motor-speed controls, military-vehicle drives, radar power supplies and aircraft power systems.

# **EAGLE'S LAUNCH**

O<sup>N</sup> May 21 Eagle International unveiled over 132 new editions to its range of consumer and industrial electronics products, including new hi-fi, public address, security, business and educational equipment. The biggest ever launch in Eagle's history.

Many of these new products are being displayed at the 1978 Radio Show, where the Eagle International stand is in the Piccadilly Hotel, Piccadilly.

The centre piece of the range of consumer products is 20 new hi-fi separates including five loudspeakers, four amplifiers, three receivers, two tuners, two turntables and a front-loading cassette deck. Eagle are also introducing a number of audio products and accessories, such as headphones, cartridges, table radios, and ribbon aerials. Important additions to the public address range with new disco and group PA systems have also been made.

Among the new products in the security field are domestic burglar and fire alarm equipment, including one single-zone combined fire/intruder panel, suitable for private homes and smaller offices or industrial premises.

Eagle is also introducing five test equipment products including multimeters; three emergency lighting products, two headsets specifically designed for educational purposes, and eight intercoms.

# **NEW MICROPROCESSORS**

NEW 16-bit microcomputer, the Intel 8086, has been formally introduced, and is Intel's highest performer yet, being seven to twelve times faster than the 8080 at program execution. It joins the 8085A and 8048 industry standard micro families, and employs the same software development tools as MCS-80 and MCS-85. To protect the customers' software investment, the 8086 is source code compatible with the 8080A and 8085 via a translator package.

The 8086 provides all the previous features with 16-bit arithmetic, signed 8- and 16-bit arithmetic dynamically relocatable programs; design features multi-processor configuration support, and it can address a megabyte of memory. The standard clock rate is 5MHz (8MHz optional).

The Intel HMOS process has put 29,000 transistors on a chip only 225mm<sup>2</sup> which is better than the average home constructor can manage!

Another new device from Intel is the 8022, and this will be of much more interest to the amateur because it is the first micro with an onboard analogue to digital converter! This most useful addition to the microprocessor is accompanied by an input port which can be directly connected to a "touch-panel" keyboard.

The 8022 has twice the program memory (2 kilo bytes) as that of the 8021. With a dual input A to D converter, variable threshold 8-bit input port of 100mV sensitivity, zero-crossing capability, and an extra test pin for conditional jumps, this microprocessor has to be a device we shall hear a lot more of.

The A to D converter is of the successive approximation type accepting inputs up to 5V, and requires an external voltage reference source.

Machine code instructions select which input is to be used, whilst the converter runs continuously, updating a results register every 40µs. This speed of conversion allows multiplexing of the two analogue inputs, to provide many analogue channels without complex handshaking, or converter stop/start instructions.

Test pin 1 of the 8022 will detect sinewave zero crossing, so that when used in conjunction with mains control, the system can switch power via triacs, etc. at the optimum time for minimum generation of electrical noise. This "symmetrical" zero-crossover switching is also preferred by the Electricity Generating Board.

The 8022 is housed in a 40-pin package, and has an internal clock generator which requires one external component—a crystal or resistor. There are also two high current drive outputs.



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Contact terminals are arranged in sets of five, each connected across the back, and in the Model 203A illustrated you get 1770 contacts, in six rows of  $59 \times 5$ , plus four double power rails, each with 100 contacts connected lengthwise and two horizontal power units with 40 contacts each. Many other models; see chart. Proto-Board breadboards will accept transistors, ICs, LSI packages, resistors, capacitors, LEDs, trimmers, relays etc.; most plug straight in.

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	PB-100	760	10	11.80	1.00	1.02	13.82	Kit—with larger capacity
	PB-101	940	10	17.20	1.25	1.48	19.93	8 distribution buses, higher capacity
	PB-102	1240	12	22.95	1.25	1.94	26.14	Large capacity, moderate price
н	PB-103	2250	24	34.45	1.50	2.88	38.83	Even larger capacity; only 1.73 pence per tie-point
u	PB-104	3060	32	45.95	1.50	3.80	51.25	Largest capacity; lowest price per tie-point
п	PB-203	2250	24	55.15	.1.50	4.53	61.18	Built-in 1%-regulated 5V, 1A low ripple power supply
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0.3" DL 704 & 707/2 59p°	PAK N: 50 x DA81/91	£1	25V 10ea 1/2/7/10		2N3055 90W	29p*
DALO PCB Pen 65p°	PAK P: 20 x P/BC109	£1	47/100/220/500/1000	If£5	2N3055 115W T03	45m°
JACKSON TUNER	PAK R: 14 x BC 107	£1°	SET 4:   Walt 5% CF		2N3819e FET	16p
0-370 pf only £1	PAK S: 14 x BC 108	f1°	Resistors 10 each 10Ω		ORP12	60p°
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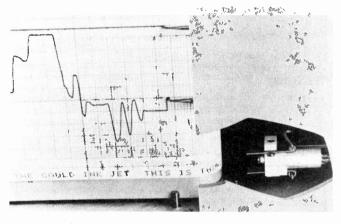
# Mews Briefs

# CHARGED AND ARRESTED

A<sup>N</sup> ingenious system for printing has been employed to produce a unique device for depositing alphanumeric characters on moving chart recorder paper, by Gould Instruments Division.

Primarily intended as an add on unit for their standard "continuous stream" ink chart recorders, Gould have developed this improved system (pictured below) whereby ink is virtually "shocked" into a set of minute uniform particles, and charged to a high potential so that it can be electrostatically deflected along one axis. The position on the paper at which a particular ink particle is arrested will depend upon the potential of the deflector plates at that time.

The characters are described as "highly readable" and are formed on a 5  $\times$  7-dot matrix. They appear along the edge of the oscillograph paper to allow annotations concerning relevant parameters whilst the recording is being made. In some cases this can allow event triggered recording, to save chart paper, with the nature of each trace and event details in juxtaposition. The "ink jet" device is instructed with ASC11 words which can originate from a manually operated keyboard or perhaps a minicomputer system for fully automatic monitoring.



The mechanism works like this: the basic impulse jet consists simply of a glass capillary tube with an orifice at one end, a coaxial piezoelectric driver, and a plastics supply line leading to an unpressurised ink reservoir. The piezoelectric driver is pulsed, and the shock waves squirt a metered amount of ink through the jet, just like a tiny microscopic valve-less pump. This art of obtaining ink particles of consistently equal masses and velocities is important for the next step; which is to charge the particles and electrostatically deflect them with a staircase waveform, and know for certain where they are going to be headed for afterwards.

As the paper advances under the head, the deflection staircase waveform builds up each character in raster fashion (5 rows of 7 dots), the pump "spitting" out (or missing out) ink at the appropriate times, controlled by the electronics.

Some of the statistics are: character width held constant over a 1,000:1 chart speed range (from 0.05mm/s to 50mm/s), achieved through paper/character generator speed synchronisation. The mechanism is silent, and could print on almost anything without damage. A single 10³cm cartridge will print over two million characters.

A real-time clock module is also available for time scale print-out along the oscillograms.

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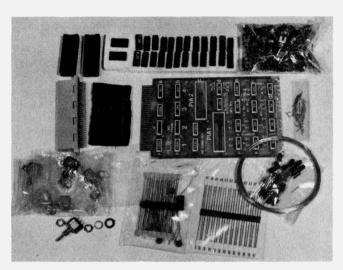
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# MICROPROCESSOR Kit Review ... By P. A. Birnie

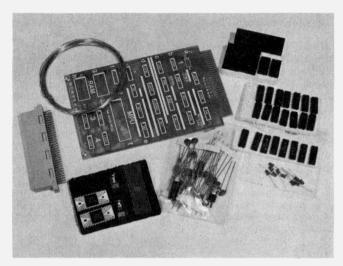


Contents of the CON-COS box as supplied in the kit.

THE APPEARANCE in the market-place of a bewildering number of microprocessors has sparked off the home computer industry—first in the U.S.A. and later in the U.K.—and has resulted in an equally bewildering number of "systems" for the amateur. These range from the simplest "keys and lamps" systems, which are more useful as teaching aids than as home computers, through the hex. keypad/hex. display systems to the keyboard and v.d.u. systems running in BASIC and capable of performing the most sophisticated of computing tasks.

Recent months have seen the emergence of several "keys and lamps" systems from such firms as Ritro and Newbear Computing, and these are designed primarily as a means of "getting started" in home computing while at the same time offering the facility of later expansion to virtually any level of system complexity. The system reviewed here is the Ritro AMI-COS system, which is 6800 based and when operational allows the user to run programs entered by means of keys in hex. machine code, and read out the "answers" on two l.e.d. arrays, i.e. it is intended primarily as a cheap means of getting into microprocessor computing.

As can be seen in the photograph, an array of 16 l.e.d.s and 16 switches allows the address bus to be monitored on l.e.d.s and have addresses entered onto itself by keys. A similar array of 8 l.e.d.s and 8 switches performs the same functions on the data bus. Other switches allow single step or clocked operation, automatic address increment when inputing data, access to the 6800 register, interrupts and other functions. In other words, access is given to all parts of the system to allow the basic principles of microprocessor operation to be rapidly learned and later applied to the solution of problems by relatively simple programs.



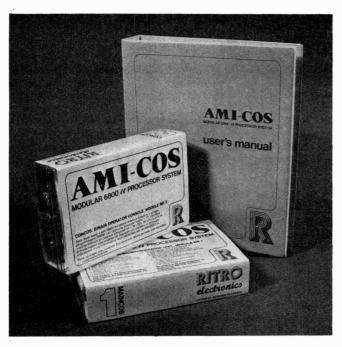
MAIN-COS components as supplied in the kit.

# THE HARDWARE

The kit of parts consists of two plastic boxes containing MAIN-COS and CON-COS and a large thick instruction manual—MAIN-COS being the name given to the circuit module containing the 6800 microprocessor and peripheral circuitry, CON-COS, on the other hand, is a circuit module which interconnects the operation panel and MAIN-COS. Both modules are impressively packed in the appropriate conducting foam or polystyrene packaging and each plastic box is slipped into a sleeve which outlines the contents and overall function of that module, and it is at this point that a problem, which was to recur, came to light. The MAIN-COS sleeve is printed in Dutch and English, but the CON-COS sleeve is printed only in Dutch, which proves no problem with such words as "processor", but rather more tricky when one is confronted with "drukknoppen" (pushbuttons?).

The manual consists of an A.4 sized loose-leaf book about 25mm thick with sections on construction of the MAIN-COS and AMI-COS modules, theory of the 6800, sample program derivation and general background of the devices used in the system. Unfortunately, the manual contains only about 50 pages of actual constructional information, about one half of its total being devoted to a reprint of device data sheets—very useful background, but few constructors will need or want to plough through this material. A section devoted to a very clear explanation of the 6800 instruction set is very well produced and the author found the information was more easily understood than that given in the Motorola Programing Manual.

A further section deals with program writing and associated flow-diagram production; the explanations are very clear and two programs are written from flow diagrams through to machine code listing. These programs, an 8 bit binary to three word BCD convertor and a "running light" program, are subsequently handy as an easy way of checking on correct function of the system when completed. The shortest section of the manual is entitled "General Mounting Directions", and is intended to give guidance on constructional techniques. The advice given is at a very basic level and is obviously translated from some other language, which has caused some amusing "directions" to be given—mentioning a "soldering rod", and requesting that a joint should be kept still "during the hardening process" (please see the footnote concerning the construction section of the manual).



Presentation of the kit including the complete manual.

## **CONSTRUCTING MAIN-COS**

The circuit board used for MAIN-COS is a simple eurocard size double-sided fibre glass board without plated through holes and thus the first task is to make a number of through board connections using the 0.8mm wire supplied. The manual says to cut 149 pieces and link as shown in a photograph of the board. Unfortunately, due to the poor quality of this photograph, it requires considerable care to link all the required holes and not link holes subsequently to be occupied by i.c. legs or component leads, particularly as the figure of 149 seems to be excessive—137 links being used in this prototype. While completing this task, ample opportunity is given to examine the circuit board, which is to a very high quality with a gold-plated double-sided 64 way edge connector and relatively high packing density of i.c.s and a few discrete passive components.

The next activity involves inserting a 7404 inverter package and a "test l.e.d." and probe. This assembly is extensively used during construction, in conjunction with "forcing wires" or earth-connected wires, to de-bug the system as it is assembled. This allows the experimenter, without even a multimeter, to confidently construct the kit—a very helpful idea. Assembly of the board is performed in several stages, each stage being followed by a comprehensive test routine using tables which instruct one to monitor with the test l.e.d. and "force" with forcing wires at specified points, thus checking each i.c. and its interconnections step by step.

The construction of the clock generator in microprocessor systems is frequently a cause for concern, but the AMI-COS module simply uses two back-to-back monostables (74123) with fixed resistors and capacitors, resulting in the prototype constructed by the author, in a clock frequency of 750kHz and a mark/space ratio of about 1:1. This frequency and mark/space ratio can, of course, only be checked using an oscilloscope, so, if the constructor requires a given clock ratio to allow real-timing in software, then he will need to have access to such an instrument.

The final stage in construction involves inserting the 6800 microprocessor and two ROM chips and applying a + 5 volt supply, at which point the processor board tests itself out using a diagnostic program contained in the ROM's. A set of eight small l.e.d.s flashes-through a defined sequence, testing, among other things, data and address lines, RAM locations and the presence of other modules. Failure of any test results in the appropriate l.e.d. being lit, allowing relatively easy debugging of the MAIN-COS module—a very neat solution to the problem of testing microprocessor systems in general, and all the more remarkable for its appearance in a basic system such as this. Assuming the manual has been followed, then the MAIN-COS board should function correctly, and may be set aside pending the construction of CON-COS; Fig. 1 shows a block diagram of MAIN-COS.

## **CONSTRUCTING CON-COS**

CON-COS occupies a second eurocard which again has to have a number of through holes linked, the number given in the manual—92—being correct this time. Again, the picture

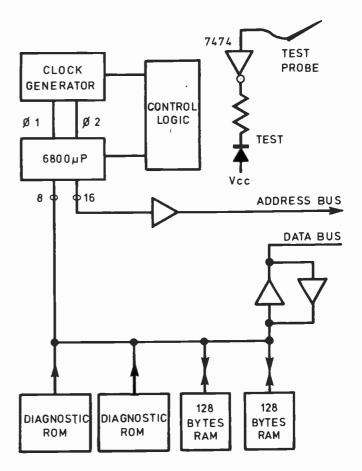
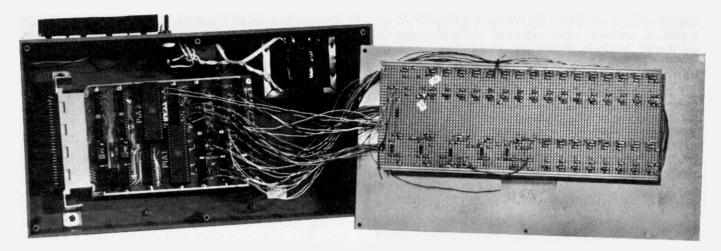


Fig. 1. MAIN-COS block diagram.



Construction of the kit in the Desko case. Veroboard was used for switch and I.e.d. wiring.

showing the positions of the holes is of very poor quality and a diagram would have been much more useful. Construction continues in stages, a test schedule allowing a thorough check to be made of all devices and interconnections. At any rate, this is the intention, but this part of the constructional information is bad, having many errors, causing much cross-reference to the circuit diagrams (see footnote). If the constructor has sufficient ability to overcome these problems, then construction and testing of the board is relatively straightforward and results in a module which controls the interface between MAIN-COS and a front panel—Fig. 2 shows the block diagram of CON-COS.

The final part of construction consists of mounting the switches and l.e.d.s in the CON-COS kit of parts on a panel, or, as was done by the author, on the front plate of a Desko, sloping front case (TEK 364 from West Hyde Developments).

# DATA BUS 8 FRONT PANEL MONITOR ROM PIA PIA ADDRESS BUS

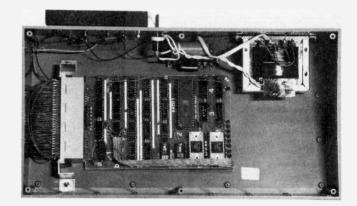
Fig. 2. Block diagram of CON-COS.

The switches and l.e.d.s can either be mounted on a sheet of Veroboard or a printed circuit board which can be obtained as an optional extra from Ritro. The front panel must be connected to CON-COS using insulated wires which are soldered direct on to the board rather than connecting via the edge connector, effectively tying the panel and CON-COS together by a harness of 61 wires. A simple power supply giving 2 amps at + 5 volts must be provided by the constructor to drive the MAIN-COS and CON-COS modules.

## **TESTING AND PROGRAMMING**

Testing of the completed system is carried out in two parts. Firstly, the test program in the two ROMs in MAIN-COS is used in conjunction with the RESET key to check out the system using the eight test l.e.d.s on MAIN-COS. This test program also clears the front panel displays and prepares the system for the second part of the test. This final test is probably best performed using the "running lamp" program—an 18 hex. byte program which causes all l.e.d.s to light except for one, which "runs" along the data and address displays at a rate which can be varied by making small changes to the program.

The program can be stepped through one instruction at a time or at full system clock rate to allow an easy check of the system performance. The author's attempts were rewarded in success, after several "hiccups" caused by errors in the front panel circuit



MAIN-COS and power supply construction.

diagram, which effectively caused some switches to be "upside down" on the panel, so that, for instance, the switch which selects either program counter or index register was inverted when connected "as diagram". In practise, this prevents one easily entering a program as the RAM address of the program bytes is not displayed on the front panel and apparently indicates that the auto-increment of the program counter is not working—all very confusing and the source of several hours of head scratching!

Having sorted out these problems, the system proved very easy to use and seemed reliable, although this aspect of the system is probably more influenced by the quality of construction than by the content of the kit itself.

## **VERDICT**

The purpose of any "keys and lamps" microprocessor system must be primarily to introduce the *newcomer* to microprocessors to the intricacies of what is a complex subject. In this respect, AMI-COS, as presented to us, cannot be said to be a complete success. The circuit boards and hardware are all top quality and the concept of step by step checking, using a built-in test l.e.d., is excellent. The use of the microprocessor to check itself and the system out with the aid of test programs in ROM is similarly a very well thought-out concept, and yet all this good engineering

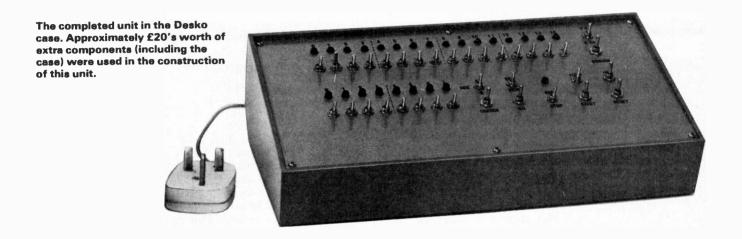
is spoiled by a poor set of assembly instructions.

The system, once constructed, is excellent as a "tutor" in microprocessors, when used in conjunction with the relevant sections of the manual, but, at a price of £166.50 plus VAT, seems expensive when, for only small additional outlay, a system running on keyboard and TV set-v.d.u. could be obtained.

For more information contact Ritro Electronics (UK) Ltd., Grenfell Place, Maidenhead, Berkshire.

## **FOOTNOTE**

As a result of our kit construction and findings concerning the manual, Ritro and Mr. P. Birnie have got together and the construction section of the manual has now been completely rewritten.



## **P.C.B. ASSEMBLY JIGS**

W. ENGLISH

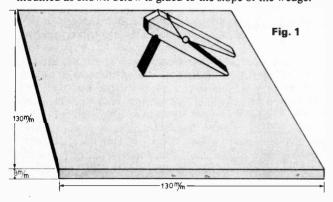
One of the main problems involved in soldering p.c.b.s and stripboard is being able to hold the boards in an accessible position to enable a satisfactory joint to be made.

The two assembly jigs described here show how this can be accomplished with both large and small boards.

## **CONSTRUCTION (TYPE 1)**

A very simple but effective jig for holding small pieces of board is shown in Fig. 1. It consists of a piece of 12mm plywood  $130 \times 130$ mm onto which is glued a wedge shaped piece of 15mm softwood cut to an angle of 30 degrees.

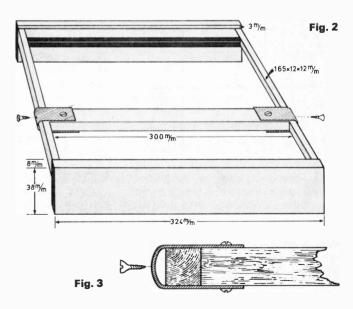
To complete the device, a spring clothes peg with the jaws modified as shown below is glued to the slope of the wedge.



## **CONSTRUCTION (TYPE 2)**

The assembly jig shown in Fig. 2 is capable of accepting boards up to  $300 \times 140 \text{mm}$ . If larger sizes are to be used, then the relevant dimensions can be scaled up.

The board to be soldered is gripped in slots cut into two bars, one of which is movable to take boards as narrow as 20mm. A self-tapping screw through the metal band at each end of the movable bar enables it to be clamped so that the board is held firmly. A detail of this is given in Fig. 3.





# P.C.Bs

## A. R. Damper

ANY readers of P.E. are newcomers to the construction of electronic circuits, and will most probably construct simple projects on tagstrips or Veroboard. It will not have escaped their notice that most large published projects give details of a printed circuit layout. The reason is simply that printed circuit boards (p.c.b.s) are simple to make (once you know how!), and provide a much neater and professional looking endproduct. Smaller published circuits often give a Veroboard layout or no constructional details at all. This article is intended to be a guide for those wishing to make p.c.b.s from circuit diagrams for the first time. Single-sided boards only will be considered. Double-sided boards are mostly used in more complex projects, and when published in magazines, can usually be obtained ready made.

There are two main types of board material to choose from, SRBP and glassfibre. In general applications either may be used, the SRBP being cheaper but not as strong as glass-fibre. In higher quality applications where maximum isolation between tracks is essential, glass-fibre boards are preferable. For small general projects SRBP is quite adequate.

## **AN EXAMPLE**

The object of the exercise is to produce a conductor network on the board by covering, or masking the areas where copper is to remain, and then dissolving away the remaining areas. However, before the tracks can be marked onto the board the layout must be determined from the circuit diagram. A simple circuit (one stage amplifier), provides an example. See Fig. 1.

The circuit is a simple one with no interconnections to other parts of a complex design, enabling the layout on the board to follow the layout of the diagram. Now see how this circuit can be

transformed into a finished p.c.b. The points marked with and "O" represent the need for a hole in the board to take a component lead. At point "A" there are four holes necessary; one for a capacitor lead, two for resistors, and one for the transistor base lead. If the components were now to mystically vanish, Fig. 2 results, and the Os indicate where the holes are to be drilled. This is the general layout and only gives a guide to the track layout.

The resistors are probably low-wattage and can therefore be mounted vertically; consequently the distances between the two holes for Rs need only be about 6mm. However, C2 is an electrolytic capacitor, and for an amplifier having a low pass characteristic, may be of large value, hence large size. The holes for C2 may need to be 50mm apart. So from Fig. 2, Fig. 3 is produced taking into account the component sizes. It is therefore very important that the components are obtained prior to building the board if their size is unknown. Figure 3 still shows the track from the component side of the board and must be reversed to give the layout as it will be etched. To ensure that the input and output are isolated, it is always best to fill in large otherwise empty spaces with conductor, and earth it making sure there is one continuous path to earth. This gives the final full size layout as in Fig. 4, the shaded area being the "filled-in" portion carried out after the main track is applied.

## **METHOD**

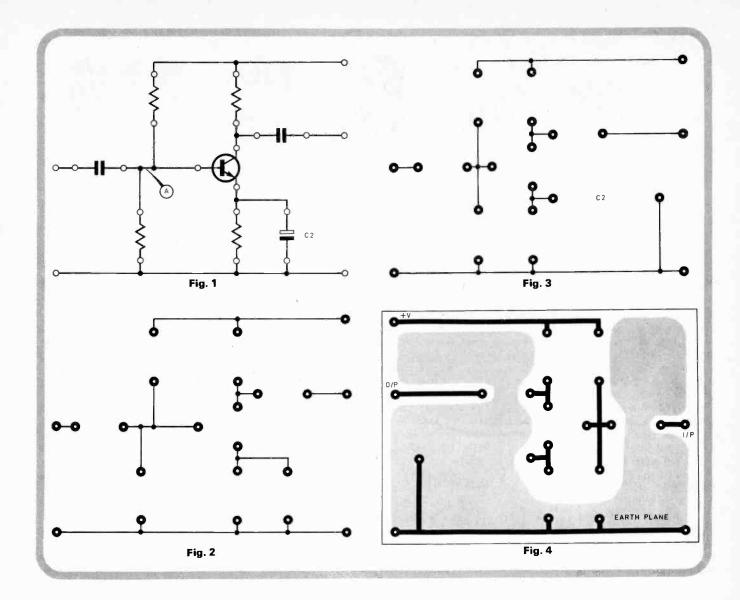
There are quite a few different types of etch resists on the market. In the author's opinion the best board is produced by a combination. Until recently the resist used was painted onto the board (enamel paint and nail-varnish being common), but these did not lend themselves to small scale work such as integrated circuit con-

nections. Then etch-resist pens appeared which enabled the circuit to be drawn directly onto the board, and although they sound fine, the author has found that they often "run" to produce very thick lines unsuitable for fine work. Without running these pens down, the dry transfer system seems the cleanest and simplest method. It is also fairly cheap, and if a mistake is made, the offending line can be scraped off. So, the author recommends that for the main track, dry transfers are used whilst the larger filled-in areas are covered with nail varnish, paint or etch-resist ink.

## **MAKING THE BOARD**

Having worked out the final layout as in Fig. 4 the board can be prepared. Firstly cut from a larger sheet, a piece of copper-clad board of the required size, using a hack-saw with a fine blade and then file the edge smooth. The surface of the copper must now be thoroughly cleaned to remove all grease, dirt and finger-marks. A good method is to rub the surface gently with a cloth after sprinkling a little "Ajax" or similar cleanser onto the board. This is very effective and no trouble whatever has ever been experienced with the fine scratches produced. The board is then rinsed in fresh water and dried.

Dry transfer systems are sold by many P.E. advertisers and complete packs consists of ten sheets, each carrying a different symbol such as lines, drilling points, transistor and i.c. sockets, etc. whilst extra individual sheets are usually available also. It is advisable to buy extra sheets of lines, as these are most frequently used. The author once used Letraset sheets of symbols and line rules, before this system became available, and in certain circumstances such as when fine lines are needed, Letraset is still handy. However, these sheets are more



expensive and therefore only used when necessary. Letraset is useful for applying lettering to the board to identify component positions. If Letraset is included in the masking the etchant should be reduced to around half the normal concentration, as this type of transfer may start to loosen. The p.c.b. transfer system is of course unaffected by the full strength solution.

Working from the layout, the transfers should be applied by placing the required symbol face down on the board and rubbing the backing sheet gently with a bluntish pencil. When transference is complete, the backing sheet is carefully peeled away and the remaining transfer symbol gently pressed onto the copper to secure it. Clean hands are necessary for this operation. Should something go wrong, the transfer can be removed by scraping it off with a finger-nail or blunt instrument.

When all the lines (as in Fig. 4) have been applied, the larger shaded area can

be filled in with etch-resist ink or paint. The board should then be left to dry.

## **ETCHING**

The etching solution used is ferric chloride, which is also obtainable from advertisers in this magazine. The solution is made up as follows. For each pound weight of ferric chloride, one pint of cold water should be added, and placed in a plastics container (a plastics orange juice bottle with the top sawn off is ideal). The ferric chloride should then be added slowly, stirring all the time with a piece of wood or plastics rod. Don't add too much at a time because the solution gets hot, and it becomes necessary to stop and let it cool. Never add water to the crystals, because the heat generated is enormous and the steam produced might shower you with hot ferric chloride, or melt the plastics container. If any ferric chloride gets on your skin, wash the area thoroughly with water. Store the solution in a plastics container with a secure stopper

To etch the board, pour some of the etchant into a shallow plastics or glass tray and lay the board face down on the solution. This allows any by-product from the etching process to fall away from the surface of the board. If the board sinks, or you would rather see what's going on, lay the board face-up in the bottom of the container, but keep the solution moving by gently rocking the container. When etching is complete, remove the board with non-metallic tweezers and rinse in cold water. After drying, the resist can be removed by rubbing the surface with medium or fine grade "wet and dry" paper obtainable at d.i.y. shops. The holes can then be drilled with a 0.8mm drill. Some components will have larger diameter leads and the appropriate drill should be at hand. To give the drill a start, it is useful to mark the position with a centre-punch, but be very gentle otherwise the board may crack.



## **GETTING STARTED**

Delta Distribution is a very new company initially concentrating on power supply transformers, regulators and common i.c.s. Good, fast service is their intention and they are at present setting up mail order and telephone credit services with Access and Barclaycard.

The product range will be expanded as soon as possible and the current price list is available from Delta Distribution Co., 75 Willowtree Ave., Gilesgate Moor, Durham, DH1 1DZ (0385 62760).

## **SOUND ON VISION**

An all British invention, the Videograph, has recently been announced. It converts sound from a record, tape, organ or synthesiser into a display on a domestic colour or black and white TV screen.

Two inputs allow direct display of stereo sound as independent left and right channels, or alternatively a mono signal may be used to feed, for example, low frequencies to one channel and high frequencies to the other.

When used with a colour TV the waves are orange and blue, while the background performs an eight stage colour cycle.

Connection to the TV is directly via the aerial socket.

The Generator Kit costs £12 and the UHF Colour Modulator Kit is £6.95. Cabinet and controls cost £6.95 + £1 p&p.

Ready built units are available at £39.95. All prices include VAT.

William Stuart Systems Ltd., Dower House, Herongate, Brentwood, Essex.

## **AMERICAN COMPUTER BITS**

Another supplier of computer bits and pieces has arrived on the scene; Interam Computer Systems Ltd, who are geared up to service both the hobbyist and small businesses.

As we move further into the "software age" more of these suppliers are sure to pop up, with all sorts of novel odds and ends. Among the literature sent for our perusal by Interam were details of such things as the Cybernetic Systems 1000 Speech Synthesiser. This p.c.b. can be programmed to talk, using standard English and American phonemes, callable using ASCII characters. It is described as a real conversation piece!

Then there is the Newtech Model 6 Music Board which is S-100 bus compatible, and with built-in audio amp and loudspeaker can be programmed to produce melodies, rhythms, sound effects, morse code, touchtone synthesis, and much more.

And yet another American product available from Interam, is the George Risk 753 ASCII Keyboard module with 53 keys on the popular ASR-33 format and 3 user definable keys.

What is PROROM? This is an 8K EPROM memory board with on-board programming circuitry intended to make high programming charges a thing of the past, and made by Mountain Hardware (USA).

Much much more is available from Interam; disk systems, optical tape readers, a Z80 c.p.u. system, software, and many American books and magazines.

More details are obtainable from Interam Computer Systems Ltd, 59 Moreton Street, Victoria, London SW1.

## **ONE-CHIP TV SOUND SYSTEM**

The TDA 1190 is a 12-pin silicon monolithic i.c., mounted in a "batwing" plastic power package. The device which performs all the functions needed for a TV sound system has an audio output power of typically 4.2 watts into a  $16\Omega$  load with a supply voltage of +24V. The TDA 1190 is particularly suited to use with 5.5MHz (PAL) sound systems.

The package provides a FM IF amplifier and detector of high sensitivity which only requires the addition of few extra components and a single tuned coil. AM rejection is excellent; figures of 55dB being typical. An active low pass filter is used to attenuate IF harmonics. Other features include an on-chip audio power output stage and a d.c. volume control.

Although primarily intended for use in TV sets the device can be used in inexpensive FM radios and other FM receiver applications at IF frequencies up to 10.7MHz.

For further information contact Fairchild Camera and Instruments (UK) Ltd, 230 High Street, Potters Bar, Herts.

## **SOLDERING TOOLS**

For many years the name Adcola has been synonymous with soldering irons. "Adcola '78" is a very well produced booklet about the other products manufactured by "The soldering equipment people".

Perhaps initially written for volume production solderers this booklet makes useful reading for any hobbyist.

The advantages of thermostatically controlled "soldering stations" are well documented. Their main improvement over the commonly used "thermal balance" iron is a more rapid rise to operating temperature and an ability to maintain a set temperature during repetitive working.

Among the numerous sizes and profiles of plain copper and iron plated bits is an 80° p.c.b. tip. Iron plated bits oxidise much less quickly than plain copper and are claimed to have a ten times greater working life.

Of particular interest to project builders is a desoldering bit for 14 or 16 pin i.c.s although it does require to be used in a 27–30 watt iron. Adcola also supply an i.c. puller. This is a simple spring loaded extractor used to withdraw i.c.s. from a board after a desoldering bit has melted the surrounding pin solder.

Other desoldering aids are a heated tip with suction bulb, a desoldering gun and various sizes of desoldering braid.

For quick access to both sides of a rigidly held p.c.b. Adcola's Variclamp deserves consideration. This is a lightweight portable holding device which can hold items in any preset position.

The right tools make the job easier and help towards a good finish. The range of cutters, nippers, pliers, shears and strippers gives the craftsman constructor the means of achieving professional quality boards.

Copies of "Adcola '78" and a full price list may be obtained from Adcola Products Ltd, Adcola House, Gauden Road, London SW4.

## TRISTATE L.E.D.

A light-emitting diode which produces red or green emission according to the polarity of the applied voltage is now available from Distronic. Known as the Xciton XC5491, the device uses a back-to-back double-diode configuration which produces red or green light of equal intensity for both colours.

The forward bias is typically 2.2V at a current of 10mA with a dynamic resistance of  $25\Omega$ . The maximum continuous forward current is 25mA for both colours and the operating temperature is  $-55^{\circ}\text{C}$  to  $+85^{\circ}\text{C}$ .

The XC5491 is supplied in a T-1-3/4 package measuring 0.2in diameter × 0.34in height, and is supplied with wire-wrappable leads.

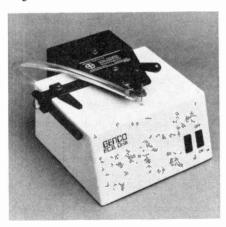
For further information contact Distronic Limited, 50-51 Burnt Mill, Elizabeth Way, Harlow, Essex.

## CHUCKLESS P.C.B. DRILLING MACHINE

A p.c.b. drilling machine operating on a new design system allows inexperienced operators to drill perfect p.c.b.s immediately.

The unit has no chuck and does not require guide bushes for turbo shank tungsten carbide drills.

The drill bits run in vee-blocks at the end of the drill arm allowing extremely accurate running at 15,000 r.p.m. Belt idler pulleys run on ballraces and the mains motor is silent running.



An integral vacuum attachment for efficient swarf removal will optionally accept standard Hoover vacuum cleaner attachments if required.

The ultra lightweight drill arm can be easily raised and lowered to allow modifications to p.c.b.s where components are already in place. The machine will accept drills from 0.35mm to 2mm diameter.

Standard fitments include back stop and side gauge—fully adjustable in both X and Y axis, and a jig to ensure accurate location when fitting drill bits.

The unit cost £140 with accessories and is available from P.B. Electronics (Scotland) Ltd, 9 Radwinter Road, Saffron Walden, Essex.

## STORAGE SCOPE

The new oscilloscope available from Gould Advance, is a general purpose two channel digital storage oscilloscope and waveform digitizer which features several new facilities, including an X-Y display and a sensitivity of 100µV/cm combined with isolation from earth to avoid hum and ground loop problems.

It is based on an 8-bit analogue/digital converter operating at a 1MHz sampling rate into a 1k bit store to provide a -3dB bandwidth up to 600kHz.

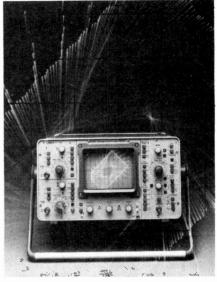
In addition to facilities for displaying the sum or difference of the input signals, the instrument has a comprehensive range of signal conditioning and trigger facilities, including a "trigger-window" feature which is unique in oscilloscopes. In this mode, trigger occurs whenever the input goes outside either of two levels, symmetrically spaced above and below the original trigger level.

Internal trigger sensitivity is equivalent to 2mV of signal at frequencies from d.c. to 1MHz, and external sensitivity is better than 100mV up to 1MHz. Trigger coupling allows selection of d.c. or a.c. with high-frequency and/or low-frequency rejection if required.

An important feature of the digital storage system is a signal delay switch, which inserts a quarter scan length delay into the digital signal path, so that events happening prior to the trigger event may be viewed on the screen.

An 18-position rotary switch varies the speed rate over a very wide range, 100µs/cm to 50s/cm, while an X-expand control offers the facility of expanding the display horizontally, even after storage has taken place.

In addition to the normal dual-channel form of display against a time axis, channel 1 can



be displayed against channel 2 in the X-Y mode.

A split-trace facility is incorporated; in the single-trace mode, alternate samples of the input signal are frozen, so that an image of the signal may be stored and superimposed on the display of the current input waveform.

The digital storage system incorporated in the Gould Advance 0S4100 offers considerable advantages over conventional tubestorage oscilloscopes incorporating expensive limited-life storage tubes. The X-Y facility means that the instrument is ideally suited for looking at transients where more than one variable is involved.

For further information including price contact Gould Instruments Division, Roebuck Road, Hainault, Essex.

## RADIOCODE CLOCK

A clock which has been specifically designed to receive the time and date information which is transmitted by the National Physical Laboratory from Rugby on MSF 60kHz is available from Circuit Services.

By decoding the Rugby signals the clock can set itself automatically within two minutes of being switched on and displays either the time or the date. No subsequent adjustments are necessary because the clock is capable of accounting for both leap years and BST.

Its estimated range is around 1,000 miles and for continental use the clock has an addon-hour facility or alternatively, a modified version can be supplied which receives a similar signal from the DCF77 transmitter at Mainflingen, West Germany. This allows the clock to be used in Eastern Europe where the MSF transmission may be weak.

The unit can be supplied with an alarm/timer module which enables the clock to control other equipment at certain times for precise periods. A record/replay unit can also be supplied which allows the time or date to be recorded on one track of a conventional tape recorder while the other tracks monitor instrument outputs, transients, etc. On replay the recorded time is shown on the Radiocode Clock display. In this mode the clock operates



exactly as if it was receiving a normal transmitted signal. Once the tape has been started on replay, the clock circuitry requires around two minutes to synchronise with the code. After synchronisation has taken place any events recorded on other tracks of the same tape will be timed to within approximately 10mS of their occurrence.

Another advantage of this system is that if the Rugby transmitter should happen to break down during an important recording period, the back up crystal clock will take over and provide an accurate time reference.

For further information contact Circuit Services, 6 Elmbridge Drive, Ruislip, Middx.

## **HONEY AT 2.50?**

The Casio F-100 digital chronograph can display time, calendar, or a stopwatch function. The 1/100th second stopwatch measures net and lap times and can record 1st and 2nd place times.

Timekeeping is  $\pm 15$  seconds per month and gains or losses of up to 30 seconds are easily adjusted by pressing two buttons and zeroing in on a time signal. A complete setting of hours, minutes and seconds takes a little longer.

The calendar display is similarly easy to set, and looks after itself with only the 29th February to contend with.

Although water resistant the watch should not be subjected to swimming, bathing or even car washing. The manufacturers say the display may disappear if kept under constant sunlight but will reappear after normal temperature resumes. Battery life is approximately 18 months.

It is not understood why the function buttons on the watch are coloured grey, yellow, brown and green whereas the user's guide refers to them as B.L.C. and A.

If you want to brush up on your watch knowledge in German, French, Spanish or Italian then Casio's user's guide serves as a miniature Hugo's. Soon, perhaps, the average music centre will have Stoppuhrfunktion: Travail buttons; oxido de plata batteries; and interfaced Luce shows.

The English language and the traditional clock face are disappearing into an oriental



sunset. The last two lines of The Old Vicarage, Grantchester by Rupert Brooke survived the attack by Peter Sellers' cafe waitress but what hope have they against the digital time display.

Stands the church clock at ten to three?
And is there honey still for tea?

F-100, £19.95, Tempus, 19-21 Fitzroy St., Cambridge, CB1 1EH.

## **DAWN CHORUS DEVICE**

Aptly named the Wren, this new quartz movement miniature alarm clock by Smith's Industries is a mere 59mm high.

The hands and hour positions are luminous and the moulded case is available in white with a black or gilt dial, or brown with a gilt dial.

The recommended retail price is £12.90.

## **AMPLIFONE**

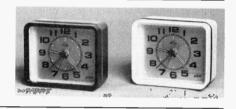
This telephone amplifier fits nearly under a standard instrument and not having any wiring to the telephone can be installed instantly.



Dialling and ringing tones and voices are amplified enabling the caler to hear incoming sound "hands off". The flight deck is simplified to one combined On/Off switch and volume control.

Posted and packed price is £10.

Southern Developments, 120 High Street, Billingshurst, Sussex, RH14 9QS.



## **SHAFT SHEAR**

Manufactured from hardened Swedish tool steel, this guillotine-type tool will cut copper, aluminium, mild and stainless steel, and plastics rod of the following diameters:  $\frac{1}{16}$ ,  $\frac{1}{8}$  and  $\frac{1}{4}$ in, and 3, 4, 5, and 6mm.



Shock and vibration have caused problems when the spindles of sensitive components have been sewn or cut on a lathe; but the Telpro Shaft Shear may be used to cut the spindles of even delicate helical potentiometers, since it does not transmit shock or vibration.

A further advantage is that it gives such a clean, smooth cut that no filing or other finishing operation is needed before control knobs are fitted.

Manufacturers are Tele-Production Tools Ltd., Stiron House, Electric Avenue, Westcliff-on-Sea, Essex SSO 9Nw.

## MINI VICE

This, Design Centre selected vice, needs only a  $\frac{5}{16}$  inch clearance hole in a work bench to give an infinitely positionable third hand. It is an ideal addition to the Home Radio Electronic Workshop (below) and is also supplied by them, at £5.50 + 8 per cent VAT and 85p postage, but post free if supplied with an Electronic Workshop.



## **TRAVEL**

If you have ever been evicted from the kitchen table just as you were getting your project into a "critical" mode you will understand the marketing theory behind The Electronic Workshop. At the first sign of an approaching ketchup bottle the self contained unit can up and away to the safety of the cupboard under the stairs.

The working surface is two feet wide and 20 inches deep. Rubber mat covers the centre area and formica protects the side portions. Pieces of pine 1½ inches high form the outer edges and also double as tool holders.

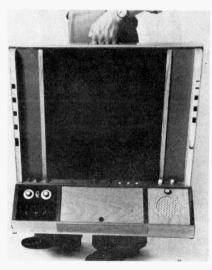
At each end of the back section is a flush 13A shuttered mains socket. The right hand

compartment contains a power pack, giving 0–20V at 1A. The left hand compartment houses a small 35 $\Omega$  speaker and volume control. The centre compartment acts as a tool box and dispenser for reels of solder, plain wire and tinned copper which feed out of three holes into the work area.

The price of the workshop complete, but for wiring up, is £45. Ready wired, £54. VAT and carriage, £4.56.

Home Radio (Components) Ltd. 240 London Road, Mitcham, Surrey CR4 3HD.

Please note that the photograph shows a mark one version which had AC and DC controls on the power supply. The present workshop has a single control.





## DIGITAL THERMOMETER REVIEW

There are many different types of digital thermometer now available which cover a very wide temperature range.

The hand-held types use CMOS technology to ensure low power consumption with either l.e.d. or l.c.d. indication.

The shape and type of sensor depends on the particular application for which the unit is required, i.e. medical, surface, liquid, powder or gas measurements.

## 800 SERIES

This series incorporates twelve different models with a wide variety of thermocouples to cover the temperature range from  $-150^{\circ}$ C to 1,750°C.

To ensure maximum life is obtained from the internal batteries a three position switch: momentary-off-on is used. This facility enables the instrument to be either switched on only for the instant at which it is required, or maintained continuously on. HP7 batteries are included with the unit and rechargeable cells with a charger are available as an optional extra.



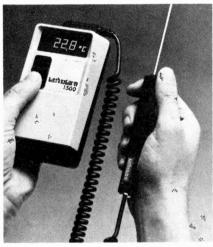
The 8000 series vary in price from £94.00 to £125.00 subject to the temperature range and resolution required.

Further details can be obtained from Channel Electronics Ltd., PO Box 58, Seaford, Sussex.

## THERMISTOR PROBES

The Technoterm 1500 uses precision thermistors with negative temperature coefficients in their probes. This enables response times of between 6 and 10 secs to be achieved over a temperature range of -40°C to 140°C, depending on the type of probe chosen.

A wide range of probes is available to suit most applications. Accessories include nickel cadmium batteries, recharger and a handy dispenser for silicone paste which reduces the response times on rough surfaces.



The Technoterm 1500 is priced at £169.00 and is available from Thermographics Ltd., 16 Canal Street, Congleton, Cheshire.

## **CLINICAL TYPE**

The 4755 has been designed specifically for medical and environmental measurements and is available in two ranges, 33°C to 42.9°C (clinical) and 1°C to 48°C (environmental).

The medical unit is capable of retaining the highest temperature detected within a patient and to prevent cross infection both the instrument and the sensor can be sterilised. To avoid the need for sterilisation after each test disposable sheaths for the sensor are supplied with the unit. The response time of the thermometer is 15 secs with rechargeable cells as an optional extra.



The Digitron 4755 is available priced £92.00 from Digitron Instrumentation Ltd., Mead Lane Industrial Estate, Hertford, Herts.

## **TEMPSTIK**

The Tempstik thermometer has been designed to meet the low cost instrument need and is capable of measuring a temperature range of -100°C to 200°C with reasonable accuracy.

The instrument has a liquid crystal display and is powered from a PP3 battery which is not included.



The Tempstik which is priced at £73.00 is available from Process Measurement Ltd., 8 High Street, Littlehampton, West Sussex.

## **BENCH TYPE**

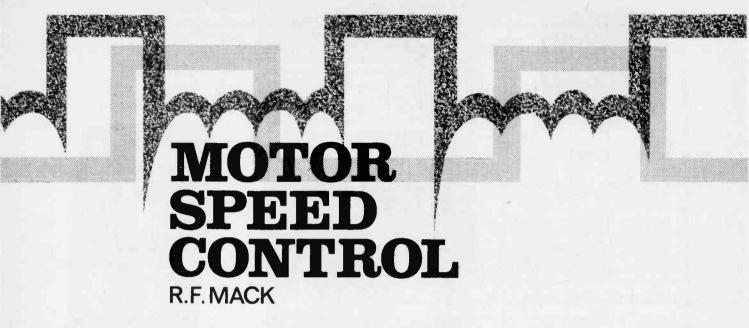
The 7000 series was designed for bench or rack mounted applications and is mains operated. The temperature is indicated on three or four 14mm Sperry gas discharge displays. Thirteen models are available for the temperature range  $-100^{\circ}\text{C}$  to 1,800°C.

All the models in this series can be fitted with an alarm circuit which consists of two totally independent alarm points each having its own relay and front panel l.e.d. The relay contacts which are rated at 240V 2A provide normally open, common and normally closed outputs at the rear of the unit.



The price of the 7000 series is between £109.00 and £149.00 depending on the temperature range chosen.

For further information contact Jenway Ltd., 26 Broomhills Industrial Estate, Rayne Road, Braintree, Essex.



THIS circuit was developed to control the speed of a small model vehicle driven by a permanent magnet electric motor, and provides the following features:

- A wide range of continuous speed control down to about 200 r.p.m. motor speed.
- Substantially constant speed despite changes in mechanical resistance due to inclines, cornering, or surface variation—carpet to lino, for example.
- Substantially constant speed despite changes in electrical resistance—varying track length in a model railway, for example.
- Economical low-speed operation, unlike some opamp based controllers.

## PRINCIPLE OF OPERATION

The controller makes use of the fact that when the permanent magnet motor is temporarily disconnected from the drive battery, it acts as a generator driven by the wheels of the free-wheeling vehicle, with the generated voltage representing the actual speed of the vehicle.

The controller compares this generated voltage with a voltage selected to represent the desired speed, and when the vehicle speed is less than the desired speed the controller momentarily reconnects the battery to the motor.

This process is repeated continuously, resulting in the motor being fed with a stream of fixed magnitude pulses, with a repetition rate governed by the external conditions, as shown in the waveform diagram.

## **CIRCUIT DESCRIPTION**

A voltage representing the desired speed is fed to terminal A. This voltage may be derived in various ways, the potential divider VR1 being shown as an example. Transistor TR1 compares this voltage with the generated voltage from the motor via filter components R9, C3, and switches on TR2 when the actual speed is less than the desired speed. Monostable M1 then produces a fixed magnitude pulse at

## COMPONENTS

## Resistors

R1	10kΩ
R2	10kΩ
R3	39kΩ
R4	39kΩ
R5	470Ω
R6	1kΩ
R7	10Ω 2\
R8	1kΩ
R9	<b>3</b> 9Ω
D10	11.0

(14W carbon except where otherwise stated)

## Capacitors

C1	0.022µF plastic
C2	0.1µF plastic
C3	0.047μF plastic
C4	0.01μF ceramic
C5	0.01µF ceramic
C6	0.01 uF ceramic

## Semiconductors

TR1	BC107	TR4	AD142
TR2	BC157	D1	AAY12 (see text
TR3	BFY50	IC1	SN74123

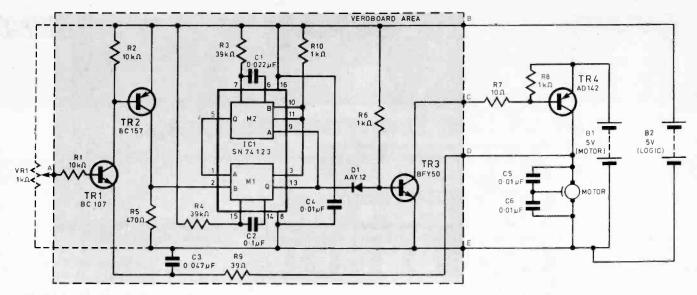
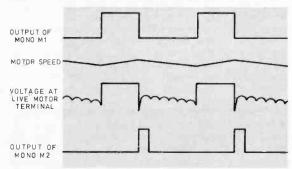


Fig. 1 (above). Circuit diagram; Fig. 2 (below) waveforms



pin 13 of the i.c. and applies power to the motor via TR4, which is an AD142, chosen for its low saturation voltage at high current levels.

Diode D1 is provided to prevent the monostable output terminal from being held low by the base-emitter junction of TR3, and must be a gold bonded germanium component to ensure that TR3 turns off adequately when required.

When the power is removed from the motor inductive effects cause a negative voltage spike at the motor terminal D, as shown in the waveform diagram, so monostable M2 is provided to prevent re-operation of M1 until this back-e.m.f. has decayed and the voltage across the motor truly represents the vehicle's speed.

Separate Nicad batteries were used to avoid interference problems caused by the large surges of motor current and the sensitivity of the TTL monostables.

## **MONOSTABLES**

The 74123 is a dual retriggerable, resettable monostable multivibrator providing an output pulse whose duration and accuracy is a function of external timing components.

There are two inputs per function, one active low and one active high. This permits triggering on either the positive going leading edge or negative going trailing edge of a pulse. Triggering is independent of input transition time or pulse width.

Since the switching voltage requirement for silicon is higher than the germanium with no pulse output from M1, D1 conducts and TR3/TR4 remain off.

With a pulse output, D1 is blocked and TR3 conducts so that TR4 provides current to the motor.

To prevent the pulse period being extended with the appearance of the inductive spike, Q output is routed back

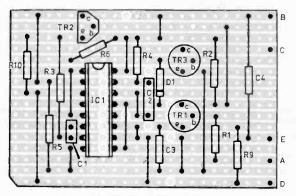


Fig. 3. Board layout

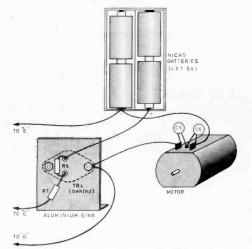


Fig. 4. Component connections to board

to M2 producing a high output at pin 5 which inhibits the Q output of M1.

As can be seen from the waveform diagrams the pulse widths at M1 and M2 outputs have been preset by choice of R4-C2 and R3-C1 respectively, the pulse period being a function of the product of these.

## CONSTRUCTION

All components except TR4, R7, R8, C5 and C6 are mounted on a piece of 0·1in × 0·1in Veroboard as shown. ★

## readout

## ... a selection from our postbag

Readers requiring a reply to any letter must include a stamped addressed envelope.

Opinions expressed in Readout are not necessarily endorsed by the publishers of Practical Electronics.

## Audio compass

Sir—A number of compasses have been, and are being, adapted to provide an audible signal for use by blind yachtsmen. However, none of these provide all the facilities that I, as a blind helmsman, would like to have incorporated into one device.

The device that I want would comprise the following: a unit which will generate an electronic signal indicating the boat's direction, detected by the strength and/or direction of the compass's magnetic field; a calculator-type keyboard to be used to enter desired courses and alterations to them; an audio output stage; and, at the heart of it all, a microprocessor to control and coordinate everything.

I have a good knowledge of programming and a basic knowledge of electronics. But I need help to design and construct this device. If you would like to help me with this, please contact me, preferably by telephone, 01-591 5491 (home) or 01-432 6277.

Kenneth C. Knowles, 3 Sheringham Drive, Barking, Essex, IG11 9AL.

## CB v TV continued

Sir—I read with interest your article "CB Radio" under Industry Notebook in the May edition of *Practical Electronics*.

While one is delighted at the content of the article with regard to the recognition of the TV receiver front end problem and the development of better systems, it is a pity that your last paragraph, re interference, is typical of the uninformed and hysterical comment in the electronic/radio press concerning CB Radio. Over the last year comments like this have caused concern to laymen and authority alike.

Of course the great mass of population would not take kindly to TV interference caused by CB Radio and rightly so. But before you spread alarm and despondency a little investigation on your part would have revealed that interference (or prevention of it) stood high on the list of priorities produced by the CB pressure groups. Indeed their call was for VHF/UHF spectrum with low power (2W) FM. Not the AM/SSB kilowatts on 27 MHz

which has been responsible for the interference problem in other countries.

A. J. Cawthorne, T.ENG(CEI). FSERT. G3TDJ. Bude. Cornwall.

Nexus comments: "As a licenced amateur Mr Cawthorne will be aware of the problems of TVI and of controlling abuses of radio usage however well the regulations are framed and policed. We all start off with good intentions. If, in fact, CB users with kilowatt outputs do exist this proves the point. There is no reason to suppose that British CB enthusiasts, once they catch the bug, will be content with 2 Watts or even 20 Watts. Mr Cawthorne will also be aware that his fellow fully-licenced amateurs, supposedly responsible, are often tempted to abuse their conditions of licence. We cannot assume that CB enthusiasts with on-demand permits, no RAE, and no signed log-books, will be better hehaved."



IC 555 PROJECTS
By E. A. Parr
Published by Bernard Babani Ltd
141 pages 180 × 115mm. Price £1.45

NE of the most versatile i.c.s available to constructors in recent years has been the 555 timer. This book explains the operation of the timer in detail and then describes the basic circuits that can be built around it.

Specific applications for the device are a collection of designs which have appeared in P.E. and other magazines and are given under four headings; model car, model railway, alarm and general circuits.

Variations of the 555, namely the 556, 558 and 559 which are the dual and two quad versions available are also briefly covered. Practical notes are given on how to construct the circuits with tables to determine the values of the timing capacitors. Many readers will find this book useful both for constructing the circuits and as a handy pocket reference book on the 555 timer.

D.J.S.

## OP-AMPS; THEIR PRINCIPLES AND APPLICATIONS

By J. B. Dance Published by Newnes Technical Books 88 pages,  $135 \times 215$ mm. Price £2·25.

S O MANY books published have been along the same lines as this, and indeed on exactly the same subject, that it is perhaps better to stick to the bare facts.

The book has been written for the non-specialist engineer and home constructor. A non-mathematical approach has been adopted, and internal workings of devices area not discussed in any depth; only applications.

The initial three chapters are devoted to the 741 i.c., followed in Chapter 4 by external frequency compensation. Chapter 5 covers f.e.t. input op-amps, and the last two chapters go into i.c.s for audio applications. At the end of the book there is a glossary of op-amp terminology.

Although the original concept of operational amplifiers was that of performing mathematical operations, no devices for performing mathematical functions are included, as part of the author's aim of keeping the book at a simple practical level. There are clear and well printed working circuit diagrams throughout, each with component values given, and anyone seeking to understand operational amplifiers could do worse than read this material, which is an updated version of the *Electronics Australia* series "Op-Amps Without Tears."

M.A.



# PATENTS BEVIEW...

Copies of Patents can be obtained from :
the Patent Office Sales, St. Mary Cray, Orpington, Kent Price 95p each

## SIGNAL CLIPPING INDICATOR

The Sony Corporation has already patented (BP 1 439 241) protective circuit for shutting down an audio amplifier when the impedance value at its output falls below a preset value, for instance due to short-circuiting of the driven loudspeaker. Now, in BP 1 458 857, Sony describes a circuit which will indicate clipping of the output signal as, for instance, may follow from over driving the amplifier into distortion.

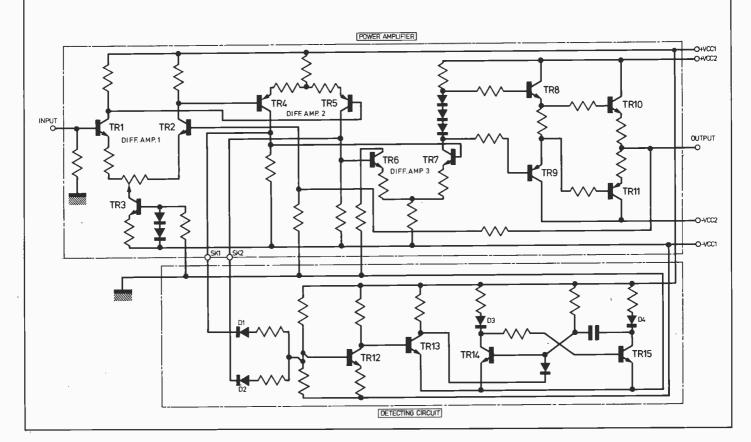
The circuit shows a power amplifier with three differential amplifiers (Diff. Amp. 1, 2, 3) and a push-pull output. The signal path

from the output to the base of TR2 forms an in-phase negative feedback loop. Detecting terminals SK1 and SK2 are connected to the collectors of TR4, TR5 respectively of differential amplifier 2.

In normal operation, similar signals of a few volts are delivered to detecting terminals SK1 and SK2. Transistor TR12 of the detecting circuit is conductive, and hence TR13 is non-conductive. This causes TR14 of the monostable multivibrator to be conductive, and transistor TR15 non-conductive. As a result, the light emitting

diode D3 is energised to emit green light which indicates that the power amplifier is operating normally.

When the amplifier is subjected to excess load or the load is short-circuited or the output signal is clipped, the voltages at terminals SK1, SK2 approach that of the voltage source  $-V_{\text{CC1}}$  for the differential amplifiers. As a result, D1 or D2 is biassed to  $-V_{\text{CC1}}$ , TR12 goes non-conductive and TR13 conductive. D3 extinguishes and the red l.e.d. D4 illuminates, to indicate overload or clipping.



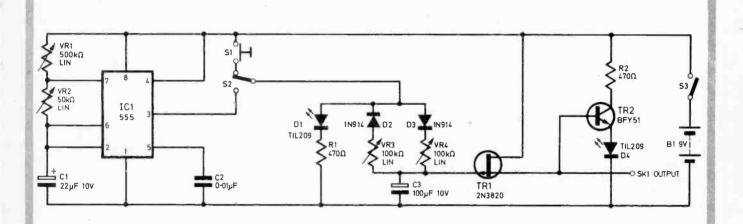


A selection of readers' original circuit ideas. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought.

Why not submit your idea? Any idea published will be awarded payment according to its merits.

Articles submitted for publication should conform to the usual practices of this journal, e.g. with regard to abbreviations and circuit symbols. Diagrams should be on separate sheets, not inserted in the text.

Each idea submitted must be accompanied by a declaration to the effect that it is the original work of the undersigned, and that it has not been accepted for publication elsewhere.



## **ENVELOPE SHAPER**

THE circuit shown above is for an attack/release envelope shaper with automatic triggering.

IC1 is a 555 timer connected in the astable mode with VR1 controlling the duration and VR2 the width of a pulse. No series resistors are used to enable maximum span and flexibility of operation. Automatic triggering is obtained by S2 with S1 used for manual triggering.

The pulse from the output of IC1 (pin 3) is fed via S2 through D3 and VR4 (which controls the attack time) and charges C3 which in turn switches on TR1.

When the pulse is finished C3 is

discharged through VR3 and D2 to D1 and R1. The purpose of D1 and R1 is to form a discharge path for C3 and to indicate when a pulse is applied to C3. The discharge time of C3 depends upon the setting of VR3. As C3 gradually discharges TR1 is turned off.

The cycle of the envelope shaper is monitored by D4 which in turn is controlled by TR2.

To operate, the circuit requires 100 to 200mA and can be driven either by a 9V PP3 battery or a separate power supply unit.

Stephen Trouse, Australia. With only a few components, a modern pH meter (acid/alkali level) can be built using the relatively new RCA 3140T operational amplifier.

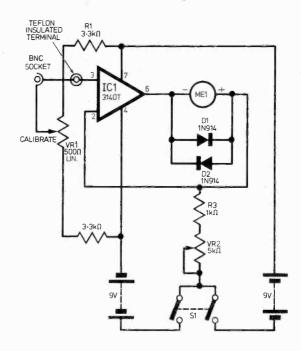
Stripboard is not suitable because of the close proximity of the tracks, and so the TO5 style op amp should be used with its leads spread out and terminated on a good quality p.c.b. with lead 3 of the i.c. soldered to a teflon insulated terminal. From there, a stiff bare copper wire should connect to the input socket.

The meter ME1 can be a cheap  $\pm 100\mu A$  movement and it should be easy to re-mark the scale from 2 to 12pH, with 7pH at the centre (being neutral), or from 0 to 14pH. The unit can be powered from two PP3 9V batteries.

With the electrode in a pH7 solution (distilled water will do) adjust VR1 for a reading of 7. Now place the electrode in a buffer solution of pH4 (acidic solution for calibrating) and adjust for a reading of 4. An alkaline buffer solution (above pH7) could be used instead. The instrument is now calibrated. See P.E. March and April 1977 for pH theory.

Walter Hediger Switzerland

## **pH METER**



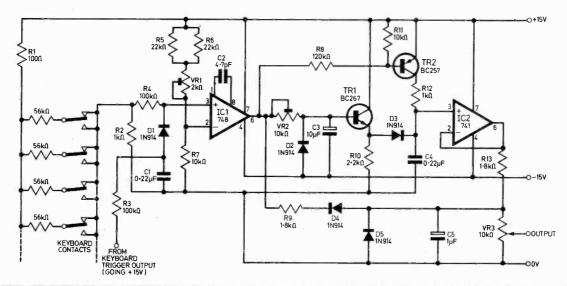
## TOUCH SENSITIVE KEYBOARD

THE circuit described here was designed to provide a synthesiser keyboard with an additional control voltage output, whose magnitude is proportional to the velocity at which a key is struck. This voltage can, for example, be used to control the maximum aplitude which a note attains during the attack time to give the keyboard a piano-like feel, in that it is sensitive to how "strongly" the music is played.

The circuit, shown below, requires an extra set of changeover contacts on the keyboard. IC1 detects when any contact spring is touching neither of its contacts. Thus the output of ICI will switch negative for a duration which is inversely proportional to the key velocity. During this time, capacitor C3 is discharged through VR2 to a voltage proportional to the key velocity. TR2, in switching on, charges C4 to a voltage governed by the charge on C3. The output is prevented from going positive at this time by D4 and D5. When the contacts remake, TR2 shuts off preventing any further charge on C4, whose voltage is now buffered by IC2 and passed to the out-

put. C3 now re-charges ready for the next cycle. This sequence of events is prevented from re-occuring when the key is released by the keyboard trigger signal, which inhibits ICI during this time. VR1 sets up the key detection circuit, and should be adjusted so that the output of ICI gives a negative pulse when a key is pressed slowly. VR2 sets up the velocity/voltage relationship, and is adjusted to give the required output voltage range.

P. R. Williams, Stevenage, Herts.



## CALCULATOR-DECADE COUNTER

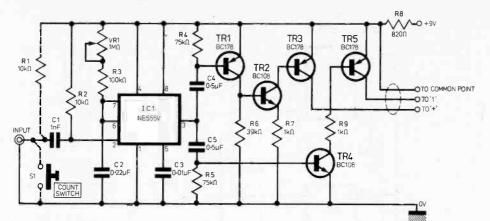


Fig. 1

conventionally-built decade counter A can be rather costly and complicated compared to a calculator with the same digit capability. However, by using the adding function, a calculator can be converted into a decade counter by entering the key sequence 1+, 1+, 1+, 1+, . . . etc. electronically. The corresponding display will then be 1, 2, 3, 4, . . . etc. The given circuit is designed for adding on to the CBM SR 7919D calculator, with part of the calculator circuit board shown, showing the three take-off points required (Fig. 2).

The circuit essentially consists of a monostable multivibrator driving two switching circuits. This circuit operates on an independent supply and it is advised not to decouple the supply with an electrolytic capacitor. When the monostable receives an input, it generates an output pulse of a given duration. The leading edge of this pulse triggers the "1" input while the trailing edge triggers the "+" input; forming the "1+" sequence for a

single input. The time delay of the monostable is made variable by VRI so that it can be set just above the minimum duration at which the calculator counter will operate. Even then the time delay (time between the "1" and "+" input) input) shows to be quite high which means that the maximum frequency input is low. In fact in my set-up, the maximum counting rate is only about 4 per second!

RINTED CIRCUIT-FULL SIZE OF PART OF THE CBM 7919D CALCULATOR CIRCUIT-BOARD SHOWING THE THREE TAKE OFF POINTS REQUIRED BOARD OF CALCULATOR LEADS OF IC ALONG THIS LINE 16 KEYBOARO TERMINALS ALONG THIS LINE TW-17 COMMON POINT

Fig. 2

This counter can be used in applications where low and extremely low counting rate suffices when the time out signal feature of the calculator can be utilised.

For example, by feeding a crystal derived 1Hz input, the counter can be used as a precision seconds timer. Similarly it can be used as a counter for registering the number of people entering a building, etc. by adding the resistor and switch as shown in dotted lines in the diagram.

Furthermore the calculator-counter may be connected to a conventional counter to increase its counting capacity. In this way the inherent low counting rate of the calculator-counter can be compensated. For example, the unit digit of the calculator-counter will become the thousand digit if appropriately connected to a conventional 3 digit counter.

Pek Yaw Kee, Sarawak, East Malaysia.

## CMOS DOORBELL

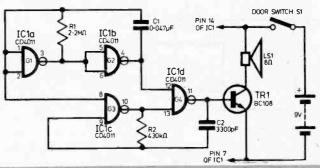
This i.c. doorbell is built around a CD4011 nand gate package, using only a handful of readily available components, and forms two oscillators.

The basic tone for the bell is produced by the high frequency oscillator (G3, G4, R2 and C2), and is interrupted by the low frequency oscillator (G1, G2, R1 and C1). These component values can of course be varied to produce different interrupt rates or basic tone.

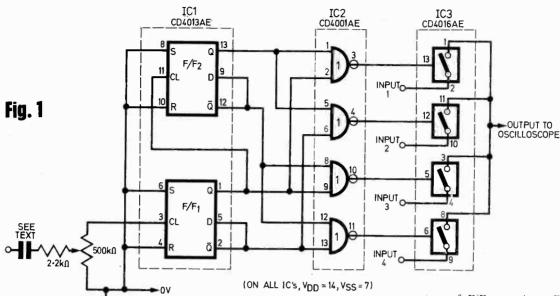
The output is fed to a BC108 tran-

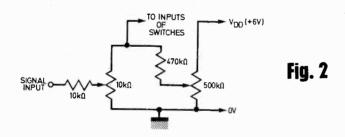
sistor which drives an 80 loudspeaker, and a PP3 battery can be used to power the circuit. The prototype was housed in a plastics case measuring  $116 \times 80 \times 35$ mm.

A. W. Cunningham, Glasgow.



## TRACE MULTIPLIER





This circuit, while using only three common cmos i.c.s allows four separate signals to be displayed on a single beam oscilloscope with independent vertical position and amplitude controls. Instead of using an internal free-running oscillator, this circuit employs the sweep output of the oscilloscope to trigger the switches and therefore displays the first trace on the whole of the screen before displaying

the second in the same way, the switch being triggered by the negative going pulse of the sawtooth wave from the sweep output as it moves back to the other side of the screen.

As the sweep output of most oscilloscopes often exceeds 50V, a series capacitor, series resistor and potentiometer are used to modify the wave and trigger flip-flop. Four sequential outputs are obtained by using the Q

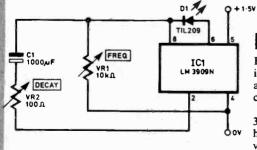
output of  $F/F_1$ , to trigger  $F/F_2$ , thus having  $F/F_2$  run at half the frequency of  $F/F_1$ . Then the Q and  $\overline{Q}$  outputs of both flip-flops are connected to the inputs of four NOR gates as shown, whose output only goes high when both inputs are low. The outputs of the four gates therefore go high in sequence and trigger the electronic switches which allow the four inputs into the oscilloscope one by one.

Each input, before reaching the switches must be attenuated to a useful amplitude relative to the others, and also must be given a different height on the screen to the other traces. This is achieved by the circuit in Fig. 2, which must be repeated for each input. For this reason, it is best to use preset potentiometers as eight normal potentiometers would cost more than the CMOS circuitry itself.

It may be necessary to use a different capacitor on the input from the oscilloscope's sweep output, but this depends on the voltage range of the output. We have found that a  $0.02\mu F$  200V capacitor works admirably where the sweep output is 100V peak-to-peak.

A. Hetherington, Nevilles Cross, Durham.

## LED FLASHER



FLASHING l.e.d. indicators are most often used to indicate a hazard. But there are times when a rather less insistant winking indication, would be appreciated, indicating to proceed at caution.

This circuit which uses an LM 3909N l.e.d. Flasher/Oscillator i.c., has a pulse frequency that can be varied by VR1, from 10-60 pulses per minute.

With the decay control VR2 set to zero, the time of each pulse of light from the l.e.d. corresponds to the discharge time of Cl, this discharge time can be lengthened, by increasing the resistance by means of VR2, between the positive of Cl and pin 2 of the i.c. So that each pulse of light fades away instead of switching abruptly "off".

Decay time of up to 1 second can be obtained with the components shown. It should be noted that a long decay is not possible with a fast frequency.

> M. Miller, Reading, Berks.

## 12v CONVERTER

## for Weller TCP 1&2 Irons

## D. J. BRADBURY

W HEN working on an automobile electrical system it can be very useful to have a soldering iron that will operate from the vehicle's battery. This relieves both the inconvenience and possible hazards involved in arranging external supplies such as a main extension lead.

The unit described in this article is a 12V to 24V d.c. converter designed to supply Weller TCP1 and TCP2 temperature controlled soldering irons from a standard car battery. The converter is housed in a small die-cast box which will also serve as a stand for the iron when it is not in use

## **CIRCUIT DESCRIPTION**

A 24V Weller iron consists of a 45 to 48W heating element in series with a magnetic "Curie" effect temperature switch. Because of this switch the iron only takes current when the soldering bit falls below its correct operating temperature. Thus to work efficiently the converter circuit must be able to supply 50W to the soldering iron and yet take minimal quiescent current when its load is open circuit.

The circuit shown in Fig. 1 achieves both these aims, operating at an efficiency of over 80 per cent whilst the iron is warming up and taking only micro-amps when the iron reaches its correct temperature.

When the circuit is connected to a battery and the soldering iron plugged in, bias current is fed to the base of TR1 via the transformer T1, diodes D1, D2 and the iron. This starts to turn TR1 on, causing its collector voltage to fall, enabling the transformer to increase the voltage applied to the load. The load thus biases TR1 on harder until the transistor finally saturates, giving a peak voltage of approximately 28V across the soldering iron.

While the transformer has a voltage across its windings, a magnetising current slowly builds up until the ferrite transformer core is saturated; it then rises rapidly as the core loses its high relative permeability. When the collector current of TR1 reaches about 10A, the transistor no longer receives sufficient base drive to remain saturated and so its collector voltage begins to rise. This causes the load voltage to fall, reducing the base drive of TR1 which further reduces the load voltage and by this feedback action the transistor is turned off

When TR1 is turned off, its collector voltage rises rapidly above the supply due to the magnetising current flowing in the transformer. Also the output voltage of the transformer goes negative, reverse biasing diodes D1 and D2, so isolating the transformer from the load. The magnetising current causes the unloaded transformer to 'ring' for half a cycle at a frequency mainly determined by its inductance and the value of C1. The high voltage half cycle 'ring' reverses the flow of the magnetising current and as a result defines the length of time for which TR1 does not conduct.

This period must be kept short if the converter is to be efficient. However, the shorter the time the higher the voltage required across T1 to reverse the magnetising current. Since part of this voltage appears across TR1 a compromise was chosen for the converter that gives the

## COMPONENTS . . .

## Resistors

R1 1Ω 2.5W wirewound

## Capacitors

C1 0.047μF polyester C2 150μF 16V elect.

## Semiconductors

D1, D2 ZS271 (2 off)
D3 1N5401
TR1 BD243B

### **Transformers**

Length of 22 s.w.g. enamel covered copper wire Bobbin (type DT2205, ITT Part No 52352B) Ferrite pot core (type FX 2241, ITT Part No 52707B)

## Miscellaneous

\*4mm banana sockets (2 off)

\*3 pin 1-5A Bulgin P430 socket
Diecast box 120 x 95 x 30mm
Support spring (Weller SK185, ITT Part No 66304X)
Funnel (Weller SK1527, ITT Part No 18668E)
FS1 Fuseholder Bulgin F55 with 5A fuse

\*See text



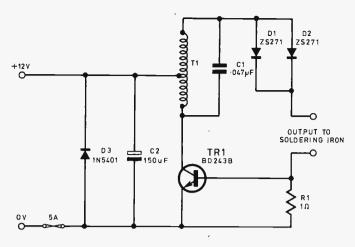


Fig. 1. Circuit diagram of the Converter

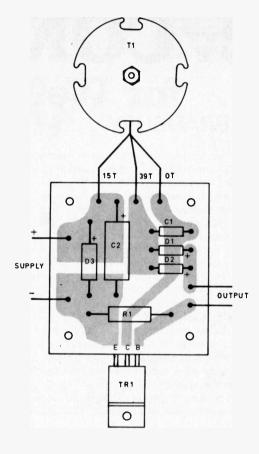


Fig. 2. Printed circuit board design

transistor a peak collector-emitter voltage of 55V during its off period which lasts for about 25 per cent of the full oscillation cycle.

When the magnetising current flowing in T1 is finally reversed, the output voltage of the transformer swings positive and turns TR1 on again thus starting another cycle. The converter continues to oscillate in this manner, feeding 24V r.m.s. to the soldering iron until its working temperature is reached and the magnetic switch opens.

As the bias for TR1 is supplied through the load, when the temperature switch opens the converter ceases to oscillate. In this condition the only current taken by the circuit is the leakage in TR1, C2 and D3, the sum of which is very small.

When the iron cools, the magnetic switch will close, and so the converter will reheat the bit. The unit will thus operate intermittently, maintaining the soldering iron at its correct working temperature.

The diode D3 has been included in the circuit to protect the converter against reverse polarity connection to the battery. Normally the diode is reverse biased and so it draws little current from the circuit. However, if the supply connections are accidentally reversed the diode will take a heavy current and blow the 5A fuse before the converter circuitry is damaged. Although a series diode would have the advantage of saving the protection fuse if the battery polarity is wrong, it was not used in this case as it would have to pass a current of 5A under normal operating conditions and so for a silicon device would nearly double the power losses of the converter.

## CONSTRUCTION

The prototype was constructed using the printed circuit board layout in Fig. 3 with the component overlay shown in

Fig. 3. Component layout and wiring diagram

Fig. 4. If the printed circuit board is to be traced, constructors should remember that the copper tracks will carry high currents and so it is recommended that the diagram is followed closely, keeping the tracks as wide as possible.

Once the board has been etched, cleaned and drilled, the components and lead out wires may be soldered. The supply input leads should be fitted with large crocodile clips for making connections to the battery. Although the power dissipation in TR1 is not very high, it is necessary to mount the transistor on the converter box to keep the device within its temperature ratings. To facilitate this, the transistor is soldered to the back of the printed circuit board with its leads left long so that they can span the gap between the box and the circuit.

The transformer for the converter consists of a 39 turn coil wound with  $0.71 \, \text{mm}$  dia. (22 s.w.g.) enamel covered copper wire mounted inside a 30mm dia. ferrite pot core. The coil should be neatly wound in layers on the plastic bobbin with a tapping taken 15 turns from the start of the winding. As the converter oscillates at a frequency of about 4kHz, the transformer can be the source of an annoying audible whistle. To minimise this, when assembling the pot core halves smear a thin layer of grease on the mating surfaces to dampen core vibrations.

The transformer is fastened to the converter box using a 1in. long countersunk 2BA bolt with nut and spring washer. The spring washer should be placed between the box and the transformer as in this position it acts as a vibration insulator. Do not overtighten the retaining nut as no advantage is gained by doing so and it could result in breaking the brittle ferrite cores.

The 120 imes 95 imes 30mm die-cast alloy box used to house

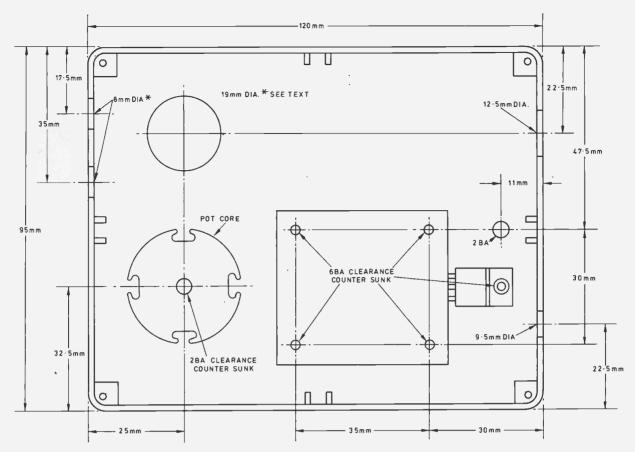
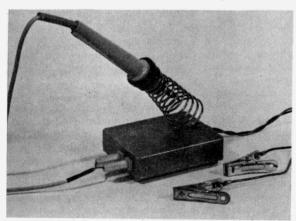
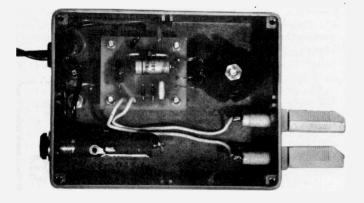


Fig. 4. Case drilling and mounting details





the converter was drilled to the dimensions shown in Fig. 4. Since the two Weller irons have different connector arrangements the diagram includes the holes for both types of sockets.

The position of the hole to mount TR1 is not given in the diagram as it will depend on how the transistor was soldered to the printed circuit. The correct location can be found by placing the component board in position inside the box and marking the hole through the transistor tab after having checked that the device is lying flat. When the transistor is mounted it should be electrically insulated from the box by using a mica washer and plastic bush.

## **TESTING**

Having completed the converter and checked its wiring, plug in the soldering iron and connect the unit to a 12V battery, being careful to observe the correct polarity. The converter should emit a soft whistling sound and the following voltages may be measured from the negative end of C2 using a moving coil voltmeter. TR1 collector  $\pm 12V$ , TR1 base  $\pm 0.8V$ , soldering iron output  $\pm 20V$ .

If there are any serious discrepancies in the voltage readings, disconnect the battery and recheck the converter for faulty components, dry joints and wiring errors. In cases where the converter cannot be heard to oscillate and all the voltage readings are zero, check the fuse and the battery polarity. Never use fuses rated at more than 5A or those with "slow blow" characteristics as they may result in damage to D3 or TR1 under fault conditions.

If the converter is operating correctly it should oscillate for between 1 and  $1\frac{1}{2}$  minutes from switch-on, after which time the soldering iron will have reached its working temperature and the soft whistle will cease. The converter may be occasionally heard as it reheats the bit.

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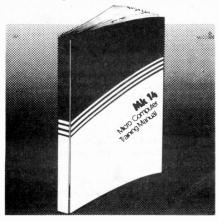
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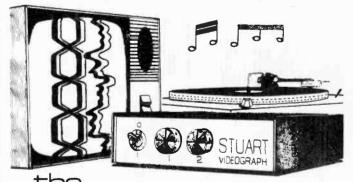
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## Semiconductor UPDATE...

FEATURING MD4301 AD3500

R.W. Coles

## **ALARMING DEVELOPMENT**

One of the problems of using modern large scale integrated circuits is that we, the users, have become obliged to surrender a lot of our design independence to the semiconductor manufacturers.

To ensure volume sales of their chips, the manufacturers tend to build devices which are aimed at the widest possible market, and we, as willing customers, have had to forego some of the "oddball" applications that we could indulge in when using discrete transistors and individual amplifiers or logic gates.

Of course, a ray of hope is visible in the shape of the microprocessor, but unless you happen to be a confirmed "Micro-nut" there are still many fearsome obstacles to deflect you from that path, not least 'the cost of it all.

When you think about it, the bastions of the LSI industry are calculators, clocks, microprocessors, voltmeters, and TV games, and precious little else. Not exactly a fertile ground for the amateur who wants the benefits of LSI but who can cope with only so many variations on the digital clock theme before trading the whole lot in for a pair of beam-tetrodes and a 50-Watt soldering iron!

The point I am trying to make is that any original large scale integrated circuits that do turn up deserve a rousing welcome from our beleaguered band, and this month I have managed to turn up a beauty!

I refer to the MD4301, from the Canadian firm of Mitel, (no—don't groan, you can get them from Rastra Electronics Limited!), which is unassumingly labelled a "CMOS Alarm Circuit." Inside its tiny fourteen pin plastic package, the MD4301 has an amazing array of odds and ends which enables it to act as, among other things, a complete fire alarm system with all the practical bits and pieces you would design in yourself, given the chance.

There is a comparator circuit, which will trigger an alarm condition for a 150mV voltage differential between its two inputs.

There is an audio oscillator which is turned on by an alarm condition, a 300mA switch output to drive a horn or siren, and a

separate pulsed l.e.d. driver for local poweron indication.

There is also a "low-battery" detector which gives an unobtrusive but hard to ignore output of 50 milliseconds each minute on all alarm outputs when the battery voltage gets too low for comfort, (which shouldn't be too often, because the standby battery drain is a miserly 25 microamps!)

There is an alarm trigger "in" and "out" which allows any number of MD4301 circuits to be cascaded so that any one active unit can trigger all the others for a full scale fire alert, and other variations and options too numerous to mention.

To use the MD4301 in a self contained fire alarm system, you need only hook it up to an ion chamber smoke detector cell, a nine volt battery, a horn or siren and a few discrete components. A much more exciting and useful prospect than building yet another digital clock!

## 31 IS TWICE AS GOOD AS 3

Some time ago I featured a 3 digit single chip voltmeter device in this column, and suggested that the traditional moving coil meters with their inherent fragility and accuracy limitations would soon be losing ground to the newcomer. A new chip from National brings the demise of springs and jewelled bearing even closer. They have managed to cram a complete  $3\frac{1}{2}$  digit voltmeter system on to a single LSI chip, a system which up to now had taken at least two chips, and usually many more, to implement.

A 31 digit display is actually twice as

good as a 3 digit display because you get a full scale output of 1999 instead of 999, double the dynamic range and precision of earlier single chip systems.

The new chip is coded **AD3500** and it contains not only the digital conversion circuitry but also the l.e.d. segment drivers, the system clock and the analogue "front end".

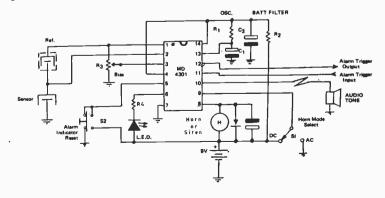
The chip uses low consumption CMOS technology and runs from a single plus five volt supply, so building a digital multimeter with the AD3500 should be child's play!

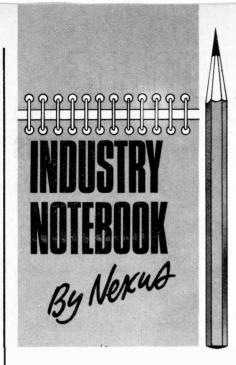
To build a complete voltmeter all you need to add (apart from some kind of power source) is an l.e.d. display, a low cost 75492 digit driver, a voltage reference, and a handful of discrete resistors and capacitors—the whole thing could be fitted on to a circuit board about 8cm square.

The addition of a range switch and a few extra resistors would allow a full complement of voltage and current ranges, and with a constant current source added, resistance ranges would be possible.

If you wanted to be really cunning, you could use the over-range outputs provided by the AD3500 to control an auto-ranging system which did the range changing for you using reed relays or solid state analogue switches, very useful for handsfree trouble shooting!

In terms of accuracy, the new device beats the moving coil meter hands down with a  $\pm 0.05$  per cent specification. You will probably degrade that figure with your external components of course, but the traditional meter is hard pressed to deliver even 2 per cent accuracy!





## The Pay-Off

Further to my recent reports on overseas investment, especially in the United States, it is worthy of note that Racal has now formed a Data Communications Group headed up by D. Leighton Davies. Leighton, a B.Sc.(Hons) graduate from the University of Wales, was ten years with Solartron and in senior positions with GEC Computers and Automation, and STC, before becoming managing director of Racal-Milgo Ltd in 1969, then a tiny UK operation owned 50/50 by Racal in the UK and Milgo Inc in the USA. It was virtually a marketing company set up to exploit Milgo products outside the Americas.

First-year turnover was in the tens of thousands of pounds. Now, less than ten years later. Leighton heads up a wholly British-controlled data communications group of world standing with a predicted £75 million profitable turnover in the current financial year and operating from manufacturing, systems engineering and marketing bases in Reading, Frankfurt, Tokyo, Miami and Sunnyvale, and through an associated company in Rio de Janeiro and Brazilia. The present huge boost in turnover came from Racal's recent acquisition of Milgo Inc and Vadic Inc in the USA and further acquisitions are being sought.

Just one example explains what overseas investment is all about. Racal-Milgo Inc, Miami, Florida, has just signed a contract with Eastern Airlines for a System 200 Management Centre to streamline Eastern's data network covering 300 locations in North America and the Caribbean. As well as the Management Centre (which monitors and controls a network of up to 16,256 communications devices and modems on as many as 64

channels) the Eastern Airlines contract includes orders for hundreds of high-speed modems. No British company confined to a UK base would have been considered for such a contract, let alone win it. The Eastern Airlines contract plus many others in the US is a pay-off for Britain.

It works in reverse, too. North Thames Gas would not have bought £120,000 of equipment to improve its data links from a company based solely in Miami, Florida. But North Thames Gas were very happy to contract with Reading-based Racal-Milgo with its full local engineering support, even though a percentage of the equipment is built by the now British-owned Racal-Milgo in the USA. For this type of business you need to be on the spot.

## Outlook

Public opinion polls are not invariably reliable but a recent poll of electronics goods manufacturers has shown a downturn in optimism (as distinct from downright pessimism) on future prospects, especially in exports in the capital goods sector where a number of respondents are clearly suffering the effects of stronger foreign competition. Paradoxically, except for the hard-pressed consumer sector, the great bulk of returns showed increased business and general buoyancy. Best sector of all is automatic test equipment (ATE) with a boom in the home market, perhaps because of the shortage of good test engineers as well as their cost, and of course it is much easier to introduce laboursaving equipment into the progressive electronics industry than into moribund industries where job protection is a worker obsession, perpetuating out-moded

Apropos my remarks in earlier paragraphs on overseas investment, there is still plenty of movement at home too. Racal, already mentioned, is spending £1.5 million on microelectronics development, Pye has just completed a £5 million complex housing 1,200 workers for mobile radio, Decca Communications has acquired the whole of the h.f. radio business of Granger Associates of California, and English Electric Valve has added 100,000 sq. ft. of manufacturing space through purchase of the former Marconi-Elliott i.c. plant at Witham, Essex.

## **Poland Buys British**

The controversial Polish order for British shipyards, heavily subsidised by the taxpayer, has turned up trumps for Redifon who landed the contract for all the electronics packages on the 22 ships involved. Redifon has undertaken to plan and commission all the equipment, together worth many millions. For starters Redifon will supply 44 of their new R1000 Series communications receivers worth,

possibly, £5,000 or more each, and this is just the fringe.

Decca Marine has also done well in the Polish market recently by contracting £330,000 worth of Decca Navigator receivers and plotters to the Polish fishing fleet operating in the Baltic. There are now some 500 Polish ships fitted with the Navigator. The Japanese have also recently contracted to expand their Decca Navigator coverage with new chain stations so that all four major Japanese ports will now have Decca coverage.

## **Employment**

I note that the IEE Annual Report comments on the scale of recruitment advertising in the past year, so high that special recruitment supplements had to be issued with the Institution journals. Anticipated revenues from situations vacant adverts were handsomely exceeded and a total of £1,000 a day was received in the year from this source.

The shortage of engineers is tending to push up salaries and I notice far more firms offering posts in the £5,000-£7,000 bracket than formerly. But is this enough when one reads that a London bus driver can make £6,000 a year plus perks like free travel? Glancing through the ads the cash plums are still overseas provided you can put up with the climate and general conditions. Up to £21,000 in Libya, £20,000 in Iran, £18,000 (tax free) in Saudi Arabia.

Such salaries are only for senior people with long experience on major products but even scaled down to average engineer level it seems overseas salaries in the Middle East are still more than twice that which can be earned at home and nearly all carry tax concessions.

More of the gentle sex are entering engineering but it is still a mere trickle. Of 190,000 chartered engineers registered in the UK there are only 200 women, less than half of whom work in industry. Of the women I note that the three senior ladies on the secretariat of the Electronic Engineering Association are all designated in the Annual Report as Ms whereas none of the men, not even the Director, is dignified by Mr.

## **More on Mats**

The French company Thomson-CSF is also in the field of mobile automatic telephones (MATS) and claims to have 8,000 subscribers world-wide using their equipment linked to public or private telephone exchanges. Their new microprocessor-controlled car telephone has a capacity of 16 pre-programmable numbers of up to 24 digits each. There is clearly going to be keen competition for this fast-growing business.

## MICRO-EUS

## Compiled by DJD

Appearing every two months, Micro-Bus will present ideas, applications, and programs for the most popular microprocessors; ones that you are unlikely to find in the manufacturers' data books. The most original ideas will probably come from readers working on their own microcomputer systems, and payment will be made for any contribution featured here. This is also the place to air your views, in general, on this new technology, so let's be hearing from you!

## SCOPE FOR GRAPHICS

OSCILLOSCOPES were used for troubleshooting with the earliest computers, and so it is hardly surprising that they soon became permanently connected as a convenient way of displaying drawings produced under computer control. Since then the CRT has remained the most widely used peripheral for high-speed graphical output.

An oscilloscope can only display a single point at a time, so to present a line or a picture it is necessary to refresh the scope by repeating the same sequence of movements of the spot over and over again; at least 30 times a second if the picture is to be seen without flicker. There are two main wavs of controlling the spot from a computer, and both will be covered here. One is to store the coordinates of every point to be displayed in memory, and use these to drive the display. The other method is to generate the individual point co-ordinates as they are to be displayed from a "display file" which contains shorthand commands for drawing lines, circles, characters, etc. A program illustrating

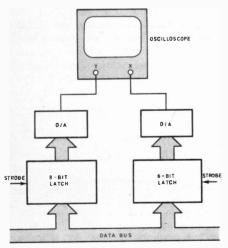


Fig. 1. Block diagram showing the circuitry needed for a microprocessor-controlled graphics display using an oscilloscope.

this approach will show how lines can be generated given the co-ordinates of their endpoints.

## SCOPE INTERFACE

The configuration needed to control a CRT from a computer is shown in Fig. 1. The two D/A converters determine the number of possible point positions; with two 8-bit D/A converters one can display any point on a 256 × 256 grid. The outputs of the D/A converters drive the X and Y inputs of the scope, and these should be d.c. coupled. Since there is no need for timebase circuitry or for sensitive input amplifiers it should be possible to construct a suitable display quite simply. The prototype used two Ferranti ZN425E 8-bit D/As, and these were interfaced to the microprocessor by two 8-bit latches and some addressing circuitry; alternatively a MC6820 PIA could have been used.

The program in Fig. 2, which is for the M6800 micro, illustrates the method of generating a display from the co-ordinates of



Fig. 2. Program for the M6800 which displays co-ordinate pairs from memory.

every spot position. BUFFER is the address of the list of co-ordinates, and with the list shown the program will display a short diagonal line from (0,0) to (4,4). In this and the next program the D/As are assumed to be located at addresses \$8100 and \$8101. If a

PIA is used to interface them with the micro a few instructions will have to be added at the start of the programs to configure it correctly.

## INTERPOLATION PROGRAM

This method of storing the co-ordinates of every spot position really eats up memory; to draw a square border around the screen would require about 2k bytes of memory (1,022 coordinate pairs). It has the advantage that any arbitrary drawing can be displayed; however most graphs and diagrams can be broken down into a number of straight line segments, so a far more economical approach is to store only the co-ordinates of the endpoints of the lines in memory, and generate the points in between as they are needed. Lines other than diagonals or horizontals and verticals cannot be exactly represented on a square lattice, so the program must generate the best approximation.

The program of Fig. 3 does just this—given the two endpoints of a line it generates the intermediate points. It has the feature that it needs no division or multiplication operations, so it can be used to generate fairly complex displays in real time. With the co-ordinate pairs shown at FIRST the program will draw a triangle between the points (0,0), (7,3), and (0,6). The first side of this triangle is shown in detail in Fig. 4: the approximated line is composed of three diagonal moves, (1,1), and four horizontal moves, (1,0).

## PROGRAM FLOWCHART

The flowchart of Fig. 5 shows how the program works, and will help those unfamiliar with the M6800 to implement the algorithm on another micro. First of all the two unit vectors DIAGAB and SINGAB are calculated; some combination of these will make up the required approximation to the line. Each point of the line is generated from the previous point by adding either the diagonal move vector, DIAGAB, or the horizontal/vertical move vector, SINGAB. The choice of which to add is determined by the test variable TEST.

NAM	PLOT		
*	7 201	004A 44 LSH	
		004B 5F CLR	
8100 XAXIS EQU	\$8100 D/A OUTPUT		A SINGLE
8101 YAXIS EQU	\$8101 PORTS	004E 97 07 STA	
		0050 C2 00 S3C	
0000 0002 NEWPR RMB	2 POINTS TO COORDINATE PAIR	0052 D7 06 STA	
0002 0002 DIAGAB RMB	2 DIAGONAL MOVE	. 0054 A6 00 LDA	
0004 0002 SINGAB RMB	2 SINGLE MOVE	0056 E6 01 LDA	
0006 0002 TEST RMB	2	0058 7D 0006 TESTM TST	
0008 0001 TOTAL RMB	I TOTAL NO. OF MOVES	0058 2A 14 BPL	
0009 0001 DOUBLE RMB	NO. OF DOUBLE MOVES	005D 98 04 SINGLM ADD	
000A 0001 SINGLE RMB	I NO. OF SINGLE MOVES	005F DB 05 ADD	
*		0061 36 PSH	
000B CE 0098 ENTRY LDX	£F1RST		A TEST+I
DODE DF GO NEWLIN STX	NEWPR	0064 98 09 ADD	
0010 CE 0101 LDX	£\$0101		A TEST+1
0013 DF 02 STX	DIAGAS		A TEST
0015 CE 0000 LDX	£\$0		A £0
0018 DF 04 STX	SINGAB		A TEST
001A DE 00 LDX	NEWPR	006E 32 PUL	
001C A6 02 LDA A		006F 20 12 BRA	
001E E6 03 LDA B		0071 9B 02 DOUBLM ADD	
0020 A0 00 SUB A		0073 DB 03 ADD 0075 36 PSH	
0022 24 04 BCC	APOS		
0024 40 NEG A			A TEST+1
0025 70 0002 NEG	DIAGAB		A SINGLE
0028 E0 01 AP05 SUB B	B 1.X		A TEST+!
002A 24 04 BCC	BPOS		A TEST
002C 50 NEG 8	8		A £0
002D 70 0003 NEG	DIAGAB+1		A TEST
0030 11 BPOS CBA			
0031 24 09 BCC	AGEB		
0033 36 PSH A	A		
0034 96 03 LDA A		0089 7A 0008 DEC 008C 26 CA BNE	
	A SINGAB+1	008C 28 CA BNE	
0038 I7 TBA		008F 0B INX	
0039 33 PUL 8	8	0090 BC 00A3 CPX	
003A 20 06 BRA	CONT	0093 27 03 BEQ	
003C 36 AGEB PSH A		0095 7E 000E JMP	
003D 96 02 LDA A		0098 7E 000B BACK JMP	
003F 97 04 STA A		TOTAL TOTAL BACK UNP	may 1 of I
0041 32 PUL A		* DRAW A	TRIANGLE *
0042 97 08 CONT STA A		0098 00 FIRST FCB	
0044 D7 09 STA B	B DOUBLE	00A3 LAST EQU	
0046 10 SBA		* *	•
	A SINGLE	•	
0049 IB ABA		FND	

Fig. 3. Program for the M6800 to display lines from the co-ordinates of their endpoints.

The photograph of Fig. 6 shows a pentagram drawn by specifying the five corner coordinates twice each in the correct order, and illustrates the maximum complexity that can be achieved before flicker becomes intolerable. It is also possible to produce moving displays by inserting instructions at BACK to alter the co-ordinates in the "display file" between each sweep of the drawing. With slight modification the program could be used to calculate the path of a moving object, such as a tennis ball in a microprocessor-controlled game.

## PROGRAMMING SWITCHES

Sometimes within a program one wants to jump to one of several addresses depending on the value of a variable. For example, a program might perform a different function depending on a number typed in or a key pressed; the "switch" routine would then cause a jump to the relevant section of code. In a high-level language like Basic or Fortran this function is achieved by a statement like:

GO TO N OF 50, 20, 45, 77, 12

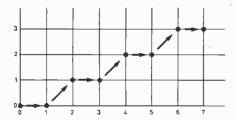


Fig. 4. Points generated by the interpolation program of Fig. 3 for the line joining (0,0) to (7,3). The initial values of the variables used by the program are shown.

where 50, 20, 45, etc. are labels in the program which will be jumped to if N = 1, 2, 3, etc. This can be implemented in machine code on a micro by means of a "jump table" containing the addresses of the various different routines.

The great variety of branch-on-condition instructions available in the M6800 micro makes possible the unusually compact "switch" shown in Fig. 7. LABEL 0 to

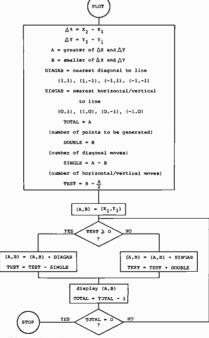


Fig. 5. Flowchart showing the operation of the main section of the interpolation program in Fig. 3.

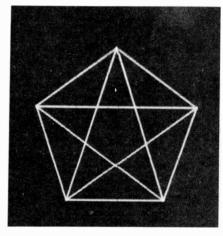


Fig. 6. Pentagram display generated using the interpolation program described in this article.

				NAM		SWITCH				
			*							
0000	В6	0100	SWITCH	LDA	A	N				
0003	06			TAP			PUT	A	IN	STATUS
0004	25	08		BCS		XXI				
0006	2 E	0 E	XX0	BGT		LABELO				
0008	26	20		BNE		LAB EL2				
DOOA	28	4A		BVC		LABEL 4				
000C	20	68		BRA		LABEL6				
000E	2E	16	XXI	BGT		LABELI				
0010	26	34		BNE		LAB EL3				
0012	28	52		BVC		LABEL5				
0014	20	70		BRA		LAB EL7				

Fig. 7. Eight-way switch for the M6800, achieved by putting the control variable into the status register and testing its effect on the condition codes.

LABEL 7 are the eight addresses which are branched to for values of N from 0 to 7 respectively, giving an 8-way switch. In this example the addresses are assumed to be \$10 bytes apart at \$0016, \$0026, \$0036, etc.

# Constant Display FREQUENCY METER



J. BECKER

AN ELEMENTARY PIECE OF WORKSHOP OR LABORATORY EQUIPMENT

r is often undesirable to engage an oscilloscope or other versatile apparatus to merely monitor frequency, and to this end the "Constant Display Frequency Counter" specification has been kept simple. The unit is not crystal controlled, but uses an elementary low frequency oscillator which necessitates far less dividing down circuitry, the whole unit thus comprising just a few readily available components. This would be an encouraging project for the beginner.

## **CLOCK GENERATOR**

The 1Hz clock signal is produced by IC1a (see Fig. 1), whose rate depends upon C1, VR1 and R1. The pulse width generated is about 45ns, and this enables the system to "read" the count almost instantaneously.

The monostable IC1b is repetitively triggered by the output from the multivibrator to produce pulses of about 70ns, controlled by C2 and R2, and which in fact occurs fractionally afterwards due to propogation delay in the i.e. of about 20ns. This second pulse is used to reset the counter at the end of each cycle.

## **DECADE COUNTERS AND LATCHES**

The input pulses to be counted are amplified and shaped by TR1 and fed to a series of decade counters (IC2-6), each of which successively divides the signal by 10. Each group of four outputs from each of the decade counters is taken. BCD fashion, to the Data inputs of the quad-latch i.e.s, IC7-11.

When the clock inputs of the latch i.e.s are held at a logic zero, the outputs remain in their previous logical states, but at the clock input positive excursion to logic 1, the outputs follow the logic states of the Data inputs. Consequently the outputs

from IC2-6 will effectively be ignored by IC7-11 until they receive the "read" pulse from IC1a, at which time, and for the curation of the pulse, the latch outputs will follow the logical states of the decade counters. Upon cessation of the "read" pulse the gate outputs will hold their new logical states and ignore further changes at their Data inputs—until they receive the next "read" pulse!

## **DECIMAL DECODERS AND DISPLAYS**

Following the latches. IC12-16 are decoders providing outputs suitable for the numeric displays X1-5. The outputs from the decoders logically follow the outputs of IC7-11 and will only change state when these change state, thus each indicator will continue to display a particular number until the latches alter outputs.

The decade counters are reset at the start of each cycle by the arrival of the pulse from IC1b approximately 20ns after the "read" pulse from IC1a. The result is that if the same number of pulses is counted by a particular decade stage in two or more consecutive sampling cycles, then the relevant display will not change its number, and will only do so if a consecutive count is different from the previous one. Thus if the frequency stays the same the display will appear to be static even though the sampling is still continuing once a second.

## **POWER SUPPLY**

The a.c. voltage from transformer T1 is rectified by D1-4, and the d.c. ripple is reduced by C4. IC17 reduces and stabilises the main power rail to a nominal 5V. d.c. It is internally protected against thermal or current overloading, and if overloaded will automatically shut itself off until the cause is

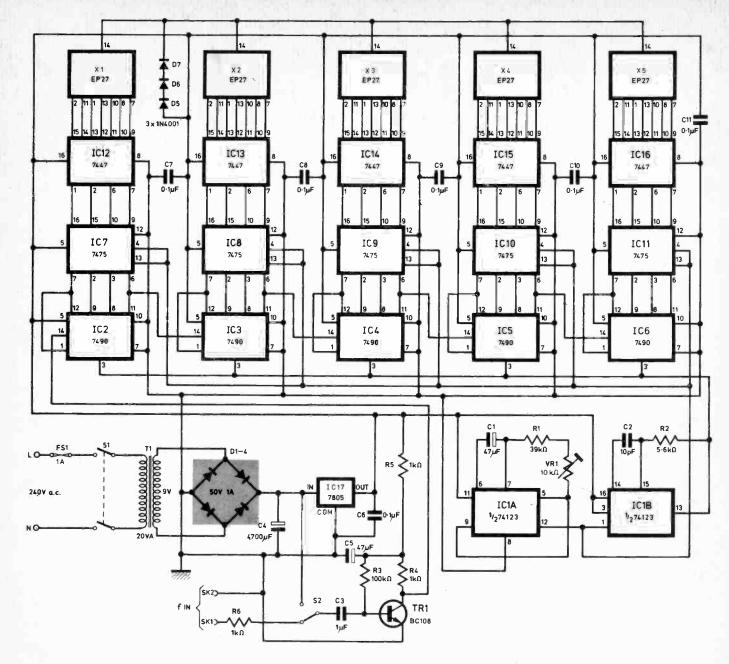
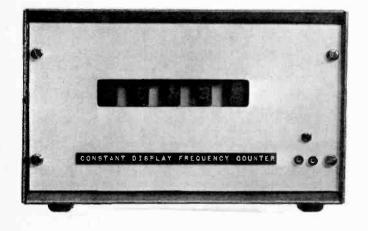
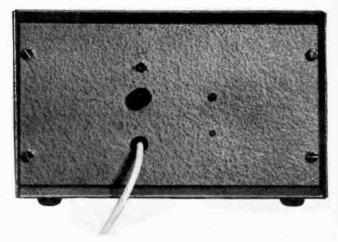


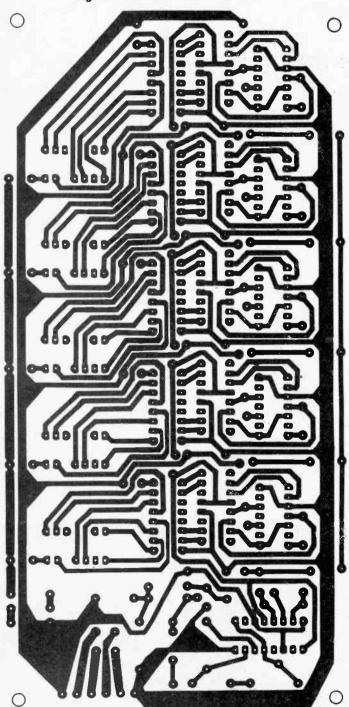
Fig. 1. Full circuit diagram of Frequency Counter





removed, whereupon it will revert to normal operation. In this particular unit it is essential that it is bolted to the metal case in order to provide an adequate heat sink, as it is being used close to its specified limits. The displays have an acceptable voltage range of 2.2V to 3.4V, and are driven from the regulated supply via three IN4001 diodes, each of which reduce the voltage by about 0.7V to provide a supply line of about 3V. Because of the high currents flowing (nearly 1A), the power line connections between the p.c.b., IC17 and C4 must be made using fairly heavy duty wire, and only in the manner shown. Failure to do so could result in unreliable performance of the counter, and "jittery" triggering of the clock generator.

Fig. 2. Printed circuit board full size



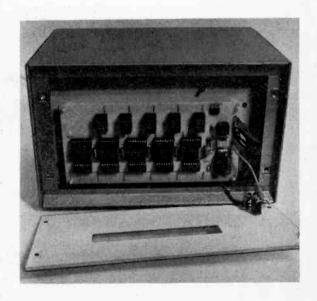
## CONSTRUCTION

The original front panel is re-mounted internally on two blocks of wood fixed to the side panels, and with the p.c.b. mounted on it. This assembly is set back just enough for the displays to level with the front panel mounting-flange of the box. A clear perspex sheet is used as the new front panel, and should be painted on the inside with emulsion (white on the prototype), after masking off the viewing window and lightly sandpapering the remaining surface area.

The mains switch, panel mounting fuse holder, transformer and reservoir capacitor are mounted in the rear section of the box. It is also advantageous to fix a tag strip on the back panel



The original front panel is re-mounted internally in the box to provide a base on which to mount the p.c.b. A new front panel is them made of clear perspex and painted, leaving a display window.



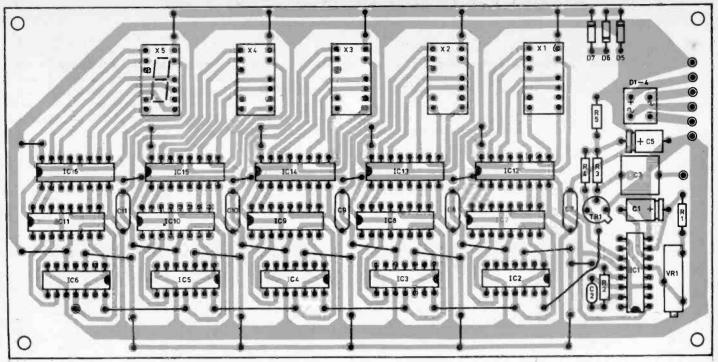
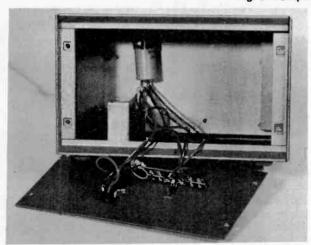


Fig. 3. Component layout (not full size)



1µF min polyester

4700µF 25V electrolytic

0.1μF polyester (6 off)

along with switch and fuseholder, to facilitate the necessary low tension wiring junctions.

The p.c.b. is shown in Fig. 2, and the component layout of this is shown in Fig. 3.

## SETTING-UP

Semiconductors

**Phonosonics** 

Following the usual checks for short circuits between tracks, preferably with a magnifying glass, and for possible assembly errors, the unit should be switched on and allowed to warm up for a few minutes. Then a known frequency can be fed in, and VR1 adjusted so that the display read-out is correct for that frequency. A hole is provided in the case immediately below VR1 to provide screwdriver access. In the absence of a good signal generator, the 440Hz of "Concert A" of a musical instrument, or the note of a mechanical tuning fork of the same frequency, can be fed into the counter via a microphone and suitable preamplifier. Alternatively the residual 100Hz ripple on C4 can be fed in, and a switch is included to enable this, but the

All components including p.c.b. are available from

### COMPONENTS . . . 74123 IC1 IC2-IC6 7490, (5 off) IC7-IC11 7475 (5 off) IC12-IC16 7447 (5 off) 7805 5V 1A regulator IC17 Resistors TR1 BC108 or BC109 39kΩ EP27 7-seg display (5 off) 5.6kΩ X1-X5 R2 50V 1A rectifier stack $100k\Omega$ D1-D4 IN4001 1kΩ (3 off) D5-D7 All resisters 1W 5% carbon film Miscellaneous S.P.D.T. toggle switch 52 **Potentiometers** D.P.S.T. toggle switch (mains) S1 10kΩ 15-turn cermet preset VR1 1 amp fuse and holder F1 2mm sockets (red and green) SK1-2 T1 0-4.5V 0-4.5V 20VA transformer (Type R.S. Capacitors 47µF electrolytic (2 off) 207-122) C1. C5 10pF polystyrene Printed circuit board, capacitor clip for C4, tag strip, probe C2 leads, metal case (RS 509888)

**C3** 

C4

C6-C11

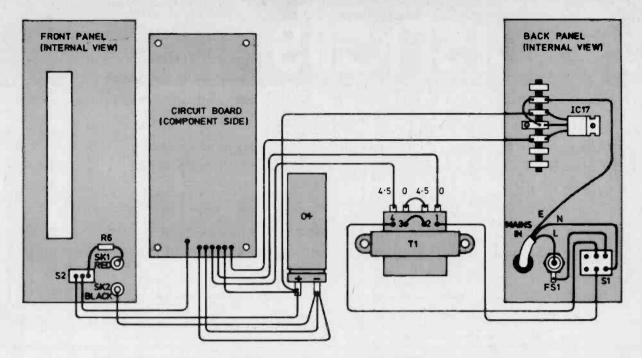


Fig. 4. Wiring diagram. Use either double wires or heavy gauge wire when connecting up C4

higher the calibration frequency the greater the potential accuracy. However, beware that many oscillators can be far less stable than the counter; indeed with the prototype the most stable oscillator tested was the Tone Generator of P.E. Joanna, but even that was found to drift when checked against a mechanical tuning fork.

## **ALTERNATIVE SAMPLING RATES**

If a sampling rate other than 1Hz is required, C1 may be increased or decreased without limit, but the resistance total of R1 and VR1 must be kept within the limiting range of  $5k\Omega$  to  $50k\Omega$  unless additional circuitry is used. Also if an external potentiometer is contemplated in place of VR1, the fixed resistor (of at least  $5k\Omega$ ) must also be kept physically close to IC1.

The clock rate frequency to be expected from changes to C1 may be approximated by assuming that doubling the capacitance will double the frequency count, and halving it will halve the count. However, in practise the actual count time is

likely to vary from that calculated due to component tolerances and capacitor leakage currents, especially with electrolytic capacitors. In respect of tolerances, the actual values obtained from a nominal value can vary by as much as  $\pm 5\%$  for R1,  $\pm 20\%$  for VR1, and -10% to +50% for C1. Capacitor leakage currents will depend, of course, upon the specific types used.

### STABILITY

The unit was checked by the author against the frequencies generated in the P.E. Joanna, which itself was kept in tune against a mechanical tuning fork, and after the initial warm-up period the counter was found to be stable within about 1 pulse per thousand, although the clock rate of IC1a was found to be slightly dependent upon ambient temperature. However, although a more accurate clock pulse might be achieved by making use of the 100Hz ripple available from C4, it was felt that the extra components required did not justify the marginal improvement.

## POINTS ARISING

## **LINEAR CAPACITANCE METER (June 1978)**

Note that in Fig. 2, resistor R9 in series with S3 (run switch) should be marked R19.

In Fig. 4, the underside link (dotted) should go to IC1 pin 7 and not pin 6. An extra wire link is necessary between IC7 pins 12 and 5.

Do not miss out the track cut on Fig. 4, which lies to the right of the junction of R1 and R2, and which has not shown up very clearly in print.

The common line between B1 and B2 should be wired to OV on the component board (not shown in Fig. 4). Also link pin 5 to pin 12 on IC7. A track break is necessary to isolate S2a wiper from IC5 pin 4.

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T	2N696	0.39	2N2219 0.38	2N3397	0.19	2N4062	0.20	2N5247	0.44	40410	0.82	TRA	NICI	CTO	DC	BC214B	0.17	BC549B	0.14	BD244A	0.70	BF182	0.37	BFX89	1.37	MJE520	0.50
Т	2 N697	0.31	2N2219A 0.39	2N3438	0.85	2N4064	1.35	2N5248	0.44	40411	3.10	IKA	A 2	1310	пə	BC214C	0.17	BC549C	0.15	BD244C	0.87	BF183	0.44	BFY50	0.27	MJE521	
П	2N698	0.49	2N2220 0.39	2N3440	0.75	2N4074	2.65	2N5294	0.44	40594	0.87			ØC182B		BC214L		BC557	0.14	BD245A	0.69	BF184	0.41	BFY51	0.27	MJE2955	
н	2N699	0.58	2N2221 0.25	2N3441	0.92	2N4121	0.27	2N5295	0.44	40595	0.98	BC147B	0.13	BC182L	0.15	BC214LB	0.18	BC558	0.13	B0245C	0.85	BF185	0.37	BFY52	0.27	MPF3055	1.05
4	2N706	0.30	2N2221A 0.25	2N3442		2N4122		2N5296		40673	0.80	BC148		8C182LA		BC214LC		8C559	0.15	BD246A	0.72	BF194	0.16	BFY90	1.35	MPF1 02	
.1	2N706A	0.30	2N2222 0.25	2N3638	0.17	2N4123	0.19	2N5298	0.44	40689	1.30	BC148B	0.13	BC182LB	0.15	BC237B	0.15	BCY70	0.21	BD246C	0.93	BF195	0.16	BR101	0.55	MPF1D3	
4	2N708	0.30	2N2222A 0.25	2N3638A	0.17	2N4124	0.19	2N5447	0.16	AC126	0.48	BC14BC	0.13	BC183	0.12	BC23BA	0.13	BCY71	0.26	BD433	0.44	BF196	0.16	BRY39	0.55	MPF104	
1	2N718	0.30	2N2369 D.27	2N3702		2N4125		2N5448		AC127	0.48	BC149	0.15		0.12	BC238B	0.13	BCY72	0.18	BD434	0.46	BF197	0.18	BSX19	0.35	MPS105	
1	2N718A		2N2369A 0.27	2N3703		2N4126		2N5449			0.48	BC149C	0.15		0.13	BC238C	0.13	80115	0.88	BD435	0.46	BF198	0.19	BSX20	0.35	MPSA05	
-1	2N720A		2N2646 0.80	2N3704			0.38	2N5457			0.43	BCI57A			0.13	BC239B	0.16	BD 131	0.55	BD436	0.46	BF199	0.19	BSX21	0.35	MPSA06	
н	2N722		2N2647 1.55	2N3705		2N4286		2N5458			0.54	BC158A			0.15	BC239C	0.17	B0132	0.75	BD437	0.55	BF224J	0.22	BU104	1.80	MPSA12	
-1	2N727		2N2903 1.60	2N3706		2N4287		2N5459			0.59	BC158B		BC183LA		BC257A	0.18	B0135	0.40	BD438	0.55	BF225J	0.27	BU105	1.55	MPSA14	
1	2N914		2N2904 0.31	2N3707		2N4288		2N5460				BC159A		BC183LB		BC258B	0.19	B0136	0.40	80529	0.49		0.38	BU126	1.08	MPSA55	
П	2N916		2N2904A 0.31			2N4289		2N5484			0.70	BC1598	0.17			BC259B	0.19	B0137	0.41	80530	0.55		0.33	BU204	2.20	MPSA56	
П	2N917		2N2905 0.31			2N4347		2N54B5		AC176	0.54	BC160	0.38	BC184	0.12	BC300	0.43	BD138	0.41	BD535	0.70	BF245A	0.44	BU205	2.40		2.45
П	2N918		2N2905A 0.31	2N3771		2N4348		2N5486		AC187	0,59	BC161	0.38		0.13	BC3D1	0.43	BD139	0.43	BD536	0.70	BF2458	0.44	BU206	2.70		2.15
П	2N929		2N2906 0.25	2N3772		2N4918		2N5490		AC187K	0.65	BC167	0.13		0.13	BC302	0.37	B0140		BD537	0.74	BF257	0.35	BU208	2.70		0.49
-1			2N2906A 0.25	2N3773		2N4919		2N5492			0.54					BC303	0.54	BD181 BD182	1.90	BD538	0.77	BF258	0.35		0.22		0.65
ł	2 N930		2N2907 0.25	2N3819		2N4920		2N5494			0.65			BC184LB		BC3D7	0.16 0.16	80183	2.35	BD539	0.60	BF259	0.35	ME0402			0.54
н			2N2907A 0.25	2N3820		2N4921		2N5496		AD161	1.00			BC184LC		BC307A	0.16	80187	0.95	B0540	0.60	BF336	0.42	ME0404 ME0412	0.17		0.54
П			2N2923 0.17	2N3821	0.96			2N6027		A0162	1.00	BC168C			0.15	BC30781	0.16	80235	0.46	80X14 B0X18	1.32	BF337	0.49	MED412			0.72
П			2N2924 0.17	2N3900 2N3901	0.28		0.75 1.15	2N6107 2N6108			0.60	BC1698 BC169C	D.13		0.15 0.15	BC3088	0.16	B0236	0.44	BOY20	1.10	BF338 BFR39	0.52		0.16		0.59
П			2N2925 0.19 2N2926 0.17	2N39D3	0.20	2N5D86		2N6108			0.16	BC177		BC212L		BC309A	0.16	BD237	0.44	B0Y55	1.90	BFR40	0.29	ME4001			0.82
п	2N1893 2N2102		2N3053 0.25	2N3904	0.18			2N6103						BC212LA		BC309B	0.16	80238	0.44	BOY58	2.10	BFR41	0.30	ME4002			0.76
П	2N2192		2N3054 0.72	2N3904		2N5088		2N6121						BC212LB		BC309C	0.16	B0239A	0.44	BF115	0.39	BFR79	0.30	ME4101			0.97
1			2N3055 0.75	2N3906		2N5089		2N6122		BC108	0.16	8C178	0.22		0.15	BC327	0.22	BD239C		BF160	0.33	BFRBO	0.30	MF4102			0.86
1			2N3390 0.50			2N5190		2N6123					0.25		0.15	BC328	0.20	BD240A		BF161	0.65	BFR81	0.30	ME4103			1.08
1			2N3391 0.40	2N4032		2N5191		2N6124					0.35		0.15	BC337	0.20	BD240C	0.59	BF167	0.37	BFX29	0.34	ME4104			0.70
-1			2N3391A 0.45			2N5192			0.47		0.17	BC179	0.25	BC213C	0.15	BC338	0.23	BD241A	0.49	BF173	0.37	BFX30	0.34	ME6101	0.22	TIP3055	0.59
-1			2N3392 0.17	2N4037	0.60	2N5193		40361	0.55		0.16	BC179A	0.25		0.17	BC547	0.13	BD241C	0.65	BF177	0.27	BFX84	0.30	ME6102			1.05
1			2N3393 0.17	2N4058			0.80	40362		BC1098	0.17	BC179B	0.25	BC213LA	0.17	BC547A	0.13	BD242A	0.55	BF178	0.27	BFX85	0.38	MJ2955	1.35	TIS42	0.50
ı			2N3394 0.17	2N4059	0.17			40383	1.45	BC109C	0.18	BC179C	0.26	BC213LB		BC5478	0.13	BD242C		BF179	0.33	BFX86	0.30	MJE340	0.62		0.47
-1	2N2218		2N3395 0.19	2N4060	0.22	2N5245	0.37	40408	0.82	BC140	0.30	BC182	0.12	BC213LC	0.17	BC548	0.13		0.65	BF180	0.37	BFX87	0.35	MJE370	0.62		0.22
4	2N22184	0.38	2N3396 D 19	2N4061	0.19	2N5246	0.38	40409	0.82	BC141	0.32	BC182A	0.12	BC214	0.17	BC549	0.14	BD243C	0.87	BF181	0.37	BEX88	0.30	MJE371	0.86	TIS91	0.27

2N2218A 0.38	2N3396 0.19	2N4061 0.19	2N5246 0.38
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CA3052 1.78	LM709 0.70	NE558N 1.98	TBA550 3.60
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CA3080A 2.10	LM70914 0.49	NE561 4.50	TBA56000 3.00 TBA570 2.10
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	74LS124N 2.70	74C157N	2.21	7472N	0.30	74182N	0.80
	74LS125N 0.50	74C160N	1.11	7473N	0.44	74184N	1.50
i	74LS126N 0.50	74C161N	1.11	7474N	0.32	74185AN	1.50
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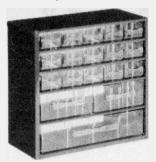
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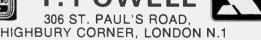
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## HY5 Preamplifier

The HY5 is a mono hybrid amplifier ideally suited for all applications. All common input functions (mag Cartridge, tuner, etc.) are catered for internally, the desired function is achieved either by a multi-way switch or direct connection to the appropiate pins. The internal volume and tone circuits merely require connecting to external potentiometers (not included). The HY5 is compatible with all I.L.P. power amplifiers and power supplies. To ease construction and mounting a P.C. connector is supplied with each pre-amplifier.

FEATURES: complete pre-amplifier in single pack; multi-function equalisation; low noise, low distortion; high overload, two simply combined for stereo.

Oslotrion; night overload, two simply combined on a stereo.

APPLICATIONS: hi-fi; mixers; disco; guitar and organ; public address.

SPECIFICATION: Inputs-magnetic pick-up 3mV; ceramic pick-up 30mV; tuner,100mV, microphone 10mV; auxiliary 3-100mV; input impedance 47κΩ at 1kHz. Outputs—tape 100mV, main output 500mV R.M.S. Active Tone Controls—treble ± 12dB at 10kHz; bass ± 12dB at 10bHz. Distortion—0-1% at 1kHz, signal/noise ratio 68dB. Overload—38dB on magnetic pick-up. Supply Voltage—±16-50V.

Price £5-22 + 65p VAT. P. & P. free

HY5 mounting board B.1. 48p + 6p VAT. P. & P. free



The HY30 is an exciting New kit from I.L.P. It features a virtually indestructible I.C. with short circuit and thermal protection. The kit consists of: I.C., heatsink, P.C. board, 4 resistors, 6 capacitors, mounting kit, together with easy to follow construction and operating instructions. This amplifier is ideally suited to the beginner in audio who wishes to use the most up to date technology available.

FEATURES: complete kit, low distortion; short, open and thermal protection; easy to build APPLICATIONS: updating audio equipment, guitar practice amplifier; test amplifier, audio oscillator SPECIFICATION: Output Power—15W R.M.S. into 8Ω. Distortion—0·1% at 15W. Input Sensitivity— 500mV. Frequency Response-10Hz-16kHz - 3dB.

Price £5.22 + 65p VAT. P. & P. free

## **HY50** 25W into 8Ω

The HY50 leads I.L.P.'s total integration approach to power amplifier design. The amplifier features an integral heatsink together with the simplicity of no external components. During the past three years the amplifier has been refined to the extent that it must be one of the most reliable and robust High Fidelity modules in the World. FEATURES: low distortion; integral heatsink, only five connections, 7 amp output transistors, no external components.

APPLICATIONS: medium power hi-fi systems, low power disco; guitar amplifier.

SPECIFICATION: Input Sensitivity—500mV. Output Power—25W R M.S. into 8Ω. Load Impedance—
4-16Ω. Distortion—0 40% at 25W at 1kHz. Signal/Noise Ratio—75dB Frequency Response—10Hz45kHz - 3dB. Supply Voltage— ±25V. Size—105 × 50 × 25mm.

Price £6-82 + 85p VAT. P. & P. free



The HY120 is the baby of I.L.P.'s new high power range, designed to meet the most exacting requirements including load line and thermal protection this amplifier sets a new standard in modular design.

FEATURES: very low distortion, integral heatsink load line protection, thermal protection, five

PEATURES: very low distortion, integral neats/ink load line protection, thermal protection, live connections; no external components.

APPLICATIONS: hi-fi, high quality disco, public address, monitor amplifier, guitar and organ.

SPECIFICATION: Input Sensitivity—500mV Output Power—60W R.M.S. into 8Ω. Load Impedance—4-16Ω. Distortion—0-04% at 60W at 1kHz. Signal/Noise Ratio—90dB. Frequency Response—10Hz-45kHz = 3dB. Supply Voltage—±35V. Size—114 × 50 × 85mm

Price £15.84 + £1.27 VAT. P. & P. free



120W into 8Ω

The HY200 (now improved to give an output of 120 watts) has been designed to stand the most rugged conditions such as disco or group while still retaining true hi-fi performance. FEATURES: thermal shutdown very low distortion, load line protection, integral heatsink, no external

components.

APPLICATIONS: hi-fi, disco, monitor, power slave, industrial, public address

SPECIFICATION: Input Sensitivity—500mV. Output Power—120W R.M.S. into 8Ω. Load Impedance—4-16Ω. Distortion—0.05% at 100W at 1kHz. Signal/Noise Ratio—96dB. Frequency Response—10Hz-45kHz-3dB. Supply Voltage—±45V. Size—114 × 50 × 85mm.

Price £23-32 + £1-87 VAT. P. & P. free

## **HY400** 240W into 4Ω

The HY400 is I.L.P.'s "Big Daddy" of the range producing 240W into 4 $\Omega^{\dagger}$  It has been designed for high power disco or public address applications. If the amplifier is to be used at continuous high power levels a cooling fan is recommended. The amplifier includes all the qualities of the rest of the family to lead the market as a true high power hi-fidelity power module.

FEATURES: thermal shutdown, very low distortion, load line protection, no external components.

APPLICATIONS: public address, disco, power slave, industrial.

SPECIFICATIONS: public address, disco, power slave, industrial.

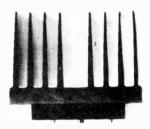
SPECIFICATION: Output Power—240W R. M.S. into 4Ω Load Impedance—4-16Ω. Distortion—0·1% at 240W at 1kHz, Signal/Noise Ratio—94dB. Frequency Response—10Hz-45kHz – 3dB. Supply Voltage — ±45V. Input Sensitivity—500mV. Size—114 × 100 × 85mm.

Price £32.17 + £2.57 VAT. P. & P. free

POWER SUPPLIES: PSU36—suitable for two HY30s £5-22 + 65p VAT. P. & P. free. PSU56—suitable for two HY50s £6-82 + 85p VAT. P. & P. free. PSU76—suitable for two HY120s £13-75 + 1-10 VAT. P. & P. free. PSU96—suitable for one HY200 £12-65 + £1-01 VAT. P. & P. free. PSU160—suitable for two HY200s or one HY400 £23-10 + £1-85 VAT. P. & P. free. 1.L.P. Electronics Ltd., Crossland House, Nackington, Canterbury, Kent CT4 7AD









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individually controlled inputs (each input has a separate 2 stage pre-amp.). Input 1, 15mV into 47k. Input 2, 15mV into 47k (suitable for use with mic. or guitar etc.). Input 3, 200mV into 1 meg, suitable for gram, tuner, or tape etc. Pull mixing facilities with full range bass & treble controls. All inputs plug into standard jack sockets on front panel. Output socket on rear of chassis for an 8 ohm or 16 ohm speaker. Output in excess of 20 wats R M S. Very attractively finished purpose buttle cabinet made from black vinyl covered steel, with a brushed anodised aluminium front escutcheon. For ac mains operation 200 240 volts. Size approx. 12-; in wide - 5 in high 7; in deep.

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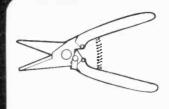
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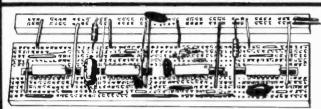
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			OA	122	10.0	24 03	ÕÃ
MAI	NS ISOLA	TING (SCR	EENED)	189	12.0	27 13	O'A
PRIM	120/240 SEC	C 120/240 CT	TAPPED	-			
Ref	VA (Wat	(15) £	PAP				
07		4 - 40	0.79		AUTO TRA	NSFORM	ERS
149	60	6 20	0.96	Ref 1	VA (Watts) V	olts .	E PAP
150	100	7.13	1:14	113	15 0-115-210		2 48 0 71
151	200	11 16	1 - 50	64	75 0-115-210		3.95 0.96
152	250	12:79	1 - 84	4 1	50 0-115-200		35 0 96
153	350	16 28	1.84		00 0-115-200		0.99 1-64
154	500	19:15	2 15		00 0-115-200	220-240 11	76 2-08
155	750	29 06	OA	93 15	00 0-115-200	220-240 2	3-36 OA
156	1000	37 - 20	ÖÄ	95 20	00 0-115-200	220-240 2	82 OA
157	1500	45 60	OA	73 30	00 0-115-200	0-220-240 41	00 OA
158	2000	54 - 80	OA		00 0 113-200	7-220-240 40	OU OA
159	3000	79 05	OA				
*Pleas	se specify 115		uirod	CAS	ED AUTO	TRANSFO	RMERS
11000	от орсону , тто	7 01 2 40 7 TEQ	uneu	240V c	able in & 11:	5V USA 2 D	in outlet
	HIGH VOL	TAGE MAI	NC	VA	£	PAP	Ref
		LATING	4.5	15	4 96	0.96	113W
	Prim 200/220	V or 400/440	V	150	8-48	1 14	4W
	Sec 100/12	0V or 200/240	N/	200	9 - 92	1 45	65W
	JEC 100/12	£	PAP	250	10.49	1.45	69W
Va	Ref						
Va 60	Ref			500	15.72	1.64	
60	243	5 89	1.32		15:73	1 64	67W
60 350	243 247	5-89 14-11	1 · 32 1 · 84	500 750 1000	15 · 73 18 · 55 22 · 68	1 76	67W 83W
60	243	5 89	1.32	750	18 - 55		67W

	SCREE	NED MINIATU	RES		Г
Ref	mA	Volts	£	PAP	ı
238	200	3-0-3	1.99	0.55	
212	1A, 1A	0-6, 0-6	2 85	0.78	П
13	100	9-0-9	2.14	0.38	
235	330, 330	0-9. 0-9	1 . 99	0.38	
207	500, 500	0-8-9-, 0-8-9		0.71	
208	1A, 1A		3 53	0.78	
236	200, 200	0-15, 0-15	1 99	0.38	
214	300, 300	0-20, 0-20	2 - 56	0.78	
221	700 (DC)	20-12-0-12-20	3-41	0.78	
206	1A, 1A	0-15-20-0-15-20	4-63	0.96	
203	500, 500	0-15-27-0-15-27	3.99	0.96	
204		0-15-27-0-15-27		0.96	
S112	500	12-15-20-24-30	2.64	0 78	
239	50	12-0-12	1 99	0.38	
				- 00	
	MIN	II-MULTIMETE	R		Ü
DC-10	DOOV AC-	1000V DC-100m	A Res-	50kΩ	1
10000	2√V Bargai	n £5 86  P & P 62	P VAT	3%.	1

20,000 ohm/V Multimeter, mirror scale. Ranges AC/DC to 1000V, DC currents to 250mA. Resistance to 3 Mohoms. 5" × 3\frac{1}{2}" × 1\frac{1}{2}"

£11 34 P&	P £1-05 VAT 8	3%.	72 11 16
	TEST M	ETERS	
1000V AC/	dget Meter DC 2-5A AC/ nd leads £15-8	DC 500K re	C 2K/V AC
AV08 AV071 AV073	£31-10 £42-50	MM5 TT169 DA116 dig Megger B1	ital £100.00
P&P £1.	£50.70 15 VAT 8%. age of AVO's, N	Battery Wee Mego	£42.50
Sp	ecial Offer AV	O Meter (1	07)

Special Offer AVO Meter (107)

Ranges DC voils 2-5, 10, 50, 100, 500, 1000V –
current 1mA, 2-5, 10, 50, 100, 500, 1 amp, AC
10V, 100, 1000, 3 ohmic ranges to 10M ohms,
10,000/V DC, 1000 AC Safety cut out £40-00.
P, & PE1-15, VAT 8%.

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		£		£		
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	0-500µA	5 50		6.70	Carriage	
	0-1mÁ 0-50V	5 50 5 50		8 40	65p	
	0-100µA	5.50		8-40 6-70	VAT 8%	
/(	J Indicator	Panel	48 x 45 250µA			

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7409	0.14	74107	0.28	74193	1.05	74LS109	0.36	74LS670	2.00	4070	0.17
7410	0.13	74109	0.45	74194	0.90	74LS112	0.38			4071	0.17
7411	0.18	74110	0.46	74195	0.84	74LS113	0.36			4072	0.17
7412	0.21	74111	0.70	74196	0.90	74LS114	0.36	4000	0.14	4073	0.17
7413	0.25	74116	1.60	74197	0.90	74LS123	0.82	4001	0.15	4075	0.17
7414	0.54	74118	0.82	74198	1.48	74LS124	2.45	4002	0.16	4076	1.05
7416	0.27	74119	1.30	74199	1.48	74LS125	0.44	4006	0.92	4077	0.46
417	0.27	74120	0.82	74221	1.50	74LS126	0.44	4007	0.16	4078	0.22
7420	0.13	74121	0.25	74273	2.15	74LS132	0.69	4008	0.92	4081	0.17
7421	0.28	74122	0.40	74279	1.25	74LS136	0.40	4009	0.45	4082	0.20
422	0.17	74123	0.53	74283	1.70	74LS138	0.53	4010	0.48	4085	0.72
423	0.25	74125	0.44	74284	6.85	74LS139	0.53	4011	0.15	4086	0.76
425	0.20	74126	0.45	74293	1.35	74LS151	1.05	4012	0.16	4089	1.55
7426	0.25	74128	0.62	74298	1.92	74LS153	0.50	4013	0.42	4093	0.65
7427	0.25	74132	0.68	74390	1.92	74LS154	1.20	4014	0.80	4094	1.80
7428	0.34	74135	0.68	74393	2.12	74LS155	0.86	4015	0.77	4095	1.10
430	0.13	74136	0.75			74LS156	0.86	4016	0.42	4096	1.10
7432	0.24	74137	0.94			74LS157	0.47	4017	0.77	4097	3.50
7433	0.32	74141	0.58	74LS00	0.19	74LS158	0.53	4018	0.87	4098	1.12
7437	0.24	74142	2.00	74LS01	0.19	74LS160	1.22	4019	0.42	4099	1.90
438	0.24	74143	2.00	74LS02	0.19	74LS161	0.69	4020	0.92	4404	1.00
440	0.13	74144	2.00	74LS03	0.19	74LS162	1.22	4021	0.82	4412	0.30
441	0.52	74145	0.64	74LS04		74LS163	0.69	4022	0.82	4428	0.80
442	0.55	74147	1.30	74LS05	0.20	74LS164	1.20	4023	0.15	4445	1.50
7443	0.90	74148	1.18	74LS08		74LS168	2.00	4024	0.66	4449	0.30
444	0.90	74150	0.99	74LS09	0.19	74LS169	2.00	4025	0.15	4501	0.17
445	0.70	74151	0.60	74LS10	0.19	74LS170	1.76	4026	1.28	4502	0.88
446	0.70	74153	0.60	74LS11	0.19	74LS173	1.05	4027	0.50	4507	0.50
7447A	0.64	74154	1.05	74LS12	0.19	74LS174	1.12	4028	0.67	4508	2.25
448	0.60	74155	0.63	74LS13	0.46	74LS175	1.05	4029	0.86	4510	1.05
450	0.13	74156	0.63	74LS14	1.10	74LS189	2.85	4030	0.48	4511	0.98
451	0.13	74157	0.63	74LS15		74LS190	0.81	4031	2.34	4512	0.92
453	0.13	74159	1.70	74LS20		74LS191	0.81	4033	1.25	4514	2.85
454	0.13	74160	0.80	74LS21	0.19	74LS192	1.80	4034	2.00	4515	2.80
460	0.13	74161	0.80	74LS22	0.19	74LS193	1.80	4035	1.00	4516	1.02
470	0.28	74162	0.80	74LS26		74LS195	1.12	4036	2.40	4518	0.99
472	0.22	74163	0.80	74LS27	0.40	74LS196	1.20	4037	0.99	4519	0.50
473	0.26	74164	0.89	74LS30	0.19	74LS197	1.20	4038	1.00	4520	1.05
474	0.26	74165	0.89	74LS32 74LS37	0.25	74LS221	1.12	4039	2.80	4521	2.00
475	0.30	7516 <b>6</b>	0.99	74LS37	0.27	74LS247	0.97	4040	0.88	4522	1.35
476	0.26	74167	2.70	74LS38	0.27	74LS248	0.97	4041	0.77	4527	1.60
480	0.45	74170	1.68	74LS40		74LS249	0.97	4042	0.72	4528	0.92
481	0.90	74172	4.00	74LS42		74LS251	1.00	4043	0.82	4529	1.10
482	0.80	74173	1.18	74LS47		74LS253	1.05	4044	0.82	4536	3.56
483	0.72	74174	0.89	74LS48	0.97	74LS257	1.05	4045	1.40	4553	4.20
484	0.90	74175	0.68	74LS49	0.97	74LS258	1.05	4046	1.32	4555	0.85
485	0.88	74176	0.88	74LS51	0.19	74LS266	0.39	4047	0.96	4556	0.85
486	0.26	74177	0.88	74LS54	0.19	74LS273	2.50	4048	0.60	4558	1.25
489	2.00	74178	1.20	74LS55	0.20	74LS279	0.50	4049	0.42	4566	1.40
490	0.35	74179	1.10	74LS73	0.30	74LS283	1.00	4050	0.42	4583	
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ACY21 54p	BSX20 24p	IN914	4p	TIL		7430	18p	
ACY22 64p	0C35 150p	IN4001	5p	7400	15p	7432	37p	
AFZ12 280p	TIS43 43p	IN4002	5p	7402	16p	7437	37p	
ASY50 120p	ZTX300 14p	IN4003	6р	7403 7404	16p	7442 7448		
BC107 9p	ZTX450 15p	IN4004	6p	7404	25p	7474		
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BC109C11p	2N3055 65p	IC	3р	7410	19a		37p	
BC154 10p BC214 17p	Diodes		28u		26e		36p	
BC413 18p	AAZ15 15e		5 Sp		41p	7493		
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3300 Top; It	330, 470 12p;	330, 470	251/	47 100	3B; Z;	20 230	1 Gm.	
FOV/1 22 22	7p; 47, 100 8p	. 220 470	33V/	1000.	79; 4	20, 330	ı əp;	
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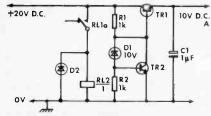
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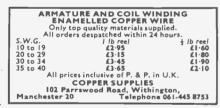
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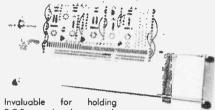
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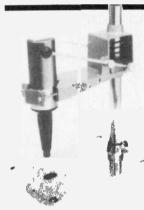
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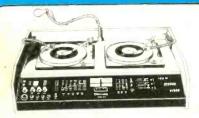
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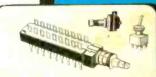
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