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Seturday. Ample Free Car Parking space avail POLYESTER CAPACITORS; Axial lead ty	· · · · · · · · · · · · · · · · · · ·	7408 20 7495 70 4008 92 4006 15 747C 70 MC14433L 12 7409 20 7486 82 4006 98 4056 380 748C 36 MC1710CG 7410 15 7497 262 4010 58 4056 380 753 150 MC670404 7411 15 7497 262 4010 58 40569 303 753 150 MK50233 ★ 5
0.033, 10p; 0.047, 0.068 14p; 0.101	15p; 0.15. 0.22 22p; 0.33. 0.47 39p; 0.68 45p. 7 22p; 0.68, 1.0 29p; 1.5 33p; 2.2 38p; 4.7 47p. 022 18p; 0.047 16p; 0.1 34p; 0.47 43p.	7412 23 74105 62 4012 1 4070 32 AV-1-0212 580 MA30362 P 7413 37 74107 33 4013 55 4070 32 AV-1-0212 580 MA2101-2 2 7413 37 74109 54 4014 99 4072 21 AV-1-5051 126 MA2101-22.4* 3 7416 35 74111 70 4015 93 4072 21 AV-1-50216 195 ME310A 2
POLYESTER RADIAL LEAD (Values in µF 0-01.0-015 6p; 0-022, 0-027 7p; 0-033, 0 0-22, 0-33 14p; 0-47 16p; 0-68 20p; 1-0	0-047, 0-068, 0-1 8p; 0-15 12p; CAPACITORS	7417 39 74116 198 4010 2 4075 23 A7-3-8500 + 510 MES560 + 7420 16 74118 50 4017 94 4075 123 A7-3-8500 + 850 NE5560 + 7420 16 74118 50 4017 94 4077 40 A7-5-1224 + 349 NE561 + 3 7422 13 74120 115 4019 60 4077 40 A7-5-1224 + 349 NE561 + 3 7422 24 7412 28 4019 60 4077 40 A7-5-1230 + 490 NE561 + 7422 24 7412 28 4019 60 4077 40 A7-5-1230 + 490 NE561 +
ELECTROLYTIC CAPACITORS: Axial lea 63V: 0.47, 1.0, 1.5, 2.2, 2.5, 3.3, 4.7, 6 50V: 100 7p; 50, 100, 220 25p; 470 50p 62p: 4700 64p: 35V: 10, 33 7p: 330 42	8 8 10 15 22 9n 47 32 50 12n 63 100 27u	1/423 32 1/41/2 48 4021 1.99 4081 22 CA3018* 82 HE555A* 1 1/425 36 74123 48 4021 1.99 4081 22 CA3018* 82 HE556A* 1 1/425 36 74125 85 4023 20 4085 21 LA3020 170 NE56A* 1 1/420 36 74125 85 4023 20 4085 74 LA3020 170 NE567* 1 1/427 36 74125 86 4023 20 4085 74 LA3020 170 NE567* 1/427 36 74126 86 4023 76 4086 73 LA3023 170 NE571 4
8p; 220, 250 (3p; 470, 640 25p; 1000 2 10, 40, 47, 68 7p; 100, 125, 8p; 470 1 640 10p; 1000 14p, TAG-END TYPE: 70V: 2000 98p; 4700	p; 1000, 2200 68p; 40V; 22, 33 9p; 100 12p; 3300 70 32p; 1000 49p; 25V: 10, 22, 47 6p; 80, 100, 160 7p; 1500 30p; 2000 34p; 3300 52p; 4700 54p; 16V: 16p; 1000, 1500 20p; 2200 34p; 10V: 4, 100 6p; 121p; 50V; 3000 75p; 40V: 4000 70p; 2500 65p;	7430 18 74135 72 4025 19 4089 150 (CA3035 140 RAM2102-2* 2 7432 32 74141 72 4026 180 4093 85 (CA3036 180 ROM2513* 7 7432 32 74141 72 4027 55 4094 190 (CA3045) 190 G5302* 7232 40 74144 314 4027 55 4094 190 (CA3045) 190 G5302* 7232 40 74144 314 4028 90 4095 105 (CA3045) 190 S03402*
Z5V: 4700 48p; 2000 37p; 40V: 2000 4 TANTALUM BEAD CAPACITORS POT 35V: 0 1µF 0.22 0.33 0.47 0.68 Carbo	TENTIOMETERS (AB or EGEN) OPTO Don Track, HW Log & HW Linear values OPTO	7438 33 74145 85 4029 108 4039 192 CA3048 200 Nh760J3N 7440 17 74147 175 4030 58 4039 310 CA3075 175 SN76013N 7441 74 74148 143 4031 230 4089 110 CA3080E 80 SN76023N 7442 66 74150 118 4032 100 4169 100 CA3081 190 SN76023N
1 0 2 2μ ^F , 3.3, 4.7, 6.8 25V: 1.5, 10 1KΩ 20V: 1.5 16V: 10μF 13p each 5KΩ 10V: 22μF, 33, 47 6V: 47, 68, 100, 5KΩ	1.8.2KΩ (lin only) Single gang 26p LEDs - clip 1-2MΩ single gang 26p TIL209 Red 13 1-2MΩ single gang OP switch 55p TIL211 Grn 24 2-2MQ ual gang stereo 70p TIL212 Yellow 27	7443 115 74153 75 4033 145 4160 103 (A3089E 210 SN7615N 7444 112 74154 140 196 4161 109 (A3090AC) 390 SN76227N 7444 112 74154 140 4035 120 4162 109 (A3123E 200 TAA621AX1 7445 94 74155 82 4035 120 4163 109 (A3123E 200 TAA621AX1 7446 94 74157 80 4035 320 4163 109 (A31304) 94 TAA661A
0 015 0.02 0 04 0 05 0.056µF 6p 0-25	T110 20 DER POTENTIOMETERS 2" Red 17 2' Wigg and linear values 60mm 0CP70 40 2-500KΩ single gang 70p 0RP12 68	/44/ 82 74159 225 4039 108 4175 99 C43275 1150 1150 130 <th< td=""></th<>
CERAMIC CAPACITORS: 50V 0.5pF to 10nF 15pE 22oE 32oE 47oE 15pE 22oE 32oE 47oE	Ω-500KΩ dual gang 80p 2N5777 54 Stick Graduated Bezels 20p 7 Seg Displays 11212 C An 3" 125	7454 17 74167 198 4042 81 4410 720 M318 195 TBA5400 7460 17 74172 244 4043 96 4411 995 IM324 350 TBA5500 2 7460 17 74172 625 4044 96 4412 1550 IM324 350 TBA5500 2 7460 17 74172 625 4044 95 44124 1550 IM324 350 TBA5500 2 7470 30 74172 175 4045 145 44124 1550 IM324 355 TBA641BX11 7470 30 74173 175 4045 145 44124 1380 IM348 395 TBA651
0-10-10-10-10-10-10-10-10-10-10-10-10-10	ESET POTENTIOMETERS TIL313 C Cth 3" 125 W 500_5M0 Miniature TIL321 C An 5" 130 tical & Horizontal 8p TIL322 C Cth 5" 130 SW 1000_3-3M0 Horiz 10p DL704 C Cth 99 SW 20007M0 Vert 10p DL704 C Cth 99	7273 32 74185 148 4046 130 4415F 795 14349N 120 1788600 7474 32 74188 65 4047 99 4415V 795 14380 98 17888105 1 7475 42 74190 140 4048 58 4419 280 14381 170 178820 7476 30 74194 140 4049 52 4422 545 14382 125 1788200 3
SILVER MICA (Values in pF) 3-3, 4-7, 6-8, 10, 12, 18, 22, 33, 47, 50, 68, 75, 82, 85, 100, 120, 150, 220 9p each RES	Sistors Erie make 5% Carbon DL747 C A 180 Sistors Erie make 5% Carbon DRIVERS iature High Stability Low noise 75491:75492 85	7480 50 74195 95 4050 52 4433 1225 LM3909N 70 T07202O 23 7481 97 74198 248 4051 89 4435 825 LM3911 125 ZN414 1 7482 82 75150 110 4052 89 4440 1275 M252AA* 750 ZN424 1
1000, 1800, 2000, 2200 20p each CERAMIC TRIMMER CAPACITORS	RANGE VAL 1 99 100 . 2-20.4 7M E24 1.5p 1p SWITCHES* 2-20.4 7M E12 2p 1.5p TOGGLE 2A 250V 2-20.10M E12 2p 1.5p TOGGLE 2A 250V 2-20.10M E12 5p 4p SPST	TRANSISTORS AC117 35 BC168C 12 BF198 18 OC46+ 35 ZTX504 25 2N3702 AC125+ 19 BC169C 14 BF20A 30 JC70+ 30 ZTX501 28 2N3703 AC126+ 15 BC170 14 BF224A 18 IOC70+ 30 ZTX550 25 2N3704
2.5 655 2 1055 10 4055 275 100	Metal Film 10Ω-1MΩ 6p 4p DPDT 35p) - price applies to Resistors of each type mixed values. 4 pole on/off 58p SUB-MIN TOGGLE SP changeover 59p	AC128 ± 15 BC170 1a BF226A 18 OC71 ± 30 ZTX550 25 2N3704 AC127 ± 18 BC171 11 BF256 ± 50 OC72 ± 30 ZN256 ± 58 ZN3705 AC128 ± 18 BC172 10 BF256 ± 29 OC77 ± 76 2N696 ± 35 ZN3706 AC141 ± 24 BC177 ± 18 BF255 ± 29 OC79 ± 76 2N696 ± 35 ZN3706 AC141 ± 24 BC177 ± 18 BF255 ± 29 OC79 ± 76 2N696 ± 35 2N3707 AC141 ± 38 BC178 ± 16 BF255 ± 29 OC79 ± 76 2N696 ± 39 2N3707
3-40pF, 10-80pF, 25-190pF 25p We	EE STOCK-LIST SP5T on/off 54p stock thousands more items Please d a large SAE for our free list. OPDT Gainsed 115p SLIDE 250V:	AC:42+2 24 BC:73+4 18 BF394 22 10 CB2+4 45 2N659+4 50 2N3709 AC:42(* 38 BC:82 10 BF594 40 OC820+45 2N659+4 50 2N3709 AC:142(* 38 BC:82 10 BF594 40 OC820+45 2N70FA+19 2N3710 AC:167+8 18 BC:82 13 BF595 38 OC83+48 2N70F+50 2N3711 AC:167+20 20 BC:183 10 BF939 25 OC84+44 2N70F+50 2N3715+2
Screened Plastic oper chrome body meta	SOCKETS FERRIC 1A DP0* 14p inn moulded CHLORIDE* 1A DP0* 16p iai with Anhydrous 4 opte clover 13p	AC188 + 20 BC1831 12 BFR40 28 OC123 + 115 2N914 32 2N3772 + 1 ACY17 35 BC184 11 BFR59 28 OC139 + 140 2N916 + 27 2N373 + 2 ACY18 + 40 BC184 14 BFR80 28 OC140 + 125 2N918 + 30 2N3819 ACY19 + 40 BC186 24 BFR29 + 28 OC141 + 157 2N920 + 51 2N3820
2-5mm 12p 8p 8p 3-5mm 15p 10p 8p MONO 23p 15p 13g STEREO 31p 18p 15p	p 20p 20p Figure 20p	ACY20 40 BC187 28 BFX81* 130 OC170* 40 2N930* 18 2N3823* ACY21 35 BC12 1 BFX84* 24 OC171* 40 2N951* 61 2N3823* ACY21 35 BC12 1 BFX85* 28 OC201* 125 2N1131* 22 2N3866* ACY22* 40 BC212 13 BFX85* 28 OC201* 125 2N1131* 22 2N3963 ACY23* 40 BC213 11 BFX85* 28 OC202* 140 2N132* 35 2N3904 ACY3* 40 BC213 14 BFX85* 20 OC202* 150 2N132* 35 2N3904
DIN PLUGS SOCKETS 2 PIN Loudspeaker 3, 4, 5 Pin Audio 13p 8p	DPDT 6 Tag 85p In Line SWITCHES * Miniature Non-Locking Push to Make 15p Push to Break 25p POCKER Within 10A 260V	ACY39 • 78 BC2131 14 BFX8/* 23 OC203* 150 2N1302* 35 2N3904 ACY40* 48 BC2141 14 BFX8/8* 26 OC204* 150 2N1303* 50 2N3905 ACY44 39 BC2141 15 BFY18 50 TIP29 43 2N1304* 50 2N3906 AD140 69 BC3078 20 BFY50* 17 TIP29A 44 2N1305* 28 2N4037* AD149* 70 BC328 15 BFY51* 17 TIP29A 60 2N1305* 35 2N4058
CO-AXIAL (TV) 14p 14p PHONO 5p single	20p ROCKER (white) 10A 250V 14p ROCKER (black) on/off 10A 250V 23p 15p ROCKER: (black) on/off 10A 250V 23p 15p Lights when on 3A 240V 52p	AD1661 + 42 BC338 + 15 BFY52 + 17 TIP30 52 2N1307 + 50 2N4061 AD162 + 42 BC441 + 45 BFY71 47 TIP300 52 2N1306 + 46 ZM4064 + 1 Ap114 + 20 BC461 + 38 BSX20 18 TIP308 64 2N1613 + 20 2N4266 + 2 2N1306 + 46 ZM4064 + 1 AP115 + 20 ZM4266 + 45 SMX20 + 18 TIP308 64 2N1613 + 20 ZM4266 + 45 SMX20 + 18 TIP308 64 2N1613 + 20 ZM4266 + 45 SMX20 + 18 TIP308 64 2N1613 + 20 ZM428 + 20 ZM4266 + 45 SMX20 + 18 TIP308 64 ZM1671 + 190 ZM1428 + 20 ZM428 + <t< td=""></t<>
assorted colours 9p Metal Screened 8p double 12p 8p double 10p 3-way BANANA 4mm 10p 12p	ROTARY: (ADJUSTABLE STOP) 1 pole / 2-12 way 2p/2 6W 3p/2-4W 4p/2-3W 41p ROTARY: Mains 250V AC, 4 Amp 42p	AF116* 20 8C547 12 BSV65* 30 TIP31* 50 2N16718* 195 2N4859 AF117* 22 BC548 12 BSV95A* 18 TIP31A* 50 2N16718* 195 2N4859 AF117* 22 BC548 12 BSV95A* 18 TIP31A* 50 2N1893* 28 2N5135 AF118* 55 BC549C 13 BU105* 140 TIP31A* 50 2N1893* 28 2N5136 AF121* 48 BC558 30 BU205* 190 TIP31C* 66 2N2160* 105 2N5138
2mm 10p 10p 1mm 8p 8p WANDER 3mm 9p 9p	DIL SOCKETS* (Low Profile - Texas) 8 pin 10p; 14 pin 12p; 16 pin 13p; 18 pin 20p; 20 pin 26p; 24 pin 30p; 28 pin 42p; 40 pin 58p.	AF124.# 55 BCY30.# 57 BU208.# 225 TIP32.# 55 2N2217.# 48 2N577.9 AF125.# 35 BCY30.# 75 E5567 65 TIP32.# 50 2N2218.4 35 2N5180.4 AF127.# 35 BCY39.# 78 MD8001.# 158 TIP328.# 75 2N2218.4.# 35 2N5180.4 AF127.# 35 BCY39.# 78 MD8001.# 158 TIP328.# 75 2N2219.4.# 22 2N5191.# AF139.# 35 BCY40.# 75 MJ400.# 90 TIP32C.# 77 2N220A.# 26 2N5305# AF178.# 70 BCY59.# 90 MJ401.# TIP32.# 85 2N2221.A.# 25 2N5457
SPECIAL OFFER	DALO ETCH Resist Pen Spare Tip 75p *	AF180 ± 70 BCY70 ± 15 MJ2955 ± 120 TIP338 ± 100 2N222 ± 20 2N5458 AF186 ± 50 BCY71 ± 20 MU5404 ± 45 TIP338 ± 100 2N222 ± 20 2N5459 AF186 ± 50 BCY71 ± 20 MU5404 ± 51 TIP334 ± 95 2N239 ± 32 2N5459 AF239 ± 42 BCY72 ± 15 MU5370 ± 80 TIP34 ± 95 2N236 ± 25 2N5457 ACY36 ± 40 BD115 ± 62 MU5371 ± 80 TIP34 ± 95 2N236 ± 25 2N577
TV GAMES "Olympic Kit" £20.80 *	COPPER BOARDS+ Fibre Glass Single Sided	ASY27* 45 BD121* 78 MJE520* 65 TIP348* 120 2N2369* 15 2N6027 BC107* 9 BD123 98 MJE521* 74 TIP35* 219 2N2476 125 40311* BC1078* 10 BD124* 115 MJE521* 71 TIP35A 225 2N2483* 28 40313* 1 BC1078* 9 BD124* 115 MJE3055* 80 TIP35A 225 2N2483* 28 40313* 1 BC108* 9 BD131* 38 MJE3055* 80 TIP35A 270 2N2484* 30 40316*
"Olympic" Colour Kit £28.50★	6x6" 78p 6x12" 130p SRBP	BC1098 + 12 BD132 + 38 MPF102 36 TIP36A + 280 2N2646 + 48 40317 BC109C + 12 BD133 + 43 MPF103 36 TIP36C + 352 2N2784 55 40326 + BC109C + 9 BD135 38 MPF104 36 TIP414 + 66 2N284 40327 + BC109B + 12 BD135 38 MPF104 36 TIP414 + 66 2N284 40347 +
EconoGame Kit £8.99★	RHYTHM GENERATOR Build this PE (Jan. '78) Easi-	BC113 17 BD138 50 MPF107 50 TIP428+ 82 2N2956+ 20 40360* BC114 20 BD139 34 MP5A05 32 TIP2955* 65 2N2906* 84 40360* BC114 20 BD139 34 MP5A05 32 TIP2955* 65 2N2906* 84 40361* BC115 20 BD140 36 MP5A05 32 TIP3055* 52 2N2907* 20 40362*
existing Black & White b Games £8.85★ e	erator. We are the sole sup-	BC117 20 BD145 ★ 198 MPSA56 30 TIS44 45 2N29266 10 40912 ★ BC118 20 BDY17 ★ 195 MPSA70 34 TIS46 45 2N29260 10 40512 ★ BC119 28 BDY60 ★ 110 MPSA02 ★ 56 TIS50 47 2N29268 8 40576 ★ 1
"Olympic" Game £8.50 + ii	pliers of the complete Kit 1A 12V 1800 Including the case, pre- IA 18V 2100 drilled printed front panel 1A 22 100 IA 18V 2100 IA 225 IA - 5V 2200	BC134 20 BOY61 * 165 MPSU05* 50 TIS74 47 2N29267 8 40603* 11 BC135 20 BF115* 22 MPSU05* 56 TIS74 47 2N29267 8 40603* 11 BC136 18 BF154* 25 MPSU05* 56 TIS74 24 2N3051* 130 40673* BC137 20 BF1154* 25 MPSU55* 55 ZTX107 22 2N3054* 49 40673* BC140* 35 BF173* 25 MPSU56* 55 ZTX108 20 2N3054* 49 40673*
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	descriptive leaflet. 0.1A 6V 51p nonstration on at our shop) 0.1A 12V 51p	BC158 11 BF194 10 0C42* 40 ZYX500 17 2N363 32 CHOKES BC159 11 BF195 10 0C43* 65 ZTX501 15 2N3614* 169 CHOKES BC159 42 BF196 12 0C44* 35 ZTX502 19 2N3614* 169 SC60 BC1670 11 BF197 15 0C45* 35 ZTX502 19 2N3663 26 100mH

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ELECTRONICS

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CONSTRUCTIONAL PROJECTS AUTO-RANGING VOLTMETER by S. Roberts 400 A useful piece of test gear that leaves your hands free STRENGTH METER by N. Riddiford 412 A game to test your grip P.E. CHAMP-6 by R. W. Coles and B. Cullen 422 CHOMP firmware put under the microscope RHYTHM GENERATOR by N. A. Cooke 432 Construction and final setting up **GENERAL FEATURES** SEMICONDUCTOR UPDATE by R. W. Coles 411 A look at some recently released devices INGENUITY UNLIMITED 437 **Telephone Monitor FAULT FINDING—2** by G. Loveday 445 Trouble shooting complete systems NEWS AND COMMENT 399 EDITORIAL **KIM1 REVIEW** 408 Report on another new microprocessor **NEWS BRIEFS** 417 Microcomputer Kit—Watts On The Road—Exhibition MARKET PLACE 418 Interesting new products **SPACEWATCH** by Frank W. Hyde 421 U.F.O.s, Life And Death From Outer Space, Landsat MICRO-BUS by DJD 429 A bimonthly focus on micro's for the home constructor **INDUSTRY NOTEBOOK** by Nexus 438 What's happening inside industry PATENTS REVIEW 441 The history of the gramophone **BOOK REVIEWS** 448 Selected new books we have received

Our March issue will be on sale Friday, 10 February, 1978

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Plays: Greensleeves

Greensleeves God Save the Queen Rule Britannia* Land of Hope and Glory Oh Come All Ye Faithful Oranges and Lemons Westminster Chimes* Sailor's Hornpipe Beethoven's "Fate Knocking" The Marseillaise Mozart Wedding March Cook House Door The Stars & Stripes' Beethoven's Ode to Joy William Tell Overture Soldier's Chorus Twinkle, Twinkle Little Star Great Gate of Kiev Maryland Deutschland über Alles Bach Colonel Bogie The Lorallie

TUNE IN TO THE WORLD OF

ICROPROCESSORS

'These tunes play longer if the push button is kept pressed

- Handsome purpose built ABS cabinet
- Easy to build and install
- Uses Texas Instruments TMS1000 microcomputer
- Absolutely all parts supplied including I.C. socket
- Ready drilled and legended PCB included
- Comprehensive kit manual with full circuit details.
- No previous microcomputer experience necessary
- All programming permanently retained is on chip ROM
- Can be built in about 3 hours!
- Runs off 2 PP3 type batteries.
- Fully Guaranteed

The Chroma-Chime is the world's first electronic musical door chime which uses a pre-programmed microcomputer chip to generate tunes. Instead of boring old buzzes, dings or dongs, the Chroma-Chime will play one of its 24 well known tunes from its memory using its tiny 'brain' to all the music synthesizing! Since everything is done by precise mathematics, it cannot play the notes out of tune.

The unit has comprehensive built-in controls so that you can not only select the 'tune of the day' but the volume, tempo and envelope decay rate to change the sound according to taste.

Not only visitors to the front door will be amazed, if you like you can connect an additional push button for a back door which plays a different tune!

This kit has been carefully prepared so that practically anyone capable of neat soldering will have complete success in building it. The kit manual contains step by step constructional details together with a fault finding guide, circuit description, installation details and operational instructions all well illustrated with numerous figures and diagrams.

The CHROMA-CHIME is exclusively designed by



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To CHROMATRONICS, River Way, Harlow, Essex, U.K.

Please send Chroma-Chime Kits at £18:00 each including VAT and post and packing PLEASE USE BLOCK CAPITALS

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Signature

N.B. The CHROMA-CHIME is also available, fully assembled, price ± 24.95 inc VAT and post and packing.

PE 2/78

BD1-The Connoisseur's Budget Choice





The Connoisseur BD1 transcription turntable is a precision engineered product designed to provide top grade performance at a moderate cost. Simplicity is the main feature of this unit giving excellent performance and reliability A slow speed synchronous motor is used and because of its construction the hum field is very low, so that even the most sensitive of pickups can be used, including the

Connoisseur SAU2 or the SME 3009 Series II. Speed change is achieved by a press button unit at the rear of the platform which automatically moves the drive belt from one pulley groove to the other whilst the turntable is turning. The BD1 turntable kit can be assembled by the home constructor within the hour and when completed will give top quality performance. No soldering is required. Complete the unit with a modern BD1 plinth and cover. The plinth is finished in walnut veneer and fitted with spherical anti-vibration feet. Add to this a strong Acrylic, bronze cover, hinged with 2-position lid stay and you have a first class turntable at a budget price!



Write for further details to: A. R. Sugden & Co. (Engineers) Ltd. Manufacturers of Connoisseur Sound Equipment, Connoisseur Works, Atlas Mill Road, Brighouse, West Yorkshire HD6 1ES Telephone: Brighouse (0484) 712 142, Telex: 517144 Sugden Crighouse, Telegrams & Cables: Connoisseur Brighouse.

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Vinyl Coa Light Blu- smart filn WB1 WB2 WB3 WB4 WB5	ted instrument Cases is tops and White lower s ish. $5 \times 2_{1}^{2} \times 2_{1}^{4}$ $6 \times 4_{2}^{4} \times 1_{2}^{4}$ $8 \times 5 \times 2_{3}^{4}$ $9 \times 5_{1}^{4} \times 2_{2}^{4}$ $11 \times 6_{2}^{4} \times 3$	60p £1-10 £1-50 £1-50 £1-80 £2-00
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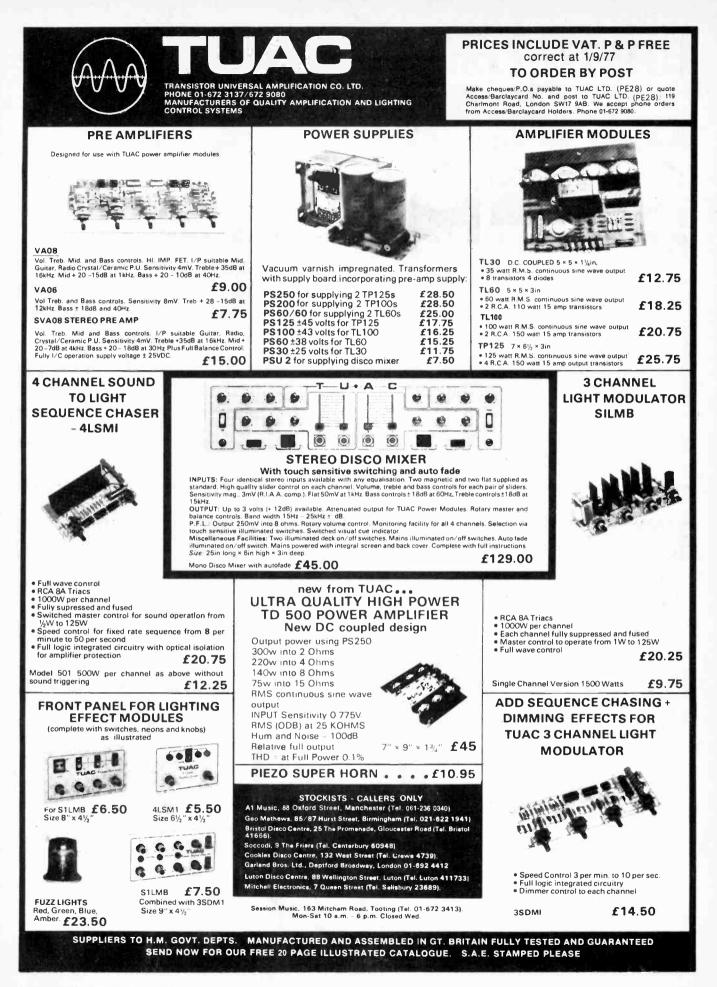
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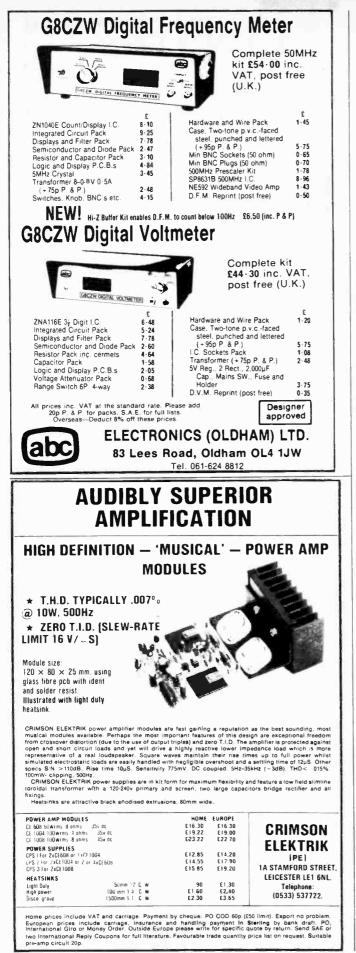
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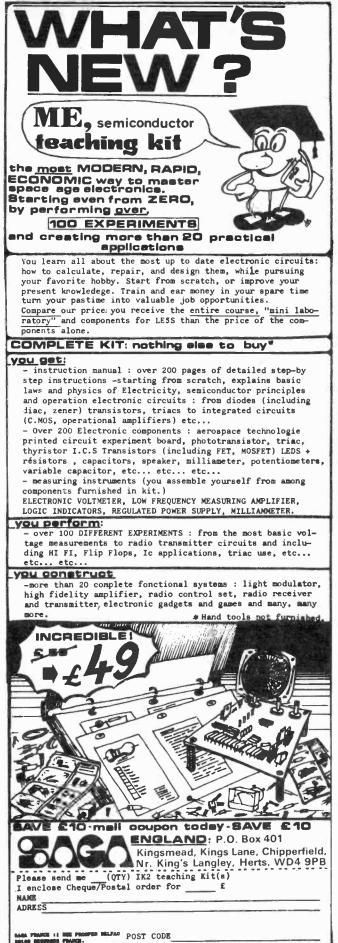
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No, THY1A/50 1 Amp. 50 volt TO5 18p No, THY1A/400 1 Amp. 400 volt TO5 32p	WE NEED THE SPAC
No. THY3A/50 3 Amp. 50 volt T064 25p No. THY3A/200 3 Amp. 200 volt T064 32p	TRANSISTORS SPECIAL OFFL
No. THY3A/400 3 Amp. 400 volt T064 40p No. THY5A/50 5 Amp. 50 volt T066 25p No. THY5A/400 5 Amp. 400 volt T066 40p	BRAND NEW – FULLY GUARANTEED UNTESTED
No. THY5A/600 5 Amp. 400 volt T066 50p No. THY5A/600 5 Amp. 600 volt T066 50p No. C106/4 6 Amp. 400 volt T0220 42p	Type Price Type Price Type Price Type Price SEMICONDUCTOR PAK AC107 25p BC177 12p BF194 •9p TIP32A 34p 2N1813 15p Code No's shown below are given as a guid AC126 14p BC178 12p BF195 •9p TIP32A 35p 2N1711 15p type of devices themselves are
TRIAC	AC127 16p BC179 12p 8F196 •12p TIP32C 36p 2N1893 28p unmarked. AC128 16p 8C182 •9p 8F197 •12p TIP41A 34p 2N2218 15p No. 16130 100 Germ. Gold bonded diode
SB4 8 Amp. 400 volt TO220 Plastic 80p (Non Isolated Tab)	AC128K 24p BC182L *9p BF200 25p TIP41B 35p 2N2216A 18p iike 0A47 AC176 16p BC183 *9p BFX29 22p TIP41C 36p 2N2219 15p No.16131 150 Germ. Point contact diode
DIACS BR100 15p	AC1B7 16p BC184 *9p BFY50 12p TIP42B 37p 2N2221 15p No. 16132 100 200mA Sil, diodes like AC1B7K 26p BC1B4L *9p BFY51 12p TIP42C 38p 2N2221A 16p OA200
D32 15p	AC188 16p BC212 *10p BFY52 12p TIP2955 65p 2N2222 15p No. 16133 150 75mA Sil. Fast switching AC188K 26p BC212L *10p MPSA05 *2p TIP3055 42p 2N2222A 16p didde like INA148 AD161 BC713 *10p MPSA05 *2p TX107 *6p 2N369 10p No. 16133 150 75mA Sil. Fast switching
SWITCHES No. 16178 5 x Mains Slide Switches 40p*	ACT NO BC213 COP MPSA06 *22 ZTX108 *6 ZN2305 14p No. 16134 507 S0mA Sil. top hat Hects. 162 MP 80p 80c213L *10p MPSA06 *22 ZTX108 *6 2N2304 14p No. 16135 203 amp Sil. stud Rect. AF139 30p 8C214 *10p MPSA55 *22 ZTX109 *7p 2N2904A 15p No. 16135 50 Autom Sol. Top Zeness D.0.7 case.
No. S17 5 x Miniature Slide Switches 40p* No. S18 4 x Standard Slide Switches 40p* No. S19 4 x Miniature Push to Make 40p*	AF239 30p BC214L *10p MPSA56 *22p ZTX300 *7p 2N2905 14p No. 16137 30 NPN Plastic trans. like 8C107 6p BC251 *10p OC44 12p ZTX301 *7p 2N2905A 15p BC107/8
No. 519 4 x Miniature Push to Make single hole mounting 40p° No. 520 3 x Miniature Push to Break	8C108 6p BCY70 12p OC45 12p ZTX302 *9p 2N2906 12p No. 1613B 30 PNP Plastic trans. like BC109 6p BCY71 12p OC71 9p ZTX500 *8p 2N2906A 4p 8c177/8 BC118 *10p BCY72 12p CZ7 12p ZTX500 *8p 2N2907 12p St NPN trans. like 2N697/
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16201 18 Electrolytics 4.7μF – 10μF 16202 18 Electrolytics 10μF – 100μF	BC169C *10p BF181 25p TIP30B 37p 2N1303 15p 2N3704 *6p BC170 6p BF182 25p TIP30C 38p 2N1304 15p 2N3704 *6p 2N3055
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16160 24 Ceramic Caps 22pF - 82pF 16161 24 Ceramic Caps 100pF - 390pF 16162 24 Ceramic Caps 470pF - 3300	No. S67 10 x 14 pin DIL Sockets No. S68 9 x 16 pin DIL Sockets
16162 24 Ceramic Caps 4700p = 3300 16163 21 Ceramic Caps 4700p = 0.047μF All 4 at SPECIAL PRICE of £1.60	Type Price Type Price Type Price Type Price Type Price No. S70 3 x 28 pin DIL Sockets
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Fitted with On/Off switch, 1 metre of tough lead with floating 2.5 and 3.5 mm plugs.	S62 4 pieces 8" x 3 #" (approx.) single sided fibreglass 50p
Impedance 200 ohms. Sensitivity 90db. Frequency 90-10,000 Hz. Size 20mm Dia. x 120mm Long	S63 3 pieces 7" x 34" (approx.) double sided fibreglass S0p P.O. RELAYS No. S45 50V (K8S 005) No. S45 100V (K8S 001) No. S46 100V (K8S 01) No. S46 100V (K8S 01)
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D.T.L. Flip Flop and other pulse circuits. It is easy to use and operates from the 5V. D.C. supply of the	5m of 18 sw Multi-core Solder. Order No. 500 500 EX. C. P.O. MICROSWITCHES
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No. S48 No. S49 No. S50	30 x 200V			60р 60р 60р		1 £p	100 £p		1 Ép	100 Ep	
140. 330	2011000			000	7400	0.09	0.00		0.70	0.68	
		1 1/01 -	TAGE SIL	CON	7401	0.11			0.12	0,10	
,				CON	7402	0.11	0		0.12	0.10	
		RECTI	FIERS		7403	0.11	0		0.12	0.10	
GR559	10mA 14KV (*	(4,000		20p each	7404	0.11	+···		0.12	0.10	
GA432	1 AMP. 2 KV (2.000}		20p each	7405	0.11	0.10		0.12	0.23	
FD2.52	5 KV Voltage	Doubler		20p each	7406	0.28	0.2.0		0.24	0.23	
					7407	0.28	0.2.0		0.20	0.22	
		TIC	ABETE	DC	7408	0.12	0.11		0.24	0.22	
	PUIEI		METE	nə	7409	0.12	v		0.44	0.40	
Slider	40mm TR	AVEL			7410	0.09	4.40		0.26	0.25	
Order N	lo.				7411	0.22			0.45	0.42	
16191	6 x 470 Ohn	n LIN Sin	gle	40p*	7412	0.22			0.90	0.88	
S24	6 x 1 K	LIN Sin	gle	40p*	7413	0.28			0.75	0.73	
S25	6 x 5 K	LIN Sin	gle	40p*	7410	0.26			0.88	0.82	
16192	6 x 10 K	LIN Sin	gle	40p*	7420	0.11			0.85	0.80	
S26	6 x 10 K	LOG Si	ngle	40p*	7420	0.19			1.10	1.00	
16193	6 x 22 K	LIN Sin	gle	40p*	7422	0.13			0.28	0.26	
16195	6 x 47 K	LOG Si	ngle	40p*	7425	0.21			2.70	2.50	
16194	6 x 47 K	LIN Sin	gle	40p*	7425	0.25			0.38	0.32	
S27	6 x 100 K	LIN Sin	gle	40p*	7420	0.25			0.65	0.62	
S28	6 x 100 K	LOG Si	ngle	40p*	7427	0.36			0.43	0.35	
S29	6 x 500 K	LOG Si	ngle	40p*	7430	0.12			0.38	0.35	
					7430	0.20			0.70	0.68	
Slider	· 60mm TR	AVEL			7432	0.38			0.60	0.58	
S30	6 x 2.5 K	LOG Si	ingle	40p*	7437	0.26			0.70	0.68	
S31	6 x 10 K	LIN Sir		40p*	7438	0.26		74100	0.95	0.90	
S32	6 x 50 K	LIN Sir		40p*	7440	0.12		74104	0.40	0.35	
S33	6 x 250 K	LOG Si	ngle	40p*	7441	0.60		74105	0.30	0.25	
S34	4 x 5 K	LOG D	ual	40p*	7442	0.80		74107	0.30	0.25	
S35	4 x 10 K	LIN Du	al	40p*	7443	0,95		74110	0.48	0.45	
S36	4 x 100 K	LOG D	uai	40p*	7444	0,95	0,90	74111	0.75	0.72	
S37	4 x 1.3 MEC	LOG D	ual	40p*	7445	0.80	0.75	74118	0.85	0.82	
	S38 MIXED	SLIDER	POTS - VARIO	DUS	7446	0.80	0.75	74119	1.30	1.20	
	VALUES	AND SI	ZES - OUR MD	ĸ	7447	0.70	0.68	74121	0.28	0.26	
		ONLY £	1.00*		Devices	may h	oe mixed to	quality	for a	uantity	pri
	S39 6 x CHI		IDER KNO8S	40p*			ries of ICs in I				
	v	VIREW	OUND		L			_			
		ound sin		s. with linear			C	CMC	SI	Cs	
Orde	erNo. V	alue	Order No	Value	Type	Pric	ce Type	Price	Тур	е	Pr
) ohms	1894	100 ohms	CD4000					4035	£1.
		ohms	1895	220 ohms	CD4001					4037	£0.
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Type AL30A AL60 AL250 SPM80 PS12 PA12 PA100 S450 MPA30	Description 10W RMS Power Amp 25W RMS Power Amp 35W RMS Power Amp 125 W RMS Power Amp 35V Power Supply 20-30V Power Supply for AL30A Stereo Pre-Amp for AL30A Stereo Pre-Amp for AL60/AL80 Stereo F.M. Tuner Magnetic-Ceramic Pre-Amp	Normal Price £3.65* £6.95* £16.95 £3.75* £3.75* £13.75* £20.45* £2.65*	Sale Price £2.95* £3.55* £14.45 £3.10* £1.15* £5.95* £12.45* £18.65* £2.55*
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WAH-WAH UNIT (P.E. Apr. 76) The Wah-Wah effect produced by this unit can be o manually or by the integral automatic controller. Component set (incl. PCB)	controlled £3-55
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COMPONENTS SETS include all necessary resistors, capacitors, semiconductors, potentiometers and transformers. Hardware such as cases, sockets, knobs, etc. are not included but most of these may be bought separately. Fuller details of kits, PCBs and parts are shown in our lists

CIRCUIT AND LAYOUT DIAGRAMS are supplied free with all PCBs designed by Phonosonics PHOTOCOPIES of the P.E. texts for most of the kits are available-prices in our lists.

P.E. JOANNA (P.E. May/Sept. 75) A five-octave electronic piano that has switchable alternative voicing of Honky-Tonk piano. or adinary piano. harpsichord. or a mixture of any of the three, together with facilities including fast and slow tremolo. loud and soft pedal switching, and sustain pedal switching. The power amplifier typically delivers 24 watts into 8 ohms. The PCBs have been redesigned by ourselves making improved use of the space available.

available. Main power supply, tone generator, 61 envelope shapers, voicing and pre-amp circuits. Set of basic component kits for above **£75.29 £75.29** .35

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UNGAR CUNVERSION AT Converts the P.E. Joanna electronic plano to also provide most of the facilities offered by the above electronic organ. Basic component set and PCB £12-34

SYNTHESISER TUNING INDICATOR (P.E. July 77) A simple 4-octave frequency comparator for use with synthesisers and other instruments where the full versatility of the P.E. Tuning Fork is not required.

Component and PCB (but excl sw.)

GUITAR FREQUENCY DOUBLER (P.E. Aug. 77) A modified and extended version of the circuit published. Details in list.



WIND AND RAIN UNIT A manually controlled unit for producing the above-named sounds. Component set (Incl. PCB) £3.72

 GUITAR OVERDRIVE UNIT (P.E. Aug. 76)

 Sophisticated, versatile Fuzz unit, including variable and switchable controls affecting the fuzz quality whilst retaining the attack and decay, and also providing filtering. Does not duplicate the effects from the Guitar Effects Pedal and can be used with it and with other electronic instruments. Component set using dual slider pot
 C6-20 C6-20 C6-20 Printed circuit board

FUZZ UNIT Simple Fuzz unit based upon P.E. Sound Design Circuit Component set (incl. PCB) £2 ·03 TREMOLO UNIT Based upon P.E. "Sound Design" circuit. Component set (incl. PCB) £3-64 TREBLE BOOST UNIT (P.E. Apr. 76) Gives a much shriller quality to audio signals fed through it. The depth of boost is manually adjustable. Component set (incl. PCB) <u>£2-40</u> P.E. TUNING FORK (P.E. Nov. 75) Produces 84 switch-selected frequency-accurate tones. A LED monitor clearly displays all beat note adjustments, Ideal for tuning acoustic and electronic musical instruments allo

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ale. Can also be used as a simple drum-be enerator. Includes power supply.	
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APE NOISE LIMITER	
/ery effective circuit for reducing the hiss found in ecordings, All kits include PCBs	n most tape
Standard tolerance set of components	£2 · 96
Superior tolerance set of components	£3 · 76
Regulated power supply (will drive 2 sets)	£4 · 69
NVELOPE SHAPER WITHOUT VCA (P.E. Oct. 7	5)

revides full manual control over attack, decay, sustain and release functions, and is for use with an existing voltage controlled amplifier. Component set (incl. PCB) £4 · 66

ENVELOPE SHAPER WITH VCA (P.E. Apr. 76) This unit has its own voltage controlled amplifier and has full manual control over attack, decay, sustain and release functione functions Component set (incl. PCB) £6 · 68

TRANSIENT GENERATOR (P.E. Apr. 77) An envelope shaper, without VCA, having the usual attack, decay, sustain and release functions, and in addition it also provides a "Repeat Effect" enabling a synthesiser to be programmed to imitate such instruments as a mandolin or banjo. Component set

	•	F4.3%
ed circuit	board	£1-82

WAVEFORM CONVERTER Slightly modified from a circuit published in a German edition of Elektor' Converts a saw-tooth waveform into four different waveforms sine-wave, mark-space saw-tooth, regular triangle form, and squarewave with an externally variable mark-space ratio. Component set (incl. PCB but excl. sw's) [\$-19

VOLTAGE CONTROLLED FILTER (P.E. Dec. 74) Part of the P.E. Minisonic now released as an independent kit for use with other synthesisers. Component set (incl. PCB) (Order as Kit 65-1) £8-22

RING MODULATOR (P.E. Jan. 75) Part of the P.E. Minisonic now released as an independent kit for use with other synthesisers. Component set (incl. PCB) (Order as Kit 59-1) £5-50

NOISE GENERATOR (P.E. Jan. 75) Part of the P.E. Minisonic now released as an independent kit for use with other synthesisers. Component set (incl. PCB) (Order as Kit 60-1) £3-35

SOPHISTICATED POWER SUPPLIES A wide range of highly stabilised low noise power supply kits is available—details in our lists.

MICROPHONE PRE-AMP (P.E. Apr. 77) Component set (incl. PCB)	£3·78
VOICE OPERATED FADER (P.E. Dec. 73) For automatically reducing music volume	durina

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'talk-over''-particularly useful for Disco work or for home-movie shows. Component set (incl. PCB) £3·97

DYNAMIC RANGE LIMITER (P.E. Apr. 77) Automatically controls sound output to within a preset level. Component set (incl. PCB) £4 · 58

EXPORT ORDERS are welcome, though we advise that a current copy of our list should be obtained before ordering as it also shows Export postage rates. All payments must be cash-with-order, in Sterling and preferably by International Money Order or through an English Bank. To obtain list send 40p.

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AND OTHER PROJECTS

PHOTOGRAPHS in this advertisement show two of our units containing some of the P.E. projects built from our kits and PCBs. The cases were built by ourselves and are not for sale, though a small selection of other cases is available.

LIST—Send stamped addressed envelope with all U.K. requests for free list giving fuller details of PCBs, kits and other components.

OVERSEAS enquiries for list: Europe send 20p. other countries—send 40p.

KEYBOARDS AND CONTACTS Kimber-Allen Keyboarde as required for many published circuits, including the P.E. Joanna, P.E. Minleoole, and P.E. Synthesiser. The manufacturers claim that these are the finest moulded plastic keyboards available. All octaves are C to C. The keys are plastic, spring-loaded and mounted on a robust aluminium frame. 3 Octave (37 notes) £25-50. 4 Oct (48 notes) £32-25. 5 Oct (61 notes) £39-75. Contact Assemblies for use with above keyboards: Single-pole change-over (type SP) as for P.E. Joanna and P.E. Minisonic. Two-pole normally-open mak-break (type DP) as for P.E. Synthesiser. Special contact assembly (type 4PS) having 4 poles, 3 of which are normally-open make-break contacts and the fourth is a change-over contact--his special assembly enables THE SAME KEYBOARD to be used with the P.E. Synthesiser, P.E. Minisonic and the P.E. Joanna simultaneously thus avoiding the cost of more than one keyboard. See our list for other contacts.

ł	Contact SP 2P 4PS	Each 24p 27p 53p	3 Octave Set 2 8-88 2 9-99 219-61	4 Octave Set £11-76 £13-23 £25-97	5 Octave Set £14-64 £16-47 £32-33

PRINTED CIRCUIT BOARDS for use with the above contacts and thus eliminating most of the inter-wiring required, are available. Details in our lists.

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	TRANSISTORS
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MORE NEW KITS!	BC108 14p
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(PE Nov. 77) The new music unit currently being	BC204 14p
published.	BC209C 14p BC212L 15p
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FORMANT SYNTHESISER (Elektor Magazine 1977). Very sophisticated music	BCY71 22p
synthesiser for the advanced constructor and for whom	BD131 44p
cost is secondary to performance.	BD132 54p
	BFY50 22p BFY51 22p
	BFY52 24p
GUITAR SUSTAIN UNIT	BSY95A 22p
(PE Oct. 77).	MD8001 172p
Details in lists. Please send S.A.E.	OC28 60p
	OC71 20p
	OC72 25p OC84 25p
	ORP12 70p
SOUND-TO-LIGHT (P.E. Aurora) (P.E. AprAug. 71)	ZTX107 12p
Four channels each responding to a different sound	ZTX108 9p
frequency and controlling its own light. Can be used with	ZTX501 13p
most audio systems and lamp intensities.	ZTX503 15p ZTX531 23p
Basic component set (excl. thyristors) £15-92 Printed circuit board for above £3-90	2N706 13p
	2N914 22p
Power supply £5-78 PCB for power supply £1-79	2N1304 22p
	2N2219 27p
	2N2905 35p
3-CHANNEL SOUND-TO-LIGHT (P.E. Apr. 76)	2N2905A 36p 2N2907 22p
A simple but effective sound-to-light controller capable of	2N3053 18p
operating 3 lamps each of approximately 700 watts. Includes	2N3054 66p
power supply, thyristors, and by-pass switches. Component set (incl. PCB) £11-95	2N3055 48p
Component set (incl. PCB) £11-95	2N3702 12p
	2N3703 12p 2N3704 12p
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4-channel light-show controller giving a choice of	2N3820 64p
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Basic component set £15-19	2N4060 12p
Printed circuit board £3-45	2N5245 51p 2N5459 33p
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BIOLOGICAL AMPLIFIER (P.E. Jan./Feb. 73)	INTEGRATED CIRTS.
Multi-function circuits that, with the use of other external	318 230p
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Total 210, £3.35 K002 Extended range, 22pF to 0.1μ F. 330 values £4.90 K003 Polyester capacitors. 10 each of these values: 0.01, 0.015, 0.022, 0.033, 0.047, 0.068, 0.1, 0.15, 0.22, 0.033, 0.047, 0.068, 0.1, 0.15, 0.22, 0.033, 0.047, 0.068, 0.1, 0.15, 0.22, 0.033, 0.047, 0.068, 0.1, 0.15, 0.22, 0.033, 0.047, 0.068, 0.1, 0.015, 0.022, 0.033, 0.047, 0.068, 0.1, 0.015, 0.022, NO04 Mylar capacitors. min 100V type. 10 each all values from 1000pF to 10,000pF. Total 130 for £3.75 K005 Polystyrene capacitors. 10 each value from 10pF to 10,000pF. E12 series 5% 160V. Total 370 for E12.30

£12.30

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4046	137p	7403	20p	7483	95p	74161	102p	74365 93p
4049	55p	7404	24p	7484	119p	74162	102p	74366 93p
4050	55p	7405	24p	7485	128p	74163	102p	74367 93p
4051	140p	7406	42p	7486	33p	74164	115p	74368 93p
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CHIPS UP!

CHIPS could be going up in the next few months! There have been various guarded comments about the cost of i.c.s, and the more popular l.s.i. devices, over the last few months; some time ago at least one of the larger manufacturers rationalised their range and increased the price of a number of items—some by very large factors.

It is not the cost of production which is likely to send prices up, since it is well known that the production cost of each item is an insignificant part of the total price. However, manufacturers have followed a policy of price reduction and this must soon (and is now in some cases) come to an end, since the major part of the cost of each item is the marketing, distribution and back up which all the devices require.

Unfortunately this price factor will probably not affect the multinational concerns that can buy tens or even hundreds of thousands of devices but it will affect the smaller companies and, of course, the hobbyist since neither he nor the component supplier is able to purchase in vast quantities. Admittedly some suppliers are connected with distribution houses and the advantage that they already have appears likely to be increased.

MADE IN SPACE

Looking ahead rather further, it seems likely that some devices may be manufactured in space and will thus be coming down an even greater path to us! It has been muted that the space (area?) availability on some space shuttle flights could be used for the manufacture of integrated devices with the obvious advantages of clean "air" etc. The technology would obviously add to the 5,000 pounds (weight) of electronics which will be a permanent part of each shuttle.

HOBBY COMPUTERS

Having indicated that we may well be in for some cost increases in devices, we must hasten to add that we fully expect to see the cost of many complete systems to continue in a downward direction. The major one—and obviously the one that many are watching at the present time—being the microprocessor based systems and the "hobby computer". You will find a review of the KIM I system in this issue and also mention of a British designed system in kit form which is now available (NASCOM I).

NEW TECHNOLOGY

We do not intend to "bury our (editorial) head in the sand" when it comes to any new technology and its possible use by the hobbyist. In fact we believe that it is part of our job to help the introduction of new systems and devices to your home and workbench. This policy is borne out by the use of modern phasing devices---c.c.d.s. or bucket brigade, call them what you will-in the P.E. String Ensemble to be featured in next month's issue. Even if the actual unit does not interest you as a constructional project, the use of these devices and the circuitry must.

In addition to the use of delay line technology to produce a rich orchestral string sound, the unit employs CMOS i.c.s. throughout the divider circuit and unique CMOS chorus drive circuitry.

Mike Kenward.

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Letters

Queries regarding articles published in PE should be addressed to the Editor, at the Editorial Offices, and a stamped, addressed envelope enclosed. We cannot undertake to answer questions regarding other items, nor to answer technical queries over the telephone.

UTO-KANDING IOLTMETER



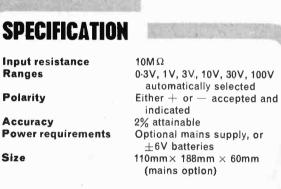
STEVE ROBERTS

TO ANYONE concerned with practical work with electronic circuits, the type of measurement most frequently required is undoubtedly voltage. Many instruments are available today which enable voltages to be measured with various degrees of accuracy, clarity or ambiguity, and which present the information on one of two types of readout—linear or digital.

The cost effective digital meter is *relatively* new upon the scene, but is felt by many people to have disadvantages over its analogue counterpart. One problem is its tendency to create false confidence; 1.32 volts displayed probably means 1.32 ± 0.015 volts. The analogue meter, by its very nature, serves as a constant reminder that the reading is not an absolutely indisputable value. Needle width and parallax effects are two sources of reminder. Another shortcoming of the digital display is its inability to provide qualitative information. A meter needle spinning wildly up to the top end of the scale, or vibrating about a reading, is much more evocative than a simple overrange indication, or a number that keeps changing.

It may also appear to be something of a paradox that when it is required to measure a voltage (implying that the voltage is initially unknown), it is first necessary to select the meter range appropriate to the measurement, for which it is required to know the voltage. This is of course not normally a problem, since the approximate voltage can usually be anticipated, and confirmation or greater accuracy is all that is required.

Much more of a problem is that of remembering to change the meter range for each measurement, or even changing the test leads over when the polarity is reversed. An auto-ranging facility overcomes these problems, and in doing so aids continuity of mental effort, not to mention prevention of damage to meters!



The design to be described is therefore a combination of the best features of analogue and digital instrumentation. It is adequate for all the more usual voltage measurements, and takes up no more room on the bench than the average multimeter.

DESIGN CRITERIA

The instrument was designed with the following points in mind:

- (a) Accuracy comparable with better quality analogue meters.
- (b) High input resistance.
- (c) As clear a display as possible.
- (d) As few controls as possible to leave hands free.
- (e) Total measurement range to cover all normal d.c. voltage reading requirements for i.c. and transistor work.
- (f) Foolproof in use.

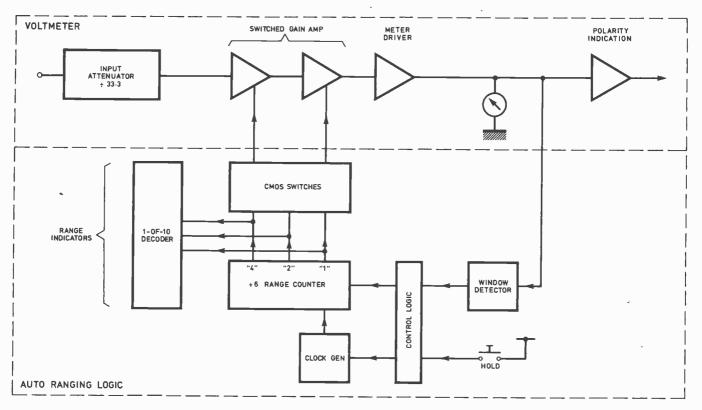


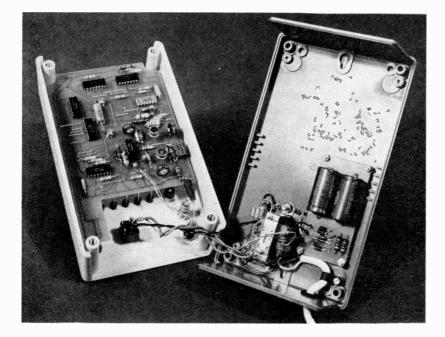
Fig. 1. Block diagram of Auto-Ranging D.C. Voltmeter

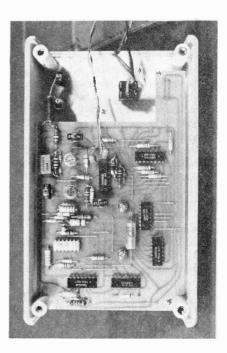
CIRCUIT DESCRIPTION

Referring initially to the block diagram of Fig. 1, the voltmeter section consists of an input attenuator, a two stage amplifier and a rectifier/meter driver.

Referring to the auto-ranging logic section, if the voltage present at the moving-coil meter does not fall within a predetermined window (between 20 per cent and 90 per cent of full scale), the output of the window detector enables the range counter on the next pulse of the clock oscillator. The range counter output controls the status of the CMOS range selector switches, and thus the gains of the voltmeter amplifiers are changed. The whole process is repeated until a gain has been selected which causes the voltage being displayed to fall within the range of the window detector, at which time the range counter is inhibited and the range remains selected. A decoder is provided which decodes the output of the range counter and drives the range indicating l.e.d.s.

For the detailed circuit description, we must now refer to the full circuit diagram, Fig. 2.





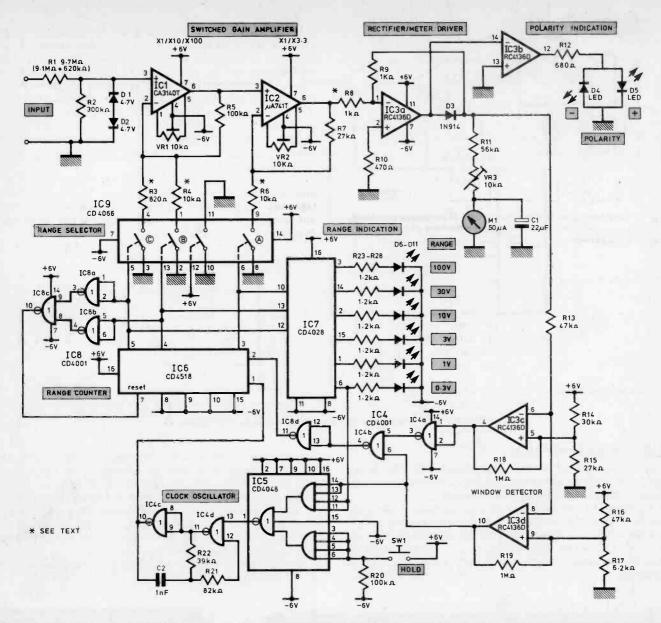


Fig. 2. Full circuit diagram of Voltmeter unit. Although the circuit contains a rectifier, it will not give the conventional true r.m.s. reading for an a.c. input

The input attenuator, R1 and R2, determines the input resistance of the instrument, and reduces the highest possible voltage presented for measurement to a level that can be handled by the input circuitry. Diodes D1 and D2 prevent damage to the circuit should a very high input voltage be applied inadvertently.

The switched-gain amplifier is formed by IC1 and IC2. Op amp IC1 is a very high input resistance device, which is necessary to preserve the integrity of the input attenuator. The gain of the amplifier is adjusted by changing the degree of negative feedback through the CMOS switches.

A conventional full-wave rectifier circuit is formed by IC3a, which presents about +3V at the cathode of D3 for full scale deflection of the meter. The polarity of the voltage at IC3 pin 3 is monitored by IC3b, and this in turn causes the appropriate polarity indicator to be illuminated.

The meter drive voltage is also presented to IC3c and IC3d, which are connected as voltage comparators. If the meter drive voltage is higher than the reference voltage provided by R16 and R17, the pin 10 output is "Low". Similarly, if the voltage is lower than the reference

voltage from R14 and R15, the pin 4 output is "High", and IC4 pin 3 is therefore "Low". The two low inputs presented to IC4b produce a high output, which is present only when the two inputs are both low. After inversion by IC8d, this output is used to inhibit the range counter IC6. Note the hysteresis resistors R18 and R19 (giving slight positive feedback) which eliminate any tendency to indecision around the comparison voltage.

Nor gates IC4c and IC4d form an oscillator of around 10kHz. The actual frequency is uncritical as it only affects the search rate of the instrument. The oscillator may be disabled by a high input from IC5, to which reference will be made later.

The dual 4-bit binary counter (IC6), has only half in use. IC8a, b and c, cause the counter to reset on a count of six, thus preventing the selection of invalid gain settings occurring. The binary outputs of the counter are used to activate the CMOS switches, thus selecting the different gain values. See Table 1 under "Test And Calibration".

The binary-to-decimal decoder IC7 provides a "1 of 10" output, which is used to drive directly the range l.e.d.s.

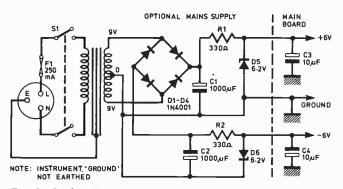


Fig. 3. Optional power supply circuit. If batteries are used, a larger case will be necessary, and a battery check facility would be advisable

LOW READING STABILITY

A problem could occur when the meter has a zero or near-zero input. The window detector would see a voltage too low for the 0.3V range, and would therefore change scales in an attempt to locate the correct range. As there is no more sensitive range, the circuit would search continuously and prevent very low voltage measurements from being made.

The output from pin 6 of IC7, which is high when the most sensitive range is selected, is monitored by IC5, as is the output of IC3d. If the lowest range is selected now, and if the measured voltage falls below the magnitude window, the clock oscillator is inhibited, thus preventing further searching.

Occasions may arise when it is desirable that the range does not automatically change; for example, when examining a voltage that is fluctuating between 8.5 and 9.5 volts. As these figures embrace a range change, meter indications would largely be meaningless unless the range is "held" at, say, 10V. The exact behaviour of the input may then be observed as long as the Hold button is pressed. Pressing this button has the effect of inhibiting the clock oscillator as before.

CONSTRUCTION

The prototype was built in a Type 103 Verobox which provided an attractive and durable housing.

Constructors should decide, before choosing a case, whether the mains, or a battery supply is to be used. As there is no 6V battery of modest dimension readily available, a somewhat larger case than the suggested Verobox would be required. This factor, and the cost of replacement batteries, led to the author's choice of a mains power supply for the prototype. See Fig. 3.

The main printed circuit board (Fig. 4) was secured by means of the meter terminals only; a method found to be quite satisfactory. With the depth of meter body used, the leads of the eight l.e.d.s were found to be just long enough to allow them to protrude through the front panel (see photograph). Mounting clips were not used as these would have made assembly and subsequent removal very difficult, and with the correct size holes a more attractive appearance is presented. Note from the photograph that the l.e.d.s are mounted on the *copper* side of the p.c.b. See Fig. 5 for assembly of the p.c.b.

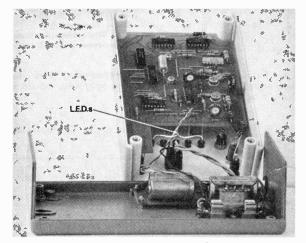
Use of the suggested printed circuit board layout is to be recommended due to the complexity of the design. There is, however, no reason why other forms of construction may not be used. If a mains supply is decided upon, note that the mains earth is *not* connected to the instrument ground. It is desirable, therefore, to use a transformer with an earthed interwinding screen, and to ensure that the instrument is connected particularly carefully where the mains wiring is concerned. Care should also be taken to ensure that this mains wiring is kept as far away as possible from the high impedance input components, as this area is susceptible to hum pick-up. Because of the rectifying action of the meter driver, any a.c. signal present at the input will register as a d.c. voltage on the meter.

The resistors used to select the amplifier gains (R3, R4 and R6) and the \pm balance resistor R8 might advantageously be mounted on extension pins which would aid component changing if required during the calibration procedure.

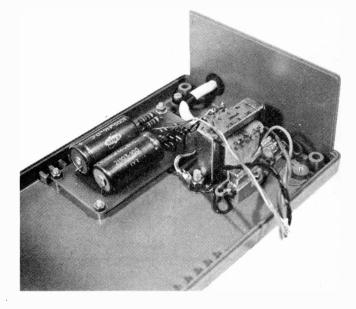
As most of the i.c.s use MOS technology, the appropriate handling precautions should be taken.

The CA3140 was chosen for IC1 as it requires no phase compensation. If this fairly new device is not readily available, a CA3130 may be used instead, with a 47pF ceramic capacitor connected between pins 1 and 8 on the copper side of the board.

If the recommended meter is used, it will need to be re-scaled as shown in Fig. 6.



Note the cut out power supply section from the main p.c.b. Also that the l.e.d.s are mounted at maximum length from the board on the conductor side



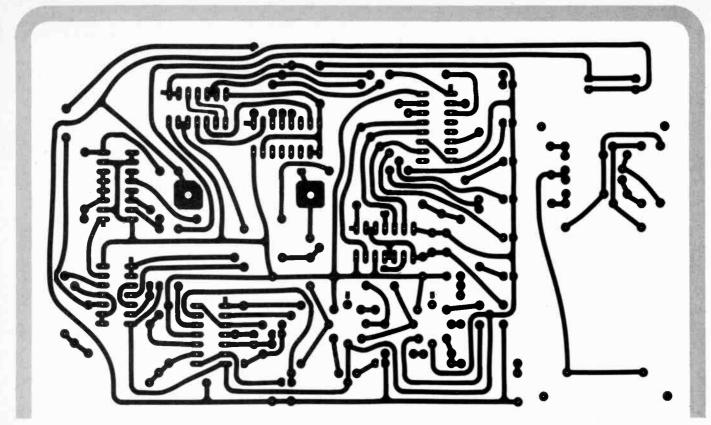
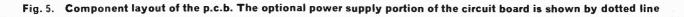
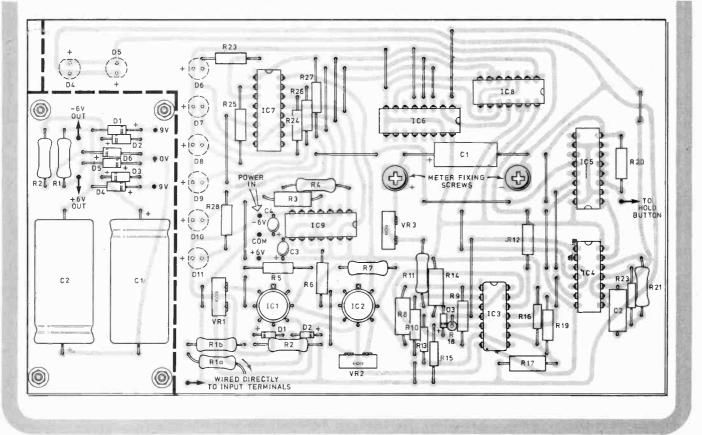


Fig. 4. Printed circuit board layout (full size). The power supply board is included on the same layout so that both can be etched simultaneously. The power supply area would still need to be cut out even if batteries are to be used. Note the shape of the p.c.b. in the photographs





AUTO-RANGING D.C. VOLTMETER

COMPONENTS . . .

BASIC AUTO	D-RANGING D.C. VOLTME	IEK
Resistors		
R1	$9.1 M \Omega + 620 k \Omega$ in series	
R2	300kΩ	
R3	820 Ω*	
R4	10kΩ*	
R5	100kΩ	
R6	10kΩ*	
R7	27kΩ	
R8	1kΩ*	
R9	1kΩ	
R10	470Ω	
R11	56kΩ	
R12	680 Ω	
R13	47kΩ	
R14	30kΩ	
R15	27kΩ	
R16	47kΩ	
R17	6·2kΩ	
R18, R19	1MΩ (2 off)	
R20	100k Ω	
R21	82kΩ	
R22	39k Ω	
R23–28	1·2kΩ (6 off)	
All resist	ors are ¼W 5% carbon.	
*Resistor	s to be selected on test, see to	ext.

AUTO RANGING VOLTMETE

Capacitors

- C1 1000pF polyester
- C2 22µF 25∨
- C3, C4 10µF 10V tant (2 off)

Diodes

D1, D2 BZY88C4V7 zener (2 off) D3 1N914 D4-D11 0.2" red l.e.d. (8 off)

Integrated Circuits

101	0/10/1407
1C2	μA741 T
1C3	RC4136D

- IC4 CD4001
- IC5 CD4048
- IC6 CD4518
- IC7 CD4028
- IC8 CD4001
- IC9 CD4066

Miscellaneous

- S1 Single pole, push-to-make
- Case 110mm \times 188mm \times 60mm
- M1 50 μ A panel meter (with scale recalibrated)
- P.c.b.
- 4mm plugs and sockets, wire, and prods for probes

COMPONENTS . . .

OPTIONAL MAINS SUPPLY

Resistors

R1, R2 330 ¼ W carbon (2 off)

Capacitors

- C1, C2 1000μF 25V (2 off) C3, C4 10μF 10V (2 off)
- 00, 04 1001 101 (2 011)

Diodes

D1-D4 1N4001 (4 off) D5, D6 BZY88C6V2 Zener (2 off)

Miscellaneous

- S1 Sub min d.p.s.t.
- F1 250mA and suitable holder
- T1 9-0-9V mains transformer with screen
- P.c.b. to design given

CONSTRUCTOR'S NOTE

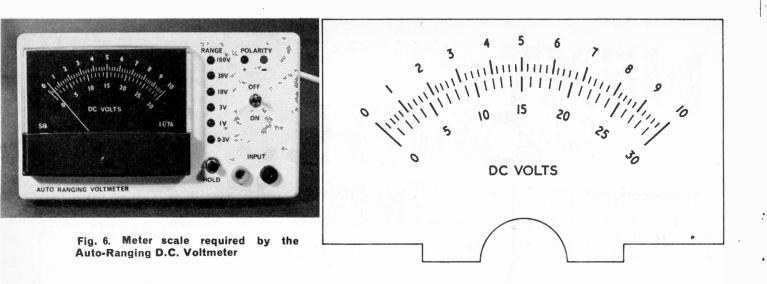
If the recommended p.c.b. design is used, the CA3140T type should be ordered for IC1 (T stands for 8-lead TO5 package).

Since P.E. does not operate a p.c.b. service we cannot quote a supplier of ready made boards for those who do not wish to make their own, but we can advise that readers keep an eye on P.E. advertisers who specialise in p.c.b. manufacture, and have in the past generally followed up with a service.

The "Large Moving Coil Meter" is available from Maplin Electronic Supplies (see advertisers' index for address).

The RC4136D (IC3) is made by Raytheon, and available from **Distronic Ltd.**, 50/51 Burnt Mill, Elizabeth Way, Harlow, Essex. Tel: Harlow 32947. Type RC4136DP may be used (D stands for d.i.l. and P for plastic).

The estimated cost to build this unit using all new parts, is in the region of $\pounds 25$.



TEST AND CALIBRATION

Before first switch-on, all preset pots should be at approximately mid-range. Any meter reading should be ignored for the present, although a large offset in IC1 may cause a range change, necessitating adjustment of VR1 to cancel this effect.

Odd combinations of RANGE l.e.d.s, or "searching" should be resolved during calibration, and this procedure is as follows:

(A) Set zero

- (1) With the power off, set the meter mechanically to zero.
 - (2) Switch on. Check that the 0.3V range is indicated, and allow a few minutes for thermal stabilisation.
 - (3) Short 1C2 pin 3 to the zero volt rail. Adjust VR2 for minimum reading on the meter. Remove short.
 - (4) Short input. Adjust VR1 for minimum reading. The meter should now read zero.

(B) Set positive/negative balance

- (1) Apply an input to the meter and adjust for a convenient reading.
- (2) Reverse the connections to the meter and check that exactly the same reading is displayed. If not, adjust R8 as necessary.

 Table 1. Should a fault exist, this table may be used to check the switching functions. Check all supply voltages first

COUNTER	SWITCHES	IC 1 GAIN	IC 2 GAIN	TOTAL GAIN	RANGE
0	-	×1	×1	×1 ,	1007
1	A	×1	x 3·3	x 3.3	30V
2	В	×10	×1	×10	107
3	A,B	×10	×3.3	x33	3V
4	C	×100	×1	×100	17
5	A,C	× 100	3.3	x 333	0-3V
6	в.с]		SETTINGS - COUNTER		
7	A,B,C	ATTEAN	- COSNIER	ALL IS A	

(C) Set meter calibration

This adjustment compensates for any small inaccuracy in the input attenuator.

- (1) Apply about 50V to the meter input, thereby selecting the 100V range.
- (2) Check meter reading against a known good meter.
- (3) Adjust VR3 for correct reading.

(D) Check ×100 amp gain

- (1) Apply about 0.5V to input, thereby selecting 1V range.
- (2) PRESS HOLD. Adjust input voltage to 1V exactly
- (3) Check that meter reads IV. If not, adjust R3 for an acceptable result.

(E) Check ×10 amp gain

- (1) Apply about 5V to input, thereby selecting 10V range.
- (2) Press HOLD. Adjust input to 10V exactly.
- (3) Check that the meter reads 10V. If not, adjust R4 for an acceptable result.

(F) Check ×3·3 amp gain

- (1) Apply about 15V to input thereby selecting 30V range.
- (2) Press HOLD. Adjust input voltage to 30V exactly.
- (3) Check that the meter reads 30V. If not, adjust R6 for an acceptable result.

(G) Check upper range-change point

(1) The range should change to the next highest at about 90 per cent of full-scale reading. If not, adjust R14/R15 as necessary.

(H) Check lower range-change point

(1) The range should change to the next lower at about 20 per cent of full scale. Adjust R16/R17 if necessary.

This completes the calibration, and the instrument, if correctly set up, should conform to the figures in the specification.

Acknowledgement

The author would like to thank Mr. D. Bowers for his helpful comments and suggestions during this project.

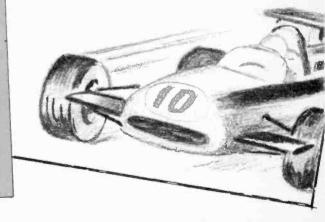


Employing modern delay line technoreverberant orchestral string sounds. Additional time and variable envelope controls can be mixed to produce a wide spectrum of sound. Features include:

- * Split keyboard with register variance in both
- * Four selectable pitches to match accompanying musical instruments
- Single contact electronic keyswitch action
- * CMOS i.c.s throughout divider circuitry
- Unique CMOS chorus drive circuitry *
- Third cost of equivalent commercial instrument

DIGITAL LA COUNTER

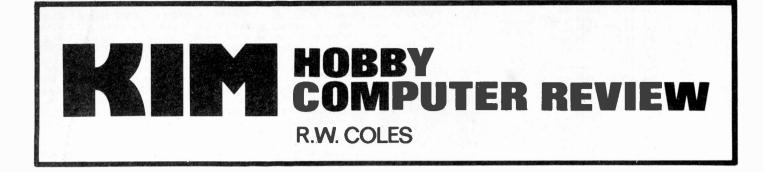
Eliminates any argument when staging a model car race. This system does not impede the cars in any way and can be used to turn off the power after a preset



PRACTICAL RONICS

OUR MARCH ISSUE WILL BE ON SALE FRIDAY, FEBRUARY 10, 1978

PE



THE LAST twelve months have been very exciting for anyone interested in microprocessors and their application.

Of course, these fascinating and powerful devices have been around for several years now and have already taken the professional electronics industry by storm, but it is really only in the last year or so that microprocessor manufacturers have turned their attention squarely towards the needs of the electronic and computer hobbyist, with some very interesting results.

The hobby market trail blazer (in terms of wide availability anyway) was the National Introkit which featured the SC/MP microprocessor. The Introkit was of course reviewed within these pages earlier in the year, and reviews of other units like the Intercept Junior, featuring the IM6100 MPU chip, and the Motorola D2 kit featuring the M6800, were soon to follow.

To start with, manufacturers were a I o start with, manufacturers were a little lazy about just who they were aim-ing their "small system" designs at. Their cautious approach was obvious from the way systems were described as "Proto-typing systems", "Introductory systems", and "Tutorial systems" with manuals written, it seemed, for professional engi-neers who were expected to rapidly move neers who were expected to rapidly move on to bigger and better things, with their loyalty to a particular MPU chip already established! With the unexpected mushrooming of the hobby computer market in the U.S.A. manufacturers soon realised that a huge new market had arisen, and also that this new breed of hobbyist was not going to be satisfied with a cheap system which had a limited use-fulness and future. The average amateur was not likely to move on to a de-luxe development system with floppy discs and a teletype: he wanted a low cost system which nevertheless could be used to do practical things, a system which had inputs and outputs available for his use, a system with a self-contained keyboard and display, a system with a reasonable RAM memory capacity, a system which could use low cost peripherals such as cassette tape recorders, and of course, above all, a system which he could expand when he felt the need for more performance.

HOBBY COMPUTER

KIM-1 is the result of a deeper understanding of the requirements of hobbyists, and is a successful attempt to provide the amateur with the things he needs at a realistic price. KIM-1 is a design from M.O.S. TECHNOLOGY, INC. and uses their own 6502 microprocessor array in a ready built system which arrives tested and guaranteed for 90 days. The cost of KIM-1 is around the £200 mark, but for this you get a well made microcomputer circuit board which includes a hexadecimal keyboard and 8 digit l.e.d. display, an audio cassette interface, 1,024 words of RAM storage, a comprehensive monitor program in 2,048 words of ROM and 15 input/output lines available on an edge connector. In addition to the KIM-1 board itself, you get a User Manual, a Programming Manual, a Hardware Manual, a system wall chart and a programmer's reference card. The three manuals together are no less than 4cm thick, and even at first glance these appeared to be very comprehensive to us!

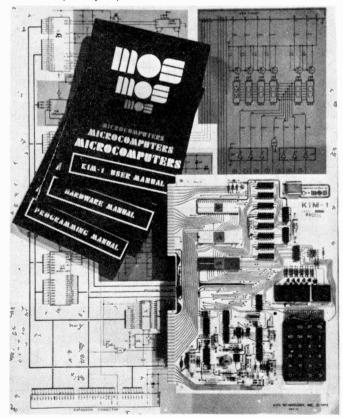
With a full 1k of user RAM available from the start, a KIM-1 owner is unlikely to feel cramped for space for quite a while, especially since programs can be stored on, and retrieved from, conventional cassette tapes with the simple addition to the system of a low cost audio cassette recorder. As a user becomes more ambitious however, the KIM-1 board can be augmented with the KIM-2, 3, 4, or 5 boards which will provide sufficient extra RAM memory to run sophisticated high level software, like BASIC for example, when this becomes available.

The 6502 microprocessor and associated circuits require only a single 5 volt supply which can be easily put together using a fixed voltage LM309K regulator. When a cassette recorder is used, an additional low current 12 volt supply is required to power the interface circuitry.

THE MPU CHIP FAMILY

The MCS6502 chip used as the heart of KIM-1 is one member of a large family of microprocessor chips produced

At a price of £199 upwards, the KIM-1 is supplied as an assembled and tested microcomputer with keyboard, display and full documentation. Available from GR Electronics Ltd., Newport, Gwent



		_		
Vss -	1	40	⊢	RES
RDY -	2	39	⊢	B2 (DUT)
1 (OUT) -	3	38	⊢	S.O.
IRO -	4	37	F	Ø0(IN)
N.C	5	36	F	N.C.
NMI -	6	35	F	N.C.
SYNC -	7	34	⊢	R/W
Vcc -	8	33	⊢	DBO
AB0 -	9	32	F	DB1
AB1 -	10	31	F	DB 2
AB2 -	11	30	\vdash	DB3
AB3 —	12	29	F	DB4
AB4 -	13	28	F	D85
AB5 -	14	27	H	DB6
A86 -	15	26	⊢	DB7
AB7 —	16	25	-	AB15
AB8 -	17	24	⊢	AB 14
A89 —	18	23	\vdash	AB 13
AB10 -	19	22	⊢	AB 12
AB11 -	20	21	\vdash	Vss
	MCS650	02		

The MCS6502 microprocessor chip used in KIM-1.

by M.O.S. TECHNOLOGY, INC. Many readers may be unfamiliar with this manufacturer and the MCS 65XX series of MPU chips, although they are fairly well known in the U.S.A. The family is described by M.O.S. as "Third generation" and it is certainly true to say that several advanced features are available within the family, which obviously owes a lot of its basic design to the Motorola M6800 chip with which its members are bus compatible.

There are nine microprocessors in the family and these offer complete software compatibility (the same instruction set) but differing hardware features such as 28 or 40 pin package, on or off chip clocks, varying address range from 4k to 65k words, and choice of interrupt facilities. All members of this family offer NMOS high speed (2MHz maximum) operation and a very efficient instruction set with 56 basic instructions. The MCS6502 is an on chip clock, 40 pin package version with an address range of 65k words, making it a very sophisticated device with lots of potential.

PERIPHERAL CHIPS

Also on the KIM-1 board are two MCS6530 chips, and these devices are not microprocessors but a powerful combination of a ROM array, a RAM array, an Interval timer and two eight bit input/ output ports, all in a single 40 pin package! It is probably the availability of these devices which makes the KIM-1 possible at such a low price, because providing these facilities separately would certainly be expensive! Each MCS6530 contains 1,024 words

Each MCS6530 contains 1,024 words of mask programmed ROM normally used to hold programs, and 64 words of RAM which can be used for scratch pad storage, stacks, etc. The interval timer is a down counter which can be preset under program control, and which will interrupt the MPU chip when a count of zero is reached. Under program control the MCS6530 timer can be used to generate a wide variety of timing functions which allows this important system task to be unloaded from the microprocessor itself, promoting software efficiency.

The sixteen input/output lines are individually programmable as either inputs or outputs under software control, and they can source 3mA at 1.5 volts when used as outputs, making interfacing straightforward.

CAUTION

One word of caution on the MCS6530; its ROM section, being mask programmable, is unsuitable for use in any "homebrew" system, although of course,

KIM-1 block diagram.

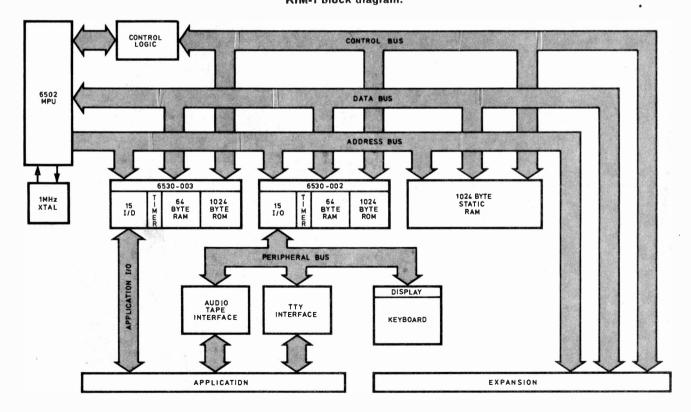
it is ideal for the KIM-1 itself where the monitor program is loaded during manufacture by M.O.S. themselves. A homebrew system *would* be possible using external EPROM chips such as the 2708 or 1702A, if required.

User program storage on the KIM-1 board is provided by eight 1024 by 1 bit 2102 type NMOS RAM chips, although as you will have gathered from the description of the MCS6530 chip, a further 128 words is available if required. The basic address range of KIM-1 is 8k words, with the MCS6530 ROM, RAM 1/O and TIMERS mapped into the upper three 1k pages, and the user RAM mapped as the lower 1k page. Expansion to the full 65k words can be carried out externally at a later date if desired.

OUR EXPERIENCES

With the system up and running with the aid of a bench 5 volt supply, we tried out the simple program on page 9 of the User Manual. The method of program entry is, in our opinion, better than the MEM, TERM system used on the SC/MP Introkit, because it is much simpler. To set an address you press the AD key followed by *four* HEX digits. To enter instructions or data you press the DA key followed by *two* HEX digits, and to increment to further locations for further entries you press the + key followed by the next two HEX digits and so on. To run a program you enter its start address using the AD mode, and press the GO key.

The other keys available are RS, which causes system reset, ST which terminates the current program and PC which allows you to display the value of the program counter at the time that an interrupt occurred or the ST key was pressed. Execution can be continued from where it was stopped by the ST key by pressing



the GO key. A slide switch on the keyboard allows you to enter the "singlestep" mode so that single instructions are executed for each press of the GO key.

key. With a feeling of "So far so good", we hooked up a 12 volt supply in addition to the 5 volts already connected then blew the dust off of our portable cassette recorder and connected it up, too, following the simple diagram in the manual.

CASSETTE

The KIM-1 monitor program controls the storage and retrieval of data on the cassette, and when recording a program a checksum is added in at the end so that verification is possible during replay into KIM-1 RAM. Each program must be given a unique "name" before recording takes place, and this "name" (actually a two digit HEX code) is used to identify the required program on replay. We dumped the simple trial program from RAM onto a cassette, switched off the power, and then attempted to reload it into RAM—failure!

After a lot of experimentation we discovered that it was necessary to use different volume control settings for record and replay to get the system to work. Now this might have been the fault of our cassette recorder, which was not new but seemed perfectly serviceable, but the manual certainly led us to understand that a unit of the type we used would be quite satisfactory, and that no adjustment of the controls would be required.

After some practice the record and replay functions were operating correctly most of the time, and we began to realise the enormous advantages of the cassette system compared with the pencil and paper method of storing programs! By hooking up a microphone to the recorder it is also possible to cue programs verbally on the tape, so that both you and your KIM-1 know what's going on! (Voice signals are ignored by the monitor routines on replay.)

K1M-1 also comes with a routine for handling teletypes or VDUs of any standard baud rate, and is equipped with a 20mA current loop interface for this purpose. We were unable to try out this particular aspect of system operation however.

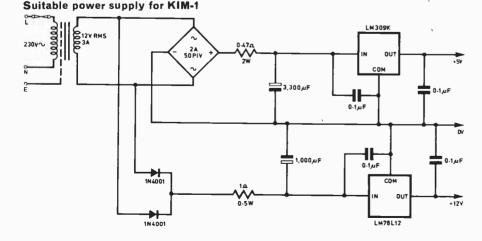
MCS6502 MICROPROCESSOR INSTRUCTION SET-ALPHABETIC SEQUENCE

ADC	Add Memory to Accumulator with	
	Carry	
AND	"AND" Memory with Accumulator	
ASL	Shift Left One Bit (Memory or	
	Accumulator)	
BCC	Branch on Carry Clear	
BCS	Branch on Carry Set	
BEQ	Branch on Result Zero	
BIT	Test Bits in Memory with	
	Accumulator	
ВМІ	Branch on Result Minus	
BNE	Branch on Result not Zero	
BPL	Branch on Result Plus	
BRK	Force Break	
BVC	Branch on Overflow Clear	
BVS	Branch on Overflow Set	
CLC		
	Clear Carry Flag Clear Decimal Mode	
	Clear Interrupt Disable Bit	
CLV	Clear Overflow Flag	
CMP	Compare Memory and	
0 D V	Accumulator	
CPX	Compare Memory and Index X	
CPY	Compare Memory and Index Y	
DEC	Decrement Memory by One	
DEX	Decrement Index X by One	
DEY	Decrement Index Y by One	
EØR	"Exclusive-or" Memory with	
	Accumulator	1
INC	Increment Memory by One	1
INX	Increment X by One	
INY	Increment Y by One	'
JMP	Jump to New Location	1

JSR	Jump to New Location Saving
	Return Address
LDA	Load Accumulator with Memory
LDX	Load Index X with Memory
LDY	Load Index Y with Memory
LSR	Shift One Bit Right (Memory or
NØP	Accumulator)
	No Operation
ØRA	"OR" Memory with Accumulator
PHA	Push Accumulator on Stack
PHP	Push Processor Status on Stack
PLA	Pull Accumulator from Stack
PLP	Pull Processor Status from Stack
røl	Rotate One Bit Left (Memory or
-	Accumulator)
rør	Rotate One Bit Right (Memory or
	Accumulator)
RTI	Return From Interrupt
RTS	Return From Subroutine
SBC	Subtract Memory from Accumulator
	with Borrow
SEC	Set Carry Flag
SED	Set Decimal Mode
SEI	Set Interrupt Disable Status
STA	Store Accumulator in Memory
STX	Store Index X in Memory
STY	Store Index Y in Memory
TAX	Transfer Accumulator to Index X
TAY	Transfer Accumulator to Index Y
TSX	Transfer Stack Pointer to Index X
TXA	Transfer Index X to Accumulator
TXS	Transfer Index X to Stack Pointer
ТҮА	Transfer Index Y to Accumulator

VERDICT

The thing which impressed us most about the KIM-1 system was the provision of the three excellent manuals which between them covered all aspects of system operation and programming in minute detail. Anyone with a basic knowledge of microprocessors, or computers in general, should be able to find their way around easily with the aid of these books. The User Manual is written in a chatty informal style which puts the reader at ease right from the word "go". Following this book in step-by-step fashion is rather like taking a programmed learning course, and most KIM-1 owners will find themselves eager to delve into the other two manuals, which are rather more formal, once they have mastered its contents.



On the hardware side, the powerful MCS6502 chip, the full 1k of user RAM and the cassette interface, speak for themselves.

KIM-1 also has that magic ingredient "expendability" so that owners need not feel boxed in. Expansion can be carried out without a soldering iron, and those who look forward to a powerful "Home computer" have every chance of achieving this later if a VDU or teletype is added to the system, and the manufacturers start to provide software on cassette (which is likely). As it is, the basic KIM-1 can be programmed easily in machine code, and can of course be connected up directly to external gadgetry by means of the input output lines, if required.

The instruction set of the MCS6502 has some powerful features, like 13 addressing modes, and the ability to set the arithmetic unit to "Decimal mode" for the duration of a B.C.D. calculation rather than having to use "Decimal adjust" instructions as is the case with other devices. The mnemonics looked easy to learn to us, although they are different to those used with the 8080, or the 6800 its two major competitors.

The construction and component quality looked good. We noticed that the cassette recording format is not of the "Kansas City" type, which means a black mark. although the system used is self clocking which is to its credit. The seven segment displays were a little difficult to decipher in high ambient lighting, but we soon cured this by adding a piece of red filter material.

All in all then, the K1M-1 seems a good buy for all low-budget micronuts, and a useful step nearer that impossible dream, the "perfect" system.



BAR DRIVER

Sometimes a digital display can actually be inferior to more traditional analogue displays such as the moving coil meter. This is particularly true where useful information can be gleaned from the rate of change of a reading, or where a simple comparision is required between the current reading and some pre-set or variable limit. Needless to say, electronics manufacturers have not just ignored this requirement, and there are a number of alternatives to the moving coil meter presently available.

One of the more attractive of these is the bar graph display, where a , column of light of variable length provides an easy to read analogue display. Bar graph displays can be made up with bar type l.e.d.s, but where high definition is required the l.e.d. solution is rather costly and power hungry, and so recourse to gas discharge technology is essential. Burroughs of the U.S.A. make an excellent dual gas discharge bar graph display which has become increasingly popular as an alternative to more conventional analogue readouts, but until now the peripheral drive circuitry to control this useful device had to be built with a collection of TTL and analogue circuits which could fill a fair sized board.

Thanks to Signetics, the Burroughs "Self-Scan" bar graph display is now a lot easier to use because a new i.c., the **NE580** has been introduced which contains 80 per cent of the necessary drive circuitry.

The "Self-Scan" display contains two 201 element bar graphs and is driven in a multiplexed fashion which requires the generation of 200 cathode clock pulses in an interlaced five phase sequence.

The display anodes are switched on at the start of a scan and off when the appropriate display level is reached, and this is accomplished by comparing the signal voltage with a reference voltage ramp. The NE580 contains most of the required external circuitry, including a clock oscillator, sample hold, ramp generator, counter, phase decoder, comparators and anode switches and requires only cathode and anode drivers to complete the system. The NE580 is housed in a 22 pin d.i.l. and runs from a single five volt supply. An example of the chip in action is shown below.

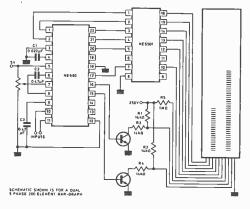
BIT BY BIT

After the four bit micros came the eight bit micros, and after the eight bit micros came the sixteen bit micros . . . but if you are expecting me to present a sneak preview of a thirty two bit mega-chip . . . forget it!

However, the latest, hottest chip from the microprocessor men is, wait for it, a one bit processor called an "Industrial control unit" (i.c.u.) by Motorola, the manufacturers.

The new i.c.u. has been coded **MC14500B**, making it a standard 1400 series buffered CMOS part which will be taking its place alongside the MC14001B quad gate and all the other common-or-garden logic blocks in the family.

If up to now you have been a "doubting Thomas", and still think that micros are a passing fad, the MC14500B is all set to convince you otherwise! This new chip is a real microprocessor all right. It has a sixteen entry instruction set, on a chip clock oscillator, and is designed to be paired up with a ROM



or PROM program store, along the same lines as its bigger cousins.

The i.c.u. does differ from other micros in its bit-by-bit logic orientated instruction set, and it is not directly capable of the arithmetic type operations which are the bread and butter of other micros. For many applications, the conventional microprocessors are just too powerful, and so relay systems or printed circuit boards full of random logic are used instead.

The new chip runs from 3V to 18V supplies, and comes in a plastic sixteen pin package. The internal oscillator requires only a single external resistor to set the clock frequency to a value between d.c. and IMhz, and system expansion can be carried out using standard CMOS components to provide input parts, output parts, and program counters of any length. With only a sixteen entry instruction set, programming should be child's play, and you can use existing TTL fusible link PROMs or the newer CMOS types to hold the programs once written. I forsee a big future for this unexpected infant!

FET DIODES

We all know that when we require a source of constant voltage the easiest way to provide it is to employ a Zener diode with the required voltage rating. But what about a source of constant current?

Probably the way most of us tackle this is to use a Zener in conjunction with a transistor and a couple of resistors—but there is a much simpler alternative in the form of the two terminal f.e.t. current regulator diode.

A better way would be to employ one of the Teledyne Crystalonics f.e.t. diodes which are produced in a range which will give accurate current regulation from 220 microamps, to 4.7 milliamps.

Thirty two devices are available coded **1N5283** to **1N5314**, and these can be put to good use in a wide range of analogue circuits. A NYONE looking for a simple and novel project to build, just for fun, may be interested in the Strength Meter described in this article.

The power of the contestant's grip is displayed on a row of l.e.d.s while he squeezes two cannisters as tight as he can. However, the indicator is not to be treated with scientific reverence since it *really* works by measuring the resistance between the hand-grips.

CIRCUIT DESCRIPTION

The circuit shown in Fig. I is designed so that the number of l.e.d.s which illuminate along the row comprising D1 to D4, increases as the resistance between the hand-grips falls; which of course happens when the contestant squeezes harder.

A potential divider is produced between 0V and +9V by R1 and R2, and since their resistance ratio is 1:1, the voltage at point "B" will be half the supply, which is +4.5V. The differential amplifier formed by IC1 uses this voltage as a reference, so that it amplifies the difference between points "A" and "B".

Voltage "A" however, is produced by a potential divider of variable ratio, which is dependent on the hand-grip resistance. This voltage, for any given degree of hand-grip squeeze, can be set using VR1, but the voltage generated by zero squeeze (no hand-grip contact at all) always starts of from 0V. This "slope" setting will also determine the amount of grip necessary to pull up all four l.e.d.s.

After amplification in the non-inverting amplifier IC1, the generated voltage is fed to the base of TR1. This stage has no voltage gain (some voltage will in fact be lost across the base-emitter junction), but simply multiplies the output current capability of the 741 by the gain figure of the BC107, a figure which of course will vary from one such transistor to another due to production spread. But in any case TR1 will add sufficient current drive to take the load consisting of the resistor chain R5 to R9.

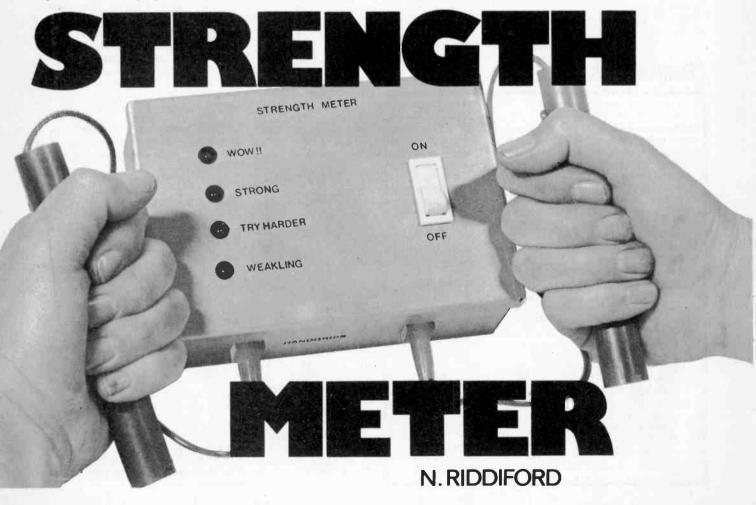
The point of the resistor chain is to divide the voltage produced at point "C" into five equally spaced potentials. This way, as the voltage at "C" increases, the voltage at "D" will eventually become sufficient to overcome the baseemitter junction potential of TR2, plus a little more to push some current through R10. When this happens D1 will illuminate as TR2 switches into conduction.

If the voltage at "C" continues to increase, then the voltage at "E" will become sufficient to bias TR3 into conduction, and so on, until all the l.e.d.s are illuminated. Just as R10 to R13 limit the base current to their respective transistors, resistors R14 to R17 limit the l.e.d. currents to around 17mA.

CONSTRUCTION

The circuit was built on a piece of 0.1 inch matrix stripboard and the layout, shown in Fig. 2, will accommodate either an 8-pin d.i.l. or the 14-pin version of the 741 amplifier. Care should be taken to ensure that the appropriate breaks are made to the copper tracks, and that no blobs of solder or shavings of copper form a bridge between conductors.

A simple aluminium box was used for the prototype, and this could be formed from a sheet of metal if a



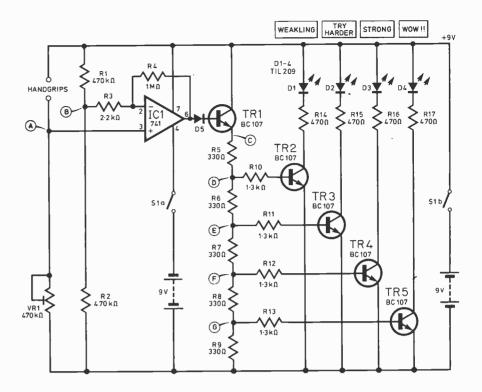


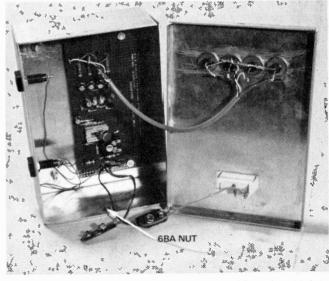
Fig. 1. Complete circuit diagram of Strength Meter. The diode D5 protects TR1 from a negative voltage swing at IC1 output. Although the photographs show a single-pole on/off switch, the arrangement detailed in this circuit diagram is recommended, and uses a two-pole rocker for total switch-off

COMPONENTS . . .

Resistors	
R1, R2	470k Ω
	2-2kΩ
R4	1ΜΩ
R5-R9	330Ω (5 off)
R10-R13	1·3kΩ (4 off)
R14-R17	470Ω (4 off)
All resist	ors ↓ W 5% carbon film
Potentiom	eters
VR1 470	kΩ horizontal preset
Semicond	uctors
IC1	741 8- or 14-pin d.i.l.
	BC107 or similar (5 off)
D1-D4	0-2 inch red l.e.d. (4 off)
D5	1N4148 or similar
Miscellane	OUS
0.1 inch s	tripboard 127 $ imes$ 63mm
14-pin i.c.	. socket (optional)
4mm plug	s and sockets (2 of each)
PP3 batte	eries (2 off)
Case: 155	5 $ imes$ 105 $ imes$ 53mm, or sheet alloy to form
Suitable I	battery studs (2 off)
Plastics	.e.d. bezels (4 off)
Rocker tv	pe on/off switch D.P.C.O.
	or handgrips

suitable size cannot be found ready made. Four holes should be drilled in the base to accommodate 4BA screws for fixing rubber feet to the unit. Two of these screws should be long enough to take spacers, the stripboard and fastening nuts. Two holes need to be drilled to mount the 4mm sockets, and a further four in the lid to house the l.e.d. bezels. Finally an oblong hole should be cut out (using an Abrafile) if the R.S. type switch is used for the ON/OFF function.

The prototype box which was "home made" had 6BA nuts held in place on the side of the base, by an epoxy resin glue, to take the lid retaining screws (see photograph).



The 741 op amp in this photograph is a TO5 type, which is not the recommended i.c. package

If the box is "home made", 6BA nuts to take the lid retaining screws can be fixed to the case using Araldite Rapid or similar resin based adhesive

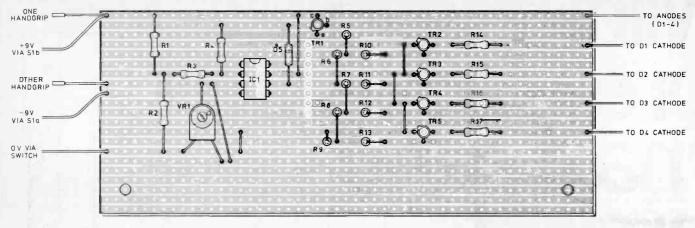
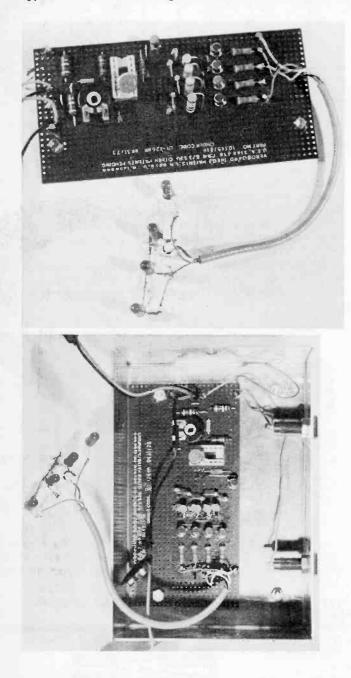


Fig. 2. Stripboard layout. A 14-way i.c. socket may be used for IC1, which can be positioned to allow either 8-pin or 14-pin 741s to be used without stripboard modification. As can be seen in the photographs, this would even allow an 8-lead TO5 type to be used if necessary. Note that R4 is connected to the wrong end of D5 in this diagram



BATTERY RETAINERS

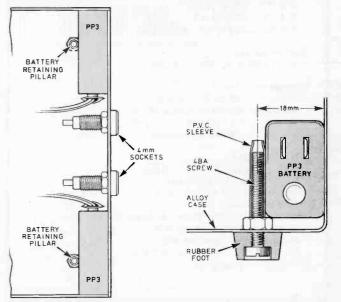
It was felt that a small modification to the prototype featured in the incidental photographs could be made, which would provide a simple but effective means of clamping the PP3 batteries.

If the "rubber feet" screws nearest to the 4mm sockets are positioned 18mm away from *that* inside edge, and are about 25mm long, then they can be used as battery retaining pillars, whereby the PP3s will squeeze between *these* and the side of the case (see Fig. 3). Lengths of p.v.c. sleeving should be slipped over them to improve appearance and protect the batteries from damage. Some sleeving stripped from 3-core mains cable (lightweight type) will do admirably for this!

If this is done, the 4mm terminals will need to be mounted nearer the centre-line of the box (at about 30mm apart) to make room for the PP3 batteries.

continued on page 417

Fig. 3. Using the 4BA "rubber feet" screws to create battery retaining studs. The positions of the rubber feet and 4mm sockets necessary for this facility will be slightly different from those appearing in the photographs



Mini-priced breadboards for maxi-sized projects.

Experimentor* low-cost solderless breadboards are the first in the world specially designed for 0.3" and 0.6" pitch DIP's.

They clip together by an exclusive interlocking system in any configuration, (just like dominoes), so you arrange the breadboards to suit your circuit, not vice-versa.

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EXCLUSIVE INTERLOCKING SYSTEM.

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BOTTOM TOP

Contact resistance is a mere 0.4 m o and interterminal capacitance is typically less than 5 pF. The Experimentor is usable to over 100 MHz.

Experimentor 600 and 650 models are ideal for RAM's ROM's and PROM's (0.6" centre IC's) while the 300 and 350 models are for smaller DIP's (0.3" centres). All four models, of course, also take all standard components, the 0.1" grid being compatible with transistors, diodes, LED's, capacitors, resistors, pots - in fact any component with lead sizes between 0.015" and 0.032."

.....

A useful quad bus strip (EXP4B) further

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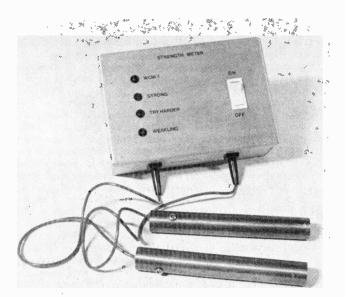
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HAND-GRIPS

The hand-grips can be made from a number of things such as curtain or stair rod, or as in the prototype, 18mm diameter brass tubing. To connect wires to these it is necessary to drill a hole in each, so that a 6BA nut and bolt can be passed through to clamp a solder tag. The wires should be soldered to the tags *before* clamping them, as objects showing thermal inertia of this magnitude will not solder readily without a very large soldering iron indeed.

The prototype used 4mm plugs and sockets to terminate the hand-grips, so that they can be disconnected, wrapped in something soft, and then stored inside the case. If the recommended size is used, there will be ample room for this.

SETTING UP

The potentiometer VR'I should be adjusted so that a gentle hold on the hand-grips will just illuminate D1, the WEAKLING light.



Exhibition

THE 1978 FEA (Instruments, Electronics and Automation) Exhibition will be held at the National Exhibition Centre, Birmingham, from March 13-17.

A computerised visitor registration and enquiry system will be operating in four languages, and this will give specific information on product categories and exhibitors to the visitor, thus providing a mutually beneficial two-way service.

The exhibitors will be of a highly international mixture, consisting of manufacturers ranging from passive components right through to computerised machine automation, and they will occupy the largest hall at the centre.

The exhibition is claimed to be the only recognised trade fair of 1978 in the U.K. covering the electronic instruments industries, and will again be held alongside ELEC-TREX, following their successful coming together in 1976.

Watts On The Road

THE first three of a planned 62 strong fleet of electric delivery vans hit the roads of London in November last year, as part of a three year plan to assess the performance of electric vehicles in urban conditions.

The machines are confined to the 0.75-1.75 tonne range, with high acceleration, regenerative braking, top speeds of around 50 m.p.h., and a realistic range of up to 60 miles per charge-up.

Under the scheme the Department of Industry is contributing in all, up to £400,000 to users of these vehicles to offset the cost over that of conventional vans.

Co-operation between the DoI, the manufacturers, the operators, the Department of Transport and the GLC, has led to the use of three types of electric vehicle being used in the scheme: 12 vehicles from Crompton Electricars, 25 "Silent Karriers" from a consortium of Chloride Technical, Chrysler Motors and the National Freight Corporation, and 25 "Bedford CF Vans" from Joseph Lucas Ltd. in association with Vauxhall Motors.

The GLC will collect data from such operators as Initial Services and National Carriers for collating, and a final report will be published by the DoI upon conclusion of the scheme.

Microcomputer Kit

In the face of much criticism concerning the potential usefulness of microcomputers in the home, Lynx Electronics have launched the NASCOM 1 microcomputer kit which carries a basic price tag of $\pounds 197.50$ plus VAT. The launch came as part of a seminar entitled Home Microcomputer Symposium which was attended by some 550 people. Over 300 kits were sold in the two weeks following the launch.

The concepts of NASCOM 1, as described by Mr K. Borland of Lynx, were: "To produce for sale a complete microprocessor system that is of intelligent use to the home users and is priced around $\pounds 200.00$.

By using the best available product on the market, within our price range, to design the maximum possible system. This is an advantage that an independent design has over an in-house design by a manufacturer with his own product range.

To design for maximum control by software. By the choice of components it should be possible to totally minimise the constrictions of hardware.

To design a system that offers major future expansion. Either expansion by the user to his own design, or by additional Lynx products.

These were the four main ideas. It followed on that certain other details were going to be necessary.

Firstly, it would be essential in providing an intelligently usable system, to have a full keyboard. The limitations of a calculator type keyboard are now well known. Also any major expansion would make a full keyboard essential.

Secondly, there must be sufficient memory for the user to load and execute reasonably sized programs.

Thirdly, incorporate a fixed command program to allow easy user communication with the system.

We are delighted that it has been possible to achieve all these goals in the NASCOM 1."

For full details write to Lynx Electronics (London) Ltd., 92 Broad Street, Chesham, Bucks.



Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned. All quoted prices are those at the time of going to press.

DESK CALCULATOR

The newest calculator to be added to the **Sinclair** range is a desk top machine, the Sinclair President. This calculator has been specifically designed for the businessman whatever the task, be it balancing the yearly budget or working out the week's expense account. The President is exactly suited to the needs of the executive.

In style, the calculator strikes a well proportioned balance—not too heavy, yet not too light to serve as a genuine desk top model—the President will fit comfortably into a slimline briefcase.

Sinclair commissioned a consumer research programme among leading executives, and found that what was required was: a battery powered unit, but with mains option, a six function memory, a bright easy to read display, and single function keys. The President incorporates all of these!

The keyboard has a split layout. On the left are found the standard numerical and arithmetical functions, % key and six function memory. To the right are located functions specifically for 'business use, parenthesis, +/-, x < >y, \sqrt{x} , 1/x, x^2 , and π .

Reflecting its desk top role, the elegant satin silver President has a large bright blue angled display, and rubber feet which keep it stable during use.

Priced at $\pm 17.95 + VAT$ the President is available at all leading stores, and carries the usual Sinclair 12 month unconditional guarantee.

Sinclair Radionics Ltd., London Road, St Ives, Huntingdon, Cambs, PE17 4HJ.



Sinclair President desk top calculator

STOPWATCH

One of the pities of metrication is that it does not extend to time measurement. With a stopwatch you can assess quite accurately the length of one cycle in hours, minutes and seconds. But you can't immediately tell how long 100 cycles will take simply by shifting the decimal point two places. You have to work instead in sexagesimal arithmetic.

To the rescue come Casio Electronics Co with their new ST-1 stopwatch/ calculator. It will time any operation up to a maximum of about ten hours, to an accuracy of a tenth of a second, and then its calculator section will perform any of the four arithmetic functions you like, on that, or any other time. It can yield an answer in decimal hours and/or conventional hours. minutes and seconds.

Alternatively, the Casio ST-1 will handle ordinary decimal arithmetic, complete with independent memory, per cent and square root keys.

As a stopwatch, this instrument offers a choice of four modes: standard start/ stop with automatic reset at every start, time-out or net timing where a restart carries on from the previous stop time, and lap timing with or without reset at each start. There is also a totalling feature whereby in standard stop timing, it tells you the total of say, a series of separately timed operations (from which the average can be calculated on the same machine). In the time-out mode it can indicate time loss during stoppages, and in split lap timing it adds the "splits" to give an overall time.

The calculation capacity is eight digits, or one second short of 100 hours, and there is a clip-on hood for increasing readout contrast in strong ambient light.

Measuring approximately $127mm \times 76mm \times 25.4mm$ and weighing under 5 ounces complete with AA size battery, Casio ST-1 sits neatly in the hand. Supplied with security wrist strap, this amazing little instrument has a recommended retail price of only £29.95.

Casio Electronics Co. Ltd., 28 Scrutton Street, London, EC2A 4TY.



SCRUMPI 2

Following the microprocessor development kit Scrumpi 1, comes Scrumpi 2 which has all the facilities of the former system plus additional PROM and RAM.

The new kit is still mounted on a single p.c.b. but increased in size to include two edge connectors for interfacing with extender cards. Developed around the new NMOS National Semiconductor SC/MP2 microprocessor, Scrumpi 2 from **Bywood Electronics Ltd** gives reduced power consumption and increased speed.

The memory consists of 768 bytes of RAM and 512 bytes of PROM. Two 4-bit latches act as an 8-bit I/O port in which each set of four can be wired as either inputs or outputs. The various functions of the kit are controlled by a flip-flop, a 555 Timer, and NAND gates, all of which are selected by eight toggle switches: RESET, SLOW, STOP, PROTECT, SENSE-A, SENSE-B, ROM/RAM START and LOAD. Programming can only be carried out during a read cycle, since during a write cycle the microprocessor is putting data on the data bus.

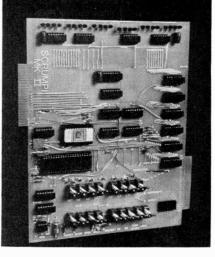
Interfacing facilities on Scrumpi 2 are suitable for either 4-bits or 8-bits and simple VDUs.

Scrumpi 2 will also drive several MM2112 RAM chips and/or PROM on EAROM chips without further buffering.

The basic kit (without RAM and ROM i.c.s) costs £55.56 and with the extra memory facilities £74.07. The PROM can be supplied blank or programmed by Bywood to customer specification for an extra £20.

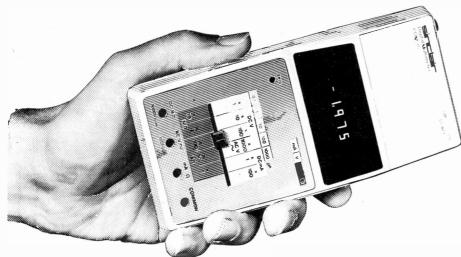
All parts are supplied in the kit, including sockets for all i.c.s. The switches are soldered directly to the board, and the circuit needs supplies of +5V, -7V and -12V (which could be derived from a 17V supply with a 5V Zener diode).

Further information from **Bywood Electronics Ltd, 68 Ebberns Road, Hemel Hempstead, Herts, HP3 9QR.**



Scrumpi 2 from Bywood

The Sinclair PDM35. A personal <u>digital</u> multimeter for only £29.95



Now everyone can afford to own a digital multimeter

A digital multimeter used to mean an expensive, bulky piece of equipment.

The Sinclair PDM35 changes that. It's got all the functions and features you want in a digital multimeter, yet they're neatly packaged in a rugged but light pocket-size case, ready to go anywhere.

The Sinclair PDM35 gives you all the benefits of an ordinary digital multimeter – quick clear readings, high accuracy and resolution, high input impedence. Yet at $f_{29.95}$ (+8% VAT), it costs less than you'd expect to pay for an analogue meter!

The Sinclair PDM35 is tailormade for anyone who needs to make rapid measurements. Development engineers, field service engineers, lab technicians, computer specialists, radio and electronic hobbyists will find it ideal.

With its rugged construction and battery operation, the PDM35 is perfectly suited for hand work in the field, while its angled display and optional AC power facility make it just as useful on the bench.

What you get with a PDM35

 $3\frac{1}{2}$ digit resolution. Sharp, bright, easily read LED display, reading to ± 1.999 . Automatic polarity selection. Resolution of 1 mV and 0.1 nA (0.0001 \pm A).

Direct reading of semiconductor forward voltages at 5 different currents. Resistance measured up to 20 M(1, 1% of reading accuracy. Operation from replaceable battery or AC adaptor. Industry standard 10 M (1 input impedance.

Compare it with an analogue meter!

The PDM 35's 1% of reading compares with 3% of full scale for a comparable analogue meter. That makes it around 5 times more accurate on average.

The PDM35 will resolve 1 mV against around 10 mV for a comparable analogue meter – and resolution on current is over 1000 times greater.

The PDM35's DC input impedance of $10 \text{ M} \Omega$ is 50 times higher than a 20 k Ω /volt analogue meter on the 10 V range.

The PDM35 gives precise digital readings. So there's no need to interpret ambiguous scales, no parallax errors. There's no need to reverse leads for negative readings. There's no delicate meter movement to damage. And you can resolve current as low as 0.1 nA and measure transistor and diode junctions over 5 decades of current.

Technical specification ⁽⁺

DC Volts (4 ranges) Range: 1 mV to 1000 V. Accuracy of reading $1.0\% \pm 1$ count. Note: 10 M α input impedance. AC Volts (40 Hz-5 kHz) Range: 1 V to 500 V. Accuracy of reading: $1.0\% \pm 2$ counts. DC Current (6 ranges) Range: 1 nA to 200 mA. Accuracy of reading: $1.0\% \pm 1$ count. Note: Max. resolution 0.1 nA.

Resistance (5 ranges)

Range: 1(1 to 20 M(1). Accuracy of reading: $1.5\% \pm 1$ count. Also provides 5 junction-test ranges. **Dimensions:** 6 in x 3 in x 1½ in. **Weight:** 6½ oz.

Power supply: 9 V battery or Sinclair AC adaptor. **Sockets:** Standard 4 mm for resilient plugs.

Options: AC adaptor for 240 V 50 Hz power. De-luxe padded carrying wallet. 30 kV probe.

The Sinclair credentials

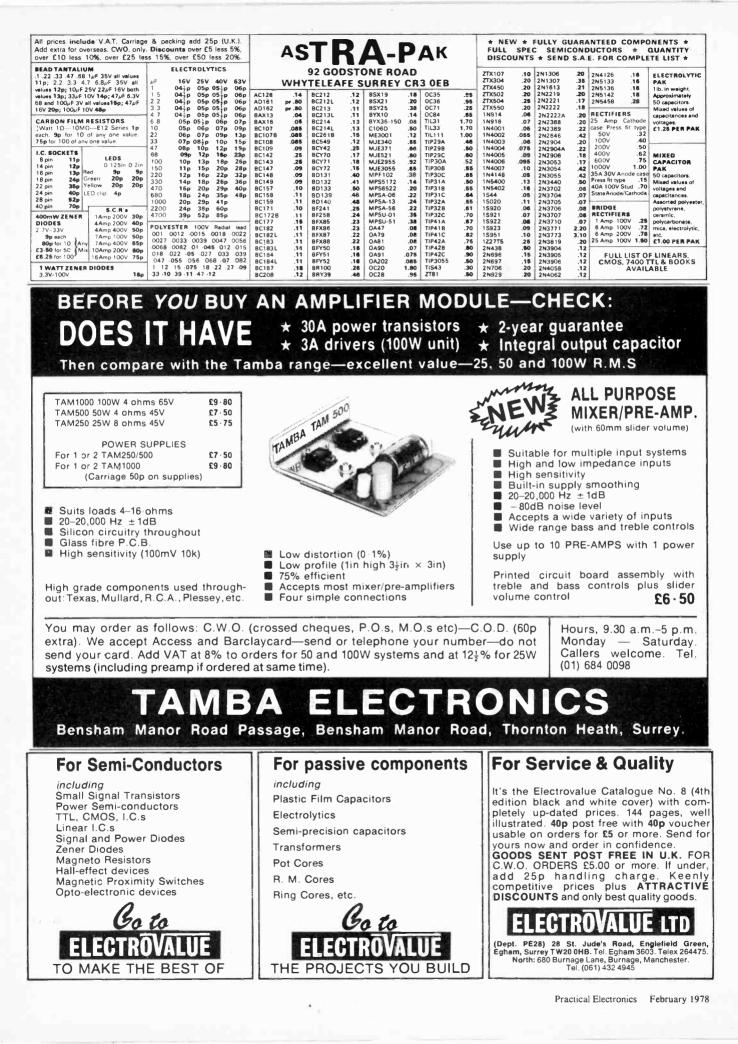
Sinclair have pioneered a whole range of electronic world-firsts – from programmable pocket calculators to miniature TVs. The PDM35 embodies six years' experience in digital multimeter design, in which time Sinclair have become one of the world's largest producers.

Tried, tested, ready to go!

The Sinclair PDM35 comes to you fully built, tested, calibrated and guaranteed. It comes complete with leads and test prods, operating instructions and a carrying wallet. And getting one couldn't be easier. Just fill in the coupon, enclose a cheque/ PO for the correct amount (usual 10-day money-back undertaking, of course), and send it to us.

Sinclair Radionics Ltd, London Road, St Ives, Huntingdon, Cambs., PE17 4HJ, England. Regd No: 699483.

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(qty) De-luxe padded	Address	
carrying case(s) @ £3.00 (inc VAT		
and P&P) each:		
(qty) AC adaptor(s) for		
240 V 50 Hz power @ £ 3.00		
(inc VAT and P&P) each:	-	
l enclose cheque/PO made payable		
to Sinclair Radionics Ltd for		
(indicate total amount):£		
I understand that if I am not completely		
satisfied with my PDM35, I may return it		
within ten days for a full cash refund.	World leaders in fingertip electronics	i i





UN-IDENTIFIED FLYING OBJECT

Now that the excitement of a possible new planet has died down it is perhaps a good time to look at the facts that are available. The suggested size is between 100 and 400 miles in diameter, that the orbit is near circular and that the orbit lies between Saturn and Uranus.

From these data it can be deduced that the object is not a comet because a comet has a highly eccentric orbit. The orbit was determined by sequential photographs so that the circular orbit is now confirmed. The probable distance from the Sun is about 1,500 million miles. It is possible that this "Object Kowal" is the first of a new swarm of asteroids. If a regular watch is kept, it could well be possible that the computation of the orbit, would show that Voyager I might observe it after leaving the vicinity of Saturn and on its way to Uranus.

Many of these small bodies are now on record and Charles Kowal now has the right to choose a name for his discovery. The number of the planetoid is 2042. It is interesting to record that by about 1890 some three hundred of these small planetary bodies were known. A year later another of those new applications of technology which open up new vistas took place. This time it was the advent of photographic methods which widened the horizons. Verv quickly many hundreds of faint objects were identified as coming from the asteroid belt which lies between the orbits of Mars and Jupiter.

Another spurt was given when computers appeared and now over 2,000 are numbered, and at least a similar figure covering those lost or not yet determined exactly. Since they can be accurately timed both into the future and back into the past their behaviour in relation to other planets in the solar system can be examined; even so, many of these bodies are just accidental discovery.

So scarce is time on the world's telescopes that searches for those lost is not economically possible. This emphasises the value of orbiting telescopes with continuous operation. In fact technically there is a great advantage, for only small telescopes are required in space for purposes of this kind. That there is very great scientific interest in knowing about these bodies is shown by the fact that already there are a number of projects for sending probes to land on or take samples from them. A great deal is already known and it would need a lengthy article to describe the present state of the art.

LIFE AND DEATH FROM OUTER SPACE

Whenever something unusual occurs in the environment or in space, outside agencies are postulated as being concerned with the welfare of the human race. Scarcely a week passes without some past happening being brought out as support for unknown origins of events. It is not surprising therefore that from science fiction and "new thought" a new look at data takes place. Much of it may be discarded at once but always there is left a glimpse of what might be. If it stirs someone or some team to relook at past happenings and link them with new possibilities then it is worth while as an exercise. In the dissemination of knowledge the negative results often have the greatest impact.

The sensational situation has arisen about the star Sirius and its "companions". On the strength of some "evidence" from religious beliefs a whole edifice of presumed happenings has been raised. Many people are now convinced that the skills and ills were brought by someone from outer space. Diagrams and pictures are produced in support of the idea mostly without careful examination and indeed in some cases manipulation to support the theory. On this particular theory great claims have been made that scientists are actively, and keenly supporting the theory. In fact this is not so.

To set the scene for this Sirius mystery, the first point of importance is that Sirius is an extremely unlikely candidate for the support of a planetary system. It is true that some very eminent astronomers have indeed been active in their examination of certain data. However, no evidence has been found to support the claims as made. There is the existence of the folk lore, which at first sight is difficult to evaluate. However, this is not really the field of astronomy or space science, still less can it be justified when more specialised branches of science engage in such matters.

Two radio observatories have just released information of their previously unpublished activities. One of these in Canada used a 46 metre radio telescope with entirely negative results. No intelligible signals were received. The other observatory is that of Ohio State University where Dr. R. S. Dixon used the 21 centimetre hydrogen line frequency. Over a period of search, carried out each day, there were no detectable transmissions. The publications from the sensational media do not take into account these tests. Indeed two British scientists found it necessary to insist on a disclaimer that they supported the theories. This particular case has been cited because it is concerned with space. It follows then that the less fanciful but certainly more tenable cases should be in the same area. Both are concerned with life on earth as well as in space.

A number of disciplines have been concerned with the possibility of life having begun outside the earth and found its way to the planet. It is so frequent for the work of some individuals and groups to be quoted out of context in support of sensation, yet in the cases now to be detailed there are sensational features. It has often been put forward that cometary bodies could be carriers of some form of life. The earth passing through a tenuous medium would not, except by the use of highly sophisticated techniques, show any indication that anything had happened.

Scientists Sir Fred Hoyle and Chandra Wickeamsingh announced that they favour the theory that in the centres of comets there exist the building blocks of life and disease. As the comets travel through the solar system changes take place which lead to the formation of new viruses and bacteria. When a comet brushes the Earth these are released. The two scientists suggest that this is a far more plausible account of new epidemics.

A number of groups are investigating the possibilities of life being brought to Earth by means of meteorites and other interplanetary debris. In Russia V. I. Goldanski of the Institute of Chemical Physics of the Academy of Sciences in Moscow is known to be working in this area. Certain changes take place near absolute zero temperature and interstellar clouds could be a source of the grains of cold life. A new planetary system rich in dust would be an ideal situation for this kind of evolution.

LANDSAT

The Landsat vehicle is to help the Navajo Indians to assess the resources of their 16 million acres of reservation, the volume of timber and its condition. This is the first time a private company has had this kind of co-operation with NASA. The activity will eventually range over five states. A great deal of headway has been made with this satellite which has justified the project.



CHAMP

Now that the "hardware" description of CHAMP is complete, we can move on to consider that magic new ingredient, "software". As you will no doubt recall, the program which makes CHAMP work is called CHOMP (CHamp Operating system and Monitor Program), and this month we shall examine the program.

.COMMERCIAL KITS

Most commercial microprocessor development kits provide the user with only a simple listing of their operating programs, and ploughing through these listings to gain an understanding of how the system operates can be a painful experience.

CHAMP is for hardware oriented people; not the software genius; so we have done more than just provide a simple listing of the code you will need in PROM chip zero to get CHAMP to work. We cannot, for space reasons, give an intimate description of *every* line in the program, but we will be discussing the overall program flow chart. As an introduction to programming techniques, we will be showing how segments of the overall flow chart are converted first into more detailed flow charts, and then into hexadecimal code. In this way we hope to use CHOMP not only as an essential part of CHAMP, but also as a sort of software training ground for fledgling CHAMP programmers!

Constructors are advised to spend some time developing a familiarity with this program, and also of course with the 4040 instruction set which it uses.

4702A PROM

CHOMP should, strictly speaking, be called a firmware program, because is resides not on paper tape or magnetic cassette, but in a ROM or Read Only Memory. The type of ROM used is in fact an eraseable and reprogrammable type using the FAMOS technology, and these devices are

more properly described as EPROMS, or just PROM for short. The actual device used is the 4702A chip which contains 256 eight bit words, has supply requirements compatible with the 4040, and can be erased by means of exposure to short wave ultra violet light. The 4702A is a selection from the 1702A family, characterised to work on +5V and -10V supplies over the full temperature range, instead of the usual +5V and -9V of the 1702A. The 4702A is also a less speedy device than the 1702A, having a 1.7μ s maximum access time. The only extra requirement the 4702A has, is for that extra volt on the supply rails, and in fact it is virtually certain that any 1702A chip will work well in the CHAMP circuit, at least over the usual domestic temperature range. This has been tried on the prototype with complete success, and opens up the possibility of using the low cost 1702As now being advertised. Of course, it is not possible for us to guarantee success with anything other than the 4040 manufacturers' recommended 4702A devices.

CHOMP uses 248 locations out of the 256 available in a 4702A, and the PROM containing CHOMP has to be plugged into the CHIP ZERO location, i.e. the left hand PROM socket.

MAIN FLOW CHART

CHAMP PROG.

Figure 6.1 shows the main flow chart of CHOMP, and this is in effect an overview of the whole program in a much simplified form. We have chosen to use just four symbols to draw the flow chart:

- (a) Circles represent the beginning and end of events.
- (b) Oblong boxes represent actions to be performed.
- (c) Diamonds represent decision points with two possible exits.
- (d) Square arrows represent "Jumps" to other pages of memory.
- When power is first applied to CHAMP, or when the

RESET button is pressed, the 4040 address counter is cleared to address 000H, and it fetches its next instruction from this address, which is of course the first location in chip zero, and the beginning of CHOMP. The flow chart can be traced from this RESET point which is located at the top left of Fig. 6.1.

The first box is not very exciting; it simply tells us that we must jump past address 003H, because this is the program location which contains the first instruction of the Interrupt routine, and we only want to go to *that* address when a hardware interrupt is acknowledged.

Box three represents the first "meaty" part of the program, and here we carry out all the preliminary housekeeping jobs required by the rest of the program. The 4265 INPUT/OUTPUT chip is programmed into mode 9; the switch flag latches are cleared (in case any were already indicating a switch closure when power was applied), and the various software counters are initialised to a required starting condition (i.e. the CHOMP address counter is set to point to the first location in program RAM, 200H). Finally, the interrupt system is enabled so that any interrupt signal from now on will cause the 4040 to save the current address on its internal stack, and jump to 003H, the interrupt vector. The only source of interrupt recognised by CHOMP itself is the keyboard, but for the moment let's assume that no interrupt has been received and continue on to box 4.

After initialisation, the CHOMP address counter holds 200H, and this box is present to load that address value into the display buffer register, so that we can see it on the right hand three display digits. Notice that box 4 is also entered via LOOP 2, and in this case the current address value (whatever it is) will be displayed.

Box 5 performs the vital job of refreshing the l.e.d. display. Each time this box is entered, a new eight bit word is presented to the segment lines and the display shift register is stepped on one position. Eight entries are required to refresh the complete display, and to ensure regular use, box 5 is made part of LOOP 1, through which the 4040 cycles continuously as long as no control switches are pressed.

Box 6 is also part of LOOP I, and the main purpose of this box is to read into the 4040 accumulator register the state of the four control switches, so that the state of these may be checked and appropriate action taken. The interrupt system is again disabled at this point to prevent interference with switch responses. The INTERRUPTS RECOGNISED zone is quite extensive enough for a prompt response to any key press, and making the rest of the program interruptible would be an unnecessary complication.

Box 7 is a decision based not upon the switch flags, but upon the separate 4040 TEST input. If the TEST button is pressed, box 7 ensures a jump to the start of Chip 1, address 100H. Chip 7 is normally used for the PROMPT programmer software of course, but if the programmer is not in use, any 4702A resident program can be started by pressing TEST.

Boxes 8, 9, 10 and 11, check each of the switch flag bits in the accumulator in turn, by shifting them into the carry flip-flop and performing a JCN instruction. If no switches are pressed at box 6 time, then LOOP 1 is completed, and is in fact repeated indefinitely, refreshing the display and checking the switches on each pass. Needless to say, CHAMP spends most of its time in this loop when CHOMP is running, only leaving it intermittently, to respond to control switch closures. If the ENTER DATA switch is pressed then CHAMP exits from LOOP 1 at box 8. Box 12 represents a routine which takes data previously entered via the keyboard and stores that data (8 bits) in the program RAM location pointed to by the CHOMP address counter, before passing on to box 16 to increment to the next address in sequence. The new address is displayed by means of box 4, and then LOOP 1 is re-entered.

If the ENTER ADDRESS switch is pressed, then LOOP 1 is left at box 9. Box 13 is then executed, and this loads the three digit hexadecimal data previously entered via the keyboard into the CHOMP address counter to replace the previous contents. In this case there is no need to increment the address counter, and so LOOP 1 is reentered via LOOP 2.

When the DUMP switch is pressed, a sequence of operations similar to those for ENTER DATA takes place, although in this case box 14 represents a routine which reads data (8 bits) from the program RAM location pointed to by the CHOMP address counter, and loads it into the display buffer for examination. When the PROGRAM MODE/RUN MODE switch is in the RUN position box 15 is entered, and a routine is executed to cause an unconditional jump to the start of the user program RAM at address 200H. From this point onwards of course, CHOMP has relinquished its control of CHAMP facilities to whatever user program is resident in RAM.

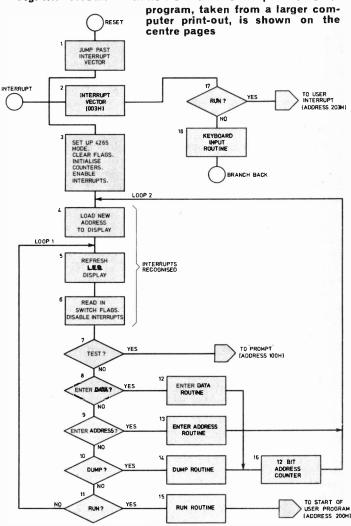


Fig. 6.1. CHOMP main flow chart. The complete CHOMP

JIN (B JUN B JUN E JUN FIRS SECC	AF LD 0	BF XCH	F5 A7 A7 A6 A6 A20 A20 A20 A20 A20 A20 A20 A20 A20 A20	740EISZ 4,400EJUN L400EINTER86TCCH 687TCCH 787TCCH 72240FIM 2,23SRC 223F51276JC PR40LD 7;A7LD 7;A6LD 7;420PROM420JUN 22480PROM56JUN 268INC 0E	BE RPM; BE RPM; 2850 FIM 0, 29 SRC 8 29 SRC 8 20 SRC 8 20 SRC 8 20 SRC 8 20 SRC 8 210 FIM 2, 22 SRC 9 23 SRC 2 23 SRC 2 23 SRC 2 23 SRC 2 23 SRC 2 24 SRC 8 24 SRC 8 25 SRC 8 26 SRC 2 26 SRC 8 26 SRC 10 27 SRC 8 26 SRC 8 26 SRC 8 26 SRC 10 27 SRC 8 26 SRC 8 27 SRC 8 26 SRC 8 27 SRC 8 26 SRC 8 27 SRC 8 27 SRC 8 28 SRC 8 29 SRC 8 20 SRC 9 20 SRC
FIRST 0EH; FIRST KBD E	H: H: H: H: H: H: H: H: H: PUT KBLE IND	PUT IN CY ARE WE IN PRO USER IR SO RES GO TO USER IR FIM 4, 80H; SELECT 4265	SB1 40H	1:0CH 1:	

CLRF DUMP HEXL LOOP 1 PROMO TABLE		00FFD 00FFD	00F6 00F7 00F9	00F3 00F3 00F5	00F0	00E7	00E5	00E3			00D8 00D A	00D4 00D5	00D1 00D2	
0097 004 A 00D D 1 0010 0 0076 0 0082*		8 F 2 F 2 F 2 F 2		9E DA	7€ 000	C 69 E	A0	69 69	A1	3 8 7 C	AD B1 50DD	AC B1 50DD	B1 50DD	78C9 79C9 C0 2800
COUNT ENTAD INTER LOOP 2 RUN TERM			DB OFEH DB OFEH DB OFEH DB OFEH		-	INC 9; BBL 0	LD 0;	INC 9;	LD 1;			LD 0CH XCH 1; JMS HEXL;	JMS HEXL;	LOOP 3: ISZ ISZ 9, LOOP BBL 0H LOKY: FIM 8,
005E 0040 0066 000E 0028*	SYMBOL									0FH;				Z 8, LOOP 3 8, 00H;
DATO ENTDA LADR LOOP 3 SECON THIRD	TABLE				гоокпь	BUMP	LAST	BUMP	FIRST	SEVEN TABLE GET SE	CONVERT	CONVERT	GET LOW CONVERT CODE	3 SET
00C5 0032 00A2 00C9 008B 008E					UP TABLE		FOUR	NIBBLE	F FOUR TO	EN SEG TAL LE BASE IN SEG CODE	VERT TO DE	VERT TO		UP ADD
DDRV FIRST LOKY PASS SKIP					3LE	NIBBLE POINTER	TO 4002	E POINTER	TO 4002	ENAB	SEVEN	SEVEN	JR SEVEN	ADDRESS
00 B 1 0088 00 CE 000C7 001D						70		R		LE LOOKUP RP 0 FROM TABLE	SEG	SEG	SEG	

003A 003B 003C 003C 003E 405E 0040 AD 0041 B3			0032 2800 0034 29 0035 A4	002F E6 0030 4200		002A 2880 002C 29			0020 1A40					0011 50B1 0013 2840			0008 D9	0005 2380 0007 29		000 00	Complete
ZCH 3	WPM	SRC 2;	0 ENTDA: FIM 8, 00H SRC 8 LD 4	JUN 200H;	CLB WR1	SRC 8	JC LOOP 1		D JNC ENTAD;		JNT	DIN:		1 JMS DDRV; FIM 8. 40H	 FIM 4, 28H;		LDM 9	SRC 8		NOP	CHOMP
WRITE MOST SIG NIBBLE CLEAR SWITCH FLAGS BUMP ADDRESS COUNT PUT KBD IN COUNTER	WRITE LEAST SIG NIBBLE TO RAM	SELECT PROGRAM RAM CHIP ADDRESS BYTE		JUMP TO USER PROG IN	BLANK DISPLAY		RUN OR BACK AGAIN	2200	NEXT FLAG TO CY	ENTER DATA?	JUMP TO CHIP 1 IF TEST SET	DISABLE INTERRUPTS	READ IN SWITCHES	DISPLAY DRIVER	DDRV COUNT	CLEAR SWITCH FLAGS	SET UP 4265 MODE		INTERRUPT VECTOR	SKID INTERRIIPT	program

00C5 00C5	00000000000000000000000000000000000000	0087 0088	0082 0083		00 A 8 00 A 9	00 A2 00 A4 00 A5 00 A6	0099 0098 0090 0095 00041	0094 0095 0096 0097	008E 0091
85 40C7 DE E0 2880	67 67 50 50 50 50 50 50 50 50 50 50 50 50 50	27 67 5 Eg	27 E9 2880 29	A3 50DD	A2 B1 50DD	280 A A4 B1 50DD	29 2A00 2C00 2E00 C0	F6 A6 2850	BD 2A00 50CE
JUN PASS DATO: LDM 0EH; WRM; PASS: FIM 8, 080H;		RDM:	DDRV: SRC 6; RDM; FIM 8, 80H SRC 8;	JMS HEXL:	LD 2 XCH 1 JMS HEXL;	LADR: FIM 8, 0AH; LD 4 XCH 1 JMS HEXL;		RAR; LD 6 BBS CLRF: FIM 8, 50H;	
FETCH WRM CODE BIT SET Z3 LOW SLOW DOWN MULTIPLEX RATE	LOW FOUR TO 4265 PORT Y BUMP NIBBLE POINTER INCREMENT SHIFT COUNTER FETCH WRM CODE BIT SET 4265 Z3 HIGH PRESET SHIFT COUNTER	BUMP NIBBLE POINTER HIGH FOUR FROM 4002	DISPLAY DRIVER ROUTINE LOW FOUR FROM 4002 LOW FOUR TO 4265 PORT X	CONVERT TO SEVEN SEG	CONVERT TO SEVEN SEG	CONVERT TO SEVEN SEG	TCH FLAGS REGISTERS	RESTORE STATUS SELECT ROM O.P. PORT 5	THIRD IN RD CLEAR KBD CHAR COUNT PUT NEW KBD DIGIT IN 4002

print,

INTERRUPT

If CHOMP is running and a keyboard switch is pressed, one interrupt is latched by IC10 and CHOMP responds (from the INTERRUPTS RECOGNISED zone) with a jump to box 2 (address 003H) which is called the interrupt vector.

Box 2 contains another jump to the start of the interrupt routine proper, which just happens to be elsewhere in chip zero (actually at address 066H). Before the keyboard handler routine is entered, CHOMP makes a check to see whether it is actually in PROGRAM MODE. Interrupts to RUN MODE user programs are also vectored to address 003H, so this check is essential, and is represented by box 17. If PROGRAM MODE *is* current, then box 18 is entered and a routine executed to read-in a single four bit hexadecimal digit from the keyboard, and store it away in a 4040 register. The keyboard routine also updates the display buffer so that each digit appears on the left hand side of the display as it is entered.

User interrupts are re-vectored to address 203H, so that the RAM resident program can define how a response is to be made. If you want to use the keyboard interrupt routine in your own program, simply carry out a JUN (Jump UNconditional) to address 066H from address 203H. Remember to use a BBS (Branch back and SRC) at the end of any "custom" interrupt routines you write!

CHOMP LISTING

Figure 6.2 is a complete listing of the CHOMP program, showing hexadecimal address data (column 1), hexadecimal instruction code data (column 2), mnemonic instruction codes (column 3) and comment lines (column 4).

The listing of Fig. 6.2 is the output of an assembler program which runs not on CHAMP, but on a much larger computer. Before anyone cries *cheat!* let me hasten to point out that CHOMP *was originally* written without the benefit of any such sophisticated facilities, directly in hexadecimal code. The reasons for eventually putting CHOMP into this form are simple:

- (a) The assembler program does produce nice neat output listings which are useful for publication purposes.
- (b) Since we are indeed saying that you do not *need* assembler programs when writing CHAMP software, we thought it only fair to show you what you are doing without!

When entering programs into an assembler, you have to enter columns 3 and 4 of Fig. 6.2 via a teletype terminal. From these the assembler produces columns 1 and 2 which tell you *what* hexadecimal code to enter *where* in program memory. The advantages of using an assembler program are firstly that the mnemonic instruction codes are all you have to remember, and that is fairly easy: and secondly, that instead of having to specify addresses in hexadecimal code you can use labels (i.e. names) instead. The assembler program will turn instruction mnemonics and address labels directly into hexadecimal code, and produce neat listings like the one shown here.

These sort of facilities sound very useful of course, and we would be the first to agree that with more complicated micros such as the Z80 or the 6800 they are very helpful indeed. The disadvantages are of course that you have to have lots of RAM available to store all those useful comments, and you also need a teletype or a V.D.U. The authors have assembler facilities available to them, but even so we prefer to write our 4040 programs directly in hex, with a pencil and paper; an exercise which is quite. simple after a little practice! Before leaving the subject of assemblies, let me explain a few things about the output listing shown in Fig. 6.2 which may be puzzling some readers:

- (a) ORG and END are pseudo instructions, nothing to do with the 4040 but understood by the assembler.
- (b) Some lines in column 2 have four hexadecimal digits. These involve two line instructions such as JUN, and will of course occupy two consecutive bytes in program memory.
- (c) Some lines are field separators required by the assembler program.
- (d) Notation. The assembler requires hexadecimal data to start with a decimal digit (don't ask us why!), and to be followed by an H. This means that FF hex is written 0FFH, while 2F hex is written 2FH.
- (e) Register references can be made in a variety of ways, but we referred to them using hexadecimal, or decimal where this was equivalent.

Putting this information together, refer to Fig. 6.3 which explains how a complete assembler line is made up.

To get a CHOMP PROM from Fig. 6.2, all you have to do is step through the PROM addresses (column 1) entering the hexadecimal instruction codes from column 2. To do this you need a PROM programmer of course, and since most constructors will not have access to such a unit, arrangements have been made for the provision of a CHAMP programming service which will carry out the programming for you. Details next month.

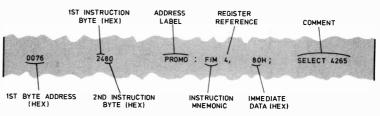


Fig. 6.3. One assembler output line and what it means

DETAILED FLOW CHARTS

No doubt many readers who felt reasonably happy with the overall flow chart in Fig. 6.1 had second thoughts when they tried to relate it to the program listing of 6.2. This is inevitable, because there is a missing link between the two, namely the detailed flow charts of each separate section of the program. Figures 6.4 to 6.8 show some of the detailed flow charts needed, but lack of space makes it impossible to reproduce all of them, so a certain amount of "unravelling" will still be necessary if any reader wishes to trace the operation of the complete program.

Let us start off with something easy, and have a look at how box 16 of Fig. 6.1 is turned into a 4040 program segment. Box 16 is a software implemented 12 bit binary counter routine which is updated each time the ENTER DATA or DUMP switches are pressed. The current count value is used during the ENTER DATA or DUMP program segments as a program memory address, and is displayed on the rightmost three display digits in hexadecimal.

Counters are implemented in 4040 software by using the ISZ (Increment and Skip if Zero) instruction which has the effect of incrementing the value of an internal four bit 4040 register by one, and jumping to a specified address if the contents of the register are not zero. If they *are* zero, the jump does not take place, and the next instruction in sequence is fetched. Figure 6.4 shows the implementation of the 12 bit address counter using ISZ.

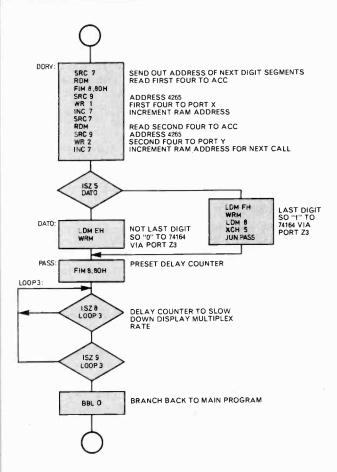


Fig. 6.5. Display driver subroutine. Refer to box 5 in CHOMP main flow chart, and address 00B1H on CHOMP program listing

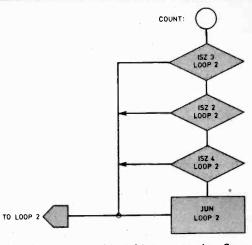


Fig. 6.4. Twelve bit address counter flow chart. Refer to box 16 in CHOMP main flow chart, and address 005EH. The CHAMP address counter should not be confused with the 4040 address counter

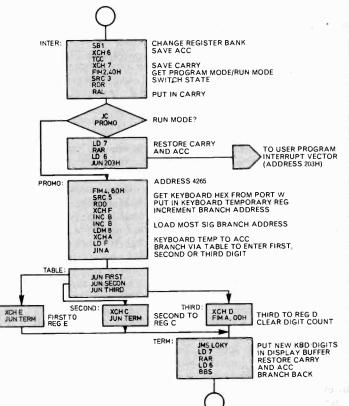


Fig. 6.6. Interrupt routine. Refer to boxes 17 and 18 in CHOMP main flow chart, and address 066H in CHOMP program listing FIRST

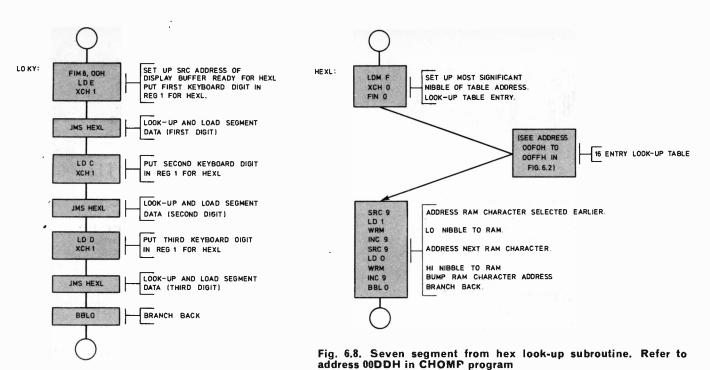


Fig. 6.7. Load keyboard subroutine. Refer to address 00CEH in CHOMP program

the registers used being 3, 2, and 4 in that order. (The order is important because the high order address bits during an SRC instruction are taken from the lower register of a pair, and of course we use the lower eight bits of the counter as a SRC value when addressing program memory, before using RPM or WPM instructions.) The required 12 bit length of the counter is arranged by using three cascaded ISZ instructions, each with a common jump address, namely LOOP 2. You can probably see that Register 3 is incremented 16 times more often than Register 2, which itself is incremented 16 times more often than Register 4, in traditional binary counter fashion.

DISPLAY DRIVER

The subroutine DDRV is the full version of box 5 in Fig. 6.1, and its detailed flow chart is shown in Fig. 6.5.

This subroutine increments a counter (Register 7) twice each time it is called, and uses the counter contents as part of a SRC address to the data RAM display buffer (RAM chip 0, register 0). On each call it reads two four bit locations from the 4002, and sends their contents to the 4265 output ports X and Y which control the display segment lines. After doing this it increments another counter (Register 5) which it uses as a digit counter. This counter is preset to 8 hex (using LDM) when it reaches zero, and a logic one is placed on the 74164 shift register DATA INPUT via 4265 output Z3, using the WRM command. If this counter does not reach zero during a call then a logic zero is placed on the shift register data input.

You can probably see how this subroutine displays eight digits, one per call; and how it recycles to repeat the process over and over again. On seven out of eight calls it shifts a logic zero into the register, but on the eighth it generates a new "digit strobe" for the display, to replace the one which has just "dropped off the end" of the 74164.

INTERRUPT ROUTINE

Figure 6.6 shows the interrupt routine, INTER, which is boxes 17 and 18 on the overall flow chart of Fig. 6.1. The main thing of interest here is the use of a "Branch Table" accessed using the JIN (Jump Indirect) instruction to route the program flow to the correct segment depending on whether the current keyboard digit entry is the first, second, or third in sequence. Notice also that at the start of the routine the current accumulator and carry flip-flop contents are saved in registers 6 and 7 of Bank 1, to be restored at the end of the routine so that the main program flow can continue normally. A subroutine LOKY is used to enter the newly entered keyboard data into the display buffer.

The subroutine LOKY is itself shown in Fig. 6.7. It takes the contents of the three keyboard registers (E, C, and D) and converts their hexadecimal data into seven segment code using another subroutine HEXL.

HEXL itself is shown in Fig. 6.8, and as you can see it uses a FIN (Fetch Indirect) instruction to access a lookup table with sixteen entries. To convert hex to seven segment code, the hex is used as part of an indirect address so that the correct segment data can be "looked up" in the table. Table look-up is a powerful and simple technique which is very useful when converting data from one format to another. HEXL also loads the seven segment data into the 4002 RAM buffer register, at the appropriate address passed to it in registers 8 and 9 by the subroutine LOKY.

There are several other detailed flow charts required for a full understanding of CHOMP, and it would be excellent practice for CHAMP users to try and draw these up for themselves using Figs. 6.1 and 6.2 for reference. Don't be discouraged if it takes a while for the flash of inspiration to arrive, programming a microprocessor takes some getting used to, and is invariably a frustrating business at first, particularly for us "hardware people".

NEXT MONTH: Putting CHAMP to work

Appearing every two months, Micro-Bus will present ideas, applications, and programs for the most popular microprocessors; ones that you are unlikely to find in the manufacturers' data books. The most original ideas will probably come from readers working on their own microcomputer systems, and payment will be made for any contribution featured here. This is also the place to air your views, in general, on this new technology, so let's be hearing from you!

MICRO-E

CALCULATING ON A MICRO

SINCE microprocessors are designed as controllers rather than as computers they do not lend themselves to arithmetic work, and most instruction sets do not even include multiply and divide operations. There are two ways to add the capability of a scientific calculator to a micro. One is to add a floating-point package: a collection of programs to handle calculations involving floatingpoint numbers, and providing trigonometrical and logarithmic functions in addition to the arithmetic operations. The disadvantage is the extra memory required—typically 1½k.

The alternative is to add a hardware "arithmetic processing unit" which performs the calculations independently of the main micro. One such device is National Semiconductor's MM57109 "Number Cruncher Unit" or NCU. This chip offers the functions of a programmable calculator (see Table 1), a fourelement stack and a memory, and floating-point arithmetic to 8-digit accuracy.

NUMBER CRUNCHER UNIT

The NCU is similar in operation to a calculator; 6-bit instructions correspond to key-presses, and these are presented to it on six input lines, 11-16. Numbers are entered digit by digit as in a calculator.

A summary of the instructions is given in Table 1. The NCU shows that it has finished executing an instruction by pulsing its RDY output high. When RDY is high you must either send it another instruction or else put HOLD high to halt it until you are ready.

The result of a calculation is obtained by presenting the OUT instruction. The NCU then puts the digits out on DO1– DO4 at regular intervals and pulses R/Wlow when each digit is valid. There are some test instructions, such as TX=O, and these cause the BR output to be pulsed low if the result is true.

The NCU is not directly compatible with a microprocessor bus but fortunately all the necessary logic is provided within a single device, the Motorola MC6820 Peripheral Interface Adapter or PIA, also manufactured by MOS Technology in their 6500 series as the MCS6520. The PIA is a versatile general purpose input/output circuit whose particular mode of operation is determined by numbers loaded into its two control registers. It consists of two similar halves, A and B, each with an 8-bit I/O port PA0-PA7 (or PB0-PB7) and two control lines CA1 and CA2 (or CB1 and CB2).

In the present application the PIA is configured to operate as represented in Fig. 1: DO1-DO4 input to location 0400; $\overline{R/W}$ and \overline{BR} are latched inputs which set the top two bits of control register A at location 0401; 11–16 are fed by latched outputs from location 0402; and RDY and HOLD are in "handshake mode" with RDY setting the top bit of control register B at location 0403. In handshake mode HOLD is taken high when RDY goes high, halting the NCU, and goes low when an instruction is written to the NCU, thus releasing the NCU to execute the instruction. This handshaking makes it unnecessary for the micro to respond immediately to the RDY pulse from the NCU.

INTERFACE

The complete interface circuit is shown in Fig. 2. The NCU is a PMOS device requiring a 9V supply (at 20mA) and to make it compatible with the microprocessor system supplies of +5V and -4V are used. The PIA side A inputs PA0-PA7 and CA2 presents one TTL load, and so pull-down resistors to the -4V rail are needed on the DO1-DO4 outputs, and \overline{BR} needs a buffer transistor. The CA1 and CB1 inputs are high impedance so a pull-down resistor to 0V is needed on the R/W and RDY outputs.

The HOLD and POR (Power-On Reset) inputs to the NCU must be driven between its supply rails and so transistor

Table 1. Summary of the instructions available in the MM57109.

i _s i _s									
00	01	10	11						
0	TJC*	INV	XEY						
I	TX=0*		EX						
2	TXLT0*		ĨÓX						
3	TXF*		SQ						
4	TERR*		SQRT						
5	JMP*		LN						
6	OUT*		LOG						
7	IN*		Ī/X						
8	SMDC*		Ϋ́X						
9	IBNZ*		+(M+)						
DP	DBNZ*		- (M-)						
EE	XEM		× (M×)						
CS	MS		((M/)						
PI	MR		PRWI						
AIN	LSH		PRW2						
HALT	RSH		NOP						
	0 1 2 3 4 5 6 7 8 9 DP EE CS PI AIN	0 TJC* 1 TX=0* 2 TXLT0* 3 TXF* 4 TERR* 5 JMP* 6 OUT* 7 IN* 8 SMDC* 9 IBNZ* DP DBNZ* EE XEM CS MS PI MR AIN LSH	00 01 10 0 TJC* INV 1 TX=0* EN 2 TXLT0* TOGM 3 TXF* ROLL 4 TERR* SIN(SIN ⁻¹) 5 JMP* COS(COS ⁻¹) 6 OUT* TAN(TAN ⁻¹) 7 IN* SFI 8 SMDC* PFI 9 IBNZ* SF2 DP DBNZ* PF2 EE XEM ECLR CS MS RTD PI MR DTR AIN LSH POP						

*indicates a two-word instruction.

Compiled by DJD.

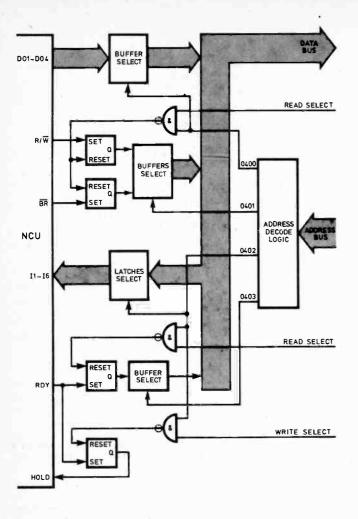


Fig. 1. Block diagram showing the logic needed to interface the Number Cruncher Unit with a micro as described. This logic is all provided in the PIA

Fig. 2. Circuit using a PIA to interface the Number Cruncher Unit with a microprocessor system such as KIM

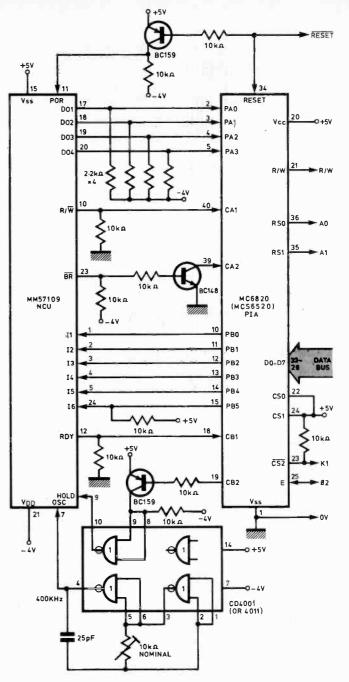
drivers are needed, and a OMOS inverter re-inverts HOLD to active high. Two other gates in the CMOS package form a simple 400kHz oscillator to drive the OSC input. Finally, a resistor is required from I6 to +5V as shown. The circuit was constructed on a plain matrix board using wire-threading (see Fig. 3) and connected to the microprocessor system by a 16-way ribbon cable.

PROGRAM

The Number Cruncher Unit circuit was used with the MOS Technology KIM development system (see review elsewhere in this issue), which is based on their 6502 micro, and the interface program is given in Fig. 4. The 6502 is similar in some respects to the 6800 and converting the program for the latter should present few problems. The 6502 has two 8-bit index registers, X and Y, and one accumulator. In the program the X register is used to point to the next instruction to be sent to the NCU, and the Y register points to the address at which digits output by the OUT instruction are to be stored.

The program first configures the PIA, and points X to the first instruction for the NCU. It then waits in a loop testing for a signal on one of the control inputs. The BIT instruction in the 6502 loads the top two bits of the memory word—the control register A in this case—into the N and V status flags. If R/W has gone low, bit 7 will be set and a branch to the label \overline{RW} is called for. If \overline{BR} has gone low bit 6 will be set and a branch to \overline{BR} is required. Finally, bit 7 of control register B will be set by RDY going high, and an instruction should be sent. If not set the program continues to wait.

The NCU's test instructions and OUT, each generate two RDY pulses; i.e. they are effectively two-word instructions. The second word is used by this program as the address (in page zero) for the jump or for the output of digits, and is ignored by the NCU. The OUT instruction causes one digit to be stored per byte, although the program could be modified to pack two per byte.



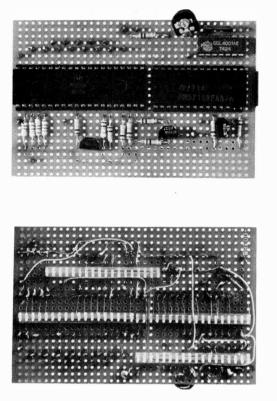


Fig. 3. The Number Cruncher Unit and interface circuits described in this article. Top and underside

A sequence of instructions for the NCU is shown in Table 2. This finds the sum of the terms of the series $1/M^2$ for M = 1to 100 and gives the result 1.6349839 (close to $\pi^2/6$, the infinite sum). The program takes 9 seconds. The NCU is slow by computer standards; the slowest instruction XY takes up to 1 second, and multiply takes 32 milliseconds.

One advantage of a hardware arithmetic processor over the software equivalent is that while instructions are being executed the micro is free to go away and do something else. In the program described it waits in a loop, but with a trivial modification the three inputs RDY, R/\overline{W} , and \overline{BR} could cause interrupts so that a negligible time would be taken up in servicing the NCU. Perhaps someone may be inspired to write a BASIC interpreter which uses an arithmetic processor working in parallel with the micro' in this way.

GENERATING SINE WAVES

The program for generating sine waves in October's Micro-Bus used a look-up table for the values. Mr. T. Froggatt of York University has shown how this can be dispensed with:

"The problem is not to generate the sine of a given angle, but to generate the sine of an angle having just generated the sine of a nearby angle. So remembering that the rate of change of a sine wave is a cosine wave, and that the rate

le view	stores the	answers i
of change of a	cosine wave is	an in-
verted sine wave,	the following p	rogram
is all we need:		

0000

0200

0202

0205

0207

020A

0200

020F

0211

0214

Ø216

0218 0218

021D

0220

R222

0223

A9 14

A9 FF

A2 00

30 17

70 1F

84 00

10

E8

A9 26

8D 01 04

80 02 04

8D 03 04

2C 01 04

AD 03 04

F4

AD 02 04

8C 02 04

Cosine = 0.0

Sine = 1.0

Loop: Output (Sine)

 $Cosine = Cosine - Delta \times Sine$ $Sine = Sine + Delta \times Cosine$ Go to Loop.

To make this program work on an 8-bit micro the sine and cosine should each be held as two-byte items, and each time round the loop the upper byte of the sine subtracted from the cosine and the upper byte of the cosine added to the sine. This avoids the need for multi-

0226	C0 0F		CFY £\$0F	HALT INSTRUCTION
0228	DØ E7		BNE WAIT	
022A	4C 4F 1C		JMP MAIN	RETURN TO MONITOR
		;		
		;	READ AND STORE	DIGITS
022D	AD 00 04	RW	LDA AREG	CLEARS IRQA1 TOO
0230	99 00 00		STA Ø, Y	STORE DIGIT
0233	C8		INY	
0234	4C 11 02		JMP WAIT	
		,		,
		1	BRANCH INSTRUC	TION
0237	98	BR	TYA	GET ADDRESS
0238	AA		TAX	POINT X TO IT
0239	AD 00 04		LDA AREG	CLEAR IRQA2
0230	4C 11 02		JMP WAIT	

Fig. 4. Complete program for the 6502 micro which sends a sequence of instructions to the Number Cruncher Unit and received back into memory

> plication and effectively fixes Delta as 1/256."

NUMBER-CRUNCHER (MM57109) INTERFACE PROGRAM PIA ADDRESSES:

CONFIGURE PIA:

CA1 & CA2 INPUTS,

PR0 - PR7 OUTPUTS.

B HANDSHAKE MODE.

FIRST INSTRUCTION

GET BITS 6 & 7

IRQA1 SET?

IRQA2 SET?

IRQB1 CLEAR?

POINT TO NEXT

SEND TO NCU

NO - CLEAR IRQB1

LOAD INSTRUCTION

AREG

ACON

BREG BCON

MATT

-\$0400 =\$0401

=\$0402

=\$0403

*=\$0200

LDA £\$04

STA ACON

LDA £\$FF

STA BREG

LDA £\$26

STA BCON

BIT ACON

LDA BOON

BPL WAIT

LDA BREG

LDY 0,X

INX STY BREG

LDX £0

RMT RM

RUS BR

The period of the sine wave produced is about $2\pi/\text{Delta}$ iterations of the loop. Mr. Froggatt described a program he has written which uses this method of generating a sine wave to sing Christmas carols, using a table to give the value of Delta for each note.

ADDENDUM

In December's Micro-Bus the second Chess Challenger game contained an error. The fourth move should have read: 4. 7a-6c 3h-2g

Table 2. Example of a sequence of instructions for the Number Cruncher Unit.
This calculates the sum of the first 100 terms of the series 1/M ² .

Address	Code	Mnemonic	Comments
00	3F	NOP	First 3 instructions are
01	3F	NOP	ignored by the NCU after
02	3F	NOP	a Power-on Reset
03	01	111	Digit input
04	0B	EE	Enter exponent
05	02	· 2 '	X = 100; push stack
06	IC	MS	Store X in memory
07	00	· 0 ·	X = 0; push stack
08	ID	MR	Recall memory to stack
09	33	SQ	$X = X^2$
0A	37	I/X	X = 1/X
0B	39	+	X = X + Y
0C	IA	DBNZ	Decrement memory and go
0D	08		to 08 if non-zero
OE	16	OUT	Output X starting at 101
0F	40		40 (i.e. 0040)
10	OF	HALT	Return to monitor



REMEA RESULT

N.A. COOKE

HIS month the second and final part will deal with constructional details and setting up procedures.

CONSTRUCTION

Construction is very straightforward as all components are mounted on two p.c.b.s with the exception of the three potentiometers, the switches, fuse holder, socket and indicators which are mounted on either the front or back panels.

Figs. 10 and 11 show the etching details and component layout of the main board.

It is advisable when assembling the p.c.b.s to fit the components of smallest dimensions first. Bending their leads to an angle of 45 degrees after insertion will prevent them from falling out when the board is turned over for soldering. Figs. 12 and 13 gives p.s.u. board assembly details.

Care should be taken to make sure diodes and radial lead electrolytic capacitors are fitted the right way round. With the general purpose 1N4148 the larger width band indicates the positive end of the diode. Positive or negative markings will be printed on the electrolytic capacitors.

The polyester radial lead capacitors should fit the p.c.b. exactly. They are very fragile and the leads will break off if the capacitor is forced into position.

If lead adjustment is necessary this should be carried out with the use of a small pair of pliers while firmly gripping each end of the capacitor.

SOCKETS

IR

SHUFFIE

RA

WALTZ

It is advisable to use sockets to fit the four CMOS i.c.s. These devices are supplied in a conductive foam or wrapped in tin foil and should not be removed until immediately prior to insertion. Although the devices are internally protected they are still vulnerable to high static charges and it is worth earthing oneself when handling them.

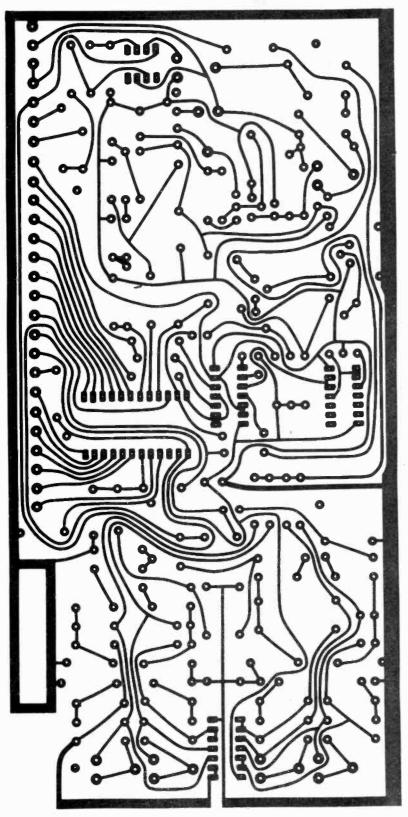
Another point to remember is that they should not be inserted or removed from their sockets while the power is switched on.

The p.c.b. should be visually checked upon completion of assembly to ensure that components are in their correct positions and the track side inspected for any dry joints or solder bridging. Figs. 14 and 15 show the positions of the components mounted to the front and back panels.

SWITCH MOUNTING

The subminiature switches used on the control panel must be tightened from the back of the panel otherwise severe scratching of the anodised finish and the legend will result. The potentiometer spindles should be cut to approximately $\frac{1}{2}$ in before fitting to the panel. The three knots used have a very fine taper on the internal $\frac{1}{4}$ in fixing bore and once pushed on and rotated into place may be difficult to remove:

The DIN socket with the 3.5mm jack socket, fuse holder and grommet are mounted to the back panel as indicated in Fig. 15.



PINS 27º OV 26° 25°}D1 VR10 0000 ICS R 240+12V C31 c 230-12V 220 VR3 210 VR2 29 8 200 514 R 51 R46 19º VR1 \bigcirc 18º VR1 FIXING 170 R30 160 Dol D7 D8 150 C23 140 1 R47 130 R 42 R43 120 LIN 11 0 R p5 100 (C2) 2 90+5V RZ R 61 80 ----70 T ICI C22 -----30 R39 40 De R38 1 1 C39 20 C12 FIXING 10 R21 CIE R31 R14 R15 R34 R20 R13 . DS 28 03 C19 C15 D2 0 0 @ C11 3 67 6 C18 C14 R29 ∋ C10) Ç 6 6 00 R30 R23 R2 -R16 R37 C316 C17 0 C 9 R32 R2 R1 R33 R26 R12 R10 R17 IC R E VR4 POINT VR7 VR6 VR5

Fig. 11. Component layout on main board

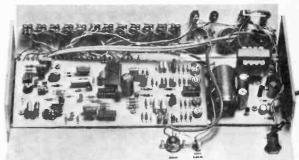


Fig. 10. Printed circuit layout of main board

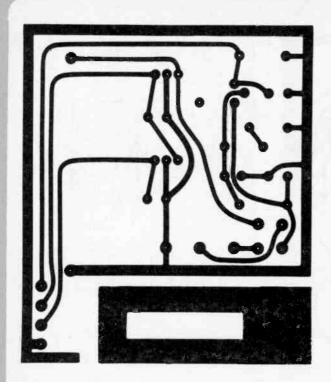


Fig. 12. Power supply board etching details

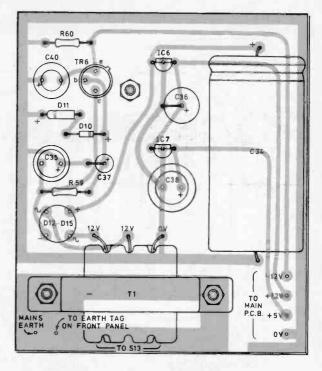
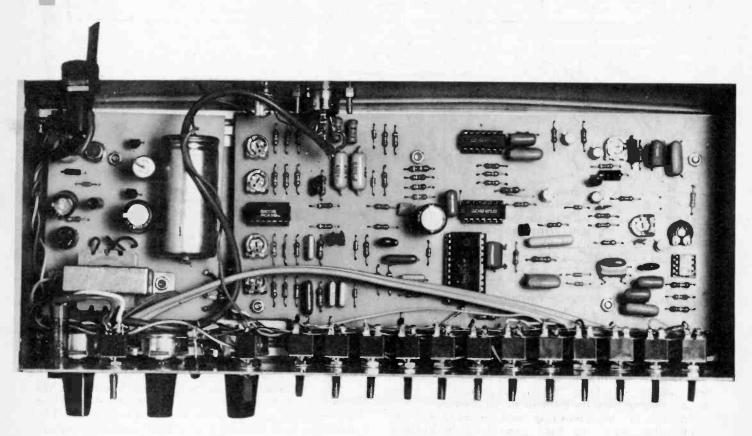
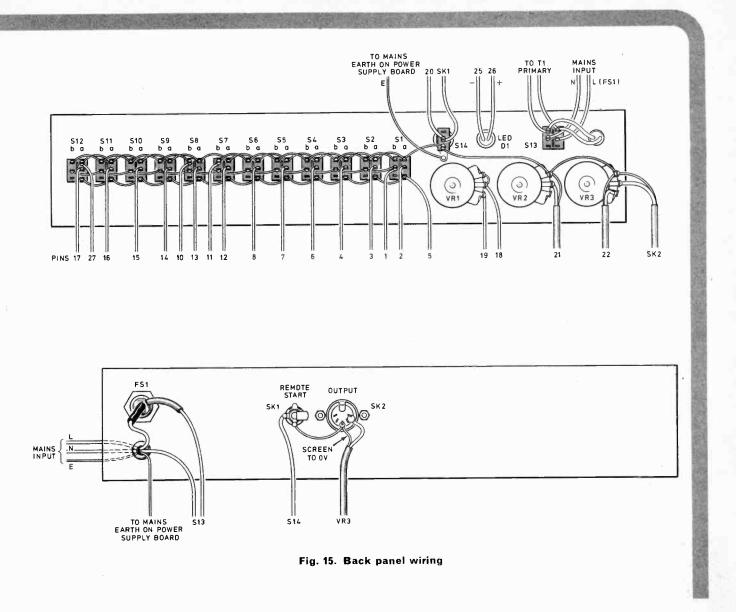


Fig. 13. Component layout of power supply board



Plan view of Generator interior



INTERWIRING

The interwiring is reasonably straightforward with the exception of the selection switch wiring.

Fig. 14 shows the back of the control panel. The five common connecting rails across the switches should be fitted first. The common 0V rail not only links the switches but also VR2 and VR3 and the stop/start switch. It is suggested as this 0V rail is the most complicated of the five that this should be fitted first.

For each of the five rails a length of 22 s.w.g. tinned copper wire should be used.

Start at one end of the line of switches and terminate the wire by wrapping and soldering it into position. The wire is then wrapped over a screwdriver which spaces the bridging link to the next switch. It is not necessary to wrap the wire around each switch tag however—each joint should be soldered quickly to prevent the wiring from springing from the previous switch contacts.

The rest of this interwiring must be made with the front panel, p.c.b. and back panel lying horizontally. The front and back panels must be arranged either side of the p.c.b.

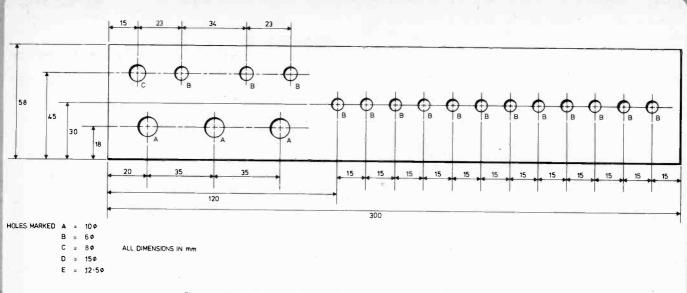
The row of Veropins should be nearest the front panel and two gaps of 30mm each should be left between the p.c.b. and front and back panel. If this gap is not left all the wires will be too short when the assembly is fitted into the case framework.

The connections from the common rails and individual switches can now be made to the p.c.b. It is worthwhile to check every joint after making it as it is possible to forget a connection and be left with one extra Veropin at the end!

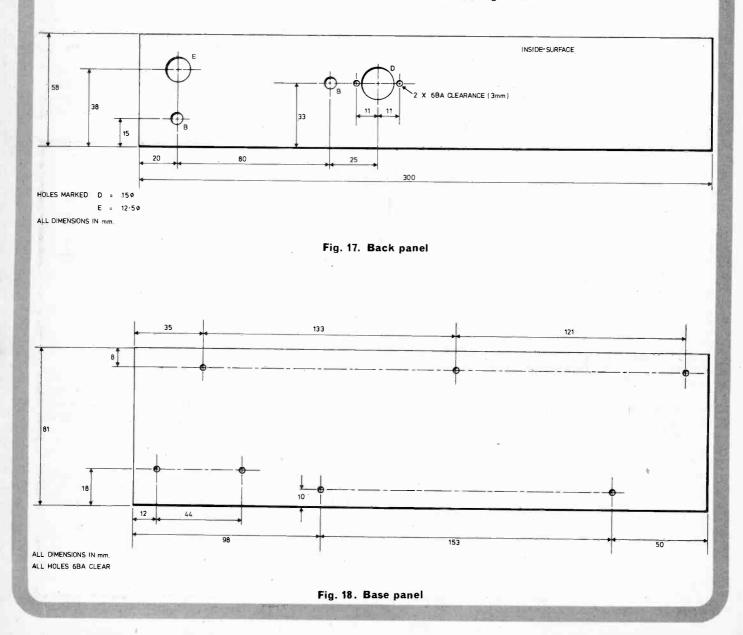
SAFETY FIRST

Whenever a metal case is used to house mains operated equipment, it is advisable to take extra care with the mains wiring connections. Each joint should be inspected to ensure a good mechanical and soldering bond.

It is advisable to scrape away a small section of the anodised finish on the internal surfaces of the four aluminium extrusions and the front and back panels. This should be done to ensure a good earth contact throughout the case, as unfortunately the anodised surfaces act as an insulator.







FINAL CHECK

Apply mains voltage (without any i.c.s in place). The neon should light. Check the voltage across pin 1 (positive) and 2 (negative) of the M253AA socket. The reading should be 17 ± 1V. Also check that the outputs from the power supply board are +12, +5 and -12V.

If the voltages check out, again isolate the supply and carefully fit the i.c.s taking the necessary precautions described earlier with the four CMOS devices.

Check that all the chips are fitted in their correct positions, but do not turn on until you have completed the initial setting up procedures.

INITIAL SETTING UP

Set all the internal preset controls as follows:

Identification	Adjustment	Control Description
VR4	Midway	Oscillator damping
VR5	Midway	Oscillator damping
VR6	Midway	Oscillator damping
V / R 7	Midway	Oscillator damping
VR8	Fully anti- clockwise	white noise generation level
VR9	Midway	Balance of noise to Snare Drum simulators
VR10	Midway	Output attenuation
et the front pane	l controls as foll	ows:
VRI	Midway	Tempo

VRI	Midway	Tempo
VR2	Fully clockwise	Tone
VR3	Fully anti-	Volume
	clockwise	

S13	Start	Stop/Start Switch
S3 to S14	Bossa Nova on	"Rhythm Select"

CONNECT UP

Connect the DIN output to the radio socket of an external amplifier and turn on.

The downbeat lamp should light and by advancing VR3 a rhythmic beat should be heard. The tempo control should be adjusted to suit the rhythm. Continuous oscillations may be heard as well and will be corrected in the final setting procedure.

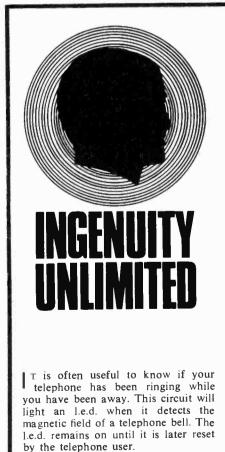
FINAL SETTING UP

With the unit operating the four presets VR4-VR7 should be adjusted just to prevent continuous oscillation. VR9 should be set to give a realistic balance between the white noise simulators and the Snare Drum. VR8 may be backed off from full anticlockwise slightly to reduce harshness of the white noise effect if necessary.

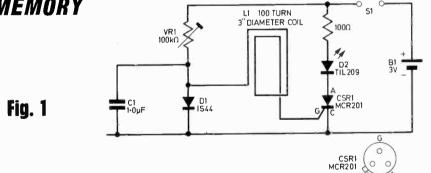
In combination with the adjustment of VR8, switch to the March rhythm and adjust VR9 to achieve the best setting for a realistic Snare Drum sound and correct Cymbals level.

VR10 controlling the output attenuation should be adjusted to suit the amplifier being used. Re-adjustment, using the prescribed procedure may be repeated once or twice to obtain the most balanced and realistic sound. ★

NOTE: In the Components List R61 is 33Ω , VR2–25k Ω logarithmic, C31-0·1µF polyrad and ICI-M253AA, Watford Electronics, 33-35 Cardiff Road, Watford, Herts, can supply a complete kit of parts for £49.95 including VAT & P. & P. £1.25 (insured).



A TELEPHONE MEMORY



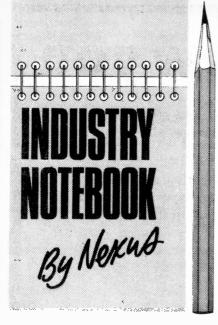
In Fig. 1 a 100-turn 3in. diameter coil of 30 s.w.g. enamelled copper wire is positioned on the underside of the telephone in a position (approximately dead centre where the bell magnetic field can be picked up. Voltage induced in the coil appears across the gate/cathode of thyristor MCR201 which is already biased close to conduction by the voltage across diode D1. This additional voltage, caused by the bell, triggers the thyristor and lights the l.e.d.

To reset the circuit a normallyclosed push button is pressed to temporarily interrupt the supply to the circuit.

As the value of VR1 is reduced, a point will be reached where the thyristor will spontaneously trigger. The value of VR1 should be increased a small amount from this point to set the circuit at its most sensitive.

This circuit draws approximately $60\mu A$ when the l.e.d. is not lit, and 7mA when it is, therefore dry batteries will give quite a good life.

A. Russell, Whinmoor, Leeds



MARINE ELECTRONICS

The slump in the shipping industry and in particular in the fishing industry has gravely affected a few companies, notably Redifon now phasing out their Cwmbran, South Wales, manufacturing plant with 250 redundancies. But some companies in the marine business continue to prosper. Prime example is Decca Radar, currently selling over 5,000 marine radars a year. Starting from nothing in 1950 the grand total is 75,000 radars sold, 15,000 in the last three years of difficult trading conditions.

Another boom sector is in the North Sea drilling rigs where the chief beneficiary is Marconi with multi-channel over-the-horizon troposcatter systems coupled into the UK telephone network. The investment by the Post Office in such systems is £5 million.

Finally, there is the VLF global navigation system code-named Omega which will get its final validation for accuracy in 1982, the aim being one nautical mile accuracy in daylight and two miles at night. The market for shipborne Omega as a master navigation system is already established but is clearly capable of enormous growth.

BIGGEST DATA BANK

Disk storage of 2,800 million bytes, all of it on-line and said to be equivalent of 10,000 books of novel length, is now available at Aberdeen University through its recently commissioned Honeywell 66/60 computer. University departments can interrogate the system through 100 remote terminals, most of them VDUs.

Of topical interest is the work of the Department of Arts and Social Science using the computer to analyse trade union bargaining and wage rounds. How sensible it would be to feed in workers' demands on the one hand and employer's ability to pay on the other. the length of time a strike could last without the employer (or the country) collapsing, or workers starving, overall cash loss to the country (there is never a gain), damage to trade both in short and long term etc., and let the computer work out the compromise solution which is invariably arrived at. If every dispute were to be solved by computer there would be no need for strikes. I doubt if the, Aberdeen researchers are thinking along these lines. I offer the idea free of charge but with little hope of its adoption. Far too many trade union officials and industrial relations officers have a vested interest in interminable argument to accept the impartial and practically instantaneous solution that the computer can and should be allowed to provide. And where could such people, if made redundant, find alternative employment?

INVENTOR'S CHANCE

Odd phenomenon of 1977 was the National Research Development Corporation's inability to attract new joint venture schemes to exploit inventions and ideas. With a pre-tax surplus of over £10 million for the year 1976–77, up from £3'7 million the previous year, NRDC has plenty of cash to back new projects but few takers. NRDC holds some 5,000 patents in the UK and overseas and is currently co-operating with nearly 1,000 companies.

Should 1978 prove to be a vintage year for inventions, NRDC has the cash but any schemes put forward needs to have originality and the prospect of profitable exploitation in the market place. Perpetual motion machines are not encouraged. In its life-time, NRDC has examined schemes from over 28,000 companies and only 7,000 have qualified for a second look.

PLESSEY STAYS FIRM

Plessey, hard hit by the Post Office cut-backs in orders, shows great underlying strength. Pre-tax profits for the quarter to last September totalled £9.6 million against £8.1 million on world sales nine per cent up at £149.7 million. Exports over a half year have increased by 51 per cent.

The weakness of being overdependent on a single large customer, in this case the British Post Office, is illustrated by the labour force of 20,000 (slimmed down from 23,600) on telecommunications which contributed only 30 per cent of sales in the last half year. Contrast this with the 8,800 people in Plessey Electronic Systems who accounted for 37 per cent of sales and 40 per cent of the pre-tax profit. The big breakthrough for Plessey may come next April when the International Civil Aviation Organisation (ICAO) is meeting in Montreal to decide on the next generation of instrument landing systems for airports. Plessey's doppler microwave system has a good chance of succeeding in the competition and if it does it will create work for years ahead and good profits from manufacturing and licence agreements.

Meantime, an example of Plessey's advanced technology is the recently announced PR2250 professional communications receiver which includes a microprocessor for programmed surveillance of spot frequencies and a memory module which allows instant tuning to 16 pre-set frequencies at the touch of a button. Real state-of-the-art, but it also costs real money, about £6,500 each says Plessey but you might be able to negotiate a quantity discount!

RACAL EXPANDS

It's still action all the way in the Racal Electronics Group with expansion at home and overseas. Dana Laboratories in Irvine, California is the latest acquisition together with the Dana sales affiliates in the UK and France. The Dana range of digital instruments is now added to the complementary range from Racal Instruments Ltd and the combined instrument operations will soon be trading with the new name of Racal-Dana Instruments Ltd under the overall direction of John Ceresa who heads up Racal Instruments in the UK.

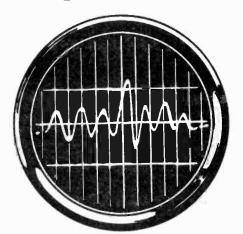
The new acquisition immediately bumps up Racal turnover in instruments by £5 million and the combined Racal-Dana is targeted for £13.8 million turnover in its first full year of operation. So Racal-Dana is now pressing hard on the heels of Marconi Instruments, at present the largest of the British-owned companies in electronic test and measuring instruments.

British Physical Laboratories, the specialist analogue panel meter company in the Racal Group has now established West Germany as its largest single export market. Among recent successes is a five-year contract for the supply of meters to Robert Bosch GmbH. Also in Germany, Racal-Redac the CAD company has opened a new sales office at Bensberg near Cologne, supplementing the Munich office which was opened in January 1977.

Of course anyone can build turnover by buying companies or selling products at give-away prices. What counts in the end is profitability and here Racal cannot be faulted, having achieved the number one spot in the profitability league table of 200 British companies published by "Management Today", topping even ICI and Shell.

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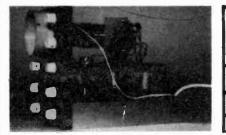
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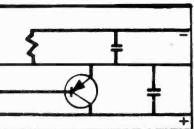
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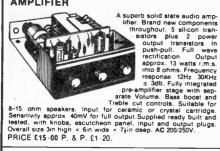
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SURPLUS

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The centenary year of recorded sound has now passed: so it seems fitting to mention briefly some of the most important patents relating to sound reproduction which have been granted over the past hundred years. All the patent specifications mentioned can be referred to, free of charge, at the Science Reference Library attached to the Patent Office, just off Chancery Lane in London, during Civil Service working hours. Where possible British rather than foreign specifications have been cited because many of these will also be available for reference in the two dozen public libraries in cities around the UK that hold patents.

INVENTOR

There is a dispute over who should be credited with the invention of the gramophone. One school of thought argues in favour of Frenchman Charles Cros, who, in April, 1877, deposited a sealed packet of documents at the Academy of Sciences, with instructions that it should not be opened until December 1877. The packet described a photo-mechanical process of recording sound on a disc, but it was never put into practice by Cros. Meanwhile, Thomas Alva Edison was working on improvements to the basic telephone and telegraph system.

In July 1877, Edison filed a British Patent (BP 2927/1877) for a scheme to make a permanent record of a telegraph message by making impressions in paper on a disc or cylinder backing. In the same month, Edison patented (BP 2909/1877) a microphone system which enabled the human voice to be transmitted over telegraph wires. The electrical resistance of a point of contact on a diaphragm varied as the diaphragm vibrated, so as to modulate a d.c. current. Although this patent appears to contain details for producing the first gramophone, or phonograph as Edison called it (by teaching how to use the vibrating diaphragm to cut a groove in a cylinder), the filing date for the relevant drawings and description is, in fact, much later-January, 1878. By this time Edison had

Copies of Patents can be obtained from :

already filed what is the master patent on the Phonograph, USA Patent 200521.

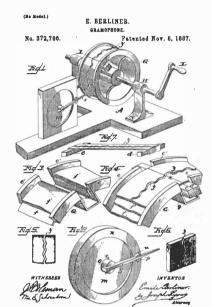
the Patent Office Sales, St. Mary Cray, Orpington, Kent

This patent described a cylinder recording system for the human voice. Its filing date, December 24, 1877, is regarded by many as the birth-date of recorded sound.

LATERAL CUT

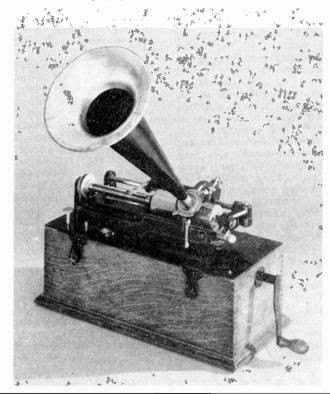
In 1887 Emile Berliner patented lateral-cut recording (USA Patent 372786) as the solution to the mass reproduction of recordings, and although Edison had already patented similar suggestions (even in the 1877 Christmas patent), Berliner's claims are regarded as the birth-date of the modern pressed disc record. Interestingly, Berliner's patent refers to a "gramophone", rather than the "phonograph" referred to by Edison.

Two years before Berliner (in 1885) Sumner Tainter had patented the basic



Price 95p each

Edison phonograph, Home Model A, American 1898 (Science Museum Photograph).



concept of magnetic recording. He proposed a disc with a groove cut in its surface to induce electric currents in a coil when tracked by a needle, with the currents transduced into sound by a telephone diaphragm (USA Patent 341287). In 1899 Valdemar Poulsen of Denmark patented (BP 8961/1899) a magnetic recorder designed to function as a phonograph or a telephone answering machine. Poulsen was probably the first man actually to make a reliable magnetic recording, and at the Paris Exposition of 1900 he won the Grand Prix. In the same year, Guglielmo Marconi patented the first tunable wireless system (BP 7777/1900).

VALVE

In 1904 John Ambrose Fleming of University College, London, patented (BP 24850/1904) "a vacuous vessel having in it two conductors . . . one of them heated" and the diode valve was born. In 1907 Lee de Forest, of New York, patented (BP 1427/1908) a modi-"evacuated vessel" which confied tained an extra electrode to make it a triode. Although de Forest is rightly credited with inventing the audion, as it was then called, it is important to note this valve really only found a valuable use, and fame, when Edwin Howard Armstrong in the USA invented and patented the feedback principle. The relevant patent is USA 1,113,149 which dates back to a notarised document of January, 1913.

It is also interesting to recall that in 1882 Edison had almost patented the valve! His USA patent No. 273,486 related to an early form of electric light bulb and described the phenomenon whereby material gradually disperses from the filament and accumulates on inside surface of the glass the envelope, blackening it and leaving the filament weak. Edison's answer, buried in the patent as an afterthought amongst other suggestions, was to use a second filament in the same envelope electrically connected to one side of the d.c. supply. This attracted or repelled the particles leaving the filament and thus prevented them from reaching the glass. In other words Edison had patented a diode, nearly twenty years before it was invented

incidentally, Edison as far back as 1878, had also patented disc and cylinder machines with facilities for electro-magnetic cutting and reproduction (British Patent 1644/1878). Oliver Lodge, of University College, Liverpool, in 1898, was almost certainly the first worker to invent and patent (BP 9712/ 1898) a moving coil microphone or speaker system.

Everything had so far, of course, been in mono, or single channel. In 1920, a Washington inventor, Samuel Waters, filed a patent (USA Patent 1520378) for a two-channel disc reproducer. The object of the exercise was to improve signal to noise ratio rather than to create true stereo, as was interesting other workers at the same time, especially in the cinema. As early as 1911 Augustus Rosenberg of High Holborn, London, had patented a twochannel optical film recording system (BP 23620/1911). Incidentally, it was in 1925 (in British Patent 258 864) that the word "stereophonic" was used almost certainly for the first time.

STEREO

In 1927, W. Bartlett Jones, of Chicago, patented (USA Patent 1855149) the first binaural, or dummy head, stereo system. And in 1931 Alan Blumlein of EMI patented loudspeaker stereo and the 45 degrees double modulation of a 90 degrees groove, as used today (BP 394 325).

In 1936, Bell Telephone Laboratories filed a patent (USA Patent 2137032) which, buried in amongst its other disclosures, taught how the apparent direction of a sound source could be manipulated by altering volume levels to the loudspeakers—the way in which modern pan-potted recordings are made and stereo balance controls function.

Earlier, in 1929, Arthur Keller of Bell Telephone Laboratories in New York had patented the basis of modern multiplexing (USA Patent 1910254), by describing how two separate channels of sound could be recorded in a single record groove by division into two separate frequency bands.

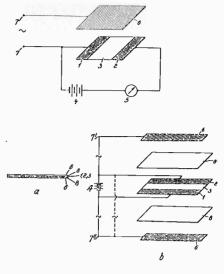
Modern multi-channel discs of discrete multiplex type (as marketed by JVC for the CD-4 system) find their origin there and in a 1946 invention made by EMI engineer William Livy (BP 612 163). The system relied on a recorded carrier to lock a demodulation oscillator to the rotational speed of the record.

Meanwhile, there was considerable invention in other closely associated areas. As early as 1900 Joseph Poliakoff of Moscow had patented (BP 18046/1900) an optical film recording system using a selenium photo-cell. The idea was taken several stages further by Eugene Lauste of London in 1906 (18057/1906). In 1924, Paul Voigt of London patented (BP 231 972) a feedback circuit for an amplifier to compensate for distortion introduced by the loudspeaker-i.e. motional feedback. In 1933, Maj. Edwin Armstrong of New York, USA, patented the basis of modern f.m. radio (USA Patent 1941069).

F.E.T.

In 1934 in Berlin, Oskar Heil invented a solid-state amplifier of semi-conductive material and patented it in Britain (BP 439 457). Oskar Heil is better known for the air-motion transformer loudspeakers sold today by ESS, but his 1934 invention was the first f.e.t.!

A workable system of video recording



Paul Voigt patent illustration of 1924

was first patented in 1955, by the Ampex Corporation of California (BP 798 927), one of the named inventors being Ray Dolby. BP 1 120 541, of 1965, is in the name of Ray Dolby alone, and constitutes the first patent disclosure of the now well known Dolby noise reduction system. Over recent years much audio patenting activity has centred around surround sound or quadraphonics, the first major matrixing patent being that filed in 1969 by Peter Scheiber of New York (BP 1 328 141 and 1 328 142). The current resurgence of interest in surround sound and the lack to-date of any standardisation on an agreed world system, suggests that the next few years will see this trend of interest continuing. Most recently, and in a slightly lighter vein perhaps, the cinema sound development, Sensurround, which enables audiences to be literally shaken in their seats by very low frequency sound waves generated by high power "effects" circuits is patented in USA Pat. No. 3 973 839. This lengthy patent and ten sheets of circuit diagrams give very full details of how the effects are generated and handled.

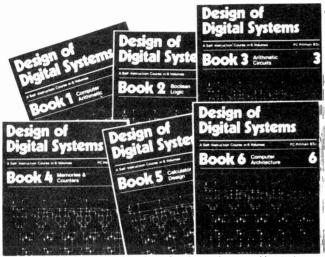
Readers who are particularly interested in the history and development of sound may find the current exhibition of over a hundred instruments from the EMI collection of vintage phonographs and gramophones, at the Science Museum, South Kensington, London, of particular interest.

Included in the display is an example of the gramophone that appears in the famous "dog-and-trumpet" trademark and an instrument that could be folded up and pocketed. The exhibited instruments illustrate developments from 1877 to about 1935 but a further display of posters, record sleeves and photographs covers the full 100 years. The exhibition is located in gallery

1, and is open daily until April.

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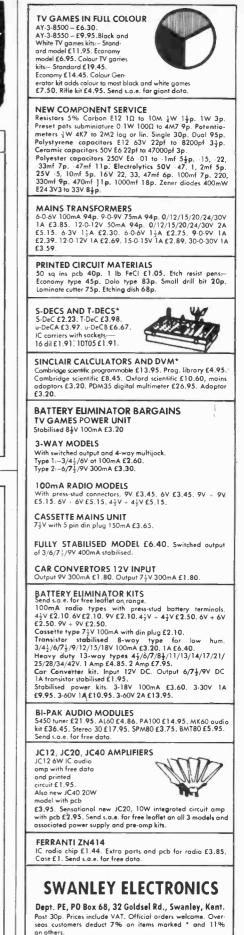
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G. LOVEDAY

Fault Finding on Systems

HE first part of this series dealt with faults caused in an electronic circuit by one component failure. It was shown that when a component fails; goes open or short circuit, then a certain set of symptoms result, and by using these symptoms it is possible to pinpoint the faulty component. The symptoms are any changes in the circuit operation, such as low output signal with distortion, and changes in the d.c .bias voltages. However, when it comes to fault finding on a complete electronic instrument, or system, the situation is made more difficult because of the size and complexity of the system. One component failure will often cause the whole system to fail, but the total number of components may number several hundred. Since time, in the service situation, is of prime importance, it's not acceptable to sit down and methodically measure every voltage and waveform until the faulty component is found. Another technique must be used.

Luckily nearly all electronic instruments can be divided up into several functioning circuit blocks and the quickest way to find the faulty component is by measuring to first of all locate which portion or block of the system has failed, then to work on that block to find the actual component.

THE BLOCK DIAGRAM

This is a really valuable aid in servicing and in helping to understand the operation of a complex piece of equipment. For example, let's look at the block diagram of a basic r.f. signal generator shown in Fig. 2.1. It is made up of six blocks, each of these performing a separate circuit function. A variable r.f. oscillator feeds a sine wave signal to an amplifier and the output of this amplifier can either be amplitude modulated at 400Hz or constant wave (c.w.) depending upon the setting of the switch.

Since these are two output signals and two possible output conditions for the r.f. output, we can use the states of the outputs as symptoms to fault find the generator. If, for example, there were no outputs at all the fault would most probably lie in the power supply, since it would be unlikely (although possible) that both oscillators had failed. Suppose, however, that the r.f. output was correct in both the modulation and c.w. switch positions but no a.f. output could be obtained. The fault lies in the a.f. attenuator or its connections. These examples show the sort of logical approach

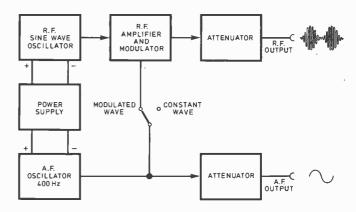


Fig. 2.1. Block diagram of r.f. generator

445

that's required. The various methods for system fault finding will be shown later in this article. What would be the symptoms for (a) an a.f. oscillator failure or (b) a modulator failure.

INTERPRETING IT

Now let's look at the way in which a block diagram can help in understanding how a unit operates. A switched mode power unit has a full circuit diagram that can look rather forbidding, but when it is drawn out in block form (Fig. 2.2) the operation can be more clearly understood and fault diagnosis is made much easier. Switch power supplies are used in relatively high power applications (e.g. 5 volts at 20 amps) because they have high efficiency, low heat loss and therefore use up less space than a conventional stabilised power unit. The mains voltage is itself rectified and smoothed giving about 340 volts d.c. This voltage is switched at a frequency above audio, usually 20kHz, by high voltage transistors to provide an alternating waveform to the transformer primary.

Since a fairly high frequency is used the transformer need not be so bulky as a 50Hz type. The a.c. voltage at the secondary is rectified and smoothed to give a d.c. voltage across the load. The output is stabilised by comparing it with a reference supply (usually a Zener) and using the different signal to alter the duty cycle of the switching signal to the transistors. If the d.c. output should fall when the load is increased the comparator gives a signal to the pulse width modulator that switches the transistors on for a longer time than they are off during the 20kHz switching period. This provides more power via the transformer to the load and the output voltage rises. The opposite occurs if the load current is reduced.

METHODS FOR SYSTEM FAULT FINDING

One of the first jobs when fault finding on a system is to accurately define the fault. To do this a functional check must be made and the exact symptoms noted. This usually entails making measurements and comparing the performance with the actual specification. In a service department the engineer would need the up-to-date figures for the performance specification plus the circuits and service manuals and also the necessary test gear. In any project work we should follow the same procedure.

At this stage, depending on the symptoms, it is wise to check that the power supply rails are at their correct voltage levels before proceeding to make measurements to narrow down the search for the faulty component to one part of the block diagram.

It's possible of course to use a completely random approach to find which block is faulty, checking the circuits in any order, but usually a systematic logical approach yields the quickest results. The three methods are called:

- (1) Input to output (or beginning to end)
- (2) Output to input (or end to beginning)
- (3) Half-split.

Here we are considering actual measurements, but don't forget that a visual inspection for broken wires, dry joints, burnt components, damaged copper track, etc., can also be worthwhile. This is especially the case when a system that you have just assembled refuses to function at all.

METHODS ANALYSED

The first two methods listed above are fairly obvious and most of us used input to output checking before we knew that somebody had given it a name! A suitable input signal (if required) is injected into the first block and then measurements are made sequentially at the output of each block in turn until the faulty block is located. Output to input is the reverse; leaving the input to block (1) measurements are made from output block towards the input. This presupposes that the units are all in series, but this is rarely the case. The s.m.p.u. for example cannot be fully checked using a straightforward sequence of tests. Suppose the unit fails with the symptom of zero output. The fault could be in almost any block. One sequence of checks to find that fault could be the following:

- (a) Measure d.c. voltage from mains rectifier block (1)
- (b) Measure output of 20kHz oscillator block (2)

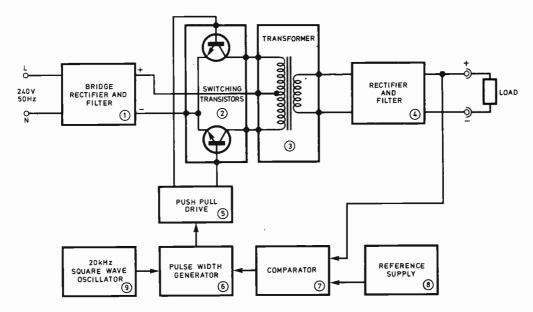


Fig. 2.2. Block diagram of switched mode power unit

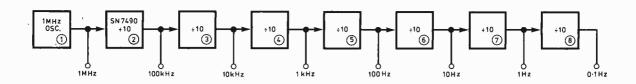


Fig. 2.3. Frequency divider chain

By doing these checks first we verify the two primary conditions for an output across the load. Assuming both these blocks are functioning correctly we can then use output to input by measuring (4), (3), (2) and then (5), (6), (7), (8) or input to output measuring from (8), (7), (6), (5), (2), (3), (4). Either method is satisfactory, but the first is probably the best as it checks early on through the circuits that probably have the highest failure rate (namely the switching transistors). Using this criterion the sequence of test could be (1), (9), then (2), (3), (4), and finally (5), (6), (7), (8). The important thing to realise is that the tests ought to follow some logical sequence.

Imagine now a fault with the symptoms of high unstabilised output voltage. From this we can conclude that blocks (1), (2), (3), (4) and (9) are all operating. The fault is somewhere in blocks (5), (6), (7), (8). Here a good start would be to measure the output of (8) since an open circuit reference supply would give these particular symptoms.

HALF-SPLIT METHOD

The half-split method for system fault location is really useful when the instrument or system is made up of a large number of blocks in series. A good example is fault finding on the frequency divider chain of a digital frequency meter (Fig. 2.3). Here the frequency of a 1MHz crystal oscillator is divided down by decade counters to give the required timing pulses. Since eight blocks are used it is possible to divide the unit into two equal parts, test to decide which half is working correctly, then split the non-working section into half again to locate the fault. Let's assume that block (6) has failed; the sequence of tests would be as follows:

1. Split whole unit into half by measuring output from block (4). This will be alright showing that the fault lies somewhere in blocks (5) to (8).

2. Split blocks (5) to (8) in half checking output of block (6). There will be no output.

3. Check output of block (5). This will be all right proving that the fault is in block (6).

Now try the method for yourself by assuming that block (3) or block (8) has failed, and you will find that the number of checks necessary to locate the fault is always three. On average more tests would be required using any other method. Unfortunately many instruments are not made up of many blocks in series. More often than not a system has feed back loops that are necessary for operation and which cannot be split. Also convergence, where two inputs are required to make a circuit block operate correctly, and divergence, where an output from a block feeds two or more other blocks are quite common. These situations complicate the use of the half split. When fault finding try and use the method, or a combination of methods that will locate the faulty block in the shortest possible time. This isn't always achieved with the minimum number of test measurements. A common sense logical approach to the problem is the basic requirement.

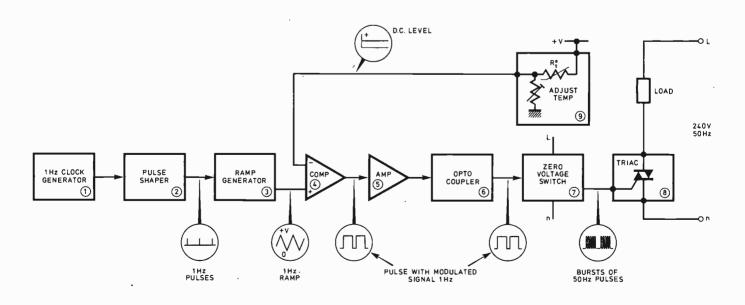


Fig. 2.4. Block diagram of temperature controller

TEMPERATURE CONTROLLER FAULT DIAGNOSIS

As a final exercise we are going to look at the block diagram of an oven temperature controller. This is a nice series type of circuit but with the added complication of feedback from the temperature sensor. The unit uses burst cycle firing of a triac to control the power dissipated in a heating element. With this type of control, power is applied for a few cycles of the mains at a time, say 40 out of 50 cycles when the temperature is lower than required, reducing to maybe 5 out of 50 cycles when the oven temperature has stabilised. A zero voltage switch ensures that the triac is only pulsed on when the mains voltage is near zero thus eliminating the generation of r.f. interference.

The operation is fairly straightforward. A clock generator gives pulses via a shaping circuit of 1Hz to a ramp generator. This ramp is compared with the d.c. level from the temperature sensor. When the temperature inside the oven is lower than required this d.c. level is also low so the output of the comparator is high. The ramp goes from a positive voltage towards zero. While the ramp voltage exceeds the d.c. voltage from the sensor the output is high. This level is amplified and then applied via an opto-coupler to the zero voltage switch. The opto-coupler ensures that the mains side of the system is isolated from the low voltage portion. While the comparator output is high the zero voltage switch delivers pulses to gate on the triac and so power is applied to the heater. As the temperature in the oven rises so does the d.c. voltage from the temperature sensor and this means that the comparator output is high for a shorter time during the 1 second clock period.

A FEW QUESTIONS

The feedback could complicate fault diagnosis but since



MODERN ELECTRONICS MADE SIMPLE By G. H. Olsen Published by W. H. Allen & Co Ltd 306 pages, 130 \times 215mm. Price £1.75

HIS book is good value indeed! It covers a wide variety of fields, and would serve as an excellent reference to have around for those whose memories occasionally require refreshment (most of us), or for the student of "A" Levels or an ONC Course, or C&G, at college.

The author has gauged the contents so that no prior knowledge of electronics is needed, other than basic electricity, and each new device covered is explained in terms of its physics before commencing with applications and design theory. The explanations are fairly thorough; for instance, the chapter entitled "Power Supplies" starts with batteries and their very chemical structure. Questions are posed at the end of each chapter, which you should be able to answer correctly before advancing to the next section.

The final chapter, "Projects", gives a number of circuits to play around with—just to satisfy yourself that what you've learned really works! These are by no means constructional projects in the sense that P.E. presents them, but if reading is the way to learn, then this is the way to remember.

all the rest of the circuit blocks are in series it is possible to use any of the methods described. We just have to ensure that a reasonable d.c. level is present on the inverting terminal (-) of the comparator. Assuming that the temperature sensor is o.k. a meter could be used to monitor this d.c. voltage or alternatively the feedback line could be broken and an adjustable d.c. voltage applied in its place.

If you are still with it, try your hand at answering a few questions:

(1) Which fault finding method should theoretically get the quickest results?

(2) What would be symptoms for the following faults? (a) Short circuit triac.

(b) Temperature sensor open circuit.

(c) No output from 1Hz unit.

(d) Ramp output failed with output permanently low.

(e) Ramp failed with reduced amplitude (lower starting voltage).

ANSWERS

(1) Half split.

- (2) (a) Oven overheating, no control. Few pulses at the output of the zero voltage switch.
 - (b) Oven overheating, no control. Many pulses at the output of the zero voltage switch.
 - (c) Ramp output will remain at +V therefore full power will be applied to the load. Many pulses at the output of the zero voltage switch.

(d) No heating. Low d.c. level from temperature sensor. Output of comparator remaining low however. (e) Slow response to changes in temperature control.

Next month: Fault diagnosis of thyristor and triac circuits.

My only criticism would be against the title, in that it's not so much a case of Modern Electronics Made Simple as just modern electronics set out clearly; but perhaps this is a trivial point since clarity is half the battle. M.A.

TV TECHNICIAN'S BENCH MANUAL By G. R. Wilding Published by Argus Books Ltd. 217 pages, 143 × 224mm. Price £4-50

T is the objective of this hardback, to present in a handy form adequate information for the service technician or enthusiastic amateur to locate television receiver faults of all kinds, fairly promptly.

Each chapter gives a brief run-down of all important aspects of the receiver section it covers, followed by the recommended servicing procedure to break down the most likely cause of trouble in order of probability.

Circuit diagrams for specific television receivers are present throughout, extracted from various manufacturers, but not too many circuit diagrams from Japanese sets are given.

There are 13 chapters, covering just about all the aspects of television receivers, and the last four chapters form a section devoted to colour.

This book gives fairly thorough coverage of its subject, but assumes a certain amount of prior knowledge, and therefore is not suitable for anyone seeking to understand television for the first time. As the name suggests, it is for the technician who already understands the overall functioning of a television. but perhaps needs a reference source for the more subtle variations he may encounter with different sets, and the appropriate servicing routines. M.A.

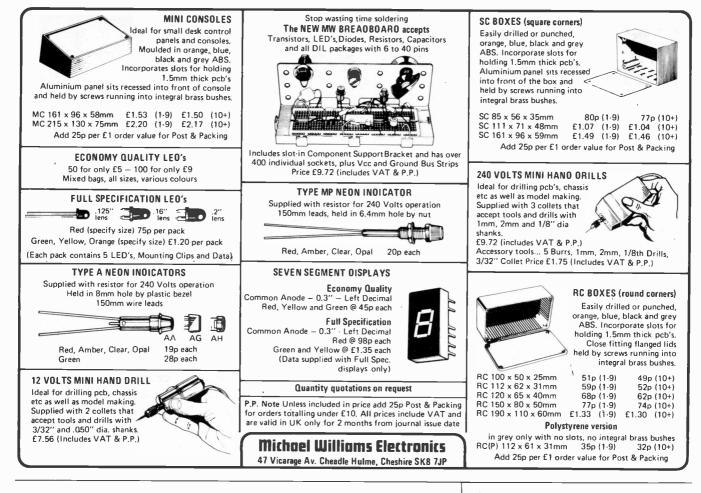
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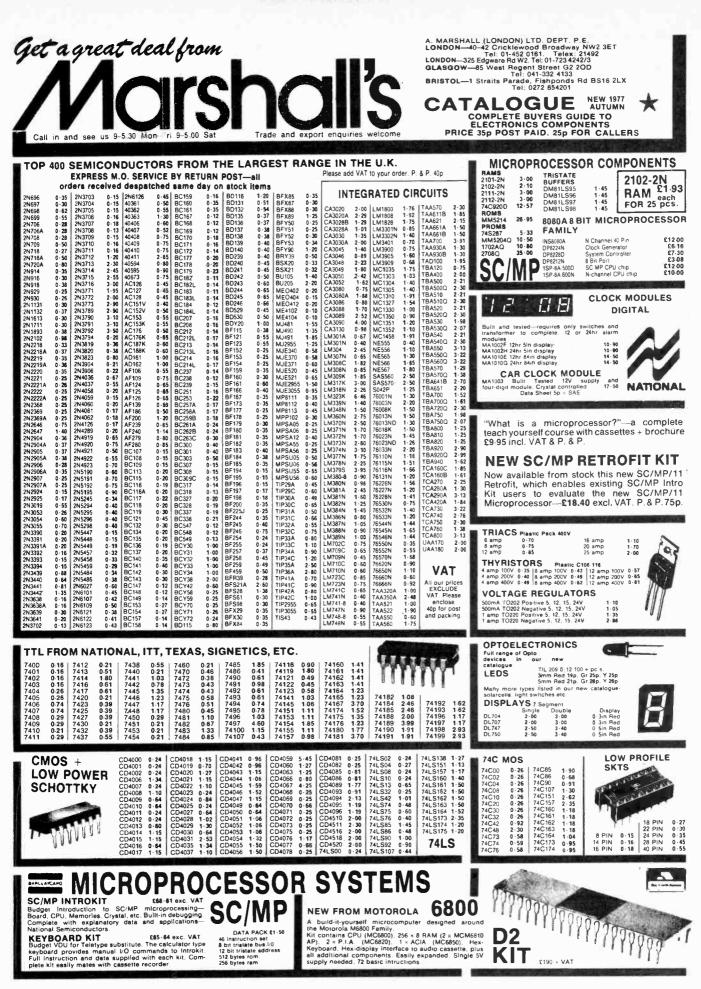
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AC127 0-28	BC182B 0 12* BC182L 0 11*	BF178 0-24 BF179 0-25	OC74 8-45 OC81 0-60	2N3705 0-14* 2N3707 0-12*	1/75 0 10° 50/10 0 10° 2 2/25 0 10° 50/15 0 10°	2200, 3000, 4700, 10000 47000pf; 1MFD 10V. All at	709 (8 PIN DIL) 0-40	7402 18p
AC128 0-20	BC183B 0-10*	BF183 0-34	OC82 0.70	2N3708 0-12*	2.2/63 0.10 100/18 0.06	6p* each. 1MFD 63V 8p*.	741 (8 PIN DIL) 0-28 AY-5-1224 3-75	7403 18p 7404 23p
AC151 0-35	BC183L 0-10*	BF184 0-25	ORP12 0-68	2N3709 0-14*	2.5/64 0.10* 100/25 0.10*	RESISTORS 2p* each	AY-3-8500 T.V. 6-00	7407 490
AC153 0-35 AC176 0-22	BC184B 0-12* BC184L 0-11*	BF185 0-28 BF194 0-10*	TIP29A 0-47*	2N3710 0-11* 2N3711 0-11*	4 7/16 0 08* 100/35 0 11* 4 7/63 0 10* 100/50 0 15*	One-third WATT E12 (5%)	CA 3130 0-87*	7408 24p
AC187 0-22	BC186 0-25	BF195 0-10*	TIP31A 0.57	2N3819E 0 25*	4 7/63 0 10* 100/50 0 15* 5/10 0 10* 100/35 0 15*	1 ohm-10m ohm.	LM 301AN 0-55 LM 308 1-40	7410 18p 7411 24p
AC188 0.20	BC187 0-26	BF196 0-12*	TIP32A 0.67	2N3820 0-45*	5/16 0.11* 220/16 0.15*	PRESET MIN. VERT.	LM 309K 2:00	7411 24p 7412 25p
A C187/188 mtch. pr.0-85	BC204A 8 16*	BF197 0-12*	TIP33A	2N3823E 0-25* 2N4036 0-40	6-8/25 0-10* 220/25 0-16* 6-8/40 0-10* 220/63 0-25*	SUB MIN V & H.	LM 324 2.05	7413 38p
AD149 0-68	BC204B 0/16* BC209B 0 13*	BF199 0-15* BF200 0-38	TIP34A 1-13 TIP41A 0-67	2N4058 0-16*	6.8/40 0.10° 220/63 0.25° 8/70 0.10° 250/12 0.12°	100ohm, 220ohm, 470ohm, IK, 2K2, 4K7, 10K, 20K, 50K,	LM 380/SL60745 1 - 29* LM 38IN 2 - 00*	7414 72p 7416 36p
AD161 0-52	BC212A 0-13*	BFX29 0-20	TIP42A 0-80	2N4059 0-10*	10/16 0.09" 250/50 0.18"	100K, 250K, 470K, 1M, 2M2.	LM 555 0-49	7416 36p 7417 36p
AD162 0-52	BC212L 0-15*	BFX30 0.25	TIP2955 0-97	2N4061 0-12*	10/25 0.09* 250/64 0.20*	\$p* each.	LM 723 0 59	7420 18p
mtch. pr.1-24 AF116 0-24	BC213B 0-12* BC213L 0-14*	BFX40 0-28 BFX84 0-22	TIP3055 0-60 TIS43 0-35*	2N4124 0-20* 2N4126 0-30*	10/35 0.10° 330/16 0.15° 10/64 0.10° 470/6V3 0.10°	THYRISTORS	LM 3900N 0-69 MC 1310/CA1310E	7421 26p 7427 32p
AF117 0-28	BC214 0 15*	BFX88 0-22	ZTX109 .14*	2N5298 0-50	10/250 0.18* 470/10 0.12*	60V 1A 0.25	2-55*	7427 32p 7428 56p
AF124 8-38	BC214L 0-17*	BFY50 0-25	ZTX300 8-13*	2N5457 0-50	15/40 0.10 470/16 0.18	100V 1A 0.38 TAG 1 100 200V 1A 0.60 TAG 1 200	MC 1327/SN76227	7430 18p
AF185 0-95 AF239 0-46	BC237A -16*	BFY51 8-25	ZTX301 0 13*	2N5458 0-40* 2N5459 0-40*	15/400 0 35° 470/25 0 20° 16/10 0 10° 680/25 0 25°	600V 1A 0-80 TAG 1 600	MC 1330P 0.75*	7432 28p
AU113 2 20	BC238A 0-15* BC261A 0-16	BFY52 0-25 BSX20 0-23	ZTX302 0 18* ZTX500 0 15*	2SC1172 3.00*	20/15 0-10* 1000/16 0-25*	700V 1A 1 40 BT 106	MC 1330P 0-75* MC 1350P 0-75*	7437 42p 7440 18p
BC107 0-11	BC262 A 0.19	BU108 2-50*	ZTX502 0-18*	40361 0-50	20/70 0.10* 100/25 0.30*	400V 4A 0.65 C106D1 500V 61A 1.85 BT 109	NE 555 0-49	7442 68p
BC107A 0-12 BC107B 0-13	BC267A 0-17	BU208 3-00*	ZTX504 0 25*	40363 0·88 40673 0·85	22/6V3 0-10* 1000/50 0-40* 22/16 0-10* 1500/25 0-35*		SK 1122 T.V.	7443 1-00p
BC108 8-16	BC268B 0-17 BC269 0-17	BY126 0-16 BY127 0-18	ZTX530 0-23* 1N914 0-05		25/25 0.11* 2200/6V3 0.30*	ZENERS (400mw) BZX 83 3V, 3V3, 5V1, 5V6, 7V5, 9V1,	Game 18-00* SN 76003N 2-80*	7444 1.00p 7446 1.00p
CIL108 0-08	BC287 28	8Y133 0-20	1N4001 0-05	VARICAP I TUNER	33/50 0.12* 2200/40 0.60*	10V 12V, 18V 22V, 30V.	SN 76013ND 1-60*	7447 980
BC108B 0-11	BC300 0-35	BY164 0-40	1N4002 8-06	ECL1043/05	47/6V3 0-10" 2500/15 0-45" 47/10 0-10" 3300/30 0-45"	All at 12p* each.	SN 76013N 1 75*	7448 98p
BC108C 0-12 BC109 0-12	BC301 0-34 BC303 0-35	ME0401 0-18* ME0402 0-18*	1N4003 0-07	£5°	47/16 0 10 5000/12 0 45	MULTI METERS	SN 76023N 1 75* SN 76023ND 1 60*	7451 18p 7460 18p
BC109B 8-13	BC327 0-20*	ME0411 0 18*	1N4004 0-98 1N4005 0-09	TRANS-		U 4324 20,000 ohms VDC	SN 76033N 2-75*	7470 320
BC109C 0-13	BC328 0-18*	ME0412 0-19*	1N4006 0-10	FORMERS	POLY. R/Lead 100VDC	AC/DC recommended at £14-50 EXCELLENT VALUE	SN 76660 0.90*	7472 30p
BC117 0-18* BC136 0-16*	BC338 0-16* BC310 0-16*	ME0413 0-15* ME0414 0-15*	1N4007 0-11 1N4148 0-05	6-0-6 100mA 1 20	0022 005 068 007		TAA 550 0-60* TBA 120ASO 1-30*	7473 30p 7474 35p
BC142 0-24	BC340 0-15*	ME0461 0 21*	1N4148 0-05 1N5400 0-13	9-0-9 75m A	0033 0.06* 1 0.07*	LED TIL 209/0-125; 0-2; Red 20p 20p	TBA 395 2 25*	7475 49p
BC143 0-24	BC461 0-35	ME0462 .21*	1N5401 0-15	1 - 20	-0047 0.06* 15 0.08* -0068 0.06* 22 0.10*	Green 29p 29p	TBA 480Q 1-25*	7476 32p
8C147A 8-09*	BC557 0-15*	ME4001 8-14*	1N5404 0-21	9-0-9 1 A 3.20 12-0-12 50 m A	01 0 06* 33 0 11*	Clip for above 3p	TBA 5200 1.70* TBA 5300 1.90*	7480 65p 7481 1.00p
BC147B 0-10* BC148 0-09*	BC558 0-15* BC559 0-15*	ME4101 0-11* MJE340 0-76*	2N708 0-20 2N1613 0-30	12-0-12 SUMA	·015 0·07* ·47 0·15*	NATIONAL SCOOP	TBA 540Q 1-99*	7485 1-30p
BC148B . 10*	BCY70 0 15	MJE30551-25*	2N1711 0 30	12-0-12 1A	022 0.07° 1.250V 0.10° 033 0.07° 1.600V 0.15°	SK 1122 TV GAME KIT	TBA 550Q 3-40*	7486 43p
BC149 0-10*	BCY71 0-18	MPF102 0-40*	2N2102 0-50	2:75 min O/P for	-047 0.07* 1.0 400V 0.12*	Colour and Sound Inc. PCB Semi-cons, Pots, Res, Caps,	TBA 560CQ 2:30* TBA 641 2:55*	7490(A) 55p 7492 55p
BC149B 0-11* BC149C 0-11*	BCY72 0-14 BD123 0-90	OA5 0-71 OA10 0-62	2N2219 0-30 2N2222 0-24	OC71/2use75p		XTAL, Data	TBA 750 1.90*	7493 55p
BC153 .18*	BD124 0-90	OA47 0-14	2N2222 0 24 2N2646 0 65	06-06 280mA	OFFER RED LED's 125 10 for £1	£21 00* (less cash discount)	TBA 800Q 1-35*	7496 90p
BC154 0-18*	BD131 0-42	O A81 0-30	2N29200 0-13*	10.0.10.150m.6	RED LED's 125 10 for £1 RED LED's 2 10 for £1	MA 1003 CAR CLOCK	TBA 8105Q 1 49* TBA 820Q 1 29*	74107 40p 74121 31p
BC157 8-12* BC157B 8-14*	BD132 0-42	0A90	2N29266 0-15*	12-0-12 150mÁ 2·40	BC108C 11 for £1 100 for £8	Built complete Incl. Data	TBA 920Q 2-80*	74123 40 p
BC158A . 12*	8D139 0-54* BD140 0-58*	OA91 8-08 OA95 8-08	2N3053 0-25 2N3054 0-58	MOT. 700 OP	2N3702 100 for £9	£17.00	TBA 9900 2-58*	74141 80p
BC159A 8-12*	BD155 0-75*	0A200 0-10	2N3663 0 28	P-1K2 8Ω	2N3704 100 for £9	CAR INTERIOR LIGHT	TCA 270Q 2.20* TDA 2020 4.25*	74145 1-15p 74151 94p
BC172A 8-15*	BDY20 8-80	OA202 0-11	2N3055 0-60	200mW 50p	POTENTIOMETERS	4 to 40 seconds variable.	U 14552 300mW	74174 1-290
BC173B 0-16* BC177 0-17	BF115 0-22 BF158 0-20*	OC35 1-20 OC44 0-45	2N3643 0-17* 2N3646 0-17*	DISPLAYS DL704 0-95	Lin/Log.	Time to find keys and clunk-	Audio with data	74180 1-20p
BC177B 0-18	BF166 0-38	OC45 0 45	2N3702 .11*	DL704 0-95 DL707 0-75	5K, 10K, 25K, 50K, 200K, 250K, 500K, 1M, 2M, 25p* each.	click. Complete, 2 wires to connect (protected). £5-25	0-35* ZN414 1-40*	74190 1-60p 74191 2-10p
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AAY32 AAZ13 AAZ15	0-15 0-25 0-31	BD115 BD121 BD123	1-50 0-60 1-50 1-50	*MPSU56 NKT401 NKT403	0-45 2-00 1-73	1N916 1N4001 1N4002	0-07 0-06 0-07	7405 7406 7407	0 - 20 0 - 55 0 - 55
AAZ17 AC107 AC125	0 · 25 0 · 75 0 · 30	BD124 BD131	1-00	NKT404 NE555 OA5	1-73 0-45 0-75	1N4003 1N4004 1N4005	0-08 0-09 0-13	7408 7409 7410	0 - 28 0 - 28 0 - 20
AC126 AC127 AC128	0-25 0-25 0-25	BD132 *BD135 *BD136	0 - 54 0 - 35 0 - 36	OA7 OA10 OA47	0 - 55 0 - 55 0 - 14	1N4006 1N4007 1N4009	0-15 0-15 0-15	7412 7413 7416	0-26 0-45 0-40
AC141 AC141K AC142	0 · 20 0 · 30 0 · 20	*BD137 *BD138 *BD139	0-37 0-40 0-43	OA70 OA79 OA81	0-30 0-30 0-30	1N4148 1N5400 1N5401	0-07 0-14 0-16	7417 7420 7422	0-40 0-20 0-25
AC142K AC176	0·25 0·25	*BD140 BD144 BD181	0 - 47 2 - 00 1 - 38	OA85 OA90	0-30 0-08	1S44 1S920	0-06 0-08	7423 7425	0-35 0-35
AC187 AC188 ACY17	0-25 0-25 0-65	BD182 BD237	1-48	OA91 OA95 OA200	0 - 08 0 - 08 0 - 10	1\$921 2G301 2G302	0+08 1+00 1+00	7427 7428 7430	0·35 0·50 0·20
ACY18 ACY19 ACY20	0-65 0-65 0-65	BD238 BDX10 BDX32	0-85 0-75 2-25	OA202 OA210 OA211	0-11 0-75 0-75	2G306 2N404 2N696	1 · 10 0 · 60 0 · 25	7432 7433 7437	0-36 0-37 0-42
ACY21 ACY39 AD149	0-65 1-25 0-70	BDY20 BDY60 BF115	1-42 0-75 0-39	OAZ200 OAZ201 OAZ206	0 - 65 0 - 65 0 - 65	2N697 2N698 2N705	0+16 0+30 0+90	7438 7440 7441AN	0 · 37 0 · 22 0 · 92
AD161 AD162	0-75 0-75	BF152 BF153 BF154	0-25 0-25 0-25	OAZ207	0-65	2N706 2N708	0 12 0 21	7442 7447AN	0-78
AF106 AF114 AF115	0-45 0-25 0-25	BF159 BF160 BF167	0-35 0-30	0C16 0C22 0C22 0C23 0C24 0C25 0C26 0C28 0C28 0C28 0C29 0C35 0C41 0C43 0C41 0C43 0C45 0C45 0C71 0C73 0C77 0C77 0C77	2·00 2·50 2·75	2N930 2N1131 2N1132	0 · 26 0 · 26 0 · 26	7450 7451 7453	0 · 20 0 · 20 0 · 20
AF116 AF117 AF139	0-25 0-25 0-40	BF173 BF177	0 - 39 0 - 39 0 - 38	OC24 OC25 OC26	3-50 0-90 0-90	2N1302 2N1303 2N1304	0-37 0-37 0-45	7454 7460 7470	0 · 20 0 · 20 0 · 35
AF186 AF239 AFZ11	1-50 0-45 2-75	BF178 BF179 BF180	0-45 0-48 0-45	OC28 OC29 OC35	2-00 2-00 1-50	2N1305 2N1306 2N1307	0-45 0-50 0-50	7472 7473 7474	0-36 0-36 0-40
AFZ12 ASY26 ASY27	2.75 0.45 0.50	BF181 BF182 BF183	0-45 0-45 0-45	OC36 OC41 OC42	1 · 50 0 · 50 0 · 50	2N1308 2N1309 2N1613	0-60 0-60 0-33	7475 7476 7480	0-59 0-42 0-60
ASZ15 ASZ16 ASZ17	1 25	BF184 BF185 *BF194	0-38 0-37 0-12	0C43 0C44	1 · 50 0 · 50 0 · 50	2N1671 2N1893 2N2147	1-50 0-33 1-40	7482 7483	0-85 1-00
ASZ20 ASZ21	0-75	*BF195 *BF196 *BF197	0 - 11 0 - 13	0C71 0C72	0-45 0-45	2N2148 2N2218	1-65	7484 7486 7490	0-40 0-52
AU113 AUY10 BA145	1-70 1-70 0-15	BF200 *BF224	0 · 14 0 · 32 0 · 20		1-00 0-75 0-60	2N2219 2N2220 2N2221	0 · 42 0 · 35 0 · 22	7491AN 7492 7493	0-85 0-60 0-70
BA148 BA154 BA155	0·15 0·10 0·12	*BF244 BF257 BF258	0-35 0-37 0-42	OC76 OC77 OC81	0-50 1-20 0-75	2N2222 2N2223 2N2368	0-25 2-75 0-17	7494 7495 7496	0-80
BA156 BAW62 BAX13	0-13 0-05 0-07	BF259 *BF336 *BF337	0-45 0-50 0-53	0C/3 0C76 0C77 0C81 CC81Z 0C82 0C83 0C84	1-00 0-75 0-55	2N2369A 2N2484 2N2646	0 · 21 0 · 21 0 · 50	7497 74100 74107	3-67 1-75 0-45
BAX16 BC107 BC108	0.07 0.12 0.12	*BF338 BFS21 BFS28	0 · 55 2 · 27 1 · 38	OC84 OC122 OC123 OC139	0-00 1-50 1-55	2N2904 2N2905 2N2906	0·35 0·35 0·25	74109 74110 74111	0-86 0-57 0-86
BC109 *BC113	0-13 0-15	*BFS61 *BFS98 BFW10	0.25 0.25 0.90	00140	2·25 1·95 2·25	2N2907 *2N2924	0-21 0-15	74116 74118	1-89 0-95
*BC114 *BC115 *BC116	0 - 18 0 - 19 0 - 19	BFW11 BFX84	0-90 0-38	OC171 OC171 OC200 OC201 OC202 OC202 OC203	0.75 0.75	*2N2925 *2N2926 2N3053	0·17 0·13 0·25	74119 74120 74121	2·00 1·10 0·45
*BC117 *BC118 *BC125	0 • 22 0 • 16 0 • 18	BFX85 BFX87 BFX88	0 · 41 0 · 35 0 · 32	OC200 OC201 OC202	1+00 1+50 1+25	2N3054 2N3055 2N3440	0-50 0-65 0-60	74122 74123 74125	0-60 1-00 0-90
*BC126 *BC135 *BC136	0-25 0-15 0-19	BFY50 BFY51 BFY52	0-28 0-26 0-26	OC203 OC204 OC205 OC206	1-25 1-25 1-75	2N3441 2N3442 2N3525	0+80 1+20 0+90	74126 74128 74132	0-80
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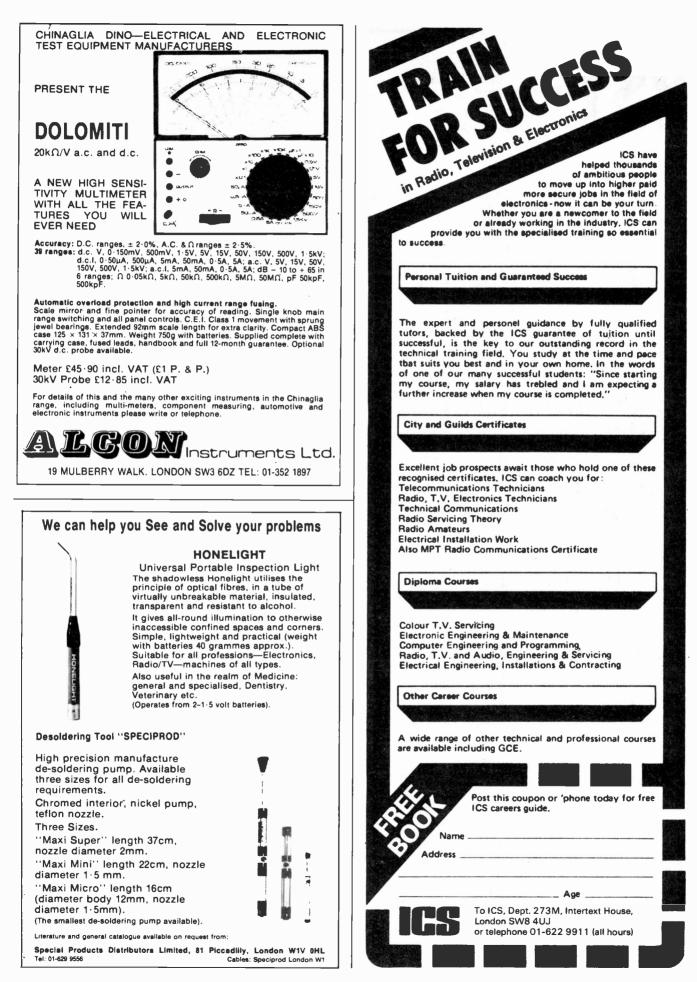
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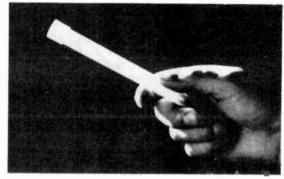
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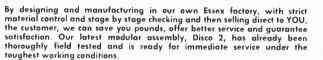
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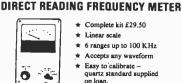
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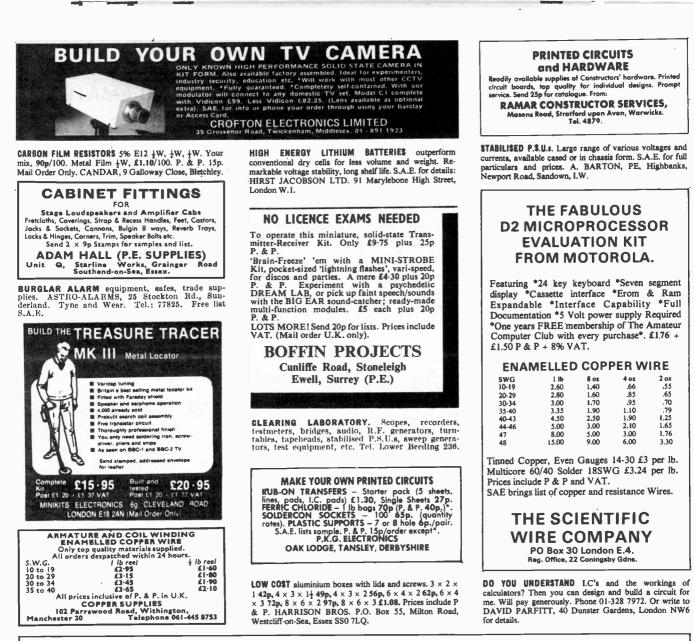
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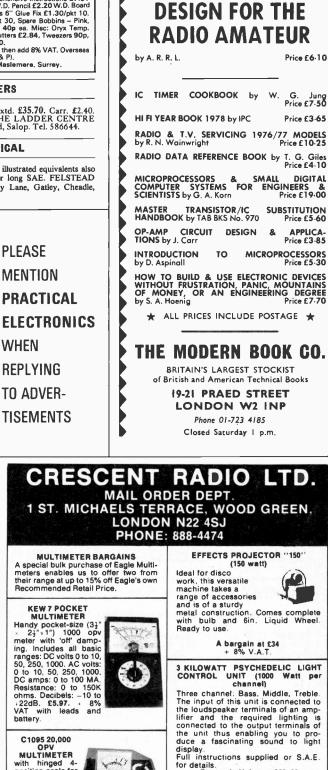
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