PRACTICAL

ELECTRONICS

NOVEMBER 1977

45p

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Special 8 Page Supplement...

Thought-Provoking

GSPECIALS

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DIY SPEAKER KITS

15-WATT KIT IN CHASSIS FORM When you are looking for a good speaker, who

not build your own from this kit. It's the unit which we supply with the enclosures illustrated below Size 13" > 8" (approx.) woofer (EMI), tweeter, and matching crossover components Power handling capacity 15 watts rms. 30 watts peak

£1700 PER STEREO PAIR + P & P £3.40



EASY-TO-BUILD WITH ENCLOSURE

Specially designed by RT-VC for cost-conscious hi-fi enthusiasts, these kits incorporate two teak-

simulate enclosures, two EMI 13" × 8" (approx.) woofers, two tweeters and a pair of matching crossovers. Easily constructed using a few basic tools. Supplied complete with an easy-to-follow circuit diagram, and crossover components. Input 15 watts rms. £2800 30 watts peak, each unit. PER STEREO PAIR Cabinet size 20" × 11" × 9½" (approx.). + p & p £5.50

COMPACT' FOR TOP VALUE

How about this for incredible bookshelf value from RT-VC! A pair of high efficiency units for only £7.50 - just what you need for lowpower amplifiers. These infinite baffle enclosures come to you ready mitred and professionally finished. Each cabinet measures

12" × 9" × 5" (approx.) deep, and is in wood simulate. Complete with two 8" (approx.) speakers for max, power handling of 7 watts



SPEAKERS Two models - Ouo IIb, teak veneer, 12 watts rms, 24 watts peak, $18\frac{1}{2}$ " × $13\frac{1}{2}$ " × $7\frac{1}{4}$

(approx.) £34 PER PAIR + p & p £6.50 Duo III. 20 watts rms. 40 watts peak, 27" × 13" × 11½" (approx.)

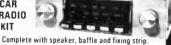




ready assembled stereo amp, module, Garrard auto/manual deck with cueing device, pre-cut and finished cabinet work. Output 4 watts per channel, phones socket and record / replay socket

£2695 p & p £4.05





The Tourist IV for the experienced constructor only. The Tourist IV has five push buttons, tour medium band and one for long wave band. The tuning scale is illuminated and attractive small aluminium control knobs are used for manual tuning and volume control. The modern style fascia has been designed to blend with most car interiors and the finished radio will slot into a standard car radio aperture. Size approx. $7" \times 2" \times 4\frac{1}{4}"$. 12 voits pos or neg earth (altered internally) p & p £1.50 £1250 Output 4 watts into 4 ohms.

FREE TO PERSONAL SHOPPERS BUYING CAR RAOIO KIT ELECTROMATE Rear window heater modern line element all wiring and switch worth £ 300



TO PERSONAL

SHOPPERS See Relow

+ £1.00 p & p

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£29

+ p & p

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20 x 20 WATT STEREO AMPLIFIER

unit in teak-finished cabinet. Silver fascia with aliminium rotary controls and pushbuttons, red mains indicator and stereo jack socket. £290

Function switch for mic. magnetic and crystal pick-ups, tape, tuner, and auxiliary Rear panel features two mains outlets. OIN speaker and input p 8 p £2.50 sockets, plus fuse. 20 + 20 watts rms, 40 + 40 watts peak

•FREE To cash or cheque personal shoppers

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SPECIAL

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Viscount Amplifier,
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On complete stereo systems using starred Products

ADD-ON STEREO CASSETTE TAPE DECK KIT Designed for the experienced O.I.Y. man. This kit comprises of

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Optional extras:

Pair of Oynamic microphones £3.95 + £1.00 p & p Mains transformer £2.50 + £1.00 p & p

STEREO CASSETTE record/replay fully built

personal Shoppers Only!

BSR MP60 TYPE

P.C. board incorporating 4 l.C.s. GRUNDIG 53 " tape 1800 ft. £120 each. 5 for £500 PAIR STEREO 8 WATT SPEAKERS 8" bass units with 3½" approx. tweeters power handling 8 watts imp8ohms. Size 16½"×11"×8½" approx. £1295 O WAITS IMPOUNDS. SIZE TO Y X 11 X 0 2 APPLOX.

PLINTH & COVER BSR OR GARRARD TEAK FINISH

GOODMAN 5" approx. 7 watt bass speaker

AM, FM. TUNER P.C.B. with Mullard L.P. 1186, 1185, 1181 module £495 70 £ 0 50 100K Multiturn Varicap tuning pots 8 for HEAVY DUTY FIBRE GLASS COPPER CLAD BOARD C190 255 x 17" x ½" Apprax, per sheet only DECCA 0C1000 Stereo Cassette Record deck P.C.B. complete with £295 £1.00 Switch oscillator coils and tape-heads and circuit diagrams.

AM. FM. STEREO MULTIPLEX CAR RADIO/cassette player in £3600

dash fixing Negative earth 5 watts output I.C. Stereo 8 Track to Cassette adaptor converts, any 8 track BSR TURNTABLES BSR automatic record player deck (Chassis form) with cueing device and Single play record player

stereo (Chassis form) £15.95 £9.95 less cartridge. P & P £2.55 head. ceramic P & P £2.55 Cartridges to suit above

ACOS MAGNETIC £4.95 STEREO CERAMIC STERED £1.95

TURNTABLE illus. diamond stylus, and de luxe plinth and Popular BSR MP.60 type, complete with cover magnetic cartridge. Ready wired

30 x 30 WATT AMPLIFIER KIT Specially designed by RT-VC for the experienced constructor, this kit comes complete in every detail. Same

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with built-in pre-amplifiers

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45 WATT MONO DISCO AMP £3500

p & p £2:50 Size approx

133 "× 51 "× 63 " Here's the mono unit you need to start off with

Gives you a good solid 45 watts rms. 90 watts neak output. Big features include two disc inputs, both for ceramic cartridges, tape input and microphone input. Level mixing controls fitted with integral push-pull switches. Independent bass and treble ontrols and master volume

70 & 100 WATTMONO DISCO AMP Size approx.

14" × 4" × 10¼". Sloping facia, you can use the controls without fuss or bother. Brushed alumimium fascia and rotary controls. Five smooth acting, vertically mounted slide controls - master volume, tape level, mic level, deck level, PLUS INTER-DECK FADER for perfect graduated change from record upon 150.
No. 2, or vice versa. Pre-fade level control (PFL) perfect graduated change from record deck No. 1 to lets YOU hear next disc before fading 70 watt *57 it in. VU meter monitors output level. 100 watt *65 Output 100 watts RMS 200 watts peak. p & pf4.00



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PYE STEREO GRAM CHASSIS

(Complete with circuit-diagrams)



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BSR auto record player deck

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ELECTRONICS

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Our December issue will be on sale on Friday, 11 November, 1977 (for contents, see page 171)

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A roundup of some neoteric i.c. packages

(between pages 184 and 185) 1-8



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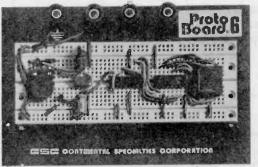
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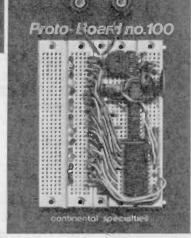
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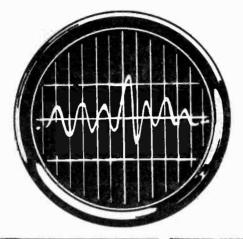
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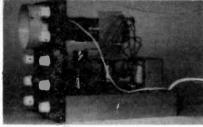
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AC107	0.75	BD124	1.00	NE555	0 - 45	1N4004	0.09	7409	0 - 28
AC125	0 - 30	BD131	0.51	OA5	0.75	1N4005	0 · 13	7410	0.20
AC126	0 · 25	BD132	0 - 54	OA7	0.55	1N4006	0 - 15	7412	0 - 26
AC127	0 · 25	*BD135	0 - 35	OA10	0.55	1N4007	0 - 15	7413	0 - 45
AC128	0 - 25	*BD136 *BD137	0 · 36 0 · 37	OA47	0.14	1N4009	0 - 15	7416	0 - 40
AC141	0.20	*BD13/	0 - 40	OA70	0.30	1N4148	0.07	7417	8 - 40
AC141K AC142	0 · 30 0 · 20	*BD138 *BD139	0.43	OA79	0 - 30	1N5400	0 - 14	7420	0 - 20
AC142K	0.25	*BD140	0 - 47	OA81 OA85	0 · 30 0 · 30	1N5401	0 - 16	7422	0 - 25
AC176	0 · 25	BD144	2.00	OA90	0.08	1S44 1S920	0.06	7423	0 - 35
AC187	0.25	BD181	1-38	OA91	0.08	15920	0 · 08	7425	0 · 35
AC188	0 - 25	BD182	1 - 48	OA95	8-08	2G301	1.00	7427	0.35
ACY17	0.85	BD237 BD238	0 - 80	OA200	0.10	2G302	1.00	7428 7430	0 · 50 0 · 20
ACY18	0.65	BD238	0.85	OA202	0.11	2G306	1 - 10	7432	0.36
ACY19	0.65	BDX10 BDX32 BDY20 BDY60	0.75	OA210	0.75	2N404	0.60	7433	0.37
ACY20	0 - 65	BDX32	2 · 25	OA211 OAZ200	0.75	2N696	0 - 25	7437	0.42
ACY21 ACY39	0 - 65	BDY20	1 - 42	OAZ200	0.65	2N697	0 - 16	7438	0.37
ACY39	1.00	BDY60	0.75	OAZ201	0 - 65	2N698	0 - 30	7440	0 - 22
AD149	0.70	BF115	0 - 39	OAZ206	0.65	2N705	0 - 80	7441AN	0.92
AD161	0 - 75	BF115 BF152 BF153	0·25 0·25	OAZ207	0.65	2N706	0 - 12	7442	0.78
AD162 AF106	0 · 75 0 · 45	DF153	0 · 25	OC16	1 - 25	2N708	0.21	7447AN	1 - 20
AF114	0.45	BF154 BF159	0.25	0020	2.00	2N930	0.26	7450	0 - 20
AF115	0.25	RE190	0.30	0022	2·50 2·75	2N1131	0 · 26 0 · 26	7451	0 · 20
AF116	0.25	BF167 BF173 BF177	0 - 39	0023	3 - 50	2N1132 2N1302		7453	0 · 20
AE117	0 - 25	BF173	0.39	0025	0.90	2N1302 2N1303	0·37 0·37	7454	0 · 20
AF139	0 - 40	BF177	0 - 38	OC26	0.90	2N1304	0 - 45	7460 7470	0·20 0·35
AF139 AF186	1 - 50	BF178 BF179 BF180	0 - 45	OAZ207 OC16 OC20 OC22 OC23 OC24 OC25 OC26 OC26 OC28 OC29 OC35 OC36	2.00	2N1305	0 - 45	7472	
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ASY27	0.50	BF183	0 - 45	OC41 OC42 OC43	0.50	2N1613 2N1671	0.33	7480	0-60
ASZ15 ASZ16	1·25 1·25	BF184 BF185	0 - 37	OC43	1.50	2N1671	1.50	7482	0.85
ASZ17	1.25	I *RF194	0.12	0044	0 - 50	2141893	0 - 33	7483	1.00
ASZ20	0.75	*BF195 *BF196 *BF197	0.11	0045	0.45	2N2147	1 - 40	7484	1.00
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BC108 BC109	0·12 0·13	*BFS61	0 - 25	OC139	2 - 25	2N2907	0·25 0·21	74111	0.86
*BC113	0-15	*BFS98	0 - 25	OC140	1-95	*2N2924	0 - 15	74116 74118	1 · 89 0 · 95
*BC114	0 - 18	BFW10	0.90	OC141	2 - 25	*2N2925	0 - 17	74119	2.00
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*BC117 *BC118	0 - 22	BFX85	0-41	OC200	1.00	2N3054	0.50	74122	0.60
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*BC126 *BC135 *BC138	0·25 0·15	BFY51	0.26	OC141 OC170 OC171 OC200 OC201 OC202 OC203 OC204 OC205 OC206 OC207 OC207 OCP71 OCP71	1 - 25	2N3441	0.80	74126	0-80
*BC138	0.19	RFY52	0.26	00204	1 . 25	2N3442	1.20	74128	0 - 80
*BC137	0 - 16	RFY64	0.30	00203	1 · 75 1 · 75	2N3525	0.90	74132	0 - 80
*BC147	0.10	BFY90	1.32	OC207	1.25	2N3614 *2N3702	1·20 0·15	74136	0.68
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*BC167	0 · 13	*BU205 *BU206	2 · 25	T1C44 T1C226D	0.36	*2N3708	0-14	74148	2.00
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13	100	9-0-9	2.14	0.38
235	330, 330	0-9, 0-9	1 - 99	0.38
207	500, 500	0-8-9-, 0-8-9	2 - 50	0.71
208	1A, 1A	0-8-9, 0-8-9	3 - 53	0 - 78
236	200, 200	0-15, 0-15	1 . 90	0.38
214	300, 300	0-20, 0-20	2 . 56	0 . 78
221	700 (DC)	20-12-0-12-20	3 - 41	0.78
206	1A, 1A	0-15-20-0-15-20	4-63	0.96
203	500, 500	0-15-27-0-15-27	3 - 99	0.96
204	1A. 1A	0-15-27-0-15-27	5 . 39	0.96
S112	500	12-15-20-24-30	2.64	0.78

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Vol. Treb. Mid. and Bass controls. HI. IMP. FET, I/P suitable Mid. Guitar, Radio Crystal/Ceramic P.U. Sensitivity 4mV. Treble+ 35dB at 16kHz. Mid + 20 –15dB at 1kHz. Bass + 20 – 10dB at 40Hz.

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Vacuum varnish impregnated. Transformers with supply board incorporating pre-amp supply:

PS250 for supplying 2 TP125s PS200 for supplying 2 TP100s PS60/60 for supplying 2 TL60s PS125±45 volts for TP125 PS100±43 volts for TL100 PS60±38 volts for TL60 PS30±25 volts for TL30 PSU 2 for supplying disco mixer	£28.50 £28.50 £25.00 £17.75 £16.25 £15.25 £11.75
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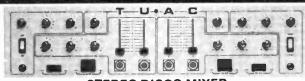
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4 CHANNEL SOUND **TO LIGHT** SEQUENCE CHASER

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STEREO DISCO MIXER

With touch sensitive switching and auto fade

INPUTS: Four identical stereo inputs available with any equalisation. Two magnetic and two flat supplied as standard. High quality sider control on each channel. Volume, treble and bass controls for each pair of sliders. Sensitivity mag., 3mV (R.I.A.A. comp.). Flat 50mV at 1kHz. Bass controls ± 18dB at 60Hz. Treble controls ±18dB at 150Hz.

15kHz.

OUTPUT: Up to 3 volts (+ 12dB) available. Attenuated output for TUAC Power Modules. Rotary master and balance controls. Band width 15Hz - 25kHz ± dB. P.F.L. Output 250mV into 8 ohms. Rotary volume control. Monitoring facility for all 4 channels. Selection via touch sensitive illuminated switches. Switched visual cue indicator. Miscellaneous Facilities: Two illuminated deck on/off switches. Mains illuminated on/off switches. Auto fade illuminated on/off switches. Mains illuminated on/off switches. Mains illuminated on/off switches. Auto fade illuminated on/off switch. Mains powered with integral screen and back cover. Complete with full instructions Size: 25in long × 6in high × 3in deep

Mono Disco Mixer with autofade £45.00

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- Full wave control RCA 8A Triacs 1000W per channel
- Fully supressed and fused
 Switched master control for sound operation from 1/2W to 125W

 Fully supressed and fused • Speed control for fixed rate sequence from 8 per
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 Full logic integrated circuitry with optical isolation
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- £20.75

Model 501 500W per channel as above without sound triggering £12.25

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(complete with switches, neons and knobs) as illustrated





For S1LMB **£6.50** Size 8" x 41/2"

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Red, Green, Blue,

Amber. £23.50



Size 61/4" x 41/4

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NEEDS NO CROSS-OVER NETWORK
FREQUENCY RESPONSE 4,000 - 30,000 Hz ± 3dB
PATENTED MOMENTUM DRIVE PRINCIPLE • NO
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IN SERIES TO FORM AN ARRAY - INCREASED
OUTPUT • POWER HANDLING CAPACITY 25 voits
BMS - see chaft

POWER HAND	LING GUIDE
System Impedance	Capacity
2 ohms	312 watts
4 ohms	156 watts
8 ohms	78 watts
16 ohms	39 watts



3 1/8 × 3 1/8 × 27/8 ins

STOCKISTS - CALLERS ONLY

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RCA 8A Triacs 1000W per channel

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Master control to operate from 1W to 125W
 Full wave control

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Single Channel Version 1500 Watts

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- Speed Control 3 per min. to 10 per sec.
- Full logic integrated circuitry Dimmer control to each channel

3SDMI

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COMPONENTS SETS include all necessary resistors, capacitors, semiconductors, potentio-meters and transformers. Hardware such as cases, sockets, knobs, etc. are not included but most of these may be bought separately. Fuller details of kits, PCBs and parts are shown in our

CIRCUIT AND LAYOUT DIAGRAMS are supplied free with all PCBs designed by Phonosonics.

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with keyboard circuits. Although having slightly fewer
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Consists of 2 log VCOs. VCF. 2 envelope shapers, 2 voltage
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Set of basic component kils
Set of printed circuit boards

from £64-25
Set of printed circuit boards

P.E. SYNTHESISER (P.E. Feb. 73 to Feb. 74)
The well acclaimed and highly versatile large-scale mains-operated Sound Synthesiser complete with keyboard circuits. Other circuits in our lists may be used with the Synthesiser to good advantage, notably P.E. Minisonic, Phasing Unit, Wind and Rain, Rhythm Generator, Sound Bender, Voltage Controlled Filter, Guitar Effects Pedal and Overdrive, Fuzz, Tremolo and Wah-Wah units.

The Main Synthesiser: PSU. 2 linear VCCs, 2 ramp generators, 2 input amps, sample hold, noise generator, reverb amp, ring modulator, peak level circuit, envelope shaper, voltage controlled amp. Full details in lists.

Set of basic component kits
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The Synthesiser to make an independent musical instrument): 2 logarithmic VCOs, divider, 2 hold circuits, 2 modulation amps, mixer, 2 envelope shapers and additional PSU. Full details in our lists.

Set of basic component kits
Set of printed circuit boards

E48-18
Set of printed circuit boards

GUITAR EFFECTS PEDAL (P.E. July 75)

Modulates the attack, decay and filter characteristics of an audio signal not only from a guitar but from any audio source, producing 8 different switchable effects that can be further modified by manual controls. Possibly the most interesting of all the low-priced sound effects units in our range. Circuit does not duplicate effects from the Guitar Overdrive Unit.

Component set with special foot operated switches
Alternative component set with panel mounting switches

switches Printed circuit board

SOUND BENDER (P.E. May 74)

A multi-purpose sound controller, the functions of kinclude envelope shaper, tremolo, voice-operated fader, automatic fader and frequency-doubler.

Component set for above functions (excl. SWs)

Printed circuit board

Optional extra—additional Audio Modulator, the use of which, in conjunction with the above component set, can produce "jungle-drum" rhythms.

Component set (incl. PCB)

PHASING UNIT (P.E. Sept. 73)
A simple but effective manually controlled unit for introducing the "phasing" sound into live or recorded music. Component set (incl. PCB)

PHASING CONTROL UNIT (P.E. Oct. 74)
For use with the above Phasing Unit to automatically control the rate of phasing.
Component set (incl. PCB)

£4-48

SOPHISTICATED PHASING AND VIBRATO UNIT
A slightly modified version of the circuit published in Elektor. December 1976, and includes manual and automatic control over the rate of phasing and vibrato. Printed circuit board

WAH-WAH UNIT (P.E. Apr. 76)
The Wah-Wah effect produced by this unit can be controlled manually or by the integral automatic controller.
Component set (incl. PCB)

\$3.55

AUTOWAH UNIT (P.E. Mar. 77)

Automatically produces Wah-pedal and Swell-pedal sounds each time a new note is played.
Component set, PCB, special foot switches £7-27
Component set and PCB, with panel switches £4-83

P.E. JOANNA (P.E. May/Sept. 75)

P.E. JUANNA (F.E. May/Sept. /5)
A five-octave electronic piano that has switchable alternative voicing of Honky-Tonk piano, ordinary piano, harpsichord, or a mixture of any of the three, together with facilities including fast and slow tremolo, loud and soft pedal switching, and sustain pedal switching. The power amplifier typically delivers 24 watts into 8 ohms. The PCBs have been redesigned by ourselves making improved use of the space available.

available.

Main power supply, tone generator, 61 envelope shapers, voicing and pre-amp circuits.

Set of basic component kits for above £75-29

Set of printed circuit boards for above £20-35

Power amplifier £15-97 Printed circuit board for power amp

ELECTRONIC ORGAN

5-octave electronic organ with 5 basic voices that can be used individually or together, 5 pitches (2ft, 4ft, 5ft, 16ft, 32ft), variable attack, tremolo, vibrato, phasing, and variable sustain. Details in our list.

ORGAN CONVERSION KIT
Converts the P.E. Joanna electronic piano to also provide most of the facilities offered by the above electronic organ.
Basic component set and PCB £12-34

SYNTHESISER TUNING INDICATOR (P.E. July 77)
A simple 4-octave frequency comparator for use with synthesisers and other instruments where the full versatility of the P.E. Tuning Fork is not required.

Component and PCB (but excl sw.)

GUITAR FREQUENCY DOUBLER (P.E. Aug. 77)
A modified and extended version of the circuit published.
Details in list.

SEE OTHER PAGE FOR KEYBOARDS, AND OUR LISTS FOR OTHER COMPONENTS AND ACCESSORIES STOCKED

A manually controlled unit for producing the above-named

Component set (incl. PCB)

GUITAR OVERDRIVE UNIT (P.E. Aug. 76)
Sophisticated, versatile Fuzz unit, including variable and switchable controls affecting the fuzz quality whilst retaining the attack and decay, and also providing filtering. Does not duplicate the effects from the Guitar Effects Pedal and can be used with it and with other electronic instruments.
Component set using dual slider pot
Component set using dual rotary pot
Printed circuit board

E1-62

mple Fuzz unit based upon P.E. "Sound Design" circuit Component set (incl. PCB) \$2.0

TREMOLO UNIT
Based upon P.E. "Sound Design" circuit.
Component set (incl. PCB)

TREBLE BOOST UNIT (P.E. Apr. 76)
Gives a much shriller quality to audio signals fed through it.
The depth of boost is manually adjustable.
Component set (incl. PCB)

£2.40

P.E. TUNING FORK (P.E. Nov. 75)

Produces 84 switch-selected frequency-accurate tones. A LED monitor clearly displays all beat note adjustments, Ideal for tuning acoustic and electronic musical instruments

Main component set (incl. PCB)
Power supply set (incl. PCB)

P.E. SYNCHRONOME (P.E. Mar. 76)
An accented-beat electronic metronome, providing duple, triple and quadruple times with full control over the beat rate. Can also be used as a simple drum-beat rhythm generator. Includes power supply.

Component set (incl. loudspeaker) £11-62

rinted circuit board

TAPE NOISE LIMITER

Very effective circuit for reducing the hiss found in most tape recordings. All kits include PCBs

Standard tolerance set of components
Superior tolerance set of components
Regulated power supply (will drive 2 sets)

£4-68

ENVELOPE SHAPER WITHOUT VCA (P.E. Oct. 75)
Provides full manual control over attack, decay, sustain and release functions, and is for use with an existing voltage controlled amplifier.

Component set (incl. PCB)

£4-66

ENVELOPE SHAPER WITH VCA (P.E. Apr. 76)
This unit has its own voltage controlled amplifier and has full manual control over attack, decay, sustain and release functions,

Component set (incl. PCB)

TRANSIENT GENERATOR (P.E. Apr. 77)
An envelope shaper, without VCA, having the usual attack, decay, sustain and release functions, and in addition it also provides a "Repeat Effect" enabling a synthesiser to be programmed to imitate such instruments as a mandolin or hand.

Component set

WAVEFORM CONVERTER

WAVEFURM CUNVERTER
Slightly modified from a circuit published in a German
edition of "Elektor". Converts a saw-tooth waveform into
four different waveforms: sine-wave, mark-space saw-tooth,
regular triangle form, and squarewave with an externally
variable mark-space ratio.

Component set (incl. PCB but excl. sw's)

£8:19

VOLTAGE CONTROLLED FILTER (P.E. Dec. 74)
Part of the P.E. Minisonic now released as an independent kit for use with other synthesisers.
Component set (incl. PCB) (Order as Kit 65-1)

\$8:22

RING MODULATOR (P.E. Jan. 75)

art of the P.E. Minisonic now released as an independent it for use with other synthesisers. Component set (incl. PCB) (Order as Kit 59-1)

NOISE GENERATOR (P.E. Jan. 75)
Part of the P.E. Minisonic now released as an independent kit for use with other synthesisers.
Component set (incl. PCB.) (Order as Kit 60-1)

£3-35

SOPHISTICATED POWER SUPPLIES

A wide range of highly stabilised low noise power supply kits is available—details in our lists.

MICROPHONE PRE-AMP (P.E. Apr. 77) Component set (incl. PCB)

VOICE OPERATED FADER (P.E. Dec. 73)

For automatically reducing music vo "talk-over"—particularly useful for Disco home-movie shows. volume Component set (incl. PCB)

DYNAMIC RANGE LIMITER (P.E. Apr. 77)

Automatically controls sound output to within a preset

Component set (incl. PCB)

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PHONOSONICS - DEPT. PE5N - 22 HIGH STREET - SIDCUP - KENT DA14 6EH

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AND OTHER PROJECTS

PHOTOGRAPHS in this advertisement show two of our units containing some of the P.E. projects built from our kits and PCBs. The cases were built by ourselves and are not for sale, though a small selection of other cases is available.

LIST—Send stamped addressed envelope with all U.K. requests for free list giving fuller details.of PCBs, kits and

OVERSEAS enquiries for list: Europe send 20p: other countries—send 40p



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ORP12

ORP12 ZTX107 ZTX108 ZTX501 ZTX503 ZTX531

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2N3704

2N3819

2N3820 2N3820 2N3823E 2N4060 2N5245 2N5459 2N5777

INTEGRATED

KEYBOARDS AND CONTACTS

KEYBOARDS AND CONTACTS
KImber-Allen Keyboards as required for many published circuits, including the P.E. Joanna, P.E.
Minlsonic, and P.E. Synthesiser. The manufacturers claim that these are the finest moulded
plastic keyboards available. All octaves are C to C. The keys are plastic, spring-loaded and
mounted on a robust aluminium frame.
3 Octave (37 notes) £25-50. 4 Oct (49 notes) £32-25. 5 Oct (61 notes) £39-75.
Contact Assemblies for use with above keyboards. Single-pole change-over (type SP) as for P.E.
Joanna and P.E. Minisonic. Two-pole normally-open make-break (type DP) as for P.E.
Synthesiser. Special contact assembly (type 4PS) having 4 poles, 3 of which are normally-open
make-break contacts and the fourth is a change-over contact—this special assembly enables THE
SAME KEYBOARD to be used with the P.E. Synthesiser. P.E. MinIsonic and the P.E. Joanna
simultaneously thus avoiding the cost of more than one keyboard. See our list for other
contacts.

Contact	Each	3 Octave Set	4 Octave Set	5 Octave Set
SP	24p		£11.76	£14-64
2P	27p	£ 9·99	£13 · 23	£16 · 47
4PS		£19·61	£25 · 97	£32 · 33

PRINTED CIRCUIT BOARDS for use with the above contacts and thus eliminating most of the inter-wiring required, are available. Details in our lists.

MORE NEW KITS!	

NEW RHYTHM GENERATOR

Redesigned, improved and extended version of the PE 1974 design and including new automatic rhythm programme selector.

TUNE-PROGRAMMABLE SEQUENCER

(PE Nov. 77) The new music unit currently being published.

FORMANT SYNTHESISER (Elektor Magazine 1977). Very sophiaticated music synthesiser for the advanced constructor and for whom cost is secondary to performance.

GUITAR SUSTAIN UNIT

(PE Oct. 77). Details in lists. Please send S.A.E.

SOUND-TO-LIGHT (P.E. Aurora) (P.E. Apr.-Aug. 71)
Four channels each responding to a different sound frequency and controlling its own light. Can be used with most audio systems and lamp intensities.

Basic component set (excl. thyristors)
Printed circuit board for above
Power supply
PCB for power supply
9 155-78

3-CHANNEL SOUND-TO-LIGHT (P.E. Apr. 76)
A simple but effective sound-to-light controller capable of operating 3 lamps each of approximately 700 watts. Includes

power supply, thyristors, and by-pass switches. Component set (incl. PCB)

DISCOSTROBE (P.E. Nov. 76)

4-channel light-show controller giving a choisequential, random, or full strobe mode of operation

Basic component set a choice of

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BIOLOGICAL AMPLIFIER (P.E. Jan./Feb. 73) Multi-function circuits that, with the use of other external equipment, can serve as lie-detector, alphaphone, cardiophone etc.

quipment, can serve as lie-detector, alpha ardiophone etc.

Pre-Amp Module Component set (incl. PCB)

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SEMI CONDUCTOR TESTER (P.E. Oct. 73) for the enterprising home

Semi CONDUCTOR TESTER (F.E. Oct. 75)
Essential test equipment for the enterprising constructor. While stocks last.
Set of resistors, capacitors, semiconductors, potentiometers, makaswitches and PCB Panel meter (500μA)

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445 123p
446 123p
447 102p
134 18p
137 38p
77 33p
78 40p
10 48p
10 99p
10 97p
10 83p 70p 83p 130p 36p 125p 55p 103p 340p 83p 135p 115p 115p 137p 137p 131p 131p 131p 131p 1305a CD4000 CO4001 CD4002 CD4006 CD4008 CD4008 CD4010 CD4011 CD4012 CD4013 CD4015 CD4016 CD4016 CD4016 CD4016 CD4016 CD4016 CD4016 CD4017 CD4018 CD 25p 25p 28p 38p 42p 10 amp 10 amp 10 amp 8R! 1 amp 1 amp 1 amp 2 amp 2 amp 2 amp 2 amp 2 amp C.e BY127 OA47 OA70 OA70 OA81 OA85 OA91 OA95 OA200 OA200 OA202 OA201 O MC1496 NE555 NE556 33p 78p 385p 385p 138p 126p 175p NE581 NE582 NE585 NE586 NE587 SN78003 185p SN76013 185p SN76023 160p SN76033 100 200 400 100 200 400 100 200 400 400 400 400 26p 42p 71p 50p 66p 61p 64p 100p 113p 130p 420p 430p SN76033 258p TAA6621 257p TAA661 175p TBA540 236p TBA641 281p TBA800 102p TBA810 113p TBA820 90p µA723 57p 6 6 10 10 10 10 15 30 10p 11p 16p 16p 18p 20p 25p 50 P.I.V. 100 P.I.V. 200 P.I.V. 400 P.I.V. 600 P.I.V. BC148 BC149 BC157 BC158 BC159 BC169 BC171 BC173 BC173 BC178 BC178 BC182 BC182 BC182 BC212 BC214 BC213 BC214 BC213 BC328 BC328 BC328 BC328 14p 14p 27p 14p 74p 17p 20p 17p 59p 47p 43p 50p 51p 51p 51p 37p 37p 37p 37p 13p 13p 13p 16p 38p 16p 37p 44p 30p 34p 31p 31p 31p 17p 17p 17p AC126 AC127 AC128 AC176 AC188 AC176 AC188 AD161 AC182 AF116 AF115 AF116 AF115 AF124 AF124 AF125 AF129 AF139 AF239 BC107 BC108 BC107 18p 10p 11p 11p 12p 12p 12p 12p 12p 13p 13p 13p 13p 14p 14p 14p 14p 15p 21p 21p 23p 23p 65p 50p 30p 27p 23p 23p 42p 42p 42p 42p 42p 53p 90 90 90 BC548 Bc549 BC547 BCY70 BCY70 BCY72 BD115 BO131 BO132 BD138 BD138 BD138 BD139 BD139 BD139 BF173 BF173 BF180 BF181 BF182 TRANSFO LT44 LT700 6-0-6 9-0-9 12-0-12 0-6-0-8 0-12-0-12 6-3V-1-5a SPST DPST DPDT SPST SPDT DPDT SPST SPDT OPDT SPST SPDT OPDT 27p 29p 35p 66p 70p 75p 54p 54p 90p 48p 52p 60p STD Potentiometers

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connector is supplied with each pre-amplifier. FEATURES: complete pre-amplifier in single pack; multi-function equalisation; low noise; low distortion; high overload; two simply combined for stereo.

APPLICATIONS: hi-fi; mixers; disco; guitar and organ; public address.

SPECIFICATION: Inputs-magnetic pick-up 3mV; ceramic pick-up 30mV; tuner 100mV; microphone 10mV; auxiliary 3-100mV; input impedance 47kΩ at 1kHz. Outputs—tape 100mV; main output 500mV R.M.S. Active Tone Controls—treble ±12dB at 10kHz; bass ±12dB at 100Hz. Distortion—0:1% at 1kHz; signal/noise ratio 8ddB. Overload—38dB on magnetic pick-up. Supply Voltage—±18-50V.

Price £5.22 + 65p VAT. P. & P. free

HY5 mounting board B.1. 48p + 6p VAT. P. & P. free

HY30 15W into 8Ω The HY30 is an exciting New kit from I.L.P. It features a virtually indestructible I.C. with short circuit and thermal protection. The kit consists of: I.C., heatsink, P.C. board, 4 resistors, 6 capacitors, mounting kit, together with easy to follow construction and operating instructions. This amplifier is ideally suited to the beginner in audio who wishes to use the most up to date technology available. FEATURES: complete kit; low distortion; short, open and thermal protection; easy to build.

APPLICATIONS: updating audio equipment; guitar practice amplifier; test amplifier; audio oscillator.

SPECIFICATION: Output Power—15W R.M.S. Into 8Ω. Distortion—0·1% at 15W. Input Sensitivity—500mV. Frequency Response—10Hz-16kHz -3dB.

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HY50 25W into 8Ω The HY50 leads I.L.P.'s total integration approach to power amplifier design. The amplifier features an integral heatsink together with the simplicity of no external components. During the past three years the amplifier has been refined to the extent that it must be one of the most reliable and robust High Fidelity modules in the World. FEATURES: low distortion; integral heatsink; only five connections; 7 amp output transistors; no

external components. Integral heatsink, only five confections, γ and object the external components.

APPLICATIONS: medium power hi-fi systems; low power disco; guitar amplifier.

SPECIFICATION: Input Sensitivity—500mV. Output Power—25W R.M.S. into 8Ω. Load Impedance—4-16Ω. Distortion—0-04% at 25W at 1kHz. Signal/Noise Ratio—75dB. Frequency Response—10Hz-45kHz – 3dB. Supply Voltage—±25V. Size—105 × 50 × 25mm.

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HY120 60W into 8Ω

The HY120 is the baby of I.L.P.'s new high power range, designed to meet the most exacting requirements including load line and thermal protection this amplifier sets a new standard in modular design.

TEATURES: very low distortion; integral heatsink; load line protection; thermal protection; five connections; no external components.

APPLICATIONS: hi-fl; high quality disco; public address; monitor amplifier; guitar and organ.

SPECIFICATION: Input Sensitivity—500mV. Output Power—60W R.M.S. into 8Ω. Load Impedance—4-16Ω. Distortion—0-04% at 60W at 1kHz. Signal/Noise Ratio—90dB. Frequency Response—10Hz-45kHz -3dB. Supply Voltage—±35V. Size—114 × 50 × 85mm.

Price £15-84 + £1-27 VAT. P. & P. free

HY200

120W into 8Ω

The HY200 (now improved to give an output of 120 watts) has been designed to stand the most rugged conditions such as disco or group while still retaining true hi-fi performance.

FEATURES: thermal shutdown; very low distortion; load line protection; integral heatsink; no external components.

components.
APPLICATIONS: hi-fi; disco; monitor: power slave; industrial; public address.
SPECIFICATION: Input Sensitivity—500mV. Output Power—120W R.M.S. into 8Ω. Load Impedance—4-16Ω. Disortion—0-05% at 100W at 1kHz. Signal/Noise Ratio—96dB. Frequency Response—10Hz-45kHz-3dB. Supply Voltage—±45V. Size—114 × 50 × 85mm.

Price £23.32 + £1.87 VAT. P. & P. free

HY400 240W into 4Ω The HY400 is I.L.P.'s "Big Daddy" of the range producing 240W into $4\Omega!$ It has been designed for high power disco or public address applications. If the amplifier is to be used at continuous high power levels a cooling fan is recommended. The amplifier includes all the qualities of the rest of the family to lead the market as a true high power hi-fidelity power module.

FEATURES: thermal shutdown; very low distortion; load line protection; no external components

APPLICATIONS: public address; disco; power slave; industrial.

SPECIFICATION: Output Power—240W R.M.S. into 4Ω. Load Impedance—4-16Ω. Distortion—0-1% at 240W at INHZ. Signal/Noise Ratio—94dB. Frequency Response—10Hz-45kHz —3dB. Supply Voltage—±45V. Input Sensitivity—500mV. Size—114 × 100 × 85mm.

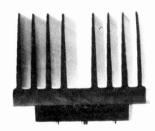
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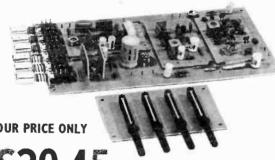
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25 Watts (RMS)

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SPM80 is especially designed to power 2 of the AL60 Amplifiers, up to 15 watts (r.m.s.) per channel simultaneously. With the addition of the Mains Transformer BMT80, the unit will provide outputs of up to 1.5A at 35V. Size: 63mm, 105mm, 30mm. Incorporating short circuit protection

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517 75 p.6.0

MK69 AUDIO KIT:
Comprising: 2 x AL60's, 1 x SPM80, 1 x BTM80, 1 x PA100, 1 front panel and knobs, 1 for parts to include or/off switch, neon indicator, stereo headphone sockets plus TEAK 80 AUDIO KIT:
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7 + 7 WATTS R.M.S.

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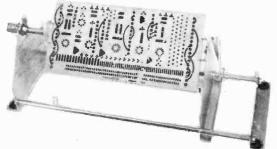
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VOLUME 14 No. 3 NOVEMBER 1977

WINDOW GAZING

Any student of electronics knows what a difficult task it is keeping up with the ever expanding range of monolithic circuit devices. Manufacturers' literature, ranging from single data sheets and application notes to impressive tomes of hundreds of pages, reveals a staggering variety of purposedesigned chips covering a multitude of applications including newly opened-up fields. It is all mouth-watering. But all too frequently, we can only gaze at the goods and not touch.

Some LSI devices hit the headlines, become household names, and feature almost continuously in constructional projects. But there is a far greater number of lesser-known i.c.s which have not been so well exposed in the constructor area, although they may be common-place in the industrial scene.

Included amongst the latter will be a host of intriguing devices which have been designed for equipment manufacturers' specific requirements, and have no immediate obvious application outside this intended area. Yet unsuspected possibilities do often come to light when these chips are subjected to scrutiny by independent and unbiased eyes. Give the amateur enthusiast a chance, and it is almost a certainty that he will come up with a new idea for exploiting some such device beyond its originally intended purpose.

In terms of devices produced, it is clear that we in the constructor area have seen only the tip of the iceberg. It is more by luck than plan when custom designed i.c.s find their way into amateur hands. More is the pity; not only for the constructor himself, but also the manufacturer and supplier. These commercial interests stand to gain by a fuller exposure of these devices.

Microcircuit manufacturers ought to consider the advantages of making their products more widely known and accessible to the amateur market. By doing so, they will be doing themselves a favour. They will be interfacing with a large body of uncommitted technical free thinkers. Any worthwhile achievements arising from these non-professional endeavours must help increase the value, repute, and sales of specific devices.

This topic was briefly touched on here last month. But it is a matter of fundamental importance and deserves underlining from time to time. And this month is particularly opportune, since we have included an extra 8-page supplement entitled I.C. Specials.

A CHOICE SELECTION

Some examples of the kind of devices we have in mind are mentioned in this supplement. It has been possible to include only a few, but these have been selected to cover a variety of applications and interests.

Musical interests are well catered for and this reflects the i.c. industry's current large commitment to this expanding area of home entertainment. What's good for

the commercial organ maker is equally good for the constructor. Electronic delay lines represent an important technical development, and have endless possibilities apart from "flanging", so this particular "bucket brigade" chip does not have to be confined to the musical domain.

Temperature controllers and fluid detectors bring us into the strictly workaday area of instrumentation. Timing requirements ranging from 5 milliseconds to over 3 months are provided for by one single chip-a device which should satisfy an awful lot of requirements. And of course TV games. Our selection would not be complete without some representation from this growing area.

There's plenty of food for thought in our supplement. It provides just a small sampling of notable devices currently available but will trigger off sufficient ideas to keep our imaginative readers busy for quite awhile.

PRICE INCREASE

As readers will have discovered, the cover price of PRACTICAL ELECTRONICS has been increased to 45p as from this issue. News of this decision came too late for mention in last month's issue. We very much regret the need for this increase, which is due to factors beyond our control.

> F. E. BENNETT, Editor.

EDITORIA!

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Letters

Queries regarding articles published in PE should be addressed to the Editor, at the Editorial Offices, and a stamped, addressed envelope enclosed. We cannot undertake to answer questions regarding other items, nor to answer technical queries over the telephone.



Can be added to Minisonic for sequencing melodies or rhythm pattern

THE sequencer circuit to be described will enable a voltage controlled synthesiser to automatically play a pre-programmed tune, consisting of up to 32 pitches, in a sequence up to 128 notes long. All programs are keyboard initiated.

BLOCK DIAGRAM

The heart of the sequencer is an NMOS RAM (random access memory) capable of storing 128 eight bit words of data. The circuit operation can best be understood by referring to the block diagram of Fig. 1. Here the RAM is driven from a clocked binary counter. The binary number at the output of this defines the position in the memory that is present at the data terminals. The sequence is written into the memory via a modified 49 note keyboard which converts the 32 possible pitches into five bit words.

The 128 note sequence is built up by stepping the counter each time a new note is written in. When a sequence is complete, it is played by clocking the counter at a steady rate by means of the clock oscillator. The five bit words are then read out from the memory into a digital to analogue converter (D-A) which produces a 32 level output. This is used to drive the v.c.o. in the synthesiser.

SEQUENCE LENGTH

Although the maximum sequence length available is 128 notes, it is often desirable to use a shorter sequence. For example, if the tune to be written consists of 32 bars with three beats to the bar, it is obvious that the total number of beats would be only 96. To cope with this type of situation the circuit was designed so that the counter could be reset at any desired point in a sequence, thus producing tunes of any length from 1-128 beats.

Only five of the eight bits of memory are used to produce a control voltage for the v.c.o., the other three bits are available to perform other functions. One of these spare bits is used to provide the variable reset function, and the other two bits are used to generate trigger pulses for envelope shapers, thus adding rhythm to the generated melody.

CLOCK OSCILLATOR AND COUNTER

The complete circuit is shown in Fig. 2. Here clock pulses are produced by a simple transistor astable multivibrator. The frequency may be varied over a wide range by adjusting VR1. Clock pulses are fed to the binary counter via S1, the stop/run switch.

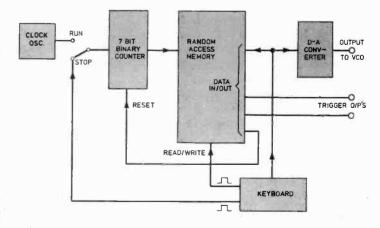


Fig. 1. Block diagram of sequencer



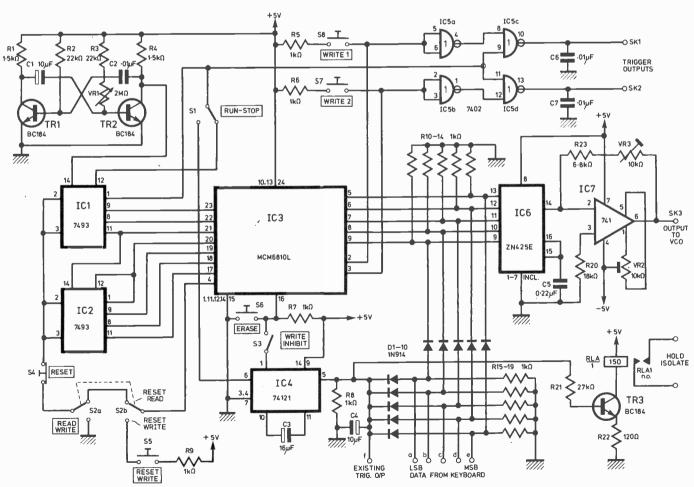


Fig. 2. Complete circuit of sequencer

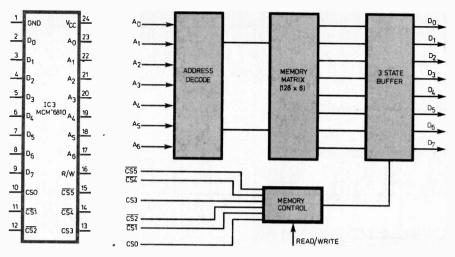


Fig. 3. IC3 pin-outs and internal block diagram

IC1 and 2 are cascaded to form a seven bit binary counter which drives the address inputs of the RAM. The stop/run switch disconnects the first stage of the counter and instead provides the counter with pulses from the keyboard. The reset inputs of IC1 and 2 are connected via S4 and S2 to one of the data lines of the RAM, the

automatic reset pulse is written into this line by selecting "Reset Write" with S2 and depressing S5.

Returning S2 to the "Reset Read" position reconnects the data line to the counter resets. Thus, when the end of a sequence is reached, the reset data line goes high and the counters reset to zero.

COMPONENTS . . .

	The second second	ARRIBATION AND SECURITY OF THE SECURITY OF THE		
Resistors				
R1 1.5kΩ	R20	1 8 kΩ		
R2 $22k\Omega$	R21	27kΩ		
R3 $22k\Omega$	R22	120Ω		
R4 1·5kΩ	R23	6·8kΩ (see text)		
R5–19 1kΩ (14 off)		A STATE OF THE STA		
All ‡W 5% carbon				
Capacitors		- 25 " - 15 15		
C1 10µF elect. 25V	C4	10μF elect. 25V		
C2 0.01 µF	C5	0·22μF		
C3 16µF elect. 25V	C6, 7	0·22μF 0·01μF		
of the first town	Co, 7	0.01με		
Integrated Circuits				
IC1 7493	IC5			
IC2 7493	IC6	ZN425E		
IC3 MCM6810L	IC7	741		
IC4 74121				
Transistors and Diodes TR1-3 BC184 or simil D1-90 Any general p	ar	type		
Relay RLA D.i.l. reed relay, (R.S. Componer		pole		
Variable Resistors		1 Lug 3		
VR1 $2M\Omega$ pot. (lin.) VR2 $10k\Omega$ min. preset		-167 1 1		
VR3 10kΩ min. preset				
VIII TOKIZ IIIII. preset				
Switches		A 1 A 1		
S1 s.p.c.o. miniature t	oggle	A characters		
S2 d.p.c.o. miniature t	oggle			
S3 single pole miniatu	ire togo	ile		
S5 miniature push to				
S7 miniature push to				
S8 miniature push to				
Miscellaneous				
PCB board, front panel				
Veroboard for diode m	ounting			

RANDOM ACCESS MEMORY

Integrated circuit IC3 is a RAM, type MCM6810 designed for use with the M6800 microprocessor system. The block diagram and pin outs of the device are shown in Fig. 3. Pins 4–9 are data input/output terminals, the state of pin 16 deciding whether the device is in the read or write mode.

Pins 17-23 are the memory address inputs. The binary code fed to these pins determines which of the 128 memory cells is connected to the data terminals. Thus, when the clock and counter are running, each memory cell in turn is presented at the data terminals of the chip.

KEYBOARD BINARY CODER

In the prototype synthesiser a four octave keyboard is used to write the required sequence of notes into the memory. This accomplished by diode keying circuitry of Fig. 4. It will be seen from this that each contact connects the five data lines to the five volt rail via a combination of diodes.

These are arranged so that a binary number corresponding to the number of the key pressed appears on the data lines. The five data lines, plus an extra line for key one are also routed through diodes to a monostable IC4 which generates a read/write pulse at pin 16 of the RAM, so that whenever a key is pressed, the binary code appearing on the data lines is written into the memory.

IC4 also produces a clock pulse which drives the counter. Therefore operation of any key causes three things to happen:

- 1. A binary number corresponding to the number of the key will appear on the data lines.
- 2. A write pulse will occur at pin 16 of IC3.
- 3. The trailing edge of the pulse from IC4 will clock the counter and hence step the memory on one position.

ENVELOPE TRIGGER OUTPUTS

There are eight data lines in the RAM. As already mentioned, five of these are used to produce pitch information, and one to provide the automatic reset facility. The two spare data lines are used in the prototype to store trigger pulses for the synthesiser's envelope shapers.

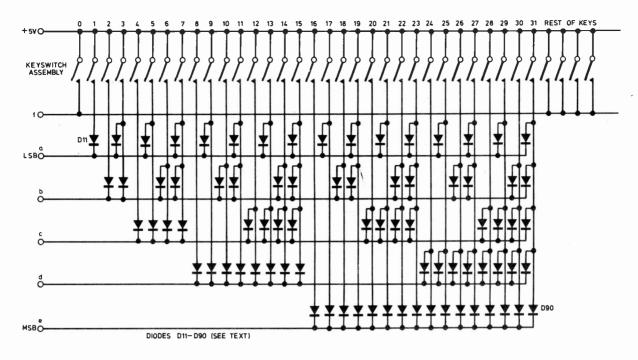


Fig. 4. Diode keying from keyboard to main sequencer circuit

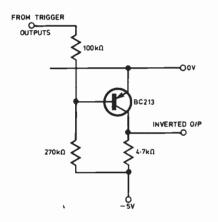


Fig. 5. Trigger inverter

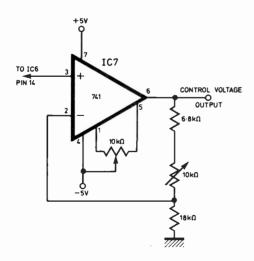


Fig. 6. Alternative output circuitry

Push button switches S7 and S8 are used to write in the trigger pulses when required. When the circuit is in the read mode, the outputs from pins 3 and 2 of IC3 are gated in IC5 with clock pulses. This ensures that whenever two consecutive pulses are written, two separate pulses appear at the output. Without the gating, only one long pulse would be produced.

It should be noted that the trigger pulses produced are positive-going, and are suitable for driving either of the ADSR envelope shaper circuits that have appeared recently in this magazine. The ES/VCA circuits of the Minisonic however, require negative-going pulses. These can be produced, if necessary, by the simple circuitry of Fig. 5 (three of these are needed).

The keyboard is fitted with two sets of contacts, one being used to drive the coding diodes, the other to drive a resistor chain for normal playing. For normal playing, a separate envelope trigger output is provided from the point which drives IC4. If the keyboard isolating relay (Minisonic Mk. 2) is being used it can be driven as shown in the main circuit diagram. (If not TR3 and associated components may be omitted.)

D-A CONVERTER

Early versions of the prototype utilised a number of different D-A converters, all of them using discrete components. All the circuits tried suffered from one problem or another, and all had the disadvantage of needing close tolerance resistors to function accurately. The integrated circuit D-A finally decided upon solved all these problems, although at somewhat increased cost.

The D-A chip feeds an inverting op-amp with gain and offset controls. The voltage at the output of the op-amp is of the correct sense for the Minisonic v.c.o.s, i.e. it is negative going for increasing pitch. For oscillators requiring positive-going control voltages the alternative output circuitry of Fig. 6 can be used.

NEXT MONTH: Construction and programming detail.

This battery powered unit displays a subject's reaction time on a "non related" scale from one to nine, and although pocket sized, it is simple to construct, costing in the region of five pounds.

It should be made clear that the device is *not* intended to indicate reaction delay on a true scale of time, such as in milliseconds, because generally speaking the usefulness of a simple reaction timer lies not in measuring reactions precisely in fractions of a second, but in comparing them.

If the object of the exercise is to sharpen one's personal reaction time, or to compare yours with another's, then it is of little consequence if the readout is, for example, 170ms, since this may mean little to a subject in any case!

Digital ACTION TIMER D.C. GREEN



This novel and robust unit was designed to fill the slot requiring simple indication, and not expensive precision timing. Digital operation with numerical display was chosen however, because this eliminates argument over the results. It also precludes the possibility of a declining reading due to a discharging capacitor while the argument takes place, something which can happen with some analogue types.

The scale factor can be set to measure only those reaction times likely to be attained, and when the one to nine range of this device has been expanded to the desired time limit, it will be found to have adequate resolution, leaving no scale redundancy. This freedom to adjust the "difficulty" aspect should be found useful.

USING THE TIMER

A reaction timer must provide the user with a subtle, but clear signal to which he can react. In this circuit, it takes the form of the seven segment display decimal point, which lights up after a semi-random time delay. After switching on, the display either remains blank, or shows a spurious number. The user then pushes the button on the front panel, and waits. Any number on the display will then be cleared.

When the signal l.e.d. illuminates, he must release the button as quickly as possible. Providing he was not so slow as to be "unclassified", his response time will remain displayed, and the lower the figure, the better. Should he attempt to cheat, or if he misses the signal altogether, the display merely remains blank. For another try, the button is pushed again, whereupon the display resets and the signal is awaited once more.

COMPONENTS...

Resistors

R1, R2 $1kΩ \frac{1}{4}W 5\%$ R3 $100kΩ \frac{1}{4}W 5\%$ R4 $47Ω \frac{1}{4}W 5\%$ R5–R11 $220Ω (7 \text{ off) } \frac{1}{4}W 5\%$

Potentiometers

 $\begin{array}{ll} \text{VR1} & 220\,\Omega \text{ 0-1W vert min preset} \\ \text{VR2} & 1\text{k}\Omega \text{ 0-1W vert min preset} \end{array}$

Capacitors

C1-C3 100μF 10V elect (3 off) C4 0·1μF

Semiconductors

 IC1
 7413
 TR1
 BC108

 IC2
 7400
 D1
 1N4148

 IC3
 7493
 D2
 1N4001

 IC4
 7447
 X1
 DL707

Switches

S1 Min slide switch (½A)
S2 Push-to-make push button

Miscellaneous

Aluminium box $100 \times 70 \times 38$ mm (type AB9, available Maplin)

Printed circuit board

Offcut of plain matrix board

Piece of copper laminate board

Battery holder for four HP7 cells, and connector stud

Socket, d.i.l. 14 pin

Four stand-off pillars (approx 23mm)

THE CIRCUIT

The complete circuit diagram is shown in Fig. 1, and may be divided into three functional sections: (a) The Delay Pulse Generator, consisting of IC1a and its associated components. This drives the signal l.e.d. and initiates a timing cycle via the latch comprising IC2a and IC2b. (b) The Clock/Counter section formed by IC1b and IC3, which performs the actual timing operation, and (c), the Display Decoder/Driver (IC4), along with display X1.

Consider the circuit with S2 held closed. To start with, the 4 bit binary counter IC3 is held in reset because pins 2 and 3 are held high by the set/reset latch. Periodically, at about once every 5 seconds, the Schmitt Pulse Generator produces a brief positive going pulse. Transistor TR1 is necessary in this circuit because the

low, pulled down by R1. This disables the clock oscillator, clamping the output high, and in turn arresting counter IC3. The BCD information on the outputs of IC3, is decoded continuously by IC4, to be displayed on X1. Therefore, when IC3 stops counting, a number corresponding to the reaction time is held on display until S2 is pushed for another try.

The zero blanking facility of the 7447 has been used to conserve battery power, and to eliminate distraction whilst awaiting the signal.

Gate IC2d is added, in order to inhibit pulses from the Delay Pulse Generator to the latch, when S2 is open. Without this, the latch could, under certain circumstances, be set with the push button up, which would cause a count the moment it was pressed. But as it stands, it is possible for the generator to be at any point in its

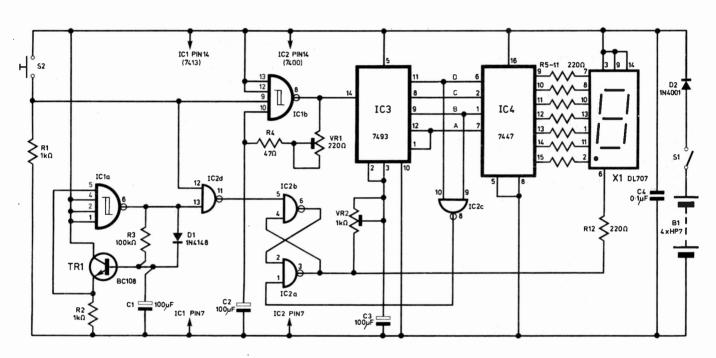


Fig. 1. Circuit diagram of the Digital Reaction Timer

minimum frequency that can be obtained from the simpler form of Schmitt oscillator, is too high for this application. Diode D1 modifies the mark space ratio of the output.

This periodical pulse is inverted by IC2d while pin. 12 is high, and is used to set the latch. The output on IC2 pin 3 then goes low. This event causes two things to happen. The signal light comes on immediately, and C3 commences discharge through VR2, and when the voltage across C3 is sufficiently low, counter IC3 is enabled, thus allowing it to be clocked by the other Schmitt oscillator comprising IC1b and VR1, etc. which runs at about 50Hz.

If S2 remains closed, IC3 will continue counting until it reaches 1010 (the binary equivalent of 10), when both inputs of IC2c will be satisfied, causing a low output. This will reset the latch again, forcing IC3 back to zero. With the arrival of the next pulse from the Delay Generator the whole cycle will be repeated.

If S2 is opened during one of these timing periods, however, the input on pin 9 of IC1b immediately goes

cycle at the instant of pressing S2. The signal can be expected at any time, ranging from almost immediately, up to about five seconds.

The circuit should be powered by four HP7 batteries. Diode D2 is necessary to drop the supply voltage to less than 5.5 volts, the maximum permissible for TTL. It will also protect the circuit from reverse polarity.

CONSTRUCTION

The prototype circuitry was housed neatly in an aluminium box, using a simple mounting method that avoids the use of nuts, bolts or screws, other than a pair of small self-tappers for securing the lid.

All the components are readily available types, the only proviso being that the capacitors, resistors, and presets are not too large physically. A recommended p.c.b. layout is shown in Fig. 2, employing a fair number of wire links on the component side of the board, so that the copper pattern is kept reasonably simple. The component layout is shown in Fig. 3.

DIGITAL REACTION TIMER

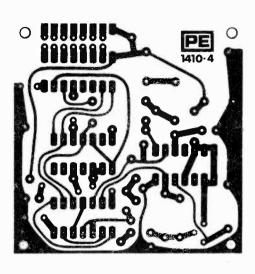


Fig. 2. Printed circuit board (full size)

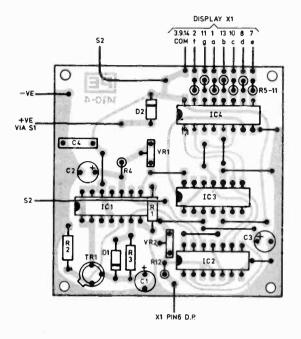
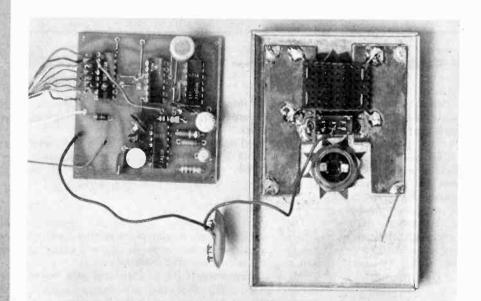
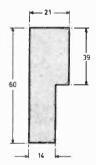
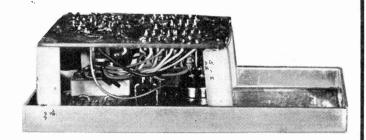


Fig. 3. Component layout and interwiring to off-board components





The left-hand blank p.c.b. plate is shown in detail above, and can be seen in position with the right-hand plate in the adjacent photograph



The method of fixing everything together can be seen in the incidental photographs. Two pieces of blank p.c.b. are cut out and stuck to the lid around the switch and display holes, with the copper side facing upwards. The display unit is mounted on a small piece of unclad perforated board (0·1 inch pitch), and a 14-way i.c. holder is pushed on from behind to secure it. Loops of tinned copper wire can now be passed through the perforated board and soldered to the copper cladding. A piece of red tinted plastics film can be placed over the display before fastening it. The switch S1 can also be soldered to the cladding by means of its mounting lugs.

When assembling the p.c.b., it is quite in order to solder the i.c.s directly to the board, providing this is done with care. Nevertheless, a socket ought to be used for X1, as this allows it to be disconnected from the flying leads to the p.c.b. during wiring up. Flying leads also connect the p.c.b. to push button S2, the battery positive via S1, and battery negative.

FINAL ASSEMBLY

At this point, with all the connections made, the unit may be tested, and if all is well, the p.c.b. can be attached to the lid. First solder four pieces of stout wire perpendicularly to the lid, on the copper clad plates previously glued to same. Position them in a square configuration to match the mounting holes of the p.c.b. A stand-off pillar is then placed over each, and the p.c.b. is threaded over the protruding wires, onto the pillars, and soldered at each corner, The p.c.b. is mounted component side down; so the stand-off pillars must be long enough to keep the components clear of the display socket, yet not so long as to exceed the space within the box. If you have an expired ball point pen of the hexagonal plastics tube type, this could be cut to provide the spacers.

Finally, snip off any surplus wire from the p.c.b. and tape the bottom of the box to prevent shorts occurring. The battery holder should fit tightly into the recommended box, and require no other fastening, but precautions may be necessary to prevent the self-tap screw from biting into one of the cells when this lid is finally secured.

ADJUSTMENTS

There are only two of these; namely clock frequency, and commencement delay, controlled by VR1 and VR2 respectively. Both of these presets are accessible with the p.c.b. in place.

It is entirely up to the user as to how these are set, but the most useful setting is realised with a relatively high clock frequency, and the delay adjusted so that an average reaction time scores 5 or 6. The higher the clock frequency, the higher the resolution

NEWS BRIEFS

System X

CONTRACTS worth £20 million have bee placed by the Post Office with British manufacturers, as the next step in the System X project, the biggest development ever undertaken in British telecommunications.

It covers the design of trunk, tandem, and small/medium capacity local exchange equipment, based on microelectronic and software control technologies, and will carry the telephone system into the 21st Century.

Already some 500 engineers are involved in System X, a modular system which should lay the foundations for an expanding range of future customer facilities, and is expected to cost more than £100 million.

CES No Longer

N September 1st, 1977, Combined Electronic Services Ltd, the service company for Philips and Pye household products, changed its name to "Philips Service".

Now part of the recently announced Philips Industries' new Central Merchandising Management Group, Philips Service (claimed to be the largest manufacturers service organisation of its kind in the UK), will continue to be responsible for the total provision of after sales service support for the Philips and Pye Consumer Division.

A new computerised order handling system was introduced, which is a customisation of a package already used in Europe by Philips Services. The basic philosophy is to provide the best possible service support on a local basis, by the creation of 25 Service Centres.

PE

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FRANK W. HYDE

SPACE SUITS

The advent of the space shuttle brings many changes in space methods and activity. One of the most important of these changes is that of the space suit. The Apollo suits had certain disadvantages which became apparent in use and were costly indeed since each suit was virtually tailored to fit and made one mission only. The same applied to the backpacks and life support systems. The new suits will be less than half the cost.

Contrasting with the Apollo suits, the new generation of space suits will have a life of fifteen years. Many missions will be flown during that time. The new suits have a rather different arrangement from the moon suits. For example, the moon suits were pressurised and designed for the 1/6 gravity of the moon. With the extra vehicular activity (EVA) of Spacelab and similar missions, zero gravity will be the norm. Also a quick turn round is necessary. The Apollo suits required about 90 minutes to don and check but the new ones will take only 15 minutes. The actual donning time is about 5 minutes.

CONSTRUCTION

The construction of the new suits is such that there are two parts. The torso and backpack are integral and hard. This allows life support systems to be solid and internal as against flexible and external in the moon suits. The lower half is soft and is "stepped into". In dressing the lower half is donned first and then the arms head and torso are "inserted" in the top half which is in a support on the wall. The two halves of the suit are closed by a ring.

Added to the ease of dressing is the extra mobility which is obtained using joints of constant volume in place of the pulley joints in the Apollo suit. There is also another important advantage in that whereas the Apollo suit worked against the effort of the astronaut the constant volume system enables free movement without great effort.

Another basic difference between the Apollo suit and the shuttle suit is the fact that Apollo had zippers which could leak whereas the shuttle ring closures are virtually leakproof. The pressure bladder used in Apollo is now replaced by a polyurethane bladder which has seams sealed by heat. The Apollo suit had latex bladders which were tape and glue sealed.

MONITORING

The new suit will be easier to monitor, as to status, than the old ones. A microprocessor/light emitting diode unit will tell the astronaut whether there is a problem with the suit systems and what to do about them. The Apollo suits had an electric warning system but no instruction readout to tell the astronaut what to do about it. The microprocessor, which is carried in the chest pack, is a great advantage in the new suit.

The joints in all the suit electronics are solderless. These necessary joints caused trouble in the *Apollo* suits. The arrangement of suit/backpack design places all controls where the astronaut can see them. The 12 character readout display replaces the *Apollo* "cuff card" systems where warnings from the suit had to be checked by reading procedure lists carried on the sleeve.

The new suits will not be allocated to individuals. Each astronaut will choose the one he or she likes. The suits will be in three basic sizes allowing for the accommodation of male or female participants. A different urine collection system will be required but the final details will await the choosing of female astronauts.

COOLING

The liquid cooling garment which is worn by the astronaut is fitted with ventilation tubes. Oxygen is fed in through the helmet and taken to the hands and feet then returned through the backpack for reuse after conditioning. The initial length of extra-vehicular activity for the missions can be up to 7 hours. Oxygen pressure will be 4·1 psi. Astronauts will have to pre-breathe oxygen at 4·1 psi for 3 hours before extra-vehicular activity to denitrogenate the blood to avoid "bends". As little work will be required to be done with their legs, as on Apollo moon mission,

there is less loading and metabolic activity.

Recharging of the systems will take only a few minutes. Battery recharging will only take an hour while replacement takes only a few minutes. Crew and specialists will wear suits for their activities but if it should be necessary to move other personnel to or from shuttle to installation this will be done in a sphere manœuvred by astronauts.

SPINNING SOLAR SAIL

Another propulsion system, for the mission to Halley's comet in 1986, is being studied by NASA. This is a rotating sail system. It consists of 12 sails each 4 miles long by 28ft wide.

The sails would be unfurled by centrifugal force after deployment of the vehicle from the space shuttle. The pressure of the solar wind would spin the sails and gradually accelerate the craft to the rendezvous point. The time of spin is expected to be one revolution every three minutes.

This system is now favoured over the square sail version. It is competing with the ion motor. A decision is expected soon.

SPACE TELESCOPE

Lockheed-Missiles and Space have been chosen to build the new space telescope. The optics are to be supplied by Perkin-Elmer. Among these will be the 94in diameter primary mirror. The space telescope is large being 43ft long and 14ft in diameter. The shuttle will launch it into Earth orbit in 1983.

JUPITER ORBITER PROBE

The house of representatives voted out the funds for the Jupiter orbiter probe mission. There has been a reversal of that decision now and the budget for 1978 has been restored. The orbiter Jupiter Probe is now ratified by the Senate Appropriations Sub-committee.

This is an important mission in view of a number of new facts regarding the largest planet in the solar system. The cost of the two spacecraft and ancillary requirements including launching is estimated at some 450 million dollars.

Orbiters will be launched by shuttle and will be the first payload to go into deep space. It will also be the first payload to be boosted by the upperstage. The probable date of launch will be January 1982 and the encounter with the planet will be late 1984.

An aeroshell will be released to descend into the Jovian atmosphere from where radio information will be received for the first time.



SIMPLE ELECTRONICS FOR MODELLERS

By I. R. Sinclair Published by Argus Books Ltd. 110 pages, 140 × 215mm. Price £2.95

In times gone by, it would have seemed ridiculous to electronically control something like a model railway, using valves and relays as large as the locos themselves. But the birth of microcircuits has reversed this situation to create a new branch of interest, and this book is based on such techniques, covering current and voltage control, generating signals and delays, measurement, counting and logic circuits, motor speed control, power supplies and p.c.b.s.

In the book, which is intended as a "methods" source rather than an instructional manual, the author proposes that many of the skills required by the modeller, are similar to those

required for modern electronics construction.

RADIO CONTROL FOR MODELS

By R. H. Warring Published by Pitman Publishing Ltd. 213 pages, 194 × 255mm. Price £6.95

EXTENSIVELY revised, this second edition of Radio Control For Models is mainly about "proportional" control, and starts with some historical notes which prepare you for a chapter on basic radio theory; but it's not too technical! In fact, the aim of the book is to show that your can treat all the electronics as simple black boxes, and just concentrate on the modelling aspect of the hobby.

There are no constructional features, although diagrams and photos of R/C "bits and pieces" are included, along with explanations of their basic principles. Practical workshop hints are given, and it is in this chapter that a jolly photograph appears showing various types of miniature switches compared to a threepenny piece—for those who can remember them!

ELECTRONICS FAULT DIAGNOSIS

By I. R. Sinclair Published by Argus Books Ltd. 108 pages, 138×216 mm. Price £2.75

FIRCUITS in this book are graded, starting with the most simple and working upwards. There is no particular tendency towards domestic equipment, since much of the servicing guidance given applies to industrial or communications type electronics. This book should be useful to students studying the C & G 272 and 222 courses.

The chapters are: Power Supplies, Audio Frequency Amplifiers, Timing Circuits, Measuring Circuits, Oscillators, Trigger Circuits, Control and Interface Circuits, and Digital and Counting Circuits.

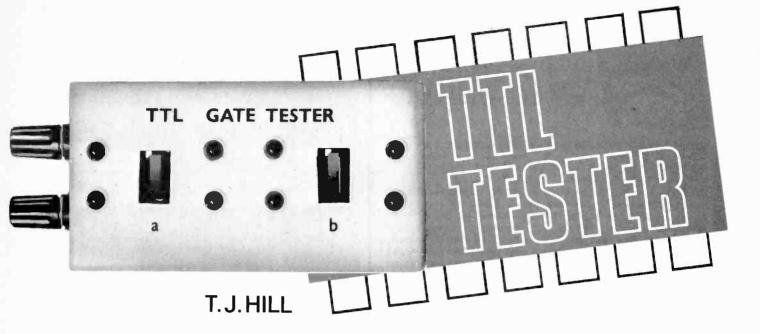
Each chapter comprises one or more circuit diagrams with corresponding sets of voltage readings, or oscillograms, for certain points. After taking in the circuit description, it is then up to you to deduce which set of readings is correct.

The answers are in the back of the book, along with an explanation of which component failures would have caused the other incorrect readings shown.

The effect on voltages of various types of measuring instrument is also covered, and in some tables your are expected to take such loadings into account when seeking the right answer. This book is not for the absolute beginner.

M.A.





FOR 74 FAMILY OF QUAD-GATE PACKAGES

THIS gate tester was designed to be cheap, and to be capable of testing a wide range of simple QUAD-GATE packages. The unit works by applying to each gate in the i.c. under test, every possible combination of inputs, and monitoring the outputs with l.e.d.s.

TEST SOCKETS

There are two basic pinout configurations used in the 7400 series of quad gate packages, and these are illustrated in Fig. 1, where the 7400, and the 7401 are shown.

Two i.e. sockets are fitted in this tester, to accommodate each pin arrangement.

THE CIRCUIT

Referring to Fig. 2, the 555 timer (IC1) is wired as an astable multivibrator with a frequency of about 2Hz. The output from this is fed to a 7470 flip-flop (IC2), which divides the signal by two. This, and the original oscillator signal are taken to every gate in the i.c. under test; each

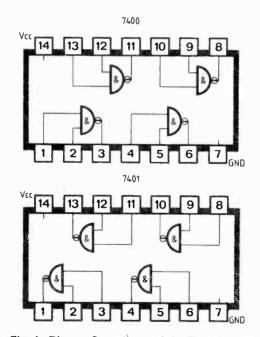


Fig. 1. Pin configurations of the 7400 and 7401

COMPONENTS...

Resistors

R1, R2 $10k\Omega \frac{1}{4}W$ 5% (2 off) R3-R10 $390\Omega \frac{1}{4}W$ 5% (8 off)

Capacitors

C1 47μF 10V elect C2 22μF 10V elect

Semiconductors

D1-D8 0.2in red l.e.d. IC1 NE555 Timer IC2 7470

Miscellaneous

Verobox type 65-2518H Veroboard 0.1in Red 4mm terminal (SK1) Black 4mm terminal (SK2) 14 pin d.i.l. sockets for test positions (2 off)

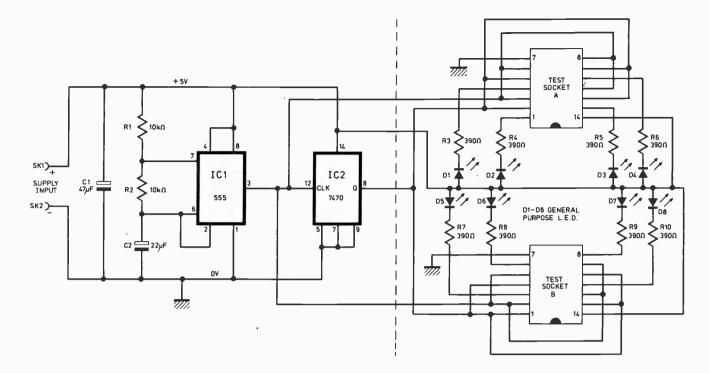


Fig. 2. Circuit diagram of the TTL tester. A capacitor of $0.01 \mu F$ connected from IC1 pin 5 to ground may be found necessary for reliable operation

signal going to each of the two inputs. These input waveforms are shown in Fig. 3, and the correct output for a 7400 is shown as an example.

The outputs, drive l.e.d.s. D1 to D8, causing them to illuminate when the signal generated by the gate under test is low, thus allowing open collector type gate to be tested with this system.

Testing a 7400, it can be seen from Fig. 3 that the output l.e.d.s should be on for one quarter of the total waveform period. This, and the relationships for other quad gate packages, can be seen in Table 1.

Table 1. Output I.e.d. illumination times for correctly operating gates. Ten 74 series quad gate packages

Package type	Test socket	l.e.d. duty cycle
7400	В	25%
7401	A	25%
7402	A	75%
7403	В	25%
7408	В	75%
7409	В	75%
7428	A	75%
7432	В	25%
7433	A	75%
7438	В	25%

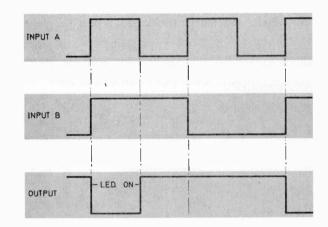


Fig. 3. Test waveforms applied to each gate. The correct output for a 7400 is shown



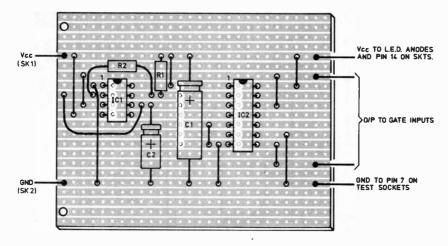


Fig. 4. Stripboard layout of prototype

CONSTRUCTION

The basic circuit was assembled on a piece of stripboard (see Fig. 4), which was then mounted in a small polystyrene case, by the integral mounting pillars.

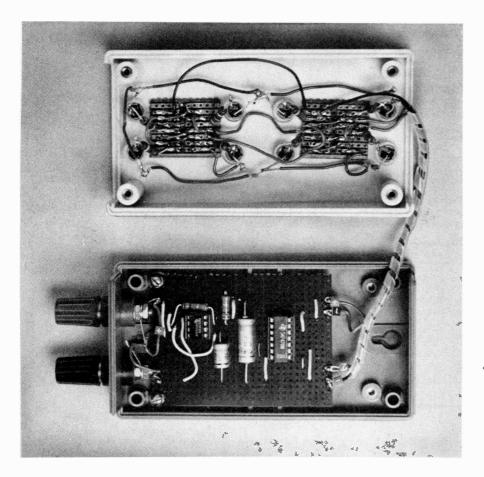
The lid of the case was cut to accommodate two 14 pin i.c. holders, and the eight l.e.d.s. Dimensions will depend upon the type of l.e.d.s preferred, and i.c. holders used, but the photographs will show the general layout involved.

The l.e.d.s can be fixed, either by adhesive, or using the proper bezels, and the i.c. holders will best be mounted

each on a small square of stripboard, to which they can be soldered. The plate so formed, can then be used to glue the holder to the lid.

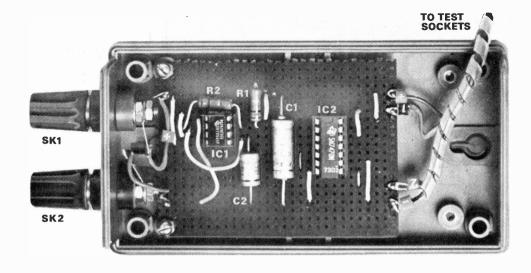
Cut holes for the two 4mm socket terminals (SK1 and SK2), and mount these. Next drill the main component board so that it can be mounted in the base of the box.

A harness of four wires should be formed, to link the main board to the i.c. socket boards. This will carry the two signal lines, and the two supply lines. Wire both the i.c. socket units for +5V and 0V, and next, the two signal



In the prototype, the i.c. sockets were soldered to pieces of Veroboard which were then glued to the lid. The sockets and l.e.d.s were linked directly using the 390Ω resistors

Power is applied via the 4mm terminals, but using a larger box would allow room for operation from an internal battery. An on/off switch could be mounted in place of the terminals



lines to all the appropriate pin numbers detailed in Fig. 2. The +5V line should also be wired common to all the l.e.d.s (check for correct polarity), and the other side of each l.e.d. wired to its respective i.e. socket pin, by means of a 390Ω resistor (R3-R10).

The l.e.d.s should be wired up so that they are adjacent to the outputs they represent. The lid was lettered using dry letter transfers sprayed with laquer, and it may be advantageous to put the related pin numbers against each l.e.d.

Finally, do not forget to connect up the two 4mm terminals for the supply input.

OPERATION

In use, the i.c. to be tested is inserted in the appropriate socket (use Table 1), power is applied, and the l.e.d.s will indicate the condition of the i.c.

A gate with a faulty output stage will cause the incorrect flashing of its associated l.e.d., and a gate with a damaged input stage will possibly cause all the l.e.d.s to flash incorrectly. The operator can learn to interpret the meaning of the various indications.

The prototype is powered by an external supply, but since current consumption is only about 30mA average, battery operation is feasible.

MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned. All quoted prices are those at the time of going to press.

CONDUCTIVE PAINT

After five years of selling exclusively to industry, Industrial Science Ltd., are now introducing one of their most successful products—Elecolit 340—into the consumer electronics market.

This is a pure, silver filled, electrically conductive acryllic paint. It exhibits excellent conductivity because of the pure silver and outstanding environmental protection due to its acryllic base and sets by solvent evaporation similar to most good lacquer systems forming a tough film with good adhesion to ceramics, glass, rubber, plastics and most plastics films.

Typical applications include r.f. shielding, printed circuit repair, use as a conductive ink, prototype circuit manufacture

and one of the most interesting and unusual applications of all which is to repair the rear window demister of a car by means of painting over the existing track which may have either broken or shorted out.

Although it is air drying, conductivity can be improved by heating.

The shelf life is a minimum of 1 year in a closed container, and the operating temperature is from -60° C to $+175^{\circ}$ C.

It can be applied by painting, silk screening or roller, and if necessary it can also be thinned with a solvent to lower the viscosity.

Details of price and further information can be obtained from Industrial Science Ltd., Leader House, Dept. P.E., 117-120 Snargate Street, Dover, Kent.



The Elecolit 340 conductive paint from Industrial Science



ALARM CLOCK

A particularly elegant digital alarm clock, the Fairchild Timeband is available from Tempus.

Available in white or black, and taking up little more space on your bedside table than an old-fashioned mechanical alarm clock, the Timeband offers timekeeping and alarm accurate to the second.

The readout is on large sevensegment l.e.d. displays, showing hours and minutes or, at the touch of a button, last minute digit and seconds. Indicators are provided for AM/PM, Mains Failure, and Alarm On. The alarm should be loud enough to waken the heaviest sleeper, and includes a "doze" feature which can call you up to six times in an hour.

The Timeband costs £14.95, including VAT, post, packing and insurance, from Tempus, 19-21 Fitzroy Street, Cambridge, CB1 1EH.

Semiconductor UPDATE...

FEATURING : TMM142C H.L.C.D. 0024 LM194

R.W. Coles

FORGET ME NOT

The nice thing about old fashioned magnetic core stores was that, like the elephant, they never forgot. Fill them full of lovely binary data and then hit the mainsoff switch, and next week when you switched on again it would all be just as you left it (brings tears to my eyes!).

Problem was, of course, that their uncanny resemblance to the elephant extended also to their physical bulk and their rather slow response, and those little drawbacks soon got them the chop when fast, cheap semiconductor RAM chips emerged from the undergrowth.

With semiconductor RAM of course, if you hit the power-off-switch all you end up with is a garbage, a problem the data processing industry decided it would have to live with if it wanted the other goodies on offer.

Where loss of data was a problem, non volatility *could* be arranged by providing battery back-up supplies, or by transferring crucial data to permanent storage media such as magnetic tapes or discs, but this proved either expensive or a headache for the software designers. In recent years the CMOS RAM has emerged to make the battery back-up solution more viable, with a stand-by life measured in years now possible with quite small batteries, but CMOS RAMs are expensive, slower, and less dense than their NMOS cousins and so the problem of volatility is still not completely solved.

A new solution to this problem has recently been introduced by Toshiba in the form of their **TMM142C** 256×4 RAM chip which uses a double cell in each bit position, to provide the rapid access read/write capability of standard RAM combined with the non-volatility of the MNOS electrically alterable ROM technology.

The MNOS (Metal Nitride Oxide Semiconductor) alone is certainly non-volatile but it can't be used in place of standard RAM because writing and erasing data is slow and requires high voltages. By combining MNOS devices with conventional RAM circuitry the best of both worlds can be achieved. With power up, normal fast read/write access is possible, but when a power fail condition is detected the RAM data is transferred to the MNOS devices where it will remain for very long periods. When power is restored the stored data is duplicated in the RAM array ready for instant use. The data also remains in the

MNOS latches and must be erased before re-use by means of a positive pulse applied to the MG input.

THE DRIVER

Liquid crystal displays are pretty, popular, offer extremely low power drain, and are, unfortunately, excrutiatingly difficult to drive.

Take a standard clock or voltmeter chip with multiplexed BCD or seven segment outputs and any fool can interface it with the l.e.d., Minitron, or gas discharge display of his choice, but the thought of hooking it up to a $3\frac{1}{2}$ digit liquid crystal panel makes brave amateurs buckle at the knees and even experienced designers cough nervously.

The l.c.d.s require an a.c. display drive supply of about 30 to 100Hz, and they cannot be multiplexed, a combination completely alien to most likely display sources. To interface to a clock chip, for example, you would first have to demultiplex and latch each display digit, then wire these to the l.c.d. via decoders and exclusive on gates, and finally provide an l.f. backplane drive source. A glance at the serried ranks of standard CMOs chips that you would need to hang around your clock chip might well convince you that l.e.d.s are not so bad after all!

Well, you know what I was going to say next, didn't you. Yes, somebody has gone out and done it all for us again, a complete multiplexed BCD input, to decoded seven segment I.c.d. output display system on a single chip. Hughes Microelectronics are the people to blame, and the device in

question is the **H.L.C.D.** 0024 which is made using CMOS technology and lives in a 40 pin plastics package.

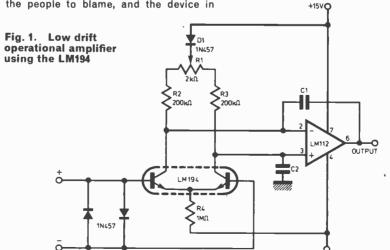
On its inputs, the H.L.C.D. 0024 talks directly to the BCD and digit strobes produced by most clock and voltmeter chips, on its outputs, it speaks parallel seven segment a.c. drive liquid crystal. Two extra uncommitted drivers are available for use with plus/minus signs, decimal points or a.m. p.m. displays, and leading digit zero blanking is provided internally.

THE PERFECT COUPLE

I remember spending hours with an AVO transistor analyser and a few dozen OC29 germanium power transistors trying to get a matched pair for use in an audio amplifier output stage. Well, I'm not sure that it was much help in the end, but I enjoyed myself anyway, there is something rather satisfying.

As a close approach to the perfect matched pair, National now produce the LM194 "Supermatch pair" which consists of two monolithic *npn* silicon transistors in a TO5 metal can. The emitter-base voltage match is within 50 microvolts, the current gain match to within 1 per cent, and the offset drift is less than 0-1 micro volts per degree C which as far as I remember, is a hell of a lot better than I was able to do with my OC29s!

Match pairs such as the LM194 are useful where extremely high performance operational amplifiers or high accuracy analogue multipliers must be assembled.



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So thin is undetectable under
carpet but will switch on with
slightest pressure. For burglar
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and twin stetho-set.
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MULTISPEED MOTORS
Six speeds are available 500, 850 and 1,000 r.p.m. and 7,000, 9,000 and 11,000 r.p.m. Shaft is \(\frac{1}{2}\) in diameter and approximately \(\frac{1}{2}\) in long, 230/240/ its speed may be further controlled with the use of our Thyristor controller. Very powerful and useful motor size approx. 2 in dia. x5 in long. Price \(\frac{1}{2}\) including post and VAT.



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Monthly list available free, send
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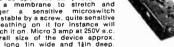
BLACK LIGHT

As used in disco's and stage effects etc.—virtually no white light appears until rays impinge on white collars and cuffs etc.—we offer mains B.L. lamps, 175 watts plugs into any lamp holder requires no choke or control gear price £7 + 95p post saand VAT or for glamorising rock specimens, looking for watermarks etc. 8 9in 6 watt tube with starter, choke lamp holds, etc. all for £4-50 post and VAT pald.

NEED A SPECIAL SWITCH
Double lead contact. Very slight pressure, closes both
contacts 12p each... Plastic pushrod supplied for operating. 10p
each. 10 for 68p.

HUMIDITY SWITCH

HUMIDITY SWITCH
American made by Ranco, their type
No. J11. The action of this device
depends upon the dampness causing a membrane to stretch and
trigger a sensitive microswitch
adjustable by a screw, quite sensitive
—breathing on it for instance will
switch it on. Micro 3 amp at 250 v. c.
Overall size of the device approx.
3\(\frac{3}{2}\)in long 1in wide and 1\(\frac{3}{2}\)in deep.
6\(\frac{5}{2}\).



PP3/PP9 REPLACEMENT MAINS UNIT

MAINS UNIT
Japanese made in plastic container
with leads size Zin × 1½in × 1½in, this
is ideal to power a calculator
or radio, litt has a full wave rectified and
smoothed output of 9% suitable for
loading of up to 100mA. £2-53.



MULLARD UNILEX

MULLARD UNILEX
A mains operated 4+4
stereo system. Rated one
of the finest performers
In the stereo field this
would make a wonderful gift
for almost any one in easy-toassemble modular form and
complete with a pair of
Plessey speakers this should sell at about £30—but
due to a special bulk buy and as an incentive for you to
buy this month we offer the system complete at only £14
including VAT and postage.

SHORTWAVE CRYSTAL SET

Although this uses no battery it gives really amazing results. You will receive an amazing assortment of stations over the 19, 25, 29, 31 metre bands. Kit contains chassis, front panel and all the parts £1-90 —crystal earphone 55p including VAT and postage. VAT and postage



DISTRIBUTION PANELS



Just what you need for work bench or lab. 4 x 13 amp sockets in metal box to take standard 13 amp fused plugs and on/off switch with neon warning light. Supplied complete with 6 feet of flex cable. Wired up ready to work.

25A ELECTRIC PROGRAMMER



25A ELECTRIC PROGRAMMER

Learn in your sleep, Have radio playing and kettle boiling as you wake—switch on lights to ward off intruders—have a warm house to come home to. All these and many other things you can do if you invest in an electrical programmer. Clock by famous maker with 15 amp. on/off set anywhere to stay on up to 6 hours. Independent 60 minute memory jogger. A beautiful unit. Price 12:95. VAT and postage 60p. or with glass front, chrome bezel, 11:50 extra.

WINDSCREEN WIPER CONTROL

Vary speed of your wiper to sult conditions. All parts and instructions to make. £3-75 post and VAT paid.



THIS MONTH'S SNIP

Breakdown Parcel—four unused, made for computer units containing most useful components and these components unlike those from most computer panels, have wire ends and of useable length. The transistors for instance have leads over 1in long—the diodes have jin leads.

List of the major components is as follows: 17 assorted transistors; 38 assorted diodes; 60 assorted resistors and condensers; 4 gold plated plugs in units which can serve as multipin plugs or as hook up boards for experimental or quickly changed circuits (note we can supply the socket boards which were made to receive these units). The price of this four units parcel is 1 including VAT and post (considerably less than value of the transistor or diodes alone).DON T MISS THIS SPLENDID OFFER.

MOTORISED DISCO SWITCH

MOTORISED DISCO SW
With six 10 amp changeover
switches. Multi adjustable
switches are rated at 10 amp
each so a total of 200W can be
controlled and this would
provide a magnificent display. For mains operating
£4.25 post and VAT paid.
Ditto 9 switch £4.95 post and
VAT paid. Ditto but 12 switch
£5.75 post and VAT paid.



8 POWERFUL **BATTERY MOTORS**

For models, Meccano's, drills, remote control planes, boats, etc. £2.



ROTARY PUMP



Self priming, portable, fits drill or electric motor, pumps up to 200 gallons per hour depending upon revs. Virtually uncorrodable, use to suck water, oil, petrol, fertilizer, chemicals, anything liquid. Hose connectors each end. £2 post paid.

MERCURY BATTERIES

MERCURY BATTERIES
Bank of 7 Mercury cells
type 625 which are apport. In diameter by ∮in
thick in plastic tube
giving a total of 10 7V.
Being in a plastic tube it is
very easy to break up the battery
into separate cells and use these for
radio control and similar equipment.
Carton of 25 batteries £1-80.



MICRO AMPLIFIER Ex behind the ear dear alds, complete with volume control \$2.16

TERMS.

Cash with order—under £6 must add 50p to offset packing etc. BULK ENQUIRIES INVITED. Tel: 01-688 1833.

J. BULL (ELECTRICAL) LTD

(Dept. PE), 103 TAMWORTH RD. **CROYDON CR9 1SG**

IT'S FREE

II 'S PMEE Our monthly Advance Advertising Bargeins List gives details of bargeins arriving or just arrived—often bargeins which sell out before our advertisement can appear—it's an interesting list and it's free—just send S.A.E. Blow are a few of the Bargeins still available from previous lines.

Mullard Audio Ampliflers

Mullard Audio Ampliflers
All in module form, each ready built complete with heat
sinks and connection tags, data supplied. Model 1153
500mW power output £1-50 including Post & VAT.
Model 1172 I'W power output £1-85
including Post & VAT.
Model EP9000 4 watt power output
£2-90 Including Post & VAT. EP
9001 twin channel or stereo preamp. £2-90 including Post & VAT.

Room Thermostat Famous Satchwell, elegant design, intended for wall mounting. Will switch up to 20 amps at mains voltage. Covers the range 0-30°C. Special snip this month £2-50, post and VAT paid.



Mains Transformer upright mounting with top tagboard primary 0–115, 210, 240, two secondaries 115 volts 5mA. and 8-5 volt 1 25A. Note this transformer is ex-new equipment. Price £2 + 16p. Post 30p + 2p.

Mains Transformer, primary 0-110, 127, 150, 180, 220. Secondaries (1) 3, 15-0-3, 15 (2) 2-5V, (3) 0-220V. Fitted primary screen. This is a 30W transformer, ex equipment £2-50 + 20p. Post 40p + 3p.

Ferric Chloride Crystals, for etching copper, making printed circuit boards, etc. Special purchase anables us to offer this in 11b bags at 50p + 4p. Post 20p + 2p.

Read Relay with double wound coll 12 volts one coil will close the read switch. 12 volts on the other coil will open the contact or still further close it depending upon whether the current is opposing or assisting. Price £1-50 + 12p. Post 20p + 2p.

Relay, Clare Elliott 670 ohm. Coil sealed in metal can size approx. $\frac{1}{2}$ in by $\frac{1}{2}$ in two pairs of changeover contacts. This type of relay is mounted by its own leads. £1 + 8p.

Desk Instrument Case with sloping front, overall size of sloping front is 4in wide and 5in long. Mounted on a heavy base for stability, base size 4in x 4in with flex lock. The heavy base is easily removed if not required. The average depth below sloping panel 3in approx. Price £1-50 + 12p. Post 50p + 4p. Note the sloping front will be supplied with each of these cases but this already has quite a lot of holes in it, however, it is a simple matter to cut and bend new aluminium front if you use this as a pattern.

Remember 7029. We are rapidly running out of this and if you have not put any into stock then this could well be your last chance. The price for 100 metre coil £9-50 + 76p. Carriage £2-50 + 20p.

carriage £2 50 + 20p.

Engine Revolution Counter. This is ex-Air Ministry litem, beautifully made. As a revolution counter it is driven by a flexible shaft and having a permanent magnet field the voltage output would be dependent upon the speed. Of course it will also run as a low voltage d.c. motor and its speed will be dependent upon the applied voltage. This is dustproof and almost waterproof so it will still run in adverse conditions. One point however, is there are no brushes fitted to these motors, these are special and as yet we have not been able to find a supplier, so you will buy without brushes. The Air Ministry ref. number of the motor is 6A/7A2. We would like to heaf from any customer who met this during his service career and who knows of a possible source of brushes. Price £2 + 18p. Post 40p + 4p.

Nicad Battery Charger in neat plastic case size $4 \pm n \times 3 \pm n \times 2 \pm n$ approx. with mains input lead and charging output lead terminated with din plug. This is a dual output charger but contains useful mains transformer which makes it easily adaptable for many voltage cells. If not wanted as a charger could very easily be rebuilt as a power unit for receiver or other device. The plastic case has a neon indicator. Price \$2:50 + 20p. Post 40p + 4p.

7 Digital Counter. Another special purchase enables us to 7 Digital Counter. Another special purchase enables us to offer this mains-operated counter for only about a quarter of its proper price. It works off 240V 50Hz mains and requires no step down. There is only one point about this—it counts in even numbers only 2. 4, 6, 8, 10, etc. If you want to count single you must divide the final figure by 2. Price 50p + 4p. Post 10p + 1p.

Garrard 4 Pole Motor, probably made for record player or tape recorder, this is 140V 40-60 cycle. We do not know the Garrard ref. no. but the figure 12 is pressed on the bottom bearing cover. Price 22 + 25p. Post 30p + 4p.

Simmerstat by Sunvic for 2500 watts Sunvic ref. 230707/10776. This is a larger than usual simmerstat dimensions approx. 2½in square by 2½in deep. Price 11:50 + 12p. Post 20p + 2p.

Flash Ernle is the name we have given to our latest disco light display because it is a random flasher and is very effective especially with coloured bulbs. Kit consists of motorised stud switch, master control switch, anti spark caps, 9 lamp holders, connecting wire and wiring diagram. Price £5 + 40p. Post 60p + 6p.

Car Cassette Power Kit. This has a stabilised output of 6V, 9V or 12V—this kit consists of transistors—zener, diode and all resistors and condensers, case, and data price is only \$2-80 including post and VAT.

Burglar Alarm—The heart of many of these is an infra red beam operated switch—and we offer a bit to make this switch complete with relay from latching and sounding alarm bell—this can also be used for door opening—counting light or dark switching etc., but consists of photo cell—relay, all resistors and condensers and constructional data only \$2.25 including post and VAT.

Emergency Light. Works from mains but automatically switches to battery should mains fail—with this your place never will be in darkness—uses PP9 battery (not supplied) otherwise complete kit with data £3-30 including post and VAT. Wall or ceiling mounting case £1-50 extra.

Stereo Gram Cabinets. Long, low, modern teak-veneered cabinet, size approximately 4ft 2ln by 15ft 5in. Probable cost to make today over £20. We have a few of these, they are slightly second, at prices ranging from £5 each, depending on condition—sorry but these are for callers only.

B. BAMBER ELECTRONICS

Dept PE. 5 STATION ROAD, LITTLEPORT, CAMBS., CB6 1QE Telephone: ELY (0353) 860185 (2 lines) Tuesday to Saturday

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18V DC RELAYS, 4 pole change-over (double contacts) (will work from 14-24V DC). Brand New, boxed, good quality, made by AEI 40p each

Slider Switches, 2 pole make and break (or can be used as 1 pole change-over by linking the two centre pins), 4 for 50p.

Smart Min. Rectangular Push to Make Switches, black rectangular surround with white rectangular button, overall size 12 × 17mm, 3 for 500.

NEW RANGE OF QUALITY BOXES &

Aluminiu	m Boxes with Lids.	
AB10	5½ × 4 × 1¾	60p
AB13	6 × 4 × 2	80 p
AB14	7 × 5 × 21	£1-00
AB15	8 × 6 × 3	£1-30
AB16	10 × 7 × 3	£1-50
AB17	10 × 4½ × 3	£1 ⋅ 30
AB25	6 × 4 × 3	£1 - 00

Vinyl Costed Instrument Cases

MACHETIC	DEVICES	DROODA	AMERIC C
WB853	8 × 5∤	× 3 [‡]	£2·00
WB7	12 × 61		£2 · 60
WB6	11 × 7‡		£2 · 25
WB5	.11 × 61		£2 ⋅ 00
WB4	9 × 51		£1-80
WB3	8 × 5		£1-60
WB2	6 × 41		£1·10
WB1	5 × 21		60p
smart flinis	h.		sections. Very

MAGNETIC DEVICES PROGRAMMERS. Contain 9 fully adjustable cams and 9 change over micro-switches (rated approx. 1A at 240VAC) Needs slow-motion motor to drive (not supplied), Ideal for disco lights, sequence switching, etc.

CALIBRATOR XTALS 100kHz + 1MHz in one 10-X can, £1-00 each.

MAINS TRANSFORMERS. Type 60/2, Mains input 200-210-220-230-240-250V a.c., output 0-20-40-60V at 2A, in Metal and Plastic case, approx. 7½ × 4½ × 4, fully fused (ideal for PSU) £3-00 each

MAINS TRANSFORMERS. Type 15/300 240V input, 15V at 300mA output, £1-50 each.

MAINS TRANSFORMERS. Type 45/100, 240, 220, 110, 20, 0V Input, 45V at 100mA output, £1-50

RED LEDs (Min. type) 5 for 70p.

VIDICON SCAN COILS (Transistor type, but no data) complete with vidicon base £8-50 each. Brand New.

FULL RANGE OF BERNARDS/BABANI ELECTRONICS BOOKS IN STOCK, S.A.E. FOR

NEW FOR THE VHF CONSTRUCTOR. A range of

parallel.
Type S (‡In. square, dumpy type).
Type SA 20 to 30MHz (when 33pf fitted in parallel).
Type SB 35 to 50MHz (with link winding).
Type SC 70 to 100MHz (with link winding).
Type SD 135 to 175MHz (with link winding)

Type SD 135 to 175MHz (with link winding) Type M (Min., jin. square types). Type MA 19 to 28MHz (when 33pf fitted in parallel). Type MB 25 to 32MHz (when 33pf fitted in parallel). Type MB 25 to 33MHz (when 33pf fitted in parallel). Type MD 38 to 50MHz (when 33pf fitted in parallel). Type MD 38 to 50MHz (when 33pf fitted in parallel). Type MF 100 to 200MHz (without slug) when 0 to 30pF variable fitted in parallel. All the above coils available in packs of five only (same type) at 50p per pack of 5.

PLASTIC PROJECT BOXES with screw on Ilds (In black ABS) with brass inserts. Type NB1 approx 3in, x 2jin, x 1jin, 40p each. Type NB2 approx. 3jin, x 2jin, x 1jin, 50p each. Type NB3 approx. 4jin, x 3jin, x 1jin, 60p each.

MULLARD 85A2 85V STABILISER VALVES (Brand New) 70p each or 2 for £1 -20

TO3 transistor insulator sets, 10 for 50p

BSX20 (VHF Osc/Mult), 3 for \$9p.
BC108 (metal can), 4 for \$9p.
BC108 (separate can), 5 for \$9p.
BC108 (separate can), 5 for \$9p.
BC108 (separate can), 5 for \$9p.
BC172 Transistors, 4 for \$9p.
RNP audio type TOS Transistors, 12 for 25p.
BF152 (UHF amp/mixer), 3 for \$9p.
BC168 RNP SILICON, 4 for \$0p.
BC168 RNP SILICON, 4 for \$0p.
BC168 RNP SILICON, 4 for \$0p.
BC318 Signal Diodes, 10 for \$3p.
BA313 Signal Diodes, 10 for \$5p.
BA121 Varicap Diodes, 4 for \$0p.

PLEASE ADD 8% VAT UNLESS OTHERWISE STATED

741CG op amps by RCA, 4 for £1.

PERSPEX TUNER PANELS (for FM Band 2 tuners) marked 88-108MHz and Channels 0-70, clear numbers, rest blacked out, smart modern appearance, size approx. 8‡in x 1‡in., 2 for 35p.

PLUGS AND SOCKETS

N-Type Plugs 50 ohm, 80p each, 3 for £1-50.
PL259 Plugs (PTFE), brand new, packed with reducers, \$5p each.
SO239 Sockets (PTFE), brand new (4-hole fixing type). 50p each.

SOLDER SUCKERS (Plunger type). Standard Model, £5. Skirted Model £5-50. Spare Nozzles 60p each.

WELLER SOLDERING IRONS
EXPERT. Bullt-in-spotlight Illuminates work.
Pistol grip with fingertip trigger. High efficiency
copper soldering tin.

copper soldering tip.

EXPERT SOLDER GUN \$100D t9-90.

EXPERT SOLDER GUN KIT (spare bits, case, etc.) £12-90.

Spare bits 35p pair.

NEW MARKSMAN RANGE OF SOLDERING

S115D 15W 240V £3-80. S125D 25W 240V £3-80. S1250 25W 240V t3-80.
S140D 40W 240V t4-20.
S125DK 25W 240V + bits etc., KIT £4-90.
S125DK 25W 240V + bits etc., KIT £4-90.
SPECIAL 12V version S125-12 25W 12V £3-80.
BENCH STAND with spring and sponge for Marksman irons £2-38.
Spare bits MT9 (for 15W) 50p, MT5 (for 25W) 45p, MT10 (for 40W) 50p, ALL PRICES + 9% VAT.
TCP2 TEMPERATURE CONTROLLED IRON.
Temperature controlled iron and PSU, £30 + VAT. (£2-40).

SPARE TIPS
Type CC single flat, Type K double flat fine tip,
Type P, very fine tip. £1 each + VAT (8p).
MOST SPARES AVAILABLE.

MULTICORE SOLDER

MULTICORE SOLDER
Size 5 Savbit 18 s.w.g. in alloy dispenser,
32p + VAT (3p).
Size C1SAV18 Savbit 18 s.w.g., 58p + VAT (4p).

Kg. (1, 1lb) 50 × 40, 20 s.w.g. on plastic reel

14 DIL REED RELAYS, 5 to 12V DC, 450 ohm coil Designed to work directly from TTL Logic, Single Pole Change over. Gontact ratings 28V +A 3W, £1-75 each.

A LARGE RANGE OF CAPACITORS AVAILABLE AT BARGAIN PRICES, S.A.E. FOR LIST.

MIXED COMPONENT PACKS, containing resistors, capacitors, pots, etc. All new. Hundreds of items. £2 per pack, while stocks

ALU-BOL ALUMINIUM SOLDER (made by Multicore). Solders aluminium to itself or copper, brass, steel, nickel or tinplate, 16 s.w.g. with multicore flux, with instructions, Approx. 1 metre coil 40p pack. Large reel £2-75.

VARICAP TUNERS Mullard type ELC1043/05. Brand New, £4-40 + 121 % VAT.

BARGAIN PACK OF LOW VOLTAGE ELECTROLYTIC CAPACITORS. Up to 50V working Seatronic Manufacture. Approx. 100. £1-50 per pack + 12½% VAT.

OSMOR REED RELAY COILS (for reed relays up to ‡in dia., not supplied) 12V, 500 ohm coil, 2 for 50p.

We now stock Spiraiux Tools for the electronic enthusiast. Screwdrivers, Nut spanners, BA and Metric sizes, pop rivet guns, etc. S.A.E. for list.

TWIN 1.F. CANS, approx. 1In. × Iin. × Iin. high, around 3-5-5MHz, 2 separate transformers in 1 can, internally screened, 5 for 50p + 12½% VAT.

Dubiller Electrolytics, 50µF, 450V. 2 for 50p. Dubiller Electrolytics, 100µF, 275V, 2 for 50p. Plessey Electrolytics, 470µF, 63V, 3 for 50p. TCC Electrolytics, 1000µF, 30V, 3 for 60p. Dubliler Electrolytics, 1000µF, 30V, 3 for 60p.
Dubliler Electrolytics, 5000µF, 50V, 90p each.
Dubliler Electrolytics, 5000µF, 50V, 60p each.
ITT Electrolytics, 5600µF, 25V, high grade, screw terminals, with mounting clips, 50p each.
PLEASE ADD 12½% VAT TO ALL CAPACITORS. TO ALL

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TV Plugs (metal type), 4 for 50p.
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TV Line Connectors (back-to-back sockets), 4 for

50p. Please add 12½% VAT.

Terms of Business: CASH WITH ORDER. MINIMUM ORDER 12. ALL PRICES INCLUDE POST & PACKING (UK ONLY). SAE with ALL ENQUIRIES Please. PLEASE ADD VAT AS SHOWN: ALL GOODS IN STOCK DESPATCHED BY RETURN. CALLERS WELCOME BY APPOINTMENT ONLY.

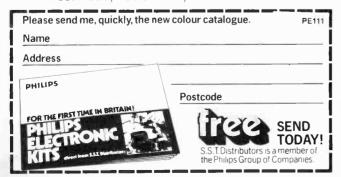
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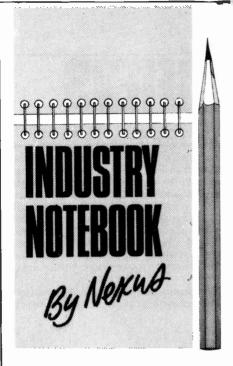
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DIGITAL INSTRUMENTS

The digital instrument market is becoming even more competitive. Never has so much been offered by so many companies, and prices are still tumbling. For any price range there is better value in specifications and facilities and you can now get a professional quality instrument for £100. Even that troublesome measurement of true r.m.s. can be yours for £150.

The dilemma facing the manufacturers is whether to cut prices to the bone or hold them and build in more performance for the money. Those taking the middle course are giving their instruments an enhanced performance with a modest price cut.

In the scramble to present instruments in the best possible light there are some big claims being made. The thing to remember is that even with the latest LSI techniques which cut instrument assembly costs, long term accuracy still costs money. If you go for price alone, don't expect too much. And prices, as advertised, can be misleading. One instrument, for example, looks world-beating value with a boldly displayed price tag of under £50. But with carrying case and accessories, plus value-added tax, you can end up paying over £60.

The new trend is towards liquid crystal displays and smaller and smarter cases. For sheer smallness there is one digital multimeter on the market which measures 48mm × 68.5mm × 99mm. It has a 7.5mm l.e.d. display described as "big".

Another model has its rear moulded to conform to the wrist and back of the hand so it can be strapped on like a wrist watch. The idea is that you can work with both hands probing a circuit and right there in front of you on your wrist is the voltage or current or resistance read-out, this one with i.c.d. Another variation on the same

theme is for the whole of the multimeter to be built into the test probe.

In the UK it is estimated that over 60 per cent of low cost and general purpose digital instruments are now sold through instrument distributors as off-the-shelf items. And when you see that a digital panel meter can be bought in one-off quantities for as little as £25 you can understand the reason why.

DISPLAYS

Electronic displays have become an industry within an industry with their own specialised exhibition and conference in London extending over three days. The displays sector of the electronics market is currently expanding at 25 per cent per year.

For sheer volume the calculator, clock and watch makers are the leading customers consuming billions of digits per year. The next huge market breakthrough, somewhat delayed but beginning to materialise, is the automotive market world-wide. The oldest form of electronic display of all, the cathode ray tube, has been given a new lease of life by the enormous growth of computer graphics and visual display units.

The problem of l.c.d.s being rather drab compared with l.e.d.s looks like being solved by a fluorescence activated l.c.d. developed by the West German Institute of Applied Solid State Physics. The new technique is said to give l.c.d.s comparable brilliance to l.e.d.s and a bonus is that a choice of colours in red, green or orange will be available. The product will be mass-produced by Siemens next year.

LOBBIES

Pressure groups, lobbies, call them what you will, multiply like bacteria. Do they do any good or do they neutralise themselves? I note that the anti-Far East electronics lobby is now counterbalanced by the International Consumer Electronics Association which represents importers and distributors of electronic goods from overseas including the powerful Japanese companies. ICEA members fear for the safety of their incomes if imports are restricted.

In all the sometimes secret, sometimes public wrangling, the poor old consumer often gets forgotten. The one irrefutable argument is that if the Japanese or any other nation can produce a better product at a cheaper price surely the man-in-the-street should be given the choice of buying it. Meanwhile, the free-traders and the protectionists seem to be winning.

The other great battle between lobbyists is the vexed question of Citizen's Band Radio. A statement released from the office of the Prime Minister concludes with, "It is a question of balance, and at present the Government feel that the balance of the argument is against the introduction of Citizen's Band".

The operative words are "at present", so this leaves the door slightly ajar and the respective lobbies will battle on, each hoping for final victory.

SAFETY FIRST

The "Earth Leakage Circuit Breaker" (ELCB) described by K. A. Smith in the July 1977 issue of P.E. seems to have aroused a lot of interest including a word of warning in our correspondence columns.

On the professional front B & R Relays have been making them for years. But it has been a long uphill struggle getting the sales message across to potential users. Everybody wants safety but when it comes to the point, few want to pay for it.

The Health and Safety at Work Act of 1975 is beginning to change the situation and now Kevin Walker, B & R's sales manager, is forecasting an immediate UK market of about £1 million rising to £5 million or more by 1980. B & R are expecting to capture 25 per cent of the business.

Walker has made a good start by selling £60,000 worth of ELCB's to Watney Mann to protect the barmen and barmaids against faults on electric beer pumps in the Watney Mann chain of pubs. The next move will possibly be to fit them to the catering equipment in pubs.

They are currently working on six new models of ELCB's, all designed for ease of fit and designed to trip within 25 milliseconds of detection of a fault.

I note that K. A. Smith says that his intention was to fit a commercial model in his colour processing darkroom—"but the frustration of trying to buy such an article for private use made me determined to make one for myself". Anyone interested in buying the commercial product could try contacting B & R Relays, Temple Fields, Harlow, Essex.

BPO BLOODHOUNDS

The Post Office's Radio Interference Service which includes a fleet of specially equipped vehicles to sniff out illegal transmissions, man-made static and other forms of interference to radio and TV reception is in process of modernisation.

The Marconi Instruments and Racal Instruments are among the firms which will benefit. MI is supplying 94 type TF2015 signal generators and RI a similar number of their type 9915 frequency meters.

The controlling authority for the Service is the Home Office so the technical requirement was drawn up by the Home Office's Directorate of Radio Technology. Both companies are delighted that their products passed evaluation tests with flying colours.

ANALOGUE / LOG AMPLIFIERS

D. F. BOWERS, BSc

OST voltage amplifiers in present use are designed to have a linear transfer characteristic—in other words, to multiply the voltage at the input by a fixed factor—and to have well-defined impedances at the input and output. There are, however, amplifiers which are termed "non-linear", which multiply input voltages by a factor in some way dependent on the magnitude of the input voltage.

Many non-linear amplifiers are designed for specialist applications, but certain types which have more general transfer characteristics are useful in wider fields. In the latter category, one of the most interesting is an amplifier having

a logarithmic or exponential transfer characteristic.

Because many sensing devices obey exponential laws (thermistors and photodiodes, for example), logarithmic amplifiers find uses here. Compression of a wide range of voltages into a more easily handled spread is also a common use of logarithmic amplifiers. In analogue computers, they are used in conjunction with exponential amplifiers to perform multiplication and division.

WHAT IS A LOGARITHMIC AMPLIFIER?

If an amplifier has input voltage V_{in} and output voltage V_{out} , and if $V_{out} \propto \log(V_{in})$, then the amplifier is said to be a logarithmic amplifier. If $V_{out} \propto \exp(V_{in})$, $[\exp(V_{in}) = e(V_{in})]$ or $\log(V_{out}) \propto V_{in}$, then the amplifier is said to be exponential or antilogarithmic.

A logarithmic amplifier in the feedback path of an operational amplifier converts the op. amp. into an exponential amplifier. Similarly an op. amp. with an exponential amplifier in its feedback path becomes a logarithmic amplifier. Hence, we need only find a way of achieving one type of transfer to

create both types of amplifier.

SHOCKLEY'S EQUATION

Although very expensive logarithmic amplifiers may use intermediate digital techniques, the vast majority of analogue logarithmic amplifiers rely on the intrinsic logarithmic behaviour of a semiconductor p-n junction when subjected to low bias voltages.

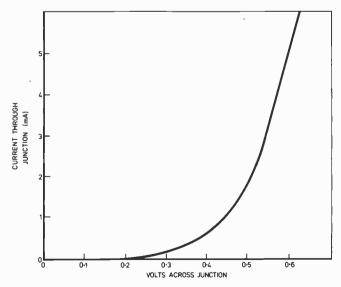


Fig. 1. Forward bias current curve for a typical silicon diode

The familiar transfer curve for a typical silicon diode in the forward bias mode is shown in Fig. 1. As the voltage across the diode increases from zero to about half a volt, very little current flows, but above about 0.6V the current increases rapidly. The inverse of this curve is shown in Fig. 2, where it can be seen that the voltage across the diode increases rapidly as the current approaches l_0 , and then more slowly until several milliamps is achieved, when the diode's bulk resistance becomes important. Between these two current values, the voltage increases (approximately) in proportion to the logarithm of the current.

To explain this, it is necessary to investigate an equation derived from statistical considerations by W. Shockley, which

 $1 = I_0 \left(\exp \left(\frac{qV}{kT} \right) + 1 \right) \dots (1)$

where

1 = Current through junction (amps)

l_o=Theoretical reverse current (amps)

(This is the same Io as previously described)

. V = Voltage across junction (volts)

q = Charge on the electron (coulombs)

k = Boltzmann's constant

T=Junction temperature (kelvin)

If qv > kT, a condition normally satisfied, then:

$$V = \frac{kT}{q} (ln \ l - ln \ l_0) \dots (2)$$

(where In=log_e=the natural or Naperian logarithm)

and hence we obtain logarithmic behaviour. Departure from this equation is mainly due to qV approaching kT at low currents, to the effect of the bulk resistance at high currents, and to misbehaviour of the semiconductor junction in between.

The latter problem can be solved to some extent by using diodes designed to have a good logarithmic behaviour (such as type G130), but not very much can be done to better the

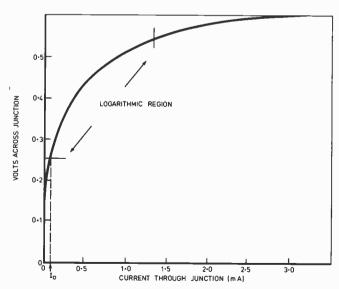


Fig. 2. Forward bias voltage curve for a typical silicon diode



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extremes. Even so, a range of over seven decades of current can be accommodated if great care is taken in the design of the logarithmic amplifier.

SIMPLE LOGARITHMIC AMPLIFIERS

A simple logarithmic amplifier based on the principles described is shown in Fig. 3. Assuming a positive input signal, the inverting input of the op. amp. will be maintained at virtual earth (by normal feedback action), and so the input current is Vin/R. This current must also flow through the diode, and hence we can show that:

$$\begin{split} V_{out} &= -(\ln\frac{V_{in}}{R} - \ln\,I_o)\,\frac{kT}{q} \\ &= -(\ln\,V_{in} - \ln\,R - \ln\,I_o)\,\frac{kT}{q} \ldots \ldots (3) \end{split}$$

Thus there is a region where (at constant temperature) the output is proportional to the logarithm of the input. In this region, the output moves about 60mV (at 25°C) for every decade change in input voltage, but this can be increased by using several diodes in series. The main drawback of this arrangement, however, is temperature dependence.

Besides the kT/q term outside the brackets, the term Io is also very dependent on temperature, and on the physical construction of the junction. It effectively causes the output level to shift up and down with small fluctuations in temperature. Although this can be corrected with simple amplifiers of this type, it is more common to replace the diode with a transistor, the base-emitter junction being used as the logarithmic law generator. A "differential" compensation method is then relatively simple to implement. Details of a practical amplifier will now be given, for the benefit of those who may wish to experiment.

A COMPENSATED LOGARITHMIC AMPLIFIER

Although the temperature problems can be solved by the junction to keep it at a constant temperature "ovening" (as in the G. D. Shaw monolithic oven used in the PE Sound Synthesiser), this arrangement is not always satisfactory, and can be difficult to set up. We will therefore explore an alternative system.

If qV≫kT, then the relationship between the collector current (Ic) and base-emitter voltage (VBE) of a transistor will be:

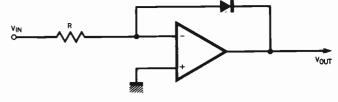


Fig. 3. Simple logarithmic amplifier using the properties of a silicon diode

and for two identical transistors operating at different collector currents, the difference in $V_{\rm BE}$ ($\stackrel{.}{\triangle}V_{\rm BE}$) will therefore be:

$$\triangle V_{BE} = -\frac{kT}{q} \, ln \! \left(\! \frac{I_{c_1}}{I_{c_2}} \! \right) \ldots \ldots \text{(5)} \label{eq:delta_beta}$$

Note that the troublesome I₀ plays no part in this relation.

A practical amplifier based upon this principle is shown in Fig. 4. Transistors TR1 and TR2 should be a thermally connected matched pair, or preferably a dual transistor (such as type MD8001).

The potential at TR2 collector is equal to $\triangle V_{BE}$ since the collector of TR1 is held at virtual earth.

 $V_{out} = -\frac{R_1R_2}{R_2} \frac{kT}{q} \ln \frac{I_{in}}{I_{ref}} \dots (6)$

This again gives 60mV/decade × gain of IC2, and by adjustment of VR2, the output can be set between 0.75V/decade and 2.3V/decade.

SETTING UP PROCEDURE

First, the value of Rin must be fixed. Since our upper current limit is 1mA (by bulk resistance considerations), then $R_{in} = V_{max}/1$ in kilohms. In this case, V_{max} is the largest input voltage to be accommodated. Next, a temporary resistor of about 10 kilohms should be connected between pins 2 and 6 of IC1 and (with no input) VR1 adjusted to give precisely zero volts at the output of IC1.

Remove the temporary resistor and set V_{in} so that 1mA flows through Rin. Adjust VR4 so that 1mA flows through R_{ref}, then adjust VR3 to give zero volts at pin 6 of IC2. Next set V_{in} so that 100 µA flows through R_{in}. Adjust VR2 to give 1V at IC2 output (for a 1V/decade scale factor), or 2V at IC2 output (for a 2V/decade scale factor). The amplifier is now ready for use.

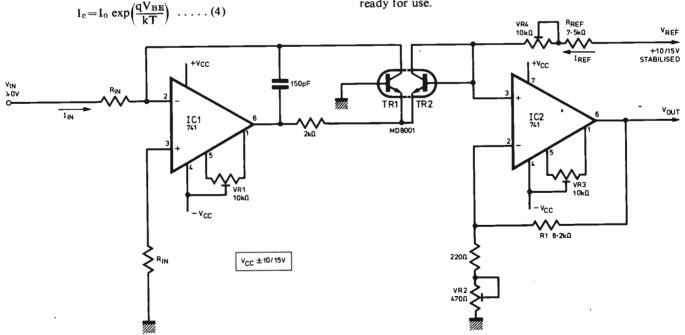


Fig. 4. Practical logarithmic amplifier utilising the differential compensation technique

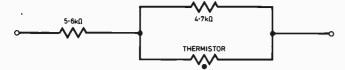


Fig. 5. Thermistor compensation circuit to be used in place of R1 in Fig. 4. The thermistor should have a resistance of 10k $\Omega_{\rm c}$ at 25°C

AN IMPROVED AMPLIFIER

The form of logarithmic amplifier described above has three major drawbacks which limit its overall performance.

1. The dynamic range is limited to about three decades of input voltage, due largely to the relatively high input offset (about 2mV) and bias current (about 100nA) of IC1.

The former can be improved by using as large an input signal as possible, together with a high value for R_{in}. To improve the latter, however, an f.e.t.-input op. amp. (such as the NE536T) should replace IC1. It should be possible to achieve over six decades range with this configuration.

2. The current $I_{\rm ref}$ does not remain constant, because the non-inverting input of IC2 is not a true virtual earth. This is not too important with power supplies in the range 10–15 volts, but for greater accuracy $V_{\rm ref}$ and $R_{\rm ref}$ could be replaced by a 1mA current source.

3. Last, but not least, the kT/q term in equation (5) introduces a temperature dependence. This causes the scale factor to alter with variations in absolute temperature. The error over normal domestic temperature variations will not exceed about ± 2.5 per cent, which will be adequate for many applications.

Special temperature proportional resistors have been developed to compensate for this error over wide temperature ranges, but these are neither easy to obtain, nor cheap. In Fig. 5 is shown a method of compensation using a resistor-thermistor network in place of R1 in Fig. 4. This circuit was designed by a colleague, Mr C. R. Francis of Sheffield University, and provides good compensation over the limited temperature range of a domestic environment, if greater accuracy is required.

EXPONENTIAL AMPLIFIER

To obtain an exponential amplifier, it is only necessary to rearrange the components of Fig. 4, as shown in Fig. 6. If V_{max} is the maximum output voltage, then $I_{out} = V_{max}/1k\Omega$. Potentiometer VR5 is adjusted to give $V_{out} = V_{max}$ when V_{in} is zero, and VR2 again sets the scale factor, which is adjustable over the range 0.43 decades/volt to 1.33 decades/volt.

INTEGRATED CIRCUIT TECHNIQUES

The amplifier system described, with its need for closely matched transistors and good op. amps., would seem a good subject for integration, and indeed this has been done by several manufacturers. Unfortunately, i.c. logarithmic amplifiers of good quality are not very cheap, but two which have proved to be good all-round performers are the Intersil 8048 (logarithmic) and 8049 (exponential) amplifiers.

The configuration of these amplifiers is basically a monolithic version of those already described, with dual f.e.t.-input op. amps. Fine temperature compensation is carried by means of a specially designed thin film resistor instead of the resistor-thermistor network, and this is effective from 0°C to 70°C. The 8048 features a 60dB voltage input range, and a 120dB current input range.

BANDWIDTH CONSIDERATIONS

Bandwidth is always a problem where semiconductor junctions operate at low currents, due to capacitive phenomena across the narrow junction. To a first approximation, the bandwith of a logarithmic amplifier will increase proportionately to the average current through the junction concerned, assuming that the perturbations are small.

It follows that to obtain the best frequency response from a logarithmic amplifier, it should be used over the upper section of its input range. Even so, it is difficult to obtain a -3dB bandwidth past 100kHz over three decades. Over five decades, the -3dB point may well be only a few kilohertz. For large fluctuations of input signal the situation is even worse, and usually less predictable.

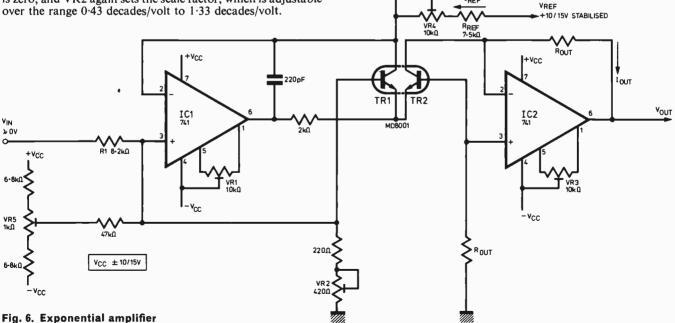
CONCLUSION

Although logarithmic circuits are not the easiest to implement, a good quality logarithmic amplifier is not over difficult to make, provided care is taken in the setting up process. It is hoped that this article will have provided a useful introduction to the subject.

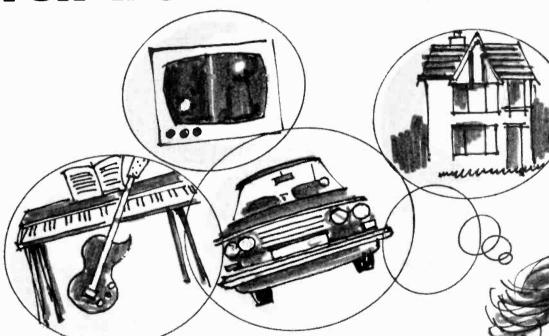
ACKNOWLEDGEMENTS

Thanks are due to Mr W. Gibbons and Mr C. R. Francis, both of Sheffield University, for help given in the preparation of this article.

IRFF



FOR the EXPERIMENTER



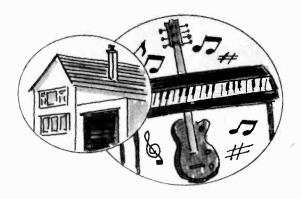
This supplement brings together a selection of specialised linear and digital integrated circuits having important and useful potentialities to the experimenter and constructor.

The areas of application embrace TV Games– Electronic Musical Instruments–Hi Fi–Control –Special Sound Effects, and Motor Cars.

It is hoped that the information and in-circuit examples of the devices might be the catalyst for additional ideas and further experiment, but it should be borne in mind that any "in-depth" information on device parameters should be obtained from manufacturer's literature.

Almost all of the i.c.s given are available from our advertisers and approximate prices are given where applicable.





AUDIO AMPLIFIER

TDA2020

The TDA2020 monolithic operational amplifier is a front runner in the power game. It is intended for use as a low frequency class B power amplifier providing 20W into 4\Omega_2 at 1 per cent total harmonic distortion with a \pm 15V supply. This is a guaranteed output. At lower power levels—less than 8W—the distortion does not exceed 0.2 per cent and at most frequencies is about 0.1 per cent.

The absolute maximum voltage is $\pm 26V$. Although higher voltages are likely to damage the i.c. it will operate quite correctly from supply voltages down to $\pm 5V$.

The 14 pin (alternative quad or d.i.p. plastic packages available), incorporates short circuit protection which automatically limits the output transistors to their safe operating area if, say, the output was short-circuited. Thermal overload protection is also incorporated which allows more economic heatsink

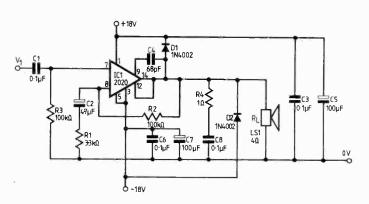


Fig. 1. The TDA2020 used in a basic 20W configuration

design as the risk of thermal runaway found in discrete amplifier designs does not exist. All of this makes the device virtually indestructible.

Fig. 2. A single channel 180W hi fi audio amplifier

Unlike most audio amplifiers the TDA2020 does not require a coupling capacitor from output pin to loudspeaker (see Fig. 1) which means a saving in money and space. The omission does make it necessary to maintain the quiescent output potential to prevent d.c. flowing through the speaker. This of course means balanced power supplies but the possibility of switch on "thump" is reduced.

A single 180W channel using a 40 loudspeaker can be built around two TDA2020's. This type of circuit (Fig. 2) is known as a bridge or push-pull amplifier. As can be seen the component count is small for such a large output.

The i.c. package includes a copper insert which is normally clamped to an external heatsink to remove circuit power dissipation. A range of heatsinks appropriate to different voltages is available from Redpoint and assembly of these is facilitated by the spacer and screws supplied with each device so that heatsink and chip will securely mate to a p.c.b.

The TDA2020 can be obtained from Technomatic Ltd., 54 Sandhurst Road, London, NW9, approximate price £4.20.

LONG DELAY TIMER



LR171E

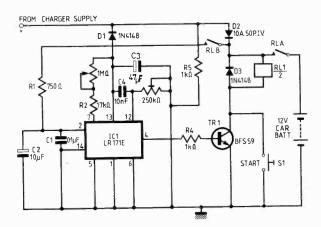


Fig. 3. A 10A battery charger timer (20 minutes to 2 days). When start button is activated RLA energises and connects the battery to the charging supply and the timer to the battery, holding RLA through TR1. At the end of the timing period the circuit switches of

A BOUT four years ago Elremco launced their 14 pin LR171E timer chip which took two years in gestation and £100,000 in develoment. Since then the price of the device has fallen by more than a third—currently £7.50.

Long duration electronic time delays using conventional CR methods require resistance of hundreds of megohms and capacitance of hundreds of microfarads. To connect components together of this dimension presents all sorts of problems most of them being inherent so that accurate timing is virtually impossible. The LR171E cleverly overcomes this using simple digital techniques to provide time delays from 5ms to over 3 months with a repetitive timing accuracy of ± 0.015 per cent.

Even more astonishing, if a second LR171E is added in series the period can really be pushed out—in this configuration an external time constant of 1s $(10k\Omega/1nF)$ would produce a six month delay.

Basically the i.c. contains a timing oscillator to which external CR components are added to determine the timing period. A chain of 12 binary dividers follows which effectively multiplies the external CR time constant by a factor of 4095.

A digital to analogue converter connected to the final six divider stages allows external meter monitoring of the elapsed time from the moment the timer is triggered. Outputs from the last three dividers in the chain provide facilities for specialised timing from $\frac{1}{8}$ T in steps of $\frac{1}{8}$ T where T is the preset time. If you combine this with the eight possible operational modes it can be seen that the device will suit almost all timing requirements.

With a suitable dropping resistor the device can work from a wide supply range since the on-chip voltage requirement is stabilised. Typical unloaded consumption is 5mA.

Some suggested applications by Elremco for the motorist are:

- 1. A time delay can be set by the user within a 0-24hr range after which the parking lights automatically switch on.
- 2. The parking lights can be switched on and off in a 0-24hr period.
- 3. A set number of minutes after switching off the ignition the headlights are automatically switched off. This prevents parking with headlights left on.
- 4. The car radio can be made to switch on after a preset time delay acting as an alarm clock or to synchronise with a favourite programme.
- 5. Providing control for a combined windscreen wiper/washer.

In the home it can be arranged to switch off any manual over-ride facility for domestic central heating.

Central heating and night storage systems are normally controlled by a programme time switch which the user presets. When heating or hot water is required outside the programme times the manual over-ride is used but usually left on with consequent fuel wastage.

The LR171E can be time adjusted for this to switch the system back to automatic. Switching on a morning kettle or radio alarm are other applications.

The approximate price of the LR171E is £7:50. For more information refer to Elremco Ltd., P.O. Box 10, Bush Fair, Harlow, Essex.

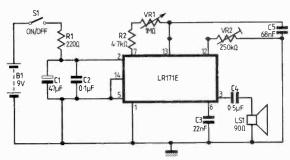


Fig. 4. Battery operated alarm timer from 2 seconds to 5 minutes duration



TV GAMES

·MM57100—LM1889—MM53104—AY-3-8550—AY-3-8600—AY-3-8700-

A FEW years ago the TV games market did not exist—today it is a multimillion pound industry and growing all the time.

Recently we published a design featuring the GIM AY-3-8500 games chip. It offered three basic games; tennis, soccer and squash. Additional discrete circuitry was required—a clock generator and a u.h.f modulator for interfacing to a monochrome receiver.

A more elegant games circuit available is the National MM57100 i.c. This offers hockey, tennis and handball in colour plus a lot more unpredictable play as a ball reflection from a bat can appear at eight possible angles. Complete game assembly is eased with the LM1889 video modulator i.c. and MM53104 clock generator i.c.

Of course, the LM1889 is a very useful chip in its own right since it can be used for relaying information from video tape recorders, closed circuit t.v. cameras or test equipment for display on monochrome or colour receivers.

A variant of the AY-3-8500 is the AY-3-8550 which provides the same basic games but the players' bats can be moved both vertically and horizontally requiring a lot more skill. The AY-3-8600 improves on the basic four games with basketball, hockey and gridball and increases in sophistication.

A spin-off from the popular microprocessor unit-based "tank battle" videogame commonly seen in amusement arcades is the GIM AY-3-8700. This offers a two player "tank battle" where each player has a completely steerable tank with forward and reverse speed controls and a firing button. The screen "battlefield" includes anti-tank barricades and exploding mines to retard each tank's progress. The object of the game is to score as many hits as possible on your opponent's tank. The first on your opponent's tank. The first player with 31 hits ends the game. Shell firing, explosion and tank sounds all add to the excitement.

All the above mentioned devices are available from A. Marshall (London) Ltd., 40-42 Cricklewood Broadway, NW2 3ET.

The MM57100 and MM53104 are available as Kit No. SK1122 for £17.18.



SOUND EFFECTS

·SAD1024/TDA1022—DELAY LINES --

N THE consumer area probably one of the most exciting chips to appear is the digital or analogue delay line otherwise known as a "bucket-brigade" device (b.b.d.).

Some of the effects that can be achieved with these are the generation of chorus—where single instruments or voices are made to multiply which has become a popular sound usually associated with the string synthesiser; "Flanging" or "phasing", another effect similar to chorus but in performance equivalent to the sound produced when using a variable comb-filter; Vibrato which is defined as a 5–10Hz cyclic pitch variation used generally to add richness to a sound produced and finally the synthesis of reverberation which is probably the most obvious application.

Of the devices around the two most readily available are the Mullard TDA1022 a PMOS circuit and the NMOS Reticon SAD1024. Both are in 16 pin d.i.l. packages.

Simply explained a "bucket brigade" delay consists of 512 capacitors separated by f.e.t.s. A sample of the incoming audio waveform is stored in the first capacitor end to the command of a clock pulse, the sample moves down the capacitor chain. to emerge 512 clock pulses later as delayed audio. For fidelity the number of samples per second clocked should be twice the band width of the incoming signal.

The successive samples can be likened to buckets of charge moving down the capacitor chain hence the analogy with the old fire-fighting "bucket brigade" line. The original signal is normally retrieved by passing the output through a low pass filter to remove the clock frequency.

The sampling frequency is very much related to the reverberation time of the bucket brigade the delay for N "buckets" being N2f seconds, where f is the clock frequency in hertz.

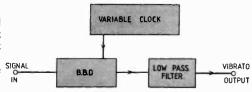


Fig. 5. Achieving a vibrato effect with a bucket brigade device (b.b.d.)

Reverberation is the echo effect produced by a sound after it has ceased and accounts for the richness in "live" performance. By using b.b.d.s in parallel or serial form it is possible to add artificial reverberation to existing music systems and so enhance the sounds produced.

A typical set-up for vibrato with a b.b.d. is shown in Fig. 5. By changing the clock rate in a slow cyclical manner (5-10Hz) the delay through the device and hence the pitch varies in manner analogous to the Doppler effect when

the clock frequency is high, delay time is low and vice versa.

For chorus or multiple voice effects a typical block arrangement would be as shown in Fig. 6.

Chorus produced by delay alone is likely to sound lifeless because each reproduction is a replica of the previous signal. If the clock rates of the b.b.d.s are varied slightly there is enough difference between the direct and delayed signal to make them appear to come from separate sources or "chorus" together. There are obviously lots of variations to this—the clock oscillators could be modulated in antiphase or run irregularly, say, from noise passed through a narrow band filter or another b.b.d. could be added.

A "flanger" or "phaser" can be created by combining an input signal with a slightly delayed version of itself as shown in Fig. 7. Obviously the magnitude of the effect is controlled by the ratio of delayed to undelayed signal (Balance Adjust) and the amount of delay which can be varied with control of the clock frequency. These are only some of the exciting possibilities of the b.b.d. but it obviously is a device we are going to see a lot more of in the future.

The SAD1024 is available for approximately £18 from Herbert Sigma Ltd, Spring Road, Letchworth, Herts.

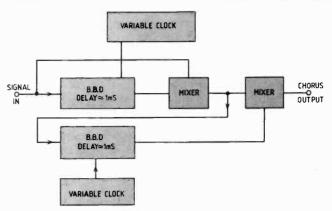


Fig. 6. A block diagram for setting up chorus effects

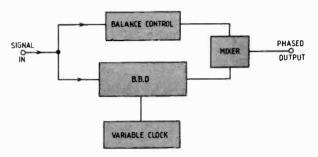
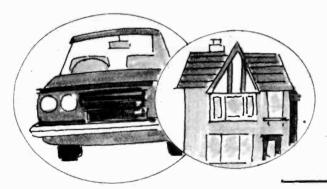


Fig. 7. Block diagram for phasing effects



MONITORING

- LM1830—FLUID DETECTOR

THE National LM1830 is a 14 pin monolithic bipolar i.e. for use in liquid detection systems. Application areas include sump pumps, aquaria, radiators, boilers, etc. in fact anywhere where high or low fluid levels need to be detected.

The basic circuit of the chip is shown in Fig. 8. To complete the oscillator circuit a capacitor is connected across pins 1 and 7. The frequency of oscillation is inversely proportional to this capacitor value. Pin 13 is normally connected to the probe via a capacitor so that there is no chance of probe plating.

The oscillator output amplitude is approximately $4_{\rm be}$ so that the emitter-base junction detector will be switched on when the probe resistance to ground is equal to the $13k\Omega$ resistor.

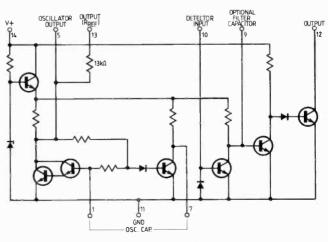


Fig. 8. Schematic of the LM1830 fluid detector i.c.

The diode at the detector transistor base symmetrically limits the input signal so that the probe is excited with $\pm 2V_{he}$ from a $13k\Omega$ source. If the $13k\Omega$ source is incompatible with the probe resistance range a variable resistor, say $0-100k\Omega$ could be connected from pin 5 to the probe coupling capacitor.

Fig. 9 shows an application where an audio warning is given when a conductive liquid falls below a certain level, for example, the water level in a car radiator. When the liquid falls below the probe tip the resistance will rise between probe and radiator causing the output transistor to conduct the oscillator tone to the loudspeaker. An l.e.d. could equally be used in this position.

In such car applications the internal regulator on the LM1830 provides protection against supply transients.

An example of the device being used for sump pump drive or drain valve opening when a liquid is high is shown in Fig. 10. Here the relay or solenoid drive is arranged to be switched off when

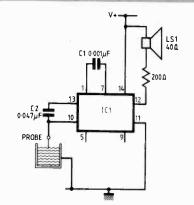


Fig. 9. Low liquid level alarm using the LM1830

the liquid level is below the probe. With the probe tip immersed it switches on. The filter capacitor ensures on-off switching.

Although the LM1830 is designed primarily for use in sensing conductive

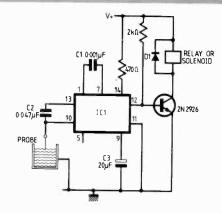


Fig. 10. High liquid level alarm suitable for opening a drain valve

fluids, a phototransistor, l.d.r. or thermistor could readily be substituted for the probe path.

The LM1830 is available from A. Marshall (London) Ltd (see below), approximate price £1.72.

LM3911—TEMPERATURE CONTROLLER

HEN making up a thermistor thermometer bridge the greatest single problem is maintaining any sort of linearity in the meter scaling. This arises because of the instrinsic nonlinearity of this transducer.

If a silicon junction diode is used as a sensor this usually requires amplification as the sensitivity is only around 2.5 to 3.5mV per degree Centigrade but there is an improvement in linearity. The usual circuit configurations are either amplification across a bridge configuration with the diode in one arm, or simply an op amp differentiating between a fixed set voltage at one input and the temperature variable diode voltage.

All of these problems have been neatly overcome in the National LM3911. Fabricated on a single monolithic chip it includes a temperature sensor, a stable voltage reference and an optional amplifier which can be used for both temperature measurement and control over a range of -25°C to +85°C.

The output voltage is directly proportional to temperature at 10mV per degree Centigrade with tracking linearity of 0.5 per cent. By using the internal op amp with external resistors any temperature scale factor is easily obtained.

By operating the device as a comparator the output will switch as the temperature traverses any set-point making the device useful as an on-off temperature controller. Lamps or a relay can be driven from the op amp

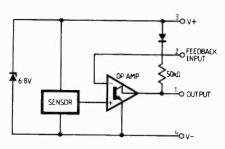


Fig. 11. Block diagram of the LM3911

output as this can be returned to a 35V rail.

The LM3911 itself has a 6.8V Zener reference for its sensing system. This allows the use of any power supply voltage with suitable external dropping resistor.

Block layout of the device is shown in Fig. 11 with an example of a basic

temperature controller in Fig. 12 and a centrigrade thermometer in Fig. 13. The unity gain comparator allows for zero setting of an attached meter.

The LM3911 can be obtained from A. Marshall (London) Ltd, 40-42 Crickle-wood Broadway, NW2 3ET, approximate price £1.03.

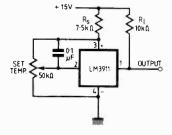


Fig. 12. Circuit of a temperature controller

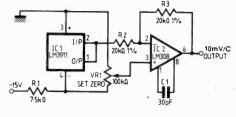


Fig. 13. A centigrade thermometer using the LM3911



PIANO CIRCUITS AY-1-0212 AY-1-5050 AY-1-1007B AY-1-1320

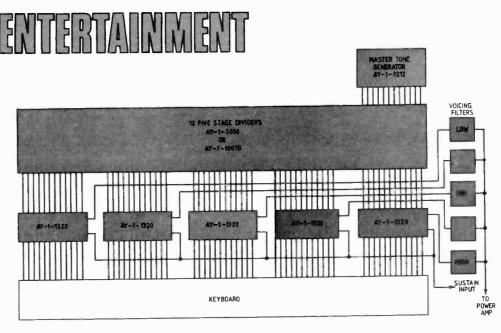


Fig. 14. Block diagram showing front end of an electronic piano

The modern electronic piano has all the features and more of the conventional strung instrument. It has a sustain and soft pedal, usually a choice of additional voices such as honky-tonk piano or harpischord, but most important of all special circuitry that ensures the loudness and tonal quality of a note sounded is proportional to the velocity of the keys as in a conventional instrument.

A strung piano also produces complex harmonic resonances which means that for successful electronic synthesis the sound produced needs to die away at a realistic rate.

To achieve this special envelope shape it has required in the past a great deal of discrete circuitry. Because of the component intensity in this area and obvious advantage of reducing assembly cost and increasing instrument reliability with an appropriate integrated circuit substitute, GIM have developed the AY-1-1320 piano envelope or keyer circuit.

This 40 pin d.i.l. package reduces the hard work of electronic piano assembly to keyboard contact wiring and discrete voicing circuitry.

A typical electronic piano block arrangement is shown in Fig. 14. Here because of harmonic variations over the conventional instrument keyboard the voicing filters are divided giving more high harmonic at the low frequency end, and lower harmonic content for the top octaves.

The twelve note top octave generator directly feeds the top keyer and twelve five stage i.c. dividers to give 60 frequencies to the keyers which is the

keyboard range plus one top note to complete the compass of a normal 61 note keyboard.

One chip keyer circuit is shown in Fig. 15. When the key is up C1 is charged to -12V. When the key is depressed C1 is first disconnected and starts to discharge through the 390kΩ with a time constant of 18ms. When the key is grounded the C1's voltage has been transferred to C2 via the gates TR2 and TR3. The faster the key velocity the larger the initial voltage on C2 and the louder the note.

The d.c. voltage on C2 is chopped via R1 and the output from a divider to give the decaying chopped waveform shown which is fed to the voicing circuit

When the key is released the 50k? damping resistor is optionally connected across C2 to damp the notes with a 110ms time constant. Different values of R1 are used for each octave to give variation in decay time across the compass.

A negative pedal voltage applied to the sustain input dampens the output with a time constant of 180ms when the key is released. This input simulates the action of the loudpedal in a piano.

The AY-1-0212 (£6·50) and the AY-1-5050 (£2·50) is available from Technomatic Ltd, 54 Sandhurst Road, London, NW9.

A complete i.c. kit based on Fig. 14 is available from Semiconductor Specialists (UK) Ltd, Fairfield Road, Yiewsley, Middlesex, price £36.25.

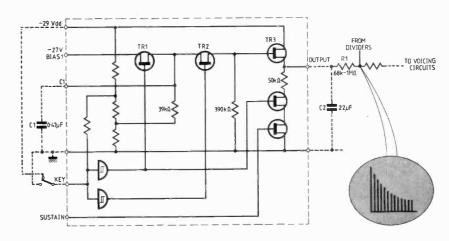


Fig. 15. The basic piano keying circuit

— AY-1-0212—AY-5-1317A—TBA 0470-D—ORGAN CIRCUITS—M147—AY-5050/1— AY-1-6721/5/6————

Top Octave Generator

The hearts of any electronic organ are the main oscillators from which all the distinctive voices derive. Years ago in the free phase system a separate oscillator was used for each note which represented an awful problem in tuning. Today, in what is known as the divider organ system, a digital tone generator produces from a single input frequency a full octave of twelve frequencies which with subsequent division can provide all the frequencies required by an electronic music synthesiser such as an organ or piano.

A good example of an i.c. top octave generator is the General Instrument Microelectronics 16 pin AY-1-0212. It is made up of twelve divider circuits which divide a typical input frequency of about 2MHz into twelve notes. If any one of the adjacent figures of division in Fig. 16 are divided they will be seen to approximate to $^{12}\sqrt{2}$ so that the whole makes up a well tempered chromatic octave.

Frequency Dividers

Another component intensive area which has surrendered to integration is the subsequent dividers to the Top Octave Generator which in combination with the latter give all the required instrument notes. GIM provide a whole range of 4-5-6 or 7 stage frequency divider in 14, 10 or 12 lead packages which have the same specification and are wholly compatible with each other to fulfil any arrangement of division. All circuits can be driven from a sine or square wave from, say, the AY-1-0212.

Choice of configurations are: AY-1-5050—7 stage frequency divider 3+2+1+1; AY-1-5051—4 stage frequency divider 2+1+1; AY-1-6721/5—5 stage frequency divider 3+2; AY-1-6721/6—6 stage frequency divider 3+2+1

Distribution

In an organ there can be several contacts under a key which when closed simultaneously route the various signals to the busbars, from the dividers, and then onto the voicing filters. The trouble is key contacts corrode and are therefore electrically unreliable, producing as they do, all sorts of nasty noises over the years. The current trend in electronic organs is to replace these contacts with electronic gates so that pressing a key and a single contact, octave related notes from a divider can be passed onto a selected voicing filter.

On this simple idea ITT came up with the TBA 0470-D organ gate which makes

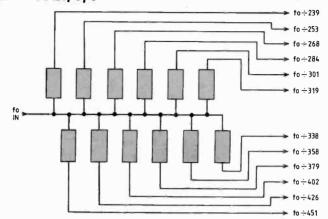


Fig. 16. Block schematic of top octave generator AY-1-0212

it possible to reduce a ten contact key assembly to one per key. The circuit simply consists of ten transistors, each transistor is a gate which is d.c. switched with the input signal information via each emitter.

Priority Latching

One bit of electronics which makes organ playing a lot easier is priority latching. This is a LSI subsystem which can be applied to pedals or keyboard but is probably more appropriate to pedals. The M147 from SGS-ATES is an example of a latch pedal sustain i.c. This has 24 pins with 13 pins for input stub pedals. When a pedal is depressed the corresponding square wave frequency spread over five octaves is immediately present at five pins. These outputs remain when the pedal is released until a new pedal is depressed. When two or more pedals are depressed only the left

one is accepted—corresponding to the lower frequency. This priority pedal produces a trigger percussion pulse when depressed and a sustain trigger with which the output sounds can be tailored.

Chord Generator

Some would say the most magical innovative thing about organs is the chord generator; as besides generating static chords the chip can be multiplexed internally to provide a walking bass, rhythm arpeggio or alternating bass.

A block diagram of the GIM 40 pin AY-5-1317A is shown in Fig 17. Here the bottom twelve notes of the divided top octave generator are fed to the chord multiplexer.

All the above devices are available from Technomatic Ltd, 54 Sandhurst Road, London, NW9.

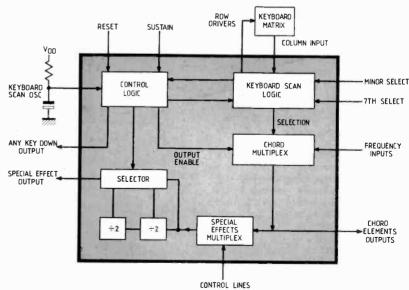


Fig. 17. Block diagram of the AY-5-1317A chord generator



PE GAME R.W. COLES B. CULLEN

PART THREE

LAST month we looked at the operation of the main system components used on the CHAMP board, including the 4040 MPU chip itself, and we are now about ready to look at the operation of the circuit in more detail. Before we start to discuss the hardware at the "gates and wire" level though, a word about the system operation as defined by the CHOMP software would be helpful.

SYSTEM OPERATION

When considering CHAMP as a development system, i.e. with the CHOMP program running, there are a number of specific tasks to be performed which can be listed as follows:—

- (a) Refresh 8-character 7-segment l.e.d. display at a rate which eliminates flicker.
- (b) Accept and store hexadecimal keyboard entries of up to three characters.
- (c) Scan the control panel to detect any of the following switch closures:—
 ENTER DATA, ENTER ADDRESS, DUMP, RUN-MODE, TEST.
- (d) In response to ENTER DATA, take data from temporary keyboard storage and load into the RAM location pointed to by the "current address pointer" register, then increment the pointer.
- (e) In response to ENTER ADDRESS, take data from temporary keyboard storage and load it into the "current address pointer" register.
- (f) In response to *DUMP*, read data in the program location pointed to by the "current address pointer" register and load it into the display buffer, then increment the pointer.

- (g) In response to RUN MODE, leave the CHOMP program by jumping to the start of a user program in the first program RAM location (Address 200 Hex).
- (h) In response to TEST, leave the CHOMP program by jumping to the start of a program in the second PROM chip (Address 100 Hex). This would normally be the PROMPT programmer firmware if fitted.

The important thing to remember about the operations listed above is that they are controlled by software. or to be more correct, firmware and are not purely hardware operations like RESET, RUN/STOP, or SINGLE STEP.

This means that although I shall be discussing the circuitry as it relates to these operations, you should bear in mind that you can use the circuitry for other purposes, providing you produce the software to do it.

This means, for example, that when you switch to RUN, your program can redefine ENTER DATA as "change points", ENTER ADDRESS as "sound horn", and DUMP as "pull the flush", without you having to change a single wire!

CIRCUIT DETAIL

Referring to Fig. 2.3 (last month), let's start with IC1, the 4201 clock generator. This device is fully described starting on page 5-77 of the users manual, but in outline it is a CMOS chip in a 16-pin package which contains the oscillator and dividers necessary to produce the 4040 two-phase clock signals and the logic for the SINGLE STEP and RESET operations.

The important point about this chip is that it provides high current clock outputs capable of driving the phase 1 and phase 2 inputs of a *complete* 4040 system, and this leads to a requirement for special decoupling circuitry.

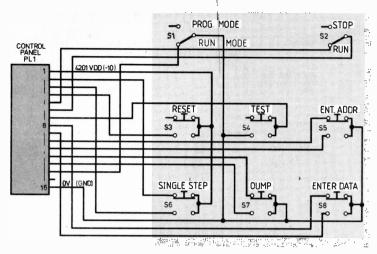


Fig. 3.1. The CHAMP control panel connections

R1, and C1, C2 isolate the drive current pulses from the supply line and R2, R3 help to reduce the rise time of the clock waveforms when a complete set of 4040 system components is not used, as is the case with CHAMP. The insertion of R1 produces a separate 4201 $V_{\rm DD}$ node and since the RESET switch and the SINGLE STEP switch require a $V_{\rm DD}$ connection, it is to this node that they must be connected.

Pin 5 on the 4201 is a mode control pin which changes the division ratio of the internal counter to slow down the resultant clock output. Since there are tangible advantages in sticking to a 10.8 microsecond clock cycle this pin is permanently connected to +5 volts in CHAMP. Pins 2 and 16 are clock outputs at TTL rather than Mos levels, and are unused in the CHAMP system, R5 and C3 provide the "power-on-reset" time constant and can be altered as necessary to set an appropriate delay which ensures that the complete system is reliably "cleared" whenever power is first applied.

4040 CHIP

The MPU chip, the centre of the CHAMP system, is of course IC2. Note that pins 1, 2, 3, and 4 carry the four-bit multiplexed bus which is the key to 4040 operation and which of course was covered in detail in Part 2 last month. This bus provides communication with the 4002 data RAMS, the 4265 I/O chip, the 4289 program memory interface chip, and can also be accessed via the sockets for system expansion when required. Note the SYNC out-put, pin 16, and its interconnection to the other system components, and also the STOP input, the STOP ACKNOWLEDGE output, and the RESET input which link to the 4201 clock generator. TEST, pin 13, is an input which can be tested directly with software (e.g. "JUMP IF TESTS EQUALS LOGIC ONE") and is a unique 4004/4040 feature.

The COMMAND RAM lines, pins 17, 18, 19 and 20 can each control a data RAM bank which in turn may consist of four 4002s, or three 4002s and one 4265. Ondy CM_{O} is used on the CHAMP board, but CHAMP PROG uses banks 1 and 2 for the two extra 4265s. These lines are activated using the DCL instruction and are used to increase the address range over that possible with only

an 8-bit SRC operation. The 4040 also has two COM-MAND ROM lines so that two separate ROM banks can be used to allow a total of 8K of program if needed. In CHAMP only CM ROM₀ is used to control a single 4289, and it is considered unlikely that CM ROM₁ would ever be used in a CHAMP derived system.

NEGATIVE LOGIC

When first introduced the 4004 and 4040 were defined with respect to a negative logic convention, because this is more "natural" in a PMOS system where a transistor turned "on" produces a positive output level and a transistor turned "off" allows its output to be pulled down to a negative level. *Inside* a 4040 system this convention still holds, so that for example, a logic 1 on the DATA BUS is actually represented by a *negative* level, but on the inputs and outputs from the 4265 the more familiar *positive* logic convention is employed.

This means that a logic inversion takes place inside the 4265, so that if for example your program writes binary 1111 (F in Hex) to 4265 port Z you can expect to see four TTL-compatible positive logic levels on the output pins even though they passed over the bus as negative levels. The 4289 PROM address and data, and the I/O and CS pins are also defined in positive logic to make life easier, and so usually you don't have to worry about which convention applies for interfacing operations, you can assume good old TTL-type positive logic.

The main exception as far as external interfacing is concerned is the 4002 RAM output port which is defined in negative logic, although this port is really only a secondary facility anyway, and only becomes available when a second 4002 is added to the system. It is of course always advisable to check in the MCS-40 User's Manual what the logic convention is on individual pins like INT or INT ACK before connecting these to external circuitry.

CONTROL PANEL INTERFACE

In Fig. 3.1 we show the interconnection of the CHAMP control panel switches, which of course are mounted on the plinth and hooked up to the CHAMP main board

via a 16-way flat strip cable. The RESET, RUN/STOP and SINGLE STEP switches connect directly to the 4201 chip IC1, but the other four switches are wired into the system via the ROM I/O lines and some TTL conditioning circuitry which forms, collectively, a special kind of four-bit input port.

The ENTER DATA, ENTER ADDRESS and DUMP push switches directly control the PRESET and CLEAR inputs of 7474 D-type flip-flops (IC11–IC13) which are used as latches to "debounce" the switch operations and provide a clean positive-going edge for each press. The outputs from these latches are used to "clock" further D-type flip flops which have logic 1s hard-wired to their D inputs, and the \overline{Q} outputs of these pass via a 74125 tri-state buffer, IC14 to the 4289 I/O bus. This second set of three latches can be cleared via a WRR instruction since they are controlled by what is, in effect, a ROM output port (part of IC24 and IC25).

Suppose the ENTER DATA switch is pressed, this sets the Q output of its associated latch to a 1 and this in turn clocks a 1 into the second flip-flop whose \overline{Q} output is then available at the input to the 74125. This sequence of events in itself initiates no further action, since the 4040 will not realise that anything has happened until it carries out an RDR instruction which strobes the 74125 and allows all four switch data bits to be transferred via the 4289 and the DATA BUS to the accumulator.

WAIT LOOP

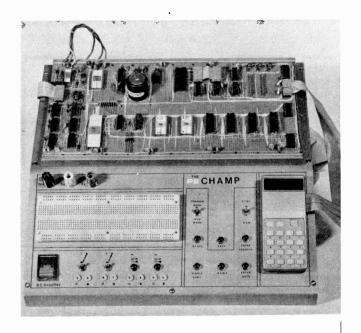
There won't be long to wait of course, and normally the 4040 sits in a "wait loop" which is embodied in the CHOMP software, continuously carrying out a read and check operation on these very control switches. When the ENTER DATA closure is recognised the 4040 jumps to a part of CHOMP which deals with the entry of data, and one of the first things this section of the program does is to clear all the switch flip-flops via the 4289 and part of IC24 and IC25. This is necessary to prevent multiple recognitions of the same switch closure, and points to the reason for the second D-type, since with this arrangement no matter how long you keep the switch pressed it can only be recognised once.

Note that the PROG MODE/RUN MODE switch is not provided with TTL latch conditioning circuitry since it is a toggle switch and is not used repetitively like the others; its contacts are connected directly to the 74125. We have termed the switch conditioning circuitry, just described, the switch FLAGS and in future we will use this shorthand name, and refer to the 74125 as the FLAG PORT.

KEYBOARD INTERFACE

The on-board keyboard interface, comprising IC7-IC10, interposed is between the 4265 ports and the keyboard sockets SK3, and also between the 4040 interrupt lines and SK3. The 4265 is connected to this interface circuitry via a 16-way flat strip jumper which connects SK7 to SK8 when the keyboard is in use. As mentioned in Part 1, this jumper can be removed for direct access to the 4265 when "custom" interfacing is required for user programs.

The keyboard produces a ready encoded hexadecimal output on four lines together with a common strobe, and the display section requires eight-segment anode drives (a-g & d.p.) and a clock and data input to the internal digit-strobe shift register (see Fig. 3.2). The internal circuitry of the keyboard will be covered in detail later on.



The four hexadecimal keyboard outputs connect directly to the 4265 port W which is defined as a mode 9 input port during 4265 initialisation under CHOMP, but the common strobe is fed to the 74123 dual monostable to produce a de-bounced strobe which sets the interrupt latch (half of IC9) aid is also used to enter the hex code into the part W input latches via the port Z1 asychronous strobe line (See MCS-40 User's Manual, pages 5-36 for further details.)

DISPLAY REFRESH

The display refresh drive is achieved by loading the next eight segment bits into output ports X and Y and then clocking the shift-register produced digit strobe along to the next common-cathode digit line. This operation has to be repeated eight times for the complete eight-character display, and has to be carried out rapidly enough to prevent display "flicker". The digit strobe is in effect a logic 1 shifting through a field of 0s, a new logic 1 being presented to the shift-register via 4265 output line Z3 under software control at the start of a new display sequence.

The shift-register clock pulses are provided by output Z2 which is a synchronous strobe produced when port Y is loaded with segment data during a WR2 instruction. IC7 and IC8 are special l.e.d. anode driver arrays (75491) which provide the high-current segment drive needed by the multiplexed display, the cathode drives (75492) are contained within the keyboard case and are of course driven by the shift-register outputs. R51–R58 perform the usual l.e.d. current-limiting function and therefore control the display brightness.

PROGRAM RAM

The original 4004 microprocessor expected its program in a ROM and its data in a RAM and never the twain shall meet, but CHAMP is a development system which requires programs to be easily modified and kept in RAM and 30

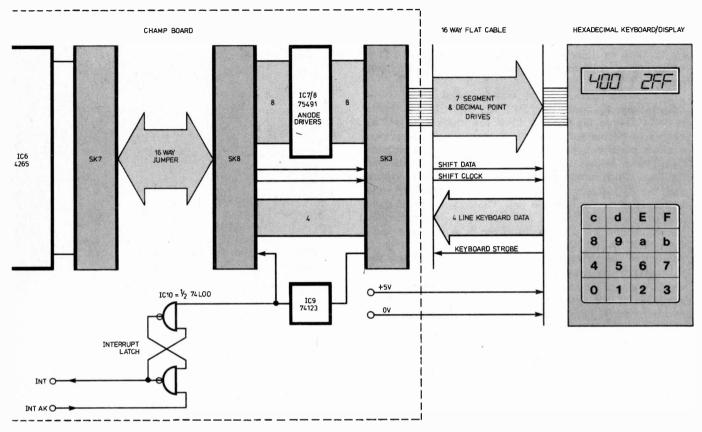


Fig. 3.2. The CHAMP board/keyboard interface

some special arrangements have to be made to provide this facility. Fortunately the 4040 does have instructions for writing to and reading from RAM program memory, namely WPM and RPM respectively, but since the 4040 deals with four-bit nibbles while its program comes in 8-bit bytes, some jiggery-pokery is still required to allow painless operation of the ENTER DATA and DUMP commands which of course are used to modify and examine program RAM when required.

When a program in RAM is actually running the program RAM is addressed via the 4289 just as if it were PROM, and eight-bit instructions are fetched from RAM via the 4289 without the MPU ever knowing the difference. The need for "special treatment" arises when the so-called transitive read or write operations using the RPM and WPM instructions are undertaken because of the nibble/byte conflict.

To achieve proper operation of the transitive instructions the 4289 contains a FIRST/LAST flip-flop which is toggled by each use of WPM or RPM. The output of this flip-flop is used externally to steer a nibble to either the FIRST half-byte or the LAST half-byte of a program RAM location during transitive write operations, or used internally to send the FIRST half-byte or LAST half-byte of program RAM data back to 4040 over the data bus during transitive read operations. To accommodate this mode of operation CHAMP program RAM is organised so that it may be read as a byte-orientated array of 512 × 8 bits but loaded as a nibble-orientated array of 1024 × 4 bits.

The program RAM write operation is achieved using the 4289 I/O bus to transfer the data a nibble at a time, the correct half-byte of RAM being selected using a logical combination of the 4289 outputs F/L, PM, and OUT to produce individual write strobes for each of the two 256 \times

4 RAM chips which together form the equivalent of a single 4702A PROM chip. This gating logic is performed by the remaining parts of IC24 and IC25.

ADDRESSING PROGRAM MEMORY

As mentioned last month, the 4289 is used to demultiplex the 4040 bus to produce a 12-bit wide address output to program memory. The lower 8 bits of this address are wired directly to each program memory device via what we shall call the 4289 address bus (pins 23 to 30 from 4289). The upper four bits are decoded by a 3205 TTL decoder to produce a unique CHIP SELECT strobe for each of the two 4702A PROM chips and each of the two pairs of 5101 RAM chips so that only one "memory chip" (one 4702A or two 5101s) can be enabled at one time.

The 12-bit address is provided by the 4040 program counter during normal operations, but when a transitive read or write is carried out the eight low order address bits must be provided by an SRC operation, and the four chip-select bits must be provided via an output port. In CHAMP the port employed for this purpose is the 4002 output port from IC4, buffered by a 74L00 gate IC3, which also provides the necessary logic level inversion.

We now have two possible sources for the four chipselect bits, either pins 31 to 34 of the 4289 (normal operation) or pins 13 to 16 of the 4002 (transitive operation) and so the 74157 quad two-line to one-line data selector (IC16) is interposed between the two sources and the 3205 decoder. The 74157 SELECT input is controlled by the 4289 PM output which is active only during transitive operations, so that proper selection of the source of chipselect data is maintained.

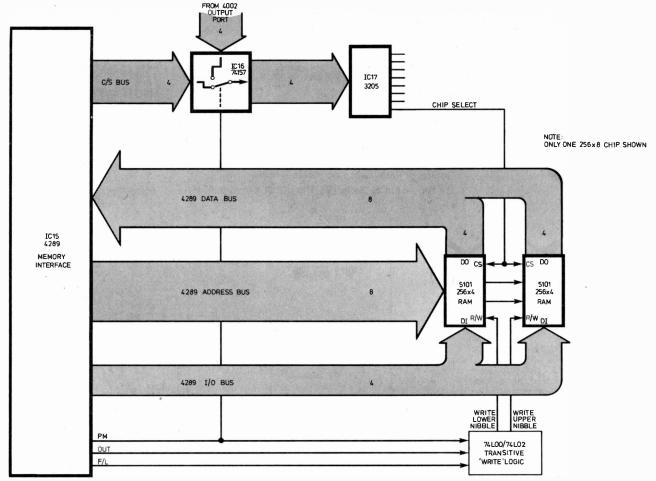


Fig. 3.3. Simplified schematic diagram of addressing CHAMP RAM program memory

To carry out a transitive write then, as required by an *ENTER DATA* command, the following sequence is necessary.

- 1. Select 4002 port
- 2. Write chip code to 4002 port
- 3. SRC to select location within chip
- 4. WPM to write first half-byte
- 5. WPM to write second half-byte.

A similar procedure is necessary to achieve a transitive read, as required by the *DUMP* command. Further details of the intricacies of addressing program memory can be gained from the 4289 data sheet, although of course to *use* CHAMP as a development system it is not *essential* to be familiar with these. See Fig. 3.3 for simplified circuit operation.

BATTERY BACK-UP

The 5101 program RAM chips are CMOS devices which have extremely low standby current drain. Components B1, D19, D20 and R40 form a battery supply circuit which will power the 5101s with the CHAMP main supplies turned off. B1 is a three-cell DEAC nickel cadmium battery which provides about 4 volts and is recharged via D20 and R40 when the power is on. When power is removed D20 becomes reverse biased, isolating the 5101s from the +5V line, and D19 becomes forward biased to supply the memory standby current. Note that a dry cell battery of 4.5 volts could be used instead of the DEAC

if R40 is left out, although you could end up losing data when the battery eventually runs flat. It is difficult to say just how long this would take.

POWER FAIL DETECT

To ensure that the memory is not corrupted by write transients during power failure or recovery, it is necessary to raise the CE₂ input to the 5101s only when the main 5 volt supply is available, and to achieve this control a "power-fail-detection" circuit formed by D13, R32, R33, TR1, R34 and part of IC10 is provided. The transistor is held on by the conduction of D13 until the 5 volt line starts to drop. When it drops below about 4.5 volts D13 and TR1 turn off and CE₂ is grounded via the 74L00 gate.

USING OTHER MEMORIES

If you can do without the non-volatile feature made possible by the 5101 devices for all or part of your program RAM, then you can leave out the battery circuit and the power fail detect circuit and plug in 2101 devices which are available at very low cost. The 2101s are completely compatible with the rest of the CHAMP circuit and have been tried on the prototype.

One final note, the 5101 cmos devices must not have their inputs taken negative more than a few hundred millivolts, and this is the reason for clamp diodes D1 to D12. The use of good quality germanium devices in these locations is essential.

NEXT MONTH: CHAMP Keyboard, power supplies, construction



PATENTS REVIEW...

Copies of Patents can be obtained from :
the Patent Office Sales, St. Mary Cray, Orpington, Kent
Price 95p each

COLUMN LOUISPEAKER BP 1 456 790

A column or line source loudspeaker for use in a public address system which is capable of directing sound "off axis" in a chosen direction is covered by Paul Taylor, of Hertford in RP 1,456,700

of Hertford, in BP 1 456 790.

Conventionally a column loudspeaker is constructed as a long box with a series of loudspeaker units arranged along its length and fed with equal, in-phase signals. Such a speaker column produces a narrow and symmetrical beam of sound which can only be directed at the intended audience by carefully mounting the column so as to point in their direction. This necessitates tilting a high column down at an awkward angle. The object of the invention is to produce a column which has an assymetrical sound characteristic and may thus beam sound down on an audience from a vertical position.

The column (Fig. 1) includes a line of loudspeaker units comprising end speakers, inner groups of equally spaced units and a central unit. The first phase reverser ensures that the input signal is fed in opposite phase to the units A

BP 1 456 790

RELATIVE AMPLITUDE

OF SIGNAL PHASE REVERSER

OF PHASE SHIFTER

(wide Bam) +90

RELATIVE AMPLITUDE

RELATIVE AMPLITUDE

AMPLITUDE

FIG. 1

above and below the central unit C. Attenuators R1, R2, R3, R4, between the units A ensure that the relative amplitudes of the sounds radiated from these units decreases progressively in each half of the column away from the centre unit. $A + 90^{\circ}$ phase shift is introduced into the signal fed to the central unit and -90° phase shift is introduced into the end units E, to minimise residual side lobes in the upper quadrant.

The phase and amplitude discrepancies along the remainder of the line produce a sound output radiation pattern which is vertically lopsided, so that a considerable amount of sound power is directed downwards and relatively little upwards. This enables the column to be installed vertically without tilt but still beam the majority of sound reproduced down at the audience rather than up and over their heads.

LIDUI TRUSHES

BP 1 475 177

There has recently been patenting activity in the field of liquid brushes for motors. In BP 1 468 155, Eric Wilcox of the Isle of Man patented a slip ring formed from an alloy having 18.8 per cent tin, 50 per cent bismuth and 31.2 per cent lead. This alloy, which has a melting point of 95°C, is kept liquid by a heater and is claimed not to react with a copper commutator.

In BP 1 475 877, Siemens A.G. of Germany claim the use of a new type of liquid brush. The object is to cope with high current levels, up to 50A/cm² and at all motor speeds, without loss of the liquid from the annular gap where

it is serving as a slip ring between the stationary and moving parts.

To-date gas pressure has been used to counteract the effect of skin-friction and centrifugal force. The proposed new answer is to use a ferro-magnetic liquid, for instance ferro-magnetic particles in a non-magnetic, metallic liquid. Sodium-potassium, gallium, or gallium-indium are suggested as the liquid metal, with iron or iron alloys suitable as the particles.

A magnetic field is generated in the area of the annular gap, by the provision of carefully located windings additional to those which form an integral part of the motor or dynamo which the slip ring is serving. When the rotor is stationary the liquid is held in a stable position by a static field from the additional coils. As the rotor turns, fric-

tional forces entrain the liquid, so that it is continually interrupting the radially directed magnetic field. The frictional forces are directed axially inwards or outwards depending on the sense of rotation and upon the direction of the magnetic field.

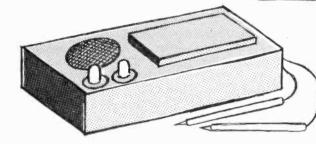
The direction of the magnetic field produced by the additional coils is thus chosen so that the magnetic containing forces act in opposite directions inwards, towards the middle of the fluid. Provision is made to reverse the direction of the magnetic field, by reversing the current flow in the coils, when the direction of the rotor is reversed. It is also possible to increase the current to the coils as the speed of rotation increases, so that the magnetic containing field is always greater than the forces tending to disturb the liquid in the gap.

...in Next Month's issue!

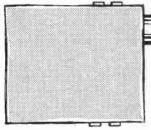
SPIECIAI. OFFIER



Provides immediate visual indication of condition of component, fuses, etc.



game. Ideal for fund-raising at school



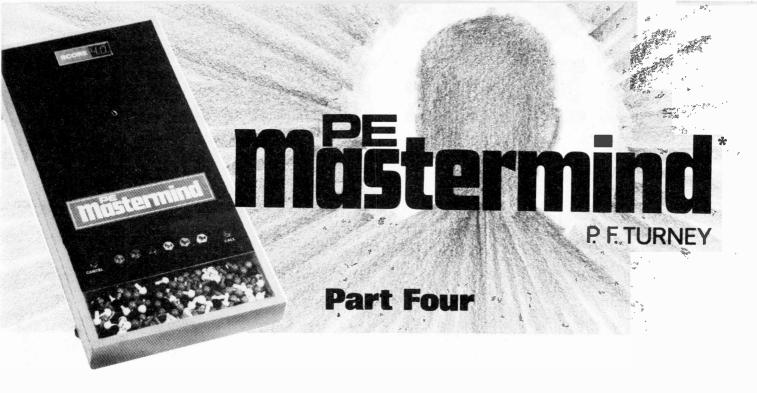
CONTROL SYSTEM

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In the last issue, the timing circuits were described and an introduction was given to the operation of the scoring logic, where the "P" flip flops were discussed. The description of the scoring logic is to be continued this month, commencing with the details of four flip flops that are used to produce the results for the number of coloured pegs correct for colour but incorrect for position, the "I" results.

COMBINATIONS THAT CAN OCCUR

At this stage it is worthwhile considering the various combinations of entries and internal colours that may occur in a typical game, as it is the nature of this combination that determines the particular mode in which the scoring logic will operate. The combinations that may occur can be divided into four categories:

- (a) The entries may be non-repeated and the internal colours may be non-repeated,
- (b) the player may repeat the colours in a deduction,
- (c) there may be repeated colours within the machine, and
- (d) a combination of (b) and (c).

Each of these categories may be sub-divided to include the cases where there are only "I", "P", or "I" and "P" results occurring.

Fig. 4.1 is the overall functional diagram of the scoring logic, and this will be referred to extensively throughout the description of the operation.

THE "I" FLIP FLOPS

Four flip flops, called the "I" flip flops, are used to produce the "I" results. These flip flops are clocked by signals $C_1\overline{C}$ to $C_4\overline{C}$, for I_1 to I_4 respectively, so as to eliminate any adverse effects that may otherwise have been produced by time delays inherent in the comparator logic, had signals C_1 to C_4 been used instead. This point was discussed in detail last month.

With reference to Fig. 4.1 it will be seen that the E (Equality) signal (from IC15) is common to the "J" inputs of all "I" flip flops, so that if, for example, $C_1\overline{C}$ and E are present simultaneously, I_1 will be set on the trailing edge of C_1C . The "K" inputs to these flip flops are connected to logical zero, so that a flip flop may only be cleared by the application of logical zero to the clear input.

A simple example, in category (a), showing the collective action of the "I" and "P" flip flops, is illustrated in Table 4.1.

An example in category (b) is shown in the simplified diagram of Fig. 4.2(iii). Here the player has entered two blue pegs, the first of which will set P_1 and I_1 ; the second one will produce no further change. However, according to the rules of play,

Table 4.1

ENTRI	ES	X CODES					
Red	{	Black $K = 1$ $C_1 = 1$ $E = 0$ $P_1 = 0$	Red $K = 1$ $C_2 = 1$ $E = 1$ $I_2 = 1$	White $K = 1$ $C_3 = 1$ $E = 0$ $I_3 = 0$	Green K = 1 C ₄ = 1 E = 0 I ₄ = 0		
Black	$\left\{ \right.$	$L = 1$ $C_1 = 1$ $E = 1$ $I_1 = 1$	$L^{4} = 1$ $C_{2} = 1$ $E = 0$ $P_{2} = 0$	$L = 1$ $C_3 = 1$ $E = 0$ $I_3 = 0$	$L = 1$ $C_4 = 1$ $E = 0$ $I_4 = 0$		
Blue	$\left\{ \right.$	$M = 1$ $C_1 = 1$ $E = 0$ $I_1 = 1$	$M = 1$ $C_2 = 1$ $E = 0$ $I_2 = 1$	$M = 1$ $C_3 = 1$ $E = 0$ $P_3 = 0$	$M = 1$ $C_4 = 1$ $E = 0$ $I_4 = 0$		
White	$\Bigg\{$	$N = 1$ $C_1 = 1$ $E = 0$ $I_1 = 1$	$N = 1$ $C_2 = 1$ $E = 0$ $I_2 = 1$	$N = 1$ $C_3 = 1$ $E = 1$ $I_3 = 1$	${}^{5}N = 1$ ${}^{6}C_{4} = 1$ ${}^{6}E = 0$ ${}^{6}P_{4} = 0$		

 $I_{1},\;I_{2}$ and I_{3} are set, indicating that the score is three white key pegs

^{*} Mastermind is the registered trade mark of Invicta Plastics Ltd

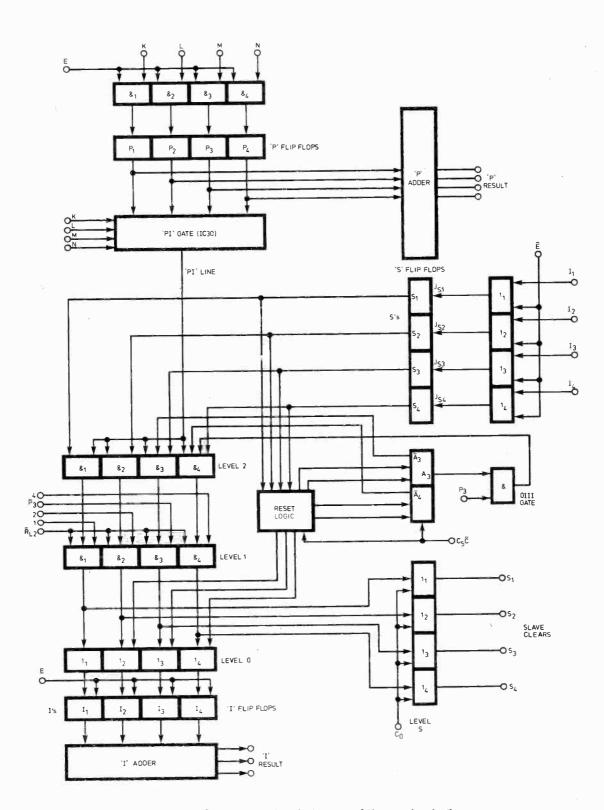
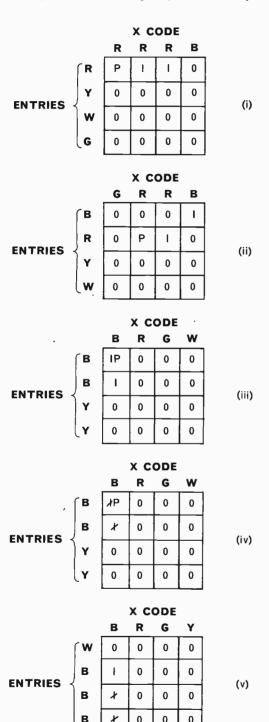


Fig. 4.1. Overall functional diagram of the scoring logic

only P_1 must remain set. Correct operation is ensured by arranging that when a given "P" flip flop sets it's corresponding "I" flip flop, I_1 in this case, is cleared and inhibited for the remainder of the deduction. A "P" correct entry is therefore a dominant one, as shown in Fig. 4.2(iv).

This dominance of a "P" flip flop over its corresponding "I" flip flop can be seen in Fig. 4.1, since the complements of



Notice that comparisons that are "ignored" or "erased" are deleted in the above tables

Fig. 4.2. Examples showing collective action of "P" and "I" flip flops

the "P" outputs are connected to the inputs of the NAND gates labelled "Level 1". If, therefore, P_1 has set, then $P_1 = 0$ acts to inhibit I_1 via the NOR gates of "Level 0".

A further example in category (b) is shown in Fig. 4.2(v), where there are repeated "I" correct entries. The first blue entered sets I_1 and the subsequent blue entries are then ignored, since I_1 can only set once.

Category (b) has now been fully explored, but before proceeding to (c) it is firstly necessary to describe the hierarchy of gates serving to clear the "I" flip flops.

RESET LEVELS

There are three levels, of four gates each, serving to generate the various resets required for correct operation of the scoring logic, see Fig. 4.1.

"Level 0", comprised of NOR gates, is an unconditional level, since a logical one applied to any gate input will clear the corresponding "I" flip flop. One input to each gate of this level is derived from "Level 1", whilst the other input is connected to the logic labelled "Reset Logic", to be described next month.

"Level 1" is likewise an unconditional level, since a logical zero applied to any input sends the gate's output high and clears an "I" flip flop via "Level 0". The four signals $\overline{P}_1 - \overline{P}_4$ are each taken to a gate in this level, performing the "clear and inhibit" function mentioned previously.

The clear line, \overline{R}_{L2} , is also connected to these gates, so that since this signal is taken low whenever the scoring logic has to be cleared, all "I" flip flops are reset unconditionally to zero.

The third set of inputs to the gates of "Level 1" comes from "Level 2". This is a conditional reset level, since all inputs to a given gate must be high in order to clear an "I" flip flop via levels 1 and 0.

THE "S" FLIP FLOPS

Just how these reset levels function in the logic will be discussed later, but in order to proceed with the description of "Level 2" the four "slave" or "S" flip flops must be introduced. Briefly, these flip flops serve to indicate which of the "I"s have set in response to any particular entry made by the player. Examples Fig. 4.2(i) and (ii) illustrate why these additional flip flops are required. Note that these are both examples in category (c).

In 4.2(i) the first colour the player enters will set flip flops P_1 , I_2 , I_3 and also S_2 and S_3 , the "slaves" corresponding to I_2 and I_3 . The fact that both S_2 and S_3 are set indicates that two "I" flip flops have been set in response to a single entry.

Example (ii) illustrates why this information cannot always be gained from the "I" flip flops themselves, since they contain not only a record of the current entry but also of any previous entries.

In both of these examples a single entry is seen to set both an "I" and a "P" flip flop. However, one entry, by the rules of play, cannot be counted as being correct for colour and position and yet correct for colour and incorrect for position at the same time, albeit with two identical internal colours in different positions. Both examples therefore give an incorrect score. It is the main function of "Reset Level 2" to overcome this problem.

Since a "P" correct entry is dominant it is necessary to clear any "I" flip flops that may also have been set by the entry. Therefore, in Fig. 4.2(i), both I₂ and I₃ must be cleared. To do this the PI signal is used, which, it may be remembered, produces a logical one output whenever a "P" correct entry has been made (until such time as a subsequent entry is made).

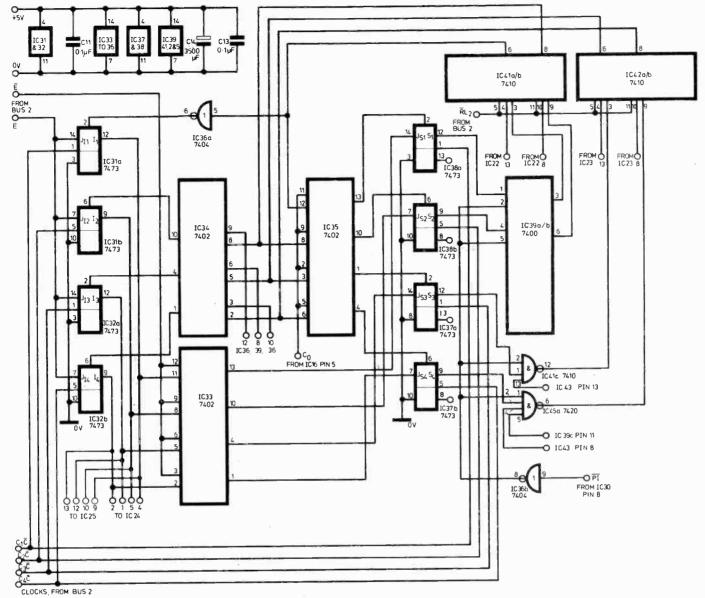


Fig. 4.3. Scoring logic circuitry

This signal is used to enable "Reset Level 2" in order to gate the outputs of the "S" flip flops to clear those "I" flip flops whose "S" flip flops have set. It will be seen from Fig. 4.1 that gates 3 and 4 of "Level 2" have three and four inputs respectively. The additional inputs are inhibit inputs and will be described next month. For the moment they may be regarded as being held at logical one.

The operation of the system, with reference to Fig. 4.2(i), is now as given below.

(1) Enter first colour—Red. K (from IC20) = 1.

KC₀ — All logic cleared.

C \overline{C} = \text{P. set I. and S. cleared and inhibited}

 $C_1\overline{C}$ — P_1 set, I_1 and S_1 cleared and inhibited. PI = 1.

 $C_2\overline{C}$ — I_2 and S_2 set. PI gates S_2 via levels 2, 1 and 0 to clear both I_2 and S_2 .

 $C_3\overline{C}$ — As for $C_2\overline{C}$ but with I_3 and S_3 .

 $C_4\overline{C}$ — No change.

(2)-(4) No change. Only P_1 remains set, which is the correct score for this deduction.

Referring to the latter sequence of events, it is seen that when PI gates S_2 to clear I_2 , S_2 is also cleared, and similarly for S_3 following $C_3\overline{C}$. The precise reasons for this will be examined next month, but it is important to note that the reliability of these resets depends solely on the existence of a time delay around the reset loop. Hazard free operation can only, therefore, be assured if "on spec" gates are used. The clearing of the "S" flip flops as described may be seen in Fig. 4.1, since the outputs of "Level 1" are connected to "Level S", which serves to clear the "S" flip flops.

The "S" flip flops must only provide a record of those "I"s set in response to a single entry, so they are cleared by Co, connected to "Level S", at the start of each entry.

CONSTRUCTION

The positions of this month's i.c.s are shown in Fig. 4.4. Construction is fairly straightforward, reference being made to the circuit diagram of Fig. 4.3 as well as to Fig. 4.4.

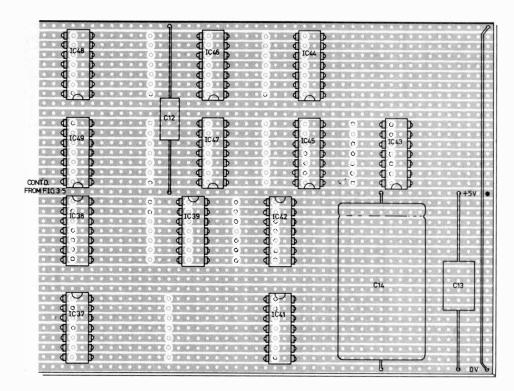


Fig. 4.4. Prototype component layout for "C" section of main board (see photo last month). For assembly details one should refer to the circuit diagram

A number of input connections cannot be completed until next month and it is therefore recommended that these be left completely unconnected for the moment.

The best order in which to complete the construction is as follows: IC31-39, 41c, 45a, 41 and 42 respectively.

The outputs from the "I" flip flops are taken to the "I" adder, described last month. Connection details are given in Fig. 4.3.

Note that \vec{E} and NOT E is taken to IC33, and also that \vec{PI} , from IC30, is inverted by IC36b.

"S" FLIP FLOP J INPUTS

Again due to the fact that these flip flops must only provide a record of those "I"s set by the current entry, an "S" flip flop must not set if its corresponding "I" flip flop has set in response to a previous entry. This is arranged by gating the J_s inputs such that $J_{s_1} = E\overline{I}_1$, $J_{s_2} = E\overline{I}_2$, etc.

COMPONENTS...

Integrated Circuits IC31-32 SN7473N (2 off) IC33-35 7402 (3 off) IC36 7404 IC37-38 7473 (2 off) IC39 7400 IC41-42 7410 (2 off) IC45 7420 Capacitors 0.1 µF (3 off) 10V ceramic C11-C13 C14 3,500µF 10V electrolytic

This gating is performed by IC33 which is a 7402 quad two input NOR gate.

The circuit diagram is shown in Fig. 4.3. All flip flops are JK types SN7473N. The reset levels are implemented as follows:

₹ IC34+IC36a—Level 0

½ IC39+IC41c+IC45a—Level 2

 $\frac{2}{3}$ IC41 + $\frac{2}{3}$ IC42—Level 1

IC35-Level S.

TESTING

Testing is somewhat complicated by the fact that a number of connections have not yet been made. For example, the "I" flip flops are always held "clear" owing to the floating inputs to IC34, awaiting connections from the "reset logic". However, provided that the constructor connects pins 9, 6 and 3 of IC34 temporarily to 0V, then very worthwhile testing may be performed by simply playing the game and noting the scores (the "I" flip flops are enabled by these temporary connections).

The randomly generated codes may firstly be monitored using a d.c. voltmeter. These codes are contained in i.c.s 3-6.

The "P" results may be "read" from Veropins 16–18 and the "I" results from pins 13–15 (see Fig. 3.5).

The scoring given by the machine should follow the rules of the game in all cases except where there are certain repeated codes within the machine, that is a combination in category (c) or (d). Remember that fault tracing can be enhanced by slowing down the internal clock, as described last month, should any problems be encountered.

NEXT MONTH: The final part of this series of articles will deal with the remainder of the scoring logic and the display circuits.



A selection of readers original circuit ideas. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought.

Why not submit your idea? Any idea published will be awarded payment according to its merits.

Articles submitted for publication should conform to the usual practices of this journal, e.g. with regard to abbreviations and circuit symbols. Diagrams should be on separate sheets, not inserted in the text.

Each idea submitted must be accompanied by a declaration to the effect that it is the original work of the undersigned, and that it has not been accepted for publication elsewhere.



WASH-WIPE CONTROLLER

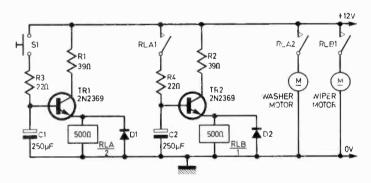


Fig. 1

A CLEAR windscreen is essential for safe driving. However, on some older cars, operating the windscreen washer and wipers simultaneously while still remaining in perfect control, is not easy.

The circuit in Fig. 1 is designed to wash the screen and then wipe it clear, having switched off the washer; all at the touch of a button. When S1 is pushed, C1 charges up almost instantly, which holds TR1 on, and operates RLA. Consequently RLA1 charges up C2 and turns on TR2, thus energising RLB also. At this point both washer and wipers are working.

When C1 has lost enough charge through the base of TR1, RLA will drop out, leaving C2 fully charged and RLB still energised. At this point, just the wipers are left operating. Eventually, when C2 has lost sufficient charge, RLB will drop out to switch off the wipers, and then the sequence is complete.

The values of C1 and C2 are a matter of choice, but with the values shown $(250\mu F)$, the washer and wipers should run together for about five seconds, and then just the wipers for a further five seconds. The resistance of the relay coils will affect this timing relationship.

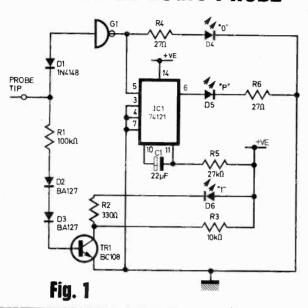
Any 12 volt relay should be suitable as long as the coil current does not exceed the rating of the transistors used. When

considering the contact ratings of the selected relay, remember that the stall (starting) current of the washer or wiper motor, may well be several times the running current.

A convenient position for the Wash-Wipe Controller switch is on the steering column, similar to indicator or headlamp flasher switches. If the button is pressed before the cycle is complete, the sequence will begin again irrespective of how far the process has gone.

J. R. Ellis, Hitchin, Herts.

SIMPLE LOGIC PROBE



A LOGIC probe is a vital instrument in the checking of digital equipment. The circuit of Fig. 1 shows a simple three-function probe which can be built very economically.

A high logic level at the probe tip causes TR1 to conduct, illuminating the l.e.d. marked "1". A low logic level produces a high at the output of the inverter G1, causing the l.e.d. marked "0" to be lit.

If, however, the logic level at the probe tip is being pulsed, either a 0 pulsing to 1, or a 1 pulsing to 0, the monostable IC1 will detect the pulses and stretch them to about 0.4s duration. The l.e.d. marked "P" will then flash briefly.

The whole circuit was constructed on Veroboard and mounted in a small metal pill box, using three 1.5V batteries to supply the power. The inverter G1 can be one section of any TTL package, such as a 7400, 7402 or 7404, which may be to hand, with inputs paralleled if appropriate.

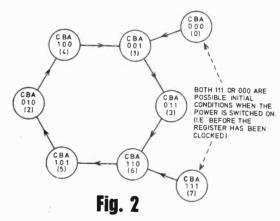
A. C. Hay, Bristol

SEQUENCE generators find wide application as counters, and in the field of digital communications. One form of sequence generator is the feedback shift register, comprising a shift register with combinational logic feedback from its outputs to its input. This feedback determines the next logical state to be entered into the register.

CLOCKO 9 CK1 SN7495 MODE 5 GND 7 BINARY O/P'S 13 12 11 1 SEGMENT DECODER BO 5 SN74.47 C O 13 10 11 2 8 4

1kΩ

SEQUENCE GENERATOR



The circuit diagram of Fig. 1 uses an SN7495 4-bit shift register, operating in the serial in, parallel out mode, and is suitable for use as the binary number generator for a digital die. As the shift register is clocked, its three outputs follow the 6-state cyclic sequence shown in Fig. 2.

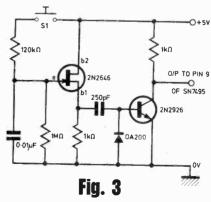
Fig. 1

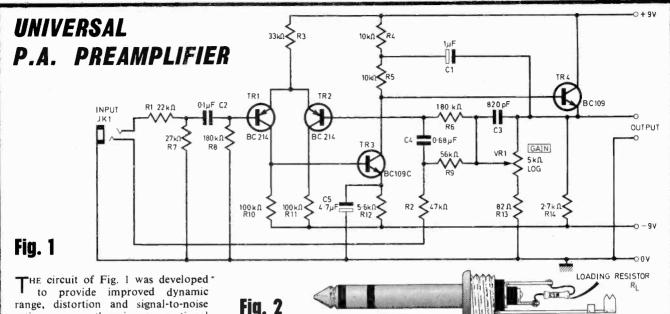
The SN7451 dual, 2-wide, 2-input AND-OR-INVERT gate forms the combinational logic feedback network which processes the outputs A, B and C to determine the next logical state for the register. This combinational logic performs the Boolean function:

F = AC + BC

A suitable clock source is shown in Fig. 3. This consists of a simple unijunction relaxation oscillator, plus a pulse amplifier to boost its output. Closing S1 activates the oscillator and thus creates the "roll" effect for the die. An important characteristic of this clock source is that when S1 is released, the effect of any contact bounce does not appear at the output of the clock source. Such contact bounce can cause the register to clock spuriously, leading to unwanted output combinations appearing, i.e. 000 or 111.

P. Hutchinson, Brockenhurst, Hants.





The circuit of Fig. 1 was developed to provide improved dynamic range, distortion and signal-to-noise ratio on an otherwise conventional 741-based, 16-channel mixer. It also incorporates a number of novel features which simplify the input switching requirements for the mixer.

This preamplifier will handle signal levels ranging from less than 1mV, such as might come from a high-quality microphone, up to several volts r.m.s., as can be produced by a high output guitar pick-up. The differential input provided by TR1 and TR2 operates over this range with low distortion, and allows a balanced input to be achieved without the expense and inconvenience of a microphone transformer.

The arrangement of the input connections eliminates the need for switching between balanced and unbalanced modes. A stereo jack is used, providing two signal connections for a balanced lead, connected by means of a stereo jack-plug. The signals are then fed via R1 and R2, giving a differential input impedance of about 90kΩ.

An unbalanced signal source would be connected via a mono jack-plug, whose sleeve will short R2 to earth, so that the amplifier functions as a non-inverting single-ended input stage, with an input impedance of about 45k().

For input impedances les than those quoted above, a loading resistor R₁ should be connected across the input ends of R1 and R2 so that the resultant paralleled value approximates to that requried (e.g. $R_{\rm L}=680\Omega$ for 60012 line). This resistor could be inserted by means of a front panel switch, but a simpler and more versatile solution is to wire an 18W resistor inside the actual jack-plug, as shown in Fig. 2. A robust screened jack-plug with solder terminals should be used, and colour-coded tape applied to the cable to show that it has been "preloaded" and now matches a standard high impedance input on virtually any amplifier.

The input stage feeds a high gain common-emitter voltage amplifier, TR3, with a bootstrapped collector load for increased efficiency. This is followed by an emitter-follower based on TR4, which provides a low-impedance output for tight control of the feedback circuit, and is capable of driving channel fader or tone controls without detriment to the signal, which is closely balanced about earth.

Gain is variable between unity and 60 (36dB), providing a minimum output of 50mV r.m.s. for further amplification. Several such preamplifiers could be incorporated into a mixer or public address amplifier, with tone and volume controls and mixing-withgain based on i.c. op. amps. The balanced supplies could then be derived from the op. amp. supply, decoupled and Zener-stabilised as appropriate.

P. J. Willcox, London W11.

TTL FREQUENCY DOUBLER

THE circuit shown in Fig. 1 is a frequency doubler using TTL gates. It provides two complete output pulses for one complete input pulse.

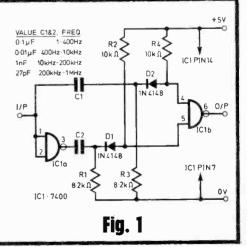
On the positive-going edge of the input pulse, the output for ICla goes low and this sudden change is passed through C2 to turn D1 hard on. This causes ICl pin 5 to go low and pin 6 to go high. If no further changes are made at the input, C2 discharges and the output returns to the low condition. On the negative-going edge of the input pulse, D2 is turned on

via C1, causing the output of IC1b to go high again, returning to low shortly after.

The two diodes are included to prevent execessive voltages being applied to the inputs of IClb. The values of Cl and C2 depend upon the input frequency being used. The table gives a rough guide to the actual values required for four different frequency ranges.

The shape of the output pulse may be improved by using a Schmitt NAND gate (such as the 7413) for IC1b.

P. J. Hambridge, Ilford.





INGENUITY UNLIMITED

THE circuit in Fig. 1 uses a seven segment l.e.d. display to show characters that indicate a car system fault, such as low hydraulic fluid or coolant, and are accompanied by an audible tone. Altogether, these eight characters and their meanings are shown in table 1.

When any one of the sensor outputs falls to logical 0 (when a fault occurs) the output of the 7430 eight

CAR SYSTEM MONITOR

input gate, goes high. This enables a simple three gate oscillator, and TR1 drives the loudspeaker. The 7430 output also enables the seven segment display drivers (7401s). The original sensor output pulls its associated driver gate (7407) output to ground. This output pulls down the 7401 driver inputs via the diode matrix. When the drivers are enabled, the output is at ground level, therefore switching on that segment connected to it, the DL707 being a common anode display.

Sensor circuits of the type used with the display are shown in Figs. 2 to 5. Fig. 2 shows a spark plug monitor. This has a discrete l.e.d. which will glow when that plug is firing. The coil picks up impulses which are fed via an amplifier to a monostable which fires for about 0.7 second. This charges up a capacitor and produces a logical 1 at the Schmitt gate input. Missing pulses will allow the capacitor to discharge, changing the state of the Schmitt trigger, and causing a final display of "S". One circuit can be used for each plug, each feeding into the SN7413.

Fig. 3 shows an oil pressure monitor. When the input falls to zero volts, the first transistor switches off and the second transistor switches LIST OF SYMBOLS PRODUCED

= COOLANT LEVEL

= BRAKE FLUID LEVEL

= OIL PRESSURE

= TEMPERATURE

= BATTERY LEVEL

SPARK PLUG NOT FIRING
= LED DISPLAY

= HEAD AND REAR LAMPS

= BRAKE LIGHTS

on. This produces a zero at the "0" input of the display circuit. The preset must be adjusted so that the display comes on only when the input is at exactly zero volts.

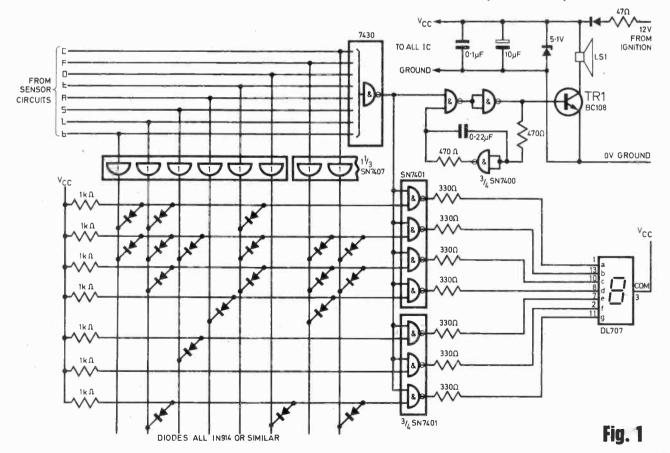


Fig. 2—SPARK PLUG MONITOR

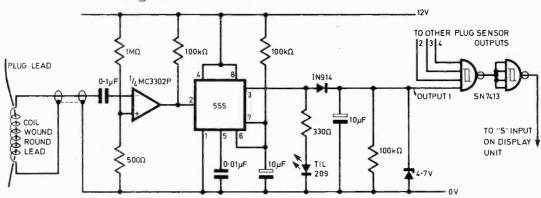


Fig. 4 shows the headlamp and brake-light sensors, one of which is required for each bulb to be monitored. When the lamp is on, a voltage is produced across the 0.5Ω resistor, turning on TR1 and consequently TR2. This produces a low input at G1, and so too does TR3 if the headlight switch is on. The EXCLUSIVE OR function of G1 produces a low output whenever the two inputs are the same.

The output of G1 is fed to the EXCLUSIVE OR array, which will produce a low, only if one or more lamps do not draw current when switched on. The brake-light will have a similar circuit, but with effectively only gates G3 and G5 in its or array. The value of the 0.512 resistor may need to be varied according to the bulb rating it is in series with.

The battery level indicator is shown in Fig. 5a. This is a simple comparitor, working from a reference Zener diode with its voltage divided down, to minimise the effects of supply voltage variation. When the input voltage falls below 11 volts, the output drops to logical

The fluid indicators apply to hydraulic and coolant levels. The output of these probe networks are connected to similar comparitors to that shown in Fig. 5a. A typical probe arrangement is shown in Fig 5b, where, if the fluid drops below the probe, conduction ceases and the output voltage drops. The comparitor output becomes logical 0, displaying "F" or "C" on the display, depending on which probe.

temperature unit is similar to the fluid level sensor, but a thermistor replaces the probe. reference voltage is connected to the positive input of the comparitor, and the signal input to the negative. The reference voltage is set so that a logical 0 is produced when the temperature becomes excessive.

Decoupling of the i.c.s is essential due to the large amount of produced electrical noise in a motor car.

P. M. Glover, Ockbrook. Derby.

Fig. 4—HEADLAMP & BRAKE LIGHT SENSOR

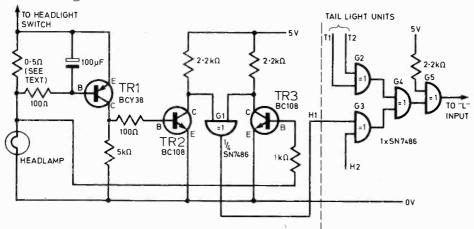


Fig. 3—OIL PRESSURE

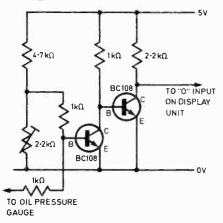
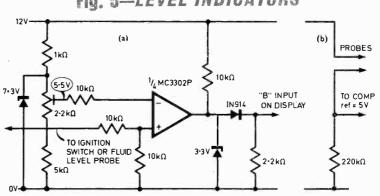


Fig. 5—LEVEL INDICATORS



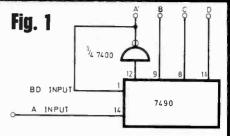
COUNTER

T is often a requirement to reset a 7490 counter to one instead of zero. The 7490 is in fact two separate counters in one package, with an external connection required between the A output of the divide-by-two stage and the B input of the divide-by-five stage.

These counters change state on a negative-going edge, so that if an inverter is put in the external loop between the stages, and the output of the inverter (A') in Fig. 1) is now read as the output of the divide-bytwo stage; on reset the output count will read one.

TRUTH TABLE						
Basic Count	Α	Α'	В	С	D	Modified Count
0	0	1	0	0	0	1
1	1	0	1	0	0	2
2	0	1	1	0	0	3
3	1	0	0	1	0	4 5
4	0	1	0	1	0	5
5	1	0	1	1	0	6
6	0	1	1	1	0	7
7	1	0	0	0	1	8
8	0	1	0	0	1	,9
9	1	0	0	0	0	0
		to	Out	puts code	r	

After the first input pulse, the A' output will go to a low logic level, and as this is a negative-going edge



the B output will go high, giving an output count of two.

It can be seen from the truth table that the normal counting sequence will be followed, but running from one through to zero instead of zero through to nine.

M. R. Oakley, Walsall.

DIGITAL CLOCK TOUCH-SWITCHES

A MAINS alarm clock using the MK50253 clock chip was built, and it was decided that touch-switches were desirable for all functions. The high input impedance, low power consumption and cost, of CMOS i.c.s made them ideal for this purpose, and in fact they worked out cheaper than ordinary push switches!

Two CD4011 quad 2 input NAND gates (G1 and G2) were used. Most of the switches consist of simple refinements to Fig. 1, which is that used for the snooze control. A $10M\Omega$ resistor (R1) holds both the inputs of G1a high, thus giving a low at the output. By placing a finger

across the input and ground, the output goes high, thereby enabling the respective pin on the clock i.c.

The circuit for setting MINUTES, TENS-OF-MINUTES, and HOURS (Fig. 2), is similar, except that two diodes connected to the inputs of G1b and G1c allow the MINUTES to be advanced.

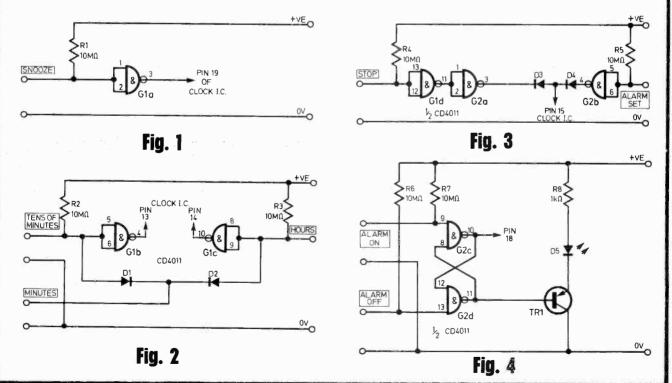
For the RUN, STOP, ALARM SET function, three gates and two diodes are required (Fig. 3). Diodes D3 and D4 are necessary to allow pin 15 of the clock i.c. to be floating when in the RUN mode.

The ALARM ON/OFF circuit shown in Fig. 4 is a simple flip-flop. The l.e.d. D5, and TR1, allow visual indication when the alarm is set.

Power can be derived straight from the existing supply if it does not exceed about 16 volts. TRI can be any cheap p.n.p. transistor such as a 2N3703. Diodes DI to D4 are small signal silicon diodes such as 1N914.

For the touch-plates, pairs of "defunct" metal cased TO18 transistors were used. The heads were passed through small holes in the top of the case, and the appropriate wire soldered to the collector lead, which is usually connected internally to the case of the transistor. This gives a very neat appearance.

G. Watts, Bordon, Hants.



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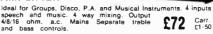
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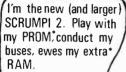
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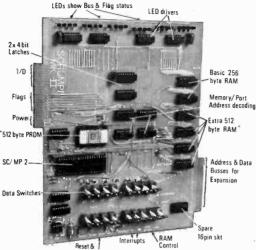
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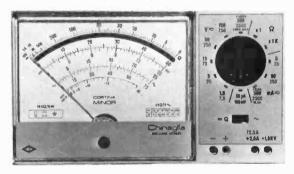
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(Fig. 3), and then etched in the

usual way. After etching, the Veroboard is

replaced on the aligning pins, and used as a template to drill the p.c.b. holes. Finally the Veroboard is stuck to the p.c.b. plain side, once again using the aligning pins, but this time with the addition of pins soldered through to make the necessary connections; see Fig. 4.

This process should work out considerably cheaper and simpler than conventional double sided p.c.b.s.

R. M. Henderson,

Newcastle upon Tyne.

DOUBLE-SIDED BOARD

Sir-There are many cases where double-sided printed circuit board is a necessity, such as to provide a ground plane, or to meet the requirements of certain r.f. circuits. Another situation, where a double-sided p.c.b. would be useful to overcome a logic layout problem is shown in Fig. 1, in which a printed data bus is to feed various i.c.s. To do this on single-sided board would require tedious and untidy hard wired links. The use of conventional double-sided p.c.b. would call for

considerable care to be taken that

both sides aligned correctly. The difficulty can be overcome using single-sided board, by placing a strip of Veroboard, track-side down, on the copper clad surface of the circuit board. The position of the Veroboard is maintained by clamping it to the circuit board via pins inserted in diagonally opposite holes drilled through both boards simultaneously. As shown in Fig. 2, now that the Veroboard is held in register the copper surface can be marked through the Vero-holes with a sharp point. Next the printed circuit can be marked out, incorporating the points made through the Veroboard

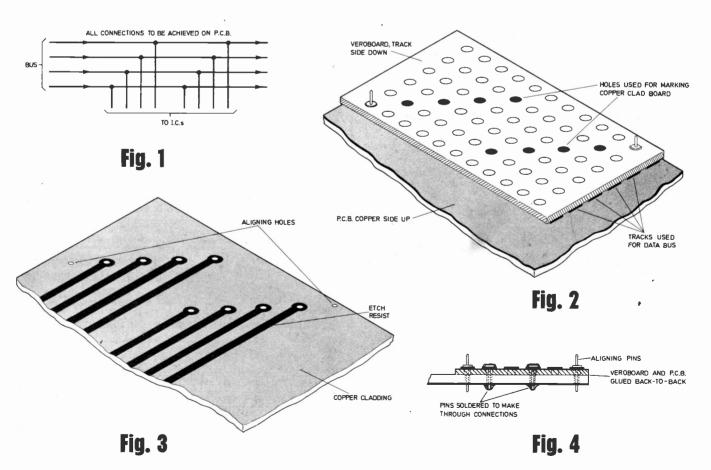
RIGHT DISPLAY

Sir-I would be grateful if any of your readers can explain to me why there are always two versions of 7-segment display available? I refer to the l.h. and r.h. decimal point options.

If only they were manufactured with the decimal point (d.p.) "half way up", we could turn them through 180 degrees and make them into l.h. or r.h. decimal point as required.

A little further thought on the pinout would ensure that no alteration need be made to the segment connections either.

C. P. Finn. Beverley.



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Two tone panel
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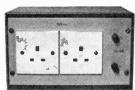
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MJ295	5 1-25	LM301N	0 - 40	NE555	0 - 40	TBA540Q	2 · 30
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MJE3		LM307N	0-65	NE565	1 - 30	TBA550Q	3 · 22
MJE3		LM308C	1-82	NE566	1 - 65	TBA560Q	3 - 22
MJE5		LM308N	0.85	NE567	1-80	TBA570	1 - 29
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TIP290	0 - 60	LM381A	2 - 45	76227N	1 - 20	TCA280A	1 · 30
TIP30/	0-49	LM381N	1.60	76228N	1 - 41	TCA290A	3 · 13
TIP300	0.65	LM382N	1 - 25	76530N	0 - 75	TCA420A	1-84
TIP31/		LM384N	1 - 45	76532N	1-40	TCA730	3 - 22
TIP310		LM386N	0-80	76533N	1 - 20	TCA740	2.76
TIP32		LM387N	1.05	76544N	1 - 44	TCA750	2 · 30
TIP320		LM388N	0.90	76545N	1-65	TCA760	1 - 38
TIP33/		LM389N	1.00	76546N	1.44	TCA800	3 · 13
TIP330		LM702C	0.75	76550N	0 - 35	UAA170	2-00
TIP34		LM709C	0.65	76552N	0.55	UAA180	2-00
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	12 amp	0.85	25	amp	2.00	7445
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			Plastic C106			10 10 10 10 10 10 10 10 10 10 10 10 10 1
100	4 amp 100V	0 · 35 8 amp	100V 0-43 [12 amp 100V	0 - 57	The second second
	4 amp 200V	0.40 8 amp	200V 0 · 49	12 amo 200V	0.65	CERTS.
H	4 amp 400V	0.49 8 amp	400V 0-62	12 amp 400V	0.81	Description of the last of the
П			<u>_</u>	_		
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я		02 Positive 5.		1 - 10		
8	500mA TO2	02 Negative 5	. 12, 15, 24V	1-05		# // //
	1 amp TO22	O Positive 5.	12, 15, 24V	1 - 35		0
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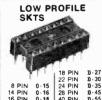
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CD4006	1 - 34.	CD4021	1 - 15	CD4044	1 - 86	CD4066		CD4086		74LS10	0 - 24	74LS160 1-40
CD4007	0.24	CD4022	1-10	CD4045	1 - 59	CD4067		CD4089		74LS13	0.65	74LS161 1-50
CD4008	1 - 10	CD4023	0.24	CD4046	1 - 52	CD4068	0.25	CD4093			0.25	74LS162 1:50
CD4009	0.64	CD4024	0.84	CD4047	1 - 15	CD4069	0 - 25	CD4094	2 · 13	74LS42	1.01	74LS162 1 · 50
CD4010	0.64	CD4025	0.24	CD4049	0.64	CD4070	0.66	CD4095	1.19	74LS74	0 · 48	74LS163 1-50
CD4011	0.24	CD4027	0.64	CD4050	0.64	CD4071	0 - 25	CD4096	1 - 19	74LS75	0.60	74LS164 1 · 52
CD4012	0.24	CD4028	1.02	CD4051	1.06	CD4072	0 - 25	CD4510	2.00	74LS76	0 - 40	74LS173 2-35
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CD4014	1 - 15	CD4030	0.64	CD4053	1.06	CD4075	0 - 25	CD4516	2.00	74LS86	0 - 48	74LS175 1 · 20
D4015	1-15	CD4031	2 - 53	CD4054	1.32	CD4076	1 - 17	CD4518	2.00	74LS90	1.00	1 -44 -
D4016	0.64	CD4035	1 - 34	CD4055	1.50	CD4077	0.66	CD4520	2.00	74LS92	0.90	74LS
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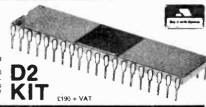
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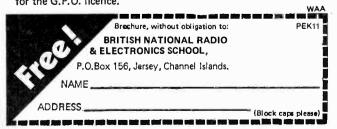
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AC125	0 - 26	BC179B	0-19	BF173	0 20	DC72	8-45	2N3704	0.13*	1/53	0.10*	47/35	6.12*	470, 560, 1000, 1500, 2200, 3000, 4700,	709 (TO99)	0-35p	7401	20p	74192	1-6
AC126	0-26	BC182B	0-12*	BF178	0 - 24	OC74	0-45	2N3705	0.14*	1/75	0·10*	50/10	0.10*	10000 47000pf; 1MFD 10V. All at 6p*	709 (8 PIN DIL)	0 · 40p	7402	180		
AC127	0 - 28	BC182L	0-117	BF179	0 - 25	OC81	0 - 60	2N3707	0.12"	2 · 2/25	0.10*	50/15	0.10*	each. 1MFD 63V 8p*.	741 (8 PIN DIL)	0-28p	7403	180		
AC128	0 - 20	BC183B	8-10*	BF183	8 - 34	OC82	0-70	2N3708	0.12*	2 · 2/63	0.10*	100/18	0.06*		AY-5-1224	3-75p	7404	23p	C/MOS	
AC151	0 · 35	BC183L	0-10*	BF184	0 - 25	ORP12	0 - 68	2N3709	0-14*	2-5/64	0-10*	100/25	0-10"	RESISTORS 2p* each	AY-3-8500 T.V.		7407	40 p	4000	0 - 19
AC153	0.35	BC184B	0-12°	BF185	0 - 28	TIP29A	0.47*	2N3710	0·11°	4-7/16	0.08*	100/35	0-11*	One-third WATT E12 (5%)	Game	6-00p	7408	240	4001	0-18
AC176	0 - 22	BC184L	0-11*	BF194	6-10-	TIP30A	0.56"	2N3711	0-11*	4 - 7/63	0.10*	100/50	0.15*	1 ohm-10m ohm.	CA 3130	0-87p°	7410	18p	4002	0.19
AC187	0.22	BC186	0-25	BF195	0 - 10 °	TIP31A	0 - 57	2N3819E	0 - 25*	5/10	0-10*	100/35	0 · 15*	t onm-tem onm.	LM 301AN	0 · 55p	7411	240	4006	1-45
AC188	0 - 20	BC187	8-26	BF196	0-12*	TIP32A	0-67	2N3820	0.45*	5/16	0.11*	220/16	0 · 15*		LM 308	1-40p	7412	25p	4007	0-19
187/188		BC204A	0-16*	BF197	0.12*	TIP33A	0-94	2N3823E	0.25*	6-8/25	0.10*	220/25	0.16*	POTENTIOMETERS	LM 309K	2 · 00p	7413	38p	4008	1.49
ntch. pr		BC204B	0-16"	BF199	0 - 15*	TIP34A	1-13	2N4036	0 - 40	6 8/40	0-10*	220/63	0.25*	Lin/Log.	LM 324	2-05p	7414	72p	4009	0.58
AD149	0.68	BC209B	0 - 13*	BF200	0-38	TIP41A	0 67	2N4058	0.16*	8/70	0.10*	250/12	6·12*	5K. 10K. 25K. 50K. 200K. 250K. 500K.	LM 380/SL60745	1-29p*	7416	36p	4010	0.58
AD161	0.52	BC212A	0-13*	BFX29	0.26	TIP42A	0 - 80	2N4059	0.10*	10/16	0.09*	250/50	8-18*	1M, 2M, 25p* each.	LM 381N	2-00p*	7417	36p	4011	0 - 19
AD162	0.52	BC212L	0 - 15°	BFX30	0.25	TIP2955	0-97	2N4061	0.12*	10/25	0.09*	250/64	8 - 20 *	Im, zm, zsp · each.	LM 555	0 · 49p	7420	18p	4012	0-19
ntch. pr	1 - 24	BC213B	0.12*	BFX40	0 - 28	TIP3055	8-60	2N4124	0.20*	10/35	0 - 10*	330/16	8 · 15*		LM 723	0 · 59p	7421	26p	4013	0.54
F116	0 - 24	BC213L	0-14*	BFX84	0-22	TIS43	6·35*	2N4126	0.30*	10/64	0.10*	470/6V3	0 - 10 *	PRESET MIN. VERT.	LM 3900N	0 · 69p	7427	32p	4014	1-42
F117	0.28	BC214	0-15°	BFX88	0 - 22	ZTX109	0-14*	2N5298	0.50	10/250	0.18*	470/10	8 · 12*		MC 1310/CA1310E	2-550"	7428	50p	4014	1-16
F124	0.30	BC214L	0-17*	BFY50	0 · 25	ZTX300	0.13*	2N5457	0.50	15/40	0 - 10*	470/16	0.18*	SUB MIN V & H.	MC 1327/SN76227	1-35p*	7430	18p	4015	0 - 52
F185	0.95	BC237A	0.16*	BFY51	0-25	ZTX301	0 - 13*	2N5458	0.40*	15/400	0.35*	470/25	8-20°	100ohm, 220ohm, 470ohm, 1K, 2K2,	MC 1330P	0.75p°	7432	28p	4016	1-12
F239	0-46	BC238A	8-15*	BFY52	0 · 25	ZTX302	8-18*	2N5459	0.40*	16/10	0.10*	680/25	0.25*	4K7, 10K, 20K, 50K, 100K, 250K, 470K,	MC 1350P	0-750°	7437	42p	4018	1-81
U113	2 · 20°	BC261A	0-16	BSX20	0.23	ZTX500	0.15*	2SC1172	3.00*	20/15	0.10*	1000/16	0.25*	1M; 2M2, Sp* each.	NE 555	0 - 490	7440	180	4019	
C107	0-11	BC262A	0 - 19	B-U108	2-50*	ZTX502	0-18*	40361	0.50	20/70	0-10*	1000/25	0-30*		SK 1122 T.V.		7442	58p	4019	0-51
C107A	0.12	BC267A	0.17	BU208	3.00*	ZTX504	0.25*	40363	88.0	22/6V3	0-10*	1000/50	0.40		Game	19 - 00p	7443	1-00p		
C107B	0.13	BC268B	0-17	BY126	8-16	ZTX530	0.23*	40673	0.65	22/16	0.10*	1500/25	0-35*	THYRISTORS	SN 76003N	2-80p*	7444	1-00p		
C108	0 - 10	BC269	0 - 17	BY127	8-16	1N914	0.05	100.0		25/25	8-11*	2200/6V3	8-30*	60V 1A 0-25	SN 76013ND	1-60p*	7446	1-00p	DIODES	
IL108	0.08	BC287	0.28	BY133	0 - 20	1N4001	0.05	l		33 50	8-12*	2200/40	0.60*	100V 1A 0-36 TAG 1 100	SN 76013N	1-750*	7447	98p	50V 3A	
3C108B	0-11	BC300	0 - 35	BY164	0 - 40	1N4002	0.06	l		47/6V3	0-10*	2500/15	0.45*	200V 1A 0-60 TAG 1 200	SN 76023N	1-75p*	7448	96p	100V 3A	0 - 13
C108C	0-12	BC301	0-34	ME0401	0-18*	1N4003	0.07	l		47/10	0 - 10°	3300/30	0.45*	600V 1A 0-80 TAG 1 600	SN 76023ND	1-60p*	7451	18p	200V 3A	0-15
C109	0 - 12	BC303	0 - 35	ME0402	0.18*	1N4004	0.08			47/16	0 · 10°	5000/12	0.45*	700V 1A 1-40 BT 106	SN 76033N	2-75p*	7460	18p		0 - 10
C109B	8-13	BC327	0.20*	ME0411	0.18*	1N4005	0.09	TRANS-						400V 4A 0-65 C106D1	SN 76660	0.90p*	7470	32p	400V 3A	0 - 21
C109C	0-13	BC328	0-18*	ME0412	0-19*	1N4006	0 - 10	FORMER	s	-			_	500V 6+A 1-85 BT 109	TAA 550	0.60p*	7472	30p		
C117	0-18*	BC338	6-16*	ME0413	0.15*	1N4007	0:11	6-0-6 100n		POLY, R/L	ead 10VD	C			TBA 120ASQ	1-30p*	7473	30p		
C136	0-16*	BC310	0.16*	ME0414	0-15*	1N4148	0.05		1-20	-001	0.06*				TBA 395	2-25p*	7474	35p	BRIDGES	
C142	0.24	BC340	8-15*	ME0461	0.21*	1N5400	0.13	9-0-9 75m		-0022	0.06*	- 068	0.07*	ZENERS (400mw) BZX 83	TBA 480C	1-25p*	7475	49p		0 - 21
C143	0-24	BC461	0.35	ME0462	0.21*	1N5401	0.15		1-20	-0033	0.06*	-1	0.07*	3V, 3V3, 5V1, 5V6, 7V5, 9V1, 10V, 12V.	TBA 520Q	1-70p*	7476	32p	100V 1A 200V 1A	8 - 30
C147A	0.09*	BC557	0.15*	ME4001	0-14*	1N5404	0-21	9-0-9 ‡A	3 - 20	-0047	0.06*	- 15	0.08*	18V. 22V. 30V. All at 12p* each.	TBA 530O	1-90p*	7480	65p	400V 1A	
C147B	0-10*	BC558	0.15*	ME4101	0-11*	2N708	0.20		50mA	-0068	0.06*	-22	0-10*		TBA 540Q	1-90p*	7481	1.00p		0-3
C148	0.09*	BC559	0·15*	MJE340	8-76*	2N1613	0 - 30		1 - 30	-01	0.06*	-33	0.11*		TBA 550Q	3-40p*	7485	1.30p	400V 2†A	0.6
C148B	0-10°	BCY70	0 15	MJE3055	1-25*	2N1711	0.30	12-0-12 1A		-015	0.07*	-47	0-15*	LED TIL 209/0 -125 0-2	TBA 560CQ	2-30p*	7486	43o		
C149	0-10*	BCY71	0.18	MPF102	0-40"	2N2102	0.50	min O/F		-022	0.07*	-1 250V	0 - 10 *	Red 20p 20p	TBA 641	2-55p*	7490(A)	55p		
C149B	0.11*	BCY72	0.14	- 0A5	0.71	2N2219	6.30	OC71/2 u		-033	0.07*	-1 600V	0.15*	Green 29p 29p	TBA 750	1-90p*	7492	55p	OFFER	
C149C	0.11*	BD123	0.90	0A10	0-62	2N2222	0 - 20		280mA	-047	0.07*	1-0 400V	0.12*	Clip for above 3p	TBA 800Q	1-35p*	7493	55p	RED LED's	
153	0.18*	BD124	0.90	OA47	8-14	2N2646	0.65	1	2.40						TBA 810SQ	1-49p*	7496	90p		10 for £
154	0.18*	BD131	0.42	OA81	0-30	2N29260	0.13*	12-0-12 15							TBA 820Q	1-20p*	74107	40p	RED LED's	
2157	0-12-	BD132	0.42	OA90	0.07	2N29266	0.15*		2 - 40	TANTALUI	M BEAD				TBA 920Q	2-80p*	74121	38 p		10 for £1
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	0-12*	BD140	0.58	OA95	80.0	2N3054	0-58	P-1K2	80	0-15MFD/3		6-8 MFD/	16V 13p*	SK 1122 TV same kit salam and	TCA 270Q	2-20p*	74141	80p		00 for CI
	0-12*	BD155	0.75*	OA200	0 10	2N3663	0 - 28	200mW	50p	0 - 22MFD/3			6V3 13p*	SK 1122 TV game kit colour and sound incl. P.C.B. semicons., pots.	U 14552 300mW	.,	74145	1·15p	2N3702	
	0.15*	BDY20	0.80	OA202	0-11	2N3055	0-60	-	-ob	0-47MFD/3			10V 14p*		Audio with data	0-35p*	74151	94p		00 for El
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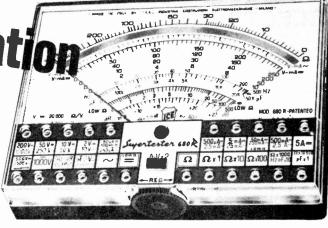
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N.B. Colum			ernal trig	ger; (b)	with inte	rnal trig	ger.			

MEMORIE

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Our Seminar will be held on 26th

	November at the Wembley Con
Land Co.	ference Centre 10 a.m-5 p.m. We hope
	to have five speakers from various
S	backgrounds but all specialists in the
	micro-computing/software field. The
3 · 60	NASCOM I micro-computer will be
4 - 75	launched at the seminar. Tickets a
7 · 95	£3.50 each are now available togethe
2 · 50	with a newsheet on the seminar
10.00	Please write or telephone for details
4 - 50	Only 40p seats are available and 11
8 - 50	have been sold at press time.
0.30	

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0.30

0.32

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7441AN 0-76

7447AN 0-81

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2-00* 1.50* 2.00* CA3045 0.85* 0.82 CA3046 0.80* 1.07 CA3130 0 - 35 MC1304P 1.60* MC1307P 0.85* 0 - 34 MC1310P 0.47 MC1351P 1.20* 0.65 MC1352P 0-75* 0.78 MC1458P 0:77 0.68 MC1496L 0-82* 1 - 30 **SAS**560

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TCA270SQ

TAA310A

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TRANSISTORS AC126 0-15 BC117 0-19" BC300 0-34 BDY20 0-80

AC127	0.16	BC119	0 - 25	BC301	0 - 32	BDY38	0.60	BFY41	0.60	OC72	0.22	2N2905A	0 - 22	
AC127 AC128	0-16	BC125			0.40	BDY60	1.70		0.20	OC84	0-40	2N2906	0-18	
AC128K	0 25	BC126			0.46	BDY61	1.65	BFY51	0.18	OC139	1.30	2N2925	0-14*	
AC141	0 23	BC140		BCY30	0.55	BDY62	1-15	BFY52	0.19	OC140	1 - 30	2N2926O	0.09*	
	0.22	BC141			0.55	BDY95	2-14	BFY53	0 - 25	OC170	0.23	2N2926FI	0.10*	
AC141K AC142	0.18	BC142		BCY32	0-60	BF121	0.50	BFY64	0 - 35	TIP29A	0.44*	2N2926Y	0.09*	
	0.10	BC143	0.23	BCY33	0.55	BF123	0.50	BFY90	0.90	TIP30A	0.52*	2N2926G	0-10*	
AC142K		BC143	0.30	BCY34	0.55	BF179	0.30	BSX19	0.16	TIP31A	0.54	2N3053	0.20	
AC176	0·16 0·32	BC147	0.09*	BCY38	0.50	BF180	0.30	BSX20	0-18	TIP32A	0.64	2N3055	0.50	
AC176K	0.32	BC148	0.09*	BCY39	1.15	BF181	0.30	BSX21	0 - 20	TIP41A	0.68	2N3137	1 - 10	
AC187		BC149	0.09*	BCY40	0.75	BF182	0.30	BSY52	0.28	TIP42A	0.72	2N3440	0.56	
AC187K	0.36	BC152	0.25*	BCY42	0 - 30	BF183	0.30	BSY53	0 - 39	2N404	0.40	2N3442	1 - 20	
AC188	0.18	BC 152	0.18*	BCY54	1.60	BF184	0.20	BSY54	0.33	2N696	0.20	2N3570	3-60	
AC188K	0.32	BC157	0.09*	BCY70	0.12	BF185	0.20	BSY55	0-74	2N697	0.20	2N3702	0 - 10*	
AD149	0.80	BC158	0.09*	BCY71	0 - 18	BF194	0.10*	BSY65	0-30	2N706	0.15	2N3703	0.10*	
AD161	0.35	BC159	0.09*	BCY72	0.12	BF196	0.12*	BSY95A	0.16	2N718	0-22	2N3704	0.10*	
AD162	0.35	BC160	0.32	BD115	0.55	BF197	0.12*	BU105	1-80*	2N929	0.16	2N3705	0.10*	
AF114 AF115	0.20	BC161	0.38	BD131	0.36	BF224J	0.18*	BU105/02		2N1131	0.15	2N3706	0.10*	
AF116	0 - 20	BC168	0-09*	BD132	0.40	8F244	0.17*	BU108	3.00*	2N1132	0.16	2N3707	0.10*	
AF117	0 - 20	BC169	0.12*	.BD135	0.36*	BF257	0 - 30	BU109	2.50*	2N1302	0 - 40	2N3708	0.09*	
AF117	0.50	BC169C	0-14*	BD136	0.39*	BF258	0.35	BU126	1.60*	2N1303	0.40	2N3709	0.09*	
AF116	0.25	BC182	0.11*	BD137	0.40*	BF259	0.48	BU133	1.60*	2N1304	0 - 45	2N3710	0.10*	
AF124 AF125	0.25	BC182L	0.12*	BD138	0 - 48*	BF336	0.35*	BU204	1.60*	2N1305	0 - 45	2N3711	0-10*	
AF125	0.25	BC183	0.10*	BD139	0.58*	BF337	0.32*	BU205	1.90*	2N1306	0.50	2N3715	1.70	
AF139	0.25	BC183L	0.10*	BD144	2 - 20	BF338	0.45*	BU206	2-40*	2N1307	0.50	2N3716	1-80	
AF239	0.37	BC184	0-11*	BD157	0-60	BFW30	1.25	BU208	2.60*	2N1308	0 : 60	2N3771	1-60	
AL102	1-45	BC184L	0.11*	BD181	0.86	BFW59	0 - 30	MJ480	0-80	2N1309	0 - 60	2N3772	1-90	
AL103	1-30	BC186	0.20*	BD182	0-92	BFW60	0.36	MJ481	1.05	2N1711	0 - 24	2N3773	2 - 10	
AU107	3.30*	BC187	0.24*	BD183	0.97	BFX29	0 - 26	MJ490	0.90	2N2102	0.44	2N3819	0.28*	
AU110	1.75*	BC207B	0.12*	BD184	1.20	BFX30	0.30	MJ491	1-15	2N2217	0 - 30	2N4347	1 - 10	
AU113	1-60*	BC212	0.11*	BD232	0-60	BFX84	0 - 23	MJE340	0.40*	2N2369	0.14	2N4348	1.20	
BC107	0.09	BC212L	0.12*	BD233	0 - 48	BFX85	0 - 25	MJE520	0 - 45	2N2369A	0.14	2N4870	0.35*	
BC107B	0.12	BC213	0.12*	BD237	0.55	BFX86	0 - 25	MJE521	0.55	2N2483	0 - 20	2N4871	0.35*	
BC107B	0.12	BC213L	0-14*	BD238	0.60	BFX87	0.20	OC43	0-95	2N2484	0 - 16	2N4918	0.60°	
BC108B	0-12	BC214	0.14*	BD410	0.60	BFX88	0.20	OC44	0'-32	2N2646	0.50	2N4919	0.70*	
BC109B	0 - 12	BC214L	0.15*	BDX32	2 - 30	BFX89	0.90	OC45	0 - 32	2N2711	0.20	2N4920	0 · 50°	
BC109B	0.12	BC237	0.16*	BDY10	1.50	BFY11	1 - 10	OC46	0 - 20	2N2712	0.15	2N4922	0.58*	
BC109B	0.12	BC238	0.16*	BDY11	2.00	BFY18	0.50	-OC70	0 - 30	2N2904A	0 - 20	2N4923	0.46*	
DC 109C	0.12	00200	0.10	50111		2								

CMOS PLASTIC 4000BF 0.20

4001BE 0·20 4002BE 0·20 4006BE 0:05

4007BE 0:20

4008BE 0.93 4009BE 0.52 4010BF 0-52

4010BE	0.52	
4011BE	0 · 20	
4012BE	0.20	1
4013BE	0.50	ı
4014BE	1.00	ı
4015BE	0.95	
		1
4017BE	1.00	ŀ
4018BE	1 · 10	L
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4069BE 0-30

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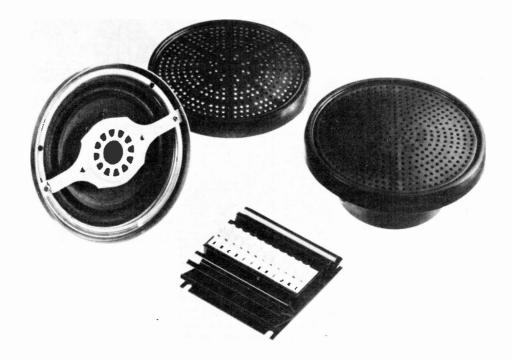
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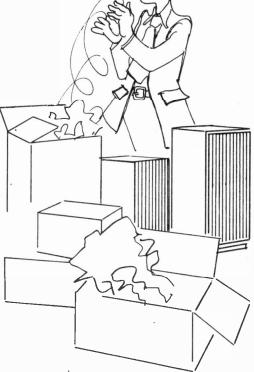
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How does the first-time buyer separate the hi-fi basics from the hi-fi mystique? This month Practical Hi-Fi & Audio gives basic advice on making the right choice of system, basic fault-finding and setting up, and publishes answers to the ten questions most frequently asked by newcomers.

A System for £800

An evaluation of the new crop of moving-coil phono cartridges and their complementary voltage step-up devices. Among those tested are the Fidelity Research FR 3, Entré 1, Sony XL55, Ultimo 10A, and Nakamichi 1000, and 7 others.

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Another big competition, with the new Autumn range of Aiwa equipment to be won.

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Complete instructions for building Chris Rogers' outstanding new valve amplifier.



November issue

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K007 Electrolytic capacitors 25V working, small physical size. 10 each of these popular values: 1, 2·2, 4·7, 10, 22, 47, 100μF. Total 70

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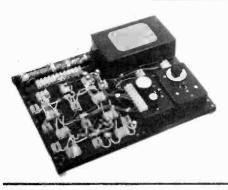
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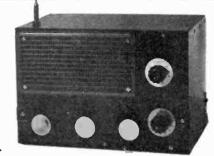
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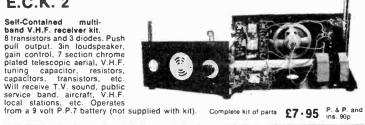
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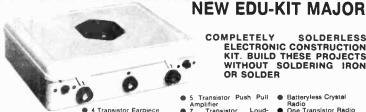


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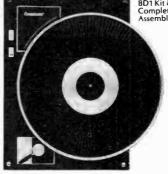
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Practical Electronics November 1977

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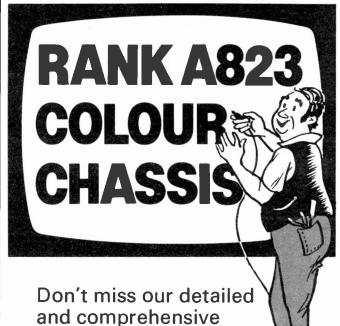
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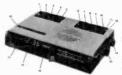
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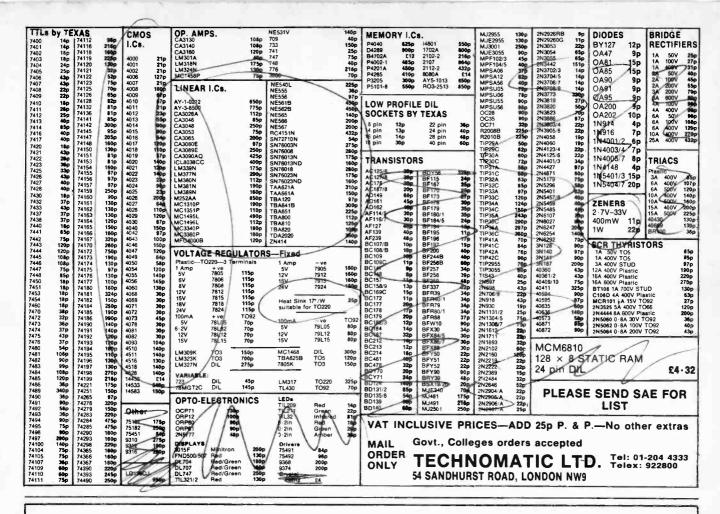
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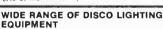
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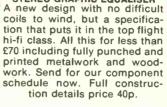
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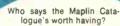
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