PRACTICAL ELECTRONICS MARCH 1976

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# ELECTRONICS

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Our April issue will be published on Friday, March 12, 1976 (for details of contents see page 223)

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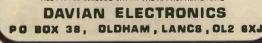
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2N2147 2N2148	0.78	BC160 BC169	0.63	QET882	0.35	0C45 0C45M 0C46	0.18	7428 7430	0.40 0.16
2N2160 2N2218	0.78	BCY31 BCY32	0.45	GET885 GEX44 GEX45/1 GEX941	0.08	OC57 OC58	0-80	7432	0-37
2N2219 2N2369A	0.25	BCY33 BCY34	0.38	GEX941 GJ3M	0.45	0039	0.60	7437 7438	0.37
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AC126 AC127 AC128	0-25	BFX84 BFX85 BFX86	0.25 0.28 0.25	NKT272 NKT273 NKT274 NKT275	0-20 0-20 0-20	OC203	1.50	74118 74119	0.90
AC128 AC187 AC188	0-15 0-21	RFX87	0.25	NKT275	0.20	OC204 OC205	1.50 1.75 1.10	74121 74122	0-50
ACY17	0-20 0-75	BFX88 BFY10 BFY11	0-50	NKT277 NKT278 NKT301	0.25	0C206 0C207 0C460	1.00	74123 74141	1.00
ACY18 ACY19	0.27	BFY17 BFY18	0.40	NKT304 NKT403	1.00	0C470 0CP71	0.30	74145 74150	1-26 1-75
ACY20 ACY21 ACY22	0-85 0-35 0-35	BFY19 BFY24 BFY44	0.55	NKT404	1.00	ORP12 ORP60	0.60	74151 74154	1.00 2.00
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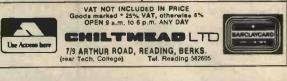
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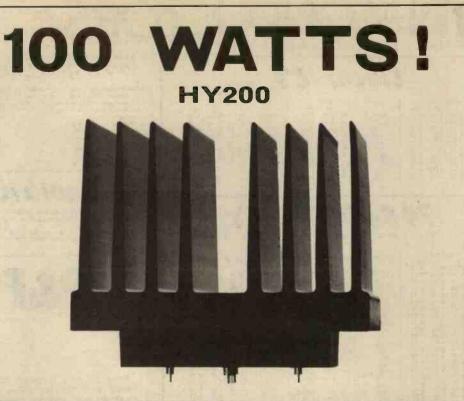
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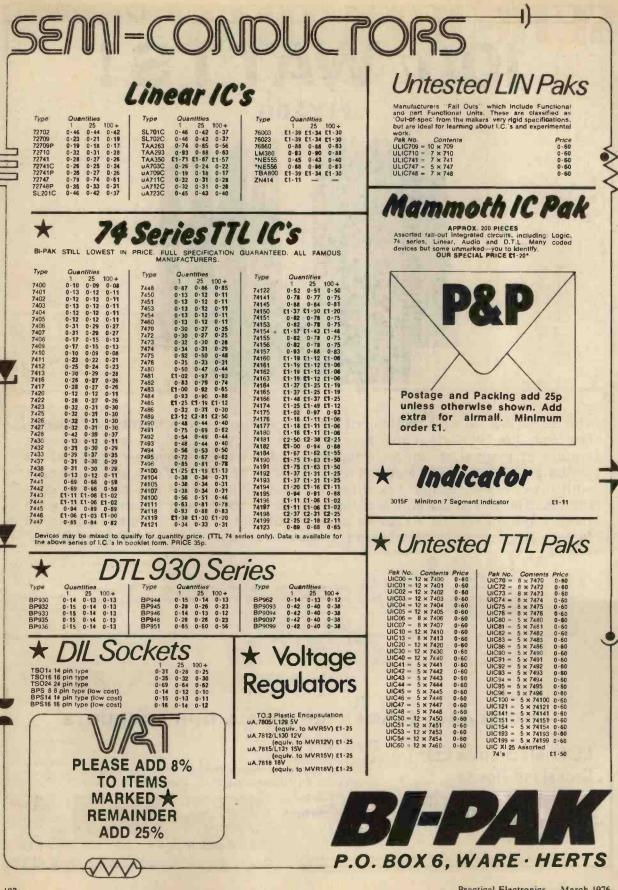
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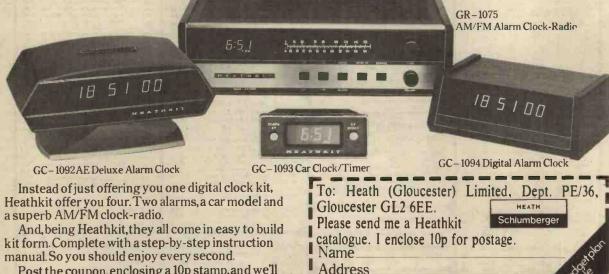
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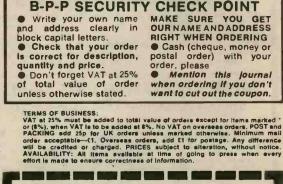
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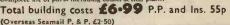
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8 Transistors and 3 Diodes 6 Transite wavebands: MW, LW, SW1, SW2, SW3 and trawler band. Sensitive forrite rod aerial tor MW and LW. Telescopic aerial for short waves. Sin speaker, 8 improved type transistors plus 3 diode. Attractive case in black with rod grille, dial and black knobs with polished metal inserts 81se 91n x 3 jin x 21in approx. Push pull output. Battery economiser switch for extended battery IIfe. Ample power to drive a larger speaker. Complete kit of parts including construction plans.





3 In approximation of parts including construction plans. Complete kit of parts including construction plans. Building **£3**-99 (Overseas Seamail Conts: P. & P. (2.30)

V.H.F. AIR **CONVERTER KIT** Build this converter kit and

receive the aircraft band by placing it by the side of a radio tuned to medium wave or the long wave band and operating as shown in the instructions supplied free with all parts.

Uses a retractable chrome plated telescopic aerial, gain control, V.H.F. tuning capacitor, transistor, etc.

All parts including case and plans

£4.35 P.P. & Ins. 40p

## **ROAMER TEN MARK 2**

WITH VHF INCLUDING AIRCRAFT Now with free carplese and switched socket. 10 translators, Latest Sin x 3in louaspeaker, 9 tuneable warebands, MWI, MW2, LW, SWI, SW3, Ki rawler band, Bill in fertite root aerisal to: MW/LW. Chrome plated of soction relescopic erial, can be angled and rotated for peak short wave and VHF listening. Push puil output using 600mW translators, Car aerial socket. 10 translators plus 3 diodes. Garged tuning condenser with VHF section. Separate coll for alrecaft band. Yolume parks to change and tone controls. Attractive Gare in rich changue and tone controls. Attractive Sin X in x din. Easy to follow instructions and Common. or marks including construction plane.

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ingrams. complete kit of parts including construction plans.

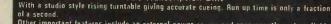
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#### New from Connoisseur - BD3 Transcription Unit



Other important features include an external power source and consequently no hum field. A belt driven turntable with neon illuminated stroboscopic disc with 3 speeds, 33, 45 and 78 - all featuring variable control.

The BD3 arm is lightweight and incorporates a unique method of magnetic stabalisation with an interchangeable head shell tracking







#### cartridges down to 0.6 grams. The unit features brushed aluminium trim and is

mounted on a matched wooden plinth complete with acrylic dust cover.

**BD2** Turntable Assembly

The famous BD2 belt drive turntable features push button speed change, an SAU2 pick up arm with damped lowering device, brushed aluminium trim. and specially designed turntable mat.

It is available in chassis form, or as illustrated mounted on a slimline wooden plinth, with acrylic cover which features an easy hinged on hinged off

#### **BD1** Turntable Kit

The BD1, well known for its excellent performance and superb quality is available in kit form, which

allows greater freedom of choice for the practical enthusiast with regard to mounting, selection of arm etc. Construction is simplicity itself with no soldering required. Now it's easy to own the best.

#### SAU2 Pick Up Arm

Recognised as one of todays most advanced pick up arms. Among its star leatures is an Auto Bias compensator, hydraulic lowering device, precision balance and an adjustable head shell which can be matched to a wide variety of decks and pick up cartridges, ideal

for the demanding practical audiophile. For further details of all Connoisseur products, the BD3 or BD2, the BD1 kit or SAU2 arm, to the still popular SCU1 cartridge and our precision stylus balance, please contact your dealer or send a stamp for brochure

Manufactured by:-

A.R. Sugden & CO. (Engineers) Ltd. Atlas Mill Rd. Brighouse, Yorks, HD61ES Tel: Brighouse (04847) 2142. Telegrams & Cables: Connoiseur, Brighouse.

## INVERTORS

Top left: The BD1 Turntable Kit.

Top: The SAU2 pick up arm.

Assembly.

Unit.



240y-50Hz from your 12y car battery.

25 watt-£4.20 40 watt-£7.35 40 watt-£7.35 75 watt-£10.71 150 watt—£19·10 300 watt (12v)—£29·85 300 watt (24v)—£23·75

All above invertors are in kit form but may be purchased built up in metal case & ready for use. Price list sent on receipt of s.a.e. Prices include post & packing.

#### P.W. AUTOMATIC EMERGENCY

SUPPLY 240v-50Hz-150 watt invertor with built in battery charger. In event of power failure switches over automatically from battery charging to invertor operation. Cct. as appeared in Dec. 72 P.W. Complete kit of parts (excluding meter) £22-50 + £1-10 p. & p.

FLUORESCENT LIGHT INVERTOR KIT 8 watt-12v-Fluorescent light, suitable for tents, caravans, houses, boats & secondary

lighting for factories, hotels, etc. 12"-8 watt-£2:90 + 25p p. & p. Built up-£4 + 25p. 21"-13 watt-£3:30 + 30p p. & p. Built up-

£4-50 + 30p. TRANSFORMERS & COILS

Both high volume & small order capacity available.

Special offer. Miniature mains transformer 12-0-12v-6V.A.-85p plus 10p p. & p. TRADE & EXPORT ENQUIRIES WELCOMED P.E. ORION STEREO AMPLIFIER



20 + 20 Watts r.m.s. into 8 ohm load, Distortion less than 0.01% 100Hz-10kHz. Frequency response ± 1dB 20 Hz to 20 kHz. Hum level virtually nil with vol. full on.

This is a power amplifier of superb quality incorporating the very latest design features. Professional hi-fi enthusiasts have classed it as fantastic and real value for money. The CCT incorporates a low flux transformer and inputs for disc. tape, tuner, etc.

Complete kit of parts including slim line bookend case, silk screened front panel & knobs. £43 incl. VAT & p. & p.

The bookend case, I.C.s & semiconductors, P.C. board, Transformer, etc. may be purchased separately if desired. Send S.A.E. for further information

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ASTRO IGNITI

ASTRO IGNITION SYSTEM Complete kit of parts for this proven and tested system £9.50 Incl. VAT. Ready built with only two connections to alter £12.50 incl. VAT. Thousands have used this system both home and abroad. Consider these advantages more power, faster acceleration, fuel economy, excellent cold starting, smoother running, no contact breaker burning. Also because of the high energy spark, the fuel mixture can be made weaker giving further economy and fewer plug problems. Fitting time when built 5 minutes approx. Please state whether positive or negative earth. Trade and export enquiries welcomed.

**ASTRO ELECTRONICS** Spring Bank noad, West Park Chesterfield.

Top right: The BD2 Turntable **Right: The BD3 Transcription** 



Trade and export enquiries welcome

A Marshall (London) Ltd Dept PE 42 Cricklewood Broadway London NW2 3ET Tel 01-452 0161 2 Telex 21492 & 85 West Regent St Glasgow G2 20D Tel: 041-332 4133 & 1 Straits Parade Fishponds Bristol BS16 2LX Tel 0272 654201 2 8 27 Rue Danton Issy Les Moulineaux Paris 92 Tel 644 2356 Catalogue price 25p

Тор	500 S	emico	nduo	ctors f	rom	the La	rges	Rang	e in	the U.	к.					ala huebdar
2N456	0-80	Orange	0-12	2N5192		AF106	0-40	BC186	0.25	BF159 BF160	0-27	LOO5T1	1.50	OC35	0-60	MULLARD RADIO MODULES
2N456A 2N457A	0-85	2N3053 2N3054	0-25	2N5195 2N5245	0-47	AF109R AF114	0-40 0-35	BC187 BC207	0.12	BF163	0.32	LM380 LM381	2.20	OC42 OC45	0-50	RF/IF AMPLIFIER LP1173 £6-68
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2N493 2N696	5-20	2N3391A 2N3392	0-29	2N5298 2N5457	0-50	AF118 AF124	0.35	BC214L BC237	0-18	BF177 BF178	0-29	8DtL 14DIL	0-38	OC83 ORP12	0-24	LP1183/2 £4-32 LP1184/2 £7-18
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2N706	0-14	2N3403	0-19	2N5494	0-58	AF139	0.85	BC253 BC257	0.25	BF182	0.35	TO99	0-40	SL611C	1.70	FM TUNER
2N706A 2N708	0-16	2N3414 2N3415	0-20	2N5496 2N5777	0-61	AF186 AF200	0-46	BC257 BC258	0-16	BF183 BF184	0.55	8DIL 14DIL	0-40	SL612C SL 620C	1.70	LP1186 £6-88 LP1400 £7-22
2N709	0-42	2N3416 2N3417	0.24	2N6027	0-45	AF239	0.65	BC259	0.17	BF185	0.30	LM747	1.00	SL621C	2.60	LF1400 EF-22
2N711 2N718	0-50	2N3440	0.29	3N128 3N139	0.73	AF240 AF279	0-90	BC261 BC262	0.25	BF194 BF195	0-12	LM748 8DIL	0.60	SL623 SL640C	4-59	
2N718A	0.28	2N3441	0-97	3N140	1.00	AF280	0-79	BC263	0-25	BF196	0.13	14DIL	0.73	SL641C	3.10	
2N720 2N914	0.57	2N3442 2N3638	0.15	3N141 3N200	0-81	AL102 AL103	1-00	BC300 BC301	0.38	BF197 BF198	0-15	LM3900 LM7805	0.70	SN76003N SN76013N	2.92	P.C. MARKER PEN DALO 33PC. 87p. ZENER DIODES 400MW 11p, 1W 17p,
2N916	0.28	2N3638A 2N3639	0.15	40361	0-40	8C107	0.14	BC302	0.29	BF200	0-40	LM7812	2.50	SN76023N	1-60	2.5W 35p.
2N918 2N929	0.32	2N3641	0.17	40362	0-45	BC108 BC109	0-14	BC303 BC307	0-54	BF225J BF244	0-23	LM7815 LM7824	2.50	SN76033N	2.92	IC SOCKETS 8 DIL 10p, 14 DIL 14p, 16 DIL 13p.
2N930	0.22	2N3702	0-12	40389	0-48	BC113	0.15	BC308A	0.15	BF245	0-45	MC1303	1.50	TAA263	1-10	RESISTORS +W 2p (100 per value 0.013p):
2N1302 2N1303	0-19	2N3703 2N3704	0.15	40394 40395	0.56	BC115 BC116	0.17	BC309C BC317	0.20	BF246 BF247	0-58	MC1310 MC1330P	2-50	TAA300 TAA350	1-80	W 3p (100 per value 0.014p). SCORPIO CAR IGNITION KIT £12.50.
2N1304	0.26	2N3705 2N3706	0-16	40406 40407	0-44	BC116A BC117	0-18 0-21	BC318	0.12	BF254	0-19	MC1351P	0.60	TAA550	0-60	JUMBO 7 SEGMENT DISPLAYS E2.
2N1305 2N1306	0-24	2N3707	0-18	40408	0.35	BC118	0-14	BC337 BC338	0-20	8F255 BF257	0-19	MC1352P MC1466	0-80	TAA611C TAA621	2.18	DL 707 £1-75. MINITRON £1-55.
2N1307	0-30	2N3708	0-14	40409	0-52	BC119	0.29	BCY30	0-80	BF258	0.53	MC1469	2.75	TAA661B	1-32	LEDs Red, Yellow, Green, 16 dia. 31p.
2N1308 2N1309	0-47	2N3709 2N3710	0-15	40410	2.00	BC121 BC125	0.35	BCY31 BCY32	0-85	BF259 BFR39	0-55	ME0402	0-20	TBA641B TBA651	2.25	20 dia. 33p.
2N1671	1-54	2N3711 2N3712	0.15	40594	0.74	BC126	0.23	BCY33	0-85	BFR79	0-24	ME0412	0-18	TBA800	1-40	STREET, STREET
2N1671/ 2N1671E	1.67	2N3713	1.20	40595	0-64	BC132 BC134	0.30	BCY34 BCY38	0-79	BFS21A BFS28	2.30	ME4102 ME4104	0-11	TBA810 TBA820	1-40	
2N1711	0-45	2N3714 2N3715	1-38	40602 40603	0-61	BC135 BC136	0-13	BCY39	1.50	BFS61	0.27	MJ480	0.95	TBA920	2.30	SEE MARSHALLS FOR CMOS
2N1907 2N2102	5-50	2N3715	1.60	40603	0-58	BC136 BC137	0.17	BCY40 BCY42	0-97	BFS98 BFX29	0.25	MJ481 MJ490	1-20	TIL209 TIP29A	0-30	
2N2147	0.78	2N3771 2N3772	2.20	40636	1.10	BC140	0-58	BCY58	0.30	BFX30	0.27	MJ491	1-45	TIP29C	0-80	CD4001 0-18 CD4019 0-52 CD4043 0-83
2N2148 2N2160	0-94	2N3773	2.65	40669 40673	1.00	BC141 BC142	0-68	BCY59 BCY70	0.32	BFX84 BFX85	0.24	MJ2955 MJE340	1-00	TIP30A TIP30C	0-58	CD4002 0-18 CD4020 0-98 CD4044 0-77 CD4006 0-99 CD4021 0-88 CD4045 1-30
2N2218/		2N3789	2-06	AC126	0.20	BC143	0.25	BCY70 BCY71	0.17	BFX87	0.28	MJE2955	1.20	TIP31A	0-62	CD4007 0-18 CD4022 D-85 CD4046 1-20 CD4006 0-82 CD4023 0-18 CD4047 0-85
2N2219 2N2219/	0-24	2N3790 2N3791	2.35	AC127 AC128	0-20	BC147 BC148	0-14	BCY72 BD115	0.15	BFX88 BFX89	0-25	MJE3055 MJE370	0.75	TIP31C TIP32A	1-00	CD4009 0-52 CD4024 0-72 CD4049 0-45 CD4010 0-52 CD4025 0-18 CD4049 0-45
2N2220	0.25	2N3792	2.60	AC151V	0.27	BC149	0.15	BD116	0.75	BFY50	0.23	MJE371	0.75	TIP32C	1.25	CD4011 0-18 CD4027 0-43 CD4510 1-25 CD4012 0-18 CD4028 0-83 CD4511 1-84
2N2221 2N2221/	0-18	2N3794 2N3819	0.24	AC152V AC153	0-49	BC153 BC154	0-18	BD121 BD123	1-00	BFY51 BFY52	0-23	MJE520 MJE521	0.60	TIP33A TIP33C	1-01	CD4013 0-48 CD4029 1-08 CD4518 1-25
2N2222	0-20	2N3820	0.64	AC153K	0-40	BC157	0.16	BD124	0.67	BFY53	0-18	MP8111	0.32	TIP34A	1-51	CD4015 0-88 CD4031 1-84 CD4520 1-87
2N22222/ 2N2368	0.25	2N3823 2N3904	0.78	AC154 AC176	0.25	BC158 BC160	0-16	BD131 BD132	0-40	BFY90 BRY39	0.75	MP8112 MP8113	0-40	TIP34C TIP35A	2-80	CD4016 0-45 CD4037 0-88 CD4017 0-64 CD4041 0-70
2N2369	0.20	2N3906 2N4036	0.27	AC176K	0.40	BC167B BC168B	0.15	BD135 BD136	0-43	BSX20 BSX21	0.21	MPF102 MPSA05	0.39	TIP36A	3.70	No. of Concession, Name
2N2369/ 2N2646	0-22	2N4037	0-42	AC187K AC188K	0.40	BC168C	0.15	BD137	0-55	BU104	2.00	MPSA06	0.31	TIP41A TIP41C	0-79	The second se
2N2647 2N2904	0-98	2N4058 2N4059	0-18	ACY18 ACY19	0-24	BC169B BC169C	0-15	BD138 BD139	0-63	BU105 C106D	2.25	MPSA12 MPSA55	0.35	TIP42A	0-90	Veroboard
2N2904/	0-24	2N4060	0.15	ACY20	0.22	BC170A	0-15	BD140	0-87	CA3018A	0.65	MPSA56	0.31	TIP42C	0.70	Copper Plain
2N2905	0-25	2N4061 2N4062	0.15	ACY21 ACY28	0.26	BC171 BC172	0.16	BD529 BD530	0-60	CA3020A CA3028A		MPSU05	0-65	TIP53 TIP2955	1.70	0.1 0.15 0.1 0.15 2.5 x 34 in 36p 26p - 17p
2N2906	0-19	2N4126	0.21	ACY30	0-58	BC177	0-26	BDY20	1.05	CA3035	1.37	MPSU55	0-63	TIP3055	0-50	2.5 x 5in 40p 39p - 19p
2N2906/ 2N2907	0.21	2N4289 2N4919	0-34	AD142 AD143	0-57	BC178 BC179	0-27	BF115 BF117	0.36	CA3046 CA3048	0.70	MPSU56 NE555V	0.80	TIY43 ZTX300	0.28	34 × 34 in 40p 39p 34 × 5in 45p 47p - 32p
2N2907	0-24	2N4920	1.10	AD149V	1.20	BC182	0.12	BF121 BF123	0.35	CA3052	1.62	NE556	1.30	ZTX301	0.13	34 x 17in £1.61 £1.26 £1.00 £1.92
2N2924 2N2925	0-20	2N4921 2N4922	0-83	AD150 AD161	1.15	BY182L BC183	0.12	BF125	0.35	CA3089E CA3090O	1-96	NE560 NE561	4-48	ZTX302 ZTX500	0-20	PINS x 36 30p 30p
2N2926		2N4923	1-00	AD162	0.50	BC183L	0-12	BF152	0-20	LM301A	0-48	NE565A	4-48	ZTX501	0.13	× 200 £1-16 £1-16
Green		2N5190 2N5191	0-96	AD161 }	PR	BC184 BC184L	0.13	BF153 BF154	0.25	LM308 LM309K	2-50	OC23 OC28	1.35	ZTX502 ZTX530	0-18	Trade and Retail Supplied
												-				
			-		1111						1				4-10	
TTL	Integ	rated	Circ	uits-(	Quali	ty and	Pric	es Yo	u Ca	n't Bea	ert	SN74145 SN74150	0-90	SN74174 SN74175	1-25	Potentiometers Linear or Log Single Double
SN7400	0-16	SN7409	0-22	SN7430	0-16	SN7448	0-90	SN7476	0-35	SN7493	0-45	SN74151	0-85	SN74176	1-44	Rotary Pots 25p 75p
SN7401 SN7401		SN7410 SN7411	0-16	SN7432 SN7437	0-28	SN7450 SN7451	0-16	SN7480 SN7481	0-50	SN7494 SN7495	0-82	SN74153 SN74154	0-85	SN74180 SN74181	1-40	Rotary Switched 55p -
	0-38	SN7412	0.28	SN7438	0-35	SN7453-	0-16	SN7482	0.75	SN7496	0.75	SN74155	1.50	SN74190	2-30	Sliders 45p 75p
SN7402 SN7403		SN7413 SN7416	0-35	SN7440 SN7441	0-16 AN	SN7454 SN7460	0-16	SN7483 SN7484	0-95	SN74100 SN74107		SN74157 SN74160	0-95	SN74191 SN74192	2-30	Full range of capacitors
SN7 404	0-19	SN7417	0-35	a della	0.85	SN7470	0-33	SN7485	1-25	SN74118	1-00	SN74161	1-10	SN74193	1-15	stocked. See catalogue for
SN7405 SN7406		SN7420 SN7423	0.16	SN7442 SN7445	0-65	SN7472 SN7473	0-26	SN7486 SN7490	0-32	SN74119 SN74121	1-92	SN74162 SN74163	1-10	SN74196 SN74197	1-60	details
SN7407	0-45	SN7425	0-29	SN7446	0.95	SN7474	0-36	SN7491	0-85	SN74122	0-50	SN74164	2.01	SN74198	2.25	Presets-Horizontal or Vertical 0-1W Sp 0-3W 10p
SN7408	0.19	SN7427	0-29	SN7447	0-95	SN7475	0-50	SN7492	0-45	SN74123	0-60	SN74165	2-01	SN74199	2-25	0.14 op 0.5w 10p

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## System 2. £85.00

Viscount IV amplifier (As System 1a) M P60 type deck (As System 1a) Two Duo Type III matched speakers — Enclosure size approx. 27"  $\times$  13"  $\times$  11 $\pm$ ". Finished in teak simulate. Drive units 13"  $\times$  8" bass driver, and two 3" (approx.) tweeters. 20 watts RMS, 8 ohms frequency range = 20 Hz to 18.000 Hz. Complete System with these speakers  $\pounds 85.000 + \pounds 7.60 \ p \ sp.$ 

PRICES: SYSTEM 1a Viscount IV R103 amplifier E72.50 + £1.90 p.8.p. 2 Ouo Type IIa speakers £30.00 + £6.50 p.8.p. MP60 uye deck.with Mag. cartridge de luxe plinth and cover £22.00 + £3.30 p.8.p. Total if purchased separately: £79.50 Available complete for only: £69 00 + £8.50 p.8.p. PRICES: SYSTEM 2 Viscount IV R103 amplifier £27.50 + £1.90 p & p. 2 Ouo Type III speakers £46.00 + £7.50 p & p. MP60 type deck with Mag.cartridge de tuxe plinth and cover £22.00 + £3.30 p & p. Total if purchased separately: £95.50

Available complete for only £85.00 Scotland and the Orkneys P & P Surcharge +£7.60 9 & p. System 1a £1.75 System 2 £3.50

••••



buttons for station selection, illuminated tuning scale covering full, medium and long wave bands. Size chassis 7" wide 2" high and 4²/₄" deep approx. Speaker including baffle and fixing strip £2.00 +45p p & p. Car Aerial Recommended - fully retractable £1.60+40p p & p.

The Tourist I Kit For the experienced constructor. If you can solder on a printed circuit board you can build this model. Same technical specification as Tourist TT. Price £8.20+£1.05 0 & 0.



The Tourist 1 Kit, same specification as Tourist TT complete with speakers, fixing kit and fully retractable aerial.

£

£10.50 +p & p £1.50

# IY SI

Elegant self selector push button player

for use with your stereo system. Compatible with Viscount IV system, Unisound module and the Stereo 21

sensitivity

As above but complete with build

Technical specification Mains

Output

26

240V

Stereo 21, easy to assemble audio system kit. No soldering required

The unit is finished in white P.V.C. end the acrylic top presents an unusuelly interesting variation on the modern deck plinth. Includes — BSR 3 speed deck, autometic, manual facilities together with stereo cartridge.

Two speakers with cabinets. Amplifier module. Ready built with control panel, speaker leads and full, easy to follow assembly instructions.

Specifications - For the technically minded: Input sensitivity 600mV. Aux. input sensitivity 120mV. Power output 2.7 watts per channel. Output impedance 8-15 ohms. Stereo headphone socket with automatic speaker cutout. Provision for

machine social with advantage spectra of outputs for taging discs. **Overall Dimensions.** Speakers approx  $15\frac{1}{2}$  % 8" × 4". Complete deck end cover in closed position approx.  $15\frac{1}{2}$  % 12" × 6".

#### Complete only £23.20 +£3.00 p & p.

input.

125mV

Extres if required. Optional Dlamond Styli £1.60. Specially selected peir of stereo headphones with individual level controls and padded earpieces to give optimum performance £5.80.



Reliant Mk IV Mono Amplifier, ideal for the small disco or house parties. Output 20 watts RMS into

B ohms (suitable for 15 ohms). Inputs ⁴ 4 electrically mixed inputs. ⁴ 3 individual mixing controls. ⁵Separate bass and treble controls common to all 4 inputs. ⁶Mixer employing F.E.T. (Field Effect Transistors). ⁵Solid State circuitry.

Attractive styling. INPUT SENSITIVITIES - Input - 1). Crystal mic. guitar or moving coil mic, 2 and 10mV. (Selector, switch for desired sensitivity.) - Inputs - 2), 3), 4). Medium output equipment - ceramic cartridge. tuner, tape recorder, organs, etc. — all 250mV sensitivity. AC Mains, 240V operation. Size approx: 121"×6"×31" £20.00 +£1.35 p & p.

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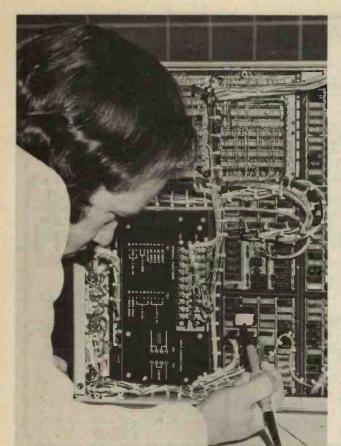
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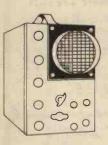
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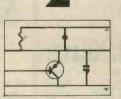
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#### THE OLD ORDER CHANGETH

T is the nature of some changes to hurt a bit and strike at established traditions; even so in electronics. In the good old days an electronic circuit was a circuit, and was seen to be so! It could be analysed quite easily, from input to output, every part recognizable and its function readily determined. Now we frequently have to content ourselves with the knowledge of the overall function of some circuit or portion thereof, and remain in ignorance of the precise manner by which particular functions are achieved.

Anyone returning to electronics after a few years abstinence must be considerably shaken when they first encounter some of today's circuit diagrams, with those frequent blank and anonymous areas bearing little more than the legend "IC1" et seq. Yet there is nothing that really need alarm the more traditionally minded enthusiast and constructor-or for that matter, the beginner.

Electronics is a changing world, that it would be idle to The home constructor certainly has to be more denv. selective in the kind of projects he tackles, that is one major change which has come about in this field. It is patent that some projects are no longer truly viable in home constructor terms-for practical or economic reasons. The pocket calculator gave the first example of the great commercial possibilities of large scale circuit integration when applied to mass production of a piece of equipment for the consumer market. Very quickly it became obvious that the home constructor had little to gain from attempting to build a calculator for himself; in any event the nature of things decreed that, in nine out of ten cases, a manufacturer's kit would have to be resorted to. Thereupon, it became an assembly job rather than a bonafide constructor job. No technical knowledge was necessary nor was it likely to be acquired during the process of assembling such a kit. On the credit side, the skill of the constructor in handling microscopic devices and in performing extremely delicate soldering operations was put to the test. If he came through this with flying colours, the completed instrument was living proof of his competence which could be overtly paraded before wondering and admiring friends.

Today, the foregoing could be said to apply to the digital wristwatch-but even more so. With this latest example of microelectronics in the consumer market, the scale of operations is further reduced and the degree of dexterity demanded of the assembler must therefore be correspondingly greater.

One thing that never changes is the fascination generated by the new and novel. That first digital wristwatch, like that very first radio of old, simply has to be built: for the experience, for the fun, for the very sense of personal achievement. For some it is an irresistable challenge. Often it is a form of baptism, since for some, assembling a kit could be their first real practical involvement with electronics. But they must not confuse kit assembly with normal constructing activities which embrace an infinite variety of projects-with or without the use of i.c.s. They should realise that many typical constructor projects have no commercial counterpart and that remains, in spite of other changes, one of the great advantages and rewards of this hobby.

F. E. BENNETT

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THE Synchronome is an accented beat metronome

which can provide duple, triple and quadruple times at the turn of a switch. It utilises six TTL integrated circuits plus a few discrete components. The unit is completely self contained and may be driven by battery or mains.

#### MAELZEL'S METRONOME

The mechanical metronome has been in existence virtually unchanged since the eighteenth century. The original design was the brainchild of Maelzel (1772-1828) and to this day such indications at the head of a piece of music as M.M. = 100 mean that the crotchet beat should be taken as the speed of Maelzel's metronome set to 100 beats/minute.

Whilst there is no dispute with the ability of the metronome to perform its function reliably there is still, however, room for improvement.

The basic metronome provides only beats. A more expensive refinement is the one that provides accented timing so that a bell operates on every second, third or fourth beat.

Whilst the purist or traditionalist may scorn the use of an electronic device to do the job the mechanical metronome has done since the time of Beethoven, the Synchronome offers an advanced design to bring musical tempo into the twentieth century.

#### **OPERATION**

The complete block diagram is shown in Fig. 1. The timing source is an oscillator running at one hundred times its required speed so that a degree of stability can be maintained. The square wave output is divided by the necessary factor of one hundred and fed at its correct rate to a monostable

We would like to thank Chappel's of New Bond St for the use of the metronome shown on this and the front cover pages

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Moderato

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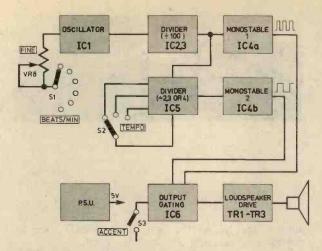
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#### Fig. 1. Block circuit of Synchronome

circuit (Monostable 1). This will give an output pulse of predetermined duration every time it is triggered by a positive transition. The output is fed to the loudspeaker drive cricuit via a gating arrangement (which will have no effect on the pulse until accented timing is selected).

The output of the main divider circuit is also fed to a further divider chain. This circuit will divide the signal by a further factor of two or three or four in conjunction with a gate dependent upon the position of the "Tempo" selection switch. The reset output of the gate to the divider is also fed to a second mono (Monostable 2) which has a much wider pulse width than the first. Now, if "Accent" is selected, then this wider pulse (when present) inhibits the narrow pulse from the first mono and routes itself instead to the loudspeaker drive circuit.

The loudspeaker drive circuit converts the square wave inputs to it to current pulses which pass through the speaker itself.

#### CIRCUIT

The full circuit is shown in Fig. 2. 74 series TTL has been used for all the integrated circuits in the Synchronome for simplicity.

The oscillator uses a 7413 Schmitt trigger with six switched ranges which are all independently variable; in addition, there is a fine frequency adjustable resistor which can vary the speed incrementally on any range. The frequency of oscillation is dictated by capacity and the total feedback resistance.

The oscillator output is fed to two conventional 7490 divider circuits to obtain the final division by one hundred. The reset inputs to the 7490s are held to the logical low state to ensure that the correct sequence is obtained.

A single chip, the 74123 dual retriggerable monostable is used for generating both the narrow and wide pulses. The output pulse width is a function of the timing capacitor and resistor for each stage. Ideally, the timing resistor should be in the range 5-50 kilohms though these values are not over critical in this application.

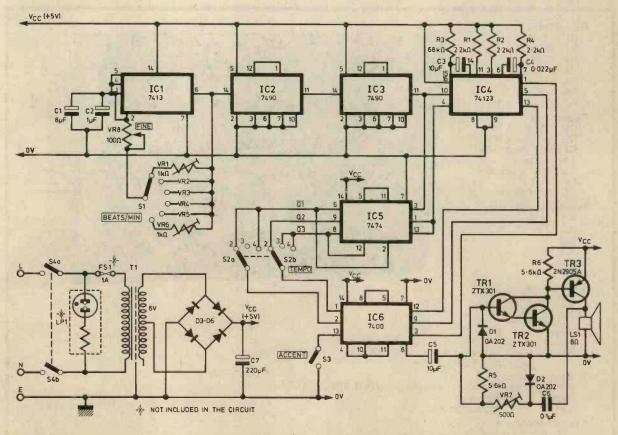
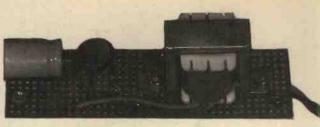


Fig. 2. Complete circuit





#### ACCENT SELECTION

The chip used here is the 7474 dual D type flip flop; however, the configuration may seem slightly strange to some readers. Since it is required to use these flip-flops as a divider circuit rather than as a conventional latch (which would be their normal function) each of the flip-flops needs to be "back primed" by feeding the NOT Q output back to the D input. In so doing, the 7474 will act as a counter provided that the input is fed in as the clock pulse. The Q and NOT Q outputs of each stage are fed to the "Accent" selection switch so that duple, triple or quadruple time may be selected. The selected

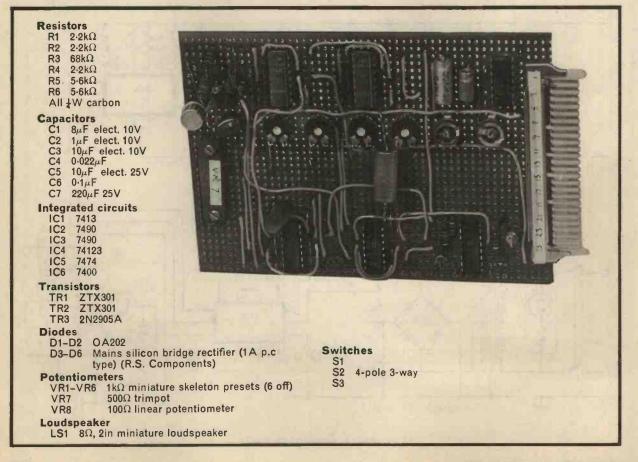
## COMPONENTS ...

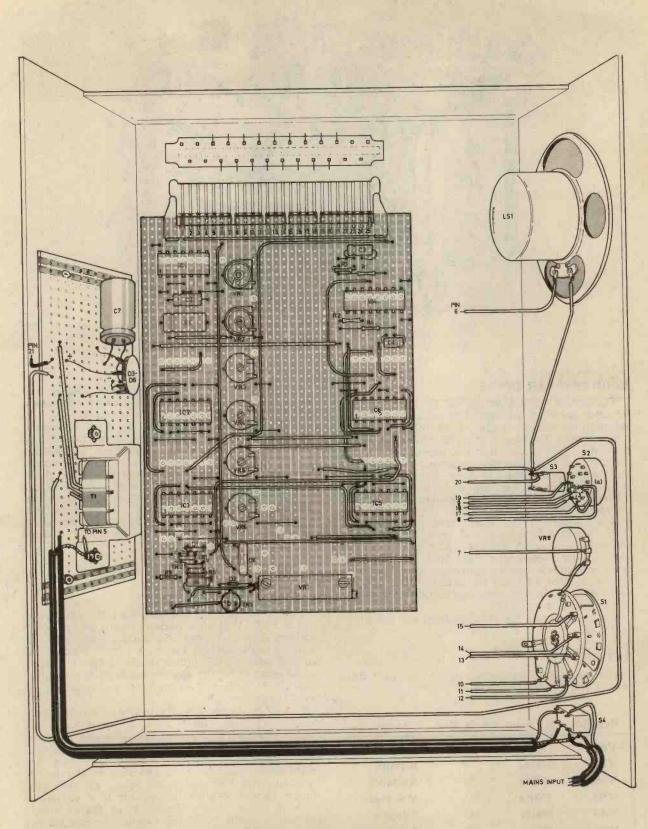
outputs are fed to the two input NAND gate to provide the reset pulse for both flip flops.

The negative reset pulse is also fed to the 74123 to generate the wider accent pulse.

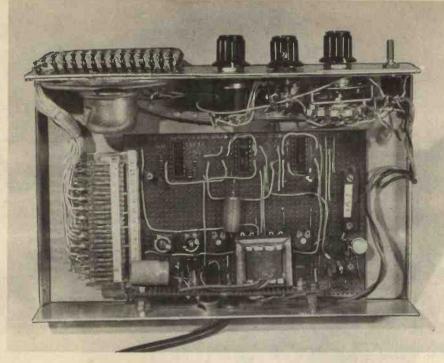
#### OUTPUT GATING

If "Accent' is switched off then the 7400 enables the narrow pulse from the 74123 to reach the loudspeaker driver stage and also inhibits the wide pulse from getting through. When "Accent" is selected then the 7400 will inhibit the narrow pulse and substitutes the wide pulse to the loudspeaker drive circuit.





#### Fig. 3. Wiring details of Synchronome



#### LOUDSPEAKER DRIVE

The square wave input to the loudspeaker drive circuit is fed via a differentiating circuit to TR1 and the negative transitions are cut off by D1. TR1 and TR2 form a Darlington pair to drive the output transistor TR3 which has the loudspeaker as its collector load. In addition, feedback is introduced via VR7 and the setting of this is given in the initial adjustment but its function is to enable sufficient current drive to reach the speaker to give the desired sound.

If a speaker greater than about three inches is used then the complete unit may be run quite successfully by a 6V battery. The prototype ran for six hours continually from four HP7 batteries but, by using a smaller speaker, more current is needed through TR3 and the speaker to achieve the same effect. It is for these applications that a 5V power supply is required.

Assembly details for the Synchronome are given in Fig. 3.

#### SETTING UP

The six ranges can be set up to suit individual needs but a suggested set is given below:

Resistor	Osc Freq	Beats Min	Name
VR1	83Hz	50	Largo
VR2	117Hz	70	Adagio
VR3	150Hz	90	Andante
VR4	192Hz	115	Moderato
VR5	240Hz	144	Allegro
VR6	313Hz	188	Presto

These ranges are flexible to a certain degree but by operation of the fine frequency control the exact rate for the individual user can be obtained.

It is important to note that when the individual ranges are being set up, the fine frequency control VR8 should be set at its mid-position. Ideally the oscillator should be set up using a frequency counter or an oscilloscope but, should neither of these be available, then the output circuit may be set up first and then the individual ranges adjusted using a watch with a second hand. If this latter method is adopted then it is advisable to finally check each range over a period of about two minutes to ensure a degree of accuracy.

#### OUTPUT CIRCUIT

For setting up the output circuit the only control is VR7. With the "Accent" switch on the "off" position adjust VR7 until the correct clicking sound is heard in the loudspeaker. Now switch "Accent" to on and adjust VR7 until a distinctly lower, longer sound is heard on the appropriate beat. When satisfied, check the sound on the other two positions of the "Tempo" switch.

If VR7 is set too low, the output circuit will self oscillate on every input pulse giving a series of loud whines, so ensure that VR7 is set to its midposition initially. When using a loudspeaker greater than about three inches a double click may be heard on the accented beat. This may be eliminated by taking out VR7 altogether but to get sufficient output current through the speaker it is advisable to keep some positive feedback so that a fixed resistor of about 1.5 kilohms should be inserted in place of VR7.

# PEAK LEVEL INDICATOR By J.T. TIERNAN

#### A stereo add-on unit for better tape recording

**T** O THE inveterate hi-fi hobbyist the steady flow of circuit designs in the many hi-fi and electronics magazines is a source of constant pleasure and interest, but, by the very nature of such things, it is unlikely that the design fits your requirements to a tee. More often than not you find yourself wanting to combine specific sections of different designs into a single unit, and whilst the modular nature of many recent designs makes this none too difficult, there can, obviously, be problems.

One particular source of concern relates to the matching of signal input and output levels between different circuits or complete equipments. Problems of this nature are often more apparent than real, but the dynamic conditions of designs which involve frequency conscious networks: pick-up preamplifiers, tone controls, and, particularly, steep cut filters, can be difficult to determine, and their characteristics can change beyond recognition when driven at, or near, overload level.

It was with such worries in mind that this simple, but effective, peak level indicator was designed. In its original form it is incorporated in an audio preamplifier, set to indicate signal levels 6dB below output clipping, and it has given sterling service for several months. The overall arrangement of the preamp functions and the position of the indicator is shown in Fig. 1.

The design has an obvious application in tape recorders, as a recording level indicator; and, with a calibrated input attenuator, it could give service as a compact a.c. voltmeter or signal detector.

For the purpose of this article a stereo indicator has been made up as a separate unit.

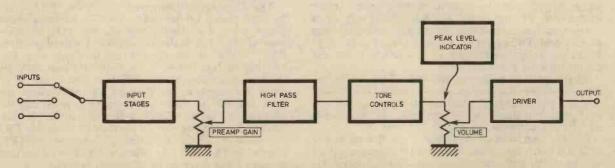
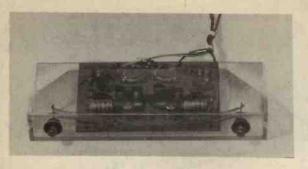


Fig. 1. Block diagram of a typical audio preamplifier showing the suggested connection point for peak level indicator



#### PERFORMANCE

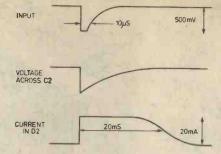
The unit has a fast attack/slow decay response and will activate an l.e.d. indicator when the input threshold level is exceeded. With the component values specified its performance is as follows:

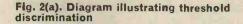
Input Sensitivity (max) 500mV

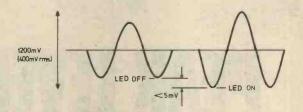
Threshold Discrimination<1% (5mV@ 400mV RMS 1kHz<br/>sine wave input)LED Active Period20mS (10µs transient input)

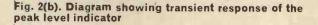
Fig. 2 illustrates the test conditions.

The  $10\mu$ s input pulse represents a 50kHz audio transient, demonstrating a bandwidth capability well in excess of that needed for audio applications; and a 20ms l.e.d. output pulse has excellent visual impact.









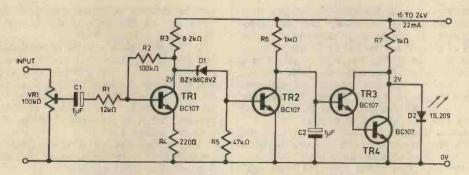


Fig. 3. Circuit diagram of the mono version of the peak level indicator

#### **CIRCUIT DESCRIPTION**

The circuit of a single channel peak level meter is shown in Fig. 3. TR1 is a conventional amplifier stage, biased near to saturation, with gain largely determined by the ratio R2/R1. TR2 acts as a current switch, controlling the charge and discharge of C2; and TR3/4 forms a high current gain stage acting as a bypass for the l.e.d. current when the circuit is in the quiescent state.

The bypass arrangement has been adopted to ensure a steady current is drawn from the power supply, whatever the circuit's state, and thus no switching transients are transferred to associated circuits via (common) power supply lines.

Circuit operation is as follows: In the quiescent state TR1 is fully conducting with its collector sitting at about 2V, and, because of the Zener diode (D1) coupling, TR2's base is effectively grounded. TR2 is passing no current and C2 ( $1\mu$ F tantalum) will

have acquired a positive charge via the  $1M\Omega$  collector load of TR2.

The Darlington connected transistors TR3/4 are forward biased by the charge on C2 and draw about 20mA from the supply rail via the 1k $\Omega$  collector resistor R7. The collector of TR4 is sitting at about 0.5V, which is insufficient to forward bias D2, and the voltage across C2 is held at about 1.1V by the base-emitter voltages of TR3/4.

On the negative portion of an input cycle the base current in TR1 will fall, and, provided the subsequent rise of TR1's collector voltage is sufficient to overcome the Zener diode threshold, TR2 will conduct. C2 is very quickly discharged by TR2; current in TR3/4 is immediately cut off; and current through R7 is diverted to D2 which lights up.

continued on page 240

## PEAK LEVEL INDICATOR

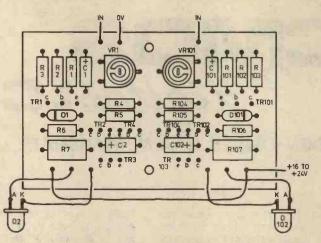


Fig. 4(a). Layout of the components of the printed circuit board. For a mono version the board can be split down the middle and only half used

## COMPONENTS ...

#### Resistors

R112kΩR547kΩR2100kΩR61MΩR38·2kΩR71kΩ  $\frac{1}{2}$ W  $\pm$  10% carbonR4220ΩAll LW15% carbon film execut B7

All ±W ± 5% carbon film except R7

Potentiometer VR1 100kΩ sub miniature horizontal preset

Capacitors C1 1µF 16V tantalum C2 1µF 35V tantalum

#### Semiconductors

 TR1-TR4
 BC107C (4 off)

 D1
 BZY88C 8V2 8·2V 400mW Zener

 D2
 TH209 light emitting diode

 For a stereo version twice the number of components specified above are required

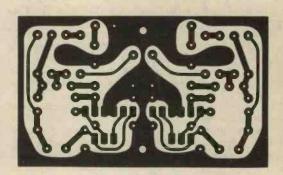
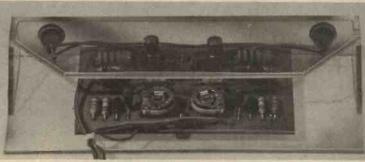
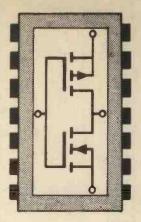


Fig. 4(b). Full size printed circuit master of the peak level indicator



The completed stereo peak level indicator mounted on a piece of casette tape case





## By D.B. JOHNSON-DAVIES & A.M. MARSHALL B.A. PART 3

THE previous parts in this series have described the basic building-blocks from which all CMOS devices are constructed—the complementary MOSFET pair and the transmission gate.

This part will cover the range of gate packages available in CMOS.

#### LOGIC GATES

The two basic types of gate in the CMOS family are the NOR and NAND, and these two functions have the added advantage that spare gates can be used as inverters in linear applications. However, it is often the case that the design of a circuit will be greatly simplified by resorting to other functions, and so a full list of the types available is given in Table 3.1, with the pin diagrams in Fig. 3.1. Note that the supply pins are always conveniently placed at opposite corners of the package.

Worthy of mention are the two special gate packages shown in Fig. 3.1(e) and (f). The 4501 contains two 4-input NAND gates and a 2-input NOR gate with true/complement output. By making the connections shown dotted in Fig. 3.1(e) the gate will work as an 8-input NAND or AND gate with the output taken from pin 15 or 14 respectively. Note that pin 14 should not be used as an input to the inverter. The 4572 contains 4 inverters, a 2-input NOR gate and a 2-input NAND gate, making it possible to construct any 2⁴ or 3-input function.

#### **INVERTERS AND BUFFERS**

digital I.Cs

The various types of inverter and buffer packages available are shown in Fig. 3.2. The 4069 is a standard unbuffered hex-inverter for use where buffering is not needed, or where it would lead to excessive power dissipation in some linear applications. The other types shown all have high-current buffered outputs, and are useful for driving displays or other logic families.

The two basic buffers are the 4049 hex inverting type and the 4050 hex non-inverting type. On these devices the  $V_{CC}$  terminal can be at any voltage up to  $V_{DD}$ , enabling them to be used for logic level conversion.

The 4049 and 4050 have replaced the earlier 4009 and 4010 which needed two supply connections.

Table 3.1. Full range of CMOS logic gates							
	FIGURE	NOR	NAND .	OR	AND	EXCLUSIVE	EXCLUSIVE
QUAD 2-INPUT	Fig. 3.1 (a)	4001	4011	4071	4081	4070 4030 4507	4077
TRIPLE 3-INPUT	Fig. 3.1 (b)	4025	4023	4075	4073		anna
DUAL 4-INPUT	Fig. 3.1 (c)	4002	4012 4501	4072	4082		
8-INPUT	Fig. 3.1 (d)	4078	4068 4501		4501		

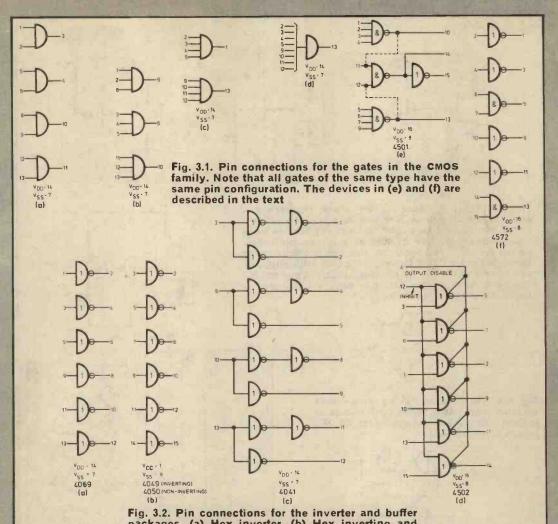


Fig. 3.2. Pin connections for the inverter and buffer packages. (a) Hex inverter. (b) Hex inverting and non-inverting buffers or level converters. (c) Quad true/complement buffer. (d) Strobed hex inverter buffer. Pin 4 is the three-state output disable, and pin 12 is the output inhibit

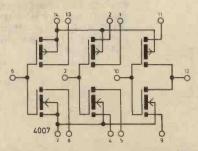
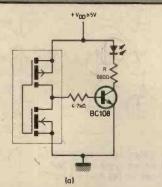


Fig. 3.3. Connection diagram for the 4007 dual complementary pair and inverter. The diode protection networks are not shown



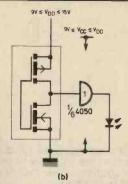


Fig. 3.4. Driving circuits. The block represents a standard CMOS output. Resistor R, where necessary, limits the current through the l.e.d. (a) Simple transistor driver. (b) Use of 4050 as a driver and level-converter;  $V_{CC}$  is chosen to give the correct current through the l.e.d. (c) Driver using 4049 with supplies of above 7 volts. (d) To provide sufficient current for the l.e.d. at very low voltages both a buffer and a transistor may be required



Fig. 3.5. R-S latch using two cross coupled NOR gates. With both inputs at logical "O" the previous state at the inputs is memorised

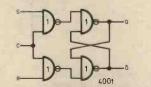


Fig. 3.6. Gated R-S latch uses one 4001 package. A logical "1" on the control input disables the R and S inputs

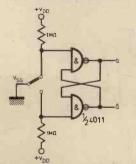
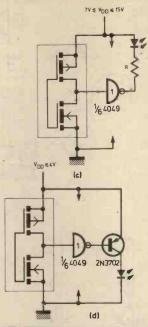


Fig. 3.7. Switch debouncer using an R-S latch. The resistors may be any large value. Alternatively NOR gates may be used, with the resistors going to  $V_{\rm SS}$  and the switch to  $V_{\rm DD}$ 



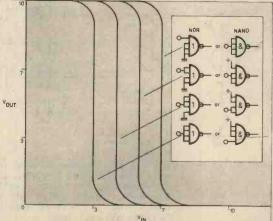


Fig. 3.8. The effect of paralleling inputs. Increasing the number in a NOR gate causes a decrease in the input 'low' noise margin and an increase in the input high noise margin. The reverse holds for a NAND gate

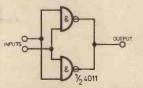
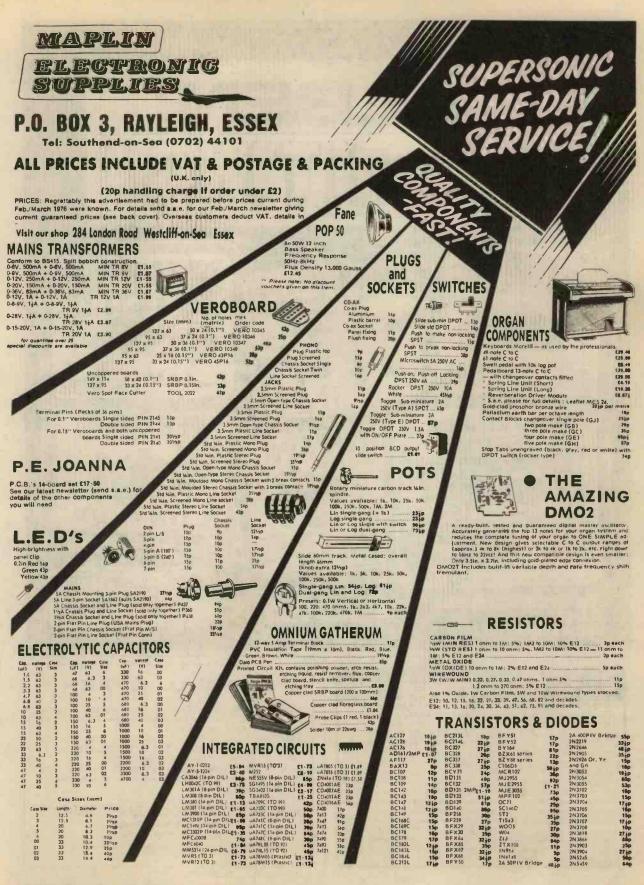
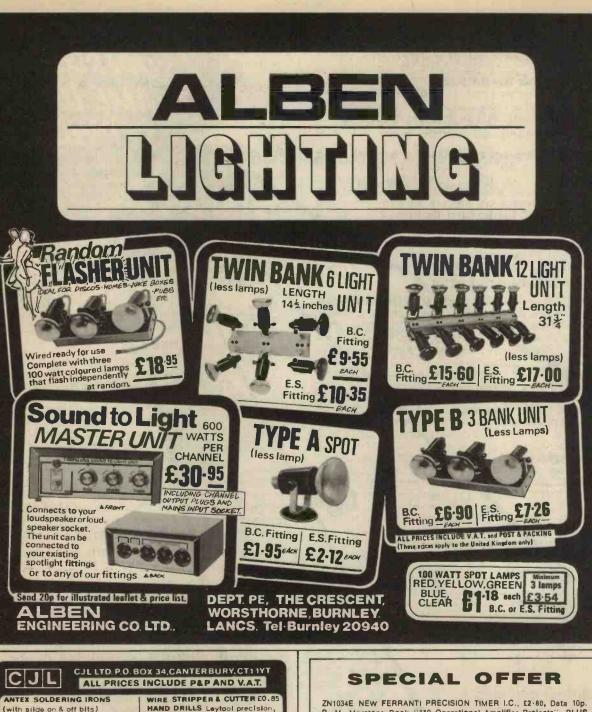


Fig. 3.9. Both source and sink current may be increased by paralleling whole gates or inverters from the same package. The speed performance will also be improved





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3/3: 1CC 25W 3/3: 1X2 1SK ST3 SOL The 4041 is a quad true/complement buffer which provides both inverted and non-inverted outputs. Finally the 4502 strobed hex inverter buffer consists of six inverters with three-state outputs. Applying a logical "1" to pin 4 puts all six outputs at high impedance (greater than 10M $\Omega$ ) making it possible for many packages to share the same output lines More than 50 three-state outputs can be "common bussed" in this way. Pin 12 is an output inhibit; a logical "1" switches the six outputs to "0".

One part does not really fit into any of the above categories; the 4007 dual complementary pair and inverter shown in Fig. 3.3. This part provides access to the individual transistor elements making it possible to construct circuits not catered for in the standard range. Furthermore, their device will replace discrete MOSFETS in many circuits, at a fraction of the cost.

#### **OUTPUT DRIVE CURRENT**

As mentioned earlier, CMOS gates have a d.c. fanout of more than 100 since CMOS inputs present a negligible resistive load. However, the driving capabilities of CMOS are not very great by other standards, most outputs only being able to sink one low-power TTL input load at 5 volts, and so some sort of interface will often be needed between the output and the external circuit.

For every device two drive currents are given; these are the "sink" current which flows through the *n*-type MOSFETS when the output is at logical "0", and the "source" current through the *p*-types when the output is at logical "1".

The source and sink currents will be equal only in devices which have symmetrical outputs, such as inverters and all parts in the B-series (which have two inverters before the outputs). The currents for other devices will depend on the arrangement of the MOSFETS at the output. These values represent limits, and the output of a gate can be shorted to  $V_{DD}$ or  $V_{SS}$  or to another output without causing any damage. This is because of the relatively high output impedance of a CMOS gate (typically in the region of 500 to 1 kilohms) and this limits the current to a safe level. High current buffers such as the 4049 can, however, suffer from supplies of more than circuits if operating from supplies of more than about 7 volts, as the overall package power dissipation will exceed the recommended 200mW, and so these types should be treated with greater care.

#### **DRIVING CIRCUITS**

Due to the complementary arrangement of CMOS outputs, the load may be connected between the output and either supply rail. Fig. 3.4 gives four circuits for driving light emitting diodes from a standard output, and these can easily be extended to other applications.

. The output currents are very dependent on the supply voltage, and choice of driving circuit will often be dictated by this. With supplies of less than about 4 volts the base current of a driver transistor can exceed the standard output current of the CMOS device, and an intermediate buffer will be needed as in Fig. 3.4(d).

#### UNUSED INPUTS

In some logic families unused inputs will look after themselves. For example, in TTL any inputs left floating will be pulled up to a logical "1" level. This is not the case with CMOS due to the near infinite input impedance of a gate. A floating gate is at an undefined level and can give rise to erratic operation, and the input capacitance may charge up to the switching point causing high power consumption. The simple cure is to hold unusued inputs at some defined logic level, either by joining them to a used input, or by connecting them to the nonsignificant logic level for that function.

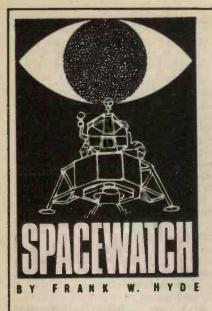
Paralleling inputs results in a slight increase in speed due to the lower "on" resistance of the paralleled devices, although this is minimised by a compensating speed decrease due to the added capacitance. More important is that the output source or sink current of the device is increased in proportion to the number of inputs tied together; in NAND gates the source current is increased, whereas in NOR gates the sink current increases, so that a gate from a 4002 package with all inputs paralleled will sink 3.2mA at 5 volts, sufficient to drive one TTL load.

#### **GATES AS LATCHES**

A one-bit memory' or R-S latch may be constructed from two NOR gates as in Fig. 3.5. Alternatively NAND gates can be used in a similar configuration. The information remains memorised when the R (reset) and S (set) inputs are both at the nonsignificant logic level, this being  $\mathbf{R} = \mathbf{S} = 0$  for NOR gates. The control input in the circuit of Fig. 3.6 performs this function by holding the R and S inputs low. One common application of the R-S latch is the switch debouncer shown in Fig. 3.7, this time using NAND gates. The pull-up resistors, which can have any value up to several megohms, hold the inputs at logical "1" when not taken to "0" by the switch contact. This ensures that a noisy contact does not change the state of the output.

Next month: Linear use of CMOS with practical amplifiers and oscillators.





#### TO MARS BY VIKING

The Viking missions to Mars is the highlight for 1976 and especially for America it marks a new milestone in Space History. These vehicles consist of two parts, the orbiter and the lander and represent the latest of the sophisticated techniques available. The lander part of the spacecraft will touch down on July 4. The whole operation will be repeated a few days later with the second spacecraft.

As a combined operation it will be unique for there will be four units at work at the same time. enabling a vast area of the red planet's surface to be observed from the orbiters and the local terrain investigated by the landers.

The two composite vehicles were dispatched into a minimum energy orbital trajectory and will be at their destinations when the planet is on the opposite side of the Sun from the Earth. Thus they will represent the unusual situation of being in operation but out of direct communication with Earth for about a month.

The orbiter is a very much enlarged version of Mariner spacecraft weighing about 2,300 kilogrammes compared with the Mariner which is about 1,000 kilogrammes. The lander is contained within the structure. The Viking composite unit contains larger propellant tanks and more powerful aids such as the computers.

The camera system is also an improved one in order that the pictures may be relayed more rapidly back to Earth than in the previous missions. This is an important point because the decision to make the actual landing will be determined by the terrain and this can only be made if mission control can see what is happening. With a communication time for the round trip of around 40 minutes per bit, the extent of the improved technique can be appreciated.

Three basic programmes are planned. The orbiters will carry on the detailed photography of the planet begun by Mariner 9 at the 1971 opposition. Second, the spacecraft will study the physical conditions of the planet which will include the atmosphere and the geology and internal structure. Thirdly, the landers will look for life and/or biological processes.

#### EXPERIMENTS AND OBSERVATIONS

The radio and radar measurements will be directed to the size of the planet, the electromagnetic properties, atmospheric disturbance, density of the atmosphere, gravitational conditions, density of the planet and surface density.

The orbiters will observe the formation of clouds and their movements and the possible changes of the concentrations of water vapour. The landers will also record their local weather at the two points on the surface where they land. Both orbiters and landers will

Both orbiters and landers will photograph the geology giving details of structure, faults, stratification, types of rock and debris erosion and other conditions. The landers will sample the soil examining it for details such as minerals and the general composition by means of the scoops and subsequent processing within the lander craft.

The seismic measurements will afford data as to the structure of the planet and whether in fact it has a core, mantle and a crust like the Earth.

#### LANDING SITES

Four sites have been chosen for the landers and they have a primary and secondary importance. They are designated Prime A1 located at the area known as Chrise. In this area there are sand dunes of the order of hundreds of metres across with ripples, There are dust deposits with material washed down from the canyons to the south. This is also a possible area for fossil water.

The alternative or back up site is the area of Tritos Lacus which is similar to the Prime area but where the material is likely to have been carried north from the equatorial highlands.

Prime B1 is at Cydonia. This is a flat stretch of plains' where it is possible that water may be present during the summer for a few weeks. The area is smooth, possibly basalt, covered with dust and sediment. The back up site is Alba which is close to a major volcanic region.

The orbiters carry advanced television cameras. At closest approach of the spacecraft to the planet on each orbit these cameras will have a resolution of 50 metres per television line at an altitude of 1,500 kilometres. Each picture from the lander cameras will take 20 minutes to complete. It will not be possible to resolve a moving object therefore from the landers. However, the optical system enables close-ups of the far horizon pictures to be sharp.

The landing sites will be selected from the orbiter pictures which will watch for any onset of dust storms that might endanger the landing sequence.

The twin cameras will survey the landscape and near to the site to determine where to dig for samples. The scoop will collect a load and transfer this to a funnel on the top of the vehcile. From here it will fall into various processing sections where the analysis will be performed and the data relayed via the orbiters to Earth.

The cameras can be used for black and white pictures, colour and infra-red over three spectral bands. Also, the two cameras can provide a stereo effect. They are extremely versatile and can look at parts. of the spacecraft, nearby objects as well as the panoramic scene.

Perhaps this conveys some of the excitement of this mission, that machines controlled from a distance of some 230 million miles and a time lag of more than 20 minutes between order and execution is now a normal part of modern technology.

#### SOVIET ACTIVITY

In the excitement of the Viking programme it must not be forgotten that the USSR have two vehicles orbiting Mars and continuing to furnish data of the conditions. There will be expected an interchange of information from both projects.

A visit to the Salyut 4 orbiting station was made on two manned occasions during its year in orbit and also one visit by an unmanned Soyus 20 which was automatically linked up with Salyut 4. The complex is continuing to study near Earth space.

Another aspect of Soviet space spin-off concerns the material used for space suits. The USA were worried as to the suitability of the material used by the USSR for space suits and called for samples. The material is known as "Lola" and has a high heat resistance able to withstand temperatures up to 1,000 degrees C.

When the Americans made their tests it was found that the material was superior to the American material (which they insisted should be used on the combined task because of fire risk) in many ways not least the claim for Lola that it is stronger, has a good electrical insulator property and the almost casual claim that it is "only slightly affected" by a concentrated solution of 96°, of sulphuric acid.





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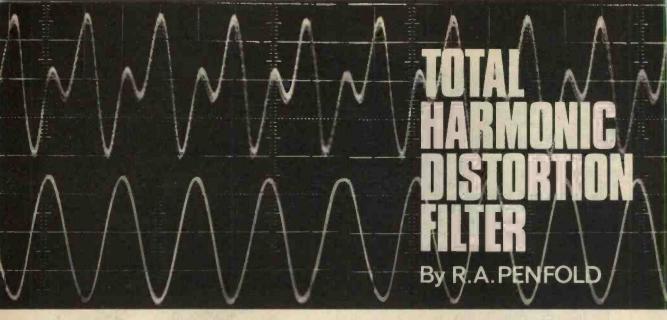
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ONE of the most important parameters of an amplifier, perhaps the most important, is its level of distortion. It is therefore somewhat paradoxical that very few amateur electronic workshops are equipped to measure distortion.

The reason for this is almost certainly due to the high cost of a distortion meter, which is rather expensive even if home constructed. However, there must be many amateur workshops which are equipped with a high quality audio signal generator, and an oscilloscope and/or an a.c. millivoltmeter. These form the basis of distortion measuring gear, and few other items of equipment are required to enable distortion to be measured. In fact the only other major item of test gear that is required is a notch filter, and this article describes a very simple and inexpensive filter for use in measuring total harmonic distortion at 100Hz and 1kHz.

The unit is quite small and neat, and is completely self contained, power being supplied by an internal 9 volt (PP3) battery. As the current consumption is less than 2mA, the running costs are negligible, and even with extensive use the battery will have virtually its shelf life. The filter has been designed to be as simple to operate as possible, but prospective constructors should bear in mind that measuring distortion in amplifiers is necessarily a fairly complex process.

#### TYPES OF DISTORTION

There are two types of distortion for which ngures are normally quoted in amplifier specifications: intermodulation distortion (i.m.d.), and total harmonic distortion (t.h.d.).

#### I.M.D.

I.m.d. is the more involved of the two and occurs when two or more signals are presented to a non-linear amplifier (any practical amplifier is non-linear to some degree). The distortion results in two main new frequencies being produced by the amplifier. If we take a simple example with only two input frequencies  $f_1$  and  $f_2$ , the new signals are equal to  $f_1 + f_2$  and  $f_1 - f_2$ , where  $f_1$  is the higher of the two frequencies. The situation is little more complicated than this would suggest as the new frequencies interact with one another, and with the original two signals, and more new signals are produced. These then interact with one another, and so on, with a multitude of new frequencies being produced by the amplifier.

Measuring this form of distortion is, not surprisingly, very involved and probably beyond the scope of most amateurs.

#### T.H.D.

Total harmonic distortion is more straightforward and is the result of a single tone being processed by a non-linear amplifier. Here the distortion of the fundamental frequency produces harmonics at the output of 2f, 3f, 4f, 5f, etc. If, for example, a 1kHz tone is applied to an amplifier, signals at 2kHz, 3kHz, 4kHz, and so on, will be produced as a result of the t.h.d.

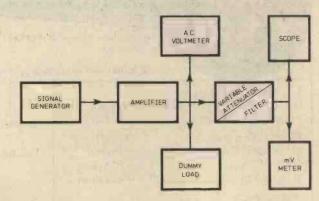


Fig. 1. Arrangement used by the author to measure t.h.d. The filter removes the fundamental enabling the distortion products (including noise) to be measured

#### MEASUREMENT OF T.H.D.

This type of distortion is much easier to measure, and the basic arangement used here is illustrated in Fig. 1.

A high purity sinewave is fed to the input of the amplifier from the signal generator. It is inevitable that the signal generator will have a certain amount of distortion on the output, and this distortion should be measured beforehand.

A dummy load resistor simulates the normal load impedance of the amplifier, and the voltmeter allows the output of the signal generator to be adjusted to give the appropriate power output level from the amplifier. The filter gives a narrow rejection notch at its operating frequency (we will assume this to be 1kHz in this example), and the signal generator is adjusted to this notch frequency.

The filter described here has two operating frequencies, and at the outset this is set to the one at which the distortion is not being measured so that the signal can pass unhindered. The attenuator is then adjusted to give a convenient reference level on the millivolt meter. 100mV or 1V r.m.s. will probably be the most convenient. 1V r.m.s. is about the maximum the filter can handle without clipping the signal and giving misleading results.

If the filter is now switched back to 1kHz it can be critically adjusted to give the lowest possible reading on the millivoltmeter. The signal generator frequency control will probably need some small adjustment as well, and the scope is very helpful in obtaining the correct settings. This procedure will be described in greater detail later.

#### CALCULATIONS

When these adjustments have been carried out properly the fundamental frequency will have been virtually eliminated, and only the distortion and noise will remain. From the reading on the meter the distortion factor can be calculated and is equal to:

> (Millivoltmeter reading  $\times$  100) -DReference level

(Where D is the percentage distortion of the signal generator.)

This gives the distortion factor as a percentage. The distortion factor is equal to the t.h.d. plus the noise present. The percentage of t.h.d. can be found by calculating the distortion factor, and the noise level as a percentage of the output level at which the measurement was made:

Output nois

U	ulpl	it noise	
		1	

 $\times 100$ Voltage measured across dummy load earlier

The percentage of t.h.d. is equal to the distortion factor minus the noise level.

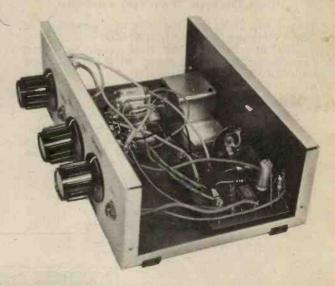
#### **EXAMPLE OF A T.H.D. CALCULATION**

The following example may help to make this a little clearer. Assume that we wish to measure the t.h.d. level of an amplifier delivering, 2 watts r.m.s. into an 8 ohm load at 1kHz.

First the signal generator is set to 1kHz and adjusted to give a reading of 4 volts r.m.s. on the voltmeter. An 8 ohm (8.2 ohms will do) resistor is used as the dummy load. The filter is switched to the 100Hz position and the attenuator is adjusted to give a convenient reading on the millivoltmeter, say I volt r.m.s. The filter is then switched to the lkHz position, and then both it and the signal generator are adjusted for the minimum fundamental output.

If, for instance, this leaves a reading of 15mV on the millivoltmeter and the signal generator has a distortion level of 0.2%, then the distortion factor equals  $(15 \times 100/1,000) - 0.2 = 1.5 - 0.2 =$ 1.3%.

The signal generator is then switched off and the millivoltmeter is used to measure the output noise of the amplifier directly at its output terminals. If



#### COMPONENTS ....

#### Resistors

R1	22kΩ	R5	47kΩ
R2	150kΩ 5% or better	R6	4.7kΩ
R3	150kΩ 5% or better	R7	4.7kΩ
R4	100kΩ	<b>R</b> 8	1·2MΩ
	All resistors 10% car	rbon 1	W unless
	otherwise stated		

#### Potentiometers

VR1 100kΩ lin carbon pot

- 100kΩ standard vertical preset VR2
- VR3 10kΩ lin carbon pot

#### Capacitors

- C1 10µF 10V elect
- 1nF polystyrene or mica, 5% or better C2
- C3 10nF polystyrene or mica, 5% or better
- C4 10nF polystyrene or mica, 5% or better
- C5 1nF polystyrene or mica, 5 % or better 20nF polystyrene or mica, 5% or better C6
- C7 2nF polystyrene or mica, 5% or better
- C8 16µF 10V elect

Integrated circuit

741C operational amplifier in 8-pin DIL package

#### Miscellaneous

Metal instrument case, Samos S3 (Doram) 3-way 4-pole rotary switch. Aluminium for battery bracket Three control knobs. PP3 battery and battery clips to suit Two 3-5mm jack sockets 0-1in matrix Veroboard

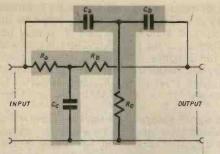


Fig 2. The basic "Twin-Tee" notch filter

this is, say 8mV, then the noise as a percentage of the 4 volt output level is  $8 \times 100/4,000 = 0.2\%$ .

The total harmonic distortion equals the distortion factor minus the noise, which in this case equals 1.3% - 0.2% = 1.1% t.h.d.

#### **TWIN-T NOTCH FILTER**

Probably the most simple filter that will give a narrow rejection notch is the twin-T notch filter. The circuit of a twin-T notch filter is shown in Fig. 2, and it should be apparent from this how the filter derives its name. which aspect of performance one wishes to improve. Here we wish to obtain a flatter response near to the resonant frequency of the filter, and this is achieved by the use of negative feedback. The circuit diagram of a practical filter employing this technique is shown in Fig. 3.

VR1 is the variable attenuator, and from here the input signal is fed to the input of the twin-T filter via Cl and R1. There are two sets of capacitors in the filter, and these can be switched by S1 to give a notch at either 100Hz or 1kHz. S1 also operates as the on/off switch. The lower value resistor of the network is made variable so that the circuit can be adjusted for optimum results.

The ouput of the filter is fed to an amplifier using a type 741 i.e. operational amplifier. As a single supply rail is used, a potential divider formed by R6 and R7 is necessary to act as a centre tap on the supply to bias the non-inverting input of the i.e. The circuit operates as an inverting amplifier with R4 and R8 setting the gain at 12.

#### SECOND FEEDBACK LOOP

There is, however, another feedback loop via R5. Thus as the attenuation of the filter increases towards

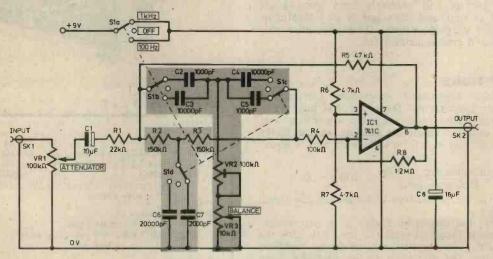


Fig. 3. Full circuit diagram of the filter

In order to give a good performance the components used in the filter should have a tolerance of 5% or better.

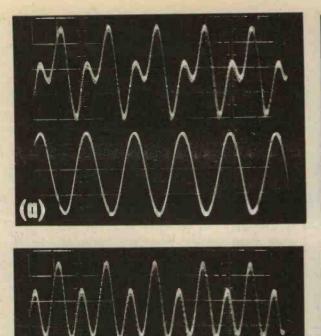
One drawback of this filter is that it attenuates the second harmonic by almost 6dB, and would also significantly reduce the noise from the amplifier. This would give rather an optimistic assessment of an amplifier's performance.

#### PRACTICAL FILTER

It is possible to improve the performance of a filter by including it in either a positive or negative feedback loop of an amplifier, depending upon its resonant frequency, the negative feedback is reduced and the gain of the circuit is increased. This counteracts the losses in the filter and gives a flatter response.

At, and very close to, the resonant frequency of the filter, the losses in the filter are extremely large, and the feedback is unable to significantly compensate for these with the maximum closed loop gain of the 741 circuitry set at only 12 by the first feedback loop.

The overall response of the circuit is therefore exactly what is required. It is flat over (and beyond) the audio frequency spectrum, except for a narrow notch of extremely high attenuation at resonance. The overall gain of the circuit is a little more than unity.



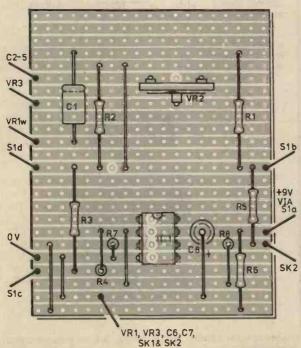
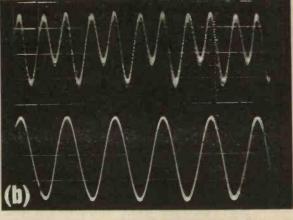


Fig. 4. Veroboard details and component layout



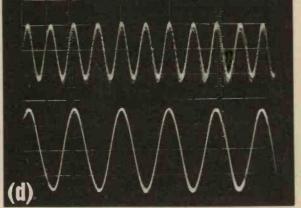


Fig. 5. Typical oscilloscope traces obtained using the filter: (a) balance control set roughly correct; (b) balance control adjusted to align tops of waveforms; (c) signal generator frequency then adjusted to align bottoms of waveforms; (d) distortion (predominantly second harmonic) and residual noise with fundamental notched out. The sinewave input is at 1kHz and the measured level of distortion is 1%

#### CONSTRUCTION

A ready made steel instrument case having outside dimensions of  $150 \times 100 \times 50$ mm provides a suitable housing for the unit.

Most of the small components are mounted on a piece of 0-1 in Veroboard having 24 strips by 19 holes. Full constructional details of this panel are shown in Fig. 4. No socket is required for the i.c. Veropins are used where connections are taken to the controls, sockets, etc. C2 to C7 were mounted on S1 on the prototype.

The general layout of the interior of the case is straightforward but make sure that the Veroboard panel is mounted in a position which enables easy access to the adjustment of VR2. A small mounting bracket for the battery is easily fabricated from a scrap of aluminium and glued in position.

#### ADJUSTMENT

Before the completed unit is ready for use, VR2 must be given the correct setting. To do this, connect a signal generator tuned to 1kHz to the input of the filter, and set the function switch of the filter to the 1kHz position. Set the slider of VR2



at the position which gives the lowest indication on an oscilloscope or millivolt meter connected to the output of the filter. VR3 should be set at its midway setting during this operation.

Now adjust the signal generator frequency control slightly either side of its initial setting in an attempt to obtain a still lower reading from the output indicator. Then readjust VR2 for the lowest possible output. Continue this procedure until no further improvement can be obtained. VR2 then has the correct setting.

#### **USING THE FILTER**

The rejection notch of the filter is very narrow and the adjustment of the input frequency and the balance control of the filter is quite critical. If the filter's output is being monitored by an oscilloscope, the following procedure can be adopted in order to quickly arrive at the correct settings of these controls.

With the controls set at roughly the right settings a waveform something like that of Fig. 5a should be obtained. The balance control is then adjusted so that the tops of the waveforms of the fundamental and first harmonic are aligned, as shown in Fig. 5b. The input frequency is then adjusted to align the bottoms of the waveforms (Fig. 5c). The balance control is then once again used to align the tops of the waveforms, as this whole sequence is repeated several times until the fundamental is almost completely suppressed, leaving only the noise and distortion (Fig. 5d).

#### **NECESSARY EQUIPMENT**

It is not absolutely essential to have an oscilloscope to monitor the output, but obviously this greatly simplifies and speeds adjustment of the equipment, and is the only way of being completely sure that the fundamental has been adequately suppressed. Also, it is not absolutely essential to have a millivoltmeter to measure the output, as most oscilloscopes will be capable of measuring the filter output level. If the distortion incudes a large amount of second harmonic distortion, however, it may be difficult to gauge the r.m.s. output level as it will not be a definite fraction of the peak to peak level, as is the case with a sinewave signal.

The signal generator needs to be a good quality type and should really have a distortion level less than 0.2% if accurate measurements are to be possible. The generator's distortion factor is measured using the set-up of Fig. 1, but of course with no amplifier intervening between the filter and the signal generator.



**NTEGRATED** injection logic  $(1^{2}L)$  is a fairly recent technology which many might have heard of in relation to the microprocessor.

In the beginning the areas of application envisaged embraced many of the products now made in CMOS, MOS and some low power TTL. Wristwatches were an obvious area of involvement since two of the advantages of 1²L are low power and low voltage requirement such as provided by small Mallory cells.

The recently announced Sinclair "Black Watch" kit utilises an 1²L i.c. and lays at once that bane to all MOS users—static electricity! There are actually no handling precautions necessary so it was with a gay heart and a nylon shirt that I got to constructing this.

#### ASSEMBLY INSTRUCTIONS

At  $\pounds 17.95$  it's obvious that an awful lot of people will have a go at this kit so simplicity in assembly instruction is paramount.

A component list allows you to first check the kit contents and to familiarise yourself with their shapes and identities. Tool requirements are next; soldering iron (suitably earthed), small wire cutter, fine-nosed pliers and non-metallic trimming tool.

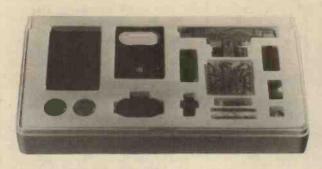
It should go without saying that anyone attempting an assembly of watch dimensions should have a steady hand and reasonable eyesight. An extension lamp and watchmaker's eyepiece is an ideal aid to this.

Of course, the iron is the most important tool. The bit should be small,  $\frac{3}{2}$  in is the best size. Recommended types are the Weller Marksman, Adcola Adamin or Antex CN. These should be earthed. It is at this point, when you have piece-parts and tools, to really read the instructions. Besides those on

It is at this point, when you have piece-parts and tools, to really read the instructions. Besides those on assembly there are some on using the watch which have important figures and there is also a separate addendum on bending details for a copper shield which can be easily overlooked.



Underside of the p.c.b. with all components assembled





#### PUTTING IT TOGETHER

Since there is no circuit diagram, the only concern is relating, with the correct orientation, the component parts to the p.c.b. provided. This little square is your work area and familiarisation with its copper geometry is to advantage. After preparation with varnish (solder and grease are also provided) the trimmer and capacitor are added. There is no need to pre-tin anything as the copper, leads and solder all showed a great affinity. When soldering in the quartz crystal an urgent iron is needed as overheating can be detrimental.

#### **DISPLAY AND I.C.**

The display has 14 pins and it is important to get the orientation right and this means picking out pin 1. An arrowed scale-of-two enlargement parades this in the instructions. All subsequent handling of the p.c.b. should be with care as the plastics lens can easily be scratched. And so on to the 18 pin d.i.p. i.e. The massive indent

And so on to the 18 pin d.i.p. i.c. The massive indent solves the orientation problem. Again a quick iron is needed. Part of the assembly time on this is spent in wrapping around a flexible p.c.b. which mates with one line of pins and provides contact pads for the batteries and touch pads for hours/minutes and minutes/seconds displays. This can be seen in the photograph.

It remains to check whether the electronics are "go". A bulldog clip is needed to make connection to the Mallory cells. You can't confuse the polarities as the clip, cells and p.c.b. are all shown in graphic perspective union in the literature. It remains to make metallic contact with the touch pads. My watch worked first time which is an endorsement to the excellence of the parts and the instructions. Obviously there will be people who will be disappointed at this point either through faulty components or an excess of zeal. Whatever—Sinclair provide a service guarantee for a charge of £3.50; this does not cover the cost of replacement parts, refundable if their components are at fault. The completed watch is covered by a one year guarantee.

#### ADJUSTMENT

After a 24-hour "burn-in" the copper shield is boxfashioned and slid over the module. The watch can now be accurately adjusted against a time signal (TIM or radio). At the trimmer, approximately 10 degrees of rotation will produce a change of one second a day.

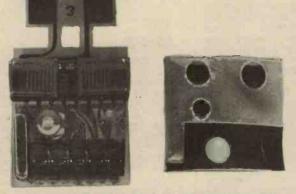
The module is now ready for case assembly which is simple and adequately described in the literature.

#### SIZE

In common with most digital matches, the "Black Watch" does cover a large area of the wrist. This with its box styling and plastic structure would seem to make it liable for easy damage.

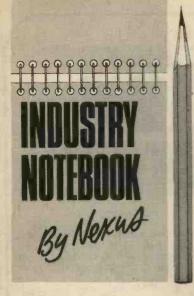
The conventional analogue watch is reassuring with its protective shockproofing and waterproofing and the habit of assessing a watch by these criteria dies hard.

However—accuracy is what timekeeping is all about and Sinclair does guarantee this to within a second a day with the possibility of improvement with adroit twiddling of the trimmer. G.G.



The assembled watch module and copper surround. It is essential that all components are closely seated on the p.c.b. and all lead ends cropped short or the copper screen will not fit. It is expected that the screen will be omitted from future kits with circuit modification.





#### COMMUNICATIONS

This year's Communications '76 Exhibition and Conference at the Metropole Convention Centre, Brighton, will be the shop window for what the British do best in electronics—communications. And so they should, having been first in the field.

The event is in June and already there are more exhibitors than for the last show in 1974 and they have booked more than double the floor space so that an additional hall in the Centre has been taken to accommodate the latecomers.

Ninety-nine learned papers are to be read. This, unhappily, means parallel sessions with up to three papers being presented simultaneously in different locations, leading to a measure of frustration. There are to be four incoming trade missions consisting of senior communications executives from 40 different countries and they will tour British industry as well as attend the exhibition.

Among the social events is a reception by Brighton Corporation's Mayor and Mayoress in the historic Royal Pavilion. Will it all lead to substantial new business? There will be well over 100 exhibitors and all expect to do well.

#### QUICK TUNING

With so much emphasis these days on satellite and microwave link communications, high-frequency radio tends to take a back seat but I am pleased to report that h.f., on which so many of us cut our teeth, still has plenty of life, not only operationally in the congested h.f. bands but also in new business. Marconi Communications has recently announced a new h.f. amplifier to be known as the H1140. It is a further development of the Marconi Self Tuning (MST) range and gives a mean or p.e.p. output of 10kW over the range of 1.6MHz to 30MHz. Input requirement may be any frequency within the range at any level between 50mW and 150mW.

The key feature, however, is that it tunes itself to any frequency in typically three seconds with no knob twiddling. Of course, Marconi is not alone in providing this type of feature which enables quick band changing either to overcome propagation variations or for security reasons.

Ten of the new h.f. amplifiers have been sold through NATO for installation at the Crimond Naval station to the north of Aberdeen. Due for delivery early in 1977, they will be used in a five-pair configuration to beef up NATO communications for Allied navies in Northern Waters. A subsequent NATO order, announced only a week later, is for low frequency drivers and amplifiers for Crimond. The first order was worth £400,000, the second £200,000.

Nice business for starters, and the NATO endorsement is excellent for future business of which Marconi expects plenty.

#### TV SAT-HOME LINK

The European Space Agency is pressing on with feasibility studies on direct colour-TV reception in the home from satellites. At present TV via satellite comes in to big receiving complexes like Goonhilly, then relayed to your local TV station and re-transmitted from there. The idea is that individual viewers should be able to receive the TV transmission direct from the satellite.

Well, there's nothing really to stop you doing that now if you are prepared to invest a million pounds or so in building a steerable 85ft diameter dish antenna in your garden, together with cooled parametric amplifiers and all the rest of the paraphernalia assoclated with space communications.

The reason why the big dishes are necessary is because of the comparative feebleness of the power transmitted from space, dictated by the type of payload put in orbit and the available power supplies. It follows that if you reduce the size of the earth dish to something that could be mounted on the roof or outside a window, the collecting area for the signal is so much reduced that, for the same results, the satellite must generate much more power.

So the drive is now on to get more powerful transmission from space, the target being 2kW of prime power and this brings its own problems, in the space environment, of thermal dissipation and equipment protection. Marconi Space and Defence Systems, who have a study contract from the European Space Agency, report that European development of high power travelling wave tubes is well advanced with 1kW already achieved in the allocated band of 11.7 to 12.5GHz.

The home receiver will have a mass-produced dish some 2½ft in diameter, expected to be plastic with a metallized reflective coating on the business side. There will, of course, also have to be an amplifier and frequency conversion equipment to feed a standard TV set.

#### POLICEMAN'S LOT

The policeman's lot is not a happy one. With terrorism added to rising figures for what we might call conventional crime, the workload is escalating and the need for quick response greater than ever. It is no wonder that police forces are investing in computerised command and control systems of a complexity approaching that used in military defence headquarters. The problems are the same in kind, differing only in detail.

Among the new installations now being fitted are one for the Suffolk Police and one for the Metropolitan Police. Suffolk is to use a system based on a GEC 4080 computer and the Metropolitan force one based on Data General hardware. Contractors, respectively, are Marconl Space and Defence Systems and International Aeradio Ltd.

Both systems make extensive use of visual display units as the interface with the computer and the IAL system, called RADIAL, also projects a map of the incident area for instant and accurate location data on which to base action.

#### LASERS

A recent building exhibition in London showed a remarkable penetration of laser technology into what is normally regarded as an industry conservative in outlook. There were laser plumb-lines, lasers for pipe-laying and trench digging, for distance measuring and for floor and ceiling alignment.

Another popular application is in meteorology and, in the electronics industry itself, Teradyne reports that there are now more than 30 automated laser trimmer systems, for hybrid microcircuitry, of their manufacture installed in Europe. Biggest users, however, are still the defence forces for range-finding, target-marking and weapon guidance.

# Next Month... Don't miss the variety of interests covered in this BUMPER ISSUE including Special 8 PAGE SUPPLEMENT

Surveys the various sound effects units currently in use. Defines terms, explains operation and outlines the circuit arrangements used to create these amusing, amazing, and sometimes quite startling, effects

# **DIGI-PROBE**

A most useful and easy to use instrument invaluable to all who work with logic circuits. Seven segment i.e.d. gives precise indication of steady state logic, and pulse decimal point Indicates high speed switching

# A.D.S.R ENVELOPE SHA

An add-on unit for electronic musical instruments such as organs and synthesisers to give a wide range of interesting effects. Four controls give a multitude of different envelope shapes which will greatly enhance the range of sounds

# Fun for all the family with this fascinating game to test your speed of reaction. All you have to do is to "hit" a moving light as it moves along a row of light emitting diodes, but each time you "miss" the game

1.7.1.7.1.1.1.1.1

# PRACTICAL RON APRIL ISSUE ON SALE MARCH 12, 1976

PLEASE NOTE:

It is in your interest to place a firm order with your newsagent-in advance. Back numbers are not available, so make sure of your copy nowl

# SENICONDUCTOR UPDATE DO By R.W. COLES

1720R 1723R MC14419 8038

#### THE BIG RED "ONE"

Ever since l.e.d. displays of the seven-segment variety first saw the light of day, they have suffered from one serious drawback—size—or rather, lack of itl The usual size range for early devices was about 2.5mm to 7.5mm character height, which meant that a good pair of eyes and/or a magnifying lens were required tor easy reading.

Of course, there are applications which require this diminutive sort of display, but manufacturers have been constantly aware of their inadequacies in this department and have been striving to compete with the larger Minitrons and Nixie tubes for the lucrative slice of the market which includes all those of us whose vision is not quite what it used to be!

The first step in the right direction came in the form of the 15mm "Jumbo" devices which use the light-pipe technology to channel the light from single-point source l.e.d. chips into fair sized segments. This light-pipe success has now been followed by an even bigger 25mm display which is easily visible over a 20m viewing distance.

This new "King-size" device is made in the U.S.A. by a firm called Industrial Electronic Engineers Incorporated but is available in the United Kingdom from the rather more familiar "Perdix Components Ltd." It is produced as a common anode type (1720R) or a common cathode type (1723R) and comes in a 14-pin package with 15mm row spacing so that it can go into a standard 24-pin d.i.l. socket. Each segment is lit from not one but two I.e.d. chips in serles so that the forward voltage per segment is about 3·3V at 20mA.

#### **KEY CODER**

It is the modern trend to replace conventional knobs and switches with a calculator style keyboard. This approach can cut out a lot of hardware for the extra cost of a handful of logic and analogue chips, and lends itself well to the allpowerful l.s.i. technology with its promise of extremely low prices for large quantities.

Signal generators, even power supplies, can now be obtained with an I.e.d. display and a functional key-pad as the only external sign of the "goodies" within. To select, say, a frequency and output level on a signal generator of this type, one would simply punch in an appropriate string of digits to get an instant response, with no necessity for knob twiddling at all!

This is all very well for the larger manufacturer, but the sad fact is that the nuts, bolts, and dial-cord approach has still been the only solution for us amateurs, or has at any rate, until now. The range of c.m.o.s. logic systems produced by Motorola has been mentioned before in this column, and a new addition to this range, the MC14419, looks like being the start of a breakthrough which will result in keyboards sprouting in the most unlikely places.

The MC14419 is the answer to the keyboard-fancier's dreams, since it combines in one easy-to-use 16-pin d.i.l. package:

- A 16 key-to-binary encoder.
- A rollover protection circuit.
- A delay circuit for key de-bouncing.
- A strobe pulse generator.

The key switches required are of the simple "push-to-make" type arranged as a  $4 \times 4$  matrix, and with a full sixteen keys to play with, there is plenty of scope for control functions, decimal points, and arithmetic operators in addition to the ten numeric keys normally employed.

#### VERY FUNCTIONAL

My next offering is an integrated circuit which has been around for about a year now, but, surprisingly, has not had the coverage it deserves. I am referring to the 8038 function

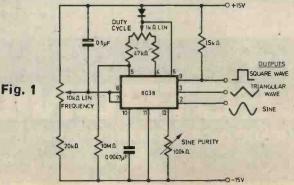
generator introduced by Intersil, and even if you have heard of it before I am sure that you will agree that it is worth a second look (Fig. 1).

The 8038 is a chip with universal appeal for electronics enthusiasts, because whether you are a "Logic person" or an "Audio person" you will find it hard to resist a single integrated circuit which gives simultaneous sine, square, and triangular wave outputs over the frequency range 0.001Hz to 1MHz. If those features are not enough to make you an instant fan, then perhaps the fact that a voltage controlled input is provided to facilitate frequency modulation or frequency sweeping, will do the trick. For the sacrifice of the sine output you can also generate a sawtooth from the triangular output and a pulse waveform from the squarewave output, simply by varying the duty cycle, and all this is available for a mere £3.00 from amateur suppliers.

Before everybody starts reaching for their piggy-banks perhaps I had better be scrupulously fair and point out a couple of snags!

The biggest flaw in the operation of the 8038 is undoubtedly the fact that the sine output is *not* distortion free, and this is not really surprising when the method of sine generation is examined. The sine waveform is produced by "whittling away" the triangular wave in the right places to give an approximation ot a sine curve, with the possibility of minimising distortion with an external pot. Performance can be improved with an external filter it required.

The outputs of the 8038 are of the high impedance type and should not be connected to a load of less than 10k ohms, which in practice means that an Op-Amp buffer may be required in certain applications.



# PART ADDITIONS TO THE BASIC DESIGN

* Mains operation plus Latch and Controller facilities

### By M. Fischer*

A simple and attractive mains only digital alarm clock can be constructed using the clock PCB (PCB2) and the display PCB (PCB3) included in last month's car clock. The changes in design involve the addition of three rectifier diodes and a 50Hz diode to PCB2 changing the value of segment current limiting resistors (R29–R35), and of course adding a mains transformer.

#### POWER SUPPLY DESIGN

Two supply lines are required providing 14V at 20mA and 6V at 500mA as seen in Fig. 12. The capacitors are needed in both versions.

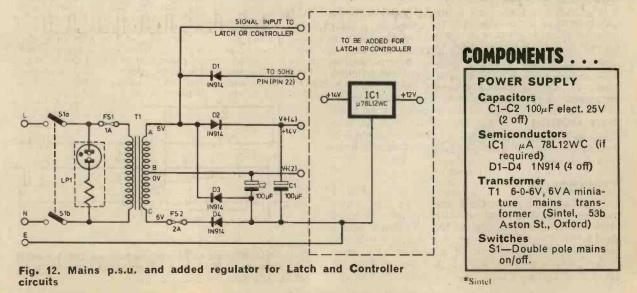
For the V + (4) supply, when pin A of Tl nears its maximum positive voltage with respect to pin C, diodes D3 and D1 conduct to charge C1, providing a half-wave rectified and smoothed 14V for the MK 50253 positive supply.

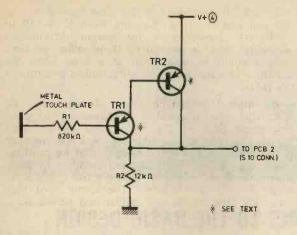
For the V + (2) supply, D1 and D2 cause a full wave rectified voltage at V + (2) with respect to 0V, with a peak voltage of approximately 7V. The current flowing between V + (2) and 0V is so large that C2 provides little smoothing and the ripple voltage is about 5V. This causes a 100Hz ripple in the display brightness, which is, however, invisible to the human eye.

If V + (2) and V + (4) had been obtained from, say, a single full wave rectified and smoothed supply, as has been the case in most other clock designs, four rectifier diodes would have been required instead of three, and Cl would have had to be increased to  $2,500\mu$ F. This would have changed the peak current through Tl from 0.5A to about 5A, which would have required a transformer with a rating of about 12VA rather than 6VA.

#### CHOICE OF TRANSFORMER

There are several 6V-0-6V, 6VA miniature transformers on the market but constructors are warned that those tried got fairly hot in mid-summer, even with no load. The various manufacturers told us that, in order to build a miniature transformer with





#### Fig. 13. Touch switch snooze control

a low variation in output voltage with load, the transformer has to be made "loosely", and hence runs hot. As this application can tolerate large percentage changes in transformer voltage, we have had some wound on a high-efficiency core, with low loss windings. This transformer runs remakably cool, and we do not recommend that constructors use any other if building the clock in the case specified.

#### TOUCH SWITCH SNOOZE

Those who want the magic of a touch switch snooze control can mount the components shown in the circuit diagram in Fig. 13 on a small piece of Veroboard.

When the touch plate is touched with a finger, the 50Hz signal picked up by the body causes the Darlington pair TR1 and TR2 to switch on and off at 50Hz, providing positive pulses for the snooze control. The touch plate can be any metal object such as a screw, etc. When the snooze is activated, the alarm tone disappears for about ten minutes.

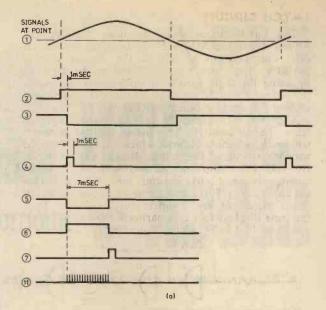
These are two functions which allow the mains clock to be used as more than a simple clock.

#### DISPLAY LATCH

The Display Latch adds a digital memory to the clock so that, when a button is pushed or a relay contact is closed, the time shown by the clock is stored in a memory, without affecting the normal operation of the clock. Switching is provided so that at any time, either the time given by the clock chip or the time contained in the memory can be displayed. So far we have used this in two applications. In the first, the unit was needed as an event timer to record the exact time of faults in an electrical sub-station. In the second the instrument was needed to record the finishing time of sailing boats in a boat race.

#### CONTROLLER

The Controller turns the digital clock into a time switch. Typical applications in mind were to use a dual unit to control a Video Tape Recorder with a facility for a warm-up period, and an alarm to sound three times a day to remind personnel at a mailorder components company to get the mail to the local Post Office in time for the various collections.



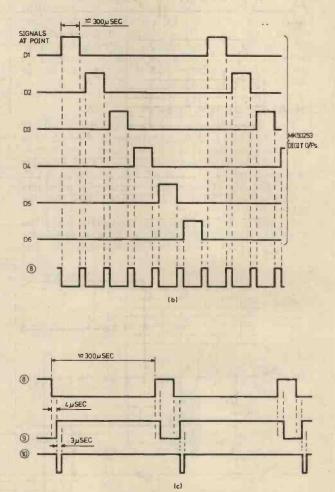


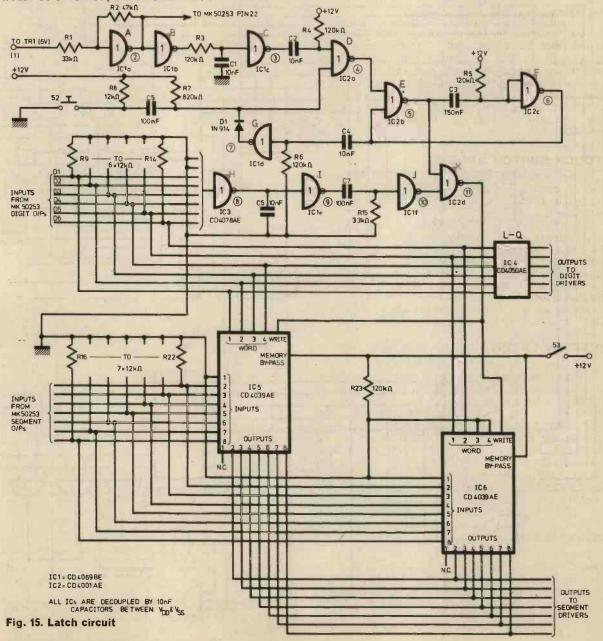
Fig. 14(a). Signals at points marked on Latch circuit (b) Signals at IC5/6 and (c) enlarged view of these at (8), (9), (10)

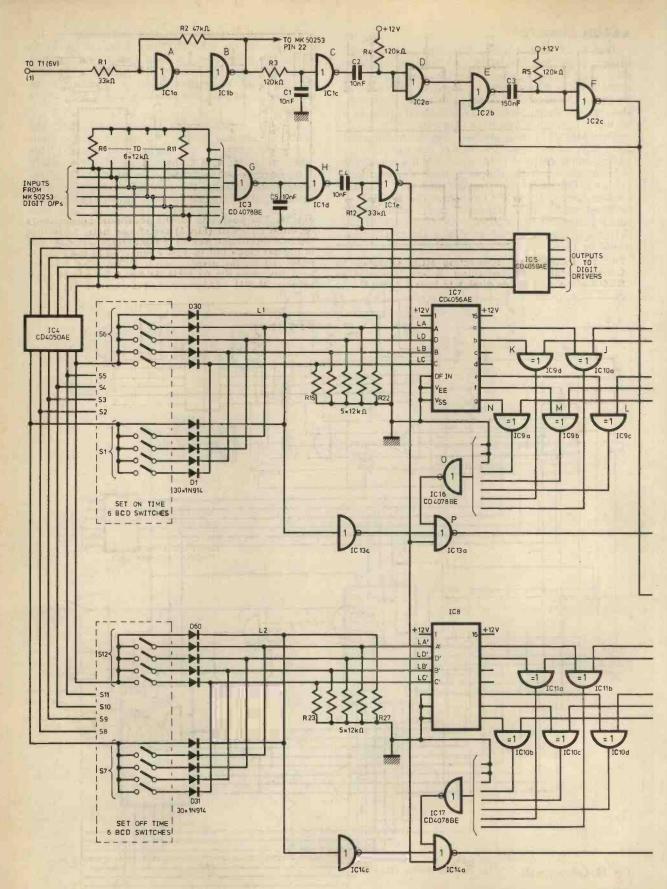
#### LATCH CIRCUIT

The Latch circuit takes the digit and segment drivers from the MK 50253 and supplies alternate digit and segment signals to the display driving circuitry. The clock time is stored in the memory by using the digit signals to write seven bit words, the segment signals, into two CD4039AE's used as a six word  $\times$  seven bit memory (Fig 14).

The MK50253 outputs are signals multiplexed from internal counters. This means that the counters will be incremented at times which are not correlated with the timing of the output signals. For example, D1 and D2 might be scanned with the internal counter being 12:01:59 and then before D3 is switched on, a 50Hz transition could occur which could increment the counters to 12:02:00. Thus the time displayed in this particular D1 to D6 scan would be 12:02:59, which is incorrect. In normal practice this does not matter as the eye just sees the time changing from 12:01:59 to 12:02:00. However, if the output information is being held in memory, it is quite possible that it could be written in at a time when the sequence of outputs is misleading, unless precautions are taken.

A little experimenting has shown that the MK50253 internal counters increment on the positive going edge of the 50Hz input signal. This means that one can confidently load the memory if the loading starts long enough after the positivegoing edge to allow the internal counters to settle down and finish before the next positive going 50Hz edge, 20 milliseconds later. The circuit used here loads the memory for a 7 millisecond period starting 1 millisecond after the edge in question.





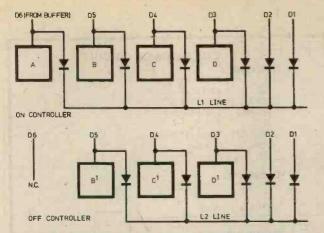


Fig. 17. Example of connecting BCD switches to Controller for on/off switching. A box indicates as BCD switch with series diodes to lines LA to LD

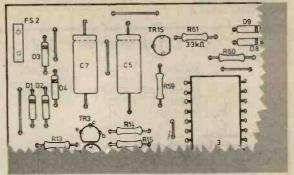
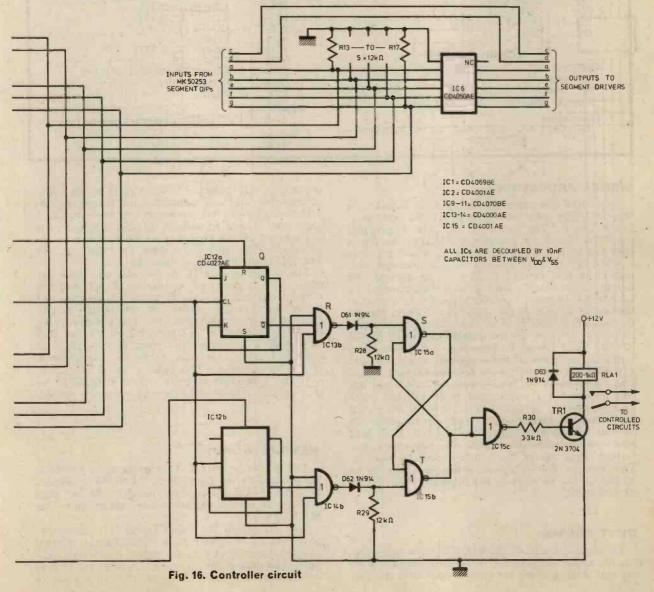


Fig. 18. The positions for the additional components required on PCB2 (Fig. 5) are shown here. Note that the rear right-hand pad on the underside was not used in the car clock but is now connected to the outside right pad on the display p.c.b. PCB4. The START I.e.d. becomes the ALARM ENABLE I.e.d. R61 is in series with S11. (Alarm circuit is given in Fig. 3)



## COMPONENTS . . .

LATCH CIRCUIT	CONTROLLER CIRCUIT
$\begin{array}{c ccccc} \textbf{Resistors} \\ R1 & 33k\Omega & R8-R14 & 12k\Omega & (7 \circ ff) \\ R2 & 47k\Omega & R15 & 3 \cdot 3k\Omega \\ R3-R6 & 120k\Omega & (4 \circ ff) & R16-R22 & 12k\Omega & (6 \circ ff) \\ R7 & 820k\Omega & R23 & 120k\Omega \\ All & 10\% & W & carbon \\ \hline \textbf{Capacitors} \\ C1-C2 & 10nF & (2 \circ ff) \\ C3 & 150nF & \pm 10\% \\ C4 & 10nF \\ C5 & 100nF \\ C6 & 10nF \\ C7 & 100nF \\ \end{array}$	Resistors           R1 $33k\Omega$ R2 $47k\Omega$ R3-R5 $120k\Omega$ (5 off)           R6-R11 $12k\Omega$ (6 off)           R12 $33k\Omega$ R13-R29 $12k\Omega$ (17 off)           R30 $33k\Omega$ All 10% $\frac{1}{4}$ W carbon           Capacitors           C1-C2         10nF (2 off)           C3 $150nF \neq 10\%$ C4-C5         10nF
C8-C13 10nF (6 off) decoupling for i.c.s.	C6-C22 10nF (17 off)
Semiconductors IC1 CD4069 BE IC2 CD4001 AE IC3 CD4078 AE IC4 CD4050 AE IC5-IC6 CD4039 AE (2 off) D1 IN914 TOUCH SWITCH	Semiconductors           IC1         CD4069 BE           IC2         CD4001 AE           IC3         CD4078 BE           IC4-6         CD4050 AE (3 off)           IC7-8         CD4056 AE (2 off)           IC9-11         CD4070 BE (3 off)           IC12         CD4027 AE           IC13-14         CD4000 AE (2 off)
Resistors         R1       820kΩ         R2       12kΩ         10% ‡W carbon         Transistors         TR1-TR2       Any pnp small signal transistor—         BC212 etc.	IC15         CD4001 AE           IC16-17         CD4078 BE (2 off)           D1-D63         IN914 (63 off)           TR1         2N3704           Switches         S1-S12         BCD switches (as many as required)           Relay         RLA1         200Ω-1k         6-12V

#### SIGNAL PROCESSING

The 50Hz sine wave signal input (1) is fed to a Schmitt trigger gate consisting of R1, R2 and inver-ters A and B. The output of this gate (2) provides the 50Hz signal for the MK50253. This output is then fed to R3, C1 and inverter C, which provides a 50Hz square wave delayed by 1 millisecond with respect to that at (2). If S1 is being pressed, the output of inverter C, having been differentiated by C2 and R4, causes a 1 millisecond pulse to appear at the output of gate D (4). If S1 is not being pressed the output of gate D stays low. The 1 millisecond pulse then triggers the monostable consisting of C3, R5 and gates E and F, providing a negative going 7 millisecond pulse at the output of gate E (5) and a positive going one at the output of gate F (6). The output of gate F is differentiated by C4 and R6, and produces a 1 millisecond positive going pulse at the output of inverter G (7). If S1 is still closed the output of inverter G charges up capacitor C5 so that the corresponding input to gate D is held high, which holds its output low, preventing any further triggering of the 7 millisecond monostable. This ensures that the time which is going to be written in the memory is the time at which the S1 closure starts.

#### DIGIT PULSES

The digit outputs of the MK50253 are non-overlapping sequential pulses. The segment outputs' leading and trailing edges are synchronous with the corresponding digit pulses. The write pulse which writes information into the memory must therefore start after a digit pulse has gone high and finish before it goes low. The digit outputs of the MK50253 are fed into a CD4048 used as a six input NOR gate. Six 12 kilohm pull-down resistors are used as the MK50253 only pulls the outputs up.

The output of gate H (8) provides one pulse per digit. This is then fed to inverter I. C6 and the output resistance of gate H cause the output of I to be an inverted version of the signal at (8), delayed by 4 microseconds (9). The positive going edge of this signal is differentiated by C7 and R15 to provide a 3 microsecond pulse at the output of inverter J (10). This pulse fulfils the requirements of the "write pulse". This pulse is gated by gate K with the 7 millisecond pulse output of gate E, so that writing only occurs when S1 has been pushed.

#### MEMORY WORDS

The memory words that are going to be written in are selected by the digit signals D1 to D6 (connected to the CD4039 word select inputs), and the data written in is the segment data, taken from the MK 50253.

With S2 closed the two CD4039's "memory bypass" inputs are held high. This causes internal switches to connect the data inputs to the data outputs. The data outputs are used to drive the display segment drivers (those of an ordinary mains clock). Thus with S2 closed the display shows the ordinary time. With S2 open, the memory outputs will be the information selected by the word select inputs in the same way as during writing. Thus the display will now show the time stored in the memory.

A hex buffer (buffers L, M, N, O, P, Q) is used to buffer the signal to the clock digit drivers. No buffer is required on the CD4039 outputs as these have a high current sourcing capability. When no word of a CD4039 is being selected, its data outputs are left floating, which allows the two i.c. outputs to be wired in parallel as shown.

A plastic transistor-sized three terminal regulator  $\mu$ A78L12WC is used to provide 12V for the CMOS and also the V_{ss} supply to the MK50253.

#### CONSTRUCTION

Full constructional details are not given but the following notes should assist.

The units may be built on Veroboard, d.i.p. board, etc. All i.c.s should be decoupled between the  $V_{DD}$  and  $V_{SS}$  pins with a 10nF capacitor.

As the segment and digit drivers, and the MK50253 connections other than digit and segment outputs are identical to those of an ordinary mains clock, the Latch may be built as an addition to the latter. The  $3\cdot3$  kilohm resistors in series with each segment and digit output can be mounted on the Veroboard rather than p.c.b. to provide input and output connections to the Latch.

As described the instrument has one display which displays either the time or the contents of the memory. If separate displays are wanted, display driving circuitry will have to be duplicated, and the original segment and digit information will have to be tapped off at the appropriate points and buffered before going to the drivers.

More than one Latch can be added to one clock, although separate displays or complex display switching will be required.

#### CONTROLLER CIRCUIT

The aspect of the Controller circuit which is common to the Latch circuit is the need to use only the outputs of the MK50253 when they are stable. For this reason gates A to I of the controller circuit perform the same functions as the corresponding gates in the Latch. The only difference is that the monostable consisting of gates E and F is fired every 50Hz cycle rather than only when a button has been pressed (Fig. 16).

The output at (1) consists of 7 millisecond pulses which define periods during which the MK50253 count will not change. The pulses at (2) are high at times when the segment and digit outputs of the MK50253 have settled down. During a particular digit time, say D1, the information present on lines LA, LB, LC and LD will correspond to the value selected by the BCD switch S1. This binary information is converted to seven segment information by the CD4056 BCD-to-seven-segment decoder. Five of these segments are then compared with the corresponding MK50253 segment outputs by EXCLU-SIVE-OR gates. The comparison only needs to be made using the five segments shown as these uniquely determine the digit value.

The EXCLUSIVE-OR gates truth table is such that their output is a "1" when their inputs differ.

The outputs of the EXCLUSIVE-OR gates are combined by the NOR-gate "0". The output of this gate is low whenever the BCD switch value and the MK50253 value of a digit differ. This output is then gated by gate **P** by two signals. One is the inverted value of line 1 and serves to blank any "digits not equal" signal which occurs during a digit time for which no comparison is required. The other blanking signal is that at (2) which only allows a "digitsnot-equal" signal to be passed once per digit time, after the MK50253 outputs, etc. have settled down.

At the beginning of a 7 millisecond pulse from (1), J-K flip-flop Q is clocked, and its Q output is set to "1". If the time indicated by the MK 50253 is different to the time set by the BCD switches, during the following 7 milliseconds one or more "notequal" pulses will apear at the output of gate P, resetting the flip-flop Q to "0". This will ensure that the output of gate R remains "0", as for it to be a "1", the "Q" output of flip-flop Q still has to be a "1" at the end of the 7 millisecond period, when (2) goes to a "0." If the two times are equal flip-flop Q's output "Q" will still be high when (2) goes low, and the output of gate R will set the alarm R-S flip-flop consisting of gates S and T, turning the controller output relay on. An identical system is used to clear this R-S flip-flop and turn the controller output off.

#### **CONTROLLER NOTES**

Some additional notes as for the Latch are in order. For example, more than one on-off Controller can be added to one MK50253 clock. That part of the circuit shown in dotted lines need not be repeated —the signal produced by it can be fed to several controllers in parallel.

The L1 and L2 lines and the diodes going to them tell the circuit which digits will be looked at to set or clear the output. This enables one to economise on BCD switches. For example, the following arrangement will switch on at an exact time defined in hours and minutes, and off up to several hours later, using a total of seven BCD switches (Fig. 17).

This controller will switch on at AB:CD:00 hrs, and switch off at the next XB':C'D':00 hrs, where X can be any value.

Where, in a given digit position, there is only a diode to the L1 or L2 lines, but no BCD switch, this circuit behaves as if there is a BCD switch with its value set to "0". Where no L1 or L2 diode is connected, that digit will be ignored by the controller. Substitutes can be used for the BCD switches shown. In some applications the BCD values can be hard-wired; in others d.il. pin headers and sockets can be used to set the times by "plugging" values in.

As shown, a single controller has two switching times, which sequentially switch an R-S flip-flop on and off. The controllers could be built with only one switching time, or with both switching times connected as switching on times, with a manual off.

NOTE: The toned area in Fig. 6 (last month) should be traced out and dropped in the centre cut-out in Fig. 7 (PCB2). The black lines from PCB1 to the tone area are the interconnecting wires to PCB2.

In Fig. 1, the V + (5) line to IC2 should be V + (3).

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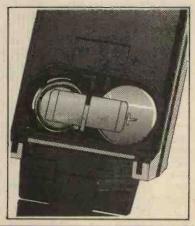
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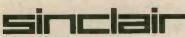
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A selection of readers suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought. Any idea published will be awarded payment according to its merits. Why not submit YOUR IDEA?

#### Please Note

Articles submitted for publication should conform to the usual practices of this journal, e.g. with regard to abbreviations and circuit symbols. Diagrams should be on separate sheets, not inserted in the text. secondary winding should be preferably 24V or more, so that the signal is not attenuated too severely. The output impedance of this system is extremely low, allowing for a perfect match to any amplifier, and a long interconnecting cable.

For best result, R5 has to be the nearest value to the d.c. resistance of the transformer's primary winding. When R5 has been chosen correctly, the voltage at TR2 collector should be about 6V; if it is not R4 should be increased or decreased as necessary. The preset VR2 should be adjusted to the highest possible output without running into distortion.

The current consumption of the unit is around 1.5mA at 9V. The supply voltage  $V_{s}$ , can be tapped

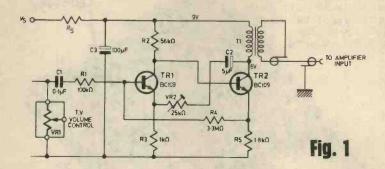
#### **TV SOUND ADAPTOR**

Most television sets do not employ a mains transformer and may not be connected directly to external amplifiers. There are some sophisticated commercial units which deal with television sound, but these are rather expensive. The circuit in Fig. 1 overcomes this problem economically and maintains the required electrical isolation of the television.

The input to the circuit is taken from the top of the television volume control. In this way, the signal presented to the external amplifier is independent of the television volume setting.

At this point, the signal has not been processed by the television audio circuitry, it does not suffer from the distortion associated with such circuits, and is suitable for reproduction through high quality audio systems.

The input impedance of this circuit is around  $500k\Omega$ , so it will not load the television audio circuits.



After amplification. the signal is presented to the external amplifier through T1, the primary of which is the collector load of TR2. Transformer T1 must be a mains

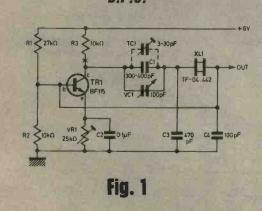
Transformer TI must be a mains type so that one may be confident that the insulation between the primary and secondary windings can stand accidental mains voltage. and provide the necessary degree of safety. The transformer can be any miniature mains type. the off the television audio board or tuner. The value of the resistor  $R_s$  should be chosen according to the formula:

$$\mathbf{R_s} = \frac{\mathbf{V_s} - \mathbf{9}}{1 \cdot 5} \mathbf{k}$$

The circuit was tried on a few different TV sets, and was proved to be capable of producing sound of truly high quality.

M. Greenfield. Leeds

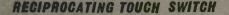


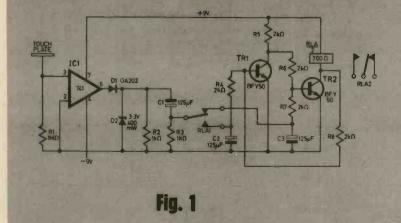


**R** EADERS interested in short wave reception who at present use a b.f.o. with the normal coil arrangement may like this circuit which will enable them to achieve a higher stability oscillator.

The circuit shown in Fig. 1 is an oscillator based on the Pierce arrangement. The series resonant frequency of the crystal is 442kHz but it can be raised by adding series capacitance. About 500pF is required to achieve the popular working frequency of 455kHz. This is made up with a 350pF fixed capacitor and a 100pF trimmer in parallel for fine adjustment.

E. Vaughan, High Wycombe.





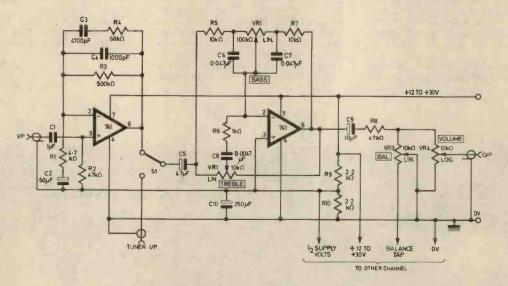
D ESIGNED to operate a bedside lamp (using the remaining contacts RLA2), the circuit shown in Fig. 1 uses an interesting form of bistable, which unlike conventional types, does not need a steep rising edge to trigger it. Despite its limitations (it will not operate at more than 0.8Hz), it does away with the need for a Schmitt trigger.

The Zener diode was found to be necessary to limit the input to three volts otherwise when a signal is applied to the touch plate the bistable becomes free-running.

Miss V. Mouricio, Lingfield.

Lingheid

#### HIGH QUALITY STEREO PRE-AMPLIFIER



M ost i.c. pre-amp circuits specify the use of specialised, and sometimes hard to obtain, integrated circuits. There is no reason, however, why the ubiquitous (and cheap!) 741 should not be employed in this application. Fig. 1 shows a circuit using these which does not require the normal dual power supply and will in fact operate satisfactorily on any single unregulated supply in the range 12 to 30V.

The circuit shown is for use with a magnetic cartridge. IC1 provides most of the overall gain and the

#### Fig. 1

network C3, R4, C4, R3 provides RIAA equalisation to within 1dB between 20Hz and 20kHz, IC2 is the active element of the tone control which provides ±10dB of control of bass and treble. An input level of 4mV gives an output of around 500mV at 1kHz with the tone controls flat. For use with cartridges other than magnetic, R2 should be adjusted to suit the manufacturer's loading recommendations, and R1 should be selected to give the required a.c. gain. A second switched input is provided for connection to a tuner, etc. and has a sensitivity of approximately 500mV.

The layout of the preamplifier is not critical provided that normal screening precautions are observed on all signal leads longer than 2 or 3 inches.

The prototype was built on Veroboard and gave excellent results with negligible hum, noise and distortion, even with 3 volts of ripple on the power supply.

> M. W. Clarke, Princes Risborough.

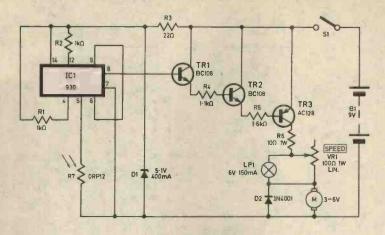
#### LIGHT OPERATED SWITCH AND MOTOR DRIVER

The purpose of this unit is to operate a motor when light stops falling upon the light dependent resistor. When light is falling upon the ORP12, it conducts and the gate is at "0" in positive logic. One of the gates is kept permanently at "1" by R1 and therefore since it is a NAND gate, the output is "1". The second NAND gate acts as an INVERT gate by having one of the inputs kept at "1" permanently, therefore the output is at "0".

The i.c. is a DTL 930 which needs a supply of 5V and this is achieved by using a Zener diode of 5¹V with a rating of 400mW, in conjunction with a 22 ohm resistor. This output is fed into the base of TR1. The base emitter voltage is kept at 0.6V by R4 and the base emitter voltage of TR2 is kept at 0.6V by R5. This resistor also drops the voltage for TR3 and provides base current.

TR3 supplies the current to drive the motor and lamp. R6 keeps the current to below the Ic max. of TR3. VR1 adjusts the speed of the motor and also the brightness of the lamp which is inversely proportional to the speed of the motor. In this case the motor is not turned on because of the "0" input to TR1.

With no light present on the ORP12 one of the inputs to the



first NAND gate is at "1" and the other input automatically becomes "1". An output of "0" is produced and this is fed into the second NAND gate producing an output of "1" which is fed into the base of TR1. This transistor switches TR2 to the logic level and then TR3 starts to conduct, producing a current which drives the motor and lamp LP1. Due to greater current consumption of the motor the more the bulb light

#### Fig. 1

diminishes the faster the motor goes. Any motor of 3-6V can be used.

The lamp indicates if the circuit is working since sometimes the motor will not work until VR1 is set for high speed.

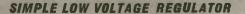
The operation may be reversed by connecting the base of TR1 to the output of the first NAND gate.

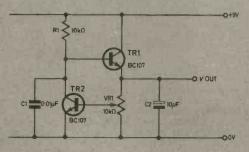
> P. V. Saduikis, Leeds, Yorks.

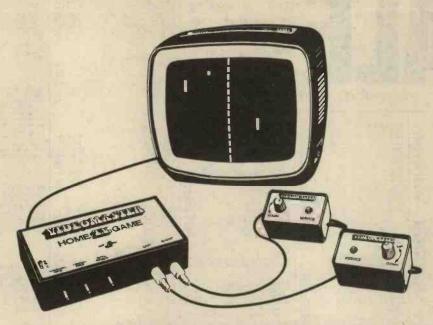
THE circuit in Fig. 1 shows a simple regulator suitable for feeding the ZN414 radio receiver i.c. The ZN414 is very voltage conscious and both the diode and transistor drive circuits recommended by Ferranti do not stabilise the supply well enough to compensate for falling battery voltage with a consequent loss in gain. Also it is useful to be able to adjust the supply voltage to the i.c. in order to obtain the optimum gain/selectivity conditions.

TR1 operates in the emitter follower mode. When the voltage at the base of TR2 rises to 0.7V, TR2's base drive via R1 is reduced, holding the output to a value preset by VR1. Capacitor C2 is present to maintain stability.

M. J. Meaken, Gatley,







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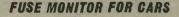
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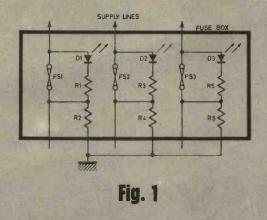
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**F** uses have a nasty habit of blowing at very inconvenient times, such as when its dark, cold or wet. This simple arrangement can provide an easy-to-see monitor as to the state of the fuses and thus can save a lot of bother.

The circuit is very straightforward; light emitting diodes are used in series with  $2.7k\Omega$  resistors across the various fuses. A further  $1k\Omega$ resistor is connected from the chassis to R1. When the fuse is good the l.e.d. and R1 are shorted out and the l.e.d. remains off. However, when the fuse is open circuit, current flows through the l.e.d. and a fault is indicated. For positive earth operation the l.e.d. must be reversed.

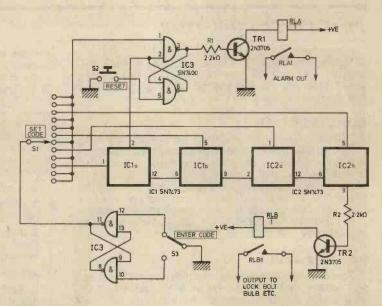
A. Foster, Germany.

#### **DIGITAL COMBINATION LOCK**

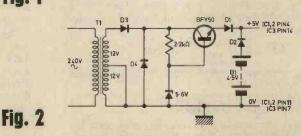
THE flip-flops (Fig. 1) have their outputs connected to the clear inputs of the next stage and the J and K inputs are left free. When flip-flop 1 (IC1a) is reset its Q output goes to logic 0. This resets the next stage and so on to flipflop 4 (IC2b). With the Q output of IC2b at logic 0, the output is inactivated. This means that each flipflop has to change state in turn (enabling the next stage) for the output to be activated.

To enter a chosen number, the number is set on the l-pole 12-way switch and S3 is pressed. The two NAND gates eliminate switch bounce so that the flip-flops do not fire twice. If a number is entered twice its corresponding flip-flop will set all the flip-flops after it. If an unallocated number is entered then the alarm will sound, and can only be stopped by pressing the reset button, which also clears all the flip-flops.

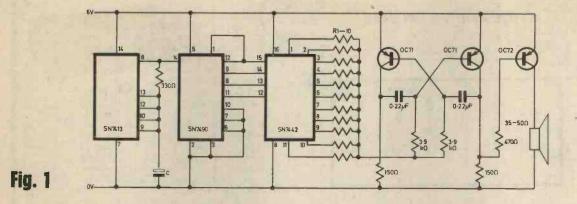
N. M. de Smith, London.







#### AUTOTONE MK 2



T HE circuit in Fig. 1 is similar to the Autotone published in P.E. about a year and a half ago. The ring counter has been replaced by a triple i.c. system. An SN7413, R1 and C1 forms an oscillator which then drives a 7490 decade counter. This then feeds a 7442 decoder which sequentially public resistors R1-10 to earth. The

frequency of operation of the astable (TR1 and TR2) is therefore determined by which resistor is grounded. The resistor values to provide reasonable operating frequencies of the astable were found to lie in the range zero to about  $10k\Omega$ . An absence of one of the resistors provides a break in the sequence. TR3 provides an output suitable for driving a loudspeaker. It must be borne in mind that the sequence of notes will repeat themselves as the 7490 resets to zero after a count of nine, but interesting tunes can nevertheless be composed.

C. R. Batchellor, Brentwood.

#### PEAK LEVEL INDICATOR

continued from page 204

When the negative voltage at TR1's base disappears TR1 and TR2 revert to their quiescent state; but TR3/4 will remain cut off (D2 "on") until C2 has charged to about +1V via the 1M $\Omega$  resistor.

#### CONSTRUCTION

All components are standard items and they may be accommodated on a printed circuit board measuring only  $6.5 \times 4$  cm (stereo version). The board layout and printed circuit pattern for the stereo version are illustrated in Fig. 4, and it must be noted that it will be difficult to fit the components unless the low wattage types, as specified, are used.

For long term reliability C2 should be a tantalum capacitor as specified.

#### **POWER SUPPLY**

The circuit will work to specification with a supply voltage in the range 16 to 24V, and this falls within the supply range of the majority of preamplifier designs. Sensitivity outside these limits may not be according to the specification, but a range of 12 to 30V can be accommodated by changing the value of R7:

$$R7 = \frac{\text{Supply volts}}{20}$$
 kilohm

The current required is approximately 22mA (44mA for stereo version).

#### SENSITIVITY IMPROVEMENT

At 500mV the sensitivity will be adequate for most monitoring applications, but it can be improved upon, if required, by modification of component values around TR1.

As mentioned earlier, the gain of the first stage is determined by the ratio R2/R1, and the value of R2 has been specified very conservatively to ensure that the stated sensitivity figure will be met, even with a relatively low gain transistor at TR1. But a decent BC107 will allow for a considerable increase in the value of R2, with a commensurate increase in overall sensitivity. To determine the optimum value:

1. Replace R2 with a  $1M\Omega$  variable resistor.

2. Vary R2 to set the voltage at TR2 collector to (no more than) +3V.

3. Measure the resultant value of the variable resistor and replace with the nearest preferred value fixed resistor below that measured.

There are two other methods:

1. Reduce the value of R1 (lower limit 470 ohms): this will give a significant increase in gain, at the expense of a lowering of the unit's input impedance, and it may need to be driven from a low source.

2. Replace the 8.2V Zener diode with a lower voltage type (minimum value equal to the voltage at TR1 collector plus 1.5V): at best this will only allow the gain to be doubled, and the threshold discrimination will be widened with consequent diminishing of the visual impact of the l.e.d. output.

The maximum sensitivities achieved with the original units were in the range 25 to 40mV.



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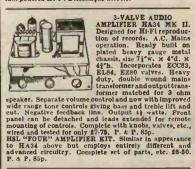
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#### **P.E. PRODUCT REVIEW**

# HEWLETT PACKARD

THE 3476A/B DIGITAL MULTIMETER

A new, competitively priced, 34 digit, autoranging digital multimeter has been introduced by rewlett Packard. The instrument is priced at £144 with built in mains unit or £175 with rechargeable batteries and charging facilities.

Capable of resolving 0 ImV d.c., 0 3mV a.c., the multimeter provides an order of magnitude of resolution greater than standard  $3\frac{1}{2}$  digit types. This is achieved by allowing the half digit to have three possible states: off altogether, 1 or 0. The first state is used when reading values such as  $2\cdot31$ ,  $23\cdot1$ , 231 etc., the second when reading  $0\cdot1017$ ,  $1\cdot017$ ,  $10\cdot17$ ,  $10\cdot17$ , etc., and the third when reading  $0\cdot0004$ ,  $0\cdot0114$  etc., the  $\frac{1}{2}$  digit therefore effectively being used as a fourth digit.

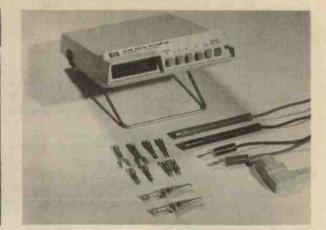
The multimeter can also measure resistance from  $1\Omega$  to  $11M\Omega$  and has a.c. and d.c. current ranges from 0.3mA to 1.1A and 0.1mA to 1.1A respectively. In order to prevent inadvertent switching into the current mode, a separate input socket is provided for current measurement. All the current ranges are fuse protected.

Access to the fuse is via a sliding panel on the side of the multimeter. The test leads are first removed, then, on sliding the panel to the side, both the active fuse and a spare pop out.

The principle of operation of the multimeter is based on the well known dual slope integration technique, all logic functions and analogue switching being contained in an N-MOS i.e. High accuracy and low temperature coefficient are achieved by the use of a thin film Tantalum Nitride resistor pack which is in fact mounted in the same package as the N-MOS chip. This contains most of the precision resistors required in the multimeter.

The 3476A/B in use





There is no "set-zero" control on the front panel as the control logic incorporated in the main i.c. automatically performs this itself, so it is claimed. Zero stability was indeed found to be good on the sample tested.

The autoranging feature is a great asset in a multimeter, the 3476A possesses this and also a facility for range holding to allow rapid readings of similar values to be taken.

Typical accuracy of the device on d.c. voltage is 0.5%; d.c. current 1%; resistance 0.6% (open circuit voltage less than 4 volts). The a.c. voltage and current accuracies were 1.5% and 2% respectively from 45Hz to 2kHz but the frequency response was rather disappointing at  $\pm 8\%$  of reading +1% of range when the bandwidth is increased to 10kHz.

The multimeter lives up to the traditional Hewlett Packard reliability expectations. The sort of tests performed on the meter to check reliability include a 1,000V square wave applied directly to the input terminals to test ability to handle transients; 220V a.c. applied to any terminals with all combinations of push buttons, and also a test involving 10kV being discharged to all exposed metal to simulate static discharges.

The multimeter is obviously aimed at the upper bracket of the amateur market but provides good value for money, the autoranging feature and high resolution giving it distinct advantages over many in this area of the market. R.W.L.

The 3476A and B (the 3476B includes rechargeable batteries) are available from Hewlett-Packard Limited, King Street Lane, Winnersh, Wokingham, Berkshire RG11 5AR.

Internal view showing i.c. containing both control logic and tantalum nitride precision resistor array



Readers requiring a reply to any letter must include a stamped addressed envelope. We regret that we cannot answer any technical gueries on the telephone.

## It's An Advantage

Sir, — Mr Timson has largely missed the point in his letter "A Protest" (Readout, February issue). He will see from my article, "Christmas Lights Flasher" (December '75) in paras. 2 and 3, that the electronic flasher has many advantages over the bi-metal strip. These are much more reliable operation (bi-metal strips tend to stick closed), ability to control a wide range of load wattages at rates set by the user, and very important, it causes absolutely no interference to radio and TV.

All these extra features are typical of the type of improvements that electronics can offer over more traditional processes in so many fields—in much the same way that the typewriter that Mr. Timson used for his letter is an advance over the pen.

What would he say to a criticism of his machine for using so many cranks, levers and springs to replace the usually reliable and inexpensive ball point pen? It's because it's better Mr. Timson, that's what! J. N. Watt, Camberley,

Surrey.

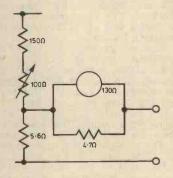
## **Engine Analyser**

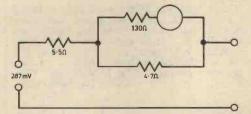
Sir.—1 found Mr Biggs's comments (Readout, February issue) on my article "P.E. Engine Analyser" very interesting. As regards increasing the tachometer range this is quite possible for engines of less than eight cylinders. For instance the timing resistor values given for an eight cylinder engine would, if used on a four cylinder engine, allow the r.p.m. scale to be multiplied by two, giving a maximum of 5,000 r.p.m. Similarly the resistors for engines of less than four cylinders could be halved to bring these into line.

If each cylinder of a multi-cylinder engine has its own separate contact assembly then each cylinder must be treated as a single cylinder engine. Also for two stroke engines the factor of  $\frac{1}{2}$  should be removed from the r.p.m. formulae in the second article and timing resistors will be half those for a four stroke engine to give the same meter calibration.

To reduce the resistance range of the continuity meter, the source impedance of the ohmmeter circuit must be reduced by shunting the meter. A circuit is enclosed which should give a reading of 10 ohms at half scale. This will result in an extra 40mA load on the 10V regulated supply but this should not cause any problems.

D. G. Haley, Hemel Hempstead.





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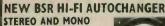
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CD4010AE 0.37 CD4028AE 0.60 TBA851 1.03 CD401AE 0.14 CD4030AE 0.37 TBA800 0.89 CD401AE 0.14 CD4030AE 0.37 TBA810 1.00 CD4014AE 0.70 CD4047AE 0.56 741c(Minidip) 0.18 TRANSISTORS C 2N037AE 0.63 70.46 200 CD4014AE 0.70 CD4047AE 0.56 741c(Minidip) 0.18 CD4014AE 0.70 CD4047AE 0.56 74 0.06 CN4037 0.35 40673 0.46 2N1711 0.18 3N140 0.76 BC108 0.06 2N1711 0.18 3N140 0.76 BC108 0.06 2N1711 0.18 3N141 0.68 BC237 0.05 2N2365 0.10 40360 0.33 BC771 0.18 2N3054 0.30 40406 0.33 BC772 0.09 2N3055 0.35 40407 0.28 BFX30 0.29 2N3055 0.35 40407 0.28 BFX30 0.29 2N3055 0.36 40407 0.28 BFX30 0.29 2N3054 0.30 12 40410 0.43 BFX85 0.26 2N3703 0.12 40410 0.43 BFX85 0.26 2N3703 0.12 40411 1.82 BFY50 0.18 2N3703 0.12 40411 0.43 BFX85 0.22 2N3703 0.12 40410 0.43 BFX85 0.26 2N3703 0.12 40411 0.43 BFX85 0.26 2N3703 0.12 40410 0.44 BFX88 0.22 2N3703 0.12 40410 0.44 BFX88 0.02 2N3704 0.15 405567 0.45 BFX51 0.17 2N3705 0.14 40595 0.69 BFY51 0.17 2N3706 0.14 40595 0.69 BFY51 0.17 2N3706 0.14 40595 0.69 BFY51 0.17 2N3708 0.14 40		0.80	CD4026AE	1.14	TAA621		
CD4012AE         0.14         CD4030AE         0.37         TBA810         1.00           CD4013AE         0.37         CD4037AE         0.63         TBA820         0.60           CD4014AE         0.70         CD4014AE         0.56         T414ctMinidip         0.18           TRANSISTORS         £         C         C         €         C         €         €           2N036         0.15         ZN526         0.35         0.46         20.35         0.47           2N056         0.15         ZN526         0.35         4.067         0.46         0.06           2N1711         0.18         BC105         0.06         20.05         20.05         20.05         20.05           2N2305         0.10         3N126         0.31         BC771         0.18         20.25           2N3053         0.21         40362         0.31         BC771         0.18         21.22           2N3054         0.30         44067         0.21         BFX29         0.26           2N3054         0.30         44067         0.21         BFX84         0.21           2N3054         0.30         44067         0.21         BFX85         0.26 <td></td> <td>0.37</td> <td>CD4027AE</td> <td></td> <td></td> <td></td>		0.37	CD4027AE				
CD4012AE         0.14         CD4030AE         0.37         TBA810         1.00           CD4013AE         0.37         CD4037AE         0.63         TBA820         0.60           CD4014AE         0.70         CD4014AE         0.56         T414ctMinidip         0.18           TRANSISTORS         £         C         C         €         C         €         €           2N036         0.15         ZN526         0.35         0.46         20.35         0.47           2N056         0.15         ZN526         0.35         4.067         0.46         0.06           2N1711         0.18         BC105         0.06         20.05         20.05         20.05         20.05           2N2305         0.10         3N126         0.31         BC771         0.18         20.25           2N3053         0.21         40362         0.31         BC771         0.18         21.22           2N3054         0.30         44067         0.21         BFX29         0.26           2N3054         0.30         44067         0.21         BFX84         0.21           2N3054         0.30         44067         0.21         BFX85         0.26 <td></td> <td>0.37</td> <td>CD4028AE</td> <td>0.60</td> <td>TBA651</td> <td></td>		0.37	CD4028AE	0.60	TBA651		
CD4013AE         0.37         CD4013AE         0.60           CD4013AE         0.56         741c(Minidip)         0.18           TRANSISTORS         £         £         £           2N4036         0.33         4.0673         0.43           2N596         0.10         3N128         0.66         0.91           2N4037         0.35         4.0673         0.46           2N706         0.10         3N128         0.61         BC108         0.06           2N102         0.56         3N141         0.68         BC237         0.05           2N205         0.21         40361         0.31         BCY71         0.09           2N3054         0.30         40406         0.31         BCY71         0.09           2N3054         0.30         40407         0.28         BFX30         0.29           2N3054         0.30         40407         0.28         BFX80         0.21           2N3054         0.30         40407         0.28         BFX80         0.22           2N3054         0.31         40407         0.28         BFX80         0.26           2N3050         0.14         0.59         BFY80         0.				0.75	18A800		
CD4014AE         0.70         CD4014AE         0.56         741c(Minidip)         0.18           TRANSISTORS         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         £         1         £         £         £         £         £         £         5         1         5         £         5         5         1         5         £         1         5         5         1         5         £         5         5         1         5         5         5         5         5         5         5         5         5         5         5         5         5         5<				0.63	TB 4820		
TRANSISTORS         C         E           2N4036         0.43         40673         0.46           2N4037         0.35         40673         0.46           2N706         0.10         3M128         0.61         BC108         0.06           2N102         0.66         3N140         0.76         BC108         0.06           2N102         0.66         3N141         0.68         BC237         0.05           2N205         0.27         40361         0.31         BCY71         0.18           2N3054         0.30         40406         0.31         BCY71         0.09           2N3054         0.30         40406         0.31         BFX29         0.26           2N3054         0.30         40409         0.43         BFX80         0.29           2N3054         0.30         40409         0.43         BFX85         0.26           2N3055         0.35         40407         0.28         BFX80         0.29           2N3054         0.30         40409         0.43         BFX85         0.26           2N3702         0.12         40411         1.82         BFY50         0.18           2N3703							
E 2N4036 0.43 40636 0.41 2N696 0.15 2N5296 0.30 BC107 0.06 2N706 0.10 3N128 0.61 BC108 0.06 2N1711 0.18 3N140 0.76 BC109 0.06 2N2102 0.66 3N141 0.68 BC337 0.05 2N2369 0.10 40360 0.33 BC770 0.09 2N205 0.27 40361 0.31 BC771 0.18 2N3053 0.14 40362 0.33 BC772 0.09 2N3054 0.30 40406 0.31 BC772 0.09 2N3055 0.35 40407 0.28 BFX30 0.29 2N3055 0.35 40407 0.28 BFX30 0.29 2N3054 0.30 40408 0.41 BFX85 0.26 2N3703 0.12 40410 0.43 BFX85 0.26 2N3703 0.12 40410 0.43 BFX85 0.26 2N3703 0.12 40411 1.82 BFY50 0.18 2N3703 0.12 40411 1.82 BFY50 0.18 2N3703 0.12 40411 1.82 BFY50 0.18 2N3703 0.12 40411 0.643 BFX85 0.26 2N3703 0.12 40411 0.643 BFX85 0.26 2N3703 0.12 40410 0.43 BFX85 0.26 2N3703 0.12 40411 0.649 BFY51 0.17 2N3706 0.14 40595 0.69 BFY51 0.17 2N3708 0.14 40595 0.69 BFY52 0.18 0.026 0.35 DIODE 5/ZENERS € € E N4005/6/7 0.04 BZY88 400mW. IN/4001/2/3/4 0.03 IN4148 0.15 AIT voltages 0.06 0.47 0.05 Terms: C.W.0. Add 10p P/P 8% VAT Cos/Mos 225% VAT OTHER Send SAE for comprehensive Cos/Mos List.	the second se	_		_			
€         2N4037         0.35         40673         0.46           2N696         0.10         3N128         0.61         BC107         0.06           2N706         0.10         3N128         0.61         BC108         0.06           2N1711         0.18         3N140         0.76         BC109         0.06           2N2102         0.56         3N141         0.68         BC237         0.05           2N205         0.21         40361         0.31         BCY71         0.09           2N3054         0.30         40406         0.31         BCY72         0.09           2N3054         0.30         40407         0.28         BFX80         0.29           2N3054         0.30         40409         0.43         BFX85         0.26           2N3054         0.30         40409         0.43         BFX85         0.26           2N3050         0.12         40409         0.43         BFX85         0.26           2N3702         0.12         40411         1.82         BFY50         0.18           2N3703         0.12         40411         1.82         BFY50         0.18           2N3706         0.14	INANSISTONA		2N4036		40636		
2N656         0.15         2N526         0.30         BC107         0.06           2N1711         0.16         3N140         0.76         BC108         0.06           2N1711         0.18         0.61         BC337         0.05           2N265         0.27         40360         0.33         BC770         0.09           2N265         0.27         40361         0.31         BC771         0.18           2N3053         0.14         40362         0.33         BC772         0.09           2N3053         0.14         40362         0.33         BC772         0.09           2N3054         0.30         40406         0.31         BFX85         0.26           2N3055         0.35         40407         0.28         BFX84         0.21           2N3055         0.36         40406         0.41         BFX85         0.26           2N3040         0.24         40408         0.41         BFX85         0.26           2N3703         0.12         40411         1.82         BFY85         0.17           2N3706         0.14         40595         0.69         BFY52         0.18           2N3708         0.12		£					
2N1711         0.16         3N140         0.76         BC109         0.06           2N2102         0.66         3N141         0.68         BC237         0.05           2N2369         0.10         40360         0.33         BCY70         0.98           2N3053         0.14         40362         0.33         BCY72         0.09           2N3053         0.14         40362         0.33         BCY72         0.09           2N3054         0.30         40406         0.31         BCY72         0.09           2N3055         0.35         40407         0.28         BFX80         0.21           2N3054         0.32         40408         0.41         BFX84         0.21           2N3442         1.32         40408         0.41         BFX85         0.26           2N3703         0.12         40410         0.43         BFX85         0.22           2N3704         0.16         40534         0.69         BFY52         0.18           2N3706         0.12         40411         1.82         BFY82         0.18           2N3708         0.12         0.05         0.65         0.65         0.65           DIODE 5/ZE	2N696					0.06	
2N2102         0.66         3N141         0.68         BC237         0.05           2N2305         0.10         40360         0.33         BCY70         0.09           2N2905         0.27         40361         0.31         BCY71         0.18           2N3054         0.30         40406         0.33         BCY72         0.09           2N3054         0.30         40406         0.31         BFX29         0.26           2N3054         0.30         40407         0.28         BFX30         0.29           2N3440         0.24         40409         0.43         BFX85         0.26           2N3702         0.12         40411         1.82         BFX50         0.18           2N3703         0.12         40411         1.82         BFY50         0.18           2N3704         0.15         40594         0.59         BFY51         0.17           2N3706         0.14         40595         0.69         BFY51         0.17           2N3706         0.14         40595         0.69         BFY52         0.18           2N3706         0.14         40595         0.69         BFY52         0.18           2N3708 </td <td>2N706</td> <td>0.10</td> <td>3N128</td> <td></td> <td></td> <td>0.06</td>	2N706	0.10	3N128			0.06	
2N2369         0.10         40360         0.33         BCY70         0.09           2N3053         0.14         40362         0.33         BCY72         0.09           2N3053         0.14         40362         0.33         BCY72         0.09           2N3053         0.14         40362         0.33         BCY72         0.09           2N3055         0.36         40407         0.28         BFX30         0.29           2N3055         0.36         40407         0.28         BFX84         0.21           2N3055         0.36         40407         0.28         BFX84         0.21           2N3442         1.32         40409         0.43         BFX85         0.26           2N3702         0.12         40410         0.43         BFX85         0.22           2N3703         0.12         40411         1.82         BFY51         0.17           2N3706         0.14         40595         0.69         BFY52         0.18           2N3708         0.12         0.05         0.65         0.65         0.65           DIODE 5/ZENERS         €         0.16         0.4788<400mW.							
2N2205         0.27         40361         0.31         BCY71         0.18           2N3054         0.30         40406         0.31         BCY72         0.09           2N3054         0.30         40406         0.31         BFX29         0.26           2N3054         0.35         40407         0.28         BFX30         0.29           2N3440         0.24         40408         0.41         BFX84         0.21           2N3440         0.24         40409         0.43         BFX85         0.26           2N3702         0.12         40410         0.43         BFX85         0.26           2N3703         0.12         40411         1.82         BFY50         0.18           2N3704         0.15         40594         0.59         BFY51         0.17           2N3706         0.12         0.14         40595         0.69         BFY52         0.18           2N3705         0.12         0.14         1.82         0.75         0.18           2N3706         0.12         0.14         0.495         0.69         BFY52         0.18           2N3708         0.12         0.14         0.497         0.49         0.492784		0.56	3N141				
2N3053         0.14         40362         0.33         BC772         0.09           2N3055         0.30         40406         0.31         BFX29         0.26           2N3055         0.36         40407         0.28         BFX30         0.29           2N3442         0.24         40408         0.41         BFX85         0.21           2N3442         1.32         40409         0.43         BFX85         0.22           2N3702         0.12         40410         0.43         BFX85         0.22           2N3703         0.12         40411         1.82         BFY50         0.17           2N3706         0.16         40595         0.69         BFY52         0.18           2N3708         0.12         0.69         BFY52         0.18           0.025         0.25         0.25         0.35         0.65           DIODE 5/ZENERS         E         IN4005/6/7         0.4         BZY88 400m K.           IN/4001/2/3/4         0.31         IN4148         0.14         AUT Cos/Mos           Zex         X/41         0.14         PP P%/2 XT Cos/Mos         25%/2 XT Cot/Mos           205%         VAT OTHER         Send SAE for comprehe							
2N3054         0.30         04006         0.31         BFX29         0.26           2N3055         0.35         40407         0.28         BFX30         0.29           2N3440         0.24         40408         0.41         BFX84         0.21           2N3702         0.12         40409         0.43         BFX85         0.26           2N3702         0.12         40410         0.43         BFX85         0.26           2N3703         0.12         40411         1.82         BFY50         0.18           2N3704         0.15         40594         0.59         BFY51         0.17           2N3706         0.14         40595         0.69         BFY51         0.17           2N3706         0.12         005/6/7         0.04         BZY88 400mW.         0.05           DIODES/ZENERS         €         0.05         0.44         0.05/6/7         0.04         BZY88 400mW.         0.06           IN/4001/2/3/4         0.03         IN4148         0.16         All voirages         0.06         0.47         0.05           Terms: C.W.0. Add 10p P/P 8% VAT OtHER         Send SAE for comprehensive Cos/Mos List.		0.27	40361				
2N3055         0.36         40407         0.28         BFX80         0.29           2N3440         0.24         40408         0.41         BFX84         0.21           2N3442         1.32         40409         0.43         BFX85         0.26           2N3703         0.12         40411         0.43         BFX85         0.22           2N3703         0.12         40411         1.82         BFY50         0.17           2N3706         0.16         40595         0.69         BFY52         0.18           2N3708         0.12         005/6/7         0.03         0.035         0.059           DIODE S/ZENERS         E         1N4005/6/7         0.41         BIX988 400m K.         0.65           VI/4001/2/3/4         0.03         IN4148         0.15         All votingers         0.06           Terms: C.W.O. Add 10p P/P 8% VAT OS/Mos         22% VAT OTHER         Send SAE for comprehensive Cos/Mos List.         Send SAE for comprehensive Cos/Mos List.							
2N3440         0.24         40406         0.41         8FX84         0.21           2N342         1.32         40409         0.43         8FX85         0.26           2N3702         0.12         40410         0.43         8FX85         0.22           2N3703         0.12         40411         1.82         8FY50         0.18           2N3704         0.15         40594         0.59         8FY51         0.17           2N3706         0.14         40595         0.69         8FY52         0.18           2N3706         0.12         0055         0.69         8FY52         0.18           2N3706         0.12         00556/7         0.04         8ZY88 400mW.         0.05           DIODES/ZENERS         €         0.16         0.41         0.42         0.41         0.69           IN/4001/2/3/4         0.03         IN4148         0.41         0.42         0.05         0.47         0.05           Terms: C.W.O. Add 10p P/P 8%         VAT Cos/Mos List.         25% VAT OT HER         25% VAT Ot Mos List.         25% VAT Ot Mos List.							
2N3442         1.32         40409         0.43         BFX85         0.26           2N3702         0.12         40410         0.43         BFX85         0.22           2N3703         0.12         40411         1.82         BFY50         0.18           2N3704         0.16         40594         0.59         BFY51         0.17           2N3706         0.14         40595         0.69         BFY52         0.18           2N3708         0.12         0.69         BFY52         0.18           DIODE \$/ZENERS         E         0.04         BZY88 400mW.         0.65           IN/4001/2/3/4         0.03         IN4148         0.15         All votingers         0.06           Terms: C.W.O. Add 10p P/P 8% VAT Cot Cos/Mos 22% VAT OTHER         Send SAE for comprehensive Cos/Mos List.         285/0000 List.							
2N3702         0.12         40410         0.43         BFX88         0.22           2N3703         0.12         40411         1.82         BFY50         0.18           2N3704         0.15         40594         0.59         BFY51         0.17           2N3706         0.14         40595         0.69         BFY52         0.18           2N3708         0.12         00596         CF         0035         0.35           DIODES/ZENERS         €         E         IN4005/6/7         0.04         BZY88 400mW.           IN/4001/2/3/4         0.03         IN4148         0.014         All voiringes         0.06           DAT         Terms: C.W.O. Add 10p P/P 8% VAT Cos/Mos         25% VAT OTHER         Send SAE for comprehensive Cos/Mos List.							
2N3703         0.12         40411         1.82         BFY50         0.18           2N3704         0.16         40594         0.58         BFY51         0.17           2N3706         0.14         40595         0.69         BFY52         0.18           2N3706         0.12         0.69         BFY52         0.18           DIODES/ZENERS         E         IN4005/6/7         0.04         BZY88         400mW.           IN/4001/2/3/4         0.03         IN4148         0.15         All voitages         0.06           Terms:         C.W.O. Add 10p P/P 8% /VAT Os/Mos         25% vAT OTHER         Send SAE for comprehensive Cos/Mos List.							
2N3704         0.15         40594         0.59         BFY51         0.17           2N3706         0.14         40595         0.69         BFY52         0.18           2N3708         0.12         0C35         0.35         0C35         0.35           DIODES/ZENERS         E         IN4005/6/7         0.04         BZY88         400mW.           IN/4001/2/3/4         0.31         IN4148         0.15         All voirages         0.06           OA7         0.05         CAT Cos/Mos         25% VAT OTHER         Send SAE for comprehensive Cos/Mos List.         5						0.18	
2N3708         0.12         0C35         0.35           DIODE \$/ZENERS         E         IN4005/6/7         0.04         EZY88         400mW.           IN/4001/2/3/4         0.03         IN4148         0.15         All volteges         0.06           Terms:         C.W.O, Add 10p         P/P         8%         VAT         CoS/Mos           25%         VAT         OTHER         Send SAE for comprehensive         Cos/Mos         List.	2N3704						
DIODES/ZENERS         E         0.04         BZY88         400mW.         E           IN/4001/2/3/4         0.03         IN4148         0.15         All voltages         0.06         0.47         0.05           Terms:         C.W.O. Add 10p P/P 8% VAT Os/Mos         25% VAT OTHER         Send SAE for comprehensive Cos/Mos List.			40595	0.69			
IN/4001/2/3/4         0.03         IN4005/6/7         0.04 (BZY88 400mW.           IN/4001/2/3/4         0.03         IN4018         0.15         All voirtiges         0.06           Terms:         C.W.0. Add 10p P/P 8% VAT Cos/Mos 25% VAT OTHER         Send SAE for comprehensive Cos/Mos List.         Send SAE for comprehensive Cos/Mos List.	2N3708	0.12			0C35	0.35	
IN/4001/2/3/4 0.03 IN4148 0.15 All voltages 0.06 OA47 0.05 Terms: C.W.O. Add 10p P/P 8% VAT Cos/Mos 25% VAT OTHER Send SAE for comprehensive Cos/Mos List.	DIODES/ZENE	RS		£	1 m	1	
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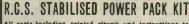
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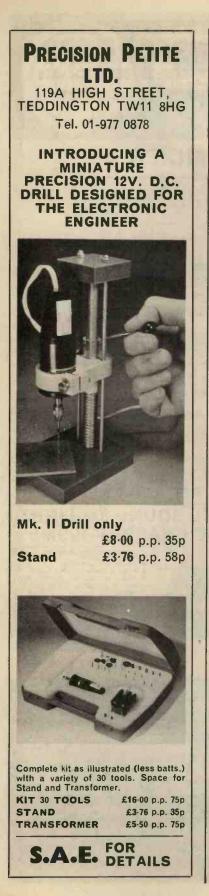
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50V	2A	35p				
100V	2A 1A	400	0010.0	POW	ER UNIT	
200V	4A	45p 65p	3-4-5-6-	7-5-9-12V a	witched it 500mA, £4	.08. P&I
400V	0.4	50p	48p. VA	T 25%		
600V	2A 10A(PM 7A6) 51					_
600V 500V		2.33			ITY MODU	LES
600V 500V P & P 1 TEST	10A(PM 7A6) E		3 W R	IGH QUAL	lity MODU	LES E2-34 E2-6
600V 500V P & P 1 TEST AVO 6 MK5	10A(PM 7A6) E1 15p. 25% VAT METERS	55-88	3 W R 5W R	IGH QUAL MS Amplifi MS Amplifi	er	£2.6
600V 500V P & P 1 TEST AVO 8 MK5 AVO 72 U4313*	10A(PM 7A6) E 15p. 25% VAT METERS	55-88 21-72 13-85	H 3 W R 5W RH 10W RH 25W RH Pre-Am	IGH QUAL MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi	er er 10W	£2-6 £2-9 £3-9
600V 500V P & P 1 TEST AVO 6 MK5 AVO 72 U4313* U4315*	10A(PM 7A6) E1 15p. 25% VAT METERS E1 E1 E1	55-88 21-72 13-85	H 3 W R 5W RH 10W RH 25W RH Pre-Am	IGH QUAL MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi	er er 10W	£2-6 £2-9 £3-9 £4-0 £13-2
600V 500V P & P 1 TEST AVO 6 MK5 AVO 72 U4313* U4315* (U\$SB) inc. 1	10A(PM 7A6) EI ISp. 25% VAT METERS EI Steel carrying	55-88 21-72 13-85	H 3 W R 5W RM 10W RM 25W RM Pre-Am Pre-Am Pre-Am	IGH QUAL MS Amplifi MS Amplifi MS Amplifi MS Amplifi Ip for 3-5- ip for 25W Supplies 3	er er er 10W	£2-6 £2-9 £3-9 £4-0 £13-2 88
600V 500V P & P 1 TEST AVO 8 MK5 AVO 72 U4313* '(USSR) inc. 1 P. & P. E ANTEX SOL	10A(PM 7A6) E3 15p. 25% VAT METERS E1 Steel carrying 1+10. VAT 8% DEFING IRONS	55-88 21-72 13-85 11-80 case	H 3 W R 5W R 10W R 25W R Pre-Am Pre-Am Power Power Transfo	IGH QUAL MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi Supplies 3 Supplies 3 Supplies 3	er er 10W ⊢5–10W 5W	£2-6 £2-9 £3-9 £4-0 £13-2 88 £3-0
600V 500V P & P 1 TEST AVO 8 MK5 AVO 72 U4313* '(USSR) inc. 1 P. & P. E ANTEX SOL 15W 62-68, 16W	10A(PM 7A6) E2 15p. 25% VAT METERS E2 steel carrying 1-10. VAT 8% DERING IRONS ( £2-45, 25W E	55-88 21-72 13-85 11-80 Case 3 2-26	H 3 W R 5W R 10W R 25W R Pre-Am Pre-Am Power Power Transfo Transfo	IGH QUAL MS Amplifi MS	er er 10W H5-10W 5W	E2-6 E2-9 E3-9 E4-0 E13-2 E13-2 E13-2 E13-2 E13-0 E1-44 E2-1
600V 500V P & P 1 TEST AVO 8 MK5 AVO 7 U4313* U4315* *(USSR) Inc. 1 P. A.P. E ANTEX SOL 15W 62-66, 18W Soldering	104/PM 746) E2 ISp. 25% VAT METERS E2 Steel carrying 1-10. VAT 8% DERING IRONS / E2-45, 25% E (For Kit E3-61,	55-88 21-72 13-85 11-80 case 3 2-26,	H 3 W R 5W R 10W R 25W R Pre-Am Pre-Am Power Transfo Transfo Transfo	IGH QUAL MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifies 3 Supplies 3 Supplies 2 Supplies 25 Drimer 25W	er er 10W H-5-10W 5W	E2+6 E2+9 E3+9 E4+0 E13+2 84 E3+0 E1+4 E3+0 E1+4 E2+6
600V 500V 765 P1 TEST AVO 6 MK5 AVO 72 U4315* *(USSR) Inc. 1 *(USSR) Inc. 1 F. 4 P. 2 ANTEX SOL 15W 52:68, 18W Soldering Stade for	10A(PM 7A6) E2 15p. 25% VAT METERS E2 steel carrying 1-10. VAT 8% DERING IRONS ( £2-45, 25W E	55-88 21-72 13-85 11-80 case 3 2-26,	H 3 W R 5W R 10W R 25W R Pre-Am Pre-Am Power Transfo Transfo Transfo	IGH QUAL MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifies 3 Supplies 3 Supplies 2 Supplies 25 Drimer 25W	er er 10W H-5-10W 5W	E2+6 E2+9 E3+9 E4+0 E13+2 84 E3+0 E1+4 E3+0 E1+4 E2+6
600V 500V 765 P 1 TEST AVO 6 MK5 AVO 72 U4315* *(USSR) Inc. 1 P. 4 P. E ANTEX SOL 15W 62:68, 18W Soldering Stand for P. 8 P.1	104/PM 746) E1 15p. 25% VAT METERS 15 15 15 15 15 15 15 15 15 15	55-88 21-72 13-85 11-80 case 3 2-26,	H 3 W R 5W R 10W R 25W R Pre-Am Pre-Am Power Transfo Transfo Transfo	IGH QUAL MS Amplift MS Amplift MS Amplift AS Amplift AS Amplift AS Amplift p for 25W Supplies 2 Supplies 2 Supplies 2 Supplies 2 Ormer 3W Ormer 5-10 Ormer 25W C. Amps/Pi Bp Transform	er er 10W ⊢5–10W 5W W re-Amps/Po ners 37p. VA	E2+6 E2+9 E3+9 E4+0 E13+2 84 E3+0 E1+4 E3+0 E1+4 E2+6
600V 500V 500V 765T AVO 8 MK5 AVO 72 U4313* '(USSR) Inc. 1 '(USSR) Inc. 1 '(USSR) Inc. 1 ANTEX SOL 15W C256, 18W Soldering Stand for P. & P. E MAGNETIC CARTRIDGE	104(PM 746) ±2 5p. 25% VAT METERS 15 15 10, VAT 8% 10, VAT 8% DERING IRONS 10, VAT 8% 10, VAT	55-88 21-72 13-85 11-80 Case S 2-26,	H 3 W R 5W R 10W R 25W R Pre-Am Pre-Am Power Transfc Transfc Transfc Piles 18 P, & P,	IGH QUAL MS Amplift MS Amplift MS Amplift MS Amplift MS Amplift P for 3-5- p for 25W Supplies 3 Supplies 3 Supplies 3 Supplies 2 Supplies 2 Supplies 2 Supplies 2 Transform Transform	er er 10W -5-10W 5W W re-Amps/Po hers 37p. V/ TROSIL	£2-6 £2-9 £3-9 £4-0 £13-2 £3-0 £1-4 £2-1 £2-16 wer Sup
600V 500V 500V 765T AVO 8 MK5 AVO 72 U4313* '(USSR) Inc. 1 '(USSR) Inc. 1 '(USSR) Inc. 1 ANTEX SOL 15W C256, 18W Soldering Stand for P. & P. E MAGNETIC CARTRIDGE	104(PM 746) ±2 5p. 25% VAT METERS 15 15 10, VAT 8% 10, VAT 8% DERING IRONS 10, VAT 8% 10, VAT	55-88 21-72 13-85 11-80 Case S 2-26,	H 3 W R 5W R 10W R 25W R Pre-Am Pre-Am Pre-Am Power Transfc Transfc Transfc P. & P. M	IGH QUAL MS Amplift MS Amplift MS Amplift MS Amplift MS Amplift MS Amplift MS Amplift MS Amplift Supplies 2 Drmer 25W Drmer 5-10 Drmer 25W Drmer 25W Drmer 5-10 Drmer 25W Drmer 5-10 Drmer 25W Drmer 25W Drmer 5-10 Drmer 25W Drmer 5-10 Drmer 25W Drmer 5-10 Drmer 25W Drmer 5-10 Drmer 25W Drmer 5-10 Drmer 25W Drmer 5-10 Drmer 25W Drmer 5-10 Drmer 5-10 Drm	er er er 10W 55W W re-Ampa/Po hers 37p. V/ CTAOSIL DE RESISTO E RESISTO	E2-6 E2-9 E3-9 E4-0 E13-2 E13-2 E13-2 E13-2 E1-4 E2-6 E1-9 E1-9 E1-9 E1-4 E2-6 E1-9 E1-4 E2-6 E1-4 E1-4 E2-9 E1-4 E1-4 E2-9 E1-9 E1-9 E1-9 E1-9 E1-9 E1-9 E1-9 E1
600V 500V 500V 765T AVO 6 MK5 AVO 72 U4313- 'USSR) Inc. 1 'S A P. E ANTEX SOL 15W 12:66, 18W Soldering Stand for P. & P.2 MAGNETIC CARTRIDGE Operating D Only E2:65 P. d	10A(PM 746) E2 550, 25% VAT METERS istoel carrying 1-10, VAT 8% DERING IRONS V E2-45, 25% E from Kit 3-61, above f1-13. 550, VAT 8% TO CERAMIC COLVERTOR P. 18p. VAT 25%	55-88 21-72 13-85 11-80 Case 3 2-26,	H 3 W R 5W R 10W R 25W R Pre-Am Pre-Am Power Power Transfc Transfc Transfc Piles 16 P. & P. M Style T	IGH QUAL MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi Supplies 2 Drimer 3W Drimer 5-10 Drimer 25W Amplifi Transform ELECI ETAL OXIL	er er 10W 5W W re-Amps/Po hers 37p. V/ DE RESISTC ; Range Pric	62-6 62-9 63-9 63-9 64-0 613-2 63-0 61-4 62-1 62-1 62-6 wer Sup AT 25%
600V 500V 500V 765T AVO 6 MK5 AVO 72 U4313- U4313- '(US\$R) Inc. 1 '(US\$R) Inc. 1 '(	10A(PM 746) E2 50, 25% VAT METERS itoel carrying 1-10, VAT 8% DERING IRONS V E2-45, 25% E tron Kit 3-81, above E1-13. 50, VAT 8% TO CERAMIC E CONVERTOR P. 18p. VAT 25% INN-DECK 54anger 55%	55-88 21-72 13-85 11-80 Case 3 22-26,	H 3 W R 5W RH 10W RH 25W RH Pre-Am Pre-Am Power Power Transfc Transfc P. & F plies 16 P. & P. M Style T TR4 25 50 50 50 50 50 50 50 50 50 5	GH QUAL MS Amplifi MS	er er 10W 55W W re-Amps/Po hers 37p. V/ TROSIL DE RESISTO ; Range Prid 300k A 300k	E2-6 E2-9 E3-9 E3-9 E3-9 E3-0 E1-4 E2-1 E2-7 E3-0 E1-4 E2-1 E2-7 E3-0 E1-4 E2-7 E3-0 E1-4 E2-7 E3-0 E10-55 E8-00
600V 500V 500V 765T AVO 6 MK5 AVO 72 U4313- U4313- '(US\$R) Inc. 1 '(US\$R) Inc. 1 '(	10A(PM 7A6) E2 5p. 25% VAT METERS 22 22 23 24 25 25 25 25 25 25 25 25 25 25	55-38 21-72 13-85 11-80 Case 3 22-26, %	H 3 W R 5W RI 10W RI 25W RI Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-A	IGH QUAL MS Amplift MS Amplift Supplies 3 Supplies 3 Supplies 2 Immer 5-10 Immer 5-10 Immer 25W Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform Transform T	er er 10W 55W w re-Amps/Po hers 37p. V/ 57AOSIL DE RESISTC : Range Prid 300kΩ 300kΩ	22-6 22-9 23-9 24-0 21-2 8 4 23-1 22-6 4 22-1 22-6 4 22-1 22-6 4 22-1 22-6 4 22-5 26 20-6 21-4 22-6 22-6 21-4 22-6 21-4 22-6 21-4 22-6 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9
600V 500V 500V P & P 1 TEST AVO 8 MK5 AVO 72 U4313- U4313- U4313- U4313- (USSR) Inc. 1 P. 4 P. E ANTEX SOL 15W E2-65, 18W Soldering Stand 10 P. 4 P. E MAGNETIC CARTIDOE Operating 1 only E2-65 P. 4 Operating 1 Only E2-65 P. 4 Stand 2 Operating 1 Only E2-65 P. 4 Stand 10 P. 4 P. E NEW 5 NEW 5	10A(PM 746) E2 50, 25% VAT METERS E2 steel carrying 1-10, VAT 8% DENING IRONS / 12-45, 25W E3 DENING IRONS / 12-45, 25W E3 TO CERAMIC CONVERTOR 10110262 001102 80-45V P. 180, VAT 25% Changer £5-0 20, VAT 25%	55-88 21-72 13-85 11-80 Case 8 :2-26, %	H 3 W R 5W RH 10W RH 25W RH 25W RH Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Power Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transfc Transf	GH QUAL MS Amplifu MS	er er 10W 55W W re-Amps/Po hers 37p. V/ TROSIL DE RESISTC : Range Pris 300k 470k -1M Ω	22-6 22-9 23-9 23-9 24-0 213-2 28 23-0 21-44 22-1 22-6 wer Sup 21-44 22-1 22-6 wer Sup 21-44 22-1 22-6 0 NS Celper 10 21-55 22-60 22-55 22-60
600V 500V 500V 765T AVO 8 MK5 AVO 72 U4313* U4315* *(US\$R) inc. 1 *(US\$R) inc. 1 *(U	10A(PM 7A6) E2 50, 25% VAT METERS 100 Carrying 110, VAT 8% DENING IRONS 110, VAT 8% DENING IRONS 100 CETA1, 100 CERAMIC CONVERTOR VOItage 20-45% ININ-DECK Changer 25% 20, VAT 25% DENING 25% 20, VAT 25%	55-88 21-72 13-85 11-80 Case 8 2-26, %	H 3 W R 5W RI 10W RI 25W RI 10W RI Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Power Transfc Transfc Transfc P. & P. B P. & P. Style T TRA 2 2 TR5 2 2 TR6 2 2 TR6 2 2	IGH QUAL MS Amplift MS Amplift Supplies 2 Supplies 3 Supplies 3 Supplies 3 Supplies 3 Supplies 3 Supplies 3 Su	er er 500 500 500 500 500 500 500 500 500 50	22-6 22-9 23-9 24-0 23-9 24-0 23-9 24-0 23-9 23-9 23-9 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0 23-0
600V 500V 500V 765T AVO 8 MK5 AVO 72 U4313* U4315* *(US\$R) inc. 1 *(US\$R) inc. 1 *(U	10A(PM 7A6) E2 50, 25% VAT METERS 100 Carrying 110, VAT 8% DENING IRONS 110, VAT 8% DENING IRONS 100 CETA1, 100 CERAMIC CONVERTOR VOItage 20-45% ININ-DECK Changer 25% 20, VAT 25% DENING 25% 20, VAT 25%	55-88 21-72 13-85 11-80 Case 8 2-26, %	H 3 W R 5W RI 10W RM 25W RI 10W RM Pre-Am Power Pre-Am Power Pre-Am Power Transfc Transfc Transfc P. & P. Style T TR4 2 2 TR5 2 2 2 2 2 2 2 2 2 2 2 2 2 2	GH QUAL MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi MS Amplifi Supplies 2 Supplies 2 Supplies 2 Supplies 2 Supplies 2 Supplies 2 Supplies 2 Supplies 2 Difference 2 Comparison MS 100- % 100- % 100- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500- % 500-	er er er 500 500 750 750 750 750 750 750 750 750	22-6 22-9 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 24-0 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9 21-9
600V 500V 500V 7 TEST AVO 8 MK5 AVO 72 U4313- U4313- U4313- 15W 12-65, 18W Soldering Stand 107 P. 4 P. 2 MAGNETIC CARTRIDGE Operating only 12-65 P. d BSR M 4 Speed Auto P. 4 P. 7 NEW S COMPLETE STE 7 + 7W RMS AM supply, front p mains frand. St	10A(PM 746) E2 50, 25% VAT METERS E2 steel carrying 1-10, VAT 8% DENING IRONS / 12-45, 25W E DENING IRONS / 12-45, 25W E 50, VAT 8% TO CERAMIC CONVERTOR 101-126 CONVERTOR 0-15% VAT 25% Changer E9-0 20, VAT 25% Changer E9-0 20, VAT 25% Changer C9-0 20, VAT 25% CHASSIS 37ERE0 30 IREO CHASSIS 37ERE0 30 15-75, Nob8	55-88 21-72 13-85 11-80 Case 3 	H 3 W R 5 W RH 10 W RH 25 W RH 10 W RH 25 W RH Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am Pre-Am	GH QUAL           MS Amplifi           Supplies 3           Supplies 2           Immer 5-10           Transform           ELEC           ELA CXII           Other           MS 100-           % 510kri           % 100-           % 500kri           % 100-           % 500kri           % 100-	er er 500 500 500 500 500 500 500 500 500 50	22-6 22-9 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 23-9 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0 24-0
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600V 500V 500V TEST AVO 8 MK5 AVO 72 U4313* 'USSR) inc. 1 'YUSSR) inc. 1 'YUSSR) inc. 1 'YUSSR) inc. 1 'YUSSR) inc. 1 'YUSSR) inc. 1 'YESSR' ANTEX SOL ANTEX SOL Soldering Stand for P. & P. 2 MAGNETIC CARTRIDGE Operating Only E2-65 P. 4 BSR M 4 Speed Auto P. 4 P. 7 COMPLETE STE 7 + 7W RMS AM Supply, front p mains trans.) Stu trans. (2:45, P. 4 Supply, front p	10A(PM 7A6) ES 150, 25% VAT METERS 100 110, VAT 8% DE RING IRONS DE RING IRONS 1 50, 25% VE 110, VAT 8% DE RING IRONS 100, 25% VAT 25% 101, 200 101, 200 100, 200 101, 200 100, 200 100, 200 100, 200	55-88 21-72 13-85 11-80 Case 5 52-26, 22-26, 22-26, 20 NC: 100Wer teeds Value Cab.	H 3 W R 5W R 10W R 25W R Pre-Am Pre-Am Power Power Power Power Power Power Power Transfc Fransfc Transfc P, & P, M TR4 2 Style T TR5 2 2 2 2 2 2 2 2 2 2 2 2 2 2	IGH QUAL           MS Amplift           Supplies 3           Supplies 3           Supplies 3           Supplies 3           Supplies 3           Supplies 3           Supplies 2           MS Amplift           MS A	er er er 500 500 600 500 600 500 600 500 600 600	22-6 22-9 13-9 24-0 213-21 84 23-0 213-21 84 23-0 213-21 84 23-0 213-21 84 23-0 213-21 84 23-0 213-21 84 23-0 213-21 84 23-0 213-21 84 23-0 213-21 84 23-0 213-21 84 23-0 21-44 22-6 84 23-0 21-44 22-6 84 23-0 21-44 22-6 84 23-0 21-44 22-6 84 23-0 21-44 22-6 84 23-0 21-44 22-6 84 23-0 21-44 22-6 84 23-0 21-44 22-6 84 23-0 21-44 22-6 84 23-0 21-44 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 84 22-6 85 21-0 55 20-55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 55 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0 21-0
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600V 500V 500V TEST AVO 8 MK5 AVO 72 U4313- U4313- "(USSR) Inc. 1 FAP.E ANTEX SOL 15W C256, 18W Soldering Stand for P. & P. 7 MAGNETIC CARTRIDGE Operating v only E2-65 P. A Speed Auto P. & P. 7 NEW S COMPLETE STE BSR M 4 Speed Auto P. & P. 7 NEW S COMPLETE STE Trans. 12:45, T NEW S COMPLETE STE Audio Accor Callers w BARTP 3,THE I	10A(PM 746) E2 50, 25% VAT METERS 10 10 10 10 10 10 10 10 10 10	55.86 21-72 11-80 case 3 22-28, 3 22-28, 1NC: case 3 22-28, 1NC: case case 22-28, 1NC: case case 22-28, 1NC: case 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28, 22-28,	3 W R 3 W R 3 W R 3 W R 10W R Pre-Am Pre-Am Power Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot Transtot	IGH QUAL MS Amplifued Ampl	er er er 500 500 w w w w w w w w w w w w ore-Ampu/Poo here 37p. 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NEAREST TUBE STATIONS: ALDGATE & LIVERPOOL ST.

Practical Electronics March 1976



### P.E. SYNTHESISER

(P.E. Feb. 1973 to Feb. 1974) The well acclaimed and highly versatile large-scale mains-operated Sound Synthesiser complete with keyboard circuits. All function circuits may be used independently, or interconnected. The greater the number of circuits, the greater the versatility. Other circuits in our lists may be used with the Synthesiser to good advantage.

### THE MAIN SYNTHESISER

Stabilised Power Supply	£12-05
<b>Two Linear Voltage Controlled Oscillat</b>	
and one inverter-all 3 circuits:	£16-38
PCB (2 are required)-each	£1.48
Two Paren Canada Anna I T	F 1.40
Two Ramp Generators and Two Input	15 13
Amplifiers-all 4 circuits	£5-62
PCB (holds all 4 circuits)	£1-38
Sample-Hold and Noise Generator-	£6-64
PCB (holds both circuits)	£1.70
Tone Control, £2.43; PCB. 80p	
Reverberation Amplifier	£6-36
Sprine Line unit for Reverb Amp	£4.95
Ring Modulator	£3.75
Peak Level Meter Circuit	£1-50
100µA Panel Meter	£3.75
PCB for Rev., R-Mod. & Meter Ccts.,	£1.94
Envelope Shaper, £5-35; PCB, £1-46	A1.24
Voltage Controlled Amp. and Diff. Amp.	£6-86
PCB (holds both circuits)	£1-32
THE SYNTHESISER KEYBOARD CIR	
Can be used without the Main Synthesiser t	o make
an Independent musical instrument)	
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### **KEYBOARDS**

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, .		3 Octave	4 Octave	5 Octave
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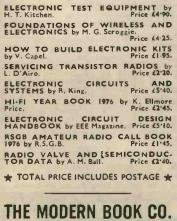
FOR ADDRESS, INFORMATION REGARDING POST AND PACKING, VAT, LISTS, AND EXPORT TERMS SEE OUR OTHER ADVERT-ISEMENT ON OPPOSITE PAGE Photos: 2 of our units containing some of the P.E. projects built from our kits and PCBs. (The cases were built by ourselves and are not for sale.)

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Danet Clip Tp         G/Y         27p         33p         Emvirt 1: 55           Clip Tp         OR         27p         33p         ORP12 35p           DPTO-ISOLATORS         SCR:a         SSR:a         SSP         100 v 400v           124         1:5kV, 150h/z         11         TOBS 1A         27p         35p         SOP 100 v 400v           1350         2:5kV, 5MHz         121         TOBS 1A         27p         35p         Sop           AC125/67.8         15p         2N2928(G)         12p         N3053         15p         SV 7805 Plastic         12v           AC125/67.8         15p         2N3054         45p         15V 7815 Plastic         all         18V 7818 E1-50           BC107.8/9         9p         2N3054         45p         15V 7815 all         50V 300 Plastic           BC178/69         11p         2N2845         35p         SOV<300 Plastic	I CO	S	0.12	5	0.2		
Danet Clip Tp         G/Y         27p         33p         Emvirt 1: 55           Clip Tp         OR         27p         33p         ORP12 35p           DPTO-ISOLATORS         SCR:a         SSR:a         SSP         100 v 400v           124         1:5kV, 150h/z         11         TOBS 1A         27p         35p         SOP 100 v 400v           1350         2:5kV, 5MHz         121         TOBS 1A         27p         35p         Sop           AC125/67.8         15p         2N2928(G)         12p         N3053         15p         SV 7805 Plastic         12v           AC125/67.8         15p         2N3054         45p         15V 7815 Plastic         all         18V 7818 E1-50           BC107.8/9         9p         2N3054         45p         15V 7815 all         50V 300 Plastic           BC178/69         11p         2N2845         35p         SOV<300 Plastic		RED	15p		19p		
paneli         OR         27p         33p         GmW 11:55           OPTO-ISOLATORS         CRF12:58p         OPTO-ISOLATORS         CRF12:58p           1230         25KV. 50KHz         CI         TOS IA. 25p         27p         45p           1230         25KV. 50KHz         CI         TOS IA. 25p         28p         50p           Data         tree         with         eff         OPTO-ISOLATORS         1000         400V           C1236:67.8         55p         28262(5)         12p         3400V         60p           AC1236:67.8         15p         28262(5)         12p         45p         5V 7805 Plastic           AC1236:67.7         34p         283034:561         5b         7805 Plastic         12V 7812         14mp           AC103C         12p         283034:561         15p         2730 DIP14         50p         723 DIP14         50p           BC14776(9         11p         283819         25p         2A100V         36p         723 DIP14         50p         2A100V         36p           BC14776(9         11p         2N3819         25p         2A100V         36p         2A100V         36p           BC14776(9         17p         11hM002		G/Y	270		33		1-5mW E1-10
OPTO-ISOLATORS         SCR's         SOV         100V 400V           LIZ4         1-SkV, 150k/tz         1         705 1A         25p         27p         46p           1230         2-SkV, SMHz         1         705 1A         25p         27p         45p           Data         free         with         atl         0PTO         7065 3A         27p         35p         50p           Data         free         with         atl         0PTO         7065 3A         27p         35p         50p           Act25/6/7.6         15p         2N2528(G)         12p         VOLTACEREGS         5V 7805 Plastic         12V 7812 1 Amp           AC107.8/9         9p         2N3702.3/4         12p         730 Plastic         50V         30p         32p         31p         15V 7815 ell         18V 7818 cl-50         30p         323 DiPlatic         50P         30p         323 DiPlatic         50V 300 3p         223 DiPlatic         30V         30p         323 DiPlatic         30V         30p         323 DiPlatic         30V         30p         323 DiPlatic         30V         30p         324 30V </td <td></td> <td></td> <td>-</td> <td>-</td> <td>-</td> <td>-</td> <td></td>			-	-	-	-	
1.74         1-5kV, 150kHz         11         705 1A         25 p         706 5A         25 p         706 5A         27 p         35 p         50 p           Data         ires         with         all         0PTO         TRIAC         TOS 5A         27 p         35 p         50 p           AC125/67.8         15p         2N2928(G)         12p         TOR 5A         70 p         35 v         700 p         72 p         72 p         710 p         700 p         72 p         72 p         710 p         70 p         72 p         710 p         72 p <td>Clip 1p</td> <td>OR</td> <td>2/p</td> <td></td> <td>335</td> <td>2</td> <td>ORP12 55p</td>	Clip 1p	OR	2/p		335	2	ORP12 55p
Image: system of the							
Data         free         with         att         OPTO         TRIAC         TOS         2A         400V         600           AC125/67/8         15p         2N2262(G)         12p         VOLTAGEREGS           AD161/162         40p         2N3053         15p         12p							
AC125/6/7.36         TSP         2N2826(G)         12p         VOLTACE REGS           AC125/6/7.36         TSP         2N3053         TSP         SV 7805 Plastic           AD161/162         40p         2N3053         TSP         SV 7805 Plastic           AF127         20p         2N3053         TSP         SV 7805 Plastic           AF124.567         34p         2N3053         TSP         SV 7815         all           AF124.567         34p         2N3053         TSP         TSV 7815         all           BC107(8)         10p         2N3903.4/561         TSP         TSV 7815         all           BC157/8/9         11p         ZN3903.4/561         TSP         TSV 7815         all           BC157/8/9         11p         ZN3903.4/561         TSP         ZA 50V         30p           BC157/8/9         11p         ZN3803         S0p         ZA 100V         30p           BC167/8/9         11p         ZN3823         30p         ZA 100V         30p           BC126/2/4/12p         IN4001         5p         ZA 50V         4p           BC198/7         12p         IN4001         5p         NE555         G1+00           BF198/7 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>							
AD161/162 40p 2N3053 15p 5V 7805 Plastic AF117 20p 2N3054 45p 12V 7812 1 Amp 15V 7815 1 Amp 15V						-	
AF117         200         2N3054         459         12V 7812         1Am           AF124/5.67         34p         2N3055         41p         18V 7815         all           BC107/8.9         9p         2N3702/34         12p         18V 7815         all           BC107/8.9         12p         2N302/34         12p         18V 7815         all           BC178/69         10p         2N2646         35p         1723         DIP14         50p           BC167/8/9         11p         MPF102         40p         2A 50V         32p         2A 100V         34p           BC168/7         11p         MPF102         40p         2A 20V         44p         2A 20V         44p           BC18/27/18/9         17p         BR100 Diac         21p         2A 20V         44p           BC18/27/18/9         11p         MPA023         6p         2 7-33V         8p           BC19/27/17/2         12p         IN40023         6p         2 7-33V         8p           BC19/27         12p         IN40025         7p         NE5556         61-0           BF198/5         12p         IN40025         7p         NE556         61-0           BF198/2				G)			
AF124.567         34p         2N3055         41p           BC107.89         9p         2N302344         1p           BC107.89         1p         2N302344         1p           BC107.89         1p         2N39034566         1p           BC157/8/9         1p         2N3819         2p           BC157/8/9         1p         2N3819         2p           BC157/8/9         1p         2N3823         30p           BC167/8/9         1p         2N3823         30p           BC1867         30p         NH010         3p           BC1867         30p         NH04         3p           BC1867         30p         NH002 3         p           BC192344         1p         NH04         3p           BC1867         30p         NH002 3         p           BC192344         1p         NH002 3         p           BC192342         1p         NH002 3         p           BF19405         1p         NA360         110           BF242         0A70 0A79         p         NE555V         60p           BF342         0A70 0A79         p         14.00         14.00           BF340							
BC 107/8-9         PD 2N3702/3-4         T23         T24         T23         T24         T23         T24		34p					
BC117/B/9         Op         2N/2846         35p           BC157/8/9         11p         MpF102         40p           BC167/8/9         11p         MpF102         40p           BC167/8/9         11p         MpF102         40p           BC167/8/9         11p         MpF102         40p           BC167/8/9         12p         2N3819         25p           BC168/7         12p         PN3823         30p           BC182/3/4/L         11p         BR100 Diac         21p           BC186/7         30p         18/37         32p           BC182/3/4/L         12p         IN401         3p           BC212/3/4/L         12p         IN4002/3         6p           BF194/5         12p         IN4004/5         7p           BF198/7         14p         IN4004/5         7p           BFY50/51         16p         IN4146         4p           BFX50         16p         IOA15         7p           BFX50         16p         IOA16         7p           BFX50         10p         OA21         OA29           BY12         14p         OA17 <oa79< td="">         6p           BFX50         10p&lt;</oa79<>							
BC157/8/9         11p         VMPF102         465         BRIDGE RECTS.           BC167/8/9         11p         2X3819         250         30p           BC169/C         12p         2X3819         250         30p           BC169/C         12p         2X3819         250         30p           BC169/C         12p         2X3819         259         2A 200V         30p           BC170/209         17p         2X3823         30p         2A 200V         41p           BC186/7         30p         IN41001         5p         27-33V         9p           BC192/3/4L         12p         IN4001*         5p         27-33V         9p           BC192/3/4L         12p         IN4004*5         7p         NE555V         60p           BF198/7         14p         IN4004*5         7p         NE555V         60p           BF198/7         14p         IN4004*5         6p         ILM380         1100         7400           BFX28         0p         0A47         6p         NL400*7         8p         7400         Thp           DA200         0p         0A47         6p         0A10 0A95         6p         0L1800CKET82         7400				4/5		-	
BC1697/8/9         11p         2N3819         25p         2A 50V         30p           BC169C         12p         2N3823         30p         2A 100V         38p           BC177/8/9         17p         BR100 Diac         21p         2A 400V         48p           BC182/3/4L         I1p         BR100 Diac         21p         2A 400V         48p           BC182/3/4L         I1p         IN401         3p         2A 400V         48p           BC182/3/4L         I1p         IN4001         5p         27-33V         9p           BF194/5         12p         IN4002/5         5p         NE555V         60p           BFY50/51         15p         IN1418         4p         NE555V         60p           BFX52         30p         OA7         0A79         6p         27400         1p           BFX84         10p         OA70         0A79         6p         2400         1p         1d           BFX81         10p         OA202         7p         7400         1p         1p         1d         1p           SU1711         20p         OA202         5p         1d         1p         1d         1d         1d         1d							
BC 193C.9         120         2N382.3         300         2A 200V         41p           BC 177.0         TPD         BR100 Diac 21p         2A 400V         45p           BC 182.3/4/L         TPD         BR100 Diac 21p         2A 400V         45p           BC 192.3/4/L         TPD         BR100 Diac 21p         2A 400V         45p           BC 192.3/4/L         TPD         IN1914         3p         ZENERS BZY88           BC 192.3/2         Tap         IN4001         5p         ZENERS BZY88           BC 192.0/3         Tap         IN4001'5         7p         NE555( 40p           BF194/5         Tap         IN4004'5         7p         NE555( 40p           BFY59/51         Top         OA47         6p         ZA100'1'''           BFX80         Top         OA47         6p         ZA10''''''''''''''''''''''''''''''''''''			2N3819				
BC182/34.11p         BR100 Diac 21p         2A 400V         46p           BC182/34.11p         INH001         5p         2ENERS         82/42.34.1           BC182/34.11p         INH001         5p         27-33V         9p           BC182/34.12p         INH001/3         6p         27-7-33V         9p           BF194/5         12p         INH004/5         7p         NE555V         60p           BF198/7         14p         INH004/5         7p         NE555V         60p           BF198/5         15p         OA47         6p         NE555V         60p           BFX82         30p         OA70         0A79         8p         24/10         7400         1p           BFX84         24p         OA81         OA95         6p         0.1.1.         SOCKETS           2N1711         20p         OA200         7p         14/201         1p         0A202         7p         14/201         14p           2N2964/564         16p         741         8p         1p         1p         1p           2N2904/564         16p         7p         748         2p         1p         1p           2N2926(R1)         7p         748			2N3823		30p		
BC186/7         30p         IN914         3p           BC212/3/4/         T2p         IN401         5p         2         7-33V         8p           BC121/3/4/         T2p         IN4023         5p         2         7-33V         8p           BF194/5         T2p         IN40245         5p         NE555V         60p           BFY50/51         T4p         IN40245         5p         NE555V         60p           BFY50/51         T6p         IN414         5p         NE555V         60p           BFY50/51         T6p         IN414         5p         NE555V         60p           BFX52         30p         OA71 <oa79< td="">         5p         7400         T10p           DAT1         OA51         OA52         5p         110p         7400         T10p           DC71         10p         OA202         5p         3pin         12p         14pin         12p           2N2910         10p         OA202         5p         3pin         12p         14pin         13p           2N2904/56A         18p         741         8pin         12p         14pin         13p           2N29264/56A         18p         741</oa79<>			BR100 0	Ha	c 21p		
BUC10234         1N40023         5p         27-33V         9p           BU102         1130         IN40023         5p         NES55V         60p           BU102         1130         IN4006/5         7p         NES55V         60p           BP1902         116p         IN4148         4p         NES56         61-10           BFX80         2400         A70         A79         B7406         71-10           BFX81         240         A70         A79         B7406         71-10           BFX81         240         A70         A79         B7406         71-10           BFX81         240         A70         A79         B740         71-10           BFX81         240         A70         A79         B7         740         TH9           BSX19/20         10p         OA81         OA90         7p         74.0         TH9           SN706         10p         OA200         6p         14-pin         Tap         14-pin         Tap           2N2304/5/6A         18p         741.8-pin         2p         TA3         TA3         TA3         TA3         TA3         TA3         TA3         TA3         TA3 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td></td<>						-	
BC 77 047072         120         INADO4:5         7p           BF194/5         120         INADO4:5         7p           BF194/5         120         INADO4:5         7p           BF194/5         140         INA148         4p           BFY50/51         16p         OA/7         6p           BFX84         240         OA/7         0479           BFX84         240         OA/7         0479           BFX84         240         OA/7         0479           DC71         10p         OA/200         6p           2N1711         20p         OA/200         6p           2N1706         10p         OA/202         7p           14-pin         12p         14-pin         12p           2N2904/5/64         18p         74.8         14-pin           2N29264/5/7         16p         73         14-pin         12p           2N29264/5/64         18p         74.8         2m         16-pin         70           2N29264/5/64         18p         74.8         70         7406         12p           2N29264/5/64         18p         74.8         70         74.6         70           2N							
BF198/7         140         IN4008/7         8p         NESSE         c110           BFYS0/51         16p         IN4148         4p         DA70         0A7         6p           BFX80         30p         OA47         0A70         0A79         6p         DM14         C1+00           BFX81         24p         OA70         OA79         6p         DM14         C1+00         ZN414         C1+00           DSX19/20         16p         OA81         OA95         6p         D1.L.         SOCKETS           2N706         10p         OA202         6p         Bpin         12p         A200         14-pin         13p           2N2904/5/6A         18p         741         6p in         12p         Mica + butes         TO3         TO66         5p           2N2904/5/6A         18p         741         6p in         2p         TO3         TO66         5p         Daio         Pain         70         TO8         5p         Daio         F1         70         TO8         5p         Daio         F1						1	
BFY50.51         16p         IN1139         4p         LM380         C1.00           BFX29         30p         OA70         0A79         8p         SA19/20         ZN414         C1.00           BFX29         20p         OA70         0A79         8p         SA19/20         Th14         C1.00           BFX29         16p         OA81         OA90         6p         D.1.L         SOCKETS           2N706         10p         OA200         6p         B-pin         12p           2N1711         20p         OA202         7p         14-pin         13p           2N2904/5/64         18p         709 all         25p         Mice + bushes           2N2926/6A         18p         748         D.1.L         30p         Pai           2N2926/6A         18p         748         D.1.L         30p         Pai         Daio Pen         70p           PRICES INCLUSIVE + 15p P. & P. (1st class)         PA         P. (1st class)         Pa         Pa         Pa         Pa         Pa							
BF X83         24p         OAro         OAro         Stat         ZMA14         C1-R0           BF X84         24p         OAs1         OAgo         Fp         7400         Tp         D           BSX 19/20         16p         OAs1         OAgo         Fp         D         L1.         SOCKETS           2N706         10p         OA202         7p         14/pin         12p           2N1711         20p         OF, AMPS         Hics         bushs         Fp           2N2904 5/64         16p         741         Pin         12p         16/pin         13p           2N2904 5/64         16p         741         Pin         25p         To 366         5p           2N29264 70         7p         748         12n         25p         To 366         5p           2N29264 70         7p         748         12p         15p         To 366         5p           2N29264 70         7p         748         12p         To 366         5p         To 37         To 366         5p           2N29264 70         7p         748         12p         Lastron         7p         Asin         7p           PRICES INCLUSIVE + 15p <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>M380 £1-00</td></td<>							M380 £1-00
BSX19/20         Tep         OA81         OA90         7p           OC71         Top         OA81         OA95         6p         D.I.L. SOCKETS           2N706         Top         OA200         6p         8-pin         12p           2N1711         Zop         OA200         6p         8-pin         12p           2N2219         Zop         OF, AM2PS         16-pin         14p           2N2904/5/6A         18p         741         8-pin         20p           ZN2926/6/7         7p         748         71         20p         TO3         TO45         5p           ZN2926/17         7p         748         0-LL         30p         To3         TO45         5p         TO3         TO45         5p         Dato Pen         70p         To45         5p         Dato Pen         70p         To45         5p         PAICES         INCLUSIVE + 15p P. & P. (1st class)         15p int 14p         15p int 14p int 14p         15p int				A75			
OC71         10p         OA81 OA95         6p         D.I.L. SOCKETS           2N706         10p         OA200         6p         8-pin         12p           2N1711         20p         OA202         7p         14-pin         13p           2N1219         20p         OA         AMPS         16-pin         14p           2N2304.5/6/7         16p         709 all         25p         Mice + buehee         TO3         TO645         5p           2N2326(R)         7p         748 D.I.L.         35p         Daio Pen         70p           PRICES INCLUSIVE + 15p P. & P. (1st class)         25p         1st class)         1st class         1st class					) 7p	100	
ZN006         10p         OA202         7p         14-pin         13p           ZN1711         20p         OF, AMPS         14-pin         13p           ZN2904.567         50p         31l         25p         15-pin         13p           ZN2904.566         18p         741         8-pin         25p         703         T066         5p           ZN2926(R)         7p         748.01.L         32p         Dato Pan         70p         Dato Pan         70p           PRICES INCLUSIVE + 15p P. & P. (1st class)         25p         21st class)         25p         25p <t< td=""><td></td><td>10p</td><td></td><td>A95</td><td></td><td></td><td></td></t<>		10p		A95			
ZN219         Zop         OF. AMPS         Top         Top         Tap           ZN2904         5/6/7         169         709         all         25p         Mice + bushes           ZN2904/5/6/7         169         n1         709         all         25p         To3         To646         5p           ZN2926(R)         7p         748         D.1.L         36p         Daio         Pen         70p           PRICES INCLUSIVE + 15p         P. & P. (1st class)         36p         All stap         All stap         All stap							
N2304/5/6/7         709 all         25p         Mice         bushes           2N2304/5/6/1         Bp         748 D.1.L         36p         Dato Pen         70p           PRICES INCLUSIVE + 15p P. & P. (1st class)				Ek.			
2N2904/5/6A         18p 7P         741 8-pin 748         28p 1.L         TO3         TO66         5p Delio         Pen         70p           PRICES INCLUSIVE         +         15p         P. & P. (1st class)						ł M	lics · bushes
PRICES INCLUSIVE + 15p P. & P. (1st class)	2N2904/5/6	A 18p					
				20		-	
	PRICE	SINCL	USIVE	+	15pP.	8 P	. (1st class)
	_			_		_	

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7450	16p 17p	74175	92p 108p	MFC6040	Electronic Attenuator	112p	21030	04 0 0A 2008	BCY71 BD131	24p 39p	TIP36A	297p 70p	BF244	40p
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