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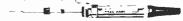
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FLUORESCENT LAMP INVERTER-P.E. SCORPIO Mk 2 IGNITION SYSTEM

Our April issue will be published on Friday, March 8, 1974

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WOI	1007	30p	- 1 1
W02	200V	32p	1
W06	600V	35p	18ac1
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2 AMPS	-		
B2/05	50 V	35p	11
B2/10	100A	40 p	11
B2/20	200V	45p	1 1
B2/60	600V	50p	•
B2/100	1000V	55p	
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4 AMPS			~
B4/100	1001	55p	7
B4/200	200∨	59p	1171
B4/400	400 V	65p	- // //
B4/600	600V	75p	11 11
B4/800	800V	£1 00	11 11
†H׆L×	∦in. dia.		.1 11
6 AMPS			
B6/05	50V	65p	
B6/10	100V	70p	
B6/20	200V	80p	
B6/40	400V	90p	
B6/60	600V	£1.00	

× åin. dia.

AMP

SILICON (RECTIFIERS Type		LLED
I AMP (TOS	APIV	1-11
CRS I/OSAF	50V	30p
	1007	
CRS I/IOAF		30p
CRS 1/20AF	200∨	35p
CRS I/40AF	400V	45p
CRS I/60AF	600V	55p
3 AMP (TO	48)	
CRS 3/05AF	50 V	40p
CRS 3/10AF	100 V	40p
CRS 3/20AF	200V	45p
CRS 3/40AF	400V	55p
CRS 3/60AF	600V	65p
5 AMP	400V	60p
CRS	5/400V	60p
T AMB /TO	40)	•
7 AMP (TO	48)	
CRS 7/100	100V	60p

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15 ZTX300
14 2N3714
1-60
15 ZTX300
18 2N3771
1-75
25 ZTX500
15 2N3773
2-25
25 ZTX500
15 2N3819
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25 ZN706
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65 2N930
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15 25 2N4661
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15 52 N1671
1-00 2N1613
10 2N51457
16 55 2N1671
1-00 2N1613
10 2N3054
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Mk III Sound to Light Unit Chassis Version



The audio drive voltage is derived directly from the amplifier output or across the speaker load. The unit converts the audio-frequency signals into a three-coloured light display when used with coloured flood lamps or similar; the coloured depending on the frequency of the signal and the intensity on the loudness of the audio source.

Max. power 1-SkW per channel at 240V a.c.
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As optional extras, an attractive ready-punched facia panel and control knobs are available. The unit is available as a ready built mixer with facia.

Size: 9 Sin x 4:8in x 1:Sin (with facia)

Construction manual available separately at 25p. Kir Price £11.



STL/I Single Channel Sound to Light Unit

Single channel "Sound to Light" unit with 60mm slider fader controls for audio trigger level and background load dimmer. This unit is switchable for response to High, Mid. and Low frequency audio signals, selected by facia control. A D.J. "pulse-flash" push button is fitted for manual flashing of the lamp load together with seen lead indicator.

neon load indicator. Maximum Load: IkW at 240V a.c. Size: 8in × 3-6in × 3in.

Price £14:30.

Practical Electronics "Scorpio" Electronic **Ignition System Kit**



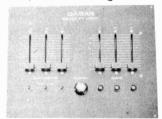
This Capacitor-Discharge Electronic Ignition system was described in the November and December issues of Practical Electronics. It is suitable for incorporating in any 12V ignition system in cars, boats, go-karssett.

Case size: 25in V. 4-Sin - 2in approx.

Complete assembly and wiring manual 25p.

Price £12-10.

STL/3 Sound to Light Unit



The performance of this unit is similar to the Mk III chassis, version above, but is provided with an attractive black anodised facia panel and designed to mount directly into equipment desks or cabinets. High, Mid. and Low frequency channel sensitivity controls employ 60mm slider faders for present-day attractive appearance and ease of use. Size Itin x 8-5in x 4in. Price £42:35.

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LOAD IMPEDANCE:
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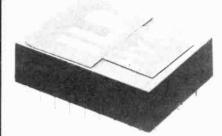
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The combination of two HY50's two HY50's sharing a common power supply (PSU50) are linked by a balance control to form a complete stereo system.



SPEC.

INPUTS
Magnetic Pick-up 3mV (within IdB RIAA Magnetic Pick-up 3mV (within curve)
Ceramic Pick-up up to 3mV.
Microphone I0mV.
Tuner 250mV.
Auxiliary 3-I00mV.
Input impedance 47kΩ | kHz

OUTPUTS Tape 100mV. Main output. 0dB (0-775V). ACTIVE TONE CONTROLS Treble ± 12dB at 10kHz Bass ± 12dB at 100Hz

OVERLOAD CAPABILITY (equalization stage) 40dB on most sensitive input. OUTPUT NOISE LEVEL (below 10mV magnetic input) 68dB.

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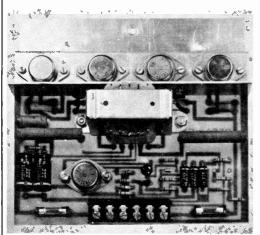
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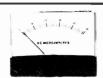
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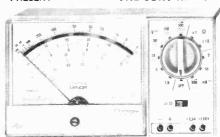
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2½ in × 1in 2½ in × 3½ in 2½ in × 5in 3½ in × 3½ in 3½ in × 5in 17in × 2½ in 17in × 3½ in	7p 24p 26½p 26½p 30p -82p	7p 18p 23p 23p 30p 63p	0-15in 12p 13p 22p 45p					
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Dip Breadboard 115 Verostrip 26								
Pin Insertion to Terminal Pins	00			54				

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	REC	TIFIE	R5	
PI.V.		1 amp	3 ami	D
50	1N4001	6 ½ p	1N5400	15 իր
100	1N4002	7½p	1N5401	16 p
200	1N4003	9p	1N5402	17 ½ p
400	1N4004	9p	1N5 4 04	22p
600	1N4005	11p	1N5406	26 ≟ p
800	1N4006	13½p	1N5407	30 p
1000	1N4007	16½p	1N5408	33p
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BY103	22p	E	3Y164	55p
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			4 4446	*****		• 4	77 64	~	-				
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AC126	13p	BC107	11p		17p	BF181		BU105	£1 - 75		99p		
AC127	13,5	BC108	11p		17p	BF184		BU105 02			36 i p		
AC128	13p	BC109	11p		28p	BF185		D13V		TIS73	£2 · 10		
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AC 187	22p	BC117	22p	BD115	74p	BF195		MJ4010	£1 - 49	2N697	16 i p	2N3055	
AC187K	20p	BC147	10p	BD124	82p	BF196		MJE340	52p	2N706	13p	2N3391A	
AC188	22p	BC148	10p	BD131	55p	BF197		MJE2955	£1-82		16 è p	2N3566	
AC188K	25p	BC149	10p	BD132	66p	BF200	32p		92p	2N914	24 p	2N3638	
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ACY20	22p	BC 158	12p		72p	BF244B	27 p		41p	2N1303	24p	2N3703	
AD140	49p	BC 159	14p	BD135	42D		25p		45 p	2N1304	24p	2N3704	
AD149	49p	BC168B	11p	BD 136	44p	BF263		MPF105	45p	2N1305	24p	2N3705	
AD161	29 p	BC189		BD137	50p	BF272	£1 21	MPF106	49 i p	2N 1306	240	2N 3706	
AD162	29p	BC171	20p	BD138	55p			OC28	50p	2N 1307	27 I p	2N3707	
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AF126	27p	BC187	27 p	BF160	25 p	BFY51		OC83	25p		46p	2N3823	
AF127	27p	BC212L	12 p	BF167	24p	BFY52		OC140	22p		16p	2N3903	
AF139	35p	BC213L		BF173		BR100		OC170	28p		16p	2N3904	
AF172	25p	BC2144	11pi	BF177	28p	BRY39	440	OC171	33p		10p	2N3905	
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12p	2N5129	16 p	BA114	9p	OA5	99p
13p	2N5172	11p	BA115	19p	OA10	94p
12 p	2N5459	69p	BA116	9p		11p
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1 5 2 2 3 3 9 6 6 10 6 10 6 10 6 10 6 10 6 10 6 10	450V	160V	100V			25V	16V	10V	6 · 3V	4V	μF
2 2 6 6 6 8 6 6 6 7 6 6 7 6 7 6 7 7 7 7 7 7	15p	8 p		6 jp							1
3 3 4 7 6 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9				6 p					-		1.5
4 7 8 8 8 8 8 8 8 8 8 8		6 p		6 j p							2.2
6 8 8 8 8 6 6 6 6 6 6 6 6 6 6 6 6 7 8 7 8				6 ∤ p			A 4		E 1		
22	17p (4µF)	8 j p		₿ġ₽			11	•			
22			6 p	6 _i p	₿≩₽		C			ĺ	6.8
22	21p						0				8
22			8 j P	6 p	-	6 g p		-			10
33 47 47 61p	24p (16µ)			6 p	6 j P		6 p				15
47 6ip 6ip 6ip 6ip 6ip 8p 11p 11p 100 6ip 8p 11p 11p 100 6ip 8ip 8p 11p 11p 14p 25p 14p 25p 11p 14p 25p 11p 14p 12p 11p 14p 12p 12p 12p 14p 14p 14p 14p 14p 14p 14p 14p 14p 14			11p	8 p		B p		9 1 b			
47 6ip 6ip 6ip 6ip 6ip 6ip 8p 11p 14p 25p 16p 8p 16p 6ip 8p 11p 14p 25p 16p 8p 11p 14p 25p 25p 25p 25p 25p 25p 25p 25p 25p 25	33p (32µF				6±p		6 į p		6 p		33
100	25p (50µF			8p	6 p	6 p	6∳b	6 jp		6 p	
150	(350V)			11p			6 p		6jp		68
220 6 p 6 p 8 p 11p 14p 13p 31p 31p 330 6 p 8 p 11p 14p 22p 44p 47p 48p 48p 48p 48p 48p 48p 48p 48p 48p 48			25p					6 ∮ p		6‡p	
330 6 p 5p 11p 25p 44p 470 8p 11p 14p 20p 25p 44p 470 8p 11p 14p 20p 25p 47p 580 13p 14p 19p 22p 25p 48p 78p 580 13p 14p 19p 22p 25p 44p 78p 580 18p 18p 25p 44p 78p 18p 24p 38p 44p 78p 149p 22p 25p 44p 78p 18p 24p 38p 44p 78p 149p 18p 25p 38p 44p 18p 25p 38p 24p 24p 24p 24p 24p 24p 24p 24p 24p 24				14p	11p	6p	6 ₁ p		6 p		150
330 6 p 8p 1p 25p 44p 470 8p 11p 14p 20p 28p 47p 680 10p 14p 20p 28p 58p 58p 58p 58p 58p 58p 58p 58p 58p 5			31p	19p	14p	11p	8p	6 ↓ p		6 _± p	220
470 8p 11p 14p 20p 26p 47p 880 10p 14p 20p 25p 59p 000 13p 14p 19p 22p 25p 44p 79p 000 18p 19p 25p 39p 44p 79p 14pp 000 18p 24p 39p 44p 79p 14pp						•	11p	8p		6 p	330
580 10p 14p 20p 25p 58p 000 13p 14p 18p 22p 25p 44p 79p 000 18p 18p 25p 25p 25p 25p 25p 25p 25p 25p 25p 25			47p	26p	20p	14p		11p			
500 18p 19p 25p 200 18p 24p 39p 44g 79p 149p			59p		25p	20p			10p		
200 18p 24p 39p 44p 79p 149p			79p	44p	25p	22p	19p	14p		13p	000
200 18p 24p 39p 44p 79p 149p							25p	19p	18p		
			149p	79p	44p	39p		24p	18p		
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CZ14 18p P54 £1-61 16p CZ13A 18p VA105 18p CZ19 18p VA105 18p CZ19 18p VA1026 18p CZ19 18p VA1034 18p E238CD A258 13p VA1055 18p E238CD A258 13p VA1055 18p E238CD A25 13p VA1055 18p E238CD D258 13p VA1058 18p E238CD D258 14p VA1058 21p E238CD D258 14p VA1058 21p E238CD D258 14p VA1068 21p E238CD D258 14p VA1098 21p E238 14p VA10	A15B	98c	GL23	£1-21
CZ13A 18p VA1005 18p CZ19A 18p VA1026 18p CZ19 18p VA1026 18p CZ19CZ19 18p VA1036 18p CZ19CZ19 18p VA1034 18p CZ19EC AZ62 13p VA1034 18p CZ19EC AZ62 13p VA1039 18p CZ19EC AZ62 13p VA1039 18p CZ19EC AZ62 13p VA1053 18p CZ19EC AZ62 13p VA1053 18p CZ19EC AZ65 13p VA1055 18p CZ19EC AZ65 13p VA1055 18p CZ19EC AZ65 13p VA1055 18p CZ19EC AZ65 14p VA1055 14p CZ19EC AZ65 14p VA1055 12p CZ19EC AZ65 14p VA1057	CZ1	164p	R53	
C219	CZ4	180	R54	£1-61
E298CD A258 13p VA1034 16p E298ED A256 13p VA1034 16p E298ED A256 13p VA1039 18p E298ED A262 13p VA1040 18p E298ED A262 13p VA1053 18p E298ED A265 13p VA1053 18p E298ED A268 13p VA1055 16p E298ED A268 13p VA1055 16p E298ED A268 13p VA1055 16p E298ED A268 13p VA1055 16p E298ED A268 14p VA1055 17p E298ED P348 14p VA1077 19p E299ED P348 14p VA1077 19p E299ED P348 14p VA1098 21p E299ED P348 14p VA1098 21p E299ED P348 14p VA1098 21p E299ED P348 14p VA1098 22p E299ED P348 14p VA1098 22p E299ED P348 14p VA1098 22p	CZ13A	18p	VA1005	16p
E298ED A256 139 VA1034 169 E298ED A262 139 VA1039 159 E298ED A262 139 VA1040 169 E298ED A265 139 VA1053 169 E298ED P268 139 VA1055 169 E298ED P268 139 VA10555 169 E298ZZ 05 139 VA10565 179 E299DD P336 149 VA10575 179 E299DD P386 149 VA1077 199 E299DD P386 149 VA1077 199 E299DD P386 149 VA1078 279 E299DD P386 149 VA1098 219 E299DD P386 149 VA1104 319 E299DD P386 149 VA1104 319 E299DD P386 149 VA1104 319 E299DD P386 149 VA1107 279 E299DD P386 149 VA1107 279	CZ19	160	VA1026	16p
E298ED A256 13p VA1034 16p E298ED A266 13p VA1039 18p E298ED A266 13p VA1040 16p E298ED A265 13p VA1053 16p E298ED P268 13p VA10555 16p E298ZZ 05 13p VA10555 16p E298ZZ 05 13p VA10565 17p E299DD P336 14p VA10575 19p E299DD P346 14p VA1077 19p E299DD P342 14p VA1098 21p E299DD P346 14p VA1104 31p E299DD P346 14p VA1104 31p E121 VA1107 25p	E298CD A258	13p	VA1033	16p
E298ED A262 13p VA1040 16p E298ED A265 13p VA1053 16p E298ED P268 13p VA10555 16p E298ZZ 05 13p VA10555 16p E298ZZ 05 13p VA10565 17p E299DD P336 14p VA10675 17p E299DD P336 14p VA1077 19p E299DD P346 14p VA1078 19p E299DD P346 14p VA1104 31p E299DD P346 14p VA1104 31p E295DD P346 14p VA1104 31p E129DD P346 14p VA1107 29p		13p	VA1034	16p
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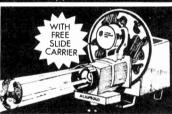
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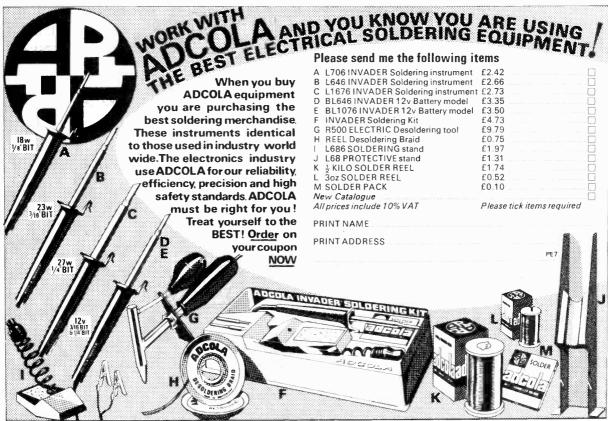
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1-0µF 63V	2½ x 33" 26p 19p 31 x 5" 31p 33p 33p 33 x 5" 31p 33p 33p 31 x 33" 28p 28p 28p 28p 22 x 11p 21 x 12p 21 x 13" (Plain) — 14p 5 x 31" (Plain) — 12p 5 x 31" (Plain) — 22p 1nsertion tool 59p 59p Track Cutter 44p 44p 44p 19n 5 x 5 x 5 x 5 x 5 x 5 x 5 x 5 x 5 x 5	DIODES PLUGS IN4001 6 pp IN40027 pp 3 Pm 12p IN4003 9p Std. Jack 14 pp IN4005 12p 2.5mm Jack 14 pp IN4006 14p Phono 5 pp IN4006 14p Phono 5 pp IN914 7p SOCKETS IN916 7p DIN 2 pn In914 7p SOCKETS IN916 7p DIN 2 pn In90 A5 42p 5 pm 180° 12p OA47 9p Std. Jack 14 pp OA81 14 pp OA81 14 pp DA81 14 p	2 22/63, 5p. 2/10, 10,10, 50/10, 100/10, 10/25, 50/25, 10/50, 5\phip. 20/10, 100/25, 50/50, 6\phip. 500/10, 200/10, 10/25, 50/50, 6\phip. 500/10, 200/25, 100/50, 9p. 1000/10, 50/25, 100/50, 9p. 1000/10, 50/25, 200/50, 11p. 2000/10, 1000/25, 500/50, 16\phip. 1000/50, 3pp. 1000/100, 6\phip. 2000/125, 27p. 2500/12, 17p. 2500/25, 33p. 2500/50, 62p. 3000/50, 72p. 5000/25, 66p. 5000/50, 9\phip. 7000/50, 60p. 25,000/25, 1\phip. 10/500, 32p. 50/520, 18p. 100/500, 33p. 45p. 50/5250, 18p. 100/500, 33p. 45p. 50/500/50, 50/50, 60/50
33µF 16V 6p 1000µF 16V 20p 33µF 40V 6p 1000µF 25V 25p 32µF 63V 6p 1500µF 6·4 15p 47µF 10V 6p 1500µF 6·4 15p 47µF 25V 6p 2200µF 16V 25p 47µF 63V 8p 3300µF 6·4 26p	BC183L 12p 2N2926 11p	μΑ709C 50p Stereo Scree μΑ741C 55p Connecting μΑ723C £1 Neon Bulb.	/ire, Metre

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Ref.	VA	Wei	ght	, Si	ze c	m.	P & P		
No.	(Wotts)	IЬ	οz				£.	30	
07	20	- 1	8	7·0 × 6·	0 ×	6.0	2.32	30	
149	60	3	12	9.9 × 7	7 ×	8.6	3 45	36	
150	100	5	8	9.9 x 8	9 x	8.6	3.79	52	
151	200	8	0	12·1 × 9	3 ×	10.2	6.45	52	
152	250	13	12	12·1 × 11	8 ×	10.2	8.41	67	
153	350	15	0	14·0 × 10	8 ×	11.8	11-20	82	
154	500	19	8	14·0 × 13	4 x	11-B	16.25		
155	750	29	0	17·2 × 14	0 x	14.0	22-10		
156	1000	38	Ó	17·2 × 16	6 x	14.0	29.87		
158	2000	60	ō	21.6 × 15	3 ×	18-1	49.25		

				AU.	TO T	RAP	SFORM	ERS		
Ref.	VA	We	ight	: Ŝ	ze cm		Auto	Tops	P 8	, P
No.	(Watt	s) Ib	οz						£	Þ
113	20	1	0	5.8 ×	5-1 ×	4.5	0-115-210	-240	1.22	22
64	75	2	4	7·0 ×	6.7 ×	6.1	0-115-210	-240	2.40	30
4	150	3	4	8.9 x	7·7 ×	7.7	0-115-200	-220-240	2-89	36
66	300	6	4	9•9 x	9.6 ×	8-6	1.1	71	5.63	52
67	500	12	8	12.1 ×	11-2 ×	10.2		**	8.36	67
84	1000	19	8	14.0 x	13·4 ×	14.3	11	11	15-19-	82
93	1500	30	4	14.0 x	15.9 ×	14-3			21.99	
95	2000	32	0	17.2 x	16.6 ×	14.0		11	28.70	
73	3000	40	ŏ	21.6 ×	13.4×	18-1		**	39-17	

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PR	ımı	ART	- 41	ノロームコレ	, , ,	LIS	1 A	NDO	PA 71	AOFI	MAI	105
Ref.	Ar	mbs.	V	Veight	:	Size ci	n.	Seco	ndary	Windin	gs P	& P
		/ 241									£	P 22
111	0.5	0.25	,	8	4.8.x	2.9 ×	3.5	0-12V	at 0.2	5A × 2	1.22	
213	1.0	0.5	- 1	4	6-1 ×	5-8 ×	4.8	0-12V	at 0.5	A×2	1-44	22
71	2	1	Ĺ	12	7.0 ×	6-4 ×	6.1	0-12V	at IA	× 2	1.90	22
18	4	2	2	12	8-3 ×	7.7 ×	7.0	0-12V	at 2A	× 2	2.68	36
70	6	3	3	8	8-9 ×	8-0 ×	7.7	0-12V	at 3A	× 2	3.20	42
108	8	4	5		9.9 ×	8-9 x	8.6	0-12V	at 4A	× 2	3.60	52
72	10	5	6	. 4	9.9 x	9.6 ×	8.6	0-12V	at 5A	× Ž	4.25	52
116	iž.	6	6	12				0-12V			5-10	52
17	16	ā	8	12	12-i×	9.9 x	10.2	0-12V	at 8A	× 2	6.56	52
115	20	10	11	B	14-0 ×	9.6 x	11.8	0-12V	at 10	A×2	8.36	67
187	30	i š	15	Ř	4.0 ×	12:1 x	11.8	0-12V	at 15.	A×2	15-40	82
226		30						0-12V			28-44	
				-						ANGE		

Ref.	Amps	Weight	Size cm.	Secondary Taps	P & P
No.		lb oz			1:42 P
112	0.5	1 4	6·1 × 5·8 × 4·8 0	-12-15-20-24-30V	1.42 27
79	1.0	2 4	7.0 × 6.7 × 6.1		1.92 36
3	2.0	3 4	8.9 x 7.7 x 7.7	11 11	2.90 36
20	3.0	4 8	9.9 × 8.3 × 8.6		3.58 42
2Ĭ	4.0	6 4	9.9 × 9.6 × 8.6		4-25 52
5 i	5.0	6 12	12·1 × 8·6 × 10·2		5-30 52
117	6.0		12·1 × 9·3 × 10·2	**	6-31 57
88	8.0		12-1 × 11-8 × 10-2	**	B-18 67
				1.5	
89	10.0	13 12	14·0 × 10·2 × 11·8		10.33 67
			50	VOLT RANG	E
D -6	A	14/-:	et - con	Consider. Take	D 8. D

Ref.	Amps	. W	eigh	t	Size cn	n.	Second	lory Taps	P 8	, P
No.		Ib o	z						£	Þ
102	0.5	1 1	2	7·0 ×	6·4 ×	6-1	0-19-25-3	3-40-50V	1.90	3
103	1.0	2 i	12	8:3 ×	7.4 ×				2.80	3
104	2.0	5	8	7.9 x	8-9 x	8.6		11	3.87	4
105	3.0	6 1	12	9-7 x	10-2 ×	8-6	1.7	,,	5.26	5
106	4.0	10			10.5 ×				6.99	5
107	6.0	iž			10.2 ×		11	1.5	10.35	6
118	8.0	18			12.7 ×			4.9	13.51	9
119	10.0	25			12.7 ×		* *	* *	16.95	- 1
117	10.0	25	v	17.2 X	12.7 X		0 VAL	RANG		
							SO VOLT			

							90 A O L	IRANG	E	
Ref.	Amps.	. W	/eig	ht	Size	cm.	Seco	ndary Taps	. P	& P
No.		160	z						£	P
124	0.5	2	4	7·0 ×	6.7	x 6·1	0-24-30-	40-48-60V	1.93	36
126	1.0	3	4	8.9 ×	7.7	× 7.7		.,	2.70	36
127	2.0	6	4	9.9					4.25	42
125	3.0	ě	12			× 10-2		**	6-46	52
123	4.0	13	iž			× 10-2			8.36	67
40	5.0		00			× i i · ē	1.2	13	9.85	67
120	6.0	15	8			II-8		**	12:14	82
								P 4		92
121	8.0		00			× II · 8			13-65	•
122	10.0	25	0	17-2 >	:12-7	× 14-0	,,		20.09	
189	12.0	29	00	17.2 x	14.0	× 14-0			22.49	

189			2 × 14·0 × 14·0	21 11	22.49	
	MINIAT	URE TR	ANSFORME	RS WITH SCRI	EENS	
Ref.	mA	Weight	Size cm.	Volts	P	& P
No.		lb oz			£	Þ
238	200	2	$2.8 \times 2.6 \times 2.0$	3-0-3	1.31	10
212	IA, IA	1 4	6-1 × 5-8 × 4-8	0-6, 0-6	1.52	22
13	100	4	$3.9 \times 2.6 \times 2.9$	9-0-9	1.12	10
235	330, 330	4	$4.8 \times 2.9 \times 3.5$	0-9, 0-9	1.52	10
207	500, 500	1 00	6-1 × 5-4 × 4-8	0-8-9, 0-8-9	2.03	22
208	IA. IA	1 12	7-0 × 6-4 × 6-1	0-8-9, 0-8-9	2.73	30
236	200,200	4	4-8 × 2-9 × 3-5	0-15, 0-15	1.52	10
214	300, 300	11 4	6-1 × 5-8 × 4-8	0-20, 0-20	1-60	22
221	700 (d.c.)	1 8	7.0 × 6.1 × 6.1	20-12-0-12-20	1.41	30
204	LALLA	2 12	0.2 ~ 7.7 ~ 7.0	0.15.20 0.15-20	3.08	38

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35W RMS uses 7 transistors and 7 diodes. Carr. paid.

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In extra slimline easy-fit case.

Using grouped pairs of inputs (high Z and low Z inputs) with individual bass, treble and volume controls on each pair, plus master control on output of M6HL. These low-noise units will feed all makes of amplifiers, making them ideal for clubs, discos, etc. Standard jack sockets, compact design. In strong metal cases. All Units guaranteed for 3 years.

- HIGH AND LOW IMPEDANCE INPUTS
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4 high Z, 4 low Z inputs, 4 sets of controls. Case 10" × 8" and only 2\{\frac{1}{2}\) in deep. Carr. paid.

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Channel section modules, for building your own: gain—16 x (24dB). Tone controls—18dB swing. Carr. paid.

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CONTROL UNITS UNBEATABLE FOR QUALITY AND VALUE

EXCITING NEW STEREO VERSION. MK. II with stereo over-ride and case. (Carr. 30p). Mono (as shown).

For 9 v. battery operation. As stereo model, less mic. **£6.50** input, Carr. 20p.



Two decks, and full headphone monitoring. The unit is mains operared and measures 17‡in × 3in × 4in deep and is finished with a smart white on black facia. The controls are: Left/Right deck fader, volume, bass, treble, Headphone Selector and volume, Microphone volume, bass treble, mains on/off. Comparable to units at over twice the price.

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World famous D.190Cthe one the professionals use—at special bargain price £19.50 Plus

GENERAL PURPOSE MIC. Dynamic professional quality. Carr. pd. £9.90 120 W HEAVY DUTY MODULE

Rugged class A driver stage This module will run from all our mixers, etc., and most other makes. Delivers 120W into an eight ohm load and employs 4 TO3 can (115W) output transistors. SPECIFICATION

SPECIFICATION
Power output, 120W into 8 ohms
Freq, response, 20–20,000Hz ± 2dB
Input sensitivity, 200mV into 10K
Construction, Fibreglass board
Size, 8in × 4in × 4in (Sin with supply)
Low distortion parallel push-pull
Constructions of the supply of the s output stage.

■ 160 watts version with power supply (Carr. 50p) £27.90

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Our popular 3 channel model handles up to 3kW (3,000W) of lighting and incorporates versatile sound control arrangement to enable professional standards to be achieved. Both units are excellent examples of Saxon quality and value.

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COMPLETE AMPLIFIERS CSE 100 This versatile unit is now available in a black vynide case and so represents even better value than even delivering speech and music powers of up to 100 VM RMS and continuous signal outputs of 70 VM. Two individually controlled inputs with wide range bass

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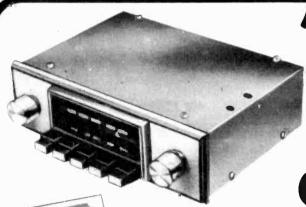
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Technical specification:

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Integrated circuit output stage, pre built three stage IF Module.

Controls Volume, manual tuning and five push buttons for station selection, illuminated tuning scale covering full medium and long wave bands.

Size Chassis 7 ins. wide, 2 ins. high and 4 18 ins. deep approx.

NOTE: The ability to solder on a printed circuitboard is necessary to complete this kit successfully. Circuit diagram and comprehensive instructions 55p.free with kit.

Car Radio Kit

£6.60 + 55p. postage & packing.

Speaker including baffle and fixing strips

£1.65 + 23p. postage & packing.

Recommended Car Aerial - fully retractable and locking. £1.35 post paid.

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QUALITY SOUND FOR LESS THAN£19.00

Stereo 21 easy to assemble audio system kit, - no soldering required Includes:—

BSR 3 speed deck, automatic, manual facilities together with ceramic cartridge.

Two 8" 5" speakers with cabinets.

Amplifier module. Ready built with control panel, speaker leads and full, easy to follow assembly instructions.

For the technically minded :-

Specifications:

Input sensitivity 600mV: Aux. input sensitivity 120mV: Power output 2.7 watts per channel: Output impedance 8-15 ohms. Stereo headphone socket with automatic speaker cutout. Provision for auxiliary inputs - radio, tape, etc., and outputs for taping discs. Overall Dimensions. Speakers approx.

 $15_2^{**}-8^{**}\times4^{**}$. Complete deck and cover in closed position approx. $15_2^{**}\times12^{**}\times6^{**}$. Complete only $\pounds18\cdot45+16p$.

Extras if required. Optional Diamond Styli £1.37

Specially selected pair of stereo headphones with individua level controls and padded earpieces to give optimum performance, £3.85.

DISCO AMPLIFIER

Reliant Mk IV Mono Amplifier, ideal for the small disco or house parties.

Outputs 20 watts B.M.S. into 8 obes (suitable

Outputs 20 watts R.M.S. into 8 ohms (suitable for 15 ohms).

Inputs *5 Electrically Mixed Inputs. *3 Individual Mixing controls. *Separate bass and treble controls common to all 5 inputs. *Mixer employing F.E.T. (Field Effect Transistors). *Solid State Circuitry. *Attractive Styling.

1) Crystal Mic or Guitar 9mV. 2) Moving coil Mic or Guitar 8mV. 3), 4), 5) Medium output equipment (Gram. Tuner, Monitor, Organ, etc.) – all 250mV sensitivity.

Size approx. 12 $\frac{1}{2}$ ins. \times 6 ins. \times 3 $\frac{1}{2}$ ins. £13.50 + 60p. postage & packing.



8TRACK CARTRIDGE PLAYER

Elegant self selector push button player for use with your own stereo system. Compatible with Viscount III system, the Stereo 21 and the Unisound module.

Technical specification.

Mains input, 240V. Output sensitivity 125mV

Comparable unit sold elsewhere at £24.00 approx.

Yours for only £10·60 + 90p. p& p



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For the man who wants to design his own stereo —here's your chance to start, with Unisound—pre-amp, power amplifier and control panel. No soldering—just simply screw together. 4 watts per channel into 8 ohms. Inputs: 120mV (for ceramic cartridge), The heart of Unisound is high efficiency I.C. monolithic power chips which ensure very low distortion over the audio spectrum.

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A suitable 3 speed tape deck, less heads. Caters up to $5\frac{3}{4}$ ins. spools. 240V AC mains. Unused but store soiled hence no

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Viscount III - R102 now 20 watts per channel. System I includes.

Viscount III amplifier - volume, bass treble and balance controls, plus switches for mono/ stereo on/off function and bass and treble filters. Plus headphone socket Specification

20 watts per channel into 8 ohms Total distortion@ 10W@ 1kHz 0 1%. P.U.1 (for ceramic cartridges) 150mV into 3 Meg. P.U.2 (for magnetic cartridges) 4mV @ 1kHz into 47K. equalised within 1dB R.I.A.A. Radio 150mV into 220K. (Sensitivities given at full power). Tape out facilities: headphone socket, power out 250mW per channel. Tone controls and litter characteristics. Bass: . 12dB to -17dB @ 60Hz. Bass filter: 6dB per octave cut. Treble control: treble 12dB to -12dB @ 15kHz. Treble filter: 12dB per octave. Signal to noise ratio: (all controls at max.) -58dB Crosstalk better than 35dB on all inputs. Overload characteristics better than 26dB on all inputs. Size approx. 133"... 9"... 33".

Garrard SP. 25 Mk III deck with magnetic cartridge, plinth and cover Two Duo Type II matched speakers

Enclosure size approx. $17\% \times 10\frac{1}{2}\% \times 6\frac{1}{2}\%$ in simulated teak. Drive unit $13\% \times 8\%$ with parasitic

tweeter. Complete System £49.00

Viscount III amplifier (As System I) Garrard SP. 25 Mk III deck (As System I) Two Duo Type III matched speakers Enclosure size approx. 23;" 11;" 9; Finished in teak veneer. Drive units approx. 13;" 81" with 31" HF speaker. Max. power 20 watts, 8 ohms. Freq. range 20Hz to 20kHz.

Complete System £65.00

PRICES - SYSTEM 1

Viscount III R 102 amplifier £24-20 £1 p & p 2 Duo Type II speakers £14.00 £2.20 o 8 o Garrard SP25 Mk. III with MAG, cartridge plinth & cover £18-00 £1-75 p & p

total £56 20

Available complete for only £49:00 - £3:50 p. & p.

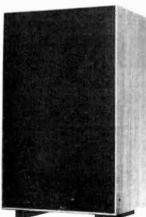
PRICES: SYSTEM 2

Viscount R 102 amplifier £24-20 - £1 p & p £32 00 £3 30 p & p 2 Dun Tyne III sneakers Garrard SP25 Mk III with MAG, cartridge plinth & cover f18:00 £1-75 n & n

total £74-20

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THE ULTIMATE COMPLETE SPEAKER SYSTEM EMILE 315



Recommended retail selling price, £86.00.

Our price £45.00 + £3.50 postage & packing. A professional standard five way speaker system with enclosure giving top quality performance

Enclosure Dimensions approx. (3 ft. √2 ft.' × 1 ft.). **Drive Units**

Hand built - 15" diameter bass with 3" voice coil. two 5" diameter Mid. Range units,

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Powder Handling Continuous rating

35 W rms., Peak power rating 70 W

Frequency Response 20 Hz 20,000 Hz.

EMI SPEAKERS FANTASTIC REDUCTION



15" 14A/780. Bass unit on a rigid diecast chassis. Superior cone material handles up to 50 watts RMS, and is treated to give a smooth frequency response Resonance 30 Hz flux density 360,000 Maxwells. Impedance at 1 kHz is 8 ohms, 3" voice coil.

Recommended retail price FAN RN OUR PRICE £18.70 + £1.50 p & p



crossover unit for handling up to 45 watts, frequency response from 20 to 20,000 Hz. Huge 19". 14" (approx.) high efficiency Bass-Speaker with 16,500-gauss magnet built on a heavy diecast frame.

The four 10,000 gauss tweeters, each 31" dia. approx., are fed by the crossover which critically adjusts signal for maximum fidelity. Impedance at 1 kHz is 8 ohms. Bass coil 2", others 0.5". Recommended list price £44-00.

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		N3403 N3404	0·19 0·24	40251	0.81	BC108 BC109	0·15	BCZ10	0.35		0.50
2G371 0	15 2	N3405	0.27	40310	0.50	BC113	0.13	BD115	0.75	BFY37	0.40
		N3414 N3415	0.10	40313	0.50	BC114 BC115	0·12 0·15		0.75		0.43
2N 404 0	43 2	N3416	0.15	40318	0.92	BC116	0.15	BD123	0.82	BFY50	0.65
2N456 0 2N456A 0	.75 2	N 3417 N 3570	0.21 1.25	40360 40361	0.46 0.48	BC116A BC117	0·18 0·21	BD124 BD131	0.67 0.40	BFY51 BFY52	0·22; 0·18; 0·20;
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2N491 3 2N696 0		N 3572 N 3702	0.97 0.11	40363	0.61 0.46	BC119 BC121	0.29 0.23		0.43	BFY56 BFY64	0·34 0·41;
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2N699 0	29 2	N3704 N3705	0·14 0·12	40406	0.44	BC126 BC132	0.20 0.30	BD139	0.63	BFY76 BFY77	0·22 0·24
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2N708 0-1	144 2	N3708	0.70	40409	0.52	BC136 BC137	0.15	BDY11	1.50	BRY39	0.28
		N3709 N3710	0·11 0·12	40410	0·52 2·25	BC137 BC138	0·15 0·24		1.50 1.75	BSX 19 BSX 20	0·13 0·20‡
2N718 0	·21 2	N3711	0.11	40414	3.55	BC140	0.34	BDY19	1.97	BSX21	0.20
2N720 0		N3712 N3713	0.96 1.20	40467 40468A	0.89 0.44	BC141 BC142	0.29		1.05 0.65	BSX26 BSX27	0.49
2N721 0	55 2	N 3714	1.38	40600	0-69	BC143	0.21	BDY60	0.85	BSX28	0.25
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2N930 0	48 2	N3790	2.40	40636	1.10	BC149	0.12	DESTITE	0-43	BSX77	0·15 0·20
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2N1132 0	54 9	N3794	0.10	AC113	0-16	BC154 BC157	0.14	BF119 BF121 BF123	0.27	BSY24	0.20
2N1302 0-1 2N1303 0-1	8 1 2 8 1 2	N3819 N3820	0·37 0·38	AC117 AC121	0.20 0.13	BC158 BC159	0·13 0·14		0.25	BSY25 BSY26	0·20 0·20
2N1304 0	24 2	N 3823	1.42	AC126	0.25	BC160	0.37	BF153	0.21	BSY27	0.15
	24 2 31 2	N 3824 N 3826	1·33 0·23	AC127 AC128	0.25 0.25	BC167B BC168B	0.13	BF154 BF158	0·16 0·23	BSY28 BSY38	0·15 0·19‡
	22 2	N3854	0.18	AC141K AC142K	0.30	RC168C	0.11	BF158 BF159 BF160	0.27	BSY39	0.191
2N1308 0- 2N1309 0-3 2N1483 0-	51 2	N3854A N3855	0.19	ACI51V	0.25	BC169B BC169C	0.13	B#161	0.411	BSY51 BSY52	0-25 0-25
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2N1613 0	33 2	N3856A	0.20	AC153K	0.25	BC172	0.11	BF167	0.21	BSY56	0.79
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		N 3900 N 3900A		ACY20	0.22	BC207 BC208	0·12 0·11	BF184 BF185	0·17 0·17	D40N3 GET111	0.55 0.45
2N2192 0	40 2	N3901	0.32	ACY21 ACY22	0.17	BC212K	0.10	BF194	0.16	GET113	0.25
2N2192A 0- 2N2913 0-	40 2	N 3903 N 3904	0.24	ACY28 ACY30	0.20	BC212L BC214L		12 F 1 Q 6	0·17 0·15	GET114 GET115	0·20 0·50
2N2193A 0 2N2194 0	61 2	N 3905 N 3906	0.24 0.27	ACY28 ACY30 ACY39 ACY40	0.651	BC237	0-09	BF197 BF198	0·15 0·18	GET119	0.35
2N2194A 0	.30 2	N4036	0.0%2		0.73	BC238 BC239	0.09	BF199	0.18	GETI20 GET535	0-40
2N2218A 0 2N2219 0		N 4037 N 4058	0·42 0·16	ACY44 AD136V	0.31	BC251 BC252	0.20	BF200 BF224J	0.40 0.14	GET536 GET538	0.20
2N2219A 0	88 2	N 4059	0.09	AD142	0.50	BC253	0.23	BF225J	0.19	GET873	0.12
2N2221 0	41 2	N 4060 N 4061	0·11 0·11	AD143 AD149V	0.45	BC257 BC258	0.09	BF237 BF238	0.22	GET875 GET880	0·15 0·35
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2N2222A 0	91 2	N4302 N4303	0-25 0-47	AD161 AD162	0·45 0·45	BC261 BC262	0-20 0-18	BF245 BF246	0.33 0.43	GET887 GET890	0·20 0·25
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2N2646 0- 2N2647 1-	12 2	N 4919 N 4920	0.84	AF114 AF115	0.25	BC302 BC303	0.29 0.54	BF257 BF258	0.47	TIP31A TIP32A	0.62
2N2711 0-	13 2	N4921	0.73	AF116	0.25	BC307	0.10	BF259 BF270	0.55	TIP33A	1.01
		N 4922 N 4923	0.84 0.83	AF117 AF118	0.20 0.50	BC307A BC308	0.08	BF270 BF272	0.21 0.53	TIP34A TIP35A	2.90
2N2714 0- 2N2904 0-		Nõ172 Nõ174	0.12	AF121 AF124	0.22 0.24	BC308A BC308B	0.12	BF273 BF274	0·15 0·17	TIP36A TIP41A	3·70 0·79
2N2904A 0-	70 2	N5175	0.26	AF125	0.20	BC309	0.10	BF457	0.53	TIP42A	0.80
2N2905 0- 2N2905A 0-	71 2 88 2	N5176 N5190	0.32	AF126 AF127	0·19 0·20	BC309A BC309B		BF458 BF821A	0.65 2.30	TIP2955 TIP3055	0.80
-2N2906 0-	65 2	N5191	0.95	AF139	0.38	BC327	0.21	BFS28	0.92	ME0401	0.18
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2N 2907A 0.	41 2	N5245 N5457	0-43	AF178 AF179	0.55	BC338	0.19	BFW11 BFX13	0.61	ME0411	0.17
2N2924 0-	14 2	N5458		AF180	0.65 0.50	BCY30 BCY31	0.43 0.51	BFX29	0.23 0.30	ME0412 ME0413	0·18 0·14
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2N3054 0	86 31	N143	0.75	AF 142 AL102	0.74 0.75	BCY43 BCY58	0.15	BFX86	0.25	ME4104 ME4101	0.11
2N3055 0- 2N3390 0-	26 31	N153	0.81	ASY26	0.70	BCY58 BCY59	0.21	BFX87 BFX88	0.28	ME4101 ME6102	0.14
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Rotary type 45: Singles (Log and linear) 15p. Single switched (Log and linear) 21p. Doubles (Log and linear) 38p. Slider type 58: Singles (Log and linear) 30p. Doubles (Log and linear) 50p.

Presets: 0.1 watt 6p, 0.2 watt 6p, 0.3 watt 7½p. Please

specify vertical or horizontal

Dio	des a	nd	Rect	ifier	S		
PIV	50	100	200	400	600	800	1000
1.5	8 p	9 p	10p	11p	12p	15p	20p
3	15p	17p	20p	22p	25p	27p	300
10		35p	40p	47p	56p		
35	84p	92p	£1.18	£2.15	£2.52	£3-65	£4-20
Cath	ode St	ud O	nlv				
IN376	6 (35A 8	300pv)	£3-65	IN3786	(35A I	000pv)	£4-20
IN34.4		BA14		BY237			7p

17p BYZ.1 12p BYZ.1 12p BYZ.11 17p BYZ.12 12p OA9 15p OA40 15p OA47 171p OA70 OA73 10p | BA141 7p | BA142 7p | BA144 7p | BA145 15p | BA154 15p | BY100 25p | BY126 25p | BY127 7p | BY140 35p OA81 35p OA81 30p OA85 30p OA90 10p OA91 20p OA95 7ip OA200 7ip OA202 10p OA210 IN914 IN916 80 10p 7p 7p 7p 7p AA119 AA129 BA100 BA102 BA110 BA115 10p

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	8/450V	18p	1000/25V	35p	32 + 32/25	OV	201
	16/450V			47p	32 + 32/45	OV	601
	32/500V		8+8/450V	22p	350+50/89	5V	55
	25/25V		8+16/450		16+16+	16/275V	45
	50/50V	100	16 + 16/45	0V 40p	100 + 50 +	50/350V	55
	100/25V		32 + 32/35				
	LOW VO	LTAGE	ELECTRO	LYTICS			
	1. 2. 4. 5.	8, 16,	25, 30, 50,	100, 200	mF 15V 10p		
•	500mF 1	2V 15	o: 25V 20p;	50V 30p			
	1000 W 1	OTT 00	OKT OF	KAST AN-	. 10017 70-		

500mF 12V 15p; 25V 20p; 50V 30p.
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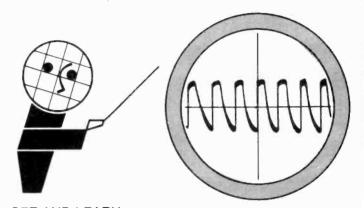
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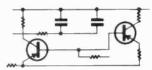
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RAPY



INSPIRING TIMES

F necessity be the mother of invention, we are now surely entering upon a period of prolificity in circuit creation and adaptation.

It is the amateur designer and experimenter who so often has the knack of hitting upon the right kind of solution to a sudden problem affecting everyday life. And problems there certainly are at this present time when restrictions in the use of electricity, if not complete cuts in the supply, affect all households; and soaring prices, if no actual shortage of petrol, make every motorist that more efficiency conscious.

This month's *Ingenuity Unlimited* includes a novel circuit devised by one of our readers and it is likely to be of interest to those with electrically controlled gas fired heating systems. A fore-runner, no doubt, of other crisis inspired ideas. We shall be happy, indeed consider it to be our duty, to publish other circuit ideas which may help overcome hardships or inconvenience experienced at home or on the road.

There already exist, of course, many circuits and systems that have relevance in the present difficult times. As a service to our readers we have prepared a special Blueprint for inclusion in this issue. It gives details for constructing two extremely useful and topical projects.

One side of this Blueprint carries details of the P.E. Scorpio Mk 2 Ignition System. The great success of the first Scorpio ignition system coupled with a continuing demand for copies of the original article made it quite clear that publication of an up-dated version would be highly welcomed; and in actual fact, could be a genuine service to the car owning public. The merits of the capacitor discharge ignition system are now well established, but they are, in any case, summarised in the article which complements the information given on the Blueprint.

The other side of the Blueprint is devoted to a design for a lamp inverter. Such devices are not by any means novel, but since design information may not be immediately to hand at the crucial moment, we expect a number of readers will appreciate the appearance of this useful design.

NEW PRICE

We ourselves, alas, are not immune from the effects of rising prices and shortages of raw materials, and we regret having to end this month with the following domestic note.

An apology is due to our readers for the lack of advance warning with regard to an increase in price of PRACTICAL ELECTRONICS. This increase to 25p takes effect as from this (March) issue. Unfortunately it was not possible to make an earlier announcement in this respect.

We trust all our readers will understand that the current high cost of materials, especially paper, makes this new price for P.E. unavoidable.

F.E.B.

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Editorial & Advertising Offices: Fleetway House, Farringdon St., London EC4A AD Phone: Editoria 01-634 4452 Advertisements 01-634 4202 PROBABLY the simplest rhythm generator is the old fashioned metronome. This device maintains the player's tempo but it cannot emphasise the down beat or create any special effects.

Down beat enhancement can be achieved electronically but for more entertaining rhythm accompaniment it is more satisfying to tie the output of an electronic metronome to electronic percussion generators in a selected sequence or rhythm pattern such as Waltz, Cha-cha, etc.

All commercially available switched rhythm generators have fixed rhythms which cannot be changed except by rewiring the switches. The generator to be described has no such limitations, it can produce any rhythm pattern of 16 pulses, for a total of 64,000 patterns, to be used to drive any one of eight percussion generators. Details for setting up the common rhythm patterns will be given.

Four time signature switches select 4/4, 3/4, 6/8 or 9/8 time for the 16 available pulses and when programming a rhythm pattern the pulse order can be monitored using a Minitron indicator. Because circuit layout is not particularly critical detailed constructional information has been omitted and instead use has been made of photographs annotated where necessary, to provide rudimentary guidelines for assembly.

BLOCK DIAGRAM

Fig. 1 shows the block diagram for the Rhythm Generator. The tempo generator is an assymetrical astable multivibrator. It will start when power is applied and run at all times from that point on. The frequency is controlled by the tempo control VR1.

The output of this generator is fed to a divide by four circuit. This expedient was used to keep the

size of the tempo generator components to reasonable levels and insure more reliable operation of that part of the circuit. The tempo generator runs then at an effective 64 beats per measure.

The four bit binary counter is used to generate 16 binary numbers which are decoded for the address information (storage address) and applied to IC6 for decoding and application to the Minitron indicator. IC5 decoding chip is used to supply reset pulses to the counter for 9 and 12 counts giving 9/8 time and 3/4 or 6/8 time respectively.

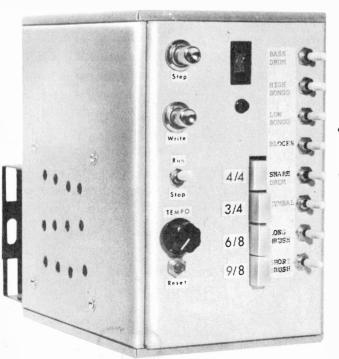
The step generator is switched to the input of the counter when the "Stop/Run" switch is placed in the "Stop" position. The divide by four output is removed at that time and the counter can be manually stepped from 0 through 15.

MEMORY CHIPS

The storage section for the programmed rhythms is made up of two SN7489, 64 bit bipolar memory chips (1C7/1C8). Each of these contains 64 flip-flops capable of storing a binary 0 or 1 (0 volts or 4 volts respectively). The particular group of four flip-flops selected per chip (eight for both chips) is controlled by the address lines which get their information from the counter. Thus 16 registers of eight bits each are available.

Each of these 16 registers is operated or selected in turn when the counter is running or being manually stepped and the contents of each can be controlled by the input switches to store either a binary 0 or 1. The actual output of each bit is inverted and is reoriented by the output gates, IC9/IC10.

Besides the address lines, input lines and output lines, there is a "chip select" and a "write" line.



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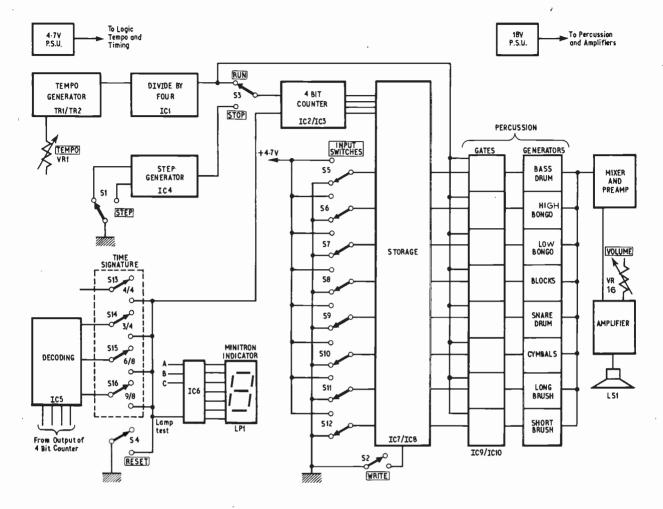


Fig. 1. Block diagram of rhythm generator

The chip select line is permanently grounded in this application because it simply makes the output available. The "write" line is used to write new information into storage when programming the rhythm generator. Setting the input switches as desired (S5 through 12) and pressing the "Write" switch will cause the new information to be stored,

otherwise, the input does not effect the condition of the storage locations.

The output of the instrument gates is controlled by the output of the storage section and the divide by four counter. The result is a positive pulse of voltage initiated when the counter changes state if, in the new count position, a "l" has been stored for that instrument.

- **# Rhythms can be programmed by the user**
- **# Eight percussion generators**
- Straight Can produce any 16 pulse rhythms up to 64,000
- * Four time signature switches for 4/4, 3/4, 6/8 or 9/8 measures
- **# Pulse order can be observed using a Minitron Indicator**

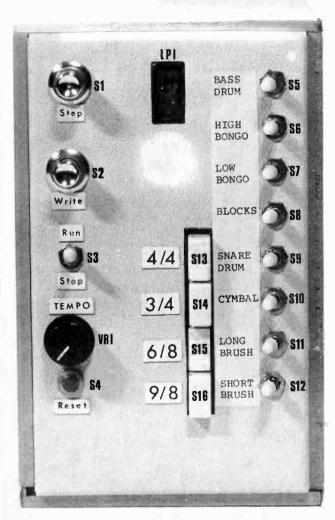
PERCUSSION GENERATORS

The percussion generators make use of various circuits to generate the sounds of drums, bongos and so forth.

The bass drum generator, for example, contains an input amplifier which converts the 5 volt input pulse to 18 volts, shapes it and applies it to a twin-T ringing oscillator. The circuitry for the bongos and blocks is similar.

The snare drum, cymbal and brushes make use of a noise diode the output of which is shaped and filtered, mixed with some basic frequency and applied to the mixer. The first four instruments are applied to a single f.e.t. stage. The final four are applied to individual fie.t. stages and the output of these five f.e.t.s is applied to a source follower as an output stage to the amplifier.

The output of the 18 volt power supply is regulated to reduce hum and noise while the 4.7V supply is held reasonably level with a Zener diode The volume control, VR16, is located on the back panel of the complete instrument.



COMPONENTS . . .

TEMPO, TIMING AND LOGIC

Resistors

R1 1k Ω

R2 22k Ω

R3 15k Ω R4 1k Ω

All 10% 1 watt carbon

Capacitors

0.01 µF ceramic 100V Č1.

C2 10μF elect. 25V

C3-C6 0.01μF polyester (4 off)

Integrated Circuits

ICT-IC3 SN7473 (3 off)

IC4 SN7400 1C5 SN7420

IC6 SN7447

IC7-IC8 SN7489 (2 off)

IC9-IC10 SN7402 (2 off)

Transistors

TR1-TR2 BC108

Switches

S1-S2 Single pole change over, break before make push-button.

S3 Single pole change over miniature toggle S4 Single pole change over, break before make push-button

S5-S12 Single pole change over miniature toggle (8 off)

S13-S16 Bank of four, four pole change over switches

All switches available from Home Radio

Potentiometer

VR1 250k Ω carbon lin.

Lamp

LP1 Minitron 3015F 7 segment indicator

Miscellaneous

Contil Mod 2B case (West Hyde Developments) 2 plug in Veroboards 5.1in x 3.744in, 0.1in matrix to suit 32 contact edge connectors, type B

POWER SUPPLY UNIT

Resistors

R5 7 Ω 2W

R6 270 Ω ½W

Canacitors

C7 2,000μF elect. 25V C8 1,000μF elect. 15V

Transistors

TR3 2N3054

Diodes

D1 ZL4·7 4·7V Zener 1W D2 ZL18 18V Zener 500mW

Bridge Rectifiers

D3-D6 MDA 942A1 Motorola

D7-D10 MDA 942A1 Motorola

T1 Pri-240V, Sec. 1 18V, 0·35A; Sec. 2 6·3V 0·7A (Henry's Radio)

Miscellaneous

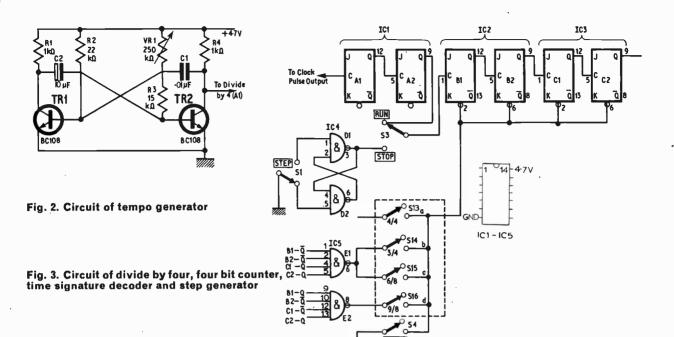
FS1-200mA cartridge fuse S17-Double pole main toggle switch

$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{lll} \textbf{Resistors} & & & & \\ \textbf{R94} & & & 4\cdot 7 \textbf{k} \ \Omega \\ \textbf{R95-R96} & & 22 \textbf{k} \ \Omega \ (2 \ \text{off}) \\ \textbf{R97} & & 1\cdot 2 \textbf{M} \ \Omega \\ \textbf{R98} & & 390 \ \Omega \\ \textbf{R99} & & 100 \textbf{k} \ \Omega \\ \textbf{R100} & & 68 \textbf{k} \ \Omega \\ \textbf{R101} & & 100 \textbf{k} \ \Omega \\ \textbf{R102-R103} & & 10 \textbf{k} \ \Omega \ (2 \ \text{off}) \\ \end{array}$
Capacitors C9 0.1μ F C10 0.02μ F C11-C15 0.1μ F (5 off) Potentiometers	C36 1μF elect. 15V C37 10μF elect. 15V C38 01μF	R104 2.2k Ω R105 150k Ω R106 82k Ω All ½ watt 10% carbon Capacitors
MDS SI O wildedness special	C42 1.5µF elect, 15V C43 500pF	C56 1μF elect. 15V C57 0·1μF C58 0.02μF
Transistors TR4-TR5 BC109	VR10 100k Ω miniature preset Transistors	C59 0-01 μF C60 2-5 μF elect. 15v C61 0-22 μF
HIGH AND LOW BONGOS Resistors	TR13-TR14 BC109 (2 off) Diodes D11 1N914	Transistors TR21-TR23 BC109 (3 off)
R19-R20 4-7k Ω (2 off) R21-R22 2-7k Ω (2 off) R23-R24 1M Ω (2 off) R25-R26 27k Ω (2 off) R27-R28 2-2k Ω (2 off)	D12 Z1J (Semitren) Inductor L1 OL130 transformer (Henry's Radio)	Diodes D16 1N914 D17 Z1J (Semitron)
R29–R30 6·8k Ω (2 off) R31–R34 56k Ω (4 off) R35–R36 1·2M Ω (2 off)	CYMBAL	MIXER AND PRE-AMPLIFIERS Resistors R107 4.7k Ω
R37–R38 68k Ω (2 off) R39–R40 100 Ω (2 off) R41–R44 82k Ω (4 off) All $\frac{1}{2}$ W 10% carbon	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	R108–R112 2·2k Ω (5 off) R113 10k Ω R114 2M Ω R115 10k Ω
Capacitors C16-C17 0·01μF (2 off) C18-C23 0·015μF (6 off) C24* 0·033μF (High bongo only) C25* 0·1μF (Low bongo only)	R72 680 Ω R80 10k Ω All $\frac{1}{2}$ watt 10% carbon	R116 2.2k Ω All ½ watt 10% carbon Capacitors C62-C66 0.01 μF (5 off)
C25* 0·1μF (Low bongo only) ΄ C26–C27 0·05μF (2 off) C28–C29 0·01μF (2 off)		C67 0·05μF Potentiometers
Transistors TR6-TR9 BC109 (4 off)	Transistors TR15-TR17 BC109 (3 off)	VR11-VR15 2-5M Ω miniature preset (5 off) Transistors
Potentiometers VR5-VR6 $5k \Omega$ miniature preset (2 off) VR7-VR8 $50k \Omega$ miniature preset (2 off)	Diodes D13-D14 1N914 (2 off) D15 Z1J (Semitron)	TR24-TR29 2N3819 (6 off) AMPLIFIER
BLOCKS	Inductor L2 OL130 transformer	Resistors R117 330k Ω R121 39k Ω R118 39k Ω R122 3·3k Ω
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	LONG BRUSH Resistors R81 4·7k Ω R88 100k Ω R82-R83 22k Ω R89-R90 10k Ω R84 1·2M Ω R91 2·2k Ω	R119 18k Ω R123 22 Ω R120 150k Ω R124 1k Ω All $\frac{1}{4}$ watt 10% carbon
All 10% ½ watt carbon Capacitors C30 0.1 µF C31-C33 0.002 µF (3 off)	R85 390 Ω R92 150k Ω R86 100k Ω R93 82k Ω R87 68k Ω All $\frac{1}{2}$ watt 10% carbon	Capacitors C68 0·1μF C71 0·1μF C69 0·002μF C72 50μF elect. 15V C70 500μF elect. 15V
C34 0·1 μ F C35 500 pF	$ \begin{array}{cccc} {\bf Capacitors} & {\bf C53} & 0.01 \mu {\rm F} \\ {\bf C50} & 4 \mu {\rm F} \ {\rm elect.} \ 15 {\rm V} \ {\rm C54} & 2.5 \mu {\rm F} \ {\rm elect.} \\ {\bf C51} & 0.1 \mu {\rm F} & 15 {\rm V} \\ \end{array} $	Potentiometer VR16 25k Ω
$ \begin{array}{ccc} \textbf{Potentiometers} \\ \textbf{VR9} & \textbf{50k} \ \Omega \ \textbf{miniature preset} \end{array} $	C52 0·02μF C55 0·22μF Transistors TR18-TR20 BC109 (3 off)	Integrated Circuit IC1 PA263 (Jermyn)
Transistors TR10-TR12 BC109 (3 off)	Diodes D16 1N914 D17 Z1J (Semitron)	Loudspeaker LS1 8 Ω, 5 watt 4in loudspeaker

SNARE DRUM

SHORT BRUSH

BASS DRUM



TEMPO GENERATOR

The circuit for the tempo generator is shown in Fig. 2. If the multivibrator capacitors were of equal value, the output would be a symmetrical square wave but C1 is 1/1000 the value of C2 creating a pulse of very short duration at a repetition rate determined largely by the value of C2. The output period is made variable by VR1 and gives a sufficient range of tempo to cover most requirements.

The output feeds a divide by four counter stage (IC1) composed of flip-flops A1 and A2 as shown in Fig. 3. The output of this counter is a symmetrical square wave with a period variable from 2 seconds to 25 milliseconds. This output is the basic timing waveform for the entire system.

FOUR BIT COUNTER

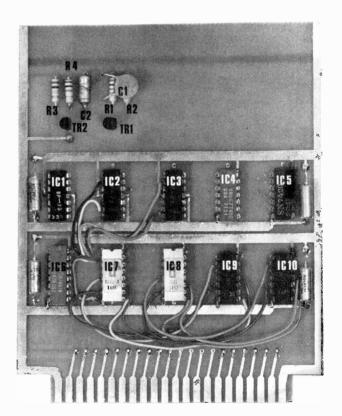
The four flip-flops labelled B1, B2, C1 and C2 (IC2, IC3) make up a four bit binary counter. Drive for this counter is obtained either from the output of the divider in the "Run" position of S3, the "Stop/Run" switch, or from the bistable latch (D1 and D2) in the "Stop" position. This allows the counter to be stepped through the count sequence manually with S1, the "Step" switch.

All four flip-flops can be reset by grounding the reset pins (2 and 6 of each chip). To reset the counter in the "Stop" position, the "Reset" switch S4 is pressed. This forces the counter to binary 0000.

In the 4/4 position of the "Time Signature" switch S13, the counter will count through 16 counts and automatically return to 0000. In the 3/4 and 6/8 positions, the counter must be forced back to 0000 after 12 counts.

This is done by applying the \overline{Q} outputs of B1 and B2 and the Q outputs of C1 and C2 to the input of NAND gate E1 (IC5). When this count is reached, the output of that gate will go immediately to 0 and the counter will be reset.

For 9/8 time, only 9 counts are allowed and the counter is then reset with NAND gate E2.



Prototype p.c.b. including tempo, timing and logic assembly. Four $0.01\,\mu\mathrm{F}$ capacitors must be included for decoupling the chip supply lines

STORAGE, OUTPUT AND INDICATOR

Fig. 4 shows the logic diagram for the storage, indicator and output gates. The four counter Q outputs from IC2/IC3 are applied to the A, B, C and D inputs of each of the memory chip address select lines.

S5 through S12 are the instrument input switches and S2 is the "Write" switch. The chip select inputs (pins 2) on both IC7 and IC8 are permanently grounded which simply means that the output will always be available.

The output of these storage or memory chips is applied to the inputs of eight NOR gates (IC9/IC10) and gated with the output of the divider IC1 to give a positive pulse out for each position and time segment that an instrument is to sound.

IC6 uses outputs A, B and C of the counter to decode the correct sequence of grounds to be applied to the Minitron indicator.

LOGIC ASSEMBLY

Although the prototype used plug-in printed circuit boards, 0·1in plug-in Veroboards can be successfully substituted for the logic and percussion circuitry.

While no constructional details are included sufficient information for this should be gleaned from the photograph of the prototype logic card showing the disposition of the tempo generator and logic chips. Note carefully the use of four $0.01\mu F$ capacitors connected between the supply and ground lines. These should be added to prevent spurious triggering.

Point to point wiring on the board should be carried out according to the circuit diagrams given. It really boils down to wiring between the i.c. pin numbers shown and taking off external wiring, such as to control switches and percussion generators, to those copper strips which will mate with the Veroboard's edge connector.

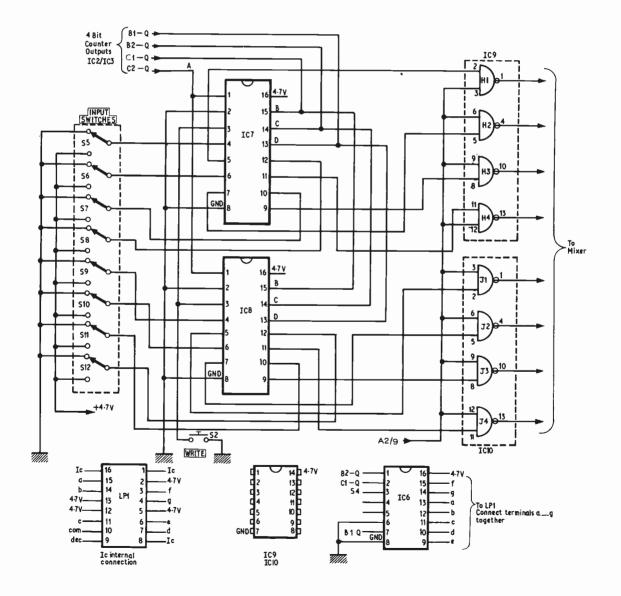


Fig. 4. Circuit for storage, lamp driver and percussion gates

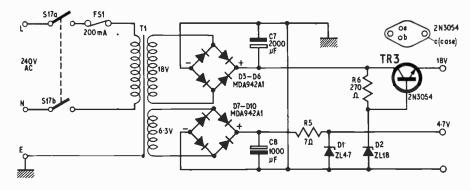
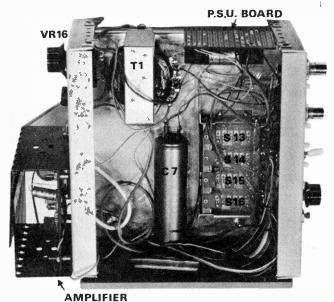


Fig. 5. Circuit of power unit



Part of the component assembly within the case. The amplifier is outboard mounted and the speaker con-

Once connections have been made and verified breaks in the copper should be made where appropriate. Finally check all wiring according to the circuits and make sure that there are no solder bridges or loose bits of wire around to cause future trouble.

POWER SUPPLY

nected to the removed plate

The power supply is made up on a $2\frac{1}{2}$ in \times $2\frac{1}{2}$ in, 0·15in matrix Veroboard. With the transformer and large electrolytic C7 these are all finally mounted on the Contil case chassis plate. With the wiring completed for this connect to the mains and ensure that the line output voltages are correct.

At this point it is a good idea to cut and drill those holes for the control panel switches and indicator. The locations for these are indicated in the photograph. The 4.7V power lines can now be connected to the logic board edge connector and the appropriate connections to the control panel switches made. A number of tests can now be made.

First plug in the board and switch on. In the "Stop" position of S3, press the "Reset" button. The Minitron indicator should show a figure eight. This is a lamp test feature and assures that all seven segments of the indicator work correctly. With the switch released the indicator should read 0. With S3 now in the "Run" position the Minitron indicator should go through 0 to 7 repetitively. The "Tempo" control can slow this process right down so that single digit changes can be easily observed.

If these tests are satisfactory, the unit is sound to this point. There are other tests that could be made but they would require additional instruments and are not really worth including.

Next month details for the percussion generators, mixer and amplifier will be given.

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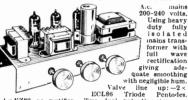
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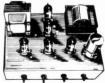
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Practical Electronics March 1974

FLIGRESCENT



NO INVERTER By C. J. MILLS

High efficiency light source from a 12V d.c. supply

VITH power cuts an annual recurrence the construction of an inverter to drive a fluorescent lamp from a 12V d.c. supply, such as a car battery, is a worthwhile investment.

Although one basic circuit is described, with minor component changes the inverter is capable of driving either an 8W, 13W or 20W lamp.

HIGH FREQUENCY OPERATION

The choice of an operating frequency above 20kHz for the inverter means a reduction in transformer size, increased lamp efficiency and the elimination of audible whistles.

The unit incorporates transistor protection against lamp removal by automatically stopping the oscillator. Diode protection against supply polarity reversal is also included.

CIRCUIT DESCRIPTION

The circuit shown in Fig. 1 is developed from the well-known Hartley oscillator. The primary winding of the pot core transformer T1 is in the emitter circuit so that the collector of the transistor TR1 can be earthed. This arrangement means that the feedback winding must give a greater voltage than the primary winding and therefore has more turns.

The feedback winding provides the drive to the transistor base via a limiting resistor R1, one of the lamp heaters and C3.

The voltage across the secondary winding is sufficient to strike the tube and the leakage inductance in conjunction with the base resistor limits the tube running current. This is necessary because the fluorescent tube tends to maintain a constant voltage.

Heater current for the tube is provided at one end by the drive current and at the other by a few extra turns on the secondary winding. The bypass capacitor across the transistor limits the peak collector emitter voltage to a safe value. This is not normally required in the 8W version.

POSITIVE AND NEGATIVE EARTH

If the circuit is being constructed in a separate metal case and used with a positive earthed supply system the transistor can be mounted directly on to the case. If the supply is negative earthed a mica washer and plastic bushes should be used to insulate the transistor which should be protected from possible shorts to earth by a plastic cover.

The circuit board should now be cut and drilled to fit the case and the components mounted as shown. The transformer leads can be connected to the printed circuit via pins and further pins can

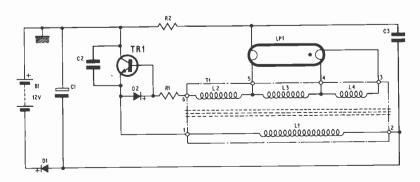


Fig. 1. Circuit diagram of fluorescent lamp inverter

be used for connecting leads to the transistor and the fluorescent lamp.

When the wiring-up is completed the circuit should be carefully checked before it is connected to the voltage supply to ensure that both diodes and the transistor are connected the right way round and that copper breaks in the Veroboard have been cleanly cut and that there are no shorts between strips due to surplus solder.

TESTING

Testing should start with a low voltage battery or a gradually increasing voltage supply with a series ammeter to check that the current consumption is not excessive and that the transistor is not overheating.

The fluorescent tube must be connected to complete the bias circuit and if the circuit is oscillating a glow will be seen from the heaters at the ends of the tube. When the full voltage is applied the lamp should strike and light up but during preliminary testing the lamp will strike easier if a fine wire is stretched between the metal end caps and connected to one of the heater pins.

If the circuit does not oscillate L1 may be reversed or there may be some shorted turns in the transformer. When operating normally with a 13 watt tube this inverter consumes about 1-4 amps at 12 volts. This current and the light output can be varied slightly by small adjustments to R1 and/or C3.

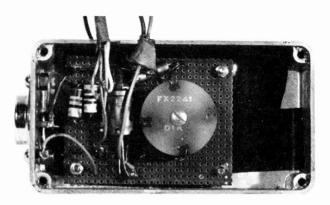
PRECAUTIONS

All metal parts, including the metal end caps on the tube, should be earthed and the fine wire connected to the heater pin during tests should be removed. The voltage across the tube is high enough to provide a nasty shock and should be treated with respect.

TRANSFORMER WINDING

The winding order is identical for the 8 watt, 13 watt or 20 watt versions of the inverter. Start by winding the primary L1 on the bobbin according to the relevant data given in the Components List. Lead ends on each coil should be colour coded for later identification.

Insulate with plastic adhesive tape and then add L2 again insulating the winding with tape. Finally



Interior assembly of 13W inverter

add L3 and L4. The direction of winding for all coils is the same.

Before bolting the two halves of the Ferroxcube pot core together onto the Veroboard, two paper spacing washers should be cut and fitted between them.

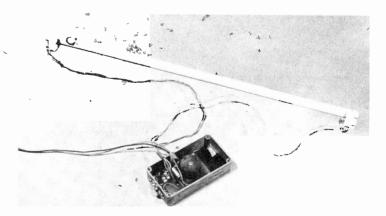
CONSTRUCTION

The Ferroxcube transformer and majority of circuit components are mounted on a $2\text{in} \times 2\frac{1}{2}\text{in}$, 0-1in matrix Veroboard with the transistor connected to case.

The mounting of the fluorescent lamp will depend on the application and to a certain extent on the constructor's preferences. For example an 8 watt tube can be used in a caravan mounted flush with the roof and components separate or on a channel support with the components mounted in the channel.

Alternatively an attractive table or hanging lamp can be constructed with the fluorescent lamp in a vertical Perspex tube with the components in a suitable case at one end of the tube.

Another idea is to construct a portable lamp using two 6V lantern batteries in a suitable case with the lamp and reflector mounted on the outside. Leads can then be connected via a plug and socket for external battery supplies such as a car battery. This makes an ideal camping light but the lantern batteries should be isolated from the car battery by diodes or a switch.



The 13W inverter with output leads terminated with clips and lamp

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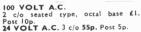
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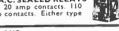
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SKYLAB-LAST MISSION

As this is being written the last Skylab mission planned before the Soviet-American rendezvous space, is not quite half way through. The longest single mission of three astronauts will bring to an end the triple series of scientific pro-

grammes.

By whatever standards these experiments may be judged they represent one of the major events in the history of the solar system. Some may regard the Skylab project as more important than the Apollo programme. Certainly, a very comprehensive coverage of observation (and running repairs) will add much to the data so far amassed. It must not, however, be forgotten that side by side with the success story go some rather disquieting happenings.

It is intended that the return of the team will be in early February. However, at the time of writing, there are possibilities that there could be an earlier termination because of certain disciplinary reactions. Perhaps it is to be a blessing, if seen in the broad context of advanced technology.

The problems that have arisen are twofold. There have been technical difficulties and some personnel problems. None of the present crew have flown in space before and this could to some extent explain the behavioural problems.

CREW CONCERN

Mission Control have been concerned about the crew in that they suffered from motion sickness for several days and attempted to conceal this from the physicians moni-toring the flight. Perhaps this is understandable since they would be worried about being recalled. On the other hand there were other signs such as proneness to error and poor disposition.

Their sleep sessions have tended to be longer than was thought to be required, compared with the previous crews. They have been moody and temperamental when in contact with control and have complained somewhat bitterly about their workload. Refusal to come in from extra vehicular activities has seemed to show a somewhat towards antagonistic attitude

instructions.

The consequences on their work has been very noticeable. The most serious error has been in relation to the operation of the cameras during observation passes of the Earth. The proper filters to six cameras were forgotten. Much of the film will be useless though some may be recoverable using certain



special techniques when they are returned to base.

The medical unit in charge at control will be seeking an answer to these rather irrational episodes. Despite this however, it cannot detract from the remarkable Skylab

project.

Some of the technical problems have been concerned with the gyroscopes. One of these has been out of use since the end of November. The other has tended to show a slowing down. Normally it would have a revolution of 8,200 per minute. It slowed by 14 revolutions and then by a further 10 per minute. This is quite serious and should it continue to fall then the mission could well be curtailed.

PIONEER 10 AND JUPITER

Some of the vital statistics so far recorded during Pioneer's mission to Jupiter have confirmed previous thinking. The magnetic field for example is recorded at 4 gauss. In a recent "SPACEWATCH" mention was made that Dr C. H. Barrow had used a figure of 9 to 10 gauss. Re-examination of his previous papers can now lead to some constructive theories.

The off-set magnetic field confirms Warwick's claim made several years ago. The higher level of the radiation belts has also been confirmed. It is also confirmed that Io has an ionosphere. This supports the earlier data that Io has an influence on the decametre radiation from Jupiter.

It will be some time yet before the accumulated data is to hand for distribution.

Perhaps another important point that might be made is the fact that so far the 8W transmitter has ful-

filled its task admirably. It remains to be seen (heard?) how far out it will continue to supply data.

One further important develop-

ment is that it is now quite definitely confirmed that there are hazards to control, in the magnetosphere of Jupiter. There is the possibility of random effects giving the same sort of command signal to the vehicle.

The case of far out probes such as Pioneer 10, introduces the long time period of signal travel. That is 45 minutes out and 45 minutes back. This could be much too long to counteract false signals. To overcome this a method of repeating commands every 30 minutes is being used. By this means the risks are minimised.

MOON AS A STANDARD LAMP

Dr J. Linsky of Boulder, Colorado, has made use of data obtained from the Apollo missions and the study of the lunar soil, to set the moon as a standard of comparison for infra-red and microwaves.

The average values have been studied and Linsky's results have shown an accuracy of 4 per cent for wavelengths between 10 micrometres and 1 metre. By averaging the radiation between successive new moons he arrived at a figure for radiation over a lunar day for the central part of the moon's disc. It is possible to use this standard to calibrate the sun and parts of the galaxy.

Linsky is able to fix the brightness at an order of magnitude better than with other methods. Possibilities of a better study of the chromosphere are therefore indicated and perhaps a better view of how the heat transfer shock waves operate.

QUASARS

The see-saw of opinion continues to operate in the controversial field of quasars. In spite of this there is growing confirmation of the claims of the radio astronomers that these are far distant rapidly receding objects.

Recent new work has offered a new dilemma for theorists since in one particular case the observers faced with deciding as to whether, in certain cases, the quasar is in fact way beyond its apparent position relative to a galaxy or whether Hubbles law is in doubt

in such cases.

It still leaves the position largely as before, that of all the new discoveries of other sources such as pulsars, black holes, X-ray stars, etc., the quasar remains the most mysterious. Near or far as to position still remains in doubt when looking at the overall picture.

One advantage of inserting a resistor in series with the source is that the slope resistance of the device is increased. This is because a change in channel current causes a change in the voltage across the resistor which alters the reverse bias on the gate. Obviously, for a given change in current, the voltage change is proportional to the resistance in series with the source.

HIGH SLOPE RESISTANCE

In applications where a very high slope resistance is required, the circuit shown in Fig. 7 can be used. In this circuit, the source resistor is replaced by an f.e.t. current generator which provides a high slope resistance in series with the source of TR1.

For proper operation, the cut-off voltage V_p of TR1 should be greater than that of TR2. The slope resistance can be increased by one or two orders of

magnitude using this technique.

The temperature coefficient of drain current depends on the value of drain current, being negative at high currents and positive at low currents. At an intermediate value of drain current $I_{D(0)}$, the two effects causing these changes cancel and the temperature coefficient is approximately zero. The current at which this occurs is given approximately by:

$$I_{\mathrm{D}(0)} = rac{0.4}{V_{\mathrm{p}^2}} imes I_{\mathrm{DSS}}$$

y AND h PARAMETERS

It is often convenient to refer to the characteristics of transistors by means of y or h parameters. There are four h and four y parameters for each of the three basic transistor connections.

The four y parameters describing a transistor operating in the common emitter configuration are: y_{1e} , y_{1e} , y_{1e} , y_{1e} , y_{1e} , and y_{0e} . The second subscript letter "e" refers to the fact that the transistor is in the common emitter connection. Similarly, "b" denotes common base, "s" denotes common source, etc. The first subscript letters refer to input, forward transfer, reverse transfer and output parameters respectively.

Each "y" parameter is the ratio of a current to a

voltage. Thus:

y_{1e} is the input admittance (the ratio of input current to input voltage);

yre is the forward transfer admittance (the ratio of output current to input voltage);

yre is the reverse transfer admittance (the ratio of input current to output voltage);

yoe is the output admittance (the ratio of output current to output voltage).

Whereas y parameters are all ratios of currents to voltages, different h parameters represent ratios of different quantities. Thus:

 h_{1e} is the input impedance (the ratio of input voltage to input current);

 h_{fe} is the forward current transfer ratio (the ratio of output current to input current);

 h_{re} is the reverse voltage transfer ratio (the ratio of input voltage to output voltage);

 h_{oe} is the output admittance.

Although common emitter parameters have been quoted, the definitions are also valid for other connections.

Of the six possible sets of parameters, only h and y parameters are widely used in transistor circuit analysis. If one set of parameters is known, any other set can be calculated quite easily. This means that the choice of parameters for a given application is largely a matter of convenience.

The characteristics of bipolar transistors are usually described by h parameters and those of field effect transistors by y parameters.

BIPOLAR TRANSISTORS

A bipolar transistor in either the common base or common emitter configuration can also be used as a constant current source as shown in Fig. 8. Since the collector-base junction is a reverse biased diode, the current through it is only slightly affected by the voltage across it.

The slope resistance in the common base connection is $(h_{te} + 1)$ times larger than the slope resistance in the common emitter connection. The difference between common base and common emitter circuits lies in the resistances in series with the base and emitter

leads.

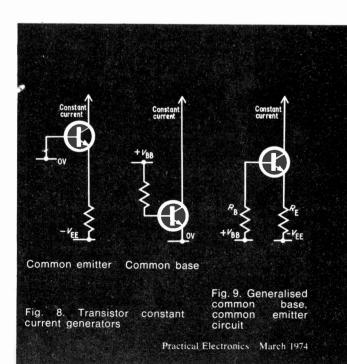
The circuit in Fig. 9 is a generalised common base or common emitter circuit. If $R_{\rm B}=0$ and $R_{\rm E}=\infty$ the slope resistance is equal to the reciprocal of the low frequency common base output admittance $h_{\rm ob}$. In practice, provided that $R_{\rm E}$ is more than a few kilohms, the slope resistance is not appreciably less than this value. If $R_{\rm B}=\infty$ and $R_{\rm E}=0$, the slope resistance equals $1/h_{\rm oe}$. Then $h_{\rm oe}$ and $h_{\rm rb}$ are related by the equation:

$$h_{\mathrm{oe}} = h_{\mathrm{ob}} \times (h_{\mathrm{fe}} + 1).$$

With intermediate values of $R_{\rm B}$ and $R_{\rm E}$ the slope resistance lies between these two values. For a BC108, $h_{\rm ob}=10^{-7}\mu{\rm S}$ and $h_{\rm oe}=3\times10^{-5}\mu{\rm S}$.

The circuit of a simple transistor constant current generator is given in Fig. 10. The base voltage is set to 4V by the potential divider across the supply.

Since the BC184 is a silicon transistor, the emitter voltage is about 3.4V. Thus the emitter current is $3.4V/6.8k\Omega = 500\mu A$ and since $\alpha \simeq 1$, the collector



current is also about $500\mu A$. Because the emitter resistance is $6.8k\Omega$, the slope resistance of this current source is very high. The knee voltage is about 4V.

The major disadvantage of the circuit in Fig. 10 is that the current is approximately proportional to the supply voltage. To produce a more stable current source, R2 is often replaced by a Zener diode so that the base voltage, and hence the emitter voltage, is less affected by supply voltage variations.

The temperature coefficient of this source depends on the temperature coefficients of the Zener diode and the base-emitter junction. If a Zener of about 4V is used, the temperature coefficients will cancel.

IN INTEGRATED CIRCUITS

Fig. 11 shows the circuit of an interesting transistor current source which is often used in integrated circuits. In this circuit, the base current for the transistor is supplied by part of the current through the resistor. The remainder of the current from the resistor flows through the diode.

In an integrated circuit, since all the transistors and diodes are produced simultaneously on the same chip of silicon, the diode can be made identical to the base-emitter junction of the transistor. Because the diode and the base-emitter diode are connected in parallel, the voltages across the two are equal. Since the two diodes have the same characteristics, the currents through them $(I_D$ and I_E) are also equal.

The current through the diode comes entirely from the resistor but the emitter current in the transistor is provided partly by the resistor and partly by the collector circuit. In other words,

$$I_{\rm D} = I_{\rm E} \\ = I_{\rm C} + I_{\rm B}$$

The base current of the transistor is about one per cent of the emitter current and can be neglected. With this assumption, it can be seen that the collector current of the transistor is equal to the current flowing through the diode. Because the base current is small, almost all of the current flowing through the resistor

flows into the diode so that the collector current of the transistor is approximately equal to the current in the resistor.

Circuits of this type have very low knee voltages, typically less than 0.5V. This circuit also has a very low temperature coefficient because the diode and transistor have equal temperature coefficients of voltage which cancel each other.

The breakdown voltage of a transistor current generator can be anything from 15 to 500V depending on the transistor employed.

SOPHISTICATED CIRCUITS

There are several more complex constant current circuits available which are used where high stability is required. The ring-of-two circuit shown in Fig. 12 is often used as a precision current generator. It is a two-terminal current source because, unlike the transistor circuits described above, no extra supply voltage is necessary.

The operation can be understood if it is considered as two constant current sources, the first consisting of D1, R1 and TR1 and the second containing D2, R2 and TR2. These sources are connected so that each one supplies a constant current to the Zener diode of the other. The knee voltage of the ring-of-two is rather high, and is equal to the sum of the Zener voltages of D1 and D2.

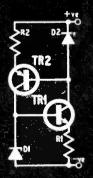
Just as it is possible to construct regulated voltage power supplies, so regulated current supplies can be made.

The current is usually measured by passing it through a resistor and comparing the voltage thus produced with a reference voltage to derive a control signal. This signal is then applied to a bipolar transistor or an f.e.t. which controls the current. A block diagram for such a scheme is shown in Fig. 13.

In the concluding part of this article next month, practical applications of constant current sources will be described.



T_D OV X_E



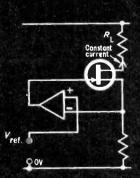
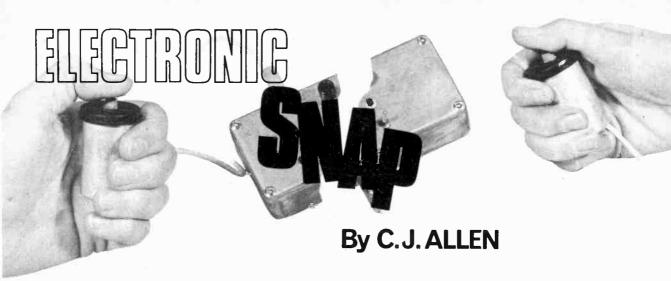


Fig. 10. Simple transistor constant current source

Fig. 11. Matched diode transistor constant current source

Fig. 12. Ring-of-two constant current generator

Fig. 13. Stabilised current power supply



HERE are many games in which contestants' reaction times play a vital part; "snap" is an obvious example and a guessing game where the first contestant to press a button is allowed to answer is another. This simple unit has two push buttons and gives a positive indication (by lighting a lamp) of the button which is pressed first.

CIRCUIT DESCRIPTION

The circuit of the Electronic Snap is shown in Fig. 11. It makes use of a single digital integrated circuit type SN7400 which is available for less than 20p. The indicators used are light emitting diodes which are simply diodes which emit light when forward biased

The SN7400 contains four NAND gates. A NAND gate is one whose output will only go to logic 0 if both inputs are logic 1. They are cross-coupled in the circuit so as to form two bistables, circuits which

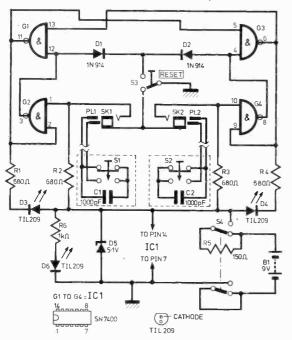


Fig. 1. Circuit diagram of the Electronic Snap

COMPONENTS . . .

Resistors

R1-R4 680Ω (4 off) R5

150 Ω R₆

1k Ω

All ±10% ¼W carbon

Capacitors

C1, C2 1,000pF polystyrene (2 off)

Diodes

D1, D2 1N914 or any general purpose silicon

diode (2 off)

D3, D4, D6 TIL209 or similar light emitting diode (3 off)

D5 5·1V 400mW Zener diode

Integrated Circuit

IC1 SN7400N Quad 2-input NAND gate

Switches

S1, S2 Push to changeover (1 pair normally

closed, 1 pair normally open) (2 off)

Push to changeover

S4 Miniature d.p.d.t. toggle

Miscellaneous

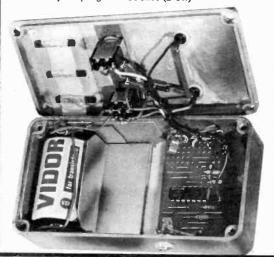
B1 9V PP4 battery

0 1in matrix Veroboard 2in \times 1½in

Diecast box $4\frac{1}{4}$ in \times $2\frac{1}{4}$ in \times 1in

35mm film cases (2 off)

3.5mm jack plug and socket (2 off)



are stable in either of two states. When the reset button is pressed inputs to gates G1 and G3 are taken to logic 0 (less than 0.8V) through diodes D1 and D2. The outputs of G1 and G3 must go to logic 1 regardless of the state of pins 13 and 5.

Switches S1 and S2 are open so the inputs on pin 1 of G2 and pin 10 of G4 are logic 1. Because the outputs of G1 and G3 are logic 1 it follows that all inputs to gates G2 and G4 are logic 1 so their outputs go to logic 0. The circuit will stay in this state even when S3 is released.

Assume S1 is now pressed. One input to G2 goes to logic 0, the output goes to logic 1 causing the output of G1 to go to logic 0 which, in turn, causes l.e.d. D3 to conduct and light up. Pin 5 of G3 is now held at logic 0 so even if S2 is pressed causing the output of G4 to go to logic 1 the output of G3 will stay at logic 1 keeping l.e.d. D4 off.

POWER SUPPLY

Power for the circuit is provided by a nine volt

battery which is dropped down to the five volts required by the integrated circuit by the 150 Ω resistor R5 and Zener diode D5.

One point that may be noticed is the connection of switches S1 and S2. These are not connected so as just to ground the inputs to G2 and G4 but to provide a very short pulse which is enough to take the inputs to logic 0 but will not drain the battery if the switches are held down.

The switches are connected as changeovers and the very short interval during which the capacitor charges is enough to momentarily take the output to ground.

CONSTRUCTION

The bulk of the circuit is built on a small piece of Veroboard as shown in Fig. 2. Jack plugs are used to connect the switches to the main unit. The switches are mounted in 35mm film cases and the capacitors C1 and C2 are mounted on the switch contacts.

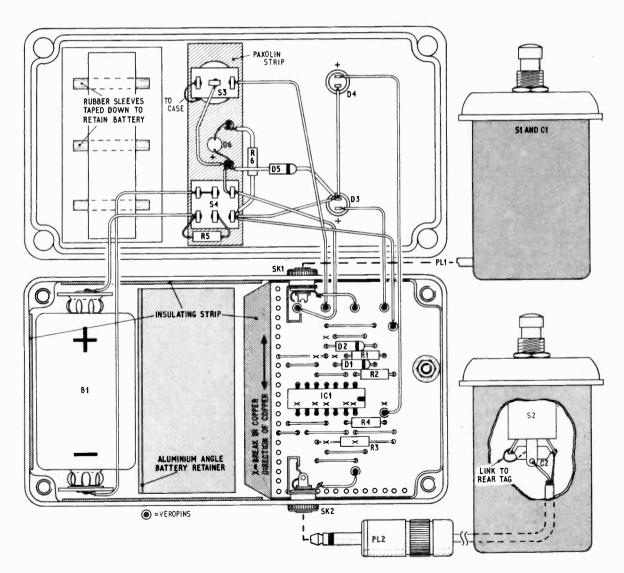


Fig. 2. Layout of the components on the Veroboard and front panel, and interwiring details

SGORPIO MK.2 IGNITION SYSTEM

By D.S.GIBBS & I.M.SHAW

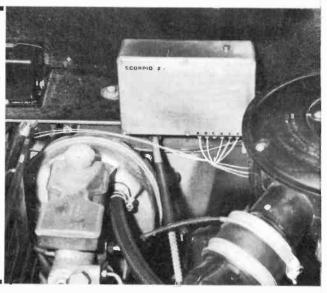
Since publication of the original Scorpio ignition system, about two and a half years ago, many requests have been received for a six volt version for use on cars and motor cycles with six volt electrical systems.

It is, unfortunately, impractical to build a unit to operate on both 6V and 12V, so two units have been designed with differing component values, and a number of improvements have been made to reduce radio interference and improve tachometer triggering. Both units give substantially the same performance and can be used on either positive or negative earth cars by altering a few connections.

PERFORMANCE

There has been a tremendous rise in interest in capacitor discharge ignition systems over the past few years and their advantages are now widely recognised. The main features are:

- (a) Easier starting from cold. The higher spark voltage and faster rise time enables it to fire wet or oiled up plugs. The electronic system can deliver twice the spark voltage of the conventional system into a load of 470kΩ and 40pF—simulating a badly fouled plug.
- (b) Smoother running at high speeds. Fig. 6 shows how the electronic system maintains an almost constant spark voltage up to 12,000 r.p.m. for a four cylinder engine (8,000 r.p.m. for six cylinder). This promotes better combustion at high speeds, eliminating misfiring and reducing the level of pollutants in the exhaust.
- (c) As a result of the improved combustion there is a small improvement in power and fuel economy.
- (d) The contact breaker will remain correctly adjusted for up to 20,000 miles. This keeps the car electrically "in tune", with a consequent improvement in fuel economy.
- (e) Spark plug wear is reduced. In the conventional system the spark current is unidirectional and causes deposition of metal from one electrode to



the other. In the electronic system the spark current is bidirectional and of much shorter duration. This increases spark plug life and reduces the need for adjustment.

CIRCUIT DESCRIPTION

The circuit of both 12V and 6V versions is the same and is shown in Fig. 1. Transistor TR1 is not required for positive earth operation but it can be left in circuit if desired. This will enable the unit to be used on either positive or negative earth cars merely by changing a few connections.

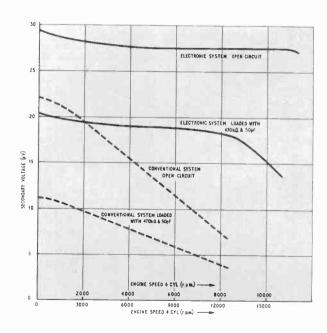


Fig. 6. Graph showing the variation of output voltage with engine speed for conventional and capacitor discharge systems

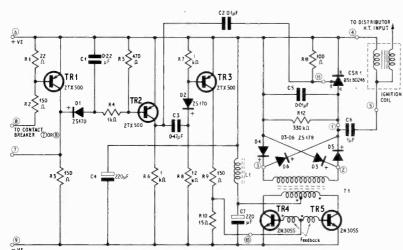


Fig. 1. Circuit diagram of the 12V version of the Scorpio Mk 2 capacitor discharge ignition system.

Refer to blueprint for full constructional details

Please note: R12 should be 1W (both versions).
TR3 (6V) should be BFS97 or

ZTX550.

The circuit operates as follows (assuming negative earth operation with tag 9 earthed and the contact breaker connected to tag 8):

With the contact breaker closed TR1 is saturated and its collector voltage is close to the positive rail. When the contact breaker opens TR1 turns off and C1 is rapidly charged by R3 and diode D1. This brings TR2 hard on, its collector voltage rises to the positive rail and this positive pulse fires the thyristor CSR1. At the same time TR3 is reverse biased by C3 and remains cut off for about 0.3 milliseconds. This removes the bias from the inverter and prevents the thyristor from latching on.

When the contact breaker points close again TR1 turns hard on, but TR2 remains on for about 0.3 milliseconds—until C1 has discharged through R4 and R5. This effectively prevents contact bounce from retriggering the thyristor at the wrong time. Further noise immunity is provided by C2 and C3, which take about one millisecond to recharge fully after TR2 turns off.

Transistors TR4 and TR5, with the ferrite cored transformer TI, form a very efficient push pull inverter oscillating at about 2kHz. The 400 volt a.c. output is rectified by diodes D3 to D6 and charges up the energy storage capacitor C6 in about 1.5 milliseconds. When the thyristor fires this charged capacitor is thrown directly across the primary of the ignition coil. The primary voltage immediately rises to 400V and this is stepped up to 20 to 30kV at the secondary, forming an arc between the plug electrodes.

CONSTRUCTION

The unit is constructed in a $7\frac{1}{4}$ in $\times 4\frac{1}{2}$ in $\times 2$ in diecast box, which acts as a heatsink for TR4, TR5, and the thyristor. Most of the other components are mounted on the printed circuit board shown in Figs. 2 and 3.

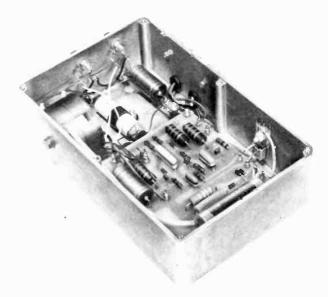
Connections to the board are made via turret tags, or the wires can be soldered direct to the board. If turret tags are used they should be expanded with a centre punch after insertion, to lock them in place, and then soldered.

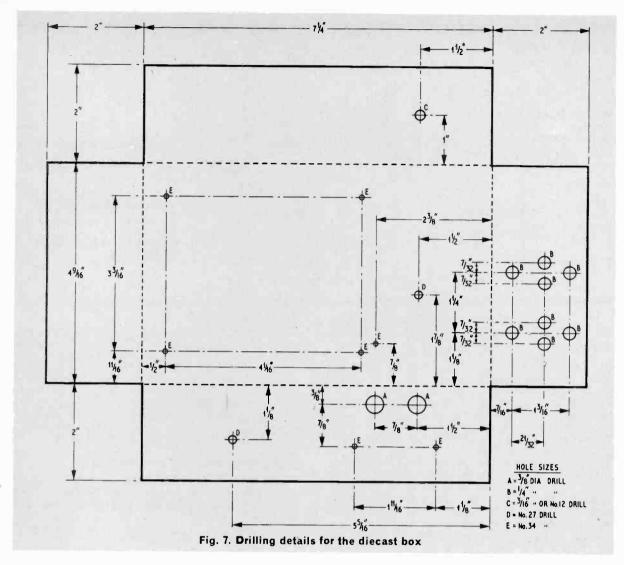
COMPONENTS

The diodes, transistors and resistors are all readily available. Capacitors C1 to C3 are not critical but Mullard type C280 miniature foil types are used in the prototype. The 1µF 440V a.c. rated capacitor (C6) is available from many of the advertisers in P.E. The Siemens thyristor is available from A. M. Marshall and Electrovalue who also supply the Siemens pot core. The address of a supplier for the printed circuit board is shown in the components list. The total cost of the unit is around £8.50.

TRANSFORMER CONSTRUCTION

Details of suitable cores and bobbins are given in the parts list and winding details in Fig. 4. Both types are very similar and give substantially the same perormance.





12V version

First wind on 400 turns of 34 s.w.g. enamelled wire in eight neat layers—taking care not to cross adjacent turns. Insulate the lead out wires with thin sleeving and insulate the whole winding with four turns of thin insulating tape. Then wind on 12 + 12 turns of 20 s.w.g. bifilar (i.e. two wires wound together), and lastly 3 + 3 turns of 30 s.w.g. bifilar. Put coloured sleeving on the wires for identification and to protect them from abrasion against the core and insulate the whole coil with several more turns of insulating tape.

It is a good idea to join the two ferrite cups with a very thin smear of Araldite to prevent the core from making an objectionable whine, but test the transformer before doing this as it will be impossible to separate the core afterwards.

6V version

As above, but with a secondary of 300 turns of 34 s.w.g., a primary of 6 + 6 turns of 18 s.w.g. and a feedback winding of 3 + 3 turns of 30 s.w.g.

ASSEMBLY

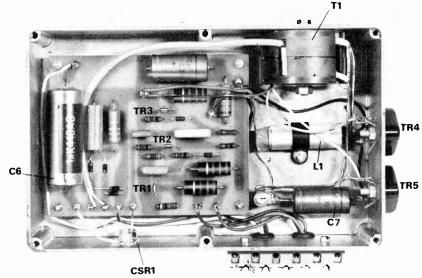
Drill the box as shown in Fig. 7, taking special care to deburr the holes for TR4, TR5, and the thyristor. Mount TR4 and TR5 with mica washers and insulators as shown in Fig. 5 and the transformer Tl with a 2BA bolt and spring washer. The stand-off insulator, and capacitor C7 can now be fixed in place and most of the inverter circuit wired up. Filter Ll is fixed with a ½in "p-clip" bolted to the case.

Assemble the printed circuit board and mount with 6BA bolts and \(\frac{1}{2}\) in spacers. Then mount the thyristor with a mica washer and a 4BA nylon bolt. It should be possible to solder the gate and cathode leads of the thyristor directly to tags 11 and 4 respectively on the printed circuit board.

It is advisable to fix down the large capacitor C6 either by tying or by gluing as the considerable vibration puts a great strain on the capacitor leads.

Wire up the circuit as shown in Fig. 5 with 14/0076 connecting wire and mount a six-way 5 amp connector block on the outside of the box for the external connections. Fit two plastic covers to the power transistors to prevent accidental short circuits.

Photograph showing the completed Scorpio Mk 2 ignition system



TESTING

Before the unit is installed in the car a few simple tests should be performed to ensure that it

is operating correctly.

Temporarily disconnect the anode of the thyristor and connect the car battery to terminals E and F on the connector block, via a 2 amp fuse. The unit should be heard to "sing" immediately and 400V d.c. should appear between tags 1 and 4 on the p.c.b. (6 volt system—300V).

If the inverter has been wired incorrectly it will probably fail to oscillate at all, but if one base winding has been connected the wrong way round the inverter can oscillate on one transistor only. Under these conditions high voltage spikes are produced and up to 800V may appear across tags 1 and 4.

INSTALLATION

Positive earth

The wire or wires connected to the SW or "—" terminal of the ignition coil should be connected to terminal F on the unit instead, and the SW terminal of the coil connected to terminal A. Connect the CB or "+" terminal of the ignition coil to B, the contact breaker to C, and a good earth from the car body or the positive battery terminal to E.

Negative earth

Disconnect the wire or wires to the "+" terminal of the ignition coil and connect them instead to E on the unit. Connect the "+" terminal of the coil to B and the "-" terminal of the coil to A. Connect the contact breaker to D and a good earth to F.

Cold start coils

Some cars are fitted with a cold start coil, consisting of a low voltage coil with a series ballast resistor. The ballast resistor is usually connected to one of the terminals of the coil, but may take the form of a resistance cable. It does not make any significant difference to the spark produced by the unit if the resistor is left in series with the coil, but ensure that the supply current for the unit does

not flow through the resistor as there will then be a considerable loss of voltage. In all cases the connection between the starter solenoid and the coil must be removed.

SEALING .

When the unit is completed and tested and operation is satisfactory the box should be waterproofed to prevent any dampness getting into the electronics. This can be done either using ignition system waterproofing aerosol available under names such as W.D. 40 or "Coldstart", or bath caulking compound. Make sure the grommet holes are sealed as well.

PRECAUTIONS

Because of the very high open circuit voltage produced by this unit *never* attempt to remove the spark plugs whilst the engine is running, since not only is there a danger of breaking down the insulation of the coil, but the experimenter stands a good chance of getting a nasty shock.

In addition the thyristor can be exposed to transient voltages of up to 1,000V under these condi-

tions, and may be destroyed.

TACHOMETERS

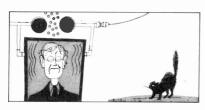
There are a large variety of tachometers in use, all differing in their exact requirements, so some experimental work may be necessary to obtain the best results.

There are two possible connection points for current operated tachos (the most common type). The lead from the ignition coil to terminal A on the unit carries a 10 amp short duration pulse and the lead to terminal E (negative earth) or terminal F (positive earth) carries a wider pulse of 4 amps amplitude. In both cases try coupling the wire through the tacho pickup both ways as the polarity of the pulse may be important.

Regarding voltage operated tachos, the high voltage type should operate if connected to terminal B on the unit whilst a low voltage type can be left connected to the contact breaker. If in doubt, try both positions.

. . . . never attempt to remove spark plug leads while engine is running





NEGATIVE IONS AGAIN

It seems only recently that we were chatting about the effects that charged atoms and molecules appear to have on us, other animals, and plant life. Since then I have read a number of quite serious reports about these "ionic beasties" and, indeed, discovered in addition that the people at the University of California actually have a faculty there which deals with the subject!

To refresh your memory about ions; generation of airborne ions all begins when sufficient energy is transferred to a gaseous molecule causing it to release an electron. This electron then "climbs aboard" any nearby molecule causing it. in turn, to become charged and in all likelihood convert to a negative ion (by virtue of the charge carried by the electron). The first molecule, however, has, in the process, turned into a positive ion. Umpteen of these molecular collisions occur, with the result that whole layers of species exist having either an overall positive or negative charge.

That, though, is by no means, the end of the story. Water molecules, too, get in on the act and jostle for position around individual ions, so forming somewhat larger ions.

According to Profesor A. Krueger of the University, mentioned earlier, these slightly larger (albeit, still tiny) molecules are of four types, namely H $^+$ (H $_2$ O) $_n$, 1 (H $_3$ O) $^+$ (H $_2$ O) $_n$, 2 0 (H $_2$ O) $_n$, and one with a hydroxyl group attached having the formula OH $^-$ (H $_2$ O) $_n$. The $_n$ in

the formulae has quite a small value.

Apparently, negative ions are the more mobile, when compared with the positive variety, and, since the Earth itself carries a negative charge, the former are repelled from the surface of the ground.

According to the experts, negative ions are decidedly the "good guys", which bears out our earlier thoughts on the subject. Unfortunately, the positive ("bad guys") are in the majority by something like a factor of 1.2 to 1. Pollution, additionally, helps to keep this



ratio looking nasty, because, as you will recall, atmospheric dust has the habit of discharging any negative ions with which it comes in contact.

At the present time we can only produce (and successfully maintain) relatively small quantities of the beneficial ions; i.e., in buildings, or in cubicals where the size of the generator/transmission network can be kept within reasonable bounds. However, there ought



to be sufficient encouragementfor contemplating some really big set-ups. For example, plant growth has been caused to increase by as much as 50 per cent as a result of moderate exposure to air ions. Silkworms, too, hatched out earlier and larval growth was also accelerated. On the other hand, positive ions have been shown to increase the death rate among mice suffering from influenza!

In the final shakedown, it is worthy of mention that negative ions are suspected of lowering the blood serotonin (5-hydroxy tryptamine, 5HT) level, and since this is a hormone which, among other things, appears to be connected with the facilitation of neural signals across the synaptic junctions

between nerves, it is not surprising to learn that high negative ion counts can result in profound mental effects. These may range from clearer headedness to a kind of tranquillity.

No amount of persuasion has yet encouraged my editor to change his mind about putting a taboo on a special high-voltage negative ion generator I intended to include. It could no doubt, be lethal in the wrong hands, so I guess his decision is the right one!

MAGNETO-CHEMISTRY

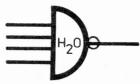
Still on the subject of chemy's, I notice that R. Skorsky of the Alabama University has discovered an interesting effect in ferric oxide, Fe₂O₃. Haematite, for that's it's other name, can, according to him, be reduced at much lower temperatures than previously achieved by simply surrounding the sample in an a.c. field of a few hundred gauss.

Skorsky has a theory that the cause of this effect is due to the increased pressure of hydrogen at the surface of the material resulting from its attraction to the magnetised iron (due to initial reduction of some of the ferric oxide at the beginning of the reaction).

Interestingly enough, C. Peters, over here, at the University of Surrey seems to think that the effect can be expected. His proposal amounts to the fact that since there is a considerable difference in the magnetic properties of the non-reduced material and final product, and because the reaction is going in a "direction" which favours a ferromagnetic substance as an end result, anyway, the outcome will be an increased tendency towards production of a magnetic material when a field of sufficient intensity is available. Sounds reasonable!

TAILPIECE

Washington, you'd think, had received its share of trouble. But it would seem the wags haven't finjshed with 'em yet. Only yesterday I came across this odd bit of logic.



A.C. DETECTOR PROBE

By B. BOWLES

T is often necessary, particularly in radio circuits, to check for the presence of high frequency oscillations but most amateurs do not possess test equipment capable of responding to frequencies greater than a few megahertz. The probe described here will respond to frequencies between 200Hz and 30MHz, allowing use in general a.c. signal tracing. Any a.c. of a few millivolts or more will light a small light emitting diode (l.e.d.). The whole instrument can be held in one hand.

CIRCUIT DESCRIPTION

The complete circuit is shown in Fig. 1. Transistors TR1 and TR2 form a high gain a.c. amplifier which also rectifies the signal to drive the l.e.d. (D2). The configuration is known as a d.c. feedback pair. TR1 is biased just into conduction by feedback from the emitter of TR2. The preset potentiometer VR1 is used to set the d.c. conditions for the circuit. Components R5 and C2 and C3 form a filter which reduces the a.c. feedback so that the a.c. gain of the circuit is not reduced.

The input impedance is roughly equal to the value of R2 since C2 and C3 form a low impedance path for a.c. C3 is used to compensate for the inductive effect of C2 at high frequency. Diode D1 protects the input from negative voltage swings.

RECTIFICATION

The diodes in the emitter of TR2 serve to rectify the signal in the following manner. When the input swings positive TR1 will conduct tending to lower the voltage at TR2 base and by emitter follower action at TR2 emitter as well. The diodes cease to conduct and the voltage at TR2 emitter drops causing the current fed back to TR1 to drop, counteracting the effect of the positive input. If, however, the input goes negative, TR1 will conduct less causing TR2 base to rise. The diodes will, however, maintain the voltage at TR2 emitter almost constant so there will be no negative feedback to the base of TR1.

The circuit thus has high gain when the input goes negative but low gain when it goes positive. Thus an a.c. input will cause TR2 to conduct and hence pass more current through the l.e.d. The resistor in parallel with the l.e.d. allows enough current to pass through the transistor to keep the diodes conducting and the resistor in series limits the maximum l.e.d. current to less than 10mA.

The circuit is so stable that the battery voltage can fall to 7V without affecting performance.

COMPONENTS . . .

R4 1-2kΩ R1 4.7kΩ R5 4.7kΩ R2 4·7kΩ

R3 120Ω

All ±5% &W carbon

Potentiometer

VR1 5kΩ linear sub-miniature skeleton horizontal mounting

Capacitors

C1 0·22μF

C2 10µF 6 3V tantalum bead

C3 1,000pF ceramic C4 47μ F 10V elect.

Diodes

D1 1N4148 D2 TIL209 light emitting diode

D3 OA91

D4 1N4148

Transistors TR1, TR2 BC107 or BFY90 (2 off)

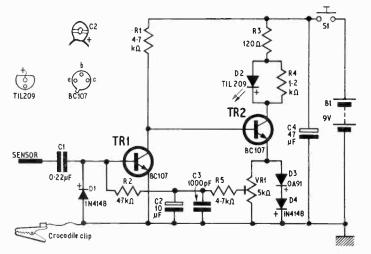
Miscellaneous

S1 Push-to-make, release-to-break push-button

9V PP3 battery

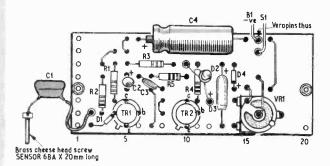
Veroboard 0-1in matrix 2in × 0-9in

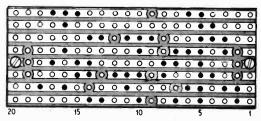
Veropins, 6BA and 8BA nuts and bolts and washers, wire, suitable case (see text)

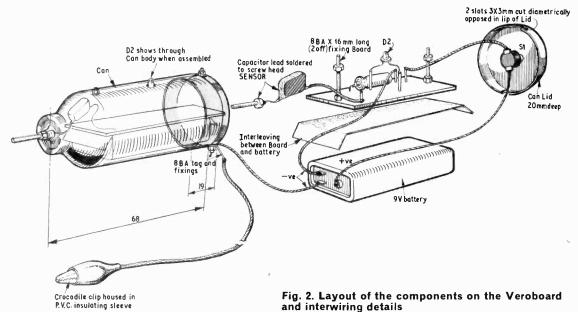


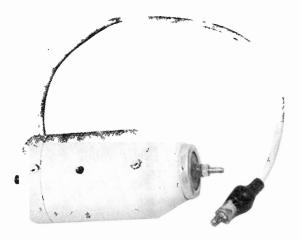
A.C. DETECTOR PROBE

Fig. 1. Circuit diagram of the A.C. Detector Probe









Photograph showing the completed A.C. Detector Probe

CONSTRUCTION

The circuit for the A.C. Detector Probe can be made very compact so that the whole unit can be held in the hand, making it convenient for testing equipment. All the components except the capacitor C1 are mounted on a small piece of Veroboard as shown in Fig. 2. Veropins are used for wire connections to the board. The l.e.d. is mounted on two pins higher than the rest of the board so that it shows through the side of the probe case. Take care not to overheat the l.e.d. when soldering.

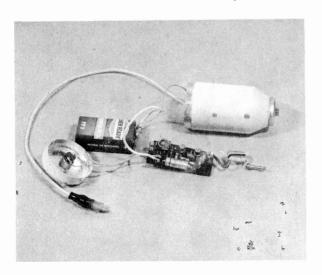
Only one end of C1 is connected to the board.

SETTING UP

Before mounting in the case VR1 must be set up.
Connect the battery to the board. The l.e.d. should light with VR1 at one end of the track and extinguish at the other end. If the l.e.d. dims but does not go out, TR1 has low gain and should be replaced.

VR1 should be adjusted so that with no input D2 is just faintly lit. Any a.c. input with a frequency

Photograph showing the construction of the A.C. Detector Probe before assembly



of 200Hz to 10MHz should now cause the l.e.d. to light.

The l.e.d. should flash each time the power is applied, this being due to the charging of C2.

CASE CONSTRUCTION

The prototype case was made from an empty butane lighter fuel container of medium size but any aluminium tube will do. Great care should be taken that there is no gas left in the container.

First pierce the container about five inches from the tip or nozzle. This should be done well away from naked lights, preferably outdoors. Then cut the case into three parts as shown in Fig. 2.

Do not drill the holes yet. After the cutting and any necessary smoothing of the edges, the body of the probe, the end cap and a 19mm ring remain. This ring should be cut with scissors, its ends overlapped and then pushed into the probe body. Mark the overlap, remove the ring and cut off the overlap so that when re-inserted into the tube it fits with the ends butted together. The ring can now be glued into the body leaving about 6mm protruding from the body.

END CAP

This now makes a push-fit seating for the end cap, and provided the cuts have been made square gives the probe a good appearance.

The end cap should now be pushed on and held

with adhesive tape and the holes drilled.

The holes in the end cap should now be enlarged into slots so that the end cap can slide over the two bolts which secure it. A hole is also drilled in the end cap to take the push button switch.

The plastic insert in the front of the tube should

also be enlarged to 3mm.

FINAL ASSEMBLY

The free end of C1 is soldered to the head of a 12mm 6BA bolt. The solder tag on the mounting bolt should be soldered to the negative line on the board. The battery is then connected up. Some insulating tape is stuck inside the tube in case the circuit should touch, and the board pushed in making sure that the bolt on C1 goes through the end of the tube. The battery is then pushed in with a piece of card between it and the board to stop the metal case shorting the board.

The end cap is now fitted and nuts fitted to the bolts holding the end cap and the probe bolt. Attachment of the earth lead and crocodile clip com-

pletes the unit.

USE AND APPLICATIONS

The A.C. Detector Probe is very sensitive and its frequency response extends up to several megahertz. If high voltages are to be measured a resistor can be connected to the probe bolt to act as an attenuator.

Bandwidth can be extended by eliminating DI and replacing TRI and TR2 with BFY90 transistors which give high sensitivity up to about 70MHz. Above this frequency the l.e.d. may actually dim when connected to a.c. this being due to phase shift causing the normal rectifying action to be reversed. This is just as valid an indication of the presence of a.c.

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- Case mouldings, with buttons, window and light-up display in position.
- 6. Printed circuit board.
- 7. Keyboard panel.
- 8. Electronic components pack (diodes, resistors, capacitors, transistor).
- 9. Battery clips and on/off switch
- 10. Soft wallet.



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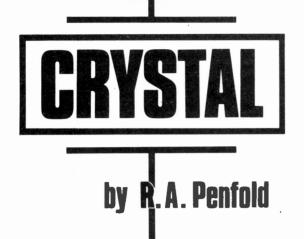
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HE PURPOSE of a crystal calibrator is to provide signals at standard frequencies over the medium and short wavebands, in order to allow accurate calibration of a radio receiver dial.

Providing the output from the calibrator is nearly a square wave it will be rich in harmonics (i.e. multiples of the fundamental frequency). A good calibration oscillator of fundamental frequency 200kHz will have harmonics which are reasonably strong right up to the upper limit of the short wave band (30MHz).

Using a crystal means that the fundamental frequency is predetermined, and extremely stable with respect to time and temperature.

In order to allow the signal to be easily identified on a receiver an audio oscillator has been included to modulate the r.f. signal.

CIRCUIT DESCRIPTION

The full circuit diagram is shown in Fig. 1 and can be seen to be divided into two sections, the audio oscillator and the crystal controlled r.f. oscillator. The active elements used in the unit are contained in two integrated circuits type µL914 whose internal circuits are shown in Fig. 2.

The μ L914 is intended for use in logic systems and is one of the family of Resistor Transistor Logic (RTL) circuits. It can be adapted for use as an amplifier by inserting a biasing resistor between the collector and the existing base resistor of one of each pair of transistors and ignoring the other, thus forming two, one-transistor amplifiers from each i.c.

CRYSTAL OSCILLATOR

A crystal has the property that at one particular frequency (known as the series resonant frequency) its impedance (resistance to current flow) becomes very low while at all other frequencies its impedance is high.

In the oscillator circuit used in the calibrator the two, one-transistor amplifiers in the μL914 are connected in series *via* the crystal and the capacitor C6.

At the series resonant frequency the impedance of the crystal is sufficiently low for the positive feedback between the two stages to maintain oscillation.

Because of the large positive feedback the switching between the two states (transistor on and transistor off) is rapid so that the output is almost square producing the large number of harmonics required. The 200kHz crystal used in the prototype gave enough harmonics to cover the long and medium bands.

AUDIO OSCILLATOR

The other i.c. and its associated components form an audio frequency oscillator with a frequency of about 2kHz. When applied to the crystal oscillator

COMPONENTS . . .

R5 100kΩ R6 $33k\Omega$ 470Ω R8 100kΩ

Capacitors

Resistors R1 2.2kΩ R2

R3 2.2kΩ

 $47k\Omega$

100kΩ

 $\begin{array}{cc} C1 & 0.1 \mu F \\ C2 & 0.1 \mu F \end{array}$ ceramic

120pF

C4 0.047µF ceramic

C₅ 100μF 10V elect.

C6 2,700pF

C7 0.01 µF

Integrated Circuits

IC1, IC2 µL914 or equivalent (2 off)

Crystal

XL1 200kHz crystal with holder (Henry's Radio type FT241A)

Miscellaneous

4-pole 3-way rotary

9V battery type PP4 with clips SK1 Coaxial panel mounting socket

2.8in × 1.4in Veroboard 0.1in matrix

Aluminium case approx. $4in \times 3\frac{1}{2}in \times 2in$

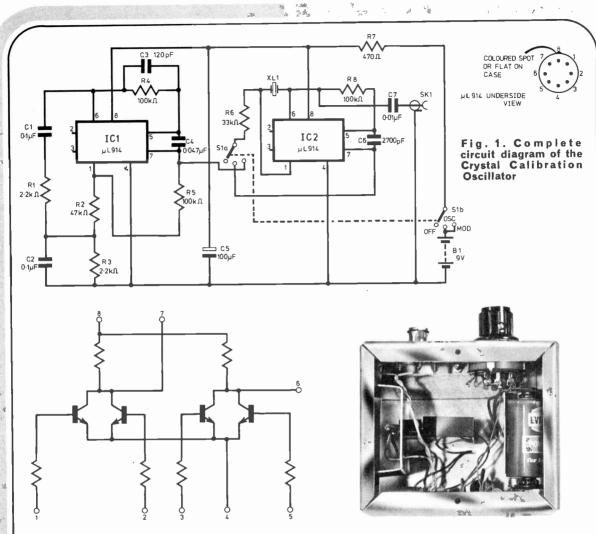


Fig. 2. Circuit diagram showing the internal circuit of the $\mu \rm L914$ integrated circuit

Photograph showing the arrangement of the components in the small aluminium case with the crystal mounted on its bracket

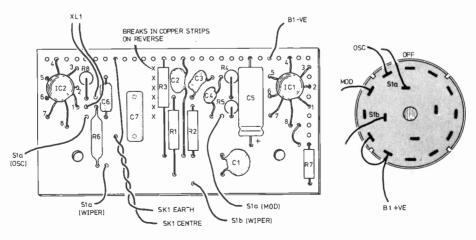
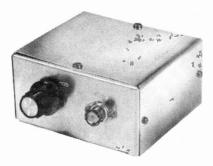


Fig. 3. Constructional details of the Crystal Calibration Oscillator



via R6 it varies the amplitude of the r.f. signal so that an audio signal of 2kHz will be heard when the receiver is tuned correctly.

The two amplifiers in the i.c. are connected in series to form an amplifier whose output is in phase with its input. The components C1, R1 and C2, R3 form what is known as a Wien Bridge, and it is these components that determine the frequency.

The switch therefore has three positions, OFF, OSC which gives the unmodulated crystal frequency and MOD which gives this frequency modulated by the oscillator.

Resistor R7 and capacitor C5 are included to reduce the supply voltage down to the 5V required by the i.c.s.

CONSTRUCTION

Construction is simple, all the components except the crystal, switch and output socket being mounted on a piece of Veroboard as shown in Fig. 3.

Any small aluminium case will do providing it is of sufficient size to accommodate all the components. It is wise to obtain a socket with the crystal as soldering to it directly could cause damage. A small bracket to hold the crystal can be mounted on the side of the box as can be seen in the photograph.

The switch used in the prototype is a four-pole three-way type with only two poles used.

USING THE CALIBRATOR

Once the unit has been completed, and all wiring checked for mistakes, a length of lead should be connected to the output socket and the unit turned on.

If the lead is now placed near a medium wave radio receiver, and the receiver is tuned over the band, strong signals from the calibrator should be received at intervals across the dial. Switching on the modulation should produce an audible note on these signals.

Using a 200kHz crystal, harmonics will be generated at 600kHz, 800kHz, 1MHz, 1·2MHz, and 1·6MHz. To find out which is which the receiver should be tuned to a known frequency (say Radio 1 on 1·214MHz) then the dial turned until the nearest signal from the calibrator is received (in the case above this will obviously then be 1·2MHz). Other frequencies can then be ascertained by counting the number of harmonics above or below the known frequency, as each corresponds to a difference of 200kHz.

This method of identification can be used on any band where the exact frequency of a station is known.

INGENUITY UNLIMITED

A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought. This is YOUR page and any idea published will be awarded payment according to its merits.

OPTICAL COMMUNICATION SYSTEM

THE circuit described here is for a novel communication system using light beams to carry audio signals. Light emitting diodes (l.e.d.s) are particularly suitable for producing modulated light beams as they produce an intense concentrated spot

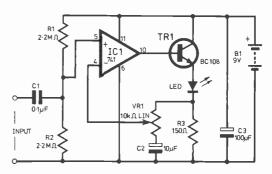


Fig. 1. Transmitter circuit diagram

BOILER GAS VALVE OPERATION AT LOW D.C.

PERHAPS the enclosed circuit idea would be of interest to your readers in view of impeding power cuts this winter. It allows a gas boiler mains operated gas valve, to be operated from a low voltage d.c. supply. The circuit has low battery consumption and low break current to minimise thermostat contact erosion.

I hesitate to recommend exact component values as the circuit was developed hurriedly to be ready for power cuts. In addition it was intended to run from a car battery so I did not bother to optimise the oscillator circuit or the capacitor and charge resistor values for minimum consumption.

I used an available Ferroxcube in the oscillator circuit and I do not know the exact turns ratios. I do not know how much variation exists between individual gas valves so that some experimentation by readers will therefore be required in both these areas.

Fig. 1 shows the circuit where R1 and C1 are included to prevent possible, radio interference.

In operation, S1 is first closed charging C5 to about 120V. After a minute or so S2 is operated. The charge on C5 operates the gas valve, the voltage of which is prevented by D1 from falling much

of light, have a linear current/light output relationship, and have a good high frequency response (the type of l.e.d. with a plastic diffusing dome is not suitable for use in this circuit).

The circuit shown in Fig. 1 will modulate the light from the l.e.d. using a cystal microphone or a loud-speaker output. IC1 acts as an a.c. amplifier with an input impedance of about 1M12. R1 and R2 are biasing resistors and together with IC1 and TR1 they produce a d.c. of 30mA in the l.e.d. VR1 and C2 control the a.c. feedback causing the input signal to be amplified and superimposed upon the bias.

To obtain the maximum range from the transmitter the optical system must be efficient. Either a convex lens or a concave mirror as shown in Fig. 2 can be used to convert the l.e.d. output into a

parallel beam.

For efficient reception the light collecting area must be large; the author used a large concave makeup mirror costing 40p, but better quality mirrors will give better results.

The received light is concentrated onto a sensitive photo-Darlington transistor as shown in Fig. 3.

Because the transistor is so sensitive the load resistor must be low to prevent saturation in daylight conditions.

At short range the signal across the load resistor is adequate to drive a crystal earpiece, though for longer range an a.c. amplifier and a loudspeaker are needed. The phototransistor output impedance is 1k\(\Omega\) and most commercially available audio amplifiers are suitable.

The overall distortion is quite low, speech being excellent and music quite acceptable. The main cause of interference is mains lighting but this can be minimised by careful design of the optical system.

Transmitter and receiver must be accurately aligned and the transmitter gain should be carefully adjusted by means of VR1 to give maximum modulation without clipping. Clipping causes obvious distortion and is easily recognised.

J. N. Jones, Cheshire.

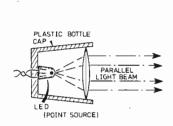


Fig. 2. Typical optical system for the transmitter

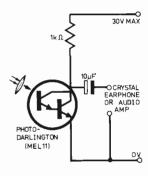


Fig. 3. Receiver circuit diagram

below the battery voltage. When the thermostat cuts out C5 recharges ready for the next operation.

C4 was included to adjust the charge rate of C5; it obviously affects the oscillator also and should not be needed in a fully developed design. D1 and D2 should have a minimum p.i.v. of say 200V and 400V respectively. D3 and D4 can be any silicon diodes.

I found that my Potterton boiler gas valve included a rectifier and that it closed at about 70V d.c. and held in at voltages below 11V. The consumption was about 2mA at 12V d.c.

For better economy of operation, a switching circuit might perhaps be devised to switch off the oscillator when the gas valve is energised but I have not tried this.

C. J. Collins, Letchworth. MAINS SUPPLY 100 A 12 - 14V THERMOSTAT 100k A 10 km 10 k J C 10 nF C5 C1 □ GAS VALVE 10µF 250V

Fig. 1. Circuit for operating gas valve from low voltage d.c. supply

SLOW TIMEBASE OSCILLATOR

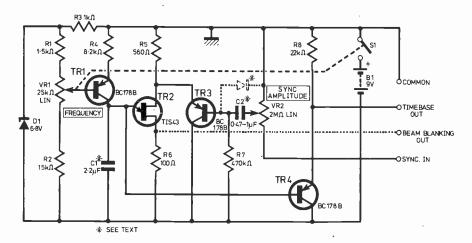


Fig. 1. Circuit diagram of the slow timebase oscillator

The sawtooth generator shown in the circuit diagram Fig. 1 was designed to extend the time-base range of a general purpose oscilloscope down to 1Hz. As well as the linear sawtooth with fast flyback, there is provision for an external synchronising signal and flyback blanking output.

The timing capacitor C1 of the relaxation oscillator, TR2, is charged by a constant current source from TR1. The base potential of TR1, controlling the constant current, is derived from the divider network R1, VR1 and R2. The Zener diode across the divider keeps the voltage at a constant level.

Since the sawtooth output at the emitter of the unijunction is at high impedance, the output is fed to an emitter follower to buffer the output against possible low impedance loads. The output should, however, not be taken to loads of less than 20k() impedance.

The synchronising input has a constant input resistance of 2M() and a portion of the signal is taken to an emitter follower via VR2 and C2. The effect of the emitter follower output is to modulate the supply voltage to the unijunction in step with the sync signal so that the sawtooth tends to be locked in frequency to the sync signal or a multiple thereof.

For adequate synchronisation even at the lowest frequencies, the input impedance of the emitter follower must be greater than the reactance of the capacitor at the lowest frequency.

The voltage rating of C2 should be sufficient to block the highest d.c. voltages likely to be encountered.

Adequate sync is available with a 0.3 to 1V r.m.s. input, but if higher voltages are used a diode should be wired as shown dotted, see Fig. 1, to prevent transistor emitter/base breakdown.

The frequency range of the oscillator is 1 to 60Hz, but could be extended up to 20kHz by varying the value of the timing capacitor C1. Capacitor C1 should be a low leakage type to ensure good linearity at low frequencies.

One of the many applications would be to use the oscillator for monitoring heart pulses in conjunction with the "Biological Amplifier" published in the January and February '73 issues (no back issues available). Care should be taken to ensure that the output from the Bio-amplifier is a.c. coupled to the vertical input of the monitoring 'scope.

M. H. George, Upminster. Essex.

AN IMPROVISED TAPE GUIDE

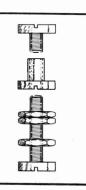
THE drawing in Fig. 1 shows an improvised tape guide with height adjustment.

The guide itself is a ‡in brass binding post and is of the type which is threaded right through. These are obtainable from most well-stocked stationers.

The guide is simply fixed and adjusted by a BA bolt and three nuts.

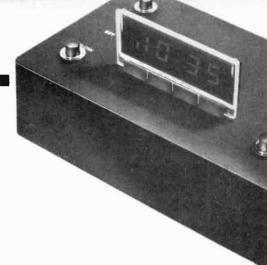
Paul A. Koh, Sunbury-on-Thames.





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A completely fresh approach to design providing a predictable result from simple rules of thumb. Opening articles deal with small signal amplifiers based on popular transistor types.

PRACTICAL

APRIL ISSUE ON SALE MARCH 8, 1974

Subject to the current National Industrial situation at the time of going to press

Boolean

Algebra—1

By B. J. Wood

A two part article providing an introduction to switching theory and concluding with a practical design of a simple adder subtractor

EORGE Boole published a treatise "An Investigation of the Laws of Thought" discussing the system now called Boolean Algebra over a century ago in 1861. The basis of his concept is that a statement in words may be represented in the first place by a letter of the alphabet.

Thus we can say that the letter A represents the statement "It is Sunday" and the letter B "It is sunny." These are positive statements and Boole

assigned them a value 1.

Using his system it is very simple to identify the opposite statements "It is NOT Sunday" and "It is NOT sunny" by simply putting a bar over the chosen letter thus \overline{A} or \overline{B} . This time Boole assigns the value 0 to these negative statements.

To test the system let us assume that we ask the question "Can I mow the lawn?", having set the conditions that one can, but only if it is sunny and

also a Sunday.

Thus for a sunny Sunday we have both A and B, or shown mathematically, A.B, where both A and B are I. Clearly the answer is I, or positive. If either of the conditions is a negative then the answer will be negative. Thus $\overline{A}.B = 0$ and $A.\overline{B} = 0$ and it is not suitable to mow the lawn.

This type of decision making is called an AND function in which the factors have been multiplied

together.

The condition could be "It is Sunday" or "It is sunny" in which case an addition of the two values would be required. If either had a value of 1 the result would be 1. This is called an OR function and in the case of the OR when both are 1 the rather odd result of I + I = 1 arises but here the AND and OR are interchangeable.

A.B + A.C A (B+C)

Two logic diagrams which both represent the same overall function. Note the simpler form of the right-hand version

If the condition "Sunday and dry" is just as suitable for mowing the lawn as "Sunday and sunny" the decision to mow the lawn or not may be stated as A.B + A.C where C means "It is dry". Boolean algebra may be manipulated like any other algebra so that A(B + C) means the same as A.B + A.C, giving the same arithmetic result.

If there are many conditions and alternatives the algebra can become quite involved. Generally, it is enough to work out one or two decisions at a time

and build up the logic gradually.

LOGIC DIAGRAMS

In logic of the electronic kind, diagrams are useful to describe the flow of information. In the initial stages such diagrams contain only simple elements whilst later a whole group of elements may be put into one box and given a label in the same way that a collection of components may be labelled "amplifier". Fig. 1 shows the two ways of connecting AND and OR boxes which will give the same decision, to mow or not to mow the lawn.

The symbols used are fairly simple, being in the form of "D" shapes with inputs to the left and output to the right, a figure in the symbol denotes the number of inputs which must assume a logic 1 state for the output to be logic 1. An & sign in the

symbol denotes an AND element.

Thus the operation to decide to mow the lawn under the Sunday and sunny or Sunday and dry conditions can be determined from these diagrams. Notice that the simplification of A.B + A.C to A.(B + C) also simplifies the diagram.

LOGIC ELEMENTS

Logic integrated circuits are available in many forms, simple and complex. They are very convenient packages, reducing external wiring to a minimum. Their low cost allows the constructor to build equipment which, a few years ago, would have been too expensive in terms of time and money. For the moment, however, elements built from discrete components will be discussed and related to the i.c.s as convenient. It does not matter that these devices are not identical as long as they react in the same way.

AND, OR, NOT ELEMENTS

These are the basic devices. More complex devices may be built from them. The AND may be made from diodes and a resistor as in Fig. 2a.

If either of the switches is closed representing an input of a 0 function then the whole of the voltage available from the supply is dropped across R1 and the output is at earth potential. Obviously, closing both switches has the same effect. It is only when both switches are open that a voltage is available at the output terminal.

The presence of this voltage is called logic 1. In its absence the state is logic 0. Why "logic"? Normally, the switches in the diagram are replaced by

the outputs of other elements.

In practice absolute voltage levels are not possible at reasonable cost and so the design must allow for fluctuation. Thus logic 0 may be 0.5V or less

and logic 1 anything over 2V.

To following elements these values are taken to represent 0 or 1. There is an electrical no-man's-land in between the two values which is avoided by the design and proper use of the devices involved.

AND

To return to the AND element, there is a table at 2a in which the states of A and B are given together with the resultant output for the four possible states of input. Called a truth table, this device shows that for a 1 output all inputs must be at logic 1. For any other combination the output is at logic 0. This applies for two, three or twenty inputs. Note that, to an AND input, an open circuit is a logic 1.

NOT

The NOT is shown at Fig. 2b It is simply an inverter in which, if a logic 1 voltage is applied at the base of the transistor it is switched hard on, the collector bottoms and the output goes to logic 0. If the base is at logic 0 the output is up near the rail voltage.

The second diagram at Fig. 2b is much more like an i.c. inverter in that the transistor is held on with a logic 0 output, unless presented with a logic 0 input. Like the AND, an open circuit input is treated as logic 1.

SYMBOLS

There are conventional symbols used to denote the various elements we have discussed so far as well as others to follow. They are used to avoid the need for either discussing or indeed even showing the actual components used in a particular element such as the diodes or transistors already noted.

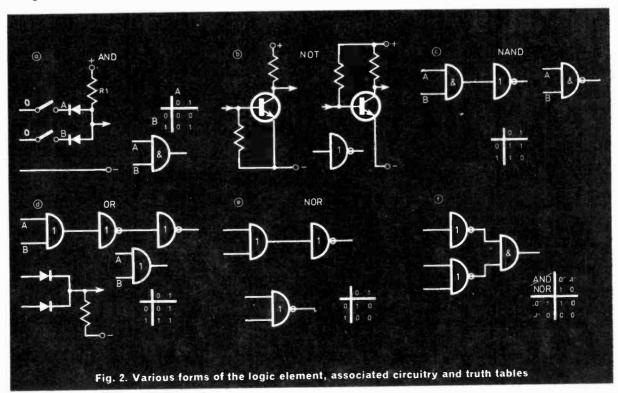
Thus the elements AND and NOT, shown in detail at Figs. 2a and 2b may be shown as the two separate 'D' shapes joined together in Fig. 2c. Here the AND element is that with the ampersand (&) inscribed. This is intended to show that the element has inputs which have to be at logic 1 for the output to go to logic 1.

The second element with the small circle on the output line is the NOT element of Fig. 2c. Here the small circle denotes the logic 0 output obtained if

the input goes to a logic 1.

NAND

The two elements at Fig. 2c denote NOT AND which is normally known as NAND. In fact this has a new symbol of its own as shown to the right in Fig. 2c, the small circle denoting the NOT output and the ampersand the requirement for logic 1 inputs for this. The truth table shows the outputs obtained for various inputs and it can be seen that only when all inputs are logic 1 will the output be logic 0. Of course, as before the logic 1 input includes an open circuit.



OR

In its simplest form the OR element is made from diodes as shown at Fig. 2d. As can be seen these point in the opposite direction from those in the AND element. If a logic 1 appears at any input it becomes available at the output. The OR treats an open circuit as logic 0. In diode form the resistance of the load must be small enough to look like a logic 0 to the following element but large enough to demand only a reasonable current from the input source. The second diagram of Fig. 2d overcomes this difficulty by the introduction of two NOTs.

In this case the first element is a basic threshold element and the number inside denotes the number of inputs which must be at logic I for the output to be at logic I. This element is followed by the two NOT elements and the whole may be shown as below.

NOR

A NOR element is an OR followed by one inverter element as shown at Fig. 2e. Only when all the inputs are at logic 0 is the output at logic 1. Under any other condition, as can be seen from the truth table the output is at logic 0.

INVERTED INPUTS AND OUTPUTS

Suppose that an AND is used with an inverter in each input so that 0 becomes 1 and vice versa. Fig. 2f truth table shows that it becomes a NOR. If, additionally, the output is inverted it then becomes OR. The reader should treat all the other truth tables in a similar fashion. It will be seen that any element may be made to exhibit the characteristics of the other three.

For what follows in this text the important point is that a NAND with inverted inputs becomes an OR. In general the devices to be used will be NANDs with diodes as ANDs when convenient plus NOTs. In the beginning it will be, perhaps, easier to recognise that an OR is required and then use a NAND with inverters in the inputs.

BINARY NUMBERS AND ARITHMETIC

In the kind of logic under discussion there are only the two states 1 and 0. Any process to be handled by the logic must therefore be described in these terms. In everyday arithmetic the radix of 10 is used with ten possible digits of 0 to 9. But if, as with Boolean logic, 2 is used as the radix, only the digits 0 and 1 are possible.

In the scale of 10 the number 286 can be written $(2 \times 10^2) + (8 \times 10^1) + (6 \times 10^\circ) = 200 + 80 + 6 = 286$.

In the scale of 2 the number 1101 means (1×2^3) + (1×2^2) + (0×2^1) + $(1 \times 2^\circ)$ = 8 + 4 + 0 + 1. (A number to the power of 1 is itself. Any number to the power of 0 is 1).

As a point of interest, decimal-to-binary conversion can be achieved as follows.

CONVERSION

Convert 83 to binary. This may be done mechanically by dividing the number 83 continuously by 2 ignoring remainders until the answer of 1 is reached.

Write (—) against odd answers and (0) against even answers. The result looks like this.

If now the paper is turned so that the (—) against the final answer of 1 is at the left then this is the result in binary:—

where 1010011 = 64 + 16 + 2 + 1 = 83.

Conversely, to convert binary notation to its decimal counterpart simply multiply the left-most digit by two and add the following binary digit. Multiply the result by two adding the next binary digit and so on until the end is reached as below.

1 1 0 1 0 1 3 6 13 26 53

The final figure, in this case 53, is the correct answer.

ADDING BINARY NUMBERS

The rules for addition of two binary digits (bits) are 0 + 0 = 0; 0 + 1 = 1; 1 + 1 = 0 and carry 1. Where there is a carry from the previous position it requires the following rules, 0 + 0 + 1 = 1; 0 + 1 + 1 = 0 and carry 1; 1 + 1 + 1 = 1 and carry 1.

Using the rules to add 6 to 7 —

Binary Decimal $\begin{array}{rcl}
111 & = & 7 \\
110 & = & 6 \\
\hline
1101 & = & 13
\end{array}$

SUBTRACTION

The rules for subtraction of two binary digits (bits) are 0-0=0; 1-1=0; 0-1=1 and borrow 1, 1-0=1. Where there is a borrow the following applies, 0-0-0=0; 1-0-0=1; 0-1-0=1 and borrow 1; 1-1-0=0; 1-1-1=1 and borrow 1, etc.

Thus if we subtract 3 from 5:

Binary Decimal 101 = 5 011 = 3 010 = 2

Of course, problems arise when larger numbers have to be subtracted from smaller numbers. Using decimal notation, the human animal in fact reverses the process, subtracts the smaller from the larger and then calls the result a "negative."

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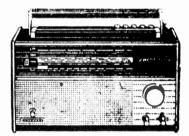
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divisions for switch setting purposes with trips
which are infinitely adjustable for position. They are also
arranged to allow 2 operations per
switch per rotation. There are 1.5 changeover
micro-switches each of 10 amp type operated by the
trips thus 15 circuits may be changed per revolution.
Drive motor is mains operated 5 revs per min.
Some of the many uses of this timer are Machinery
control, Bpiler firing, Dispensing and Vending
machines, Display lighting animated and signs,
Signalling, etc. Price from makers probably over
£10 each. Special sinp price £6.33 pins 25p post and
insurance. Don't miss this terrific bargain.



12 VOLT 11 AMP POWER PACK

This comprises double-wound 230/240V mains transformer with full wave rectifier and 2000 mF smoothing. Price \$2.20, plus 20p post & packing.

Heavy Duty Mains Power Pack. Output voltage adjustable from 15-40V in steps—maximum load 250W—that is from 6 anup at 40V to 15 anup at 15V. This really is a high power heavy duty unit with dozens of workshop uses. Output voltage adjustment is very quick—simply interchange push on leads. Slicon rectifiers and amoothing by 3,000mF. Price 26-33 plus 65p post.



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Al. Measures only im wide x in
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contact rating but estimate this at
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it, likeal for models and miniaturised equipment. It's a plug in relay
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Whilst a machine can be made to do this it is not part of the present discussion as it is complex and

requires very lengthy explanation.

Take the case of subtracting 7 from 3. In decimal the answer is obvious, it is minus 4 (-4). Equally, if you take 5 from 2 the answer is -3. In binary terms using the methods so far discussed this is not so. Thus in the case of 3-7:

In both cases there is a borrow 1 with nothing to subtract it from and in fact even if there were more positions to the left the resultant row would be filled with figure 1's with an unsatisfied borrow 1

emerging at the far left.

The same thing happens in decimal notation if one persists in trying to subtract using this type of approach. Thus in decimal the results could be shown as (1)6 and (1)7, the figure in the bracket being the unsatisfied borrow.

In fact the two answers 6 and 7 are the tens complements of the correct answers, subtract the 6 and the 7 from 10 and you have, in positive form,

the correct answer.

Similarly, with the binary computation the results must be subtracted from 8 which, in binary is 1000 There are two snags to this situation. First the operator needs to know before the event that a negative result will arise and re-arrange the inputs.

COMPLEMENT

The word complement was mentioned. This is the key to the answer. In the 1 and 0 binary system the 1s complement of 1 is 0 and vice versa.

Ignoring the unsatisfied borrow in the two binary answers, if 1 is changed to 0 and vice versa 100 becomes 011 and 101 becomes 010 or 3 and 2 in decimal, both wrong by being 1 too few. What is



IMPROVING YOUR HI-FI

By John Earl Published by Fountain Press 203 pages, 8\frac{2}{3}in \times 5\frac{1}{2}in. Price £3.00

The title of this book is slightly misleading as the theme is not really improving hi-fi systems but getting the best out of them. Written in a non-technical style, it appears to be directed towards the people who are not satisfied with low-fi but are not au fait with all the technicalities and jargon of high-fi and are perhaps not getting all they could from their set-up.

This is strictly a practical book dealing with things like the importance of correct earthing, the need to really needed is the complement of 7 which can be arranged by subtracting 1 before the complement is taken. To do this the unsatisfied borrow from the left is carried round to the right to form part of the subtraction. Using the examples again—

011 111	010 101	Subtract
(1) 100 1		Subtract
011		Answers Complements, both in fact
		negative.

The complements give the answer in positive form but it is known that the answer is negative because the mode of operation is subtract and there is the

borrow 1.

The following table gives all the possible results for the system. The reader is advised to work out columns b, c and d to gain an understanding.

a		b	c	d	
Decimal	positive	negative	neg - 1	complement	
				of c	
0	0000				
1	0001	1111	1110	0001	
	0010	1110	1101	0010	
2					
3	0011	1101	1100	0011	
4	0100	1100	1011	0100	
2 3 4 5 6	0101	1011	1010	0101	
6	0110	1010	1001	0110	
7	0111	1001	1000	0111	
8	1000				
9	1001				
10	1010				
11	1011				
12	1100				
13	1101				
14	1110				

Next month: Constructional details of a simple adder/subtractor will be given

maintain correct dynamic ranges throughout the system, and the meaning of specifications.

For the non-technical enthusiast this book would be essential reading before he considers buying expensive hi-fi equipment S.R.L.

FET APPLICATIONS HANDBOOK

Edited by Jerome Eimbinder Published by Foulsham-Tab 350 pages, 8½in × 5½in. Price £1·85

This book is a collection of applications data from a wide number of manufacturers and provides an excellent reference work for anyone who is involved in the use of field effect transistors (f.e.t.s).

All types of f.e.t.s are described from the simple junction types to the complementary M.O.S. systems used in the pocket calculators of recent years. Many applications of f.e.t.s are described ranging from voltage controlled resistors to amplifiers, switches and digital circuits.

S.R.L.



"... more things in heaven and earth..."

The first reaction of many readers when they read the above title was probably to ask "What's a subject like this doing in P.E.?" You may well ask. Others may have taken the view that our friend Ed is off his rocker and yet others may take the opposite view, and exclaim "At last Ed has come to his (extra) senses, and allowed publication of this previously 'tabooed' subject."

The fact is, this article was written long before Uri Geller's impressive fork—(if not mind)—bending demonstration on BBC television, but friend Ed was a little sceptical I think before that night when I talked him into viewing it! We must all be grateful for his open-minded approach in allowing

this article to appear.

'Naturally, there will be those for and those against, but whether you are a sheep or a goat (these are the two rather inappropriate terms that sceptics use to describe the believers and non-believers, respectively) there is always a good reason to give the whole matter another look. Remember, times change, and so do peoples' ideas, evidence, equipment, and even phenomena.

First, let us get quite clear what is meant by extra-sensory perception (E.S.P.). Take the words literally, and you will get the best definition possible. They mean perception of events (etc.) by some means not obviously connected with

any of the five normal senses.

Let me hasten at this point to make a quick distinction or two. Unfortunately, the Press, Radio, and TV media often treat all subjects which cannot be explained by presently-accepted terms of analysis—witchcraft, black magic, ghosts what-have-you—as E.S.P. This is a great pity, because there are quite different forms of unexplained phenomena, and the only true umbrella titles which could be fairly used to embrace the lot, would be "the occult" (unknown), or "paraphysics."

However, when writing a subject which must be sensational, so-called evidence is often dragged in from as many different fields as possible to try and get the reader all excited and on the edge of his chair. In fact, the opposite often happens, and many are left believing less one way or the other than when they first started reading!

So, though other subjects come under the above general headings, they are not all E.S.P. Such subjects will be described in this series as the etceteras.

Reasonable Approach

It must always be remembered that there is no commonplace thing of today that, at some time past, was not considered impossible. We are all still learning, and humility is, to the truly rationally-minded, something which can only in-crease, not decrease, with in-creased knowledge. Just because humans have relied on speech, sight, etc., for communication and direct physical intervention for getting things done, is not to say that there is no need of a set of equally valid alternatives in his make-up, which needs only to be developed, once discovered—always given he adopts a reasonable approach. Ø Ø

E.S.P. is nothing new. One can go back to the New Testament, if this is considered far enough, and find references to "gifts of the spirit". I will not digress further, other than to say that evidence of the possibility of E.S.P. has cropped up probably as long as man has inhabited the earth, and in other forms, before.

E.S.P. rarely occurs under controlled laboratory conditions. Read a person's thoughts say, once, and then try to continue the pattern under strict control, and the chances are that you will not succeed again even once. This is the very thing the sceptic looks for, and when it occurs he jumps in with both feet and says "Pooh what did I tell



you?" Ok, ok, I say, I am as aware as you that the effect is not repeated under these conditions, but might this not be a point worthy of investigation? "Why?" he would say, and then would come my first analogy, speaking as an electronics bod.

Take out your comb and comb your hair, or if this is greasy, rub it on your Harris Tweed jacket. The comb is now charged, and you can prove this by picking up small bits of tissue paper from the table. What voltage? Would you believe there's probably more than 5kV on it? There probably is!

Now ask the sceptic to get his voltmeter and place one lead on the gas or water pipe (earth) and the other on the comb and see what he gets. Tell him the meter is at least 20 kilohms per volt. Naturally, he gets no reading. Why, you were on the 250V scale and the needle didn't even flick. Reason is that the meter requires current to flow to operate its needle, and the amount of current required for this is in excess of what the comb could supply despite over 5kV on it, at the point of contact with the meter lead.

Could E.S.P. be elusive for some similar reason? By this I mean by trying to "tap" its power to prove an experiment, could we require too much "current" for the source to supply and operate our "meter"? Perhaps the tension caused by the anticipation of all spectators present draws off the very power we are trying to use!

9

Next month: The Scientists Investigate.





An A to Z guide to component buying

On the index page of Catalogue 7, between "Aluminium Boxes" and "Zener Diodes" are over 200 references to contents amounting in all to thousands of items, classified, described, often illustrated, and priced. There is a wealth of technical diagrams and data. At 25p, Catalogue 7 is excellent value by any standard. With the 25p Refund Voucher it costs you virtually nothing when you order £5-worth or more.

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2.	2 —	_	_	_	11p	_	8р	9p
4.	7 —	_		11p		8р	9p	8p
- 1	0 —	_	_	—	Вp	9p	8p	8p
2			8p	_	9p	8р	8p	10p
4		_	9p	8р	9p	8p	10p	130
ΙÓ		βр	8p	8p	9p	10p	12p	19p
22		вρ	9p	10p	10p	Hp	17p	28p
47		10p	100	110	13p	17p	24p	45p
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Code	Watts	a hm s	l-9	10-99	100 up
			(see	note belov	
C	1/20	82~220K	9	8	7.5
Ċ	¥.	4-7-470K	1 - 3	1:1	0.9 nett
CCC	Ĭ.	4·7-10M	1.3	1:1	0.9 nett
č	i	4-7-10M	1.5	1.2	0.97 nett
č	i	4:7-10M	3.2	2.5	1-92 nett
MO	į	10-1M	4	3 - 3	2:3 nett
ww	i	0.22-3.9	7	7	8
ww	3	1-10K	7	7	8
ww	7	1-10K	9	9	8

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Values: All EI2 except CaW, CaW and MOaW at

E.12. 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82. E12, 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82. E24 as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 75, 91 and their decader Tolerances—All 5% except MO at 2% and WW at 10% ± 0.05 Ω.

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14p	ZTX383	15p	ZS120	8p	ZS274	19p
14p	ZTX384	18p	ZS121	10p	ZS276	26 p
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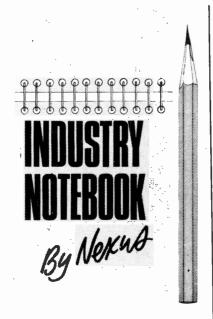
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BEATING THE CLOCK

Coming into service in a few weeks is Cantat 2, the 2,805-mile long transatlantic cable costing £30 million and capable of handling 1,840 telephone conversations simultaneously.

Laying of the cable had its share of drama. The mini-submarine Pisces 3 sank while burying part of the cable on the UK continental shelf. The two-man crew were rescued, happily, after three days of being trapped on the sea-bed. The craft was also recovered and will be in service again soon.

The cable-laying ship Mercury was also damaged in a storm of force 11, forcing her to operate for a time on emergency power. But despite all the upsets, the cable-laying was completed six days ahead of schedule which makes quite a change in a world of go-slow or stop.

The other heartening news out of the Cantat 2 saga is that because of the vastly increased number of channels available, the new cable is 20 times cheaper per circuit than the transatlantic cable laid between the UK and USA in 1956. But don't expect the cost of a call to go down.

HI-FI HIT

Hi-Fi, like the motor car, has become the index of a nation's prosperity. But what was astonishing in the good old days of 1973 was the number of equipments advertised to the general public—not the addict—at prices of £200 up, and reportedly selling well. Top weight equipment for the real enthusiast was typically Trio's Package 10

quadraphonic package listed by Lasky's at £460 cash or £577.48 on HP. At the bottom of the pack were plenty of modest units around £30.

A survey of the audio market "Finresearch Audio Industry Service" published by Ovum Ltd. at £30 lists 380 companies active in the audio business which has trebled in size in three years. Such was the boom, according to editor Tony Beaumont, that three new companies have been entering the field every week for the past two years.

First "audio separates" I recall was back in 1937 when I was enchanted with the reproduction of 78 r.p.m. discs on the famous corner horn loudspeaker developed by P. A. H. G. Voigt. But I see Ferguson claiming they "invented" what they call Unit Audio just 30 years later in 1967. Claims and counter-claims in the colour ads are numerous and often funny.

This clearly will not be a good year for the audio business. HP restrictions and a general tightening of belts will see to that. But the audio scene will not collapse. It'll still be comparatively big-biz as well as show-biz.

MAINTENANCE PROBLEM

Try to imagine 15,000 fixed transmitter/receivers of powers from five to 300W and 25,000 mobile vehicle-mounted transmiter/receivers. Tack on 30,000 personal portable transmitter/receivers and 200,000 nickel/cadmium batteries to power them. And just add to that little lot 15,000 pocket alarm receivers and all their batteries.

In round figures, this is the size of the maintenance problem of the Home Office Directorate of Telecommunications which looks after the procurement and servicing of Britain's police and firefighting networks as well as a few others.

The problem was discussed in some detail by A. N. Holdstock in a paper given at "Automatic Testing 73", the first full-scale exhibition and conference to be held on the subject. The magnitude of the Home Office's task was such that automatic testing was seen as a solution as early as 1967. Hold-stock reports several equipments now in full service but reports that no radio equipment manufacturers are yet designing sets with in-field maintenance by ATE as a prime consideration. Consequently, there are always snags in having to build special jigs and adaptors before ATE can be successfully used in the field.

The next big job is provision of ATE for 1,000 alpha-numeric videodisplay terminals now being fitted in police stations throughout the country. Each of them has six large PCBs and 530 TTL integrated circuits.

A new and profitable outlet for ATE on production lines is in the automotive industry. No less than six papers were read on the subject including one on the experience of Ford in checking out car electrical systems. Ford will, in fact, move 100 per cent to ATE for this purpose in the UK during this year.

So successful was "Automatic Testing 73" that organiser John Shearsmith has already announced November 5, 1974, as opening day for the next show. The first exhibition attracted 50 companies and 4,000 visitors. Seven hundred delegates attended the technical conference.

INNOVATION

I have to confess that I was one of the sceptics when Advance Electronics went into the calculator business in mid-1972. Like many others I had underrated their ingenuity.

Advance didn't take the easy path by buying off-the-shelf LSI devices. They designed their own in conjunction with General Instrument Microelectronics and did it in such a way that they could be used in many other applications. So watch out for some competitive lines from Advance in business machines.

MINICOMPUTER LEAGUE

A league table of minicomputer manufacturers prepared by Modern Data in the USA shows Digital Equipment Corporation still way ahead with 16,473 units shipped in 1973. Runner up is Data General with 4,230 and Hewlett Packard in third spot has a score of 2,855, marginally ahead of Varian with 2,337. Honeywell ranks only No. 8 with 1,564 while Texas Instruments, mighty in other fields, is bottom and unlucky thirteenth with 452.

Computer Automation, who came to the market with the concept of the Naked Mini, ranks fifth with 1,915 units shipped in the year. Stripped of all frills, the Naked Mini was offered at a rock-bottom price. Since then CA has offered the "Computer-on-a-card" with the whole package on a single printed circuit board, an even lower priced unit for people who want to build a computer into their own equipment.

Digital Equipment still has the stranglehold in minis that IBM has in the larger machine market. But watch out for increased competition and a re-shuffling of positions lower down the table.

PATENTS BEVIEW...

AUTOMATIC COMMENTARIES

The Secretary of State for Defence has a new British patent (BP 1 325 161) which concerns automatic machines for playing commentaries to accompany exhibits in museums or exhibitions.

The object of the invention is to provide a replay device which works on the closed loop principle and will always be at the correct start point when brought into action by a new listener. This is relatively easy to achieve if the loop is only to play once, but much more difficult to achieve if the listener is to be afforded the opportunity of

when the earpiece is lifted off its rest. The switch is open while the earpiece is on its rest. Amplifier 1 is coupled to the headset earpiece through transformer T1.

When a would-be listener picks up the earpiece S1 closes and the Schmitt trigger changes state to start the tape transport motor. The audio frequencies from the tape are reproduced through the earpiece and used, after rectification, to hold the Schmitt in its active state. This holding action will continue even when the earpiece is returned to its rest.

However, when the audio signals cease, the voltage across C1 dies away and the Schmitt trigger reverts to its former state and the

BP 1 325 161

AMP1

T1

E ARPIECE

R2

R3

R5

TAPE

REPLAY

DEVICE.

listening to the loop more than once.

The tape replay device works with an endless loop of magnetic tape and its audio output passes through the pre-amplifier to two amplifiers, see Fig. 1. The output from amplifier 2 is fed to a simple rectifier circuit, D1 and C1, and passed via R1 to a Schmitt trigger circuit, TR1, TR2. The Schmitt trigger is connected to the power supply and controls operation of the tape replay motor.

The switch S1 is mounted as part of a telephone handset and closes

tape motor stops. Thus the loop stops at its start position. The decay time constant of the voltage across C1 must, of course, be long enough to tide over natural pauses in the commentary.

If the listener wishes to hear the commentary through again, then he keeps the earpiece off its rest; the switch S1 holds the trigger circuit active and the loop is replayed.

The patent specification also details a twin channel system which can be used to control visual displays.

SCORING FOR BOXING AND OTHER Sports BP 1 325 644

Although BP 1 325 644 from E. J. Sweeny of Ohio, USA, is intended primarily for the scoring of boxing matches by judges, its technology will find wider uses.

The specific intention is to enable three judges to score independently with the sum of their points displayed on a common board.

A master console and three identical scoring booths are spaced round a boxing ring with a visual score board mounted above. A single point will be recorded on the score board only after the master console has received a multiple number of point pulses from the individual scoring booths, e.g. three point pulses must be accumulated from one or more booths before a single point is recorded on the board.

The controls within the booths are duplicated for the two fighters.

VEHICLE GUIDANCE BP 1 320 314

Interest appears to be growing in the technology of automatic vehicle guidance. In BP 1 320 314 Autotrack Systems Ltd., and P.C.D. Ltd., jointly describe the automatic remote control of a tractor ploughing a field. The principle of the invention, however, is much more widely applicable, e.g. garden lawn mowing to model car control.

Guide wires are buried half a metre deep and six metres apart along the routes which the vehicle should take. These guides carry a continuous tone current of 2kHz and the a.c. field that this produces is detected by a detector head on the vehicle.

The detector head has a vertical pick-up coil and a horizontal pick-up coil. With the head exactly above the guide wire there is no phase difference between the outputs of the two coils, but if the head is moved to one side a phase difference appears in the appropriate sense and of magnitude proportional to the distance moved.

The two coils in the patented circuit control solenoids for left and right turn and operate pneumatic, hydraulic or electrical steering gear on board the tractor.

Copies of Patents can be obtained from the Patent Office Sales, St. Mary Cray, Orpington, Kent. Price 25p each

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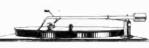
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Phono

Car Aerial

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Log and Lin

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AL10/AL20/AL30 **AUDIO AMPLIFIER MODULES**



similar in their appearance and in their general specification. However, careful selection of the plastic power devices has resulted in a range of output powers from 3 to 10 watts R.M.S.

The versatility of their design makes them ideal for use in record players, tape recorders, stereo amplifiers and cassette and cartridge tape players in the car and at home

Parameter	Conditions	Performance
HARMONIC DISTORTION	Po = 3 WATTS f = 1KHz	0.25%
LOAD IMPEDANCE		8-16Ω
INPUT IMPEDANCE	f = 1KHz	100 kΩ
FREQUENCY RESPONSE -3dB	Po = 2 WATTS	50 Hz-25KHz
SENSITIVITY for RATED O/P	$V_8 = 25V$. $R_1 = 8\Omega$ $f = 1KHz$	75mV. RMS
DIMENSIONS	-	3" × 2½" = 1"

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions.

Parameter	AL10	AL20	AL30
Maximum Supply Voltage	25	30	30
Power out for 2% T.H.D. $(RL = 8\Omega f = 1KHz)$	3 watts RMS Min.	5 watts RMS Min.	10 watts RMS Min

AUDIO AMPLIFIER MODULES

AL 10. 3 watts AL 20. 5 watts AL 30. 10 watts £2·19 £2·59 £3·01

POWER SUPPLIES

PS 12. (Use with AL10 & AL20) SPM 80. (Use with also AL30 & AL3 .50) £3-**25** FRONT PANELS PA 12 with Knobs £1.00

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PA 12. (Use with AL10 & AL20) #4-35 PA 100. (Use with AL30 & AL50) £13-15

TRANSFORMERS

T461 (Use with AL10) \$1.88 P & P 15p T538 (Use with AL20) £1.93 P & P 15p BMT80 (Use with AL30 & AL50) £2:15 P & P 25p

PA12 PRE-AMPLIFIER SPECIFICATION

The PA12 pre-amplifier has been designed to match into match into most budget stereo systems. It is compatible with the match into m AL 10, AL 20 and AL 30 audio power amplifiers and it can be supplied from their associated power supplies. There are two stereo inputs, one has been designed for use with *Ceramic cartridges while the auxiliary input will suit most †Magnetic cartridges. Full details are given in the specification table. The four controls are, from left to right: Volume and on/off switch, balance, bass and treble. Size lå2mm × 84mm × 35mm

20HZ-50KHZ (-3dD)

Bass control—

± 12dB at 60Hz

Trebie control—

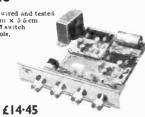
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Input I. Impedance
| Meg. ohin
| Sensitivity 300mV †Input 2, Impedance 30 K ohms Sensitivity 4mV

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The **STEREO 20**

The "Stereo 20" amplifier is mounted, ready wired and tested on a one-piece chassis measuring 20 cm × 14 cm × 5.5 cm. This compact unit comes complete with on/off awitch yolune control, balance, bass and treble controls. volume control, balance, base and treble contransformer, Power supply and Power amps. Attractively printed front panel and matching control knobs. The 'Stereo 20' has been designed to fit into most turntable plintable without interfering with the mechanism or, alternatively, into a separate cabinet. Output power 20w peak. Input 1 (Cer.) 300mV into 1M. Freq. res. 25Hz-25kHz. Input 2 (Aux.) 4mV into 30K. Harmonic distortion. Base control ± 12dB at 60Hz typically 0-25% at 1 watt. Treble con. ± 14dB at 14kHz.



50W pk 25w (RMS)

0.1% DISTORTION! HI-FI AUDIO AMPLIFIER

THE AL50

- ★ Frequency Response 15Hz to 100,000--1dB.
- ★ Load—3, 4, 8 or 16 ohms.
- ★ Distortion—better than ·1% at
- ★ Signal to noise ratio 80dB.

- ★ Supply voltage 10-35 Volts.
- ★ Overall size 63mm 105mm \times 13mm.

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STABILISED POWER **MODULE SPM80**

AP80 is especially designed to power 2 of the AL60 Amplifiers, up to 15 watt (r.m.s.) per channel simultaneously. This module embodies the latest components and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Trainformer MT80, the unit will provide outputs of up to 1-5 amps at 35 volts. Size: 63mm × 105mm × 30mm. These units enable you to build Audio Systems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including:—Disco Systems, Public Address, Intercom Units, etc. Handbook available 10p PRICE £3:25

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Built to a specification and NOT a price, and yet still the greatest value on the market, the PA100 stereo pre-amplifier has been conceived from the latest circuit techniques. Designed for use with the AL50 power amplifier system, this quality made unit incorporates Designed for use with the AL50 power amplifier system, this quality made unit incorporates no less than eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the input stages.

Three switched stereo inputs, and rumble and scratch filters are features of the PA100, which also has a STEREO/MONO switch, volume, balance and continuously variable bass and treble controls.



SPECIFICATION

Bass Control Treble Control Treble Control
Filters: Rumble (High Pass)
Scratch (Low Pass)
Signal/Noise Ratio
Input overload
Supply
Dimensions

100Hz 8KHz better than -65dB

+ 26dB + 35 volts at 20mA 292mm × 82mm × 35mm

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IN 253	0-50	A8 Y27	0.80	BYZ12	0.40	OAZ208	0.40	ZT43	0-25
IN256	0-50	A8Y28	0-25	BYZ13	0-85	OAZ209	0-40	ZT X 107	0.12
IN 645 1N 725 A	0·16 0·20	A8Y29 A8Y36	0.80 0.85	BYZ15 BYZ16	1.25 0.60	OAZ210	0-40	ZTX 108	0.10
1N914	9.06	ASY50	0.20	BYZ88C	4 A 3	OAZ211 OAZ222	0-40	ZTX300	0-14
1N 4007	0-12	A8Y51	0-40	DILLOGO	0.10	OAZ223	0-45 0-45	ZTX 304	0-24
18113	0.25	ABY53	0.80	BZY88C	3 V 3	OAZ224	0-45	ZTX500 ZTX503	0·15 0·16
18131	0.18	ASY55	0.20		0.10	OAZ241	0-25	ZTX531	0.25
18202	0.28	A8 Y62	0-25 0-88 1-00	C111 .	0.55	0AZ242	0.15	LIAUUI	0.00
26371	0.40	ASY66	0.88	CR81/05	0.80	0AZ244	0-25	INTEGRA	TED
2G381	0.22	ASZ21	1.00	CR81/40	0-45	OAZ246	0-15	CIRCUIT	3
2G414	0.80	ASZ23	0.75	CB4B	1.90	OAZ290	0.88	7400	
2G417	0.25	AU101	1.50	C810B	8-50	OC16	1.00	7401	0.20
2N404	0.22	AUY10	1.00	DD000	0.15	OC16T	1.00	7402	0.20
2N697	0.15	BC107	0.18	DD003 DD006	0.15	OC19	0.50	7403	0.20
2N698	0.80	BC108 BC109	0-12 0-12	DD007	0-25 0-40	0C20 0C22 0C23	2.00 1.00	7404	0-20
2N706 2N706A	0-10 0-12	BC113	0.18	DD008	0.88	0022	1.25	7405	0.80
2N708	0.15	BC115	0.20	GD3	0-88	0023	1.10	7406	0.40
2N709	0.40	BC116	0.20	GD4	0.10	0C24 0C25	0.40	7407	0-40
2N1091	0.55	BC116A	0-28	GD5	0.88	1 OC26	0.40	7408	0.25 0.88
2N1131	0.25	BC118	0.20	GD8	0.95	0C28 0C29	0.70	7409	0.88
2N1132	0-25	BC118 BC121	0.20	GD12	0.10	OC29	0.65	7410	0.20
2N1302	0.18	BC122	0.20	GET102	0.50	OC30	0.40	7411	0.88 0.88
2N1303	0.18	BC125	0.68	GET103	0-40 0-85	OC35	0.55	7412	0.80
2N1304	0.22	BC126 BC140	0.65	GET113	0-85	OC36	0.65	7413 7416	0.80
2N1305	0.22	BC140	0.55	GET114 GET115	0.80	0C41	0.85	7417	A. 90
2N 1306 2N 1307	0.28 0.28	BC147 BC148	0·12 0·10	GET116	0.75 0.85	OC42 OC48	0-40	7420	0.20
2N1308	0.28	BC149	0.12	GET120	0.50	0C44	0.18	7422	0.28
2N2147	0.75	BC157	0.14	GET872	0.80	OC44M	0.17	7423	0.20 0.28 0.40
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2N2218	0.88	BC169	0.14	GET881 GET882	0.25	OC46	0.27	7428	0-48
2N2219	0.25	BCY31 BCY32	0-45	GET882	0.85	OC57 OC58	0.60	7430 7432	0-20
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2N2904A 2N2906	0.20	BCY40 BCY42	0.80	GJ5M	0-25	OC72 OC73	0.50	7442	0-85
2N2907	0.58	1 HCY70	0.15	GJ7M	0.50	1 OC74	0.80	7450	0.80
2N2924	0-18	BCY71 BCZ10	0.80	HG1005	0.50 0.20	OC75 OC76	0.80	7451 7453	0.80
2N2925	0.15	BCZ10	0.80	H8100A	0-20	OC76	0.80	7454	0.20
2N2926	0.10	BCZ11	0.65	MAT100 MAT101	0.20	OC77	0.55	7460	0.80
2N3054	0.50	BD121	1.00	MAT120	0-25	OC78 OC79	0-25 0-30	7470	0.88
2N3055	0.80	BD123 BD124	0.80	MAT121	0.25	0079	0.88	7472	0.88
2N3702	0-11 0-15	BDY11	1.45	MAT121 MJE520	0-85	0C81D	0.88	7473	0.44
2N3705 2N3706	0.11	BF 115	0.28	MJE2955	1.10	OC81M	0.20	7474	0-48
2N3707	0.18	BF117	0.50	MJE3055	0-75	OCSIDM	0.18	7475	0.59
2N 3709	0-10	BF167	0.25	MPF102	0.40	OC81Z OC82	0.45	7476	0-45
2N3710	0-11	BF173 BF181 BF184	0-88	MPF103	0.80	OC82_	0.28	7480 7482	0.87
2N3711	0.11	BF181	0-85	MPF104 MPF105	0-85 0-46	OC82D OC83	0-25	7483	1.20
2N3819	0.85	BF184	0.22	NKT128	0-45	0083	0.88	7484	1.00
2N 4289	0.20	BF185	0-22 0-18	NKT129	0.80	0084	0-80 0-88	7486	0.50
2N5027	0.58 0.88	BF194 BF195	0.18	NKT211	0.25	OC114 OC122	1.00	7490	0-75
2N5088 28301	0.59	IRRIGE	0.15	NKT213	0-85	OC123	1.10	7491A	1.10
26304	1.15	BF197	0.15	NKT214	0.24	OC123 OC139	0-40	7492	0-75
28501	1·15 0·75	BF861	0.25	NKT216	0-40	OC140	0-65	7493	0.75
26703	1.00	BF898	0.25	NKT217	0-45	OC141 OC169	0.80	7494 7495	0-85
AA129	0.20	BFX12 BFX13	0.20	NKT218	1.18	OC169	0.80	7498	0.85 1.00
AAZ12	0.75	BFX13	0.88	NKT219 NKT222	0.88	1.001170	0-25	7497	4.82
AAZ13	0.10	BFX29 BFX30	0-28 0-28	NKT224	0-80 0-88	OC171 OC200 OC201	0.80	74100	8.16
AC107	0.85 0.85	BFX 85	0.98	NKT251	0.24	00200	0-55 0-80	74107	0.51
AC126	0.25	BEYES	0.50	NKT251 NKT271	0-20	00201	0-90	74110	0.57
AC127 AC128	0-25	BFX63 BFX84	0.25	NKT272	0.20	OC202 OC203 OC204	0.55	74111	0.86
AC187	0-20	BFX85	0.28	NKT273	0.20	OC204	0-85	74118	1.00
AC188	0.20	BFX86	0.25	NKT274	0.20	OC205	1.00	74119	1.92
ACY17	0.85	BFX87	0.25	NKT275	0.25	OC206	1·10 1·00	74121 74122	0.57
ACY18	0-27	BFX 88	0.22	NKT277	0-20 0-25	OC206 OC207		74122	0-80 1-44
ACY19	0-27	BFY10	1.00	NKT278 NKT301	0-25	OC460	0.20	74141	1.00
ACY20	0-22	BFY11	0-50 0-40	NKT904	0.75	OC470 OCP71	0-80 1-00	74145	1-44
ACY21	0.88	BFY17 BFY18	0.40	NKT409	0-70	ORP12	0.55	74145 74150	2.80
ACY22	0.16	BFY19	0.55	NKT304 NKT403 NKT404	0-70 0-80	ORP12	0.45	74151	1.15
ACY27 ACY28	0-25 0-25	BFY24	0-45	NKT678	0.80	ORP61	0.48	74154	2.80
ACY89	0.85	BFY44	0.55 0.45 1.00	NKT713	0.80	PIC44	0.29	74155	1.15
ACY40	0.22	BFY50	0.20	N B.T773	0.25	8X68	0.80	74156	1.15
ACY41	0.88	BFY51	0.80	NKT777	0.88	8X631	0.45	74157	1.09
ACY44	0.88	BFY52	0.20	078B	0.38	8X 635	0.55	74170	2.88
AD140	0.50	BFY53 BFY64	0-17	OA6 OA47	0·12 0·08	8X640	0.75	74174	1.80
AD149	0.50	BFY90	0-45 0-75	0A70	0.10	8X641 8X642	0-75 0-60	74175	1-29
AD161	0-89	B8X27	0.50	OA71	0-20			74176	1.44
AD162	0.89	B8X 60	0.88	OA73	0-15	8X644 8X645	0-85 0-85	74190	2-80
AF106 AF114	0-80	B8X76	0.18	OA74	0-15	TIS43	0.26	74191	2-80
AF115	0.25	BSY26	0.17	OA79	0.10	V15/30P	0.75		2.80
AF116	0.25	BSY27	0.20	OA81	0.10	V30/201P	0.75		2.80
AF117	0-20	BSY51	0-50	OA85	0.15	V60/201	0-50	74194	1.72
AF118	0.50	BSY95A	0.18	OA86 OA90	0.15	V60/201P	0.75		1.44
AF119	0.80	BSY95	Q-18	OA90 OA91	0.07	XA101	0.10	74195	1.58
AF124	0.80	BT102/50	0·75	OA95	0.07	XA102	0.18	74196	
AF125	0-80	BTY42	0.92	OA200	0-08	XA151 XA152	0·15 0·15	74197	1-58
AF126 AF127	0-80	BTY79/10	10 R	OA202	0.10	XA161	0.25		3.16
AF189	0-88		0.75	OA210	0.80		0.25	74199	2-88
AF178	0.55	BTY79/40	00R	OA211	0.25	XA162		Dlug !	leat-
AF179	0-65	D1/1-0	1.10	OAZ200	0.50	XB101	0-48	Plug in soc	mets
AF180	0.55	BY100	0.15	OAZ201	0.45	XB102	0.80	—low profi	46
AF181	0-50	BY126	0-14	OAZ202	0-45	XB103	0-85	p.m 211	0.15
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Model 320

D

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Pair crocodile clips 1 red. I black insulated sleeve 79.

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0/6/30/1200V DC
0/6/30/1200V DC
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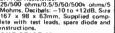


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High sensitivity, overload protected.
20,000opv. Ranges.
0,6/1,2/3/12/30
60/120/600/120/600/120/600/120/600/120/600/000
DC. 3/6/15/60/150/
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20,000pv, Overload
20,000pv, Overload
20,000pv, Overload
20,000pv, Overload
20,000pv, Overload
250/500/1000v AC
250/500/1000v AC
Current: 50uA/1/5/
25/100mA/0.5/2.5A
C. 5/25/100mA/
0.5/2.5A AC. Resista
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P&P 35o

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AC. 3/10/50/250/1000W
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PS200 Regulated POWER SUPPLY UNIT Solid state, Variable output 5 – 20V DC up to Ampute 10 – 10 monitor voltage and current. Output 220/240V AC. Size: 190 x 136 x 98mm.

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USED EXTENSIVELY BY INDUSTRY, GOVERNMENT DEPARTMENTS, EDUCATIONAL AUTHORITIES ETC. Over 200 ranges in stock—other ranges to order, Quantity discounts available. Send for fully illustrated brochure.

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10V DC 20V DC 50V DC 300V DC

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300V AC S Meter 1 m A ... VU Meter 1A AC 15A AC 10A AC 20A AC 30A AC

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type, all others are Moving Coil CLEAR PLASTIC MODEL SD830 Size: 110 x 83mm

£3.75 £3.70 £3.65 £3.45 £3.75 £3.70 £3.40 £3.40 £3.40 £3.40 £3.40 £3.40 £3.40

CLEAR PLASTIC MODEL 45P Size: 50 x 50mm

£3.00 £2.85 £2.75 £2.70 £2.90 £2.65 £2.65 £2.65 £2.65 £2.65 £2.65 £2.65 £2.65 £2.65 £2.65 £2.65 £2.65 £2.65 £2.65 £2.65 £2.65 £2.70

CLEAR PLASTIC MODEL 38P Size: 42 x 42mm

Size: 110 x 83m
50uA
100uA
200uA
200uA
500uA
500uA
500uA
100-0-100uA
100-0-100uA
100mA
50mA
100mA
50mA
500mA
100mA
500mA
10 DC
5A DC
10A DC
5V DC

Size: 50 x 50mi

50uA ...
100uA ...
200uA ...
50uA 500uA ...
100-B-100uA ...
50u-B-500uA ...
100-B-100uA ...
100-B-100uA ...
100-B-100uA ...
100-B-100uA ...
100mA ...
100mA ...
100mA ...
100mA ...
100mA ...
100mC ...
200

CLEAR PLASTIC MODEL SD640 Size: 85 x 64mm

			£3.35
100u A		٠.	£3.30
200u A			£3.30
500u A			€3.25
50-0-50u			£3.35
100-0-10			£3.30
1mA		٠	£3.20
5mA	••		£3.20
			£3.20
10mA		••	
50mA			£3.20
100mA			£3.20
500mA			£3,20
1A DC			£3.20
5A DC			£3.20
10A DC			€3.20
5V DC			€3.20
0.00	•••	•••	



State Days	1000
20V DC	 £3,20
50V DC	 £3.20
300V DC	 £3.20
15V AC	 £3.30
300V AC	 £3.30
VU Meter	 £3.45

CLEAR PLASTIC MODEL SW100 Size: 100 x 80mm

50uA			£4.55
			£4.35
500u A			£4.10
50-0-50u			£4.35
100-0-10	Ou A	١	£4.30
1mA			£3.95
1A DC			£3.95
5A DC			£3.95
20V DC			£3.95
50V DC			£3,95
300V DC			£3.95



EDGWISE MODEL PE70

Size: 90 x 34mm	
50uA	£4,15
100uA	£3.95
200u A	£3.75
500u A 50-0-50u A	£3.50 £3.95
50-0-50uA 100-0-100uA	£3.85
1mA	£3.50
300V AC	£3.50
VU Meter	£4.25



MODEL ED107 EDUCATIONAL METER Size: 100 x 90 x 150mm including terminals

moving condens of the search o	oil i sch d o ons. e m asil	nstr icol ithei 3" neter	experi- bench mirror move- cessible
50u A 100u A 50-0-50u 1A DC 5A DC 5V DC 10V DC 15V DC 20V DC 50V DC	A		£7.60 £7.05 £7.05 £6.55 £6.55 £6.55 £6.55 £6.55 £6.55



£7.05 £6.55 £6.55	WHEN THE PARTY OF	
£6.55	300V DC	£6.5
£6.55	500mA/5A DC	£7.7
£6.55	5V/50V DC	£7.7
£6.55	5V/15V DC	£7.7
£6.55	1A/15A DC	£7.7

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240° Wide Angle 1mA METERS MW 1-6 60x60mm

£3.97 P&P 15p

£4.97

MW 1-8 80×80mm

P&P 15p

Size: 120	χţ	10m	m
50uA			£4,85
100u A			£4.70
200u A			£4,45
			£4,30
50-0-50u A			£4.70
100-0-100			£4.45
500-0-500	λuΑ		£4.30
1mA			£4.30
1-0-1mA	**		£4.30
5mA			£4.30
10mA		**	£4.30
50mA			£4.30
100mA			£4.30
500mA			£4.30
1A DC			£4.30
5A DC			£4.30
15A DC			£4.30
30A DC		**	£4.35
10V DC		••	€4.30
20V DC			£4.30
50V DC			£4.30
150V DC	**		£4.30



4.30	THE PERSONS	
4.30		
4.30		
4.30	300V DC	£4.30
4.30	15V AC	£4.35
4.30	300V AC	£4.35
4.30	S Meter 1mA	£4.30
4.30	VU Meter	£5.00
4.35		° £4.30
4.30	5A AC	 £4,30
4.30	10A AC	 £4.30
4.30		 £4.30
4.30	30A AC	 £4.30

£2.80 £2.765 £2.65 £2.50 15V DC ... 20V DC ... 50V DC ... 150V DC ... 150V DC ... 300V DC ... 750V DC ... 750V DC ... 50V AC ... £2.50 £2.50 £2.50 £2.50 £2.50 £2.50 £2.55 £2.55 £2.55 £2.55 £2.55 £2.55 £2.55 CLEAR PLASTIC MODEL SD460 Size: 59 x 46mm 50u A 100u A 200u A 500u A £3.10 £3.05 £3.00 £2.80 £3.10 £3.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 200u A 500u A 50-0-50u A ... 100-0-100u A ... 1mA ... 5mA ... 50mA ... 100mA 500mA 1A DC 5A DC 10A DC 5V DC

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AUTO TRANSFORMERS 0/115/250V, Step up or step down. Fully shrouded.

10V DC 50V DC 300V DC 15V AC



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£2.85 £2.85 £2.85 £3.00 £3.00 £3.20

CLEAR PLASTIC MODEL 65P Size: 86 x 78mm





2.85 2.85 2.85 2.85 2.85 2.85	
2.85	50V AC £3.10
2.85	150V AC £3.10
2.85	300V AC £3.10
2.85	500V AC £3.10
2.85	S Meter 1mA £3.15
2.85	VU Meter £4.10
3.10	1A AC * £2.85
3.20	5A AC £2.85
2.85	10A AC * £2.85
2.85	20A AC * £2.85
2.85	30A AC • £2.85
2.85	50mA AC • £2.85
2.85	100mA AC * £2.85
2.85	200m A AC * £2.85
3.10	500m A AC * £2.85

BAKELITE MODEL S80 Enlarged Window

SIZE. OU X	or	251111	
			£3.85
100⊔A			£3.75
500u A			£3.35
50-0-50u	۹.		£3.75
100-0-100)u/	۸	£3.65
1mA			£3.00
1A DC			£3.30
5A DC			£3.30
20V DC			£3.30
50V DC			£3,30
300V DC			£3.30
300V AC			£3.30
VU Meter			£4.05



CLEAR PLASTIC MODEL 52P

GIZE. 00 x 0011	
50uA	£3.85
100u A	
500u A	£2.90
50-0-50uA .	
100 0 100u A	
1mA	
5mA ,	£2.75
10mA	
50mA	
100mA	. £2.75
500mA	
1A DC	. £2.75
5A DC	
10V DC	. £2.75
20V DC	£2.75
50V DC	
300V DC	
15V AC	£2.85
300V AC	



5			195		
5	S Meter 1	mA	١		2.85
5	VU Meter				3.95
5	1A AC				2.75
5	5A AC				2.75
5	10A AC				2.75
5	20A AC				2.75
5	30A AC			* £	2.75

BAKELITE MODEL 65 Size: 80 x 80mm

50uA	£5.05 £3.90 £3.30 £3.30 £3.35 £3.30 £2.85 £2.85 £2.85 £2.85	AA AA
50mA	£2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85	30V AC



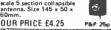
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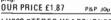
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Complete with
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Moving coil, Ideal for language teaching, OUR PRICE £5.95 P&P 30p



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TRIO JR599 RECEIVER



Nine wwo bands covering 1.8-29.7 MHz, 144 - 465MHz of 10MHz WWV SSB, CW, AM and Fin. AF cotput is more than 1 watt. S Mater. Squelch control. BFO. Variable AF and RF controls. 4-16 ohm output and jack for phones. Power requirement 100/ 240V AC, 12/14V OC. Size: 270 x 140 x 310mHz

Our Price £132.50 PART TRIO 9R590S RECEIVER

AND SHOW SHOWING



Four bands covering 550kHz to 30 MHz continuous and electrical bands spread on 10, 15, 20, 40, and 800 ks spread on 10, 15, 20, 40, and 800 ks spread on 10, 15, 20, 40, and 800 ks spread on 10, 15, 20, 40, and 10 ks spread band spread to speak SSE-CW, ANL, variable BFO. S Meter and separate band spread tolal. IF frequency 445kHz, audio output 1½ watt. Variable RF and AF gain controls. 115/250V AC, with instructions.

Our Price £42.50 PARO



Covers 3.5, 7, 14, 21, 28, 28.5 and 29 1MHz bands and WWV 15MHz. SSB, AM and CW. AF output more than 1W. Crystal controlled BFO for SSB. S Meter, ANL etc. AC 110/120–220/240V. Size: 330 x.179 x.310mm. OUR PRICE £75.00 Carr. paid

TRIO TR2200 TRANSCEIVER

Fully transistor ised portable VHF transceiver Will transmit and receive on six channels between 144–146MHz. 1 watt trans-mitter. 12V DC internal or ext-ernal supply. Built-in charger for Ni-Cad cells. for Ni+Lad cells.

Power/volume
switch, squelch control, channel selector, mic. socket, earphone/external
speaker socket. Complete with microphone and 144.48. 144.72 & 145.32
crystals. Size: 134 x 58 x 180mm.

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UNR30 RECEIVER



Four bands covering 550 KHz/30MHz BFO, Built-in speaker, Operates from 220/240V AC, Brand new with instr-

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BELTEK W5400 CAR TRANSCEIVER



Solid state mobile transcrier for 12 volt DC neg. Transmits and receives on any 12 of 28 channels between 144 and 146MHz. Power output 10W and 1W switchable. Controls: On/off volume, squeich and channel selector. Internal 3" speaker, Complete state of crystals for 144.48, 144,6 rese state of crystals for 144.48, 144,6 rese state of crystals for 144.48, 144,6 rese than 145MHz, mounting bracket and instructions. Size: 150 x 70 x 220mm. OUR PRICE £75.00

LAFAYETTE HA600 Receiver



General coverage 150-400kHz, 550 kHz-30MHz. FET front end 2 mechanical filters, product detector. Noise limiter, variable BFO, S Meter, Bandspread and RF gain, 220/240V AC or 12V DC. Brand new with instructions. OUR PRICE 650 00 P&P 50p

BVD5 Vernier TUNING DIAL BV US VERNIER I UNING UTAL App. 7:1 ratio planetary drive vernier dial, Log scale 0 – 180 degrees. Blank scales 1 – 5. Dial size 128 x 76mm. Overall size 190 x 117 x 41mm. deep including knob and coupling. X" diam. shaft OUR PRICE £1.62 P&P 15c

AUDIOTRONIC AHA101 Stereo Headphone Amplifier

All silicon.

remotive roper atter from mag netuc, ceramic or tuner netuc, ceramic or tuner netuc, ceramic or tuner separate volume controls for each channel. Operates from 9V battery. INPUTS. 5mW yer channel. OUTPUT: 50mV per channel.

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EMI LOUDSPEAKERS Model 350 13 x 8" with single tweeter/crossover 20-20,000Hz, 15 watts RMS, Available 8 or **OUR PRICE** £7.25 each P&P 37p Model 450 13 x 8" with twin tweeter/crossover 55-13 000Hz, 8 watts RMS, Available 8 or 15 ohn

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Built-in driver unit. Impedence 16 ohms. Power rating 10W. Response 380-7000Hz. Size app. 6" x 6". Weather and shock protected. OUR PRICE £4.97

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STEPEUSUUN Matched pair of stereo bookshelf speakers. Deluxe teak veneered finish. Size: 368 x 229 x 190mm. 8 ohms. 8 watts RMS, 16 watts peak. Complete with Din lead.



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27 y 9V DC.,

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E1 100mW output stage.,

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Recorder, 2 track BSR deck

2 track BSR deck with push button controls for easy operation. Tape counter and volume control Complete with hand microphone, direct recording lead, 1,200′ reel of tape and spare reel. 200/250V AC. Fully guaranteed. **OUR PRICE £17.50** P&P 75p

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Master and two sub-stations. Can be used on desk or wall mounted, Complete with cable and batteries DUR PRICE 65.25 P&P 50p SINCLAIR CAMBRIDGE CALCULATOR

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Output 125mV.
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MP7 MIXER-PREAMPLIFIER MP7 MIXER-PREAMPLIFIER
5 Microphone
inputs each with
individual grain
controls anabling
controls anabling
facilities. Battery operated. Size: 235
x127 x 76mm. Inputs: Mics, 3 x 3mV
50k; 2 x 3mV 50k; 2 x 3mV
50k; 2 x 3mV
60k; 2 mr. Phono. Mag,
4mV 50k; Phono Ceramic 100mV 1
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Z40 Power Amplifier
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6 transistor 6 transistor high quality tuner. Size only 153 x 101 x 63mm 3 IF stages. Double tuned discriminator.



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Specification as above FM chassis but complete in cabinet with on/off switch. Size: 184 x 86 x 127mm,

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alarm sleep switch. Illuminated rotary dial with hours, minutes and seconds. Automatically turns off radio, TV, light etc. and with auto-switching will turn on again when required. 2dOV AC operation. Switch rating 2015, 20

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BINATONE OS100 Digital

EINAL UNIE USTUD Ulgstal
Clock
240V mains
operation.
lvory case
with large
clear numbers
for hours,
minutes and seconds. Saxe 159 x 76 x
82mm.

OUR PRICE £4.50

PRP 30n



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Global AM/FM Portable Radio
1 www-bands
535—160fkHz.
LW: 150—380
Hz. MB 1.64MHz. SW1:
6-24MHz.
PSB1: 30—50
HMz. PSB2: 148—174MHz. FM.88—
108MHz. Air: 108—136MHz. Fasture
time zone map and timing dial. Linguist
navial. AFC on FM. 6" 'A" 'speaker
and parsonal earpice. Battery/mains
operation. Size: 345 x 133 x 305mm.
HIR PRIEC £36.00 P&P 500

OUR PRICE £36.00

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Noise Reduction Units
Reduce tape hiss by 3dB at 600Hz,
6dB at 1200Hz and 10dB for all frequencies above 3000Hz. Size: 460 x
203 x 79mm AC 220/240V



PROCESS 4

For use with semi-professional tape recorders. Frequency response 30Hz -20kHz ±2dB. S/N better than 70B. Full source/tape monitoring. Switchable multiplex filter. Supplied with test tape.

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FOULESS 2
For use with cassette and tape recorders. Frequency response 30Hz – 20kHz
Switchable multiplex filter. 2 Dolby
calibration meters. Off tape monitoring. S/N better than 70dB. Supplied
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CT5050 Cassette Recorder



Instant recording and playing, Piano key controls, Automatic level control. Built-in speaker, Complete with remote control microphone, carrying case and shouluer strab.

OUR PRICE £8.50 P&P 50p

AUDIOTRONIC ACD660 Stereo Cassette Deck



A beautifully styled four track stereo deck with an outstanding specification of fered at a remarkably low price. Incorporates a host of features including switchable noise filter, normal/chrome tape selector, twin VU meter slider record/playback level controls, front panel headphone socket, recording indicator lamp, phono/Uni line interest lamp, phono/Uni line in

OUR PRICE £39.50 P&P 50o AUDIOTRONIC LOW NOISE CASSETTES TYPE C60 C90 C120 10 £2.61 £3.70 £4.50 5 £1.37 £1.95 £2.38 AUDIOTRONIC CrO2 CASSETTES

5 £3.41 £4.63 CR60 CR90 £6.72 £9.19 AUDIOTRONIC 8 TRACK CARTRIDGES

Each 75p 99p 5 £3.50 £4.70 P&P Cassettes 3p, Cartridges 5p each OVER 10 of either POST FREE!



SKYFON 100mW OUR PRICE £24.95 per pair P302 Two Channel 300mW OUR PRICE £52 50 per pair P1003 Three Channel 1 Watt OUR PRICE £71.25 per pair P&P 50p per pair

NB. Licence required for use in UK

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For balancing
and gain selection
of loudspeakers
with additional
facility for stereo
headphone
switching. Wo
witching. Wo
witching. Wo
witch, stereo headphone socket.

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HEADPHONES LSH20 Individual volume controls. Stereo/mono switch. 8 ohms. 40-19,000Hz. **OUR PRICE** £3.75 P&P 30p



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AMPLIFIER Self contained transistorised, battery operated Simply plug in microphone, guitar your amplifier. V depth of reverbera walnut cabinet. 1 ol. Beau 108mm OUR PRICE £7.50 P&P 20p

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High quality 2 way speaker systems 25 Watts, 4-8 ohms, 40Hz-18kHz Size 560 x 340 x 255mm, approx

Wood grain finish with black	fronts.	6
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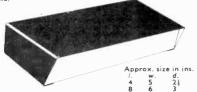
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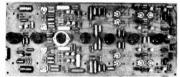
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(PE Nov. 70/Mar. 71) Stereo Sets & PCBs. Pre-amp—S/c/s. £1-80. Rs, Cs, Pots and Sw's—with \(\frac{1}{2}\) WO Rs, £11-32—with \(\frac{1}{2}\) Wo r\(\frac{1}{2}\) WC Fs, £9-60. PCB (3\(\frac{1}{2}\) in x 10\(\frac{1}{2}\) in y or sets with MO and \(\frac{1}{2}\) WS, £1-80 holds rotary or slider pots and Maka-Sw's, £1-90, Main Amp—Rs, Cs, Pots, £5-39. PCB (3\(\frac{1}{2}\) in x 5in), £1-15. PSU—Rs, Cs, Pot, £3-97, PCB (2\(\frac{1}{2}\) in x 4in), 65p.

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CS, Fot, £3-97, FCD (£11 × 7111), 53p.

GEMINI STEREO TUNER
(PE Apr./Jun. 72). PCB as publ., £1-50.

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(PE Apr. 69). S/c's, Rs, Cs, Pots, PCB (3½ in × 7½ in) (Stereo) also holds rotary or slider pots and Sw. £1-50. Main Amp—spec or 4 slider pots, £3-70.

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(PE Mar./Apr. 73). S/c's, i.c.'s, Rs, Cs, Relay and pe-bases, Pot Cores and pe-bases, Sw's, Pots, Panel Lamp—Mono, £11-80; Sereo, £18-70. PSU, rolds relay and cores, £1-85. PCB—Main Circuit (3½ in × 9 in) (Stereo) also lods Sw, Rs, Cs, Presets and mounts on Sw's, 80p.

REVERBERATION UNIT

(PW Nov./Dec. 72). S/c's, Rs, Cs, Rotary Posts, 7/fmr, £6-44: PCB (2in × 11½in) also holds sliders, £1-20. 9in Spring Unit, £3-75.

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(PW Sept. 70). Incl. Mic P/A, 2-Guitar P/A, Trem and Tone Controls, Master Volume. S/c's, Rs, Cs, LDR, Rotary Pots, Lamp, Coupling T/fmr, £6-97. PSU, £3-57. PCB (3½in × 10½in) Mk. 2, also holds 7 rotary or slider pots, £1-75.

ULTRASONIC
TRANSMITTER-RECEIVER
(PE May 72). S/c's, Rs, Cs, Pot,
Relay, Dual PCB (2in × S\(\frac{1}{2}\)in), £3-90.
T/ducers excluded.

ALSO
CBs as published (while stocks last)

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3p 3p 3p 3p 3p

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4PCO 12V £1-30
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Clip 20p
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6-9V 85p

12p

Relay 85p

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(PE Feb. 72). S/c's, Rs, Cs, Pot, PCB
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PCB (I½in × 2½in), £3·30.

VERSATILE LIGHT EFFECTS UNIT
Single Channel Sound Controlled Light with built-in variable strobe. (PE June 72). S/c's, Rs, Cs, Pots, T/fmrs, Keyswitch, £10-38, PCB (3‡in x 7‡in) Mk. 2, also holds pots, Sw, T/T7 T/fmr, £1-50, SCRs—1A, 50p.

PHOTOPRINT PROCESS
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(PE Jan./Feb.72). For colour and B & W
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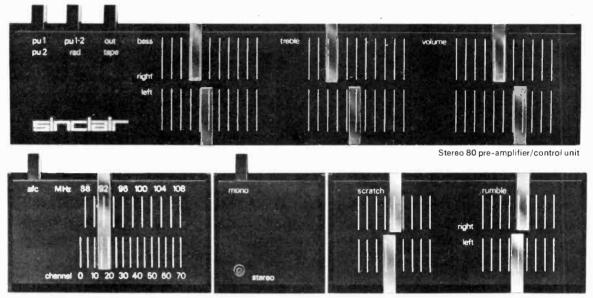
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Sinclair Project 80 exciting



Project 80 tuner

Stereo decoder

Project 80 Active Filter Unit (AFU)

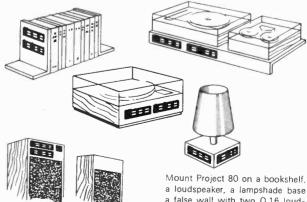
only $\frac{3}{4}$ " deep x 2" high

Living with hi-fi takes on new meaning with Sinclair Project 80. The electronics of these revolutionary new modules are all contained within elegantly designed matching cases no more than three-quarters of an inch deep. They are designed for mounting on any appropriate flat surface by means of 6BA bolts extending from the rear of each module and which pass through suitably drilled holes. Connections are taken away out of sight in a similar manner. The possibilities opened up by Project 80 are endless - superb hi-fi systems can be installed in ways hitherto only dreamed about and never before made practical. No more cutting out and shaping to put modules in position. A few holes drilled with the aid of templates supplied and the job is done. Now you need never again be faced with problems of keeping the hi-fi from clashing with carefully thought-out furnishing schemes. (That will surely please wives!) Slider controls have been introduced in place of knobs and all modules in the range incorporate new up-dated circuitry with emphasis on performance standards and built-in protection against overload and shorting. The aim was to re-think modular construction completely - to make it infinitely more versatile, even simpler and more reliable – the result – Project 80 – another triumph for Sinclair, and the most exciting construction modules ever,

the slimmest, most elegant hi-fi modules ever made

System	The Units to use	Units cost
Simple battery record player	Z.40	£5-45 +54p V.A.T.
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50W (8 Ω) RMS continuous sine wave de luxe stereo amp		£33-83 +£3.38 V.A.
Indoor P.A.	Z.60, PZ.8	£14-93 +£1.49 V.A.

Project 80 FM tuner, decoder, and A.F.U. may be added as required



a false wall with two Q.16 loudspeakers . . . almost anywhere.

Practical Electronics March 1974

new thinking in modular hi-fi

Stereo 80 pre-amplifier and control unit ■ For P U radio and tape Tape monitoring switch Simplest ever fixing

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TECHNICAL SPECIFICATIONS

Size $-260 < 50 \times 20$ mm $(10\frac{1}{4} \times 2 \times \frac{3}{4} ins)$

Finish – Black with white indicators and transparent Sliders Inputs – Magnetic pick-up 3mV RIAA corrected; Ceramic pick-up 300mV

Radio 300mV; Tape 30mV

Signal/noise ratio -- 60db Frequency range -- 20Hz to 15KHz ± 1dB . 10Hz to 25KHz ± 3dB

Power requirements – 20 to 35 volts
Outputs – 100mV + AB monitoring for tape
Controls – Press button for tape radio and P.U. Sliders for volume,
bass (= 12dB to – 14dB at 100Hz) treble (+ 11dB to – 12dB at 10KHz)

R.R.P. £11.95 +£1.19 V.A.T.

Project 80 FM tuner

and stereo decoder





R.R.P. £11.95 $^{+£1\cdot19}_{V.A.T.}$

R.R.P. £7.45 $^{+0.74}_{VAT}$

Twin dual varicap tuning: 4 pole ceramic filter: switchable A.F.C.

On the decoder, solid state stereo indicating

Making the Project 80 F.M. tuner and decoder available separately gives a wider choice of systems and saves money where stereo reception may not be required. The tuner is a triumph of electronic design and assures excellent performance. The decoder gives a 40dB channel separation with 150mV output per channel. Both units may be used with other than Project 80 systems.

TECHNICAL SPECIFICATIONS OF TUNER

Size $-85 \times 50 \times 20 \text{mm} (3\frac{1}{2} \times 2 \times \frac{2}{4} \text{ins})$ Tuning range -87.5 to 108 MHzDetector -1.C balanced coincidence for good A.M. rejection

One I.C. equal to 26 transistors

Distortion - 0.2% at 1 KHz for 30% modulation

4 pole ceramic filter in I.F. section Aerial impedance $-75~\Omega$ or 240-300 $~\Omega$

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Power requirements - 23 to 33 volts

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Practical Electronics March 1974

Z.40 & Z.60 power amplifiers totally short-circuit proof





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Z.40 TECHNICAL SPECIFICATIONS

Size – $55\times80\times20$ mm ($24\times34\times\frac{3}{4}$ ins) 9 transistors Input sensitivity – 100mV

Output – 15 watts RMS continuous into 8 Ω (35v)

Frequency response -10Hz -100KHz ± 1 dB Signal/noise ratio -64dB

Distortion – at 10 watts into 8 Ω less than 0.1% Power requirements – 12 to 35 volts

Z.60 TECHNICAL SPECIFICATIONS

Size $-55 \times 98 \times 15$ mm ($2\frac{1}{4} \times 3\frac{3}{2} \times \frac{3}{8}$ ins) 12 transistors Input sensitivity -100-250mV

Output – 25 watts RMS continuous into 8 Ω (45V)

Distortion - typically 0.03%

Frequency response -10Hz to more than 200KHz ± 1 dB

Signal/noise ratio - better than 70dB Built in protection against transient overload and short circuiting Load impedance – 4 $\,\Omega$ min, max safe on open circuit

Z.40 R R P. £5.45 + 0 54 V A T; Z.60 R R P. £6.95 + 0.69p V.A.T.

Project 80 active filter unit

Makes a highly desirable part of any worthwhile system where inputs may be from record, radio or tape. As with Stereo 80, separate controls applied to each channel make it easier to obtain ideal stereo balance.

TECHNICAL SPECIFICATIONS

Size $= 108 \times 50 \times 20$ mm ($4\frac{1}{4} \times 2 \times \frac{3}{4}$ ins) Voltage gain = minus 0.2dB

Frequency response – 36Hz to 22KHz controls minimum Distortion – at 1 KHz – 0.03% using 30V supply HF cut off (scratch) – 22KHz to 5.5KHz, 12dB/oct. slope

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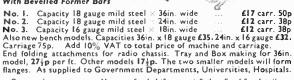
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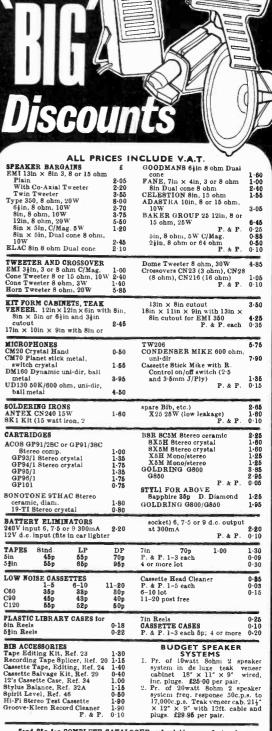
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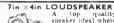
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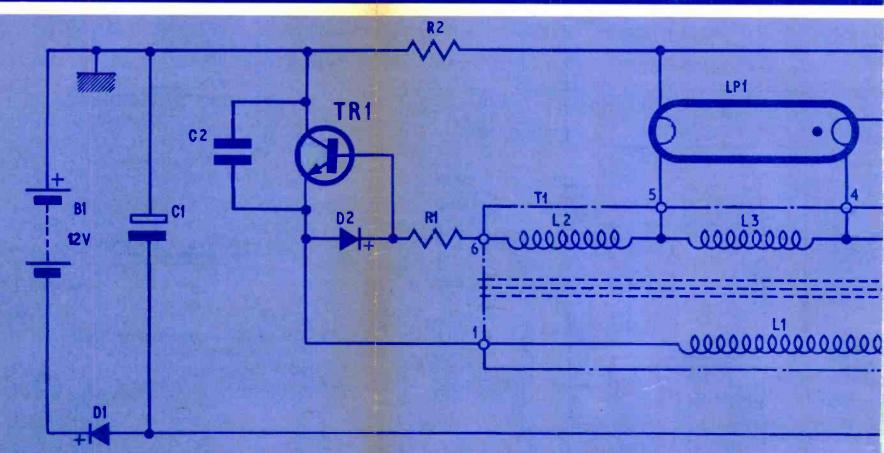
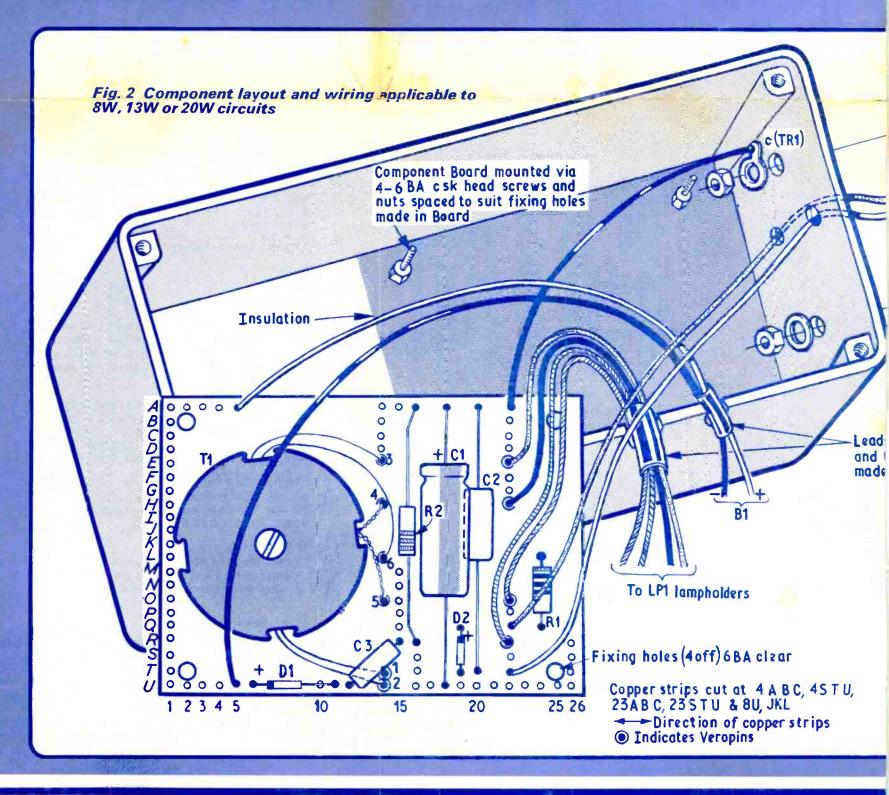


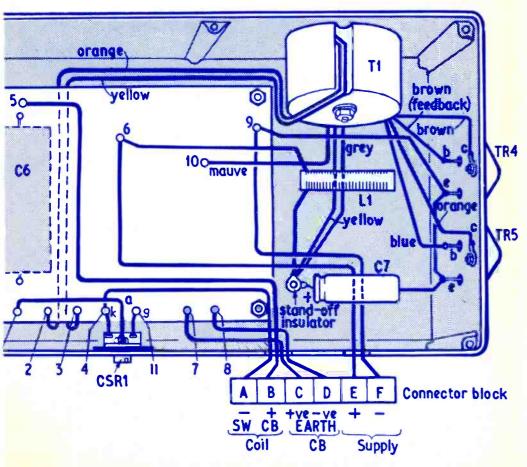
Fig. 1 Circuit diagram of lamp inverter. Component values applicable to 8W, 13W or 20W units are given in



RIGNITION SYSTEM

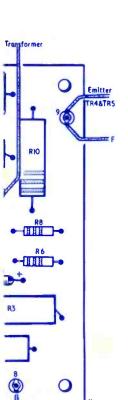
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nterwiring details of the ignition system. Also shown are are and thyristor mounting details

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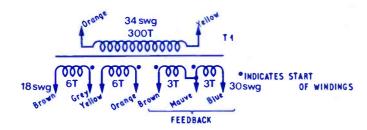


Fig. 4 Transformer winding details for the 6V version

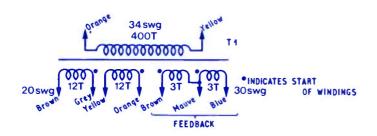
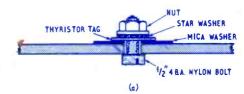
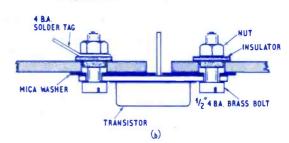


Fig. 4 Transformer winding details for the 12V version



Mounting details for thyristor



Mounting details for inverter transistors

COMPONENTS...

12V VERSION	6V VERSION

Resi	istors	
R1	22Ω	33Ω
R2	150Ω 2W	100Ω 1W
R3	150Ω 2W	100Ω 1W
R4	1kΩ	1kQ
R5	470Ω	470Ω
R6	1kΩ	1kΩ
R7	1kΩ	10kΩ
R8	1-2kΩ	1kΩ
R9	150Ω 2W	33Ω 2W
R10	15Ω 1W	5Ω 2W
R11	100Ω	100Ω
R12	330kO	330k0

All $\pm 10\% \, \frac{1}{2} W$ carbon unless otherwise specified

Capacitors

C1	0-22µF	0-33µF
C2	0-1µF	0-22µF
C3	0-47µF	0-47µF
C4	220µF 40V elect.	220µF 40V elect.
C5	0-01µF 1000V	0-01µF 1000V
C6	1µF 440V a.c. rated	
	220µF 40V elect.	

Transistors

	R2 ZTX500 anti (2 off)		R2 ZTX500 anti (2 off)
TR3	ZTX500	TR3	BFS97 or
Ferr	anti	ZTX	500
TR4, T	R5 2N3055 (2 o	ff) TR4, T	R5 2N3055 (2 off)

Diodes and Thyristor

D1, D2 ZS170 or ZS270 Ferranti (2 off)
D3 - D6 ZS178 or ZS278 Ferranti (4 off)
CSR1 BStBO246 Siemens

Transformer

T1 Two Mullard FX2243 ferrite cups with DT2206 former or two Siemens B65631 - J0000 - R026 with B65632 - A0000 - P001 former

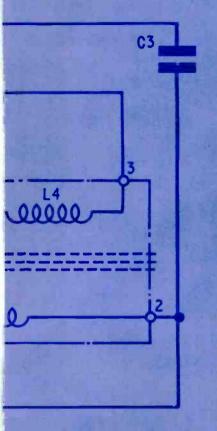
Miscellaneous

L1 Filter coil 60 turns 20 s.w.g. wound in two layers on 2in of $\frac{3}{6}$ In diameter ferrite rod Eddystone diecast box $7\frac{1}{4}$ In x $4\frac{1}{2}$ In x 2in 6-way 5 amp connector block, mica washers, screws, $\frac{3}{6}$ In spacers, turret tags, connecting wire, T03 transistor covers Printed circuit board (available from Davian Electronics, P0 Box 38, Oldham, Lancs.)

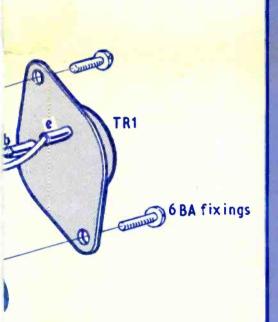
AMP INVERTER

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the Components List



s taped together taken out via notches : in lip of Box

- * Ideal Emergency Lighting
- * Up to 20watts Output
- * Automatic Circuit Protection

COMPONENTS...

8 WATT	13 WATT	20 WATT	
Resistors			
R1 33 Ω ½w	4.7Ω1w	4.7Ω2w	
R2 10kΩ½w	10kΩ ½w	10kΩ½w	
Capacitors			
C1 125µF/16v	125µF/16v	250µF/16v	
C2 —	0.02µF/30v	0.05µF/30v	
C3 0.04µF	1µF/10v	2μF/10ν	
Transistors			
TR1 MJE 520	BDY 62	BDY 62	
Diodes			
D1 IN 4001	IN 5401	REC 31	
D2 IN 4001	IN 4001	IN 4001	
Transformer (T1)			
L1 10T/26 s.w.g.	10T/22 s.w.g.	10T/22 s.w.g.	
L2 14T/30 s.w.g.	15T/26 s.w.g.		
L3 105T/30s.w.g.		. 55T/30s.w.g.	
L4 6T/30 s.w.g.	5T/30 s.w.g.	5T/30 s.w.g.	
Ferroxcubes			
FX2240	FX2241	FX2241	
(both ferroxcube pot cores and bobbins to suit			

(both ferroxcube pot cores and bobbins to suit can be obtained from Gurneys Radio, 91 The Broadway, Southall, Middlesex).

Miscellaneous

Eddystone diecast box $4\frac{1}{4}$ in $\times 2\frac{1}{4}$ in $\times 1$ in $2\frac{3}{4}$ in $\times 2$ in, 0·1 in Veroboard, insulating washer, Veropins, 2-pin lampholders (2 off).

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SCORPIO MK2 CAI

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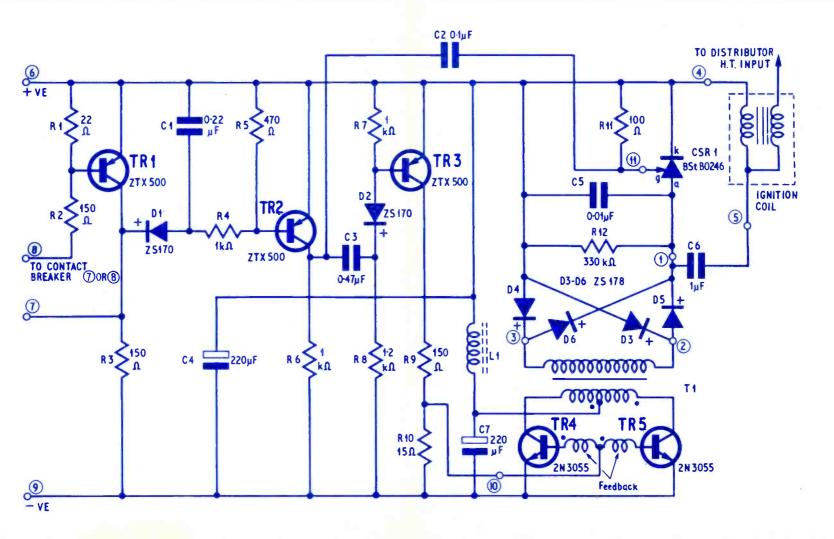
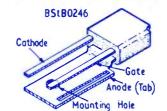


Fig. 1 Circuit diagram for the Scorpio Mark 2 ignition system. The component values shown are for the 12V version, for the 6V version see the accompanying component list



C b e ZTX 500



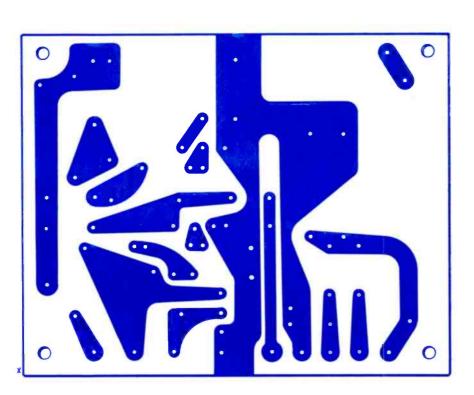


Fig. 2 Printed circuit board for the Scorpio Mark 2. The board is shown full size, the blue areas indicating copper

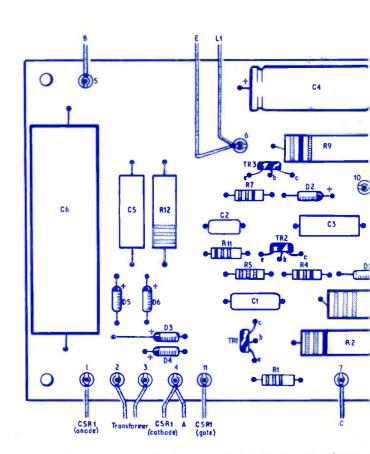


Fig. 3 Layout of the components on the pricircuit board

Fig. 5

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