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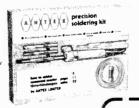


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VOLUME 9 No. 12 DECEMBER 1973

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LOGIC TUTOR EXPERIMENTS—8 by M. J. Hughes The full adder	1070
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Our January issue will be published on Friday, December 14, 1973

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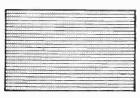






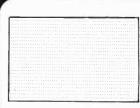
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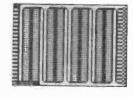
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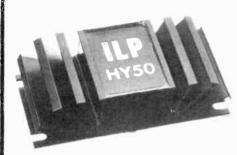
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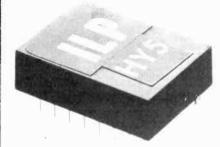
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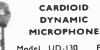
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151	200	B	0	12·1 ×	9.3	×	10.2	5-31	52
152	250	13	12	12-1 ×	11.8	×	10.2	7.01	67
153	350	15	0	14·0 ×	10.8	×	11.8	9.40	82
154	500	19	8	14·0 x	13-4	×	11.8	13.55	
155	750	29	Õ	17·2 ×	14-0	×	14.0	19-26	*
156	1000	38	Ó	17·2 ×	16.6	×	14.0	24.97	
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	0.3	0.75	,		70/		^ , ,	0-12 4 2	L O 43 ~ ^ 4	1 02	
213	1.0	0.5	- 1	4	6:1>	5-8	× 4.8	0-12V at	t 0·5A × 2	1.22	22
71	2	1	- 1	12				0-12V at		1.60	22
18	- 4	2	2	12				0-12V at		2.24	36
70	6	3	3	8	8.9>	(8-0	× 7.7	0-12V at	t 3A × 2	2.70	42
108	8	4	5	8	9.9 >	(8-9	× 8.6	0-12V at	t 4A × 2	3.00	52
72	10	5	6	4	9.9 x	9.6	× 8.6	0-12V at	t 5A × 2	3.55	52
116	12	6	6	12	9.9 >	<10∙2	× 8.6	0-12V a	t 5A x2	4.30	52
17	16	8	8	12	12:1>	9.9	× 10-2	0-12V at	t 8A × 2	5-48	52
115	20	10	11	8	14.0 >	9.6	× 11.8	0-12V a	t 10A × 2	6.98	67
187	30	15	15	8	14.0 >	CF2-1	×11.8	0-12V a	t 15A × 2	12.90	82
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51	5.0	6 12	12·1 × 8·6 × 10·2	17 17	4-42 52
117	6.0	8 0	12·1 × 9·3 × 10·2		5.28 52
88	8.0	12 0	12-1 × 11-8 × 10-2	ii ii	6.82 67
89	10.0	13 12	14-0 × 10-2 × 11-8		0.36 67
				50 VÖLT RANGI	E

Ref.	Amps.	. W	eigh/	nt .	Size cr	n.	Secor	ndary Taps	P 8	L P	
No.		16 0	z						£	Þ	
102	0.5	- 1	12	7·0 ×	6.4 ×	6·1	0-19-25-	33-40-50V	1.60	30	
103	1.0	2	12	8-3 x	7-4 x	7.0			2 34	36	
104	2.0	5	8	7-9 x	8.9 ×	8.6	- 11	11	3 - 25	42	
105	3.0	6	12	9.9 x	10-2 ×	8.6		11	4-41	52	
106	4.0	10	ō	12:1 x	10.5 ×	10.2		11	5.84	52	
107	6.0	12	Ó	14·0 ×	10.2 ×	11.8		11	8-63	67	
118	8.0	18	Ŏ	14:0 x	12.7 ×	11.8		11	11.27	97	
119	10.0	25	ň	17.2 x	12.7 x	14-0		11	14-13		

							SO VOLT	T RANG	E	
Ref.	Amps.	. W	/eig	ht	Size	m.	Secor	idary Taps	: P	& P
No.		1b c	Z						£	Þ
124	0.5	2	4	7·0 ×	6.7 ×	6.1	0-24-30-4	0-48-60V	1.62	36
126	1.0	3	4	8·9 ×	7·7 ×	7.7		13	2.26	36
127	2-0	- 6	- 4	9.9 ×	9.6 x	8.6	- 11		3.55	42
125	3.0	8	12	12·1 ×	9.9 x	10.2		11	5-41	52
123	4.0	13	12	12:1 x	11.8 ×	10.2	11	11	6.98	67
40	5.0	12	00	14·0 ×	10.2 ×	11.8		7,	8.28	67
120	6.0	15	8	14·0 ×	12:1 ×	11.8	11		10-12	82
121	8.0	25	00	14·0 ×	14.7 ×	11.8	11		11-40	
122	10.0	25	Ö	17.2 ×	12.7 ×	14.0			16.75	
189	12.0	20	00	17-2 x	14:0 ×	14:0			18.75	

183	12-0 29	00 17-	2 × 14·0 × 14·0	17 11	18-75
			RANSFORME		
Ref.	mA	Weigh	t Size cm.	Volts	P & P
No.		lb oz			£ p
238	200	2	2.8 × 2.6 × 2.0	3-0-3	1-10 10
212	IA. IA	1 4	6·1 × 5·8 × 4·8	0-6. 0-6	1.27 22
13	100	4	3.9 x 2.6 x 2.9	9-0-9	64 10
235	330, 330	4	4-8 × 2-9 × 3-5	0-9, 0-9	1-27 10
207	500, 500	1 00	6·1 × 5·4 × 4·8	0-8-9, 0-8-9	1.70 22
208	IA, IA	1 12	7.0 × 6.4 × 6.1	0-8-9, 0-8-9	2.28 30
236	200.200	4	4-8 × 2-9 × 3-5	0-15, 0-15	1-27 10
214	300, 300	1 4	6·1 × 5·8 × 4·8	0-20, 0-20	1.34 22
221	700 (d.c.)	1 8	7.0 × 6·1 × 6·1	20-12-0-12-20	1-20 30
206	IA, IA	2 12	8·3×7·7×7·0	0-15-20, 0-15-20	3.08 38
203	500.500	2 4	8·3 × 7·0 × 7·0	0-15-27. 0-15-27	2.36 38
204	IA, IA	3 4	8-9 × 7-7 × 7-7	0-15-27, 0-15-27	2-39 38
	,				

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AC132 16				BF187 30	MJE3440 55	2G308 39	2N2160 66	2N3393 16	2N4288 19
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AC155 22	AF180 55	BC171 16	BD178 72	BF257 50	OC24 62	2G373 19	2N2221 22	2N3415 17	2N5457 54
AC156 22	AF181 55	BC172 16	BD179 77	BF258 86	OC25 42	2G374 19	2N2222 22	2N3416 31	2N5458 35
AC157 27	AF186 55	BC173 16	BD180 77	BF259 94	OC26 32	2G377 38	2N2368 19	2N3417 31	2N5459 34
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AC177 27	ASY29 28	BC181 27	BD195 94	BF274 39	OC44 17	2N388 39	2N2712 28	2N3703 13	28305 86
			BD196 94	BFW10 86	OC45 14	2N388A 61	2N2714 23	2N3704 14	28306 86
AC178 81		BC182 11	BD197 99	BFX29 30	OC70 11	2N404 22	2N2904 19	2N3705 18	28307 86
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AC180 22	A8Y52 28	BC183 11			OC72 18	2N524 46		2N3707 14	
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ACY21 22	BC114 17	BC225 28	BF121 50	B8Y25 17	OC140 22	2N711 33	2N2926(O) 11	2N 3905 31	40362 50
ACY22 18	BC115 17	BC226 39	BF123 55	BSY26 17	OC169 28	2N717 39			
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7402	0.18	0.17	0.16	7454	0.18	0.17	0.16	74151	1.30	1.20	1.10
7403	0.18	0.17	0.16	7460	0.18	0-17	0.16	74153	1.98	1.90	1.75
7404	0.18	0.17	0.16	7470	0.32	0.29	0.27	74154		1.45	1.35
7405	0.18	0.17	0.16	7472	0.32	0.29	0.27	74155	1.50	1.45	1.35
7406	0.39	0.34	0.31	7473	0-41	0.39	0.85	74156	1.50	1.90	1.80
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7417	0.48	0.44	0.42	7485	3-50	3-40	3.80	74174	2.50	2.40	2-80
7420	0.18	0.17	0.16	7486	0.35	0.84	0.33	74175	1.75	1.65	1.55
7422	0.55	0.53	0.50	7489	4.00	3.75	3.50	74176	1.85	1.75	1.65
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7425	0.55	0.53	0.50	7491	1.10	1.05	1.00	74180	1.50	1.40	1.80
7426	0-50	0.46	0-44	7492	0.74	0.71	0.64	74181	5.00	4.50	4.00
7427	0.50	0.46	0.44	7493	0.74	0.71	0.64	74182	2.00	1.90	1.75
7428	0.55	0.53	0.50	7494	0.85	0.82	0.75	74184	3.20	3.10	3.00
7430	0.18	0.17	0.16	7495	0.85	0.82	0.75	74190	2.15	2.10	2.00
7432	0.50	0.46	0.44	7496	0.96	0.93	0.86	74191	2.15	2.10	2-00
7433	0.75	0.73	0.70	74100	1.50	1.45	1-40	74192	2.15	2.10	2.00
7437	0.70	0.68	0.65	74104	1.07	1-04	1.00	74193	2.15	2.10	2.00
7438	0.70	0.68	0.65	74105	1.07	1.04	1.00	74194	2.98	2.86	2.75
7440	0.18	0.17	0.16	74107	0-44	0.42	0.40	74195	2.00	1.95	1-90
7441	0.74	0.71	0.64	74110	0.60	0.55	0.50	74196	1.95	1.90	
7442	0.74	0.71	0.64	74111	1.38	1.27	1.21	74197	1.95	1.90	1.85
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UIC03 = 1		0-55		12 × 7451
UIC04 = 1		0.55	1	
UIC05 ≈ 1		0.55		12×7453
UIC06 = 5		0.55		12×7454
UIC07 = 8		0.55		12×7460
UIC10=1		0.55	UIC70 ==	
UIC20 = 1		0.55	UIC72 =	
UIC30 = 1		0.55	UIC73=	
UIC40=1	2×7440	0.55	U1C74 ==	8×7474
UIC41 = 5	× 7441	0.55	UIC76=	8×7476
UIC42 = 5	$\times 7442$	0.55	UIC80 =	5×7480
UIC43 = 5	×7443	0.55	UIC81 =	5×7481
UIC44=5	×7444	0.55	UIC82=	5×7482
UIC45 = 5	× 7445	0.55	UIC83 =	5×7483
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400 v RMS

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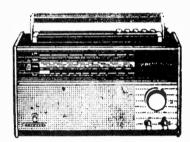
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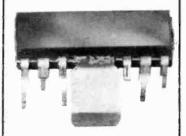
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RESISTORS - 10%, 5%, 2%

Code	Power	Tolerance	Range	Values	i to 9	10 to 99	100 up
CCCCC MO	1/20W 1/8W 1/4W 1/2W 1/2W 1/2W 1/3W	5% 5% 5% 5% 5% 5% 2% 10% ± 1/20 Ω	Range 82 Ω = 220K Ω 4-7 Ω = 470K Ω 4-7 Ω = 10M Ω 4-7 Ω = 10M Ω 10 Ω = 1M Ω 0-22 Ω = 3-90 1 Ω = 10K Ω	available E12 E24 E12 E24 E12 E24 E12		10 to 99 te note belo 8 0.9 0.9 1 2 3	
ww	700	5%	Ι Ω-ΙΟΚ Ω	E12	7 9	9	8

Codes: C = carbon film, high stability, low noise. MO = metal oxide, Electrosil TRS, ultra low noise. WW = wire wound, Plessey.

E12 denotes series: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82

E12 denotes series: 10, 12, 15, 16, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. E24 denotes series: as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51 62, 75, 91 and their decades.

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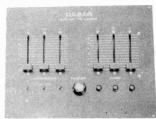
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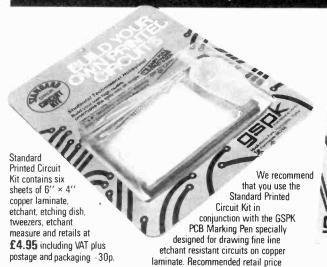


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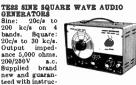
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	1 amp	£8-10
	5 amp	£3-10
	10 amp	£3-10
0	5V d.c	£8-10
0	10V d.c	£3-10
5	20V d.c	£8-10
5	50V d.c	£3-10
10	300V d.c	£3-10
5	15V a.c	£3-30
Ö	300V a.c	
^	VII Motor	49 KC

10mA \$8.10

1mA		300V a.c		
5mA	£3.10	VU Meter	£8.50	
Type SD.460	iamm >	59-5mm Fron	i e	500μA
.,,		OO-OMM I TON		1mA
$50\mu A$	£2-80	1 amp	£2-60	5m A
50-0-50μA	£2-80	5 amp	£2-60	10m A
100μA	£2.75	10 amp	£2.60	50mA
100-0-100μA .	£2.75	5V d.c	£2-60	100mA
200μΑ	£2.70	10V d.c	£2-60	
500μA	£2-55	20V d.c	£2-60	Type MR.65P. 3
1mA	£2-60	50V d.c	40.60	50μA
5mA	£2.60		40.00	50-0-50μA
10mA	\$2.60	300V d.c		
		15V a.c	£2.70	100μΑ
50mA	£2.60			100°0°100μA.
100mA	£2-60	300V a.c	£2.70	200μA
500mA	£2.60	VU Meter	£2.90	500μΑ
				EOO OEOO

Type MR.45P, 2in. square Fronts.				
50μA	£2.70	5 amp	£2-40	
50-0-50µA	22-65	10V d.c	£2-40	
100μΑ	£2-60	20V d.c	£2-40	
100-0-100μA .	£2.50	50V d.c	£2-40	
200μΑ	£2-50	300V d.c	£2-40	
500µA	£2-45	15V d.c	£2-40	
500-0-500µA .	£2-40	300 V d.c	£2-40	
1mA	£2-40	8 Meter linA.	£2-50	
5mA	£2-40	VU Meter	£2.70	
10mA	£2-40	1 amp. a.c.* .	£2-40	
50mA	£2-40	5 amp. a.c.* .	22-40	
100mA	£2-40	10 amp. a.c.*	£2.40	
500mA	£2-40	20 amp. a.c.*	£2-40	
1 amp	£2-40	30 amp. a.c.*	£2.40	

Type MR.38P, 1 21/32	in. square Fronts	
/ pages access of minute	200mA	\$2-25
2 20	300mA	£2-25
and the same of	500mA	\$2.25
A A	750mA	\$2.25
1 1	1 amp	£2.25
	2 amp	£2.25
ALC: 100 MILES	5 amp	£2-25
To the second second	10 amp	£2,25
Sett of the Steins.	3V d.c	22.25
50μA 12.55	10V d.c	£2.25
50-0-50μA £2-50	15V d.c	£2.25
100μA £2·45	20V d.c	£2-25
100-0-100µA . £2-40	50V d.c	£2.25
200μA £2.25	100V d.c	£2-25
500μA £2-25	150V d.c	£2.25
500-0-500μA . £2-25	300 V d.c	22.25
1mA £2.25	500V d.c	£2.25
1-0-1mA £2-25	750V d.c	22.25
	15V a.c	£2.35
2mA £2-25	10 Y a.c	80.00

30	500mA	£2-25
-0-	750mA	\$2-25
3	1 amp	£2-25
4	2 amp	£2.25
1	5 amp	£2-25
10	10 amp	£2.25
	3V d.c	£2-25
£2.55	10V d.c	£2-25
£2.50	15V d.c	£2.25
£2-45	20V d.c	£2-25
£2-40	50V d.c	£2-25
£2-25	100V d.c	£2-25
£2-25	150V d.c	£2.25
£2-25	300 V d.c	22-25
£2.25	500V d.c	£2.25
£2-25	750V d.c	22-25
£2-25	15V a.c	£2-35
£2-25	50V d.c	£2-80
£2.25	150V a.c	£2-80
£2-25	300V a.c	£2-30
£2.25	500V a.c	£2.80
£2-25	S Meter 1mA.	£2.30
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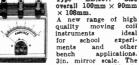
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-			
Туре	PE.70.	3 17 2†in. (7/32in. × 1 15/32in. × deep.
50μΑ 50-0-5 100μΑ 100-0- 200μΑ	0μA 100μA .	£3.75 £3.60 £3.60 £3.50 £3.40	500μA

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3in. mirror scale. The meter movement is easily accessible to demonstrate internal working. Available in the following species.

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£2.90				
\$2.90	Type MR.52P.	24in. 1	quare Fronts.	
£2-90	50μA	£8-50	10V d.c	£2.50
£2-90	50·0-50μA	48-05	20V d.c	£2.50
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\$2.90	100.0-100μA .	£2-95	300V d.c	£2.50
£2-90	500μA	22-65	15V a.c	£2-60
£8-00	1mA	42-50	300V a.c	£2.60
£8-00	5mA	£2-50	8 Meter 1mA.	£2.60
£3·15		£2.50	VU Meter	£8-60
	50mA	£2.50	1 amp. a.c.* .	22.50
	100mA	£2.50	5 amp, a.c	42-50
£2-60	500mA	£2.50	10 amp. a.c.*	£2.50
£2.60	1 amp	£2.50	20 amp. a.c.*	£2-50
£2.60	5 amp	£2-50	30 amp. a.c.*	£2-50
£2.60				

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5 amp. 15 amp

2 amp.

£2.60 £2.60 £2.60 £2.60

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	\$2.60
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	24.60
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50mV d.c	\$2.90
100mV d.c	\$2-90
30V a.c.*	\$2-65
50V s.c.*	49.65
	£2-65
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	50mV d.e. 100mV d.c. 30V a.c.* 50V a.c.* 150V a.c.* 300V a.c.* 500W a.c. 500mA a.c.* 1 amp. a.c.* 5 amp. a.c.*

Type 8-80 80mm squ	are Fronts
50μA	nA.
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Self contained, transistorised, battery operated. Simply plug in microphone, guitar, etc., and out-Õ O I guisar, etc., and out-put into your amplifier. Volume control, depth of reverberation control. Beautiful walnut cabinet. 7¼in × 3in × 4¾in.

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For balancing and gain selection of outspks, with additional facility for trols, speaker on-off slide switch, stereo headphone sockete 6in × 4in × 24in.

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MP7 MIXER PREAMPLIFIER



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wperated.
9lin × 5in × 3in.
Inpute Mice: 3 ×
3mV 50K: 2 × 3mV
4mV 50K. Phono ceramic 100mV 1
Output 250mV 100K. Battery operated. 91in × 5in × 3in.

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All silicon transistor amplifier operates from magnetic ceramic or tuner inputs with twin stereo headphone outvolume controls for each channel. Operates from 9V battery. Inputs 5mV/100mV. Output 50mW per channel.

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Features 24 hour alarm setting with built in buzzer. On/off and auto-darm 'sleep' awitch. Automatically turns off TV, radio, light, etc. and with autosetting will switch on again when required. A.c. 240V operation. Switch rating 250V. OUR E5-95 930P.

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TRIO TR2000 TRANSCEIVER

Fully tran-sistorised portable VHF Trans-ceiver. Will transmit and receive on



144-146MHz. 1W transmitter. 12V d.c. internal or external supply. Built in charger for ni-cad Power/volume ewitch cells. Power/volume switch, squelch control, channel selector, mike socket earphone/external speaker socket. Complete with microphone, 144-48, 144-72 and 145-32 crystals.

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4 bands covering 550kHz-30MHz continuous and electrical bandspread on 10, 15, 20, 40 and 80 metres. 8 valve plus 7 diode circuit. 4/8 ohm output and phone jack. 88B-CW. ANL. Variable BFO. 8 meter. 8ep. bandspread dial. 1F frequency 445kHz audio output 1-5W. Variable RF and AF gain controls 115/250V a.c. 8lize: 7in 13in x 10in with instruction manual.

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4 Bands covering 550kHz-30MHz, FET, 8 Meter. Variable BFQ for SBB. Bull: In Speaker. Band-spread. Sensitivity Control. 220/ 240V a.c. or 12V de. 121 x 41m x 7in.Brand new with instructions. SSR spread. Sensitivity 240V a.c. or 12V d. OUR **£25.00** Carr. 370

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4 Bands covering 550kHz-30MHz. BFO Bullt-in Speaker 220/240V a.c. Brand new with Instructions.

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TRIO JR310 SSB RECEIVER



Covers 3.5, 7, 14, 21, 28, 28.5 and Covers 3:5, 7, 14, 21, 28, 28-5 and 29-1MHz bands, and WW 15MHz. 88B, AM and CW. AF output more than IW. Crystal controlled BFO for 88B. 8 meter, ANI., etc. Ac. 110/120-220/240V. 8ize 330 × 179 × 310mm.

OUR £75.00 Carr.



1 TRIO JR599 RECEIVER



9 wavebands covering 1.8-29-7MHz, 144-146MHz and 10-00 MHz WWV. 88B, CW, AM and FM. AF output more than 1W. S. Meter. Squelch control. BFO. Variable RF and AF controls. 4-16 ohm output and phone jack. Power requirements 100/240V a.c., 12-14V d.c.

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TRIO TS515/PS515 TRANSCEIVER



High quality T8515 88B/CW amateur band receiver dovering 80, 40, 20, 15 and 10 netre bands with P8515 power supply and speaker unit. Transmit/receive frequency 3-5-29-7MHz. Output 1-5W. Power requirements 110-120/220-240V a.c.

OUR £210.00 Carr.

BELTEK W5400 CAR TRANSCEIVER



Solid state mobile transceiver for 12V d.c. neg. use. Transmits and Receives on any 12 of 28 channels hetween 144 and 146MHz. Power output 10W and 1W switchable. Controls: Volume/on/off, squelch, channel selector. Internal 3in speaker. Complete with dynamic nike, PTT switch, there sets of crystals for 144-48MHz, 145-00MHz, 145-00MHz, mounting bracket and instructions. ing bracket and instructions

£75.00

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General coverage 150-400kHz, 550kHz-30MHz. FET front end, 2 mech. filters, product detector, variable BFO, noise limiter, 8 Meter. Bandanced, PE. Coli. Meter Bandspread. RF Gain. 15in × 9\frac{1}{2}in × 8\frac{1}{2}in, 18 ib. 220/240V a.c. or 12V d.c. Brand new with instructions.

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Battery operation. Volume and squelch controls, Call button and press to talk button. Telescopic Aerial, Complete with carrying

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Casees. 8K YFON
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Incorporates built in ampliflers giving 2½ + 2½W r.m.s. output. Push-button track selector, illu-



controls for volume, balance and tone. Attractive cabinet with black and silver trim. Output impedance 8 ohns. 220/240V a.c.

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AUDIOTRONIC AHP8D 8 TRACK STEREO TAPE DECK

Can be used with most hi-fi amplifiers. Push buttor button



Push button track selector andilluminated track indicators. Attractive cabinet with black and silver trim. Outputlevel 750mV. 220/240Va.c. OUR £11-95 P. & P. PRICE £11-95 OP. PILO

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A beauti-fully styled 4 track stereo deck

stereo deck
with a n
outstanding specific a tion
offered at a
remarkably low price. Incorporates
a host of features including switchable noise filter, normal/chrome
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socket, recording indicator lamp,
phono/Din line input sockets,
scocket, etc.,
etc. Frequency response 1008kHz (100-12kHz C70-2). 8/N
-45dB, Crosstalk -45dB.
Separation -35dB. Noise limiter
-6dB at 10kHz. Complete with
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LSH20. Individual volume controls. Stereo mono switch. 8 ohms. 19,000Hz. 40-

£3.50 P. & P. 30p L8H30. Open back type. Individual type. Individua-tone and volume controls. 8 ohms. 30-20,000 Hz.

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Matched pair of compact bookshelf spea-kers of unique design incorporating

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4 track, 7½, 3½, 1½ i.p.s. Stereo mono record/play. 7 in reels

7in reels. Inputs for dynamic mikes,
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Manual tuning of Medium and Long waves. 12V pos. or neg-earth. Complete with speaker, mounting brackets and instructions OUR. £6.50 P. & P. 500

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12V neg. earth. Slider controls for Volume, Tone and Balance. Channel selector button with pilot lamp. With speakers, mounting brackets and instructions.

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CHASSIS Famous BSR 8 track chassis as

used in M o d e l
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complete with silver
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ready to fit into cabinet. Output
125mV A.C. 240V. Overall sire 125mV A.C. 240V. Overall size approx. 185 × 215 × 80mm.

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Model 350. 13in × 8in with single tweeter /crossover. 20-20,000 Hz. 15W RMS. Avail-Hz. 15W RMS. Available 8 or 15 ohms.

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wavebands

10 wavebands c o v e r i n g A.M.:535-1605kHz; L.W.: 150-380kHz; M.B. 1-6-4-0MHz; S.W.1:4-0-8-0MHz; S.W.2: 8-0-1-6MHz; S.W.3: 16-24MHz;



S.W.2: 8-0-1-6MHz:
S.W.3: 16-24MHz:
P.S.B.1: 30-50MHz;
P.S.B.1: 30-50MHz;
174MHz: F.M. 88-108MHz; A.I.R.:
108-136MHz: Features time zone
map and tinning dial. Large clear
scale. Telescopic aerial and builtin aerial. A F.C. on F.M. 6in x
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Battery/mains operation. Size
345 x 133 x 305mm.

OUR \$2.36-00 P.&P.
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5 wavebands covering MW 535 -1605KHz and F.M. 88-175MHz. All transistor.
Battery or mains operation. Builtin aerial and 8 section telescopic aerial. Complete with batteries, shoulder strap and earpiece. transistor.



OUR PRICE £6.95

AUDIOTRONIC AR1000 Sportsman AM/FM Portable

AM/FM F
5 wavebands
covering A.M.:
535 - 1065kHz:
F.M. 88108MHz; A.I.R:
108 - 135MHz;
P.B. 147174MHz; W.B.:
162-5MHz Large
horizontal slide
dial with logging
scale. Slider volume

volume and squeich controls. 7 section telescopic aerial for F.M. and built in ferrite bar for A.M. A.F.C. 3in speaker. Earpiece socket. Green leatherette covered cabinet with metal side panels. 81ze 152 x 79 x 219mm. Battery/mains operation.

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RADIO AR3000

4 wavebands covering FM 87-108MHz,
MW 510-1605KHz,
BW 5-8-12-5MHz.
Push button wave
change plus AFC
and on/off. Thumbwheel tuning.
Slider volume and tone controls.
Earphone socket. Built in and
telescopic aerials. Car serial
socket. Battery/Mains operation,
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AM-FM RADIO ADC. I



Covers AM 540—1600kHz. FM 88—108MHz with AFC. 24 hour leaf type digital clock with one minute division time change. Illuminated dial. 24 hour alarm setting. Wake up to the sound of music or loud buzzer. Unique sleep switch will automatically turn off radio when you have gone to sleep. Blider volume control. Internal speaker plus socket for earpiece or pillow speaker. Ac. 240V. Size 264 x 92 x 178mm. Complete with earpiece, and operating instructions.

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Outstanding value. Soft ear pade, adjust-able headband. 8-16 ohms. 20-20,000 Hz. 20,000 Complete with lead and stereo plug.

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Lightweight headphones with padded earpieces. 4-16 ohms. 20-20,000 Hz. Complete with 6 ft cord and plug. cord plug.

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Sensitive magnetic headset with soft carpads. Imped-ance 2,600 ohms, (d.c. 600 ohms). Frequency response 200-4,000 Hz.

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Complete with and plug.

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Moving coil.
Headphone
imp. 16 ohns.
Mike imp. 200
ohms. Ideal
for language for language teaching, com-munications Complete with leads

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Matched pair
of bookshelf
speakers. De
luxe teak
veneered finish. Size 144
in × 9in × 74
in 8 ohms. 8W
RMS. 16W
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STEREO CASSETTE

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For conventional or Chromium Dioxide tape. 4 track record/playback. Volume and tone controls. Frequency response (using CrO2 tape), controls. Frequency response 40-16kHz (using CrO2 tape), distortion better than 2%, wow and flutter better than 0.2%, RMS. Complete with pair of matching Akai CSS8 speakers. Rec. Price 202.10 £96·10.

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rast forward and rewind. Output 500mW; 220/240V a.c. or 6V d.c. operation. Complete with remote control microphone, mains lead, earpiece and batteries.

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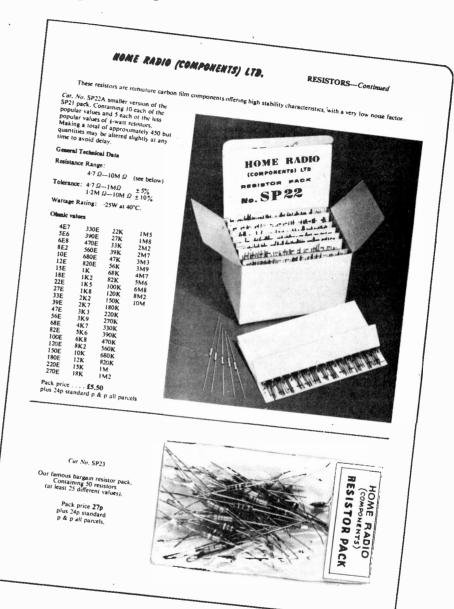


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TWENTY-FIVE YEARS ON

THE 25th year of the transistor draws to its close. A quarter century of exciting and rapid technological growth justifiably referred to as a revolution, and unlikely to be paralleled within the seeable future.

In this issue appears a final article in our special series marking this anniversary of the dawn of the new solid state era. It is written, most fittingly, by a well known contributor and dwells on those now far off days when the transistor was still much of a curiosity and just beginning to cause an upheaval in constructor circles. Established methods of building clearly had to change, but it was far from clear just how.

Much water has flowed under the bridge since then . . . but those early experiments with transistors are worth recalling, though it will all sound very strange to a fair proportion of our readers since there is now a whole generation of constructors brought up entirely on semiconductors.

Yet even our younger post-valve-era readers are not denied the excitement of being involved in great changes in technology. Right at this present moment we are witnessing a "quiet revolution." With hindsight, we know that the discrete semiconductor device represented but the opening phase of this solid state revolution; the culminating achievement has been the creation of the integrated circuit.

So let us turn now from the past and consider what the future holds for the constructor. It will be a future dominated by the i.c., that is obvious. Until, of course, another spectacular discovery leads to the obsolescence of semiconductors—a development not entirely improbable but sufficiently remote in time to be left out of any sensible prognostications at this particular moment.

The i.c. is, in circuit terms, a very large building block and is tending to become even bigger, thanks to l.s.i. This type of device influences very considerably, if it does not dominate entirely, the general pattern of any design in which it is called upon to play a part.

In the future, the drift towards more custom designed i.c.'s may well limit the total number of new devices suitable for constructor applications. Yet amongst the balance there are bound to be an abundance of types than can be usefully employed by the amateur. In this respect, particularly noteworthy at the present time are phase-locked loops. These i.c.'s are beginning to mould the pattern of many equipment designs. They are opening up new fields and revolutionising some traditional designs, especially in the radio receiver area.

Immediately following its introduction, the i.c. was thought by some to represent a threat to home construction activities. Such a pessimistic view has already been proved ill-founded. Looking ahead, there is no reason to suppose any drying up of individual enterprise and ability to extract the maximum advantage from monolithic devices yet to emerge from the microelectronics plants.

F.E.B.

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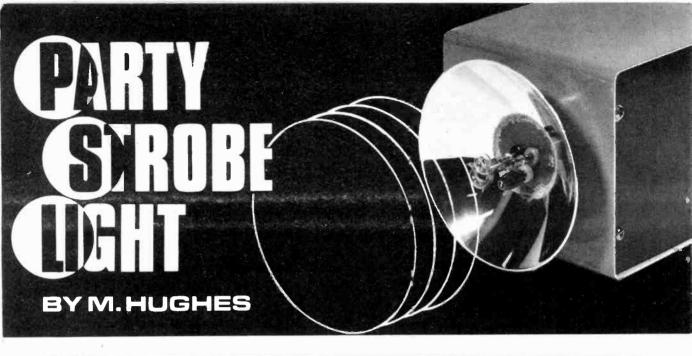
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This stroboscope is designed primarily for use as a lighting effect for parties and discotheques. Its flashing rate is continuously variable from about 2Hz to 20Hz. It can be used—with limitations—for specialised photography but the output power (about half a joule) limits it to use with only medium to high speed black and white films at distances of a few feet. For discotheque work, however, it can be classified as of medium power.

SOME WARNINGS

Those who intend building the equipment should be fully aware at the outset of their social responsibilities in the operation of such equipment; strobing in the frequency range of 10 to 20Hz can, in some instances, produce hypnotic effects. Excessive use of the strobe should thus be avoided; however, if handled carefully and used in moderation some particularly pleasing lighting effects can be produced.

A further word of warning regarding the construction. Very high voltages are used to charge up high value capacitors—these can be lethal if mishandled. When testing it is not sufficient simply to switch off the power; the plug should be completely removed from the socket and all capacitors shorted out with an insulated handled screwdriver before any attempt is made to handle the circuitry.

OPERATION

The principle of operation is quite simple. All we have to do is apply a high voltage across a Xenon gas filled tube from a reasonably high value capacitor. This voltage is arranged to be below the breakdown voltage of the tube so initially no electrical discharge takes place. At some pre-determined time a very high voltage pulse (at low current) is applied to a third electrode fixed to the outside

of the tube—this is called the trigger electrode—and we cause a localised electrical breakdown of the gas between the trigger and one of the primary electrodes. The gas in that locality becomes electrically conducting (or ionised), and the ions produced move rapidly throughout the length of the tube and cause main conduction between the primary electrodes.

For a fraction of a second the tube becomes a short circuit across the capacitor and the full charge held on the latter flows through the tube giving rise to the very bright short duration flash. As soon as the capacitor has fully discharged the tube is extinguished and a fraction of a second later the residual ions of gas revert to their non-conducting state and the tube once more becomes inert. The capacitor can now be recharged and a second trigger pulse applied for the next flash.

FLASH ENERGY

The energy of the flash is measured in joules and is equivalent to the amount of electrical energy stored in the main capacitor (C4 in Fig. 1). This energy is calculated by using the formula:

Energy =
$$\frac{1}{2}CV^2$$
 joules

where C is the value of the capacitor in farads and V is the voltage to which it is charged. In Fig. 1 C4 charges up through a half wave rectifier (D2) and limiting resistor, R3, direct from 250V r.m.s. mains; this means the peak voltage on the capacitor when it is fully charged is about 350V. The energy produced in each flash for the capacity used will be about 0.48 joules.

LIMITED OUTPUT

Because of the tube rating, if it is flashed too often at too high an energy it will get extremely hot. The tube specified is made of hard glass that has a

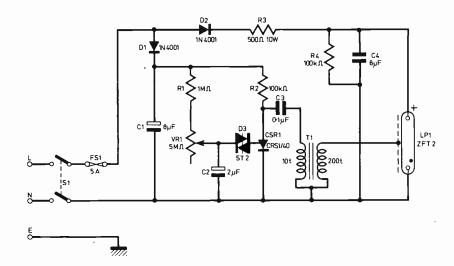


Fig. 1. Circuit diagram of the Party Stroboscope. Note that the case is connected to mains earth

maximum dissipation of 10 watts. It is possible to obtain tubes having a high permitted dissipation but these are quite expensive, particularly those made from quartz.

We can calculate dissipation by multiplying flash energy by the maximum frequency of flashing, with the stroboscope this is $0.48 \times 20 = 9.6$ watts.

Since this represents nearly the limit of the tube, experimenters should not try to get more light output by increasing the value of C4 without limiting the maximum flash rate proportionally.

Before describing the trigger system, which forms most of the circuitry, a word about R3. The value is reasonably important because it prevents the main capacitor charging before the discharge tube is completely de-ionised; at the same time it must be of low enough a value to ensure that C4 is fully charged before the next trigger pulse. Quite high peak currents flow through this resistor so it should be of at least 10 watts rating and even so will get quite warm in use.

TRIGGER SYSTEM

To produce the trigger pulses there must be a timing circuit that is adjustable in the range from ½ second to ½ second. D1 and C1 form a simple auxiliary d.c. supply of about 350V. C2 will charge up towards 350V and the rate of charge is controlled by the value of R1 and VR1—as the latter is adjustable we can vary the charging rate. In actual fact the potential across C2 will never reach 350V because as soon as it reaches about 25V the diac D3 will start to conduct and any charge held on C2 is applied to the gate electrode of the thyristor.

As soon as C2 is completely discharged the diac becomes non conducting and C2 is able to charge back up towards the 350V. This is a repetitive cycle and the timing is controlled, as we have already said, by the time constant of C2 with the charging resistors but also by the differential between the breakdown voltage of the diac and the potential towards which C2 is charging. Different diacs—particularly the cheaper ones—may have slightly different breakdown voltages so there may be some

variance in timing between different assemblies. This can be compensated for in practice by increasing or decreasing the value of C2. Increase its value if you require a slower repetitive cycle and vice versa.

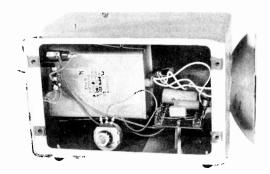
It is most important that you do not exceed a flash rate of 20Hz because you might exceed the power rating of the tube.

TURN ON

The discharge current from C2 through D3 into the gate of the thyristor causes the thyristor to turn on. C3 has been charged to 350V through R2 and when the thyristor turns on this is discharged through the circuit C3, CSR1, and the primary of T1. The instantaneous current is quite high and the rate of change of flux in the primary of T1 causes a very high voltage pulse across the secondary windings (approximately 7,000V). This pulse is fed to the trigger electrode of the discharge tube.

Component values have all been carefully chosen so that everything happens in the correct time sequence, e.g. C4 and C3 must be fully charged before the highest rate of trigger pulse is generated by C2 and the diac circuitry so do not use values other than those specified.

R4 is a bleed resistor across the main capacitor to ensure that when the unit is switched off any



The strobe unit with a panel removed showing the large paper capacitor (C4)

COMPONENTS . . .

Resistors

R1 1MO

R2 $100k\Omega$

R3 500Ω 10W wirewound

R4 100kΩ 1W

All 10% 4W except where otherwise stated

Capacitors

C1 $8\mu F$ elect. 500V C2 $2\mu F$ elect. 200V

C3 0.1µF 400V polyester C4 8µF 500V paper

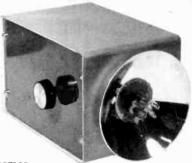
Diodes

D1-D2 IN4001 (2 off)

D3 ST2 Diac (G. W. Smith)

Xenon Tube

LP1 Hivac ZFT2 (Townsend and Coates Ltd., Coleman Rd., Leicester)



Transformer

T1 Primary, 10 turns 18 s.w.g. enamelled wire: secondary, 200 turns 36 s.w.g. enamelled wire both layer wound on 2in length, in dia, ferrite rod

Miscellaneous

S1 Double pole mains switch; FS1-5A fuse with panel mounted holder; group board; stand off spacers; 3 wander plug sockets; 1 wander plug

high charge stored on C4 is reduced over a short period of time. Do not, however, rely on this-it is always safer to discharge high value capacitors with a screwdriver before touching them.

C4 must be a paper dielectric capacitor rated in excess of 500V. An electrolytic must not be used in any circumstance

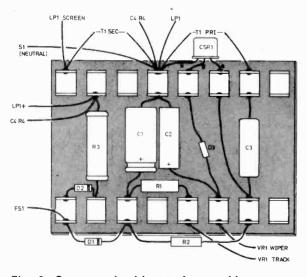


Fig. 2. Component wiring and assembly on group board. Stand-off spacers should be used when connecting to case

CONSTRUCTION

Nearly all the circuitry is mounted on a length of group board (Fig. 2) and the only precautions necessary in the layout are that the secondary of T1 (winding details given in Fig. 3) should not be routed too close to any other wiring and R3 should not touch any other components as it gets quite warm. As the discharge current from C4 is very high, fairly heavy gauge wire should be used to connect its terminals to the discharge tube to prevent excessive line drop.

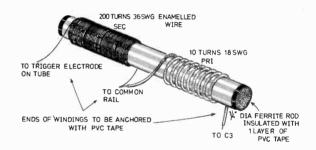


Fig. 3. Winding details of trigger transformer. Both windings are wound in the same sense

All the components should be mounted in a metal case that can be properly earthed; this is essential as all the wiring is live to mains. Wander plug sockets form a convenient way of mounting the tube within the reflector and enable easy change of tubes which have a life expectancy of about a million flashes (this is equivalent to about 25-30 hours of operation at 10 flashes per second).

REFLECTOR

The reflector was the hardest single item to find. In the end a tour round surplus shops solved the problem where a reflector from on old projector system was found for a few pence. An old car headlight reflector (pre sealed-beam era) would be ideal.

The reflector should be bolted or stuck on the main box and the tube sockets fixed through the rear of the reflector and the case—these add extra mechanical support to the reflector. To make the unit tamper proof it would be advisable to place a clear Perspex guard in front of the tube—if different coloured lighting was required tinted Perspex could be used for this purpose.



This fader unit was developed for use in a Discotheque console where it will automatically fade out the music being played when the D.J. makes an announcement via the microphone. When the announcement is finished the music is then restored to its original volume.

As the finished unit in its original form measures only $3.75 \times 2.5 \times 0.5$ in, it should fit easily into

the corner of a Discotheque console.

Whilst no complicated adjustments of the console wiring are required the unit will require some form of power supply as it consumes some 7mA at 9V. This could be taken from the Discotheque supply or be provided by a battery if required.

CIRCUIT

The circuit is shown in Fig. 1 and, as can be seen, is constructed around the Motorola integrated circuit MFC 6040 which is used as an electronic attenuator. It provides zero attenuation for control voltages below 3.5V and about 90dB attenuation for a 6V control voltage. Thus to give the required control effect we have to derive a rising and falling d.c. level from the microphone signal to fade the deck signal in and out.

TR1 and its associated resistors form an emitter follower which gives the input a high impedance and thus prevents undue loading of the console preamplifier. TR2 forms a simple amplifier the output of which goes to the base of TR3 via diodes D1 and D2 and VR1. The diodes clamp and rectify the amplified microphone signal and VR1 controls the amount of signal applied to the base of TR3. Thus it controls the sensitivity of the unit.

When there is an input signal at the microphone of sufficient amplitude TR3 is turned hard on and the collector is thus at 0V. C4 prevents this voltage rising appreciably during any short breaks in speech which might occur such as between words or sentences.

Without an input signal TR4 conducts and the collector lies about 2V above earth potential. When TR3 turns on TR4 turns off and C5 charges up via R7, providing a rising potential at the control input of IC1.

This in turn attenuates, at a rising rate, the signal from the deck. The initial attenuation must be fairly rapid if the initial part of the announcement is not to be drowned in music.

When TR3 turns off again TR4 turns on and C5 discharges to earth through TR4 and R8 until it reaches a steady level. This gives a falling voltage level to decrease the attenuation provided by IC1.

POWER SUPPLY

As mentioned, a 9V supply giving about 7mA is needed. If such is already available within the console, all well and good. If not then it is simply a matter of dropping and stabilising the console preamplifier supply and this may be done simply by using the circuit of Fig. 2.

In Fig. 2, the resistor R9 drops the supply voltage from the console rail value to 9 volts at which it is clamped by the Zener D3. Capacitor C9 gives smoothing of the output. Using Ohms Law, and given a pre-amplifier voltage of V volts then:—

 $R9 = \frac{(V-9)}{11} k\Omega$, where R9 is $\frac{1}{4}$ watt if V is less than 30V or otherwise $\frac{1}{2}$ watt.

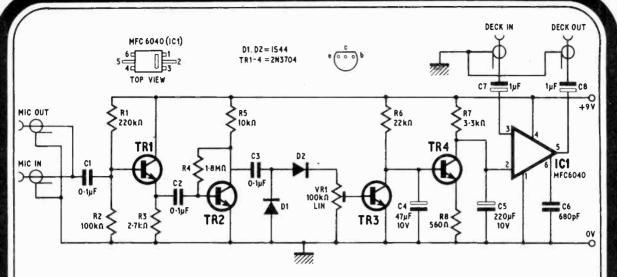


Fig. 1. Circuit diagram of the complete fader which is based on the Motorola MFC 6040 attenuator integrated circuit

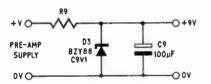


Fig. 2. Circuit of a simple power supply for use with the fader

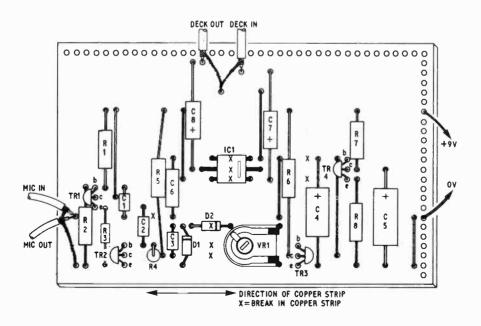


Fig. 3. Component layout and 0.1 in track Veroboard cutting details

COMPONENTS . . .

VOICE OPERATED FADER

Resistors R1 220kΩ

R2 100k Ω R3 2·7k Ω R4 1·8M Ω

R5 10kΩ R6 22kΩ R7 3.3kΩ

R8 560Ω R9 See text

Capacitors

C1-C3 $0.1 \mu F$ Mylar film C4 $47 \mu F$, 10V elect. C5 $220 \mu F$ 10V elect. C6 680 F polystyrene C7, C8 $1 \mu F$ 16V elect. C9 $100 \mu F$ 10V elect.

Semiconductors

TR1-TR4 2N3704 D1, D2 1S44

D3 BZY88 C9V1, 9·1V Zener

IC1 MFC 6040 (Motorola). Available from Jermyn or Arrow Electronics

Potentiometers

VR1 100k Ω linear horizontal mounting pre-set

Miscellaneous

0-1in Matrix Veroboard measuring 3-75in \times 2-75in Wire and coaxial cable as needed



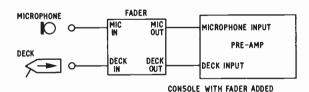


Fig. 4. Discotheque console circuit with and without voice operated fader

CONSTRUCTION

The unit is quite simple to construct as can be seen from Fig. 3. Using standard 0·1in matrix Veroboard 3·75 × 2·5in the layout of Fig. 3 may be followed. Coaxial cable should be used for the microphone leads to avoid hum pick-up.

Equally, circuit installation is simple as is shown in Fig. 4.

If the circuit of Fig. 2 is to be used this may be added to the board carrying the main components or simply suspended in the wiring since it consists of so few components.

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ELECTRONICS

JANUARY ISSUE ON SALE DECEMBER 14, 1973

ASE LOCKED LOOP

KED (W)

BY J.B. DANCE

THE BASIC theory of phase locked loops has been reviewed in a non-mathematical way in the previous articles in this series. We will now consider in detail the types of phase locked loops which are currently available together with examples of the types of circuit in which they can be used.

Monolithic phase locked loops are necessarily fairly complex devices. In general the various manufacturers have evolved devices which are quite different from one another and they must therefore

be considered separately.

SIGNETICS H.F. LOOPS

The Signetics International Corporation manufacture three rather similar monolithic phase locked loops which can operate at high frequencies. They are the NE560B, the NE561B and the NE562B devices.

These three phase locked loops all employ the same phase detector, the same voltage controlled oscillator and the same voltage regulator stages. The basic parameters are therefore very similar for all the three devices, but there are differences in the metallic interconnections which make some types especially suitable for certain applications.

NE560B

The NE560B can be regarded as the most fundamental of the three devices. It has the basic phase locked loop structure shown in the block diagram of Fig. 3.1. This device is suitable for high linearity f.m. demodulation, for telemetry decoding, for use in signal generators, in frequency shift keying receivers, in tracking filters, in circuits for exact frequency duplication in a high noise environment,

The voltage controlled oscillator in this device provides two outputs of opposite polarity to each other.

NE561B

The NE561B contains all the circuitry of the NE560B, but also has an analogue multiplier which can be used as a quadrature detector. This allows the device to be employed for the synchronous detection of amplitude modulated signals if an external 90 degree phase shift network is added.

The NE561B can also be employed in a.m./f.m. i.f. strips, in signal generators, in telemetry decoders, in tracking filters, etc.

NE562B

The NE562B is similar to the NE560B, but the loop is broken between the voltage controlled oscillator and the phase comparator. A frequency dividing circuit can therefore be inserted in the loop at this point if it is desired that the voltage controlled oscillator shall operate at a harmonic of the input frequency.

The NE562B is therefore especially useful in frequency synthesisers and for frequency multiplication and division. In addition, it can also be used in f.m. i.f. strips and for most of the other applica-

tions for which the NE560B is suitable.

SUMMARY OF DATA

Each of these three phase locked loops can be operated over a frequency range from less than 1Hz to over 15MHz, the centre or free-running frequency being set by the value of a capacitor connected between two pins of the voltage con-

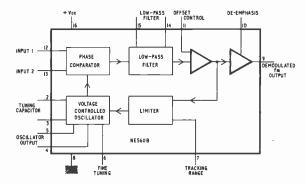
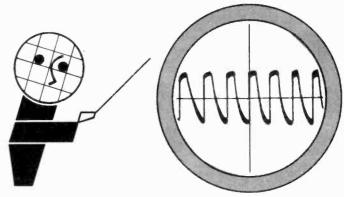


Fig. 3.1. Block diagram of the NE560B phase locked loop. The numbers refer to pins on the dual-in-line versions

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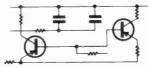
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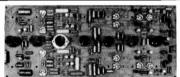
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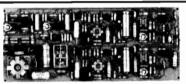
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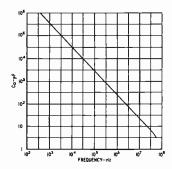


Fig. 3.2. Graph showing the relationship between the centre frequency and the value of the timing capacitor

trolled oscillator. The variation of this frequency with the value of the capacitor is shown in Fig. 3.2.

The control voltage is prevented from exceeding a preset level by a limiter between the control voltage amplifier and the voltage controlled oscillator. This range is known as the tracking range and is set by a control current into pin 7 of the i.c.

The typical operating voltage of these devices is 18V. The NE560B consumes less than 11mA, the NE561B less than 12mA and the NE562B less than

14mA.

The NE560B and the NE561B require a minimum of $100\mu V$ for locking, and can take 1V r.m.s. maximum. The corresponding figures for the NE562B are $200\mu V$ minimum and 3V r.m.s. maximum.

The maximum output voltage swing is 4V peak-

to-peak.

If one applies a 1mV, 10.7MHz f.m. input signal which has a ± 75 kHz deviation and a 50 ohm source impedance, the demodulated output is typically 60mV in amplitude with a total harmonic distortion of 0.3% (typical).

When one of these loops is used for demodulating f.m. signals a capacitor may be connected from pin 10 to ground to provide de-emphasis.

At operating frequencies below 5MHz the low pass filter may be formed by connecting a capacitor (or capacitor and resistor in series) across the low pass filter terminals. At higher frequencies a capacitor from each terminal to ground should be used to ensure loop stability.

APPLICATIONS

In order to illustrate the usefulness of phase locked loops some circuit diagrams will be given. Whilst it is not possible to give sufficient detail for the systems to be built it is hoped that the information given will give the reader an appreciation of the practical aspects of phase locked loop i.c.s.

F.M. DEMODULATION

A phase locked loop can replace almost the whole i.f. strip, limiter and f.m. detector of a conventional receiver. A typical circuit using the NE560B as f.m. demodulator with an i.f. amplifier and limiter is shown in Fig. 3.3.

The input from the f.m. tuner unit is first amplified by the two sections of a Signetics NE510A dual high frequency differential amplifier. The low output impedance signal from the NE510A is coupled by C4 to pin 12 of the NE560B. The other input (pin 13) of the phase comparator is grounded with respect to radio frequencies by C5. The capacitors C4 and C5 may each have a value of 20pF when the signal frequency is 10.7MHz.

The frequency of the loop is set by the variable capacitor C9 which is connected between pins 2 and 3 so that the centre frequency becomes approximately equal to the signal frequency. The value of C9 may be estimated from Fig. 3.2.

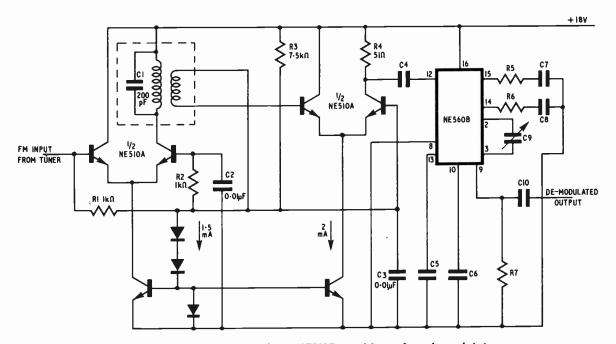


Fig. 3.3. Circuit diagram of the NE560B used in an f.m. demodulator

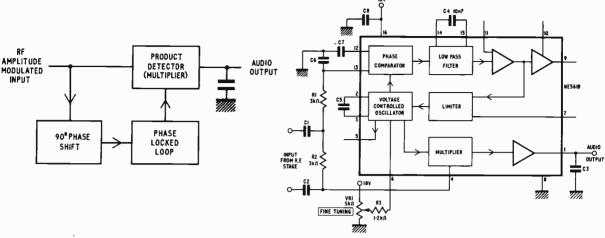


Fig. 3.4a. Block diagram showing the NE561B used as an a.m. demodulator

Fig. 3.4b. Practical circuit of the a.m. demodu-

Fine tuning is easily accomplished by using a variable capacitor for C9. However, a potentiometer connected between the power supply lines with the slider connected to pin 6 via a 200 ohm current limiting resistor may be employed.

Components R5, R6, C7 and C8 form the low-pass filter which controls the capture range and the selectivity. The value of the capacitors in microfarads is approximately 2660 divided by the required bandwidth in hertz.

DE-EMPHASIS

The de-emphasis is introduced by merely connecting pin 10 via a capacitor to ground. The value of this capacitor multiplied by the internal eight kilohm resistance should produce a time constant of about 50 µs for the standard f.m. broadcasts in the U.K. Thus $C_6 = 50 \times 10^{-6}/8000 = 6.25 \text{nF}$, but this value is in no way critical.

THE NE561B FOR A.M. RECEPTION

The NE561B can be connected as in the block diagram of Fig. 3.4a for the detection of a.m. signals.

The 90 degree phase shift circuit changes the phase of the input signal so that the voltage controlled oscillator in the phase locked loop operates in phase with the input signal. The output from this oscillator is fed to the product detector where it provides the local oscillator signal.

A practical a.m. detector circuit using the NE561B is shown in Fig. 3.4b. It can be used over a fairly wide frequency range, but component values will be quoted for the medium wave band (550kHz to 1.6MHz).

The values of the by-pass and coupling capacitors should be chosen for a low impedance at the operating frequencies. For medium wave use C2, C7 and C8 may therefore be 0.1μ F.

CAPACITOR TUNING

The value of C5 must be selected so that the voltage controlled oscillator operates at the required input signal frequency. If desired, the capacitor C5 may be a variable one, in which case the connections to pin 6 (R3 and VR1) may be omitted.

When a variable capacitor is employed for C5, its value will be approximately 300 divided by the input signal frequency in megahertz at the capacitor setting concerned. For the 550kHz to 1.6MHz range, the value of C5 should range from about 550pF to about 180pF.

RESISTOR TUNING

If the tuning is to be carried out by the variable resistor VR1, the value of C5 should be chosen so that when no current is injected or removed from pin 6, the voltage controlled oscillator operates at the geometric mean frequency of the band to be received. This geometric mean is equal to the square root of the product of the lowest and highest frequencies in the band. In the case of the 550kHz to 1.6MHz receiver, this mean frequency works out as 940kHz.

The complete medium wave band may be tuned by VR1; this potentiometer may be a ten-turn helical type to permit accurate setting. The value of R3 is selected to give the desired tuning range and will be about 1.2 kilohm when an 18V power supply is employed.

PHASE SHIFT

The component values of the phase shift circuit may be determined in the following way. If $R_1 = R_2 = 3k\Omega$, the $C_1 = C_6 = (1.3 \times 1.3)$

where f is the midband frequency. In the medium wave receiver, f is 0.94MHz and $C_1 = C_6 = 1.35 \times 10^{-10} \text{F} = 135 \text{pF}$.

LOW-PASS FILTER

The value of the low-pass filter capacitor, C4, is not at all critical, since no information is derived directly from the loop error signal. One merely requires to establish stable operation. A 10nF capacitor is suitable for C4.

TAPE RECORDER FLUTTER METER

A circuit devised by R. Blair of Houston using the NE561B in a tape recorder flutter meter is shown in Fig. 3.5. A 3kHz sinewave is fed to the recording head. The output from the replay head is fed to the phase locked loop which detects any variations in frequency from the 3kHz value.

The NE561B circuit is set to a nominal value of 3kHz using the fine tuning control. The demodulated output is capacitively coupled to an amplifier of high input impedance. The output level changes with any change in the frequency of the signal

applied to the phase locked loop.

An oscilloscope may be employed to measure the peak deviations and a true r.m.s. voltmeter to make r.m.s. flutter measurements. (The waveform is complex and therefore meters which read the peak or average value will not give true readings.) The output can be filtered to study any selected bands of frequencies.

THE 565

One of the best known low frequency phase locked loops is the 565 device. This is available as the Signetics NE565A device and as the National Semiconductor LM565CN device in a 14 pin dual-in-line encapsulation. The NE565K and the LM565CH are electrically equivalent devices in a TO-99 circular encapsulation.

The basic circuit for all of these devices together with the pin connections is shown in block form

in Fig. 3.6.

The loop is broken between the output of the voltage controlled oscillator and the input to the phase comparator (pins 4 and 5 respectively) so that frequency divider circuits can be inserted at this point for frequency synthesis applications. The low-pass filter is formed by the internal resistor marked RA in Fig. 3.6 and the external capacitor C2.

FREQUENCY RANGE

The maximum frequency at which the voltage controlled oscillator of the 565 devices can operate is

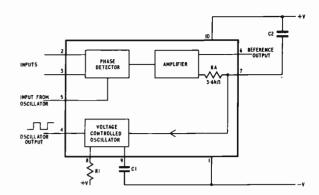


Fig. 3.6. Block diagram of the 565 low frequency phase locked loop. This is the pin numbering for the NE565A (Signetics) and the LM565CN (National Semiconductor), both 14 pin dual-inline

about 500kHz. The minimum practical operating frequency is set by the maximum value of the timing capacitor (C1 in Fig. 3.6) which can reasonably be used. If one decides that this maximum value is $10.000\mu\text{F}$, one can obtain a frequency as low as 0.001Hz

The free-running frequency of the voltage controlled oscillator is only partly determined by the value of the timing capacitor C1. The frequency can be changed over a range of at least 10:1 using a single value of C1 by varying the value of R1 in the pin 8 circuit; alternatively the value of the current fed to pin 8 may be varied.

The typical variation of the free-running frequency with the value of R1 for four values of the timing capacitor is shown in Fig. 3.7. For any given value of the timing capacitor, the free-running frequency is about an order of magnitude lower than that of the high frequency loops.

The free-running frequency of the 565 oscillator is given by the approximate equation $f=1.2/(4R_1C_1)$ where R1 and C1 are the timing components shown in Fig. 3.6.

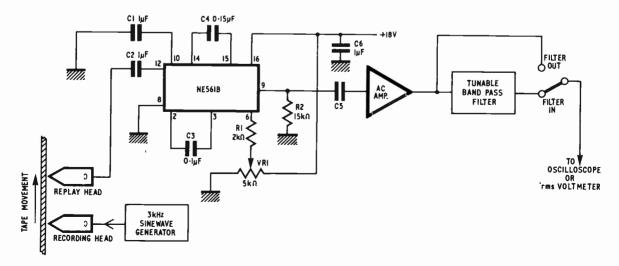


Fig. 3.5. A tape recorder flutter meter using the NE561B phase locked loop

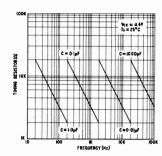


Fig. 3.7. Relationship between the centre frequency and the timing components for the 565 integrated circuit

The value of the timing capacitor C1 can vary over wide limits, but the resistor R1 should have a value of between $2k\Omega$ and $20k\Omega$, the optimum being about $4k\Omega$.

When using power supply lines which are symmetrical with respect to ground, the range of voltages which may be employed is $\pm 5V$ to $\pm 12V$. When $\pm 6V$ power supplies are employed, the typical current taken is 8mA with a maximum value of 12mA. The maximum permissible power dissipation is 300mW.

THE OSCILLATOR

The voltage controlled oscillator circuit used in the 565 devices can be obtained as a separate integrated circuit type 566. It is available as the Signetics 8 pin dual-in-line device type NE566V and the similar National Semiconductor device type LM566CN. The circular TO-99 equivalents are types NE566T and LM566CH. The SE566T and LM566H are close tolerance devices.

In the 565 phase locked loops, triangular and square waves are generated by the voltage controlled oscillator, but no buffer stage is provided to give a triangular wave output as in the 566. The square wave output (about 5.4V peak-to-peak) is available at pin 4 of the 565.

The output of the low-pass filter (pin 7 of Fig. 3.6) is connected internally to the voltage control input of the oscillator. The oscillator frequency can therefore be controlled by a signal fed to the demodulated output terminal (pin 7).

LOCKING RANGE

The range of input frequencies over which the loop will remain in lock on each side of the centre frequency is given by the approximate expression $\pm 8f/V$ where f is the centre frequency and V is the total voltage between the power supply lines.

The 565 can therefore track the input frequency over a very wide range (typically $\pm 60\%$ of the centre frequency). Locking can be obtained over a greater fraction of the input frequency than in the case of high frequency loops.

The 565 input impedance is typically 10 kilohm (minimum 5 kilohm). The minimum input signal required to produce tracking is typically 1mV r.m.s.

The linearity of the f.m. response is very good (typically about 0.2%).

FREQUENCY MULTIPLICATION

In the circuit of Fig. 3.8, a frequency divider circuit has been inserted in the loop between pins 4 and 5. The output of the voltage controlled oscillator is divided in frequency by a certain factor and the frequency divided circuit locks with the input signal. The oscillator therefore operates at a higher frequency than the input signal.

The value of C2 should be adequate to eliminate variations in the demodulated output voltage at pin 7 in order to stabilise the voltage controlled oscil-

lator frequency.

The square wave output frequency can be taken from pin 4.

METAL DETECTOR

Phase locked loops can be used to detect changes of frequency. Such changes can be produced when the coil of a tuned circuit approaches a piece of metal. Phase locked loops can therefore be used in metal detectors.

A circuit of this type which has been designed by J. Blecksmith of California is shown in Fig. 3.9. The 8in diameter search coil comprises 30 turns of copper wire (26 s.w.g.) and has an inductance of about 0.5mH. It is connected in the Colpitts oscillator circuit of TR1 which operates at about 100kHz.

This oscillator is coupled by C3 into the input of the 565 circuit (pin 2). A current source (TR2 and TR3) is employed to supply most of the current of about 2.5mA which passes to pin 8 and which equals the charging and discharging current of C4. The use of this current source increases the output of the loop at pin 7 to about 0.5V for a 1% frequency deviation. (This follows from the fact that the $20k\Omega$ resistor R7 will produce a change in the current to pin 8 of 0.5/20,000 = 0.025mA for a 0.5V change. In other words a change of 0.5V produces about 1% change in the pin 8 current.)

The output voltage at pin 7 is compared with the reference voltage at pin 6 by the differential amplifier of TR4 and TR5. The output of this amplifier drives a centre reading meter which has a $\pm 100 \mu$ A scale. The meter zero is set by VR2 and the sensitivity by VR3.

When the search coil is brought near to a nonferrous metal object, the frequency of the TR1 oscillator circuit will rise and so will the meter indication. Any object containing iron will increase the inductance of the loop and reduce the frequency of oscillation; the meter reading will therefore fall.

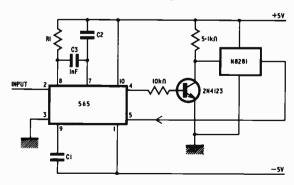
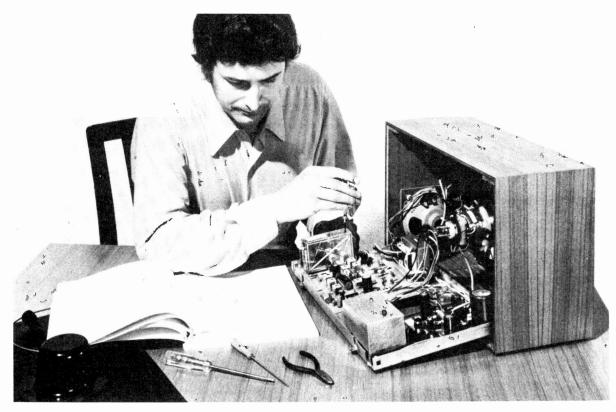


Fig. 3.8. A frequency multiplier using the 565 and a divider



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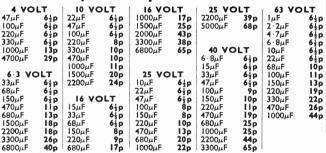
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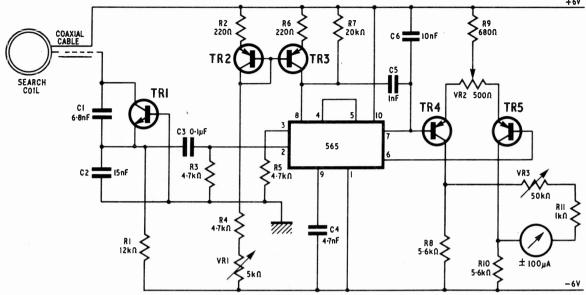


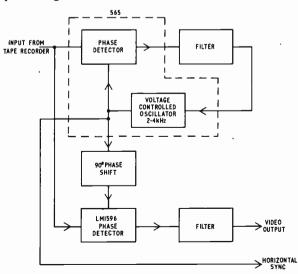
Fig. 3.9. A metal detector using the 565

WEATHER SATELLITE APPLICATION

As an example of a very different application of the 565, its use in a weather satellite picture demodulator will be outlined.

Weather satellites continually photograph the earth from a distance of typically a few hundred miles. The pictures are stored in an electrostatic Vidicon tube and are read out during the succeeding 200 seconds.

The signal is transmitted on a 137.5MHz carrier frequency modulated with a 2.4kHz sub-carrier; the latter contains the picture information. demodulated 2.4kHz tone is normally recorded on tape at the receiving station for subsequent processing.



Flg. 3.10. A system for demodulating video signals from the 2-4kHz sub-carrier which is used by weather satellites

When the tape is replayed, it is desirable to reproduce the 2.4kHz sub-carrier using a phase locked loop, since the latter will effectively filter out most of the noise and will track any flutter in the magnetic tape mechanism.

The basic circuit used in this application is shown in Fig. 3.10. The loop locks at the 2.4kHz frequency. If this is also the centre frequency of the loop, the square wave output from pin 4 of the 565 will be 90 degree out of phase with the input.

However, the zero crossing times of the triangular wave across the timing capacitor may be applied to the LM1596 doubled balanced modulator so that switching occurs in phase with the 2.4kHz subcarrier.

The picture may be reproduced on a cathode ray tube. Detailed circuit information is available in the National Semiconductor report AN-46.

AVAILABILITY

The Signetics phase locked loops are about the most widely available type at the present time and are available from many of the advertisers in Practical Electronics. The NE560B, NE561B and NE562B are available from S.D.S. Components Ltd., Portsmouth PO3 5JW at about £4.20 in small quantities. The Signetics 565, 566 and 567 are obtainable from the same source at about £4, £1.44 and £3.25 respectively.

National Semiconductor devices can be obtained from Semiconductor Specialists, Farfield Road, West Drayton.

Further information on these devices may be obtained from the Signetics Linear Integrated Circuit book and in data and applications notes from Signetics and National Semiconductors.

Next month: more applications of phase locked loop integrated circuits will be described including stereo decoding

LOGIC TUTOR

EXPERIMENTS.



THE FULL ADDER

N PRACTICE we must be able to add together two multidigit numbers and as we saw last month the HALF ADDER does not go quite far enough to doing this. We have to design a circuit that is capable of accepting the two digits of the column (A with B) and incorporate a possible carry over from the previous (less significant) column.

TWO STAGES

The simplest way of doing this is to carry out the operation in two stages; first add together the digits that are in the higher significance column—this is done in the HALF ADDER 1 of Fig. 8.1.

If the digits were 0 and 0 we would get a partial sum of 0 and a carry of 0. If either of the digits were 1 we would get a partial sum of 1 and a carry of 0 but if both digits were 1 we would get a partial sum of 0 and a carry of 1.

We shall come back to this carry in a moment but remember that if we get a carry, at all, at the output of HALF ADDER 1 the sum output of it is bound to be 0.

We now take the partial sum from the first HALF ADDER and combine it with the carry digit—that might have been generated by the previous column. This is done in HALF ADDER 2. This will generate a final sum and could generate a carry.

If you think about it you will see that if a carry is generated at the output of HALF ADDER I it is not possible to get a carry from HALF ADDER 2 (because the sum from the first stage would have been bound to be 0). However, if the sum from the first stage was I it *might* be that there was a carry in from the previous column and these combine in the second stage to give a carry out as well as the final sum. Whatever happens it is not possible to get a carry out of both stages at the same time so there is no question of having to add two carries together.

FULL ADDER

Thus to generate a final carry out of the complete unit we only have to OR together the two possible sources of carry. This circuit is called a FULL ADDER and can be made using the building blocks we have already described in NAND form. We need two HALF ADDERS and an OR gate.

An unsimplified circuit showing the discrete stages in NAND logic appears in Fig. 8.2. Do not make this on Logic Tutor because we can simplify the circuit a little. Notice that we have double inversion on the two lines feeding the final NAND gate of the OR block. These negate each other and we are left with a complete FULL ADDER using nine NAND gates in Fig. 8.3. This you can make on Logic Tutor.

Using the switches and lamps and a piece of paper and a pencil show that the circuit truthfully follows the rules of arithmetic necessary to add the three input digits together.

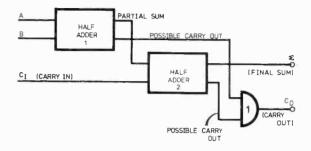


Fig. 8.1. Two HALF ADDERS are combined to form a FULL ADDER

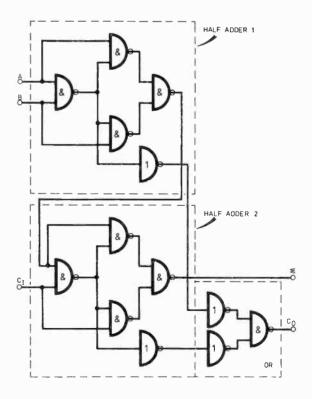


Fig. 8.2. A FULL ADDER using blocks of logic in unsimplified form. Note the two sets of double inversion before the final NAND gate in the \mathbf{C}_0 line

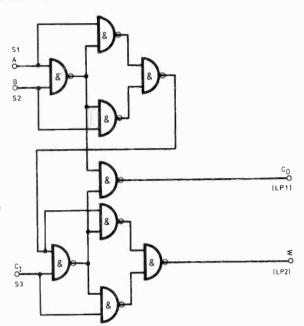


Fig. 8.3. A FULL ADDER that can be built on the Logic Tutor

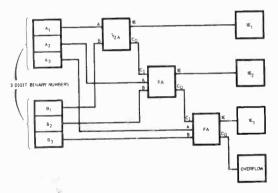


Fig. 8.4. Block diagram of a parallel adder capable of summing two, three-digit binary numbers to give a three- or four-digit answer

MULTIDIGIT NUMBERS

In practice we have to add multidigit numbers together and the simplest way of doing this is to cascade FULL ADDERS—one after the other. The carry out from the previous column is connected directly to the carry in of the next. Fig. 8.4 is a block diagram of such a summing unit.

Al and Bl are the least significant digits of the respective multidigit numbers and because of this they only need a HALF ADDER to produce a true sum and carry; however, all higher order digits have to be combined in FULL ADDERS.

You would need as many adding stages as there are digits when carrying out the process in parallel form consequently a parallel adder can be quite expensive but it is very fast in operation. A cheaper form is the serial adder (not shown in this series) but there is rather more complexity in handling the carry signals.

by M. J. Hughe's



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R.D.R.

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S.R.L.

PERORDO PART 4 MEGNANIGAL ASSEMBLY & INTERWIRING

BY R.A.COLE

FACIA

SURROUND

INTERWIRING & HARNESS

Note that Note that Note that the norm of the main chassis member which forms a trough-like carrier for the power sections of the system. Now we come to a discussion of the general mechanical assembly and the wiring of the system.

GENERAL CONSTRUCTION

The facia of the RONDO system supports both the controls and the r.f. tuning unit, whilst the remainder of the boards are assembled in the chassis pan itself. Thus, as can be seen from Fig. 4.1 the facia consists of an aluminium framework supported on four columns which are held in the main chassis by screws.

The columns support two crossmembers (Fig. 4.1b) made from aluminium angle (½in × 1in) which in turn support two sections of aluminium extrusion made specially for the RONDO system and available from a number of kit suppliers. The two sections are separated by an inverted "U" section of brushed aluminium provided with ventilation louvres.

For those who wish to make their own facia this may be made up from sheet material bent up into the form at Fig. 4.1a, again supported on the columns and drilled so as to carry a simple aluminium facia in plain sheet. Drilling for this is identical to that for the pre-form material with the addition of master tone board mounting screw holes added.

The plain face area shown above the four input selector push-buttons on the left of the RONDO is allocated to the tuner section, yet to be described.

The final main part of the mechanical assembly is the "wrap-round" or surround which forms the sides of the RONDO. This is made from wood, veneered chipboard, or the like according to taste.

From Fig. 4.2 which shows the surround it will be seen that there are two alternative methods of fixing between the surround and the basic trough chassis. The first is to make use of the natural spring in the bent-up chassis by springing the two longer sides apart slightly such that when the surround is finally lowered over the facia to abut the two flanges on the trough, these are pushed in against the spring action. As the surround is lowered further they will then spring out to engage with the two grooves cut in the inner long surfaces of the surround.

If the constructor prefers, he may replace this method with one in which the surround is reduced in depth by the distance between the lower edge and the grooves and is supported on an extension bolted to the two trough flanges as shown in Fig. 4.2.

WIRING DETAILS

The P.E. RONDO quadraphonic system is quite complex and, if not carefully wired, will result in an untidy maze. It is therefore strongly recommended that a prefabricated wiring harness, or cableform, be made to cover the bulk of the inter-unit wiring.

This cableform is constructed by means of a simple jig illustrated in Fig. 4.3 and made from a suitable piece of wood into which a pattern of "pins" is fixed; 1½ in panel pins are ideal for this purpose. They are hammered into the appropriate points as shown and the heads are then clipped off and the sharp ends smoothed.

When assembling the cableform make certain that each wire or cable is inserted in the order given in Table 4.1, since otherwise both simple mechanical and electrical problems can arise.

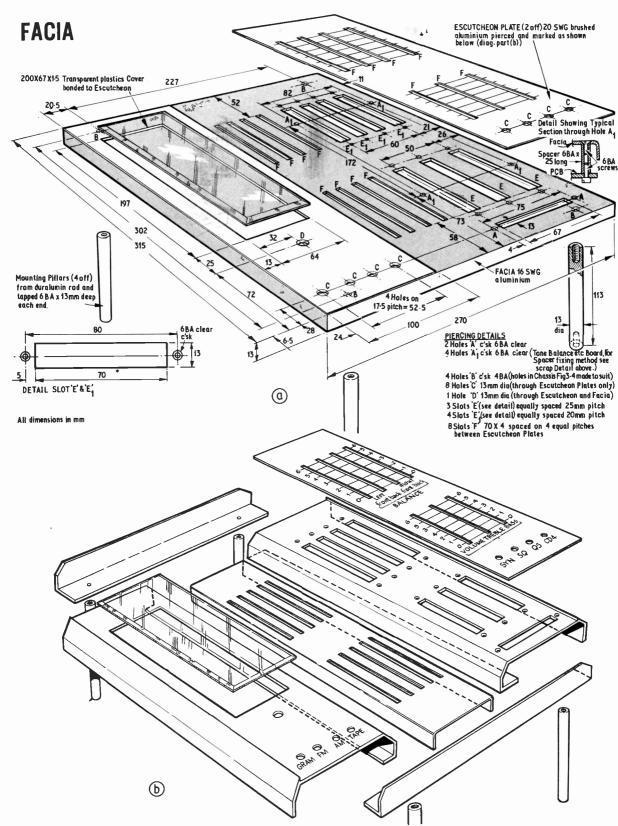


Fig. 4.1. Construction of the facia. The upper drawing (a) shows the method of assembly using "home-made" aluminium panels and the lower drawing (b) shows the method of assembly using ready-made aluminium extrusions

SURROUND & LOOM

(mide dimension)

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Fig. 4.2. Construction of the wooden surround with details of the two methods of fixing the trough

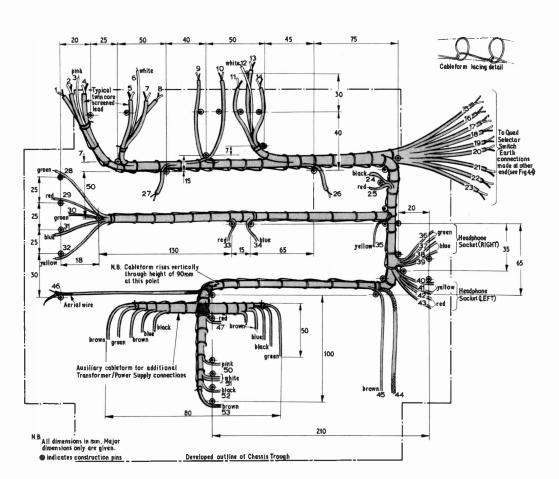


Fig. 4.3. Details of the cableform wiring harness. Interwiring between the units is greatly simplified if a cableform system is constructed as shown here

Each piece of wire is firmly secured by wrapping its start end round the first pin and then laying it along the route shown in Fig. 4.3 and the point-to-point wiring and assembly diagram of Fig. 4.4.

The intermediate pins along a route are used as guides and gentle tension is applied to each wire in order to produce a neat and tidy result. At the termination point the wire is again secured to the adjacent pin by wrapping. With the heavier wires it may be found necessary to knot the wire around the pin.

A "tail" some two to three inches long should be left at each end of each wire for later circuit connecting.

The cableform may now be "laced" up using lacing twine or, failing the availability of this, a waxed heavy thread or light nylon line. A simple form of lacing is shown in Fig. 4.3 from which it will be seen that this is merely a matter of tying the cableform into one cohesive unit by using a series of loops around the cables every $\frac{3}{4}$ in or so.

After lacing, the cableform is gently eased from the pins and is now ready for positioning in the trough.

MECHANICAL ASSEMBLY

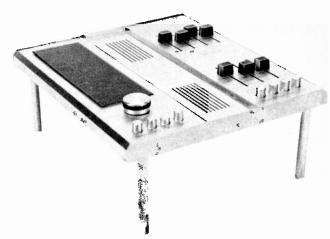
The two power amplifiers, already assembled complete with heat sinks, are laid side by side, copper side upwards on the bench. The power rails and earth rails are connected and flying leads are soldered as shown in Fig. 4.6.

The next step is to fit all sockets, rubber feet and mains lead grommet to the chassis as shown in Fig. 4.4. The wiring harness is then laid in the bottom of the main chassis as shown.

Starting at the rear of the chassis carefully identify each wire and its connecting point. Cut the wire tails to length and carefully strip the ends, wrap round and then solder. Repeat this procedure until

Table 4.1

Start	Finish	Signal	Cable Type
1 2 4 5 7 8 8 11 13 14 9 10 3 6 12 24 25 35 40 34 39 33 43 30 36 53 46	15 16 17 18 19 20 21 22 23 26 27 50 51 51 52 47 40 32 39 31 43 29 36 28 45 44	CD4 " SQ " QS " LAI/P RAI/P + 24V Rail + 20V Rail + 15V Rail LF O/P " B O/P " RB O/P " RB O/P " RB O/P " RB O/P " Aerial	Twin screened 14/0.0076 Pink White Black Red Yellow Red Red Green Brown Miniature Co-Ax



all wires that are shown to be terminated are soldered.

The remaining wires and their terminations are associated with the tuner unit which is to be the subject of a separate article and they will be described in detail then.

The two power amplifier boards, now joined together, are placed component side upwards in the chassis. The two right-hand limbs of the wiring harness (as seen from the front of the chassis) should be under the boards and the left-hand limb along the edge of the heat sink.

Ensure that the yellow, blue, red and green wires, in the centre limb of the harness, protrude above the boards at the appropriate outlet points. Cut, strip, wrap and solder them. Similarly treat the red and black wires in the right-hand limb, soldering them to the positive and negative 15 V rails on the power amplifier board.

The two rails are duplicated on the rear power amplifier board and the two boards are joined with short lengths of red and black wire interconnecting the rails.

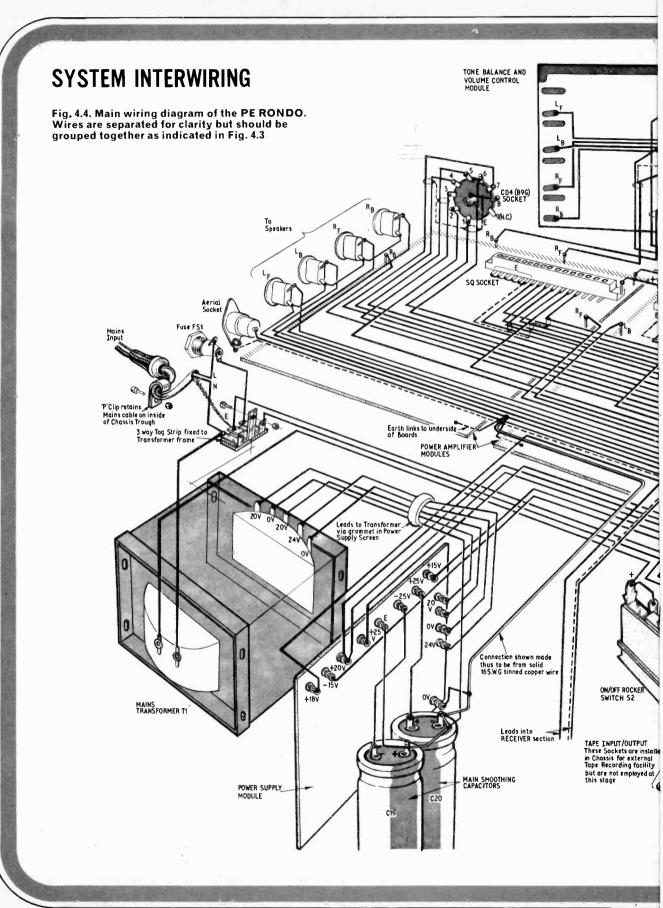
HEADPHONE SOCKETS

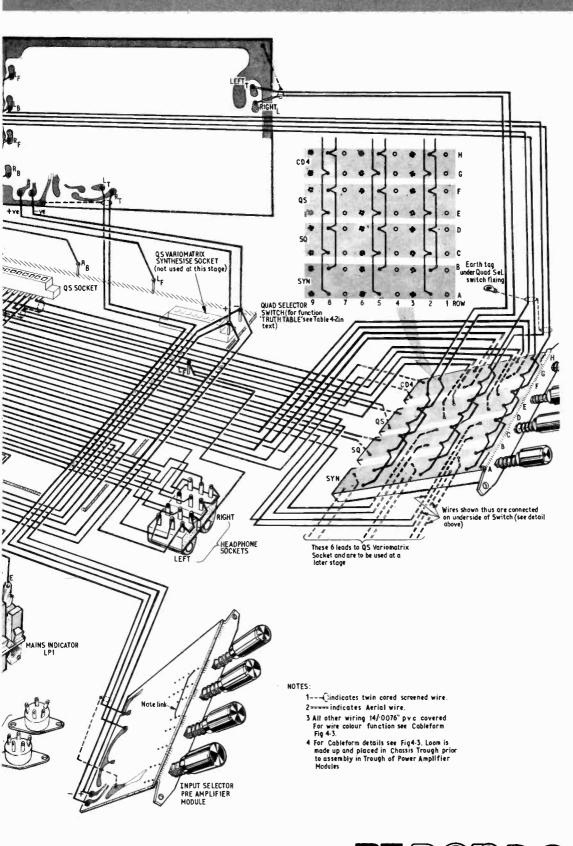
A group of four pairs of wires, each pair of one colour, namely yellow, blue, red and green, protrudes from the front of the harness in line with the headphone sockets. These wires are connected to the headphone sockets, as shown, ensuring that the leads from the power amplifiers go to the appropriate tags on the *right* side of the headphone sockets as viewed from the front of the chassis. If these connections are not correctly made the headphones will not function correctly.

The headphone sockets shown are of the normal three-wire type which can exhibit problems with the amplifiers set to high output levels. It is possible to either damage the headphones or the eardrums if care is not taken when plugging the headset in.

It is therefore recommended that the constructor either takes great care under these circumstances or adopts the use of a new style or socket which has just come onto the market. The new socket interposes a load in series with the headphones in order to limit the output level and current to a safe value.

Using the new sockets, a suitable load resistor for most applications is 220Ω , $\frac{1}{2}W$.





POWER SUPPLY SUB-ASSEMBLY

Returning now to the power supply sub-assembly; fit the complete sub-assembly to the chassis with four ‡in round-head 4BA screws, plain washers, lock washers and nuts. Similarly secure the power amplifiers to the chassis by means of the heat sinks. Fit the main smoothing capacitors to the chassis by means of capacitor clips.

The power supply includes transformer, power board and main smoothing capacitors and is shielded by means of two steel screens. The smaller of these screens, shown in Fig. 3.6, acts as a support-

ing baffle for the power supply board.

It is first fastened to one end of the mains transformer by four ½in round-head 4BA screws, each fitted with one plain washer, one lock washer and a nut. The board is then secured to this baffle by three ¾in round-head 6BA screws, washers and nuts and, in each case, a ¾in spacer is interposed between the board and the baffle.

The larger of the two steel screens is now fitted

· to the chassis.

Refer to Fig. 4.4 and connect the leads to the power supply coming from the harness. Connect the mains lead and switch/pilot light as shown in Fig. 4.4.

Prepare the pre-amplifier board with flying leads

for connection to the main chassis components. Similarly connect the master volume/tone/balance control board. Reference to Fig. 4.4 will give the necessary guidance.

The four-way, six-change-over, pushbutton bank is now pre-wired in accordance with Fig. 4.4 and

Table 4.2.

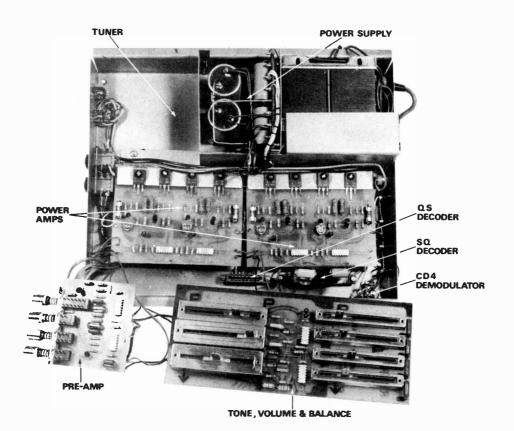
The nine pairs of screened leads protruding from the right-hand front of the wiring harness are carefully stripped and identified. Connection of these leads to the switch bank is carried out with reference to the figure.

Please note that no wiring is provided for the SYNTHESISE position on the pushbutton bank. Details of this facility will be given in a later article together with the wiring of the tape sockets.

Fuses are now inserted into the holders on the power amplifier boards and into the mains fuse holder. See components list for ratings.

AMPLIFIER CHECKING

Before commencing, carefully check the accuracy and completeness of the wiring. Extra time spent here can save expensive components coming to undue harm. Ideally, a parallel check between the unit, layout drawings and theoretical circuit should be performed.



Connect the speaker outlets to dummy 8Ω loads. The dummy load may be made up from 15, 120Ω ½W carbon resistors connected in parallel. Only one load need be made as each amplifier is tested individually.

As the initial output power will be fairly low on setting up, 2W resistors are adequate. If a cheap 80 loudspeaker is available to monitor each channel as it is set up, so much the better. Do not, however, risk a good loudspeaker at this stage.

Turn the presets on all power amplifier channels to maximum, that is clockwise. Reduce all level and balance controls on the master board to mini-

mum and set the tone controls mid-way.

COMPONENTS . . .

Resistors

Headphone load resistors $220\Omega \pm W$ (4 off) Dummy load for testing $120\Omega \frac{1}{2} \hat{W}$ (15 off)

Plugs and Sockets

Speaker sockets Tape in/out sockets Aerial socket Headphone sockets

CD4 connector SQ edge connector

QS Variomatrix Synthesise socket QS edge connector Fuse holder

2 pin DIN (4 off) 5 pin 180° DIN (2 off) Coaxial recessed Switched stereo headphone sockets (2 off)

B9G valve base 16 way 0.15in pitch edge connector

8 way 0.15in pitch edge connector 8 way edge connector 20mm chassis type

Switches

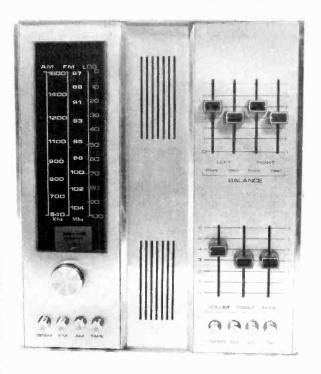
Push button bank, 4 bank, 17.5mm spacing, with each bank 6-changeover per bank

Wiring

32ft 14/0.0076in stranded single p.v.c. (yellow 3ft, blue 3ft, red 5ft, green 5ft, white 5ft, pink 3ft, brown 6ft, black 2ft) 20ft twin screened lightweight audio wire 2ft single screened light co-ax. 8ft lacing cord Mains lead 3-core to suit 2ft tinned copper 16 s.w.g. wire

Aluminium extrusion for facia (available from Sonax Electronics) or plain 18 gauge sheet aluminium if alternative construction method is used. Aluminium "L" or "U" form and §in rod for support members for facia. Boxform surround (from Sonax) or wood to make

Miscellaneous 3-way terminal tag strip Rubber feet (4 off) Grommet $\frac{1}{2}$ in $\times \frac{1}{4}$ in, sleeved grommet for mains in 4BA roundhead screws (17 off) 4BA nuts, plain washers and lock washers (17 off) in 6BA roundhead bolts (16 off) in 6BA roundhead bolts (6 off) ∦in 6BA roundhead bolts (3 off) 6BA nuts, plain and lock washers (25 off)



Connect a d.c. millivoltmeter across resistors R29 and R30 as shown in Fig. 4.6 on one power stage. The sum of these two resistors is approximately 1Ω . Switch on the complete system.

At this stage a variable input transformer (Variac) to adjust the mains supply slowly is very useful,

but not essential.

The millivoltmeter should now read from 2 to

10mV d.c.

If the reading is more than 50mV switch off and check wiring again. If all is well, slowly rotate the preset VR8 anticlockwise until a reading of approximately 20mV is obtained. This reading corresponds to approximately 20mA quiescent current.

Disconnect the meter and repeat the procedure on

all the remaining power amplifiers in turn.

The main amplifiers are now set for optimum quiescent current conditions and should not require re-setting at all.

FINAL MECHANICAL ASSEMBLY

The master volume and tone board, preamplifier board and quadraphonic selector switch are all assembled on the facia as shown in Fig. 4.1. It must be remembered that the wiring to these boards should be kept as short as possible to avoid interference and hum. However, they must be sufficiently long to allow both initial assembly and possible later dissembly.

The facia may now be attached to the trough by its pillars and 4BA screws inserted upwards from

beneath the trough in the holes provided.

The surround may now be placed over the facia and dropped down to engage with the lips on the trough for either of the two fixing methods described earlier to be effected.

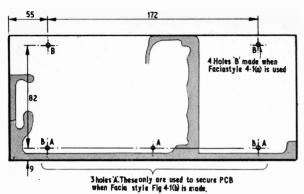


Fig. 4.5. Drilling details of the Tone/Master volume board to suit the facia of Fig. 4.4a.

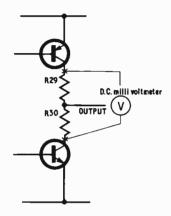


Fig. 4.6. Location of the test points for measurement of the quiescent current in the power amplifiers

Where "spring" locating method is used to retain the surround the exact fit is adjusted as required by applying a slight set to the sprung chassis sides. Be careful not to overdo the tension as this will make subsequent removal of the surround difficult.

Ideally the springing should just cause the flanges to "bite" the surround as it is lowered into position and adjustment can be made in small steps until correct setting is achieved.

To remove the surround using the same method it is simply a matter of placing the finger tips against the long sides from below and pressing lightly inwards until the lips of the flanges release from the grooves. The approach from below is important as working from above is rather difficult. Thus it is simplest to place the unit on a box or other object first so that the hands can be positioned lower than the bottom of the unit.

After releasing from the grooves a gentle upward pressure will slide the surround free for removal.

EARTHING

The use of a wiring loom reduces the problems encountered with hum and stray pickup and it is for this reason that we have described a loom here. Further steps can be taken to minimise these unwanted signals.

Firstly, ensure that both screens are electrically connected to the main chassis which must be itself

Table 4.1 WIRING OF QUAD SELECTOR SWITCH

TOP SIDE WIRING			
UNDERSIDE WIRING			
Synthesise $\begin{cases} R_F = 3A \\ R_B = 3B \end{cases}$	$L_F=6A$ $R_T=9A$ $L_B=6B$ $L_T=9B$		

Synthesise	$\begin{cases} R_F = 3A \\ R_B = 3B \end{cases}$	$L_F=6A$ $L_B=6B$	$R_T = 9A$ $L_T = 9B$
SQ	${R_{\rm F}=3C \atop R_{\rm B}=3D}$	$L_F=6C$ $L_B=6D$	$R_T = 9C$ $L_T = 9D$
QS	$ \begin{cases} R_F = 3E \\ R_B = 3F \end{cases} $	$L_{\mathrm{F}} = 6E$ $L_{\mathrm{B}} = 6F$	$R_T = 9E$ $L_T = 9F$
CD4	${R_{\mathrm{F}}=3G \atop R_{\mathrm{B}}=3H}$	$L_{\mathrm{F}}{=}6G$ $L_{\mathrm{B}}{=}6H$	$R_T = 9G$ $L_T = 9H$
Rows 1, 4 a	nd 7 have no	connections	

connected to mains earth. Thus if there is any doubt about good conduction between the screens and chassis it is advisable to either insert a wire link or clean the adjoining faces thoroughly before assembly.

Secondly, there is a very useful technique which can be applied to the RONDO screened leads. Simply make certain that all screens are earthed at the end nearest to the signal source for that particular length of lead. With a system as complex as the RONDO this does make for complexity in deciding which end must be earthed but the results bear out the effort. The constructor may find Fig. 1.15 in the September issue of PRACTICAL ELECTRONICS useful in this context.

If hum is experienced and the circuitry in the area of the decoders is suspected it is advisable to remove the earth connections from both ends of the screened leads between the boards and the selector switch and replace each connection in turn until the hum loop is isolated. This may involve connecting from either end of a cable.

NOTE.

The output transistors in the power amplifiers should be MJE 3055K and MJE 2955K.

Next Month: Loudspeaker enclosure design and construction



RADIO STARS

In the early days of radio astronomy astronomers were constantly pointing out that there were radio sources but no known radio stars. In consequence the actual discovery on rare occasions of a radio star made headlines. Now, however, particularly over the last few months, quite a number have been added to the list. The chance discoveries have now been supplemented by those discovered as a result of a definite programme of search.

Theory suggested that an early type of star which shows emission lines and an excess of infra-red would be a candidate. It is maintained that the infra-red occurs in the surrounding dust and gas. This was the place to look for radio emission.

It is quite a neat piece of work by a team from the Algonquin Radio Observatory in Canada since a comparatively small telescope was used. The telescope operates at a wavelength of 2.8 centimetres and the dish is a mere 46 metres in diameter. Drs Feldman, Marsh and Purton have managed to secure this scoop with apparent ease.

Now, no doubt, the larger telescopes will turn their attention to the matter. Since the astronomers will now know what to look for and where to look, it is to be expected that more will be found and new data will be obtained. It could mean that a new and more successful model of infra-red stars will emerge.

ANOTHER INTERPRETATION OF THE SIBERIAN METEORITE

The spectacular terrestrial catastrophe that took place in Siberia in 1908, has led to much speculation. No remnants of the meteorite have ever been found so many quite bizarre explanations have been forthcoming, from a crashed space vehicle to a lump of anti-matter.

The force that produced the blast is said to have had an energy output of 0.2 to 20 megatons. The physical effect of this is observable even after many years. There is no crater as such for it is a swampy area.

Dr Stephen Hawking has suggested, in the last year or so, that if black holes do exist they would be of all sizes. Many of these could be quite tiny and may well have been formed after a "big bang" start to the universe.

Since in their travels these small units would suck into themselves matter through which they passed they may well be at the centre of stars and even galaxies. Perhaps here might be found a solution to

the problem of gravitational waves.
From the University of Texas
comes a suggestion by Dr A. A. Jackson and Dr M. Ryan. They put



forward the idea that one of the small black holes moving at high speed and passing through the atmosphere would produce temperatures of the order of 105 degrees K.

This would cause ultraviolet radiation and a plasma column would be formed. The black hole would pass right through the Earth because of its small size but would have the mass of an asteroid. This energy would carry it onwards into space.

The plasma column would be dissipated in the surrounding area of entry. This plasma column would be of a deep blue colour. Is it perhaps significant that the many evewitnesses described the appearance of the sighting as a "bright blue

EXTRA VEHICULAR ACTIVITY

A new method of control for astronauts is under development by the RCA Company. The astronaut's voice is used to control movements.

This is a truly significant move. It means that the actual movements required can be initiated by voice commands only. There are 12 basic commands that operate the manoeuvering and propulsion system. Thus right, left, up, down, etc. can be brought to any situa-tion. A dream come true for many applications. It is surely not far from this point to the control of vehicles in terrestrial situations.

Other activities planned for the future concern two satellites to be launched in 1975. Some of the instruments to be carried are for the determination of the immediate Earth environment. More data will be made available from the higher levels of the atmosphere particularly the thermosphere. The sort of instrumentation that is required for this work includes an electron temperature probe as well as the usual photometers and spectrometers.

The data to be gathered will be neutral particle and ion compositions, ion and the natural gas temperature, information about the air-glow and the detection of thermal electrons and photoelectrons.

The satellite will weigh about 1,300 pounds and will carry a momentum wheel for stabilisation.

SKYLAB PRELIMINARY RESULTS

So much data has been gathered on the second Skylab period of observation, that it will take some years to evaluate it all.

Perhaps the most consistent of the findings relate to the Sun. The better observation of the structure of the atmosphere of the Sun and in particular the great hole that has been found in the corona may unlock

secrets far away from the Sun.
Recently Dr C. H. Barrow of the University of the West Indies has been trying a new correlation of micropulsations from the Sun and those observed in the radiations from Jupiter.

It could well be that the information returned from the Jupiter probe, which should be close to the planet on December 10th, will help to establish a positive result. The micropulsations have been known for some years but because of lack of data from the Sun the matter was only spasmodically reviewed.

The hypothesis involved is an important one for, though there have been a number of models evolved, all lack the sort of confirmation required to establish the

COMET KOHOUTEK

Skylab will have a special mission with respect to the comet Kohoutek. The next mission (Skylab 4) is the last in the projected series and begins on November 9th.

Seven of the existing instruments will be brought to bear on the comet and the astronauts will have with them a new far-ultraviolet camera. It should be possible to photograph the neutral hydrogen cloud which is estimated to surround the comet and extend to more than six million miles.

Initially the plans are for the Skylab mission to be completed by January 4th. It would be a pity if this could not be extended January 14th to allow further observation. Such a unique opportunity to study the period immediately after the perihelion passage may never come again.

The best time to view the comet for Earth-based observers is at about 12.00 to 14.00 hrs, right ascension, in the morning sky near the area of the bright star Spica. This will be around December 4th.

PE Sound Synthesiser 11

KEYBOARD

By G.D.SHAW

THE article this month deals with the remainder of the electronics sited within the keyboard unit and details the divider system, the analogue memory or hold circuits, modulation amplifiers, envelope shaper/v.c.a.s and mixer. The overall system has been extensively redesigned to take maximum advantage of the greater versatility of the logarithmic v.c.o.s and with the aim of improving the live performance capability of the instrument.

BLOCK SCHEMATIC

A block schematic arrangement of the keyboard unit is shown in Fig. 11.1 and the unit has been designed to accommodate a four-octave Kimber-Allen keyboard. The specified keyboard may be obtained through the Electronic Organ Constructors Society at 4 Lees Barn Road, Radcliffe-on-Trent, Nottingham NG12 2DS. The E.O.C.S are also able to supply the contact assemblies and mounting strips. The type of contact assembly required is the G.B.-2 paired contact unit, also by Kimber-Allen.

Although a four-octave keyboard is specified it should be made clear that smaller—or larger—units may be employed with no changes to the circuitry other than the adjustment to the number of divider resistors employed. With respect to the use of smaller keyboards, the E.O.C.S. have informed the author that they have a limited number of two-octave organ keyboards by Herrburger Brooks.

These are full sized timber keys faced with plastic and mounted on a hardwood frame. The keys themselves are in reverse colours with black naturals and white sharps, and although they will require to be sprung by the constructor, the additional work required is reflected in the attractive pricing of £5 per keyboard.

Reverting again to Fig. 11.1 it will be seen that the keying system is divided into two channels each channel having its own electronic assemblies and signal path. Signals from both channels join together in the final circuit, a simple virtual-earth mixer. The purpose of this arrangement is to allow a rhythm accompaniment and melody line to be programmed at the same time, channel 1 programmed by the upper 31 keys and channel 2 by the remainder.

The tuning arrangement allows the transition between the two channels to be musically consecutive. Spread apart by one or more octaves or the channels juxtaposed in terms of frequency with the 31 note channel providing a bass line to a treble channel 2. Since the combined effect of the tuning controls is continuously variable there are a number of intermediate possibilities such as channel 2 dupli-

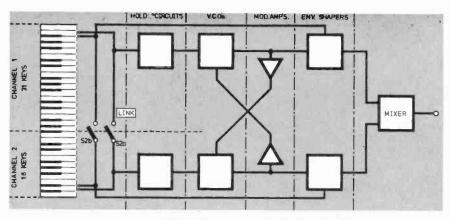


Fig. 11.1. Block schematic of keyboard unit

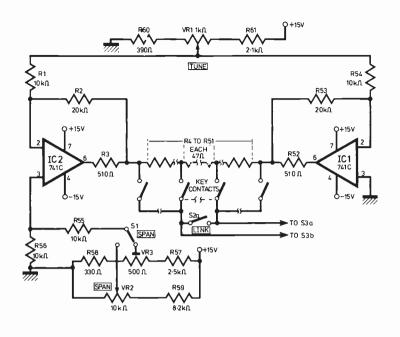


Fig. 11.2. Keyboard divider network

d.p.c.o. miniature toggle the i.c.s may be swung through a range of rather more than 8 volts.

COMPONENTS . . .

Resistors

 $10k\Omega$

 $20k\Omega$

510Ω R4-R51 47Ω (48 off)

2.5kΩ

 330Ω

All 2% metal oxide

Integrated circuits ICI-IC2 741C (2 off)

Potentiometers

wound

carbon VR3 500Ω cermet

Switches

R54-R56 10kΩ (3 off)

R52 510 Ω R53 20k Ω

R60 390Ω R61 2·1kΩ

R₁

R₂

R3

R57

R58 R59 8-2kO

DIVIDER

VR1 1kΩ semi-precision wire-

VR2 10kΩ midget moulded linear

S1 s.p.c.o. miniature toggle

cating sections of channel 1 or, in more bizarre terms, both channels programmed in different keys.

The programming voltage from the keyboard is led to a memory circuit which holds the last voltage entered until such time as a new voltage is programmed or until the hold circuits are grounded. The output voltage from the hold circuit is used to program its respective v.c.o. to the desired frequency which is then amplitude modulated in the envelope shaper/v.c.a. Triggering of the envelope shaper takes place each time a key is depressed in the appropriate channel and each envelope shaper is provided with separate attack and decay controls together with an additional percussive attack facility which may be switched in as desired.

Frequency modulation between oscillators may be achieved by means of the modulation amplifiers which have sufficient gain to swing the frequency of the v.c.o.s through the entire audio spectrum. Finally, a link switch is provided to enable both channels of the system to be programmed in parallel.

THE DIVIDER NETWORK

Fig. 11.2 shows the theoretical circuit of the keyboard divider network in which resistors R4-R51 inclusive form the actual divider which is "floated" between the outputs of two operational amplifiers. The output of IC1 is coupled to the high frequency end of the divider and IC2 to the low frequency end. R60, VR1 and R61 together form an adjustable divider which is coupled to the inverting inputs of both i.c.s. Thus, by means of VR1, the main tuning control, the voltage on output of

Since this latter effect will be equal at both ends of the keyboard it is necessary to apply an offset to one of the i.c.s in order that a voltage differential will exist across the divider chain. The offset is applied to the non-inverting input of IC2 through the medium of either one of two divider chains.

SPAN FACILITY

R57, VR3, R58 provide what has been termed the fixed span facility with the preset VR3 having sufficient swing to enable the V/Octave range to be adjusted between about 400mV/octave to rather more than 1V/octave. R59, VR2 provide the variable span facility which is adjustable over a range of about 8.0V. The setting of VR3 is normally adjusted so that one octave width on the keyboard spans precisely one frequency-octave. VR2 on the other hand enables the frequency spread of one keyboard-octave to be varied between a fraction of a semitone (micro-tones) to several tens of semitones (macro-tones). The actual effect, in terms of frequency range, resulting from the swing on both VR2 and VR3 will depend very much on the requirements demanded by the v.c.o. as a result of the "Law Adjust" setting.

The exact value of the divider resistors R4 to R51 is not too critical except that they should be of sufficiently low a value so that the combined loading of the v.c.o.s does not cause a measurable change in the voltage at any point on the divider. Values between 10 and 60 ohms should meet all the necessary criteria. For best results, however, it is important that, whatever the nominal value of divider resistor chosen, the individual resistors are

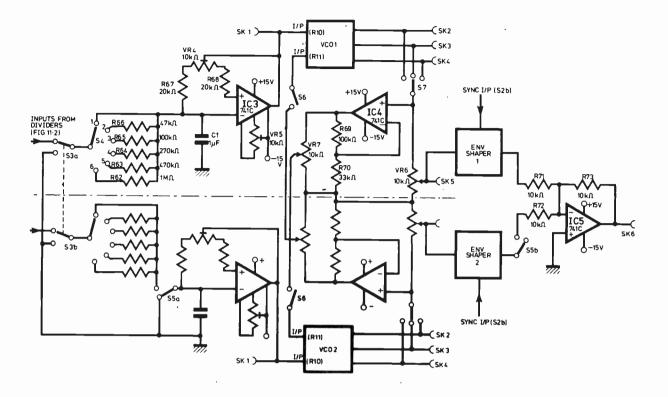
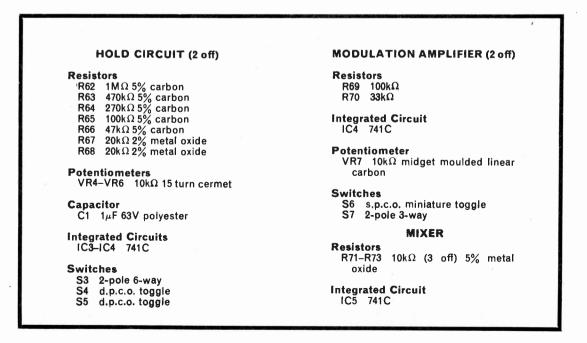


Fig. 11.3. Circuit of hold, modulation amplifier and mixer for both channels with v.c.o. interconnections. The component values for the mirrored hold and modulation amplifier circuits are identical

COMPONENTS...



as closely matched to the nominal value as possible. It is particularly important that the ohmic value of any 12 consecutive resistors in the divider should be a close match with any other selection of 12

consecutive resistors.

The junctions between individual resistors in the divider are hard wired to the moving contact of their respective contact assemblies mounted below the keyboard, the fixed contacts being joined into two bus-bar units which can be joined by means of a link switch. A similar arrangement is employed for the second pair of contacts which serve to provide the sync pulse necessary for the envelope shapers.

ANALOGUE MEMORY

The divider voltage resulting from the depression of any particular key is routed into the analogue memory circuits via S3 and S4 as shown in Fig. 11.3. The purpose of the hold circuit is to retain the last programmed keyboard voltage for sufficient time to enable the desired tone processing to be completed. For example, with S4 in position 1, the depression of a key is sufficient to cause C1 to become charged to the value associated with that particular key. At the same time a sync-pulse is routed to the envelope shaper which, if it is set to provide a rapid attack, will turn on the v.c.a. and allow the oscillator tone to be heard. If the envelope shaper is also set to provide a long decay, the oscillator tone will immediately begin to die away.

In operation the hold circuit utilises the commonmode rejection of the 741 operational amplifier to provide a very high input impedance. Positive and negative feedback are applied by means of R67 and R68 with VR4 serving to provide a balance between the respective levels of feedback to the inverting and non-inverting inputs of the amplifier. C1 is the reservoir capacitor and is coupled directly to the

non-inverting input.

The input impedance of the circuit is given by the paralleled value of R67 + part of VR4, and R68 + part of VR4 times the open loop gain of the amplifier. Thus depending on component tolerances the input impedance can be anywhere within the range 250 to 2,500 megohms and since a 1·0μF capacitor is specified the leakage time constant of the network will similarly vary between 250 and 2,500 seconds.

PORTAMENTO

When keyboard voltages are routed direct to C1 in the hold circuit the change in level of the charge on C1 is virtually instantaneous. However, if a resistance is interposed between the keyboard and C1 the rate of change of charge is inversely proportional to the value of the resistor. This provides a very convenient means of adding a portamento facility and R62-R66 are included for this purpose, being switched in as required by S4.

Portamento is the name given to the effect when the transition between two successive notes in a musical piece is accomplished in a gliding manner encompassing all the intermediate frequencies.

The nature of the hold circuit requires that the setting-up procedure be followed with great care since any output offset voltage present will inevitably cause the holding ability of the circuit to wander. With VR4 in its electrical mid position, and with the wiper grounded, a 10 megohm resistor is connected between the output and inverting input of the amplifier. With power on, VR5 is then adjusted so that the output is precisely zero when observed on the most sensitive setting of the oscilloscope. When satisfied that the initial setting up has been correctly accomplished the circuit connections may be made as generally shown in Fig. 11.3 but omitting the connections to the v.c.o. and portamento resistors. With power on again, and observing the output of IC3 on the oscilloscope, apply about -6V transiently to the junction of R67 and C1. Careful adjustment of VR4 will result in virtually negligible drift and, in the prototype, it was found that a drift of 6mV/20 minutes was quite easily attainable.

The -6V charge on C1 during the setting-up procedure is also quite an important value since it will be found that the circuit will have a much greater degree of drift if the applied voltage is significantly higher or lower than this value. For this reason S5 is provided to ground the input of the hold circuit during switch-on or when the keyboard is "idling" for any length of time thus ensuring that the v.c.o. is not over or under driven.

The output of the hold circuit is routed directly to the R10 input of the v.c.o. the three output waveforms of which are, in turn, routed to a selector

switch, S7.

MODULATION AMPLIFIERS

The wiper of S7 is coupled to the v.c.o. level control VR6 and also directly to the non-inverting input of what has been termed the modulation amplifier. The output of the modulation amplifier driven by VCO1 is then routed to the R11 input of VCO2 through S6, a similar arrangement existing between VCO2 and the R11 input of VCO1.

The net result of this arrangement is that each oscillator can frequency modulate the other either separately or at the same time. Although simple in concept this system is capable of generating waveforms having very complex harmonic structures and is thus able to produce an enormously wide range of

sounds and effects.

In the modulation amplifiers R69 and R70 set the gain at about 4.5 and VR7 provides a modulation depth control. S5a/b provide a means of turning VCO2 off in the sense that its input and output are isolated and its frequency controllable either by its own manual frequency control or by its associated modulation amplifier or both. The main purpose of this arrangement is to allow VCO2 to provide a vibrato modulation to VCO1.

ENVELOPE SHAPERS

From the wiper of VR6 the v.c.o. signal is routed into a v.c.a. based on the MFC6040 which is, in turn, controlled by an envelope shaper triggered by depression of any of the keys on the keyboard. The working of the circuit shown in Fig. 11.4 is as

IC1-TR1 represent a current amplifier/follower with overall feedback. The output at the emitter normally is +4.5V under quiescent conditions thus

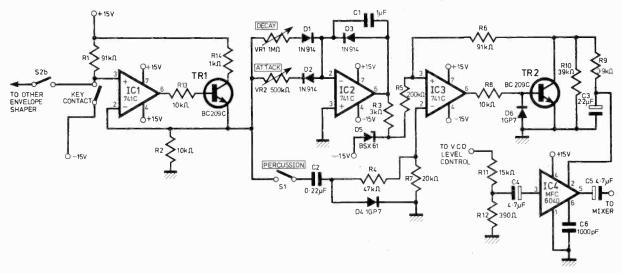


Fig. 11.4. Circuit of keyboard envelope shaper and voltage controlled amplifier

COMPONENTS

ENVELOPE SHAPER (2 off)

			٠		٠				
₹	ρ	s	1	ς	t	o	r	s	

R1	91kΩ		R8	10kΩ
R2	10kΩ		R9	3-9kΩ
R3	3kΩ		R10	39 kΩ
R4	47kΩ		R11	15k Ω
R5	200kΩ		R12	390Ω
R6	$91k\Omega$		R13	$10k\Omega$
R7	20kΩ		R14	1kΩ
All	5% }W	carbon		

Transistors

TR1-TR2 BC209C (2 off)

Integrated Circuits

IC1-IC3 741C (3 off) IC4 MFC6040

Diodes

D1-D3 1N914 (3 off)

D4 1GP7

D5 BZX61 V Zener

D6 1GP7

Capacitors

C1 1μF polyester

0.22µF polyester

C3 $2.2\mu\text{F}$ 35V tantalum C4 $4.7\mu\text{F}$ 35V tantalum

4·7μF 35V tantalum

C6 1,000pF polystyrene

Miscellaneous

S5 d.p.c.o. toggle, S7-4 pole 3 way rotary (2 required), VR6- $10k\Omega$ midget moulded carbon (2 off), 2mm miniature sockets (12 off), 1-4 octave keyboard, G.B-2 pair contacts (49 off) (see text), contact locating strip.

driving IC1 hard negative, or to -12.5V as determined by the divider R3-R5. negative input signal to the non-inverting input of IC2 the output of this device is also negative and TR1 is turned off. With TR2 off the control input of the MFC6040 rises to +6V and thus attenuates the audio input signal by about 77dB.

The application of a negative trigger pulse to the input of IC1 causes TR1 to turn off and the output at R2 to go to -15V. C1 thus discharges via D2/VR2 and the output of IC2 rises from -12.5V to about -4V. Under these conditions the noninverting input of IC3 becomes positively biased, its output goes positive turning on TR2 which thus effectively short circuits R10 and causes the control voltage to IC4 to fall to about +4.3V. When the trigger pulse is removed C1 charges to a level again via D1/VR1 and the original situation is positive restored.

A separate percussive attack can be obtained by differentiating the trigger pulse to the envelope shaper by means of C2. The negative differentiated trigger pulse is applied to the inverting input of IC3 with the effect previously described except that in this case the magnitude of the pulse causes the v.c.a. control voltage to fall to +3.7V corresponding to an audio signal amplification of about 12dB. The percussive attack may be used on its own by advancing the trapezoid attack control to the slowest rate and playing the keys in a staccato manner. Alternatively the percussive attack may be mixed with the normal trapezoid control waveform or it may be switched out altogether by means of S1.

The audio signal outputs of the envelope shapers are led to a simple unity gain, virtual earth mixer shown in Fig. 11.3. The level of signal from each channel is controlled directly from VR6 on each of the oscillators.

Next month: construction of the keyboard housing, wiring and tuning instructions. Details will also be given of a small p.s.u. which will enable the keyboard unit to be operated independently of the main synthesiser.

Strictly

by K. Lenton-Smith

STUDENTS of the Hammond organ can usually detect aurally which models use tone wheels and which use integrated circuits. The "Concorde", introduced over a year ago, was the first Hammond drawbar organ not to use tone wheels. Using L.S.l. techniques it is now possible to synthesise the unique sounds produced by these electromagnetic devices.

Another novel feature of this organ is the multiple derivative divider which divides down the 12 top notes to the sub-octave frequencies giving locked tuning.

Both of these features are also found in the "Regent" cinema type organ which was released recently from the same stable. An adjunct to both instruments is the Automatic Rhythm 3 unit which is unusual in that the waltz may be selected with any other pattern for a rhythm variation (such as waltz/cha-cha!).

NOTHING NEW

There seems to be nothing radically new in the manufacture of electronic instruments at present. The various makers appear to be using integrated circuits wherever possible, having relegated the transistor to "slave" duty.



The Lowrey Venus Stereo with a.o.c. and a Genie supplying rhythm patterns

Though R/C oscillators are usually considered to be less stable than L/C oscillators, manufacturers are now using carefully designed R/C master oscillators—presumably to reduce weight and the possibility of interaction on small printed circuit boards. The Lowrey "Genie" uses this system.

Lowrey are transistorising their automatic orchestra computer circuit, which hitherto used a diode matrix. Unless you play a Lowrey, a.o.c. will not mean much, but the sound is probably unconsciously recognised by those that enjoy light music. Harry Stoneham began to broadcast regularly some six years ago and has been featured by Sam Costa, in "Breakfast Special" and on the Pete Brady Show: more recently, he has appeared in Michael Parkinson's programme. His distinctive sound is usually produced on a Lowrey with the a.o.c. in action, though Harry also plays Hammond with equal dexterity.

A.o.c. allows the performer to play a single note melody on the upper manual (at the selected pitches) which is automatically harmonised with any chord played on the lower manual. Whilst this feature was probably designed with the beginner in mind, the experienced player can produce breathtaking runs of chords. Lelt hand chords must be sustained when using a.o.c. as the harmonising facility is lost when the accompaniment keys are released.

REVERBERATION

An electronic instrument played in a public hall may not need reverberation, though a crowd of people will absorb both reverberation and output power. In a small room with fitted carpets and curtains, the instrument will be dead without some reverberation. Adding echo makes the sound source seem to come from deeper within the speaker enclosure and gives a more natural effect.

Tape, delay lines or spring units may be used, the latter still being the

simplest. Some commercial spring units are too small and consequently produce short delay times, often with too much "direct" signal that can only be reduced by going to work on the circuit board.

It is possible to add reverberation to an existing installation without running to the expense of a further power amplifier if some care is taken. The main amplifier loudspeaker signal is tapped off and fed to the secondary of a small output transformer. It is a good precaution to put a 100Ω resistor in series with one lead to prevent robbing, and a small 6V lamp in series with the other to act as a current limiter. The primary winding of this transformer feeds the driver coil of a magnetic unit such as the Gibbs-Hammond.

The driven coil produces only a few millivolts and requires a preamplifier with a gain of about 50. It is a fairly easy matter to arrange a pair of BC109 transistors, directly coupled, to recover the signal. Small capacitors should be used at both input and output of this preamplifier. The base of the first transistor should be biased by means of a resistor from the emitter of the second transistor.

A $50k\Omega$ potentiometer across the pre-amp output is suggested, with a T attenuator from the slider followed by 250pF before feeding into the main amplifier at a point after the main volume/swell control. The small capacitor tends to accentuate top response. Needless to say, there is some danger of howl due to feedback and the $50k\Omega$ variable should be kept near minimum while setting up. Ideally, the spring driver coil should be fed from a push-pull driver amplifier, but the method outlined above will probably give sufficient echo for most needs, and it has the merit of simplicity.



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- 6. Printed circuit board.
- 7. Keyboard panel.
- 8. Electronic components pack (diodes, resistors, capacitors, transistor).
- Battery clips and on/off switch.
- 10. Soft wallet.



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GW BATTERY FLIMINATOR

BY A.M.RUDKIN B.Sc.(Eng.) Hons.

THERE are many battery operated transistor radios which are used almost entirely in the home, and with the rising cost of replacement batteries the question of a battery eliminator comes to mind. To the home constructor the thought of buying a ready-made unit goes against the grain, but it is not easy to achieve a professional finish in a home-made unit. Fortunately, the battery manufacturer provides us with an easily available case of exactly the right size. The current trend amongst manufacturers is to use a thin metal casing and a battery case of this type can be re-used quite successfully.

Most portable radios used in the home take PP9 batteries or an equivalent and this size is large enough to hold the necessary components to make the eliminator. With a component cost of about £1:50p the unit will pay for itself quite quickly and, of course, the eliminator can easily be removed whenever battery operation is required.

CIRCUIT DESCRIPTION

As can be seen from Fig. 1, the circuit of the battery eliminator is relatively simple, but despite the simplicity the unit delivers a regulated output voltage and provides protection against overloading or short circuits.

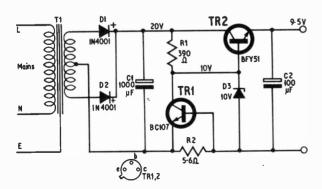


Fig. 1. Circuit diagram of the 9V Battery Eliminator

A miniature mains transformer with a centretapped secondary feeds a full-wave rectifier. The reservoir capacitor, C1, smooths the rectified output before it is applied to the series regulator circuit. A 10 volt Zener diode, D3, provides a fixed base voltage to transistor TR2, which in turn provides a fixed output voltage of about 9.5 volts at low impedance.

À second transistor, TR1, provides current limiting protection since its base-emitter junction is connected across a current sensing resistor, R2.

When the current flowing through the resistor exceeds 100mA the transistor begins to turn on and reduces the voltage across the Zener diode thereby reducing the output voltage so that even under short circuit conditions the current through the series regulator never exceeds a safe value.

COMPONENTS . . .

Resistors

R1 390 Ω R2 5.6 Ω $\pm 10\% \pm W$ carbon

Capacitors

C1, C2 100µF 25V elect. (2 off)

Semiconductors

TR1 BC107 TR2 BFY51

D1, D2 1N4001 (2 off)

D3 10V 400mW Zener

Transformer

T1 Mains primary, 14-0-14 50mA secondary (Henry's type MT991)

Miscellaneous

Printed circuit board, 4BA studding, mains cable, nuts and washers, old PP9 battery case, interconnecting wire

The graph in Fig. 2 shows the way the output voltage varies with load current and the rapid drop in voltage as the current approaches the 120mA limit can clearly be seen.

An electronic "fuse" of this kind may seem a luxury but in fact it costs less than a fuse link and fuse holder whilst offering a high degree of protection. The simple regulator used in the battery eliminator is quite adequate for use with radio receivers and the ripple on the output is low enough not to cause any audible hum in the radio loud-speaker.

MOUNTING COMPONENTS

The electronic components are mounted on two small boards which are supported by screwed rods and it is recommended that printed circuits are used. Dimensions of the boards and the track layouts are shown full size in Fig. 3 and Fig. 5. If facilities for making printed boards are not available then as an alternative 0·lin matrix board (without copper strip) may be used with point to point wiring.

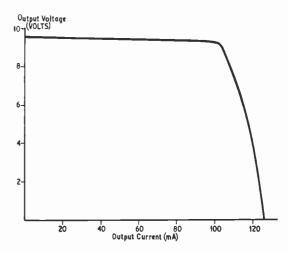
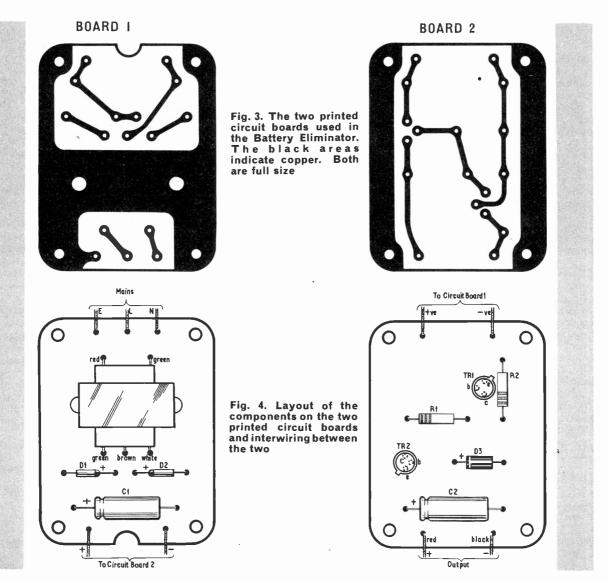
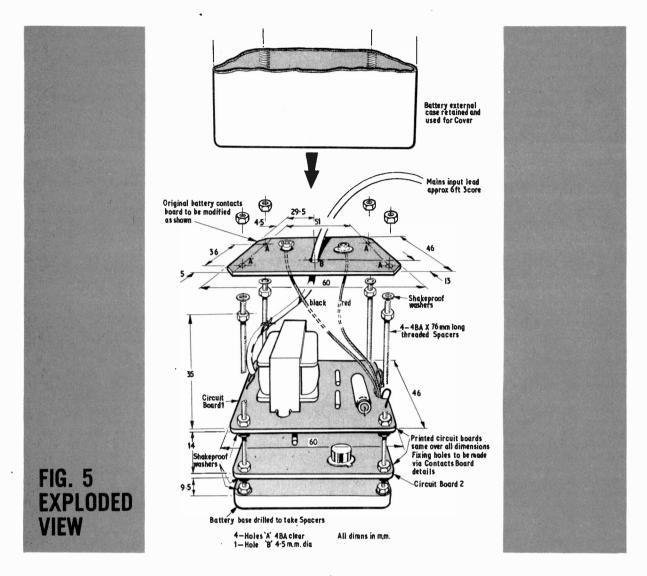


Fig. 2. Graph showing the variation of output voltage with current. The fall off at 100mA is due to the current limiting effect of TR1





Before mounting the mains transformer onto the printed circuit board shorten the leads to about \(\frac{1}{2}\) in and strip the sleeving back to expose \(\frac{1}{2}\) in of the wire. Mount the transformer on the board and bend back the fixing lugs to hold it securely in place. Fit the other components and interconnect the two boards as shown in Fig. 4.

Temporarily connect a mains lead and, as a safety precaution during testing, cover the mains connections with self adhesive p.v.c. tape. Apply the mains and check that the output voltage of the regulator board is approximately 9.5 volts. A voltage very different from this value indicates a fault condition and the voltages indicated on the circuit diagram (Fig. 1) may be used to aid in fault finding.

USING AN OLD BATTERY CASE

It is quite easy to take a battery apart, but some care should be taken in order that the casing may be re-used. The battery should not be so old that the cells have started to leak or the case may be damaged.

In the battery used for the prototype the bottom plate was made of plastic and was held in place by the metal jacket which was folded over the rim of the plate. This fold was carefully straightened by bending back the metal with a small pair of pliers. After this the contents of the battery can be removed by pressing the top plate of the battery downwards.

The six cells are, of course, no longer required, but the other parts should be kept. Contact between the cells and the top plate with the "snap" connectors is by a thin piece of brass strip and a spring contact. Cut off the brass strip and remove the piece of cardboard which separated the top plate from the cells by cutting around the contacts with a knife blade.

Drill holes in the top and bottom plates in accordance with the dimensions given in Fig. 5. The hole for the mains lead is drilled in the top plate only.

ASSEMBLY .

When the boards are functioning correctly they can be assembled onto the screwed rods. The distances between the boards and the plates are shown

continued on page 1097



A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought. This is YOUR page and any idea published will be awarded

This is YOUR page and any idea published will be awa payment according to its merits.

TRACE DOUBLER FOR TTL COMPATIBLE SIGNALS

THE diagram in Fig. 1 shows a circuit for a trace doubler, which displays the time relationship between two series of pulses.

Gate G1 and its associated diode plus two resistors and capacitor form a clock generator with a mark to space ratio of 1 to 1. Gate G3 provides an inverted clock waveform. One input of G4 is the signal input, "A". One input of G5 is the other signal input, "B". The other input of G4 is connected to the output of G3, the inverted clock. The other input of G5 is connected to the output of G2, the true clock.

These two clock signals are always the opposite of

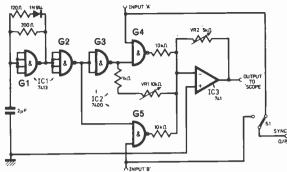


Fig. 1

each other, thus gates G4 and G5 are alternately enabled or disabled. Any output from G4 or G5 is fed to the summing junction of IC3, via a $10k\Omega$ potentiometer and a $1k\Omega$ resistor. The operational amplifier combines the signals and feeds them to the oscilloscope to be displayed.

The idea behind the operation of this circuit is that any signal information from input "A" is added to a constant voltage, the inverted clock and is then

displayed below the trace for input "A".

The 10kΩ potentiometer VR1 varies the separation between the traces and VR2 in the operational amplifiers feedback path controls the overall gain of the instrument.

C. Nicol, Brixton, S.W.9.

SIMPLE VARIABLE-DELAY PULSE CIRCUIT

Variable delay time on a repetitive pulse is frequently required, particularly in those applications concerning transient phenomena. A simple, low cost, and easily constructed electronic circuit is described which enables continuously variable delayed times in the range $10\mu S$ to 80mS to be achieved.

The circuit, shown in Fig. 1, consists of two monostables, the first providing the controlled variable delay time and the second giving the delayed output pulse. The master pulse to be delayed is first differentiated by the R1C1 network. The negative-going spike obtained from this network is then used to turn the first monostable over. The

turn-over period is given by: -

 $T = 0.7 VR_1 \times C_2$, 3, or 4

The positive pulse from the collector of TR1 is fed into the second monostable via another differentiating network. Again the negative-going spike turns the monostable over and a rectangular pulse can be taken from the collector off TR3.

A negative output pulse could be taken from the collector of TR4, but it would be of poor shape due to capacitance C7 charging up via the load R8 in the collector of TR4.

By both making VR1 variable from 100Ω to $10k\Omega$ and by selecting the C2, C3, C4 capacitors having fixed values of 0·1, 1·0 and 10μ F a continuously variable delayed output pulse in the range 10μ S to 80mS has been obtained.

The delayed times are measured from the negative-going edge of the master pulse. Both shorter than 10 µS, and

longer than 80mS can be obtained by suitable choice of the passive components VR1 and C2, C3 C4.

The minimum width of the output pulse is $2\mu S$. This is varied using VR2 (100 Ω to 10k Ω) and C7 (4000pF).

The sum of the delayed time and the pulse width must, of course, be shorter than the periodic time of the master pulse. The rise and fall times of the output pulse are respectively, 25 and 30nS.

The delay times of the present circuit have been calibrated against a standard time marker and found

to be both reproducible and reliable.

Drs. R. Hackham and P. Johnston University of Sheffield.

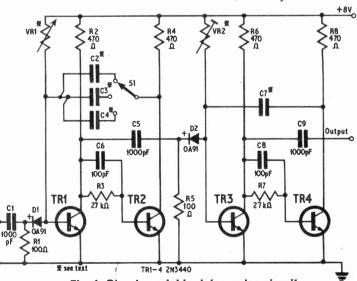
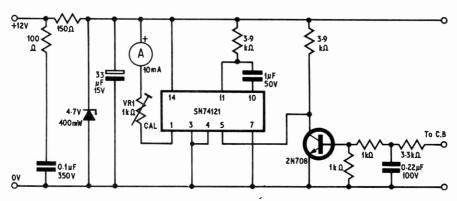


Fig. 1. Simple variable-delay pulse circuit



THE CIRCUIT of a tachometer shown in Fig. 1 is based on the integrated circuit SN74121. This is a monostable device available for under 50 pence.

The circuit can be adapted for a wide range of meters up to 10mA f.s.d. by simply connecting a resistor in series with the meter if required. Initially the design was made for a 12V system but providing the 1500 series dropper is altered there should be no difficulty in adapting for other voltages.

The timing components are the $3.9k\Omega$ resistor and $1\mu F$ capacitor connected to pins 10 and 11, and the capacitor should preferably be a reasonable quality

non-electrolytic tpye.

Meter movement at very low frequencies may be countered by connecting a capacitor across the meter but a good movement should not need this.

Calibration is via VR1 preferably against a pulse

TABLE 1: Calibration Frequency corresponding to 1,000 r.p.m.

No. of Cylinders	2-stroke	4-stroke
	freq	uency
1	16.7Hz	8.4Hz
2	33.4Hz	16.7Hz
3	50Hz	_
4	_	33.4Hz
6	_	50Hz
8	<u> </u>	67Hz

generator of reasonable accuracy. Calibration frequencies are given in Table 1.

C. J. Nother, Portsmouth, Hants.

SCREENWASHER TIMING UNIT

THE device to be described operates the electric screenwashers of a car for a period of up to 10 seconds after a single press of the switch so that one hand does not have to leave the steering wheel for more than a second or so.

Only two main components are used, a relay and a capacitor, and from Fig. 1 it can be seen that when the washer control button is pressed, C1 is immediately charged up to the full 12V battery voltage and discharges over a period of 10 to 15 seconds through the coil of RLA so closing the contacts RLA1 and operating the washer pump motor.

As C1 discharges through the relay, the current eventually falls to below the hold-in value for the relay, contacts RLA1 separate and the pump stops.

VR1 is used to set the operating time of the pump motor. By filing the copper rivet on the armature flat with the face, the hold-in time can be slightly increased and also has the advantage that the relay drops out suddenly so preventing arcing of the contacts which might occur if they separated more slowly.

The relay used is a PO 3000 type with a $1,000\Omega$ coil with all the contacts removed except for one pair of "make" contacts to increase sensitivity, though if a second pair was fitted combined wash and wipe with "one shot" operation could be achieved.

The can of C1 should be completely insulated before mounting, using p.v.c. tape or tube and the

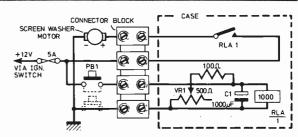


Fig. 1. Arrangement of the screenwasher unit

complete unit should be mounted in a closed steel case in a dry spot away from exhaust pipes. The prototype has functioned perfectly over 1,000 miles with no maintenance being required.

The circuit shown is for 12V negative earth systems. For positive earth the connections to C1 and the washer pump motor merely need to be reversed.

The dotted lines in Fig. 1 show a slight modification which is necessary where the existing switch operates the original washer circuit by shorting one side of the motor to earth, the other side being permanently live, as is often found in the horn circuit.

In both cases, connection to the supply should be *via* a 5A fuse to a "live when on" part of the ignition switch or terminal A4 on the fuse box.

A. Calder, Leigh, Lancs.



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Suitable for Disco, PA, Guitar. 4 inputs, 2 volume controls. Master volume, treble, middle and bass controls. Rugged circuit, rugged leather-cloth covered case, short and open circuit protection. Tone control specification as VA08 pre-amp. FULLY FUSED.



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Constructed on glass fibre P.C. board, individually

P.C. board, individually tested.
Three channel light modulator will control three separate sets of lights, up to 1000 Watts each set. One



to 1000 Watts each set. One channel responds to the bass, one to the middle, and one to the high frequencies.

Input sensitivity only 0:5
Watt! Three Individual controls allow for adjustment of the three channels, and a master sensitivity control allows for input levels up to 100 Watts to be salely accommodated. Full interference suppression. Full wave control, isolating input transformer does not affect Amplifier operation. Fully Fused.

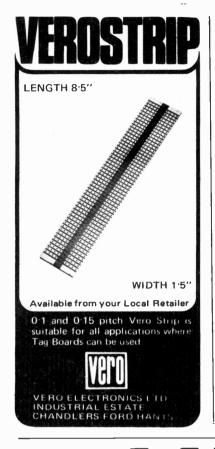
SIMME CHANNEL VERSION SILMS

SINGLE CHANNEL VERSION S2LMB Increased capacity of 1800 Watts. Sensitivity control. Isolating input transformer does not affect amplifier operation.

MANUFACTURERS OF ELECTRONIC AND AMPLIFICATION EQUIPMENT SPECIALISTS IN QUALITY TRANSISTOR EQUIPMENT OPEN 6 DAYS A WEEK. 9.30 a.m. - 6.00 p.m



TRANSISTOR UNIVERSAL AMPLIFICATION COMPANY LTD. 163 MITCHAM ROAD, LONDON SW17-9PG 01-672 3137/9080



6 WATT





High quality amplifiers giving 3W/channel RMS. With low distortion (0-2%). The circuit is designed around the Plessey Integrated Circuit Type SL414A.

Integrated Circuit 1996 SL414A. There is a single and a two-tone control model each designed to accept a crystal pick up. Giving a frequency response from 50 to 154kHz with a load of 8 ohm impedance 3W/channel.

Transformers for above amplifiers

£1-08 **£6∙55** each Single Tone Controls **Dual Tone Controls** £8-25 each

LOUDSPEAKER ENCLOSURE



Incorporating 6 × 4in Fane speaker 10,000 Gauss. Voice coil Gauss. Voice coil impedance 8 ohm. With 6ft of lead. Teak Vinyl covered enclosure with slotted Scandinavian type front. Size 122 × 72 × 34 in, Ideal syin, Ideal extension speakers. Price, £4-60 each.

Plessey I.C.'s Type \$L414A-complete with circuit diagram, £1-38.

Trade enquiries invited. Post and packing 40p for speakers and amplifiers.

ALL PRICES INCLUDE V.A.T.

CIRTEC PRINTED CIRCUITS LTD HIXON INDUSTRIAL ESTATE, HIXON STAFFORD

THE NUMBER FOR CLOCKS, LSI CHIPS,KITS & DISPLAYS.

Choose a combination from the tables below, get out your Access card and ring the above number, or send us a cheque, MO,PO,etc. BYWOOD for ADVICE, SERVICE and of course COMPONENTS.

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Clock	1224	4/6	BCD	7869	MPX	Ŧ	AM/	Alar	Date	Sno	Slee	F.	TIL3	013	170	970	5	TAB	Drive	Priv	Te y	Avail	PRICE
MM5311	Υ	Υ	γ	Υ	Υ	Г	Г	П	П	П		28	D	D	т	Т	-	-	11-19	8		Stock	11.50
MM5314	Υ	٧	П	Y	Y							24	D	D	τ	Ţ	-	-	11-19	8	imple Drive	3 Days	11.00
MM5316	٧	4	l	Y	1	٧	٧	٧		Y.	Υ	40	-	-	-	-	ь	ĸ	8-29	4	is o	Stock	16.00
5017AA	Y	6	1	Υ	Υ	γ	٧	٧		Y		24	т	т	τ	τ:	ĸ	-	1118	16	Na is	Stock	14.00
5017BB	γ	6		γ	γ				٧			24	τ	τ	τ	Ŧ	ĸ	-	11-18	16	Direc Trans	Ltd	14.00
CT 7001	Y	6		γ	γ	Y	γ	Y	٧	٧	Υ	28	т	τ	τ	τ	D	-	11-18	<u> </u>	A T.T.	Feb74	18.00

Display Code	Туре	Pack	Digs		Drive- Req.	Common	Digit £	Unit Cost €
T1L360	LED	16 DIL	6	0.1 ins	2v 10mA	Cathode	2.50	15.00
DL707	LED	14 "	1	0,3 ins	3v 30mA	Anode	2.00	2.00
DL34	LED	14 -	4	0,1 ins	5v 10mA	Cathode	2,50	10.00
DL62	LED	16 "	1	0.6 ins	6 v 30mA	Anode	6.50	6,50
DG12H	Phosphor Diode.	TUBE	1	12.5mm	25v 1mA	Htr Anode	2.00	2.00
TA8055	Liq-Crys.	EDGE	4	0,6 ins	30v125uA (A,C.)	N/A	3.25	13.00

Sockets-24or28pin 115p, 40pin 135p. Case - Warm red Perspex 250p.

Kits 5017AA or BB + PCB + socket + 4 DG12s + Instructions £24.

MM5316 + " + " + TA8055 + " £32.

CLOCK DATA SHEETS -SAE. ADVICE - PHONE 0442-62757 CATALOGUE 15p POST & PACKING - 10p. OVERSEAS (AIRMAIL) 50p. VAT - ALL PRICES EXCLUDE VAT. PAYMENT C.W.O. or ACCOUNT. ACCESS. ORDERS & PAYMENT BY PHONE ACCEPTED. QUANTITY DISCOUNTS ON MOST ITEMS - STATE REQUIREMENTS FOR QUOTATION.



Bywood Electronics 181 Ebberns Road **Hemel Hempstead** HP3 9RDB

PARTRIDGE MAINS ISOLATION TRANSFORMER, Pri: 105-250V, 5V steps, Sec: 240V, 13 amps. \$15, carr. pack. £1.50.

PARMERO MAINS TRANSFORMER isolated windings. Pri: 200-250V. Sec: 90-120V at 4-5 amp.,

GARDHER'S POTTED TRANSFORMER, 0-250V. Pri. 200-250V. Sec. Input: 18V 500m/n, 50V 150m/a, 6V 250m/a output. Size: 3in × 2½ln × 2½ln, £1, p.p. 25p. Ex equip. tested.

RIPLEY MAINS TRANSFORMER, Pri: 110V-240V, Sec: 12-5V: 0:12-5V 750m/A 7V:0:7 V1A, \$1, Sec: 12-p.p. 25p.

MAINS TRANSFORMER, Pri: 100-250V, Sec: 22:0:22 200m/A. 22:0:22 100m/A 0:24V 20m/A, 80p, p.p. 25p

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120 amps. \$15, p.p. £1·50.

MAINS TRANSFORMER, Pri: 100-240V a.c.
36·5·0-36·5·V, 27 m/A, 0·21·5, 260 m/A, 80p, p.p. 25p. TRAMSISTOR OUTPUT TRAMSFORMER, Ratio 8:1, 120mH. Centre tap 2 watts. output, 20p, p.p. 8p.

SMOOTHING CHOKE, 11MH, 12in × 12in × 14in,

\$00, p.p. 8p.

FINNED ALUMINIUM HEATSINK, 4\(\frac{1}{2}\)in \times 6\(\frac{1}{2}\)in \(\frac{2}{2}\) \times 2N3055, \$1, p.p. 13p.

GOODMANS Sin SPEAKERS 3 Q 21.50, p.p. 28p.

FINNED ALUMINIUM HEATSINK. 9in × 8in × 1in. in C.: 4 × 2N3055, \$2, p.p. 29p.

GARRARD MAG. TAPE DECKS: 1\(\frac{1}{4}\)i.p. solenoid operated brakes, etc. Mains motors \$7.50 each, p.p. 60p.

MOTER 3 speed tape deck (1½in × 3½in × 7½in) reel to reel 7in mains operated, \$7-50, p.p. 63p.

10 REED SWITCHES operated by push buttons and magnets, 50p, p.p. 25p.

COMPONENT PANEL, 6 scr's (300V, 1.6A) 6 cond., 12 resistors, 6 diodes, 45p, p.p. 8p. COMPONENT PANEL, 6 s'crs (200V 4 amps), 6 condensers, 12 resistors, 30p, p.p. 8p.

COMPONENT PANEL (9 ICs FJH131) (1-CA300), 1 crystal 7-68kHz + various other components,

\$1, p.p. 8p. COMPONENT PANEL, $2 \times 500 \mathrm{mF}$ 50V, $3 \times 100 \mathrm{mF}$ 25V, cap. 1×200 12, 2×200 44, 3 diodes plus various other components, 10p, p.p. 9p.

COMPONENT PANEL, 24 0A81 diodes, 10p, p.p. 6p. VEEDER ROOT ELECTRICAL IMPULSE COUNTER NON-RESETABLE, A.C. 200-250V, \$1.10, p.p. 13p.

GEC MAINS CIRCUIT BREAKERS, 2 amp or 5

LEVER ACTION P.O. 1000 TYPE SWITCHES
Lock 4-pole changeover, 15p, p.p. 4p. Ex equip.
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MULLARD & MALLORY SCREW TERMINAL
CAPACITORS 4,500µF 64V, 7,100µF 60V, 50p each,
20,000 30V, 28,000 20V, 35,000 15V, 30p each, p.p. 21p.

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6-48V, 15 amp, 75p, p.p. 10p.
BELLING LEE 1-5 amp in-line rubber covered interference suppressor, 25p, p.p. 8p.

RUBBER 8 PIN 5 AMP NON-REVERSIBLE CABLE CONNECTORS, 20p, p.p. 5p.

SOLENOIDS 12 VOLT PULL ACTION 2in × 1in × lin, 40p, p.p. 8p.

SOLENOIDS 12-24V d.c. pull action 1fin × 1fin ×

lin, 40p, p.p. 5p.

SOLENOIDS 240V a.c. pull action 2in × 1in × 1in, 50p, p.p. 9p.

SANGAMO WESTON TIME LAPSED METER

Mains operated. 14in × 14in × 2in, 41.50 p.p. 7p. ARROW RELAY, 240V a.c. coil, double pole change over, 1 make contact's 10A, 240V a.c., 25p, p.p. 9p. OMRON MK2 MIDGET POWER RELAY, 12V d.c.

Double pole changeover. New, 70p, p.p. 5p. STC VARLEY, miniature relays 700Ω, 17.5-37V, perspex cover, 4 pole changeover, 40p, p.p. 5p.

POTTER BRUMFIELD 12V d.c. 3 pole changeover with base, contacts rated 7A d.c., \$1, p.p. 10p.

with mass, contact rates 17, 42, 52, 719. 107. LTT. LOW PROFILE RELAYS. 4 pole c/overs. 500 \(\text{12-18V}, 75\text{p}, \text{p.p. p.p. 5p.} \)

MAINS RELAYS, 200-250V a.c. 2 makes. Heavy duty contacts, 50\text{p.p.p. 7p.}

TELESCOPIC AERIALS
Chromed 7in closed, 28in extended, 6 section ball jointed base, 23p, p.p. 5p new.

PRINTED CIRCUIT BOARD/19 ACY 19's 10 OA200 Dlodes: I reed relay: 1 AZ 229 zenner ass. capacttor/resistors. Power supply 22V, 250 m/A d.c. Output 240V a.c., \$1, p.p. 25p. Ex equip.

WIRING CABLE Size-1-020. Various colours. 350yds, 60p, p.p. 28p. TAPE POSITION INDICATOR Re-settable 3 digits, 80p, p.p. 5p.

All orders add 10% V.A.T.

FIELD ELECTRIC LIMITED 3 Shenley Road Borehamwood, Herts. Tel. 01-953 6009

MAINS NEON FLASHER

This is a circuit which I have developed to remind you to un-plug mains appliances as well as switch them off. The neon glows when the appliance is switched on and flashes when it is switched off until it is unplugged.

With S1 (on/off switch of the appliance) closed (see Fig. 1) the neon lights, R2 dropping the mains voltage to the firing voltage of the neon. With S1 open C1 charges via R1 until it reaches the firing voltage of the neon and then discharges through it, thus making it flash until S1 is closed or the appliance is unplugged.

With such devices fitted to all appliances, a quick look round the room last thing at night will tell you that they are all off and unplugged.

M. J. Maynard,
Wednesbury, Staffs.

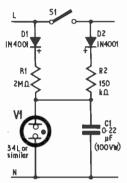


Fig. 1. Circuit diagram for the mains neon flasher

VEWPOINT

Sir—Am I alone in thinking that quadraphony (and indeed stereo) is a "con"—or at least an attempt by the industry to create a demand?

I remember several years ago an article in this or a similar magazine, reporting a Continental idea whereby the orchestra performed in the wide end of a large exponential horn—the audience obtaining the effect of hearing a live orchestra through a metre-square hole!

Now this seems infinitely more sensible to me than quadraphony.

Surely the fact that an orchestra, or a pop-group, is ten metres wide is irrevelant. If width is necessary per se, why not spread the musicians out more? In fact musicians have always stood as close together as possible. Why?

A group of musicians constitutes a certain size purely because human beings are the size they are, and similarly with instruments.

"Stereo" and "quad" are NOT analogous to stereo pictures. Surely it follows that the industry should be putting the effort into improved colour, stereo pictures instead of the absurdities of "quad"! The present colour T.V. picture is on a par with a washed-out, amateur transparency viewed through a 50p lantern.

E. Wadsworth, Huddersfield, Yorks

9V BATTERY ELIMINATOR

continued from page 1092

in Fig. 5, although the dimension between the connector plate and the mains transformer board may need to be varied slightly to ensure a snug fit inside the battery casing.

Before fitting the connector plate pass the output leads of the regulator board through the slot in the mains transformer board and solder them to the contacts. The plain contact is positive and the castellated contact is negative (on some modern batteries the castellated contact has been replaced by a split contact)

Pass the mains lead through the hole in the connector plate and fit the plate onto the rods. Using p.v.c. lacing cord or thin p.v.c. sleeving, tie the mains lead tightly to one of the screwed rods to prevent the soldered joints being stressed.

The length of the screwed rod is 3in where the battery has a plastic bottom plate, but a slightly longer rod will be needed if a different bottom plate is fitted. The rod is normally supplied in 3ft lengths and can be sawn very easily with a "junior" hacksaw.

and can be sawn very easily with a "junior" hacksaw.

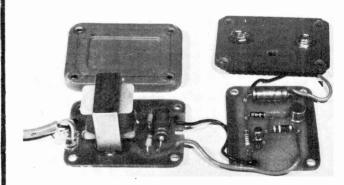
One "trick of the trade" when sawing threaded rod is to thread a nut onto the length to be sawn. After cutting and deburring with a file the nut can be removed and this will automatically re-form the thread on the cut end. This simple procedure saves a good deal of time and temper.

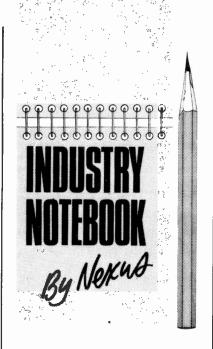
FINISHING OFF

When the power supply assembly fits the battery case satisfactorily the ends of the brass rod may be filed down level with the tops of the nuts. Finally fit the unit into the case ensuring that "+" marking on the case is closest to the plain contact and carefully re-fold the casing over the bottom plate.

The battery eliminator can then be fitted into the portable radio in place of the normal battery although a slot will need to be made in the radio casing to allow for the mains lead. On the few occasions that the radio is required as a true portable the mains unit can be removed and a battery inserted in exactly the same time as it would take to replace a flat battery.

Photograph showing the two component boards and the end plates of the battery before mounting on brass studding





LIGHT FINGERS

Shop-lifting by well-heeled women in London's West End has been making the headlines. Not so well publicised is the wave of petty and not-so-petty pilfering in the electronic components industry since the upsurge in world demand created a component famine.

As usual, the incidence of crime appears greatest in the United States. Few of the semiconductor manufacturers are immune and hardest hit, according to reports, is Signetics with over £40,000 of goods mysteriously disappearing. Fairchild has also been hit.

It's not only straight pilfering that's worrying the industry. Huge quantities of below - standard products have been hived off onto the market at give-away prices in recent years and many of these are now re-appearing freshly remarked and not necessarily with the original manufacturer's name. These are being bought in good faith and equipment manufacturers have found performance not up to scratch. Motorola has been one company receiving back for replacement falsely marked semiconductors. Over in the States, the police have been sleuthing away and some arrests have been made.

The racketeers have not confined activities to the USA. The very nature of semiconductor devices with their small size, light weight and high intrinsic value makes them a natural for shipping round the world and Bill Richardson, Chairman of Britain's Association of Franchised Distributors of Electronic Components (AFDEC) has warned the industry against dishonest brokers.

Members of AFDEC are bound by constitution to guarantee all products they sell and this is the best protection. Richardson quotes a case where a UK manufacturer disposed of a bulk quantity of substandard products 12 years ago which have recently re-appeared on the UK market through sources which can be traced back through Tel Aviv and Geneva. Buyers beware!

DEFENCE BOOM

The Royal Navy Equipment Exhibition at Greenwich showed defence equipment manufacturers in good shape, technically and economically. Defence exports have been booming and climbing in value every year. In 1968-69 exports were £150 million, in 1972-73 they had climbed to £345 million and this year will top £400 million, about 40 per cent of all defence equipment manufactured in the UK.

The sales success of recent years owes much to the pioneer work of Sir Raymond Brown who resigned his Chairmanship and business interests in Racal Electronics to become the first Head of Defence Sales in 1966. Present Head of Defence Sales is Sir Lester Suffield

The sales organisation does market research, organises exhibitions, assists industry with advice and generally smooths the path between initial enquiry and final sale. Even Royal Fleet Auxiliary vessels are pressed into use as floating exhibition centres. For the past three months RFA Tarbatness has been touring the Middle East and Far East on just such a mission.

FIFTY YEARS ON

This has been a great year for Golden Jubilees marking the 50th anniversary of broadcasting and of many of the pioneering companies that sprang into existence to serve the needs of what was to become an industry in its own right. Of all the celebrations one of the cosiest, if not the biggest, was the informal party given by Eddystone Radio.

Although the company is now part of the giant GEC-Marconi complex, Eddystone's managing director Dick Carroll has managed to preserve the family atmosphere—perhaps not too difficult with so many of the staff having been around for more years than they care to remember.

Enough of the past. How is Eddystone shaping up to the future? Today's sets are all solid-state, modular, up-to-the-minute and selling well. Eddystone profits are buried deep in the corporate

accounts of the parent group but I can reveal that they are healthy in every way. Watch out for new models and an expanded component line in 1974.

COMPUTERISED METROLOGY

Herbert Controls and Instruments Ltd. was formed in 1969 from three companies in the Alfred Herbert Group and started life with a 50-year background in measurement techniques stretching back to Sigma gas gauges, modern versions of which are still sold to the gas industry. But more recently HCIL moved into the field of mechanical inspection equipment and rapidly established a world reputation for solving difficult problems.

One of HCIL's most remarkable machines is the Sigmatrace designed specifically for inspection of the aerofoil profile of gas and steam turbine compressor blades. This was traditionally a skilled job which took a lot of time and involved lengthy written records which were passed to a blade polisher to iron out humps and hollows and get each blade right. The inspector would compare the workpiece under inspection with a perfect master.

Sigmatrace does the whole job in a minute, complete with a printed record of deviation. Moreover, no master blade is required because all the master profile information is fed into a computer store direct from the drawings. HCIL is 'doing a roaring trade world wide with this sort of electronic-based metrology and supplies most major automotive and aerospace manufacturers.

The chief engineer of HCIL, Dr. Colin Gaskell, sees computer-controlled gauging becoming really significant in engineering shops where more than 30 measurements are needed on a workpiece. When you get up to 80 measurements a computer is practically a necessity.

DUCKS AND GROUSE

Mallard is dead—long live Ptarmigan. They are the code names for the army's trunk communications systems. Mallard died afterendless discussion. Now Plessey has been appointed prime contractor for the new system, Ptarmigan, with Marconi and STC as subcontractors. Initial contracts are worth £17 million but the project could lead to £100 million of business over the years.

I marvel at the wit of those who invent code-names. Mallard always seemed a dead duck. And if Ptarmigan doesn't come up to scratch, we'll have something to grouse about.

Come home to this fine 8 track stereo system

Elegantly styled in teak finished cabinets with satin aluminium trims and controls.

Automatic and manual channel selection with at-a-glance

illuminated track indicator.

Separate bass treble and volume controls for exact tone balance.

Full 5 + 5 watt rating from latest integrated circuit amplifiers.

Solidly built bookshelf speaker units house high performance

elliptical loudspeakers.

The complete package including mains and speaker leads is ready to play in minutes.

Quentronic



Manufactured and distributed by Quentronic Ltd., 4-6 Mill Lane, Brighouse, Yorks. Telephone: 048 47 4837

RECORD PLAYBACK HEADS

(TRUVOX)
Individual prices of these are:—
2 track record playback heads 50p each.
4 track record playback heads 72p each.
Erace heads are also available separately—2 track

389—4 track 559.

MV metal mounting shields 899 each.

2 track-heads already fixed on heavy mounting plate with shield \$1.22.



CONTROLLER NEW IKW MODEL

PRILL
SPEEDS

| Speed | From approximately | 10 revs. to maximum. Full power at all speeds by finger-tip control. Kit includes all parts, case, everything and full instructions. 21.95. 13p post and p. Made up model also available. \$2.95.

MIGHTY MIDGET

Probably the finest possible radio, as described in *Practical Wireless*, January 73. All electronic parts \$2.20 post paid.



TIME SWITCH

TIME SWITCH
Smith's mains driven clock with
15 amp switch, also notes
showing how you can wake up
with music playing, kettle
boiling or come home to a warm
house, warn off burglare, keep
pets warm, halve your heating
bills, etc. £1.95.

I CHIP RADIO

Ferranti's latest device ZN414 gives results better than superhet. Supplied complete with technical notes and circuits. \$1.38 each. 10 for

HI-Q TUNER COMPONENTS

HI-Q TUNER COMPONENTS
For experimenting with the ZN414.
KIT NO. 1. Plessey Minlature Tuning Condenser
with built-in LW switch and 3in Ferrite slab and
litz wound MW coil, 72p.
KIT NO. 2. Air spaced tuning condenser fin
ferrite rod litz wound MW and LW coile, 94p.
KIT NO. 3. Air spaced TC with slow motion
drive 8in ferrite rod, with litz wound LW and MW
coils, 81.10.

coils, \$1.10.

KIT No. 4. Permeability tuner with fast and slow motion drive and LW loading coils, 50p.

AUTO-ELECTRIC CAR AERIAL

with dashboard control switch-fully with dashboard control switch—fully extendable to 40in or fully retractable. Suitable for 12V positive or negative earth. Supplied complete when fitting instructions and ready wired dashboard switch. £6:35 plus 25p post and insurance



AERIAL for portable, car radio or

transmitter. Chrome plated sections, extends from 'Hole in bottom for 6BA віх KNUCKLED MODEL FOR F.M. 55p.



EXTRACTOR FAN

EXTRACTOR FAN
Cleans the air at the rate of
10,000 cubic ft. per hour.
Suitable for kitchens, bathrooms, factories, changing
rooms, etc. it's so quiet it can
hardly be heard. Compact. 5i in
casing with 5i in fan blades.
Kit comprises motor, fan
blades, sheet steel casing, pull
switch, mains connector, and
fxing brackets. \$28.75 + 20p
P. & P.

MAINS OPERATED SOLENOIDS



MAINS TRANSISTOR POWER PACK

PACK
Designed to operate transistor sets and ampliflers. Adjustable output 6v., 9v., 12 volts for up
to 500m A (class B working). Takes the place of
any of the following batteries: PP1, PP3, PP4,
PP6, PP7, PP9, and others. Kit comprises: mains
transformer rectifier, smoothing and load resistor
condensers and instructions. Real snip at only
\$1.10. Plus 20p postage.

DESK, TELEPHONES

DESK, TELEPHONES

EX G.P.O. Black standard model with dialing dial but no internal bell. Supplied with connection diagram \$1 each. Ditto, with bell but without dialing dial \$1.85. Model as illustrated with bell and dial \$1.50 each plus 50p post for single then 65p ber pair.



SMOKE WILL KILL—GAS WILL KILL—FIRE WILL KILL

But, if you install SAGA (our smoke and gas alarm) your family will have the latest electronic protection, against these killers. Saga uses a fantastic electronic sensor which "smells" killers. Saga uses a fantastic electronic seneror which "smells" smoke and gas and sounds the alarm immediately, in a neat case measuring approx. 5in × 3 lin × 2 lin, it has its own internal slarm, also a connector for additional bells. You just plug it in to the mains and hang it near the ceiling. Saga uses so little electricity that it will hardly move the meter, leave it on always to give night and day protection. One year's guarantee, also "chay cash return offer, (or kit of parts 25-99. Battery model kit only 24-99), 26-99 plus 30p post and service.

CENTRIFUGAL FAN

Mains operated, turbo blower type. Pressed steel housing contains motor and impeller. Motor is 1/10th h.p. giving considerable air flows but virtually no noise. Approx. dimensional distribution of the contained sions 10 in wide x 12 in dia. outlet into trunking 10 x 4 in. \$6.55 plus £1 post and insurance.

STANDARD WAFER SWITCHES

Standard size 1 in wafer—silver-plated 5 amp contact, standard fin spindle 2in long—with locking washer and nut.

No. of Poles 2way 3way 4way 5way 6way 8way 9way10way12way

1	pole	44p	44p	44p	44p	44p	44p	44p	44p	44p	
-2	poles	44p	44p	44p	44p	44p	44p	44p	77p	77p	
3	poles	44p	44p	44p	44p	77p	77p	77p	\$1.04	£1-04	
4	poles	44p	44 p	44p	77p	77p	770	77p	£1.82	\$1.32	
5	poles	44p	44p	77p	77p	\$1.04	£1-04	\$1.04	\$1.60	\$1.60	
6	poles	44p	77p	77p					£1.87		
7	poles	77p	77p	77p					#2-15		
8	poles	77p	77p	77p	\$1.04	£1.82	£1.82	£1.82	£2-42	£2.42	
9	poles	77p	77p						42.70		
10	poles	77p	77p	£1.04	£1.82	£1.60	£1.60	\$1.60	#8.00	£8.00	
11	poles	77p	\$1.04	£1.04	£1.82	£1.87	£1-87	£1.87	£8-25	£8-25	
12	poles	77p	£1.04	£1.04	£1.32	£1.87	£1.87	£1.87	\$8.52	£8.52	

THE TWENTYLITE

Fluorescent lighting units with polyester choke and finished white enamel. 2ft. model, ideal kitchen, bedroom, hallway, porch, lift, etc., with tube. Assembled ready to install. Price \$2.20 + 40p P. & P.



RADIO STETHOSCOPE
Easiest way to fault find—traces signal from aerial to speaker—when signal stops you've found the fault. Use it on Radio TV, amplifier, anything—complete kite comprises two special transistors and all parts including probe tube and crystal earpiece. 82:20—twin stethoset instead of earpiece 83p extra—post and ins. 20p.

TANGENTIAL HEATER UNIT



TER UNIT
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Transistors & Constructors

By D. Bollen

The start of a great revolution in home construction is recalled by a well-known contributor in this article, which brings to a conclusion our special series commemorating the invention of the transistor

N THE TYPICAL home electronics workshop of twenty-five years ago the enthusiast would be surrounded by machines for bending, punching, drilling, and rending asunder sheet metal. Constructional techniques were based upon the chassis, a box-like structure full of holes into which were inserted spindles, screws, valveholders, grommets, and trapped fingers.

Sometimes, when the burden of bashing metal became tiresome, a piece of easily punctured Bakelite might be pressed into service as a breadboard, but this was considered very unprofessional, a throwback to the days of coil winding, capacitor building, and

generally doing it yourself.

Components came from two main sources; sturdy ex-government equipment which was cannibalised, sometimes with the aid of a hammer and cold chisel, and the "junk box" where reposed an amorphous heap of very second-hand items, ranging from a leaking electrolytic capacitor dated 1941 to a speaker grille woven to depict a scene of nymphs and satyrs dancing in a woodland setting. These were the lean years just after the war, with no oriental imports, kits of parts or regular sources of "bits".

Into this man's world of hot cathodes and 100 watt soldering irons was born the sub-midget transistor, and the wonder is that it managed to survive at all, let alone replace valves, which everyone said

it would never do.



A TOUGH TIME

Transistor manufacturers were having a tough time trying to fabricate the new device, probably because they were ham-fisted too. In any event, if you were fortunate enough to get hold of a sample in the early fifties it was likely to be one that everybody else had rejected, with a leakage current of two or three milliamps, a current gain of five, and dying from slow contamination.

Compared with a valve this was a pathetic thing

indeed!

Assume that you were the proud possessor of a device no bigger than a resistor with three wires sticking out of it. Where did you go from there? Published information was scanty and far from standardised. Maximum ratings were mere hearsay. At the devaluation equivalent of £2 to £4 each, the safest policy was to power the device at the lowest voltage and current at which it was capable of supplying useful work.

As far as circuits went, which was not very far, there was a limited choice between the upside down, thread-in-a-maze American sort, or the UK variety which favoured the powering of each transistor in a multi-stage circuit by its own personal 1.5V cell.

Apart from earth symbols and batteries floating all over the page, there was also a general tendency for transistor symbols to be shown doing a basedown nose dive into the earth rail, this being the only way they could be made to function above 10kHz.

GREAT DIFFICULTIES

So, in the face of great difficulties you managed first of all to identify the leads on your transistor with an ohmmeter and then to find, or rashly devise a transistor circuit.

Were you supposed to solder the thing to a tagstrip, and mount the resulting assembly on the customary two acres of sheet aluminium? After all, we were here dealing with impedances of a very low order, for which electrolytic capacitors the size of milk bottles would have to be accommodated for coupling and decoupling purposes.

DELICATELY SOLDERED

The delicately soldered transistor clings to its tagstrip. The scope (ex-government of course) displays a straight line on its axis. Several meters are linked to those parts of the circuit where a voltage or current might conceivably occur.

After inserting the power supply plug into the lowest voltage tap of a grid-bias battery . . . yes, we

have oscillation!



True, it is but a crude imitation of what would normally pass as a sine wave from a valve circuit, but it is early days yet. A few more volts perhaps? Why is that meter reading creeping higher and higher? Should the transistor run hot? It has stopped oscillating.

"Grrr! They will never replace valves."

AVAILABLE TO AMERICAN

The transistor was available to American enthusiasts for about \$18 in 1953. Over here, the ubiquitous OC71 and "red spot" transistors (the latter a polite name for manufacturer's reject) came on the scene in 1956 priced at 24/- and 10/- respectively. Full praise must be given to those suppliers who struggled to bring us the amplifying crystal less than eight years after its invention.

The silicon transistor also took only eight years to reach the home after being first manufactured in

1952.

More than one enterprising magazine contributor of the period went one better and gave full instructions for making a point-contact transistor from an old crystal diode, but the problem here was that an excess of audio signal or marital strife in the home could dislodge the triple catswhisker and thus degraded performance.

Another bright spark discovered that when the paint was scraped off the glass encapsulated OC71 it responded to light in the manner of a phototransistor. The manufacturers quickly countered this cunning move by filling their transistors with opaque blue putty, labelling the clear putty variety OCP71

and charging more for it.

NEST OF SNAKES

An innovation of the middle fifties was the transistor radio, which incorporated the new "nest of snakes" unrepairable printed circuit and the fragile ferrite rod aerial. Also at this point in time, the word "transistor" was press-ganged into common English usage to signify a radio receiver which could be employed to annoy people on beaches, and also render the user deaf in one ear by means of a simple unhygienic earphone.

The printed circuit defied all former rules of

construction.

Components were held in position by solder alone, a practice which previously would have been considered very naughty. With the passing of the chassis, there was no longer anywhere to mount controls, and this caused quite a few headaches in constructional circles.

Eventually, it was tacitly agreed that serious projects would have their controls mounted on smart metal front panels, while silly projects could use sheet plastic or even wood. Alas, these attempts at

standardisation failed miserably.

One breakaway group defiantly insisted on using metal tobacco tins for all projects, while another sect mounted their controls on the printed circuit itself! The latest trend seems to be to bung everything inside a transparent plastic cube or sphere and hope for the best, so confusion still persists.

ADVANCED STAGE

Valve audio amplifiers had reached an advanced stage of development prior to the introduction of the "jump-a-groove" long-playing record in 1950, but with the coming of the difficult-to-tune f.m. radio in 1955, hi-fi purists were at last able to take time off to just sit and listen to the music, without having to bother about all that nasty distortion of former years.

Unfortunately, this idyllic state lasted only until 1961, when the easy-to-blow power transistor started to appear in output stages, accompanied by some-

thing called "the transistor sound".

This unusual effect was characterised by a rattling buzz from loudspeakers when gain controls were turned low. After a good deal of concentrated sleuthing, it transpired that transistor audio amplifiers were subject to crossover distortion, so the purists had to climb out of their armchairs and set about exorcising the demon with cabbalistic circuitry.

Since then there has been no further opportunity to listen to music. Elimination of the output transformer led to severe difficulties in trying to match the then extant 15 ohm loudspeakers to amplifiers requiring a four to eight ohm load, and all problems were multiplied by two when stereo came along.

Now they are about to be multiplied by four.

SURVIVE THE TRANSITION

What has the future in store for those who have managed to survive the transition from valve to transistor? Clearly, the introduction of a new device is often accompanied by unpleasant side-effects. For example, with i.e.s. we have already experienced circuits which are best understood if held upside down in front of a mirror, and the use of postal codes for device numbering is to be deprecated.

Above all, one thing is patently clear. A new device seems to take eight years to mature to amateur status. Furthermore, all information concerning a new device is automatically witheld for five years, or until it becomes obsolete, whichever period is shorter. So it follows that there is no need to get too agitated when a new device comes along, because the threat to one's peace of mind is not immediate.

NOTE: This last point is not quite true since it is the avowed object of PRACTICAL ELECTRONICS to ensure that the reader is informed of interesting developments as soon as possible. Indeed, the problem nowadays would be to avoid doing so—ED.

PATENTS BEVIEW...

FUEL MONITOR

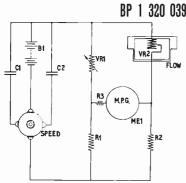


Fig. 1

With petrol likely to be very scarce or more expensive or both in future, devices for accurately measuring vehicle fuel consumption will become more popular.

In BP 1 320 039 Alan Westwood, Peter Davidson and Brian Dean describe and claim just such a device. The circuit Fig. 1 shows a vehicle speed measuring device, a flow meter to measure fuel rate of flow (and thus proportional rate of consumption) and an ammeter for reading m.p.g.

The meter is connected between opposite junctions of a Wheatstone bridge comprising VR2 (which forms part of the flow meter), R2, R1 and VR1 for pre-settling bridge balance. The use of R3 in series with the meter is only necessary with certain meters.

The opposite corners of the bridge are connected together by the vehicle speed measuring device. This includes a rotor geared to the vehicle transmission with brushes which alternately connect capacitors C1, C2 across the vehicle battery and discharge them through the bridge. The capacitors C1, C2 thus charge and discharge alternately to give a signal representative of the vehicle speed.

The flow meter will generally be in the form of a chamber with inlet and fuel outlet pipes and a bellowstype diaphragm. Fuel passing to the engine flows through the chamber to compress the diaphragm in dependence upon fuel flow rate. As the diaphragm is compressed, the value of VR2 resistance is varied by movement of the slider over its track. The value of VR2 resistance is in practice an inverse function of the fuel flow rate.

The reading given on the meter is approximately proportional to an arithmetical relationship between the two signals controlled respectively by the flowmeter and the speed measuring device, being approximately proportional to the current received from the rotor of the speed measuring device multiplied by the imbalance of the bridge circuit due to the flow meter. This reading represents an indication of distance travelled by the vehicle per unit of fuel consumed and the meter ME1 can be calibrated to provide direct readout in miles per gallon.

NEW APPROACH TO TONE CONTROL

In BP 1 304 774 Wilfred Palmer of Dagenham, Essex, describes a three part tone control circuit for an audio amplifier. By way of example he gives a list of specific values for all the components, see Fig. 1.

The variable potentiometer VR1 and d.c. blocking capacitor C1 form a normal volume control. The slider of VR1 acts as a common input line to the three sections of the tone control, shown dotted.

The bass circuit includes R1 and R2 in series with VR2. The slider of VR2 is in series with R3 which feeds the output terminal.

The mid-range circuit has R4 and R5 in series with VR3, and the slider is also connected to the output via R6 and C2.

The high frequency circuit comprises VR4, the slider being connected to the output via C3.

The resistor R7 between C2 and C3 is intended to isolate the infinite variations of time constant of the treble circuit from the infinite variations of time constant of the mid-range circuit. Also, the resistor acts as an impedance to high frequencies from the bass and mid-range circuits. The inventor suggests that in this way the signals from the middle and treble circuits are cleanly and fully mixed.

The bass circuit presents a high impedance to high frequencies, thereby attenuating them but passing low and mid-range frequencies. This is due to the presence of resistors R1 and R2. The inventor points out that any resistor can be represented by a pure resistance in parallel with the self capacitance across the resistor terminals and there is thus attenuation of high frequency signals by the changes of self capacitance with increasing frequency. By using the resistors in series, total self capacitance is lowered.

The treble circuit presents an increasing impedance as the frequency decreases, thus attenuating low frequencies but passing the high and part of the mid-range frequencies.

The inventor claims that the circuit eliminates the need for attenuators in crossover units and allows infinite variations of the signal fed to loudspeakers over the whole audio spectrum.

BP 1 304 774

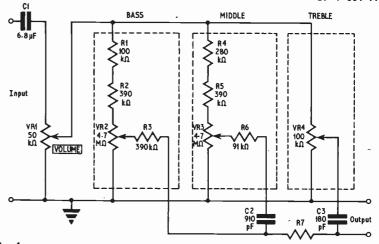


Fig. 1

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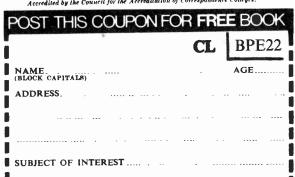
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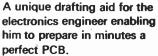
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	8N7422AN	38	38	83	8N7493N	75	70	63	SN74176N	1.44	1.44	1-26
	8N7423N	87	34	32	8N7494N	85	80	75	8N74177N	1.44	1.44	1.26
	8N7425N	87	37	32	8N7495N	85	80	75	8N74180N	1-44	1.44	1.26
	SN7427N	87	87	32	SN7496N	1.00	90	83	SN74181N	5-18	5-18	4.53
	8N7428N	48	48	37	8N74100N	2.16	1.89	1.89	SN74182N	1.44	1.44	1.26
	8N7430N	20	18	16	SN74104N	60	58	45	SN74184N	2.16	2.16	1.89
	8N7432N	87	87	82	8N74105N	60	53	45	8N74185AN	2.16	2.16	1.89
	BN7433N	43	48	38	8N74107N	51	51	45	8N74188N	6.48	6-48	5-67
	8N7433AN	57	57	50	8N74110N	57	57	50	SN74190N	2.30	2.30	2.01
	8N7437N	48	43	37	SN74111N	86	86	75	SN74191N	2.80	2.30	2.01
ì	8N7438N	48	48	37	8N74116N	2.16	2.16	1.89	SN74192N	2.30	230	2.01
ı	8N7438AN	57	57	50	8N74118N	1.00	90	83	SN74193N	2-30	2.30	2.01
ı	8N7440N	20	18	16	SN74119N	1.92	1.92	1.68	SN74194N	1.72	1.72	1.51
ı	8N7441AN	85	79	73	8N74120N	1.05	1.05	92	SN74195N	1.44	1.44	1.26
ı	8N7441AN	85	79	73	SN74121N	57	57	50	SN74196N	1.58	1.58	1.38
ı	8N7442N	1.50	1.27	1.13	SN74121N	80	80	70	8N74197N	1.58	1.58	
ı		1.50	1.27	1.13	8N74123N	1.44	1.44	1.26	SN74198N	3.16	3.16	
ŀ	8N7444N		0.18	1.60		1.47	69	60		2.88	2.88	2.52

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CRS 1/10AF 100V 30p CRS 1/20AF 200V 35p CRS 1/40AF 400V 45p CRS 1/60AF 600V 35p CRS 3/05AF 50V 40p CRS 3/10AF 100V 40p		50V	
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CR5 3/05AF 50V 40p CR5 3/10AF 100V 40p			33p
CR5 3/10AF 100V 40p		48)	
CR5 3/20AF 200V 45p			
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CR5 3/60AF 600V 65p	CR5 3/60AF	600V	
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CR5 5/400V 60p		5/400V	60p
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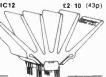
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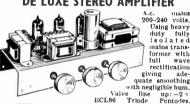


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Beautifully made teak finish enclosure with most attractive Tygan-Vynair front. Size 16in high X-10jin widex 6in deep. Fitted with E.M.I. Ceramic Magnet 13in x8in bass unit, two H.F. tweeter units and crossover. Max, power handling 10W. Available 3, 8 or 15 ohm impedance.

Our Price £9.25 Carr. 75p CABINET AVAIL. SEPARATELY 24-95. Carr. 65p. Also available in 8 ohns with EMI 13in×8in, bass speaker with parasitic tweeter. 27-15. Carr. 75p.

HARVERSON'S SUPER MONO AMPLIFIER

AAVENSUN'S SUPER MUNU AMPLIFIER
A super quality gram amplifier using a double wound fully
isolated mains transformer, rectifier and ECL82 triode
pentode valve as audio amplifier and power output stage.
Impedance 3 ohms. Output approx. 3-5 watts. Volume
and tone controls. Chassis size only 71n. wider 2 in. deep /
6in. bigh overall. AC mains 200/240V. Supplied absolutely
Brand New, completely wired and tested with good
quality output transformer.

OUR ROCK BOTTOM BARGAIN PRICE

£3.30 P. & P.

LOUDSPEAKER BARGAINS

5in 3 ohm \$1-05, P. & P. 15in, T. × 4in 3 ohm \$1-15, P. & P. 20p. 10 × 6in 3 or 15 ohm \$1-90, P. & P. 30p. E.M.I. 8×5in 3 ohm with high flux magnet \$1-62, P. & P. 20p. E.M.I. 31 × 8in with high flux ceramic magnet with parasitic tweeter 3, 8, or 15 ohm \$1-30, P. & P. 30p. E.M.I. 134 × 8in, 3 or 8 or 15 ohm with two inbuilt tweeters and crossover network \$24-65, P. & P. 30p.

EMI CERAMIC MAGNET HEAVY DUTY TWEETER.

PDFOS. 34in. Av. 3 or 8 or 15 ohns. £1.25 plus 20p p. & p.

BRAND NEW. 12in 15w H/D Speakers, 3 or 15 ohns.

Current production by well-known British maker. Now

with Hiffux ceramic ferrobar magnet assembly £7.50.

Guitar models: 25w £7.50. 35w £9.35. P. & P. & P. & P. dep each.



SPECIAL OFFER!

LIMITED NUMBER OF BRAND NEW ELAC 10" TWIN CONE LOUDSPEAKERS. With large ceramic magnet and plasticised cone surround. S ohm impedance. £2.70. P. & P. 35p.

Also available specification as above but size 10" \$2.70 and size 8" round \$2.60 P. & P. 35p.

LIMITED NUMBER EM1 2½ 8 ohm Tweeters. Mounted on flat bracket, size 2½ wide × 7½ long. 70p per pair plus 15p P. & P. Ex equipment but new and tested. 70p per pair plus 15p P. & P.

12in "RA" TWIN CONE LOUDSPEAKER
10 watts peak handling, 3, 8 or 15 olum, \$2.45, P. & P. 36p.
35 ohm SPEAKERS 3". ONLY 70p. P. & P. 25p.

"POLY PLANAR" WAFER-TYPE, WIDE RANGE ELECTRO-DYNAMIC SPEAKER

BLEGUTRU-DYNAMIC SPEAKER
Size 112 in × 14 in × 1,4 in 1 dep. Weight 19oz.
Power handling 20W r.m.s. (40W peak). Impedance
s ohm only. Reaponse 40Hz-20kHz. Can be mounted
on ceilings, walls, doors, under tables, etc., and used with
or without baffle. Send 8.A.E. for full details. Only
\$6.55 each. P. & P. 34p.

HI-FI STEREO HEADPHONES

Adjustable headband with comfortable flexifoam ear-muffs. Wired and fitted with standard stereo in jack plug. Frequency response 30-15,000Hz. Matching nuffs. Wired and fitted with standard successful plug. Frequency response 30-10,000Hz. Matching impedance 8-16 ohms. Easily converted for mono. PRICE

HAVERSONIC SUPER SOUND 10 + 10 STEREO AMPLIFIER KIT



MEW FURTHER IMPROVED MODEL WITH HIGHER OUTPUT AND INCORPORATING HIGH QUALITY READY DRILLED PRINTED CIRCUIT BOARD WITH COMPONENT IDENTIFICATION CLEARLY MARKED FOR EASIER CONSTRUCTION

MARKED FOR EASIER CONSTRUCTION

A really first-class Hi-Fl Stereo Amplifier Kit. Uses that transistors including Silicon Transistors in the first five stages on each channel resulting in even lower noise level with improved sensitivity. Integrated pre-amp with Bass, Treble and two Volume Controls. Suitable for use with Ceramic or Crystal cartridges. (Very simple to modify to suit magnetic cartridge—instructions included.) Output stage for any speakers from 5 to 15 ohms. Compact design, all parts supplied including drilled printed circuit board, smart brushed anodised aluminium front panel with matching knobs, wire, solder, nuts, bolts—no extras to buy. Simple step by sten data work, but to be proud of. Brief specification: Power output 14W 12-00,000Hz. Benaitivity better than 86mV into 18 12-00,000Hz. Benaitivity better than 86mV into 18 12-00,000Hz. Sensitivity better than 86mV into 18 12-00,000Hz. Sensitivity better than 90mV into 180. Negative feedback 180 ever main amp. Power requirements 35V at 10 amp. Overall size—12 wide×8 feedback 181 to 1912 the sensitivity in the sensitivity in the sensitivity better than 90mV into 180. Negative feedback 180 ever main amp. Power requirements 35V at 10 amp. Overall size—12 wide×8 feedback 181 the 1912 the sensitivity in the

meints 35V at 1-0 amp. Overall size—12 wide x b neep x 21 high.
Fully detailed 7-page construction manual and parts list free with kit or send 18p plus large 8.A.E.
PRICES AMPLIFIER KIT, 41.55 P. & P. 25p.
Amplifier Components 33p extra.
POWER PACK KIT, 43.30 P. & P. 35p.
CABINET, 25.30 P. & P. 35p.
(Post Free if all units purchased at same time). Full after asles service. Also available ready built and tested, 233-10. Post Free.

223:10. Post Free. Note: The above amplifier is suitable for feeding two mono sources into inputs (e.g. mike, radio, twin record decks, etc.) and will then provide mixing and fading facilities for medium powered Hi-Fi Discotheque was, etc.



3-VALVE AUDIO

AMP. HA34 MK II
Designed for Hi-Fi reproduction of records. A.C. Mains
operation. Ready built on

operation. Ready built on plated heavy gauge metal chassis, size 7 Ji n w. < 4 in. d. x. 4 Ji n. h. Incorporates ECC83, FL84, EZ80 valves. Heavy duty, double wound main speaker. Separate volume control and now with improved wide range tone controls giving bass and treble lift and cut. Negative feedback line. Output 44 wats. Front panel can be detached and leads extended for remote mounting of controls. Complete with knobs, valves, etc., wired and tested for only \$5.50. P. & P. 45p.

HSL "FOUR" AMPLIFIER KIT. Similar in appearance to HA34 above but employs entirely different and advanced circuitry. Complete set of parts, etc. \$4.50, P. & P. 45p.

10/14 WATT HI-FI AMPLIFIER KIT

A stylishly finished monaural amplifier with an output of 14 watte from 2 EL84s in push-pull. Super reproduction of both music and speech, with negligible hun. Separate inputs for mike and gram allow records gram allow records and announcements to follow each other



to follow each other
Fully shrouded section wound output transformer to
match 3-15Ω speaker and 2 independent volume controls,
and separate bass and treble controls are provided giving
cood lift and cut. Valve line-up 2 EL84s, EVC83, EF86 and
EZ80 rectifier. Simple instruction booklet 15p julus 8.a. E.
(Free with parts). All parts sold separately. ONLY \$8.80.
P. & P. 80p. Also available ready built and tested \$12.10.
P. & P. 70p.

VYNAIR & REXINE SPEAKERS & CABINET FABRICS app. 54 in. wide. Our price 85p yd, length. P. & P. 25p per yd. (mln. 1 yd.). S.A.E. for samples.

HARVERSON SURPLUS CO. LTD.

Dept. PE, 170 High St., Merton, London, S.W. 19 Tel. 01-540 3985 SEND STAMPED ADDRESSED ENVELOPE WITH ALL ENQUIRIES

(Please write clearly)

PLEASE NOTE: P. & P. CHARGES QUOTED APPLY TO U.K. ONLY. P. & P. ON OVERSEAS ORDERS CHARGED EXTRA.

YATES ELECTRONICS

(FLITWICK) LTD. PE, ELSTOW STORAGE DEPOT KEMPSTON HARDWICK BEDFORD

C.W.O. PLEASE. POST AND PACKING PLEASE ADD 10p TO ORDERS UNDER 42.

Catalogue which contains data sheets for most of the components listed will be sent free on request. 10p stamp appreciated.

CALLERS WELCOME Mon.-Sat. 9 a.m.-5 p.m. PLEASE ADD 10% VAT

W lskra high stability carbon film—very low noise—capless construction. W Mullard CR25 carbon film—very small body size 7.5 x 2.5mm. W 2% ELECTROSIL TR5

Power			Values	Price	
watts	Tolerance 5% 10% 2% 10% 5%	Range 4-70-2-2MΩ 3-3MΩ-10MΩ 10Ω-1MΩ 1Ω-3-9Ω 4-7Ω-1MΩ 1Ω-10Ω	available E24 E12 E24 E12 E12 E12	1-99 1p 1p 3-5p 1p 1p 6p	0.8p 0.8p 3p 0.8p 0.8p 5.5p

Quantity price applies for any selection. Ignore fractions on total order.

DEVELOPMENT PACK

0.5 watt 5% Iskra resistors 5 off each value 4.7Ω to IMΩ. El 2 pack 325 resistors £2.40. E24 pack 650 resistors £4.70.

POTENTIOMETERS

Carbon track $5k\Omega$ to $2M\Omega$, log or linear (log $\frac{1}{2}W$, lin $\frac{1}{2}W$). Single, 12p. Dual gang (stereo), 40p. Single D.P. switch 24p.

SKELETON PRESET POTENTIOMETERS

Linear: 100, 250, 500Ω and decades to 5MΩ. Horizontal or vertical P.C. mounting (0·1 matrix).

Sub-miniature 0·1W, 5p each. Miniature 0·25W, 7p each.

32n | BE177 | 28n | OC45 | 12n | 2N3710 | 110

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T	RA	N	SI	ST	O	RS	,
A	010	١7		15.			E

ACIU/ ISE	AF137	JAD	DF+//	Tab	0045			1177
AC126 12p		32p	BF178	32p	OC70	12p	2N3711	Hp
AC127 15g		40p	BF179	32p	OC71	12p	2N3819	32p
AC128 15		40p	BF180	32p	OC72	12p	2N 4062	12p
		12p	BFIBI	32p	OCSI	120	2N4286	20p
AC131 12p					OC82D	12p	2N4289	20p
AC132 12p	BC108	12p	BFI94	14p				
AC176 15p	BC109	12p	BF195	14p	2N2646	60p	40360	35p
AC187 226		12p	BF197	15p	2N2904	20p	40361	35p
AC188 226		12p	BF200	32p	2N2926	10p	40362	40p
			BFY50	20p	2N3054	58p	40408	40p
AD140 50p		12p						15p
AD149 45p	BC157	14p	BFY51	20p	2N3055	60p	ZTX108	
ADI61 336	BC158	14p	BFY52	20p	2N3702	13p	ZTX300	15p
AD162 36		14p	BUY105		2N3703	12p	ZTX 302	20p
AFI14 20		22p		2.25	2N3704	130	ZTX500	15p
			OC26	45p	2N3705	12p	ZTX503	20p
AF115 20p		75p					Z1 X303	Tob
AFII6 20g	BD132	75p	OC28	50p	2N3706	Пр		
AFI 17 201	BDI33	75p	OC35	50p	2N3707	12p		
AFI18 38		25p	OC42	120	2N3708	10p		
		20p	OC44	120	2N3709	Hp		
AF126 20	DF1/3	ZUD	0044	1 AP	2143707			

ZENER DIODES	I WIRE WOUND POTS, 3W.	10, 2	5
400mW 5% 3.3V to 30V, 12p,	50 Ω and decades to 100kΩ, 35p.		

RECTIF				SIGNAL	_
BY 127	1250V	LA	12p	OA85	7p
IN4001	50V	ÍΑ	7 _P	OA90	5p
IN4002	100V	IA	8p	OA91	5p
IN4004	400V	IA	8p	OA202	7 p
IN4006	800V	I.A.	10p	IN4148	5p
IN4007	1000V	IA	10p	BAII4	Вp

BRUSHED ALUMINIUM PANELS $12in \times 6in = 25p$; $12in \times 2\frac{1}{2}in = 10p$; $9in \times 2in = 7p$

SLIDER POTENTIOMETERS

86mm × 9mm × 16mm, length of track 59mm,
SINGLE 10K, 25K, 100K log, or lin. 40p,
DUAL GANG, 10K + 10K etc. log. or lin. 60p,
KNOB FOR ABOVE 12p,
FRONT PANEL 65p,
18 Gauge panel 12in × 4in with slots cut for use
with slider pots. Grey or matt black finish comnlare with fixings for 4 pots.

with slider pots. Grey or plete with fixings for 4 pots.

THERMISTORS

15p 15p 15p £1-35 VA1055S VA1066S VA1077 R53

THYRISTORS 2N5060 50V 0.8A 30p. 2N5064200V 0.8A 47p. CR51/40 400V IA 25p. 106F 50V 4A 40p, 106D 400V 4A 65p.

MULLARD POLYESTER CAPACITORS C296 SERIES
400V: 0.001μF, 0.0015μF, 0.0022μF, 0.0033μF, 0.0047μF, 2‡p. 0.0068μF, 0.01μF,
0.015μF, 0.022μF, 0.033μF, 3p. 0.047μF, 0.068μF, 0.1μF, 4p. 0.15μF, 6p. 0.22μF, 7‡p.
0.33μF, 11p. 0.47μF, 13p.
160V: 0.01μF, 0.015μF, 0.022μF, 0.033μF, 0.047μF, 0.068μF, 0.1p. 0.1μF 3‡p. 0.15μF 4‡p.
0.22μF, 5p. 0.33μF, 6p. 0.47μF, 7]p. 0.68μF, 11p. 1.0μF, 13p.
MULLARD POLYESTER CAPACITORS C280 SERIES
250V P.C. mounting: 0.01μF, 0.015μF, 0.022μF, 3p. 0.033μF, 0.047μF, 0.068μF,
3‡p. 0.1μF, 4p. 0.15μF, 0.22μF, 5p. 0.33μF, 6‡p. 0.47μF, 8‡p. 0.68μF, 11p. 1.0μF, 13p.
1.5μF, 20p. 2.2μF, 24p.

MYLAR FILM CAPACITORS 100V 0·001μF, 0·002μF, 0·005μF, 0·01μF, 0·02μF, 0·05μF, 0·01μF, 0·02μF, 2½p. 0·04μF, 0·05μF, 0·068μF, 0·1μF, 3½p.

CERAMIC DISC CAPACITORS 100pF to 10,000pF, 2p each.

ELECTROLYTIC CAPACITORS-MULLARD 015/6/7

ELECTROLITIC CAPACITORS—MULLARD O15/6/7 $(\mu F|V) \ 1/63, \ 1.5/63, \ 2.2/63, \ 3.3/63, \ 4.7/63, \ 6.8/40, \ 6.8/63, \ 10/25, \ 10/63, \ 15/16, \ 15/40, \ 15/63, \ 22/10, \ 22/25, \ 22/63, \ 3.3/63, \ 3.3/40, \ 4.7/4, \ 4.7/10, \ 4.7/25, \ 4.7/40, \ 6.8/6-3, \ 6.8/16, \ 100/4, \ 100/10, \ 100/25, \ 150/16-3, \ 150/16, \ 2.20/4, \ 2.20/6-3, \ 2.20/16, \ 3.30/4, \ 6.9, \ 4.7/63, \ 100/40, \ 150/25, \ 2.00/25, \ 3.30/10, \ 4.70/6, \ 4.70/26, \ 6.80/16, \ 1.50/6-3, \ 13.96, \ 3.11p. \ 100/63, \ 150/63, \ 2.20/63, \ 1.000/10, \ 1.2p. \ 4.70/25, \ 6.80/16, \ 1.500/6-3, \ 13.96, \ 4.70/40, \ 6.80/25, \ 1.000/16, \ 1.500/16, \ 1$

SOLID TANTAL	M BEAC	CAPACIT	ORS			12p
0·14F		2-2µF	35∨	22µF	16V	
0·22µF	35V	4:7uF	35∨	33µF	100	
	35∨	6-84F	25V			
	35V	10µF	25V	100µF	3 🗸	

VEROBOARD			JACK PLUGS AND SOCKETS
2½ × 3½ 2½ × 5 3½ × 3½ 3½ × 5 17 × 2½	0-I 22p 24p 24p 27p 75p 100p	0-15 16p 24p 24p 27p 57 ¹ p 78p 82p 60p 42p 12p	Ståndard screened 18p 2-5mm insulated 8p 25mm consulated 12p 3-5mm insulated 8p 25mm screened 13p 3-5mm screened 15p 25mm socket 15p 2-5mm soc
Pin insertion too Spot face cutter Pkt. 50 pins	52p 42p 20p	52p 42p 20p	BATTERY ELIMINATOR 9V mains power supply. Same size as PP9 battery.

1600µF 2500µF 2500µF	64V 40V	74p 74p	2500μF 2800μF 3200μF	100V	£2.60	4500μF 4500μF 5000μF	25V	€1-68
2500µF	20 V	38p	3200μ	104	Job	3000		

HIGH VOLTAGE TUBULAR CAPACITORS—1,000 VOLT
0.01 µF 10p 0.047µF 13p 0.22µ
0.022µF 12p 0.1 µF 13p 0.47µ 0·22μF 0·47μF

POLYSTYRENE CAPACITORS 160V 21% 10pF to 1,000pF E12 Series Values 4p each-

SMOKE AND COMBUSTIBLE GAS DETECTOR—GDI

SMOKE AND COMBUSTIBLE GAS DETECTOR—GDI
The GDI is the world's first semiconductor that can convert a concentration of gas
or smoke into an electrical signal. The sensor decreases its electrical resistance when
it absorbs deoxidizing or combustible gases such as hydrogen, carbon monoxide,
methane, propane, alcohol, North Sea gas, as well as carbon-dust containing air or
smoke. This decrease is usually large enough to be utilized without amplification.
Full details and circuits are supplied with each detector.
Detector GDI, £2. Kit of parts for detectors including GDI and P.C. board but
excluding case. Mains operated detector £5:20. 12 or 24V battery operated audible
alarm £7:30. As above for PP9 battery, £6:40.

97p
PRINTED BOARD MARKER
Draw the planned circuit onto a copper laminate board with the P.C. Pen, allow to
dry, and immerse the board in the etchant. On removal the circuit remains in high
relief.

ITT/TEXAS IC'S NOW IN STOCK LARGE RANGE

							_			-				
		PRI	CES ARE	CALCU	LATED	ON TOTA	LNUN	IBER OR	DERED	REGARDLES	SS OF	MIX		
	1-11	12-24	25-99	100+	1 7448	185	175	170	165	74118	100	82	73	64 36
	1-11	12024	23-77	P	7450	18	16	14	13	74121	43	40	38	85
7400	18	16	14	13	7451	iš	16	14	13	74141	100	95	90	130
7401	18	16	- i4	i3	7453	18	16	14	13	74145	150	140	135	220
7402	iš	16	i i i	13	7454	18	16	14	13	74150	330	280	250	89
7403	18	16	14	13	7460	18	16	14	13 ′	74151	110	100	95 105	95
7404	20	18	16	i4	7470	30	28	25 27	24	74153	120	110	170	160
7405	20	18	16	14	7472	30	28	27	23	74154	200	180		86
7406	50	45	40	35	7473	40	38	36	30	74155	150	120	100	96
7407	56	50	44	38	7474	40	36	32	28	74156	130	120	112	105
7408	36	30	27	23	7475	55	52	50	49	74180	155	136	185	180
7409	36	30	27	33	7476	40	36	32	30	74190	195	190	185	180
7410	18	16	14	13	7480	100	95	90	85	74191	195	190 190	180	164
7411	23	21	20	18	7481	125	115	110	105	74192	200	180	170	150
7412	36	30	27	23	7482	100	96	90	85	74193	200	190	180	170
7413	34	28	26	22	7483	100	97	95	92	741.96	200	195	180	170
7416	45	43	39	34	7484	120	115	110	105	74197	200	193	100	
7420	18	16	14	13	7485	250	245	240	230	-				
7421	36	30	27	23	7486	45	42	37	33			LINEARI	C's	
7426	32	29	23	20	7490	75	67	60	52 79	709		14 pin DIL		40p
7430	20	18	16	14	7491A	100	92	85	60	741		8 pin DIL		40p
7432	40	36	32	28	7492	75	70	65	52	1 7 4i		14 pin DIL		38 _p
7440	20	18	16	14	7493	75	68 90	60 85	80	723		14 pin DIL		95p
7441	80	75	70	65	7494	95		95	90	747		14 pin DIL		85p
7442	80	75	70	65	7495	105	100	73	65	748		8 pin DIL		45p
7443	125	120	115	115	7496	100	95	235	230	DIL socket		14 pin and	l6 pin	16p
7447	175	145	150	120	74100	250	240	T33	230	1 DIF SOCKER	•	i + pin and		

I ENTERTAINMENTS L

STANDARD & CUSTOM-BUILT AUDIO & ELECTRONIC EQUÌP. MENT. NEW & SECONDHAND MUSICAL INSTRUMENTS. DISTRIBUTORS FOR A.K.G. HIGH QUALITY MICROPHONES

Better built Better performance Better value

SAYON HI.FI POWER AMPS FOR DOMESTIC & COMMERCIAL USE

New Versions using 3A "Plastic Power" Driver Transistors now available.

meet demand, we hav included a more powerful module in our well-established and proven range module in our well-established and proven range. All these power amplifiers are carefully assembled, tested and guaranteed. They offer superb value for reliability and varsatility.



SA35

35W RMS uses 7 transistors and 7 diodes. Carr. paid.

£4·45

A NEW ADDITION IS THE SA50 at £5.65

Carr. paid. A rugged, well built unit, capable of 50W RMS out, with all the advantages of Saxon Amplifier design and quality. Ready now.

SA 100 makes an ideal unit in disco assemblies

A real glutton for work. Reliable, tough and compact. Il transistors, tough and compact. 6 diodes. Carr. paid.

£10.90

BRIEF SPEC. FOR ALL THREE MODULES

Freq. response Distortion Loads Quiescent current Noise Supply voltage Size

PS70

15-40,000 Hz ± IdB 0-2% at lkHz 4 to 16 ohms 15mA

Better than -75dB \$A35-45V \$A50 45/65V \$A100 40-70V 4\frac{1}{1}n \times \text{lin} (\$A100) 4\frac{1}{1}n \times \text{lin} (\$A35/\$A50)

OPEN AND SHORT SHORT CIRCUIT PROTECTION, plus proof against over-dissipation and faulty inductive loads in its SA100

All modules

Circuits, connecting instruction and application data are supplied free with all modules.

POWER SUPPLIES FOR THE SA35, SA50 AND SA10 POWER AMPS. ABOVE

Unstabilised supply for 2 SA35's £4.90 Unstabilised supply for one or two SA50 or 5A100 £7.75 carr. 40p PU45 PU70 SA50 or 5A100 Stabilised module for two SA35's £3.50 carr, free PS45 Transformer for above, heavy duty
£2.85 carr. 20p MT45 MT30

Transformer for unstabilised supply complete with rectifier diodes mounted 43-50 carr. 20p Stabilised supply module for one or two SA100's £4.90 carr. free £4.90 carr. free

M T70 ALL MODULES ARE BUILT ON GLASS FIBRE P.C. BOARD AND SUPPLIED FULLY TESTED

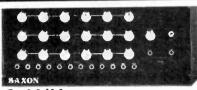
SAXON PA MIXER-CONTROL UNITS

In extra slimline easy-fit case.

Using grouped pairs of inputs (high Z and low Z inputs) with individual bass, treble and volume controls on each pair, plus master controls. These lownoise units will feed all makes of ampliflers, making them ideal for clubs, discos, etc. Standard jack sockets, compact design. In strong metal cases. All Units guaranteed for 3 years.

HIGH AND LOW IMPEDANCE INPUTS

- BASS/TREBLE/VOLUME ON EACH PAIR
- CONTROL ON MASTER OUTPUT



M4H

4 high Z, 4 low Z inputs, 4 sets of controls. Case 10" × 8" and only 2\frac{1}{2} in deep. Carr. paid.

M6HL

Channel section modules, for building your own: gain—16 × (24dB). Tone controls—18dB swing. Carr. paid.

£3.50 + v.a.t.

CONTROL UNITS

Mono (as shown). **£6.50** Carr. 20p. For 9 v. battery operation. As stereo model, less mic.

input. Stereo. Carr. 30p.

Two decks, and full headphone monitoring. The unit is mains operated and measures 17½ in × 3 in × 4 in deep and is finished with a smart white on black facia. The controls are: Left/Right deck fader, volume, bass, treble, Headphone Selector and volume, Microphone volume, bass treble, mains on/off. treble, mains on/off.
COMPARABLE TO UNITS AT OVER TWICE THE PRICE.

PLEASE ADD 10% FOR V.A.T. TO TOTAL VALUE OF YOUR ORDER

S.A.E. brings Saxon equipment and bargains list

• 160 watts version with power supply (Carr. 50p) £27.90

120 W HEAVY DUTY MODULE

Rugged class A driver stage. This module will run from all our mixers, etc., and most other makes. Delivers 120W into an eight ohm load and employs 4 TO3 can Celivers 120W into an eight ohm load and employs 4 TO3 can (115W) output transistors. SPECIFICATION
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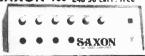
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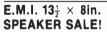
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Price £1:40 £1:60 X25 25 watt CCN240 15 watt ST3 Stand X25E Replacement 25W Element CCN240E Replacement 15W Element

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HH-101 Straight Headphone Cable HH-102 15ft Coiled Headphone Extension Cable

GL20 20ft Coiled Guitar Cable, Straight Jackplug to Angled Jackplug £1-30 SEND FOR OUR FREE CATALOGUE (ENCLOSING 5p STAMP)

HILLS COMPONENTS

DEPT. PE12, UNIT No: 6, MELINITE INDUSTRIAL ESTATE, BRIXTON ROAD, WATFORD, HERTS. WD2 5SL. Tel. Watford 27711



FAN/ **BLOWER**

Precision-built in Germany. Dynamically balanced mains Dynamically Dynamically balanced mains unit (200/240) continuous rated, reversible 60mA m rm. Size: 5½ dia. × 2½ deep. Back plate is tapped for 4 fixing sorews (aupplied). Well under maker's price at 23. P. & P. 20p. Similar unit to above but 7½ dia. × 3° deep. 23.30. P. & P. 250.

P. & P. 250



SMITHS RINGER-TIMER

Reliable 15 minute times, spring wound (concurrent with time setting) 15 x 1 min. divisions, approximately 2* between divisions, approximately divisions, approximately 3 between divisions. Panel mounting with chrome bezel 34 dia. £1.40, P. & P. 15p.



GEARED MOTORS

Parvalux" Reversible 100 rpin geared motor. Type 8D14, 230/250V a.c., 22 lb/in. 2 spindle. BRAND NEW. £13.70 each. P. & P. 50p.

REVERSIBLE Parvalux type SD19, 240V a.c. 30rpm. 40 tb/in. Variable angle drive shaft. Ex-equipment in good condition. \$7. P. & P. 50p.

SHADED POLE Mains motor. 11 × 11 × 2" high. Double ended & shaft projecting 12" each side of motor. 21. P. & P. 20p.

OPEN FRAME shaded pole GEARED MOTORS

(Ours) gear case)
240 a.c., 28rpin. NEW
HIGH TORQUE, approx.
overall size: 3½ × 3½ ×
3½ + spindle ½ dia. as illustrated 43. P. & P. 30p.
3½ + spindle ½ dia. as illustrated 43. P. & P. 30p.
110rpin with pressed steel gear case (aimliar to above but slightly smaller). 22-70, P. & P. 30p.



SPIT MOTOR

 $5\frac{1}{4}$ rpm. $2\frac{1}{4}$ " × $1\frac{1}{4}$ " × $6\frac{1}{4}$ " high. 240V a.c. Shaft $\frac{1}{4}$ " o/d, $1\frac{1}{4}$ " length with hexagon socket inside. **\$2**. P. & P. 30p.



AMPEX 7.5v. DC

AMPEX 7.5v. DC MOTOR
This is an ultra precision tape motor designed for use in the AMPEX model AG20 portable recorder. Torque 4300M/cM. Stall load at 300mA. Draws 60mA on run. 600rpm ± speed adjustment. Internal AF/RF suppression. 1 dia x 1 spindle, motor 3 dia x 1 v. Original cost £16:50. OUR. 25p. Large quantities available

PRICE £3,30, P. & P. 25p. Large quantities available (special quotations). Mu-metal enclosure available (special quotations). M 75p each. P. & P. FREE.

"DAVENSET" MAINS SOLENOID

travel, 8lb pull (approx.). Size: 21" long × 23/16" × high. Similar in appearance to "SORENG". £1-65

MAINS SOLENOID

This little unit gives vertical lift of approximately 1" through hinged Bracket incorporates 2 fixing screws. Length of arm, 2½, 240V a.c. Pull at coil is approximately 11b. 21. P. & P. FREE. Special quotes for quantities.

SOLENOIDS by WESTOOL

240 a.c. type MM6. 3lb. pull, 2; x 1 x 1; Travel 1'. 90p each. P. & P. 10p.

240 a.c. type MM4. 2lb. pull. 1½" × 1½" × 1". Travel ½" 70p each. P. & P. 10p. Quantity discounts; 10-50 10%. 50 upwards 25%.



"DECCO" MAINS SOLENOID

Compact and very powerful. 16lb. pull. $\ref{pull.}$ travel which can be increased to 1^a by removing captive-end-plate. Overall size: $2^a \times 2^a \times$



MAINS SOLENOID by MAGNETIC DEVICES LTD.

A beautifully constructed solenoid at half normal price. A 2-sided bracket is incorporated for vertical or horizontal mounting. Size: 2° × 14° × 14°. Pull is approximately 2lb, plunger travel 11°. Fixing eye takes up to 1° boit, plunger non-captive. NEW in original maker's boxes. 81-20. P. & P. 20p. Large number available, special price for quantity.

"CROUZET" MOTORS **Type 965**



115/240V. 50Hz. 48W. Stoutly constructed, 2 11/16" dia. × 31" long plus spindle 1" × 4" dia. Anticlock. \$3:30 each. P. & P. 25p.

"RE CIRK IT" Mains 10amp cut-out

by "Neimman Electric" Germany. Eliminates fuses. Size: 2" × 4" × 14" deep. 75p each. P. & P. 10p. 4 or more 55p each. P. & P. 20p.



KNOWLE (U.S.A.) MINIATURE MICROPHONE CAPSULES

Impedance approx. $200\,\Omega_{\odot}$ output 60 or 80 DB at 1 Kc. As used in deaf aids, bugging devices, etc. Size (60 DB) $7/32^{\circ} \times 5/32^{\circ} \times \frac{1}{2}^{\circ}$; (80 DB) $\frac{3}{8}^{\circ} \times 5/32^{\circ} \times \frac{3}{8}^{\circ}$. Exequipment, all tested. £1-40 each. P. & P. FREE.

UNLESS OTHERWISE STATED

all items are NEW and UNUSED. Postal or carriage

an items are NEW and UNUSED. Postal or carriage charges are for Gt. Britain only. We welcome orders from established companies, educational depts., etc. All orders under \$2:50. C.W.O., please. Company orders under \$2:50, surcharge 60p. unless C.W.O.

PLUG-IN RELAYS by SCHRACK (Perspex enclosed)

OCTAL (2c/o) 8 amp contacts at following voltages: 48 d.c., 60 d.c., 60 a.c., 110 d.c., 380 a.c. PRICE EACH £1:10.

PRICE EACH #1-10.

11 pin (3 c/0) 6 amp contacts:

12 a.c., 48 d.c., 48 a.c., 60 a.c., 60 d.c., 110 d.c., 115 a.c.,

240 a.c. PRICE EACH £1-40.

RA and RN Series (4 c/0) 3 amp Gold Plated Contacts.

Handsome modern construction #* ** ** ** *12 high.

Following voltages: 6 a.c., 12 a.c., 24 a.c., 48 a.c., 48 d.c.,

60 a.c., 110 d.c., 115 a.c., 120 a.c.

PRICE EACH £1.

Base sockets for all above types 15p.

Please add 10p towards P. & P. on all orders.

From JAPAN. TAKAMISAWA Perspex enclosed relays. Type MQ308 24V d.c. 600 ohms (4c/o). Complete with base socket. 90p. P. & P. 10p.



(P. & P. 12p)

SILVANIA

MAGNETIC SWITCH Now complete with reference magnet!

A magnetically activated switch, vacuum sealed in a glass envelope. Silver contacts, normally closed. Rated 3 amp at 129V. 1½ amp at 240V. Size: (approx.) 1½° long x½° dia. Ideal for burglar alarms, security systems, etc. and wherever non-mechanical switching is required. 10 for £2. P. & P. 15p; 30 for £8:80; 100 for £16:50. P. & P. FREE over 10.

NORPLEX

The famous American fibre-glass copper-clad laminate. Finest quality with woven glass base of Epoxy-resin. Excellent Mech. and Elec. conductive properties. Heat resistant, ideal for P.C.'s, etc. THIS IS A SPECIAL PURCHASE AND ONLY AVAILABLE WHILE STOCKS LAST! Sizes: 12' x 12'; 24' x 12'; 24' x 24'; PULL SHEET 43' x 37' (11 suj.ft.) Single-sided Copper with thickness of 1/32'; 3/64', 3/32'. Also double-sided 1/32', 1/64', 3/32'. By per sq.ft. Cut sizes (1-0 sq.ft. P. & P. 25p. Full Sheet 28 each. Carr. £1 for 1st sheet plus 25p each additional sheet. plus 25p each additional sheet

TANGENTIAL HEATER

Silently driven by shailed pole Mycalex motor, powerful and amooth running with aluminium impeller (outlet \$\frac{9}{2}^{\chi} \times 1\frac{1}{2}^{\chi} \t

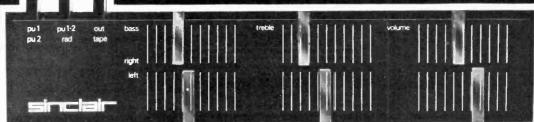
ALL PRICES NOW INCLUDE V.A.T.

ELECTRO-TECH COMPONENTS LTD.

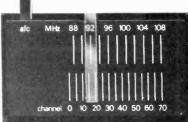
315/317 EDGWARE ROAD LONDON, W.2 Tel. 01-723 5667 01-402 5580

now... Project 80

--- exciting new thinking in modular hi-fi design

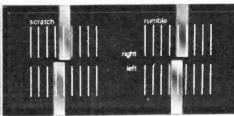


Stereo 80 pre-amplifier/control unit



mono'

© stereo



Project 80 tuner

Stereo decoder

Project 80 Active Filter Unit (AFU)

the slimmest, most elegant hi-fi modules ever made



Living with hi-fi takes on new meaning now that Project 80 is here. These amazing new modules mark a brilliant technical advance all round; their size and presentation bring exciting new opportunities to install systems in ways hitherto only dreamed about but never before made practical. You can build a Project 80 system virtually anywhere and it is unbelievably simple to install and connect up. Everything that could possibly be wanted in a top quality do-it-yourself domestic hi-fi system will be found in Project 80 – compactness, elegantly ultra-modern styling, ease of fixing and operation, new control methods, and above all superb performance. New as well as popular established ideas on installation are featured on page four of this announcement to provide just a few examples of the system's fantastic versatility.



Project 80 new modules

Stereo 80 pre-amplifier and control unit

As with other Project 80 units, the Stereo 80 is mounted by means of two bolts fixed at the rear which pass through holes drilled in the wood or plastic on which modules are to be mounted. All the electronics are contained within the 3 deep front panel! Connecting leads are taken away similarly out of sight. Each channel in the Stereo 80 has its own independent tone and volume controls operated by sliders. This enables exceptionally good environmental matching to be obtained Provision is made for magnetic and ceramic pick-ups, radio and tape in and out A virtual earth input stage forms part of the up-dated circuitry of the Stereo 80 to ensure the finest possible quality from all signal sources. Generous overload margins are allowed on all inputs. Clear instructions with template are supplied

TECHNICAL SPECIFICATIONS

Size - 260 × 50 × 20mm (10½ × 2 × ¾ins)

Finish – Black, with white markings Inputs – Mag P U 3mV RIAA corrected: Ceramic P.U. 300 mV Radio 300 mV. Tape 30 mV

S/N ratio - 60db

Frequency range - 20Hz to 15KHz + 1dB · 10Hz to 25KHz + 3dB

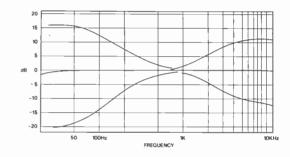
Power requirements - 20 to 35 volts

Outputs - 100mV + AB monitoring for tape

Controls - Press button for tape, radio and P.U. selection Volume.

Bass+ 12dB to -14dB at 100Hz, Treble+11dB to-12dB at 10KHz

For P.U., radio and tape Tape monitoring switch Two-hole fixing R.R.P. £11.95 + £1.19 V.A.T.



Project 80 FM tuner smaller, more efficient

A truly remarkable tuner in every way - its unbelievably compact size its original circuitry - its dependable performance - all this in a boldly designed modern case measuring 85 × 50 × 20mm (3½ × 2 × ½ ins). Greater adaptability (and possibly financial convenience) results from the tuner and stereo decoder section being made available separately

TECHNICAL SPECIFICATIONS

Size - 85 · 50 · 20mm (approx 3½ · 2 · 3 ins)

Tuning range – 87 to 108 MHz

Detector – I C. balanced coincidence, for good A.M. rejection

AFC - Switchable, with thermistor control to prevent from drift

One 26 transistor I.C.

Twin dual varicap tuning

Distortion - 0 3% at 1 KHz for 75 KHz deviation

Ceramic filter in I.F. section Aerial impedance $-75~\Omega$ or 240-300 Ω

Sensitivity - 4 microvolts for 30dB quieting Power requirements - 12 to 45 volts

AFC switch Twin dual varicap tuning. 4-hole ceramic filter Slider tuning R.R.P £11.95 + £1.19 V.A.T.

Project 80 stereo decoder

Making the Project 80 decoder separate from the F.M. tuner gives the constructor a wider choice of systems as well as saving money in cases where stereo reception may not be required. This unit gives a 40dB channel separation with an output of 150mV per channel. The gallium arsenide light emitting beacon automatically lights up to show when a stereo transmission is tuned in. Designed essentially as an integral part of Project 80 systems, this multiplex stereo demodulator may be used in many cases with existing single channel frequency modulated tuners to provide stereo reception

Size - 47 × 50 × 20mm (1 2 · 2 · 1 ins)

One 19 transistor I.C



- Solid-state stereo indicating beacon
- Readily adaptable for use with other tuners

R.R.P. £7.45 + 0.74p

new constructional techniques

...and again Sinclair leads the world

- 1962 Micro-miniature power amp small enough to stand on a 10p. piece. Slimline pocket receiver smaller than a 20 cigarette pack
- 1963 Micro-6 receiver smaller than a matchbox
- Pocket F.M. receiver; PWM amp.
- 1965 Z.12 power amplifier module: PZ.3 power supply
- 1966 Stereo 25 pre-amp/control unit
- 1967 Micromatic: Q.14 loudspeaker; the first Neoteric
- 1968 IC.10, the first ever integrated circuit for constructors' use

Project 80 active filter unit

This efficiently designed unit makes a highly desirable part of any worthwhile system where inputs may be from record, radio or tape. As with Stereo 80, separate controls are applied to each channel thereby making it easier to obtain ideal stereo balance in any kind of indoor environment.

TECHNICAL SPECIFICATIONS

Size $-108 \times 50 \times 20$ mm $(41 \times 2 \times 1$ ns)

Voltage gain - minus 0 2dB

Frequency response - 36Hz to 22KHz, controls minimum

Distortion - at 1 KHz - 0 03% using 30V supply

HF cut off (scratch) - 22KHz to 5 5KHz, 12dB/oct slope

L.F. cut off (rumble) - 28dB at 20Hz, 9dB/oct. slope

Z.40 & Z.60 power amplifiers totally short-circuit proof

Either of these entirely newpower amplifiers is intended for use in Project 80 installations although, of course, they are readily adaptable to an even wider range of applications. Both Z.40 and Z.60 incorporate builtin protection against shortcircuiting and risk of damage arising from mis-use is greatly reduced. Comprehensive instructions are supplied with each of the modules.

Z.40 Technical Specifications Size $-55 \times 80 \times 20$ mm (21×31×3ins) 9 transistors Input sensitivity - 100mV Output - 15 watts RMS continuous

into 8 Ω (35V), 30 watts music power(into 4 Ω (30V) Frequency response – 10Hz–100KHz±1dB

Signal to noise ratio - 64dB Distortion – at 10 watts into 8 Ω less than 0.1%

Power requirements - 12-35 volts

Z 60 Technical Specifications Size - 55 × 98 × 20mm

(21×31×31ns) 12 transistors Input sensitivity - 100-250mV Output - 25 watts RMS into $8~\Omega~(45V)$, 50~watts~music~powerinto 4 Ω (50V)

Distortion - typically 0 03% Frequency response - 10Hz to more than 200KHz±1dB Signal to noise ratio - better

Built-in protection against transient overload and short

than 70dB

Load impedance - 40min; max safe on open circuit

Sinclair power supply units PZ.8

the worlds most

advanced unit in its class

Stabilised power supply unit. Reentrant current limiting makes damage from overload or even direct shorting impossible, a principle never before inorporated in a com mercially available constructor mod-ule. Normal working voltage (adjus-table) 45V

R.R.P. £7.98 + 0.79p V A.T Without mains transformer PZ.5 30V unstabilised R.R.P. £4.98+0.49p V.A.T PZ.6 35V. stabilised R,R P. £7.98+0 79p V A.T





R.O. London Rd., St. Ives, Huntingdon PE17 4HS Reg. England 699483 December 1973 Practical Electronics

Q.16 - improved version of Q.14 Systems 2000 and 3000: Project 60 launched

1C.12 Project 605 1970

1971 Project 60 stereo FM tuner Z.50: PZ.8

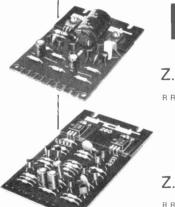
1972 Improvements to Project 60 with Z.50 MK.2 and PZ.8 Mk.3 The Executive Calculator: Digital multi-meter Q.30 speaker

1973 Cambridge Calculator

PROJECT 80 LAUNCHED

...and next?





NEW

Z.40

RRP 65.45 + 0.54p

Z.60

RRP £6.95 + 0.69p

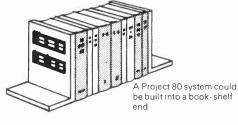
Recommended Project 80 applications

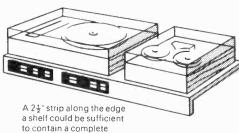
The Units to use	Units cost
Z.40	£5.45 +54p V A.T.
Z.40, PZ.5	£10.43 +£1.04 V.A.T.
2 < Z.40s, Stereo 80; PZ.6	£30.83 +£3.08 V.A.T.
2× Z.60s, Stereo 80; PZ.8	£33.83 +£3.38 V.A.T
Z.60, PZ.8	£14.93 +£1.49 V.A.T.
F.M. tuner, Z.40	£16.40 +£1.64 V.A.T.
	Z.40 Z.40, PZ.5 2 × Z.40s, Stereo 80; PZ.6 2 × Z.60s, Stereo 80; PZ.8 Z.60, PZ.8 F.M. tuner,

From Sinclair the worlds most advanced hi-fi modules

Sinclair Project 80 the ultra-modern non-obtrusive hi-fi

system







The modules mount very easily onto a playing plinth



A novel application would be to build around the base of a lampshade



suitably positioned together with Project 80 could be mounted on to a false wall.



Project 80 could be easily mounted onto a loudspeaker



When you have seen for yourself how fantastically slim and cleverly designed these modules are, further ways will suggest themselves in which they can become a pleasing part of your particular domestic environment.

Please send post paid	
for which I enclose Cash/Cheque for £	including V.A.T.
Name	
Address	

Guarantee

If, within 3 months of purchasing any product direct from us you are disproduct direct from us, you are dis-satisfied with it, your money will be refunded on production of receipt of payment. Many Sinclair appointed Stockists also offer this guarantee. Should any defect arise in normal use, we will service it without charge.

For damage arising from mis-use a small charge (typically £1.00) will be made.



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VARIABLE VOLTAGE TRANSFORMERS

INPUT 230/240V a.c. 50/60 OUTPUT VARIABLE 0-260V

All Types from \(\frac{1}{2}\) to 50 amp from \(\frac{1}{2}\) to 50.

SHROUDED TYPE A £8.75, Post 50p -5A £10-10, Post -60p



5A £14-60, Post 37-5A 75p 50A £ CARRIAGE AND PACKING EXTRA unless shown (Panel Mounting)
(Pamel Mounting)
(Pamel Mounting)
(Pamel Mounting)
(Pamel Mounting)
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(Pamel Mounting)

RING TRANSFORMERS

Functional Versatile Educational Functional Versatile Educational
These multi-purpose Auto Transformers,
with large centre aperture, can be used
as a Double wound current Transformer,
Auto Transformer, H.T. or L.T. Transformer, by simply hand winding the
required number of turns through the
centre opening. E.g. using the RT.100
VA Model the output could be wound
8V @ 12½A, 4V @ 25A or 2V @ 50A, etc. wound to give

rice: 43-00. Post 35p. RT.18VA 1-82 turns per V. RT.1KVA 1-82 turns per V. RT.2KVA 1-5 turns per V. RT.3KVA 1-5 turns per V. RT.3KVA 1-5 turns per V. RT.3KVA 1-5 turns per V.

VOLTAGE CHANGING TRANSFORMER M.f.g. to highest W.D. spec. Auto wound, and capped 0-130-160-200-250 at least 2kVA. Can also pased as 230-240V input, 115V out for U.S.A. equipment, or reverse to obtain 240V from 115V. The ideal transformer for making up solid state constant voltage unit, by use of taps the following voltages may be obtained 30-40-50-70-90V at 10 amps. Weight 40lb, length, 260mm, height 190mm, width 230mm, In original maker's wooden case, £8. Carr. £1. VOLTAGE CHANGING TRANSFORMER

BLOWER UNIT 200-240 Volt A.C. Precision German built. Dynamically balanced, quiet, continuously rated, reversible motor. Con-sumption 60mA. Size 120 mm. dia.x 60 mm. deep. Price £3. Post 30n



4 BANK 3c/o PUSH BUTTON ASSEMBLY Black rectangular buttons. 5 units (min. order) 85p.



PARVALUX Type: SDI. S/86896/OJ 230/250V A.C. 50 r.p.m. 7 lb/in. Continuously rated. £6. Post 30p incl. base.



WATT DIMMER SWITCH Easily fitted. Fully guaranteed by makers. Will control up to 600W of all lights except fluorescent at mains voltage. Complete with simple instructions. £2.75. Post 25p.

2000 WATT POWER CONTROL For Power tools, Heating, Sewing Machines, Lighting, etc. £8-00, Post 27p.

ENNER TIME SWITCH TYPE MSQP

200/250 Volt 2-ON/2-OFF every 24 hours at any manually pre-set time. 20 amp contacts. Fitted diecast case. Tested and in perfect condition £4 75.Post 25p.



FOOT SWITCH

Suitable for Motors, Drills, etc., etc. 5 amp. 250 volt. Price 75p. Post 15p.



AHH

UNISELECTOR SWITCHES NEW 4 Bank 25 Way,

24V d.c. operation. £6-90. Post 30p. 6 Bank 25 Way, 24V d.c. £7-90. Post 30p. 8 Bank 25 Way, 24V d.c. operation. £9.50. Post 40p



All Mail Orders—Callers—Ample Parking Dept. PEII, 57 BRIDGMAN ROAD CHISWICK, LONDON W4 5BB Phone 01-995 1560

Showroom open Mon.-Fri.

STROBE! STROBE! STROBE!

Build a Strobe Unit, using the latest type Xenon white light flash tube. Solid state timing and triggering circuit. 230/250V a.c. operation. EXPERIMENTERS' ECONOMY KIT Speed adjustable 1 to 30 flash per sec. All electronic components including Xenon Tube and instructions 66-30. Post 300.

and instructions 26-30, root sop.

NEW INDUSTRIAL KIT
Ideally suitable for schools, laboratories, etc.
Speed adjustable 1-80 f.p.s.
Approx. 2 output of Hy-Lyght, Price £10-50.

Post 50p

Post 5UP.

HY-LYGHT STROBE MK III

For use in large rooms, halls and utilises a silica
tube, printed circuit. Speed adjustable 0-20 f.p.s.
Light output greater than many (so called 4
Joule) strobes. £12. Post 50p.

THE 'SUPER' HY-LYGHT KIT

Approx, four times the light output of our well proven Hy-Lyght strobe

Variable speed from 1-3 flash per sec.

 Reactor control circuit producing an intense white light. ONLY £20. Post 75p.

ROBUST, FULLY VENTILATED METAL CASE, For Hy-Lyght Kitincluding reflector £4-75. ost 25p

Super Hy-Lyght Kit including reflector £7. Post

Over Trinch POLISHED REFLECTOR Ideally suited for above Strobe kits, Price 55p. Post 15p.

RAINBOW STROBE FOUR LIGHT

Will operate four of our Hy-Lyght or Super Hy-Lyght Strobes in either 1, 2, 3, 4 sequence; 2 + 2; or all together. Thoroughly tested and reliable. Complete with full connection instructions. Price: £18. Post 50p. Send S.A.E. for details.

COLOUR WHEEL PROJECTOR

Complete with oil-filled colour wheel. 100 watt lamp. 200/ 240V AC. Features 240V AC. Features extremely efficient optical system. £18-50. Post 50p.
6 INCH COLOUR WHEEL



As used for Disco lighting effects, etc. Price £5. Post 30p. 1 R.P.M. MOTOR 220/240 volt a.c., 1 r.p.m. synchronous motor. 2 watt. A/clock. Spindle 10mm long, 3mm dia

Motor only 20mm deep. Fixing centres 44mm. Price £1-10. Post 5p. Suitable for above wheel

BIG BLACK LIGHT

BIG BLACK LIGHT
400Watt. Mercury vapour
ultra violet lamp.
Powerful source of u.v.
Innumerable industrial applications also ideal for stage,
display, discos, etc. P.F. ballast
is essential with these bulbs.
Price of matched ballast and
bulb £16, Post £1.
Spare bulb £7, Post 40p.
BLACK LIGHT ELINDESCENT



BLACK LIGHT FLUORESCENT U.V. TUBES 4ft 40 watt. Price £5.50. Post 30p. 2ft 20 watt, £4.25. Post 25p. (For use in stan. bi-pin

fetigs. Fost 25p. (Follows) to the mixtures. MINI. 12in 8 watt, £1-60. Post 15p. 9in 6 watt, £1-30. Post 15p. Complete ballast unit and holders for 9in and 12in tube. £1-70. Post 25p. (9in and 12in measures



ORGAN KIT

Easy to build. Solid State. Two full octaves (less sharps and flats). Fitted hardwood case. Powered by two penlite 14V batteries. Complete set of parts including speaker, etc., together with full instructions and 10 tunes. Price 63-25. Post 35p.

50 in 1 ELECTRONIC PROJECT KIT
50 easy to build Projects. No soldering, no special tools required. The kit includes Speaker, Meter. Relay, Transformer, plus a host of other components and a 56-page instruction leaflet. Some examples of the 50 possible Projects are: Sound Level Meter, 2 Transistor Radio, Amplifier, etc. Price £773, P. & P. 25p.

All prices are subject to

10% VAT. (10p in the L) To all orders add 10% VAT to total value of goods including carriage/ packaging.

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Superior Quality Precision Made NEW POWER RHEOSTATS

New ceramic construction, vitreous enamel embedded winding, heavy duty brush assembly, continuously rated.

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100 WATT 1/5/10/25/50/100/250/500/1k/1-5k/2-5k/3-5k/5k ohm £2-35. Post 15p.
Black Silver, Skirted knob calibrated in Nos.
1-9. 1-§1n. dia. brass bush Idealfor above Rheostats.

// Sk ohm £2.35. Post 15p. k Silver, Skirted knob calibrated in Nos.

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Coil ohms	52	4-6	6M	60p*
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Working	185	8-12	6M	60p °
d.c. voits	280	8-16	2 c/o	60p*
C-1 3	410	10-18	4 c/o	70p*
Col. 3	700	16-24	4M 2B	60p*
Contracts	700	16-24	4 c/o	80 p*
Col. (4)	700	15-35	2 c/o HD	70p*
Price	700	16-24	6M	60p*
,,,,,,	700	6-12	I c/o HD	50p*
HD=	700	20-30	6 c/o	80p
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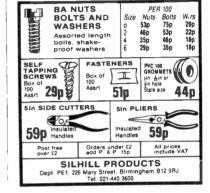
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1483	0.90		0.16	ACY19	0-27	aligned			1N5171 (1·5.	A 50pv)	84	IN5402 (3	3A 200pv)	1
11613	0.88	2N3860 2N3866	0.20 1.69	ACY20 ACY21	0-22 0-26	All prices p and plus 15p (lus 10%	VAT	1N5172 (1·5.	A 100pv)	9p 10p	1N5404 (3 CL7005 (3	(A 400pv) (A 600pv)	1
11631 11637	0.85 0.86	2N3877	0.25	ACY22	0.16	and plus 15p	post & r	packing.	IN4517 (1 5, IN5173 (1 5,	A 400px)	11p	('L7006 (3	3A 800pv) 3A 10 0 0pv)	
11638 11701	0.32 1.10	2N3877A 2N3900	0.26 0.20	ACY28 ACY30	0.20 0.42	All kits with			[N5176 (1.5) [N5177 (1.5)	A 800pv)	12p 15p	CL1002 (1	[0A 100pv)	:
11702	2.15	2N3900A	0.21	ACY39 ACY40	0-65 0-17	instructions a	nd cove	ered by a	PL4007 (1·5.	A 1000pv)	20p 15p	CT.1004 (1	10A 200pv) 10A 400pv)	
71711 71893	0.45 0.81	2N3901 2N3903	0.32 0.24	ACY41	0.17	full gu	arantee	e.	IN5400 (3A IN5401 (3A	100pv)	17p	CL1005 (1	10A 600pv)	
2102 2147	0-80 0-70	2N3904 2N3905	0·27 0·24	ACY44 AD136V	0.31 0.96						E AND C			an
2148 12192	0-94	2N3906	0·27 0·46	AD140 AD142	0.55 0.50	BC302 6-97 BF82	8 0-92	MJ430 0-75	IN 1183 (35A IN 1184 (35A		92p £1·12		35A 400pv) 35A 600pv)	23 88
72192A	1.21	2N4037	0.40 0.16	AD143 AD149V	0.45	BC303 0.54 BFS9	8 0.28	MJ440 0.71 MJ480 0.75	IN1186 (35A	A 200pv)	£1.57			
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2195	0.87	2N4062	0·11 0·25	AD161 } AD162 }	1.05	BC308A 0-09 BFX2 BC308B 0-09 BFX3	0.25	MJ802 4-12 MJ901 2-65	IN914	10p BAI 7p BAI	142 17p	BYZ10	35p OA81	
2195A 2218A	0.86	2N4302 2N4303	0.47	AF109R	0.40 0.25	BC309 0-10 BFX:	37 0-30	MJ1001 2-34 MJ1800 1-88	1N916 AA119	7p BA1	145 17p	BYZ11 BYZ12	32p OA85 30p OA90	
12219 12219A	0.57 0.86	2N4916	0·20 0·17	AF114 AF115	0.24	BC309B 0-10 BFX	63 2-48	MJ2500 2-92	AA129	15p BA	154 12p	OA9 OA10	10p OA91 20p OA95	
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12368 12369	0.31 0.37	2N4923	0.83 0.12	AF125	0-20 0-19	BCY32 1-15 BFX	89 0-45	MJE340 0-47 MJE370 0-73	OPTOE	LECTRO	NICS		NTIOMETER	ıs
12369 A 12646	0.41	2N5174	0.22	AF127	0.20 0.38	BCY34 0-35 BFY	11 0-45	MJE371 0-80	INDICATO	N 3015F 7- OR (16 PIN	[)[L) £2.	Log. or L	in., less switch, 1	7 jp.
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