

## ThisG6iristmas

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Our January issue will be published on Friday, December 14, 1973

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155
156
158 $\begin{array}{cc}\text { Votts) } & \text { lb } \\ 20 & 1 \\ 60 & 3 \\ 100 & 5 \\ 200 & 8 \\ 250 & 13 \\ 350 & 15 \\ 500 & 19 \\ 750 & 29 \\ 000 & 38 \\ 2000 & 60\end{array}$ $\begin{array}{cc}i b & 0 z \\ 1 & 8 \\ 3 & 12 \\ 5 & 8 \\ 8 & 0 \\ 13 & 12 \\ 15 & 0 \\ 19 & 8 \\ 29 & 0 \\ 38 & 0 \\ 60 & 0\end{array}$ 7.0
9.9
9.9 $\times$
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2
2 $\begin{array}{r}6.0 \\ \times 7.7 \\ \times 8.9 \\ 9.3 \\ \times 11.6 \\ \times 13 . \\ \times 14 \\ \times 16 \\ \times 15 \\ \hline 15\end{array}$
AUTO TA

| Ref. | VA | Weight | AUTO TRA Size cm. | $\begin{aligned} & \text { SFOMMERS } \\ & \text { Auto TODS } \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No | (Wot | 15 or |  |  | C | P |
| 113 | 20 | 10 | $5.8 \times 5.1 \times 4.5$ | 0-115-210-240 | 1.02 | 22 |
| 64 | 75 | 2 | $7.0 \times 6.7 \times 6.1$ | 0-115-210-240 | 2.00 | 30 |
| 4 | 150 | 34 | $8.9 \times 7.7 \times 7.7$ | 0-115-200-220-240 | 2.42 | 36 |
| 66 | 300 | 64 | $9.9 \times 9.6 \times 8.6$ | , , | 4.70 | 52 |
| 67 | 500 | 128 | $12.1 \times 11.2 \times 10.2$ | ., ., | 6.98 | 67 |
| 84 | 1000 | 198 | $14.0 \times 13.4 \times 14.3$ | ., ., | 12.69 | 82 |
| 93 | 1500 | 304 | $14.0 \times 15.9 \times 14.3$ | ., .. | 18.39 |  |
| 95 | 2000 | 320 | $17.2 \times 16.6 \times 14.0$ | ., .' | 24.00 | , |
| 73 | 3000 | 400 | $21.6 \times 13.4 \times 18.1$ |  | 32.67 |  |

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 115500 W enclosed transformer, with mains lead and two 115 Voutlet sockets, $69.49, \mathrm{P} \& \mathrm{P} 67 \mathrm{p}$. 20 W version, $62.02, \mathrm{P}$ \& P 22 p . LOW VOLTAGE SERIES (ISOLATED) PRIMARY 200-250
Ref, Amps, Weigh
No, 12 V 24 V ib oz No. $\begin{array}{lllll}1 & 0.5 & 0.25 & B^{2} & 4.8 \\ 3 & 1.0 & 0.5 & 4\end{array}$ $4.8 \times 2.9$
$6.1 \times 5$
$7.0 \times 6$
$8.3 \times 7$
$8.9 \times 8$
$9.9 \times 8$
$9.9 \times 8$
$9.9 \times 10$
$12.1 \times 8$
$14.0 \times 9.6$
$14.0 \times 12.1$
cm.
$\times 3$
$\times 4$
$\times 4$
$7 \times$
0
0
$9 \times 8$
$6 \times 8$
$2 \times 8$
$9 \times 10$
$6 \times 11$


MINIATURE TRANSFORMERS WITH SEREENS
$\begin{array}{lll}16 & & \text { lb } \\ 18 & 200 & \\ 2 & 1 A, 1 A & \\ 3 & 100 & \\ 35 & 330,330 & \\ 07 & 500,500 & \\ 08 & 1 A, 1 A & 1 \\ 36 & 200,200 & \\ 14 & 300,300 & 1 \\ 21 & 700 \text { (d, c.) } & 1 \\ 06 & 1 A, 1 A & 2 \\ 03 & 500,500 & 2\end{array}$ $2.8 \times 2.6 \times 2.0 \quad 3-0.3$ $\begin{array}{ll}6.1 \times 5.8 \times 4.8 & 0.6 .0 .6 \\ 3.9 \times 2.6 \times 2.9 & 9.0 .9\end{array}$ $\begin{array}{lll}4.8 \times 2.9 \times 3.5 & 0.9 .0 .9\end{array}$ $0061 \times 5.4 \times 4.8 \quad 0-8.9 .0 .8 .9$ $\begin{array}{lll}7.0 \times 6.4 \times 6.1 & 0.89 .0 .8-9 \\ 4.8 \times 2.9 \times 3.5 & 0.150 .15\end{array}$ $\begin{array}{lll}4.8 \times 2.9 \times 3.5 & 0.15,0.15 \\ 6.1 \times 5.8 \times 4.8 & 0.20 & 0.20\end{array}$ $\begin{array}{ll}6.1 \times 5.8 \times 4.8 & 0-20,0-20 \\ 70 \times 6.1 \times 6.1 & 20-12-0.12-20\end{array}$ $\begin{array}{lll}8.3 \times 7.7 \times 7.0 & 0.15-20.0-15-20 \\ 8.3 \times 7.0 \times 7.0 & 0.15 .27 & 0.15\end{array}$ $8.3 \times 7.0 \times 7.0$
$8.9 \times 7.7 \times 7.7$ $0.15-27,0.15-27$
$0.15-27,0.15-27$

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| ACl2j | 19 | ADT140 | 55 |
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| ACl27 | 20 | AFI15 | 27 |
| $\mathrm{ACl}^{28}$ | 80 | AF116 | 27 |
| AC132 | 18 | AF117 | 27 |
| AC134 | 16 | AF118 | 矿 |
| AC137 | 18 | AF124 | 33 |
| AC141 | 20 | AF125 | 33 |
| AC141K | 82 | AF126 | 31 |
| ACl 42 | 20 | AF127 | 31 |
| AC142K | 28 | AF139 | 33 |
| $\mathrm{ACl}^{51}$ | 17 | AF138 | 55 |
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| ACl05 | 22 | AF180 | 35 |
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| AC167 | 22 | Ali03 | 2 |
| AC168 | 27 | ASY 26 | , |
| AC16.4 | 16 | AgY2 ${ }^{\text {a }}$ | 38 |
| AC176 | 22 | Asy 28 | 28 |
| AC177 | 27 | A8Y 29 | 28 |
| AC178 | 81 | ASY50 | 28 |
| AC178 | 31 | A8Y51 | 88 |
| AC180 | 28 | ABY 62 |  |
| AC180K | 82 | A8Y54 | 88 |
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| AC181K | 32 | A8Y56 | 88 |
| AC187 | 24 | ASY57 | 28 |
| AC187K | 25 | A9Y58 | 88 |
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| ACY22 | 18 | EC115 | \% |
| ACY27 | 20 | BC116 | 17 |
| ACY28 | 21 | BC117 | 20 |
| ACY29 | 39 | BC118 | 11 |
| ACY30 | 31 | BC119 | 38 |
| ACY ${ }^{1}$ | 31 | BC120 | 8 |
| ACY34 | 23 | HC125 | 18 |
| ACY 35 | 23 | BC126 | 80 |
| ACY38 | 31 | BC132 | 13 |
| ACY40 | 19 | BC134 | 80 |
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| AD130 | 42 | BC137 | 17 |
| AD140 | ${ }^{3}$ | ${ }^{\mathrm{BCl} 39}$ | 44 |
| AD142 | 58 | ${ }_{\text {BC141 }}$ | 33 |
| AD143 | 42 | BC142 | 33 |
| AD149 | 55 | BC143 | 33 |


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| :---: | :---: | :---: | :---: |
| HC140 | 50 | HDifio | ${ }^{68}$ |
| RC147 | 11 | BD116 | 88 |
| BC148 | 11 | BD121 | 68 |
| BC149 | 13 | HD123 | 78 |
| нC100 | 20 | BD124 | 76 |
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| BClis? | 19 | BD132 |  |
| BC153 | 31 | BD133 | 72 |
| BC154 | 33 | BD130̆ | 4 |
| BC197 | 20 | BD136 | 44 |
| BC158 | 13 | BD137 | 50 |
| 3C159 | 13 | BD138 | 55 |
| BC160 | 50 | RD139 |  |
| BC161 | 56 | BD140 | ${ }^{66}$ |
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| BC168 | 13 | BD175 | 86 |
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| 13 C 172 | 18 | BD179 | 77 |
| BC173 | 16 | BD180 |  |
| 13 C 174 | 18 | BD185 |  |
| BC175 | 24 | HD186 | 72 |
| BC17 | 21 | BD187 | 77 |
| BC178 | 21 | BD188 |  |
| BC179 | 21 | BD189 | 8 |
| BC180 | 27 | BD190 | 88 |
| BC181 | 27 | BD195 |  |
| BC182 | 11 | BD196 | 4 |
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| BC209 | 18 | HF115 | 27 |
| BC212L | 12 | BF117 | 80 |
| BC213L, | 12 | BF118 | 77 |
| BC214L | 16 | BF119 | 77 |
| BC225 | 28 | BF121 |  |
| BC226 | 39 | BF123 | 55 |
| BC301 | 30 | BF125 |  |
| BC302 | 27 | BF127 | ${ }^{65}$ |
| BC303 | 36 | HF152 |  |
| BC304 | 40 | BF153 |  |
| BC440 | 34 | BF164 | 50 |
| BC460 | 40 | BF155 |  |
| BCY30 | 27 | BFlut | 53 |
| BCY3] | 29 | BF157 | ${ }^{61}$ |
| BCY32 | 33 | BF158 |  |
| BCY 33 | 24 | BF159 | 66 |
| BCY34 | 28 | BF160 |  |
| BCY 70 | 16 | BF162 | 4 |
| BCY71 | 22 | HF163 | 44 |
| BCYT2 | 16 | BF164 |  |
| 13CZ 10 | 22 | BF165 | 4 |
| BCZ11 | 28 | BF167 | 24 |
| BCZ12 | 28 | BF173 | 24 |


| Type ${ }_{\text {BF17 }}$ | 39 |
| :---: | :---: |
| bFipt | 39 |
| BF178 | 33 |
| BF179 | 33 |
| BF180 | 33 |
| BF181 | 38 |
| BF182 | 4 |
| BF183 | 44 |
| BF184 |  |
| 13F18í | 38 |
| BF187 |  |
| BF188 | 44 |
| BFi94 |  |
| BF195 | 13 |
| BF 196 | 18 |
| BF197 | 16 |
| BF200 |  |
| BF222 | 21.05 |
| 8 F 25 ¢ | 50 |
| BF258 | 6 |
| BF259 |  |
| BF262 | 81 |
| BF263 | 81 |
| BF270 | 38 |
| BF271 |  |
| BF272 | 88 |
| BF273 |  |
| BF274 | 39 |
| BFW 10 |  |
| BFX29 | 30 |
| BFX84 | 24 |
| BFX85 | 33 |
| BFX86 | 24 |
| BFX 87 | 27 |
| BFX88 |  |
| BFY 50 | 22 |
| BFY51 | 22 |
| BFY ${ }^{\text {a }}$ ? | 8 |
| BFY53 | 19 |
| BPX 25 | 94 |
| BSX 19 |  |
| B8X 20 | 17 |
| BEY2\% | 17 |
| BSY 26 |  |
| BSY27 | 17 |
| BSY28 | 17 |
| BEY 29 |  |
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| H8Y39 | 20 |
| BSY 40 | 31 |
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C44:


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28
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2 N 3010
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18 TODES ATD BECTIFIERS

| AA119 | 0.09 | HY 114 | 0.13 | BYZ18 | 30 |
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| AA120 | 0.09 | BY126 | 0.18 | BYZ19 | 0.81 |
| A 4129 | 0.09 | BY127 | 0.17 | CG62 |  |
| AAY30 | 0.10 | BY128 | 0.17 | (0A91 Eq.) 0.06 |  |
| AAZ13 | 0.11 | BY130 | 0.18 |  |  |
| BA100 | 0.11 | BY133 | 0.23 | CG651- |  |
| BA116 | 0.23 | BY1ti4 | 0.55 | (0.470-0A79) |  |
| H:126 | 0.24 | BYX3 | 0 |  | 0.07 |
| 13, 148 | 0.16 |  | 0.48 | OAs | 0.39 |
| HAl54 | 0.13 | $13 Y Z 10$ | 0.89 | OA5sL | 0.28 |
| HA155 | 0.18 | BYZ11 | 0.83 | 0 O10 | 0.38 |
| HAlof | 0.16 | BYZ12 | 0.38 | 0.475 | 0.08 |
| BY100 | 0.17 | BYZ13 | 0.28 | OA70 | 0.08 |
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|  | TYPE, Tu | e $16 \mathrm{~m} / \mathrm{n}$ | 1.87 |
| GR116 | Side Viewin | g NIXI |  |
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## ROTARY SWITCHES

Radiospares Miniature Maka-switch (in assembly kit BBMIPI2W. $2 \mathrm{P} 6 \mathrm{~W}, 3 \mathrm{P} 4 \mathrm{~W}, 4 \mathrm{P} 3 \mathrm{~W}, 6 \mathrm{P} 2 \mathrm{~W}, 32 \mathrm{p}$ each

## WAYECHANGE SWITCHES

P12W, 2P6W, 3P4W, 413W, 24p each

## ELECTROLYTIC CAPACITORS

 Capacity $\mu \mathrm{F}$| $\mathrm{Capacity}_{0.47} \mu \mathrm{~F}$ | - | - | - | - |  | - | 10p | 7p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.0 | - |  |  | - |  | 10 p |  | 7p |
| $2 \cdot 2$ | - | - | - | $\square$ | 10p | - | $7 p$ | 8 p |
| 4.7 | - | - | - | 10p | - | 7p | Bp | $7 p$ |
| 10 | 二 | - | 7 | 7 | 7p | 8 p | Tp | $8 \mathrm{8p}$ |
| 22 | 7 | - | 7p | 7p | - | $7 p$ | $7 p$ | 9p |
| 47 | 7p | 7 | 8p | 8 p | 8 p | $7 p$ | Pp | 12p |
| 100 | $8 \mathrm{8p}$ | $7 p$ | 7p | 7 p | 7p | $9 p$ | $117 p$ | 19p |
| 220 | 7p | 8p | 8 p | 8 p | 9 p | 10p | 17p | 27p |
| 470 | 8p | 9 p | 9p | l0p | 12p | 17p | 24p | 43p |
| 1.000 | 10p | 12p | 12p | 17p | 20p | 24p | 40p |  |
| 2.200 | 14 p | 17p | 22p | 25p | 36p | 40p | - | - |
| 4,700 | 25p | 28p | 37p | 41p | 54p | - | - | - |
| 10,000 | 40p | 43p |  |  |  |  | - | - |

POLYCAREONATE- $5 \%$ 250 V UP to $0.1 \mu \mathrm{~F}: 100 \mathrm{~V}, 0.1 \mu \mathrm{~F}$ and $0.01 ; 0.012 ; 0.015 ; 0.018 ; 0.022$ 0.027: 0.033; 0.047; 0.056; 4p each. $0.068 ; 0.082 ; 0.1 ; 0.12 ; 0.15 ; 4 p$ each. $0.18 ; 0.22 ; 5 p$ each. $0-27$; $0.33 ; 6 p .0 .39$ 7p. 0.47 8p. 0.56 10p. $0.68 \mathrm{IIp} .1 \mu \mathrm{~F} 13 \mathrm{p}$. Prices subject to amendment by the manufacturer
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Decoder driver type FLL
I21T nett $\mathbf{C 1} \cdot \mathbf{3 6}$. DIL socket, nett $\mathrm{E2}$.

## RESISTORS - $10 \%$, 5\%, 2\%

| Code | Power | Tolerance | Range | Values | 1 to 9 | $10 \text { to } 99$ | 00 up |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C | 1/20W | $5 \%$ | 82@-220Kc | available ${ }_{\text {E12 }}$ | 9 | (see note below) | 7.5 |
| ${ }^{\circ}$ | 1/8W | 5\% | $4.7 \mathrm{n}-470 \mathrm{Kf}$ | E24 | ? | ${ }_{0}^{6} 9$ | 0.75 nett |
| C | 1/4W | $5 \%$ | $4.7 \Omega-10 \mathrm{M} \Omega$ | E12 | 1 | 0.9 | 0.75 nett |
| C | 1/2W | 5\% | $47 n-10 M n$ | E24 | $1 \cdot 2$ | 1 | 0.95 nett |
| C | IW | $5 \%$ | $4.7 n-10 M \Omega$ | E12 | $2 \cdot 5$ | 2 | 1.6 nett |
| MO | 1/2W | 2\% | 10n-1Ma | E24 | 4 | 3 | 2 nett |
| WW | IW | 10\% $\pm 1 / 20 n$ | $0 \cdot 22 \Omega-3.9 \Omega$ | E12 | 7 | 7 | 6 |
| WW | 3W | 5\% | $1 \mathrm{n}-10 \mathrm{~K} \mathrm{n}^{\text {a }}$ | El2 | 7 | 7 | 6 |
| WW | 7W | 5\% | $1 \Omega-10 \mathrm{~K} \Omega$ | El2 | 9 | 9 | 8 |

Codes: $C=$ carbon film, high stability, low noise.
$M O=$ metal oxide, Electrosil TR5, ultra low noise. $W W=$ wire wound, Plessey.
El 2 denotes seri
and their decades
and their decades.
E24 denotes series: as E12 plus $11,13,16,20,24,30,36,43,51$
62. 75. 91 and their decades.

KNOBS -see Caralogue Nor orher types 38p; F. 12 ( 33 mm ) pack of $2,40 \mathrm{p} ; \mathrm{F} .19$ (20mm) pack of $2,32 \mathrm{p}$; F. 18 ( 26 mm ) pack of $2,38 \mathrm{p} ; \mathrm{F} .17(33 \mathrm{~mm})$ pack of 2, 40p; KB. 4 ( 20 mm ) pack of 4, 40p; K30/3 ( 17 mm ) aluminium, 24p each.


KB4

$\times 30$

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$\begin{array}{ll}100,000 & \text { O．P．V．} \\ \text { Byin scale } \\ \text { buzzer }\end{array}$
short circuit check．
Sensitivity： 100,000
OPV d．c．5／Volt a．c．
D．c．volts： $0.5,2.5$ ，
$10,50,250,1,000 \mathrm{~V}$ ．

$50,250,500,1,000 \mathrm{~V}$ ．D．c．current： 10 ， $100 \mu \mathrm{~A}, 10,100,500 \mathrm{~mA}, 2 \cdot 5,10 \mathrm{~A}$ ．Resistance： $1 \mathrm{~K}, 10 \mathrm{~K}, 100 \mathrm{~K}, 10 \mathrm{meg}$ ． 100 meg ．Decibels： handle，aize 7 in $\times 6$ in $\times 3$ in．sig．05． hande，ilz
P．\＆P． 25 p ．
$240^{\circ}$ Wide Angle Ima

## Meters

MWI－6 60 mm square ts．97 MW1－8 80 mm aqua



## 200 band 20 0 2 2 2 8 new t

bands．Square：
$20 \mathrm{c} / \mathrm{s}$ to $30 \mathrm{kc} / \mathrm{s}$
Outp Output imped－ ance 5,000 ohma． Supplied brand new and guaran－

teed with instruc－
tion manual and leads．217．50．Carr． 37 p ． ARP－800 AP／RF SIGAAL GESLERATOR pact，fully portsble， AF pact，fully portable．AF
sine wave 18 Hz to 220 KHz ．AF square wave
18 Hz to 100 KHz ．Out－ put aine／square $10 \%$ ． P－P．RF 100 KHz to 200 MHz ．Output 1 v ． maximum．Operation
$220 / 240 \mathrm{v}$ ．AC．Complete $220 / 240 \mathrm{v}$ ．AC．Complete leads． 29.95 ．Post 50p．


MODEL AT201 DECADE ATHENDATOR Frequency
$0-200 \mathrm{kHz}$ ． 0－200k Hz．

## Attenuator0 0111 dB ，



Impedance 600 $=-2$ ohms．Max．Input power 30 dBm ． 81 ize $180 \mathrm{~mm} \times 90 \mathrm{~m}$
812.50 ．Post 37 p.

BELCO AP－5A SOLID STATE SINE BQUABE WAVE C．R．OSCHLATOR Square $\quad 18-50,000$ Hz ．Output max． +10 dB （ 10 K ohms） Operation internal batteries．Attrac－
tive 2 －tone came $71 \mathrm{in} \times 5 \mathrm{ln} \times 2 \mathrm{in}$ ．


TE－40 HIGH 8ENBEIVITT A．0．VOLTMETER
10 meg．Input 10 ranges： $01 / \cdot 003 / \cdot 1 / 3 / 1 / 3 / 10 / 30 / 100 /$
300V．R．M．S． 300 V ．R．M．S． $4 \mathrm{cps} .-1-2 \mathrm{Mc/g}$.
Decibels -40 to +50 dB. supplied brand new complete Operation 230 V ．a．c． 817.60 ． Carr．25p．
TME MODEL 117 F．E．T．ELECTRONIC VOLTMETER
Battery－operated，Il
meg input． 26 ranges． meg input．mirror scale． Bize $5 \frac{1}{2} \times 41$ in $\times 2 \ln$ ． D．c．volta $0.3-1,200 \mathrm{~V}$ ． $\begin{array}{ll}\text { A．c．volta 3－300V R．M．8．} \\ 8.0-800 \mathrm{~V} & \text { P－P．} \\ \text { D．c．}\end{array}$ Current 0．12－12MA．Re－

sistance up to $2,000 \mathrm{~m}$ ohm．Decibels -20 to ＋5ldB．Complete with leads／instructions． 817－50．P．\＆P．20p．
190DEL 449A IR CIRCDIT TRATBIS－ TOR TESTER
Checks true a．c bets
in／out．Checks Icbo． Checks diodes in／out． $\begin{array}{ll}\text { Checks SCR，} \\ \text { Bets HI } & \text { etc．} \\ \text { B－} 500 & \text { LO }\end{array}$ Bets HI 10－500 LO
$2-50$ Ibco $0.5000 \mu \mathrm{~A}$ ． 220／240V a．c．operation．217．50．Post 25p EAMODEN HMG－500 IRSULATIOM R乏 SISTAMCE TESTER
Rang e $0-1,000$
Megohms， 500 Volt． Batter $\bar{y}$ operated． Wide range clear
 luxe carrying case， \＄19．05．Post 30p．

MODEL T4811 SUB－ETANDARD
MULTI－RAIGE VOLT ANIETMR Sensitivity 330 obms／ Volt a．c．and d．c．Accur－
acy $0.5 \%$ d．c． $1 \%$ a．c acy $0.5 \%$ d．c． $1 \%$
Scale length 165 mm ． $0 / 300 / 750 \mu \mathrm{~A} / 1 \cdot 5 / 3 / 7 \cdot \mathrm{~B}$ 15／30／75／150／300／
$750 \mathrm{~mA} / 1 \cdot 5 / 3 / 7 \cdot 5 \mathrm{am}$ d．c． $0 / 3 / 7-5 / 15 / 30 / 75 / 150 /$ $300 / 750 \mathrm{~mA} / 1 \cdot 6 / 3 / 75$ amp．a．c． $0 / 75 / 150 / 300 /$ $750 \mathrm{mv} / 1 \cdot 5 / 3 / 7 \cdot 5 \cdot 15 \cdot 30 /$ $75 / 150 / 300 / 750 \mathrm{~V}$ d．c．o／ $75 / 150 / 300 / 750 \mathrm{~V}$／
Automatic cut out．Supplied compicte with 80．Post 50 p ．

## MCA， 280 AUTOMATIC

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## GABLISER

$176-250 \mathrm{~V}^{88-125}$ a．c．A．c．output 120 V
$\frac{\text { rating．s11－97．Post 50p．}}{\text { PS．} 800 \text { REGULATED P．S．U }}$
Solid state．Variable output S－20V d．c．up to 2 amp．
Independent meters to
monitor voltage and cur－
rent．Output $220 / 240 \mathrm{~V}$ ．
a．c．Size $7 t i n . \times 51 \mathrm{in}$ ． X
3 Hin ． 219.95 ．Post 25 p ． P8．100B REGULATED POWER SUPPLY
Bolid state．Output 6， 9 or 12 V d．c．up to 3
or
amps．Meter to nionitor current．Input $220 / 240 \mathrm{~V}$ a．c．Size 4 in ．$\times 34 \mathrm{in}$ ．$\times$
Btin．E11． 97 ．Post 25 p ．


 +62 dB ． 24.95 ．Post 15 p ． CI－5 PULSE OSCILLO SCOPE For display of pulsed and periodic wavelorms in electronic circuita VERT AMP．Bandwidth 10 MHz ．
Sensitivity at 100 kHz Sensitivity at 100 kHz
$V$ RMS $/ \mathrm{mm}$ ． $0 \cdot 1-2 \overline{5} ;$ HOR．AMP．Bandwidth $\begin{array}{ll}100 \mathrm{kHz} & V \quad R M 8 / \mathrm{mm} .\end{array}$
 0．3－25；Pre－set triggered sweep 1－3，000 $\mu$ sec．： free running $20-200,000 \mathrm{Jz}$ in nine ranges． Calibrator pips． $220 \mathrm{~mm} \times 360 \mathrm{~mm} x$ $430 \mathrm{~mm}, 11$ o－230 a．c．operation． 889．Carr．paid．

TO－3 PORTABLE OSOHLLOSCOPE Bin tube，Y atnp．Sensitivity $0 \cdot 1 \mathrm{~V}$ p－p／CM．Bandwidth
$1 \cdot$ ops－1．5MHz．Input Imp． 2 mes $\AA 25 \mathrm{pF} \mathrm{X}$ amp．
sensitivity 0.9 V ． $\mathrm{p}-\mathrm{p} / \mathrm{CM}$ ． sensitivity 0.9 V ．p－p／CM．
Bandwidth $1.5 \mathrm{cps}-800 \mathrm{kHz}$ ． Input imp 2 nieg 20 pF ． Input imp． 2 meg $\Omega 20 \mathrm{pF}$ ． 300 kHz ．Synchronisation． Internal／external．Hluminated senfe 140 mm $\times 215 \mathrm{~mm} \times 330 \mathrm{~mm}$ ．Weight $15 \frac{1}{2 l b} .220 /$ book．E58．50．Carr． 50 p ．

| BUSELAN CL－16 DO OSCLLLOSC |
| :---: |
| $5 \mathrm{MHz} \mathrm{Pass} \mathrm{Band}. \mathrm{Sep-}$ |
| arate Y1 and Y2 |
| amplifiers．Rectangular |
| $\overline{\operatorname{Lin} \times 4} \times 4 \mathrm{n}$ C．R．T．Calb - |
| brated triggered sweep |
| from $0.2 \mu / \mathrm{sec}$ to 100 |
| inilli－sec per cmi．Free running tine base 50 |
| Hz－1MHz．Built－in |
| time base callibrator and |
| amplitude calibrator． |
| Supplied complete with |
| all accessories and ins |
| 287．Carr．paid． |
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High quality ceramic construc tion．Windinga embedded in vitreous ensmel．Heavy duty brush wiper．Continuous rat－ ing．Wide range available tin dia．ghafts．Bulk fuxing，
\＆5 WATP．10／25／50／100／250／500／1000 ohme 21．15．P．\＆P．10p．
50 WATT．10／25／50／100／250／500／1000／2500 or 5000 ohms．41．62．P．\＆P．10p
100 WATT， $1 \cdot 5 / 10 / 25 / 50 / 100 / 250 / 500 / 1000$ or 2500 оһme．22．84，P．\＆P．15p

${ }^{230}{ }_{50}$ VOLT A．C． RELAYS Brand new． 3 sets of
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$100 \mathrm{~mm} \times 80 \mathrm{~mm}$ Fronta | 50 |
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## 50 50 100

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$0-0-50 \mu \mathrm{~A} \cdots$

00-0-100 11 A .

$50-0 \cdot 50 \mu \mathrm{~A} \ldots$
$100 \mu \mathrm{~A} \ldots$
$100 \cdot \mathrm{~A} \cdot 100 \mu \mathrm{~A}$
$200 \mu \mathrm{~A} . \ldots$.
$500 \mu \mathrm{~A} . . . .$.

200
500
1 m

## 10

- 10
100 mA
500 mA
Type MR.45P. 21





EA. 41 REVERBERATION AMPLIFIER Self contained, tran-
sistorised. batery
operated. Simply operated. Simply
plug in microphone,
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Folume conirol, put into your amplifier. Folmme conlrol,
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AUDIOTRONIC AHAIOI STEREO HEADPHONE AMPLIFIER


All silicon trandistor amplifier operates from
magnetic ceramic or magnetic ceramic or atereo headphone out-
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OUR
PRICE E E E
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| DIGITAL CLOCK MECHANISM DT.55B <br> Features 24 hour alarm setting with built in buzzer. <br> On/off and auto <br> alarm "sleep" switch. <br> Automatically turns of TV, radio, jight, etc. and with autosetting will awitch on again when required. A.c. 240 V operation. Switch rating 2505, OUR \& E O P P.\&P. 3A. PRICECH +3 30p |
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[^2]
## 



4 bands covering $550 \mathrm{kHz}-30 \mathrm{MHz}$ pread on $10,15,20,40$ and 80 metres. \& valve plus 7 diode circult. $4 / 8 \mathrm{ohm}$ out put and phone sFE. 88B-CW. ANL fariable liol IF meter. sep. banispread hal. 1 irequency 1.5 w , F gain controls $115 / 250 \mathrm{y}$ a ive: 7 in $\times 13 \mathrm{in} \times 10 \mathrm{in}$ wit nstruction manual.
OUR ㅇ, 4. - 9 Carr PRICE 544 Pald
FULL RANGE OF TRIO STOCKED

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4 Bend covering $550 \mathrm{kHz}-30 \mathrm{MHz}$, GB, Beter. Variable BFO fo pread Nultin Bpeaker. Band 40 V ...c. or 12 V d.c. $121 \times 48 \mathrm{in}$


UNR 30 RECEIVER


Bands covering $050 \mathrm{kHz}-30 \mathrm{MHz}$ BFO Bullt-in Speaker $220 / 240 y$


## TRIO JR3IO SSB

RECEIVER


Covers $3 \cdot 5,7,14,2 \mathrm{I}, 28.28 \cdot 0 \mathrm{an}$ 15 MHz gas and and WW output tuore than 1 W controlleci BFO for $88 B$ Crysta ANL etc A C $110 / 100-300 / 040 \mathrm{~V}$ Bize $330 \times 179 \times 310 \mathrm{~mm}$.



High quallty Ts5ly ssB/CW amateur band receiver dovering 80, 40, 20, 15 and 10 metre bands with PSois power rupply and frequency $3 \cdot \bar{u}-29 \cdot 7 \mathrm{MHz}$. Output 1-6W. Power requirements 110 $120 / 220-240 \mathrm{~V}$ a.c
$\begin{array}{lll}\text { OUR } \\ \text { PRICE } & \text { C210.00 } & \text { Carr. } \\ \text { Paid }\end{array}$
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Solid state mobile tranaceiver for 12V d.c. neg. use. Tranamita and Receives on any $1: 2$ of 28 channels hetween 144 and 146 MHz , Power
output 10 W and 1 W awitchable. Controls: Volume/on/off, squelch. channel aelector. Internal 3in apeaker. Complete with dynamic mike. PTT switch, three sets of $\begin{array}{ll}\text { crystals } \\ 144.60 \mathrm{MHz} & \text { for } 145 \cdot 00 \mathrm{mHz} \\ 148 \mathrm{MHz} \text {, }\end{array}$ $144 \cdot 60 \mathrm{mHz}, \quad 145.00 \mathrm{mHz}$, mount-
$\underset{\text { price }}{\text { OUR }}$


General coverage $150-400 \mathrm{kHz}$, $550 \mathrm{kHz}-30 \mathrm{MHz}$. FET front end, 2 mech. Blters, product detector,
variable BFO, noise limiter, $\$$ Meter Bandspreall. RF Gain. $16 \mathrm{in} \times 92$ in $\times 8 \mathrm{in}^{2} .18$ ib. 220 f 240 V a.c. or 12 V d.c. Brand new
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## AUDIOTRONIC AHP8A 8 TRACK

 stereo tape player Incorporatea fiere giving 2
elector, illu
minated track indicatory. slider controls for volume, balance and tone. Attractive cabinet with black and silver trim. Output




## fifered at a

how price. Incorporate hoat of features including switch tape selector, twin VU meter ilder record/playback level con trols, front panel headphone socket, recording indicator lamp, phono/Din line input Bockets, .5 mm mike input socketa, etc tt. Frequency response 100 $8 \mathrm{kHz}(100-12 \mathrm{kHz}$ CrO2). \$/5 -45 dB . eparation - 3.5dB. Noiae limiter -6 dl at 10 kHz . Complete with connecting leals.



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## Mat coned paif of compac

bookaheit spea
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orating 2 in
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ance. 10 watts power handing. Size $345 \times 228 \times 110 \mathrm{~mm}$
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Manual tuning of Mediuin Long waves. 12 V pos. or neg earth. Complete with speaker,
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12 V neg. earth. Slider controls for Volume, Tone and Balance. Channel selector button with pilot ismp. With speakers, mounting

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ready to fit into cabinet. Output 125 mV A.C. 240 V . Overall size approx. $185 \times 215 \times 80 \mathrm{~mm}$.
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## 6

UDSPEAKERS Model 350. $13 \mathrm{in} \times$ in with single tweeter
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3 in $\times 31 \mathrm{in}$.


AUDIOTRONIC AMR-9000 GLOBAL AM/FM PORTABLE 10 wavebands
 (O) aty
 s.W.1.: $4 \cdot 0 \cdot \mathrm{o} \cdot \mathrm{omHz}$ : S.W.2: $8.0-1 \cdot 6 \mathrm{MHz}$ :
8.W.3: $16-24 \mathrm{MHz}$ : P.8.B. $1: 30-50 \mathrm{MHz}$ :
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174 MHz ; F.M. $88-108 \mathrm{MHz}$; A.I.R.: $108 \cdot 136 \mathrm{MHz}$. Features time zone map and timing diai. Large clear in aerial. A F.C. on F.M. fin $x$ 4 in spesker and personal bin $x$ Battery/mains operation. Slze $345 \times 133 \times 305 \mathrm{~mm}$. OUR P


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AUDIOTRONIC AM/FM PORTABLE RADIO AR3000 4 wavebands cover MW FM $87-1005 \mathrm{KHz}$, LW $145-285 \mathrm{KHz}$, gW
Push button wave change plus AFC nd on/oft. Thumb Adder volume and theel tuning Earphone socke guilt controls. telescopic aerisls Car aerial ocket. Battery/Maing operation
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AUDIOTRONIC DIGITAL CLOCK/ AM-FM RADIO ADC. I
 Covers AM $540-1800 \mathrm{KHz}^{\mathrm{CH}}$. FM $88-108 \mathrm{MHz}$ with AFC. 24 hour leal type digital clock with one minute division time change setting. Wake up to the sound of music or toud buzzer. Unlque sleep switch will automatically turn off radio when you have gone to sleep. Slider volume control Internal speaker plus socket for earpiece or pillow spearer. A.c 240 V . 8lze $254 \times 92 \times 178 \mathrm{~mm}$ Complete with earpiece, and operOUR
PRICE
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TE1018 DE-LUXE MONO HIGH IMPEDANCE HEADSET到ensitive magnetic carpads.
ance
2,600 ance $\quad 2,600$ ohmat
(d.c. 800 ohms). Frequency res
$200-4.000 \mathrm{~Hz}$.
 BH001 HEADSET AND
BOOM MICROPHONE
 Moving coil.
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impa imp. 16 ohme.
Mike imp. 200 ohms. Ideal teaching, come munications ete. Com
pluge. $\begin{array}{ll}\mathrm{OUR} \\ \mathrm{PRICE} & 84.95 \\ \text { P. } & \text { P. }\end{array}$ STEREOSOUND

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SUPER AKAI HI FI CASSETTE BARGAIN


CS35
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For conventional or Chromiurn Dioxide tape, 4 track recurd/
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MICROPHONES (P. \& P. JOp)
ADM Dynamic (pair)
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CASSETTE RECORDER Portable twin
track track
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With recording level
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Fast forward and rewind. Output 500mW: 220/240V a.c. or 6 V d.c.
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MP60/TPD1/ADC K8 MP60/M44-7. HT70/TPD1/G800 GOLDRING
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MP60/TPD2
HT70/G800
HT70/G800
HT70/TPD
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G101P/C
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Among the $\mathbf{2 4 0}$ pages of the famous HOME RADIO COMPONENTS Catalogue, are seven pages listing Resistors


## TWENTY-FIVE YEARS ON

THE 25th year of the transistor draws to its close. A quarter century of exciting and rapid technological growth justifiably referred to as a revolution, and unlikely to be paralleled within the seeable future.

In this issue appears a final article in our special series marking this anniversary of the dawn of the new solid state era. It is written, most fittingly, by a well known contributor and dwells on those now far off days when the transistor was still much of a curiosity and just beginning to cause an upheaval in constructor circles. Established methods of building clearly had to change, but it was far from clear just how.

Much water has flowed under the bridge since then . . . but those early experiments with transistors are worth recalling, though it will all sound very strange to a fair proportion of our readers since there is now a whole generation of constructors brought up entirely on semiconductors.

Yet even our younger post-valve-era readers are not denied the excitement of being involved in great changes in technology. Right at this present moment we are witnessing a " quiet revolution." With hindsight, we know that the discrete semiconductor device represented but the opening phase of this solid state revolution; the culminating achievement has been the creation of the integrated circuit.

So let us turn now from the past and consider what the future holds for the constructor. It will be a future dominated by the i.c., that is obvious. Until, of course, another spectacular discovery leads to the obsolescence of semiconductors-a development not entirely improbable but sufficiently remote in time to be left out of any sensible prognostications at this particular moment.

The i.c. is, in circuit terms, a very large building block and is tending to become even bigger, thanks to l.s.i. This type of device influences very considerably, if it does not dominate entirely, the general pattern of any design in which it is called upon to play a part.

In the future, the drift towards more custom designed i.c. 's may well limit the total number of new devices suitable for constructor applications. Yet amongst the balance there are bound to be an abundance of types than can be usefully employed by the amateur. In this respect, particularly noteworthy at the present time are phase-locked loops. These i.c.'s are beginning to mould the pattern of many equipment designs. They are opening up new fields and revolutionising some traditional designs, especially in the radio receiver area

Immediately following its introduction, the i.c. was thought by some to represent a threat to home construction activities. Such a pessimistic view has already been proved ill-founded. Looking ahead, there is no reason to suppose any drying up of individual enterprise and ability to extract the maximum advantage from monolithic devices yet to emerge from the microelectronics plants.

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F.E.b.


THIS stroboscope is designed primarily for use as a lighting effect for parties and discotheques. Its flashing rate is continuously variable from about 2 Hz to 20 Hz . It can be used-with limitations--for specialised photography but the output power (about half a joule) limits it to use with only medium to high speed black and white films at distances of a few feet. For discotheque work, however, it can be classified as of medium power.

## SOME WARNINGS

Those who intend building the equipment should be fully aware at the outset of their social responsibilities in the operation of such equipment; strobing in the frequency range of 10 to 20 Hz can, in some instances, produce hypnotic effects. Excessive use of the strobe should thus be avoided; however, if handled carefully and used in moderation some particularly pleasing lighting effects can be produced.

A further word of warning regarding the construction. Very high voltages are used to charge up high value capacitors -these can be lethal if mishandled. When testing it is not sufficient simply to switch off the power; the plug should be completely removed from the socket and all capacitors shorted out with an insulated handled screwdriver before any attempt is made to handle the circuitry.

## OPERATION

The principle of operation is quite simple. All we have to do is apply a high voltage across a Xenon gas filled tube from a reasonably high value capacitor. This voltage is arranged to be below the breakdown voltage of the tube so initially no electrical discharge takes place. At some pre-determined time a very high voltage pulse (at low current) is applied to a third electrode fixed to the outside
of the tube-this is called the trigger electrode-and we cause a localised electrical breakdown of the gas between the trigger and one of the primary electrodes. The gas in that locality becomes electrically conducting (or ionised), and the ions produced move rapidly throughout the length of the tube and cause main conduction between the primary electrodes.
For a fraction of a second the tube becomes a short circuit across the capacitor and the full charge held on the latter flows through the tube giving rise to the very bright short duration flash. As soon as the capacitor has fully discharged the tube is extinguished and a fraction of a second later the residual ions of gas revert to their non-conducting state and the tube once more becomes inert. The capacitor can now be recharged and a second trigger pulse applied for the next flash.

## FLASH ENERGY

The energy of the flash is measured in joules and is equivalent to the amount of electrical energy stored in the main capacitor (C4 in Fig. 1). This energy is calculated by using the formula:-

$$
\text { Energy }=\frac{1}{2} \mathrm{CV}^{2} \text { joules }
$$

where C is the value of the capacitor in farads and V is the voltage to which it is charged. In Fig. 1 C4 charges up through a half wave rectifier (D2) and limiting resistor, R3, direct from 250 V r.m.s. mains; this means the peak voltage on the capacitor when it is fully charged is about 350 V . The energy produced in each flash for the capacity used will be about $0 \cdot 48$ joules.

## LIMITED OUTPUT

Because of the tube rating, if it is flashed too often at too high an energy it will get extremely hot. The tube specified is made of hard glass that has a


Fig. 1. Circuit diagram of the Party Stroboscope. Note that the case is connected to mains earth
maximum dissipation of 10 watts. It is possible to obtain tubes having a high permitted dissipation but these are quite expensive, particularly those made from quartz.
We can calculate dissipation by multiplying flash energy by the maximum frequency of flashing, with the stroboscope this is $0.48 \times 20=9.6$ watts.
Since this represents nearly the limit of the tube, experimenters should not try to get more light output by increasing the value of C 4 without limiting the maximum flash rate proportionally.

Before describing the trigger system, which forms most of the circuitry, a word about R3. The value is reasonably important because it prevents the main capacitor charging before the discharge tube is completely de-ionised; at the same time it must be of low enough a value to ensure that C4 is fully charged before the next trigger pulse. Quite high peak currents flow through this resistor so it should be of at least 10 watts rating and even so will get quite warm in use.

## TRIGGER SYSTEM

To produce the trigger pulses there must be a timing circuit that is adjustable in the range from $\frac{1}{2}$ second to $\frac{1}{2}$ second. D1 and Cl form a simple auxiliary d.c. supply of about 350 V . C2 will charge up towards 350 V and the rate of charge is controlled by the value of R1 and VR1-as the latter is adjustable we can vary the charging rate. In actual fact the potential across C2 will never reach 350 V because as soon as it reaches about 25 V the diac D3 will start to conduct and any charge held on C2 is applied to the gate electrode of the thyristor.

As soon as C 2 is completely discharged the diac becomes non conducting and C2 is able to charge back up towards the 350 V . This is a repetitive cycle and the timing is controlled, as we have already said, by the time constant of C2 with the charging resistors but also by the differential between the breakdown voltage of the diac and the potential towards which C2 is charging. Different diacsparticularly the cheaper ones-may have slightly different breakdown voltages so there may be some
variance in timing between different assemblies. This can be compensated for in practice by increasing or decreasing the value of C2. Increase its value if you require a slower repetitive cycle and vice versa.

It is most important that you do not exceed a flash rate of 20 Hz because you might exceed the power rating of the tube.

## TURN ON

The discharge current from C2 through D3 into the gate of the thyristor causes the thyristor to turn on. C3 has been charged to 350 V through R2 and when the thyristor turns on this is discharged through the circuit C3, CSR1, and the primary of T1. The instantaneous current is quite high and the rate of change of flux in the primary of T 1 causes a very high voltage pulse across the secondary windings (approximately $7,000 \mathrm{~V}$ ). This pulse is fed to the trigger electrode of the discharge tube.

Component values have all been carefully chosen so that everything happens in the correct time sequence, e.g. C4 and C3 must be fully charged before the highest rate of trigger pulse is generated by C2 and the diac circuitry so do not use values other than those specified.

R4 is a bleed resistor across the main capacitor to ensure that when the unit is switched off any


The strobe unit with a panel removed showing the large paper capacitor (C4)

## COMPONENTS . . .

## Resistors

R1 $1 \mathrm{M} \Omega$
R2 $100 \mathrm{k} \Omega$
R3 $500 \Omega 10 \mathrm{~W}$ wirewound
R4 $100 \mathrm{k} \Omega 1 \mathrm{~W}$
All $10 \% \frac{1}{4} \mathrm{~W}$ except where otherwise stated

## Capacitors

C1 $8 \mu \mathrm{~F}$ elect. 500 V
C2 $2 \mu \mathrm{~F}$ elect. 200 V
C3 $0.1 \mu \mathrm{~F} 400 \mathrm{~V}$ polyester
C4 $8 \mu \mathrm{~F} 500 \mathrm{~V}$ paper

## Diodes

$$
\begin{array}{ll}
\text { D1-D2 } & \text { IN4001 (2 off) } \\
\text { D3 } & \text { ST2 Diac (G. W. Smith) }
\end{array}
$$

## Xenon Tube

LP1 Hivac ZFT2 (Townsend and Coates Ltd., Coleman Rd., Leicester)

## Transformer

T1 Primary, 10 turns 18 s.w.g. enamelled wire; secondary, 200 turns 36 s.w.g. enamelled wire both layer wound on 2 in length, $\frac{1}{4}$ in dia. ferrite rod

## Miscellaneous

S1 Double pole mains switch; FS1-5A fuse with panel mounted holder; group board; stand off spacers; 3 wander plug sockets; 1 wander plug
high charge stored on C4 is reduced over a short period of time. Do not. however, rely on this-it is always safer to discharge high value capacitors with a screwdriver before touching them.

C4 must be a paper dielectric capacitor rated in excess of 500 V . An electrolytic must not be used in any circumstance


Fig. 2. Component wiring and assembly on group board. Stand-off spacers should be used when connecting to case

## CONSTRUCTION

Nearly all the circuitry is mounted on a length of group board (Fig. 2) and the only precautions necessary in the layout are that the secondary of T 1 (winding details given in Fig. 3) should not be routed too close to any other wiring and R3 should not touch any other components as it gets quite warm. As the discharge current from C4 is very high, fairly heavy gauge wire should be used to connect its terminals to the discharge tube to prevent excessive line drop.


Fig. 3. Winding details of trigger transformer. Both windings are wound in the same sense

All the components should be mounted in a metal case that can be properly earthed; this is essential as all the wiring is live to mains. Wander plug sockets form a convenient way of mounting the tube within the reflector and enable easy change of tubes which have a life expectancy of about a million flashes (this is equivalent to about 25-30 hours of operation at 10 flashes per second).

## REFLECTOR

The reflector was the hardest single item to find. In the end a tour round surplus shops solved the problem where a reflector from on old projector system was found for a few pence. An old car headlight reflector (pre sealed-beam era) would be ideal.

The reflector should be bolted or stuck on the main box and the tube sockets fixed through the rear of the reflector and the case-these add extra mechanical support to the reflector. To make the unit tamper proof it would be advisable to place a clear Perspex guard in front of the tube-if different coloured lighting was required tinted Perspex could be used for this purpose.


THIS fader unit was developed for use in a Discotheque console where it will automatically fade out the music being played when the D.J. makes an announcement via the microphone. When the announcement is finished the music is then restored to its original volume.

As the finished unit in its original form measures only $3.75 \times 2.5 \times 0.5 i n$, it should fit easily into the corner of a Discotheque console.

Whilst no complicated adjustments of the console wiring are required the unit will require some form of power supply as it consumes some 7 mA at 9 V . This could be taken from the Discotheque supply or be provided by a battery if required.

## CIRCUIT

The circuit is shown in Fig. I and, as can be seen, is constructed around the Motorola integrated circuit MFC 6040 which is used as an electronic attenuator. It provides zero attenuation for control voltages below 3.5 V and about 90 dB attenuation for a 6 V control voltage. Thus to give the required control effect we have to derive a rising and falling d.c. level from the microphone signal to fade the deck signal in and out.

TRI and its associated resistors form an emitter follower which gives the input a high impedance and thus prevents undue loading of the console preamplifier. TR2 forms a simple amplifier the output of which goes to the base of TR3 via diodes D1 and D2 and VR1. The diodes clamp and rectify the amplified microphone signal and VR1 controls the amount of signal applied to the base of TR3. Thus it controls the sensitivity of the unit.

When there is an input signal at the microphone of sufficient amplitude TR3 is turned hard on and the collector is thus at 0 V . C4 prevents this voltage rising appreciably during any short breaks in speech which might occur such as between words or sentences.

Without an input signal TR4 conducts and the collector lies about 2 V above earth potential. When TR3 turns on TR4 turns off and C5 charges up via R7, providing a rising potential at the control input of ICl .

This in turn attenuates, at a rising rate, the signal from the deck. The initial attenuation must be fairly rapid if the initial part of the announcement is not to be drowned in music.

When TR3 turns off again TR4 turns on and C5 discharges to earth through TR4 and R8 until it reaches a steady level. This gives a falling voltage level to decrease the attenuation provided by IC1.

## POWER SUPPLY

As mentioned, a 9 V supply giving about 7 mA is needed. If such is already available within the console, all well and good. If not then it is simply a matter of dropping and stabilising the console preamplifier supply and this may be done simply by using the circuit of Fig. 2.

In Fig. 2, the resistor R9 drops the supply voltage from the console rail value to 9 volts at which it is clamped by the Zener D3. Capacitor C9 gives smoothing of the output. Using Ohms Law, and given a pre-amplifier voltage of V volts then:-
$R 9=\frac{(\mathrm{V}-9)}{11} \mathrm{k} \Omega$, where R 9 is $\frac{1}{4}$ watt if V is less than 30 V or otherwise $\frac{1}{2}$ watt.


Fig. 1. Circuit diagram of the complete fader which is based on the Motorola MFC 6040 attenuator integrated circuit


Fig. 2. Circuit of a simple power supply for use with the fader


Fig. 3. Component layout and 0.1 in track Veroboard cutting details

## COMPONENTS . . .

## VOICE OPERATED FADER

| Resistors |  |  |
| :---: | :---: | :---: |
| R1 | 220k $\Omega$ |  |
| R2 $100 \mathrm{k} \Omega$ |  |  |
| R3 $2.7 \mathrm{k} \Omega$ |  |  |
| R4 1.8M $\Omega$ |  |  |
| R5 10k $\Omega$ |  |  |
| R6 $22 \mathrm{k} \Omega$ |  |  |
| R7 $3.3 \mathrm{k} \Omega$ |  |  |
| R8 $560 \Omega$ |  |  |
| R9 See text |  |  |
| Capacitors |  |  |
| C1- |  | $0.1 \mu \mathrm{~F}$ Mylar film |
| C4 |  | $47 \mu \mathrm{~F}, 10 \mathrm{~V}$ elect. |
| C5 |  | $220 \mu \mathrm{~F} 10 \mathrm{~V}$ elect. |
| C6 |  | 680pF polystyrene |
|  |  | $1 \mu \mathrm{~F} 16 \mathrm{~V}$ elect. |
| C9 |  | $100 \mu \mathrm{~F} 10 \mathrm{~V}$ elect. |

Semiconductors

| TR1-TR4 | 2N3704 |
| :--- | :--- |
| D1, D2 | 1S44 |
| D3 | BZY88 C9V1, 9.1V Zener |
| IC1 | MFC 6040 (Motorola). Available |
|  |  |
|  | from Jermyn or Arrow Electronics |

Potentiometers
VR1 100k $\Omega$ linear horizontal mounting pre-set

## Miscellaneous

0.1 in Matrix Veroboard measuring 3.75in $\times 2.75 \mathrm{in}$ Wire and coaxial cable as needed


CONSOLE WITH FADER ADDED
Fig. 4. Discotheque console circuit with and without voice operated fader

## CONSTRUCTION

The unit is quite simple to construct as can be seen from Fig. 3. Using standard 0.1 in matrix Veroboard $3.75 \times 2.5$ in the layout of Fig. 3 may be followed. Coaxial cable should be used for the microphone leads to avoid hum pick-up.

Equally, circuit installation is simple as is shown in Fig. 4.

If the circuit of Fig. 2 is to be used. this may be added to the board carrying the main components or simply suspended in the wiring since it consists of so few components.


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## PRACTICAL <br> EHETRONIES

JANUARY ISSUE ON SALE DECEMBER 14, 1973

## PART 3: <br> Applications of <br> PHASE LOXKED LOOP <br> IWTEERATE GROUTS

## PHASE LCKKED LCPSS

 EYJ.B.DANCE m.sc.The basic theory of phase locked loops has been reviewed in a non-mathematical way in the previous articles in this series. We will now consider in detail the types of phase locked loops which are currently available together with examples of the types of circuit in which they can be used.

Monolithic phase locked loops are necessarily fairly complex devices. In general the various manufacturers have evolved devices which are quite different from one another and they must therefore be considered separately.

## SIGNETICS H.F. LOOPS

The Signetics International Corporation manufacture three rather similar monolithic phase locked loops which can operate at high frequencies. They are the NE560B, the NE561B and the NE562B devices.

These three phase locked loops all employ the same phase detector, the same voltage controlled oscillator and the same voltage regulator stages. The basic parameters are therefore very similar for all the three devices, but there are differences in the metallic interconnections which make some types especially suitable for certain applications.

## NE560B

The NE560B can be regarded as the most fundamental of the three devices. It has the basic phase locked loop structure shown in the block diagram of Fig. 3.1. This device is suitable for high linearity f.m. demodulation, for telemetry decoding, for use in signal generators, in frequency shift keying receivers, in tracking filters, in circuits for exact frequency duplication in a high noise environment, etc.
The voltage controlled oscillator in this device provides two outputs of opposite polarity to each other.

## NE561B

The NE561B contains all the circuitry of the NE560B, but also has an analogue multiplier which can be used as a quadrature detector. This allows the device to be employed for the synchronous
detection of amplitude modulated signals if an external 90 degree phase shift network is added.
The NE561B can also be employed in a.m./f.m. i.f. strips, in signal generators, in telemetry decoders, in tracking filters, etc.

## NE562B

The NE562B is similar to the NE560B, but the loop is broken between the voltage controlled oscillator and the phase comparator. A frequency dividing circuit can therefore be inserted in the loop at this point if it is desired that the voltage controlled oscillator shall operate at a harmonic of the input frequency.

The NE562B is therefore especially useful in frequency synthesisers and for frequency multiplication and division. In addition, it can also be used in f.m. i.f. strips and for most of the other applications for which the NE560B is suitable.

## SUMMARY OF DATA

Each of these three phase locked loops can be operated over a frequency range from less than 1 Hz to over 15 MHz , the centre or free-running frequency being set by the value of a capacitor connected between two pins of the voltage con-


Fig. 3.1. Block diagram of the NE560B phase locked loop. The numbers refer to pins on the dual-in-fine versions

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(PE APMINI STEREO TUNER

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| :---: | :---: |
|  |  |
|  |  |

$A C$
$A C$
$A D$
$B C$
$B C$
$B C$
$B$
$B$
$B$
$B$
$B$
$B$
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0
0

 | C176 | 20p | 2TX531 | 2Np | 2NLECTROLYTIC |
| :---: | :---: | :---: | :---: | :---: |
| 161 | 13p |  |  |  | $A D 161$

BC107 | 107 | 40p | $2 N 914$ |
| :--- | :--- | :--- |
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Fig. 3.2. Graph showing the relationship between the centre frequency and the value of the timing capacitor
trolled oscillator. The variation of this frequency with the value of the capacitor is shown in Fig. 3.2.

The control voltage is prevented from exceeding a preset level by a limiter between the control voltage amplifier and the voltage controlled oscillator. This range is known as the tracking range and is set by a control current into pin 7 of the i.c.

The typical operating voltage of these devices is 18 V . The NE560B consumes less than 11 mA , the NE561B less than 12 mA and the NE562B less than 14 mA .

The NE560B and the NE561B require a minimum of $100 \mu \mathrm{~V}$ for locking, and can take 1 V r.m.s. maximum. The corresponding figures for the NE562B are $200 \mu \mathrm{~V}$ minimum and 3 V r.m.s. maximum.

The maximum output voltage swing is 4 V peak-to-peak.

If one applies a $1 \mathrm{mV}, 10.7 \mathrm{MHz}$ f:m. input signal which has a $\pm 75 \mathrm{kHz}$ deviation and a 50 ohm source impedance, the demodulated output is typically 60 mV in amplitude with a total harmonic distortion of $0.3 \%$ (typical).

When one of these loops is used for demodulating f.m. signals a capacitor may be connected from pin 10 to ground to provide de-emphasis.

At operating frequencies below 5 MHz the low pass filter may be formed by connecting a capacitor (or capacitor and resistor in series) across the low pass filter terminals. At higher frequencies a capacitor from each terminal to ground should be used to ensure loop stability.

## APPLICATIONS

In order to illustrate the usefulness of phase locked loops some circuit diagrams will be given. Whilst it is not possible to give sufficient detail for the systems to be built it is hoped that the information given will give the reader an appreciation of the practical aspects of phase locked loop i.c.s.

## F.M. DEMODULATION

A phase locked loop can replace almost the whole i.f. strip, limiter and f.m. detector of a conventional receiver. A typical circuit using the NE560B as f.m. demodulator with an i.f. amplifier and limiter is shown in Fig. 3.3.

The input from the f.m. tuner unit is first amplified by the two sections of a Signetics NE510A dual high frequency differential amplifier. The low output impedance signal from the NE510A is coupled by C4 to pin 12 of the NE560B. The other input (pin 13) of the phase comparator is grounded with respect to radio frequencies by C5. The capacitors C4 and C5 may each have a value of 20 pF when the signal frequency is 10.7 MHz .

The frequency of the loop is set by the variable capacitor C9 which is connected between pins 2 and 3 so that the centre frequency becomes approximately equal to the signal frequency. The value of C9 may be estimated from Fig. 3.2.


Fig. 3.3. Circuit diagram of the NE560B used in an f.m. demodulator


Fig. 3.4a. Block diagram showing the NE561B used as an a.m. demodulator

Fine tuning is easily accomplished by using a variable capacitor for C9. However, a potentiometer connected between the power supply lines with the slider connected to pin 6 via a 200 ohm current limiting resistor may be employed.
Components R5, R6, C7 and C8 form the low-pass filter which controls the capture range and the selectivity. The value of the capacitors in microfarads is approximately 2660 divided by the required bandwidth in hertz.

## DE-EMPHASIS

The de-emphasis is introduced by merely connecting pin 10 via a capacitor to ground. The value of this capacitor multiplied by the internal eight kilohm resistance should produce a time constant of about $50 \mu \mathrm{~s}$ for the standard f.m. broadcasts in the U.K. Thus $C_{6}=50 \times 10^{-6} / 8000=6.25 n \mathrm{~F}$, but this value is in no way critical.

## THE NE561B FOR A.M. RECEPTION

The NE561B can be connected as in the block diagram of Fig. 3.4a for the detection of a.m. signals.
The 90 degree phase shift circuit changes the phase of the input signal so that the voltage controlled oscillator in the phase locked loop operates in phase with the input signal. The output from this oscillator is fed to the product detector where it provides the local oscillator signal.

A practical a.m. detector circuit using the NE561B is shown in Fig. 3.4b. It can be used over a fairly wide frequency range, but component values will be quoted for the medium wave band $(550 \mathrm{kHz}$ to 1.6 MHz ).

The values of the by-pass and coupling capacitors should be chosen for a low impedance at the operating frequencies. For medium wave use C2, C7 and C 8 may therefore be $0 \cdot 1 \mu \mathrm{~F}$.

## CAPACITOR TUNING

The value of C 5 must be selected so that the voltage controlled oscillator operates at the required input signal frequency. If desired, the capacitor C5

Fig. 3.4b. Practical circuit of the a.m. demodulator
may be a variable one, in which case the connections to pin 6 (R3 and VR1) may be omitted.

When a variable capacitor is employed for C5, its value will be approximately 300 divided by the input signal frequency in megahertz at the capacitor setting concerned. For the 550 kHz to 1.6 MHz range, the value of C5 should range from about 550 pF to about 180 pF .

## RESISTOR TUNING

If the tuning is to be carried out by the variable resistor VR1, the value of C 5 should be chosen so that when no current is injected or removed from pin 6, the voltage controlled oscillator operates at the geometric mean frequency of the band to be received. This geometric mean is equal to the square root of the product of the lowest and highest frequencies in the band. In the case of the 550 kHz to 1.6 MHz receiver, this mean frequency works out as 940 kHz .
The complete medium wave band may be tuned by VR1; this potentiometer may be a ten-turn helical type to permit accurate setting. The value of R3 is selected to give the desired tuning range and will be about 1.2 kilohm when an 18 V power supply is employed.

## PHASE SHIFT

The component values of the phase shift circuit may be determined in the following way.
If $R_{1}=R_{2}=3 \mathrm{k} \Omega$, the $C_{1}=C_{6}=(1.3 \times$ $\left.10^{-4} / f\right) \mathrm{F}$
where $f$ is the midband frequency. In the medium wave receiver, $f$ is 0.94 M Hz and $C_{1}=C_{6}=1.35$ $\times 10^{-10} \mathrm{~F}=135 \mathrm{pF}$.

## LOW-PASS FILTER

The value of the low-pass filter capacitor, C4, is not at all critical, since no information is derived directly from the loop error signal. One merely requires to establish stable operation. A 10 nF capacitor is suitable for C 4 .

## TAPE RECORDER FLUTTER METER

A circuit devised by R. Blair of Houston using the NE561B in a tape recorder flutter meter is shown in Fig. 3.5. A 3 kHz sinewave is fed to the recording head. The output from the replay head is fed to the phase locked loop which detects any variations in frequency from the 3 kHz value.

The NE561B circuit is set to a nominal value of 3 kHz using the fine tuning control. The demodulated output is capacitively coupled to an amplifier of high input impedance. The output level changes with any change in the frequency of the signal applied to the phase locked loop.

An oscilloscope may be employed to measure the peak deviations and a true r.m.s. voltmeter to make r.m.s. flutter measurements. (The waveform is complex and therefore meters which read the peak or average value will not give true readings.) The output can be filtered to study any selected bands of frequencies.

## THE 565

One of the best known low frequency phase locked loops is the 565 device. This is available as the Signetics NE565A device and as the National Semiconductor LM565CN device in a 14 pin dual-in-line encapsulation. The NE565K and the LM565CH are electrically equivalent devices in a TO-99 circular encapsulation.

The basic circuit for all of these devices together with the pin connections is shown in block form in Fig. 3.6.

The loop is broken between the output of the voltage controlled oscillator and the input to the phase comparator (pins 4 and 5 respectively) so that frequency divider circuits can be inserted at this point for frequency synthesis applications. The lowpass filter is formed by the internal resistor marked RA in Fig. 3.6 and the external capacitor C2.

## FREQUENCY RANGE

The maximum trequency at which the voltage controlled oscillator of the 565 devices can operate is


Fig. 3.6. Block diagram of the $\mathbf{5 6 5}$ low frequency phase locked loop. This is the pin numbering for the NE565A (Signetics) and the LM565CN (National Semiconductor), both 14 pin dual-inline
about 500 kHz . The minimum practical operating frequency is set by the maximum value of the timing capacitor (CI in Fig. 3.6) which can reasonably be used. If one decides that this maximum value is $10,000 \mu \mathrm{~F}$. one can obtain a frequency as low as 0.001 Hz .

The free-running frequency of the voltage controlled oscillator is only partly determined by the value of the timing capacitor C 1 . The frequency can be changed over a range of at least $10: 1$ using a single value of Cl by varying the value of R1 in the pin 8 circuit: alternatively the value of the current fed to pin 8 may be varied.
The typical variation of the free-running frequency with the value of R 1 for four values of the timing capacitor is shown in Fig. 3.7. For any given value of the timing capacitor, the free-running frequency is about an order of magnitude lower than that of the high frequency loops.
The free-running frequency of the 565 oscillator is given by the approximate equation $f=1.2 /$ $\left(4 R_{1} C_{1}\right)$ where RI and Cl are the timing components shown in Fig. 3.6


Fig. 3.5. A tape recorder flutter meter using the NE561B phase locked loop


Fig. 3.7. Relationship between the centre frequency and the timing components for the 565 integrated circuit
The value of the timing capacitor Cl can vary over wide limits, but the resistor RI should have a value of between $2 \mathrm{k} \Omega 2$ and $20 \mathrm{k} \Omega$, the optimum being about $4 \mathbf{k} \Omega$.
When using power supply lines which are symmetrical with respect to ground, the range of voltages which may be employed is $\pm 5 \mathrm{~V}$ to $\pm 12 \mathrm{~V}$. When $\pm 6 \mathrm{~V}$ power supplies are employed, the typical current taken is 8 mA with a maximum value of 12 mA . The maximum permissible power dissipation is 300 mW .

## THE OSCILLATOR

The voltage controlled oscillator circuit used in the 565 devices can be obtained as a separate integrated circuit type 566. It is available as the Signetics 8 pin dual-in-line device type NE566V and the similar National Semiconductor device type LM566CN. The circular TO-99 equivalents are types NE566T and LM566CH. The SE566T and LM566H are close tolerance devices.

In the 565 phase locked loops, triangular and square waves are generated by the voltage controlled oscillator, but no buffer stage is provided to give a triangular wave output as in the 566 . The square wave output (about 5.4 V peak-to-peak) is available at pin 4 of the 565 .

The output of the low-pass filter (pin 7 of Fig. 3.6 ) is connected internally to the voltage control input of the oscillator. The oscillator frequency can therefore be controlled by a signal fed to the demodulated output terminal (pin 7).

## LOCKING RANGE

The range of input frequencies over which the loop will remain in lock on each side of the centre frequency is given by the approximate expression $\pm 8 f / V$ where $f$ is the centre frequency and $V$ is the total voltage between the power supply lines.
The 565 can therefore track the input frequency over a very wide range (typically $\pm 60 \%$ of the centre frequency). Locking can be obtained over a greater fraction of the input frequency than in the case of high frequency loops.
The 565 input impedance is typically 10 kilohm (minimum 5 kilohm). The minimum input signal required to produce tracking is typically 1 mV r.m.s.
The linearity of the f.m. response is very good (typically about $0.2 \%$ ).

## FREQUENCY MULTIPLICATION

In the circuit of Fig. 3.8, a frequency divider circuit has been inserted in the loop between pins 4 and 5. The output of the voltage controlled oscillator is divided in frequency by a certain factor and the frequency divided circuit locks with the input signal. The oscillator therefore operates at a higher frequency than the input signal.

The value of C 2 should be adequate to eliminate variations in the demodulated output voltage at pin 7 in order to stabilise the voltage controlled oscillator frequency.
The square wave output frequency can be taken from pin 4.

## METAL DETECTOR

Phase locked loops can be used to detect changes of frequency. Such changes can be produced when the coil of a tuned circuit approaches a piece of metal. Phase locked loops can therefore be used in metal detectors.
A circuit of this type which has been designed by J. Blecksmith of California is shown in Fig. 3.9. The 8in diameter search coil comprises 30 turns of copper wire ( $26 \mathrm{~s} . \mathrm{w} . \mathrm{g}$.) and has an inductance of about 0.5 mH . It is connected in the Colpitts oscillator circuit of TR1 which operates at about 100 kHz .

This oscillator is coupled by C3 into the input of the 565 circuit (pin 2): A current source (TR2 and TR3) is employed to supply most of the current of about 2.5 mA which passes to pin 8 and which equals the charging and discharging current of C4. The use of this current source increases the output of the loop at pin 7 to about 0.5 V for a $1 \%$ frequency deviation. (This follows from the fact that the $20 \mathrm{k} \Omega$ resistor R7 will produce a change in the current to pin 8 of $0.5 / 20,000=$ 0.025 mA for a 0.5 V change. In other words a change of 0.5 V produces about $1 \%$ change in the pin 8 current.)
The output voltage at pin 7 is compared with the reference voltage at pin 6 by the differential amplifier of TR4 and TR5. The output of this amplifier drives a centre reading meter which has a $\pm 100 \mu \mathrm{~A}$ scale. The meter zero is set by VR2 and the sensitivity by VR3.
When the search coil is brought near to a nonferrous metal object, the frequency of the TR1 oscillator circuit will rise and so will the meter indication. Any object containing iron will increase the inductance of the loop and reduce the frequency of oscillation; the meter reading will therefore fall.


Fig. 3.8. A frequency multiplier using the 565 and a divider


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| SN7400 | 0.17 | 0.16 | SN7426 | 0.50 | $0 \cdot 46$ | SN7454 | 0.17 | $0 \cdot 16$ | SN7494 | -85 | 0.82 |
| SN7401 | 0.17 | 0.16 | SN7427 | 0.50 | 0.46 | SN7460 | 0.17 | 0.16 | SN7495 | 0.85 | -82 |
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| SN7420 | 0.17 | 0.16 | 8N7448 | £1.10 | 41.07 | 8N7490 | 0.68 | 0.60 |  |  |  |
| 8N7422 | 0.55 | 0.53 | 8N7450 | 0.17 | 0.16 | 8N7491 | 41.10 | 21.05 | * 100 plus less $10 \%$ off 25 plus break |  |  |
| 8N7423 | 0.55 | 0.53 | 8N7451 | 0.17 | $0 \cdot 16$ | 8N7492 | 0.74 | 0.71 |  |  |  |
| 7425 | 0.55 | 0.53 | 745 | -1 | -1 | SN7493 | 0.74 | 0.71 |  |  |  |

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307 \& DIL \& $\mathbf{0 . 8 8}$ \& 710 C \& DIL \& 0.44 \& 747 C \& DIL \& $\mathbf{0 . 8 0}$
\end{tabular}

## Electrolytic Capacitors

| 4 VOLT | 10 VOLT | 16 VOLT | 25 VOLT | 63 VOLT |
| :---: | :---: | :---: | :---: | :---: |
| $47 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{p}$ | $22 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{p}$ | $1000 \mu \mathrm{~F} \quad 17 \mathrm{p}$ | 2200 F F 39p | $1 \mu \mathrm{~F}$ |
| $100 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{p}$ |  | $1500 \mu \mathrm{~F}$ 25p | 5000 F ( 68p | $2 \cdot 2 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ |
| 220, $\mathrm{F} \quad 6 \frac{1}{4} \mathrm{P}$ | $100 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | 2000 F F 43p |  | 4.7 $\mu \mathrm{F}$ ( $6 \frac{1}{2} \mathrm{P}$ |
| 330 F ( $6 \frac{1}{19}$ | 220 F F 8p | 3300 F F 38p |  | $6.8 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{p}$ |
| $1000 \mu \mathrm{~F} \quad 13 \mathrm{p}$ | $330 \mu \mathrm{~F} \quad 10 \mathrm{p}$ | $6800 \mu \mathrm{~F}$ 6 6 p | 40 VOLT | $10 \mu \mathrm{~F}$ ( $6 \frac{1}{2} \mathrm{p}$ |
| 4700 F F 29p | 470 F F 10p |  | $6.8 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | $22 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ |
|  | $1000 \mu \mathrm{~F} \quad 11 \mathrm{P}$ |  | $15 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | $68 \mu \mathrm{~F}$ ( 10p |
| $6 \cdot 3 \mathrm{VOLT}$ | 1500 F F 20p | 25 VOLT | $33 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | $100 \mu \mathrm{~F}$ ( 11 p |
| $33 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | 2200~F 24p | $10 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{p}$ | $47 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{p}$ | 150нF 13p |
| $68 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ |  | 22 $\mu \mathrm{F} \quad 6 \frac{1}{2} \mathrm{P}$ | $100 \mu \mathrm{~F} \quad 9 \mathrm{p}$ | 220 F F 19p |
| $150 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | 16 VOLT | $47 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | $150 \mu \mathrm{~F} \quad 10 \mathrm{p}$ | $330 \mu \mathrm{~F} \quad 22 \mathrm{p}$ |
| $470 \mu \mathrm{~F}$ (11P | $15 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | $100 \mu \mathrm{~F}$ ( ${ }^{1}$ | $220 \mu \mathrm{~F}$ ( \\|p | 470 $\mu \mathrm{F}$ 26p |
| $680 \mu \mathrm{~F} \quad 13 \mathrm{P}$ | $33 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{p}$ | $150 \mu \mathrm{~F}$ - 8p | $470 \mu \mathrm{~F}$ - 19p | $1000 \mu \mathrm{~F}$ - 44p |
| 1500 F F 18p | $68 \mu \mathrm{~F} \quad 6 \frac{1}{2} p$ | 220んF 10p | $680 \mu \mathrm{~F} \quad$ 25p |  |
| 2200 F F 18p | $150 \mu \mathrm{~F} \quad 8 \mathrm{P}$ | 470 F - 13p | 1000 F F 25p |  |
| 3300 HF 26p | 220 F F 9p | 680 F F 20p | 2200~F 44p |  |
| 6800 FF - 40p | $680 \mu \mathrm{~F}$ - 17p | $1000 \mu \mathrm{~F} \quad 22 \mathrm{p}$ | $3300 \mu \mathrm{~F}$-65p |  |

## Mullard Polyester's

MULLARD POLYESTER CAPACITORS C280 SERIES
250 V P.C. mounting: $0.01 \mu \mathrm{~F}, 0 \cdot 015 \mu \mathrm{~F}, 0.22 \mu \mathrm{~F}, 34 \mathrm{p} .0 .33 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 4 \mathrm{D}, 0.1 \mu \mathrm{~F}, 44 \mathrm{p}$
$0.15 \mu \mathrm{~F}, 0.22 \mu \mathrm{~F}, 54 \mathrm{p} .0 .33 \mu \mathrm{~F}, 7 \mathrm{p} .0 .47 \mu \mathrm{~F}, 94 \mathrm{p} .0 .62 \mu \mathrm{~F}, 12 \mathrm{p} .1 .0 \mu \mathrm{~F}, 14 \mathrm{p} .15 \mu \mathrm{~F}, 22 \mathrm{p} .2 \cdot 2 \mu \mathrm{~F}, 27 \mathrm{p}$

## MULLARD POLYESTER CAPACITORS C296 SERIES

$400 \mathrm{~V}: 0.001 \mu \mathrm{~F}, 0.0015 \mu \mathrm{~F}, 0.0022 \mu \mathrm{~F} .0 .0033 \mu \mathrm{~F}, 0.0047 \mu \mathrm{~F}, 2 \ddagger \mathrm{p} .0-0068 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}$ $0.033 \mu \mathrm{~F}, 31 \mathrm{p}, 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, 41 \mathrm{p} .0 .15 \mu \mathrm{~F}, 61 \mathrm{p} .0 .22 \mu \mathrm{~F}, 81 \mathrm{p} .0 .33 \mu \mathrm{~F}, 12 \mathrm{p} .0 .47 \mu \mathrm{~F}, 14 \mathrm{p}$ $033 \mu \mathrm{~F}, 81 \mathrm{p} .047 \mu \mathrm{~F}, 81 \mathrm{p} .0 .68 \mu \mathrm{~F}, 12 \mathrm{p}$. $1 \cdot 0 \mu \mathrm{~F}, 141 \mathrm{p}$.

## Popular Transistors and Diodes

## (Many other types stocked)







 \begin{tabular}{rr|lr|l}
AC176 \& $15 p$ \& AF117 \& 15 p \& BC18 <br>
ACl \& 14 p \& BC 107 \& 9 p \& BC184

 

AC187 \& 14 p \& BC107 \& $9 p$ \& BC184 <br>
AC188 \& 14 p \& BC108 \& 9 p \& BC212

 

AC187K 25p \& BC109 \& 10 p \& BC213

 AC188K 24p 

ACY20 \& 22 p \& BC148 \& 11 p \& BF194 <br>
AD140 \& 40 p \& BC149 \& 12 p \& BF195

 

AD140 \& 40p \& BC149 \& 12p \& BF195
\end{tabular}



Carbon
skeleton presets
*inall high quality type (linear only
Atl values 100-5 meg ohms.
0.25 watt 7 p each

## Vereoboard

|  | 0.15 | 0.1 |
| :---: | :---: | :---: |
|  | matrix | matrix |
| 21.31 | 17p | 22p |
| $21 \times 5$ | 22p | 24p |
| $34 \times 31$ | 22p | 24p |
| $31 \times 5$ | 28p | 28p |
| 2 ¢ $\times 17$ | 60p | 79 p |
| $3 \% \times 17$ | 81p | 21.05 |
| Pin filsertion tool |  | 82 p |
| Spot face cutter | 52p | 52 p |
| Pack of 36 pins | 42p | 42p |
|  | 20D | 20p |

## P.E. RONDO KITS

Supplied to lull specifications complete with top quality P.C. boards, components
CBS SQ Matrix Decoder (incluting licence fees) $\mathbf{2 8 \cdot 0 0}+80$ p VAT
Preampliter Board $£ 3 \cdot 00+30 \mathrm{p}$ V AT
Master Volume/Tone Controls/4 cbannel Balance Control Board $\mathbf{8 8} \mathbf{5 0}+8 \mathrm{~J} p$
Power Amplifer Board and Heat Sink (each board contains a stereo pair of


Power Supply Board $\quad 45.00+\overline{0} 01 \mathrm{VAT}$
Mains Smoother Capacitor
Mains Transformer
75D + inVAT
Mains Transformer $\quad \mathbf{\varepsilon 6 . 2 5 + 6 2 2 p ~ Y A T ~}$
Puached Cheasit $\quad £ 2 \cdot 25+\stackrel{.2}{2} \mathrm{p}$ VAT
Hard
Control Section Facia $\mathbf{£ 3 \cdot 5 0 + 3 5 1 , ~ \ T ~}$
All other kits and components utsed in the P.E. Rondo pill bc available as they appear in this series.

## Transformers

12-24 volt
Secondary

| Volts | Amps | Volts | Amps | Part No. | Price |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 500 | 24 | 250 mA | MTI | inc. P/s E1. 20 |
| 12 | 1 | 24 | 500 mla | MT213 | 21.26 |
| 12 | 2 | 24 | 1 | MT71 | 11.89 |

30 volt
Secondary $12,15,20,24,30 v$
Amps Part No. Price fne, P/P
MT79
MT3
MY51

50 volt
Secondary 19, 25, 33, 40, 50v
Alıps Part No. Prlee inc. $\mathrm{P} / \mathrm{P}$
P
MT 103 MT103.
MT104. MT104.
MT106.
Asny other types arailsble
See our Catalorue.


We are now Stockists of AMTRON High Quality Construction Kits (S.A.E. for full list)

UK65 Transistor Tester
UK92 Telephone Amplifier
UKIlO Stereo Amplifier $5+5 w$
UKIIS Hi-Fi Amplifier 8w
UKI20 Hi-Fi Amplifier 12w
UK 125 Stereo Control Unit
UK 160 1.C. Amplifier 8w
9p UK220 Signal Injector
UK235 Acoustic Alarm for Absent-minded Drivers
UK240 Parking Lights Automatic Switch
UK500 LW/MW/FM Radio Receiver
UK515 MW Radio Receiver
UK640 200mw Light Dimmer
UK790 Capacitive Burglar Alarm
UK840 Adjustable time lag car Burglar Alarm
UK875 Capacitive Discharge Electronic Ignition for internal
Combuscion Engines
TRA 1 24-hour Digital Clock


Fig. 3.9. A metal detector using the $\mathbf{5 6 5}$

## WEATHER SATELLITE APPLICATION

As an example of a very different application of the 565 , its use in a weather satellite picture demodulator will be outlined.

Weather satellites continually photograph the earth from a distance of typically a few hundred miles. The pictures are stored in an electrostatic Vidicon tube and are read out during the succeeding 200 seconds.

The signal is transmitted on a 137.5 MHz carrier frequency modulated with a 2.4 kHz sub-carrier; the latter contains the picture information. The demodulated $2 \cdot 4 \mathrm{kHz}$ tone is normally recorded on tape at the receiving station for subsequent processing.


Flg. 3.10. A system for demodulating video signals from the 2.4 kHz sub-carrier which is used by weather satellites

When the tape is replayed, it is desirable to reproduce the 2.4 kHz sub-carrier using a phase locked loop, since the latter will effectively filter out most of the noise and will track any flutter in the magnetic tape mechanism.
The basic circuit used in this application is shown in Fig. 3.10. The loop locks at the 2.4 kHz frequency. If this is also the centre frequency of the loop, the square wave output from pin 4 of the 565 will be 90 degree out of phase with the input.
However, the zero crossing times of the triangular wave across the timing capacitor may be applied to the LM1596 doubled balanced modulator so that switching occurs in phase with the $2 \cdot 4 \mathrm{kHz}$ subcarrier.
The picture may be reproduced on a cathode ray tube. Detailed circuit information is available in the National Semiconductor report AN-46.

## AVAILABILITY

The Signetics phase locked loops are about the most widely available type at the present time and are available from many of the advertisers in Practical Electronics. The NE560B, NE561B and NE562B are available from S.D.S. Components Ltd., Portsmouth PO3 5JW at about $£ 4 \cdot 20$ in small quantities. The Signetics 565, 566 and 567 are obtainable from the same source at about $£ 4, £ 1.44$ and $£ 3 \cdot 25$ respectively.
National Semiconductor devices can be obtained from Semiconductor Specialists, Farfield Road, West Drayton.

Further information on these devices may be obtained from the Signetics Linear Integrated Circuit book and in data and applications notes from Signetics and National Semiconductors.

Next month: more applications of phase locked loop integrated circuits will be described including stereo decoding

## LOGIC TUTOR 

## THE FULL ADDER

|N PRACTICE we must be able to add together two multidigit numbers and as we saw last month the HALF ADDER does not go quite far enough to doing this. We have to design a circuit that is capable of accepting the two digits of the column (A with B) and incorporate a possible carry over from the previous (less significant) column.

## TWO STAGES

The simplest way of doing this is to carry out the operation in two stages; first add together the digits that are in the higher significance column-this is done in the HALF ADDER 1 of Fig. 8.I

If the digits were 0 and 0 we would get a partial sum of 0 and a carry of 0 . If either of the digits were I we would get a partial sum of $I$ and a carry of 0 but if both digits were $I$ we would get a partial sum of 0 and a carry of $I$.

We shall come back to this carry in a moment but remember that if we get a carry, at all, at the output of HALF ADDER 1 the sum output of it is bound to be 0 .

We now take the partial sum from the first HALF ADDER and combine it with the carry digit-that might have been generated by the previous column. This is done in HALF ADDER 2. This will generáte a final sum and could generate a carry.

If you think about it you will see that if a carry is generated at the output of HALF ADDER $I$ it is not possible to get a carry from HALF ADDER 2 (because the sum from the first stage would have been bound to be 0 ). However, if the sum from the first stage was I it might be that there was a carry in from the previous column and these combine in the second stage to give a carry out as well as the final sum. Whatever happens it is not possible to get a carry out of both stages at the same time so there is no question of having to add two carries together.

## FULL ADDER

Thus to generate a final carry out of the complete unit we only have to OR together the two possible sources of carry. This circuit is called a FULL ADDER and can be made using the building blocks we have already described in NAND form. We need two HALF ADDERS and an OR gate.

An unsimplified circuit showing the discrete stages in NAND logic appears in Fig. 8.2. Do not make this on Logic Tutor because we can simplify the circuit a little. Notice that we have double inversion on the two lines feeding the final NAND gate of the OR block. These negate each other and we are left with a complete FULL ADDER using nine NAND gates in Fig. 8.3. This you can make on Logic Tutor.

Using the switches and lamps and a piece of paper and a pencil show that the circuit truthfully follows the rules of arithmetic necessary to add the three input digits together.


Fig. 8.1. Two HALF ADDERS are combined to form a FULL ADDER


Fig. 8.2. A FULL ADDER using blocks of logic in unsimplified form. Note the two sets of double inversion before the final NAND gate in the $\mathbf{C}_{0}$ line


Fig. 8.3. A FULL ADDER that can be built on the Logic Tutor


Fig. 8.4 Block diagram of a parallel adder capable of summing two, three-digit binary numbers to give a three-or four-digit answer

## MULTIDIGIT NUMBERS

In practice we have to add multidigit numbers together and the simplest way of doing this is to cascade FULL ADDERS -one after the other. The carry out from the previous column is connected directly to the carry in of the next. Fig. 8.4 is a block diagram of such a summing unit.

Al and Bl are the least significant digits of the respective multidigit numbers and because of this they only need a HALF ADDER to produce a true sum and carry; however, all higher order digits have to be combined in FULL ADDERS.

You would need as many adding stages as there are digits when carrying out the process in parallel form consequently a parallel adder can be quite expensive but it is very fast in operation. A cheaper form is the serial adder (not shown in this series) but there is rather more complexity in handling the carry signals.

# HOW TO LISTEN TO THE WORLD 7th EDITION 

By J. M. Frost
Published in the U.K. by Fountain Press
160 pages, 9 in $\times 6$ in. Price $£ 1 \cdot 90$

WHILST not exactly filled with "do it yourself" information on the making and using of radio receiving equipment, it does contain considerable information of general interest.

For example, how many people know the frequencies and addresses of a variety of Irish "pirate" stations currently in operation? A section of this volume provides details of a number of revolutionary stations throughout the World and gives information on their mode of operation.

On the technical side there is some interesting discussion on the use of front-end tuners for RX equipment, together with details of some the reader can make. Other chapters cover medium wave working, improving a second-hand set, working South America and a listing of the major broadcast stations.
R.D.R.

## PHOTOCELL APPLICATIONS <br> Published by English Universities Press <br> 

AS AN introduction to electronics, photocells of various types provide an excelient starting point as they are easy to understand, they have a multitude of applications and are relatively cheap.

Only a basic knowledge of electronic principles is assumed and practical points such as resistor colour code and circuit symbols are fully covered. The projects range in complexity from a simple exposure meter to a modulated light transmitter and receiver.

Through this book the reader can obtain not only a knowledge of photocells but also other electronic components such as transistors, and thus can discover some of the fascination of electronics.
S.R.L.

IBA TECHNICAL REVIEW-DIGITAL TELEVISION Published by the IBA 64 pages, 9 in $\times 7 \frac{3}{4}$ in
| N This the third of the IBA's Technical Reviews ane extremely interesting account of the IBA Engineering Section and its work on digital television is presented. The book includes descriptions of the recent work of the IBA in developing digital standards converters, among them the first digital intercontinental conversion equipment (DICE) now in operational service at Independent Television News.
This book is written by members of the IBA Engineering staff and provides a valuable insight into the design techniques and philosophy behind some interesting projects.
Copies of this book may be obtained on request from: IBA Engineering Information Service, 70 Brompton Road, London, SW3 1EY.
S.R.L.

## FACIA

## BURROUND

## INTERWIRING \& HARNESB

IN the previous parts of the RONDO series we have discussed the construction of the main chassis member which forms a trough-like carrier for the power sections of the system. Now we come to a discussion of the general mechanical assembly and the wiring of the system.

## GENERAL CONSTRUCTION

The facia of the RONDO system supports both the controls and the r.f. tuning unit, whilst the remainder of the boards are assembled in the chassis pan itself. Thus, as can be seen from Fig. 4.1 the facia consists of an aluminium framework supported on four columns which are held in the main chassis by screws.
The columns support two crossmembers (Fig. 4.1b) made from aluminium angle ( $\frac{1}{2}$ in $\times$ lin) which in turn support two sections of aluminium extrusion made specially for the rondo system and a ailable from a number of kit suppliers. The two sections are separated by an inverted "U" section of brushed aluminium provided with ventilation louvres.

For those who wish to make their own facia this may be made up from sheet material bent up into the form at Fig. 4.1a, again supported on the columns and drilled so as to carry a simple aluminium facia in plain sheet. Drilling for this is identical to that for the pre-form material with the addition of master tone board mounting screw holes added.

The plain face area shown above the four input selector push-buttons on the left of the rondo is allocated to the tuner section, yet to be described.

The final main part of the mechanical assembly is the "wrap-round" or surround which forms the sides of the rondo. This is made from wood, veneered chipboard, or the like according to taste.

From Fig. 4.2 which shows the surround it will be seen that there are two alternative methods of fixing between the surround and the basic trough chassis. The first is to make use of the natural spring in the bent-up chassis by springing the two longer sides apart slightly such that when the surround is finally lowered over the facia to abut the two flanges on the trough, these are pushed in against the spring action. As the surround is lowered further they will then spring out to engage with the two grooves cut in the inner long surfaces of the surround.

If the constructor prefers, he may replace this method with one in which the surround is reduced in depth by the distance between the lower edge and the grooves and is supported on an extension bolted to the two trough flanges as shown in Fig. 4.2.

## WIRING DETAILS

The P.E. RONDO quadraphonic system is quite complex and, if not carefully wired, will result in an untidy maze. It is therefore strongly recommended that a prefabricated wiring harness, or cableform, be made to cover the bulk of the inter-unit wiring.

This cableform is constructed by means of a simple jig illustrated in Fig. 4.3 and made from a suitable piece of wood into which a pattern of "pins" is fixed; $1 \frac{1}{2}$ in panel pins are ideal for this purpose. They are hanmered into the appropriate points as shown and the heads are then clipped off and the sharp ends smoothed.

When assembling the cableform make certain that each wire or cable is inserted in the order given in Table 4.1, since otherwise both simple mechanical and electrical problems can arise.


Fig. 4.1. Construction of the facia. The upper drawing (a) shows the method of assembly using "homemade" aluminium panels and the lower drawing (b) shows the method of assembly using ready-made aluminium extrusions

## SURROUND \& LOOM

Fig. 4.2. Construction of the wooden surround with details of the two methods of fixing the trough


Fig. 4.3. Details of the cableform wiring harness. Interwiring between the units is greatly simplified if a cableform system is constructed as shown here

Each piece of wire is firmly secured by wrapping its start end round the first pin and then laying it along the route shown in Fig. 4.3 and the point-topoint wiring and assembly diagram of Fig. 4.4.

The intermediate pins along a route are used as guides and gentle tension is applied to each wire in order to produce a neat and tidy result. At the termination point the wire is again secured to the adjacent pin by wrapping. With the heavier wires it may be found necessary to knot the wire around the pin.
A "tail" some two to three inches long should be left at each end of each wire for later circuit connecting.

The cableform may now be "laced" up using lacing twine or, failing the availability of this, a waxed heavy thread or light nylon line. A simple form of lacing is shown in Fig. 4.3 from which it will be seen that this is merely a matter of tying the cableform into one cohesive unit by using a series of loops around the cables every $\frac{3}{4}$ in or so.

After lacing, the cableform is gently eased from the pins and is now ready for positioning in the trough.

## MECHANICAL ASSEMBLY

The two power amplifiers, already assembled complete with heat sinks, are laid side by side, copper side upwards on the bench. The power rails and earth rails are connected and flying leads are soldered as shown in Fig. 4.6.

The next step is to fit all sockets, rubber feet and mains lead grommet to the chassis as shown in Fig. 4.4. The wiring harness is then laid in the bottom of the main chassis as shown.

Starting at the rear of the chassis carefully identify each wire and its connecting point. Cut the wire tails to length and carefully strip the ends, wrap round and then solder. Repeat this procedure until

Table 4.1

| Start | Finish | Signal | Cable Type |
| :---: | :---: | :---: | :---: |
| 1 | 15 | CD4 | ) |
| 2 | 16 |  |  |
| 4 | 17 |  |  |
| 5 | 18 | SQ |  |
| 7 | 19 | Q |  |
| 8 | 20 | "'' | Twin screened |
| 11 | 21 | QS |  |
| 13 | 22 | " |  |
| 14 | 23 |  |  |
| 9 | 26 | Lal/P |  |
| 10 | 27 | $\mathrm{R}_{\mathrm{A}} / \mathrm{P}$ |  |
| 3 | 50 | +24V Rail | 14/0.0076 Pink |
| 6 | 51 | +20V Rail | White |
| 12 | 51 |  | " B"̈ck |
| 24 | 52 | - 15V Rail | " Black |
| 25 | 47 | +15V Rail | Red |
| 35 | 40 | LF O/P | Yellow |
| 40 | 32 |  | " Blü |
| 34 | 39 | $L_{B} 0 / P$ | Blue |
| 39 33 | 31 |  | " Rëd |
| 33 43 | 43 29 | $\mathrm{R}_{\mathrm{F}} \mathrm{O} / \mathrm{P}$ | " Red |
| 30 | 36 | $\mathrm{R}_{\mathrm{B}} \mathrm{O} / \mathrm{P}$ | ", Green |
| 36 | 28 |  | " Br' |
| 53 | 45 | +18V Rail | , Brown |
| 46 | 44 | Aerial | Miniature Co-Ax |


all wires that are shown to be terminated are soldered.

The remaining wires and their terminations are associated with the tuner unit which is to be the subject of a separate article and they will be described in detail then.

The two power amplifier boards, now joined together, are placed component side upwards in the chassis. The two right-hand limbs of the wiring harness (as seen from the front of the chassis) should be under the boards and the left-hand limb along the edge of the heat sink.

Ensure that the yellow. blue, red and green wires, in the centre limb of the harness, protrude above the boards at the appropriate outlet points. Cut, strip. wrap and solder them. Similarly treat the red and black wires in the right-hand limb, soldering them to the positive and negative 15 V rails on the power amplifier board.
The two rails are duplicated on the rear power amplifier board and the two boards are joined with short length of red and black wire interconnecting the rails.

## HEADPHONE SOCKETS

A group of four pairs of wires, each pair of one colour, namely yellow, blue, red and green, protrudes from the front of the harness in line with the headphone sockets. These wires are connected to the headphone sockets, as shown, ensuring that the leads from the power amplifiers go to the appropriate tags on the right side of the headphone sockets as viewed from the front of the chassis. If these connections are not correctly made the headphones will not function correctly.

The headphone sockets shown are of the normal three-wire type which can exhibit problems with the amplifiers set to high output levels. It is possible to either damage the headphones or the eardrums if care is not taken when plugging the headset in.
It is therefore recommended that the constructor either takes great care under these circumstances or adopts the use of a new style or socket which has just come onto the market. The new socket interposes a load in series with the headphones in order to limit the output level and current to a safe value.

Using the new sockets, a suitable load resistor for most applications is $220 \Omega$, $\frac{1}{2} \mathrm{~W}$.

## SYSTEM INTERWIRING

Fig. 4.4. Main wiring diagram of the PE RONDO.
Wires are separated for clarity but should be grouped together as indicated in Fig. 4.3



## POWER SUPPLY SUB-ASSEMBLY

Returning now to the power supply sub-assembly; fit the complete sub-assembly to the chassis with four $\frac{1}{2}$ in round-head 4BA screws, plain washers, lock washers and nuts. Similarly secure the power amplifiers to the chassis by means of the heat sinks. Fit the main smoothing capacitors to the chassis by means of capacitor clips.

The power supply includes transformer, power board and main smoothing capacitors and is shielded by means of two steel screens. The smaller of these screens, shown in Fig. 3.6, acts as a supporting baffle for the power supply board.

It is first fastened to one end of the mains transformer by four $\frac{1}{2}$ in round-head 4BA screws, each fitted. with one plain washer, one lock washer and a nut. The board is then secured to this baffle by three $\frac{3}{4}$ in round-head 6BA screws, washers and nuts and, in each case, a $\frac{3}{8}$ in spacer is interposed between the board and the baffle.

The larger of the two steel screens is now fitted to the chassis.

Refer to Fig. 4.4 and connect the leads to the power supply coming from the harness. Connect the mains lead and switch/pilot light as shown in Fig. 4.4.

Prepare the pre-amplifier board with flying leads
for connection to the main chassis components. Similarly connect the master volume/tone/balance control board. Reference to Fig. 4.4 will give the necessary guidance.

The four-way, six-change-over, pushbutton bank is now pre-wired in accordance with Fig. 4.4 and Table 4.2 .

The nine pairs of screened leads protruding from the right-hand front of the wiring harness are carefully stripped and identified. Connection of these leads to the switch bank is carried out with reference to the figure.

Please note that no wiring is provided for the SYNTHESISE position on the pushbutton bank. Details of this facility will be given in a later article together with the wiring of the tape sockets.

Fuses are now inserted into the holders on the power amplifier boards and into the mains fuse holder. See components list for ratings.

## AMPLIFIER CHECKING

Before commencing, carefully check the accuracy and completeness of the wiring. Extra time spent here can save expensive components coming to undue harm. Ideally, a parallel check between the unit, layout drawings and theoretical circuit should be performed.


Connect the speaker outlets to dummy $8 \Omega$ loads. The dummy load may be made up from $15,120 \Omega$ $\frac{1}{2} W$ carbon resistors connected in parallel. Only one load need be made as each amplifier is tested individually.

As the initial output power will be fairly low on setting up, 2 W resistors are adequate. If a cheap $8 \Omega 2$ loudspeaker is available to monitor each channel as it is set up, so much the better. Do not, however, risk a good loudspeaker at this stage.
Turn the presets on all power amplifier channels to maximum, that is clockwise. Reduce all level and balance controls on the master board to minimum and set the tone controls mid-way.

## COMPONENTS

## Resistors

Headphone load resistors $220 \Omega \frac{1}{2} \mathrm{~W}$ ( 4 off) Dummy load for testing $120 \Omega \frac{1}{2} W$ ( 15 off )

Plugs and Sockets

## Speaker sockets

Tape in/out sockets
Aerial socket
Headphone sockets
CD4 connector
SQ edge connector
QS Variomatrix Synthesise socket QS edge connector Fuse holder
${ }_{5} \mathrm{pin}$ DIN (4 off)
5 pin $180^{\circ}$ DIN (2 off)
Coaxial recessed
Switched stereo headphone sockets (2 off)
B9G valve base
16 way 0.15 in pitch edge connector

8 way 0.15 in pitch edge connector
8 way edge connector
20 mm chassis type

## Switches

Push button bank, 4 bank, 17.5 mm spacing, with each bank
6-changeover per bank

## Wiring

32 ft 14/0.0076in stranded single p.v.c. (yellow 3 ft , blue 3 ft , red 5 ft , green 5 ft , white 5 ft , pink 3 ft , brown 6 ft , black 2 ft )
$20 f t$ twin screened lightweight audio wire
2 ft single screened light co-ax.
8 ft lacing cord
Mains lead 3-core to suit
2 ft tinned copper $16 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. wire

## Materials

Aluminium extrusion for facia (available from Sonax Electronics) or plain 18 gauge sheet aluminium if alternative construction method is used. Aluminium " $L$ " or " $U$ " form and $\frac{3}{8}$ in rod for support members for facia. Boxform surround (from Sonax) or wood to make

## Miscellaneous

3-way terminal tag strip
Rubber feet ( 4 off)
Grommet $\frac{1}{2}$ in $\times \frac{1}{4} \mathrm{in}$, sleeved grommet for mains lead
$\frac{1}{2}$ in 4BA roundhead screws (17 off)
4BA nuts, plain washers and lock washers (17 off)
甬in 6BA roundhead bolts ( 16 off)
$\frac{1}{2}$ in 6BA roundhead bolts ( 6 off)
sin 6BA roundhead bolts ( 3 off )
6BA nuts, plain and lock washers ( 25 off)


Connect a d.c. millivoltmeter across resistors R29 and R30 as shown in Fig. 4.6 on one power stage. The sum of these two resistors is approximately 1!. Switch on the complete system.

At this stage a variable input transformer (Variac) to adjust the mains supply slowly is very useful, but not essential.

The millivoltmeter should now read from 2 to 10 mV d.c.
If the readiff is more than 50 mV switch off and check wiring again. If all is well, slowly rotate the preset VR8 anticlockwise until a reading of approximately 20 mV is obtained. This reading corresponds to approximately 20 mA quiescent current.

Disconnect the meter and repeat the procedure on all the remaining power amplifiers in turn.

The main amplifiers are now set for optimum quiescent current conditions and should not require re-setting at all.

## FINAL MECHANICAL ASSEMBLY

The master volume and tone board, preamplifier board and quadraphonic selector switch are all assembled on the facia as shown in Fig. 4.1. It must be remembered that the wiring to these boards should be kept as short as possible to avoid interference and hum. However, they must be sufficiently long to allow both initial assembly and possible later dissembly.

The facia may now be attached to the trough by its pillars and 4BA screws inserted upwards from beneath the trough in the holes provided.

The surround may now be placed over the facia and dropped down to engage with the lips on the trough for either of the two fixing methods described earlier to be effected.


Fig. 4.5. Drilling details of the Tone/Master volume board to suit the facia of Fig. 4.4a.


Fig. 4.6. Location of the test points for measurement of the quiescent current in the power amplifiers

Where "spring" locating method is used to retain the surround the exact fit is adjusted as required by applying a slight set to the sprung chassis sides. Be careful not to overdo the tension as this will make subsequent removal of the surround difficult.

Ideally the springing should just cause the flanges to "bite" the surround as it is lowered into position and adjustment can be made in small steps until correct setting is achieved.

To remove the surround using the same method it is simply a matter of placing the finger tips against the long sides from below and pressing lightly inwards until the lips of the flanges release from the grooves. The approach from below is important as working from above is rather difficult. Thus it is simplest to place the unit on a box or other object first so that the hands can be positioned lower than the bottom of the unit.

After releasing from the grooves a gentle upward pressure will slide the surround free for removal.

## EARTHING

The use of a wiring loom reduces the problems encountered with hum and stray pickup and it is for this reason that we have described a loom here. Further steps can be taken to minimise these unwanted signals.

Firstly, ensure that both screens are electrically connected to the main chassis which must be itself

Table 4.1 WIRING OF QUAD SELECTOR SWITCH

TOP SIDE WIRING

| TOP SIDE WIRING |  |  |  |
| :---: | :---: | :---: | :---: |
| $\left.\begin{array}{l}\text { Join } A 8, C 8, E 8, G 8=R_{T} \text { input } \\ \text { Join } B 8, D 8, F_{8}, H 8=L_{T} \text { input } \\ \text { Join } A 5, C 5, E 5, G 5=L_{F} \\ \text { Join } B 5, D 5, F 5, H 5=L_{B} \\ \text { Join } A 2, C 2, E 2, G 2=R_{F} \\ \text { Join } B 2, D 2, F 2, H 2=R_{B}\end{array}\right\}$ To Fader Inputs |  |  |  |
| UNDERSIDE WIRING |  |  |  |
| Synthesise | $\left\{\begin{array}{l}R_{F}=3 A \\ R_{B}=3 B\end{array}\right.$ | $\mathrm{L}_{\mathrm{F}}=6 \mathrm{~A}$ $\mathrm{~L}_{\mathrm{B}}=6 \mathrm{~B}$ | $\begin{aligned} & \mathrm{R}_{\mathrm{T}}=9 \mathrm{~A} \\ & \mathrm{~L}_{\mathrm{T}}=9 \mathrm{~B} \end{aligned}$ |
|  | $\left\{\begin{array}{l}R_{F}=3 \mathrm{C}\end{array}\right.$ | $\mathrm{L}_{\mathrm{F}}=6 \mathrm{C}$ | $\mathrm{R}_{\mathbf{T}}=9 \mathrm{C}$ |
| SQ | $\left\{\begin{array}{l}R_{B}=3 D\end{array}\right.$ | $\mathrm{L}_{\mathrm{B}}=6 \mathrm{D}$ | $\mathrm{L}_{\mathrm{T}}=9 \mathrm{D}$ |
| QS | $\left\{\begin{array}{l}R_{F}=3 \mathrm{E} \\ \mathrm{R}_{\mathrm{B}}=3 \mathrm{~F}\end{array}\right.$ | $\mathrm{L}_{\mathrm{L}}=6 \mathrm{E}$ | $\mathrm{R}_{\mathbf{T}}=9 \mathrm{E}$ $\mathrm{LT}_{\mathbf{T}}=9 \mathrm{~F}$ |
| CD4 | $\left\{\begin{array}{l}R_{B}=3 \mathrm{~F} \\ \mathrm{R}_{\mathrm{F}}=3 \mathrm{~S}\end{array}\right.$ | $\mathrm{L}_{\mathrm{F}}=6 \mathrm{G}$ | $\mathrm{R}_{\mathrm{T}}=9 \mathrm{G}$ |
|  | $\left\{\begin{array}{l}R_{B}=3 \mathrm{H}\end{array}\right.$ | $L_{\text {B }}=6 \mathrm{H}$ | $\mathrm{L}_{\mathrm{T}}=9 \mathrm{H}$ |

Rows 1, 4 and 7 have no connections
connected to mains earth. Thus if there is any doubt about good conduction between the screens and chassis it is advisable to either insert a wire link or clean the adjoining faces thoroughly before assembly.

Secondly, there is a very useful technique which can be applied to the rondo screened leads. Simply make certain that all screens are earthed at the end nearest to the signal source for that particular length of lead. With a system as complex as the RONDO this does make for complexity in deciding which end must be earthed but the results bear out the effort. The constructor may find Fig. 1.15 in the September issue of Practical Electronics useful in this context.

If hum is experienced and the circuitry in the area of the decoders is suspected it is advisable to remove the earth connections from both ends of the screened leads between the boards and the selector switch and replace each connection in turn until the hum loop is isolated. This may involve connecting from either end of a cable.

## NOTE.

The output transistors in the power amplifiers should be MJE 3055K and MJE 2955K.

Next Month: Loudspeaker enclosure design and construction


## RADIO STARS

In the early days of radio astronomy astronomers were constantly pointing out that there were radio sources but no known radio stars. In consequence the actual discovery on rare occasions of a radio star made headlines. Now, however, particularly over the last few months, quite a number have been added to the list. The chance discoveries have now been supplemented by those discovered as a result of a definite programme of search.

Theory suggested that an early type of star which shows emission lines and an excess of infra-red would be a candidate. It is maintained that the infra-red occurs in the surrounding dust and gas. This was the place to look for radio emission.

It is quite a neat piece of work by a team from the Algonquin Radio Observatory in Canada since a comparatively small telescope was used. The telescope operates at a wavelength of 2.8 centimetres and the dish is a mere 46 metres in diameter. Drs Feldman, Marsh and Purton have managed to secure this scoop with apparent ease.

Now, no doubt, the larger telescopes will turn their attention to the matter. Since the astronomers will now know what to look for and where to look, it is to be expected that more will be found and new data will be obtained. It could mean that a new and more successful model of infra-red stars will emerge.

## ANOTHER INTERPRETATION OF THE SIBERIAN METEORITE

The spectacular terrestrial catastrophe that took place in Siberia in 1908, has led to much speculation. No remnants of the meteorite have ever been found so many quite bizarre explanations have been forthcoming, from a crashed space vehicle to a lump of anti-matter.

The force that produced the blast is said to have had an energy output of 0.2 to 20 megatons. The physical effect of this is observable even after many years. There is no crater as such for it is a swampy area.

Dr Stephen Hawking has suggested, in the last year or so, that if black holes do exist they would be of all sizes. Many of these could be quite tiny and may well have been formed after a "big bang" start to the universe.

Since in their travels these small units would suck into themselves matter through which they passed they may well be at the centre of stars and even galaxies. Perhaps here might be found a solution to the problem of gravitational waves.

From the University of Texas comes a suggestion by Dr A. A. Jackson and Dr M. Ryan. They put

forward the idea that one of the small black holes moving at high speed and passing through the atmosphere would produce temperatures of the order of $10^{5}$ degrees K .

This would cause ultraviolet radiation and a plasma column would be formed. The black hole would pass right through the Earth because of its small size but would have the mass of an asteroid. This energy would carry it onwards into space.

The plasma column would be dissipated in the surrounding area of entry. This plasma column would be of a deep blue colour. Is it perhaps significant that the many eyewitnesses described the appearance of the sighting as a "bright blue tube".

## EXTRA VEHICULAR ACTIVITY

A new method of control for astronauts is under development by the RCA Company. The astronaut's voice is used to control movements.
This is a truly significant move. It means that the actual movements required can be initiated by voice commands only. There are 12 basic commands that operate the manoeuvering and propulsion system. Thus right, left, up, down, etc. can be brought to any situation. A dream come true for many applications. It is surely not far from this point to the control of vehicles in terrestrial situations.

Other activities planned for the future concern two satellites to be launched in 1975. Some of the instruments to be carried are for the determination of the immediate Earth environment. More data will be made available from the higher levels of the atmosphere particularly the thermosphere. The sort of instrumentation that is required for this work includes an electron tem-
perature probe as well as the usual photometers and spectrometers.
The data to be gathered will be neutral particle and ion compositions, ion and the natural gas temperature, information about the air-glow and the detection of thermal electrons and photoelectrons.

The satellite will weigh about 1,300 pounds and will carry a momentum wheel for stabilisation.

## SKYLAB PRELIMINARY RESULTS

So much data has been gathered on the second Skylab period of observation, that it will take some years to evaluate it all.
Perhaps the most consistent of the findings relate to the Sun. The better observation of the structure of the atmosphere of the Sun and in particular the great hole that has been found in the corona may unlock secrets far away from the Sun.

Recently Dr C. H. Barrow of the University of the West Indies has been trying a new correlation of micropulsations from the Sun and those observed in the radiations from Jupiter.

It could well be that the information returned from the Jupiter probe, which should be close to the planet on December 10th, will help to establish a positive result. The micropulsations have been known for some years but because of lack of data from the Sun the matter was only spasmodically reviewed.

The hypothesis involved is an important one for, though there have been a number of models evolved, all lack the sort of confirmation required to establish the facts.

## COMET KOHOUTEK

Skylab will have a special mission with respect to the comet Kohoutek. The next mission (Skylab 4) is the last in the projected series and begins on November 9th.

Seven of the existing instruments will be brought to bear on the comet and the astronauts will have with them a new far-ultraviolet camera. It should be possible to photograph the neutral hydrogen cloud which is estimated to surround the comet and extend to more than six million miles.

Initially the plans are for the Skylab mission to be completed by January 4th. It would be a pity if this could not be extended to January 14th to allow further observation. Such a unique opportunity to study the period immediately after the perihelion passage may never come again.

The best time to view the comet for Earth-based observers is at about 12.00 to 14.00 hrs , right ascension, in the morning sky near the area of the bright star Spica. This will be around December 4th.

# PE Sound Synthasiser 11 

## 

## By G.D.SHAW

THe article this month deals with the remainder of the electronics sited within the keyboard unit and details the divider system, the analogue memory or hold circuits, modulation amplifiers, envelope shaper/v.c.a.s and mixer. The overall system has been extensively redesigned to take maximum advantage of the greater versatility of the logarithmic v.c.o.s and with the aim of improving the live performance capability of the instrument.

## BLOCK SCHEMATIC

A block schematic arrangement of the keyboard unit is shown in Fig. 11.1 and the unit has been designed to accommodate a four-octave KimberAllen keyboard. The specified keyboard may be obtained through the Electronic Organ Constructors Society at 4 Lees Barn Road, Radcliffe-on-Trent, Nottingham NG12 2DS. The E.O.C.S are also able to supply the contact assemblies and mounting strips. The type of contact assembly required is the G.B.- 2 paired contact unit, also by Kimber-Allen.

Although a four-octave keyboard is specified it should be made clear that smaller-or larger-units may be employed with no changes to the circuitry other than the adjustment to the number of divider resistors employed. With respect to the use of smaller keyboards, the E.O.C.S. have informed the author that they have a limited number of twooctave organ keyboards by Herrburger Brooks.

These are full sized timber keys faced with plastic and mounted on a hardwood frame. The keys themselves are in reverse colours with black naturals and white sharps, and although they will require to be sprung by the constructor, the additional work required is reflected in the attractive pricing of £5 per keyboard.

Reverting again to Fig. 11.1 it will be seen that the keying system is divided into two channels each channel having its own electronic assemblies and signal path. Signals from both channels join together in the final circuit, a simple virtual-earth mixer. The purpose of this arrangement is to allow a rhythm accompaniment and melody line to be programmed at the same time, channel 1 programmed by the upper 31 keys and channel 2 by the remainder.

The tuning arrangement allows the transition between the two channels to be musically consecutive. Spread apart by one or more octaves or the channels juxtaposed in termis of frequency with the 31 note channel providing a bass line to a treble channel 2. Since the combined effect of the tuning controls is continuously variable there are a number of intermediate possibilitie's such as channel 2 dupli-


Fig. 11.1. Block schematic of keyboard unit


Fig. 11.2. Keyboard divider network

COMPONENTS

## DIVIDER

Resistors
R1 $10 \mathrm{k} \Omega$
R2 $20 \mathrm{k} \Omega$
R3 $510 \Omega$
R4-R51 $47 \Omega$ ( 48 off)
R52 $510 \Omega$
R53 $20 \mathrm{k} \Omega$
R54-R56 $10 \mathrm{k} \Omega$ (3 off)
R57 $2.5 \mathrm{k} \Omega$
R58 $330 \Omega$
R59 $8.2 \mathrm{k} \Omega$
R60 $390 \Omega$
R61 $2.1 \mathrm{k} \Omega$
All 2\% metal oxide
Integrated circuits
ICl-IC2 741C (2 off)
Potentiometers
VR1 $1 \mathrm{k} \Omega$ semi-precision wirewound
VR2 $10 \mathrm{k} \Omega$ midget moulded linear carbon
VR3 $500 \Omega$ cermet
Switches
S1 s.p.c.o. miniature toggle
S2 d.p.c.o. miniature toggle
cating sections of channel 1 or, in more bizarre terms, both channels programmed in different keys.

The programming voltage from the keyboard is led to a memory circuit which holds the last voltage entered until such time as a new voltage is programmed or until the hold circuits are grounded. The output voltage from the hold circuit is used to program its respective v.c.o. to the desired frequency which is then amplitude modulated in the envelope shaper/v.c.a. Triggering of the envelope shaper takes place each time a key is depressed in the appropriate channel and each envelope shaper is provided with separate attack and decay controls together with an additional percussive attack facility which may be switched in as desired.

Frequency modulation between oscillators may be achieved by means of the modulation amplifiers which have sufficient gain to swing the frequency of the v.c.o.s through the entire audio spectrum. Finally, a link switch is provided to enable both channels of the system to be programmed in parallel.

## THE DIVIDER NETWORK

Fig. 11.2 shows the theoretical circuit of the keyboard divider network in which resistors R4R51 inclusive form the actual divider which is "floated" between the outputs of two operational amplifiers. The output of IC1 is coupled to the high frequency end of the divider and IC2 to the low frequency end. R60, VR1 and R61 together form an adjustable divider which is coupled to the inverting inputs of both i.c.s. Thus, by means of VR1, the main tuning control, the voltage on output of
the i.c.s may be swung through a range of rather more than 8 volts.

Since this latter effect will be equal at both ends of the keyboard it is necessary to apply an offset to one of the i.c.s in order that a voltage differential will exist across the divider chain. The offset is applied to the non-inverting input of IC2 through the medium of either one of two divider chains.

## SPAN FACILITY

R57, VR3, R 58 provide what has been termed the fixed span facility with the preset VR3 having sufficient swing to enable the V/Octave range to be adjusted between about $400 \mathrm{mV} /$ octave to rather more than 1V/octave. R59, VR2 provide the variable span facility which is adjustable over a range of about 8.0 V . The setting of VR3 is normally adjusted so that one octave width on the keyboard spans precisely one frequency-octave. VR2 on the other hand enables the frequency spread of one keyboard-octave to be varied between a fraction of a semitone (micro-tones) to several tens of semitones (macro-tones). The actual effect, in terms of frequency range, resulting from the swing on both VR2 and VR3 will depend very much on the requirements demanded by the v.c.o. as a result of the "Law Adjust" setting.

The exact value of the divider resistors R 4 to R51 is not too critical except that they should be of sufficiently low a value so that the combined loading of the v.c.o.s does not cause a measurable change in the voltage at any point on the divider. Values between 10 and 60 ohms should meet all the necessary criteria. For best results, however, it is important that, whatever the nominal value of divider resistor chosen, the individual resistors are


Fig. 11.3. Circuit of hold, modulation amplifier and mixer for both channels with v.c.o. interconnections. The component values for the mirrored hold and modulation amplifier circuits are identical

## COMPONENTS ...

## HOLD CIRCUIT (2 off)

| Resistors |  |
| :--- | :--- |
| R62 | $1 \mathrm{M} \Omega$ |
| R63 | $5 \%$ carbon |
| R63 | $470 \mathrm{k} \Omega$ |
| R64 | $270 \mathrm{k} \Omega$ |
| R carbon |  |
| R65 | $100 \mathrm{k} \Omega 5 \%$ carbon |
| R66 | $47 \mathrm{k} \Omega 5 \%$ carbon |
| R67 | $20 \mathrm{k} \Omega 2 \%$ metal oxide |
| R68 | $20 \mathrm{k} \Omega 2 \%$ metal oxide |

Potentiometers
VR4-VR6 $10 \mathrm{k} \Omega 15$ turn cermet

## Capacitor

C1 $1 \mu \mathrm{~F} 63 \mathrm{~V}$ polyester
Integrated Circuits
IC3-IC4 741C

## Switches

S3 2-pole 6-way
S5 d.p.c.o. toggle

MODULATION AMPLIFIER (2 off)
Resistors
R69 100k $\Omega$
R70 33k $\Omega$
Integrated Circuit
IC4 741C
Potentiometer
VR7 $10 \mathrm{k} \Omega$ midget moulded linear carbon

Switches
S6 s.p.c.o. miniature toggle
S7 2-pole 3-way

## MIXER

Resistors
R71-R73 10k $\Omega$ (3 off) $5 \%$ metal oxide

Integrated Circuit
IC5 741C
as closely matched to the nominal value as possible. It is particularly important that the ohmic value of any 12 consecutive resistors in the divider should be a close match with any other selection of 12 consecutive resistors.

The junctions between individual resistors in the divider are hard wired to the moving contact of their respective contact assemblies mounted below the keyboard, the fixed contacts being joined into two bus-bar units which can be joined by means of a link switch. A similar arrangement is employed for the second pair of contacts which serve to provide the sync pulse necessary for the envelope shapers.

## ANALOGUE MEMORY

The divider voltage resulting from the depression of any particular key is routed into the analogue memory circuits via S3 and S4 as shown in Fig. 11.3. The purpose of the hold circuit is to retain the last programmed keyboard voltage for sufficient time to enable the desired tone processing to be completed. For example, with S 4 in position 1, the depression of a key is sufficient to cause Cl to become charged to the value associated with that particular key. At the same time a sync-pulse is routed to the envelope shaper which, if it is set to provide a rapid attack, will turn on the v.c.a. and allow the oscillator tone to be heard. If the envelope shaper is also set to provide a long decay, the oscillator tone will immediately begin to die away.

In operation the hold circuit utilises the commonmode rejection of the 741 operational amplifier to provide a very high input impedance. Positive and negative feedback are applied by means of R67 and R68 with VR4 serving to provide a balance between the respective levels of feedback to the inverting and non-inverting inputs of the amplifier. Cl is the reservoir capacitor and is coupled directly to the non-inverting input.

The input impedance of the circuit is given by the paralleled value of R67 + part of VR4, and R68 + part of VR4 times the open loop gain of the amplifier. Thus depending on component tolerances the input impedance can be anywhere within the range 250 to 2,500 megohms and since a $1 \cdot 0 \mu \mathrm{~F}$ capacitor is specified the leakage time constant of the network will similarly vary between 250 and 2,500 seconds.

## PORTAMENTO

When keyboard voltages are routed direct to Cl in the hold circuit the change in level of the charge on Cl is virtually instantaneous. However, if a resistance is interposed between the keyboard and Cl the rate of change of charge is inversely proportional to the value of the resistor. This provides a very convenient means of adding a portamento facility and R62-R66 are included for this purpose, being switched in as required by S 4 .

Portamento is the name given to the effect when the transition between two successive notes in a musical piece is accomplished in a gliding manner encompassing all the intermediate frequencies.

The nature of the hold circuit requires that the setting-up procedure be followed with great care
since any output offset voltage present will inevitably cause the holding ability of the circuit to wander. With VR4 in its electrical mid position, and with the wiper grounded, a 10 megohm resistor is connected between the output and inverting input of the amplifier. With power on, VR5 is then adjusted so that the output is precisely zero when observed on the most sensitive setting of the oscilloscope. When satisfied that the initial setting up has been correctly accomplished the circuit connections may be made as generally shown in Fig. 11.3 but omitting the connections to the v.c.o. and portamento resistors. With power on again, and observing the output of IC3 on the oscilloscope, apply about -6 V transiently to the junction of R67 and C1. Careful adjustment of VR4 will result in virtually negligible drift and, in the prototype, it was found that a drift of $6 \mathrm{mV} / 20$ minutes was quite easily attainable.

The -6 V charge on Cl during the setting-up procedure is also quite an important value since it will be found that the circuit will have a much greater degree of drift if the applied voltage is significantly higher or lower than this value. For this reason S5 is provided to ground the input of the hold circuit during switch-on or when the keyboard is "idling" for any length of time thus ensuring that the v.c.o. is not over or under driven.

The output of the hold circuit is routed directly to the R 10 input of the v.c.o. the three output waveforms of which are, in turn, routed to a selector switch. S7.

## MODULATION AMPLIFIERS

The wiper of S7 is coupled to the v.c.o. level control VR6 and also directly to the non-inverting input of what has been termed the modulation amplifier. The output of the modulation amplifier driven by VCOI is then routed to the R11 input of VCO 2 through S 6 , a similar arrangement existing between VCO2 and the RII input of VCOI.

The net result of this arrangement is that each oscillator can frequency modulate the other either separately or at the same time. Although simple in concept this system is capable of generating waveforms having very complex harmonic structures and is thus able to produce an enormously wide range of sounds and effects.

In the modulation amplifiers R69 and R70 set the gain at about 4.5 and VR7 provides a modulation depth control. S5a/b provide a means of turning VCO2 off in the sense that its input and output are isolated and its frequency controllable either by its own manual frequency control or by its associated modulation amplifier or both. The main purpose of this arrangement is to allow VCO 2 to provide a vibrato modulation to VCOI.

## ENVELOPE SHAPERS

From the wiper of VR6 the v.c.o. signal is routed into a v.c.a. based on the MFC6040 which is, in turn, controlled by an envelope shaper triggered by depression of any of the keys on the keyboard. The working of the circuit shown in Fig. 11.4 is as follows.

IC1-TRI represent a current amplifier/follower with overall feedback. The output at the emitter normally is +4.5 V under quiescent conditions thus


Fig. 11.4. Circuit of keyboard envelope shaper and voltage controlled amplifier
ENVELOPE SHAPER (2 off)
Resistors

| R1 | $91 \mathrm{k} \Omega$ | R8 | $10 \mathrm{k} \Omega$ |
| :--- | :--- | :--- | :--- |
| R2 | $10 \mathrm{k} \Omega$ | R9 | $3.9 \mathrm{k} \Omega 2$ |
| R3 | $3 \mathrm{k} \Omega$ | R10 | $3 \mathrm{k} \Omega \Omega$ |
| R4 | $47 \mathrm{k} \Omega$ | R11 | $15 \mathrm{k} \Omega$ |
| R5 | $200 \mathrm{k} \Omega$ | R12 | $390 \Omega \Omega$ |
| R6 | $91 \mathrm{k} \Omega$ | R13 | $10 \mathrm{k} \Omega$ |
| R7 | $20 \mathrm{k} \Omega$ | R14 | $1 \mathrm{k} \Omega$ |
| All $5 \% \frac{1}{2} W$ carbon |  |  |  |

Transistors
TR1-TR2 BC209C (2 off)
Integrated Circuits
IC1-IC3 741C (3 off)
IC4 MFC6040
Diodes
D1-D3 1N914 (3 off)
D4 1GP7
D5 BZX61 V Zener
D6 1GP7
Capacitors
C1 $1 \mu \mathrm{~F}$ polyester
C2 $0.22 \mu \mathrm{~F}$ polyester
C3 $2.2 \mu \mathrm{~F} 35 \mathrm{~V}$ tantalum
C4 $4.7 \mu \mathrm{~F} 35 \mathrm{~V}$ tantalum
C5 $\quad 4.7 \mu \mathrm{~F} 35 \mathrm{~V}$ tantalum
C6 1,000pF polystyrene

## Miscellaneous

S5 d.p.c.o. toggle, S7-4 pole 3 way rotary (2 required), VR6$10 \mathrm{k} \Omega$ midget moulded carbon ( 2 off), 2 mm miniature sockets (12 off), 1-4 octave keyboard, G.B-2 pair contacts (49 off) (see text), contact locating strip.
driving ICI hard negative, or to -12.5 V as determined by the divider R3-R5. With a negative input signal to the non-inverting input of IC2 the output of this device is also negative and TR1 is turned off. With TR2 off the control input of the MFC6040 rises to +6 V and thus attenuates the audio input signal by about 77 dB .

The application of a negative trigger pulse to the input of ICI causes TRI to turn off and the output at R2 to go to -15 V . C1 thus discharges via D2/VR2 and the output of IC2 rises from -12.5 V to about -4 V . Under these conditions the noninverting input of IC3 becomes positively biased, its output goes positive turning on TR2 which thus effectively short circuits R10 and causes the control voltage to IC4 to fall to about +4.3 V . When the trigger pulse is removed Cl charges to a level again via DI/VRI and the original situation is positive restored.

A separate percussive attack can be obtained by differentiating the trigger pulse to the envelope shaper by means of C2. The negative differentiated trigger pulse is applied to the inverting input of IC3 with the effect previously described except that in this case the magnitude of the pulse causes the v.c.a. control voltage to fall to $+3 \cdot 7 \mathrm{~V}$ corresponding to an audio signal amplification of about 12 dB . The percussive attack may be used on its own by advancing the trapezoid attack control to the slowest rate and playing the keys in a staccato manner. Alternatively the percussive attack may be mixed with the normal trapezoid control waveform or it may be switched out altogether by means of S1.

The audio signal outputs of the envelope shapers are led to a simple unity gain, virtual earth mixer shown in Fig. 11.3. The level of signal from each channel is controlled directly from VR6 on each of the oscillators.

Next month: construction of the keyboard housing, wiring and tuning instructions. Details will also be given of a small p.s.u. which will enable the keyboard unit to be operated independently of the main synthesiser.

## Strictly

## by K. Lenton-Smith

STUDENTS of the Hammond organ can usually detect aurally which models use tone wheels and which use integrated circuits. The "Concorde", introduced over a year ago, was the first Hammond drawbar organ not to use tone wheels. Using L.S.I. techniques it is now possible to synthesise the unique sounds produced by these electromagnetic devices.
Another novel feature of this organ is the multiple derivative divider which divides down the 12 top notes to the sub-octave frequencies giving locked tuning.
Both of these features are also found in the "Regent" cinema type organ which was released recently from the same stable. An adjunct to both instruments is the Automatic Rhythm 3 unit which is unusual in that the waltz may be selected with any other pattern for a rhythm variation (such as waltz/cha-cha!).

## NOTHING NEW

There seems to be nothing radically new in the manufacture of electronic instruments at present. The various makers appear to be using integrated circuits wherever possible, having relegated the transistor to "slave" duty.


The Lowrey Venus Stereo with a.o.c. and a Genie supplying rhythm patterns

Though R/C oscillators are usually considered to be less stable than L/C oscillators, manufacturers are now using carefully designed R/C master oscillators-presumably to reduce weight and the possibility of interaction on small printed circuit boards. The Lowrey "Genie" uses this system.

Lowrey are transistorising their automatic orchestra computer circuit, which hitherto used a diode matrix. Unless you play a Lowrey, a.o.c. will not mean much, but the sound is probably unconsciously recognised by those that enjoy light music. Harry Stoneham began to broadcast regularly some six years ago and has been featured by Sam Costa, in "Breakfast Special" and on the Pete Brady Show: more recently, he has appeared in Michael Parkinson's programme. His distinctive sound is usually produced on a Lowrey with the a.o.c. in action, though Harry also plays Hammond with equal dexterity.
A.o.c. allows the performer to play a single note melody on the upper manual (at the selected pitches) which is automatically harmonised with any chord played on the lower manual. Whilst this feature was probably designed with the beginner in mind, the experienced player can produce breathtaking runs of chords. Lelt hand chords must be sustained when using a.o.c. as the harmonising facility is lost when the accompaniment keys are released.

## REVERBERATION

An electronic instrument played in a public hall may not need reverberation, though a crowd of people will absorb both reverberation and output power. In a small room with fitted carpets and curtains, the instrument will be dead without some reverberation. Adding echo makes the sound source seem to come from deeper within the speaker enclosure and gives a more natural effect.
Tape, delay lines or spring units may be used, the latter still being the
simplest. Some commercial spring units are too small and consequently produce short delay times, often with too much "direct" signal that can only be reduced by going to work on the circuit board.

It is possible to add reverberation to an existing installation without running to the expense of a further power amplifier if some care is taken. The main amplifier loudspeaker signal is tapped off and fed to the secondary of a small output transformer. It is a good precaution to put a $100 \Omega$ resistor in series with one lead to prevent robbing, and a small 6 V lamp in series with the other to act as a current limiter. The primary winding of this transformer feeds the driver coil of a magnetic unit such as the Gibbs-Hammond.

The driven coil produces only a few millivolts and requires a preamplifier with a gain of about 50 . It is a fairly easy matter to arrange a pair of BC109 transistors, directly coupled, to recover the signal. Small capacitors should be used at both input and output of this preamplifier. The base of the first transistor should be biased by means of a resistor from the emitter of the second transistor.

A $50 \mathrm{k} \Omega$ potentiometer across the pre-amp output is suggested, with a $T$ attenuator from the slider followed by 250 pF before feeding into the main amplifier at a point after the main volume/swell control. The small capacitor teuds to accentuate top response. Needless to say, there is some danger of howl due to feedback and the $50 \mathrm{k} \Omega$ variable should be kept near minimum while setting up. Ideally, the spring driver coil should be fed from a push-pull driver amplifier, but the method outlined above will probably give sufficient echo for most needs, and it has the merit of simplicity.


The Hammond Regent

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## g

 BATITERTV ELIMINATOR BY A.M.RUDKIN ${ }_{\text {b.sc.(Eng.) Hons. }}$THERE are many battery operated transistor radios which are used almost entirely in the home, and with the rising cost of replacement batteries the question of a battery eliminator comes to mind. To the home constructor the thought of buying a ready-made unit goes against the grain, but it is not easy to achieve a professional finish in a home-made unit. Fortunately, the battery manufacturer provides us with an easily available case of exactly the right size. The current trend amongst manufacturers is to use a thin metal casing and a battery case of this type can be re-used quite successfully.

Most portable radios used in the home take PP9 batteries or an equivalent and this size is large enough to hold the necessary components to make the eliminator. With a component cost of about f1.50p the unit will pay for itself quite quickly and, of course, the eliminator can easily be removed whenever battery operation is required.

## CIRCUIT DESCRIPTION

As can be seen from Fig. 1, the circuit of the battery eliminator is relatively simple, but despite the simplicity the unit delivers a regulated output voltage and provides protection against overloading or short circuits.


Fig. 1. Circuit diagram of the 9 V Battery Eliminator

A miniature mains transformer with a centretapped secondary feeds a full-wave rectifier. The reservoir capacitor, C 1 , smooths the rectified output before it is applied to the series regulator circuit. A 10 volt Zener diode, D3, provides a fixed base voltage to transistor TR2, which in turn provides a fixed output voltage of about 9.5 volts at low impedance.

A second transistor, TR1, provides current limiting protection since its base-emitter junction is connected across a current sensing resistor, R2.

When the current flowing through the resistor exceeds 100 mA the transistor begins to turn on and reduces the voltage across the Zener diode thereby reducing the output voltage so that even under short circuit conditions the current through the series regulator never exceeds a safe value.

## COMPONENTS . . .

## Resistors

$\begin{array}{ll}\text { R1 } & 390 \Omega \\ \text { R2 } & 5.6 \Omega\end{array}, \pm 10 \% \frac{1}{2} W$ carbon
Capacitors
C1, C2 $100 \mu \mathrm{~F} 25 \mathrm{~V}$ elect. (2 off)
Semiconductors
TR1 BC107
TR2 BFY51
D1, D2 1N4001 (2 off)
D3 10 V 400 mW Zener
Transformer
T1 Mains primary, 14-0-14 50mA secondary (Henry's type MT991)

## Miscellaneous

Printed circuit board, 4BA studding, mains cable, nuts and washers, old PP9 battery case, interconnecting wire

The graph in Fig. 2 shows the way the output voltage varies with load current and the rapid drop in voltage as the current approaches the 120 mA limit can clearly be seen.

An electronic "fuse" of this kind may seem a luxury but in fact it costs less than a fuse link and fuse holder whilst offering a high degree of protection. The simple regulator used in the battery eliminator is quite adequate for use with radio receivers and the ripple on the output is low enough not to cause any audible hum in the radio loudspeaker.

## MOUNTING COMPONENTS

The electronic components are mounted on two small boards which are supported by screwed rods and it is recommended that printed circuits are used. Dimensions of the boards and the track layouts are shown full size in Fig. 3 and Fig. 5. If facilities for making printed boards are not available then as an alternative $0 \cdot 1$ in matrix board (without copper strip) may be used with point to point wiring.


Fig. 2. Graph showing the variation of output voltage with current. The fall off at 100 mA is due to the current limiting effect of TR1


Fig. 3. The two printed circuit boards used in the Battery Eliminator. Theblack areas indicate copper. Both are full size

Fig. 4. Layout of the components on the two printed circuit boards and interwiring between the two

BOARD 2


## FIG. 5 <br> EXPLODED VIEW



Before mounting the mains transformer onto the printed circuit board shorten the leads to about fin and strip the sleeving back to expose fin of the wire. Mount the transformer on the board and bend back the fixing lugs to hold it securely in place. Fit the other components and interconnect the two boards as shown in Fig. 4.

Temporarily connect a mains lead and, as a safety precaution during testing, cover the mains connections with self adhesive p.v.c. tape. Apply the mains and check that the output voltage of the regulator board is approximately 9.5 volts. A voltage very different from this value indicates a fault condition and the voltages indicated on the circuit diagram (Fig. 1) may be used to aid in fault finding.

## USING AN OLD BATTERY CASE

It is quite easy to take a battery apart, but some care should be taken in order that the casing may be re-used. The battery should not be so old that the cells have started to leak or the case may be damaged.

In the battery used for the prototype the bottom plate was made of plastic and was held in place by
the metal jacket which was folded over the rim of the plate. This fold was carefully straightened by bending back the metal with a small pair of pliers. After this the contents of the battery can be removed by pressing the top plate of the battery downwards.
The six cells are, of course; no longer required, but the other parts should be kept. Contact between the cells and the top plate with the "sriap" connectors is by a thin piece of brass strip and a spring contact. Cut off the brass strip and remove the piece of cardboard which separated the top plate from the cells by cutting around the contacts with a knife blade.
Drill holes in the top and bottom plates in accordance with the dimensions given in Fig. 5. The hole for the mains lead is drilled in the top plate only.

## ASSEMBLY.

When the boards are functioning correctly they can be assembled onto the screwed rods. The distances between the boards and the plates are shown


A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought.
This is YOUR page and any idea published will be awarded payment according to its merits.

## TRACE DOUBLER FOR TTL COMPATIBLE SIGNALS

The diagram in Fig. 1 shows a circuit for a trace doubler, which displays the time relationship between two series of pulses.

Gate Gl and its associated diode plus two resistors and capacitor form a clock generator with a mark to space ratio of 1 to 1 . Gate G3 provides an inverted clock waveform. One input of G4 is the signal input, "A". One input of G5 is the other signal input, "B". The other input of G4 is connected to the output of G3, the inverted clock. The other input of G5 is connected to the output of G2, the true clock.
These two clock signals are always the opposite of


Fig. 1
each other, thus gates G4 and G5 are alternately enabled or disabled. Any output from G4 or G5 is fed to the summing junction of IC3, via a $10 \mathrm{k} \Omega$ potentiometer and a $1 \mathrm{k} \Omega \Omega$ resistor. The operational amplifier combines the signals and feeds them to the oscilloscope to be displayed.

The idea behind the operation of this circuit is that any signal information from input " A " is added to a constant voltage, the inverted clock and is then displayed below the trace for input "A".
The $10 \mathrm{k} \Omega_{2}$ potentiometer VR1 varies the separation between the traces and VR2 in the operational amplifiers feedback path controls the overall gain of the instrument.
C. Nicol, Brixton, S.W.9.

## SIMPLE VARIABLE-DELAY PULSE CIRCUIT

Variable delay time on a repetitive pulse is frequently required, particularly in those applications concerning transient phenomena. A simple, low cost, and easily constructed electronic circuit is described which enables continuously variable delayed times in the range $10 \mu \mathrm{~S}$ to 80 mS to be achieved.
The circuit, shown in Fig. 1, consists of two monostables, the first providing the controlled variable delay time and the second giving the delayed output pulse. The master pulse to be delayed is first differentiated by the R1Cl network. The negativegoing spike obtained from this network is then used to turn the first monostable over. The turn-over period is given by:-

$$
\mathrm{T}=0.7 V R_{1} \times C_{2}, 3, \text { or }{ }_{4}
$$

The positive pulse from the collector of TR1 is fed into the second monostable via another differentiating network. Again the negative-going spike turns the monostable over and a rectangular pulse can be taken from the collector off TR3.

A negative output pulse could be taken from the collector of TR4, but it would be of poor shape due to capacitance C7 charging up via the load R8 in the collector of TR4.

By both making VR1 variable from $100 \Omega$ to $10 \mathrm{k} \Omega$ and by selecting the C 2 , C3, C4 capacitors having fixed values of $0 \cdot 1,1 \cdot 0$ and $10 \mu \mathrm{~F}$ a continuously variable delayed output pulse in the range $10 \mu \mathrm{~S}$ to 80 mS has been obtained.
The delayed times are measured from the negative-going edge of the master pulse. Both shorter than $10 \mu \mathrm{~S}$, and
longer than 80 mS can be obtained by suitable choice of the passive components VR1 and C2, C3 C4.
The minimum width of the output pulse is $2 \mu \mathrm{~S}$. This is varied using VR2 ( $100 \Omega$ to $10 \mathrm{k} \Omega$ ) and C7 ( 4000 pF ).

The sum of the delayed time and the pulse width must, of course, be shorter than the periodic time of the master pulse. The rise and fall times of the output pulse are respectively, 25 and 30 nS .

The delay times of the present circuit have been calibrated against a standard time marker and found to be both reproducible and reliable.

Drs. R. Hackham and P. Johnston University of Sheffield.


Fig. 1. Simple variable-delay pulse circuit


The CIRCUIT of a tachometer shown in Fig. 1 is based on the integrated circuit SN74121. This is a monostable device available for under 50 pence.

The circuit can be adapted for a wide range of meters up to 10 mA f.s.d. by simply connecting a resistor in series with the meter if required. Initially the design was made for a 12 V system but providing the 15022 series dropper is altered there should be no difficulty in adapting for other voltages.

The timing components are the $3.9 \mathrm{k} \Omega 2$ resistor and $1 \mu \mathrm{~F}$ capacitor connected to pins 10 and 11 , and the capacitor should preferably be a reasonable quality non-electrolytic tpye.

Meter movement at very low frequencies may be countered by connecting a capacitor across the meter but a good movement should not need this.

Calibration is via VR1 preferably against a pulse

TABLE 1:
Calibration Frequency corresponding to 1,000 r.p.m.

| No. of <br> Cylinders | 2-stroke | 4-stroke |
| :---: | :---: | :---: |
|  | frequency |  |
| 1 | 16.7 Hz | 8.4 Hz |
| 2 | 33.4 Hz | 16.7 Hz |
| 3 | 50 Hz | - |
| 4 | - | 33.4 Hz |
| 6 | - | 50 Hz |
| 8 | - | 67 Hz |

generator of reasonable accuracy. Calibration frequencies are given in Table 1.
C. J. Nother,

Portsmouth, Hants.

## SCREENWASHER TIMING UNIT

THE device to be described operates the electric screenwashers of a car for a period of up to 10 seconds after a single press of the switch so that one hand does not have to leave the steering wheel for more than a second or so.

Only two main components are used, a relay and a capacitor, and from Fig. I it can be seen that when the washer control button is pressed, Cl is immediately charged up to the full 12 V battery voltage and discharges over a period of 10 to 15 seconds through the coil of RLA so closing the contacts RLA1 and operating the washer pump motor.

As C1 discharges through the relay, the current eventually falls to below the hold-in value for the relay, contacts RLA1 separate and the pump stops.

VR1 is used to set the operating time of the pump motor. By filing the copper rivet on the armature flat with the face, the hold-in time can be slightly increased and also has the advantage that the relay drops out suddenly so preventing arcing of the contacts which might occur if they separated more slowly.

The relay used is a PO 3000 type with a $1,000 \Omega$ coil with all the contacts removed except for one pair of "make" contacts to increase sensitivity, though if a second pair was fitted combined wash and wipe with "one shot" operation could be achieved.

The can of Cl should be completely insulated before mounting, using p.v.c. tape or tube and the


Fig. 1. Arrangement of the screenwasher unit
complete unit should be mounted in a closed steel case in a dry spot away from exhaust pipes. The prototype has functioned perfectly over 1,000 miles with no maintenance being required.

The circuit shown is for 12 V negative earth systems. For positive earth the connections to Cl and the washer pump motor merely need to be reversed.

The dotted lines in Fig. 1 show a slight modification which is necessary where the existing switch operates the original washer circuit by shorting one side of the motor to earth, the other side being permanently live, as is often found in the horn circuit.

In both cases, connection to the supply should be via a 5A fuse to a "live when on" part of the ignition switch or terminal A4 on the fuse box.
A. Calder,

Leigh, Lancs.



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COMPOR1RTT PANRL， 240481 diodes， 10 p ，p．p． 6 p ． VEEDER ROOT RLECIRICAL MMPULBE COUFTRE TOM－REGETABLE，A．C． $200-280 \mathrm{~V}$ ， $81-10, \mathrm{p} . \mathrm{p}, 13 \mathrm{p}$ ． GRC MAIMS CIRCUIT BREAKRES， 2 amp or 5 amp， 11 each，p．p．14p．
LETER ACTION P．O． 1000 TXRE BWITCHES Lock 4－pole changeover， $15 p$ ，p．p．4p．Ex equip Lock 2 －pole changeover， 10 p，p．p．4p．Ex equip． MULLARD \＆MALLORY GCREW TERMEMAL CAPACITORS $4,500 \mu \mathrm{~F} 64 \mathrm{~V}, 7,100 \mu \mathrm{~F} 40 \mathrm{~V}, 50 \mathrm{p}$ each $20,00030 \mathrm{~V}, 25,00025 \mathrm{~V}, 35,000 \mathrm{15V}, 30 \mathrm{p}$ each p．p． 21 p ．
MULLARD FULLTAVE RECTMFIERB
$6.48 \mathrm{~V}, 15 \mathrm{amp}, 75 \mathrm{p}, \mathrm{p} . \mathrm{p} .10 \mathrm{p}$ ．
BELLING LRE $1 \cdot 5 \mathrm{smp}$ in－line rubber covered interference suppressor， 25 p, p．p． 8 p．
ROBBER 8 PIN 5 AMP NON－REVBRGIBLE CABLE CO2NECTORS，20p，p．p．5p．
8OLEHODS 12 VOLT PULL ACTIOR
$2 \ln \times 1 \ln \times \operatorname{in}, 40 \mathrm{p}$, p．p． 8 p ．
soLswomg 12.24 V d．c．pull action 1 in $\times 1$ in $\times$ $1 \frac{1}{2} \mathrm{n}, 40 \mathrm{p}, \mathrm{p} . \mathrm{p} .5 \mathrm{p}$ ．
SOLEHOMS 240 V a．c．pull action $2 \mathrm{ifin} \times 1$ in $\times$ $1 \pm \ln , 50 \mathrm{p}, \mathrm{p} . \mathrm{p} .9 \mathrm{p}$ ．
SATGAMO WESTOM TDEE LAPGED METER
Mains operated． $1 \frac{1}{3}$ in $\times 1 \frac{1}{2}$ in $\times 2 \mathrm{in}, \mathbf{8 1 . 5 0}$ p．p． 7 p ． ARROW RELAYY， 240 V a．c．coil，double pole change over， 1 make contact＇s 10A， 240 V a．c．， $25 \mathrm{Fp}, \mathrm{p} . \mathrm{p} .9 \mathrm{p}$ ． OIRON MKE LIDGET POWER RELAY，12V d．c． Double pole changeover．New，70p，p．p． sp ．
gTC VARLEY，miniature relays $700 \Omega, 17 \cdot \bar{j}-37 \mathrm{~V}$ ， perspex cover， 4 pole changeover， $40 \mathrm{p}, \mathrm{p} . \mathrm{p} .5 \mathrm{p}$ ．
POTTEA BRUMFIELD 12V d．c． 3 pole changeover with base，contacts rated 74 d．c．，81，p．p．10p．
L．T．T．LOW PROFILE RELAYB． 4 pole c／overs． $500 \Omega$ 12－18V，75p，p．p．5p．
MADS RELAYB， $200 \cdot 250 \mathrm{~V}$ a．c． 2 makes．Heavy duty contacts， 50 p，p．p． 7 p．
TELESCOPIC AERIALS
Chromed 7 in cloeed， 28 in extended， 6 section ball jointed base，28p，p．p． 5 p new
PRIFTTED GIRCOIT BOARD／19 ACY 19＇s 10 OA200 Diodes： 1 reed relay： 1 AZ 229 zenuer ass，capacitor 240 V a．c．11，p．p． 25 p ．Ex equip．
WIRDIG CABLE
Size－1．020．Various colours．350yds，60p，p．p．28p TAPE POSITIOI IHDICATOR
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All orders add $10 \%$ V．A．T．
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3 Shenley Road
Borehamwood，Herts．
Tel．01－953 6009

## MAINS NEON FLASHER

THis is a circuit which I have developed to remind you to un-plug mains appliances as well as switch them off. The neon glows when the appliance is switched on and flashes when it is switched off until it is unplugged.

With S1 (on/off switch of the appliance) closed (see Fig. 1) the neon lights, R2 dropping the mains voltage to the firing voltage of the neon. With Sl open Cl charges via R1 until it reaches the firing voltage of the neon and then discharges through it, thus making it flash until S 1 is closed or the appliance is unplugged.

With such devices fitted to all appliances, a quick look round the room last thing at night will tell you that they are all off and unplugged.
M. J. Maynard,

Wednesbury, Staffs.


Fig. 1. Circuit diagram for the mains neon flasher


Sir-Am I alone in thinking that quadraphony (and indeed stereo) is a "con"-or at least an attempt by the industry to create a demand?

I remember several years ago an article in this or a similar magazine, reporting a Continental idea whereby the orchestra performed in the wide end of a large exponential horn-the audience obtaining the effect of hearing a live orchestra through a metre-square hole!

Now this seems infinitely more sensible to me than quadraphony.

Surely the fact that an orchestra, or a pop-group, is ten metres wide is irrevelant. If width is necessary per se, why not spread the musicians out more? In fact musicians have always stood as close together as possible. Why?

A group of musicians constitutes a certain size purely because human beings are the size they are, and similarly with instruments.
"Stereo" and "quad" are NOT analogous to stereo pictures. Surely it follows that the industry should be putting the effort into improved colour, stereo pictures instead of the absurdities of "quad"! The present colour T.V. picture is on a par with a washed-out, amateur transparency viewed through a 50 p lantern.
E. Wadsworth, Huddersfield, Yorks*

## 9V BATTERY ELIMINATOR

continued from page 1092
in Fig. 5, although the dimension between the connector plate and the mains transformer board may need to be varied slightly to ensure a snug fit inside the battery casing.

Before fitting the connector plate pass the output leads of the regulator board through the slot in the mains transformer board and solder them to the contacts. The plain contact is positive and the castellated contact is negative (on some modern batteries the castellated contact has been replaced by a split contact).

Pass the mains lead through the hole in the connector plate and fit the plate onto the rods. Using p.v.c. lacing cord or thin p.v.c. sleeving, tie the mains lead tightly to one of the screwed rods to prevent the soldered joints being stressed.

The length of the screwed rod is 3 in where the battery has a plastic bottom plate, but a slightly longer rod will be needed if a different bottom plate is fitted. The rod is normally supplied in 3 ft lengths and can be sawn very easily with a "junior" hacksaw.

One "trick of the trade" when saxing threaded rod is to thread a nut onto the length to be sawn. After cutting and deburring with a file the nut can be removed and this will automatically re-form the thread on the cut end. This simple procedure saves a good deal of time and temper.

## FINISHING OFF

When the power supply assembly fits the battery case satisfactorily the ends of the brass rod may be filed down level with the tops of the nuts. Finally fit the unit into the case ensuring that " + " marking on the case is closest to the plain contact and carefully re-fold the casing over the bottom plate.

The battery eliminator can then be fitted into the portable radio in place of the normal battery although a slot will need to be made in the radio casing to allow for the mains lead. On the few occasions that the radio is required as a true portable the mains unit can be removed and a battery inserted in exactly the same time as it would take to replace a flat battery.

## Photograph showing the two component boards and the end plates of the battery before mounting on brass studding




## LIGHT FINGERS

Shop-lifting by well-heeled women in London's West End has been making the headlines. Not so well publicised is the wave of petty and not-so-petty pilfering in the electronic components industry since the upsurge in world demand created a component famine.

As usual, the incidence of crime appears greatest in the United States. Few of the semiconductor manufacturers are immune and hardest hit, according to reports, is Signetics with over $£ 40,000$ of goods mysteriously disappearing. Fairchild has also been hit.
It's not only straight pilfering that's worrying the industry. Huge quantities of below - standard products have been hived off onto the market at give-away prices in recent years and many of these are now re-appearing freshly remarked and not necessarily with the original manufacturer's name. These are being bought in good faith and equipment manufacturers have found performance not up to scratch. Motorola has been one company receiving back for replacement falsely marked semiconductors. Over in the States, the police have been sleuthing away and some arrests have been made.

The racketeers have not confined activities to the USA. The very nature of semiconductor devices with their small size, light weight and high intrinsic value makes them a natural for shipping round the : world and Bill Richardson, Chairman of Britain's Association of Franchised Distributors of Electronic Components (AFDEC) has warned the industry against dishonest brokers.

Members of AFDEC are bound by constitution to guarantee all products they sell and this is the best protection. Richardson quotes a case where a UK manufacturer disposed of a bulk quantity of substandard products 12 vears ago which have recently re-appeared on the UK market through sources which can be traced back through Tel Aviv and Geneva. Buyers beware!

## DEFENCE BOOM

The Royal Navy Equipment Exhibition at Greenwich showed defence equipment manufacturers in good shape, technically and economically. Defence exports have been booming and climbing in value every year. In 1968-69 exports were $£ 150$ million, in 1972-73 they had climbed to $£ 345$ million and this year will top $£ 400$ million, about 40 per cent of all defence equipment manufactured in the UK.

The sales success of recent years owes much to the pioneer work of Sir Raymond Brown who resigned his Chairmanship and business interests in Racal Electronics to become the first Head of Defence Sales in 1966. Present Head of Defence Sales is Sir Lester Suffield.

The sales organisation does market research, organises exhibitions, assists industry with advice and generally smooths the path between initial enquiry and final sale. Even Royal Fleet Auxiliary vessels are pressed into use as floating exhibition centres. For the past three months RFA Tarbatness has been touring the Middle East and Far East on just such a mission.

## FIFTY YEARS ON

This has been a great year for Golden Jubilees marking the 50th anniversary of broadcasting and of many of the pioneering companies that sprang into existence to-serve the needs of what was to become an industry in its own right. Of all the celebrations one of the cosiest, if not the biggest, was the informal party given by Eddystone Radio.

Although the company is now part of the giant GEC-Marconi complex, Eddystone's managing director Dick Carroll has managed to preserve the family atmosphere -perhaps not too difficult with so many of the staff having been around for more years than they care to remember.

Enough of the past. How is Eddystone shaping up to the future? Today's sets are all solid-state, modular, up-to-the-minute and selling well. Eddystone profits are buried deep in the corporate
accounts of the parent group but I can reveal that they are healthy in every way. Watch out for new models and an expanded component line in 1974.

## COMPUTERISED METROLOGY

Herbert Controls and Instruments Ltd. was formed in 1969 from three companies in the Alfred Herbert Group and started life with a 50 -year background in measurement techniques stretching back to Sigma gas gauges, modern versions of which are still sold to the gas industry. But more recently HCIL moved into the field of mechanical inspection equipment and rapidly established a world reputation for solving difficult problems.

One of HCIL's most remarkable machines is the Sigmatrace designed specifically for inspection of the aerofoil profile of gas and steam turbine compressor blades. This was traditionally a skilled job which took a lot of time and involved lengthy written records which were passed to a blade polisher to iron out humps and hollows and get each blade right. The inspector would compare the workpiece under inspection with a perfect master.

Sigmatrace does the whole iob in a minute, complete with a printed record of deviation. Moreover, no master blade is required because all the master profile information is fed into a computer store direct from the drawings. HCIL is doing a roaring trade world wide with this sort of elec-tronic-based metrology and supplies most major automotive and aerospace manufacturers.

The chief engineer of HCIL, Dr. Colin Gaskell, sees computercontrolled gauging becoming really significant in engineering shops where more than 30 measurements are needed on a workpiece. When you get up to 80 measurements a computer is practically a necessity.

## DUCKS AND GROUSE

Mallard is dead-long live Ptarmigan. They are the code names for the army's trunk communications systems. Mallard died after endless discussion. Now Plessey has been appointed prime contractor for the new system, Ptarmigan, with Marconi and STC as subcontractors. Initial contracts are worth $£ 17$ million but the project could lead to $£ 100$ million of business over the years.

I marvel at the wit of those who invent code-names. Mallard always seemed a dead duck. And if Ptarmigan doesn't come up to scratch, we'll have something to grouse about.

## Come home to this fine $\mathbf{8}$ track stereo system

Elegantly styled in teak finished cabinets with satin aluminium trims and controls.

Automatic and manual channel selection with at-a-glance illuminated track indicator.

Separate bass treble and volume controls for exact tone balance.

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Individual prices of these are:-
2 track record playback hesds 50 p each.
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tractal mounting shields 89 p each plack-heads already ,
plate


## DRILL

 CONTROLLER NEW IKW MODEL $\begin{array}{cc}\text { speed } \\ \text { from apply } & 10 \\ \text { revs. }\end{array}$ maximurn. Full power at all speeds by Anger tip control.Kif includes all parts, case, tlons. E1.95. 13p post and $p$. Made up model also available. 82.95

## MIGHTY MIDGET

Probably the finest possible radio, as deacribed in Practicat Wireleat, January 73. All electronic

(2)
TIME SWITCH
Smith's malne driven clock with thowing how you, also noter with music playing, kettle boiling or come home to a warm house, warn off burglars, keep peti warm, halve your heating bills, etc. 81.95
I CHIP RADIO
Ferrantl's latest device ZN414 gives results etter than superhet. Supplied complete wlth 11.11. notes and circuits. $\$ 1.88$ each. 10 for

## HJ-Q TUNER COMPONENTS

or expermenting wich the ZN414
KIT NO. 1. Plessey Minlature Tuning Condenser with buit-in LW switch and 3 in Ferrite slab and Itz wound MW coil, 72p.
KIT NO. 2 . Air spaced tuning condenser 6 in GITrite rod Jitz wound MW and LW coils, 84p. rive sin. Air apaced TC with slow motion coils, $81 \cdot 10$. KIT'No. 4 low motion drive and LW loading coils, 50 p .

## AUTO-ELECTRIC CAR

## AERIAL

With dashboard control switch-iully axtendable to 40 in or fully retrachegative earth. Supplled complet Then fitting instructions and resd Fired dasbboard awitch. $\mathbf{2 6 - 3 5}$ plus
25 p post and insurance. 25pp post and insurance.

## TELESCOPIC AERIAL

 Chrome platio or transmitter Chrome plated42p. KNUCKLED MODEL FOR FM BCrewCoseEXTRACTOR FAN Cleans the air at the rate of 10,000
suitable for kitchens, bathrooms, factories, changing rooms, etc. it's so quiet it can hardly be heard. Compact, oftin casing with 5 in fan blades. Kit comprises motor, fan blades, oheet steel casing. pull switch, mains connector, snd
fring brackets. $88.75+20 \mathrm{p}$

MAINS OPERATED SOLENOIDS
 Model 772 - small but
 $\begin{array}{lll}\text { midel } & 4001 / \text { in. } & \text { pult. } \\ \text { Size } & 2 f \times 2 \times 1 \text { in. } & 88 \mathrm{p} . \\ \text { Model } & \text { TT1-1tin } & \text { pull. }\end{array}$ Size $3 \times 21 \times 2$ in pull.
plus 20 p post and ingurance.

## MAINS TRANSISTOR POWER

 PACKDealgned to operate transistor seta and ampll to 500 mA (class B working, 9 v ., 12 volte for up any of the following batteries: PP1 PP3 place o PPY, PP7, PP9, sind others. Kit comprisen, PP4, trannformer rectifler, smoothing and load resistor condensere and instructions. Real snip at only 11-10. Plus 20 p postage.

## DESK,TELEPHONES

 Ex G.P.O. Black standar model with dialling dial but no internal bell. Bupplied with conneetfon diagram sleach. Ditto, with bell but without djaiing dial 81.28 . Model as illustrated plut 50 p poat forsingle then 65 p

SMOKE WILL KILL-GAS WILL KILL - FIRE WILL KILL But, if you install SAGA (our smoke and gaa alarm) your
tamily will have the latest electronic protection againat these killers. Saga uses a fantasticelectronlc sensor which .. ame th smoke and gas and sound the slarm immediateig in a nea case messuring approx. bin $\times 31$ in $\times 2$ in, it has its own internal alarm, also a connector for additional bells. You juat plug it in to the mains and hang it near the ceiling. Saga uses so iittle electricity that it will hardly move the meter,
leave it on always to give night and day protection leave it on always to give night and day protection. One year's guarantee, aloo
e5. 90 . Battery model kit only 24.98 ), 86.99 plus 30 p post and


## CENTRIFUGALFAN

Mains operated, turbo blower type. Pressed steel housing containe motor and impeller. Motor is $1 / 10$ th h.p. giving considerable air flows but virtually no noise. Approx. dimensions $10 \frac{1}{2}$ wide $\times 12$ in dia. outlet into trunking 104 4 tin . 88.65 plus $\& 1$ post and insurance


Standard size 14 in wafer-silver-plated 5 amp contact, standard fin spindle 2 in long-with locking washer and nut.
No. of Poles 2way 3 way 4 way sway 6 way 8 way 9 way 10 wayl2way

| 1 pole | 44p | 44p | 44p | 44p | 44p | 44p | 44p | 44 p | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 poles | 44p | 44 | 44p | $44 p$ | 440 | 44p | 44p | 77 p | 77p |
| 3 poles | 44p | 44 | 44] | $44 p$ | 77p | 77p | 77p | 81.04 | 81.04 |
| 4 poles | 44 p | 440 | 445 | 77p | 77 p | 77p | 77p | 21.82 | 81.82 |
| 5 poles | 44 p | 445 | 77p | 77p | 21.04 | 21.04 | 81.04 | \$1.60 | 81.60 |
| 6 poles | $4 \mathrm{4p}$ | 77p | 77p | 77 p | 81.04 | S1.04 | 21.04 | 21.87 | 21.87 |
| 7 poles | 77 p | 77p | 77 p | 81.04 | 81.82 | \$1.82 | E1-82 | 48.15 | 28.15 |
| 8 poles | 77p | 77 p | 77p | \$1.04 | 21.82 | 21.82 | E1.82 | 38-48 | 28.42 |
| 9 poles | 77 | 77p | 21.04 | 81.04 | 21.60 | 81.60 | \$1.80 | 28.70 | 82.70 |
| 10 poles | 77p | 77p | 21.04 | 21.82 | 81.60 | 21.60 | 81.60 | 88.00 | 28.00 |
| 11 poles | 77 | 21.04 | E1.04 | \$1.82 | 81.87 | 81.87 | 81.87 | 88.25 | 48.25 |
| 12 poles | 77p | 21.04 | 11-04 | 81.32 | 81.87 | 81.87 | \&1.87 | 88.68 | 88.58 |

THE TWENTYLITE
Fluoreacent lightlog units with polyeater chole and tinished white enamel. 2 ft . model, ideal kitchen, bedroom, hallway, porch, lift, etc.,
with tube. Assembled ready to install. Price $28.20+40$ p P. \& P

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Easieat wiy to fanlt find-traces signal from aerial to apeake -when signal stops you ve found the fault. Use it on Radio TV. amplifier, anything-complete kit comprises two special transistors and all
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This hester unit is the very latest trpe efficlent, and quietrunning. Is as fitted in Hoover and blower heaters costing is as fitted in Hoover have a few only. Comprises motor, impeller, akW element and 1 kW element allowing switching 1,2 and 3 kW and with thermal safety cut-out. Can be fitted ir,to any metal line case or cabinet Only needs control switch. $28-85$. 2 kW Mode as above except 2 kW e8.75. Don't mise this Control Switch 44p. P. \&P. 40p.

Room Thermostat nade by the famous Smith' Company. 15 amp at $2 \overline{50} 0 \mathrm{~V}$ Elegant white and beige case, size $4!$ in long by $1 \neq i n$ square approx. Adjust Special Special Snip price 81.65 .

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liorld about a year a go. We can aupply kit of parts for an improved and even more efficient version (Practical Wireless, June). Price $86 \cdot 55$ plup
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Made by Smiths, these are A.C. mains operated, NOT
CTOCKWORK. Ideal for mounting on rat CIOCKWORK. Ideal for mounting on rack or shelf
or can be built into box with 13 A or can be built into box with 13A socket. Two completely adjustable time periods per 24 hours, 5 A rluring these periods. 28.75 post and ins or of Additional time contacts 50 sp pair.
PHOTO ELECTRIC KIT
Contains photo cell, relay, transistor and all parts to make
light operated awitch. 21.76 plus 20p post and ins.

## MULLARD <br> UNILEX <br> STEREO AMPLIFIER



We demonstrate these daily and alnost always a sale realts ireally is a cracking amplifier. Only Mullard with their know-how could have made it possible at this low price. SPEC.: Mains operated. 4 watts music or apeech per channel. Double wired power supply eliminates cross talk. Harmonic distortion less than $2 \%$. Frequency response $\overline{50 H z}$ 15 kHz . Input suitable for pick up tuner or microphone. 6 -month guarantee.


## NEW ITEMS THIS MONTH

 White Rocker Switches. Four types available, all snap in firing through oblong hole appror 1 in $x$ in in, all rated at 10A a.c. All have white rocker ercept 83, which is anber. Our ret RS 81 , push to make, spring return, 14p. Our ref Ro, push to break, spring return to on, 14 . mot normal rocker, 16Rocker ${ }^{\circ}$ witches. 15 A Pritmac panel mounting, hole size 1 in $x$ fin. Our ref RS 8 in price 11 p ach. $\overline{\text { DA }}$ made by Mem, their type ref $\mathbf{1 6 0 0}$, our ref R8 s6, price 11p each.
Ministure Band Ticrophone. Dynamic, for tape recorders but equally suitable for ampliflers, good quality with lead and plug, price 81.87 .
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Mains Contactor. This serves the same purpose as a treble pole relay but owing to the more robust construction and more positive saction it is much malna circuits for example, where a thermostat has to control a large number of heaters. The contactor has four switches each in its own compartment separate from the others and each able to make and break 10 A with complete safety. German made, these messure approx. $2 \ln x$ $2 \ln \times 2 \ln$, price $\boldsymbol{2} \mathrm{E}$ - 20 .
GOOD COMPANION I.C. VERSION We can now offer these again in
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ZN414 and Mullard AF Module
 ZN414 and Mullard AF Module 1172. Cabinet aize approx. 1 lin wide $\times 8$ in high $\times 3$ in deep. Excellent assembly instructionExcellent tone wood cabinet
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Maine Transtormers. All by firto clase makers, all with normal 230 V primary and atatic acreen. Our ref TR 81, $6.3 \mathrm{~V}, 3 \mathrm{~A}$, with clamp and feet, 88p. Our ref TR 82, made by Hinchley for Decca primary tapped $200 / 340$ volt two secon-
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3 A , this is for above chassis mounting, open 3A, this is for above chassis mounting, open constructlon, price E1-76 plus 25p post. Our ref TR 83, upright mounting with metal shrouds, pecondaries 50 volt at 2 A and B volt at $1 \mathrm{~A}, 55.50$ plus 25p post.

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Falve action fbre tipped marking pen filled with black etch resist-it'g easy with this to make a perlect PC board, just draw straight on to the copper-allow 15 minutes to dry,
then immerse in ferrtc cloride or other then immerse in ferrtc cloride or other etchant on
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# Transistors \& Constructors By D. Bollen 

## The start of a great revolution in home construction is recalled by a well-known contributor in this article, which brings to a conclusion our special series commemorating the invention of the transistor

| N THE TYPICAL home electronics workshop of twenty-five years ago the enthusiast would be surrounded by machines for bending, punching, drilling, and rending asunder sheet metal. Constructional techniques were based upon the chassis, a box-like structure full of holes into which were inserted spindles, screws, valveholders, grommets, and trapped fingers.
Sometimes, when the burden of bashing metal became tiresome, a piece of easily punctured Bakelite might be pressed into service as a breadboard, but this was considered very unprofessional, a throwback to the days of coil winding, capacitor building, and generally doing it yourself.

Components came from two main sources; sturdy ex-government equipment which was cannibalised, sometimes with the aid of a hammer and cold chisel, and the "junk box" where reposed an amorphous heap of very second-hand items, ranging from a leaking electrolytic capacitor dated 1941 to a speaker grille woven to depict a scene of nymphs and satyrs dancing in a woodland setting. These were the lean years just after the war, with no oriental imports, kits of parts or regular sources of "bits".

Into this man's world of hot cathodes and 100 watt soldering irons was born the sub-midget transistor, and the wonder, is that it managed to survive at all, let alone replace valves, which everyone said it would never do.


## A TOUGH TIME

Transistor manufacturers were having a tough time trying to fabricate the new device, probably because they were ham-fisted too. In any event, if you were fortunate enough to get hold of a sample in the early fifties it was likely to be one that everybody else had rejected, with a leakage current of two or three milliamps, a current gain of five, and dying from slow contamination.

Compared with a valve this' was a pathetic thing indeed!

Assume that you were the proud possessor of a device no bigger than a resistor with three wires sticking out of it. Where did you go from there? Published information was scanty and far from standardised. Maximum ratings were mere hearsay. At the devaluation equivalent of $£ 2$ to $£ 4$ each, the safest policy was to power the device at the lowest voltage and current at which it was capable of supplying useful work.

As far as circuits went, which was not very far, there was a limited choice between the upside down, thread-in-a-maze American sort, or the UK variety which favoured the powering of each transistor in a multi-stage circuit by its own personal 1.5 V cell.

Apart from earth symbols and batteries floating all over the page, there was also a general tendency for transistor symbols to be shown doing a basedown nose dive into the earth rail, this being the only way they could be made to function above 10 kHz .

## GREAT DIFFICULTIES

So, in the face of great difficulties you managed first of all to identify the leads on your transistor with an ohmmeter and then to find, or rashly devise a transistor circuit.

Were you supposed to solder the thing to a tagstrip, and mount the resulting assembly on the customary two acres of sheet aluminium? After all, we were here dealing with impedances of a very low order, for which electrolytic capacitors the size of milk bottles would have to be accommodated for coupling and decoupling purposes.

## DELICATELY SOLDERED

The delicately soldered transistor clings to its tagstrip. The scope (ex-government of course) displays a straight line on its axis. Several meters are linked to those parts of the circuit where a voltage or current might conceivably occur.

After inserting the power supply plug into the lowest voltage tap of a grid-bias battery . . . yes, we have oscillation!


True, it is but a crude imitation of what would normally pass as a sine wave from a valve circuit, but it is early days yet. A few more volts perhaps? Why is that meter reading creeping higher and higher? Should the transistor run hot? It has stopped oscillating.
"Grrr! They will never replace valves."

## AVAILABLE TO AMERICAN

The transistor was available to American enthusiasts for about $\$ 18$ in 1953. Over here, the ubiquitous OC71 and "red spot" transistors (the latter a polite name for manufacturer's reject) came on the scene in 1956 priced at $24 /$ - and $10 /$ - respectively. Full praise must be given to those suppliers who struggled to bring us the amplifying crystal less than eight years after its invention.

The silicon transistor also took only eight years to reach the home after being first manufactured in 1952.

More than one enterprising magazine contributor of the period went one better and gave full instructions for making a point-contact transistor from an old crystal diode, but the problem here was that an excess of audio signal or marital strife in the home could dislodge the triple catswhisker and thus degraded performance.
Another bright spark discovered that when the paint was scraped off the glass encapsulated OC71 it responded to light in the manner of a phototransistor. The manufacturers quickly countered this cunning move by filling their transistors with opaque blue putty, labelling the clear putty variety OCP71 and charging more for it.

## NEST OF SNAKES

An innovation of the middle fifties was the transistor radio, which incorporated the new "nest of snakes" unrepairable printed circuit and the fragile ferrite rod aerial. Also at this point in time, the word "transistor" was press-ganged into common English usage to signify a radio receiver which could be employed to annoy people on beaches, and also render the user deaf in one ear by means of a simple unhygienic earphone.

The printed circuit defied all former rules of construction.

Components were held in position by solder alone, a practice which previously would have been considered very naughty. With the passing of the chassis, there was no longer anywhere to mount controls, and this caused quite a few headaches in constructional circles.

Eventually, it was tacitly agreed that serious projects would have their controls mounted on smart metal front panels, while silly projects could use sheet plastic or even wood. Alas, these attempts at standardisation failed miserably.

One breakaway group defiantly insisted on using metal tobacco tins for all projects, while another sect mounted their controls on the printed circuit itself! The latest trend seems to be to bung everything inside a transparent plastic cube or sphere and hope for the best, so confusion still persists.

## ADVANCED STAGE

Valve audio amplifiers had reached an advanced stage of development prior to the introduction of the "jump-a-groove" long-playing record in 1950, but with the coming of the difficult-to-tune f.m. radio in 1955, hi-fi purists were at last able to take time off to just sit and listen to the music, without having to bother about all that nasty distortion of former years.

Unfortunately, this idyllic state lasted only until 1961, when the easy-to-blow power transistor started to appear in output stages, accompanied by something called "the transistor sound".

This unusual effect was characterised by a rattling buzz from loudspeakers when gain controls were turned low. After a good deal of concentrated sleuthing, it transpired that transistor audio amplifiers were subject to crossover distortion, so the purists had to climb out of their armchairs and set about exorcising the demon with cabbalistic circuitry.

Since then there has been no further opportunity to listen to music. Elimination of the output transformer led to severe difficulties in trying to match the then extant 15 ohm loudspeakers to amplifiers requiring a four to eight ohm load, and all problems were multiplied by two when stereo came along.
Now they are about to be multiplied by four.

## SURVIVE THE TRANSITION

What has the future in store for those who have managed to survive the transition from valve to transistor? Clearly, the introduction of a new device is often accompanied by unpleasant sideeffects. For example, with i.c.s. we have already experienced circuits which are best understood if held upside down in front of a mirror, and the use of postal codes for device numbering is to be deprecated.

Above all, one thing is patently clear. A new device seems to take eight years to mature to amateur status. Furthermore, all information concerning a new device is automatically witheld for five years, or until it becomes obsolete, whichever period is shorter. So it follows that there is no need to get too agitated when a new device comes along, because the threat to one's peace of mind is not immediate.

NOTE: This last point is not quite true since it is the avowed object of Practical Electronics to ensure that the reader is informed of interesting developments as soon as possible. Indeed, the problem nowadays would be to avoid doing so-ED.

# PRTEMTI 

## FUEL MONITOR



Fig. 1

With petrol likely to be very scarce or more expensive or both in future, devices for accurately measuring vehicle fuel consumption will become more popular.

In BP 1320039 Alan Westwood, Peter Davidson and Brian Dean describe and claim just such a device. The circuit Fig. 1 shows a vehicle speed measuring device, a flow meter to measure fuel rate of flow (and thus proportional rate of consumption) and an ammeter for reading m.p.g.

The meter is connected between opposite junctions of a Wheatstone bridge comprising VR2 (which forms part of the flow meter), R2, R1 and VR1 for pre-setting bridge balance. The use of R3 in series with the meter is only. necessary with certain meters.

The opposite corners of the bridge are connected together by the vehicle speed measuring device. This includes a rotor geared to the vehicle transmission with brushes which alternately connect capacitors C1, C2 across the vehicle battery and discharge them through the bridge. The capacitors $\mathrm{C} 1, \mathrm{C} 2$ thus charge and discharge alternately to give a signal representative of the vehicle speed.

The flow meter will generally be in the form of a chamber with inlet and fuel outlet pipes and a bellowstype diaphragm. Fuel passing to the engine flows through the chamber to compress the diaphragm in dependence upon fuel flow rate. As the diaphragm is compressed, the value of VR2 resistance is varied by movement of the slider over its track. The value of VR2 resistance is in practice an inverse function of the fuel flow rate.

The reading given on the meter is approximately proportional to an arithmetical relationship between the two signals controlled respectively by the flowmeter and the speed measuring device, being approximately proportional to the current received from the rotor of the speed measuring device multiplied by the imbalance of the bridge circuit due to the flow meter. This reading represents an indication of distance travelled by the vehicle per unit of fuel consumed and the meter ME1 can be calibrated to provide direct readout in miles per gallon.

## NEW APPROACH TO TONE CONTROL

In BP 1304774 Wilfred Palmer of Dagenham, Essex, describes a three part tone control circuit for an audio amplifier. By way of example he gives a list of specific values for all the components, see Fig. 1.

The variable potentiometer VR1 and d.c. blocking capacitor C1 form a normal volume control. The slider of VR1 acts as a common input line to the three sections of the tone control, shown dotted.

The bass circuit includes R1 and R2 in series with VR2. The slider of VR2 is in series with R3 which feeds the output terminal.

The mid-range circuit has R4 and R5 in series with VR3, and the slider is also connected to the output via R6 and C2.

The high frequency circuit comprises VR4, the slider being connected to the output via C3.

The resistor R7 between C2 and C3 is intended to isolate the infinite variations of time constant of the treble circuit from the infinite variations of time constant of the mid-range circuit. Also, the resistor acts as an impedance to high frequencies from the bass and midrange circuits. The inventor suggests that in this way the signals from the middle and treble circuits are cleanly and fully mixed.
The bass circuit presents a high impedance to high frequencies, thereby attenuating them but passing low and mid-range frequencies. This is due to the presence of resistors R1 and R2. The inventor points out that any resistor can be represented by a pure resistance in parallel with the self capacitance across the resistor terminals and there is thus attenuation of high frequency signals by the changes of self capacitance with increasing frequency. By using the resistors in series, total self capacitance is lowered.
The treble circuit presents an increasing impedance as the frequency decreases, thus attenuating low frequencies but passing the high and part of the mid-range frequencies.

The inventor claims that the circuit eliminates the need for attenuators in crossover units and allows infinite variations of the signal fed to loudspeakers over the whole audio spectrum.


Fig. 1

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LIN. L/S 15p. D.P. 25p. $\begin{array}{ll}\text { LIN. L/S 15p. D.P. 25p. } & \text { AERAXIAL-AIR SPACED } \\ \text { STEREO L/S } 55 \mathrm{p} \text {. D.P. } 75 \mathrm{p} . \\ \text { ED Yd, } 1.40 ; 60 \text { Yd, } 2 .\end{array}$ STEAEO L/S 55p. D.P. 75p. FRINGE LOW LOSS
Ideat $\mathbf{1 0}$
$\mathbf{1}_{\mathrm{p}}$ yd
8in. or 10in. ELAC HI-FI SPEAKER
Dual cone plesticised roll sur round. Large ceramic magnet. $55 \mathrm{c} / \mathrm{s}$. of ohm impodance
sin 10 watte, 101 in 12
watt music power.
£3. 75 Pont 25p
E.M.I. $13 \frac{1}{2} \times 8 \mathrm{in}$.

SPEAKER SALE!
Why twin tweeters
And crostover. 10
£4.50
15 ohm . Ai hluatrafed. Post 25p
With flered tweeter cone and ceramic
magnet. 10 watt .



State 3 of of or 15 ohm. Post 25 p


Bookshelf Cablinet ${ }_{16} \times 10 \times$ 9in. $£ 5 \cdot 50$
SET OF 3 MOTORS FOR COLLARO STUDIO TAPE DECK
£2.50 Post 50p
blank aluminium chassis. 18 e.w.g. $2, \ln$ aides 6
14
$\times 40$
$\times 10$ $14 \times \ln 2 p ; 18 \times 8 \ln \mathrm{sep} ; 12 \times 3 \ln 50 \mathrm{p} ; 16 \times 101 \mathrm{n} 81$.
 LUMINIUM PANELS 11 s.w.g. $8 \times 4$ in $9 p ; 8 \times$ in $15 p ;$
 $16 \times$ ain 2ip; $14 \times$ In 34p; 12
PAXOLIN PANEL $10 \times$ ain 15 p .

## ANOTHER R.C.S. BARGAIN!

## 4 TRANSISTOR MONO AMPLIFIER

Powerlul 3 watt output, 15 ohm. AC maine operated with transformer. ${ }^{3 \text {-Controls, volume, freble, base and On/Off }}$ switch with knobs. Ready made on pr make, ize in wide $x$ An deep $x \operatorname{in}=5-95$ Post
R.C.S. STABILISED POWER PACK KITS All parti and Intructiona with Zoner Dlode, Printed Circult, Bridge Rectiflers and Double Wound Melins Transformer 15 or 18 or 20 V d.c. 100 mA of lase. 15 or 18 Or 20V d.c. It 100mA of lase.
PLEASE STATE VOLTAGE REQUIRED.


## R.C.S. GENERAL PURPOSE TRANSISTOR

 PRE-AMPLIFIER BRITISH MADEIdeal for Mike, Tepe, D.U., Gultar, tc. Can be used with Beftery $0-12 \mathrm{~V}$ or $\mathrm{H} . \mathrm{T}$. IIne $200-300 \mathrm{~V}$ d.c. operation. Slze: For use with. valve or tranalator equlpment. 090 Poat
Full inatructions eupplled. Detalle S.A.E. Full inatructions euppled. Detalle S.A.E. 0 20p

## E.M.I. WOOFER AND TWEETER KIT

Woofer $10 \frac{1}{\times 6} 6 \mathrm{I} \mathrm{In}$. Ceramic Magnet, 4402. 13,000 Ilnes, Tweeter $3 \dot{I} \mathrm{In}$. square, 10,000 Innes. Crossover condenaar 12 watts. $£ 5.75$ Post 25p.

## BRITISH FM/VHF TUNING HEART

of to 100 M/CS British made. 2 Tranalstoris ready allgned requires $10-7$ M/CS I.F. Complete with tuning gang. essential.

Our price $£ 3.95$ (pont zop
MAINS TRANSFORMERS




 HEATER TRANS. 6.3 V 3 I
GENERAL PURPOSE LOW VOLTAGE. Tapped outputa it $2 \mathrm{amp} .3,4,5, B, 8,9,10,12,15,18,24$ and 30 V 汭-90
 $5 \mathrm{amp}, 8, \mathrm{c}, 10,12,16,18,20,24,30,34,40,44,60 £ 3 \cdot 80$

 $500 \mathrm{~mA} 45 \mathrm{p}, 12 \mathrm{~V} 750 \mathrm{~mA} 95 \mathrm{p}, 40 \mathrm{MV} 1 \mathrm{smp} \mathrm{E1.75}$.
AUTO TRANSFORMERS. 115 V to 230 V or 230 V to 115 V 150W £2-25; S00W £6-25; 750W £10; 1000 W ₹15 CHARGER TRANSFORMERS. InPut 200/250V
 BATTERY CHARGERS. Rendy bullt with leade and cilpe 1. amp £2; 4 amp 4 ; 5 amp E4. 50 .

6 or 12 V outputioge $1 \%$ amp 40p; 2 amp $55 \mathrm{p} ; 4 \mathrm{amp}$ asp
MAINS ISOLATING TRANSFORMER
Primary 0-110-240V. Secondary $0-240 \mathrm{~V}$. 3A. 720 W . insulated terminala. Varniah Impregnated. Fully enclosed In ateel case with fixing 1eet.
Famous make. (Value f19). OUR PRICE f10 ${ }_{50 \text { p }}^{\text {Corr }}$ Can be uaed a\& a00W a uto tranaformers 240-110
IDEAL FOR COLOUR T.V. OR GARDEN TOOLS

|  | NEW ELECTROLYTIC CONDENSERS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2/350V | ...14p | 250/25V | $14 p$ | $50+50 / 300 \mathrm{~V}$ | .50p |
| 4/350V | 14p | 500/25V | 20p | $80+100 / 350 \mathrm{~V}$ | 8p |
| $8 / 450 \mathrm{~V}$ | 14p | 1000/25V | 35p | $32+32 / 250 \mathrm{VV}$ | 20 p |
| 18/450V | 229 | 1000/50V | 47p | $32+32 / 450 \mathrm{~V}$ | 45p |
| 39/450V | 35p | $8+1 / 450 \mathrm{~V}$ | 2pp | $350+50 / 325 \mathrm{~V}$ | 55p |
| $25 / 25 \mathrm{~V}$ | 10p | $8+18 / 450 \mathrm{~V}$ | 25 p | $32+32+32 / 3$ | 55p |
| $50 / 50 \mathrm{~V}$ | 10p | $16+18 / 450 \mathrm{~V}$ | .40p | $100+50+50 /$ | 55p |
| 100/25V | 10p | $32+32 / 350 \mathrm{~V}$ | * |  |  |

LOW VOLTAGE ELECTROLYTICS.
$1,2,4,5,1,18,25,30,50,100,200 \mathrm{mF} 15 \mathrm{~V} 10 \mathrm{p}$.
$500 \mathrm{mF} 12 \mathrm{~V} 15 \mathrm{p} ; 25 \mathrm{~V} 20 \mathrm{p} ; 50 \mathrm{~V} 30 \mathrm{p}$
7000mF 12V 17p; 2sV 35p; 50V 47p; 100V 70p

5000 mF 6V 25p; 12V 42p; 25V 75p; 35V 85p; 50V 95p.
CERAMIC, 1 pF to $0.01 \mathrm{mF}, 4 \mathrm{p}$. SHver Mice 2 to 5000 pF , 4p.
PAPER $350 \mathrm{~V}-0.14 \mathrm{p}, 0.513 \mathrm{p} ; 1 \mathrm{mF} 15 \mathrm{p} ; 2 \mathrm{mF} 150 \mathrm{~V} 15 \mathrm{p}$.
$500 \mathrm{~V}-0.001$ to $0.054 \mathrm{4p} ; 0.15 \mathrm{p} ; 0.25 \mathrm{Ip} ; 0.4725 \mathrm{p}$.
SILVER MHCA. Close tolerance $1 \%$. 2-2-500pF Ep; sso2,200pF 10p; 2,700-5,400 pF 20p; 8, 500pF-0.01, mfd 30p each
 $385 \mathrm{pF}+355 \mathrm{pF}$ wh $25 \mathrm{pF}+25 \mathrm{pF}$, Slow motlon drive 50 p SHORT WAVE SINGLE. 10 pF , $30 \mathrm{p}, 25 \mathrm{pF}, 55 \mathrm{p}, 50 \mathrm{pF}$, 55 p RESISTORS TW IW $1 w, 20 \% 10$ ACIDC. Amber 200 p . RESISTOAS. 1 W, iW, 1W, 20\% 1p; 2W, 5p. $10 \Omega$ to 10M MGH STABILITY. W $2 \% 10$ ohma to 8 meg., 10 p .
WIRE-WOUND RESISTORS 5 watt, 10 watt, 15 watt, 10 ohm to 100 K 10p each; 0.5 ohm to 8.2 ohms 10 p .
TAPE OSCILLATOA COIL Valve type 35 p .

NEW MODEL "BARER LOUDSPEAKER", 12IN SO WATT. GROUP SO/I2: OR 15 OHM HIGH POWER. $£ 17.60$
FULL RANGE PROFESIONAL OUALITY.
BAKER MAJOR12" 19.90

$30-14,500 \mathrm{c} / \mathrm{e}, \mathrm{i} 1 \mathrm{in}$. double cone, wooter and tweeter coramic magnet asambly having tlux denalty of of 145,000 Maxwelle. Base resonence $40 \mathrm{c} / \mathrm{s}$. Reted 20 w . NOTE: 3 or 1 or 15 ohme muat be stated.
Module hth , 30-17,000 $\mathrm{c} / \mathrm{s}$ whit tweter, cromaover, bathe and
instructions.
$£ 12.50$ Please atate 3 or 8 or 15 ohms. Po it free
baker "big-SOUND" SPEAKERS Poat free
'Group 25'| 'Group 35'| 'Group 50'
 3 or 8 or 15 ohm 3 or a or 15 ohm or 15 ohm
TEAK VENEERED HIFF SPEAKER CABINETS For 121 in or 10 In dla. apeaker $20 \times 13 \times 9 \mathrm{nn}, 59.90$. Dost 25 p
 For $\mathrm{f} \times \mathrm{Sin}$ opanker
 For sin and Twooter
LOUDSPEAKER CABINET WADDING 1aln wide, 15p tt.
GOODMANS $\left.6 \frac{1}{2} \right\rvert\, \mathrm{In}$. HI-FI WOOFER 8 ohm. 10W. Large ceramic magnot. Spectal Cambric cone surround. $30-12,000 \mathrm{c} / \mathrm{a}$. |deal P.A
30-12,000 C/a. ideal P.A
Sultable Cabinet $12 \times 8 \times 8$ Syetema, atc.

## ELAC CONE TWEETER

The moving call diaphragm glves a good redlatlon pattern to the higher frequencles and emooth extonsion of 10 alalsoponse from $1,000 \mathrm{c} / \mathrm{s}^{\text {to }} \mathrm{th}$ deep. Rating $10 \mathrm{~W}, 3 \mathrm{ohm}$. $34 \times 2$ in deep. Rating
Croseover 95p
\&1. 90
Post 20p.
SPEAKER COVERING MATERIALS. Samples Large S.A.E. Horn Tweetors $2-18 \mathrm{kc} / \mathrm{s}$, 10W a ohm or 15 onmi 81.85 . De Luxe Horn Twestors 2-18kc/e, 15W, 15 ohm c 3.



 $15 \mathrm{ohm}, 3 \mathrm{in}$ dia, $\mathrm{E} \times 4 \mathrm{in} 7 \times 4 \mathrm{n}, 8 \times 5 \mathrm{n}$. C . K
 8in. DIAMETER AW $\mathrm{E}_{2} \cdot 50$. 10In dlameter $5 \mathrm{~W} \mathrm{E} 2 \cdot 50$;
12 In dlameter, 6W, en.95.
VALVE OUTPUT TRANS. 25p; MIKE TRANS. $50: 122 \mathrm{p}$. 5 WATT MULTI-RATIO, 3 , 8 and 15 ohm E0p
Mike trans. mu metal $100: 1 \mathrm{\varepsilon 1} \cdot 25$.

## MAJOR 100 WATT

ALL PURPOSE
GROUP
AMPLIFIER
All purpose tranalstorleed
Idesl for Groups, Disco and P.A
4 inpute speech and muslc. 4 way
mixing. Output st ohm. a.c. waint
Soparate ireble and bay controle


SUPER VALVE MODEL, 100W, callers only, xas.

| BARGAIN AM TUNER. Medlum Wave. |  |
| :--- | :--- |
| Tranalstor Superhet, Ferrlte a a rial. 9 volt. | $\mathbf{8}, 95$ |

BARGAIN 4 CHANNEL TRANSISTOR HONO MIXER. Add musical highlighte and sound aflacta to recordings.
Will mix Microphone, records, tape and tuner $£ 3.95$
 TWO CHANNEL STEREO VERSION $£ 5.95$ BARGAIN 3 WATT AMPLIFIER. 4 Tranalator $£ 4 \cdot 50$ Push-pull Ready bulti, with volume, is volt. D.C. Trable and basas controls.

COAXIAL PLUG 10p. PANEL SOCKETS 10p. LINE 1Ap. OUTLET BOXES, SURFACE OR FLUSH 25p.
BALANCED TWIN RIBBON FEEDER 300 ohms. 5p yd. JACK SOCKET Std. open-circuth 14p, closed clrcutt 23p: Chrome Lead-Socket 45p. Phono Plupe 5p. Phono Socket 5p. JACK PLUGS Sid. Chrome 15p; 3.3 mm Chrome $1 \%$. DIN SOCKETS Chatels 3 -pin 10p; g-pin 10p. Din SOCKETS tead $3-\mathrm{pIn}$ 1tp; ${ }^{5-p i n} 15 p$. DIN PLUGS 3-pin 11p; 5-pin 25p.
VALVE HOLDERS, 5 F ; CERAMICS Ap; CANS 5p.

## gres <br> REVERSIBLE 4 POLE MOTOR <br> 

ONE RPM GEARED MOTOR
240V A.C. malne
ideel for diepleys/deco light wheels. Poif 25p.
E.M.I. GRAM. MOTOR.

120 V or 240 V a.c 25p

WHITEHORSE ROAD, CROYDON Buses 50, 68, 159, Rall Selhurst. Tel. 01-684 1665

 good condition. 27. P. \& P. 50p Double encled $\hat{S}^{*}$ shat
motor. 21 . P. \& 20 p .

OPEN FRAME shaded pole GEARED

## MOTORS

(Dural gear HIGHTORQ1F NE NEK overall size: $3 \frac{1}{3} \times 31^{*} \times$ $3 t^{+}+$spindie $4^{+}$dia. as illustrated. 23
Simitar to above, 19 rpm .42 .70 . P. AP. 30 p , but alighty smalter). 28.70, P. \& P. 30p.



PRICE £3.30 Priginal cost £16.50 OÚR (special funtatims). Mu-metal enclosure availahle 75peach. F \& $\mathrm{I}^{2}$.FREF
'DAVENSET" MAINS SOLENOID - high. Similar in appearance to "SORENG". El.8S $\mathrm{P}^{\prime}, \& \mathrm{P}^{\prime}, 20 \mathrm{p}$.

## AMPEX 7.5v, DC MOTOR

This in an ultra litecision tape
motor denigned for nse int the $A M P E X$ mosiel Ad:20 poriable recorder Torine tioGM/CM Stall loart at 500 mA . Drawa homa in rim. di00rmis sliced adjustment. Internal Aト/RF
 Original cost \& lifer our Mu-metal enclosure a vailahle.


SMITHS RINGER-TIMER Keliable 15 minute times, spring wound
(concurrent with time setting) $[5 \times 1$ min. Hivisionn, approximately, between


## GEARED MOTORS

 rping geared motor. Type 8D14 each. I's P. 50p
REVERSIBLE Parvalux type SDI4. 240V a.c. 30 rpm $40 \mathrm{tb} / \mathrm{in}$. Variable angle drive shaft. Ex-equipment in

SHADED POLE Mains motor, $13^{\prime \prime} \times 11^{\prime \prime} \times 2^{+4}$ high


110 rpm with pressed steel gear case (amilar to ahore
SPIT MOTOR
shalt ${ }^{2} \times 40 \mathrm{~V}$ a.c wocket inside. 28. 1 , AF. 30 p .

## MAINS SOLENOID

 This lifle lift of gives vertical lift of approximatelyhinged ing ellow


Bracket incorporates : fixing ncrews. Length of arm, ${ }^{2}$ - 240 a.c. Pull at coil is approximately llb. 21


## "DECCO" MAINS

## SOLENOID

Compact and very powerful 161 b . pull. ${ }^{\text {" }}$ travel which can be increased Overall size: $\left.2^{\prime \prime} \times 2 \ddagger^{*} \times 2\right\}^{*}$ high \&2-20. P. \& P. 20

MAINS SOLENOID by MAGNETIC DEVICES LTD.
A heautifully constructed solenoid at hall normal price. A 2 -siled bracket is incorporated for vertical
or horizontal mounting. Size: $2^{*} \times 14^{*} \times 1 \frac{1}{*}^{*}$. Pull is approximately ?llb, plunger 1 ravel $l^{\prime}=$. Fixing eye taker up to " bolt, plunger non-captive. NEW in original maker's hoxen \&1-20. P. \&P . 20p. Large number avallable, special price for quantity.

## CROUZET' MOTORS

 Type 965
$115 / 240 \mathrm{~V}, 50 \mathrm{~Hz} .48 \mathrm{~W}$. Stoutly conntructed,
plus apindle $1^{\prime \prime} \times \mathrm{m}^{*}$ dia. long clock. 83.30 each. P. \& P. 25p.
'RE CIRK IT'' Mains 10amp cut-o ut
all items are NEW and UNUSED. Postal or carriage charges arc for Gt. Britain only. edncatlonal depta., etc. All orllers under $\varepsilon$ companien, please. Company orders under $2=50$, surcharge 60p phease. C.w.O. MICROPHONE (U.S.A.) NULES
Impeilance approx. $200 \Omega$, output 60 or 80 DB at 1 Kc A f used in deal aids. hugging devices, etc. Size ( 60 DB ) equipment all teated $\varepsilon 1-40$ each. $P$ P FREF

## UNLESS OTHERWISE STATED

PLUG-IN RELAYS by SCHRACK (Perspex enclosed)
OCTAL ( $2 \mathrm{c} / 0$ ) 6 amp contacta at following voltage

11 pin ( $3 \mathrm{c} / \mathrm{o}$ ) 6 amp contscts:

RA and RN Series ( $4 \mathrm{c} / \mathrm{o}$ ) 3 amp Gold Plated Contacto RA and RN Series (4 c/o) 3 amp Gold Plated Contact


80 a.c.. 110 i.e. 115 a.c. 120 a.c.
Hase sockets for all above types 15p.
Please add 10 p towards P. d P. on all orders.
From JAPAN. TAKAMISAWA Perspex encloted relays. Type MQ308 24 y d.c. 600 ohms (fe/o
Complete with base socket. 90 p . P. P

## SILVANIA

## MAGNETIC SWITCH

Now complete with reference magnet!
A magnetically activated switch, vacuum sealed in a glass envelope. Silver contacts, normally in a glass envelope. siver contacts, normaly
closed. Rated 3 amp at $120 \mathrm{~V}, 1 \frac{1}{4}$ amp at 240 V . size: (approx.) 1$]^{*}$ long $x{ }^{\prime \prime}$ dia. Ideal for burglar alsrms, security syatenis, etc. and whereever non-mechanical switching is required. 10 for 88 . P. \& P. 15 p ; to tor \&8.80: 100 for
210. 50 . P. P. FREE over 10 .

## NORPLEX

The famous American fibre-glass copper-clayl laminate. Finest quality with woven glass base of Epoxy-resin Excellent Mech. and Elec. conductive properties. Hest PURCHABE STOCKS LABT! Sizes: $12^{*} \times 12^{*} ; 24^{*} \times 12^{*} ; 24^{*} \times 24^{*}$ FULL SHEET $43^{\circ} \times 37^{\circ}\left(11\right.$ s4, $\mathrm{ft}^{\prime}$.). Single-gidel Copper with thickness of $1 / 32^{*}, 3 / 64^{*}, 3 / 32^{*}$. Also double-8ided $1 / 32^{*} .1^{1 / 16^{*}}, 3 / 32^{*}$. $£ 1$ per 8q.ft. Cut sizes (1-10 sq.ft. P. \& P. 25p. Full Sheet $£ 8$ each. Carr. $\& 1$ for 1 st aheet plus 25p each additional sheet.

## TANGENTIAL HEATER

Silently driven by shauled pole Mycalex motor, poweriul and smooth running (outh alumininn impletler voltage PLUS matching heater unit with spiral heater unit with spira for 500 or $1,000 \mathrm{~W}$. $\mathbf{2 8 . 8 0}$. P. \& P. 30p.

ELECTRO-TECH compontrs tro

## now...



Project 80 tuner
Stereo decoder
Project 80 Active Filter Unit (AFU)
the slimmest,most elegant hi•fi modules ever made


Living with hi-fi takes on new meaning now that Project 80 is here. These amazing new modules mark a brilliant technical advance all round; their size and presentation bring exciting new opportunities to install systems in ways hitherto only dreamed about but never before made practical. You can build a Project 80 system virtually anywhere and it is unbelievably simple to install and connect up. Everything that could possibly be wanted in a top quality do-it-yourself domestic hi-fi system will be found in Project 80 - compactness, elegantly ultra-modern styling, ease of fixing and operation, new control methods, and above all superb performance. New as well as popular established ideas on installation are featured on page four of this announcement to provide just a few examples of the system's fantastic versatility.


# Project 80 new modules 

## Stereo 80 pre-amplifier and control unit

As with other Project 80 units, the Stereo 80 is mounted by means of two bolts fixed at the rear which pass through holes dilled in the wood or plastic on which modules are to be mounted All the electronics are contained within the $\frac{3}{2}$ deep front panel! Connecting leads are taken away similarly out of sight Each channel in the Stereo 80 has its own independerit tone and volume controls operated by sliders This enables exceptionally good environmental matching to be obtained Provision is made for magnetic and ceramic pick-ups, radio and tape in and out A virtual earth mput stage forms part of the up-dated circuitry of the Stereo 80 to ensure the finest possible quality from all signal sources Generous overload margins are allowed on all inputs Clear instructions with template are supplied

TECHNICAL SPECIFICATIONS
Size $-260 \times 50 \cdot 20 \mathrm{~mm}$ ( $10 \frac{1}{4} \times 2 \times$ 을ins)
Finish - Black. with white markings
Inputs - Mag PU 3mV RIAA corrected: Ceramıc P.U. 300 mV Radio 300 mV . Tape 30 mV
S/Nratio - 60db
Frequency range -20 Hz to $15 \mathrm{KHz}!-1 \mathrm{~dB} \cdot 10 \mathrm{~Hz}$ to $25 \mathrm{KHz} \pm 3 \mathrm{~dB}$
Power requirements -20 to 35 volis
Outputs $-100 \mathrm{mV}+A B$ monitoring for tape
Controis - Press button for tape. radio and P.U selection Volume. Bass - 12 dB to - 14 dB at 100 Hz . Trebie +11 dB to -12 dB at 10 KHz


## Project 80 FM tuner smaller, more efficient

A truly remarkable tuner in every way - its unbelievably compact size its original cricuitiy - its dependable performance - all this in a boldly designed modern case measuring $85 \times 50 \times 20 \mathrm{~mm}$ ( $3 \frac{1}{2} \times 2 \times \frac{3}{4}$ ins) Greater adaptability (and possibly financial convenience) results from the tuner and stereo decoder section being made available separately

TECHNICAL SPECIFICATIONS
Size-85 - $50 \cdot 20 \mathrm{~mm}$ (approx $3 \frac{1}{2} \cdot 2 \cdot \frac{3}{\mid}$ Ins)
Tuning range -87 to 108 MHz
Detector-1 C. balanced coincidence, for good A. M. rejection
AFC - Switchable, with thermistor control to prevent from difi
One 26 transistor I.C.
Twin dual varicap tuning
Distortion-0 $3 \%$ at 1 KHz for 75 KHz deviation
Ceramic filter in I.F. section
Aerial impedance-75 $\Omega$ or $240-300 \Omega$
Sensitivity - 4 microvolts for 30 dB quietıng
Power requirements - 12 to 45 volts

## Project 80 stereo decoder

Making the Project 80 decoder separate from the F.M. tuner gives the constructor a wider choice of systems as well as saving money in cases where stereo reception may not be required This unit gives a 40dB channel separation with an output of 150 mV per channel. The gallium arsenide light emitting beacon automatically lights up to show when a stereo transmission is tuned in Designed essentially as an integral part of Project 80 systems, this multiplex stereo demodulator may be used in many cases with existing single channel frequency modulated tuners to provide stereo reception
Size $-47 \times 50 \backslash 20 \mathrm{~mm}$ (12-2, 3ns)
One 19 transistor I.C.


Solid-state stereo indicating beacon

- Readily adaptable for use with other tuners
R.R.P. f $7.45+\begin{gathered}0.74 \text { V.A.T } \\ \text { V. }\end{gathered}$


## new constructional techniques

## ... and again Sinclair leads the world

1962. Micro-miniature power amp small enough to stand on a $10 p$. piece. Slimline pocket receiver smaller than a 20 cigarette pack
1963 Micro-6 receiver, smaller than a matchbox
1964 Pocket F.M. receiver: PWM amp.
1965 Z. 12 power amplifier module: PZ. 3 power supply
1966 Stereo 25 pre-amp/control unit
1967 Micromatic: 0.14 loudspeaker: the first Neoteric
1968 IC. 10 , the first ever integrated circuit for constructors' use

## Project 80 active filter unit

This efficiently designed unit makes a highly desirable part of any worth while system where inputs may be from record, radio or tape As with Stereo 80. separate controls are applied to each channel thereby making it easier to obtain ideal stereo balance in any kind of indoor environment.

TECHNICAL SPECIFICATIONS
Size $-108 \times 50 \times 20 \mathrm{~mm}\left(4 \frac{1}{4} \times 2 \times\right.$ ans $)$
Voltage gain - minus 02 dB
Frequency response -36 Hz to 22 KHz . controls mınımum
Distortion - at $1 \mathrm{KHz}-003 \%$ using 30 V supply
HF cut off (scratch) -22 KHz to $55 \mathrm{KHz}, 12 \mathrm{~dB} /$ oct slope
L.F. cut off (rumble) -28 dB at 20 Hz . $9 \mathrm{~dB} /$ oct. slope

## Z. 40 \& Z. 60 power amplifiers totally short-circuit proof

Either of these entirely newpower amplifiers is intended for use in Project 80 installations although, of course, they are readily adaptable to an even wider range of applications Both $Z .40$ and $Z .60$ incorporate builtin protection against shortcircuiting and risk of damage arising from mis-use is greatly reduced. Comprehensive instructions are supplited with each of the modules
Z.40 Technical Specifications Size $-55 \times 80 \times 20 \mathrm{~mm}$
$\left(2 \frac{1}{8} \times 3 \frac{1}{8} \times \frac{10}{3}\right.$ ins) 9 transistors Input sensitivity - 100 mV Output -15 watts RMS continuous into $8 \Omega(35 \mathrm{~V}) .30$ watts music power|into $4 \Omega(30 \mathrm{~V})$
Frequency response $-10 \mathrm{~Hz}-$ $100 \mathrm{KHz}+1 \mathrm{~dB}$
Signal to noise ratio - 64 dB
Distortion - at 10 watts into $8 \Omega$
less than 0 1\%
Power requirements - $12-35$ volts

Z 60 Technical Specifications Size $-55 \times 98 \times 20 \mathrm{~mm}$
(21 $\times 3 \frac{3}{3} \times \frac{3}{2} \mathrm{n}$ ) 12 transistors Input sensitivity - $100-250 \mathrm{mV}$ Output-25 watts RMS into $8 \Omega(45 \mathrm{~V}) .50$ watts music power into $4 \Omega(50 \mathrm{~V})$
Distortion-typically $003 \%$ Frequency response -10 Hz to more than $200 \mathrm{KHz} \pm 1 \mathrm{~dB}$ Signal to noise ratio - better than 70dB
Built-in protection against transient overload and short circuit
Load impedance $-4 \Omega$ min: max safe on open circuit

Sinclair power supply units PZ. 8
the worlds most
advanced unit in its class
Stabilised power supply unit. Reentrant current limiting makes dam age from overload or even direc shorting impossible, a principle never before inorporated in a com. mercially avallable constructor modle. Normal working voltage (adjus abie) 45 V
R.R.P. £ $7.98+0.79 p \vee$ A.T

Without mans transtorme PZ.5 30V unstabilised
R.R.P. f $4.98+0.49$ p V.A.

PZ. 635 V stabilised

R.R P. £7.98+079p V A.T


[^5]Practical Electronics December 1973

1969 O .16 - improved version of Q .14 Systems 2000 and 3000:
Project 60!aunched
1970 IC. 12 Project 605
1971 Project 60 stereo FM tuner Z.50: PZ. 8
1972 Improvements to Project 60 with Z. 50 MK. 2 and PZ. 8 Mk. 3 The Executive Calculator: Digital multi-meter. Q. 30 speaker

1973 Cambridge Calculator
PROJECT 80 LAUNCHED


## From Sinclair <br> the worlds most advanced hi-fi modules

## Sinclair Project 80 the ultra-modern non-obtrusive hi-fi

 a shelf could be sufficient
be built into a book-shelf to contain a complete


The modules mount very easily onto a playing plinth

A novel application would be to buld around the base of a
lampshade

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