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## VALUE ADDED TAX

Prices quoted in this issue were correct at time of going to press. From Ist April 1973 there will be no purchase tax, but a large number of goods will carry Value Added Tax.

Our May issue will be published on Friday, April 13, 1973

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Better than -75dB
25 45V, SA25/35
40-70V, SA100
Size
$4 \frac{1}{2}$ in $\quad 4 \mathrm{in} \quad \operatorname{lin}(S A 100)$
4 in 3 in $\operatorname{lin}(S A 2 S, S A 35$
Circuits, connecting instructions and application data are supplied free with all modules

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Frea. response $\quad 20-20,000 \mathrm{~Hz} \pm 2 \mathrm{~dB}$
$\begin{array}{ll}\text { Construction } & \text { Fibreglass board }\end{array}$
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Low distortion parallel push-pull
Low distortion parallel push-pull output stage
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(As illustrated below. S.A.E. details. $9 V$ operation)
OUTPUTS UP TO IV RMS
OUTPUTS UP TO IV RMS


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$\mathbf{6 2 3 . 2 0 .}$

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## STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the market,
the PA100 stereo pre-amplifler has Designed for use with the AL50 power amplifier aystem, this quality made unit tecaniques. no less than eight silicon planar transictors, two of these are specislly selected low noige NPN devices for use in the input stages.
Three owitched stereo inputs, and rumble and scratch filters are features of the PA100, Which also has a STEREO/MONO switch, volume, balance and continuously variable bass and treble controls.

## SPECIFICATION


$20 \mathrm{~Hz}-20 \mathrm{KHz} \pm 1 \mathrm{~dB}$ Harmonic Distortion
2. Radio, Tuner
1.25 mV into $50 \mathrm{~K} \Omega$ 35 mV into $50 \mathrm{~K} \Omega$ 1.5 mV into $50 \mathrm{~K} \Omega$

All input voltages are for an output of 250 mV . Tape and P.U. inputs equalised to RIAA curve within $\pm 1$ liB. from 20 Hz to 20 KHz .

Bass Control
Rumble (High Ps8s) scratch (Low Pass) Ignal/Noise Ratio Input overload Supply
Dimensions
$\pm 15 \mathrm{~dB}$ at 20 Hz $\pm 15.18$ at 20 KHz KHz
better than -65 dB +28 dB
+35 vol
+35 volts at 20 mA
ONLY £11.95
SPECIAL COMPILETE KIT COMPRISING 2 AL50's, 1 SPM80, 1 BMT80 \& 1 PA100 ONLY £23.00 FREE p. \& p



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## II) <br> 1.2.-(Electronics)Ltd



THE HY41
The HY41 supersedes the popular HY40 introduced by ILP last vear. This highly improved module achieves true High Fidelity with a dramatic reduction in distortion (typically 0.05\% at 1 KHz into 8 ohms! and is electronically and mechanically compatible with the HY 40

With this important improvement the HY41 retains all of the quality characteristics found in the earlier version and P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete power amplifier of extremely high performance sufficiently versatile to provide power not merely for Hi-FI but also for public address systems and industry

The free manual gives a full circuit diagram of the HY41 and its various applications including a complete stereo amplifier.

Like its predecessor the HY41 is based on conventional and proven circuit techniques developed over recent vears.
OUTPUT POWER: British Rating 40 WATTS PEAK, 20 watts
R.M.S. continuous.

LOAD IMPEDANCE: 4-16 ohms.
INPUT IMPEDANCE: 30 K ohms at 1 KHz
VOLTAGE GAIN: 30 db at 1 KHz
TOTAL HARMONIC DISTORTION: less than 0.15\% (typical 0.05\%)
at 1 KHz .
FREQUENCY RESPONSE: $5 \mathrm{~Hz}-50 \mathrm{KHz}+1 \mathrm{db}$
SUPPLY VOLTAGE: +22 .5volts D.C
SUPPLY CURRENT: $\overline{0} 8$ amps maximum.
PRICE: inc. comprehensive manual, P.C. board, five extra components and $P$ \& $P$ :MONO: $£ 4.90$

## UVIQUE HYBRID PRE-AMPLIFIER

The HY5 has rapidly established a position in the WORLD as the sole hybrid pre-amplifier to contain all feedback and equalization networks within an integrated preamplifier circuit

Supplied with the HY5 are two stabilizing capacitors and by the addition of volume, treble and bass potentiometers it is ready for use.

Internally the HY5 provides equalization for almost every conceivable input, the desired function is achieved by use of a multi-way switch or by direct interconnection

Two distinctive features of the HY5 are its inbuilt stabilization circuit allowing it to be run off any unregulated power supply from 16-25 Volts and a balance circuit which, when linked by a balance control to a second HY5, forms a complete stereo priamplifier.

Specifically and critically designed to meet exacting Hi-Fi standards, the HY5 combines extremely low noise with a high overload capability. When used in conjunction with the HY41 and PSU45 forms a completely intergrated system.

## INPUTS

Magnetic Pick-up (within $\pm 1 \mathrm{db}$ RIAA curve) $2 \mathrm{mV} .47 \mathrm{~K} \Omega$
Tape Replay lexternal components to suit head). $4 \mathrm{mV} .47 \mathrm{~K} \Omega$
Microphone (flat) $10 \mathrm{mV} .47 \mathrm{~K} \Omega$
Ceramic Pick-up (equalized and compen. satable) $20-2000 \mathrm{mV}$. variable.
Tumer (flat) 250 mV . $100 \mathrm{~K} \Omega$
Auxiliary $1250 \mathrm{mV} .47 \mathrm{~K} \Omega$
Auxiliary $22-20 \mathrm{mv} .100 \mathrm{~K} \Omega$

OUTPUTS
Main Pre-amp output 500 mV .
Direct tape output 120 mV .
ACTIVE TONE CONTROLS (Bexendall)
Treble +12 db
Bass +12 db .
INTERNAL STABILIZATION
Enables the HY5 to share an unregulated

- supply with the Power Amplifier

SUPPLY VOLTAGE
16-25 volts
PRICE:
MONO: $£ 3.60$
STEREO: $£ 7.20$

POWER SUPPLY PSU45
The versatile P.S.U. 45 is designed to supply your HY 41 's + HY 5 's in stereo or mono format.

Specification
Input: 200-240 Volts.
Output: $\pm 22.5$ Volts at 2 amps .
Overall Dimensions: L. $7^{\prime \prime} ;$ D. $3.8^{\prime \prime} ;$ H. $3.1^{\circ}$
PRICE: $£ 4.50$ inc. $P . \&$ P.

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INTEGRATED CIRCUITS $S p+1 p$ ach added

| 1N21 | $\begin{aligned} & 80 \\ & 0.17 \end{aligned}$ | $\begin{array}{ll}  & 81 \\ \text { AFZ12 } & 1.00 \end{array}$ | ВY\％10 | $\begin{aligned} & e_{p} \\ & 0.86 \end{aligned}$ | 0AZ211 | $\begin{aligned} & \text { Pp }_{0} \\ & 0.82 \end{aligned}$ | 28170 | $\begin{aligned} & 80 \\ & 0.10 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1N23 | 0.20 | A8Y26 0.25 | BYZII | 0.32 | OAZ222 | 0.45 | 78271 | 0.18 |
| 1N85 | 0.88 | ASY27 0.82 | BYZ12 | 0.80 | OAZ223 | 0.46 | 2T01 | 0.25 |
| 1N253 | 0.60 | AsY28 0.26 | BYZ13 | 0.25 | OAZ224 | 0.45 |  | 0.25 |
| 1N256 | 0.80 | A8Y29 0.80 | ${ }^{\text {BYZ }}$ BYZ ${ }^{\text {a }}$ | 0.20 1.00 | OAZ241 | 0．22 | $7 \mathrm{~T} \times 107$ | 0.15 |
| 1N645 | 0.45 | A9Y36 0．25 | BYZ10 | 1.00 | OAZ242 | 0.28 | $7 \mathrm{TX107}$ | 0.18 |
| iN726A | 0.80 | A8Y50 0.17 | BYZ16 | 0.62 | 0.08244 | 0.22 | 7．TX108 | 0.12 |
| 1N914 | 0.07 | AsY01 0.40 | BYZARCW |  | 0.87248 | 0.23 | ZTX 300 | 0.18 |
| 1N4007 | 0.20 | ASY53 0.20 |  | 0.15 | OAZ290 | 0.88 | ZTX304 | 0.25 |
| 18113 | 0.16 | AsYǘ 0.20 | C111 | 0.65 | OC18 | 0.60 | 7TX500 | 0.16 |
| 18130 | 0.18 | ASY 0.20 .25 | CRslioj | 0.25 | $0 \mathrm{Cl} 6^{\prime} 1$ | 0.88 |  |  |
| 18131 | 0.18 | Asy8a 0.88 | CRSI／40 | 0.46 | ${ }_{0} \mathrm{CL} 19$ | 0.87 | \％TX503 | 0.17 |
| 18202 | 0.28 | AsZ： 10.48 | CSt ${ }^{\text {c }}$ | 2.60 | OC20 | 0.88 | $2 \mathrm{TX031}$ | 0.25 |
| $2 G 371$ | 0.28 | ${ }^{\text {Asze3 }} 0.76$ | Cs10］ | 8.18 | OC2\％ | 0.60 | INTEGRATED CIRCUITS |  |
| 2G881 | 0.25 | Aly ${ }^{0.98}$ | DD000 | 0.16 | Or 23 | 0.80 |  |  |
| $2 \mathrm{Cl4}$ | 0.30 | AL101 1.60 | DD003 | 0.16 | 0 OL 24 | 0.80 |  |  |
| $2 \mathrm{G417}$ | 0.29 | BCl 07 0.10 | Dpoos | 0.18 | $00^{20}$ | 0.87 | 74111 | 0.20 |
| 2 N 404 | $0-20$ | BC10s 0.10 | DD007 | 0.40 | Oc25 | 0.25 | T401 | 0.20 |
| 9N607 | 0.16 | $\begin{array}{ll}\text { BC109 } & 0.10\end{array}$ | DD00\％ | 0.88 0.88 | OC2\％ | 0.80 | $7+(1)$ | 0.20 |
| ${ }^{2} \mathrm{~N} \times 898$ | 0.40 | $\begin{array}{ll}\mathrm{BCl13} & 0.15 \\ 0.20\end{array}$ | GD3 | 0.88 | OC28 | 0.80 | $\underline{3} 403$ | 0.20 |
| 2N706 | 0.10 | RC115 0.20 | OD4 | 0.06 | OC29 | 0.60 | 7404 | 0.20 |
| 2N706A | 0.12 | BC116 0.26 | CD3 | 0.88 | O（3） | 0.40 | 740． | 0.20 |
| 2N708 | 0.15 | BC116A 0.80 | 9D8 | 0.28 | OC35 | 0.50 | － 4010 | 0.30 |
| 2N709 | 0.68 | $\begin{array}{ll}\mathrm{BCL1} \\ \mathrm{BCl} & 0.25\end{array}$ | GD1： | 0.08 0.80 | OC3i | 0.60 | 7404 | 0.30 |
| 2N1091 | 0.88 | $\begin{array}{ll}\text { BC121 } & 0.20 \\ \text { BC122 } & 0.20\end{array}$ | （ ${ }^{\text {E ET } 102}$ <br> （EET103 | 0.80 0.82 | OC＋1 |  | 7404 | 0.20 |
| 2N1181 | 0.25 | $\begin{array}{ll}\mathrm{BC122} & 0.20 \\ \mathrm{BCL}_{5} & 0.88\end{array}$ | （iETT03 GET113 | 0.28 0.20 | OCH | 0.26 0.80 | Ti09 | 0.45 0.20 |
| 2N1132 | 0.28 0.18 | $\begin{array}{ll}\mathrm{BC125} & 0.68 \\ \mathrm{BC124} & 0.85\end{array}$ | ${ }_{\text {GET }}^{\text {GET113 }}$ | 0.20 | OC42 | 0.80 0.40 | $i+10$ | 0.20 0.23 |
| 2N 1303 | 0.18 | BC140 0.65 | （iET115 | 0.46 | OC44 | 0.17 | i＋19 | 0.42 |
| 2 N 1304 | 0.22 | BC14 0.18 | GET11i | 0.60 | 0 CH 4 M | 0.17 | $\bigcirc 113$ | 0.80 |
| 2 N 1305 | 0.28 | BC148 0.18 | GET120 | 0.25 | $0 \mathrm{OC45}$ | 0.12 | － | 0.30 |
| 2N1306 | 0.85 | BC149 0.16 | GET87： | 0.30 | $0 \mathrm{CH5}$ | 0.18 | $\bigcirc$ | 0.30 |
| $2{ }^{2} 1307$ | 0.85 | $13 \mathrm{Cl5} \quad 0.15$ | GET870 | 0.25 | $0 \mathrm{C46}$ | 0.27 | －+1.20 | 0.20 |
| 2N1308 | 0.25 | BC158 0.12 | （ ${ }^{\text {ETP680 }}$ | 0.37 | Oc57 | 0.80 | \％ | 0.48 |
| 2 N 214 | 0.78 | BC160 0.68 | （ ${ }^{\text {ETPT881 }}$ | 0.25 | OCä | 0.60 | 7423 | 0.48 |
| 2 N 2148 | 0.80 | BC169 0．13 | GETB8： | 0.25 | OC59 | 0.85 | － 42 | 0.48 |
| 2 N 2160 | 0.60 | BCY31 0.85 | GET885 | 0.25 | 0C68 | 0.50 | 74：27 | 0.42 |
| ${ }^{2} \mathbf{2 N} 2218$ | 0.20 0.20 | BCY3： 0.56 | （：EX44 <br> （1）EX45／1 | 0.08 0.10 | OC70 | ${ }_{0}^{0.12}$ | －＋ | 0.60 0.80 |
| ${ }_{2} \mathrm{~N} 2369 \mathrm{~A}$ | 0.16 | нe：Y33 0.25 | GEX941 | 0.16 | $0 \mathrm{Cb}^{2}$ | 0.20 | 74．301 | 0.20 0.48 |
| 2 N 2444 | 1.99 | BCY34 0.30 | GJ3M | 0.28 | OC73 | 0.80 | －139 | 0.48 0.70 |
| $2 \mathrm{~N}^{2813}$ | 0.28 | BCY38 0.40 | （i， 5 M | 0.88 | OC74 | 0.80 | 74：37 | 0.85 |
| 2N 2646 | 0.45 | BCY39 1.00 | （iJ5M | 0.26 | OCis | 0.88 | － | 0.65 |
| 2 N 2904 | 0.20 | BCY40 0.50 | （1J7M | 0.87 | 0 C 76 | 0.25 | $7+41$ | 0.20 |
| $2{ }^{2} 2904.4$ | 0.25 | BCY4： 0.85 | hatious | 0.80 | $\mathrm{OCO}_{0}$ | 0.40 | －4＋1心 | 0.76 |
| 2N2906 | 0.20 | BCYTO 0.16 | H8100A | 0.20 | 0 C78 | 0.20 | －4t： | 0.76 |
| $2 \mathrm{~N}^{2907}$ | 0.28 | ${ }^{\text {RCY }} 710.80$ | Mati00 | 0.85 | OC79 | 0.28 | － 4.95 | $0 \cdot 20$ |
| 2 N 2924 | 0.28 | BCZ10 0．85 | Matl0］ | 0.80 | $0{ }^{0} 81$ | $0 \cdot 20$ | T＋51 | 0.20 |
| 2 N 2925 | 0.16 | $\begin{array}{ll}\text { BCZ11 } & 0.60\end{array}$ | Mati？0 | 0.25 | oc811 | 0.80 | － | 0．20 |
| 2 N 2926 | 0.10 | B1121 0.85 | Matipl | 0.30 | 0c81M | 0.20 | － $7+54$ | 0.20 |
| $2 \mathrm{~N}^{2} \mathbf{0 5 4}$ | 0.60 | $\begin{array}{ll}\text { BD123 } & 0.80 \\ \end{array}$ | MJE520 | 0．87 | OC81D ${ }^{\text {ch }}$ | 0.18 | T 46 | 0.20 |
| 2 N 3055 | 0.75 | BD124 0.75 | MJE295\％ | 1.37 | OC817 | 0.40 | 74\％ | 0.30 |
| $2 \mathrm{2N}^{3} 702$ | 0.10 | BDY11 1.68 | MJE3050 | 0.87 | $0 \mathrm{OC82}$ | 0.26 | 隹里 | 0.80 |
| 2 N 3706 | 0.10 | BF115 0．25 | NKT128 | 0.38 | OC． $\mathrm{Ca}_{2} 11$ | 0.20 | －173 | 0.40 |
| 2 N 3706 | 0.28 | EF11i 0．50 | NKT129 | 0.30 | 0 C 83 | 0.25 | \％ 714 | 0.40 |
| 2N3707 | 0.12 | BF167 0．26 | NKT211 | 0.26 | OC84 | 0.85 | －4， | 0.56 |
| 2N3709 | 0.10 | BF173 0.25 | NKT213 | 0.25 | OCll4 | 0.38 | 84 | 0．48 |
| 2 N 3710 | 0.10 | ${ }^{\text {BFP181 }} 00.85$ | NKT214 | ${ }_{0}^{0.15}$ | $0 \mathrm{OC122}$ | 0.60 | \％ $4 \times 4$ | 0.48 0.80 |
| 2 N 3711 | 0.10 | BF184 0.20 | NKT216 | 0.37 | $0 \mathrm{OC123}$ | 0.86 | － $4 \times 4$ | 0.80 0.87 |
| 2 N 3819 | 0.85 | BF185 0.20 | NKT217 | 0.35 | OC139 | 0.88 | 74 $7 \times 4$ | 0.87 1.00 |
| 2 N 5027 | 0.88 | ${ }^{\text {BF }} 1940.17$ | NKT218 | 1．18 | OCl40 | 0.85 | － | 1．80 |
| 2N5088 | 0.88 | ${ }^{\text {BF }} 19500.16$ | NKT219 | 0.88 | OC14 1 | 0.60 | i484 | 0.90 0.45 |
| 28801 | 0.60 | BF196 0.15 | NKT222 | 0.20 | 0 Cl 69 | 0.20 | － | 0．45 |
| 29304 | 0.76 | BF197 0．15 | NKT224 | 0.22 | ${ }_{0} \mathrm{OC170}$ | 0.85 |  | 0.76 1.00 |
| 28501 | 0.87 | BFB61 0．28 | NKT251 | 0.24 | $0 \mathrm{Cl171}$ | 0.80 | 7491． | 1.00 0.75 |
| 28702 | 0.62 | AFS98 0．28 | NKT271 | 0.25 | OC200 | 0.40 | 7492 | 0.75 0.76 |
| AA129 | 0.80 | BFX12 0.20 | NKT27： | 0.25 | OC201 | 0.70 | － 493 | 0.76 0.80 |
| AAZ12 | 0.80 | $\begin{array}{ll}\text { BFX } 13 & 0.25\end{array}$ | NKT273 | 0.15 | OC20：2 | 0.80 | 7494 |  |
| Aaz13 | 0.12 | BFX 290.25 | NKT274 | 0.20 | Oc203 | 0.40 | 749．j | 0．80 |
| AC107 | 0.37 | $\begin{array}{ll}\text { BFX } 30 & 0.25\end{array}$ | NKT275 | 0.28 | OC204 | 0.40 | ${ }_{7}+96$ |  |
| AC126 | 0.20 | BFX35 0.98 | NKT437 | 0.20 | oc20b | 0.78 | ${ }^{7} 497$ | 8.25 |
| AC127 | 0.25 | BFX63 0.50 | NKT278 | 0.28 | OC206 | 0.90 | ${ }^{2} 4100$ | 2.50 |
| AC128 | 0.20 | BFX84 0．25 | NKT301 | 0.40 | OC20\％ | 0.90 | ${ }^{74107}$ | 0.50 |
| AC187 | 0.25 | BFX85 $\quad 0.30$ | NKT304 | 0.76 | OC460 | 0.20 | T4710 | 0．80 |
| AC188 | 0.85 | BFX86 0．25 | NKT403 | 0.76 | 0C470 | 0.30 | 74111 | $1 \cdot 45$ |
| ACY 17 | 0.80 | BFX87 0.25 | NKT404 | 0.85 | OCPil | 0.97 | T＋118 | $1 \cdot 00$ |
| ACY18 | 0.25 | BFX88 0.20 | NKT678 | 0.30 | ORP12 | 0.50 | 74114 | 1.00 |
| ACY 18 | 0.25 | BFY10 1.00 | NKTild | 0.28 | ORP60 | 0.40 | 74121 | 0.80 1.85 |
| ACY20 | 0.20 | BFY11 1.26 | NKT733 | 0.25 | 0RP61 | 0.42 | 741 | 1.85 |
| ACY21 | 0.20 | BFY17 0.25 | NKT77\％ | 0.38 | \＄19T | 0.20 | 74123 | 2.70 |
| ACY22 | 0.10 | BYF18 0.25 | 07813 | 0.38 | sactu | 0.25 | 74141 | 1.00 |
| Acy 27 | 0.26 | HFY19 0．25 | OAS | 0.20 | SFT308 | 0.88 | 74145 | 1．80 |
| ACY28 | 0.17 | BFY24 0.46 | оаб | 0.12 | $8 \mathrm{ST}^{42}$ | 0.88 | 7410f | 3．85 |
| ACY39 | 0.60 | BFY44 ${ }^{1.00}$ | OA47 | 0.10 | ${ }_{4 T}{ }^{\text {S }} 681$ | 0.68 | 74151 |  |
| ACY40 | 0.15 | HFY50 0．22 | OAJ0 | 0.10 | 8x68 | 0.20 | 74104 | 8.00 |
| ACY41 | 0 －16 | ${ }^{\text {BFY51 }} 0.20$ | OA7！ | 0.10 | 8X631 | 0.30 | 7415 | 1.55 |
| ACY44 | 0.25 | BFY02 0．22 | 0at3 | 0.10 | $8 \times 635$ | 0.40 | 74156 | 1.55 |
| AD140 | 0.50 | $13 \mathrm{FY53} \quad 0.17$ | OA74 | 0.10 | 8x 840 | 0.60 | 74157 | 1.80 |
| AD149 | 0.50 | BFY64 0.42 | OA79 | 0.10 | $8 \times 641$ | 0.55 | 7＋10］ | $4 \cdot 10$ |
| AD161 | 0.87 | BFY90 0．65 | OA81 | 0.08 | SX642 | 0.60 | 74174 | ع．00 |
| AD162 | 0.37 | BSX27 0.50 | 0.885 | 0.12 | 5X644 | 0.75 | $\underline{4175}$ | $1 \cdot 35$ |
| AF106 | 0.30 | BgX 600.98 | 0.886 | 0.15 | SX645 | 0.75 | 74176 | 1.60 |
| AF114 | 0.25 | B9xi6 0.16 | 0 A 90 | 0.08 | F15／30P | 0.60 | 7＋190 | 1.95 |
| AF115 | 0.25 | BSY26 0．18 | OA91 | 0.07 | V30／201P | P 0.75 | 74191 | 1.96 |
| AF116 | 0.25 | Bsy27 0．17 | $0 \times 95$ | 0.07 | 160／201 | 0.50 | $7+192$ | 2.00 |
| AF117 | 0.25 | BEY51 0.50 | OA200 | 0.07 | ＇60／2011 | 0.75 | $7+193$ | 2.00 |
| AF118 | 0.62 | BSY95A $\quad 0.12$ | OA202 | 0.10 | X 101 | 0.10 | 74194 | $2 \cdot 50$ |
| AF119 | 0.20 | B9Y95 0.12 | OA210 | 0.26 | X 1102 | 0.18 | $7+10.7$ | $1 \cdot 66$ |
| AF124 | 0.25 | HT102／500R | OA211 | 0.30 | x 1151 | 0.16 | $7+196$ | 1.50 |
| AF125 | 0.20 | 0.75 | OAZ200 | 0.55 | X． 1152 | 0.16 | $7+197$ | 1.50 |
| AF128 | 0.17 | BTY4： 0.82 | OAZ201 | 0.50 | XA161 | 0.25 | 7419 H | 4.60 |
| AF127 | 0.17 | 13T $\times 79 / 100 \mathrm{R}$ |  |  | XA162 | 0.25 | $7+199 \quad 4 \cdot 80$ |  |
| AF139 | 0.80 | HTY\％9／400 0.75 | OAZ203 | 0.42 | XB101 | 0.48 | $\begin{aligned} & \text { lug insucket* } \\ & \text { how profle } \\ & \text { H fin } 1 \text { OHL } \\ & 0.15 \\ & 16 \text { !in D } 1 \mathrm{~L} \\ & 0.17 \end{aligned}$ |  |
| AF178 | 0.55 |  | OAZ204 | 0.30 | X B101 $\times 8102$ |  |  |  |
| AF179 | $0 \cdot 65$ | 1.25 | OAZ205 | 0.48 | X 8102 | 0.10 |  |  |
| AF180 | 0.62 | BY100 0.15 | OAZ206 | 0.42 | X Bl 103 | 0.25 |  |  |
| AF181 | 0.42 | BY126 0.15 | $0 \mathrm{OAZ207}$ | 0.47 | X B 113 | 0.12 |  |  |
| AF188 | 0.40 | $\begin{array}{ll}\text { BY127 } & 0.17\end{array}$ | OAZ208 | 0.32 |  |  |  |  |
| AFY19 | 1.18 | $\begin{array}{ll}\text { BY } 182 & 0.85\end{array}$ | OAZ209 | 0.82 | ${ }^{\text {X }}$－${ }^{\text {P124 }}$ | 0.68 |  |  |
| AFZ11 | 0.80 | $\begin{array}{ll}\text { BY213 } & 0.25\end{array}$ | OAZ210 | 0.22 |  |  |  |  |

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## P．E．SOUVD SYTIIESSER

Get away to a flying start with this exciting Space Age project． Precision cut metal parts to form modular units as described in the March issue are available NOW．
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## FASHIONS IN BUILDING

As a constructors magazine Practical Electronics is naturally very much concerned with building methods and materials. In its fairly short history, electronics has evolved through three distinct periods represented by different fashions in constructional techniques. First was the wood or original "breadboard" era; then the metal era dominated by the box-like chassis; now the plastics era is here with s.r.b.p. board (in some form or another) providing the main platform for the assembly of circuit components.

In many modern designs metalwork is no longer an essential part of the structure carrying the circuit components. Frequently, metalwork is used in a subservient role, merely to enclose or protect an electronic assembly which exists as a more or less self-contained entity built upon a piece of laminated plastics board.

The "plastics era" dawned soon after the arrival of the transistor. Right at the outset of this momentous technological event, industry was able to accommodate this newcomer by adopting printed circuit techniques. These techniques were already well established and in use with miniature valves. While the printed circuit was an ideal technique for mass production of electronic assemblies. it was not so ideal for the private constructor and his "oneoff 's". So when transistors became available to the individual, improvisation was called for, and a period of great inventiveness ensued. Many varied (and some quite unexpected) building techniques were tried out.

As a start. existing standard items such as component group boards and tag strips were commonly pressed into service as a platform for a transistorised circuit. Assemblies of varying degrees of elegance were built on odd scraps of s.r.b.p. laminate board, hardboard, and even cardboard. The arrival of perforated s.r.b.p. board helped towards a tidier form of construction and eliminated the drudgery of drilling countless holes. However, there was no universally adopted method for home construction until, some 12 years after the first transistor, there appeared in this country the first purpose-designed proprietary printed wiring board. Like many brilliant and successful ideas, this product was, in essence, beautifully simple and-after the event-so obvious. In due course this printed wiring board, though of course initially conceived with the professional user in mind, was to prove the answer to most private constructors' needs, and in time it rationalised the construction of electronic circuits.

Practical Electronics played not an insignificant part in bringing this constructional method to the attention of the amateur. This particular board was introduced to constructors in the very first issue of this magazine, and subsequently has been used in the majority of our projects.
Though very popular, the printed wiring board has no monopoly however. and the constructor has a fair choice of alternative methods, including home-made printed circuits. But practically all methods used today are based on the plastics board, the indispensable material which provides, the foundations for modern electronic assemblies.- F.E.B.

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# PE SoundSyntheriser 3 volinceronianted ostilditivis and IWUERTE: <br> <br> By G.D.SHAW 

 <br> <br> By G.D.SHAW}

THis month the voltage controlled oscillator and voltage inverter will be described as well as details for assembling them.

## THE VOLTAGE CONTROLLED OSCILLATOR

Perhaps the most important reason for the employment of a voltage controlled oscillator lies in the resultant ability of the oscillator to produce tone patterns by application of varying voltages to its control input. If these voltages are derived from what is essentially another oscillator, or series of oscillators, running at ultra low frequency, then the performance of the tone generating oscillator becomes quite automatic and dependent only on the continued operation of the programming devices.

The oscillators in the Synthesiser are based on the operational linear integrator and the circuit is shown in Fig. 3.1. In this arrangement ICl acts as the integrator while IC2 is connected as a comparator and serves to switch the direction of integration.

The integrator programming signal is applied across the diode bridge D1-D4 and it is important that the polarities are maintained as shown.

## CIRCUIT ACTION

To describe the circuit action assume that the comparator is sitting at its positive saturation level then diodes D1 and D3 in the integrator input bridge are reverse biased. There is a current flow into the integrator summing junction through R1, D2 and similarly a current flow away from the bridge through D4, R2, shown by solid arrows, so that the integrator begins to ramp negatively. The negative excursion of the integrator output voltage will continue until the current driven through R5 is equal to or greater than the current driven through R4 as a result of the output voltage of the compartor. At this time the voltage at point $P$ will go negative and the comparator will switch rapidly to its negative saturation level.

Under these conditions diodes D2 and D4 in the integrator input bridge are reverse biased and current flows are established as shown by the dotted arrows. In the case of the current flow away from the integrator summing junction, this causes the integrator to ramp positively.

## WAVESHAPES DEVELOPED

Providing that R2 is the same value as R1 and both polarities across the input bridge are at the same potential then the rate of change of integrator
output voltage is the same as before and the result is a symmetrical triangular waveform appearing at point $Q$. The oscillogram of Fig. 3.1 shows the phase relationship between the triangular waveform generated by the integrator and the switching waveform generated by the comparator at point $R$ in the circuit.

When the integrator output voltage is again equal to or greater than the level of positive feedback set by R4 the comparator switches back to its positive saturation level and the cycle repeats.

## FREQUENCY CONTROL

Consideration of the foregoing reveals that R4 actually plays a part in the determination of fre-

quency by setting the point at which the integrator output causes the comparator to switch.

Lowering the value of this component has the effect of increasing the level of positive feedback to the comparator thereby requiring a higher integrator output voltage to switch the comparator and thus lowering the frequency of operation of the integrator.

Conversely, if the value of R4 is increased the overall frequency of operation is also increased.

## PRACTICAL V.C.O.

The circuit shown in Fig. 3.2 is the three stage prototype v.c.o. arrangement. Starting from the output end, the third stage is a practical form of the oscillator shown schematically in Fig. 3.1. The second stage consists of two operational amplifiers arranged to provide a differential output across the oscillator input bridge. This particular stage is necessary since, in order to attain the full frequency range, the oscillator requires a drive potential greater than the individual power supply rails can provide.

The first stage of the circuit is a buffer/follower which serves to reduce the current drive required from the control source and which also provides a test-bed on which to try out various forms of circuit response without the necessity of disturbing the settings of the oscillator and differential driver. The type of input stage used in the v.c.o. is of some importance since it has a bearing, not only on the performance of the oscillator as a whole, but also on the design and operation of other circuits in the synthesiser. The response of the input stage may therefore be either linear or logarithmic and there are advantages and disadvantages attached to both methods.

## LOGARITHMIC OSCILLATORS

Most commercially available synthesisers use logarithmic v.c.o.s in which the slope of the response


Fig. 3.1. Basic voltage controlled oscillator. Oscillogram shows phase relation between integrator and comparator outputs. The inclusion of the capacitor shown dotted linearises the input voltage/frequency relationship.
is adjusted so that equal increments of input voltage raise the frequency of oscillation by one semitone.

A typical response curve is shown in Fig. 3.3. This has the distinct advantage that if, say, three oscillators are programmed simultaneously by the same control voltage, two of the oscillators may be manually offset by fixed multiples of the semitonal voltage increment so that the effect of the mixed oscillator output is that of producing a chord by the depression of only one key.

The arrangement of having equal voltage increments per semitone also allows for a simplification in the construction of the keyboard divider network and some commercial instruments use a series chain of equal value resistors with a form of "tuning" control which varies the voltage across the chain.


Fig. 3.2. Circuit diagram of the three stage voltage controlled oscillator

## LINEAR V.C.O.'s COMPARED

The oscillators in this Synthesiser are arranged with an input stage having a linear performance such that the overall response is as shown in Fig. 3.4.

The resulting loss of the ability to play "chords" was not considered a disadvantage when weighed against the advantages of simplification in building and setting up. Furthermore, the use of linear characteristics in the oscillators provides greater justification for the use of a parallel divider network in the keyboard which, although rather more complex than the series arrangement, means that the accuracy of each semitone is dependent only on the accuracy and stability of its own resistors and not upon the remainder of the chain.

The overall performance of the oscillator, however, is solely dependent upon the response characteristic of the buffer/follower stage and it will be noted that space has been left on circuit board B (Fig. 3.6) for the benefit of constructors who may wish to try out their own ideas of logarithmic response.

The SN76502 manufactured by Texas Instruments is a logarithmic amplifier in integrated circuit'form.

## MAJOR COMPONENTS

The estimated total cost of this project is around $\mathbf{2 2 0 0}$. Obviously this figure can be reduced if bulk purchase of components which will appear in quantity is made. To make this possible, components in excess of 12 are listed below.

| Resistors | Quantity |
| :---: | :---: |
| $10 \mathrm{k} \Omega$ | 52 |
| $33 \mathrm{k} \Omega$ | 12 |
| All 5\% $\frac{1}{2}$ watt carbon |  |
| $5.1 \mathrm{k} \Omega$ | 13 |
| 7.5ks | 36 |
| 10 k S 2 | 15 |
| All $2 \% \frac{1}{2}$ watt metal oxide |  |
| Potentiometers | Quantity |
| $10 \mathrm{k} \Omega$ carbon linear | 19 |
| All 25 mm dia. midget moulded carbon types |  |
| $10 \mathrm{k} \Omega$ carbon linear horizontal presets | s 12 |
| $100 \Omega$ linear horizontal Cermet presets | S 53 |
| $10 \mathrm{k} \Omega$ linear horizontal Cermel presets | - 21 |
| Integrated Circuits | Quantity |
| 741C 8 pin D.I.L. | 56 |
| Diodes | Quantity |
| $\begin{aligned} & \text { 1N914 } \\ & \text { 1SJ50 } \end{aligned}$ | $\begin{aligned} & 39 \\ & 14 \end{aligned}$ |
| Capacitors | Quantity |
| $470 \mu \mathrm{~F}$ elect. 25 V $0.01 \mu \mathrm{~F}$ polyester | $\begin{aligned} & 12 \\ & 46 \end{aligned}$ |
| Sockets | Quantity |
| 3.5 mm miniature jack sockets | 15 |
| 2 mm miniature sockets | 48 |



Fig. 3.3. Logarithmic response curve showing the positive exponential relationship obtained when control voltage required is IV/octave


Fig. 3.4. Linear response curve of v.c.o. showing frequency range of keyboard

The advantage of this device is that its response slope may be varied by adjustment of one external component so that performance matching becomes a relatively simple matter.

## BUILDING THE OSCILLATOR

Due to the restricted space in the finished module construction should start by assembly and wiring of all the components on to the front panel before the panel is mounted to the circuit board support plate. Figs. 3.5 and 3.6 give the front panel drilling details and component layout. The leads from the controls should be formed into a harness which passes down the centre of the panel between the potentiometers as shown, those for routing to the circuit boards being about ten inches long.

Next mount the McMurdo plug to the rear of the circuit board support plate complete with its wire leads already soldered into position. Fit the eight stand-off supports to the plate-transipillars are recommended but six B.A. screws with metallic spacers may be used providing that these are isolated from the conducting strips on the circuit boards.

The front panel should now be fixed to the circuit board support plate using a 4B.A. countersunk screw and nut in the upper hole, and the locking rod and bush in the lower one. If the assembly seems to be


Fig. 3.5. Front panel component assembly and wiring with details of mounting and disposition of boards on the module support plate. The small ringed $X$ at the board edges indicates orientation. (See board details)
on the slack side this may be corrected by fitting a thin steel washer between the bush and lug on the circuit board support plate.

It is useful, at this stage, to make up a jumper lead carrying power supplies from the main busbars so that modules may be tested and set up outside the main frame assembly. The lead should be about 24 in ( 61 cms ) in length terminated at one end by a McMurdo plug and at the other by a McMurdo socket wired to match the power supply outputs.

Figs. 3.7 and 3.8 show the circuit board layouts for the oscillator. Board A carries the differential output stage together with the oscillator itself and two of these boards are required.

Board B carries the buffer input stages and power supply decoupling stages for both the other boards.



Fig. 3.6. Drilling details for v.c.o. module front panel

## BOARD B

The next stage of construction covers assembly of the buffer input stage and power supply decoupling Board B. 1 Fig. 3.7 shows the recommended layout. Wiring of the completed board into the support frame is simplified if single ended Veropins are inserted into the boards at the indicated positions of the lead out wires.

Mount Board B to the support plate adjacent to the front panel and couple up the leads to the power supply, VRI (manual frequency control) and external input sockets. The leads to. Boards $A$ may be omitted at this stage.

## COMPONENTS . . .

VOLTAGE CONTROLLED OSCILLATOR (2 REQUIRED)

| Resistors |  |  |  |
| :---: | :--- | :--- | :--- |
| R1 | $10 \mathrm{k} \Omega$ | R 13 | $62 \mathrm{k} \Omega$ |
| R2 | $10 \mathrm{k} \Omega$ | R 14 | $750 \Omega$ |
| R3 | $120 \mathrm{k} \Omega$ | R 15 | $750 \Omega$ |
| R4 | $24 \mathrm{k} \Omega$ | R 16 | $62 \mathrm{k} \Omega$ |
| R5 | $10 \mathrm{k} \Omega$ | R 17 | $10 \mathrm{k} \Omega$ |
| R6 | $10 \mathrm{k} \Omega$ | R 18 | $10 \mathrm{k} \Omega$ |
| R7 | $9.1 \mathrm{k} \Omega$ | R 19 | $100 \mathrm{k} \Omega$ |
| R8 | $9.1 \mathrm{k} \Omega$ | R20 | $47 \Omega$ |
| R9 | $82 \mathrm{k} \Omega$ | R21 | $47 \mathrm{k} \Omega$ |
| R10 | $75 \mathrm{k} \Omega$ | R22 | $470 \mathrm{k} \Omega$ |
| R11 | $200 \mathrm{k} \Omega$ | R23 | $1 \mathrm{M} \Omega$ (see text) |
| R12 | $200 \mathrm{k} \Omega$ | R24-R25 | $10 \Omega$ (2 off) |
| All |  |  |  |

All $2 \% \frac{1}{2}$ watt metal oxide

## Capacitors

C1-C10 $\quad 0.01 \mu \mathrm{~F}$ Polyester (10 off)
C11-C12 1,000 pF Silver Mica (2 off)
C13-C14 1,500 pF Silver Mica (2 off)
C15 300 pF Silver Mica
C16-C17 $470 \mu$ F elect. 25 V (2 off)
Diodes
D1-D8 1N914 (8 off)
Potentiometers
VR1 $10 \mathrm{k} \Omega$ carbon log
VR2 $100 \Omega$ horizontal preset
VR3 $10 \mathrm{k} \Omega$ horizontal preset
VR4 $47 \mathrm{k} \Omega$ horizontal preset
VR5 $10 \mathrm{k} \Omega$ horizontal preset
VR6 $10 \mathrm{k} \Omega$ horizontal preset
VR7 $10 \mathrm{k} \Omega$ horizontal preset
VR8 $10 \mathrm{k} \Omega$ horizontal preset
VR9 $10 \mathrm{k} \Omega$ midget moulded carbon linear
VR10 $10 \mathrm{k} \Omega$ midget moulded carbon linear

## Integrated Circuits

IC1-IC5 741C 8 pin dual-in-line (5 off)

## Miscellaneous

SK1-3.5mm jack socket, SK2-SK3 2mm miniature socket ( 2 off) 0.1 in matrix Veroboards as required.

## CHECK-OUT

Set VR3 to mid position and VR2 to the minimum position and attach the jumper lead: With the power supply switched on and VR1 at minimum position measure the voltage at VR1 wiper. Adjust VR2 on both drivers so that voltages are exactly the same.

The value is not critical at this stage but is preferably in the range -5 mV to -10 mV . Measure the output voltage of both drivers and adjust VR3 until it is equal to whatever voltage has been set on the wipers of VR1.

Connect a temporary link between the external input and ground on both drivers. The purpose of these links is to simulate a zero-voltage prewired programming connection and they will be removed on completion of the setting up of the oscillators. Finally, set VR1 to its maximum position and measure the voltage at the sliders. This should be about -750 mV , depending on the actual potential of the power supply rails, any discrepancy between the two readings being corrected by adjustment of the values of R3 and/or R4.

## BOARD A: ASSEMBLY AND CHECK-OUT

Assembly of Board A should commence with the differential output stage which should be constructed up to and including R11 and R12. This stage should now be set up before proceeding with the construction of the oscillator.

Make temporary power supply connections from Board B, attach an input lead to the differential output stage and connect this directly to ground. With VR4 and VR5 at their maximum settings and VR6 and VR7 at their mid positions switch on.

Monitor the output voltages of both halves of the stage and adjust VR6 so that the output of IC2 reads +5 mV and VR7 so that the output of IC3 reads -5 mV . Now reconnect the input of the differential stage to the output of the driver from which the power supply is being taken and set the output voltage of the driver to -25 mV by means of VRI.

Monitor the outputs of IC2 and IC3 and adjust VR4 and VR5 until these read +255 mV and -255 mV respectively. Repeat the measurements at various settings of VR1 to ensure that the gain of each half of the stage is linear at $\times 10$ throughout the working range. Remember that the actual readings should be, in the case of IC2, $+[5 \mathrm{mV}+$ ( $10 \times$ driver output voltage)] and in the case of IC 3, $-[5 \mathrm{mV}+(10 \times$ driver output voltage $)]$.

Having set the gain and offset of the differential output stage the assembly of the oscillator section may now be completed (Fig. 3.8).

## CHOICE OF CAPACITOR

The type of capacitor used in the integrator is of some importance as far as frequency stability is concerned and it is best to use a type having low leakage and as low a value of inductance as possible. Silver mica is thus the best choice and the value shown may be made up of two or more parallel wired capacitors.

R23 serves to limit the current output of the comparator. With this omitted the comparator has only the forward resistance of $D 5-8$ between its output and ground and, although IC5 is capable of handling the current involved, this means that a substantial ripple will be present on the oscillator power supply rails and could possibly be transmitted through to


Fig. 3.7. Component layout and wiring for Board B. Since two v.c.o.'s are required, components for each are arranged in board areas B1 and B2


Fig. 3.8. Component layout and wiring for Board $A$. Two of these are required as shown in Fig. 3.5
the main bus-bars. Thus, where it is intended to use the comparator square wave output as a signal source the value of R23 should be 2.2 kilohms, that is, sufficient to reduce the ripple to an acceptable level. When the square wave output is not to be used, such as in the keyboard oscillators, the value may be increased to 1 Megohm to reduce ripple to negligible proportions. The inclusion of this resistor will however reduce the triangular wave voltage swing to 200 mV p-p and limit the maximum frequency of the oscillator to about 8.3 kHz .

R13 to R16 and VR8 form a divider network which provides a value of bias current to the summing junction of the integrator.

## MOUNTING THE A AND B BOARDS

The completed A boards should be mounted on the support plate such that one is immediately


Fig. 3.9. Circuit diagram of voltage inverter

## COMPONENTS . . .

## INVERTER <br> Resistors <br> R1-R3 10k $\Omega$ (3 off)

## Integrated Circuit

IC1—741C 8 pin D.I.L.

## Miscellaneous

SK1-SK3 2 mm miniature sockets (3 off) 0.1 in matrix Veroboard as required


Copper strips broken at holes $614,15,16,17$
Fig. 3.10. Inverter component Board $C$ layout and wiring
adjacent to the McMurdo plug and the other directly above Board B. It is best to mount and set-up the oscillator boards one at a time. When a board has been fully connected, set VR8 and VRI to their mid positions and switch on the power supply. Observe the triangular waveform on the oscilloscope -the frequency of oscillation should be about 7 kHz .
Gradually reduce the setting of VRI until the waveform begins to exhibit marked signs of assymmetry. At this point adjust the setting of VR8 with great care to restore the symmetry, this latter operation also being seen to cause an increase in the frequency.

Continue reducing the setting of VRI, adjusting VR8 as necessary, until VR1 is at its minimum setting and the output waveform is symmetrical.

At very low frequencies the setting of VR8 is extremely critical, too large a shift in either direction causing IC4 to saturate. If this happens, VRI should be set to its mid position again and the various steps repeated.

With VRI in its minimum position final setting of the very low frequency end of the range is accomplished by adjustment of VR2 in conjunction with VR8 as before. If IC4 saturates at or before minimum setting of VR1 the setting of VR2 will have to be increased.

Very low frequency instability can be a problem with this type of oscillator and although it can be made to operate at less than 1 Hz with the component values given it is best to set the minimum operating frequency to about 5 Hz .

## MATCHING THE OSCILLATORS

If the component values and tolerances specified have been adhered to, comparison of performance between both oscillators will show that the input voltage/frequency relationship is substantially similar, any differences in performance characteristic being due to tolerance variations in the components.

Extreme accuracy in the matching of oscillators is not necessary since linear response is involved.

## INVERTER

Little need be said concerning the assembly of the voltage inverter which is essentially an inverting unity gain amplifier of the simplest kind. The circuit is shown in Fig. 3.9 while the recommended circuit board layout is shown in Fig. 3.10.

The completed board should be mounted directly over the A board furthest from the front panel.

## USING THE MODULE

On completion of the whole module use the voltage inverter to investigate the effects of mixing triangular and square waves at varying frequencies.

The output may be fed to the high level input of most power amplifiers, but bear in mind that the output will be equal to the sum of the voltage swings at the inputs.

Additionally it is possible to carry out some simple experiments in frequency modulation by setting one of the oscillators to modulate the other. A low amplitude modulation at about 7 Hz produces a true vibrato to the tone of the modulated oscillator whilst varying the amplitude and frequency of modulation can produce some strange, even bizarre effects.

Next month: the ramp generators and input amplifiers are described.


This article describes a d.c. power supply unit with the unusual feature of being contained in a 13 A flat pin mains plug. It will supply 60 mA at 9 V suitable for radio, cassette or record players.

## UNIT ADVANTAGES

One of the disadvantages of conventional battery eliminators is that you are left with a box which must either be strung between plug and unit or replace the batteries in the battery compartment.
This design overcomes both problems. The lead from the mains plug goes directly to the unit and plugs in with a simple jack plug. The batteries of the unit are left in place but simply disconnected when the jack plug is attached. The batteries are reconnected when the plug is removed. The project becomes even easier if the unit has a socket for a battery eleminator.

## CIRCUIT

The circuit diagram of the battery eliminator is given in Fig. 1 together with suitable battery cut-out circuit in cases where a socket is not available on the unit to be supplied.
The transformer has a $6-0-6 \mathrm{~V}$ secondary with the centre tap unconnected. This feeds a four diode bridge rectifier, the output being smoothed by the reservoir capacitor C1 and R2. The Zener diode D5 provides a final 9 V regulated output.

## MODIFYING THE PLUG

The plug used for housing the circuit components is an Ever-Ready type which has to be modified. This is accomplished by cutting a if in step at the bottom rear of the plug as in Fig. 2. A piece of $1 \frac{7}{8}$ in $\times 1 \frac{1}{4}$ in $\times \frac{1}{8}$ in hardboard is cut to form a new base for the plug. This is Araldited into place ensuring that the ends of the plug are upright and parallel.
A $\frac{3}{18}$ in hole is drilled and countersunk in the upper half of the plug directly above the brass screw insert for the neon LP1.

For the d.c. leadout pair a $\frac{1}{6}$ in hole is drilled $\frac{3}{4}$ in up from the base at the centre rear of the plug.

## ASSEMBLING THE COMPONENTS

The components may now be mounted in the expanded plug. First, the transformer is loosely held in position by two 6 B.A. screws.
The mains neon is now positioned and connected to the plug terminals together with the transformer primary windings.
With the capacitor and diodes in place the transformer is tightened down. The output lead is connected across the Zener diode after R2 has been added in series, in the positive line, as shown in the circuit diagram.
With all the components mounted in place care should be taken to see that none are touching the mains pins or their screws. If necessary more room can be made by discarding the screws on the back of the mains pins and soldering instead of clamping. Once all appears to be correct inside a cover has to be constructed for the plug.

## COMPONENTS

## Resistors

R1 $220 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ carbon
R2 $82 \Omega \frac{1}{2}$ watt $10 \%$ carbon
Capacitor
C1 $400 \mu \mathrm{~F} 10 \mathrm{~V}$ elect.

## Diodes

D1-D4 IN4003 (4 off)
D5 9.1V 400 mW Zener

## Transformer

T1 Eagle miniature mains transformer 240 V primary $6-0-6 \mathrm{~V}$ secondary at 100 mA .

## Miscellaneous

13A fused mains plug (Ever Ready Type 7032), LP1 mains neon, $1 \frac{7}{6}$ in $\times 1 \frac{1}{4}$ in $\times \frac{1}{\frac{1}{i n}}$ in hardboard, tin 6 B.A. countersunk screws ( 2 off), 咅in self tapping (2 off), FS1 fuse to suit equipment. PL1 3.5 mm jack plug


Fig. 1. The circuit diagram of the battery eliminator together with a suitable battery circuit cut-out for the equipment to be supplied


Fig. 2. Assembly and wiring details for the battery eliminator



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Good results can be obtained by using good quality card about ${ }^{\frac{1}{6}} \mathrm{i}$ in thick. The card is bent to fit around the top and two sides of the plug snugly. The inside of the card may be scored with a knife to make it bend more easily. With the card bent around the plug mark off, with a pencil, the exact dimensions. When cut to shape check to ensure a good fit, if necessary a former may be made to hold the card in the required shape.

The cover is held onto the plug by two self tapping screws. These screws tighten into 5 in blocks of plywood about to accept the screws and glued in the bottom front of the plug as shown.

Now is the time to fill any gaps between plug and base. A plastic filler is used, which can be sandpapered smooth when dry. The cover and base may be painted to match the plug, sprayed paint gives good results on a suitable primer.

## CONNECTING THE UNIT

Consideration now has to be given to the method of connecting the battery eliminator to the unit which it will power. A number of radio and cassette players on the market have facilities for battery eliminators, and in this case it is only necessary to obtain the correct plug. If your unit does not have facilities such as this, or you are unable to obtain the plug, the following will serve as an alternative.

A 3.5 mm jack plug is connected to the eliminator's outlet lead with the matching socket in the unit. The jack plug is connected to the outlet lead wire with the positive line going to the tip. The socket may now be fitted to the unit, a suitable position must be found to ensure it will not interfere with any internal workings.
With the hole drilled and socket fitted the supply wiring must be adapted to cater for the new facility. The positive lead to the battery compartment must be broken and the jack socket connected in the break. The negative lead goes to the third contact on the socket as well as the battery compartment.
With the jack plugged into the socket the positive line from battery to unit is broken and connected instead to the outlet of the power supply.

The $400 \mu \mathrm{~F}$ electrolytic capacitor may be difficult to obtain, but good results can still be obtained with a smaller one.


ELECTRONICS IN MUSIC

By F. C. Judd<br>Published by Neville Spearman<br>169 pages, 9 in $\times 6$ in. Price $£ 3.15$

M"R JUDD has condensed into this book the fruit of many years' experience in electronics. The six main chapter headings cover virtually every aspect of the subject ranging from the application of electronics in the production of music through a survey of electronic musical instruments, the production of synthetic sound and electronic music, the uses of the tape recorder in the field and, finally, a rundown on the parameters involved in the high fidelity reproduction of music.

The text throughout seems designed to guide the reader into this fascinating and ultra-technical subject without once getting bogged down in an excess of detail. Despite this tendency there is sufficient data presented to enable the home constructor to build and experiment with several interesting circuits. The book is well illustrated with sixteen pages of half tone plates and plenty of clear line diagrams and circuits. The author could have perhaps usefully expanded his treatment of the subjects of synthetic sound and electronic music in view of the current high level of interest although the shortfall in this respect does little to mar the overall presentation of the book which is excellent.
"Electronics in Music" is likely to be welcomed enthusiastically by technical and non-technical readers whose interest in the subject matter may be frustrated by the lack of definitive texts.
G.D.S.

TELEVISION INTERFERENCE MANUAL
By B. Priestley, B.Sc., G3JGO
Published by Radio Society of Great Britain 92 pages, $148 \mathrm{~mm} \times 210 \mathrm{~mm}$. Price 80 p

Television interference from s.w. transmitters is something which many amateur radio enthusiasts find very difficult to eliminate. The Radio Society of Great Britain must therefore be congratulated for attempting to bring this problem to the notice of radio hams and for providing many hints on suppression which, if followed, could greatly reduce the annoyance of TV viewers near to a transmitter.

Television interference can arise from many sources and one of the main problems is tracking down the exact cause. Of course, a well-designed transmitter should include effective circuits for suppressing this unwanted output and transmitter design is included in the book. However, even the best transmitter can have a component failure and the book points out that a careful check on meter readings should be kept and any change in performance noted. R. F. injection into the mains and its suppression is also discussed.

This book has a spiral binding so that the pages lie flat on the bench. The manual may be obtained from RSGB Publications, 35 Doughty Street, London, WCIN 2AE, price 90 p including postage.
S.R.L.


|N this final part, quartz crystal controlled watches and clocks are examined together with various time displays.

## QUARTZ TIMEPIECES

Quartz crystal piezo-electric oscillators are now well known for their great frequency stability. Although the piezo-electric effect was discovered by J . and P . Currie in 1880, it was not used for frequency control until 1921 by Cady. Natural quartz can be used, but synthetic quartz often gives a better performance.

## CLOCKS

Various clocks using quartz crystal oscillators are available. For example, the General Time Company produce "Quartzmatic" clocks using $262,144 \mathrm{~Hz}$ crystal oscillators with an integrated circuit to reduce the frequency to 64 Hz . The Simplex Company produce quartz controlled master time centres for driving a number of clocks in an establishment with an accuracy of two seconds per month.

The Golay Company produce marine chronometers using a 12 kHz oscillator which has a stability of 0.005 second per day at constant temperature or 0.1 second per day over the range 4 to $36^{\circ} \mathrm{C}$ : this clock employs about 29 transistors.

A quartz clock with a digital display is available from Girard-Perregaux; it is mains driven with stand-by battery power and provides an accuracy of 0.02 second per day. The Junghans 750 quartz movement is powered by a 1.5 V battery which lasts a year.

## QUARTZ CONTROLLED WATCHES

Quartz crystal controlled wrist-watches have been available since April 1971. Special CMOS (Complementary Metal Oxide Silicon) integrated circuits have been developed which consume a current only during the pulses and which are small enough to be fitted into a normal wrist-watch. In many cases a number of manufacturers have pooled their resources to produce quartz watch movements. The quartz
crystals used have to be specially aged so that they provide high accuracy at all times. They are normally sealed in a vacuum enclosure.

The first types of quartz wrist-watches to become available to the public employed the "Beta 21" movement developed by the Centre Electronique Horloger S.A. and marketed in various models under many brand names. The quartz crystal oscillator in this movement operates at $8,192 \mathrm{~Hz}$. An integrated circuit divides this frequency by a factor of 32 to produce a 256 Hz signal. The current consumption averages about $16 \mu \mathrm{~A}$ and the accuracy is about one minute per year.

## CYBERNETIC WATCH

The Longines "Ultra-quartz" wrist-watch was first made available on 21st August, 1971. It is especially interesting because it does not contain any integrated circuits, but only a small printed circuit containing miniature electronic components.
The quartz resonator in this watch operates at 9.350 Hz and a mechanical vibrator at 170 Hz . The signals from the quartz oscillator are used to correct

The Girard-Perregaux quartz watch. The quartz crystal can be seen on the left-hand side, the integrated circuit near the top and the power cell on the bottom right-hand side

the mechanical vibrator 170 times per second. This correction is carried out by a relatively simple circuit employing only 14 transistors, 19 resistors and seven capacitors. The logical deductions made by this circuit are fed to the motor as correction signals. This watch is said to be the first cybernetic watch, since it employs a comparison circuit or "brain".
The vibrator motion is transformed into a rotary motion by means of a pawl system like that of Fig. 6. The toothed wheel rotates once per second. The centre second hand appears to rotate continuously without jumping. The accuracy is about one minute per year.

## QUARTZ BALANCE WHEEL WATCH

The " $\mu$-Quartz" or "TS Caliber" watch movement employs an electronically driven balance wheel having four magnets; the exact frequency of this balance wheel (about 4 Hz ) is controlled by a quartz crystal oscillator. The watch has been developed by B. Golay of Switzerland.

The hair spring fixed to the balance wheel has a special shape which results in the frequency of oscillation being somewhat dependent on the amplitude of movement; the frequency is slightly lower at small amplitudes and vice-versa. This effect is known as the isochronism defect.

The quartz oscillates at $32,768 \mathrm{~Hz}$. This frequency is divided down by part of a CMOS integrated circuit containing some 450 components. The strength of the pulse given to the balance wheel depends on the phase of its motion relative to the frequency divided signal from the quartz oscillator.

If the balance wheel is running too fast, the pulses to the coil which drives this wheel will be relatively weak, whereas if the wheel is running too slowly, they will be stronger. Thus the frequency of the balance wheel is stabilised at the, value determined by the signals derived from the quartz oscillator.

If the isochronism defect amounts to 10 seconds per day for each degree of amplitude variation, the balance wheel frequency need only be adjusted to $\pm 100$ seconds per day if an amplitude variation of $\pm 10$ degrees is acceptable.

As in other quartz controlled watches, the regulation is effected by means of a trimmer capacitor which adjusts the exact frequency of the quartz oscillator. In this watch the capacitor is adjustable

The Golay $\mu$-Quartz movement partially dismantled. The magnets can be seen fixed to the balance wheel in the lower part of the photograph, whilst the driving coil is seen above after it has been swung out from the movement. The quartz crystal, which has been removed, is fitted above this coil

in steps which correspond to a change of 0.25 second per day. The accuracy is about one minute per year.

## QUARTZ WATCH WITH STEPPING MOTOR

The Girard-Perregaux " 250 " quartz watch employs a $32,768 \mathrm{~Hz}$ quartz oscillator. The pulses from the latter are divided by an integrated circuit to produce 0.5 Hz pulses. These operate a miniature stepping motor which causes the centre second hand to jump once per second.

## QUARTZ WATCH KITS

The Motorola Company has a section which supplies kits of parts to large watch manufacturers. These kits each comprise a $32,768 \mathrm{~Hz}$ NT cut quartz crystal, a CMOS integrated circuit and a miniature rotary stepping motor. The additional parts required are a power cell, a trimmer capacitor, a conventional watch dial and hands together with gearing to couple the motor to the hands.
The oscillator frequency chosen is a compromise between the size of the oscillator crystal and the current consumption of the integrated circuit. The use of a higher frequency would enable a smaller quartz crystal to be used, but the increased switching frequency results in a greater power consumption by the divider circuit.
The MC 6061 integrated circuit divides the oscillator frequency by a factor of 65,536 so as to produce 0.5 Hz pulses which can drive the motor.

The integrated circuit contains 312 transistors in a six lead ceramic package, but consumes only about $4.5 \mu \mathrm{~A}$ from a 1.3 V cell or $5 \mu \mathrm{~A}$ from a 1.5 V cell. Motorola use ion implantation techniques to dope the semiconductor material used in their integrated circuits.
The 6 mm diameter motor takes a mean current of about $7.2 \mu \mathrm{~A}$ at 1.3 V or $8.3 \mu \mathrm{~A}$ at 1.5 V . The 0.5 Hz pulses from the integrated circuit have an amplitude of about IV and a duration of about $31 \cdot 25 \mathrm{~ms}$, successive pulses being of opposite polarity and separated by one second.

The motor rotates by 180 degrees at intervals of one second, all movements being in the same direction. It has a resistance of about 5 kilohms and contains about 50 metres of wire of a diameter about one-tenth of that of a human hair.

The three parts of the Motorola kit depicted inside an empty watch case. The quartz crystal is shown at the top, the integrated circuit on the left and the stepping motor on the lower right-hand side



Fig. 8. The operation of the Bulova Accuquartz is depicted here

## QUARTZ TUNING FORK WATCHES

The new Bulova "Accuquartz" watch is especially interesting because it contains a quartz oscillator which controls a tuning fork movement. This watch was introduced in the U.S.A. in December 1971 and became available in Europe towards the end of 1972 at prices from $£ 115$. It is much thinner than many other .. quartz models (including an earlier "Accuquartz" model which used the "Beta 21 " movenent). The new "Accuquartz" range for men and women display the day of the week and the date in addition to the time.

The "Accuquartz" crystal oscillates at $32,768 \mathrm{~Hz}$. This frequency is divided by an "Intersil" CMOS integrated circuit containing 126 transistors, etc. The tuning fork oscillates at $341 \frac{1}{3} \mathrm{~Hz}$, this being one-third of the frequency $1,024 \mathrm{~Hz}$. See Fig. 8.

The Bulova Accuquartz is shown in the foreground together with a much thicker Accuquartz model using the CHE movement


In this watch the tuning fork mechanism advances the gearing $341 \frac{1}{3}$ times per second by the same type of mechanism as used in the Bulova "Accutron" range. Thus the centre second hand appears to move continuously instead of jumping once per second as in some types of watch.

The "Accuquartz" has an accuracy of about 1 to 2 seconds per week.

## THE ASTROQUARTZ

The Junghans "Astroquartz" watch is said to be the smallest quartz watch being manufactured. It employs a $32,768 \mathrm{~Hz}$ quartz oscillator, but the quartz crystal used is unusual in that it is in the shape of a tuning fork, the prongs of which vibrate like an ordinary tuning fork but at a much higher frequency.
As illustrated in Fig. 9, an integrated circuit acts as oscillator and frequency divider. The 15 cascaded binary stages divide the pulse rate by $2^{15}$ to produce one output pulse per second. The size of the integrated circuit is only $1.6 \times 2.1 \mathrm{~mm}$.


Fig. 9. The above illustration depicts the operation of the Junghans "Astroquartz" watch

The output pulses from this circuit drive an electro-magnetic transducer. The pulses are applied to the coil which turns in a strong magnetic field. The escapement fitted to the axis of this coil engages and turns a wheel with 60 teeth to which a centre second hand is fitted.

## THE MEGAQUARTZ

The "Megaquartz" watch is probably the most accurate wrist-watch yet designed, although it is being produced only in small quantities. It has been designed by the Batelle Institute in collaboration with the Omega Watch Company. The accuracy is about 1 second per month.

The main feature of this watch is the use of a circular AT cut quartz crystal oscillating in a shearing mode at $2,359,296 \mathrm{~Hz}$-far higher than in any other design. An integrated circuit frequency divider is used.

Omega also offer a quartz watch which has an 8.192 Hz oscillator. This frequency is divided by a factor of 32 to produce 256 Hz pulses which drive an. electro-magnetic motor. The accuracy is about 1 minute per year.


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Neat, custom-made appearance slide fader control for balance of front and rear speaker volume. Simulated wood finish panel which can be quickly fitced below car dash Supplied with generous connecting cable and fitting screws. Will suit $4,8,16 \mathrm{ohm}$ installations. $100 \times 38 \times 30 \mathrm{~mm}$ (including knob but excluding

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G5555 PROFESSIONAL STEREO
HEADPHONE
Lightweight materials are skilfully used in the construction of this model in black crackle moulding and kid-soft leathercloth with contrasting bright metal. Each ear pad houses a highly efficient 60 mm reproducer unit and features ear muffs removable for cleaning. 10 -self-coiled lead plug fitted.
Frequency Response: $20 \quad 20,000 \mathrm{~Hz}$. Impedance 4 . 16 ohms. Sensitivity: 110 dB . Power: 0.5 W Weight: 0.39 kg .
f9. 25

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are used for both units. 120 mW output. 9 V are used for both units. 120 mW output. 9 V
internal battery operation. Master unit: $77 x$ $40 \times 105 \mathrm{~mm}$ internal batery operation. Master unit: $77 \times$ $40 \times 105 \mathrm{~mm}$. Slave unit: $70 \times 32 \times 90 \mathrm{~mm}$
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tance: 0 . 150 K ohms.



- exclusive Wireless World design in the April \& May issues

See full construction details of the versatile multiple measurement meter which was first described in our March issue. Intended for both amateur and professional use, the design - based on integrated circuits - is arranged so that you can build either the whole instrument or just the particular measurement facilities you require. Measurements are shown in a "window" on a four digit numerical display. Survey of the Compatibility of Audio Magnetic Tapes.

With the wide variety of tapes available, it is desirable to establish the compatibility of one type or brand against any other for a particular recording machine. Detailed tests have been made and the results interpreted to produce a table of interchangeable and compatible products.


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APRIL ISSUE On sale now 20p


(Right): the Avia watch which employs a liquid crystal display. This is expected to be available in the U.K. at about $£ 135$ soon
(Left): the Swissonic 2000
watch. This displays the date,
the hours, minutes and seconds
continuously by means of a
liquid crystal system
(Left): the Swissonic 2000 This displays the date, continuously by means of a liquid crystal system


## DIGITAL WATCHES

Digital watches which employ no moving parts have just begun to appear on the market. They employ quartz oscillators and provide an accuracy of about one minute per year.

Two forms of display have been employed, namely electroluminescent diodes which provide a red display and liquid crystal displays.

## ELECTROLUMINESCENT WATCHES

Watches employing gallium arsenide-phosphide electroluminescent diodes provide a display which shows the time in red digits. Unfortanately the display diodes require so much current that it is not possible for the time to be continuously displayed if the power cells are to have a reasonable life. A button on the watch must therefore be pressed each time the user wishes to read the time. The cell life is dependent on the number of times the time is displayed. The display may have to be shaded with the hand if the ambient light level is high.

The "Pulsar" watch manufactured by the Hamilton Company employs light emitting diodes. The brightness of the display is automatically adjusted to suit ambient lighting levels, although it requires shading from direct sunlight when the display is being read.

Each time the button is pressed, the hours and minutes are displayed for 1.25 seconds, but if the button is held down, the seconds are displayed for as long as it is depressed.

The watch employs a $32,768 \mathrm{~Hz}$ oscillator and a CMOS integrated circuit containing over 1,200 transistors. It is powered by two silver oxide cells which have a life of over one year under normal use (about 25 time readouts per day).

A slight variation of this watch is offered by the Omega Company as their "Time Computer".

## LIQUID CRYSTAL DISPLAYS

The other form of digital display used in watches employs liquid crystals. This type of display requires very little power, since it does not emit light. The liquid crystals simply reflect a different proportion of the incident light in regions where an electric field is applied to them. Thus the display cannot be
viewed in the dark. A moderately high ambient light intensity is desirable.

The thickness of the liquid crystal material may be about 0.5 mm . The special nematic material is placed between two electrodes like a capacitor, but the electrode nearest the face of the watch must be transparent.

In the absence of any field, the liquid is perfectly clear and transparent, any incident light falling on it being absorbed by a black background. When an electric field is applied by suitably shaped electrodes in certain regions (which are in the shape of the digit to be displayed), the liquid becomes opalescent as the crystals come into mutual alignment. They reffect the incident light back from these regions to the observer.

Although watches using liquid crystal displays have the advantage over those using luminescent diode displays in that the digits can be made visible at all times, the life of the present liquid crystal systems seems somewhat doubtful. Even when an alternating voltage is applied, some degradation of the material may occur so that the display gradually becomes less clear. The life should be considerably over one year, but it is too early to estimate it accurately. At least one manufacturer feels that liquid crystals may have an indefinite life if contamination is avoided. The price of replacement units should fall rapidly during the next few years.

## THE AVIA WATCH

One watch with a liquid crystal display is marketed by Avia-S.G.T., the liquid crystal system for this watch being produced by the Optel Corporation of the U.S.A. The hours and minutes are continuously displayed, but the seconds are shown by means of two flashing points appearing between the hours and the minutes digits.
The quartz oscillator operates at $32,768 \mathrm{~Hz}$. This frequency is divided by a factor of 512 and the 64 Hz output operates counters. The latter control the decoders which feed the display.
The 1.5 V power cell has a life of 14 months. A circuit is employed to convert the 1.5 V from the cell to the 15 V required for the decoder-display operation.


The Staiger 2000 quartz crystal controlled clocks. The ITT crystals used are shown at the front

## A DETAILED DISPLAY

Another liquid crystal watch has been developed by Texas Instruments, Ebauches S.A. and Longines. The eight character display provides a continuous readout of the day of the month, hours, minutes and seconds. The accuracy is about 1 minute per year. The watch contains two integrated circuits containing about 700 transistors and is powered by two 1.35 V mercury cells.

The hour display can be set by an internal switch to provide either a 12 hour or a 24 hour cycle. The indicated time is set by four micro-switches on the back of the watch which alter the seconds, minutes, hours and date respectively.

Another watch with a liquid crystal display has been produced by the Seiko Company; it displays hours, minutes and seconds.

A Geneva lever movement (about 100 years old) from the Science Museum being compared with an ITT quartz crystal designed for use in a watch


## CLOCKS USING LIQUID CRYSTALS

A limited number of clocks with liquid crystal digital displays are available, for example, from the Seiko Company. An impressive digital alarm clock (type S1736) has been constructed on a single chip by American Microsystems; it is interfaced with their liquid crystal readout.

## ATOMIC CLOCK

In a totally different sphere it may be mentioned that the standard of time is now based on the frequency of radiation emitted between two hyperfine levels of the caesium-133 atom. The second amounts to $9,192,631,770$ cycles of this radiation. This definition provides a more accurate measure of this unit than the motion of the earth.

Ebauches S.A. have made precision time centres using caesium atomic clocks which have an error of less than one microsecond per day (corresponding to one second in about three thousand years!).

## POWER CELLS

The cells used to drive electronic watches pose many manufacturing problems. Three of the main manufacturers are Union Carbide, Leclanche and, in England, Mallory.

A new area has recently been opened by Mallory at Crawley for the manufacture of special mercury button cells used in watches. Such cells must give satisfactory service for at least one year after a variable period of storage before sale.

Extreme care must be taken to prevent contamination of the materials used in cell manufacture. All air is filtered before it enters the watch cell manufacturing area at Crawley to prevent dust from being sealed in the power cells. Great care must be taken to prevent the possibility of internal leakage of current.

The electrolyte used in watch cells is chosen for the lowest practical seepage rate, since if it escaped from a cell it would probably damage the delicate watch mechanism.

In conclusion it may be mentioned that the tweezers used to fit new cells into watches should be made of a plastic material, since metal tweezers can easily short the cell. Care should be taken to fit new cells in the correct way so that they provide the circuits with a voltage of the correct polarity.

## CONCLUSION

We are in the midst of a revolution in watch design. Although no manufacturer has really broken through the price barrier with a moderately priced quartz controlled watch, it may not be too long before one company does so and the "quartz war" will have begun. The developments in the last few years have been very rapid and it is expected that many of the estimated 300 million watches per annum required by 1980 will be electronic ones.

The traditional place of watch making, Switzerland, has played a large part in the development of electronic watches, but the U.S.A. has initiated much of the work.

The normal skills of the watchmaker will be required to attend to watches employing moving parts, but if digital watches become common, the watch repairer may have to have a very elementary knowledge of electronic engineering with microminiature equipment.

## SPACE BUDGET

The United States space agency will have more money to spend this year, 74 million dollars in fact. A total of 3,136 million dollars is set aside for space matters. This amount will cover a number of NASA projects, for example two new projects as well as the programme for space stations and shuttles.

The two new projects are a new kind of satellite for geodesy known as a Terrestrial Reference Satellite, and an advanced version of the Nimbus weather satellite to monitor pollution.

The reference satellite, due for launch in 1976, will use laser beams for the measurement of distances between locations on different continents. The accuracy that can be achieved is of the order of a few inches so that small changes of movement of land masses will be detected.
The new Nimbus satellites will monitor both air and ocean pollution. The programme is for the launch of two satellites, one in 1974 and the other in 1976.

The current major projects will continue to be developed, but there will be a phasing out of communications satellite interests. This is because the space agency consider that the viability of these programmes has been proved and the time is now ripe for commercial responsibility for this activity.

The Science Foundation will increase their programme of investigations and some major projects involve visual and radio astronomy. Some 10 million dollars will go to the rail mounted mobile arrays of aerials in New Mexico for the large scale study of distant sources and the detection of signals from any civilisation that may exist in other parts of the Universe.

The visual telescope under construction at the Cerro Tololo interAmerican Observatory in Chile, will be given 2.6 million dollars for the completion of the work on what will be the largest optical telescope in the southern hemisphere. The diameter of the mirror is 158 inches and the site offers spectacular advantages over other places for useful viewing time.

## LUNOKHOD 2

The Russian moon vehicle, Lunokhod 2, which landed on the Moon in January has a special set of programmes. It was landed some 175 km from the landing site of Apollo 17. The data obtained from the two sources should be complementary.

Landed in the Sea of Serenity, the Lunokhod 2 task is to examine the boundary area where older


BYFRANK W. HYDE
rocks may be found. At the boundary area of the highland regions, from which anorthites rise up, the floor of the mare is covered with basalt type lava.
Other experiments will measure and observe the Zodiacal light near the Sun, observe the Milky Way and the centre of the Galaxy with a space photometer. It is hoped also to decide whether there are traces of cosmic dust in the Lunar atmosphere. The possibilities of studying the Universe by optical means from stations on the moon is another experiment which the Soviet team are known to be considering.

The vehicle is also carrying a French laser reflector for measuring the Earth-Moon distance.

The Lunokhod, which is of a similar design to the previous vehicle, carries on its outside an orientation device, a lunar surface photometer, soil analysis experiment, a fixed television camera, a steerable television camera, the space photometer, a solar battery, a magnetometer, a photo receiver and aerials which include a corner reflector and a high gain system.

## MOON GRAVITY

Analysis of the gravitational variations of the moon recorded by the command module of Apollo 15 has yielded data about mascons, and the lunar orbiter added to this data when being precisely tracked.
This problem, to which selenologists have devoted considerable time and study, can now be set up as a model. The model now suggested agrees well with the idea that the mascon of Mare Serenetatis is a thin body with well defined boundaries. The previous speculations on
this theme have been borne out for Mare Nectaris also.

So far as Serenetatis is concerned the model fits the surface features extremely well. At the moment the data gives support to the volcanic hypothesis.

## ORBITING WORKSHOP

As the launch date for the Skylab, the first orbiting space station, draws near it may be useful to describe the project and the sequence of events which will be the step in space that many have waited for almost impatiently.

The first crew will be an all Navy one and Charles Conrad, veteran of Apollo 12, is the only member of the team who has had astronaut experience. The other two men are J. P. Kerwen, a doctor, and P. J. Weitz, an aeronautical engineer.

Skylab will go into a 270 -mile orbit. The sequence is to be the launch of the skylab unit unmanned into the prescribed orbit, the next day. May Day. the launch of the command module with the crew to the calculated rendezvous. When linked up the total length of the units will be 118 ft . The diameter will be 22 ft at the workshop section.

The arrangement of the airlock and docking sections allow normal joining of the command vehicle to the end of the whole unit. There is also a second docking point on the side of the docking module which could be used for a second command module to attach itself or for rescue purposes.

When the space station is launched the telescope covers the docking section. On attaining its correct location in orbit the telescope will swing to the side and the solar power paddles will open. The ports for docking will then be uncovered.

## LIFE SUPPORT SYSTEMS

The station main body is 48 ft by 22 ft and there is an intermediate section next in the sequence which is 17 ft long and is an airlock section. Here all the power control and distribution systems are located.

The air conditioning system, the life support system together with communications control and data management are also arranged there. There is room for two fully suited astronauts with personal life support systems in the section. From here the crew can pass to the docking module to work outside the vehicle or to pass to and from the command module.

The whole assembly with the launcher, a Saturn 5 rocket, will stand 334 feet high at take off. The combined weight at the time will be 3,110 tons.


LAST month the circuit of the Tape Link was described in detail. In this the final part, the construction of the Tape Link, the fitting of the heads and the setting up procedure will be described.

## TWO ASSEMBLIES

The Tape Link is made up of two assemblies (the amplifier and the power supply) in order to keep the mains ransformer away from hum sensitive circuits and enabling the power supply to be positioned where it induces the minimum hum in the replay head.

The folding of the metal should present no problems to a handyman equipped with a vice. Cutting the metal to size is not quite so easy and is best done with a guillotine and a fly press for the cut out parts. Constructors may find it convenient to purchase the metal cut to size from a sheet metal shop.

## POWER SUPPLY CONSTRUCTION

Dealing first with the power supply, drill the chassis and bend up as indicated in the photograph.

Next, affix the mains transformer using 4BA $\times$ $\frac{1}{2}$ in screws and nuts. Do not tighten as they will have to be undone again when the power unit is finally mounted in the case. A tag strip carrying the rectifier diodes should now be assembled and bolted to the chassis.

Wiring between this and the mains transformer is best done at this stage as the tag strip will be difficult to get at once the smoothing capacitors are in place. These and the fuseholder can now be put into position and the wiring completed.

The power lead-out wires and the mains lead are secured by a plastic cable clip bolted down to the
mains transformer. Having completed the power supply it can now be tested.

With mains applied and no load imposed upon the outputs, the supplies should read 56 volts and 28 volts respectively. Provided that the voltages measured are within a couple of volts either way and that the mains transformer and capacitors do not get hot after a few minutes' operation, all should be well.

## AMPLIFIER CHASSIS

Mark out the front panel to suit components (see Fig. 7). Drill all the holes starting first with an $\frac{1}{8}$ in drill. Next, open out the holes for the record indicator lamp, the switches and potentiometers with the appropriate drill.

The DIN sockets are mounted beneath the panel and the $\frac{5}{8}$ in hole required to allow entry of the plugs is most neatly cut with a chassis punch, e.g. a "Qmax cutter". The cut outs for the meters are made by drilling all round just inside the edge with a small drill, pushing out the centre and then truing up to the marked line with a file.

A similar technique should be used for the meter switch cut-out. Drill two holes side by side and open up to the required size with a needle file. Finally countersink all the screw holes.

The strap for mounting the meters, and the Uchannel complete the metal work. To make the folding easier, the front panel fixing flanges should be bent over first. The sheet can then be bent up to complete the chassis. Once again, the use of a chassis punch is recommended for the larger holes (see Fig. 4).

The front panel can be finished in any way desired. One method which gives a pleasing appearance is to
satin finish it by stroking lengthwise with a wire brush such as is supplied for cleaning suede shoes. This results in a series of parallel scratches. The panel is then cleaned with a rag soaked in methylated spirit to remove loose material and grease.

Letraset may be used to label the panel, finally protecting the finish with two coats of lacquer.

After fixing the front panel to the chassis the B9A valve holders and the stand-off spacers are mounted and the components assembled to the front panel. The slider switch used by the author for the bias/Vu selector was supplied with its mounting holes tapped at 8 BA .

These were drilled out and retapped at 6BA. However if 8BA screws are used, allowance must be made for this in the front panel drilling.

## COIL WINDING

Because many readers find it difficult to obtain specified coils, the author wishes to point out that virtually any 14 mm coil is suitable for L1 and L101. Most catalogues specify the number of turns per millihenry and because inductance is proportional to the square of the number of turns, twice this number will give the number of turns required for 4 mH . Some easily available pot cores and their turns per millihenry are given in Table 1.

Using 34 s.w.g. enamelled copper wire, wind the required number of turns onto the bobbin. On completion the winding should be secured with a layer of adhesive tape (not Sellotape).

Before assembling the two halves of the pot core, slightly rub the mating surfaces with a sheet of paper to remove any dust which could alter the inductance of the completed coil. The lead wires should be brought out separately through adjacent slots at 90 degrees.

Photograph showing construction of the power supply for the Tape Link. The switch and indicator neon are mounted near the mains input Positioning of the power supply module within the finished tape deck is best found b.y trial and error being that which gives minimum hum

 details of the metalwork

Table 1: ALTERNATIVE POT CORES FOR L1 AND L101

| Type | Turns $/ \mathrm{mH}$ | Turns required for 4 mH |
| :--- | :---: | :---: |
| LA 2503 | 52 | 104 |
| T26/2100R | 47.5 | 95 |
| FX 1636 | 34.8 | 70 |
| FX 1011 | 24.3 | 49 |
| FX 2236 | 32 | 64 |

Table 2: ALTERNATIVE POT CORES FOR BIAS AND ERASE OSCILLATOR T2

|  |  | Turns required <br> Type |  |
| :--- | :---: | :---: | :---: |
| Turns/mH | Primary | Secondary |  |
| LA 2301 | 53.8 | $5+5$ | 80 |
| LA 2105 | 54.7 | $6+6$ | 96 |
| LA 2517 | 42 | $5+5$ | 80 |
| N22/250A | 40 | $5+5$ | 80 |

Fig. 5. Method of winding the primary of the bias and erase oscillator coil


## BIAS AND ERASE OSCILLATOR TRANSFORMER

Again the pot core used for this transformer is by no means critical. A 25 mm type was used in the prototype but any high frequency 18 mm type will do just as well provided the inductance is that specified (see Table 2 above).

Measure off two 20 in lengths of 21 s.w.g. wire and twist them lightly together. Allowing a few inches for leadout wires, begin winding the required number of primary turns making sure that the first turn of one half of the primary lies adjacent to the first of the other half and so on (see Fig. 5). After the required turns have been wound the windings should be secured with adhesive tape.

The secondary should then be wound using 30 s.w.g. wire starting in the same place and winding in the same direction. Cover this layer with one layer of tape. Then assemble the pot core with the same precautions as for the previous coil.




Fig. 6. Layout of the components on the perforated board. Note that there are some components under the board. C27 should be mounted away from board to avoid heat

The primary windings must now be identified with some form of continuity tester such as a bulb and battery. After scraping the enamel from the four primary wires select one wire and call this the start.

Next find the other end of this wire with the continuity tester. If the method of winding shown is followed then the starts of both primary halves will be at the top of the coil and the other ends at the bottom. The end of the identified wire should then be soldered to the start of the remaining wire, this becoming the centre tap. The remaining wire then becomes the other end of the total primary.

## CIRCUIT BOARD

The amplifier is constructed on perforated board which accommodates all the components with the exception of the relay for which a cut-out must be made (Fig. 6). The holes will also have to be opened out for some of the pots and for the fixing screws.

The wiring should proceed logically from one end of the board to the other inserting Veropins where the flying leads are to be soldered to the board. The oscillator tuning capacitor is mounted up in the air on Veropins to keep it away from the hot components near it.

TRII and TR12 are fitted with clip-on heat sinks (TO5 can). There are four components mounted underneath the board which must not be forgotten.

## CONSTRUCTION

Upon completion thoroughly check, the board wiring. The connections from the underside of the board to the B9A sockets are then wired, allowing sufficient slack to enable the board to be tilted up through 90 degrees to facilitate servicing should it be required.
The board is next screwed into position and the wiring completed. To facilitate identification. the use of an assortment of colours for the connecting wires is suggested, and screened leads of low capacity must be used where indicated (see Fig. 7).

For ease of assembly it is suggested that the switch wafers nearest to the metalwork are wired first. Note the screen between the wafers and the spacers required to give good isolation between the two sections. In the prototype three-pole three-way wafers were used for S1 but the easier to obtain four-pole three-way wafers are perfectly suitable.
Prevention of earth loops is essential with this equipment and the constructor should note that there is only one connection between the chassis and amplifier earth.
At this stage the wiring on the front panel and the chassis should be completed as in Fig. 7.

## TESTING

After having thoroughly checked the wiring (mistakes can be expensive) the power supply is plugged into the appropriate socket on the amplifier and mains applied. Providing that there is now no obvious indication of a fault, e.g. smoke, it can be assumed that there are no serious errors.

Measure the supply voltages with a multimeter. These should be 55 volts and 27 to 28 volts approximately. It is then prudent to go around the circuit

Table 3: APPROXIMATE VOLTAGE SETTINGS

| Junction of R1 and R2 TR1 emitter collector | 17.3 18.0 0.7 |
| :---: | :---: |
| Junction of R1 and R21 | 54.0 |
| TR2 collector | 25.3 |
| base | 0.7 |
| Junction of R11 and R13 | 27.0 |
| TR4 base | 28.7 |
| emitter | 28.0 |
| TR3 base | 25.3 |
| emitter | 26.0 |
| TR5 base | 7.7 |
| emitter | 7.0 |
| collector | 18.3 |
| TR6 base | 18.3 |
| emitter | 19.0 |
| collector | 7.0 |
| TR7 emitter | 6.0 |
| collector | 26.0 |
| VR4 wiper (dependent on setting) | 6.0 |
| Junction of R25 and VR4 | 8.0 |
| Junction of R26 and VR4 | 4.0 |
| TR8 base | 28.0 |
| emitter | 28.7 |
| collector | 20.0 |
| TR10 base | 19.4 |
| collector (dependent on VR4) | 12.0 |
| Terminal 6 IC1 (dependent on VR5) | 12.0 |

checking voltages in accordance with Table 3. These are the design figures obtained by calculation and, generally speaking, provided that correlation within plus or minus 20 per cent is obtained all should be well.

When these checks have been made rotate VR4 and VR104 fully clockwise. The meters should now show a reading.

Disconnect the mains and temporarily short pins 5 and 6 of SK 3 together. Set the meter switch to bias and the function switch to stereo. Then reconnect the mains. The record indicator light should come on and the meter show an indication which is adjustable by means of the bias control. Failure of the meter to read suggests an oscillator fault and the power should be switched off immediately to prevent damage. Remove the temporary link.

## TAPE TRANSPORT

With the old heads and/or electronics stripped out, the new heads have to be fitted to the base plates. Two methods of accomplishing this for the record/ replay head are depicted in Fig. 8. It is essential that the tracks interleave correctly and the baseplate may need to be packed up or filed down accordingly.
When correctly positioned, the upper edge of the top track lies just below the edge of the tape (about 0.15 mm ). With regard to the Collaro deck the slot in the baseplate had to be widened with a file and the


Fig. 7. Interwiring diagram showing the connections between the board and the other components. The numbers indicate the terminal pins on Fig. 6


Fig. 8. Methods of fitting the new heads of the tape deck
baseplate packed up to raise the head. The dimensions of the strap are given and it was screwed to the baseplate with self-tapping screws.

The erase head has a single hole through it to clear 10BA, and this is the best means of securing it. The azimuth of the erase head gap is not critical and therefore a rocking plate is not required. On the author's deck this hole was tapped at 8BA and the head then secured directly to the head mounting plate stood-off by an 8BA nut drilled out to clear the thread. The top of the erase head upper track should extend to the edge of the tape.

## PRESSURE PADS

A modification made by the author to his deck concerning the pressure pads may be of interest. The original pads were of hard felt requiring quite a high pressure to ensure contact between the tape and the head. These felt blocks were removed and replaced by a pad of composite construction, i.e. a layer of $\frac{1}{h}$ in thick foam plastic covered finally with a $\frac{1}{16}$ in layer of supple felt.

This gives improved contact at far less pressure thus reducing the wear on the heads and improving the flutter performance of the transport. At the same time a mu-metal screen cut from an old screening can was fixed to the rear of the RECORD/REPLAY head pressure pad to reduce the hum pick-up on playback.

## RECORD/REPLAY SWITCH

Most tape recorders have their record/replay switch contacts interlocked with the function buttons. In order to change the function of the amplifier to RECORD, one set of "make" contacts are required. If these are not present on the recorder a switch must be provided and this should have contacts designed for switching capacitive loads.

The heads are wired up to the plug using low capacity screened lead. The deck chassis is earthed
to the screens of one of the record/play leads. Care should be taken to ensure that the metalwork of the amplifier does not touch the tape deck. If this is unavoidable the earth link mentioned above must be omitted.

The power supply should not be fixed down yet as its positioning is critical for minimum hum injection. To determine this position the deck should be set in motion as it would be when playing a tape. The power pack is then moved around the cabinet whilst listening to the replay hum level until it is subjectively at its lowest.

The recorder is now complete and ready for setting up.

## SETTING UP PROCEDURE

The equipment required to set up the completed recorder is a d.c. voltmeter, an audio sine wave generator and an oscilloscope, or failing this an a.c.


Pholograph showing the heads in position on the prototype
millivoltmeter. The setting up should follow the order outlined below as in some cases one stage depends on the setting of the previous.

## AZIMUTH SETTING

Before the electronics are adjusted the heads must be correctly aligned with the tape. Adjustment of the record/replay head gap in relation to the tape is known as azimuth alignment and is essential in order to facilitate the interchangeability of recordings between machines. This is correctly done with the aid of a professional test tape but any commercially prerecorded tape or a tape recorded on a machine with a known correct azimuth can be used. (Choose a tape with a good high frequency content.)

Whilst the tape is playing the head should be rocked up and down until the maximum high frequency output (measured simply by listening to the output) is obtained, then fixed in this position.


Fig. 9. Graph to show the dependence of frequency response and distortion on the bias level


Photographs showing the two wafer switches

Photograph of the completed Tape Link. The meters are held on to the front panel by a strap which is shown

## REPLAY AMPLIFIER AND METERING ADJUSTMENTS

Using the voltmeter adjust VR5 and VR105 until the voltage at the emitters of TR9 and TR109 is 12 volts. Next rotate VR4 and VR104 fully clockwise (maximum resistance) then turn back so that the respective meters just read zero.

## OSCILLATOR ADJUSTMENT

In the absence of suitable test equipment, a satisfaciory result may be obtained by setting the adjuster to its mid position. The exact frequency of operation is not critical and in fact the tolerances of the frequency determining components are wider that the adjustment range.

If an oscilloscope or frequency meter is available then set the oscillator selector switch to Stereo, the bias control to mid range and the machine to the RECORD mode, then adjust the oscillator coil T2 until the frequency is as near to 100 kHz as possible.

## DETERMINATION OF BIAS SETTING

The correct bias setting is important as it affects many of the parameters of the recorder. The bias setting required depends on the tape speed, the tape in use and the mode of the recorder (MONO or stereo). The settings should be determined as below and tabulated for reference:

## $7 \frac{1}{2}$ i.p.s.

Record a 1 kHz sine wave at a level 6 dB below the maximum modulation, adjusting the bias from -3 dB to +3 dB in $\frac{1}{2} \mathrm{~dB}$ steps. Replay the tape and note the amplitude of the output for each of the bias settings.

A series of results should be obtained which rise to a peak then fall off. The correct setting is that which gives a sensitivity $\frac{1}{2} \mathrm{~dB}$ (approximately 5 per cent) down from the maximum, i.e. slightly more bias than is required for maximum sensitivity (see Fig. 9).
continued on page 341



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The system consists of small "bleeper" pocket receivers; five f.m. transmitters, situated at Reading, Stokenchurch, Bagshot, Slough and Maidenhead; and computer-controlled terminal equipment at the Reading Trunk Exchange.

## RECEIVERS

The receivers, small enough to be clipped into a pocket, give a high-pitched 10 second "bleep-bleep" signal when activated by a phone call. Powered by a 1.5 V alkaline battery, each receiver will operate for approximately 900 hours, representing three months of average use.

The f.m. receivers are basically a double superhet built around six CMOS integrated circuit modules. Sensitivity is better than $10 \mu \mathrm{~V} / \mathrm{m}$ and reception is in the 150 MHz band. Following detection, the paging tones are decoded by two plug-in active filter modules; 60 frequencies are employed in the range 288.5 to $1,433 \cdot 5 \mathrm{~Hz}$ and a two-tone sequence is used to provide a system usable by 3,540 customers. Later the system will cater for 100,000 customers.
Detection of the first coded tone switches the receivers on, reception of the second tone is decoded and once accepted will sound a 2 kHz bleep note.
The only control on the receiver is a three position switch: "on', "off" and 'memory". In the memory position, used when the person does not want to be disturbed, the incoming signal is stored in a CMOS bistable memory device and when the receiver is switched back to the on position the bleeper will emit its signal.

Each receiver has its own 10-digit number (the first four digits are an STD code common to all receivers) and dialling this number instructs the transmitting equipment to send a signal to activate the bleeper. Communication is one-way only, so the user must prearrange the action to be taken on receipt of a radio-paging call.

## COMPUTER CONTROL

Tie heart of the system is a Digital Equipment, type PDP11, mini-computer with a basic storage capacity of 192,000 bits. Installed at the Reading Trunk Exchange, the computer receives the "telephone calls", converts them (by an interfacer between the telephone network and computer) into a binary-coded format.
The calls are queued and released in batches at 15 second intervals. When the number dialled is recognised and accepted an announcement to replace the telephone handset is given. Once accepted the call is converted to the pager code by the computer, and passed to a frequency synthesiser and then to the relevant transmitters.

The transmitters are switched by command signals from the control complex slightly ahead of the transmission of the pager-code modulation.

Although the system is only a feasibility study, plans have already been made to extend the service to other regions, such as London, Manchester and Birmingham.

More advanced pagers are already being developed and the present receivers are claimed to work inside buildings, cars and on trains. Engineers have, it is claimed, achieved more than a 95 per cent reception in the defined boundary limits.

The radio-paging receivers will cost $£ 5$ a month to rent. with an initial fee of $£ 5$. Call to a receiver will be free during the introductory service.

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | － |  |  |  |  |  |  |  |
| $2 \cdot 2$ | 二 | 二 | 二 | 二 | 7p | 7 p | 7 p | 7p |
| 4.7 | － | － | － | $7 p$ | ${ }^{7}$ | 7p | 7 p | 7 p |
| 10 | － | － | 7p | － | 7p | 7p | 7 p | 7 p |
| 22 | 7 | － | 7p | 7 p | － | $7 p$ | 7 p | 8 p |
| 47 | 7p | 7 | $7 \mathrm{7p}$ | 7p | 7 p | 7p | 8 p | 12p |
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| 220 | 7 p | $7 p$ | $7 p$ | 8 p | 9 p | 10p | 17p | 26p |
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| 1，000 | 9p | 12p | 12p | 17p | 20p | 23p | 40p | ¢ |
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| 4，700 | 23p | 26p | 37p | 40p | － | － | － | － |
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#  

# by K. Lenton-Smith 

POPULAR MUSIC is a lucrative and highly competitive field these days and the net is cast to take in an even younger age group each year. Ten-year-olds now have their own idols! To be successful in the "pop" field involves a constant search for new sounds by electronic processes, especially as there is a practical limit to what can be done with the vocal if the lyrics are to remain intelligible. (Some readers may query the use of the word "intelligible" in this context!)
The Survey of Electronic Musical Instruments, published as a supplement to the November 1972 edition (issues unobtainable), showed how manufacturers are catering for this search for new tonal ideas. Though initially featured by recording artists, new effects are copied by local groups as they struggle to keep abreast of the times. Amateur musicians, who prefer "pop" music though never play publicly, like to re-create at home some of the sounds they hear on radio, tape and discs. The younger generation has always, as a tradition, looked for change and new experience, the popular music field being no exception. Over the years, the specification of available electronic musical instruments has taken this into account increasingly.

## LIGHT MUSIC TODAY

A certain line in 'Fings ain't wot they used to be', referring to the light music scene at that time, mentioned musicians "backing themselves with three chords only". When that song was written, there was an element of truth in Lionel Bart's cynicism: a number of performers only seemed able to strum the tonic, sub-dominant and dominant seventh chords on their highly-amplified guitars. This deficiency was often covered up by a show of vocal and physical gymnastics!

The advent of the Beatles brought more tuneful melodies and the use of less closely related chords. Though the Beatles, as a group, no longer exist they underlined the fact that, if a song is to survive, the melody must be original and tuneful. Many modern "pop" numbers will be forgotten a few months hence, but the Lennon and McCartney compositions have already taken their place with those of the established Old Masters such as George Gershwin, Cole Porter, Jerome Kern and Richard Rodgers.

Burt Bacharach is today's prime example of a composer who writes enjoyable music which will be remembered many years hence: Antonio Carlos Jobim is in the same category, specialising in the LatinAmerican field. The reader who plays their music, or attempts the transcriptions of Dave Brubeck or Dudley Moore, will appreciate that the days of "three chords only" have long passed and things certainly ain't what they used to be! These composers frequently use complex chord sequences which demand a high degree of musical ability to perform them.

Whereas our sphere of electronics -especially integrated circuitryhas enjoyed a spin-off from space research, classically trained musicians who have turned to lighter music have also benefited that field. The music for a number of West End shows running currently has come from composers with classical backgrounds, whilst we have previously commented on Walter Carlos, Robert Moog and the music for "Clockwork Orange'.

## RETROGRADE

Today's standard of compositions and the requisite musicianship in light music is higher than it was a generation ago. At the same time, the true standard of many electronic musical instruments has fallen.

Manufacturers appear to be attempting to get the proverbial quart into a pint pot, especially where organs are concerned. Perhaps this is understandable where many instruments are sold to be installed in clubs, or other public places, where the audience expects a really professional performance-by their standards.
The organ studio demonstrator will show convincingly what a wonderful instrument you are about to purchase. It will no doubt have many extras such as a built-in rhythm unit, waa waa, percussion, arpeggiator, automatic chord unit, Leslie speaker, cassette tape recorder and perhaps a small synthesiser keyboard, to name but a few. Underneath all this, how much real organ is there? All these additions are expensive and the makers are probably working to a given price range, so something has to give.

The accompaniment manual is usually the victim, and the buyer is lucky if he is offered more than one pitch on that keyboard. We should perhaps remember that not all users of electronic organs are light music orientated or require the help of automatic chord/rhythm units. No serious organist would consider a single-pitch manual, or for that matter a short spinet manual of 44 notes and a set of stub-pedals. A number of users are primarlly interested in baroque music or are simply church organists who require a home organ for practice purposes which will produce conventional pipe-organ tonal quality.

## SOUND SYNTHESISER

For those who wish to experiment with unusual effects, the synthesiser is ideal. Mr Shaw's P.E. Sound Synthesiser should prove to be a fascinating project for readers seeking new musical sounds: we hope it will also alert organ makers to the fact that organs should sound as such and not attempt to compete with the synthesiser. Both are separate and distinct musical devices with identities of their own.
Incidentally, readers who went to the Audio Fair to hear Mr Shaw's synthesiser last year might also have listened to some of the stereo demonstrations on various stands. One of the records used for this purpose was "Moog Indigo" (VSD 6549) featuring Jean Jacques Perrey, is recommended to those who like the Moog and can appreciate the performer's skill and have a strong sense of humour.


THIS alarm system was developed to protect the house and buildings remote from it, for example, garage, workshop, etc., which might be subject to burglary or vandalism. It can of course be used to protect all other types of property.

## SEARCH LOOP SYSTEM

Many alarms use the search loop system in which the doors and windows have micro-switches fitted. The switches are wired in series and should any one switch be opened the circuit is broken. When the loop is connected to a simple alarm breaking the search loop will cause a bell or other device to sound. However, if the loop can be shorted out before the switches the alarm can be rendered inoperative.

This is particularly easy if the building protected is remote from the house as the search loop wires may be run back together and offer an opportunity for short circuit. Short circuits could be caused in a number of ways, by accident, fire or deliberately.

## BALANCED BRIDGE

To overcome these problems a simple bridge was devised for the prototype security alarm as seen in Fig. 1.

Here, one arm is made up of the search loop wire resistance Rx. With the bridge balanced, that is, when $\mathrm{Rx} \times \mathrm{R} 2=\mathrm{R} 1 \times \mathrm{R} 3$, no voltage will appear at the alarm input points XY . If the search loop is made either open or short circuit, outputs will appear at these points but of opposing polarity.

## POLARISING DIODES

To overcome this and to provide voltages of a single polarity for the open and short circuit conditions, a diode bridge was arranged so that any change of balance in the resistance bridge provides a negative going input to the alarm circuit as in Fig. 2.

In this, the finalised circuit of the Security Alarm, the resistance bridge is made up of $\mathrm{R} 1, \mathrm{R} 2, \mathrm{R} 3, \mathrm{VR} 1$ and the loop resistance Rx.

Arm resistances are made 150 kilohms so that the standing current is low. VR1 is included to balance any difference in the bridge arms and also provides a test facility as described later.

## LATCH CIRCUIT

As the output resistance of the bridge is relatively high it is necessary to multiply the input impedance


Fig. 1. Basic bridge system


The completed security alarm control unit
of any device connected across it. In the latch circuit this is achieved by connecting TR1 and TR2 as a Darlington pair.

TR2 output drives TR3 which is a higher power device suitable for driving a relay or lamp up to 800 milliamps when saturated.

Latching or hold on is achieved as follows. When TR3 is turned on by TR2 the collector voltage falls due to the drop across the relay and when TR3 is saturated is approximately 0.3 V .

As TR3 collector goes negative, this turns TR2 on harder and positive feedback holds TR2 and TR3 in saturation regardless of input current to TR1.

The current to TR3 base is limited by R5. Once tripped the circuit will stay on until the supply is interrupted. C2 is included to ensure the circuit resets.
In the prototype a relay was used to switch on an external bell. It could also be used to turn on lights or activate other warning systems.

## CONSTRUCTION

Most of the small components given in the circuit diagram can be assembled on a piece of 3 in $\times 1 \frac{1}{2}$ in Veroboard as is Fig. 3. When assembled and wired, 6in sleeved flying leads should be connected where indicated.

The choice of housing for the board and ancillary pieces was a 4 in $\times 6$ in $\times 2 \frac{1}{2}$ in standard aluminium chassis. First the mounting holes for VR! are drilled together with those for the double-pole switch and Veroboard spacers.

With these items fitted interwiring can be completed as in Fig. 4.

## TESTING

To test the assembled alarm connect up batteries B1 and B2 only and fit a 200 kilohm resistor across the loop terminal. If a high impedance multimeter is available connect across capacitor Cl as seen in Fig. 2.

Set the meter to the ten volt range, and switch the unit on. If now VR1 is rotated from end to end a null should be found.

If all is in order, connect B3 and switch on. The relay should stay out. If this is not so check that the null balance is correct.

Now rotate VR1 in a clockwise direction and the relay should pull in. If the null is now reset the relay should remain in.

Now reset the alarm by flicking switch S1 off and on, then rotate VR1 anticlockwise when the


Fig. 2. Circuit diagram of the security alarm

relay should again pull in. Return VR1 to null and reset the alarm with the switch.

Note that the relay cannot be reset unless VR1 is at null.

## TESTING WITHOUT A METER

Disconnect R4 from the base of TR2 and connect a $200 \mathrm{k} \Omega$ resistor across the loop terminals as before. Connect all batteries and switch on.

Rotate VR1 until the relay pulls in, then back off until the relay drops out. Note the point at which the relay pulled in.

Rotate VR1 in the opposite direction until the relay pulls in again, and note this point. The centre of the two points at which the relay pulled in is the null point of the bridge.

Reconnect R4 and check that when VR1 is rotated in either direction the relay pulls in and remains when VR1 is set to null.

## FINISH

Once the instrument has been checked and the null and test points have been determined, Letraset may be used to apply a legend to the front panel. A coat of clear varnish will ensure the case stays bright.

## INSTALLATION

As explained previously the search loop resistance must total $150 \mathrm{k} \Omega-200 \mathrm{k} \Omega$. This is extremely high and any amount of wire used to make up the search loop will not affect this figure, therefore it is necessary to insert resistance in the form of two $100 \mathrm{k} \Omega$ resistors in the loop

Arrangement of switches in the loop need not be confined to microswitches on doors and windows. Switches can be placed under carpets, etc., depending on the amount of security required. One further idea to protect windows apart from microswitches, is to fix a screen of fine copper with tape or clear varnish directly to the glass. This is included in the search loop; should the window be broken, the alarm will sound.
The alarm control unit would normally be installed in some part of the house, perhaps in a cupboard or concealed behind furniture. However, when siting the alarm, bear in mind the wires will have to run to parts of the house or outbuildings to be protected.

## WARNING DEVICE

No actual warning device is shown as this will be governed by personal requirements, possibly only a warning light will be required, however the relay could turn on house lights or ring a large bell.

Once installed and assuming the alarm has been tested as above, no difficulty should be encountered. Before connecting the search loop check with an ohmmeter for continuity and correct resistance. Connect the search loop to the control unit and set VR1 to null; switch on the alarm and check that both shorting and open-circuiting the search loop cause the alarm to operate.

When in use periodically check the alarm by rotating VR1 first clockwise and then anticlockwise. In both cases the alarm should sound. This forms a test of battery condition. Batteries should operate the unit for their shelf life.

HI-FI TAPE LINK.
continued from page 332

## 33 i.p.s.

Repeat as for $7 \frac{1}{2}$ i.p.s. using a test frequency of 500 Hz .
$1_{8}^{\frac{7}{8}}$ i.p.s.
As for $7 \frac{1}{2}$ i.p.s. but using 250 Hz .
The bias must be determined separately for mono and stereo modes.

## PRE-EMPHASIS

Adjustment of the pre-emphasis gives a maximally flat overall frequency response.

## $7 \frac{1}{2}$ i.p.s.

Apply an input signal from a signal generator at $15 \cdot 4 \mathrm{kHz}$ and adjust LI until peak output is obtained at the output of the replay amplifier (junction of R11 and R13). Next set the generator frequency to 4 k Hz and record at a level of -10 dB . Replay the tape and note its output as this is to be used as a reference.

Reset the frequency to 15.4 kHz and make another recording leaving the level control untouched. Note the playback level and then make successive recordings adjusting VRI to give a playback level at 15.4 kHz which is $\frac{1}{2} \mathrm{~dB}$ greater than at 4 kHz . The overall response should now be reasonably flat. However, a check should be made at a number of points between 4 kHz and 15.4 kHz adjusting VR1 so that the undulations in the response curve lie equally about the 4 kHz figure.

Then repeat this procedure for the other channel.

## 3 ${ }^{\frac{3}{4}}$ i.p.s.

Record a 800 Hz reference level once again at -10 dB . Set the generator to 9.6 kHz and repeat the above procedure but this time adjusting VR2 then VRI02.

## 17 i.p.s.

In this case a 200 Hz reference level is used at -10 dB . The generator is set initially to 6.0 kHz and VR3 then VR!03 are set up as above.

## MODIFICATIONS

Readers wishing to save the expense of two meters can parallel the outputs of the meter drive amplifiers into one storage capacitor. The meter will then show the larger of the two input signals.

If this design is to be used with the P.E. Gemini amplifier then it is advisable to fit attenuators to the input and output sockets. This allows reasonable use of the gain control to be made when recording and on playback gives an output consistent with the input sensitivity of the Gemini.

Correction: In the first part (March 1973) Figs. 2b and 2c should be transposed.


## By R.W.COLES

 PART 10
## M COUNTER BOARDS

T
His months article deals with the m(COUNTER) bourds whici are the last of the arithmetic unit plug-in cards to be described.

## M COUNTER FUNCTION

The basic system used to erable the multiplicaTION and DIVISIGN operations to be carried out was desctited in Part 1, where it was mertioned that the successive adcitions and subiractions carried out were counted in a counter circuit.

It is this co-nter which is housed on the two identical $m$ boards, together with the comparator circuit required during mULTEPLIEATION to register an equality tetween the count and the contents of the 1 register.

## BLOCK DIAGRAM

A block dagram of the COUNTER/COMPARATGR circuits and their related data paths is shown in Fig. 1D.I, which can be placed in context by reference to the owerall system black diagram, Fig. 1.3 of Part 1.

The counter itself consists of a serial string of six, four-bit, decade counter units which have a maximum count capacity of 999999.

The cOUNTER can be cleared or pieset by appropriate control signals from the progranme, and is triggered by the plus/minus complete signa from board CB, which is produced during each addition and subtraction.

The six, four-bit, B.C.D. ouputs from the counter are fed to the comparator circuit and also to the a register into which they can be enterad lat the end of a DIVISION sequence as required.

When the comparator registers an equality between the sount and the E REGISTER contents during a multiplication, it sets a latch which produces the comparator equal signal, whict i申 turn slops the arithmetic clock.

Before a multiplication sequence, the bouals latch is cleared by a signal from the frogramme.


Fig. 10.1. Block diagram of the ZOUNTER/ CCMPARATOR circuits and their related data paths


## PARTITIONING

A six decade counter and comparator requires too many i.c.s, even when using M.S.I. devices, for it to be housed on a single DL109 card, so the circuit is split into two identical sections, each comprising a three decade counter and a commensurate amount of comparator circuitry. This is described more, fully in Fig. 10.2.

Only one equals latch is required, but in practice a latch is incorporated on each board to ensure interchangeability, which is an advantage in fault finding, and initial testing.

The latch in use is determined by the external edge connector wiring, no connection being made to the latch inputs and outputs on the board in the M2 position.

## FULL CIRCUIT

The full circuit of one of the m COUNTER boards is shown in Fig. 10.3. The counter chain is easily identified as IC's 123, 124 and 125 which are SN7490 devices connected to count in a B.C.D. code by connection on the $A$ output to the $B$ input.


Fig. 10.2. Partitioning of the COUNTER/COMPARATOR between the two $M$ boards


Fig. 10.3. Circuit diagram of one of the $M$ boards. The other board is identical to this, both being built on DL109/44 boards

The count input to the board comes either from the plus/minus complete line (in the case of M1) or from the LS + 2, D output of board M1 (in the case of M2).

Each of the SN7490 devices has a decoupling capacitor connected between its power supply lines, in addition to the two standard board decoupling capacitors C41 and C42.

## LINE DRIVING

Special precautions are necessary for absolute integrity of the count, without false triggering or commutation, because the ABCD counter outputs are taken off the board as inputs to the a register.

Line driving from counters in this way can cause problems due to the high peak current required to charge the stray capacitance of the line during a 0 to 1 transition. Having an extra reservoir of charge available directly across the i.c. power pins goes a long way toward preventing the mistriggering problems which could result.

## COUNTER PRESETS

The reset 0 (R0) and reset 9 (R9) inputs to the SN7490 set the COUNTER outputs to 0000 or 1001 respectvely.

The RO inputs are connected together to form the clear counter line, controlled by the programme, and the R9 inputs together make up the reset to 999 line.

As mentioned in Part 1, it is necessary to preset the m COUNTER to 999999 before a division so that the final number of subtractions counted when the A register contents go negative and stop clock generation, is not the full number of subtractions performed, but the full number minus one.

Setting the count to 999999 is the same as starting to count from minus one, since on the first plus/ minus complete pulse, the count will change to 000000 , the number registered by the counter always being one behind the true number of subtractions performed.

During multiplication the true number of additions performed has to be counted-the programme ensuring this by energising the clear counter input and not the reset to 999 input.


Fig. 10.4. Equivalent logic for an EXCLUSIVE-OR gate and truth tables for both positive and negative logic conventions

COMPONEXIS

## Resistors

R72, R73 $560 \Omega \frac{1}{4} \mathrm{~W} \pm 10 \%$ (2 off)
Crpacitors
$\begin{array}{ll}\text { こ41, C46 } & 10 \mu \mathrm{~F} 15 \mathrm{~V} \text { elect. (2 off) } \\ \text { C42-45, C47-50 } & 0.047 \mu \mathrm{~F} \text { (8 off) }\end{array}$
Integrated Circuits

| IC123-125, IC132-134 | SN7490 (6 off) |
| :--- | :--- |
| IC126-128, IC135-137 | SN7486 (6 off) |
| IC129, IC138 | SN7400 (2 off) |
| IC130, IC131, IC139, IC140 | SN7405 (4 off) |

## Printed Circuit Boards

Type DL109/44 Shirehall (2 off)
In each case components are divided equally between the two $m$ boards

## COMPARATOR

The counter as described is all that is needed to allow the division operation to take place, but during multiplication comparison of the count with the eregister contents is required.

The COMPARATOR is made up of the remaining i.c.s on each board and is concerned solely with detecting the equality of e register and counter outputs so that a control signal can be produced to stop the clock at this point.

The 24 bits of e register data and the 24 bits of COUNTER data are individually compared on a one-to-one basis in a series of 24 exclusive-or gates formed from six SN7486 packages, housed three to a board.

## EQUIVALENCE GATE

The SN7486 package is a member of the M.S.I. family and is described as a quad exclusive-or gate in TTL literature. The very useful exclusive-or function has its own logic symbol, but is in fact made up of a series of simpler gates, as has its own logic symbol, but is in fact made up of a series of simpler gates, as shown in Fig. 10.4.

Readers may recognise the equivalent logic as being simply the common AND-OR-INVERT function together with a couple of inverters to produce the NOT version of the $A$ and B inputs.
The reason for the exclusive-or name becomes obvious when the basic (positive logic) truth table is examined. The output from the gate is a logic 1 if either input $A$ OR input b is a logical 1 but not if both are logical I's.
This response is that of a non-equivalence gate since a logic 1 output is produced only when the inputs are different, but the situation is changed when the gate is examined in operation as a negative logic system, as the second truth table demonstrates.

## NEGATIVE LOGIC

In the second truth table we can see that when a low voltage is interpreted as a logic 1 , rather than as a logic 0 , the output of an SN7486 gate is a logic I when the inputs are identical, giving the equivaence function.

## M COUNTER BOARDS



Layout of components on upper side of M COUNTER board, and interconnection details of the M1 edge connector. See Fig. 6.9 for disposition of edge connectors


Layout of capacitors on underside (ignore unmarked capacitor) and interwiring details of M 2 socket

To disbelievers, all this talk of switching logic conventions to suit the circumstances can be confusing, and really it is only a convenient way of looking at things.
In practical terms, the output of an SN7486 gate will go low when its inputs are identical, so to determine when all 24 gates have low outputs, i.e. when $m$ equals $E$, we need a 24 input NaND gate which responds to negative logic inputs.

## NEGATIVE LOGIC NAND GATE

No such gate is available in the standard TTL range, but if it were, it would be listed as a NOR gate because TTL is described in the positive logic convention.

All is not lost however since by using an opencollector inverter connected in the input of each SN7486, and then joining all the open collectors through a single common resistor to $\mathrm{V}_{\mathrm{cc}}$, i.e. by performing the wIRED-Or function at their outputs, a negative logic NAND gate of virtually unlimited size can be formed (Fig. 10.5).

The way a gate operates is fairly straightforward: if all SN7486 outputs are low, i.e. if M equals E , then the output of all inverters will be high, and the common resistor ensures a high voltage output.
If any one or more of the SN7486 outputs is high, however, one or more of the inverter outputs will go low and pull the common output to a low level.

## INVERTERS

The inverters used on the $m$ boards are type SN7405, which have the required open collector output circuitry. Note that the SN7404 devices are not suitable for use in this position due to their standard totem-pole outputs.

Although only one "pull-up" resistor is required for the full 24 inverters, electrically speaking in fact a separate resistor is used on each board to allow the boards to operate autonomously when required.

The inverter outputs from the two boards are united by means of the COMPARE EXPANSION input/ output line, so that the two resistors are effectively in parallel.

## LATCH FUNCTION

When an equality is registered by the comparator, the common output line rises to a high level and this signal is used to set the simple latch flip-flop made from cross-coupled SN7400 gates G2 and G3.
Setting the latch is carried out via another gate G1, which is controlled by the clock input line to


Fig. 10.6. PLUS/MINUS COMPLETE waveform from the COUNTER board
the first SN7490. In practice this line will carry the plus/minus complete waveform, since only the latch on the M1 board is wired into circuit.

The reason for this gated latch input circuit is explained in Fig. 10.6, which shows the plus/minus COMPLETE waveform from the COUNTER board.

The SN7490 counters are triggered from the negative going signal, but because these devices operate in the ripple count mode, there will be a significant count propagation delay time down the chain which can and will lead to transient spurious outputs from the comparator gating.

Using the plus/minus complete signal to gate the comparator output prevents the spurious outputs from setting the equals latch until count propagation is complete, since GI is enabled by the positive going edge of the waveform.

## EQUALITY

When a genuine state of equality exists between the COUNTER and e register the latch is set, energising the counter equal line which in turn stops the supply of clock pulses to the $\Lambda, z$ and ADDER boards.

Before a further multiplication sequence is initiated, the programme clears the equals latch ready for a new comparison.

## CONSTRUCTION

Construction of the two m boards follows the by now familiar pattern, two DL109/44 cards ieing used. All wiring should be kept as short as possible whilst avoiding "bird's nests".
Speed problems decrease by a factor of ten for each stage of the counter meaning in effect that only the first stage could be a problem in this respect. For this reason it is best to select which board is to be installed in the M1 position during test calculations, since the first stage of one board might perform better than the other at speed.

## TESTING

The M boards are easy to check in isolation if required, but if the recommended sequence of construction has been followed and the calculator is operational on add/subtract, it is easier to test the boards in situ, using the multiply/Divide pro-grammes-but more of this next month.

Fig. 10.5. The use of inverters to form a 24 input NOR gate

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Caraerial
Comaxial
D.I.N. 2 pin (speaker) D.I.N. 3 pin
D.I.N. 5 pin, $180^{\circ}$
D.I.N. 6 pin'

Jack, $2 \frac{1}{} \mathrm{~mm}$ unscreened
lack, $2 \frac{1}{2} \mathrm{~mm}$ screened
jack, $3 \frac{1}{2} \mathrm{~mm}$ unscreened Jack. $3 \frac{1}{2} \mathrm{~mm}$ screened jack, tin unscreened Jack, stereo, unscreened lack, stereo, screened Phono, plastic top Whono, plated metal Banana 4 mm , red or black $\quad 3 \frac{1}{2} \mathrm{p}$

## LINE SOCKETS

## Car aerial

D.I.N. 2 pin (speaker)
D.I.N. 3 pin $180^{\circ}$ D.I.N. 5 pin, $180^{\circ}$ jack, $3 \frac{1}{2} \mathrm{~mm}$ lack, $\operatorname{tin} \mathrm{mm}$ screened lack, stereo, screened Phono, plated metal


TRANSFORMERS
all with 0.250 Volt primaries

## Miniature

MM6 $6 \mathrm{~V}, 500 \mathrm{~mA}+6 \mathrm{~V}, 500 \mathrm{~mA}$. MM12
MM2
$20 V, 250 \mathrm{~mA}+12 \mathrm{~V}, 250 \mathrm{~mA}$
$150 \mathrm{~mA}+20 \mathrm{~V}, 150 \mathrm{~mA}$ 61.42 plus 14p p. \& p.
L.T1. $6 \cdot 3 \mathrm{~V}, 1 \cdot 5 \mathrm{~A}-82 \mathrm{p}$ plus 20p p. \& p . LT2 $6.3 \mathrm{~V}, 3 \mathrm{~A}-98 \mathrm{p}$ plus 28 p p. \& p . LT3 $12 \mathrm{~V}, 1.5 \mathrm{~A}-96 \mathrm{p}$ plus 28 p p. \& p . LT4 $12 \mathrm{~V}, 3 \mathrm{~A}-\mathrm{E1} 45$ plus 33 D p. \& $p$.
LT5 $9-0-9 \mathrm{~V}, 0.5 \mathrm{~A}-33 \mathrm{p}$ pius 23 p p. \& LT5 $9-0-9 \mathrm{~V}, 0 \cdot 5 \mathrm{~A}-83 \mathrm{p}$ pius 23p p . \& p .
LT6 $12-0-12 \mathrm{~V}, \mathrm{~A}-\mathrm{El} \cdot 04$ plus 29 p p. \& p
Multi-tapped
MT30/2 0-12-15-20-24-30V, 2A- 12.15 plus 33p p. \& p. ${ }^{\text {MT6011 }} 0$-5-20-30-40-60V, IA- 62.31 plus 33p p. \& p.
MT602
O-5-20-30-40-60V, 2A—63-25 plus $37 \mathrm{p} p$. \& $p$.
Chareer
CT/011A- $11 \cdot 16$ plus 28p p. \& D
CT/03 4A- 1.76 plus 33 p D. \&
Secondaries $0-5-11-17 \mathrm{~V}$.
Speaker Matching 3-8-16 Example: $16 \Omega$ speaker
99 p plus 22 p p. \& p.


## CASSETTE OWNERS

For Philips and similar cassette recorders. PUI2 power unit for connection to $12 \mathrm{~V}+$ or -E P. \& 75 mains power supply. output $7 \frac{1}{2} V$ D.C.$62 \cdot 15+16 \mathrm{p}$ p. \& p . Both units are complete with eables and 5 pin

## CASSETTE MICROPHONE

 Low impedance dynamic with remotecontrol switch. Fitced $2 \frac{1}{2} \mathrm{~mm}$ and $3 \frac{1}{2} \mathrm{~mm}$
plugs. $\& 2.20$ plus 15 p p. $\& \mathrm{p}$.

## ELECTROLYTICS

|  |  | 1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $1 \mu \mathrm{~F}$ | 450 V | $21 p$ | $1000 \mu \mathrm{~F}$ | 50 V | 46p |
| $2 \mu \mathrm{~F}$ | 450 V | 22p | $2000 \mu \mathrm{~F}$ | 25 V | 43 p |
| 4 $\mu \mathrm{F}$ | 350V | 151p | $2000 \mu \mathrm{~F}$ | 50 V | 58p |
| $8 \mu \mathrm{~F}$ | 450V | $18 \frac{1}{2} \mathrm{p}$ | $2500 \mu \mathrm{~F}$ | 25 V | 50p |
| $16 \mu \mathrm{~F}$ | 450 V | 20p | $2500 \mu \mathrm{~F}$ | 50 V | 66 p |
| $25 \mu \mathrm{~F}$ | 25 V | $7 \frac{1}{\text { P }}$ P | $3000 \mu \mathrm{~F}$ | 25 V | 53 p |
| $25 \mu \mathrm{~F}$ | 50 V | $11 p$ | $5000 \mu \mathrm{~F}$ | 25 V | $66 p$ |
| $32 \mu \mathrm{~F}$ | 450 V | 30p | $5000 \mu \mathrm{~F}$ | 50 V | 41.21 |
| $50 \mu \mathrm{~F}$ | 50 V | $11 p$ | $8-8 \mu \mathrm{~F}$ | 450 V | 20p |
| $100 \mu \mathrm{~F}$ | 50 V | 12p | 8-16 4 F | 450 V | 22p |
| $250 \mu \mathrm{~F}$ | 25 V | 151p | 16-16 $\mu \mathrm{F}$ | 450 V | 30 p |
| $250 \mu \mathrm{~F}$ | 50 V | 19p | $16-32 \mu \mathrm{~F}$ | 450 V | 69 p |
| $500 \mu \mathrm{~F}$ | 25 V | 20p | 32-32 $\mu \mathrm{F}$ | 450 V | 54 p |
| $500 \mu \mathrm{~F}$ | 50 V | 271 ${ }^{2}$ | $50-50 \mu \mathrm{~F}$ | 350 V | 42p |
| $1000 \mu \mathrm{~F}$ | 25V | 30p |  |  |  |

## Build yourselfaTRANSISTOR RADIO <br> WITH AF'TER SALES SERVICE

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10 TRANSISTORS. $\theta$ TUNABLE WAYEBAMDS, MW1, MW2, LW, SW1, SW2, SW8 TRAWLER BAND, VHF AND LOCAL STATIONS ALSO AIRCRAFT BAMD.
Built-in ferrite rod aerial for MW/LW. Retractable, chrome plated 7 section telescopic aerial, can he angled antl rotated for peak short wave and VHF listening. Puah-pult output using 600 mW transistors. Car Aerial and tape record aockets. 10 transistore plus 3 diodes. Fine tone unoting coil speaker. Ganged tuning condenser with VH section. Separate coil for Aircraft Band. Volume/on off, wave change and tone controls Attractive case in black with silver blocking. Size 9 in $\times 7$ in $\times 4$ in.
Easy to follow instructions and diagrans. Parts price liat and easy build plans 30 p (FREE with parts). Earpiece with plug and switched socket fur private listening $30 p$ extra

TOTAL BUILDING costs

## £8:50

P.P. INS. 50p (OVERSEAS P. © P. ©I)


## ROAMER

 SIX6 TUNABLE


TUNABLE WAVEBANDS: MW1, MWR, LW. SW1 W2. SW8 AND TRAWLER BAND. l built-in ferrite rod acopic aerial tor short waves. Push-pult output using 600 mW transistors. Car serial and tape record sockets. Belectivity switch. 8 trangistors phis 3 dioies. Fine tone denser. Solume/on/ofr, tuning, wave change and tone controle. Attractive case in rlch chestnut shade with gold blocking. Size 9in $\times$ Tin $\times$ tin approx, Easy to follow instructions and diagrame. Parts price list and easy build plans 26p (FREF: witli parts). Earpiece with plug and awitched socket for pritate listening 30p extra.
TOTAL
f6.98 $8^{\circ} \mathrm{d}$
BUILDING COSTS $50^{\circ}-\left(\begin{array}{l}\text { (OVERSEAS } \\ \text { P. RP. EI) }\end{array}\right.$
POCKET FIVE


8 TUNABLE WAVE-
BANDS: MW, LW,
TRAWLER BAND
WITH EAND FOR EASIER TUNING OF LUXEM MW BAND FOR EASIER TUNING OF LUXEM-
BOORG, ETC. 7 etages-5 transistors and 2 diodes. BODRG, ETC. 7 atages-5 transistors and 2 diodes. speaker. Attractive black and gold case. Size $5 \frac{1}{4}$ inx lifin $\times 3$ in. Easy build plans and parts price list 10p (FREE/with parts).


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future use. Ideal for Schools, Educafuture use. Ideal for schools, Educa terested in radio conatruction. Parts price list and eass build plans 25 p (FREE with parts).
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INCLUDING ES E E
CASE AND PLANS
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Address


## FIRST AWARDS

The Society of Radio and Electronic Technicians, now almost 6,000 strong, has awarded its first three Honorary Fellowships. Proud recipients were Lord Orr-Ewing, Edwin Spreadbury and Kenneth Tempest, all of whom have played a major role in establishing the Society.

The awards were made at a dinner in The Cholmondeley Room, House of Lords, with this vear's SERT president, James Redmond, director of engineering BBC, in the chair. Among the distinguished guests were Sir Eric Eastwood, chief scientist and director of research GEC, and Sir Cyril English, director general of the City and Guilds of London Institute.

Of the three Honorary Fellows it was probably "Spread" who enjoyed the distinction most keenly for it was he who helped in the formation of the Radio Trades Examination Board back in 1941 and, later, as chairman of RTEB, he was instrumental in founding SERT of which he became first chairman.

Lord Orr-Ewing, top man in Ultra Electronics, was first president of SERT in 1966 and gave influential support. Immediate past chairman Kenneth Tempest had the satisfaction of seeing membership pass the 5,000 mark during his term of office.

SERT has not wavered in its policy of insisting on good qualifications for members and thus has helped raise the status of technicians and brought them into the professional class of employment.
The properly qualified electronic technician engineer deserves his
professional status and quite clearly the work of SERT and the IEETE (which caters more broadly for the electrical technician engineer although many members are in electronics) is important in establishing a better business and industrial status for members.

## MAGIC MILLION

A million pounds is a nice round figure for turnover-indeed a magic figure to aim at for those with the guts to go it alone without benefit of shelter from working within a big group.

Bill Coates, top man in Leices-ter-based component distributor Townsend-Coates gets his taste of magic this year. He started up in 1961 with a first year sales turnover of $£ 2,500$, largely to local concerns. Now he has a staff of 46 , stocks 16,000 different items from nearly a dozen manufacturers and sells on a nation-wide basis.

Two go-it-aloners who are working on the magic million, although still with some way to go, are Ray Vincent and Jim Griffith. In 1966 they took over ailing Plastronics Ltd., at Watford, a moulding and sub-assembly shop serving the electronics industry. Staff today is 40 after a move to new premises in 1969 and, says Jim, it will be necessary to make another move for expansion before long.

Among the more important customers for Plastronic moulded products are Garrard, BSR, British Radio Corporation, Lotus cars and Scammell lorries. The computer industry is also a big customer.

## EXHIBITION NEWS

The first commercial full scale exhibition and conterence on Automatic Testing Equipment-fastest growing sector of the instrument industry-will take place at the popular Metropole Convention Centre, Brighton, opening on November 26. Stands are already being booked by leading manufacturers and a call for papers has gone out.

Microwave 73, also at the Metropole is a sell-out. It will be opened officially on June 19 by His Royal Highness the Duke of Kent in his capacity as a member of the National Electronics Council and a Companion of the IERE.

Sir Gerald Narbarro is to hop over to the USA to open Coil Wind-ing-Chicago 73 organised by British-based Electromation Exhibitions Ltd. and opening on March 27. Sir Gerald is first president of the International Coil Winding Association.

The International London Electronic Components Show opening at Olympia on May 22 is to have 350 exhibitors. Biggest stand is occupied by a consortium of

French companies who are clearly determined to cash in on the opportunities of the enlarged EEC.
The Soviet Union will be showing valves, passive components and test gear through British agents $Z$ \& I Aero Services. Previous showings of Russian components both in the UK and France have left me totally unimpressed-perhaps there will be more of interest this vear.

## BIPOLAR PROCESS

Plessey's Bipolar Process III technology for integrated circults has now moved from pilot production at the Ailen Clark Research Centre at Caswell, to full productlon at the maln semiconductor plant at Swindon:

Whole familles of new devices have been planned and with higher speeds now available a new range of appllcations has been opened up. Among the first commercially avallable products are high speed dividers capable of accepting an input of $1 \cdot 2 \mathrm{GHz}$, and a range of logic circults compatlble with Motorola's MECL III range. Selected varlants. say Plessey, have a considerable performance gain over standard MECL III.

The production technique uses an epitaxlal layer only 4 microns thick with emitter-base and basecollector junctions well under a micron deep. This is obviously not a cheap process but every milestone on the path to improved performance must exact its price.

## half century

Eddystone Radio is approaching its 50 th birthday with record growth and a firmer policy than it has had for years. Eddystone's Big Three, managing director Dick Carroll, chief engineer Bill Cooke, and sales manager Ken Wilkins are now dedicated to total solid state equipment and minimum production targets of 10,000 receivers on any new models.

The last of the Eddystone valve receivers, the popular 830, has been delivered and is being superseded by the new solid state 1830 rance of general purpose receivers which have already won full approval from the British and $a$ number of other PTT administrations.

During a visit to Eddystone's Birmingham works, I was told that the 958 Series of high-stability receivers, of which over 1,000 have now been delivered, is now available in nine versions. What has given Eddystone this flexibility in production is a big switch to modular construction and this has also had its effect on manufacturing and testing methods.


W/e have spoken in general about digital instrumentation and counters and this month will consider how the counters can be constructed. We will first examine in detail the individual integrated circuits used in a typical decade counter.

## SN7490N DECADE COUNTER

The SN7490N consists of four master-slave bistables internally interconnected to provide a divide-by-five and a divide-by-two counter. There are also gated direct reset lines to inhibit the count inputs and return all the outputs to a logical 0 or binary coded decimal ( $B C D$ ) count of nine.

The output from the first bistable is not internally connected to the next stage, and so three different count modes are possible, Fig. 7.1.

1. The BD input is externally connected to the A output, and the A input receives the incoming count. A count sequence is obtained as shown in the truth table. The outputs can be reset to a conventional zero or to a BCD count of nine for nines complement decimal applications.
2. Where a symmetrical divide-by-ten count is required (the previous arrangement divides by ten, but not symmetrically) the $D$ output is connected to the A input. The input count is applied

## BINARY CODED DECIMAL

A binary numbering system for coding decimal numbers in groups of four bits. Thes binary value of these four-bit groups ranges from 0000 to 1001 and codes the decimal digits 0 to 9. To count to 9 takes four bits, to count to 99 takes two groups of four bits, etc.

## RESET

Also called clear. It is an input which makes the output go to a desired state, usually 0 or 9 .
to the BD input and a divided-by-ten symmetrical square wave is obtained at the A output. The circuit thus divides by five first and then by two.
3. For divide-by-two and divide-by-five operations the two counters can be used independently. Bistable A is used to divide-by-two while the BD input is used to obtain a divide-by-five operation at the $B, C$, and $D$ outputs. However the


Fig. 7.1. The three count modes possible with the SN7490N

## INTEGRATED CIRCUITS

Why buy alternatives when you can buy the gonuine articie from uat compeat

Type 1/1112/2420/99
$\begin{array}{lllll} & \mathrm{p} & \mathrm{p} & \mathrm{p} \\ \text { SN7400 } & 0.20 & 0.18 & 0 \\ \text { 8N7401 } & 0.80 & 0.18 & 0.16\end{array}$
8N7401
$\begin{array}{llll} & 0.20 & 0.18 & 0.16 \\ \text { EN7403 } & 0.20 & 0.18 & 0.18\end{array}$
BN7404

|  |  |  |
| :--- | :--- | :--- |
| SN7405 | 0.20 | 0.18 |
| SN | 0.18 |  |
| SN 7406 | 0.30 | 0.18 |

$\begin{array}{llll}\text { SN7406 } & 0.20 & 0.18 & 0.16 \\ \text { SN7407 } & 0.30 & 0.27 & 0.25\end{array}$
$\begin{array}{llll}\text { SN7407 } & 0.30 & 0.27 & 0.25 \\ \text { BN7408 } & 0.20 & 0.19 & 0.18\end{array}$

| BN7409 | 0.45 | 0.42 | 0.85 | SN7474 |
| :--- | :--- | :--- | :--- | :--- |
| BN 7410 | 0.80 | 0.18 | 0.16 | SN745 |

BN 7410

GN 7411 |  |  |  |  |
| :--- | :--- | :--- | :--- |
| BN7411 | 0.28 | 0.82 | 0.16 |
| BN7412 | 0.42 | 0.40 | 0.85 |

$\begin{array}{llll} \\ \text { BN7413 } & 0.42 & 0.40 & 0.85 \\ \text { BN7 } & 0.80 & 0.27 & 0.25\end{array}$
$\begin{array}{llll}\text { SN7417 } & 0.30 & 0.27 & 0.25 \\ \text { SN7420 } & 0.20 & 0.18 & 0.16\end{array}$
$\begin{array}{llll}\text { BN7420 } & 0.20 & 0.18 & 0.16 \\ \text { BN7422 } & 0.48 & 0.44 & 0.40 \\ \text { B }\end{array}$

| SN7422 | 0.48 | 0.44 | 0.40 | SN7490 |
| :--- | :--- | :--- | :--- | :--- |
| BN7423 | 0.48 | 0.44 | 0.40 | SN7 |

BN7423
BN7425
$\begin{array}{lllll}\text { GN7425 } & 0.48 & 0.40 & 0.35 \\ \text { SN } 7427 & 0 & 42 & 0.39 & 0.35\end{array}$
$\begin{array}{llll}\text { BN7427 } & 0.42 & 0.38 & 0.35 \\ \text { BN7428 } & 0.50 & 0.45 & 0.42\end{array}$
$\begin{array}{llll}\text { BN7428 } & 0.50 & 0.45 & 0.42 \\ \text { EN7430 } & 0.20 & 0.18 & 0.16 \\ \text { BN7432 } & 0.42 & 0.39 & 0.35\end{array}$
$\begin{array}{llll}\text { SN7432 } & 0.42 & 0.89 & 0.35 \\ \text { SN7433 } & 0.70 & 0.61 & 0.44 \\ \text { SN7437 } & 0.65 & 0.60 & 0.50\end{array}$
$\begin{array}{llll}\text { GN } 7437 & 0.65 & 0.60 & 0.50 \\ \text { BN7498 } & 0.65 & 0.60 & 0.50\end{array}$
$\begin{array}{lllll}\text { EN7440 } & 0.85 & 0.60 & 0.50 \\ \text { RN } & 0.8441 \text { AN } & 0.75 & 0.78 & 0.16 \\ \text { BN } & 0.70\end{array}$
$\begin{array}{llll}\text { EN7441AN } & 0 \cdot 75 & 0.72 & 0 \\ \text { SN7442 } & 0.75 & 0.72 & 0.70\end{array}$
$\begin{array}{lll}\text { BN7442 } & 0.76 & 0.72 \\ \text { SN7443 } & 1.00 & 0.95 \\ \text { SN } & 0.00\end{array}$
$\begin{array}{llll}\text { SN7445 } & 2.00 & 1.75 & 1.60 \\ \text { BN7446 } & 2.00 & 1.75 & 1.80\end{array}$
$\begin{array}{lllll}\text { SN7446 } & 2 \cdot 00 & 1 \cdot 75 & 1 \cdot 80 \\ \text { SN7447 } & 1 \cdot 75 & 1 \cdot 60 & 1.45\end{array}$
$\begin{array}{lllllllll} \\ \text { RNFICES } & 1.75 & 1.60 & 1.45 & \text { SN74141 } & 1.00 & 0.05 & 0.80\end{array}$ LARGER QUANTITY PRICES PHONE (OI) 4024891
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| AAY 30 | 10p | BC147 12p | BU105 225 | OC44 15p | TIE43 35p | 2N3055 55p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AAY42 | 15p | BC169C 12p | BY100 15p | OC45 15p | V405A 25p | 2 N 3440 76p |
| AAZ13 | 10 D | nc182 10p | BY12' 15D | OC5 7 50p | ZTx108 12p | 2N3442 1-25 |
| AC107 | 35p | 13 C 214 15p | BY127 15p | 0071 16p | ZTX 30012 p | 2 N 352575 p |
| ${ }_{\text {ACl26 }}$ | 25 p | BCY32 75 p | BYZ13 35p | $0 \mathrm{C72}$ 25p | zTX301 15p | 2N3614 59p |
| AC127 | 25p | 13CY34 35p | C106D 65p | OC77 45p | ZTX30218p | 2N3615 75p |
| ACl28 | 25p | 13CY39 1.00 | CET111 56p | $0 \mathrm{C81}$ 25p | ZTX341 20p | 2 N 370210 p |
| $\mathrm{ACl}^{\text {c }} 76$ | 25 p | BCY42 30p | GET115 55p | $0 \mathrm{C83}$ 25p | ZTX500 15p | 2N3704 10p |
| AC187 | $25 p$ | BCY43 25p | G ET880 45p | 0 Cl 40 55p | ZTX503 17p | 2 N 370510 p |
| ACl88 | 25 p | BCY55 250 | LM309K | $0 \mathrm{Cl170}$ 85p | 2G301 30p | 2N37141.80 |
| ACY17 | 80p | BCY70 15p | (T03) 1.87 | 0 Cl 11 30p | 2 N 404 20p | 2N3771 1.75 |
| ACY 20 | 20p | BCY71 20p | MATI21 25p | OC200 45D | 2N527 35p | 2N3773 2.00 |
| ACY21 | 20 p | BCY72 15p | MJE340 50p | OC201 75p | 2N696 15p | 2N3790 2.25 |
| ACY39 | 550 | BCY87 2.89 | MJE370 70p | OC202 80p | 2N697 15p | 2N3819 35p |
| ADI40 | ${ }^{50}{ }^{\text {D }}$ | BCZ11 50p | MJE520 75p | OC203 50p | 2N706 10p | 2 N 3820 50p |
| AD149 | 50 D | BD124 80p | MJE295s | OCP71 1.25 | 2 N 930 O 20 | 2N386\% 85p |
| ADi6I | $85 p$ | BD131 75p | 110 | ORP12 500 | 2 N 987 45p | 2 N 390315 p |
| ADI62 | 350 | BD132 80p | MJE3055 | ORP60 40p | 2N1131 25p | 2N3906 12p |
| AF17 | 20p | Br'115 25p | 75p | P348A 20p | 2N1132 25p | $2 \times 406112 \mathrm{p}$ |
| AF118 | 50p | BF167 25p | MPF105 40p | RAB310AF | 2N1302 18p | 2N406: 12 p |
| AF124 | 25p | FF173 25p | NKT21420p | 45p | 2N1304 22 p | $2 \mathrm{~N}+126$ 15p |
| AF139 | 80p | BF179 30p | NKT21840p | RAB508AF | 2N1305 22p | 2N4871 35p |
| AF186 | 40p | BF180 30p | NKT21740p | 55p | 2N1307 25p | $2 \mathrm{~N} 4578 \mathrm{30p}$ |
| AF239 | 40 p | BF194 16p | NKT403 70p | TAA263 75p | 2N1308 25p | 2 N 5777 55p |
| ASY27 | 30 p | RF195 15p | NKT40460p | TIL209 30p | 2N1ti3 20p | 28001100 |
| A8Y28 | 25 p | 13F861 25p | OA5 50p | TIP29A 50p | 2N1671 1-00 | 2801210.00 |
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| BAX 13 | 5p | ${ }^{\text {nFX }} 37$ 30p | 0 A 2007 p | TIP33A | $2 \mathrm{~N} 222 \mathrm{~T}^{20 \mathrm{D}}$ | 2830365 |
| BAX16 | 7p | BFX88 200 | OA202 100 | 1.00 | 2 N 2222 A | 28324 95p |
| BC107 | 10p | 1FFY50 20p | OC1\% 75p | TIP34A | 25p | $40250 \quad 60 \mathrm{p}$ |
| BC108 | 10p | BFY51 20p | OC20 95p | 150 | 2N2369A | 40360 40p |
| BC109 | 10 D | BFY52 20p | $00^{023} 85$ | T1P35A | 15p | 40361 40p |
| BC109C | 12p | BFY64 50p | 0 O 25 40p | 2.50 | 2N2906 20p | 4036250 p |
| BC113 | $15 p$ |  | OC28 6 | TIP38A | $2 \mathrm{~N}^{2926}$ (ail | 4040850 p |
| BC117 | 20 D | BLY36 <br> R8X20 <br>  <br> 150 <br> 150 | $\begin{array}{ll}\text { OC35 } & 50 p \\ 0 \text { O36 } & 85 p\end{array}$ | TIP414 $\begin{array}{r}3.00 \\ 75 \mathrm{p}\end{array}$ | cols) <br> 2 N 3053 <br> 10 p <br> 10 p | $40486 \quad 75 p$ |
| 8C143 | 35 D | BSY27 15p | OC42 40p | TIP42A 85p | 2N3054 50p | $\begin{array}{ll}40430 & 110 \\ 40430 & 100\end{array}$ |

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counters are reset simultaneously because the reset lines are common.

## SN7475N QUADRUPLE BISTABLE LATCH

The SN7475N is a bistable latch which is used as a temporary store for binary information, Fig. 7.2. Information which is present at a data input (D)
is transferred to the Q output while the clock is high. The $Q$ output follows the data for as long as the clock is high but the last information is retained at the data output when the clock goes low.

## SN74141N DECODER-DRIVER

The SN74141N is one of several decoder-drivers available in the TTL range and is designed to drive


Fig. 7.2. The SN7475N quadruple bistable latch ( $\mathrm{t}_{\mathrm{n}}=$ bit time before clock negative-going transition, $\mathrm{t}_{\mathrm{n}}+1=$ bit time after clock negativegoing transition)


Fig. 7.4a. A typical counting module

Fig. 7.4b. Typical wavetorms in the circuit above


Fig. 7.5. Cascading the modules for multi-decade operation
cold cathode indicator tubes. It accepts a BCD input which it decodes to drive the cathodes of an indicator tube without the need for external components, as in Fig. 7.3.

## SINGLE COUNTER MODULE

A typical application for a single counting module is shown in Figs. 7.4a, b, with the counting sequence.
(a) During $\mathrm{t}_{1}$ the decade counter is reset to 0 .
(b) During $\mathrm{t}_{2}$ a BCD count of three is available at the output of the SN7490N, but the indicator still displays 0 .
(c) At the start of $t_{3}$ the indicator will display 3 , and at the end of $t_{3}$ the BCD count of three is committed to the memory of the SN7475N. The decade counter is free to count again.
(d) During $t_{4}$ the decade counter is reset to 0 and will then repeat the cycle to display five.
For multi-decade operations the modules may be cascaded as shown in Fig. 7.5.

## PRACTICAL DETAILS

For those constructors who wish to experiment with these applications, R.S. Components produce the three integrated circuits, a printed circuit board, and the indicator tube.

The 5 V logic supply and the h.t. can be derived from a transformer which gives 6.3 volts and 250 volts.

For testing purposes the reset and transfer lines may be derived from switches, and the input signal derived from a Schmitt trigger SN7413N oscillator.

## FAN-IN PROBLEMS

(a) ReSET (SN7490)

The reset line of the SN7490 can have a fan-in of one if the other reset input is returned to $V_{\mathrm{cc}}$, so that an SN7400 (fan-out of 10) can drive an adequate number of decades.
(b) COUNT InPuTS (SN7490)

The A or BD inputs of the SN7490 can be driven from an SN7400.
(c) TRANSFER Clock (SN7475)

The transfer line of each SN7475 has a fan-in of eight (two per latch). The solution is to use one quarter of an SN7400 for each SN7475 package or to use a buffer (such as the SN7437 or SN7440) which has a fan-out of 30 .

## CONCLUSION

This article has shown how three integrated circuits can be used to interface with cold cathode indicator tubes. Where the intermediate outputs are not required the new SN74142N combines these three circuits into one 16 pin dual-in-line package, with a considerable space saving.

For driving displays other than cold cathode indicators the SN74141N would be replaced by one of the other drivers in the range. Although seven segment indicators (for example) are popular because they only need a 5 V rail, cold cathode indicator tubes are still preferred by many people, since the required h.t. is not difficult to provide.

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$\begin{array}{lllllllllllll}(\mu \mathrm{F} / \mathrm{V}) & 1 & 0 / 63,1 & 5 / 63, & 2 & 2 / 63, & 3.3 / 63,4.7 / 63,6.8 / 40, & 10 / 25 & 10 / 63, & 15 / 16, & 15 / 40, & 15 / 63\end{array}$ $22 / 10,22 / 25,22 / 63,33 / 6 \cdot 3,33 / 40,47 / 4,47 / 10,47 / 25,47 / 40,47 / 63,68 / 6 \cdot 3,68 / 16,100 / 4$, $100 / 10,100 / 25,100 / 40,150 / 63,150 / 16,150 / 25,220 / 4.220 / 10,220 / 16,330 / 4,330 / 10$, 470/6.3. 5p each. 68/63, 150/40. 220/25, 330/16, 470/10, 680/6.3, 1.000/4. 9p. $100 / 63$. $150 / 63,220 / 40,470 / 25,680 / 16,1,000 / 10,1,500 / 6 \cdot 3,12 p .220 / 63,470 / 40,680 / 25$. $1,000 / 16,1,500 / 10,2,200 / 6 \cdot 3,15 p .330 / 63,680 / 40,1.000 / 25,1.500 / 16,2.200 / 10$,
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| Pin insertion cool | 52p | 52p |
| Spot face cutcer | 42p | 42p |
| Pkt. 50 pins | 20p | 20p |

D.I.N. PLUGS AND SOCKETS

2 pin, 3 pin, 5 pin $180^{\circ}, 5$ pin $240^{\circ}, 6$ pin
Plug 12p. Socket 8p.
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9V mains power supply. Same size as PP9 battery.

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| $2500 \mu \mathrm{~F}$ | 40 V | 74 p | $2800 \mu \mathrm{~F}$ | 100 V | 62.60 | $450 \mu \mu \mathrm{~F}$ | 25 V |
| 201.68 |  |  |  |  |  |  |  |
| $2500 \mu \mathrm{~F}$ | 50 V | 58 p | $3200 \mu \mathrm{~F}$ | 16 V | 50 p | $5000 \mu \mathrm{~F}$ | 50 V |

$\begin{array}{ccccc}\text { HIGHVOLTAGE TUBULAA CAPACITORS—1,000 VOLT } & \\ 0.0 \mid \mu \mathrm{F} & 10 \mathrm{p} & 0.047 \mu \mathrm{~F} & 13 \mathrm{p} & 0.22 \mu \mathrm{~F} \\ 0.022 \mu \mathrm{~F} & 12 \mathrm{p} & 0.1 \mu \mathrm{~F} & 13 \mathrm{p} & 0.47 \mu \mathrm{~F}\end{array}$
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## Now-the Z.50 Mk. 2

## with built-in automatic transient overload protection


#### Abstract

When originally introduced, the Sinclair 2.50 proved how it was possible to design and produce a popularly priced modular power amplifier having characteristics to challenge the world's costliest amplifiers. Many thousands of $Z .50$ s are now giving excellent service day in. day out. But we have also learned that constructors do not always use their 2.50's ideally. That is why we have introduced modifications whereby risk of damage through mis-use. is gieatly reduced and performance further enhanced. The 2.50 Mk 2 has improved thermal stability, more accurately regulated D.C. limiting to ensure more symetrical output voltage swing and clipping and still less distortion at lower power. Z.50 Mk. 2 is compatible with all other Project 60 modules, and may be incorporated to advantage in existing systems. Eleven silicon epitaxial planar transistors are now used. Wwo more than in the original 2.50 . circuitry has been re-designed, making this versatile high performance amplifier better than ever.



Z. 30 the power amplifier for quality and economy

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Brilliant new
technical specifications
Input impedance $100 \mathrm{~K} s_{2}$
Input (for 30 w into 8 s ) 400 mV
Signal to noise ratio, referred to full o/p at 30 vHT 80 dB or better
Distortion $0.02 \%$ up to 20 W at 86 . See curve Frequency response 10 Hz to more than
$200 \mathrm{KHz} \pm 1 \mathrm{~dB}$
Max. supply voltage 45v ( $4 \Omega 2$ to $8 \Omega$ speakers) ( $50 \mathrm{v} 15 \Omega$ speakers only)
Min. supply voltage 9 v
Load impedance - minımum $4 s$ at 45 v HT Load impedance - maximum safe on open circuit
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The 2.30 provides excellent facilities for the constructor requiring a high fidelity audio system of less power than that available from 2.50 s Using a power supply of 35 volis. Z 30 wilt deliver 15 watts RMS into 8 ohms. or 20 watts RMS into 3 ohms using 30 volts Total harmonic distortion is a fantastically low $002 \%$ at 15 watts into 8 ohms with signal to noise ratio better than 70 dB unweighted Input sensitivity 250 mV into 100 K ohms. Size $80 \times 57 \times 13 \mathrm{~mm}\left(3 \frac{1}{6} \times 2 \frac{1}{4} \times \frac{1}{2}\right) Z 30 . Z 50$ and Z.50 MK. 2 modules are compatible and interchangeable

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Each Project 60 module is tested before leaving our factory and is guaranteed to work petfectly. Should any defect arise in normal use, we will service it al once and without any charge to you. if it is returned within two years from the date ol purchase. Outside this period ol guarantee a small charge (typlcally $£ 1,00$ ) will be made. No charge is made for postage by surface mail. Air Mail is charged at cost.

Typical Project 60 applications

| System | The Units to use | together with | Units cost |
| :---: | :---: | :---: | :---: |
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| 25W. RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers | $2 \times 2.30 \mathrm{~s}$, Stereo 60: PZ. 6 | High quality ceramic or magnetic P.U... F.M Tuner, Tape Deck etc. | £26.90 |
| BOW (3 ohms) RMS <br> continuous sine wave de luxe stereo amplifier. ( 60 W . RMS into 8 ohms) | $2 \times 2.50$ s, Stereo 60; PZ.8, mains transformer | As above | £34.88 |
| Indoor P.A. | Z.50, PZ.8, mains transformer | Mic. guitar. speakers. etc. controls | f19.43 |

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SPECIFICATIONS-Input sensitivities: Radio - up to 3 mV . Mag. p.u. 3 mV : correct to R.I.A.A. curve $\pm 1 \mathrm{~dB}: 20$ to $25,000 \mathrm{~Hz}$. Ceramic p.u. - up to 3 mV : Aux - up to 3 mV . Output: 250 mV . Signat to noise ratio: better than 70 dB . Channel matching: within 1 dB . Tone controls: TREBLE +12 to -12 dB at 10 KHz . BASS $+1210-12 \mathrm{~dB}$ at 100 Hz . Front panel : brushed aluminium with black knobs and controls. Size: $66 \times 40 \times 207 \mathrm{~mm}$.

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## Project 60 Stereo F.M. Tuner

Esin culax


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SPECIFICATIONS—Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108 MHz . Sensitivity $7 \mu \vee$ for lock-in over full deviation. Squelch level: Typically $20 \mu \mathrm{~V}$. Signal to noise ratio; $>65 \mathrm{~dB}$. Audio frequency response: $10 \mathrm{~Hz}-15 \mathrm{KHz}( \pm 1 \mathrm{~dB}$ ). Total harmonic distortion: $0.15 \%$ for $30 \%$ modulation. Stereo decoder opersting level; $2 \mu \mathrm{~V}$. Cross talk: 40 dB . Output voltage: $2 \times 150 \mathrm{mV}$ R.M.S. maximum Operating voltage: $25-30 \mathrm{VDC}$. Indicators: Stereo on : tuning. Size: $93 \times 40 \times 207 \mathrm{~mm}$.

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other applications which this remarkable IC. make possible. It is the equivalent of a 22 tran-
sistor circuit contained within a 16 lead DIL package, and the finned heat sink is sufficient for all requirements. The Super IC. 12 is compatible with Project 60 modules which would be used with the $Z .50$ and $Z .30$ amplifiers. Complete with free manual and printed circuit board

## SPECIFICATIONS

Output power: 6 watts RMS continuous (12 watts peak). 6-8 . Frequency Response: 5 Hz to $100 \mathrm{KHz} \pm 1 \mathrm{~dB}$. Total Harmonic Distortion: Less than $1 \%$. (Typical $0.1 \%$ ) at all output powers and frequencies in the audio band ( 28 V ). Load Impedance: 3 to 15 ohms. Input Impedance: 250 Kohms nominal Power Gain gedB (1.000 000.000 times) atter feed Gin Supply Voltage: 6 to 28 V . Quiescent curSupply voltage: 6 to 28 V . Quiescent cur-
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