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ELECTRONICS

VOLUME 9 No. 4 APRIL 1973

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VALUE ADDED TAX

Prices quoted in this issue were correct at time of going to press. From 1st April 1973 there will be no purchase tax, but a large number of goods will carry Value Added Tax.

Our May issue will be published on Friday, April 13, 1973

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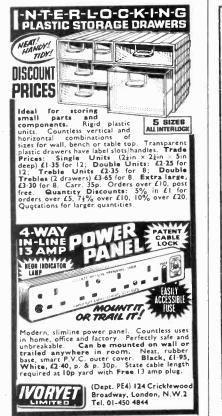
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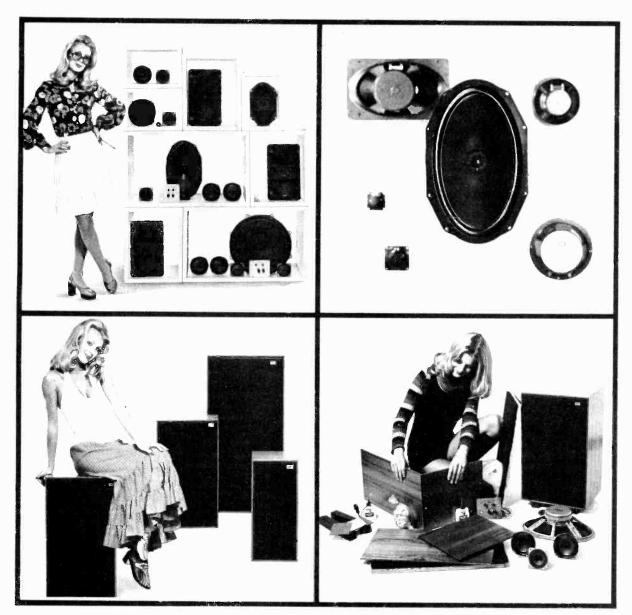
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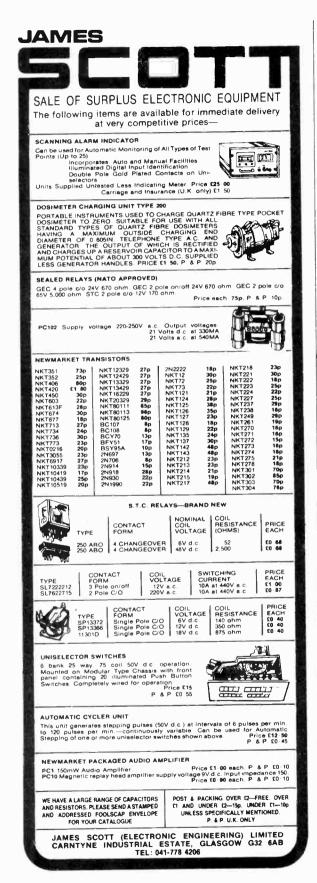
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PANELS 2

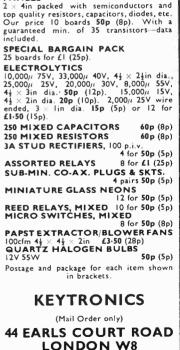
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- ★ Distortion-better than 1% at 1KHz.
- ★ Signal to noise ratio 80dB.

Tailor made to the most stringent specifications using top quality components and incorporating the latest solid state circuitry and ALSO was conceived to fill the need for all your A.F. amplification needs. FULLY BUILT — TESTED — GUARANTEED.



STABILISED POWER **MODULE SPM80**

£3.25p each

★ Supply voltage 10-35

★ Overall size 63mm ×

 $105mm \times 13mm$.

AP80 is especially designed to power 2 of the AL50 Amplifiers, up to 15 watt (r.m.s.) per channel simul-taneously. This module embolies the latest components and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Trans-former MT80, the unit will provise outputs of up to 1:5 amps at 35 volts. Bize: (Smm × 105nm × 30mm.) These units enables you to build Autio Systems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including.— Disco Systems, Public Addiress, Intercom Units, etc. Handbook available, 10p **PRICE £2:95**.

Volts.

TRANSFORMER BMT80 £1.95 p. & p. 25p.

STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the market, the PA100 stereo pre-amplifier has been conceived from the latest circuit tecnniques. Designed for use with the AL50 power amplifier system, this quality made unit incorporates no less than eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the lnput stages. Three ewitched stereo inputs, and runnble and soratch filters are features of the PA100, which also has a STEREO/MONO switch, volume, balance and continuously variable bass and treble controls.



 $\begin{array}{l} 20 Hz ~-~ 20 K\,Hz ~\pm~ 1 dB \\ better ~than~ 0 \cdot 1\% \\ 1 \cdot 25 ~mV ~into~ 50 K ~\Omega \\ 35 ~mV ~into~ 50 K ~\Omega \\ 1 \cdot 5 ~mV ~into~ 50 K ~\Omega \end{array}$ All input voltages are for an output of 250mV. Tape and P.U. inputs equalised to RIAA curve within $\pm 14B$. from 20112 to 20KHz. ± 15dB at 20Hz ± 1541 100Hz 154B at 20K Hz 8KHz better than -65dB+ 26dB

Supply Dimensions

+ 250 B + 35 volts at 20mA 292mm × 82mm × 35mm ONLY £11.95

SPECIAL COMPLETE KIT COMPRISING 2 AL50's, 1 SPM80, 1 BMT80 & 1 PA100 ONLY £23'00 FREE p. & p.

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	Goldring G800		AMPLIFIERS Please add 65p P. & P. & I Amstrad 6000 Mk. II Amstrad IC2000 Amstrad integra 4000 Armstrong 521 (Teak cased)	£14-95 £27-50 £22-50
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	Garrard SP25 Mk. III Garrard AP76 C Garrard SL65B C Garrard 401 C Garrard Zero 100 (Auto) C BSR MP60 Garrard Zero 100 (Single) C Goldring GL72 P Goldring GL72 P	12.75 49.90 17.20 13.95 28.75 36.90 29.40 20.90 27.45 26.85 34.95	Metrosound ST60 Pioneer SA5000 & 610 Pioneer SA5000A Pioneer SA5000A Rogers R/brook (Chassis) Rogers R/brook (Cased) Rogers R/bourne (Cased) Sinclair PR060 2 × Z30 PZ6 Sinclair PR060 2 × Z30 PZ6 Trans Sinclair AFU (Filter Unit)	£16-70 £22-95 £4-20
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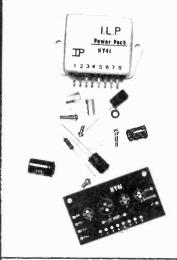


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L.P. (Electronics) Ltd



THE HY41

The HY41 supersedes the popular HY40 introduced by ILP last year. This highly improved module achieves true High Fidelity with a dramatic reduction in distortion (typically 0.05% at 1KHz into 8 ohms!) and is electronically and mechanically compatible with the HY40.

With this important improvement the HY41 retains all of the quality characteristics found in the earlier version and P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete power amplifier of extremely high performance sufficiently versatile to provide power not merely for Hi-Fi but also for public address systems and industry.

The free manual gives a full circuit diagram of the HY41 and its various applications including a complete stereo amplifier.

Like its predecessor the HY41 is based on conventional and proven circuit techniques developed over recent years.

OUTPUT POWER: British Rating 40 WATTS PEAK, 20 watts R.M.S. continuous. LOAD IMPEDANCE: 4–16 ohms. INPUT IMPEDANCE: 30K ohms at 1KHz. VOLTAGE GAIN: 30db at 1KHz

TOTAL HARMONIC DISTORTION: less than 0.15% (typical 0.05%) at 1KHz

FREQUENCY RESPONSE: 5Hz-50KHz + 1db. SUPPLY VOLTAGE: + 22.5volts D.C. SUPPLY CURRENT: 0.8 amps maximum.

PRICE: inc. comprehensive manual, P.C. board, five extra components and P. & P.:-MONO: £4.90 STEREO: £9.80

UNIQUE HYBRID PRE-AMPLIFIER

The HY5 has rapidly established a position in the WORLD as the sole hybrid pre-amplifier to contain all feedback and equalization networks within an integrated pre-amplifier circuit.

Supplied with the HY5 are two stabilizing capacitors and by the addition of volume, treble and bass potentiometers it is ready for use. Internally the HY5 provides equalization for almost every conceivable input, the

desired function is achieved by use of a multi-way switch or by direct interconnection. Two distinctive features of the HYS are its inbuilt sublication circuit, allowing it to be run off any unregulated power supply from **18–25** Volts and a balance circuit which, when linked by a balance control to a second HYS, forms a complete stereo pre-amplifier.

Specifically and critically designed to meet exacting Hi-Fi standards, the HY5 combines extremely low noise with a high overload capability. When used in conjunction with the HY41 and PSU45 forms a completely intergrated system.

INPUTS

Magnetic Pick-up (within \pm 1db RIAA curve) 2mV, 47K Ω

Tape Replay lexternal components to suit head). 4mV. $47K\Omega$ Microphone (flat) 10mV, 47KΩ

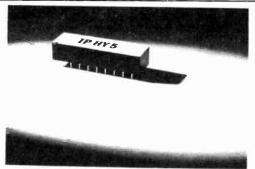
Ceramic Pick-up (equalized and compensatable) 20–2000mV, variable. Tuner (flat) 250mV, 100K Ω Auxiliary 1 250mV, 100K Ω Auxiliary 2 2–20mV, 100K Ω

OUTPUTS

Main Pre-amp output 500mV Direct tape output 120mV

ACTIVE TONE CONTROLS (Bexendall) Treble + 12db. Bass + 12db. Bass + 1230. INTERNAL STABILIZATION Enables the HY5 to share an unregulated ______supply with the Power Amplifier. SUPPLY VOLTAGE

16-25 volts PRICE: MONO: £3.60



SUPPLY CURRENT 6mA approx OVERLOAD CAPABILITY better than 26db on most sensitive input infinite on tuner and auxl. OUTPUT NOISE VOLTAGE: 0.5mV



POWER SUPPLY PSU45

The versatile P.S.U.45 is designed to supply your HY41's +HY5's in stereo or mono format.

STEREO: £7.20

Specification Input: 200-240 Volts.

Output: ± 22.5 Volts at 2 amps. Overall Dimensions: L. 7"; D. 3.8"; H. 3.1"

PRICE: £4.50 inc. P. & P.

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RS		16a	CIAL		ROA	MAIL O	IDON RDE	SW16	2 B\$ V/CE
	\$p 0·17	AFZ12	Expr 1 1.00	BYZ10	žp i	OAZ211	sp + 1 0-82	ZS170	fp 0.10
1N21 1N23	0.20	A8¥26	0.52		0.32	OAZ222	0.45	Z8271	0.18
1N85 1N253	0-88	ASY27 ASY28	0-82 0-25			OAZ223 OAZ224	0-45	ZT21	0-25 0-25
1N256 1N645	0-50	ASY29 ASY36	0.90	BYZ13 BYZ15	0-28 1-00	O AZ241 O AZ242	0-22 0-28	ZT43 ZTX107	0-25
1N726A	0.20	A8 Y 50	0.17	BYZ16	0-62	OAZ244	0-22	ZTX108	0-12
1N914 1N4007	0-07 0-20	ASY51 ASY53	0-40	BYZ88C3V	0·15	OAZ246 OAZ290	0-28	ZTX 300 ZTX 304	0-12 0-25
19113 19130	0-15 0-18	ASY55 ASY62	0-20	CIII CR81/05	0-65	OC16	0.50	ZT X 500	0.16
18131	0.18	ASY86	0.88	CRS1/40	0.45	OC16T OC19	0-87	ZT X 503 ZT X 531	0-17 0-25
18202 2G371	0-28	ASZ21 ASZ23	0-42	CS4B CS10B	8.18	0C20 0C22 0C23	0-85		
20381 20414	0-25	AUY10 AU101	0-98	DD000 DD003	0·15 0·15	OC23 OC24	0-60	INTEGRA CIRCUIT	TED
20417	0.22	BC107 BC108	0.10	DD006	0.18	OC25	0.87	7400	0-20
2N 404 2N 697	0-20	BC109	0·10 0·10	DD007 DD008	0-88	OC26	0-25		0-20 0-20
2N698 2N706	0-40	BC113 BC115	0·15 0·20	GD3 GD4	0-38	OC28 OC29	0-60	7403 7404	0-20
2N 706 A	0.12	BC116	0-25		0-88	OC30	0-40	7 10 -	0.20
2N708 2N709	0.68	BUILE	0.25	GD12	0-05	OC35 OC36	0-50	7407	0-30 0-30
2N1091 2N1131	0-88 0-25	BC121 BC122	0.20	GET102 GET103	0-22	OC41	0.25	7408 7409	0-20
2N1132 2N1302	0-25	BC125 BC126	0-68	GET113 GET114	0-20 0-15	0C42 0C43	0-80 0-40	7410	0.20
2N1303	0.18	BC140	0-55	GET115	0-45	0C44 0C44M	0.17	7412	0-23 0-42
2N1304 2N1305	0-22 0-22	BC147 BC148		GET116 GET120	0.25	OC45	0·17 0·12	7413 7416	0-80 0-80
2N1306 2N1307	0-25	BC149 BC157	0-15 0-15	GET875	0-30	OC45M OC46	0-18 0-27	$7417 \\ 7420$	0-30
2N1308 2N2147	0-25 0-75	BC158 BC160	0-12	GET880 GET881	0-87	OC57 OC58	0-60 0-60	1 7422	0-48
2N2148 2N2160	0-60	BC169	0.13	GET882 GET885	0-25	OC59 OC66	0-65	7423 7425 7427	0-48 0-48
2N2218	0.20	BCY31 BCY32	0-85 0-56	GEX44	0-08	0C70 0C71	0.12	1.2108	0-42
2N2219 2N2369A		BCY33	0-25	GEX45/1 GEX941	0-10 0-15	OC72	0-12 0-20	7430 7432	0-20 0-42
2N2444 2N2613	1-99 0-28	BCY34 BCY38 BCY39	0-80 0-40	GJ3M GJ4M	0-25 0-88	0C73 0C74	0-80 0-80	7433	0-70 0-65
2N2646 2N2904	0-45	BCY39 BCY40	1-00 0-50	GJ5M GJ7M	0-25 0-87	OC75 OC76	0-25	7437 7438	0-65
2N 2904A	0.25	BCY42	0.25	HG1005	0-50 0-20	0C77 0C78	0-40 0-20	7440 7441 A N	0-20
2N2906 2N2907	0-20 0-28	BCY42 BCY70 BCY71	0-20	HS100A MAT100	0.25	0C79	0-22	7442 7450	0-76 0-20
2N2924 2N2925	0-28 0-15	BCZ10 BCZ11	0-86	MAT101 MAT120	0-80 0-25	0C81 0C81D	0-20	7451	0-20
2N2926 2N3054	0-10 0-50	BD121 BD123	0-65	MAT121 MJE520	0-80 0-87	OC81M OC81DM	0-20 0-18	7453 7454	0-20
2N 3055	0.75	BD124	0-75	MJE2955 MJE3055	1.87	0C81Z 0C82	0-40	7460	0.20
2N3702 2N3705	0.10	BDY11 BF115	1-62 0-25	NKT128 NKT129	0-35	OC82D	0.20		0-80
2N3706 2N3707	0-23 0-12	BF117 BF167	0.50	¹ NKT211	0-25	OC83 OC84	0-25	7474	0-40 0-55
2N 3709 2N 3710	0·10 0·10	BF173 BF181	0-25 0-85	NKT213 NKT214	0-25 0-15	0C114 0C122	0.38	7475 7476	0-45
2N3711 2N3819	0-10	BF184 BF185	0.20	¹ NKT216	0-37	OC123 OC139		7480	0-80 0-87
2N5027	0.58	BF194	0.17	NKT217 NKT218	1.13	OC140	0-85	7483	1.00
2N5088 28301	0-88 0-50	BF195 BF196	0·15 0·15	NKT219 NKT222 NKT224	0-88 0-20	OC141 OC169	0.60	7486 7490	0-45
28304 28501	0-75 0-87	BF197 BF861	0.15	NKT251	0-24	OC170 OC171	0.25	, 7491AN	1.00
28703 A A 129	0-62	BFS98	0-28	NKT271 NKT272 NKT273	0-25 0-25	OC200 OC201	0-40	1402	0-75 0-75
AAZ12	0-80	BFX13	0-25	NKT273	0.15	OC202 OC203	0-80		0-80
AAZ13 AC107	0-12 0-37	BFX29 BFX30	0.25	NKT274 NKT275	0.20	0C204	0-40	1 7496	1.00 6.25
AC126 AC127	0-20	BFX35 BFX63	0-98 0-50	NKT277 NKT278 NKT301	0.20	OC205 OC206 OC207	0-75	74100	2.20
AC128 AC187	0.20	BFX84 BFX85	0.25	NKT304	0.76	1 OC460	0-90	; 74110	0-50 0-80
AC188	0-25		0.25	NKT403	0-75 0-55	OC470 OCP71	0-80	74111 74118	1.45
ACY17 ACY18	0-25	BFX88	0-20	NKT678	0.80	ORP12	0-50	74119	1.90 0.60
ACY19 ACY20 ACY21	0-25 0-20		1.00	NKT773	0.25	ORP60 ORP61	0-42	74122	1.85
ACV99	0-20 0-10	BFY17	0-25 0-25		0-88	SI9T SAC40	0.80	74141	2.70 1.00
ACY27 ACY28 ACY39	0-25	BFY19 BFY24	0-25	0A5 0A6	0-20 0-12	SFT308 ST722	0-88	74145 74150	1.50
ACY39	0.20	BFY44	1.00	0.447	0.10	ST7231 SX68	0-68	1 74151	1.10 2.00
ACY40 ACY41 ACY44	0.15 0.15	BFY51	0-20	OA71	0.10	SX631	0.30	1 74155	1.55
ACY44 AD140	0-25 0-50 0-50	BFY52 BFY53	0-22	0A74	0-10 0-10	8X635 8X640	0-40	74157	1.80
AD149 AD161	0-50 0-87	BFY90	0-42		0-10 0-08 0-12	8X641 8X642	0-55	74174	4·10 2·00
AD162	0.87	BSX27	0-50	OA85	0-12 0-15	SX644 SX645	0.75	74175	1.35
AF106 AF114	0-80	BSX76	0.15	OA90	0.08	V15/30P	0.60	74190	1.95
AF115 AF116	0-25 0-25	BSY27	0·18 0·17	OA95	0.07	V30/201 V60/201	0-50	1 74192	1.95
AF117 AF118	0-25	BSY51	0-50	OA200	0.07	V 60/201	0-10	5 74193 74194	2.00 2.20
AF119 AF124	0-20	BSY95	0.18	0A210 0A211	0-25 0-30	XA102	0.18	74195	1.85
AF125	0.20	· `	0-78 0-99	6 OAZ200	0.55	X A 152	0.16	74197	1.20
AF126 AF127	0.17	BTY79,	100R	- OAZ202	0.42	XA161	0.20	- 1100	4-60 4-60
AF139 AF178	0-80 0-55	BTY79,	0.72 400R	OAZ204	0-42	X B101	0-48	Plue in	sockets
AF179 AF180	0.60		1.20	6 OAZ205	0-42	¥ B103	0-10	low p	rofile
AF161	0-45	BY126	0.10	0AZ207	0.47	X B113	0.11	2 , ¹⁴ pm -	0.15
AF186 AFY19	1.18	BY182	0.88	OAZ209	0.82	X B121	0-41		DIL 0-17
AFZ11					-		-		
C	Open	daily 1	to ca	liers :		Fri. 9			
				ansistor	5 · C	Josed S	at. 1	p.m3	μ.m. 7
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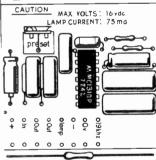
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A complete set of parts from Jermyn to build a stereo decoder module that will convert your existing monotuner for stereo reception whilst maintaining a high standard of reproduction.

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Practical Electronics April 1973





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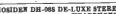


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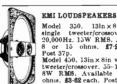
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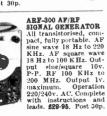
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FASHIONS IN BUILDING

A s a constructors' magazine PRACTICAL ELECTRONICS is naturally very much concerned with building methods and materials. In its fairly short history, electronics has evolved through three distinct periods represented by different fashions in constructional techniques. First was the wood or original "breadboard" era; then the metal era dominated by the box-like chassis; now the plastics era is here with s.r.b.p. board (in some form or another) providing the main platform for the assembly of circuit components.

In many modern designs metalwork is no longer an essential part of the structure carrying the circuit components. Frequently, metalwork is used in a subservient role, merely to enclose or protect an electronic assembly which exists as a more or less self-contained entity built upon a piece of laminated plastics board.

The "plastics era" dawned soon after the arrival of the transistor. Right at the outset of this momentous technological event, industry was able to accommodate this newcomer by adopting printed circuit techniques. These techniques were already well established and in use with miniature valves. While the printed circuit was an ideal technique for mass production of electronic assemblies, it was not so ideal for the private constructor and his "one-off's". So when transistors became available to the individual, improvisation was called for, and a period of great inventiveness ensued. Many varied (and some quite unexpected) building techniques were tried out.

As a start, existing standard items such as component group boards and tag strips were commonly pressed into service as a platform for a transistorised circuit. Assemblies of varying degrees of elegance were built on odd scraps of s.r.b.p. laminate board, hardboard, and even cardboard. The arrival of perforated s.r.b.p. board helped towards a tidier form of construction and eliminated the drudgery of drilling countless holes. However, there was no universally adopted method for home construction until, some 12 years after the first transistor, there appeared in this country the first purpose-designed proprietary printed wiring board. Like many brilliant and successful ideas, this product was, in essence, beautifully simple and-after the event-so obvious. In due course this printed wiring board, though of course initially conceived with the professional user in mind, was to prove the answer to most private constructors' needs, and in time it rationalised the construction of electronic circuits.

PRACTICAL ELECTRONICS played not an insignificant part in bringing this constructional method to the attention of the amateur. This particular board was introduced to constructors in the very first issue of this magazine, and subsequently has been used in the majority of our projects.

Though very popular, the printed wiring board has no monopoly however, and the constructor has a fair choice of alternative methods, including home-made printed circuits. But practically all methods used today are based on the plastics board, the indispensable material which provides the foundations for modern electronic assemblies.—F.E.B. Editor F. E. BENNETT

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PE Sound Synthesiser 3 VOLTAGE CONTROLLED OSCILLATORS and INVERTER

By G.D.SHAW

T HIS month the voltage controlled oscillator and voltage inverter will be described as well as details for assembling them.

THE VOLTAGE CONTROLLED OSCILLATOR

Perhaps the most important reason for the employment of a voltage controlled oscillator lies in the resultant ability of the oscillator to produce tone patterns by application of varying voltages to its control input. If these voltages are derived from what is essentially another oscillator, or series of oscillators, running at ultra low frequency, then the performance of the tone generating oscillator becomes quite automatic and dependent only on the continued operation of the programming devices.

The oscillators in the Synthesiser are based on the operational linear integrator and the circuit is shown in Fig. 3.1. In this arrangement IC1 acts as the integrator while IC2 is connected as a comparator and serves to switch the direction of integration.

The integrator programming signal is applied across the diode bridge D1-D4 and it is important that the polarities are maintained as shown.

CIRCUIT ACTION

To describe the circuit action assume that the comparator is sitting at its positive saturation level then diodes D1 and D3 in the integrator input bridge are reverse biased. There is a current flow into the integrator summing junction through R1, D2 and similarly a current flow away from the bridge through D4, R2, shown by solid arrows, so that the integrator begins to ramp negatively. The negative excursion of the integrator output voltage will continue until the current driven through R5 is equal to or greater than the current driven through R4 as a result of the output voltage of the compartor. At this time the voltage at point P will go negative and the comparator will switch rapidly to its negative saturation level.

Under these conditions diodes D2 and D4 in the integrator input bridge are reverse biased and current flows are established as shown by the dotted arrows. In the case of the current flow away from the integrator summing junction, this causes the integrator to ramp positively.

WAVESHAPES DEVELOPED

Providing that R2 is the same value as R1 and both polarities across the input bridge are at the same potential then the rate of change of integrator



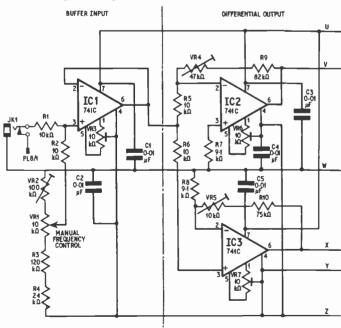
INVERTER

output voltage is the same as before and the result is a symmetrical triangular waveform appearing at point Q. The oscillogram of Fig. 3.1 shows the phase relationship between the triangular waveform generated by the integrator and the switching waveform generated by the comparator at point R in the circuit.

When the integrator output voltage is again equal to or greater than the level of positive feedback set by R4 the comparator switches back to its positive saturation level and the cycle repeats.

FREQUENCY CONTROL

Consideration of the foregoing reveals that R4 actually plays a part in the determination of fre-



quency by setting the point at which the integrator output causes the comparator to switch.

Lowering the value of this component has the effect of increasing the level of positive feedback to the comparator thereby requiring a higher integrator output voltage to switch the comparator and thus lowering the frequency of operation of the integrator.

Conversely, if the value of R4 is increased the overall frequency of operation is also increased.

PRACTICAL V.C.O.

The circuit shown in Fig. 3.2 is the three stage prototype v.c.o. arrangement. Starting from the output end, the third stage is a practical form of the oscillator shown schematically in Fig. 3.1. The second stage consists of two operational amplifiers arranged to provide a differential output across the oscillator input bridge. This particular stage is necessary since, in order to attain the full frequency range, the oscillator requires a drive potential greater than the individual power supply rails can provide.

The first stage of the circuit is a buffer/follower which serves to reduce the current drive required from the control source and which also provides a test-bed on which to try out various forms of circuit response without the necessity of disturbing the settings of the oscillator and differential driver. The type of input stage used in the v.c.o. is of some importance since it has a bearing, not only on the performance of the oscillator as a whole, but also on the design and operation of other circuits in the synthesiser. The response of the input stage may therefore be either linear or logarithmic and there are advantages and disadvantages attached to both methods.

LOGARITHMIC OSCILLATORS

Most commercially available synthesisers use logarithmic v.c.o.s in which the slope of the response

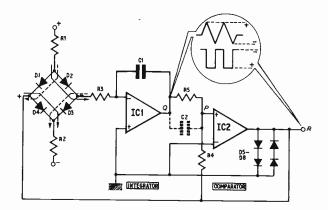


Fig. 3.1. Basic voltage controlled oscillator. Oscillogram shows phase relation between integrator and comparator outputs. The inclusion of the capacitor shown dotted linearises the input voltage/frequency relationship.

is adjusted so that equal increments of input voltage raise the frequency of oscillation by one semitone.

A typical response curve is shown in Fig. 3.3. This has the distinct advantage that if, say, three oscillators are programmed simultaneously by the same control voltage, two of the oscillators may be manually offset by fixed multiples of the semitonal voltage increment so that the effect of the mixed oscillator output is that of producing a chord by the depression of only one key.

The arrangement of having equal voltage increments per semitone also allows for a simplification in the construction of the keyboard divider network and some commercial instruments use a series chain of equal value resistors with a form of "tuning" control which varies the voltage across the chain.

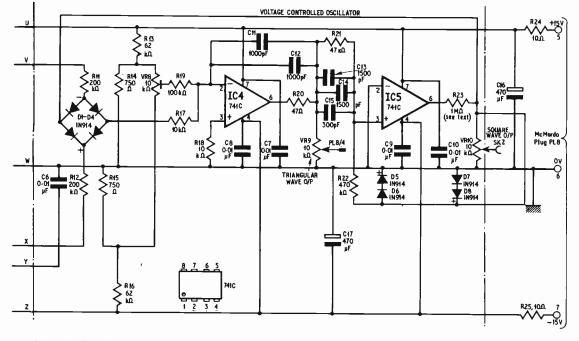


Fig. 3.2. Circuit diagram of the three stage voltage controlled oscillator

Practical Electronics April 1973

LINEAR V.C.O.'s COMPARED

The oscillators in this Synthesiser are arranged with an input stage having a linear performance such that the overall response is as shown in Fig. 3.4.

The resulting loss of the ability to play "chords" was not considered a disadvantage when weighed against the advantages of simplification in building and setting up. Furthermore, the use of linear characteristics in the oscillators provides greater justification for the use of a parallel divider network in the keyboard which, although rather more complex than the series arrangement, means that the accuracy of each semitone is dependent only on the accuracy and stability of its own resistors and not upon the remainder of the chain.

The overall performance of the oscillator, however, is solely dependent upon the response characteristic of the buffer/follower stage and it will be noted that space has been left on circuit board B (Fig. 3.6) for the benefit of constructors who may wish to try out their own ideas of logarithmic response.

The SN76502 manufactured by Texas Instruments is a logarithmic amplifier in integrated circuit form.

MAJOR COMPONENTS

The estimated total cost of this project is around £200. Obviously this figure can be reduced if bulk purchase of components which will appear in quantity is made. To make this possible, components in excess of 12 are listed below.

Resistors	Quantity
10k Ω	52
33k Ω	12
All 5% ½ watt carbon	
5·1kΩ	13
7·5k Ω	36
10k Ω	15
All 2% ½ watt metal oxide	
Potentiometers	Quantity
10kΩ carbon linear	19

10K12 carbon linear	19
All 25mm dia. midget moulded carbon	types
10kΩ carbon linear horizontal presets	12
100Ω linear horizontal Cermet presets	53
10k Ω linear horizontal Cermet presets	21
Integrated Circuits	Quantity
741C 8 pin D.I.L.	56
Diodes	Quantity
1 N914	39
1SJ50	14
Capacitors	Quantity
470μF elect. 25V	12
0·01µF polyester	46
Sockets	Quantity
3-5mm miniature jack sockets	15
2mm miniature sockets	48

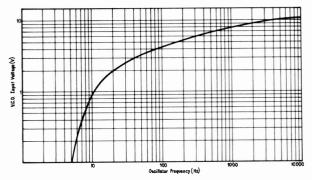


Fig. 3.3. Logarithmic response curve showing the positive exponential relationship obtained when control voltage required is IV/octave

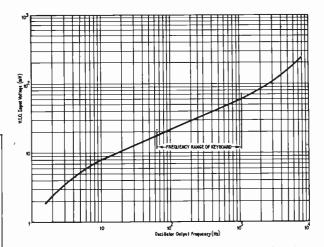


Fig. 3.4. Linear response curve of v.c.o. showing frequency range of keyboard

The advantage of this device is that its response slope may be varied by adjustment of one external component so that performance matching becomes a relatively simple matter.

BUILDING THE OSCILLATOR

Due to the restricted space in the finished module construction should start by assembly and wiring of all the components on to the front panel before the panel is mounted to the circuit board support plate. Figs. 3.5 and 3.6 give the front panel drilling details and component layout. The leads from the controls should be formed into a harness which passes down the centre of the panel between the potentiometers as shown, those for routing to the circuit boards being about ten inches long.

Next mount the McMurdo plug to the rear of the circuit board support plate complete with its wire leads already soldered into position. Fit the eight stand-off supports to the plate—transipillars are recommended but six B.A. screws with metallic spacers may be used providing that these are isolated from the conducting strips on the circuit boards.

The front panel should now be fixed to the circuit board support plate using a 4B.A. countersunk screw and nut in the upper hole, and the locking rod and bush in the lower one. If the assembly seems to be

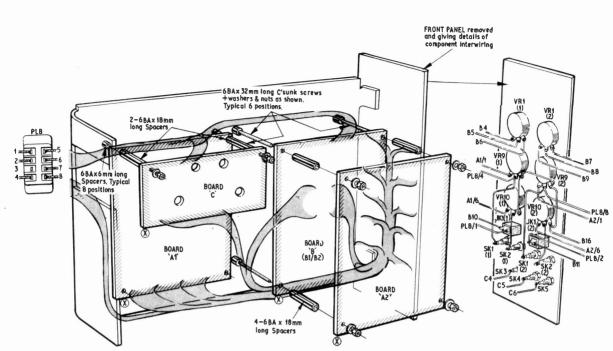


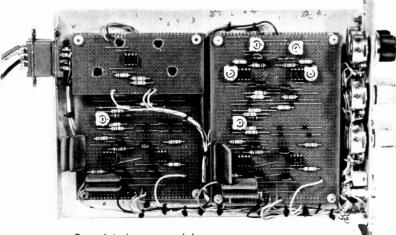
Fig. 3.5. Front panel component assembly and wiring with details of mounting and disposition of boards on the module support plate. The small ringed X at the board edges indicates orientation. (See board details)

on the slack side this may be corrected by fitting a thin steel washer between the bush and lug on the circuit board support plate.

It is useful, at this stage, to make up a jumper lead carrying power supplies from the main busbars so that modules may be tested and set up outside the main frame assembly. The lead should be about 24in (61 cms) in length terminated at one end by a McMurdo plug and at the other by a McMurdo socket wired to match the power supply outputs.

Figs. 3.7 and 3.8 show the circuit board layouts for the oscillator. Board A carries the differential output stage together with the oscillator itself and two of these boards are required.

Board B carries the buffer input stages and power supply decoupling stages for both the other boards.



Completed v.c.o module Practical Electronics April 1973

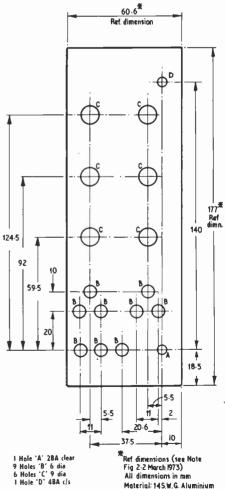


Fig. 3.6. Drilling module front panel

details for v.c.o.

BOARD B

The next stage of construction covers assembly of the buffer input stage and power supply decoupling Board B.1 Fig. 3.7 shows the recommended layout. Wiring of the completed board into the support frame is simplified if single ended Veropins are inserted into the boards at the indicated positions of the lead out wires.

Mount Board B to the support plate adjacent to the front panel and couple up the leads to the power supply, VR1 (manual frequency control) and external input sockets. The leads to Boards A may be omitted at this stage.

COMPONENTS . . .

VOLTAGE CONTROLLED OSCILLATOR (2 REQUIRED)						
Resisto	rs.					
R1	10k Ω	R13	62 kΩ			
R2	10kΩ	R14	750 Ω			
R3	120kΩ	R15	750 Ω			
R4	24kΩ	R16	62 k Ω			
R5	10kΩ	R17	10k Ω			
R6	10k Ω	R18	10kΩ			
R7	9·1kΩ	R19	100kΩ			
R8	9·1kΩ	R20	47 Ω			
R9	82kΩ	R21	47k Ω			
R10	75kΩ	R22	470k Ω			
R11	200k Ω	R23	$1M\Omega$ (see text)			
R12	200k Ω	R24-R25	10Ω (2 off)			
All 2%	🛓 watt metal o	oxide				
Capacit	ors					
C1-C1	•	lyester (10 off)				
C11-C	12 1,000pF Si	lver Mica (2 of	Ť)			
C13-C	14 1,500pF Si	lver Mica (2 of	Ť)			
C15	300pF Silv	er Mica				
C16-C	17 470µFeleo	:t. 25V (2 off)				
Diodes						
D1-D8	1N914 (8 off)				
Potenti	ometers					
VR1	$10k\Omega$ carbon	log				
VR2	100 Ω horizon	tal preset 👌				
VR3	10k Ω horizon	tal preset	*			
VR4	47k Ω horizon	tal preset	miniature			
VR5	$10k\Omega$ horizon	car product /	cermet			
VR6	10k Ω horizon	tal preset	types			
VR7	$10k\Omega$ horizon	tal preset				
VR8	10k Ω horizon	tal preset				
VR9	10k Ω midget	moulded carb	on linear			
VR10	10k Ω midget	moulded carb	on linear			
Integrat	ed Circuits					
		duration that of	a)			

IC1-IC5 741C 8 pin dual-in-line (5 off)

Miscellaneous

SK1—3-5mm jack socket, SK2–SK32mm miniature socket (2 off) 0-1in matrix Veroboards as required.

CHECK-OUT

Set VR3 to mid position and VR2 to the minimum position and attach the jumper lead. With the power supply switched on and VR1 at minimum position measure the voltage at VR1 wiper. Adjust VR2 on both drivers so that voltages are exactly the same.

The value is not critical at this stage but is preferably in the range -5mV to -10mV. Measure the output voltage of both drivers and adjust VR3 until it is equal to whatever voltage has been set on the wipers of VR1.

Connect a temporary link between the external input and ground on both drivers. The purpose of these links is to simulate a zero-voltage prewired programming connection and they will be removed on completion of the setting up of the oscillators. Finally, set VR1 to its maximum position and measure the voltage at the sliders. This should be about -750 mV, depending on the actual potential of the power supply rails, any discrepancy between the two readings being corrected by adjustment of the values of R3 and/or R4.

BOARD A: ASSEMBLY AND CHECK-OUT

Assembly of Board A should commence with the differential output stage which should be constructed up to and including R11 and R12. This stage should now be set up before proceeding with the construction of the oscillator.

Make temporary power supply connections from Board B, attach an input lead to the differential output stage and connect this directly to ground. With VR4 and VR5 at their maximum settings and VR6 and VR7 at their mid positions switch on.

Monitor the output voltages of both halves of the stage and adjust VR6 so that the output of IC2 reads +5mV and VR7 so that the output of IC3 reads -5mV. Now reconnect the input of the differential stage to the output of the driver from which the power supply is being taken and set the output voltage of the driver to -25mV by means of VR1. Monitor the outputs of IC2 and IC3 and adjust

Monitor the outputs of IC2 and IC3 and adjust VR4 and VR5 until these read +255mV and -255mV respectively. Repeat the measurements at various settings of VR1 to ensure that the gain of each half of the stage is linear at \times 10 throughout the working range. Remember that the actual readings should be, in the case of IC2, + [5mV + (10 \times driver output voltage)] and in the case of IC3, - [5mV + (10 \times driver output voltage)].

Having set the gain and offset of the differential output stage the assembly of the oscillator section may now be completed (Fig. 3.8).

CHOICE OF CAPACITOR

The type of capacitor used in the integrator is of some importance as far as frequency stability is concerned and it is best to use a type having low leakage and as low a value of inductance as possible. Silver mica is thus the best choice and the value shown may be made up of two or more parallel wired capacitors.

R23 serves to limit the current output of the comparator. With this omitted the comparator has only the forward resistance of D5-8 between its output and ground and, although IC5 is capable of handling the current involved, this means that a substantial ripple will be present on the oscillator power supply rails and could possibly be transmitted through to

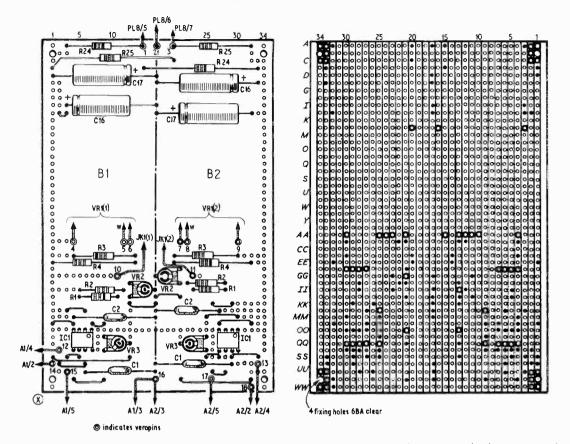
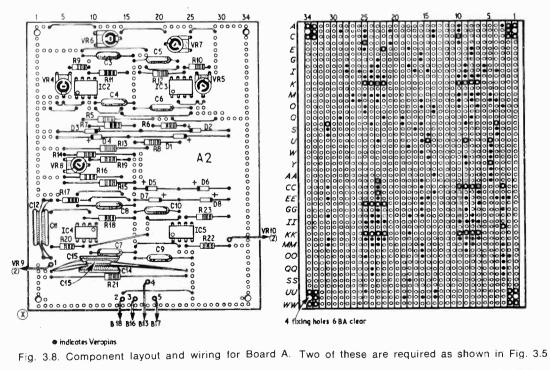


Fig. 3.7. Component layout and wiring for Board B. Since two v.c.o.'s are required, components for each are arranged in board areas B1 and B2



the main bus-bars. Thus, where it is intended to use the comparator square wave output as a signal source the value of R23 should be 2.2 kilohms, that is, sufficient to reduce the ripple to an acceptable level. When the square wave output is not to be used, such as in the keyboard oscillators, the value may be increased to 1 Megohm to reduce ripple to negligible proportions. The inclusion of this resistor will however reduce the triangular wave voltage swing to 200mV p-p and limit the maximum frequency of the oscillator to about 8.3kHz.

R13 to R16 and VR8 form a divider network which provides a value of bias current to the summing junction of the integrator.

MOUNTING THE A AND B BOARDS

The completed A boards should be mounted on the support plate such that one is immediately

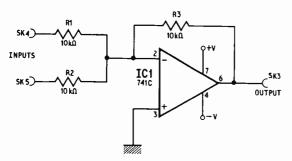


Fig. 3.9. Circuit diagram of voltage inverter

COMPONENTS . . .

INVERTER

Resistors

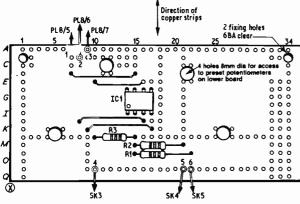
R1-R3 10k Ω (3 off)

Integrated Circuit

IC1-741C 8 pin D.I.L.

Miscellaneous

SK1-SK3 2mm miniature sockets (3 off) 0.1in matrix Veroboard as required



Copper strips broken at holes G14, 15, 16, 17

Fig. 3.10. Inverter component Board C layout and wiring

adjacent to the McMurdo plug and the other directly above Board B. It is best to mount and set-up the oscillator boards one at a time. When a board has been fully connected, set VR8 and VR1 to their mid positions and switch on the power supply. Observe the triangular waveform on the oscilloscope —the frequency of oscillation should be about 7kHz.

Gradually reduce the setting of VR1 until the waveform begins to exhibit marked signs of assymmetry. At this point adjust the setting of VR8 *with great care* to restore the symmetry, this latter operation also being seen to cause an increase in the frequency.

Continue reducing the setting of VR1, adjusting VR8 as necessary, until VR1 is at its minimum setting and the output waveform is symmetrical.

At very low frequencies the setting of VR8 is extremely critical, too large a shift in either direction causing IC4 to saturate. If this happens, VR1 should be set to its mid position again and the various steps repeated.

With VR1 in its minimum position final setting of the very low frequency end of the range is accomplished by adjustment of VR2 in conjunction with VR8 as before. If IC4 saturates at or before minimum setting of VR1 the setting of VR2 will have to be increased.

Very low frequency instability can be a problem with this type of oscillator and although it can be made to operate at less than 1Hz with the component values given it is best to set the minimum operating frequency to about 5Hz.

MATCHING THE OSCILLATORS

If the component values and tolerances specified have been adhered to, comparison of performance between both oscillators will show that the input voltage/frequency relationship is substantially similar, any differences in performance characteristic being due to tolerance variations in the components.

Extreme accuracy in the matching of oscillators is not necessary since linear response is involved.

INVERTER

Little need be said concerning the assembly of the voltage inverter which is essentially an inverting unity gain amplifier of the simplest kind. The circuit is shown in Fig. 3.9 while the recommended circuit board layout is shown in Fig. 3.10.

The completed board should be mounted directly over the A board furthest from the front panel.

USING THE MODULE

On completion of the whole module use the voltage inverter to investigate the effects of mixing triangular and square waves at varying frequencies.

The output may be fed to the high level input of most power amplifiers, but bear in mind that the output will be equal to the sum of the voltage swings at the inputs.

Additionally it is possible to carry out some simple experiments in frequency modulation by setting one of the oscillators to modulate the other. A low amplitude modulation at about 7Hz produces a true vibrato to the tone of the modulated oscillator whilst varying the amplitude and frequency of modulation can produce some strange, even bizarre effects.

Next month: the ramp generators and input amplifiers are described.



By J. S. GODDARD

THIS article describes a d.c. power supply unit with the unusual feature of being contained in a 13A flat pin mains plug. It will supply 60mA at 9V suitable for radio, cassette or record players.

UNIT ADVANTAGES

One of the disadvantages of conventional battery eliminators is that you are left with a box which must either be strung between plug and unit or replace the batteries in the battery compartment.

This design overcomes both problems. The lead from the mains plug goes directly to the unit and plugs in with a simple jack plug. The batteries of the unit are left in place but simply disconnected when the jack plug is attached. The batteries are reconnected when the plug is removed. The project becomes even easier if the unit has a socket for a battery eleminator.

CIRCUIT

The circuit diagram of the battery eliminator is given in Fig. 1 together with suitable battery cut-out circuit in cases where a socket is not available on the unit to be supplied.

The transformer has a 6-0-6V secondary with the centre tap unconnected. This feeds a four diode bridge rectifier, the output being smoothed by the reservoir capacitor C1 and R2. The Zener diode D5 provides a final 9V regulated output.

MODIFYING THE PLUG

The plug used for housing the circuit components is an Ever-Ready type which has to be modified. This is accomplished by cutting a f_{0} in step at the bottom rear of the plug as in Fig. 2. A piece of $1\frac{1}{8}$ in $\times 1\frac{1}{4}$ in $\times \frac{1}{9}$ in hardboard is cut to form a new base for the plug. This is Araldited into place ensuring that the ends of the plug are upright and parallel.

A $\frac{1}{16}$ in hole is drilled and countersunk in the upper half of the plug directly above the brass screw insert for the neon LP1.

For the d.c. leadout pair a $\frac{1}{6}$ in hole is drilled $\frac{3}{2}$ in up from the base at the centre rear of the plug.

ASSEMBLING THE COMPONENTS

The components may now be mounted in the expanded plug. First, the transformer is loosely held in position by two 6 B.A. screws.

The mains neon is now positioned and connected to the plug terminals together with the transformer primary windings.

With the capacitor and diodes in place the transformer is tightened down. The output lead is connected across the Zener diode after R2 has been added in series, in the positive line, as shown in the circuit diagram.

With all the components mounted in place care should be taken to see that none are touching the mains pins or their screws. If necessary more room can be made by discarding the screws on the back of the mains pins and soldering instead of clamping. Once all appears to be correct inside a cover has to be constructed for the plug.

COMPONENTS . . .

Resistors

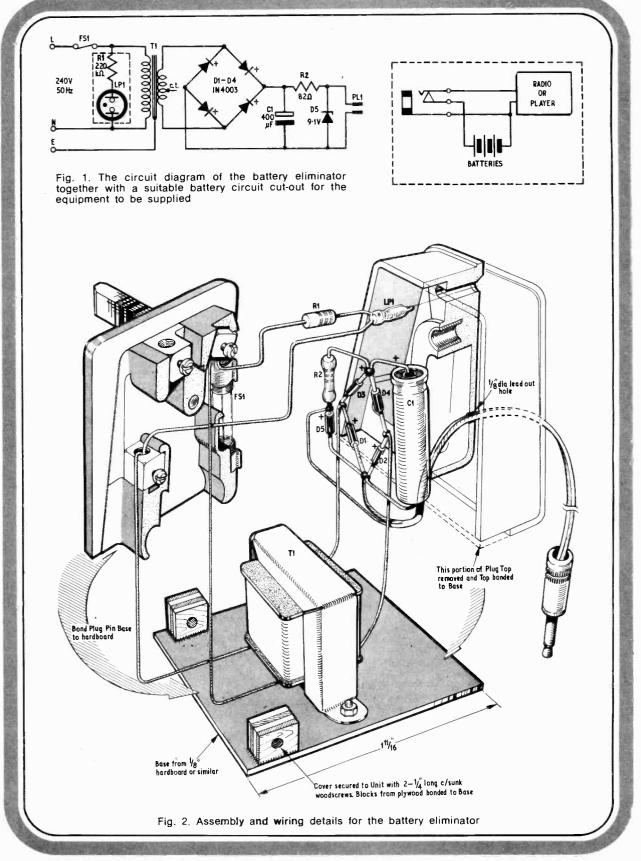
- R1 220k $\Omega \frac{1}{2}$ W carbon R2 82 $\Omega \frac{1}{2}$ watt 10% carbon
- Capacitor

C1 400µF 10V elect.

- Diodes
 - D1-D4 IN4003 (4 off)
 - D5 9-1V 400mW Zener
- Transformer
 - T1 Eagle miniature mains transformer 240V primary 6-0-6V secondary at 100mA.

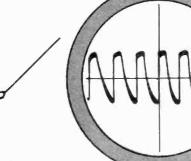
Miscellaneous

13A fused mains plug (Ever Ready Type 7032), LP1 mains neon, 1∦in × 1≹in × ∦in hardboard, ‡in 6 B.A. countersunk screws (2 off), ∦in self tapping (2 off), FS1 fuse to suit equipment. PL1 3.5mm jack plug.



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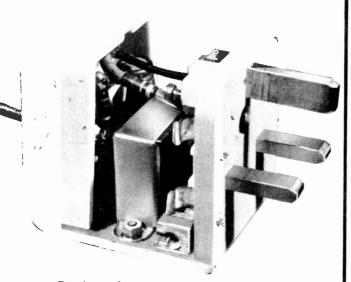
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Good results can be obtained by using good quality card about 16 in thick. The card is bent to fit around the top and two sides of the plug snugly. The inside of the card may be scored with a knife to make it bend more easily. With the card bent around the plug mark off, with a pencil, the exact dimensions. When cut to shape check to ensure a good fit, if necessary a former may be made to hold the card in the required shape.

The cover is held onto the plug by two self tapping screws. These screws tighten into $\frac{1}{16}$ in blocks of plywood about $\frac{3}{2}$ in square. The blocks must be drilled to accept the screws and glued in the bottom front of the plug as shown.

Now is the time to fill any gaps between plug and base. A plastic filler is used, which can be sandpapered smooth when dry. The cover and base may be painted to match the plug, sprayed paint gives good results on a suitable primer.

CONNECTING THE UNIT

Consideration now has to be given to the method of connecting the battery eliminator to the unit which it will power. A number of radio and cassette players on the market have facilities for battery eliminators, and in this case it is only necessary to obtain the correct plug. If your unit does not have facilities such as this, or you are unable to obtain the plug, the following will serve as an alternative.

A 3.5mm jack plug is connected to the eliminator's outlet lead with the matching socket in the unit. The jack plug is connected to the outlet lead wire with the positive line going to the tip. The socket may now be fitted to the unit, a suitable position must be found to ensure it will not interfere with any internal workings.

With the hole drilled and socket fitted the supply wiring must be adapted to cater for the new facility. The positive lead to the battery compartment must be broken and the jack socket connected in the break. The negative lead goes to the third, contact on the socket as well as the battery compartment.

With the jack plugged into the socket the positive line from battery to unit is broken and connected instead to the outlet of the power supply.

The 400μ F electrolytic capacitor may be difficult to obtain, but good results can still be obtained with a smaller one.



ELECTRONICS IN MUSIC By F. C. Judd Published by Neville Spearman 169 pages, 9in \times 6in. Price £3.15

M^R JUDD has condensed into this book the fruit of many years' experience in electronics. The six main chapter headings cover virtually every aspect of the subject ranging from the application of electronics in the production of music through a survey of electronic musical instruments, the production of synthetic sound and electronic music, the uses of the tape recorder in the field and, finally, a rundown on the parameters involved in the high fidelity reproduction of music.

The text throughout seems designed to guide the reader into this fascinating and ultra-technical subject without once getting bogged down in an excess of detail. Despite this tendency there is sufficient data presented to enable the home constructor to build and experiment with several interesting circuits. The book is well illustrated with sixteen pages of half tone plates and plenty of clear line diagrams and circuits. The author could have perhaps usefully expanded his treatment of the subjects of synthetic sound and electronic music in view of the current high level of interest although the shortfall in this respect does little to mar the overall presentation of the book which is excellent.

"Electronics in Music" is likely to be welcomed enthusiastically by technical and non-technical readers whose interest in the subject matter may be frustrated by the lack of definitive texts.

G.D.S.

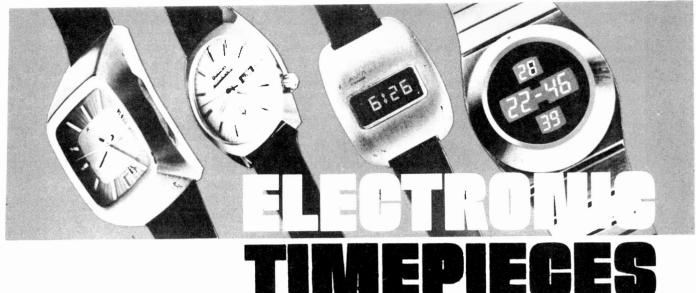
TELEVISION INTERFERENCE MANUAL By B. Priestley, B.Sc., G3JGO Published by Radio Society of Great Britain 92 pages, 148mm × 210mm. Price 80p

TELEVISION interference from s.w. transmitters is something which many amateur radio enthusiasts find very difficult to eliminate. The Radio Society of Great Britain must therefore be congratulated for attempting to bring this problem to the notice of radio hams and for providing many hints on suppression which, if followed, could greatly reduce the annoyance of TV viewers near to a transmitter.

Television interference can arise from many sources and one of the main problems is tracking down the exact cause. Of course, a well-designed transmitter should include effective circuits for suppressing this unwanted output and transmitter design is included in the book. However, even the best transmitter can have a component failure and the book points out that a careful check on meter readings should be kept and any change in performance noted. R. F. injection into the mains and its suppression is also discussed.

This book has a spiral binding so that the pages lie flat on the bench. The manual may be obtained from RSGB Publications, 35 Doughty Street, London, WCIN 2AE, price 90p including postage.

S.R.L.



By J. B. DANCE, M.Sc.

N this final part, quartz crystal controlled watches and clocks are examined together with various time displays.

QUARTZ TIMEPIECES

Quartz crystal piezo-electric oscillators are now well known for their great frequency stability. Although the piezo-electric effect was discovered by J. and P. Currie in 1880, it was not used for frequency control until 1921 by Cady. Natural quartz can be used, but synthetic quartz often gives a better performance.

CLOCKS

Various clocks using quartz crystal oscillators are available. For example, the General Time Company produce "Quartzmatic" clocks using 262,144Hz crystal oscillators with an integrated circuit to reduce the frequency to 64Hz. The Simplex Company produce quartz controlled master time centres for driving a number of clocks in an establishment with an accuracy of two seconds per month.

The Golay Company produce marine chronometers using a 12kHz oscillator which has a stability of 0.005 second per day at constant temperature or 0.1 second per day over the range 4 to 36° C: this clock employs about 29 transistors.

A quartz clock with a digital display is available from Girard-Perregaux; it is mains driven with stand-by battery power and provides an accuracy of 0.02 second per day. The Junghans 750 quartz movement is powered by a 1.5V battery which lasts a year.

QUARTZ CONTROLLED WATCHES

Quartz crystal controlled wrist-watches have been available since April 1971. Special CMOS (Complementary Metal Oxide Silicon) integrated circuits have been developed which consume a current only during the pulses and which are small enough to be fitted into a normal wrist-watch. In many cases a number of manufacturers have pooled their resources to produce quartz watch movements. The quartz crystals used have to be specially aged so that they provide high accuracy at all times. They are normally sealed in a vacuum enclosure.

The first types of quartz wrist-watches to become available to the public employed the "Beta 21" movement developed by the Centre Electronique Horloger S.A. and marketed in various models under many brand names. The quartz crystal oscillator in this movement operates at 8,192Hz. An integrated circuit divides this frequency by a factor of 32 to produce a 256Hz signal. The current consumption averages about 16μ A and the accuracy is about one minute per year.

CYBERNETIC WATCH

The Longines "Ultra-quartz" wrist-watch was first made available on 21st August, 1971. It is especially interesting because it does not contain any integrated circuits, but only a small printed circuit containing miniature electronic components.

The quartz resonator in this watch operates at 9,350Hz and a mechanical vibrator at 170Hz. The signals from the quartz oscillator are used to correct

The Girard-Perregaux quartz watch. The quartz crystal can be seen on the left-hand side, the integrated circuit near the top and the power cell on the bottom right-hand side



the mechanical vibrator 170 times per second. This correction is carried out by a relatively simple circuit employing only 14 transistors, 19 resistors and seven capacitors. The logical deductions made by this circuit are fed to the motor as correction signals. This watch is said to be the first cybernetic watch, since it employs a comparison circuit or "brain".

The vibrator motion is transformed into a rotary motion by means of a pawl system like that of Fig. 6. The toothed wheel rotates once per second. The centre second hand appears to rotate continuously without jumping. The accuracy is about one minute per year.

QUARTZ BALANCE WHEEL WATCH

The " μ -Quartz" or "TS Caliber" watch movement employs an electronically driven balance wheel having four magnets; the exact frequency of this balance wheel (about 4Hz) is controlled by a quartz crystal oscillator. The watch has been developed by B. Golay of Switzerland.

The hair spring fixed to the balance wheel has a special shape which results in the frequency of oscillation being somewhat dependent on the amplitude of movement; the frequency is slightly lower at small amplitudes and vice-versa. This effect is known as the isochronism defect.

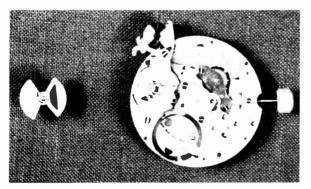
The quartz oscillates at 32,768Hz. This frequency is divided down by part of a CMOS integrated circuit containing some 450 components. The strength of the pulse given to the balance wheel depends on the *phase* of its motion relative to the frequency divided signal from the quartz oscillator.

If the balance wheel is running too fast, the pulses to the coil which drives this wheel will be relatively weak, whereas if the wheel is running too slowly, they will be stronger. Thus the frequency of the balance wheel is stabilised at the, value determined by the signals derived from the quartz oscillator.

If the isochronism defect amounts to 10 seconds per day for each degree of amplitude variation, the balance wheel frequency need only be adjusted to ± 100 seconds per day if an amplitude variation of ± 10 degrees is acceptable.

As in other quartz controlled watches, the regulation is effected by means of a trimmer capacitor which adjusts the exact frequency of the quartz oscillator. In this watch the capacitor is adjustable

The Golay μ -Quartz movement partially dismantled. The magnets can be seen fixed to the balance wheel in the lower part of the photograph, whilst the driving coil is seen above after it has been swung out from the movement. The quartz crystal, which has been removed, is fitted above this coil



Practical Electronics April 1973

in steps which correspond to a change of 0.25 second per day. The accuracy is about one minute per year.

QUARTZ WATCH WITH STEPPING MOTOR

The Girard-Perregaux "250" quartz watch employs a 32,768Hz quartz oscillator. The pulses from the latter are divided by an integrated circuit to produce 0.5Hz pulses. These operate a miniature stepping motor which causes the centre second hand to jump once per second.

QUARTZ WATCH KITS

The Motorola Company has a section which supplies kits of parts to large watch manufacturers. These kits each comprise a 32,768Hz NT cut quartz crystal, a CMOS integrated circuit and a miniature rotary stepping motor. The additional parts required are a power cell, a trimmer capacitor, a conventional watch dial and hands together with gearing to couple the motor to the hands.

The oscillator frequency chosen is a compromise between the size of the oscillator crystal and the current consumption of the integrated circuit. The use of a higher frequency would enable a smaller quartz crystal to be used, but the increased switching frequency results in a greater power consumption by the divider circuit.

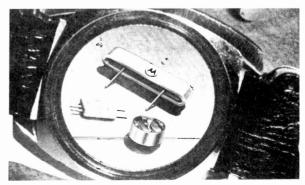
The MC 6061 integrated circuit divides the oscillator frequency by a factor of 65,536 so as to produce 0.5Hz pulses which can drive the motor.

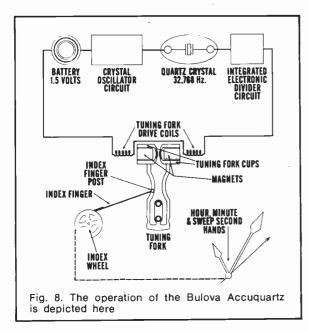
The integrated circuit contains 312 transistors in a six lead ceramic package, but consumes only about 4.5μ A from a 1.3V cell or 5μ A from a 1.5V cell. Motorola use ion implantation techniques to dope the semiconductor material used in their integrated circuits.

The 6mm diameter motor takes a mean current of about 7.2μ A at 1.3V or 8.3μ A at 1.5V. The 0.5Hz pulses from the integrated circuit have an amplitude of about 1V and a duration of about 31.25ms, successive pulses being of opposite polarity and separated by one second.

The motor rotates by 180 degrees at intervals of one second, all movements being in the same direction. It has a resistance of about 5 kilohms and contains about 50 metres of wire of a diameter about one-tenth of that of a human hair.

The three parts of the Motorola kit depicted inside an empty watch case. The quartz crystal is shown at the top, the integrated circuit on the left and the stepping motor on the lower right-hand side





QUARTZ TUNING FORK WATCHES

The new Bulova "Accuquartz" watch is especially interesting because it contains a quartz oscillator which controls a tuning fork movement. This watch was introduced in the U.S.A. in December 1971 and became available in Europe towards the end of 1972 at prices from £115. It is much thinner than many other quartz models (including an earlier "Accuquartz" model which used the "Beta 21" movement). The new "Accuquartz" range for men and women display the day of the week and the date in addition to the time.

The "Accuquartz" crystal oscillates at 32,768Hz. This frequency is divided by an "Intersil" CMOS integrated circuit containing 126 transistors, etc. The tuning fork oscillates at 3411Hz, this being one-third of the frequency 1,024Hz. See Fig. 8.

The Bulova Accuquartz is shown in the foreground together with a much thicker Accuquartz model using the CHE movement



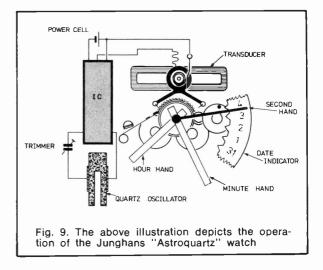
In this watch the tuning fork mechanism advances the gearing 341¹ times per second by the same type of mechanism as used in the Bulova "Accutron" range. Thus the centre second hand appears to move continuously instead of jumping once per second as in some types of watch.

The "Accuquartz" has an accuracy of about 1 to 2 seconds per week.

THE ASTROQUARTZ

The Junghans "Astroquartz" watch is said to be the smallest quartz watch being manufactured. It employs a 32,768Hz quartz oscillator, but the quartz crystal used is unusual in that it is in the shape of a tuning fork, the prongs of which vibrate like an ordinary tuning fork but at a much higher frequency.

As illustrated in Fig. 9, an integrated circuit acts as oscillator and frequency divider. The 15 cascaded binary stages divide the pulse rate by 2^{15} to produce one output pulse per second. The size of the integrated circuit is only 1.6×2.1 mm.



The output pulses from this circuit drive an electro-magnetic transducer. The pulses are applied to the coil which turns in a strong magnetic field. The escapement fitted to the axis of this coil engages and turns a wheel with 60 teeth to which a centre second hand is fitted.

THE MEGAQUARTZ

The "Megaquartz" watch is probably the most accurate wrist-watch yet designed, although it is being produced only in small quantities. It has been designed by the Batelle Institute in collaboration with the Omega Watch Company. The accuracy is about 1 second per month.

The main feature of this watch is the use of a circular AT cut quartz crystal oscillating in a shearing mode at 2,359,296Hz—far higher than in any other design. An integrated circuit frequency divider is used.

Omega also offer a quartz watch which has an 8,192Hz oscillator. This frequency is divided by a factor of 32 to produce 256Hz pulses which drive an electro-magnetic motor. The accuracy is about 1 minute per year.





D1075 Wireless Intercom DIO75 Wireless Intercom The grat merit of wireless intercoms is that the grat merit of wireless intercoms providing the stations are on the same can be up to a distance of § of a mile providing can be up to a distance of § of a mile providing that one up to a distance of § of a mile providing can be up to a distance of § of a mile providing that one up to a distance of § of a mile providing that one up to a distance of § of a mile providing that one up to a distance of § of a mile providing that one up to a distance of § of a mile providing that one up to a distance of § of a mile providing that is can be used and the same creuit. Solid state model D1075 is fully une control and a pilot light. The fawn moulded cabinets can be desk located or wall mounted and are supplied already fitted with Microphone: Dynamic S5mm. Power Output: 120mW. Size: 98 - 40 130mm. Printed Circuit: 3 transistors. I diode. **£11:60**

AUTO

£11.60

SOLID STATE TACHOMETER

Functionally styled for under or over dashboard installation, this over dashboard installation, this electronic tachometer fits all 4-cycle, 4-cylinder, or 2-cycle, 2-cylinder 12V vehicles. Negative or positive earth. Calibrated white on black 0-8,000 r.p.m. in 100 r.p.m. divisions together with setable "danger" line, simple installation-2 screws 4 wires 80mm (3ind dia 2 screws, 4 wires. 80mm (3in) dia. dial, 50mm deep. On adjustable angle bracket. Sealed black crackle finish £6.86



AUTO BURGLAR ALARM PLUS "POP-OUT" CIGARETTE LIGHTER

SPECIAL OFFER !

Designed for easy installation on any car (whether 6 or 12V) this device activates the horn when a theft is attempted of equipment or personal belongings. This neat unit reacts when the vehicle is disturbed or rocked and continues its when the vehicle is disturbed or rocked and conti warning for 15 sec. after tampering. The sensitivit device is adjustable and controlled by a separate ON/OFF panel which can be located wherever convenient. Supplied with connecting wires and screws in attractive bubble pack, containing isstal-The sensitivity of the lation instructions and diagrams. 150 20mm plus panel $65 \times 45 \times 20$ mm,

£2.10 FOR BOTH



FANTAVOX STEREO LOUDSPEAKER SYSTEM These high quality speaker enclosures are made of tough black moulded plastic and have been designed for fitting on to almost any vehicle surface. The smart louvred fronts are silver trimmed and house heavy duty Sin (125mm) ceramic loudspeakers rated at 3/5 watts. 8 ohms impedance. Already wired with generous length connecting leads and supplied in packs of speaker pairs complete with fixing screws. Each cabinet measures 190 × 105 × 165mm. VEADER CONTROL Weight: 0.55 kg.

1052 FADER CONTROL Neat, custom-made appearance slide fader control for balance of front and rear speaker volume. Simulated wood finish panel which can be quickly fitted below car dash. Supplied with generous connecting cable and fitting screws. Will suit 4, 8, 16 ohm installations. 100 × 38 × 30mm (including knob but excluding fitting bracket). All for £4.70



420ES MICROSCOPE

An extremely modestly priced yet efficient microscope capable of magnification up to 750 times with clear sharp images. This model is of the self-illuminating (ype and incorporates an easily rotable position turret magnifying lens with rack and pinion focusing. The crackle black metal body houses the batteries for adjustable illumination. Packed in carton with built-in carrying handle and full notes for user. A sample slide also provided. IOSmm at base: 180mm high. Weight: 0-40 kg.



D1019 "Doorphone" with

Metal Unit

G5555 PROFESSIONAL STEREO HEADPHONE

Lightweight materials are skilfully used in the construction of this model in black crackle moulding and kid-soft leathercloth with con-trasting bright metal. Each ear pad houses a highly efficient 60mm reproducer unit and for compared to the second state of the second transmission multiple second state of the second transmission of the second state state of the second state of the features ear muffs removable for cleaning. self-coiled lead plug fitted. 10

Frequency Response: 20-20,000Hz. Impedance 4-16 ohms. Sensitivity: 110dB. Power: 0.5W Weight: 0.39kg. £9.25

Three transistor solid state two-way intercom

system with specially engineered weatherproof slave unit in heavy gauge metal. Sensible design features include rain protective speaker louvres,

simple push-pull button, internal socket connec-

simple push-pull button, internal socket connec-ting lead and removable back plate for wall and door panel mounting. Master unit in high impact white moulding has complementary silver "pinhole" grille and silver/black panels with ON/OFF volume control and push-to-talk witch. Gomm duramic repeated microbace

"SPRITE" LIGHTWEIGHT STEREO HEADPHONE

An outstanding achievement following lengthy development by one of the world's leading audio manufacturers, the T.T.C. "Sprite" offers the following specification: Extreme lightness (only 150 grammes) (50z); Instant waring adjustment with sliding ear-pieces and flexible headband; Highly efficient Mylar reproducer units; Removable, washable foam padded ear muffs;

3-metre lightweight lead with stereo plug fitted. Frequency Response: 30-13,000Hz. Power: 0.2W

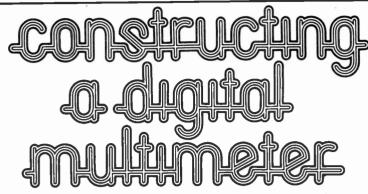
Sensitivity: 105dB. Impedance: 4-16 ohms. £2.25 Weight: 0.15kg.

DFI00 MICROPHONE

Bijou sized model in matt silver finish with machined capping to insert housing and supplied with unique pocker/lapel clip which also doubles as a desk support. Supplied with lavalier cord, 2 metre lead fitted 3 Smm moulded plug and packed in the latest style click-fast manufactured from smart durable padded case plastic.

Impedance: 200 ohms. Sensitivity: 82 Frequency: 100-9,000Hz. Size: 13mm dia. 82dB. 92mm £3-50





 - exclusive Wireless World design in the April & May issues See full construction details of the versatile multiple measurement meter which was first described in our March issue. Intended for both amateur and professional use, the design – based on integrated circuits – is arranged so that you can build either the whole instrument or just the particular measurement facilities you require. Measurements are shown in a "window" on a four digit numerical display.
 Survey of the Compatibility of Audio Magnetic Tapes. With the wide variety of tapes available, it is desirable to establish the compatibility of one

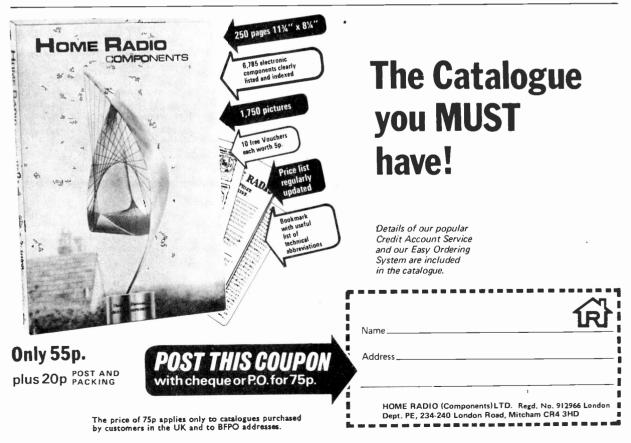
type or brand against any other for a particular recording machine. Detailed tests have been made and the results interpreted to produce a table of interchangeable and compatible products.



The Wireless World digital multimeter will measure : voltage (199.9 millivolts to 199.9 volts, d.c. and a.c.) resistance (1.999k Ω to 1.999M Ω), capacitance (1999pF to 1.999µF), frequency (0 to 5MHz) and time intervals (20 microseconds minimum).

WirelessWorld

APRIL ISSUE On sale now 20p





(Right): the Avia watch which employs a liquid crystal display. This is expected to be available in the U.K. at about £135 soon

(Left): the Swissonic 2000 watch. This displays the date, the hours, minutes and seconds continuously by means of a liquid crystal system



DIGITAL WATCHES

Digital watches which employ no moving parts have just begun to appear on the market. They employ quartz oscillators and provide an accuracy of about one minute per year.

Two forms of display have been employed, namely electroluminescent diodes which provide a red display and liquid crystal displays.

ELECTROLUMINESCENT WATCHES

Watches employing gallium arsenide-phosphide electroluminescent diodes provide a display which shows the time in red digits. Unfortunately the display diodes require so much current that it is not possible for the time to be continuously displayed if the power cells are to have a reasonable life. A button on the watch must therefore be pressed each time the user wishes to read the time. The cell life is dependent on the number of times the time is displayed. The display may have to be shaded with the hand if the ambient light level is high.

The "Pulsar" watch manufactured by the Hamilton Company employs light emitting diodes. The brightness of the display is automatically adjusted to suit ambient lighting levels, although it requires shading from direct sunlight when the display is being read.

Each time the button is pressed, the hours and minutes are displayed for 1.25 seconds, but if the button is held down, the seconds are displayed for as long as it is depressed.

The watch employs a 32,768Hz oscillator and a CMOS integrated circuit containing over 1,200 transistors. It is powered by two silver oxide cells which have a life of over one year under normal use (about 25 time readouts per day).

A slight variation of this watch is offered by the Omega Company as their "Time Computer".

LIQUID CRYSTAL DISPLAYS

The other form of digital display used in watches employs liquid crystals. This type of display requires very little power, since it does not emit light. The liquid crystals simply reflect a different proportion of the incident light in regions where an electric field is applied to them. Thus the display cannot be viewed in the dark. A moderately high ambient light intensity is desirable.

The thickness of the liquid crystal material may be about 0.5mm. The special nematic material is placed between two electrodes like a capacitor, but the electrode nearest the face of the watch must be transparent.

In the absence of any field, the liquid is perfectly clear and transparent, any incident light falling on it being absorbed by a black background. When an electric field is applied by suitably shaped electrodes in certain regions (which are in the shape of the digit to be displayed), the liquid becomes opalescent as the crystals come into mutual alignment. They reflect the incident light back from these regions to the observer.

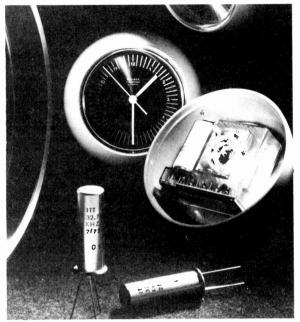
Although watches using liquid crystal displays have the advantage over those using luminescent diode displays in that the digits can be made visible at all times, the life of the present liquid crystal systems seems somewhat doubtful. Even when an alternating voltage is applied, some degradation of the material may occur so that the display gradually becomes less clear. The life should be considerably over one year, but it is too early to estimate it accurately. At least one manufacturer feels that liquid crystals may have an indefinite life if contamination is avoided. The price of replacement units should fall rapidly during the next few years.

THE AVIA WATCH

One watch with a liquid crystal display is marketed by Avia-S.G.T., the liquid crystal system for this watch being produced by the Optel Corporation of the U.S.A. The hours and minutes are continuously displayed, but the seconds are shown by means of two flashing points appearing between the hours and the minutes digits.

The quartz oscillator operates at 32,768Hz. This frequency is divided by a factor of 512 and the 64Hz output operates counters. The latter control the decoders which feed the display.

The 1.5V power cell has a life of 14 months. A circuit is employed to convert the 1.5V from the cell to the 15V required for the decoder-display operation.



The Staiger 2000 quartz crystal controlled clocks. The ITT crystals used are shown at the front

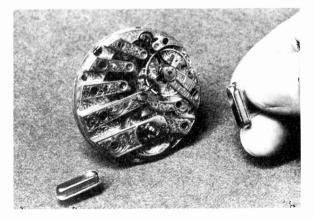
A DETAILED DISPLAY

Another liquid crystal watch has been developed by Texas Instruments, Ebauches S.A. and Longines. The eight character display provides a continuous readout of the day of the month, hours, minutes and seconds. The accuracy is about 1 minute per year. The watch contains two integrated circuits containing about 700 transistors and is powered by two 1:35V mercury cells.

The hour display can be set by an internal switch to provide either a 12 hour or a 24 hour cycle. The indicated time is set by four micro-switches on the back of the watch which alter the seconds, minutes, hours and date respectively.

Another watch with a liquid crystal display has been produced by the Seiko Company; it displays hours, minutes and seconds.

A Geneva lever movement (about 100 years old) from the Science Museum being compared with an ITT quartz crystal designed for use in a watch



CLOCKS USING LIQUID CRYSTALS

A limited number of clocks with liquid crystal digital displays are available, for example, from the Seiko Company. An impressive digital alarm clock (type S1736) has been constructed on a single chip by American Microsystems; it is interfaced with their liquid crystal readout.

ATOMIC CLOCK

In a totally different sphere it may be mentioned that the standard of time is now based on the frequency of radiation emitted between two hyperfine levels of the caesium-133 atom. The second amounts to 9,192,631,770 cycles of this radiation. This definition provides a more accurate measure of this unit than the motion of the earth.

Ebauches S.A. have made precision time centres using caesium atomic clocks which have an error of less than one microsecond per day (corresponding to one second in about three thousand years!).

POWER CELLS

The cells used to drive electronic watches pose many manufacturing problems. Three of the main manufacturers are Union Carbide, Leclanche and, in England, Mallory.

A new area has recently been opened by Mallory at Crawley for the manufacture of special mercury button cells used in watches. Such cells must give satisfactory service for at least one year after a variable period of storage before sale.

Extreme care must be taken to prevent contamination of the materials used in cell manufacture. All air is filtered before it enters the watch cell manufacturing area at Crawley to prevent dust from being sealed in the power cells. Great care must be taken to prevent the possibility of internal leakage of current.

The electrolyte used in watch cells is chosen for the lowest practical seepage rate, since if it escaped from a cell it would probably damage the delicate watch mechanism.

In conclusion it may be mentioned that the tweezers used to fit new cells into watches should be made of a plastic material, since metal tweezers can easily short the cell. Care should be taken to fit new cells in the correct way so that they provide the circuits with a voltage of the correct polarity.

CONCLUSION

We are in the midst of a revolution in watch design. Although no manufacturer has really broken through the price barrier with a moderately priced quartz controlled watch, it may not be too long before one company does so and the "quartz war" will have begun. The developments in the last few years have been very rapid and it is expected that many of the estimated 300 million watches per annum required by 1980 will be electronic ones.

The traditional place of watch making, Switzerland, has played a large part in the development of electronic watches, but the U.S.A. has initiated much of the work.

The normal skills of the watchmaker will be required to attend to watches employing moving parts, but if digital watches become common, the watch repairer may have to have a very elementary knowledge of electronic engineering with microminiature equipment.

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SPACE BUDGET

The United States space agency will have more money to spend this year, 74 million dollars in fact. A total of 3,136 million dollars is set aside for space matters. This amount will cover a number of NASA projects, for example two new projects as well as the programme for space stations and shuttles.

The two new projects are a new kind of satellite for geodesy known as a Terrestrial Reference Satellite, and an advanced version of the *Nimbus* weather satellite to monitor pollution.

The reference satellite, due for launch in 1976, will use laser beams for the measurement of distances between locations on different continents. The accuracy that can be achieved is of the order of a few inches so that small changes of movement of land masses will be detected.

The new Nimbus satellites will monitor both air and ocean pollution. The programme is for the launch of two satellites, one in 1974 and the other in 1976.

The current major projects will continue to be developed, but there will be a phasing out of communications satellite interests. This is because the space agency consider that the viability of these programmes has been proved and the time is now ripe for commercial responsibility for this activity.

The Science Foundation will increase their programme of investigations and some major projects involve visual and radio astronomy. Some 10 million dollars will go to the rail mounted mobile arrays of aerials in New Mexico for the large scale study of distant sources and the detection of signals from any civilisation that may exist in other parts of the Universe.

The visual telescope under construction at the Cerro Tololo inter-American Observatory in Chile, will be given 2.6 million dollars for the completion of the work on what will be the largest optical telescope in the southern hemisphere. The diameter of the mirror is 158 inches and the site offers spectacular advantages over other places for useful viewing time.

LUNOKHOD 2

The Russian moon vehicle, Lunokhod 2, which landed on the Moon in January has a special set of programmes. It was landed some 175km from the landing site of Apollo 17. The data obtained from the two sources should be complementary.

Landed in the Sea of Serenity, the Lunokhod 2 task is to examine the boundary area where older



rocks may be found. At the boundary area of the highland regions, from which anorthites rise up, the floor of the mare is covered with basalt type lava.

Other experiments will measure and observe the Zodiacal light near the Sun, observe the Milky Way and the centre of the Galaxy with a space photometer. It is hoped also to decide whether there are traces of cosmic dust in the Lunar atmosphere. The possibilities of studying the Universe by optical means from stations on the moon is another experiment which the Soviet team are known to be considering.

The vehicle is also carrying a French laser reflector for measuring the Earth-Moon distance.

The Lunokhod, which is of a similar design to the previous vehicle, carries on its outside an orientation device, a lunar surface photometer, soil analysis experiment, a fixed television camera, a steerable television camera, the space photometer, a solar battery, a magnetometer, a photo receiver and aerials which include a corner reflector and a high gain system.

MOON GRAVITY

Analysis of the gravitational variations of the moon recorded by the command module of Apollo 15 has yielded data about mascons, and the lunar orbiter added to this data when being precisely tracked.

This problem, to which selenologists have devoted considerable time and study, can now be set up as a model. The model now suggested agrees well with the idea that the mascon of Mare Serenetatis is a thin body with well defined boundaries. The previous speculations on this theme have been borne out for Mare Nectaris also.

So far as Serenetatis is concerned the model fits the surface features extremely well. At the moment the data gives support to the volcanic hypothesis.

ORBITING WORKSHOP

As the launch date for the *Skylab*, the first orbiting space station, draws near it may be useful to describe the project and the sequence of events which will be the step in space that many have waited for almost impatiently.

The first crew will be an all Navy one and Charles Conrad, veteran of Apollo 12, is the only member of the team who has had astronaut experience. The other two men are J. P. Kerwen, a doctor, and P. J. Weitz, an aeronautical engineer.

Skylab will go into a 270-mile orbit. The sequence is to be the launch of the skylab unit unmanned into the prescribed orbit, the next day, May Day, the launch of the command module with the crew to the calculated rendezvous. When linked up the total length of the units will be 118ft. The diameter will be 22ft at the workshop section.

The arrangement of the airlock and docking sections allow normal joining of the command vehicle to the end of the whole unit. There is also a second docking point on the side of the docking module which could be used for a second command module to attach itself or for rescue purposes.

When the space station is launched the telescope covers the docking section. On attaining its correct location in orbit the telescope will swing to the side and the solar power paddles will open. The ports for docking will then be uncovered.

LIFE SUPPORT SYSTEMS

The station main body is 48ft by 22ft and there is an intermediate section next in the sequence which is 17ft long and is an airlock section. Here all the power control and distribution systems are located.

The air conditioning system, the life support system together with communications control and data management are also arranged there. There is room for two fully suited astronauts with personal life support systems in the section. From here the crew can pass to the docking module to work outside the vehicle or to pass to and from the command module.

The whole assembly with the launcher, a *Saturn 5* rocket, will stand 334 feet high at take off. The combined weight at the time will be 3,110 tons.



LAST month the circuit of the Tape Link was described in detail. In this the final part, the construction of the Tape Link, the fitting of the heads and the setting up procedure will be described.

TWO ASSEMBLIES

The Tape Link is made up of two assemblies (the amplifier and the power supply) in order to keep the mains transformer away from hum sensitive circuits and enabling the power supply to be positioned where it induces the minimum hum in the replay head.

The folding of the metal should present no problems to a handyman equipped with a vice. Cutting the metal to size is not quite so easy and is best done with a guillotine and a fly press for the cut out parts. Constructors may find it convenient to purchase the metal cut to size from a sheet metal shop.

POWER SUPPLY CONSTRUCTION

Dealing first with the power supply, drill the chassis and bend up as indicated in the photograph.

Next, affix the mains transformer using $4BA \times \frac{1}{2}$ in screws and nuts. Do not tighten as they will have to be undone again when the power unit is finally mounted in the case. A tag strip carrying the rectifier diodes should now be assembled and bolted to the chassis.

Wiring between this and the mains transformer is best done at this stage as the tag strip will be difficult to get at once the smoothing capacitors are in place. These and the fuseholder can now be put into position and the wiring completed.

The power lead-out wires and the mains lead are secured by a plastic cable clip bolted down to the

mains transformer. Having completed the power supply it can now be tested.

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With mains applied and no load imposed upon the outputs, the supplies should read 56 volts and 28 volts respectively. Provided that the voltages measured are within a couple of volts either way and that the mains transformer and capacitors do not get hot after a few minutes' operation, all should be well.

AMPLIFIER CHASSIS

By P. S. EWER

Mark out the front panel to suit components (see Fig. 7). Drill all the holes starting first with an $\frac{1}{8}$ in drill. Next, open out the holes for the record indicator lamp, the switches and potentiometers with the appropriate drill.

The DIN sockets are mounted beneath the panel and the $\frac{4}{5}$ in hole required to allow entry of the plugs is most neatly cut with a chassis punch, e.g. a "Qmax cutter". The cut outs for the meters are made by drilling all round just inside the edge with a small drill, pushing out the centre and then truing up to the marked line with a file.

A similar technique should be used for the meter switch cut-out. Drill two holes side by side and open up to the required size with a needle file. Finally countersink all the screw holes.

The strap for mounting the meters, and the Uchannel complete the metal work. To make the folding easier, the front panel fixing flanges should be bent over first. The sheet can then be bent up to complete the chassis. Once again, the use of a chassis punch is recommended for the larger holes (see Fig. 4).

The front panel can be finished in any way desired. One method which gives a pleasing appearance is to

satin finish it by stroking lengthwise with a wire brush such as is supplied for cleaning suede shoes. This results in a series of parallel scratches. The panel is then cleaned with a rag soaked in methylated spirit to remove loose material and grease.

Letraset may be used to label the panel, finally protecting the finish with two coats of lacquer.

After fixing the front panel to the chassis the B9A valve holders and the stand-off spacers are mounted and the components assembled to the front panel. The slider switch used by the author for the BIAS/VU selector was supplied with its mounting holes tapped at 8BA.

These were drilled out and retapped at 6BA. However if 8BA screws are used, allowance must be made for this in the front panel drilling.

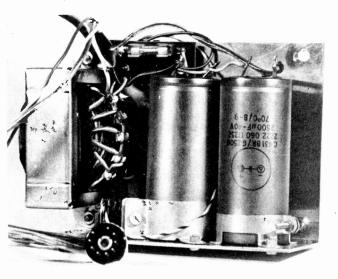
COIL WINDING

Because many readers find it difficult to obtain specified coils, the author wishes to point out that virtually any 14mm coil is suitable for L1 and L101. Most catalogues specify the number of turns per millihenry and because inductance is proportional to the square of the number of turns, twice this number will give the number of turns required for 4mH. Some easily available pot cores and their turns per millihenry are given in Table 1.

Using 34 s.w.g. enamelled copper wire, wind the required number of turns onto the bobbin. On completion the winding should be secured with a layer of adhesive tape (not Sellotape).

Before assembling the two halves of the pot core, slightly rub the mating surfaces with a sheet of paper to remove any dust which could alter the inductance of the completed coil. The lead wires should be brought out separately through adjacent slots at 90 degrees.

Photograph showing construction of the power supply for the Tape Link. The switch and indicator neon are mounted near the mains input Positioning of the power supply module within the finished tape deck is best found by trial and error being that which gives minimum hum



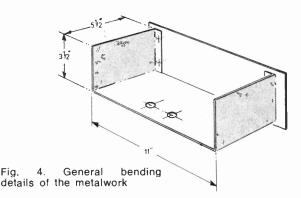


Table 1: ALTERNATIVE POT CORES FOR L1 AND L101

Туре	Turns/mH	Turns required for 4mH
LA 2503	52	104
T26/2100R	47.5	95
FX 1636	34.8	70
FX 1011	24.3	49
FX 2236	32	64

Table 2: ALTERNATIVE POT CORES FOR **BIAS AND ERASE OSCILLATOR T2**

		Turns required			
Туре	Turns/mH	Primary	Secondary		
LA 2301	53.8	5 + 5	80		
LA 2105	54.7	6 + 6	96		
LA 2517	42	5 + 5	80		
N22/250A	40	5 + 5	80		

Fig. 5. Method of winding the primary of the bias and erase oscillator coil

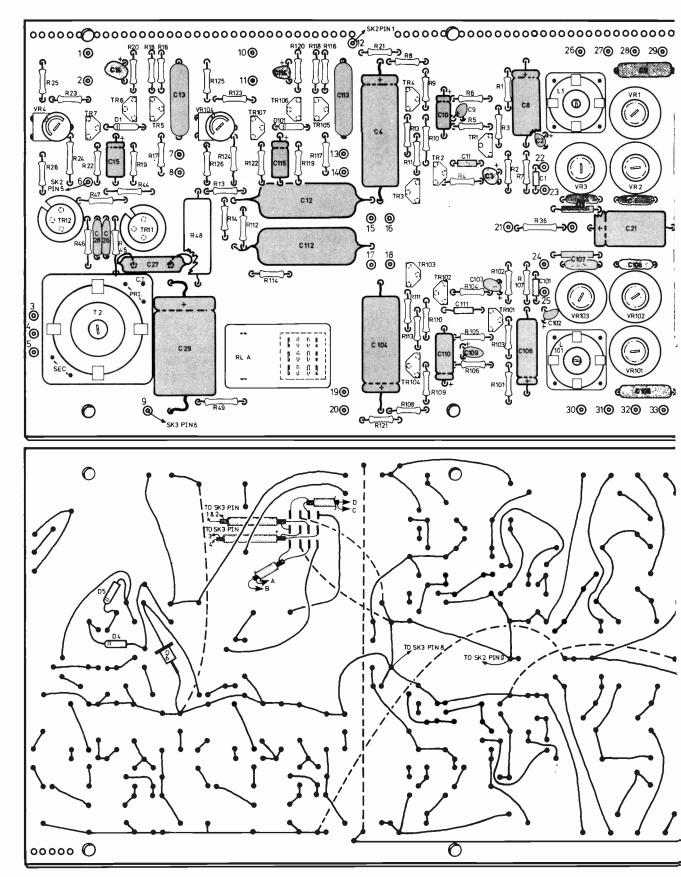
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BIAS AND ERASE OSCILLATOR TRANSFORMER

Again the pot core used for this transformer is by no means critical. A 25mm type was used in the prototype but any high frequency 18mm type will do just as well provided the inductance is that specified (see Table 2 above).

Measure off two 20in lengths of 21 s.w.g. wire and twist them lightly together. Allowing a few inches for leadout wires, begin winding the required number of primary turns making sure that the first turn of one half of the primary lies adjacent to the first of the other half and so on (see Fig. 5). After the required turns have been wound the windings should be secured with adhesive tape.

The secondary should then be wound using 30 s.w.g. wire starting in the same place and winding in the same direction. Cover this layer with one layer of tape. Then assemble the pot core with the same precautions as for the previous coil.



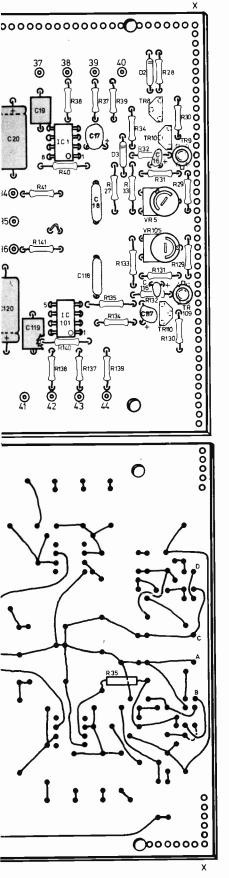


Fig. 6. Layout of the components on the perforated board. Note that some there are components under the board. C27 should be mounted away from board to avoid heat

TR1-8210

101-108 8 110

The primary windings must now be identified with some form of continuity tester such as a bulb and battery. After scraping the enamel from the four primary wires select one wire and call this the start.

Next find the other end of this wire with the continuity tester. If the method of winding shown is followed then the starts of both primary halves will be at the top of the coil and the other ends at the bottom. The end of the identified wire should then be soldered to the start of the remaining wire, this becoming the centre tap. The remaining wire then becomes the other end of the total primary.

CIRCUIT BOARD

The amplifier is constructed on perforated board which accommodates all the components with the exception of the relay for which a cut-out must be made (Fig. 6). The holes will also have to be opened out for some of the pots and for the fixing screws.

The wiring should proceed logically from one end of the board to the other inserting Veropins where the flying leads are to be soldered to the board. The oscillator tuning capacitor is mounted up in the air on Veropins to keep it away from the hot components near it.

TR11 and TR12 are fitted with clip-on heat sinks (TO5 can). There are four components mounted underneath the board which must not be forgotten.

CONSTRUCTION

Upon completion thoroughly check the board wiring. The connections from the underside of the board to the B9A sockets are then wired, allowing sufficient slack to enable the board to be tilted up through 90 degrees to facilitate servicing should it be required.

The board is next screwed into position and the wiring completed. To facilitate identification, the use of an assortment of colours for the connecting wires is suggested, and screened leads of low capacity *must* be used where indicated (see Fig. 7).

For ease of assembly it is suggested that the switch wafers nearest to the metalwork are wired first. Note the screen between the wafers and the spacers required to give good isolation between the two sections. In the prototype three-pole three-way wafers were used for S1 but the easier to obtain four-pole three-way wafers are perfectly suitable.

Prevention of earth loops is essential with this equipment and the constructor should note that there is only one connection between the chassis and amplifier earth.

At this stage the wiring on the front panel and the chassis should be completed as in Fig. 7.

TESTING

After having thoroughly checked the wiring (mistakes can be expensive) the power supply is plugged into the appropriate socket on the amplifier and mains applied. Providing that there is now no obvious indication of a fault, e.g. smoke, it can be assumed that there are no serious errors.

Measure the supply voltages with a multimeter. These should be 55 volts and 27 to 28 volts approximately. It is then prudent to go around the circuit

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	Table 3: APPROXIMATE VOLT SETTINGS	AGE
Junct	ion of R1 and R2	17.3
TR1	emitter	18-0
	collector	0.7
	ion of R1 and R21	54.0
TR2	collector	25.3
	base	0.7
	ion of R11 and R13	27.0
TR4	base	28.7
	emitter	28.0
TR3	base	25.3
	emitter	26-0
TR5	base	7.7
	emitter	7.0
	collector	18.3
TR6	base	18.3
	emitter	19.0
	collector	7.0
TR7	emitter -	6.0
	collector	26.0
VR4 w	iper (dependent on setting)	6.0
	on of R25 and VR4	8.0
	on of R26 and VR4	4.0
TR8	base	28.0
	emitter	28.7
	collector	20.0
TR10	base	19-4
	collector (dependent on VR4)	12.0
Termi	nal 6 IC1 (dependent on VR5)	12.0

checking voltages in accordance with Table 3. These are the design figures obtained by calculation and, generally speaking, provided that correlation within plus or minus 20 per cent is obtained all should be well.

When these checks have been made rotate VR4 and VR104 fully clockwise. The meters should now show a reading.

Disconnect the mains and temporarily short pins 5 and 6 of SK3 together. Set the meter switch to BIAS and the function switch to STEREO. Then reconnect the mains. The record indicator light should come on and the meter show an indication which is adjustable by means of the bias control. Failure of the meter to read suggests an oscillator fault and the power should be switched off immediately to prevent damage. Remove the temporary link.

TAPE TRANSPORT

With the old heads and/or electronics stripped out, the new heads have to be fitted to the base plates. Two methods of accomplishing this for the record/ replay head are depicted in Fig. 8. It is essential that the tracks interleave correctly and the baseplate may need to be packed up or filed down accordingly.

When correctly positioned, the upper edge of the top track lies just below the edge of the tape (about 0.15mm). With regard to the Collaro deck the slot in the baseplate had to be widened with a file and the

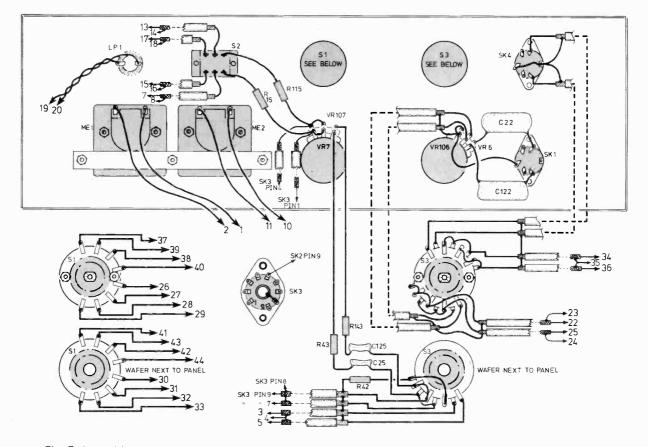


Fig. 7. Interwiring diagram showing the connections between the board and the other components. The numbers indicate the terminal pins on Fig. 6

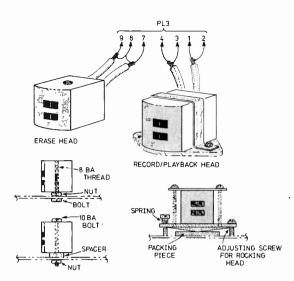


Fig. 8. Methods of fitting the new heads of the tape deck

baseplate packed up to raise the head. The dimensions of the strap are given and it was screwed to the baseplate with self-tapping screws.

The erase head has a single hole through it to clear 10BA, and this is the best means of securing it. The azimuth of the erase head gap is not critical and therefore a rocking plate is not required. On the author's deck this hole was tapped at 8BA and the head then secured directly to the head mounting plate stood-off by an 8BA nut drilled out to clear the thread. The top of the erase head upper track should extend to the edge of the tape.

PRESSURE PADS

A modification made by the author to his deck concerning the pressure pads may be of interest. The original pads were of hard felt requiring quite a high pressure to ensure contact between the tape and the head. These felt blocks were removed and replaced by a pad of composite construction, i.e. a layer of $\frac{1}{8}$ in thick foam plastic covered finally with a $\frac{1}{16}$ in layer of supple felt.

This gives improved contact at far less pressure thus reducing the wear on the heads and improving the flutter performance of the transport. At the same time a mu-metal screen cut from an old screening can was fixed to the rear of the RECORD/REPLAY head pressure pad to reduce the hum pick-up on playback.

RECORD/REPLAY SWITCH

Most tape recorders have their RECORD/REPLAY switch contacts interlocked with the function buttons. In order to change the function of the amplifier to RECORD, one set of "make" contacts are required. If these are not present on the recorder a switch must be provided and this should have contacts designed for switching capacitive loads.

The heads are wired up to the plug using low capacity screened lead. The deck chassis is earthed

Practical Electronics April 1973

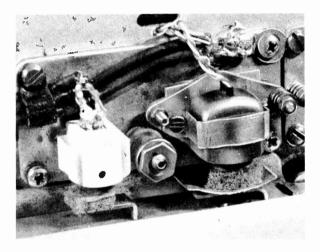
to the screens of one of the record/play leads. Care should be taken to ensure that the metalwork of the amplifier does not touch the tape deck. If this is unavoidable the earth link mentioned above must be omitted.

The power supply should not be fixed down yet as its positioning is critical for minimum hum injection. To determine this position the deck should be set in motion as it would be when playing a tape. The power pack is then moved around the cabinet whilst listening to the replay hum level until it is subjectively at its lowest.

The recorder is now complete and ready for setting up.

SETTING UP PROCEDURE

The equipment required to set up the completed recorder is a d.c. voltmeter, an audio sine wave generator and an oscilloscope, or failing this an a.c.



Photograph showing the heads in position on the prototype

millivoltmeter. The setting up should follow the order outlined below as in some cases one stage depends on the setting of the previous.

AZIMUTH SETTING

Before the electronics are adjusted the heads must be correctly aligned with the tape. Adjustment of the record/replay head gap in relation to the tape is known as azimuth alignment and is essential in order to facilitate the interchangeability of recordings between machines. This is correctly done with the aid of a professional test tape but any commercially prerecorded tape or a tape recorded on a machine with a known correct azimuth can be used. (Choose a tape with a good high frequency content.)

Whilst the tape is playing the head should be rocked up and down until the maximum high frequency output (measured simply by listening to the output) is obtained, then fixed in this position.

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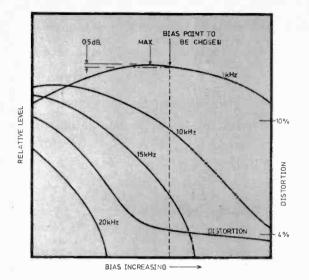
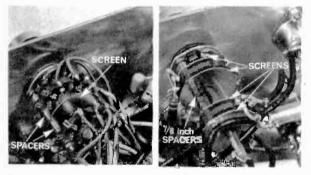


Fig. 9. Graph to show the dependence of frequency response and distortion on the bias level



Photographs showing the two wafer switches

Photograph of the completed Tape Link. The meters are held on to the front panel by a strap which is shown

REPLAY AMPLIFIER AND METERING ADJUSTMENTS

Using the voltmeter adjust VR5 and VR105 until the voltage at the emitters of TR9 and TR109 is 12 volts. Next rotate VR4 and VR104 fully clockwise (maximum resistance) then turn back so that the respective meters just read zero.

OSCILLATOR ADJUSTMENT

In the absence of suitable test equipment, a satisfactory result may be obtained by setting the adjuster to its mid position. The exact frequency of operation is not critical and in fact the tolerances of the frequency determining components are wider that the adjustment range.

If an oscilloscope or frequency meter is available then set the oscillator selector switch to STERFO, the bias control to mid range and the machine to the RECORD mode, then adjust the oscillator coil T2 until the frequency is as near to 100kHz as possible.

DETERMINATION OF BIAS SETTING

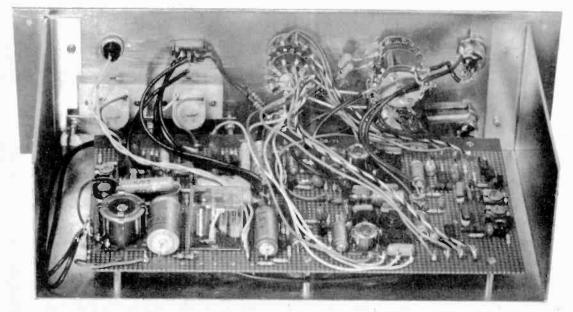
The correct bias setting is important as it affects many of the parameters of the recorder. The bias setting required depends on the tape speed, the tape in use and the mode of the recorder (MONO or STEREO). The settings should be determined as below and tabulated for reference.

71 i.p.s.

Record a 1kHz sine wave at a level 6dB below the maximum modulation, adjusting the bias from -3dB to +3dB in $\frac{1}{2}$ dB steps. Replay the tape and note the amplitude of the output for each of the bias settings.

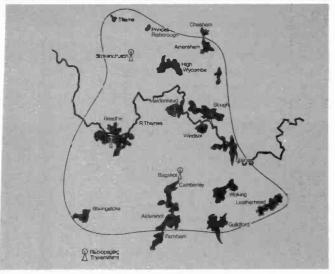
A series of results should be obtained which rise to a peak then fall off. The correct setting is that which gives a sensitivity #dB (approximately 5 per cent) down from the maximum, i.e. slightly more bias than is required for maximum sensitivity (see Fig. 9).

continued on page 341

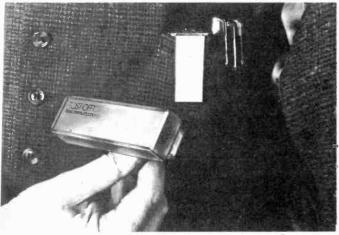




ELECTRONORAMA

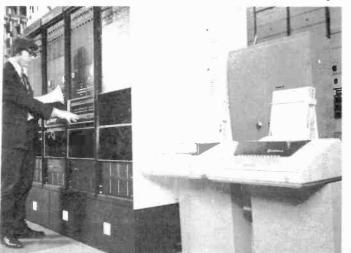


Area covered by the Post Office radio-paging service



One of the miniature pocket pagers

Computer control complex at Reading Trunk Exchange



Telephone Paging

WITH the aid of a new Post Office telephone paging system, the businessman, doctor, service engineer and many other people on call within a 500 square mile area of Reading can be easily contacted, even though their whereabouts is not known, simply by dialling a 10-digit telephone number.

The system consists of small "bleeper" pocket receivers; five f.m. transmitters, situated at Reading, Stokenchurch, Bagshot, Slough and Maidenhead; and computer-controlled terminal equipment at the Reading Trunk Exchange.

RECEIVERS

The receivers, small enough to be clipped into a pocket, give a high-pitched 10 second "bleep-bleep" signal when activated by a phone call. Powered by a 1.5V alkaline battery, each receiver will operate for approximately 900 hours, representing three months of average use.

The f.m. receivers are basically a double superhet built around six CMOS integrated circuit modules. Sensitivity is better than 10μ V/m and reception is in the 150MHz band. Following detection, the paging tones are decoded by two plug-in active filter modules; 60 frequencies are employed in the range 288-5 to 1,433-5Hz and a two-tone sequence is used to provide a system usable by 3,540 customers. Later the system will cater for 100,000 customers.

Detection of the first coded tone switches the receivers on, reception of the second tone is decoded and once accepted will sound a 2kHz bleep note.

The only control on the receiver is a three position switch: "on", "off" and "memory". In the memory position, used when the person does not want to be disturbed, the incoming signal is stored in a CMOS bistable memory device and when the receiver is switched back to the on position the bleeper will emit its signal.

Each receiver has its own 10-digit number (the first four digits are an STD code common to all receivers) and dialling this number instructs the transmitting equipment to send a signal to activate the bleeper. Communication is one-way only, so the user must prearrange the action to be taken on receipt of a radio-paging call.

COMPUTER CONTROL

The heart of the system is a Digital Equipment, type PDP11, mini-computer with a basic storage capacity of 192,000 bits. Installed at the Reading Trunk Exchange, the computer receives the "telephone calls", converts them (by an interfacer between the telephone network and computer) into a binary-coded format.

The calls are queued and released in batches at 15 second intervals. When the number dialled is recognised and accepted an announcement to replace the telephone handset is given. Once accepted the call is converted to the pager code by the computer, and passed to a frequency synthesiser and then to the relevant transmitters.

The transmitters are switched by command signals from the control complex slightly ahead of the transmission of the pager-code modulation.

Although the system is only a feasibility study, plans have already been made to extend the service to other regions, such as London, Manchester and Birmingham.

More advanced pagers are already being developed and the present receivers are claimed to work inside buildings, cars and on trains. Engineers have, it is claimed, achieved more than a 95 per cent reception in the defined boundary limits.

The radio-paging receivers will cost £5 a month to rent, with an initial fee of £5. Call to a receiver will be free during the introductory service.

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Strictly

by K. Lenton ~ Smith

POPULAR MUSIC is a lucrative and highly competitive field these days and the net is cast to take in an even younger age group each year. Tenyear-olds now have their own idols! To be successful in the "pop" field involves a constant search for new sounds by electronic processes, especially as there is a practical limit to what can be done with the vocal if the lyrics are to remain intelligible. (Some readers may query the use of the word "intelligible" in this context!)

The Survey of Electronic Musical Instruments, published as a supplement to the November 1972 edition (issues unobtainable), showed how manufacturers are catering for this search for new tonal ideas. Though initially featured by recording artists. new effects are copied by local groups as they struggle to keep abreast of the times. Amateur musicians, who prefer "pop" music though never play publicly, like to re-create at home some of the sounds they hear on radio, tape and discs. The younger generation has always, as a tradition, looked for change and new experience, the popular music field being no exception. Over the years, the specification of available electronic musical instruments has taken this into account increasingly.

LIGHT MUSIC TODAY

A certain line in "Fings ain't wot they used to be", referring to the light music scene at that time, mentioned musicians "backing themselves with three chords only". When that song was written, there was an element of truth in Lionel Bart's cynicism: a number of performers only seemed able to strum sub-dominant and the tonic, dominant seventh chords on their highly-amplified guitars. This deficiency was often covered up by a show of vocal and physical gymnastics

The advent of the Beatles brought more tuneful melodies and the use of less closely related chords. Though the Beatles, as a group, no longer exist they underlined the fact that, if a song is to survive, the melody must be original and tuneful. Many modern "pop" numbers will be forgotten a few months hence, but the Lennon and McCartney compositions have already taken their place with those of the established Old Masters such as George Gershwin, Cole Porter, Jerome Kern and Richard Rodgers.

Burt Bacharach is today's prime example of a composer who writes enjoyable music which will be remembered many years hence: Antonio Carlos Jobim is in the same category, specialising in the Latin-American field. The reader who plays their music, or attempts the transcriptions of Dave Brubeck or Dudley Moore, will appreciate that the days of "three chords only" have long passed and things certainly ain't what they used to be! These composers frequently use complex chord sequences which demand a high degree of musical ability to perform them.

Whereas our sphere of electronics —especially integrated circuitry has enjoyed a spin-off from space research, classically trained musicians who have turned to lighter music have also benefited that field. The music for a number of West End shows running currently has come from composers with classical backgrounds, whilst we have previously commented on Walter Carlos, Robert Moog and the music for "Clockwork Orange".

RETROGRADE

Today's standard of compositions and the requisite musicianship in light music is higher than it was a generation ago. At the same time, the true standard of many electronic musical instruments has fallen. Manufacturers appear to be attempting to get the proverbial quart into a pint pot, especially where organs are concerned. Perhaps this is understandable where many instruments are sold to be installed in clubs, or other public places, where the audience expects a really professional performance—by their standards.

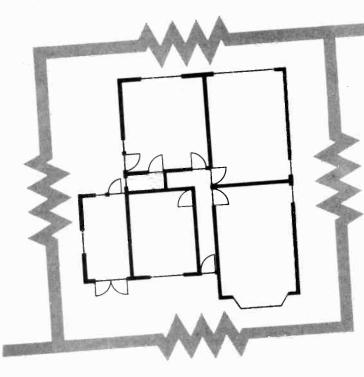
The organ studio demonstrator will show convincingly what a wonderful instrument you are about to purchase. It will no doubt have many extras such as a built-in rhythm unit, waa waa, percussion, arpeggiator, automatic chord unit, Leslie speaker, cassette tape recorder and perhaps a small synthesiser keyboard, to name but a few. Underneath all this, how much real organ is there? All these additions are expensive and the makers are probably working to a given price range, so something has to give.

The accompaniment manual is usually the victim, and the buyer is lucky if he is offered more than one pitch on that keyboard. We should perhaps remember that not all users of electronic organs are light music orientated or require the help of automatic chord/rhythm units. No serious organist would consider a single-pitch manual, or for that matter a short spinet manual of 44 notes and a set of stub-pedals. A number of users are primarily interested in baroque music or are simply church organists who require a home organ for practice purposes which will produce conventional pipe-organ tonal quality.

SOUND SYNTHESISER

For those who wish to experiment with unusual effects, the synthesiser is ideal. Mr Shaw's P.E. Sound Synthesiser should prove to be a fascinating project for readers seeking new musical sounds: we hope it will also alert organ makers to the fact that organs should sound as such and not attempt to compete with the synthesiser. Both are separate and distinct musical devices with identities of their own.

Incidentally, readers who went to the Audio Fair to hear Mr Shaw's synthesiser last year might also have listened to some of the stereo demonstrations on various stands. One of the records used for this purpose was "Moog Indigo" (VSD 6549) featuring Jean Jacques Perrey, is recommended to those who like the Moog and can appreciate the performer's skill and have a strong sense of humour.





By J. Andrews

THIS alarm system was developed to protect the house and buildings remote from it, for example, garage, workshop, etc., which might be subject to burglary or vandalism. It can of course be used to protect all other types of property.

SEARCH LOOP SYSTEM

Many alarms use the search loop system in which the doors and windows have micro-switches fitted. The switches are wired in series and should any one switch be opened the circuit is broken. When the loop is connected to a simple alarm breaking the search loop will cause a bell or other device to sound. However, if the loop can be shorted out before the switches the alarm can be rendered inoperative.

This is particularly easy if the building protected is remote from the house as the search loop wires may be run back together and offer an opportunity for short circuit. Short circuits could be caused in a number of ways, by accident, fire or deliberately.

BALANCED BRIDGE

To overcome these problems a simple bridge was devised for the prototype security alarm as seen in Fig. 1.

Here, one arm is made up of the search loop wire resistance Rx. With the bridge balanced, that is, when $Rx \times R2 = R1 \times R3$, no voltage will appear at the alarm input points XY. If the search loop is made either open or short circuit, outputs will appear at these points but of opposing polarity.

POLARISING DIODES

To overcome this and to provide voltages of a single polarity for the open and short circuit conditions, a diode bridge was arranged so that any change of balance in the resistance bridge provides a negative going input to the alarm circuit as in Fig. 2.

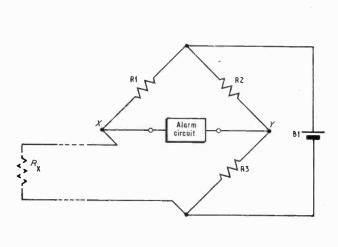
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In this, the finalised circuit of the Security Alarm, the resistance bridge is made up of R1, R2, R3, VR1 and the loop resistance Rx.

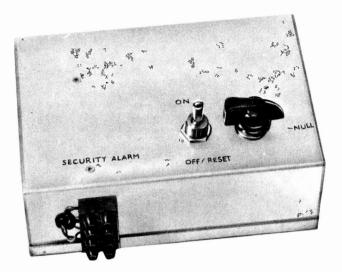
Arm resistances are made 150 kilohms so that the standing current is low. VR1 is included to balance any difference in the bridge arms and also provides a test facility as described later.

LATCH CIRCUIT

As the output resistance of the bridge is relatively high it is necessary to multiply the input impedance







The completed security alarm control unit

of any device connected across it. In the latch circuit this is achieved by connecting TR1 and TR2 as a Darlington pair.

TR2 output drives TR3 which is a higher power device suitable for driving a relay or lamp up to 800 milliamps when saturated.

Latching or hold on is achieved as follows. When TR3 is turned on by TR2 the collector voltage falls due to the drop across the relay and when TR3 is saturated is approximately 0.3V.

As TR3 collector goes negative, this turns TR2 on harder and positive feedback holds TR2 and TR3 in saturation regardless of input current to TR1. The current to TR3 base is limited by R5. Once tripped the circuit will stay on until the supply is interrupted. C2 is included to ensure the circuit resets.

In the prototype a relay was used to switch on an external bell. It could also be used to turn on lights or activate other warning systems.

CONSTRUCTION

Most of the small components given in the circuit diagram can be assembled on a piece of $3in \times 1\frac{1}{2}in$ Veroboard as is Fig. 3. When assembled and wired, 6in sleeved flying leads should be connected where indicated.

The choice of housing for the board and ancillary pieces was a $4in \times 6in \times 2\frac{1}{2}in$ standard aluminium chassis. First the mounting holes for VR1 are drilled together with those for the double-pole switch and Veroboard spacers.

With these items fitted interwiring can be completed as in Fig. 4.

TESTING

To test the assembled alarm connect up batteries B1 and B2 only and fit a 200 kilohm resistor across the loop terminal. If a high impedance multimeter is available connect across capacitor C1 as seen in Fig. 2.

Set the meter to the ten volt range, and switch the unit on. If now VR1 is rotated from end to end a null should be found.

If all is in order, connect B3 and switch on. The relay should stay out. If this is not so check that the null balance is correct.

Now rotate VR1 in a clockwise direction and the relay should pull in. If the null is now reset the relay should remain in.

Now reset the alarm by flicking switch S1 off and on, then rotate VR1 anticlockwise when the

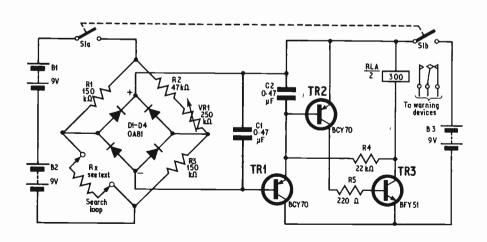
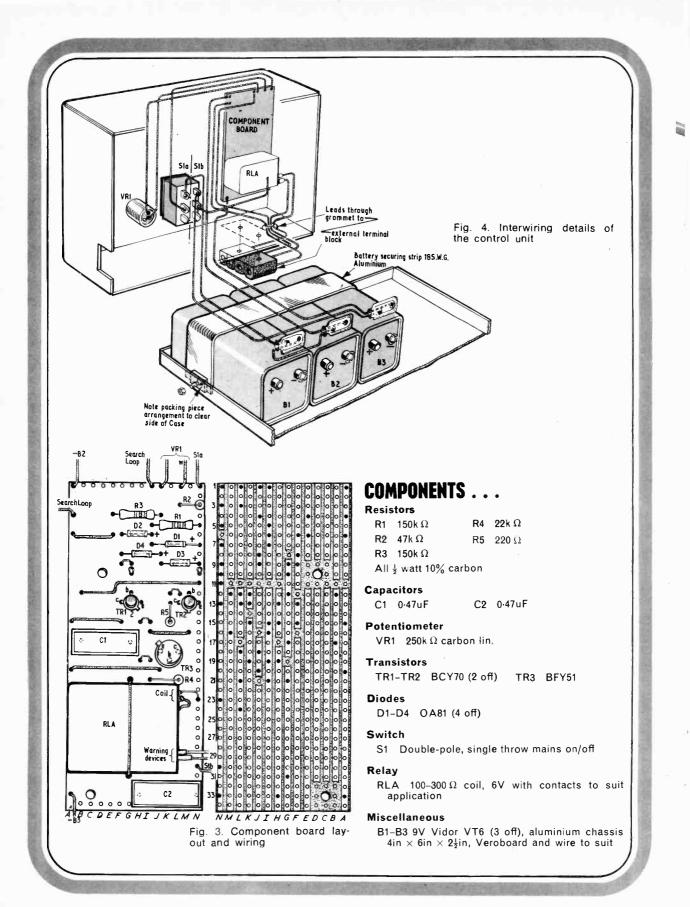


Fig. 2. Circuit diagram of the security alarm



relay should again pull in. Return VR1 to null and reset the alarm with the switch.

Note that the relay cannot be reset unless VR1 is at null.

TESTING WITHOUT A METER

Disconnect R4 from the base of TR2 and connect a $200k\Omega$ resistor across the loop terminals as before. Connect all batteries and switch on.

Rotate VR1 until the relay pulls in, then back off until the relay drops out. Note the point at which the relay pulled in.

Rotate VR1 in the opposite direction until the relay pulls in again, and note this point. The centre of the two points at which the relay pulled in is the null point of the bridge.

Reconnect R4 and check that when VR1 is rotated in either direction the relay pulls in and remains when VR1 is set to null.

FINISH

Once the instrument has been checked and the null and test points have been determined, Letraset may be used to apply a legend to the front panel. A coat of clear varnish will ensure the case stays bright.

INSTALLATION

As explained previously the search loop resistance must total $150k\Omega-200k\Omega$. This is extremely high and any amount of wire used to make up the search loop will not affect this figure, therefore it is necessary to insert resistance in the form of two $100k\Omega$ resistors in the loop

Arrangement of switches in the loop need not be confined to microswitches on doors and windows. Switches can be placed under carpets, etc., depending on the amount of security required. One further idea to protect windows apart from microswitches, is to fix a screen of fine copper with tape or clear varnish directly to the glass. This is included in the search loop; should the window be broken, the alarm will sound.

The alarm control unit would normally be installed in some part of the house, perhaps in a cupboard or concealed behind furniture. However, when siting the alarm, bear in mind the wires will have to run to parts of the house or outbuildings to be protected.

WARNING DEVICE

No actual warning device is shown as this will be governed by personal requirements, possibly only a warning light will be required, however the relay could turn on house lights or ring a large bell.

Once installed and assuming the alarm has been tested as above, no difficulty should be encountered. Before connecting the search loop check with an ohmmeter for continuity and correct resistance. Connect the search loop to the control unit and set VR1 to null; switch on the alarm and check that both shorting and open-circuiting the search loop cause the alarm to operate.

When in use periodically check the alarm by rotating VR1 first clockwise and then anticlockwise. In both cases the alarm should sound. This forms a test of battery condition. Batteries should operate the unit for their shelf life.

HI-FI TAPE LINK

continued from page 332

3³/₄ i.p.s.

Repeat as for $7\frac{1}{2}$ i.p.s. using a test frequency of 500Hz.

17 i.p.s.

As for $7\frac{1}{7}$ i.p.s. but using 250Hz.

The bias must be determined separately for mono and stereo modes.

PRE-EMPHASIS

Adjustment of the pre-emphasis gives a maximally flat overall frequency response.

7½ i.p.s.

Apply an input signal from a signal generator at 15.4kHz and adjust L1 until peak output is obtained at the output of the replay amplifier (junction of R11 and R13). Next set the generator frequency to 4kHz and record at a level of -10dB. Replay the tape and note its output as this is to be used as a reference.

Reset the frequency to 15.4kHz and make another recording leaving the level control untouched. Note the playback level and then make successive recordings adjusting VR1 to give a playback level at 15.4kHz which is $\frac{1}{2}$ dB greater than at 4kHz. The overall response should now be reasonably flat. However, a check should be made at a number of points between 4kHz and 15.4kHz adjusting VR1 so that the undulations in the response curve lie equally about the 4kHz figure. The respect this measure for the other channel

Then repeat this procedure for the other channel.

3³/₄ i.p.s.

Record a 800Hz reference level once again at -10dB. Set the generator to 9.6kHz and repeat the above procedure but this time adjusting VR2 then VR102.

17 i.p.s.

In this case a 200Hz reference level is used at -10dB. The generator is set initially to 6.0kHz and VR3 then VR103 are set up as above.

MODIFICATIONS

Readers wishing to save the expense of two meters can parallel the outputs of the meter drive amplifiers into one storage capacitor. The meter will then show the larger of the two input signals.

If this design is to be used with the P.E. Gemini amplifier then it is advisable to fit attenuators to the input and output sockets. This allows reasonable use of the gain control to be made when recording and on playback gives an output consistent with the input sensitivity of the Gemini.

Correction: In the first part (March 1973) Figs. 2b and 2c should be transposed.



By R.W.COLES PART 10

M COUNTER BOARDS

This month's article deals with the M(COUNTER) boards which are the last of the arithmetic unit plug-in cards to be described.

M COUNTER FUNCTION

The basic system used to enable the MULTIPLICA-TION and DIVISION operations to be carried out was described in Part 1, where it was mentioned that the successive additions and subtractions carried out were counted in a counter circuit.

It is this counter which is housed on the two identical M boards, together with the COMPARATOR circuit required during MULTIPLICATION to register an equality between the count and the contents of the REGISTER.

BLOCK DIAGRAM

A block diagram of the COUNTER/COMPARATOR circuits and their related data paths is shown in Fig. 10.1, which can be placed in context by reference to the overall system block diagram, Fig. 1.3 of Part 1. The counter itself consists of a serial string of six, four-bit, decade counter units which have a maximum count capacity of 999999.

The COUNTER can be cleared or preset by appropriate control signals from the programme, and is triggered by the PLUS/MINUS COMPLETE signal from board CB, which is produced during each addition and subtraction.

The six, four-bit, B.C.D. outputs from the counter are fed to the comparator circuit and also to the A REGISTER into which they can be entered at the end of a DIVISION sequence as required.

When the COMPARATOR registers an equality between the count and the E REGISTER contents during a multiplication, it sets a latch which produces the COMPARATOR EQUAL signal, which in turn stops the arithmetic clock.

Before a MULTIPLICATION sequence, the EQUALS LATCH is cleared by a signal from the FROGRAMME.

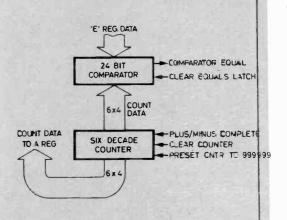
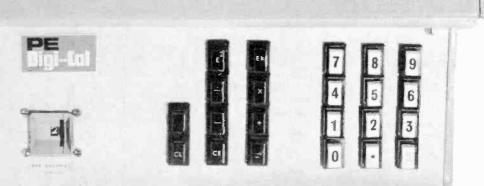


Fig. 10.1. Block diagram of the COUNTER/ COMPARATOR circuits and their related data paths



PARTITIONING

A six decade counter and comparator requires too many i.c.s, even when using M.S.I. devices, for it to be housed on a single DL109 card, so the circuit is split into two identical sections, each comprising a three decade counter and a commensurate amount of comparator circuitry. This is described more₄ fully in Fig. 10.2.

Only one EQUALS LATCH is required, but in practice a latch is incorporated on each board to ensure interchangeability, which is an advantage in fault finding, and initial testing.

The latch in use is determined by the external edge connector wiring, no connection being made to the latch inputs and outputs on the board in the M2 position.

FULL CIRCUIT

The full circuit of one of the M COUNTER boards is shown in Fig. 10.3. The counter chain is easily identified as IC's 123, 124 and 125 which are SN7490 devices connected to count in a B.C.D. code by connection on the A output to the B input.

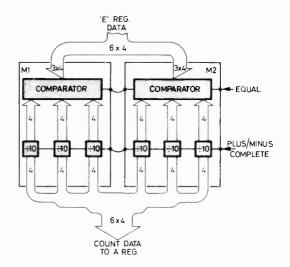


Fig. 10.2. Partitioning of the COUNTER/COM-PARATOR between the two M boards

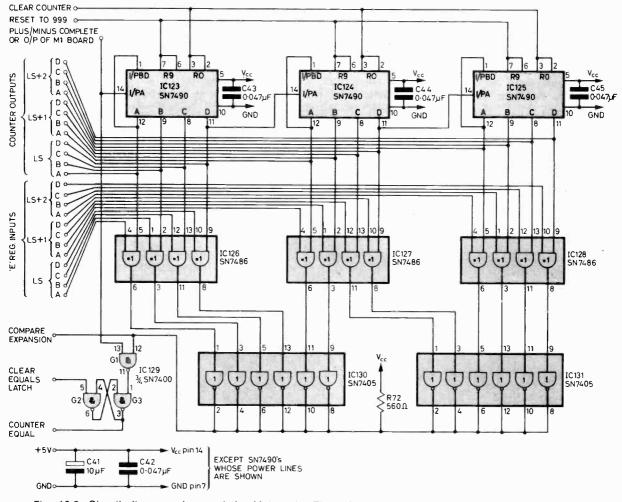


Fig. 10.3. Circuit diagram of one of the M boards. The other board is identical to this, both being built on DL109/44 boards

The count input to the board comes either from the PLUS/MINUS COMPLETE line (in the case of M1) or from the LS+2, D output of board M1 (in the case of M2).

Each of the SN7490 devices has a decoupling capacitor connected between its power supply lines, in addition to the two standard board decoupling capacitors C41 and C42.

LINE DRIVING

Special precautions are necessary for absolute integrity of the count, without false triggering or commutation, because the ABCD counter outputs are taken off the board as inputs to the A REGISTER.

Line driving from counters in this way can cause problems due to the high peak current required to charge the stray capacitance of the line during a 0 to 1 transition. Having an extra reservoir of charge available directly across the i.c. power pins goes a long way toward preventing the mistriggering problems which could result.

COUNTER PRESETS

The RESET 0 (R0) and RESET 9 (R9) inputs to the SN7490 set the COUNTER outputs to 0000 or 1001 respectively.

The R0 inputs are connected together to form the CLEAR COUNTER line, controlled by the PRO-GRAMME, and the R9 inputs together make up the RESET to 999 line.

As mentioned in Part 1, it is necessary to preset the M COUNTER to 999999 before a division so that the final number of subtractions counted when the A REGISTER contents go negative and stop clock generation, is not the full number of subtractions performed, but the full number minus one.

Setting the count to 999999 is the same as starting to count from minus one, since on the first PLUS/ MINUS COMPLETE pulse, the count will change to 000000, the number registered by the counter always being one behind the true number of subtractions performed.

During MULTIPLICATION the true number of additions performed has to be counted—the PROGRAMME ensuring this by energising the CLEAR COUNTER input and not the RESET to 999 input.

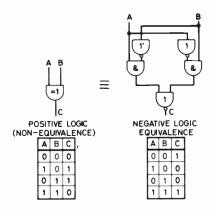


Fig. 10.4. Equivalent logic for an EXCLUSIVE-OR gate and truth tables for both positive and negative logic conventions

COMPONENTS . . .

Resistors

R72, R73 560 $\Omega \ {}^{+}_{\pm}W \ \pm$ 10% (2 off)

Crpacitors

C41, C46 10μF 15V elect. (2 off) C42-45, C47-50 0·047μF (8 off)

Integrated Circuits

IC123-125, IC132-134	SN7490 (6 off)
IC126-128, IC135-137	SN7486 (6 off)
IC129, IC138	SN7400 (2 off)
IC130, IC131, IC139, IC140	SN7405 (4 off)

Printed Circuit Boards

Type DL109/44 Shirehall (2 off)

In each case components are divided equally between the two M boards

COMPARATOR

The COUNTER as described is all that is needed to allow the DIVISION operation to take place, but during MULTIPLICATION comparison of the count with the E REGISTER contents is required.

The COMPARATOR is made up of the remaining i.c.s on each board and is concerned solely with detecting the equality of E REGISTER and COUNTER outputs so that a control signal can be produced to stop the clock at this point.

The 24 bits of E REGISTER data and the 24 bits of COUNTER data are individually compared on a one-to-one basis in a series of 24 EXCLUSIVE-OR gates formed from six SN7486 packages, housed three to a board.

EQUIVALENCE GATE

The SN7486 package is a member of the M.S.I. family and is described as a quad EXCLUSIVE-OR gate in TTL literature. The very useful EXCLUSIVE-OR function has its own logic symbol, but is in fact made up of a series of simpler gates, as has its own logic symbol, but is in fact made up of a series of simpler gates, as shown in Fig. 10.4.

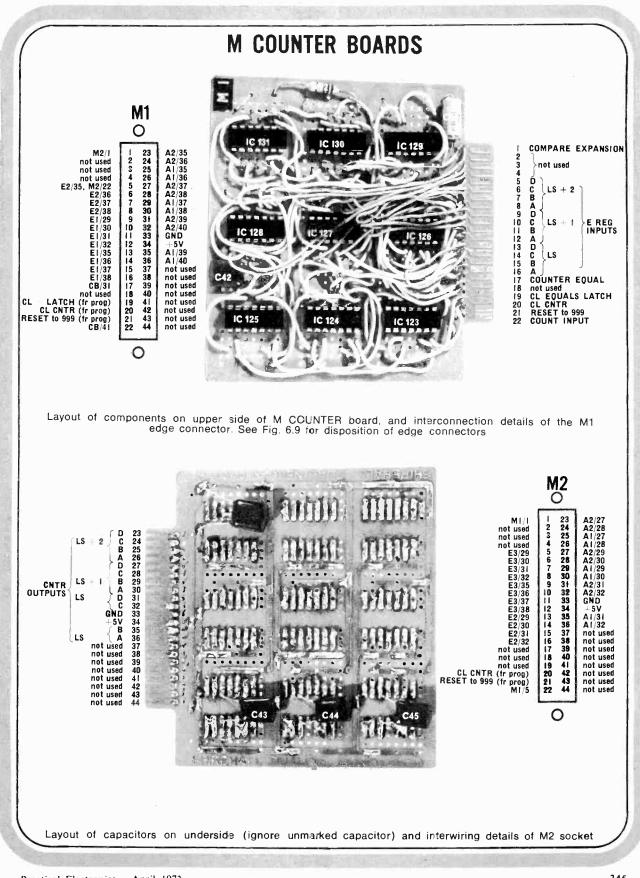
Readers may recognise the equivalent logic as being simply the common AND-OR-INVERT function together with a couple of inverters to produce the NOT version of the A and B inputs.

The reason for the EXCLUSIVE-OR name becomes obvious when the basic (positive logic) truth table is examined. The output from the gate is a logic 1 if either input A OR input B is a logical 1 but not if both are logical 1's.

This response is that of a non-equivalence gate since a logic 1 output is produced only when the inputs are different, but the situation is changed when the gate is examined in operation as a negative logic system, as the second truth table demonstrates.

NEGATIVE LOGIC

In the second truth table we can see that when a low voltage is interpreted as a logic 1, rather than as a logic 0, the output of an SN7486 gate is a logic 1 when the inputs are identical, giving the equivaence function.



To disbelievers, all this talk of switching logic conventions to suit the circumstances can be confusing, and really it is only a convenient way of looking at things.

In practical terms, the output of an SN7486 gate will go low when its inputs are identical, so to determine when all 24 gates have low outputs, i.e. when M equals E, we need a 24 input NAND gate which responds to negative logic inputs.

NEGATIVE LOGIC NAND GATE

No such gate is available in the standard TTL range, but if it were, it would be listed as a NOR gate because TTL is described in the positive logic convention.

All is not lost however since by using an opencollector inverter connected in the input of each SN7486, and then joining all the open collectors through a single common resistor to $V_{\rm CC}$, i.e. by performing the WIRED-OR function at their outputs, a negative logic NAND gate of virtually unlimited size can be formed (Fig. 10.5).

The way a gate operates is fairly straightforward: if all SN7486 outputs are low, i.e. if M equals E, then the output of all inverters will be high, and the common resistor ensures a high voltage output.

If any one or more of the SN7486 outputs is high, however, one or more of the inverter outputs will go low and pull the common output to a low level.

INVERTERS

The inverters used on the M boards are type SN7405, which have the required open collector output circuitry. Note that the SN7404 devices are not suitable for use in this position due to their standard totem-pole outputs.

Although only one "pull-up" resistor is required for the full 24 inverters, electrically speaking in fact a separate resistor is used on each board to allow the boards to operate autonomously when required.

The inverter outputs from the two boards are united by means of the COMPARE EXPANSION input/ output line, so that the two resistors are effectively in parallel.

LATCH FUNCTION

When an equality is registered by the comparator, the common output line rises to a high level and this signal is used to set the simple latch flip-flop made from cross-coupled SN7400 gates G2 and G3.

Setting the latch is carried out via another gate G1, which is controlled by the clock input line to

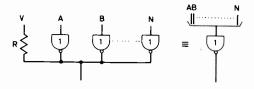


Fig. 10.5. The use of inverters to form a 24 input NOR gate

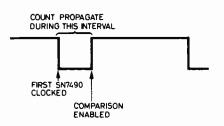


Fig. 10.6. PLUS/MINUS COMPLETE waveform from the COUNTER board

the first SN7490. In practice this line will carry the PLUS/MINUS COMPLETE waveform, since only the latch on the M1 board is wired into circuit.

The reason for this gated latch input circuit is explained in Fig. 10.6, which shows the PLUS/MINUS COMPLETE waveform from the COUNTER board.

The SN7490 counters are triggered from the negative going signal, but because these devices operate in the ripple count mode, there will be a significant count propagation delay time down the chain which can and will lead to transient spurious outputs from the COMPARATOR gating.

Using the PLUS/MINUS COMPLETE signal to gate the COMPARATOR output prevents the spurious outputs from setting the EQUALS LATCH until count propagation is complete, since G1 is enabled by the positive going edge of the waveform.

EQUALITY

When a genuine state of equality exists between the COUNTER and E REGISTER the latch is set, energising the COUNTER EQUAL line which in turn stops the supply of clock pulses to the A, Z and ADDER boards.

Before a further MULTIPLICATION sequence is initiated, the PROGRAMME clears the EQUALS LATCH ready for a new comparison.

CONSTRUCTION

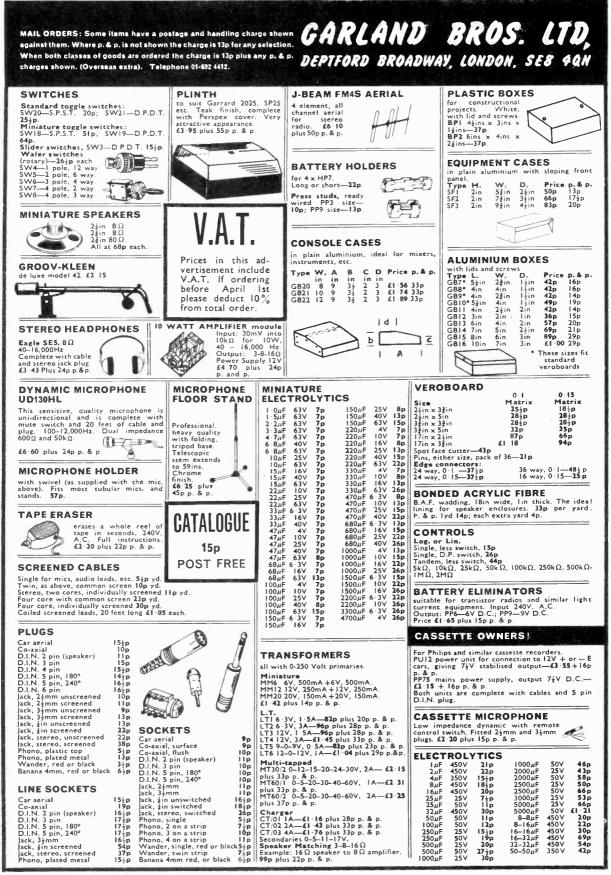
Construction of the two M boards follows the by now familiar pattern, two DL109/44 cards being used. All wiring should be kept as short as possible whilst avoiding "bird's nests".

Speed problems decrease by a factor of ten for each stage of the COUNTER meaning in effect that only the first stage could be a problem in this respect. For this reason it is best to select which board is to be installed in the M1 position during test calculations, since the first stage of one board might perform better than the other at speed.

TESTING

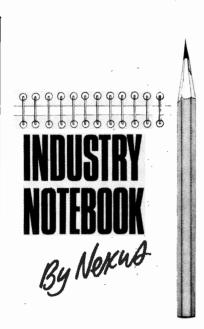
The M boards are easy to check in isolation if required, but if the recommended sequence of construction has been followed and the calculator is operational on ADD/SUBTRACT, it is easier to test the boards in situ, using the MULTIPLY/DIVIDE programmes—but more of this next month.

Next month: E² Logic, Error Detection and Testing



Practical Electronics April 1973





FIRST AWARDS

The Society of Radio and Electronic Technicians, now almost 6,000 strong, has awarded its first three Honorary Fellowships. Proud recipients were Lord Orr-Ewing, Edwin Spreadbury and Kenneth Tempest, all of whom have played a major role in establishing the Society.

The awards were made at a dinner in The Cholmondeley Room, House of Lords, with this year's SERT president, James Redmond, director of engineering BBC, in the chair. Among the distinguished guests were Sir Eric Eastwood, chief scientist and director of research GEC, and Sir Cyril English, director general of the City and Guilds of London Institute.

Of the three Honorary Fellows it was probably "Spread" who enjoyed the distinction most keenly for it was he who helped in the formation of the Radio Trades Examination Board back in 1941 and, later, as chairman of RTEB, he was instrumental in founding SERT of which he became first chairman.

Lord Orr-Ewing, top man in Ultra Electronics, was first president of SERT in 1966 and gave influential support. Immediate past chairman Kenneth Tempest had the satisfaction of seeing membership pass the 5,000 mark during his term of office.

SERT has not wavered in its policy of insisting on good qualifications for members and thus has helped raise the status of technicians and brought them into the professional class of employment.

The properly qualified electronic technician engineer deserves his

professional status and quite clearly the work of SERT and the IEETE (which caters more broadly for the electrical technician engineer although many members are in electronics) is important in establishing a better business and industrial status for members.

MAGIC MILLION

A million pounds is a nice round figure for turnover—indeed a magic figure to aim at for those with the guts to go it alone without benefit of shelter from working within a big group.

Bill Coates, top man in Leicester-based component distributor Townsend-Coates gets his taste of magic this year. He started up in 1961 with a first year sales turnover of £2,500, largely to local concerns. Now he has a staff of 46, stocks 16,000 different items from nearly a dozen manufacturers and sells on a nation-wide basis.

Two go-it-aloners who are working on the magic million, although still with some way to go, are Ray Vincent and Jim Griffith. In 1966 they took over ailing Plastronics Ltd., at Watford, a moulding and sub-assembly shop serving the electronics industry. Staff today is 40 after a move to new premises in 1969 and, says Jim, it will be necessary to make another move for expansion before long.

Among the more important customers for Plastronic moulded products are Garrard, BSR, British Radio Corporation, Lotus cars and Scammell lorries. The computer industry is also a big customer.

EXHIBITION NEWS

The first commercial full scale exhibition and conference on Automatic Testing Equipment—fastest growing sector of the instrument industry—will take place at the popular Metropole Convention Centre, Brighton, opening on November 26. Stands are already being booked by leading manufacturers and a call for papers has gone out.

Microwave 73, also at the Metropole is a sell-out. It will be opened officially on June 19 by His Royal Highness the Duke of Kent in his capacity as a member of the National Electronics Council and a Companion of the IERE. Sir Gerald Narbarro is to hop

Sir Gerald Narbarro is to hop over to the USA to open Coil Winding-Chicago 73 organised by British-based Electromation Exhibitions Ltd. and opening on March 27. Sir Gerald is first president of the International Coil Winding Association.

The International London Electronic Components Show opening at Olympia on May 22 is to have 350 exhibitors. Biggest stand is occupied by a consortium of French companies who are clearly determined to cash in on the opportunities of the enlarged EEC.

The Soviet Union will be showing valves, passive components and test gear through British agents Z & I Aero Services. Previous showings of Russian components both in the UK and France have left me totally unimpressed—perhaps there will be more of interest this year.

BIPOLAR PROCESS

Plessey's Bipolar Process III technology for integrated circuits has now moved from pilot production at the Ailen Clark Research Centre at Caswell, to full production at the main semiconductor plant at Swindon:

Whole families of new devices have been planned and with higher speeds now available a new range of applications has been opened up. Among the first commercially available products are high speed dividers capable of accepting an input of 1.2GHz, and a range of logic circuits compatible with Motorola's MECL III range. Selected variants, say Plessey, have a considerable performance gain over standard MECL III.

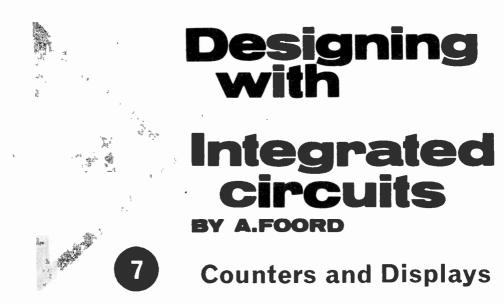
The production technique uses an epitaxial layer only 4 microns thick with emitter-base and basecollector junctions well under a micron deep. This is obviously not a cheap process but every milestone on the path to improved performance must exact its price.

HALF CENTURY

Eddystone Radio is approaching its 50th birthday with record growth and a firmer policy than it has had for years. Eddystone's Big Three, managing director Dick Carroll, chief engineer Bill Cooke, and sales manager Ken Wilkins are now dedicated to total solid state equipment and minimum production targets of 10,000 receivers on any new models.

The last of the Eddystone valve receivers, the popular 830, has been delivered and is being superseded by the new solid state 1830 range of general purpose receivers which have already won full approval from the British and a number of other PTT administrations.

During a visit to Eddystone's Birmingham works, I was told that the 958 Series of high-stability receivers, of which over 1,000 have now been delivered, is now available in nine versions. What has given Eddystone this flexibility in production is a big switch to modular construction and this has also had its effect on manufacturing and testing methods.



E HAVE spoken in general about digital instrumentation and counters and this month will consider how the counters can be constructed. We will first examine in detail the individual integrated circuits used in a typical decade counter.

SN7490N DECADE COUNTER

The SN7490N consists of four master-slave bistables internally interconnected to provide a divide-by-five and a divide-by-two counter. There are also gated direct reset lines to inhibit the count inputs and return all the outputs to a logical 0 or binary coded decimal (BCD) count of nine.

The output from the first bistable is not internally connected to the next stage, and so three different count modes are possible, Fig. 7.1.

1. The BD input is externally connected to the A output, and the A input receives the incoming count. A count sequence is obtained as shown in the truth table. The outputs can be reset to a conventional zero or to a BCD count of nine for nines complement decimal applications.

2. Where a symmetrical divide-by-ten count is required (the previous arrangement divides by ten, but not symmetrically) the D output is connected to the A input. The input count is applied

BINARY CODED DECIMAL

A binary numbering system for coding ... decimal numbers in groups of four bits. The binary value of these four-bit groups ranges from 0000 to 1001 and codes the decimal digits 0 to 9. To count to 9 takes four bits, to count to 99 takes two groups of four bits, etc. €. #×4₈₆

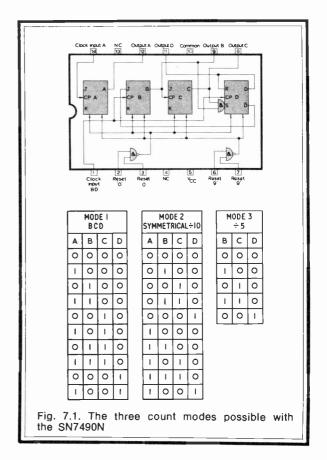
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RESET

Also called clear. It is an input which makes the output go to a desired state, usually 0 or 9.

* 1 F

to the BD input and a divided-by-ten symmetrical square wave is obtained at the A output. The circuit thus divides by five first and then by two. 3. For divide-by-two and divide-by-five operations the two counters can be used independently. Bistable A is used to divide-by-two while the BD input is used to obtain a divide-by-five operation at the B, C, and D outputs. However the



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A A



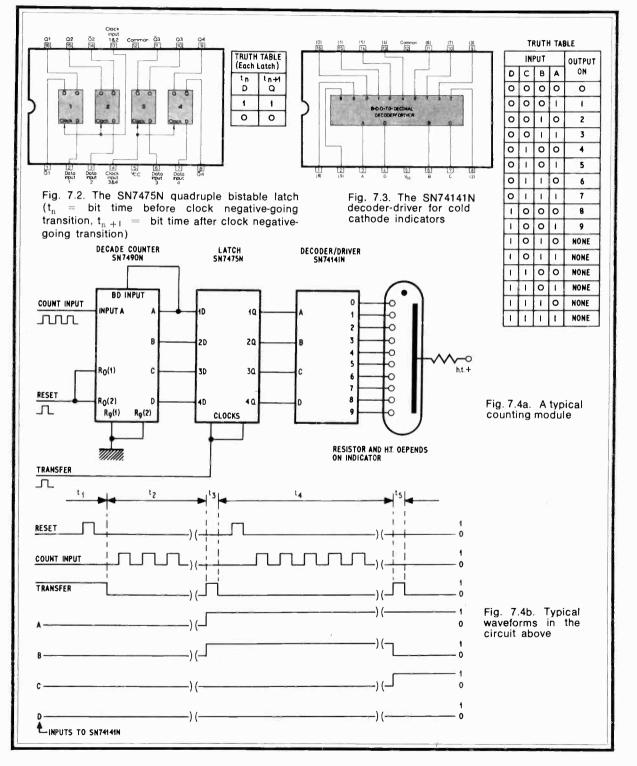
counters are reset simultaneously because the reset lines are common.

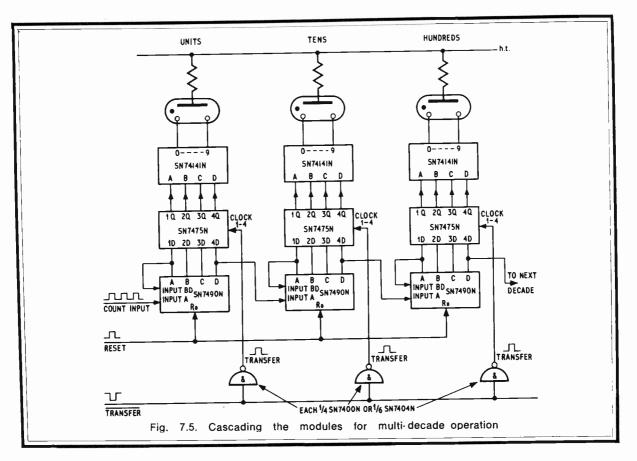
SN7475N QUADRUPLE BISTABLE LATCH

The SN7475N is a bistable latch which is used as a temporary store for binary information, Fig. 7.2. Information which is present at a data input (D) is transferred to the Q output while the clock is high. The Q output follows the data for as long as the clock is high but the last information is retained at the data output when the clock goes low.

SN74141N DECODER-DRIVER

The SN74141N is one of several decoder-drivers available in the TTL range and is designed to drive





cold cathode indicator tubes. It accepts a BCD input which it decodes to drive the cathodes of an indicator tube without the need for external components, as in Fig. 7.3.

SINGLE COUNTER MODULE

A typical application for a single counting module is shown in Figs. 7.4a, b, with the counting sequence. (a) During t_1 the decade counter is reset to 0.

(b) During t_1 a BCD count of three is available at the output of the SN7490N, but the indicator still displays 0.

(c) At the start of t_3 the indicator will display 3, and at the end of t_3 the BCD count of three is committed to the memory of the SN7475N. The decade counter is free to count again.

(d) During t_4 the decade counter is reset to 0 and will then repeat the cycle to display five.

For multi-decade operations the modules may be cascaded as shown in Fig. 7.5.

PRACTICAL DETAILS

For those constructors who wish to experiment with these applications, R.S. Components produce the three integrated circuits, a printed circuit board, and the indicator tube.

The 5V logic supply and the h.t. can be derived from a transformer which gives 6.3 volts and 250 volts.

For testing purposes the reset and transfer lines may be derived from switches, and the input signal derived from a Schmitt trigger SN7413N oscillator.

FAN-IN PROBLEMS

(a) RESET (SN7490)

The reset line of the SN7490 can have a fan-in of one if the other reset input is returned to $V_{\rm CC}$, so that an SN7400 (fan-out of 10) can drive an adequate number of decades.

(b) COUNT INPUTS (SN7490)

The A or BD inputs of the SN7490 can be driven from an SN7400.

(c) TRANSFER CLOCK (SN7475)

The transfer line of each SN7475 has a fan-in of eight (two per latch). The solution is to use one quarter of an SN7400 for each SN7475 package or to use a buffer (such as the SN7437 or SN7440) which has a fan-out of 30.

CONCLUSION

This article has shown how three integrated circuits can be used to interface with cold cathode indicator tubes. Where the intermediate outputs are not required the new SN74142N combines these three circuits into one 16 pin dual-in-line package, with a considerable space saving.

For driving displays other than cold cathode indicators the SN74141N would be replaced by one of the other drivers in the range. Although seven segment indicators (for example) are popular because they only need a 5V rail, cold cathode indicator tubes are still preferred by many people, since the required h.t. is not difficult to provide.



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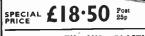
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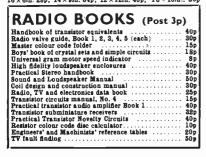
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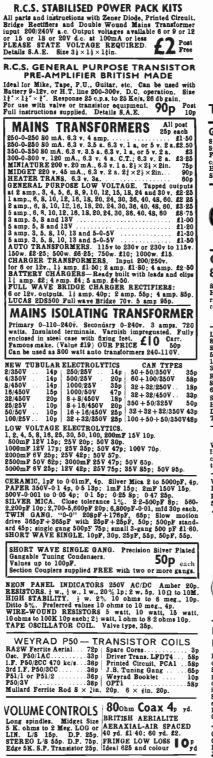
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MODEL "A". 20 × 13 × For 12in. dia. or 10in. speaker. **£9**

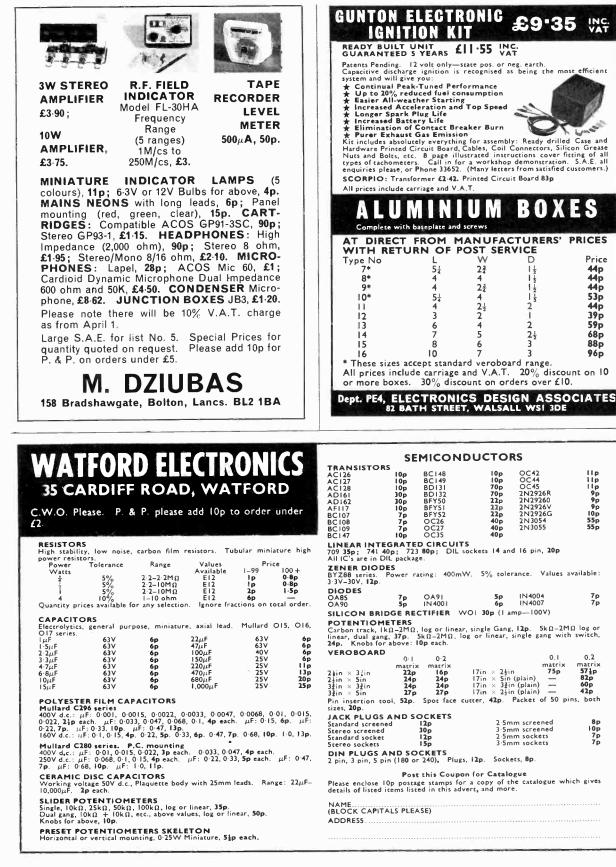
BARGAIN 4 CHANNEL TRANSISTOR MONO

TRANSISTOR MONO MIXER. Add musical bigblights and sound effects to recordings. Will mix Microphone. records, tape and tuner with separate controls into single output. 9 volt, battery operated.

BARGAIN FM TUNER 88-108 Mc/s Six Tran-sistor. 9 volt. Printed circuit. Calibrated slide

For 10 × 6in. 6in. speaker.

LOUDSPEAKER



AUTO-ELECTRIC CAR AERIAL

with dashboard control switch-fully with dashboard control switch—tuny extendable to 40in or fully retrac-table. Suitable for 12V positive or negative earth. Supplied complete with fitting instructions and ready wired dashboard switch. **25-75** plus 25p post and insurance



No. of Poles

1 pole

poles poles poles

poles

poles

noles poles

11 poles

12 poles

6 poles

TAPE HEADS

We are gradually obtaining more information about the Truvox tape heads we have, we are told that these have been wound in a very ingenious way so that winding may be coupled either in parallel or in series depending whether high or low impedance is required. We also have matching erase heads and now offer these in pairs. I record and 1 erase head. Price of the 2 track 45 per pair. 4 track 75 p er pair. Pair mounted on plate 45 pertia.

MAINS OPERATED CONTACTOR

for portable, car radio or transmitter. Chrome plated-six sections, extends from 74 to 47in. Hole in bottom for 6BA screw. . KNUCKLED MODEL FOR F.M. 509.

CR & HIPE SWITCH Smith's main's driven clock with 15A programmable switch also notes showing how you can use this to wake up with music playing, kettle boiling or come home to a warm house, warn-off burglars, keeps pets warm, halves your beating bills etc., etc. £1.75 +20p

£1.75 +20p p. & p.

MAINS CLOCK & TIME SWITCH

WATERPROOF HEATING ELEMENT 26 yards length 70W. Self-regulating temperature control. 50p post free.

with scaling washers suitable for 200-240V a.c. Depth into tank 11in. 2kW or 3kW. **\$1:50** µlus 40p each post and insurance.

NEED A SPECIAL SWITCH ? Double Leaf Contact. Very slight pressure closes both contacts. 6p each, 60p loc. Plattic pushrod suit-able for operating, 5p each, 45p doz.

IMMERSION HEATERS BY

220/240V 30 cycle solenoid with laminated core so very silent in operation. Closes 4 circuits each rated at 10A. Extremely well nade by a German Electrical Company. Overall size 24 × 2 × 2in. \$1.56 each each.

88n.

REMPLOY Standard fitting for domestic water

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domestic water tanks, made by the

famous Remploy Company. Complete



(A 30A switch.) Just the thing if you want to come home to a warm house without it costing you a fortune. You can delay the switch on time of your electric fires, etc., up to 14 hours from setting time or you can use the switch to give a boost on period of up to 3 hours. Equally suitable to control processing. Regular price probably around \$5. Special snip price \$1.50, p. & ins. 23p.



Offered at less than wholesale price your opportunity to replace those dangerous adaptors-brown bakelie flush mounting-standard fitting. Unswitched **20p** each separ-ately switched **20p** each. Less 10% ten or more +20p postage if order under £5.

4 WATT AUDIO AMPLIFIER

power pack. Only 21-45. This low price possible only because the make is over-produced. Un-repeatable once stocks are cleared. Maile by the famous case, amplifier may be used for Mono or Steree, music or speech. Hundreds of applications. Frequency response 3013-16KH3. Supplied complete with connection diagram and operating notes. Postage & Ins. 20p. FREE All purchasers receive Mullard bookist "Do It Yourself Stereo" tells all you need to know to build your own stereo system. Write today to avoid missing this terrific offer.

HONEYWELL PROGRAMMER

This is a drum type timing device, the drum being calibrated in equal divisions for switch setting purposes with trips which are infinitely adjustable for position.

THERMOSTAT

Continuously variable 30°-90°C. Has sensor bulb connected by 33in of flexible tubing. On operation a 15A 250V switch is opened and in addition a plunger moves through approx. in. This could be used to open valve on valve on ventilator, etc. £1.50 plus 23p

p. & ins. HIGH ACCURACY THERMOSTAT

Uses differential comparator I.C. with thermistor as probe. Designer claims temperature control to within 1/7th of a degree. Complete kit with power pack £5.50.



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NUMICATOR TUBES

For digital instruments, counters, timers, clocks, etc. Hi-vac. XN. 3. Price £1-45 each. 10 for £13.

12-WAY SUB-MINIATURE MULTI-CORE CABLE

7.0076 copper cores each core. P.V.C. insulated and of different colour. P.V.C. covered overall and approx. 3/16in thick. Price **20p** per yard.

From April 1st VAT must VAT be added to total orders.

STANDARD WAFER SWITCHES

£1.20

Standard size 11" wafer—silver-plated 5-amp contact, standard 2" spindle 2" long ~ with locking washer and nut. 2 way 3 way 4 way 5 way 6 way 8 way 9 way 10way 12way 40p 40p 40p 40p 40p 40p 40p 40p 70p 70p 95p 95p 40p 40p 40p 40p 40p 40p 40p 40p 40p 70p 700
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£1.20 £1.70 £1.70 £1.70 £8.20

THYRISTOR LIGHT DIMMER

95p 95p

950

40p

40p 40p 40p 40p 70p 70p 70p 70p 70p 70p

700



For any lamp up to 250W. Mounted on writch plate to fit in place of standard awitch. Virtually no radio interferences. Price 42:95 plus 20p post and insurance. Industrial model 5A with control knob but not mounted on switch plate 43.

HORSTMANN "TIME AND SET" SWITCH



£1-45 Works off dry batteries, car battery or mains power pack. Only **21-45**. This low price

which are infinitely adjustable for position. They are also arranged to allow 2 opera-tions per awitch per rotation. There are 15 changeover micro witches each of 10A type operated by the trips thus 15 circuits may be changed per revolution. Drive motor is mains operated 5 revs per min. Some of the many uses of this timer are Machinery control, Boller fring, Dispensing and Vending machines. Display lighting animated and sigue, Signalling, etc. Price from makers probably over £10 each. Special snip price **£5-75** plus 25p post and insurance. Don't miss this terrific bargain.

MIGHTY MIDGET

Probably the timiest possible radio, as described in Practical Wireless, January 73. All electronic parts £2 post paid.



Very stable and reliable crystal control-led circuit. Capable of work in excess of 13MHz. Construction simplified by use of 15 integrated circuits. Complete kit with case **239**50 or construction data

and price list 50n

DIGITAL COUNTER TIMER

INTEGRATED CIRCUIT BARGAIN

A parcel of integrated circuits made by the famous Plewey Company. A once-insa-lifetime offer of Micro-electronic devices well below cost of manufacture. The parcel contains 5 1Cs all new and perfect. first-grade device, definitely not sub-standard or seconds. 4 of the ICs are single silicon chip GP amplifiers. The 5th is a monolithic NPN matched pair. Regular price of parcel well over 55. Full circuit details of the ICs are included and in addition you will receive a list of many different ICs available at bargain prices 25p upwards with circuits and technical data of each. Complete parcel only 21 Post paid. DON'T MISS THIS TERRIFIC BARGAIN.

TERMS:-10% discount if ten of an item ordered, send postage where quoted other terms post free if order for these over \$6 otherwise add 20p.



EXTRACTOR FAN Cleans the air at the rate of 10,000 cubic ft per hour. Suitable for kitchens, bath-rooms, etc., it's so quici ti can hardly be heard. Compact 54 in casing with 54 in fan blades. Kit comprises motor, fan blades, sheet steel casing, will witch, mains connector. pull switch, mains connector, and fixing brackets, **£2-50** plus 30p post and ins.

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EXTRACTOR FAN

QUICK CUPPA

QUICK CUPPA Mini Immersion Heater, 350W 200/240V. Bolls full cup in about two minutes. Use any socket or lamp holder. Have at hethide for tea, baby's fool, etc. §1.25, host and insurance 14p. 12V car model also available same price. Jug heater \$1.50 plus p. & p. 14p.

MAINS TRANSISTOR POWER PACK

PACK Designed to operate transistor sets and amplifiers. Adjustable output 6V, 9V, 12V for up to 300mA (class B working). Takes the place of any of the following batteries: PP1, PP3, PP4, PP6, PP7, PP9, and others. Kit comprises: mains trans-former, rectifier, sunoching and load resistor condensers and instructions. Real snip at only & lous 20 mostage #1 plus 20p postage.



TREASURE TRACER Complete Kit (except wooden battens) to make the metal detector as the circuit in Practical Wireless, August issue, \$2.95 plus 20p post and insurance.

WINDSCREEN WIPER CONTROL Beat dirty roads, drizzle, fog, etc. Kit of parts to make this useful accessory with circuit details. #2-25.



12 VOLT 14 AMP power PACK This comprises double-wound objective and the standard standard with full wave rectifier and with full wave rectifier and with full wave rectifier and woo mi/f/d smoothing. Price #2 plus post & packing.

ONE CHIP RADIO

Ferranti's latest device ZN414-gives results better than superhet. Supplied complete with technical notes and circuits. **£1-25** each. 10 for \$11

HI-Q TUNER COMPONENTS

For experimenting with the ZN414 Kit No. 1—Plessey Miniature Tuning Condenser with built in LW switch and 3in Ferrit slab and litz wound MW coil. 65p.

Kit No. 2—Air spaced tuning condenser fin ferrite rod, litz wound MW and LW colls, 889. Kit No. 3—Air spaced TC with slow motion drive Sin ferrite rod, with Litz wound LW and MW

coils, £1. Kit No. 4— Permeability tuner with fast and slow motion drive and LW loading coils, 45p.

6 VOLT CLOCK MOTOR Works from 50 cycle mains through condenser, resistor or vtcp-down transformer. This is a synchronoux motor made by Smiths, vo it is an extremely accurate speed controller. Very small in size (2W) and with a polythene cover. Price 30p each. 10 for \$2-70.



SOLDER GUN A must for every busy man, gives almost instant heat also illumi-nated job. 100W \$2.25 plus post and ins. 20p. BIG JOB 250W model \$4.75 plus post and ins. 40p.

MAINS OPERATED SOLENOIDS Model 772—small but power-ful lin pull—approx. size 1 lin x 1 lin x 1 lin 60p. Model 400/1 lin pull. Size 2 lin x 2 lin x 1 in 75p. Model TTI0 1 lin pull, size 3 x 2 l x 2 lin 21.80 plus 20p post and insurance.

3 STAGE PERMEABILITY TUNER



TUNER Male originally for Radiomobile car radios. This is a medium wave time with a frequency coverage lock-252kc. Aerial, RF and oscillator sections (long wave coil available) small size, only $2^{2}_{1} \times 2^{2}_{1}$ jin. Can be used with our 1F module and AF modules and a few inter connection com-lake a complete connect receiver ponents to make a complete compact receiver. Circuit supplied. Price 65p less 10% for 10.

J. BULL (ELECTRICAL) LT (Dept. P.E.), 7 Park Street, Croydon CRO IYD Callers to 102/3 Tamworth Road, Croydon







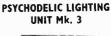
PRACTICAL ELECTRONICS "SCORPIO" ELECTRONIC IGNITION SYSTEM



This Capacitor-Discharge Electronic Ignition system was described in the November and December issues of November and December issues of Practical Electronics. It is suitable for incorporating in any I2V ignition system in cars, boats, go-karts, etc., of either pos, or neg. earth and up to six cylinders. The original coil, plugs, points and contact-breaker capacitor fitted in the vehicle are

plugs, points and contact-breaker capacitor fitted in the vehicle are used. No extra or special com-ponents are required. Helps to promote easier starting (even under sub-zero conditions), improved acceleration, better high-speed performance, quicker engine warm-up and improved fuel economy. Eliminates excessive con-tact-breaker point burning and the need to adjust point and spark-plug gaps with precision. Construction of the unit can easily be completed in an evening and installation should take no longer than half an hour. A complete component of components is supplied with each kit together printed-circuit board, custom-wound transformer and fully-machined disc-cast case. All com-ponents are available separately. Complete assembly and wiring and wiring

Case size 7211 approx. Complete assembly and wiring manual 25p, refundable on purchase of kit. Price: £10:50 plus 50p P. & P.





This unit represents a natural pro-gression from our phenomenally successful Mk. I and 2 Units. As before the drive voltage is derived directly from the amplifier output or across the speakers. The unit converts the audio frequency sig-nals into a three-coloured light display; the colour depending on the frequency of the signal and the intensity on the loudness of the audio source. audio source. The unit is constructed on profes-

audio source. The unit is constructed on profes-sional fibre-glass printed-circuit board material and use latest full-wave triac circuitry. There is a master-level control, together with independent sensitivity controls for each channel. The original minimum ambient light level controls have been redesigned permitting their use as faders; allowing dimming from max to zero at the turn of a knob. R.F.I. suppression is now incorporated as standard as well as provision for D.J. "Pulse-Flash" controls. The choice of two inputs enables operation from both high and low power amplifiers. Max. power 1.5kW per channel at 2404 a.c.

and low power amplifiers. Plax. power 1-SkW per channel at 240V a.c. Complete assembly built and tested. Size 9in × 7in × 3in. Price £25 carr. paid.

PLEASE NOTE ALL THE ABOVE PRICES ARE SUBJECT TO V.A.T. ADJUSTMENT





YATES ELECTRO (FLITWICK) LTD. ELSTOW STORAGE DE KEMPSTON HARDWI BEDFORD	POT
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DEVELOPMENT PACK 0.5 watt 5% Iskra resistors 5 off each value 47Ω to IMΩ. E12 pack 325 resistors £2.40. E24 pack 650 resistors £4.70. POTENTIOMETERS Carbon track 5kΩ to 2MΩ, log or linear (log ‡W, lin ‡W). Single, I2p. Dual gang (stereo), 40p. Single D.P. switch 24p. SKELETON PRESET POTENTIOMETERS	$ \begin{array}{ c c c c c c c c c c c c c c c c c c $
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$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	LARGE (CAN) ELECTROLYTICS 64V 80p 4500μF 16V 50p 1600μF 64V 74p 2500μF 64V 80p 4500μF 16V 50p 2500μF 00V 74p 2800μF 10V 42:60 4500μF 50V £1:68 2500μF 50V 58p 3200μF 16V 50p 5000μF 50V £1:10 HIGH VOLTAGE TUBULAR CAPACITORS—1,000 VOLT 0.01μF 10p 0.47μF 13p 0.22μF 20p 0.022μF 12p 0.1μF 13p 0.47μF 22p POLYSTYRENE CAPACITORS 160Y 21% 160Y 21%
$\label{eq:results} \hline \begin{array}{ c c c c c c c c c c c c c c c c c c c$	10pF to 1,000pF E12 Series Values 4p each. SMOKE AND COMBUSTIBLE GAS DETECTOR—GDI £2 The GDI is the worlds first semiconductor that can convert a concentration of gas or smoke into an electrical signal. The sensor decreases its electrical resistance when it absorbs deoxidizing or combustible gases such as hydrogen, carbon monoxide, methane, propane, alcohol, North Sea gas, as well as carbon-dust containing air or smoke. This decrease is usually large enough to be utilized without amplification. Full details and circuits are supplied with each detector. PRINTED BOARD MARKER 97p Oraw the planned circuic onto a copper laminate board with the P.C. Pen, allow to diry, and immerse the board in the etchant. On removal the circuit remains in high
PRICES ARE CALCULATED ON TOTA	CAS IC'S NOW IN STOCK
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	CES OF IC's ON ALL ORDERS RECEIVED BEFORE THE END OF RCH, 1973 175 174 165 74118 100 82 73 64 16 14 13 74121 41 40 38 15 16 14 13 74141 100 95 90 85 16 14 13 74145 150 140 135 130 16 14 13 74150 330 280 250 220 16 14 13 74151 100 100 95 89 28 25 24 74153 120 100 160 170 160 38 36 30 74155 150 120 100 86 36 312 28 74190 195 190 185 180 155 136 112 105 36 312 200 190 185 180 155 136 112
7421 36 30 17 13 7486 45 7426 32 29 23 20 7490 75 7430 20 18 16 14 7491 A 100 7432 40 36 32 28 7492 75 7441 80 75 70 65 7494 95 7441 80 75 70 65 7494 95 7443 125 120 115 115 7496 100 7443 125 120 15 120 7496 100	42 37 33 LINEAR IC's 67 60 52 709 14 pin DIL 32p 70 65 60 741 8 pin DIL 34p 68 60 52 741 14 pin DIL 28p 90 85 80 723 14 pin DIL 28p 90 85 80 723 14 pin DIL 85p 95 90 85 748 8 pin DIL 85p 95 90 85 748 8 pin DIL 35p 240 235 230 DIL socket, 14 pin and 16 pin 16p

Sinclair Project 60

Now-the Z.50 Mk.2

with built-in automatic transient overload protection

When originally introduced, the Sinclair Z.50 proved how it was possible to design and produce a popularly priced modular power amplifier having characteristics to challenge the world's costliest amplifiers. Many thousands of Z.50's are now giving excellent service day in, day out. But we have also learned that constructors do not always use their Z.50's ideally. That is why we have introduced modifications whereby risk of damage through mis-use, is greatly reduced and performance further enhanced. The Z.50 Mk.2 has improved thermal stability, more accurately regulated D.C. limiting to ensure more symetrical output voltage swing and clipping and still less distortion at lower power. Z.50 Mk.2 is compatible with all other Project 60 modules, and may be incorporated to advantage in existing systems. Eleven silicon epitaxial planar transistors are now used, two more than in the original Z.50, circuitry has been re-designed, making this versatile high performance amplifier better than ever.



the constructor requiring a high fidelity audio system of less power than that available from Z.50's. Using a power supply of 35 volts. Z.30 will deliver 15 watts RMS into 8 ohms. or 20 watts RMS into 3 ohms using 30 volts. Total harmonic distortion is a fantastically low 0.02% at 15 watts into 8 ohms with signal to noise ratio better than 70 dB unweighted. Input sensitivity 250mV into 100K ohms. Size 80 x 57 x 13 mm (3_4^3 x 2_4^3 x 3_3^3 Z.30. Z 50 and Z.50 MK.2 modules are compatible and interchangeable.

Guarantee

If, within 3 months of purchasing any product direct from Sinclair Radionics Ltd., you are dissatisfied with it, your money will be refunded at once. Many Sinclair appointed Stockists also offer this same guarantee in co-operation with Sinclair Radionics Ltd.

Sincial readionics Ltd. Each Project 60 module is tested before leaving our factory and is guaranteed to work perfectly. Should any defact arise in normal use, we will service it at once and without any charge to you, if it is returned within two years from the date of purchase. Outside this period of guarantee a small charge (typically £1.00) will be made. No charge is made for postage by surface mail. Air Mails charged at cost.



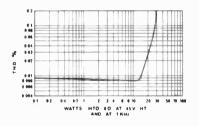
Brilliant new technical specifications

Input impedance $100 \text{ K}\Omega$ Input (for 30w into 8Ω) 400mVSignal to noise ratio, referred to full o/p at 30v HT 80dB or better Distortion 0.02% up to 20W at 8Ω . See curve Frequency response 10Hz to more than $200 \text{ KHz} \pm 1\text{dB}$ Max. supply voltage 45v (4Ω to 8Ω speakers) (50v 15Ω speakers only) Min. supply voltage 9vLoad impedance – minimum. 4Ω at 45v HT

Load impedance -- maximum : safe on open -- circuit



with free manual £5.48

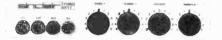


Typical Project 60 applications

System	The Units to use	together with	Units cost
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control, etc.	£4.48
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P.U. volume control, etc.	£9.45
12W. RMS continuous sine wave stereo amp. for average needs	2 x Z.30s, Stereo 60; PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£23.90
25W, RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers	2 x Z.30s, Stereo 60 ; PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck. etc.	£26.90
80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms)	2 x Z.50s, Stereo 60 ; PZ.8, mains transformer	As above	£34.88
Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43

the world's most advanced high fidelity modules

Stereo 60 Pre-amp/control unit



Designed specifically for use on Project 60 systems, the Stereo 60 is equally suitable for use with any high quality power amplifier. Since silicon epitaxial planar transistors are used throughout, a really high signal-to-noise ratio and excellent tracking between channels is achieved. Input selection is by means of press buttons, with accurate equalisation on all input channels. The Stereo 60 is particularly easy to mount.

SPECIFICATIONS—Input sensitivities: Radio – up to 3mV. Mag. p.u. 3mV; correct to R.I.A.A. curve ±1dB.20 to 25,000 Hz. Ceramic p.u. – up to 3mV. Aux – up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE+12 to – 12dB at 104Hz. BASS +12 to –12dB at 100 Hz. Front panel: brushed aluminium with black knobs and controls. Size: 66 x 40 x 207mm.

Built, tested and guaranteed. £9.98

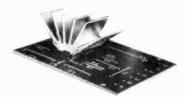
Project 60 Stereo F.M. Tuner



The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other advanced features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stero decoder and switchable squelch circuit for silent tuning between stations. In terms of high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems. SPECIFICATIONS—Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108MHz. Sensitivity: $T_{\rm JV}$ for lock-in over full deviation. Squelch level: $T_{\rm ycall}$ $y_{\rm 201V}$ Signal to noise ratio: \sim 65dB. Audio frequency rasponse: 10Hz - 15KHz ($\pm 1dB$). Total harmonic distortion: 0.15% for 30% modulation. Stereo decoder operating level: 2μ . Cross talk: 40dB. Output voltage: 2x 150mV R.M.S. maximum Operating voltage: 25-30VDC. Indicators: Stereo on: $293 \times 40 \times 207m$.

Built and tested. Post free, **£25**

Super IC.12 Integrated circuit high fidelity amplifier



Having introduced Integrated Circuits to hi-fi constructors with the IC.10, the first time an IC had ever been made available for such purposes, we have followed it with an even more efficient version, the Super IC.12, a most exciting advance over our original unit. This needs very few external resistors and capacitors to make an astonishingly good high fidelity amplifier for use with pick-up, F.M. radio or small P.A. set up, etc. The free 40 page manual supplied, details many other applications which this remarkable IC. make possible. It is the equivalent of a 22 transistor circuit contained within a 16 lead DIL package, and the finned heat sink is sufficient for all requirements. The Super IC.12 is compatible with Project 60 modules which would be used with the Z.50 and Z.30 amplifiers. Complete with free manual and printed circuit board.

SPECIFICATIONS

Output power: 6 watts RMS continuous (12 watts peak). δ -80. Frequency Response: 6Hz to 100KHz \pm 1d8. Total Harmonic Distortion: Less than 1%. (Typical 0-1%) at all output powers and frequencies in the audio band (28V). Load Impedence: 3 to 15 ohms. Input Impedance: 250 Kohms nominal. Power Gain: 90d8 (1.000,000,000 times) after feedback. Supply Voltage: 6 to 28V. Quiescent current: 8mA at 28V. Size: 22 × 45 × 28mm including pins and heat sink.

Manual available separately 15p post free.

With FREE printed circuit board and 40 page manual. **£2.98** Post free

Power Supply Units The new

PZ.8 Mk.3



The most reliable power supply unit ever made available to constructors. Brilliant circuitry makes failure from over load and even direct shorting of the output impossible. This is due to an ingenious re-entrant current limiting principle which, as far as we know has never before been available in any comparable unit outside the most expensive laboratory equipment. Ripple and residual noise have been reduced to the point of almost total elimination. This is, of course, the perfect unit for Project 60 assemblies, particularly where the new Z.50 MK.2 amplifiers are used. Nominal working voltage – 45.

PZ.8 Mk.3-£7.98

(Mains transformer, if required) £5.98

PZ.5 30v. unstabilised (not suitable for Project 60 tuner) £4.98

PZ.6 35v. stabilised (not suitable for IC. 12) £7.98



Project 60b in one pack contains, one PZ 5, two Z.30's, one Stereo 60 and one Masterlink, which has input sockets and output components grouped on a single module and all necessary leads cut to length and fitted with clips to plug straight on to the modules thus eliminating all soldering.

Complete with comprehensive manual, post free All you need for a superb 30 watt high fidelity stereo amplifier

Order form

Please send

Name

Address

PE/4/73

£29.95

SINCLAIR RADIONICS, Business Reg. No. 699483 : London Rd, St. Ives, Hunts, PE17 4HJ





PHOTOELECTRIC KIT

CONTENTS. P.C. Chassis Board, Chemicals, Etching Manual, Infra-Red Phototransistor, Latching Relay, 2 Transistors, Diode, Resistors, Gain Control, Terminal Block, Elegent Case, Screws, etc. In fact everything you need to build a Steady-Light Photo-Switch/Counter/Burglar Alarm, etc. (Project No. 1) which can be modified for modulated-light operation with a few additional components.



YORK ELECTRICS Mail Order Dept. 335 BATTERSEA PARK ROAD, LONDON, S.W.11 Send S.A.E. for full details, a brief description of all Kils and Projects

COMPARE (paker Bargains E.M.I. 13in × 8in 3, 8 & 15 ohns plain with tweeter 2:25	ACOS GP91/28C or GP91/38C stereo compatible 1-05 ACOS GP94 stereo ceramic 1-75 ACOS (FP95 stereo crystal 1-85
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k of age 2.0 per apleased 50 2 jin 8 or 64 ohm 7.1. Ipp 50 Kit-torm cabinets, teak 50 (17in \times 10in \times 6in) 2.75 with a 13in \times 8in or 8in ent out 2.75 (12in \times 12in 6in) with a kin of 8in ent out 2.25 (j)lease specify cut out) 2.25 Add 36p per Cabinet for post & packing	Battery Eliminators 240v input 6 or 9v d.c. ontput at 150 mA 240v input 6, 7 J or 9v output at 300 mA 299 12v d.c. input (for cars) 6, 7 J or 9v d.c. output at 300 mA 2.99 P. & P. 10p
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AC107 30p BCY AC126 20p BCY	70 150 CA3044	£1-73 0A81 £1-42 0A90	8p 1N4007 8p 1N4148	19p 2N6027(E	45 p	Vo	oltage			Voltage	
AC127 25p BCY	72 15p CA3048	86p () A91 £2 34 () A95	5p 1N5400 5p 1N5404	14p 3N84 18p 3N128	£1-30 88p	1-0 1-0	40v 100v	7p 5p	100 100	16v 25v	6p 6p
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AC152 15p BDY AC153 19p BF11	20 92p CD4001AE 5 23p CD4000AE	72p OC28	70p 1S5009 76p 1S5012	80 p 7400 80 p 7401	16p	10	63v	5p 6p	470 1000	25v	9p 12p
AC176 16p BF16 AC153/176K 32p BF16	3 35p CD4011AE 7 18p CD4012AE	72p OC35	60p 1S5015	75p 7402	20 p 20 p	22	25v 40v	6p	2200	25v 25v	16p 30p
AC187 17p BF17 AC188 23p BF17	7 25n CD4015AE	\$1.48 OC41	63p 1S5018 40p 1S5024	75p 7403 75p 7404	20 p 25 p	47 47	25v 40v	6p 6p	4700	16v	33 p
AC187/188K 40p BF17	8 31p CD4015AE	£3.90 OC42	40p 1 55047 20p 2 N404	23p 7405 23p 7408	25 p 25 p	CAPACI	TORS-		LLISE	D POLYES	TER
ACY18 20p BF19	4 15p CD4018AE	£4-34 0C45	20p 2N696 20p 2N697	15 p 7409 17 p 7410	25 p 20 p	Stock values 0.01, 0.015, 0	: MFD				ice each 3p
ACY19 20p BF19 ACY20 20p BF19	6 15p CR1/051C	45p 0C72	20p 2N698 25p 2N706	30p 7413 10p 7420	30 p	0.047, 0.068, (4p
ACY21 19p BF20 ACY22 10p BF25	4 14p CRS3/05A	F 0C/6	25p 2N706A 40p 2N708	12p 7425	20 p 30 p	0-33					5p 7p
AD140 55p BF25 AD149 50p BFX1	5 15p	£1.08 Con	20p 2N911	16p 7430 50p 7440	20 p 24 p	0.68					8p 11p
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AD161/162 70p BFX8 AF106 24p BFX8	15 34p D10 (NTG		25p 2N929 25p 2N930	250 7444 280 7445	£1-45 £2-06	2-2 Order as "Pe	olyesters''	+ Capaci	tance.		24p
AF114 25p BFX8	7 30p IRT84	£2.90 OC140	35p 2N1131 25p 2N1132	24p 7446 24p 7447	£1-45 £1-25	CAPACI				ENE	
AF115 25p BFX8 AF116 25p BFY5	150 10700010	42P OC171	30 p 2N 1302	17p 7450	20 p					erance. 160 volt	
AF117 25p BFY5 AF118 44p BFY5	1 15p LIC723C/5 2 15p LIC723C/14	£1.02 ORP12	50p 2N1304	17p 7451 24p 7453	20 p 20 p	Stock values	200-5	20.5	-E	E 600 E 600	Price each
AF124 25p BFY5 AF125 24p BFY9	5 I/PLIC/4/C/5	45P ORP61	40p 2N1305 40p 2N1306	24 p 7454 30 p 7460	20 p 20 p	1000pF, 150pF	pF, 2200pF,	3300pF, 470	700pF, 5	F, 680pF, 820 600pF, 6800pF,	рF, 3р
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AF186 40p BRY3 AF239 36p BSX1	39 40p MC1307P	£1-65 PN107	9p 2N1309 7p 2N1559 (C	34p 7473 R1/ 7474	45p	ALUMIN 10DN 34p (PI	lain Ali un	drilled)			
AF279 47p BSX2 ASY26 25p BSX2	20 16p MC1312P	£2.75 PN100	7p 401C) 7p 2N1613	60 p 7475 15 p 7476	45p 45p	10DDR 43p (
ASY27 30p BSY2	7 20p MC1352P	£2.00 PN3019(2	20 p 2N1711 20 p 2N1893	15p 7480	67p	DRD 7 14 Pir					
ASY28 22p BSY2 ASY29 30p BSY9	5A 12p MC4044P	£2 20 £2 20 ST2	28n 2N2218	54p 7482 33p 7483	87p £132		_				
BA138 15p BY10 BAX16 8p BY12	0 20p MFC6030 7 22p MFC6040	£1-63 SL103A £1-15 SL403A	50p 2N2218A (Rect) 2N2219	44 P 7486 38 P 7490	33p 60p	NYLON Cheese head	d screw bo	olts. Nuts	with in	tegral washer.	Moulded
BB103 16p BTY7 BB104 28p BT106	9/400R 92p MFC8010	£1-38	80p 2N2368	53p 7491 A 17p 7492	£1-28 85p	in high den power transi	sity nylon	. Ideal fo	r mount	ing "live" as	semblies,
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BC107/BC177 BZY8	8C3V9 13p MJE520 8C4V3 13p MJE521	65 n A A 203	75p 2N2484 97p 2N2646	42p 7495 45p 7496	80 p	HSN1 HSN3	6BA 6BA	1 Leng	g = 1 1	4 4	10p
BC108 10n BZV8	9CAV7 1to ALLEGORE	62p TAA293 £1 06 TAA310	£1 25 2N2904	44p 74100 49p 74107	£1-48 £1-64	Order as "N	uts and Boi		ck No.	•	10p
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BC159 12p BZY8 BC147/157 22p BZY8	8C16V 13p MPF103(2N 8C18V 13p MPF104(2N 8C20V 13p MPF104(2N	49p VA1000s	15p 2N3703	9p 74193 9p 74196	£1-74 £1-50	Metal Oxide	resistors	by Electr	osti. Uli	ra low noise	¥ Watt,
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BC179 14p BZX6'	1C10V 23p NKT216	46p ZTX107 50p ZTX108	12p 2N3819	25p 40360 60p 40361	56p 45p	characteristic	cs and long	⊒life. Tole	erances.	ranges and wa	ttages as
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BC1831 10p BZX61	C15V 230 NKT271	18n ZTX303	15p 2N3004	£1 10 40407 28p 40408	40p 54p	UPM050 0)-5 5 1-5 10	0% 1M	-1M -4·7M	E12	1p each 1p each
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BC212 120 BZX61	C20V 230 NKT281	12p ZTX320 29p ZTX330	30p 2N4058 18p 2N4060	11p 40430	£1-22		-00 10	0% 10E	-1M		p each
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BCY34 25p CA302 BCY38 30p CA303	28A 88p OA47	8p 1N4005 8p 1N4006	12p 15p 2N5777	46p 40673 45p 40739	68p £1-50					100	6.96
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19 19 <t< th=""><th>Ref. VA Weight Size cm. P & P No. (Wotts) Ib oz £ b</th><th>400V: (μF) 0.001, 0.0015, 0.0022, 0.0033, 0.01, 2p; 0.015, 0.033, 3p; 0.068, 4p.</th></t<>	Ref. VA Weight Size cm. P & P No. (Wotts) Ib oz £ b	400V: (μF) 0.001, 0.0015, 0.0022, 0.0033, 0.01, 2p; 0.015, 0.033, 3p; 0.068, 4p.
	07 20 7'0× 6'0× 6'5 6 30 100 60 3 8 8'9× 8'0× 7'7 2.39 36 6 100 5 2 0'2× 8'9× 8'3 2.62 52	MULLARD C437: (µF/V) 64/64, 9p; 160/25, 9p; 160/40, 11p; 040/014, 9p;
1 1	62 250 12 4 9·5 × 12·7 × 11·4 5·80 67 55 350 15 0 14·0 × 10·8 × 12·4 7·77 82	1600/6-4, 149. ELECTROLYTIC CAPACITORS. Tubular and large can (μF/V) 2:5/50, 3p; 4/10, 10/25, 16/15, 20/25, 25/15, 25/25, 40/6, 64/10, 200/6.
1 1	92 1000 40 0 17.8 × 17.1 × 21.6 20.63 * 128 2000 63 0 24.1 < 21.6 × 15.2 34.10 *	250/10, 4p; 10/6, 10/50, 25/50, 32/50, 50/10, 64/25, 100/25, 5p; 50/50, 64/40, 250/15, 1,000/3, 6p; 100/50, 250/25, 400/10, 500/10, 500/12, 640/10, 1,000/6, 8p; 500/25, 10p; 500/50, 12p; 1,000/12, 10p; 1,000/12, 2,000/12, 2,500/12, 15p; 300/25, 10p; 500/25, 10p; 500/50, 12p; 1,000/12, 10p; 1,000/25, 2,000/12, 2,500/12, 15p; 300/25, 2,000/12, 2,000/12, 2,000/12, 300/25, 2,000/12, 2,0
4 30 10 20 40 30 10 <td< th=""><th>Ref. VA Weight Size cm. Auto Taps P&P</th><th></th></td<>	Ref. VA Weight Size cm. Auto Taps P&P	
¹ / ₂ <t< th=""><th>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</th><th>50V: (pF) 22, 27, 33, 39, 47, 56, 68, 82, 100, 120, 150, 180, 220, 270, 330, 390, 470, 560, 680, 820, 1K, 1K5, 2K2, 3K3, 4K7, 6K8. (µF) 0.01, 0.015, 0.022, 0.033, 2p. 0.047, 30V, 3p. 0.1, 1, 100V, 5p.</th></t<>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	50V: (pF) 22, 27, 33, 39, 47, 56, 68, 82, 100, 120, 150, 180, 220, 270, 330, 390, 470, 560, 680, 820, 1K, 1K5, 2K2, 3K3, 4K7, 6K8. (µF) 0.01, 0.015, 0.022, 0.033, 2p. 0.047, 30V, 3p. 0.1, 1, 100V, 5p.
13 13 <t< th=""><th>67 500 12 8 14·0 × 10·2 × 11·4 5·78 67 84 1000 16 0 11·4 × 14·0 × 14·0 10·49 82</th><th>IM, Ip each or 100 for 55p; 1,000 for £4. METAL FILM RESISTORS IW 5% 22 ohms—10M, Itp each or 100 for £1.</th></t<>	67 500 12 8 14·0 × 10·2 × 11·4 5·78 67 84 1000 16 0 11·4 × 14·0 × 14·0 10·49 82	IM, Ip each or 100 for 55p; 1,000 for £4. METAL FILM RESISTORS IW 5% 22 ohms—10M, Itp each or 100 for £1.
And wild wild work wild be dated a transformer between the comparison of the property and the	95 2000 40 0 17.8 × 16.5 × 21.6 19.84 * 73 3000 45 8 17.4 × 18.1 × 21.3 26.99 *	24 × 5in 25p 25p IN4002 7n SPECIAL BULK BUY PRICES
Arrive Low youth to be a part of the part of th	115V 500 Watt totally enclosed auto transformer, complete with mains lead and two 115V outlet sockets, £7.87, P & P 67p.	34 × 32 in 25p 25p IN914 6p PROJECTS
Product	LOW VOLTAGE SERIES (ISOLATED) PRIMARY 200-250 VOLTS 12 AND/OR 24 VOLT RANGE	5×3±in (plain) — 40P OCR3 IBn April I
1 1 1 0	No. 12V 24V lb oz	Track cutter 40p 40p Screened wire, yd. 5p Pins, pkt. 25 8p 8p Twin screened wire, yd. 9p Screened wire, yd. 9p
19 8 3 9 9 8 3 9 9 9 8 3 9	71 2 1 1 0 7 $\cdot 0 \times 6 \cdot 4 \times 5 \cdot 7$ 0 2 2 4 8 3 \times 7 $\cdot 0 \times 7 \cdot 0 \times 12$ V at 1A $\times 2$ 1 33 2 2 18 4 2 2 4 8 3 \times 7 $\cdot 0 \times 7 \cdot 0 \times 7 \cdot 0$ 2 1 2 V at 2A $\times 2$ 1.86 36 7 0 6 3 3 12 10 $\cdot 2 \times 7 \cdot 6 \times 8 \cdot 6$ 0 -12 V at 2A $\times 2$ 2.24 42	2 pin DIN Plug, 12p: Skt. Quad screened wire vd
Participanti Pa	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	B0°, ISp; Skt., IZp. Iran- sistor Equiv. Book, 40p. Carbon pots SK-2M log, & C.W.O. only. P. & P. IOp on orders below £5.
Area August models P & P 19 0.5 1 9 2.5 7.4 0.1 1.3 2.4 2.4 1.3 2.4 2.4 2.4 1.3 2.4	187 30 15 16 12 13 3 × 12 1 × 12 1 0-12 V at 15A × 2 10-67 82	switch 24p, dual 42p. Export Order enquiries welcome
1 1	Ref. Amps. Weight Size cm. Secondary Taps P & P No. Ib oz	Near LEIGHTON BUZZARD, BEDS. LU7 9AQ Tel.: Cheddington 668446 STD. (0296)
21 40 60 102 100 85 124 52 19 60 100 140 17 146 52 19 100 140 17 146 52 19 100 12 140 17 146 52 100 12 140 17 146 52 100 12 140 17 146 52 100 12 140 17 70	79 1·0 2 0 7·0 × 6·4 × 6·0 1·35 36 3 2·0 3 2 8·9 × 7·0 × 7·6 2·01 36	
B9 80 10 0 140 17 46 71 67 Ref. Amps. Weight Size cm. Size ondory Tops 4 67 71 67 10 10 12 140 10 <t< th=""><th>21 4·0 6 0 10·2 × 10·0 × 8·6 2.94 52 51 5·0 6 8 12·1 × 10·0 × 8·6 3·66 52</th><th>250y 50 Hz-150 watt Inverter. Full kit of parts excluding meter. Circuit</th></t<>	21 4·0 6 0 10·2 × 10·0 × 8·6 2.94 52 51 5·0 6 8 12·1 × 10·0 × 8·6 3·66 52	250y 50 Hz-150 watt Inverter. Full kit of parts excluding meter. Circuit
Ref. Amps. Weight Size cm. Secondary Taps P & P 103 10 10 93 × 73 × 70 109 23 × 109 P & P 103 104 10 93 × 73 × 70 109 23 × 109 P & P 103 104 10 93 × 73 × 70 109 24 × 109 × 80 × 104 × 103 × 104 × 103 × 104 × 103 × 104 × 103 × 104 × 103 × 104 × 103 × 104 × 103 × 104 × 103 × 104 × 103 × 104 × 103 × 104 × 10	88 8·0 10 0 14·0 × 11·7 × 10·0	OTHER INVERTERS AVAILABLE IN KIT FORM
103 10 2 10 83 × 73 × 70	Ref. Amps. Weight Size cm. Secondary Taps P & P No. Ib oz £ p 102 0-5 1 11 7-0 × 7-0 × 5-7 0-19-25-33-40-50 × 1-33 30	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
1001011	103 10 2 10 83 7.3 70 1.94 36 104 2.0 5 0 10.2 × 8.9 × 8.6 2.69 42 105 3.0 6 0 10.2 × 10.2 × 8.3 3 3.65 52	24 volt types are also available, alternative outputs or taps can be supplied.
60 YOLT RANGE StreemRef. Amps. WeightSize m. 124 0 5 2 4 83 × 95 × 67 0-24-30-40-46-60V1.38 3 1.38 3 124 10 10 2 89 × 76 76 1.28 3 3 123 10 10 2 89 × 76 76 124 30 10 11 2 8 30 10 2 89 × 76 76 124 30 10 11 2 8 30 10 2 89 × 76 76 124 30 10 11 2 8 30 10 2 89 × 76 76 76 124 30 10 11 2 8 30 10 2 89 × 76 76 76 124 30 10 11 2 8 30 10 2 89 × 76 76 76 124 30 10 11 2 70 × 70 × 60 % 124 30 10 10 12 70 × 70 × 60 % 124 10 10 2 70 × 60 × 60 % 124 10 10 2 70 × 60 × 60 % 124 10 10 2 70 × 60 × 60 % 124 10 10 10 2 70 × 60 × 60 % 124 10 10 2 70 × 60 × 60 % 124 10 10 2 70 × 60 × 60 % 124 10 10 2 70 × 60 × 60 % 124 10 10 2 70 × 60 × 60 % 124 10 10 2 70 × 60 × 60 % 124 10 10 10 10 10 2 70 × 60 % 124 10 10 10 2 70 × 60 % 60 % 124 10 10 10 10 10 2 70 × 60 % 60 % 124 10 10 10 10 10 2 70 × 60 % 60 % 124 10 10 10 10 10 10 10 10 10 10 10 10 10	107 6·0 12 4 12·1×11·1×13·3 7·14 67 118 8·0 18 9 13·3×13·3×12·1 9·32 97	SPECIAL OFFER
1240.5248.39.56.70.24-30-40-46-60V13535125100199.57.61.443.5141.5144151251010161.149.51.141.3<	Ref. Amps. Weight Size cm. Secondary Taps P & P	lighting for factories, hotels, etc. 12 inch—8 watt—£3:40 post paid.
125 30 8 6 114 9 5 10 5 74 57 67 120 60 16 12 133 12 138 52 138 52 LEAD ACID BATTERY CHARGER TYPES Ref. Amps. Weight Size continuous 138 5 138 5 138 5 14 90 132 102 102 102 102 102 114 123 102 138 14 102 14 102 138 14 102 102 114 133 103 102 102 114 133 103 103 116 113 103 103 103 103 103 103 103 103 103 161/162 60 134 103 103 103 103 103 103 103 103 103 103 103 103 103 100 100 100 100 100 100 100 100 100 100 100 100 100 1	124 0.5 2 4 8.3 × 9.5 × 6.7 0.24-30-40-48-60V 1.35 36 126 1.0 3 0 8.9 × 7.6 × 7.6 1.88 36	Fibre glass P.C. board-£2:00 + 10p P. & P.
122 100 23 2 165 × 127 × 165 13.85 13.85 14.95	125 3·0 8 8 11·9× 9·5×10·0 4·48 52 123 4·0 10 6 11·4× 9·5×11·4 5·78 67	Other components including Teak Cabinet—£24:00 + Postage.
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FULL SPEC. TRANSISTORS BC107/108/109 9-9p each 25+ 7p 100+ 6-5p Pices this range. 2N 3053 68p each 25+ 35p 50+ 40p AD 16/162 60p pair trics and bushes 25+ 35p 500+ 40p AD 16/162 60p pair trics and bushes 25+ 35p 500+ 40p SCORPIO ELECTRONIC 500+ 40p COMPLETE KIT WITH ALL PARTS AND COMPREHENSIVE CONSTRUCTION AND FAULT FINDING DATA AVOMETERS · MAINS KEYNECTOR ELECTROSIL RESISTORS CARRIAGE VIA BRE COMPLETE KIT 004 ELECTROSIL RESISTORS COMPLETE KIT 004 ELECTROSIC 004 COMPLETE KIT 004 ELECTROSIC 004 AU 16/100 AU BARRELE CLOCOLL RESISTORS *CARRIAGE VIA BRE *CARRIAGE VIA BRE COMPLETE KIT 004 ELECTROSIC 004 COMPLETE KIT 005 ELECTROSIC FOOSCARD BARRELE CLOCOLL RESISTORS *CARRIAGE VIA BRE *CARRIAGE VIA BRE E2:00 + V.A.T	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	AMC ELECTRONICS ITD
^{500 + 40p} ^{100 + 45p} ^{100 + 45p} ^{100 + 45p} ^{100 + 40p} ^{100 +}	tags and wax impregnation. Enclosed styles to order.	
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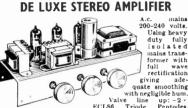
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 Infl. wave rectification is rectification giving ade-quate smoothing with negligible hum. Valve line up: -2 · ECL56 Triode Pentoiles.
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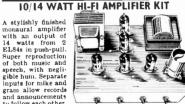


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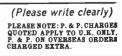
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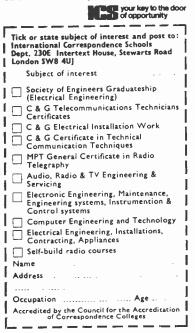
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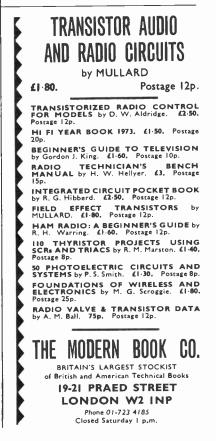
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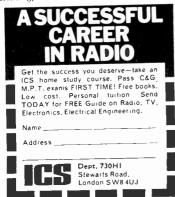
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 47μF: ±0% OD: ±2% 90D: ±1% 81.80 67μF: ±0% 81.91: ±2% 81.40; ±1% 81.80 10μF: ±0% 81.40; ±2% 81.80 10μF: ±1% 81.80 10μF: ±0% 81.40; ±2% 81.80 10μF: ±1% 10μF: ±1% 81.80 10μF: ±1% 10μF: ±1% 81.80 10μF: ±1% 10μF: ±1% 10μF: ±1% 81.80 10μF: ±1% 10μF: ±1% 10μF: ±1% 81.80 10μF: ±1% 10μF: ±1%	
TANTALUM BEAD CAPACITORS. Vilue: available 0:1, 0:22, 0:47, 1:0, 2:2, 47, 6:8µF at 38V, 10µF 25V, 15µF 20V, 22µF 15V, 33µF 10X, 47µF 6V, 100µF 3V—all at 9p each; 6 for 50p; 14 for 41. Special pack 6 off each value (78 capacitors) 45. NEW 1—TRANSISTORS. BC107, BC108, BC109, All at 9p each; 6 for 50p; 14 for 41. All brand new and marked. Full spec. devices. May be mixed to qualify for quantity prices. AF178 — 40p each; 3 for 41. POPULAR DIODES, IN914, 7p each; 8 for 50p; 18 for 41. IN916, 5p each; 6 for 50p; 14 for 61. Special offer 6 off each voltage (66 zeners) 44. NEW LOW PRICE — 400 mW Zeners, Values available 47, 5:6, 6:8, 7:5, 8:2, 9:1, 10, 11, 12, 13:5, 15V. To1, ±5% at 5mA. All new and marked. Price 10p each; 6 for 50p; 14 for 61. Special offer 6 off each voltage (66 zeners) 64-50, RESISTORS. Carbon film 5%, 4W at 40°C, 4W at 70°C, Range from 2:20 to 2:2/M1 in E12 series, 1.e. 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decade. High stability, low noise. All at 1p each; 8p for 10 of any one value; 70p for 100 of any one value; 50p each; 64 for 50p. Special pack, 50p each; 64 for 50p. Special pack in 53p; 1:0µF, size 21m X in, 45p; 3:0µF, size 21m X in, 35p; 1:0µF, size 21m X in, 45p; 3:0µF, size 21m X in, 5p; SULCON PLASTIC RECTIFIERS 1:5A— Brand new wire-ended DO27. 100P1V at 8p each or 4 for 30p; 400P1V at 9p each or 4 for 30p; 400 pack, E2, The Maitings, Station Road Werm, Shropshire COMPUTER PARELS. 9in X 71in long lead Trans, and Compa, E6, 8 Trans, 28p (10p); E43, 16 Trans, 40p (10p); E47, 10 Trans, 30p (10p). Bank of 3w with 5 C407 Driver Trans, 45p (10p); E43, 16 Trans, 40p (10p); E47, 10 Trans, 30p (10p). 20 was STEPPING SWITCH with Reeet, Mains Operation, 80p (15p). SP JOURE REBETTABLE COUNTER. 13/22V, will work on 12V, 42 (15p). SILICON DIODES 650V 14A. 10 on Tagboard, 30p (15p). Bank of 3w AS ABOYE, £1-25 (25p). CROUZET GEARED MOTOR. Mains, 15 r.p.n., aclw., 75g (16p). STIGUER REBETTABLE COUNTER. 13/20V, will work on 12V, 42 (15p).	L 4・7//ド・ エ5% 20m・ エク% 90m・ エ1% 41.35
available 0-1, 0-22, 0-47, 1-0, 2-2, 4-7, 6-8µF at 35V, 10µF 25V, 15µF 20V, 32µF 15V, 33µF 10V, 47µF 6V, 100µF 3V—all at 9p each; 6 for 50p; 14 for 61. Special pack 6 off each value (78 capacitors) 65. NEW 1—TRANSISTORS. BC107, BC108, BC109, All at 9p each; 6 for 30p; 14 for 61. All brand new and marked. Full spec. devices. May be mixed to qualify for quantity prices. AF178 — 40p each; 3 for 41. POPULAR DIODES. IN914, 7p each; 8 for 50p; 18 for 61. IN916, 6p each; 6 for 50p; 14 for 61. 1544, 5p each; 11 for 50p; 24 for 61. All brand new and marked. NEW LOW PRICE — 400 mW Zaners. Jans earlie 4-7, 56, 68, 7.5 2, 9-1, 10, 11; 12, 13, 5V, 150, 14, 50% at 5mA. All new and marked. Price 10p each; 6 for 50p; 14 for 61. Special offer 6 off each voltage (65 reares) 44-50. RESISTORS. Carbon film 5%, 4W at 40°C, 4W at 70°C, Range from 2:20 to 2:2/M1 in El 2 series, i.e. 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. High stability, low noise. All at 1p each; 8p for 10 of any one value; 70p for 100 of any one value; 50p; 14 for 41. Special offer 6 and 20 registors) 65. Hat 1p each; 8p for 10 of any one value; 70p for 100 of any one value; 50p; 10 of 47 and 05µF, size 1in X jin, 30p; 1-0µF, size 1in X jin, 45p; 3:0µF, size 1in X jin, 30p; 0-47 and 05µF, size 1in X jin, 30p; 10 dr 41 05µF, 100PH Az 14p each or 4 for 50p. Sp post and packing on all orders below 25. MARCO TRADING (Formerly V. ATTWOOD) Dept: E2, The Maltings, Stacion Road Wern, Shropshire COMPUTEE PANELS. 91 no 745p (10p). MIRE DOLYSTYRENE, 81 no 745p (10p). MIRE 200LYSTYRENE, 81 no 745p (10p). MIRE 40 WAY AS ABOYE, 41-25 (25p). CROUZET GEARED MOTOR. Mains, 13 r.p.m., a.cl.w., 759 (15p). Sti AASORTED COMPONENTS, 11-50. HASSORTED COMPONENTS, 134 NORTH END (DA	10µr. ±0% area, ±3% as 10, ±1% as 10
Capacitors) 4.5. NEW 1-TRANSISTORS. BC107, BC108, BC109, All at 9p each; 6 for 30p; 14 for £1. All brand new and marked. Full spec. devices. May be mixed to qualify for quantity prices. AF178 - 40p each; 3 for £1. POPULAR DIODES, IN914, 7p each; 8 for 50p; 18 for £1. IN916, 8p each; 6 for 50p; 18 for £1. POPULAR DIODES, IN914, 7p each; 6 for 50p; 18 for £1. NEW LOW PRICE - 400 mW Zeners. NEW LOW Sector States and the sector of the sector	TANTALUM BEAD CAPACITORS. Values available 0·1, 0·22, 0·47, 1·0, 2·2, 4·7, 6·8μF at 35V 10μF 25V 15μF 20V 22μF 15V 33μF 10V
Capacitors) 42. NEW 1-TRANSISTORS. BC107, BC108, BC109, All at 9p each; 6 for 30p; 14 for £1. All brand new and marked. Full spec. devices. May be mixed to qualify for quantity prices. AF178 - 40p each; 3 for £1. POPULAR DIODES, IN914, 7p each: 8 for 50p; 18 for £1. IN916, 8p each; 6 for 50p; 14 for £1. 1544, 5p each; 11 for 50p; 24 for £1. All brand new and marked. NEW LOW PRICE - 400 mW Zeners. Values available 47, 56, 66, 75, 52, 91, 10, 11, 12, 135, 15V. To1. ± 5% at 5mA. All new and marked. Price 10p each; 6 for 50p; 14 for £1. Special offer 6 off each voltage (66 zeners) £4.50, RESISTORS. Carbonfilm 5%, 4W at 40°C, 4W at 70°C, Ramge form 2:20 to 2: 2M10 in E12 series, i.e. 10, 12, 15, 16, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. High stability, low noise. All at 1p each; 8p for 10 of any one value; 70p for 100 of any one value; 50p each or 4 for 50p, 13 for 35µf, 5ize 13in × £in, 30p; 047 and 05µf, size 18in × £in, 30p; 10µf, 5ize 21in × £in, 45p; 20µf, size 2in × 1 in 75p. StlLCON PLASTIC RECTIFIERS 1:5A- Brand new wire-ended DO27. 100P114 at 8p each or 4 for 30p; 400P1V at 9p each or 4 for 50p. 5p post and packing on all orders below £5. MARCO TRADING (Formerly V. ATTWOOD) Dept: E2, The Maltings, Station Road Werm, Shropshire COMPUTER PARELS. 9 in x 71 in long lead Trans. and Compa. E6, 8 Trans., 28p (10p); E43, 16 Trans., 40p (10p); E47, 10 Trans., 30p (10p). AMERICAN PARELS. 4 for 60p (12p) with data. M.C. METERS. 2-3in, three assorted, 21-05 (25p). 22 WAY STEPPING SWITCH with Renet, Mains Operation. 80p (15p). NEW 46 WAY AS ABOYE, £1-25 (25p). CROUZET GEARED MOTOR. Mains, 15 r.p.m., a.cl.w., 75g (16p). S HAYFEED DAEONS. 10 for 75g (10p). SOPPEE CLAD PAX. PARELS. 3(in x 3in) 15 or 30p (10p). NEW 46 WAY AS ABOYE, 12-85, 120, 100 pr fo 7012, 20p dosen; 0-013 to 0-068, 30p dozen (if vortered along). MIXED POLYSTYRENE/S. MICA CAPS. 100 for 15p. ASSORTED COMPORENTS, 12-50. 15 ASSORTED COMPORENTS, 124, 100 mords. 40p 15 DASORTED COMPORENTS, 124, 10	47μ F 6V, 100μ F 3V—all at 9p each; 6 for 50p; 14 for £1. Special pack 6 off each value (78
De mixed to quanty for quantity prices. Arive 40p each; 3 for 41. POPULAR DIODES. IN914, 7p each; 8 for 50p; 18 for 41. IN916, 8p each; 6 for 50p; 14 for 41. 1544, 5p each; 11 for 50p; 24 for 41. All brand new and marked. NEW LOW PRICE - 400 mW Zeners. Values available 47, 5c, 66, 75, 52, 52, 91, 10, 11, 12, 13-5, 15V. Tol. ± 5% at 5mA. All new and marked. Price 10p each; 5 for 50p; 14 for 41. Special offer 6 off each voltage (66 zeners) 64-50. RESISTORS. Carbon film 5%, 4V at 40°C, 4W at 70°C. Range from 2-20 to 2-2M0 in E12 series, i.e. 10, 12, 15, 16, 22, 27, 33, 59, 477, 56, 68, 97, 58, 68, 75, 16, 10, 12, 15, 16, 22, 27, 33, 59, 477, 56, 68, 90, 10 their decades, High atability, low noise. All at 19 each; 59 for 00 of any new size 20 to 2-2M0 in E12 series, i.e. 10, 12, 15, 16, 22, 27, 35, 19, 477, 56, 68, 90, 10 their decades, High atability, low noise. All at 19 each; 59 for 00 of any provide the for 30 provide the for 30 provide the first 41, 35p; 1-0, 47, size 21m X fin, 45p; 2-0, 47, size 21m X fin, 35p; 1-0, 47, size 21m X fin, 45p; 2-0, 47, size 21m X fin, 35p; 1-0, 47, size 21m X fin, 45p; 2-0, 47, size 21m X fin, 35p; 1-0, 47, size 21m X fin, 45p; 2-0, 47, 107 Tanas, 30p (10p). Sp post and packing on all orders below C5. MARCO TRADING (Formerly V. ATTWOOD) Dept. E2, The Maltings, Station Road Werm, Shropshire COMPUTER PARELS. 9in X 7in long lead Trans, and Compa, E6, S Trans, 25p (10p); E45, 16 Trans, 40 (10p); E47, 10 Tanas, 30p (10p). AMERICAN PANELS. 10 for 65 (25p). AMERICAN PANELS. 10 for 65 (25p). AMERICAN PANELS. 10 for 65 (25p). Bank of 30 with 5 C407 Driver Trans, 45p. Bank of 30 with 5 C407 Driver Trans, 45p. (10, DIDER 560V 1jA. 10 on Tagboard, 30p. (5p)	Capacitors) 12.
 −40p each; 3 for 1. POPULAR DIODES, IN914, 7p each; 8 for 50p; 14 for 4. POPULAR DIODES, IN914, 7p each; 8 for 50p; 14 for 4. Is44, 5p each; 11 for 50p; 24 for 4. MEW LOW PRICE – 400 mW Zeners. Yalues available 47, 5: 6, 6:8, 7:5, 8:2, 9:1, 10, 11. Z1, 13:5, 15, 19, 12:5, 3: 5m. All new and marked. Price 10g each; 6 for 50p; 14 for 4. Special offer 6 off each voltage (66 zeners) 44:50. RESISTORS. Carbon film 5%, 4: Yw at 40°C, 4W at 70°C. Range from 2:20 to 2:2M 0 in E12 series. e. 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 66, 82 and their decades. High stability, low noise. All at 1p each; 80 for 10 0 any one value: 70 for 100 of any one value: 70 for 100 of any one value. Yog to 2:2M 0; 730 resistors) 45. 440¥ A.C. CAPACITORS. 0:4µF, size 1/in X in, 30p; 0:47 and 0:5µF, size 1/in X in, 30p; 0:400 PIV at 19p each or 4 for 30p; 400 PIV at 19p each or 4 for 30p; 400 PIV at 19p each or 4 for 30p; 400 PIV at 19p each or 4 for 30p; 400 PIV at 19p each or 4 for 30p; 400 PIV at 19p each or 4 for 30p; 400 PIV at 19p each or 4 for 30p; 100 (10p); E43, 10 Trans., 30p (10p). Dept: E2, The Maltings, Station Road Were, Shropshire 	brand new and marked. Full spec. devices, May be mixed to gualify for guantity prices. AF178
 Values available 47, 56, 6, 69, 75, 8-2, 9-1, 10, 11, 12, 13-5, 15V. 101, ±5% at SmA. All new and marked. Price 10p each; 56 or 500; 14 for 41. Special offer 6 off each voltage (66 zeners) 64-50. RESISTORS. Carbon film 5%, ±V at 40°C, ±W at 70°C. Range from 2-20 to 2:2M0 in El 2 series, i.e. 10, 12, 15, 18, 22, 27, 33, 39, 47, 55, 68, 82 and their decades. High stability, low noise. All at 1p each; 59 for 10 of any one value; 70p for 100 of any one value; 70p for 100; 100	40p each: 3 for £1.
 Values available 47, 56, 6, 69, 75, 8-2, 9-1, 10, 11, 12, 13-5, 15V. 101, ±5% at SmA. All new and marked. Price 10p each; 56 or 500; 14 for 41. Special offer 6 off each voltage (66 zeners) 64-50. RESISTORS. Carbon film 5%, ±V at 40°C, ±W at 70°C. Range from 2-20 to 2:2M0 in El 2 series, i.e. 10, 12, 15, 18, 22, 27, 33, 39, 47, 55, 68, 82 and their decades. High stability, low noise. All at 1p each; 59 for 10 of any one value; 70p for 100 of any one value; 70p for 100; 100	50p; 18 for £1. 1N916, 9p each; 6 for 50p; 14 for £1. 1S44, 5p each; 11 for 50p; 24 for £1. All brand new and marked
 Special offer Orage (00 Zelf) Av 30, 42 A0°C, 4W RESISTORS. Carbon film 5%, 4W at 40°C, 4W RESISTORS. Carbon film 5%, 4W at 40°C, 4W RESISTORS. Carbon film 5%, 2W at 40°C, 4W RESISTORS. Carbon film 5%, 2W at 40°C, 4W RESISTORS. Carbon film 5%, 5%, 68, 82 and their decades. High stability, low noise. All at 1p each: 8p for 10 0 any one value: 70p for 100 of any one value: Special pack—10 off each value 2.20 to 2.24M (0.730 resistors) £5. 440Y A.C. CAPACITORS. 0·1µF, size 1µ × 1µ, 3p; 0·47 and 0·5µF, size 1µ × 1µ n 3p; 0·47 and 0·5µF, size 1µ × 1µ n 3p; 0·47 and 0·5µF, size 1µ × 1µ n 3p; 0·47 and 0·5µF, size 1µ × 1µ n 5p; 1·0µF, size 2µ × 1µ × 5p; 20µ × 1µ ×	NEW LOW PRICE - 400 mW Zeners. Values available 4-7, 5-6, 6-8, 7-5, 8-2, 9-1, 10, 11,
 Special offer Orage (00 Zelf) Av 30, 42 A0°C, 4W RESISTORS. Carbon film 5%, 4W at 40°C, 4W RESISTORS. Carbon film 5%, 4W at 40°C, 4W RESISTORS. Carbon film 5%, 2W at 40°C, 4W RESISTORS. Carbon film 5%, 2W at 40°C, 4W RESISTORS. Carbon film 5%, 5%, 68, 82 and their decades. High stability, low noise. All at 1p each: 8p for 10 0 any one value: 70p for 100 of any one value: Special pack—10 off each value 2.20 to 2.24M (0.730 resistors) £5. 440Y A.C. CAPACITORS. 0·1µF, size 1µ × 1µ, 3p; 0·47 and 0·5µF, size 1µ × 1µ n 3p; 0·47 and 0·5µF, size 1µ × 1µ n 3p; 0·47 and 0·5µF, size 1µ × 1µ n 3p; 0·47 and 0·5µF, size 1µ × 1µ n 5p; 1·0µF, size 2µ × 1µ × 5p; 20µ × 1µ ×	12, 13.5, 15V. Tol. ±5% at 5mA. All new and marked. Price 10p each; 6 for 50p; 14 for £1.
 ALC. CAPACITORS. 107(LT. SIZE 1417), 2017 0-37 and 03(LF, size 1417), 2017 0(LF, size 217), 217, 217, 217, 217, 217, 217, 217, 217	Special offer 6 off each voltage (66 zeners) 44-30, RESISTORS. Carbon film 5%, ±W at 40°C, ±W
 ALC. CAPACITORS. 107(LT. SIZE 1417), 2017 0-37 and 03(LF, size 1417), 2017 0(LF, size 217), 217, 217, 217, 217, 217, 217, 217, 217	i.e. 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. High stability, low noise. All at
 ALC. CAPACITORS, 107(LT, SIZE 14) A. X. ALC. CAPACITORS, 107(LT, 10(LT, 3)), 10(LT, 3) ALGON PLASTIC RECTIFIERS 1: SA- Brand new wire-ended DO27. 100P1V at 8p each or 4 for 30p. 400P1V at 9p each or 4 for 30p. 30p; 300P1V at 14p each or 4 for 50p. Sp post and packing on all orders below 65. MARCO TRADING (Formerly V. ATTWOOD) Dept. E2, The Maltings, Station Road Wern, Shropshire COMPUTER PANELS. 9in x 71in long lead (Formerly V. ATTWOOD) Dept. E2, The Maltings, Station Road Wern, Shropshire COMPUTER PANELS. 9in x 71in long lead (Formerly V. ATTWOOD) Dept. E2, The Maltings, Station Road Wern, Shropshire COMPUTER PANELS. 9in x 71in long lead (Formerly V. ATTWOOD) Dept. E2, The Maltings, Station Road Wern, Shropshire COMPUTER PANELS. 9in x 71in long lead (Formerly V. ATTWOOD) Dept. E2, The Maltings, Station Road Wern, Shropshire COMPUTER PANELS. 9in x 71in long lead (Formerly V. ATTWOOD) Dept. E2, The Maltings, Station Road Wern, Shropshire COMPUTER PANELS. 9in x 71in long lead (Formerly V. ATTWOOD) Dept. E45, 16 (Sp). MERGEN PANELS. 9-3in, three assorted, §1:05 (25p). REW 40 WAY AS ABOVE, £1:26 (25p). REW 40 WAY AS ABOVE, £1:26 (25p). SPIGUEE RESETABLE COUNTER. 18/22V, will work on 12V, 26 (15p). SPIGUEE RESETABLE COUNTER. 18/22V, will work on 12V, 26 (25p). STILCON DIODES 650V 11A. 10 on Tagboard, 30p (5p). C, 7400 SERIES ON PANEL(S). 10 for 75p (10p). DOLYSTYRENE CAPACITORS. 123V, 100pF to 1012, 200 dosen: 0:015 to 0:068, 30p dozen (ff ordered alone 10p). MIXED POLYSTYRENE/S. MICA CAPS. 100 for 15p. ABSORTED COMPONENTS, 41:50. ASSORTED COMPONENTS, 41:50. ASSORTED COMPONENTS, 51:50. ASLE BIN X in FOR LISTS. J.W.B. RA	Ip each; 8p for 10 of any one value; 70p for 100 of any one value. Special pack—10 off each value 2:20 to 2:2M0 (730 resistors) 45
ARCO TRADING (Formerly V. ATTWOOD) Dept. E2, The Maltings, Station Road Wem, Shropshire COMPUTER PANELS. 9in x 7iin long lead Trans. and Comps., E6, 8 Trans., 209 (109). E43, 10 Trans., 409 (109): E47, 10 Trans., 309 (109). AMERICAN PARELS. 4 for 609 (129) with data. M.C. METERS. 2-3in, three assorted, £1-05 (259). WIRE ENDED NEONS. 10 for 459 (89); 20 for 759 (80). Bank of five with 6 (307 Diver Trans., 459; Bank of 30 with 5 C407 Driver Trans., 459; Distribution Distribution Bank, 15 r.p.m., a.c.w., 759 (139). Strotter BERSTABLE COUNTER. 18/22V, will work on 12V, 42 (139). Strotter CLAD PAX. PANELS. 3(100 ro 1507 509; (109). POLYSTYRENE CAPACITORS. 123V, 1000pF to 1012; 209 dozen; 0-013 to 0-068, 309 dozen (if ordered along. MIXED POLYSTYRENE/S. MICA CAPS. 100 for 150. DASSORTED COMPORENTS, 41-50. BASSORTED COMPOTER PANELS, 41-50. BASSORTED COMPOTER PANELS, 51-50. BASSORTED COMPOTERS, 134 NORTH END COM 1st APRIL ADD 10% FOR V.A.T. TOM 1st APRIL ADD 10% FOR V.A.T. DOMENS COMPONENTS, 134 NORTH END ROAD, LONDON, W14. (Mail order only) ST AUTO TRACTION. Thousands of spains in surplus radio equipment, Meters, tors, relays, TR/TX, telephone equipment, Mete	440V A.C. CAPACITORS. 0.1µF, size 1↓in × 4in, 25p: 0.25µF, size 1↓in × ↓in, 30p: 0.47 and
ARCO TRADING (Formerly V. ATTWOOD) Dept. E2, The Maltings, Station Road Wem, Shropshire COMPUTER PANELS. 9in x 7iin long lead Trans. and Comps., E6, 8 Trans., 209 (109). E43, 10 Trans., 409 (109): E47, 10 Trans., 309 (109). AMERICAN PARELS. 4 for 609 (129) with data. M.C. METERS. 2-3in, three assorted, £1-05 (259). WIRE ENDED NEONS. 10 for 459 (89); 20 for 759 (80). Bank of five with 6 (307 Diver Trans., 459; Bank of 30 with 5 C407 Driver Trans., 459; Distribution Distribution Bank, 15 r.p.m., a.c.w., 759 (139). Strotter BERSTABLE COUNTER. 18/22V, will work on 12V, 42 (139). Strotter CLAD PAX. PANELS. 3(100 ro 1507 509; (109). POLYSTYRENE CAPACITORS. 123V, 1000pF to 1012; 209 dozen; 0-013 to 0-068, 309 dozen (if ordered along. MIXED POLYSTYRENE/S. MICA CAPS. 100 for 150. DASSORTED COMPORENTS, 41-50. BASSORTED COMPOTER PANELS, 41-50. BASSORTED COMPOTER PANELS, 51-50. BASSORTED COMPOTERS, 134 NORTH END COM 1st APRIL ADD 10% FOR V.A.T. TOM 1st APRIL ADD 10% FOR V.A.T. DOMENS COMPONENTS, 134 NORTH END ROAD, LONDON, W14. (Mail order only) ST AUTO TRACTION. Thousands of spains in surplus radio equipment, Meters, tors, relays, TR/TX, telephone equipment, Mete	0·5μF, size Ižinמin, 35p; 1·0μF, size 2inמin, 45p; 2·0μF, size 2in× lin 75p.
ARCO TRADING (Formerly V. ATTWOOD) Dept. E2, The Maltings, Station Road Wem, Shropshire COMPUTER PANELS. 9in x 7iin long lead Trans. and Comps., E6, 8 Trans., 209 (109). E43, 10 Trans., 409 (109): E47, 10 Trans., 309 (109). AMERICAN PARELS. 4 for 609 (129) with data. M.C. METERS. 2-3in, three assorted, £1-05 (259). WIRE ENDED NEONS. 10 for 459 (89); 20 for 759 (80). Bank of five with 6 (307 Diver Trans., 459; Bank of 30 with 5 C407 Driver Trans., 459; Distribution Distribution Bank, 15 r.p.m., a.c.w., 759 (139). Strotter BERSTABLE COUNTER. 18/22V, will work on 12V, 42 (139). Strotter CLAD PAX. PANELS. 3(100 ro 1507 509; (109). POLYSTYRENE CAPACITORS. 123V, 1000pF to 1012; 209 dozen; 0-013 to 0-068, 309 dozen (if ordered along. MIXED POLYSTYRENE/S. MICA CAPS. 100 for 150. DASSORTED COMPORENTS, 41-50. BASSORTED COMPOTER PANELS, 41-50. BASSORTED COMPOTER PANELS, 51-50. BASSORTED COMPOTERS, 134 NORTH END COM 1st APRIL ADD 10% FOR V.A.T. TOM 1st APRIL ADD 10% FOR V.A.T. DOMENS COMPONENTS, 134 NORTH END ROAD, LONDON, W14. (Mail order only) ST AUTO TRACTION. Thousands of spains in surplus radio equipment, Meters, tors, relays, TR/TX, telephone equipment, Mete	SILICON PLASTIC RECTIFIERS 1-5A— Brand new wire-ended DO27, 100PIV at 8p each or 4 for 30p: 400PIV at 9p each or 4 for
MARCO TRADING (Formerly V. ATTWOOD) Dept. E2, The Maltings, Station Road Wem, Shropshire COMPUTER PANELS. 9in x 74 in long lead Trans. and Comps., E6, 8 Trans., 269 (10p); E45, 16 Trans., 409 (10p); E47, 10 Trans., 309 (10p). AMERICAN PANELS. 4 for 609 (12p) with data. M.C. METERS. 2-3in, three assorted, 21-05 (25p). WIRE ENDED NEONS. 10 for 459 (25p). Bank of 30 with 5 C407 Driver Trans., 459, Bank of 30 with 5 C407 Driver Trans., 429, Dank of five with 5 C407 Driver Trans., 459, Bank of 30 with 5 C407 Driver Trans., 429, Denation, 809 (13p). REW 46 WAY AS ABOVE, 21-25 (25p). CROUZET GEARED MOTOR. Mains, 15 r.p.n., a.cl.w., 759 (15p). S FIGURE RESETTABLE COUNTER. 18/22V, will work on 12V, 22 (15p). SILCON DIDES 650V 14. 10 on Tagboard, 309 (5p). COPPER CLAD PAX. PANELS. 34in x 54in' for 309 (10p). MIXED POLYSTYRENE (APACITORS, 125V, 100p)F to DOLYSTHENE CAPACITORS, 125V, 100p F to DOLYSTYRENE CAPACITORS, 125V, 100p F to DOLYSTYRENE CONFORENTS, 21-50. BASORTED CONFORENTS, 11-50. BASORTED CONFORENTS, 11-50. BASORTED CONFORENTS, 11-50. BASORTED CONFORENTS, 11-50. BASORTED CONFORENTS, 11-50. BASORTED CONFORENTS, 11-50. BASORTED CONFORENTS, 134 NORTH END ROAD, LONDON, W14. (Mail order only WITH AUTO TRACTION. Thousands of STA AUTO TRACTION. Thousands of STA AUTO TRACTION. Thousands of STA AUTO	34p; 800PIV at 14p each or 4 for 50p. Sp post and packing on all orders below £5.
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M.C. METERS. 9-3in, three assorted, \$1.05 (25p). WIRE ENDED NEONS. 10 for 45p (8p); 20 for Top (8p), Bank of five with 6 (407 Diriver Trans., 45p, Bank of 30 with 5 (407 Diriver Trans., 25 (15p). 28 WAT STEPPING SWITCH with Reset, Mains Operation, 80p (15p). NEW 44 WAT AS ABOYE, £1-26 (35p). CROUZET GEARED MOTOR. Mains, 15 r.p.nl., A.d.w., 75p (13p). STIGUER ERESTTABLE COUNTER. 18/22V, will work on 12V, 42 (15p). SILICON DIODES 650V 14A. 10 on Tagboard, 30p (5p). LC, 7400 SERIES ON PANEL(8). 10 for 75p (10p). DOPPER CLAD PAX. PANELS. 3jin × 3jin 5 for 30p (10p). MIXED POLYSTYRENE/S. MICA CAPS. 100 for 15 or 30p (10p). MIXED POLYSTYRENE/S. MICA CAPS. 100 for 15 ASSORTED COMPOTER PANELS, 51-50. 34.A.E. 9in × 4in FOR LISTS. J.W.B. RADIO 5 HAYFIELD ROAD, SALFORD 6, LANCS Postage in brackets Mail order only FROM 1st APRIL ADD 10% FOR V.A.T. 100 WAATT AMPLIFIER Value Counter 100. Trinted circuit board and full instructions. 1-45p + 10p P. & P. S.a.e. for list of omponent bargains. EDMUNDS COMPONENTS, 314 NORTH END ROAD, LONDON, W14. (Mail order only) SIT AUTO TRACTION. Thousands of tors, relays, TR/TX, telephone equipment, Traft equipment. S.A.E. enquifies. 27a ragon Road, Twickenham, Middx.	Trans. and Comps., E6, S Trans., 25p (10p); E45, 16 Trans., 40p (10p); E47, 10 Trans., 30p (10p).
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3 for 309 (109). POLYSTYRENE CAPACITORS. 123V, 100pF to 7012, 20p dozen; 0.013 to 0.068, 30p dozen (if ordered alone 109). MIXED POLYSTYRENE/S. MICA CAPS. 100 for 159. The ASSORTED COMPONENTS, £1-50. BASEORTED COMPONENTS, £1-50. BASEORTED COMPONENTS, £1-50. BASEORTED COMPOUTER PANELS, \$1-50. SA.E. Bin × 4in FOR LISTS. J.W.B. RADIO 75 HAYFIELD ROAD, SALFORD 6, LANCS Postage in brackets Mail order only FROM 1st APRIL ADD 10% FOR V.A.T. 100 WATT AMPLIFIER 145 protected, transformerless, 9 transisor circuit. Input 500 mV. Output into 1 ohms. 0.1% distortion. 17145 pt 100 P. R. P. S.a.e. for list of omponent bargains. EDMUNDS COMPONENTS, 134 NORTH END ROAD, LONDON, W14. (Mail order only) BIT AUTO TRACTION. Thousands of gains in surplus radio equipment. Meters, tors, relays, TR/TX, telephone equipment, radfor equipment. Middx.	(5p). I.C. 7400 SERIES ON PANEL(S). 10 for 75p (10p).
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The ASSORTED COMPONENTS, £1-50. The ASSORTED COMPUTER PANELS, £1-50. SA.E. Bin × 4in FOR LISTS. J.W.B. RADIO TS HAYFIELD ROAD, SALFORD 6, LANCS To the APPIL ADD 10% FOR V.A.T. TOM 1st APRIL ADD 10% FOR V.A.T. 100 WATT AMPLIFIER fully protected, transformerless, 9 transis- or circuit. Input 500 mV. Output into 10 ohms. 0-1% distortion. Trinted circuit board and full instructions. 1:45p + 10p P. & P. S.a.e. for list of omponent bargains. EDMUNDS COMPONENTS, 134 NORTH END ROAD, LONDON, W14. (Mail order only) BIT AUTO TRACTION. Thousands of tors, relays, TR/TX, telephone equipment, traff equipment. S.A.E. enquiries. 27a tagon Road, Twickenham, Middx.	MIXED POLYSTYRENE/S. MICA CAPS. 100 for
A.E. Bin × 4in FOR LISTS. J.W.B. RADIO 75 HAYFIELD ROAD, SALFORD 6, LANCS Postage in brackets Mail order only FROM 1st APRIL ADD 10% FOR V.A.T. 1000 WATT AMPLIFIER INPUT 500 mV. Output into or circuit. Input 500 mV. Output into ohms. 0.1% distortion. Frinted circuit board and full instructions. 1:45p + 10p P. & P. S.a.e. for list of omponent bargains. EDMUNDS COMPONENTS, 134 NORTH END ROAD, LONDON, W14. (Mail order only) BIT AUTO TRACTION. Thousands of trans, relays, TR/TX, telephone equipment, traff equipment. S.A.E. enquifries. 27a ragon Road, Twickenham, Middx.	71b ASSORTED COMPONENTS, £1.50.
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BIT AUTO TRACTION. Thousands of gains in surplus radio equipment. Meters, tors, relays, TR/TX, telephone equipment, raft equipment. S.A.E. enquiries. 27a ragon Road, Twickenham, Middx.	EDMUND8 COMPONENT8, 134 NORTH END
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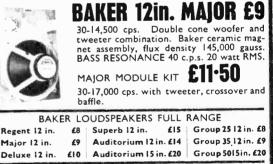
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